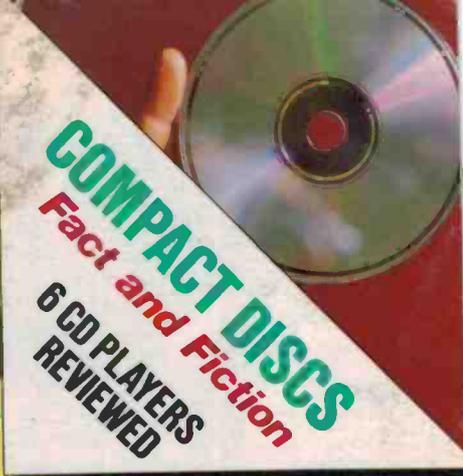




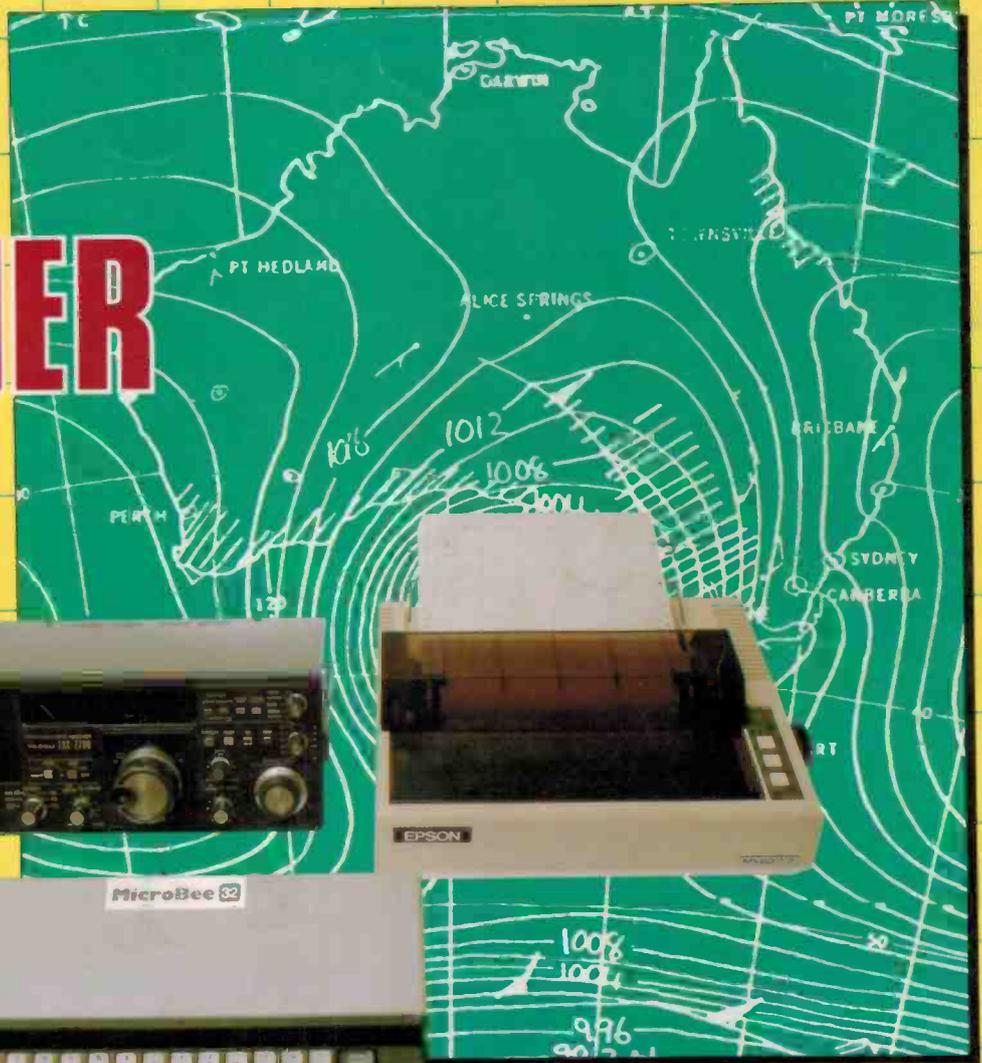
**ELECTRONICS
TODAY
INTERNATIONAL**



How to

PRINT WEATHER MAPS

on your computer using our radio facsimile decoder project.



TO BUILD:

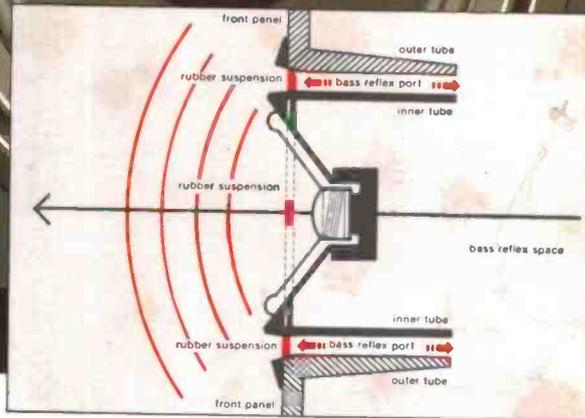
3-WAY SPEAKERS

HANDHELD DIGITAL FREQUENCY METER

VIDEO DISTRIBUTION AMPLIFIER

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**32-PAGE FET COOKBOOK
BONUS**



Are your speakers prepared for Digital Audio? Jamo are.

The new range of JAMO loudspeakers from Denmark's leading loudspeaker manufacturer has been designed with the digital audio in mind.

Digital Audio is here. It will expose the limitations in all hi-fi systems, especially the loudspeakers. So why buy speakers, which are outdated tomorrow. Be part of the future of JAMO.

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With JAMO you will get excellent sensitivity, unsurpassed stereo image and phase linearity. You'll also get fully electronic overload protection and acoustic attenuators. But you won't get empty pockets . . . We quote:

"Our conclusion is that JAMO CBR-1303 is a handsome, very well constructed and finished speaker whose sound quality, high sensitivity, and ruggedness merit its serious consideration by anyone contemplating buying speakers in its price class." (Stereo Review, USA, April 1983)

"We do not know any loudspeaker in this price range, which at once offer an excellent performance, high sensitivity and the possibility to get the instruments up in a natural size." (High Fidelity, Scandinavia)

JAMO has developed and patented the unique CBR-system (Centre-Bass-Reflex). It eliminates distortion caused by cabinet resonances found in most traditional speakers. The woofer is mounted in the cabinet by means of only four rubber suspension points, which effectively absorb all vibrations from the woofer.

These JAMO developments represent excellent uncoloured sound reproduction, which has acclaimed JAMO by hi-fi critics all over the world.



For further information and nearest dealer contact: SCAN AUDIO, P.O. Box 242, Hawthorn, Vic. 3127. Phone (03) 819 5352.

JAMO HI-FI 

Use Reader Information Card for full details.



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NEWS DIGEST	6
COMPACT-DISC PLAYERS — FACT AND FICTION	16
FET COOKBOOK	99

SIGHT & SOUND

SIGHT & SOUND NEWS	12
THE PIONEER SYSTEMS REVIEW	19
A DISCERNING DISCOURSE ON DIGITAL DISC PLAYERS	30

COMPUTING TODAY

ADAM — APPLE OF COLECO'S EYE	45
COMPUTING TODAY NEWS	46
USING SOUNDEX CODES FOR WORD-MATCHING	58
ZX COLUMN	63
MICROBEE COLUMN	69
'660 SOFTWARE	72
VIC-20 COLUMN	74

TECHNICAL

EQUIPMENT NEWS	79
COMPONENT NEWS	83
PROJECT 421 THREE-WAY COMPACT LOUDSPEAKERS	85
PROJECT 736 RADIO FACSIMILE PICTURE-COMPUTER DECODER	92
FET COOKBOOK	99
PROJECT 175 HANDHELD 20 MHZ DIGITAL FREQUENCY METER	133
PROJECT 166 FUNCTION/PULSE GENERATOR	140
PROJECT 1517 VIDEO DISTRIBUTION AMPLIFIER	147
SHOPAROUND	151
IDEAS FOR EXPERIMENTERS	153
IDEA OF THE MONTH	155

COMMUNICATIONS

COMMUNICATIONS NEWS	157
SCANNERS' WORLD	159

GENERAL

COMMENT	5
MAIL-ORDER BOOKS	65
MINI-MART	160
DREGS	162

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48-50 A'Beckett Street, Melbourne. Ph (03) 347 9251

THIS MONTHS KITS



ETI-736 Fax Picture Decoder

Print weather maps with your MicroBee. This project goes between the Audio Output of a shortwave receiver and the 8-bit port of the MicroBee and allows you to print weather maps and satellite pictures on a dot-matrix printer with quite acceptable results. Do your own forecasts.



ETI-1517 Video Distribution Amplifier

This will let you drive up to five video displays from one video source, simple to build... low in cost. Tons of applications—great for direct video out from computer to you, drive several displays from a video recorder, etc. etc.



ETI-175 Digital Frequency Meter

A handheld digital frequency/period counter that goes to 20MHz and features a 4 1/2 (and a half) digit display. Low cost—simple to build, battery operated.



ETI-166 Function/pulse Generator

At last—the ETI function/pulse generator. Here's how to have a top-class instrument in your lab/workshop. Covers 1 Hz to 1 MHz, generates sine, square, triangle, ramp and pulse signals with top specs.



\$48.50

Dual Tracking Power Supply



\$87.50

EA ELECTRONIC STARTER FOR FLUORESCENT LAMPS



\$5

OCTOBER EA 1982

EA DIGITAL READOUT FOR SW RECIEVERS



\$72.00 COMPLETE

OCTOBER EA 1982

100w Sub-Woofer Amplifier



\$85.00

JULY EA 1982

EA GUITAR BOOSTER



\$17.50

JUNE EA 1982

STEREO SYNTHESISER FOR TUNERS AND VCRs

Enjoy the benefits of stereo sound from your video cassette recorder, TV or AM tuner with this Stereo Synthesiser. The circuit uses just four ICs and is easy to build.



\$55.00

SEPTEMBER EA 1982

Eprom Programmer



\$55.00

JANUARY EA 1982 INCLUDES TEXTTOOL SOCKET

EA POWER UP



\$38.50

EA NOV 1982

OVER 200 NOW SOLD EA INVERTER INCLUDING TRANSFORMER 300 WATTS

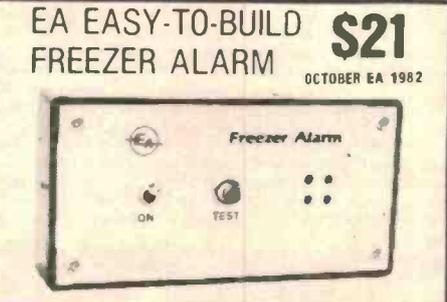


\$195

JUNE EA 1982

P & P \$10.00 Anywhere in Australia

EA EASY-TO-BUILD FREEZER ALARM



\$21

OCTOBER EA 1982

Led Head Lightchaser



(Battery and headband extra)

\$12

PH METER



\$129

with probes

BOGGLE GOGGLES



\$9.60

Short form

Tacho/dwell meter with digital display



\$79

MAY EA 1982

Driveway Sentry



\$32

12/240 volt Inverter 40 WATTS



\$49.50

MAY EA 1982

Portable 3 1/2 Digit Heart Rate Monitor



\$79.00

JULY EA 1982

Analogue and Digital Storage CRO Kit



\$189.00

ADVERTISERS' INDEX

Australian Government	32,33
Applied Technology	42,43
A.E.D.	54
Altronics	56,57,88,89 136,137,152,156
Alphatron	73
Billco	130
Back Issues	78
Comx	50
Dick Smith	28,29 62,90,91
Daneva	61
Elmeasco	11
Emona	44
Electromed	53
Energy Control	59
Electronic Agencies ..	70
Ferguson	73
G.F.S.	159
Hitachi	123
Imark	84
Jaycar	8,76,77,80 81,131,138,139
K-Nar	53
Magraths	27
National	14,15
Neotronics	82
Pioneer "Zip Out" 19-26	
Pre Pak	48
Rose Music	O.B.C.
Rod Irving	4,60,71,75 146,150,154,158,161
Radio Despatch	51
Rock Soft	59
Scan Audio	I.F.C.
Sony	I.B.C.,9
S.M.E.	44
Software Source ..	47,49
Scientific Devices	78
Sheridan	112, 132
Truscotts	84
Videoactive	52

COMMENT

I HAVE JUST returned from the Electronics Show in Perth — Australia's *only* consumer electronics show. And what a show! Virtually every major distributor of consumer electronics equipment was represented among the 90 exhibitors, and the organising committee estimated over 100 000 people poured through the gates over the four days of the show, from August 4-7. The consumer electronics industry is alive and well — and living in Western Australia!

What is wrong with the industry that it can't organise a show in the eastern states? One would think that's where the bulk of the marketplace existed. The last consumer electronics show in the east was held in Sydney in 1980. Since then, the industry has not been able to get another one off the ground. There was a false start for a show in 1981, and again for 1982, but the support and effort just fizzled away.

The Perth show is organised by a committee made up of managers from firms representing different sectors of the industry. Is there any barrier to the industry in the eastern states getting together and doing the same thing here? They're getting together in the west, so why not over here? I think a few very valuable lessons can be learned from the success of the Perth Electronics Show. The organisation that got it together should provide an excellent model to follow. The Perth show is now five years old and has grown enormously in the past three years. I'm not suggesting the Perth show should be transferred to the east, rather the east should emulate the west.

As there are now national industry bodies representing the various sectors of the trade, how about getting together and putting on a show? You've got all to gain and little to lose — except your inhibitions about getting together.

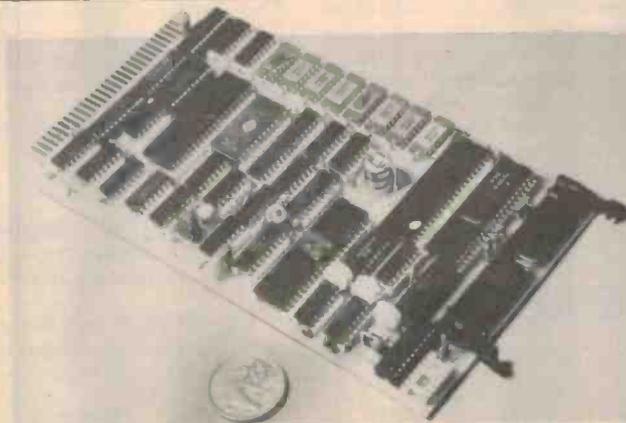


"Ill fares it with the flock, if shepherds wrangle when the wolf is nigh."

—Sir Walter Scott

Roger Harrison
Editor

NEXT MONTH



THE 'LITTLE BIG BOARD' COMPUTER

Here is a Z80-based single-board computer featuring 64K of RAM on board, two RS232 ports and a floppy disk controller that will handle up to four disk drives, either 5¼" or 8" double-sided double-density. It runs CP/M 2.2 and all fits on a board

measuring just 115 x 204 mm! But that's not all. The CPU runs at 4 MHz, a real-time battery-backed clock is included and the RS232 ports are software configurable to suit yourself. It uses the increasingly popular and very versatile 56-pin STD buss. Our last computer was the popular Learner's Micro. This one's for the 'big boys'. Don't miss it.

GETTING PRINTOUT FROM YOUR MICROBEE

There are two ways to get it — the cheap way and the not cheap way. Either way, you'll need an interface. We show you how to build and get working two simple interfaces — one for each method. Both cheap.

WIN A SCANNER!

You could win yourself one of the most popular scanners of the Australian market, worth over \$500, in our big Scanners' World Contest next month. You've got to be in it to win it, they say.

THE INS AND OUTS OF VIDEO ENHANCERS
LED AUDIO PEAK PROGRAMME METER
SANSUI 'COMPU RECEIVER' REVIEWED

SERVICES

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ELECTRONICS CONVENTION IN SYDNEY THIS MONTH

REECON '83, the 19th International Convention and Exhibition, mounted by the Institution of Radio and Electronics Engineers Australia, will be held at the Sydney Showground from September 5-9.

IREE conventions are the recognised regular forums for engineers, technicians, scientists and management executives engaged in every field of electronics. The technical exhibition will be complemented by a comprehensive lecture program presented by leading authorities in all areas of electronics from Australia and overseas.

The Governor-General, Sir Ninian Stephen, will officially open the convention on Tuesday, September 6. The keynote address on the convention theme, World Communications Year, will be presented by the secretary-general of the International Telecommunications Union (ITU), Dick Butler.

The 260 technical papers to be presented at the convention will cover a wide cross-section of topics in the electronics field. The papers will be in lecture and

poster presentations, with more than 30 overseas authors personally presenting their papers.

Two papers on studies aimed to facilitate automated sheep-shearing will be given by representatives of the research teams at the University of New South Wales and the University of Adelaide. They will discuss the feasibility of different sensing devices which will warn the fast-moving shear of obstacles in its path.

Recent research in Australia suggests that video computer games might play a role in the treatment of children with specific learning difficulties. Shirley Goodhew, an occupational therapist, reports in her paper that video computer games practice results in an upward trend in all of the four parameters of motor behaviour.

An educational experiment

conducted in South Australia is the subject of another paper. The results of this experiment show that isolation in the Australian Outback need no longer be a barrier to specialist training in the latest technological developments.

The latest results of Project Jindalee, HF skywave radar which is currently collecting wind- and sea-state information from the Indian Ocean, will be presented at the conference.

Another paper which will be presented will discuss the development of the microwave radiometer by CSIRO scientists. This method of measuring temperatures below skin level without breaking the skin will be used in the heat treatment of cancer.

Contact the IREE for further information.

COVER

Be your own forecaster — print weather maps with your Microbee! Cover design by Ali White. Background weather map is a facsimile print courtesy of the Bureau of Meteorology.

Last month's cover credit was omitted, unfortunately. The background picture was of the Cone Nebula, a strong infrared source, courtesy of D.F. Malin of the Anglo-Australian Observatory, NSW. Ali White designed the layout.

NEW WAY WITH PC ASSEMBLIES

A new method of surface-mounting electronic components, combining flexible printed-circuit board and chip-carrier technology, has been devised by Welwyn Electric, the British resistor and microelectronics manufacturer.

The technique makes use of Welwyn's range of flexible printed circuits to interconnect an array of chip carriers and other face-bonded devices. To this, the company has added a special heat-sink to create an easily assembled package that offers a high degree of mechanical strength and is suitable for a wide range of professional, defence and telecommunications applications.

The heat-sink is made of aluminium or copper with studs or pillars which protrude through the holes in the printed circuit and contact the underside of each chip carrier, providing efficient thermal conduction for the entire circuit board.

on cell selection, temperature correction, discharge data, charging, recharging and maintenance.

The Exide Faure-X range offers more than 20 different cell capacities from 50 to 3200 Ah at the 10-hour rate.

For more information, contact **Chloride Batteries Australia, 147 Woodpark Road, Smithfield NSW 2164. (02)604-0522.**

THE LARGE AND SMALL OF EXIDE BATTERIES



The biggest and the smallest of Exide's maintenance-free RE systems batteries for industrial use have been released by Chloride Batteries.

The RE6-1, with a size of 51 x 42.5 x 57.5 mm, is an ideal 6 V, 1 Ah power source where space is a premium.

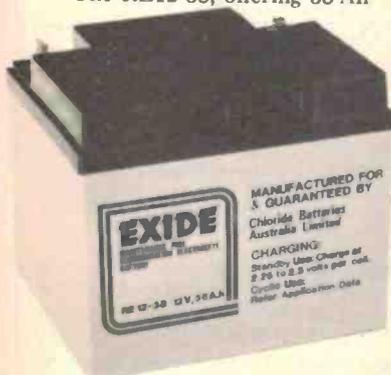
The RE12-38, offering 38 Ah

in 12 V circuits, meets the heavier power needs of emergency lighting, uninterruptible power supplies, communications, instrumentation and propulsion as in electric wheelchairs. It measures 177 x 165 x 170 mm.

The Exide RE range now has seven batteries of various shapes and sizes of 6 V offering 1-10 Ah, and six of 12 V, also of various shapes and sizes, offering 1.2-38 Ah.

There is a new 24-page catalogue from Chloride giving the specifications, performance data and application advice on Exide Faure-X pure lead positive grid batteries used for standby power in solar, computer or emergency situations.

In this glossy catalogue, graphs and tables illustrate text



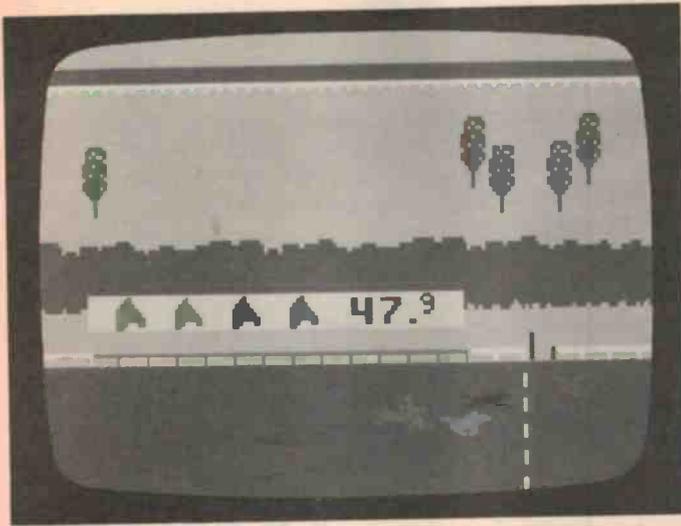
NOTES & ERRATA

Equipment News, April Issue, page 10. The price of the BWD Model 821 oscilloscope, featured on this page, was mistakenly quoted at \$750 retail when it should have been given as \$750 plus sales tax.

Project 1513, June issue, page 76. The Parts List shows R16 as 18K, but the circuit diagram gives it as 560R. The circuit diagram is correct.

Project 698, June issue, page 47. At date of going to press with this project, Chuck Simmers had only tried the National bipolar PROMs so check the specifications before attempting to program other makes using this project.

'660 Software, August '83, page 68. In the item at the bottom of the page headed "Cure For Colour Problems", we goofed. The solution is to cut the track between pin 11 of the 4066 (IC21) and the junction of R16-R17, then insert a 10nF capacitor across the cut. Sorry about that.



TELEGAMBLING: A SUREFIRE BET

A televised network featuring gambling at home may provide the impetus for the widespread use of interactive teleshopping services, such as Videotex and Teletext, according to a 314-page report released by International Resource Development, an independent United States consulting firm.

"Gambling services may be the answer to get consumers to use Teletext and Videotex," according to IRD.

"The average punter receives his betting information from

the newspaper, and then either places a bet at the track, at an off-track betting shop or with an illegal bookmaker. The use of Teletext and Videotex could result in one-stop gambling."

Videotex is basically a consumer-oriented time-sharing network which allows two-way communications with a central computer through an interactive home terminal. Teletext involves one-way transmission of text and graphics through the vertical blanking interval (VBI) of a

regular television transmission, or through a full cable channel.

According to IRD, telegambling would be a boon to advertisers on Videotex and Teletext systems, and would serve to weaken organised crime and the underground economy. The situation is also a 'natural' for the major television networks that are set to launch Teletext systems.

"These networks carry a great deal of sports programming. The provision of telegambling would surely serve to boost ratings and advertising revenues for the networks," says IRD's report.

IRD sees potential for a cable network devoted exclusively to television programmes designed around gambling.

"This telegambling network could feature dramatic shows on which the viewer could place bets as to the actions of particular characters, similar to the informal betting that occurred with the *Who Shot JR?* episode of *Dallas*," explained IRD researcher Dave Ledecy.

"People will bet on just about anything. They'll bet on the sunrise, as long as it's easy and convenient to do so."

Further information on the US\$1285 report, which is entitled *Teleshopping*, including a free description and table of contents, are available from International Resource Development, 30 High Street, Norwalk, CT 06851, United States. Telex 643452.

BOSCH'S ELECTRONIC DRIVER

Bosch has become the first European manufacturer to market a fully electronic instrument cluster for passenger cars.

The Bosch cluster, installed in the latest production versions of the Audi Quattro, has green vacuum-fluorescence displays which are used for presenting the information.

In addition to the functions of the conventional instrument panels, such as speedometer, tachometer, fuel gauge and indicator lamps, there is an integrated trip computer. This provides instantaneous consumption, average consumption, average speed, range on tank, driving time and time of day.

The driver can also select a 'minimum-display mode' in which only the road speed, mileage indicator and trip meter are shown. In critical cases, such as high coolant temperature, less than 10 litres in the fuel tank or a continuous driving time of more than two hours, the relevant individual display automatically flashes.

For more information, contact Robert Bosch Australia, P.O. Box 66, Clayton Vic. 3168.

STOP SHAKING, WE'RE ON VIDEO

Fresh air has been used to guarantee a vibration-free picture from one of Australia's most sophisticated video installations, at the new Sydney Entertainment Centre.

The centre's \$500,000 Swiss Eidophor projector has been mounted on a platform suspended upon inflatable rubber springs.

The method employs a principle which can also be used by transport companies, computer firms and industry to isolate sensitive loads and equipment from shock.

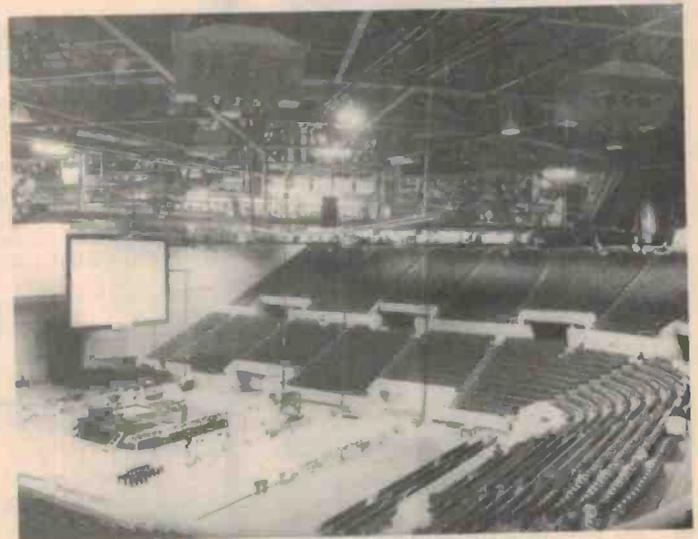
The projector is mounted on a catwalk high within the centre to throw images up to 11 metres

by 7.3 metres on to a screen below.

The potential problem was that any vibration — higher frequency from footfalls, or lower frequency from flexing of the box-girder roof — would have been magnified on-screen.

The solution, devised by the projector's importer, Hawker Pacific, in conjunction with Air Springs Supply, was to mount the camera on the platform incorporating air springs inflated by a compressor.

A total of six Model 116 single convoluted air springs of 228 mm diameter were used to suspend the 500 kg camera, which is used to provide spec-



tacular backdrops, close-up and replays of performances.

For further information, con-

tact Air Springs Supply, 137 Bowden Street, Meadowbank NSW 2144. (02)807-4077.

JAYCAR No. 1 for Components

A minor revolution is going on around the world in the semiconductor industry at present. Many Digital IC's (i.e. 4000 series CMOS and 74LS TTL) have almost doubled in price in the past 3 months! This is bad enough but the lead time (i.e. delivery from the manufacturers) has gone from 2-3 days to 4-6 months! Linears are seriously affected also. This is very bad news for all of us — especially for our kit production. To offset this serious problem, Jaycar has allocated a massive increase in funds to finance larger stockholdings. We have had to do this to try to overcome the very long delays that are currently occurring. Unfortunately on many occasions we have had to pay much more than we normally pay for semis. We are holding our prices where we can but, inevitably, there are price rises. We have committed ourselves to pare our operating margins to the bone so that price increases cause as little hardship as possible.

But even in the middle of all of this, we are STILL able to bring bargains in semiconductors to you!!
Check the specials below and SAVE!

JAYCAR — No. 1 FOR SEMICONDUCTORS

6116 RAM

WERE
\$12.50



Cat. ZZ8430

NOW **\$8.95**
10 + \$7.95 ea

6116 RAM — check us first!
The price on this one appears to have "bottomed out". Lately we have seen price increases in fact. To keep our prices to you as low as possible we have bared our margins to the bone! Right now you can buy the 6116-P3 from us for only \$8.95! 10 up \$7.95 each
Remember Jaycar prices include sales tax and IC's are packed in quality Velostat foam — a must for safety!
Cat. ZZ-8430 \$8.95 each — 10 up \$7.95 each

MJ802/MJ4502 POWER TRANSISTORS



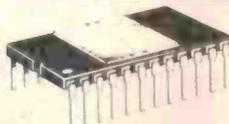
VERY RARE BEASTIES!!

Legendary Motorola Power Transistors
The MJ802/MJ4502 are an NPN/PNP complementary bipolar transistor pair designed for high power audio amplifier applications. They feature matched gain, 30 amp collector current and a Vce of 100V. They have a case dissipation of 200 watts. Jaycar is one of the few stockists of these devices.
MJ802 Cat. ZT-2232 \$7.95 10 up \$7.25
MJ4502 Cat. ZT-2234 \$7.95 10 up \$7.25

2764

EPROM

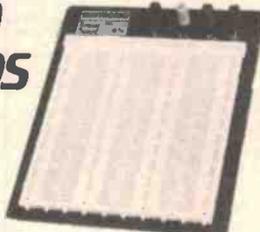
SAVE OVER
50%



This is a quality Japanese made 64K EPROM. This is the single +5V power (for read operation). We sold this unit recently for \$35. Now they are realistically priced at only \$14.95 & \$12.95 10 up.
Cat. ZZ-8464

EXPERIMENTER BREAD BOARDS

FROM
ONLY
\$3.45
EACH



Cat. PB8810 WBDN 100 holes **\$3.45**
Cat. PB8812 WBTN 640 holes **\$10.95**
Cat. PB8814 WB2N 840 holes **\$16.95**
Cat. PB8816 WB4N 1680 holes **\$29.50**
Cat. PB8818 WB6N 2420 holes **\$45.00**

SAB0600 DOOR CHIME IC



SAVE
\$2.50

This is the fabulous "DOOR CHIME" IC which plays melodic chords. Normally this unit sells for \$12.50 for September only — \$9.95! A saving of over \$2.50
For each SAB0600 sold, we will provide a free circuit diagram of a complete Door Chime!
Cat. ZK-8860 \$9.95

TK-104 KNOB

SAVE OVER
50%

This deluxe knob is fitted with a brass bush with grub screw to take a 1/4" diameter shaft. The knob measuring 27mm high features a wide skirt (36mm dia.) with a metal panel indicating 0 at centre and 5 units on either side of centre. It is ideal for control or test equipment. We have a surplus quantity of these knobs. Normally they sell for \$0.85 cents.
Cat. HK-7549

Sept. only \$2 for 5
unbelievable
price
\$0.40
EA



10 AMP/400V BRIDGE RECTIFIER

SUPER RED HOT PRICE
ONLY \$2.45 each — \$1.95 each 10 up
Die cast base, 1/4" "Quick Connect Terminals"
Cat. ZR-1315

FROM \$1.95

FROM
\$1.95



TAA611B

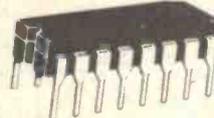
TAA611B * Low distortion * Over 2 watts RMS output! * High input impedance * 6-15 volt rail * Low quiescent current
Buy a TAA611 B for September only and receive a free spec. sheet with two recommended amplifier circuits!
LOW COST AMPLIFICATION!

Cat. ZL-3750

ONLY 50 cents!

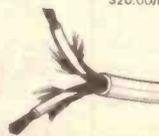
UAA180 LED LIGHT BAND DRIVER

This device will drive up to 12 LEDs in linear fashion from an analogue voltage input. (As used in the EA/Playmaster AM Tuner). Ideal for any low cost LED driver application. Normally \$3.50 each, September only \$1.95 each. Save a fortune!!



TWIN SCREENED AUDIO CABLE

Twin screened round audio cable. (Two screened conductors NOT fig '8')
This cable normally sells for \$0.48/metre or \$42.00/roll. For September only \$20.00/roll!!
Cat. WB-1504 \$20.00/roll



SAVE
OVER
50%.

BD677 DARLINGTON TRANSISTOR

BD677 Popular Philips Darlington Transistor
The BD677 is an NPN, TO-18, 60 volt 4 amp Darlington transistor. Its gain (hFE at 1.5A) is — would you believe 750!
We have a bulk-buy of this snappy little transistor so you save!
ONLY 75 cents each 10 up 65 cents each

FROM

65¢



24 VOLT CRADLE RELAY

What can we say? 24V DC coil, 4PDT gold flashed contacts. Quality brand. Complete with cradle relay socket worth \$0.50 alone.
Relay normally \$4.95. This month \$2.95
Limit 2 per customer.
Cat. SX-4010

SAVE \$2.00!!

BT151-650R

This is the 650 volt version (for extra safety) of the C122E SCR which we use in the popular 'Fluorescent Lamp Starter' Kit as described in October 1982 EA. Normally \$1.50 each. This month only \$0.95 each! (Minimum 5 pieces). Makes the Fluoro starter kit very cheap!
(PCB's for the kit) Cat. HPB747

ONLY \$1.95



Cat. ZX7022
(8 amp 650V SCR)

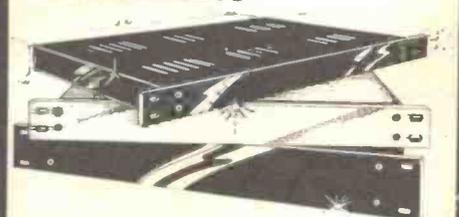
1N914 DIODES — INCREDIBLE SAVINGS

The 1N914 (for 1N4148 if you like) is probably the most popular diode in the history of electronics. We probably use over 1M a year ourselves! Jaycar has made a bulk purchase of these diodes and we can pass on great savings!
We must sell these in minimum lots of 500
Cat. ZR1100 1N914/1N4148
500 ONLY 3 1/2 cents each
1,000 ONLY 2 8 cents each
10,000 ONLY 2 cents each and these prices include tax!!
The glass envelope is really too small to have markings, however some are branded. We reserve the right to supply units that are the same size as the 1N914/1N4148 but are electrically superior.

FROM

2 cents
each!!!

RACK CABINETS



Beautifully crafted all aluminum rack cabinets with top and bottom removable panels. Plain or black finish. Vandalized lid. Deluxe brushed anodized front panel. Supplied in flat pack but take only minutes to put together. Dimensions conform to International Standard.

Cat. No.	Finish	Front panel height	Price
HB5411	Plain	44	\$39.95
HB5410	Black	44	\$39.95
HB5413	Plain	88	\$49.50
HB5412	Black	88	\$49.50
HB5415	Plain	132	\$54.95
HB5420	Black	132	\$54.95

JAYCAR

SEE PAGE 77 FOR JAYCAR ADDRESSES AND PHONE NUMBERS

IREECON 1983
SYDNEY SHOWGROUND
SEPTEMBER 5-9, 1983

Sony (Australia) Pty. Ltd.
has much pleasure in inviting
All IREE Delegates
to enjoy their hospitality
at the
Sony IREE exhibition in the
Ford Pavilion
and to view the release of an
exciting range of new
Broadcast, Institutional and
Pro-Audio equipment.

SONY®



CAMBRIDGE COMES TO AUSTRALIA

Cambridge Learning, the British publisher of educational books and kits, has launched an Australian subsidiary, Cambridge Learning Australia.

The parent company is well known in Britain, the United States and the Middle East for its electronics and computing

self-instruction courses, all of which use the easy-to-follow 'programmed learning system'.

The company's best-seller is *Cambridge Learning Superkit*, a self-instruction course in digital electronics. It comes with a 'breadboard' on which the user can build all the circuits, without soldering, so the components can be used repeatedly. The kit, complete with manual, components and breadboard, costs \$40.50, including postage and packing.

For more information, write to Cambridge Learning Australia, P.O. Box 173, Kwinana WA 6167.

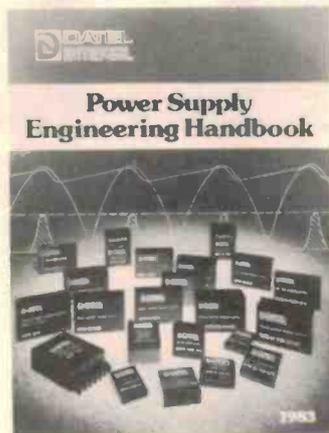
POWER-SUPPLY HANDBOOK

A new 40-page, full-colour power-supply handbook by Datel-Intersil details the electrical and mechanical parameters on more than 175 power suppliers.

The line of power conversion products includes modular encapsulated single, dual and triple output and chassis mounts; modular switching; plug-in power adaptors; dc-dc converter modules 1-10 W miniature 4.5 W dc-dc converters; and 24 V and 48 V dc-dc converter modules.

The handbook, which is free, is complete presentation to the design engineer.

Detailed specifications on Datel-Intersil's power supplies are presented in tabular form and includes complete case, pin and socket configurations. Additionally, an outline of modern power-supply principles and



practices and a section on power-supply terminology have been incorporated.

For more information, contact Elmeasco Instruments, P.O. Box 30, Concord NSW 2137. (02)736-2888.

'ULTIMATE' POCKET PAGER

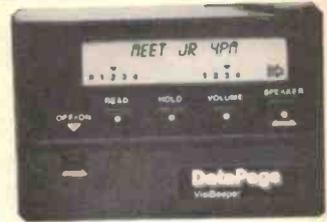
Visibeeper, claimed to be the 'ultimate' in pocket pagers, has been launched in Australia.

Visibeeper, which clips on to a belt or fits into a purse or pocket, has a small screen on which messages can be delivered in words and numbers.

Text messages of up to 80 characters are received directly by the pager. As many as four messages, totalling 160 characters, can be stored in the pager's memory.

At the user's command, the message moves across the instrument's readout screen. The readout can be stopped and held.

DataPage, which markets Visibeeper, has installed a computer and radio transmitting network which allows messages to be sent to Visibeepers anywhere in Metropolitan Sydney or Melbourne.



People wanting to send a message to a Visibeeper user phone the DataPage communications centre, where the message will be entered into a VDU terminal and transmitted. Alternatively, businesses can set up their own VDU and datalink into the computer and transmit messages without any DataPage operator intervention.

DataPage is the marketing arm of **Advanced Communications Australasia**, Building C, World Trade Centre, Flinders Street, Melbourne Vic. 3000.

BOOST FOR BIONIC EAR

The Federal Minister for Science and Technology, Mr Barry Jones, has announced that a further \$2 million will be expended to develop the implantable hearing prosthesis (bionic ear) through clinical trials and into commercial production.

The Department of Science and Technology will provide 75% of the amount. The rest will come from Nucleus Ltd, the Sydney-based electronics firm which will conduct the trials.

"This agreement will ensure the progress of high-technology industry in Australia, and help nerve-deaf people with a profound or total hearing loss, through the world," Mr Jones said.

The clinical trials will bring the project to the stage of determining its suitability for world marketing. The United States is the main export market for the device, and it is necessary to prove the safety and efficacy of any such product to the satisfaction of United States Food and Drug Administration.

Nucleus Ltd will co-ordinate the systematic analysis of 100 experimental human implants in centres around the world, and advance essential support systems such as training packages for patient selections, surgery

and rehabilitation, moving the project closer to full commercialisation.

The Department of Science and Technology has already contributed \$3 million to the project under the public-interest provisions of the Australian Industrial Research and Development Incentives Act.

The University of Melbourne initially developed the 'bionic ear', which is based on the principle of electronically receiving, processing and coding sounds on a manner similar to that which occurs naturally in the nerve fibres of people with normal hearing.

A coded signal is sent by an external worn transmitter to a miniature receiver-stimulator implanted behind the ear. This converts the signals to electrical impulses which are conducted to the inner ear, where the nerve fibres are stimulated electrically to enable the nerve-deaf to recognise speech and other sounds.

The clinical trials are expected to take about 18 months, with the device being commercially available by the mid-1980s.

For further information, contact Nucleus Ltd, 14 Mars Road, Lane Cove NSW 2066. (02)428-1011.

LOOK AT THESE EXTRAS YOU GET WITH FLUKE MULTIMETERS

8060A OFFERS FREQUENCY, TRUE RMS & DIRECT dB

This remarkable state of the art DMM combines the accuracy and resolution of larger, more expensive instruments with the convenience of a hand-held instrument. Fluke's own LSI/microcomputer design provides:

- Wideband true RMS AC measurements to 100kHz
- Frequency measurement to 200kHz
- dBm and relative dB
- 10µV sensitivity
- Direct resistance measurement to 300Meg
- Relative reference on any range or function
- Microcomputer-based self diagnostics

8062A

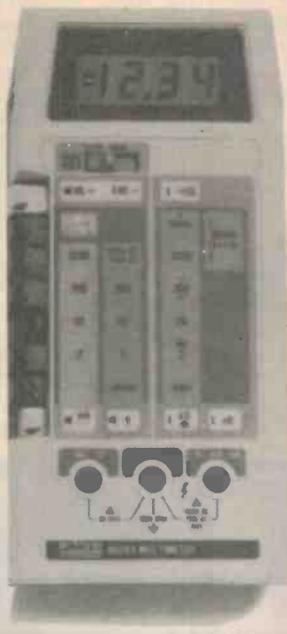
As 8060A above but without frequency and dB ranges. Provides true rms to 30kHz and relative reference functions.



8024B OFFERS PEAK HOLD AND DIRECT TEMPERATURE

The 8024B state of the art multimeter offers two important extra features – peak hold and temperature. Peak hold is a useful tool for capturing and retaining elusive voltage or current surges long enough to check and record the displayed reading. If your work involves measuring temperature then connect a K-type thermocouple and you can get direct temperature readings (we have a range available specially to suit the 8024B).

- 11 functions including temperature with K-type thermocouples
- Peak hold on voltage and current ranges
- Logic detection and continuity
- Audible and visible indicators
- 0.1% basic accuracy, 3½ digit



8026A OFFERS TRUE RMS AND CONTINUITY TESTING

The 8026A is the latest addition to the Fluke range and offers the advantage of true rms readings on ac functions. While most meters measure ac voltages almost all use the average-sensing, rms-scaled technique. In many applications average sensing does not give an accurate result – especially with non-sinusoidal waveforms. If you work with motors or data transmission type circuitry, true rms is critical to your measurements. For quick circuit checking the 8026A also incorporates the Fluke high speed continuity beeper.

- 8 functions
- True rms AC measurements to 10kHz
- Conductance and diode testing
- High speed continuity beeper



CHECK THE COMPLETE FLUKE 8020B SERIES

	DC Voltage	AC Voltage	DC Current	AC Current	Resistance	Diode Test	Continuity	Logic Level	Temperature	Peak Hold	DC Accuracy
8022B	•	•	•	•	•	•	•	•	•	•	0.25%
8021B	•	•	•	•	•	•	•	•	•	•	0.25%
8020B	•	•	•	•	•	•	•	•	•	•	0.1%
8024B	•	•	•	•	•	•	•	•	•	•	0.1%



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	100 kHz	200 kHz	0.04%	0.01%
8060A	•	•	•	•
8062A	•	•	•	•

All prices are plus Sales Tax if applicable and subject to change without notice.

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CROWDS FLOCK TO AUSTRALIA'S ONLY CONSUMER ELECTRONICS SHOW — IN PERTH

An estimated 110 000 people flocked to Perth's Claremont Showground to see all the latest and greatest in audio, video and home electronics gear from 90 exhibitors over four days in the first week of August.

Exhibitors crowded into the three largest pavilions available, the overflow taking another six pavilions. Last year's show took up only two pavilions and attendance was around the 80 000 mark. Since the Sydney CES show folded a few years ago, Perth's Electronics Show, now in its fifth year, has taken the industry (and W.A. consumers) by storm.

A wealth of new products — not yet released to the huge eastern states market — was on show, attracting enormous attention.

Two-speed VCRs were legion. As Akai found out, first in doesn't always mean best dressed (it released its VS4 two-speed VCR last March). National Panasonic, Sharp and AWA released two-speed machines — all up-market from the Akai, but the VS4 holds the lowest price point in the market at \$899.

National's NV-788 is a five-speed machine. Two are used for normal speed, a different pair for long play and the fifth head for rock-solid freeze frame without noise bars. It automatically knows what speed the tape was recorded at and switches to the correct replay speed. It will sell at \$1399 retail.

Sharp's two-speed VCR has four heads and is based on its current stereo machine, although the two-speed machine will not have stereo sound. AWA's machine is a four-head stereo model.

The big attraction on almost every stand was the digital disc. New machines were legion. Arena Distributors had a Dual-model CD120 (from Falk Electro-sound). This one, like most, plays the disc vertically and in typical Dual style, the player's panel layout is straight-forward and pragmatic.

Arthur Muldoon, from Falk, was there, and he told me that NAD would release its CD player early next year, featuring demultiplexing and dual chan-

nel D-A conversion. Sounds interesting.

Pioneer was surrounded on two sides (true! — you had to see it to believe it) by Marantz and Hitachi. After two days of absolute furore from CD demonstrations, they decided that everybody would get a go if they took it in turns. The most-popular tracks from the Polygram demo disc were Roxy Music (all 6dB of dynamic range), Chariots of Fire (sounding like helicopters in the jungle) and the 1812 Overture (speaker cones at five paces).

I was looking forward to seeing the Luxman (is it still around?) CD player, but local importer Vince Ross unluckily missed getting one in time for the show. Rank-NEC had one display, too. I think it's black and has a digital display, but it's hard to see thorough four-deep crowds.

Philips had its (after all, it started this!) and I actually saw a National Technics CD player

for the first time here since I saw it in Japan last year. Technics, you're slow. JVC followed the trend to black (Philips and Marantz having silver and gold — they gotta be different) and Sony's CDP101 also attracted a lot of attention. I was surprised K-Tel wasn't there with CD player and spin dryer (also available on cassette).

For something completely different, Danish hi-fi (why does that name always make me think of pig's ear pastries?) had Bang and Olufsen's 'Master Link' hi-fi system which lets you have sound in every room of the house and to be able to control it from wherever you are. The 7002 Master Link has a sophisticated microprocessor controller and a special bus cable that carries the audio wherever you want it, plus the control lines. Styling is typical B&O, as is the price.

Getting back to video, JVC was showing off its latest camera, which features a tube that works with light levels down to 10 lux — pretty well the light left after you've blown out the candles. But it couldn't seem to hold a candle to Sony's video attraction — the Betamovie

camera. Maybe it was the Sony girls dressed in the leotards that did it.

Convoy, more renowned for its Nakamichi and Monster Cable products, has entered the video fray with a highly unusual product. It's a stereo sound processor for VCRs that also cleans up the noise and enhances the dynamic range. If you've got mono tapes you can give them stereo sound as well as adding considerable sparkle to the reproduction.

Hip stereos were everywhere (K-Tel, where are you?). But Sony has stolen the march on everyone again and produced a sportsman model that works underwater (and sand, and snow, and...).

I haven't got around to the video games, home computers and similar paraphenalia yet, room's running out and this is Sight & Sound, anyway. Watch for the Electronics Show Report in next month's ETI.

Easterners frustrated? Well, you could try National's "Shaping the Future" C.E. show at Sydney's Centrepont from 1-9 September.

—ROGER HARRISON



KEYBOARD CASSETTE DECK

Due for release in Australia in September, AIWA's three-model AD-F triple-head cassette deck series has been designed to meet the demands of all types of programme material, whether digital or analogue.

The range features Dolby's HX Professional circuitry, a new system which ensures that signals at all volume and frequency levels receive the ideal amount of bias during recording.

Other features include a keyboard-style control panel, micro-grain dual capstan trans-

port, automatic de-magnetising, automatic tape adaptation for bias, sensitivity and equalisation, and a tape-remaining time display.

The top-of-the-range model is the AD-F990, which will retail at \$729. The mid-range model AD-F770 will have a \$599 tag, and the AD-F660 will be \$499.

All three models share the same dimensions, 420 x 110 x 280 mm. Weight is 5.5 kg.

A cordless remote-control handpiece, the RG-R200, will be available as a recommended optional extra.



PROFILE II TONEARM

Pro-Acoustic's Profile II tonearm, now available in Australia, utilises design techniques which the Canadian manufacturer claims reduce tonearm anomalies and permit proper interface to the cartridge.

The result, Pro-Acoustics says, is maximum retrieval of information and minimal colouration.

The Profile II has an aluminium headshell, which is fitted with Litz wire leads and gold-plated cartridge tags. It is detachable, but mates tightly to the arm tube, while high-spring

tension on the gold-plated pin contacts ensures ideal electrical contact.

The arm tube is stepped to break up resonances during play. Residual resonances are terminated by precision hardened bearings — two bearings for vertical movement, in a gimbal, and two for lateral movement, located inside the arm pillar.

The rear counterweight is decoupled and disc-shaped to allow close placement to the pivot point, reducing inertia and resonances further still.

Priced at \$169, the Profile II is handled in Australia by Convoy International, 400 Botany Road, Alexandria NSW 2015. (02)698-7300.



BUDGET-PRICED SPEAKER

Concept Video has introduced the MS20, a 200 mm two-way high performance unit, to its Mordaunt Short range of loudspeakers, imported from Britain.

The bottom-of-the-range MS20, which has a five-year guarantee, retails at \$398.

The Mordaunt Short range now comprises the MS20, Carnival 3, Festival 3, Pageant 3 and Signifier speakers. The top-of-the-range Signifier is priced at \$1998.

For further details, contact Concept Audio, 17/98 Old Pittwater Road, Brookvale NSW 2100. (02)938-3700.



THE COMPACT DISC GOES MOBILE

The latest advance in sound, the compact disc player, has recently arrived on the Australian market, and Mitsubishi Electric has stolen a march on the market and installed a compact disc player in a car. It will appear for the first time in Australia at this year's Sydney Motor Show.

The advanced technology of the compact disc will offer many advantages for the car sound enthusiast, including improved protection against damage. The laser-based player will provide superior music reproduction range and stereo separation, and can counteract the problems of road noise, Mitsubishi claims. The 115 mm compact disc is also easily stored.

Mitsubishi Electric's car audio digital disc player is expected to be available on the Australian market next year and will retail at approximately \$1000.

BRISBANE HI-FI EXPO

Queensland's electronic enthusiasts will be kept up-to-date with the latest hi-fi and video developments at the Hi-Fi and Video Expo '83, from September 9-11 at Brisbane's Park Royal Motor Inn.

One of the largest shows of its type staged in Queensland, the Expo will be a showcase for the digital audio disc, with up to 10 manufacturers demonstrating the new laser technology.

For more information, contact the show organiser, Robert Woodland, 50 Sherbrooke Road, Acacia Ridge Qld 4110. (07)372-3380.

Why Direct

Don't tangle with Technics.

The majority of audio systems – even the most beautifully designed – have something ugly to hide.

It's that mass of jumbled-up connecting leads that you find, all too easily, at the rear of the equipment. Not only are they ugly, they're inconvenient, too.

And as audio components become smaller, the problem becomes bigger and more unsightly.

To solve this problem, Technics developed their Direct Connector systems, which eliminate all audio connecting leads between the tuner, amplifier, graphic equalizer and cassette deck.

Each of these components features a special flip-up connector to allow them to be literally plugged in to each other!

It's an elegant piece of Technics technology that results in a stylish, neat installation that can be put together or taken down for re-location in a matter of seconds.

The 315 Series.

But Direct Connector capability is not the only innovative feature in this new and compact series from Technics.

The SL-5 direct-drive, linear-tracking turntable employs its own plug-in connector system for the pickup cartridge.

This unique Technics development has been adopted as a World Standard.

It means you can compare and evaluate cartridges from leading manufacturers like Audio Technica, Ortofon, Shure, Stanton, Empire, Pickering, ADC and, of course, Technics without conventional setting up procedures.



Technics developed Connector systems.

No adjustment of tracking weight or bias correction is needed.

The innovations continue in the rest of the components: the SU-5 amplifier includes a Super Bass switch to enhance the bass response of a speaker system without inducing bass boom; the ST-5 quartz synthesizer digital tuner provides random access memory for 16 pre-set stations; the SH-E5 graphic equalizer – offers adjustment of 12 audio bands from 16Hz to 32Hz on each channel; whilst the RS-5 cassette deck – has soft touch controls, auto selection of metal, CrO₂ and normal tape settings plus convenient Cue and Review functions.

Finally, a pair of SB-F5 speakers with horn-type tweeters and bass reflex porting turn the high quality electrical signals of the rest of the system into the high quality sound you expect.

Compact components, full-size warranty.

All components in this series are perfectly matched in styling and performance.

And all are covered by a full 2-year warranty backed by Technics' reputation. Visit your Technics stockist soon and experience the superb styling and brilliant sound of Technics' compact Series 315 for yourself.



Technics
National Panasonic (Australia) Pty Ltd
Expanding the music experience.

Compact disc players— *fact not fiction*

Are compact disc players really as incredible as they are claimed to be? Can all those amazing statements flourished by the press about these revolutionary units really be true?

Louis Challis

I DON'T WISH to be critical of some of the articles written by my fellow writers, but I must state from the outset that not all I have read about compact disc players is actually true.

I am a bit of a pedant on the need for accuracy on what goes into print (as is the editor), so I am going to try to set the record straight on some of the more outrageous statements.

THE FICTION

"Compact discs don't suffer from the scratch problems of micro-groove records because they are tracked optically by a laser, not by a stylus."

THE FACT

Well, that statement isn't really correct as you can scratch a compact disc. And if it is scratched badly then the damage will be almost as effective as a scratch on a microgroove record.

A bad scratch on a disc will cause the CD player to either reject it, stop tracking or have an apoplexy, depending on the brand of player.

We played a thoroughly scratched disc on four different players and observed four different responses. Most of the players had difficulty in tracking various sections of the scratched disc and at least two of them seemed to suffer a case of what I can only describe as 'electronic apoplexy'; they stopped tracking, stopped working and switched themselves off.

However, all is not lost if the disc is only mildly scratched as it can be gently polished back to a playable state with a mild abrasive polish, followed by careful wax polishing. This is something you cannot do with a microgroove record.

THE FICTION

"All compact discs are virtually indestructible."

THE FACT

I was quite amused when I read this statement in the Bulletin, June 21, 1983.

I had received one disc from Pioneer Australia which had been very badly scratched, and innumerable discs from

other suppliers which had suffered various degrees of scratching. So I know that the discs are not indestructible. They can be damaged by mechanical handling or simply from normal abuse.

I was extremely concerned that the compact discs are liable to thermal distortion, particularly in cars where the temperature under the dashboard is known to exceed 65 °C in typical Australian summer conditions.

I was aware that such temperatures affected conventional compact cassettes, particularly the cheaper thermal plastic types, causing them to droop and seal themselves into your unsuspecting cassette player. So I felt that we should find out how compact discs reacted under these conditions.

We took a brand new and playable compact disc and placed it into our controlled temperature oven which produces temperatures up to 80 °C. We monitored the droop characteristics of the disc when it was edge-supported in a horizontal position and the best distortion we could get out of it was a 1 mm droop after 24 hours at 80 °C.

We then took the same disc and placed it in a controlled temperature bath in which the water was circulated and slowly raised to boiling point. Even at 100 °C the disc retained its shape and suffered no adverse effects. We were able to play it without any ill effects in three different CD players.

We did note, however, that at that temperature there were positive signs of surface softening on the disc, but we did not prolong the agony to find out how long you have to boil your disc to make it 'whiter than white'.

If you are prepared to store, play or subject your compact discs to temperatures of 100 °C, do so with our blessings and commiserations.

The sample disc we tried to destroy was provided by Philips, but we feel reasonably sure that Sony-CBS and the other producers have also taken the time and the trouble to specify a thermal plastic which is not going to melt in either your automotive or residential CD player.

The thermal resistance of the sample disc we tried to destroy was better than we expected but it is nonetheless clear that the

CD discs are destructible. I believe that it is unwise for the manufacturers or their marketing personnel to suggest otherwise.

THE FICTION

"Different CD players sound different even when played with the same compact disc."

THE FACT

When I first read that statement I was sceptical, as you probably are too. So we put the issue to test and took four different CD players from four different manufacturers and played them through the same equipment in my living room.

The job was made a bit easier as three of the manufacturers had each provided a copy of the Polygram demonstration disc 800-104-2. This made it feasible to set up two machines with the music almost synchronised and it was possible to switch from one player to another in groups of up to three.

Lo and behold, I believe that I could hear small but discernible differences between the individual CD players and my family backed me up by confirming the phenomena. Unlike the other illustrious gentlemen who had rushed into print, I did not feel that I was justified in saying anything unless I could back up my statements. I believe that I should be able to explain why there was a difference and present some objective evidence.

My staff and I set out to determine why these differences should exist in the audible content.

We discounted the compact discs used as we believe they are a common element. So all we can possibly have left is the digital to analogue converter and the subsequent amplification stages in each CD player.

We believe that it is in these areas where there are significant differences between one manufacturer's machine and the next, and maybe between two machines of the same type.

"How can that be?" you say. Well, it's easier than you think. The problem is that each CD player uses a monolithic 16-bit or 14-bit digital to analogue conversion chip. The chip's conversion from digital format to analogue format is intended to be absolutely linear, however, this never really



occurs and each chip has some small degree of non-linearity inherent in its conversion characteristics.

Our detailed measurements on four sample machines, from four manufacturers, revealed small but measurable (and we believe audible) differences between the machines, particularly at levels between -30 dB and -90 dB relative to 0 dB (the theoretical maximum) recorded level.

The total harmonic distortion (THD) levels measured between -60 dB and -90 dB were very significant and far more so than at high signal levels where our measurements confirmed that they are *incredibly* low.

By contrast, the absolute converse is true for microgroove records which tend to have lower distortions at low signal levels and higher distortions at high signal levels.

THE FICTION

"Panels of listeners prefer the sound from conventional microgroove records to that from compact discs."

THE FACT

Well, that statement may be either right or wrong depending on how they were as-

sessed, what software was used for this assessment and what questions were asked following the assessment. Obviously you can get any answer you want to any proposition, merely by selecting your sample (audience and software) and by posing your questions *in the appropriate manner*.

The facts are simple; if the programme content or the *same* signal is originally recorded on an *analogue* tape recorder and is then recorded on both microgroove records and compact discs, the resulting sound *is* different. Some auditors will think that the conventional records sound better and some will prefer the sound on the compact disc.

The fact of the matter is that virtually all the pre-recorded content that I have listened to on compact discs appears to incorporate a higher proportion of high frequencies than the same material recorded on either half speed masters (45 rpm microgroove records) or conventional high quality microgroove records.

The reasons for this have not yet been positively confirmed. However, I believe it may be a result of the mix-down equalisation characteristics which are selected by the record or disc producers. These characteristics obviously need to be slightly different for each format and appear to be inappropriate on a number of new compact discs recently imported into Australia.

The only sure way of confirming this will involve considerable ingenuity and, in particular, assessment of the record production facilities at one or more of the major software mix-down facilities overseas. Needless to say, I am going to follow this one through.

The assessment of the differences between compact discs and conventional microgroove records is also affected by the equipment used when the programme content is being recorded. If the software was digitally recorded before being transferred to records and discs, the differences between them can almost be paraphrased as being 'astounding' and, in my opinion, 'incomparable'.

I make this statement unabashedly after having played two different selections which I possess on two microgroove records; one of them was based on an analogue recording, the other was from a digital recording. These were subjectively compared with the same material presented as two separate recordings on compact discs.

Following this assessment, it is easy to state categorically that the compact disc is clearer and more realistic than the conventional microgroove records. More importantly, the background noise heard on conventional records, due to the interaction of the stylus with the vinyl surface and often dust as well, is completely absent.

THE FICTION

"You don't need new equipment with a CD player as all your old equipment is fully compatible."

THE FACT

Well, after testing six different CD players and using them with a wide range of consumer high fidelity equipment, I must say that I disagree with that statement. If your old equipment is good, i.e. if you have a good amplifier with a power rating of better than 100 watts peak output power ▶



A badly scratched disc. Most CD players will have difficulty tracking bad scratches, with audible results.

and your speakers are equally good, then the chances are that your system will be compatible with a CD player.

However, if your amplifier is a modest 20-40 watts unit and your speakers are nondescript then I think that you would be wasting money to buy a CD player. Not only will you be unable to extract the full dynamic range, but more significantly, chances are that the distortion and intermodulation characteristics of your speakers will stand out like a sore thumb.

I used a large number of different consumer amplifiers and loudspeakers to make up several combinations of hi-fi equipment with the CD players, to compare the sound when playing compact discs. It soon became apparent that using a low power amplifier, and especially if a set of nondescript speakers was used as well, could do terrible things to the quality of the sound.

If the amplifier is driven to peak levels anywhere near overload, which of course depends on the level at which you play your system, then the likelihood of inducing peak clipping ranges between 30 times and 100 times more often than it would occur if a microgroove record or cassette tape was the program source.

Quite apart from that, the loudspeakers are then subjected to their own 'trial by torture' as they attempt to reproduce the wide dynamic and frequency range, the likes of which they most probably have never come across before.

The results of listening to wide ranging and uncompressed music may well be to your ears what they were to mine — disturbing, to say the least. Good speakers sound good, poor ones sound terrible.

The moral of the story is, if your equipment is nondescript you should seriously consider upgrading your speakers and amplifier to better units before you spend money on buying a CD player.

THE FICTION

"Compact discs will not replace microgroove records because people will not wish to throw away their collection of records."

THE FACT

Well, I can't really argue with that statement. I know many people who still have magnificent collections of 78 rpm records and I even have quite a few myself. However, these records are rarely played, except when they are used to illustrate the works of some great singer or musician whose works have not been re-recorded on the conventional microgroove.

Ho hum! You too will sooner or later join the ranks of antique collectors. I can almost see the vintage microgroove collectors in the year 2052 trying to buy pristine Beatles' records recorded 'the way they were sold in 1972'.

The CD players are an astounding state-of-the-art advance in the field of electro-acoustic technology. They have more attributes than disadvantages, but by setting reproduction standards so high (which they alone can achieve) they highlight the deficiencies of their more worldly relatives such as the amplifiers, loudspeakers and even the lowly rooms in which they are installed.

The high standard of the players also

determines the quality of the software and the mode, place and recording techniques chosen. This has created new and unexpected problems for the whole recording industry. What used to be good enough for the ubiquitous microgroove recording is just not good enough for a CD recording.

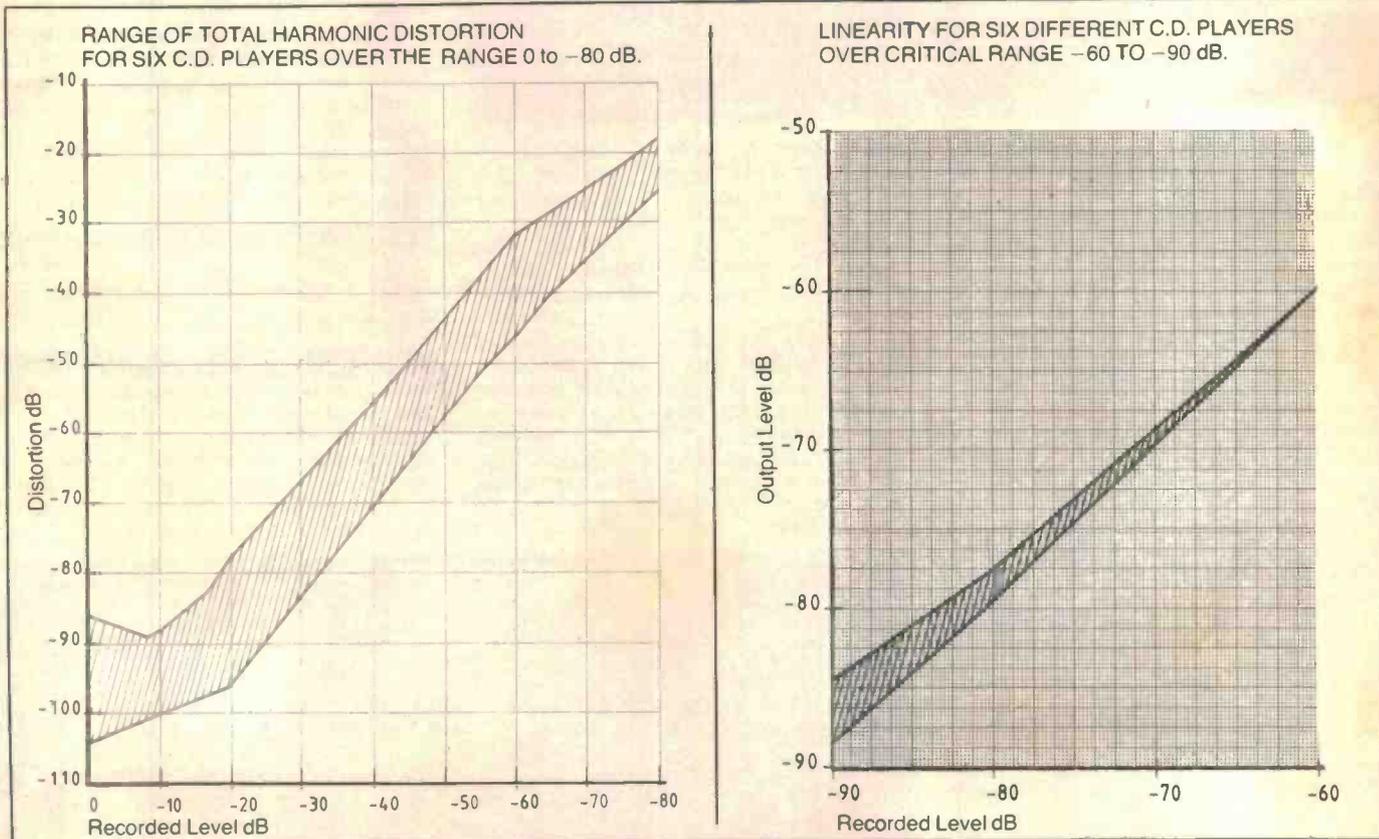
If you think you have problems then there are many people with longer faces than yours. They are not just faced with the cost of a new amplifier or loudspeakers but with the cost of multi-track digital recorders, new studios, new microphones and the need to introduce and master a new recording technology.

Obviously, a number of you will, in the near future, contemplate buying a CD player. This magazine will endeavour to assist you by presenting accurate objective and subjective assessments of the latest CD players in the market place. It will then be easier for you to compare their performance and features.

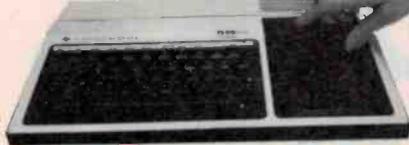
We have already seen in the trade literature that each manufacturer stresses the low harmonic distortion, flat frequency response, extended dynamic range and signal-to-noise ratio, as well as the immeasurable wow and flutter.

What they have all tended to ignore, so far, are the wide differences in the other important features which include shape, special control functions for replay and automatic programme selection and reliability, which is still an unknown factor.

With all this fact and fiction, the fiction will obviously dominate over the fact until you have your own CD player side by side with your youthful record player. Then you can assess whether the expense has been worth it, both to you and to the industry. ●



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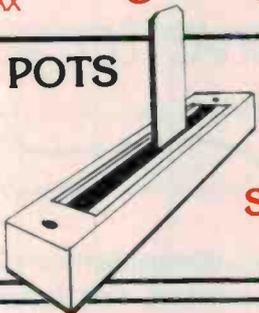


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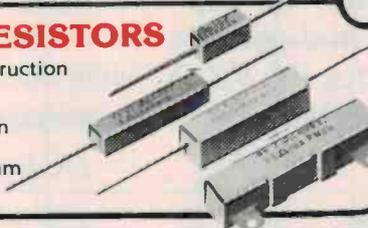
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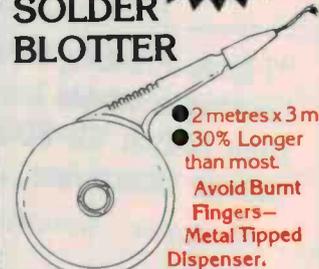


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22 180 1K8 18K 180K 1M8	1.8 18 180 1K8 18K 180K 1M8
27 220 2K2 22K 220K 2M2	2.2 22 220 2K2 22K 220K 2M2
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47 390 3K9 39K 390K 3M9	3.9 39 390 3K9 39K 390K 3M9
56 470 4K7 47K 470K 4M7	4.7 47 470 4K7 47K 470K 4M7
68 560 5K6 56K 560K 5M6	5.6 56 560 5K6 56K 560K 5M6
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1.8 18 180 1K8 18K 180K 1M8	1.8 18 180 1K8 18K 180K 1M8
2.2 22 220 2K2 22K 220K 2M2	2.2 22 220 2K2 22K 220K 2M2
2.7 27 270 2K7 27K 270K 2M7	2.7 27 270 2K7 27K 270K 2M7
3.3 33 330 3K3 33K 330K 3M3	3.3 33 330 3K3 33K 330K 3M3
3.9 39 390 3K9 39K 390K 3M9	3.9 39 390 3K9 39K 390K 3M9
4.7 47 470 4K7 47K 470K 4M7	4.7 47 470 4K7 47K 470K 4M7
5.6 56 560 5K6 56K 560K 5M6	5.6 56 560 5K6 56K 560K 5M6
6.8 68 680 6K8 68K 680K 6M8	6.8 68 680 6K8 68K 680K 6M8
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1.2 12 120 1K2 12K 120K	1.2 12 120 1K2 12K 120K
1.5 15 150 1K5 15K 150K	1.5 15 150 1K5 15K 150K
1.8 18 180 1K8 18K 180K	1.8 18 180 1K8 18K 180K
2.2 22 220 2K2 22K 220K	2.2 22 220 2K2 22K 220K
2.7 27 270 2K7 27K 270K	2.7 27 270 2K7 27K 270K
3.3 33 330 3K3 33K 330K	3.3 33 330 3K3 33K 330K
3.9 39 390 3K9 39K 390K	3.9 39 390 3K9 39K 390K
4.7 47 470 4K7 47K 470K	4.7 47 470 4K7 47K 470K
5.6 56 560 5K6 56K 560K	5.6 56 560 5K6 56K 560K
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A discerning discourse on digital disc players

Louis Challis

AKAI CD-D1 • HITACHI DA-1000 • PIONEER P-D1 • SANYO DAD 8 • SONY CDP-101 • YAMAHA CD-1

PHILIPS AND SONY previewed the first CD players in Australia just over 12 months ago. Since then it has become obvious that CD players have 'taken off', making a tremendous impact on the hi-fi scene.

Already more than 70 firms have been licensed to produce software (the compact discs containing the programme content) and over 40 firms have been licensed to manufacture the hardware (the players).

In the market place the dealers are fighting furiously for the inadequate number of machines that are allocated by the importers to their clamouring distributors.

In the record shops that I visited most of the discs seem to sell more quickly than even the shop assistants would like. However, not one of the record shops I visited had yet installed a CD player, so the purchase of a disc would have to be based on the reputation of the musicians or the composer, and not on the proven quality of the software.

The main problem now, when you want to buy a CD player, is that you won't be able to compare the different units in the shop as the stocks of most dealers are close to zero.

An equally significant problem is the wide range of recommended retail prices and diverse range of features that the competing brands are offering.

AKAI CD-D1

Manufacturer: Akai in Tokyo, Japan
Distributor: Akai Australia Pty Ltd, Unit 11, Eden Park, 31 Waterloo Rd, North Ryde NSW 2113. (02)887-2311.

HITACHI DA-1000

Manufacturer: Hitachi Sales Corp. in Tokyo, Japan
Distributor: Hitachi Sales Australia Pty Ltd, 153 Keys Rd, Moorabbin Vic. 3189. (03)555-8722.

PIONEER P-D1

Manufacturer: Pioneer Electronic Corp. in Tokyo, Japan.
Distributor: Pioneer, 178 Boundary Rd, Braeside Vic. 3195. (03)580-9911.

SANYO DAD 8

Manufacturer: Sanyo Electric Trading Co Ltd, Osaka, Japan
Distributor: Sanyo Aust Pty Ltd, 225 Miller St, North Sydney NSW 2060. (02)428-5822.

SONY CDP-101

Manufacturer: Hi-fi audio division of Sony Corp, Japan
Distributor: Sony, 453 Kent St, Sydney NSW 2000. (02)266-0655.

YAMAHA CD-1

Manufacturer: Yamaha Nippon Gakki Co Ltd, Hamamatsu, Japan
Distributor: Rose Music, 28 Kent St, Belmore NSW 2142. (02)750-8999.

At last — a test disc

This review assesses the performance and compares the features of six of the first available CD players.

We found that nearly all of the players we tested easily exceeded most of their stated performance specifications. The trouble with these figures is that they tend to be an 'under-statement', rather than an over-statement of the real performance characteristics.

Our testing revealed that the performance varied from brand to brand and it also varied, to a lesser degree, among players of the same type.

When CD players were first released in Australia we were faced with a problem. We couldn't test them properly as there was initially a lack of special software for evaluating the players; their technical characteristics are unique.

Sony in Japan and Philips in Holland produced a series of test discs early last year but Sony withdrew the first of their discs not long after they were released. We had to wait until June '83, when the third series of Sony's test discs was released, before we could start our serious testing.

Philips also released its test discs but only received one set in Australia (test discs 3,4 and 4A) which we were not able to borrow until mid-July.

So with the first Sony test disc in Australia firmly in our hands we were able to evaluate the characteristics of each of the CD players. We made one assumption which was that the Sony software provides the precise parameters that are stated on the cover sheet. This is extremely important when trying to measure the non-linearities in the equipment without measuring the deficiencies in the software.

We didn't receive the Philips test discs until after we had finished testing the players. However, we compared the Sony test disc and the Philips test discs and we believe that the most critical of our measurements are reasonably close to the values of 'least uncertainty' for the test discs themselves, particularly where the distortions or linearities are approaching five-digit resolution.

With some of the test material available for testing turntables and cassette recorders the manufacturer will provide, when requested, data in terms of the value of 'least uncertainty'. However, Sony has not yet provided comparable data.

But we have found that the Sony test disc does provide adequate precision and resolution for us to be able to measure and

quantify the differences between each of the CD players reviewed.

The CD players that we reviewed are the first releases from Akai, Hitachi, Pioneer, Sanyo, Sony and Yamaha. We did have the Marantz player prior to receiving the test software, but it was recalled for an interstate demonstration and was so much in demand that we didn't see it again.

These machines are intended to do the same job and have general mechanical characteristics in common, but after that all similarity ends.

It is not the frequency response or the dynamic range that create the differences between one player and the next, but the facilities provided for handling, processing and selecting the programmes and playing the disc.

As these machines perform so well we have paid particular attention in the evaluation to refinements of performance, user controls and unusual features.

The machines are reviewed in alphabetical order which does not necessarily indicate a rating of performance or preference.

Akai CD-D1

The AKAI CD-D1 incorporates a large number of well designed ergonomic features. One feature that I particularly liked is that the disc holder is manually closed rather than electronically closed; this relies on the natural response of most users to 'push the darn thing closed' and not to look for another switch with which to close it.

In the centre of the panel is the display module which is divided into four horizontal layers. The top layer provides mode information, telling you whether the unit is in standby, pause or play mode.

The second level of the digital display tells you the number of the selection that is actually playing. If the unit is not playing a zero is displayed.

The third row provides the elapsed playing time in minutes and seconds. The programming keys on the right hand side of the panel also tell you the time in minutes and seconds at which the start of a cycle or sequence should commence.

The bottom section is a quasi-analogue display which shows the position of the recording head using an array of light emitting diodes.

The control switches consist of one double sized 'play' button with its own self indicating LED, four buttons for 'stop-eject', 'pause', 'fast forward' and 'fast rewind' and two buttons labelled 'PLS' for automatic location of either the previous selection or next selection on the disc.

TABLE 1

	Compact disc player Priced at approx. \$1300	Conventional turntable Priced at approx. \$1300
Number of channels	2	2
Digital to analogue conversion	16-bit linear (except Philips)	not applicable
Frequency response	5 Hz to 20 kHz \pm 0.5 dB	20 Hz to 20 kHz +1 dB -2 dB
Harmonic distortion	less than 0.004% (1 kHz 0 VU)	typically 1% (1 kHz 0 VU)
Dynamic range	more than 90 dB	60 dB
Signal-to-noise ratio	more than 90 dB	60 dB on a clean record
Channel separation	more than 90 dB	28 dB at 1 kHz
Wow and flutter	below measurable limits	0.03% RMS

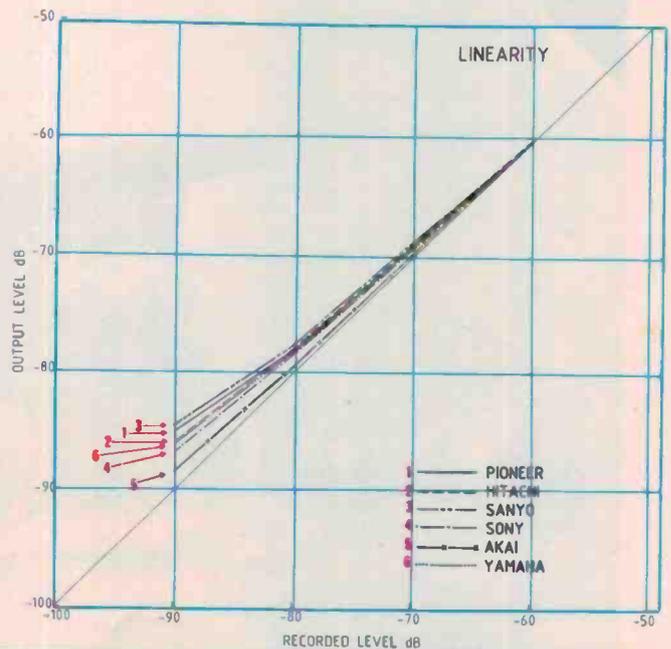
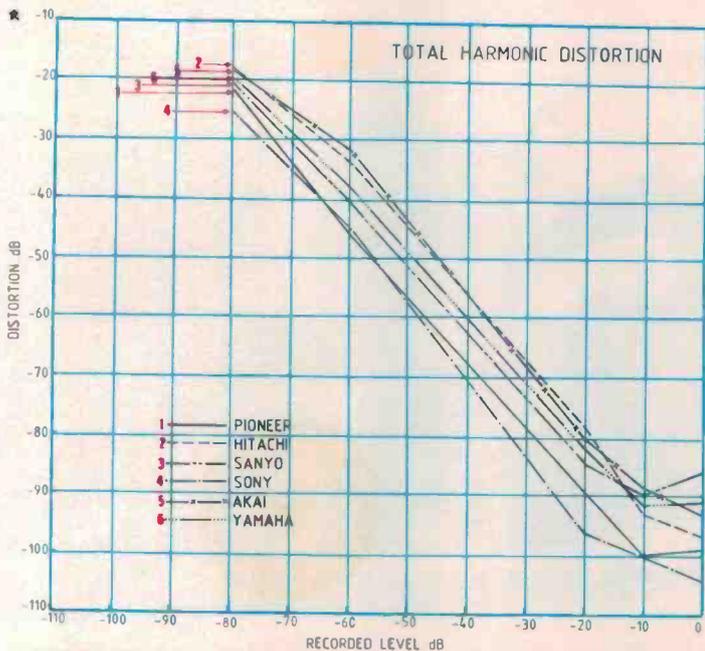


Table 2

Make and Model	Recom. Retail Price	Dimensions W x H x D mm	Weight kg	Remote Control	Disc Rotation	Electronic Open/Close	Dynamic Range With Emphasis	Distortion @ 1 kHz re 0 VU	Distortion @ -60 dB re max recorded level
AKAI CD-D1	\$1329	440 x 145 x 320	7.4	No	Vertical	Open only	95.9 dB Lin 106.4 dB(A)	0.0021%	-31.9 dB
HITACHI DA-1000	\$1150	320 x 145 x 234	5.6	No	Vertical	Open & close	100.4 dB Lin 103.3 dB(A)	0.0014%	-33.9 dB
PIONEER P-D1	\$1399	420 x 140 x 330	12.1	No	Vertical	Open only	96.0 dB Lin 100.5 dB(A)	0.0011%	-46 dB
SANYO DAD 8	\$1099	335 x 145 x 285	7.3	No	Vertical	Open & close	95.0 dB Lin 97.5 dB(A)	0.005 %	-40.6 dB
SONY CDP-101	\$1199	355 x 105 x 325	7.6	Infrared unit	Horizontal	Open & close	109.9 dB Lin 113.0 dB(A)	0.006 %	-45 dB
YAMAHA CD-1	\$1999	435 x 116.5 x 357	13.5	No	Horizontal	Open & close	99.0 dB Lin 104.0 dB(A)	0.0028%	-38.3 dB

On the right hand side of the console are ten keys for keying in numerical data, a 'set' switch, a 'cancel' switch and six elongated keys.

The top elongated key is for the selection of 'phrase', a term commonly used by all the manufacturers meaning the selection of the time or section in seconds.

The 'index control' is used on those compact discs that have the display IN:DEX. These discs, which are not currently available, will allow you to select the music sequence number and select a particular segment within that sequence. This is achieved by selectively pressing the 'index' key then pressing the sequence

number. As none of the discs that I was playing had the IN:DEX display I could not check this function.

The 'time' switch tells you the residual playing time on the disc, the 'memo call' allows you to check what you have stored as memory instructions, the 'repeat' switch allows you to repeat one sequence over and over again and the 'total time' switch tells you the total time on the disc.

On the back of the unit is a volume control with which you can adjust the player's output level to match your amplifier's auxiliary input requirements. This unit also has a pair of gold plated phono sockets which is a common feature

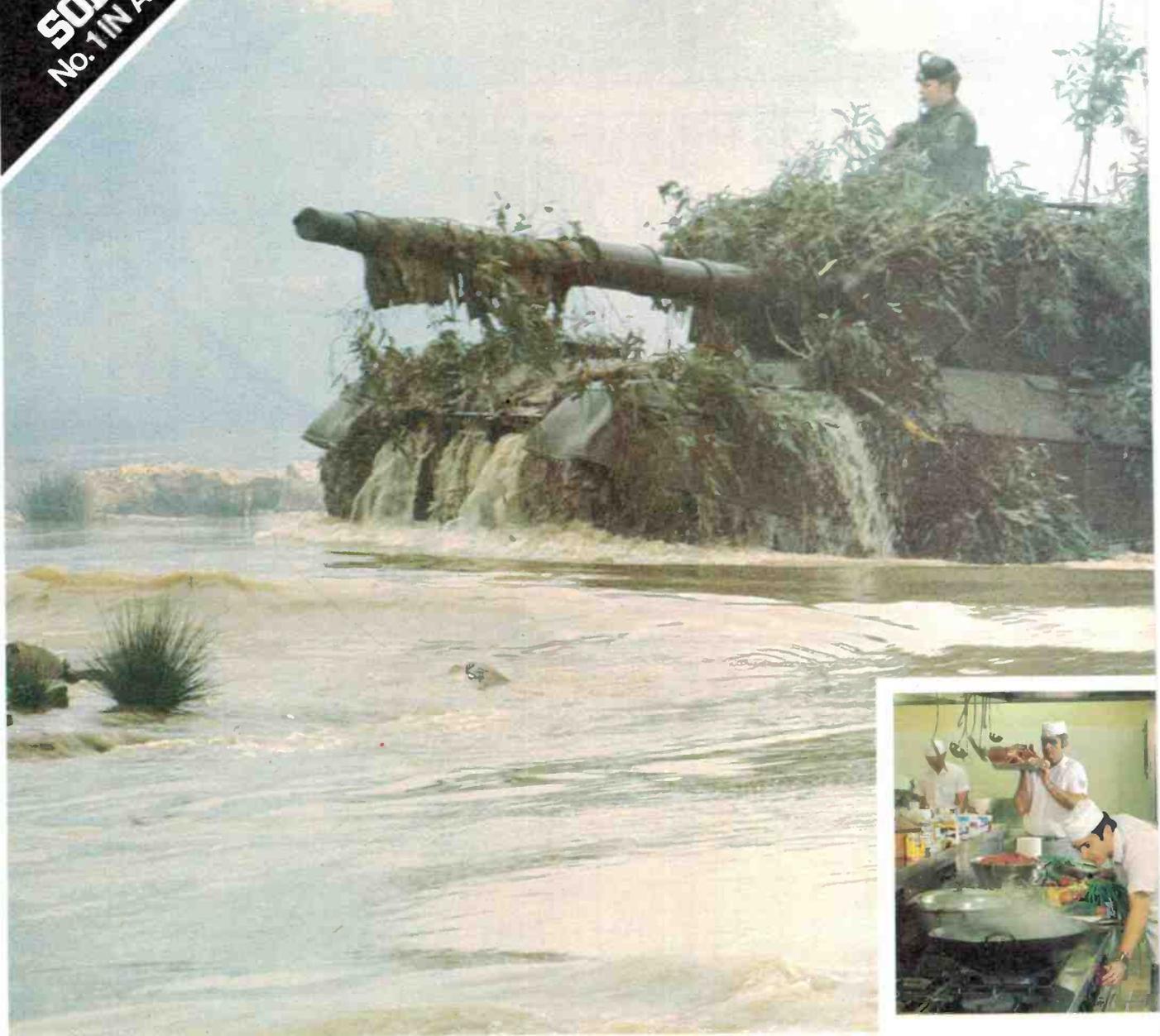
on all the CD players reviewed.

The performance characteristics of the Akai player are excellent. The frequency response is \pm 0.2 dB from 20 Hz to 20 kHz and the replay linearity is almost perfect from 0 dB to -60 dB, 0.5 dB high at -80 dB and 1.4 dB high at -90dB.

The A-weighted signal-to-noise ratio both with and without emphasis is 106.4 dB which is significantly better than claimed for the unit by Akai.

The channel separation from right to left is better than -103.9 dB at 100 Hz, better than -95 dB at 1 kHz, better than -89 dB at 10 kHz and better than -92 dB at 20 kHz.

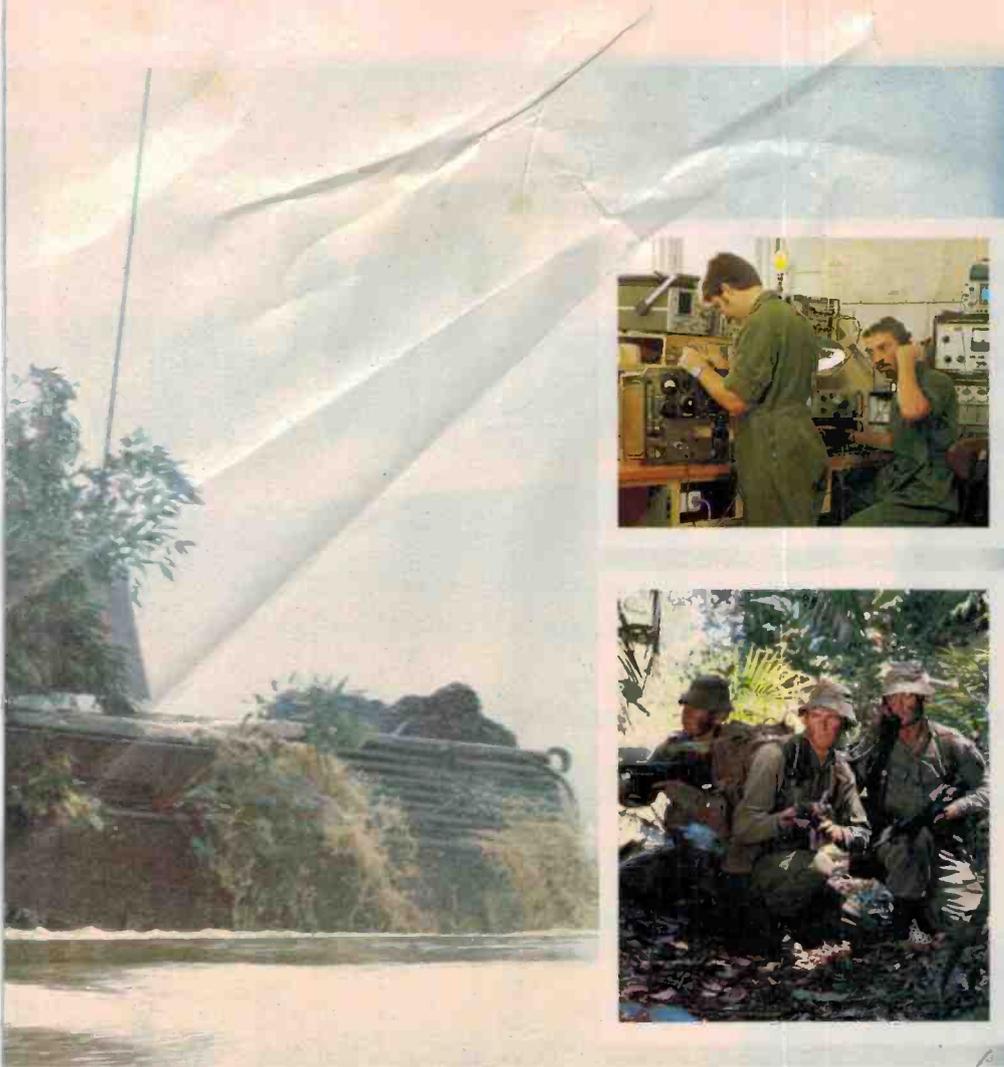
**"I'm a
Soldier."
No. 1 IN A SERIES**



**"Not every bloke who
wants to drive**

Sydney 212 1011; Parramatta 635 1511; Newcastle 2 5476; Wollongong 28 6492;
Adelaide 212 1455 (Also Northern Territory); Lismore 21 6111; Melbourne 61 3731; Geelong 21 1588;

Authorised by Director-General of Recruiting, Dept. of Defence.



ARMY

Australian Regular Army

joins the Army a Leopard Tank."

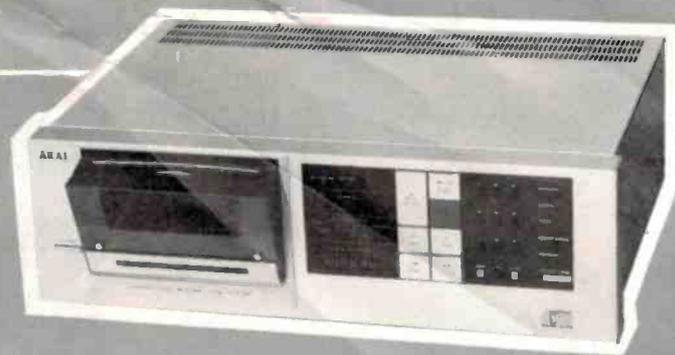
These days the Army can train you in one or more of 150 different jobs, from Plant Operator to Computer Operator; from Electronic Technician to Assault Pioneer. First they assess your ability and potential, then they give you the skills to do the job that's right for you. And because the Army is one of the country's biggest employers, you have the challenge of a rewarding career plus a better-than-average chance for further training and promotion. If you'd like to know more, phone your nearest Army Careers Adviser.

Bendigo 43 8008; Ballarat 31 1240; Brisbane 226 2626; Townsville 72 4566; Albury 55 2248; Hobart 34 7077; Launceston 31 1005; Canberra 82 2333; Perth 325 6222.

AKAI CD-D1

Distributor:

Akai Australia Pty Ltd
Unit 11, Eden Park
31 Waterloo Rd
North Ryde NSW 2113
(20)887-2311

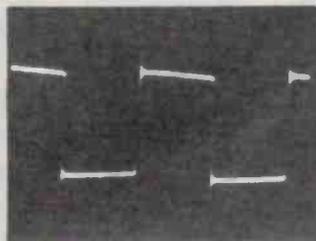


SIGNAL-TO-NOISE RATIO

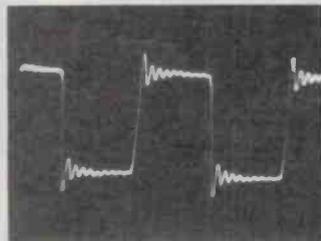
Without Emphasis 93.0dB(Lin) 106.4dB(A)
With Emphasis 93.0dB(Lin) 106.4dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	-119.4	-103.9
1kHz	-104.3	-95.0
10kHz	-89.6	-93.0
20kHz	-92.3	-99.3



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB

	100Hz	1kHz	10kHz	
2nd	-96.7	-93.7	-90.5	dB
3rd	-90.4	-110.6	out	dB
4th	-103.7	-107.6	of	dB
5th	-110.4	-111.6	Range	dB
T.H.D.	0.0034	0.0021	0.0027	%
T.dB	-89.3	-93.4	-90.5	dB

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	-90.0	-81.8	-34.5	-12.5	dB
3rd	-95.2	-88.5	-37.3	-13.2	dB
4th	-104.9	-89.1	-41.2	-18.5	dB
5th	-102.9	-101.4	-46.6	-28.6	dB
T.H.D.	0.0037	0.0096	2.53	12.0	%
T.dB	-88.6	-80.3	-31.9	-18.4	dB

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.4 dB	-0.3 dB
5kHz	-4.53dB	-4.5 dB	-4.3 dB
16kHz	-9.04dB	-9.3 dB	-9.1 dB

The distortion levels at 0 dB are 0.0034% at 100 Hz, 0.0021% at 1 kHz and 0.0027% at 10 kHz. The distortion level increases as the signal level decreases, so that at -80 dB (reference 0 dB level) the distortion level is 12%. This was just about the highest level of distortion recorded from any machine, although I must make it clear that these distortion levels would be totally inaudible and during the subjective testing we could not detect them.

Functionally, the performance of the Akai CD-D1 could not be faulted and I really liked the neat control format and the multiple design features. The best demonstration discs produced a scintillating sound which impressed everybody who heard it.

Hitachi DA-1000

The Hitachi DA-1000, the smallest CD player I reviewed, has a layout for the controls which is quite different to the other machines.

The disc is loaded into the disc holder in the centre of the front panel using an electronic switch for opening and closing the holder.

At the extreme left hand side of the fascia is a triangular power on-off switch with the visual displays located in four rows below. At the top is the quasi-analogue digital display which indicates the position of the laser pickup in units of five minutes. Below this is the time counter with a display in minutes and seconds showing either total playing time or elapsed time.

Further down are two LEDs which indicate programme 'play' or 'repeat'. Adjacent to this are two numerical displays indicating the total number of programmes on the disc and the programme number which has been selected or is being searched for by the random memory programme.

The bottom row of lights is a unique feature. Ten LEDs indicate the output volume into either the headphones or the coaxial line sockets so that you can see not

only the level of sound but also if the amplifier is likely to distort or overload.

Immediately to the right of the hinged disc-well door is a vertical array of eight push-buttons. The top one is the 'programme' button which is for programming the random memory search function. Below this are two buttons labelled '10' and '1'. The idea is that you press the '1' button as many times as the number that you want and press both the '10' and '1' buttons for numbers from 11 upwards.

The 'clear' button will delete a selected programmed track. The 'call' button allows you to check the numbers of the programmed tracks and pressing the 'repeat' button will repeat the whole disc.

The bottom two buttons replace the conventional volume control, allowing you to electronically increase or decrease the amplification which is indicated on the array of LEDs at the bottom left hand corner of the unit.

The only controls which I did not appreciate were the '10' and '1' buttons

HITACHI DA-1000

Distributor:
Hitachi Sales Australia Pty Ltd
153 Keys Rd
Moorabbin Vic. 3189
(03)555-8722

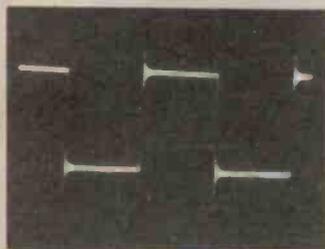


SIGNAL-TO-NOISE RATIO

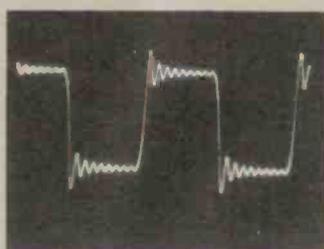
Without Emphasis 94.0dB(Lin) 98.5dB(A)
With Emphasis 100.4dB(Lin) 103.3dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	-91.6	-93.8
1kHz	-97.1	-98.6
10kHz	-91.1	-93.1
20kHz	-83.6	-88.9



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB

	100Hz	1kHz	10kHz	
2nd	-94.8	-99.2	-86.5	dB
3rd	-84.2	-105.1	out	dB
4th	-122.0	-116.9	of	dB
5th	-101.0	-103.8	Range	dB
T.H.D.	0.0064	0.0014	0.0047	%

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	-101.4	-97.4	-	-	dB
3rd	-98.4	-79.5	-34.3	-21.7	dB
4th	-104.7	-95.9	-	-	dB
5th	-96.4	-87.5	-44.6	-20.5	dB
T.H.D.	0.0022	0.012	2.01	12.5	%
T.dB	-93.15	-78.4	-33.9	-18.06	dB

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.4 dB	-0.3 dB
5kHz	-4.53dB	-4.9 dB	-5.0 dB
16kHz	-9.04dB	-8.7 dB	-8.8 dB

which create more work than the equivalent key pad display used on the other CD players.

On the right hand side of the unit is a rocker-bar which provides 'fast back' and 'fast forward' for searching out sections of the track. Immediately below is a very large 'play' control and another rocker bar. One end of the rocker bar allows you to memorise any point on the track to which you can return at any time by pressing the 'fast back' control. The disc will then continue playing from that position which is noted by the memory control.

At the other end of the lower rocker bar is the 'pause' control and below it is the 'stop' button. In the bottom quadrant of the unit is the electronic 'open' and 'close' button with a tip-ring-and-sleeve socket inserted into it for the headphones.

On the back of the unit are two sets of gold plated contacts; one is for fixed level output and the other is for variable level output which is controlled by the electronic volume controls on the front panels.

The performance of this unit is also very good with a frequency response of ± 0.2 dB from 20 Hz to 20 kHz. The total harmonic distortion levels at 0 VU are 0.0064% at 100 Hz, 0.0014% at 1 kHz and 0.0047% at 10 kHz. The distortion level increases slowly down to -60 dB where it reaches a significant level of 2%, which then rises to 12.5% at -80 dB.

The signal-to-noise performance is 98.5 dB(A) without emphasis and 103.3 dB(A) with emphasis. The channel separations up to 10 kHz are all better than -90 dB while at 20 kHz the separation drops down to -83.6 dB and -88.9 dB for the left and right channels respectively.

I was impressed by the way in which this small, neat unit can sit on a shelf next to a bed, so that with a set of headphones it can create a delightful bedroom music centre. If I was to buy a CD player for this specific role then the Hitachi unit would be my first choice as its visual indications and controls really lend themselves to this particular role.

Pioneer P-D1

The Pioneer P-D1 offers a wide range of ergonomic features which I liked. Pioneer, like Akai, have also chosen to electronically open the disc door but to manually close it, a concept which I strongly support.

By placing the disc door at the extreme left hand side of the player the designers have achieved a very pragmatic fascia layout. In the middle of the fascia is an illuminated power on-off switch while to the right are the display and control modules.

The display module features 'programme check' and 'total time' switches at the top. Below these are LEDs indicating the function of the switches and a numeric display indicating the programme sequence number.

Immediately below this are two, double digit displays to show the time in minutes and seconds and the phrase numerals for a section of a number. These are dependent on the settings on the controls on the right hand side.

PIONEER P-D1



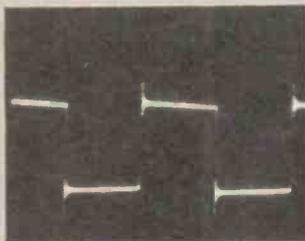
Distributor:
Pioneer
178 Boundary Rd
Braeside Vic. 3195
(03)580-9911

SIGNAL-TO NOISE-RATIO

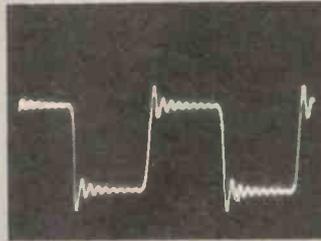
Without Emphasis 90.0dB(LIn) 96.5dB(A)
With Emphasis 96.0dB(LIn) 100.5dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	-114	-100.5
1kHz	-114	-99.9
10kHz	-95.5	-89.5
20kHz	-87.3	-83.7



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB

	100Hz	1kHz	10kHz	
2nd	-96.7	-99.7	-89.3	dB
3rd	-93.8	-	out	dB
4th	-114.9	-112.4	of	dB
5th	-117.0	-118.3	Range	dB
T.H.D.	0.0025	0.0011	0.0034	%

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	-109.4	-	-	-	dB
3rd	-101.4	-90.7	-47.0	-26.8	dB
4th	-113.2	-	-	-	dB
5th	-111.1	-95.2	-53.2	-23.8	dB
T.H.D.	0.00098	0.0034	0.49	7.9	%

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.3 dB	-0.3 dB
5kHz	-4.53dB	-4.7 dB	-4.6 dB
16kHz	-9.94dB	-9.6 dB	-9.8 dB

At the bottom of the visual display section are five rectangular LEDs to display the play-back mode. The functions offered are matched by the controls on the right hand side of the console. 'Index scan' allows you to sample the first seven seconds of each song on the disc, 'music repeat' just plays one song, 'one side repeat' is self explanatory, 'searching' illuminates during the searching or 'skipping' sequence and 'programme' indicates normal playing.

Four main controls, located in the middle of the display/control module, are the 'eject', 'play', 'pause' and 'stop' buttons.

This group of simple controls means that anyone can use the player without reference to the other controls or displays. They constitute an excellent ergonomic feature and their position and layout will endear themselves to sales people wishing to make a strong and sensible sales pitch to someone who is not quite 'with it' in the digital technology age.

A 10-button key pad is for entering song numbers or time and 'phrase' data for

searching and finding an exact spot within a section of the disc. The 'skip forward' and 'backwards' button allows you to advance forward or backwards to the start of the next or previous number.

The technical performance of the Pioneer player is excellent with extremely low distortion levels; measured at 0 VU they are 0.0025% at 100 Hz, 0.0011% at 1 kHz and 0.0034% at 10 kHz. At -60 dB the distortion figures are still less than 0.5% and they only climb to 7.9% at -80 dB.

The frequency response is flat from 20 Hz to 20 kHz except for an excursion of -0.7 dB at 18 kHz.

The signal-to-noise ratio without emphasis is 96.5 dB(A) and with emphasis is 100.5 dB(A). The channel separation is typically -100 dB to 1 kHz, just under -90 dB to 10 kHz and -83.7 dB at 20 kHz.

When we received the new Philips compact test discs we evaluated three of the machines for intermodulation distortion, using the Philips test discs. The Pioneer

player produced the best results with an intermodulation distortion which was at least 3 dB lower than the next best unit, under any test condition and at any level or frequency.

I spent a lot of time listening to compact discs on the P-D1, set up with either a complete Pioneer System or with my monitoring system at home. I found it a delight to use and a great pleasure to listen to.

Sanyo DAD 8

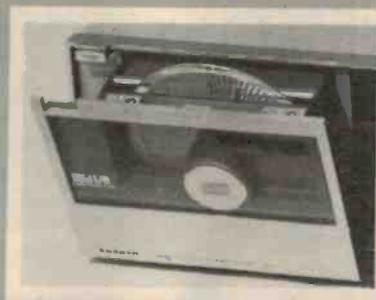
The Sanyo DAD 8 is a very small, lightweight player.

The front fascia is dominated by the disc holder door on the left hand side with a power on-off switch at the top left hand corner. To the right of the door is a display module, flanked on the right by the control module.

The display module has three separate display areas. At the top is the real time counter which indicates the time of each

SANYO DAD 8

Distributor:
Sanyo Australia Pty Ltd
225 Miller St
North Sydney NSW 2060
(02)428-5822

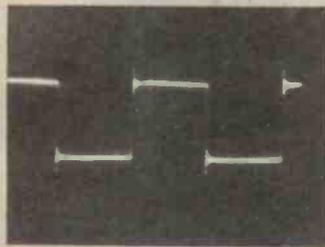


SIGNAL-TO-NOISE RATIO

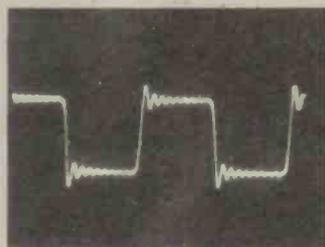
Without Emphasis 90.0dB(Lin) 93.6dB(A)
With Emphasis 95.0dB(Lin) 97.5dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	-104.0	-102.0
1kHz	-94.6	-93.1
10kHz	-73.8	-74.5
20kHz	-70.4	-69.3



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB(Maximum)

	100Hz	1kHz	10kHz	
2nd	-86.9	-86.2	-85.0	dB
3rd	-87.9	-98.8	out	dB
4th	-	-	of	dB
5th	-111.6	-109.0	Range	dB
T.H.D.	0.005	0.005	0.0056	%

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	-97.5	-	-	-	dB
3rd	-91.4	-86.0	-40.6	-27.0	dB
4th	-	-	-	-	dB
5th	-99.9	-90.3	-	-22.0	dB
T.H.D.	0.00032	0.0059	0.93	9.1	%
T.dB	-89.9	-84.6	-40.6	-20.8	dB

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.1 dB	-0.1 dB
5kHz	-4.53dB	-4.3 dB	-4.4 dB
16kHz	-9.04dB	-9.5 dB	-9.5 dB

selection or the total playing time in minutes and seconds.

Below this is the multi-display window which provides information on the third-level display. This will be either the music number and index number of the music being played now; the music number being played now and the next number to be played, or during programming, the music number to be played and the order in which it will be played.

Below the display module are the ten soft touch keys used to designate the selection number when programming your music sequence.

On the extreme right hand side of the fascia are the primary and secondary controls: 'real time counter' switch; 'open/close' switch; 'fast forward' switch; 'return' switch that allows you to jump to the next or previous number.

Below these are controls that only a few of the other units offer: 'fast forward'; 'fast reverse'; 'play'; 'pause'; 'stop'; repeat.

At the bottom right hand corner are the

soft touch switches for 'recall', 'memory' to accept the encoded numerical number, 'programme play', 'programme write/display', 'memory clear', and 'programme clear'. There is also a volume control and a headphone socket.

The functional performance of the Sanyo unit is generally good although the measured values just exceed the typical values stated in Table 1. The distortion figures are typically 0.005% at 100 Hz, 1 kHz and 10 kHz, measured at 0 VU. These figures climb to 0.93% at -60 dB but are still only 9.1% at -80 dB.

The frequency response is flat except for two excursions, +0.3 dB at 100 Hz and -0.8 dB at 18 kHz.

The signal-to-noise ratio is 93.6 dB(A) without emphasis and 97.5 dB(A) with emphasis. The channel separation droops quite noticeably with increasing frequency, being greater than -102 dB at 100 Hz, -93 dB at 1 kHz, -74.5 dB at 10 kHz and -69.3 dB at 20 kHz.

The performance of the unit is good

although I believe I could hear a difference in the characteristics of the sound when compared to some of the other units during A-B testing.

The Sanyo unit is a particularly neat unit which most people would appreciate but the layout and functions are not quite as straightforward as some of the other units. It is, however, the least expensive of the six units and consequently still has an awful lot to offer in terms of value for money.

Sony CDP-101

The Sony CDP-101 is a most impressive CD player and is different to the other five CD players in a number of discrete ways. It has a horizontal playing format for the disc and, except for Yamaha, the other four units reviewed have a vertical format.

The Sony CDP-101 also has an infrared remote control which is a delight to use.

The neat, black unit has an interesting appearance. The cassette well slides out with a gentle whirring sound rather than

SONY CDP-101



Distributor:

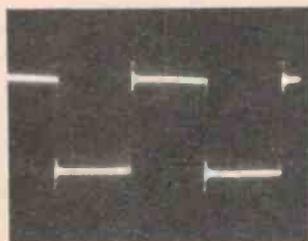
Sony
453 Kent St
Sydney NSW 2000
(02)266-0655

SIGNAL-TO-NOISE RATIO

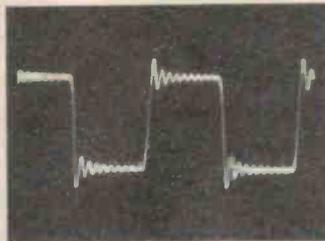
Without Emphasis 92.5dB(Lin) 99.0dB(A)
With Emphasis 109.0dB(Lin) 113.0dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	>-114.0	-100.5
1kHz	>-114.0	-99.0
10kHz	-95.5	-89.4
20kHz	-87.3	-83.7



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB(Maximum)

	100Hz	1kHz	10kHz	
2nd	-101.8	-109.5	-97.1	dB
3rd	-86.3	-106.3	out	dB
4th	-112.3	-	of	dB
5th	-112.5	-	Range	dB
T.H.D.	0.0048	0.0059	0.0014	%

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	None	-	-	-	dB
3rd	Detectable	-	-45.6	-34.3	dB
4th	at this-	96.5	-	-	dB
5th	level	-	-50.3	-26.1	dB
T.H.D.	-	0.0015	0.56	5.3	%
T.dB	-	-96.5	-45.0	-25.5	dB

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.1 dB	-0.1 dB
5kHz	-4.53dB	-4.6 dB	-4.5 dB
16kHz	-9.04dB	-9.8 dB	-9.6 dB

opening out on a hinge, as do the other units. All you need to do is touch the 'open-close' button on the front of the sliding shelf and the tray slowly slides out. You then gently drop the compact disc onto the specially shaped tray with its hollow centre, touch the 'open-close' button again, or touch the 'play' button, and the tray closes to complete the sequence.

To the left of the tray is the power on-off switch, the 'timer play' switch, the 'headphone level' control and the headphone tip-ring-and-sleeve socket.

On the right hand side of the disc compartment is a display window which provides four sets of information. The 'disc set' indicator flickers while the disc compartment is moving and illuminates the 'disc set' wording when the disc is ready to play. Next to this display is the 'track number' indicator and the time counter which shows elapsed time or remaining time on the disc.

To the right of these displays is the remote sensor detector for the remote

control, displaying a light to indicate that it has responded to a remote instruction.

Below the display window is the 'reset' button and some of the most unusual controls found on any of the CD players. One button will repeat the program actually being played and the next button will repeat the whole disc on a single cycle basis.

The 'A-B' button allows the replay of selected sections between any point designated 'A' and any other point designated 'B'. I must admit that after you have used this function the first time you may never want to use it again. However, it does provide a powerful facility for those people who want such an unusual capability.

Actually the 'A-B' facility was very useful at the beginning of this year when we tested the first Sony CD player in the country (see ETI Feb 1983). It was long before the Sony test discs became available, so the 'A-B' facility was used to help us assess the dynamic characteristics of small samples of recorded material.

The 'clear' button will clear the 'A-B'

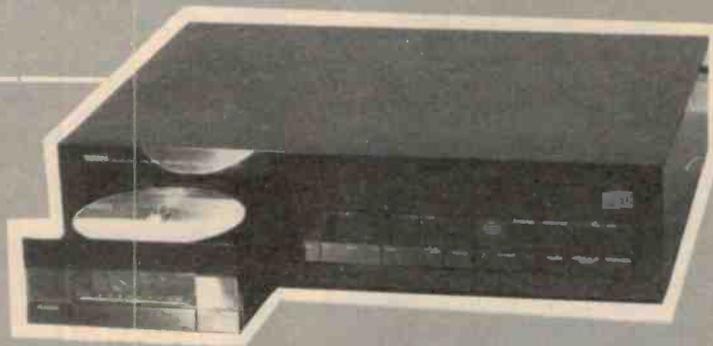
function.

Below these special controls are the normal main controls of 'play' and 'pause'. There are two large keys with double arrows for fast forward and fast reverse. Below these are four smaller buttons which can be used while the programme is being played to provide rapid forward or reverse searching at three times and at ten times the normal playing speed. None of the other CD players reviewed offered this facility. Conversely, most users may not appreciate or want to use this facility.

On the rear panel of the unit there is an 'auto pause' switch to automatically produce pauses between numbers and an 'anti-shock' switch to provide additional compensation for locations subject to high vibration. A 'beep buzzer' on-off switch under the player responds to the remote control unit.

Unlike all the other units, the Sony unit does not incorporate a transit screw system for locking down the laser disc traversing head.

YAMAHA CD-1



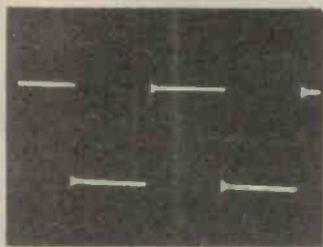
Distributor:
Rose Music
28 Kent St
Belmore NSW 2142
(02)750-8999

SIGNAL-TO-NOISE RATIO

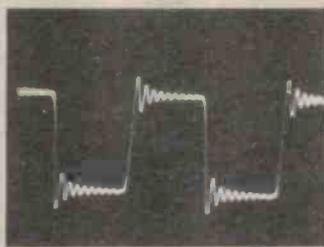
Without Emphasis 94.0dB(Lin) 99.0dB(A)
With Emphasis 99.0dB(Lin) 104.0dB(A)

CHANNEL SEPARATION

FREQUENCY	RIGHT INTO LEFT dB	LEFT INTO RIGHT dB
100Hz	-100.8	-98.3
1kHz	-101.1	-99.2
10kHz	-86.5	-90.9
20kHz	-78.1	-90.6



100 Hz



1 kHz

DISTORTION

AT MAXIMUM OUTPUT LEVEL = 0dB(Maximum)

	100Hz	1kHz	10kHz	
2nd	-91.3	-91.0	-85.3	dB
3rd	-89.3	-	-	out
4th	-	-	-	of
5th	-	-	-	Range
T.H.D.	0.0044	0.0028	0.0054	%
T.dB	-87.2	-91.0	-85.3	dB

AT INDICATED LEVELS FREQUENCY = 1kHz

	Level = -10dB	Level = -20dB	Level = -60dB	Level = -80 dB	
2nd	-92.4	-88.5	-	-29.5	dB
3rd	-	-85.2	-39.1	-23.5	dB
4th	-99.8	-96.4	-	-33.6	dB
5th	-	-88.2	-46.3	-23.5	dB
T.H.D.	0.0026	0.0078	1.21	10.2	%
T.dB	-91.6	-82.1	-38.3	-19.8	dB

EMPHASIS

Frequency	Recorded Level	Output Level (Left)	Output Level (Right)
1kHz	-0.37dB	-0.2 dB	-0.3 dB
5kHz	-4.53dB	-4.8 dB	-5.0 dB
16kHz	-9.04dB	-8.9 dB	-9.2 dB

The technical performance of the Sony player is particularly good. The distortion figures, measured at 0 VU, are 0.0048% at 100 Hz, 0.0059% at 1 kHz and 0.0014% at 10 kHz. The measured distortion levels are still exceptionally good at -60 dB where a very low figure of 0.56% is produced, and at -80 dB the distortion is only 5.3%. The intermodulation distortion is better than -73 dB re 0 VU.

The frequency response is flat until 5 kHz and then it gradually drops down to -1.7 dB at 18 kHz.

The signal-to-noise ratio without emphasis is 99 dB(A) and with emphasis it is good at 113 dB(A). The channel separation is better than -100 dB at 100 Hz, better than -99 dB at 1 kHz, better than -89 dB at 10 kHz and better than -83 dB at 20 kHz.

The Sony player is delightfully easy to use and has an exhilarating sound. It is clear that Sony has gone to extreme lengths to develop and produce what I consider to be an outstanding piece of engineering design.

Yamaha CD-1

The Yamaha CD-1 is based on an entirely different design philosophy to the other CD players. The major difference, and what the manufacturer claims is its most important feature, is the total duplication of the digital circuitry to achieve, say Yamaha, superior technical performance.

Other brands of CD players apparently use a single digital to analogue converter to convert the multiplexed analogue (audio) signal, which must then be demultiplexed into the left and right channels. Yamaha, however, uses a digital demultiplexing circuit prior to feeding the digital signals to two separate digital to analogue converters.

The major attribute claimed for this circuitry is a reduction of switching noise and distortion in the output. The disadvantage of this approach is more circuitry and the result is a much higher price for this unit, when compared to all of the other units reviewed.

The frontal appearance of the CD-1 is striking and attractive. Like the Sony player, it has a horizontal disc compartment which slides out under full electronic control, but it is even quieter than the Sony unit.

The front panel has the power on-off switch on the left hand side of the disc compartment. Adjacent to the switch is a direct analogue-type display showing the position of the recording head in terms of ten, six-minute increments.

To the right of the disc compartment are a series of bright red numerical displays showing the music sequence number and the time in minutes and seconds. The pre-programming data displays the next programming number, the music number and also the time in minutes and seconds for the following sections.

The primary controls, simpler and more straight forward than those on the other players are 'stop', 'play' that also doubles for 'forward' and 'reverse', 'fast forward' or 'fast rewind' and 'pause'.

The other controls provided for pre-programming are incorporated in an entirely separate motorised key tray which is located on the right hand side of the unit. These controls are recessed, right out of harm's way until you need them, and are opened by a separate 'open/close' button located on the right hand end of the fascia.

The added controls make it possible to programme up to fifteen selections in any sequence or combination. Unlike many of the other players, there are no long delays with this system, even when skipping from the first to the last selection on the disc. The unit also provides a very easy 'check' function for both verification of the programme sequence or for reprogramming that sequence to suit.

Like a few of the other units, in particular the Sony CDP-101 player, this unit provides a 'phrase' play-back capability where any segment of the disc, several selections of the disc or even a small section of a selection, can be programmed to play singly or repeatedly.

The performance of this unit is very good but is not, however, demonstrably superior to the other players. The measured frequency response is flat except for a +0.5 dB excursion at 7 kHz.

The distortion levels of 0 VU are 0.0044% at 100 Hz, 0.0028% at 1 kHz and 0.0054% at 10 kHz. These levels are still good at -60 dB where the distortion is 1.2% and at -80 dB the distortion rises to 10.2%.

The signal-to-noise ratio without emphasis is 99 dB(A) and with emphasis it is a very respectable 104 dB(A). The channel separation is better than -98 dB at 100 Hz and 1 kHz, better than -86 dB at 10 kHz and is -78 dB at 20 kHz.

The digital to analogue converter linearity is very good all the way to -60 dB and then has a slow but gradual droop to -90 dB. The unit has an excellent performance. However, the double digital conversion system does not seem to provide a measurable improvement in overall performance, compared with the other units evaluated.

The subjective performance and the practical use of this unit is absolutely first class. Hiding away the auxilliary programming and pre-programming functions is very sensible, but obviously an expensive approach.

Summary

The engineers at Philips in Eindhoven had a brilliant vision when they conceived the idea of the compact disc player. Fortunately, they realised that for it to work in practice they would need a Japanese partner to make sure that the concept became an industry standard.

The review has shown that there are considerable differences between each brand of player, in terms of functions, performance and flexibility in using the machines.

However, the cheapest player, which sells at a recommended retail price of \$1099, and the most expensive player, selling at almost twice that price, have objective performance figures which are disproportionately small, considering the difference in price. ●

TABLE 1

Track number	Signal	Level	Ch	Contents min sec, phrase	Purpose
1	1 kHz	0 dB	L&R	00M02S00F	Reference
2	20 Hz	"	"	02 02 00	Frequency Response
3	40 Hz	"	"	03 02 00	
4	100 Hz	"	"	04 02 00	
5	200 Hz	"	"	05 02 00	
6	500 Hz	"	"	06 02 00	
7	1 kHz	"	"	07 02 00	
8	5 kHz	"	"	08 02 00	
9	7 kHz	"	"	09 02 00	
10	10 kHz	"	"	10 02 00	
11	16 kHz	"	"	11 02 00	
12	18 kHz	"	"	12 02 00	
13	20 kHz	"	"	13 02 00	
14	1 kHz	0 dB	L&R	14 02 00	Linearity
15	"	- 1 dB	"	15 02 00	
16	"	- 3 dB	"	16 02 00	
17	"	- 6 dB	"	17 02 00	
18	"	- 10 dB	"	18 02 00	
19	"	- 20 dB	"	19 02 00	
20	"	- 60 dB	"	20 02 00	
21	"	- 80 dB	"	21 02 00	
22	"	- 90 dB	"	22 02 00	
23	Infinity Zero w/o emphasis		L&R	23 02 00	
24	" with emphasis		"	24 02 00	
25	400 Hz + 7 kHz (4:1)	0 dB	L&R	25 02 00	1 M of 2 Signals
26	"	- 10 dB	"	26 02 00	
27	19 kHz + 20 kHz (1:1)	0 dB	"	27 02 00	
28	"	- 10 dB	"	28 02 00	
29	100 Hz	0 dB	L	29 02 00	Channel Separation
30	1 kHz	"	"	30 02 00	
31	10 kHz	"	"	31 02 00	
32	20 kHz	"	"	32 02 00	
33	100 Hz	0 dB	R	33 02 00	
34	1 kHz	"	"	34 02 00	
35	10 kHz	"	"	35 02 00	
36	20 kHz	"	"	36 02 00	
37	100 Hz Square Wave		L&R	37 02 00	Transient Response
38	1 kHz Square Wave		"	38 02 00	
39	1 kHz w/emphasis	- 0.37 dB	L&R	39 02 00	Emphasis
40	5 kHz w/emphasis	- 4.53 dB	"	40 02 00	
41	16 kHz w/emphasis	- 9.04 dB	"	41 02 00	
42.99	1 kHz	0 dB	L&R	42 02 00	Reference and TNO check
				(each TNO is same signal, with duration of 4 seconds)	
				45 54 00	LEAD OUT SIGNAL

RECORDING TIME: TNO 1) 1min 56sec; TNO 2.41) 56sec each;
TNO 42.99) 4sec each, total 3min 52sec.
PAUSE TIME: TNO 1) 2sec; TNO 2.42) 4sec each; 43.99) none.
*other channel is infinity zero

Sony Test Disc. Signal performance section.

TEST DISCS EXPOSED

If there's one thing that's harder to get at the moment than a compact-disc player, it's a compact-disc test record. Philips released its latest three-disc set, *Audio Frequency Test Samples, Numbers 3, 4 and 4A*, in Europe last November, and Sony released its improved *CD Test Disc Type 3 for Signal Performance Testing and Optical Readout Testing* in Japan only a few months later. We finally managed to get hold of all of them...

The Sony Test Disc Type 3 has a series of formatted signal bands, designed to test the CD player's audio output specifications. The material used in the disc and the designated measurements are those specified in the CD digital audio system Red Book, resolved and accepted by Sony and Philips in May 1982.

The test signals have been recorded from digital sources whose frequency accuracy is precise to one part in 10⁹. Both companies claim the level setting accuracy for 16-bit resolution is accurate to ±0.1 dB. The discs have time signal data from the starting position of each track, even during the pause signals. Therefore, the time in minutes and seconds from start to finish and from the start of any track is also encoded for those CD players which provide time, number and phrase information.

Both Sony and Philips use spot frequency checks, starting at 20 Hz and finishing at 20 kHz, to evaluate frequency response, total harmonic distortion and modulation noise of a player. Philips also provides a sweep covering 20 Hz to 20 kHz. Spot frequencies suit a technician better than sweep frequencies, however, most laboratories would prefer a swept signal format covering the range 10 Hz to 20 kHz. This would be more suitable as there are thousands of level recorders from Bruel and Kjaer, General Radio and Neutrik available world wide, which could track a continuous logarithmically swept signal.

While the evaluation of frequency response is very straightforward, given the availability of an audio analyser, precision audio voltmeter or a level recorder, the same cannot be said for the ease of measuring total harmonic distortion and certainly not for measuring modulation noise. Our tests have shown that at 0 VU the best of the CD players produces distortion components as low as 0.0002%, which can also be expressed as two parts per million THD, or distortion products to the order of -114 dB. There are very few systems available which enable you to measure distortion components as low as these.

Our approach is to use a special multiple notch filter, calibrated at

the fundamental, second, third, fourth, fifth and sixth harmonics. Its fundamental rejection is 100 dB while the rejection at the second and higher order harmonics ranges between 10 dB and 3 dB. This approach enables us to measure the distortion components as low as -130 dB, which is approaching what I regard as the ultimate figure for measurable distortion.

The signal track numbers 14 to 22 on the Sony test disc provide reference signals at 1 kHz with simultaneous left and right channel modulation at 0, -1, -3, -6, -10, -20, -60, -80 and -90 dB. It is important to note that with a dynamic range in excess of 90 dB encoded on the disc, and with insignificant distortion at the highest possible sound levels, it is only in the realm of encoding linearity or decoding linearity that you are likely to have your first order differences between one CD player and the next.

That is, if the CD player displays a significant non-linearity in the digital decoding circuitry, then there is a possibility when comparing the same programme content played by two CD players, that you will hear a subjective difference.

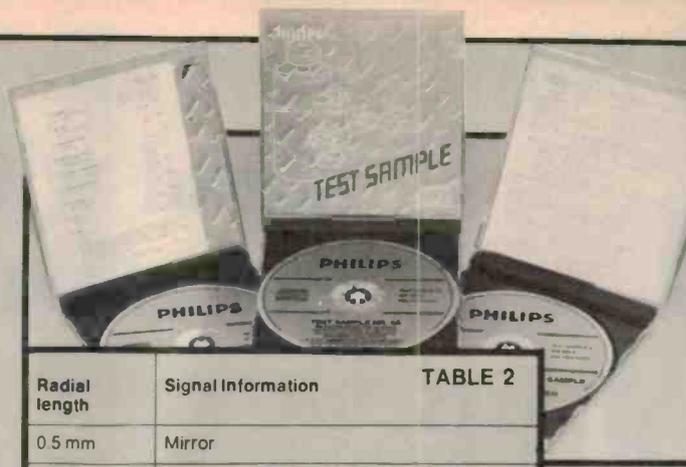
All CD players show varying degrees of non-linearity in the dynamic region from -60 dB to -90 dB. It is in this region that both the Sony and Philips test discs have provided too few bands for testing. Both manufacturers can argue that the resolution I would like to see on the test discs is commercially unwarranted, but I would still like to see the additional data encoded.

It is particularly important to note that at -90 dB the residual dynamic range available on the CD players' and the linearity of the encoding system originally used to manufacture these test discs, must be severely limited. Therefore, any CD player that provides a total harmonic distortion level of better than five or six per cent at the -80 dB level (relative to 0 VU) is an exceptional piece of equipment.

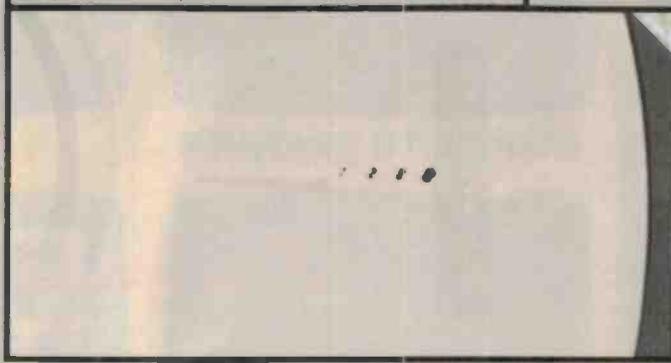
Compact disc players which achieve an encoding error of less than 1 dB at the -80 dB level and less than 2 dB at the -90 dB level are an exceptional piece of equipment.

Tracks 23 and 24 and 39 to 41 on the Sony disc provide test signals with and without emphasis. This enables us to determine whether the de-emphasis circuits are responding accurately to the original pre-emphasis encoded on the discs. This is an important requirement as if the de-emphasis is wrong then the second order colouration of the test signals will also affect your ability to discriminate between one CD player and the next.

Tracks 29 to 36 on the Sony disc provide a series of left and right channel encodings to allow the direct evaluation of channel separ-



Radial length	Signal Information	TABLE 2
0.5 mm	Mirror	
1 mm	Multiburst Signal 100 kHz, 1.4 MHz, 200 kHz, 1.3 MHz, 300 kHz, 1.2 MHz, 400 kHz, 1.1 MHz, 500 kHz, 1 MHz, 600 kHz, 700 kHz, 800 kHz (repeat signals from 100 kHz to 800 kHz) Duration of each signal is 8.2msec.	
0.5 mm	Mirror	
1 mm	Duty Cycle Measurement Signal F ₀ : 750 kHz, F ₁ : 100 kHz, with different amplitude of -20 dB after limiter	
Outer Section	Mirror	
Sony test disc. Optical readout section.		



ation. This is important for evaluating the overall decoding quality of the CD player. With distortions of parts per million and dynamic ranges of greater than 90 dB, one must expect channel separations approaching the dynamic range of the disc, even if the original commercial software signal content does not approach half those figures.

Though similar in many ways, there are also striking differences between the Philips and Sony test discs. The first difference is that track No 2 on the Philips disc provides a 20 Hz to 20 kHz sweep. This matches the capability of Bruel & Kjaer level recorders, enabling direct recording of frequency response on a frequency calibrated level recorder.

The second difference between the Philips and Sony test discs is their choice of frequencies for evaluating harmonic distortion. Philips uses frequencies of 41, 101, 997, 3163, 6363, 10 007, 16 001 and 19 997 Hz instead of the conventional rounded-off figures to which we have become accustomed.

The advantage of using these

frequencies lies in their ability to reject and discriminate against main hum components and other interacting frequency components associated with the typical CD player. These particular signals and frequencies are repeated at -24 dB and also at -30 dB.

Linearity measurements are provided with a frequency of 997 Hz at 0, -1, -6, -12, -24, -60, -80 and -90 dB, for the left and separately for the right channel. These levels are included on both the Sony and Philips discs which we tested on three CD players with very similar results.

The feature I was most impressed with was that tracks 12, 13, 14 and 15 provide a swept test signal with a logarithmic sweep rate extending from 300 Hz to 20 kHz. These tracks contain two frequencies recorded at the same level so that the value of $F_2 - F_1$ is a constant 70 Hz. By passing this signal through a heterodyne analyser with a 3 Hz band width (and a signal-to-noise ratio of better than 70 dB) I was able to compare the performance of three CD players.

This signal showed how good the

CD players really are at medium to high signal levels. It is in the range of -60 dB to -90 dB re 0 VU that we are aware of the increase in non-linearity of the digital to analogue encoders, and of the increase in total harmonic distortion (THD).

Philips provide more general information on the importance of the test equipment to be used by their technical staff in conjunction with the CD test record No 3. They provide block schematics of this equipment, as well as nominating the types of analysers for Inter-modulation distortion.

One statement that continually catches my eye is "because the rotational control on CD players uses circuitry with crystal accuracy, no measurements are required or necessary for wow and flutter". Though this may be true with a new and functional CD player, it is questionable whether it would apply to an old and tired CD player.

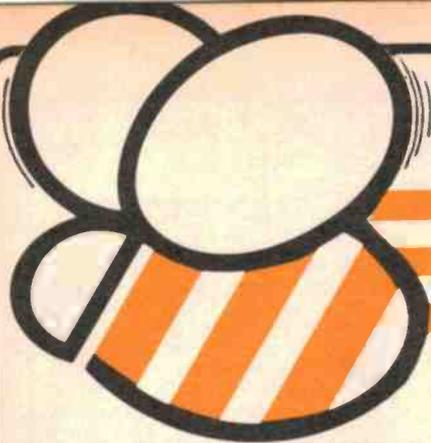
Aside from the technical importance of the discs, I found the Philips disc No 4 to be a collector's delight. It contains a range of exquisitely recorded classical and pop music, from Handels Water Music to Elton John and the Bee Gees.

Philips' disc No 4A has the same content but is supplemented by 'encoded defects'. These are printed on the surface as strips of thin black lines which simulate fingerprints and black spots of varying diameter. The intention is to test the ability of CD players to play over interruptions to their content without audible error. Unfortunately, this disc arrived too late for this month's test programme, and we couldn't evaluate this feature in all the players. However, both the Sony CDP-101 and the Pioneer P-D1 were able to track all of these man-made faults without problems. A badly scratched disc provided by Pioneer Australia wouldn't track in the worst scratched areas.

In future test discs I would like to see an expanded number of reference test levels between -60 dB and -90 dB, and the introduction of test frequency signals as specified for the IEC 'total difference frequency distortion meter'. Many laboratories now use this Australian system to measure the distortion characteristics of the latest generation of advanced performance amplifiers and tape recorders. It has obvious applications to testing CD players and the Sony and Philips organisations should take note of its advantages. With these refinements I believe that Sony and Philips will have 'covered all the bases'.

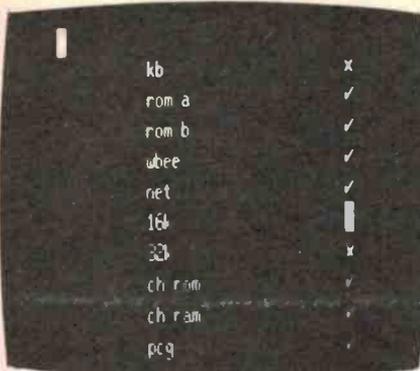
Compact disc players have not yet revealed any unusual faults, but it is clear new test records will be released which will make it easier to find those faults, as well as making the complex evaluation task more simple and straightforward.

▲ Above: The Philips set of test discs.
▼ Below: Disc with 'encoded defects'.

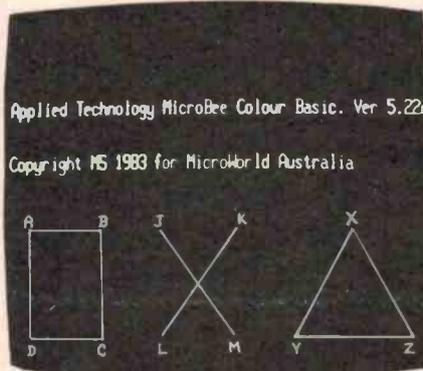


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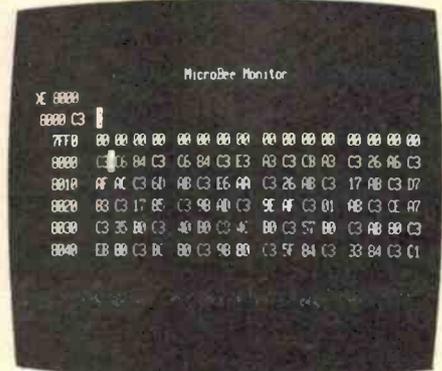
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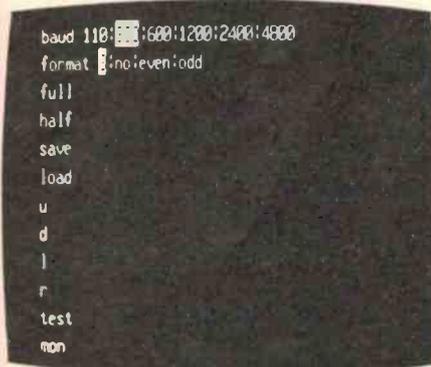
SELF TEST.



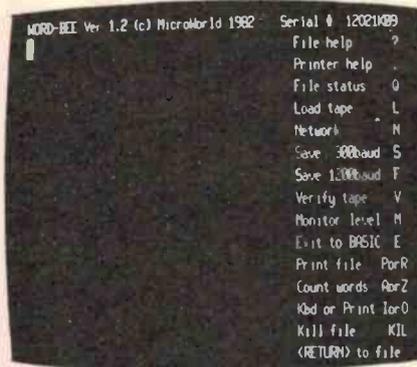
BASIC WITH GRAPHICS



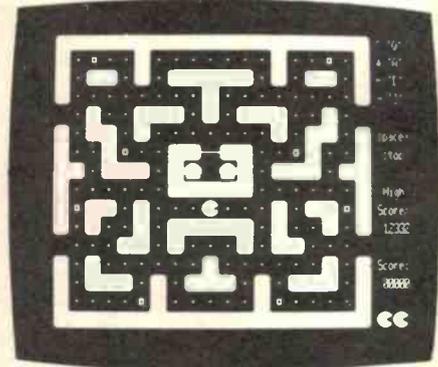
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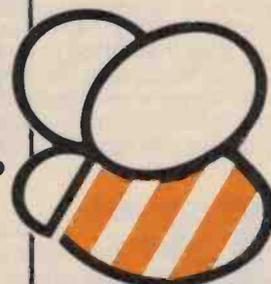


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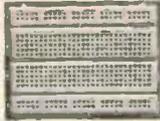
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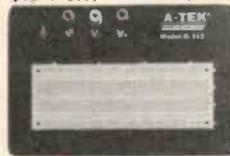


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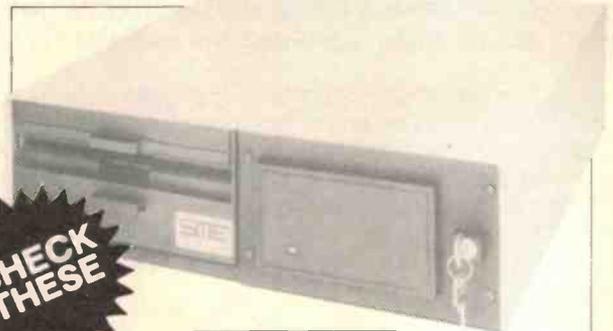
Built around Tandem's sturdy TM603S mini-Winchester drive coupled to an 8" QUME floppy the HDU-1001 gives you the storage capacity you need to handle large data base applications; the ability to transfer data to and from the hard disk; and back up facilities all in one compact package.

Employing the latest bit slice technology the HDU-1001's Winchester drive controller offers rapid reliable data collection, micro diagnostics for fault finding and error detection, plus the option to add another 10Mb of storage with the addition of another Winchester drive.

Housed in a rugged steel based, aluminium bodied enclosure the HDU1001 is rack-mount compatible and is supplied fully tested and ready to go to work for you ... hard.

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FEATURES

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- 1Mbyte 8" double sided floppy disk.
- Internal Winchester controller.
- High speed data throughput.
- Very quiet operation.
- Separate 50 way connector interface.
- CP/M 2.2 and MP/M 2.2 available.
- Designed and manufactured in Australia.



QDP MULTI-USER SYSTEM

A computer system that 'offers more user friendliness' and better computing power for a lower cost for both single- and multiple-terminal systems, is the positioning claimed for the QDP 300 series microcomputer, released in Australia by Insystems.

The QDP, manufactured by Quasar Data Products, of Cleveland, Ohio, is possibly the fastest Z80 computer yet released, but sidesteps many of the complexities normally associated with the CP/M and MP/M operating systems.

The QDP system options include one to four terminals, twin 20 cm 1.2-megabyte floppy disk

drives, or a floppy and a 10- or 15-megabyte internal Winchester drive and both CP/M and MP/M operating systems, with expansion boards for extra RAM and 16-bit processors. It also has a battery backed real-time clock.

The CP/M QDP comes with its own word-processing, spelling, data base and financial spreadsheet software, along with a number of other utility programs.

One of these is Systat which, apart from telling the user how the system is set up, also keeps a record of all disk errors during normal disk operations.

The system is fully CP/M and

MP/M compatible, allowing it to use most software written under these common systems, but it also contains an extremely friendly menu program to buffer new users from the more complicated aspects of the operating system.

Expansion slots have been left for new boards which will be available later this year. These will include a high-capacity RAM card, which will simulate an extremely fast disk drive, and a 16-bit computer card built on the 80186 chip.

For further details, contact Insystems, 337 Moray Street, South Melbourne Vic. 3205. (03)690-2899.

HIGH-SPEED JOYSTICK

Discwasher, the American company previously associated with record-cleaning accessories, has expanded its product range to cater for the video game and computer accessory market.

Heading the new range is the Pointmaster, a joystick that plugs into Atari and Commo-

dore VIC-20 game centres. It features a high-speed thumb trigger, comfortable handgrip, self-centring mechanism and a 1.5 m cord. It costs about \$29.99.

The manufacturer claims the Pointmaster has a very fast reaction time, enabling the operator to achieve much higher

game scores than normal.

Also available is a rapid-fire adaptor (\$14.99) which allows the joystick to be fired continuously, like a machine gun.

The Discwasher range is handled in Australia by Arena Distributors, 642 Albany Highway, Victoria Park WA 6100. (09)361-5422.

MYER LOOKS TO FUTURE

The Myer Emporium, which started its computer and business centres with the opening of the Melbourne centre last February, has confirmed that it will be opening more centres in the coming months.

Centres have already been opened in Sydney, Brisbane, Adelaide and Perth, as well as Melbourne.

Since the initial five centres were opened, Myer has closely observed their own operation, while enjoying "excellent" trading. In the four and a half months of trading up until the end of June, the Myer Computer and Business Centres reported a turnover of more than \$2.25 million.

Sales were 90% computer-related products and 10% business equipment products.

The main market thrust has been to corporations, small businesses and middle management.

Recently, Myer has been negotiating to secure a hand-held computer of "excellent quality and for extremely good value". The company hopes to make the computer available by mid-September.

For further details, contact Myer Computer and Business Centre, 275 Lonsdale Street, Melbourne Vic. 3000. (03) 661-3342.

NEW SLANT ON VDUS

AED Microcomputer Products now supplies a general-purpose swivel and tilt VDU monitor base.

The rugged unit, which is designed to improve the ergonomic presentation of existing monitors, in particular BMC and Sanyo styles, can be used with the majority of popular video monitors.

For more details, contact AED Microcomputer Products, 130 Military Road, Guildford NSW 2161. (02) 681-4966.

ZILOG DEVELOPS NEW 32-BIT MICROPROCESSOR

A new 32-bit microprocessor that offers on-chip cache and memory management, and which can execute up to five million instructions per second, has been announced by Zilog.

The Z80,000 CPU features full 32-bit architecture and implementation, a complete 32-bit instruction set, 32-bit internal and external data paths, and full support for all 32-bit data types. The chip is fully compatible with Zilog's Z8000 CPU family, but offers greater computer power and applications flexibility.

The chip also has four gigabytes of directly addressable memory, and features three selectable modes of address representation: 32-bit linear, 32-bit segmented and 16-bit compact.

According to Zilog, the Z80,000 CPU can execute up to five million instructions per second via a 'pipelined' scheme which allows more than one instruction to be executed at a time.

Designed for clock speeds

ranging from 10 to 25 MHz, the chip can operate as fast as one instruction per processor cycle. Prototype performance tests have yielded an average of 2.2 cycles to execute all instructions, including jumps, multiples and divides, and an average speed of 3.4 cycles in instances of cache misses and memory bus transactions.

The Z80,000 gives users of Zilog's Z8000 family of 16-bit microprocessors a natural migration path to a 32-bit performance, because the new chip's software is a binary-compatible extension of the Z8000 CPU's, and upgrading to the new chip requires no recompiling or program changes.

It uses the Zilog Z-BUS, an advanced chip interconnect protocol used by all Zilog devices introduced since 1979, and works with all Z8000 peripherals.

For more information, contact Zilog Corporation, 1315 Dell Avenue, Campbell, CA 95008, United States.

DIRECT-CONNECT MODEM

A new direct-connect 300 bps modem that is no taller than a 50-cent piece, and fits under the base of a telephone, has been released by Electromed.

Called the Sendata 300, the modem is installed simply and does not require any operator training. It attaches to the existing telephone wall-socket plug and becomes fully operational with the flick of a switch by the operator.

The Sendata 300, which contains operating lights on the front panel, indicating when it

is receiving or transmitting data, comes in a small rectangular casing, the same size as a conventional telephone base and only 30 mm high. It has been field-tested for almost a year by an independent evaluator and has received Telecom approval.

The recommended retail price is \$240, which includes tax.

For more information, contact Electro Medical Engineering, 69 Sutherland Road, Armadale, Vic. 3143. (03)509-5844.



How can I write better software, faster? Write it in BASIC/Z!

BASIC/Z. A new standard in compilers for the CP/M system. BASIC/Z is the most powerful implementation of the BASIC language on CP/M. BASIC/Z generates executable machine code compatible with 8080, 8085, Z-80 under CP/M 80 and 8086/8088 processors under CP/M 86 and MS-DOS.

Syntax testing as you type. BASIC/Z has a powerful program editor with built in syntax testing as you type. Time saving features include global search and replace, fifteen local edit commands and extensive debugging facilities. Line trace, error line retention, and the unique ability to 'single step' a program with a continuous display of selected variables are just a few of the features which will save you time.

Multitiered error handling allows your program to trap logical errors, including previously fatal BDOS errors. Only BASIC/Z can trap that 'BDOS ERROR ON A: READ ONLY' before it happens.

Printer/terminal customizing is built in. The runtime library of BASIC/Z (included in the package) includes installation routines for the majority of CP/M machines on the market. Your software will have near universal application without further modification. Just one set of programs will run on practically any hardware.

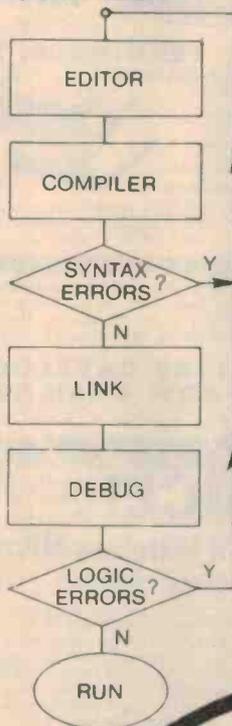
Unsurpassed accuracy. Floating point numerics with a range of $1E-61$ to $1E+61$, with a choice of precision from six to eighteen digits. All floating point maths are performed in decimal (BCD), avoiding rounding off errors.

Powerful executive functions aid programming. Using SORT, it can sort 2,000 elements in two seconds. User defined functions are fully recursive, support multiple arguments and may contain an unlimited number of statements.

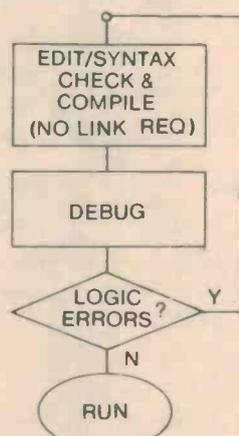
No Royalties. BASIC/Z has no royalties nor runtime charges. The license agreement confers the right to distribute support software such as the BASIC/Z runtime module and the installation hardware configuration utility, subject only to specified copyright acknowledgements.

What does it all cost? BASIC/Z documentation & Software: \$495* inc. tax. Available from your computer supplier or from Software Source direct. Available on 21 days approval (if software seal not broken). Or clip out the coupon and send in for further details.

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D	0-110, 0-110-130	0-22-24V 2A 0-27V, 1A 0-12V, 1A
E	0-240	0-18V, 400mA 0-17.5-60-180 -300V, 100mA
F	0-240	0-18V, 2A 0-8.5V, 3A
G	0-110-240	0-33V, 1.25A
H	0-240	0-12.6V, 1A
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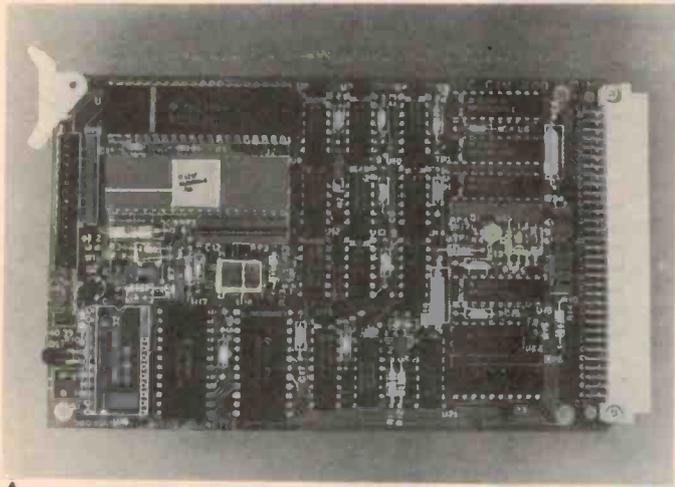
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Hewlett Packard chose Spellbinder over all other CP/M wordprocessors.



HIGH-SPEED BOARD FROM NATIONAL

National Semiconductor has added two models to its range of industrial computer boards: the CMOS Industrial Microcomputer CIM-804 and the CIM-802A.

The top-of-the-range CIM-804 is a high-speed 4 MHz central processing unit board, while the CIM-802A is an enhanced version of the company's proven 2 MHz CIM-802.

Both new boards operate in ambient temperatures, from -40°C to +85°C at low power-consumption levels for remote

station and process-control applications, such as industrial instrumentation, numeric machine control, pipeline monitoring and control, robotics and uninterruptable power supplies.

The high-speed CIM-804 is a board-level computer featuring 2K of static RAM, provision for 4K of 'shadow' PROM, up to 22 programmable input/output lines, 12 vectored interrupts and two 16-bit counter/timers with pre-scalers.

New features of the upgraded CIM-208A include a PROM "shadowing" capability.

Both CPUs are based on the eight-bit NSC800 microprocessor.

For further details, contact National Semiconductor, Cnr Stud Road and Mountain Highway, Bayswater Vic. 3153. (03)729-6333.

VERSATILE PLOTTER FOR MICROCOMPUTERS

A versatile graphic plotter, designed for use with personal and small-business computers, has been released by Sourceware, the Sydney computer-products distributor.

The Sweet-P personal plotter, which is plug-compatible with the IBM, Apple, Osborne and Kaypro personal computers, is suitable for graph processing, engineering graphics and overhead transparencies.

Sweet-P is provided with its own software for plotting standard and business graphics and fits into a slim briefcase. It is priced at \$1499.

One of the plotter's main advantages is its ability to

interface automatically to all the major graphics software, such as Lotus 1-2-3, Fastgraphs and BPS Graphs.

Sweet-P can be used to create, store and draw coloured pie charts, bar graphs, line graphs and illustrations on any type of paper or overhead transparency materials from 21 x 27 cm up to three metres long.

The plotter, which has a drawing speed of 15 cm per second, also can give a resolution of 250-line segments in 2.5 cm.

For more information, contact Sourceware, 4/73 Albert Avenue, Chatswood NSW 2067. (02)411-5711.

Why?

Hewlett Packard conducted exhaustive research before selecting a CP/M wordprocessor program to run on their HP125 business computer. The result? Spellbinder was judged superior in all key areas. Here are some of the reasons:

Spellbinder is fully customizable. Function keys and cursor keys really work on Spellbinder! This means faster training and more efficient use.

The most useful and workable mailing list capabilities. Sort by post code then merge any individual information from a mailing list into text.

Powerful sorting facilities. Sort clients by income and then print out a list in order of income with telephone numbers. Sort alphabetically or numerically. Eg. Print up mailing labels for only NSW customers from an all states list and have them sorted by post code.

Note: These facilities are built in. They are not expensive add-ons.

Boilerplating. The user can create entire documents by specifying the numbers of pertinent paragraphs on a master 'boiler plate' file and printing them in any order.

Advanced printing features. Includes the ability to print in two columns and to print multiple documents.

Forms generation facilities. Create a template that 'looks like' your invoice. Spellbinder will show you where to fill in the blanks - then print just the information on your pre-printed stationery.

Ease of use. The three interactive levels of help are fully customizable so they are right for YOUR system. You can even view other documents on your disk without disturbing your current text.

Arithmetical facilities are built in. Total your invoices, prices or statements automatically. Full 16 digit precision with up to 15 decimal places.

Full support. Software Source is dedicated to the support of this powerful package. A growing library of applications programs is available, from mail list entry to invoice generators.

Contact Software Source for further details and the name of your nearest dealer. Come and find out what real wordprocessing is all about.

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- Memory size can be expanded from standard 35K to 67K and expansion connector for serial ports, printers, disk drive to be added.

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**TWO NEW
TRS-80
MODELS**

The Tandy TRS-80 Micro Colour Computer Model MC-10, aimed primarily at first-time computers buyers, will be available in October, for \$199.95.

The Model MC-10, which has a 4K capacity, features a standard keyboard with true moving keys. Key word input can be accomplished with only two key strokes. Low-resolution graphics also can be generated with two key strokes.

A serial port allows use of modems and printers, and there is a cassette port for loading and saving of programs on cassette tape.

The 836 g Model MC-10 measures 5 x 20 x 18 cm — small, but still considerably larger than Tandy's new pocket computer, the TRS-80 PC-4, which retails for \$99.95.



The PC-4 measures just 1 x 16.5 x 7 cm and has a typewriter-style keyboard of 53 keys for alphabetic input, plus a 10-key numeric data-entry keypad. A 12-character LCD scrolls horizontally to up to 62 characters, including lower-case.

The PC-4 operates on two lithium batteries and has an automatic power-off feature to preserve battery life.

An optional user-installable 1K RAM memory module, costing \$29.95, expands the PC-4's 544-step, 26 variable-memory RAM to a maximum of 1568 possible steps or up to 222 memories.

A cassette interface (\$59.95) allows the user to store and load programs at 300 baud, using an optional cassette recorder. The lightweight interface, which

plugs into the back of the PC-4, operates on two "AA" alkaline batteries.

Tandy also offers a PC-4 printer (\$109.95) which prints 20 characters per line (60 lpm) in an electro-thermal 5 x 7 dot matrix.

For more details, contact Tandy Electronics, 91 Kurrajong Avenue, Mount Druitt NSW 2770. (02)675-1222.

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SOME COMPUTERS ARE BETTER THAN OTHERS

COMPUTER COMPARISON CHART						
	SPECTRAVIDEO SV-318	APPLE II PLUS	ATARI 800	COMMODORE 64	COMMODORE VIC 70	TANDY TRS-80
BASE PRICE	\$499	\$2100	\$1100	\$699	\$299	\$549
COMPUTING POWER FEATURES						
BUILT-IN ROM	32K	12K	10K	20K	20K	8K
EXPANDABLE TO	96K	N/A	42K	N/A	N/A	14K
BUILT-IN EXTENDED MICROSOFT BASIC	YES	YES	ADDITIONAL COST		NO	NO
BUILT-IN RAM	32K*	48K	16K	64K	5K	4K
EXPANDABLE TO	144K**	64K	48K	N/A	32K	32K
KEYBOARD FEATURES						
NUMBER OF KEYS	71	51	61	66	66	53
USER DEFINE FUNCTIONS	10	N/A	4	8	8	N/A
SPECIAL WORD PROCESSING	YES	NO	NO	NO	NO	NO
GENERATED GRAPHICS (FROM KEYBOARD)	YES	NO	YES	YES	YES	YES
UPPER/LOWER CASE	YES	UPPER ONLY	YES	YES	YES	UPPER ONLY
GAME/AUDIO FEATURES						
SEPARATE CARTRIDGE SLOTS	YES	NO	YES	NO	NO	NO
BUILT-IN JOYSTICK	YES	NO	NO	YES	YES	NO
COLORS	16	15	128	16	16	8
RESOLUTION (PIXELS)	256 x 192	280 x 160	320 x 192	320 x 200	196 x 184	192 x 256
SPRITES	32	N/A	4	8	8	N/A
SOUND CHANNELS	3	1	4	3	3	1
OCTAVES PER CHANNEL	8	4	4	9	9	3
A.D.S.R. ENVELOPE	YES	NO	NO	YES	YES	NO
PERIPHERAL SPECIFICATIONS						
CASSETTE	2 CHANNEL	1 CHANNEL	2 CHANNEL	1 CHANNEL	1 CHANNEL	1 CHANNEL
AUDIO IO	YES	NO	YES	NO	NO	NO
BUILT-IN MIC	YES	NO	NO	NO	NO	NO
DISK DRIVE CAPACITY (LOW PROFILE)	256K	143K	96K	170K	190K	156K
	YES	NO	NO	NO	NO	NO
CP/M COMPATIBILITY (80 column programs)						
CP/M* 2.2	YES	NO***	NO	NO****	NO	NO
CP/M* 3.0	YES	NO	NO	NO	NO	NO

* 16K user addressable plus 16K graphic support
 ** 128K user addressable plus 16K graphic support

*** Apple II can accept modified 40 or 80 column CP/M
 **** Commodore 64 accepts 40 column CP/M

Microsoft is a registered trademark of Microsoft Corporation
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OURS IS MUCH BETTER

When you start comparing Spectravideo's SV-318 to other personal computers, you'll find there really is no comparison. The SV-318 is the only logical choice, because it does more than some computers costing 4 times as much. And its abilities simply embarrass other computers in this price range.

The SV-318 isn't just more capable. It's much more capable. No other computer at even twice the price comes near its 32K ROM expandable to 96K. Or to its 32K RAM expandable to 144K. And no other computer has a built-in joystick/cursor control—an immeasurably useful feature when it comes to playing your favorite video game. Further, the SV-318 has, as its resident "language" Extended Microsoft Basic, the industry standard. It even has built-in CP/M (standard 80-column program), so you can immediately utilize over 10,000 existing software programs.

The SV-318 isn't just more expandable. It's much more expandable. Unlike many other so-called computer systems, all our important peripherals are available at once. That means you can get almost full usage out of your SV-318 from the day you buy it. With the Super Expander, Data Cassette, Floppy Disk Drive, Dot Matrix Printer, Graphic Tablet and SV-800 Serles Expansion Cartridges, there's almost no end to the work you can do. Or to the fun you can have. The SV-318 is well designed to interface with new options as they become available, too. All this adds up to a computer you'll grow into, not out of.

The SV-318 is not only eminently affordable, it's the first real bargain of the computer age! Besides business application, home budgeting, word processing, programming and self-teaching, the SV-318 is the best entertainment value in town. Not only can you use it with your TV or color monitor to play hundreds of different video games,



FOR UNDER \$500

with the optional SV-105 Graphic Tablet you can draw pictures, graphs, charts and other visual images on your TV screen. Considering what you get for what little you pay, the SV-318 is once again the only logical choice.

Whether you're investing in your first computer, or are already well versed in today's most important machine, you'll find that the SV-318 is the only logical choice for you.

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S100 Z80 System Cards

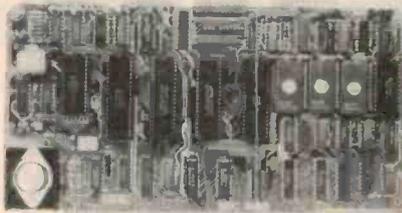
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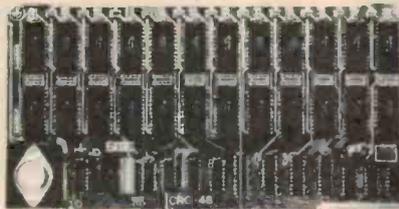


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Sendata 300 Modem Direct Connect

A new direct connect 300 bps modem that is no taller than a 50c piece and fits snugly under the base of a telephone, has been released by Australian communications manufacturer, Electromed. Called the Sendata 300 the modem is simple to operate and does not require operator training. It attaches to the existing telephone wall socket with the flick of a switch by the operator.

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AUSTRALIAN MICROCOMPUTER BOASTS MANY ADVANCED FEATURES

This column in July looked closely at AED's unique Instant Program Selection feature 'MPS'. In August we examined the UNIVERSE's advanced dual 8 & 16 bit high speed CPU, and intelligent DMA floppy controller. This month we look in depth at two more of the technology leading features that make this machine the fastest, most flexible and expandable, S100 CP/M and CP/M-86 based system available.

UN-SERIAL TERMINAL

Unlike typical computers the AED UNIVERSE incorporates a memory mapped intelligent terminal. This non serial terminal provides higher speed than serial types, combined with the special facilities required by powerful operating system features such as SUPERAED and MPS. The keyboard is a high reliability Honeywell Hall effect data entry and word processing type with 17 user definable keys, numeric pad, and 12 special cursor control keys. The keyboard is separable from the screen unit for optimum user comfort. The screen is a high resolution, green or amber, anti-glare, monitor mounted in an attractive and functional swivel and tilt housing. The terminal electronics are driven by intelligent video driver software which is incorporated in the AED CP/M extensions 'SUPERAED' and 'MPS'. This standard terminal driver responds to the usual codes and escape sequences of serial types, however, instead of being locked in, the driver, lends itself to code modification or extension. The sheer speed and direct driving capability of the 'UN-SERIAL' terminal makes it extremely suitable to word processing systems such as 'WORDSTAR' under which it performs more like a sophisticated dedicated wordprocessing machine than the normal computer fitted with a serial terminal.

INTELLIGENT D.M.A. HARD DISK CONTROLLER

The hard disk controller in the UNIVERSE computer incorporates many advanced features to compliment the design of the floppy controller described last month. Unlike many inferior interfaces this controller caches in on all of the increased transfer speed of the Winchester hard disk mechanisms. The controller has its own 7.16 Meg 8x300 Bipolar processor, therefore the data arrangement on the disk is not limited by special purpose LSI controller chips. This intelligence relieves the main CPU of time consuming processes such as head positioning and rotational delays, etc. The main processor is further freed by the DMA system which independently transfers the data bytes directly from the disk into the system memory. This "channel" concept allows the controller to communicate with S100 memory by "stealing" bus cycles from the main CPU or using the bus in "burst mode" for ultra-fast transfer. This idea of an intelligent channel was first implemented on mainframes, now, this powerful concept has been implemented on an S100 bus microcomputer system. The interface can drive the full 24 address line space and has priority logic allowing it to contend with up to 15 other temporary bus masters.

The AED UNIVERSE combines many more technology leading features in one system than nearly all other microcomputer systems. Over the last few months we have looked at several of them and more will be detailed in this column next month.

UNIVERSE

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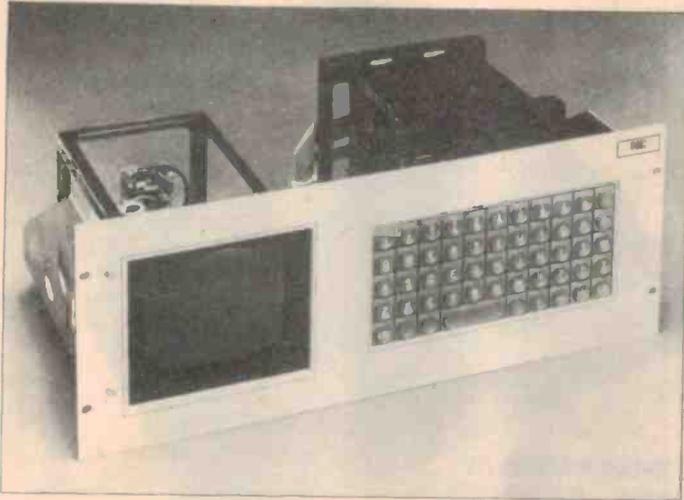
For a complete information kit on the AED UNIVERSE send a stamped self addressed A4 envelope to:



SYDNEY: AED COMPUTERS, 24 Darcy St, Parramatta, NSW 2150. Phone: (02) 689 1744, (02) 681 4966.

MELBOURNE: AED COMPUTERS (MELBOURNE), Elston Micro, 53 Waverly Rd, East Malvern, Vic 3145. Phone: (03) 211 5542. Telex: AA30624 ME447.

CANBERRA: AED COMPUTERS (CANBERRA), 217 Northbourne Ave, Canberra 2601. Phone: (062) 475 348. Telex: AA62898 HARSUR.



ANCA INDUSTRIAL TERMINAL

Australian NC Automation, the Melbourne-based company specialising in the design and manufacture of micro-computer-based industrial control systems and sub-assemblies, has released its Model VT5 industrial YDU terminal.

Designed specifically for industrial applications where clear, precise messages need to be displayed, and where input data is required from factory personnel, the ANCA VT5's features include a solid-state hall-effect QWERTY keyboard,

a 13 cm green phosphor display with 32 characters by 16 rows, 20 mA and RS232 interface to 9600 baud, and both dc and ac operation.

Programmable aspects of the VT5 are double-size characters, reverse video characters, flashing characters, cursor blank, blink and box, cursor addressing, and underlining.

The unit measures 178 x 482 x 230 mm and weighs 6 kg.

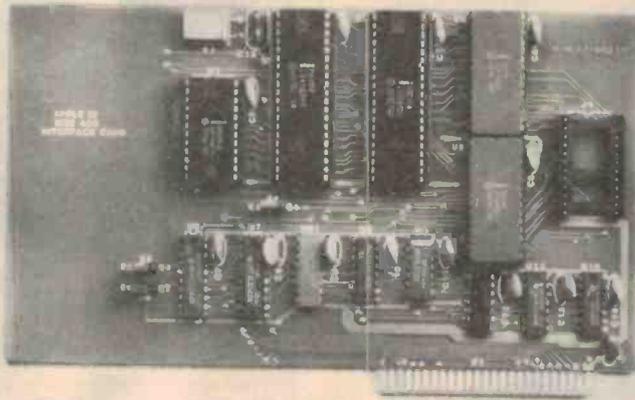
For further details, contact ANCA, 204-206 Bell Street, Preston Vic. 3072. (03)44-0722.

SPELLBINDER NETWORK GROWS

Sydney's Software Source has signed a sub-distribution agreement with Sky Systems for Oasis versions of the Spellbinder word-processing and office management system.

While Software Source remains the sole Australasian distributor for Spellbinder, Sky Systems — located at 36 Second Avenue, Willoughby NSW 2068; phone (02)95-5503 — will enhance the backup and service aspect for the package.

For further information, contact Software Source, 344-348 Oxford Street, Bondi Junction NSW 2022. (02)389-6388.



CONTROLLER FOR APPLE III

Innovated Peripheral Systems, a leading American manufacturer of magnetic tape controllers and peripherals for the data-processing industry, has

introduced a new IEEE-488 controller for the Apple III series of computers.

The APL-488CT requires a single slot in the Apple III, and

provides the users with IEEE-488 Standard 1978.

The controller's driver is SOS compatible, allowing the user to use simple print or input statements to control the bus function. Because the driver is within the SOS, all high-level languages are supported, making it very user-friendly.

Using the APL-488CT, more than 2000 IEEE-488 compatible instruments, peripherals and other devices can be added to the Apple III.

For further information, contact the Australian agent, Mostyn Enterprises, 35 Alexander Street, Dundas NSW 2117. (02)871-6297.

THE WIZARDRY OF OZ1

OZtronics Australia has announced the release of OZ1, a data-acquisition system that allows almost any computer to gather analogue and digital information from 'the real world'.

A supervising computer communicates with OZ1 via the serial port. Consequently, many portable computers, small business computers and personal computers may be used with OZ1 for data acquisition without modification or addition of special interface cards, requiring only that a serial interface be available.

The unit can be connected to the serial port of the host computer, either as a single unit or as a network of up to 16 units.

It provides for 30 single-ended or 15 differential analogue channels and two digital channels, and a fully implemented network provides for 480 single-ended or 240 differential analogue channels and 32 digital channels.

For additional details, contact OZtronics Australia, 8 Glenfern Avenue, Upwey Vic. 3150. (03)438-2638.



Using Soundex codes for approximate matching

If your spelling is not the best, your filing methods are a bit haphazard and, worse still, you can't remember things like you used to, don't panic. This program will sort you out — it sorts words that sound alike.

Tom Moffat

39 Pillinger Drive, Fern Tree, Tasmania 7101

IMAGINE A SMALL data base system in a newspaper office. A reporter remembers an interview done about three years ago, with a fellow named Franz. He would now like to contact this person again, and asks the computer to search out the name and provide details of where the person works, and how he can be contacted.

The computer responds: NAME NOT FOUND. And a potentially good story bites the dust. Well, three years is a long time to remember a name.

Now consider the same computer, with a little option included in its data base program. The reporter types in 'Franz' and the computer responds with FRANS, FRANCS, FRANKS, FRANCE. Aha! It was Franks. That's the one, call up the information on him.

In the first case the computer was looking for an exact match, and it bombed out when it didn't find one. In the second case, near enough was close enough, thanks to the 'Soundex' algorithm.

The Soundex scheme has been around for some time, but for some reason it hasn't been widely used, especially in micro systems. What it does is sort words into certain categories that sound alike, although their spellings can differ widely. Each word entered into the system is assigned a code which describes its sound. When a match is asked for, words with identical Soundex codes are displayed.

Works amazingly well

Soundex codes are developed as follows: When a word is entered, its first letter becomes the letter portion of the code. Then each succeeding letter is inspected and assigned a group number as per Table 1. Everything in group 0, the vowels and 'H', is disregarded, leaving the other group designators 1 through 6 where the letters were. Double group numbers are disregarded, that is, 34455 would become 345. Finally every number after the fourth is chopped off. This leaves a code consisting of a letter and up to four numbers.

The Soundex algorithm is one of those strange procedures that work a lot better than it has any right to. It's quite amazing to see what horrible mis-spellings it will accept, to come up with the right answers.

The person who cooked up the scheme must have been a really clever thinker.

Listing 1 is a BASIC program that will let you play around with a Soundex algorithm. You type in a name, and the program checks to find if it's seen that word before. If not it computes the word's Soundex code,

and stores both the word and the code. The word, and others with the same code, are then displayed, along with the codes themselves.

Although not necessary in this demonstration program, the actual Soundex code generation process is given as a

```
00100 REM Demonstration of SOUNDEX algorithm; prints previous
00110 REM entries that sound like the new word. If not in the
00120 REM table, the new word is stored. Maximum 100 words.
00130 REM by Tom Moffat, 28/4/83
00140 REM
00150 CLS: E=0
00160 STRS (2000)
00170 DIM A0(99): FOR A=0 TO 99: A0$(A)="": NEXT A
00180 DIM B0(99): FOR A=0 TO 99: B0$(A)="": NEXT A
00190 DIM D(25)
00200 FOR F=0 TO 25: READ D(F): NEXT F
00210 PRINT: INPUT "ENTER A WORD: ";A1$: PRINT
00220 GOSUB 340
00230 FOR F=0 TO E
00240 IF A1$=A0$(F) THEN NEXT* F 280
00250 NEXT F
00260 A0$(E)=A1$
00270 B0$(E)=B1$
00280 FOR G=0 TO E
00290 IF B0$(G)=B1$ THEN PRINT A0$(G), B0$(G)
00300 NEXT G
00310 E=E+1
00320 GOTO 210
00330 REM Soundex sub: Input = WORD (A1$), Output = CODE (B1$)
00340 K=LEN(A1$)
00350 C1$=""
00360 B1$=A1$(;1,1)
00370 H=0
00380 IF K<2 THEN RETURN
00390 FOR F=2 TO K
00400 I=ASC(A1$(;F))
00410 IF I<65 OR I>90 THEN 450
00420 I=I-65
00430 J=D(I)
00440 IF J<>0 THEN LET C1$=C1$+CHR$(J+48)
00450 NEXT F
00460 K=LEN(C1$)
00470 IF K=0 THEN 540
00480 FOR F=1 TO K
00490 I=ASC(C1$(;F,F))
00500 IF I<>H THEN LET B1$=B1$+C1$(;F,F)
00510 H=I
00520 NEXT F
00530 IF LEN(B1$)>5 THEN LET B1$=B1$(;1,5)
00540 RETURN
00550 DATA 0,1,2,3,0,1,2,0,0,2,2,4,5,5,0,1,2,6,2,3,0,1,0,2,0,2
00560 END
```

subroutine, so you can pinch it word for word and use it in your own program. You also need to load up a 26 character array with group numbers for each letter, as line 200 loads data from line 550.

To get an idea of what to expect, have a look at the sample run containing some well known names with alternative spellings, nicely matched up by Soundex codes.

Although the BASIC version of the program is a bit messy with all that breaking apart of strings, a machine code version should be dead easy. By the time you read this I should have a small 'newsroom data base' program up and running, in machine code, using the Soundex algorithm.

All this probably sounds a bit far out, too good to be true. You may suspect it's another con job like that 'Gutenberg Transform' program in the April issue. But rest assured, this one is fair dinkum, really.

TABLE 1

Group	Letters
0	A E I O U Y W H
1	B F P V
2	C G J K Q S X Z
3	D T
4	L
5	M N
6	R

ENTER A WORD: HAWKE

HAWKE H2
HAWK H2
HAAWK H2
HAUK H2
HWACK H2

ENTER A WORD: PEACOCK

PEACOCK P2
POECKOCK P2
PEECKOCK P2
PEEKOCK P2

ENTER A WORD: HAYDEN

HAYDEN H35
HAADNE H35
HEYDNE H35
HAIDINN H35

ENTER A WORD: FRASER

FRASER F626
FRAESEUR F626
FROESUR F626
FRASSRE F626
FRASSEARE F626

ENTER A WORD: DRACULA

DRACKULAE D624
DRACKYOLAH D624
DRACULA D624
DRAKOOLA D624

ENTER A WORD: FRANKENSTEIN

FRANKENSTEIN F6525
FRUENKINSTINE F6525
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SHARP SCORES WITH 20MM DIAMETER "JUMBO" LEDS

(JAPAN) Coloured red, green or yellow, these outsized domed devices are an ideal replacement for filament lamps in electrical or control panels. Indoor scoreboards will also benefit from their wide viewing angle and high brightness.

WHISTLE, BEEP, HONK, CHEEP, CHIME, TICK, RING, CLICK ZOUNDS - WHAT SOUNDS!

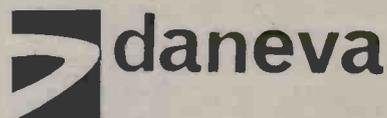
(U.S.A.) General Instrument's Sound Synthesizer, I.C. AY-3-8910, will add new dimensions to your computer's audio repertoire. For less than \$9.00 you could have your computer express itself in sounds, symphonic or even naughty.

INDUSTRIAL ACTION EXPECTED FROM SINGLE CHIP PROGRAMMABLE CONTROLLER

(U.S.A.) L.S.I. Computer Systems LS7270 Programmable Logic Controller (PLC) could grab a large chunk of the timer, sequencer and relay combinational logic action. At around \$28.00 this 40 pin part has features which rival top-drawer packaged PLC's costing hundreds of dollars, Summarizing:- 12 latched outputs, 20 debounced inputs including 12 discretes, 4 downcounters, 4 priority interrupts, on-chip clock generator and up to 2048 instructions from an external ROM or PROM. This device is geared to individual bit processing, Boolean processing, turn-on turn-off functions, counting and timing operations, not numeric computation - so don't confuse the LS7270 with your common or garden variety micro.

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ZX COLUMN

A ZX81 CLOCK

Jack Creasy, Elizabeth Park, SA

The following program was written to overcome a severe case of frustration with the way Sinclair implemented the PAUSE command on the ZX81.

One would imagine the implementation of a clock would be easy given a counter that decrements at 50 Hz — nothing could be further from the truth!

Two main problems manifest when implementation is attempted:

- 1) Exit from a PAUSE causes the ZX81 to go into FAST mode while pointers are updated — this causes a momentary loss of synch and an infuriating flash on the screen.
- 2) While PAUSE is executing nothing else can be done, the CPU simply counts frames — and any alteration to the length of the program will affect the pause count needed to get the time reasonably accurate.

Allied with the above is the inability to easily adjust the time-keeping to give long term accuracy and the difficulty of getting the clock to run at a one second rate.

The obvious answer to these restrictions is to use an assembly language routine to update the clock, and this is the solution submitted.

Program 'B' is the clock program and can be described as follows:

Line 10 is a 64 byte assembly program with one entry point which maintains a six digit 24 hour clock (HH:MM:SS). This routine also controls the least significant byte of the frames counter that is decremented by the ZX81 every TV frame in slow mode.

On entry to this routine the clock is incremented by one second, then corrected for 24 hour operation. Before returning to BASIC, it waits for the frames to reach its terminal count (205 or 204), signalling the expiry of one second.

Line 20 contains the clock locations updated by the assembly routine. Note that lines 10 and 20 must be together and the first two statements in the program.

Lines 20 and 30 form a subroutine used to update TS on the variable stack.

Line 40 is the initial start line, it sets frames low to 255. Line 50 calls routine (20,30) to update TS. Line 60 prints the time (TS) near the centre of the screen.

Lines 70 and 80 correct the long-term accuracy of the clock by increasing the 1s period by 50 ms to slow the clock down. The time in line 80 can be altered to suit individual ZX81s.

Line 90 calls the assembly routine to update the time. Line 100 is the loop back to line 50 after 1s expires.

The program will run in a 1K or larger ZX81. BASIC statements can be added without affecting time-keeping, providing the loop time of the program does not exceed one second.

To test programs, POKE 16567,201 and the clock will run at maximum speed, so revealing loop time. Ensure your programs run at least 10% fast when testing to ensure that all contingencies are allowed for.

For those adept at assembly routines, the listing is provided. This can be easily altered to provide elapsed time to 99 hours, or 12 hour timekeeping if desired.

The counter maintenance routine is a general purpose 8-digit software counter with the overflow and reset values for each digit set in a table. You will notice that the '?'s in the clock are treated as digits and toggle between '?' and '?', although TS only every contains '?'.

```

METHOD OF LOADING ZX81 CLOCK PROGRAM
*****
1) TYPE 'NEW'
2) LOAD PROGRAM (A)
3) 'RUN' PROGRAM (A) AND ENTER VALUES FOR
   ASSEMBLY LANGUAGE PROGRAM FROM LISTING
4) TYPE 'CLEAR'
5) TYPE IN LINES 20 TO 100 OF PROGRAM (B)
6) 'LIST' PROGRAM AND ENSURE THERE ARE NO
   ERRORS
7) 'SAVE' 'CLOCK' ONTO CASSETTE
8) 'EDIT' LINE 20 TO CURRENT TIME
9) 'RUN' 40 TO START CLOCK
10) LINES 70 AND 80 ADJUST THE CLOCK'S
    LONG TERM ACCURACY --- LINE 80 CAN
    BE ALTERED TO SUIT INDIVIDUAL NEEDS

PROGRAM (A)
*****
***** PROGRAM TO ENTER ASSY CODES *****
10 REM.....TYPE 64 DOTS.....
20 LET X=16513
30 FOR Y=1 TO 64
40 INPUT D
50 PRINT D;";";
60 POKE (X+Y),D
70 NEXT Y

PROGRAM (B)
*****
***** CLOCK PROGRAM WITH CORRECTION *****
10 REM (-----64 BYTE ASSY PROGRAM-----)
20 LET T$='00:00:00'
30 RETURN
40 POKE 16436,255
50 GOSUB 20
60 PRINT AT 5,10;T$;
70 IF T$(4 TO 8)='30:00' THEN POKE 16571,204
80 IF T$(4 TO 8)='33:41' THEN POKE 16571,205
90 LET A=USR 16530
100 GOTO 50

*****
***** DECIMAL VALUES FOR ENTRY BY PROGRAM (A) *****
*****
16514          38,28,34,28,15,14
16520          38,28,34,28,15,14,38,28,38,28
16530          6,8,33,211,64,17,130,64,52,26
16540          19,190,32,6,26,119,43,19,16,244
16550          42,204,64,69,76,33,224,225,9,48
16560          6,33,28,28,34,204,64,33,52,64
16570          62,205,190,32,253,54,255,201

TOTAL 64 BYTES

```

```

*****ASSY LANGUAGE ROUTINE*****
NOTE !!! ALL NUMERICS IN DECIMAL FOR THE EASE
=====
        OF THE ZX81 USER AND FRUSTRATION OF
        THE HEXAMANIACS

.LOC 16514
-----CLOCK DIGIT CONTROL TABLE-----
38          ;SECONDS O'FLO=A
28          ;SECONDS RESET=0
7;         ;X10 SEC O'FLO=6
28          ;X10 SEC RESET=0
15         ;-):(- O'FLO=?
14         ;-):(- RESET=:
38         ;MINUTE O'FLO=A
28         ;MINUTE RESET=0
34         ;X10 MIN O'FLO=6
28         ;X10 MIN RESET=0
15         ;-):(- O'FLO=?
14         ;-):(- RESET=:
38         ;HOURS O'FLO=A
28         ;HOURS RESET=0
38         ;X10 HRS O'FLO=A
28         ;X10 HRS RESET=0
-----PROGRAM START
.LOC 16530
-----COUNTER MAINTENANCE ROUTINE-----
LD B,B      6,8      ;LOOP COUNT - # OF DIGITS
LD HL,16595 33,211,64 ;POINTER TO END OF CLOCK
LD DE 16514 17,130,64 ;POINTER TO DIGIT TABLE
BEGIN: INC (HL) 52      ;INCREMENT DIGIT
LD A(DE)   26      ;GET O'FLO CONSTANT
INC DE     19      ;POINT TO RESET VALUE
CP (HL)    190     ;HAS IT O'FLOWED
JRNZ CHECK 32,6    ;NO - SO EXIT
LD A(DE)   26      ;YES - LOAD RESET VALUE
LD (HL)A   119     ;RESET DIGIT
DEC HL     43      ;POINT TO NEXT DIGIT
INC DE     19      ;POINT TO NEXT O'FLO
DJNZ BEGIN 16,244  ;LOOP IF MORE DIGITS

-----24 HR CLOCK CORRECTION ROUTINE-----
CHECK: LD HL (16588) 33,204,64 ;LOAD X10 HRS INTO HL
LD B,L     69      ;SWAP X10 HRS INTO BC
LD C,H     76      ;
LD HL 57824 33,224,225 ;LOAD HRS TEST VALUE
JR NC,END1 48,6    ;TEST IF HRS=24
LD HL 7196 33,28,28 ;LOAD CODE 00 FOR HRS
LD (16588) HL 34,204,64 ;RESET HRS TO 00

-----FRAMES MONITOR ROUTINE-----
THIS IS LOCATION 16567
I          SET IT TO 201 TO RUN
U          AT MAX SPEED
END1: LD HL 16436 33,52,64 ;POINTER TO FRAMES
LD A,205  62,205  ;TIMEDOUT VALUE FOR FRAMES
TEST: CP (HL) 190   ;HAS FRAMES EXPIRED
JRNZ TEST 32,253  ;NO - SO GO TEST AGAIN
LD (HL)255 54,255 ;RESET FRAMES VALUE
RET       201     ;GO BACK TO BASIC -----)

```

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amateur radio, dx communications

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CALENDAR Noel Bailey, Maryland NSW

This program will print out a calendar for you, either for years ahead of the present, or years past. The program should work for any date from 1753 onwards since our modern calendar dates from this time. I believe that our calendar will be out of phase with the seasons by one whole day around 10 000 AD. I don't think that I'll be worried when the time comes.

The listing was done on a Model 15 teleprinter

which does not have the relational operators 'greater than' and 'less than' and most importantly, semicolons which have been used a lot in this program. Consequently I have penned them in (and hope not to have missed any!).

Lines 160 and 560 may be removed from the program or altered for whatever configuration of printer is being used. My system uses 1200 baud output to a 2650

microprocessor which converts 1200 baud ASCII to 50 baud baudot. The 2650 sends back a 'ready' flag to hold the MicroBee until the machine is ready to accept the next character. To the ear, the baudot seems to be going at full speed, but it is still slow in this age of line printers.

Note that the 'pound' sign (£) equates to the 'hash' symbol (#) on the MicroBee.

```
00100 REM 'CALEND' PROGRAM - THIS PROGRAM WILL PRINT OUT A
00110 REM CALENDAR FOR ALL YEARS PAST 1752
00120 REM THE FIRST PART OF THIS PROGRAM CALCULATES THE DAY
00130 REM THAT NEW YEAR'S DAY FALLS ON. WRITTEN BY NOEL BAILEY
00140 REM ON THE 6TH FEB 1983.
00150 DIM B(12),D(12)
00160 OUT £5 ON:REM DIRECTS OUTPUT STREAM TO 1200 BAUD PRINTER.
00170 REM YOU MAY NEED TO CHANGE THIS FOR YOUR OWN PRINTER.
00180 PRINT 'WHAT YEAR WOULD YOU LIKE?'
00190 INPUT Y
00200 IF Y<1753 THEN PRINT'YEAR MUST BE AFTER 1752':GOTO 180
00210 PRINT'CALENDAR FOR 'Y
00220 PRINT'-----'
00230 PRINT
00240 L=Y-1
00250 P=L/100
00260 A=P/4;Z=(5X1)/4
00270 Z=36+Z-P+A
00280 D(1)=Z-7X(Z/7)
00290 GOSUB 680
00300 REM A IS THE COUNTER FOR EACH PAIR OF MONTHS.
00310 FOR A=1 TO 6
00320 REM PRINT MONTH HEADINGS.
00330 ON A GOSUB 620,630,640,650,660,670
00340 REM PRINT WEEKDAY HEADINGS.
00350 GOSUB 580
00360 REM R IS THE COUNTER FOR HORIZONTAL ROWS.
00370 FOR R=1 TO 6
00380 REM C IS A COUNTER FOR VERTICAL COLUMNS FOR ODD MONTHS.
00390 FOR C=1 TO 7
00400 IF R=1 AND D(AX2-1)=>C THEN PRINT ' ';GOTO 430
00410 IF C-D(AX2-1)+(RX7-7)>B(AX2-1)THEN PRINT ' ';GOTO 430
00420 PRINT TAB(CX4-3);C-D(AX2-1)+(RX7-7);
00430 NEXT C
00440 REM K IS A COUNTER FOR VERTICAL COLUMNS FOR EVEN MONTHS.
00450 FOR K=1 TO 7
00460 IF R=1 AND D(AX2)=>K THEN PRINT ' ';GOTO 490
00470 IF K-D(AX2)+(RX7-7)>B(AX2)THEN PRINT ' ';GOTO 490
00480 PRINT TAB(KX4-3);K-D(AX2)+(RX7-7);
00490 NEXT K
00500 PRINT
00510 NEXT R
00520 FOR L=1 TO 7:REM 7 LINE FEEDS
00530 PRINT
00540 NEXT L
00550 NEXT A
00560 OUT £5 OFF
00570 END
00580 GOSUB 600:PRINT TAB(35);:GOSUB 600:PRINT
```

```
00590 RETURN
00600 PRINT'SUN MON TUE WED THU FRI SAT';
00610 RETURN
00620 PRINT TAB(11);'JANUARY';TAB(45);'FEBRUARY':RETURN
00630 PRINT TAB(12);'MARCH';TAB(46);'APRIL':RETURN
00640 PRINT TAB(13);'MAY';TAB(47);'JUNE':RETURN
00650 PRINT TAB(13);'JULY';TAB(46);'AUGUST':RETURN
00660 PRINT TAB(10);'SEPTEMBER';TAB(45);'OCTOBER':RETURN
00670 PRINT TAB(11);'NOVEMBER';TAB(45);'DECEMBER':RETURN
00680 IF Y-Y/4X4=0 THEN 700
00690 L=0;GOTO 730
00700 IF Y-Y/400X400=0 THEN LET L=0;GOTO 730
00710 L=1
00720 REM L=1 FOR LEAP YEAR ELSE L=0
00730 FOR M=2 TO 12
00740 IF M>2 THEN 790
00750 A=M-1
00760 IF L=0 THEN LET A=AX63 ELSE LET A=AX62
00770 A=A/2
00780 GOTO 820
00790 A=M+1
00800 A=INT(FLT(A)X30.6)
00810 IF L=0 THEN LET A=A-63 ELSE LET A=A-62
00820 A=A+D(1)
00830 D(M)=A
00840 REM THIS IS THE DAY NUMBER OF THE YEAR FOR THE
00850 REM FIRST DAY OF EACH MONTH
00860 NEXT M
00870 REM TO CALC THE DAY NO THAT THE 1ST OF EACH MONTH
00880 REM FALLS ON
00890 FOR I=2 TO 12
00900 D(I)=D(I)-D(I)/7X7
00910 NEXT I
00920 REM NOW TO GET THE NUMBER OF DAYS PER MONTH.
00930 FOR I=1 TO 12
00940 READ B(I)
00950 NEXT I
00960 IF L=1 THEN LET B(2)=29
00970 RETURN
00980 DATA 31,28,31,30,31,30,31,31,30,31,30,31
```

SEPTEMBER							OCTOBER						
SUN	MON	TUE	WED	THU	FRI	SAT	SUN	MON	TUE	WED	THU	FRI	SAT
					1	2	3						1
4	5	6	7	8	9	10	2	3	4	5	6	7	8
11	12	13	14	15	16	17	9	10	11	12	13	14	15
18	19	20	21	22	23	24	16	17	18	19	20	21	22
25	26	27	28	29	30		23	24	25	26	27	28	29
							30	31					

PROGRAM DATA GENERATOR Hans Beilharz, Kareela NSW

I was pleased to see the Character Generator program in the June Issue. The program is very good but if large shapes are generated a lot of work is required to transfer the data, if you want to use the shape in another program.

This program can be added to the Character Generator program or any similar program, to automatically generate DATA statements and store them on tape so that they can be merged to another program. This saves having to write down the values from the screen and then typing the lot.

The DATA line numbers start at 10000 although this can be changed to any value; see line 540. When the shape is finished press tab and then follow the instructions for using the tape recorder.

To merge DATA to another program first load the other program, making sure no lines conflict with the DATA line numbers. Then type IN#2 return, start the tape and the DATA lines will be added to the program.

It is best to set SPEED to 0 for all merge operations. Press reset (warm start) to get control back when finished.

Add line 285 to the Character Generator program then add the lines 500 to 620. 285 IF ASC (A1\$) = 9 THEN 500.

```
505 CLS
510 PRINT "Set up tape recorder, press RETURN when ready"
520 A1$=KEY$: IF ASC(A1$)=13 THEN 530 ELSE 520
530 PRINT" recording DATA"
540 OUT#2 ON: L=10000
550 X=USED-1:FOR A=63488 TO 63488+X*16 STEP 16
560 PRINT L; " DATA";PEEK(A);
570 FOR B= 1 TO 15
580 PRINT ", ";PEEK(A+B);
590 NEXT B: PRINT " "
600 L=L+10:NEXT A
610 OUT#2 OFF:PRINT"Finished switch off tape recorder"
620 END
```

MICROBEE COLUMN

SCREEN DUMPER

Jon McCormack, Brighton East Vic.

This program in machine language can be assembled anywhere in memory, provided it does not overlap with your current BASIC program.

To call in the program use the following statements in your program:

```

OUT#1
X=USR(decimal address of program)
OUT#0
    
```

The OUT#1 outputs the screen to the I/O port, however, output could be directed to the RS232 port or the cassette port or even all three. This enables the screen to be dumped to a printer, cassette, modem or any other output device.

Since the program was intended for my Dick Smith graphics printer there are several changes that can be made to suit individual requirements.

1. Characters greater than CHR\$(128) are replaced by an asterisk (*). This portion of the program can be removed by deleting lines 160-180 and 300-310 of the assembler listing.

2. The character for my printer to do a carriage return and line feed is CHR\$(10) (0A hex); change this value (line 230) to suit your output device.

The routine at 8024 hex (in the BASIC ROMs) sends the contents of the A register to the current output device(s) which is defined by the OUT# instruction.

SCREEN DUMPER

```

0400          00110      ORG      400H      ;CHANGE TO SUIT PROGRAM
0400 2100F0    00120      LD        HL,0F000H ;PUT SCREEN START ADD. IN HL
0403 0E0F     00130      LD        C,15      ;PUT NO. OF LINES IN C
0405 0640     00140      LD        B,64      ;PUT SCREEN WIDTH IN B
0407 7E      00150      LD        A,(HL)    ;PUT CURRENT SCREEN POS. IN A
0408 57      00160      LD        D,A      ;STORE BYTE IN D
0409 DE80     00170      SAC        A,128    ;CHECK IIF GRAPHICS CHAR.
040B 3013    00180      JR        NC,AST   ;IF YES THEN GOTD AST
040D 7A      00190      LD        A,D      ;PUT BYTE BACK IN A
040E CD4280   00200      CALL     8042H    ;OUTPUT BYTE TO PRINTER
0411 23      00210      INC        HL      ;MOVE TO NEXT SCREEN POSITION
0412 10F3    00220      DJNZ     LOOP    ;DEC COUNTER FOR LINE
0414 3E0A    00230      LD        A,0AH   ;LOAD A WITH LINE FEED CHAR.
0416 CD4280   00240      CALL     8042H    ;OUTPUT BYTE TO PRINTER
0419 0D      00250      DEC        C      ;DECREMENT LINE POINTER
041A 79      00260      LD        A,C      ;PUT NO OF LINES IN A
041B FE00     00270      CP        0       ;CHECK IF END OF SCREEN
041D 20E6    00280      JR        NZ,LOOP ;IF NOT END THEN BACK FOR MORE
041F C9      00290      RET        ;END OF PROGRAM
0420 3E2A    00300      LD        A,2AH   ;PUT A " * " IN A
0422 18EA    00310      JR        PRINT  ;PRINT IT!!!
0000          00320      END
00000 Total errors
    
```

PRINT 040E AST 0420 LOOP 0407 0LOOP 0405

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SPECIFICATIONS

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PAKMAN

W.F.Kreykes, St Alban s Vic.

This program has been designed to run as fast as possible at the expense of memory.

Due to the restrictions of the colour display of the 660, the game is in black and white. However, the colour of the background will change indicating the level you are currently playing at and the number of men that are left. Initially the screen will be green (three men), then red (two men) and then blue (last man).

After the last man has been eaten the screen goes black and the score flashes indicating the end of the game. To restart the game press any key, except 'reset' and 'step', and the game will start again.

For those who like to 'roll their own', the whole screen is recorded at 0988. Individuals can change the maze, but not the homes or the score box, provided they keep the dots on the same horizontal and vertical lines and there are not open spaces i.e. a wall three dots wide all over the screen. The walls control the Pakmen; they travel in the same direction until they hit a

wall, but they never double back.

The extra dot space between the dot and the thin walls is necessary so the man cannot eat the ends off the walls. A bit of experimenting may be required and when this is done the dots on the screen must be counted and the data at 06C1 changed.

If we take my program as an example, there are 328 dots; subtracting 256 leaves 72 which is 48 in Hex and this is the data at 06C1. 346 dots = 90 = 5A.

If you run this on a B&W monitor and the colour gives an unclear picture then you can

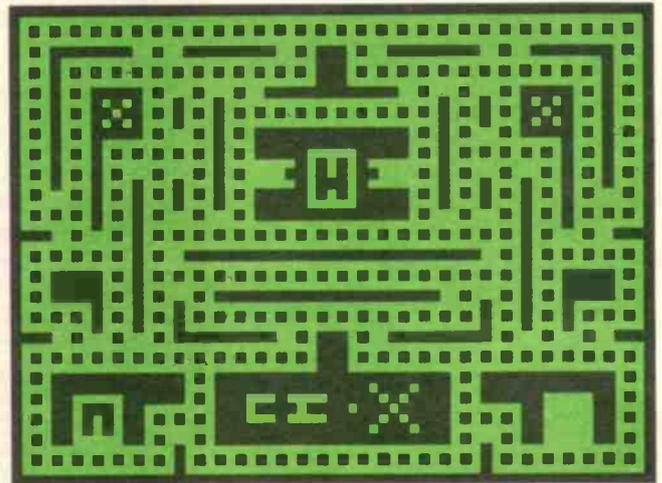
```

0600 0963 0963 A637 6012 F055 6803 6D00 6E00
0610 26D2 7901 49F0 28BC 49A0 2638 A94A F365
0620 E3A1 6300 E2A1 6302 E1A1 6305 E0A1 6303
0630 330C 267A 2842 1612 3BCC 00EE 6B00 1818
0640 2654 6912 F900 F918 7901 4970 1640 E99E
0650 1648 1602 A985 FE33 A983 FD33 A984 F365
0660 6917 6526 F029 2674 7901 F129 2674 F229
0670 2674 F329 D955 7905 00EE A970 FA1E D673
0680 8A30 A970 FA1E 4A00 7602 4A05 76FE 4A02
0690 7702 4A03 77FE D673 3F00 1828 4BCC 00EE
06A0 A952 D672 3F01 183A FF18 7E01 7C01 3CFE
06B0 16B8 A6C5 60FF F055 3B00 2922 4E64 290E
06C0 3C48 00EE 00EE 6BA0 FB00 FB18 7BFD 3B00
06D0 16C8 0934 2654 288C 60EE A6C5 F055 6B00
06E0 6C00 2764 6400 2904 28CA 6404 1904 A637
06F0 6040 F055 601D A97C F055 A980 1872 28F2

0700 3BCC 179A 2818 6B02 28A4 F300 F318 7303
0710 3321 170A 8DB4 28A4 6B00 00EE 76FE 1722
0720 70FE 70FD 7001 4B00 173C 6305 4218 6303
0730 4210 6302 4208 6300 93A0 16FE 286E 4BCC
0740 263C 3B00 2916 2654 6B70 FB00 FB15 FB07
0750 FB18 3B00 174E A970 FA1E D673 78FF 0963
0760 4800 16EE 2876 60F0 3B03 60B0 4801 6070
0770 A615 F055 60A0 3B03 6080 4801 6060 A619
0780 F055 6042 4801 603E A635 F055 6900 C608
0790 3608 6636 6726 6A02 1682 2916 6B01 1708
07A0 7102 9170 6F00 71FE 9170 6F00 4210 17B8
07B0 7702 9170 6F00 77FE 3F00 17D8 7004 9060
07C0 1720 70FE 9060 1722 7602 9060 171C 76FE
07D0 70FD 9060 1724 7001 D015 4210 7102 6310
07E0 8323 C208 8233 4210 71FE A94E F21E D015
07F0 3F01 186E D015 4210 7102 6308 8233 4210

0800 71FE 4208 70FE A94E F21E D015 3F01 186E
0810 28F2 3B00 00EE 6BCC 6318 6526 A95A D354
0820 7309 A96B D355 00EE D673 4A00 76FE 4A05
0830 7602 4A02 77FE 4A03 7702 D673 00EE C404
0840 2848 6400 2848 6404 A97C F41E F265 401D
0850 00EE A94E F21E D015 4200 7002 4208 70FE
0860 4210 71FE 4218 7102 D015 4F01 17A0 A97C
0870 F41E F255 00EE 2654 287A 8080 A970 6119
0880 6227 D123 70FF 7106 3000 1882 6050 6212
0890 F000 F218 F215 F207 3200 1896 70F0 3010
08A0 188E 00EE A945 6316 6426 D345 631D FB29
08B0 28B6 A118 28B6 D345 7305 00EE 4B00 18C4
08C0 2916 6B00 6404 28CA 6400 A97C F41E F265
08D0 301D 00EE A966 D015 6020 F000 F018 6110
08E0 C208 3200 601A A94E F21E D015 186E 00FF
08F0 00FF D015 8540 28C4 8450 F500 F51E 7502

0900 3520 18FA 6218 601D 6110 6900 17EA 7D01
0910 6E00 6900 6B0A 292A 631A F318 A95A D344
0920 00EE 292A 7BFF 4B00 1918 6325 6426 FB29
0930 D345 00EE 93BD F888 ADAF 96BF 4D5F 199F
0940 FFO6 3A3C D420 20F8 2020 030A 0B0C 3C08
    
```



```

0950 3C00 0040 0000 7820 7800 00EF 84EF 0028
0960 3828 28E9 61D4 2828 3828 0011 0A44 0A11
0970 E080 E0A0 A0E0 20E0 0000 0000 ---- ----
0980 ---- ---- ---- ---- 7FFF FFFF FFFF FFFF
0990 4000 0000 0000 0001 5555 5555 5555 5555
09A0 4000 0000 0000 0001 57F9 3FE5 D3FE 4FF5
09B0 4400 0001 C000 0011 5555 5555 D555 5555
09C0 4400 0001 C000 0011 557D 113F FE44 5F55
09D0 4454 4400 0011 1511 556D 5555 5555 5B55
09E0 4454 4400 0011 1511 557D 157F FF54 5F55
09F0 4440 047F FF10 0111 5555 557C 1F55 5555

0A00 4440 0404 1010 0111 5551 150C 1854 4555
0A10 4444 4404 1011 1111 5155 557C 1F55 5545
0A20 4044 447C 1F11 1101 5555 117F FF44 5555
0A30 4044 0000 0000 1101 7915 5555 5555 544F
0A40 4004 0000 0000 1001 5555 3FFF FFPE 5555
0A50 4004 0000 0000 1001 57D5 5555 5555 55F5
0A60 47C4 0000 0000 11F1 57D5 13FF FFE4 55F5
0A70 4044 4000 0001 1101 5555 5555 5555 5555
0A80 4044 4000 0001 1101 7911 7FE5 D3FF 444F
0A90 4000 0001 C000 0001 5555 5555 D555 5555
0AA0 4000 0001 C000 0001 57FF D7FF FFF5 FFF5
0AB0 47FF C7FF FFF1 FFF1 5600 D7FF FFF5 F835
0AC0 460C 07FF FFF0 1831 560D 57FF FFF5 5835
0AD0 460C 07FF FFF0 1831 560D 17FF FFF4 5835
0AE0 4000 4000 0001 0001 5555 5555 5555 5555
0AF0 4000 4000 0001 0001 7FFF FFFF FFFF FFFF
    
```

Data underlined is altered by the program.

"----" = Work area.

660 SOFTWARE

disable it by changing 0963 to D4.

The object of the game is to reach the highest score by moving your man around the maze as he eats all the specks, while avoiding the Pakmen. He must attack the Pakmen at each opportunity when he is supercharged to obtain a bonus of points.

When the game starts the maze comes up on the screen and shows your score (0000) and the number of men (three). The colour of the background is green and there are two homes at the bottom of the screen where your man will start, moving either left or right. The Pakmen's home is centre top and this is where they start and return when eaten.

You have to move your man around the maze as he eats all the specks while keeping out of the Pakmen's way. If all the specks are eaten before you lose your last man a new set of specks will come up. There are 328 specks in each maze.

At each count of 100 specks eaten a sign will come up in the score box with the letter A next to it. Then your man is supercharged and you

can attack a Pakman to obtain a 100 point bonus, but you must attack *head on*. You must not eat more than nine specks or you will no longer be supercharged. There is also a time limit and when that expires the sign will disappear and you will no longer be supercharged.

Each time the Pakmen collide with each other one will return home and the sign in the score box will be a speck and cross. Once again you will be supercharged and you can attack the Pakman *head on* to obtain a bonus of 200 points. This time you will not be able to eat any specks and when the time limit expires the sign will disappear and you will no longer be supercharged.

Each time a man is eaten by the Pakmen your score will be displayed with the number of remaining men. The screen colour will change and the game will continue. When you are down to your last man, and the screen is blue, the Pakmen take one-and-a-half steps to your one; the timing periods shorten each time you lose a man.

You'll occasionally get a free supercharged 200 points. The game ends when your last man is eaten. The screen will go black and the score will flash until you press a key to restart the game.

UP key 3; DOWN key B; LEFT key A; RIGHT key C.

V0, V1 is the position of the Pakman; V2 is the direction currently travelling; V4 is the Pakman you are dealing with; V6, V7 is the position of the man; V8 sets number of men at start of game; V9 is for the timing periods to release Pakman and cancels supercharge; VA is the direction the man is travelling; VB detects bonuses, and if supercharged; VC counts number of specks eaten; VD, VE is the score; VD = 100s; VE = 0-99 count at 100 triggers VD.

There is no 00E0 in the program because the machine code subroutine at 0934 transfers the data from 0988 onwards direct to the video refresh at 0488 until register F (of the 1802) is equal to 0600 (register D = 0B00).

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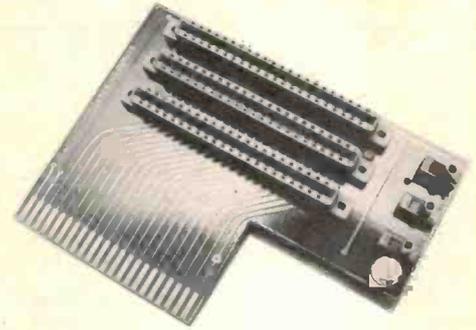
Ozi-Soft, in conjunction with Computer Technics, is offering to donate a VIC-20 expansion board for the best software item submitted to this column every month.

The board is Australian designed and manufactured and simply plugs into the VIC-20's expansion slot. It features three sockets that can be independently switch-selected, plus an on-board reset switch. With it you can plug in up to three separate expansion units to your VIC-20 and avoid the hassle of plugging things in

and out and turning the computer on and off each time. It is distributed by Computer Technics, P.O. Box 25 Kogarah NSW 2217 and costs \$59.95.

All submissions must be accompanied by a signed letter from you stating that it's your original work. The winning submission will be judged by the Editor and no correspondence will be entered into. All published submissions will be paid for.

Send entries to: **The Editor, VIC-20 Column, ETI Magazine, P.O. Box 21, Waterloo NSW 2017.**



You don't have to be good with numbers to figure out who won the VIC-20 expansion board this month. Add it up and the result is N.R. Sheehan of

Riddells Creek Vic. who wrote Multiplication, and that's the name of the game. But this is no game.

MULTIPLICATION N.R. Sheehan, Riddells Creek Vic

There are two problems which continually confront people who attempt to use small micros for complex scientific or mathematical purposes: small memories and limited precision (nine digits on the VIC-20).

This program, although slow, performs multiplication with up to 255 digit precision (the maximum length of a string variable), while minimising memory usage.

The program comprises an I/O routine (lines 10

to 220) which passes two string parameters (A\$ and B\$) to a subroutine (lines 5000 to 5170).

This subroutine counts and stores the number of decimal places in the two numbers, converts them to integers and passes them to a second subroutine (lines 6000 to 6190).

The second subroutine carries out a form of integer multiplication which results in a reversed answer (X\$). The answer is changed to the correct order (Y\$) and passed back to the calling

subroutine which restores the decimal point (if required) and returns the answer to the I/O routine.

Running times and memory usage are demonstrated in the test results.

The two subroutines can operate independent of the calling routine and could be included in any program.

The subroutines carry out no checking of either input format or overflow conditions.

MULTIPLICATION

```

100 XM=19967-FRE(1): OPEN 3,4
110 INPUT A$,B$
120 XT=TI
130 REM PASS A$, B$ TO SUBROUTINE
140 GOSUB 5000
150 REM ANSWER RETURNED IN Y$
160 PRINT#3,(TI-XT)/60;" SECONDS ELAPSED"
170 PRINT#3,A$;" * ";B$
180 PRINT#3," = ";Y$
190 PRINT#3,"PROGRAM : ";XM;" BYTES"
200 PRINT#3,"VARIABLES : ";19967-FRE(1,-XM);" BYTES"
210 PRINT#3:CLOSE 3
220 END
5000 PF=0:DP=0:LA=LEN(A$)
5010 PF=PF+1:IF MID$(A$,PF,1)<>". AND PF<LA THEN 5010
5020 IF MID$(A$,PF,1)<>". THEN AI$=A$:GOTO 5060
5030 I=PF-1:AI$=LEFT$(A$,I)
5040 IF PF=LA THEN LA=LA-1:GOTO 5060
5050 DP=LA-PF:AI$=AI$+RIGHT$(A$,DP):LA=LA-1
5060 PF=0:LB=LEN(B$)
5070 PF=PF+1:IF MID$(B$,PF,1)<>". AND PF<LB THEN 5070
5080 IF MID$(B$,PF,1)<>". THEN BI$=B$:GOTO 5120
5090 I=PF-1:BI$=LEFT$(B$,I)
5100 IF PF=LB THEN LB=LB-1:GOTO 5120
5110 BI$=BI$+RIGHT$(B$,LB-PF):DP=DP+LB-PF:LB=LB-1
5120 GOSUB 6000
5130 REM INPUT ARGUMENTS = AI$,LA,BI$,LB
5140 REM OUTPUT = Y$
5145 IF DP=0 THEN 5170
5150 I=LEN(Y$)-DP
5160 Y$=LEFT$(Y$,I)+". "+RIGHT$(Y$,DP)
5170 RETURN
6000 X$="" : Y$=""
6010 FOR K=0 TO LB-1
6020 CA=0:I=LB-K
6030 FOR H=0 TO LA-1
6035 J=LA-H
6040 M=VAL(MID$(BI$,I,1))*VAL(MID$(AI$,J,1))+CA:CA=0
6050 IF M>9 THEN CA=INT(M/10):M=M-CA*10
6060 TC=H+K+1
6070 IF LEN(X$)<TC THEN X$=X$+RIGHT$(STR$(M),1):GOTO 6120

```

```

6080 XI=VAL(MID$(X$,TC,1))+M
6090 IF XI>9 THEN XC=INT(XI/10):XI=XI-XC*10:CA=CA+XC
6100 LE=TC-1:RI=LEN(X$)-TC
6110 X$=LEFT$(X$,LE)+RIGHT$(STR$(XI),1)+RIGHT$(X$,RI)
6120 NEXT H
6130 IF CA>0 THEN X$=X$+RIGHT$(STR$(CA),1)
6140 NEXT K
6150 I=LEN(X$)-
6160 FOR K=0 TO I-1
6170 J=I-K:Y$=Y$+MID$(X$,J,1)
6180 NEXT K
6190 RETURN

```

READY.

```

.166666667 SECONDS ELAPSED PROGRAM : 1376 BYTES
3 * 3 VARIABLES : 174 BYTES
= 9
PROGRAM : 1376 BYTES
VARIABLES : 132 BYTES
.783333333 SECONDS ELAPSED
3333 * 33 = 109989
PROGRAM : 1376 BYTES
VARIABLES : 178 BYTES
.25 SECONDS ELAPSED
3 * 33 = 99
PROGRAM : 1376 BYTES
VARIABLES : 136 BYTES
.25 SECONDS ELAPSED
33 * 3 = 99
PROGRAM : 1376 BYTES
VARIABLES : 136 BYTES
.45 SECONDS ELAPSED
33 * 33 = 1089
PROGRAM : 1376 BYTES
VARIABLES : 170 BYTES
.616666667 SECONDS ELAPSED
333 * 33 = 10989
PROGRAM : 1376 BYTES
VARIABLES : 185 BYTES

```



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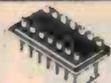
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DA 15P	15 PIN MALE	4.50	4.20	3.90
DA 15S	15 PIN F MALE	5.10	4.90	4.70
DA 15C	15 PIN COVER	2.30	2.10	2.00
DB 25P	25 PIN MALE	5.90	5.60	5.10
DB 25S	25 PIN F MALE	6.90	6.60	6.10
DB 25C	1 pr Grey Hood	2.40	2.20	2.00
DB 25C2B	2 pr Black Hood	2.80	2.70	2.50
DB 25C2G	2 pr Grey Hood	2.70	2.50	2.40
DC 37P	37 PIN MALE	7.90	7.50	7.10
DC 37S	37 PIN F MALE	10.90	9.90	9.10
DC 37C	37 PIN COVER	4.90	4.50	4.10
DH S	Hardware set (2 Pairs)	2.10	1.90	1.80

RITRON DIGITAL MULTIMETERS



Q16010 specifications

1-4	5+
\$59.95	\$54.95

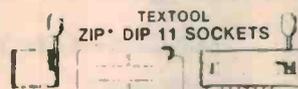
Q1704Q specifications

1-4	5+
\$89.95	\$84.95

- 28 Ranges
- Push Button Operation
- Auto Polarity
- Low Battery Indicator
- Full Overload Protection
- Finger Guards on Probes and Shrouded Plugs for Safety
- Accuracy: 1 year 18°C to 28°C (+ % of reading + No. of Digits) 200 hour battery life

Range	Resolution	Accuracy	Function
V _{DC}	0.1-1000	±0.5%	DC
V _{AC}	0.1-1000	±1.0%	AC
Ω	0.1-1000	±1.0%	Ω
Hz	0.1-1000	±1.0%	Hz
Cap	0.1-1000	±1.0%	Cap
Ind	0.1-1000	±1.0%	Ind
Temp	0.1-1000	±1.0%	Temp

Range	Resolution	Accuracy	Function
V _{DC}	0.1-1000	±0.5%	DC
V _{AC}	0.1-1000	±1.0%	AC
Ω	0.1-1000	±1.0%	Ω
Hz	0.1-1000	±1.0%	Hz
Cap	0.1-1000	±1.0%	Cap
Ind	0.1-1000	±1.0%	Ind
Temp	0.1-1000	±1.0%	Temp



16 Pin Zip* Dip 11	\$11.50
24 Pin Zip* Dip 11	12.50
40 Pin Zip* Dip 11	17.50

*Zero Insertion Pressure

DIP SWITCHES SPST

P N	No of Switches	Price
SD3	3	\$1.60
SD4	4	1.70
SD5	5	1.90
SD6	6	2.30
SD7	7	2.40
SD8	8	2.50
SD9	9	2.70
SD10	10	3.00

DIP SWITCHES SPST



cermet single TURN TRIM POT

Spectral model 63P ACTUAL SIZE

STOCK VALUES	
10R 20R 50R 100R 200R 500R 1K	
2K 5K 10K 20K 50K 200K 500K	
1M 2M	

1 9	\$1.20
10 99	\$1.00
100	\$0.90

Values may be mixed.

HEATSINKS

High Thermal Capacity Black Anodised

Model	1-4	5-9	10-49	50-99	499 plus
HS1 - 38mm	1.85	1.75	1.50	1.35	1.00 0.90
HS2 - 75mm	3.00	2.90	2.50	2.00	2.00 1.50
HS3 - 150mm	5.80	5.40	4.90	3.80	2.90 2.70
HS4 - 225mm	8.10	7.60	7.10	5.90	4.50 4.30
HS5 - 300mm	8.90	8.40	7.90	6.50	4.90 4.60

Unanodised

Model	1-4	5-9	10-49	50-99	499 plus
HS11 - 38mm	1.40	1.20	1.00	0.90	0.80 0.70
HS12 - 75mm	2.50	2.20	1.90	1.60	1.25 1.20
HS13 - 150mm	4.90	4.50	4.00	3.20	2.45 2.40

BLANK CASSETTES T.D.K.

TDK ADC60	1 for \$3.60	10 for \$26.00
TDK DC60	1 for \$2.10	10 for \$18.00
TDK DC60	1 for \$3.50	10 for \$31.00
TDK SAC60	1 for \$3.50	10 for \$31.00
TDK SAXC60	1 for \$5.70	10 for \$46.00
TDK DC90	1 for \$2.40	10 for \$21.00
TDK ADC 90	1 for \$3.50	10 for \$30.00
TDK SAC 90	1 for \$4.20	10 for \$39.00
TDK DDC90	1 for \$4.70	10 for \$45.00
TDK SAXC90	1 for \$5.50	10 for \$49.00
TDK DC120	1 for \$4.50	10 for \$37.00
TDK ADC120	1 for \$5.40	10 for \$46.50

Post & Pack \$2.50 small kits, heavier kits add extra postage.

Prices subject to change without notice. Send 60c and SAE for free price list and inclusion on all future mailing lists.

MAIL ORDERS: PO Box 235, Northcote, Vic 3070. Min P & P \$1.00.

Ph: (03) 489 8131. ERRORS AND OMISSIONS EXCEPTED

ROD IRVING ELECTRONICS

425 HIGH STREET, NORTHCOTE 3070, MELBOURNE, VICTORIA. Ph (03) 489 8131 Telex No. 38897
48-50 A'BECKETT STREET, MELBOURNE (03) 347-9251

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Mail Orders
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Please debit my Bankcard.

Bankcard No.

Expiry Date

Name

Signature



NEW STORE
opening September
HURSTVILLE

NEW STORE CHECK



WE ARE PROUD TO ANNOUNCE THE OPENING OF HURSTVILLE. TO CELEBRATE THE EVENT, WE ARE HAVING A GIANT SALE!

Robot Turtle *Hebot II* Save 20%!

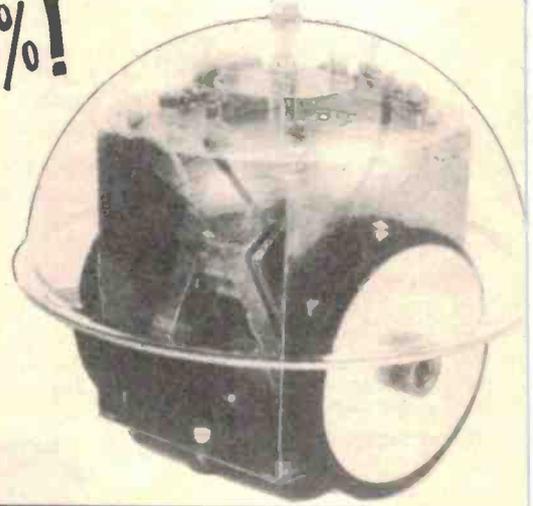
The HEBOT 11 turtle is not just a fun device, it is a positive aid to education. It takes programming out into the real 3 dimensional world instead of the flat two dimensional world of the VDU. When connected to the I/O ports of your computer and given a DC supply of 9-15V the turtle runs around under computer control moving forwards, backwards, right and left with independent control of each wheel. It has blinking eyes, will beep with a choice of two tones and when ordered by the computer, presses down a pen to chart its progress and provide hard copy of the results of the program. When set free to run around the turtle discovers its environment. When the turtles shell bumps into an unmovable obstacle touch sensors send back data to the computer for it to calculate evasive or exploratory action.

If the computer has no I/O ports it doubtless has an expansion bus and the turtle can be controlled and listened to using this bus together with the universal computer interface board. This board enables the turtle to be treated as a memory mapped I/O device.

COMPLETE "HEBOT II" UNIVERSAL INTERFACE \$39⁵⁰
KIT INCLUDING ALL HARDWARE, DOME, WHEELS etc. Cat. XR1020

SEPTEMBER ONLY

~~\$399~~ inc tax **\$319**



1/4" TAPE

2500' - 1.5 mil
Cat. AL-1560

3600' - 1.0 mil
Cat. AL-1561

\$19⁹⁵

FABULOUS TAPE SENSATION

Amazing Quality

Jaycar has done it again - for all of the Hi Fi buffs who have professional NAB centre reel-to-reel tape recorders - a superb METAL spool complete with either 2500' or 3600' of quality tape. Both tapes are priced the same, the only difference between tape lengths is the thickness of the tape itself. The 3600' tape is 1.0 mil thick and the 2500' tape is 1.5 mil thick. You make your choice from these two superb bargains. The spool size is 10%"

Only a few left!

EXPERIMENTER'S MAGNET KIT

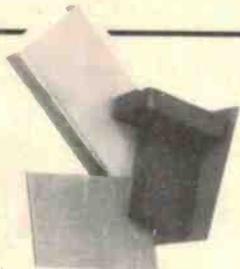
Magnets never cease to amaze - yet most of us know very little about them.

With this in mind Jaycar has had a special "Magnet Kit" produced. The kit contains: 2 very powerful Ceramic magnets, flux concentrator, pole pieces and a short manual written by experts in magnetism. Magnet experiments are also shown as well as a technique to actually make your magnets stronger!!
Cat. KJ6512

MAGAZINE BINDER LOW IMPORT PRICE

Keep your precious (and expensive) magazines in order for easy references. Smart blue colour with gold lettering. Heavy gauge and richly chromed metal fittings.
Cat. BB7000

ONLY \$4.95 \$3.96 LESS 20%
4 up \$4.50 ea \$3.60 SEPT. ONLY



EA PHOTON TORPEDO KIT

EA "Photon Torpedo" Kit - NEW LOW PRICE
Ref: EA September 1981
This great kit comes complete with Jiffy box and front panel featuring "Deep Space" background. We've seen this kit selling for up to \$29.95 - NOT from this month!!
ONLY \$19.95. Be quick. Why not buy one, build it, and give it as a gift to a young one?
Cat. KA-1370

\$19.95

\$19.95

ONLY **\$4⁹⁵**

SEPTEMBER ONLY

\$3.95 SAVE \$1



SPECIALS- US OUT! * * *

OUR NEW SHOWROOM AT 121 FOREST ROAD
YOU CAN GRAB THESE BARGAINS AT ANY OF OUR STORES THOUGH!

NEW STORE
Opening September
HURSTVILLE

low cost hi fi

FROM
\$19.98



Woofers not to same scale as other components

That's right a 3-WAY HI FI speaker kit from only \$19.98!! Each kit contains a massive 10" (250mm) woofer, cone midrange and DOME tweeter!! You also get, at no extra charge, the special cross-over capacitors!
The system is rated at approximately 20 watts RMS so it is ideal as an economical but reasonably powerful main HI FI unit or as a second system for another room or outdoors.
Each 3-way kit comes with a recommended enclosure design which you can build yourself easily!
You would normally pay well over \$60 for the equivalent from major kit speaker suppliers so this is an outstanding bargain. Sensitivity of system 93dB/1m/1 watt. Cat. AK3700
HURRY LIMITED STOCKS and they are made in JAPAN!!

3-WAY SYSTEM
\$24.95 a set

2 SETS FOR STEREO (6 spkrs)
ONLY \$39.95

codemaster

Many of you know the clever parlour game that uses coloured tokens to stretch the brain to work out a hidden code in a minimum number of moves.
The people that came up with the game used a descriptive name which no-one else can use. It is a popular game and is well known under this name. Our game is similar to this game but - naturally - its electronic!! And, what's more, you can play against the machine - alone.
Each XM7015 Codemaster measures 140(l)x85(w)x25(d) looks similar to a pocket calculator and runs off a standard 9V cell. Provision is made for a mains adaptor as well.
The Codemaster once sold for \$29.50 but Jaycar has made a huge scoop purchase. You save a fortune!
Grab one now for only \$4.98
* (For a further clue to the origin of this game read this page carefully)



WERE
\$9.95

ONLY

\$4⁹⁸

low cost IC inserters

AND
EXTRACTORS

Up until now these have cost a fortune!!

Features:

- CMOS SAFE conductive plastic
- Exclusive bent pin alignment guides in handle . 8 to 40 pins.
- Ground strap can be connected.
- One hand operation.

INSERTERS

Cat. No	Model	Description	Normally	Sept. Only
TH1810	CIT820	8 - 20 pin	\$5.95	\$4.95
TH1812	CIT22	22 pin	\$6.50	\$5.50
TH1814	CIT2428	24 - 28 pin	\$6.95	\$5.95
TH1816	CIT3640	36 - 40 pin	\$8.95	\$7.50

EXTRACTOR

Deceptively simple looking device. One piece metal construction. 8-40 pins

Cat. No	Model	Normally	Now
TH1818	ET480	\$2.95	\$2.50

IMPORTANT!!

Don't be conned into buying a non conductive inserter/extractor. The possible static damage to your MOS I.C.'s could cost you a fortune!!



HEAVY DUTY MAINS FILTER

There are an enormous number of Desk-top micros now having problems with mains borne interference. Our MS4004 filter has been invaluable where mains interference is a problem. When a free standing unit is required the MS4004 is ideal. It will pass 2 amps (conservative) at 240V AC. This unit is a grey painted metal case that plugs into a standard mains socket. On one end of the case is an unswitched 240V outlet. Virtually the only thing that comes out of this socket is mains. All frequencies above 50Hz are very heavily attenuated. Ideal for problem areas.
Cat. MS-4004

\$99.00



MOTOROLA SILICON RECTIFIER MANUAL

This totally underrated book of around 500 pages & 17 chapters describes diode and rectifier theory in great detail. Typical chapter headings include: Basic Electrical Characteristics of Diodes, Basic Thermal Properties of Semiconductors, Rectifier Specifications & Ratings, Rectifier Filter Systems, Rectifier Voltage Multiplier Ccts, Transient Protection of Rectifier Diodes, Selector Guide, Data Sheets and more. A must for the serious electronic enthusiast as well as the design engineer. Cover dimensions: 235 x 177mm
Cat. BM-420B

ONLY \$5.95

VOYAGER CAR COMPUTER ICE WARNING UNIT

SAVE \$10!

ONLY
\$19⁹⁵

Do you buy a hot water bottle in December?
Hundreds of 'Voyager' Car Computers are now operating all over Australia. A feature of the European model was an 'Ice Warning' unit. This device, fitted in the engine bay near the radiator grille, detected conditions that led to icy roads - particularly dangerous 'black ice'. We felt that the extra cost of this unit was not justified in the standard Australian model. Many people have asked for it however.
We should have advertised these 3 months ago in the winter but we forgot!! Now its almost summer and Voyager users in the colder areas probably won't need one for another 6 months!! So we're slashed \$10 (or 1/3rd) off the normal price to encourage you to buy now.
Normally \$29.95. This month \$19.95 - instructions included. Easy fitting. Can be used as basis for ice warning system without Voyager car computer.
Cat. XC-2028

\$19.95

Jaycar NUMBER 1 FOR KITS

SYDNEY SHOWROOM

125 YORK STREET - PHONE: (02) 264 6688
TELEX: 72293

HURSTVILLE SHOWROOM

121 FOREST ROAD - PHONE: (02) 570 7000

CARLINGFORD SHOWROOM

Cnr. CARLINGFORD & PENNANT HILLS ROAD
PHONE: (02) 872 4444

MAIL ORDERS & CORRESPONDENCE

BOX K 39 HAYMARKET, SYDNEY 2000

POST AND PACKING CHARGES

\$5 - \$9.99 (\$1.50) \$10 - \$24.99 (\$3.20)

\$25 - \$49.99 (\$4.50) \$50 - \$99.99 (\$6.50)

\$100 - \$198 (\$8.00) Over \$199 (\$10)

"Free Insurance for Road & Registered post over \$200"

SHOP HOURS CARLINGFORD & HURSTVILLE

Mon - Fri 9am - 5.30pm; Sat - 9am - 12pm; Thurs night 8.30pm

SHOP HOURS SYDNEY

Mon - Fri 8.30am - 5.30pm; Sat - 8.30am - 12pm; Thurs night 8.30pm



Mail Order By

BANKCARD

Via Your Phone

NEOTRONICS MARKETS HIGH-PERFORMANCE 'SCOPE

Neotronics OS620 high-performance oscilloscope, just released on the market, features dual-trace operation and incorporates a 150 mm square CRT with internal graticule.

The acceleration voltage of the South Korean-made unit, specially built for Neotronics, is 2 kV.

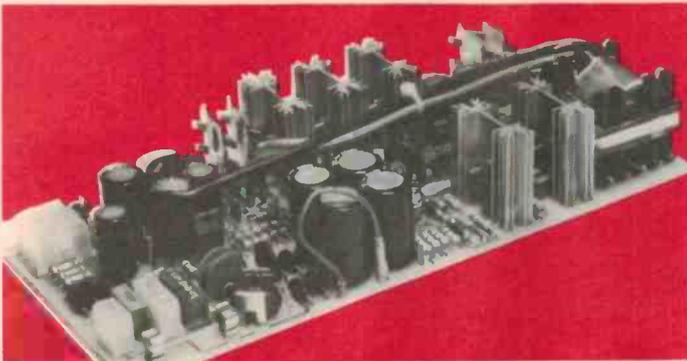
Ideal for television work, the trigger circuit incorporates a line and frame synch separator, allowing both frame and line pulses to be displayed.

The component tester is a special circuit which checks components either in or out of circuit without the need for external voltages. The results

are displayed on the screen.

A sensitivity of 5 mV/cm and a maximum input voltage of 600V p-p allows a large range of voltages to be measured. Also featured are an add mode, which can be used to add or subtract A and B input signals, and a Z-modulation mode.

For further information, contact Neotronics P.O. Box 289, Newport, NSW 2106. (02) 918-8220.



POWERFUL TWO-CHANNEL FFT ANALYSER FROM SD

Menu-driven with full annotation facilities, Spectral Dynamics' new SD375 two-channel FFT analyser can be used as a signal correlator for time, amplitude and frequency up to 100 kHz.

The SD375 FFT is also a transfer function analyser for mechanical, electrical, acoustic and hydraulic measurements, while Modal Analysis Engineering software programs can utilise it as a processor.

Options available are a digital

translator (up to x100 zoom), 1/3 and 1/1 octave analysis, digital I/O and a synchronous signal generator for external system or network excitation.

Vipac Instruments provides full service support for the SD375 and training and application support is readily available.

For further details, contact Vipac Instruments, 30 Claremont Street, South Yarra, Vic. 3141. (03)240-8471.

MULTI-RAIL POWER SUPPLY

Power-supply specialist firm Scientific Electronics has two new multi-rail power supplies, the five-rail SM80AE1 and the four-rail SM80AE2.

Designed and manufactured by Scientific Electronics to meet Telecom specification 1302, the new multi-rail switch-mode supplies offer 80 W total output and high reliability in small packages.

Standard output voltages are available, as well as output rails to customer specifications.

The five rails on the standard-model SM80AE1 are +5 V at 8 A continuous, +12 V at 2.5 A continuous, +24 V at 0.2 A continuous, -5 V at 0.5 A continuous and -12 V at 1.0 A continuous.

The four rails on the

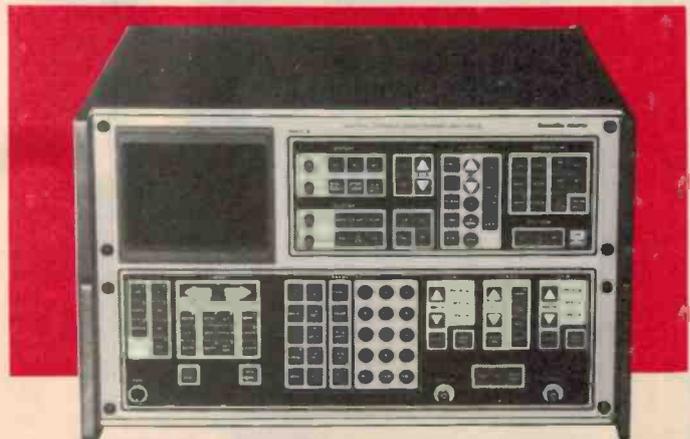
standard-model SM80AE2 are +5 V at 8 A continuous, +12 V at 2.5 A continuous, -5 V at 0.5 A continuous and -12 V at 1.0 A continuous.

All outputs on both units are short-circuit protected, and the +5 V and the +12 V outputs have overvoltage protection.

Total allowable output power is 80 W continuous, 100 W peak. Isolation is greater than 3.5 KV and efficiency greater than 60% at full load.

The units measure 108 x 240 x 45 mm and are fully supported by a five-year warranty and complete local technical back up.

For further information, contact Scientific Electronics, 6 Holloway Drive, Bayswater Vic. 3153. (03)762-5777.



JAYCAR

Sparkrite

The Brandleaders in Auto Electronics



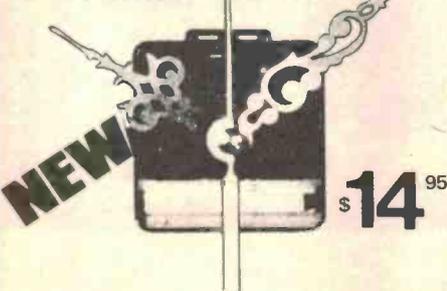
Sparkrite SX2000

- A Reactive Discharge System combines all features of the SX500 plus:
- Reactive Discharge electronics combining all the advantages of both Inductive and Capacitive Discharge for maximum spark performance.
 - Gives the most thorough combustion of air/fuel ratios especially current lean mature emission controlled engines.
 - Voted 'Accessory of the Year' and the best as tested by Popular Motoring Magazine.
 - Patented clip-to-coil fitting.
 - Systems Function Light as well as Static Timing Light.
 - The ultimate brand leading contact-breaker triggered system.

\$59 SAVE **\$10** **\$49**

Quartz Crystal Clock movement

Cat. XC6000



\$14.95

- Very compact and reliable
 - Self-starting one-second stepping motor has strong torque
 - Powered by 1.5V AA battery that lasts for a year
 - Supplied with two sets of hands, one short and one long
 - ±15 second/month accuracy
 - 56mm square, 15mm deep
- Complete with data sheet, instructions and wall hanger bracket.

IEC Cable Connectors

INCREASED RANGE



Most imported equipment these days now uses IEC-320 style AC power inlet connectors. Indeed, the electronics mags will soon be specifying these connectors on many of their mains-powered projects to simplify (and therefore make safer) mains wiring. Jaycar now stocks a range of ELECTRICITY AUTHORITY APPROVED mains line cords. We have them in straight entry, left and right entry with and without standard 240V mains moulded plug. Each cord is a generous 2 metres long and is rated at 7.5 amp continuous.

Cat. No	Description	Price
PS4302	LINE CORD STRAIGHT ENTRY 2M	\$3.95
PS4304	LINE CORD R/HAND ENTRY - 2M	\$3.95
PS4305	LINE CORD L/HAND - 2M	\$3.95
PS4306	LINE CORD STRAIGHT ENTRY WITH 240V PLUG 2M	\$4.95
PP2302	IEC 320 CHASSIS PLUG	\$2.95
WM4530	2 PIN 240V PLUG MOULDED TO 2M FIG. 8 7.5 AMP CORD - BLACK IN COLOUR (Note: the first 5 items are grey in colour)	\$2.95

50V/5A laboratory power supply



Ref: EA May/June 1983
By far the most exciting high power supply we have seen! Using the latest switch mode principle, very little energy is wasted with high dissipation in the regulators - a cause of considerable heat dissipation and high hardware costs. The Jaycar kit comes with every originally specified component down to the last nut and bolt. Also included are special Scotchcal meter scales. Beware of inferior kits that do not supply such components. (Not for sale as a separate item).
Cat. KE-1520 **\$149.00**

This handy 200 gram spray enables you to do all manner of things. You can spray sheets of Styrene foam and make them suitable for storing your MOS IC's. Far cheaper than other methods!! You can make conducting screens inside plastic boxes to shield RF. You can re-coat the back of CRT's. You can make conductive parts of equipment cabinets to reduce static. The paint dries to a hard varnish like film. Non-inflammable and Non toxic. Grab a can now. You never know when you will need it!
Cat. NA-1010 - \$6.95

SPRAY ON CONDUCTIVE PLASTIC...

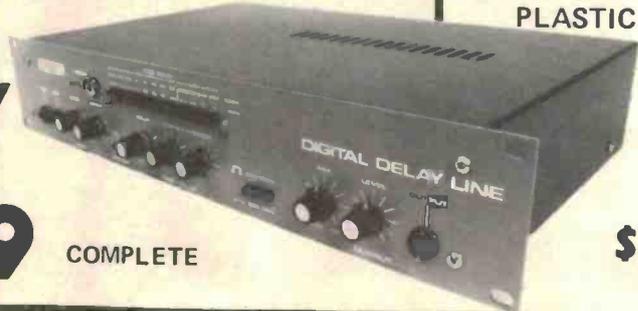


Digital Delay Line Kit

400ms VERSION ONLY

\$449

COMPLETE



\$6.95

The Digital Delay Line is designed to produce a huge variety of electronic effects. It works very well but the amazing thing is the low low price! The effects depend on the time delay selected and some of those included are: Phasing, Flanging, Chorus, ADT (Automatic Double Tracking), Echo, and Vibrato. The delay time can be varied from 0.32ms to 1.6 seconds! Because the signal is stored in digital form there is, unlike analog systems, no degeneration of the signal with time and unlimited repetition is provided by use of the freeze control.

All the controls mount directly upon PCB's to eliminate wiring and to further simplify construction the main board is 'plated-through' i.e. there are no wire links or link-through pins. The whole of the memory whether for the basic 400ms machine or the fully expanded 1.6 second model all fits on the main board. The cabinet which is free standing but also suitable for 19" rack mounting, is fully finished to a very high standard. The panel is deep blue whilst the cover is sprayed with a durable black enamel. The kit is available for only \$449 - compare that with inferior units that can cost over \$2,000!!
Cat. KJ6621 **\$449.00**

FM Transmitter Module

We have been working on this one for years!! Basically we wanted something akin to the \$6.50 kit "wireless microphone" transmitter but with greater signal strength and far, far greater frequency stability.

WE NOW HAVE IT!
Basically the (dotted) unit measures a small 90 x 22 x 15mm and has connections for power, antenna and input. An AC signal between 20 and 15kHz will modulate the transmitter. The signal can be coded single or multiple frequency tone bursts etc.

- FEATURES**
- Ultra low noise output (-60dB or better attainable with a suitable tuner)
 - Excellent frequency stability
 - Not a kit - ready for immediate use
 - Connections required
 - (a) Power supply or battery
 - (b) Antenna
 - (c) Audio input
 - Full instructions supplied
 - Suits any application where a stable low noise FM link is required

- SPECIFICATIONS**
- Frequency - 88 - 108MHz adjustable
 - Usable range - 50 metres
 - Supply - 6 to 9V at 20mA
 - Input sensitivity - adjustable - maximum 30mV
 - Pre-emphasis - 50µs/second standard
 - Dimensions - 90 x 22 x 15mm (approx)

\$49.95 Cat. DT5450

LOW COST DIGITAL MULTIMETER KIT

Ref: EA March 1983 (This month). Almost everybody we see asked for a multimeter kit. Up until now we thought that it was just not worth it considering the fine low-cost built-up units available. The DP2010 changed all that. This kit, fully imported from the UK, uses the famous DPM-88 custom LCD/Multimeter to achieve phenomenal accuracy at very modest cost! All parts are included to complete the meter, including an attractive and colourful front panel. (A 9V battery is required).

Set of test probes to suit **\$2.95**
Probe to suit Cat. WTS312 **\$2.50**
Eveready 216 (free!) 9V Battery Cat. SB2370 **ONLY \$1.40**

DP2010 kit Cat. KJ710 **ONLY \$45**

SPECIFICATIONS

Function	r.e.d.	Resolution	Accuracy	Protection
Volts (d.c.)	2V	1mV	1%±1 digit	500V for one minute
	20V	10mV	1%±1 digit	500V for one minute
	200V	100mV	1%±1 digit	500V for one minute
	500V	1V	1%±1 digit	500V for one minute
Current (d.c.)	2mA	1µA	1%±1 digit	1A/250V
	20mA	10µA	1%±1 digit	1A/250V
	200mA	100µA	3%±1 digit	1A/250V
	2000mA	1mA	5%±1 digit	1A/250V
Volts (a.c.)	2V	1mV	2%±5 digit	500V for one minute
	20V	10mV	2%±5 digit	500V for one minute



45 ONLY

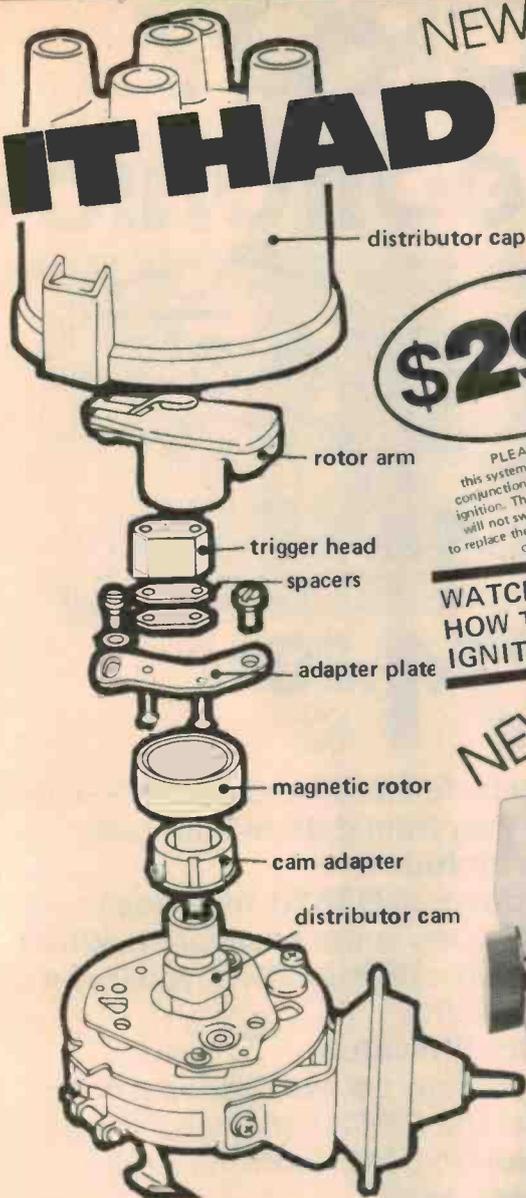
\$39.95
SAVE OVER **\$5.00!**

AC VOLTAGE AND CURRENT RANGES: When SA selects a.c. functions the output from either the voltage attenuator or current shunt is fed through CI to remove any d.c. component.

Function	r.e.d.	Resolution	Accuracy	Protection
Current (a.c.)	200V	100mV	2%±5 digit	1A/250V
	500V	1V	2%±5 digit	1A/250V
	2mA	1µA	2%±5 digit	1A/250V
	20mA	10µA	2%±5 digit	1A/250V
Resistance	2K	1	1%±1 digit	260V
	20K	10	1%±1 digit	260V
Diode Test	200K	1K	1%±1 digit	260V
	2V	1mV	1%±1 digit	260V

IT HAD TO HAPPEN

NEW



\$29⁹⁵

PLEASE NOTE
this system must be used in conjunction with an electronic ignition. The Hall Effect device will not switch enough current to replace the contact breaker points on their own!

A professionally-engineered electronic ("breakerless") contact breaker system. Yes, only Jaycar has a complete Hall-effect triggerhead assembly designed to adapt to an extensive number of cars. Each kit contains the following:

- HALL EFFECT TRIGGER HEAD
 - MAGNETIC ROTORS FOR BOTH 4 & 6 CYLINDER CARS
 - OVER 6 CAM-LOBE ADAPTORS
 - OVER A DOZEN DIFFERENT ADAPTOR PLATES FOR YOUR PARTICULAR DISTRIBUTOR
 - OTHER HARDWARE (i.e. SCREWS etc.)
- YOU CAN REMOVE THIS SYSTEM AND RE-EQUIP YOUR CAR WITH THE ORIGINAL BREAKER POINTS WHEN YOU SELL THE CAR! AS EASY TO INSTALL AS A SET OF POINTS! INSTRUCTIONS (SIMPLE TO FOLLOW) INCLUDED!

This set is designed to fit most European and Japanese cars. In fact it will also fit many Australian cars fitted with Lucas, Bosch, Motocraft, AC Delco or Autolite electrics. If you wish to check first, please send SAE for car/distributor list.

Because we have no way of knowing, you get the fitting set for ALL of the distributors available. Basically you end up with a jar full of parts that you don't need to use! (Perhaps for your next car?)

Quite frankly, we are amazed that we can supply such a comprehensive kit for this price. To produce a kit that will adapt to the dozens of different distributors around is amazing!

Remember, once you have installed a breakerless system it will never wear out and that part of your system will remain in tune FOR EVER.

We expect this kit to sell well. To ensure that you receive one, check with us early!

Cat. KJ6855

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FUNCTIONAL SPECIFICATIONS

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Printing format: Alpha-numeric - 7 x 8 in 8 x 9 dot matrix field
Semi-graphic (character graphic) - 7 x 8 dot matrix
Bit image graphic - Vertical 8 dots parallel, horizontal 640 dots serial/line
2.1mm (0.083") W x 2.4mm (0.09") H/7 x 8 dot matrix
228 ASCII characters, Normal and Italic alpha-numeric fonts, symbols and semi-graphics
80 CPS, 640 dots/line per second
Line feed time: Approximately 200msec at 4.23mm (1/16") line feed
Printing direction: Normal - Bidirectional, logic seeking
Superscript and bit image graphics - Unidirectional, left to right
Normal - 640 dots/190.5mm (7.5") line horizontal, Compressed characters - 1,280 dots/190mm (7.5") line horizontal
Normal - 4.23mm (1/16")
Programmable in increments of 0.35mm (1/72") and 0.118mm (1/216")
Columns/line: Normal size - 80 columns
Double width - 40 columns
Compressed print - 142 columns
Compressed/double width - 71 columns
The above can be mixed in a line
Adjustable sprocket feed and friction feed
Paper feed: Fanfold, Single sheet. Paper width - 101.6mm (4") to 254mm (10")
Paper type: Original plus 3 copies by normal thickness paper
Number of copies: MECHANICAL SPECIFICATIONS
Ribbons: Cartridge ribbon (exclusive use), black
MTBF: 5 million lines (excluding print head life)
Print head life: Approximately 30 million characters (replaceable)

INTERFACE SPECIFICATIONS

- Interface: Standard Centronics parallel
Data transfer rate: 4,000 CPS max.
Synchronization: By external supplied STROBE pulses
Handshaking: By ACK/NLG or BUSY signals
Logic level: Input data and all interface control signals are TTL level
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RAM: 16K, 8K, 4K, 2K, 1K, 512, 256, 128, 64, 32, 16, 8, 4, 2, 1, 512, 256, 128, 64, 32, 16, 8, 4, 2, 1
BASIC: More than 90 instructions stronger than those for Apple II
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Text, low-resolution graphics, high-resolution graphics (3 modes are mixed)
950 characters/128 lines, 40 columns
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Connects to color TV or video display
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SEE PAGE 77 FOR JAYCAR ADDRESSES AND PHONE NUMBERS

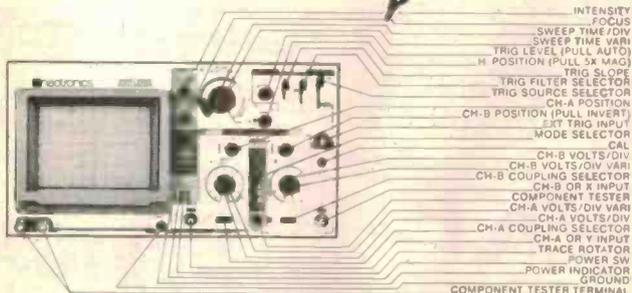
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- CAL
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- CH-B COUPLING SELECTOR
- CH-B OR Y INPUT
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- CH-A VOLTS/DIV
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LOW-DROPOUT DUAL VOLTAGE REGULATOR

National Semiconductor's linear products group has released the LM2935 low-dropout dual regulator, the first dual-output regulator of its kind to provide up to 750 mA.

The LM2935 regulator operates with extremely low input-output differentials (less than 0.6 V to 0.5 A) and maintains a low quiescent current of 3 mA or less when supplying 10 mA loads from the standby regulator output.

The LM2935 is equipped with two regulated 5 V outputs. The first output is capable of regulating 750 mA and the second provides standby low-current of 10 mA. The device has an on/off switch for the high-current output.

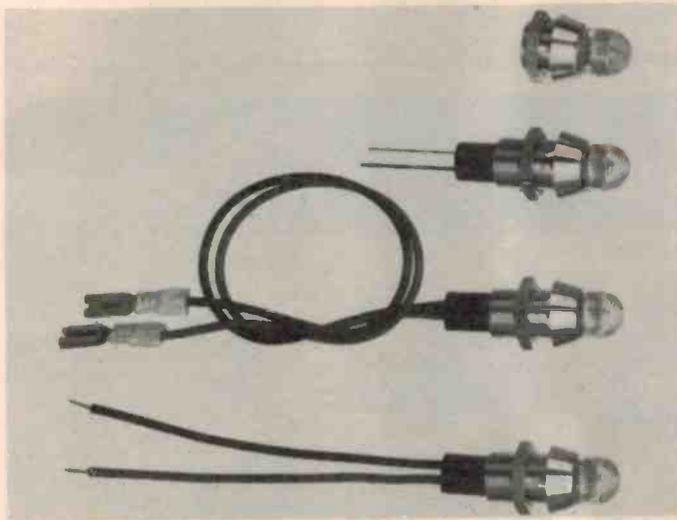
Other features include short-circuit protection and thermal overload protection.

Suited for applications in the

automotive industry, the regulator safeguards against reverse battery installations and two-battery jumps, and provides 60 V load dump and -50 V reverse transient protection.

During line transients, the LM2935 will automatically shut down to protect both the internal circuit and the load while the standby regulator continues to power any standby load. The device cannot be harmed by temporary mirror-image insertion.

For more information, contact **National Semiconductor, Cnr Stud Road and Mountain Highway, Bayswater Vic. 3153. (03)729-6333.**



ULTRABRIGHT INDICATOR LAMP FROM SLOAN

Sloan of Switzerland has released its new Series 176 indicator lamp range.

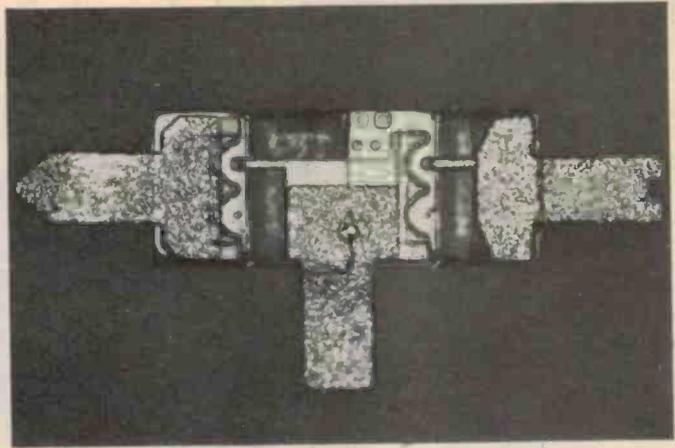
The indicator's front-panel presentation has a machined, chrome-plated body and bezel with high-dome plastic lens. The lens, designed with Fresnel Rings, allows 180° visibility and the ultrabright version offers brightness levels of up to 500 mcd.

The standard terminals are

0.6 mm square-section wire wrap, though insulated stranded-wire variations are available to customer specification.

The operating voltage is nominally about 1.7 V to 2 V; 'built-in' resistor versions can be obtained for a range of voltages from 5 V to 28 V.

For further information, contact **C&K Electronics, 15 Cowper Street, Parramatta NSW 2150. (02)635-0799.**



MICROWAVE SCHOTTKY BEAM LEADS IN PAIRS

Microwave Schottky beam leads in pair configuration, with a guaranteed maximum capacitance of 0.10 pf, are now being offered by Hewlett-Packard.

The low capacitance enables the designer to achieve a low-noise figure (7.0 dB maximum at 16 GHz) for systems operating at high frequencies.

The Hewlett-Packard beam leads utilise a tri-metallisation process that produces repeatable, reliable diodes capable of operating within a temperature range of -60 to +200°C.

Exceptional beam strength is achieved without sacrificing capacitance, using a glass-fill pro-

cess that produces beam-pull results of six grams (typical).

Intended for use in balanced and double-balanced mixers, the HSCH-5500 series beam-lead pairs are designed to address the needs of the high-performance/high-frequency mixer marketplace.

Some typical applications include satellites, microwave receivers, EW wide-band signal processing and guidance control.

For more information, contact **Hewlett-Packard Australia, 31-41 Joseph Street, Blackburn Vic. 3130. (03) 890-6351.**

HIGH-SPEED DIGITAL SPEED CONTROLLER

A new digital motor speed-controller circuit designed to maintain brushless three-phase dc motors at their required speed with an accuracy of 0.1%, and to bring them up to that speed at maximum torque, has been announced by LSI Computer Systems.

The circuit's voltage range is 10-28 V, covering the range of most popular brushless dc motors, such as those used in rotating memories.

The new chip, designated the LS7263, is optimised for motors operating at 3600 rpm when used with a 3.58 MHz crystal.

By using a 2.6 MHz crystal, it can be used to control motors operating at 5400 rpm.

The chip is also mask programmable for a wide range of loads, speeds and motor drive characteristics.

The LS7263 is an ion-implanted PMOS integrated circuit in an 18-pin dual-in-line package. It is available in a plastic (0° to 70°C) or ceramic (-25 to +125°C) package.

For more details, contact **Daneva Australia, 66 Bay Road, Sandringham Vic. 3191. (03)598-5622.**

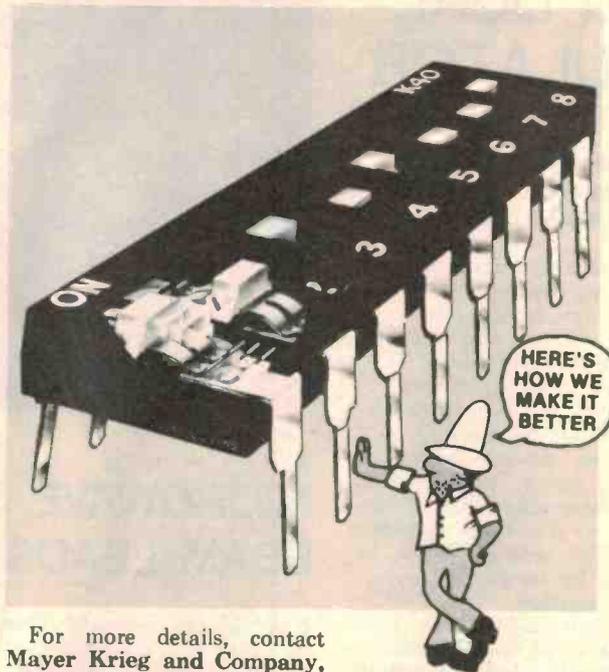
COMPACT DIP SWITCH

American Research and Engineering has incorporated three new patent designs, representing 40% less parts, into its eight-position K40 DIP switch.

The K40, which is the same size as an ic, has slide contacts that make a full wipe, aiding low-current contact.

The slides are split, with two separate slides for each contact point. This doubles the contact reliability, as there are two independent contacts at each switch point.

The slides are made from beryllium copper, heat-tempered to a full hardness, spring-formed, plated in a 100 ml nickel bath and then spot gold-plated 30 ml deep at all contact points. All the switch contact surfaces on the main lead frame are plated with 30 ml gold and more than 50 ml nickel.



For more details, contact
Mayer Krieg and Company,
49/51 Brodie Street, Rydal-
mere NSW 2116.
(02)684-1900.

FAIRCHILD'S JK NEGATIVE FLIP-FLOPS

Fairchild's new 74F112 flip-flop contains two independent high-speed JK flip-flops with direct set and clear inputs.

Synchronous-state changes are initiated by the falling edge of the clock. Triggering occurs at a voltage level of the clock and is not directly related to the transition time.

The J and K inputs can change when the clock is in either state without affecting the flip-flop, provided they are in the desired state during the recommended setup-and-hold times relative to the falling edge of the clock.

For more details, contact
Fairchild Australia, 366
Whitehorse Road, Nunawad-
ing Vic. 3131. (03)877-5444.

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These compact three-way speakers are easy to build and provide a wide-range response

Since we published a number of economical hi-fi amplifiers over the past few years, we have had increasing requests for speakers to suit. With the cooperation of Dick Smith Electronics, here is a three-way design that is compact and gives good performance at an economical price.

Roger Harrison

NOT EVERYONE likes the loudspeakers of a stereo hi-fi system to dominate the lounge room furniture. Indeed, 'bookshelf' and 'compact' loudspeakers have long been popular, particularly amongst those who live in units or townhouses. While these speakers are certainly compact, they aren't quite as small as many bookshelf models on the market. They stand two-thirds of a metre tall and measure a little over 300 mm wide by 230 mm deep overall.

Tiny bookshelf loudspeakers may have a significant drawback. It is extremely difficult to achieve reasonable bass response in a small cabinet. Since much popular music, and certainly much classical music, has a great deal of bass content, a bass response extending below 100 Hz is important.

Design aspects

This loudspeaker employs a 'pressure box' or 'infinite baffle' design. That is, the box is completely sealed. It is sometimes called an 'acoustic suspension' system, too. Such an enclosure prevents sound radiated from the front of the drivers being coupled to the sound radiated from the rear of the drivers and causing constructive and destructive interference which produces big peaks and dips in the frequency response.

Why use three drivers? Well, a loudspeaker of the type used here — that is, the moving coil type — will only operate over a limited frequency range where the cone acts as a 'piston'. Below a certain frequency, the area of the cone will not move enough air to create audible sound waves. At the other end of the range, the sound commences to travel out *along* the cone, which no longer acts as a piston and the sound output drops off because compression and rarefaction waves are generated which tend to cancel each other.

Ideally, in designing a loudspeaker, any driver should be used only over its 'piston

operating range'. The problem is, all but the most expensive and/or specially constructed drivers only have a piston operating range of three to four octaves (an octave is a 2:1 frequency range). You can use a driver over a greater range if some compromises are accepted — otherwise you'd end up with a speaker having five drivers to cover the 10 octaves of the audio spectrum! Expensive.

A popular technique is to use three drivers (hence 'three-way'); one to cover the bass end (the 'woofer') below 1 kHz, one to cover the mid-range from 1 kHz to 4 kHz or 5 kHz and one (usually called the 'tweeter') to cover the top end above that. Acknowledging that the most sensitive portion of the ear's frequency response is in the mid-range, three-way designs generally concentrate on using the mid-range driver over its piston operating range and accepting compromise operation with the other two drivers. That's what has been done with this project — and it achieves quite an acceptable result.

The bass response in a pressure box design is very dependant on the internal volume of the box. The bass driver, the air contained within the box, and the box's volume and shape all interact in a very complex way and it's a bit of a juggling act to make the best of things.

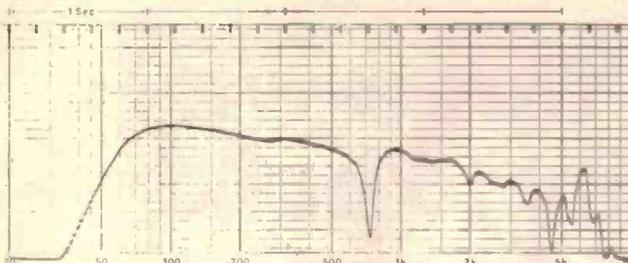
Basically, a sealed box with a driver in it acts like a high-pass filter. That is, the frequency response drops off rapidly below a certain frequency — the 'rolloff' or the 'corner' frequency. The greater the internal volume of the box, the lower the corner



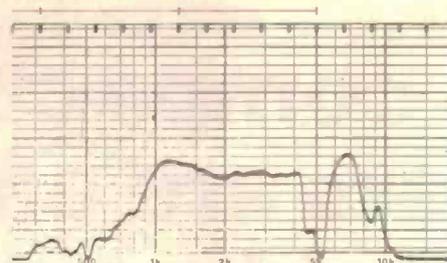
NOMINAL SPECIFICATIONS ETI-421 3-WAY SPEAKERS

Nominal impedance.....	8 ohms
Frequency response.....	45 Hz to 17 kHz (-6 dB) 45 Hz to 19 kHz (-10 dB)
Nominal power handling.....	40 watts
Box volume.....	30 litres

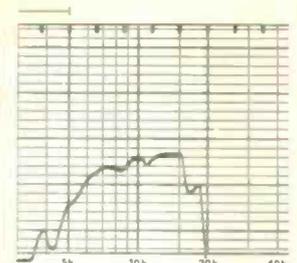
Project 421



Woofer. The piston operating range extends over at least three octaves. The 'dip' near 700 Hz does not show up in the overall response. Vertical scale: 1 dB/increment.



Mid-range. Its piston operating range extends from about 1 kHz to about 4.5 kHz.



Tweeter. This shows reasonable response from about 5-15 kHz.

frequency — and vice versa. But there's a limit to the size of the speaker enclosure that "... s/he who must be obeyed" will accept in the lounge room. Another compromise — but this one's easy to satisfy and still get good bass response.

The enclosure dimensions settled on for this project result in quite a compact box having an internal volume of near as damn to 30 litres which, together with the 200 mm bass driver selected, delivers a bass end which extends to 60 Hz. Not a bad result. Many compact and bookshelf speakers barely make it to 100 Hz.

The mid-range and tweeter both have a sealed rear so that sound pressure inside the box, from the bass driver, does not interfere with their operation.

The piston operating range of the mid-range driver chosen appears to extend from about 1 kHz to 4.5 kHz or thereabouts. Hence, this determines where the operation of the other two drivers has to 'cross-over', from bass to mid-range and mid-range to tweeter. A filter system is used to effect this, rather than just connecting all the drivers in parallel. This filter is called the 'crossover network'.

The response of the bass driver is 'roled off' at the frequency where you want it to cross-over into the mid-range. Thus, a low pass filter is employed. In this case, a simple inductor (L2) has been used connected in series with the bass driver. A series capacitor (C2) 'rolls in' the mid-range in the same region. A simple inductor-capacitor high pass filter (L1-C1) rolls in the tweeter at around 4.5 kHz.

A fairly simple crossover network like this avoids difficulties with phase response and driver-network interactions, resulting

in no 'little surprises' in the general response of the loudspeaker.

The resistors connected to the mid-range and tweeter are there to attenuate their output levels so that the three drivers have generally equal output. The mid-range and tweeter are more sensitive than the bass driver employed.

The capacitors used are 'bipolar' electrolytic types. That is, they are manufactured so that they are not polarised — no positive or negative terminal. This allows them to be used in purely ac applications.

Construction

The box supplied by Dick Smith Electronics is generally constructed of 15 mm chipboard with a base made from 18 mm chipboard — the base is likely to take more punishment during handling! The outside faces are covered in plastic wood veneer. The front panel, with the three cutouts for mounting the drivers, is set flush with the front of the cabinet and the front surface is covered in black vinyl, for appearance's sake.

Four 'sockets' are set into the front panel near the corners. The grille cloth is stretched over a polycarbonate moulding which has four pins projecting from the rear that set into the sockets on the front panel, providing a simple, yet effective, method of securing the front grille.

The rear panel is recessed slightly. The crossover network pc board is screwed on the inside to this and speaker connecting terminals pass through from the outer rear.

As Dick Smith Electronics will be providing pre-cut box panels, construction is quite simple. Fold the top-bottom-side panels around the rear panel, running

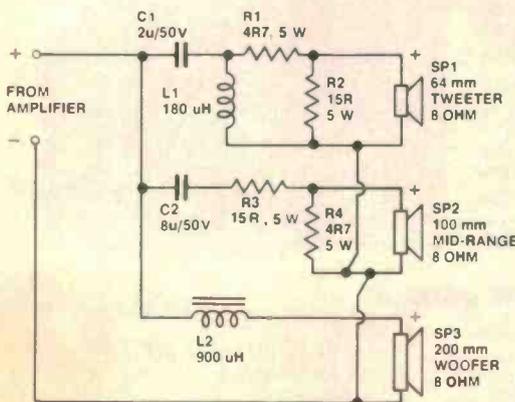
generous quantities of PVA glue (Aquadhere, or similar) in the folds as you go. Position the rear panel so that it's recessed about 10 mm (not critical) from the rear of the box and run a bead of glue around the joint on the *inside* of the cabinet. Small 'chocks' are used to strengthen the rear panel and these should be positioned around the joint on all four sides and thoroughly glued in place. Lay the box on its back to do this and leave it there while the glue cures.

When the box is ready to handle again, take some sealing or caulking compound (Silastic is very good) and run a bead around all the joints. All joints must be

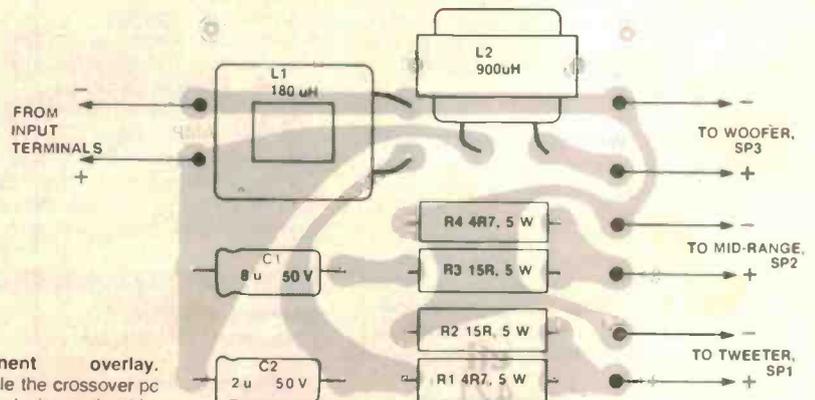
PARTS LIST ETI-421

Resistors	all 5 W, 10%
R1, R4	4R7
R2, R3	15R
Capacitors	
C1	2u/50 V non-polarised electro.
C2	8u/50 V non-polarised electro.
Inductors	
L1	180 uH air-cored
L2	900 uH Iron-cored, open-end
Miscellaneous	
SP1	8 ohm, 64 mm tweeter (part of D.S.E. C-2046)
SP2	8 ohm 100 mm mid-range (part of D.S.E. C-2046)
SP3	8 ohm 200 mm woofer (part of D.S.E. C-2046)

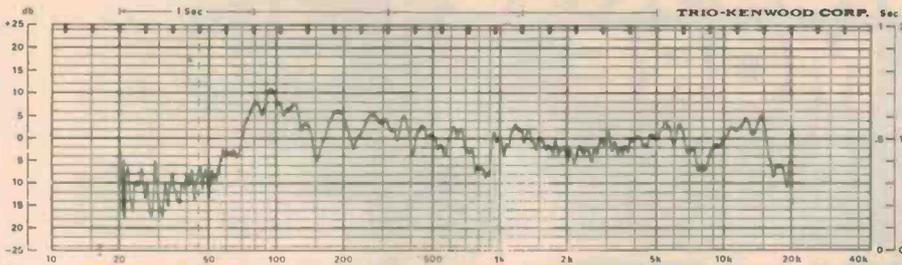
ETI-421 pc board for crossover; box to dimensions in drawings; speaker terminals; wire, speaker box lining, etc.



Circuit. How the drivers and crossover are connected.



Component overlay. Assemble the crossover pc board and wire up the drivers as shown here.



The result. No speaker has a truly 'flat' response and this speaker is no exception! But, the result is very good, achieving a frequency response from 45 Hz to 17 kHz (-6 dB from average).

airtight if the pressure box is to work properly.

Now, run a generous amount of glue around the rabbet at the front of the box, where the front panel will set in. Make sure it's generous as this will have to seal the front panel. Run more glue around the edges of the front panel and then set it in place. Wipe off any excess glue that may be on the outside faces of the box. Allow the glue to cure before proceeding.

Stand the box on its top and assemble the base, carefully gluing it in place. Run the glue on the mating surfaces of the base pieces. Leave the box while the glue cures.

Now for the crossover. This is assembled on a small pc board. The overlay diagram shows the general layout. It can be constructed in any order, but I'd suggest you start by mounting the resistors and capacitors first. Stand the resistors a few millimetres off the board so that heat can escape. The resistors will sure get hot at party time!

Mount the inductors last of all. Both are supplied prewound. The 900 uH inductor has a set of 'E' laminations to obtain the inductance required on the small bobbin. This inductor is secured to the board passing the lugs through two holes drilled in the board for them, and bending over them at the rear. The other inductor is simply wound on a bobbin which can be glued to the board in the place indicated.

Solder pc stakes in place for terminating the input and speaker wires.

Now, back to the cabinets. The speaker terminals need to be mounted. Two holes

are drilled in the rear of the cabinet somewhere near the middle. The lugs of the speaker terminals will pass through these. But first, solder a 400 mm length of red insulated hookup wire (heavy duty, 24 x 0.2 mm, wire is best) to the terminal marked with a red spot. This is the "positive" terminal (marked with a plus on the circuit). Solder a 400 mm length of black insulated hookup wire to the other terminal.

Pass the wires almost right through the holes in the cabinet rear and then put caulking compound in the holes to seal them. Press the terminal strip in place and screw it down. Go to the inside of the cabinet and caulk the holes again just to be sure.

Wires should now be soldered to each driver. Use heavy duty hookup wire (24 x 0.2 mm, at least). Each driver will have the positive terminal marked in some way — maybe with a '+', with a red spot or with a red-coloured insulating washer. Attach a 400 mm length of black insulated hookup wire to each driver's negative terminal. Then, attach a 400 mm length of coloured wire to each driver's positive terminal — using a different colour for each driver (say, white for the tweeter, yellow for the mid-range and blue for the woofer).

Next, place the crossover pc board on the inside of the rear panel, opposite the woofer's hole (it's easier to get at through the large hole). Screw it in place. Solder the input wires to the two input terminals on the board. *Be careful to observe the correct polarity.* Place each driver on the front face,

adjacent to its mounting hole. Pass the wires from each driver, through its mounting hole, and solder them to their respective terminations on the crossover board. Be careful, once again, to *observe correct polarity.*

Now, completely stuff the inside of the cabinet with innerbond.

Before screwing each driver in place, attach adhesive foam tape (available from hardware stores, used for sealing cupboards, etc) around the lip of each driver hole so that a good seal is made. Then screw the drivers in place.

Powering up

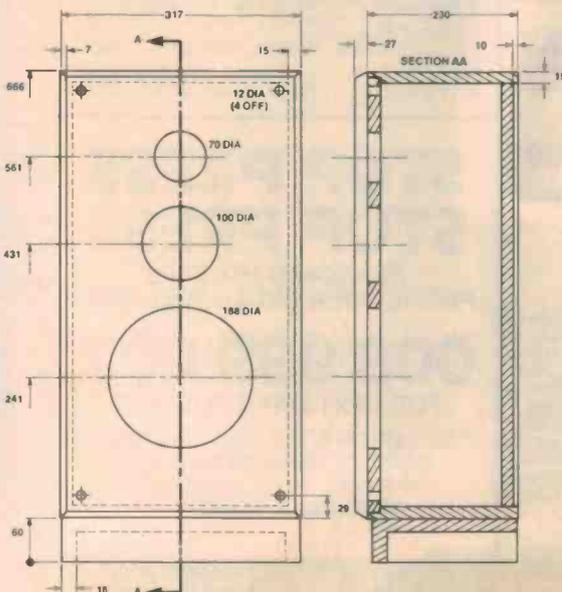
Before connecting the speakers to an amplifier, take a single 1.5 V cell and briefly touch its terminals to each speaker's input terminals — positive to the terminal marked with a red spot. The woofer cone should move forward as you do this, and the loudspeaker should make a loud thump. *Do not* use a battery any larger than a 1.5 V cell for this test or you could damage the woofer.

If all is well, connected the speakers to an amplifier, select your favourite record or tape, turn the volume up slowly and sit back and enjoy the satisfaction of having built your own speakers!

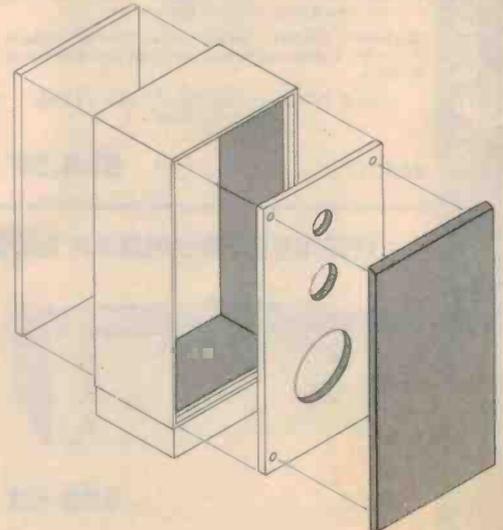
A word of caution. These speakers should be able to comfortably handle 40 W of power. This is not a peak rating. In fact, transients up to 100 W should cause no ill effects. The most dangerous condition for using any speaker is when the amplifier is clipping heavily. Under these conditions, the amplifier's output approaches dc and even a 20 W amp is capable of doing irreparable damage if clipping operation is prolonged.

For safety's sake (and to save the expense of replacing drivers), you might add our Signal-Powered Loudspeaker Protector, ETI-494, published in the October 1982 issue. This will protect your speakers from both overpower abuse and from amplifier faults that might apply dc to the speakers.

Good listening.



Cabinet details. All the cabinet dimensions are shown on the left and an exploded view of the assembly is shown at right. Dick Smith Electronics supplies precut panels with kits, which makes the assembly job a breeze. The front grille is an open weave black cloth stretched over a polycarbonate frame.



ALTRONICS KITS COST MORE

**[Around
\$1
more]**

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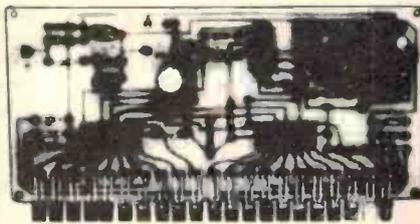
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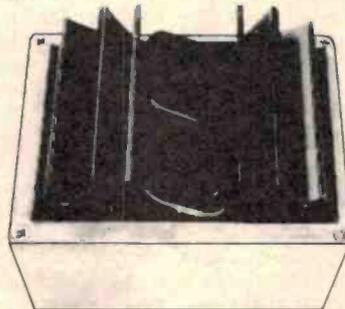
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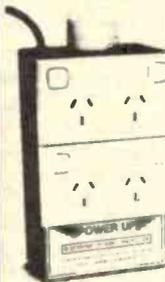
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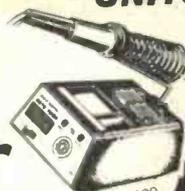
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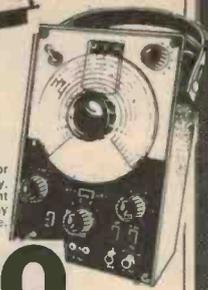
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We have been advised that wiring in a small number of these monitors could develop a fault which, in conjunction with incorrect mains power point wiring could make them potentially dangerous.

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Print weather maps with your Microbee using our "picture plucker" facsimile decoder

Be the first on your block to have your own weather maps! This project allows you to decode the signals of shortwave stations transmitting 'radio facsimile' weather maps and satellite pictures and then reproduce them on your dot-matrix printer.

Tom Moffat VK7TM

39 Pillinger Drive, Fern Tree, Tasmania 7101

MAY 29, 1983, was the day the drought well and truly broke in Tasmania. The rain poured down from dawn till dusk. The roof leaked and the lawns became mudholes. The farmers rejoiced and everyone else grizzled about their ruined weekend. If they'd had some weather charts they could have grizzled with more authority ... the charts told the whole story in graphic detail!

The accompanying series of charts was received on an ordinary home-style short-wave receiver, a Drake SSR-1 to be exact. The audio was processed by a phase-locked loop decoder and a Microbee computer into graphics print data which was fed to a C-ITOH 8510 printer.

The transmission process is called 'facsimile', which we'll call 'fax' for short. Now I've spelled *that* once, I won't do it any more times. Let's call it *fax*, like the cogniscenti do.

As far as I know this is the first time the world of fax has been opened to the electronics-computing enthusiast. The secret, of course, is the computer.

Traditional fax methods are mostly mechanical, and to home-brew a decent fax machine would require access to a lathe and a lot of time and trouble. They appear to be non-existent on the disposals market. The mechanical fax systems now in use are so well made they seem to last forever. Maybe, when more electronic systems appear ...

but we're getting ahead of ourselves. Before we go much further we'd better get down to the bare fax.

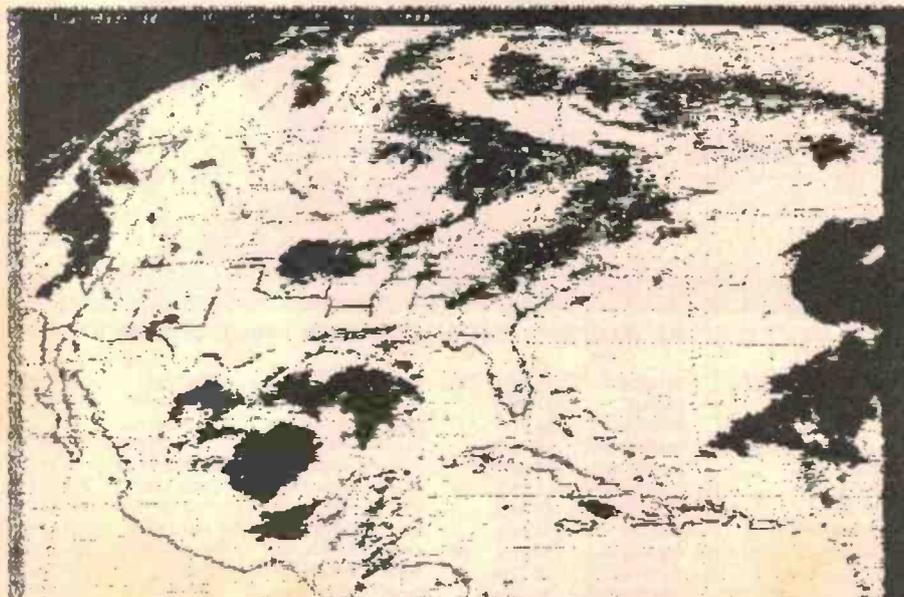
Facsimile explained

The object is to send pictures over a distance. Written data can be transmitted by teletype, but for pictures, or written data in one's own handwriting (such as signatures), fax is the only way to go. Fax is really *veeerry slooooww* television. If the data rate is slow enough you can squeeze an extremely sharp and detailed picture through the restricted bandwidth of a telephone line, or a radio transmitter. Television delivers a complete picture in 1/25th of a second. Fax can take more than 20 minutes for one picture.

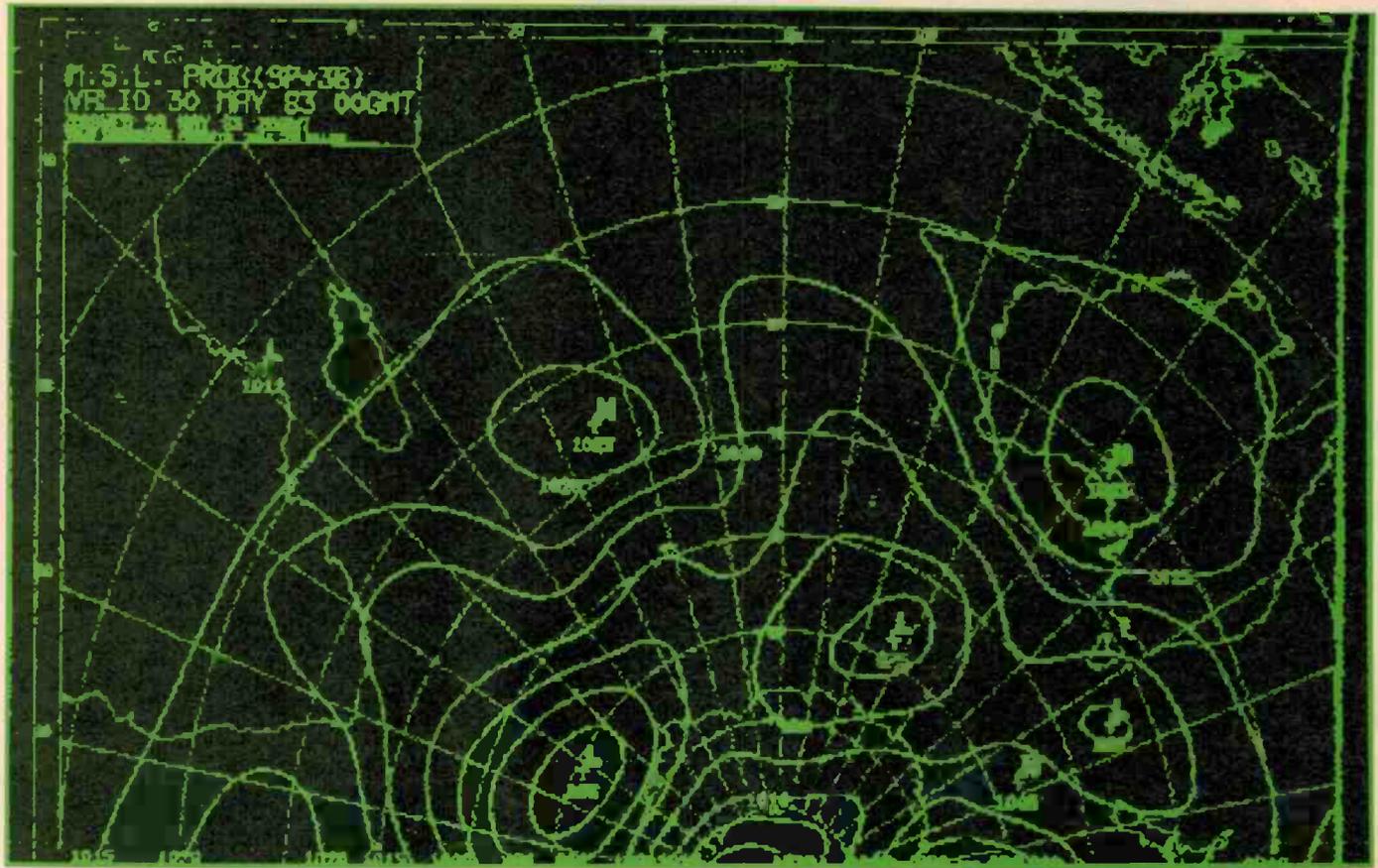
Both television and fax work on a system of scanning lines; only the speed of the scanning and the density of the lines is different. Television, with its wide bandwidth of 5 MHz or so, is restricted to the line-of-sight coverage of VHF. But since narrowband fax can be transmitted on HF, the range is world-wide, and it makes for some interesting viewing.

The traditional method of fax transmission is shown in a much simplified form in Figure 1. The system consists of two metal drums, one at the transmitter and the other at the receiving end. The two drums are rotating at (hopefully) the same speed. Near the top of the transmitting drum is a lamp illuminating the whole surface.

Above the drum is a 'telescope', a system of lenses, feeding into a light dependent resistor (LDR). The light falling on the LDR is only that from the image of the tiniest pinprick portion of the drum, directly at the focal point of the telescope. The whole telescope is connected to a leadscrew arrangement that moves it slowly along the length of the drum.



Believe it or not. Believe it or not, satellite pictures too! (See later.)



The breaking of the drought. Wide-angle view of the southern hemisphere, Africa and Madagascar to the left, Australia to the right. The low that broke the drought has just passed east of Tasmania. Printout shown actual size.

The receiver has a similar telescope over its drum, although there is a lamp in place of the LDR. The receiver lamp is connected via a pair of wires to the transmitter LDR, via a battery to power the lamp.

To the transmitter drum we will attach a piece of paper with some wavy lines drawn on it which is held in place with a piece of black electrician's tape. To the receiver drum we will attach a sheet of photographic printing paper (first turning out the light).

Now we can start the drums rotating in unison. As the telescope at the sending end 'sees' the white paper, the LDR will pass maximum current from the battery via the pair of wires to the lamp at the receiving end. The lamp, through its lenses, will expose at any instant a tiny portion of the photographic paper.

When the first of the wavy lines appears under the sending telescope, its black colour will cause less light to fall on the LDR, less current will pass, less light will fall on the photographic paper, and the image will be reproduced.

As the process continues, lines of whiteness or blackness will begin to build up on the paper, a new line for each rotation of the drum. If the drum turns 1000 times, there will be 1000 lines, quite a high resolution picture, which is better than the television's 625 lines. (Purists will note that since photographic paper is negative-working, the resulting picture will have its blacks and whites reversed. But it illustrates how the system works.) Also note that the image of

the black electrical tape will be reproduced. This is important, as we'll see shortly.

Now that we are instant experts on the basic fax system, we can see the problems it generates. If the drums aren't running at exactly the same speed, the picture will slant one way or the other, like on a TV set with misadjusted horizontal hold control.

If the drums don't start rotating from exactly the same angular position, the left of the picture will be on the right and the right will be on the left and the edge will be in the middle. What a muddle!

If the transmitter sends 1000 lines and your receiver needs 1500 lines to cover the paper, your image will be squashed into the upper 2/3 and the lower 1/3 will remain unexposed.

Let's tackle the problems one by one, beginning with the matter of getting the transmitter and receiver to start together. Most fax systems transmit what are called *phasing pulses*; bursts of white against a black background, before the actual picture begins.

One pulse is sent for each line, and the end of the pulse, the white to black transition, says, 'the next line starts here!'. At the receiving end the machine adjusts its motor speed faster or slower until the edge of its paper coincides with the finish of each phasing pulse. Normally about 30 seconds of phasing pulses are provided, and if the receiver doesn't 'lock up' in that time the picture is going to be a mess. ▶

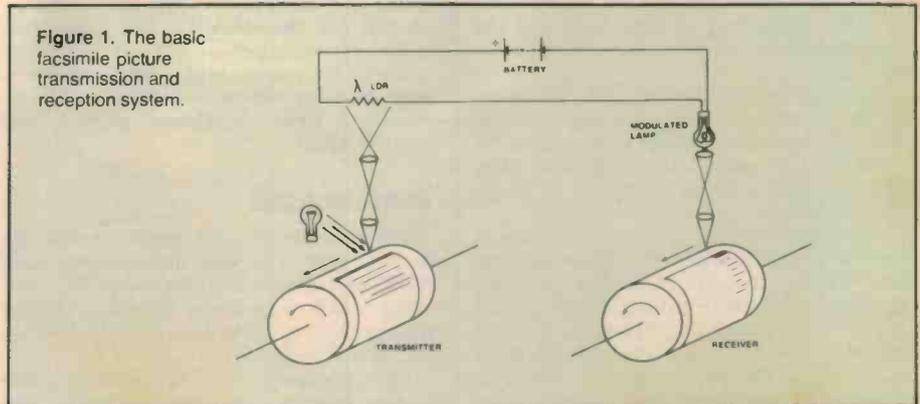
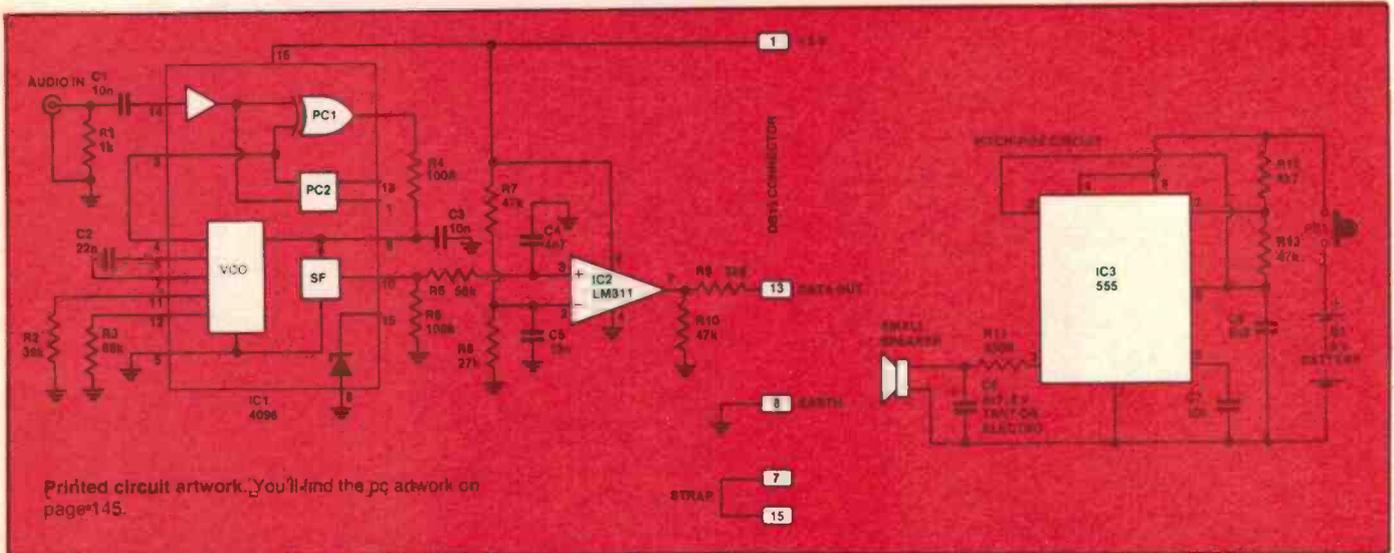


Figure 1. The basic facsimile picture transmission and reception system.

Project 736



HOW IT WORKS — ETI 736

There are two basic parts to the project: the decoder itself, and the pitchpipe tuning aid. A shortwave receiver, set to receive the upper sideband mode, is tuned to a station transmitting radio facsimile (see main text). The pitchpipe is used to tune the receiver so that the 'high' tone is around 2300 Hz. The receiver output is then recorded on tape. The tape is played back and the decoder inserted between the tape recorder's output and the Microbee's 8-bit port. The computer does the rest.

The decoder is built around a 4046 CMOS phase-locked loop IC. The incoming audio consists of two tones 800 Hz apart. These tones are around 2300 Hz (high) and 1500 Hz (low). They are applied to the PC1 phase-comparator input of IC1. The output goes via a low pass filter to the voltage-controlled oscillator (VCO) control input (pin 9). The VCO output goes to the other PC1 input so that the incoming frequency and the VCO frequency are compared. The 'lock' range is determined by R2 and R3. The VCO's free-running frequency is 'pulled' according to the incoming high and low tones.

The 'error' signal generated at the output of PC1 is buffered (after conditioning by the low-pass filter R4-C3) and appears at pin 10. The buffer output at pin 10 is passed to a voltage comparator, IC2, which generates high and low pulses for the input port at pin 13 of the DB15 connector (DATA OUT). Resistors R7-R8 set the non-inverting input of the comparator, IC2, to about 1.8 V. C4-C5 are bypasses.

Supply for the decoder is derived from the Microbee's 8-bit port. Note that the ARDY and ASTB signals are tied at the connector (pins 7 and 15).

The pitchpipe circuit consists of a 555 connected as an astable multivibrator. The oscillation frequency of IC3 is determined by R12-R13 and C8. R11-C6 form a low-pass filter so that a relatively 'pure' tone is issued from the loudspeaker. The output level is low, but then you don't need watts of power to do the job.

Now to the problem of keeping both drums going at the same speed, once phasing has been achieved. There are several ways of going about this, and they're all currently in use.

The simplest method of 'sync' is to use synchronous motors at each end. This method is common in simpler fax machines for use on 'phone lines. It assumes that both transmitter and receiver are running from the same power grid, so their mains supplies are synchronised.

A more elegant way of going about it involves driving both the transmit and receive motors from power supplies derived from crystal oscillators. If the oscillators are stable to within 0.001% good fax pictures will result, and there's no dependence on mains frequencies. So reception is possible aboard a ship, for instance. This is currently the most common sync method.

A third and slightly older system involves the transmission of sync pulses at the start of each line, just like in television. The receiving motor is set to run slightly fast and when it reaches the end of a scan line it slows or stops until told to go ahead by a sync pulse. Sync pulses show up as a black line down the left hand side of a picture (or the right side if it's been sent upside down).

The faithful reproduction of shape is determined by the system's *index of co-operation*. This is the product of the length of a line measured in some unit and the number of lines per the same unit. Confusing? Yup.

Let's try again. Assume that our transmitter drum can take a picture 38.4 cm wide. Assume that it sends 15 scan lines for each vertical centimetre of picture. The system's 'index of co-operation' is $15 \times 38.4 = 576$.

Now assume that our receiving system is only 18 cm wide (which just happens to be the width of our computer graphics printout). If we still went for 15 lines per cm the resulting picture would be very tall and narrow. To stay with the transmitter's index of co-operation of 476, our line density must be $576/18$ or 32 lines per cm.

If this is so, a circle from the transmitter will look like a circle on the receiver. For various reasons the computer receiver index of co-operation isn't exactly 576, and the resulting circles are slightly 'tall'.

One fact that emerged from researching this article is that there is no single standard for fax transmission. Scan speeds can range from 68 lines per minute (one a second) to 360 lpm. Scan densities can be just about anything.

Radio fax can be sent as AM where the amplitude of the carrier varies with the picture, or as FM where the frequency varies. A picture may run for seven or 10 or 20 minutes and it seems some stations transmit non-stop strips of picture and never any phasing pulses. Pictures may be black and white only (binary), or they may contain many shades of grey (analogue).

From observations on the shortwave bands, certain systems seem popular. Every one I've got printable pictures from seems to use an index of co-operation of 576, which certainly makes life easier. About 80% scan at 120 lpm, about 18% use 60 lpm and the remaining 2% use some weirdo system. All seem to use FM with *white* as the *higher* frequency, and most seem to shift their carriers about 800 Hz between white and black.

So, the computer system described here is set up for the most likely signals: I.O.C. of 576 (or thereabouts), 120 lpm, 'sync pulse' synchronisation, FM with shift in the 800 Hz region, and a picture time of nine minutes which is plenty of time to receive a 'right-way-around' picture from station AXM.

Station AXM

AXM was the inspiration for this whole project. You've possibly heard mention of AXM regarding radio-teletype (ETI, April 1983) which it generally transmits during the first half of every hour. For the rest of the time it sends fax.

I first encountered AXM fax during a trip to the Antarctic last summer aboard the

Nella Dan. In the ship's chart-room is a large Japanese-made fax machine that uses a flat bed recorder instead of a rotating drum. Two or three times a day an officer would press a few buttons and the machine

would emit from its top a large weather map which was then posted on the wall. As well as serving in more traditional roles, these weather maps would allow the ship's company to estimate how seasick they were going to be the next day.

The fax decoder

To be the first in your block to have 'fax-in-the-home' you're going to need a few items of equipment:

1. A singlesideband shortwave receiver.
2. A good quality cassette recorder.
3. An ETI-736 Fax Decoder and Pitchpipe circuit.
4. A 32K Microbee computer.
5. A C-ITOH 8510 printer (or Epson MX-80).
6. Lots of patience.

I won't launch into a long technical description of the Fax Decoder here. It's a good old phase-locked loop, very similar to the ETI-733 Radio Teletype to Computer Decoder (April '83). This new circuit has been optimised for fax data rates and frequency shifts (both very large) and it is working its poor little guts out just to stay in lock.

Considering what is being asked of it, the decoder works very well and it can recover lockable pictures even in the presence of noise or multipath distortion. With the comparator circuit, the decoder will even decode analogue pictures and turn them into binary along the way; just right for feeding to the Microbee.

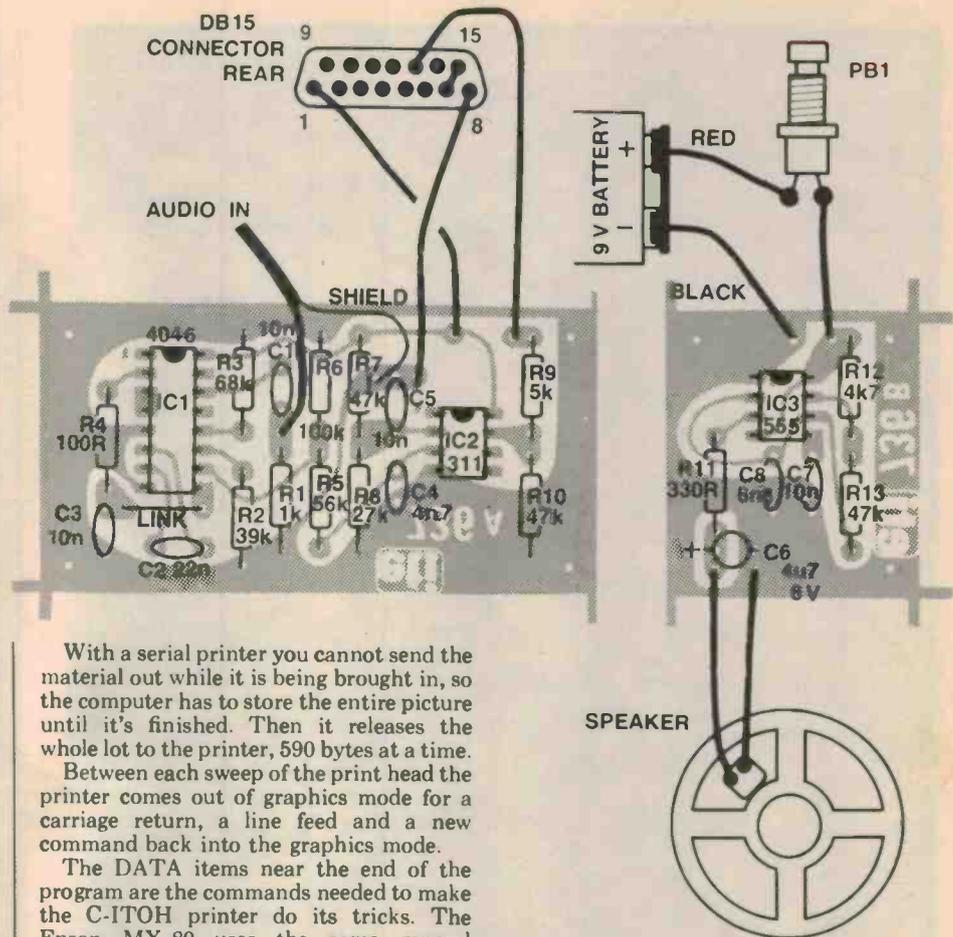
The ETI-736 Fax Decoder is made up of two independent circuits, the Fax Decoder and the Pitchpipe tuning aid. If your receiver is in one room and the computer set-up in another, you can separate the two circuits with a hacksaw so the Pitchpipe stays with the receiver.

The software for the Microbee is one of those big bit-shuffling programs that's a natural for machine code. It provides for the collection and storage of precisely 637 200 bits of fax information. That is 1080 lines with 590 dots per line. Actually we compress three adjacent fax lines into one, with each vertical group of three dots logically ORed together.

So, after compression 212 400 bits are stored in 26 550 bytes. They make up 360 lines for the printer. Before a picture starts the program locks onto any one phasing pulse and shows the remainder as a continuous black bar. So it's best to wait till they're nearly finished before running the program. During the run, the program waits for a black sync pulse before it inputs the next fax line.

The printer, running in the graphics mode, uses its eight dot-matrix print wires to 'paint' eight lines of fax (24 before compression) onto the paper in one sweep of the print head. A smaller than normal line feed is given so each sweep just touches the one above it. In a byte sent to the printer under the graphics mode, each bit controls the action of one of the print wires.

With 590 dots per line, the software must first do 590 bit zeroes, then 590 bit ones, etc, until all eight bits in each byte are set high or low as required.



With a serial printer you cannot send the material out while it is being brought in, so the computer has to store the entire picture until it's finished. Then it releases the whole lot to the printer, 590 bytes at a time.

Between each sweep of the print head the printer comes out of graphics mode for a carriage return, a line feed and a new command back into the graphics mode.

The DATA items near the end of the program are the commands needed to make the C-ITOH printer do its tricks. The Epson MX-80 uses the same general principle in its graphics mode, so substituting its control codes in the DATA area should make it work the same as the C-ITOH.

If you'd like a ready-to-run cassette of the software (set up for the ITOH printer), send the usual \$12 to the author for a speedy post-paid return. If there's a demand I might even be able to cook up an Epson version.

Construction

This project is very simple to assemble. First thing to do, no matter whether you've made your own pc board(s) or bought a kit, is to check the board(s) to see that there are no broken tracks, copper bridges (especially between IC pins) and that all holes are correctly drilled. Separate the Pitchpipe board from the Decoder board before assembling the components.

Start construction by installing the resistors and capacitors on the Decoder board. Then install the link at the end of the 4046. Last of all, install the two ICs, making sure you get them the right way round. Now wire the DB15 plug to the board, not forgetting to link pins 7 and 15.

Now tackle the Pitchpipe board. Solder the resistors and capacitors in place first, making sure you put the electrolytic in the correct way. Then solder the 555 in place, taking care to orientate it correctly, also. Finish by wiring in the pushbutton, speaker and battery clip.

PARTS LIST — ETI 736

Resistors all 1/4W, 5% unless noted

R1	1k
R2	39k
R3	68k
R4	100R
R5	56k
R6	100k
R7,10,13	47k
R8	27k
R9	5k6
R11	330R
R12	4k7

Capacitors

C1,3,5,7	10n greencap
C2	22n greencap
C4	4n7 greencap
C6	4u7/10V single-ended electro.
C8	6n8

Semiconductors

IC1	4046B
IC2	LM311, uA311
IC3	uA555, LM555, NE555

Miscellaneous

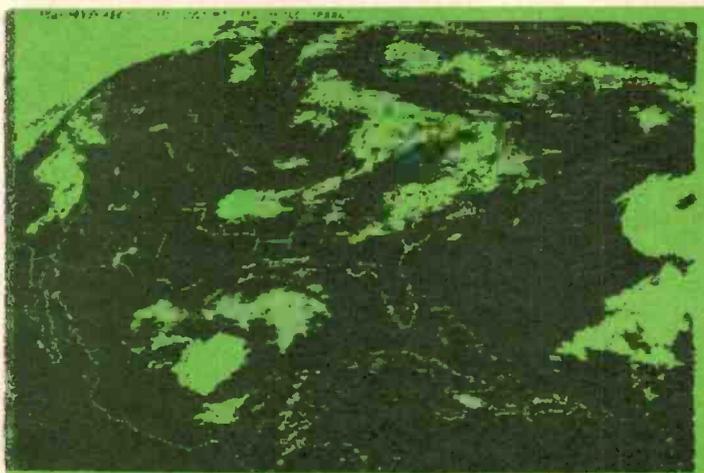
PB1 min. momentary-action pushbutton.
ETI-736 a and b pc boards; DB15 plug;
50 mm 8 ohm speaker; No. 216 9V battery;
jiffy boxes to suit; audio connectors to suit;
wire, shielded cable, nuts, bolts etc.

Estimated cost: \$25-\$30



Picture 3. Satellite picture from AXM, actual size, rotated 90 degrees.

Picture 5. Doctored US satellite picture, transmitted from New York.



If you've got a frequency counter — you only need an audio frequency counter accurate to a few Hertz — then check that the Pitchpipe output is close to 2300 Hz. If you haven't got an audio frequency counter, then turn your Microbee into one! Details were given in the Microbee Column on page 56 of the July '83 issue.

Get the picture

Now here's how to collect your pictures: Connect a speaker, nine-volt battery and a press button switch to the pitchpipe circuit. It should beep at 2300 Hz when you hit the button.

With pitchpipe and cassette recorder at hand, tune the receiver until you hear that chorus of crickets called fax; 11 030 kHz is a good place to start. Switch to 'upper sideband'. If a picture is already running, wait for the next one.

The start of a new picture is signalled by a loud *blurt*, actually five seconds of carrier modulated by 300 Hz. Start the recorder. Next, you'll hear the lower tone, punctuated by some 'pip ... pip ... pips' from the higher tone. Push the button on the pitchpipe circuit and tune the receiver until the pips sound the same pitch. This might sound like a rough and ready method of tuning but it's really quite accurate.

Some 30 seconds or so after the pips begin the picture itself should start, with the high tone becoming more dominant. Hold down the pitchpipe button and check the tuning pitch again. Now let the recording continue, checking the tuning from time to time. When the picture is finished the receiver will blurt again; switch off the recorder and take it to the computer.

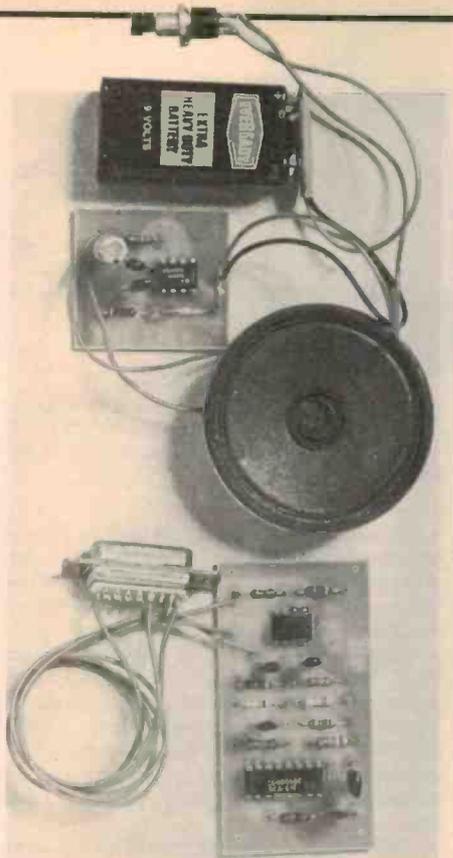
Now rewind the tape and cue it up so it is sitting just a few pips (phasing pulses) in front of the picture. Set the recorder's volume near where you would to load a tape into the Microbee. With the decoder plugged into the computer's parallel port and the audio line plugged into the cassette 'earphone' jack, roll the tape and then run the program. Turn the printer on and wait. Nine minutes later the computer will beep and your picture will begin painting onto the printer. Two minutes after that you'll be hooked on fax.

About the pictures

All the Australian pictures were received from the Bureau of Meteorology's broadcast station, AXM. The 'studios' are located in the Weather Bureau's Melbourne office, although the actual transmitters are in Canberra, operated by the Navy. There's a sister station, AXI, in Darwin.

AXM transmits continuously on four frequencies: 5100, 11 030, 13 920, and 19 690 kHz. Its index of co-operation is 576, scan speed is 120 lpm, frequency shift is 800 Hz and transmission is binary, black and white only, with no shades of grey.

AXM depends on the 'crystal lock' method of sync. It doesn't transmit 'official' sync pulses. But there is something similar to the black electrical tape mentioned earlier ... a black line that always appears on the left hand edge (or the right, if the



Set to go. The completed decoder and pitchpipe, before housing in jiffy boxes.

picture is sent upside down). As far as the Microbee is concerned, it's a sync pulse, and it locks up with ease.

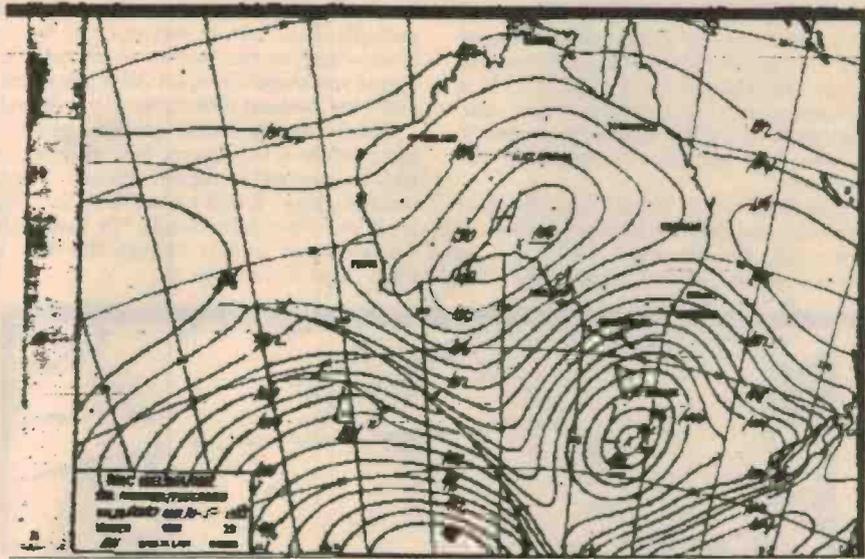
Picture 1 is a standard weather chart just like you see on television every night. Note the big nasty low just south of Tasmania. There's also a cold front sweeping in from the southwest.

Picture 2 is much the same thing, only showing the isobars at 20 000 feet instead of sea level. The low is still much in evidence.

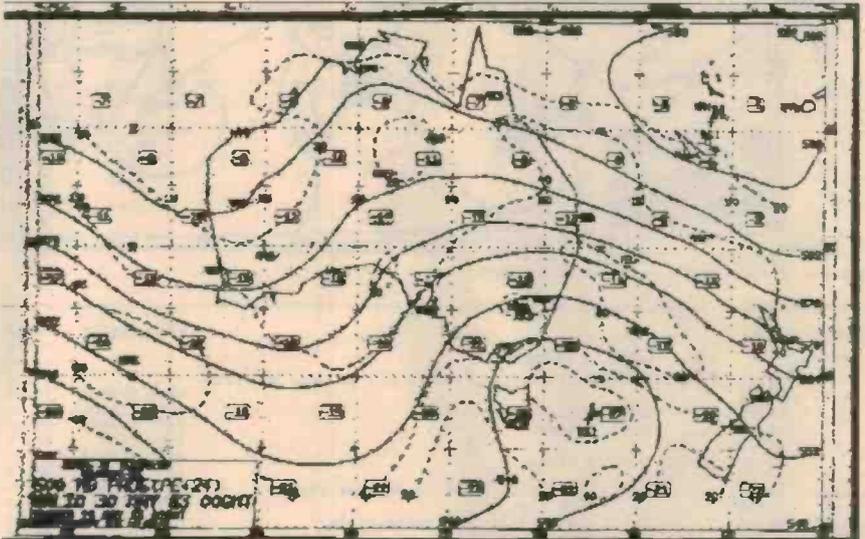
Picture 3 is not a weather map, it's a proper satellite picture transmitted from AXM. Since it's a binary fax system the shades of grey are lost but it's still a pretty smashing view of mother earth, or at least part of it. The picture was too big for all of it to fit in the computer. Rotate it 90 degrees to get the writing the right way up and you'll see the picture in the proper perspective. According to AXM it's the 'southern half of the earth disc as seen from the Japanese satellite GMS'. (That means 'Geostationary Meteorological Satellite'.)

Picture 4 is a 'Nephanalysis'... a study of the cloud situation in the southern hemisphere. The raw data is a satellite picture which is interpreted and re-drawn by meteorologists, with special symbols indicating the cloud types. Again, that big low blots out Tasmania. Obviously this type of chart would not have been possible before the days of satellites.

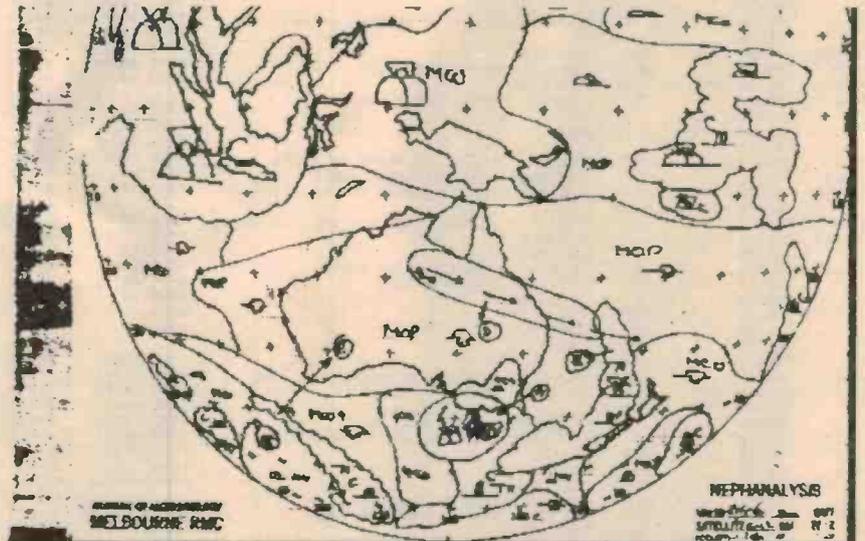
Now to **Picture 5**. You can say you're amazed and astounded now, or later. This one originated from one of America's NOAA satellites and was transmitted from space to the USA where it was souped up



Picture 1. A standard weather chart, from station AXM, 11.30 am, 29 May '83.



Picture 2. Similar to Picture 1, but isobars at 20 000 ft; 2.30 pm same date.



Picture 4. Nephanalysis. 11.45 am 29 May '83, AXM 11 030 kHz.

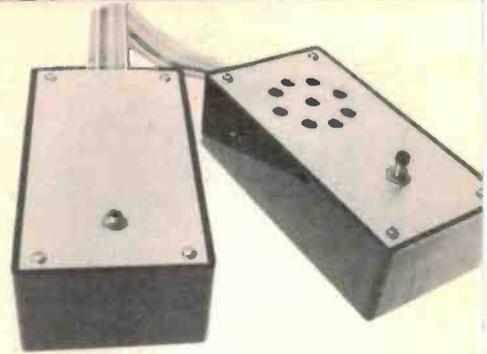
fax-computer decoder

The rest of Australia is gloriously clear! with state borders and the like. Then it was sent back out on HF radio many thousand more kilometres into my humble cassette recorder. In other words it's 'fax DX'. It is an analogue picture that was forced into binary state by the decoder's comparator. It has also had its video inverted in the computer.

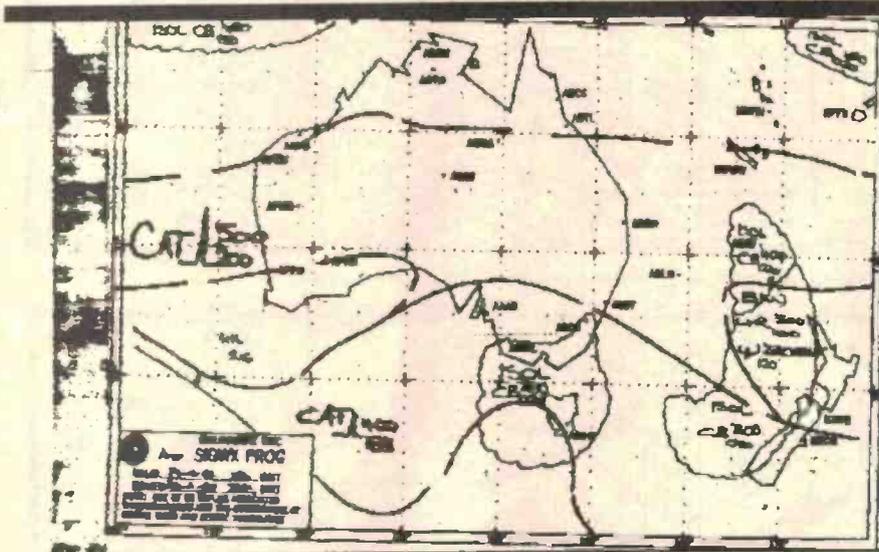
Picture 6 is a 'Significant Weather Prognosis', designed especially for pilots. It shows high altitude wind trends and jet streams, and significant cloud areas. The

word 'CAT' means 'clear air turbulence' to be avoided if at all possible. This particular example looks like it was put out by the Queensland tourist bureau. It shows Tasmania smothered in cloud (that low again), and New Zealand is about to cop it as well.

Those 'mostly black' satellite pictures, like Picture 3, play merry hell with printer ribbons, so we've turned Picture 8 into 'mostly white'. It still looks OK, huh? That is, if you like black clouds. To invert the video on any picture change the data at 0426 (hex) from 38 to 30.



Housing. Two small jiffy boxes served admirably to house the decoder (left) and pitchpipe (right). The ribbon cable goes to the DB15 plug which plugs into the Microbee user port.



Picture 6. One for the pilots, another AXM picture.

So now you know all about fax, as do thousands of other enthusiasts throughout Australia. Perhaps home fax will join home video and compact disc and all the latest electronic pastimes.

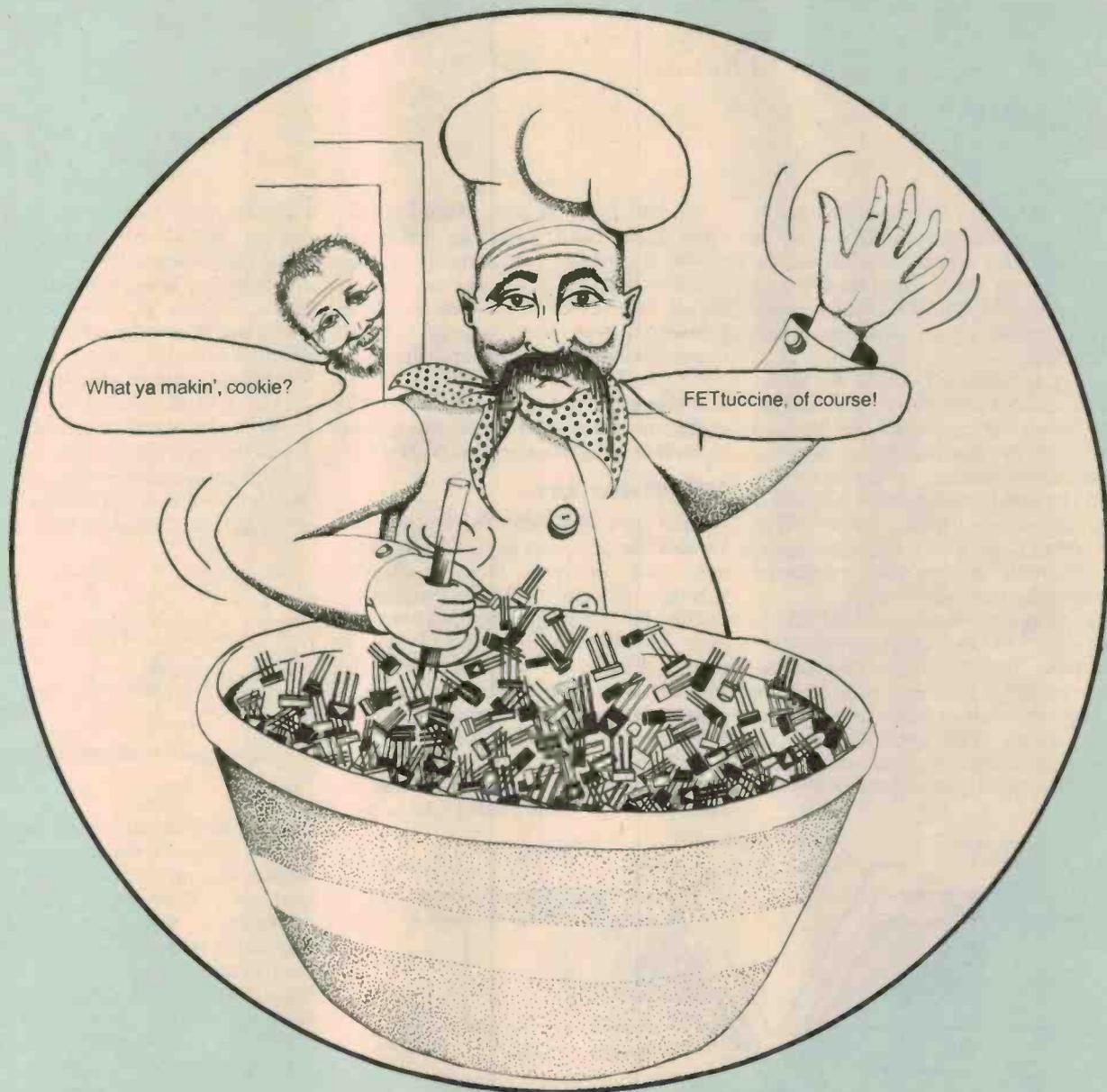
Maybe AXM will even join the ratings race, "Hey folks! You're on AXM! 5000 watts of picture power! And tonight a request from Melbourne listener Randy Oldfellow! Randy asks us to drop tonight's naphanalysis and play a picture of Bo Derek instead. OK, Randy, this one's for you!"

Seriously, though, fax can be useful, and it's certainly a lot of fun. Faxinating. I'd like to thank all those people at the Bureau of Meteorology who suffered my silly questions and helped with the preparation of this article.

PROGRAM LISTING

ADDR	CODE	LINE	LABEL	MNEM	OPERAND		0446 C08C88	00600	CALL	800CH	BEEP WHEN FINISHED	
		00100			Facsimile Receiver Program by Tom Moffatt: May 20, 1983			00610				
		00110						00620			Send out the picture to the printer:	
0400		00120		DEFR	16		0449 218904	00630				
0400		00130		DRG	0400		044C 118680	00640	LD	HL,DATA1		
		00140					044F C07E04	00650	LD	DE,6		
		00150			Clear the data stores:		0452 0620	00660	CALL	PRINT	SET LINE FEED PITCH	
		00160					0454 210010	00670	LD	B,2DH	45 GROUPS OF 8 LINES	
		00170		LD	HL,1000	START OF PICTURE STORE	0457 E5	00680	LD	HL,1000	START OF DATA STORE	
0400	210010	00170		LD	HL,1000	START OF PICTURE STORE	0458 218F04	00690	PUSH	HL		
0403	110110	00180		LD	DE,1001		045B 1E88	00700	LD	HL,DATA2		
0406	01B667	00190		LD	BC,67B6	CLEAR 26550 BYTES	045D C07E04	00710	LD	E,8		
0409	3600	00200		LD	(HL),0		0450 E1	00720	CALL	PRINT	CR/LF AND GRAPHICS INIT.	
040B	E5	00210		PUSH	HL		0461 114E02	00730	POP	HL		
040C	ED00	00220		LDIR			0464 CD7E04	00740	LD	DE,24EH	590 DOTS PER LINE	
		00230					0467 18EE	00750	CALL	PRINT	8 LINES OF PICTURE	
		00240			Synchronize the computer with a phasing pulse:		0469 218F04	00760	DJNZ	LP5	IF NOT 45 GROUPS	
		00250					046C 1E82	00770	LD	HL,DATA2		
040E	CD7504	00260	LP1	CALL	SAMPLE		046E CD7E04	00780	LD	E,2		
0411	30FB	00270	JR	NC,LP1	WAIT FOR WHITE		0471 2AA200	00790	CALL	PRINT	CR/LF	
0413	CD7504	00280	LP2	CALL	SAMPLE		0474 E9	00800	LD	HL,(0A2)	PICTURE FINISHED,	
0416	30FB	00290	JR	C,LP2	WAIT FOR BLACK			00810	JP	(HL)	JUMP TO MONITOR	
		00300						00820				
		00310			Start of picture:		0475 3E43	00830	SAMPLE	LD	A,63	SET DELAY TIME BETWEEN DOTS
		00320		POP	HL	POINT TO START OF STORE	0477 3D	00840	DEC	A	1847 US PER DOT	
0418	E1	00330	LD	DE,24EH	590 DOTS PER LINE		0478 20FD	00850	JR	NZ,*-1		
041C	01012D	00340	LD	BC,2001	LINE COUNTER AND ROTATING BIT		047A D000	00860	IN	A,(0)	GET A PIXEL	
041F	C5	00350	LD	BC			047C 0F	00870	RRCA		SHIFT IT TO CARRY	
0420	0603	00360	LD	B,3			047D C9	00880	RET			
0422	CD7504	00370	LD	B,3	3 FAX LINES = 1 PRINTER LINE		047E 7E	00890	PRINT	LD	A,(HL)	
0425	7E	00380	LD	A,(HL)			047F CD7FAB	00900	CALL	0A07FH	1200 bd SERIAL PRINT ROUTINE	
0426	3001	00390	LD	A,(HL)			0482 23	00910	INC	HL	GET NEXT BYTE	
0428	01	00400	JR	C,*+3	SKIP NEXT IF WHITE		0483 18	00920	DEC	DE	BYTE COUNTER	
042B	01	00410	OR	C	PRINT A DOT		0484 7A	00930	LD	A,D		
0429	77	00420	LD	(HL),A			0485 B3	00940	OR	E		
042A	23	00430	INC	HL			0486 20F6	00950	JR	NZ,PRINT		
042B	10	00440	DEC	DE			0488 C9	00960				
042C	7A	00450	LD	A,D				00970				
042D	03	00460	OR	E				00980				
042E	20F2	00470	JR	NZ,LP3	FOR ONE COMPLETE FAX LINE		0489 1854	00990	DATA1	DEFW	541BH	ESC T
0430	D000	00480	SYNC	IN	A,(0)		048B 3136	01000	DEFW	3631	1 6	LINE FEED PITCH
0432	0F	00490	RRCA				048D 185B	01010	DEFW	5B1BH	ESC I	INCREMENTAL MODE
0433	30FB	00500	JR	C,SYNC	WAIT FOR BLACK		048F 0D0A	01020	DATA2	DEFW	0A0DH	CR LF
0435	114E02	00510	LD	DE,24EH	FOR 590 HORIZONTAL DOTS		0491 1853	01030	DEFW	531BH	ESC S	
0438	ED52	00520	SBC	HL,DE			0493 3035	01040	DEFW	3530	0 5	
043A	10E6	00530	DJNZ	LP3			0495 3930	01050	DEFW	3039	9 0	
043C	C1	00540	POP	BC			0000	01060	END			
043D	C001	00550	RLC	C	ROTATE THE BIT							
043F	30DE	00560	JR	NC,LP4	GO TO START OF LINE							
0441	19	00570	ADD	HL,DE			DATA2 048F	LP5	0457	PRINT	047E	DATA1 0489
0442	10DB	00580	DJNZ	LP4			SYNC 0436	LP3	0422	LP4	041F	LP2 0413
0444	0607	00590	LD	B,7			SAMPLE 0475	LP1	040E			

THE UNFETTERED FET FIDDLER'S FANTASTIC COOKBOOK!



THE RECIPE

7 pp	Power MOSFETs — the technology, the techniques	100
5 pp	VFETs for everyone, Part 1	107
6 pp	VFETs for everyone, Part 2	113
5 pp	The junction FET — its haunts and habits	119
7 pp	Using BiFET and BiMOS op-amps	124

Power MOSFETS — the technology, the techniques

Brian Dance

IN 1976 Siliconix startled the semiconductor world with a new type of power MOSFET device. Recently other manufacturers have produced many other types of MOSFET products which are challenging power transistors and Darlingtons.

The name MOSFET stands for Metal Oxide Silicon Field Effect Transistor. Field effect transistors (FETs) are essentially voltage controlled devices, unlike conventional transistors in which the small base current controls a larger collector output current. FETs have very high input impedances so that very little input current is required to control their output current.

The input impedance of MOSFETs is especially high because they have an insulating film of silicon dioxide between the input gate electrode and the channel through which the output current flows. The gate electrode is therefore essentially completely insulated and virtually no input current can flow.

Various types of small MOSFET devices have been available for many years. Internally they contain a very small silicon chip on the surface of which the MOSFET device has been fabricated. Any current passes through these devices in a horizontal direction through the very thin surface layers and therefore the maximum current is quite low; maximum power dissipation in such devices is not normally over 1W.

VMOS devices

In the so-called VMOS devices, developed by Siliconix about eight years ago, the current flows vertically through the semiconductor material — hence the name VMOS. This name is also associated with the V-shaped groove formed in the surface of the semiconductor material of such devices. Figure 1 shows a cross-section of a VMOS transistor.

If the gate electrode is connected to the source and the drain contact at the bottom of Figure 1 is made positive rela-

tive to the source, no appreciable current will flow from drain to source, since the internal diode formed between the p and n type materials will be reverse biased. If, however, the gate electrode is made positive with respect to the source, the electric field produced by the gate potential creates a channel in the position shown in Figure 1. A current can now flow upwards from the drain through the channel to the source. As the gate becomes more positive, the width of the channel increases and the current from drain to source increases.

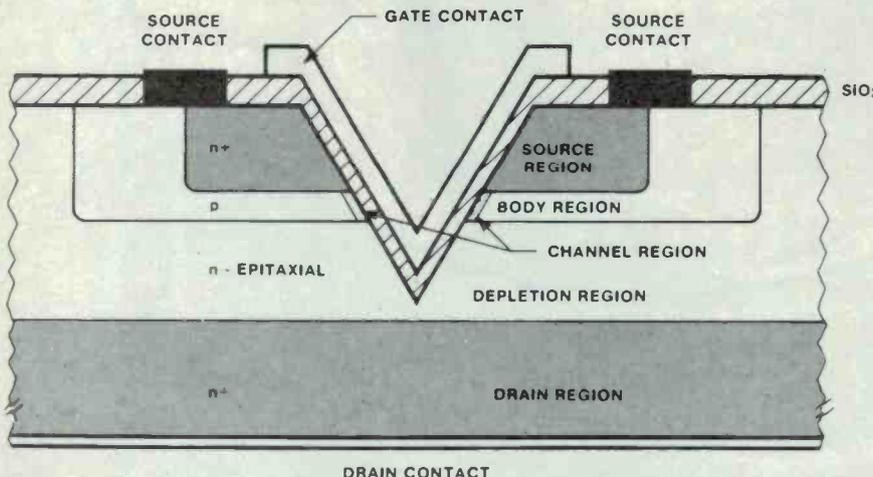


Figure 1. Structure of the VMOS device developed by Siliconix. With the gate biased positive with respect to the source, current flows from the drain region to the source via the channel region indicated. As the gate is biased more positive, the channel region increases, increasing the drain-source current. VMOS FETs are majority-carrier devices and can switch current in less than 10 ns. Bipolar transistors cannot compete as they suffer from minority carrier storage in the base region.

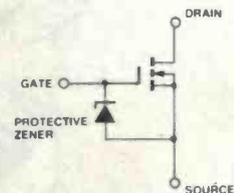


Figure 2. Zener protection of the gate.

If small changes in the gate voltage are to produce the required channel depth, the insulating layer must be extremely thin, which results in an appreciable gate input capacitance (typically some 50 pf). The thin layer also imposes a limit to the maximum voltage which can safely be applied to the gate without the risk of breaking down this thin layer and thus destroying the device. As the gate input resistance is so high (often of the order of a million megohms), it is very easy for small stray electrostatic charges to be picked up on the gate and produce voltages which can puncture the insulating film.

In some devices a small zener diode is connected between the gate and the source, as shown in Figure 2. If the gate to source voltage exceeds the zener voltage, the zener conducts and shorts out the voltage, protecting the MOSFET.

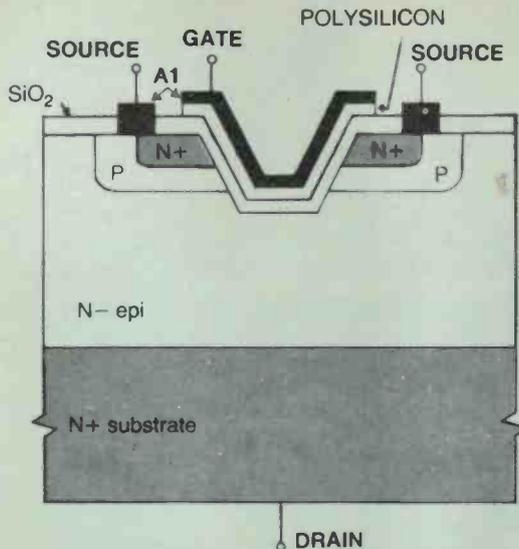


Figure 3. The U-groove device, introduced by Intersil, reduces problems associated with the intense electric field at the edge of the V-notch in VMOS devices. The polysilicon layer prevents migration of sodium impurity ions through the gate oxide layer, a source of chip failure in VMOS.

However, the maximum zener current is quite small, so the zener can easily be damaged. The maximum input voltage 'in circuit' should not exceed the zener voltage so that the zener is used to provide protection against electrostatic charges only.

If the gate becomes more than a fraction of a volt negative with respect to the source, the zener will conduct in its forward direction. If one wishes to operate a MOSFET with the gate voltage negative with respect to the source at any part of the duty cycle, a device not containing a zener should be selected, but then one must take precautions to avoid electrostatic charge pick up.

The first VMOS devices marketed were n-channel devices, with an n-type channel formed in the p-type material shown in Figure 1.

Comparison with bipolars

As the early VMOS devices could not handle so much current or so much applied voltage as conventional transistors, yet were more expensive than the latter, they obviously had some advantages or their manufacture would not have been a viable proposition.

Ordinary bipolar transistors suffer from the disadvantage of minority carrier storage in the base region. VMOS products are majority carrier devices and can therefore switch a current in less than 10 nanoseconds and operate up to several hundred megahertz. For example, the 2N6657 can switch 1 A on or off in less than 4 ns, this being 10 to 200 times faster than a comparable bipolar device.

'Secondary breakdown' is another problem with bipolar transistors. If the

current density increases at one point, the temperature rises in this region, leading to a still greater current density — a positive feedback effect which can lead to the rapid destruction of the device. In VMOS devices, an increase in the current density in the channel produces an increased temperature which results in a lower current density in that region, so that the current density automatically equalises itself throughout the chip without the formation of hot spots.

It follows that it is possible to connect two or more VMOS devices in parallel (often without any additional components), since the total current is automatically shared equally between the devices. Any device passing more current than the mean will become hotter and this will reduce the current somewhat in that device.

Apart from their higher cost, one of the disadvantages of VMOS devices is that their saturation voltage (typically 2V, maximum 4V for some devices when passing 1A) is much greater than for bipolar transistors. Although the V-shaped groove utilises the silicon area quite efficiently, the relatively sharp bottom of the groove is a disadvantage, since a strong electric field can be developed at this point between the gate and the drain where the insulating layer tends to be thinner than elsewhere. This results in a limited operating voltage capability owing to the possibility of gate to channel breakdown.

A perfect switching device would have an infinite resistance in the off state, but the drain current of many VMOS devices is in the nA region when

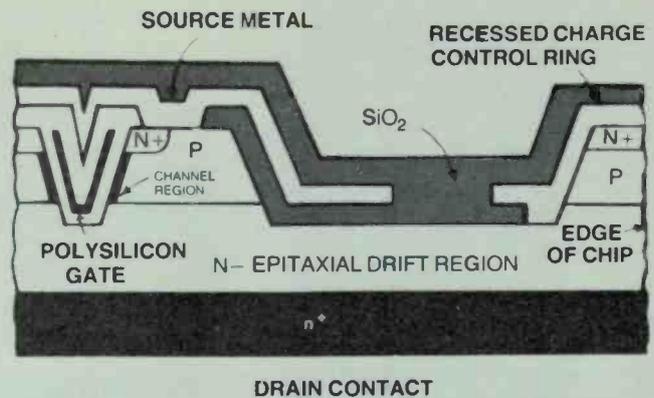


Figure 4. Having introduced power MOSFET technology, Siliconix have gone on to improve the devices. The tri-planar construction shown here allows much higher packing densities on the chip, the smaller size resulting in lower on state resistance. Polysilicon gates are buried in the oxide layers allowing source metallisation to cover a greater fraction of the chip area.

in the off state with gate and source voltages equal. The resistance in the conducting state is normally a few ohms instead of the zero resistance of the perfect switch. This on-resistance is greater for devices with higher voltage ratings.

U-groove devices

The problem of the relatively intense electric field at the edge of the V-shaped notch of VMOS devices has already been mentioned. Intersil, followed by some other manufacturers, reduced this problem by producing devices with the structure shown in Figure 3, where the bottom of the groove is flat. Note that there is an additional layer of phosphorus-doped polycrystalline silicon between the gate and the insulating layer of silicon dioxide. This overcomes another problem of the early VMOS devices, namely the migration of sodium impurity ions through the gate oxide layer, which can cause reliability problems.

Other VMOS products

In 1980 Siliconix announced an improved triplanar VMOS process with the device structure shown in Figure 4. The source, the gate and the drain are each fabricated in a different plane. It is stated that this type of structure allows much higher packing densities on the chip and the smaller size will enable lower on state resistances to be obtained. Polysilicon gates are buried under the oxide layers so that the source metallisation can cover a greater fraction of the chip area.

Another major improvement from the triplanar structure arises from the use

of thin low-resistivity doped layers and from a re-arrangement of the V grooves for optimum use of the epitaxial layers.

Vertical DMOS

Although the modified VMOS processes are very good for devices rated up to about 150 V, they are not ideal for higher voltages. The vertical DMOS structure shown in Figure 5 has been found very suitable for high voltage devices. The current flows upwards from the drain into the n-epitaxial layer, but then flows horizontally for a short distance through a channel to the source.

Supertex of California originally used this technique to make devices with ratings of up to about 500 V, but somewhat higher voltage devices of this type have since become available. Figure 5 shows how the main junction region is surrounded by a concentric second junction which is in turn surrounded by a third junction. Apart from high voltage capability, this process can produce devices with a very low on-resistance (down to 0.05 ohm). In addition the devices are very fast, owing to the low gate capacitance. For example, a 1 A device can operate at about 2 GHz and a 10 A device at about 500 MHz.

The Ferranti Company of Oldham, England has co-operated with Supertex to develop vertical DMOS devices, both n-channel and p-channel, with ratings up to 650 V and drain currents up to 16 A continuous.

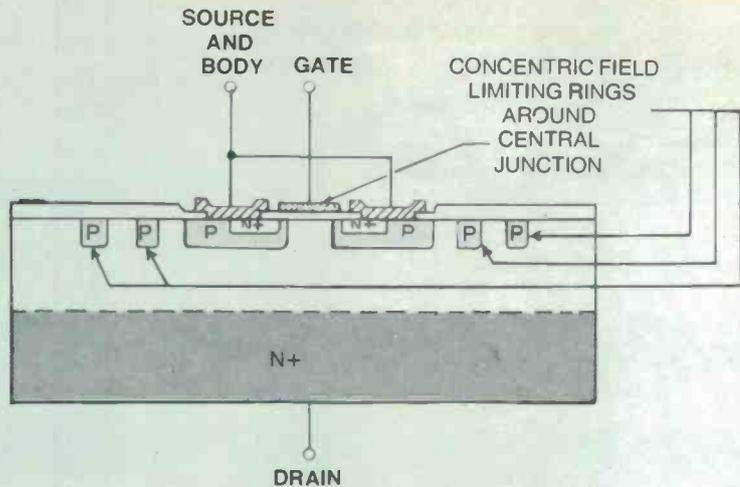


Figure 5. In the vertical DMOS device, current flows from the drain (N+) into the n-epitaxial layer (N-) then flows horizontally through a channel into the source. The concentric rings of p-type material around the main junction help improve the current capability and reduce the on-resistance. This form of construction achieves significantly higher voltage and current ratings compared to prior power MOSFETs.

Hitachi devices

Hitachi has developed a MOSFET device with the structure shown in Figure 6. The gate oxide layer is designed to handle only 20 to 30 V, so a field plate is provided to prevent high electric fields from forming near the gate. This type of device is most suitable for audio frequencies and for operation at up to a maximum of a few MHz. Both p-channel and n-channel types are available with ratings of up to 200 V and 8 A.

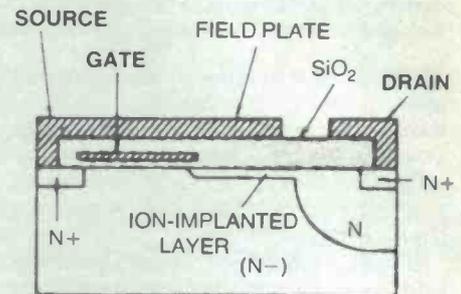


Figure 6. Hitachi MOSFET construction.

HEXFET devices

In mid-1980 International Rectifier introduced a range of devices named HEXFET after the hexagonal structure of the source cells which are connected by a common silicon gate (see Figure 7). The density of these source cells is over half a million per square inch.

HEXFET devices are available in both p-channel and n-channel polarities and can handle high power levels. They have voltage ratings of up to 500 V and continuous current ratings of up to 25 A. Values of channel resistance as low as 0.05 ohm can be obtained in the on state.

Some of the main applications for HEXFETs include servo motor control, RF induction heating, welding control equipment, audio amplification and other uses where the control of high power is required.

SIPMOS

The latest technology to emerge in the power MOSFET field is SIPMOS from Siemens of West Germany, which is an extension of the vertical DMOS technique. Siemens has used this technique to fabricate the first 1000 V MOSFET device, the BUZ 54, which can handle 5 A. It has found wide uses in switching

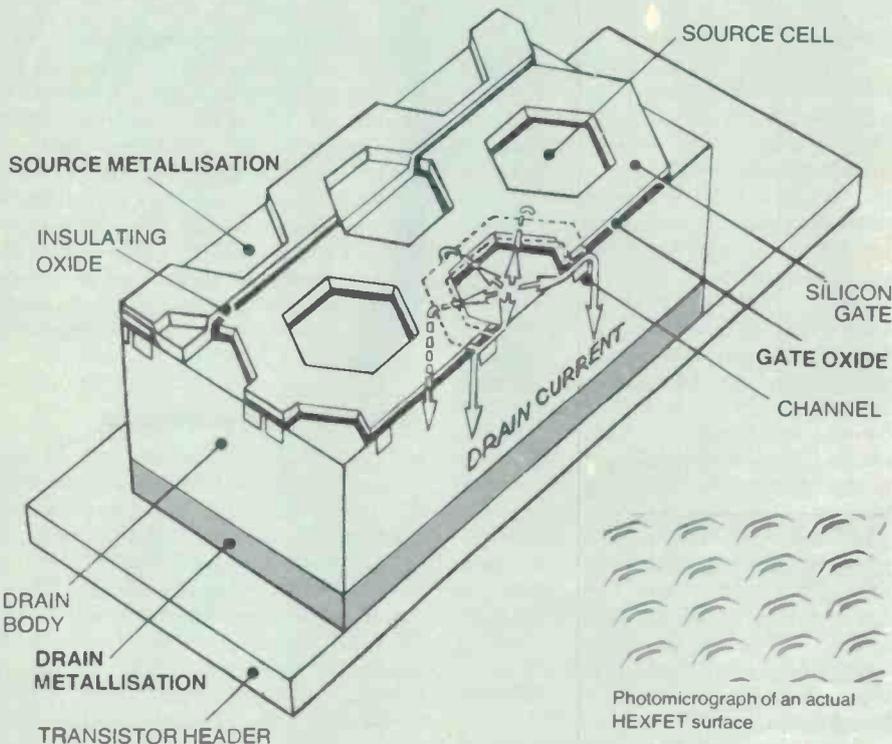
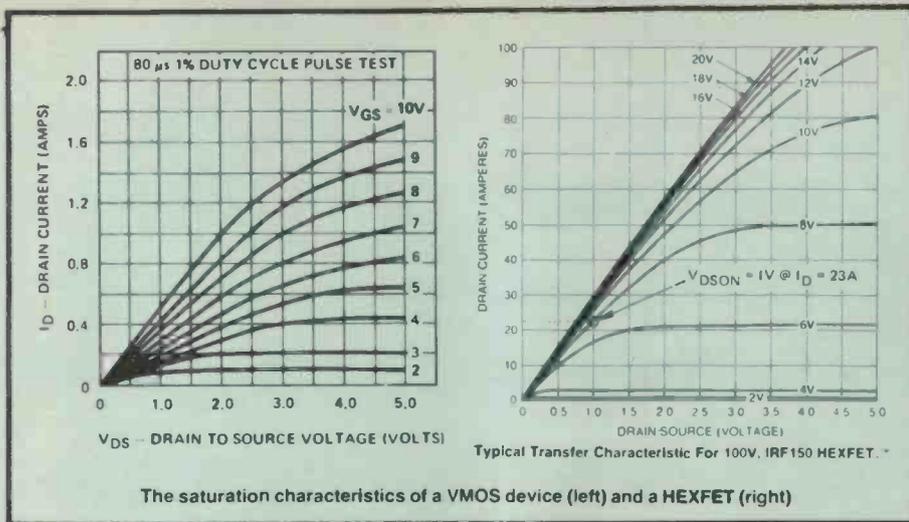


Figure 7. Construction of the HEXFET device introduced by the International Rectifier company in mid-1980. The hexagonal source cells (hence the name) are connected by a common silicon gate. Claimed advantages include high voltage and current ratings plus very low on-resistance.



mode power supplies.

Other SIPMOS devices have ratings in the range of 50 V to 500 V, all being n-channel types. SIPMOS transistors can switch loads of up to 5 kW using inputs to the gate of less than 1 mA at 5 V. Maximum drain currents of up to 30 A can be handled, while on-resistance values can be as low as 0.03 ohm.

Applications

Power MOSFET devices can be used as alternatives to power transistors and power Darlington devices in many applications, but they are generally more expensive than the latter and the circuit designer must decide which types of device are most suitable for his own application.

The use of power MOSFET products is particularly attractive when one can take advantage of their high switching speed or their high frequency capability. Although they may be somewhat more expensive than other transistors, the use of these new devices may simplify circuitry and reduce the overall costs. For example, a conventional power transistor requires a considerable current at its input and one or more driver stages may be required to provide this current, whereas the high input impedance of the power MOSFET enables the latter to operate with such small input currents that power driver stages can usually be eliminated.

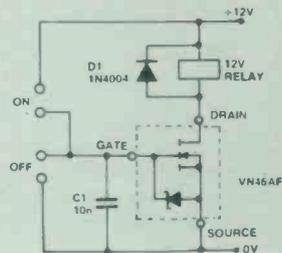


Figure 8. Simple touch switch.

Simple touch switch

The circuit of Figure 8 shows how the very high input impedance of a VMOS power MOSFET can be employed in a simple touch switch. When the circuit is first switched on, the capacitor C1 is normally fully discharged, so the VN46AF VMOS device passes negligible drain current.

When the upper pair of contacts is touched, current flows from the +12 V line, through the person's skin and charges C1. The VN46AF device is thus biased to conduction and the relay closes. If a finger is now placed across the lower touch contacts, C1 discharges and the VN46AF is turned off, opening the relay. The diode D1 is used to bypass the transient voltages formed when the current ceases to flow through the relay coil — such voltages can destroy MOSFETs.

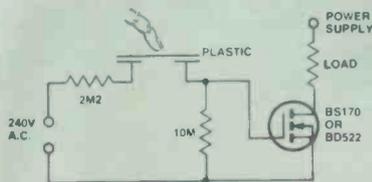


Figure 9. Capacitive touch switch.

Capacitive touch switch

The gate circuit impedance of VMOS devices is so high that circuits can be designed as touch switches in which no part of the circuit is actually touched. In Figure 9 (designed by ITT Semiconductors), the presence of a finger just above the plastic material at the point of separation of the electrodes under the plastic is sufficient to cause current to flow in the load.

The capacitance between each of the electrodes and the finger allows a small alternating current to flow through the 2M2 safety resistor to the gate circuit of the small BS170 or the larger BD522 n-channel device.

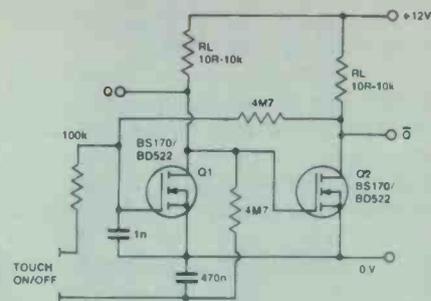


Figure 10. Capacitive touch switch will cycle on and off if finger is held on the sensor.

Figure 10 shows another touch switch designed by ITT Semiconductors, only a single touch point being used for on/off operation. When power is first switched on, T1 will conduct and T2 is kept non-conducting. Touching the sensor contacts will cause T2 to conduct and feedback from the drain of this device through the 4M7 resistor to the gate of T1 will keep the latter device in the non-conducting state. The 470nF capacitor now becomes charged.

If the sensor is touched again, the positive potential from this capacitor is transferred to the gate of T1 and the latter device is switched to conduction, whilst T2 is turned off. If the sensor is touched for longer than about one second, the circuit will operate as a relaxation oscillator which changes its state about once per second. The load impedances employed in this circuit need not be identical, any values from about 10 ohm to 10k being suitable.

CMOS interfacing

The 4000 series of CMOS logic devices can provide only small output currents, but sometimes one wishes to use the output from such a device to control a relay or other load which requires a relatively large current. A VMOS device can conveniently be employed to match the high output impedance of a CMOS device to a relatively low load

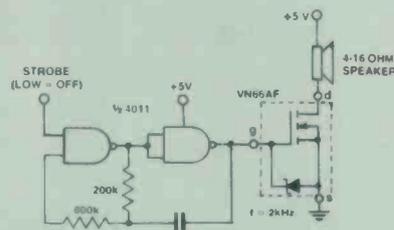


Figure 11. Audio alarm.

impedance such as a tungsten filament lamp.

An example is the audio alarm circuit of Figure 11. Two of the four logic gates of a CD4011 device are connected as a standard 2 kHz oscillator. Any appreciable current taken from the output of this oscillator affects the operation of the circuit, but the VN65AF requires negligible current and forms an ideal

interface device between the CMOS oscillator and the loudspeaker.

When the upper input of the left hand CMOS gate is connected to the +5 V line, oscillation takes place, but when this input is connected to ground, oscillation ceases. Thus a high impedance logic output can be used to switch the oscillator on and off through the use of this input to the left hand gate.

Figure 12 is an interesting variation of the circuit of Figure 11 in which the four gates of a 4011 device are used to form two oscillators. The two left hand gates form a sub-audio frequency oscillator which modulates the audio oscillator formed by the two right hand gates of Figure 12. Thus one obtains a much more impressive two-tone alarm sound than with the simpler constant-note circuit of Figure 11.

The timer circuit of Figure 13 is another example of VMOS interfacing between a CMOS device and a relay. In the quiescent state, the upper input to the left hand gate will be low and the output from this gate high. Thus the output from the right hand gate will be low and the relay will remain open.

If the start switch is momentarily closed, the high input applied to one input of the left hand gate will cause the output from this gate to go low, while the output from the right hand gate goes high and switches the VN46AF to conduction. Thus the relay closes.

The capacitor between the two gates charges slowly through the fixed and variable resistor from the positive supply line. When the inputs to the right hand gate become sufficiently high in potential, the output of this gate goes low and by feedback to the left hand gate the circuit switches back rapidly to its quiescent state in which

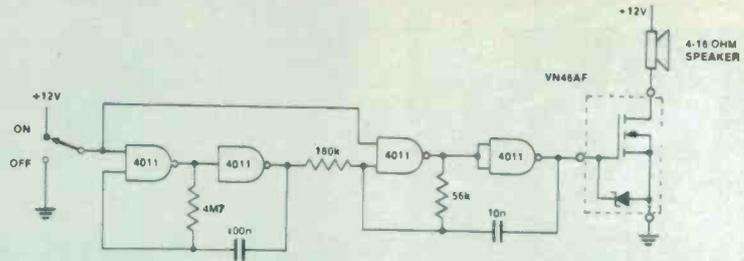


Figure 12. This two-tone alarm is a variation of the Figure 11 circuit.

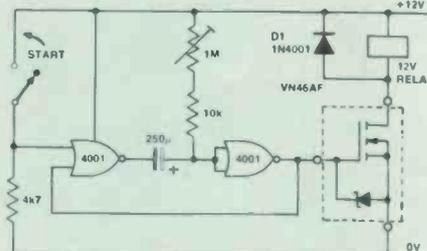


Figure 13. Simple timer has a variable range from a few seconds to a few minutes. The 1M pot sets the time the relay holds in.

negligible current passes through the relay. The length of time for which the relay remains closed can be set by the 1M pot or by altering the value of the capacitor connected between the two gates. When the values shown are used, times obtained range from a few seconds to a few minutes as the variable resistor is moved.

Delay switch

A simple VMOS delay switch is shown in Figure 14. When the switch is closed for a moment, the capacitor becomes fully charged and the VN46AF passes current through the load. The capacitor slowly discharges through the 10M resistor, so the gate voltage of the VN46AF will eventually fall to a value where very little current can pass through the load.

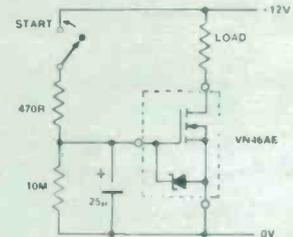


Figure 14. Simple delay timer. The load could be a lamp, relay or whatever.

Auto devices

The fast switching ability of MOSFET devices renders them very suitable for use in vehicle electronic ignition systems. Timing pulses from a magnetic or other contactless pickup may be fed to an IC which provides a voltage output for the control of a MOSFET device. The latter switches the current through an ignition coil to provide the required high voltage.

An automobile circuit using a SIPMOS transistor as a power switch is shown in Figure 15. As in so many applications of MOSFET devices, the high input impedance of the SIPMOS device is utilised here, since it can be voltage driven by a suitable IC. This circuit is for an automobile alternator voltage regulator and has been designed for a SIPMOS device rated at

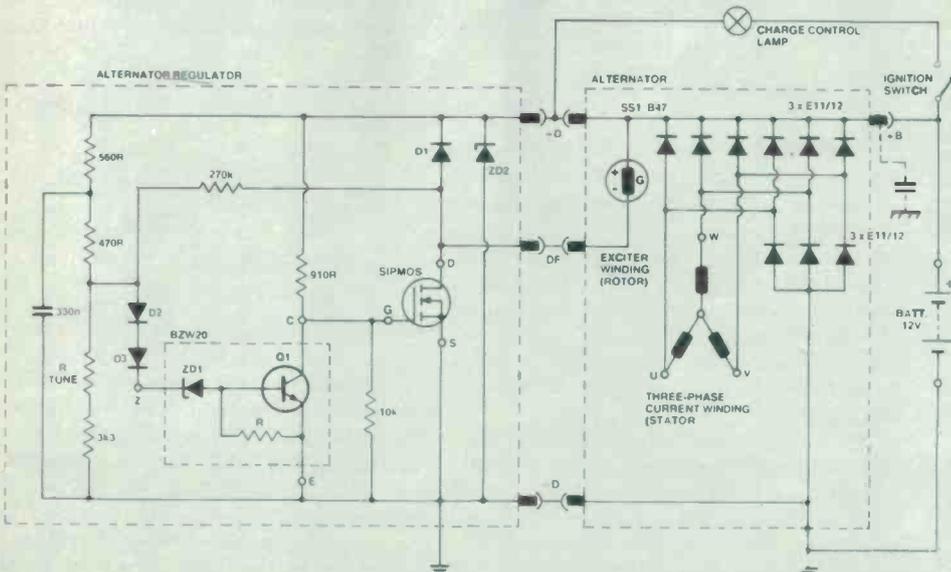


Figure 15. The latest power MOSFET development, SIPMOS, has already found application in automotive electronics. This circuit is an alternator regulator and employs a SIPMOS device rated at 500 V/8 A and an on-resistance not greater than 0.2 ohm.

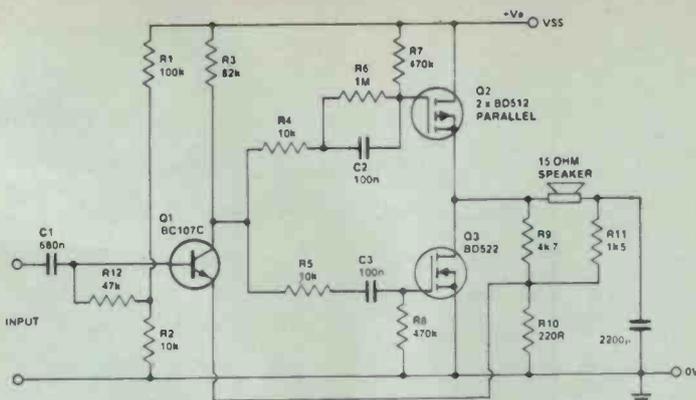


Figure 17. Class ABC amplifier circuit from ITT Semiconductors is simple but has 3½% distortion at 1.75 W and is only suited to general applications.

about 500 V maximum drain-to-source voltage, 8 A current and an on-resistance of not more than 0.2 ohm.

Simple audio applications

The excellent linearity of VMOS devices has attracted considerable interest in their possible use in the audio field but the relatively high price of these devices and their previously limited power handling capability retarded their adoption until recently. They may be used in simple, low-power circuits, but moderately high power ultra-low distortion circuits have also been designed using VMOS devices. The very fast switching ability of VMOS devices also makes them very suitable for Class D pulse width modulation circuits.

To operate a VMOS device as a simple class A amplifier, it is only necessary to provide a bias network so that the device operates in its linear region without cutoff. The gate is connected to a tap on a resistive potential divider across the power supply lines and the input signal is capacitively coupled to the gate. The gain will be approximately equal to the mutual conductance of the device multiplied by the load resistance; gain values of over 30 dB are obtainable, and this gain extends well into the MHz region.

A circuit of this general type is shown in Figure 16. The bias level of the

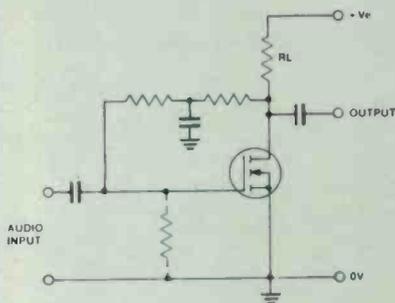


Figure 16. General circuit of a simple class-A audio amplifier using a power MOSFET.

VMOS device is stabilised by means of negative voltage feedback from the drain to the gate circuit.

Figure 17 shows a particularly interesting circuit from ITT Semiconductors which they call a class ABC amplifier, since it is basically a Class B amplifier, but one of the transistors is more in Class A, while the other is definitely in Class C. It is a simple circuit not designed for particularly low distortion.

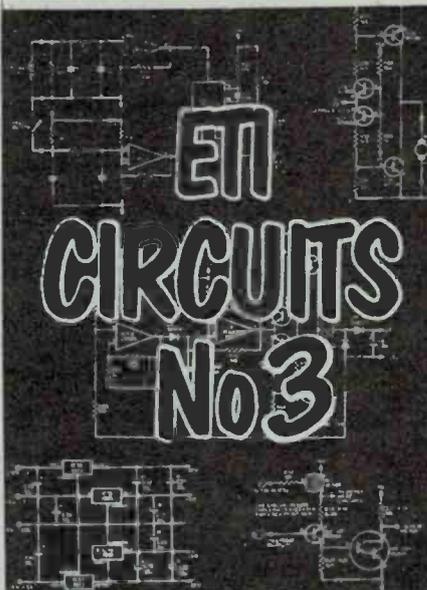
The output stage is unusual in that it comprises two BD512 p-channel VMOS devices in one part and a complementary BD522 single device in the other part. This is because hole mobility in the p-channel BD512 is only half that of the electron mobility in the n-channel BD522s so two p-channel devices are required to obtain about the same mutual conductance as that provided by the single n-channel device. As explained earlier, MOSFETs can be connected in parallel without extra circuitry because they automatically share the current.

As the drain electrodes of the VMOS devices in Figure 17 are connected to the device tabs, all of the tabs can be bolted to the same heatsink without the need for insulating washers. The negative feedback circuit compensates for any variations in the biasing requirements of the particular VMOS devices employed. Both ac and dc feedback are employed, but there is heavier dc feedback through R11 and R10 to stabilise the quiescent dc output voltage at half the supply potential so as to ensure a maximum available output voltage swing.

This circuit provides a voltage gain of 30 and a bandwidth extending from 35 Hz to 125 kHz at the -6 dB points. Distortion increases at ultrasonic frequencies above about 25 kHz (as with most audio amplifiers). When a 25 V supply is used, the distortion is a minimum of about 0.4% at about 0.5 W, rising to about 0.8% at 1 W, 2% at 1.5 W and 3½% at 1.75 W.

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High fidelity

In 1976 Siliconix published a circuit for a high quality 40 W amplifier using VMOS devices, but each half of the output stage required three VMP12 (now designated 2N6658), 90 V TO-3 devices in parallel. Thus, twelve of the devices were required in a stereo amplifier providing 40 W per channel. Rather cumbersome — and costly. However, distortion at the mid-frequency range was only about 0.04% at the 40 W level and about 0.025% at the 1 W level. Only 22 dB of feedback was needed to obtain a response flat to 4 MHz and the slew rate was 100V/ μ s!

One of the advantages claimed for VMOS amplifiers is the lack of transient intermodulation (TIM), because the power bandwidth exceeds the small signal bandwidth. For any frequency below 500 kHz, the amplifier simply overloads before TIM appears.

Taking things a step further, the circuit in Figure 18 is a simple power amplifier first published in the Hitachi MOSFET application notes. The 2SK133 and 2SJ48 have an on-resistance of roughly two ohms, so that at 7 A peak output current you can expect a voltage drop of about 14 V across each device. With the power supply vol-

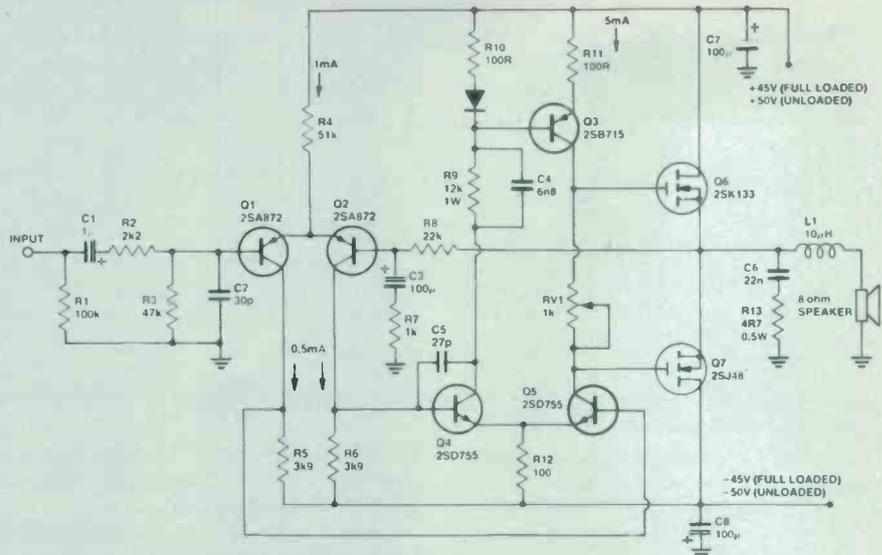


Figure 18. Circuit of a 50 W hi-fi amplifier from the Hitachi MOSFET application notes. Performance is quite good but dependent on the driver transistors.

tages shown the circuit is capable of around 50 W.

Transistors Q1 and Q2 form an input differential pair that compares the input signal with the output signal of the amplifier. The difference between these two signal voltages is fed to a second differential pair, Q4 and Q5. This ensures that the open-loop voltage gain of the amplifier is high and allows a fairly high feedback factor when negative feedback is applied. A relatively large amount of negative feedback is essential when using MOSFETs like this in audio amplifiers to linearise the MOSFET characteristics which have, on average, 10 times the distortion of a typical bipolar transistor of similar power capabilities.

The transistors forming the driver stage, Q3 and Q5, have been specially designed by Hitachi to drive MOSFETs. They're superb devices, having a V_{ce0} of 100 V and a typical gain (h_{FE}) of around 500. With these transistors the distortion characteristics shown in Figure 19

can be expected. Unfortunately, these transistors are not available in Australia at the present time and substituting alternative available transistors degrades performance considerably. A BD139/BD140 complementary pair for instance, with typical h_{FE} of around 50, is not capable of providing the necessary open-loop gain, especially at high frequencies. An experimental circuit we built with BC177s and BD139/BD140s gave less than 0.02% at 1 kHz at full power, rising to as much as 0.1% or more at 20 kHz. So, MOSFETs with all of their advantages have disadvantages too — mainly due to the fact that the forward transconductance is only a fraction of that of a good bipolar transistor.

In order to design an extremely high quality amplifier employing MOSFETs, we are really faced with a new set of problems to solve, but with the promise of performance that makes it worthwhile. (This section on Figure 18 inserted by David Tilbrook . . . Ed.)

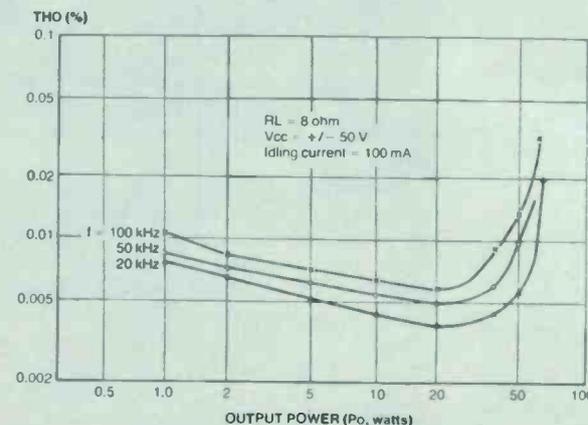


Figure 19. Distortion characteristics of the circuit in Figure 18.

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VFETs for everyone — Part I

Wally Parsons looks back to valves to explain VFETs.

Wally Parsons

A DIODE VALVE emits electrons from a heated cathode and these are then attracted by an electric field to the positive anode. Since only the cathode is heated, current can flow in only one direction. The diode will thus act as a rectifier, conducting only on alternate half-cycles of an AC voltage (see Fig. 1).

If a grid structure is placed between these electrodes, it can be used to control current flow. A negative potential will repel electrons, opposing their flow to the anode, and by placing the grid close to the cathode, a small change in grid potential will have the same effect on anode current as a much larger change in anode potential. Therefore, the device will amplify. Since the anode current is controlled by the electric field in and around the grid, the triode is, in a sense, a field effect device.

The action is direct, and electron flow responds rapidly to changes in control potential. Moreover, in switching applications it can switch an inductive load rapidly, because the back EMF sees an extremely high impedance and no reverse current flows.

Figure 2 shows the relationship of anode voltage, grid volts, and anode current for a triode. It can be seen that anode current can be controlled by both anode volts and grid volts. If a load is inserted in the anode circuit, current changes will cause voltage changes across the load. These can be plotted in the form of a load line as shown, and also as a transfer curve for the specific load.

The amplification is quite linear, but gain and output are limited — as shown by the semi-vertical slope of the curves.

Inserting a second grid between the control grid and anode and applying a fixed positive voltage somewhat lower than on the anode further accelerates

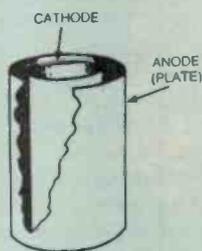


Fig 1. Basic diode tube construction and operation.

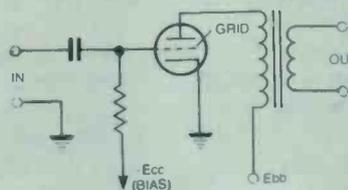
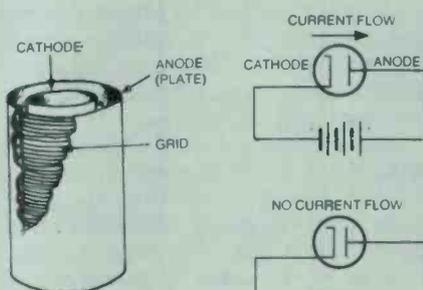
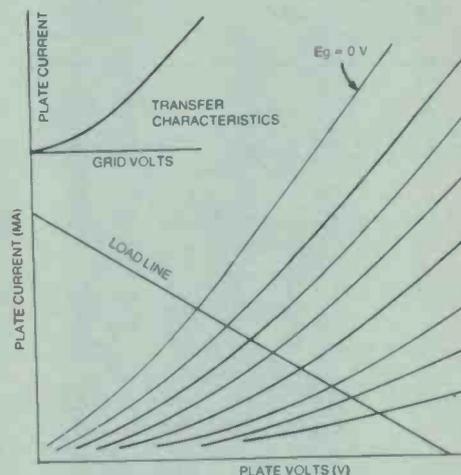


Fig 2. Triode construction, circuit and characteristics.

electrons, but because of the grid's open structure, most of them continue on to the anode. Note the screen voltage takes precedence over the anode in controlling current. And we can swing the anode voltage further for more output, and get higher gain too.

The addition of the second grid with a fixed high potential results in a current flow essentially independent of anode voltage, but still subject to the action of the control grid. (Figure 3). Trouble occurs, however, when we try



to produce an anode voltage swing lower than the screen voltage. Electrons are moving so fast that when they strike the anode they dislodge other electrons, which are attracted to the higher potential screen grid, thus reducing current through the load.

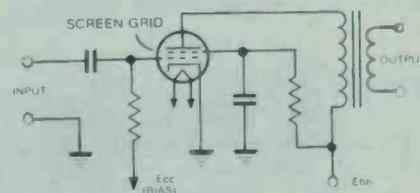
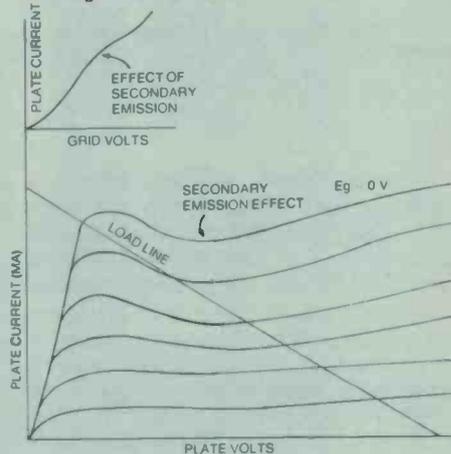


Fig 3. Series output arrangement.

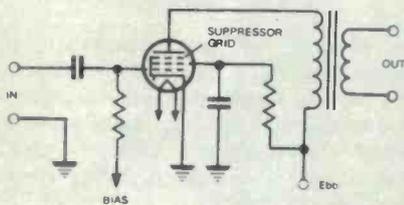
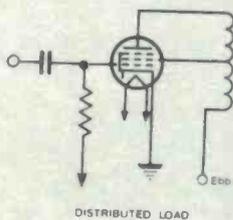
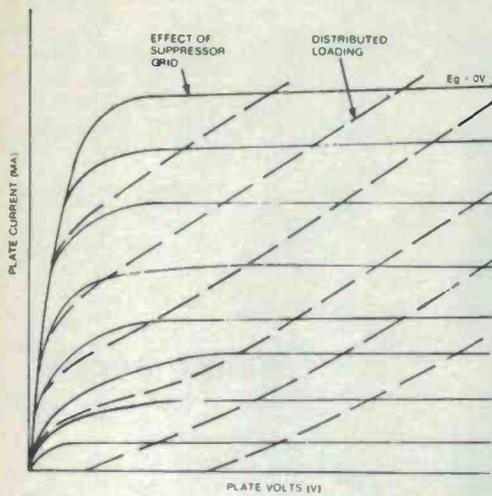


Fig 4. Single ended output with current source.

This problem was overcome by adding a third grid between the screen and plate and tied to the cathode. Because it is at cathode potential the grid pushes the secondarily emitted electrons back to the anode, resulting in a family of curves as in Figure 4.

Distributed loading is also possible by dividing the load between screen and anode, and results in Figure 4a. This kind of flexibility makes it possible to design circuits of exceptional linearity.

Problems

So far so good — except for a few problems. To begin with, the valve, like a light bulb, converts more electricity to heat than to useful work. It's very inefficient — for example the author (who is associated with the Canadian

version of ETI) uses two 75 watt output class AB valve amplifiers to keep his studio at 25° C. without any additional heating in a Canadian mid-winter!

Also like a light bulb, a valve's performance deteriorates from the moment power is applied. Thus, direct coupled circuits can give real headaches in maintaining correct operating characteristics.

And then there's the output transformer. In order to match the thousands of ohms impedance to a low impedance load such as a loudspeaker, a transformer is virtually a necessity. With the inefficiencies already involved we can't afford the resultant impedance mismatches if we try to eliminate transformers. And we can't use gobs of feedback to reduce the resulting distortion. It's bad enough that, if we don't opt for a delicately balanced direct coupled circuit we have a low frequency roll-off and 90° phase shift at every R-C coupling point, but we have in any case the additional phase shift and internal resonances of the transformer. In practice, we are limited to between 20 and 26 dB of overall feedback. Obviously, a high level of open loop linearity must be designed into such an amplifier.

A great deal of engineering energy was spent designing output transformerless amplifiers, but few were successful, and those that were often created more problems than they solved.

Some legendary amplifiers were built using tubes. The Williamson, (I have one in daily use and it still sounds great), Quad, Leak Point One, MacIntosh Unity Coupled. The Quad, for example, delivered all of 15 watts — and was rock stable driving an electrostatic (Quad, of course) at live performance levels. Mac's drove a lot of disc cutters (at 60 watts) to produce discs which still sound spectacular.

But many were anxious to do something with the new-fangled transistors, and we did.

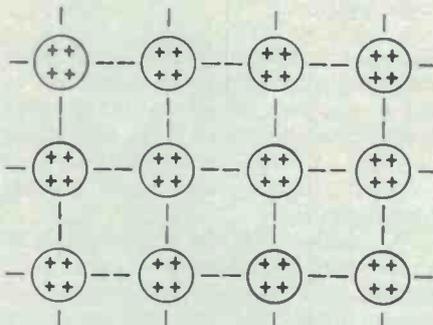


Fig 5a. Basic lattice structure

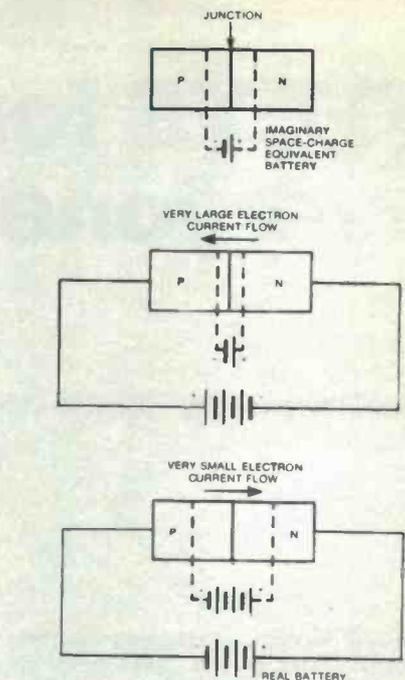


Fig 6. Drain to source resistance against temperature (Siliconix).

Transistors

The bi-polar transistor is composed of three materials, either a p-type semiconductor between two n-types, or an n-type between two p-types, (Figure 7a). A semiconductor such as silicon or germanium has a crystalline structure in the form of a diamond lattice with each atom having four adjacent neigh-

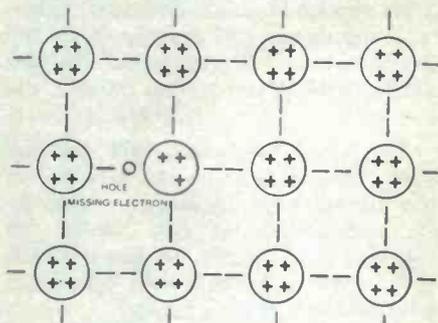


Fig 5b. P-type lattice structure.

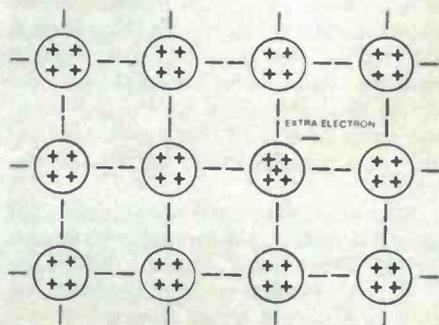


Fig 5c. N-type lattice structure.

bours, held together by co-valent bonds, each bond involving a shared pair of electrons. These electrons are not available for conducting current, so conduction is very semi. Indeed, resistance being around 100 million times that of copper.

However, if we introduce an impurity such as phosphorus or arsenic which has five valency electrons four of which form bonds while the fifth is only lightly held and is available for conduction. This is an n-type material (negative as it has an excess of electrons). If we add an impurity such as aluminium, only three valence electrons are available. Therefore, one of the valence bonds is not completed, resulting in a vacancy or hole in the lattice structure (Fig. 5). An electron from an adjacent electron pair bond may absorb enough energy to break its bond and fill the hold. This is a p-type material. This doesn't look like much of a big deal, but the result is quite dramatic.

Note that the atomic structure is in equilibrium — there is no net charge. However, if a free electron breaks its bond, it leaves behind a positive net charge; if it completes a bond by entering a hole, a negative net charge results. Current flow is produced by bringing about this carrier mobility. What was originally a very high resistance is now, under the right conditions, able to conduct substantial current, just as a small impurity (e.g. sulphuric acid) added to non-conductive pure water, makes electrolytic conduction possible.

When p and n-type materials are joined together, a p-n junction is formed (Fig. 6). Some of the free electrons from the n-type material diffuse across the junction and recombine with holes of the p-type material. The opposite process takes place with holes from the p-type material, producing a space charge or depletion region on either side of the junction, giving the p-type material a slight negative charge, and the n-type a slight positive charge. This process is finally limited by the resulting potential gradient.

If a battery is connected, as shown in Figure 6a, free electrons from the n-type material are attracted to the positive terminal, while holes from the p-type material are attracted to the negative terminal, widening the space charge region and increasing the potential gradient until it approaches that of the external battery. There is now little or no voltage difference across each region and little or no current flow. The junction is reverse biased.

If we reverse these polarities (Fig. 6b) electrons in the p-type material break their bond and enter the battery

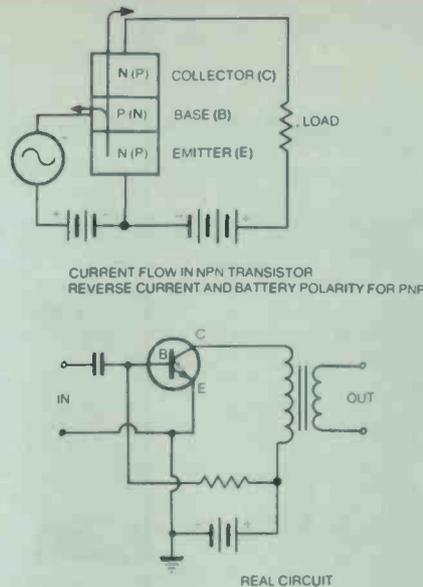


Fig 7a. Current flow in a semiconductor and circuit diagram.

creating new holes, while electrons from the battery negative terminal enter the n-type material and diffuse toward the junction. The space charge region narrows and the energy barrier becomes insignificant, so that excess electrons from the n-type material can penetrate the junction and move via the p-type holes to the positive battery terminal, for as long as voltage is applied. The junction is now forward biased.

Work!

In the device shown in Figure 7, the forward-biased emitter-junction injects electrons into the base region. The impurity or doping levels chosen are such that almost all the emitter current is composed of these electrons, and very few holes are injected into the emitter. The base region is very thin so that nearly all injected electrons diffuse to the edge of the depletion region of the reverse-biased base-collector junction where the field sweeps them across the collector bulk. Since for an equal current more power is developed across a high resistance than a low resistance, amplification occurs as a result of current being transferred from the low-resistance emitter-base junction to the high resistance collector junction.

The curves show that, as with the pentode tube, current is controlled mostly by the control electrode (base), but in this case the controlling parameter is current, not voltage. We have an inherently low-impedance device, and since it requires current into its input impedance, its signal source must be capable of delivering power. An ideal

transistor requires input current, unlike an ideal vacuum tube. This reduces efficiency but we don't have to heat up a cathode to shake a few electrons loose, so our overall efficiency is vastly greater.

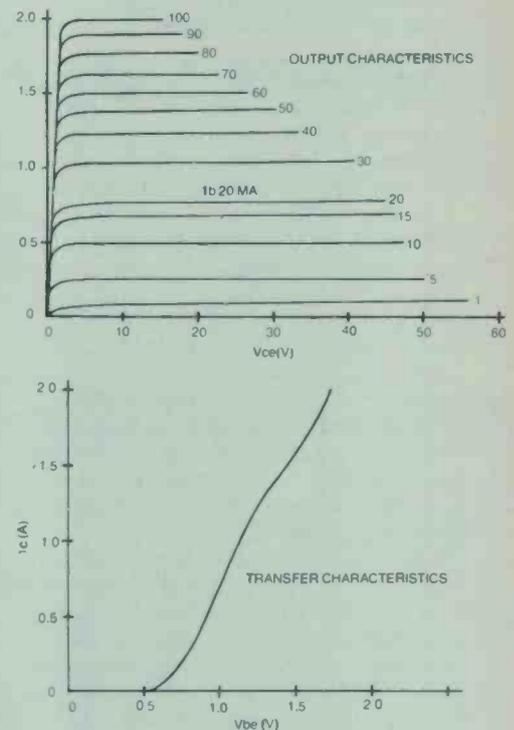


Fig 7b. Output and transfer characteristics of the 2N3054.

Disadvantage

The major disadvantage of this type of device lies in the nature of the depletion layers at the junctions, particularly the emitter-base. When current flows in a transistor, excess charge is stored in the base region. If the base-emitter junction is changed from a forward to reverse bias state, as in the negative swing of a class B or AB stage, or when a class A stage is overdriven, the junction cannot immediately switch to the reverse blocking state due to the presence of these excess charge carriers. They have the effect of allowing current to flow in reverse as if forward biased, until these charge carriers are removed.

In addition, there is capacitance effect associated with the barriers of a reverse-discharge time. The result is a switching transient during part of a cycle, sometimes erroneously referred to as crossover distortion (the latter occurs in any device in push-pull and is due to a discontinuity in the transfer function, usually caused by incorrect bias). This can be reduced by reducing the junction area but this reduces the dissipation capability. In fact, a transistor design favouring one characteristic usually does so at the expense of others.

Also, as temperature rises in the

device (due to current flow, for example) carrier mobility at the junctions increases, causing further increase in current. The current increase further raises temperature, which raises current — which further raises temperature — and so on. The resulting thermal runaway can quickly destroy the device. In milliseconds!

In large area transistors, current tends to become nonuniform in distribution. The temperature rise in the high current region leads to localized thermal runaway until equilibrium is reached by a sharp drop in collector voltage, (called secondary breakdown) frequently destroying the device. This is more true at high voltage and low current than the reverse, and frequently means that rated dissipation cannot be reached. This leads to overdesign, unnecessarily high voltage and dissipation ratings (and remember, a design which favours one characteristic often does so at the expense of others) plus elaborate protective circuits.

High levels of feedback are generally used to control distortion, and this in conjunction with the excess charge condition in the base, leads directly to transient overload, and resultant transient intermodulation. Output is delayed during this charge/discharge, which delays application of feedback. It simply isn't available. The input signal is not immediately reduced by feedback, and passes through at high initial level.

The millenium has not quite arrived after all!

The FET

Since a semi-conductor is precisely that, a battery connected across the ends of a p-type or an n-type bar will cause current to flow through the material, just as it does through a vacuum tube. We discussed earlier the characteristics of a pn junction. If, for example, a p-type material is joined to the surface of an n-type bar, located between the battery terminals, a pn junction is formed, and if this junction is reverse biased, a space charge or field is produced of opposite polarity which will inhibit current flow, just as the control grid inhibits current flow in a vacuum tube. Changing this reverse voltage causes a large current change, and amplification results.

A simple junction FET is shown in Figure 8. With a given drain-source voltage, maximum current flows at zero gate voltage, and at some reverse voltage, determined by device geometry and doping levels, no current will flow. Also, as in the vacuum tube, load characteristics are not reflected to the input circuit, because current is not controlled

by carrier injection as in bipolars, but by voltage levels.

A variation is the Metal Oxide Semiconductor Field Effect Transistor. (MOSFET) (Fig. 9) a far more versatile device whose technology is virtually the cornerstone of modern computer technology, although it has had less use to

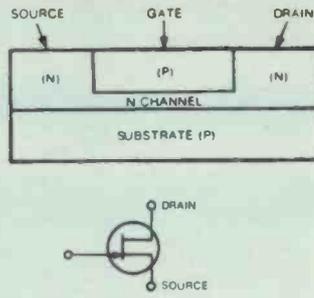


Fig 8. N-channel JFET construction and symbol.

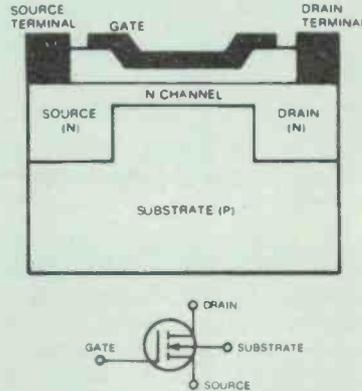


Fig 9a. N-channel depletion horizontal MOSFET construction and symbol.

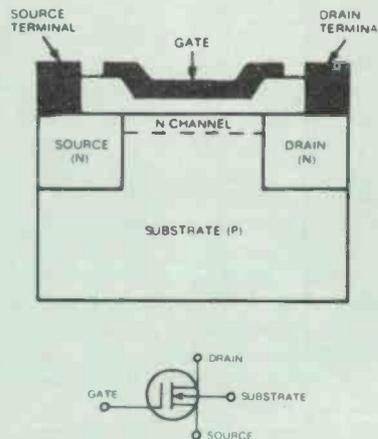


Fig 9b. N-channel enhancement horizontal MOSFET construction and symbol.

date in linear applications such as audio amplification.

MOSFETS come in two basic types. In both the gate consists of a metal electrode separated from the channel by a thin oxide layer. In the depletion type current flow is controlled by the electrostatic field of the gate when biased. When a depletion MOSFET is so biased the device may be driven on both sides of the zero volts point as with vacuum tubes. Unlike vacuum tubes, under these conditions, the gate draws no current, therefore does not require the driver to deliver power.

The enhancement type MOSFET shown in Figure 9b, is more widely used. The source and drain are separated by a substrate of opposite material, and under zero gate volts no current flows. However, when sufficient forward bias is applied to the gate the region under the gate changes to its opposite type (e.g. p-type becomes n-type) and provides a conductive channel between drain and source. Carrier level, and conduction is controlled by the magnitude of gate voltage.

Although MOSFETS are handy devices they are not capable of handling high power levels. The channel depth available for conduction is limited by the practical limits on gate voltage. The lower current density has been the primary limitation due to the horizontal current flow.

VFETS

Recent years have seen the introduction and commercial use of Vertical Channel J-FETS, notably by Sony and Yamaha (Fig. 10). The vertical channel permits a very high width-length ratio, permitting a decreased inherent channel resistance and high current density. Unfortunately it suffers the same disadvantages as the small signal J-FET, plus, in currently available devices, a very high input capacitance, ranging from 700 pF to around 3000 pF, limiting high frequency response. In addition, since they must be biased into the off condition, bias must be applied before supply voltage and removed after the supply if it is to be operated anywhere near its maximum ratings. This problem doesn't exist with vacuum tubes because of heater warm-up time, although some

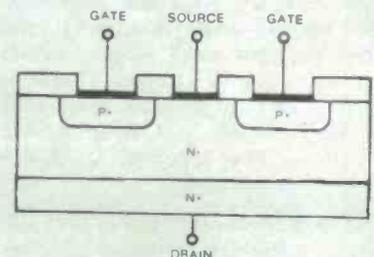


Fig 10. Vertical junction FET construction.

"instant-on" circuits impose heavy turn-on surges.

This necessitates a complex power supply, and Yamaha, for example, uses more devices in the supply than it does in its amplifier circuits. However, the construction does make possible the design of complementary types and both Nippon Electric and Sony have high power devices available.

However, the Vertical MOSFETS by Siliconix are readily available, at reasonable prices, and the manufacturer most generous in providing data. The following information is extracted from their application note AN76-3, Design Aid DA 76-1, plus device data sheets.

The device

Notice in Figure 11, that the substrate and body are opposite type materials separated by an epi layer (similar to high speed bi-polars). The purpose of this structure is to absorb the depletion region from the drain-source junction thus increasing the drain-source breakdown voltage. An alternative would have involved an unacceptable trade-off between increasing the substrate-body depth to increase breakdown voltage (but increasing current path resistance)

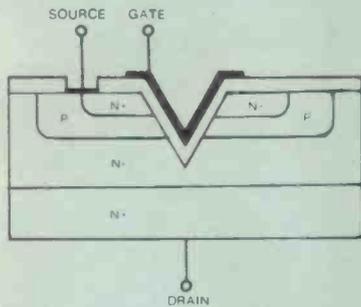


Fig 11. Vertical MOSFET construction (Siliconix).

and lengthening the channel. In addition, feedback capacitance is reduced by having the gate overlap n-epi material instead of n+.

In manufacture, the substrate-drain and epi layer are grown, then the p-body and n+ source diffused into the epi layer, in a similar manner as the base and emitter of a diffusion type transistor. A V groove is etched through the device and into the epi layer, an oxide layer grown, then etched away to provide for the source contact and an aluminium gate deposited. This type of device allows current flow in one direction only; this is not always so with a similar type of horizontal FET, where source and drain may be identical in structure and of the same material. Therefore, no reverse current flows (we hope) when used in switching applications, as was also the case with vacuum tubes.

In-circuit operation is refreshingly simple: Supply voltage is applied between source and drain, with the drain positive with respect to the source, under which conditions no current flows, and the device is off. This is an enhancement type device, and is turned on by taking the gate positive with respect to the source and body. The electric field induces an n channel on both surfaces of the body facing the gate, and allows electrons to flow from the negative source through the induced channel and epi and through the substrate-drain. The magnitude of current flow is controlled almost entirely by the gate voltage, as seen in the family of curves (Fig. 12) with no change resulting from supply voltage changes above 10 V.

Advantages

The vertical structure results in several advantages over horizontal MOSFETS.

- 1) Since diffusion depths are controllable to close tolerances, channel length, which is determined by diffusion depth, is precisely controlled. Thus, width/length ratio of the channel, which determines current density, can be made quite large. For example, the VMP1 channel length of about 1.5μ , as against a minimum of 5μ in horizontal MOSFETS, due to the lower degree of control of the shadow masking and etching techniques used in such devices.
- 2) In effect, two parallel devices are formed, with a channel on either side of the V groove, thus doubling current density.
- 3) Drain metal runs are not required when the substrate forms the drain contact, resulting in reduced chip area, and thus reduced saturation resistance.
- 4) High current density results in low chip capacitance. Also, unlike horizontal MOSFETS, there is no need to provide extra drain gate overlap to allow for shadow mask inaccuracies, so feedback capacitance is minimized.

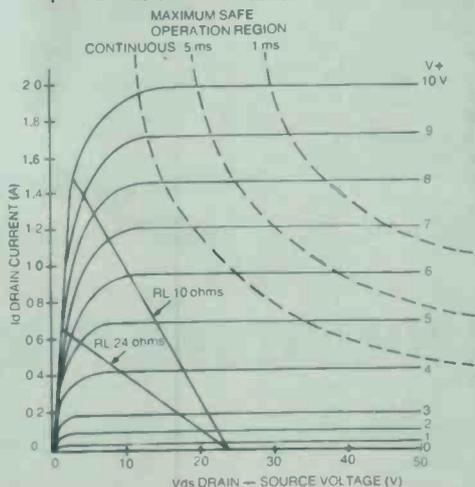


Fig 12a. Output characteristics VMP1.

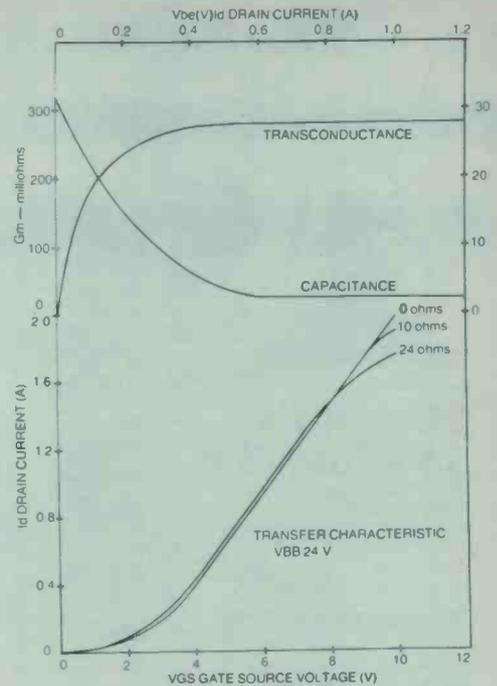


Fig 12b. Other VMP1 characteristics.

In comparison with bi-polars, especially power devices, the advantages are even more impressive.

- 1) Input impedance is very high, comparable to vacuum tubes, since it is a voltage controlled device, with no base circuit drawing current from the driver stage. A 7 V swing at the gate, at virtually 0A, represents almost 0W of power, but can produce a swing of 1.8 A in output current. This represents considerable power gain and will interface directly with high impedance voltage drivers.
- 2) There is no minority carrier storage time, no injection, extraction, recombination of carriers, resulting in very fast switching and no switching transient in class B and AB amplifiers. Switching time for a VMP1 is 4 ns for 1 A, easily 10-200 times faster than bi-polars, and rivaling many vacuum tubes.
- 3) No secondary breakdown, and no thermal runaway. VMOS devices exhibit a negative temperature coefficient with respect to current, since there is no carrier recombination activity to be speeded up with temperature. Thus, as current increases so does temperature, but the temperature rise reduces current flow. It is still possible to destroy the device by exceeding its maximum ratings, but a brief near-overload does not result in an uncontrollable runaway condition. Usually, simple fusing and/or thermistor protection is sufficient for maximum safety, and even this may be unnecessary with conservative design. Absence of secondary breakdown means that full dissipation can be realized even at higher supply voltages. In this respect they resemble vacuum tubes.

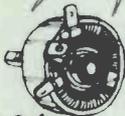


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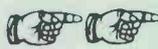
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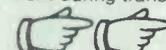
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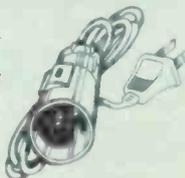
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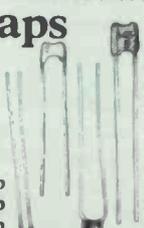


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VFETS for everyone — Part II

In the first part of this article we examined the structure and features of a new type of semiconductor, the vertical channel power metal oxide semiconductor, Vertical MOSFET, or V-MOS, introduced by Siliconix. The second part of the article covers the actual use of V-MOS.

Wally Parsons

V-MOS POWER FETS like signal MOSFETS, may be used to perform many different functions. However, no matter what the circuit, certain conditions, common to all applications, must be provided. These are supply power, loading, drive signal, and establishment of appropriate operating points.

The electrical characteristics of the VMP1, VMP11, and VMP12, are shown in Fig. 1, and Fig. 2 shows them in graphic form. Since these are unidirectional devices, the source and drain are not interchangeable, and as they are n-channel devices conduction can occur only if the drain is positive with respect to the source, and high enough to ensure operation in the linear region — as with a vacuum tube, bi-polar transistor, or signal FET.

Like the vacuum tube, the absence of secondary breakdown allows full dissipation at any voltage supply up to maximum voltage and current ratings.

Thus, where two different designs require the same dissipation but different voltage/load current, no derating is required. This is shown in the "safe operating area" curves. The only bi-polar transistor possessing this characteristic is the single-diffused type, which is also the least suitable for any application requiring wide bandwidth and/or high speed.

This characteristic also simplifies the establishment of suitable load-lines allowing greater safety margin in driving reactive loads where the load-line may be elliptical to the point of leaving the safe-operating area. Designers accustomed to using high voltage high dissipation devices to assure adequate safety margins at relatively low power levels need not therefore be too disconcerted at the 25 watt rating of these devices.

A 10 watt class A amplifier suitable

for driving a tweeter in a bi-amped speaker system, for example, need not suffer excessive dissipation except perhaps with an electrostatic unit where such a power level would be inadequate anyway, unless it were operating at a very high cross-over frequency.

Output

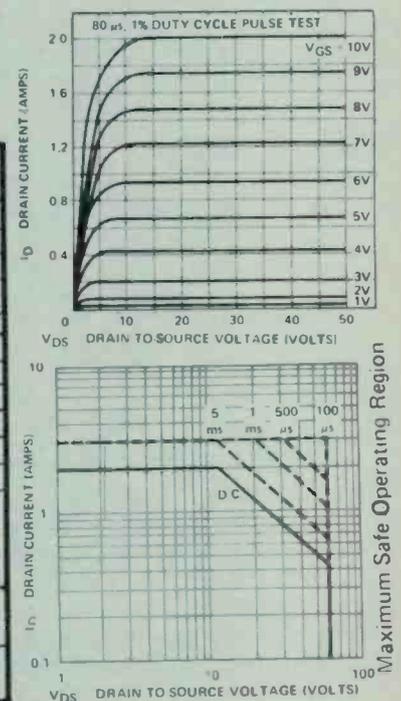
These devices may use any of the types of output circuits in general use with tubes and bi-polars, including transformer coupled (Fig. 12) where the benefits of the absence of charge carrier storage become apparent in the absence of severe ringing at the cross-over point, conventional series output such as in Fig. 3, which is a straight-forward transformation from a bi-polar

Fig. 2 Typical VMP1 performance curves (Siliconix).

Fig. 1 Electrical characteristics of the VMP devices (Siliconix).

Characteristics	VMP 11			VMP 1			VMP 12			Unit	Test Conditions
	Min	Typ	Max	Min	Typ	Max	Min	Typ	Max		
1 BV _{DSS} Drain-Source Breakdown	35			60			90			V	V _{GS} = 0; I _D = 100 μ A
2 V _{GS(th)} Gate Threshold Voltage	0.8		2.0	0.8		2.0	0.8		2.0	V	V _{GS} = V _{DS} ; I _D = 1 mA
3 I _{GSS} Gate-Body Leakage			0.5			0.5			0.5	μ A	V _{GS} = 15 V; V _{DS} = 0
4 I _{D(off)} Drain Cutoff Current			0.5			0.5			0.5	A	V _{GS} = 0; V _{DS} = 24 V
5 I _{D(on)} Drain ON Current*	1	2.0		1	2.0		1	2.0		A	V _{DS} = 24 V; V _{GS} = 10 V
6 I _{D(on)} Drain ON Current*	0.5			0.5			0.3			A	V _{DS} = 24 V; V _{GS} = 5 V
7 r _{DS(on)} Drain-Source ON Resistance*		2.0	2.5		3.0	3.5		3.7	4.5	Ω	V _{GS} = 5 V; I _D = 0.1 A
			2.4	3.0		3.3	4.0		4.6	Ω	V _{GS} = 5 V; I _D = 0.3 A
			1.2	1.5		1.9	2.5		2.6	Ω	V _{GS} = 10 V; I _D = 0.5 A
			1.4	1.8		2.2	3.0		3.4	Ω	V _{GS} = 10 V; I _D = 1 A
11 g _m Forward Transconductance*	200	270		200	270		170		m Ω	V _{DS} = 24 V; I _D = 0.5 A	
12 C _{iss} Input Capacitance		48			48			48		pF	V _{GS} = 0; V _{DS} = 24 V
13 C _{rss} Reverse Transfer Capacitance		7			7			7		pF	f = 1 MHz
14 C _{oss} Common Source Output Capacitance		33			33			33		pF	V _{GS} = 0; V _{DS} = 24 V
15 t _{ON} TurnON Time**		4	10		4	10		4	10	ns	See Switching Time Test Circuit
16 t _{OFF} Turn OFF Time**		4	10		4	10		4	10	ns	See Switching Time Test Circuit

*Pulse Test **Sample Test
Pulse Test Pulse Width = 80 μ sec, Duty Cycle = 1%



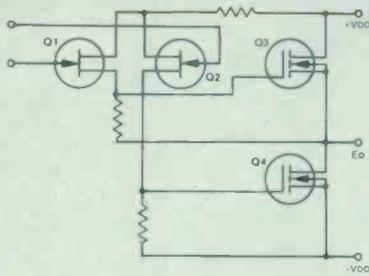


Fig. 3 Series output arrangement

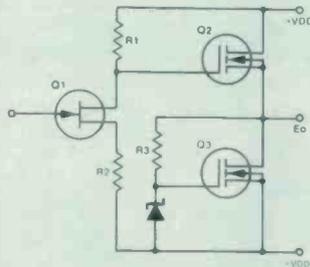


Fig. 4 Single ended output with current source.

circuit (1), and single-ended output with current source, also transposed from an excellent bi-polar circuit (2) (Fig. 4).

Bias and drive

These series of devices are n-channel, enhancement type MOSFETS, and may be biased and driven using methods appropriate to signal types and bi-polars. The drain is made positive with respect to the source and the gate enables conduction by being forward biased with respect to the source, that is to say it is biased in a positive direction. Unlike bi-polars, however, they are voltage, rather than current controlled, and circuit values are selected to provide the required voltage. Any current drawn is by the bias network itself.

Three bias methods are shown in Fig. 5. Figure 5a shows bias supplied from a fixed bias supply. It is the simplest possible method, allows extremely high input impedances since R_g may be almost any very high value desired, and its stability is limited only by the stability of the bias supply.

The design shown in Fig. 5b has the advantage of requiring no extra supply voltage since it is taken from V_{DD} . Disadvantages are low impedance and

stability. Input impedance consists of the parallel combination of R_1 and R_2 (disregarding input capacitance of the MOSFET and the very low input leakage.) There are practical limits as to how high this combination can become; if for example, we have a 60 volt supply and require 6 volts bias, we might have some difficulty obtaining higher values than 9 megohms and one megohm for R_1 and R_2 .

Higher values become more difficult to obtain, stability becomes less reliable, internal inductance and distributed capacitance become problems, and overcoming these difficulties usually costs money. In addition, if V_{DD} is subject to variation, then bias varies. In a class AB amplifier this could be quite serious, since V_{DD} varies considerably with output level; at high levels, V_{DD} can be expected to drop, causing a reduction in bias.

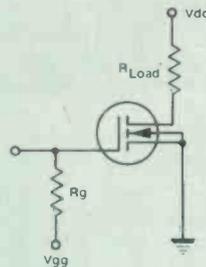


Fig. 5a. Hi-Z separate bias supply.

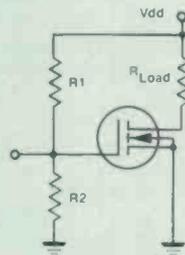


Fig. 5b. Moderate impedance supply.

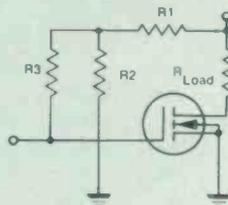


Fig. 5c. Hi-Z common supply.

While this may reduce the danger of over-driving the device, it will be forced to operate in its non-linear region which may result in unacceptable performance characteristics unless taken into consideration in the overall circuit design (e.g.

choice of feedback values). It does provide some degree of overload protection, and with correct choice of values can provide for class AB operation at low levels, shifting to class B at high levels. With these considerations in mind, and/or where moderate impedances are required, it offers a low cost, simple, and reasonably reliable method of establishing the operating point.

The method used in Fig. 5c is similar except that with the addition of R_3 higher input impedances are possible. Its configuration is similar to a noiseless biasing system frequently used in low-level bi-polar amplifiers and integrated circuits (e.g. National LM381A) but its function is somewhat different. Resistors R_1 and R_2 form a voltage divider as in Fig. 5b, but their junction now forms a fixed bias source as in Fig. 5a. Resistor R_3 can be quite high since no current flows. Meanwhile, since the parallel combination of R_1 and R_2 are effectively in series with R_3 they can be reduced to more manageable values. Alternatively R_2 can be replaced by Zener diode for stability comparable to Fig. 5a.

Input protection

Unlike most signal MOSFETS, the gate of each of these devices, with the exception of the VMP4, is protected with an internal 15 volt, 10 mA zener diode. Most signal MOSFETS, as well as the VMP 4, are unprotected, or where extremely high impedances are not required, are protected by back to back zeners. I have no information as to why this different technique is used.

This different technique is used, but it is obvious that a negative signal swing on the gate will result in forward current through the zener. If the device is to be driven beyond cutoff, the driver must be capable of delivering current during its negative swing. Alternatively, a constant current source can be used, a series limiting resistor or a driver biased to the same class of operation as the V-MOS FET.

A constant current source (we'll examine an example of its use a little later) will limit current drive to the value of the constant current diode used; a series resistance will drop the drive voltage as the diode draws current. In both cases, diode current must be limited to 10 ma maximum. Higher currents will damage the protective zener diode.

In amplifier applications, a class A driver is commonly used. However, if a class B output is used, conduction only occurs during positive half-cycles. Therefore drive signal is not required during negative half-cycles. If a source or

emitter follower driver stage is biased so as to pass no negative drive, the problem does not occur. However, great care must be exercised in the design of such a stage to ensure that drive does not disappear before the output device is cut off.

This is not too difficult with a class B or near class B stage; If the output device is operated at zero bias, then a small amount of bias on the driver will ensure conduction during slightly more than 180 degrees. Class AB operation is a little more tricky. If conduction is to occur for 270 degrees, for example, the driver should conduct for slightly more than this period.

Two types of drive circuits familiar to designers of bi-polar circuits are the Darlington and super beta, commonly used together to provide a quasi-complementary circuit. Both circuits are current amplifiers designed to provide a compound device with very high hfe and provide base current to the output device. However, similar circuits can be used with these devices to provide phase inversion in a series output stage.

Thermal considerations

As described earlier (Part 1) these devices exhibit a negative temperature coefficient with respect to current, so that as temperature rises, current is reduced, thus providing a self-inhibiting action which provides some protection against overload. However, this is not an unconditional effect Fig. 6 shows the relationship between RDS(on) and temperature (3), based on a worst case temperature coefficient of 0.7 per cent per degree C.

Suppose that the device when 'on' passes a current of 1 amp which causes it to heat up. The 'on' resistance increases (which is why current drops), increasing the voltage drop across the device and the device dissipation. Now, if adequate heat sinking is used there is no real problem but if it isn't, the 'on' resistance and junction temperature will rise to the point where extra charge carriers are generated, thus stabilizing

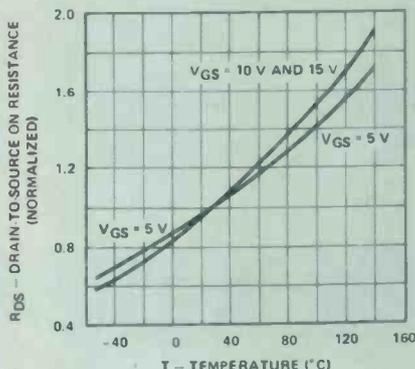


Fig. 6 Drain to source resistance against temperature (Siliconix).

RDS(on). That's great, except for the fact that this doesn't occur until the maximum safe junction temperature of 150 degrees has been exceeded.

You'll remember that we said earlier that the device was free of thermal runaway problems because of its negative temperature coefficient, but it isn't free of thermal destruction problems, and in any case, excessive temperatures will reduce output conductance. Heat-sinking requirements are, therefore, similar to those of bi-polars. The calculations of thermal operating conditions are beyond the scope of this article, but interested readers are referred to the Siliconix literature listed in the references, (4).

Extending the ratings

The current handling and therefore total dissipation capability may be increased by simply connecting several devices in parallel (Fig. 7). No ballast resistors are needed to ensure proper current sharing since if one device draws more current than another it simply gets a little warmer which causes it to draw less (assuming adequate heat sinking, of

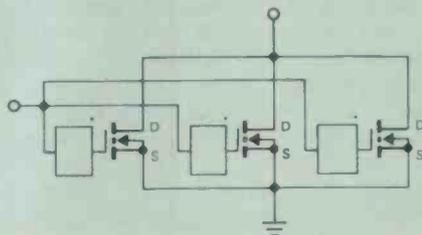


Fig. 7 Basic circuit for parallel operation (Siliconix).

course). The only major precaution needed is to keep lead inductance in the gate and source connections to a minimum to prevent parasitic oscillations, unless the devices are driven from a low impedance source.

It may be advisable to insert what the British call "stoppers" — small resistors (100 to 1000 ohms) in series with each gate, wired directly to the socket, or ferrite beads mounted on the leads close to the socket terminals. An additional plus when paralleling several devices is that the gm is multiplied by the number of devices used. Mutual conductance gm is specified as the ratio of a large change in current to a small change in control voltage. If, for example, a change of 0.4 volts on the gate produces a change of 0.1 amp through one device, connecting two devices in parallel will give us an output swing of 0.2 amps, but it will still require only the original 0.4

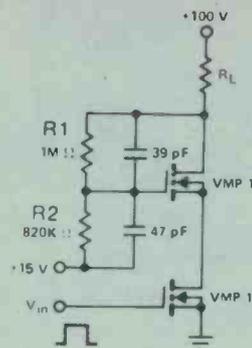


Fig. 8 Diagram for series operation (Siliconix).

volts gate swing. Since voltage gain $A = gm \times RL$, if gm is increased, A is increased.

In real use, of course, the internal resistance of two devices in parallel is less than of one, the optimum load is less, so in amplifier applications, the net amplification A is the same. But notice that the drive requirements have not changed. With bi-polars current would have to be supplied to each base, thus increasing the output requirements of the drivers. Indeed, with many high-power amplifiers using multiple output devices the drivers are also power devices.

We can also extend the voltage ratings by series operation of two or more devices Fig. 8 shows the technique. Resistors R1 and R2 bias Q2 'on', while C1 and C2 ensure fast switching. The input control signal is inserted between gate and source of Q1. Ordinarily the bottom of the divider chain is at ground potential for signal frequencies, so that circuit is really a cascade.

Maximum current and gm are the same for one device.

Practical applications

An efficient light dimmer circuit as proposed by Siliconix is shown in Fig. 9. The 4011 acts as a pulse width modulated oscillator whose duty cycle is determined by the ratio of R1 to R2, with R2 adjusted to control the brightness of the W-90 bulb. Of special interest here is the fact that with its fast switching time, the VMP1 is especially suited to pulse width modulation at power levels and suggests it as being suitable for use in switching, or class D linear amplifiers.

A DC to DC converter is outlined in Fig. 10. The VMP1s form an oscillator with positive feedback provided by the additional coil in the gate circuits. In operation the upper V-MOSFET is biased 'on', and the lower V-MOSFET

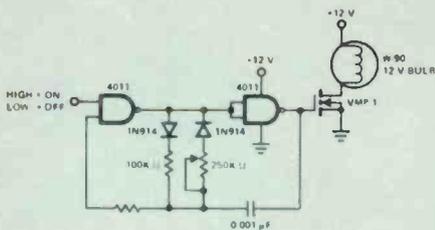


Fig. 9 Circuit of a high efficiency light dimmer (Siliconix).

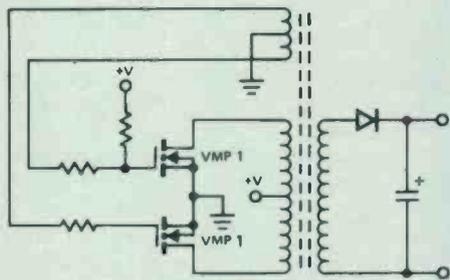


Fig. 10 A d.c. to d.c. converter (Siliconix).

is 'off'. When power is applied the upper device conducts causing current to flow from V_{dd} through the upper half of the transformer primary and the upper V-MOSFET to ground. The induced current flow through the feedback coil develops a voltage such as to shift the bias in the upper device 'off' (if the winding is connected with the correct polarity) and the lower device 'on'. This causes current flow from V_{dd} through the lower half of the transformer primary and the lower V-MOSFET to ground.

The secondary circuit consists of a single rectifier and filter. The resistor in the upper gate prevents shorting out gate bias, and the one in the lower gate keeps both sides balanced. In addition, each resistor limits current through the protective diodes. These are expen-

sive devices for such an application, but the high reliability, the reduced rf radiation (due to reduced switching transients) and the circuit simplicity easily make up for the cost. The very high circuit impedance enables running frequency to be set by the self-resonance of the transformer.

Single-ended push-pull transformer coupled audio amplifiers are shown in Figs. 11 and 12. Both utilize the biasing system described in Fig. 5b. A load-line drawn on the output characteristic will show the optimum load to be 24 ohms. In Fig. 11 gate drive is supplied by a single junction FET, and voltage feedback is taken from the output transformer secondary and series fed to the source of the input device. Distortion is under 2% at full output (try to get that with a single ended tube or bi-polar) and could probably be reduced even further by adopting a source follower output stage.

A push-pull version of Fig. 11 is shown in Fig. 12 using a differential input to provide phase splitting, drive, and a feedback point. Although the transformer winding ratio implies the use of a low impedance loudspeaker, a step-up ratio could be used for direct coupling to an electrostatic speaker, a balanced transmission line (both with some modification of the feedback circuit) an unbalanced transmission line, or a 70 volt speaker distribution line.

Notice in both circuits, and in the biasing circuits of Fig. 5, that no source resistors have been used, either for local feedback or for bias setting. In tube and bi-polar circuits it's a useful technique, and with bi-polars can be used to stabilize bias and control thermal runaway by using the increased current flow to increase the voltage drop, thus reducing base-emitter voltage. However, if used with these devices, it will actually impair the self-limiting action of its negative temperature co-efficient. If temperature rises due to high current, current flow is reduced. This would reduce the voltage drop across a source

resistor, lowering the source voltage and increasing the gate-to-source voltage, causing an increase in current flow. The circuit would work great while it lasted — which wouldn't be for long.

Record amp

Figure 13 shows a magnetic recording amplifier derived from a tube circuit. Its biggest advantage lies in its ability to provide equalization for head losses by incorporating the head within the feedback loop. Additional equalization is then required only for gap losses and tape self-demagnetization. Q1 acts as a driver for Q2, the output stage, which, with series resistor R9, provides a high impedance current source for the record head, as well as providing a mixing pad between audio and bias currents.

The record head's return path to ground is through R11. The inductance of the record head results in an impedance characteristic which rises with frequency. At frequencies at which the impedance of the head is low in comparison with R9 and R10 in series, load current is essentially constant. As frequency rises, however, head impedance becomes appreciable. With appropriate selection of R9 and R11, depending on head characteristics, the voltage across R11 decreases as the head impedance becomes significant. If feedback is taken across R11 it will decrease with rising frequency, causing an increase in gain, at a rate of 6dB/octave.

Feedback is applied across R3 via R10 and C8 (which supplies bass boost below 80 Hz) C5 and C6 provide additional high frequency boost for a total ultimate slope of 12 dB/octave. This circuit is so effective that no additional boost is needed at 15 ips, and only a small amount at 7.5 ips with high coercivity tape.

The biasing method used is that of Fig. 5c. The large amount of local current feedback provided by R2 and R3 results in a high output impedance

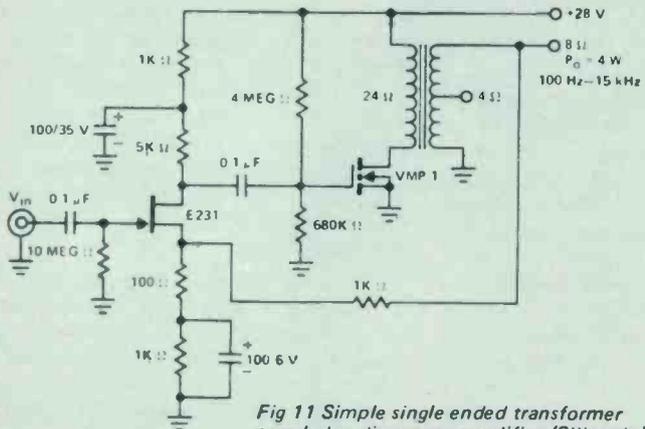


Fig. 11 Simple single ended transformer coupled audio power amplifier (Siliconix).

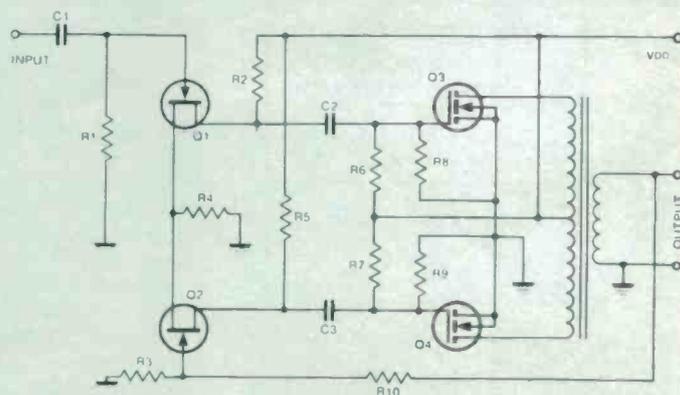


Fig. 12 Transformer coupled output.

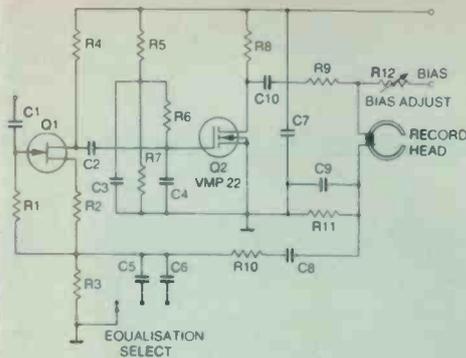


Fig. 13 Tape recording amplifier.

for Q1, so the biasing network is selected to provide high impedance with reasonable values. Capacitors C3, C4, C7 and C9 bypass bias signal to avoid overloading Q2, and to prevent attenuation of bias current.

Power amp

Figure 14 shows a high quality power amplifier designed by Siliconix Inc. (5) and described in their application notes. Output current capability is increased by using three VMP12's in parallel, providing for 6 amp current 75 watt dissipation and load optimized at 8 ohms. Q11-13 operate as a source follower, while Q8-10 form a quasi-source follower. This is accomplished by applying local feedback from drain to gate via R14, R15, and driving the gate by a modified current source. This consists of a cascade circuit with a constant current diode as the load.

For the benefit of those not familiar with these devices, a constant current diode is really a FET connected internally as shown in Fig. 15. Since current in a FET is controlled essentially by the gate-to-source voltage, changes in load

or in applied drain-to-source voltage have negligible effect since gate-to-source voltage is held constant. This is a current analogue to the zener diode and is described in detail in Siliconix literature (6).

The design is push-pull from input to output, thanks to differential circuitry throughout, prior to the drivers. Open loop distortion is low, bandwidth wide, allowing satisfactory performance with only 22 dB of feedback. Lead compensation only is used (via C4), along with the liberal use of local feedback (R4, R5, R11, R12,). The result is very low transient IM and a slew rate of over 100 V/microsecond. THD is quite respectable even though the numbers might not impress the average audiophile accustomed to amplifiers with great specs and poor sound.

Incidentally, D8 and D9 illustrate an excellent method of providing output current limiting. In this case, 9.1 volt zener diodes limit drain current to slightly less than 2 amps. At first one might be tempted to depend on the built-in protection diodes to accomplish this, but it should be remembered that these devices are for protection against static discharge. Their zener voltage of 15 volts at 10 mA cannot possibly be used since the absolute maximum permissible drain current occurs at a gate-to-source voltage of 10 volts.

Commercial amps

A simplified version of Yamaha's B1 amplifier is shown in Fig. 16, (8). In this circuit a cascade drive system is used, but in a differential form with the constant current source in the

Fig. 14 A high quality 40W amplifier (Siliconix).

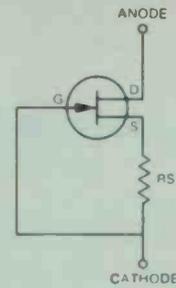


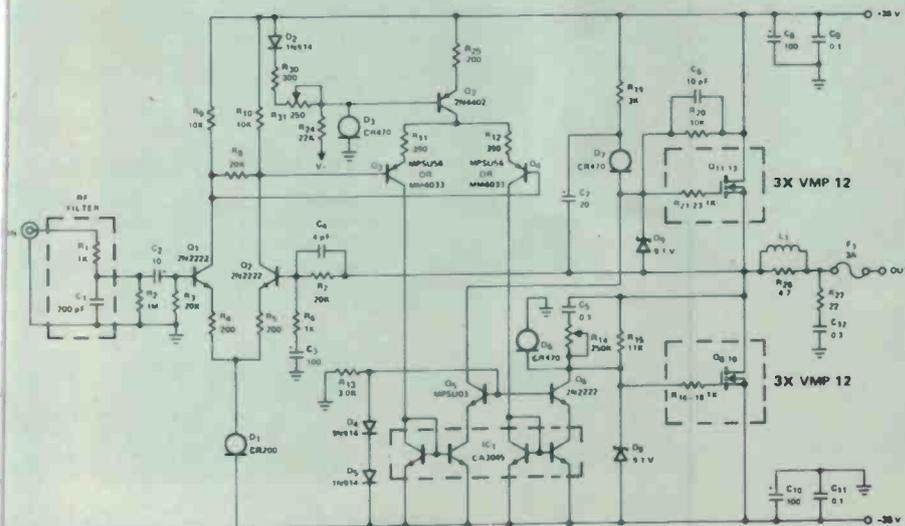
Fig. 15 A FET as a constant current diode.

common source circuit. This is an example of all FET design of excellent performance and received rave reviews in several publications including ETI. It's also inexpensive!

The VHF linear amplifier in Fig. 17 will deliver 5 watts peak envelope with second and third order intermodulation at -30 dB from 144-146 MHz. It will also prove useful as a receiver pre-amp with a noise figure of 2.4 dB. V-MOSFETS show considerable promise in rf applications because of their linear transfer characteristic, the high gain capabilities even with Ft somewhat above 600 MHz, low noise and (in receiver front ends) very wide dynamic range. Although this article has dwelt on the VMP 1 family, there is also the VMP 4, designed specifically for rf applications and which is now available.

Finally, how about something elegant for its simplicity, such as the tapered current voltage limiting battery charger shown in Fig. 18. This is especially useful with Ni-Cad batteries which are intended for stand-by use and are permanently on charge, such as electronic clocks. Overnight shut-downs of a few hours are occasionally but irregularly experienced. You know what this can do to clocks. Especially alarm clocks which are supposed to make noises, turn on radios, start the coffee at a pre-set time in the morning so you can go to work. Battery operation is not too satisfactory if the readout is on continuously, and Ni-Cads should not be on permanent floating charge.

With this little device current is supplied to the battery via the VMP-1. Gate voltage is set at a value equal to the desired end-of-charge voltage. As the battery charges, its voltage increases, reducing gate-to-source voltage, thus reducing charging current. When the battery reaches full charge its voltage, and that of the source, equals gate voltage, and charge is terminated. If a load is placed across the battery it will draw current, and as the battery voltage drops slightly below gate voltage, charging at a trickle rate occurs — automatically.



Experimentation

The various applications shown are intended as suggestions for further experimentation. They are mainly designed to illustrate various characteristics of the device under consideration, and are not necessarily representative of commercial practice or of finished designs. In some cases this may be just as well! But we would be delighted to hear of any readers' experience with any of these or other circuits.

The author's feeling is that V-MOS constitutes a genuine breakthrough in semi-conductor technology, as important as the silicon transistor and the FET itself. We'll be seeing more of these devices, with higher ratings (a 10 amp 200 volt unit is already under development) and specialized characteristics. They are said already to be in use commercially as magnetic core drivers.

Digital enthusiasts may be somewhat impatient with the strong emphasis on audio applications in this piece but other literature has placed great emphasis on digital applications, with little attention paid to linear techniques beyond the 40 watt amplifier described here. The serious reader in all areas is referred to the references at the end.

Have fun.

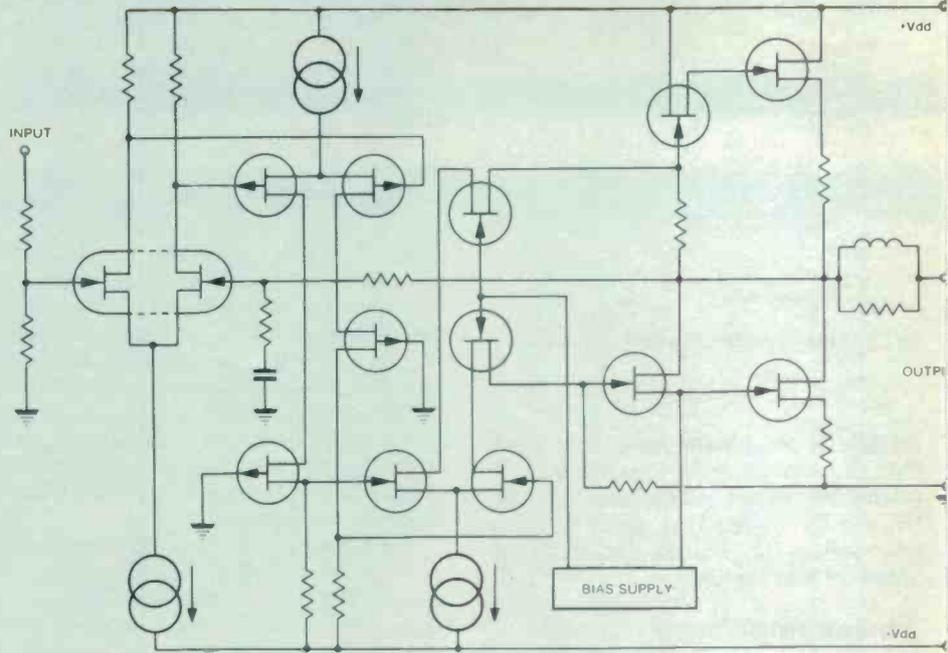


Fig. 16 Simplified Yamaha VFET amplifier diagram.

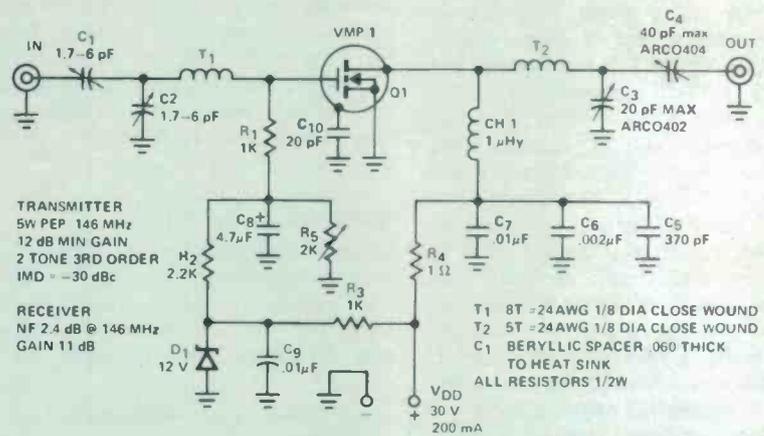


Fig. 17 144-146 MHz linear amplifier (Siliconix).

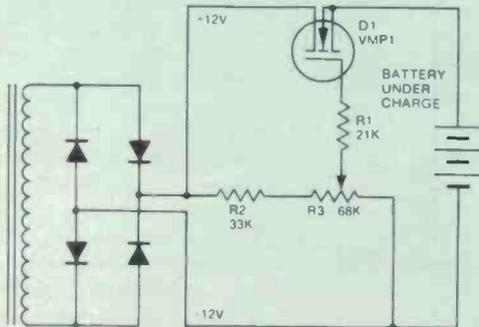


Fig. 18 Tapered current voltage limited battery charger.

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The junction FET — its haunts and habits

The first in a whole family of field effect transistors, the junction FET is found in many and varied applications. If you're new to electronics, or unfamiliar with the device, this article should introduce you to the haunts and habits of the JFET.

Brian Dance

THE JUNCTION Field Effect Transistor or JFET is a small electronic device much like a transistor in appearance which normally has three connections, although a fourth connection is attached to the metal case of some types for high frequency screening. Junction field effect transistors are one of the two main types of field effect transistor, the other type being known as the MOSFET (Metal Oxide Semiconductor Field Effect Transistor) or as the IGFET (Insulated Gate Field Effect Transistor).

Field effect transistors can be used as amplifiers and oscillators as well as for other applications for which an ordinary or bipolar transistor could be employed, but have particular advantages for certain applications. Field effect transistors are also used in the internal circuitry of integrated circuits.

Connections

As in the case of npn and pnp bipolar transistors, junction field effect transistors can be obtained in two polarities, these being known as n-channel and p-channel types. A far wider variety of n-channel types is manufactured than p-channel devices, since they tend to have a better performance, but devices of both polarities are readily obtainable.

The electrodes and circuit symbols for the two types are shown in Figure 1. The current flowing in a channel between the drain and the source is controlled by a voltage applied to the gate electrode. The gate is therefore the input electrode

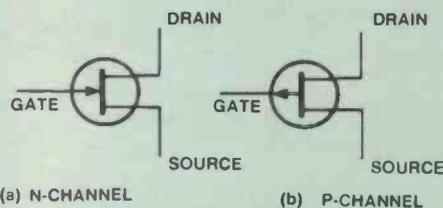


Figure 1. Symbols for n-channel (a) and p-channel (b) junction FETs.

and may be compared with the base of a conventional transistor. Similarly the drain and source may be compared with the collector and the emitter respectively.

One of the main differences between field effect transistors and bipolar transistors is that field effect transistors are essentially voltage amplifiers whereas bipolar transistors are basically current amplifiers. Thus the field effect transistor behaves more like the old thermionic valve in its circuits.

Field effect transistors tend to be more expensive than most of the common bipolar types — probably because the bipolar types are sold in much larger numbers. The economical 2N3819 n-channel field effect transistor is probably the most commonly used type and is very suitable for the readers who wish to carry out their first experiments with field effect transistors. This device is encapsulated in a black plastic or epoxy body and has the connections shown in Figure 2. The 2N3820 is a similar economical p-channel device.

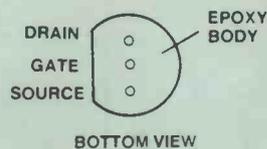


Figure 2. Connections for the common 2N3819 plastic-encapsulated n-channel JFET.

High input impedance

One of the main advantages of a field effect transistor is that it has a very high input resistance and therefore takes very little current from the circuit which feeds it — typically far less than a microamp. This means that it has very little effect on the circuit which feeds it, even if this circuit has such a high output impedance that it can deliver only a very minute current.

In order that an n-channel device shall operate correctly and have a high input impedance at its gate, it must be suitably biased with its gate negative

with respect to the other electrodes. Similarly the gate of a p-channel device has a high impedance when it is positively biased.

APPLICATIONS

Pierce oscillator

In the circuit of Figure 3 the field effect transistor is employed in a Pierce type of oscillator whose frequency is controlled by the quartz crystal shown. The advantage of using a field effect transistor in this type of circuit is that the gate imposes only a very small load from the crystal and therefore the quality factor or Q factor of the crystal is not appreciably affected, so excellent frequency stability can be obtained.

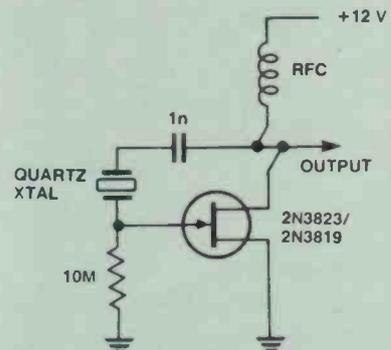


Figure 3. A Pierce crystal oscillator (National Semiconductor).

National Semiconductor recommend their 2N3823 n-channel device for use in this circuit, but the more economical 2N3819, which is made by the same type of process, is also suitable. The supply voltage is not at all critical, but the radio frequency chokes used in the supply lead should have a high impedance at the frequency of oscillation.

An advantage of this circuit is that one can change the crystal over quite a wide range of frequencies without making any other changes to the circuit and still obtain a satisfactory performance. The exact frequency range over

which the circuit will operate depends very much on the choke used and to some extent on the circuit layout.

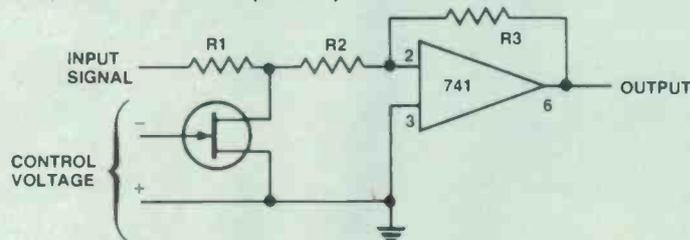
This type of circuit is suitable for use in a crystal calibrator for a receiver. If a 1 MHz crystal is employed, the output may be fed to a radio receiver to produce a signal at 1 MHz and at each multiple of 1 MHz up through the shortwave bands to provide calibration points.

Electronic attenuator

A junction field effect transistor can be used as a variable resistor, the value of which is controlled by the voltage applied to the gate electrode. As the applied bias becomes smaller, the resistance between the drain and source electrodes falls.

This property is used in the circuit of Figure 4 to design an electronic attenuator for audio signals. When the negative control voltage applied to the gate electrode is relatively large, little drain current passes through the device and the circuit behaves as if the field effect transistor were not present. However, as the control voltage falls at the gate electrode, the drain draws current from the junction of R1 and R2 so that the output signal amplitude is attenuated progressively.

Figure 4. An electronic attenuator (Siliconix).



Tone control

The circuit of Figure 5 is a tone control circuit with bass and treble boost and cut facilities. In this circuit the 2N3684 field effect transistor is used to enable the circuit to have a very high input impedance. It is used as a source follower circuit (analogous to an emitter follower) which provides a low output impedance signal coupled by a 1μ capacitor to the tone control network. This network is in the feedback circuit of the LM301A operational amplifier circuit. The 2N3684 enables a good low-noise performance to be obtained.

Lambda oscillator

A very simple sinewave oscillator is shown in Figure 6; it is essential that one n-channel and one p-channel field effect transistor are used in this circuit. The two source electrodes are connected

together and the gate of each device is connected to the drain electrode of the other device. This type of connection produces a negative resistance region in the current/voltage graph for the circuit with a peak in the graph like a Greek lambda (λ)—hence the name given to this type of circuit.

It is only necessary to connect the dual device circuit in series with a parallel tuned circuit, as shown in Figure 6, to produce oscillations at the resonant frequency of the tuned circuit used. It will oscillate at any frequency from the low audio region up to some tens of MHz, but the gate capacities of the devices used prevent operation in the regions above 100 MHz.

It is interesting to note that two separate parallel tuned circuits may be connected in series with the lambda circuit instead of the single tuned circuit shown in Figure 6. If one of these tuned circuits resonates at an audio frequency and the other at a radio frequency, the output will consist of an amplitude modulated radio frequency oscillation. This is perhaps one of the simplest possible modulated signal generators!

The output voltage from the circuit of Figure 6 is equal to twice the steady

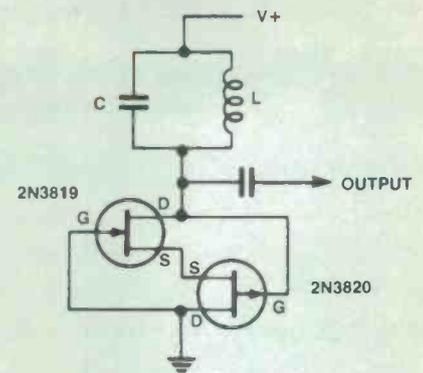


Figure 6. Sinewave oscillator using a 'Lambda' circuit.

power supply voltage applied to the circuit. Therefore this type of circuit can be very useful when one requires an output oscillation whose amplitude is accurately related to a steady applied voltage.

Complementary pairs of field effect transistors used in lambda circuits have other applications apart from simple oscillator uses.

High-impedance buffer stage

The circuit of Figure 7a shows a buffer or isolating amplifier which has a very high input impedance and low input capacitance. National Semiconductor recommend a 2N4416 field effect transistor for this circuit because it has a low input capacitance, but this is further reduced by the circuit feedback. The device is used as a source follower, so the voltage gain is about unity.

Although a 2N5139 pnp transistor is specified for this circuit, the 2N3906 plastic encapsulated type is much more readily available and is fabricated by the same process, so it can be used in this application.

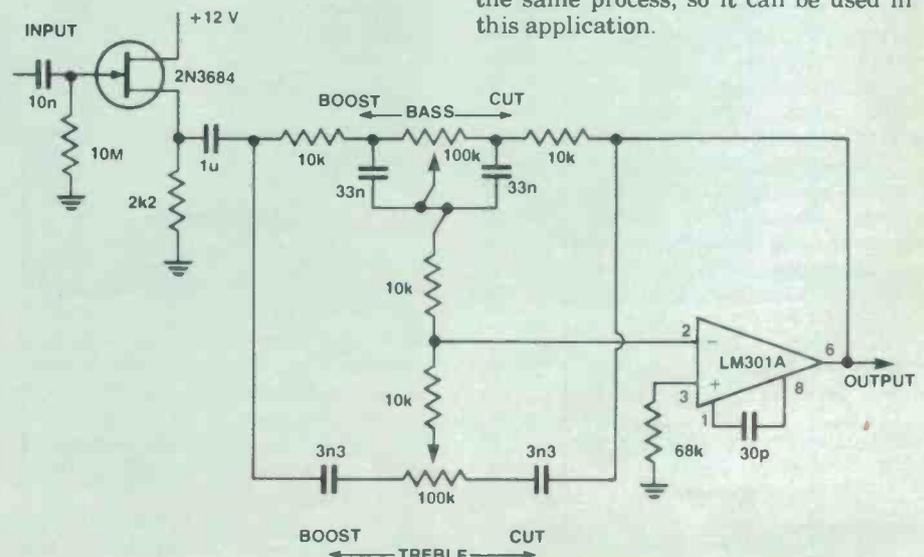


Figure 5. High input impedance tone control circuit (National Semiconductor).

High-impedance amplifier

The circuit of Figure 7b is very similar to that of Figure 7a except that the feedback circuit has been modified so that a voltage gain can be obtained. The circuit provides a gain of $R2/R1$ or 10 with the component values shown. Both the circuits of Figure 7 and of Figure 8 can be operated at high frequencies into the tens of MHz region.

RF amplifiers

Junction field effect transistors are much used in the radio frequency stages of HF, VHF and UHF receivers, since they offer a noise performance equivalent to that of bipolar transistors with improved crossmodulation and intermodulation performance. Crossmodulation is the transfer of the modulation of one carrier onto the carrier of another signal. Intermodulation occurs when two or more signals outside the pass-band combine in the circuit to form a signal within the pass-band which causes interference with the wanted signal.

The better linearity of field effect transistors over bipolar transistors is responsible for this improvement. Mullard have quoted a 12 dB improvement in crossmodulation in a narrow-band FM receiver and a 20 dB improvement in a VHF broadcast receiver as having been achieved by the replacement of a bipolar mixer circuit with a junction field effect transistor circuit.

Figure 8 shows a high-performance amplifier using two JFETs connected in 'cascode' (series) with automatic gain control (AGC) applied to the gate of the upper device. The supply is applied to the 'cold' or 'ground' end of L2 via a feedthrough capacitor. Only the L-C values need be changed to operate this stage on other frequencies to the limits of the JFETs.

Simple voltmeter

The high input impedance of a junction field effect transistor is used in the circuit of Figure 9 to produce a voltmeter with an input resistance of over 10M; in some measurements this high input impedance is necessary to prevent the current taken by a conventional voltmeter from dragging down the voltage being measured.

The input voltage being measured is divided by R1 and R2 so that a voltage of +0.2 V is present at the gate electrode when the full scale input voltage is applied for the range in question. In practice R1 should consist of a fixed resistor of a value somewhat less than that shown in the table, in series with a preset potentiometer so that the sen-

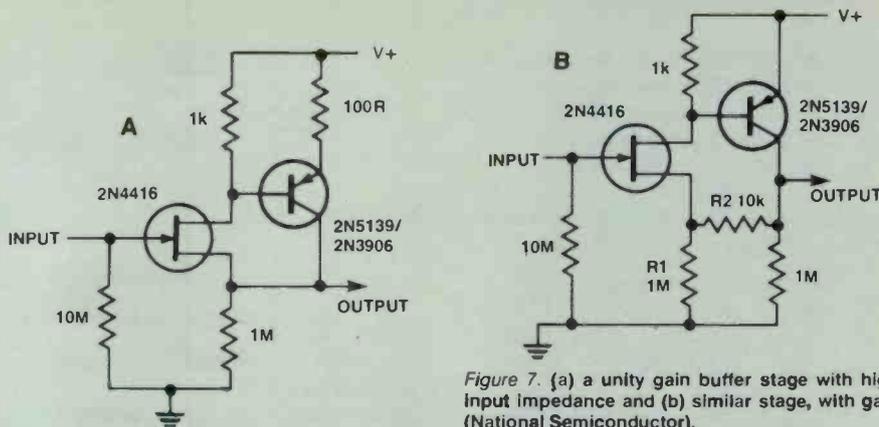


Figure 7. (a) a unity gain buffer stage with high input impedance and (b) similar stage, with gain (National Semiconductor).

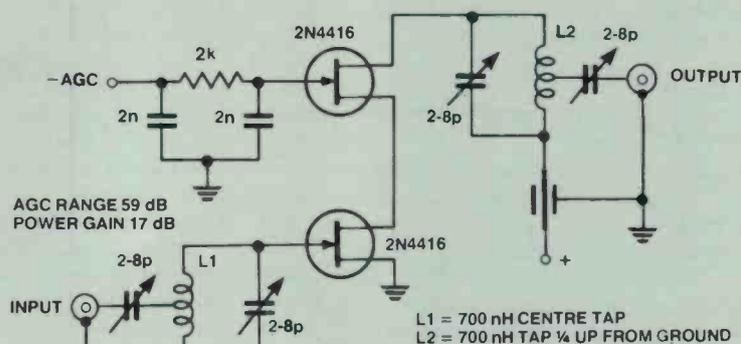


Figure 8. Typical high-performance amplifier stage employing two JFETs in 'cascode'. Values given for 200 MHz. A wide variety of RF FETs may be substituted (National Semiconductor).

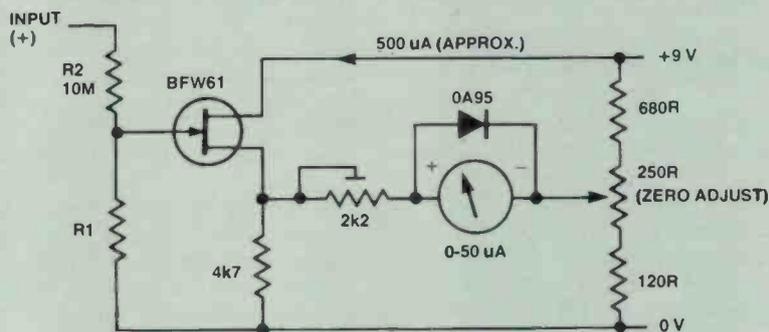


Figure 9. High input impedance voltmeter. Note that a BFW10 could substitute for the BFW61 (Mullard).

Table showing the value of R1 to be used in Figure 9 for various ranges.

Meter range	R1
250 mV	40M
500 mV	6M67
1 V	2M5
10 V	204k
50 V	40k
100 V	20k
250 V	8k
500 V	4k

sitivity of the range can be adjusted. If desired, R1 may be switched to provide a number of ranges.

the 2k2 resistor in series with the meter enables the full-scale meter current to be adjusted to allow for the characteristics of the particular device used. The diode protects the meter from overloading.

PhotoFET

Photosensitive field effect transistors (photoFETs) can be made which have a window or a lens, so that any light falling on this window affects the junc-

tion and hence the drain current of the device in much the same way that light affects a phototransistor. However, photoFETs are not very common devices.

An application of a Teledyne Crystallonics photoFET as a light-controlled variable attenuator is shown in Figure 10. The drain-to-source resistance of the

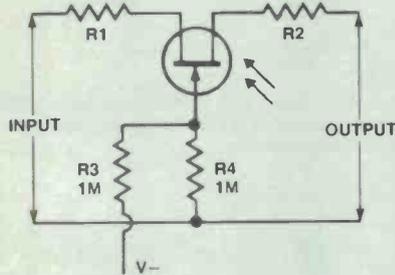


Figure 10. Example of a light-controlled attenuator (Teledyne Crystallonics).

photoFET is a function of the intensity of the illumination, so as more light shines on the device, the output rises. The negative voltage to which the resistor R3 is returned determines the range in which the drain-to-source resistance falls. Like other silicon photosensitive devices, the photoFET is sensitive to the red and near infrared regions of the spectrum, such as the radiation from an incandescent filament bulb.

HOW DO THEY WORK?

An n-channel field effect transistor consists of a channel of n-type semiconductor material between the drain and the source surrounded by p-type material of the gate electrode. Almost all of the devices are made of silicon, but a few special devices are produced in other semiconductor materials. As shown in Figure 11, the gate normally receives a

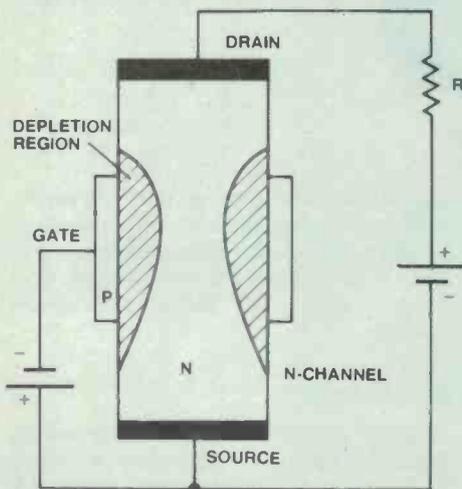


Figure 11. Control of channel width in an n-channel device.

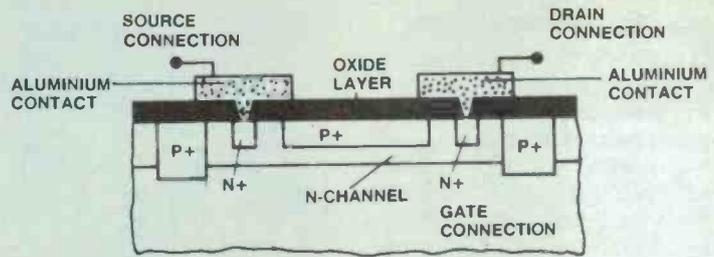


Figure 12. Structure of a silicon planar device (Mullard).

negative bias relative to the source and the drain a positive bias.

As the p-type gate material receives a negative bias, the junction formed between this material and the n-type channel is reverse biased. In any reverse-biased junction, a region which is depleted of charge carriers (electrons and holes) is formed. As this depletion region contains very few mobile charges, it acts almost as an insulator and has a very high resistance.

The gate is normally much more heavily doped than the channel material, since this results in the depletion region spreading fairly deeply into the channel and not very far into the material of the gate. As the drain is normally made positive with respect to the source electrode, the voltage between the drain and the negative gate is larger than that between the source and the gate. The electric field is therefore greater on the drain side of the gate electrode and this results in the depletion region becoming deeper on the drain side and thus producing a narrower channel on this side, as shown in Figure 11.

If the voltage applied to the gate becomes more negative, the depletion region goes deeper into the n-channel material until eventually the channel becomes completely cut off on the drain side of the gate. Very little drain current can then flow through the device. As the gate voltage becomes less negative, the channel opens again and becomes wider as the gate voltage approaches that of the source; the widening of the channel under the control of the gate voltage results in the channel current from the drain to source increasing.

As the gate-to-channel capacitance comprises a reverse-biased pn junction, the gate has a very high input resistance and passes only a very minute current (often in the pA region). However, the gate capacitance is appreciable and therefore an appreciable alternating current may flow to this electrode at high frequencies. Even when the gate and source potentials become equal, there is still a small depletion region and the gate input resistance is high.

However, if the gate of an n-channel device receives a positive bias of more than about 0.65 V, current can flow in the gate circuit and this current may damage the device.

Structure

The design of a modern field effect transistor is not implemented in the form of Figure 11, which has been used for explanatory purposes, but silicon planar technology is usually employed to produce a structure such as that of the Mullard/Philips BFW11 shown in Figure 12. This has a surface or planar structure which is covered with a protective layer of silicon dioxide at all points except where electrode connections are attached. This oxide layer prevents impurities from contaminating the surface of the material and thus producing unwanted currents.

The aluminium contacts at the source and drain electrodes allow current to flow from them into the heavily doped small n+ regions, which make good contact with the n-channel region. In some devices a number of n-type channels are connected in parallel to enable a larger current to flow at the expense of an increased gate capacitance.

P-channel types

P-channel field effect transistors have the same type of structure as shown in Figures 11 and 12, but the p and n type materials are interchanged. The gate is made of n-type material and must therefore be biased positively, as shown in Figure 13. The drain is normally biased negatively.

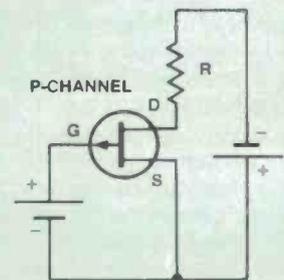


Figure 13. A p-channel device requires supplies of the opposite polarity to those used with n-channel devices.

Limiting voltages

If the bias applied to the gate is taken far beyond that required for normal operation, a point will eventually be reached at which reverse breakdown occurs. Similarly there is a limit to the voltage which should be applied between the drain and the source electrodes. However, junction devices cannot be damaged by the ordinary electrostatic charges which can accumulate on people and clothing and which can damage MOSFET devices.

Testing JFETS

It is relatively easy to check that a junction field effect transistor is able to function correctly. The circuit of Figure 14 may be used for an n-channel device and that of Figure 15 for a p-channel device.

If the gate is initially connected directly to the source (and not as shown), it will be found that the meter provides a reading of a few mA. This current is limited by the 1k resistor in the drain circuit to a safe value.

If the gate electrode is now connected to the 10M resistor as shown, the gate to channel junction is reverse biased. Thus the channel width decreases and with

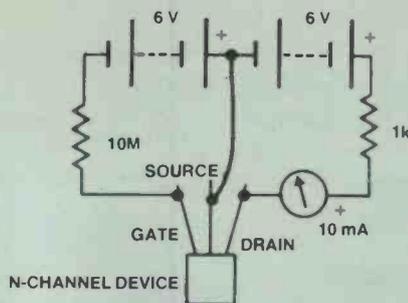


Figure 14. Testing an n-channel device.

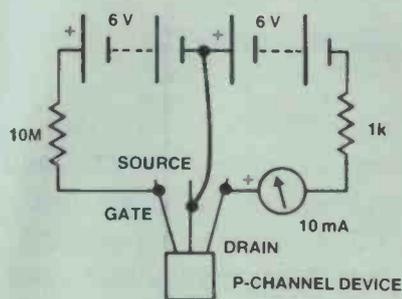


Figure 15. Testing a p-channel device.

most devices the drain current will fall to zero in the circuits shown. As the gate circuit has a very high resistance, the

voltage can be applied to it through a high-value resistor; indeed, it is interesting to note that the human body can be used in place of the 10M resistor shown when testing junction field effect devices.

If one wishes to test a device and does not know the connections, one can first find two connections in which a small current will pass in either direction. These are the source and drain connections.

A current should pass from the third electrode, the gate, only in one direction to either of the other two electrodes. If conduction takes place when the gate is positive, one has an n-channel device, whereas if conduction takes place when the gate is negative, the device is of the p-channel polarity.

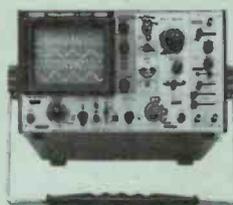
One cannot easily determine which electrode is the drain and which is the source, but these electrodes are to some extent electrically interchangeable. ●

USEFUL BOOKS

Two very useful books, though difficult to obtain, are: 'FET Databook' from National Semiconductor and 'Field Effect Transistors' from Philips.



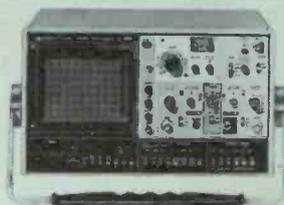
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Lab Notes

Using BiFET and BiMOS op-amps

The availability of BiFET and BiMOS op-amps has revolutionised circuit design since they appeared on the scene six years ago. While we've used devices like the CA3140 op-amp in projects we've not got around to describing practical applications circuitry. This 'Lab Notes' fills that gap.

Brian Dance

THE AVAILABILITY of BiFET and BiMOS devices in various packages with one to four operational amplifiers per package has revolutionised the operational amplifier market. Apart from the relatively expensive hybrid FET input devices, other FET input operational amplifiers had been available for some considerable time, so why should BiFET and BiMOS devices be so important?

The first point to note is that amplifiers with FET input stages can offer far higher input impedances than devices with ordinary bipolar transistors in their input stages. For example, the well-known 741 has an input impedance

of the order of 1M and a maximum input bias current of 500 nA. The use of bipolar transistors to obtain a high input impedance has been pushed to the limit in devices such as the LM108, using supergain input devices to provide a typical input impedance of 70M and an input bias current of just under 1 nA. These values may be compared with those of some of the economical BiFET and BiMOS devices, where typical input impedances are of the order of 1 Terrahm (one million Megohms!) and input currents are some tens of picoamps (pA) at room temperature.

Thus if one connects the input of one of these BiFET or BiMOS amplifiers to

almost any circuit, it will impose a very small load on that circuit. This can be a vital consideration when one is designing such high-impedance circuits as those used in pH meters or in ionisation chamber smoke detector circuits, whose output current is inadequate to drive devices such as the 741.

If one considers the very early types of monolithic FET input operational amplifiers (such as the Fairchild μ A740), they do have the desired high input impedance, but their disadvantage is that their input offset voltage and its temperature coefficient are so high that they do not approach the high standard of performance required by the modern

INTRODUCTION TO THE BIMOS AND BIFET OP-AMP

The first BiFET products were announced by National Semiconductor in 1975 (the LF155, LF156 and LF157 series, where LF signifies Linear FET device). The main advantages of these products is that the junction FET devices used in their input stages are fabricated on the same silicon chip as the remainder of the operational amplifier. Although hybrid operational amplifiers with FET input stages had been available for some considerable time previously, all of these hybrid devices contained the junction FET devices fabricated on a separate silicon chip from the remainder of the operational amplifier. Such hybrid devices can be made to have a very good performance if adequate trouble is taken in their design, but the extra labour costs involved in the testing of the separate chips for appropriate matching characteristics and in connecting the two chips in a single hybrid package inevitably resulted in a price

tag far above that of modern BiFET devices. The general type of construction of a BiFET device is shown in Figure 1, the channel between the source and the drain electrodes of the FET input devices being fabricated by ion implantation.

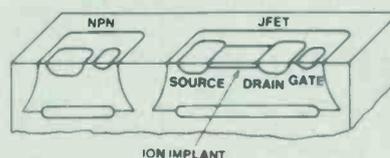


Figure 1. Construction of a BiFET device.

Although National Semiconductor produced the first BiFET products, it was not long before other manufacturers entered the BiFET market, and such products are now available from Advanced Micro Devices, Analog Devices, Fairchild, Harris

Semiconductor, Motorola, Intersil, Precision Monolithics, Raytheon and Texas Instruments, although National Semiconductor still offer the widest range of BiFET products, details of which can be found in their Linear Databook.

Very soon after National Semiconductor had announced the first BiFET products, RCA introduced their first BiMOS product, the economical CA3130 operational amplifier. This has some similarities to the BiFET amplifiers, but employs MOSFET transistors in the input stage rather than junction FET devices. RCA soon introduced further BiMOS devices, one of the best known type being the CA3140, which can be used as a pin-for-pin replacement for the 741 when a higher performance is required. More recently the CA080 series has been introduced as pin-for-pin replacements for the Texas Instruments series of TLO80 BiFET types.

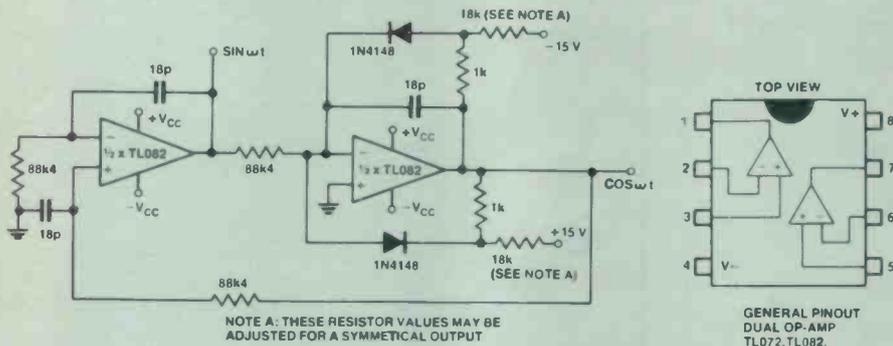


Figure 3. Quadrature oscillator producing two outputs 90° out of phase, using a TL082 dual op-amp — pinout at right.

professional engineer. Modern BiFET and BiMOS devices provide a very high input impedance with relatively good stability and temperature performance — although the input impedance of any of these devices at 25°C is much greater than over the full temperature range.

In general BiFET and BiMOS economical devices offer a comparable performance. If anything, BiMOS devices tend to offer the lower input bias currents and BiFET products the lower noise levels. However, premium devices of both types are available with performances far above the average for the type of device concerned.

Half-Hertz oscillator

Figure 2 shows the use of the economical TL081 device in a simple 0.5 Hz square wave oscillator. The TL081 is a

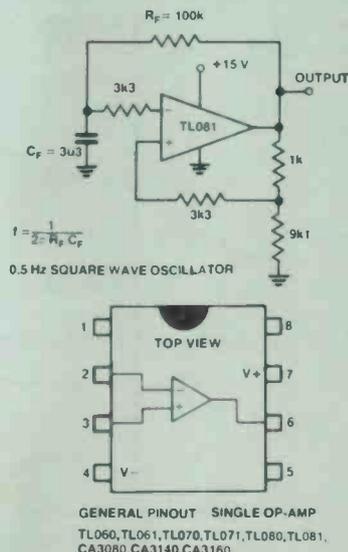


Figure 2. Half-Hertz oscillator using a TL081 — pinout below.

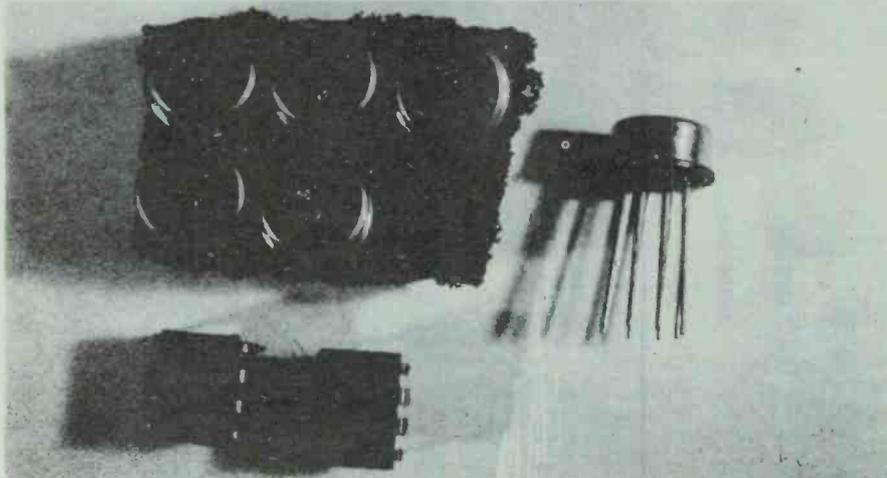
single operational amplifier in a dual-in-line package with the connections shown in Figure 2; the pin connections are the same as those of the well-known 741 devices, internal frequency compensation being employed so that no external compensating capacitor is required. External offset adjustment can be made when required by means of an external variable resistor. The TL071 is a similar low-noise device with the same connections, and is quite suitable for use in this circuit, but its low-noise characteristics are not needed. The TL061 is a low-power device with the same connections.

The frequency of oscillation of the Figure 2 circuit is given by $f = 1/(2\pi R_F C_F)$, or about 0.5 Hz with the values shown. The high input impedance of the circuit enables a relatively high value of feedback resistor, R_F , to be employed, so the value of C_F can be reasonably small for a given frequency of operation. About nine-tenths of the output voltage is fed back to the non-inverting input to provide positive feedback to maintain oscillation. The capacitor C_F charges and discharges through R_F according to whether the state of the output voltage is 'high' or 'low' at the time concerned.

The circuit of Figure 2 generates square waves which are approximately symmetrical. However, if a circuit which generates waves with an unequal mark-to-space ratio is required, it is only necessary to connect a resistor of perhaps 10k to 50k in series with a diode across R_F . The direction in which the diode is connected determines whether the output spends the greater part of its time in the 'high' or in the 'low' state.

100 kHz oscillator

Figure 3 shows the circuit of a 100 kHz oscillator providing two outputs which are 90° out of phase with each other. Although the TL081 is perfectly satisfactory for use in this circuit, it is more convenient to use the dual TL082 device so that this one device is all that is needed. The connections of the 8-pin dual-in-line TL082 device are shown in Figure 3; it employs internal frequency compensation, but has no external offset adjustment facilities.



Modern BiMOS and BiFET op-amps come in both can and DIL packages.

Lab Notes

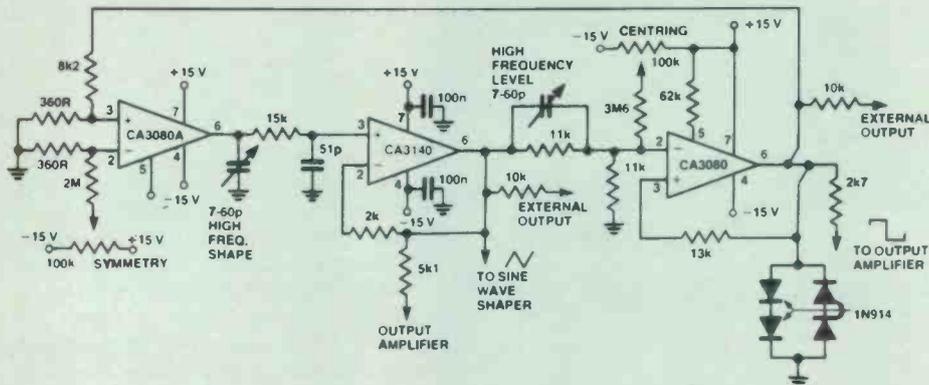


Figure 4. Function generator circuit. Sourcing or sinking current from pin 5 of the left hand CA3080 will vary the frequency.

BiMOS generator

A function generator which produces square and triangular waveforms is shown in Figure 4. It employs a CA3140 BiMOS device together with a CA3080A and CA3080. A particular feature of this circuit is that a frequency range of one million to one can be obtained by the use of a single variable resistor, or alternatively by the use of an auxiliary sweeping signal.

A CA3130 device may be employed instead of the CA3140 shown, but in this case a frequency compensating capacitor (about 56p) must be connected between pins 1 and 8, since the CA3130

is not internally compensated. The CA3160, which does not require any external frequency compensation, is also suitable for use in this circuit.

The high frequency linearity of the ramp is adjusted by the 7-60pF variable capacitor connected between the output of the CA3140 and the output CA3080 device. The triangular wave output level is determined by the four 1N914 level-limiting diodes in the output circuit and the network connected to pin 2 of the CA3080.

It is important to minimise lead length and parasitic coupling capacitance in this circuit by careful layout.

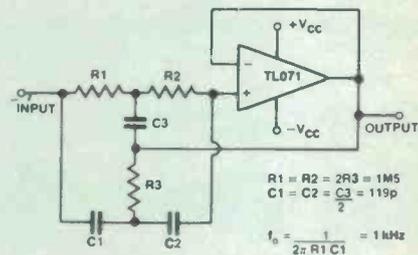


Figure 5. Notch filter using a 'Twin-T' filter section on the input of a TL071 op-amp.

Notch filter

The circuit of Figure 5 shows the use of a TL071 low-noise amplifier in a notch filter circuit. This is the normal 'twin-T' filter in the input circuit, in which one of the 'T' sections consists of R1, R2 and C3 and the other part of C1, C2 and R3. It is designed to reject signals of one particular frequency (the notch frequency), whilst passing signals of any other frequency virtually unattenuated.

For optimum performance, when a sharp notch in the frequency response is required, the components should have matched values (to within 1% or 2%). When the values shown are employed, the notch frequency occurs at approximately 1 kHz. An advantage of using a high input impedance device such as the TL071 is that relatively large values may be employed for R1, R2 and R3 and,

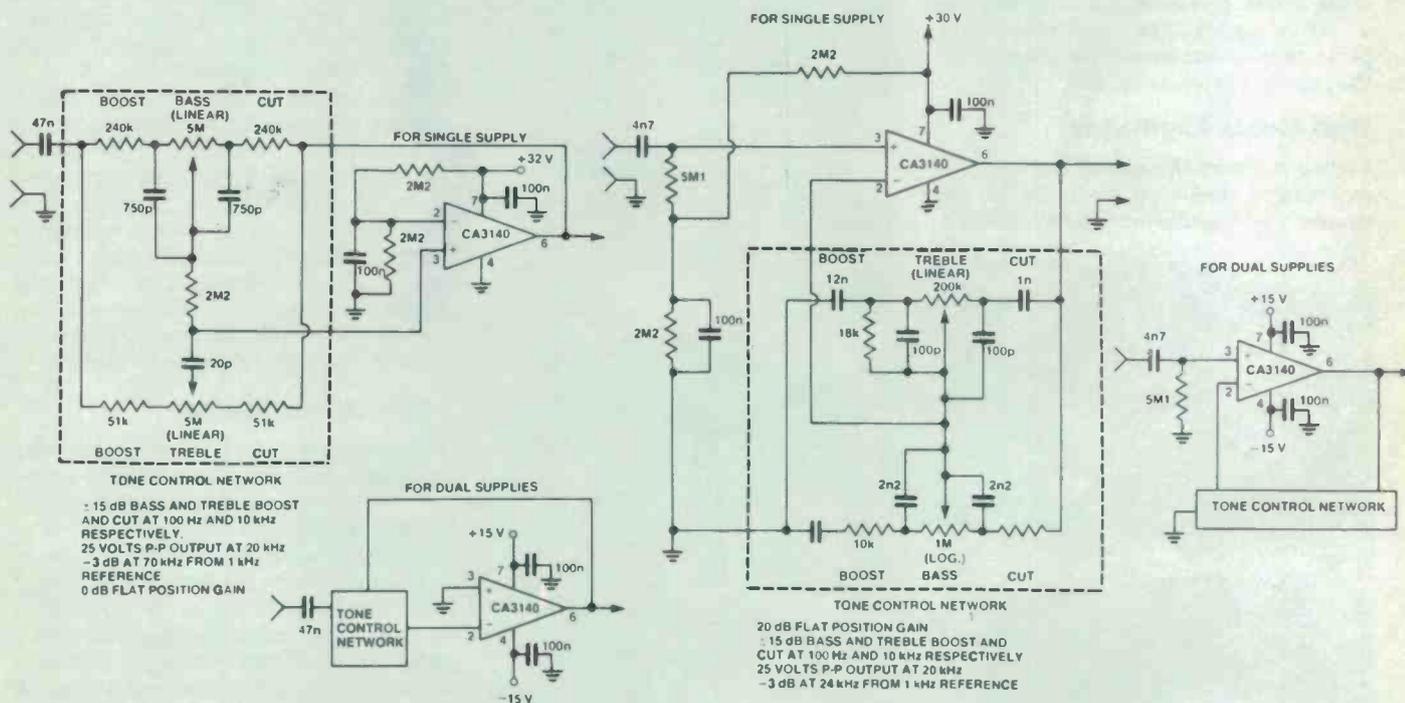


Figure 6. Baxandall type tone control circuitry, with unital gain (flat position).

Figure 7. Tone control circuit with 20 dB of gain, flat position.

Lab Notes

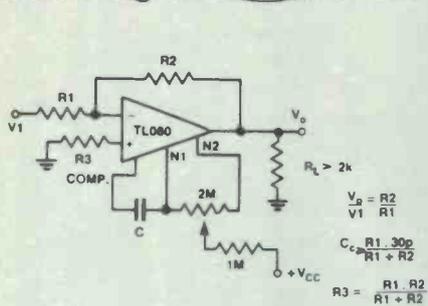


Figure 12. Simple voltage-variable gain amp using the TL080.

Variable gain

The simple circuit of Figure 12 is an amplifier which provides a variable gain set by the potentiometer. A TL080 device is employed, so the compensating capacitor C_c is required, since this device is not internally compensated.

Ice warning

The circuit of Figure 13 employs three of the four amplifiers of the TL084 device in an ice warning detector. It is especially suitable for use in vehicles to warn the driver when the temperature of the thermistor (placed outside the vehicle) falls below 0°C .

When the temperature of the thermistor falls, its resistance rises and the current flowing through the thermistor decreases. Thus the inverting input of the TL084 connected to this thermistor receives less current from the positive supply line and its output voltage tends to rise. This output voltage is fed to the TL084 output amplifier and produces a voltage across the LED, which lights, providing the required warning.

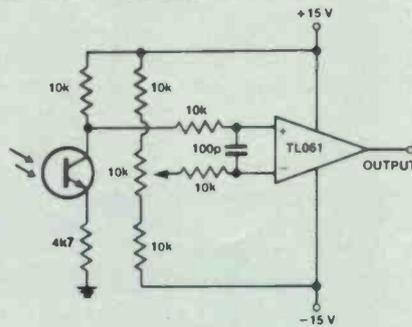


Figure 14. Low-level light detector using FPT100 or similar phototransistor.

Light detector

The circuit of Figure 14 is a low-level light detector preamplifier using the low-power TL061 device with a TIL601 or similar phototransistor. The variable resistor can be used to balance the output at any particular value of light level.

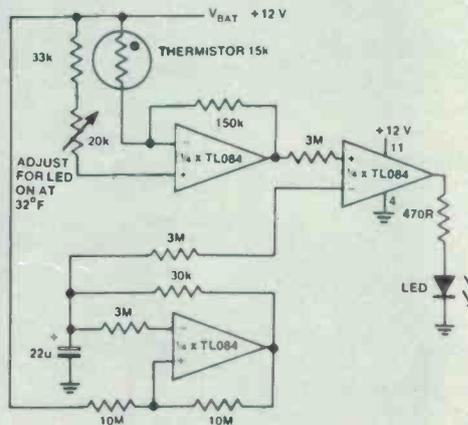


Figure 13. An ice warning indicator.

Sine shaper

The circuit shown in Figure 15 uses a CA3140 as a voltage follower in combination with diodes from the CA3019 array to convert the triangular signal from a function generator into a sinewave output, which has typically less than 2% harmonic distortion.

The circuit is best adjusted using a distortion analyser, but a fairly good adjustment can be made by comparing its output signal on an oscilloscope with that from a good sinewave signal generator. The initial slope is adjusted by R_1 , followed by an adjustment of R_2 . The final slope is established by adjusting R_3 , thereby adding additional segments that are contributed by these diodes. Repetition of the adjustments may be necessary, since there is some interaction between the adjusting potentiometers.

Wien bridge

A CA3140 BiMOS amplifier is used in the circuit of Figure 16, together with a CA3019 diode array, to form a Wien bridge oscillator. The zener diode shunts the 75k feedback resistor and, as the output signal amplitude increases, the zener diode impedance rapidly decreases so as to produce more feedback, with a consequent reduction in gain. This action stabilises the output signal amplitude. This combination of a monolithic zener diode and the bridge rectifier tends to provide a zero temperature coefficient for this regulating system.

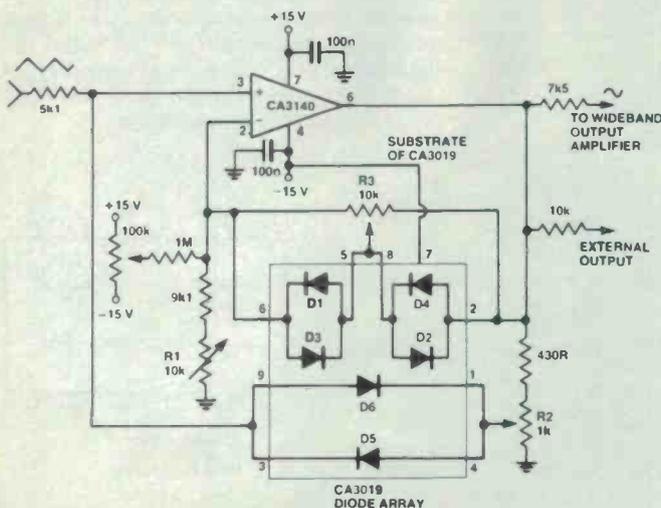


Figure 15. A triangle-to-sine waveshaping circuit employing a CA3140 op-amp and a CA3019 diode array.

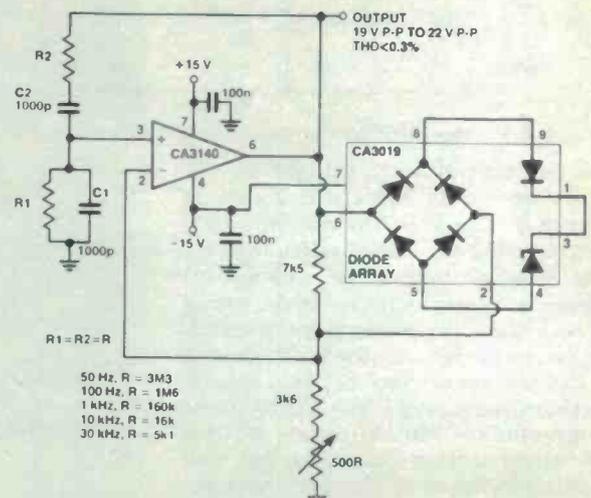


Figure 16. A Wien bridge oscillator featuring amplitude stabilisation via the zener action from the CA3019 diode array.

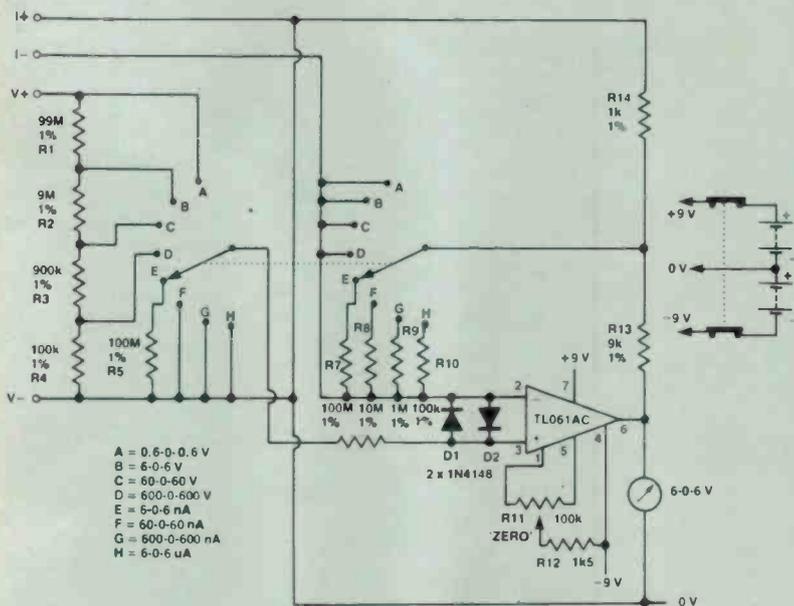


Figure 17. A multi-range voltmeter with high impedance input plus multi-range low-current meter.

As the output circuit contains no RC time constant, there is no lower frequency limit for operation. If $C1 = C2 = 1\mu$ (polycarbonate) and $R1 = R2 = 22M$, the operating frequency can be about 0.007 Hz. At high frequencies, as the frequency is increased the amplitude of the signal must be reduced to prevent slew rate limiting from taking place. An output frequency of about 180 kHz will reach a slew rate of about 9 V/us when the output voltage amplitude is about 16 V peak-to-peak.

Meter

The high input impedance of BiFET and BiMOS devices has led to their use in many voltmeters of high input resistance and also in meters to measure very small currents.

The circuit of Figure 17 was designed by Texas Instruments for the measurement of voltages in the range ± 0.6 V to ± 600 V, where the source resistance may be quite high, and to measure currents from 6 nA to 6 uA. The instrument was required to accept inputs of either polarity and be inexpensive, robust and reliable. It also had to have a long battery life, so a TL061 low-power operational amplifier device was selected. An inexpensive centre zero meter is considerably cheaper than a liquid crystal display and would provide adequate accuracy for the purpose.

When the switch is in one of the positions A to D inclusive, the instrument is set for the measurement of voltages.

The amplifier has a non-inverting gain of 10 and range selection is achieved by a simple potential divider network with a fixed input impedance of 1000 megohm. A panel-mounted 'centre zero' control is included in the circuit to facilitate corrections for the mechanical movement of the meter zero and for the change in the operational amplifier input voltage offset (for example, with temperature).

In the current measuring mode of switch positions E to H inclusive, the amplifier operates as a current-to-voltage converter. For the most sensitive range of 6 nA, a transimpedance of 1 Gigaohm is required to produce a full-scale deflection of the meter. Rather than use a resistor of such a high value, a resistance multiplier arrangement was devised with a 100M feedback resistor for the most sensitive range.

The two diodes across the input of the operational amplifier in conjunction with R6 provide protection against any

gross overloading of the instrument. A suitable arrangement incorporating a fullwave rectifier into this circuit would allow alternating input signals to be measured, but arrangements would have to be made to allow for frequency roll-off of the response at high frequencies.

3 pA meter

A CA3160 and a CA3140 are used in the circuit of Figure 18 to construct a picoammeter with ± 3 pA full scale deflection (one picoamp = 10^{-12} amps). Pins 2 and 4 of the CA3160 are connected to ground, so the input pin 3 between them is effectively 'guarded'. If slight leakage resistance is present between terminals 3 and 2 or 3 and 4, there would be zero voltage across this leakage resistance and this would reduce the leakage current by a large factor.

It is preferable to operate the CA3160 with its output pin 6 near the ground potential, so as to reduce the dissipation by reducing the device supply current. The CA3140 serves as a x100 gain stage to provide the required plus and minus output voltage swing for the meter and feedback network. A 100:1 voltage divider network consisting of a 9k9 resistor in series with a 100 ohm resistor sets the voltage at the 10 kMohm resistor to ± 30 mV full-scale deflection. This 30 mV signal results from ± 3 V appearing at the top of the voltage divider network, which also drives the meter circuitry.

It is possible to switch the 9k9 and 100 ohm network in the output circuit so that current ranges from 3 pA to 1 nA can be handled using the single 10kM resistor.

The writer has seen circuits using BiMOS devices published for use in measuring currents down to 100 femtoamps (0.1 pA), but obviously extreme care is required to ensure the insulation is adequate when such small currents are being measured.

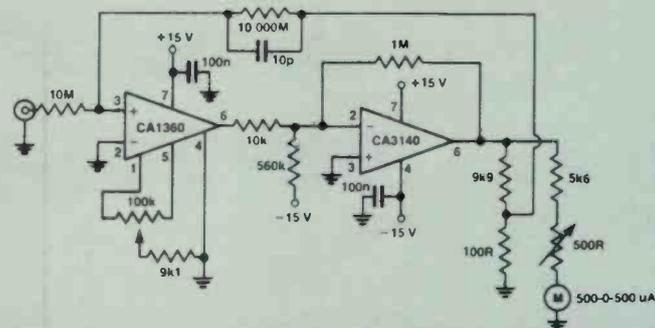
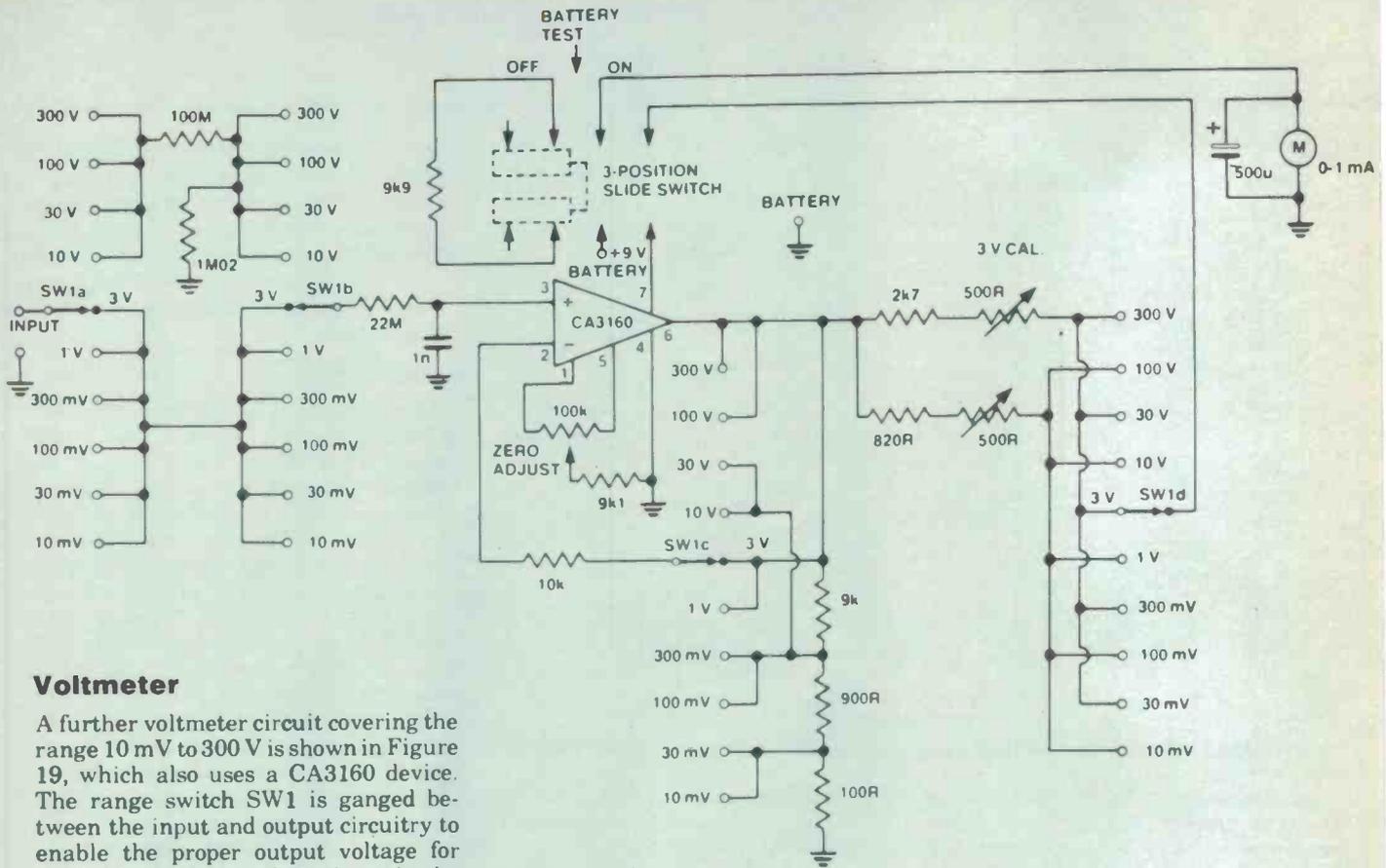


Figure 18. This circuit will measure very low currents — full-scale deflection is \pm three picoamps!



Voltmeter

A further voltmeter circuit covering the range 10 mV to 300 V is shown in Figure 19, which also uses a CA3160 device. The range switch SW1 is ganged between the input and output circuitry to enable the proper output voltage for feedback to terminal 2 through the 10k resistor to be selected.

This circuit is powered by a single 8.4 V mercury battery, the power supply current being somewhat less than 500 uA plus the meter current required to indicate a given voltage. Thus the supply current rises to about 1.5 mA at full-scale deflection.

Any readers who experience problems

Figure 19. Example of a multi-range voltmeter measuring from 10 mV to 300 V.

in obtaining a CA3160 may use a CA3130 with a frequency compensation capacitor of about 56p between pins 1 and 8.

The aim of this article has not been to introduce readers to all the latest

BiFET and BiMOS devices (of which there are large numbers), but rather to give an indication of the wide selection of circuits that can be made with just a few of the standard types of device which are readily available.

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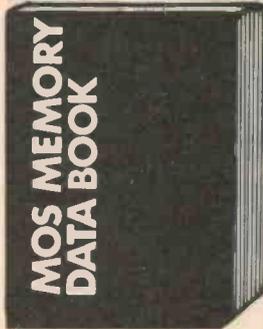
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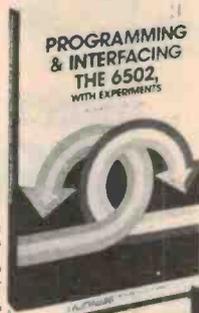
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Hand held 20 MHz digital frequency/period meter features liquid crystal display

This project features a 4½-digit liquid crystal display and is completely portable as it's battery powered. It counts to 20 MHz in four ranges (2 kHz, 20 kHz, 2 MHz, and 20 MHz) and measures period from 200 ms to 200 us (full scale).

Part 1
Geoff Nicholls

NO MATTER HOW you're involved with electronics, there's always a need to measure various quantities — voltage, current, resistance, frequency, etc. What you want to do is put a *number* to that quantity and the best way to do that is to employ a digital display.

Digital displays, based on neon-filled vacuum tubes called 'Dekatrons' first appeared in the late '50s-early '60s. With the advent of seven-segment LED displays, digital measuring instruments rapidly became commonplace. With the introduction of liquid crystal displays, which require virtually no power to operate, battery-operated portable measuring instruments burgeoned.

Portable instruments can be used almost anywhere — right where you want to make the measurement. It's not always possible or convenient to take the equipment to the workshop. The majority of multimeters are portable, handheld devices and we thought, "why shouldn't a frequency meter be the same?"

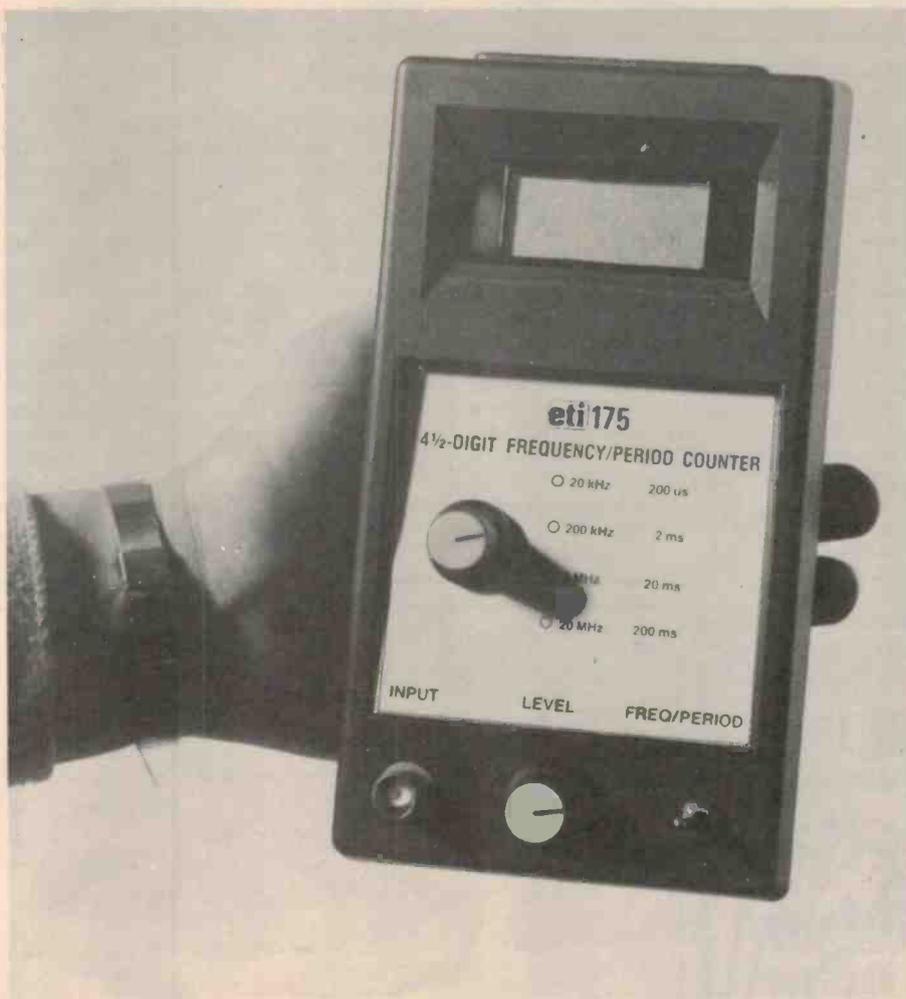
There are so many occasions in electronics today (... err, pardon the pun) where you need to measure frequency. In times past, it was almost the exclusive reserve of 'the RF man'. These days even those involved in audio and computing need to have frequency measuring facilities.

Just being able to measure frequency is great, but what sort of accuracy is generally required? I asked around and, for the great range of applications, it seems six-figure accuracy, while seemingly desirable, is not really necessary.

Take a computer modem for example. These use two audio tones to signal the 'high' and 'low' bits of the digital information transmitted through them. The accuracy required is a few Hertz in several thousand Hertz — about 0.1%.

The accuracy and temperature stability of your 'off-the-shelf' quartz crystal is 100 parts per million (ppm) and 20 ppm/°C, respectively. Put another way — 100 Hz per megahertz accuracy, 200 Hz per megahertz for a 10°C temperature range.

All that adds up to this — a 4½-digit display has all the accuracy you need for the greater range of applications. (The left-most digit on a 4½-digit display will only



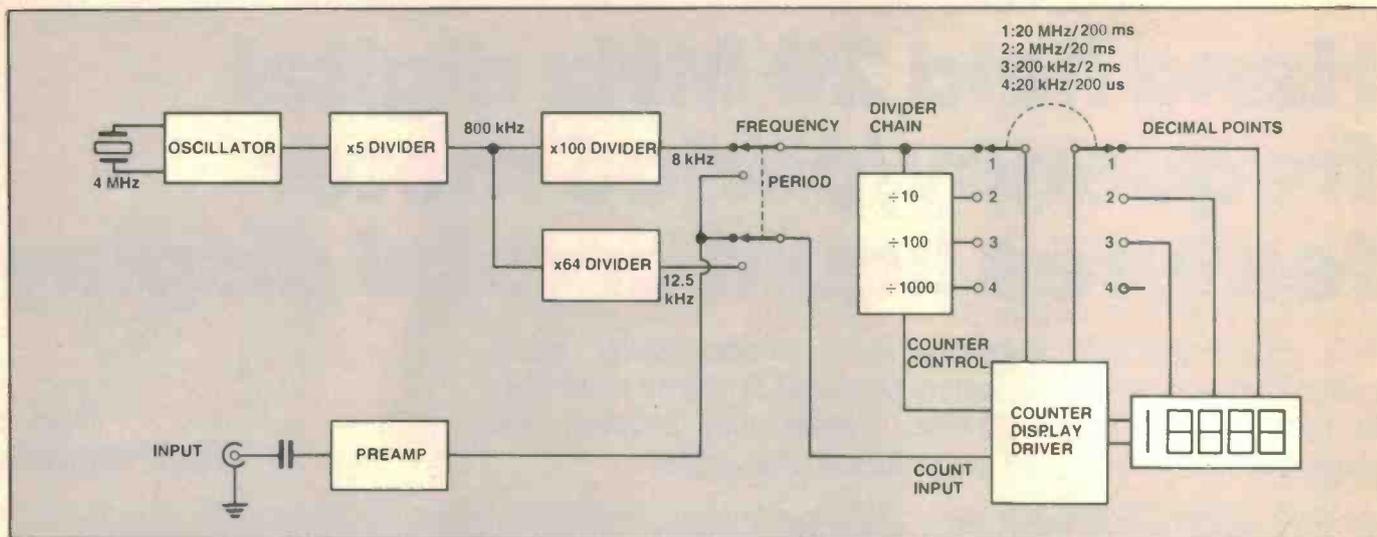
read '1', while the other four will read 1 to 9).

That's when I went searching for a 4½-digit counter-display driver as 4½-digit liquid crystal displays are readily available.

I turned up Intersil's ICM7224IPL, which is perfect for the job, and what's more, it's capable of counting to 20 MHz! A portable, battery-operated digital frequency meter was a distinct possibility, so I obtained several samples from R&D Elec-

tronics, the Intersil agents, through All Electronic Components in Melbourne.

Many months before we tackled this design, a representative from Mayer Krieg & Co had called in and left us a range of sample 'Unimes' cases, amongst which was a small handheld case just made for the application. It was palm-sized and featured a 'sculpted' front with a window just the right size for a liquid crystal display. It also had a battery compartment to take a ▶



standard No 216 9 V battery. It was all too easy!

The electronic design was a 'snack' but it was obvious that fitting the components on a pc board and into that case was going to require some pretty fancy juggling. Right here, Murphy stepped in. After considerable effort with the mechanical design, it was abandoned and another case sought. But Mayer Krieg came to our rescue with a somewhat larger handheld case with all the features we wanted. Known as the Unimes 2, it measures 180 mm long by 100 mm wide and from 35 to 44 mm deep. It has a battery compartment in the rear to take 4 x AA cells, plus a wire tilting bail so that the case can be either laid flat or stood up on a flat surface. There is a recessed window in the front, up top, for a display and a recessed, sloping section for a front panel label.

Design

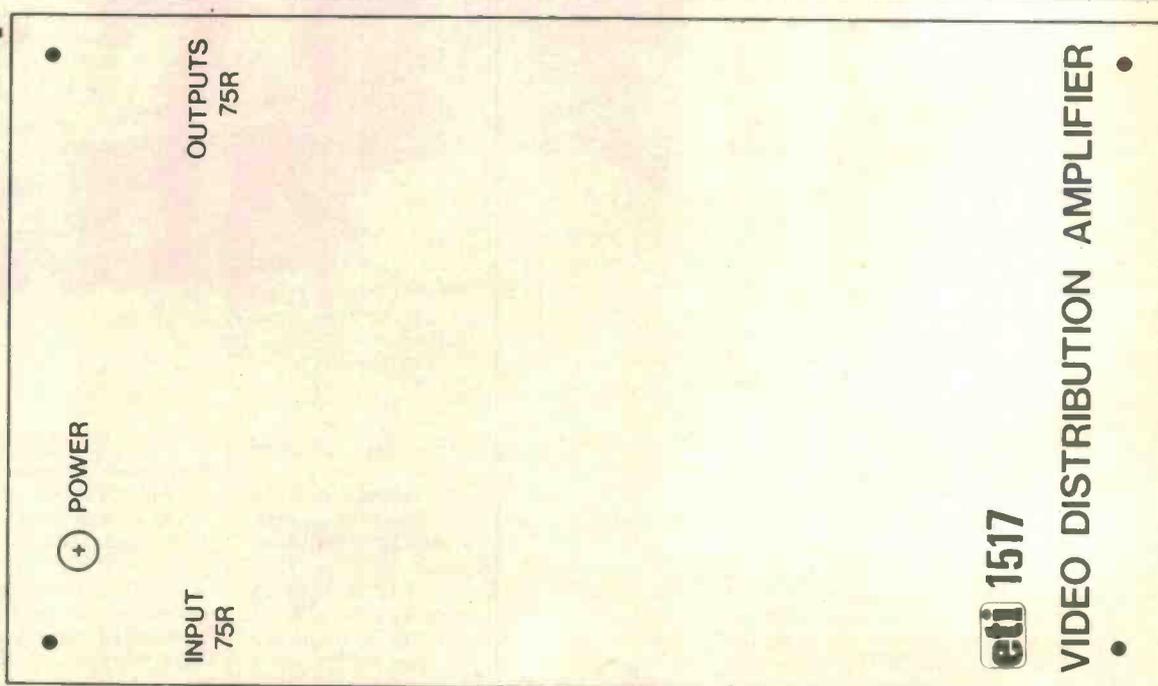
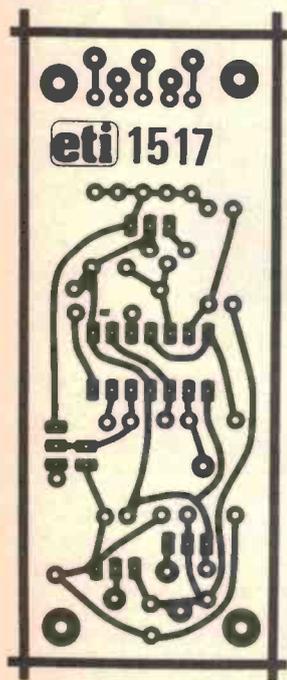
Frequency counter designs may be classified according to the type of range switching employed. In low-cost designs there are only two common types, the *switched gate period* type and the *input divider* type. The latter divides the input signal down by various ratios, according to the range selected, while keeping a fixed gate period, typically one second. This allows the actual counter to operate at a low frequency while counting a high input frequency but requires high speed dividers for one or two stages. I decided to take advantage of the excellent high frequency counting ability of the Intersil ICM7224IPL and use a switched gate period. The block diagram here shows the overall arrangement of the instrument.

The count input of the Intersil device has

a Schmitt trigger first stage with a typical hysteresis of 0.5 V, centred on 2.0 V. When operating in the frequency mode, the preamplifier output is fed to the COUNT input while the 8 kHz reference is divided to select gate times of 1 ms, 10 ms, 100 ms or one second, corresponding to ranges of 20 MHz, 2 MHz, 200 kHz and 20 kHz. The actual gate time is eight cycles of the frequency sent to the divider chain.

In period mode, the count input of the ICM7224IPL is switched to a fixed 12.5 kHz reference, while the input signal from the preamplifier goes to the divider chain. Once again, the gate period is eight cycles, so the counter ends up counting at the rate of 12.5 kHz for eight input periods. This produces a 'true' decimal period readout in microseconds or milliseconds.

Next month I'll reveal the circuit and describe the construction. ●



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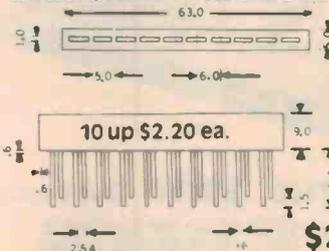
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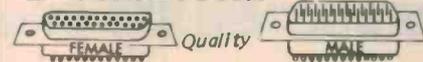
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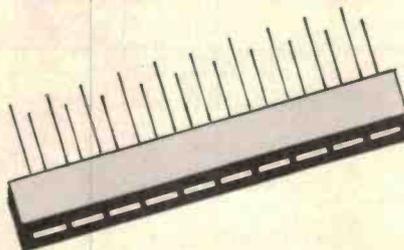
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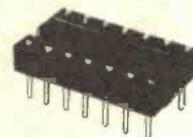
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P0900 DB25 Male 25 Pin	4.50	3.95	3.60
P0901 DB25 Female 25 Pin	4.95	4.50	3.98
P0905 DB25 Backshell	2.85	2.50	2.30

☆ PROTOTYPE SOLDERLESS BREAD BOARDS ☆

MINI STRIP 100 HOLES

P 1000.....**\$1.95**

640 HOLES

P 1005.....**\$8.50**

640 + 100 HOLES

P 1007.....**\$10.00**

640 + 200 HOLES

P 1009.....**\$12.00**

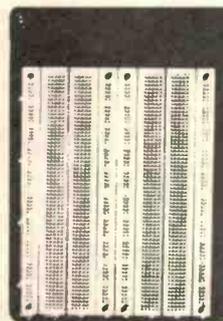
NON-CORROSIVE NICKEL ALLOY CONTACTS RELIABLE FOR 50,000 INSERTIONS

There's a limit to just how many times you can resolder components while prototyping before you either destroy the component or lift a track from the vero.

These solderless breadboards enable circuits to be literally thrown together in an instant, yet all components remain reusable.

A necessity in all research laboratories to save on expensive development costs.

- ☆ Standard 0.1 inch spacings.
- ☆ Accepts all LSI'S, semis, transistors, diodes, leds and passives.
- ☆ 22-30 gauge solid hook up wire for interconnections.
- ☆ Boards are "Keyed" to enable easy expansion.



400 + 1280 HOLES

ACCEPTS UP TO 16 x 16 pin D.I.L. IC'S

SCREW TERMINALS FOR PS CONNECTIONS

P1012.....**\$26**



500 + 1920 HOLES

ACCEPTS UP TO 24 x 16 pin D.I.L. IC'S

METAL BACKING PLATE FOR SHIELDING OF SENSITIVE CIRCUITRY

P1015.....**\$38**

ALTRONICS BANKCARD JETSERVICE DELIVERY NEXT DAY

ALTRONICS BANKCARD JETSERVICE DELIVERY NEXT DAY

ALTRONICS
NEW 20 WATT P A AMPLIFIER
 UNCONDITIONALLY STABLE
 2 YEAR WARRANTY



The AS-20 is a rugged, reliable general purpose public address amplifier. Designed and manufactured in Australia this amp is suitable for use by schools, sporting clubs, function centres and in professional installations (paging systems, background music).

- * Balanced Low Z mic input
- * Unbalanced Low Z mic input
- * Mic muting function (mutes program music with PA announcement)
- * 4-16 OHM output → AUX Treble and Bass controls
- * 100V Balanced line output
- * Full 20 Watts RMS into 8 OHMS
- * Short circuit load protection
- * Less than 1% Distortion.

WHY PAY OVER \$200.00 FOR AN INFERIOR UNIT?

A2000..... **\$149.00**

TOP QUALITY PAGING MIC



STURDY ROBUST BASE

Has tapered low frequency response for articulate speech reproduction. Low impedance balance line. PTT switch with lock facility. Additional switch contacts for remote switching, muting etc. Gooseneck approx. 350mm.

C0166..... **\$59.95**

SUPER SPECIAL SPEAKER TWIN FLEX

2 x 19/.193

W0204 RED TRACE **35c/m**
 W0205 BLACK TRACE **\$34/200m**

PROFESSIONAL HORN SPEAKERS

BOTH MODELS FULLY WEATHER PROOF



NOW IN USE WITH THE WEST AUSTRALIAN EDUCATION DEPT AND PWD
30 WATT WITH LINE TRANSFORMER

Multitap Inbuilt line transformer allows taps 330/30W, 660/15W, 1000/10W, 2000/5W. Universal swivel mounting bracket supplied.

C2033 **\$69.95**
 4 or more..... **\$67.80**

15 WATT WITH LINE TRANSFORMER

Multitap Inbuilt line transformer allows 2 taps 660/15W, 1K/10W, 2K/5W, 4K/2.5W. Mounting bracket clears line T x allowing rear wall mounting.

C2030 **\$59.95**
 4 or more..... **\$56.00**

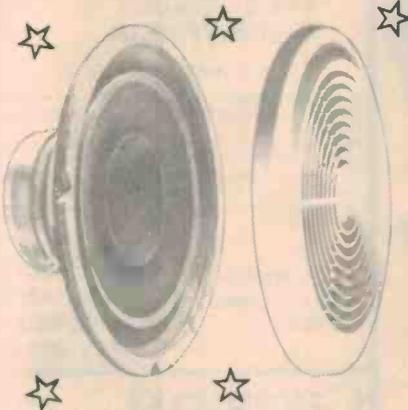
8 INCH WIDE RANGE DUAL CONE SPEAKER

200mm (8 in.) 10 Watts Max. power input. Public Address, Background Music. Ideal Hi Fi extension speaker. Includes transformer holes at 51mm. Over 30,000 sold in Australia! Mounting holes 140 x 140mm.

C2000..... **\$9.50 ea**
 10 Up..... **\$8.70**

8 INCH CEILING SPEAKER GRILL

C0800..... **\$2.75**
 10 Up..... **\$2.00**



20W HIGH POWER SPEAKER TRANSFORMER

Primary Power Taps (100V Line) 1.25/2.5/5/10/15/20W
 Frequency Response: 30 Hz
 Secondary Taps 4/8/16 OHMS.

M1120... **\$10.80**
 10 or more **\$9.90**



4W MULTI-PURPOSE SPEAKER TRANSFORMER

Primary: 2.5K, 5K OHMS
 Secondary: 2, 4, 8, 16 OHMS
 Frequency Response: 30 Hz - 12 KHz. Mounting hole centres 51mm. Ideal for high quality constant voltage PA systems.

M1105..... **\$4.95**
 10 Up each **\$4.50**



GRAIN ORIENTED STEEL CORE

SAVE 25%
 THE SET OF TEN
\$79.50
 B9995 PLUS \$10 P&P

TOP SELLING MOTOROLA BOOKS

IF YOU MISSED OUT LAST TIME, ORDER NOW!
 LATEST EDITIONS JUST ARRIVED

MOTOROLA CMOS DATA B 1105..... \$11.50

A comprehensive reference covering 40K, 45K CMOS families along with specialty devices such as LCD drivers, telephone and general communication functions and industrial control. 862 pages essential in all spheres of electronics.



MOTOROLA MASTER SELECTION GUIDE B 1104..... \$7.95

The most useful book ever printed. Covers MOS IC's listed by function, LINEAR IC's listed by function, INTER-FACE IC's listed by function, LSI memory, TTL, ECL power products, SCR's, diodes, transistors listed by application and ratings, RF, small signal and opto devices listed by application and ratings. Essential data given for all devices. TERRIFIC VALUE



MOTOROLA MICROPROCESSOR DATA B 1120..... \$14.95

Over 1200 pages covering all aspects of Motorola's microprocessor, microcomputer and peripheral components. A clearly written Manual providing all the data necessary to design and build a working computer system from scratch. 100's of circuit examples, flow charts, Truth Tables and programme routines.

MOTOROLA MEMORY DATA B 1113..... \$8.95

An absolute must for the microprocessor Buff. This is the latest reprint of Motorola's famous Memory Data Manual and includes all the latest specifications and design application data on TTL RAM, TTL PROM, MECL MEMORY, MECL RAM, MECL PROM, MOS dynamic RAM, MOS static RAM, MOS EPROM, MOS EE PROM and MOS ROM. Worth many dollars more!



MOTOROLA MECL DATA B 1100..... \$9.95

Emitter Collector Logic (ECL) is today's fastest form of digital logic providing the most direct way of improving system performance. This previously hard to get manual provides data on the 10K, 10K and III families, MECL memory and PLL CHIPS.



MOTOROLA LINEAR IC'S B 1114..... \$9.95

Popular data manual. At last readily available. Approx. 800 pages, full Data Design procedures and equivalent listings for 1000's of devices under headings OP AMPS, VOLTAGE REGULATORS, CONSUMER CIRCUITS (eg TV AUTOMOTIVE, POWER), HIGH FREQUENCY CIRCUITS and SPECIAL-PURPOSE CIRCUITS.

MOTOROLA OPTO DATA B 1118..... \$8.95

Handy reference provides data and application notes on opto couplers, Infra red LEDs, Photo transistors and a complete chapter on Fibre Optics, a communications system which is fast gaining usage worldwide. VERY EDUCATIONAL.

MOTOROLA POWER DATA B 1101..... \$12.95

Motorola are the undisputed world leader in Power Transistors, renowned for their low cost and reliability. Book includes a 9 page selection guide, application notes and Data sheets for over 700 Devices, 989 pages. Previously over \$20.00.

MOTOROLA LINEAR INTERFACE IC'S B 1115..... \$11.50

Complements the Linear IC Manual. Gives data, design procedures and equivalent listings for: MEMORY MICROPROCESSOR SUPPORT, LINE DRIVERS/RECEIVERS, TELEPHONE, COMPARATORS, VOLTAGE REFERENCE AND DATA CONVERSION DEVICES. Includes comprehensive selector guide.



SCHOTTKY TTL DATA B 1109..... \$9.95

Essential reference for the enthusiast and engineer alike. Designing, building and servicing digital circuitry is an absorbing past time. Data for the LS, ALS and FAST families along with design considerations and circuit characteristic are logically presented in this manual, making it quick and easy to use.

ALTRONICS • BANKCARD JETSERVICE DELIVERY NEXT DAY • ALTRONICS

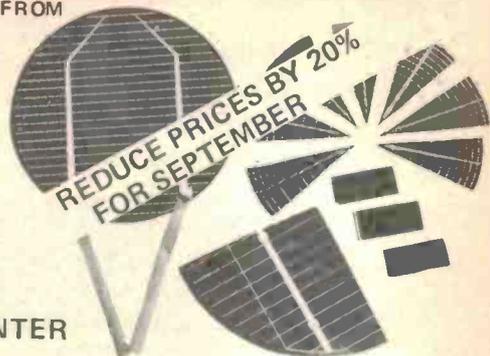
ALTRONICS • BANKCARD JETSERVICE DELIVERY NEXT DAY • ALTRONICS

NEW STORE
opening September
HURSTVILLE

YOU CAN NOW PURCHASE ITEMS FROM
JAYCAR THROUGH
ALL REPAYMENTS
INCLUDE INSURANCE



Customers must satisfy the requirements of
HFC to purchase. All repayments are monthly



Breath Tester

\$24⁹⁵

SAVE \$5
Normally \$29.95

Cat. KA1522

In all states and territories in Australia it is an offence to drive a vehicle with an alcohol/blood concentration above a certain limit. In most states it's 0.05 others 0.08. Either way it's only a relatively small number of drinks, many people (quite wrongly) believe that they remain below the statutory limit.

The KA1522 Breath Tester can help here. A unit with the same circuit diagram was featured in May "Electronics-Australia". It CANNOT give you an actual blood/alcohol content reading, however it can go close. And it can give you a relative reading between inebriated friends!!! Great at parties!!!

Grab the whole kit now for only \$24.95. You never know, it may save your licence or your life!



SILICON SOLAR CELLS IDEAL FOR THE EXPERIMENTER

We now stock a COMPLETE range of high efficiency Silicon Solar Cells. All cells give 0.45V under rated load and they can be stacked in series or in parallel for higher current.

ZM9002	Rect. 10x20mm 45mA	1 - 9	10+
ZM9003	3" diameter 1 amp	\$2.45	\$1.95
ZM9004	3" diameter x 30° segment 78mA	\$26.50	\$22.50
ZM9005	4" diameter x ¼ segment 450mA	\$3.25	\$2.95
		\$12.45	\$11.95

minitune

\$42⁹⁵



FAR CHEAPER THAN DPM SEPARATELY

Following the spectacular success of the DP2010 Digital Multimeter kit, we now have an ENGINE ANALYSER KIT! But the spectacular thing is the price! It is ACTUALLY CHEAPER than the DPM-05 Display and Case!! The Minitune will measure voltage, resistance (down to a very low range), RPM and Dwell Angle.
Cat. KJ-7012

TEST LEADS TO SUIT ONLY \$2.95

\$42.95

Function	F.S.D.	Resolution	Accuracy	Ref:
Voltage (d.c.)	20V	10mV	0.5% - 1 digit	EA
Resistance	200Ω	100mΩ	0.5% - 1 digit	June
	20kΩ	100	0.5% - 1 digit	1983
R.P.M.	20,000r.p.m.	10r.p.m.	1% - 3 digits	
Dwell	90	0.1	2% - 3 digits	

BBD EFFECTS BOX

Fantastic low-cost instrument using the versatile MN3001 Bucket-Brigade Delay Line to achieve brilliant sonic effects. Now you can emulate the commercial rack groups with Phasing, Flanging, Reverb and Echo. The Jaycar kit includes all components INCLUDING IC sockets and the TU.04 box. (Not cut down but this is easily done). Jaycar has a specially built cabinet for this kit with all holes pre-punched etc., at only \$10 extra but only if you buy the original kit from us. Available as a separate item for \$29.50. WHEN THE KIT IS PURCHASED WITH THE DE-LUXE CASE THE TU.04 CASE WILL NOT BE SUPPLIED.



COMPLETE KIT
Cat. KE1522
\$79.00

Special cabinet to suit \$10.00
Cat. HB6445

VIDEO SENSATION AT LAST A Video Enhancer/ Distribution Amplifier designed EXCLUSIVELY for AUSTRALIA

Cat. AV6501

Jaycar has had designed a high quality, high performance Video Enhancer which is specifically for the Australian 625 line 50 frame PAL-D system.

As far as we know it is the ONLY Australian designed, Australian built unit available!!

But, guess what? The Jaycar AV6501 Enhancer is CHEAPER than its inferior imported Asian counterparts!!

This unit is professionally designed and University tested! It works and it works well.

12 Volt AC
Adaptor only
\$12.95

NOT A KIT
BUILT, TESTED
AND GUARANTEED
KIT VERSION
ONLY \$39.50



VALUE
\$49⁵⁰

SPECIFICATIONS

- #1 Maximum enhancement, not less than +8.3dB @ 2MHz
- #2 Enhance disabled (Bypass) response, DC to 5MHz, -0.8-1.0dB, 0.6dB, all settings.
- #3 Colour Subcarrier 0dB notch frequency, tunable to 4.43 MHz, +/- 0.6dB.
- #4 Amplifier group delay, less than 0.075µs
- #5 Signal handling capability not less than 1.38 volts p-p. (Sync. is clipped first).
- #6 Power 12V AC @ 100mA
- #7 Controls, ON/OFF, ENHANCE, ENHANCE/BYPASS SWITCH, CORE/GAMMA CONTROL
- #8 Input connector, RCA socket
- #9 Output connector, RCA socket x 3

DESIGN FEATURES

- #1 A unity gain notch at the colour subcarrier frequency, whose purpose is to prevent chrominance to luminance errors at high enhance levels.
- #2 A closed loop configuration with lead lag compensation to achieve stable, well defined gain.
- #3 DC coupling, eliminating large capacitors in series with the video signal end achieving DC response for applications requiring it.
- #4 Low output impedance prior to termination resistors, enabling up to three outputs to exist and be used or left unterminated.
- #5 A level dependent closed loop response or Gamma control ('Core')
- #6 Clip on negative going signals at -67 volts into 75 ohms to prevent sync errors owing to overshoot.

Cannon XL connectors-great new range * * *

5 PIN AND
RIGHT ANGLE
TYPES

NOW IN
STOCK

PP2120 - 3pin male line	\$3.50	PP2116 - 5pin male chassis	\$5.95
PS4020 - 3pin female line	\$3.95	PS4016 - 5pin female chassis	\$6.95
PP2112 - 3pin male chassis	\$3.25	PS4010 - 240V mains line	\$6.50
PS4012 - 3pin female chassis	\$3.95	PP2110 - 240V mains chassis	\$5.25
PP2117 - 5pin male line	\$6.95	PP2113 - 3pin male r/angle	\$4.95
PS4026 - 5pin female line	\$7.95	PP4030 - 3pin female r/angle	\$5.95

TRANSISTOR ASSISTED IGNITION

Ref: EA Jan '83. Latest version of this popular kit. The Jaycar kit has a genuine die cast box - as used in the EA prototype. Beware of others that use flimsy sheet metal.
Cat. KA1506 \$35



"Fluoro Starter"

Ref: EA Oct 1982
One of our most popular kits. Enables you to replace the electromechanical starter with an electronic one! The Fluoro starts up instantly without a flicker!
All electronic components supplied including high quality mains cap. (Fluoro starter case required)
NORMALLY \$5.00

THIS MONTH \$4
SAVE \$1.00
Cat. KA-1480

Edge Connector No.1
This component has a 0.1" pitch 72 way (2 x 36) configuration. Each contact is heavily gold plated and bifurcated for lower contact resistance. The 0.025 square terminations will PC mount or take one level of wire-wrap. The body is moulded in high quality Diallyl Phthalate with integrally moulded mounting feet on the ends. Outstanding quality for the price.
1 - 9 \$2.95
10+ \$2.45

Edge Connector No.2
This component has a 0.156" pitch 86 way (2 x 43) configuration. Once again each contact is heavily gold plated and bifurcated. The termination is of the solder-lug type. The body is identical in fashion to the HE-8655.
1 - 9 \$3.45
10+ \$2.95

Edge Connector No.3
This component has a 0.1" pitch 72 way (2 x 36) configuration. Each contact is heavily gold plated and bifurcated for lower contact resistance. The 0.025 square terminations will PC mount or take one level of wire-wrap. The body is moulded in high quality Diallyl Phthalate with integrally moulded mounting feet on the ends. Outstanding quality for the price.
1 - 9 \$2.95
10+ \$2.45

Video Amplifier/ Buffer

Ref: EA Aug 1983

The answer to a maddens prayer!
This device can be made to fit inside a TV set (or in a separate box if necessary). It basically enables you to connect straight into the video drive of your TV, turning it into a colour monitor. This means that the video signal from your computer, VCR, TV game etc., does not need to be converted to RF and go through the TV IF strip. You will be amazed by the clearer, sharper signal that has less interference! Notes on how to fit to various TV sets are included.
Cat. KA 1527 \$14.95



Cat. KE4570

\$49⁵⁰

- Fully protected
- Output variable from 0-30V DC
- Selectable current limit
- Both voltage and current metering
- After a multimeter & soldering iron an absolute must for the enthusiast.

Ref: ETI
December
1982

You will never own a more useful piece of gear.

Touch Lamp Timer

Ref: EA Aug 1983

This project is very similar to the EA touch dimmer which has been very popular. Basically, you touch the wallplate and the light stays on for a predetermined amount of time. The same wallplate is used as the dimmer.
As usual the Jaycar kit contains quality components as originally specified, including a quality HPM wallplate.
Cat. KA 1525 \$21.00



0-30V 1amp power supply

ETI 162



Cat. No.	DESCRIPTION OF KIT	Ref.	PRICE	KE4052	100 WATT AMP MODULE	ETI 480	\$ 27.00
KA1300	FUZZ BOX COMPLETE	EA 1/81	\$ 19.50	KE4064	PREAMPLIFIER MODULE	ETI 480	\$ 30.00
KA1320	LE GONG	EA 3/81	\$ 13.95	KE4090	GENERAL PURPOSE PREAMPLIFIER	ETI 445	\$ 7.99
KA1346	PC BIRDIES SHORT FORM	EA 5/81	\$ 14.95	KE4092	AUDIO LIMITER	ETI 446	\$ 12.00
KA1370	PHOTON TORPEDO	EA 9/81	\$ 29.50	KE4094	BALANCED MICROPHONE PREAMPLIFIER	ETI 449	\$ 5.50
KA1400	METRONOME	EA 1/82	\$ 16.95	KE4105	CAR ALARM	ETI 330	\$ 29.50
KA1402	EPROM PROGRAMMER	EA 1/82	\$ 59.00	KE4205	LED LEVEL METER	ETI 458	\$ 59.00
KA1406	CUDLIPP CRICKET SHORT FORM	EA 2/82	\$ 12.50	KE4206	MC MOVING COIL PREAMPLIFIER	ETI 478	\$ 26.50
KA1408	DIGITAL STORAGE CRO ADAPTOR	EA 2/82	\$110.00	KE4207	MM MOVING MAGNET PREAMPLIFIER	ETI 478	\$ 19.50
KA1430	VOCAL CANCELLER	EA 4/82	\$ 19.50	KE4210	MOSFET AMPLIFIER	ETI 477	\$ 69.00
KA1432	VOX RELAY SHORT FORM	EA 4/82	\$ 14.50	KE4220	150 WATT MOSFET AMPLIFIER	ETI 499	\$ 79.50
KA1450	GUITAR BOOSTER	EA 6/82	\$ 14.50	KE4222	150 WATT MOSFET PREAMPLIFIER	ETI 498	\$ 39.50
KA1452	SUBWOOFER MOSFET AMP	EA 7/82	\$ 79.00	KE4225	BRIDGING ADAPTOR	ETI 479	\$ 9.95
KA1454	SUBWOOFER ENCLOSURE	EA 8/82	\$ 79.00	KE4405	±/- 15 VOLT POWER SUPPLY	ETI 581	\$ 17.50
KA1476	STEREO SYNTHESISER SHORT FORM	EA 9/82	\$ 39.50	KE4410	POWER SUPPLY 13.8 VOLT/10 AMP	ETI 160	\$ 79.50
KA1478	STEREO SYNTHESISER COMPLETE	EA 9/82	\$ 49.50	KE4505	SOUNDENVELOPE SHORT FORM	ETI 492	\$ 24.50
KA1482	POWER UP KIT COMPLETE	EA 11/82	\$ 39.50	KE4552	UHF CONVERTOR	ETI 735	\$ 32.50
KA1484	SUPER SIREN SHORT FORM	EA 11/82	\$ 5.00	KE4554	VIDEO MODULATOR	ETI 760	\$ 12.99
KA1490	BOGGLE GOGGLES	EA 12/82	\$ 9.50	KE4560	LOW OHMS METER	ETI 158	\$ 29.50
KA1492	PH METER LCD	EA 12/82	\$ 69.00	KE4570	POWER SUPPLY 0 - 30 VOLTS 1 AMP	ETI 162	\$ 49.50
KA1494	PROBE FOR PH METER WITH BUFFER		\$ 69.00	KE4600	MODEM SHORT FORM	ETI 644	\$169.00
KA1498	AM WIDEBAND TUNER	EA 12/82	\$249.00	KE4602	MODEM COMPLETE	ETI 644	\$189.00
KA1500	LED HEAD SHORT FORM	EA 1/83	\$ 9.95	KJ6502	SYNTOM DRUM SYNTHESISER KIT		\$ 36.50
KA1510	STEREO SYNTHESISER SHORT FORM	EA 4/83	\$ 11.95	KJ6508	CHORUS GENERATOR KIT		\$ 69.95
KA1516	ALIGNMENT KIT AM TUNER	EA 3/83	\$ 7.95	KJ6510	SHORT FORM IONISER KIT		\$ 14.50
KE4050	50 WATT AMP MODULE	ETI 480	\$ 23.00	KJ6511	FULL IONISER KIT		\$ 29.50

CD-424 14 BIT P.C.M. HIGH RESOLUTION DIGITAL DELAY

- * Pro quality with high signal to noise ratio and wider frequency response * Long delay time from 0 to 1,024mm/s * 8 step sub-delay preset from 5/- 764mm/s
- * superb combination effect with main and sub-delay * 2 inputs and 3 output levels * Low/High equalizer for sound variation

magnificent!

NOT a kit

\$795
Cat. AZ-5020

CX-230 ELECTRONIC CROSSOVER



\$257

Cat. AZ-5030

- * 2-way electronic crossover in stereo * 3-way electronic crossover in mono * 8 steps dividing points from 250Hz to 6KHz * Rack mountable compact dimensions (19") * Convenient 2-way input jacks of balanced (50K ohms) and unbalanced (25K ohms)

Piezo Horns

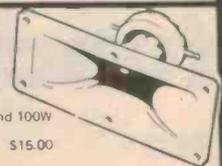
PH 1005A
3 1/2" Square Super Horn for PA's, Disco's etc. Very efficient. Around 50Wrms equivalent capacity.
Cat. AS-3100

\$9.95



Amazing Value

\$15



Jaycar has broken the price barrier for Piezo Horn Speakers!!
We now DIRECT IMPORT a range of piezo horns at prices that will stagger you. Similar units are used everywhere in P.A., Disco and Hi Fi applications. Only Jaycar, however, can bring you these products at low Jaycar prices!!
We now stock the most popular piezo models at new low prices.

PH 1025A
This design is one of the most popular for high power PA/Disco's around 100Wrms equivalent power handling capacity! (6 x 2" rectangular)
Cat. AS-3106

\$15.00

Quality Speakers

PH 1038A
Hi Fi version of the PH 1005A. Slightly less sensitive but a smoother response.
Cat. AS-3102

\$9.95

\$9.95

FUEL SENSOR

almost 2/3 off!

GENUINE
'MORAY'
FUEL
SENSOR



This is the 'genuine' unit as used in the EA Car Computer (Ref: EA August 1982). It is accurate to within 2% and will measure the flow of many other liquids besides petrol. It will give a TTL compatible pulse for flows from 1-100 litres/hour. In September only we are letting these go for - \$19.95! Under HALF our normal price.

Be early as this is a genuine limited offer.
Cat. XC 2020 NORMALLY \$59.50 SEPTEMBER ONLY \$19.95
SAVE ALMOST \$40!!

Free data sheet and connection diagram with each unit.
THAT IS BELOW OUR COST!

FULL ROAD QUALITY 1/3 OCTAVE EQUALISER



\$225
ONLY

SPECIFICATIONS

Signal-to-Noise: -102dB with respect to 1 Volt
Frequency Response: 12Hz - 105kHz to -1dB
Boost/Cut: 14dB (28dB total)
Distortion: 100Hz - 0.007%
1kHz - 0.007%
10kHz - 0.008%
(essentially irrespective of cut or boost)
Current Consumption (DC): Approx 100mA @ 15V
(Requires 30V AC CT)
Output short-circuit proof

Jaycar is renowned for their famous 2801 1/3 Octave Equaliser. Over 1000 of these units are giving reliable service in all parts of Australia and overseas. People recognise the value of this unit when they can get one for less than 1/2 the price of the cheapest ready built - with no deterioration in performance!! We are proud to announce a COMPLETELY BRAND NEW DESIGN based on the 5000 1/3 Octave unit. The specs on the totally new 2801 Mk 111 are UNKNOW in a 1/3 Octave graphic under \$1000!!!

The 2801 Mk 111 comes with complete fused power supply for 240V AC operation. It is also fitted with standard Cannon Male/Female chassis connectors for ease of professional use. It is output short circuit proof and will drive very long unbalanced lines without degradation. Naturally it comes in a rugged 19" road quality rack cabinet. The 2801 Mk 111 looks almost the same as the 1/3 Octave 5000 except that it has brand new front panel livery. You can have a 2801 Mk 111 for only \$225 in kit form.
Cat. KJ-6531

\$225.00

JAYCAR



A laboratory standard function and pulse generator

Part 4

David Tilbrook

This instalment covers the preparation of the chassis and installation of the power supply and output amplifier modules. Do the chassis preparation carefully and you'll be assured of a 'professional' result, with no hassles during assembly. The front panel is particularly critical in this regard, the rear panel and chassis bottom, less so. A fully-dimensioned drawing for all the front panel holes has been prepared and is reproduced elsewhere in this article.

The case I have used is made by the Victorian firm, K&W. It is case No. C1066, the same as used in the ETI-163 Lab-standard Power Supply. In fact, I have designed that

power supply and this generator to have a compatible appearance. The chassis of this case is of aluminium, while the lid is steel, having a number of ventilation slots and painted hammertone blue.

The place to start is the rear panel of the chassis. As layout here is generally non-critical, no dimensional drawing has been done. The power supply and the mains transformer are mounted on the rear panel and the mains cable enters at the lower right, when viewed from the front. A drawing of the general layout and wiring diagram of the power supply module and mains shows the details. Mark out the panel with a soft lead

pencil, using the components as templates, where applicable. The power supply pc board artwork (reproduced in the last part) can be used as a template to mark the position of this module's mounting holes.

When you've marked all the hole centres, centre punch them before attempting to drill the panel. Drill a pilot hole first where large diameter holes have to be drilled (e.g. for the fuse and cable clamp). When the holes have been drilled, check that everything will fit without fouling anything or being cramped. Remove all burrs from the hole rims. Don't assemble anything yet.

Video Amplifier/ Buffer

Ref: EA Aug 1983

The answer to a maiden prayer! This device can be made to fit inside a TV set for in a separate box if necessary. It basically enables you to connect straight into the video drive of your TV, turning it into a colour monitor. This means that the video signal from your computer, VCR, TV game etc. does not need to be converted to RF and go through the TV IF strip. You will be amazed by the clearer, sharper signal that has less interference! Notes on how to fit to various TV sets are included. Cat. KA 1527 \$14.95



Cat. KE4570

- Fully protected
- Output variable from 0-30V DC
- Selectable current limit
- Both voltage and current metering
- After a multimeter & soldering iron an absolute must for the enthusiast.

You will never own a more useful piece of gear.

\$49⁵⁰

Ref: ETI
December
1982

Touch Lamp Timer

Ref: EA Aug 1983

This project is very similar to the EA touch dimmer which has been very popular. Basically, you touch the wallplate and the light stays on for a predetermined amount of time. The same wallplate is used as the dimmer. As usual the Jaycar kit contains quality components as originally specified, including a quality HPF wallplate. Cat. KA 1525 \$21.00



0-30V 1amp power supply

ETI 162



Cat. No.	DESCRIPTION OF KIT	Ref.	PRICE	100 WATT AMP MODULE	ETI 480	\$ 27.00
KA1300	FUZZ BOX COMPLETE	EA 1/81	\$ 19.50	PREAMPLIFIER MODULE	ETI 480	\$ 30.00
KA1320	LE GONG	EA 3/81	\$ 13.95	GENERAL PURPOSE PREAMPLIFIER	ETI 445	\$ 7.99
KA1346	PC BIRDIES SHORT FORM	EA 5/81	\$ 14.85	AUDIO LIMITER	ETI 446	\$ 12.00
KA1370	PHOTON TORPEDO	EA 9/81	\$ 29.50	BALANCED MICROPHONE PREAMPLIFIER	ETI 449	\$ 5.50
KA1400	METRONOME	EA 1/82	\$ 16.95	CAR ALARM	ETI 330	\$ 29.50
KA1402	EPROM PROGRAMMER	EA 1/82	\$ 59.00	LED LEVEL METER	ETI 458	\$ 59.00
KA1406	QUILIFF CRICKET SHORT FORM	EA 2/82	\$ 12.50	MC MOVING COIL PREAMPLIFIER	ETI 478	\$ 26.50
KA1408	DIGITAL STORAGE CRO ADAPTOR	EA 2/82	\$110.00	MM MOVING MAGNET PREAMPLIFIER	ETI 478	\$ 19.50
KA1430	VOCAL CANCELLER	EA 4/82	\$ 19.50	MOSFET AMPLIFIER	ETI 477	\$ 59.00
KA1432	VOX RELAY SHORT FORM	EA 4/82	\$ 14.50	150 WATT MOSFET AMPLIFIER	ETI 499	\$ 79.50
KA1450	GUITAR BOOSTER	EA 6/82	\$ 14.50	150 WATT MOSFET PREAMPLIFIER	ETI 498	\$ 39.50
KA1452	SUBWOOFER MOSFET AMP	EA 7/82	\$ 79.00	BRIDGING ADAPTOR	ETI 479	\$ 9.95
KA1454	SUBWOOFER ENCLOSURE	EA 8/82	\$ 79.00	+/- 15 VOLT POWER SUPPLY	ETI 581	\$ 17.50
KA1476	STEREO SYNTHESIZER SHORT FORM	EA 9/82	\$ 39.50	POWER SUPPLY 13.8 VOLT/10 AMP	ETI 160	\$ 79.50
KA1478	STEREO SYNTHESIZER COMPLETE	EA 9/82	\$ 49.50	SOUNDBENDER SHORT FORM	ETI 492	\$ 24.50
KA1482	POWER UP KIT COMPLETE	EA 11/82	\$ 39.50	UHF CONVERTOR	ETI 735	\$ 32.50
KA1484	SUPER SHREK SHORT FORM	EA 11/82	\$ 5.00	VIDEO MODULATOR	ETI 760	\$ 12.99
KA1490	BOGGLE GOGGLES	EA 12/82	\$ 9.50	LOW OHMS METER	ETI 158	\$ 29.50
KA1492	PH METER LCD	EA 12/82	\$ 69.00	POWER SUPPLY 0 - 30 VOLTS 1 AMP	ETI 162	\$ 49.50
KA1494	PROBE FOR PH METER WITH BUFFER		\$ 69.00	MODEM SHORT FORM	ETI 644	\$169.00
KA1498	AM WIDEBAND TUNER	EA 12/82	\$249.00	MODEM COMPLETE	ETI 644	\$189.00
KA1500	LED HEAD SHORT FORM	EA 1/83	\$ 9.95	SYNTOM DRUM SYNTHESIZER KIT		\$ 36.50
KA1510	STEREO SYNTHESIZER SHORT FORM	EA 4/83	\$ 11.95	CHORUS GENERATOR KIT		\$ 69.95
KA1516	ALIGNMENT KIT AM TUNER	EA 3/83	\$ 7.95	SHORT FORM IONISER KIT		\$ 14.50
KE4050	50 WATT AMP MODULE	ETI 480	\$ 23.00	FULL IONISER KIT		\$ 29.50
				KE4052		
				KE4064		
				KE4090		
				KE4092		
				KE4094		
				KE4105		
				KE4205		
				KE4206		
				KE4207		
				KE4210		
				KE4220		
				KE4222		
				KE4225		
				KE4405		
				KE4410		
				KE4505		
				KE4552		
				KE4554		
				KE4560		
				KE4570		
				KE4600		
				KE4602		
				KJ6502		
				KJ6508		
				KJ6510		
				KJ6511		

CD-424 14 BIT P.C.M. HIGH RESOLUTION DIGITAL DELAY

- * Pro quality with high signal to noise ratio and wider frequency response * Long delay time from 0 to 1,024mm/s * 8 step sub-delay preset from 5/- 764mm/s
- * superb combination effect with main and sub-delay * 2 inputs and 3 output levels * Low/High equalizer for sound variation

magnificent!

NOT a kit
\$795
Cat. AZ-5020



CX-230 ELECTRONIC CROSSOVER

- * 2-way electronic crossover in stereo * 3-way electronic crossover in mono * 8 steps dividing points from 250Hz to 6KHz * Rack mountable compact dimensions (19") * Convenient 2-way input jacks of balanced (50K ohms) and unbalanced (25K ohms)



\$257
Cat. AZ-5030

Piezo Horns

PH 1005A
3 1/2" Square Super Horn for PA's, Disco's etc. Very efficient. Around 50Wrms equivalent capacity.
Cat. AS-3100

\$9.95



Amazing Value \$9.95

\$15



Jaycar has broken the price barrier for Piezo Horn Speakers!! We now DIRECT IMPORT a range of piezo horns at prices that will stagger you. Similar units are used everywhere in P.A., Disco and Hi Fi applications. Only Jaycar, however, can bring you these products at low Jaycar prices!! We now stock the most popular piezo models at new low prices.

PH 1038A
Hi Fi version of the PH 1005A. Slightly less sensitive but a smoother response.
Cat. AS-3102

PH 1025A

This design is one of the most popular for high power PA/Disco's around 100Wrms equivalent power handling capacity (16 x 2" rectangular)
Cat. AS-3106 \$15.00

Quality Speakers



\$9.95

FUEL SENSOR

almost 2/3 off!

GENUINE
'MORAY'
FUEL
SENSOR



This is the genuine unit as used in the EA Car Computer (Ref: EA August 1982). It is accurate to within 2% and will measure the flow of many other liquids besides petrol. It will give a TTL compatible pulse for flow from 1-100 litres/hour. In September only we are letting these go for - \$19.95! Under HALF our normal price.

Be early as this is a genuine limited offer.
Cat. XC-2020 NORMALLY \$59.50 SEPTEMBER ONLY \$19.95
SAVE ALMOST \$40!!

Free data sheet and connection diagram with each unit.
THAT IS BELOW OUR COST!

FULL ROAD QUALITY 1/3 OCTAVE EQUALISER



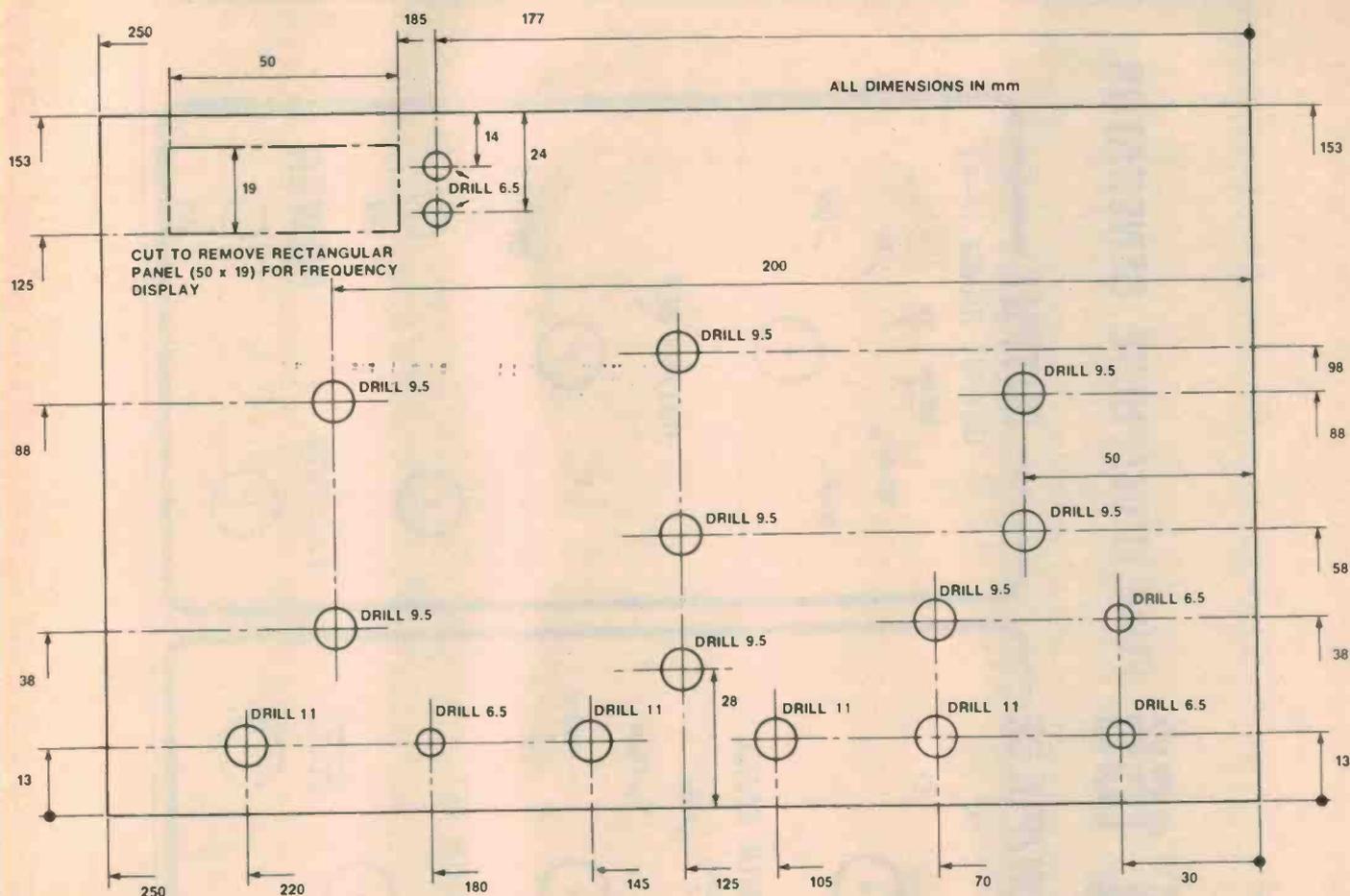
\$225
ONLY

SPECIFICATIONS

- Signal-to-Noise: -102dB with respect to 1 Volt
- Frequency Response: 12Hz - 105kHz to -1dB
- Boost/Cut: 14dB (28dB total)
- Distortion: 100Hz - 0.007%
1kHz - 0.007%
10kHz - 0.008%
- (essentially Irrespective of cut or boost)
- Current Consumption (DC): Approx 100mA @ 15V (Requires 30V AC CT)
- Output short-circuit proof

Jaycar is renowned for their famous 2801 1/3 Octave Equaliser. Over 1000 of these units are giving reliable service in all parts of Australia and overseas. People recognise the value of this unit when they can get one for less than 1/2 the price of the cheapest ready built - with no deterioration in performance!! We are proud to announce a COMPLETELY BRAND NEW DESIGN based on the 5000 1/3 Octave unit. The specs on the totally new 2801 Mk 111 are UNKNOWN in a 1/3 Octave graphic under \$1000!!!
The 2801 Mk 111 comes with complete fused power supply for 240V AC operation. It is also fitted with standard Cannon Male/Female chassis connectors for ease of professional use. It is output short circuit proof and will drive very long unbalanced lines without degradation. Naturally it comes in a rugged 19" road quality rack cabinet. The 2801 Mk 111 looks almost the same as the 1/3 Octave 5000 except that it has brand new front panel livery. You can have a 2801 Mk 111 for only \$225 in kit form.
Cat. KJ-6531 \$225.00

JAYCAR



Now mark out the bottom of the case to take the mounting holes for the output amplifier module and the main generator pc board. The main artwork for the ETI-1520 module (reproduced in the article on the '1520) can be used to mark its mounting hole positions. The template drawing for the main generator pc board, reproduced here, can be used to mark out its mounting hole positions. Again, use a soft pencil to mark the hole positions and centre punch them before drilling. Check it after drilling and de-burr the holes.

Now for the front panel. I have to stress that this should be done with the *utmost care*. Follow the accompanying drawing carefully and you should have no difficulty. There is an option, though, that I should point out, with regard to the mounting of the 4-digit LED frequency display. This board, ETI-166c, is mounted with four long screws. The panel could be drilled and countersunk screws employed, but I found that, owing to the thinness of the chassis material, this was not going to be very satisfactory as the screw heads would not sit flush with the panel and thus would show beneath the Scotchcal front panel. Instead, I mounted the screws to the board so that the displays were held a millimetre or so back from the panel cutout and actually *glued* the screw heads to the front panel after carefully siting the display board. The choice I leave to you.

Mark out all the holes very carefully, measuring only from the bottom edge and the bottom right-hand corner, to ensure consistent accuracy. Centre punch all the holes before drilling. Drill a pilot hole first for all the holes, then the correct size drill. De-burr all the holes when you're finished. The LED display slot can be cut out in a number of ways. One way is to drill a series of holes around the inside edge of the hole, a millimetre or so from the marked edges. Break out the centre piece when you've completed the series and then file the edges smooth and straight. Alternatively, drill one large hole for a 'hole nibbler' and cut around the edge with that tool. Some filing will be necessary in this case too.

When you're satisfied the panel's finished, you can install the Scotchcal label. I used a plastic one - blue on a white background to match my ETI-163 Lab Supply - but an aluminium one can be used too. If you're using a plastic Scotchcal, paint the panel white first, as the Scotchcal is translucent. Let the paint dry thoroughly before proceeding.

Whether you've made your own or purchased one, the Scotchcal panel should be installed carefully. Start by cutting it carefully to size, then remove a 10 mm strip off the backing from the left-hand edge. Carefully line up the edge of the Scotchcal and the edge of the panel, ensuring that it will lay

FUNCTION/PULSE GENERATOR



This bit. The assembly of this section and the power supply is covered in this instalment.

eti 166 FUNCTION/PULSE GENERATOR

Hz kHz

FREQUENCY

FREQUENCY SET

FREQUENCY RANGE

x10 x100 x1k x10k x100k

x1

EXT SWEEP MANUAL SWEEP

FUNCTION/PULSE

PULSE WIDTH RANGE

x100us x1ms x10ms x100ms

x10us x1us x100ns

PULSE WIDTH SET

PULSE PULSE

OUTPUT

OUTPUT RANGE (P-P)

300mV 1V 3V 10V

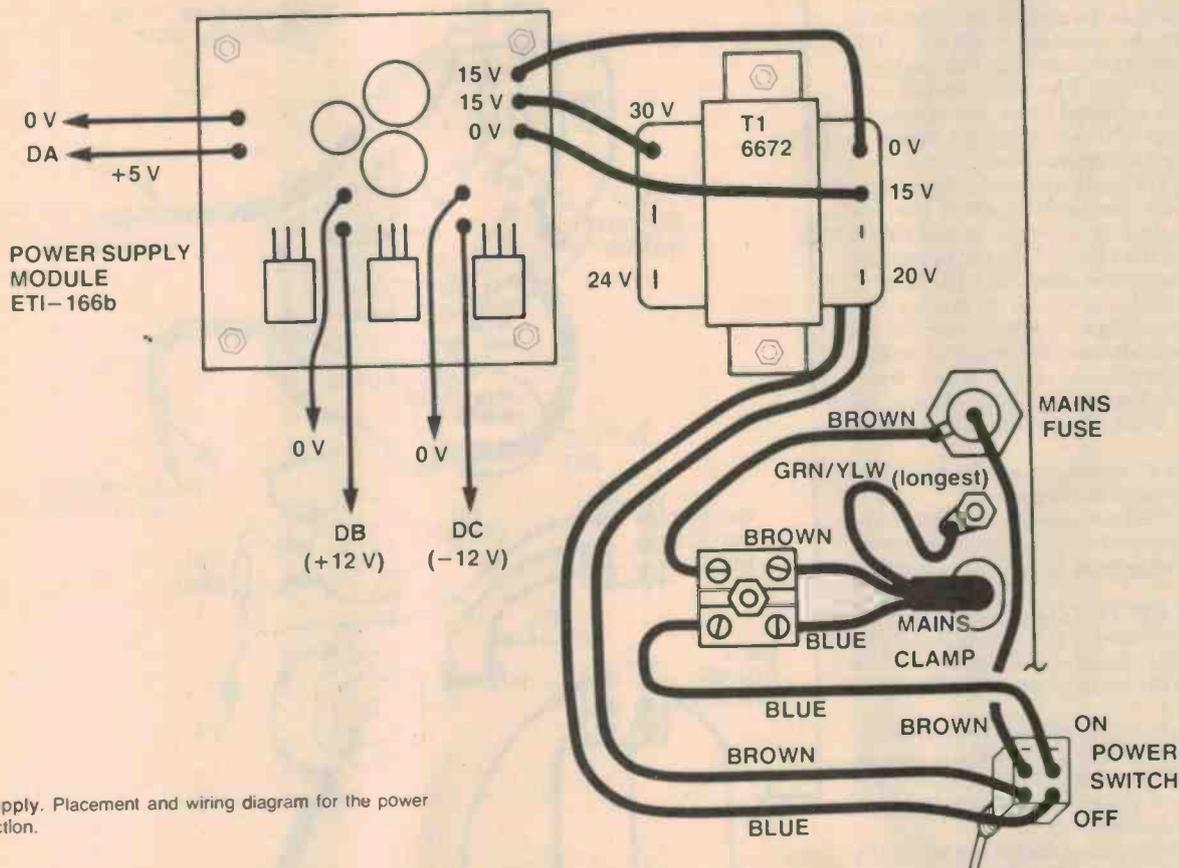
100mV 30mV

OUTPUT SET

DC OFFSET OFFSET OFF ON

FUNCTION POWER ON

TOP, REAR PANEL OF CASE



Power supply. Placement and wiring diagram for the power supply section.



Start with the BNC socket. This has to be installed from the front panel. What I did was to take a 6 mm i.d. rubber grommet and force (roll) it onto the socket's thread after removing the nut, washer and earth lug. This then slips neatly in the 11 mm mounting hole marked FUNCTION. Secure it by putting the washer on first, then the earth lug, followed by the nut. Check that it isn't shorted to the chassis. Then mount the power

switch (DPDT), followed by the two pots and the rotary switch. Take care not to scratch the Scotchcal.

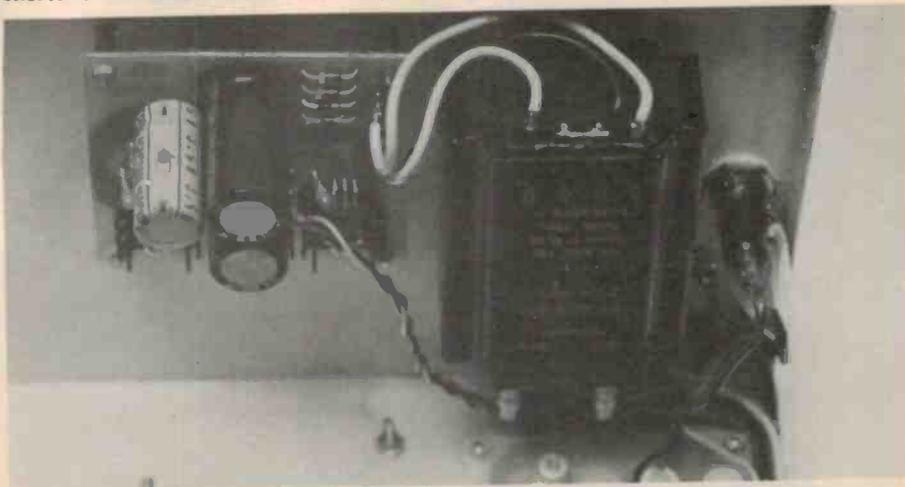
Now tackle the rear panel. Mount the terminal block and earth lug, then the mains cable. Strip the end of the mains cable so that the active (brown) and neutral (blue) leads are about 40 mm long and the earth lead (green with yellow stripe) is about 60-70 mm long. Terminate the leads as per the wiring

straight, and rub down firmly along the edge. Then, carefully peeling off the backing and rolling it under, rub the Scotchcal down, moving across the panel. This way, you should get no, or very few, bubbles under it. Any you may get can be rubbed away towards one edge as they occur.

Using a sharp knife point or modeller's scalpel, cut the Scotchcal away from all the holes, being careful not to make any slips or you'll spoil your panel. Tsk, tsk.

Now you can mount the controls in the OUTPUT section of the front panel. There are two toggle switches, two pots and a rotary switch. Here's what you'll need:

- 1 x BNC socket, panel-mount, with earth lug.
- 1 x two-pole, 6-position rotary switch.
- 1 x 1k/A (lin.) pot.
- 1 x 10k/A (lin.) pot.
- 1 x SPDT miniature toggle switch.
- 1 x DPDT 240 Vac/1.5 A min. toggle switch.



Rear panel assembly. View of the rear panel showing placement of the various pieces of the power supply. I used a different transformer from the 6672 specified as I had one on hand but no 6672. Note the rear edge of the ETI-1520 output amplifier module.

Project 166

diagram. The neutral lead (blue) from the terminal block to the mains switch should be attached to the terminal block next. This should be about 300 mm long, but don't wire it to the switch yet. The active lead (brown) between the terminal block and the mains fuse is about 200 mm long and should be attached to the terminal block next, but not to the fuse. The lead between the fuse and the mains switch can be attached to the fuse now, first slipping a length of heatshrink tubing over the two leads to the fuseholder. After the leads are soldered to the fuseholder, apply a blast of hot air to the sleeve so that the fuseholder terminals are not exposed. Now solder two 400 mm long leads to the mains terminals of the power transformer, one brown, one blue. Sleeve the terminals. Then mount the power transformer.

Note that all mains wiring should be done with mains-rated hookup wire.

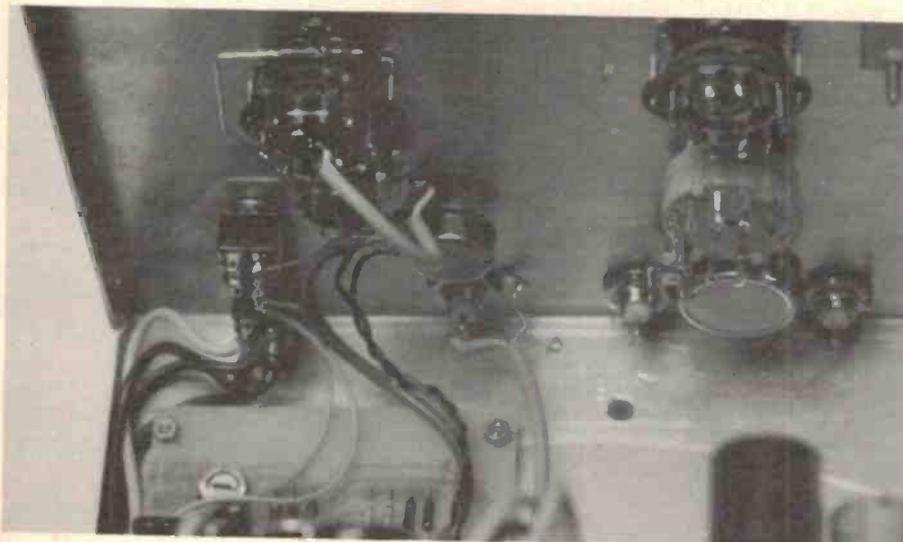
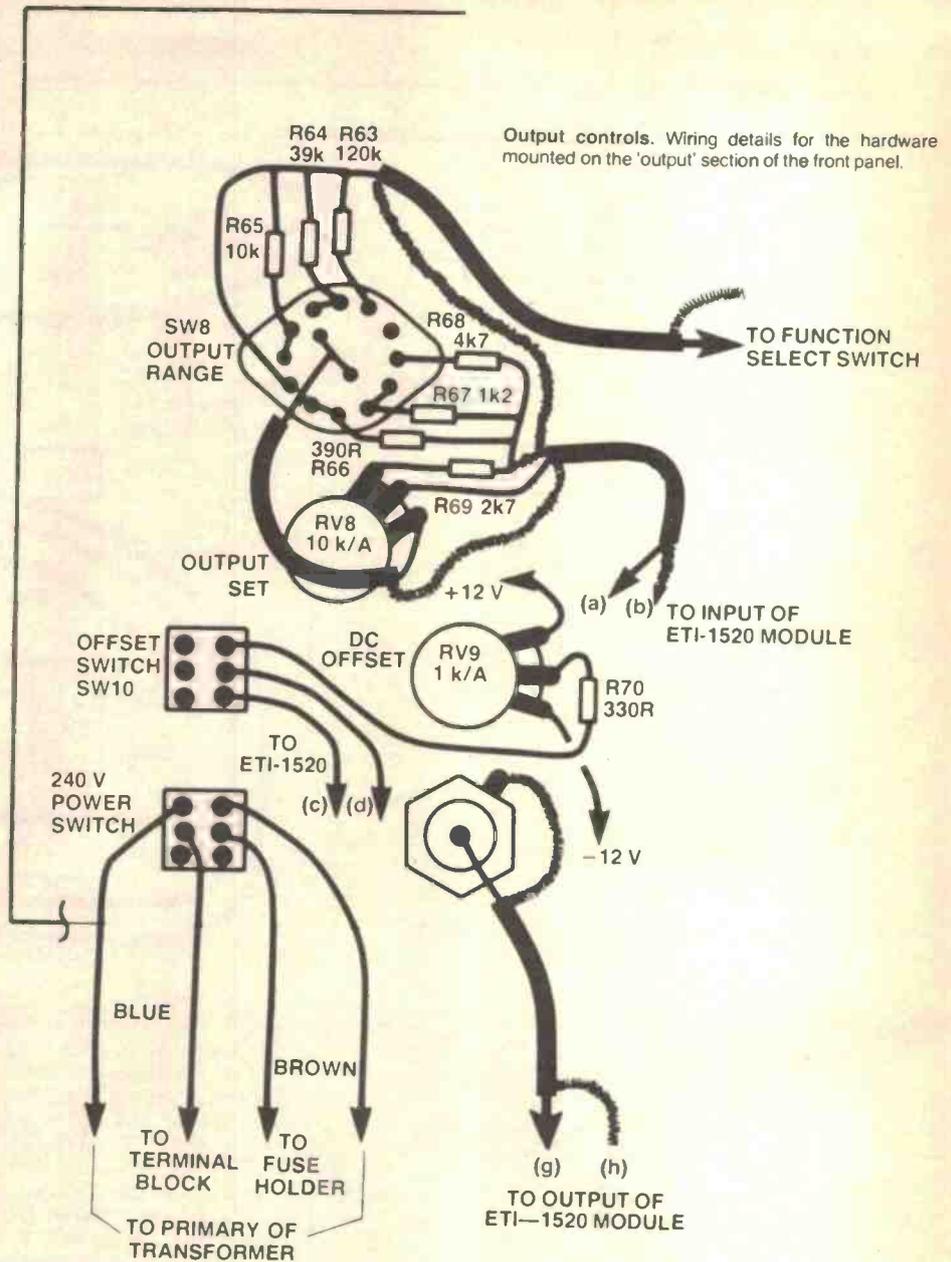
The ETI-166d power supply module can be mounted next and wired to the transformer. Use heavy duty hookup cable, at least 24 x 0.2 mm.

Now the ETI-1520 output amplifier module can be mounted in place. Note that the pc stakes or short lengths of tinned copper wire are used on the board for attaching the external wiring.

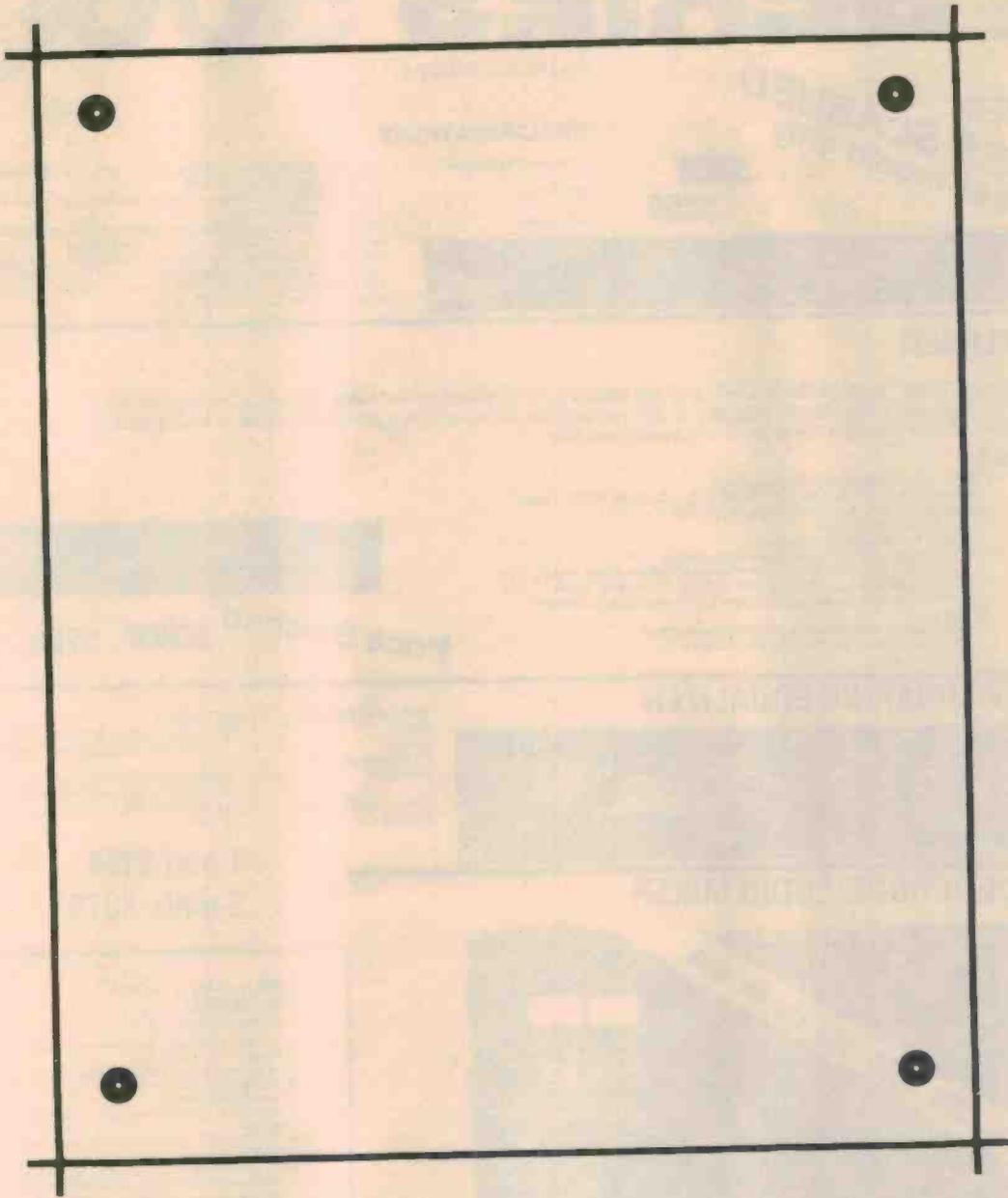
The power switch can now be wired up. Note that the neutral side wiring is nearest the edge of the chassis, for safety's sake. Don't forget to sleeve, or otherwise cover, all exposed mains connections.

With that completed, tackle the rest of the output stage wiring. The details are clear from the accompanying wiring diagram. The components you need are shown there. Don't worry about the numbering at the moment, all that will come together with the next instalment. The resistors are all 1/4 W, 5% types. Note the use of shielded cable on the ETI-1520 input and output lines.

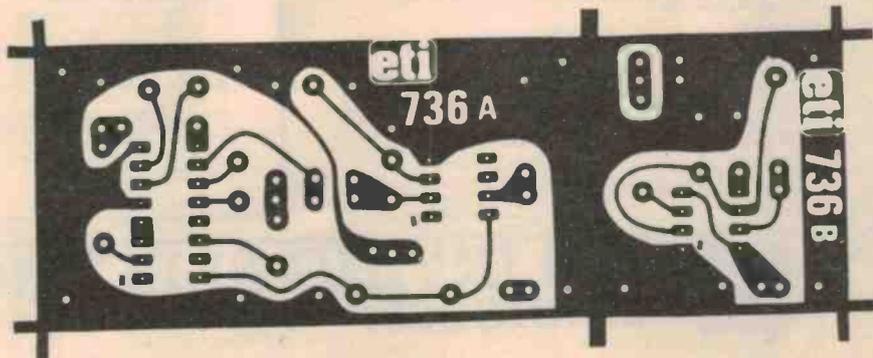
That's as far as you can go for the moment — but that lot should keep you occupied for some time.



Behind the front. General view of the hardware mounted behind the front panel.



Template. This is a full-size template to enable you to locate the drilling positions for the main generator board mounting holes.



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SERIES 5000

PRICES SLASHED

As designed by ETI

PREAMPLIFIER

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~~\$269~~
\$259

SPECIFICATIONS

Frequency response: High-level input: 15Hz-130 kHz, +0, -1 dB Low-level input — conforms to RIAA equalisation, ±0.2 dB
1kHz <0.003% on all inputs (limit of resolution on measuring equipment due to noise limitation).
Distortion: High-level input, master full, with respect to 300 mV input signal at full output (1.2V): >92 dB flat >100 dB A-weighted.
S/N noise: MM input, master full, with respect to full output (1.2V) at 5 mV input, 50 ohm source resistance connected: >86 dB flat >92 dB A-weighted.
MC input, master full, with respect to full output (1.2V) and 200 μV input signal: >71 dB flat >75 dB A-weighted.



POWER AMPLIFIER

Please note that the "Superb Quality" Heatsink for the power amp was designed and developed by Rod Irving Electronics and is being supplied to other kit suppliers. This product cost \$1,200 to develop so that your amplifier kit would have a professional finish as well as sound. We also have a new range of rack mounting boxes which will be released soon.

SPECIFICATIONS

Power output: 100W RMS into 8 ohms (±55 V supply).
Frequency response: 8 Hz to 20 kHz, +0—0.4 dB 2.8-Hz to 65 kHz, +0—3 dB. NOTE: These figures are determined solely by passive filters.
Input sensitivity: 1V RMS for 100W output.
Hum: —100dB below full output (flat).
Noise: —116 dB below full output (flat, 20 kHz bandwidth).
2nd harmonic distortion: <0.001% at 1 kHz (0.0007% on prototypes) at 100 W output using a ±56 V supply rated at 4 A continuous. <0.003% at 10 kHz and 100 W.
3rd harmonic distortion: <0.0003% for all frequencies less than 10 kHz and all powers below clipping.
Total harmonic distortion: Determined by 2nd harmonic distortion (see above).
Intermodulation distortion: <0.003% at 100 W. (50 Hz and 7 kHz mixed 4:1).
Stability: Unconditional



Price Slashed ~~\$299~~ **\$289**

THIRD OCTAVE GRAPHIC EQUALIZER



SPECIFICATIONS E.T.I. Dec. 1982
Bands: 28 Bands from 31.5 Hz to 16 kHz
Noise: <0.003 mV, sliders at 0, gain at 0 (—102 dB).
20 kHz bandwidth
Distortion: 0.007% at 300 mV signal, sliders at 0, gain at 0; max. 0.01% sliders at minimum.
Frequency Response: 12 Hz-105 kHz, +0, —1 dB, all controls flat.
Boost & Cut: 14 dB

MX-1200 MICROPHONE/AUDIO MIXER



MX 1200 \$599 this month only.

This unit features: 12 microphone line inputs with pan, bass, treble, effect and fold back controls for each channel • LED peak indicators for each channel • 2 turntable inputs with cross-fade and individual output controls • master equaliser for bass, midrange and treble • variable headphone output etc. etc. • complete with carrying case.

~~\$699~~

SPECIFICATIONS:
INPUTS: 12 channel fader, Slide, 60mm, LOG 25%
Level/Impedance Mic. -46 db/1K
Line 22 db/16K ± 12
Phono 32 db/50K STEREO ± 21 (2mV) at 1KHz
Effect Return (Aux) 20 db/50K ± 1
OUTPUTS: 2 Master 300, LOG 15%
Level/Impedance L & R 0 db/2K
Effect Send 0 db/2K F/B Out 0 db/2K
Head phone Stereo, ±10 db/500 (100, 1K)
EQUALISATION: 1 Head Phone, 300, LOG 15%
Change Bass ± 15db
Treble ± 15db
Master Bass ± 12db
Treble ± 10db
Mode ± 12db

FADER & CONTROLLERS
12 F/B Volume, 300, LIN
1 F/B Master level, 300, LIN
12 Effect Send, 300, LOG 15%
1 Effect Return, 300, LOG 15%
2 Phono, 300, LOG 15%
1 Head Phone, 300, LOG 15%
SN, 58DB
FREQUENCY RESPONSE: 20-20 KHz
TOTAL HARMONIC DISTORTION: Less than 0.1%
METER, 2 illuminated VU Meters 0db = 0.775V
PEAK INDICATOR, 12 LED Peak Indicators
VOLTAGE, 240 V/AL, 50Hz
POWER CONSUMPTION: 7.2 watts
DIMENSIONS: 820 (W) × 386 (D) × 108 (H) mm (supplied complete with carrying case)

EXTRA FEATURES OF OUR KITS POWER AMPLIFIER

- KIT PRICE \$299 P&P \$8.00
- 1% Metal Film Resistors are used where possible
 - Prewound Coils are supplied
 - Aluminum case as per the original article
 - All components are top quality
 - Over 2000 Kits now sold
 - We have built this unit and so know what needs to go into every kit
 - SUPER FINISH Front panel supplied with every kit at no extra cost to you
 - We are so confident of this kit that we can now offer it assembled and tested so that people who do not have the time can appreciate the sound that this amplifier puts out. This is done on a per order basis delivery approx. two weeks after placement.

only \$425
*All parts available separately for both kits.

PREAMPLIFIER

- KIT PRICE \$259 P&P \$8.00
- 1% Metal Film Resistors are supplied
 - 14 metres of Low Capacitance Shielded are supplied (a bit extra in case of mistakes)
 - English "Larkin" Switches are supplied no substitutes as others supply
 - We have built and tested this unit and so know what needs to go into every kit
 - Specially imported black anodised aluminium knobs
 - Again as with the power amp we are offering this kit A & T at a price which we do not believe there is a commercial unit available that sounds as good. Same delivery as the PA
- only \$425

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Video distribution amplifier

This simple, low-cost project will allow you to drive, say, five video monitors from one source, such as a video cassette recorder or a computer.

John Power

PIPING VIDEO around has become quite common place: from a computer to a video display unit, from a video cassette recorder to a video monitor, etc. Occasions arise, however, when you need to 'drive' more than one display or whatever, from a single source. For example; when playing a videotaped lecture at a club meeting, it's more convenient for the audience to have several monitors placed at appropriate positions rather than everyone trying to strain to watch one small screen. Or, when doing a computer/computing demonstration, it's much handier to have several monitors hooked up rather than have the audience crowd around the one. Anyway, I expect many readers will have their own applications already in mind for this project.

Design

The requirements of a video distribution amplifier are quite straightforward. The unit must be able to take a single input and to drive the required number of outputs while retaining video fidelity. The bandwidth at full output level must be at least 5 MHz or more so as to retain video fidelity. The input and output impedances must be matched to standard 75 ohms widely used in video work and adding or subtracting units to or from the outputs should not affect any other device connected to an output. In essence, that's what this project does.

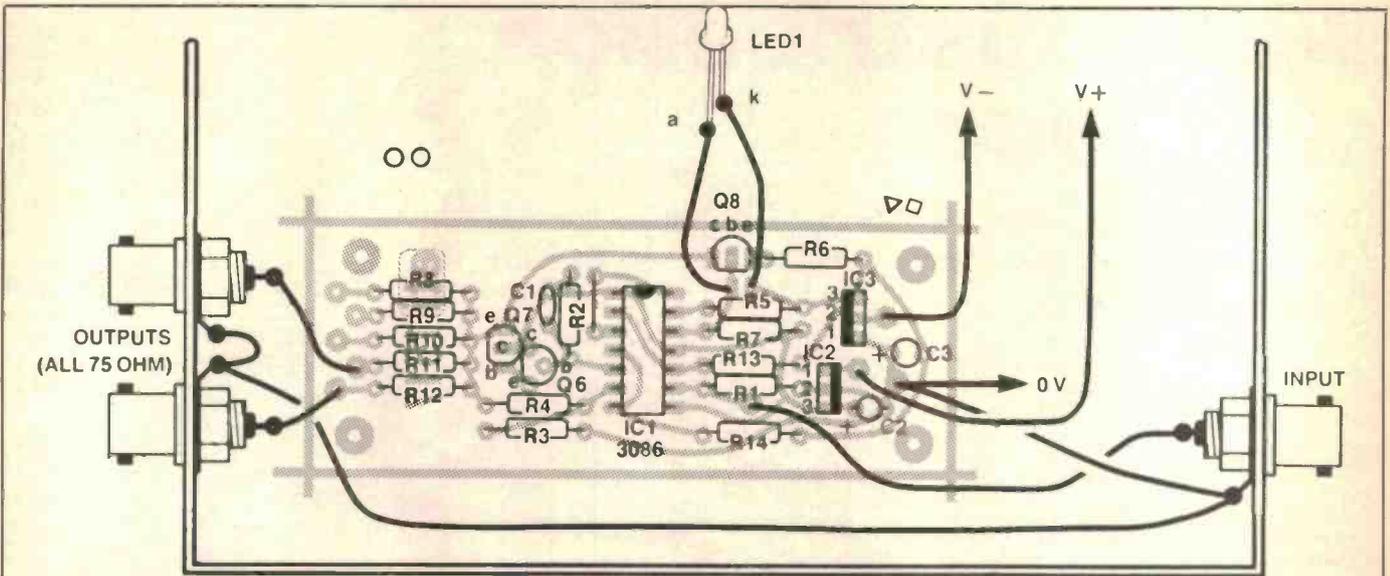
The heart of the unit is a transistor array IC — a CA3086. If you want to know more about this IC and its associated family, see Lab. Notes in the November 1980 issue. The transistors inside this package have been connected as a differential amplifier, the output of which drives a power output stage. Feedback provides a gain of one (i.e.: unity) and ensures a wide bandwidth. Regulated ± 5 V supplies are used so that the whole amplifier can be direct-coupled, yet maintain the output point at dc earth potential. In practice, the 'dc offset' at the output is on the order of 100 mV or so (it could be positive or negative).

Construction

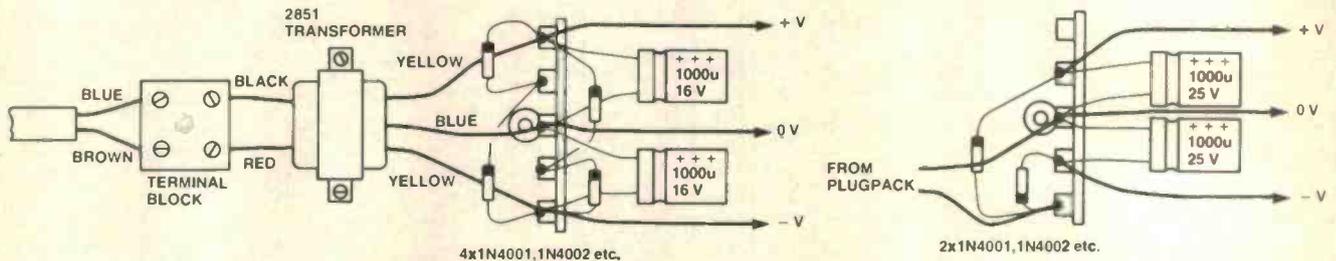
I built the video amplifier into a 50 x 95 x 158 mm jiffy box along with its own mains supply. This has the advantage of convenience, though it is possible to run the circuit off a 12 volt plugpack, which would make the whole a little cheaper if you already have the plugpack. Plugpacks are also safer for the constructor who is unfamiliar with mains wiring, though more



▶ Wrapped up, ready to go. The project and its power supply fit neatly in a large zippy box, leaving enough room to add a video enhancer later.



Overlay and wiring diagram. Showing how the pc board is assembled and wired up.



Power supplies. Wiring details for the two types of power supplies suggested.

expensive in the first place. Anyway, details are given for both situations.

In any case, the first stage is to select a box which will fit the parts comfortably. Ideally the project would be best in a tough metallic box, but the design is very stable and not liable to interference, so a cheaper plastic box such as the jiffy box I used is adequate, especially in a domestic situation.

Next, select the connectors you intend to use. Some video systems use RCA sockets and cables rather than the more robust BNC type. You may not require the full five outputs which the unit is capable of driving. Thus you may elect to economise and fit only two BNC sockets. (BNC sockets, if good ones, are not cheap). Or, you may fit two BNCs and an RCA type, in case. Note that solder lugs are needed for earthing.

Having selected the connectors you must decide on the power supply. I include the full mains transformer, rectifier, filter and so on, all of the components for which came to about half the cost of a plugpack, cord included! I recommend this approach as cost effective as well as convenient. (You cannot easily lose the parts you bolt in like you can lose a plugpack.)

Next, drill the box to allow the entry of the mains cable or the mounting of a plugpack connector as appropriate. Also, mounting holes for the connectors, the LED, printed circuit boards and power

transformer, if applicable, will be needed.

It is convenient to use the pc board as a template for marking the position of its mounting holes, before you fit any components to the board. I placed the board right up one end of the box the power supply at the other end, leaving room for a video enhancer board in the middle (...it's coming — Ed.).

It should be possible to use one of the transformer mounting bolts for a cable clamp to hold the mains cable if one of those special hole clamps is not used at the entry to the box. The ribbed insides of jiffy boxes often prevent the use of the hole clamp brackets and, as the cable must be clamped for safety reasons, be sure to allow for a clamp strap if you are not using a hole clamp.

Once the drilling is finished fit the components to the pc board after checking that all holes are correctly drilled and that all the tracks are OK. Be sure to get the ICs, and the tantalum capacitors and transistors the correct way around. If you are using a BD139 rather than BD639 for Q7, you will find that it has a different package and thus does not match the overlay diagram — be very careful to get it in the right way around. Attach short lengths of hookup wire to the pc board input, output and power connections. These can be trimmed and soldered to their respective desti-

nations once the board is bolted in place.

Next fit the transformer, mains cable and connectors in their respective positions in the box. Clamp the mains cable carefully and connect it to the terminal block, along with the transformer wires.

Now wire up the tagstrip, following the diagram carefully. Solder onto it the transformer secondary wires and the wires leading to the pc board. Mount the tagstrip and the pc board. Run an earth lead to each of the connector ground lugs, as shown in the wiring diagram, and then the 0V point on the pc board. Finally, connect the input and output leads and the LED wires.

Test

To test it, apply power and check that the rectifier outputs are correct. If you're using the 2851 transformer, you should measure around 9 V across each of the 1000u filter capacitors. If you're using the plugpack supply, you should get around 16-17 V across the 1000u filter capacitors. If they're OK, check the outputs of the two regulators. These should each be 5 V. The LED should be lit.

If there are any faults to this stage, switch off and sort them out before continuing. A wiring error is the usual culprit.

If all's well, connect it up and try it out.

HOW IT WORKS — ETI 1517

The unit is basically a dc-coupled feedback amplifier. It comprises a differential input stage, a buffer stage and a power output stage which together form a small but fast and powerful operational amplifier. This is suitably configured to give an overall gain into 75 ohm matched loads of precisely one, and a bandwidth of better than five megahertz — the requirement for a video distribution amplifier.

The differential input stage is created from a CA3086 IC (IC1) which contains five discrete transistors. Four (Q1 to Q4) are used to provide a Darlington long-tailed pair, with the fifth transistor (Q5) acting as the current source for the stage. The use of this IC, rather than having five discrete transistors guarantees good thermal matching for low offset and good matching of the transistors for predictable balance and gain.

The use of a Darlington configuration produces high input impedance and permits the stage to deliver an output swing sufficient to comfortably achieve the ± 2 V required to deliver colour video levels into a matching resistor and load. The fifth transistor is set to deliver around 2 mA into the Darlington pair, using a red LED as a voltage reference; this LED doubles as the power-on indicator.

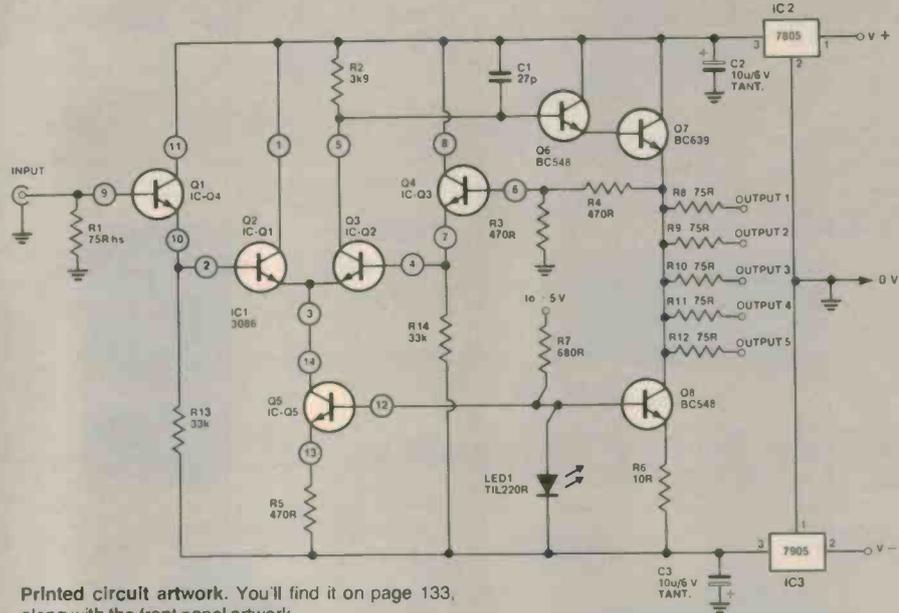
This current would provide a transconductance of sufficient value to give a gain of 35 if it were not for the two 33k resistors, R13-R14. These boost the gain to more like 65, as well as ensuring that charge storage effects in the bases of the two central transistors (Q2, Q3) do not limit the slew rate of the circuit to an unacceptable level.

The open loop bandwidth of the circuit is defined by the capacitor C1 in conjunction with the 3k9 load resistor, R2, and other minor effects.

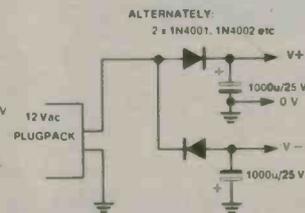
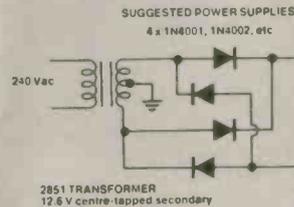
Transistor Q6 is a common collector circuit which buffers the differential pair output and provides a negative dc shift of about 0.6 volts. Q7 and Q8 form the output stage. Q8 is a current source setting the output quiescent current to about 100 mA, which is required (worst case) to drive five parallel output lines of 75 Ohms each. Q7 is a common collector stage which drives the output. Q8 also uses the LED as a voltage reference.

A BC548 or similar transistor has been specified for Q8, though a slightly more powerful one is required for Q7. In fact Q8 is just below the rated power level for a BC548 while Q7 may just exceed the maximum current rating. Neither transistor is very critical, owing to the feedback-type design employed, so some substitution is possible.

Resistors R3 and R4 form the feedback



Printed circuit artwork. You'll find it on page 133, along with the front panel artwork.



ratio defining resistors. High stability metal film types have been specified here. In practice, they define the gain of the whole amplifier and hence should be precise enough to ensure that the standard video levels are maintained. However, their value is not critical, only that they should be equal. It would be possible to use a pair of selected resistors of any value from 330 to 560 Ohms.

The input termination resistor and the output termination resistors are also specified as metal film types. This is in order to minimise mismatches with the cables used to connect to other video systems. It would be possible to use 47 or 51 Ohm metal film resistors if your system is 50 Ohm. In this case, the output stage could handle only four parallel loads.

The amplifier runs off + and -5 volts, provided by two three-terminal regulators. These are prevented from oscillating by the two tantalum capacitors, C2 and C3, which also provide supply rail bypassing over a wide bandwidth.

PARTS LIST ETI-1517

Resistorsall 1/4W, 5% unless noted
R1, R8-1275R, 1%
R23k9
R3, R4470R, 1%
R5470R
R610R
R7680R
R13, R1433k
Capacitors	
C127p
C2, C310u/6 V tant.
Semiconductors	
IC1CA3086, LM3086
IC27805, LM7805, LM340/T5
IC37905, LM7905, LM345/T5.0
Q6, Q8BC548
Q7BC639
LED1TIL220R red LED

Miscellaneous

ETI-1517 pc board; UB1 zippy box (50x90x150 mm); required number of BNC sockets; Scotchcal front panel; plugpack (12 Vac) or power supply components to suit — see text; wire, nuts, bolts, etc.

Price estimate: \$35-\$45

SPECIFICATIONS ETI-1517 VIDEO DISTRIBUTION AMPLIFIER

Number of outputsup to five
Peak output2 V peak-to-peak
Power bandwidth8 MHz (-3 dB @ 1 Vp-p output)
Small signal bandwidth26 MHz (-3 dB @ 200 mVp-p output)
Input impedance75 ohms
Output impedance75 ohms (any port)

(performance measured on prototype)

ROD IRVING ELECTRONICS IS YOUR No. 1 KIT SUPPLIER

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STEREO SIMULATOR

EA APRIL 83

\$12

for PCB version.



Self-contained version will cost approx. **\$20**
(does not include plugpack supply).

ETI-733 RADIOTELETYPE CONVERTER FOR THE MICROBEE

\$20.00

ETI April 1983

Have your computer print the latest news from the international shortwave news service. Just hook up this project between your shortwave receiver's audio output and the MicroBee's parallel port. A simple bit of software does the decoding. Can be hooked up to other computers too. P.O.A.



OVER 300 NOW SOLD

EA INVERTER INCLUDING TRANSFORMER

\$195

300 WATTS



P & P \$10.00
Anywhere
in Australia

JUNE EA 1982

ETI-335 PUSHBUTTON-PROGRAMMABLE WIPER CONTROLLER



ETI March 1983 **\$28.50**

No more fiddling with knobs and not getting the delay between wipes that you want — this windscreen wiper controller is simply programmed with two pushbuttons to provide the wiping delay you need.

PHOTON TORPEDO GAME

EA September 81

\$24.50



7-SLOT \$100 MOTHER BOARD

ETI May 80

\$90.00



FUZZBOX

\$19.90



Simple Fuzz Box for electric guitars. The no fuss, no nonsense Fuzz Box Confused — So are we. Seriously though if you want a sound with a difference, build this project and you can distort the waveform. It produces a sound which is buzzy (like politicians at election time). EA February 81

150W MOSFET POWER AMP

\$79.00

Plus Transformer **\$43.50**
Plus Heatsink Drilled,
Tapped and Black
Anodised **\$42.50**



A general purpose 150W Mosfet Power Amp Module. Here's a high power, general purpose Power Amplifier Module for guitar and PA applications employing rugged, reliable Mosfets in the output. ETI 499 March 82

CYLON VOICE

EA December 80

\$19.95



Sound like Darth Vader

SLIDE CROSS FADER **\$85.00**

EA November 81



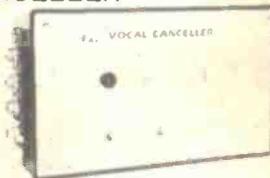
TV CRO ADAPTOR **\$38.50**

Includes Plug Pack EA August 80



VOICE CANCELLER

\$22.50



Ever wondered how your voice substituted for your favourite vocalists would sound, well now its possible! You can cancel out the lead vocal on almost any stereo record and substitute your own voice or musical instrument. EA April 82

Oct 82 ETI

ETI'S BRILLIANT NEW DIRECT-CONNECT COMPUTER MODEM



**Our Price
\$169.00**

Employs unique 'Commutated Filter' design overcoming virtually all the problems involved with conventional modems. Super flexible unit facilitates communications between computers over cables, the telephone network and radio links. Unit connects to a standard RS 232 interface and is capable of both 1200/75 Baud and 300/300 Baud transmission and reception. Line switching, answer and dialing facilities on board. **EXCLUSIVES:** ★ Plated through, double sided PCB ★ Complete set of IC sockets ★ Kit requires 85 1N914 Diodes for programming these are included ★ Ceralock resonator and matching balanced load capacitor used for long life and high accuracy ★ Telecom approved isolating transformer and Reed relays included.

LOUD SPEAKER PROTECTOR

ETI 455 March 80



\$32.50

DIGITAL ENG. ANALYSER **\$48.50**



EA August 86

DIGITAL CAPACITANCE METER **\$47.50**



Here is an inexpensive Digital Capacitance Meter which measures from 1pF to 99.99uF in just three ranges. It's simple to use and features a big bright four-digit display with automatic updating and decimal points. EA March 80

ELECTRONIC DUMMY LOAD **\$99.00**

With this unit you can test power supplies at currents up to 15 Amps and Voltages up to 60 Volts. It can 'sink' up to 200 Watts on a static test and you can modulate the load to perform dynamic tests. ETI 147 October 80



ROD IRVING ELECTRONICS — YOUR MAIL ORDER SPECIALISTS

General Enquiries: (03) 489 8131

425 HIGH ST, NORTHCOTE, VICTORIA 3070

Mail Order Hot Line (03) 481 1436

SHOPAROUND

This page is to assist readers in the continual search for components, kits, printed circuit boards and other parts for ETI projects and circuits. If you are looking for a particular item or project and it is not mentioned here, check with our advertisers.

ETI-736 Fax decoder

Be your own weather forecaster - and with some authority, because you'll have all the weather maps and satellite pictures to hand! This project will be widely stocked as a kit and, as parts are all bog-standard items, constructors should have little difficulty getting it all together.

To date, the following firms have indicated they'll be stocking kits: **Altronics** in Perth, **Electronic Agencies** in Sydney, **Jaycar** in Sydney (now with three stores - 'Silicon Alley', Carlingford and Hurstville) and **Rod Irving** in Melbourne. You might also try **All Electronic Components** in Melbourne, **Avtek** in Sydney and **Tomorrow's Electronics** in Gosford.

Ready-made printed circuit boards should be available from the suppliers listed at the end of this column, or, if you're making your own, a positive or negative transparency can be obtained from us for \$1.50 from **ETI-Artwork**, **ETI Magazine**, P.O. Box 21, Waterloo NSW 2017. Make cheques or money orders payable to 'ETI Artwork Sales', and ensure you ask for a positive or negative according to the type of photoresist you're using.

ETI-421 3-way speakers

Known as the Dick Smith 'Series 200' loudspeakers, these will be available in kit form, as well as built-up, from all Dick Smith stores. You get a pair in the kit for just \$249.50 complete, or \$299 the pair built-up.

ETI-1517 Video distribution amplifier

This project should be popular among the video buffs et al. It's cheap, easy to build and uses readily available bits. Not everyone stocks the CA3086, but they are widely available nonetheless.

Kits should be available from **Jaycar** in Sydney, **Rod Irving Electronics** in Melbourne, **All Electronic Components**, also in Melbourne and **Dick Smith** stores all over. **Altronics** may possibly stock this project as a kit, also.



No muffin for nuffin'. That's right, folks, you can't get a Muffin-style rotary fan for nothing, but you can occasionally get a good price. This German-made 240-V, 150 mm diameter fan is currently available from **Radio Despatch** in Sydney at a price we can't disclose for fear of causing such a stampede that their premises would never recover. First in, best dressed. Keep your cool, stroll down to 869 George St., Broadway, and shout your family/friends to lunch at McDonalds next door with your savings.

Printed circuit boards should be available from the suppliers listed at the end of this column. If you want to make your own, a positive or negative transparency is available from us for a piddling \$1, post paid. Send your rustproof money to: **ETI-1517 Artwork**, **ETI Magazine**, P.O. Box 21, Waterloo NSW 2017. Make out cheques or money orders to 'ETI Artwork Sales', and make sure you ask for a positive or negative transparency, according to what you require.

ETI-166 Function/pulse generator

The saga continues, once again. As this is an unusual project, requiring construction techniques that would not be familiar to most constructors, we're describing it in detail - and it's taking up a lot of room! But we like to ensure that any reader tackling such a project will be reasonably ensured of success. Be patient and you will be rewarded with a fine instrument.

More of the saga next month.

Gee, they look after you

In ever-increasing efforts to look after the whims and fancies of all you happy hobbyists out there, **Altronics** and **Jaycar** have just increased their services.

Altronics, manned by that Irishman-who-walks-on-water, **Jack O'Donnell**, and his happy band of leprechauns, has installed a 'toll free' telephone ordering service. For the cost of a local 'phone call (12 measly cents), bankcard holders may phone their order for any advertised **Altronics** products from anywhere in Australia. Just call 008-999007.

Don't forget **Altronics'** overnight jetservice - 'phone in the afternoon, have your order delivered the next morning. **Jack O'Donnell** maintains that an order phoned through up to 6 pm eastern standard time will normally be delivered the next morning to any capital city or suburb east of Perth; the following day to country areas.

Jaycar has opened another store in Sydney. For southside

constructors, from the first of September, you'll be able to get **Jaycar** kits, components and products from their new store located at 121 Forest Rd, Hurstville. The 'phone number is 570-7000. Call in for a browse, or to buy the latest copy of **ETI**.

Printed circuit board and panel suppliers

Almost every pc board ever published by **ETI** may be obtained from the following suppliers:

All Electronic Components
118 Lonsdale St
Melbourne Vic. 3000

RCS Radio
651 Forest Rd
Bexley NSW 2207

Panels, meter scales and dial faces for almost every **ETI** project published may also be obtained from the above two firms.

For pc boards produced over the last three to five years, the following suppliers generally keep stocks on hand:

Electronic Agencies
115-117 Parramatta Rd
Concord NSW 2137
and

117 York St
Sydney NSW 2000

Radio Despatch Service
869 George St
Sydney NSW 2000

Rod Irving Electronics
425 High St
Northcote Vic. 3070

James Phototronics
522 Grange Rd
Fulham Gardens SA 5024

Jemal Products
P.O. Box 168
Victoria Park WA 6100

Jaetronics
58 Appian Drive
St Albans Vic. 3021

Sunbury Printed Circuits
Lot 14, Factory 3
McDougall Rd
Sunbury Vic. 3429

Billeo Electronics
Shop 2, 31 Pultney St
Dandenong Vic. 3175

Mini Tech
P.O. Box 9194
Auckland N.Z.

IDEAS FOR EXPERIMENTERS

These pages are intended primarily as a source of ideas. As far as reasonably possible all material has been checked for feasibility, component availability etc, but the circuits have not necessarily been built and tested in our laboratory. Because of the nature of the information in this section we cannot enter into any correspondence about any of the circuits, nor can we produce constructional details.

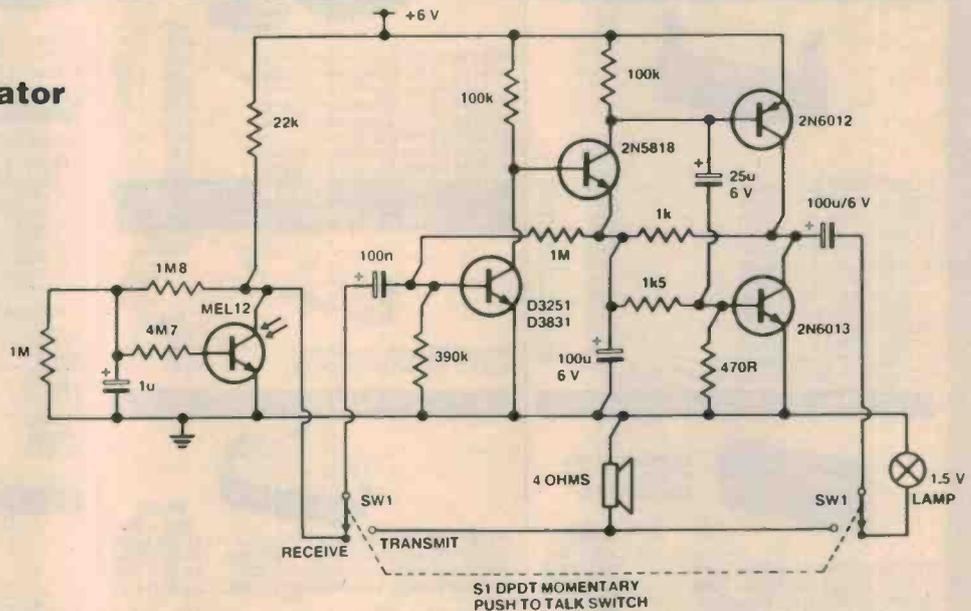
Flashlight communicator

This simple, portable, visually-aligned transceiver, designed by **Chris McRae of West Pymble NSW**, is quite effective and can be easily built into a flashlight.

The lamp current, modulated at an audio frequency, modulates the light beam. The light beam is detected by a photodarlington transistor and drives a small speaker for audio output.

The lamp is driven by an ac signal which cuts the RMS voltage to about one-third of the six volts, which is why a 1.5 V bulb is used in a 6 V circuit.

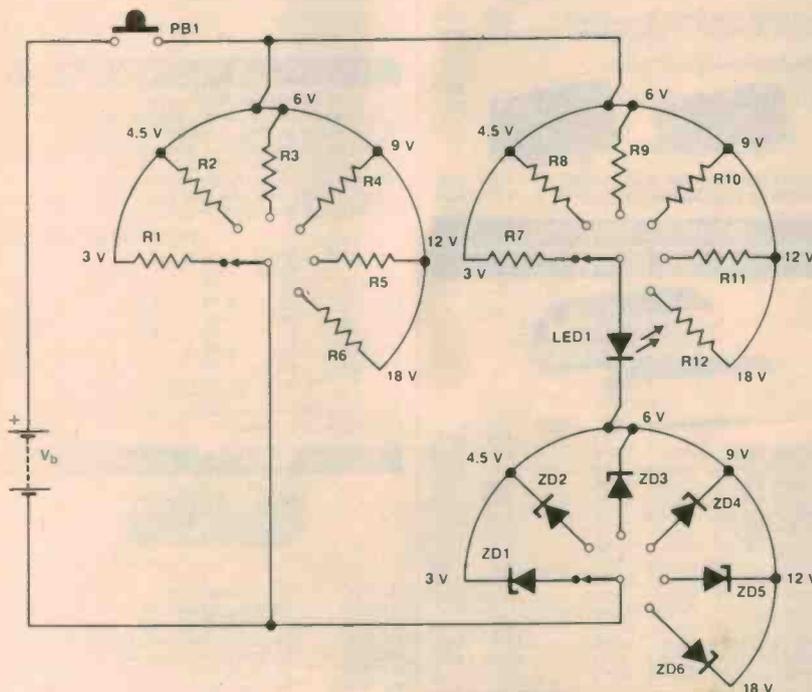
The photodarlington can be mounted on the axis of the beam or you may get better sensitivity by placing it so that it faces the reflector of the flashlight just above the bulb (the bulb filament is at the focal point of the reflector).



Fidelity is not high due to the low pass characteristics of the bulb filament, but I have been

able to have intelligible conversations at distances up to 30 metres.

Modification to battery condition indicator



Jerry Stamatelatos of St Kilda Victoria has come up with a modification for the battery condition indicator circuit which appeared in ETI Circuits No 4 on page 70.

The modification is based on the addition of three rotary switches which provide a selection of six voltages.

Resistors	all 1/4 W, 5%
R1	270R
R2,R12	390R
R3	470R
R4	820R
R5	1k
R6	1k5
R7	68R
R8	100R
R9	120R
R10	180R
R11	220R

Semiconductors	
ZD1	0V7*
ZD2	2V1*
ZD3	3V3
ZD4	5V6
ZD5	8V2
ZD6	13 V

*For these low zener voltages, use one or more silicon diodes in series forward biased.



ROD IRVING ELECTRONICS

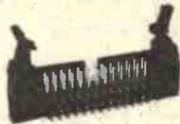
2 BRANCHES:

425 High St. Northcote, Ph.: (03) 489 8131
48-50 A'Beckett St. Melb. Ph.: (03) 347 9251

Mail orders: P.O. Box 235 Northcote, Vic. 3070 min p&p \$3.00

Errors and omissions excepted.

INSULATION DISPLACEMENT CONNECTORS PC MOUNTING HEADERS



	PRICE	
	1-9	10+
P12010 10 Pin S T Header	3.95	3.90
P12011 10 Pin R.A Header	3.95	3.50
P12020 20 Pin S.T Header	5.95	5.25
P12021 20 Pin R.A Header	5.95	5.25
P12026 26 Pin S.T Header	6.95	6.25
P12027 26 Pin R.A Header	6.95	6.25
P12034 34 Pin S.T Header	7.95	7.25
P12035 34 Pin R.A Header	7.95	7.25
P12040 40 Pin S.T Header	8.95	8.25
P12041 40 Pin R.A Header	8.95	8.25
P12050 50 Pin S.T Header	9.95	8.95
P12051 50 Pin R.A Header	9.95	8.95

Mounts on PCB and Mates with IDC Sockets.

CARD EDGE CONNECTORS



Edge Connectors to suit Disk Drives Etc.

	PRICE	
	1-9	10+
P12060 10 Way Card Edge Conn	7.95	7.10
P12062 20 Way Card Edge Conn	8.50	7.95
P12064 26 Way Card Edge Conn	8.95	8.10
P12066 34 Way Card Edge Conn	9.95	8.95
P12068 40 Way Card Edge Conn	11.50	10.50
P12070 50 Way Card Edge Conn	12.50	11.50

WIRE WRAP HEADERS



	PRICE	
	1-9	10+
P12080 10 Pin W.W Header	6.95	5.95
P12081 10 Pin W.W R.A Header	6.95	5.95
P12082 20 Pin W.W Header	7.95	5.95
P12083 20 Pin W.W R.A Header	7.95	5.95
P12084 26 Pin W.W Header	8.95	7.95
P12085 26 Pin W.W R.A Header	8.95	7.95
P12090 34 Pin W.W Header	9.95	8.95
P12091 34 Pin W.W R.A Header	9.95	8.95
P12092 40 Pin W.W Header	12.95	11.95
P12093 40 Pin W.W R.A Header	12.95	11.95
P12094 50 Pin W.W Header	13.95	12.95
P12095 50 Pin W.W R.A Header	13.95	12.95

IDC SOCKETS



	PRICE	
	1-9	10+
P12100 10 Pin Socket	4.95	3.95
P12102 20 Pin Socket	5.95	4.95
P12104 26 Pin Socket	6.95	5.95
P12106 34 Pin Socket	7.95	6.95
P12108 40 Pin Socket	8.95	7.95
P12110 50 Pin Socket	9.95	8.95

CABLE PLUGS



	PRICE	
	1-9	10+
P12114 14 way crimp	1.95	1.50
P12116 16 way crimp	2.25	1.95
P12124 24 way crimp	3.95	3.25
P12140 40 way crimp	6.50	5.95

COMPONENT CARRIERS



	PRICE	
	1-9	10+
P12148 8 Pin Component Carrier	1.75	1.50
P12152 14 Pin Component Carrier	1.95	1.70
P12154 16 Pin Component Carrier	2.25	1.95
P12156 18 Pin Component Carrier	2.75	2.50
P12158 20 Pin Component Carrier	3.50	3.10
P12160 24 Pin Component Carrier	3.95	3.50
P12162 28 Pin Component Carrier	4.95	4.50
P12164 40 Pin Component Carrier	5.95	5.40

25PIN "D" CONNECTORS 10C CRIMP



	PRICE	
	1-9	10+
P12170 25 Pin Plug Crimp	12.95	11.95
P12171 25 Pin Socket Crimp	13.95	12.95

CENTRONICS



	PRICE	
	1-9	10+
P12200 36 Way Centronics Plug IDC	12.50	11.50
P12201 36 Way Centronics SCKT IDC	13.50	12.50
P12203 50 Way Centronics Plug IDC	14.50	13.50
P12204 50 Way Centronics SCKT IDC	15.50	14.50
P12210 36 Way Solder Plug	15.95	14.50
P12211 36 Way Solder Line SCKT	15.95	14.50
P12213 36 Way Solder Chassis SCKT	15.95	14.50

STRIP HEADERS

30 Way Male .1" x .1" Matrix



P12230 30 Way Single Strip Header	3.95	3.75
P12231 30 Way Oval Strip Header	4.95	4.75

30 Way Female .1" x .1" Matrix



P12234 30 Way Single Plug Header	4.95	3.95
P12235 30 Way Dual Plug Header	5.95	4.95

SOLDER CONNECTORS

D RANGE CONNECTORS



	PRICE	
	1-9	10+
P10880 DE9P Male 9 Pin	3.50	3.00
P10881 DE9S Female 9 Pin	4.50	4.00
P10882 DE9C Cover 9 Pin	2.50	2.20
P10890 DA15P Male 15 Pin	3.90	3.50
P10891 DA15S Female 15 Pin	4.90	4.50
P10892 DA15C Cover 15 Pin	2.50	2.20
P10900 DB25P Male 25 Pin	4.90	4.10
P10901 DB25S Female 25 Pin	4.95	4.50
P10902 DB25C Cover 25 Pin	2.50	2.20
P10910 DC37P Male 37 Pin	8.90	8.20
P10911 DC37S Female 37 Pin	10.90	9.90
P10912 DC37C Cover 37 Pin	5.50	4.90
P10920 DD50P Male 50 Pin	12.90	11.90
P10921 DD50S Female 50 Pin	14.90	12.90
P10922 DD50C Cover 50 Pin	6.50	5.50

LOGIC BOARD SOCKETS

P10915 15/30 .156"S.T.	6.95	1-9	10+
P10918 18/36 .156"S.T.	6.95		6.50
P10920 20/44 .156"S.T.	7.95		6.50
			6.95

LOW PROFILE IC SOCKETS

		PRICE	
		1-9	10+
Economical Solderfall			
P10550 8 Pin		.25	.20
P10560 14 Pin		.35	.30
P10565 16 Pin		.40	.35
P10567 18 Pin		.50	.40
P10568 20 Pin		.50	.40
P10569 22 Pin		.50	.40
P10570 24 Pin		.50	.40
P10572 28 Pin		.60	.50
P10575 40 Pin		.70	.60

		PRICE	
		1-9	10-25
Precision Machined Gold Insert			
P10620 8 PIN		1.20	1.00
P10624 14 PIN		1.60	1.40
P10626 16 PIN		1.90	1.70
P10628 18 PIN		2.00	1.80
P10630 20 PIN		2.20	2.00
P10632 22 PIN		2.40	2.20
P10634 24 PIN		2.60	2.40
P10640 28 PIN		2.90	2.70
	40 PIN	4.40	4.00

WIRE WRAP SOCKETS



	PRICE	
	1-9	10+
P10579 8 Pin	1.20	1.00
P10580 14 Pin	1.40	1.20
P10585 16 Pin	1.60	1.40
P10587 18 Pin	1.90	1.70
P10590 20 Pin	2.20	2.00
P10592 22 Pin	2.40	2.10
P10594 24 Pin	2.50	2.20
P10596 28 Pin	2.80	2.40
P10598 40 Pin	3.30	2.90

MOLEX PINS

Make your own IC Sockets. Supplied on a Breakoff Header.

P10700 Pack 100	\$2.25
P10701 Pack 1000	\$16.00

IDC RIBBON CABLE

This is the only Ribbon Cable to use in I.D.S. or crimp style connectors. We use in our computer productions. As the exact spacing and quality is critical for ultra reliable long term computer operations. Do not try and use cheaper Ribbon Cables as you will find that the reliability doesn't justify the cheaper prices. Colour is Grey with wire one being colour coded to match up with Pin one of I.D.C. Connectors.

	PRICE PER METRE			
No. of Cond.	1-9	10-99	100+	
W12616 16	1.90	1.70	1.40	
W12624 24	2.90	2.60	2.10	
W12634 34	3.90	3.50	3.10	
W12640 40	4.90	4.40	3.90	
W12650 50	5.90	5.20	4.60	
W12660 60	6.90	5.90	4.90	

WARNING

This is the only type of Cable to use for Insulation Displacement Connectors. I.D.C.

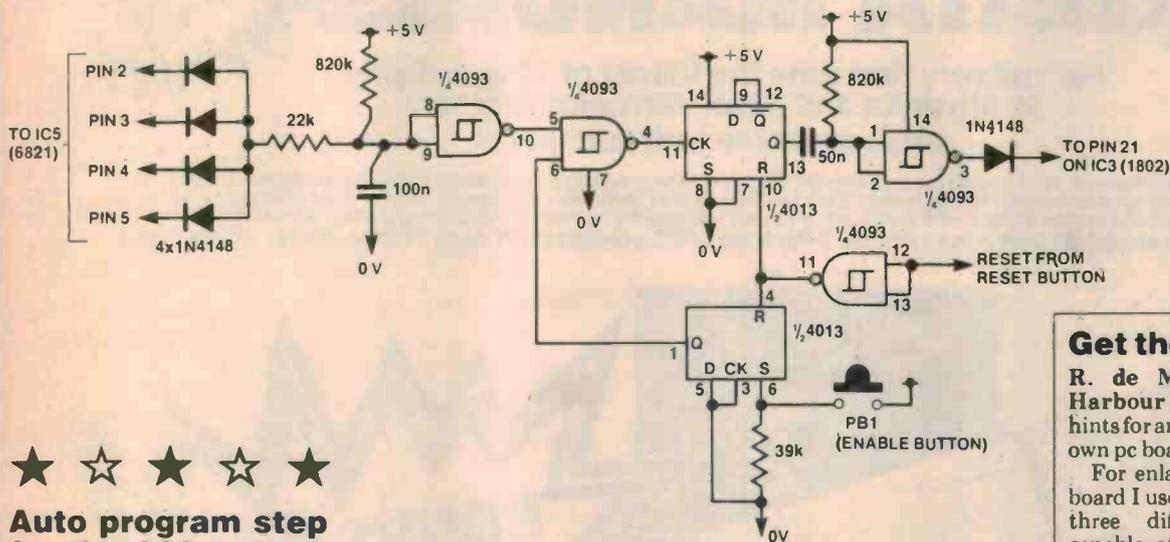
UNPROTECTED HEADERS



	Dual In Line 2.54mm	
	1-9	10+
P12240 10 Way Unprot. Header	1.95	1.75
P12246 16 Way Unprot. Header	2.95	2.50
P12250 20 Way Unprot. Header	3.25	2.95
P12256 26 Way Unprot. Header	3.75	3.25
P12260 30 Way Unprot. Header	3.95	3.50
P12264 34 Way Unprot. Header	4.95	4.45
P12270 40 Way Unprot. Header	5.95	5.25
P12275 50 Way Unprot. Header	6.95	6.25
P12280 60 Way Unprot. Header	8.95	7.95

100+, less 10% from 10+ price

IDEA OF THE MONTH



Auto program step for the 660

H. Greber, North Rockhampton Qld

This circuit eliminates the need to press the step key on the ETI-660 when you want to advance the address when you're programming it.

The annoying problem of contact bounce in the step key, which causes the computer to jump locations when programming, is also solved with this circuit.

The circuit is enabled by pressing SW1 which I set up as a

spare key on my keyboard. With the circuit enabled you then type in the program as you would normally do, however, you don't have to press the step button after every second hex digit as this is done automatically.

When you have finished typing in the program press the reset button to disable the circuit. If a mistake is made the correction procedure is the same except the

enable key must be pressed again, after correcting the mistake, to continue programming.

The step key operates normally when this circuit is enabled or disabled so you can still skip locations with it when programming.

When building up the circuit change the value of the capacitor across the reset button from 100n to 200n.

Get the drill on vice

R. de Moulpied of Coffs Harbour NSW has some useful hints for anyone who makes their own pc boards.

For enlarging holes in the pc board I use a small pin vice with three different size collets capable of holding small drills from 0.8 mm to 3.5 mm. This is also very handy for inserting pc board stakes, instead of using a pc board insertion tool.

The problem of sharpening small drills has been overcome by using an old electric can opener. I removed the can cutter section and also the back plate covering the knife grinder. Then I put a switch on the side of the unit, connected the power and I had a small drill grinder.

I also use the pin vice for holding the drill while I am sharpening it, as I look through a head-type x10 magnifier.

'IDEA OF THE MONTH' CONTEST

PRIZE WORTH \$90!

COUPON

Cut out and send to: Scope/ETI 'Idea of the Month' Contest, ETI Magazine, 140 Joynton Ave, Waterloo NSW 2017.

"I agree to the above terms and grant Electronics Today International all rights to publish my idea in ETI Magazine or other publications produced by them. I declare that the attached idea is my own original material, that it has not previously been published and that its publication does not violate any other copyright."

* Breach of copyright is now a criminal offence.

Title of Idea

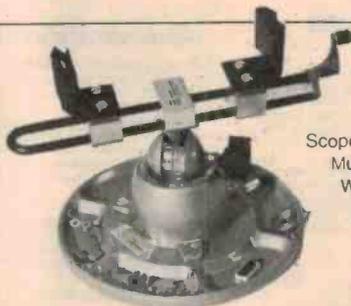
Signature

Name

Date

Address

Postcode



Scope Panavise Multi-purpose Work Centre.

Scope Laboratories, who manufacture and distribute soldering irons and accessory tools, have offered to sponsor a contest with a prize to be given away every month for the best item submitted for publication in the 'Ideas for Experimenters' column — one of the most consistently popular features in ETI. Each month we will be giving away a Scope Panavise Multi-purpose Work Centre, Model 376/300/312, comprising a self-centering head (376), standard base (300) and tray base mount (312), all worth about \$90! Selections will be made at the sole discretion of the editorial staff of ETI Magazine. Apart from the prize, each winner will be paid \$10 for the item published. You must submit original ideas of circuits which have not previously been published. You may send as many entries as you wish.

RULES

This contest is open to all persons normally resident in Australia with the exception of members of the staff of Scope Laboratories, Federal Publishing Company Proprietary Limited, ESN, The Litho Centre and/or associated companies.

Closing date for each issue is the last day of the month. Entries received within seven days of that date will be accepted if postmarked prior to and including the date of the last day of the month.

The winning entry will be judged by the Editor of ETI, whose decision will be final. No correspondence can be entered into regarding the decision.

Winner will be advised by telegram the same day the result is declared. The name of the winner, together with the winning idea, will be published in the next possible issue of ETI.

Contestants must enter their names and address where indicated on each entry form. Photostats or clearly written copies will be accepted but if sending copies you must cut out and include with each entry the month and page number from the bottom of the page of the contest. In other words you can send in multiple entries but you will need extra copies of the magazine so that you send an original page number with each entry.

This contest is invalid in states where local laws prohibit entries.

Entrants must sign the declaration on the coupon that they have read the above rules and agree to abide by their conditions.

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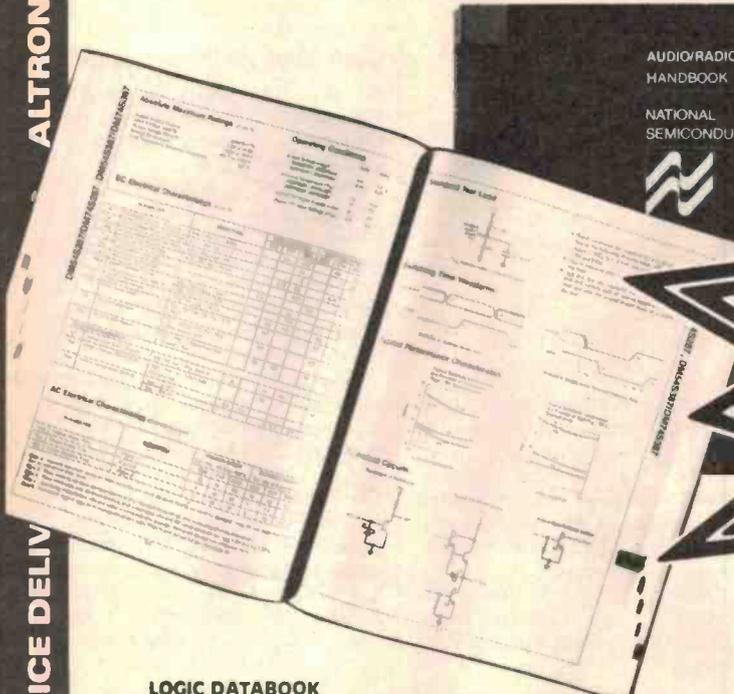


NATIONAL SEMICONDUCTOR DATA MANUALS



For the very first time the full set of 10 is available at Altronic and Major Altronic Resellers (Also available individually)

Without doubt these National Semiconductors Data Manuals are the very best available in the world today, but until now they've been almost impossible to get (the National People forever giving excuses such as "Australia's allocation is only so many books per year etc"). So we've beaten our competitors to the punch and arranged a special Print Order for Altronic and Major Altronic Resellers. But Once they are gone there may not be a further print edition until June 1984 — Order yours now!



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LOGIC DATABOOK

National's new Logic Databook covers five of their logic families: TTL (54/74), Schottky (54S/74S), low power Schottky (54AS/74AS), high speed (54HL/74HL), and low power (54L/74L).

The Logic Databook—especially organized for quick and easy referencing—offers two complete functional indices and selection guides, one for SSI and one for MSI devices. In addition, it includes over 100 connection diagrams and test waveforms to help speed the design-in cycle.

All in all, it's probably the most comprehensive collection of practical information ever assembled on such a broad line of practical components.

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The Hybrid Products Databook is the only National Semiconductor publication that contains complete information on all of our hybrid semiconductor products. Included are precision thin film and thick film products which provide the user with standard functions from operational amplifiers to converters with capabilities beyond those of current monolithic technology.

Product selection guides and an application section are also included.

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This handbook exists to acquaint those involved in audio systems design with National Semiconductor's broad selection of integrated circuits specifically designed to meet the stringent requirements of accurate audio reproduction.

Far from just a collection of data sheets, this manual contains detailed discussions, including complete design particulars. Thorough explanations and complete design examples makes clear several audio areas never before available to the general public.

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With the variety of fixed- and variable-regulator technology currently available, the 336-page Voltage Regulator Handbook becomes a must for the selection of three-terminal and dual tracking components that meet the system requirement while utilizing the most cost-effective approach.

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The new 1983 edition of the National Semiconductor Linear Databook is the most comprehensive available. It presents approximately 2000 pages of specifications for high technology linear products within its two volumes. Applications, descriptions, features and diagrams in this databook include detailed sections for Voltage Regulators, Op Amps, Voltage Comparators, A to D, D to A Converters, Industrial Blocks and Audio, and TV Circuits.

The Databook also features advanced telecommunication devices and speech synthesis (DIGITALKER™), plus other non state-of-the-art linear products offering performance, economy, quality and reliability.

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THE INTERFACE DATABOOK

In National Semiconductor's Interface Databook, 702 pages of specifications describe one of the industry's broadest lines of interface products.

Over 300 data sheets have been compiled, covering transmission line drivers/receivers, bus transceivers, peripheral/power drivers, level translators/buffers, display drivers, MOS and magnetic memory interface circuits, microprocessor support circuits, applicable TTL and CMOS logic circuits.

An industry cross reference guide gives National Semiconductor's exact replacement for 7 other manufacturers' Product selection guides and a complete product applications section make it easy to find the correct part number for these specialized ICs.

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National Semiconductor has added many new transistors and product families since publication of the last databook. Many have already been widely acclaimed by users.

In addition to small-signal, power-bipolar and field-effect transistors that have been the mainstay of our catalog, there is a section for multiple-field-effect transistors. More part numbers will be added as market needs expand.

To keep current on all new National transistors, please contact your National sales representative or franchised distributor and ask to be placed on the customer mailing list.

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CMOS DATA BOOK

This databook contains information on National Semiconductor's standard SSI/MSI CMOS products. This includes the popular 54C74C series logic family, which is pin for pin, function for function equivalent to the 7400 family of TTL devices. All device outputs are LPTTL compatible, capable of sinking more than 360µA = 1 LSTTL load. The AC parameters are specified with a 50pF capacitive load.

In addition, this book describes National Semiconductor's extensive line of CD40XXB and CD45XXB series devices. These parts meet the standard JEDEC "B-Series" specifications.

Special Function, LSI: A/D Converters and Memory device specifications contained herein offer the designer unique, high-density low-power system solutions. All devices are compatible with 54C/74C series and CD4XXB series products.

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MEMORY DATABOOK

National Semiconductor has continued its reputation as a high-volume supplier of high-quality, cost-effective components by expanding into the design and processing of semiconductor memories.

While developing this state-of-the-art technology, National met the problems of industry standardization by proposing and utilizing new terminology and symbols to make all memory data sheets consistent. Hence, a cohesive, 464-page databook that includes selection guides, diagrams, and test characteristics for RAMs, EPROMs, MOS ROMs, and magnetic bubble memories.

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EXTRA KICK FOR OSCAR

The kick-motor firing of AMSAT Oscar 10, on July 12, injected the satellite into an intermediate orbit of 3900 km at perigee and 35 800 km at apogee, with an inclination of 26 degrees.

The motor burn lasted about 90 seconds longer than scheduled, causing the perigee to be higher than expected. This extra-length burn used more of the helium supply than it should have, making AMSAT unsure whether the next burn will be totally successful.

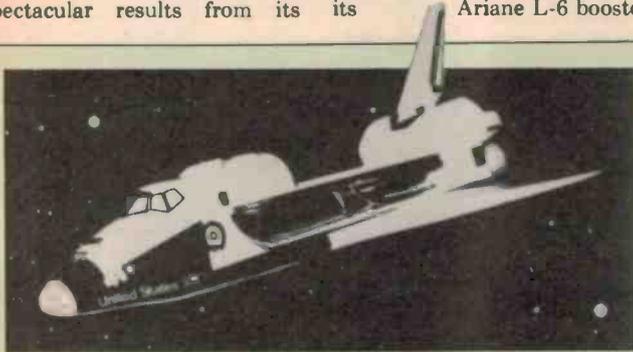
Even if the second kick-motor firing is not totally successful or is cancelled, AMSAT says the satellite will still produce some spectacular results from its

present orbit.

The only serious ramification of a failure in the second motor burn would be to users in the Northern Hemisphere, who would not have as much access to the satellite over the next five years as they will if a successful firing occurs.

In its present orbit, Oscar 10 will be a Northern Hemisphere satellite for the next several years, but eventually the apogee will precess, changing it to a primarily southern latitude bird.

Oscar 10's initial problems after the orbital injection were probably caused by its being 'bumped' by the third stage of its Ariane L-6 booster.



A HAM IN SPACE!

Doctor Owen Garriott is set to become the first radio ham to operate a station from space. On September 30, when Dr Garriott (W5LFL) rides into Earth orbit as a crew member of the United States space shuttle Columbia, he will have with him a 5 W FM transceiver for operation on the two-metre band.

To contact W5LFL, who will be using a 'split-ring' antenna mounted in one of Columbia's windows, ground stations will need a rig with programmable offset, or separate receive-and-transmit VFOs. Alternatively, two different radios can be used, one for transmitting and the other for receiving.

Ground stations will transmit on frequencies between 144.91 and 145.49 MHz, with W5LFL acknowledging the callsigns he hears on a frequency between 145.51 and 145.77 MHz.

The maximum duration from time of acquisition to loss of signal, from any given geographic point, will be about eight minutes for a pass directly overhead. Access time will be shorter if Columbia passes closer to the horizon at the ground-station location.

Unless they are adept at satellite tracking, radio amateurs have been advised to avoid using highly directional antennas. The speed of the shuttle will be about 27 000 km/h, so unless the rotor system can operate under computer-tracking control, use of a highly directional antenna array will be more of a hindrance than a help.

Amateurs who are unfamiliar with the intricacies of satellite tracking should use omni-directional antennas, with the 'turnstile' crossed-dipole array deemed the best choice.

Dr Garriott has requested that high-power amplifiers be avoided. A 10 W output FM signal into a turnstile-type antenna will be more than adequate to reach W5LFL.

50-50.15 MHz OPEN FOR BUSINESS!

The lower 150 kHz of the 'international' sector of the six-metre band can now be used by Australian amateurs on a restricted basis, according to recent advice from the Federal Department of Communications

As from the last week in July this year, amateurs will be allowed to operate between 50 MHz and 50.150 MHz subject to the following restrictions:

- No interference is caused to reception of Channel 0 transmissions (i.e. operation is generally in accordance with the provisions of paragraphs 5.37 to 5.39 of the Amateur Operator's Handbook — DOC 1978).
- Operation is restricted to outside the hours of broadcast of Channel 0 stations.
- Operation in Western Australia, the Australian external territories and Antarctica is not time limited.

It's a pity this de-restriction long missed the peak of Cycle 21, but some intercontinental DX can still be had, undoubtedly. It should certainly 'open the window' to a lot of trans-Pacific DX.

If you're thinking of arranging skeds with west coast United States and Central American stations (via trans-equatorial propagation), you should start sked sessions around the equinoxial periods (around March 21 and September 21), commencing when the mid-path time is midday and running for some hours following. That's about 8-8.30am EST.

CHANGES TO VK2 BEACONS

The Sydney beacons, located at the WIA transmitting site at Dural, have changed callsign from VK2WI to VK2RSY and the new 70 cm band beacon is now operational.

The beacon frequencies are: 28.262, 52.420, 144.420 and 432.420 MHz.

The new 70 cm beacon runs 15 watts to a horizontally polarised omnidirectional antenna at a height of 20 metres above ground. Identification is by fre-

quency shift keying, as with the VHF beacons.

The Dural two-metre and 70 cm repeaters now operate under the one licence, using the callsign VK2RWI. The 70 cm repeater previously had the callsign VK2RUS.

An information sheet detailing the operation of these repeaters may be obtained by writing to the WIA NSW Division, P.O. Box 1066, Parramatta NSW 2150.

MELBOURNE'S BIGGEST COMMUNICATIONS EXPO

Communications Expo '83, a combination hamfest and communications exhibition, is to be held in Melbourne on September 3.

The largest event of its kind held in Melbourne, the Expo is being staged at the Nunawading Civic Centre (Whitehorse Road, Nunawading) by the Eastern and Mountain District Radio Club, as part of World Communications Year.

The Expo will feature a work-

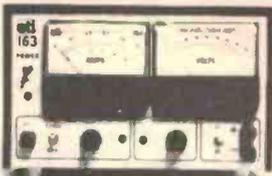
ing amateur radio station and a variety of communications technology, displayed by emergency services, electronics companies and the Army.

VK3WCY will be on HF and VHF from 9.30 am to 4.30 pm on the day of the Expo.

For further information, contact Jim Linton, Eastern and Mountain District Radio Club, P.O. Box 87, Mitcham Vic. 3132. (03)232-3534.

**ETI-163
LAB SUPPLY**

\$159.00
ETI May 1983



Fully variable 0-40 V current limited 0-5 A supply with both voltage and current metering (two ranges 0-0.5 A/0-5 A). This employs a conventional series-pass regulator, not a switchmode type with its attendant problems, but dissipation is reduced by a unique relay switching system switching between taps on the transformer secondary.

\$47.50

ETI-688 BIPOLAR PROM PROGRAMMER Every digital workshop should have one! Can be used to program the popular fusible-link PROMs like the 74S188/288, 82S23 and 82S123 etc.
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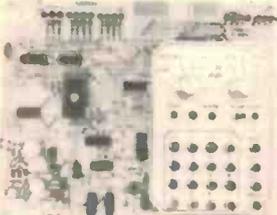
ETI-688 MICROBEE EPROM PROGRAMMER Simple, low cost programmer for the MicroBee can program 2716s, 2516s, 2732s and 2764s.
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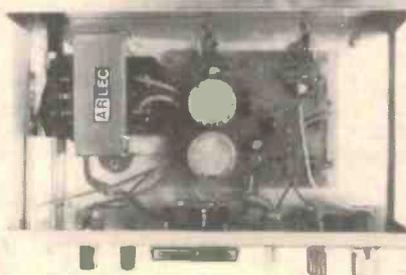
EPROM PROGRAMMER
\$43.00

No need for a Micro with EA's great Eprom Programmer suitable for 2716/2758 Eproms.

With Textool Sockets \$55.00
EA January 82



DUAL TRACKING POWER SUPPLY
\$83.50



Build around positive and negative 3-Terminal Regulators, this versatile dual tracking Power Supply can provide voltages from $\pm 1.3V$ to $\pm 22V$ at currents up to 2A. In addition, the Supply features a fixed +5V 0.9A output and is completely protected against short circuits, overloads and thermal runaway EA March 82

SOUND TRIGGERED FLASH
\$26.50

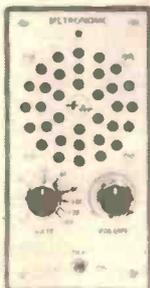
This easy to build sound or light operated flash trigger has many features. Catch those spectacular and humorous moments like that time your mother-in-law slipped on the moss covered patio and broke her neck ETI 568 October 80



ELECTRONIC METRONOME

\$16.90

Great new Metronome Circuit with low current drain (less than one milliamper) drives a Loudspeaker and a Led Indicator. EA January 82



"LE GONG"

\$14.95

The "Le Gong" Doorbell with those unmistakable chimes generated by the LSI. A must for the man who has everything! EA February 81



3 1/2 DIGIT LCD CAPACITANCE METER

Handy pocket size Digital Capacitance Meter, runs off a 9V battery and measure 1pF to 19.99uF in just three ranges.
EA March 82



\$79.00

VOICE OPERATED RELAY
\$14.95



EA's great new Voice Operated Relay can be used to control a tape recorder, as a VOX circuit for a transmitter, or to control a slide projector EA April 82

LED LEVEL METER

\$27.00

Build a Led Level Meter with simultaneous peak and average display plus 60dB dynamic range. This kit is ideal for any application requiring a wide dynamic range level display. ETI 458 June 81



DIGITAL THERMOMETER: 3 1/2 DIGIT LCD

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Measure temperatures from below freezing point to around boiling point EA February 82



FUNCTION GENERATOR \$79.50



This Function Generator with digital readout produces Sine, Triangle and Square waves over a frequency range from below 20Hz to above 160kHz with low distortion and good envelope stability. It has an inbuilt four-digit frequency counter for ease and accuracy of frequency setting. EA April 82

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You have to be in it to win it. Take the chance out of winning the Pools as well as Lotto, and build the great new Pools/Lotto Number Selector. EA July 81



LARGE SCREEN TV STORAGE CRO ADAPTER
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For a low cost Storage CRO with Synchronised Display Electronic Gatecure, One-Shot Triggering and Optional Storage of up to four Screen Displays it can't be beaten EA February 82

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\$34.50

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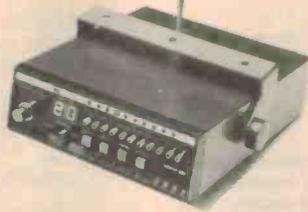


SOUNDBENDER
\$29.00

Have great fun creating your own recording effects with music and voice. The Sound Bender can receive from Electric Guitar, Microphones, etc. ETI February 82



IMARK'S MOBILE SCANNER



The Tri-Star Compu-20D scanner is different from most in that it is specifically designed to be mounted in a vehicle for mobile use. Available from Imark, it operates on the vehicle's 12 Vdc supply and is compact enough to be conveniently mounted in almost any vehicle.

While a telescopic antenna is supplied, the receiver is fitted with a Motorola-type connector on the rear to accept the normal car-type antenna lead.

The unit features a programmable PLL-type double-conversion FM receiver which covers both the VHF high and low bands, from 70.010 MHz to 84.410 MHz and from 156.010 MHz to 170.410 MHz, in 15 kHz steps. Any 20 frequencies of the 1920 frequencies within these ranges can be programmed.

The receiver is solid state for low battery consumption and uses one crystal filter and two ceramic filters to ensure excellent sensitivity and selectivity. Back-up batteries are included to provide memory keep alive of the programmed frequencies even if the power is removed.

Manual channel change and automatic scanning function, as well as a channel bypass feature, are standard equipment. A green LED display is used for channel number indication. Other features include adjustable squelch control and scanning delay function.

Further details are available from Imark, 167 Roden Street, West Melbourne Vic. 3003. (03)329-5433.

BIG-MEMORY SCANNER

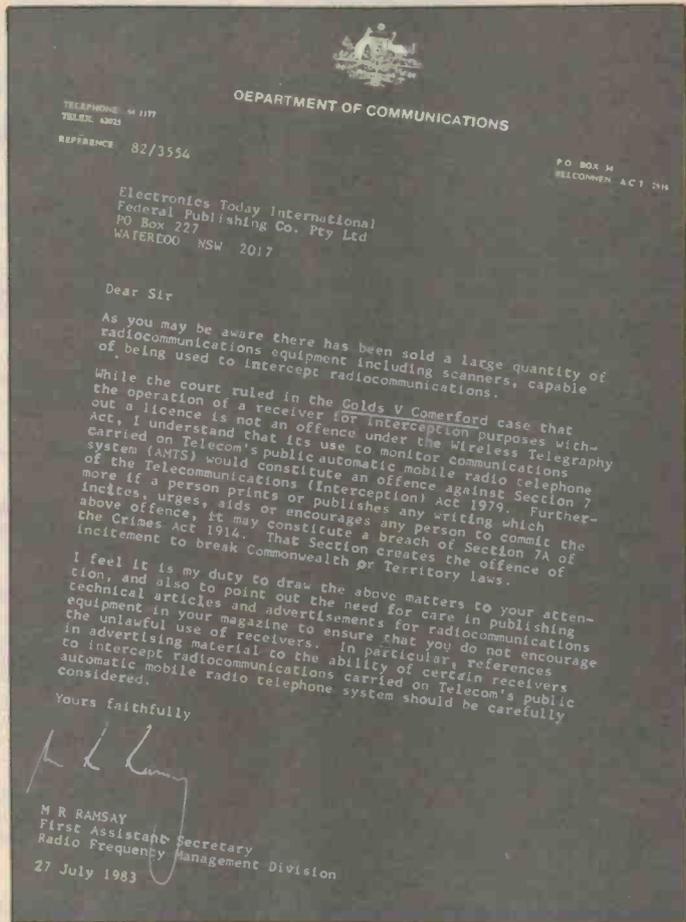


The Saiko SC7000 scanner allows you to store up to 70 channels in memory and pro-

vides coverage from 60-89 MHz, 108-138 MHz, 140-179 MHz and 380-519 MHz plus both AM and FM reception.

You can manually select any frequency or any of the memory channels, scan between preset limits within any of the four bands or scan the memory channels.

Operation of the rig is via a calculator-style keyboard. A



'priority' channel feature is included so that you can program your favourite channel or a particularly interesting frequency into memory channel 1.

The scanner holds on a busy channel for two seconds. In addition, certain channels may be 'locked out' of a scanning sequence by using the lockout.

The SC7000 can be operated from the mains (using a plugpack power supply) or from 12 Vdc. In our April scanning feature, we inadvertently attributed this receiver as being sold by Imark. In fact, it is sold through Time Plus, 55 Sydney Road, Brunswick 3056 Vic. (03)380-4942.

JIL SX-200

COVERS 26-88 MHz & 108-180 MHz & 380-514 MHz



A BETTER SCANNING MONITOR RECEIVER.

Monitors over 33,000 frequencies from 26 to 88 MHz, 108 to 180 MHz and 380 to 514 MHz. Bands included within this range are HF and UHF CB, 27 and 155 MHz MARINE, Australian LOW BAND, AIRCRAFT band, VHF SATELLITE band, 10 Mx, 6 Mx, 2 Mx and 70CMx AMATEUR BANDS, VHF High BAND as well as UHF two-way band.

Mechanically rugged the SX-200 uses high quality double-side Epoxy-Glass printed circuit boards throughout. Some of its other outstanding features include 3 MODE SQUELCH circuitry which allows the lockout of spurious and carrier only signals, extremely low spurious count, AM and FM detection on all bands, FINE TUNING control for off channel stations, 240 VAC or 12 Volt DC operation, Accurate QUARTZ CLOCK, Squelch operated OUTPUT for switching a tape recorder etc, 16 Memory channels, MEMORY BACKUP, which lasts up to two years, high SENSITIVITY and SIGNAL-TO-NOISE ratio on all bands, CRYSTAL FILTER for excellent SELECTIVITY and easy servability due to component layout as well as a 90 day warranty.

Its high quality and performance is testified by the fact that it is in use by a large number of State government and Federal bodies including most state and federal police departments. Contact GFS, the Australian Distributors, or our Interstate outlets for full technical specifications. We also market a range of pocket scanning receivers and transceivers. Contact us for full details.

PRICE \$599 INC. S.T. + \$12 P&P; SERVICE MANUAL \$12 + \$1.50 P&P; SCAN-X BASE ANTENNA \$62 + \$10 P&P; EXP-32-32 CHANNEL MEMORY EXPANDER KIT \$53 + \$5 P&P; A4-AM AUTO AM KIT FOR AIRBAND \$32 + \$5 P&P; CVR-1B CONVERTER 225-380 MHZ \$199 + \$5 P&P; CVR-2 CONVERTER 5-26 MHZ \$189 + \$5 P&P; LOG S DIRECTIONAL ANTENNA 100-520 MHZ 9e1 \$89 + \$10 P&P; LOG-SP DIRECTIONAL ANTENNA 65-520 MHZ 13e1 \$125 + \$10 P&P; INTERSTATE DEALERS: NSW: (02) 211 0531; QLD: (07) 397 0808; SA: (08) 269 4744; WA: (09) 328 4160; VIC: (03) 329 7888

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• Conditions: Name and address plus phone number (if required) must be included with the 24 words. Reasonable abbreviations, such as 25 W RMS or 240 Vac, count as one word. Adverts must relate to electronics, audio, communications, computing etc — general adverts cannot be accepted.

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140 Joynton Ave, Waterloo NSW 2017.

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FOR SALE: NAIM 42/110 MC Input \$1100. Supex 900 Super \$90, sell after Naim. Newcastle (049)51-4439.

SELL: SERIES 5000 preamp and amp (Blue-print), \$780. Pair speakers, 80 WRMS, 12" driver, piezo tweeters, \$400. All \$1100. Chris Tolley, P.O. Box 2, Renmark SA 5341. (085)85-1377.

FOR SALE: REALISTIC (Tandy) stereo bass enhancer/subsonic filter. No alterations made to unit, good condition, ten months old. New \$75, will sell for \$60 ono. T. Firman, P.O. Box 498, Cheltenham Vic. 3192.

AMPLIFIERS: SANSUI 2900 stereo integrated 25 WRMS/ch, \$55. Monarch A-5000, 40 WRMS, \$50, mint condition. (02)896-2975.

GOODMANS AUDIOM 15P, 15" bass woofers. Still in original carton. New price \$300.

AMCRON LABORATORY reference stereo power amplifier. Dc 300 A, 155 WRMS/ch, 0.01% THD. Mint condition, \$730 ono. (02)896-2975.

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FOR SALE: AWA radio equivalent to AR7 in rack, handbook, spare valves, ac power supply, complete set of coils, \$25 ono. (02)427-2326 evenings.

FOR SALE: COLOUR TV game. Ten games, joystick controls, volume control, \$20. (03)277-6987.

SELL: FRONT-WHEEL drive R/C car C/W radio, batteries, fast charger, spares, electronic speed controller. Very little use. VGC, \$240. (03)857-7463 ah.

FOR SALE: WIRELESS WORLD back issues 1946 to August 1983. Almost complete, best offer. (03)589-1511 ah.

FOR SALE: HEATH oscilloscope, model no. 10-4105. Mint condition, \$700. (08)250-4776 ah.

WANTED: ANY BOOKS containing circuit diagrams or information on radios made before 1949. (02)524-8082.

FREE: ONE model 15 teletype plus handbook. Good working order, just come and get it. R. Watters, 33 Captain Cook Drive, Willmot NSW 2770. (02)628-9187.

MANUALS WANTED: CBS710, B&K1503/1602, Taylor 45D, Haltronics 201B, Khan SP58-1A, AWA Voltomyst, AWA 1A57321, MAGNA-TECH 34B, PULTEC EQP-1A/MEQ5. GMT 303. R. Hibberd, P.O. Box 318, Willoughby NSW 2068. (02)406-5782.

WANTED: CIRCUIT diagram for Fluke differential dc voltmeter model 801. (02)92-4025.

COMPUTERS

FOR SALE: 48K SYSTEM 80MKII, green screen, printer, one disc drive. Used six months, half price at \$1100. (02)440-8428.

MICROBEE GAMES: Lunar Lander with inputs of time, thrust and angle, and Golf. Both feature hi-res graphic. \$6 each. Both \$10. Chris Dalitz, 12 Paperbark Close, Wyoming NSW 2250.

SELL: SINCLAIR SPECTRUM 16K, BASIC, manuals, power pack, printer, games tapes, \$450 ono. Tony Andrews, International House, Uni of NSW, Kensington NSW 2033.

FOR SALE: ZX81 (two available), as new, \$110. ZX81 16K RAM pack, \$100. Tony, 14 Wulagi Cres, Wulagi NT 5793. (089)27-5539.

FOR SALE: \$100 16K static memory board. Suits DGZ80 CPU, \$70 ono. TI LCD programmer, \$50. Jurgen Rochelmeyer (02)487-1816 ah.

APPLE II PLUS compatible computer: 48K RAM, all standard Apple features plus upper/lower case, RF modulator and handbook, \$650. Disc drive and interface, \$500. Will separate. Sth Melbourne (03)699-8844.

FOR SALE: TRS-80 Model 1 cassette test editor. Bank cheque \$10 payable to Mr E. Hughes, 52 Lowry St, Cardiff NSW 2285.

FOR SALE: SORCERER 32K MK1, with monitor, cassette and many tapes. Excellent condition, \$800 ono. K. Lakeman (02)74-9040.

FOR SALE: DREAM 6800. 4K RAM, 3K ROM, Dreamsoft expansion board, Soundex, joystick, ASCII keyboard and model 15 tty, cassette software. Price negotiable. Jim McCabe (062)88-2768 ah.

APPLE GAMES to swap, many good games in stock, over 30 available. Good titles such as Sneakers, Flight Simulator, Wizard, Alien Rain and Apple Panic etc. (02)412-2352.

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FOR SALE: FLOPPY discs. 10 brand new unopened Verbatim, single-sided, double-density, 40-track, 5¼" mini-floppy discs for \$25. (02)516-9528 bh.

FOR SALE: SORCERER computer, full 56K RAM, 8K BASIC ROM pac, \$700. (02)633-4915 ah.

ACT BIMONTHLY VIC-20 newsletter. August issue \$1.50. Subscriptions \$8 per year. Write to Chris Groenhout, 25 Kerferd St, Watson ACT 2602.

FOR SALE: NEW AMERICAN video terminal with technical and operator's manuals, separate keyboard, \$450 including delivery. J. Solomon, 16 Lennox St, Glenbrook NSW 2773.

SELL: Chip-8 editor for '660. Inserts, deletes, etc., GOTOs etc. Adjusted. Listing and instructions \$8. Tim Parish, 10 Rodda Rd, Myrtle Bank, Adelaide SA 5064.

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Built and tested

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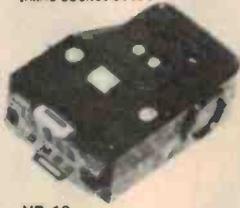
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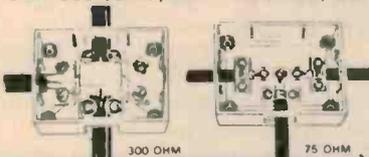
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I'M SICK of hearing about that bug-eyed, skinny-necked extraterrestrial. His bumbling shuffle as he blundered his way around this planet, rasping out a few words, seems to have captured the imagination of thoughts-less earthlings.

But I think he was a fake. He couldn't even ride a bicycle. You've probably heard that 'real men don't eat quiche' and now I'm told that 'real women don't pump gas'. Well, I know that real extraterrestrials don't phone home. How they manage to get back home is beyond me.

And speaking of what real people do, which I wasn't, but just so we know who is really for real. 'Real programmers' can't even spell quiche, unless it's in hexspell.

Real programmers don't read 'Creative Computing'.

Real programmers read 'Byte'.

Real programmers don't jump out of FOR...NEXT loops.

Real programmers don't read the manuals - it takes too much time.

Real programmers solve 'adventure' games by disassembling the program.

Real programmers have messy desks.

Real programmers don't wear suits (except to interviews).

Real programmers patch object code rather than recompiling.

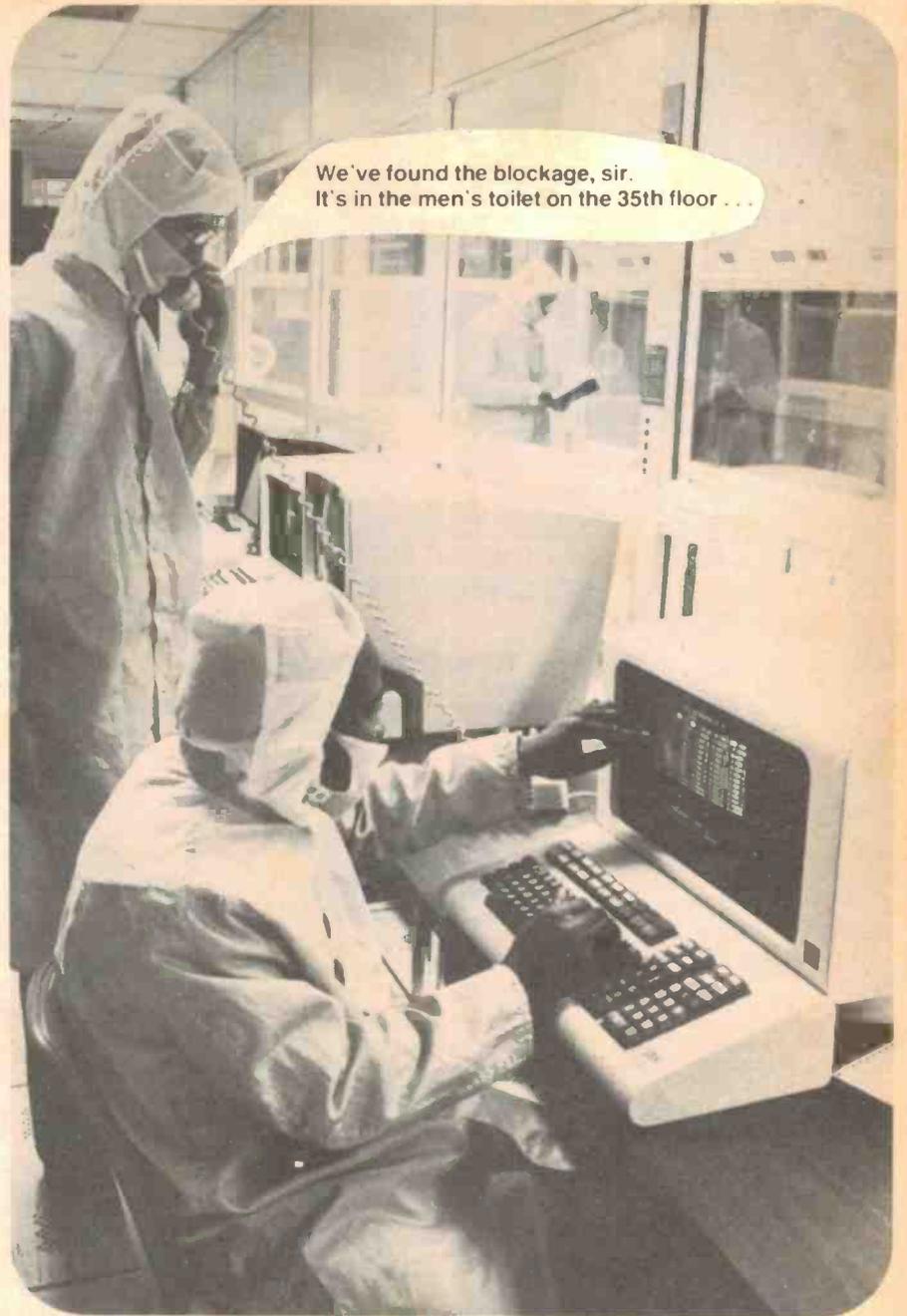
Real extraterrestrials probably don't eat quiche either. And if they drink beer, they shouldn't.

Since this is for real, I'd like to know what is a 'real bug'. 'Real bugs' don't live happily at a temperature of 250° C. Or so I thought until I read about certain bacteria which have their home in the output of sulphurous, hydrothermal vents deep in the floor of the east Pacific Ocean.

At 250° C these bacteria will still grow, beating by a comfortable margin the record of 105° C set by another heat-loving strain.

So what can one do with a hot bug? Throw away your old hotwater bottle and take a hot bug to bed instead, to keep you warm on those cold, winter nights. 'Well, I'll be' could have a whole new meaning.

Instant hot drinks, just add a hot bug to your cold cup of tea or coffee. Save on your heating costs during winter, scatter a few hot bugs around your home or office.



Scuba divers wouldn't have to freeze in that cold current; warm diving could be guaranteed all year by slipping a few hot bugs down one's wetsuit and they (the bugs) should be happy in their natural environment. But hot bugs trapped between one's skin and the wetsuit could lead to a ticklish situation. Or even worse, hysterical bugs out of control.

Out-of-control hot bugs. 'Breeder reactor' could have an entirely new meaning if a few hot bugs took a fancy to each other. The fundamental laws of physics would have to be rewritten - energy can be created - all that is needed is the fusion of two hot bugs to create an increasing supply of energy.

Electronic eavesdropping devices would be outdated by big-eared bugs. These microscopic bugging devices would be invaluable in the foreign service, especially in cold countries like Russia. With a temperature of 250° C they could easily tunnel through the ice and snow.

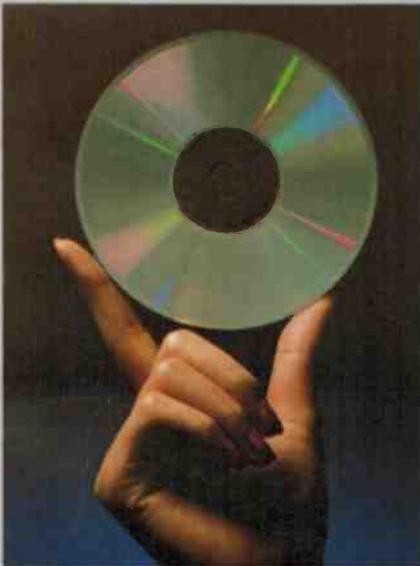
I knew I'd find some association between bugs and electronics. As we all know, the biggest problem with a circuit is trying to get the bugs out of it so that it will work. And debugging a computer program is not everyone's idea of fun. But now the discovery of volcanic bugs has erupted in our lives we have a better idea of the size of the problem; small but too hot to handle.

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Sony's CDP-101 uses an optical laser pick-up (incorporating three micro processors), it is easier to use than a conventional turntable and connects easily to your existing system.

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- flat frequency

- automatic music sensor • dual function digital readout of playtime • audible fast forward and reverse • 10 function wireless remote control.

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CDP-101 Specifications

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Harmonic Distortion	less than 0.004% (at 1kHz)
Wow and Flutter	immeasurable



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