

ELECTRONICS

Australia

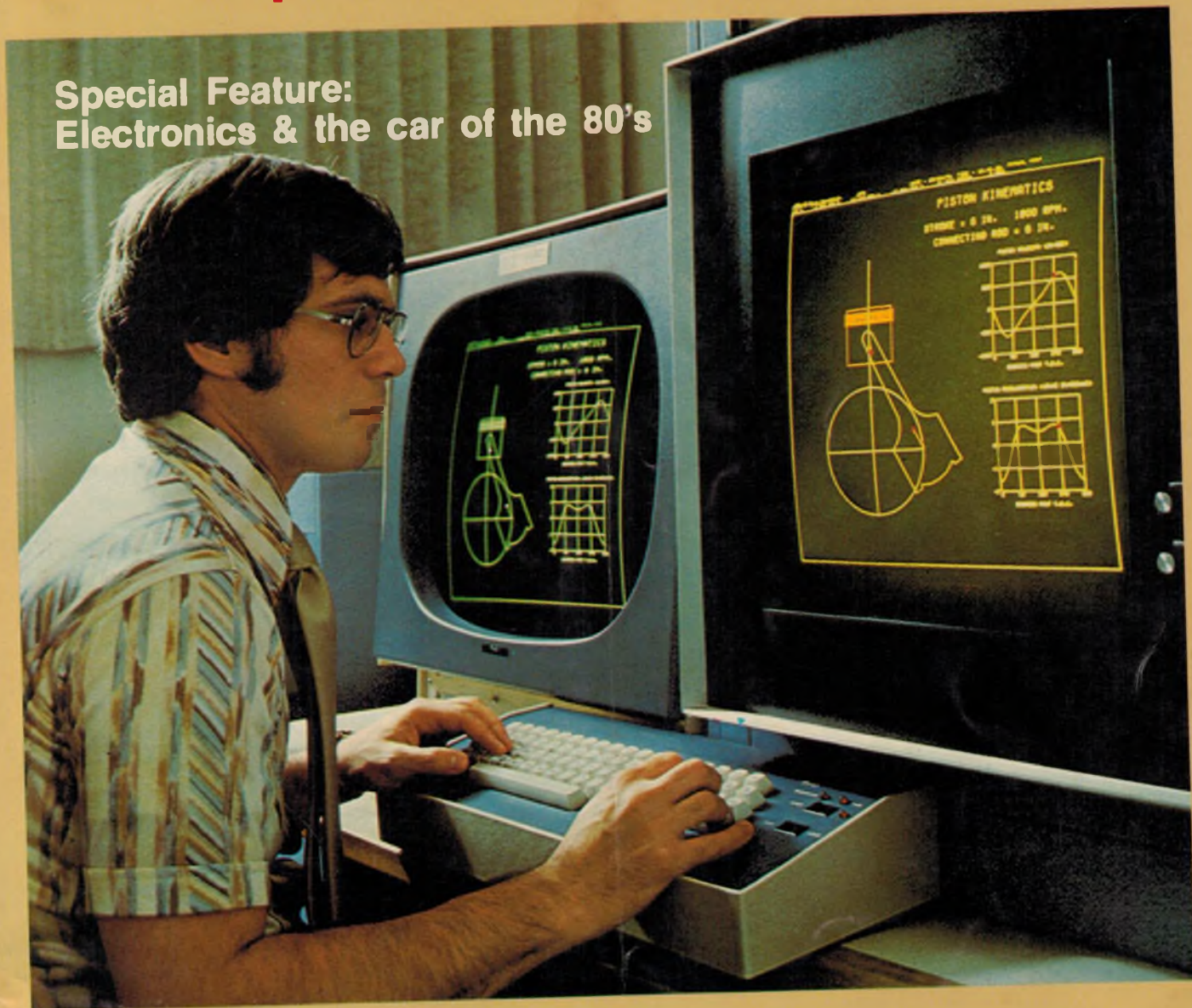
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FEBRUARY 1980

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Technics

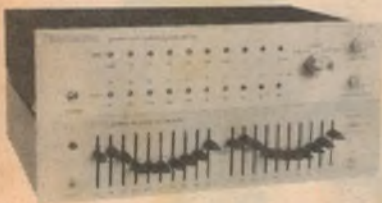
ELECTRONICS

Australia

Volume 41 No. 11

February, 1980

Australia's largest selling electronics magazine



Designed around 13 low-cost ICs our new Playmaster Graphic Analyser matches any equaliser and has a built-in pink-noise generator and microphone for monitoring loudspeaker and room response. It can also function as dynamic display of amplifier power output or signal level. Full details on p50.



Combine this super-bass filter with a separate amplifier and super-woofer loudspeaker and you'll get bass that you can feel. Details on p42.

COMING NEXT MONTH! — Find out what's coming by turning to p34.

On the cover

A Chrysler engineer in Detroit uses a colour graphics terminal to analyse piston performance. Computers will play an extremely important role in designing and controlling the new generation cars of the 80s (see p14). Photo courtesy Control Data Corporation, Minneapolis, USA.

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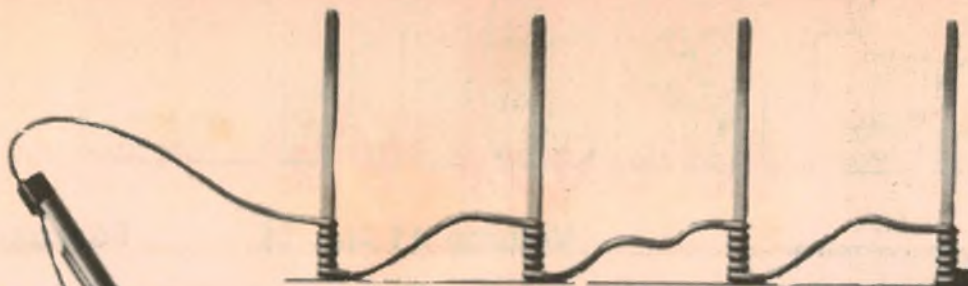
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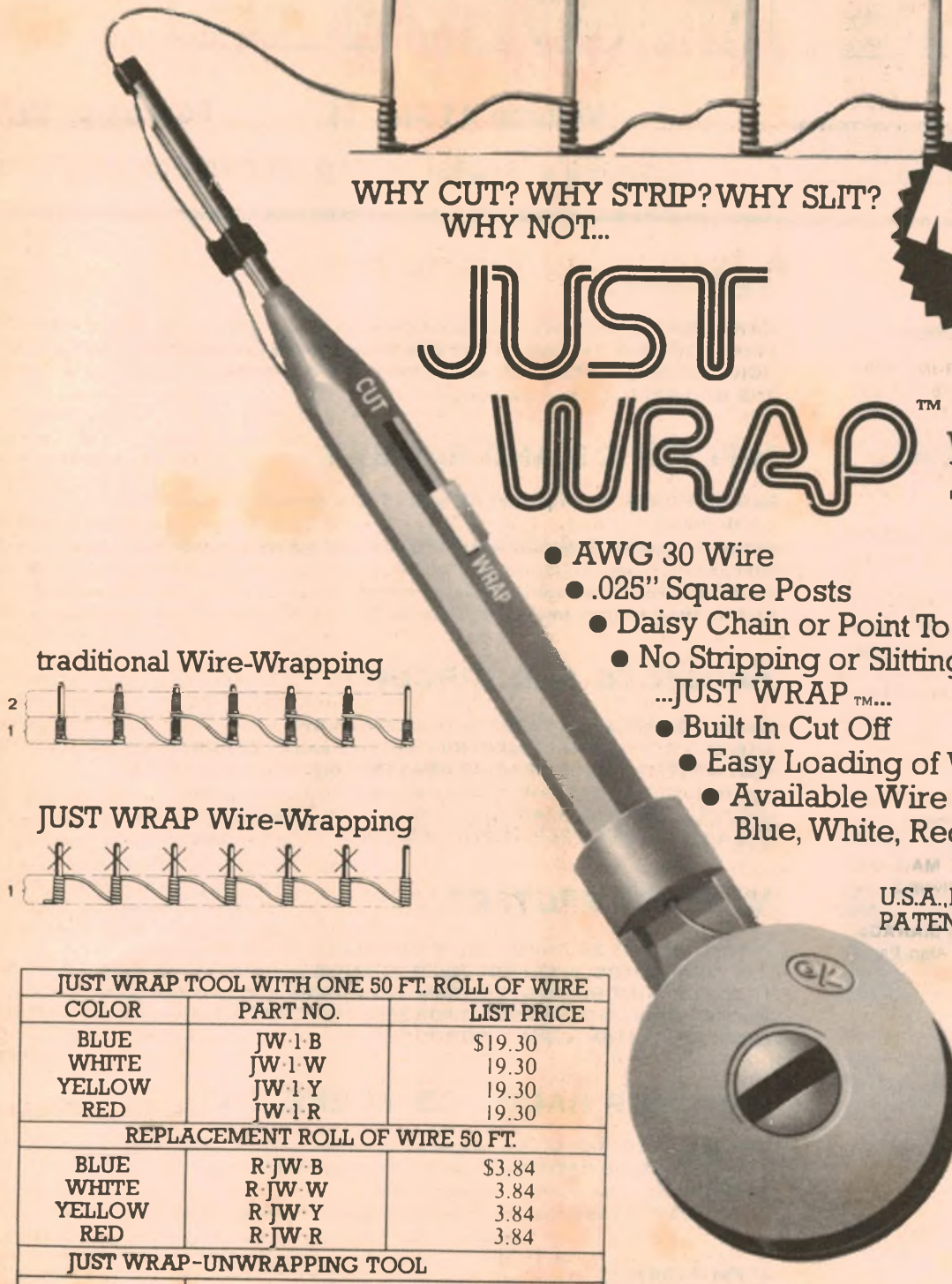


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NEW

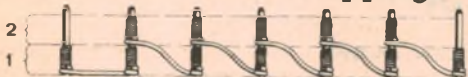
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Editorial Viewpoint

A fascinating future, but . . .

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Seen from the editorial chair, each new decade has had its own special interest. The 40's were dominated by World War II, with its tensions and its tragedies. But it was also a period of tremendous technical development, judged on the standards of the day.

The 50's brought peace and the exciting prospect of applying wartime technology to more personal ends. While amateurs and experimenters picked their way through a mountain of disposals gear, industry turned its attention to a new generation of radio receivers, to television and to electronics in the broader sense.

With the 60's came the full challenge of solid-state technology, and the opportunity — indeed the necessity — to re-think and up-date virtually everything electronic, from portable radios to elaborate commercial and professional equipment.

That process continued into the 70's with ever-increasing momentum. But this last decade will surely be remembered as the one which saw the emergence of the computer, the calculator, the microprocessor, and a whole range of digital technology to threaten the analog way of doing things.

What lies ahead for the 80's is nothing short of breathtaking: multi-channel, superquality digital discs and players, long-playing video discs and video cassettes, highly sophisticated communications equipment, satellite and cable television, personal and domestic computers, and so on, without even mentioning educational, commercial and professional products.

But, exciting as it may seem, the 80's may become notable as the decade in which technological achievement outstripped human need — or inclination. How much music can we really cope with, no matter how "perfect" the system? How much time can we really devote to video, no matter how wide the choice of subjects? What real use can we make of a parlour full of TV games, or communications devices, or computer-like gadgetry? Surely we're in danger of becoming a nation of adult children, oversupplied with sophisticated toys — most of them imported.

For sure, entrepreneurs, advertising people and sales reps. will have truckloads of "goodies" in the 80's but they may well discover a new kind of sales resistance, having much in common with the environmental movement. When you've had your fill of gadgets, it's amazing how much satisfaction you can rediscover in simply doing your own thing — playing a musical instrument, reading a book, building a rock garden, or just walking in the bush!

Neville Williams

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News Highlights

Voice recognition device controls colour TV set

Sanyo Electric has developed a voice recognition device capable of controlling a domestic colour TV set and other consumer electronic appliances. While existing voice recognition devices have been mostly based on minicomputers, the new device is based on an 8-bit microprocessor.

The recognition performance averages 95% which, according to Sanyo, is good enough for effective control if the applications are selected intelligently.

Control functions include power supply on/off, volume adjustment and channel selection. The command is composed of two words. For example, "television power" switches the power supply on or off, and "channel 8" selects channel 8.

The volume is controlled by selecting one of 10 levels and issuing the appropriate command, eg "volume 4".

Sanyo has yet to indicate the likely cost and whether the system will be marketed commercially.

Power stations in space

Britain is to seek a major role in the plan to establish giant solar power stations in space.

The UK Department of Industry has revealed that it had placed a \$200,000 contract with a group of companies to study the idea of using the sun to power the national grid. The group is headed by the British Aerospace Space Centre at Bristol, and includes the Marconi Space and Defence Systems Company.

British Aerospace engineers have already studied plans to develop solar arrays capable of producing up to 500kW of power. It is thought that a series of these could be linked up to produce a space station with an output of up to 2MW.

The solar panels of such stations would cover many square kilometres and be assembled in space from basic units and materials transported from Earth by the Space Shuttle, now being completed in the United States.

The massive solar power satellites would be put into geostationary orbit some 36,000km above the equator, where they would continually convert the Sun's rays into electrical energy. This energy would then be transmitted to antenna "farms" on Earth by microwave radiation.

RAAF tests laser bomb guidance kits

The RAAF recently conducted a series of tests to evaluate the effectiveness of laser bomb guidance kits. The kits are manufactured by Texas Instruments for the US air force.

Specially wired Mirage III test aircraft of the Aircraft Research and Development Unit (ARDU), based at the Edinburgh AFB, South Australia, conducted a series of carriage and release trials at Woomera to provide the RAAF and specialists from the Defence Research Centre with first hand information on the capabilities of this important area of modern weapon technology.

The laser-guided bomb (LGB) is a highly accurate weapon which homes

onto laser energy reflected from a surface target designated by either a soldier on the ground or an airborne FAC (Forward Air Controller).

Although there is no immediate indication of the RAAF acquiring airborne laser designators for FAC aircraft, the Australian Army is already equipped with several laser devices.

The tests to prove the feasibility of fitting LGBs to the Mirage are closely related to the RAAF's intention to maintain the Mirage in its inventory for another decade. Local production of the laser-guidance kits would have significant potential for Australian industry involvement.

COMBINED AM/FM RADIO, CALCULATOR & CLOCK

Sanyo has released a combination AM/FM radio, clock, and calculator, all combined in a package only 161mm high, 65mm wide, and 18mm thick.

The clock has an alarm function, using either a buzzer or the radio. The clock and calculator use LCD readouts, giving low battery consumption and good daylight visibility. Both are powered from two C-13 cells.

The radio delivers 100mW of audio power to a 45mm diameter speaker, and operates from two type AA cells. It is fitted with a small telescopic aerial.

Recommended retail price is \$124.00. Further details from Sanyo Australia Pty Ltd, 225 Miller St, North Sydney, NSW.

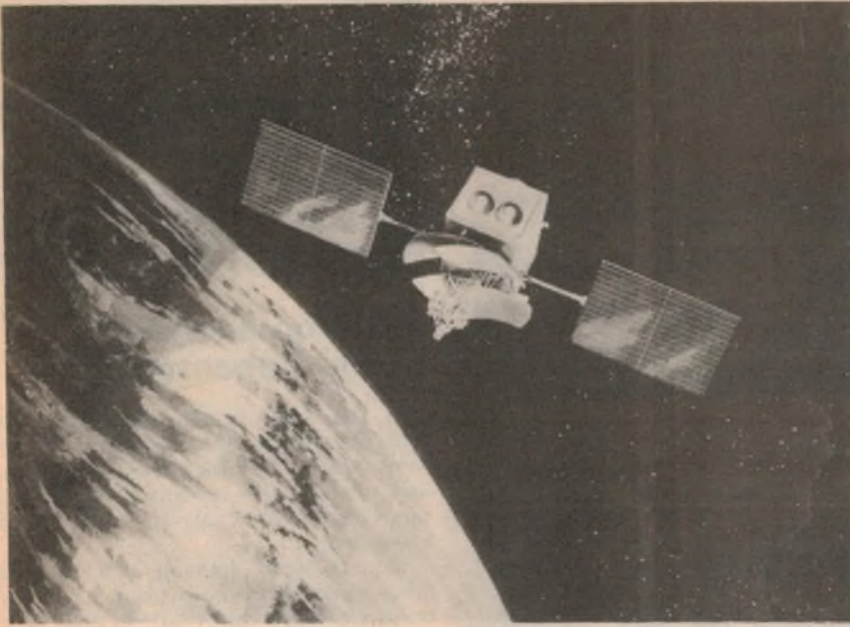


RCA to market video disc player

Latest news on the video disc front is that RCA has finally launched its version onto the US market. The RCA system user capacitive pick-up as distinct from the rival Magnavox-Philips system which uses a laser. It remains to be seen which system will ultimately capture the public's attention, or whether the two systems can exist side by side.

RCA plans to back its player with an array of about 300 disc titles, with plans for additional titles to be added at between 10 and 15 per month for the first year. The latest version of the RCA player has been reduced in weight compared with the original concept, but the price has risen from under \$US400 to around \$US500.

\$20 million satellite lost in space!



Artist's concept of RCA's Satcom III, lost in space shortly after its launch from Cape Canaveral on December 6. The \$US20 million communications satellite disappeared from tracking screens just 15 seconds after a booster motor was fired and may have exploded according to space officials.

Britain facing TV invasion — Sir Harold warns

Sir Harold Wilson, Britain's former Prime Minister, has warned that the development of satellite relay systems for TV programs poses a threat to the British TV industry — particularly ITA's advertising revenue — by allowing European TV systems easy access to British audiences.

Speaking in an Opposition debate on TV licences, Sir Harold said that this type of viewing was now a real possibility. Continental broadcasters were planning £100m satellites, each of which could earn advertising revenue of £150m in the first year.

A space TV system could be beamed to nearly every home in the land and by 1984 satellites would be a real force. A small dish type aerial in the loft was all that was needed to receive signals.

"We have received evidence showing maps of Europe and the areas which could receive such programs," Sir Harold explained.

"It is clear that programs from Continental satellites will cover the whole of Britain."

Magnetic bubble memories from TI

A new family of physically and electrically interchangeable magnetic bubble memories with the largest capacity device having one-million bits of storage has been introduced by Texas Instruments Incorporated.

Bubble domains for all the new memories are two-microns in diameter. Access time for the megabit bubble memory is 11.2 milliseconds, twice as fast as a previously announced megabit bubble memory.

The first two devices — to be available as board-level systems — are the TIB1000, a binary megabit device organised as 512K x 2, and the TIB0500,

a half-megabit device with 512K x 1 organisation. A binary quarter-megabit device, compatible with the two larger devices, will be made available later in 1980. The family approach will allow designers to vary system storage capacity by interchanging the bubble devices.

All members of the new bubble memory family are packaged in a 24-pin 3.3 x 3.56cm package with pins on 2.54mm centres. The devices use the same support circuits, including the TIB0903 monolithic custom controller, TIB0804 coil driver, TIB0953 function timing generator, TIB0833 sense amplifier and TIB0863 and TIB0883 function drivers.

Steam power set for a comeback

Britain's Overseas Development Administration (ODA) believes a new age of steam could be one answer to the present dependence of developing countries on costly imported fuels and technology.

With this in mind, the UK Intermediate Technology Development Group has joined forces with the Department of Engineering at Reading University, near London, in a 14-month program to design and develop a small-scale steam electricity generating system in the 5-50kW power range.

Under the \$60,000 project being funded by ODA, a market survey will be carried out to evaluate the potential

use of steam for agricultural duties such as milling and water pumping, and as an electric power source for domestic users and small industries in rural areas. This will be followed by a design study on a steam-driven electricity plant that has low maintenance costs and above all can be built and operated locally in any country.

Interest is also being shown in the possibility of introducing steam trains using a new form of fluidised-bed combustion which is promising to revolutionise coal-fired power stations. This form of pollution-free combustion burns a variety of different fuels on a bed of ash or sand.

VLSI devices in doubt for space applications

The future of very large scale integrated (VLSI) devices is somewhat uncertain at present, as far as space applications are concerned, due to the likely risk that cosmic radiation could cause both device failure or momentary device malfunction.

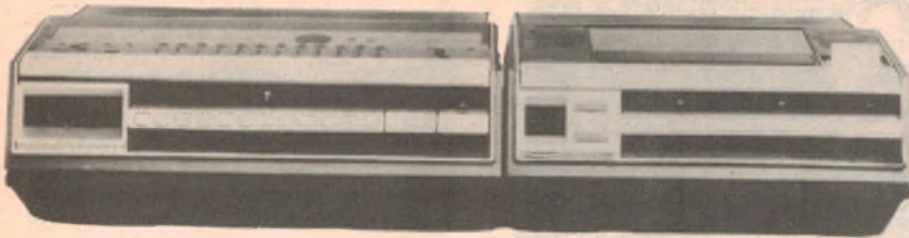
The degree of risk is not yet clear, although some researchers are claiming that the devices should not be used until a major breakthrough provides a much higher order of protection. Other authorities claim, however, that the risk of error or total failure is small, and can be allowed for by employing proven error correcting techniques and built-in redundancy.

Skid warning system for motor cars

Alfred Teves, Frankfurt, Germany, one of Europe's largest motor car brake manufacturer's, has announced development of a system to warn drivers of the risk of skidding on a wet road. Sensors mounted on the wheels sense changes in rotational speed which indicate that the wheel is about to lose its grip on the road.

The information is directed to a central system, no larger than a cigarette package, which can operate an acoustic or optical warning system to alert the driver. The firm is about to submit samples to various vehicle manufacturers for appraisal.

Single head, high speed VTR — a new concept from BASF



Yet another home video recording system has been added to the market, this time by BASF of West Germany, making a total of five non-compatible systems competing for public approval. Initial marketing is to begin by mid-1980.

Called the Longitudinal Video Recording (LVR) system, it features a single fixed head of relatively simple design. The tape is of chromium dioxide, 8mm wide x 8.5µm thick x 600m long, and is housed in the world's smallest video cassette (114 x 106 x 17mm). It moves across the head at a rate of 4m/s.

After each pass, the head steps to the next of 72 tracks recorded on the tape and the tape direction is reversed — all in a period of 100ms. Playing time is three hours.

Among the advantages claimed by the makers are ease of access to any recording on the tape, and ease of tape duplication. Each track lasts for 2.5



minutes so any part of the recording is available in less than this time by selecting the appropriate track. A track number indicator is provided.

Duplication is simplified because all 72 parallel tracks can be copied simultaneously in one pass through the copying system.

For further information contact Mr N. Price, BASF Australia Ltd, 55 Flemington Road, North Melbourne, Vic 3051.



Raindrop analysis on the Concorde!

In the time it takes to read this sentence this British camera could take some 2500 million pictures of the structure change of a specimen inside this vacuum chamber at the Rutherford Laboratory.

The Hadland Imacon 675 camera takes over 600 million frames per second. It is so fast that it will take "streak" photographs that can detect a change over a period of less than five picoseconds.

The camera's speed makes it able to solve a wide range of problems. These include the progressive recording of crack propagation in solid materials such as glass, rock and metals, providing records for ballistic tests, aiding the study of spark discharges and surface flashover on conductors and for work with lasers. A camera similar to this one was first used to study the effects of raindrops on the windscreen materials chosen for the supersonic Concorde airliner.

Further information from John Hadland (Photographic Instrumentation) Ltd, Newhouse Laboratories, Newhouse Rd, Bovingdon, Hemel Hempstead, Hertfordshire HP3 OEL, England.

Business Briefs:

National Semiconductor Corporation and Intel Corporation have signed an agreement transferring Intel's computer marketing and service operations in Australia and New Zealand to National, as from January 1, 1980. Under the agreement, National will market Intel's current range of medium to large IBM compatible computer products.

Multi-Contact Australia has announced the appointment of two new distributors: Halley and Mellowes Pty Ltd, 20 Gault Rd, Belair, SA 5052; and Martin de Launay Pty Ltd, King & Darby Sts, Newcastle, NSW 2300. Multi-Contact handle the range of Tschudin and Held products, as well as high current connectors, laboratory components, switchgear and relays.

A 550 page comprehensive directory of **CSIRO research programs** is now available. The directory contains descriptions of all of CSIRO's 700 research programs and sub-programs and includes details on location, staff and expenditure.

Copies of the book, titled **CSIRO Research Programs 1979-80**, are available at \$10 a copy (postage included) from the CSIRO Editorial and Publications Service, PO Box 89, East Melbourne, Victoria, 3002.

National Semiconductor Corporation, California, has announced a \$50 million credit agreement with five American banks and two foreign banks. The loan is for three years, with a further four years option. The loan will be used for working capital and general corporate purposes.

One-board Teletext & Viewdata decoder

Expansion of the British Teletext and Viewdata systems beyond the current "experimental" stage has been brought a step nearer by the development of a single printed board containing all the necessary circuits to decode these signals. The board is based on a microprocessor and measures just 100 x 150mm.

Made by General Instrument Microelectronics, the system is to be known as **Televue** and is described by the company as being sufficiently cost effective to attract manufacturers of add-on equipment, as well as the television set makers, once quantity production levels have been reached. Significant performance advantages over existing dedicated Viewdata or Teletext systems are claimed.

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Matrox ALT 512** (512x256)
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NEWS HIGHLIGHTS

The menace of gasoline!

We came across this gem in a recent copy of "Atom" (published by the UK Atomic Energy Authority). It's from the "US Congressional Record" for 1875:

"A new source of power, which burns a distillate of kerosene called gasoline, has been produced by a Boston engineer. Instead of burning the fuel under a boiler, it is exploded inside the cylinder of an engine. This so-called internal combustion engine may be used under certain conditions to supplement steam engines. Experiments are under way to use an engine to propel a vehicle.

"This discovery begins a new era in the history of civilisation. It may

some day prove to be more revolutionary in the development of human society than the invention of the wheel, the use of metals, or the steam engine. Never in history has society been confronted with a power so full of potential danger and at the same time so full of promise for the future of man and for the peace of the world.

"The dangers are obvious. Stores of gasoline in the hands of the people interested primarily in profit would constitute a fire and explosive hazard of the first rank. Horseless carriages propelled by gasoline engines might attain speeds of 14 or even 20 miles per hour. The menace to our people of vehicles of this type

hurtling through our streets and along our roads and poisoning the atmosphere would call for prompt legislative action even if the military and economic implications were not so overwhelming. The Secretary of War has testified before us and has pointed out the destructive effects of the use of such vehicles in battle. Furthermore, the supplies of petroleum, from which gasoline can be extracted only in limited quantities, make it imperative that the defence forces should have first call on the limited supply. Furthermore, the cost of producing it is far beyond the financial capacity of private industry, yet the safety of the nation demands that an adequate supply should be produced. In addition, the development of this new power may displace the use of horses, which would wreck our agriculture. "... The discovery with which we are dealing involves forces of a nature too dangerous to fit into any of our usual concepts."

Automatic radio telephone system

The British Post Office has announced plans to introduce an improved radio telephone system for private vehicles in the London area. Installation is expected to commence in May 1980 and to be completed by mid-1981.

The new system will supplement, rather than replace, the present manual operator system. This currently provides for 3500 subscribers and suffers from the disadvantage that calls must be booked with the operator, who then directs the caller to a vacant channel.

By comparison, the new system is completely automatic. The mobile telephone is equipped with a push-button type dial with which the subscriber simply dials the number he wants — to any of Britain's 25 million telephones. Also, the new system provides a full duplex circuit; it will no longer be necessary to use the press-to-talk technique.

VW to purchase Hall-effect sensors for ignition timing

Honeywell's Micro Switch division in Freeport, UDS, has signed an agreement with Robert Bosch GmbH, West Germany, to supply 1980 Volkswagen cars with Hall-effect ignition timing sensors. Similar Hall-effect sensors, which replace the mechanical breaker points, have been supplied by Micro Switch for use in Chrysler's Omni and Horizon cars since 1977.

New microscope 'sees' atoms

A new 600kV high-resolution electron microscope (HREM), built by scientists and engineers at Britain's Cambridge University, will enable researchers to see individual atoms for the first time.

The microscope has already produced some outstanding results including an image of a gold crystal magnified seven million times ... at the same degree of magnification a man would look as big as the earth. The image clearly shows rows of gold atoms — some of the smallest objects yet shown on an electron microscope image.

The microscope will be used to examine a wide range of materials to gain a better insight into their structure and, more importantly, their defects. This will help scientists to understand their behaviour as materials.

At present the researchers have mainly inorganic samples in mind, although the microscope could be used to study the structure of organic molecules. To do this it would be



necessary to solve the problem of the barrage of electrons that illuminate the sample breaking the weak bond that holds organic atoms together.

Britain plans major television expansion

Britain's Independent Broadcasting Authority (IBA) has announced major expansion plans for the country's television network. The IBA aims to have 30 high-power transmitting stations for the new "Fourth Channel" colour television network completed and ready for simultaneous launch in all ITV regions (except the Channel Islands) by November 1982.

From the outset, the Fourth Channel

will be available to over 80% of the population of the United Kingdom — more than 40 million potential viewers. An additional 18 stations will join the network during 1983 and 1984.

Contracts totalling more than £16 million have already been awarded by IBA to Marconi Communication Systems Ltd and Pye TVT Ltd for supply and installation of the 48 new UHF transmitters.

Information at the press of a button

Car computers

— new electronic know-it-alls

by BILL HAWKINS

These new car computers give instant readouts of fuel consumption, distance to go, time of arrival, and more — all at the push of a button.

You've been on the road for hours. The clock says you're running late, the gas gauge says you're running low. And there's a desolate stretch of highway ahead between you and your destination. Should you take the extra time to look for a gas station or do you continue, hoping the lonely roadway is shorter than your fuel supply?

Messy situation? Not for an onboard computer. Just push some buttons and digital readouts will tell you how many miles you've got to go, how long it will take and how much fuel you'll have — if any — when you get there. And it's accurate. The answers are based on information from electronic sensors placed under your hood that monitor your speed, gas consumption, mileage, and more.

If this sounds like something out of the 1980s, you're dead right — these add-on black boxes are available in the US now and you can install one yourself. Prices vary — from \$US160 to \$US350, depending upon what the unit will do and the features it has. One, the CompuCruise, does everything but steer; you push a button and it automatically brings you up to the right legal speed to arrive at your destination on time. Another, the Prince, is CB-oriented: punch in mile markers along the highway and it alerts you to an accident, detour, or Smokey (police, in CB language) a mile before you get there. Still a third unit, Avantar, doesn't really "compute" at all. It's designed for the car buff who wants to know precise information such as rpm and oil temperature. Using the data it supplies, however, you can accurately figure out your ETA (estimated time of arrival) yourself.

The idea of a car computer isn't new. A year ago, Cadillac began to offer a true digital (on-off pulses) computer as

an option. But at \$US875 — attached to a \$US16,000 car — the gadget was only for big spenders.

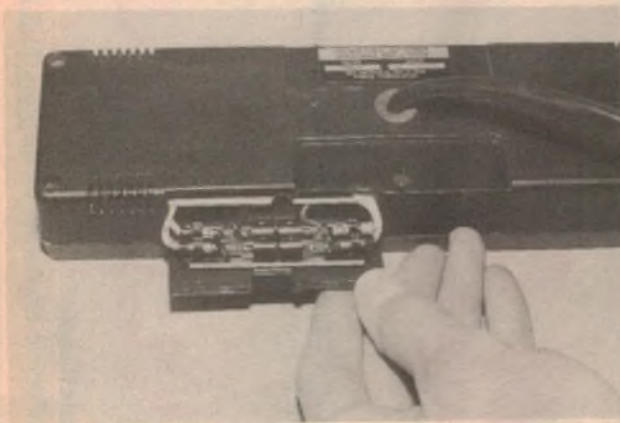
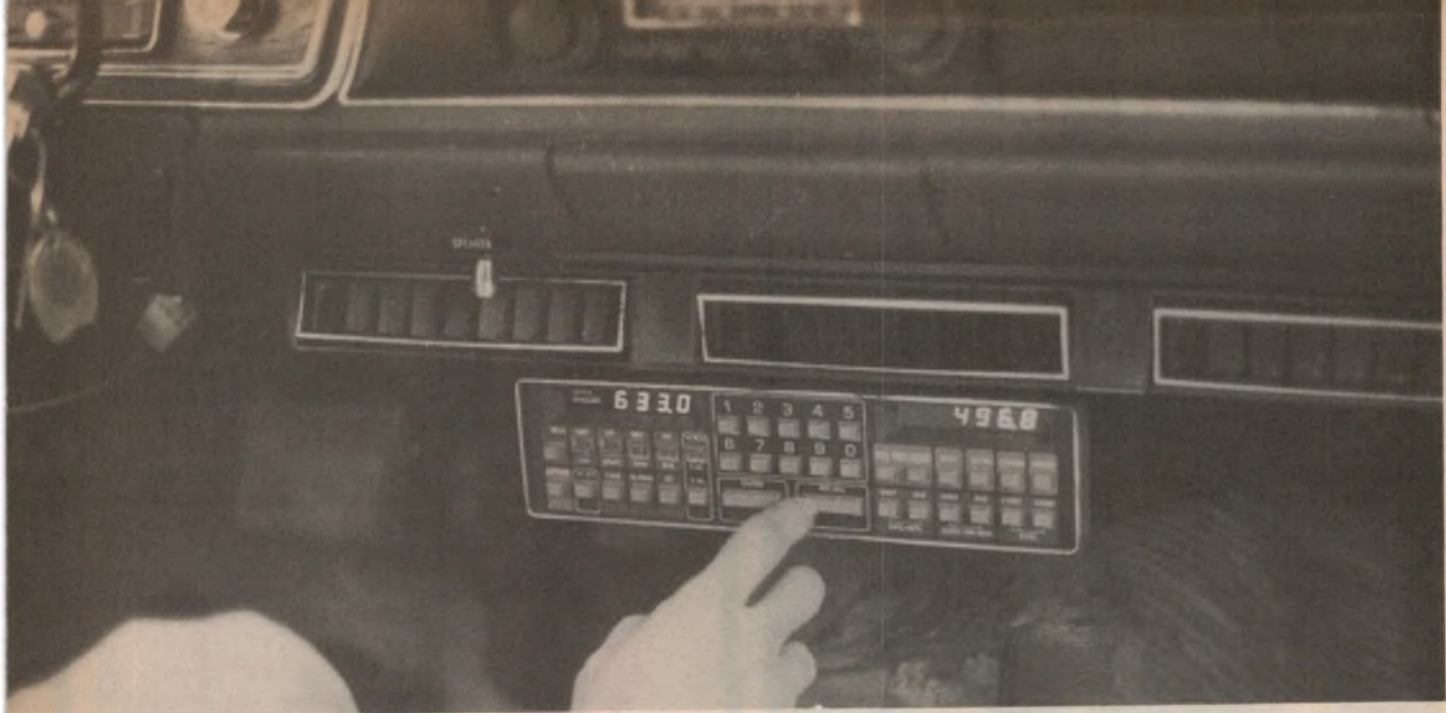
Not so for the new generation of car computers. Their lower cost, ease of installation, and dependable accuracy could make them the hula hoop of the add-on industry for autos and vans.

How they work

As you drive, things are happening under the hood that relate to your exact position. When you step on the gas, fuel flows, increasing with engine rpm. The engine turns the transmission, and the transmission turns the wheels un-

der you. You begin to move and, through it all, time is passing by. Just how far you move — distance — will depend on your speed — rate — and how long you've been travelling — time. The old equation — Distance =





Installation is not difficult, but usually takes several hours. Plug-in cables run from dash, through fire wall, to sensors mounted throughout the engine block. These systems are virtually maintenance-free except, possibly, for changing one of the bulbs used to backlight keyboard panel.

Rate x Time — holds for new computers, too. The trick, however, is in measuring these numbers.

These systems use microprocessors, tiny computers on a single integrated circuit chip that can be programmed to step through any sequence of commands: add, subtract, save data, display the results. But digital computers require single pieces of on-off pulses (bits) to work. A spinning crankshaft hardly conforms to this requirement, so transducers (sensors) are used to convert the mechanical motion into a usable electric signal.

The most important sensor is called the speed transducer (although its output is used to represent distance, not speed). It's basically a coil of wire and a magnet. In the Compucruise system, four magnets glued and taped to the driveshaft are used; the coil mounts nearby on the underside of the car. The Prince system puts the magnet and coil in one package, which splices into the speedometer cable. The idea and results are the same: As you move, the cable or crankshaft turns, allowing a magnet to pass in front of the coil. When it does, a small voltage pulse is induced in the coil, representing a full

or partial turn. Since the crankshaft and odometer cable revolve in proportion to the movement of your car, a specific number of pulses will represent a specific distance.

How much distance? That depends on such things as the rear-axle ratio and tyre size. But that's where the computing power of the microprocessor comes in: before using any of these systems, you make a simple calibration. At the beginning of a measured mile, you push a button. That tells the computer to begin at zero. Then, as you travel the mile stretch, the computer counts the pulses. At the end of the mile, push the button again. The number of accumulated pulses are then stored as a reference base. If, for example, the computer counted 800 pulses for the measured mile, it knows that 400 represent one-half mile, 1600 mean two miles, and so on, for any distance you travel. And all this will automatically take tyre size and other variables into account, since they were part of the original calibration. (And this, of course, means that you must recalibrate the system if you change your tyres.)

Okay, the computer now knows how far you've gone, but it must also know

your speed to do any useful work. To determine it accurately, the system computes it. Since the speed — or rate — is equal to how long it took you to go a certain distance, and the distance is known from the calibration, all that's needed to calculate the speed is the time ($R = D \div T$).

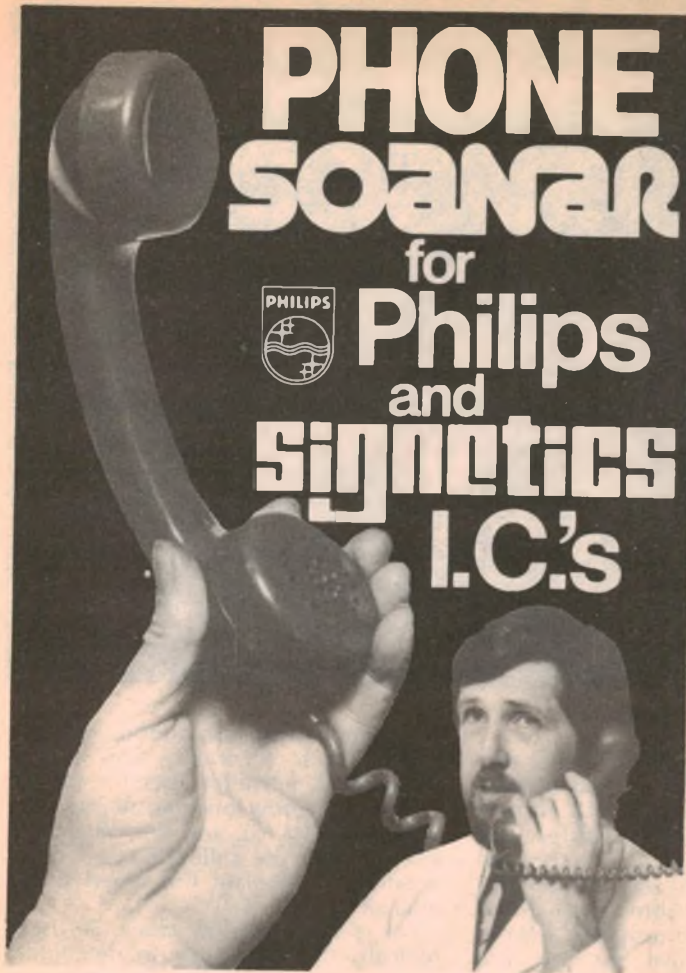
For that, a digital clock is used, basically the same type as the digital clock on your desk. The clock circuitry starts with a quartz-crystal-controlled oscillator — merely a circuit that switches on and off at a precise rate, thousands of times a second. Other digital circuits within the clock divide this time down into thousandths, hundredths, tenths, and finally single pulses per second.

The computer can use any of these time bases as a "window" — a single moment in time to count distance pulses from the transducer. If, for instance, it counts four pulses during a 1/10-second window, that's equal to 40 pulses per second; 2400 pulses per minute; 144,000 pulses per hour. And, from the original distance calibration, if each pulse represented one foot of movement, then you would be moving at 144,000 feet per hour or 27.3 miles per hour.

If all that has you confused, don't worry. Fortunately, the computers do it all automatically — every second — and show the results on a digital display. But that's not all.

More tricks

Besides a speed transducer, the Compucruise and Prince units use a flow transducer on the gas line. It, too, uses pulses to indicate the amount of fuel passing through to the carburettor. And once calibrated by entering in the amount of fuel consumed at your next fill-up, along with the capacity of your fuel tank and the cost per gallon of gas,



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Car computers: new electronic know-it-alls

Who makes them

Avatar — Grass Valley Instruments, 12555 Loma Rica Dr, Grass Valley CA 95945; Compucruise — Zemco Inc, 1136 Saranap Ave, Walnut Creek CA 94595; Prince — OBC Products Div, 35 Madison St, Holland MI 49423.

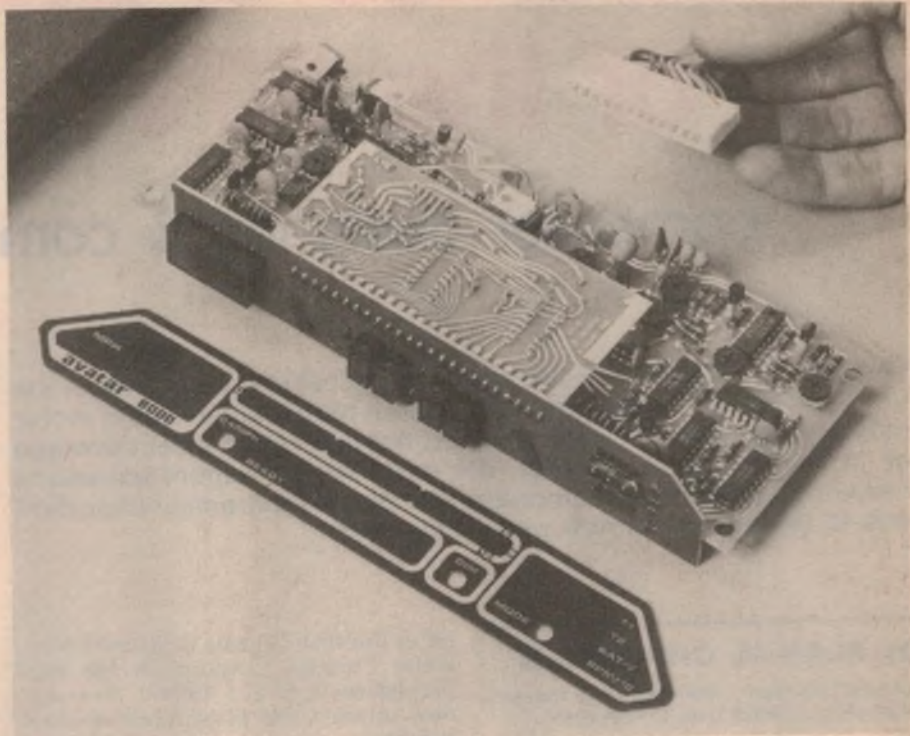
The Compucruise is distributed in Australia by Antelope Engineering Pty Ltd, 68 Alfred St, Milsons Point, NSW 2061. Phone 929 4033.

there's no end to what these systems can predict.

"We've got all this information coming into the computer — what we've done is to try and take full advantage of each piece," said Don King, vice president of Compucruise. He's not kidding. The small, 20-button box can perform 44 different functions, including instant mpg, cost per mile, average speed, lap timer, ETA, fuel to empty, present time. Even external temperature sensors can be connected for an inside/outside temperature display. And as a \$40 option, the mechanics for a cruise-control system are thrown in, all precisely controlled by the black box on your dash.

Since each key of the Compucruise system performs multiple functions, it's possible to get the correct sequence mixed up when you first start to use it. But the computer out-thinks you there, too: Push the wrong button and the display shows ERROR, and adds an audible alert.

The Prince system is a bit more straightforward in its operation; each button is assigned a specific purpose. The system also contains a programmable memory. Enter in up to five mile markers and the unit reminds you when you're a mile away from a detour, an accident, or other roadway perils. It's assumed this information would come from "Good Buddies" over the CB, but the computer is just as handy for storing mileage markers for direc-



Avatar is the simplest of the three units, gives engine and time information on LED readouts. Unlike Compucruise and Prince, it doesn't contain a microprocessor.

tions — at the next beep, you know to look for route 287 on the left, for instance.

The Avatar is the simplest of the three units. It's designed to give precise engine and time information: surface- and fluid-temperature display, digital speedometer, clock, elapsed time, battery voltage, digital tachometer, and a string of LED indicators that light in proportion to rpm, serving as an analog tachometer.

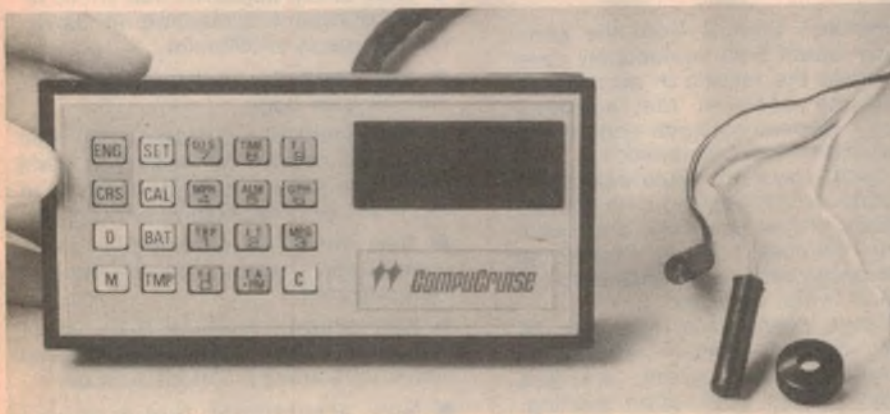
Just three buttons operate the system, but since it does not contain a microprocessor, any computations you do will have to come from your brain.

On the road

As I rode through the streets of New York and onto a parkway system, at the same time pushing buttons and reading digital displays, I was happily alert to one point: A friend was doing the driving.

The myriad of digital displays and pushbuttons are not meant to be the centre of your attention while you're at the wheel. Rather, as the instruction manuals point out, the system should be set up before starting a trip so you can glance at the unit occasionally to see that you're on course.

As we rode, I couldn't help but think this was just the beginning. Under the hood of his car, a microprocessor-based electronic ignition system was controlling our fuel flow for optimum mpg, firing spark plugs for precise engine performance, and advancing timing for instant acceleration when we needed it. Inside the box in front of me, another microprocessor was controlling our speed, indicating our location, displaying how much fuel we had, and telling us when we'd arrive at our destination. All that's left, I thought, is the steering — and that may be just a matter of time.



Compucruise is small, so it may be mounted directly in dash. Two temperature sensors may be placed anywhere. Third component is an audible alarm.

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Electronics & the car of the 80's

computer designed & computer controlled

The decision of the US Government to put car manufacturers in the front line of the battle to save oil is about to revolutionise the motor industry. By 1985, US vehicles must not only reach a fleet average of 11.7km/l (around 33mpg), but must meet stringent emissions requirements as well. Computers will play an extremely important role in designing the new generation cars.

by **ALAN M. CHRISTMAN**

General Manager, Manufacturing Industry Marketing, Control Data Corporation.

An era of revolutionary change is underway for the US automobile industry. An ever-changing series of government fuel-economy, emissions and safety standards has mandated a complete re-design of each manufacturer's automobile product line.

To meet the government-imposed standards, it is estimated that American car manufacturers will spend \$US50 to \$US70 billion between now and 1985 in massive product re-design programs — more than was expended to place the first astronaut on the Moon.

Ford Motor Company alone expects to spend \$US20 billion in its re-design efforts, more than the total profits earned

in the first 74 years of its existence, while Chrysler Corporation has embarked on a \$US7.5 billion, five-year new product and plant modernisation program.

The regulatory process causing such expensive new product programs in the automobile industry began innocently enough in 1965 when Congress passed the National Highway Traffic Safety Act, and followed it up a year later with the Clean Air Act.

Since then, however, Congress has not only continued to progressively tighten safety and emissions standards, but has also imposed fuel-economy standards that require a fleet average of 11.7km/l (33mpg) by 1985 for each manufacturer.

The regulations are becoming more stringent. Here's what's been proposed or enacted in the last year alone:



Computer-controlled seat adjustment system from Recaro and National Semiconductor. The seat automatically adjusts to one of two pre-programmed positions at the press of a button.

On-board computers by 1981 says GM

US giant General Motors, the world's largest car maker, says that "virtually every GM car will have an on-board computer in 1981, primarily for the control of emissions and for fuel economy".

The company's main emphasis seems to be on central computer control. It believes that given computer control of the ignition, fuel flow and transmission, it would be possible to take the next step and disconnect the throttle from the floor pedal.

The accelerator would then serve only to transmit electrical signals, representing the driver's desired rate of acceleration, directly to the

computer. Signals from the computer would then immediately open or close the throttle in accordance with the optimum fuel efficiency curve, depending upon engine and transmission characteristics.

Such a system would essentially modify driver behaviour in the interests of fuel economy, and could even eliminate certain aspects of anti-social behaviour concerning the use of motor vehicles.

Other possibilities foreseen by GM include plug-in automatic diagnostic equipment, keyless doors, coded pushbutton starting, radar braking, and electronic anti-theft devices.

- New emissions standards that will require car makers to cut tailpipe emissions by more than 93% from uncontrolled levels compared to an 83% requirement today. The technological challenge to the industry is to offset possible fuel-economy penalties of up to 12% while meeting the emissions standards.

- New safety standards that could require occupant protection in barrier crash impacts at 80km/hr.

- New passive restraint requirements, including air bags.

- New emissions standards that one day could require car makers to build engines to meet standards, in effect, at the worst possible engine adjustment.

- New service requirements to make engines and emissions control systems "tamperproof".

- New altitude standards that require cars in 1985 to meet the national emissions standards "at all altitudes".

- New accelerated fuel-economy standards, requiring a fleet average of 9.4km/l in 1981, 10.2km/l in 1982, 11km/l in 1983, and 11.5km/l in 1984.



A Chrysler engineer uses a colour graphics terminal to analyse a car body design. Computers will help Chrysler meet stringent new government regulations.

As if these regulations were not tough enough, there are proposals for even higher fleet fuel-economy standards — perhaps up to 17km/l (50mpg), according to Joan Claybrook, National Traffic Safety Administrator.

Meeting any one of these standards requires an immense amount of fast-paced, high-priced technological development over and above the normal requirements for new product development. Meeting them all at the same time requires pushing far beyond the state-of-the-art today, and somehow working around the irrefutable fact that reliable, time-tested solutions to the problems of safety, emissions and fuel economy fight each other when all the regulatory screws are tightened simultaneously.

Computer aided design, or CAD, has become an indispensable tool for the automobile industry in making the "impossible" possible. The plain fact is that government regulations are so stringent, and have been mandated so rapidly, that it would be impossible for humans alone to make the necessary engineering changes fast enough.

Both Ford Motor Company and Chrysler Corporation have installed large-scale Control Data CYBER-class computer systems to help them meet the technological challenges outlined earlier. CAD is allowing Ford and Chrysler to:

- Design, test, re-design and re-test component parts by simulating them on the computer, thus significantly reducing the costly and time-consuming process of testing prototype parts which previously had to be made and re-made until the desired configuration was achieved.

- Compress design time, giving management more time to consider alternative proposals before making final decisions.

- Complete considerably more engineering projects in the same amount of time.

- Relieve design engineers of the tedium of doing drawings by hand, allowing them more time to be creative and to make critical decisions.

- Interface more efficiently with manufacturing and assembly operations on design and engineering issues.

Computer-controlled fuel injection

Robert Bosch GmbH, Germany, has developed a microprocessor-based system that controls both fuel injection and ignition.

Heart of the system is an RCA Cosmac 1802 microprocessor. In operation, sensors under the hood pick up information on engine speed, crankshaft position, throttle position, intake-air temperature, and intake-air flow. The data is fed to the computer which calculates injection and ignition timing, and the amount of fuel to be injected.

The system results in substantial fuel savings, improves engine performance, and reduces engine emissions according to Bosch.

A similar system has been developed by Lucas Electric, the British auto parts manufacturer.

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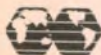
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Electronics & the car of the 80's

At the Ford Engineering Center in Dearborn, Michigan, for example, nearly 5,000 computer technicians interact with six general-purpose and more than 100 special-purpose computer systems — the most powerful of which is a Control Data CYBER 176 — on a 24-hour-a-day, 7-day-a-week basis.

Through this extensive computer information system, Ford provides data that can be used by engineers, designers and planners to control and compress the product development process. Among the uses of Ford's extensive computer network are:

- To maintain day-to-day control of Corporate Average Fuel Economy for current and future models to assure compliance with government regulations. The system lists all of the powertrain and vehicle combinations and suggests specific mixes to achieve the standards on a continuing basis.

- To select the optimum mix of weight-reduction actions to achieve specific reductions. The data bank currently has 700 weight-reduction possibilities, and plans are to include cost-reduction, safety and reliability programs.

- To build finite element models for structural analysis of components. Design engineers take digital information from the Design Center, where the design of major parts of the car begins, and refine the lines to ensure that they meet packaging and manufacturing requirements.

By means of computer graphics, a car body is divided into specific panels or sections for closer analysis. Through use of a finite element structural analysis program called NASTRAN, engineers evaluate new designs involving lighter materials, reinforced plastics and other materials.

The computer predicts stresses or vibration characteristics which result when the analytical model is subjected to simulated loads. Graphics displays are used for constructing and interpreting the finite element models.

An indication of what the future holds is a prototype vehicle being built by Ford using graphite components that are stiffer than titanium, as strong as high-strength steel and one-third the weight of steel with equal performance.

This prototype vehicle incorporates a

Crisis for tradesmen — anti-skid braking — anti-collision radar — joystick control

The growing use of electronic and computer technology in modern cars is rapidly overtaking the ability of motor vehicle tradesmen to service and repair them, according to a recent industry report.

The report, published by Australia's National Retail Motor Industry Training Committee (NRMITC), says that the local industry does not understand or appreciate the "staggeringly rapid transformation into computer technology" that is about to revolutionise the motor car.

It says that within the next four years, possibly two years for some makes and models, many new vehicles will have computers controlling the engine, instrumentation and transmission functions. This development is being hastened by emission-control laws which demand exacting monitoring of carburation setting and ignition timing.

The need for manufacturers to improve fuel economy is also an important factor here.

Many other vehicle functions, such as trip meters, self tuning radios, and seat positioning memory

devices will also be controlled by computer. Most vehicles will be fitted with anti-skid braking systems, anti-collision radar and other electronically controlled safety equipment such as self-levelling headlights. The various operating functions will be continuously monitored, and dashboard readouts used to indicate faults.

Other major changes forecast by the report include the use of plastics for body, trim, and even engine parts. Dashboard driver information systems — warning of approaching emergency vehicles, and providing traffic flow and speed limit information — will be fitted, and switches will be touch operated.

The steering wheel could even be replaced by a joystick control!

It is not yet clear whether the automobile's various sensing, control and display systems will be all controlled by a central computer or by an automotive version of distributed processing. Both systems may even be used. Either way, the car of the mid-1980's will be a rolling computer centre in which multiplexing will have become a necessity.

number of graphite components — doors, hood, driveshaft, suspension arms, bumper, floor pan, wheels and even the frame. It will be roughly the size of today's intermediate car, but will weigh about 570kg less.

Some part-by-part reductions are impressive: an 18kg steel hood weighs in at 7kg in graphite fibre and a wheel weighs only 4kg compared to 8kg in steel.

Of special significance is the design of hybrid materials that combine graphite and glass for maximum cost effectiveness. Since limited field test data exists for these materials, computer technology plays an important role in evaluation.

CAD also is helping Chrysler Corporation — an industry leader in the use of this advanced technology — make vehicle changes. At Chrysler's Technical Computer and Instrumentation Center in Detroit, four large-scale Control Data CYBER 170 and 70 series computers, supported by a broad range of Control Data peripheral equipment, are linked together to provide computer services 24 hours a day, 7 days a week to engineers in the US and Europe.

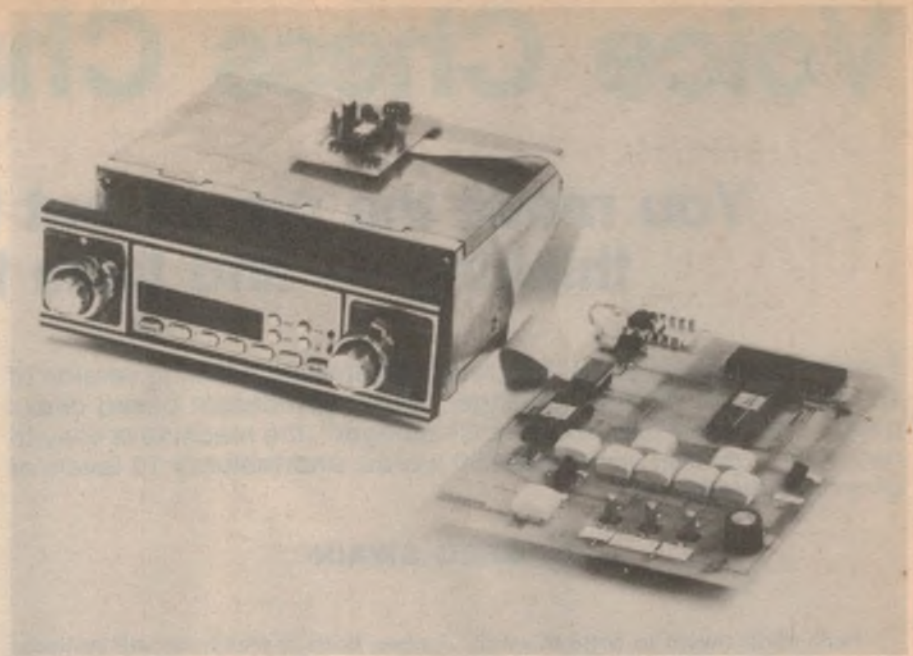
In addition, three CDC 1700 series computers support large screen interactive graphics, analog-digital and digital-analog conversion and computational services for Chrysler's vehicle proving grounds.

The Company's extensive computer network, which includes about 100 graphics and 300 teletype terminals, enables users in many locations to share a common data base that is continually updated as engineers and designers create and test new solutions to the government-mandated vehicle changes.

Chrysler engineers also use the NASTRAN finite element structural analysis program extensively in building models on a display screen to evaluate the use of new materials in making vehicles lighter and more fuel efficient. Through use of such lightweight materials as plastics, graphite, composites and high-strength steel, Chrysler expects by 1985 to reduce the average weight of its entire fleet of automobiles by 600kg — a 30% reduction on current models.

Weight reductions have a snowballing effect. Once weight is taken out of a car, it becomes possible to lighten up other parts. Less overall weight permits the use of smaller, lighter components — including lighter brakes, wheels, tyres, engines and transmissions. Computers also are used to package these components in the smaller car bodies.

Examples of Chrysler products that nearly meet 1985 standards are the basic four-speed manual 1978 Omni and Horizon, which have been certified by the government at 11.5km/l for city driving and 17km/l on the highway —



New style AM-FM car radio from National Semiconductor features a microprocessor controlled digital tuning system, keyboard entry of station frequency, pushbutton scanning, a clock, and storage of several stations in memory.

Dashboards will also go electronic

Solid-state electronic instrument displays with bright readouts are likely to be part of the new generation electronic cars. Inaccurate fuel gauges and speedometer cables will be eliminated.

General Instruments Microelectronics (UK), for example, has recently developed a vehicle display system based on one of its single-chip processors. The devices can be masked programmed to user requirements and, depending on dashboard needs, can drive fluorescent display tubes, LED displays, or liquid crystal devices.

Pulses derived from the gearbox output shaft are processed by the chip to drive speed, trip information and fuel displays. Engine parameters can also be displayed using analog or digital electronic

readouts.

Another British company, Smiths Industries Ltd, has developed a vehicle display system that uses a laminated glass construction enclosing phosphor patterns. When a direct current is passed through the phosphor, the molecular layer in immediate contact with a conductive pattern etched into the glass emits light.

The most highly developed phosphor is zinc sulphide which emits a predominantly yellow light. This may be filtered to provide green and red displays. Display thickness is just 12mm and, subject to the conductive pattern, the information can be displayed in either digital or analog form, and as horizontal, vertical, curved, circular, expanding or contracting patterns.

performances that convince Chrysler officials that the company's \$7.5 billion, five-year new product and plant modernisation program will pay off.

An innovative use of computers at Chrysler involves a manikin called "Cyberman". When designers want to evaluate a new seat, armrest or a radio knob location, they call on "Cyberman", a montage of human measurements which they can call onto a display screen or computer printout.

Designers use the manikin to evaluate the packaging of interior features so that drivers of all shapes and sizes can be comfortable behind the

wheel and can operate controls conveniently. An operator can program "Cyberman" into a number of pre-selected positions, displaying the manikin on a graphics terminal as a stick figure or as a complete "wire frame" outline.

The role of computer technology is making the "impossible" possible, as car makers use innovative approaches in designing and building the new generation of automobiles that Americans will be driving in the mid-1980's. That new generation will be radically different from the cars we drive today.

Voice Chess Challenger

You move the pieces but it does the thinking — and talks to you!

Fidelity Electronics (USA) has recently released a talking version of its now famous Chess Challenger, a microprocessor based chess game. Called the "Voice Chess Challenger", the machine is easy to use, has a vocabulary of over 50 words, and features 10 levels of playing difficulty.

by **GREG SWAIN**

I really didn't want to write this article — not after the battering my ego took at the hands of a smart-alec backgammon computer some 18 months back. Well it's happened again! Once more my ego has been trampled on, this time by the "Voice Chess Challenger", a talking chess computer from American manufacturer Fidelity Electronics!

I can't even claim that the computer cheated. Chess is a game of skill, not luck, and there's simply no opportunity for the computer to resort to skulduggery. So I have no excuse — except to say that I was badly out of practice.

Actually, I had a lot of fun playing Fidelity's Voice Chess Challenger. It's a fantastic product, not only because it's a complete chess playing computer, but because it also "talks" using computer synthesised speech. It's almost like playing a human opponent!

Voice Chess Challenger is based on the Zilog Z80A CPU and is said to include the most powerful chess program ever placed in a microprocessor. Backing up the CPU are 8k bytes of ROM which store the game program, another 4k bytes of ROM to store the voice program, and 1k bytes of RAM to store the positions of the pieces as the game progresses.

The unit itself is compact and portable. It comes housed in a solid hardwood case that incorporates all the electronics (except for the plugpack power transformer), a keyboard, a 4-digit 7-segment LED display, and the playing board. It fits neatly into an attractive plastic carrying case, and is supplied complete with chess pieces and instructions.

Approximate dimensions are 31 x 20 x 3cm (L x W x H).

Adding a voice to the Chess Challenger has certainly resulted in a product which is much more interesting than the earlier Chess Challenger 7 and Chess Challenger 10

games, both of which are still available by the way. The machine incorporates a vocabulary of over 50 words. It announces each key as it is pressed, tells you which pieces it has moved and captured, and informs you when your king is in check.

The cold, nasal-sounding computer voice will even remind you to "enter your move" if it thinks you're taking rather a long time to make up your mind. The voice facility may be turned off (or on) at any time without affecting the game in progress.

You approach the Voice Chess

Challenger by switching on the power and pressing the reset key. The machine introduces itself with the words "I am Fidelity's Chess Challenger, your computer opponent. Select your level". By then pressing the level (LV) key, the player is able to choose one of 10 levels of playing difficulty, the unit simultaneously announcing and displaying the level each time the key is pressed.

To play the game, the player keys in his move on the keyboard, and moves the piece to its new position. The computer then announces and displays its own move. Keyboard entry is quite logical and straightforward as the following example will illustrate.

Let's say that, at the start of the game, the player wishes to move a knight from position g1 to position F3. The sequence of keystrokes is: g7, A1, F6, C3, EN (enter). That's five keystrokes in all! Simple, isn't it?

The average response time of the computer to the various levels ranges

Comment by Robert Jamieson,

Australian Chess Champion

The first question most people will ask about the Voice Chess Challenger is "how well does it play?". I would classify its strength as that of a fair club player, with a rating of about 1100, which places it above 95% of social players who make up the vast majority of the chess playing public.

The computer, like human chess players, has its own strengths and weaknesses. It develops its pieces well, and will take advantage of most tactical errors on your part, ie, if you give it the opportunity to capture an unguarded piece or to win material by a knight fork, etc. However, its depth of calculation appears to be short so that it plays less well in endgames, where one must calculate a longer series of moves, and when it is being attacked it may miss some threats which are beyond

its vision.

As a teaching instrument for inexperienced players the Voice Chess Challenger should be rather effective. It develops its pieces along classical lines, tells you if you make an illegal move and can let you know what it thinks is the best move for you to make, as well as having a repertoire of 40 "book" openings for you to follow if you like. Regrettably these openings are poorly classified on the instruction sheet, which makes it a little difficult to look up the line that you want.

Stronger players will be interested in the Voice Chess Challenger, not only because they want an opponent that can give them a good game, but because it is intriguing to try to work out how the computer "thinks" and to test its reaction to different types of play.

from just five seconds for level 1 up to 11 minutes for level 9. If level 10, the most difficult level, has been selected however, the response may take many hours — or even days. The player can ask the computer which move it is considering at any time, and can even halt the search effort and make the computer enter its next move.

Essentially, what happens is this: When set to level 1, the computer examines only a few of the more obvious move and countermove combinations, thus making it an easier opponent and taking no more than five seconds to respond. But, beginning with level 2, the search levels are progressively ex-

played. In the higher levels of play (above level 1), the Voice Chess Challenger may start to flash a victory and announce "mate in two", even before the actual checkmate. This feature tells you that it has set up a "mate in two" situation from which you cannot escape.

If all that sounds impressive enough, consider the following:

- the position of every piece on the board can be audibly listed (and displayed) on demand;
- the player can choose to play either white or black, and can change sides during the game;
- the computer will recognise and

its knights, bishops and centre pawns early in the game. The king is usually "castled" into safety as soon as possible.

The machine is also very quick to take advantage of human blunders, such as leaving the queen or some other valuable piece unguarded. And once it's got you by the throat, it doesn't let go!

In case you're wondering, I did manage to beat the Challenger — eventually. The game took just on 1½ hours to complete, this with the machine set to the easiest level. It's very sporting about losing too — no temper tantrums or sulking here. It announces

The Voice Chess Challenger has a vocabulary of 50 words and 10 levels of playing difficulty.



panded, with increasing numbers of move combinations considered and corresponding increases in the response time.

Illegal moves are met with " - - - " on the display and the announcement "illegal move". This situation is corrected by pressing the clear (CL) key and re-entering the move, making sure that the error has been corrected. The CL key can also be used to clear an unwanted move, provided it has not been entered.

At the conclusion of the game, the computer announces the winner with the words "I lose" or "I win" and, if it loses, displays the number of moves

played. In the higher levels of play (above level 1), the Voice Chess Challenger may start to flash a victory and announce "mate in two", even before the actual checkmate. This feature tells you that it has set up a "mate in two" situation from which you cannot escape.

If all that sounds impressive enough, consider the following:

- it's possible to set up and solve chess problems, to alter the position of pieces during the game, and to "resurrect" pieces which have been captured;
- there are over 40 book opening variations, either randomly selected or chosen by the player; and

versions of the Voice Chess Challenger are available in German, French and Spanish!

So what's it like to play against? Well, it's certainly no pushover, even when set to the easiest level. It tries to control the centre of the board, and develops

the result without emotion, and sits there waiting to take its revenge in the next game.

The only sad note is the price, which, at \$495, seems likely to be beyond the means of many people. Still, the price is not unreasonable, especially when one considers what the unit does. Perhaps I could console myself with one of the lower priced non-talking models!

You can buy the Voice Chess Challenger from large department stores (Grace Bros, Myers, etc), and from specialty games shops. Further inquiries to the importers Futuretronics Pty Ltd, 79-81 Levenswell Rd, Moorabbin 3189.

Solid state magnetic switches . . .

The Hall Effect

what it is and how it works

Ever heard of the Hall Effect? You haven't?! Well read on. Hall Effect devices are now available at quite a moderate cost, making it possible for the electronics enthusiast to experiment with these fascinating devices. Imagine being able to measure the flux intensity of a permanent magnet, or use magnets in all sorts of control applications.

by **GERALD COHN**

The Hall effect was discovered in 1879 by Edward H. Hall, at the John Hopkins University. Mr Hall found that when a magnet was placed in a position where its field was perpendicular to one face of a thin rectangle of gold through which current was flowing, a difference in potential appeared at the

opposite edges. He found that this voltage was in turn proportional to the current flowing in the conductor and the flux density or magnetic induction perpendicular to the conductor.

Today, semiconductors are used rather than gold for the Hall element. The Hall voltages obtained are much

higher using semiconductors.

Fig. 1 illustrates the Hall principle. Shown is a thin strip of semiconductor material (Hall generator) through which a constant control current is passed. When a magnet is brought near, such that its field is directed at right angles to the face of the semiconductor, a small voltage appears at the contacts placed across the narrow dimension of the strip. As the magnet is removed the voltage drops to zero.

The Hall voltage is dependent on the presence of the magnetic field and on the current flowing in the element. If either input is zero, the Hall voltage is zero. If the current flow through the Hall element is held constant, the Hall voltage is proportional to the magnetic field, and conversely, if the magnetic field is held constant, Hall voltage is proportional to the control current.

In typical Hall effect devices the control current is held essentially constant and the flux density is changed by the

Left: Typical Hall effect sensors. Shown are a vane sensor, a current sensor and three general purpose devices.

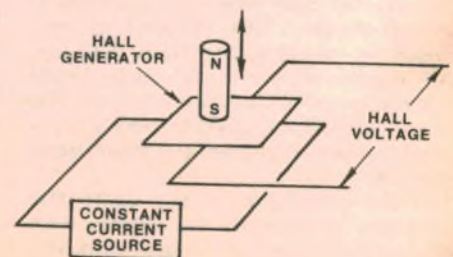
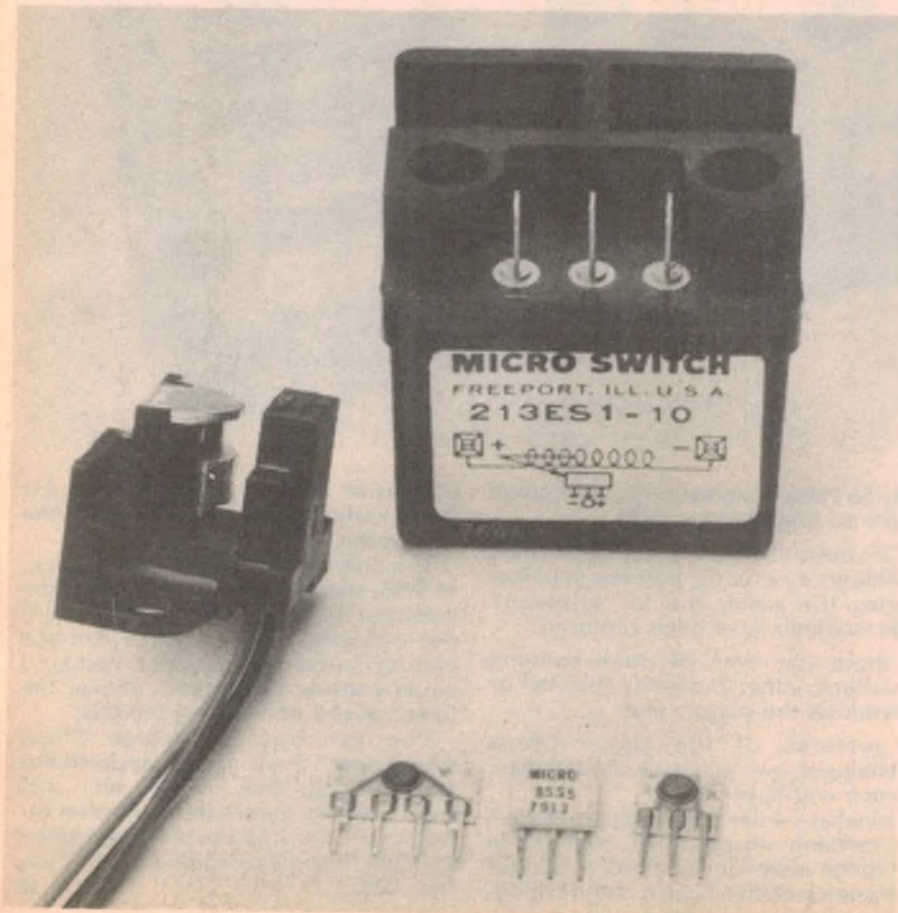


FIG. 1: HALL EFFECT PRINCIPLE



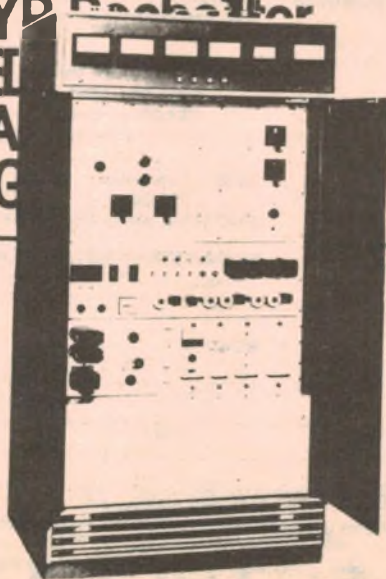
Over 1300 CCA transmitters are in use world wide. The CCA FM range covers everything from a modest 10W. to 80KW. Why do so many broadcasters rely on CCA? Because all CCA transmitters are designed to cut operating costs. By using proven grounded-grid design. Grounded-grid design cuts the expense of frequent replacement which is inherent in designs using HF tetrodes for FM trans-

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WEEL
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WMG

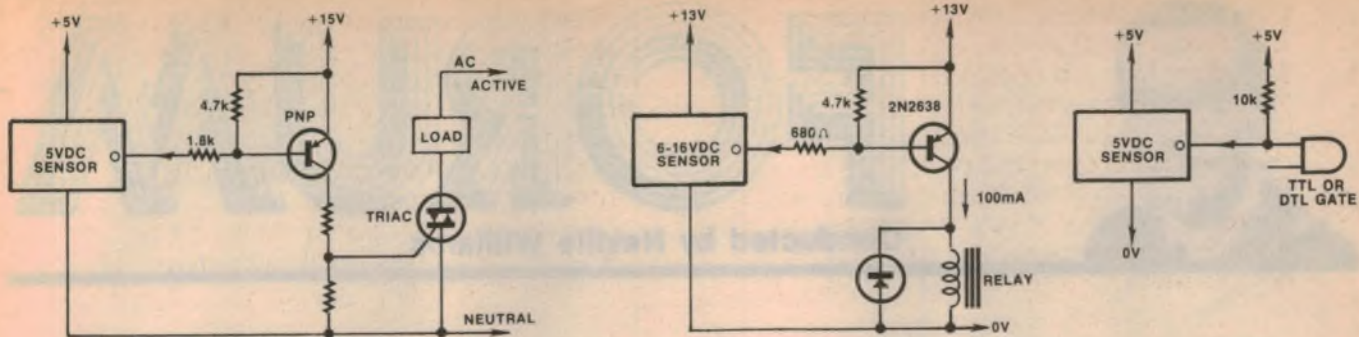
WFCN Nashville
WAMB Nashville
KRBB Houston
KHCB Houston
KRSP Salt Lake City
WQFM Milwaukee
WFMR Milwaukee
CBC Toronto
CBC Calgary
CBC Winnipeg
CBC Peace River
CBC Kitimat
CBC St. Johns
CBC Halifax
CBC Ottawa



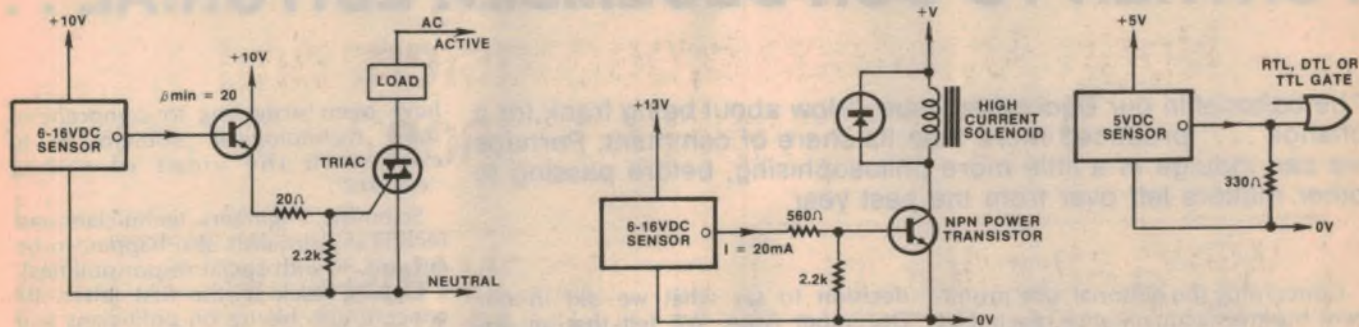
CCA-FM transmitters are available with ratings from 10, 40, 100, 250, 1000, 2500, 3000, 4000, 5000, 8000, 12000, 20000, 25000, 27500, 40000, 55000 and 80000 watts. CCA also offers a full line of AM, FM, HF, UHF and VHF transmitters and TV translators. Accessories include limiters, auto switchers, auto power controls, studio equipment and consoles.



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CURRENT SINKING SENSORS



CURRENT SOURCING SENSORS

FIG. 4: DIGITAL/HALL EFFECT INTERFACE

the output of which is then amplified and fed to a trigger circuit. This, in turn, drives an output transistor to provide the digital output.

The digital devices are available with two types of outputs: current sinking and current sourcing. The current sinking output consists of an open collector that is capable of sinking in the region of 10mA. The emitter of the transistor is internally connected to the ground rail of the chip. The current sourcing type has an open emitter output, capable of sourcing 10mA. The collector of this transistor is internally connected to the supply line of the Hall element.

The digital devices can be interfaced to external circuitry in quite a number of different ways, some examples of which are shown in Fig. 4.

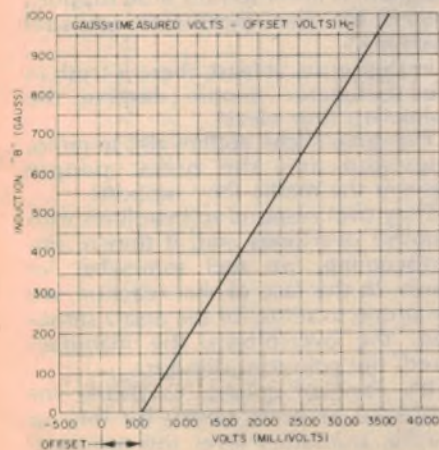


Fig. 3: Hall element characteristic.

Hall effect devices have several big advantages over their electro-mechanical counterparts. These include longer life, greater reliability, and the elimination of contact bounce (since there is no mechanical switching action). This latter advantage has been exploited by such companies as Honeywell and IBM (to name just two) for a range of computer and typewriter keyboards.

The basic scheme is quite simple. Small magnets are attached to the various keys, and activate Hall effect devices whenever the keys are depressed. By eliminating the contact bounce problem of mechanical keyswitches, the interfacing circuitry to the keyboard is considerably simplified.

Another commercial application for Hall effect devices, and one that is increasing in popularity, is in auto ignition systems. Here a cup-shaped vane, with as many teeth as there are engine cylinders, rotates through a Hall effect vane sensor mounted in the engine distributor. The resultant logic pulses are used to trigger an electronic ignition system without the use of points.

Hall effect devices can also be used in flow meters and computer peripherals, and as current and position sensors in a wide range of industrial machinery and

home appliances. They can, for example, be used to control the commutation of field current in brushless DC motors, to sense tone arm position in record players, and to control conveyor belts on production lines.

Electronic sewing machines, coin operated machines, office machines, telephone systems, electronic keyboards on musical instruments, and utility meters with remote reading capabilities can all make use of Hall effect devices.

Typical applications in which the hobbyist could use Hall effect devices include burglar alarm installations (instead of reed switches, for example), or as detectors in model railway layouts. The Hall device could be mounted in the middle of the railway track, at the point where it is desired to detect the presence of a train, and activated by a magnet fastened to the underside of the locomotive or one of the carriages. The output of the device could be used to switch points or signals, or even provide signals to a computer that is controlling the layout.

Well, that's at least a basic introduction to the Hall effect and the way in which it can be applied. It's now up to you to find your own applications for these interesting devices.

This article has been prepared from information supplied by Micro Switch, division of Honeywell Pty Ltd. Micro Switch manufactures a wide range of Hall effect devices and sensor packages, including vane sensors, proximity sensors, current sensors and plunger operated sensors. Further information on these may be obtained from Honeywell Pty Ltd, 863-871 Bourke St, Waterloo, NSW 2017. Telephone (02) 699 0155.



FORUM

Conducted by Neville Williams

FURTHER TO OUR DECEMBER EDITORIAL . .

The editorial in our December issue, "How about being frank for a change . . ." produced more than its share of comment. Perhaps we can indulge in a little more philosophising, before passing to other matters left over from the past year.

Concerning the editorial, one prominent business acquaintance reacted by describing it as "one of the best you have ever run". Spare our blushes, but it did have the advantage of expressing something that we feel quite strongly about. Evidently, others in the technical community share those feelings.

By way of example, I quote a further message to hand, on the letterhead of an old and well known company:

Dear Neville,

Just a line to tell you how pleased I was to read your editorial in the December EA.

I believe there are many who wish that politicians would learn statesmanship and get on with the job for which they are paid.

There are many who wish reporters would stop manufacturing news. How sick one feels when reporters, who have not yet mastered their native language, subject eminent interviewees to a series of questions intended to establish a preconceived viewpoint.

What has happened to the self-regulatory bodies that pretend to uphold honesty and objectivity in the media?

BS (North Ryde, NSW).

But not everyone saw it that way. A NSW country reader had this to say:

Dear Sir,

Whilst I agree 100% with what you say in your editorial in the December 1979 edition, I still feel we (your readers) must object to our (your readers') magazine entering into the political arena.

Be frank, but stay in electronics! Reader from 1951. RP (Orange, NSW).

Let me assure RP and his friends that politics, as such, played no part in our

decision to say what we did in our December issue. We felt that an unremarkable situation at the Lucas Heights reactor had been sensationalised by the media, and compounded by a statement attributed to the NSW Premier. Our criticism would have been the same, had the Premier been aligned with one of the other parties — or no party!

The overwhelming reaction we received was not political either — or should we say not party-political. It was simply concern that politicians of all hues are responding to expedience rather than to fact. "What was said in the December editorial needed to be said" was the most frequent observation.

We would not like to see this magazine, or any other technical medium or body assume a permanent political bias, but we don't like the other extreme, either: where informed opinion is withheld just because it might seem to support the current stance of one or other political faction.

We have often felt that our learned societies have been guilty in this respect. They have remained virtuously aloof while politicians, press and public

have been struggling to comprehend some technological problem, or to cope with the views of ratbag "experts".

Scientists, engineers, technicians and technical journalists also happen to be citizens — with social responsibilities!

Getting back to the first letter, BS concentrates his ire on politicians and the media but, like my original editorial, omits any reference to the third group in an unfortunate triangle: the public at large including you (perhaps) and me.

We also lack objectivity and we contribute to the emotionally based environment in which we live.

As a general rule, it is not necessary to go beyond one's immediate acquaintances to discover a whole array of strongly held opinions — based, not on objective assessment, but on readily perceived attachments and preconceptions. Challenge those ideas and the usual response is one of passionate defense, rather than a readiness to re-think and re-evaluate.

We all tend to discount opinions which differ from our own and to relish those which coincide.

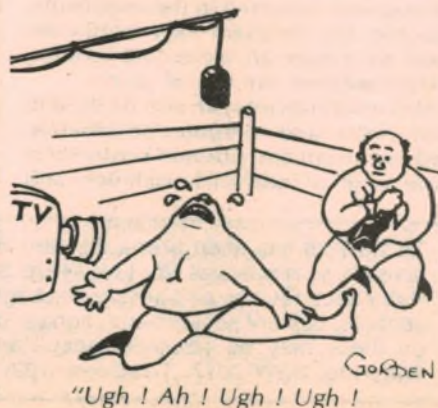
When we go to the ballot box, we vote for people who hold to our particular viewpoint. A candidate who presents himself as an objective thinker, open-minded, and unattached, is likely to rally little support, unless he also possesses unusual charisma.

In this sense, at least, there is truth in the sentiment: people deserve the politicians they elect!

The same cliché applies also to radio, television and the press: people deserve the media they support!

They (we) respond to headlines with emotive overtones and, if they're not forthcoming, we feel somewhat let down. In the face of that reaction, we are prone to settle for the ersatz sensation; the over-blown, the manufactured, the colourful rumour.

It's easy, of course, to blame the broadcast or press barons for this; or maybe, at another level, the commentators, the reporters and the sub-editors. But we delude ourselves.



The fact is that it would be a lot easier for all these people to be matter-of-fact (objective, if you like) and to report events as they happened — rather than to be everlastingly turning over rocks in an effort to find today's sensation. Unfortunately, experience has taught them that it doesn't work.

The public rejects it as unspeakably dull!

Hence our earlier reference to an unfortunate triangle, a feedback loop if you like, in which public, politicians and media each affect, sustain and control the other.

Short of changing the entire system (Socialism? Communism? Otherism? Dictatorship?), our only recourse seems to be to education and enlightenment in the hope of modifying one or more of the factors in the loop.

Where technical matters are involved, technically minded people have a clear duty to seek out and promulgate the best available information, as distinct from rumour and emotion. That was the thinking behind our December editorial.

Oh yes; if you're wondering what the wrestling cartoon has to do with all this, it did seem to have something in common with the posturing and the agonising of our political leaders, of all shades of opinion.

ENERGY SOURCES

Changing the subject completely, 1979 saw a lot of discussion about energy and energy sources, ranging from nuclear, through fossil fuel systems to "natural" sources such as wind, tidal, hydro-electric and solar.

One of the important truisms that seems gradually to be seeping into public consciousness, is that environmental problems and hazards are not unique to nuclear technology. If the World's growing population and changing life-style demands the tapping and harnessing of large amounts of energy, then there are going to be large-scale environmental implications — some obvious, some less so.

Scars on the countryside and oil spillage at sea are very apparent, as also is smog, smoke and fumes. Increased radioactivity, loss of ozone and acid-rain occur with less fuss. Extinction of fauna and flora by flooding and damming may be appreciated only in retrospect, but it is all happening.

Windmills — wind turbines in modern terminology — have been promoted as a promising "clean" source of energy.

They have also been seen as potential visual blots on the landscape, as subject to structural failure, and as likely sources of interference to radio and TV signals, radio links and aircraft communication and guidance systems.

According to a recent issue of "Electronics" magazine, the possibility of interference to television reception, at least, has now become a reality to

residents of Block Island (adjacent to Rhode Island, USA) who live within 1½km of NASA's developmental wind turbine. Operated by the Block Island Power Company, its whirling metal blades modulate the incoming television signals, causing severe picture flutter. It is in clear contravention of Federal Government laws relating to the environment.

Rather than dismantle the turbine, the US Government has reportedly opted for an alternative measure: to spend \$600,000 on a community coaxial cable system which will supply clean signals to each one of the affected homes.

There has to be a lesson there.

Also on the subject of energy, the December 1979 issue of "Scientific American" carried a major article on Energy Storage Systems.

The writer points out that it is becoming progressively less practical for supply authorities to meet peak daily demands by cycling supplementary (and often ageing) fossil-fuelled stations and gas turbines. Low efficiency, rising fuel costs and environmental considerations all present mounting difficulties.

It is becoming vital for the power generating industry to maximise the use of modern base generating equipment, and to supplement it with energy storage and release facilities to cope with peak demand. Such storage facilities would also be valid for energy gained ultimately from natural sources which may be cyclic (solar, tidal), spasmodic (wind) or even seasonal (hydro-electric).

PUMPED WATER STORAGE

The article carries a photograph of the World's largest pumped-storage hydroelectric plant at Ludington, on the shores of Lake Michigan, USA. It involves an artificial lake 10km long which can be filled by pump-turbines to a water height averaging 75 metres above that of the lake itself. When discharging back through the turbines, it has the potential to produce a short-term peak output of about 2000 megawatts, equivalent to two large power stations. The efficiency is about 66%, which means that two-thirds of the energy absorbed in raising the water level is recovered during the discharge/generate cycle.

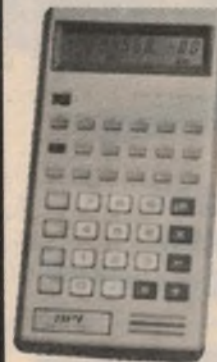
These figures notwithstanding, the writer, Fritz R. Kalhammer, says that the scope for similar projects is very limited. They need a special kind of topography but, in any case, large artificial lakes are seen by many as a threat to the natural environment.

Much more promising, according to the writer, is the idea of large underground caverns, or reservoirs, which can be smaller in size than surface installations but compensated by much greater vertical displacement —

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The BS 610 employs a high brightness 140mm Rectangular CRT with internal graticule assuring easy and accurate observation of waveforms without any parallax.

External DC-Powered operation expands the versatility of this oscilloscope to FLOATING Measurements as well as field operation.

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SPECIFICATIONS:

SENSITIVITY: 5mV to 10V/DIV on 11 ranges in 1-2-5 step with fine control. BANDWIDTH: DC to 15MHz (-3dB). RISE TIME: 24nS. OPERATING MODES: CH-A, CH-B, DUAL, ADD and CHOP. TIME BASE: 0.5µsec to 0.5sec/DIV in 19 ranges and X-Y in 1-2-5 step with fine control. MAGNIFIER: x5 at all ranges. X-Y OPERATION: X-Y mode is selected by SWEEP TIME/DIV switch. CH-A Y axis, CH-B X axis. POWER REQUIREMENTS: AC: 115/240V DC: 11-30V, 7.2VA. SIZE: 145 (H) x 280 (W) x 369 (D)mm. WEIGHT: 6.7kgs.

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FORUM: Energy sources, storage — cont.

eg. 300 metres. This is the technology that will probably have to be exploited if pumped storage systems, in the USA at least, are to rise much above the present level of about 2.5% of all generating capacity.

Once beneath the ground, an alternative is to use large caverns to store air, which is compressed when there is surplus power available to the grid, and released through cascaded turbines when additional power is required.

A pilot plant in Huntorf, near Bremen, in West Germany, can compress air to 70 atmospheres in a 300,000 cubic metre twin chamber leached out of salt deposits deep underground. The system can contribute up to 290,000 kilowatts for 2 hours during periods of peak demand. A problem which has to be faced with such a system is the need to cool the air during compression, to protect the cavern walls, and to add substantial heat during the expansion cycle, to prevent freezing. Energy has to be expended for both purposes, affecting overall efficiency.

Other possibilities are being investigated by power authorities — flywheels, hydrogen generation and storage, and superconductive magnets — but the other area being given major attention is that of storage batteries.

JUMBO BATTERIES . . .

While the scale required dwarfs anything to date, in terms of battery technology, such facilities could be dispersed as necessary in large or small modules, the stored power being immediately accessible at any time. Power authorities are re-assessing batteries of various types, on the basis that the performance and economics of large cells for fixed installations may be quite different from those of small batteries required for powering vehicles. One project, under the auspices of the US Department of Energy, calls for a 30,000 kilowatt/hour lead-acid battery installation by 1984, coupled to a 10,000 kilowatt AC/DC converter. The aim is to gain first-hand experience with battery-stored energy.

AND JUMBO INVERTERS

Which brings me to another matter flowing over from our August and November issues. In the last-named, I was gently chided for being less than aware of the scale and usage of present-day static inverters.

Spokesmen for Telecom and STC indicated that locally produced 415V 3-phase inverters, rated to about 100kW were in everyday use to ensure uninterrupted power to Telecom exchange equipment, etc. They are normally powered by DC derived from the AC power mains but can switch instant-

ly to a large battery bank if the mains supply is interrupted.

A rating of 100kW is tiny compared with the power levels in a grid but, if authorities are looking seriously at jumbo battery banks for energy storage, it is reasonable to assume that jumbo inverter banks are also in view.

Another company which is active in the field of inverters is Topaz Electronics, of San Diego, California. They are represented in Australia by Marine and Aerospace Engineering Pty Ltd, of Suite 501A, 220 Pacific Highway, Crows Nest NSW 2065. Tel (02) 929 5377. (I give the details purely to save ourselves from a sequence of "How do I get in touch?" calls).

From the literature to hand, their

equipments appears to be slanted to US requirement and to smaller applications — but they are very necessary applications in these days of electronic whatnots. Not only do these involve computers, as such, with volatile memories, but other devices like cash registers, where a power dropout can have serious consequences.

No less intriguing, in the literature, is a whole array of power line regulators, isolators and conditioners, intended to protect equipment from voltage variations, surges, spikes, noise pulses and what-have-you. If our concept of DC/AC inverters was limited — as expressed last August — the Topaz equipment is likewise way ahead of traditional ideas about line filters, etc.

Technology certainly breeds technology and my guess is that the rate of propagation will continue to climb through the 80's.

The National Research Council of Canada:

"The problem is not that we are running out of oil — there is more untapped oil in the Canadian tar sands than in all the Middle East — but that the cost of getting it out of the ground is soaring. Ten years ago, it cost about \$200 to find and tap a unit flow of oil of one barrel per day in the Middle East. That figure jumped to about \$10,000 for the North Sea. The pilot plant at the tar sands in Alberta cost \$16,000 per barrel-a-day unit of capacity, and future plants will cost more. Getting a flow of oil of one barrel per day from the ocean floor off Labrador is projected to cost at least \$20,000." (From "Science Dimension" Vol. 11, No 4, 1979).

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NEW KITS (and new kit components)

Remember parts for most kits in most of the electronic magazines are normal stock lines. So even if a kit isn't listed, we may be able to help you anyway. Call in and ask us!

EA ANALYSER/LEVEL METER (See EA February)
Complete kit, including instructions Cat K-3510 \$99.50
Printed circuit boards (set of two) Cat H-8313 \$8.50

SUPERBASS FILTER (See EA February)
Printed Circuit Board Cat H-8370 \$2.40

FLASH EXPOSURE METER (See EA January)
Printed Circuit Board Cat H-8371 \$2.10
Solar Cell Cat Z-4820 \$2.50

GUITAR PRACTICE AMPLIFIER (See ETI January)
Printed Circuit Board Cat H-8625 \$4.60

PLAYMATE AMPLIFIER (See EA January)
Printed Circuit Board Cat H-8369 \$4.60

TRANSISTOR ASSISTED IGNITION (See EA December)
Complete kit including instructions Cat K-3300 \$32.50
Printed circuit board Cat H-8367 \$2.20
BUX80 power transistor Cat Z-2160 \$10.95

FAN SPEED CONTROL (See EA December)
Short form kit (PCB components, no hardware) Cat K-3090 \$11.50
Printed Circuit Board Cat H-8368 \$2.50
SC141D Triac Cat Z-4510 \$1.28
(zippy box, etc. normal stock lines - or build it in to appliance.)

NEW METAL LOCATOR (See EA November)
Complete kit (excluding dowel & former) Cat K-3504 \$19.50
Printed Circuit Board Cat H-8366 \$2.40

INFRA-RED REMOTE CONTROLLER (See EA October)
CQY89A Infra red diodes Cat Z-3235 \$1.50
BPW34 photo transistors Cat Z-1954 \$3.50
Printed circuit boards (pair) Cat H-8365 \$5.95

PROCESS TIMER (See ETI October)
Printed circuit board Cat H-8623 \$3.95

DISCO STROBE Mk 11 (see ETI September)
Complete kit, including instructions Cat K-3152 \$34.50
Printed circuit board Cat H-8572 \$1.95
Flashtube Cat S-3882 \$2.95
Trigger transformer Cat M-0104 90c
Discharge capacitors (each) Cat R-2856 \$3.75
Reflector Cat K-6016 \$4.50

WINDSCREEN WIPER DELAY (See EA September)
Printed circuit board Cat H-8364 \$2.50
Other components for this project are normal stock lines.

AUTO CHIME (See EA September)
Complete kit Cat K-3502 \$29.75
Printed circuit board Cat H-8363 \$3.70
TMS-1000 Integrated Circuit Cat Z-6825 \$16.50

INDUCTION BALANCE METAL DETECTOR (See ETI)
Short form kit (not inc. dowel or former) Cat K-3100 \$35.50
Printed circuit board Cat H-8578 \$1.50

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Our brand new up-dated colour kit catalogue is now available. Send for your copy NOW - it is

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- Advanced Electronics**
5a The Quadrant, Launceston Tas. Ph 317 075
- Aero Electronics**
123a Bathurst Street, Hobart Tas. Ph 348 232
- Peter Brown Electronics**
9 Davon Street North, Ballarat Vic. Ph 323 035
- Crystal TV Rentals Pty Ltd**
86 Crystal Street, Broken Hill NSW. Ph 6897
- Decro Electric**
Cnr Magellan St & Brunner Hwy, Lismore NSW. Ph 214 137
- Elektron 2000**
181 Wharf Road, Newcastle, Ph 262 644
- Hital Hi Fi**
Shop 12, Ventura Arcade, High St Penrith. (Also at St Marys)
- Hutchesson's Communications**
5 Elizabeth Street, Mt Gambier SA. Ph 256 404
- Keller Electronics**
218 Adelaide Street, Maryborough, Qld. Ph 214 559
- M & W Electronics**
48 McNamara Street, Orange NSW. Ph 626 491
- Mellor Enterprises**
Shop 2/15 Forsythe St, Whyalla, Norrie, SA. Ph 454 131
- Power & Sound**
147 Argyle Street, Traralgon, Vic. Ph 743 638
- Purely Electronics**
15 East Street, Rockhampton Qld. Ph 21058
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42 Victoria Street, Mackay, Qld. Ph 511 723
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- Variety Discounts**
113 Horton Street, Port Macquarie NSW. Ph 835 486
- Viking Electronics**
3108 Gold Coast Hwy, Surfers Paradise, Qld
- Wagga Wholesale Electronics Sales**
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- Wellington Electrical Services**
110 Lee Street, Wellington NSW. Ph 325

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It's an alarm module that doesn't look like an alarm module! Handsome wood-grain finish. Looks like a small speaker. Inside is the complete 'works' for a professional quality home or office alarm system. Link it to sensors (see below) and you can turn your home into a veritable Fort Knox! Installation is easy, any handyman can do it!



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INFRA-RED BEAM ALARM

Great for hallways, doorways (shop doors especially). Easy installation, just connects to master alarm system. Complete with infra red reflector.

\$89



\$49.50
Cat L-5102

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REED SWITCHES
Twin set of magnet and reed switch. Wire them into windows and doors for protection.
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Hide under carpets, mat etc. Pressure of person walking sets it off.
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CAR PROTECTION

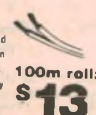


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Termination blocks for above. Cat L-5205 **30c each**



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THE PAKETTES AVAILABLE (only from Texas Instruments):
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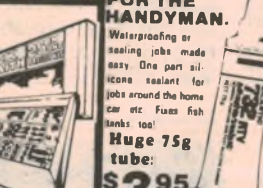
For the weekend boating set take along a bit of security - this handy marine transceiver. Huge 5 watts output (maximum legal power), with 6 channel capacity (comes with one channel fitted on the 27.88MHz boating safety channel). Comes with illustrated case - attractive and durable. Easy to use - and it's handy to find out where the fish are biting!

Cat D-1120. Approved by the PBT Dept for operation on the 27MHz marine band.



SOLAR KIT: 25-IN-1 EXPERIMENTS

Top value for a gift for the budding scientists in your family. 25 experiments in electronics using solar power. Up-to-the-minute technology. Solar power!
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PLUG-IN TIME SWITCH

Incredible! Up to 3 on/off actions per 24 hours, fully soft-start, auto and manual control. Contacts rated at 2400 watts (same rating as your power point), your blenders, simply plug in. Pool filters, security lights, battery chargers, electric blankets, etc etc. Auto or manual control too.
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Kit includes all parts to build the module. Add a transformer, heatsink and case and you have a complete mono power amplifier capable of 300W output!
NOTE: If you plan to use the amplifier at full output you will need two of the heatsinks and a cooling fan.
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\$1.00
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COMPUTER PHONE DIALLER with 32 number memory!

- Phone dialler
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- Number Store

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\$179.00

Cat X-1178

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Dick Smith and Staff

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HIDE IT!

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\$2.75

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Includes pages of actual treasure maps and lots of useful data.

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IS THIS THE ULTIMATE?

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Handy size, full of information. Take it along on your next trip. Cat B-4625

\$1.95

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You asked for them here they are. TO-3 package, a massive 5 amp rating. Great for computer power supplies, etc. etc. Cat Z-8570

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Hi-Fi Topics

Microphones, music, reverb. and all that!

During a recent lecture-demonstration in Sydney, Dr Fritz Sippl of AKG dealt at considerable length with psychoacoustics, or subjective reactions to sound. Implicit in the lecture was a conviction that AKG has a firm grasp of the field in which they are active — undoubtedly the message AKG wanted to get across!

by NEVILLE WILLIAMS

A notable feature of Dr Sippl's presentation was its low key efficiency and the complete absence of the bull-dust and ear-crushing sound levels which commonly characterise audio/hifi demonstrations.

Although surrounded by quality microphones (AKG, of course), a multi-channel mixer and an array of other gear, the lecturer quickly realised that sound reinforcement was not really necessary in the excellent acoustics of the Sydney Science Centre. He turned the mics right off and addressed the audience face-to-face from the floor of the lecture hall.

And when the time came to demonstrate mics and reverb units, the sound pressure levels were adjusted to what one would expect from an orchestra in a concert hall, or a grand organ in a cathedral. Perhaps the values of AKG's home city of Vienna were showing through!

There was a moment of confusion to do with the audio-visual presentation. The sound came through very clean but was also rather loud. It didn't stay that way for long.

Dr Sippl went over to the amplifier and actually turned it down!

As a member of the audience, I couldn't escape the feeling that there was a message on the day for promoters of other audio/hifi products, in respect both to the presentation and the venue.

Speaking first about microphones, Dr Sippl emphasised that they can no longer be regarded as devices — good, bad or indifferent — intended merely to pick up sound. They now have a very



Dipl. Ing. Fritz Sippl, MAES, Director (Market Development) for AKG Acoustics, Austria, represented in Australia by AWA.

active role in producing the kind of sound that a musician wants and must therefore be regarded as one of his/her tools of trade, along with an ever increasing array of other electronic aids.

Time was when microphones could be divided roughly into three groups: (1) "Cheapie" types intended for non-professional applications, tape recorders, communications, paging etc; (2) Public address, platform and stage microphones with the emphasis as much on ruggedness as on audio quality; and (3) studio microphones with the emphasis on quality and on the assumption that they would be treated always as delicate, precision instruments.

The distinctions between the three classes are now less distinct. Cheapie microphones generally are capable of much better quality, while AKG in particular are effectively bridging the "impossible" gap between ruggedness and quality, and offering microphones which meet both requirements.

According to Dr Sippl, pressure to achieve the impossible can be traced to the ever-changing pop music scene. By and large, the reputation and the "sound" of individual groups is established by their recordings, made under studio conditions.

But groups also have to perform live on stage and, if their sound is not clearly recognisable to the fans, concert

appearances can become an embarrassing anti-climax. They simply have to go on stage with full electronic paraphernalia and top quality mics — even though those same mics are subjected to brutal treatment during the course of a performance.

AKG's latest answer to this problem is their 300-series "musicians" dynamics: the D310, the D320B and the top-of-the-line D330BT. While credited with studio-quality sound, the new microphones are built to withstand very rough treatment. While using a D330BT, Dr Sippl gave the audience repeated jitters by deliberately throwing it on the floor, sideways, end-on, etc, then picking it up and carrying on with the demonstration. It appeared to be completely unaffected, either physically or electrically.

The reason for this ruggedness was revealed when he unscrewed the stainless steel outer grille to reveal a washable anti-pop cushion and, beneath it, a shock absorbent plastic basket designed to have a progressive resistance to mechanical distortion. Inside that again is the plug-in electroacoustic element, fully cushioned within the main zinc alloy die-cast housing.

As the demonstration showed, it is a very simple matter, even for a non-technical person, to dismantle a 300-series microphone and insert a new

Operators of radio, TV and recording studios should address inquiries about AKG products to Bill Bolton, AWA Engineering Products Division, 422 Lane Cove Rd, Nth Ryde, NSW 2113; phone (02) 888 8111. Otherwise to Adrian Wackwitz, National Product Manager Audio, AWA, 554 Parramatta Rd, Ashfield NSW 2131; phone (02) 797 5757.

acoustic element in the event that something does fail.

The carefully designed suspension obviates much of the noise that might otherwise be produced by handling — an important characteristic in any microphone that is likely to be handheld. In addition, potentially explosive transients due to bumping or dropping are curtailed, thereby safeguarding also the loudspeakers in the P.A. system and the ears of the audience!

All three in the 300 "Musicians" series mics have an inherent "presence" characteristic: a gentle prominence extending from about 2kHz to 12kHz and reaching about 6dB at 5kHz. A miniature 3-position switch in the D330BT provides the option of varying the "presence", while another similar switch allows the bass response to be rolled off quite severely. Bass roll-off only is available on the D-320B.

Dr Sippl stressed that these characteristics are what musicians, and particularly vocalists, currently demand. For the most part, they simply do not want a microphone with a completely flat top response. In fact, the slightly undulating top response of the D310 is a deliberate provision for one of their often stated preferences.

Said he: "Don't ask me why; we only know that musical fashions change with the period."

At the bass end, the curves may not be what they seem, because a bass boost effect operates when the microphone is very close to the sound source. Thus a microphone which exhibits a built-in bass roll-off when measured at one metre, may seem flat or even bass boosted when used close-up due to the so-called "proximity" effect.

Vocalists rely on this fact when they wish to project an intimate, sensual mood.

But if they want to emphasise to the audience that "I hate you", full sensual bass would be all wrong. For that number, bass cut would be preferred. Similarly, bass cut could also be used if the venue presents problems with building rumble, acoustic feedback and so on.

Microphone directivity is another vitally important quality. Omni-directional or bi-directional microphones have an important place in studio situations where the acoustic environment has been carefully designed and controlled. However, for general use, so-called cardioid pattern microphones are much more practical, with a response which is (hopefully) confined to the hemisphere in front of the diaphragm.

With such a pattern, microphones can be positioned so that they favour sound from the performer (or stage), while attenuating sound from the audience, or from the public address loudspeakers. The higher the front/back ratio, and the greater the freedom from response peaks, the less

WHATEVER YOUR CASSETTE NEEDS — SONY CAN MEET THEM!

Already prominent in the audio cassette field, Sony have recently rationalised and up-dated their range, with the obvious intent of providing a tape for every need — from general purpose ferric to pure metal particle. All you need to understand the range is an eye for colour or an ear for initials!

First off, all the new tapes use the Sony "SP" cassette body, the initials standing for "Super Performance" mechanism. Of screwed construction, the body contains guides, stepped hubs, and ribbed liners, all aimed at ensuring the smoothest possible tape run during actual use. Sensor slots are provided for CrO₂ tapes and generous viewing ports so that the tape remaining on the spools can readily be seen.

Now for the individual cassettes, the initials and the colours:

- CHF — Orange: A general purpose ferric tape, broadly equivalent to the earlier low-noise type. Normal bias and normal (120uS) compensation. Available as C30, C46, C60, C90 and C120. The cheapest tape in the range, at the old "low noise" price.
- BHF — Green: New to the range. A somewhat more expensive ferric tape, still requiring normal bias and equalisation but with slightly higher output and extended top response. Suitable for all applications. C46, C60, C90, C120.
- AHF — Blue: Similar to, and priced the same as the earlier HF tape. A top grade ferric tape, for normal bias and equalisation, but with improved output, dynamic range and treble response. C46, C60, C90.
- CD — Alpha — Silver: A top quality chromium — dioxide tape, re-



quiring CrO₂ bias and equalisation. Intended for top quality recording. C46, C60, C90.

- FeCr — Gold: Regarded by Sony as their Top-of-the-line conventional tape. Double layer, similar in specifications and price to the earlier Ferrichrome tape and suitable for top quality applications. Normal bias but equalisation the same as for CrO₂ (70uS). C46, C60, C90.
- Metal: A recent addition to the range is a pure iron particle tape for use with decks having "metal tape" facilities. A C46 cassette is currently available for \$12.50 retail, but C60 and C90 cassettes will be available shortly.

Further information is available from Sony outlets or direct from Sony (Australia) Pty Ltd, 453 Kent St, Sydney, 2000.

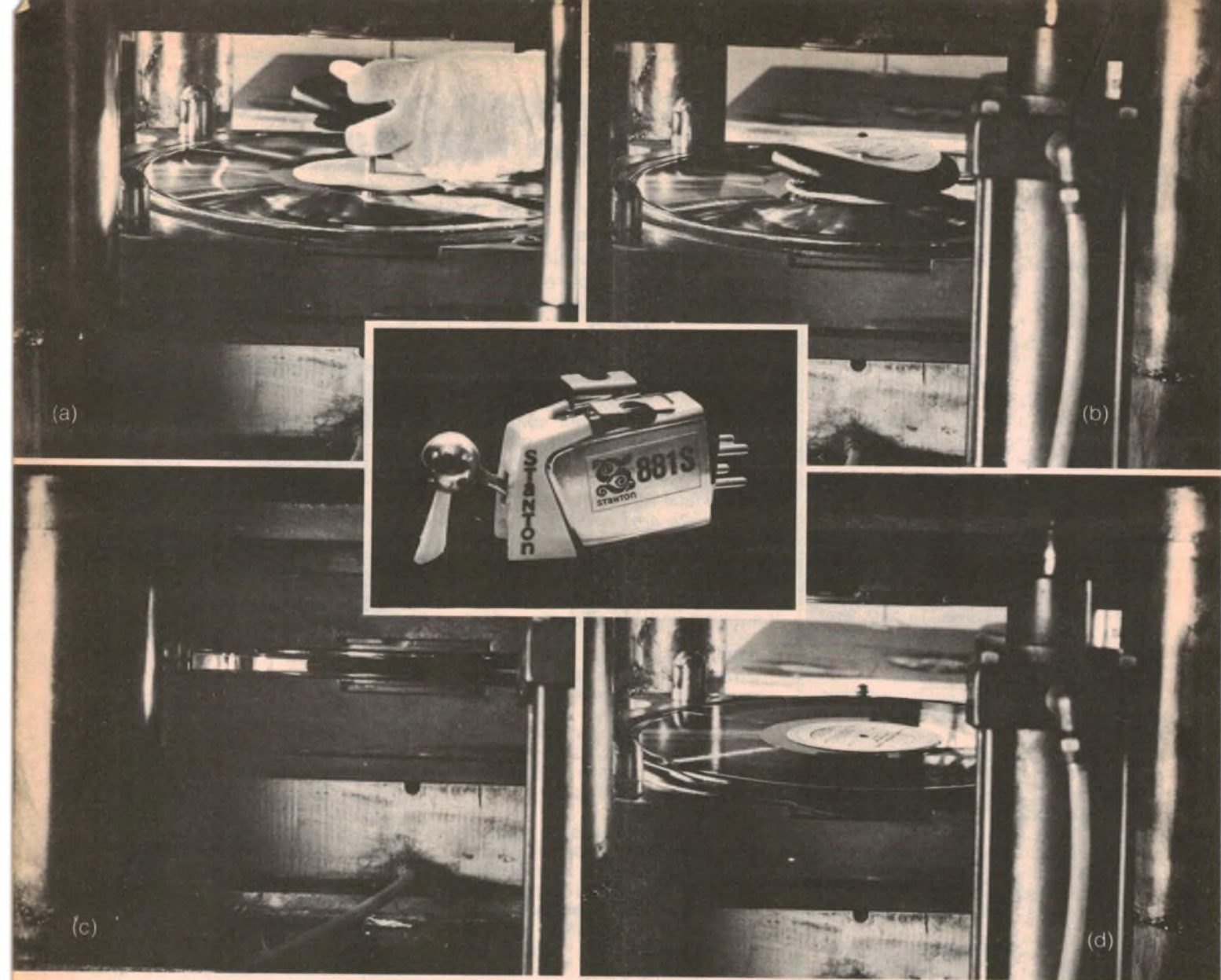
likely the problem of acoustic feedback.

Dr Sippl pointed out that the cardioid pattern is normally obtained by admitting sound arriving from the back of the microphone to the rear surface of the diaphragm. By balancing the amount of sound so admitted against what would reach the front of the diaphragm from the rearward source, a substantial degree of cancellation can be achieved.

Unfortunately, it is difficult to achieve good cancellation over a wide range of frequencies. It often transpires

that a microphone having a good cardioid pattern and a good front/back ratio at 1000-2000Hz, may have quite poor directivity at lower and higher frequencies. In their 300 series, AKG employ a twin access system for rearward sound to extend the cancellation and produce a more uniform cardioid pattern.

Where directivity is a paramount consideration, AKG can offer their 200 series which, in fact, use two complete transducer systems in tandem, one covering the range from 800-20,000Hz and the other from 800Hz down to



Stanton-The Professional in The Recording Industry

Application — Stanton monitors the quality of the pressing

Record pressing is one step in the process that delivers sound to you. The process begins when a premeasured amount of pure poly vinyl chloride preheated to 300 degrees is dispensed in the form of a vinyl biscuit (a) which is sandwiched between the two record labels (b). The biscuit is then squeezed between two nickel plated stampers by a hydraulic press (c) spreading the vinyl to form the record, (d) which is then trimmed and stacked for testing and packaging. The average press turns out 8500 records daily. Last year's largest single pressing of a particular album was over 14,000,000 copies.

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A REVOLUTIONARY NEW COBALT TAPE

A practical microcassette music system may be just around the technological corner!

Hard on the heels of metal-particle tape comes an announcement by Matsushita Electric of "Angrom" — a radical departure in technology which eliminates the binder and results in a thinner tape, with undiminished strength and up to ten times normal data storage capability.

With all conventional tapes — whether oxide or metal particle — the powdered magnetic material is first suspended in a resin-based adhesive binder, and then coated on to the plastic tape base. The coating is usually about 3 microns thick, compared with about 6 microns for the base, so that it adds significantly to the total thickness — and to the bulk when the tape is spooled.

No less to the point, only about 30% of this added thickness (and bulk) is represented by useful magnetic material; all the rest is binder, serving only to keep the particles in place, and to stabilise them chemically in the case of pure iron.

In the new Angrom tape, the magnetic coating is a cobalt derivative and is applied directly to the polyester base film by an "evaporation" process. The technology is apparently related to that involved in the manufacture of metal film capacitors and is therefore well known. The breakthrough by Matsushita has been in extending it to a continuous coating process and in achieving adequate adhesion and wear resistance. It is about five years ahead of what the industry expected, they say.

Having the appearance of a bright, plated surface, the new cobalt coating is only 0.2 microns thick and barely adds to the thickness of the base film. It gives the option of using a thicker film for additional strength, or of retaining the original film and increasing the length and therefore the playing time by about 50%.



Above: The National Panasonic 2-speed microcassette recorder RN-Z06. It works well with a conventional microcassette but Angrom tape offers improved high frequency response.

Measuring 50 x 33 x 8mm, a microcassette pictured left, is tiny by comparison with the normal compact cassette. But it is being considered as the basis for a new miniaturised music system.

The highly homogenous coating offers a much improved high frequency response at low speeds but can operate with normal bias and erase levels.

At present, Matsushita are talking about their Angrom tape only in the context of the microcassette, which, at the moment, is mainly used for verbal note-taking and other voice recording. We tested it in connection with National's new RN-Z06 microcassette two-speed recorder, as pictured.

At the normal speed of 2.4cm/sec and loaded with Angrom tape, the RN-Z06 had high frequency response to spare on voice, with sibilants somewhat exaggerated. At half speed, giving a playing time of 90 minutes per side, the sibilants largely disappeared but voice quality was still eminently satisfactory.

While an Angrom-equipped RN-Z06 would have obvious attractions for an itinerant business executive, the hot tip is that Matsushita (National-Panasonic) are looking beyond it to a microcassette music system. If they can solve the problems of miniaturised deck design, the 10:1 improvement in data storage offered by Angrom should provide the tape they need.

Angrom microcassettes should be on the market in Australia within the next two or three months but microcassette music systems are further back in the pipeline.

HIFI TOPICS: Microphones, music, reverb. — continued.

around 30Hz with switchable bass cut to compensate for possible proximity effect. With this series front/back ratio is maintained in the region 15 to 20dB across the audio spectrum.

For still greater directivity and a narrower frontal lobe, AKG offer a number of "machine gun" microphones, in which the transducer element is mounted at the rear end of a long tube, being in effect an acoustic resistance line. Sound arriving directly from the front passes down the tube to the transducer; sound from the sides and rear are subject to cancellation.

But again the warning was sounded: super-directional qualities are only as

good as the basic design and not all microphones with long frontal tubes exhibit good directivity at all frequencies.

Dr Sippl also demonstrated a number of AKG "condenser" microphones, including module kit types, where various transducers, amplifier and fitments can be assembled in different ways to meet particular requirements. Also demonstrated were electret condenser units, which have more recently been introduced into the AKG range.

Questioned about the apparent delay, the lecturer said that his company wanted to be satisfied that they could offer such microphones with the

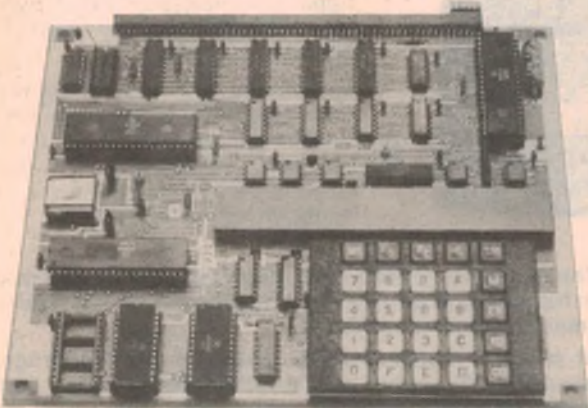
confidence that they would retain their characteristics during a reasonable service life. In no way was AKG prepared to market something that could lose its sensitivity within four or five years, as some electrets had reportedly done.

Dr Sippl said that he tended to avoid the word "electret", because it had acquired an association with inexpensive mass-produced units built into tape recorders, etc. He preferred to think of them as permanently polarised condenser microphones, and legitimate alternatives to the externally polarised types.

The lecturer also drew attention to AKG's current range of phono car-

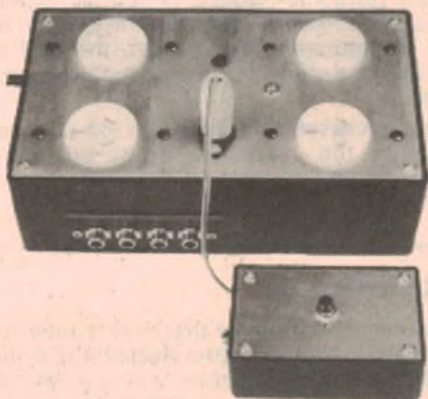
Next Month

Don't miss our review of the Motorola 6802D3 microcomputer



Our March issue features an in-depth review of Motorola's new MEK6802D3 microcomputer, which replaces the old workhorse 6800D2 evaluation kit. The new unit uses 6800 hardware and software and is greatly expandable. Get hold of the March issue for the details.

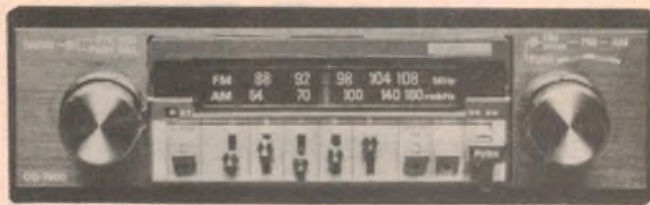
Automatic Switch for your hifi system



Here's a really neat addition for your hifi system. It monitors the tape output terminals of your stereo amplifier and, if no audio signals are received for a period of 30 seconds, automatically switches off the mains power. As a bonus, the unit acts as a junction box so you can tidy up those unsightly mains cords from all your equipment.

Our planning for this issue is well advanced but circumstances beyond our control may change the final content. However, we will make every attempt to include the articles mentioned above.

HIFI TOPICS — continued



The new National Panasonic model CQ-7600 AM/FM car stereo radio tuner and cassette system, boasts a 5-band graphic equaliser, Dolby noise reduction, auto replay on cassette, tape direction indicator lights and more. It is designed to mate with Panasonic's 4-speaker main amplifier, model CJ-3000 and with recommended dual-cone and coaxial speakers. The cost of the complete in-car hifi system would approximate \$730, plus installation charges. (National Panasonic Aust. Pty Ltd, 57-69 Anzac Pde, Kensington NSW 2033.

tridges and headphones, but it was the final demonstration of AKG's artificial reverberation that really stole the show.

Dr Sippl emphasised that a reverberant content is not an optional quality in our sound environment. Subjectively, we need it.

A person confined in an anechoic chamber becomes acoustically disorientated, because the clues are missing by which they normally position themselves. Similarly, confinement in an echo chamber can be emotionally quite disturbing.

It is only to be expected, therefore, that reproduced sound should exhibit the right kind of reverberant quality if it is to be subjectively satisfying and convincing. Cave, cathedral, concert hall and chamber all have their own distinctive kind of reverberation.

Unfortunately, recording groups do not always have economic access to ideal venues and rather than accept a totally wrong ambience, it is reasonable to seek a method by which reverberation and ambience can be synthesised. Hence the various artificial systems which have been devised, with varying degrees of success.

Echo chambers, echo plates, tape loops and simple Hammond-type spring systems have obvious disadvantages and even the more modern "bucket brigade" systems have proved to be disappointing because of their discrete echoes, their uneven frequency response and their poor signal-to-noise ratio.



Through an unfortunate combination of circumstances, Yamaha missed out in last month's review of cassette decks. Currently, they have four models of which the TC-1000 is currently top of the line. It offers a wow and flutter figure of 0.05%, a response to 18kHz with CrO2 tape and a signal/noise ratio of better than 60dB, even without the in-built Dolby anti-noise circuitry. Facilities include dual line outputs, separate headphone amplifier and full mic-line mixing. Yamaha is represented in Australia by Rose Music in Sydney and Melbourne and retailed by hifi stores around Australia.

Toshiba Micro HiFi

Toshiba's new System 10 micro components series offers a 20+20W integrated amplifier, an AM/FM stereo tuner with AFC and a metal-compatible Dolby cassette deck. Toshiba are at 16 Mars Rd, Lane Cove, 2066.



AKG's answer to the problem is a combination of their own spring system and a digital system involving A/D conversion, digital storage and delay, then D/A conversion and re-mixing. The equipment demonstrated in Sydney was an up-date of equipment that produced quite a sensation in Europe some years ago, and reported in our May 1975 issue (page 9).

The spring system is basically similar to that developed by Hammond for use on electronic organs but the springs have been critically designed and interconnected to ensure a response within a + and -5dB strip over the audio range, with good signal/noise ratio and freedom from electrical and acoustic penetration. Selectable reverberation times from 1.5 to 4.5 seconds are available, depending on the model.

While spring reverberation of this type can be very effective, it lacks an important characteristic of true building reverberation: the discrete bounces which follow the original sound, depending on the major dimensions of the auditorium. A digital system can provide these missing "clues" and can be set up easily to provide the desired number of bounces, their relative delays and relative amplitudes.

To demonstrate the potential of the system, Dr Sippl played an excerpt by as much of an orchestra as could be

crowded into an anechoic room. Unprocessed, it was dull indeed.

With purely digital repeat added, it sounded rather like two voices and two orchestras playing slightly out of step in a larger chamber; or three voices and orchestras, or four, and so on.

With only spring reverb, the effect was more natural but still not quite convincing.

But with spring and digital in operation, and set up to give the right mix of bounce(s) and ambient, the anechoic chamber had been transformed into a concert hall. Similarly for recording of an organ in a cathedral and so on.

Dr Sippl capped off the demonstration by revealing that some of the signals we had heard processed were not even stereo to begin with. The Science Centre had been filled with all-pervading sound from a mono original!

The whole point of it was not to convince the audience that all sound should henceforth be reverberated as a matter of course. The intention, rather, was to indicate the resources which now exist to enrich and enhance recordings where the need exists.

If you can't take an orchestra to a concert hall, then you can do it the other way round.

And, if your listening room, by necessity, is of closet-like dimensions, technology is one way to push the walls out — acoustically at least!

Metal particle tape announced by BASF

Well known for their range of conventional oxide tapes, BASF are planning to release their new metal pigment (pure iron particle) cassettes as soon as practicable. They will be marketed as "Metal IV" and be available in two forms: C60 and C90. BASF say that manufacturers have agreed on an equalisation standard of 70uS, as for CrO2 tape, and on a case design which will activate automatic sensing in future decks. However, some of the other characteristics remain to be standardised before BASF — or any other company — can issue a true reference standard tape for the industry. The subject is under constant discussion



between involved companies in Germany, the Netherlands, Japan and USA. For further information, contact Mr N. Price, BASF Australia Ltd, 55 Flemington Rd, Nth Melbourne 3051.

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Specs.

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YES! Don't take the risk of having non-approved CBs confiscated on arrival in New Zealand. And why put up with exorbitant prices for 'unknown' brands at home?

CB ACTION received a copy of the price list put out by [redacted] in Christchurch and we were surprised by the price of rigs and accessories.

The cheapest 11 channel 2 watt transceiver listed on the brochure was \$275 for a Great GT418. The most expensive was \$299.50 for a Laser 555. Both rigs have only 11 channels with 2 watts AM output which is the maximum allowed under NZPO rules.

The price list also included some accessories and while antennas were slightly higher than Australia, supplies and external speakers were very expensive.

For example, a combined power supply and speaker retails for between \$64 and \$85, according to the list. The supplies probably would not be rated in excess of 1.5 amps continuous unless the transceiver.

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 RIPPLE : 2mV RMS
 LOAD REGULATION : 0.04% or 10mV

TYPE NO.	VOLTS	AMPS
ECA160-12/3	0-12	3.0
ECA160-24/1.5	0-24	1.5
ECA160-35/1	0-35	1.0



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FERGUSON TRANSFORMERS PTY. LTD.
 31 HIGH STREET, CHATSWOOD, N.S.W. 2067.

Philips GP-412 II moving-magnet cartridge

The GP 412 II, successor to the outstanding GP 412 VE, is one of the top of the range of Philips Super-M series cartridges. Weighing 6 grams, it has a bi-radial stylus and recommended tracking force of 0.75 to 1.5 grams.

The Philips cartridge is supplied in inexpensive but attractive packaging in the form of a black plastic case. Included with the cartridge are spare mounting screws, some pin connectors and a miniature information booklet.

Operating on the magneto-dynamic (moving magnet) principle, the GP 412 II cartridge uses a very high flux density magnet to make it possible to reduce the moving mass to below 0.1 milligram, while still keeping the sensitivity at a sufficiently high level. Philips claim that with such a low tip mass to enable high compliance, excellent trackability is obtained.

At 6 grams, the GP 412 II is a light cartridge. It has a bi-radial stylus, 7 x 18 microns and the standard (EIA/DIN) vertical tracking angle of 20 degrees. Inductance of the cartridge is 620 millihenries and DC resistance is 1400 ohms. Output voltage at 5cm/sec is 7.5 millivolts.

Integrated with the removable stylus assembly is a flip-down stylus cover which is more useful than detachable covers which are likely to be misplaced. The stylus cover has click stops which are very positive, providing good protection for the stylus when in the down position.

Mounting the cartridge in a standard headshell is a straightforward process. The cartridge has the standard 12.7mm mounting centres and its output terminals are coded with embossed lettering on the cartridge body.

We used the manufacturer's maximum recommended tracking force of 1.5 grams and this gave very good tracking performance. On the CBS STR 110 test disc, the GP 412 handled all the high-level 300Hz tracks without audible distress, although some visible waveform distortion occurred on the +18dB lateral test track.

On the W&G 25/2434 test/disc, the GP 412 only slightly mistracked on the +16dB drum track. At lower signal levels, distortion was not apparent. With the Shure "Audio Obstacle Course", the cartridge displayed virtually faultless tracking except for some

mis-tracking on the "violin level 5" test. Overall then, the cartridge has very good tracking performance.

We tested the cartridge with the recommended load of 47k, shunted by cable and test instrument input capacitance of 180pF. With this loading the frequency response was very smooth and within ± 3 dB from 20Hz to 20kHz with the exception of a resonant

At right, the Philips GP 412 II moving magnet cartridge shown in its presentation case.



peak of +5dB at 15kHz. Channel balance was within 0.5dB over most of the range.

Separation was uniformly wide over the whole audio range. We measured it as 20dB at 1kHz in one direction and 35dB in the other. At 10kHz the respective figures were 20dB and 22dB. Even at 20kHz the figures were 20dB, however, at the region of resonance (15kHz) the separation dropped to -10dB.

Square wave response at 1kHz was very good, with only slight ringing. Response to sinewave signals exhibited only slight sawtooth shape at the 6kHz to 20kHz region which is normal for most cartridges. At lower frequencies the sine wave response was excellent.

On listening tests the GP 412 II performs very well and confirms the high performance indicated by the measurements. There is a smooth response on all types of music ranging from classical to rock. Above all the sound is very clean without muddiness and provides excellent clarity.

In summary, our overall impression of the GP 412 II is very favourable. It performs well with excellent trackability and smooth response. Recommended retail price is \$118.88 + 27½% sales tax. Further information on Philips products can be obtained from high fidelity retailers or from Philips Service, 443 Concord Road, Rhodes, NSW 2138, or from branches in your nearest state capital city. (JC)

Play cassettes through your car radio

Although in no sense a piece of hifi equipment, a unit currently being offered by Classic Radio and ACE Radio will certainly appeal to the music enthusiast with a limited budget. For around \$20 it can turn an ordinary car radio into a cassette player.

Although intended primarily for use in a car, the BICOH converter illustrated below can be used with any AM radio system.

These days, a great many car radios have the cassette replay facility in-built but there are countless others which are limited to off-air music. In urban areas this may be adequate but, on longer journeys, the ability to relax to a handful of favourite cassettes is an undoubted advantage.

The BICOH cassette converter model CC-007A, currently being offered by the two abovementioned firms, offers a neat solution to the problem. It is essentially a cassette player with an in-built 3-transistor amplifier, which modulates an RF oscillator, preset to the middle of the AM broadcast band. The signal can be tuned on an AM receiver in the same way as a broadcast station, with the receiver volume and tone controls performing their normal function.

Electrically, connection to the receiver is very simple. The normal car radio antenna lead is plugged into the converter and a jumper lead, supplied in the package, completes the connection to the receiver. As far as the radio is concerned, it is a straight-through connection but a small capacitor injects the additional signal, when the converter is in use.

NEGATIVE GROUND

Connection is also required to the +12V supply line in the car and this involves a single lead with its own fuse fitting. It is important to note that the converter is designed only for a negative-ground system, with the return circuit being provided by the mounting arrangements. The current drain is quoted as a modest 200mA, indicating the use of a "battery" style transport mechanism.

The converter is quite small, measuring nominally 110mm wide x 53mm high x 150mm deep. As such, there should be a reasonable chance to find a spot for it in most vehicles. Basically, it is intended to sling beneath the fascia, within reach of the driver, and brackets are provided with this in view. It must protrude far enough to allow the cassette to be inserted into the top of the unit.

Controls are limited to three push



buttons: power on/off; eject; and play. There are no spooling or rewind facilities and, of course, no provision for recording. The assumption is that the converter will be used with cassettes which have been pre-recorded and which will be played through and turned over as necessary.

Loading and changing cassettes tends to be a little on the fiddly side, but should not present too much of a difficulty if the unit is strategically placed.

By hifi standards, the specifications are modest indeed with wow and flutter quoted at 0.35% and signal/noise ratio at "more than 30dB". Having in mind that these figures apply only to replay and are not cumulative record/replay figures, they do not impose any significant limitation on the sound, as heard through a normal car radio.

Indeed, signal/noise ratio, distortion and certainly the frequency response would be substantially that of the car and radio system. In practice, it is reasonable to assume that the converter will sound like an ordinary AM transmission — except that you control it yourself!

The converter is set to a nominal 830kHz, suggested by the manufacturers as a normally unused frequency. This would not necessarily be true in all areas of Australia but a trimmer is provided (accessible through the PC

board on the underside) to permit a frequency adjustment of plus and minus 50kHz.

The level of RF signal produced is quite small — adequate for a car radio installation but certainly too small to cause any problems with general radiation.

As a matter of curiosity, and to get a better idea of the basic sound, we connected the converter to an AM tuner — part of a normal hifi system. To couple to the ferrite rod antenna, we wound a half-dozen turns around it and took the respective ends to the inner and outer connections of the converter output cable. And although subjected to the normal sideband losses of the AM tuner, cassette quality sounded quite clean, with good bass. Overall, it was eminently listenable.

This would suggest that anyone with an existing AM system, and able to provide the requisite filtered DC (12V at 200-plus milliamps) could add cassette playing facilities in a very cheap and compact form.

The unit, as inspected, was supplied by Classic Radio of 245 Parramatta Rd, Haberfield NSW 2045. Phone (02) 798 7145. Advertised price is \$18.50 plus \$1.50 post and package. We understand that the converters are available at the same price from ACE Radio, 136 Vic-torial Rd, Marrickville NSW 2204. Phone (02) 51 3845. (WNW)

The new generation of factory-built or kit-set Peerless loudspeakers



It's true most speakers *look* alike and that price alone never tells the whole story. But now the new generation Danish-built Peerless loudspeakers give you a recognizable difference in sound quality—a difference that has set Peerless a notch above the others for over 50 years.

The range of new generation Peerless loudspeakers includes the fully assembled *PAS series* plus the money-saving *PLK kit-sets*. Both series contain drive units with the following characteristics.

Peerless 'X' Line Woofers

- Large ceramic ferrite magnets for high power handling.
- Specially coated cones reduce colouration to a minimum.
- Cones are supported by a single-roll foam or rubber surround to maintain excellent linear motion.
- Bass response is clean and tight at all listening levels.

Peerless Midrange Units

- Sealed back units prevent interaction with the woofer. Distortion and colouration are reduced to a minimum.
- The rear side of the cone is coated with a special damping material to eliminate colouration.
- Specially impregnated polyurethane cone rim provides high degree of linearity.

Peerless Tweeters

- Dome tweeters designed for the highest accuracy of reproduction with low distortion flat response and wide dispersion.
- The sealed back isolates the tweeter from interference.
- Specially developed dome fabric ensures no degradation of performance even after prolonged heavy loading.
- Assembly mounted on a precision diecast plate where rigidity ensures permanent alignment.

Peerless Dividing Networks

- Peerless crossovers use air-cored chokes for maximum power handling, and special electrolytic capacitors to ensure long term reliability.
- All components are mounted on fibreglass printed circuit boards for maximum durability, while coded clip connectors eliminate the need for soldering.

Power handling

The power handling capacity is high and conservatively rated at 100W RMS, however, due to the high efficiency of Peerless speakers, the recommended amplifier power is between 25-100W RMS.

Whether you settle for the smart timber-veneered PAS assembled series or the PLK kit-set, you're getting the same Danish-made Peerless quality—a quality selected by many of the world's most reputable names in loudspeakers, for inclusion in their own speaker systems.

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AUDIO TALK

by LEO SIMPSON

Transformers and Solid State Amplifiers

In our "Circuit and Design Ideas" pages for this month there is an idea proposed by one of our readers for varying the speed of a turntable which has an induction or synchronous motor. The method involves feeding an audio signal into one channel of a stereo amplifier which drives a step-up transformer to feed variable-frequency 240VAC to the turntable motor.

On the face of it, the idea is worthwhile but a number of objections can be raised. As I thought about the subject, it seemed unfair to try to allude to them all as a notation to the reader's idea, without seeming like the proverbial wet blanket. So, we overcame this without offence to the contributor concerned (I hope) by referring readers to this column.

The fact is that there are quite a few potential problems inherent in connecting transformer loads to solid-state amplifiers. Consider first the transformer problem which is most easily solved: direct current (DC) in the transformer primary.

This problem can readily occur when a direct-coupled amplifier is used to drive a transformer. To give an example, if the DC amplifier has a DC offset voltage at the output of 50 millivolts (positive or negative) and the transformer primary winding has a DC resistance of 100 milli-ohms, then the current flowing in the transformer primary would be 500 milliamps. Yes, half an amp!

Clearly, the amplifier would not survive for very long if this situation was maintained. Again, the transformer would be pushed toward saturation, even if the amplifier could sustain such a load.

It may seem that I have picked a rather extreme example to illustrate the point, but that is not the case. It is quite conceivable for a DC amplifier to have a DC offset voltage at the output of up to 100 millivolts, and that this would not cause problems with a conventional loudspeaker load. It is also quite conceivable for a transformer to have a very low primary resistance, particularly

if it is a high quality auto-transformer intended for high fidelity or public address applications.

Fortunately, this problem can be easily circumvented by connecting a large value non-polarised capacitor (or two electrolytic capacitors back-to-back in series with the output of the amplifier. Alternatively, some, if not most, DC amplifiers have a means of offset adjustment which can be set to minimise any offset voltage at the output.

A second problem which may arise when a transistor amplifier is used to drive a transformer is instability. Depending on the characteristics of the transformer and the phase margin of the amplifier, the resulting instability may take the form of supersonic oscillation or low frequency "motorboating".

There is no easy cure for this problem, short of modifying the amplifier. If the amplifier specifications make a claim to "unconditional" stability, then it is fairly safe to assume that it will drive a transformer satisfactorily, but subject to the constraints outlined in the following paragraphs.

The following set of problems may apply to any transistor amplifier driving a transformer, whether or not it has unconditional stability and freedom from DC offset at the output. The first of these problems occurs when the amplifier is subjected to overdrive, ie, it is driven into clipping. Depending on the inductance of the transformer, this may generate excessive voltages across the output transistors which could cause failure.

Amplifiers which are specifically designed to drive inductive loads such as transformers and motors overcome this problem by connecting reverse-biased power diodes across the output transistors. Thus any "spike" voltages generated by the inductive loads are bypassed safely to the amplifier supply rails.

Two potential problems remain to be discussed and they are both related to "second breakdown" of the amplifier's output transistors. In the first case, just

driving the transformer above a certain power level (which may be well short of clipping) may cause the output transistors to exceed their "safe operating areas" and subsequently be damaged by "second breakdown". By way of explanation, "second breakdown" is an effect whereby, at high voltage and high currents, the voltage distribution across the semiconductor chip causes current "crowding" and localised hot spots which can cause failure of the device.

Some amplifier designs take special measures to avoid "second-breakdown" of the output transistors by including "load-line" protection circuitry. This circuitry monitors the voltage and current conditions through the output transistors and switches off the transistor drive should the load line be exceeded. What can happen when this sort of circuit interacts with a transformer or other inductive load is that the voltage spike generated when the output transistor is turned off may cause it to turn on again. The result is a burst of high frequency oscillation on the signal waveform. So the protective circuit can give rise to considerable distortion when used with a highly inductive load.

To some experimenters who have successfully used transistor amplifiers to drive transformers, all the foregoing may sound unnecessarily alarmist. However, their degree of success may have just been a lucky coincidence. Whether or not the match between amplifier and transformer is compatible depends on the parameters of these components.

I can summarise the message of this month's column by stating that if you propose to connect a transformer to an amplifier's output, proceed with caution. Don't just blithely connect the two up and assume that "everything will be apples". It may not; it may be "lemons".

Above all, do not assume that your ruggedly beautiful "professional grade" amplifier with rack mounting handles will drive a transformer. It might not. It might just quietly expire inside a few milliseconds. That would be sad.

At the very least, check to see if the amplifier has a DC offset voltage at the output. Then measure the DC resistance of the transformer primary. If the combination of the two will produce a primary current of more than about 20 milliamps, then you should take the steps outlined above to minimise or circumvent the DC offset.

Make sure that you do not drive the amplifier into clipping. If at all possible, use an oscilloscope to monitor the amplifier output, to check that all is well. If that checks out OK and the amplifier does not fail within the first few minutes due to "second breakdown" problems, then you may be reasonably sure that the amplifier and transformer are compatible. ☺

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For the lowest musical octave you need a Super-Bass Filter

for the Bass you can feel!

A most effective method of extending the bass response of a stereo system is to add a super-woofer. Although the associated loudspeaker system may be somewhat bulky it can be disguised as a piece of furniture, such as a coffee table. This article presents a design for a Super Bass Filter, a necessary part of a super-woofer system.

by **RON DE JONG**

Most run-of-the-mill loudspeaker systems provide a useable bass response down to around 50Hz or so. This is adequate for satisfactory reproduction of most music, including most so-called "heavy rock". Those enclosures that are smaller than average will generally provide a higher "cut-off" frequency or, if they do have an extended bass response, are inefficient, in the sense that they require significantly more drive power.

Even those loudspeaker systems which are larger than average or which purport to have really extended bass rarely provide much in the way of useable response below about 40Hz.

This simply means that the majority of hifi enthusiasts have to make do with loudspeaker systems which lack at least the lowest octave of the audible spectrum. For most music, this is a satisfactory compromise. Most people just do

not have the resources necessary to obtain and accommodate loudspeaker systems which cover the whole audio spectrum.

So most people never enjoy the rich sound of a truly wide range loudspeaker system — one which can really come into its own when playing classical organ music or music produced on electronic synthesizers. Sad.

Well there is a way to recover those lost octaves and this is within the reach of even those people with compact bookshelf loudspeakers: Use a separate "super-woofer" which can be housed in an enclosure with does double duty as a coffee table or end table. Powered by a separate amplifier, the super-woofer takes over where the stereo speakers leave off.

By disguising the necessary bulk of a super-woofer system in a useful piece of furniture, the hifi enthusiast can

employ smaller enclosures for the main stereo speakers and yet still obtain very deep bass.

Only one super-woofer is required for a stereo system. This is because there is no directional information provided at signal frequencies below 100Hz. This also means that the super-woofer can be positioned almost anywhere within the listening room.

What is needed to drive the super-woofer is a separate power amplifier with at least as much power as the total of the existing stereo amplifier. This is to take into account that, for a super-woofer to have tolerable enclosure size, it must necessarily be relatively low in efficiency.

The signal for the super-woofer amplifier is derived from the outputs of the existing stereo amplifier. The circuit presented here is designed for this purpose. We call it a Super Bass Filter.

Our Super Bass Filter mixes and

PARTS LIST

- 1 PC board coded 795B10, 97mm x 57mm
- 1 3-pole 4-position rotary switch
- 1 9 volt plug pack transformer, Ferguson model PPA 9/500
- ½ Metre of rainbow cable

SEMICONDUCTORS

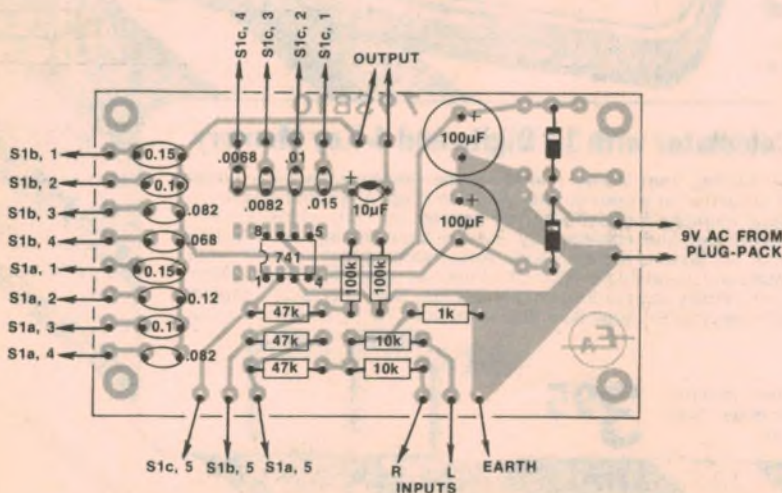
- 2 1N4002 diodes
- 1 741 op amp

CAPACITORS

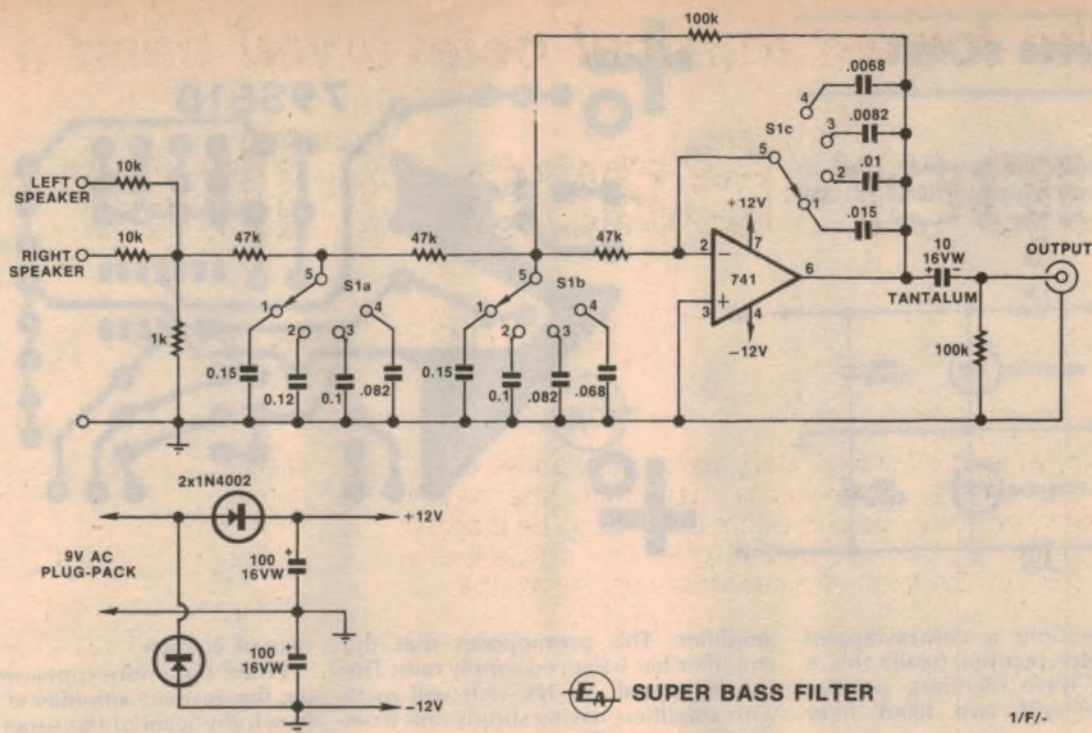
- 2 100uF 16VW electrolytics
- 1 10uF 16VW tantalum
- 2 0.15uF metallised polyester (greencap)
- 1 0.12uF metallised polyester
- 2 0.1uF metallised polyester
- 2 0.082uF metallised polyester
- 2 .068uF metallised polyester
- 1 .015uF metallised polyester
- 1 .01uF metallised polyester
- 1 0.0082uF metallised polyester
- 1 .0068uF metallised polyester

RESISTORS

- all ¼ watt: 2 x 100k, 3 x 47k, 2 x 10k, 1 x 1k



All the components except for the frequency range selector switch are mounted on a small PC board.



EA SUPER BASS FILTER

1/F/-

Circuit of the super bass filter. It uses only one IC — an inexpensive 741.

attenuates the signals from both channels of the existing stereo amplifier. Frequencies above the cut-off frequency are rolled off at the rate of 18dB/octave. Frequencies below the cut-off point are fed to the superwoofer amplifier. There is a switch to select the cut-off frequencies: nominally 50, 70, 80 and 100Hz.

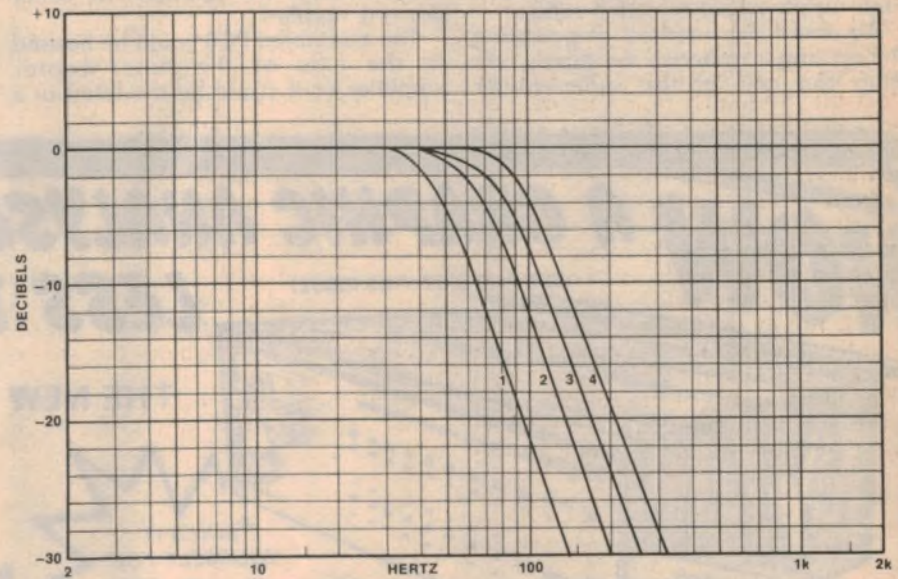
Now refer to the complete circuit of the Super Bass Filter. It uses just one operational amplifier IC, the readily available 741. This op amp is connected in a conventional low-pass filter network which has three RC networks. It is known as a third-order Butterworth filter.

A three-pole, four-position switch is used to switch the capacitors to obtain the four cut-off frequencies.

Apart from the attenuation provided by the input voltage divider, the filter circuit has a gain of unity, below the cut-off frequency. The input voltage divider has been designed to suit the output of most amplifiers. If the filter is fed from the line outputs of the stereo amplifier (or preamplifier), the input network should be changed.

This would involve omitting the 1k resistor, increasing the two 10k resistors to 47k each and substituting a link (on the PCB) for the first 47k resistor following the input mixing resistors. This modification assumes that the source impedance of the line outputs of the amplifier is low, ie, less than about 5k.

Power requirements for the op amp circuit are +/-12V DC at about 3 milliamps or less. This can be provided in two ways. The first involves the use of plugpack transformer, Ferguson



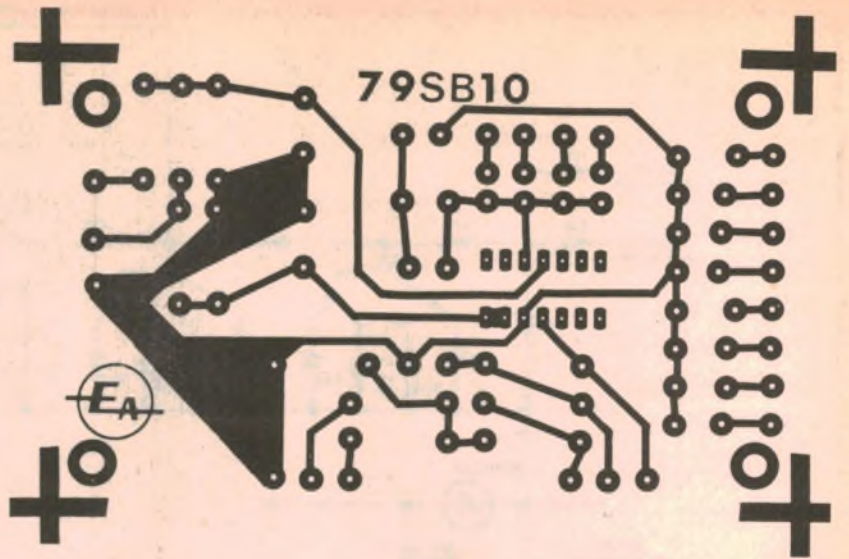
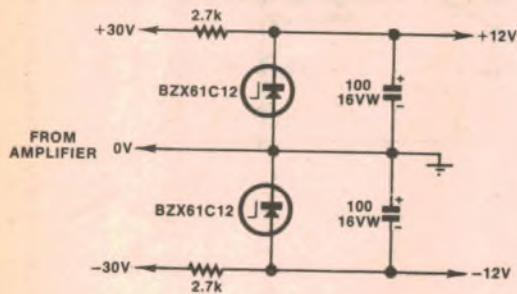
Response curves of our prototype unit for the four different frequency ranges.

SPECIFICATIONS

HARMONIC DISTORTION:	Typically .012% at 60Hz with respect to 100mV RMS
SIGNAL-TO-NOISE RATIO:	88dB unweighted with respect to 100mV RMS
MAXIMUM OUTPUT VOLTAGE:	5V RMS
INPUT IMPEDANCE:	10k
OUTPUT IMPEDANCE:	less than 1k
CUT-OFF FREQUENCIES:	50, 70, 80, 100Hz
FILTER SLOPE:	18dB per octave

SUPER BASS FILTER

BELOW: Circuit to connect filter to amplifier power supply. RIGHT: Actual size artwork for the PC board.



PPA9/500, feeding a centre-tapped voltage doubler rectifier (really this is just two half-wave rectifiers, positive and negative) with two 100 μ F filter capacitors.

This modest degree of power supply filtering is adequate for the circuit because of the low current drain and the fact that the 741 op amp has quite a high supply ripple rejection ratio.

An alternative method of powering the op amp is to derive the supply rails from the rails of the super-woofer

amplifier. This presupposes that the amplifier has balanced supply rails. The zener derived ± 12 V rails will mate with amplifiers having supply rails from ± 30 to ± 60 V.

All the components for the circuit are mounted on a PCB measuring 57 x 97mm (code 79sb10). This has space to accommodate the rectifiers or zener derived supplies.

The assembled PCB could be housed in the case of the super-woofer amplifier or it could be mounted in a

case of its own.

When the entire super-woofer is set up, the auxiliary amplifier is adjusted to match the level of the super-woofer to the stereo loudspeakers. Once this is done, the stereo amplifier volume control is used and the auxiliary amplifier requires no further adjustment.

Just a final point: do not rotate the rotary switch for the filter while the system is powered up otherwise a loud thump will be delivered by the super-woofer.

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by IAN POGSON

Signal injectors have been around for a long time now. We have described a number of them in the past, the last two being presented in February 1964 and more recently, in June 1973. However, some of our younger readers may not have come across this type of instrument before. It may be considered as a very rough type of "signal generator". In its simplest form, it consists of a low frequency audio oscillator designed to produce a waveform as rich in harmonics as possible. As such, it produces a large number of frequencies which are multiples of the fundamental and these appear at the output of the unit.

A signal injector therefore becomes a source of signals across a wide frequency band and which may be used for testing such things as audio amplifiers, broadcast radio receivers, etc.

By limiting the concept to a single audio oscillator, the band of frequencies will also be limited. By adding an extra and similar type of oscillator, this time with its fundamental frequency in the lower RF range, it follows that its harmonics will extend further into the high frequencies and even into the VHF range. The audio frequency oscillator can be made to "modulate" the RF oscillator and we then have an even more useful and versatile instrument. This is the principle on which our new signal injector is designed.

Because many integrated circuit chips are readily available at low cost and include a number of separate circuits which may be combined or used separately, the extended concept of the signal injector becomes very easy to implement.

In this particular case, we have made use of the IC type 4069, or 74C04, described as a "hex inverter". With six separate inverters available, we are able to use three of them for an audio oscillator and the other three for an RF oscillator. By adding just a few components around this chip, we are able to produce a versatile signal injector at a very modest cost.

With the component values given, the frequency of the audio oscillator is about 300Hz and the RF oscillator comes out to about 700kHz. This means that the signal injector may be used, not only for audio and broadcast radio tests, but it may also be used for high frequency receivers and even for making some checks on television receivers.

To be a little more specific, perhaps the most basic use for the signal injector is to make stage-by-stage checks on a faulty audio amplifier, similar to the old "finger-on-the-grid" technique used when valves held sway. With many valve amplifiers still in use, the technique still applies, with its extension to what may now be called "finger-on-the-base" method.

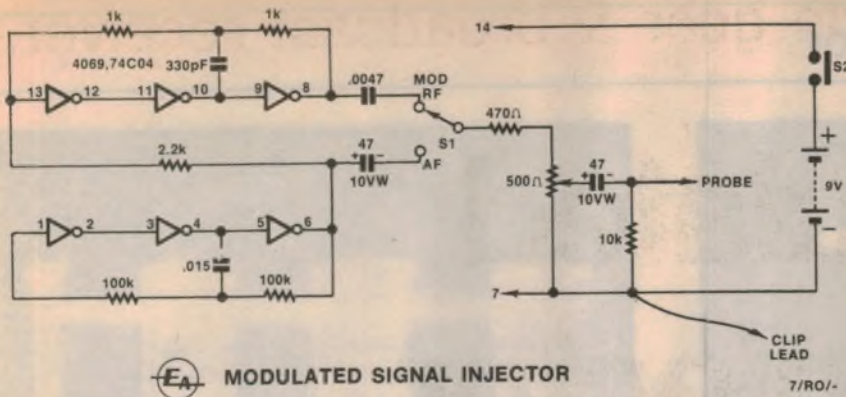
Only a short step away is the application to ordinary broadcast receivers, whether valve or transistor equipped. It is just a matter of probing along, stage-by-stage with the injector, until the faulty stage is isolated.

These tests are possible by using the audio oscillator section. By using the added modulated RF oscillator, we can extend the tests to receivers covering the HF range and well beyond.

Because of the heavy modulation of the RF oscillator by the audio oscillator, a series of "bursts" of RF is produced. This feature and the almost square

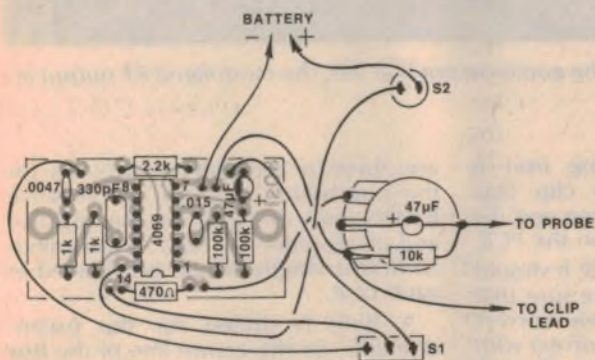


A diecast metal case was used to house the prototype. The probe was made from a stout piece of tinned-copper wire soldered to the centre lug of a jack plug.

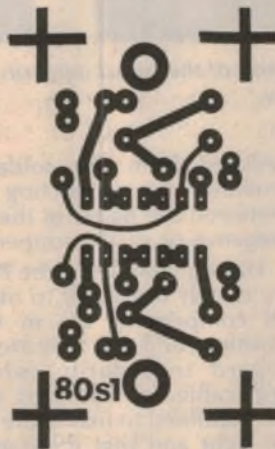


EA MODULATED SIGNAL INJECTOR

Two CMOS oscillators form the basis of the circuit. The audio oscillator has a frequency of about 300Hz; the RF oscillator a frequency of 700-800kHz.



The wiring diagram for the Modulated Signal Injector. At right is an actual size artwork of the PC board.



waves produced by the RF oscillator make it very useful for testing the signal circuits of television receivers. By applying the probe at appropriate spots along the signal line, a definite pattern of bars is produced on the screen. It should be noted, however, that the upper RF range is limited and we found that the prototype was good up to 100MHz as previously mentioned and so only the first few TV channels may be checked.

A switch has been provided to take the output from the audio oscillator only, to cope with audio amplifiers and broadcast frequencies, or the modulated RF output may be selected when tests are to be made on HF and television receivers.

To increase the versatility of the signal injector even further, we have provided means of controlling the level of the output to the probe. This feature could be used to ascertain whether or not any gain is available over any particular stage. The gain control is a simple potentiometer in the output circuit and it is very effective on the audio output but there is a reasonable amount of leakage at RF by virtue of the "hop-on" effect of the potentiometer. This means that when applied to some aerial inputs, the amount of signal is still quite high but in practice this is not a significant restriction.

Although there is not much to it, let us have a look at the circuit of our signal injector. The heart of the circuit is the hex inverter chip. Three of the inverters are connected in series (input to output) to form an audio oscillator when two resistors and a capacitor are added. As mentioned earlier, the two 100k resistors and the .015uF capacitor set the frequency of oscillation to about 300Hz. The other three inverters are similarly connected and this time, there are two 1k resistors and a 330pF capacitor, giving a frequency of 700 to 800kHz.

The output of the audio oscillator is connected to the input of the RF oscillator, via a 2.2k resistor, for the modulation process. The output of the audio oscillator is taken off also via a 47uF tantalum capacitor, to one pole of the output selector switch. Similarly, the output of the RF oscillator is taken via a .0047uF capacitor to the output switch.

The output of the switch is fed via a 470 ohm resistor to a 500 ohm carbon track potentiometer, the rotor of which is coupled via a 47uF tantalum capacitor and a 10k resistor, to the probe. The 470 ohm resistor in series with the potentiometer is to prevent the oscillators from being excessively loaded.

A small 9V battery is used as the source of supply for the IC. This is

PARTS LIST

- 1 Diecast metal box, Eddystone 89mm x 30mm x 35mm
- 1 Printed circuit board, 48mm x 25mm code 80s1
- 1 Potentiometer, 500 ohm linear carbon
- 1 Knob
- 1 Miniature toggle switch, SPDT
- 1 Miniature pushbutton switch
- 1 Battery, 9V No. 216
- 1 Lead for battery
- 1 Jack socket, 3.5mm
- 1 Jack plug, 3.5mm
- 1 IC, 4069/74C04 14-pin DIL
- 1 IC socket, 14-pin DIL
- 1 330pF polystyrene capacitor
- 1 .0047uF greencap (metallised polyester) capacitor
- 1 .015uF greencap capacitor
- 2 47uF/10VW tantalum capacitors

RESISTORS:

- 1 x 470 ohm
- 2 x 1k
- 1 x 2.2k
- 1 x 10k
- 2 x 100k

MISCELLANEOUS:

Screws, nuts, solder, hookup wire, 16-gauge tinned copper wire for probe.

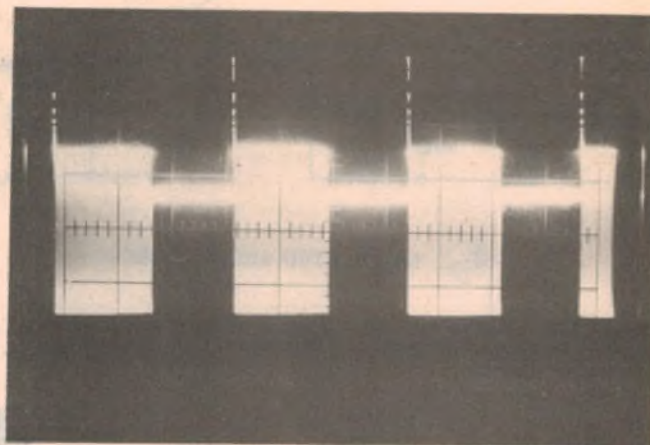
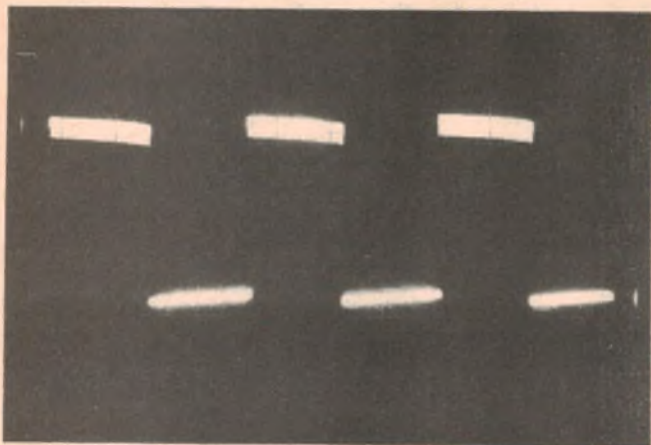
NOTE: Ratings are those used on the prototype. Components with higher ratings may generally be used providing they are physically compatible.

applied via a momentary pushbutton, which ensures that the battery will not be left on unintentionally.

It will be noticed that we have provided two large-value capacitors in the output circuit, each in such a way that they will be charged by any voltage applied to the input side. This was done so that the square wave of the audio oscillator would be passed on to the circuit being checked with a minimum of distortion. However, this feature may not be required and there may be some cases where it may be desired to test circuits with voltages in excess of the ratings of these two components. In such an event, the capacitors could be reduced to .01uF polycarbonates rated at 400V. The 10k resistor could also be omitted.

To give some idea of the waveforms to be expected from the signal injector, we took pictures from the CRO screen and these are reproduced here. The photographic process has resulted in some changes to the detailed appearance of the waveforms. One obvious point is that some of the lines have been somewhat increased in width. This applies particularly to the square wave picture and to the "DC" level of the modulated RF waveform.

Modulated signal injector



These two photos show the output waveforms of the signal injector. The audio output is at left, the modulated RF output at right. CRO settings: 0.5V/div and 1ms/div.

Also, the RF component assumes a solid block, rather than each cycle being visible. Finally, the vertical components of the square wave were so thin that they have been lost completely. However, these points do not detract from the overall impression.

CONSTRUCTION

Because the signal injector has only a few component parts, construction is not difficult. However, it demands a certain amount of care, particularly when it comes to fitting the components into the small diecast box.

Before attempting to fit any components into the box, the printed circuit board should be assembled. It is quite small and should present no problems. In keeping with normal procedure, the smallest items, such as resistors and capacitors should be soldered in first, followed by larger items. Although it is not essential, I favour the use of sockets for ICs, particularly for CMOS devices.

Readers who elect to solder the IC in directly are reminded that it is important to make sure that any possible

leakage from the soldering iron is nullified by connecting a clip lead between the barrel of the iron and the negative or earthy copper on the PCB.

Having completed the PCB, it should be closely inspected to make sure that all components are in their correct positions and that they are correct with regard to polarity, where that is applicable. All soldered joints should be examined to make sure that they are all right and that there are no solder bridges.

Reference to the picture will help in the assembly. Two screws are needed to fix the PCB. Two holes should be drilled on the correct centres and such that the PCB just clears the corner buttress of the box. Also, the board should only just clear the bottom of the box. This will ensure that the top edge of the PCB will not foul the lid of the box. The PCB is stood off the side of the box by using two half nuts between the box and the board, making three nuts in all for each screw.

Before finally screwing the PCB into place, seven leads should be soldered to it, for external destinations. These

are: three for the toggle switch, one for the pushbutton, one for the negative battery lead, one each for the negative and active sides of the potentiometer. Sufficient length should be allowed in each case.

A hole is drilled for the potentiometer, on the centre line of the box and so that the body of the potentiometer just clears the end of the box. The spindle will be cut to suit the knob used. Before tightening the nut, orientate the potentiometer so that the lugs are nearer to the pushbutton side, with the earthy lug about on the centre line.

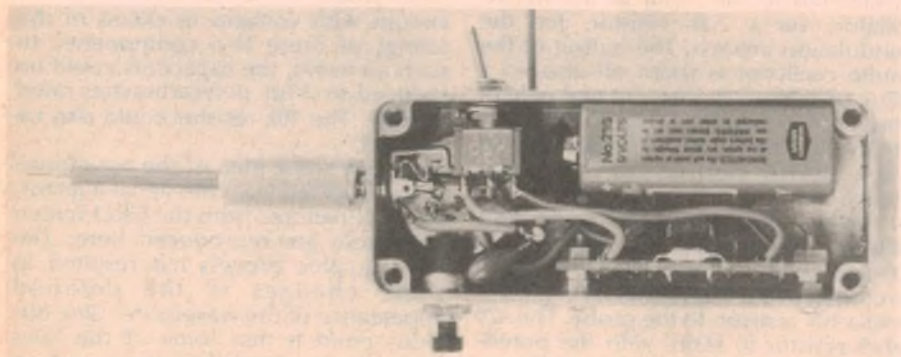
A hole is drilled to take the pushbutton, so that its body just clears the potentiometer and the buttress of the box.

Next, a hole is drilled in the end of the box to take the jack socket for the probe. The socket should be placed so that it just clears the potentiometer and the lugs on the pushbutton. You may find that the position for the socket is off centre, as it was on the prototype.

Now drop the battery in place temporarily, so that it butts against the buttress on the box. It may be necessary to dress some of the leads from the PCB, to allow space for the battery. The toggle switch is mounted on the side of the box, between the battery and the jack socket. The switch should be placed so that it clears the potentiometer, with a gap between the switch and the jack of between one and two millimetres. Care should also be taken to make sure that the lugs of the toggle switch and the pushbutton do not interfere. The pushbutton lugs may be bent if necessary.

Drill another hole, just large enough to clear a piece of hookup wire, on the toggle switch side and opposite the earthy lug on the potentiometer. The earth clip lead passes through this hole.

Most of the wiring from the PCB to



View inside the completed prototype. Assemble the various components into the case as described in the text and take care to avoid inadvertent "shorts".

EASY TO BUILD

the other components will be left to the builder but a few comments may be helpful. A convenient common earth point is the lug on the potentiometer. A wire is run from here to the earth lug on the jack socket, to earth the box. Also, the 10k resistor is earthed at the potentiometer lug. The other end is connected to the 47 μ F tantalum capacitor "in mid air", with the other end of the capacitor going to the rotor lug on the potentiometer.

The probe is made up by a piece of 16-gauge tinned-copper wire, about 55mm long and soldered to the centre lug of the jack plug. A piece of spaghetti tubing, about 45mm long, is slipped over the tinned-copper wire and it is then crimped onto what is normally the earth lug of the plug. The outer case is screwed back into place and the probe is then plugged in.

This almost completes the assembly work. If a socket is used, the IC should be plugged into its socket, taking care that no pins are bent over in the process. It is sometimes necessary to bend the pins inwards slightly, to make them enter the socket. This done, the battery plug is connected to the battery


We estimate that the current cost of parts for this project is approximately

\$12.00

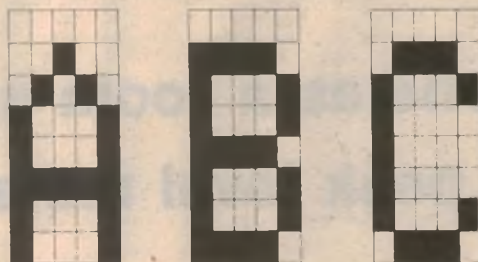
This includes sales tax.

and the unit is ready for checks to see that it is in working order.

The signal injector is very easy to use and a little practice is all that is necessary to make best use of the device. The normal procedure is to start testing at the high level, working backwards towards the lower level stages. By adopting this method, the offending stage can usually be isolated. If you wish to check whether or not a particular stage is giving any gain, the signal should first be injected at the output of the stage and noting the amount of output. The injector is then moved to the input of the stage and an increase in output should be noted.

When making tests with the signal injector, the level control can often be useful when coping with different signal level requirements. Also, the output may be switched between the audio and the modulated RF sources, depending on the nature of the checks being made. Experimentation during the initial stages could be helpful in getting the best out of the instrument. 

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Playmaster Stereo Graphic Analyser

Functions as a room analyser or peak level meter with 20 LED display

While graphic equalisers have considerable potential to improve the sound quality of any high fidelity system, they are difficult, if not impossible, to use without supporting equipment such as a graphic analyser. Our new Playmaster Graphic Analyser is the perfect complement to our recent Playmaster stereo graphic equaliser or any commercial equaliser.

by **RON de JONG & LEO SIMPSON**

When we published our highly successful Playmaster graphic equaliser back in May 1979, we indicated that we would follow it with a companion analyser. We have always been of the opinion that graphic equalisers are merely a source of frustration and confusion for keen audiophiles, unless they have access to a suitable analyser. Now, after some delay, we present the Playmaster Graphic Analyser.

Our new Playmaster Graphic Analyser provides a visual display of

frequency response; as with the Playmaster graphic equaliser and the better commercial graphic equalisers it divides the audio spectrum into ten octave bands with the same centre frequencies, ie. 64, 125, 250, 500, 1k, 2k, 4k, 8k and 16kHz.

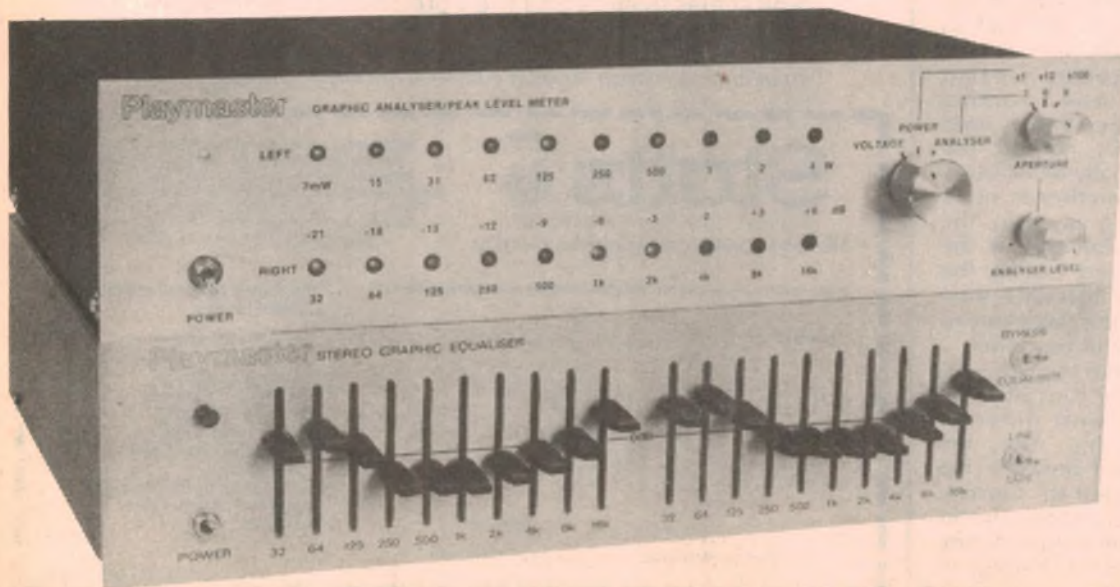
Each octave band has a vertical display consisting of two LEDs. If the amplitude of the input signal within one of these frequency bands exceeds a certain limit the lower LED for that band will turn on; if the amplitude in-

creases further, the top LED in the band will turn on as well.

The difference in signal level between the top and bottom LEDs in a band is set by what is termed the "aperture" control. We have provided three aperture settings: 3dB, 6dB and 9dB. The idea of having two LEDs per octave band is to display the frequency response within narrow limits, as defined by the aperture control.

When equalisation is performed with a graphic equaliser and our companion analyser, a pink noise signal is fed to the amplifier and speakers. The signal is monitored by a microphone and then displayed on the graphic analyser. The equaliser slider controls are then adjusted to obtain an optimum flat frequency response as displayed by the two LEDs in each octave band.

Pink noise is similar to white noise except that it is "pink", ie. the energy content decreases as the frequency increases. To define it more precisely,



Teamed with our Playmaster Graphic Equaliser or just about any commercial equaliser, our new Playmaster Graphic Analyser enables loudspeaker systems and the rooms in which they are used to be accurately analysed. At other times, the Analyser functions as a dynamic display for power output or signal level.

pink noise is random noise with an equal energy distribution for each octave bandwidth. This means that it has the same energy content for the octave centred on 64Hz as it does for the octave centred on 16kHz, or any other frequency.

Normally, pink noise is produced by passing the signal from a white noise generator through a filter which rolls off the high frequency response at the rate of 3dB/octave. The inbuilt pink noise generator in our analyser is provided in the same way. A preamplifier is also incorporated to enable a microphone to be connected.

With pink noise fed through a system, flat frequency response is indicated when only the bottom row of LEDs in the front panel display are on. If the aperture control was set to 3dB then this would mean that the frequency response between bands was equalised within at least 3dB. Aperture settings of 6dB and 9dB would likewise imply equalisation to within 6dB and 9dB respectively.

Naturally, when you begin to equalise your system, the overall frequency response of the system/room combination will probably be anything but flat and so not all the LEDs on the analyser panel will be alight. You may have to first make some changes in the positions of loudspeakers and perhaps the positions of some pieces of furniture. A guide to this process is given in our article entitled "Locating Peaks and Troughs with an Equalisation Analyser" published in the February 1978 issue of "Electronics Australia".

Assuming that this initial procedure has been carried out, then adjustment of the equaliser controls can begin. The level of the pink noise signal is adjusted so that it is high enough to mask out any ambient noise in the system or room. Then the analyser level (sensitivity) control is adjusted so that about half the LEDs are alight.

Now if both LEDs for a particular octave band are both out, then the response for this band is too low. Similarly, if both LEDs for a particular band are alight, then the response for that band is too high. The slider controls on the graphic equaliser should then be adjusted accordingly.

Besides this most important function of system or room equalisation, our new Analyser provides a bonus. When not displaying room or system response, it can provide a dynamic horizontal "bar-graph" display of the signal levels in both channels of a stereo system. Thus, it may be used to monitor signal levels during tape recording or the power delivered by an amplifier.

When measuring power, the analyser can indicate powers up to 400 watts (referred to an 8-ohm load). When measuring signal level, the display may be calibrated to agree with 0VU of the tape recorder being used, by adjusting

SPECIFICATIONS OF THE THREE FUNCTIONS

GRAPHIC ANALYSER

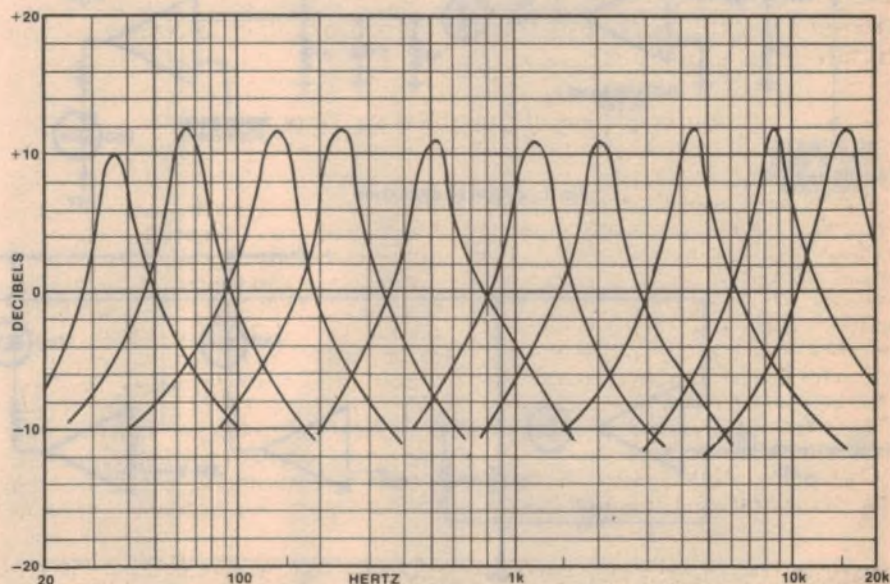
Display: 10 frequency bands, 2 LEDs per band
 Centre frequencies of bands: 32, 64, 125, 250, 500, 1k, 2k, 4k, 8k, 16kHz
 Q factor of filters: 5
 Aperture: 3dB, 6dB, 9dB
 Line input sensitivity: 15mV RMS with 50k input impedance
 Microphone input sensitivity: 80uV RMS with 10k input impedance
 Averaging period: 4 seconds

PEAK LEVEL METER

Display: Left and right channels, 10 LEDs per channel
 Scale: 3dB per step from -21dB to +6dB
 Accuracy: ± 0.5 dB with respect to 0dB indication
 Response decay time: 50ms
 Line input sensitivity for 0dB indication: 75mV

PEAK POWER METER

Display: Left and right channels, 10 LEDs per channel
 Scale: 7mW, 15, 31, 62, 125, 250, 500, 1W, 2, 4
 Range: x1, x10, x100
 Maximum power indication: 400 watts
 Calibration: with respect to an 8 ohm load.



The shape of these filter curves in the Analyser complements the filters in our Playmaster graphic equaliser. Because of the shape of these filters it may be found that a high boost setting on one slider control will cause more than one Analyser LED to light.

the rear-mounted "peak level" control.

In total, our new Playmaster Graphic Analyser/Peak Level Meter, to give it its full name, can be regarded as a real bargain. At around \$95 in kit form it is a mere fraction of the cost of equivalent commercial equipment. It is also easy to build and uses readily available parts.

CIRCUIT DESCRIPTION

The circuit of our Analyser is pretty daunting to look at, especially if you consider that nine op amps have not been shown, to simplify it. In all, there are 39 operational amplifiers in the circuit but these are actually in the form of uA4136 quad op amps, so the number

of IC packages is relatively small. One op amp, IC 9d, is not used.

Beside the 39 op amps, there are two three-terminal regulator ICs and a noise generator IC, plus, incidentally, a lot of resistors and capacitors.

As can be seen on the upper half of the circuit diagram, there are two rows of LEDs, each driven by an op amp. The LEDs are depicted in rows in the same order as they appear on the analyser front panel. In the peak level meter mode, the top row of LEDs displays the signal in the left channel of the amplifier while the bottom row displays the signal from the right channel.

Whereas the peak level meter mode

PLAYMASTER GRAPHIC ANALYSER

results in a horizontal display, the analyser mode results in a vertical display, ie. ten columns with two LEDs each. This may seem complicated but it turns out to be quite easy to arrange the op amps to provide either mode quite simply.

The mode in which the display works is set by the function selector switch, S1. We shall discuss the analyser mode first.

Input signals to the analyser are fed from the Mic/Line switch S3 to op amp IC7c which is a non-inverting amplifier.

shown in Fig. 2. This shows the circuit for the left channel display only.

IC10d operates a negative peak level detector which is referenced to +6V. If the input has a peak value of 150mV, for example, then the capacitor at the output of IC10d will be charged to 150mV below +6V. As a further example, if the input signal has a peak value of 4V then the capacitor at the output of IC10d will be charged to 4V below +6V, ie. +2V.

Each of the 10 op amp comparators following IC10d has a reference input voltage which ranges from 100mV to

when in the analyser mode.

Notice also, that while IC10d drives the non-inverting inputs of its associated ten comparators, IC10c, for the left channel, drives the inverting inputs (not the non-inverting inputs) of its associated ten comparators. The latter set of comparators would not work in the correct "sense" were it not for the fact that their associated LEDs are driven from the -12V line rather than the +12V line.

For the same reason, there is a fundamental difference between the complete circuit and Fig. 1 in that the inputs to the lower comparator are reversed.

The need to drive the top set of LEDs from the positive 12V line while the lower set of LEDs is driven from the negative 12V line really has nothing to do with the operation of the circuit. It was done merely to simplify the layout of the printed circuit board.

About the only major point left to be explained about the circuit operation is how the reference voltages for the two strings of ten comparators are provided. These are actually provided by voltage dividers made up from R2 and R3 on the output of each octave band filter. Since the octave band filters are not operating when in the peak level mode, their output is zero and so R2 and R3 can provide a fixed voltage reference from the +6V output from IC9c.

The pink noise generator is a standard circuit which we have published

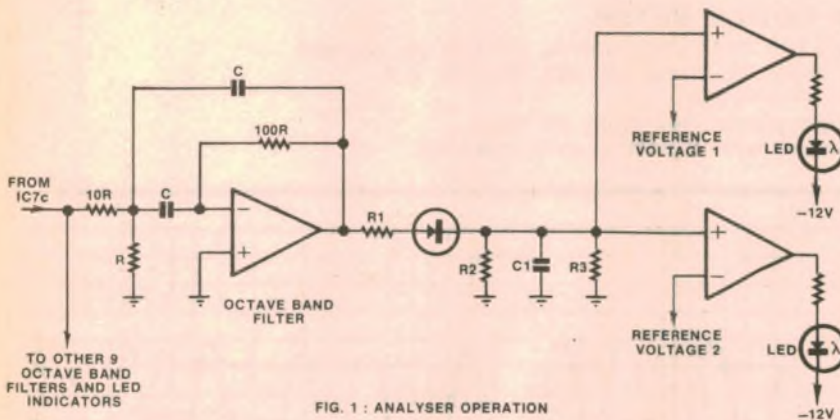


FIG. 1: ANALYSER OPERATION

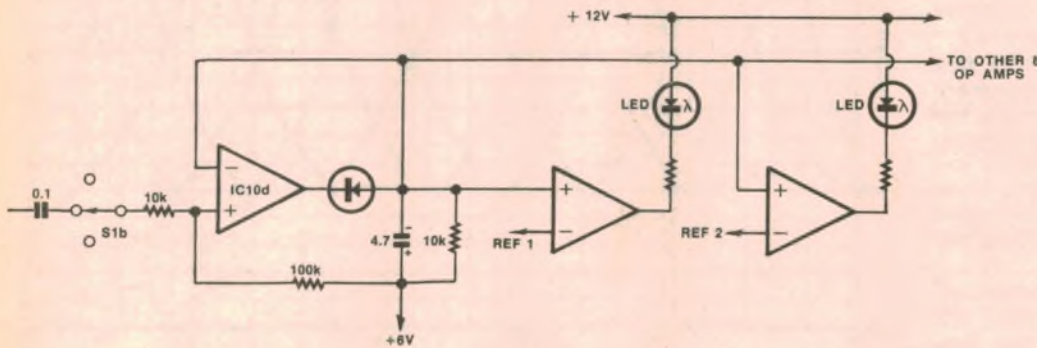


FIG. 2: PEAK LEVEL METER OPERATION

Figs 1 and 2 illustrate the operation of the Analyser and Peak Level Meter functions, respectively. Opposite page: the full circuit diagram. Only one filter is shown. The component values for the ten filters are tabulated on page 55.

IC7c drives ten octave-band-filters which correspond to the ten centre frequencies listed above. Each filter is followed by a half-wave rectifier and filter.

Each rectifier output is fed to a pair of op amps which are each connected as comparators and drive a LED. The comparators are referenced to one of two voltages to set their thresholds. The basic circuit concept is shown in Fig. 1. Later we shall explain the differences between Fig. 1 and the main circuit diagram.

Almost the entire circuit of the graphic analyser is reconfigured to provide the peak level metering mode. The basic circuit arrangement is

2.7V below +6V. If the input signal exceeds 100mV peak, then the first LED will be turned on. If the input signal exceeds 2.7V peak, then all LEDs will be turned on. The ten comparators thus provide a signal display range of close to 27dB total.

While the analyser and peak level functions depicted in Figs. 1 and 2 are both relatively simple in themselves, the whole circuit has to be virtually turned upside down to provide either function.

For example, while IC10d drives the non-inverting inputs of the ten comparators in the peak level mode, it (IC10d) is used to hold those comparator inputs at a fixed reference

before. It uses a National Semiconductor IC, type MM5873. This generates white noise digitally, using a "pseudo-random bit sequence" (PRBS). The white noise is then passed through a filter network which provides a piecewise approximation to a 3dB/octave slope. The output of the filter is buffered and amplified by IC6d.

The microphone preamplifier consists of two high gain amplifiers in series, IC6c and IC7d. These provide the high gain necessary for an electret or low impedance microphone. Input impedance is 10k. This may be increased to 47k by increasing the input resistor to this value. This will also reduce the preamplifier gain by five

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The ever popular ETI Disco Strobe has been updated - improvements in the electronics necessitated a new PCB and this plus the all new case makes this an essential kit for parties. The kit comes complete with instructions and these instructions include details on extending the kit to include two flash tubes

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SEE EA DEC '79

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\$11.50

This is a shortform kit (does not include case etc) for use with fans or other 'squirrel type' motors which are unsuitable for normal speed controllers. Build this kit into the appliance itself! Not illustrated

SEE EA AUG '79

MAST HEAD AMP

NEW K-3232

\$29.50

Not illustrated

If you are plagued with TV reception problems then this masthead kit could solve them for you! Designed for TV plus FM and UHF, it is simple to build and includes power supply and full instructions

C.D.I. SAVES ON PETROL



This kit will pay for itself over and over. Installed in your car, it will give easier starting from cold, keep your points & plugs in better condition thereby keeping your car in tune for a longer time.

\$32.50

DRILL SPEED CONTROLLER

Thousands of these simple to build kits have been sold. Use with your 240V universal brush type motor drill to give speeds down to near zero.



\$13.50

PLAYMASTER 40/40 STEREO AMPLIFIER

(E.A. December '76)
Our most popular kit ever. Thousands sold.

Cat. K-3411.....\$129.50

PLAYMASTER TWIN 25 AMPLIFIER

(E.A. May '76)
Similar to above, but less power. A great kit.

Cat. K-3410.....\$105.00

PLAYMASTER AM/FM TUNER

(E.A. Nov/Dec '78)
Matches Playmaster amplifiers - with in-built digital clock.

Cat. K-3494.....\$129.50

PLAYMASTER GRAPHIC EQUALIZER

(E.A. May '79)
Adds depth and dimension to your Hi-Fi system.

Cat. K-3500.....\$99.50

LED LEVEL METER

(E.A. June '76)
Easy to make, fully solid state.

Cat. K-3370.....\$13.50

CAR STEREO BOOSTER

(E.A. January '79)
Boosts power output of your car stereo to 12 watts per channel.

Cat. K-3493.....\$29.50

MUSICOLOR Mk111 COLOUR ORGAN

(E.A. September '76)
Turns your music into light! Just add the lights.

Cat. K-3140.....\$65.00

ET1601 MINI ORGAN

(E.T. August '78)
YOU can play your favourite tune in style

Cat. K-3430.....\$26.50

LOUDSPEAKER PROTECTOR

(E.A. June '76)
Eliminates turn-on and turn-off surges from most amplifiers.

Cat. K-3425.....\$13.50

WHISTLE FILTER

(E.A. Feb '79)
Rid your tuner of heterodyne whistles

Cat. K-3496.....\$19.75

45 WATT VHF AMPLIFIER

Fibreglass PCB, 13.8V operation. Requires 8-12W drive

Cat. K-3132.....\$29.50

30 WATT 80 METRE AMPLIFIER

Ideal for the novice. 13.8V. Adaptable to 50W output.

Cat. K-3133.....\$35.75

CAR ALARM

Easy to build and protects your investment.

Cat. K-3250.....\$11.50

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Communicate with a computer.

Cat. K-3460.....\$97.50

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(E.A. April '78)
Allows above VDU to be used with any TV set.

Cat. K-3462.....\$4.50

ASCII KEYBOARD ENCODER

(E.A. April '78)
Uses our standard keyboard (Cat. X-1180)

Cat. K-3464.....\$39.50

CASSETTE INTERFACE

(E.A. April '77)
Use any cassette to communicate with a computer.

Cat. K-3465.....\$24.50

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(E.A. August/September '78)
Versatile piece of test gear. Easily upgraded to 200MHz by adding 95H90 Pre-scaler IC

(Cat. Z-5360.....\$12.50)

Cat. K-3437.....\$99.50

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(E.A. July '78)
Checks most transistors and FETs quickly and easily.

Cat. K-3052.....\$19.75

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(E.A. March '78)
Ideal project for the beginner or enthusiast.

Cat. K-3468.....\$34.50

AUDIO OSCILLATOR

(E.A. June '78)
Outstanding value for a service aid

Cat. K-3469.....\$32.00

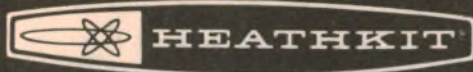
PRICES CORRECT AND STOCK AVAILABLE AT TIME OF GOING TO PRESS

DICK SMITH ELECTRONICS



SEE OUR OTHER ADVERTS IN THIS MAGAZINE FOR OUR STORE ADDRESSES AND RESELLERS

DSE652



Build your own Weather Station

Fully Computerised Five-Function Digital Weather Station

The Heathkit ID-4001 Weather Station is microprocessor controlled and computes and displays weather data on easy-reading LED's — stores data in memory for instantaneous retrieval! Monitors indoor and outdoor temperatures and wind chill, barometric pressure, wind speed and direction, and time/data — all with electronic accuracy and reliability. It's ideal for home or office, boat clubs etc. anywhere accurate and instant weather information is needed.

1. Wind Speed. Two significant digits are displayed with your choice of average or instantaneous readings. Indicators show whether display is in miles-per-hour, knots or kilometres-per-hour. Date, time and magnitude of maximum wind gusts are retained in the memory and recalled whenever needed. Accuracy $\pm 5\%$ or better.

2. Wind Direction. Current wind direction is displayed by one of 16 indicators arranged in a circular compass configuration, and identified by both compass points and radial degrees.

3. Temperature & Wind Chill. Displays include a 2½-digit readout with + and - signs, alternately displayed indoor/outdoor readings and switch-selected Fahrenheit and Celsius readouts. Temperature range extends from -40° to $+70^{\circ}$ C and from -40° to $+158^{\circ}$ F. Computes wind chill reading automatically at the touch of a button. Date and time of maximum and minimum temperatures are stored in memory for future retrieval. Accuracy $\pm 1^{\circ}$ C.

4. Barometric Pressure. A 4-digit readout is displayed, with indicators to show whether pressure is rising or falling, and whether display is in inches of mercury or millibars. Range of pressure is 28.00 to 32.00 in. Hg (981.9 to 1050 millibars). Date, time and magnitude of maximum and minimum pressure are stored in memory and instantly recalled. Compensated temperature range is 0° C to 50° C (32° F to 122° F).



5. Time. 6-digit display with 12 or 24-hour format time readout, 4-digit date readout and AM/PM indicator in 12-hour format. Includes outdoor transducer assembly. Optional cable below. For 120/240 VAC.

Kit ID-4001 \$680.00 inc. tax
 Assembled IDW-4001 \$800.00 inc. tax
 IDA-1290-1, 50 ft. cable \$16.00
 IDA-1290-2, 100 ft. cable \$28.00
 IDA-1290-3, 150 ft. cable \$37.50

Digital Indoor/Outdoor Thermometer



You'll never have to "gauge-guess" again! This fun-to-build kit monitors indoor/outdoor (or any two temperatures) with a big, bright 3" high digital readout. The readout includes plus and minus signs as well as indoor and outdoor indicator lights, so you know at a glance which temperature is being monitored.

ID-1390AE SPECIFICATIONS: Temperature Range: Fahrenheit -40 to $+120^{\circ}$, Celsius -40 to $+50^{\circ}$.

KIT ID-1390AE \$103.50

Digital Wind Speed and Direction Indicator



Outstanding accuracy and easy-to-read digital display make this kit a "must" for pilots, boaters, and anyone whose activities are affected by the wind.

ID-1590E SPECIFICATIONS:

Wind Speed 0-99 in miles per hour, knots or kilometres per hour.

KIT ID-1590E \$125.50

ORDER BY COUPON NOW OR COME TO OUR SHOWROOM

Please rush me the Heathkit of my choice. My cheque for \$ is enclosed plus \$7.00 for package and post.

- Kit ID-1590E Kit ID-4001 Assembled IDW-4001
 Kit ID-1390AE For Kits ID-1590E, ID-4001 & IDW-4001 indicate either:-
 IDA-1290-2, 100ft cable IDA-1290-1, 50ft cable
 IDA-1290-3, 150ft cable

Name

Address

..... P / Code.....

Send to: W. F. Heathkit Centre
 220 Park St., South Melb. 3205. Phone: 699-4999

PLAYMASTER GRAPHIC ANALYSER

size can be used to isolate the socket from chassis.

With all the hardware mounted in the chassis you can install the mains wiring and some of the other wiring which does not involve the PCB. With that complete, you can turn attention to the PCBs. The display PCB is relatively straightforward as it accommodates only the twenty LEDs. It measures 203 x 59mm and is coded 80ga3b.

Each LED should be mounted so that it is spaced about 8mm from the PCB surface. Solder only one lead of each LED so that it can be adjusted later.

The main PCB measures 203 x 143mm and is coded 80ga3a. Mount all the links and small components first. We recommend that PC pins be installed for external connection. Take particular care to install the diodes and electrolytic capacitors with correct polarity. A

they have no internal connections.

The three terminal regulator ICs require heatsinks. We made those for the prototype from 16-gauge aluminium, each measuring approximately 20 x 30mm.

With both PCBs complete, they can be soldered together. Position the display PCB exactly at 90° to the main PCB so that the top of the edge-connector pattern on the display PCB is just visible above the component side of the main PCB. Now tack the two edge connector patterns together in several places and then temporarily mount the assembly in the chassis to check that the LEDs will pass through the front panel holes. If not, adjust the two PCBs and solder all the connectors together. Now all the wiring can be connected to the PCB assembly. Use rainbow cable as much as possible, to give a neat appearance.

Parts List

- 1 PC board, 203 x 143mm, 80ga3a
- 1 PC board, 203 x 59mm, 80ga3b
- 1 plated steel chassis, 370 x 80 x 245mm with wrapover steel cover
- 1 front panel
- 1 adhesive label for rear panel
- 1 transformer, A&R 2155, DSE 2155
- 1 6-way RCA socket panel
- 1 4-way spring-loaded speaker terminal panel
- 1 100k rotary (log) potentiometer
- 1 100k dual ganged rotary (log) potentiometer
- 2 4-pole 3-position rotary switches
- 2 SPDT miniature toggle switches
- 1 6.5mm jack socket
- 4 adhesive rubber feet
- 4 brass spacers, 10mm long
- 1 3-pin mains plug and cord
- 1 3-way mains terminal strip
- 1 rubber grommet and cord clamp
- 32 PC stakes
- Plus: hookup wire, solder lug, screws, nuts, washers, tinned copper wire, shielded audio cable.

SEMICONDUCTORS

- 2 1N4002 power diodes
- 12 1N4148 silicon signal diodes
- 20 large red LEDs

- 1 small green LED
- 1 LM340T-12 regulator
- 1 LM320T-12 regulator
- 1 MM5837 IC
- 10 μ A4136 quad op amps

CAPACITORS

Electrolytics (PC mounting): 2 x 1000 μ F/25VW, 2 x 100 μ F/16VW, 4 x 47 μ F/16VW, 2 x 22 μ F/16VW, 2 x 10 μ F/16VW, 3 x 4.7 μ F/25VW.

Tantalum: 4 x 10 μ F/25VW

Metallised polyester (greencap): 1 x 1 μ F, 3 x 0.27 μ F, 3 x 0.18 μ F, 7 x 0.1 μ F, 4 x 0.47 μ F, 1 x 0.27 μ F, 2 x .022 μ F, 2 x .01 μ F, 2 x .0047 μ F, 2 x .0022 μ F, 4 x .001 μ F.

Polystyrene or Ceramic: 4 x 470pF, 3 x 39pF.

RESISTORS

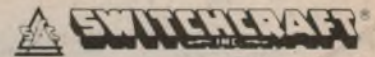
3 x 2.2M, 2 x 1M, 1 x 820k, 4 x 680k, 3 x 560k, 2 x 390k, 4 x 220k, 2 x 180k, 5 x 150k, 2 x 120k, 6 x 100k, 1 x 82k, 4 x 68k, 2 x 56k, 2 x 47k, 3 x 39k, 3 x 33k, 2 x 27k, 3 x 22k, 1 x 18k, 2 x 15k, 1 x 12k, 18 x 10k, 2 x 8.2k, 4 x 6.8k, 3 x 5.6k, 2 x 3.9k, 5 x 3.3k, 5 x 3.3k, 3 x 2.7k, 1 x 2.2k, 2 x 1.8k, 20 x 1.5k, 1 x 1k, 1 x 470 ohm, 1 x 330 ohm, 1 x 100 ohm, 2 x 15 ohm.

similar comment applies to the orientation of the IC packages. Leave the MM5837 IC till last as it is a MOS device and requires precaution to prevent damage from static charges.

When you are ready to solder in the MM5837, connect the barrel of the soldering iron to the 0V line of the PCB, using a clip lead. Now solder pins 1, 2, 3 and 4 of the MM5837. The other pins may now be soldered although

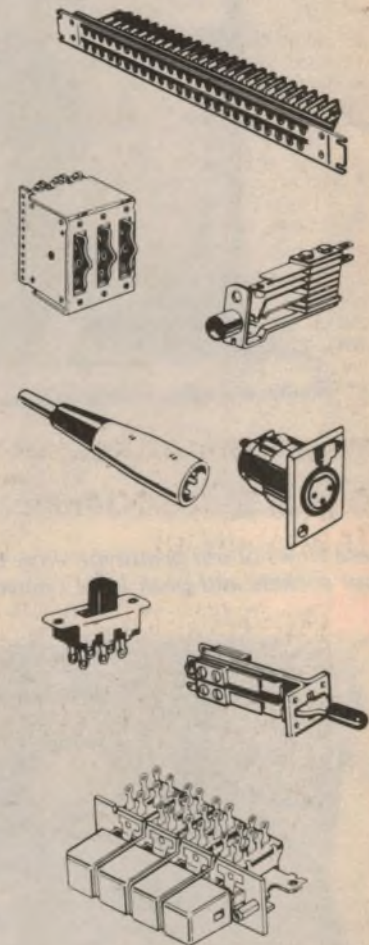
When all wiring is complete, make a thorough check of all your work and then apply power. Measure the voltages marked and then you should be ready to switch on and check the analyser functions. Connect the unit to your amplifier. Feed the pink noise into the amplifier and check that it works.

Now connect a good quality microphone and check that the LEDs in each octave band respond as the ap-



CONNECTORS & ELECTRONIC COMPONENTS

Superb quality and reliability from one of the oldest and most experienced manufacturers in the U.S.A.



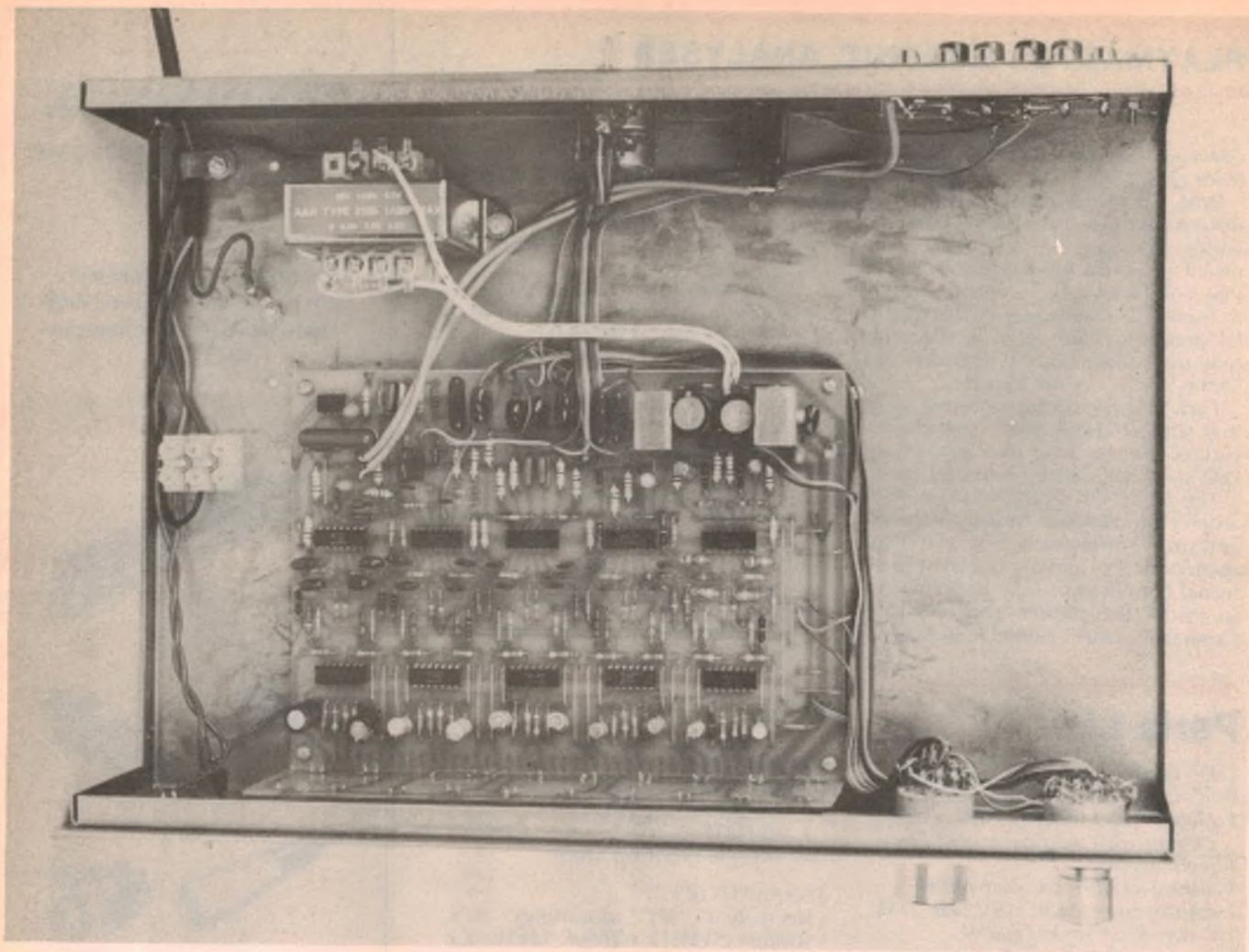
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AUDIO TELEX COMMUNICATIONS PTY. LTD.

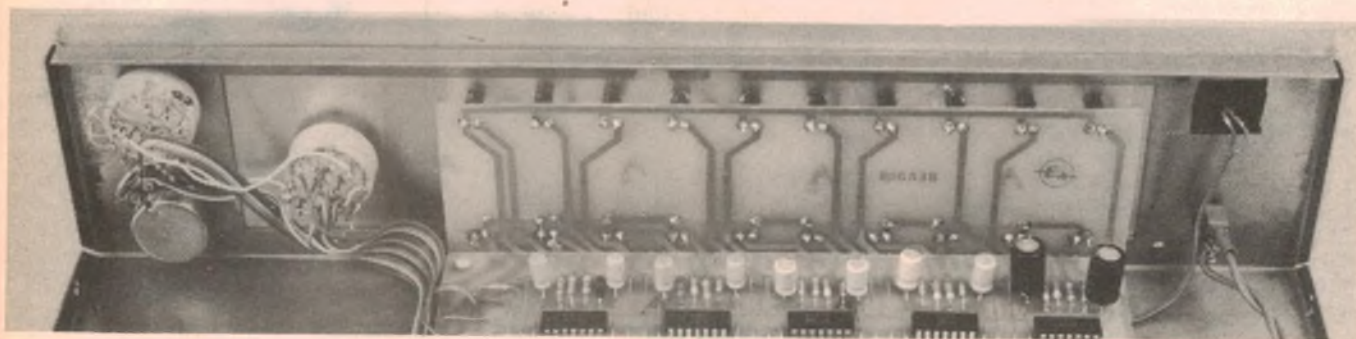
SYDNEY
1 Little Street,
Parramatta, 2150
Tel: 633 4344

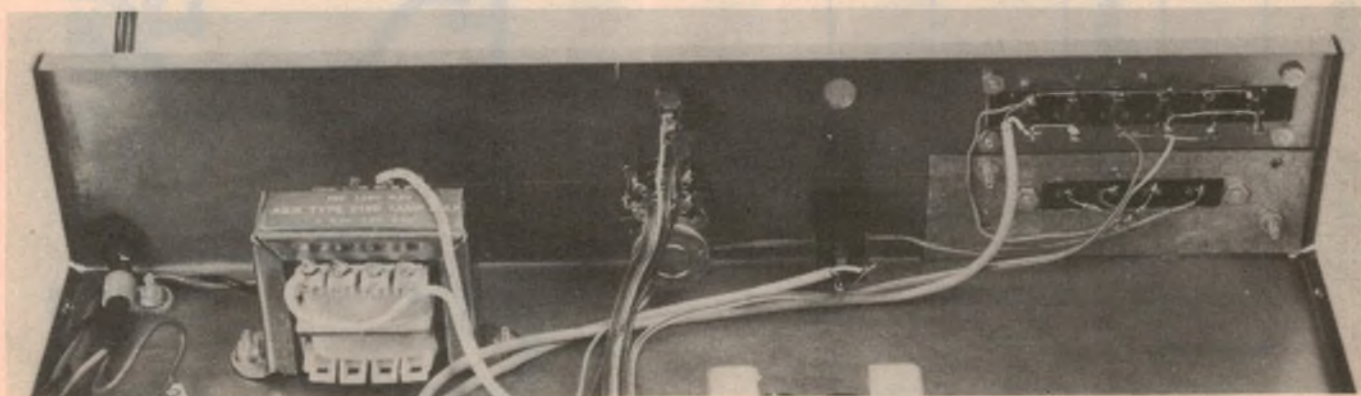
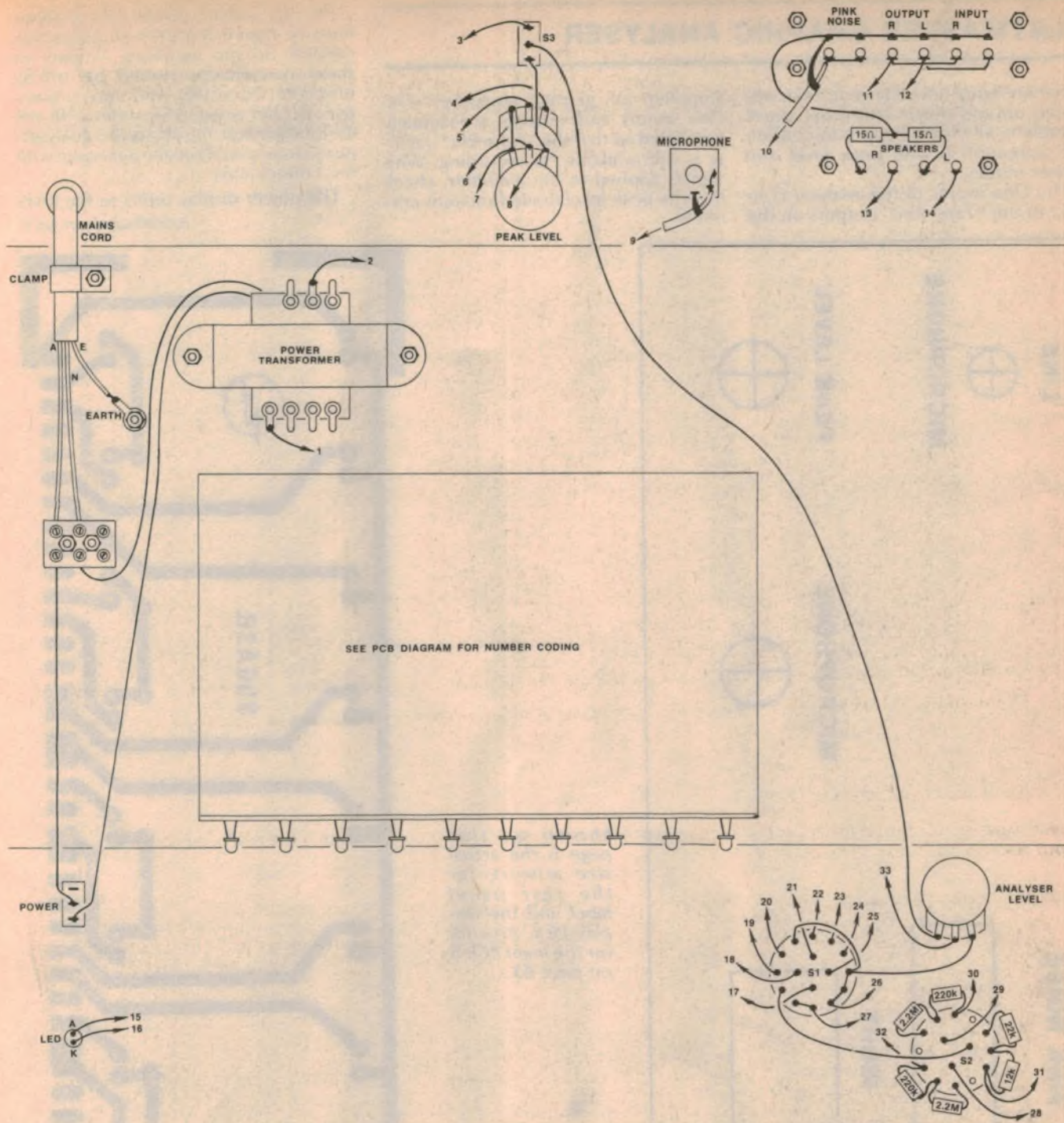
MELBOURNE
7 Essex Road,
Mt. Waverley, 3149
Tel: 277 5311

BRISBANE
394 Montague Road,
West End, 4101
Tel: 44 6328



These views of our prototype show the simplicity of construction. At bottom of the page is the rear view showing the input sockets and peak level control.





PLAYMASTER GRAPHIC ANALYSER

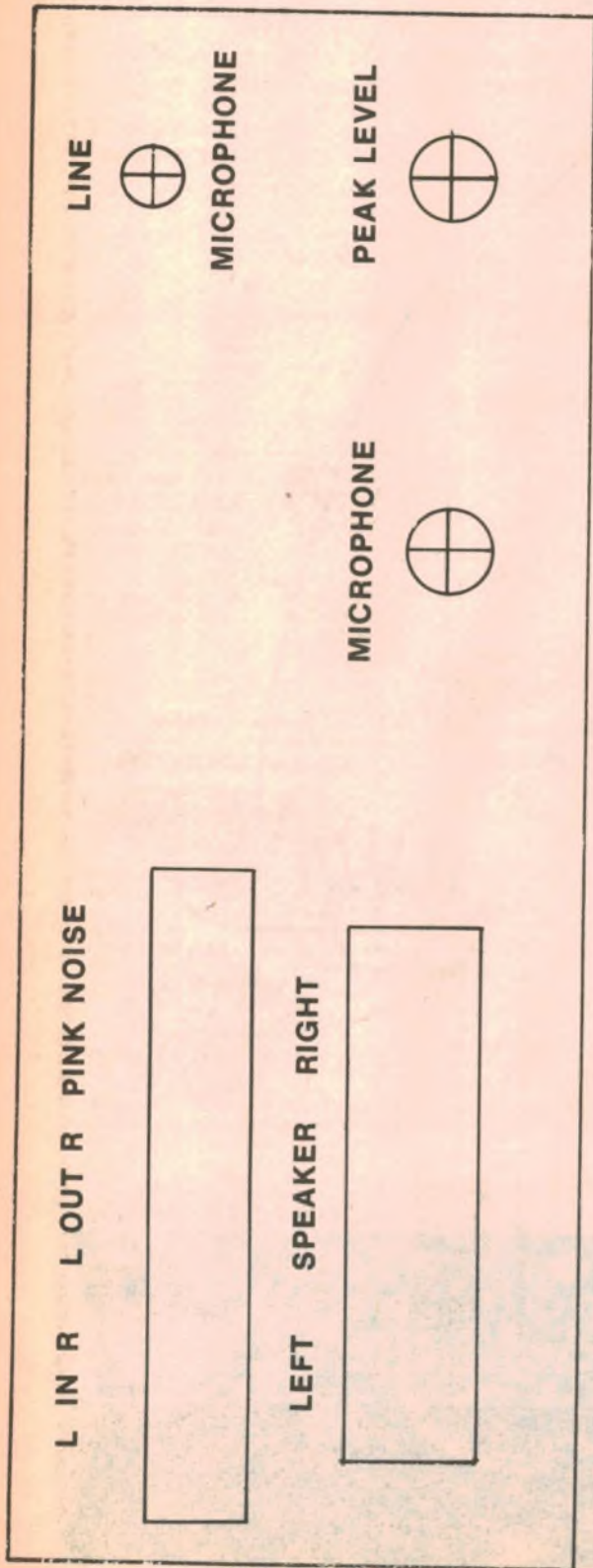
appropriate equaliser slider control is adjusted up and down. With that check complete, all that remains is to confirm the operation of the peak level and power modes.

The Line inputs of the analyser connect to the "Tape Rec" outputs on the

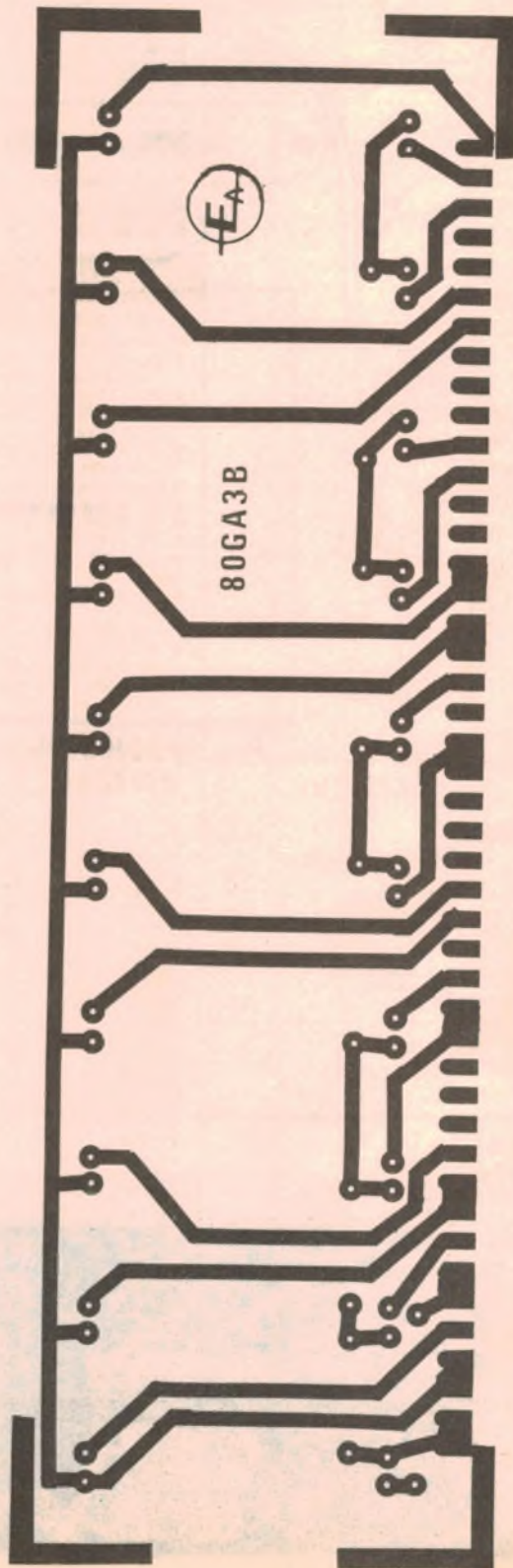
amplifier (or graphic equaliser). The Line inputs and outputs are actually paralleled so that the "Tape Rec" facility is still available for recording. With signals applied to the amplifier, check that the peak level mode functions correctly.

For the power mode, the analyser must be connected to the loudspeaker outputs on the amplifier. Polarity of these connections should be strictly observed. Note that there are protective 15 ohm resistors in series with the 0V loudspeaker inputs to the analyser, just in case you do make a mistake with the connections.

The power display refers to the RMS
(continued on p63)



Shown on this page is the actual size artwork for the rear panel label and the display PCB. Artwork for the main PCB is on page 63.



ROD IRVING ELECTRONICS

499 HIGH STREET, NORTHCOTE 3070, MELBOURNE VICTORIA. Ph. (03) 489 8131.

NEW PRODUCTS

RIE are now distributors for 3M products including Scotchcal range

8016 blue on white plastic	\$4 10
8018 green on white plastic	\$4 10
8011 red on white plastic	\$4 60
8012 black on transparent plastic	\$4 10
8013 black on yellow plastic	\$4 10
8015 black on white plastic	\$4 10
8009 light blue on aluminium	\$4 10
8001 red on aluminium	\$4 10
8005 black on aluminium	\$4 60
8007 reversing film	\$3 75

*Note — all above sheets 10in x 12in

8500 Photosensitive developer	\$4 40
3900 clear coating (glossy finish)	\$9 30
3930 clear coating (matte finish)	\$9 30
ML 3 Applicator block	\$3 90
ML-4 developer pads 10 for 8002KA evaluation kit	\$8 90



Digital hand-held multimeter \$77

EA METAL DETECTOR

EA 79md 9	\$2 60
As A Kit	19 90
(without H/phones)	
ET576	4 90
Dream 6800	9 90
ETI 472	2 90
ETI 471	9 90
ETI 470	2 75
ETI Series 4000 Kit	179 00
ETI 585 Rx ultrasonic Rx	15 95
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INTERSIL ICL7106 LCD EVALUATION KIT \$32.50

INTERSIL LCD 3 1/2 DIGIT PANEL METER KITS

Build a working DPM in 1/2-hour with these complete evaluation kits.

Test these new parts for yourself with intersil's low cost prototyping kits complete with A/D converter and LCD display (for the 7106) or LED display (for the 7107). Kits provide all materials including PC board for a functioning panel meter ICL7106EV (LCD).

COMPONENTS

2114 RAMS	\$6 25
2708 EPROM	8 50
741 s 10 up	2 50
555 s 10 up	2 90
BD139 10 up	4 00
BD140 10 up	4 00
SC141D 10 up	11 00
SC151D 10 up	21 10
RED LEDS 10 up	1 40
RED LEDS 100 up	11 00
YELLOW LEDS 10 up	2 90
8 PIN I/C SKTS 10 up	2 00
BC547 10 up	1 00
BC548	0 15 ea
BC549	0 19 ea
MJ802	3 60
6 800/50V CAPS (LUG)	4 50
5 600/40V CAPS (PCB)	1 90

KITS & CIRCUIT BOARDS

ETI SERIES 4000 AMP

- Complete Kit \$175 00
- Quality front panel to suit above \$7 99
- ETI 470 kit of parts 19 90
- ETI 480 kit of parts 100w (incl bracket) 19 75
- ETI 470 PS kit of parts (includes relay not transformer) 19 50
- Transformer to suit 22 90
- ETI 471 pre-amp 45 50
- ETI 585R ultra sonic RX 15 95
- ETI 585T ultra sonic TX 8 95
- EA 79 SF9 sound flash trigger 15 00
- All parts available for DREAM computer project

- PCB's (all quality fibreglass boards)
- ETI 574 disco strobe 2 80
- ETI 549A metal detector 2 75
- DREAM circuit board 9 90

PROJECT BOARDS (FIBREGLASS)

ETI 043	1 40	ETI 481M	2 00
ETI 044	1 30	ETI 481PS	3 50
ETI 047	1 50	ETI 483	2 20
ETI 061	1 40	ETI 484	3 90
ETI 062	1 80	ETI 485	2 90
ETI 063	1 70	ETI 486	2 90
ETI 064	1 70	ETI 489A	2 50
ETI 065	1 70	ETI 499	1 99
ETI 067	1 80	ETI 528	2 20
ETI 068	1 40	ETI 541	2 20
ETI 071	1 40	ETI 547	2 20
ETI 072	1 80	ETI 581	2 20
ETI 081	1 50	ETI 583	2 20
ETI 083	1 80	ETI 585R	1 60
ETI 084	1 70	ETI 585T	1 40
ETI 085	1 30	ETI 586	2 30
ETI 130	1 90	ETI 603	2 50
ETI 134	1 90	ETI 604	1 60
ETI 135	1 90	ETI 635	2 90
ETI 136	1 80	ETI 638A	3 90
ETI 137A	2 90	ETI 708	1 90
ETI 137B	2 90	ETI 713	3 90
ETI 139	1 90	ETI 714	1 90
ETI 245	1 60	ETI 717	2 90
ETI 417	1 80	EA 78A0B	2 90
ETI 445	1 50	EA 78TMB	2 00
ETI 446	1 90	EA 78N6	3 20
ETI 449	1 50	EA 78NG4	2 50
ETI 450A	1 90	EA 78UT4	3 90
ETI 450B	1 90	EA 78T3	4 20
ETI 480	2 40	EA 78C5	3 90
ETI 480PS	2 40		

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STATIC RAM KIT 16K S-100

KIT FORM \$269.00
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Ideal for use with flat ribbon cable or to mount components on



24 pin \$0 94
 40 pin \$2 00

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SPECIALLY DESIGNED FOR MICROCOMPUTERS

- See Feb 1979 EA for full details
- Good regulation electrostatic shield
- SE 805
- 8V @ 5A 2x15V @ 1A \$18 50
- SE 810
- 8V @ 10A 2x15V @ 1A \$20 50
- SE 820 8V @ 20A 15V @ 1A 15V @ 3A \$30 50

20 TURN CERMET TRIM POT



SPECTROL 43P ACTUAL SIZE

STOCK RESISTANCE VALUES
 10R 20R 50R 100R 200R 500R 1K 2K 5K 10K 20K 50K 100K 200K 500K 1M 2M

1-9	\$1 20
10-99	0 95
100	0 90

Values may be mixed

Hexadecimal Keypad \$19.50/each

19-key pad includes 1-10 keys ABCDEF and 2 optional keys and a shift key

Ideal for dream project

MULTIDIALS

Dials to suit 10 T Pots

Model 21 1 8" dia	\$9 90
Model 16 9" dia	\$9 50
Model 18 1 1" x 1 75" dia	\$17 50

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Muffin fan 4 1/2" square

110V	\$26 50
240V	\$24 50

Sprite fan 3 1/2" square

110V	\$26 50
240V	\$24 50

Range of larger fans available. Send for details



cermet single TURN TRIM POT
 Spectrol model 63P ACTUAL SIZE

STOCK VALUES

10R 20R 50R 100R 200R 500R 1K 2K 5K 10K 20K 50K 200K 500K 1M 2M	
1-9	0 95
10-99	0 85
100	0 75

Values may be mixed.

P.C. EDGE CONNECTORS



\$100 gold plated wire wrap	\$6 50
\$100 solder tail	\$6 90
D2 Motorola bus	
43/86 solder tail	\$6 34
43/86 gold plated wire wrap	\$7 40

DREAM

ELECTRONIC AUSTRALIA MICROCOMPUTER PROJECT

Kit for main board (including programme 2708)

\$109 00

PCB (fibre glass) only	\$9 90
2708 programmed	\$15 60
Key Pad 19 keys	\$17 50
Kit (less key pad)	\$90 00
PCB for power supply	\$3 50

10 TURN POTENTIOMETERS

Stock resistance values

50R 100R 200R 500R 1K 2K 5K 10K 20K 50K 100K	
--	--

Spectrol model 534 1/4" shaft

Price 1-9	\$6 25
10 + values may be mixed	\$5 75

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DC Volts: 0.25, 2.5, 10, 50, 250, 1000 (100kV)
 AC Volts: 5, 10, 50, 250, 1000
 DC Current: 10uA, 25uA, 0.5mA, 5mA, 50mA, 500mA,
 & 10A AC current: 10A
 Resistance: 20, 200, 20k & 200k centre scale
 Decibels -10 to -62
 Transistor: h_{FE} 0-500; I_{CE} 0-50uA
 Capacitance: 50pF to 3uF; 0.01uF to 50uF

ONLY
\$69.50

Q-1140

See the review in February
Electronics Today Intl.

More than a multimeter. More than a transistor checker. This one measures capacitance, too!!!

Incredible value! This superb 100,000 ohm per volt multimeter is probably the handiest instrument you will ever own. For with its 36 ranges, you can not only measure voltages, currents, resistances, etc like most other multimeters, you can actually check transistors and capacitors! And with the optional RF probe, you can extend the range of your meter up to 30MHz - ideal for trouble-shooting RF circuits too!

Whether you're a hobbyist, amateur, service technician, or engineer you'll find this meter will give years of accurate, reliable service. It's fully protected (internal fuse protection); has large, mirrored scale for accurate reading and even has a polarity reversal switch. Supplied complete with instruction manual, test leads and transistor connection leads.

YES! We have many other feature-packed multimeters in stock, from a low \$12.50. Call in and see our superb range soon - along with a host of other test gear!

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Dick's new lab. oscilloscope ...



Cat Q-1280

A bargain! 5MHz bandwidth; 10mV/div (vert) and under \$200.00!!

That's right - it's the new Dick Smith Laboratory Oscilloscope; just right for the amateur, hobbyist or service desk. Why pay up to \$100.00 more for a CRO and do no better?

\$199.00

DUE IN STOCK LATE THIS MONTH!

IS SERVICING YOUR GAME?

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Ideal for the test bench or service vehicle.



Cat Q-1380

\$49.50

WANT TO GO DIGITAL?



Cat Q-1440

\$145.00

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Battery operated, or mains operation with optional 'plug-pack' adaptor (M-9525 @ \$6.90).

High impedance input - 10Mohm AC & DC; ranges 200mV - 1kV DC, 200mV - 700V AC, 200uA - 2A AC & DC, 2k to 20M ohms. Better than 0.1% accuracy on DC!

THE DIPPER...

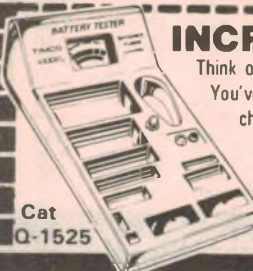


Cat Q-1322

Ask an amateur how handy his 'dipper' is! He'll tell you he wouldn't be without one. For circuit checking, signal generation, as an absorption wavemeter, modulation checker... the list of uses for this incredible instrument goes on and on. There are a lot of 'cheapie' dippers on the market: this is one of the top models available. Recommended.

\$99.50

INCREDIBLY HANDY...



Cat Q-1525

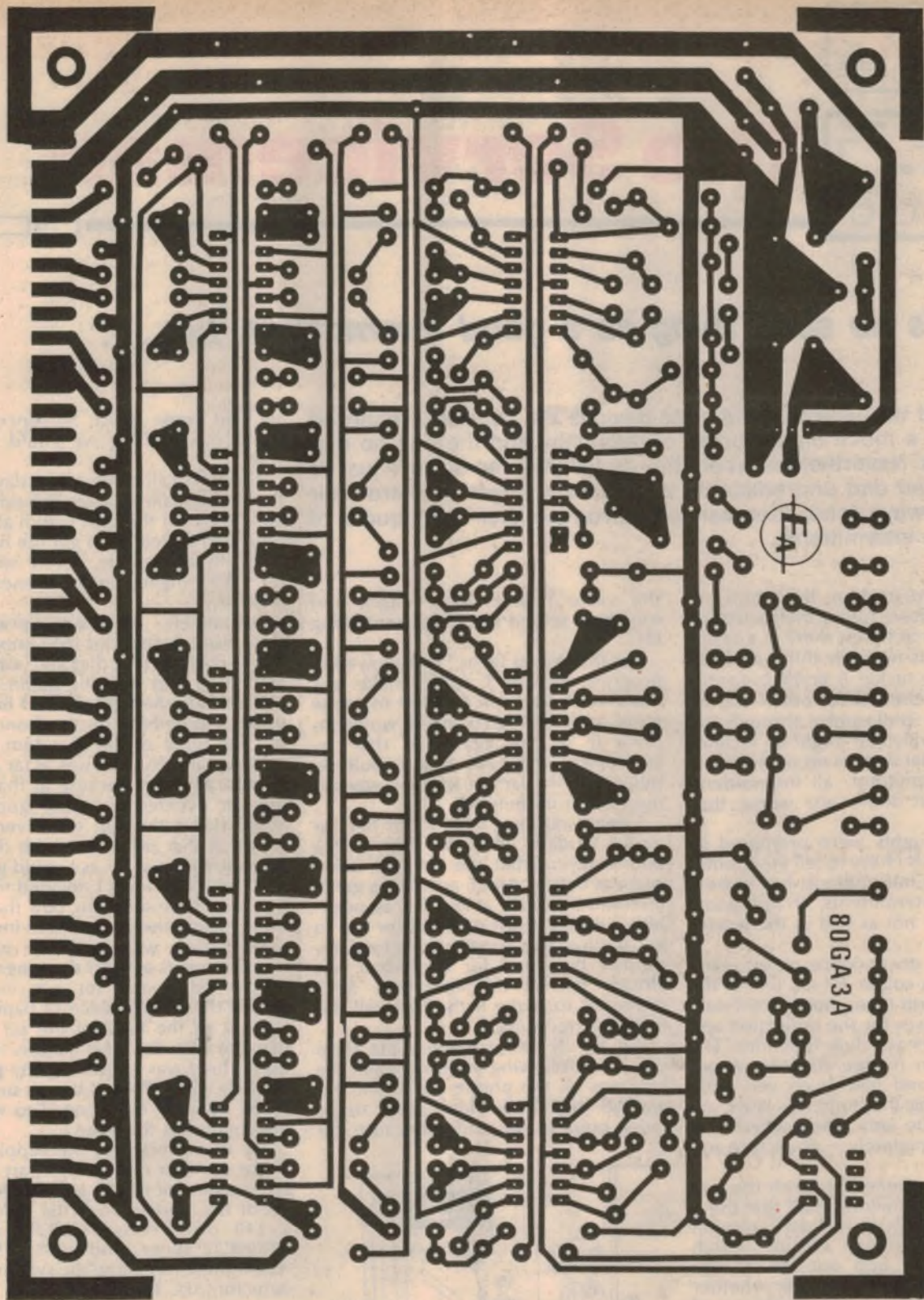
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sinewave power into a resistive 8 ohm load. You can refer the power into 4 ohm loads or 16 ohm loads by changing the circuit slightly. For 4 ohm loads, the 10k resistor in the input voltage divider (associated with the S1b and S1a) should be changed to 4.7k. For 16 ohm loads, change it to 22k.

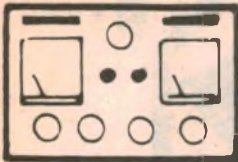
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imum, and there are no connections to the line inputs supersonic oscillation may result and some of the LEDs will turn on. This is not a fault and is a natural consequence of the high input impedance and large gains used. The condition will disappear immediately when normal connections are made to the line inputs, whether or not there is an input signal.



The Serviceman

There's no such thing as a good intermittent, but . . .

Compared with valves, solid state devices are generally regarded as having a much higher order of reliability, and there is no disputing this. Nevertheless, when they do fail they can do so in just as many varied and unpredictable ways as did valves. Nor are their failures always total; they can also produce their own quota of tantalising intermittents.

Among Australian bushmen, or others who have found themselves on short rations at times, there is a saying that "there is no such thing as crook tucker." Any tucker is good, but some tucker is better than other tucker! Shifting this philosophy through 180 degrees, servicemen might be inclined to observe that there is no such thing as a good intermittent; all intermittents are bad, but some are worse than others!

These thoughts were prompted by the two stories I have to tell this month; both involve intermittents but in both cases the intermittents, if not good, were at least not as bad as the worst I have known.

The first story concerns an early model Decca colour TV set, one of the 33 series hybrid type; mostly solid state but using valves for the deflection and some other heavy duty functions. The set had been in operation for about three years and had given very little trouble during that time. But now, according to the lady who owned it, it had failed completely — no picture and no sound.

When she phoned me with the bad news I immediately recalled that these sets have a thermal overload cut-out in the mains primary circuit which sometimes will pop out for no apparent reason. So I asked her whether she was aware of this button and whether she had checked it. She was not aware of it but, following my instructions, she checked it while I waited on the phone. She returned in a minute or so and reported that this had made no difference.

When I made the service call the set started out exactly as the lady had described it; no picture and no sound. But when I removed the back I realised that it was not completely dead, in that

the valve heaters were alight and somehow sensed that it was generating EHT.

But that was as far as I was allowed to progress. Before I could make any more tests, the set decided to come good, and nothing I could do would induce it to fail again. In the circumstances, there was little I could do but advise the lady to call me when it decided to misbehave.

I heard nothing more from her for about 10 days; then she was on the phone saying that the set had failed again as before. Much as I like to get at intermittent faults as quickly as possible, it was just not practical for me to get at it that day. For one thing I was extremely busy and for another it was already late in the afternoon. So I promised to make it the first call the following morning.

But hardly had I opened the shop doors the following morning when the lady was on the phone again. She explained that there didn't seem to be much point in my calling because the

set had come good. So, once more, there was nothing we could do but wait.

The next call came a few days later; the set had failed again. This time I was able to be on the spot within about an hour and I decided to get the back off, as gently as possible, before switching on — keeping my fingers crossed in the process.

Fortunately, the fault decided to show itself, at least for long enough for me to confirm that that EHT was being generated and that the audio section was alive. In the light of this I began to suspect something up the front of the set; the tuner or the IF system.

Unfortunately, that was as far as I was able to progress because at that point the set decided to come good. I'm afraid that I thought some very rude words at that point but, with the lady present, that was far as I could go. At a more practical level I decided to make the best of the situation, now that I had some idea of the general area involved.

The idea was to take voltage measurements around the tuner and IF circuits while the set was working, record these on a piece of paper, and leave it in the back of the set in anticipation of the next failure. Having done this I was explaining my plan to the lady when, Presto! the set suddenly failed again. (I didn't need to restrain my comments this time.)

My first check was the supply rails. There are two rails in this part of the set; a main rail of 25V and a secondary rail of 12V, derived from the 25V rail via a 110 ohm resistor (R29) and a BZX61C12 zener diode (D2). This rail supplies the tuner and the synchronous detector/AFC IC chip TCA 270.

The 25V rail read normal but I knew I was getting close when the 12V rail read only about 3V. Well, at least that was something, even if I still had to find the exact cause. I felt that the most likely possibility was excessive current drain due to a failure of some component fed by this rail, so I began progressively disconnecting everything connected to it.

I finished up with virtually everything disconnected, including some electrolytics immediately adjacent to the



*"There's no time like the present when you're up against an intermittent!"
(From "Radio-Electronics").*

zener, and still had only 3V. This left only the 110 ohm resistor and the zener and I quickly cleared the resistor of suspicion. This left the zener and, doubtful though I was, I disconnected it also.

The voltage shot up immediately to something over 12 and I knew I had found it. I fitted a new zener, restored the other connections, and switched on. The voltage pegged immediately at 12 and, as the valves warmed up, up came the picture and sound.

So there it was, a zener diode with an intermittent breakdown; something which I certainly have not struck before and which I confess I still find rather puzzling. An intermittent open circuit is not hard to visualise, but I always imagined that once a junction in any solid state device had broken down that it was broken down completely and for good. Now I know better.

ANOTHER ONE!

My next story also involves an intermittent fault but, once again, it was in a less vicious form than these things can sometimes be. There was also some similarity in the cause, as will become apparent.

The set was a Rank Arena 22in, model 2201. The initial fault was complete failure and the owner, who had some electronic background, had established that the tripler had failed. However, in the light of what I subsequently found, it is obvious that there was a lot more to the history of the set than I was told about. In fact, I strongly suspect that the failed EHT tripler may well have been caused by a clumsy effort to locate an earlier fault.

But, not knowing this, I simply took the owner's word for it and ordered a replacement tripler. The only other comment by the owner was a somewhat garbled comment about the set losing colour on occasions, but there was little I could do about this until the tripler was replaced and I had a picture to look at.

When the tripler arrived and was fitted the EHT came good, but this only served to reveal another fault; complete lack of vertical deflection. This, I suspect, was what the owner was trying to fix when he damaged the tripler.

At this point I realised that I was lacking some essential data for this set. I had a copy of the circuit, but no manual. This would have not been so bad, had the circuit featured the various waveforms, but it didn't. These were presented separately in the complete manual. So the first thing to do was contact the makers and order a manual.

At the same time I had the opportunity to talk to one of the company technicians, and he suggested several components which would be most suspect for this fault, in this model. Armed with this information and a few other points, I went back to the set and

began checking waveforms from the vertical oscillator onwards. Even without the exact waveforms, I reckon I could pick the point of total failure.

In this set the vertical amplifier and a couple of following amplifier stages are located on the "deflection board", while additional amplifier stages and the output stage are on a separate board, the "deflection output board." It was easiest to check the waveform at the input to the output board and here I found what seemed to be a reasonable shape and amplitude. (When the manual subsequently arrived, it was shown to be spot on.)

The first stage on the output board is the third vertical amplifier (TR410), followed by the vertical drive stage (TR411), and the vertical output stage (TR409). As already stated, the waveform into the third amplifier stage was normal, but the output from it was anything but. My first reaction was to blame this stage, except that the manufacturer's technician had warned me that the next stage, the driver, was the more likely culprit.

In addition to the transistor in this stage there are three diodes in what appears to be some kind of wave shaping network, and he had warned that any of these four components should be suspect and that, in some circumstances, the fault could load the previous stage.

The easiest way to check this possibility was simply to replace the transistor and three diodes, which I did. This proved to be the right thing to do, even though it did not effect a complete cure. I now had vertical scan, but limited to about one third of the screen height.

So what now? Was the third amplifier stage also faulty? In the light of the checks I had made so far it seemed very likely, so out came that transistor and in went a new one. And that was the answer. Up came the vertical scan to full height and, after a few routine adjustments, the set was delivering a first class picture.

A LINGERING DOUBT

At that stage I could easily have regarded the job as finished, except for two things. One was the hint of a possible intermittent colour fault, the other was the fact that the owner was on holidays and I could not have returned the set to him anyway.

In fact, in the vague description of the colour fault a comment had been made which suggested that the symptom was not loss of colour in the total sense, but rather loss of chroma lock. It is fairly easy to adjust the reference oscillator APC loop in this set. The stage is provided with a small slide switch (SW751) which allows the oscillator to run free while the APC adjustment pot (VR706) is adjusted to give the best approach to a locked colour pattern.

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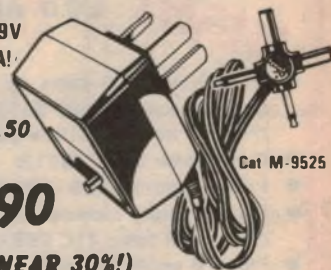
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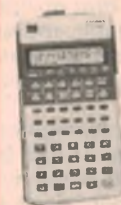
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SERVICEMAN: Problems with intermittents

I went through this routine, and everything seemed normal except that the pot needed to be set fairly close to one end of its travel. I didn't take a great deal of notice of this at the time, but simply moved the set into "intermittent corner" and let it run while I went on with other jobs.

All went well for a couple of days, when I happened to look up from another job and realised that the frame had partially collapsed by about two inches at the top and bottom. And a little while later — I could not attend to it immediately — it suddenly went out of chroma lock. Then, to cap it all, it developed intermittent flashes on screen, seemingly not related to anything.

It is times like these that one is sorely tempted to give the whole game away and buy a chicken farm. While I had been half expecting the chroma lock fault, the reappearance of vertical scan problems, which I thought I had solved, was a cruel blow — with the flashes thrown in just to make it harder!

I went through the chroma lock routine again and it came good, but with the difference that VR706 was now set at about its mid position — more or less where I imagined it should be. At the same time I re-set the height, mainly to see how the scan responded, and again everything seemed to come up normally. But, needless to say, I wasn't convinced.

The set ran like this for several days then just as suddenly as before, it dropped out of chroma lock. And, very significantly, I realised that it was now overscanning vertically, and that the flashing had returned. It was too much of a coincidence to suggest that all three faults could all pop up at the same time without there being some common cause, widely separated as the vertical scan and chroma lock circuits might be.

A VITAL CLUE

As it turned out, it was this wide separation of the circuits which gave me a clue. About the only thing they had in common was the supply rail, so I decided to check that first. There are two main supply rails in this set, one regulated at 120V and the other, also regulated, at 19V.

It was the latter one I suspected, since it supplies the vertical oscillator and amplifier circuits, plus the chroma board, among others. The voltage is derived from a small winding on the EHT transformer, via a diode (D554) a filter capacitor (C562) and a regulator transistor (TR505). The latter derives its base voltage from the 120V rail via an 8.2k resistor (R561) and a zener diode network.

The zener diode network delivers

19.7V, and consists of the zener diode itself, plus two ordinary diodes in series. I am not exactly sure as to the purpose of these diodes, but I suspect that it is to pad the voltage up slightly, above that available from a standard zener. Anyway, the end result is that the transistor develops 19V at its emitter after allowing for its own losses.

At least, it was supposed to develop 19V. When I measured it in what I regarded as the fault condition, it was closer to 25V. I knew then that I was on the right track. My first reaction was to blame the regulator transistor which, if it had shorted internally, could produce excessive voltage. On the other hand, and in spite of my experience related in the previous story, I hesitated to accept the idea of an intermittent short circuit.

An intermittent open circuit was a more likely possibility, and this suggested the zener diode as the likely culprit. A meter between base and chassis showed 25V plus, thereby confirming that the transistor was doing its job and narrowing the search to the zener network.

A measurement across the zener showed about 15V, which didn't make much sense in itself. Next I measured across the diode nearest the chassis and

found about 0.3V — about what one would expect — but it was a different story across the other diode. This had about 9V across it; a quite ridiculous figure.

Replacing it pulled everything back into line. The rail supply came up spot on 19V, the chroma lock pot settled into its mid position, and the vertical overscan vanished. And, for good measure, there was no immediate sign of the intermittent flashes. Nor have any of the symptoms shown up since, and it has now been running in the workshop for two weeks. The owner is due back shortly and by that time I imagine that I will be able to return it to him with complete confidence.

But what a sequence of events. And what potential for misunderstanding and recrimination. If it hadn't been for the casual mention, almost as an afterthought, of the colour problem, I could easily have imagined that I had finished the job after replacing the vertical amplifier and driver stages. After all, I had already found two faults which nobody had mentioned and which I didn't expect.

Had this happened the owner would, at best, have been thumping my counter and complaining that I had not done the job properly. At worst he wouldn't even have bothered to tell me — but he would have told everybody else!

As I said at the beginning, there is no such thing as a good intermittent. ☹

Another Chapter in the History of Wireless —

Stanley Mullard 1883-1979

A significant chapter in British (and Australian) electronics history came to a close with the death of Stanley Mullard in September last. He left behind a brand-name which will not easily be forgotten by those who have grown up with the industry.

Born in 1883, Stanley Mullard attended Sussex Polytechnic and took a position with an electric lamp manufacturer. Continuing his studies at the Northampton Institute, he became a director of the Company at 24, but left it to join Ediswan in 1915.

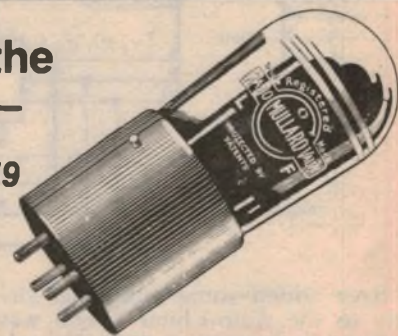
Even though a member of the R. N. Reserve, he continued with Ediswan during the war, involved in the production of valves for the British Admiralty. He later took charge of a special laboratory at Imperial College, London.

In 1920, he established the Mullard Valve Company and, with production exceeding two million

valves per year in 1924, he became one of the fathers of Britain's radio industry.

At about that time, he also established links with Philips in Holland, who acquired all the shares in the company over the next few years. Stanley Mullard resigned as Managing Director in 1929 but remained active in the company affairs until 1970. During that period Philips in England was — Mullard!

And in Australia, during that period, Mullard competed vigorously in its own right, even against its parent company, under the guidance of the late Eric Dare and, subsequently, the late Maurice Brown. More recently, when Philips reorganised in Australia, Mullard was officially absorbed.

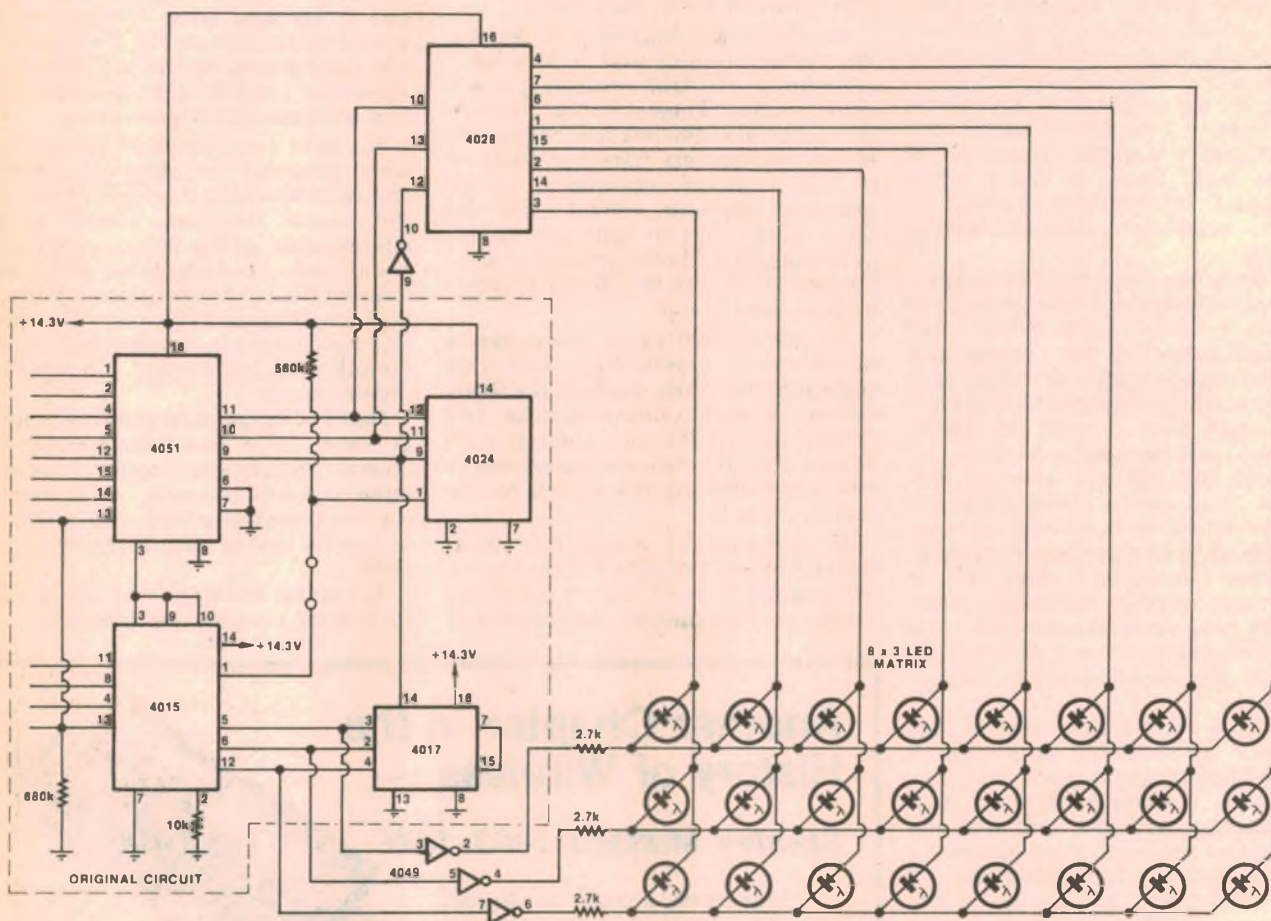


CIRCUIT & DESIGN IDEAS

Interesting circuit ideas and design notes selected from technical literature, reader contributions and staff jottings. As they have not necessarily been tested in our laboratory, responsibility cannot be accepted. Contributions to this section are always welcome, and will be paid for if used.

Conducted by Ian Pogson

Auto-chime — which tune is next?



I have added some additional circuitry to the Auto-Chime which was described in September, 1979. The additions are arranged to give an indication as to which tune is to be played next. It is quite simple to add, I used a piece of Veroboard to carry the two extra ICs.

I chose LEDs for the indicators in preference to a 7-segment readout because I think that it has a better appearance and it is a simpler approach. I built the LEDs around a square box but they may be arranged as each individual constructor wishes. The repertoire list may also be added to the

LEDs and the next tune may then be read off.

The added circuitry has proved to be very satisfactory and it cost me about \$7.00, including the LEDs.

(By Mr R. Gareb, 17/37-39 O'Donnell Street, Bondi, NSW 2026.)

Novel way to play your old 78s

I built a Wien bridge audio oscillator and I have found it to be a very useful piece of equipment in enabling me to play my old 78 recordings on my two-speed synchronous motor turntable.

Rather than build a separate power amplifier for it, I fed the output of the audio oscillator into the right channel of my existing stereo amplifier. The left channel carries the signal from the pickup as usual. I wired in a 12V to 240V power transformer between the right

channel speaker terminals and the turntable motor, with the 240V winding connected to the motor. This arrangement gives the necessary speed of 78rpm when the turntable is set to 45rpm and the audio oscillator set to 86.6Hz.

I have found this arrangement to be a satisfactory one and I thought that other readers in a similar position may be interested to try it.

(By Mr M. R. Lewis, 26 Waterdale

Road Ivanhoe, Victoria 3079.)

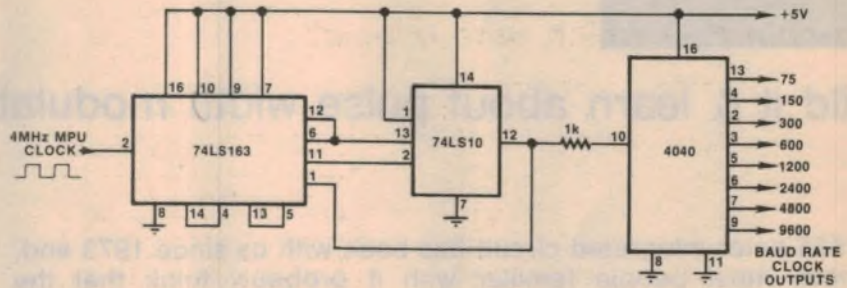
Editorial note: This idea is a good one but readers should be alerted to the possible dangers involved. Some amplifiers may not like being connected to a transformer as described, for a number of reasons. Unless readers are familiar with the ramifications and able to adjust for the right amount of drive etc, it would be wise to avoid taking any risks. (See "Audio Talk" P40).

Direct derivation of baud rate clock signals from a 4MHz clock signal

The specific ICs designed to provide these signals are generally rather expensive and tend to use a separate non-standard quartz crystal. This generally results in a system costing of the order of \$30 merely to generate those I/O clock signals.

After some thought and the use of a calculator, it became clear that another far less expensive method of obtaining these important signals was possible. The result is a circuit which produces 16x baud rate clock signals only +0.16% above the nominal values and which is in a constant timing and phase relationship with the MPU clock signals.

In operation, the 74LS163 (any 4 bit resettable counter may be used) is driven by the 4MHz clock signal, derived in the author's system from a 6875 clock generator. The 74LS10 is used to decode a count of 13 (decimal), hence



we have a modulo 13 counter. The resulting signal has a repetition rate equivalent to 307.692kHz, as against the nominal 307.2kHz.

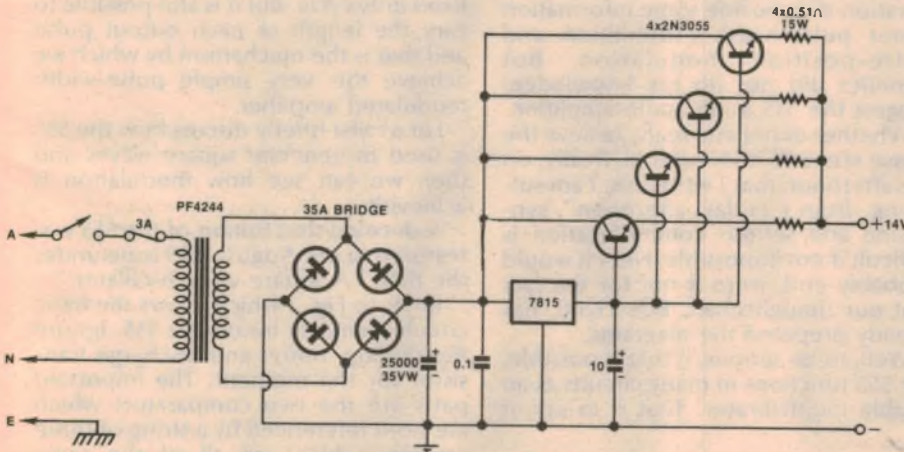
This is further divided by the 4040 12-stage binary counter to give appropriate output frequencies for 9600 baud, 4800 baud, 2400 baud, 1200 baud, 600 baud, 300 baud, 150 baud and 75 baud. Since the author's system does not include a TTY it was thought an un-

necessary refinement to generate a 110 signal.

The outputs of the 4040 may be buffered as required to suit the system in use. I hope that this information may be of use to other interested readers.

(By Mr C. C. Wright, Architecture Laboratory, The University of Auckland, Private Bag, Auckland, New Zealand.)

Simple high current regulated power supply



The need arose for a simple high current regulated power supply and the circuit shows how that need was met. The circuit delivers approximately 14V up to about 18A.

A Ferguson type PF4244 transformer is used. It is rated at 300VA and the two secondary windings, rated at 16V and 9A are connected in parallel. The rectifier unit is a diode bridge rated at 35A. Filtering is by a 25000uF 35VW electrolytic capacitor.

A series regulator consists of four 2N3055 power transistors in parallel. These are supplied with 15V from a type 7815 regulator IC. This gives an output voltage very close to 14V. A 7812 IC may be used but this would only give an output of about 11V, which is not really sufficient for mobile use.

In the prototype, the output voltage dropped less than 0.5V at a load of 10A. It is most important to provide adequate heat sinking for the diode bridge and the 2N3055s.

(By Mr K. Taylor, VK3YOS, 48 Albert Street, Warragul, Victoria 3820.)

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An unusual audio amplifier

Build it & learn about pulse width modulation

The 555 timer integrated circuit has been with us since 1973 and, by now, most people familiar with it probably think that the applications for it have been exhausted. But did you know the 555 can be used as an audio amplifier? Well it can! It may not be really practical but it can be done.

by LEO SIMPSON

The main application for the 555 integrated circuit is in timing and oscillator circuits. It is not a linear device and cannot be used to amplify audio signals in the usual way. But it can be used to provide the basis for a simple "pulse width modulation" amplifier. As such, it is not a practical amplifier — it is not likely that you would use it in preference to a more conventional amplifier. But it can be demonstrated.

The idea for this article came to the author on an otherwise uneventful day when he was staring into the middle-distance during postprandial depression. This latter remark means that I had had quite a lot to eat and I wasn't sure whether it was for the best.

But in spite of its inauspicious origins (it must have been the garlic prawns), the idea has a certain compelling quality about it. After all, the 555 has apparently been used in just about every thinkable application (and probably a

few that are unthinkable) except as an audio amplifier. Now that is a challenge that no self-respecting designer could possibly overlook.

Here I must confess that the idea is not completely original. After all, the original literature from Signetics Corporation did provide some information about pulse-width modulation and pulse-position modulation. But Signetics did not (to my knowledge) suggest the 555 as an audio amplifier.

Whether or not you really believe the above scenario is immaterial. Really, on the afternoon that I write this, I am suffering from "Friday afternoon" syndrome and serious communication is difficult if not impossible. Here it would probably end, were it not for the fact that our draughtsman, Bob Flynn, has already prepared the diagrams.

Well, to be serious, if that is possible, the 555 functions in many circuits as an astable multivibrator. That is to say, it

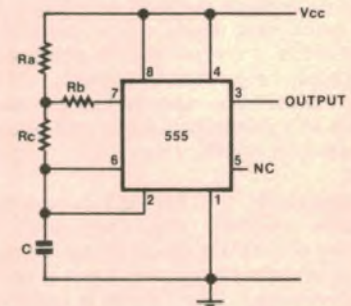


FIG. 2: THE 555 AS AN ASTABLE

can be a source of square waves with a fixed duty cycle. But it is also possible to vary the length of each output pulse and that is the mechanism by which we achieve this very simple pulse-width modulated amplifier.

Let us first briefly discuss how the 555 is used to generate square waves and then we can see how modulation is achieved.

A detailed description of the 555 was featured in our August 1979 issue under the title, "A square wave oscillator".

Refer to Fig. 1 which shows the basic circuit elements inside the 555. Ignore the flipflop, buffer and discharge transistor for the moment. The important parts are the two comparators which are both referenced by a string of three resistors which are all of the same value, 5k. Thus, comparator A is referenced to $2/3 V_{cc}$ while comparator B is referenced to $1/3 V_{cc}$. V_{cc} is the supply rail.

ASTABLE MULTIVIBRATOR

Now refer to Fig. 2 which shows how the 555 is connected in a typical astable multivibrator circuit. Pins six and two of the 555 are connected together, which means that the non-inverting input of comparator A connects to the inverting input of comparator B. In this way, the comparators monitor the voltage across capacitor C which is charged from V_{cc} via resistors R_a and R_c .

When power is first applied to the circuit, there is no voltage across the capacitor and thus the inputs of both comparators are held low. This means

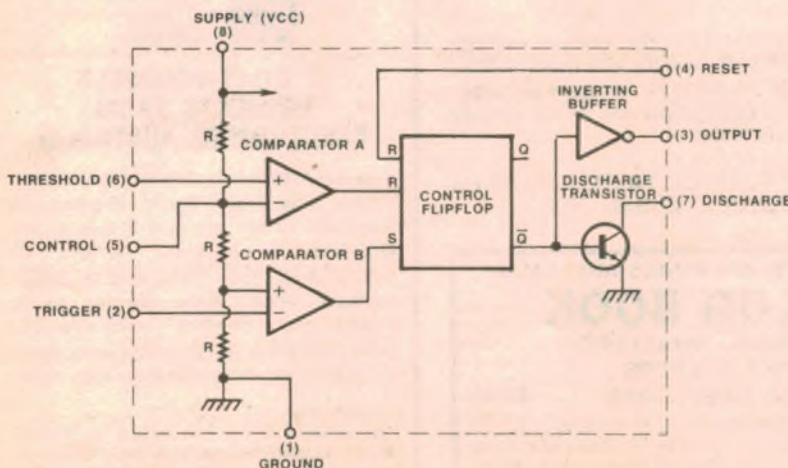


FIG. 1: INSIDE THE 555

that the output at pin three is high and the discharge transistor at pin seven is held off. The capacitor now charges up towards 2/3 Vcc. When it reaches this point, the output of comparator A toggles the flipflop and the output at pin three goes low. At the same time the discharge transistor at pin seven turns on.

Capacitor C now discharges towards 1/3 Vcc via resistors Rb and Rc. When the capacitor voltage drops to 1/3 Vcc, the output of comparator B toggles the flipflop again so that the output at pin three goes high and the discharge transistor at pin seven turns off. Capacitor C then begins to charge up again.

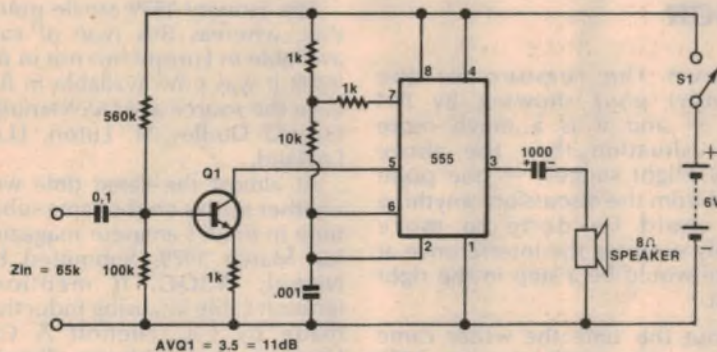


FIG. 3

This unconventional circuit will function as an audio amplifier when fed with a signal of up to several hundred millivolts RMS. Why not try it just for fun?

This cycle continues indefinitely, or until you turn the power off! The result is a pulse waveform at pin three and a sawtooth waveform across capacitor C. By suitable selection of resistors Ra, Rb and Rc we can arrange for the output at pin 3 to be an almost exact square wave.

MARK/SPACE RATIO

There is another method whereby we can change the mark/space ratio of the output waveform. This uses pin five which is labelled "control" or "FM" in some manufacturers' data. Pin five is connected to the string of 5k resistors which set the thresholds for comparators A and B. It is possible to change these comparator thresholds merely by connecting external resistors from Vcc or Ground to pin five, or by feeding an external voltage into this point.

Normally, pin five is set at 2/3 Vcc by the internal voltage divider of 5k resistors, referred to earlier. If pin five is held higher than 2/3 Vcc by external means, capacitor C will take longer to reach the new threshold for comparator A and longer for the capacitor to discharge to the threshold for comparator B. The net effect of this is to lower the repetition rate of the output square wave.

Similarly, if pin five is held lower than

normal by external means, the repetition rate of the output square wave will be increased. But if the voltage at pin five is continuously changed by an audio signal the net effect will be to change the mark/space ratio of the output waveform. This is shown in Fig. 4.

Reference to the complete circuit of Fig. 3 shows just how this modulation is performed. An NPN transistor Q1 is connected as a common-emitter amplifier with its collector connected to pin five of the 555. Q1 provides a higher input impedance than is available at pin five and also gives a modest order of gain, about 3.5 times.

Feeding an audio signal into the base of Q1 produces an amplified version of

follows the input sinewave.

In effect, the loudspeaker functions as a mechanical low-pass filter, removing the high frequency "carrier" and reproducing only the modulating signal.

This amplifier really does work and gives quite good results although the effective power output is low, of the order of a few milliwatts at maximum. Any signal source such as a cassette deck or tuner, will drive it to full output. Why not give it a try?

FOOTNOTE

Some readers may not be fully satisfied with the explanation of this amplifier. While it does demonstrate

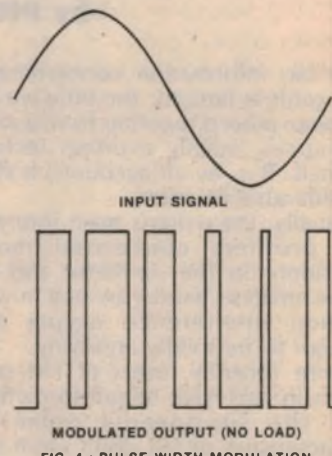


FIG. 4 : PULSE-WIDTH MODULATION

The loudspeaker functions as a mechanical low-pass filter and so responds to the average value of the output waveform.


the signal at pin five. Pin five then continuously changes the thresholds of the two internal comparators in the 555 to produce an output square wave with a continuously changing mark/space ratio. This waveform is coupled to a loudspeaker via a 1000uF capacitor.

With no signal applied to Q1, the output square wave is roughly 66kHz. Naturally, the loudspeaker does not respond directly to this high frequency. Instead the loudspeaker responds to the average DC value of the modulated square wave. Referring again to Fig. 4 it can be seen that the average DC value of the output square wave roughly

the principle of pulse-width modulation, it is, strictly-speaking not a pulse-width modulation amplifier. More correctly speaking, the circuit produces "pulse-position modulation" or, more simply, frequency modulation. Literature supplied by Signetics Corporation gives a more complicated circuit employing the 555 which does result in pulse-width modulation. We preferred the circuit presented here as it is simple and self-contained.

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Ignition interference — is this the answer?

Inductive ignition cable

Ignition interference in mobile radio equipment has always been a problem, and the increasing popularity of FM car radios has highlighted it in a new context. This article discusses a special type of ignition cable, claimed to have superior suppression characteristics, which is being used overseas.

by PHILIP WATSON

So far, information concerning the new cable is limited; the little we have has been pieced together from a variety of sources, mainly overseas technical journals. But, by all accounts, it shows considerable promise.

Initially, the writer's main interest in the problem concerned mobile operation on the six-metre and two-metre amateur bands; an area in which ignition interference occurs often enough to be mildly annoying.

More recently, users of FM stereo radios in cars have begun to complain that the supposedly noise-free characteristics of FM don't seem to be working out in practice; ignition interference is making itself evident in an area where they were led to believe they would receive beautiful music against a quiet background.

The problem was highlighted when a reader (J.R. of Wahroonga, NSW) wrote to our "Forum" column (September 1978) complaining about ignition and other noises in his domestic FM system and querying why the FM system appeared not to be living up to the claims made for it.

This brought a letter from N.H. of North Carlton, Victoria (December 1978), drawing attention to the much more serious situation involving FM radios in cars. A professional car radio installation mechanic, he claimed that it was almost impossible to eliminate ignition interference from FM car radios by any economical means.

This prompted a comment from T.B. of St Ives, NSW (February 1979), who pointed out that effective noise cancelling systems were available and that he was surprised that N.H. was not aware of these.

Back came a reply from N.H. (May 1979) saying that he was well aware of these devices but that they had a number of drawbacks. They were fairly expensive to buy and, in some cases, even more expensive to fit. In addition, they introduced some distortion and also reduced the stereo separation.

It seemed we were back to square one!

Whatever the reasons for the (apparently) poor showing by FM systems — and it is a much more complex situation than the above summary might suggest — one point emerged from the discussion; anything which could be done to more effectively suppress the interference at its source would be a step in the right direction.

At about this time the writer came across an article in the January 1979 issue of "Radio Communication", the British amateur journal published by the Radio Society of Great Britain. It referred to an article in their May 1976

issue, by Dennis Morris, G3AYJ, of Lucas Electrical Ltd, dealing with vehicle interference suppression in general, and mentioning inductive ignition cable. (Apart from this, this article is a very good one in its own right.)

The January 1979 article pointed out that, whereas this type of cable was available in Europe but not in Britain in 1976, it was now available in Britain. It gave the source as MAS Manufacturing Ltd, 43 Dudley St, Luton, LU2 ONP, England.

At almost the same time we found another article on the same subject, this time in the US amateur magazine, "73" for March 1979. Submitted by Larry Nickel, W3QG, it mentioned an ignition cable kit, using inductive cable, made by C.E. Niehoff & Co, 4925 Lawrence Ave, Chicago, Illinois 60630, USA. The author went on to give a glowing account of how this cable virtually wiped ignition interference in his own car on the 2-metre band.

Resistive plugs may also help

Another weapon in the fight against ignition interference, and one which is already used extensively both overseas and in Australia, is the resistive spark plug. While its use to date has been mainly limited to professionally installed two-way radio systems, particularly marine systems, the current interest in entertainment FM systems may result in it becoming more widely accepted.

Resistive spark plugs look the same as conventional plugs, but have a resistor inside the porcelain insulator, between the terminal and the centre electrode, joining the latter at about the level of the outer

metal shell. The resistance is about 4000 ohms.

These plugs are intended for use with conventional resistive suppressor cable, but probably would be just as valuable if added to inductive ignition cable. They may also be used with lumped resistance inserted in wire ignition cables, although this approach is generally regarded as less effective than that using resistive cable.

Resistive spark plugs are handled in Australia by the Champion Spark Plug Co, who stock them in all popular types. While they are not generally available from service stations, they are stocked by the larger distributors. They carry the letter "R" in the type number, e.g., RBL-11Y.

Champion also have available an informative booklet entitled "Giving Two-Way Radio its Voice" (No. 7R) which contains a lot of useful advice concerning vehicle noise suppression in general, as well as descriptions of the resistive plugs.

This booklet is available for the asking from Champion Spark Plug Co, (Aust) Pty Ltd, PO Box 165, Alexandria, NSW, 2015.



Comparison of ignition suppression devices

These were not the first references to inductive cable we had encountered. We first heard of it at an RF interference workshop conducted by the IREE and the University of NSW, at the University, in February 1970 — nearly 10 years ago. At that time it was mentioned by J. M. Waldron, of the Army Design Establishment, in a paper on interference suppression of military vehicles. The reference stated that it was "somewhat better" than distributed resistance cable, but that it was relatively costly.

When the more recent references appeared the writer was inspired to try to find out more about it and, particularly, whether it was available in Australia. We also wrote to MAS Manufacturing Ltd, requesting any technical information they could supply.

At the same time we approached a number of local cable distributors and manufacturers, in an effort to find a local source, if one existed. In the latter respect the exercise served only to confirm what we feared; no one had even heard of the product, let alone being able to nominate a source!

The only bright spot was that one firm, Beale Prichett Pty Ltd, 2b Northcote St, St Leonards, NSW, showed sufficient interest as to contact their principals in the US and enquire whether such cable was available, and the likely cost structure in Australia.

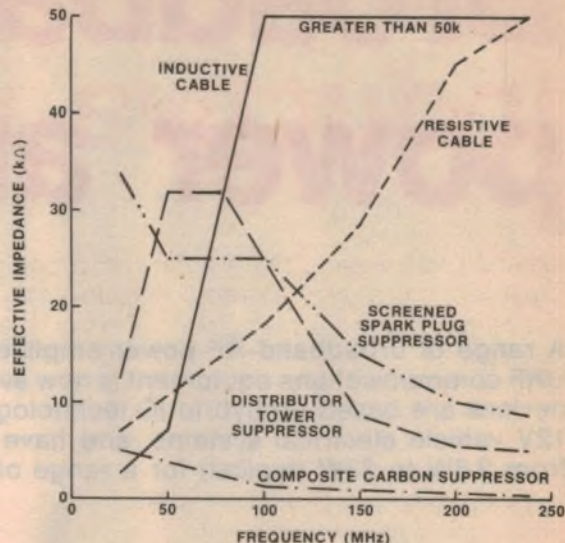
Several months later, at the time of writing, both steps have paid dividends. MAS Manufacturing have replied with some limited, but useful, technical literature, while Beale Prichett have located a source of the cable and are negotiating price structures, order quantities etc. Hopefully, they may find it a proposition to import it.

What is the idea behind inductive ignition cable, what does it consist of, and how good is it?

The idea behind the cable appears to be fairly basic. While resistance in a cable can provide a certain order of suppression, there is a limit to the resistance value beyond which engine performance is likely to be impaired. We cannot go beyond this.

Inductance on the other hand can more easily discriminate between the wanted current, across the plug gap, and the unwanted currents, resulting

This graph gives a good indication as to the effectiveness of the different suppression methods. The inductive cable has by far the best characteristic, with an effective impedance greater than 50k for frequencies above 75MHz.



from it, which occur at a much higher frequency. On this basis suppression should be more effective as the frequency increases, and this seems to be borne out in practice.

A sample of the cable we have seen consists of a central core of very fine fibreglass filaments, impregnated with ferrite, over which is wound a coil of fine resistance wire. (About .09mm or 39B&S.) Over this is the main insulating material, then a layer of fabric braid, and an outer covering of Hyperlon.

The resistance is low, at about 1700 ohms per metre, compared with carbon track leads at between 10,000 and 20,000 ohms per metre, but it still reinforces the inductive effect.

Mechanically, it would appear to be superior to the carbon resistance type cable, which can be damaged by careless handling, and is also less likely to deteriorate with age, as some authorities claim can happen to carbon leads.

How good is it? Unfortunately, we have not had the opportunity to make as many tests as we would like, due mainly to very limited supplies of sample cable available at the moment. Most of our assessment is therefore based on overseas reports.

It appears to be popular in Europe, where it is fitted as standard to many locally manufactured cars. In fact, according to MAS Manufacturing, a total of 27 car manufacturers, world-wide, are using it.

It is generally regarded as being most effective in the VHF band (30 to 300MHz). Indeed, it is considered to be less effective at HF than the conventional resistive cable. Where both VHF and HF suppression are required, it is recommended that additional resistive suppression be added, to bring the resistance up to conventional values.

This limited HF performance may be

responsible for a couple of reports, including the one from the Army Design Establishment, which suggested only a limited improvement. On the other hand, the European car manufacturers appear to have adopted it to meet legislative requirements, in some countries, covering interference to TV signals.

In addition, there was the previously mentioned report from the American amateur who found it the only solution to a particularly stubborn case of interference on the two-metre band, which had defied most of the accepted suppression methods.

Our own tests were made using a few metres of sample cable which Beale Prichett had obtained from the US. They were conducted on a four cylinder Torana fitted with conventional resistive cable, using an Icom 22S 2-metre transceiver.

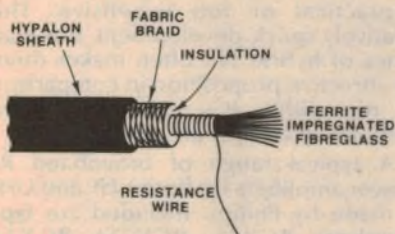
Unfortunately, the tests proved inconclusive. The level of ignition interference was not high anyway, but our reaction was that the new cable gave exactly the same results as the original resistive cable.

We hesitate to condemn the cable on the basis of only one test, particularly in view of the favourable reports from overseas. Beale Prichett are still negotiating with their US principals for more technical information and a more useful amount of sample cable, with which to conduct additional tests.

And that, at the moment, is about all we can tell you. If we have an opportunity to make more tests, and the results are worth reporting, we will certainly do so.

In the meantime we suggest you keep your eyes open for any other references and, particularly, for any local source.

We still think it would be worth trying when all else fails.



Construction of the inductive ignition cable. The core is very much finer and consists of many more strands than can be shown in a simple drawing.

Broadband RF power amplifiers

A range of broadband RF power amplifier modules for VHF and UHF communications equipment is now available from Philips. The devices are based on hybrid IC technology, operate directly from 12V vehicle electrical systems, and have power outputs ranging from 2.5W to 23W (typical) for a range of frequencies.

by GREG SWAIN

Until recently, if you wanted a few watts of RF power you had to employ an RF amplifier based on discrete components. The circuit had to be carefully designed, built and adjusted in order to obtain optimum performance, and special protection circuitry had to be incorporated to protect the circuit against wide variations in load impedance.

This made RF amplifiers quite expensive when compared to other electronic circuits of similar complexity. In addition, they tended to be fairly bulky, a definite drawback where mobile communications equipment is involved.

In recent years, these drawbacks have been largely overcome. Thanks to modern hybrid IC technology, the design engineer can now choose from a range of broadband VHF and UHF

power amplifier modules to suit his particular requirement. These hybrid IC modules have several advantages over their discrete component counterparts including lower cost, more compact size, greater reliability, and reduced assembly and troubleshooting time.

The hybrid IC modules have better performance too. The tuned circuits are etched directly onto a ceramic or PC substrate and are accurately tuned during manufacture. The tuning is effectively locked in — there are no coil slugs to adjust or to drift out of tolerance.

Let's back up a little and find out what a hybrid IC is.

A hybrid integrated circuit is a small encapsulated module containing a substrate of integrated conductors, designed to accept a variety of semiconductor

chips and miniature components. A variety of substrates, encapsulations and pin-formats are possible. The added components can be capacitors, diodes, transistors in SOT packages, MOS and bipolar monolithics in SO packages, or MOS and bipolar naked chips.

The components themselves are automatically positioned and fixed into place during the manufacturing process. Electrical connections to the substrate conductors are made either by reflow soldering or wire bonding, the method depending upon the type of component and the product specification.

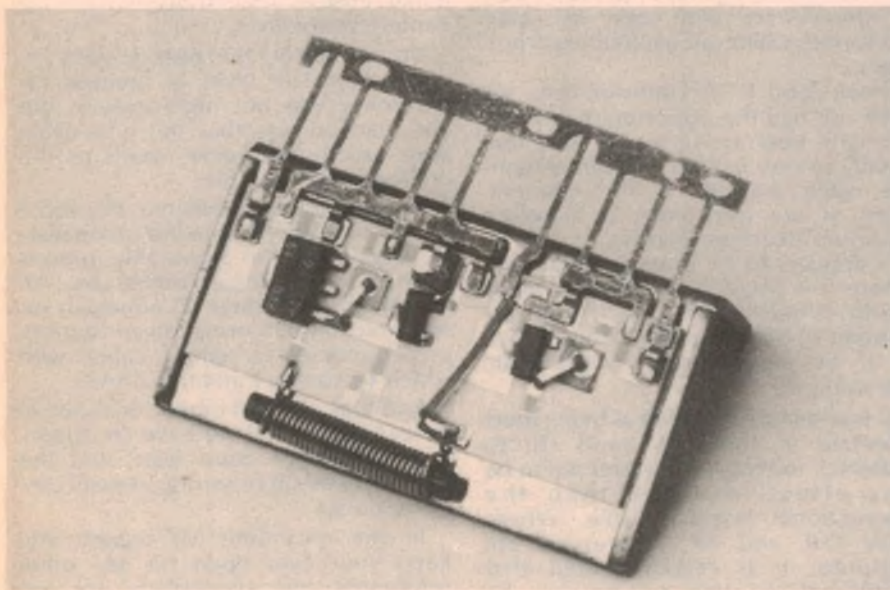
Reflow soldering or parallel-gap soldering is also used to attach the lead-frame to the substrate. The completed IC is then encapsulated in some suitable material, either resin, plastic, metal or ceramic.

A number of technologies are possible in a single package. The speed of bipolar, the low power of MOS and the high impedance of FETs can be brought together, for example. In short, hybrids give the flexibility of discrete components while approaching the small size and reliability of monolithic ICs.

When is a hybrid IC used? The answer is when a discrete component circuit would be too bulky or too unreliable, and a monolithic IC would be impractical or too expensive. The relatively quick development and lead times of hybrid ICs often makes them an attractive proposition in comparison to monolithic ICs, especially when medium quantities are required.

A typical range of broadband RF power amplifiers for both VHF and UHF is made by Philips. Included are type numbers BGY22, BGY22A, BGY23, BGY23A, BGY32, BGY33, BGY35, BGY36, BGY38 and BGY41. The latter is designed for UHF work; the other types are all for VHF.

A range of wide-band VHF/UH



3M337 hybrid IC amplifier module. This three-stage design covers frequencies from 40-860MHz, and is designed for use in MATV systems and as a general purpose VHF/UHF receiving amplifier. Gain is typically around 26dB.

receiving amplifiers using similar hybrid IC technology is also offered. These are usually designated by an "OM" type number and are mainly intended for use in mast-head booster amplifiers and as preamplifiers for MATV systems. Typical type numbers are OM320, OM321, OM322, OM335 and OM337.

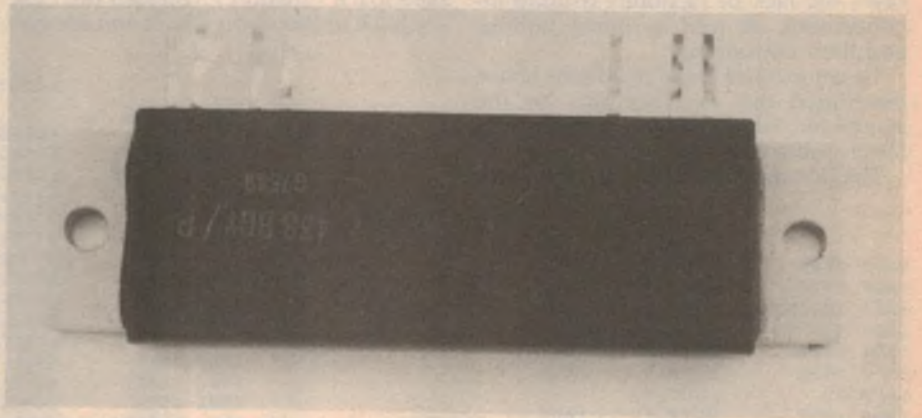
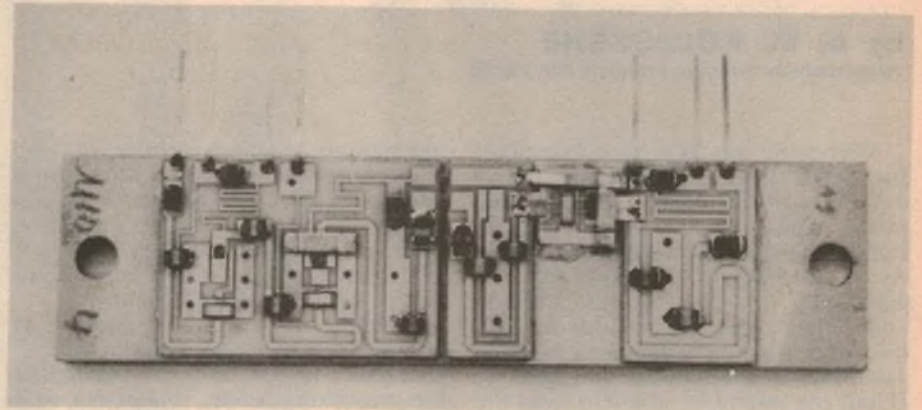
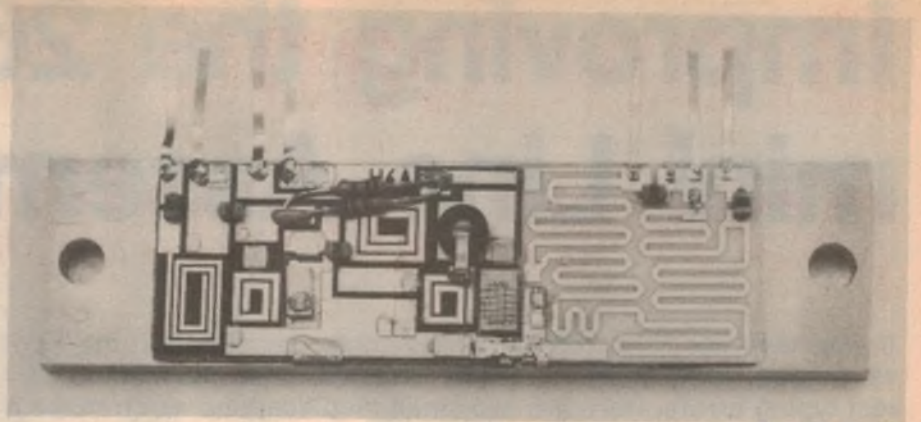
Specifications for the BGY series devices are set out in the accompanying table. All are designed for class C operation and offer typical power outputs ranging from 2.5W up to about 23W. Drive powers are in the range 100-150mW for type numbers BGY32-36. Types BGY22(A) and BGY23(A) are designed for cascaded operation; i.e. the 2.5W output of the BGY22(A) can be coupled directly into the BGY23(A) for an output of 7W.

Physically, the BGY32-36 series and the BGY41 are made up of one or more rectangular substrate modules mounted on a metal flange. This flange measures 68 x 17mm, is about 3.5mm thick, and provides good heatsinking capability and mechanical rigidity. It is made of gold plated copper. A hole is drilled at either end of the flange to allow convenient mounting.

As for the electronics, this consists of a two stage RF amplifier using NPN transistors, together with lumped-element matching components. An interesting point here is that the driver and output transistors are run off separate supply lines. By varying the driver supply voltage, the designer can provide both high and low power capability from the same module.

The completed modules are capable of withstanding load mismatches of up to 50 VSWR for short periods, provided the matched RF output power rating is not exceeded. To ensure good thermal transfer, the module should be mounted onto a heatsink, with heat conducting compound between the module and the heatsink.

So there you have it — a range of rugged RF power amplifiers to suit a variety of design situations. For further information, contact Philips Electronic Components and Materials, 67 Mars Rd, Lane Cove, NSW 2066.



Top and centre: BGY38 VHF and BGY41 UHF power amplifier modules before encapsulation. The photo immediately above shows how the modules look after encapsulation.

Type number	Mode of operation	Frequency MHz	Supply voltage	Drive power (mW)	Load power (W)	Load impedance
BGY22	c.w.	380-512	13.5	50	2.5	50
BGY22A	c.w.	420-480	12.5	50	2.5	50
BGY23	c.w.	380-480	13.5	2.5W	7	50
BGY23A	c.w.	420-480	12.5	2.5W	7	50
BGY32	c.w.	68-88	12.5	100	23	50
BGY33	c.w.	80-108	12.5	100	22	50
BGY35	c.w.	132-156	12.5	150	22	50
BGY36	c.w.	148-174	12.5	150	21	50
BGY38	c.w.	156-163	13.5	250	31	50
BGY41	c.w.	400-512	13.5	150	13	50

Improving the 2650 mini Line Assembler

If you have used the 2650 Mini Assembler described in the April 1979 issue, you'll know it is a little inflexible when you want to correct typing errors. Here are two small modifications which make it very much easier and faster to use.

by **A. M. KOLLOSCH**

Higginbotham Avenue, Armidale NSW 2350

After using the 2650 Mini Assembler for a while, I became a little irritated by its lack of any facility to let you correct minor typing errors as soon as you notice them, before the end of the line. As you'll know if you've used the assembler, you have to finish the line and either reset the original to step back and re-type the line (assuming the assembler doesn't throw you out), or restart the assembler and also reset the origin (if it has thrown you out). In both cases the lack of flexibility is quite inconvenient, as well as being tedious and time consuming.

To get around these problems I have developed two modifications for the assembler, which make it considerably faster and more convenient to use.

The first modification is to the line in-

put routine. Its effect is to let you step back along the line input buffer, using "delete" (rubout) characters. So if you spot a typing error before you have finished a line, you can step back to it and then type the rest of the line again before typing a carriage return.


Actually the modified routine is arranged to echo "backspace" characters to the terminal, instead of the incoming "delete" characters, so if your terminal can perform the backspace function it will step the cursor back to show you where you are go-

ing. With terminals which don't perform backspacing you'll have to count back yourself, but this is usually no problem.

A disassembler listing of the modified input routine is shown below. It is one byte longer than the existing routine, ending at X'1AFF instead of 1AFE.

The second modification is a little more elaborate. It involves an additional error handling routine, a modified starting sequence and a couple of subroutines, together with changes to all the error throwout addresses.

The idea of this modification is that instead of throwing you right back to PIPBUG when it finds an error, the assembler now prints a curt "? ERROR" message, and reprints the address of the line concerned so you can re-type it correctly.

The disassembler listing for this modification is also shown below. I think you'll find it worthwhile. 

```

*MODIFIED LINE INPUT ROUTINE
1ACD 0700      LODI,R3      00
1ACF E73C      COMI,R3      3C
1AD1 1C15B0    BCTA,Z       15F0
1AD4 3F0236    BSTA,UN      0236
1AD7 E47F      COMI,R0      7F
1AD9 9303      BCFR,Z       1AE6
1ADB 03        LODZ,R3
1ADC 1871      BCTR,Z       1ACF
1ADE 0438      LODI,R0      03      MOD BEGINS HERE
1AE0 B3A0      ZBSR         *0022    PRINT BACKSPACE
1AE2 A701      SUBI,R3      01      DECREMENT BUFF PTR
1AE4 1B69      BCTR,UN      1ACF    & LOOP BACK
1AE6 0503      LODI,R1      03
1AE8 ED7AC9    COMA,R1      1AC9#
1AEB 1809      BCTR,Z       1AF6
1AED F979      BDRR,P       1AE3
1AEF CF7A02    STRA,R3      1A32#
1AF2 BBA0      ZBSR         *0020
1AF4 DB59      EIRR,UN      1ACF
1AF6 CF0429    STRA,R3      0429
1AF9 CD042A    STRA,R1      042A
1AFC 0700      LODI,R3      00
1AFE 9BA5      ZBRR         *0025
  
```

ABOVE: A disassembler listing of the modified line input routine, which lets you step back to correct typing errors.

RIGHT: A similar listing of the modifications to allow you to re-type lines that are thrown out by the assembler. It now types "?ERROR", and repeats the address.

```

159E 00 00
15A0 0D040D
15A3 0E040E
15A6 C976
15A8 CA75
15AA 17
15AB 0971
15AD 0A70
15AF 17
15B0 75FF
15B2 740F
15B4 0503
15B6 0D75C3
15B9 BBA0
15BB F979
15BD BBA5
15BF 3B6A
15C1 1F160C
15C4 524F52
15C7 524520
15CA 203F
160C 3BF0
160E 3F15A0
1611 3BDC
1613 02
1614 C1
1615 3BD8
1617 042E
1619 3F02B4
161C 3BD3
*MODIFICATION FOR IMPROVED ERROR HANDLING
*LOAD & STORE SUBR
LODA,R1 040D
LODA,R2 040E
STRR,R1 159E
STRR,R2 159F
RETC,UN
*LOAD ADDR SUBR
LODR,R1 159E
LODR,R2 159F
RETC,UN
*NEW ERROR HANDLING ROUTINE
CPSL FF
CPSU 0F
LODI,R1 03
LODA,R1 15C3#
ZBSR *0020
BDRR,P 15B6
ZBSR *0025
BSTR,UN 15AB
BCTA,UN 160C
*ERROR MESSAGE
ROR
RE
?
*MODIFIED START SEQUENCE
BSTR,UN *15FE
BSTA,UN 15A0 GO TO NEW SUBR
BSTR,UN *15EF
LODZ,R2
STRZ,R1
BSTR,UN *15EF
LODI,R0 2E
BSTA,UN 02B4
BSTR,UN *15F1
  
```

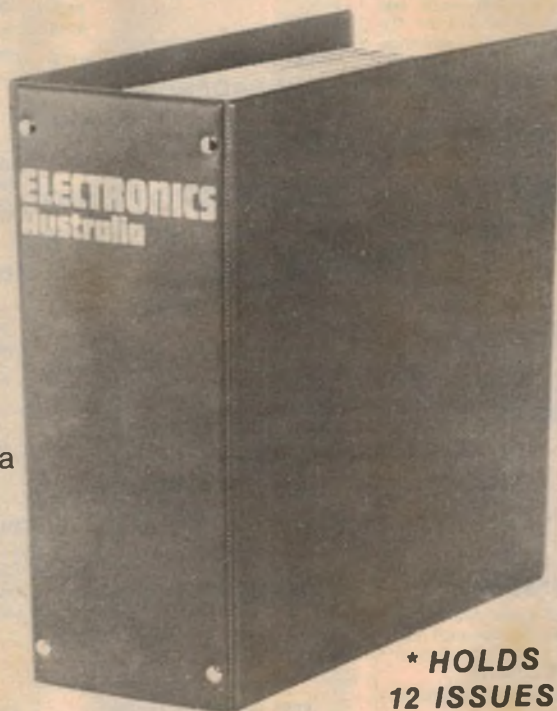
MODIFY THE ERROR THROWOUT ADDRESS TO X'15B0 AT THE FOLLOWING LOCATIONS:

```

162F-30 16BA-EB 1704-05 1745--46
17B0-B1 1A93-94 1AD2-D3
  
```


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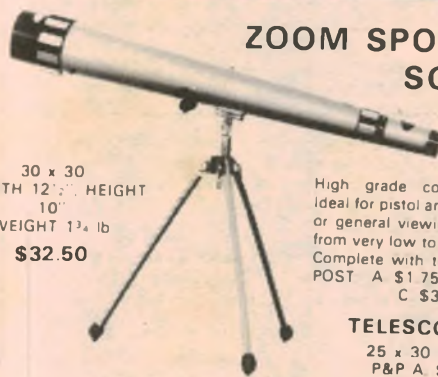
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don't exactly know what this does technically as I am only an amateur. I found out only by accident about this because without it I have no control over it and it goes haywire (LEDs flickering here there and everywhere). I have no IR filter on the unit yet, maybe that would make a difference. This filter is very hard to obtain in Melbourne.

As regards to the remote control, an employee of Dick Smith's in Melbourne told me that a friend of his said that the photodiode (BPW34) is in fact not a diode but a photovoltaic cell. Apparently this chap is into this sort of thing and also says that by using this (photocell) the best you can hope for is a range of about 1m because IR has very little effect on it. Could you please advise me. (F.S., Boronia Vic.).

● Starting with point (b) we find it difficult to believe it worked at all with the 100k resistors mentioned removed. The 100k resistors are simply in series with the RCA inputs; if they were removed there would be no output. We can only suggest that you may have the unit incorrectly connected to your stereo.

As far as points (a) and (c) are concerned, they are related. The low range is a direct result of the 50k trimpot which you inserted in the circuit. This also has the effect of reducing the gain of the receiver, not to mention altering the bandwidth.

The flickering of the LEDs is to be expected if an infra-red filter is not used; in fact the filter is extremely important for proper operation. If you cannot obtain the filter material from a photographic store then we suggest that you replace the BPW34 with a BP104 which has an integral infra red filter, as mentioned in the original article.

Finally the information you were given about the BPW34 not being a photodiode, and that it is insensitive to infra-red is incorrect. It most certainly is a photodiode and one that is specifically intended for infra-red applications — it has a peak spectral response of 850nm which is well into the infra-red region of the spectrum.

LF & VLF RECEPTION: Some time ago I built the LF and VLF Converter (March 1976, File No 3/CV/3). With a 15m wire antenna, I fed the converter into my Drake SSR-1 receiver and I received a number of LF stations, both local and interstate with reasonable clarity. However, during evening reception was generally unsatisfactory because of noise and interference from local MF stations. I decided to try the RF Preselector (April 1979, File No 2/SW/76) by adapting it to the LF band.

Instead of the ferrite rod antenna I used a coil consisting of 230T of 30B&S enamel wire close wound on a former made from a 100mm length of 50mm OD PVC electrical conduit. An antenna

primary winding of 45T was wound over the earthy end of the large winding, with a strip of paper insulating the two windings. The input winding for the gate of the FET is 30T spaced about 5mm from the other windings. Tuned with a 415pF variable capacitor, the main winding covered about 200-400kHz. The 30pF trimmer was deleted and a low pass filter consisting of a 2.5mH RF choke and a .0015uF capacitor was placed between the antenna and the coil winding.

The RF preselector, the LF converter and the receiver were coupled together with 50 ohm coaxial cable. With this set up and using the same wire antenna as before, many LF stations, local and interstate were received satisfactorily.

Using the LF converter down to the VLF band, I have been able to tune NWC (North West Cape) on 22.3kHz, the Naval station in Canberra on 44kHz and NAA (Cutler, Maine, USA) on 17.8kHz. In the future I intend to experiment further with the RF preselector for use on this band as well. (A.A. Lindisfarne, Tas).

● Thank you for your interesting letter A.A. As you can see, we have had to reduce the length of your letter but we have given enough information so that

answers, undertake special research or discuss design changes.

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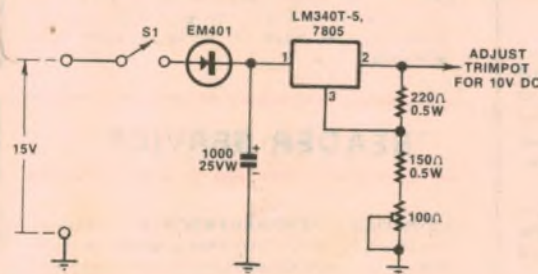
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For those readers who have been unable to obtain a 10V regulator for the Sound Effects Synthesizer described in September 1979, we suggest this modified circuit which uses a 5V regulator instead. Note that it will be necessary to cut the PCB pattern.

interested readers could duplicate your arrangement. Incidentally, there are a number of other VLF stations which you should be able to receive. In addition to the American VLF stations, NWC and NAA, they have several others. Try listening on 17.4kHz, 18.6kHz, 21.4kHz, 23.4kHz and 24.0kHz, as well as GBR in Rugby, England, on 16.0kHz. Oh yes, there is Omega too!

ELECTRONIC BONGOS: Back in 1970 I made a suggestion regarding the bongos published in the April, 1970 issue. This suggestion was the fitting of a third plate between the two existing touch plates so as to eliminate the need for a separate hand-held wire.

The same set-up can be used again with the bongos published in the Dec. '79 issue.

The etched PCB could be divided into three separate plates with the centre plate connected to the +9V line. In use, two or more fingers are made to bridge the gap between the centre and either of the two outer plates using skin resistance. (K. Y. Nunawading, Vic.).

● This idea was tried when the bongos were first designed but was considered to be impractical since we found hand movement is restricted. We leave it up to the reader to decide.



INFORMATION CENTRE

DREAM 6800: Since your articles on the "Dream 6800" I have built the power supply from details published in the June 1979 issue. I have found that 470-ohm resistor and LED overheated and blew up the 12V 100mA regulator. I solved this problem by replacing the regulator with a 1-amp type and removing the LED from the circuit.

This solved the regulator problem but I feel that the power supply is now unsafe due to the lack of a power on indicator. Could you supply any information that would help me to overcome this problem. Also, thank you for the Dream 6800 series, and I hope that more software will be printed in future issues. (D.H. Nth Caulfield, Vic.)

● Your problem with the regulator is one that could be expected if you are using a 100mA type. The specified worst case current drawn from this regulator is stated as being 100mA, and this is not allowing for the 22.6mA drawn by the LED. Now that you have replaced this with a 1-amp type we suggest that you

try replacing the LED in to the circuit. You should not experience any further problems due to the larger current handling capability of the new regulator.

As for your question regarding further software for the Dream, we do have plans to publish more during 1980.

CAR ALARM PROBLEMS: I constructed the Car Burglar Alarm as published in the April 1979 issue. I have spent quite some time checking the alarm but am unable to get it to work. I have had quite a problem in trying to obtain the BC148B and BC212B transistors and have had to accept what are claimed to be alternative part numbers. I have substituted a BC549 for the BC148B and a BC557 for the BC212B. Are these substitutions suitable?

In your parts list you specify a 1N4001 diode but this is shown as a 1N4006 diode in the circuit diagram. On page 47 you refer to the 0.05uF capacitor and this is shown to be 0.047 in the circuit.

Which is the right value? Have there been any errata published to the article? If not I would be pleased if you could give me some answers to these questions. There is also the question of transistor lead orientation. I cannot make out your drawings. Can you please advise? (J.H.T. Bilunga, Qld).

● The problem regarding the availability of the specified transistors should not pose a problem as the BC549 will substitute for the BC148B, and the BC557 will substitute for the BC212B. As far as the diodes are concerned, almost any general purpose rectifier diode will do the job, and both the 1N4001 and the 4006 are suitable.

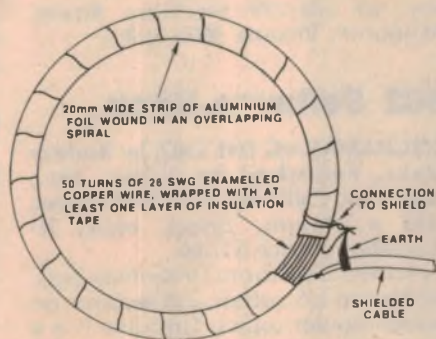
In the case of the capacitor, the difference between .05uF and .047uF can be considered negligible when tolerances are taken into account. The diagrams of the transistors are shown with the leads facing up. In the case of the UJT you will find that there is a small tag on the case body. The lead nearest to this tag is B2. We hope that this clears up any problems that you have experienced.

METAL LOCATOR: I have been interested in your article on the "Prospector" metal locator in the November edition of your magazine. However, since I am not too conversant in the art of coil winding I find it difficult to wind same. Would it be critical for instance to wind the coil in layers, or should it consist of one single winding only? It would be very much appreciated if you could enlighten me on the above. (W.B., Caloundra, Qld).

● Your letter is typical of many we have received, either enquiring about construction of the coil or the Faraday screen. In an attempt to clear up any confusion about these problems we will try to expand on the description given in the original article.

The Faraday screen is made up from a long strip of aluminium of about 20mm width. Starting from one end of the coil near where the two coil leads come out, wrap the foil tightly around the coil with the foil edges overlapping to ensure the whole coil is covered. When you get back to the beginning, make sure there is a gap of no more than about 10mm between the two ends so that the foil does not form a shorted turn.

The screen has to be connected to



earth as shown on the circuit diagram. This is accomplished by connecting to the earth side of the shielded cable which connects the search coil. To facilitate connection to the aluminium foil we recommend that a few turns of copper wire be wrapped around one end of the foil as shown in the diagram. It should be emphasised that the coil and Faraday screen should be tightly constructed and fixed rigidly to the base of the locator. Naturally even slight deformations of the coil or screen will change the capacitance or inductance of the coil with a consequent change in the pitch.

Note also that the number of turns and gauge of wire used in the search coil is not critical.

SQUELCH: I recently built a converter to receive the 108-136MHz aircraft band. The converter is fed into my FRG-7 communications receiver. It works very well but there is a problem with an excessive amount of hiss in between stations. What I need is a simple squelch arrangement to fit to my receiver. Could you please supply me with a circuit for a suitable squelch. (H.D. West Ulverstone, Tas.)

● We understand the problem which you have H.D. but we regret that we have not described a circuit which would help. In the meantime, perhaps it would be a good idea to keep the volume control on the receiver set well back when no signals are being received. The volume could be increased when a signal is tuned in.

REMOTE CONTROL: I recently built the remote control for a hifi that you published and have some problems with it. (a) I only have a range of approximately 2 metres, (b) my unit (stereo) will only operate if I remove the 100k resistors that form the voltage dividers on IC7&8, otherwise I get no sound from the speakers. Also (c) I placed a 50k trimpot across the 470pF capacitor for some sort of adjustment. I

Books & Literature

devices in the home. Other chapters cover non-transmitter interference sources, noise in vehicular installation, and problems arising from the operation of CB transceivers.

The author's approach is logical and systematic and he suggests most of the standard things that one tries in trying to cure interference. It is not his fault that line filters only help sometimes, or that domestic light dimmers can rarely be silenced completely.

A couple of points puzzled me: page 5, his definition of cross modulation; page 43 diagrams that show the null of a DF loop in line with its edges. Also, somewhat unfortunately, much of the material in the appendices is more appropriate to the USA than to Australia. However, if interference is driving you round the bend, Larry Kahaner may just happen to have the answer.

Our review copy came from Butterworths, 586 Pacific Highway Chatswood, NSW 2067. (W.N.W.)

Digital Electronics

BEGINNERS GUIDE TO DIGITAL TECHNIQUES, by G. T. Rubaroe. Bernard Babani (publishing) Ltd, London, 1979. Soft covers, 108 x 181mm, 62pp, with illustrations.

As a book supposedly written for the beginner, I feel that this one leaves a lot to be desired. In the opening chapter the author makes no reference to the basic concepts of digital electronics, but starts off with analog to digital conversion, hardly the right starting point.

In the chapters that follow, the author discusses number systems, codes, combinational logic, A-to-D converter circuits, and finally touches on the subject of digital computers. The level at which the text is written makes the assumption that the reader has at least a basic familiarity with the subject, although the title of the book suggests otherwise.

In short, the beginner that wishes to learn more about the subject of digital electronics is advised to look elsewhere for more instructive material as this book does not fall into the category of recommended reading.

The review copy came direct from the publisher. (G.C.)

Building a Computer

HOW TO BUILD A MICRO-COMPUTER, by Sam Creason K6EW. Published by 73 Inc., Peterborough, New Hampshire 1979. Soft covers, 218 x 282mm, 112pp, many illustrations. Price \$13.30.

The full title of this book is "How to

Build a Microcomputer . . . and Really Understand It". Although it may sound unduly harsh, I must comment that to my mind it neither gives an adequate description of the construction of a microcomputer, nor gives sufficient information for even a rough understanding of its operation.

From what one can glean from the book, the microcomputer design developed by the author was fairly appropriate as a small teaching system. It does seem a little clumsy, using a "do-it-yourself ROM" with lots of plug-in diode modules to provide a "monitor" program, but this is perhaps acceptable in a system for this type of application.

The real shortcoming is in terms of the book itself. There just isn't anywhere near enough information given, either for the construction of the microcomputer or for understanding its operation. In fact, some of the chapters are so brief and superficial that they scarcely scratch the surface — for example the chapter introducing microprocessor systems consists of ONE page of text, spread over two pages! Similarly the chapter on the microcomputer's processor board has slightly over two pages of text, and doesn't even give a block diagram of the registers inside the 6502.

In short, very disappointing indeed.

The review copy came from Technical Book and Magazine Company, of 289-299 Swanston Street, Melbourne, Victoria 3000. (J.R.)

6502 Software Book

PROGRAMMING THE 6502, by Rodney Zaks. Published by Sybex, Inc., Berkeley, California 1978. Soft covers, 138 x 216mm, 305pp, many illustrations. Price \$17.60.

A further book from Dr Rodney Zaks, well known US author and lecturer on microcomputer topics. This time it is a text on programming, with particular emphasis on the 6502 processor. And as we have come to expect from Zaks, it is well planned and executed.

There are a number of chapters offering basic introductory material on programming in general: basic concepts and programming techniques, addressing techniques, data structures and generalised program development. These are augmented with chapters treating the specifics of the 6502 processor and its programming: its hardware organisation, its instruction set, its addressing modes, input-output techniques, system configurations and so on. And there are also a good many explanatory examples, together with tutorial exercises.

The text is clearly and concisely written, although a little on the dry

side; it even borders on the pedantic at times. But the subject material is smoothly graded, and should be found both readable and helpful.

In short, a worthwhile text on 6502 programming, although at \$17.60 it is not cheap.

The review copy came from McGills Authorised Newsagency, of 187-193 Elizabeth Street, Melbourne 3000. (J.R.)

Computer Game

SCELBI'S 8080 GALAXY GAME, by Raymond Edwards. Published by Scelbi Computer Consulting, Inc, Milford, Connecticut 1978. Soft covers, 210 x 280mm, approx 8mm thick, some illustrations. Price \$13.50.

This is not so much a book but a comprehensive document on a space-war type game written in 8080 assembly language and suitable for running on most 8080-based microcomputer systems. It is apparently a revised version of an earlier program created by Robert Findley.

The documentation is quite thorough. It covers the rationale and operation of the game, system requirements, memory usage, input/output requirements, data tables, messages and subroutines and a sample of the game in operation. Also given are a full commented source listing and a machine code dump in octal. In short, just about everything you would need in order to get the game going on any suitable system. It's quite well written, too.

The review copy came from McGill's Authorised Newsagency, 187-193 Elizabeth Street, Melbourne, Victoria 3000. (J.R.)

BASIC Programming

COMPUTER PROGRAMMING IN BASIC, by Peter Bishop. Published by Thomas Nelson and Sons Ltd, Sunbury-on-Thames, Middlesex, 1978. Soft covers, 190 x 245mm, 140pp, many diagrams. Recommended retail price \$8.95.

An introduction to programming in BASIC, intended not so much for the newcomer to personal computing but rather for the student or school pupil doing a course in computer studies. As such it presents the material in a pedagogic fashion rather than an entertaining one, and would not fare well in comparison with books like Dr Lien's TRS 80 Level 1 User's Manual.

Still, it is a methodical and businesslike book, with many tutorial examples for the serious student. It could therefore make worthwhile supplementary study material.

The review copy came from the Australian office of the publisher, who advise that the book is currently available from Thorburn's Technical Bookshop, 114 Castlereagh Street, Sydney. (J.R.)

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ARRL on Antennas

THE ARRL ANTENNA ANTHOLOGY. Edited by Marian S. Anderson, WB1FSB. Stiff paper covers, 151 pages 275mm x 207mm, freely illustrated by photographs and diagrams. Published 1978 by the ARRL, Newington, USA. Price in Australia \$6.75.

By way of clarification, this book is subtitled "The best of recent QST HF antenna articles and theory presentations". Perhaps we should add the further remark that it has been compiled primarily for the amateur who is not blessed with acres of space and unlimited funds; it's very much for the amateur who has to do it himself.

The first section on vertical HF antennas includes a dozen or more designs, supplemented by interspersed material to do with feeding, matching, etc.

A second, somewhat shorter section deals with about a half-dozen mainly compact beams and this leads naturally into section 3 dealing with quad arrays of one kind and another.

Section 4 contains a number of odd but interesting antennas, such as a loop, delta loop, half-square, DDDR and installations for caravans.

The book is rounded off by section 5, comprising about 40 pages of assorted articles on comparative gain, matching, instrumentation, etc.

If you're one of the many amateurs who don't quite know what to do about installing an antenna at your place, this anthology may provide just the idea you've been looking for.

Our review copy came from Technical Book and Magazine Co, 289-299 Swanston St, Melbourne 3000. (W.N.W.)

RF Interference

AUDIO AND VIDEO INTERFERENCE CURES, by Larry Kahaner. Stiff paper covers, 114 pages, 209mm x 135mm, illustrated by drawings and circuits. Published 1979 by Hayden Book Co Inc, New Jersey, USA, Price in Australia \$7.50.

In this new book, Larry Kahaner has made a valiant effort to solve a problem that, in many cases, defies solution. At least, the reader is encouraged to "have a go" and, in some cases it may help.

In chapter 1, the author talks about transmitters and the ways in which they can cause interference. Chapter 2 deals with TV interference of various kinds, and chapter 3 with hifi and audio

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Books & Literature

Our review copy came from Thomas C. Lothian Pty Ltd, 4-12 Tattersall's Lane, Melbourne, Victoria 3000. Copies are now available and should be obtainable from technical booksellers. (I.L.P.)

HiFi Speakers

HOW TO SELECT AND INSTALL YOUR OWN SPEAKERS by Norman Crowhurst. Stiff paper covers, 234 pages, 208mm x 130mm, freely illustrated. Published 1979 by TAB Books, USA. Price in Australia \$7.50.

From the title, I rather expected a down-to-earth discussion: needs which have to be met — typical speakers to meet those needs — how to choose — how to install.

In fact, the secondary title "Everything you need to know about speakers" would have been more to the point. Norman Crowhurst covers a lot of ground from domestic hi-fi to indoor public address, but its a meandering mix of practice and theory; of past and present.

Some of it gives evidence of perceptive thought; some of it seems vague, even suspect. For example, buried in a lot of talk about reflex enclosures, etc, is a section about "Designing Your Own". It boils down to copying any suitable commercial design and fiddling until you get it right. That would be turning the clock back a decade or more, to when we didn't know any better!

If you want to browse and pick up a lot of general knowledge about speakers, fair enough. But if you want down-to-earth guidance for a minimum of reading time, I suggest you look for a text which is better organised for the purpose.

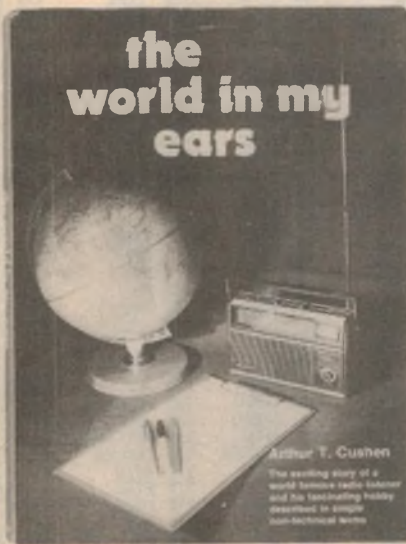
Our review copy came from Technical Book & Magazine Company, 289 Swanston St, Melbourne, 3000. (W.N.W.)

Audio Projects

ELECTRONIC PROJECTS IN AUDIO by R.A. Penfold. Published 1979 by Newnes Technical Books. Stiff paper covers, 88 pages 215mm x 135mm, illustrated with diagrams and photographs. Price in Australia \$6.00.

First impression of this is a nicely presented small book, with good printing, good paper, and the use of pickout colour to add visual interest and to highlight circuit details. Inspection and sample reading confirms that the material has also been carefully prepared and it should be of interest to anyone who likes to build up and use simple audio gear.

It details 15 projects as follows: Rumble filter, scratch filter, dynamic mic preamp, magnetic cartridge preamp, crystal mic preamp, dynamic noise limiter, miniature power amp, quasi-quad adapter, 3/6 channel mixer, slave amp, audio limiter, stereo peak level in-



THE WORLD IN MY EARS by Arthur T. Cushen. Hard covers, 204 pages 212mm x 156mm, freely illustrated. Published 1979 by the Author at 212 Earn St, Invercargill, NZ. Price in Australia \$15.95.

Readers of this journal will need no introduction to Arthur Cushen, who conducts our monthly feature "Shortwave Scene". This reviewer has visited Arthur and his wife Ralda in their home and been profoundly impressed by the way in which he has overcome blindness and turned a one-time hobby into a profession.

The first part of the book is personal, and amongst other things, tells how he became deeply involved in short wave listening during World War II, recording prisoner-of-war messages, and following propaganda and news broadcasts from enemy stations. So through to the present.

From page 67 onwards, the Author seeks to introduce the reader to shortwave radio listening with an explanation of what it is all about: receivers, antennas, frequencies, times, conditions and so on. It is all readily readable and avoids off-putting technicalities.

The book can be recommended especially to those who may want to get into DX and shortwave listening, or to old-timers who would like to re-live

past experiences. Congratulations, Arthur!

The review copy came direct from the Author/Publisher. Copies can be obtained in hard cover form from the Author/Publisher, or in both hard and soft cover from McGill's Newsagency in Melbourne. (W.N.W.)

Shortwave DX Guide

WORLD DX GUIDE, First Edition, arranged and compiled by Jim Vastenhoude. Published by Billboard Ltd under licence from the Billboard Group. Soft covers, 208 pages 146mm x 228mm, illustrated by diagrams, tables and photographs. Recommended Australian retail price \$17.95.

According to the Introduction by Jim Vastenhoude, this book is a compilation of selected articles from previous editions of the "World Radio TV Handbook" and supplemented by several articles written by Jim Vastenhoude. As such, the contents are a mixture of new material and some which has been published before.

The text seems to be pitched mainly towards the beginner in the art of DX listening, along with TV DX viewing, although there is a considerable amount of material which would be of value to the more experienced enthusiast. The book consists of 28 fairly short chapters, the headings of which are too numerous to list here. The text is divided into four sections.

The Section headings are: (1) Getting on your way, (2) Getting ahead further, (3) Some backgrounds, (4) References. Suffice to say that the various sections cover most aspects of shortwave listening, including propagation, sunspots, jamming, SSB reception, MW DXing, etc. The reference section gives information on such items as azimuthal maps, world time charts, standard frequency and time signal stations and other useful information.

While I am of the opinion that this book would be very useful to all interested in the fascinating subject of DXing, at the price I do not consider it good value for money. It would be a good idea to have a look before you buy.

New Products

Drafting aids for PC artwork



Bishop Graphics of the USA has recently released a range of printed circuit drafting aids onto the hobby market. The range of products is very extensive and covers almost every imaginable item required to produce good quality artwork.

Pictured are the catalog, some sample packs of cut shapes and slit tapes, alphabetical designators and a magnifying glass for checking both artworks and completed PCBs.

One other essential tool for the successful production of a quality artwork is a good sharp knife. Bishop also supplies the range of "X-Acto" knives together with a wide range of replacement blades.

The drafting tapes are made from black opaque crepe which is self adhesive, making application a simple task. Other standard items include a range of donut pads of varying internal and external diameters, targets for photographic registration, 90-degree bends, T-junctions and universal curves.



Since these tapes and pre-cut shapes are the same as those used in the preparation of professional artworks, it is possible for the hobbyist to achieve a professional result.

Hints and application notes for the various products are provided as an integral part of the catalog.

Bishop Graphics products are available from the following retail outlets: Radio Despatch Service, Sydney; Ellistronics, Melbourne; and Zero-One Electronics, Brisbane.

For further information contact the importers and distributors: Circuit Components, 383 Forest Road, Bexley, NSW 2207. Phone: 59 6550.

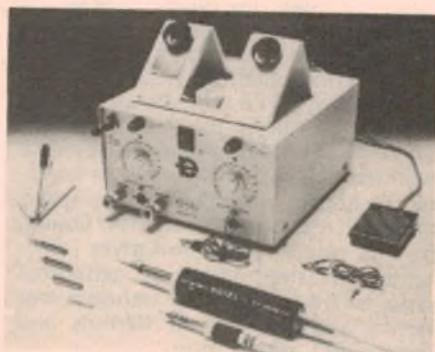
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79PG9	3.00	79MD9	2.80	79PS11	2.00
ET573	2.80	ET577	2.80	ET606	3.00
79QM9	3.00	79PS10	2.80	ET473	3.50
79RR8	4.20	79SF10	2.50	79R18	2.80
79BT9	2.60	79TT7	2.60	79AL9abc	4.20
79AC9	3.50	79SF9	2.60	79W9	2.80
ET576	4.20	ET574	2.80	ET731	3.00
ET730	3.50	ET814	2.80	ET575	2.20
ET252	3.00	79SR8	2.80	ET725	3.50
79WF8	3.20	79UT8	3.00	79TRF5	2.50
79PS6	2.80	79FR6	3.50	79M8	2.80
ET451	2.50	ET472	3.00	ET148	2.50
6,800	8.50	79CL7	4.80	ET724	2.20
79UPS6	2.50	79SA5	8.00	79K87	2.80
ET144	3.50	ET254	2.50	ET651	4.50
79R05	3.00	79EQ2C	2.50	ET471	5.00
77EQ2A	3.50	ET249	—	79EQ2B	4.50
		ET249	—	ET594	2.50
ET320	2.20	ET253	—	ET470	3.20
ET595	2.80	7905	—	79A3	3.00
491	4.50	559	3.80	721	3.00
79PS3	2.60	78SE3	4.00	79PB2	3.20
79P1B	2.80	79P1A	2.80	78C1B	2.80
79C1A	3.00	558	2.50	557	3.00
142B	4.00	142A	8.00	79UP1	5.00
79S1	4.50	78W3	2.60	79CL1	2.60
791T2	5.00	78SB12	3.00	78S12B	2.20
78S12A	5.50	781M12	3.00	78UP10	7.00
78N10	2.60	78C11	3.10	78DT10D	2.00
78DT10C	2.50	78DT10B	2.80	78DT10A	6.50
ET813	3.50	ET143	3.20	ET141	4.20
ET812	2.80	ET593	3.20	ET490	2.80
ET556	6.00	78DB11	2.80	78UP9	6.00
78BB9	3.50	555	4.00	650C	2.60
650B	2.60	650A	4.00	138	3.80
718	2.60	553	3.00	811	3.30
590B	8.00	590A	8.00	78MC10	4.00
78E09	2.50	ET605	7.00	ET391B	2.50
ET391A	2.50	ET551	3.00	ET641	ON AP
ET591C	2.20	ET550	2.80	ET592	4.50
78UT9	16.00	78MX9	3.30	78T9	2.30
78UM8	2.60	78CL8	3.00	ET630B	3.00
ET630A	4.00	ET248	2.30	ET318	7.00
ET591	4.00	ET810	2.80	78TM8	2.80
78TSC7	2.50	78PT7	2.50	78VBG7	3.50
ET137B	2.80	ET137A	3.50	ET139	2.50
ET717	3.50	ET587	7.00	ET640	16.50
78FB8	3.50	78M	2.80	78A06	2.80
246	4.00	489B	2.50	489A	2.80
78CD4	2.60	78PS5	2.50	78C5	3.20
78UP5	5.00	ET140D	4.00	ET140A	14.00
ET140P	5.50	ET136	2.50	ET487B	7.50
ET487A	7.50	ET588 20	10.00	78NG4	3.00
78UT4	4.00	78EK3	3.30	78T3	3.60
78B2	3.00	781A2	2.60	ET450B	2.60
ET450A	2.80	ET716	4.00	ET715	3.00
ET486	3.20	ET245	2.50	78C2	3.00
78AF2	3.00	78S3	2.60	78CF1	2.80
77CB12	2.60	77PH12	2.60	77PM12	3.50
ET135	3.00	ET586	2.80	77MX11	2.50
77SC11	3.80	77PS11	2.50	77UPA	3.00
77MX11	2.50			77PS11	2.50
ET604	2.50	ET585T R	3.00	ET635	2.80
ET713	3.00	ASC11	2.80	77UP11	6.50
77TS9	3.00	ET603	3.00	ET593	2.50
ET134	2.60	77AL8	2.50	77T10	2.50
77DVM9	2.80	ET065			4.20
ET067	2.20	ET063	2.50	ET083	2.20
ET072	2.50	ET085	2.00	ET084	2.50
ET485	2.80	ET484	3.00	ET581	2.50

ALL SILICON 30/60w PA PORT AMP
6 1/2" W x 8 1/2" D x 3 1/4" H 12 — 16V two inputs 5 & 100mV 125, 250, 500 ohm output only No 763A
\$70 ea. 240V operation \$33 extra. Freight collect.
COILS and IF's All \$2.50 ea plus post 60c
3/4" W x 3/4" D x 2" H

MAIL cheque or money order
(add postage) direct to —

RCS radio pty ltd
651 FOREST RD BEXLEY
NSW 2207 587 3491

SPECIAL PURCHASES

NEW B.S.R. RECORD CHANGERS-PLAYERS



MODEL C197
\$47.50

This is a new model just released and is fitted with a ceramic cartridge & diamond stylus. Auto or manual operation. Three speed 33, 45 & 78rpm. Cueing control and bias compensation. Changer & player spindles supplied. 11" turntable. Post & packing extra. NSW \$2.75 Vic. Qld \$3.75 WA NT & Tas \$4.75

SPEAKER GRILLE FABRIC AT 1/2 PRICE

AVAILABLE IN BLACK, BLACK WITH GOLD FLECK, LIGHT & MID BROWNS. WIDTH 54"

\$4.80 Per YARD. Post & Pack \$1.75.

Send two 20c stamps for samples.

GARRARD CC10A RECORD CHANGER

\$15.75

Fitted with a Sonatone Garrard Ceramic Cartridge Sapphire Stylus supplied with template & instructions. Posts & Packing: NSW \$2.50. Inter. \$3.50.

MODEL C142R

HI-FI UNIT WITH ADC MAGNETIC CART & DIAMOND STYLES

\$55.00



A precision automatic and manual record-playing unit fitted with 4 pole motor to provide constant speed conditions for the 11 1/2 inch turntable. The low resonance tubular pickup arm is counter-balanced with a resiliently mounted weight to permit light sensitive tracking, and the slide-in cartridge carrier enables styles inspection and the interchange of replacement of cartridges to be carried out simply and quickly. Fine stylus force adjustment and bias compensation are both calibrated for accurately setting the arm to given optimum playing conditions for the chosen cartridge.

The fluid-damped level type cue and pause control ensures gentle lowering of the pickup to the surface of the record. A short spindle is supplied for single record play records. Precision engineering is reflected in the styling of the 142R which is elegantly finished in black and silver.

POST AND PACKING EXTRA
NSW \$3.75
Tas WA & NT \$7.00

Vic. SA & Qld \$5.75
(Reg post \$2.00 extra)

NEW RANK-ARENA F.M.-A.M. TUNER AMPLIFIER

MODEL RA402. Output 24 watts RMS (12+12). Response 50HZ to 50KHZ. Mag or ceramic inputs. High & low filters. Loudness control. Provision for 4 speakers.

Freight Extra
\$147.00

NEW AWA HI-FI SPEAKER KITS 8" 2 WAY 3 SPEAKER SYSTEMS

AT LESS THAN 1/2 LIST PRICE

POWER RATING 20 WATTS R.M.S.
IMPEDANCE 8 OHMS
FREQUENCY RANGE 46 TO 18000 CYCLES

Supplied in kit form (less cabinet) each kit comprises: One AWA 8WAC 8in. bass unit, two AWA 4MBC 4in. tweeters with ceramic magnets & curve-linear cones, crossover components, grille cloth, innabond lining and cabinet plans.

CABINETS AVAILABLE
Post & packing extra. NSW \$2.50. Interstate \$3.50.

\$18.50
Per Kit

NEW E.M.I. AND HITACHI RECORDING TAPE AT BARGAIN PRICES

HI-DYNAMIC EMITAPE — HIGH OUTPUT — LOW NOISE — HI-FIDELITY

HLP18 7" reel 1800ft. long play \$5.95 P & P \$1.00

HDP12 5" reel 1200ft. double play \$3.95

NEW E.M.I. SUPE C90 CASSETTES, 5 FOR \$10.00. P&P \$1.00

NEW E.M.I. HI-FI C90 CASSETTES 5 for \$12.50.

Hitachi LN 8-track 90 minute cartridge 5 for \$10. P & pack \$1.50.



NEW GOODMAN-FOSTER 3-WAY 4-SPEAKER HI-FI SYSTEM

\$39.00 PER KIT

Frequency Range 45 to 22 000 cycles. Power rating 25 watts. RMS Imp. 8ohms. Supplied in kit form (less cabinet) each kit comprises two English Goodman 8" bass units, Foster 5" mid range, Foster 1" dome tweeter crossover components, Ocodensers and inductance innabond, speaker fabric and plans of cabinet. Cabinet dimensions 23" x 13" x 10". CABINETS AVAILABLE

Post & packing extra. NSW \$2.70. VIC. SA. QLD \$4.70. WA \$5.70 (REGISTERED POST \$2.00 EXTRA IF REQUIRED) cabinets available.

NEW HOKUTONE HI-FI SPEAKER KITS AT A FRACTION OF LIST PRICE

NEW THREE WAY HIGH FIDELITY SPEAKER SYSTEM WITH A FREQUENCY RANGE OF 35 TO 20,000 CYCLES. POWER RATING 50 WATTS.

Supplied in Kit form (less cabinet) Woofer HFV-302, 12" Mid range HM-24 dome, Tweeter HT-60 dome. Three way crossover with separate controls for mid range & tweeter. Innabond lining, grill fabric & cabinet plans supplied. Cabinet dimensions 668 high, 435 wide, 310 deep.

\$69.00 per kit

Freight extra by rail, air or road transport.

NEW GARRARD 6-200 CP RECORD PLAYERS

Fully automatic turntable automatically or manually as required. 11" turntable. Cue & pause control. Record speeds 33 1/3, 45 and 78 rev/min. Finished in black with silver trim. Fitted with ceramic cartridge. Post & packaging extra. NSW \$2.70. Vic. Qld. SA \$3.70. WA \$4.70 (registered post \$2 extra if required).



\$34.00

RANK-ARENA 2 WAY SPEAKER

- 10 Watts RMS
- 8 ohm impedance
- 8" woofer with tweeter
- Supplied with lead and plug
- Teak finish

Dimensions 18" H, 11" W, 9" D
Freight extra per rail, air or road transport



\$42.00
PER PAIR

NEW HOKUTONE 12" HI-FI SPEAKERS

Model 300F W09YL 12" power rating 20 watts, 80HM IMP cone resonance 30 cycles. Manufactured by Hokutone Onkyo Co Japan.

\$14.50 POST & PACK \$2.50

NEW CAR CASSETTE CONVERTERS BICOH MODEL NA100/CC-007A AT APPROX. 1/2 LIST PRICE

By connecting this model with your existing AM car radio, you can enjoy the music of any cassette that has been pre-recorded.

Connection requires no alteration to the car radio. Plug your car aerial into the cassette recorder and using the patch cord supplied, connect the recorder to the aerial connection of your car radio. By following the instructions, installation is a simple procedure. All cords & brackets are supplied. Can be used in any car with a 12 volt neg. earth system can also be used with any AM radio by using a 12V supply. Dimensions 150 x 110 x 53mm.



\$18.50
post & pack
\$1.50 extra

CLASSIC RADIO

245 PARRAMATTA RD, HABERFIELD 2045. PHONES 798-7145, 798-6507.

New Products

2-metre amateur transceiver



Icom has released a new 2-metre all-mode amateur radio transceiver, the IC251A.

Following the tradition of the earlier IC211 2-metre multimode transceiver, the IC251A has improved performance and facilities, apart from introducing new power supply technology. A pulse type (50kHz) power supply is used on AC, allowing a reduction in weight and heat.

Using microcomputer control, a multi-purpose scanning facility allows

monitoring of three different memory channels, a program scan giving scanning between two programmed frequencies. The scanning speed is adjustable and automatically stops when a signal is received.

Continuous coverage is provided over the 2-metre band with either 1kHz steps on FM or 100Hz steps on SSB, with a fast tuning facility also provided.

Further information from Vicom International Pty Ltd, 68 Eastern Rd, South Melbourne, Vic 3205.

Low-cost 1.2V voltage reference

A new, low cost 1.2V reference is available from Analog Devices Semiconductor. The AD589 will operate from 50 μ A to 5mA, dissipating only 60 μ W at 50 μ A, and is free from oscillations when shunted by capacitive loads over 1,000pF. The temperature compensated, two-terminal bandgap device is an exact replacement for other 1.2V references.

The low output impedance, — 0.6 ohm typical, 2 ohm maximum — is a factor of ten lower than typical zener diodes and allows operation with no external components required to maintain full accuracy under changing loads. No frequency compensation is required; RMS noise voltage is 5 μ V at 500 μ A from 10Hz to 10kHz. The output voltage is rated at 1.200V minimum, 1.235V typical, and 1.250V maximum.

The AD589 is available in seven grades; J, K, L and M grades for operation over the 0 $^{\circ}$ to +70 $^{\circ}$ C temperature range, and S, T and U grades for the -55 $^{\circ}$ C to +125 $^{\circ}$ C range. All S, T and U devices are available fully processed to MIL-STD 883B. Temperature coefficients are 10ppm/ $^{\circ}$ C for M grades, 25ppm/ $^{\circ}$ C for L and U grades, 50ppm/ $^{\circ}$ C for J and S grades.

Further information from Parameters Pty Ltd, 68 Alexander St, Crows Nest, NSW 2065 (phone 439 3288).

RADIO DESPATCH SERVICE

869 George St, Sydney 2000

Phone 211 0816, 211 0191



Hirose and Ansley Ribbon Cable Connectors fitted same day.



Bourns ten Turn wire wound Pots
Bourns Ten Turn Dials

BEYSCHLAG LABORATORY RESISTOR KIT LMC0309

Type MBC0309 TK100 metal film 2% 1/2W, resistors. Kit contains 10 each, value from 4.7ohms to 1M E24 (Total 1290) in three reusable trays. \$50.00

Special Limited Offer



E.A. DEC. 79 TRANSISTER-ASSISTED IGNITION SYSTEM

Complete kits
Drilled Box and heat-sink \$35.00
Undrilled box and heat-sink \$30.00



SPECIAL PACK

Contains:

5 NE555, 5-LM741, 5 0.33/100V
5 0.22/100V, 15 0.1/100V
10.047/100V
10 .01/50V Greencaps
2 1 pole 6-position rotary switches
10 Miniature push-on switches
10 DPDT slide switches
10 1N914, 101N60, 101N4004 Diodes
1 100k lin pot, 1-25k lin pot
1 1.5amp 400V Bridge Rectifier

Normal Price \$29.00

Special Pack Price \$15.00

All new components

ELECTRONICS CENTRE

BARGAIN PRICES ● PERSONAL ATTENTION ● SLICK MAIL ORDER SERVICE ● SATISFACTION ●

NEW BSR STEREO CHANGER/PLAYERS MODELS

C198 (ILLUSTRATED)
S SHAPE TONE ARM
4 POLE MOTOR
WITH CERAMIC CART

\$55.00

WITH MAGNETIC CART

\$65.00

PACK & POST: NSW \$2.75, V/SA/Q \$3.76, TAS/WA/NT \$4.75



C197
STRAIGHT TONE ARM
2 POLE MOTOR
CERAMIC CART

\$47.50

With all the wanted facilities ● Auto or manual operation ● Cueing lever ● Bias compensator ● Adjustable stylus pressure ● 33, 45, 78rpm ● Plays 7", 10", 12" records ● Separate changer and player spindles ● Operating instructions ● Template for cut-out ● Big 28cm turntable ● Diamond stylus ● 240V AC 50Hz.

BSR BELT DRIVE RECORD PLAYER ●

ABSOLUTE
LATEST MODEL P-200

\$95.00

P&P NSW \$3.50
INTERSTATE \$4.50



STYLISH S SHAPE
PICK-UP ARM ●
ADC MAGNETIC
CARTRIDGE
DIAMOND STYLUS
INCLUDED ●

ALSO AVAILABLE WITH WALNUT BASE AND
PERSPEX COVER WITH HINGES

\$119

P&P NSW \$5.00
INTERSTATE \$7.50

Specs. 240VAC 50Hz, auto or manual operation ● Plays 17, 25, 30cm (7, 10, 12in) records ● 33 and 45 rpm, adjustable counter weight and stylus pressure ● cueing lever ● Bias compensator and anti skate control ● Die-cast platter with mat ● RCA audio plugs and cable, 3-core power cable and plug ●

C-CORE TRANSFORMERS

LOW NOISE ● HIGH EFFICIENCY ● PRIMARY 240V 50Hz CONT. RATING



MODEL	SEC V	AMPS	PRICE	PACK AND POST		
				V Q	SA T	WA NT
JT 266	0-18V	8A	\$25.95	\$2.95	\$3.75	\$5.50
JT 235	260-26V	2A	\$24.95	\$2.95	\$3.75	\$5.50
JT 248	0-10V	10A	\$25.95	\$2.95	\$3.75	\$5.50
JT 249	8.5-0.8.5V	4A	\$26.50	\$2.95	\$3.75	\$5.50
	15VCT	1A				
JT 274	0-10V	10A				
	2x0-12V	1A	\$26.50	\$2.95	\$3.75	\$5.50
JT 253A	0-18V	12.5A				
		30A				
		PEAK	\$45.95	\$3.50	\$5.50	\$7.00

SUPER SCOOP



PASSIVE RADIATOR HI FI SPEAKER SYSTEM

Excellent frequency response from the 8 ohm 15 watt 200 mm (8") woofer and 200 mm tweeter with cross-over ● modern styling sturdy walnut cabinet ● 445H 280 W 178 DMM

Pack and Post NSW \$2.75
V Q SA T \$3.75
WA NT \$5.50

\$65

PAIR

STEREO CASSETTE DECK FRONT LOAD

SUPER SCOOP ● TOP BRAND ●

Pack and Post NSW \$2.50 V. Q. SA. T

\$3.50 WA. NT \$4.50

\$99.95

240V AC 50Hz ● HiFi Freq Response ● Twin illuminated V-U meters ● recording indicator ● Tape Counter ● Auto stop ● Pause ● Headphone Jack ● 2 mic inputs ● Bias/Equalizer switch for normal, FeCr, Cr O2 ● Line in/out jacks ● woodgrain cabinet 380 w x 240d x 135 h mm.



PLESSEY ROLA SPEAKER SPECIAL



GUARANTEED TOP QUALITY
BRAND NEW BARGAIN

Model C12PX, 15 ohms, 31cm (12in) twin cone Specs. 30W rms, Reson. Freq. 40Hz Freq. respon. 35-13000Hz

\$19.95 ea. P&P: NSW \$2.00
INTERSTATE \$2.75

2 for

\$37.00

P&P: NSW \$2.75
INTERSTATE \$3.75

12V SIREN ALARM

WARBLER TONE ● 100dB AT 1 Metre
● 8 WATTS OUTPUT



INDOOR

\$15.50

OUTDOOR

P&P NSW \$1.50 Interstate \$2.50

HIGH EX PMG POWER

SILICONE DIODES
200PIV, 100AMP

Good order and condition guaranteed.

\$4.75 ea

4 for \$16

HEAT SINK TO SUIT \$1.75 P&P 75c

P&P 75c

P&P \$2.50

HEAT SINK TO SUIT \$1.75 P&P 75c

PA REFLEX HORN SPEAKERS

A1 Quality, Weatherproof.

8 Ohms, 150Hz — 13KHz



6" 10 WATT	\$21.95	8" 15 WATT	\$25.50
8" x 5" 15 WATT	\$26.50	12" 25 WATT	\$39.95

Pack and Post NSW \$1.50, Interstate \$2.50

FAMOUS IMPORTED EMI CASSETTES

SUPER FERRIC ● COMPARABLE TO CHROME ● TOP QUALITY PERFORMANCE

● LOW NOISE ● HIGH OUTPUT

C60 — 5 for \$7.50 P&P \$1.50

C90 — 5 for \$10.00 P&P \$1.50

LIGHT DIMMER

240VAC 18A Aust made approved Complete with cover plates. The latest trend in home lighting.

ADDS THAT LITTLE EXTRA ATMOSPHERE

Only **\$4.50**, P&P 90c

TO CLEAR PANEL METERS

Top quality clear plastic front Type MRAB5 118 x 112mm Bar dia 85mm 30ADC 1ADC 500VDC **\$9.50 ea**
Type MRA70 85 x 77mm Bar Dia 70mm 1ADC 500MA 100MA **\$7.50 ea**
P&P NSW 75c Interstate \$1.25

SOLID STATE FAN - MOTOR SPEED CONTROLLER

240VAC 2.8A Fully sealed, complete with pot and knob **\$4.50** P&P 75c

50V DC 2AMP POWER SUPPLY

240VAC 50Hz input, Ex Ferguson and Hallam factory surplus Transformer can be used for 240/110V 1A stepdown.

Only **\$15.00** P&P \$2.50

HEAVY DUTY NI-CAD RECHARGEABLE BATTERIES

1.2v



Top quality guaranteed. Used by many Govt Depts

SIZE D 4AH **\$6.25 ea** P&P 75c

4 for \$23

P&P NSW \$1.50

INTERSTATE \$2.50

SIZE C 1.8AH **\$3.75 ea** P&P 75c

4 for \$14

P&P NSW \$1.50

INTERSTATE \$2.50

FIBREGLASS P-C BOARD

1.5mm SINGLE SIDED A1 QUALITY

350 x 82mm 5 for **\$3.50**

P&P NSW \$1.50 INTERSTATE \$2.75

365 x 330mm 5 for **\$7.50**

P&P NSW \$2.00 INTERSTATE \$3.00

BUTTERFLY VARIABLE CONDENSOR

1000PF IDEAL FOR ATU BALL BEARINGS BRASS PLATES 70 x 65 x 30mm OA

\$3.50 P&P 90c

PUSH BUTTON PHONE DIAL — WITH MEMORY



\$43.95

TELECOM APPROVED

PACK & POST \$1.25

EASY TO INSTALL

If wanted number is engaged (including strd and isd) unit will re-dial with the push of a single button Dial dia 100mm. Compatible with telecom type phones.

SERVICE

Moderate charges — Repairs guaranteed. Radios, Tape Recorders, Cassettes, Amps.

Calculator or computer? — the latest from HP

Hewlett-Packard has released a hand-held calculator package, the HP-41C, that functions very much like a small computer. It has expandable memory, alphanumeric, card reader, printer and application program modules.

The HP-41C is the most advanced and versatile hand-held calculator HP has ever developed. In addition to preprogrammed scientific and mathematical functions, the continuous memory, RPN logic machine can be tailored to perform any number of other calculations through programs written by the user or through plug-in applications software available from HP.

These plug-in application "pacs" provide the user with programs to solve problems in real estate, aviation, physics, engineering, small business, surveying, personal finance, and dozens of other dedicated applications.

The calculator's alphanumeric capability enables the user to label programs in English. Word messages alert the user to errors in calculations and programs and report on the status of programs and the calculator itself. The "alpha" feature also allows "prompt" messages to be built into programs. The display is a high-resolution LCD that minimises power consumption.

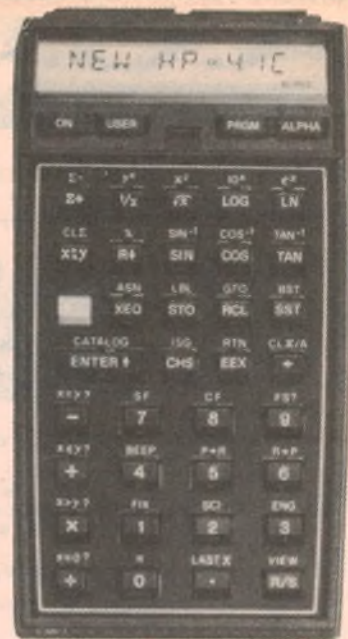
More than 130 of the most commonly used scientific and mathematical functions are programmed into the machine. The calculator keyboard identifies 58 of these functions. Upon user demand, the calculator will

provide a "catalogue" of the other available functions which can be easily accessed from the keyboard. The catalogue can also list user-defined functions.

A versatile feature of the HP-41C is that nearly any function the calculator can perform — either those built into the machine or programmed into it — can be assigned to most key locations on the keyboard. This enables the user to personalise the calculator by positioning functions on the keyboard where they are most convenient. Two keyboard overlays and a set of labels enable the user to change the keyboard markings to reflect the functions assigned to each key.

The basic machine becomes a powerful, personal calculating system with the addition of a series of options:

- Up to four memory modules can be plugged into the calculator, raising program memory from a base 400 lines, or 63 data storage registers, to as many as 2000 lines or 319 registers.
- A plug-in card reader allows the user to enter programs from recorded magnetic cards or to record programs on blank cards.
- A portable thermal printer provides hardcopy records of calculations, high-resolution plots, and complete



The basic HP-41C comes preprogrammed with 130 mathematical functions and features continuous memory and alphanumeric liquid crystal display.

alphanumeric output.

- An optical wand (available early 1980) reads and enters programs or data from printed bar codes.

- Sixteen plug-in application modules offer 4000 program steps each of preprogrammed solutions to problems in specific areas.

The HP-41C can be connected to any of these devices through four ports built into the calculator.

In addition to its built-in functions, the HP-41C is keystroke programmable by the user to perform any number of calculations. The user assigns the program a name and then presses keys on the calculator in the same order that would be used to solve a problem or perform an operation. To use the program, the user can key in the name of the program, and the entire series of keystrokes is executed automatically.

A continuous memory feature permits retention of user programs and data, even after the power has been turned off.

As with any small computer, the HP-41C also has decision-making power. A program can automatically compare data, constants, or results, and then alter execution based on the outcome of the comparison. It can also test two alphabetic strings for equality.

Recommended retail prices are as follows: HP-41C \$315; Card Reader (82104A) \$209; Printer (82143A) \$375; Memory Modules \$48. These prices do not include sales tax.

Further information on the HP-41C from Hewlett-Packard Australia Pty Ltd, 31-41 Joseph St, Blackburn, Victoria 3130.



The addition of memory modules, printer, card reader, applications modules and optical wand make the HP-41C as powerful as some small computers, according to Hewlett-Packard.

New Products

Hitachi V-152 dual trace 15MHz oscilloscope

A range of Hitachi oscilloscopes have been released onto the competitive Australian market. We tested the Hitachi V-152 which is a dual trace model with 15MHz bandwidth and maximum sensitivity of 1mV/cm. Circuitry is all solid-state with a power consumption of 40 watts.

Overall dimensions of the Hitachi V-152 are 275 x 190 x 400mm (W x H x D) including knobs, feet and rear projections. Mass is 8.5kg. The screen is an attractive blue which is a change from the usual green of most oscilloscopes.

Vertical deflection sensitivity is variable in 10 ranges from 5mV/cm to 5V/cm, with continuous variation in each range available from a knob located next to the range switch. The sensitivity can be increased to 1mV/cm with the use of the x5 gain knob.

Nineteen ranges in a 1-2-5 sequence are provided for the timebase, with continuous adjustment available from the "SWP VAR" knob to the side of the range switch. In addition, the horizontal trace position control can be pulled out to provide a 10x magnification of the sweep signal. This will give a maximum sweep speed of 100ns/division.

An attractive feature of the timebase switch is the ability to turn the switch to X-Y operation, with the second channel displaying the horizontal component. This makes Lissajous figure operation for comparison of two signals an easy matter. The full gain of the second channel (5mV/cm) can be used, making this feature very attractive.

Two switches and a knob provide comprehensive trigger selection facilities. The TV line and TV frame sync pulse triggering facility is incorporated into the timebase switch and is automatically selected depending on the timebase range. Similarly, selection of chopped or alternate trace operation is incorporated into the range switch.

Five display modes are available: CH1, CH2, CH1 and CH2 (dual), Add and Difference. Input signals to the vertical inputs can be AC or DC coupled or grounded. Input impedance is 1M shunted by 30pF. AC bandwidth is 10Hz to 15.2MHz (-3dB points).

Additional features of this CRO are the blanking facility located at the rear of the CRO and the trace rotation adjustment at the front panel. No graticule lighting is provided. We did not miss the graticule lighting but would have preferred the V-152 with a tilting bail to enable a more convenient

The Hitachi V-152 oscilloscope is one of a range of four models distributed by Standard Components Pty Ltd.



viewing angle.

Internal layout of the V-152 is clean and uncluttered. One very large PC board containing the vertical amp, power supply and high voltage circuitry covers the entire base of the CRO. Two smaller PC boards accommodate the sweep generator, horizontal and vertical output amplifiers. The calibration circuitry is located on another, small PC board.

All switches and controls are wired directly to the PC boards and all connections between boards are made via quickly disconnectable plugs and connectors. All the boards can be quickly removed from the chassis.

We counted eleven integrated circuits. Eight of these are 7400 series TTL ICs. There should be no problem here

with replacements if they are ever needed.

Shielding is provided for the high voltage supply by way of a brass shield. Most of the heatsinks for the transistors were made from copper rather than aluminium. The Cathode Ray Tube is screened with a steel plate protecting it from stray magnetic fields.

We found the V-152 a delight to operate. The simplicity of the controls belies its performance. It has the full 15MHz bandwidth available at deflections up to 8cm and a maximum sensitivity of 1mV/cm. The traces are sharp and waveforms with fast risetimes are easily viewed. We can recommend this

CRO for laboratory or hobbyist use.

A comprehensive operation manual is supplied with the oscilloscope, but probes are extra. The distributors, Standard Components, however, advise that they have a range of probes available. The prices range from \$20 + tax for a 1:1 probe to \$35 + tax for 10:1 probes.

Price of the V-152 dual trace oscilloscope is \$540 plus sales tax if applicable. This includes the operation manual mentioned above. This is good value considering the price of similar performance oscilloscopes.

Further information can be obtained from the distributors, Standard Components Pty Ltd, 10 Hill Street, Leichhardt, NSW 2040. (J.C.)

11655kHz, which is transmitted over the long path, while the short path service continues on 21500kHz, the signal coming across Asia to Australia. The broadcast at 1200GMT is now on 17560, a move from 17565. The power on all transmitters on the lower frequencies is 300kW. Other transmissions in English are at 2000 and can be heard on 9425, 11655 and 15425kHz.

VOICE OF AMERICA FACILITIES

The Voice of America has established relay bases in several countries and in recent months there has been a move by these countries to request time on the VOA facility. In the past the Greek radio has been relayed on the VOA transmitters and the powerful million watt transmitter in Thailand has also been used by that Government for relays of its domestic program. The Voice of America relay base in Morocco, 20km south of Tangier, is now being used by the Moroccan Government to relay some of its domestic programs. The 21735kHz channel was formerly used by the Rabat transmitters of the Moroccan radio to relay its programs in Arabic but this frequency is now operated from VOA Tangier 1100-2200 GMT. The program is also carried on the Tangier transmitters at various times on 6090, 6170, 9540, 15155, 15160, 15335 and 15360kHz.

RADIO VERITAS ASIA

The latest schedule from Radio Veritas Asia indicates that they have made some frequency changes and are generally operating three frequencies in parallel. The broadcast for our morning reception, indicates they open at 2155GMT in Chinese on 9740, 11725 and 15285kHz. English is broadcast at 0030-0100 on 15135, 15285 and 17790kHz. A further transmission in English at 0300-0330 can be heard on 15285, 15320 and 17790kHz.

The evening broadcasts open at 0955GMT on 9615, 11775 and 15215kHz. English programs are at 1130-1200 on the same frequencies, while the last English program for the day, at 1430-1500, is on 9605, 11955 and 15215kHz.

The programs are of a gospel nature

and in most of the Asian languages. Radio Veritas Asia welcomes reception reports to P.O. Box 939, Manila, Philippines.

SWAZILAND BOOSTS POWER

Trans World Radio in Swaziland has recently installed a new 100kW transmitter which is now in regular operation and, according to the schedule received from the station, is using 11840kHz at 1530-1930 to Central and East Africa and this transmission should be one of the best received here.

Trans World Radio has been broadcasting for more than five years from Swaziland and over that period used 25kW transmitters. The new 100kW transmitter has a frequency range of 3-26MHz and can be preset to cover 10 frequencies. The higher power will boost TWR signals: into Central Africa as they are fed into a 4 x 4 curtain antenna directed to the north. The aerial is capable of being slewed by 30° either side of centre, providing even more focusing of the signal onto specific target areas. The new 100kW transmitter is housed with the four 25kW transmitters. The mailing address is PO Box 64, Manzini, Swaziland.

LISTENING BRIEFS EUROPE

FINLAND: Helsinki has been heard on 9575kHz with a transmission closing at 0730GMT. The broadcast was in Finnish but at 0725GMT suffered interference from Trans World Radio at Bonaire, which opens at that time with a gospel program in Portuguese.

FRANCE: "Paris Calling Africa" is the only English language service broadcast from Paris and is now heard 1700-1800GMT. Many frequencies carry the transmission and these include 11845, 15300, 15360, 15425, 17795, 17850, 17860, 21580, 21620 and 21675kHz.

AUSTRIA: Vienna is widely reported with its 13-metre band signals by Z. Hayder of Mt. Isa, Queensland, who notes signals on all frequencies being used. The transmission, in English, at 0830-0900 is best received on 21640 and 21735kHz. On Sunday Austrian Short-

wave Panorama is broadcast at 0900 and can be heard on 21585kHz.

EAST GERMANY: Radio Berlin International has revised its English broadcasts and is now heard at 1415-1500GMT on 9730, 11700, 15240 and 15285kHz. Broadcasts to Australia in English at 0645 are now on 15110, 17700 and 21465, while at 1200 the transmissions are on 15115, 17880, 21465 and 21540kHz.

AFRICA

ALGIERS: Since the retiming the English broadcasts by Radio Algiers, which are now heard at 2100-2130GMT, a further out-of-band frequency has been noted. Leigh Morris of Palmerston North, NZ reports reception on 10935kHz while, at the same time, we have been hearing the signals on 11615 and 11810kHz. The schedule change also means that the Spanish broadcast is now heard 2130-2200GMT. **UGANDA:** Leigh Morris also reports Uganda Broadcasting Corporation at Kampala being heard on 15250kHz at 1835GMT with an English commentary but with interference from another station. Kampala continues to be well received in its transmission to Australia at 0300-0400GMT on 15325kHz. This frequency provides good reception, but the schedule is such that transmission is always running a little late.

ASIA

NEPAL: According to the BBC Monitoring Service, Radio Nepal's External service program in English to India is currently observed from 1435-1520 on 7174kHz instead of 3245 and 5008kHz. Victor Goonetilleke of Sri Lanka reports that test transmissions have been heard from a 100kW transmitter on 9590 at 1150-1720GMT. He also comments that other frequencies are available, including 7165, 11970, 15200 and 17800kHz.

UZBEKISTAN USSR: Radio Tashkent has two English broadcasts daily at 1200 and 1400GMT. The signals are now received on three frequencies; 6025, 9540 and 11875kHz. The best reception is on 6025kHz and Tom Chisnali, of Nelson, NZ reports interference on the other two frequencies.

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SHORTWAVE SCENE



by Arthur Cushen, MBE

Short-wave stations experiment at high end of HF band as sunspot count increases

The current increase in sunspot activity has encouraged several short-wave stations to experiment with relatively low power stations at higher than normal frequencies, notably in the 26MHz band. One of these, HCJB in Quito, Ecuador, is using a 100W transmitter and has been heard at our listening post.

The tests transmissions from HCJB are on the air 24 hours a day and in the South Pacific are best around 0800GMT to past 1000GMT, but have also been noted at 1900GMT. The frequency is 26000kHz and is blocked by the Voice of America in the Philippines on this frequency from 2200GMT, but the channel is free from other interference. The fact that this very low powered signal has also been reported from North America indicates the long distances possible on the 11-metre band during these high sunspot conditions.

It is interesting to recall that in 1958 the Radio Norway engineers also tested a 100W transmitter in this band on 25900kHz with the call sign LLA. This transmission was also heard well in New Zealand and proved to be one of the best catches of that period when one takes into consideration the low power and the higher frequency. The broadcasts from HCJB are not mentioned on station announcements, no reference is made to 26000kHz, and the program material broadcast can be taken from any of those being transmitted by HCJB. Thus, it is necessary to get fairly good reception of this low powered signal to be able to compile your reception report. We have noticed that, on the whole, English programs are used

Notes from readers should be sent to Arthur Cushen, 212 Earn Street, Invercargill, NZ. All times are GMT. Add eight hours for WAST, 10 hours for EAST and 12 hours for NZT. In areas observing Daylight Saving Time add a further hour.

and this will make identification easier for listeners world wide.

THE VOICE OF CHILE

The latest information from the Voice of Chile (Santiago) indicates a new schedule is in operation up to March 1, 1980. The transmission covers broadcasts in Spanish, English, and French and the best times for the English broadcasts are 1000, 1100 and 1230GMT on 17790kHz. Morning reception at 2100GMT is on 17715 and 17790kHz; 2200 on 15150, 17790 and 17800kHz. The afternoon transmissions include one at 0330GMT on 11720kHz.

The latest schedule shows 13 broadcasts in English during the daily transmission and the station confirms reception with a verification card and schedule, though it is about eight months before a reply is received. The address is the Voice of Chile, Casilla 244-V, Santiago, Chile.

BANGLADESH BROADCASTS

Radio Bangladesh at Dacca is using three frequencies for their English broadcasts at 0445-0515GMT. These are 15400, 17890 and 21685kHz; 21685kHz giving the best reception. There is some interference from Radio Australia on 21680, but the program of news, commentary, and music can be followed throughout the transmission. The other two frequencies suffer interference; 15400kHz from the BBC World Service and 17890kHz from Radio Australia on the same channel.

Other English transmissions are at 1230-1300GMT on 15285 and 21670kHz; 1815-1900 on 11765 and 15285kHz.

AFRTVS CHANGES

The American Armed Forces Radio and Television Service has changed frequency for its Bethany transmission 0900-1100GMT. This is now on 9660kHz (replacing 9575) but in this area suffers interference from ABC Brisbane. The transmission is actually beamed to Europe and Africa. The Greenville transmitter on 9585 is using the same schedule.

Broadcasts to the Pacific and Far East are on 9700kHz at 0900-1600GMT: 11805, 0900-1800: 15330, 0430-0700: 17765, 0200-0700 and 1600-2200: 21570, 1800-0430: 25615, 2200-0200. The AFRTVS does not issue a regular program schedule but these are sent on request to AFRTVS, 1117 North 19th Street, Arlington Virginia 22209, U.S.A.

RADIO MOSCOW DX PROGRAM

Radio Moscow World Service has recently retimed some of its broadcasts and the DX Program is now heard on Saturday at 0810GMT. The 20 minute session includes information on new schedules, replies to listeners' technical questions, and information about a Soviet Union station.

The World Service is broadcast at 0400-1400 and 1900-2300GMT to Australia and New Zealand. At 0800GMT the DX Program can be heard on 9780, 15130, 15380, 17800, 17820 and 21530kHz.

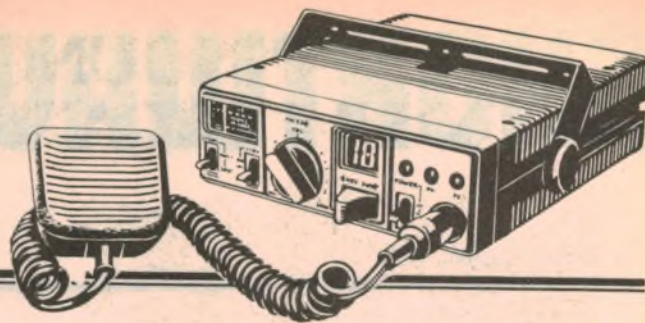
Moscow Mailbag is broadcast on Sunday at 0610 and Monday at 1010 on 9780 and 17820kHz.

ISRAEL CHANGES

The Israel Broadcasting Authority has moved to 29720kHz at 0530GMT in Russian. This transmission is on Saturday and Sunday only and replaces 29705kHz. The broadcast continues to 0600GMT and is carried on several other frequencies which are generally jammed.

The changes to listeners in Australia from Israel include the English broadcast at 0500GMT, 11637 replacing

The Australian CB SCENE



FIGHT NOW — OR FACE A DEBACLE IN '82

Will CBers be banned from using 27MHz in 1982? The NCRA says now is the time for all who want that band retained to stand up and be counted!

by JAN CHRISTENSEN*

As all CB operators are aware, or at least should be aware, the Government has decreed that Citizens' Band operations on the 27MHz band will cease in 1982. This was stated categorically in the original RB 14, but in the new RB 14, it says that "Current policy anticipates that the HF band will cease to be available to the CBers on June 30, 1982. Hence any licence for HF equipment renewed after July 1, 1981, shall expire on June 30, 1982."

This, I feel, is where we should fight. Neither the operators nor the Industry know where they stand, and the Government's indecision is killing the Service.

We have all paid our \$25 a year licence fees, and with 35,000 licenced operators in Queensland alone, that amounts to around \$875,000 per year. If you add to that the fees collected from the thousands of other operators in the remaining State and Territories, you have the Government with a multi-million dollar a year revenue raiser, for which it gives very little in return.

The Citizens' Band Radio Service is costing the Government very little to administer, simply because so little is being done. In fact, if the CB operators were shareholders in a company called the CBRS, and the Government (or the Department) was the Board of Management of our business, they would have been sacked a long time ago!

One of the reasons that the Government's present stance on the 1982 question is so ridiculous is that they are earning big money for next to no outlay, and yet are talking about:

- (1) Doing away with the HF side of the CBRS and the money it brings in, and

- (2) The need for cutbacks in Government spending!

CB has opened so many new horizons for the citizens of Australia that I firmly believe that it would be nothing short of criminal for the Government to take the most popular band away from the people.

There are two types of equipment available to us to use on the CBRS at this time; HF and UHF. If a person is looking for reliable short distance communications, with no background noise or overcrowded channels, then UHF is for them. On the other hand, if an operator is seeking longer distance communications, remembering that now it is legal to work any licenced station within the geographic boundaries of Australia and its Territories, then HF is the logical choice.

Unfortunately, the 27MHz band is severely overcrowded. Ironically the Government realises this and unofficially says that, if the NCRA can win the battle to keep 27MHz, extra frequencies will be allocated to the band.

CB operators are faced with the farcical situation of the Government saying that, after 1982, CB will be permitted only on UHF. But it also admits that operations will continue on HF after that date, with next to no-one paying licence fees, because they will be pirating again! This means that the Department won't be collecting the revenue out of which its officers are paid so that the restrictions can be policed! The position would be reminiscent of the pre-legalisation days, with the exception that there would be many thousands more operators for the Department to contend with.

The National Citizens' Radio Association of Australia (NCRA) has lobbied the Government since 1977 for the retention of the 27MHz band within

the CBRS. We can see no reason why there can't be a dual HF-UHF Service. We have also lobbied for the betterment of conditions on the CBRS, and will continue to do so, hopefully with the support of CBers right across Australia.

We fail to see why Australians should pay out hundreds of dollars for HF equipment, plus \$25 dollars a year for the right to use it, and then be forced to throw the lot on the rubbish heap.

We also fail to see why the Government should wish to deprive itself of millions of dollars every year in licence fees, import and sales taxes and the untold amounts collected through the personal taxation on the wages of the people who earn their living through the Industry. If there is a valid reason for this, then I'm afraid that we can't see it.

Will CBers be allowed to keep 27MHz, or must we be forced back to being pirates once more?

If every CB operator in Australia, whether affiliated with the NCRA or not, whether a casual or constant user of CB, wrote now to his local MP in protest against the elimination of the HF band; if every operator thought deeply and acted; if we could all join together as a united force and demand our rights, then I would say that we will win. But until that day arrives, the future of the 27MHz CB band is in grave danger. And once it is gone, it is too late then to say what should have been done! NOW is the time! Stand up and be counted . . . if you care.

Anyone wishing information on CB in general, on the NCRA or wishing to find out how to join the NCRA either as an Individual Member or through a club, please contact me either through this magazine or direct at PO Box 406, Fortitude Valley, Qld 4006. ☺

* Jan Christensen is National Liaison Officer of NCRA, the National Citizens' Radio Association of Australia.

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THETA 7000E COMMUNICATIONS COMPUTER

Due to the most up-to-date computer technology, just one piece of equipment can now handle both transmitting and receiving in CW, RTTY and ASCII.

VHF and Composite video output provided:

Both home TV set and video monitor outputs are provided for display purposes.

Printer interface.

Centronics Compatible interface enables easy connection of a low-cost dot printer for hard copies.

Wide range of transmitting and receiving speeds

10 communication speeds for transmitting (with automatic CW speed adjustment on receive) and 8 communication speeds for transmitting and receiving in RTTY and ASCII. The multiple speed feature makes the Theta-7000E ideal for Amateur, business and commercial use.

Built-in demodulator for high performance.

Three-step shift (either 170Hz, 425Hz, 850Hz) can be obtained in High Tone and Low Tone by the switch. Manual adjustment is available by FINE TUNING control.

Crystal controlled modulator

A transceiver without AFSK function can transmit in RTTY mode by utilising the high stability crystal-controlled modulator controlled by the computer.

Convenient ASCII key arrangement.

The keyboard layout is the same as a regular typewriter and automatic insertion of LTR/FIG code makes operation a breeze.

Large capacity display memory.

The two-page display memory contains 32 characters x 16 lines per page. Page selection is operated via the keyboard.

Split-screen

With a keyboard command, the same page can be divided in two: the upper half for transmit and the lower half for receive. Sentences can be edited whilst receiving.

Automatic Transmit/Receive switch.

The transmit/receive switch is controlled by the microprocessor. (Manual operation is also available). Built-in remote control key function controls the transmit/receive switch of the transceiver.

Anti-noise circuit.

A new anti-noise circuit prevents garbled messages when there is no signal.

Battery backed-up memory

Data in the battery backed-up memory is retained when the external power source is removed. The Theta-7000E has provision for 64 characters x 7 channels in the non-volatile memory. Data in this memory can be repeated 1-9 times from a keyboard instruction. Every channel can read out continuously. The channel number in use is displayed on the screen.

SEND function

The SEND function sends the whole data displayed on the screen, including the stored data in channels, with an instruction from the keyboard. The message can be stopped and easily restarted.

Buffer memory.

A 53-character-buffer-memory is displayed on the 17th and 18th lines on the screen. The characters move to the left erasing one by one as soon as they are transmitted. Data in the channels can be displayed in the buffer.

Rub out function.

Mistakes can be erased whilst the information is still in the buffer memory. If the mistake has already been sent correcting code will be transmitted.

Simultaneous access of the memory

Whilst receiving, it is possible to write into the channel memory and the buffer memory from the keyboard. When sending from the channel memory or the screen it is possible to write into the buffer memory.

Pre-loading function.

The buffer memory can momentarily store data and release it on an instruction from the keyboard.

Channel No., Page No., and Case No.

Channel No., Page No., and Case (FIG/LTR) in RTTY are displayed in the 17th line of the screen.

CR (Carriage return)/LF (line feed) cancel function.

When receiving CR or LF they are replaced by = (equal) and (underline) respectively for effective use of the screen.

Cursor control function.

Full cursor control (up/down — left/right) is available from the keyboard.

WORD MODE operation.

Characters can be transmitted by word groupings.

Automatic CR/LF

While sending, CR/LF are automatically inserted once every 72 (60 or 80) characters.

Echo function.

With a keyboard instruction, received data can be read and sent out at the same time. A cassette tape can be used as the source data.

WORD-WRAP-AROUND function.

In receive mode word-wrap-around prevents the last word of line from splitting in two.

Transmit/receive in ASCII mode in RTTY.

On instruction from the keyboard, the same AFSK signals as used in RTTY are transmitted in ASCII mode.

CW Identification function.

Keyboard controlled CW identification is available if required.

MARK-AND-BREAK (SPACE-AND-BREAK) system.

Either mark or space tone can be used to copy RTTY.

Monitor circuit.

A built-in monitor circuit with an automatic transmit/receive switch enables checking of the transmitting and receiving state. In receive mode it is possible to check the output of the mark filter, the space filter and AGC amplifier prior to the filters.

CW practice function.

The Theta-7000E reads data from the key and displays the characters on the screen.

Variable CW weights.

For CW transmission, weights (ratio of dot to dash) can be changed within the limits of 1.3:1.6.

Cross-pattern checking output terminal

Provision has been made for attachment of an oscilloscope to aid tuning. This supplements the tuning LED and audio monitor provided in the system.

Log-computer output provided.

The Theta-7000E has an output terminal for connection to a log-keeping computer.

Test message function

"RV" and "QBF" test messages can be repeated with this function.

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KENWOOD R-1000

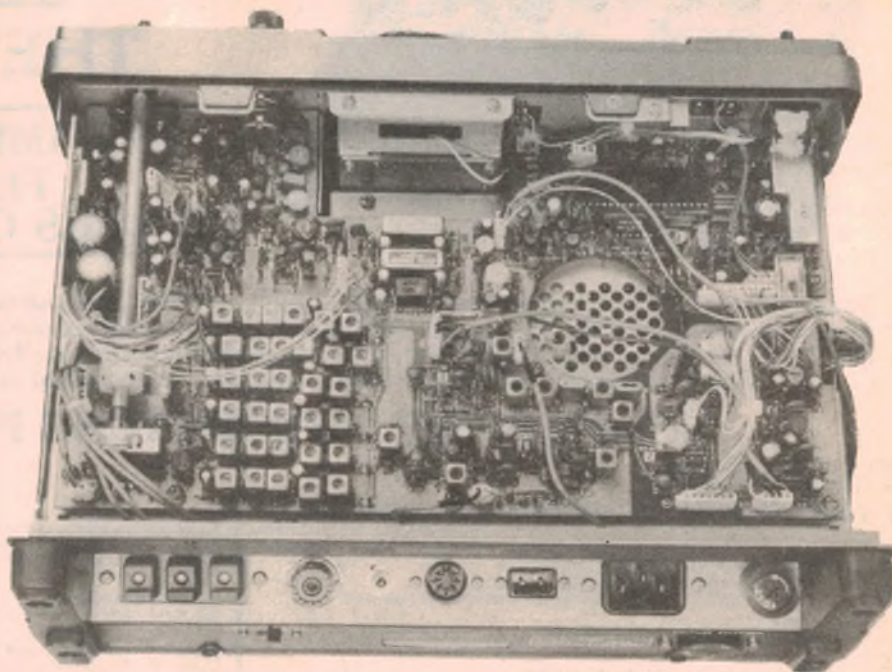
2MHz, and 0.5uV and 5uV for SSB and AM respectively, from 2MHz to 30MHz. These figures are for a signal plus noise to noise ratio of 10dB minimum. Measurements showed that the actual sensitivity was comfortably within these figures and in many cases, very much better.

The AGC performance was equally impressive. The generator input at 10MHz to give about S1 reading on the meter was well below 1uV and an increase of 100dB in signal level resulted in less than 2dB increase in audio output. The noise blanker also works very well, so much so that under noisy conditions, many weak signals which are below the noise level can be copied when the noise blanker is switched on.

A couple of points which attracted my attention relate to the loudspeaker and the AGC release characteristic. While I have no strong feelings about it, I prefer to have the inbuilt loudspeaker mounted on the front panel if possible, or underneath. The AGC release time is quite long and this is good for SSB reception. However, when tuning from a very strong signal, to look for an adjacent weak one, the sensitivity is reduced by the AGC and one has to wait for a few seconds before the weak signal is tunable.

Apart from the above minor points, my overall impression of the R-1000 is that it is an excellent piece of equipment. It should be a strong competitor in its field and it offers very good value for money at under \$500. A well illustrated manual is provided, which includes a circuit diagram.

At the time of writing, the importers have a large number of back orders to fill but supplies should become available in March, 1980. The unit for review was supplied by Trio-Kenwood (Australia) Pty Ltd, 31 Whiting Street, Artarmon, NSW 2064. Telephone (02) 438 1277. (I.L.P.)



A single PCB accommodates all the circuitry of the Kenwood R-1000 receiver.

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Supply voltage to be nominated by user

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Nominated by user

Maximum Crystal Frequency:

5 Volt Supply - 5MHz max 12 Volt - 9MHz max

Crystal Frequency:

Required frequency X number counters
Frequency X 2x

NUMBER OF COUNTERS

Model BSC 6 - 14
BSC 13 - 16
BSC 22 - 28 Stages
BSC 11 - 14

BSC 11 has varicap

Fine and Course trimming for higher setting accuracy

Crystal Locked:

for maximum stability

Output Options:

2¹ through 2²⁸

FORMULAR for crystals frequency:

(Required output frequency X 2x to give a crystal frequency of 2 to 8MHz ie. 100Hz X 2¹⁶ = 6553.6)

Output: Square wave 0 - 99 supply volts I - 20 MA Max

Supply voltage 5 - 12 Volts Dc

Stability: ± 0.03% / 0-60°C

P.C.B. Dimensions

	length	width	height
BSC 6	43 mm	27 mm	20 mm
BSC 13	52 mm	40 mm	26 mm
BSC 22/11	54 mm	48 mm	26 mm

If the module you require is not listed then please inquire.

We have many others.



Model BSC 11



Model BSC 6



Model BSC 13/22

Kenwood R-1000 receiver

The Kenwood Model R-1000 communications receiver has recently been released by Trio-Kenwood (Australia) Pty Ltd. It uses a phase-locked loop and covers the frequency range of 200kHz to 30MHz. Capable of reception in AM, SSB and CW modes and featuring digital readout, the receiver appeals as an excellent unit for use by short-wave listeners and amateurs, as well as being useful for some commercial applications.

Since the introduction of the principle of tuning across the RF range in discrete 1MHz steps, it has virtually become the norm with receivers of recent design. The now well known Wadley loop has been used on many receivers but the R-1000 uses instead the phase locked loop principle to provide stable internal frequencies.

The RF amplifier is rather unique in that it is not tuned to the incoming signal frequency in the normal way. Rather, there is a number of discrete bandpass filters, covering the range 200kHz to 30MHz. The appropriate filter is switched into circuit automatically, using diode switching, so that the need to continually peak up the RF stage tuning has been eliminated.

The signal is passed through an RF amplifier to the first mixer, consisting of a balanced pair of dual gate FETs, where it is upconverted to 48.055MHz. The first IF is a band-pass filter with a bandwidth of 17kHz. A second mixer follows, similar to the first, where conversion to a second IF of 455kHz takes place. Injection for the second mixer is from a 47.6MHz crystal oscillator associated with the PLL. Injection for the first mixer (48.055-78.055MHz) is synthesised in the PLL together with the VFO (4.545-4.545MHz) to produce the first IF of 48.055MHz from the incoming signal.

The VFO constitutes the main tuning in kHz for the receiver. MHz selection is by a 30 position switch (calibrated 0-29MHz) which actuates the PLL and, in addition, selects the appropriate RF band-pass filter.

Immediately following the second mixer is a noise blanker. Then there are three band-pass filters, one each to give wide band or narrow band for AM and a third for SSB and CW. There are two stages of IF amplification and separate detectors for AM and SSB. Two carrier insertion oscillators are provided for SSB, one each for upper and lower sideband resolution. Audio amplifica-

tion is provided for a tape recorder as well as for the usual headphones and built-in or external loudspeaker.

In addition to the circuit of the receiver proper, there is the circuitry to do with facilities such as a clock and ON and OFF timer and the counting and display circuitry for digital readout for the receiver tuning, clock and timer.

The R-1000 is housed in a dark grey metal cabinet, 300mm wide x 115mm high x 218mm deep. The front panel is diecast and the overall finish provides an attractive professional appearance.



Controls on the front panel are well placed and give an uncluttered appearance.

Tuning signals on this receiver is about as easy as it could be. The main tuning knob has a fast tuning recess for a finger and, although there is no flywheel effect, it has a good smooth feel to it; so much so that SSB signals can be tuned without effort and fast changes across the range may also be made with ease. Readout for tuning is by a five digit LED display, giving an accuracy to the nearest kHz. There is also an analog scale which is calibrated in

10kHz steps.

The digital readout also performs the added functions for the clock and for setting the timer operations.

A signal strength meter is calibrated in "S" points and up to 40dB above S9. The analog dial scale and the meter are illuminated and a push-button is provided to dim the light level.

Other controls on the front panel include the 30-position MHz selector switch, a four-position antenna attenuator switch, tone and volume controls, four mode push-buttons, switches for the clock and timer functions, power switch, phones and record outlets.

There are also extra facilities on the back panel: a coaxial socket takes an antenna lead-in of 50 ohms for HF use. Also, there are terminals, one for an earth wire, one for a random wire for HF and one for a random wire for use below 2MHz. A switch selects either the 50 ohm or random wire input for HF use. Sockets are provided for mains input (with fuse and voltage selector), 13.8V DC input, remote control for use with a transmitter and an external speaker.

The built-in loudspeaker is on the top panel of the cabinet. A carrying handle with a series of detents may be used as a prop to raise the front panel for easier access to the controls. Also, although the receiver is not intended as a portable, it may be used as such by virtue of the handle and the facility to

operate from an external 13.8V DC supply.

Some measurements which I made on the R-1000 were quite impressive. A drift check taken at 10MHz, from one minute after switch-on, to 60 minutes showed a drift of 530Hz and another 140Hz in the next 30 minutes. This is well within the specification which quotes 2kHz maximum for the first 60 minutes and 300Hz maximum in any subsequent 30 minutes.

Sensitivity figures given in the specification are: 5uV and 50uV for SSB and AM respectively, from 200kHz to

AMATEUR RADIO

struction, and practical construction projects.

Full details may be obtained from Jim Harper, VK2VFC on telephone (02) 457 9158.

RADIO CLUB NEWS

CENTRAL COAST AMATEUR RADIO CLUB: A final reminder that the annual field day will be held at the Gosford Showground on Sunday 17th February, 1980. An invitation has been extended to all amateurs, their families, and friends to attend. Full details were given in last month's notes.

LIVERPOOL AND DISTRICT AMATEUR RADIO CLUB: The club will hold a field day on Sunday 23rd March, 1980, at Catherine Fields Hall, Cnr Catherine Fields and Chisolm Roads, Catherine Fields (opposite Post Office).

There will be something for everybody. The whole family will be catered for with equipment displays, disposal sales, hidden transmitter hunts, quiz competitions and novel events.

Registrations commence at 8.30am and activities will continue until 4.00pm with prize presentation.

Registration fees: Children under 16 years and pensioners \$2.00; Adults \$4.00 per person; Families \$6.00.

Catherine Fields is 16km west of Liverpool on the old Hume Highway. Map references are: UBD 106, E3; Gregory's 143 D6.

For further information or accommodation booking inquiries ring (02) 72 1107 or (02) 605 4461 or write to Llyod Anderson, 105 Willan Drive, Cartwright, 2168.

CANADIAN S-W-L INTERNATIONAL: Founded on 21st May, 1977, it aims to promote all activities associated with short-wave listening.

Membership is open to anyone in the world. Annual dues outside Canada or USA \$US12.00 which includes airmail delivery of club bulletin "CANDX" containing 40 pages of SWL news and information.

For further information contact Kelvin Hudson, 39 Warwick Avenue, Kurralta Park, South Australia 5037, who is honorary publicity officer for Australasia, the Far East, and Seychelle Islands.

COFFS HARBOUR AND DISTRICT AMATEUR RADIO CLUB: Thirty members attended the second annual

meeting of the club and elected Max Francis, VK2BMK president; Paul Ireland, VK2VQI, secretary; Norm Napper, VK2VMP treasurer, plus a committee of five licensed members. The club conducts classes for the novice licence and, each Monday night, conducts a club net and news session commencing at 8.00pm on 3610kHz. Preparations are being made for the 1980 Urunga Radio Convention planned to commence at 8.00pm Good Friday 4th April. Registration fee will be \$5.00. Program will include all the popular events. For further details contact Paul Ireland, PO Box 655, Coffs Harbour, NSW 2450 or telephone (066) 52 4389.

ILLAWARRA AMATEUR RADIO SOCIETY: The society's monthly newsletter, "The Propagator", advises that The School of General Studies at the Wollongong Technical College will be running its course in electronics again in 1980.

The course offers an excellent opportunity to obtain the necessary qualification to gain the novice licence or to upgrade to a full licence.

Class times are from 6.00pm — 9.00pm each Friday night, commencing 15th February, 1980. Enrolment is on the first night of the course in Room 213, Mathews Building, Wollongong Technical College at 6.00pm.

Further information from Brian Wade, VK2AXI. Phone after hours (042) 84 1381.

WOULD YOU LIKE TO JOIN THE RANKS OF AMATEUR RADIO ENTHUSIASTS?

The Institute conducts Courses for the A.O.C.P. or L.A.O.C.P. with the benefit of expert guidance throughout your studies.

PERSONAL CLASSES for 1980 will commence on Tuesday, February 5th, at 6:00pm at Crows Nest, and will continue for three terms to December in readiness for the February 1981 examinations.

CORRESPONDENCE COURSES may be commenced at any time.

For further information, write to:

The Course Supervisor, W.I.A.
PO Box 123,
St Leonards, NSW 2065

IONOSPHERIC PREDICTIONS FOR FEBRUARY

Reproduced below are radio propagation graphs based on information supplied by the Ionospheric Prediction Service Division of the Department of Science. The graphs are based on the limits set by the MUF (Maximum Usable Frequency) and the ALF (Absorption Limiting Frequency). Black bands indicate periods when circuit is open.

2.80

14MHz EAST		01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23
EAST AUST TO BARBADOS (SR)																								
JOHANNESBURG																								
MURDO SOUND																								
NEW DELHI																								
NEW YORK																								
RIO DE JANEIRO																								
TOKYO																								
VANCOUVER																								
WELLINGTON																								
WEST AFRICA																								
WEST EUROPE (SR)																								
WEST EUROPE (LR)																								
ADELAIDE TO SYDNEY																								
BRISBANE TO MELBOURNE																								
PERTH																								
SYDNEY																								
DARWIN TO SYDNEY																								
MELBOURNE TO PERTH																								
SYDNEY																								
21MHz GMT		15	16	17	18	19	20	21	22	23	24	01	02	03	04	05	06	07	08	09	10	11	12	13
EAST AUST TO BARBADOS (SR)																								
JOHANNESBURG																								
MURDO SOUND																								
NEW DELHI																								
NEW YORK																								
RIO DE JANEIRO																								
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DARWIN TO SYDNEY																								
MELBOURNE TO PERTH																								
SYDNEY																								
28MHz EAST		01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23
EAST AUST TO BARBADOS (SR)																								
JOHANNESBURG																								
MURDO SOUND																								
NEW DELHI																								
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SYDNEY																								

AMATEUR RADIO

frequency allocations between 4.000MHz and 27.000MHz: "The amateur service has been allocated additional bands at 10100 — 1015kHz on a secondary basis; 18068 — 18163kHz, including amateur satellite, on an exclusive basis, and at 24890 — 24990kHz, also including amateur satellite on an exclusive basis. The availability of the latter two bands to the amateur service is dependent upon the completion of the satisfactory transfer of all assignments operating in these bands and recorded in the Master Register."

In the sections dealing with the bands 960MHz to 40GHz and 40GHz to 400GHz the following statement appears:

"Extensive allocations have been made jointly to the amateur-satellite and the amateur services, both on an exclusive basis and sharing with other services on a secondary basis."

Standard frequency and time signal services have been added to the table, for Region III, on 8000kHz and 16000kHz.

ANOTHER SAFARI

From time to time your correspondent has reported on unusual VHF contacts made during a holiday safari. Here is another one.

During the first week in December, 1979, a week was spent at Cooma, in southern New South Wales. As has become a habit, the ICOM 215 VHF packet transceiver was included in the baggage.

At the motel in Cooma not a signal was heard. This was probably due, in part, to being off the usual interstate route and in part to the distance of the nearest repeater. This was VK1RGI (channel 7) at Mt Ginini, ACT, over 81km away and shielded by some of the most rugged country in the Snowy Mountains. However, we hoped to make contacts during two trips through the mountains.

The first was to Threadbo and the Mount Kosciusko winter resorts which, in December, are sprinkled with wild flowers and have an entirely different beauty. The second was to Cabramurra, the highest town in Australia at 1122m asl.

At Threadbo village is Australia's longest chairlift; it is 2km long and rises 600 metres above the valley. From its summit it was hoped that a contact through VK1RGI on Mount Ginini might be possible.

However, a more unusual contact was to be made. About halfway up the

chairlift I unexpectedly recognised a fellow amateur, Lyle Patison, VK2ALU, on the downward side of the chairlift returning to the valley. The eyeball QSO as we passed was one of surprise and a vocal inquiry revealed that Lyle had two metre equipment with him in his car at the bottom.

At the top of the chairlift time did not allow me to walk higher up the mountain to where contact through VK1RGI may have been possible. However, returning on the chairlift an unusual contact — VK2ALU/M and VK2APQ/chairlift mobile — took place during the 15 minute descent. In the discussion which followed the handshake to seal the unexpected meeting it was agreed that the contact, although unexpected and unusual, was not in quite the same category as Lyle's moon-bounce contacts from VK2AMW at Dapto.

Later on the same trip, a call was made from a Charlotte pass lookout which is within sight of Mount Kosciusko and 107km from Mount Ginini. No difficulty was experienced working through VK1RGI and joining a group which included VK2DO at Yass, VK1AOP/M in Canberra and several others.

On the trip to Cabramurra contact was made through VK1RGI with VK1ZAS/M and VK1AOP/M, both in Canberra.

Later in the evening, after return to Cooma, a check was made from the hill overlooking Cooma railway station and contact was made through VK1RGI with VK2ZWQ at Bundanoon.

From Cabramurra to Mount Ginini is 55km and from Cooma 81km.

Next morning a further check was made from the hill in Cooma and contact through VK1RGI was made with VK1AOP/M Canberra, VK2DO/M Yass, and later, with VK5OZ/M between Goulburn and Yass.

So, once again, amateur radio added to the pleasure of a holiday, not only by reason of the contacts made through a normally remote repeater, but particularly by the unexpected meeting of a friend and fellow amateur, and the unusual contact it provided. If you have portable gear take it with you on holidays; it can provide many pleasant surprises, as well as increasing your knowledge of repeater performance and serving as a valuable aid in case of emergency.

NOVICE LICENCE COURSE

The Novice Amateur Radio Group of New South Wales will hold a course to prepare candidates for the May 1980 P&T Dept novice licence exam. Classes will be held at the Wireless Institute Centre, 14 Atchison Street, Crows Nest, each Saturday afternoon at 1.00pm, commencing Saturday 2nd February, 1980.

The course will include lectures on theory and regulations, Morse Code in-

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AMATEUR RADIO

by Pierce Healy, VK2APQ



Finish of WARC 79 — how the amateurs fared and the likely scene for the 1980's

WARC 79 has come and gone and, while many of the details have yet to be worked out, and may take some time, the overall picture should be one of optimism. Several new HF channels have been tentatively allocated, there appear to be no serious losses, and there has been some rationalisation of the Morse code requirements.

Although there have been some authoritative statements up to the time these notes were being compiled (mid December 1979), there is still a lot of work to be done by delegation members on behalf of their national administrations. The impact of footnotes to various regulations in the final document, inserted to meet requirements of individual nations, will need careful study. The full implementation of the decisions may be a continuing process for some years.

In general, it appears that amateur radio has retained its status as an international communication service, and will continue to be available to those who have the necessary technical qualifications.

One of the major decisions was to retain the Morse code requirements for amateur licenses in the HF band. However, the regulation has been brought into line with the technical demarcation point between HF and VHF at 30MHz; instead of 144MHz as previously.

A report from the federal president of the Wireless Institute of Australia, Dr David Wardlaw, VK3ADW, (an accredited member of the Australian delegation at Geneva) was broadcast over WIA stations in New South Wales. It contained these points.

- There were no losses to existing frequency allocations in the HF bands.
- Three new HF bands have been created: 10.100MHz to 10.150MHz, with amateur as secondary to fixed commercial primary service; 18.068MHz to 18.168MHz and 24.890MHz to 24.990MHz, as amateur

and amateur satellite primary service.

- 50.00MHz to 54.00MHz remains as an exclusive amateur band in regions II and III. However, there are many footnotes for countries in region III which refer to broadcasting.

- 144MHz to 146MHz remains an international amateur and amateur satellite allocation. In region III 146MHz to 148MHz is shared with commercial fixed and mobile services on an equal basis. In effect this means the band was retained by accepting sharing, despite extreme pressures. This does not mean that sharing will be introduced into Australia, although other countries will.

- Although there was pressure on the 70cm UHF band, footnotes resulted in no losses to Australian amateurs in the 420MHz to 450MHz band.

- The 1215MHz to 1240MHz band was lost to make way for a global radio navigation service. However, there is a footnote for 1260MHz to 1270MHz for earth to amateur satellite communication.

- In the GHz range several additional bands have been made available for amateur satellite communication.

- There are also other favourable changes to the amateur satellite service.

It is beyond doubt that the amateur service was admirably represented by the International Amateur Radio Union delegation, which co-ordinated the views of amateurs expressed through their national amateur radio societies. Also by amateurs representing national societies who were accredited members of their countries' official delegations.

ITU NEWS

From the International Telecommunication Union in Geneva it is reported that WARC 79 completed 74 days of work on 6th December, 1979. The new Radio Regulations will come into force on 1st January, 1982.

No less than 894 plenary meetings or meetings of committees and working groups were held, without counting the large number of smaller meetings.

One point of interest is that the conference recommended that the administrative council should consider, from 1990, whether it is necessary to convene a World Administrative Radio Conference for the general or partial revision of the Radio Regulations.

A number of other points were noted, several of which are expansions on the points made in Dr David Wardlaw's summary.

The conference allocated frequency bands on the basis of the three regions defined in the existing Radio Regulations. However, it considered that the present divisions, dated back to 1947, no longer fully met the requirements of all countries. It therefore requested the CCIR to study a possible revision of the division of the world, for frequency allocation.

Fifty three radio services have been allocated frequency bands between 10kHz and 275GHz, which gives some idea of the need for world-wide co-ordination if these services are to function satisfactorily.

A new band has been allocated exclusively to the amateur service between 1810kHz and 1850kHz in Region I, and between 1800kHz and 1850kHz in Region II.

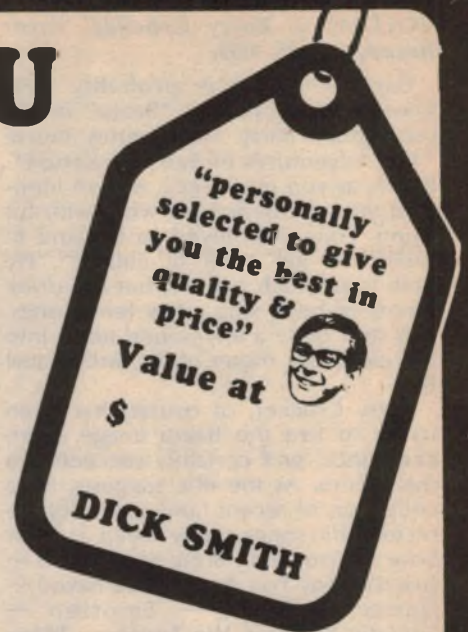
A new footnote (details not given) was added to the table covering the use of bands allocated to the amateur service between 3.5MHz and 144MHz in the event of a natural disaster. The amateur service was given an exclusive allocation between 3500kHz and 3750kHz in Region II.

In the section dealing with amateur

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BARRY CROCKER SINGS THE HITS — VOLUME 2. Barry Crocker. Astor Records. ALPS 1059.

Barry Crocker is probably best known for his role as "Bazza" in the outrageous Barry Humphries movie "The Adventures of Barry McKenzie". Bazza, as you may recall, was an innocent young colonial lad who, with his Aunt Edna, journeyed to England in order "to get a bit of culture". He didn't get much culture, but did drink plenty of beer, sing a few lewd songs, and stuff quite a few pound notes into the electricity meter of his Earl's Court flat.

Barry Crocker, of course, has been trying to live the Bazza image down ever since, and certainly succeeds on this album. As the title suggests, it's a collection of recent (and some not-so-recent) hit songs: How Deep is Your Love — You Don't Bring Me Flowers — Just the Way You Are — Blue Bayou — Dance With Me — Emotion — Sometimes When We Touch — Three Times A Lady — Too Much Heaven — Kiss You All Over — MacArthur Park — Can't Smile Without You — You Needed Me — Higher and Higher.

In summary, an album that Barry Crocker fans definitely should not miss. Recording quality is good, with negligible surface noise. (G.S.)

GUITAR SPECTRUM. Guitar Spectrum. Astor Records Pty Ltd. SPLP 1570.

Maybe I've missed something but, as far as I'm concerned, the treatment of the titles on this album is rather heavy handed. Even those titles that are familiar are difficult to recognise at times, although one doesn't doubt that the musicians making the sounds are all

very clever. The best advice I can offer is to listen before buying.

The titles: Don't Cry for Me Argentina — Fields — Fascinating Rhythm — Etoile — Norwegian Wood — Scarborough Fair — Heigh Ho — Nauges — Lisbeth — Jesus Christ Superstar.

Recording quality is generally quite okay but with some surface noise on side two. (G.S.)

KEVIN BORICH EXPRESS ... LIVE. Kevin Borich. Avenue Records L 37139. Festival release.

This live album was recorded at Bombay Rock, Melbourne; Mount Pleasant Leagues Club, Wollongong and Parramatta Jail.

Seven of the nine tracks were composed by Kevin Borich, including a new version of the La De Das classic, "Gonna See My Baby Tonight".

The nine tracks on the album are: Not Fade Away — The Place — Going Down Town — Little Red Rooster — Gonna See My Baby Tonight — Bellhop Blues — K.B.'s Boogie — Good To See You Again — Going Somewhere. (D.H.)

DANCIN' IS MAKING LOVE. Gap Mangione. A&M L 36965. Festival release.

If Disco is your scene, this disc will no doubt find favour with your ears with six lengthy tracks, mainly in that idiom.

Dancin' is Makin' Love — Girl Good-bye — Takin' It Back — You're The One — Dreamflow — I'm Home.

The quality is what one has come to expect from A&R records, bright, clean and with a good stereo image. If you are planning a dance party this would be a good starter. (N.J.M.)

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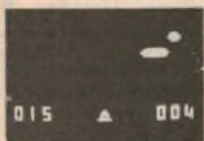
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RECORDS & TAPES — continued

of two discs, one by a veteran of the local theatre circuit, the other by one of the younger generation of Australian organists.

Playing his own electronic Conn organ, Reubert Hayes offers: Beyond The Blue Horizon — Spanish Eyes — Kismet Selections — Stranger On The Shore — Swanee — Old Comrades March — Estrellita — Begin The Beguine — My Way — I Don't Know How To Love Him — We'll Meet Again. It's pleasant organ, all in the traditional theatre organ style.

The second album was originally reviewed in June 1976 and, on that occasion, I rated it as a most entertaining performance of wide potential appeal. Ray Thornley relies heavily on over-recording and arrangement to produce a one-man orchestral effect quite distinct from the Reubert Hayes style. The program: That's Entertainment — Great Race Selection — Tara's Theme — In The Mood — Brother Sun, Sister Moon — The Old Piano Roll Blues — The Holy City — Duelling Banjos — March Militaire — Killing Me Softly With His Song — Anchors Aweigh.

In summary, "Blue Horizon" has mainly nostalgic appeal; Ray Thornley offers a more up-to-date style and treatment. The albums are priced at \$4.00 each including pack and post, or \$7.00 posted for the two. Only from Parker Recordings, 9 Carmel Place, Winston Hills NSW 2153. (W.N.W.)

HOW GOOD IS YOUR HIFI SYSTEM?

— and what about your ears?



STEREO TEST RECORD, "Stereo Review" Model SRT-14, for home and laboratory use. (From M.R. Acoustics, PO Box 165, Annerley, Qld 4103).

When I set about to review this record, I immediately gained the impression of "having been there before". Checking back, I realised it was an up-date of an earlier test record also sponsored by the American "Stereo Review" magazine, model SR12. It was reviewed in these columns in March 1978.

As in the earlier disc, side one is occupied by tracks which will allow an enthusiast to assess his hifi system overall, by careful listening and without resort to test equipment.

As before, bands one and two provide half-octave warble tones between 20Hz and 20,480Hz, which allow the listener to judge the extent and balance of frequencies which are getting through the system and through his/her ears — the last named being a likely problem for the over 40s!

Succeeding tracks on side one permit a subjective evaluation of channel separation, cartridge tracking across the spectrum, channel balance using wide-band noise, speaker phasing, hum and rumble content, and turntable wow and flutter. A booklet explains what to do and what to look for.

Side two is intended more for the laboratory and includes a 40kHz separation test for CD-4 characteristics, L&R response sweep from 500-20,000Hz, a 500Hz square wave, tone burst, intermodulation check, anti-skating adjustment signal, 1000Hz reference tone at four stated levels, 3120Hz flutter and speed test signal, and gunshots to test stereo spread.

As before, a handy disc to have around. (W.N.W.)

DEVOTIONAL: Choral — brass & organ — rock beat

THE PSALMS OF DAVID. VOL 3. The Kings College Choir, Cambridge. World Record Club Wrc QR 03476 Quadraphonic.

This is part of a series of Liturgical music in the best Anglican tradition, released over a period by the World Record Club, and featuring one of the world's best known and best disciplined Church choirs. The record has been recorded in Quadraphonic technique but, played on stereo equipment, it provides a delightful reproduction of the ambience of a big church. The psalms, in the order they are sung, are: 93-94-49-107-45-37-53-130-131. The cover notes give an interesting account of how the uses of the Psalms has changed and evolved over the centuries, plus biographical notes of the arrangers. (N.J.M.)

☆ ☆ ☆

NUTSHELL, "BEGIN AGAIN". Myrrh records MSB-6513. (From Ward Records Aust, 18-26 Canterbury Rd, Heathmont, Vic 3135.)

A very fresh "now" sound would be the best description of this collection of 10 gospel songs with a decided rock accent. The three singers, Mo McCafferty, Annie McCaig and Paul Field have somewhat "mid Atlantic" accents but their treatment of the following titles leaves no doubt as to where their hearts lie: Love With No Limit — Don't Let Me Fall — Caroline — In The Father's Hand — Starry Eyed And Laughing — First Snow — Take Me Down — Stay Close — The Dancer — Heaven In Your



Heart.

A liner sheet with the record carries the thought provoking lyrics and photos of the three singers. The sound quality is really excellent. (N.J.M.)

☆ ☆ ☆

HYMNS FOR BRASS AND ORGAN. Harry Mortimer and the Cathedral Brass; Michael Austin, organ. Stereo, World Record Club WRC-R-02982.

In terms of content, there is quite a feast here for those who like traditional

hymn tunes, identified both by the theme title and by the tune: "Crimond", "Horsley", etc.

There are 15 in all: Praise My Soul — The Lord's My Shepherd — Mine Eyes Have Seen The Glory — There Is A Green Hill — Alleluia, Sing To Jesus — Silent Night — And Did Those Feet — Ye Holy Angels Bright — Once In Royal David's City — Thou Whose Almighty Word — Abide With Me — The Day Thou Gavest — O Thou Who Camest — Rock Of Ages — Who Would True Valour See.

Recorded in the De Montfort Hall, Leicester, England, the brass is much more evident than the organ. For all practical purposes it could as well be titled "Hymns For Brass".

From a Polydor original, I would judge it to be a fairly old recording that "gets by" — without being notable either for sonic definition or musical enterprise. Still, its presence in the WRC catalog indicates a continuing appeal as a collection of time-honoured hymn tunes. (W.N.W.)

FOU TS'ONG PLAYS CHOPIN — continued

Fou Ts'ong stands revealed as possibly the most lyrical of Chopin's current followers.

The Chinese pianist's approach can best be observed by direct comparison with some of his predecessors; in the sonata, I have chosen Malcuzyński, generally acclaimed in recent decades, to serve: from the very start, it is clear that Fou Ts'ong employs a much lighter touch, eschews solid drama and manages to imbue even the sombre Marche Funebre with considerable lyricism. His musicianship is firm and reasoned, nowhere more so than in the

erie Finale which he invests with a fluttering of bats' wings.

For the Fantasy and Etudes, I chose Arrau's recordings for comparison. There is, in the Fantasy, little to choose between the two versions; Arrau is a little more dramatic and employs a more relaxed rhythm here and there, but the differences are not very marked ones. The Nouvelles Etudes are another matter, though; where Arrau is a little perfunctory and seems to regard the D flat major Etude, with its simultaneous use of staccato and legato as a bit of a bore, Fou Ts'ong reveals even these works to be quite lovely music, delightful to the listener and, presumably, to this pianist. The rarely-heard C minor march is beautifully played, with delicacy and a feeling of gentle resignation. The recorded sound is, on the whole, very good and the disc is highly commended. (P.F.)

☆ ☆ ☆

CHORALE VARIATIONS: Peter Hurford at the organ of Our Lady of Sorrows Church, Toronto, Canada. World Record Club stereo, R 05871.

Lovers of baroque organ music won't want to miss this one. A WRC re-release of a recording made in 1976 by Decca, it features well-known organist Peter Hurford at the delightful neo-classical two manual Casavant Freres organ at Our Lady of Sorrows Church in Toronto. Not only that, but he plays some really enjoyable baroque music.

The first piece is John Bull's Revenant, a set of chorale variations on the old German drinking song More Palatino. Then follows Buxtehude's Chorale Fantasia on the hymn How

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Dowd) has not a single first-rate mature tenor of Australian provenance. This, then, is a disc to enjoy, but I suggest you do not send it to discriminating opera-lovers abroad. (P.F.)

☆ ☆ ☆

BEETHOVEN: Piano Concerto No. 3 in C minor, op. 37. Maurizio Pollini, piano; Vienna Philharmonic Orchestra; conductor Karl Bohm. DG Stereo disc 2531 057.

There is a pretty general consensus among the world's music-lovers that Pollini is one of the great pianists and musicians of our time; I have heard him on disc and live and, although I had some reservations earlier in his meteoric career, I now wholeheartedly subscribe to the above consensus. As might be expected, his interpretation of this Beethoven concerto is authoritative, sensitive and very beautiful.

Despite the obviously first-rate performance, first listening to this record left me a little dissatisfied. I recalled some rather strange occasions of recent years when Bohm, noticeably ageing, had adopted uncommonly slow tempi; I listened again, compared the performance with older, excellent ones, by Solomon and by Schnabel, employing tried and reliable conductors and found that there's nothing sluggish about Bohm's tempi: total performance times are almost identical for Pollini and Schnabel while Solomon (with conductor Menges) took about 1½ minutes longer.

After repeated checks, I have concluded that there is some slight, but consistent, lack of communication between soloist and conductor — they simply did not take the same view of many little details; also, the recorded orchestral sound, while good, is not as clear and precise as I might have wished.

To me, then, this disc is just a bit short of what it ought to be: the conductor not entirely fair to the soloist and the recording technicians not quite fair to what is still one of the world's best orchestras. (P.F.)

☆ ☆ ☆

ISADOR GOODMAN PLAYS CHOPIN.

Etudes in E major, op 10 No. 3, C minor, op 10 No. 12, A flat major, op 25 No. 1; Mazurka in B flat minor, op 24 No. 4; Nocturne in F major, op 15 No. 1; Polonaise No. 6, A flat major, op 53; Waltz in E flat major, op 18; Ballade No. 3, A flat major, op 47; Berceuse in D flat major, op 57; Scherzo No. 3, C sharp minor, op 39. Philips stereo disc 6508 004. (Also available on cassette.)

This Chopin recital was recorded to mark Goodman's 70th birthday and it is a fitting tribute to a musician who, over many decades, has contributed a great

A NEW "1812" — Telarc cuts loose with the guns!

TCHAIKOVSKY: 1812 Overture; Capriccio Italien; Cossack Dance from Mazeppa. Cincinnati Symphony Orchestra conducted by Eric Kunzel. Stereo, Telarc DG-10041. (From P. C. Stereo, PO Box 272, Mt Gravatt, Qld 4122.)

With this album comes a leaflet advising caution during the first playing, in case the extreme groove excursions should upset the cartridge, the amplifier, or the loudspeaker system. Look at the grooves carrying the cannon shots and you'll see why.

By all means follow the advice but don't be surprised if a first cautious playing robs the performance of its vitality. It will almost certainly drop the level of the soft passages down into the ambient noise of an average suburban on-street dwelling — such is the dynamic range.

A second playing, with the gain turned up to the safe limit should correct any such reservation, although I still felt that the microphone placement could have captured a little more ambience and a little more spread.

But the recording is nevertheless very quiet and very clean and, when the

bells and particularly the cannon shots are heard — the result of a computer controlled digital mix — that is where the quality really stands out. What tends to degenerate into noise-on-noise in some other versions emerges here as a series of incredibly clean and gutsy transients, that literally shake the house.

On side 2 "Capriccio Italien" is an appropriate and familiar coupling, with Cossack Dance from "Mazeppa" providing, between them, another 20 minutes of clean, vibrant sound.

Mastered on a Soundstream digital system and processed in Germany, the disc comes in a double-fold album with notes on the system, the music and the conductor and orchestra. This is another superb album. (W.N.W.)



Available also on cassette

deal to Australia's cultural life. The periods during which he was most widely known were the pre-war years, when he appeared regularly in Sydney's major movie theatres, giving audiences far better music than they were used to; and, later, touring army camps all over the place, introducing many a soldier and airman to the delights of Chopin, Liszt and Schumann.

In terms of today's virtuosi, Isidor Goodman is, of course, a very minor figure; no amount of affection can blind us to that. All the same, even at 70 he can still produce a seductively enchanting sound and his sure touch seldom deserts him. As in earlier days, Goodman shows at his best in music of a strongly romantic cast: on this occasion, the "Aeolian Harp" Etude from opus 25 receives a fine and delicate reading, as good as I've yet heard. The same goes for the Berceuse, even though he is easily tempted into tempi

that are just a trifle too fast for the most thorough enjoyment of the music. Again, in the Nocturne and the slow sections of the Ballade, I find Goodman thoughtful and quietly sensitive, playing with a lovely sense of contemplation that Chopin is rarely accorded.

In fairness to those who may not be familiar with Goodman's work, some shortcomings cannot be glossed over; the Mazurka is decidedly bumpy, the Waltz is, to my taste, too fast and full of oompapah and there are, here and there, signs of flurry in the faster runs. They are blemishes, but not of a major kind and not such as would spoil one's enjoyment of the record. The quality of the sound, recorded in an ABC studio, is very good and the record surfaces are quiet. (P.F.)

☆ ☆ ☆

FOU TS'ONG PLAYS CHOPIN: Sonata No. 2, B flat minor, op. 35; Fantasy F minor, op. 49; Trois Nouvelles Etudes, op. posth.; Funeral March in C minor, op. 72 No. 2. Odyssey stereo disc ODA 5134.

As I indicated in my review of the Chopin Nocturnes, Fou Ts'ong has suddenly emerged as an authoritative interpreter of this composer's music; this is the more surprising as this pianist, by no means a newcomer, was previously known almost exclusively for his playing of Mozart. Just as he played Mozart's music with the cleanest of classical attention, so now



REVIEWS OF RECENT

Records & Tapes

CLASSICAL ● POPULAR ● SPECIAL INTEREST

John Mack, oboe: "utterly musical"

SCHUMANN: Three Romances, op. 94; BRITTEN: Six Metamorphoses after Ovid, op. 49; SAINT-SAENS: Sonata op. 166; PALADILHE: Solo de Concert. John Mack, oboe; Eunice Podis, piano. Telarc (US) stereo disc 5028 (From PC Stereo, PO Box 272, Mt Gravatt, Qld, 4122).

John Mack's name was familiar to me — the leading oboist in the Cleveland Orchestra and the most widely acclaimed of Tabuteau's students ought to be worth hearing. In the event, his playing far exceeded my expectations; it is no small matter for the oboe never to appear excessively penetrating and utterly musical in every phrase: yet, these are Mr Mack's achievements.

Schumann's op. 94 was certainly composed for the oboe and sounds delicious when played on it; I had not heard it on disc since the days of Leon Goossens. Too often, live or on disc, it is played by flute, violin, even clarinet — good to have the real thing for once. Britten's Six Metamorphoses, written in

1951, is one of the composer's most successful essays with an unaccompanied voice; far from sounding thin or obsessive. Britten's musical line is ideally realised in one of the happiest of his works.

The sonata by Saint-Saens, written in 1921, is another piece which shows a composer at his most skilful and best. The three concise movements are utterly delightful; this is remarkably fine chamber music, quite unjustly neglected. If Emile Paladilhe's name seems unfamiliar, don't worry: although he appears to have been quite a prolific composer (he died at 82 in 1926), no other work of his graces the catalogue. The piece heard here was written as a virtuoso showpiece and that's what it is — melodic, quite charming, fiendishly difficult and brilliantly played.

Special mention must be made of the outstanding quality of recorded sound on this record from Cleveland — sound worthy of the magnificent playing and, on the whole, very fine and unusual music. (P.F.)



Destino, Il Trovatore and Don Carlo; the bass and the contralto are heard twice each, the soprano gets three showings and the baritone — overworked as is usual — is heard on four tracks. Of the four artists, Lauris Elms is probably the only one whose experience in the concert hall and recording studio is as extensive as her operatic stage work; this may well be the reason why she, alone of the four, performs here as freely and unembarrassedly as if she was in a full operatic performance.

As far as singing goes, all four artists are excellent, even though Mr Allman shows some slight strain at the top of his range. The singing is fine, but it simply is NOT opera. The artists are hampered by the absence of familiar coprotagonists as well as by an unfamiliar conductor and orchestra; worst, they seem, each one of them, to be struggling against uncommonly slow tempi which tend to negate every genuine dramatic effort.

Of the pieces included, I was mystified by the Rigoletto scene described as a Duet between Rigoletto and Sparafucile — it does seem a bit odd! The things that are wrong can most strongly be observed in the Willow Song: Miss Carden sounds quite glorious in the gentle and tender sections, but of real drama there is no trace.

The members of the SSO, wherever there is something to get their teeth into, perform quite splendidly and, as I said, there is a great deal to enjoy on the record. That such a disc should be made without the participation of a tenor is, of course, rather ridiculous. However, as anyone who subscribed this season will know, the company presently (and since getting rid of Ron

Australian Opera: A disc to enjoy — but ..

STARS OF AUSTRALIAN OPERA SING VERDI. Joan Carden, soprano; Lauris Elms, contralto; Robert Allman, baritone; Neil Warren-Smith, bass; The Sydney Symphony Orchestra; conductor Eric Clapham. ABC stereo disc AA 9059.

This disc should have been one any of us would be proud to send abroad as a Xmas gift and as proof of the Australian Opera's high standards. To be sure, there are some glorious sounds on the record and there is quite a lot to be proud of — including first-rate recording technique, decent acoustics and a well-compiled set of notes in a

sleeve which shows John Coburn's "Curtain of the Sun" for the Opera Theatre stage. Alas, the disappointments almost outweigh all these fine things!

The music, nine tracks, is taken from seven Verdi operas: two items each from Traviata and Rigoletto, one each from Nabucco, Otello, La Forza del



Reviews in this section are by Paul Frolich (P.F.), Neville Williams (W.N.W.), Jamieson Rowe (J.R.), Leo Simpson (L.D.S.), Norman Marks (N.J.M.), Greg Swain (G.S.), and Danny Hooper (D.H.).



Letters to the editor

Cigarette advertisements

I wrote to you on August 16 protesting at the inclusion in that month's issue of a "foreign matter" advertisement in a publication I had purchased as a specialist journal since its inception (as Radio and Hobbies) in 1939.

I feared I was a lone voice crying in the wilderness but was heartened by the reply I received from the then editor Jamieson Rowe.

I was saddened to read his farewell leader in the November issue and to note the inclusion in that issue, and that of December, of the offensive (to me) advertisement.

As this now seems to be confirmed policy, I have no option but to express my disapproval in the only manner now open to me — the transfer of my subscription to your competitor. Their December issue, at least, does not carry any such extraneous advertisements — something I would have thought axiomatic in such a journal.

In closing I must say that I find it incredible that I was the only one to protest in writing (at least no other letters were published).

Chas Fletcher,
Toongabbie West, NSW.

COMMENT: We were naturally very sorry to see Jim go, but wish him well in his new position. We too, would be happier without "extraneous" adverts but they are legal and the result of an overall space booking involving the parent companies.

Politicians & the press

I wish to congratulate you on your Editorial in the December 1979 issue of EA. Your comments are so accurate and so necessary that the item should be made compulsory reading for all media personnel and for all politicians.

To show my reaction to the present situation, and to support your statements, I would point out that I no longer buy any of the daily newspapers and only subscribe to those technical or semi-technical publications which are reasonably factual in approach. My own experience over the years, whenever I have been involved in a newsworthy matter, is that the press is

incapable of accuracy, even when an accurate report might be stimulating to sales. The record was one item which had 23 fundamental incorrect statements in one short report.

Your comments regarding the political scene are also valid. During periods of regular car driving I used to listen to the broadcast of our national Parliament, not to become well informed, but as a form of amusement akin to Amos and Andy.

With rare exceptions, the utterances of our representatives would have brought scorn on a third form debating team at school.

Perhaps if enough citizens indicate to the news media that dramatic, inaccurate and misleading reports are not what is desired by thinking people, and perhaps if enough politicians are made aware of the low level of esteem in which they are generally held, we may have some improvement. If you have sufficient response to your Editorial, perhaps circulation of that copy and the supporting letters should be made to those whom we have criticised.

J. M. Swan,
Girraween, NSW.

Nuclear power & the December editorial

I found your editorial in the December issue of "Electronics Australia" somewhat disturbing.

You state that "truth itself is being sacrificed to personal and political point scoring" and quote examples of pressmen asking for guarantees of safety from a Lucas Heights' spokesman. Perhaps their questions and the scepticism of government agencies can be condoned in the light of the following:

(1) At the 1972 AEC hearings on emergency core cooling in US reactors, interventionists Cherry and Ford were continually misled and misinformed by the AEC as to the recommendations of a scientific group, included in a manuscript known as the Brockett report.

The Brockett report showed that emergency core cooling has not been developed to a level where it would work reliably; but the AEC was being pressured by the manufacturers — and hence fought to have the report excluded from evidence, claiming that emergency core cooling was a reliable and well developed technology.

Cherry and Ford subsequently exposed this deceit and reactor orders fell from 1000 to 200.

(2) In Australia, Queensland Mines' submission on water management in the proposed Northern Territory uranium mines used rainfall figures from 1962-69 — inordinately dry years. The figures from 1970-77 indicated that leaching of tailings could be a very real problem indeed.

The Queensland Mines submission was accepted as proof of safety by government agencies.

(3) At the site of the Shippingport nuclear plant in Pennsylvania, a survey of local health was undertaken by the National Utilities Corporation. The figures that emerged showed that the child mortality rate was more than double the state average. They showed that there is more than twice as much leukaemia, and that in 1970 — the year of highest infant mortality — the level of Strontium 90 in milk at local dairies reached an all time high.

When considering these findings, frightening enough in their own right, one must take into account that, in the opinion of the AEC, the Shippingport complex was one of the industry's safest and that all the radition levels recorded and encountered during the health survey were within the recommended levels set by the Australian AEC.

(4) The "no-one has ever been killed by a nuclear power plant" argument is one of the greatest dupes.

After the recent death from leukaemia of one of the Lucas Heights workers due to a sudden and accidental blast of radiation, the AAEC quietly settled out of court with the widow. This takes a little of the sting out of the "white as snow" front of the industry.

Furthermore, death from radiation overexposure is a very slow process, and information about the long term health of workers in the industry is difficult to obtain. This is mainly due to the fact that medical records of employees have not been kept for any significant time (15-20 years) in any nuclear institution in the world.

The "spirit of honest enquiry" is indeed a casualty of our present era, but I would suggest that, in the light of the foregoing, this spirit has been quashed by the protagonists of nuclear power; not, as your editorial suggests, by those who oppose it.

When the lure of the dollar is subtracted and when people recognise the fact that waste disposal, reactor integrity and other critical issues have not been solved, perhaps then the humbug will be allayed.

Martin Levins,
Wahroonga, NSW.

COMMENT: The December editorial was neither pro nor anti-nuclear. Its thrust was against emotional, sensational and political verbage, as distinct from reasoned debate and consensus.

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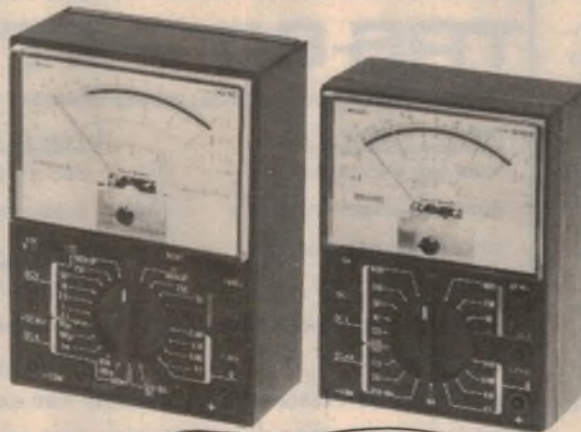
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Voltage Drop 100 mV /250 mV

A.C. VOLTAGE
Full Scale Value 10/50/250/500/1000V
Accuracy ± 3% of rated value
Internal Resistance 10,000Ω/V

A.C. AMPERAGE
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Internal Resistance 30,000Ω/V

D.C. AMPERAGE
Full Scale Value 50μA/2.5/25/250mA/10A
Accuracy ± 3% of rated value

A.C. VOLTAGE
Full Scale Value 10/50/250/1000V
Accuracy ± 3% of rated value
Internal Resistance 13,500Ω/V

A.C. AMPERAGE
Full Scale Value 10A
Accuracy ± 4% of rated value

RESISTANCE (OHMS)
Full Scale Value 5k/50k/500k/5mΩ (Rc 50Ω)
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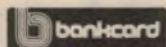
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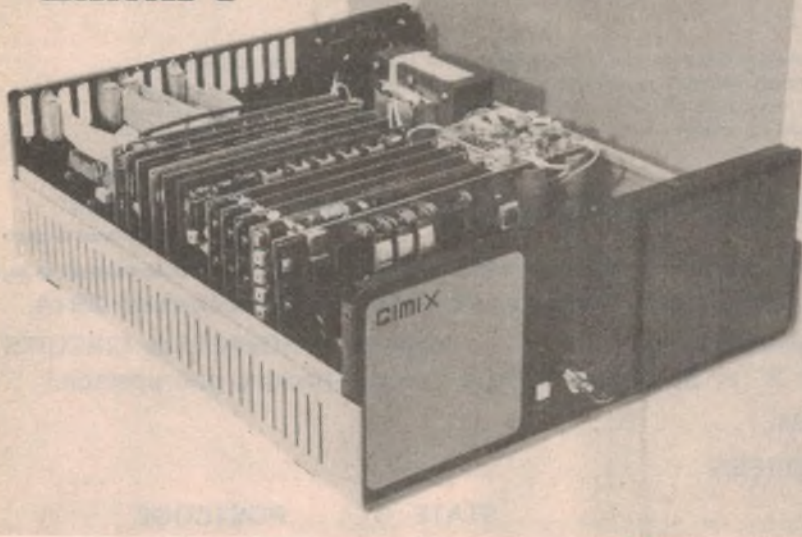
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Gimix Inc of the USA have just announced their new System 68 6800-based microcomputer system.

The system is SS-50 bus compatible for both hardware and software. The system is video based, the high speed of the Gimix video board filling the screen instantly. It is limited only to the entire systems software limits, whereas a terminal limits the user to the intelligence of the terminal.

The system also features the Gimix-bug resident operating software. The monitor ROM is installed on the CPU board and features all the standard utility routines found in other MIKBUG compatible systems.

A video board, GMXBUG, a parallel keyboard, and a video monitor give you a complete video based system. No terminal is required.

Further system backup is provided in

the form of additional boards that can be fitted to the system by plugging into the mother board. These include — 16K and a 32K static memory boards, 8K PROM boards, and 4K PROM programmer and duplicator boards.

Gimix also offer a range of serial and parallel I/O boards, as well as special relay driver boards for AC mains interface and control.

Further information can be obtained from the Australian distributor, Paradio Electronics, 7a Burton Street, Darlinghurst, NSW 2010. Telephone (02) 31 3273.

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Microcomputer News & Products

200mm floppy disk systems, and a 16M byte hard-disk system.

Price for the basic 8K system is \$560 plus 15% sales tax where applicable. The system is in kit form but can also be purchased as a fully assembled unit for \$660 plus 15% sales tax.

The system is available from South West Technical Products Corporation, 7a Burton Street, Darlinghurst, NSW 2010. Phone (02) 31 3273.

STEWART ELECTRONICS MOVE

As from 1st February 1980, Stewart Electronics will be moving from their current Mount Waverley address to much larger premises at 44 Stafford Street, Huntingdale, Vic.

The new phone number is (03) 543 3733 and the telex No. is 36908.

TEXAS FLOPPY-DISK CONTROLLER

Texas Instruments has just announced the release of a new floppy-disk controller that is compatible with their series of TM990 microcomputer board products.

The board, designated TM990/303, supports up to 4 double-sided drives and features programmable stepper-motor rates and data transfer format.

In addition the board also features write precompensation, 125mm or 200mm diskette compatibility, soft sec-

tor compatibility, internal phase acquisition and address mark detection.

For further information contact your nearest Texas Instruments distributor.

TROUBLESHOOTING AND DEBUGGING MICROS

Hewlett-Packard have released a specially written application note for designers and users of microcomputer systems.

The 16-page booklet, "Microcomputer Analysis Techniques Using Logic Analysers", includes theory and examples of procedures for software evaluation, code optimisation, performance analysis, and troubleshooting complex digital systems. Listed as Application Note 292 (publication number 5953-2704), the booklet is available from Hewlett-Packard free of charge.

Further information can be obtained from Hewlett-Packard Australia Pty Ltd, 31-41 Joseph Street, Blackburn, Victoria 3130. Phone (03) 89 6351.

NATIONAL MICROCOMPUTER CONFERENCE

MICSIG, the Microprocessor Special Interest Group, are sponsoring a National Microcomputer Conference, the subject of which is "Personal Computing In The Eighties". Interested parties are invited to submit papers which should be pertinent to the Personal Computer scene.

Abstracts should be forwarded to: Microcomputer Conference, Subcommittee, MICSIG-Canberra, PO Box 446, Canberra City, ACT 2601.

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ternal components for interfacing and incorporates 2K bytes of ROM, 128 bytes of RAM, two timer/counters, 5 interrupts, and 32 I/O lines. This complete minimum system dissipates only 100mW.

Other new products announced by National include an ECL 256-bit RAM, the DM10414, with typical access times of only 7 nanoseconds and three new Maxi-ROMs. The three new devices are 16K, 32K and 64K chips that have maximum access times quoted at 450ns. All three chips operate from a single 5V supply and dissipate a maximum of 1 watt.

Also available from National are two new intelligent floppy disk controllers. These have been introduced as part of their Series/80 family of microcomputer products. The boards can interface directly with a variety of standard mini-sized floppy-disk drives and can control up to four single and two double-sided floppy drives.

National's BLC-8201 is a single board replacement for Intel's two-board SBC 201 and requires 71% less power. The BLC-8221 is unique to National, and has buffered data transfer for system efficiency.

Further information of these products can be obtained from: NS Electronics, Cnr. Stud Road and Moun-tain Highway, PO Box 89, Bayswater Victoria 3153. Phone (03) 729 6333.

LOW COST LINE PRINTER



A low cost matrix printer with innovative features has been released on the Australian market. The Microtek MT80 offers three character widths of 5, 10 and 15 cpi, buffer sizes up to 4K byte and a choice of RS232, parallel and IEEE-488 interfaces. The microprocessor controlled unit has comprehensive self-testing software, and carries a full one year warranty.

Printing speed is 125 characters per second and multiple forms from 11.5cm to 24cm may be used. It has pin-feed drive, and will print an original and three copies.

The unit weighs 10kg and is housed in an attractive moulded plastic case 450mm wide x 376mm deep x 185mm high.

Reliability is quoted as one million hours MTBF.

For further information contact Image 10 Pty Ltd, 27/67, Queens Road, Melbourne 3004. Phone (03) 51 0671.

NEW SWTPC 6809 MICRO COMPUTER SYSTEM

The new system is very similar to the older SWTP 6800 system in appearance but is more powerful due to the greatly enhanced instruction set of the 6809.

The basic system consists of a 6809 CPU plus a 2K monitor ROM that is 2716 EPROM compatible. It provides 8K of memory (expandable to 56K) and features full buffering on all output lines.

The system also has built in multi-user capability, needing only the addition of extra I/O boards to operate a multi-terminal system.

The system is well supported with both software and hardware. Some of the software available for the 6809 includes the FLEX-9 operating system, a Text Editor, Mnemonic Assembler, Debug, Sort-Merge, BASIC, Extended BASIC, Multi-user BASIC and PILOT.

The range of peripherals available for the system includes Dot-Matrix printers, Daisy wheel printers, 125 and

MICRONEWS
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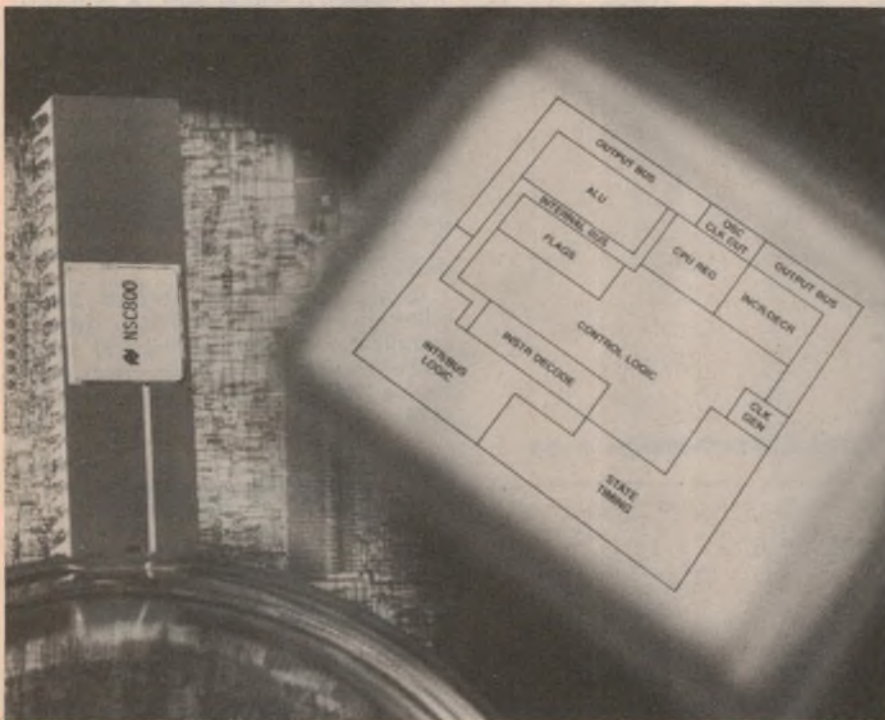
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Microcomputer News & Products



New microprocessor from National features Z-80 instruction set & Z80/8085 architecture



National Semiconductor have just announced a new range of products including a new microprocessor, the NSC-800. This chip combines the low power requirements of CMOS with the high performance of existing NMOS processors. The chip has a very interesting architecture in that it combines the best architectural features of the 8085 and the Z80.

It uses the address data bus structure of the 8085 and the register structure and instruction set of the Z80.

Two support chips, both dedicated memories (NSC810 and NSC830) incorporate on-chip logic to interface directly with the multiplexed bus. Combining the three devices results in an efficient design that significantly reduces chip count as well as power, without degrading system performance.

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```

1 P"ENTER COMMAND" P G35
2 L4096=Z P"ENTER NEW FILE" S44
3 AB TZ=8190 G33
4 MB>Z JZ TB:13 G1<
5 P"MEMORY LEFT="8190,Z-, "BYTES" LZ=Q G4<
6 P"ENTER DATA" P
7 L4070=C
8 AD
9 MD>C JC TD:13 G1<
10 P"SEARCHING" S44
11 P
12 L4096=Z
13 L4070=C TZ=Q G34
14 MB<Z MD<C
15 TB:D JZ TD:13 G2<
16 TD=13 G2>
17 JZ JC G3<
18 [Z
19 MB<Z
20 TB:42 [Z G1<
21 JZ
22 MB<Z
23 OB JZ TB:42 G1<
24 TF=2 G1
25 TF=3 L4070=C P G12<
26 TF=4 P"TYPE NEW LINE" [Z P
27 [Z
28 MB<Z TB:42 G1<
29 JZ MB<Z TB=42 G2>
30 AB MB>Z G1<
31 P"LINE FULL"
32 G1
33 P"MEMORY FULL" G1
34 P"END OF FILE="Z G1
35 L42=K MK>4095 IF
36 TF=1 G2
37 TF=2 G6
38 TF=3 G6
39 TF=4 G6
40 TF=5 LQ=Z P"ADD TO FILE" P"BYTES LEFT="8190,Z- P G3
41 MB<Z
42 TB:38 JZ G1<
43 LZ=Q G1
44 P"CALLSIGN NAME DATE RST" P R

```

```

G1
ENTER COMMAND
?5
ADD TO FILE
BYTES LEFT=3939
VK2XYZ FRED 23/3/89 594 *
MEMORY LEFT=3905 BYTES
ENTER COMMAND
?3
ENTER DATA
VK2XYZ
SEARCHING
CALLSIGN NAME DATE RST
VK2XYZ FRED 1/2/89 599 *
VK2XYZ FRED 23/3/89 594 *
END OF FILE=4285
ENTER COMMAND
?

```

Fig. 3 above is the full listing of the amateur log program while Fig. 4, at left, is a sample of its operation.

This is like command 2, except that program will print out all lines in current file containing the data. Is to allow altering an existing line file. Note that the new line must same length as the original. add to the current file. Each should be delimited by a asterisk as before.

If the file in memory is to be saved on cassette, the last character in the file should be an ampersand (&). This is required by the alternative start-up routine, in order to set up the end of file pointer when the file is re-loaded into memory. When a file has been re-loaded from cassette, start the program at line 41 instead of line 1, to ensure

that the end of file pointer is set up properly. Otherwise it will be ignored.

Note that searching a full 4K byte file can take up to four minutes. This is mainly because the Micro Basic interpreter is rather slow in operation — although Mr Leykam notes that his program may well be capable of improvement (it was his first programming effort).

Finally, a note regarding Micro Basic itself for the benefit of those who may not have seen the earlier story. Micro Basic is a tiny version of BASIC, written by Alan Peek for small 2650 microcomputer systems. The editor/interpreter for Micro Basic squeezes into a mere 1.6K bytes of memory, so that it can even run in systems with only 4K of RAM (although Mr Leykam's program will require a system with 7K of RAM).

As you may have deduced from the program listings in this article, Micro Basic achieves this remarkable economy by the use of single-character commands, reverse Polish notation and an efficient way of packing the source program into memory. Its unorthodox approach takes a bit of getting used to, but the ability to program rapidly even in small systems makes it well worth persevering.

A cassette of the Micro Basic editor/interpreter (in PIPBUG format) complete with instructions and a full source listing is available from Alan Peek at 10 Gale Street, Woolwich NSW 2110.

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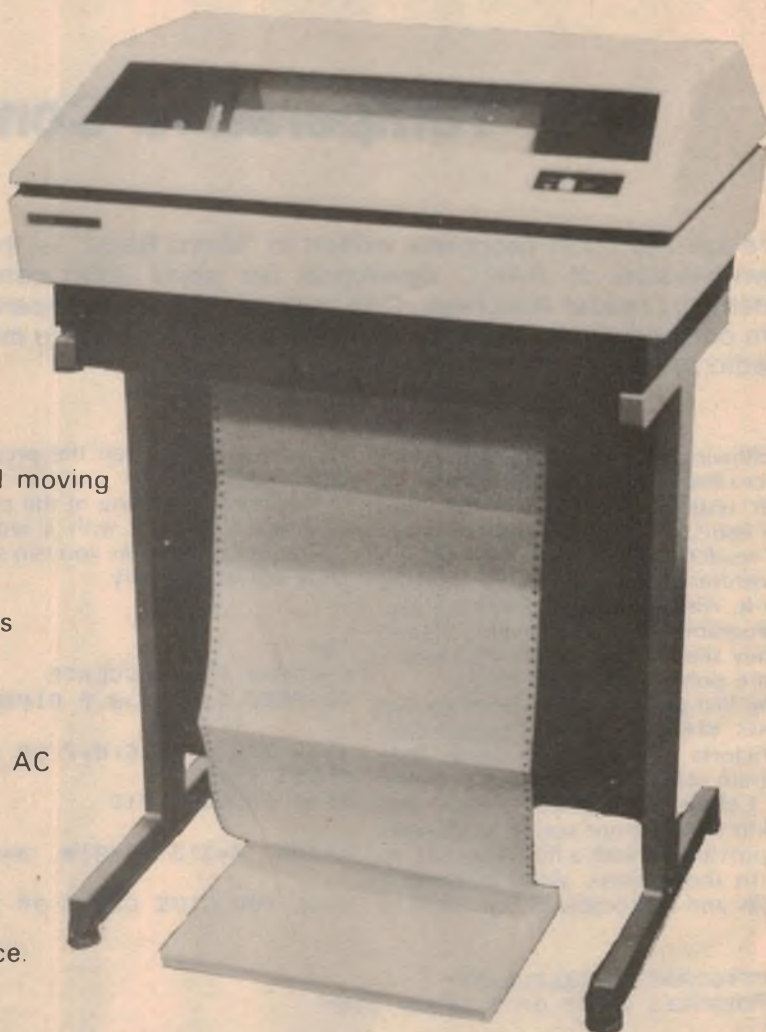
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Micro Basic Programs for 2650 systems

Temperature Conversion, Radio Log

Here are two short programs written in "Micro Basic" — the cut-down version of BASIC developed for small 2650 computer systems by reader Alan Peek. One program converts temperatures from one scale to another, while the other is a program to manage a radio amateur's contact log.

Following our review of Alan Peek's "Micro Basic" for small 2650 microcomputer systems, published in the April 1979 issue, it would seem that quite a few readers have obtained Mr Peek's interpreter and have been working with it. Already two readers have sent in programs they have developed, and as they seem likely to interest readers we are publishing details here.

The first program came from Mr Syd Brooks, of 6 Edgar Street, Ferntree Gully Victoria 3156. It is a simple little program which can convert between the Celsius, Fahrenheit, Kelvin and Rankin temperature scales. Mr Brooks has provided it with a little humour, to add to the interest, along with some checks and reprompts in the event of

an invalid entry when the program is being used.

The complete listing of the program is shown in Fig. 1, with a sample of operation in Fig. 2. As you can see, it is fairly self-explanatory.

```
G1
PROGRAM TO CALCULATE
DEGREES C,K,F OR R GIVEN ONE

WILL YOU GIVE C,K,F OR R? F
PRESS + OR -+
WHAT IS TEMP?212

C=100 K=373 F=212 R=672

WILL YOU GIVE C,K,F OR R?
```

```
1 P"PROGRAM TO CALCULATE"
2 P"DEGREES C,K,F OR R GIVEN ONE"
3 P
4 P"WILL YOU GIVE C,K,F OR R? " AA
5 TA:70,A:75,A:67,A:82 G1<
6 P"PRESS + OR -" AB TB=43 LI=X G3>
7 TB=45 LI=#X G2>
8 G2<
9 P"WHAT IS TEMP" IE LEX*=E
10 TA=70 G4>
11 TA=82 G4>
12 TA=67 G4>
13 TA=75 G4>
14 LE460+=R,R=E
15 LE460-=F,F32-5*9/=C,C273+=K,E=R G3>
16 LE273+=K,K=E
17 LE273-=C,C9*5/32+=F,F460+=R,E=K
18 TK<0 P"THAT'S IMPOSSIBLE STILL!" G3>
19 TC<40# P"THAT'S COLD!" G2>
20 TC>1999 P"GUESS" G3
21 P
22 P"C="C," K="K," F="F," R="R
23 G3
24 $A=C,F,K OR R B=SIGN E=TEMP$
25 $C=CELSIUS F=FAHRENHEIT K=KELVIN $
26 $R=RANKIN $
27 E
```

Fig. 1, at left is the full listing of temperature conversion program while Fig. 2 above is a sample of its operation.

The second program came from Mr Horst Leykam, of 165 Victor Street, Dee Why NSW 2099. Mr Leykam is a radio amateur, with the call sign VK2BHF, and explains that he wrote the program in an effort to produce a more elegant and effective way of maintaining and referencing his contact log.

What this program does is maintain a log of contacts, with each contact represented by callsign, the name of the operator contacted, the date and the readability/signal strength details. It allows you to add to the log "file" when each contact is made, and then to have an automatic search made for previous contacts with the same callsign. This lets you "refresh" your memory regarding the name of the operator, and the previous times that you exchanged calls.

A file can be expanded until it fills the allocated memory buffer space (hex 1000—1FFF, or decimal 4096—8191). As each entry is made to a file, the program tells you how many bytes of memory are left — in decimal. This allows you to save a file at any time on cassette tape, using the normal PIPBUG dump command, and then re-load it into the buffer later using the L command.

The program can search for either the first file entry matching the supplied data (typically the callsign), or for all matching entries. It also allows you to alter an existing file entry, providing the change will fit into the same space. This allows you to correct a previous mistake, when it is discovered.

A full listing of the program is shown in Fig. 3, with a sample of its operation shown in Fig. 4. When the program starts up, it immediately asks you for a command. You have five options, each command being represented by a single digit (1-5) terminated by a carriage return.

1 — Is to enter a new file. Each line should be delimited by a space and an asterisk.

2 — Is to accept a data entry (say the callsign), and search through the current file for a match. The first line found to contain the data will be printed out.

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"Trace" routine helps debug 2650 programs

When you're trying to debug a tricky program in assembly language, a breakpoint isn't always the answer — you can generally only call it once. Here is a "trace" routine for 2650 systems which can be rather more helpful. You can call it any number of times, and each time it is called it prints out the contents of all processor registers.

by JAMIESON ROWE

Like most small microcomputer systems, the 2650 Mini Computer provides only one debug aid: a pair of breakpoints, which are software implemented by the PIPBUG monitor program. These can be quite handy, but there are many occasions when they just don't help enough.

For a start, each breakpoint can only be used once. When it is executed once, PIPBUG replaces it with the original instruction. So you can't use the breakpoints to track down bugs which are inside loops, for example — the breakpoint disappears first time you go around the loop!

The other main drawback is that the breakpoint "runtime" routine simply saves the processor register contents in RAM, and then transfers control back to the PIPBUG command loop. So if you actually want to examine the registers, you then have to use the PIPBUG "see and set the registers" (S) command. This can be very tedious and time consuming when you have to use the breakpoints over and over.

Most of these disadvantages can be avoided by using the "trace" routine described in this article. It was developed some months ago for this very purpose, and since then it has helped me considerably in tracking down elusive bugs.

Basically it consists of a subroutine which may be called any number of times, by temporarily patching appropriate BSTA or BSTR instructions into the program you are trying to debug. When it is called, it first saves the contents of all of the 2650 registers. Then it prints them all out on the terminal, to provide a "snapshot" of the current processor status. Then it restores all of the registers again, and does a return.

Before it prints out the register contents, it prints three spaces. This is to prevent confusion if the program you are testing already involves printing. After the spaces it prints the registers in the same order that they are provided by PIPBUG: R0, R1, R2, R3, R1', R2', R3', PSU and PSL. Finally it prints a carriage return and line feed, so that each "snapshot" is on a different line.

A full source listing of the trace routine is shown below, together with a sample of its operation. As listed the routine is located from 0440 to 0495, but it may be relocated anywhere in page 0 without changes. Note that it stores the processor registers in locations 0400-0408 — ie, the same locations used by PIPBUG for this purpose.

The sample tracing shown below was produced by patching a call into the author's Disassembler program, at the end of the PRINT MESSAGE subroutine (1D9C). The code at 1D9C was changed to 1B39, to branch to 1DD6 where a patch of 3F0440, 1F1D94 was located. As you can see this gives a "snapshot" after each character is printed from the line buffer.

```
*G1B00 1B00 1B02
1 001A0200003100E2B0
B 001A0200100420E2B0
0 001A0200200300E2B0
0 001A0200300300E2B0
001A0200400200E2B0
7 001A0200500370E2B0
6 001A0200600360E2B0
6 001A0200700360E2B0
0 001A0200800300E2B0
001A0200900200E2B0
001A0200A00200E2B0
001A0200B00200E2B0
001A0200C00200E2B0
001A0200D00200E2B0
001A0200E00200E2B0
P 001A0200F00500E2B0
P 001A0210005000E2B0
S 001A0211005300E2B0
U 001A0212005500E2B0
001A0213002000E2B0
001A0214002000E2B0
001A0215002000E2B0
001A0216002000E2B0
001A0217002000E2B0
001A0218002000E2B0
6 001A0219003600E2B0
0 001A021A003000E2B0
```

RIGHT: A full listing of the trace routine, complete with comments so that you can see how it works.

LEFT: A sample of the routine in operation. Here it was patched into the Disassembler program, so that a "snapshot" of the processor registers is printed after each character from the Disassembler's line buffer.

*DIAGNOSTIC "TRACE" ROUTINE FOR
*2650 SYSTEMS. J. ROWE MARCH 1979

```
0440 CC0400 STRA,R0 0400 SAVE R0
0443 12 SPSU & PSU
0444 CC0407 STRA,R0 0407
0447 7660 PPSU 60 FORCE TO MARK,INHIBIT INT.
0449 13 SPSP SAVE PSL
044A CC0408 STRA,R0 0408
044D 7710 PPSL 10 FORCE TO BANK 1
044F CD0404 STRA,R1 0404 SAVE BANK 1 REGS
0452 CE0405 STRA,R2 0405
0455 CF0406 STRA,R3 0406
0458 7519 CPSP 19 FORCE TO BANK 0,CLR C & WC
045A CD0401 STRA,R1 0401 SAVE BANK 0 REGS
045D CE0402 STRA,R2 0402
0460 CF0403 STRA,R3 0403
0463 3F035B BSTA,UN 035B PRINT 3 SPACES
0466 07FF LODI,R3 FF SET R3 AS INDEX
0468 0609 LODI,R2 09 & R2 AS COUNTER
046A 0F2400 LODA,R3 0400+ FETCH SAVED REG
046D C1 STRZ,R1 MOVE TO R1
046E 3F0269 BSTA,UN 0269 PRINT VIA BOUT SUBR
0471 FA77 BDRR,N 046A LOOP BACK TIL DONE 9
0473 3F008A BSTA,UN 008A THEN GIVE CRLF
0476 0D0401 LODA,R1 0401 RESTORE ALL REGS
0479 0E0402 LODA,R2 0402
047C 0F0403 LODA,R3 0403
047F 7710 PPSL 10
0481 0D0404 LODA,R1 0404
0484 0E0405 LODA,R2 0405
0487 0F0406 LODA,R3 0406
048A 0C0407 LODA,R0 0407
048D 92 LPSU
048E 0C0408 LODA,R0 0408
0491 93 LPSL
0492 0C0400 LODA,R0 0400
0495 17 RETC,UN & RETURN
```

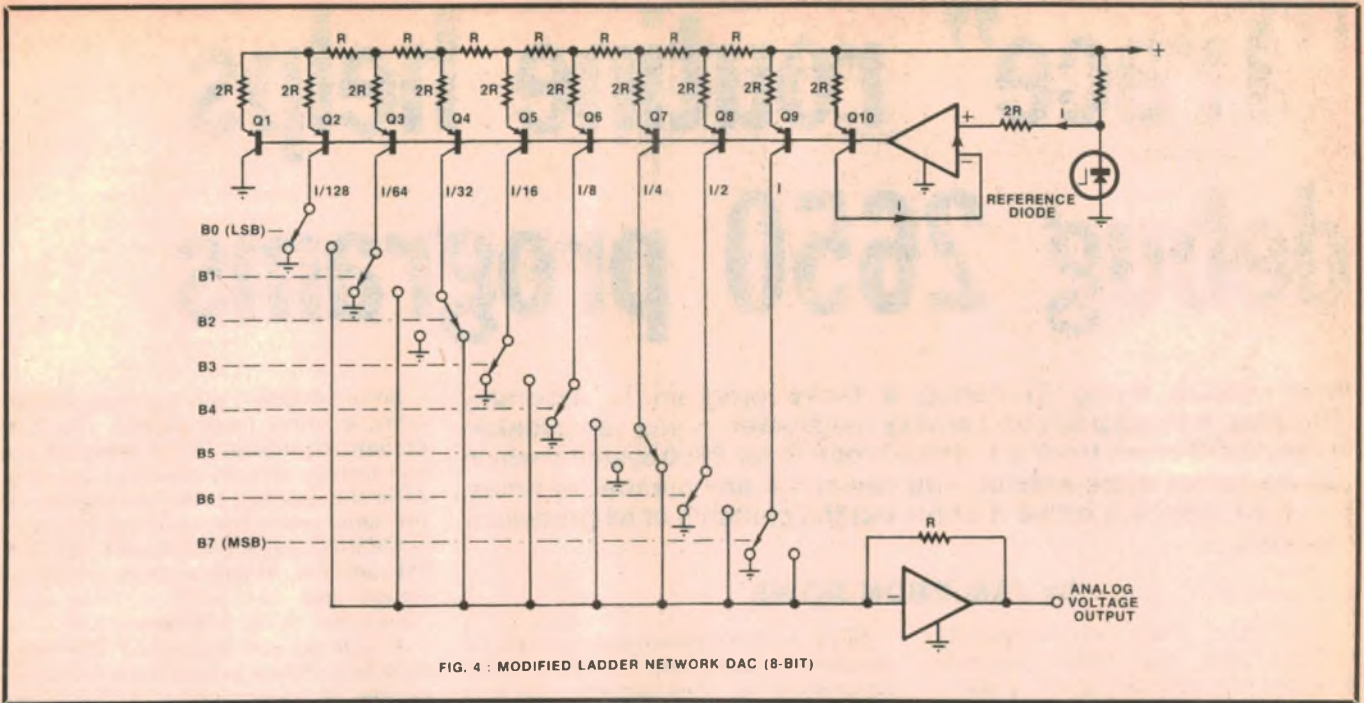



FIG. 4 : MODIFIED LADDER NETWORK DAC (8-BIT)

accurately matched, and to maintain this condition despite supply voltage and loading variations.

Q10's collector current is thus set accurately to equal I . As Q10 is matched to all the other transistors, and its emitter resistor is also matched to the other resistors, this automatically sets the current levels in all of the transistors. Hence Q9's current is set to I , Q8's to $I/2$, Q7's to $I/4$ and so on down to Q2 whose current is set to $I/128$.

Note that there is a tenth transistor, Q1, whose collector is connected directly to earth. This is necessary in order to terminate the ladder correctly, and ensure that the binary sequence of current levels is maintained accurately over a range of supply voltages.

The actual current switching in most modern DACs is performed using MOS transistors. Fig. 5 shows how complementary MOS transistors are used to perform the SPDT switching in a circuit like that of Fig. 4.

A P-channel device is used for the "grounding" function, while an N-channel device is used for the gating function. As the two devices are complementary, the digital input B is simply connected to both gates in parallel. When the input is at logic low level, the N-channel device is cut off while the P-channel device conducts, directing the current increment to ground. Conversely when the input is raised to logic high level the P-channel device cuts off and the N-channel conducts, switching the current increment into the output amplifier.

Before leaving DACs, there are a number of terms used to describe DAC performance with which you should be familiar. These are resolution, non-linearity and settling time.

The **resolution** of a DAC is a measure of the number of discrete voltage or current levels which its output can adopt. Naturally enough, this is directly related to the number of digital input bits. The output of an 8-bit DAC like that of Fig. 4 can adopt any of 256 discrete levels, equal to the number of combinations of 8 bits. Similarly the output of a 12-bit DAC can adopt any of 4096 levels, while that of a 16-bit DAC can adopt 65,536 levels.

The **linearity** of a DAC is a measure of the degree to which its analog output amplitude corresponds to the magnitude of the digital input. Nothing is perfect in the real world, and all DACs have small errors due to things like resistor matching errors and the fact that the electronic switches do not have zero resistance in their "on" state.

Generally, DAC linearity is expressed in terms of either a percentage of the maximum DAC output amplitude, or as a fraction of the LSB output increment. It is sometimes also expressed in terms of the number of input bits required for a DAC with resolution equal to the linearity error concerned.

For example the linearity of an 8-bit DAC might be described as "within 0.1% of full output", or "within $\pm 1/8$ LSB", or as being of "10 bits". These all mean much the same thing.

The **settling time** of a DAC is a measure of the time taken for its analog output to re-stabilise when the digital input is changed to a new value. When such a change takes place, one or more current switches must operate, and the output feedback amplifier must readjust its output to the new level. Needless to say the switches take a finite time to operate, while the amplifier has a finite response and out-

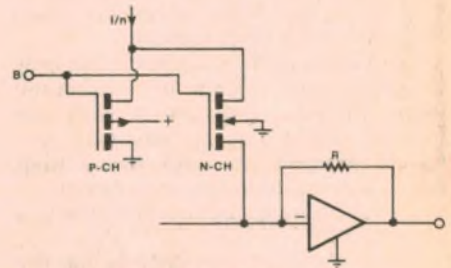


FIG. 5 : SPDT CMOS SWITCHING

put slew rate. These delays collectively form the settling time.

A final note. Some modern DACs are designed so that they may be used not only as a digitally programmed voltage or current generator, but alternatively as an attenuator with digitally programmed attenuation. These are known as "multiplying DACs".

Essentially a multiplying DAC is rather like those in Figs. 2 and 3, except that an analog input signal may be fed into the switched weighting resistors or the ladder network, in place of the fixed precision reference voltage. The DAC's output signal amplitude will then depend not only upon the magnitude of the digital input, but also on the analog input amplitude. In effect, the DAC multiplies the digital and analog inputs together.

Some multiplying DAC's are designed to accept bipolar (AC) analog input voltages, and to treat the digital input as a signed binary quantity. The analog output signal is also bipolar, with a polarity depending upon both the sign of the digital input and the polarity of the analog input. DACs of this type are often described as being capable of "4-quadrant" operation, or as a "4-quadrant multiplying DAC".

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D-TO-A CONVERTERS

to the weighted resistor type, but in place of the set of weighted resistors there is a "ladder" of resistors controlled by two-position electronic switches. Only two resistor values are required, "R" and "2R", the ladder network itself ensuring that these produce the desired progression of binary weighted currents.

Like the weighted resistor DAC the ladder-network circuit uses a feedback amplifier to provide a very low load resistance and ensure linear conversion.

As you can see from Fig. 2 the resistor values in the weighted resistor DAC reduce in value by a factor of 2. This means that for each additional bit involved in the conversion, the required resistance range doubles. For an 8-bit DAC, the B7 or MSB resistor must have a value 128 times smaller than the B0 or LSB resistor. This tends to make the weighted-resistor DAC relatively difficult to implement in integrated circuit (IC) form.

In contrast, the ladder-network DAC has only two resistor values in the network regardless of the number of bits involved, and the two values have a modest 2:1 ratio. This makes the ladder-network DAC much more suitable for IC implementation, and in one form or another it is now used more often than the weighted-resistor approach.

Fig. 4 shows a modified version of the ladder-network technique, which has been evolved for use in modern DACs implemented in a single monolithic IC. Here the ladder-network is not used alone to set the current increments, but in conjunction with a set of carefully-matched transistors connected in the constant-current configuration.

As you can see the ladder-network itself is connected to the normal supply line, which could not be relied upon to have the accuracy or stability required for the DAC's reference. However, the bases of all the transistors are connected together, and the common base line connected to the output of a current-differencing operational amplifier. This amplifier is used to control the base line potential, to set and maintain accurately all of the transistor collector current levels.

The non-inverting input of the amplifier is connected via a matched resistor to a reference diode, which derives from the supply line a source of accurately stabilised voltage. This produces an accurately maintained input current, I. The inverting input of the amplifier is connected to the collector of one of the current-source transistors, Q10, as shown. The action of the amplifier is thus to adjust the base line potential until the two currents are

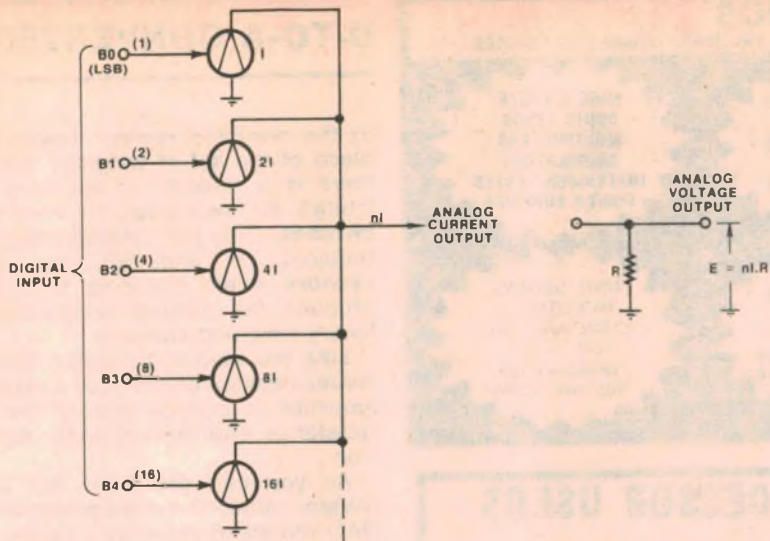
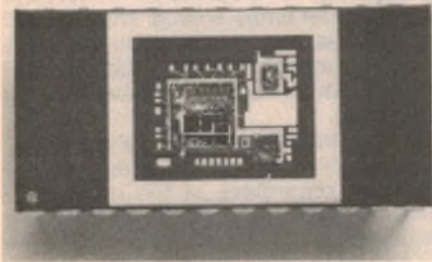


FIG. 1 : BASIC CURRENT-INCREMENT DAC

set the currents through the weighting resistors. Instead of remaining fixed, these would vary considerably depending upon the number of other resistors in circuit.

The feedback amplifier consists of a high-gain operational amplifier with heavy negative feedback around it, via resistor R_f . The main effect of the high gain and negative feedback is to reduce the input impedance of the amplifier to a very low value, creating a "virtual earth" condition. This provides a very low load resistance for the weighting resistors, ensuring that the voltage across each resistor is substantially constant regardless of the number of resistors in circuit.

The output of the feedback amplifier forms the output of the DAC, and as the amplifier acts as an impedance converter, the output is in the form of a voltage. Each voltage increment will



The Analog Devices AD DAC80, a 12-bit D-to-A converter which uses 3 chips in a 24-pin DIL package. (Parameters)

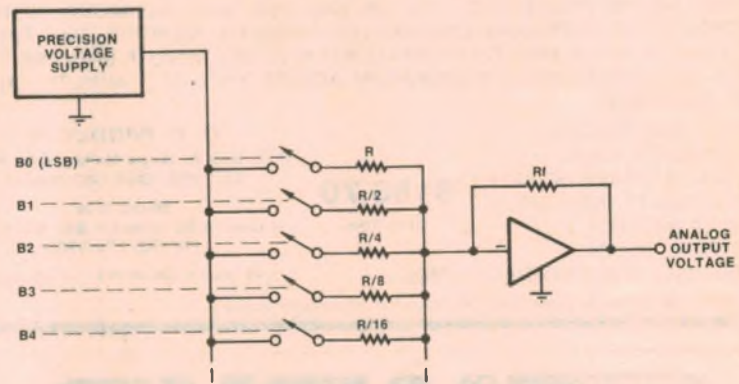


FIG. 2 : WEIGHTED-RESISTOR DAC

DAC is simply the sum of all the incremental currents from the individual generators. And since the individual generators are controlled by the input bits, this means that the sum will have an amplitude proportional to the overall binary number applied to the DAC inputs: "ni", where n is the binary number.

Essentially all that is needed to produce an analog voltage from this output current is to feed it into a resistor. Ohm's law will then cause the resistor's voltage drop to equal $ni.R$, where R is the resistor value.

Practical DACs use one of two basic techniques to perform the operation shown in Fig. 1. These are generally known as the "weighted resistor" and "ladder network" techniques, and they are illustrated in Fig. 2 and Fig. 3 respectively.

As its name suggests, the **weighted resistor DAC** involves a set of resistors whose relative values vary in binary weighted fashion. The resistors are connected between a precision regulated voltage supply and the input of a feedback amplifier (inverting), with each resistor in series with an electronic switch controlled by one of the binary input bits.

The feedback amplifier is necessary to ensure that the currents which flow in

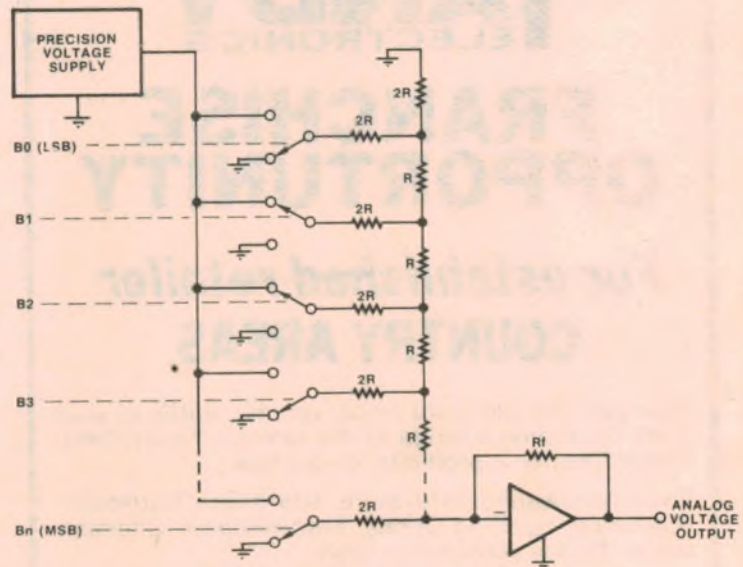


FIG. 3 : LADDER NETWORK DAC

the weighting resistors are themselves also accurately weighted, and that they add together linearly. Because the circuit uses resistors and a voltage source instead of the ideal current sources shown in Fig. 1, the junction of the resistors cannot be fed to a simple load resistor because the varying voltage drop across the load resistor would

have an amplitude of $(E.R_f/R_w)$, where E is the voltage of the DAC's precision voltage supply and R_w is the weighting resistor for the bit concerned. Thus the increment corresponding to B0 (the LSB) will be $E.R_f/R$, that for B1 will be twice this value, and so on.

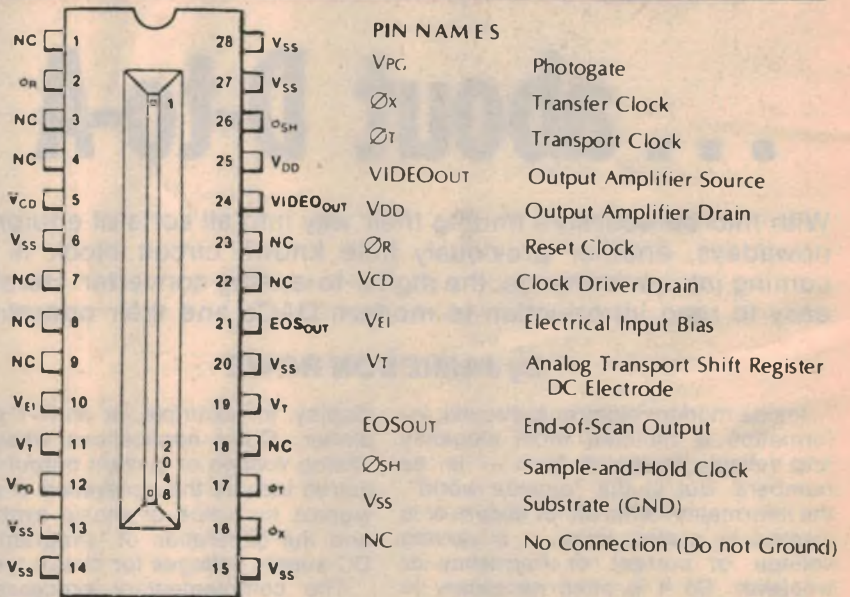
As you can see from Fig. 3 the **ladder-network DAC** is broadly similar

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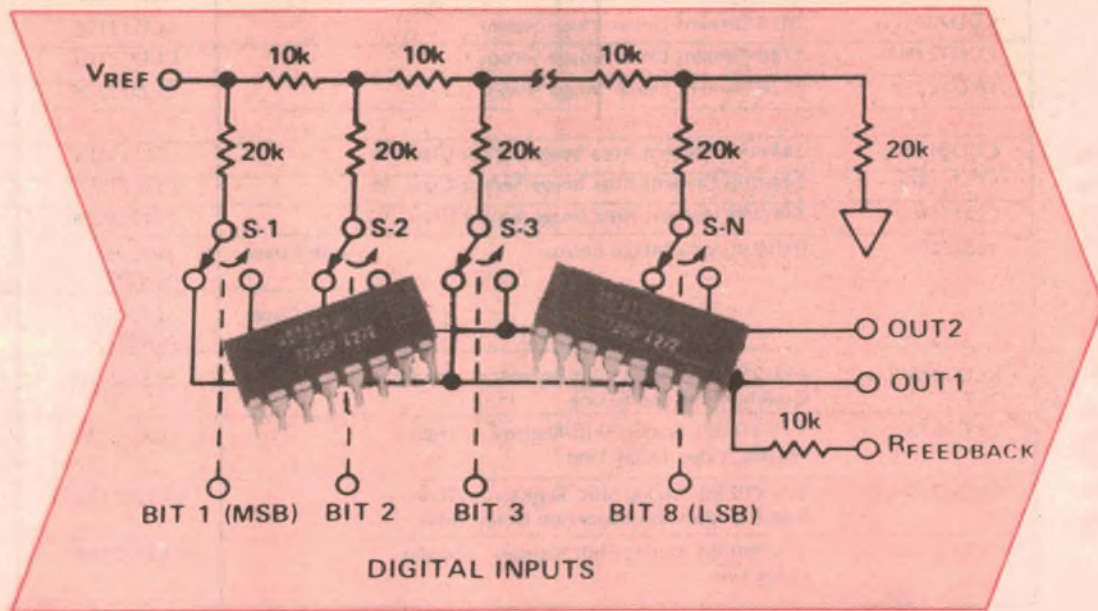
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. . . about D-to-A Converters

With microprocessors finding their way into all sorts of equipment nowadays, another previously little known circuit block is also coming into prominence: the digital-to-analog converter. Here's an easy to read introduction to modern DACs and their operation.

by JAMIESON ROWE

Inside modern electronic circuits, information is handled most elegantly and reliably in digital form — ie, as numbers. But in the "outside world", the information often either occurs or is wanted in analog form — a varying voltage, or current, or frequency or whatever. So it is often necessary to perform digital-to-analog and analog-to-digital conversion where the information has to pass between a digital system and the outside world.

For example at the input interface of a system, the information may be in the form of a varying analog voltage or current. It could be a voice or music signal, perhaps, which is to be processed or transmitted within the digital system. Understandably the first thing which must be done with such signals is to convert them from analog into digital form.

Similarly at the system's output interface, the output information may be needed in the form of an analog voltage or current in order to use it effectively for the desired purpose. It could be needed as a varying analog voltage or current to operate a high-speed visual

display, for example, or an X-Y paper plotter. Other applications where an analog voltage or current output is required include the generation of audio signals for voice or music synthesis, and the generation of "programmed" DC supply voltages for circuit testing.

The complementary processes of analog-to-digital (A/D) and digital-to-analog (D/A) conversion are therefore performed in many digital systems. And with the microprocessor revolution bringing digital systems into almost every sphere of electronics, this means that A/D and D/A converters are becoming very important — so you're going to need some knowledge of how they work.

In this article we're going to look first at D/A converters or "DACs". A following article will deal with A/D converters or "ADCs".

Essentially, D/A conversion is the process of taking a piece of digital information — usually, a binary number — and generating an analog voltage or current whose amplitude is proportional to the number's magnitude. This is done by using each binary bit of the

number to control an increment of voltage or current, whose amplitude is proportional to the binary weighting of the bit concerned. The various incremental voltages or currents are then added together to produce the full analog output.

In most practical D/A converters or "DACs" current increments are used, as it is easier to add them together. This gives the basic converter an analog current output, but changing this into an equivalent voltage signal is generally quite straightforward. The basic idea of a current-increment DAC is shown in Fig. 1.

As you can see, each bit of the digital input is effectively used to control a current generator, whose current magnitude is proportional to the binary weighting of the bit concerned. Hence bit 0 (the least significant bit or LSB), with a weighting of 1, is used to control a current generator with an output "1". Bit 1, with a weighting of 2, controls a generator with an output of "2I". Bit 3 controls a generator of output "4I", and so on.

There are as many current generators as the number of input bits that the DAC is designed to accept. Typical DACs are designed to accept either 8, 12 or 16 input bits, and therefore have the same number of controlled current generators.

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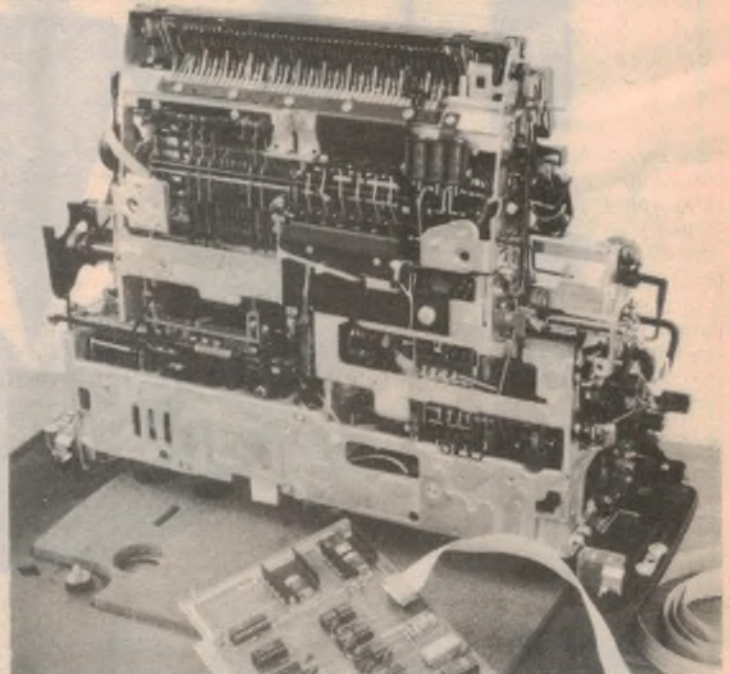
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