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AUSTRALIA'S NUMBER ONE ELECTRONICS MAGAZINE

ELECTRONICS

AUSTRALIA

COMPUTERS:
What to look for

JUNE 1984 AUST \$2.30 NZ \$2.75

*Cruise control
for cars*

\$599
**Yamaha CD
player review**

**VHF AMATEUR
TRANSCEIVER**



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AUSTRALIA'S LARGEST SELLING ELECTRONICS MAGAZINE

ELECTRONICS AUSTRALIA

Volume 46, No. 6, June 1984



On the cover

Two contributed projects share the limelight this month: a versatile cruise control, and an up-to-the-minute VHF amateur transceiver from Dick Smith Electronics. Construction begins on pages 44 and 58.

VHF Amateur Transceiver



Are you an amateur wanting to upgrade your two-metre gear? This up-to-the-minute transceiver comes as a kit and is yours for just \$199. Construction starts on page 58.

What's coming?

Next month, we intend to publish details of a vintage shortwave receiver featuring 1930s triode valves and plug-in spiderweb coils. Watch for it in our July issue (see also p.147).

DFM Adaptor for Function Generator



This add-on board lets you use the EA Function Generator (April '82) as a 300kHz DFM. As a bonus, it drastically improves the linearity of the coarse frequency control. (p.68)

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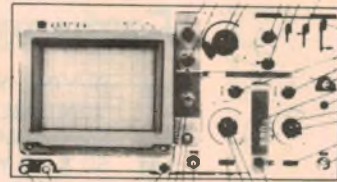
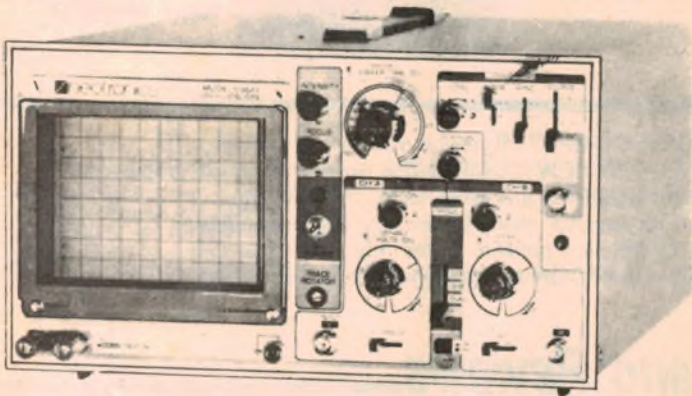


Buying your first computer

Many thousands of people have bought personal computers and many more would if they knew what computers were all about. Our article on page 12 offers some practical advice.

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SWEEP TIME DIV
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TRIG LEVEL (PULL AUTO)
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TRIG SCOPE
TRIG FILTER SELECTOR
TRIG SOURCE SELECTOR
CH A POSITION
CH B POSITION (PULL INVERT)
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CH B VOLTS DIV
CH B VOLTS DIV VARI
CH B COUPLING SELECTOR
CH B OR INPUT
COMPONENT TESTER
CH A VOLTS DIV VARI
CH A VOLTS DIV
CH A OR Y INPUT
TRACE ROTATOR
POWER SW
POWER INDICATOR
GROUND
COMPONENT TESTER TERMINAL

\$465.00
TAX FREE

Price Breakthrough

The Neotronics Model OS620 is a powerful 20MHz dual trace oscilloscope with performance and features normally found on scopes costing \$200-\$500 more. We sell at lower profit margins and import directly from the manufacturer. You reap the benefit!!

Compare the Features

The Neotronics OS620 is a precision measuring instrument. The tube is 150mm flat screen/internal graticule type with 2kV acceleration potential. The bandwidth is a full 20MHz on both channels. Others offer round faced tubes, plastic graticules, less bandwidth, yet cost more! Intensity modulation is built in. By importing directly we offer you the best value on the Australian market.

\$536.80
INC. TAX

Built-in component tester

The component tester allows you to make full use of the OS620. With no additional test gear, you can check resistors, capacitors and zener diodes as well as trouble shoot solid state circuits. Testing signals are available via the COMP. TEST terminals.

Probes included in price.



Probes included

Most users will need a set of probes. These are sold as very expensive 'extras' with some other brands - often costing over \$60.00 a pair (we think this is a bit like selling a car and then saying it's extra for the tyres!). The Neotronics OS620 comes complete with a pair of high quality probes.

Check these specs

- Vertical sensitivity: 5 mV/div to 10 V/div. 11 ranges
- Operating modes: ch-A, ch-B, dual, add, invert ch-B.
- Rise time: 17nsec
- Time base speed: 0.5µsec to 0.5s/div. 19 Ranges (plus 5X mag.)
- Trigger source: Int, ch-A, ch-B, line, ext and auto.
- Trigger coupling: AC, HF reject, TV line and TV frame.
- X-Y operation: Ch-A becomes Y axis, Ch-B becomes X axis.
- Trace rotation on front panel.

neotronics

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Prices correct and goods expected in stock at time of going to press.

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Editorial Viewpoint

Anyone for a three-year battery?

Few people would decry the increasing evidence of electronics in today's cars. As time goes on we are sure to see the process accelerated as the auto makers try to meet the requirements for more reliability, more economy and power and less pollution.

Already, features such as alternators, hybrid voltage regulators and breakerless ignition systems have proved their worth. They are reliable (on most cars anyway), seldom require adjustment and work better than the old systems they replace.

In the future we shall see more cars with computers for engine management and diagnostics. Electronic fuel injection will become commonplace. And luckily, in view of the shortage of competent technicians to service this equipment, the new technology is very reliable.

Does this mean that car electrical systems are super-reliable these days? Sadly, the answer is no. While the electronic components are reliable the side is being increasingly let down by the battery itself. The truth is that "they don't build 'em like they used to."

It is becoming more common for batteries to fail while they are just a few months old. They just drop dead. Technicians shake their heads and drop in a new one. Some have theories such as "It's the air-conditioners. They beat the hell out of batteries". Others maintain that batteries don't last because of the simpler construction.

Whatever the reason, it is a ludicrous situation. There is no reason why the average auto battery cannot be made to last three or four years or much longer. Nor need the cost be much higher.

Car makers had better realise that it is no use putting in all the technology if the battery is going to drop dead in six months. The public is being short-changed.

The AM stereo debacle

Earlier this year an announcement was expected from the Department of Communications concerning AM stereo. In an editorial in the October 1983 issue I stated the desirability of deciding on one system. We did not want the same botch-up as occurred in the USA. There, the four competing AM stereo systems have been left to fight it out.

In Australia, the situation is less clear cut. About 30 stereo excitors have been purchased with some stations buying two different systems. Harris is leading in numbers sold. Some 14 stations were running experimental stereo transmissions during May but these were due to stop at the end of the month.

This month, all concerned are due to come together in a working party to consider results so far and make a decision. The committee members are from the Department of Communications, the Federation of Australian Radio Broadcasters, the Special Broadcasting Service, the Public Broadcasting Service of Australia and the Australian Broadcasting Corporation.

Let us hope that they can come to a quick decision. What is important is that they decide on one system. This will remove doubt and let AM stereo broadcasting go ahead. It will also allow the local manufacture of AM stereo tuners to develop which will be good for employment in Australia.

Leo Simpson

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Hey! Calling all FT1012D owners - and anyone else looking for an absolute bargain! FV101DM Digital VFO's - original price over \$200 ...huge scoop purchase now only \$99 each! Standard 5 - 5.5MHz output, 10 memories, optical coupling, digital keypad, etc. etc. - they should be adaptable to suit most HF transceivers. Hurry in for this one - don't say you weren't told!
Cat D-2948

\$99



Manufacturer's surplus stock... you reap the benefit!!

Giant Rubber Feet Pack
As used by giants everywhere. 25mm diam., 20mm high. With steel insert for strength. Use on big projects, appliances, jumbo jets, etc.
Pack of 4 for 60c
Cat H-1738

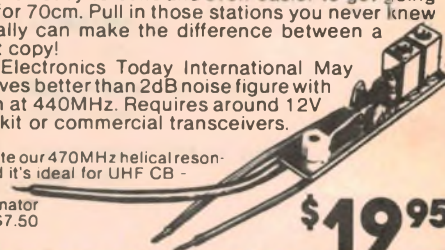
Fantastic Replacement Speaker
7 x 5 inch oval speaker, ideal for cars, etc. Impedance - 8 or 15 ohms. 5W power rating
Slashed to just **\$4.50 each!!**
(Buy 5 or more and they're just **\$4.00 each!!**) Cat A-7137

Huge shipment of distressed stock arriving mid June...see next months mags for details and grab some while they last!

Build a deluxe 70cm Preamp Kit

Here's great value: an easy-to-build and even-easier-to-get-going receiver preamp for 70cm. Pull in those stations you never knew were there. It really can make the difference between a noise and a great copy!
As described in Electronics Today International May 1984 issue, achieves better than 2dB noise figure with around 18dB gain at 440MHz. Requires around 12V @ 5mA. Ideal for kit or commercial transceivers.

Cat K-6306
CB Version - substitute our 470MHz helical resonator in above kit and it's ideal for UHF CB - with similar specs!
470MHz Helical Resonator
Cat L-1860 \$7.50



\$19.95

Get a load of these new computer connectors...while stocks last!

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PLUS our existing range:

25 Pin Plug 'D' type.....	P-2690	\$3.95
25 Pin Socket 'D' type.....	P-2691	\$4.75
Backshell to suit.....	P-2692	\$2.50
57-30360 Printer Plug.....	P-2680	\$19.95
57-403360 Printer Socket.....	P-2681	\$15.95

For a Dashing Dashboard! 12V Bezel

Bezel in dashboard tells thief there's an alarm - so he tries another car! Most alarms have flashing circuitry built in - lamp rated at 12V



95c

Cat S-3510



\$299 'Go anywhere' 2M Hand Held FT203R

Small enough to go in the briefcase, the back-pack, anywhere! Fully detachable battery pack for instant replacement, full 144-148MHz coverage in 10kHz steps plus 5kHz up switch. A must for the amateur on the go! Cat D-3500

Accessories for your FT203R:

Headset Mic/phone
Gives complete hands-free VOX operation. Lightweight and comfy.
Cat C-4200 \$29.00

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For mobile or base use, gives external PTT too. Ideal for noisy locations. Cat C-1112 \$39.00

Mounting Bracket
Holds over car window, holds the FT203R securely with access to all controls. Cat D-3501 \$19.50

KEYBOARDS!!

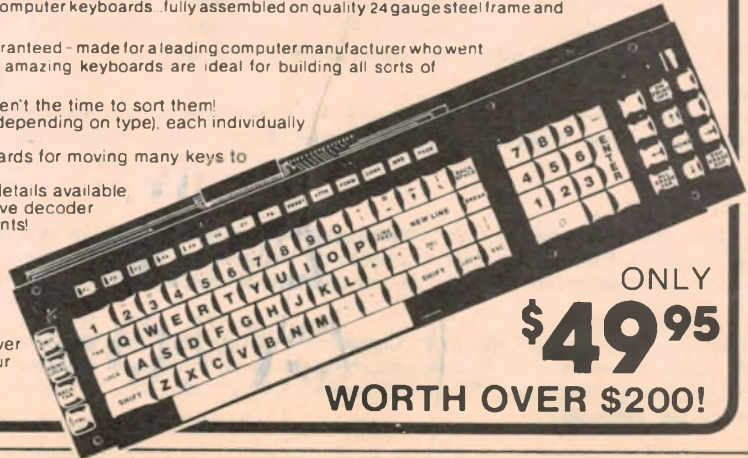
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World famous 'Cherry' brand computer keyboards...fully assembled on quality 24 gauge steel frame and fibreglass PCB!

Absolutely brand new and guaranteed - made for a leading computer manufacturer who went broke (don't they all?) these amazing keyboards are ideal for building all sorts of computer projects.

- ★ 4 different types - we haven't the time to sort them!
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- ★ Matrixed output - matrix details available
- ★ Some keyboards even have decoder chips and other components!
- ★ Buy two keyboards, use the switches from one to make up a massive 117 key keyboard in some types!

Cost original manufacturer over \$100 each...worth over \$200 normally...look at our ridiculous price!
Cat K-3621



ONLY **\$49.95**

WORTH OVER \$200!

Alarming Switches!

Reed Switch

The old faithful! Actuated by magnet, extremely reliable switch for all alarm systems. Tiny size is ideal for concealment, too.
L-5215



\$1.85

Mercury 'Tilt' Switch



For boot/bonnet switches or low-away sensors, etc. Mercury ball makes contact when tilted.

\$1.50 Cat S-1935

Stick it in! Vehicle Alarm Switch

Normally closed switch opens when door is closed. Ideal for alarms or interior lights, etc. Two in a pack
Cat L-5256



\$1.80



OWN A VIDEO?

Sick of the lousy sound most videos give you? Now you can build a kit to fix it - and what's more, get synthesised stereo as well! Yes - a graphic equaliser specifically intended for video use: now you can really get the most from your video:



- Suits ALL VCR's
- Easy-to-build kit.

\$49⁹⁵

Cat K-3422

Go Mobile . . .

Our kit antennas make it easy! And you'll save heaps by doing it yourself!!

VHF

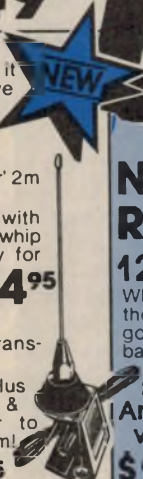
(suits new 'Commander' 2m transceiver)

Deluxe Gutter Gripper with low-loss co-ax, plus VHF whip & cutting guide ready for two metre mobile. **\$24⁹⁵**

UHF

(suits 70cm 'Explorer' transceiver)

Gutter Gripper base plus low-loss co-ax, whip & cutting guide similar to above. A must for 70cm! Cat D-4014 **\$24⁹⁵**



No leak! Rechargeable! 12V Gel Cell

What happens if the crook cuts the car battery wire? The alarm goes off - if you have this back-up battery fitted! Cunning isn't it? 2.6Ah cap., 12V.

Amazing value!

\$24⁹⁵



Cat S-3320

COMPUTER TIME

Want to be a two or three computer family? Try this one! Novelty LCD clock inside a tiny computer-shaped case. What a great gift idea too. Don't miss out - limited stocks.

\$4⁹⁵

Cat Y-1039



BUILD THE BEST CAR ALARM IN AUSTRALIA!

Every possible feature to protect your car - even provision for battery back-up!

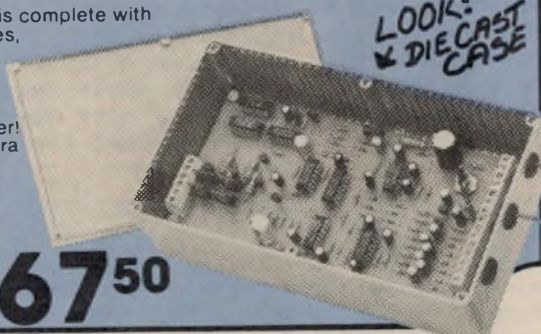
* As described in Electronics Australia May 1984 - scores 9 out of 10 (the BEST commercial units score only 8!)

The Dick Smith Deluxe Car Alarm kit comes complete with a die-cast case - essential for use in a car. Don't buy el cheapo kits in plastic boxes!

And our kit is complete with ALL switches, sensors, dash bezel, front panel and quality horn speaker! Nothing extra to buy!

Cat K-3252

\$67⁵⁰

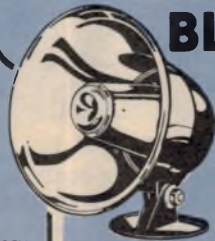


LOOK: DIE CAST CASE

BLOW YOUR HORN! Make a noise!

Deluxe horn speaker is ideal for alarms. Very efficient, makes a real din with siren in alarm itself. Cat C-2705

\$10²⁵



AT LAST! TOP QUALITY PASSIVE I/R SENSOR

SWISS MADE

We've waited for a while to find these top quality units (not like a lot of inferior types you can find elsewhere!) Passive Infra Red sensor is by far the best type of sensor for your alarm - wind, curtains, etc. won't be set off.

Senses body heat from across a room - extremely sensitive and effective! Add on to any alarm system for real protection!

Cat L-5010

\$119

No. 1 in Australasia!

DICK SMITH ELECTRONICS

See page 108 for address details



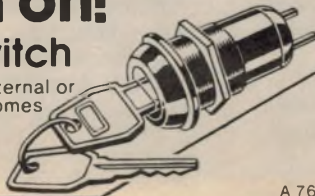
Switch it on!

Barrel Key Switch

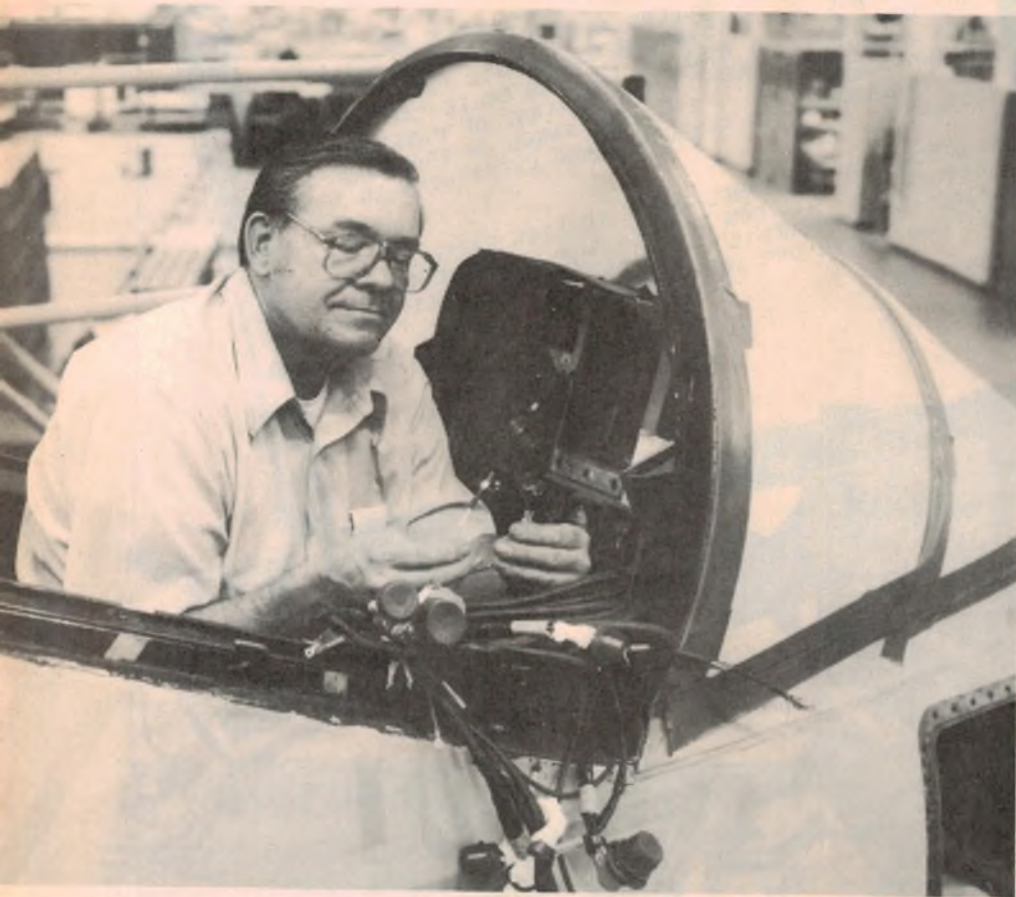
Use with any alarm for internal or external key control. Comes complete with two keys.

Cat L-5290

\$7²⁵



News Highlights



First fibre optics for combat aircraft

The McDonnell Douglas Corporation is building the first combat aircraft to be equipped with fibre optics in place of electrical wiring. The fibres are used in the radio equipment of the McDonnell Douglas AV-8B Harrier II, the US Marine Corp version of the British Harrier vertical-takeoff-and-landing jet.

Fibre optics are much lighter and more compact than conventional cables but can transmit immense amounts of

information. Data equivalent to a set of encyclopedias (about 40 million words) can be transmitted over a fibre optics system in just 16 seconds.

Optical fibres are also immune to electrical interference from external sources such as lightning and ground-based and airborne radar transmitters. They do not themselves interfere with other electronics aboard the Harrier.

The photo above shows McDonnell Douglas technician Mr Arkie Hilborn installing fibre optic cables in the cockpit of an AV-8B Harrier at the company's St Louis plant.

Australia Telescope for bicentenary

In December, 1988, on the 200th anniversary of the arrival of the First Fleet, Australia could well set out on another voyage of discovery, reaching across 20 billion years of history from the sensitive receivers of the giant Australia Telescope project.

In 1988, antennas at Culgoora near Narrabri and Siding Spring mountain near Coonabarabran in NSW will be connected by microwave links with the existing 64-metre diameter dish of the Parkes radiotelescope. The result will be an "aperture synthesis" radiotelescope with a range and sensitivity equivalent to a single dish 300 kilometres across.

The project has been organised by the CSIRO Division of Radiophysics with backing from the Federal Department of Science and Technology. It will provide an advanced tool for scientists of the 1990s and into the 21st century. It is one of the most exciting developments in Australia's long history of innovation in radio and telecommunications and as such has been endorsed by The Australian Bicentennial Authority as an official commemorative activity for 1988.

The designers of the \$30 million Australia Telescope aim to probe some of

New videodisc player uses solid-state laser

Hitachi has begun advertising, in the United States, a new laser video disc player which uses a semiconductor laser rather than the fragile helium/neon laser tubes of other players.

Hitachi research engineers had to overcome the problem of fluctuations in the output of the laser caused by temperature variations.

Applications of semiconductor lasers in video disc players should allow the production of more compact, reliable units and ultimately a reduction in the price of the players.

Preparations for IREECON '85 underway

IREECON '85 will be the 20th International Convention and Exhibition staged by the Institution of Radio and Electronics Engineers Australia (IREE Australia). The biennial event has grown steadily since its inception in 1938 to become

Australia's largest and most comprehensive exhibition of professional electronics equipment.

Even at this early stage much of the floorspace for the exhibition has been allocated, while scores of technical papers are being prepared. The Conventions are held alternately in Sydney and Melbourne, with the 1985 convention to be held in Melbourne

around the theme "The Australian Position in the New Era of Communications".

Further information on preparations of IREECON '85 is available from Heather Harriman, Executive Officer, The Institution of Radio and Electronic Engineers Australia, PO Box N127, Grosvenor Street, Sydney, 2000. Phone (02) 29 4051.



Pictured at the endorsement ceremony for the Australia Telescope are Dr David Armstrong (left), General Manager, The Australian Bicentennial Authority, and Dr Robert Frater, Australia Telescope Project Director, CSIRO.

the major problems of modern astrophysics. The flexibility of the system will enable scientists to use a wide range of radio frequencies to explore stellar phenomena.

Dr Andrew Pik of the Radiophysics Division of the CSIRO says, "The Parkes telescope will have outlived its usefulness by the 1990s. But when it becomes part of the Australia Telescope it will gain a

new lease of life. It will enable us to delve deeper into the cosmos and to resolve its finer details and thus help to unlock the mysteries of the universe".

Footnote: Culgoora, the main site of the Australia Telescope, is also the site of the CSIRO's radio heliograph, which has worked in collaboration with the Solar Max satellite recently repaired by the crew of the Space Shuttle *Challenger*.

National Semiconductor settles with Government

National Semiconductor Corporation has announced that it has accepted an agreement with the United States government to dispose of civil and criminal liabilities arising from a probe into National's testing and certification of military standard microcircuits supplied between 1978 and 1981.

The agreement covers 40 charges filed by the government charging National with falsely certifying that all required testing on certain military and aerospace devices had been performed. National agreed to pay a \$US247,000 fine, costs of \$US105,000 and \$US1,405,000 in damages and civil penalties to the government.

Charles E. Sporck, president of National Semiconductor, said of the settlement "We will be pleased to finally resolve this entire matter. It is important to us that the Government's investigation did not uncover any instances in which undertested devices had failed in the field".

According to Sporck, after the irregularities in test procedures were discovered in 1982 National implemented strict controls to ensure that all testing would be performed to full military specifications. "This error will not recur. We now follow every jot and every dash of every military specification," he said.

Dual sound TV broadcasting begins

Two television stations, in Sydney and Melbourne, recently began dual-sound, or stereo broadcasting, following approval of alterations to equipment by Mr Michael Duffy, the Minister of Communications.

Announcing the commencement of dual sound broadcasting Mr Duffy said: "The start of stereo broadcasts represents yet another advance in communications technology. At the moment there are only a limited number of stereo receivers on the market, but this number can be expected to increase rapidly. The stereo transmissions will enhance people's enjoyment of such programs as concerts and films. The second sound channel can also enable a station to transmit programs in an alternative language to that on the video version, or provide spoken data".

TCN Channel 9 in Sydney and GTV Channel 9 in Melbourne began stereo transmissions at the end of March.



This new stereo sound TV set from Blaupunkt features a 67cm picture tube.

Since then several other TV stations, including WIN-4, Wollongong, NSW, have been granted approval, and a

number of others, including ATN-7, Sydney, are expected to be given approval within a few weeks.

News Highlights

US "supercomputer" R&D

The US Defence Department is budgeting \$US600 million for supercomputer research and development over the next five years. Included in the total is funding for a new national software institute to be set up near a major university.

The Department's effort last year to increase support for a major national "fifth generation" computer project has met with little success in Congress. Several influential spokesmen called it a "road show" which appealed only to those already interested in the subject and did nothing to explain the importance of the research to a public "already concerned with cuts for funding of federal social welfare programs".

Solar cell shipments boom

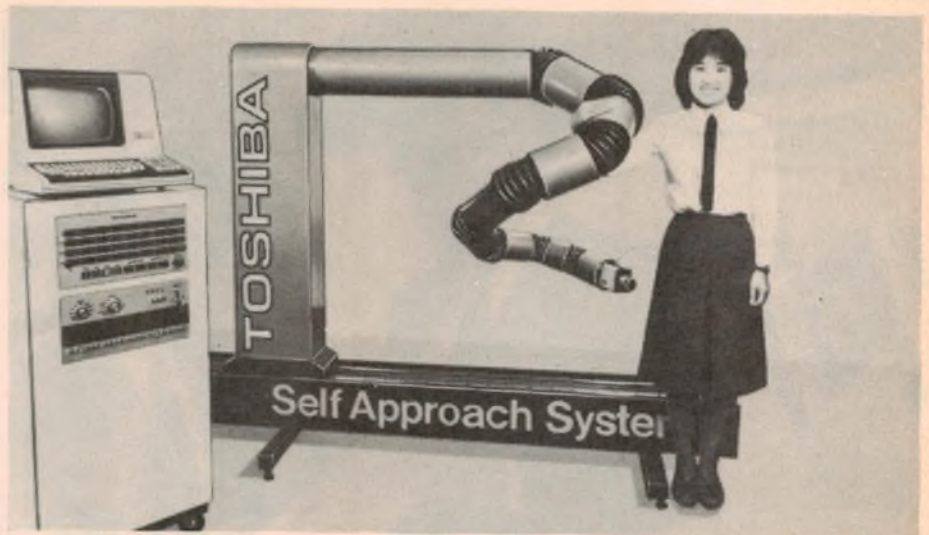
Shipments of photovoltaic solar cell modules boomed last year with an estimated 133% increase. Solar cells with a capacity equivalent to 21.7MW were fabricated and distributed, compared to 9.3MW in 1982. Most of the increase is ascribed to American solar projects financed by tax concessions and the Japanese use of solar cells in consumer products such as calculators.

Expansion of Australian microelectronic research

The Minister for Industry and Commerce, Senator John Button, officially opened new microelectronics research facilities at the Royal Melbourne Institute of Technology in April.

The new facilities have been installed with the assistance of the Commonwealth Government's Special Research Centre scheme.

A Joint Microelectronics Research Centre was established with a \$2 million grant to two institutions, the University of NSW and RMIT in February 1982. At RMIT the grant has been used to undertake major improvements to microelectronics laboratories, to purchase key



Robots versus the Japanese workforce

The worm, it seems, is about to turn! The "worm", in this case, is the Japanese worker, and the subject of his wrath is the increasing use of industrial automation. Until recently this area of Japanese industry has appeared, outwardly at least, to be relatively trouble free, but it has suddenly run into a wall of resistance from human workers.

Half-a-million workers in the electrical machinery industry have said they will not co-operate in any more automation schemes unless they receive guarantees on job security, retraining, and safety conditions. The Federation of Electric Machine Workers Unions, representing the workers, wants guidelines on the use of robots written into labour contracts this year, the first time such a demand

has been made by a major group of unions.

The unions have called for more consultation before the arrival of new labour-saving robots and are seeking guarantees of job security and work safety. The call for industry-wide guidelines follows one landmark agreement between the management and 74,000 workers at Japan's Nissan Motor Company.

That agreement calls for plans for the use of robots to be shown to workers first, prevents the company from dismissing any worker whose job is taken by a robot, and guarantees that working conditions for humans will not deteriorate in robot factories.

Nissan has nearly 1,000 robots operating in its car factories, and Japan's overall production of industrial robots is expected to grow by 25% this year, with 30,000 automated machines being built.

equipment, and to recruit full time research and technical staff.

The RMIT Microelectronics Technology Centre conducts research and development in three main areas: research into semiconductor materials and production processes; development of computer-aided design tools, skills and software for integrated circuit production; And the establishment of a silicon chip manufacturing facility. Researchers have already achieved results of international significance in the areas of ion implantation and the "doping" of silicon, a "stitching" process which improves the adhesion of thin films of metal to other materials, and in the production of gallium arsenide integrated circuits.

The Government funding and the new facilities at RMIT "has given an enormous boost to Australian microelectronics research. It has

facilitated the build up of a professional research team, and access to top-class laboratories" says Dr Jim Williams, director of the RMIT Microelectronics Technology Centre.

"By selecting areas of research which are specifically geared towards Australian expertise, and are commensurate with Australian industry, it is possible, for the first time, to both compete and collaborate with leading overseas laboratories. For instance, RMIT has strong collaborative links with Bell Telephone Laboratories and recently IBM announced a major research agreement with the Research Centre at the University of New South Wales. Such international collaboration allows Australian scientists to keep abreast of rapidly changing high technology", he said. (See New Highlights, EA April 1984 for details of the IBM agreement).

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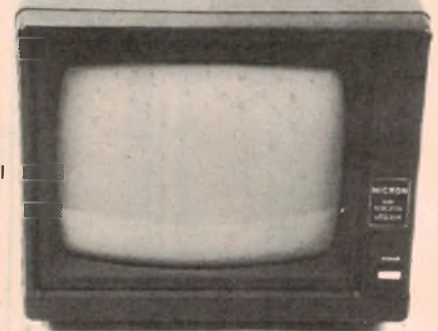
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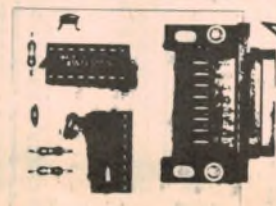
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 (See Review ETI AUGUST 1983)

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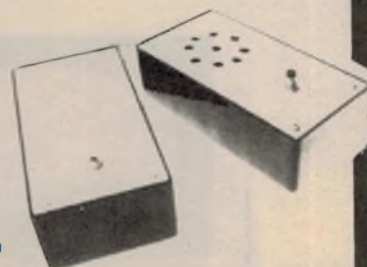
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Buying your first computer

Many thousands of people have bought computers for the home and perhaps many more would if they knew what they were all about. If you think you'd like a personal computer but are unsure which way to go, read on.

by PETER VERNON

Buying a computer is not a decision to be taken lightly. At the very least a small computer will set you back about \$200 and that's without any of the essential accessories, programs and books that go with the hobby. A personal computer can quickly become an open invitation to spend money. How can you be sure this money is well spent?

The first step is *not* to rush out to a dealer or computer store. Instead, do some work with pencil and paper to define your own requirements. What do you want a computer to do? The expected applications of a computer define what is required by way of memory size, screen display format, keyboard and accessories.

The Commodore 64 is one of the largest-selling computers in the home market. Features include 16 colour graphics, sound effects and plug-in software cartridges for games and home management applications. While it is a system with a lot of potential considerable programming effort is required to bring out the best in the machine because of the limited Basic language supplied. See EA June, 1983 for an in-depth review.

Personal computer applications

By far the most popular use of a computer in the home is to play games, with educational applications a close second. Word processing, home management, control of household appliances and communications are other uses. With the increasing number of computer clubs, owning a computer can also be an introduction to a large circle of friendly, like-minded people.

There are some things, however, which buying a computer will not do. It will not make you into an expert programmer — no more than buying a piano will make you a musician. Long

hours of learning and practice are required to master anything but the simplest programming.

Nor will owning a personal computer guarantee you a job, although it can help. Some people have graduated from a computer club to working with a computer manufacturer or distributor of computers or software, but the competition is fierce and opportunities are scarce. Familiarity with computers can have indirect benefits at work, or may impress a prospective employer!

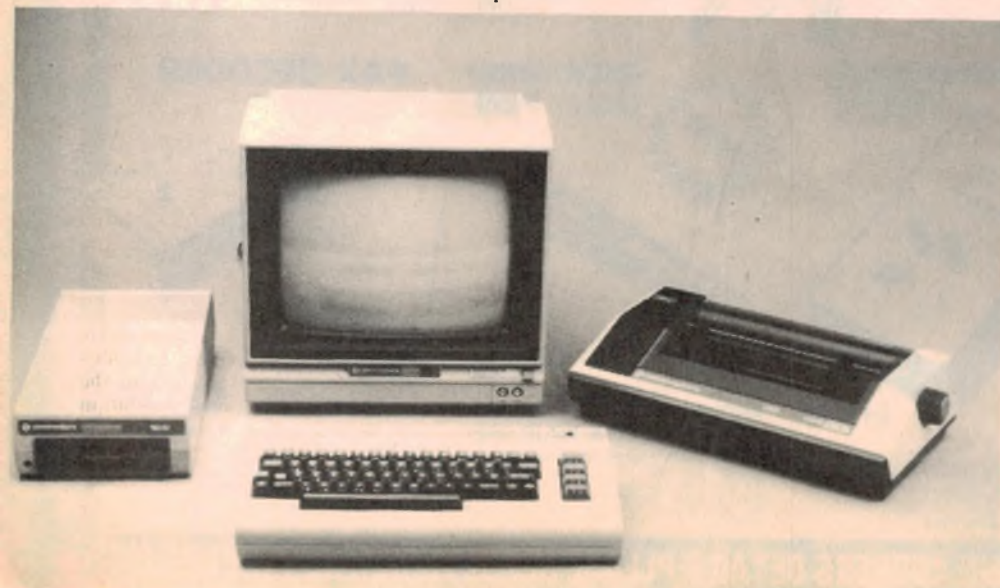
What to look for

Having decided what a computer can and cannot do for you the next step is to start looking around. Read reviews, advertisements and the brochures produced by manufacturers and retailers. Talk with other computer users but remember that they are the last place to go for unbiased advice. To most users, the best microcomputer is the one they own!

If your primary interest is games, look at the capabilities for colour graphics, sound effects, joystick facilities and available software. Although games programs are sold for computers which do not have a colour display capability, they are intended as adjuncts to other applications. Colour adds immeasurably to the impact of computer games, so if this will be the main use of your computer there is little point in going for a monochrome display.

The features required for educational uses of a computer are similar to those required for a games machine. The best educational software uses colour graphics, sound effects and interaction to maintain the student's interest. Old style "drill and practice" programs are rarely worth buying.

For word processing and information management, colour is not an essential requirement. The ability to display both upper and lower case letters and a reasonably sized text display are much more important.





The standard screen format for business word processing is 25 lines of 80 characters each. Home TV sets, even those converted for direct video entry, just do not have the bandwidth required for a legible display of this line length. It is for this reason that most low cost computers display 32 or 40 characters per line. Longer lines exclude the use of colour.

If colour is not required, a monochrome monitor or converted black and white television receiver can be used. The legibility of the display will depend on the bandwidth of the monitor. Television receivers converted for direct video entry can be used to display 64 character lines, but for a crisp 80-column display a higher priced video monitor will be required.

The VZ-200 from Dick Smith Electronics is one of the lowest-cost systems on the market. It offers low resolution graphics in eight colours and limited sound effects but is a good starter system at around \$200. The Tandy MC-10 is comparable. The July, 1983 issue of EA contains a review of the VZ-200.

A video monitor is just one of the "hidden costs" of a personal computer. Prices range from around \$200 to over \$700 for a 34cm (diagonal) colour unit, although the experienced electronics enthusiast can save some of the cost by converting a surplus television set, as described in the August, 1983 issue of EA. As well as allowing full time use of a computer, a video monitor generally provides a sharper picture and is less prone to interference than a television set driven by an RF modulator.

Note however that some computers limit the choice of methods. Some, like the VZ-200 and Commodore 64, provide

both modulated RF video and direct video output, while others such as the TRS-80 Color Computer provide only a modulated RF output, and cannot be used with a monitor unless the case is opened (voiding the warranty) and additional connections made. Others, such as the VIC-20 and TI-99/4A require an RF modulator in the form of an external box, usually supplied with the computer.

Naturally, a printer is also required for word processing applications. We won't go into the relative merits of dot matrix, thermal and daisywheel printers here, other than to point out that a printer can cost much more than the computer itself. Unless word processing is going to be your main application it is not necessary to purchase a printer immediately. Wait until the need becomes evident.

More important, however, is a place to connect the printer. A surprisingly large number of personal computers are not equipped with either parallel or serial ports but require separate "printer cards" and communications interfaces as an extra cost option. Other computers can



Tandy's TRS-80 Color Computer is available with one of two versions of Basic. Extended Color Basic is required to make use of the computer's sound and high resolution graphics capabilities. Other features include plug-in cartridge software and a range of disk operating systems.

Buying your first computer

be used only with a printer from the same manufacturer because they use a non-standard interface. Since these printers are usually more expensive than standard types, another extra cost is involved.

If your main use for a computer is to learn about hardware and design techniques, access to the circuitry of the computer is important. Adding your own devices to a computer is one of the best ways to develop an understanding of the principles of computer engineering. If this is impossible, either because the system is not readily expandable or there is no information available on the expansion facilities, the computer is not suitable for the electronics hobbyist.

Documentation is important here, however. The mere presence of an expansion port or cartridge connector is not enough unless there is sufficient information available to allow the use of the facilities. At the very least, a description of the pin-outs of the connector and the allocation of memory is required.

Graphics — what's available

Graphics capability depends on two factors; the number of different colours which can be displayed on the screen and the resolution of the display. Resolution is usually expressed as the number of dots or "pixels" which can be displayed across the screen by the number which can be displayed vertically. (Pixel stands for picture element.) The more dots



Discontinued last year by TI because of marketing problems, the Texas Instruments TI-99/4A is currently available at bargain prices. Features include excellent colour graphics (including 32 sprites) and sound effects, and a very good version of the Logo language. Some software in plug-in cartridges is still obtainable at dealers and the computer is supported by a very active users group with branches around Australia. This system was reviewed in the December, 1982 issue of EA.

horizontally and vertically, the smaller the size of each dot and the greater the detail which can be displayed.

For systems costing less than \$500, 16 colours and a resolution of 256 (horizontal) by 192 (vertical) are reasonable. Like most aspects of personal computers however, graphics capabilities

can be expressed in many ways, some of them ambiguous. A reference to 16 colours, for example, always includes black and white as colours. There are also trade-offs between colour and resolution. Some computers restrict the use of colour in high resolution displays because of memory or processing limitations.

Computers such as the VZ-200, TRS-80 Color Computer and the MC-10 provide low resolution "chunky graphics" and boast eight colours. In actuality, the low resolution graphics mode only allows four colours to be displayed simultaneously, selected from one of two sets. Since the background of



The CAT computer from Dick Smith Electronics is one of the newest on the market. For \$699 it offers limited Apple II compatibility and enhanced graphics and sound, while a \$99 "soft emulator" is available to allow the CAT with a disk drive to run the majority of Apple II software. A detailed review of this system appeared in EA in May, 1984.



The Atari XL computer system forms a compatible range from the 600 to the 800 and up. The family is known for extensive colour graphics, ease of use and the availability of a wide range of software and peripheral equipment. The 600XL shown here comes with 16K of RAM, and is expandable to 64K.

the display must be one of these colours, actually only three colours are available from graphics displays.

The TRS-80 Color Computer has a higher resolution (256 x 192) graphics mode, but only two colours are available in this mode. Of the popular personal computers only the Atari, VIC 20, Commodore 64 and Texas Instruments TI-99/4A allow 16 or more colours with relatively high resolution.

Another factor contributing to ease of programming for games is the availability of "sprites"; blocks of graphics which can be defined and moved independently of the remainder of the display. Because sprites ease the task of creating animated displays they can allow "arcade quality" video games programs to be written, even in a slow language such as Basic. Used with assembly language, they allow effects which frequently surpass dedicated video games machines.

Music and sound effects

Sound effects add considerably to the impact of computer games, quite apart from the opportunities provided for learning music theory. Computer circuits for producing sound can be divided into two types — so-called "single bit" sound and those that use a separate sound generator chip.

Single bit sound, as the name implies, uses one line of an output port to drive a transistor amplifier and speaker. Some

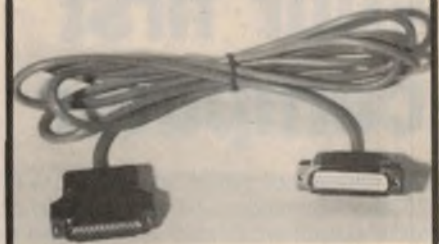
systems use more than one line, however, driving and rudimentary digital to analog converter. The significant point is that the frequency and duration of the sound is controlled by the microprocessor, so all other operations come to a stand-still while sound is produced. Simultaneous sound and movement, for instance, can only be programmed with difficulty.

Computers using dedicated sound generator chips, such as the Commodore 64's "Sound Interface Device" (SID), provide a wider range of sounds, including white noise, and produce sounds simultaneously with video displays and other processing. Often the volume of the sound can also be controlled by software, unlike the single bit approach.

The other factor to be considered is the means of sound output. Methods range from incorporating an internal speaker (as in the Apple II and lookalikes) to modulating the sound onto the RF video carrier (as with the Tandy Color Computer and Commodore machines). When computers which use this method are connected to a video monitor the sound is lost unless the monitor includes a speaker and provision is made for a separate audio connection.

Few direct entry video monitors include an audio input (one exception is the Dick Smith monitor, actually a converted portable television set). For

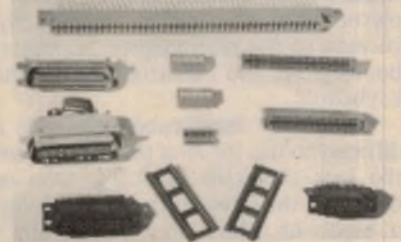
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Buying your first computer

this reason, computers such as the VIC 20 and Commodore 64 have a separate audio output which can be connected to an external amplifier.

Keyboards

The type of keyboard available on a personal computer also affects its usefulness for a variety of roles. Generally keyboards are of three types; flat plastic membrane switches, such as those of the Sinclair ZX81, rubber or plastic buttons (so called "chiclet" style, because of the resemblance to pellets of bubblegum), and full-stroke "typewriter" keyboards.

Flat plastic membrane keyboards are difficult to use for long periods because of the lack of tactile feedback. One user described the sensation as "like typing on a block of wood". In an attempt to overcome this, most such systems provide an audible "beep" to indicate that a keystroke has been registered.

Half-way between flat keyboards and full typewriter style are "pushbutton" keyboards, as used by the TRS-80 Color Computer and the IBM PCjr. This type of keyboard is easier to use than the flat



The MPF-III provides Apple II compatibility in a compact, low profile design with detachable keyboard. Features include an 80-column display, 64K RAM, printer and cassette ports and an Apple compatible hardware expansion slot. As yet however, no colour graphics are available. The February 1984 issue of Electronics Australia has a review of the system.

type and is more suitable for applications around the home.

Apart from the style of a keyboard there are very few guidelines which can be laid down. Separate numeric keypads, while convenient on office computers

used for large scale data processing, are of little use on a personal computer. Far better is a cluster of cursor control keys and special function keys which can be re-defined by the user.

As long as a keyboard is comfortable there is very little to choose between alternative offerings. Any keyboard used for more than a month tends to become a natural arrangement, and one quickly becomes familiar with various quirks and foibles.

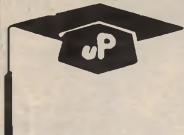
Software

The availability and method of loading software is one of the most important aspects of a computer to be used in the home. By far the best method is the solid-state ROM cartridge, which avoids the problems and delays caused by loading a program from disk or cassette.

Most of the popular low cost computers for home use are designed to accept program cartridges, but cartridges

The Australian-made MicroBee computer has attracted a lot of attention from home and educational users. This is one of the few low cost machines to offer text displays of more than 40 characters per line (almost essential for word processing) and is supplied with a range of software. The photograph shows the start-up menu of WordBee, the MicroBee's built-in word processor. The MicroBee IC model was reviewed in EA in November 1983.





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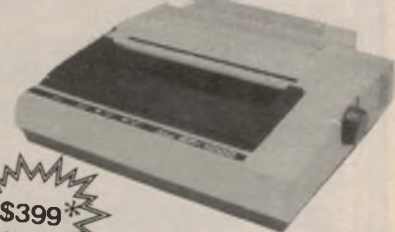


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3" COMPACT FLOPPY GRABS LEAD IN STANDARDS RACE

Chinon Industries of Japan recently joined the ranks of companies supporting the \overline{C} -standard. This compact 250KB (500KB in floppy mode) storage unit features low power consumption and 5¼" compatible operation. Chinon's CFO31 has a 3ms track-to-track access time and uses standard Compact Floppy media. Schools and remote recording applications will benefit from the rigid jacket and dust protection features of Compact Floppy disks.

GENERAL INSTRUMENTS' SPEECH RECOGNITION CHIP SPEAKS FOR ITSELF

Claimed to be the only real-time linear-predictive-coding-analysis chip on the market, this chip, when teamed with a micro-processor, manages both recognition and synthesis with just one reconfigurable filter. Known as the SP1000, the combo chip will work with most micro-processors and will also work with no hardware interface with the 6502 device.

WESTERN DIGITAL CORP. RIDES THE IEEE STD 488 BUS

A general purpose interface bus (GPIB) controller performs the interface function between the micro-processor and the GPIB. Western Digital's WD9914 is a second source for TI's TMS9914A. The chip automatically handles talker, listener and controller operational modes, relieving the micro-processor from bus protocol maintenance. The WD9914 features system controller service request, serial/parallel polling device, clear trigger and DMA facilities. Look for this one early 1984.

IBM® PC STYLE KEYBOARDS TO TRUE DIN PROFILE

Advanced Input Devices' packaged and encoded keyboard features ergonomically designed tactile feel keys and comes complete with curly cord. Measuring a mere 30mm in height to the home row of keys, the Ergokey Tm ED-184-243 also incorporates a two position angle adjuster. This keyboard is the vanguard for the Ergokey Tm series and is predicted to cost less than \$200 plus tax in small quantities.

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Buying your first computer

intended for one type of machine are not transferable to another. The range of programs available in this form may also be limited, so it is best to assess the variety and cost of program cartridges available for a particular computer before committing yourself to a purchase.

Other programs may be distributed on disk or cassette, and in any case you'll need some form of "mass storage" to permanently retain copies of your own programs and data. The lowest cost method is to use a standard cassette recorder. Disk drives are faster, but more expensive, and are better left until you have some experience with the computer and come to feel the need for faster response time and greater storage capacity.

Be aware that some computers cannot use an ordinary cassette recorder. They require a specialised device made by the computer manufacturer and often selling for twice the price of a budget portable cassette player. The Commodore VIC 20 and 64 and the Spectravideo machines follow this practice. The VZ-200 also requires a comparatively expensive cassette player for reliable performance.

Memory size and the choice of a processor

Surprisingly, the size of a computer's programmable memory is not as important as it first appears. Most personal computer systems are provided with enough memory for typical applications, while those using software ROM cartridges can run programs without reducing the size of RAM.

Because of the low cost of dynamic RAM chips, memory sizes of 16K are most common, with expansion in increments of 16K. One "K" is 1024 bytes or characters, but because Basic programs are usually stored in a compressed form, more space is available than would first appear. Machine language programs, of course, are even more compact.

16K of memory is adequate for programming and educational applications. Word processing may require more, as a single typed page may contain around 2400 characters, limiting in-memory storage to around seven pages of text in 16K.



The Spectravideo SV-318 offers colour graphics and sound effects and a built-in joystick for \$399. The graphics mode features 32 "sprites" or patterns which can be defined and moved around the screen independently of the remainder of the display, easing the task of writing fast-moving games and other display programs. The larger SV-328 does not have the built-in joystick but offers a larger, full-stroke keyboard. See EA for February 1984 for a review of the SV-318.

As important as the absolute size of a computer's memory is the use made of it. All computer operating systems require some RAM for storage of temporary variables and for display memory. What matters is "usable memory", which can be quite different from the total memory advertised. The Commodore 64, for example, is commonly advertised as a 64K system, but in fact only around 31K is usable from Basic.

The important distinction to be aware of is the difference between RAM and ROM. RAM, or Random Access Memory, holds the user's programs and data. ROM holds the computer's operating system and (usually) a Basic interpreter.

Read Only Memory size can vary between two models of the same computer. Many machines, such as the TRS-80 Color Computer or the TI-99/4A, offer two versions of Basic, one standard and the other an extra-cost "Extended" version which is required to make effective use of the computer's graphics and sound capabilities. You should be aware of which version you are getting for your money, as the most advanced facilities are usually only available with Extended Basic.

So far no mention has been made of the varieties of microprocessor chips

which form the basis of all personal computers. There is a good reason for this — if a computer has the capabilities that you want, it doesn't matter which microprocessor it uses. Debates on the merits of the 6502 or Z80, or 8-bit versus 16-bit processors are irrelevant to the actual applications of a computer in the home. If a machine does the job that you want it to do, what more can you ask?

In conclusion

A computer console, cassette recorder and a television set are enough to get you started in personal computing. It is only a start, though not the end of the road (or the expense). If you intend to keep up the hobby, look for an expandable system which is well supported by software supplies and publishers.

Consider joining a computer user group, possibly even before you purchase your own computer. As a source of advice and assistance, for a subscription of around \$20 per year, such groups are worth their weight in microchips!

In the end however, the decision on what sort of computer to buy is your own. The more time you put into defining your own requirements and applications, the easier the final choice will be.

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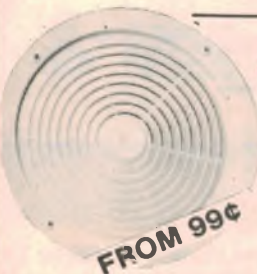
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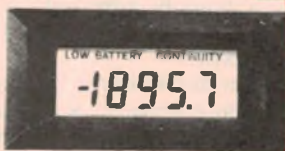
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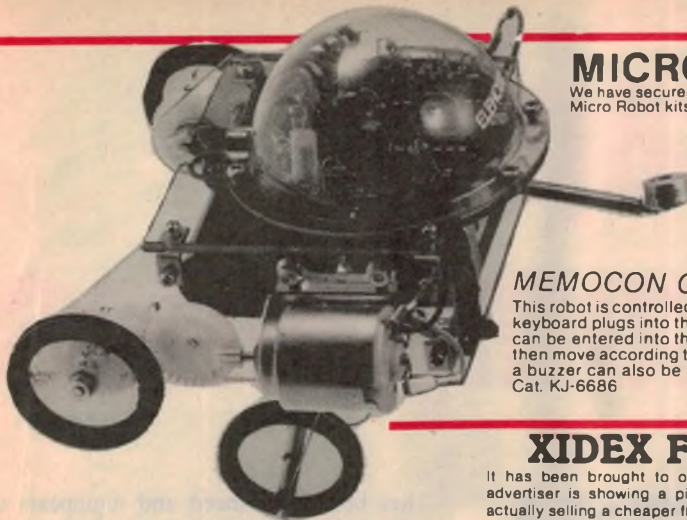
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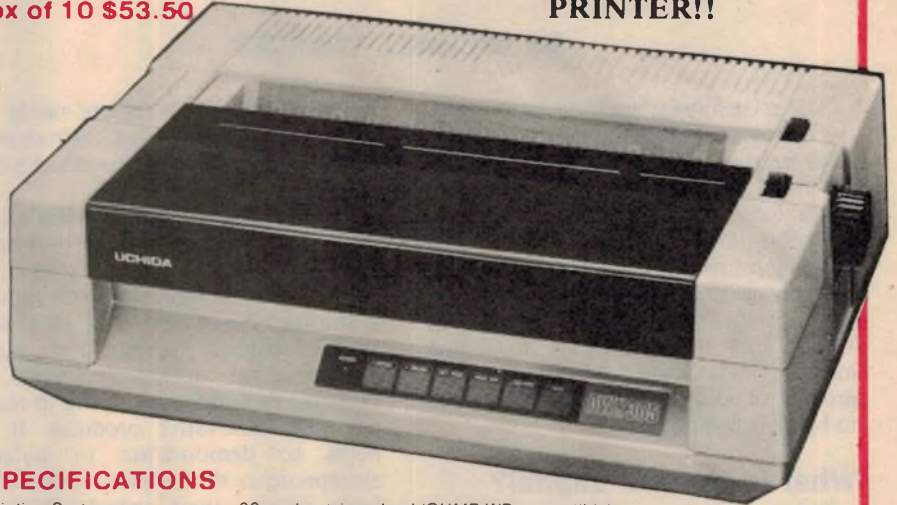
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Venture capital for new companies

The development of new ideas and products is often hampered by a lack of money. Recent efforts by the Federal Government to establish a venture capital market in Australia will change this situation.

by MICHAEL WILKINS

The prize money has been announced, the referees are in place, the rules of play have been set and the potential players are ready to take centre stage — Australia's fledgling venture capital market is almost set to go. But what will the establishment of this market mean to the average man in the street who has a good idea and an entrepreneurial nature? What, too, will it mean to home inventors who have discovered a new product or service, but need the finance to bring it to market?

What is venture capital?

Before starting any discussion of initiatives or incentives, I think that it is important to understand what is meant by the term "venture capital". Venture capital is just what the name suggests — capital which is available for investment in worthwhile ventures. However, it is more than that — it is risk capital which is invested in companies or products which would not normally be eligible for financing by a bank or finance company. Often, these funds are invested in little more than a person or an idea.

The establishment of a venture capital market in Australia is a direct result of the Federal Government's desire for the nation to adopt a more aggressive role as an exporter of high technology products. They appear to have recognised that traditional heavy manufacturing industries can no longer provide the

stimulus that our economy needs and, accordingly, have focused their attention on the development of so-called sunrise industries.

Overseas experience, particularly in the US and UK, has shown that one of the best ways to nurture the development of new high-tech products is through the operation of an efficient venture capital market. This market ensures that sufficient funds are available to develop and bring to market new and innovative products. It also helps to demonstrate to potential entrepreneurs the benefits to be derived from owning their own business and from taking a chance to back a product that they believe in.

Venture investors also need to be encouraged to take a chance. As they are making significant funds available for investment in untried persons or products, they naturally expect a correspondingly higher rate of return. However, these high returns are not always achieved and, in cases where a product is a failure, their total investment is lost. Recognising this fact, the Federal Government has introduced a series of incentives designed to encourage people to provide funds for use in venture investments.

These incentives take the form of taxation deductions and will be available to persons or companies who subscribe funds to venture capital investment companies. These companies are to be known as Management and Investment Companies (MIC's) and will be administered by a Government formed MIC Licensing Board (MICLB).

The initial membership of this Board

has been announced and it appears to contain a well-rounded group of people drawn from all walks of life. The Government has indicated that \$40 million worth of taxation deductions will be allowed in the first year and this amount should be extended in the second year of operation of this scheme.

These MIC's will be required to provide capital and, if necessary, management expertise to suitable "Eligible Businesses". The eligibility of businesses in which an MIC proposes to invest must be certified by the MICLB prior to this investment being made and a series of criteria have been established for this purpose. Basically, Eligible Businesses must be primarily engaged in one of the following fields: manufacturing; agriculture, forestry or fishing; producing postal, teleprinter, telephone or telegraph communications services; architectural services; computer software; consultant engineering services; traded educational and training services; scientific and technical services; data processing services.

In addition to these criteria, there are requirements for growth potential and company size. In order to be designated as an Eligible Business, a company must have:



The author is a specialist in venture finance with the Sydney chartered accountants firm Deloitte, Haskins & Sells.



- A projected average annual sales growth of more than 20% over the next three years of operation; and
- Less than 100 employees or less than \$6 million in net assets.

If you feel that you and your product meet these criteria (and you must admit they are very wide) then read on. Even if you don't quite measure up to these requirements, continue reading — there's more good news.

Most companies and persons who have indicated that they have funds to invest in the venture capital market will not be constrained by the Government's criteria. What they will, however, be looking for is a person or product which they believe is viable and which has a reasonable chance of success.

The best way to make contact with a venture capitalist is through an introduction which can usually be arranged by a chartered accountant or solicitor. But before making this contact, be sure that you understand the information requirements that venture investors have and the products in which they are prepared to invest.

A business plan

Almost without exception, prospective investors will require a business plan. This document is a concise summary of your overall strategy in regard to your product, the amount of funding needed to develop and support that product, and the persons who will assist you to ensure that your product will be a success. Ideally it should include:

- a complete description of the product and its manufacture;
- resumes of all people involved in the project, including those who are to be involved in the day-to-day running of the business;
- market statistics (eg market size and segmentation);
- information regarding potential competitors and their products;

- details regarding potential customers (eg persons who have indicated a need for and an interest in purchasing your product);
- research and development information.
- regulations or laws (including relevant patent and copyright information) which may affect your product;
- type and amount of funding required and the uses which are to be made of it.

As much of the information to be included in a business plan is of a highly complex nature, particularly in regard to the financial projections, it is not uncommon for a consultant to be employed to assist with its development. A chartered accountant can usually assist with this preparation, or can arrange to introduce you to persons who can assist you.

What about research?

If you are thinking of seeking venture financing to develop your product, it is useful to be aware of the stages at which venture capitalists will become involved. Due to the limited amount of funds presently available in Australia for venture investment, large quantities of research and development (R&D) funds (seed capital) are not available. Rather, venture capitalists will be more willing to examine proposals which are based on a proven working model or prototype of the item which is to be produced. They are more likely to become involved with a product which has already been technically proven as they believe these products will have a better chance of success.

Recognising the need to promote the development of products at their conceptual or R&D stage, the Federal Government and various State Governments have made available a number of grant and loan schemes. Probably the best known of these is the

Industrial Research and Development Grant which provides up to \$60,000 for eligible expenditure on research and development projects.

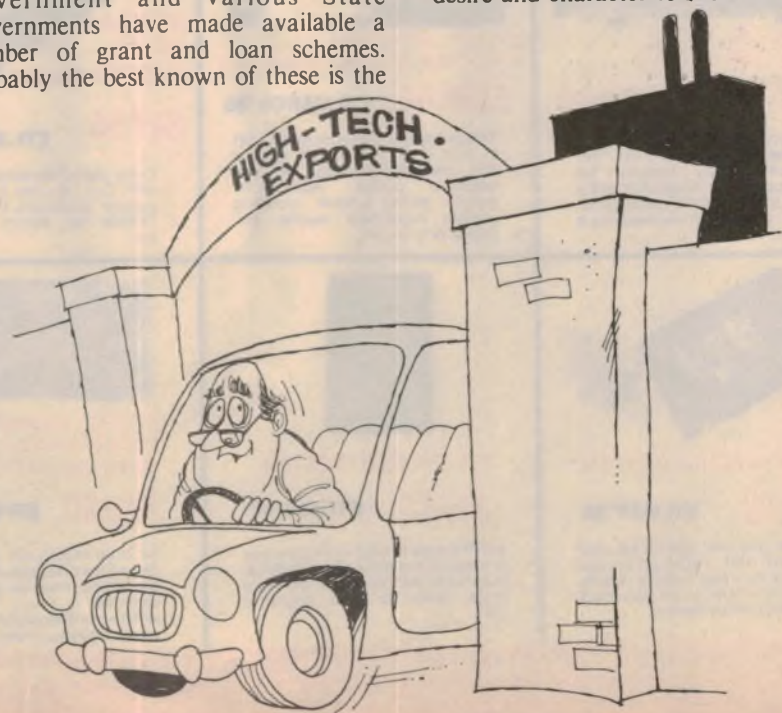
A number of similar grants and subsidies are available and a chartered accountant will be able to advise you regarding the steps necessary to obtain these.

In conclusion

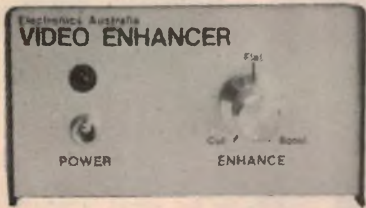
What does all of this mean for the person with a good idea or product and the desire to develop it? It means that now, more than ever, is the time to seek funds to develop these products. Through a series of direct incentive grants and the encouragement that is being given to the establishment of a venture capital market, the Federal Government is actively seeking to place Australia in the forefront of the development of new technology.

The Government, in its plan to encourage Australian innovation, appears to have catered for all types of products at all stages of development. The criteria as to what constitutes an Eligible Business is exceedingly broad and the incentives being offered to people willing to invest in MICs are very generous.

Recognising, however, that these MICs may not always provide finance for ideas which are still on the drawing board or in their early stages of development, the Government has established R&D and numerous other encouragement schemes. As mentioned earlier, now is the time to reap the benefits made available by the provision of these sources of finance. All that is needed is a supply of innovators who are willing to take a chance on themselves and their product and who have the desire and character to succeed!



100's SOLD
VIDEO ENHANCER \$35



Like tone controls in a hifi amplifier, touch up the signal with this Video Enhancer. EA OCTOBER 83

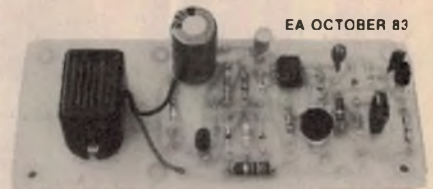
NAIL FINDER \$10



Essential for the home handyman the Nail Finder will help locate timber studs behind Gyprock or plasterboard wall surfaces as well as locating pipes and wiring buried in walls

EA OCTOBER 83

SPEED SENTRY \$21



EA OCTOBER 83

Paying speeding fines can be a painful business. Build this Speed Sentry and avoid further pains in the wallet

1000's SOLD

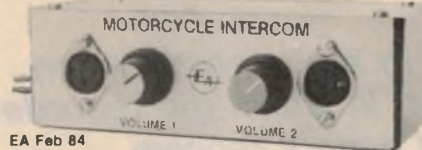
TRANSISTOR TESTER \$15



Have you ever desoldered a suspect transistor, only to find that it checks OK? Troubleshooting exercises are often hindered by this type of false alarm, but many of them could be avoided with an "in-circuit" component tester such as the EA Handy Tester.

EA SEPTEMBER 83

MOTORCYCLE INTERCOM \$40

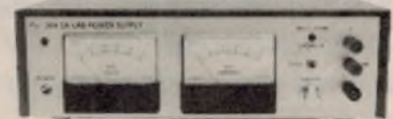


EA Feb 84

Motorcycling is fun but conversation between rider and passenger is usually just not possible. Build this intercom and you can converse with your passenger at any time while you are on the move.

OVER 300 SOLD

50V 5A LABORATORY POWER SUPPLY



New switchmode supply can deliver anywhere from three to 50V DC and currents of 5A at 35V or lower. Highly efficient design

EA May, June 1983 **\$2 PS5 \$140.00**

SLIDE CROSS FADER



CAR IGNITION KILLER



Our kit includes the metal box **\$16.95** EA Feb 84

Most car burglar alarms are easily circumvented, but not our cunning "Ignition Killer". This sneaky anti-theft device uses a 555 timer to place an intermittent short circuit across the points. Until disabled by its hidden switch the circuit effectively makes the car undrivable — a sure deterrent to thieves!

CAR ALARM \$29.00



This Car Alarm uses the battery earth strap as a sensor to detect when a "courtesy" light or other electrical load occurs when a thief enters a vehicle. The circuitry is simple and immune from false triggering problems. ETI July 81

PHONE MINDER \$25

EA Feb 84



Dubbed the Phone Minder, this handy gadget functions as both a bell extender and paging unit, or can perform either function separately.

VIDEO AMPLIFIER \$15



EA AUG 83

Bothered by smeary colours, signal beats and RF interference on your computer display? Throw away that cheap and nasty RF modulator and use a direct video connection instead. It's much better. The Video Amplifier features adjustable gain and provides both normal and inverted outputs. Power is derived from a 12V DC plugpack supply. **INCLUDES JIFFY BAG**

±12V RAILS FOR LAB POWER SUPPLY

EA July 1983



\$13

An inexpensive addition to the 50V 5A Lab Power Supply which should prove its worth many times over. It provides additional fixed ±12V outputs for lower power applications.

Electric fence \$19.50



Check our prices

SEPTEMBER EA 1982

Mains or battery powered, this electric fence controller is both inexpensive and versatile. Based on an automotive ignition coil, it should prove an adequate deterrent to all manner of livestock. Additionally, its operation conforms to the relevant clauses of Australian Standard 3129.

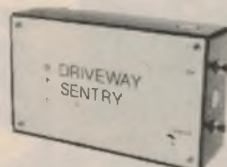
LOW OHMS METER \$34.50

How many times have you cursed your Multimeter when you had to measure a low-value resistance. Well alas, with the "Low Ohms Meter" you can solve those old problems and in fact measure resistance from 100 Ohms down to 0.005 Ohms. ETI 158 November 81



Driveway Sentry

\$32



Activated by your car's headlights, the "Driveway Sentry" will turn on a driveway or garage light so that you can make a safe exit from your car on the darkest of nights. At the end of five minutes, it will automatically turn the light off again.

EA GUITAR BOOSTER

\$17.50



JUNE EA 1982

A novel all-in-one video player/monitor

Who could possibly want to buy a combination video recorder and TV set, in which the recorder cannot record and the TV cannot receive television stations? According to a small company in Sydney, there are quite a few customers out in the marketplace ready and waiting to pay good money for just such a product.

by NEVILLE WILLIAMS

The Company concerned, Tracker Electronics, has specialised to date in servicing audio visual equipment, primarily for major clients such as the AVES Group and Telex Australia. In the process, they have become increasingly aware of video-based AV (Audio Visual) equipment, with its potential — and its limitations.

One such limitation caught the eye of David Digger, co-founder of Tracker Electronics. He noted that

representatives needing to show a video tape to a client had to rely on portable equipment providing, typically, a 13cm (diag) picture.

When a larger picture was required for a larger audience, representatives appeared to have no option but to take along a VCR and a separate TV receiver, clear a space to put them, connect cables, push buttons — and hope everything worked. No one, it seemed, had come up with a larger-screen composite video



The Labelle "Showman", a traditional point-of-sale AV unit using film strip and audio tape. The screen size is about the same as that of the VS-1.

player/monitor designed for AV situations.

David Digger wondered why? Could it be that nobody had got around to it yet? Perhaps the concept had been a bit too specialised for large companies and a bit too demanding for small ones!

Questions in the marketplace seemed to confirm the need and also suggested a further potential demand from schools and colleges. Most educational institutions, these days, have VCRs and monitors, sometimes separate, sometimes trolley mounted, sometimes in wired systems. The problem is that they are not always available or accessible for brief, spontaneous use. It would be quite a boon if a teacher could pick up a self-contained video playback unit and use it at any time in a classroom for a five or ten minute video segment.

Should such a unit be designed for playback only or retain the ability to receive and record TV programs off air? On balance, it seemed likely that the units would be used, most of the time, to play back tapes recorded elsewhere — professionally or privately. A playback-

Greg Roberts (left) and David Digger with the new Tracker VS-1 video player/monitor.



only unit should be simpler to operate, cheaper to manufacture and, as AV equipment, might attract only 20% sales tax as against 32½% for a receiver/recorder.

It seemed like an opening and a challenge for Tracker Electronics — one that they felt they had the background and the ability to meet.

In his younger days, David Digger had been trained in Britain as an engineer but, somewhere along the line, he took a step sideways into photography. For a while, he took technical pictures for industrial and commercial engineering firms but later spent seven years touring the world as a professional photographic expert on board luxury liners. There he met his future wife, and the English/American duo decided to make their home in Australia in 1971.

Digger took a job as Sales Manager of a struggling photographic company, made an abortive take-over bid for it, and then started his own company, importing and servicing photographic equipment. It was successful enough but it was tough going and Digger began to look with growing interest at the audio visual field.

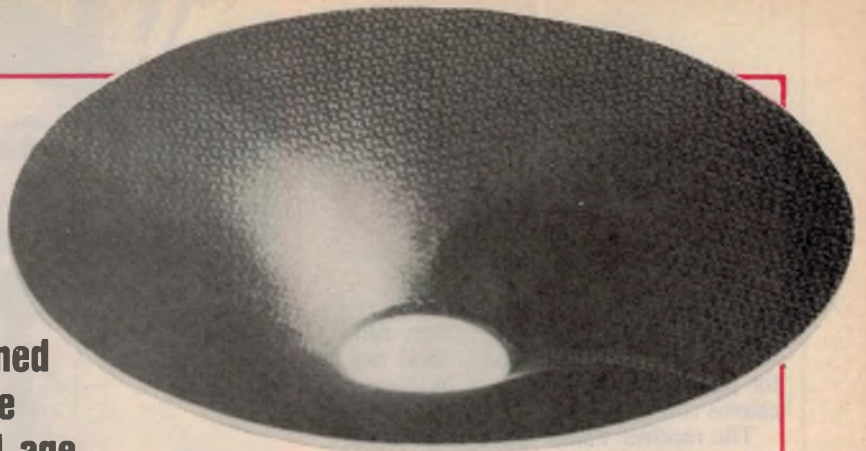
It was about then that he met up with Michael Herts, a very experienced electronic service technician and, in 1979, the two jointly formed a new company: Tracker Electronics. Their concept was to provide complete servicing for audio visual equipment, particularly as operated by large companies. Having one organisation responsible for the total service would avoid the confusion of having different technicians looking at different sections of an installation or of intergrated equipment.

The concept proved sound, contracts followed and Tracker Electronics was on its way. But with the new venture came the awareness of a need for a different kind of audio-video unit and the challenge to expand into manufacture and marketing. Digger and Herts asked questions, looked into the possibilities and decided to give it a go!

In fact, it turned out to be a tough assignment, with size and weight posing early problems. According to David Digger, their first effort weighed the best part of 20kg, even before they had fitted all the parts!

There were problems, too, arising from the concept of operating a VCR, not merely very close to a receiver, but within the same cabinet. The greatest single difficulty facing Michael Herts was in preventing harmonics from the receiver's 50Hz field deflection system from penetrating the video and audio input circuits of the VCR.

They found a way around the size and weight problem by bringing together a standard Sharp 34cm TV receiver and



**Designed
for the
digital age**

New Sansui speaker cone

Described as a product for the digital age, a new loudspeaker cone developed by Sansui is claimed to be the lightest and strongest yet, outperforming not only traditional paper-based cones but other types of multi-layer or "sandwich" construction.

Sansui point out that, in principle, loudspeaker cones must be as light and as rigid as possible if they are to propagate a wide range of frequencies efficiently, without themselves absorbing drive energy or producing spurious sound by reason of surface vibration modes.

With the development of suitable materials and high-performance adhesives, loudspeaker manufacturers have been able to borrow sandwich construction technology from aircraft and boat builders and apply it to loudspeaker cones, particularly those for low-end

and mid-range transducers.

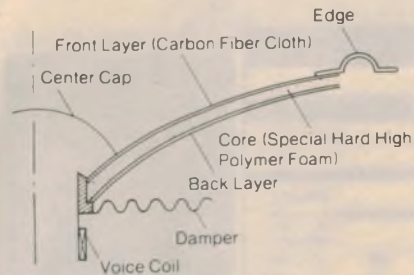
A variety of materials have been used for the outer skin and inner core of sandwich cones including metal alloys (aluminium, titanium, etc) compound plastics and processed paper, along with aluminium honeycomb, paper honeycomb and foam plastic.

According to Sansui, a major problem of many of the combinations is that they can only be produced as a flat disc or a simple cone. They cannot be given a smooth, continuous curve — a shape that, of itself, tends to increase rigidity and inhibit structural resonance.

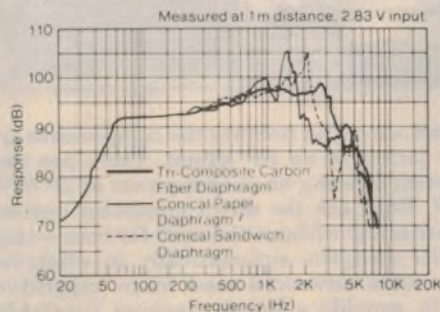
The new cone developed by Sansui has a core of hard, high-polymer plastic foam which is ductile at high temperatures and capable of being formed into the desired shape. It has an airtight surface and good adhesion characteristics.

For the surface layers, Sansui has used a pure carbon fibre cloth bonded to and taking the shape of the core. Since the core is airtight, porosity of the carbon fibre cloth is of no consequence. Weight of the cone according to Sansui is only half that of other comparable but conventional honeycomb diaphragms, while the rigidity is about 350 times that of paper.

They claim that the cone is unique in both design and performance. Because of the convex ("curvilinear") shape, the "tri-composite carbon fibre diaphragm" has fewer peaks and a smoother response than comparable convex cones, of either paper or sandwich construction.



Cross-section of the new Sansui Tri-composite carbon fibre diaphragm.



Comparative frequency response for three different types of cone.

Video player/monitor

National's NV-100A portable VCR — probably the smallest and lightest full-facility VCR available and a good one for portable use by reason of its diecast chassis construction.

The receiver was stripped of its tuner and control panel, and the loudspeaker re-positioned to create a space for the VCR. Part of the side of the cabinet had to be cut away to provide access of the cassette but, that done, the VCR mounted naturally into place.

Internal modifications to the NV-100 limit its use to playback only, an internal connection providing direct signal feed to the video circuitry of the receiver. A separate small supply, mounted inside the receiver cabinet, powers the VCR and obviates any conflict between the direct video feed and the live-chassis design of the receiver.

Because the deflection yoke of the Sharp receiver is unshielded, it was necessary to provide extra shielding for the VCR and to resort to other circuit tricks to obviate interference effects.

Says Michael Herts: "People sometimes say: 'You just pushed a portable VCR into a Sharp receiver' but, believe me, there was a lot more to it than that."



Betamovie helping to boost format sales

According to Mr Haranobu Murakami, Managing Director of Sony Australia, his company is doubly pleased with the reception accorded to Betamovie, its unique combination video camera/recorder. Not only is Betamovie proving popular in its own right but it has helped to boost the Beta format's share of the Australian home video market by 8% during the last quarter of 1983. He stressed Sony's continuing commitment to the format, its acceptance in commercial and Government circles and the impending introduction of Beta hi-fi-stereo sound. Betamovie is compatible with all Beta format VCRs released in Australia and is being sold under their own brand names by both Sanyo and Toshiba.

The new Tracker Electronics VS-1 composite video player/monitor uses VHS format cassettes, conforming to the Pal D colour system. Overall dimensions

are quoted as 446 × 315 × 361mm and the all-up weight as 13kg. Power consumption for receiver and VCR total 67W (at 240VAC). An inverter is available which allows the complete unit to operate from a 12V vehicular supply.

The monitor controls are grouped mainly at the top and rear of the cabinet, while the VCR controls are accessible from the front. Provision for remote control of the VCR has been retained, as also has the "RF Out", allowing the video signal to be fed, if desired, to an external TV receiver or video system via VHF channel 1.

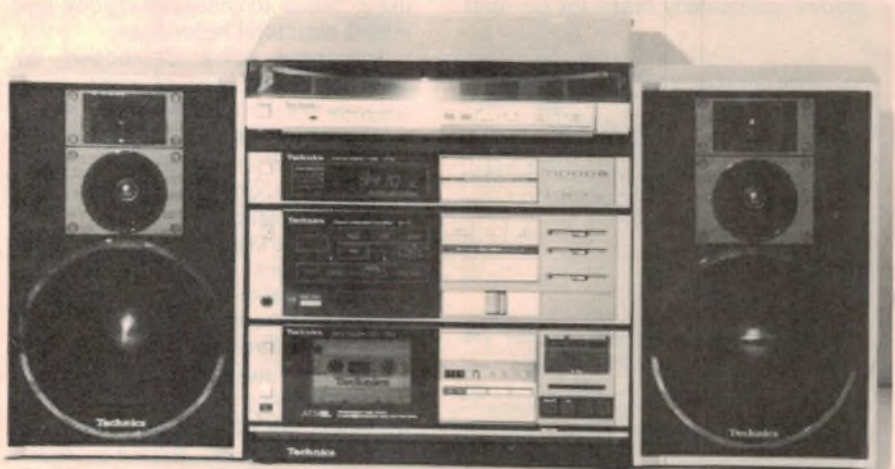
Current price of the VS-1 is quoted as \$2850 including sales tax.

In marketing the VS-1, Tracker Electronics will have the full support of the AVES Group which, for more than 20 years, has been heavily involved in the production of software for the industrial sales, training and education side of the audio visual industry.

At a function to launch the VS-1, Managing Director of the AVES Group, Greg Roberts, had this to say:

"Increasingly, we felt hampered by the clumsiness, the lack of portability of the video hardware available to satisfy the market we were servicing.

"We knew that a truly portable desk top video system would open up areas which up till now have remained untapped."



Pictured above is Technics' new 315 system, so called because the components are all 315mm wide — the same size as the jacket of an LP album. There are two versions at present, the Series 66 (illustrated) offering an output power of 2×40W RMS and the Series 44, offering 2×20W. Both use the direct connector system which links all components (except the turntable) without the need for connecting wires. In addition, the Series 66 amplifier switches automatically to whatever input source is activated. It also uses more advanced (and more expensive) components than the Series 44 but both provide a linear tracking turntable, AM/FM-stereo tuner, cassette deck, amplifier and loudspeakers, with optional graphic equaliser and equipment rack. Both can be used with the 315mm wide SL-P7 compact disc player. (Details from all Technics dealers).

Rust proof tape



3M Australia has just released five new audio cassette tapes for the consumer market, headed up by the new metal-coated Scotch "XSM-IV" and backed by an unconditional warranty.

According to David Henderson, 3M Home Products Marketing Manager, the formulation used for Scotch XSM-IV provides greater protection for the pure metal particles, inhibiting rusting effects, particularly along the edges where the tape has been slit and the binder parted.

Other cassettes in the new range include the "XSI", a dual-layer high performance tape for standard bias and the "XSM-II", a dual-layer cobalt-doped formulation for "chrome" bias and equalisation.

The "BX" and "CX" are "workaday" cassettes for use in portable and car players, the CX being an interesting combination of a hardy tape with performance not far short of the audiophile class.

That prediction appears already to be heading towards fulfillment. At last contact Greg Roberts said:

"We have confirmed sales for such diverse organisations as the Yellow Pages Directories in Melbourne, a large medical equipment distributor, two TV stations and the sales department of a national newspaper. The newspaper company and the medical company plan to use the VS-1 as a sales aid overseas, including a Trade Fair on the China mainland.

"As well, the Army is interested in evaluating the VS-1 for use in combat training programs.

[Tracker Electronics and the AVES Group are both located at 29 Albany St, Crows Nest, NSW 2065. Phone numbers: Tracker Electronics (02) 439 1349; The AVES Group (02) 439 1455]

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The IBM PC compatible that beats the IBM ... on price, on performance, on features, on expandability ... on everything!

The Challenger is the computer for the small to medium size business (it has 10 times the memory of Dick Smith Electronics first mainframe computer!)

But it's more than that: because it is compatible with IBM PC software and hardware, it makes a superb scientific or industrial computer ... or even a low-cost IBM terminal. And you'll save a fortune!

The CAT

Why waste hundreds of dollars buying an Apple computer when you can buy The Cat ... Dick Smith Electronics' latest computer masterpiece! It's twice as fast as the Apple IIe. It has a bigger and better BASIC. A larger keyboard. Super hi-res colour graphics. More sound channels. Just compare the two computers and judge for yourself! (Ask for our free comparison brochure).

Compatible with most Apple IIe software, The Cat is THE computer for education, for the student at home, for the hobbyist, for dedicated functions in industry ... even for the small business.

As Electronics Australia Magazine says 'Dick Smith Electronics has come up with a winner with the CAT personal computer'.

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The ideal computer for the beginner who wants a computer to grow with. Dick Smith Electronics incredible VZ-200. It's the low-cost way to go computing - without buying an 'orphan' or 'dumped' computer with no back-up.

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The 'works' of the computer ... keyboard, CPU, 128K RAM, input/output ports, etc. Ideal for cassette-based applications as it is with nothing more to buy. Includes Centronics parallel printer port, cassette port, joystick & light pen ports plus RF, video and RGB outputs.

Cat X-8600 All this for only ...

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Electronics



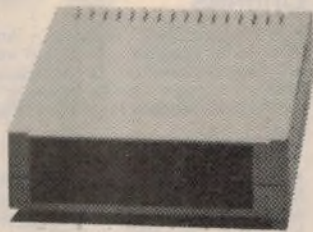
Apple IIe compatibility... but half the price! That's The CAT. It's the best of both worlds: the very latest and most powerful hardware, plus the ability to run a very broad range of tried-and-proven software.

And because we import direct, there's no middleman to force up the price. It really is outstanding value for money. Again from EA: "If you want a machine which is compatible with the Apple II and which is supported by a reputable dealer, the CAT with emulator is good value". Check the CAT out at your nearest Dick Smith Computer City. It purrs.

Cat X-7500

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That's far less than half the price of the Apple with similar features!



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A selection of ANY 6 software tapes normally \$12.50 each (X-7241 Learjet or X-7249 Air Traffic Control not included)

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For address details see page 108.

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A must for your system!
Cat X-8620



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Challenger Printer Cable

Cat X-8614

\$69

Challenger Software



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X-8750 ELECTRIC PENCIL – An easy to use yet sophisticated word processing program. Function keys definable up to 16 keystrokes of any key combination. Colour available for colour monitor. Underline and bold on screen. Menus give quick and easy reference to all system operations. Manual and Quick Reference Card included. **\$199.00**

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X-8650 MICROSOFT FLIGHT SIMULATOR – The best program of its type in the world. A highly accurate simulation of flight in a single-engine aircraft. Adaptable to any interest or ability level! **\$95.00**

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X-8710 SNOOPER TROOPS 1 – (As per CAT software) **\$67.95**

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Cassette Software

X-8649 STARSHIP CHALLENGER – **\$19.95**

X-8704 TYPING TUTOR – **\$19.95**

Electronics

CAT Software

Utilities

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- X-7650 SNOOPER TROOPS 1 - Someone is haunting the old Cable Mansion. It's up to you to find out who. But don't get caught! Full colour graphics & sound. Helps children learn to take notes, draw maps, classify information & develops vocabulary and reasoning skills. **\$64.95**
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Adventure & Arcade Games

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- X-7712 APPLE PANIC - Great arcade game action. Destroy the apples chasing you by digging holes in the floor and knocking them through. Be quick though - they may crawl out and get you! **\$39.95**
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- X-7716 WAY OUT - With compass and Map makers your task is to find your WAYOUT of the selected maze. But which way is the wind blowing, and is the Cleptangle creeping up from behind? **\$44.95**
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* Arriving End June

VZ-200 Software



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Coming Soon

WORD PROCESSOR (TO SUIT VZ-200)

DICK SMITH ELECTRONICS



For address details see page 108

A762/LL

Electronics Australia reviews

Yamaha's \$599 compact disc player

Recently released, the Yamaha CD-X1 is the first compact disc player to break the \$600 price barrier. Does it represent a reduction in the previously high compact disc player standards or have there been manufacturing breakthroughs?

Up until recently, compact disc players have been priced for the well-heeled few. Even the Yamaha CD-1 was a really top-priced model and so not too many found their way into Australia. But now the picture has changed with the release of this new model Yamaha.

Removing the top cover of the CD-X1 gives a few clues on how the price has been reduced. For a start, the chassis is virtually all plastic. Apart from the steel covers for the top and underside, there is very little metal used in the construction.

At first sight even the transport mechanism appears to be made entirely of plastic too. Closer examination reveals that the pliantly mounted transport

baseplate is of punched steel. All the gears for the transport mechanism are also plastic which is a factor in their quiet running.

This all means that while the initial tooling cost for the CD-X1 may have been very high, labour cost must be much lower than for competitive models.

Not only has the labour cost been reduced in the chassis and transport, there is also considerably less electronic componentry. Much of this reduction has been achieved by the production of two new large scale integrated circuits. The degree to which this integration has proceeded can be seen by looking at the boards. There aren't very many IC's in

the whole unit.

This does not mean that corners have been cut in the electronic design. The digital to analog conversion method is 16-bit linear rather than the 14-bit conversion used by some makes. As well, Yamaha have used an over-sampling method to double sampling rate to 88.2kHz. This is claimed to increase the resolution while enabling a fairly simple 7th order LC filter to remove the residual sampling signal.

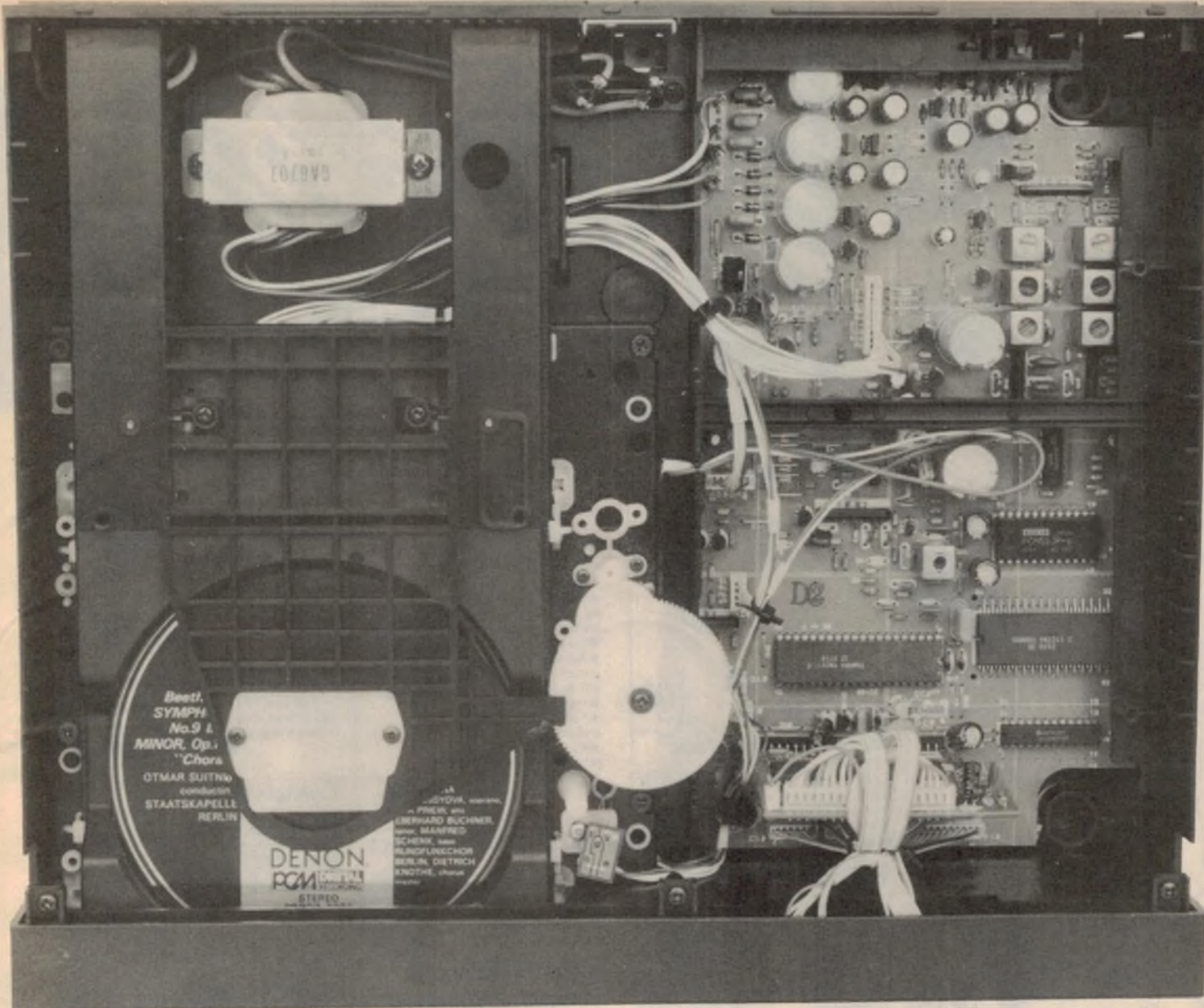
Besides making the CD-X1 very light, at only 3.6kg, the predominantly plastic construction makes it relatively easy for the machine to comply with the standards for double insulation. As such, the CD-X1 is fitted with a two-core mains flex.

In emphasising the light plastic construction we don't want to give the impression that the Yamaha is in any way cheap or "tacky". It isn't. It looks and is well finished and offers the full range of operational features, as we shall see.

Styling of the new Yamaha CD-X1 is

The Yamaha CD-X1 is well finished and offers the full range of operational features.





subdued, in the Yamaha manner, with an overall matt charcoal finish. Panel lighting is also subdued with digital displays for track selection and playing time.

Overall dimensions of the CD-X1 are 340mm wide, 290mm deep and 92mm high. As is becoming the norm, the CD-X1 is a front-loading drawer type machine. This has the advantage of producing a machine with a low profile but it does mean that the disc is well out of sight of the user.

The number of controls is certainly not overwhelming and so the Yamaha is very easy to drive without having to peruse the owner's manual in great and laborious detail.

One step which must be carried out before use is that the transport screws on the underside of the deck must be removed. These three screws lock the laser mechanism in place to avoid damage while in transit. No damage would result if an attempt was made to

use the machine while the screws are in place but the machine cannot play discs.

One problem which arises with most compact disc players is where do you store the locking screws? In most households they are likely to be misplaced and lost which is a problem if the deck subsequently must be transported for any distance.

We would like to see Yamaha and other compact disc manufacturers either do away with the need for locking screws or provide a means of storing them within the machine itself.

Record changer manufacturers solved a similar problem many years ago so we can see no real difficulty this time around.

Control features

On the lefthand side of the control panel is a push-on, push-off power switch. When power is first applied a soft green light under the disc drawer flashes on and off for a few seconds as the

mechanism tests for the presence of a disc in the drawer. Finding none, the light is extinguished and the unit becomes quiescent with just the faintest of panel lighting to tell that it is waiting.

Pushing the open/close button then causes the drawer to slide out rapidly to accept a disc. Just drop the disc in, push the same button again and the drawer slides back. The green indicator then flashes a couple of times while the mechanism cues up to the first track and then the machine is ready to play.

As the cueing up is taking place, the machine briefly displays the number of tracks on the disc and the total playing time. Pressing the play/pause button then initiates the first track within about two seconds. A fairly bright green "play" indicator then lights up and the elapsed time of the disc track is displayed continuously.

At any point the user can press the "check/RT" button to find out the total remaining playing time.

1 pole/10 position thumbwheel switch

Selling for around 1/3 normal cost. Very high quality construction. Limited stock

\$2.25 each
10 for \$20.00



Quality LEDs at Tiny Prices

Super quality 3mm LEDs from Stanley at knockout prices. Only in bags of 100 at this price.

\$6.00 for 100

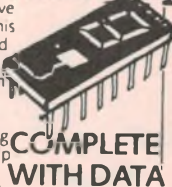


What a Bargain

Fantastic TI TIL308 display - Amazing features

This incredible display chip has thousands of uses. The experimenter and constructor will have thousands of uses for this amazing display. 27 red 7 segment display has BCD to 7 segment latch decoder driver circuitry and BCD to buffered BCD output. LED testing and LED blanking or chip enable is also built in. Left hand decimal point.

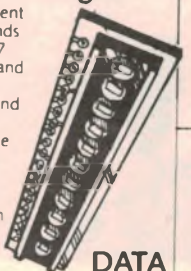
\$1.75 each
\$1.50 10 up



COMPLETE WITH DATA

12 Digit LED Display - Experimenter's Delight

These superb 7 segment displays have thousands of uses. Each digit is 7 segment with right hand decimal point. Eight inputs for segments and 12 inputs for digits (cathodes). Anodes are internally connected. They were selling for \$1.50 each. Reduced this month - grab 'em now!!



only \$1.00

DATA INCLUDED

240V AC Open Frame Motors - going fast

These gutsy universal type motors have thousands of uses. Grab a few while they last.

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Tiny Price on these amazing Tiny lamps

We are selling these amazing little lamps for only 10% of their original price. 12V/60mA and a tiny 5 1/2mm high by 2 1/2mm wide. Perfect for miniature projects, modellers, regulators etc.

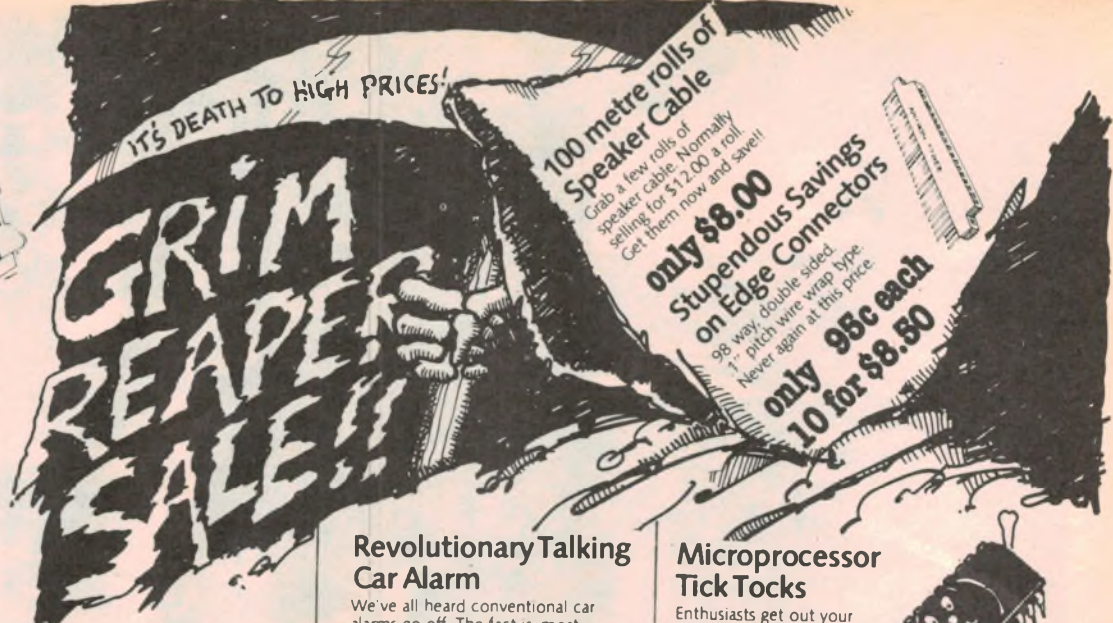
only \$10 for 100



TV Balun at 1/2 price

300Ω to 75Ω balun if you're fitting 300Ω ribbon to your TV set. Don't pay \$2.00!!

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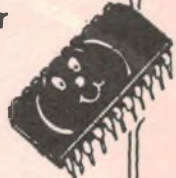
- ★ protects your whole car including the boot, bonnet and stereo
 - ★ No external key
 - ★ Automatic arming (when ignition turned off) and reset
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 - ★ Fully self contained and tamper proof
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Microprocessor Tick Tocks

Enthusiasts get out your soldering irons. These amazing OKI MSM5832RS microprocessor controlled clock calendars are back in stock. You'll spend hours learning about all their functions.



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14 pages packed with applications ideas and technical specs

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Micro Switches at Micro Prices

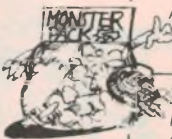
Top quality Cherry brand microswitches at giveaway prices. 15A/250V AC rating. Normally open contact with lever.



only 75c each
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Monster Trimpot Pack

100 mixed values and types. These normally sell for 30c to 50c each. Grab a few packs for the spare drawers and always have them on hand.



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Monster Tagstrip Pack

50 assorted tagstrips. Thousands of uses. Some of our competitors are selling them for \$1.00 each!! They must be kidding!!



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150 Ω/25W rheostats

Massive savings on these ceramic body 1/4 shaft rheostats. Ideal for speaker attenuators etc. Normally selling for around \$12.00 each.



only \$1.20 each
complete with knob

16μF/100V Bipolar Electrodes at Tiny Prices

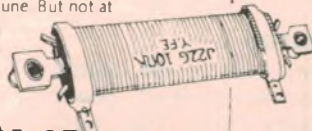
These PC mount bipolar electrodes normally sell for around \$1.00 each. We've made a scoop purchase so you get them at a tiny price. In packs of 20 only at this price!!



20 for \$2.00

10 Ω Power Resistors at Puny Prices

These 10Ω/25W power resistors are perfect for making up dummy loads, attenuators for speakers etc. etc. Normally they cost a fortune. But not at Sheridan's.



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Yamaha's \$599 compact disc player

Full music search facilities are provided by four touch-buttons. You can rapidly step forward or back through the track numbers to arrive at a given selection. And if you want to find a given musical phrase you can fast forward or reverse while listening to very rapid bursts of music — it's just like the cue and review facilities on some cassette decks.

Using these buttons while in the pause mode can cover a minute's worth of program in just one second, which is pretty fast. But the way it works it can be used to cue very easily. When you first touch the advance button it works slowly for the first three seconds and then speeds up, so with just a couple of touches you can quickly find the selection and cue it to play — release the pause and the music starts immediately.

When you have found the wanted musical phrase you can set the Yamaha to repeat it continuously by touching the two repeat buttons. All very simple.

Full memory facilities are also provided. The CD-X1 can store up to 23 selections. Again, the facility is easy to use.

We don't have the space to fully detail the playing facilities but the foregoing should be enough to give an idea of the capabilities and features of the CD-X1.

About the only features which have been left out when compared to much more expensive players are remote

control, a headphone socket and an output level control. At the price of this deck, this is no hardship.

How does it work?

First and foremost, the CD-X1 is quiet. Depending on how loud you are playing the music, you may have difficulty hearing the deck running at all. Of course with the volume turned off and in a quiet room you will hear it but it is not troublesome. When changing tracks it makes a slight whirring noise and when the disc comes to a stop you can hear a slight rubbing noise.

The loudest mechanical noise it makes is when the drawer slides in or out but even this cannot be criticised.

Control legends could have been made a little more legible. As it is, Yamaha must think that their buyers have even keener eyesight than their hearing. The lighting is on the dim side too and could be increased quite a lot before it became obtrusive. Not that this is a really major point because you quickly become familiar with the CD-X1 and thereafter seldom need to read the control labels.

Some decks are very sensitive to the slightest bump and will jump tracks easily. The Yamaha was good in this

respect and required a fairly deliberate bump to make it jump tracks. We would rate it as one of the better decks in this regard.

The Yamaha handles disc defects well too. To test this aspect, we used the Philips No 4A defect test disc. This includes track interruptions up to 900µm wide in the form of simulated scratches and black dots and also has a simulated fingerprint. The Yamaha sailed through all these without so much as one audible hiccup.

While this is the first compact disc player we have tested using the defect disc we are aware that most decks produced to date cannot achieve this.

Lab tests substantially confirm the specifications which are shown in a panel accompanying this review. Noise and harmonic distortion is quoted as .005% at 1kHz at 0dB and we obtained a result very close to that in both channels. From there it rose very gradually to 0.3% at 15kHz and thereafter to 0.22% at 20kHz.

The high result at 20kHz is not really a distortion product but is an artefact of the CD-X1's filter circuit and was actually a very low level sine wave at 24.1kHz. This is similar to the result produced by a number of other compact disc players.

Separation between channels was quoted as 90dB at 1kHz. We measured 87dB at 100Hz and 1kHz and 77dB at 10kHz; figures you could hardly complain about.

On the other hand we did feel that the CD-X1 could have been made quieter with very little extra refinement. Hum was 89dB down with respect to 0dB reference level while residual noise was 97dB down, a much more respectable figure. While we did not investigate the

Continued on page 150

Specifications

Frequency response	5-20,000Hz ±0.5dB
Dynamic range	More than 95dB
S/N ratio	More than 95dB
Harmonic distortion	Less than .005% (1kHz, 0dB)
Channel separation	More than 90dB
Wow & Flutter	Unmeasurable
Power consumption	20W
Output volts	2V (at 0dB)

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TWO MODELS ARE AVAILABLE

1) DIALLER ONLY

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and complete composite control module with N.O. and N.C. inputs, delay etc. This unit has a tamper proof steel box with space for a backup battery (Charger is included in price)

BOTH UNITS PLUG STRAIGHT INTO A TELEPHONE SOCKET!

Cat. LA-5120 - Full alarm/control unit **\$399**

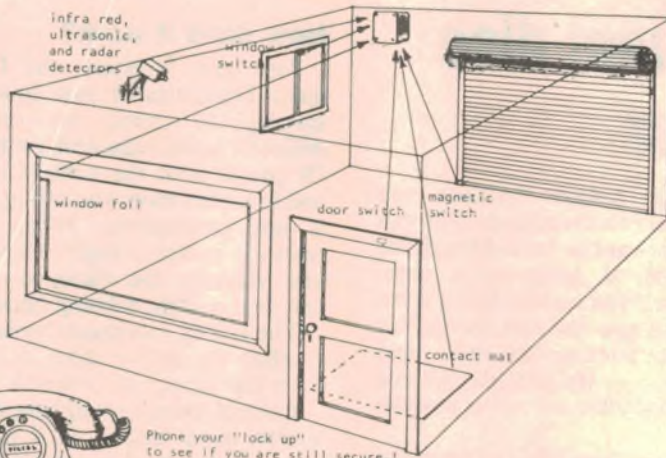
Cat. LA-5130 - 4 zone dialler only **\$299**

Both units are supplied in a metal cabinet.

OPERATION OF DIALLER

○ When ALARMED the following takes place: ○ The unit "grabs" the Telecom line from all other extensions ○ The dialler listens for "Dial Tone", when it hears the dial tone it dials out ○ Will even dial out an STD number or even from a switchboard (0 access) ○ After dialling the unit listens for "Ringing Tone" when it stops it: will give a "bleep" message (the number of beeps indicating the zone or zones alarmed) will repeat bleep message and close down ○ If no dial tone is detected, the unit will go "off line" again and then try again (like replacing the receiver and then picking it up again) ○ If the line is engaged or none answers after a short time period the dialler will close down and dial the next number that is programmed in (a maximum of 6 attempts) ○ The units have 4 input zones which can be

connected for all operating from N.O. contacts (or +12V dropping to less than 1/2V) or for all operating from N.C. contacts (or 1/2V rising to +12V) ○ A No AC signal is available which can be looped into a NO zone to give indication of supply failure (provided that the standby battery is fitted) ○ A Normally Closed contact is fitted to the case, to dial out if the unit is tampered with ○ The units have a return channel so that you can dial the unit up from a remote location and it will send beeps indicating the last message that was transmitted. ○ Will operate with the following sensors: N/C contacts - window foil - window/door switches, N/O contacts - mats, heat detectors, or operated and the contacts from Ultra-Sonic, radar, I.R. detectors and from most sector control units ○ Operates from 12V AC or from most sector control units ○ Operates from 12V AC or 13.6V DC (for recharging 12V battery) (or mains LA-5120)



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FEATURES:

○ It is a complete microprocessor based burglar alarm control unit with integral dialler, with facilities for 3 alarm zones and 1 test zone. ☆ It has the following zone options: i) Delay zone for entry/exit with 30 second delay before dialling out and bringing in the alarm relay, unless switched 'off' with a key switch, before this. ii) Instant zone, after the arming delay will dial out immediately and bring the alarm relay in. iii) Silent zone, will dial out but not bring relay in - option 1 can be switched 'OFF' with the unit - option 2 or a 24 hour panic or armed hold-up button iv) Test zone will ring in and tell you alarm is working at weekends etc. ☆ Can be programmed or re-programmed for all standard security receivers ☆ Unit is reset every time system is switched 'OFF' ☆ Can be installed by handyman ☆ No flashing lights to alert intruder ☆ Will phone up to 3 - 12 digit telephone numbers, silent zone can ring a 4th number (i.e. armed hold-up alarm could go to the shop next door and not an empty home) ☆ Will even phone STD Nos interstate ☆ Can signal fridge failure, mains failure, or fire etc.

NEW!! LARGE COLOUR LED DISPLAYS!

Jaycar is proud to announce a NEW range of 7 segment LED displays featuring LARGE digits and alternate colours!

NOTE THE LOW PRICES!!

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ZD1870	0.4" (10mm) Com Anode Red	\$1.00	0.95
ZD1875	0.5" (15mm) Com Anode Red	\$2.50	\$2.25
ZD1880	0.5" (15mm) Com Cath Green	\$2.95	\$2.50
ZD1885	0.6" (15mm) Com Cath Yellow	\$2.95	\$1.25
ZD1890	12x15mm rect diff block Red	\$1.50	\$1.60
ZD1891	12x15mm rect diff light block Red	\$1.80	\$1.60
ZD1892	12x15mm rect diff light block Red	\$1.80	\$1.60
	Yellow		

The light blocks are simply a rectangular block of diffused light. They can be seen over great distances and are generally used as status indicators. All devices have connection data supplied.

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A-F Spray whilst designed for cleaning metal surfaces and leaving no residue it is absolutely ideal for cleaning video heads. It comes with an extension tube to get to remote spots. Leaves absolutely no residue and blasts away grime with no danger of scratching. A sound investment in VCR care. Also great for audio heads of course.

Cat. NA-1007 400 gram can **\$8.95**



NEW!!

DESK TOP MAGNIFIER

Superb magnifying glass 90mm diameter mounted in a chrome ring supported on a 240mm flexible gooseneck. A sturdy cast base supports the unit. Ideal for checking solder joints, PCB cracks, component identification etc. High magnification over large area will pick up finest flaws! A must in every serious workshop.

Cat. OM-3500

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NEW!! UHF TUNER MODULE

This factory made unit enables you to cover the entire Australian UHF Band. The fundamental output frequency is actually around 35MHz, not VHF channel 1 as previously stated. A strong 'image' at VHF channel 1 appears, however. This enables the unit to connect straight to the antenna input of many VHF sets to enable UHF reception. The knob and reduction coil mechanism gives direct UHF channel readout!!

USES: - Can convert VHF (only) TV's to VHF/UHF
- Enables you to watch UHF output VCR's on VHF TV!
- Ditto for home computers & video games

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Cat. DM-9000 UHF Tuner Module **\$34.50**

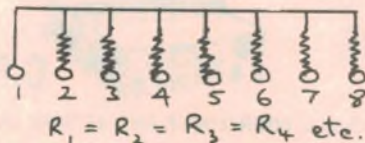
Cat. DM-9002 Knob and Dial to suit **\$5.45**



NEW!! PCB CLEANING SOLVENT

It may not be obvious, but many circuit problems occur when flux and other residues (even finger prints) remain on the PCB causing 'leakage' between tracks. If you work RF, high input impedance (i.e. FET OP amps etc), Ioniser or other circuits PCB cleanliness is a MUST. The Jaycar PCB Cleaning Solvent is a spray that dissolves all flux residue and grime leaving the track work and board absolutely clean. We then recommend that you "tropicalise" the underside with spray-on lacquer. (Also available Cat. NA-1002 350 gram can \$8.95).

Cat. NA-1008 454 gram can **\$8.95**



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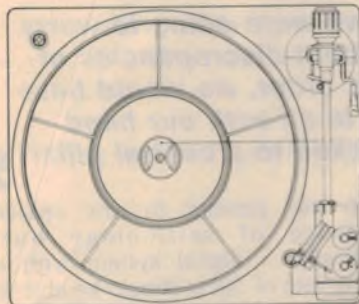
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The 'New Wave' of reviewers

If reader feedback to recent remarks is any criterion, the "Golden Ear" set, who express their views so freely in British hifi magazines, are not exactly overburdened with fans in Australia. Many and varied are the cracks that I hear, mostly at the expense of our tweedy cousins.



FORUM

Conducted by Neville Williams

As I remarked on a previous occasion, their ideas would be taken a lot more seriously if they were presented in reasoned terms, more appropriate to what are supposedly refinements to an already commendable system.

But no! Rarely are the writers satisfied to note a small but subtle improvement; that's much too tame. They fiddle with this or that and suddenly a whole new world of sound is revealed — expressed in terms that are totally out of proportion to what they have done. For the most part, any possible merit in their observation is discarded along with the language in which it is expressed.

Those responsible tend to be written off in not very complimentary terms.

One tongue-in-cheek theory is that the aforesaid writers and correspondents have got caught up in a nation-wide leg-pulling competition. The more outrageous their claim and the more convincingly it is stated, the greater is the number of points awarded. The outright winner has yet to be named but, in the meantime, those who qualify for consideration win the right to have their submissions published!

The more outrageous their claim and the more convincingly it is stated, the greater is the number of points awarded

While accepting that this is where it all started, someone else has suggested that many of the statements have been put — and subsequently defended — with such fervour that they are being accepted as dogma, with the "competitors" well and truly hoisted with their own petard.

One well known Sydney hifi dealer won't have a bar of all this. He maintains that, although there might appear to be a small army of way-out golden-eared correspondents in Britain, there's really only about half a dozen of them — all busily churning out articles and letters to the Editor under different names!

"Why would they want to do this?"

"That's easy", someone else chortles.

"The British hifi industry can't compete with Japanese mass-produced products, so they rubbish them.

"They rubbish copper wire, PC boards, transistors, ICs and all the things the Japanese rely on. They make out a case for doing it some other way and then make a quid on the strength of it!"

"It's ridiculous" says a local manufacturer of loudspeaker systems.

"Would you believe that I've had systems back for service in which the owners have replaced my original, perfectly adequate leads with little bits of supposedly special cable?"

"How crazy can they get?"

While it affords the participants a certain amusement, it is a bit sad for those of us who can look back on an era when the British hifi industry led the world; when it was characterised by enthusiasts and contributors of a very different breed: Gilbert Briggs of Wharfedale; Arthur Haddy of Decca; Percy Wilson of "Gramophone" fame; Peter Walker of Acoustical Quad; Henry Hartley of Hartley Loudspeakers; Stanley Kelly with his ribbon loudspeakers; Harold Leak with his "sandwich" system; and many others, not forgetting "Wireless World's" inimitable "Free Grid".

One might almost repeat the classic lament: "They don't make 'em like that any more!"

In a letter set out in a separate panel, B.C. of Darwin takes up one of the matters raised in our March issue, namely the policy of some Japanese manufacturers to use a single, switched D/A decoding chip in their CD players, and not to bother about restoring the original time relationship between the time-interleaved left and right channels. Could the resulting 11.34 microsecond lag in one channel upset the stereo image and prejudice the overall sound quality?

Responding to this, we drew attention to a diagram from Matsushita (National-Panasonic) which indicated that this order of time lag was totally negligible; that it would result, for example, from a discrepancy of a mere 3mm in the position of a loudspeaker — or the head

— in a symmetrical listening situation.

If we were going to worry about discrepancies of this order, we would have to sit with our head locked to a central pillar; hence the original jocular reference to "the man in the iron mask".

I hadn't thought about headphone listening but, as B.C. points out, an 11-microsecond time lag in one channel could be compensated for by inserting a 3mm foam spacer between the opposite phone and the ear. But let's not call it a foam spacer, or a sponge rubber pad, or anything else as common as that. Let's call it a "Japanese Compact Disc Phase Corrector".

B.C.'s reference to this, and the basis on which it's selling price should be determined will not be lost on those who take note of the adverts and the write-ups for hifi products of arguable merit.

But, enough of that for the moment.

In his letter, B.C. goes on to debate the adequacy of the 44.1kHz sampling rate used for present-day compact discs. Scaling up from his experience with seismic signals, he feels that the sampling rate for hifi audio should not be less than 100kHz.

If we were going to worry about discrepancies of this order, we would have to sit with our head locked to a central pillar

I do not pretend to any special knowledge of seismology but, theoretically, a digital system with a sampling rate of 50Hz should be able to cope with transients equivalent to about 22Hz. If the engineers did have a figure of 10Hz in mind, their 5-times sampling rate would have allowed for cyclic phenomena of up to 10Hz, plus a margin for some distortion content.

The claim that seismologists could pick the difference between digital and analog signals seems clearly to indicate that the original signals contained transients faster than 22Hz, and that their presence or absence was evident on inspection. Even so, the system designers

have a few things to sort out!

Dear Neville,

As a regular reader of your "Forum", I found your comments on "BBC fingers time lag" (March '84) very interesting.

I wonder if the "golden eared" people are actually listening to compact discs through regular hifi systems or whether, perchance, they are listening through headphones.

If the latter is the case, your "man in the iron mask" concept is especially applicable and we should, maybe, look at marketing a piece of 3mm thick sponge rubber as a "Japanese Compact Disc Phase Corrector". It could sell for anything up to \$100, as any improvement in this high class hifi field should logically cost a small percentage (1%-2%) of the value of the total system.

I might just rush off to my local patent office with this one!

On quite another subject, I had experience in a previous job with digitising seismic signals: .001 to 10Hz at 16 bits. The engineers selected a sampling rate of five times the highest usable frequency for the output filter — hence 50Hz at 48db/octave.

The seismologists maintained that they could always distinguish a digital signal from analog, not by dynamic range or noise floor but by transient response. They claimed that 5 samples per cycle was not high enough but, by reason of the 24-hour monitoring and economy of storage, it was left at that.

On this basis, I don't see how a sampling rate of less than $5 \times 20\text{kHz}$ can be justified for hifi sound. I am told that the figure of 5 was chosen because of aliasing considerations. Food for thought, don't you think?

One other thing comes to mind, as I write, namely the issue of playing

stereo channels in mono mode. My practice when adjusting the azimuth of stereo tape heads was to set up in mono mode and adjust for maximum output — and hence minimum phase shift.

This was taken a step further in our digital tape driver by having a 4-bit buffer on the output of the read amplifier circuits and variable delays on the record circuits. So the problem has been known about for years:

Maybe the use of a single, switched D/A converter was a cost-saving decision by the Nippon manufacturers: "The customers won't know, so why worry about it?" I'm willing to bet that we see later model Nippon players with modified boards.

Keep up the good work but, in the meantime, I must nip off to the Patents Office!

B.C. (Darwin, NT)

opted for a restricted bandwidth as an economy measure for recording, presumably on the basis that the vital information was concentrated mainly between .001 and 10Hz.

The comparison between seismic and audio signals breaks down at this point. If we accept that, by definition, an audio signal is one that is audible, then the upper limit, even for humans with exceptional hearing, is about 17kHz. Far from having a restricted bandwidth, the CD system, which is consistently measured as flat to 20kHz, has bandwidth to spare.

It may indeed be possible, with test equipment, to identify supersonic output from some musical instruments and to demonstrate that it is or is not preserved by recording equipment of one kind or another. But that is not relevant to the listening experience unless it can be shown unequivocally that human beings are in some way responsive to supersonic energy — in this case to energy beyond 20kHz.

We debated this subject a few months ago, without any revelation to that effect.

In short, I doubt that B.C.'s observations about seismic equipment give any cause to question CD practice, although I am sure that there will be plenty more arguments to come.

(It is interesting to note, in this connection, that Doug Sax of Sheffield Labs in California, a long-time opponent

of digital sound, has recently modified his views. While still rejecting certain compact disc practice, he says that recent experience with the Sony/Nakamichi PCM-F1 recorder "tells me my expressed opinions regarding a 44kHz 16-bit system will have to be revised.")

Finally, and reverting to his earlier point, B.C. offers a bet that Japanese manufacturers will go over to the use of dual D/A converters and 11-microsecond buffers. I certainly wouldn't put up money against him.

It has all been picked over, seized upon and proffered in fragmentary fashion as possible explanation for allegedly "sweeter" sound

The Japanese are nothing, if not pragmatic. Having demonstrated to their own satisfaction that an 11-microsecond delay in one channel was of no consequence, they would not have hesitated to omit the apparently redundant circuitry.

But, if they sense that the decision is being used to their disadvantage, I wouldn't expect them to dig their heels in and doggedly defend their position, no matter how justified. They'll simply come up with a bigger and better IC and offer the ultimate in left/right signal matching — x% better than anybody else's!

They're experts in saving phase!

Getting back to the original theme, I seem to have collected — or been given — quite a clutch of clippings about connectors and leads, the merits or otherwise of various metals, purity, polarity and so on.

Looking at them, I get the impression that the writers have spent hours poring over unfamiliar textbooks, searching for differences between metals, even to their atomic number, the physical shape of conductors, the influence and chemistry of insulation and so on.

It has all been picked over, seized upon and proffered in fragmentary fashion as possible explanation for allegedly "sweeter" sound — irrespective of whether the characteristics have the slightest relevance to audio frequency applications.

Kilo, Mega and Giga are all Hertz, so what's the difference?

It has become so tedious that, for the present, I prefer to let the wafflers waffle on. If something startling emerges, fair enough but, in the meantime, I'll stay with what is accepted and demonstrable "good practice".

I do, however, want to add a few remarks about two other aspects of "golden ear" theorising, namely opposition to PC (printed circuit) boards and the use of valve rather than solid-state technology.

PC boards were taken up by the electronics industry more or less

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Table listing various electronic components such as resistors, capacitors, diodes, and transistors with their respective part numbers and quantities.

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coincident with the changeover to solid-state. They had become more practical with the elimination of valve sockets and more appropriate as a means of supporting the ever-growing number of small components involved. And, of course, they lent themselves to mass production.

PC boards brought their own problems with shorts, dry joints and hairline cracks in the copper but, essentially, they were only a variation of the problems which had always bugged traditional wiring methods and hand soldering. With the density of components in modern electronic equipment, and the number of individual soldered joints, it is doubtful whether the industry could even manage without modern PC board technology.

Not surprisingly, however, the use of PC boards in hifi equipment has been questioned by the golden ear set, not because of shorts and dry joints, but presumably because they involve thin copper strip conductors bonded intimately to bulky insulation. It stands to reason (?) that it can't be as good as stranded wires, encased (if necessary) in PVC insulation and kept more out in the open!

I agree that some of the early boards left much to be desired but it didn't take engineers long to put their finger on problems such as crosstalk and common-mode noise, instability and/or distortion produced when the input signal happens to share a common return path with the output signal and/or the supply. Nowadays, with any design worthy of the description, problems such as these would not get beyond the drawing board.

In any case, they are not unique to PC boards and can as easily occur (and did occur) with hand wiring. So don't rush for your soldering iron on the strength of somebody's advice, and I quote:

"... printed circuits are another super-audio no-no".

In the act of "improving" your system by re-building this section or that, you may inadvertently build back in the very faults that the original designer was careful to exclude.

This, in addition to invalidating any warranty or even the option of normal distributor service.

On the subject of valves and transistors, arguments about the relative merits of the two have been going on ever since transistors made it into consumer radio and audio equipment. Users were startled by their economy in battery-powered situations and impressed by the increased power

available in domestic amplifiers.

But there were reservations about the tonal quality of solid-state amplifiers — and with good reason. Most used class-B output stages which, in valve equipment, were regarded as acceptable only for public address purposes. Too much reliance was placed on copious negative feedback, without allowing for the transient overload effects which could occur inside the feedback loop. And so on.

Solid-state audio equipment has been improved enormously since those days, to the point where it is accepted without question by most hifi enthusiasts and by most engineers involved in handling audio at a professional level. More than that, virtually all modern high technology test equipment is also based on solid-state circuitry.

“ There are people who cling tenaciously to the doctrine that there is something uniquely satisfying about an amplifier using valves ”

But some of the mud has stuck — as to a politician — and there are writers, readers and a few professionals who cling tenaciously to the doctrine that there is something uniquely good and sweet and satisfying about an amplifier using thermionic valves, referred to affectionately as “glass”.

Now don't mistake me. With modern components and our extended knowledge of audio design, it is possible, these days, to produce a “glass” power amplifier or an “all glass” system capable of superb, even if not transcending, quality. For most people if may be unacceptably costly, or cumbersome, or hungry in terms of power consumption but, if those considerations don't bother you, go right ahead.

I would expect you to be keen about your unusual purchase, to show it off, to rave on a bit, as most of us do at times. You might be described as a “bit keen” but that's where it would end.

But how does one react to an observation by Ken Kessler in his “Classical Glass” article in the March '84 issue of “Hi-Fi News & Record Review”? Discussing the relative merits of valve and solid-state amplifiers, he discounts historic criticism of valve-type output transformers and observes:

“I've never paid too much attention to that argument, never having heard a solid-state amplifier which challenges even the humblest of valve units . . .”

Does he really mean that? If he does,

what credence can you attach to any further assertions? If he doesn't mean it, why does he say it?

Does it not read like one of those gross exaggerations that I complained about, right at the beginning?

Having spent many years in the Production and Applications lab of the Amalgamated Wireless Valve Company, and many years since then in our own lab designing valve amplifiers, I am not without some background in the subject. Nor am I so detached as not to experience some nostalgia in respect to the valve “Playmaster” series, which were built by tens of thousands in Australia and New Zealand.

But I also remember the struggle we had up front to keep noise, hum and microphony within bounds and, at the back end, to offer reasonable power, frequency response, stability and distortion minima, without having costs going through the roof. What was true of the Playmasters was also true of the equivalent commercial amplifiers in that last-of-the-valves era.

It seems ludicrous to me to suggest that those amplifiers (“even the humblest” of them) with their comparatively high noise and distortion, and their comparatively lower power and dynamic range, could withstand a challenge from a modern high-performance solid-state amplifier. If Ken Kessler insists that such is the case, then I must insist on my right to reject him as a reliable witness.

If, on the other hand, he is talking about “even the humblest” of the current audiophile “glass” models then, for Heaven's sake, he should say so!

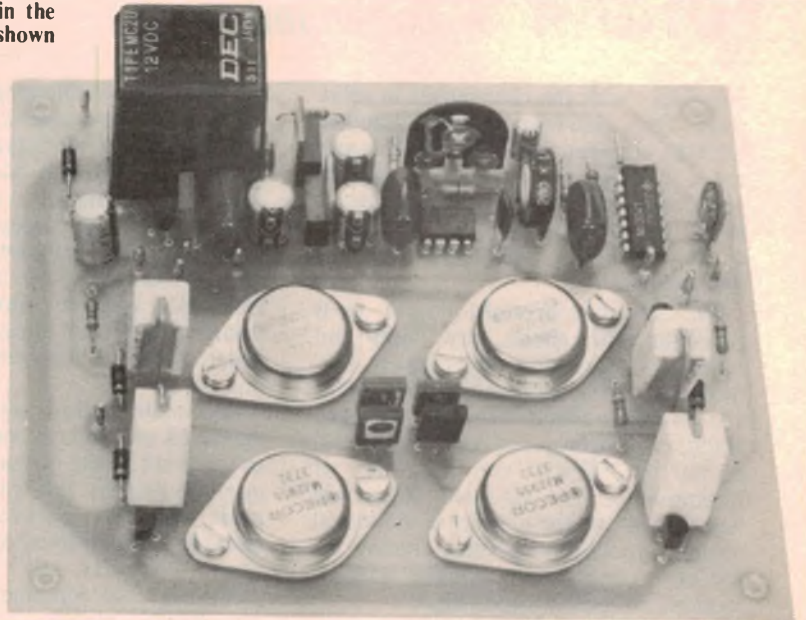
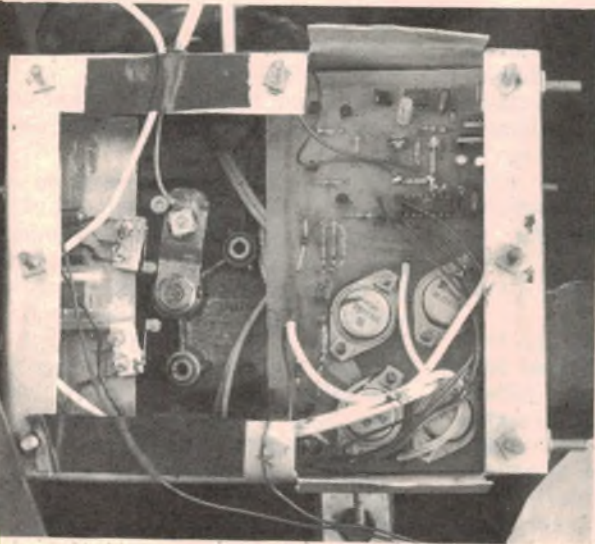
He goes on, in the article, to talk about a valve preamplifier from a small British company, Croft Acoustics. Apart from a toroidal power transformer, the underside picture is strongly reminiscent of the construction we used back in the days of the aforesaid “Playmasters”: valves and sockets on an angle bracket, components on a tagboard nearby, with loosely anchored hand wiring to connectors on the rear, controls on the front and the power supply, concentrated around a second tagboard.

The preamplifier is provided with a moving-magnet rather than a moving-coil phono input — praised by Ken Kessler as one who, like the designers, prefers the Decca cartridge to moving coil types. Unfairly, perhaps, the “devil's advocate” in me sees this as a very convenient preference for glass people!

As for noise level with MM input, the

Continued on page 145

Below is an early prototype throttle actuator as installed in the author's Mazda Capella. The final version of this board is shown below, right.



Cruise control

Commercial cruise controls are available on some new cars and on the aftermarket, but usually cost around \$200. This versatile design can be built for less than half that figure.

Have you ever driven long distances in the country, your foot getting cramped and wishing you had something that would automatically control the speed of the car? This cruise control will do the job. It is easy to build and install, uses readily available parts, and will maintain the speed of your car to within about 2% of the set speed.

To operate the unit, it is only necessary to bring the vehicle up to the desired speed and press the engage button. Press another button or the brake pedal and the cruise control is disengaged. Press the resume button and the car will resume the previous speed setting.

Passing another car is no problem since pressing the accelerator pedal further simply overrides the cruise control. When your foot is removed from the accelerator, the cruise control takes over as before and the car resumes the set speed. A new cruising speed can be set at any time simply by pressing the engage button at the desired speed.

In operation, the cruise control keeps the acceleration proportional to the

difference between the set speed and the actual speed. A windscreen wiper motor is used to control the throttle setting and this can be obtained cheaply from a wrecker's yard.

How it works

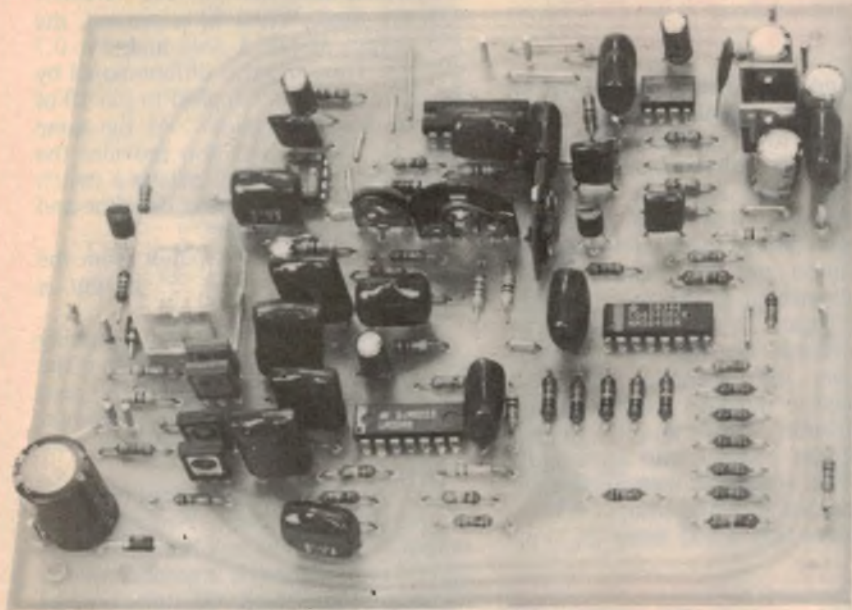
The cruise control circuitry has been split into two sections. One part, called the *signal processor*, sits under the dashboard and tells the other part, called the *throttle actuator*, what to do. The throttle actuator sits in the engine compartment and controls the throttle setting.

The signal processor sends a control voltage to the throttle actuator. This is called the *error signal*. If the error signal is above 5V, the throttle is opened further. Conversely, if the error signal is below 5V, the throttle is backed off. The rate at which the throttle is opened up or

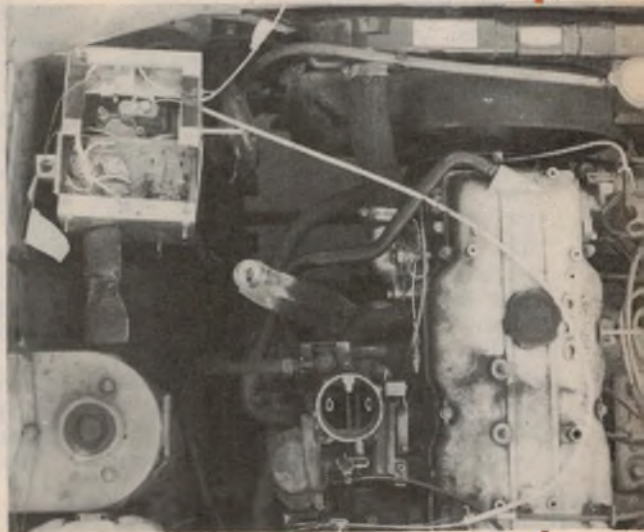
backed off is proportional to the difference between the error signal and the 5V rail.

The error signal is actually a voltage that is dependent upon the set speed, the actual speed, and five times the derivative of the actual speed. Note that the derivative of the speed is acceleration.

Zero, +5V, +10V and +12V supply rails are required for the circuits of both parts. This is achieved by using two 7805 voltage regulators in each section. Both 7805 inputs are connected to the car battery. One has its ground connection to earth (negative terminal of the car battery) and its output is +5V. The other 7805 uses this output as its ground, so its output is +10V. A 1k Ω resistor is connected between the output of the first 7805 and earth to ensure that no current flows back into the output of the first 7805. The +12V rail is simply the car battery voltage.



The signal processor (left) controls the throttle actuator. Below is another view of the throttle actuator installation.



for cars

by JOHN KONING

Signal processor

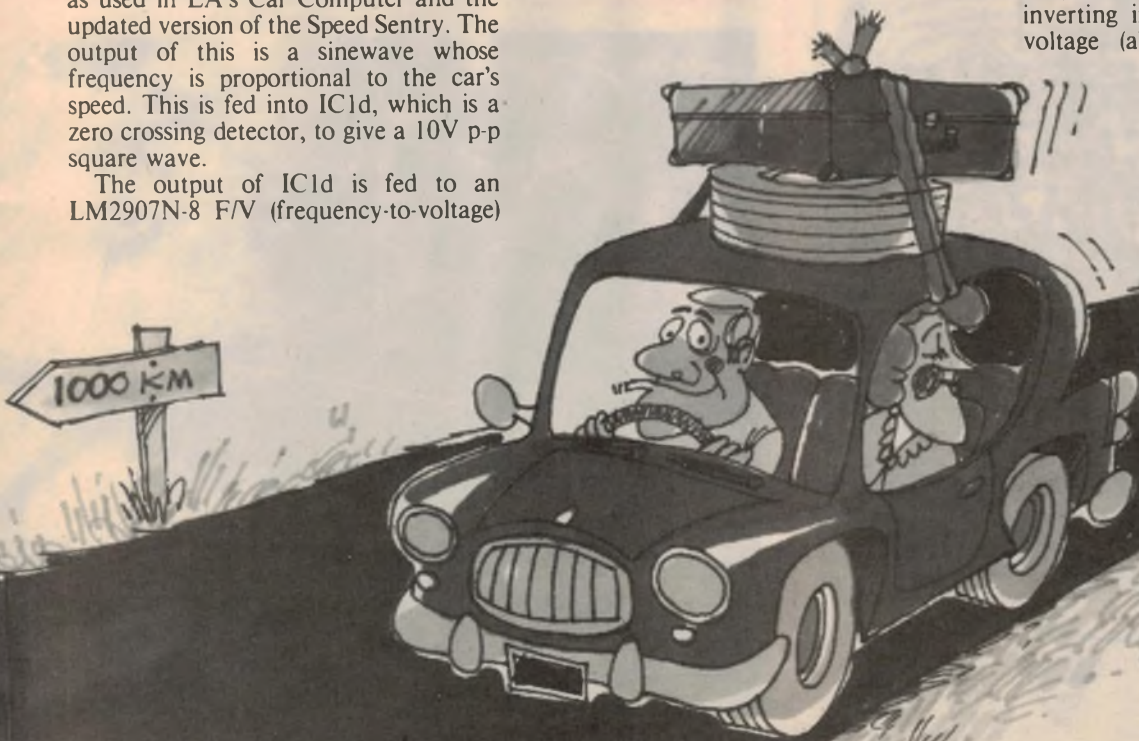
The speed sensor consists of a coil and four magnets attached to the driveshaft as used in EA's Car Computer and the updated version of the Speed Sentry. The output of this is a sinewave whose frequency is proportional to the car's speed. This is fed into IC1d, which is a zero crossing detector, to give a 10V p-p square wave.

The output of IC1d is fed to an LM2907N-8 F/V (frequency-to-voltage)

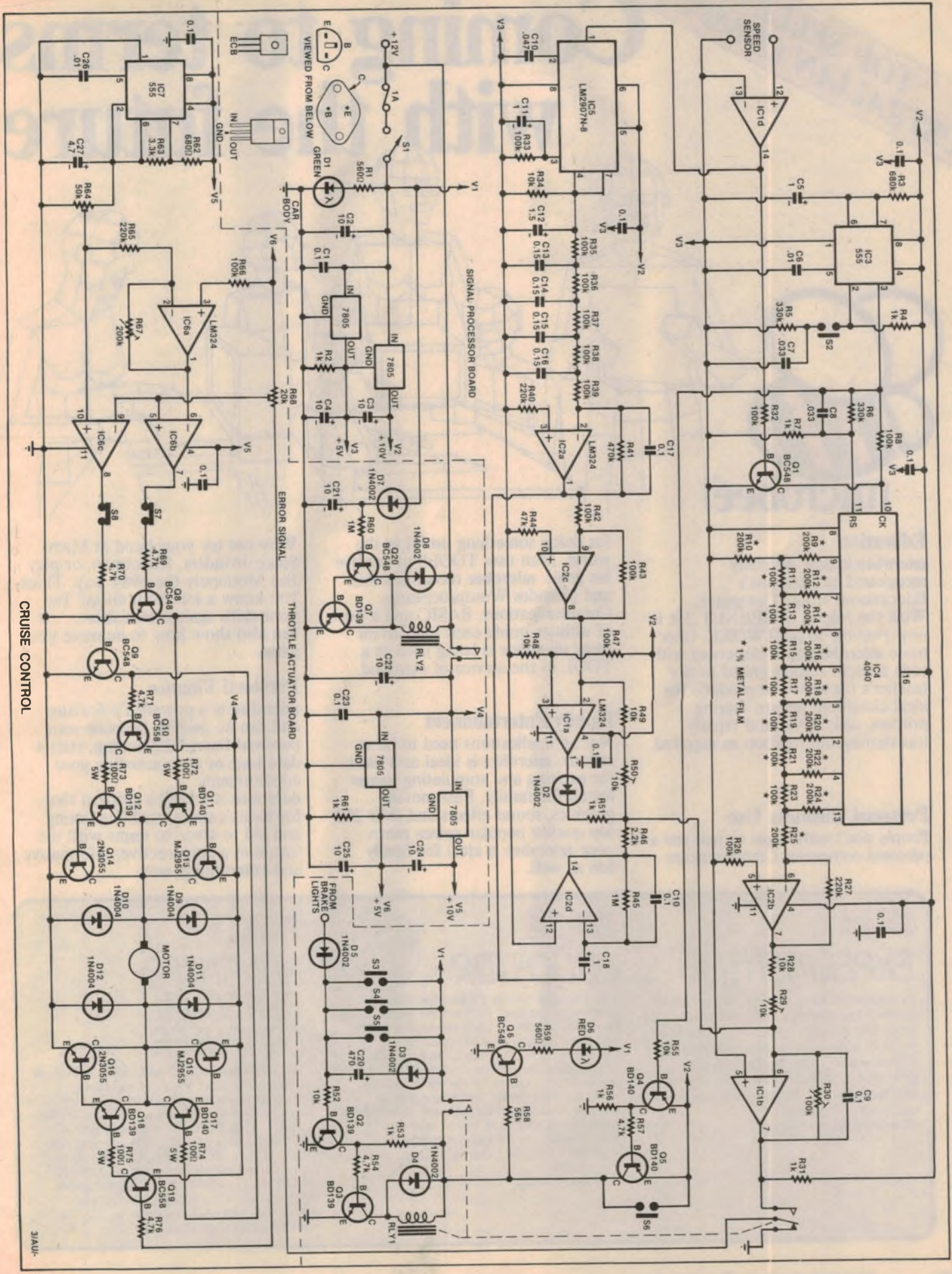
converter (IC5) which gives a voltage that is proportional to the car's speed. This voltage is then fed to a multi-stage

RC filter network and thence to buffer amplifier IC2a. From there, the signal passes via C18 to differentiator stage IC2d and also via R42 to unity gain inverter IC2c. The outputs of the differentiator and the inverter are then fed into a summing amplifier involving IC1b.

The output of IC2c is also fed into comparator IC1a which has its output connected to the summer via a diode (D2) and a 1kΩ resistor (R51). The non-inverting input of IC1a is at a preset voltage (about ½V) due to voltage



The author is a student at the Bendigo College of Advanced Education.

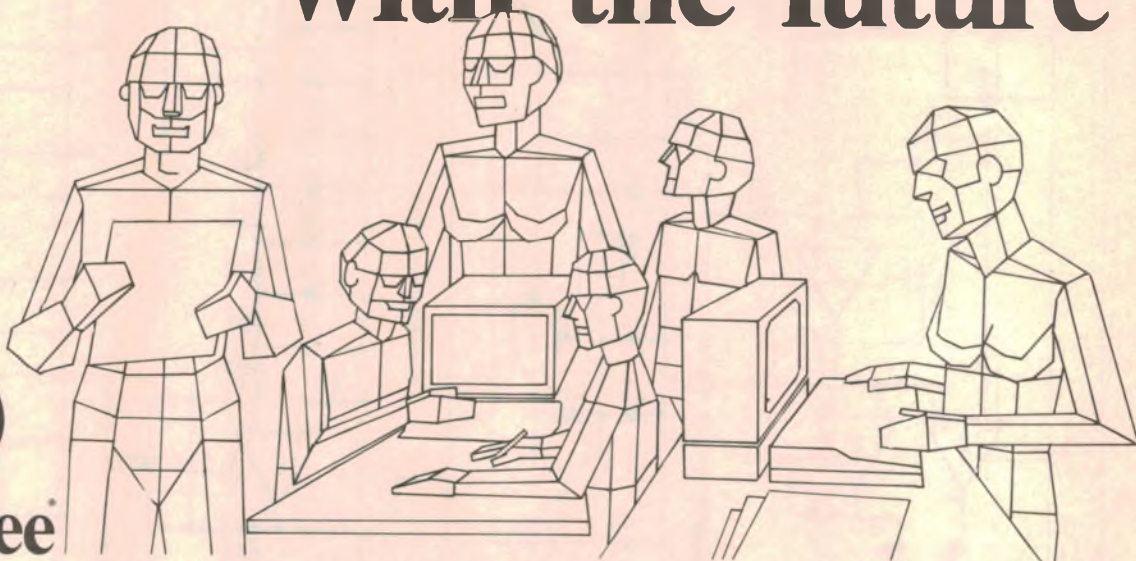


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Cruise control for cars

throttle is released when the Cruise Control is disengaged.

Note that when S1 is initially closed, current flows via D3, C20, R52 and the base of Q2 until C20 is charged up. This holds the Cruise Control disengaged for about five seconds after switch on and is necessary because the 555 triggers when S1 is closed.

S6 is the resume switch and allows the Cruise Control to be re-engaged at its previous speed setting. It is simply wired in parallel with Q5 and, when pressed, latches on the relay. Alternatively, the Cruise Control can be re-engaged by bringing the car back to the desired speed and pressing S2.

The status of the Cruise Control is indicated by LEDs D1 and D6. D1 is a green or orange LED that indicates when the Cruise Control has been turned on (S1 closed), while D6 is driven by Q6 and turns on when the Cruise Control is engaged (ie, when relay 1 is latched on).

Throttle actuator

So much for the signal processing circuitry. Let's now turn our attention to the throttle actuator. This comprises ICs 6 and 7, transistors Q7 to Q20, and the windscreen wiper motor.

The windscreen wiper motor is driven by a dual totem pole transistor arrangement so that the full battery

voltage is applied in both forward and reverse directions. The four diodes D9 to D12 are flywheel diodes and protect transistors Q13 to Q16 by quenching back EMF from the motor.

Pulse width modulation of the windscreen wiper motor driving voltage is used to ensure maximum mechanical torque at various speeds, a measure which also ensures maximum electrical efficiency since the transistors operate in switchmode.

The pulse width modulation is achieved by using a 555 (IC7) in astable mode and an LM324 quad op-amp (IC6). The 555 oscillates at 42Hz. The output is taken from pin 6 of the 555 and consists of a triangular waveform that peaks at 6.7V ($\frac{2}{3}V_{cc}$) and bottoms at 3.3V ($\frac{1}{3}V_{cc}$). This is reduced to peak at 5V and bottom at 2.5V by R64, which is a trimpot connected as a voltage divider.

When the signal processor output falls

below 5V (indicating that the car is over the set speed or is over-accelerating), comparator IC6c drives Q9. Q9, in turn, drives Darlington pair Q17 and Q15, as well as Q10, Q12 and Q14. Thus, when the signal processor output falls below 5V, Q14 and Q15 are pulsed on and the windscreen wiper motor is driven in one direction to close the throttle.

Similarly, when the signal processor output rises above 5V, Q8 is driven by IC6a and IC6b. This turns on Q13 and Q16, and so the windscreen wiper motor is driven in the opposite direction to open the throttle. S7 and S8 are limit switches which open at the throttle extremities to prevent the motor from being overdriven. S7 opens when the throttle is fully open, while S8 opens when the throttle is fully closed.

The duty cycle of the driving pulses increases the further that the throttle actuator output is away from 5V. Note that R67 is adjustable so that the duty cycle of the throttle opening driving pulses can be made longer relative to the throttle closing driving pulses, for a given error. The reason for this will be explained later.

Transistors Q7 and Q20, in association with C21 and R60, ensure that power to the throttle actuator is maintained for about 10 seconds after S1 is opened. This is to ensure that the throttle is fully released when the Cruise Control is switched off. When S1 is closed, C21 charges up via D7 and Q20 and Q7 are turned on. Relay R2 is thus also on and supplies power to the throttle actuator.

When S1 is opened, C21 discharges via

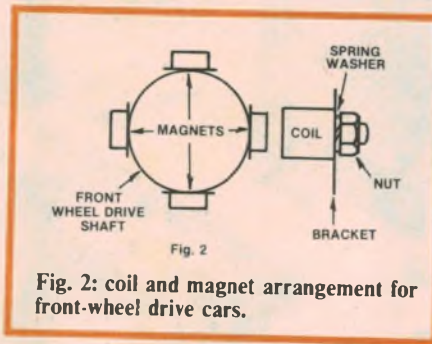


Fig. 2: coil and magnet arrangement for front-wheel drive cars.

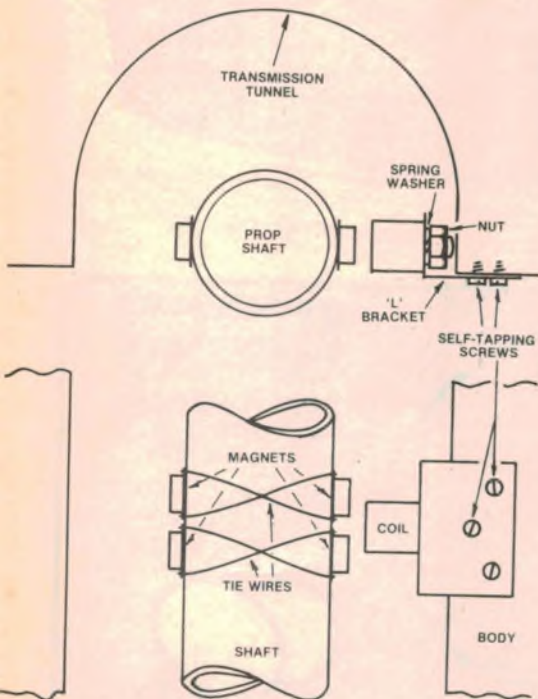
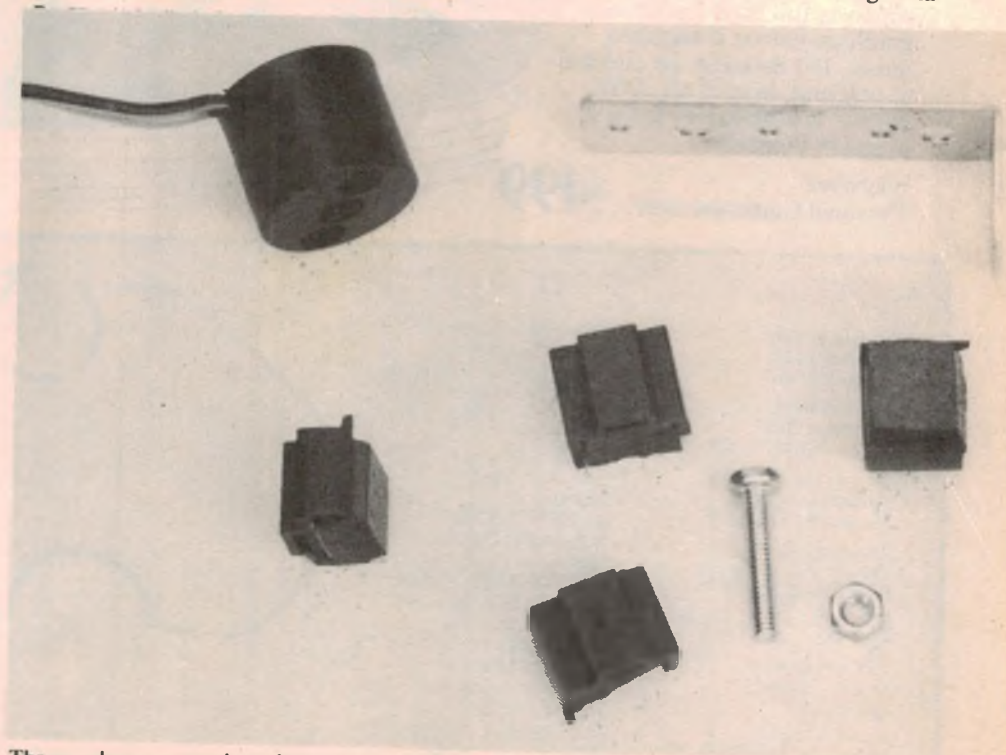


Fig. 1: speed sensor arrangement for rear-wheel drive cars. Note the twin magnet arrangement (see text).



The speed sensor consists of a pick-up coil, four magnets and a mounting bracket.

R60, keeping Q20, Q7 and relay 2 on for about 10 seconds. Relay 1 is off during this time and so the throttle actuator quickly closes the throttle.

The microswitches on the clutch (manual cars only) and gear lever are there to prevent the engine from revving if the clutch is pushed in or the car is knocked out of gear. The clutch microswitch should be closed when the clutch is depressed, while the gear lever microswitch should be open when the car is in top gear (manual) or drive (automatic) and closed otherwise.

Construction

Construction of the Cruise Control is straightforward. The signal processor circuit is built on a printed circuit board (PCB) coded 84au6a (140 x 120mm), while the throttle actuator is built on a PCB coded 84au6b (131 x 110mm). These boards are housed in separate metal cases.

Begin construction by installing the parts on the signal processor PCB (84au6a). Install the resistors and wire links first, then the capacitors, relay and semiconductors in that order. Note that the resistors used in the R:2R ladder network are close-tolerance 1% types. These are marked with asterisks on the wiring diagram.

Take care to ensure that all polarised components are installed correctly. The CD4040 (IC4) is a CMOS device so the usual precautions apply. Earth the barrel of your soldering iron to the earth track on the PCB and solder the supply pins (8 and 16) first.

Note that the LM2907 is available in both 8-pin and 14-pin versions. The PCB is designed to accept the 8-pin version (ie, the LM2907N-8).

Once assembly of the PCB has been completed, it can be installed in its metal case. The front panel of the case carries the on/off, disengage, engage and resume switches and the two LEDs, while the rear panel carries an 8-way terminal block and an in-line fuseholder. Install the PCB on 12mm spacers, then complete the wiring to the front and rear panel hardware.

The case used for the prototype was homemade, but there's no reason why you can't use a standard metal case if you so wish. Because requirements will differ from vehicle to vehicle, the details are left to the individual. Some constructors, for example, may wish to mount the control switches and LED indicators on a separate panel which can be mounted in a more convenient location.

If ignition interference subsequently proves a problem, try using shielded audio cable for the switch leads.

Do not install the signal processor in the car at this stage. Before doing this, it

PARTS LIST

- 1 PCB, code 84au6a, 140 x 120mm
- 1 PCB, code 84au6b, 131 x 110mm
- 1 mini PCB relay, 12V DPDT (Cat No. S4061, Jaycar, Altronics, Rod Irving)
- 1 DPDT relay, 10A contacts (DSE Cat No. S7200)
- 1 SPST toggle switch
- 3 momentary contact pushbutton switches
- 4 microswitches (S4, S5, S7 and S8 — see text)
- 1 panel-mounting 3AG fuseholder
- 1 1A 3AG fuse
- 2 LED mounting bezels
- 8 12mm spacers
- 1 8-way terminal block
- 2 metal cases to suit (see text)
- 1 windscreen wiper motor
- 1 bicycle brake cable
- 1 speed sensor (coil plus magnets, Jaycar)

Semiconductors

- 3 LM324 quad op amps
- 2 555 timers
- 1 CD4040 12-stage ripple counter
- 1 LM2907N-8 F/V converter (Geoff Wood Electronics)
- 4 7805 5V voltage regulators
- 5 BD139 NPN transistors
- 4 BD140 PNP transistors
- 5 BC548 NPN transistors
- 2 BC558 PNP transistors

is necessary to make a few adjustments and these will be described later on.

Attention can now be turned to the throttle actuator PCB (84au6b). Take particular care when installing the transistors and note that Q11 and Q12 face in the opposite direction to Q17 and Q18. The four power transistors are bolted directly to the PCB using machine screws and nuts.

It is a good idea to solder the nuts on the copper side of the PCB in order to ensure a reliable electrical connection.

The four 100Ω 5W resistors are mounted vertically on the PCB. Once mounted, these should be glued to the board with epoxy adhesive in order to prevent undue strain on the leads due to vibration.

There are two ways of installing the throttle actuator: either you can mount the PCB, windscreen wiper motor and microswitch assembly in a single metal case, or you can install the PCB in a smaller case and mount the windscreen wiper motor and microswitch assembly externally. The second option is recommended since it provides greater flexibility when installing the parts under the bonnet.

- 2 2N3055 NPN transistors
- 2 MJ2955 PNP transistors
- 6 1N4002 diodes
- 4 1N4004 diodes
- 1 red LED (5mm)
- 1 green LED (5mm)

Capacitors

- 1 470μF/16VW PC electrolytic
- 7 10μF/16VW PC electrolytics
- 1 4.7μF/16VW PC electrolytic
- 1 1.5μF PC electrolytic
- 3 1μF PC electrolytics
- 4 0.15μF metallised polyester (greencap)
- 12 0.1μF metallised polyester
- 1 .047μF metallised polyester
- 2 .033μF metallised polyester
- 2 .01μF metallised polyester

Resistors (¼W, 5% unless stated)

- 2 x 1MΩ, 1 x 680kΩ, 1 x 470kΩ, 2 x 330kΩ, 3 x 220kΩ, 10 x 200kΩ 1%, 13 x 100kΩ, 7 x 100kΩ 1%, 1 x 56kΩ, 1 x 47kΩ, 6 x 10kΩ, 6 x 4.7kΩ, 1 x 3.3kΩ, 1 x 2.2kΩ, 8 x 1kΩ, 1 x 680Ω, 2 x 560Ω, 4 x 100Ω 5W

Trimpots

- 1 x 200kΩ, 1 x 100kΩ, 1 x 50kΩ, 1 x 20kΩ, 2 x 10kΩ

Miscellaneous

Machine screws and nuts, lockwashers, scrap aluminium, automotive cable, automotive wiring connectors, etc.

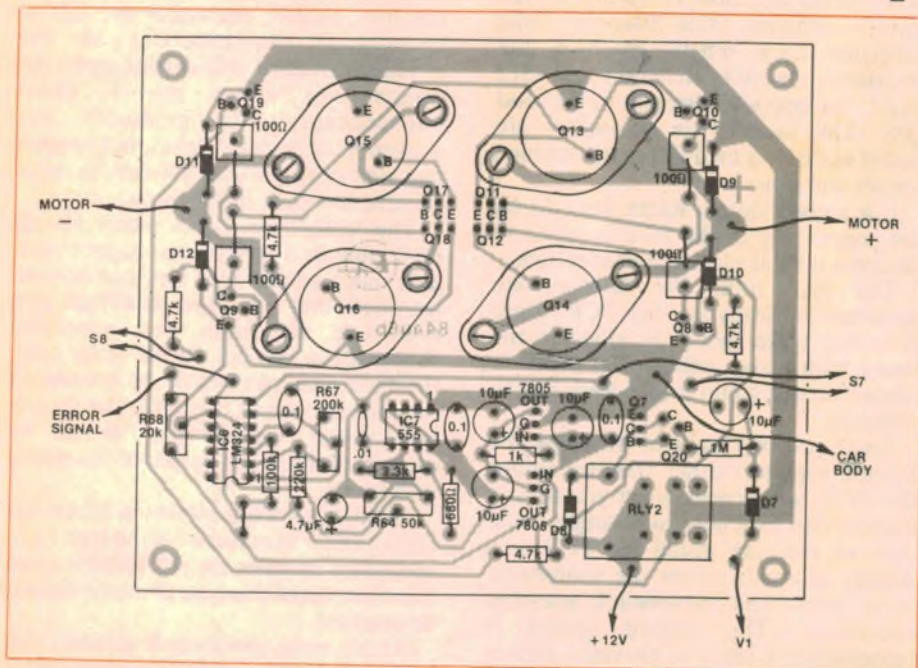
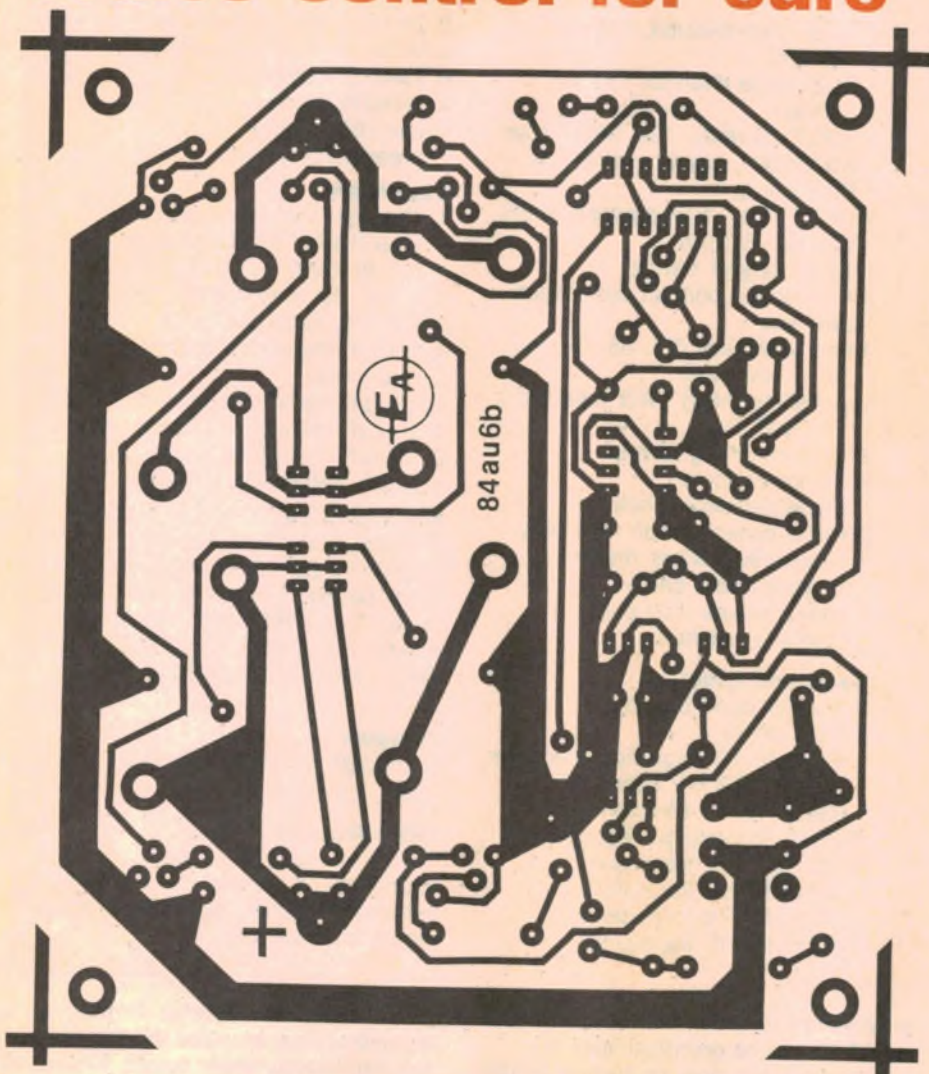
A bicycle brake cable is used as a throttle linkage between the throttle and the windscreen wiper motor. Details of the limit switch assemblies are left to individual constructors as the arrangement used will depend upon the windscreen wiper motor. Most constructors will probably use conventional microswitches, but magnet and reed switch assemblies may be more suitable for some installations.

The windscreen wiper motor should preferably be a permanent magnet type, although a wound field type can be used provided that the field windings and armature windings are normally connected in parallel. In the latter case, the field windings should be connected between the output of relay 2 and the car body while the armature should be connected across the output of the power transistors.

Windscreen wiper motors in which the field and armature windings are connected in series are not suitable since the direction of this type of motor cannot be reversed.

At this stage, the throttle actuator can be installed in the vehicle but note that it will be necessary to retain access to the

Cruise control for cars



Parts layout for the throttle actuator PCB. Take care with component orientation.

trimpots for adjustments. The PCB has a "+" sign marked on it to indicate the output that goes positive when the throttle is being opened. The corresponding "positive" terminal of the windscreen wiper motor can be determined during installation by momentarily connecting it across the car battery and noting the polarity required to open the throttle.

Final adjustments

For proper operation of the cruise control, several trimpot adjustments have to be made. To do this, a signal source, a 12V power supply and an oscilloscope are necessary. If you don't have an oscilloscope, then an AC voltmeter will do.

After installing the throttle actuator and connecting it to the car battery, turn trimpot R68 fully towards pin 14 of the LM324. Turn R64 fully towards the LM324 and R67 towards the power transistors. Now connect the anode of D7 to the positive battery terminal.

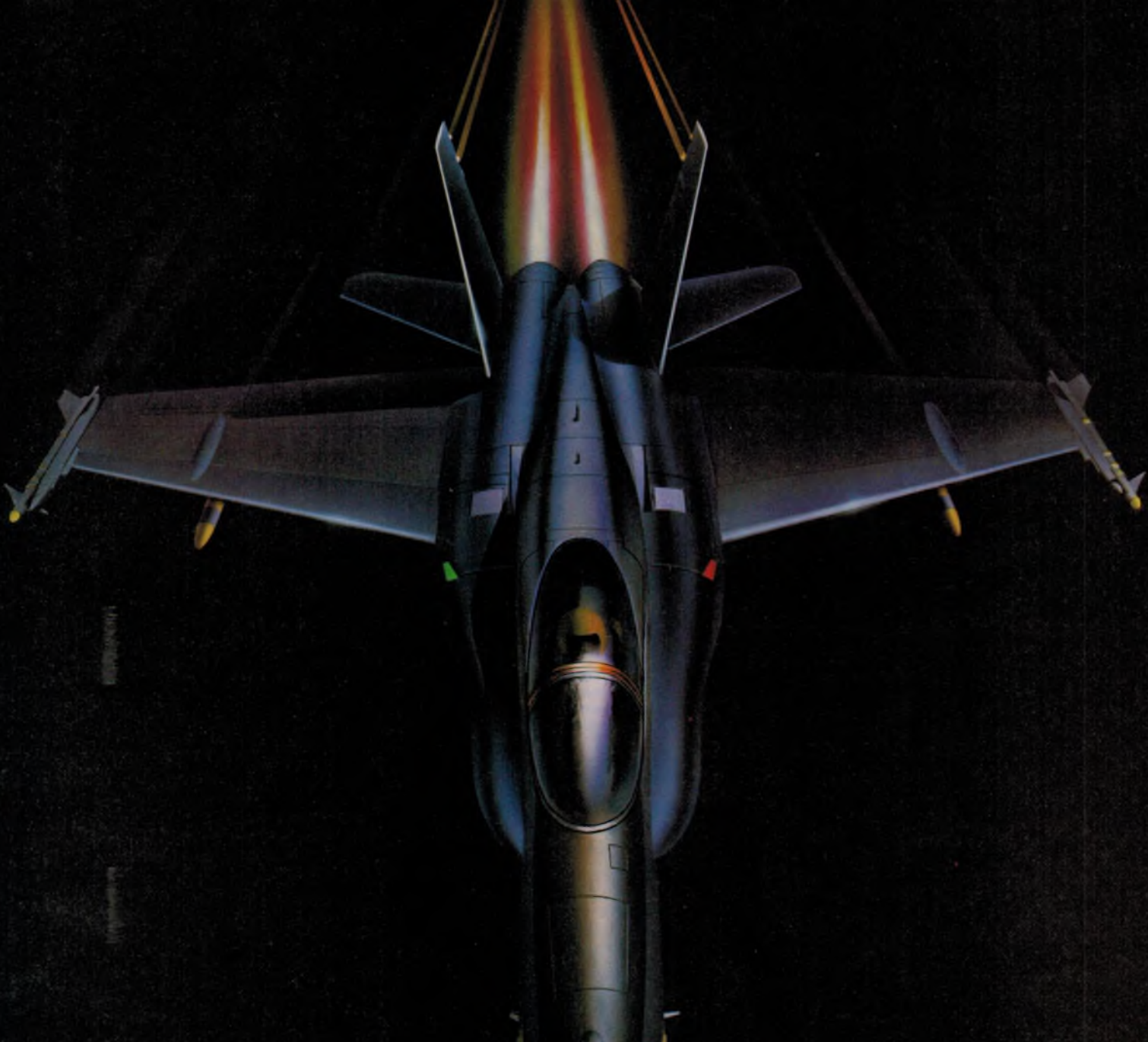
If you have a dual-trace oscilloscope, set the traces to "dc" and connect the earth leads of the probes to the car body. Make sure both traces are centred on the screen when the inputs of the probes are earthed. Connect one probe to the 5V rail and the other (set to 10:1) to the wiper of R64. Adjust R64 until the triangle waveform just touches the 5V rail trace.

Alternatively, if you don't have a CRO, connect an AC voltmeter across the output of the throttle actuator and adjust R64 until the voltmeter gives a reading. R64 should then be backed off to the point where the voltage just disappears.

For the rest of the throttle actuator adjustments, disconnect the fuel line from the carburettor to avoid flooding the engine. Now connect the error signal input to the 10V rail. Turn R68 until the windscreen wiper motor slowly pulls the throttle open. Allow the windscreen wiper motor to fully open the throttle and trip limit switch S7. Now connect the error signal input to the 0V rail. The windscreen wiper motor should close the throttle, but at a faster rate than when it was opened. This is due to the throttle return spring.

You now have to alternatively open and close the throttle, each time turning R68 a bit further until the windscreen wiper motor travels at the maximum speed without ploughing through the microswitches. Now adjust R67 so that the windscreen wiper motor opens and closes the throttle at an equal rate.

On the signal processor board, turn trimpot R29 fully away from C9, turn R50 fully towards R29 and turn R30 fully away from R50. Connect the signal processor to a 12V power supply or a car



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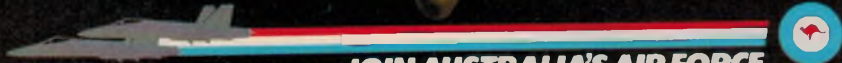
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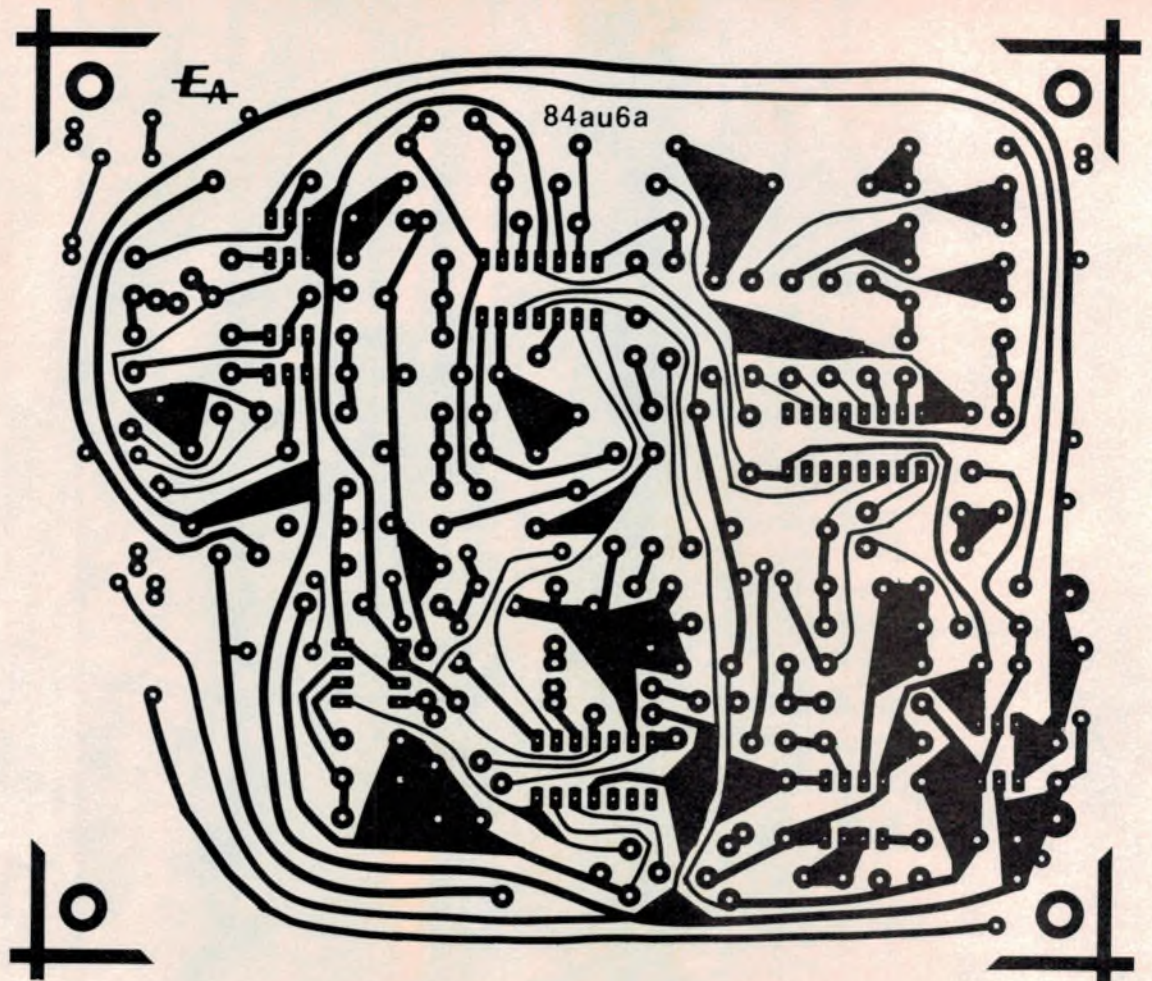
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Cruise control for cars



Actual size artwork for the signal processor PCB. The throttle actuator PCB is on page 52.

battery. Connect the speed sensor inputs to a signal source of about 100Hz. Connect an oscilloscope or voltmeter between the 5V rail and the error signal output.

Now press the engage button. If the error signal output is above the 5V rail, turn R29 until the error signal is equal to the 5V rail. If the error signal is below the 5V rail, turn R50 until the error signal is equal to the 5V rail.

The signal processor can now be installed in the vehicle and the wiring run to the speed sensor, brake lights, throttle actuator, and clutch and gear lever microswitches. A normally closed spring loaded automotive switch will probably be the best way to go for the clutch microswitch, while the gear lever microswitch can take any form that's convenient. The main point to ensure is that the switch is open when the car is in top gear, and is closed otherwise.

Do not leave any of these switches out. The cruise control will not operate correctly if you do, and could even prove dangerous.

Figs. 1 and 2 show how the speed sensor is installed in rear-wheel drive and front-wheel drive cars respectively.

On rear-wheel drive cars, the sensor should be mounted as close to the gearbox as possible, where vertical movements of the tailshaft are minimal.

The magnets are secured using tie wire and epoxy adhesive. Two magnets are shown at each position to compensate for longitudinal movements of the driveshaft.

The coil is mounted on an L-shaped bracket and secured to the car using self-tapping screws. Position the bracket so that there is a 25mm air gap between the coil and the magnets when they are directly opposite each other. Finally, carefully route the two-core cable from the coil to the speed sensor inputs on the signal processor.

On front wheel drive cars, the magnets are mounted at four locations, 90° apart. This is because the driveshaft on a front-wheel drive vehicle rotates much more slowly than the tail shaft on a rear-wheel drive vehicle. The magnets should be positioned either on the driveshaft coupling flange or, if this is not possible, as close to the inboard end of the driveshaft as possible.

Check to ensure that there is little relative movement between the pickup and the magnets as the suspension moves. Check also that the installation does not foul any other part of the vehicle over the full extent of the suspension travel.

Now we come to the road test. Drive to a quiet, preferably hilly, road, bring the car up to normal cruising speed, and

engage the cruise control. Now ease your foot off the accelerator pedal — the cruise control should take over.

It is now a matter of adjusting R30, which is the error signal gain control, so that the cruise control gives a smooth response when going up and down hills, but keeps the speed to within reasonable limits. You should be able to adjust the gain to give a smooth response while keeping the speed to within 3km/h of the set speed.

Once the gain has been set, install the signal processor permanently under the dashboard.

Other speed setting methods

There are other ways of setting the speed besides bringing your car up to cruising speed and pressing a button, as in this design. You can in fact substitute a potentiometer for half the circuit of the signal processor and use this to set the speed.

If you wish to set the speed by adjusting a pot, then delete: IC3 and 4; Q4 and Q5; R3 to R24; R55, R56 and R57; and C5 to C8. Connect a 1kΩ pot between the 5V rail and the 10V rail and connect its wiper to R25. Replace R27 with a 100kΩ resistor and trimpots R29 and R50 with links.

The cruise control is now engaged by pressing the resume switch S6, while the speed is set by the 1kΩ pot.

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Straight sail

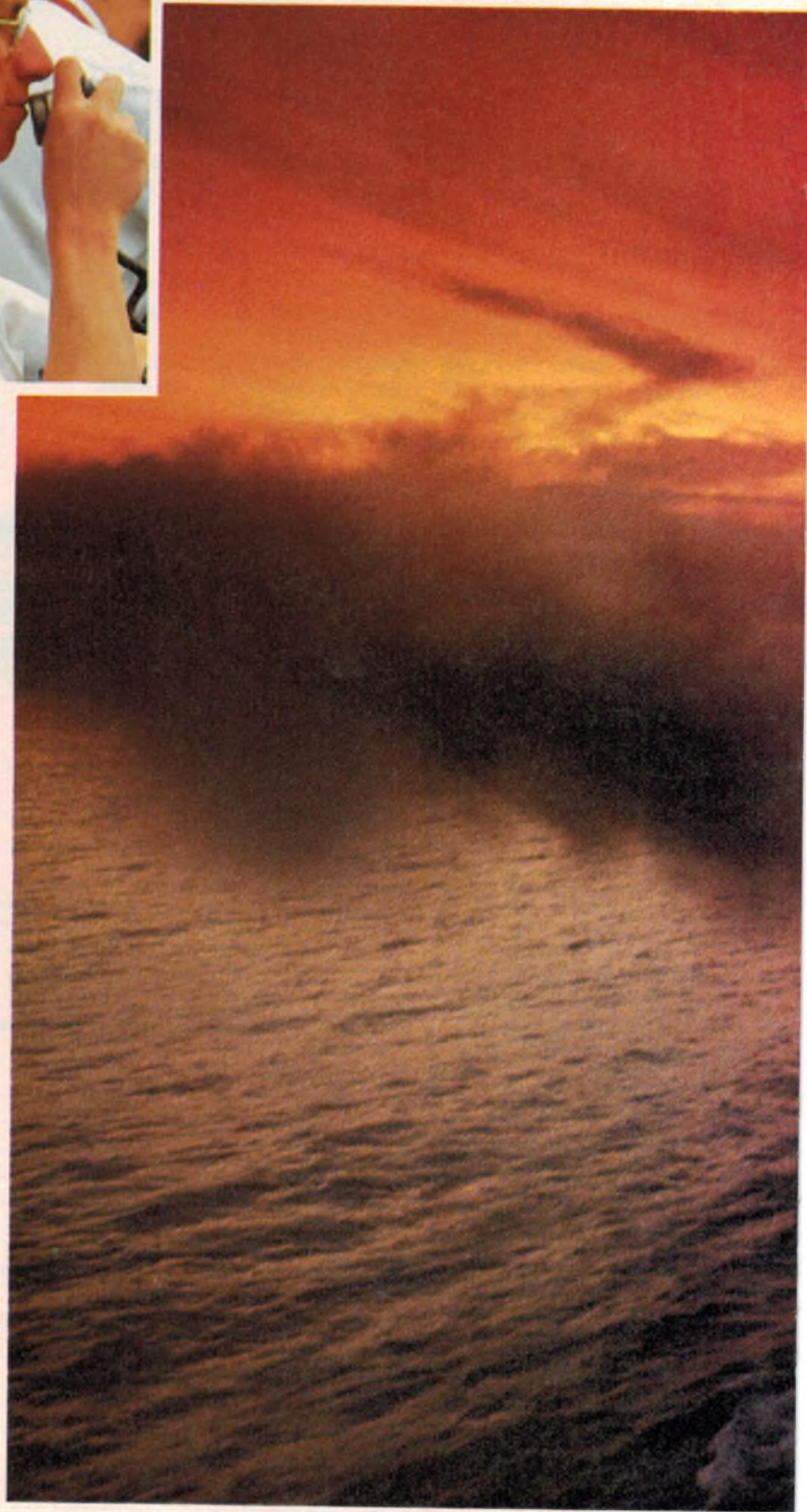


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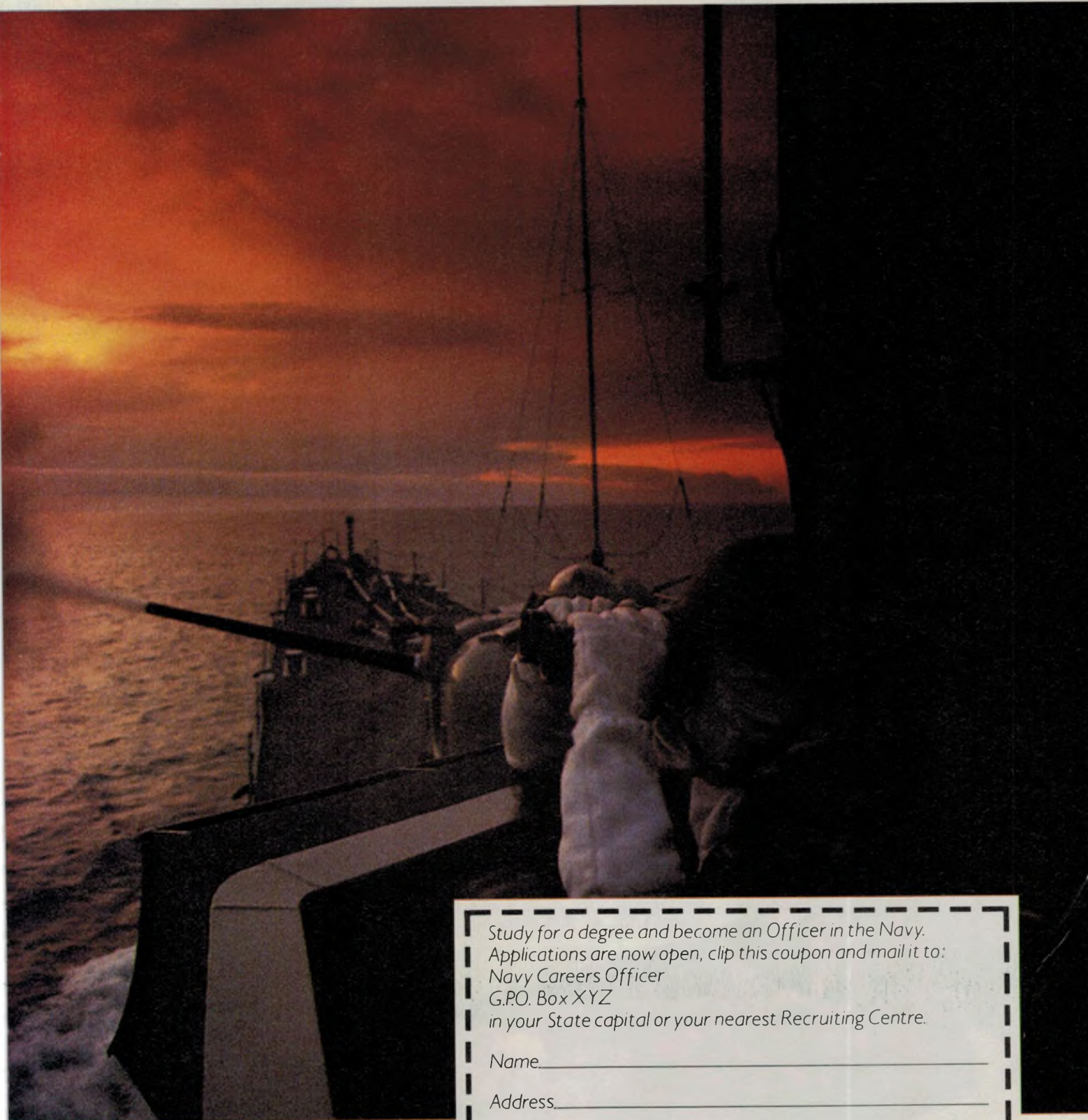
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ELECTRONICS Australia, June, 1984

By any standard, the UHF transceiver described in the September, October and November 1983 issues of EA has been an outstanding success. Many hundreds have been successfully built and the kit supplier responsible, Dick Smith Electronics, has not been able to keep up with the demand.

As the reputation of the UHF transceiver has grown, more and more amateurs have decided to have a go at building a really worthwhile piece of gear for themselves. At the same time, they can save a substantial amount of money over the price of an equivalent commercial unit.

We're very glad to be able to report this development because it signals a resurgence in the construction of gear amongst amateurs who, for a long time, have been content to buy rather than build.

In fact, the UHF transceiver kit has been hailed both here and overseas as being perhaps the most significant amateur radio construction project to be published anywhere for a long time!

Just as night follows day, there was bound to be a call for a two-metre version of the transceiver. We ourselves remarked that the VHF version was just crying out to be produced.

Well now it has happened. The same team that produced the UHF kit, Garry

by LEO SIMPSON

BUILD THIS: **VHF amateur transceiver**

Are you an amateur wanting to upgrade your two-metre gear? Then here's your chance to do it by putting together this up-to-the-minute transceiver which has all the most wanted features. The price? Just \$199.

Crapp VK2YBX/T, and Gill McPherson, VK2ZGE, have put their thinking caps on and produced a two-metre transceiver that will certainly set any keen amateur longing.

Features

As the accompanying spec panel shows, this new two-metre transceiver from Dick Smith Electronics has very good performance which is matched by the features that most amateur radio operators want. Note also that there are very few options available because they are all built in to the basic price.

Topping the list of features is, of course, the price. One hundred and ninety-nine dollars buys you a complete transceiver with all the features pictured, including the press-to-talk dynamic microphone. That has to be a really good deal.

And Dick Smith Electronics has gone one step further in providing a basic antenna kit so that there will be no

temptation to switch on the transmitter with no load as soon as it is completed. The antenna kit comprises a quarter-wave vertical radiator, gutter-grip mounting base and feed, a PL-259 connector and three metres of good quality coax cable, all for \$24.95.

For those amateurs not in a club and not sure of their ability to complete the transceiver successfully, DSE have their "Sorry Dick, it doesn't work" service coupon. This costs an additional \$50 and may take up to three weeks service time if the constructor decides to take advantage of the offer but at least it is a sure way of getting an operational unit, if all else fails.

Operating facilities on the new transceiver are all that most amateurs would want without all the "bells and whistles" of some of the fancy imported models. There are none of those hard-to-remember-how-to-use memories and the frequency readout and selection is via no-nonsense push-button type "thumbwheel" switches.

As is usual practice with two-metre amateur transceivers, the two most significant digits of the frequency section are omitted which means that there is an assumed decimal point between the first and second digits of the three-digit readout (ie, 14--MHz). In the photos, this means that the transceiver is set for a frequency of 147.02MHz.

Standard controls for volume and squelch require little comment as does the signal strength-cum-power meter. The microphone socket is a standard configuration allowing press-to-talk operation.





In addition, there is a three-position switch for simplex and plus or minus 600kHz transmitter offset for working into repeaters and there is also an anti-repeater button so that the transceiver can be used to listen in on the repeater receiving frequency.

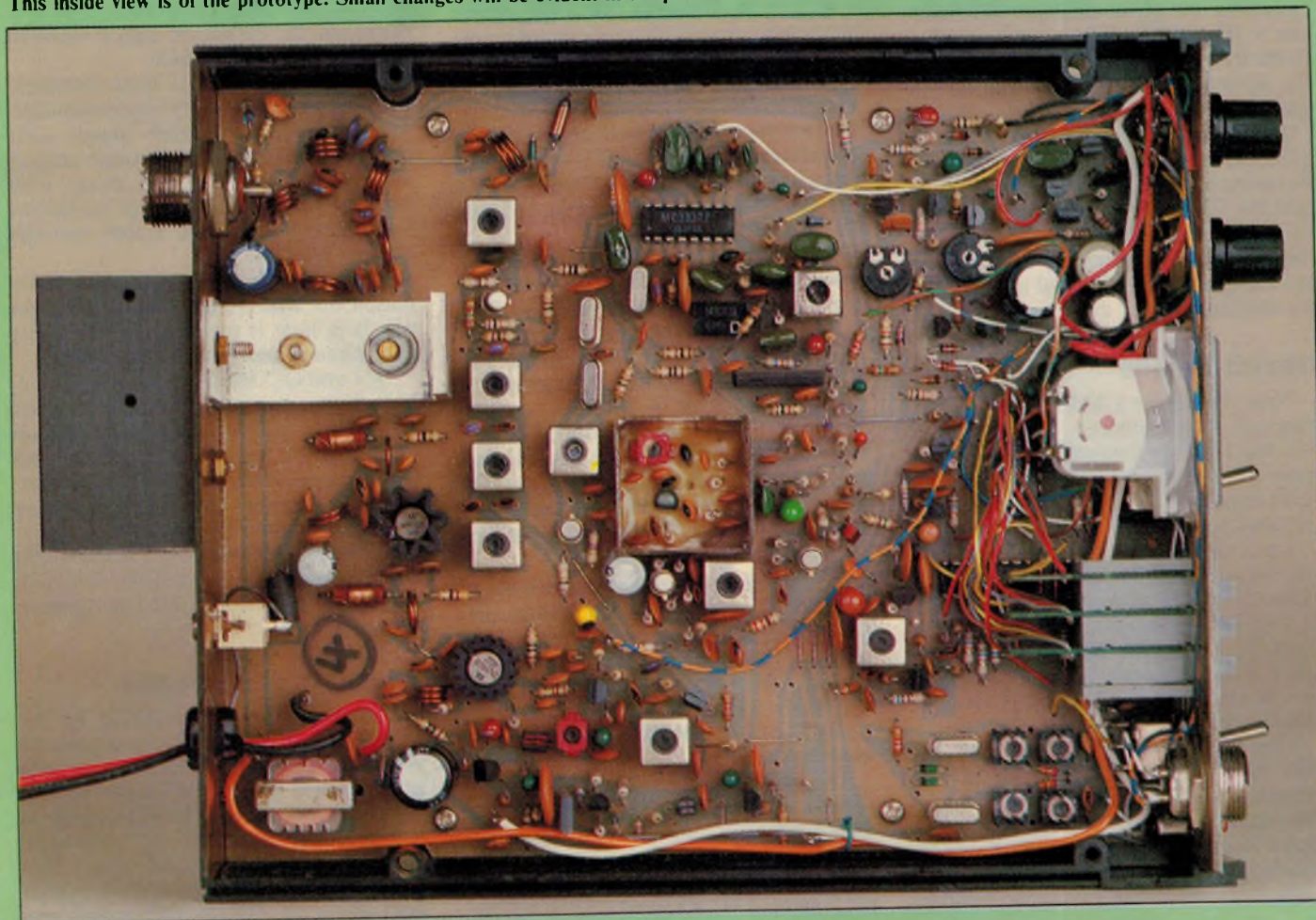
Finally, there is the 5kHz offset switch which effectively doubles the number of channels from 400 to 800, albeit with 5kHz channel spacing.

How it works

Readers who have already taken a

look at the circuit and block diagrams will have noted the similarities to the circuit of the abovementioned UHF transceiver described last year. Some sections of the circuit, notably the microphone preamplifier and audio power amplifier, are identical while other

This inside view is of the prototype. Small changes will be evident in the production models.



VHF transceiver

sections, such as the antenna filter, IF strip and power supply, are also very similar.

For those not familiar with the series of articles on the UHF transceiver, let's now go through the block diagram, before attacking the main circuit diagram. Refer now to Fig. 1.

The block diagram shows that the transceiver is split into two sections, receiver and transmitter, which come together in the antenna filter. Both these sections employ a common frequency synthesiser and voltage controlled oscillator.

The receiver is a conventional double conversion superheterodyne with intermediate frequencies at 10.7MHz and 455kHz. The second conversion from 10.7MHz to 455kHz is achieved in an integrated circuit which also includes limiting amplifiers and an FM quadrature detector. From there the signal is passed to an audio amplifier.

The VCO (voltage controlled oscillator) has two modes and, as you might have guessed, these are transmit and receive. In the transmit mode, the VCO is set to an exact frequency within the range of 144 to 148MHz by the frequency synthesiser which, in turn, is controlled by the offset oscillator. The output of the VCO is fed via Q17 and Q18 to the RF power amplifier and thence via the antenna filter circuit to the output socket.

In the receive mode, the VCO is set at a frequency exactly 10.7MHz below the incoming frequency. This is necessary to give the 10.7MHz intermediate frequency at the output of the mixer, Q7. The lower VCO frequency is obtained by switching a different crystal into the offset oscillator.

Circuit details

Now let's have a look at the circuit diagram. Don't shudder. If you figured out the UHF transceiver described last year, this one is more straightforward in most respects. We'll consider the receiver circuitry first.

Input signals from the antenna are fed via the antenna filter and RF switching network on the extreme righthand side of the circuit diagram. The signals pass via L30, L29, L27, L26 and L28 and C123. From there they go to the input of Q6 via transformer L2 and C11 (on the extreme lefthand side of the circuit).

The RF switching is performed by D13 (near L28, on the RH side of circuitry). In the transmit mode, D13 is forward biased and thus shorts out any RF signal from the transmitter which would otherwise be fed into the receiver input.

Q6 is a conventional common emitter

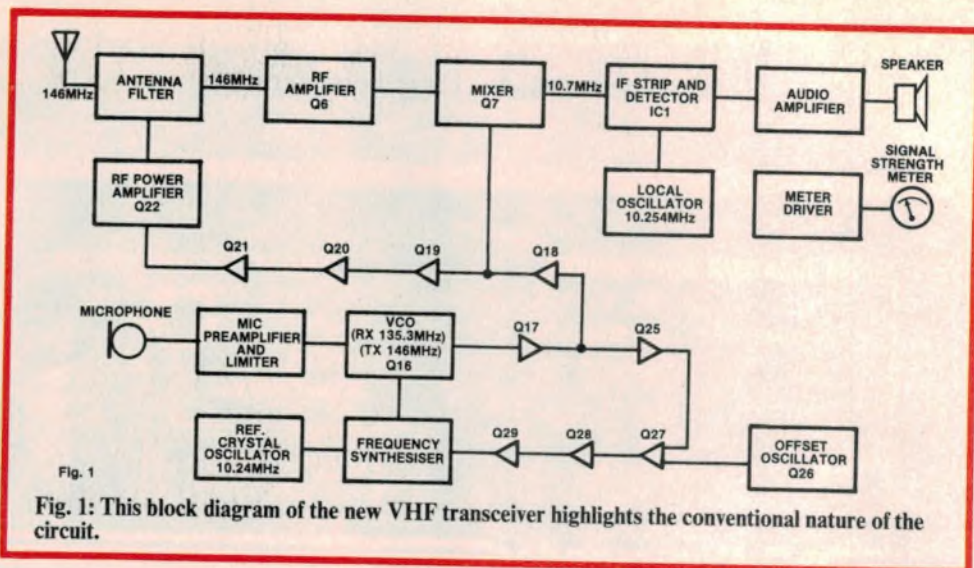


Fig. 1: This block diagram of the new VHF transceiver highlights the conventional nature of the circuit.

amplifier with L3 as its collector load. L3 is part of the three-stage bandpass filter which only accepts signals in the 144 to 148MHz range.

Mosfet Q7 is the mixer. Gate 1 of Q7 is the incoming RF signal while gate 2 is the VCO (local oscillator) signal. L6 is the drain load of Q7 and the mixer output is the difference frequency, 10.7MHz. This is passed via FL1, a two-pole filter, to IC1.

IC1 is a Motorola MC3357 device specifically designed for use in a narrow-band FM dual conversion communications receiver which is exactly what this circuit is. We have already talked about the first conversion which is from 144 (to 148MHz) down to 10.7MHz which takes place in mixer Q7. The MC3357 handles the second conversion using an internal 10.245MHz local oscillator.

This gives a second intermediate frequency signal of 455kHz which is amplified, limited and detected by IC1. IC1 also provides the squelch function.

In greater detail, crystal X1 at pin 1 of IC1 sets the local oscillator frequency to 10.245MHz. This is internally mixed with the 10.7MHz signal from Q7 to produce a 455kHz IF which is then fed to an external filter at pin 3. Transistor Q8 amplifies the filtered 455kHz signal and feeds it back into the limiting amplifier input at pin 5.

The limiting amplifier is a five-stage differential amplifier which boosts the 455kHz signal well into clipping, at its output. That is, we say the signal is limited. This effectively removes any amplitude variations (AM) so that the signal only contains frequency modulation.

The limited signal is then fed to the internal FM quadrature detector associated with coil L7 and capacitor C37 at pins 7 and 8.

The detected audio is extracted from pin 9 and fed via R33 and C35 to VR40,

the volume control. At the same time, a sample of the signal is coupled via R32 and C33 to an internal amplifier between pins 10 and 11.

This amplifies any noise signal (hiss) above the expected audio passband which is then rectified by D7 and used to "squell" the audio output via control pin 12. VR39 is the squelch control.

Transistor Q8 feeds a portion of the 455kHz signal (before limiting is applied) to IC7, the meter amplifier. This produces an indication of signal strength when in the receive mode.

Transistors Q9 to Q12 form a conventional audio amplifier. Q9 is a straightforward common emitter stage with negative feedback applied to the emitter via R44. Q10 is a class-A driver with bootstrapping via the output capacitor, C47. Its collector load is R49 and the speaker itself.

If the speaker is disconnected for any reason the whole amplifier will latch up which is how it manages to withstand open-circuits continuously (see specs).

Q11 and Q12 form a fully complementary output pair with quiescent current set by R46 and D8. R47 and R48 are rather high in value at 2.2Ω which gives good bias stability, limits the power output to some extent and gives momentary short circuit protection.

Resistors R44 and R43 set the audio amplifier gain to around 25 (ie, 5600/220 = 25) while C45 rolls off the response above 3kHz.

Transmitter operation

The transmitter is controlled by the press-to-talk switch on the microphone and this controls the various supply rails, as mentioned above. We'll come back to that. The signal from the microphone is fed to the pre-amplifier, Q13 and Q14, which provide substantial gain. The amplified signal is fed via C52 to a diode limiting circuit, D9 and D10, which pre-

vent the following stages from being overloaded.

The signal from D10 is fed to Q15, a two pole active filter stage with a gain of unity. The output of this stage is the modulating signal which is applied from trimpot VR61 to varicap diode D11 via R62, C57 and R64. D11 is in the tank circuit of the VCO (Q16), and thus is able to frequency modulate the VCO according to the microphone signal voltage.

The VCO is a conventional grounded gate oscillator using an N-channel FET. It oscillates at a nominal 146MHz (centre of band) as set by L8 and C64. Varicap D12 sets the VCO to the exact frequency required, as controlled by the frequency synthesiser.

The main VCO output signal is taken from its source and fed to Q17 and Q18, which are transformer coupled, and thence to Q19 and Q20 which are more or less conventional common emitter amplifier stages. Q21 and Q22, on the other hand, are class-C power amplifier stages which operate without forward bias at their bases.

By way of explanation, in a class-C amplifier such as Q22, the collector current flows for substantially less than every alternate half cycle with the tuned circuit preventing the generation of harmonics. In effect, a class-C amplifier tank circuit can be considered as the analog of a flywheel which has a short burst of energy applied to it during every cycle. It is a highly efficient amplifier.

The output power from Q22 is coupled to the antenna filter circuit mentioned previously. The path is via L26, L27, L29 and L30 to the output socket. A measure of the transmitter output is provided as follows: Gimmick capacitor C169 (two wires twisted together) feeds a small portion of the transmitter output to D14 which rectifies the signal and applies the resultant DC to the signal meter via R109 and filter capacitor C134.

Frequency synthesis

The method of frequency synthesis is essentially a variation on the conventional phase lock loop (PLL) circuit. A PLL normally comprises a voltage controlled oscillator (VCO), a reference oscillator, a programmable frequency divider (fed by the VCO), and a phase comparator which compares the frequency divided output of the VCO with the reference oscillator.

For a VHF transceiver it is usual to have three oscillators: a VCO, a reference oscillator and an offset oscillator. In this case the VCO is Q16, the reference oscillator is associated with IC6 and the offset oscillator is Q26. IC5 is the phase comparator and IC4 is the programmable divider.

Let's start by looking at IC6. This IC is

SPECIFICATIONS

GENERAL

Frequency Coverage	144 to 148MHz (see text)
Channel Spacing	10kHz; with 5kHz offset
Number of Channels	400 @ 10kHz; 800 @ 5kHz (see text)
Frequency Stability	within ± 10 ppm from 0 to 60°C
Modulation	Frequency Modulation
Temperature Range	from 5 to 50°C
Duty Cycle	two minutes transmit, two minutes receive
Supply Voltage	12 to 15V DC; test voltage 13.8V DC
Polarity	negative chassis
Current Drain	Receive: muted, 110mA; unmuted, 300mA Transmit: 1.9A at 10W; 2.5A at 15W
Protection	(a) 3A in-line fuse (b) diode reverse polarity protection (D1) (c) RF power amplifier can withstand up to 5:1 VSWR and open or short-circuit conditions for at least two minutes (d) audio power amplifier can withstand open circuit continuously and momentary short circuits

TRANSMITTER

Power Output	10 watts nominal; 15 watts maximum
Maximum Deviation	limited to 5kHz under normal operation; up to 10kHz with overdrive
Distortion	less than 10% at 3kHz deviation
Spurious Emissions	less than 60dB with respect to carrier
Harmonics	less than 60dB
Microphone Sensitivity	5mV RMS

RECEIVER

Sensitivity	0.5 μ V into 50 Ω for 12dB SINAD; typically 0.4 μ V
Selectivity	better than 60dB at ± 25 kHz
Audio power	1W at 1% THD into 8 Ω
Frequency response	6dB/octave rolloff above 1kHz

a combined oscillator and divider with a division ratio of 1024. It drives crystal X2 at a frequency of 10.24MHz which when divided by 1024 produces a reference frequency of 10kHz at pin 7.

IC5, the phase comparator, compares the 10kHz reference frequency from IC6 against the 10kHz output from the programmable frequency divider, IC4. The output at pin 3 of IC5 is the PLL error voltage which is a series of pulses. These are filtered to produce smooth DC by R91, C156, R87, R86 and C153. This DC error voltage is then applied to D12 in the VCO (Q16) to maintain control over the VCO output.

As shown on the circuit, when the PLL is in the lock condition and the VCO output is 144MHz, then the error voltage at TP3 is 2.7 volts DC (after setting up).

Where the frequency synthesiser circuit diverges from normal PLL practice is that the programmable divider does not merely "divide down" the output of the VCO. Instead, IC4 divides the difference between the VCO output and

the third harmonic of the offset oscillator.

The reason for this indirect procedure is that it is not possible to easily provide for programmable division directly from 144MHz.

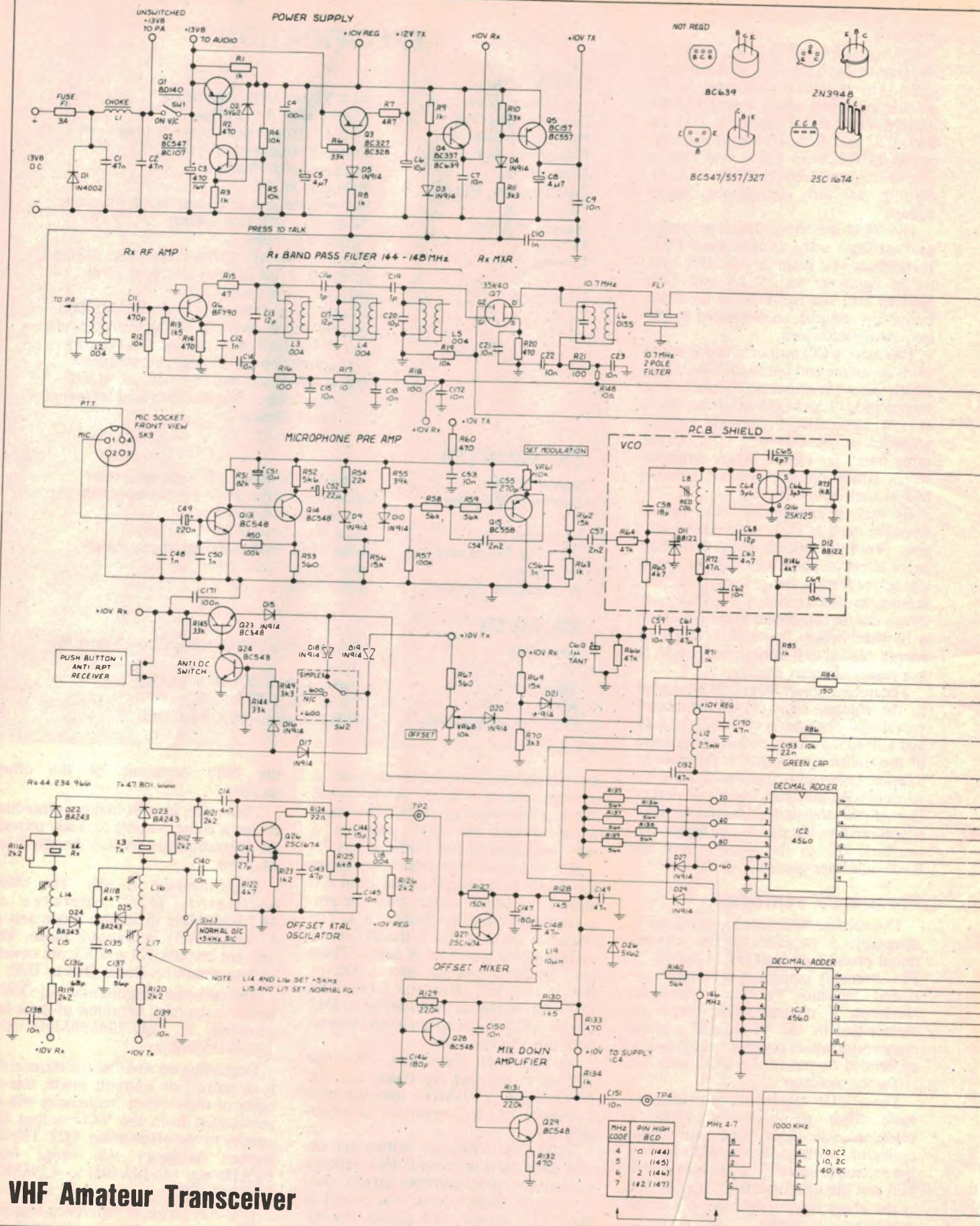
What happens is this. The offset oscillator, Q26, operates at 44.234966MHz in receive mode and at 47.801666MHz in transmit mode. The relevant crystals, X4 and X3, are switched into circuit by diodes D23 or D22.

The collector output circuit of Q26 is tuned to the third harmonic of these frequencies ie, 132.704898MHz and 143.404998MHz.

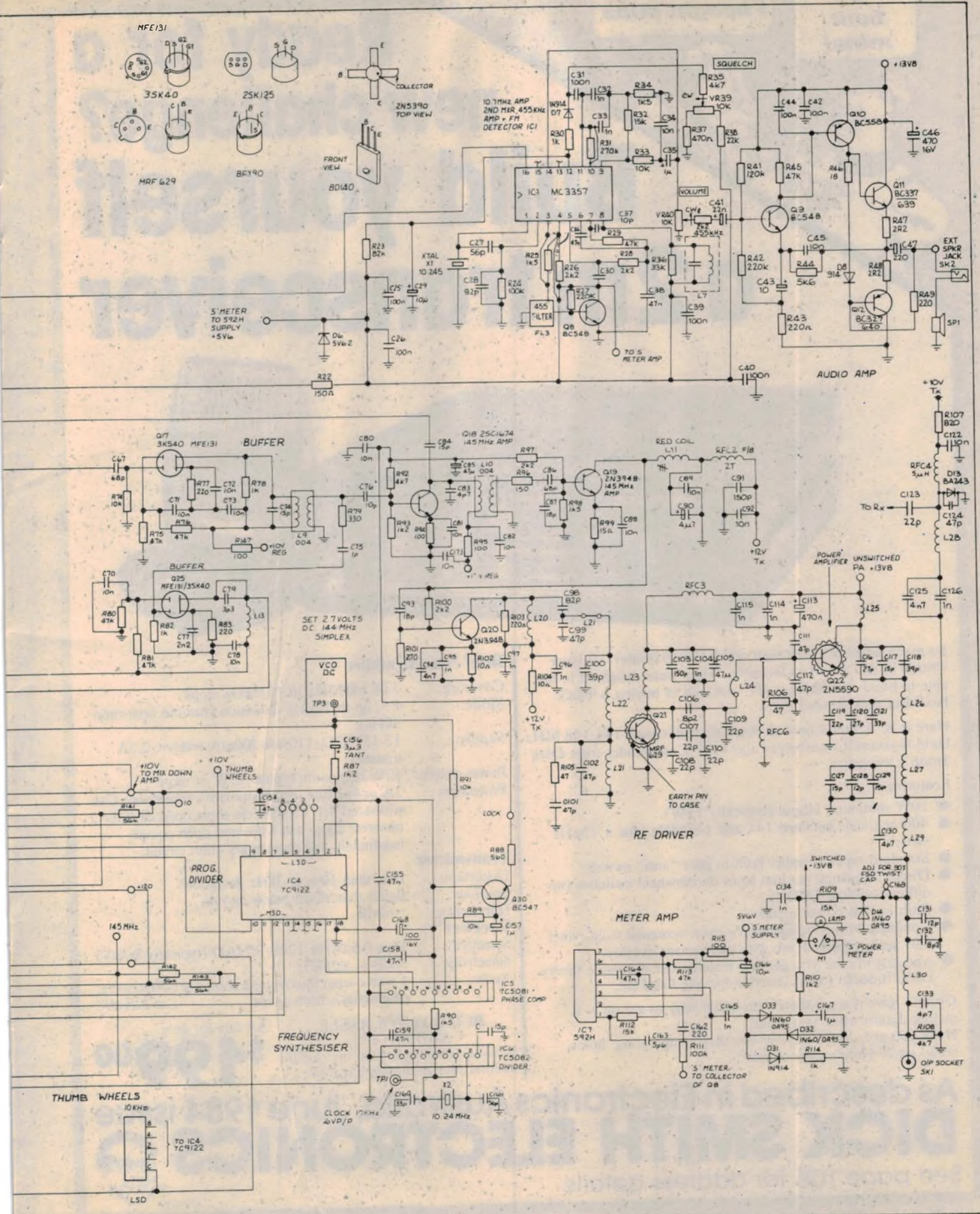
Depending on whether the transceiver is in receive or transmit mode, one or other of these offset frequencies will be subtracted from the VCO output frequency by the offset mixer, Q27. The difference frequency will range from 595kHz (eg, 144-143.405) to 4.595MHz (148-143.405).

It is this range of difference frequency

Continued on page 65



VHF Amateur Transceiver



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I bought mine



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Brief Specifications

- Coverage: 144-148MHz in 10/5kHz steps
Mode: F3, up to 10kHz deviation (normal operation 5kHz)
Supply: 12-15V DC, 110mA-300mA receive, 2.5A transmit
Power output: 10W minimum, typical 15W or more
Protection: 3A in-line fuse, reverse polarity protection. Can withstand 5:1 VSWR (inc short/open circ) for 2 minutes; audio can withstand open circuit indefinitely and momentary short circuit.

Transmitter

- Distortion: Less than 10% at 3kHz deviation
Spurious: Better than 60dB below carrier.
Harmonics: -60dB

Receiver

- Sensitivity: Max 0.5uV for 12dB SINAD (typically 0.4uV)
Selectivity: 60dB at ± 25 kHz
Audio: 1 watt output into 8 ohms response 6dB/octave, de-emphasis from 1kHz Cat K-6308

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As described in Electronics Australia, June 1984 issue

DICK SMITH ELECTRONICS

See page 108 for address details



A764/KT

VHF transceiver

cies which is applied to the programmable frequency divider, IC4, via Q28 and Q29.

So IC4 is programmed by the thumb-wheel switches to divide the relevant difference frequency from Q27 to provide a 10kHz output which is applied to the phase comparator, IC5.

Note, by the way, that the difference between the transmit and receive offset frequencies is 10.7MHz which is the required intermediate frequency.

So far so good. But now we have to backtrack a little. There is a problem in that IC4 cannot precisely divide frequencies that are not an exact multiple of 10kHz. Therefore that example of 595kHz (the lowest difference frequency) is not valid. And in fact, those offset oscillator frequencies given above are not quite correct.

Because of the provision for 5kHz channel spacing, the offset oscillator crystals are in fact 1666Hz too high. When the third harmonic of each crystal is considered it will be 5kHz high. So in normal operation, the crystals are pulled low by L14 and L15 for X4 and L16 and L17 and X3. So the normal offset transmit frequency is 47.8MHz (143.4MHz 3rd harmonic) and the offset receive frequency is 44.2333MHz (3rd harmonic is 132.7MHz).

When these offset frequencies are subtracted from the VCO the range of difference frequencies will be 600kHz to 4.6MHz. And note that 600kHz is an exact multiple of 10kHz.

When the +5kHz facility is switched on, L15 and L17 are switched out of circuit by diodes D24 and D25, so that now the crystals do run 1666Hz high and so the VCO frequency is shifted up by 5kHz.

Rear panel view (left to right): supply leads, remote speaker socket, RF power transistor heatsink and antenna socket.

Band protection

Note that when the 10kHz outputs of IC6 and IC4 (the programmable divider) are locked together IC5 turns on Q30. This turns on Q18 and Q19 and thus allows the transmitter to operate. Thus the transmitter is prevented from producing signals which are outside the 144 to 148MHz band.

But what about that +5kHz offset we have just discussed. When that is applied it would be possible for the VCO to operate at 148.005MHz and still produce a lock condition. The circuit design takes care of this possibility too since the thumbwheels are wired to only permit a maximum VCO frequency of 147.99MHz. When the 5kHz is added this gives a maximum VCO frequency of 147.995MHz which is still inside the band limits.

Strictly speaking then, this means that only 399 channels are available with 10kHz spacing and 798 channels with 5kHz spacing (144.005 to 147.995MHz).

± 600kHz offset

Yet another factor has to be taken care of by the frequency synthesiser circuitry. For repeater operation, the transmitter frequency usually has to be offset by minus 600kHz from the receive frequency. Less often, it may have to be changed by plus 600kHz. This condition could be met by adding more crystals to the offset oscillator circuitry but in this circuit it has been achieved digitally.

As well as avoiding the expense of extra crystals, the digital method of offset does not require any alignment. IC2 and IC3 are digital adders. They add a code of 60 or 120 to the code applied by IC4. In the normal simplex mode, the addition of the 60 code is the standard. For -600kHz repeater operation, this code is removed (controlled by D18 and IC2).

For +600kHz operation, IC2 and IC3 are brought into play by D29 and D27 to add a code of 120 to IC4.

A neat advantage of this scheme is that it allows the "anti-repeater" operation whereby the receiver only can be shifted by ±600kHz. This is achieved by the pushbutton in conjunction with Q23, Q24 and associated diodes. The advantage of the anti-repeater function is that it allows the operator to listen directly to his contact instead of via the repeater.

Note that when the 600kHz offset facility is in use, the out-of-band protection circuitry does not prevent transmission outside the band limits. In this case it is up to the operator to make sure he or she does not transgress.

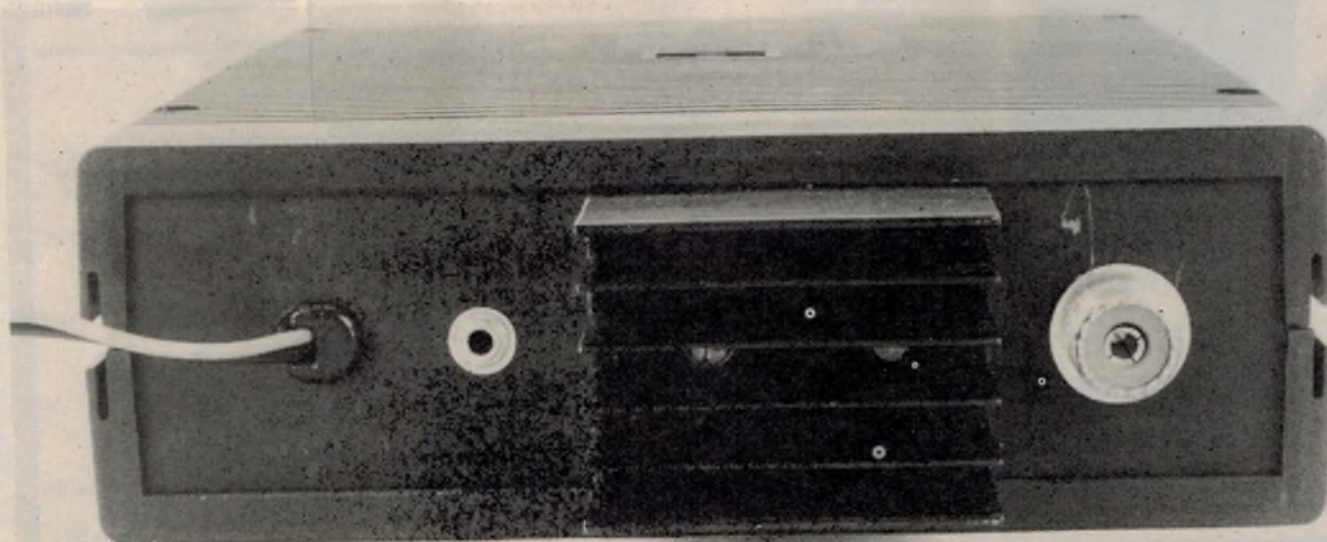
Power supply

A +10V regulated supply derived from Q1, Q2 and D2 supplies power directly to the VCO, offset oscillator, frequency synthesiser circuitry and mix down amplifier (Q28 and Q29). The +10V regulated rail is also switched to various other sections of the circuit by Q4 and Q5, depending on whether the transceiver is in the receive or transmit mode.

When in the receive mode, the press-to-talk switch is open and D3, D4 and D5 cannot conduct. Therefore Q4 supplies the +10V Rx rail. When the PTT switch is closed for transmit mode, D3 and D4 conduct, turning off Q4 and turning on Q5 to supply the +10V Tx rail. D5 also conducts, turning on Q3 to supply the +12V Tx rail.

The final two stages of the RF power amplifier, Q21 and Q22, are powered directly from the 13.8V (battery) supply, as is the audio amplifier. This is OK since Q21 and Q22 are normally biased off and can only operate when Q19 and Q20 are turned on by the +12V Tx rail.

Continued next month



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Character set — 228 ASCII characters. Normal and italic alpha-numeric fonts, symbols and semi-graphics.
Printing speed — 80 CPS 640 dots/lines per second.
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Printing direction — Normal — Bidirectional logic seeking. Superscript and bit image graphics — Unidirectional left to right.
Dot graphic intensity — Normal — 640 dots 190.5mm (7.5") line horizontal. Compressed characters — 1,280 dots/190.5mm (7.5in) line horizontal. Line spacing — Normal — 4.23mm (1/6"). Programmable in increments of 0.35mm (1/72") and 0.118mm (1/216").
Columns/line — Normal size — 80 columns. Double width — 40 columns. Compressed print — 142 columns. Compressed double width — 71 columns. The above can be mixed in a line.
Paper feed — Adjustable sprocket feed and friction feed.
Paper type — Fanfold Single sheet. Thickness — 0.05mm (0.002") to 0.25mm (0.01"). Paper width — 101.6mm (4") to 254mm (10").
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The new Ferguson single-board computer has a multiple-density disk controller, it can use 1793 or 8877 controller chips since it generated the signal with TTL parts. The board has two connectors for disk signal with 34 pins for 5.25" drives, the other with 50 pins 8" drives.

VASTLY IMPROVED CRT DISPLAY

The new Ferguson SBC uses a 6845s CRT controller and 8002 Video Attributed controller to produce a display that will rival the display of quality terminals. Characters are formed by a 5 x 7 dot matrix on 15.75 KHz monitors and 7x9 dot matrix on 15.75 KHz monitors. The display is user programmable with the default display 24 lines of 80 characters.

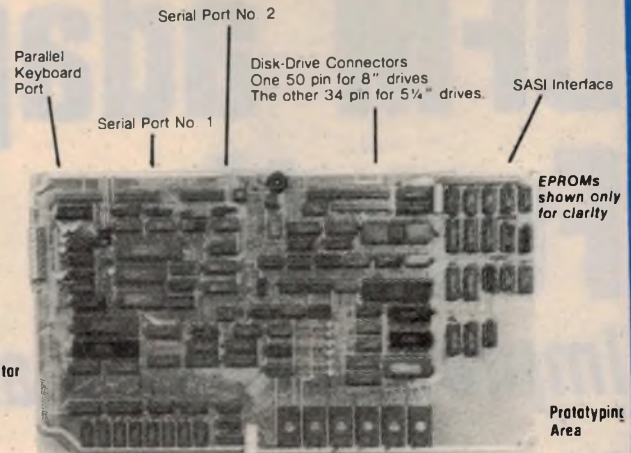
STD BUS CONNECTOR

The Ferguson computer brings its bus signals to a convenient place on the PC board where users can solder a DSTD bus cards can be plugged directly into it, and it can as well be connected by bus cable to industry-standard card cages.

A Z80-A S10/0 = TWO ASYNCHRONOUS/SYNCHRONOUS SERIAL PORTS

TWO Z80-A CTCs = EIGHT PROGRAMMABLE COUNTERS/TIMERS

The new Ferguson computer has two Z80-A CTCs. One is used to clock data into and out of the Z80-A S10/0, while the other is for systems and application use.



PROM PROGRAMMING CIRCUITRY AND SOFTWARE

The new Ferguson SBC has circuitry and drivers for programming 2716s, 2732(A)s, or pin-compatible (E) EPROMs. Software \$25 extra.

CP/M

CP/M with Russell Smith's CB10S for the new Ferguson computer is available for \$230 + TAX. The CB10S is available separately for \$65 + TAX. Actual board size: 39.6cm x 22.2cm. 5 inch B10S being developed. Approx price \$95 + TAX.

Kit Price

\$695 inc tax Less 10% for 3+

\$895 Assembled and Tested

KIT PRICE FOR THIS MONTH

\$649.00

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- ★ Centronics compatible parallel printer interface. (6522)
- ★ Buss expansion interface with DMA channel. (6844)
- ★ Dual timer for real time clock application.
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DFM adaptor for the Function Generator

Improves linearity and measures to 300kHz

Did you build the Function Generator described in April 1982? Now you can add this enhancement which lets it operate as a frequency meter and improves the linearity of the coarse frequency control.

by JEFF SKEEN & LEO SIMPSON

The Function Generator was and still is a very popular project. Now, in response to a number of requests, we have produced a small printed circuit board which enhances the capabilities of the project.

For those not familiar with the Function Generator and who do not have access to the original April 1982 article, the circuit itself was republished in last month's issue in an article entitled, "What to do if your project doesn't work". Reference to that circuit will show that there are two major sections: the oscillator, involving the XR2206, and the frequency meter, involving the 74C926.

In the original design the frequency meter section of the circuit was permanently connected to the output of the XR2206 oscillator; it could not measure the frequency of external signals. The rationale for this approach was that we did not want to unduly complicate the design. That the project has proved so popular indicates that this was a good decision. Now we are providing an option to those who wish to make use of that frequency meter.

The modification gives the Function Generator the ability to measure frequencies up to 300kHz and above, depending on the signal level. The accompanying graph shows a plot of input sensitivity versus frequency. For most of the range the sensitivity is around 20 millivolts peak-to-peak or better which is more than adequate for most applications.

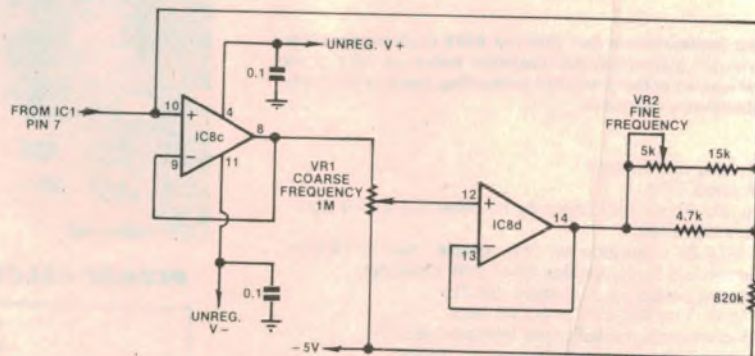
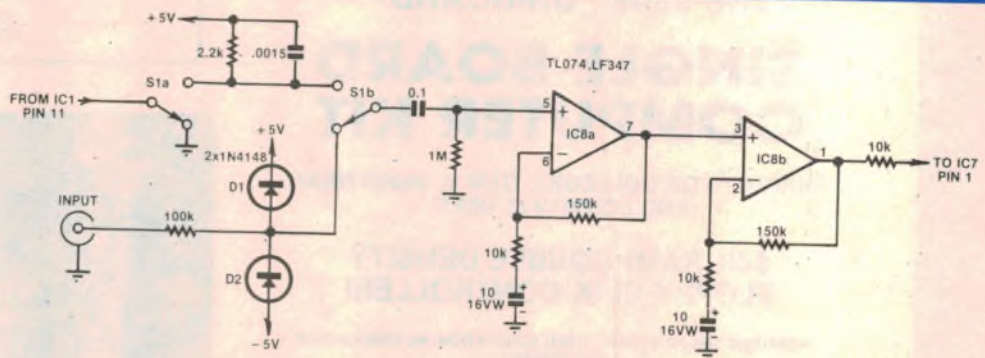
The other feature of this option is an

improvement to the coarse frequency control, making it more linear and much easier to use to select a given output frequency. In the original design, the frequency control is essentially a potentiometer wired as a variable resistor; the lower the resistance, the

higher the output frequency. Hence, the control has a very non-linear 1/x or hyperbolic law.

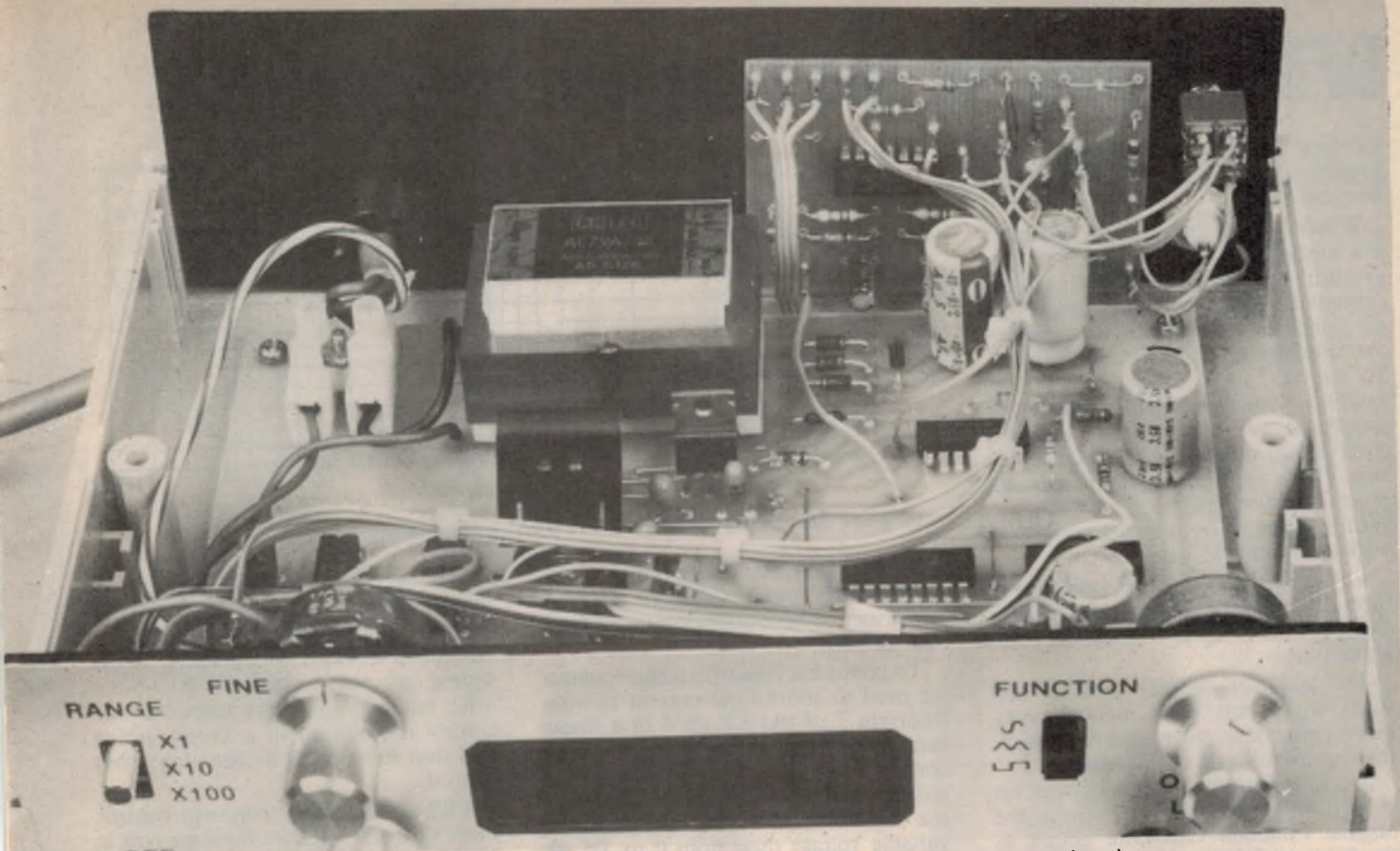
Again, we were aware of this drawback when we produced the original design but it does have the virtue of simplicity. The add-on circuit is a big improvement though and makes it very easy to set the frequency output.

Mechanically, the modifications entail the addition of a BNC socket and a toggle switch on the rear panel plus a small printed circuit board. Quite a lot of rewiring is involved too, which is the hardest part of the whole job. The cost is quite minor though, so it is quite a worthwhile addition to an already useful piece of test equipment.



EA FUNCTION GENERATOR ENHANCEMENT

7/AO/



Above: interior of the function generator with the new board on the rear panel. Below: close-up of the new board.

Circuit description

Relatively few components are needed for this modification. There is just one quad op amp IC package and a few other passive components.

Let's have a look at the frequency meter side of the circuit first. Incidentally, the quad op amp on the add-on PCB is referred to as IC8, which continues the numbering used in the Function Generator to avoid confusion.

At first sight, adding the external frequency meter facility to the Function Generator is quite straightforward. All that is necessary is to break into the signal measuring chain involving the hex Schmitt trigger IC7 and install an amplifier with sufficient gain to give an adequate sensitivity.

In practice, it is not so easy. What you need is an amplifier which can provide gain and sufficient output signal to exceed the positive and negative thresholds of the Schmitt trigger.

The problem is that typical CMOS Schmitt trigger ICs have positive and negative thresholds which are within a volt or so of the supply rails. For example, if the supply rails are $\pm 5V$, as in this case, the input signal to the Schmitt trigger will need to be in excess of 8V peak-to-peak for reliable operation.

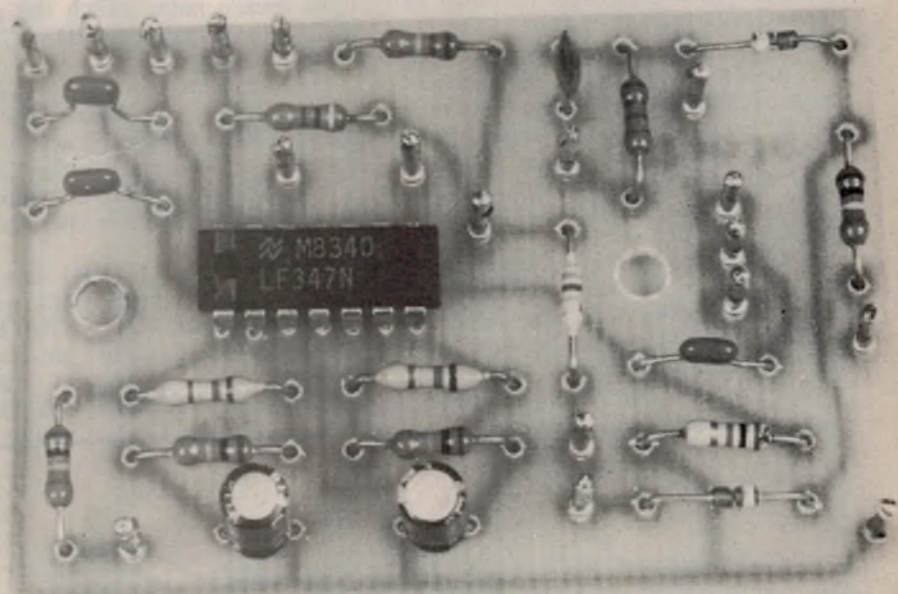
Typical op amps running from the same $\pm 5V$ rails cannot satisfy this requirement. They just don't have enough output voltage swing. To

overcome this problem, the quad op amp package is powered from the unregulated supply rails of the Function Generator, which are around ± 13 volts DC.

The unregulated supply rails do not present any problems to the op amps in this circuit since they have a very high supply voltage rejection ratio of 80dB or more. This is another way of saying that fluctuations of the supply voltage rails do

not affect the output of the op amps.

The input source to the amplifier is controlled by S1. When this switch is in the "generator" position, the squarewave output from pin 11 of the XR2206 IC passes via S1a and S1b to the input of the amplifier. The 2.2k Ω resistor is a pull-up resistor necessary for correct operation of the XR2206 output while the .0015 μF capacitor was a circuit modification



DFM adaptor for the Function Generator

(published in June, 1982) to prevent false triggering of the counter circuit at low frequencies.

When S1 is in the "counter" position, S1a shorts the output of the XR2206 to ground to prevent stray circuit capacitance from coupling spikes into the amplifier input while S1b connects the amplifier input to the BNC socket. To prevent gross overloading of the amplifier, voltage limiting diodes are placed between the input and the positive and negative 5V power supply rails. These limit the maximum voltage at the amplifier input to $\pm 5.6V$ and are in turn protected from excess current by a 100k Ω limiting resistor.

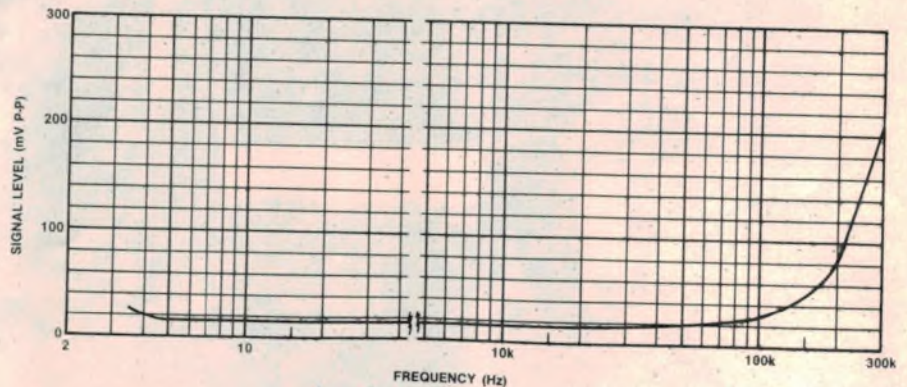
Following S1b, a 0.1 μF capacitor is used to couple the input signals while a 1M Ω resistor sets the amplifier input impedance.

The amplifier consists of IC8a and IC8b which are both used in non-inverting mode to give a gain of 16 each, thus an overall gain of 256 times.

The output of the amplifier passes via a 10k Ω limiting resistor and rejoins the original Function Generator circuit as the input to Schmitt trigger IC7a. This Schmitt trigger squares up the output of the amplifier and provides the drive to the following counter section.

Because the amplifier output voltage can swing higher than the Schmitt trigger supply voltage, voltage protection is required on the Schmitt trigger input. This is achieved by the internal protection diodes in the Schmitt trigger in conjunction with the 10k Ω limiting resistor just mentioned.

Now let's have a look at the second part of the circuit which involves the frequency control on the XR2206 oscillator chip. As previously mentioned, this originally used a pot wired as a variable resistor. The actual frequency



This graph plots the input sensitivity as a function of frequency.

produced is directly proportional to the current drain from pin 7 of the XR2206 which can be varied over the range from 1 μA to 3mA.

To produce a linear frequency control we need to control the current flowing from pin 7 of the XR-2206 in a linear fashion. Our method for doing this is to control the voltage drop across the resistance in series with pin 7. By fixing the resistance at 4.7k Ω and using a variable voltage drop from 0 to 3V we can alter the frequency by a factor of around 200 to 1. When coupled with the three decade range switch this gave a total frequency range of 12Hz to 220kHz on the prototype.

The remaining op amps, IC8c and IC8d, provide this function. IC8c is connected as a voltage follower to buffer the fixed -2V at pin 7 of the XR2206, IC1. The output of IC8c is connected to VR1 which has its other end connected to -5V.

Thus the wiper of VR1 can swing linearly over the range from -2V to -5V and drives IC8d which is also connected as a unity gain voltage follower. IC8d drives a network consisting of VR2 and two resistors

which are also connected to the -2V output of IC1.

So IC8d functions as a variable current sink which is controlled by the setting of potentiometer VR1. Since VR1 has a linear characteristic it will control the current in a linear fashion and thus function as a linear frequency control.

VR2 acts as a fine frequency control. Both VR1 and VR2 are the same pots as used in the original Function Generator design. In fact, in a simplified design, the coarse frequency control is so effective that VR2 could be dispensed with.

The 820k Ω resistor at the output of IC8d is used to set the minimum frequency of oscillation of the XR2206. The 820k Ω resistor is permanently connected between pin 7 of the XR2206

PARTS LIST

- 1 PCB, code 82a03c, 70 x 48mm
- 18 PC stakes
- 1 DPDT toggle switch
- 1 panel-mounting BNC socket
- 2 6mm PCB spacers
- 2 sets 12mm x 1/8-inch nuts and bolts
- 1/2 metre 10-way ribbon cable

Semiconductors

- 1 LF347 or TL047 quad op amp IC
- 2 1N4148 diodes

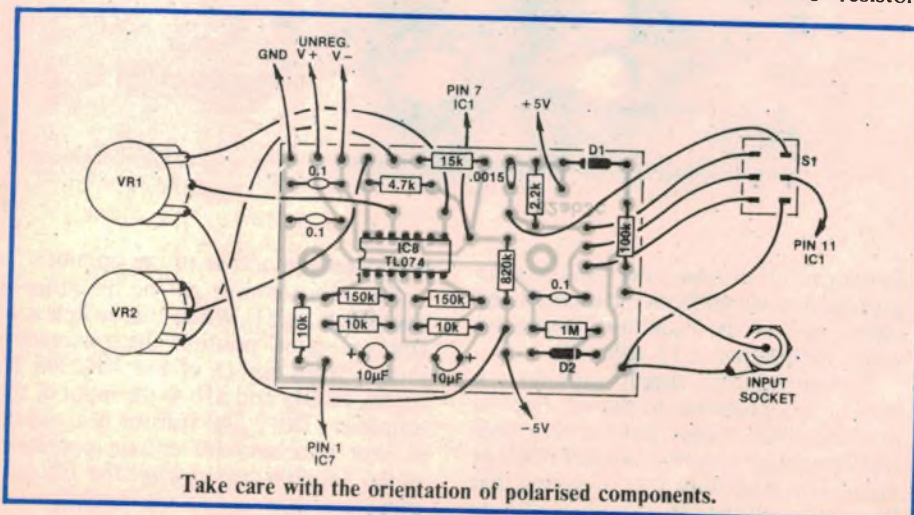
Capacitors

- 2 10 μF 16VW PC mount electrolytics
- 3 0.1 μF metallised polyester

Resistors (1/4W, 5%)

- 1 x 1M Ω , 1 x 820k Ω , 2 x 150k Ω , 1 x 100k Ω , 1 x 15k Ω , 3 x 10k Ω

NOTE: As discussed in the text, the two potentiometers, two resistors and one capacitor on the PCB are from the Function Generator and do not need to be purchased.



Take care with the orientation of polarised components.

and the negative supply rail. This means that there will always be a 3V drop across it and so it will always draw about $3.7\mu\text{A}$ from pin 7 regardless of the settings of the fine and coarse frequency controls. This minimum current corresponds to a frequency of around 12Hz.

Construction

The circuit is constructed on a small printed circuit board (PCB) coded 82ao3c and measuring 70 x 48mm. Use the overlay diagram as a guide to the component locations and double check the orientation of the polarised components — the two diodes, the op amp and the two electrolytics.

PC stakes are used to terminate all wires leading to and from the PCB. This allows connections to be made easily to the PCB when it is mounted in position. There are 18 PC stakes to be placed on the board in all.

Separate the two halves of the Function Generator case from the PCB and front and rear panels. Several components must be removed from the function generator PCB and installed on the new PCB. These components are: the $2.2\text{k}\Omega$ resistor adjacent (and connected to) pin 1 of IC7, the $.0015\mu\text{F}$ capacitor in parallel with the $2.2\text{k}\Omega$ resistor, and the $4.7\text{k}\Omega$ resistor in series with the fine and coarse frequency controls.

In addition, the connection between pin 11 of the XR2206 and pin 1 of IC7 must be broken. This is most easily done by removing the wire link by which the connection is made.

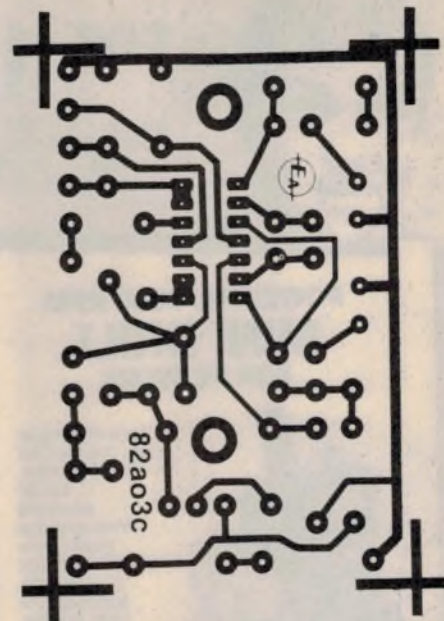
Once all components are mounted on the PCB, the rear panel should be removed from the Function Generator and the mounting hole positions for the PCB, BNC socket and toggle switch laid out. The positions shown in our

photograph give the best clearance between the existing PCB and the new components. Drill the mounting holes, fit standoffs to the PCB mounting screws, then attach the PCB, BNC socket and toggle switch to the rear panel.

The existing wiring leading to the frequency controls should be removed now and the wiring leading to the new PCB commenced. Follow our wiring diagram carefully and use colour coded ribbon cable so that identification of the individual wires is made easier. Most connections to the original PCB can be made from the component side via vacant component mounting holes. The exceptions are the connections to the unregulated power supply rails and ground which are made to the underside of the PCB.

When the wiring is completed, reassemble the Function Generator into its case and switch on. Set the rear panel toggle switch to the frequency generator position and check that the display changes frequency as the coarse frequency control is rotated. Rotating the fine frequency control will give only a slight change at the lowest frequencies but should have more effect at higher frequencies where it is most likely to be used. There should be a big difference apparent in the operation of the coarse frequency control now, with the frequency range not being bunched towards one end of the potentiometer.

With the Frequency Generator position tested, the toggle switch is set to the counter position and a test signal with an amplitude greater than 20mV and a frequency between 20Hz and 100kHz applied to the BNC input. The digital display should indicate the frequency of the applied signal. When acting as a frequency counter, the Function Generator will still deliver sine



Full size PCB artwork.

We estimate the cost of parts for this project to be approximately

\$12

This includes sales tax.

and triangular waves but the square wave output will be a squared up version of the frequency counter input. This signal may be used as an external trigger signal for oscilloscopes if required.

If you wish to still have the Function Generator square wave output available when in the counter mode it will be necessary to isolate pin 3 of IC7 from pins 2 and 5 by cutting tracks. The amplifier output should then be connected to pin 3 of IC7 rather than pin 1. The $2.2\text{k}\Omega$ resistor, $.0015\mu\text{F}$ capacitor and wire link should be left in position if this is done.

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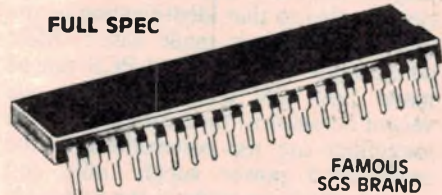
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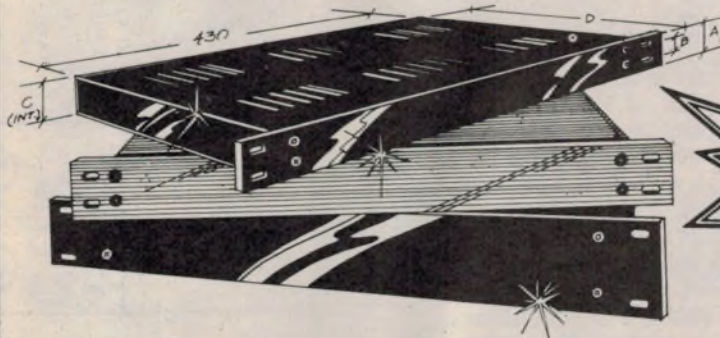
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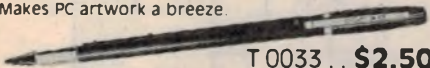


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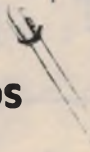


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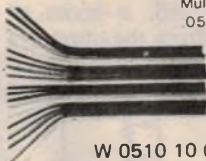
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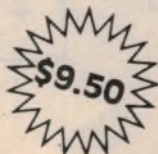
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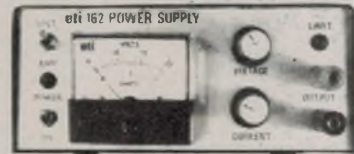


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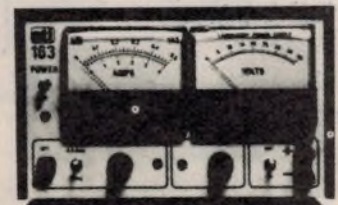
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FEATURING: VARIABLE CURRENT LIMIT-DUAL METERING

Circuit & Design Ideas

Interesting circuit ideas from readers and technical literature. While this material has been checked as far as possible for feasibility, the circuits have not been built and tested by us. As a consequence, we cannot accept responsibility, enter into correspondence or provide constructional details.

Audible indicators for panel lamps

The low current requirements and wide operating voltage range of continuous-tone piezoelectric alarms enable the production of transient sounds using passive RC networks.

The circuit of Fig. 1 produces a "ding" whenever the associated panel lamp turns on. The sound decays exponentially in volume as the capacitor charges to the full applied voltage.

When the lamp is turned off, the capacitor discharges via the diode and the lamp filament. If a low power diode is used, a small series resistor (10 to 1000Ω) may be used to limit the diode current if the lamp normally draws more than one amp. This circuit has been used as an automotive oil warning indicator and on custom built switchboards.

An interesting variation is shown in Fig. 2. Here the piezo alarm is used as a shop entry annunciator. It rings once each time the pressure mat is stepped on. A 9V transistor radio battery should

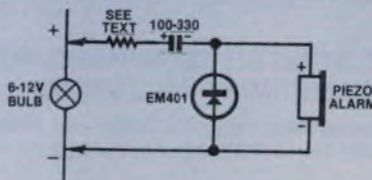


Fig. 1

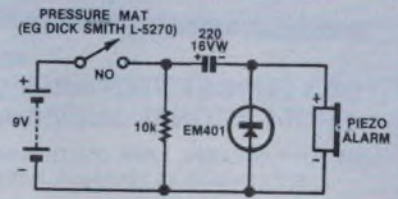


Fig. 2

power this circuit for at least six months.

Finally, the circuit of Fig. 3 uses a small bridge rectifier or four low cost diodes to produce a sound whenever the associated lamp goes on or off. Using a smaller capacitance gives a "dik-dik" sound which makes the circuit ideal as an audible blinker indicator for cars with "quiet" flasher units.

By using a non-polarised electrolytic or plastic dielectric capacitor, the circuit may be connected directly across the associated lamp without any need to check the polarity.

These circuits use so few components that construction can consist of gluing the diode(s) and capacitor(s) to the back

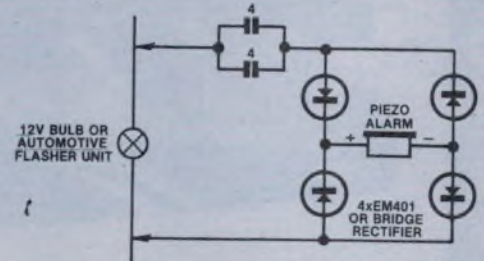


Fig. 3

of the piezo alarm. After wiring and testing the whole assembly can be potted in Araldite.

S. Payor,
Kogarah Bay, NSW.

\$25

Extended response sound switch

Most sound switches respond immediately a sound is detected. This can be a problem in some applications. For example, if the circuit is to respond to a doorbell it may be triggered when a door is slammed or any other short loud noise occurs.

This circuit can be set to respond only to sounds of a specific duration, or longer. Short sounds will cause no response.

Part of the circuit of Cudlipp (featured in EA, February 1982) is used here (IC1). This functions as a microphone

preamplifier and source of pulses which are delivered while ever a sound is present. IC2a is connected as a retriggerable monostable which provides a pulse of half to one-second duration when triggered by the output of IC1b.

IC3 is a comparator with a normally low output which goes high when the voltage at pin 2 exceeds $\frac{1}{2}V_{cc}$. IC2b is connected as a non-retriggerable monostable which operates the relay via a BC548 when it is triggered by IC3's output.

When the circuit is first switched on, R1 and C1 will reset the monostables. When sound is detected, a series of negative-going pulses from the output of

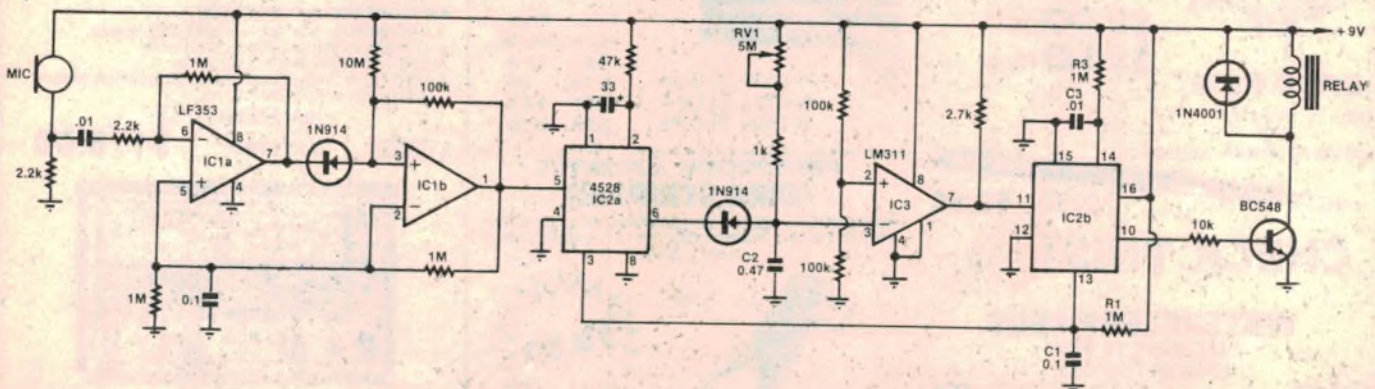
IC1b will trigger IC2a. Since IC2a is retriggerable, its output (pin 6) will remain high until the sound has ceased.

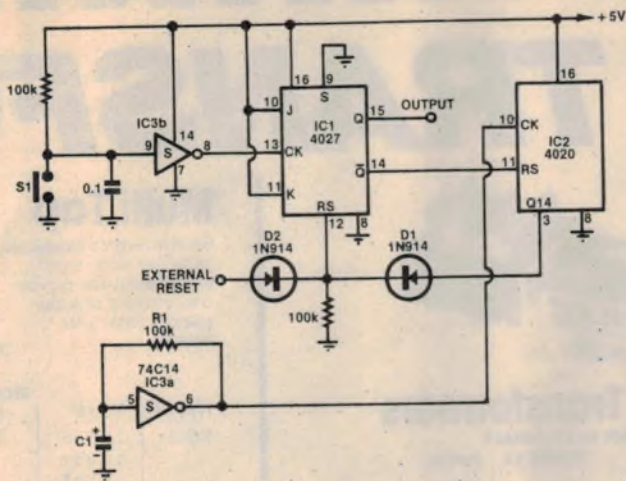
While the output of IC2a is high capacitor C2 will charge at a rate set by RV1. If the output of IC2a remains high for sufficient time, the voltage across C2 will exceed $\frac{1}{2}V_{cc}$ and so flip the comparator and thus trigger IC2b which will operate the relay for a time set by R3 and C3.

If C2 is not able to charge for long enough, it will merely discharge via the diode when the output of IC2a goes low and thus the relay cannot be turned on.

P. Vandermost,
East Brighton, Vic.

\$25





Single pushbutton long-period timer

With this circuit, only a single pushbutton switch is required to initiate or terminate a long-period timing cycle. IC1 is a 4027 JK flipflop and changes state on a rising clock edge. This occurs every time switch S1 is pressed, the output appearing at pin 15 (Q).

If Q is initially low, Q is high and binary counter IC2 is held reset with its Q14 output low. Closing S1 will cause Q to go high and Q to go low, thus releasing the reset on IC2 which is now clocked by Schmitt trigger oscillator IC3a. IC2 is subsequently reset (ie, Q low and Q high) either by a further switch operation or when Q14 of IC2 goes high.

In addition, the circuit may be reset during the timing cycle by applying an external reset signal to D2.

The maximum timing period (P) is nominally $P = 1.4(R1)(C1) \times 2^{n-1}$ seconds where Q_n is the 4020 output (for the circuit shown, $n = 14$). Possible applications include use as a verandah light or exhaust fan controller.

G. Cutter
Bentleigh, Vic.

\$20

Automatic volume control

Here is a simple circuit that will automatically adjust the volume of a car radio or cassette deck according to the ambient road of engine noise.

A microphone is placed under the bonnet of the car, either adjacent to the engine or one of the wheels, which ever causes the greatest noise problem. Its output is rectified by D1, filtered to provide a steady DC voltage, and fed to op amp IC1. The gain of IC1 is variable between one and 30 by means of a 100kΩ trimpot, while the non-inverting input is biased to half supply by two 100kΩ resistors.

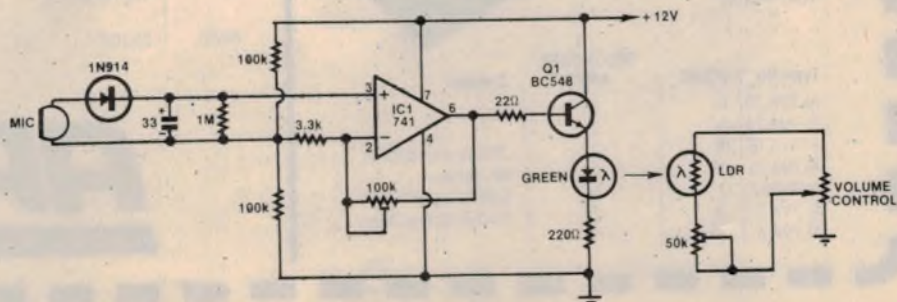
The output of IC1 drives transistor Q1 which varies the current through a green LED. The output of the LED is then coupled to an LDR which, in turn, varies the resistance between the active and wiper terminals of the volume control. Thus, when the engine noise rises, the

LED brightness increases, the value of the LDR decreases, and the volume increases.

In practice, the 100kΩ trimpot should be adjusted so that the LED just lights with the engine at idle. The LED and the LDR should then be mounted inside a light-proof tube. The 50kΩ trimpot in series with the LDR functions as a sensitivity control.

B. Paterson,
Glen Iris, Vic.

\$15



Modified supply for storage CRO Adapter

Some imported 2155-type transformers exhibit poor regulation characteristics and this can sometimes lead to problems in areas of low mains voltage. In the case of the Digital/Analog Storage CRO Adapter (EA, November 1980 and March 1981), it can lead to a very high ripple content on the $\pm 8.2V$ supply rails.

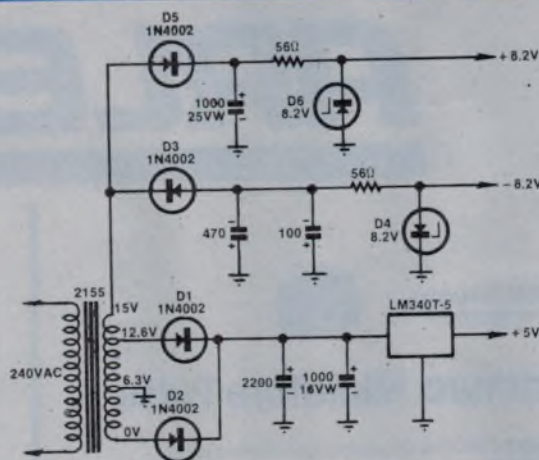
This problem can be overcome by altering the transformer tapings and adding a few extra components as shown. The 5V regulator now derives its supply from the 0, 6.3 and 12.6V tapings

instead of the 0, 7.5 and 15V tapings previously used. An extra 1000μF capacitor has also been added at the input, in parallel with the existing 2200μF capacitor, and this ensures that the regular input remains above its dropout voltage while reducing its dissipation.

The $\pm 8.2V$ supplies are derived from the 15V tapings. Diodes D3 and D5 provide half-wave rectification of the AC supply, while zener diodes D4 and D6 regulate the supply rails to $-8.2V$ and $+8.2V$ respectively. Note that an extra 100μF capacitor has been added across the 470μF capacitor used in the negative supply.

I. Stevenson,
Bracken Ridge, Qld.

\$15



Wanted: your brain-waves

Come on now. You must have had some bright circuit and design ideas which are worth publishing. Why not send them in and make a little extra brass for more electronic components? We pay between \$5 and \$40 per item published, depending on the merit and the amount of work we have to do to publish it. Why not jot your idea down now and send it in?

ARLEC TRANSFORMERS

O.E.M. Enquiries welcomed



Tamura Miniature Pulse

Designed principally for computers and measuring instruments

Type No.	Primary Inductance (uH)	Details
G 52 J12C	800	Centre tap
G 53 E21C	2500	Centre tap
G 50 J111	8	3 windings
G 51 H111	50	
G 52 E111	250	
G 52 H111	500	
G 52 J111	800	
G 73 H111	5000	
G 74 B111	12500	
G 52 E211	250	

O.E.M. Enquiries welcomed



Tamura Green Chip Series

Miniature transformers designed for transistor circuitry

Type No	PRI	SEC	Details
MG 24	500	50	AUDIO
MG 22	500CT	600	
MG 25	600CT	12	
MG 21	600CT	600CT	
MG 23	1K	50	
MG 17	10K CT	1.5K CT	
MG 16	10K CT	2K CT	
MG 15	10K CT	10K CT	
MG 14	20K CT	1K CT	

Type No	Inductance	OH	Inductor
MG 106			

Low Profile

AL 7 VA Series Insulated to AS 3126 P.C.B. mounting pins compatible with other current models and provision for additional anchorage to PCB's 240V 50HZ PRIMARY



Type No	VOLTS	SECONDARY AMPS	Details
AL 7VA 30	30	23	
AL 7VA 24	24	29	
AL 7VA 18	18	39	
AL 7VA 15	15	47	2 equal secondaries for - Series -
AL 7VA 12	12	58	Centre Tap or
AL 7VA 9	9	78	Parallel Connection
AL 7VA 6	6	117	



P.C.B. Transformers

250V 50 HZ PRIMARY

Type No.	VOLTS	POWER VA	Details
75000 Series	2 12V	1.2, 5, 7 10, 12	2 Secondaries May be used separately or connected in Series or Parallel



Low and Extra Low Voltage

240V, 50 HZ PRIMARY

Type No.	VOLTS	SECONDARY AMPS	Details
2150	12 6CT	1 25	
2155 A	8 5 9 5 12 6CT 15CT	1	
5502	44CT	1 25	
5504	15	2	
5508	12 6CT	2	
5579	6 3	1	
5755	40CT	1 25	
6474	12 6CT	0 15	
6625	25	0 5	
6672 A	17 5 20 24CT 27 5CT 30CT	1	
6978 A	9 10 5 12 6CT 15CT	2	
7309	12	2 5	
7310	24	1 25	
60817	24	1 25	
5503	11 5 17	4	
7243	19 33 40 50CT	2	
7311	24	4 2	
9583	10 9 18 5 2	4 7 0 87 2	
60202	17 5 20 24CT 27 5 30CT	3	
60203	30CT 40CT 50CT 60CT	2	Two secondaries can be series or parallel connected
60291	25 2CT	3 5	

Multi Tap

General purpose transformers for special projects and experimental work provide a wide choice of output voltages 240V 50HZ PRIMARY

Type No.	VOLTS	SECONDARY AMPS
60202	2 5 3 3 5 4 5 5 5 6 6 5 7 5 8 9 10 12 12 5 15 17 5 18 20 24 27 5 30	3
60203	5 10 15 20 25 30 45 50 55 60	2 A Ser 4 A pa
2155 A	1 1 2 2 2 2 4 3 1 3 2 4 1 5 1 5 5 6 3 6 5 7 5 8 5 8 7 9 5 12 6 15	1
6978 A	1 2 1 5 2 1 2 4 2 7 3 3 6 4 2 4 5 5 1 6 6 3 7 5 8 7 9 10 5 12 6 15	2
5672	2 5 3 3 5 4 5 5 5 6 6 5 7 5 8 9 10 12 12 5 15 17 5 18 20 24 27 5 30	1

Thyristor (SCR) Trigger Transformer

For power supplies, lamp dimmers, motor speed controls

Type No.	VOLTS	SECONDARY AMPS
XT1185	415 (Max voltage between windings)	70

HEAD OFFICE VICTORIA
30-32 Lexton Road, Box Hill Vic.
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47 Drummond St. Helmore, N.S.W.
WAGGA
K.J. Warden (Agencies) Pty Ltd.
7 Norton Street, Wagga, N.S.W. 24
A.C.T.
K.J. Warden (Agencies) Pty Ltd.
24 Geelong St. Fishwick, A.C.T.
SOUTH AUSTRALIA
10 Beulah Rd. Norwood, S.A. 50

ARLEC

FORMER GUIDE



Secondary PS
Details
Centre tapped
5V 24V 30V

Centre tapped
10 20 30 40
50 and 60V

Centre tapped
2 12 6 and 15V

Centre tapped
3 12 6 and 15V

Centre tapped
5 24 and 30V



Secondary SCR PS

028 Ph (03) 840222 telex 32286

2192 Ph (02) 7896733 telex 22874

350 Ph (069) 21273 telex 69960

609 Ph (062) 805519 telex 62475

67 Ph (08) 428918 telex 89234



Enclosed Stepdown Transformers

240V, 50 HZ PRIMARY

Ideal for garden lamps, pond lights and water pumps, automatic trouble lamps, safety lights, pool lighting etc

Type No.	VOLTS	SECONDARY AMPS	Details
60269	32	2.25	Type No. 60280, 60426, and 60480 have two fuses in the secondary output for pool lighting applications
60279	32	7.8	
60280	32	5.9	
60425	24	3	
60426	24	7.9	
60453	12	6	
60480	12	15	

Portable Stepdown Transformers



Type No.	VOLTS	SECONDARY AMPS	Details
PT 5578	115	0.35	For shavers radios, tape recorders, heating blankets, TV receivers, appliances and instruments. 2 Pin socket
PT 2164	115	0.87	
PT 2166	115	2.17	
PT 2168	115	4.35	
PT 2170	115	8.7	
PT 9585	240	1	
PT 9789	240	2	

Constant Voltage

isolated, constant RMS Voltage output

Type No.	INPUT	OUTPUT
CV 9024	190-260 RMS	240V 1A
CV 9027	190-260 RMS	240V 4.17A

QUEENSLAND

City Victoria Road, & Elm St, Newstead Qld, 4006 Ph (07) 322 2221

WESTERN AUSTRALIA

611 Hay St, Inglewood WA, 6144 Ph (08) 940 0800

TASMANIA

Launceston 5201 The Arcade, 75 York St, Launceston Tasmania 5201 Ph (03) 322 2221

Hobart 6901 Electronics, 162 Argyle St, Hobart Tasmania 6901 Ph (03) 322 2221

Audio



Type No.	PRIMARY IMPEDANCE	POWER	Details
45012	70 100V Line 4 8 16 ohm	4 WATTS	Line to speaker impedance
45035	600 ohm	0dbm	PCB Mounting, Telecom approved
45065	600 ohm	20 dbm	Line isolation to Telecom 1053 1054
1T 347	600 ohm 600 ohm		

Control Circuit

For switchboards PRIMARY 240V 50 HZ. Insulation to AS 3126



Type No.	IMPEDANCE	POWER	Details
PT 9169	32 24	1.88	SEC approved
PT 9170	32 24	3.12	
PT 9171	32 24	6.25	

Soldering Iron

For low voltage soldering irons or similar applications. PRIMARY 240V 50 HZ



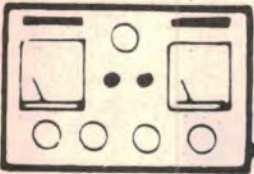
Type No.	VOLTS	SECONDARY AMPS	Details
60158	3.3	30 amp	SEC approved

Bell and Chime Transformer

PRIMARY 240V, 50 HZ



Type No.	VOLTS	SECONDARY AMPS	Details
60999	Choice of 5 8 12 and 16 Volts		Specially designed to power door bells and chimes. Double insulated and short circuit protected



The Serviceman

Reader contributions month

It's catch-up time again this month. I have had so many reader contributions that are worth passing on that I will have to devote this month's notes to presenting them. They cover a range of subjects and will probably provide a refreshing change from the purely professional approach.

The first story comes from a regular contributor, J.E. of Bullcreek, Western Australia. It concerns a problem with a homemade "EA" amplifier. Here's how he tells it.

A problem which could trouble experimenters of a few years ago, who built equipment to their own designs, was that of RF instability which evidenced itself in the form of a popping sound — often referred to as motorboating — and other unpleasant noises.

Today's hobbyists can build a wide range of electronic projects from magazines such as "Electronics Australia", using printed circuit boards, with an almost certain guarantee that they will work first time, because the bugs have already been eliminated by experts. I was therefore surprised when presented with an "EA" Playmaster Twin Stereo Amplifier (May — June 1979) with signs of RF instability.

It had been built in a metal cabinet smaller than that specified, with the result that the mains transformer had

been mounted externally. The six power transistors were mounted on a "Z" shaped aluminium heatsink bolted to the rear of the metal chassis.

One advantage of this arrangement was that the bottom of the cabinet could be easily removed for access to the wiring side of the board. Apart from this the layout was identical with the original, although more compact. All components were new and the soldering was first class.

The audible symptoms, which seemed to be stronger on the right channel, were popping noises and some background hum, both of which can be caused by a faulty main power supply filter. I bridged the 2500 μ F filter capacitor with another, but the fault remained.

Next I disconnected the main amplifier from the preamplifier by unsoldering the shielded leads to the base capacitors of Q6 and Q106 respectively. This did not make any difference, so the fault had to be associated with one or both of the main amplifiers (Q6 to Q9 and Q106 to Q109).

I then disconnected all DC power supply to the right main amplifier by removing the two links feeding the emitter of Q7 and the collector of Q8, and also lifted one end of the 100k Ω decoupling resistor feeding Q6 and the 1k Ω resistor feeding the base of Q7. The left amplifier then worked perfectly.

To confirm that the fault was, as I now suspected, in the right main amplifier, I restored the DC supply to it and disconnected the DC from the left amplifier. The fault immediately re-appeared.

Instability

Tackling the right amplifier, I bypassed each capacitor with another of the same value in case one of them was open circuit. This had no effect, so I decided to see what clues I could find using my DVM and a simple demodulator probe which can provide comparative RF voltage measurements.

This indicated RF at a number of points. The readings tended to be erratic, but were highest on the leads of the driver transistor, Q7, a BD140. The frequency must have been very high because even the aluminium heatsink, which was firmly bolted to the metal chassis in several places, gave indications varying from 0.5V at one end to 2V at the other.

My first reaction was that Q7 was a



"rogue" transistor with an unusually high h_{fe} and F_T , so I replaced it with another of a different make, but without any improvement.

One of the standard cures for this problem is to fit a "stopper" resistor, such as is used in the base lead of Q3. I cut the copper foil to the base of Q7 at a point next to the transistor and bridged it with a 220Ω resistor which I thought should be more than enough for a power transistor. This had no effect and was removed and the foil repaired.

At this stage I was rapidly running out of ideas, but was still prepared to back the indications of the DVM that Q7 was the source of the RF oscillation. Most puzzling was the fact that the left amplifier, with almost identical layout, showed no signs of instability.

Almost as a last resort I decided to try to reduce the gain of Q7 by inserting a 4.7Ω in its emitter circuit in place of the link between it and the 40V DC supply. Then — oh joy — it worked perfectly. Smaller values were tried until, with 1Ω the fault returned.

To provide a margin of safety I decided to revert to the 4.7Ω resistor and, after cutting its leads to make the connections as short as possible, used it to replace the link between the emitter and the DC supply. Alas, the fault returned.

What now?

The only change, apart from the fact that the resistor was now on the other side of the board, was that the leads had been cut off almost next to the body of the resistor. Then I remembered that the RF readings on the heatsink suggested that the frequency must have been very high. If this was so then a straight piece of wire would have significant reactance. Perhaps the reactance of the leads was more significant than the resistance of the resistor.

To test this theory I took about 7cm of single strand wire, wound it into a coil on a 6mm former, and used it as the link between the emitter of Q7 and the supply rail. The amplifier then worked perfectly on both channels and all signs of RF instability, including those indicated by the DVM, disappeared.

I can only assume that the frequency of the RF instability was unusually high and that this small coil in the emitter circuit provided sufficient negative feedback at this frequency to prevent instability. A larger resistor may also have been effective.

I would like to have tried interchanging the two BD140s to see if it would shift the fault to the other channel, but there is a limit to the time one can afford to spend investigating unusual faults like this one, intriguing though they may be.

Thank you J.E. for a most interesting story. Like yourself, I would be most interested to know exactly why this fault occurred but, on the other hand, I have to agree that there is a very definite limit to the time one can spend investigating such things.

I did discuss it with a certain member of the "EA" staff, who is known as the "fountain head" (from which all knowledge flows!) but, at this distance, he could offer no suggestions which would solve the mystery. The best we can hope for is that someone who reads this, and may have encountered a similar situation, may be able to add something to the story.

A rash diagnosis

My next story comes from Mr K.H. of Bundaberg, Queensland.

I am a retired radio and TV serviceman from Victoria, now residing near Bundaberg, Queensland. I began working with Radio Corporation in Melbourne in 1945. I was trained and worked in the industry until just prior to colour TV. In all this time, I have been a regular reader of your articles and the magazine, and feel now that, as I have the time, I will try to give back a little for all the information, laughs, and pleasure I have received over those years.

I am enclosing a story that I think would be interesting to your many readers. I have also included a photograph of the offending part and a copy of the relevant section of the circuit diagram (not published). The story tells how the thought of a picture tube failure can shut off one's mind from observing other fault indications. Making such rash decisions was the very thing I used to tell my customers to be careful of.

When I was young, I read a report in "Radio, TV & Hobbies" that Sony had taken out patent rights for a single gun, three cathode colour picture tube, with vertical stripe phosphor colour bands. The reduction in EHT to excite the Trinitron colour tube intrigued me. So, when I purchased my first colour set, it was a Sony. It served us well until someone tripped over it in the dark one night and it landed flat on its face. That seemed to cause the picture to slowly get worse from then on, but I kept it going by increasing the preset colour controls when required.

In the meantime I retired and we moved to Queensland. So, it was here in Bundaberg that a second opinion was obtained on the cause of the poor picture. As I expected, it confirmed my suspicion of low emission.

During the following months, the set slowly blacked out completely and the cost of replacing the tube was considered. We discovered that a rebuilt tube was not available and a new tube

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The Serviceman

cost more than the value we had for the old set. So a decision was made; a new colour set. The old set became valueless except for the bits and was placed out of sight while I dried the tears from my cheeks.

We have two daughters still living with us and, here in Bundaberg, we have two TV channels. Yes, they want to watch one program and my wife and I the other. At the time, a black and white TV set was performing well for the girls, then Murphy arrived and the black and white set's power transformer primary shorted and I discovered that it was not worth repairing.

I brought out the Sony colour set and found, to my surprise, that it worked. It was not a wonderful picture but it did work and it made the kids happy again. Then a month or two went by and it gradually passed out again, causing the usual program hassles over one TV set.

One day recently, one of the children remarked that she had had the old set on, listening to the sound, and when it was turned off, the three basic colours appeared briefly. I took note and filed the information for future treatment. Could there be another fault? I considered it worth a further look and on checking I found that as the voltages collapsed, decreasing bands of red, green and blue appeared on the screen.

Off came the back and a "what have I got to lose" knock was scientifically applied to the picture tube neck. Guy Fawkes appeared in the gun and the power supply shut down. "That's it", I thought. "I won't have to worry about that TV set again", and turned it off. But I have had experience with these power supplies before, so I waited a minute and tried it again. There it was — a picture in full colour.

Meal time was on me, so I left the set running and when I returned, there was sound but no picture. Could I perform the miracle again? I had no luck this time. I always kept in the back of my mind the possibility of grounding the tube filaments and arcing the EHT over the base pins, as I used to do on the old black and white tubes, but I saved this for a last ditch attempt.

On the other hand, I was now mad enough to hit everything or anything. By tapping with almost destructive blows to the underside of the video amplifier colour board, I produced a part picture for a flash. I was on the track of something. A little more judicious bashing and I was at transistor Q454 (2SC633A).

It was time to take a look at the circuit diagram that I had procured from the

manufacturer years earlier. Yes, if Q454 was leaky or shorted it could, without doubt, alter the critical gun supply voltages and cut off the tube. The transistor was removed and replaced. Good Lord, that was the fault. The picture appeared in all its glory, better than it had been for years.

I studied the now removed transistor with my jeweller's eye glass, to check the transistor number. I noticed on the underside what looked like small dots of moisture, probably due to our humid climate. And on more careful study, I could see a gold tinge on the plastic case between the supposedly once gold plated leads. What I was looking at was very typical of a fault, well known to me, that used to be found on the base of a certain brand of 9-pin valves, it was caused by silver being deposited on the glass between the pins. Many old technicians will remember the havoc that this short between the pins caused. Well here I was, seeing the same fault in a new guise with solid state devices.



The faulty transistor (Q454). Note the metal deposition on the body of the transistor adjacent to the three leads.

I am enclosing some colour photographs which I took through my jeweller's eye glass. I hope they may reproduce well enough in black and white to allow the gold plating to be seen. I also hope that my discovery of this fault may help unravel other unsolved faults, particularly in humid climates. (P.S. The picture tube really is low in emission, but is still working fine.)

Thank you K.H for a most interesting story. As you commented yourself, it is all too easy to be sidetracked by the proven existence of one fault, and blame all the symptoms on that. I think there is a lesson there for us all.

As for the fault itself, I must confess that this suggestion is completely new to me, although I well remember the problem with the 9-pin valves. In fact,

I'm sure that I ran such a story in these notes many years ago, though it would probably be too hard to find now. As K.H suggests, it was a very serious problem at the time.

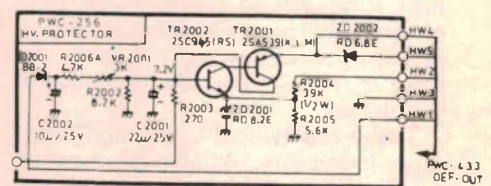
If this really is a new version of the old fault it may well explain some of the mysterious partial failures or loss of performance which most of us have encountered from time to time, in both transistors and ICs, and which seemed to run contrary to the generally accepted idea that solid state devices either work properly or not at all. Perhaps someone else has had a similar experience.

Rank protection circuit

My next contribution concerns a story I told back in September 1983 (goodness, how the time flies!). This concerned a Rank 2603 and, particularly, a high voltage protector circuit which this model employs. In those notes I happened to mention that I had little information about this circuit and would like to catch up on it.

The response to this casual remark was quite surprising and most gratifying. One gentleman, from Queensland was even kind enough to forward a complete 2603 service manual to the "EA" editorial office, who passed it on to me. My sincere thanks to him.

Another contribution came from Mr I.W., a professional serviceman from Bateau Bay, NSW, who gave his explanation of how the circuit functions. Having translated the slightly fractured English in the Rank manual and studied I.W.'s explanation — which was particularly well presented — here is a composite of the two. The circuit is from the Rank manual.



The circuit is designed to sense any excessive voltage at HW1, which is a pulse derived from pin 2 on the line output transformer, T552. In normal operation the emitter/base junction of TR2002 is reversed biased by about 1V by the zener diode ZD2001 and associated resistor network.

Under normal conditions the EHT is about 27kV. If for any reason it should rise to 33kV, or higher, the pulse at HW1 will rise to the point where the rectifier/ filter network, D2001/C2002, will produce a high enough voltage on the base of TR2002 to turn it on. This turns on TR2001.

Because of the positive feedback from the collector of TR2001 to the base of TR2002, both transistors bottom very

rapidly. This introduces a virtual short circuit between HW4, connected to the 120V rail via R551, 3.3k Ω , and the cathode of zener diode ZD2001. Under these conditions HW4 drops to about 9V and, because of the 6.8V generated by ZD2002, HW5 drops to between two and three volts.

HW5 is connected to the horizontal oscillator (TR501) supply rail, normally at 13.5V. When it drops the horizontal oscillator ceases to function, output from the horizontal output transistor (TR503) falls and, with it, all voltages derived from this stage. The receiver is thus rendered inoperative.

Because of the feedback between TR2001 and TR2002, the system will remain locked in this condition until the receiver is switched off, and for about 10 seconds thereafter, until the positive voltage on the base of TR2002 falls due to leakage. Assuming that the fault is cleared before switching on again, the set will function normally.

According to I.W., a likely cause of excessive EHT is the failure (open circuit) of C553, from the collector of TR503 to deck. In these circumstances the EHT can rise high enough to punch through the neck of picture tube between the anode and the yoke. This is a similar condition to that occurring in other brands of receivers, and which has been described in these notes previously (Philips K9, July 1983).

A better heat source

And, finally, from G.H., a serviceman in Hyghett, Victoria, comes this brief comment: I read your column in this latest (December 1983) issue of "EA". I was quite surprised at the method used to heat sections of the K9 chassis to locate the fault. We have always used a cheap pistol grip hair dryer which I carry in my tool kit. This is a very easy way to cope with such a job. Then use a can of freeze and the job can be completed in a very short time. It may even avoid carting the set to the workshop.

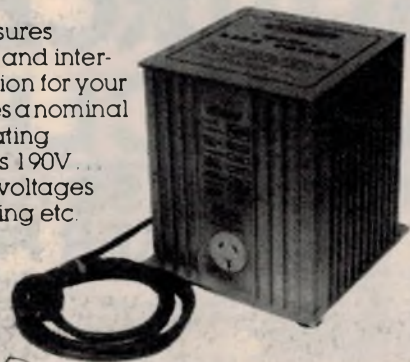
Keep up the column; I do appreciate being able to get a line on some very odd faults.

Thank you for the comments G.H., and I am glad to learn that you enjoy the notes, and may even find them useful on occasions. As for the method of heating the K9 — well, that's fair comment too. I am not averse to using a hair dryer on occasions — in fact I have been known to pinch Mrs Serviceman's unit when my own was out of commission or not readily available.

In this particular case, a hair dryer may well have been a better approach but the blanket just happened to be handy. Later, a radiator proved better than the hair dryer because it left both hands free to take measurements. ☺

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Number 3

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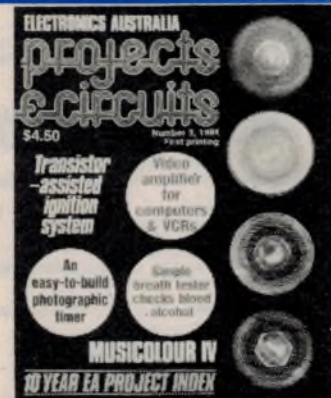
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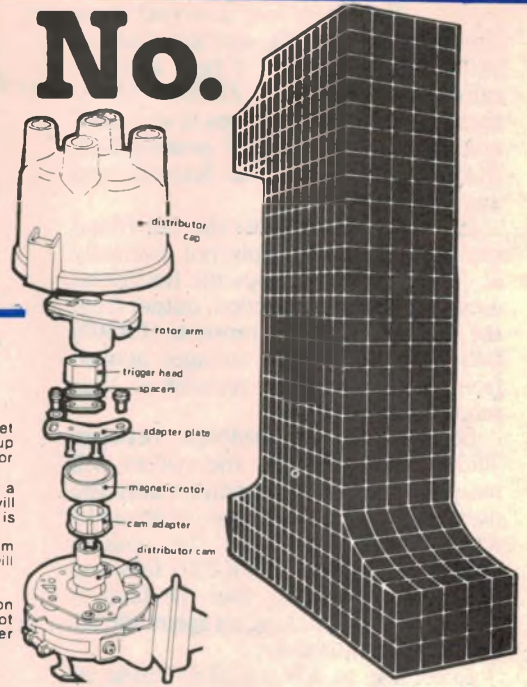
This set is designed to fit most European and Japanese cars. In fact it will also fit many Australian cars fitted with Lucas, Bosch, Motorcraft, AC Delco or Autolite electrics. If you wish to check first, please send SAE for car/distributor list.

SEE EA DECEMBER 1983

Because we have no way of knowing, you get the fitting set for ALL of the distributors available. Basically you end up with a jar full of parts you don't need to use! (Perhaps for your next car?) Quite frankly, we are amazed that we can supply such a comprehensive kit for this price. To produce a kit that will adapt to the dozens of different distributors around is amazing! Remember, once you have installed a breakerless system it will never wear out and that part of your system will remain in tune FOREVER. Cat. KJ-6655

PLEASE NOTE: This system must be used in conjunction with an electronic ignition. The Hall-Effect device will not switch enough current to replace the contact breaker points on their own!

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'TRANSISTOR ASSISTED IGNITION HALL-EFFECT "BREAKERLESS" VERSION

REF: EA DECEMBER 1983

This kit is virtually identical to the KA-1506 except that it contains the interface electronics for the KJ-6655 Hall-Effect triggerhead. Cat. KA-1505

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TRANSISTOR ASSISTED IGNITION

REF: EA JANUARY 1983

Latest version of this fantastically popular kit! The Jaycar kit comes COMPLETE down to the plastic TO-3 transistor covers, genuine heatsink and DIECAST BOX - as used in the original EA unit. Beware of flimsy kits that use sheetmetal boxes.

\$35

This kit is designed to be used with contact breaker points. If you want Hall-Effect breakerless ignition, we suggest the KA-1505 version of this kit shown elsewhere on the page. Cat. KA-1506

NEW! - DELUXE CAR BURGLAR ALARM

(Ref: EA May 1983) Great new design from EA. This one is very sophisticated. (Auxiliary battery extra) Complete kit of parts. Cat. KA-1550

\$69.50

NEW - MOTORCYCLE INTERCOM

(Ref: EA March 1984) Now you can talk freely and safely to your pillion passenger with this handy kit! Cat. KA-1533

\$39.95

NEW - IGNITION KILLER

(Ref: EA March 1984) Handy little project fits under your car to foil thieves. At this price can you afford not to have one? Cat. KA-1535

\$14.95

THE RED FLASHER - (not illustrated) A de-luxe Swiss switch with electronics to make it flash plus deterrent stickers to make your car look as if it has an expensive alarm. Cat. KJ-7000

\$20.95

NEW! "SPARKRITE" LOW COST CAR ALARM KIT

This low cost alarm is ideal for the budget conscious motorist. It has many features:

- ★ 10 amp output relay
- ★ Optional door, bonnet switch input
- ★ Accessory loop
- ★ Horn relay and headlamp output
- ★ Optional entry delay i.e. external disarm switch can be fitted obviating need for entry delay
- ★ Exit delay
- ★ Auto alarm disable. (To meet local noise/environmental rules)



ETI340 CAR ALARM

Ref: ETI April 1984

A versatile security system that provides full protection for almost any vehicle. This unit will protect your valuable vehicle from virtually any sort of interference - from hub-cap stealing to being towed away! It does not rely on voltage or current sensing to trip the alarm, but 'resonance microphones' - it can also protect 'perimeter accessories' like driving lights and racks. The project meets the major requirements of car alarms set down by the NRMA. We believe that this alarm is one of the most comprehensive that we have seen. Once again Jaycar has taken the no compromise approach.

The Jaycar kit includes two of the specified resonance microphones, original die-cast box etc (we supply 'chocolate block' multiway connectors as well). The complete kit is only \$69.50 inc. sensors. Extra sensors are available for \$10 each. Cat. AM-4000.

\$69.50

Sparkrite SX2000

A Reactive Discharge System combines all features of the SX500 plus:

- Reactive Discharge electronics combining all the advantages of both Inductive and Capacitive Discharge for maximum spark performance.
- Gives the most thorough combustion of air/fuel ratios especially current lean mixture emission controlled engines.
- Voted 'Accessory of the Year' and the best as tested by Popular Motoring Magazine.
- Patented clip to coil fitting.
- Systems Function Light as well as Static Timing Light.
- The ultimate brand leading contact-breaker triggered system.

\$59

Cat. KJ-6650



Sparkrite TX2002

A Reactive Discharge System - with unique auxiliary circuit. Combines all features of the TX1002 plus:

- Reactive Discharge electronics combining all the advantages of Inductive and Capacitive Discharge for maximum spark performance.
- Gives the most thorough combustion of air/fuel ratios especially current lean mixture emission controlled engines.
- Unique 3-way change over switch incorporating an auxiliary back up circuit - ELECTRONIC/OFF/AUXILIARY.
- Robust die-cast case - fully resistant to moisture and heat.
- The ultimate system - REACTIVE DISCHARGE - CONTACTLESS OR CONTACT TRIGGERED - AUXILIARY BACK UP CIRCUIT - CLIP TO COIL FITTING - FOUR CONNECTIONS ONLY - ALL PARTS IN ONE BOX TO FIT OVER 500 APPLICATIONS.

TX APPLICATIONS

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HOW IT WORKS

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- Guards doors, boot, bonnet PLUS radio/tape and auxiliary fog/spot lamps. Also inhibits ignition.
- Flashes headlamps and intermittently sounds horn for both visual and audible alarm.
- Unique programmable personal code entry system to arm and disarm.

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Cat. KJ-6660



Sparkrite TX1002

An Inductive Discharge System

- Can be operated utilising Hall-Effect triggerhead, or existing contact breakers.
- Extended dwell inductive discharge for maximum spark efficiency.
- Three position switch.
- Static timing light.
- Systems Function Light.
- Patented clip to coil fitting.
- Robust die-cast case.
- Fully waterproof.
- Protected from the hostile environment of the engine compartment.

\$79



TX-1002: Slightly lower powered version of the TX-2002. Ideal for most 4 cylinder cars. All fitting pieces included! Cat. KJ-6651

Cat. KJ-6651

VCR SOUND PROCESSOR KIT

(Ref: EA April 1984)

Great new kit for Video Enthusiasts! • Stereo Simulator • 5 Band Graphic Equalisation • Noise Filtering
The Jaycar kit once again is truly original - down to the genuine multicoloured knobs on the front panel (watch for substitutes). The only extra that you will need to buy is the optional whistle filter (Cat. EE-3814 \$19.95)
Cat. KA-1545

\$55

NEW!!



MUSICOLOR IV

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Complete kit

Cat. KA-1010

\$89.90

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NOT NEW!! - EA DIGITAL CAPACITANCE METER

(Ref: EA September 1980) Ideal for a bench type mains powered application. Measures from 1pF to 99.99uF in only 3 ranges! Large easy to read LED display.
Cat. KA-1105

\$59.90



DUAL TRACKING #22V POWER SUPPLY

Dual polarity can provide up to #22V at up to 2 amps. Also has fixed output of +5V at 0.9A. Complete kit

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\$89.50

(Ref: EA March 1982)



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(Ref: EA June 1982)



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High efficiency emitter head - Fits completely inside a high quality ABS box (NOT a metal lid) - Only 2-core mains flex protrudes from the box - You can pay over \$80 for a built-up inferior unit!
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runs directly from 240V mains
low power consumption
produces high intensity electric field
output around 7.5kV
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ideal for those who wish to 'try' an ioniser at an economical price.
Cat. KJ-6510

NORMALLY \$24.50

\$15.00

ETI644A

See ETI Jan '83!!

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Ref: ETI October 1982

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Arlec transformer as used in this project only \$22.00



NEW MODEL

SHORTFORM KIT
Cat. KE-4600

ONLY \$169

COMPLETE KIT
Cat. KE-4601

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Mask the sounds that irritate

by COLIN DAWSON

Noise Simulator

Sick of being woken by noisy neighbours or traffic? Fed up with barking dogs?

The EA Noise Simulator provides a soothing noise, like rain on the roof or waves on the beach, to mask the sounds that irritate.

As many flat dwellers will know, modern high density residential tend to have poor sound proofing. Between the numerous TV sets, stereo systems, tomcats, and noisy vehicles in the vicinity, the devotee of serenity can be driven to the point of distraction. Of course, some people have a high level of tolerance for noise pollution but, for those unfortunates who resort to stuffing their ears with cotton wool at 2am so that they can get some peace, the Noise Simulator may be a more pleasant solution.

The problem of getting a good

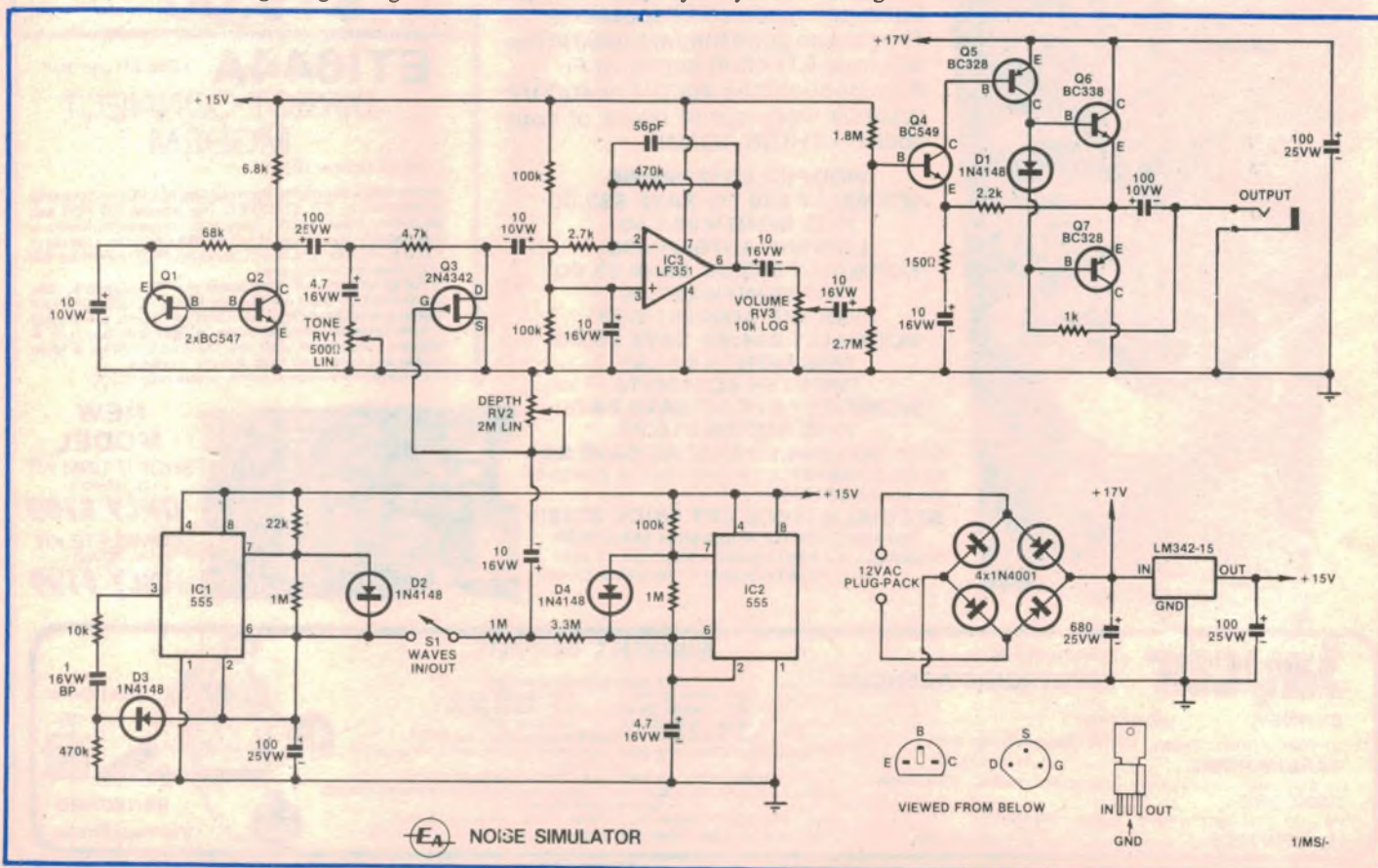
“night’s” sleep is more acute for shift workers who may in fact be trying to sleep during the day. And tinnitus sufferers, no matter when they are trying to sleep, have to put up with continual ringing in their ears. Both groups of people could benefit from a Noise Simulator.

There are, of course, other ways to mask irritating sounds. An air conditioner provides a useful pseudo white noise source but is certainly not viable in this capacity alone. Similarly, a TV set tuned between stations may help but who could justify its all night

operation. A radio tuned between stations can be quite acceptable — provided it has a tone control and can be powered from the mains. It should preferably have a large speaker (15cm or more). If your radio doesn’t quite fit the bill, or is not portable, then a Noise Simulator may be a better solution.

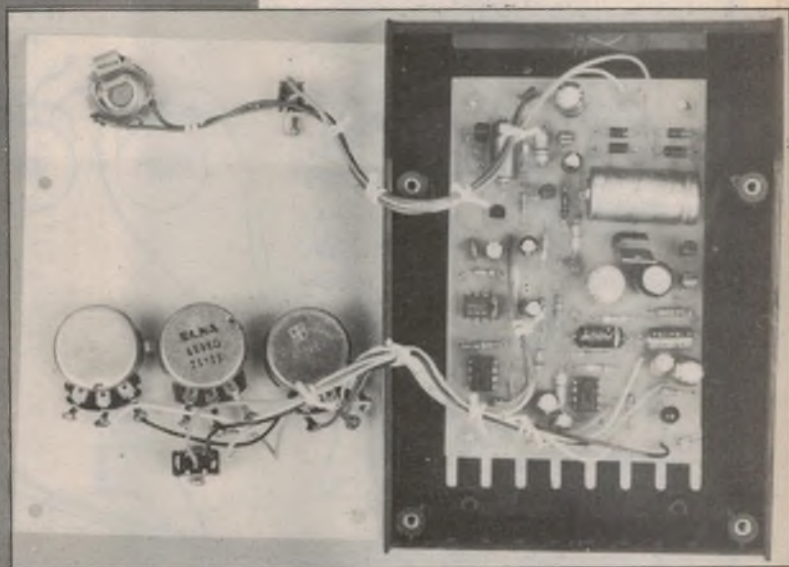
There is another aspect of the Noise Simulator’s operation which diverges slightly from the original concept. The noise can be modulated. In fact the design incorporates two modulation circuits which can provide a number of familiar sounds. The most startling is the surf simulation — sounds just like the beach with a high surf. This may be useful as a sound effect for recording or theatrical effects.

The depth of modulation can be adjusted so that the sound is more like that of a beach in the distance. Or the “waves” can be switched out to leave a simple repetitive modulation more like a rain storm.





Left: the finished unit and, below, interior shot showing board assembly and controls.



We estimate that the current cost of components for this project is approximately

\$30

This includes sales tax but not the cost of a plugpack.

Part of the inspiration for this project came from an advertisement in an overseas magazine. We had already decided to design a modified white noise generator as a sound masker. We were undecided with respect to the surf simulation, until the advertisement. This described a device almost identical in concept, except that it had surf, rain and waterfall simulation. Besides noise masking, there was a claimed increase in "Alpha" sleep (we suppose that's an advantage — we're not too sure what "Alpha" sleep is!).

We are certain, however, that sleeping is preferable to lying in bed pondering the most satisfying form of retribution to the various noisy miscreants.

White noise

Actually, "white" noise — an equal distribution of sound energy across the audio spectrum — is not ideal for the function of noise masking. It tends to sound too urgent and irritating, like a tyre being deflated rapidly. Far more acceptable is a modified white noise, ie, with some of the high frequency content removed. The Noise Simulator has a tone control which provides an adjustable amount of treble cut. This can vary the sound from a hiss (useful for the surf simulation) to a rumble.

To mask irritating sounds, a rumble is

the preferred noise. Most people will quickly become oblivious to this and hopefully the offending sounds will be relegated to "background" where they are not so troublesome.

As well as the big "breakers", we found that small fill-in waves were needed. It just doesn't sound right to have a thunderous wave arriving periodically with virtual silence in between. The circuit is designed so that the "big" waves and "little" waves can interact, producing a moderate amount of irregularity in the sound.

How it works

The most important parts of the circuit are the white noise generator and the amplifier. This accounts for about half of the components. The rest are used to derive the control necessary for the "effects" — it turns out that a convincing wave sound requires a surprising circuit complexity.

The white noise is actually generated by a reverse biased BC547 (Q1). Initially, various diodes were tried in this role but the BC547 proved more suitable for low voltage operation. Even with this device, a useful amount of white noise cannot be generated with a power supply of much less than 11V.

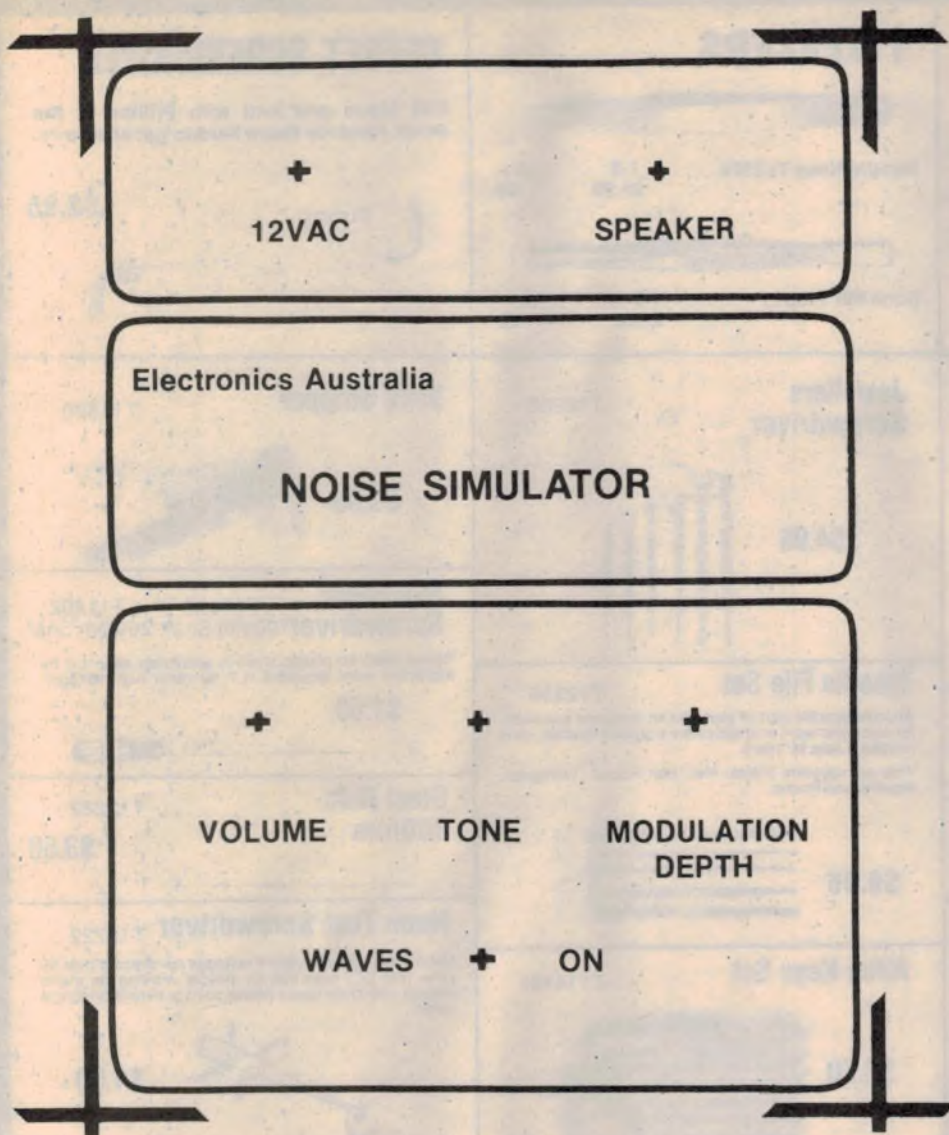
Given that the project may be operating for hours at a time, and the

voltage limitation of the BC547, batteries are clearly out. Instead, a 12VAC plugpack is used. In fact, the output of these plugpacks will frequently be closer to 13V for this circuit, yielding 18V after rectification. Only the power amplifier section of the circuit operates directly from this "raw" supply. The rest of the circuit is powered via a 15V regulator.

Amplification of the white noise is provided by Q2, another BC547. About 600mV of signal will appear at its collector. This is fed to the tone control which consists of a 4.7µF capacitor and 500Ω potentiometer. Quite severe treble cut can be achieved with this control, providing the desired rumble.

The modified white noise is taken from the tone control and fed to the amplifier section of the circuit. The amount of noise reaching the amplifier can be affected by the modulation circuitry, but for the moment, assume that this is not working. A steady level of noise would therefore reach the inverting input (pin 2) of IC3. This is a FET input op-amp (LF351 or TL071) configured as an inverting amplifier with a gain of 37.

From IC3, the signal is fed to a 10kΩ volume control and subsequently to a four transistor power amplifier. With the tone control set for maximum treble cut, much of the sound energy has been removed from the signal. Consequently, quite high volume settings may be needed for a large room.



The operation of IC1, then, is as follows: about once every 15s, the wave begins to build up. This takes only three or four seconds whereupon the wave breaks. For about 0.5s immediately after the break, a very rapid decay occurs. After this period, decay continues more slowly until the beginning of the next build-up.

Switch S1 in the output circuit of IC1 allows the sound of the large waves to be switched in or out of circuit as required. Since the output of IC1 is coupled to the FET gate circuit via a 1MΩ resistor, compared to the 3.3MΩ coupling resistor of IC2, it has a far greater effect on the sound.

Construction

The printed circuit board (PCB) is coded 84ms4 and measures 72 x 110mm. There is one wire link to be mounted on the board — this should be done first. The other components can then be mounted, starting with the small horizontal devices such as resistors and diodes.

We have prepared a Scotchcal front panel label which suits the plastic sloping front project box. If you intend to use this label apply it first so that it can be used for a template for drilling the front panel.

When mounting the input sockets, make certain that the 12VAC input and the speaker output do not share a common earth. This means that, with a metal front panel or Scotchcal label, one of the sockets (preferably the 12VAC socket) should be insulated. This can be done by placing a short length — about 2mm — of plastic tubing over the shaft of the socket and placing an insulated

PARTS LIST

- 1 PCB, 72 x 110mm, code 84ms4
- 1 plastic project box (Bimbox No. 6005 or similar)
- 1 6.5mm panel socket (mono)
- 1 6.5mm jack plug (mono)
- 1 3.5mm panel socket (mono)
- 1 3.5mm jack plug (mono)
- 3 knobs to suit potentiometers
- 1 SPST toggle switch

Semiconductors

- 2 BC547 NPN transistors
- 1 BC549 NPN transistor
- 1 BC338 NPN transistor
- 2 BC328 PNP transistors
- 1 2N4342 P-channel FET
- 1 LF351 or T1071 FET input op-amp
- 2 555 timer ICs
- 1 LM342-15 or LM340-15 regulator
- 4 1N4001 diodes
- 4 1N4148 diodes

Capacitors

- 1 680μF/25VW axial electrolytic
- 4 100μF/25VW PC electrolytics
- 1 100μF/10VW axial electrolytic
- 5 10μF/16VW PC electrolytics
- 2 10μF/10VW axial electrolytics
- 2 4.7μF/16VW PC electrolytics
- 1 1μF/16VW bipolar electrolytic
- 1 56pF ceramic

Resistors

- 1 x 3.3MΩ, 1 x 2.7MΩ, 1 x 1.8MΩ,
- 3 x 1MΩ, 1 x 470kΩ, 4 x 100kΩ, 1 x 68kΩ, 1 x 22kΩ, 1 x 10kΩ, 1 x 6.8kΩ, 1 x 4.7kΩ, 1 x 2.7Ω, 1 x 2.2kΩ, 1 x 1kΩ, 1 x 150Ω, 1 x 2.2MΩ log potentiometer, 1 x 10kΩ log potentiometer, 1 x 500Ω linear potentiometer.

washer under the retaining nut.

To test the Noise Simulator, set the volume to near minimum, the tone to low and the waves to Off. After applying power there will be a delay of about 2 to 4 seconds before any sound is produced (it takes that long for the white noise generator to become operative). Once the sound begins, vary the controls to verify the operation. Remember that only one wave occurs every 15 seconds.

BASIC ELECTRONICS

For the beginner, or for the hobbyist as a reference book and almost certainly the most widely used manual on basic electronics in Australia.

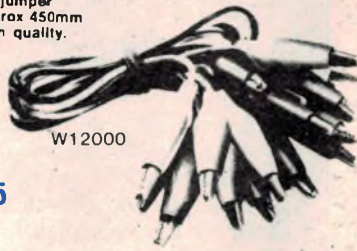
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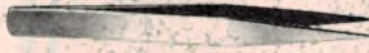
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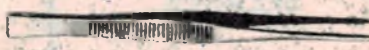
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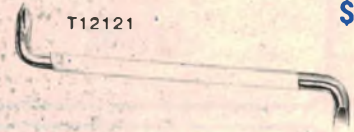
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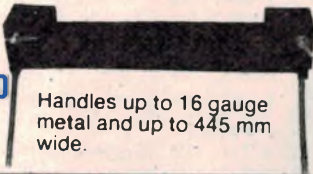
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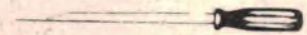
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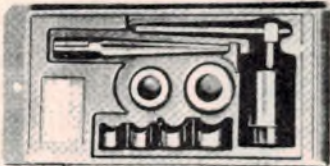


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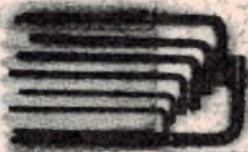
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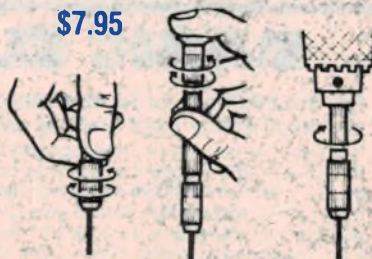
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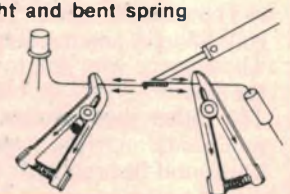
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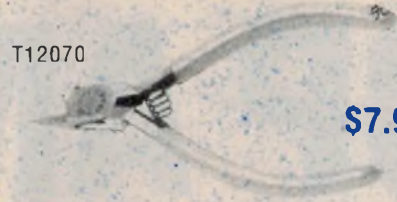
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T12001

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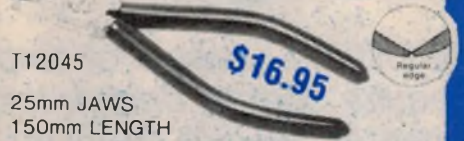
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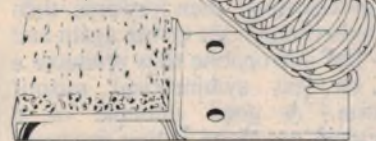
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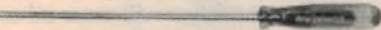
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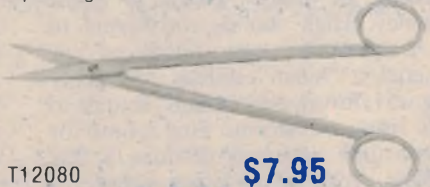


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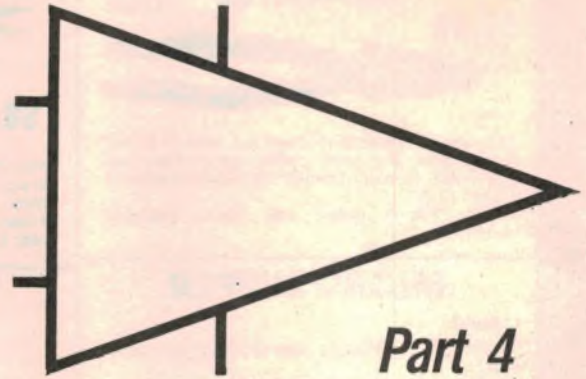
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OP AMPS Explained



Part 4

Amplifiers capable of amplifying DC signals require special design techniques. In this chapter, we will consider the implications of DC coupling, bandwidth, drift and high gain.

If we require a DC coupled amplifier circuit of high gain, it is not sufficient to simply couple together a number of ordinary designs. Neither should we attempt to achieve very high gain in one ordinary operational amplifier stage. So how should we do it? The answer is that we must begin at the input socket and design a complete system to meet our requirements.

But first, why would we want to go to all this trouble? We will look at this question from two points of view: individual stages using op amps, and large amplifiers of many stages.

Fun and music

Once upon a time, most electronic circuits were designed solely for reproduction of music or speech (or cricket). Radio transmitters and receivers, record players, and public address systems accounted for most of the effort expended and the inventiveness evident. Designs were small, large or huge but they all had one common feature: their voltage and current waveforms had a certain *symmetry*.

By this we mean that, by and large, whatever a voltage did above the zero line (positive excursions) it usually did much the same thing below the zero line (negative excursions). Most sounds correspond to a voltage waveform consisting of many cycles of some frequency. High sounds correspond to high frequencies; deep sounds to low frequencies; "harsh" sounds to steeply rising waveforms; and "round" sounds to gently rising waveforms. Sing a note for a short time and you produce a few complete cycles of a voltage waveform

from a microphone. If they can't shut you up, your microphone generates a long train of complete waveform cycles.

Basically, the sound moves the microphone diaphragm back from its centre rest position, then forwards, then backwards through the centre again and so on. The microphone thus produces a more or less symmetrical output waveform. A good example of a symmetrical waveform is that produced by a sinewave generator as illustrated in Fig. 1. Note that the positive and negative signal excursions are symmetrical about the centre zero line.

The modern generation

Today, electrical signals are generated by a whole host of sources. A modern music group may have microphones and guitars generating the aforesaid bipolar signals, along with synthesisers and other digital signal generators. The common TV receiver is renowned for its strange voltage waveforms and delights in generating square wave voltages, triangular waves and half-cycles of sinewaves. Computers, terminals, and logic circuits live by generating square voltage pulses of single polarity as Fig. 2 illustrates.

To cap it all off, we want amplifiers to increase the sensitivity of some of our DC voltmeters and oscilloscopes. *Voltage wave symmetry has been lost.*

So what? — you quickly retort — who cares? What does it matter if our voltage signals are symmetrical or not? Until single-sided voltage-pulses came along, many did not realise how fortuitous the double-sided voltage waveforms were to the circuit designer as the following story shows.

Fig. 3 shows a very dated, and rather horrible, microphone preamplifier of medium gain. Glossing over such details as the awfully high output impedance, let's consider the average or quiescent circuit voltages. The base voltage divider on the input transistor provides a positive DC bias, some of which is cancelled by the emitter resistor (in a stabilising attempt). The quiescent voltage at the collector (2) is some function of the resultant bias, the transistor's temperature and the h_{FE} . These usually provide us with such a delightfully unpredictable set of numbers that it is very difficult to precisely predict the voltage at collector 2. But, you see, the world is indeed good to us for it doesn't matter at all.

For — lo and behold! — coupling capacitor C1 is usually described in the textbooks as being put there to remove the collector DC potential, leaving only the signal variations to pass on to the second stage. The real truth is that the coupling capacitor was put there because we have no idea what the collector voltage might be at different times on different days.

Let the transistor h_{FE} vary! Who cares if the operating conditions are different in summer or winter? So what if the quiescent collector voltage is 3V at lunch time and 5V at night when it's cooler! The coupling capacitor will erase all our sins; the world and the following stage will never know! We owe a lot to that humble component; just as well conditions allowed us to use it!

And just what were those conditions? Symmetry — yes, signal voltage symmetry — allowed us to use that indispensable little coupling capacitor. To explain, let's consider the real action of that erstwhile component.

As Fig. 4 shows, we imagine C to be simply coupling a signal from input to output. In actual fact, C is being charged by V_{in} through R_{source} . After that, C supplies voltage V_{out} while being discharged by R. To make any sense, R is

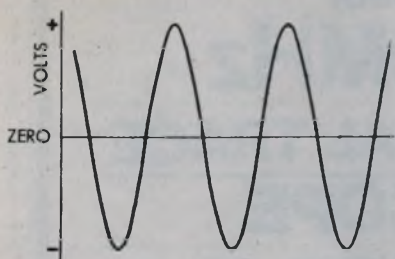


Fig. 1a: voltage output from a sinewave generator. Note waveform symmetry about the 0V line.

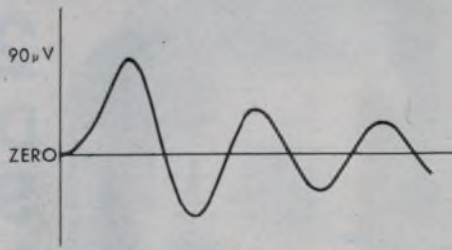


Fig. 1b: voltage waveform produced by a microphone in response to a sharp transient. The waveform still has approximate symmetry despite exponential decay and harmonic content.

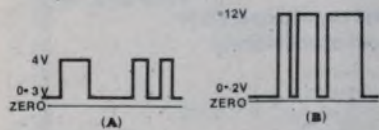
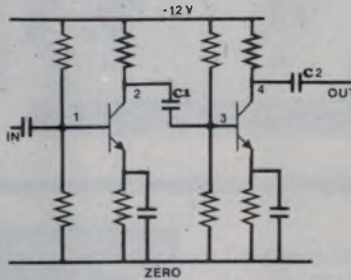


Fig. 2: digital logic gates produce voltage waveforms that are asymmetrical about the 0V line. These examples are from TTL (A) and CMOS (B) circuits.

Fig. 3: early microphone preamplifier design. Coupling capacitors C1 and C2 isolate the collector DC potentials from the following stages.



much greater than R_{source} . Therefore the rate of discharge of C is simply the time constant RC . If R is measured in ohms and C in Farads, then their product (RC seconds) is the time constant of the coupling circuit. R is the parallel resultant of the physical resistive path to ground and the input resistance of the following stage.

Results

(a) When the input signal is a sine wave there is no problem. The output is also a sine wave with a phase shift.

(b) Fig.4 also shows a single-sided input voltage waveform, swinging between zero and positive voltages only and with a small mark-space ratio. Observe that at 1 the input and output rise to the same height, as we would expect. Between 1 and 2, V_{in} maintains a constant voltage (ie, the top of the waveform is level). But during this time, C is discharging through R and so the voltage V_{out} falls a little. This "droop" is actually due to the exponential discharge curve but, if short enough, looks approximately like a straight line sloping downwards.

By the time point 2 is reached, the output voltage is down to about 0.9V instead of the original 1.0V. Then, at 2, V_{in} drops by exactly 1V; ie, the potential on the left plate of C changes abruptly by $-1V$. Because the voltage across a capacitor cannot change instantly (it takes time for a capacitor to charge), this means that the voltage on the right plate of C must also drop abruptly by 1V.

So, theoretically, V_{out} should drop abruptly from $+0.9V$ to $-0.1V$ at time

2. And that's exactly what happens. Between times 2 and 3, V_{in} is zero so the capacitor simply discharges from its $-0.1V$ state towards zero. Notice we said *towards zero*. *The capacitor does not discharge completely to zero.*

When time 3 arrives, the capacitor still has a small negative charge on its output plate, perhaps $.01V$. V_{in} rises by another 1V step at time 3, lifting the output plate of C from $-0.1V$ to $+0.99V$, which decays as before from $+0.99V$ down to $+0.89V$ by time 4. This time the 1V drop of V_{in} is accompanied by a drop of V_{out} from $+0.89V$ to $-0.11V$; notice this level is a little lower than before.

Repeated pulses continue this trend, as shown in the diagram, with the step up and down always exactly 1.0V, and the overall level between each step slowly falling.

How far will these levels fall? Right down through the bench and onto the floor? No, not at all. It can be shown that equilibrium will be reached and the voltage levels will fall no longer when the area enclosed between the positive part of the voltage waveform and the zero line is equal to the area enclosed between the negative part and the zero line. The proof of that statement we won't go into; it involves a smattering of integral calculus and assorted mathematics. The strict statement of the theorem is that after equilibrium is reached the total integral of the waveform is zero over any complete number of cycles.

Mark-space ratio

For one-sided "square" voltage

waveforms such as that in Fig.4b, we define the mark-space ratio as the ratio of the time that the voltage is high to the time it is zero. Fig.4b shows a mark-space ratio of approximately 1:9. Some readers may think that the expression "square wave" should really only apply to Fig.4c because it looks square, not rectangular. However, common practice is to use the expression "square wave" for any waveform with vertical sides, or nearly so, as long as the mark-space ratio is not too small.

Note that the absolute square wave Fig.4c has a mark-space ratio 1:1. An alternative expression also used is *duty cycle*, which is the percentage of up time in one complete cycle. Fig.4c thus has a 50% duty cycle and Fig.4b a 10% duty cycle.

The mark-space ratio has a profound effect on the depression of the single sided waveform below the baseline. Fig.4b shows only a small depression, but this is still sufficient for the "negative area" to be equal to the "positive area". Now observe in Fig.4c that a 1:1 mark-space ratio results in an output waveform that is symmetrical about the baseline.

But worse is to come. Consider Fig.4d where V_{in} is a single sided waveform from zero to $+1V$, with the waveform mostly high (ie, at $+1V$). The vertical sync waveforms look like this. The resultant V_{out} discharges so much during the up time that it soon decays down to about $+0.1V$, with the 1V step down taking it down to $-0.9V$. The very large mark-space ratio of 9:1 quickly pushes the output waveform down until it is mostly negative.

Uses

If our pulse were to be used for sound output there would be no trouble. Both V_{in} and V_{out} in Fig.4d would make much the same sound in a speaker. But that is not the usual purpose of such waveforms. Instead, they are mostly used in digital circuits where the presence of a pulse above some predetermined threshold for a certain time is the vital consideration.

Perhaps an industrial process produces small amplitude pulses which we want to count. We need an amplifier to bring them up to usable size, as well as a circuit to record how many times the input voltage waveform exceeded a threshold. We could, for example, choose a threshold of $+0.8V$ as shown in Fig.5. A smaller threshold could be chosen, but this may lead to error because of noise and other voltage fluctuations.

Many industrial processes give rise to rather random strings of pulses of various lengths as depicted. The

OP AMPS Explained

threshold counter circuit cannot be applied to V_A as the 1mV level is far too small to use. So it is applied to V_B with its zero to 1V excursions.

But look what the coupling capacitor has done! V_B has many different values of voltage below the baseline because it has many different values of mark-space ratio. Poor coupling capacitor! Guilty! No suitable threshold can be chosen for the counter circuit. No satisfactory equipment can be designed. The counter will inevitably miss some counts of the industrial process.

Other reasons

The foregoing is but one example of the havoc wrought by that shameful component, the coupling capacitor, on DC signals. Countless others could be cited.

Example two is a very short story of a student who decided one morning to measure the amplitude of a 0.4V 0.5Hz sinewave signal using an ordinary oscilloscope. He measured a quite erroneous value of 0.15V instead of 0.4V, as being not yet fully awake he left the oscilloscope input switched to "AC coupling". Thus, his low frequency signal was coupled to the oscilloscope's amplifiers via an internal coupling capacitor.

In the case of a sinewave, equally balanced above and below zero, no depression of the signal occurs. But what does happen is that X_c and R form a signal voltage divider, where X_c is the capacitive reactance of the capacitor to sinewaves. At frequency f , the reactance is

$$X_c = 1/2\pi fC \text{ ohms}$$

and the lower the frequency the higher the value of X_c in ohms.

At low frequencies, X_c is greater than R and much of the signal voltage is lost as in Fig.6. In this case only 0.15V is being developed across R as output. (The voltage drop due to X_c is not simply the remainder as vector additions are involved here).

The cure for the student's wrong measurement, by the way, was to switch the oscilloscope to DC coupling, which effectively bridges out the internal coupling capacitor.

Measuring instruments

All sorts of sensitive measuring instruments such as microvoltmeters, millivoltmeters, DVMs, CROs, low level wattmeters and null indicators must

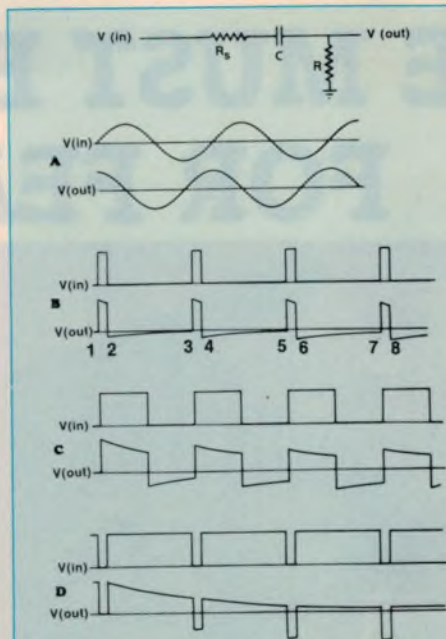


Fig. 4: the effect capacitor coupling has on various signals. Note particularly the effect on DC signals of different mark-space ratios.

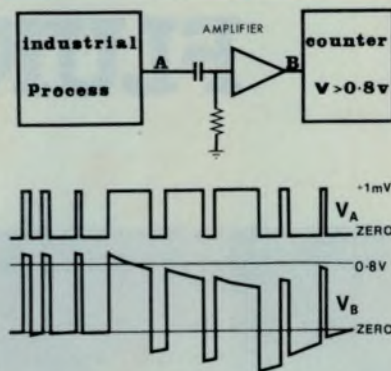


Fig. 5: how capacitive coupling can lead to errors. Some of the pulses at V_B will be missed by the counter due to signal depression below the 0V line.

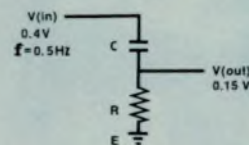


Fig. 6: X_c and R form a voltage divider where $X_c = 1/2\pi fC$ is the reactance of the capacitor to sinewaves.

contain amplifiers to raise a small input signal level to a usable value. Instruments to measure DC current, voltage or power must therefore contain amplifiers capable of amplifying small DC voltages.

Fig.7 shows what happens is we try to amplify a 1mV DC signal using a capacitively coupled amplifier. If the instrument contains an amplifier with a gain of 1000 and an indicating meter requiring 1V DC for full scale deflection, then why shouldn't it behave as a DC millivoltmeter? If it works, a 1mV input should result in a full scale reading on the meter.

Of course, it won't work at all as the voltage diagrams in Fig.7 show. The meter does read 1V initially, responding to the first abrupt voltage change, but the reading then falls gradually to zero as capacitor C charges. Any effort to use very large values of C or R , or both, will just prolong the time constant and cause the meter reading to decrease to zero at a slower rate. But decrease it will, and nothing will make this circuit successful while that coupling capacitor is present.

DC restoration

When television was first invented, a crying need for a circuit to amplify DC signals came with it. The abrupt changes in voltage level from white picture to black picture, through to the tips of the sync pulses, are critical to the operation of a TV receiver. If these voltage levels are incorrect, your TV picture could lack contrast, roll or even be torn to bits. Other faults, such as failure to separate picture from sound, can follow as side effects.

The root cause of our problems is that the demodulated video signal is unbalanced about the zero line. It lacks symmetry. Early TV circuit designers used capacitor-coupled video amplifiers, then ingeniously devised additional circuitry to re-insert the correct amount of DC level. While this overcame any problems caused by the coupling capacitor, it represented a way out rather than an ideal.

Feedback requirements

Negative feedback around an amplifier stage can also cause problems due to phase shifts or time delays. As shown in Part 2 of this series, sufficient phase delay or lead can make negative feedback look like positive feedback. This will immediately cause instability in the amplifier if the gain around the loop is greater than one.

Getting back to Fig.7, the coupling capacitor-resistor combination causes a phase shift which varies according to the input frequency — a nasty situation indeed! As all our operational amplifier circuits, by their very nature, use heavy negative feedback, it is mandatory that DC coupling (ie no coupling capacitors) be used within any one stage. If feedback is applied around more than one stage, then DC coupling should be used overall.

The cure

Once upon a time, a circuit designer of great wisdom and experience gave his apprentice one piece of advice: "if a component gives you design trouble, don't use it at all".

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OP AMPS Explained

factor in common, one source of trouble: that ubiquitous coupling capacitor! Clearly the cure is not to use a larger capacitor, nor a different type, nor a more expensive one. No! The cure is not to use one at all!

But wait! Fig.3 showed clearly that some designs are rather uncertain of their DC output levels and we only got away with it by using coupling capacitors to hide all our errors. So the panic begins — can we really design amplifiers so well that the output DC level is well known, predictable and quite stable? If so, then that DC collector potential in Fig. 3 will be a known quantity. The trick is to devise some method whereby we subtract a known DC voltage from the collector circuit without changing the signal content. Fig.8 shows the basic idea.

Requirements

There are two requirements for this scheme to work:

1. The collector resting voltage must be stable at some value when the input is reduced to zero.
2. The subtraction circuit we construct must provide a constant DC voltage drop across it and, at the same time, appear as a low impedance so that we do not unduly attenuate the signal passing through it.

All integrated circuits on the market intended for use as operational amplifiers fulfil both requirements. Should we wish to design our own circuits, as has been done in some EA record playing preamplifiers, we must achieve both requirements ourselves. We will consider some of the standard methods in use.

Fig.9 shows Q1, the original amplifying transistor, with a gain of -50 . Q2 is an emitter follower and D1 is a 9.4V zener diode. Q1's collector resting potential is +10V when there is no signal input, falling to +9.5V when a 10mV signal is applied to the base.

The zener voltage drop (9.4V) and Q2's base-emitter drop (0.6V) are subtracted continuously from Q1's collector potential to provide output V_{out} . With zero input, $V_{out} = 10V - 9.4V - 0.6V = 0V$. This is always the design aim: zero input should give zero output.

Because each component used has those stated voltage drops at all times, the circuit can follow changes as slowly as we like. No component is low frequency dependant and no low

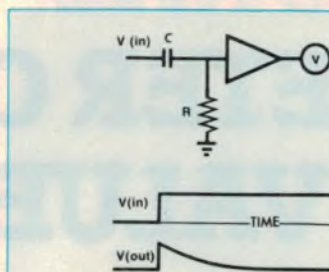


Fig. 7: this figure shows an unsuccessful attempt to drive a DC voltmeter using a capacitively-coupled amplifier. The DC voltmeter responds to $V(out)$ and so is quite useless.

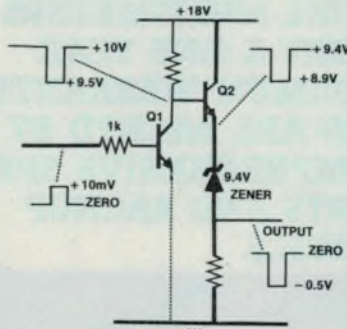


Fig. 9: first steps in constructing a DC-coupled amplifier. The quiescent resting potential of Q1 is +10V. Thus we use the emitter-base potential of emitter follower Q2 (0.6V) and the zener voltage 9.4V to subtract 10V from Q1's collector.

frequency phase shifts occur. There is no charge-discharge effect and the amplifier will respond at any low frequency right down to 0Hz, ie. it is DC coupled. Naturally we still have the high frequency limitations common to all amplifiers.

Of the two requirements listed above, the second, that the zener plus Q2 base-emitter voltage drop be a constant 10V and appear as a low impedance, is well satisfied. But the first, that Q1's collector resting voltage be stable, is *not* well met by the simple circuit shown in Fig.9. The quiescent voltage on Q1's collector is a function of collector current which, in turn, varies according to temperature and rail voltage. Therefore, we must improve our first basic effort to stabilize collector current.

The favourite method is to use a *long tailed pair* as in Fig.10.

The long tail pair

The beautiful DC stability of the long tail pair is due to the fact that resistor R_T , the "tail", has a very high value. High value resistors are sometimes described as "long", a term that probably originated in the early days of wireless when megohm carbon resistors had to be physically long to achieve that high value. We all know Mr Ohm's famous law about current, resistance and

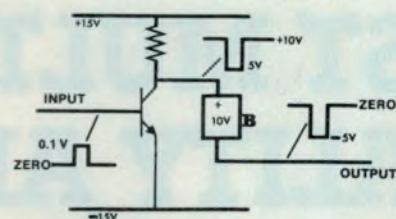


Fig. 8: basic DC-coupled amplifier. A 100mV input signal is amplified to provide a $-5V$ swing at the collector ($+10V$ to $+5V$). Block B subtracts the $+10V$ quiescent collector potential thus providing a 0 to $-5V$ output. With this arrangement, zero input will give zero output which is what we want.

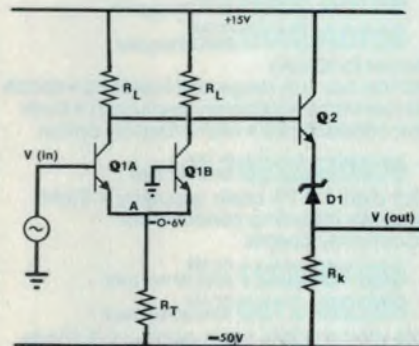


Fig. 10: DC-coupled amplifier using long tailed pair to stabilise Q1 collector current. Though workable, the $-50V$ rail is inconvenient and diode D1 has no gain.

voltage, but do we realise its subtle implication? It implies that when two resistors are in series, the larger has the greatest influence in deciding the value of the current.

In Fig.11, we place a high voltage and a high resistance in a box and, through terminals A and B, connect it to a much lower resistance outside. The outside world has very little control over the current flowing under these conditions. That is decided almost entirely by the things within the box. In fact, the box seems to the outside world as being hell-bent on generating its own current no matter what we do outside. That box seems to us to be a *constant current generator*.

So too, in Fig.10, the $-50V$ rail and R_T form a constant current generator, with Q1 and R_L acting as the outside world. This is because $R_T = 500,000$ ohms is by far the highest resistance present. Thus the total current through both halves of Q1 and R_L is held at almost a constant value and is not greatly influenced by temperature changes in the transistor.

Now let's specify Q1A and Q1B as a matched pair which are thermally coupled together on a common silicon substrate (ie, the transistors will always be at equal temperature). This will cause them to share current i_T equally as they

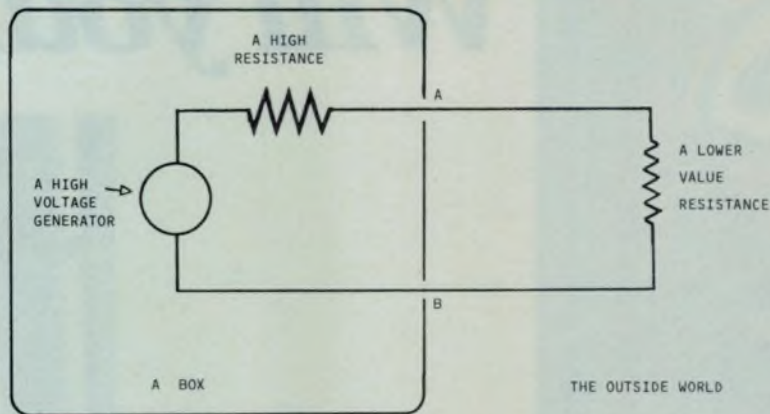


Fig. 11: basic constant current generator.

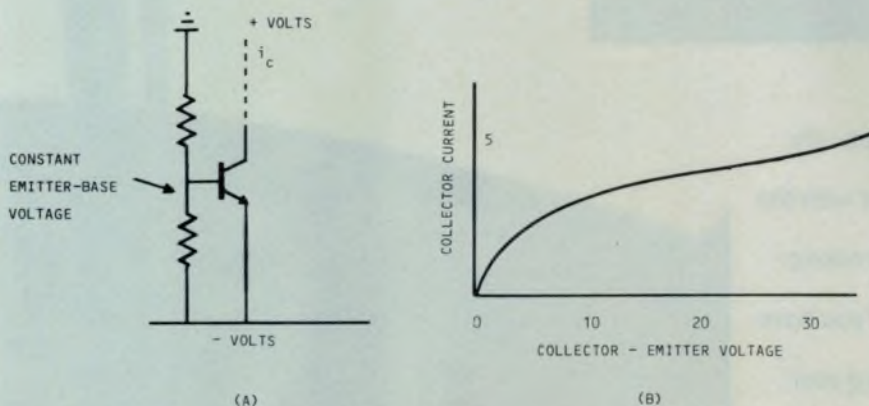


Fig. 12: improved constant current source. If temperature remains constant, an approximately constant collector current flows as curve B indicates. More complex designs may have improved characteristics. Collector current scale in B is milliamps for 20 microamps base current.

have a common bias system provided by a negative voltage of about $-0.6V$ at A. Note that both bases are returned to ground zero. No further bias circuitry is necessary.

With zero input to Q1A, the resting potential at Q1A's collector remains constant at $+10V$. A positive signal on Q1A's base, however, causes Q1A to pass more collector current. Therefore, Q1B must pass less collector current since the sum of the two collector currents is a constant equal to i_T . Hence, Q1A's emitter voltage at A will not change.

That rings a mental bell! Here we have a changing signal and changing individual currents in Q1A and Q1B, but no change in voltage at A! Could it be that A is another example of a virtual earth? Yes! It's true! It's similar to our earlier discussion on the "virtual earth" at an operational amplifier's summing junction.

The inability of the voltage at A to change in the presence of an input signal means that A *appears* to be at ground potential, at least for *changes* in signal, despite the $-0.6V$ DC potential there. This fact has a far-reaching implication.

It means that no degeneration of gain occurs in the tail resistor R_T . Thus, there is no need to bypass R_T as we usually did to the emitter resistors in those awful little single-sided amplifiers as in Fig.3.

Improvements

Though Fig.10 will work, a $-50V$ supply is both inconvenient and expensive. We need to make a few improvements to the circuit, particularly to the constant current source.

Consider the transistor stage shown in Fig.12a. This has a constant emitter-base voltage and thus operates with constant collector current. Even reasonably wide changes in collector-emitter voltage have little effect on collector current as Fig.12b shows.

So Fig.12a behaves as a constant current source and can thus be substituted for R_T in Fig. 10. The big advantage of this scheme is that we no longer require a high voltage ($-50V$) supply; a $-15V$ supply can be used instead. Beauty! That was easy.

Now if you would like more improvements, consider that while Q2, D1 and R_k in Fig.10 are nice stable components, they contribute no gain. By

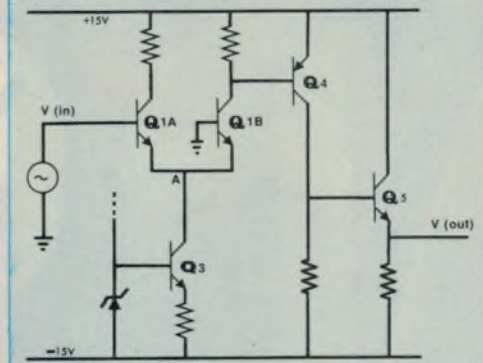


Fig. 13: improved high gain DC-coupled amplifier. Q1A and Q1B form the input balanced long tail pair, Q3 is the constant current tail, and Q4 contributes gain and carries out the DC level shifting function. Q5 is an emitter follower stage to give low output impedance.

substituting transistor Q4 as in Fig.13, we can perform the DC shift function and derive some gain at the same time. Q3 performs the aforesaid tail function (ie, it functions as a constant current source) while emitter follower Q5 provides a low output impedance. Integrating such an amplifier is slightly more complicated as both NPN and PNP transistors must be fabricated on the one silicon chip.

Fig.13 is a simplification of the type of circuit commonly used in op amp ICs. If you wish to see such circuits, you will find them drawn in detail in manufacturer's databooks, such as National Semiconductor's "Linear Integrated Circuits". Any of these integrated amplifiers may be used to assemble one operational amplifier stage as in Figs.14 or 15. As shown, both phase reversing and non-reversing circuits are simple to put together with a handful of components. Any one stage is thus fully DC-coupled from input to output, enjoying all the desirable properties mentioned above.

Performance limits

Many applications demand quite high gain, so we should consider the gain range available from circuits. Figure 4.14, the phase reversing case, has an overall closed loop gain given by:


Approximate gain = $-R_f/R_i$ and as shown in the first part of this series:

$$\text{True gain} = (-R_f/R_i)[G/(1 + G + (R_f/R_i))]$$

where G is the open loop gain of the amplifier, R_i the input resistor, and R_f the feedback resistor. These expressions allow us to design low gain amplifiers with accuracy limited only by resistor tolerance. A gain of -1 is quite in order, and even fractional gains are quite legitimate if required.

The upper limit on usable gain is an interesting question. Typical values of G

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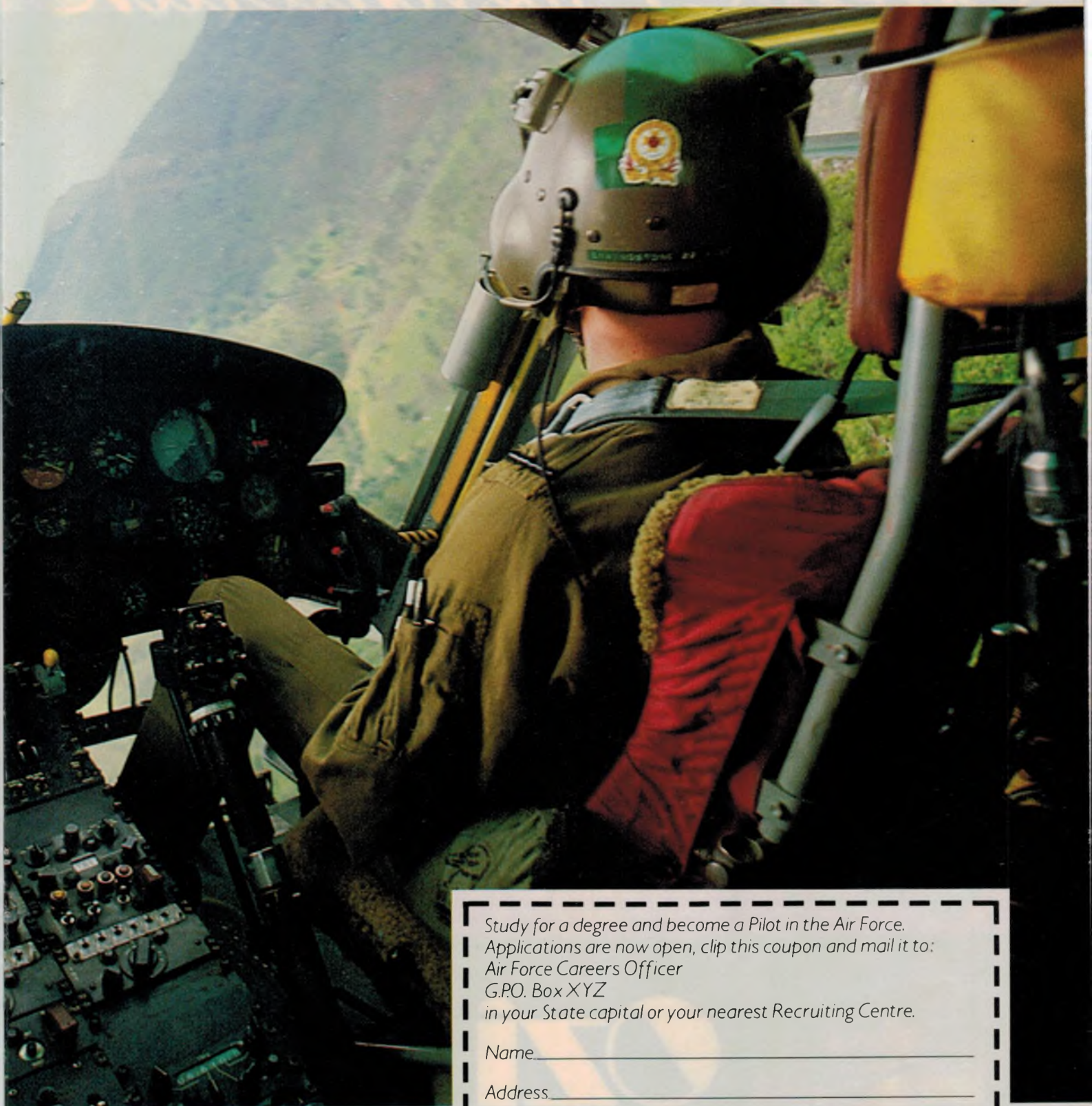
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for common integrated amplifiers are 25,000 (minimum) for the 741, 60,000 (minimum) for the LM3D8A, and 800,000 (measured) for the LM725CH. A little calculation shows that DC gain error for a 741 is quite small for closed loop gains of up to 100. Table 1 tells the story.

TABLE 1

Closed Loop Gain	Gain Error
-1	0.01%
-10	0.05%
-100	0.5%
-1000	4%
-10,000	29%
-50,000	Impossible

High frequency problems

If we choose an op amp IC without an in-built compensation capacitor C_x (eg, LM301, LM308), then we must add C_x ourselves. The correct value for common amplifier chips, as described in part 2 of this series, is:

$$C_x = 33\text{pF}/(\text{closed loop gain}).$$

Closed loop gains of 1 and 10 thus require $C_x = 33\text{pF}$ and 3.3pF respectively. For gain 100, we simply leave the capacitor out as the stray capacitance approximates the required 0.33pF . Gains of 1000 or 10,000 theoretically require $.033\text{pF}$ and $.0033\text{pF}$, but both are smaller than the stray capacitance and so are not realisable. A closed loop gain greater than 100 thus results in severe high frequency loss.

Integrated amplifiers which do contain C_x built into the chip, (eg, 714, AD545,

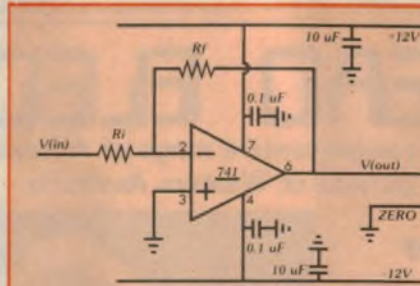


Fig. 14: phase inverting operational amplifier. The closed loop gain is approximately $-Rf/Ri$ (see text).

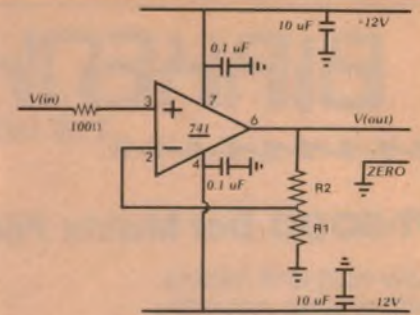


Fig. 15: non-inverting operational amplifier. The closed loop gain for this circuit is approximately $(R1 + R2)/R1$.

LH0052) use a compensation capacitor suitable for gain = 1. This means that the IC will be overcompensated at higher gains and will thus have restricted bandwidth.

Gain limit

On both counts, limit by errors and limit by high frequency losses, we cannot build an operational amplifier with a closed loop gain much above 100 over the entire audio bandwidth. At the same time, amplifiers for voltmeters, motor controllers and other low frequency applications can require closed loop gains up to 1000. Gains of this order (and with just 0.1% DC error) are achievable using products like the LM725 which has an open loop gain of approximately 1,000,000.

For higher gain or lower error (eg, in applications such as six figure digital voltmeters), special hybrid amplifiers are available with open loop gains up to 100,000,000.

Large gain amplifiers

Being now convinced that, for high gain, we must build a multistage system, let's look at some workable ideas. One point to remember is that output from the first stage will be amplified by subsequent stages. In practice, this calls for careful design of the first stage in order to ensure adequate low noise performance.

In Part 3 last month, we saw that noise generated by the first semiconductor junctions is the major noise source. This can be minimised by careful design and also by reducing the bandwidth of our amplifiers to no more than is necessary.

DC offset of the output voltage is another problem. The DC drift is measured by connecting the input to ground (ie, $V_{in} = 0$) and measuring the output voltage with a DC voltmeter. Ideally this output voltage should be zero, any departure from zero being a measure of the offset.

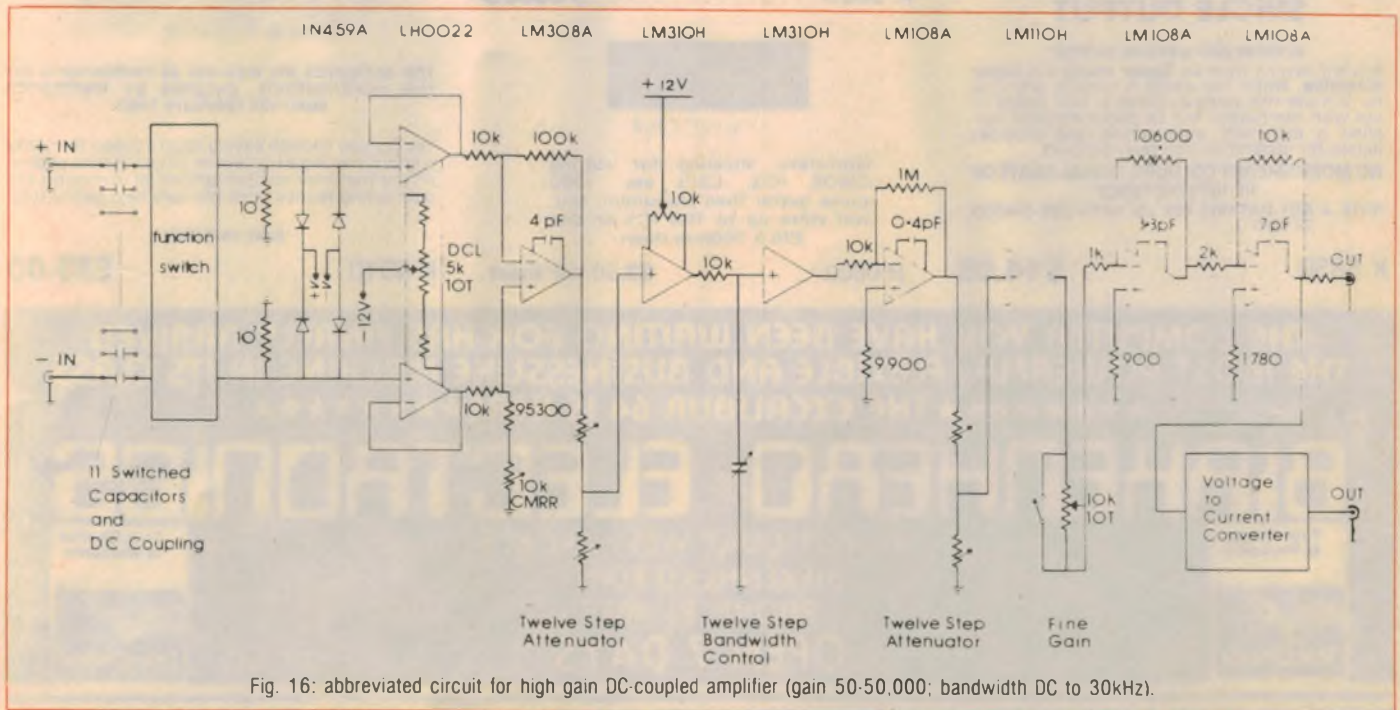


Fig. 16: abbreviated circuit for high gain DC-coupled amplifier (gain 50-50,000; bandwidth DC to 30kHz).

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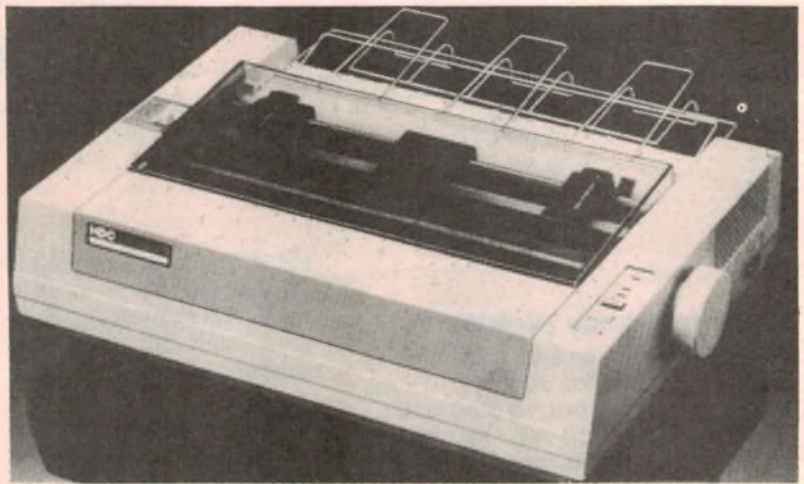
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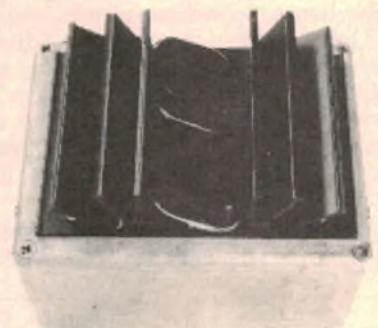
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As a basis for comparison of different designs, it is common practice to express the drift of a stage as the measured offset at its output divided by the stage closed loop gain. This is called "offset referred to the input". It assumes that the offset at the output is simply the offset of the front end junctions amplified by the stage gain.

While reduction of bandwidth does reduce noise, it has no effect on offset in a DC-coupled amplifier system. We have two choices: either cleverly design the stage so that the offset is insignificant, or invent some ingenious offset correction scheme. For the time being, we will consider the first choice only. The latter scheme is used in *chopper amplifiers* and will be discussed next month.

Pure DC amplifier

Figs.16 and 17 depict a pure linear amplifier with bandwidth from DC to 30kHz (reducible by switching if required); overall gain switchable from 50 to 50,000; and switchable AC or DC-coupling of the inputs. Two potentiometers were used to initially set the output of the amplifier to zero. The drift rate achieved (less than $60\mu\text{V}$ after warm up) is extremely small for a pure amplifier — see Fig.18.

The term *pure amplifier* means that this circuit contains no tricks. It is a simple linear system that achieves low DC offset by dint of careful design and stable DC supply rails. All components were carefully chosen for high-stability, while the low current drain assures cool operation.

Each stage in Fig.16 is an excellent example of current op amp design practice. The four diodes following the function switch provide input stage protection, the LH022s act as unity gain high input impedance voltage followers, and the LM308A provides a gain of -10 .

All LM310 and LM110 stages are unity gain voltage followers and are used

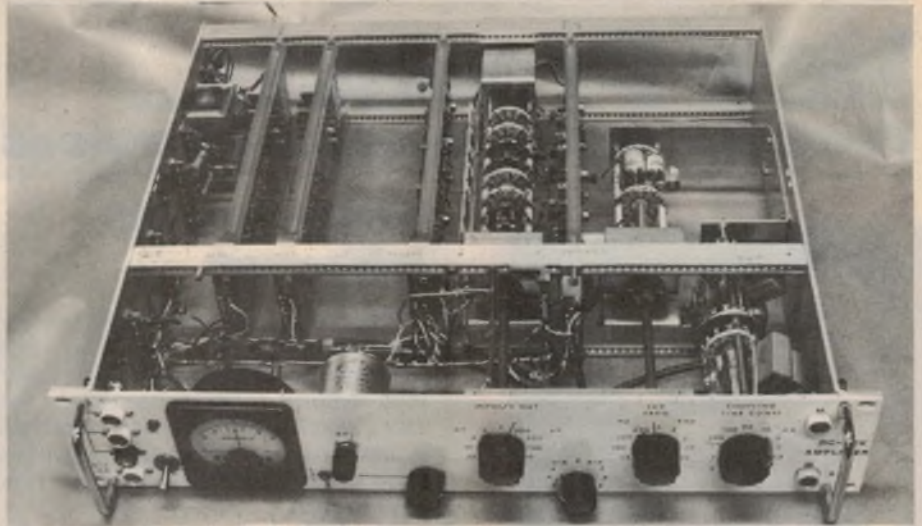


Fig. 17: practical realisation of the circuit shown in Fig. 16.

to provide high stage input impedance following an attenuator or filter. The leftmost LM108A provides a gain of -100 while the two LM108As at the right provide gains of -10 (variable) and -5 . Total overall gain with attenuators at maximum, is the product from left to right:

$$\text{Gain} = (+1) (-10) (+1) (+1) (-100) (+1) (-10) (-5) = +50,000.$$

Note that the bandwidth of the amplifier is maintained by carefully selecting the compensation capacitor for each stage, the value chosen being close to $33\text{pF}/(\text{stage gain})$. Four design criteria essential for achieving low drift are used in Fig.16:

- Each gain stage input has a path to ground (or to a low impedance output point) not greater than $11\text{k}\Omega$.
- Each unbalanced amplifier stage (LM108A) has the signal applied to its inverting input and a compensating resistor connecting from its non-inverting input to ground. This compensating resistor is equal to the parallel resultant of the input resistor and the feedback resistor.

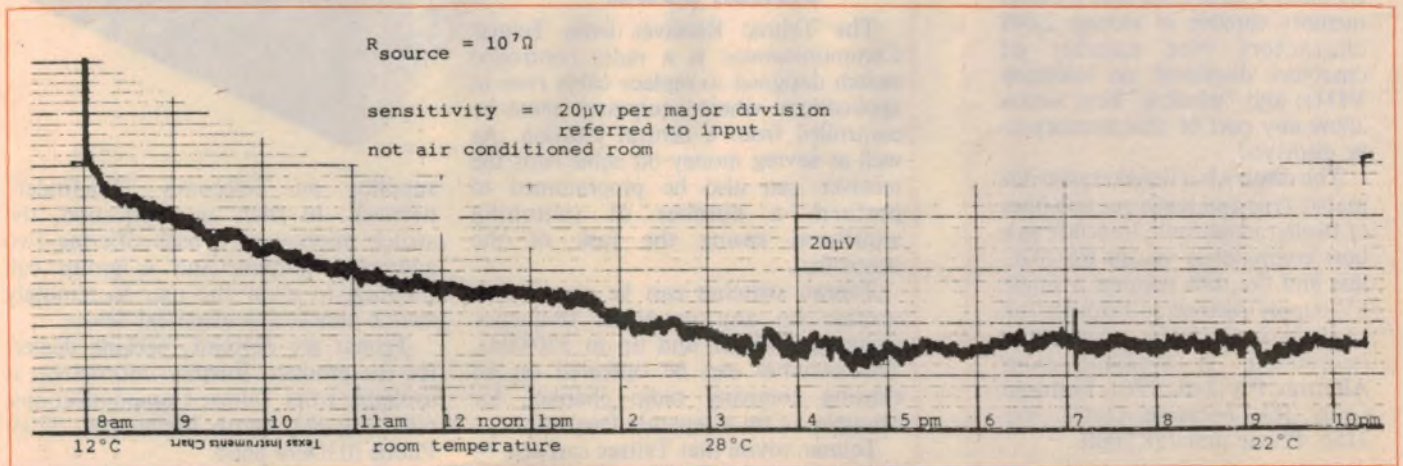
The reason for the compensating resistor is as follows. Because all gain stages have an input bias current, a small DC voltage is present on each LM108A input when the input resistor is connected to 0V . This spurious voltage is not only affected by temperature changes but is amplified along with the wanted signal. The compensation resistor cancels this effect by introducing an equal voltage on the non-inverting terminal.

Thus, the first LM108A stage in Fig.16 uses a $9.9\text{k}\Omega$ compensating resistor which is the parallel resultant of $R_i = 10\text{k}\Omega$ and $R_f = 1\text{M}\Omega$.

- Stable $\pm 12\text{V}$ regulators are used to provide the supply rails. The supply voltage drifts from its nominal value by no more than $100\mu\text{V}$.
- All resistors used are 1% metal film types.

So endeth the fourth lesson. Next month we will take a look at differential inputs and examine some very clever tricks used when even higher gain and lower DC offsets are necessary.

Fig. 18: measured drift rate for the DC-coupled amplifier shown in Fig. 17 and 18 (see text).



New Products...

Product reviews, releases & services



Portable terminal for hand-held data entry

Alfatron Pty Ltd has announced a new portable terminal, the Profort 801, a compact unit which fulfils the same functions as a conventional video display terminal. Features include a buffer memory capable of storing 2,048 characters (the number of characters displayed on ordinary VDTs) and "window" keys which allow any part of this memory to be displayed.

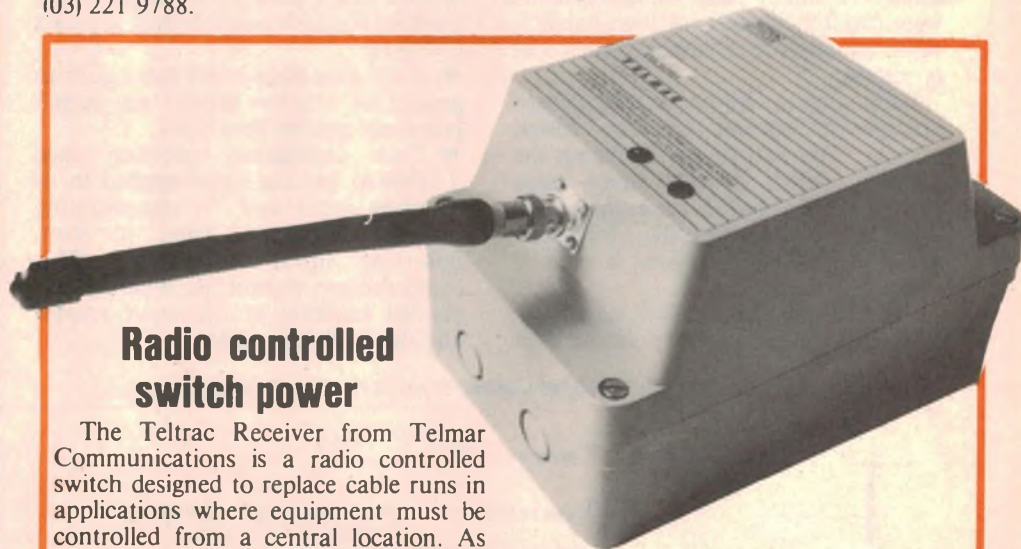
The display is a liquid crystal dot matrix type and reads out two lines of 16 characters each. Interface to a host computer is via an RS-232C line and the unit requires a single 5V supply connected through the serial interface. Further information is available from Alfatron Pty Ltd, 1761 Ferntree Gully Rd, Ferntree Gully, Vic 3156. Phone (03) 758 9000.

Versatile laser bar code scanner

Intermec has released a new laser bar code scanner for industrial and commercial applications. The new Laser 1600 features a helium-neon laser and optics which allow codes to be scanned on flexible and curved surfaces as well as labels which are hard to reach with pen-type readers.

The high scan rate (40 scans per second) means that even dirty or smudged labels can be read correctly in most cases, while legible labels allow an increased throughput as scanning time per label is considerably reduced. Low density codes can be scanned from up to 30cm from the reader and the depth of field of the scanner means that no special techniques are required of operators.

The 1600 can also be mounted in a fixed position and triggered by remote control for applications such as conveyor belts and automated warehousing. Further information is available from Intermec Australia Pty Ltd, 9 Woodbine Court, Wantirna, Vic. 3152. Phone (03) 221 9788.



Radio controlled switch power

The Teltrac Receiver from Telmar Communications is a radio controlled switch designed to replace cable runs in applications where equipment must be controlled from a central location. As well as saving money on cable runs the receiver can also be programmed to perform a number of switching sequences, easing the task of the controller.

Taltrac switches can be supplied to operate on any permitted frequency including 27MHz and up to 520MHz. The switches can be operated on an existing company radio channel, for example, or on a separate frequency.

Telmar advise that Teltrac can also be

supplied on Telecom's "Telefinder" network. In such an application, the switch appears as a page offering two addressed outputs and a group call function to allow the user to remotely switch almost any electrical device.

Telmar are currently seeking dealers for the product. Further information is available from Telmar Communications, 604 City Rd, South Melbourne, 3205. Phone (03) 690 8666.

New chips for stepper motor control

Ellistronics now has available the new SGS L297 stepper motor controller and the L298 dual bridge driver, described as the "simplest, most compact and efficient way" to drive bipolar stepper motors.

Together with a few passive components, the two chips form a complete microcomputer-to-stepper motor interface with simple step and

direction inputs and drive capability of up to 200W. The combined unit directly drives motors at up to 2A and 46V per phase using a pulse width modulation scheme. Applications include carriage positioning in computer printers or control of machine tools, while for light duty applications the L298 can be replaced with the L293E, a dual bridge rated at 1A/36V per bridge.

For further information contact Ellistronics Pty Ltd, 797 Springvale Rd, Mulgrave, Vic 3170. Phone (03) 561 5844.

New test gear released by Neotronics

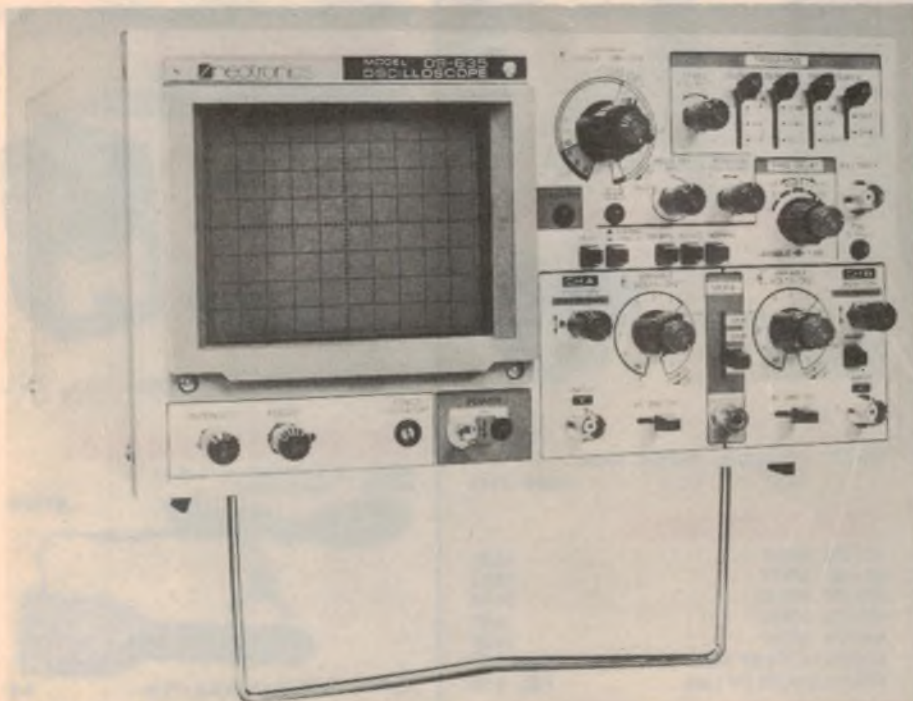
Neotronics now has available the Model OS 635 dual trace 35MHz oscilloscope with a 150mm rectangular tube providing an effective display area of 8 x 10 divisions (one division equals 10mm). The vertical deflection range is 5mV/div to 10V/div and can be increased to 1mV/div at reduced bandwidth. Four sweep modes are available: normal, auto, single and delayed trigger. In the delayed trigger mode a delay of from 100ms to 1μs is available.

Also available from Neotronics are the new Aaron model MM-220 and MM-230 3½-digit digital multimeters. The hand-held units feature automatic ranging on AC, DC and resistance, a diode test facility and audible continuity tester. Voltage measurement ranges are

from 200mV to 1000V DC and from 200mV to 750VAC. Resistance ranges are from 200Ω to 20MΩ and AC and DC current ranges from 200μA to 10A. Both models are based on a custom-made 80-pin LSI chip.

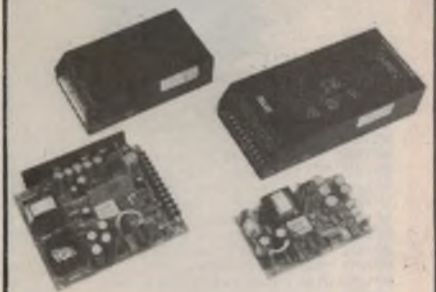
Overload protection is standard (except on the 10A range) and includes transient protection to 6kV. On the voltage ranges maximum input is 1100V while resistance ranges can handle a maximum 250V. Two type AA batteries are used to power the instruments, with typical battery life quoted as around 500 hours.

An 8-page catalog on the range of Neuberger panel meters is also available from Neotronics. Full specifications and pricing details are included in the manual. For details of Neotronics oscilloscopes, multimeters and other test equipment contact Neotronics, PO Box 289, Newport, NSW, 2106.



NEW! LOW COST SWITCHERS

Here is a range of switching power supplies for the budget conscious user. They are designed especially for micro to medium computer systems and use a series flyback design to provide multiple outputs.



Model	Outputs	Output	Max power	Price
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HSC40-31	5V 2.5A, 12V 2A, -12V 0.25A	open frame	40 Watt	\$60
HSC55-41	5V 6A, -5V 0.5A, 12V 2.5A, -12V 0.5A	enclosed	55 Watt	\$80
HSC75-32	5V 3A, 24V 2.2A, -12V 0.2A	open frame	75 Watt	\$95
HSC125-40	5V 10A, 12V 3.5A, -12V 0.5A separate 12V 2.5A	enclosed	125 Watt	\$150

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240V 15-30V 1A
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M21004	PL12/5VA 6.06V @ 0.42A	9.95
M21006	PL15/5VA 7.5 0.7 5V @ 0.33A	9.95
M21008	PL18/5VA 9.0 9V @ 0.28A	9.95
M21010	PL24/5VA 12-12V @ 0.21A	9.95
M21012	PL30/5VA 15.0 15V @ 0.17A	9.95
M21014	PL40/5VA 20.0 20V @ 0.1A	9.95
M21016	PL16/15VA	13.95
M21024	PL18/12VA 9.0 9V @ 0.67A	14.95
M21026	PL24/12VA 12.0 12V @ 0.5A	14.95
M21028	PL30/12VA 15.0 15V @ 0.4A	14.95

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M21038	PL30/20VA 15.0 15V @ 0.67A	17.95
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M21044	PL12/40VA 6.0 6V @ 3.33A	19.95
M21046	PL15/40VA 7.5 0.7 5V @ 2.67A	19.95
M21048	PL18/40VA 9.0 9V @ 2.22A	19.95
M21050	PL24/40VA 12.0 12V @ 1.66A	19.95
M21052	PL30/40VA 15.0 15V @ 1.33A	19.95
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M21064	PL24/60VA 12.0 12 @ 2.5A	26.95
M21066	PL30/60VA 15.0 15 @ 2.0A	26.95
M21068	PL40/60VA 20.0 20 @ 1.5A	26.95
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M21092	PF 3577 28.0 28V @ 2A	37.50
M21094	PF3783 35.0 35V @ 5.0A	79.95
M21096	PF3787	26.50
M21098	PF3788 30V, 27V, 24V, 18V, 6V @ 4A	47.50
M21100	PF3993 20.0 20V @ 1.5A	29.50
M21102	PF4244 16.0 16V @ 9A	53.50
M21104	PF4354	69.50
M21106	PF4361/1 35.0 35V @ 2.5A	47.50
M21108	PF4362 35.0 35V @ 4A	59.50
M21110	PF4363 47.0 47V @ 3A	59.50
M21112	PF4673	52.50
M21114	PF4405 9v @ 10A	49.95

A.C. PLUG PACKS

A.C. Plug Adaptor



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M21142	PPB8/1000 AC Plug Pack	19.95
M21144	PPB12/500 AC Plug Pack	19.95
M21146	PPA12/670 AC Plug Pack	18.95
M21148	PPA12/450 AC Plug Pack	18.95
M21150	PPC12/1250 AC Plug Pack	24.95
M21152	PPC18/830 AC Plug Pack	24.95

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M21182	AL7VA/9V 9V @ 0.77A	9.95
M21184	AL7VA/12V 12V @ 0.58A	9.95
M21186	AL7VA/15V 15V @ 0.46A	9.95
M21188	AL7VA/18V 18V @ 0.38A	9.95
M21190	AL7VA/24V 24V @ 0.29A	9.95
M21192	AL7VA/30V 30V @ 0.23A	9.95
M21194	AL7VA/40V 40V @ 0.18A	9.95



CONVENTIONAL

M21200	2150 6.3V @ 2.5A or 12.6V @ 1A	24.95
M21204	5502 22V @ 2.5A or 44V @ 1.25A	22.50
M21206	5503 17V @ 11.5V @ 4A	34.50
M21208	5504 15V @ 2A	14.95
M21212	5508 6.3 @ 4A or 12.6 V @ 2A	22.50
M21214	5578 Stepdown 115V 40VA	43.50
M21216	5579 6.3V AC @ 1A	7.95
M21218	5755 40V AC CT @ 2A	17.95
M21222	6625 25V AC @ 0.5A	9.50
M21228	7243 4 Tapes, 19V to 50V @ 2A	37.50
M21230	7309 12V AC @ 2.5A	17.50
M21234	7311 24V AC @ 4.2A	29.40
M21238	9585 240V AC-240V AC @ 1A	67.50
M21240	9789 240V AC-240V AC @ 2A	159.00
M21246	60202 7 Taps, 12V-30V @ 3A	34.50
M21248	60203 2X15-30V @ 2A	39.50
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M21126	MT620	9.95
M21128	MT627	14.95
M10216	1KCT/8 O/P Trans	1.00 0.90
M10226	500CT/8 O/P Trans	1.00 0.70

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BARGAIN PRICES AT ROD IRVING ELECTRONICS

New Products...

New switchmode power supplies

Scientific Electronics has released details of their newest power supply, the switch mode SM45AD1. Designed and manufactured by the company, the new supply has four output rails providing a total capacity of 45W.

Standard outputs are +5V at 4A, +12V at 1.5A, -12A at 0.5A and -5V at 0.1A, but output rails to customer specifications are also available. All outputs are protected against short circuits and the positive rails have over-voltage protection.

The SM45AD1 meets Telecom specification 1302 for test equipment, with isolation greater than 3.5kV and efficiency claimed as better than 70% at full load. Dimensions are 85 x 254 x 60mm. As with all power supplies from Scientific Electronics, the SM45AD1 is supported by a five year warranty and local technical back-up.

Scientific Electronics has also added to its range of "Invert-A-Lite" modules with new 18W and 36W units designed for low energy slimline fluorescent fittings. The new solid-state inverters are available to operate from 12V to 24V DC supplies and are fully encapsulated.



Features include screw terminals for easy installation, quick start, and protection against reverse polarity inputs or unloaded outputs. No ballast or starter need be used with the inverters.

Other inverters are also available with outputs of from 8 to 40W and input voltages from 6 to 110V (although some

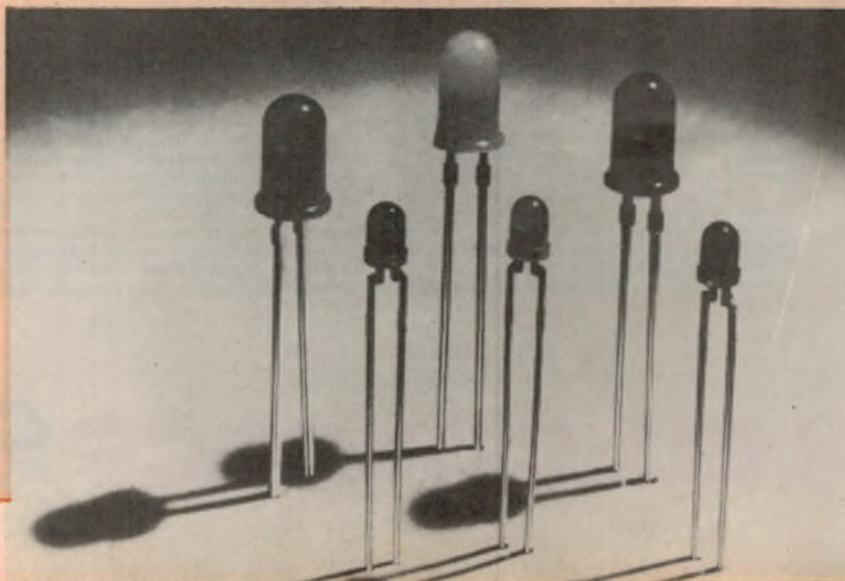
units are only available on special order). For further information contact Selectronic Components Pty Ltd, 25 Holloway Drive, Bayswater, Vic. 3153. Phone (03) 762 4822.

More LEDs with in-built resistors

Hewlett-Packard has expanded its range of resistor-LED lamps with 5V and 12V types, in T-1 and T1 $\frac{3}{4}$ packages, in high efficiency red, yellow, green and standard red. The LED's save space and cost because

they incorporate current limiting resistors as an integral part of the package. TTL and battery-operated circuits are particularly suitable for applications of HP's Series 1100, 1600 and 3100 and 3600 LEDs.

For further information contact Hewlett-Packard Australia Ltd, PO Box 36, Doncaster East, Vic 3109. Phone (03) 895 2895.



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Thanks,

Dick Smith Electronics

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STORE HOURS

All Dick Smith stores are open for trading during the normal trading hours for their particular area (either 9-5:30 or 8:30-5). Many stores are also open for late night trading. Please ring the store concerned for their particular hours.



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\$50.00-\$99.99	\$6.00
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DICK SMITH ELECTRONICS



New Products...

"Zip-on" tubing shields against RFI

Now available in Australia, Zippertubing jackets are flexible cable shields with a zip-lock closure, available in various materials for shielding wire and cables from electromagnetic interference. Standard cable coverings can be combined with a choice of shielding materials, either laminated or sewn inside the jacket. A tinned copper wire braid incorporated in the jacket allows easy connection of ground terminations.

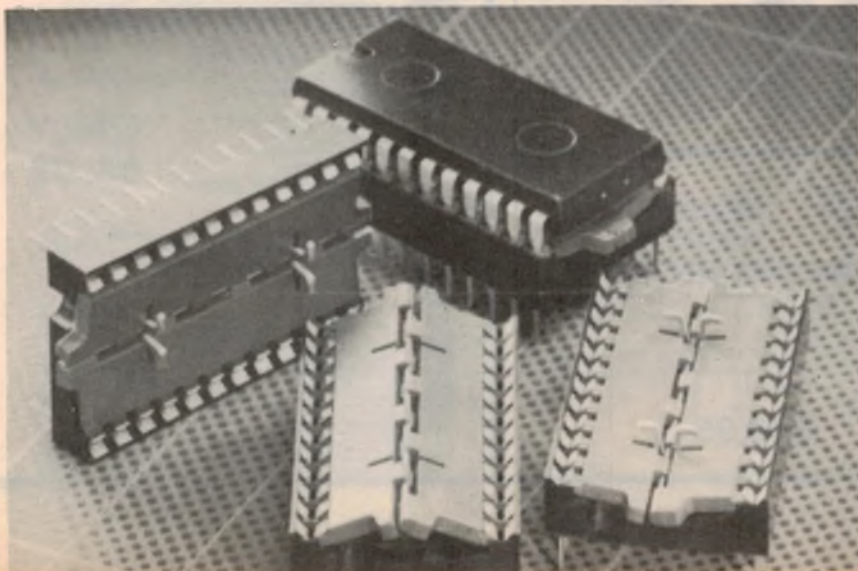
Suggested applications include shielding of cables in communications installations, computer systems and sensitive audio equipment from radiated interference, and the reduction of crosstalk between adjacent cables. The ease of installation of the shielding jackets means that equipment can be treated "in situ" immediately the RFI problem becomes evident.

Zippertubing jackets are distributed in Australia by the Adimex Trading Company, PO Box 219, Ringwood, Vic.

Zero insertion force IC socket

Mayer Krieg & Co now has available what is claimed to be the world's first "No Insertion Force" IC socket with dimensions conforming to standard sockets. Compatible size means that the NIF socket can be used in place of ordinary sockets without changing the board layout. High density layouts can be achieved by laying the low profile sockets side-by-side.

The NIK socket is based on a



Optical power meter checks lasers

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Ando also has available a chopped Light Power Meter and a range of electro-optical converters and LED light sources for optical power measurement applications.

Further information is available from Paton Electronics, 90 Victoria St, Ashfield, NSW, 2131.

hinged, locking top plate. In use, an integrated circuit is placed on the socket so that it comes to rest on two centrally mounted spacers. When the tabs at the ends of the socket are pressed down the lockplate is activated and clamps the socket contacts against the pins of the chip. No force is exerted on the IC until it is correctly positioned in the socket.

NIF sockets can be supplied in 24, 28, 40 and 48 pin sizes. Further information is available from Mayer Krieg & Co, GPO Box 1803, Adelaide, SA, 5001. Phone (08) 233 6766.



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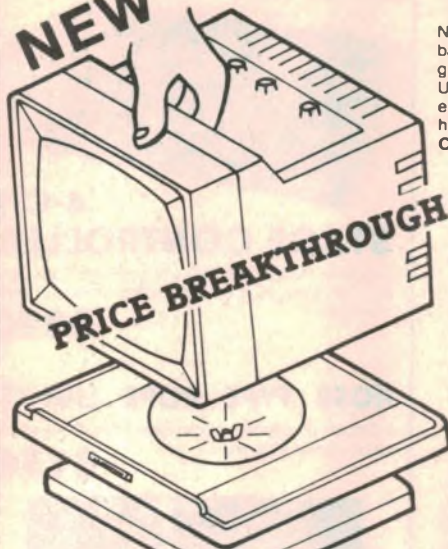
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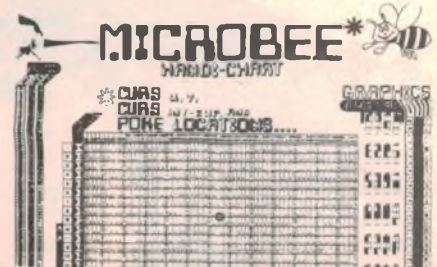
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This fantastic Microcomputer was reviewed in ETI Oct 1982. They were very enthusiastic about it, the printer and its legal Apple software compatibility (around 90%). If you always wanted an Apple but just could not afford it, this could be a fantastic opportunity to get the nearest thing at a fraction of the normal price!!

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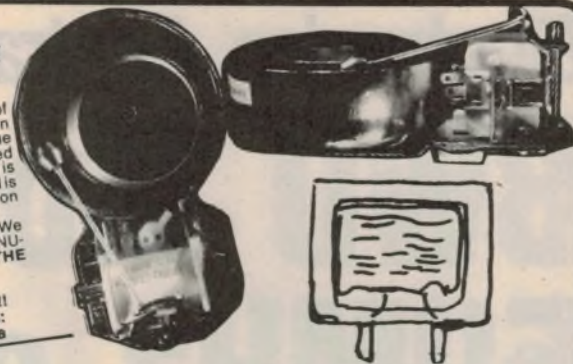
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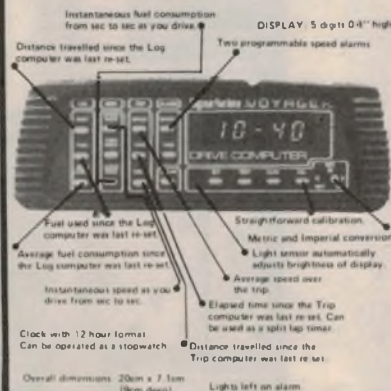
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Electronics Australia reviews the **BWD Model 821** **50MHz oscilloscope**

Recently released by BWD, the Model 821 is an Australian-made CRO that offers excellent value for money. Features include 50MHz bandwidth, dual trace operation and comprehensive facilities.

by JOHN CLARKE

Right from the outset, we were impressed with the Model 821 50MHz oscilloscope from BWD Instruments Pty Ltd. BWD is an Australian company that, over the years, has built an enviable reputation for high-quality test equipment. This new CRO will do nothing to tarnish that reputation.

In fact, it makes a welcome change to review an item of electronic test

equipment that is of Australian manufacture. As this review will show, the Model 821 is highly competitive when compared to its imported rivals, both in terms of finish and performance. It has all the features of the imports and offers a few more tricks besides.

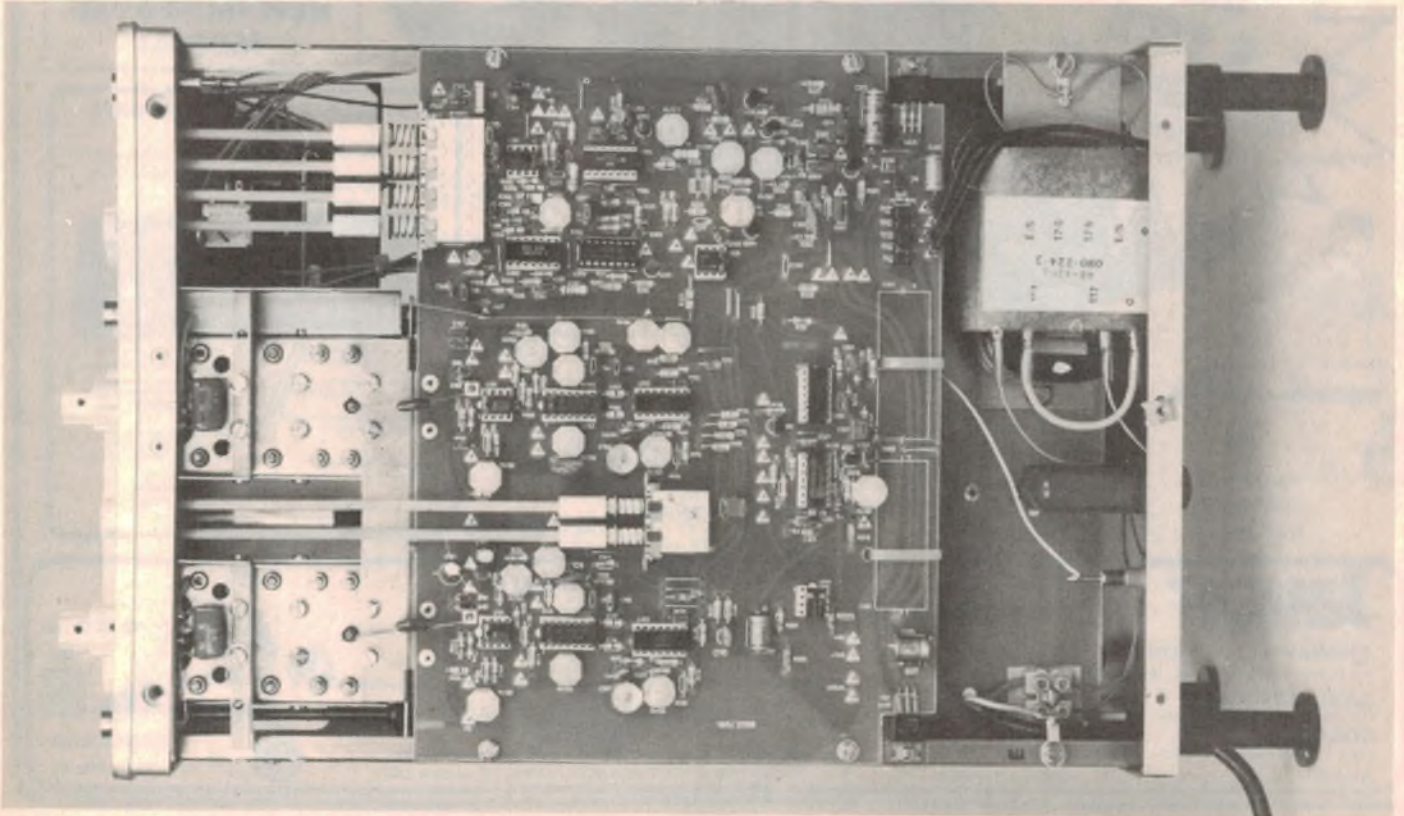
At first glance, the Model 821 looks much the same as its rivals although the green highlights used in the colour

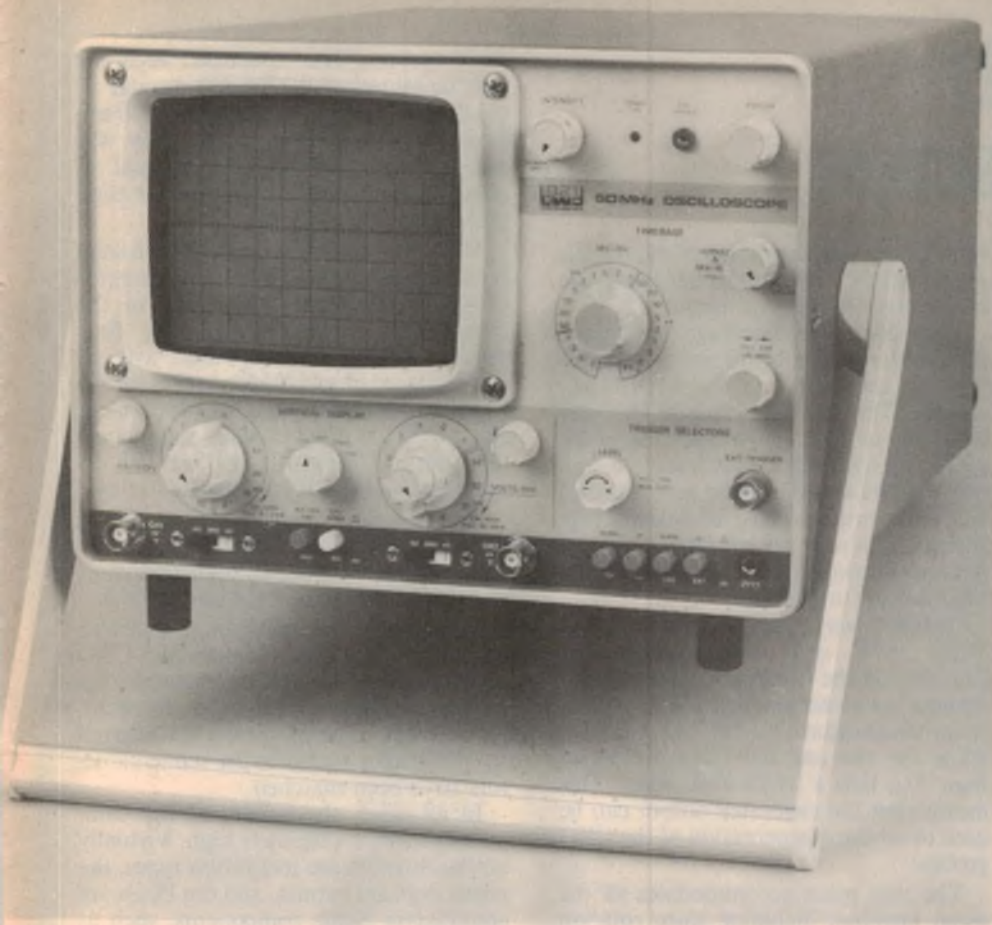
scheme are a little unusual. The unit measures 250 x 430 x 178mm (W x D x H) and is supplied complete with an instruction manual and two P32 100MHz probes. With most CROs, probes are an optional extra.

The front panel is very well laid out. It has an uncluttered appearance and there is ample room between the controls for easy finger access. As is the fashion these days, the vertical sensitivity controls are mounted directly beneath the CRT (cathode ray tube) while the timebase control is mounted to the right.

The CRT is a blue phosphor PDA (post deflection acceleration) type fitted with an internal 10 x 8 division graticule (1 division = 9.5mm). Internal graticules are now virtually a standard feature on

View inside the BWD Model 821. The standard of construction is excellent.





new CROs and have the advantage of eliminating parallax error when taking readings. In addition, this unit features 10, 90 and 100% markings on the CRT face to assist in determining pulse rise and fall times.

The quality of the on-screen trace is exceptional. We have yet to see a trace as fine and as clear as it is on this CRO.

The vertical sensitivity controls comprise the usual 5-2-1 stepped attenuators, each covering the range from 20V to 5mV/division. In addition, concentric variable attenuators with detented calibrate positions extend the input signal range to about 50V/division. By pulling the concentric knobs, the sensitivity is multiplied by 5 to give a minimum input sensitivity of 1mV/division.

The 20V/division position is useful for observing the full 250VAC mains waveform when using a divide-by-10 probe. When displaying mains waveforms in this way, both channels can be comfortably accommodated on the screen. This is the first CRO we have seen with this capability and is a feature that we like.

Another excellent feature is the complete lack of DC shift when switching from one setting to another. This is due to the fact that the attenuators are ahead of the preamplifier stages. In some imported CROs, part of the attenuation is carried out after the

preamplifiers. While this is a simpler method (it reduces the number of compensation components needed), it can cause a DC shift on the trace when switching from one setting to another.

In addition to the attenuators, the vertical channel controls comprise the vertical position controls; input coupling switches (AC, GND, DC); a mode selector switch (CH1, CH2, ALT, CHOP and ADD); and finally a pushbutton switch to invert CH2. This last feature converts the ADD facility on the mode selector switch so that it subtracts CH2 from CH1.

Trigger selection

Trigger selections can be either INTERNAL or EXTERNAL. For INTERNAL, either CH1 or CH2 can be selected as the trigger source or, alternatively, the mains frequency can be used for triggering as selected by the NORM/LINE switch. When the EXTERNAL position is selected, triggering is initiated by a signal applied at the EXTERNAL TRIGGER input.

For all types of inputs, selection can be made for + or - slopes and NORM/TV triggering. The Trigger level can be adjusted with the LEVEL knob and either AUTO or manual triggering is available by pulling this knob for non-auto.

For the TV trigger selection, there is a video sync separator circuit which gives

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BWD Model 821 50MHz oscilloscope

automatic frame lock for timebase settings between 0.1s to 100 μ s and line lock above 50 μ s/division. One very useful feature of this circuit is that it will also demodulate a modulated carrier, enabling the envelope to be displayed. This will be handy when working on VCRs, colour TV receivers and other video equipment.

Timebase calibration is in 21 steps in a 1-2-5 sequence from 0.2 μ s to 1s/division. The horizontal position switch provides a x10 magnification of the trace when pulled out. This extends the trace calibration to a minimum .02 μ s/division.

At the extreme clockwise setting of the timebase control is the XY position. This converts CH1 to Y and CH2 to X (the vertical and horizontal axis respectively) and allows Lissajous displays for phase and frequency comparisons of two waveforms. For this to be effective it is important that the X and Y amplifiers show minimal phase shift with frequency. The 821 excels here by phase shifting less than 2° from DC to 200kHz.

MIX-MAG control

To the right of the timebase control is the VERNIER and MIX-MAG (mixed magnification) control. When the control is pushed in, it operates as a rotary vernier and reduces the timebase speed by at least 2.5 times at its maximum setting. When the control is pulled out, the MIX-MAG facility is engaged and the timebase is locked in its calibrated position.

The MIX-MAG control has a rather unusual effect on the waveform. When the control is fully clockwise, the timebase is displayed with normal x1 magnification. If, however, the control is

rotated, the right hand side of the trace is magnified by 10 while the left hand side of the trace remains at normal x1.

In practice, the percentage of the trace displayed at x10 magnification is dependent on the setting of the MIX-MAG control. This can be varied all the way from 0% to 80% of the trace for sweep speeds up to 2 μ s/div. This feature is unique to BWD oscilloscopes and is useful when the extra expense of delayed triggering facilities is not warranted. It also has the advantage of being easier to use than delayed triggering.

Another very useful feature is the 1kHz 0.5V p-p calibrated output available on the front panel. This output voltage has an accuracy of 1% at normal room temperatures (+15°C to +35°C), while the rise and fall times are better than 5 μ s into a 1M Ω /40pF load. This means that the calibrated output can be used to set the compensation of the CRO probes.

The rear panel accommodates all the usual facilities, including trace rotation and astigmatism screw adjustments, Z modulation input, and timebase gate output. The Z modulation input requires about +4V to blank the trace at normal intensity, while the timebase gate output is 0V during the sweep and +3V during blanking.

Test results

We measured the bandwidth of the Model 821 as 3dB down at 50MHz, which is right on specification. The waveform was usable right up to 95MHz at which point the oscilloscope had problems with triggering. In the XY mode, CH2 has a bandwidth of 1.5MHz.

In general, the 810 offers excellent

performance. The timebase accuracy was measured at 0.32% for normal x1 settings and 0.68% for x10 and x100 settings. Vertical calibration accuracy was measured as 1.5% for both x1 and x5 gain. These figures are far better than those specified by BWD.

We were also impressed with the solid construction and well engineered interior of the BWD Model 821. Most of the components are mounted on four separate printed circuit boards, with all ICs mounted in sockets for ease of servicing. For the most part, the component types used are quite familiar and include 4000 series CMOS ICs, LF351/353/356 op amps, and CA3086 transistor arrays.

The diodes and transistor type numbers are also familiar and are supplied by a National Semiconductor, Fairchild, Motorola, RCA and Philips.

In fact, with the exception of specialised parts such as the switches and CRO tube, virtually all the components are readily available in Australia. Even so, service requirements should be referred to BWD since many of the semiconductors have been matched.

In all cases, the quality of the components used is extremely high. Virtually all the resistors are metal film types, the preset pots are cermet, and the PCBs are epoxy glass. Some components, such as the power transformer, beam rotating coil, converter transformer and CRT shield, are specially manufactured by BWD for the Model 821.

The two P32 probes are also of good quality and incorporate x1, GND and x10 settings. Several special tips are provided with the probes and include the standard hook, a BNC plug and several plastic fittings. These latter are used to shroud the probe tip so that it may be applied directly to an IC pin without the danger of shorting onto adjacent pins.

Finally, the service manual supplied with the Model 821 is very well written. It describes the various controls, measurement techniques, adjustment and maintenance procedures, and lists the full specifications. And unlike many of its competitors, BWD give the purchaser a full set of circuit diagrams, together with a written circuit description and PCB layouts.

To summarise, at \$850 + 16% sales tax it would be difficult to find a CRO to equal the performance of the Model 821 from BWD. Its excellent specifications and original features make it highly competitive, both in Australia and overseas.

An additional upmarket model is also available from BWD: the 60MHz Model 835 (with delayed triggering) for \$1550 plus sales tax.

For further information contact BWD Instruments Pty Ltd, Miles St, Mulgrave, Victoria 3170; or 10 Euston St, Rydalmere, NSW 2166.

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INSTRUMENTS

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BWD's Model 821 oscilloscope is a dual-trace unit with 50 MHz bandwidth, 1 mV to 20 V per division sensitivity and a special 'mix-mag' expanded trace function

The mix-mag facility, unique to the BWD 821, enables you to get a 10 times magnification of any proportion of the trace from 0% to 80% simply by pulling and turning a knob.

Normal x10 magnification is incorporated and the trace can be expanded to x100 using the mix-mag function to provide facilities similar to a delayed sweep CRO but without the complexity.

The mix-mag facility can be used to magnify each line to examine teletext, sync pulse or video signals of VCRs, television receivers or studio equipment.



821 50MHz MIX-MAG

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Other features of the BWD 821 include: a 7ns rise time from 5 mV/div., 20ns/div maximum sweep speed, 75MHz triggering, TV line and frame triggering selection, bright trace with 6kV EHT and internal tube graticule.

Two 100MHz probes are included, a x1 and a x10. High sensitivity vertical amp inputs enable low level signals to be viewed, such as from tape recorder heads, pickups and microphones, etc.

The BWD 821 is suited to use in communications, industrial control, research and development, video and microprocessor applications.

Designed and manufactured in Australia by
BWD Instruments Pty. Ltd.

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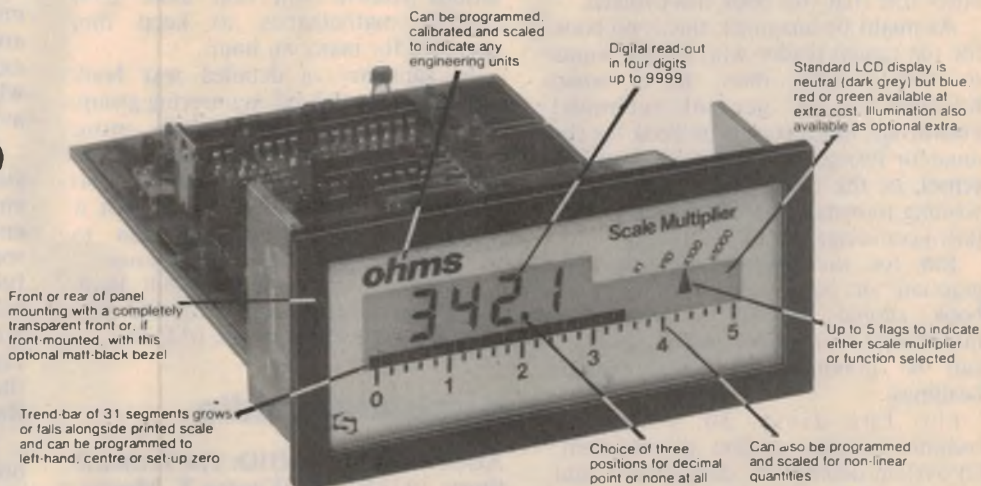
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Satellite communications

MANUAL OF SATELLITE COMMUNICATIONS by Emanuel Fthenakis. Published 1983 by McGraw-Hill Book Company, USA. Hard covers, 351 pages, 228mm x 145mm, illustrated with photographs and diagrams. ISBN No. 0 07 022594-X. Recommended retail price \$71.85.

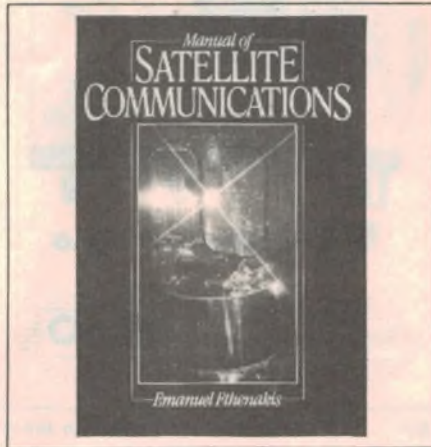
This is an in-depth text book aimed at communication engineers faced with the need to upgrade their background to encompass the commercial communication satellite scene. In view of the impending establishment of Australia's own satellite system, AUSSAT, there may well be those in the Australian communications scene who require a text book of this type.

The author is senior vice president of Fairchild Industries, with responsibility for the space, communications and electronics group. Previously he worked at Bell Laboratories, General Electric's Space Division, the Philco-Ford Space Division (as founder and director), and the American Satellite Company. He also teaches a graduate level course in space and communications at the University of Maryland. It is from this latter role that this book has evolved.

As might be imagined, this is no book for the casual reader who simply wants to add a little more to a broad background of general technical knowledge; in short, it is no book for the amateur (using the word in its broadest sense), or the cattle station handyman wishing to install a satellite antenna and down-converter for TV reception.

But for the engineer, involved in graduate or post-graduate studies, the book should contain a wealth of information. Some idea of the coverage can be obtained from the chapter headings.

(1) The first 20 years of communications satellite development; (2) System description, deployment, and cost; (3) Orbits, launch sequence, and positioning on station; (4) The communications spacecraft; (5) Spacecraft communications system; (6) Earth stations and terrestrial links; (7) The space communications link; (8) Linear systems and signals, summary of



fundamental principles; (9) Random processes and noise; (10) Analog modulation; (11) Digital communications; (12) Coding and forward error detection; (13) Transmission impairment; (14) Networks and systems; plus five appendices.

The author claims that, for various practical reasons, "... the depth of presentation has had to be limited in some cases." And, "Since there are several excellent references... I did not attempt to deal with these (certain) subjects with strict mathematical rigor." In spite of this we feel sure that the serious student will find more than enough mathematics to keep him occupied for many an hour.

In summary, a detailed text book aimed at a specialised engineering group, for whom it will undoubtedly prove extremely valuable. Unfortunately, the high price may deter some students who might otherwise benefit from it, but it would make an useful addition to technical college and similar libraries.

Our copy from McGraw-Hill Book Company Australia Pty Ltd, PO Box 239, Roseville, NSW 2609. (P.G.W.)

Australian radio

AUSTRALIAN RADIO: The Technical Story, 1923-83. By Winston T. Muscio. Published 1984 by Kangaroo Press, Kenthurst, NSW Australia. Hard covers, 137 x 220mm, 243 pages. Some illustrations. ISBN 0 949924 82 2. \$19.95.

The author of this new book,

Winston Muscio, has been a long-time personal friend of this reviewer, with interests in common at both a personal and a professional level. I was delighted when he told me of his plan to do what many in our generation have contemplated but few have actually attempted: namely to set down the history of Australian radio as they have observed it — in this case over a period approaching 50 years.

He does so as an Associate in radio engineering of the original Sydney Technical College, a member of the Institution of Engineers (Aust) and a senior member of the Institution of Radio and Electronics Engineers (Aust).

Significantly, while he pursued his wide-ranging career mainly in the formal engineering and administrative environment of STC, Winston Muscio remained an enthusiast at heart, reading widely and always ready to discuss technical subjects outside his everyday activity. It was not surprising, therefore, that during the preparation of the book, he spent a considerable time chasing up references and going through file copies of "Wireless Weekly", "Radio & Hobbies" and "Electronics Australia" to refresh his memory of past practice and past events.

His book opens with a general survey of broadcast receivers and broadcast reception through the years (chapters 1 & 2) and of Communication Receivers (chapter 3). The emphasis is on trends rather than statistics or specific models.

Chapters 4 to 8 inclusive cover Broadcast Transmitters, Communications Transmitters, Mobile Radio Systems, Multiplexed Communications Systems, and Integrated Radio Communications Systems. All of these were areas where the author acquired special expertise in the STC/ITT Group, but which are not well understood by the average enthusiast.

In chapters 9, 10 and 11, the author steps out of his role as a formal radio engineer, to be revealed as an audio enthusiast from way back and as someone who spent an interim period full-time in the audio industry. The subjects here are: Audio Frequency Reproduction, Record Playing Equipment (from early phono pickups to the compact disc) and Magnetic Tape Recording Equipment.

There is final comment on FM broadcasting in Australia, the patent situation over the years, a brief bibliography and a comprehensive index.

The book has been very carefully compiled and is well written by an author who has considerable natural ability in this area.

It should make fascinating reading for



all who have been involved in — or been observers of — the technical side of Australian radio. But, more than that, it is a book which can round out the background of a younger generation of engineers and students, giving them a feeling for what has gone before.

“Australian Radio — The Technical Story” should be available through technical and university booksellers but, if necessary, inquiries can be directed to Kangaroo Press Pty Ltd, 3 Whitehall Rd (PO Box 75), Kenthurst, NSW 2154. In the latter case, remit \$19.95 plus \$1.50 to cover pack and postage. Recommended. (W.N.W.)

MicroBee applications

WILDCARDS by R.A. Burt, P.T. Ford and A. Nallawalla. Volumes 1 & 2. Published 1983 by BF&N Publishing, Williamstown, Vic. Soft covers, 210 × 278mm, 100 pages (Vol. 1), 120 pages (Vol. 2). Illustrated with charts and tables. ISSN 0811-577X.

Sub-titled “A potpourri of applications notes and tips for the MicroBee Personal Computer”, these two volumes were written by a group of three Melbourne MicroBee users who pooled their experiences and resources to produce the books.

Volume 1 has six chapters covering general programming style and tape handling, sound and music, utility programs, graphics, games and printers. Twelve appendices are also included with illustrations of graphics characters, aids to the creation of programmable characters, routines for cursor positioning, a blank table for records of the user's program variables, Microworld Basic tokens, a memory map and hex, decimal, binary and ASCII conversion tables.

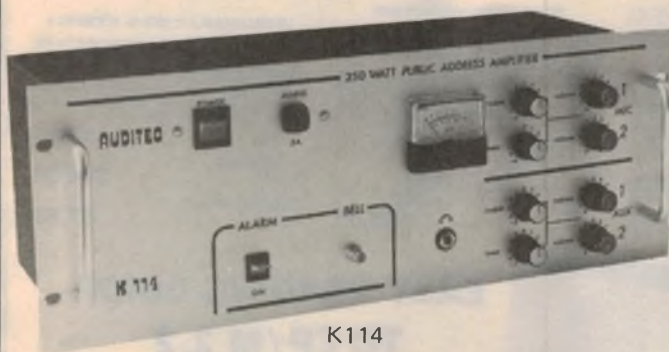
Throughout the book each point discussed is illustrated with example programs and helpful charts and

diagrams. The sections on graphics, music and games alone make Volume 1 worthwhile, but the inclusion of useful utility routines and general advice to users adds further value.

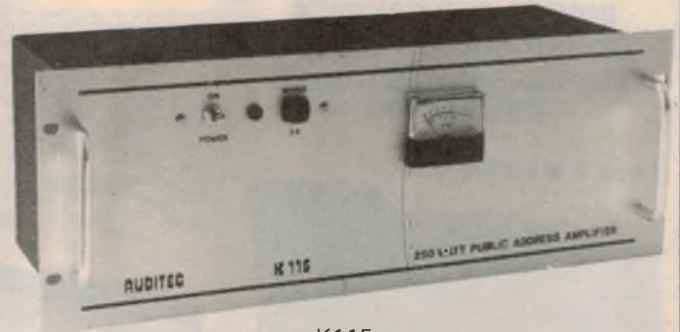
Volume 2 continues the theme with sections on machine language, sorting, more utility programs, conversions from other versions of Basic (including the NOS-BASICODE broadcast over shortwave by various European stations), more graphics techniques, games programs and peripherals, including disk drives. Four appendices are provided covering Microworld equivalents to other versions of Basic, printer control and escape codes, a seven page memory map (very detailed) and a questionnaire on the reader's preferences for Wildcards Vol. 3!

This volume is slightly longer than the previous book but the material is all new. Colour is also dealt with for the first time. Both these books are designed for “intermediate level” readers who have worked through the MicroBee manual and would like to go further. Together they contain a wealth of information for the MicroBee user in a clear and understandable style. Our review copies came direct from the publisher, but some retailers have the volumes, at around \$15 for Vol. 1 and \$16 for Vol. 2. (P.V.)

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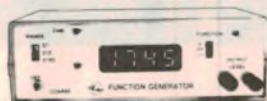


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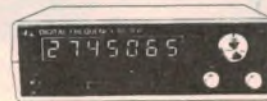
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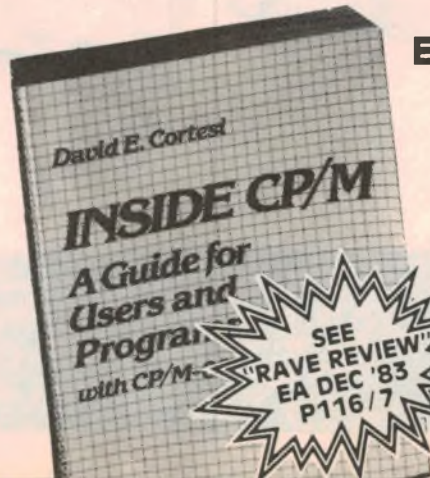
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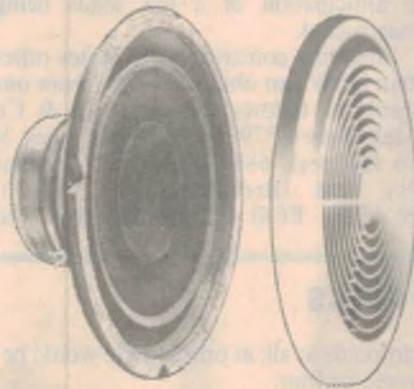
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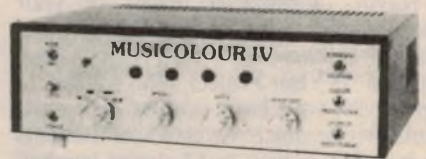
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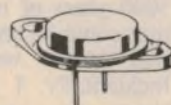
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P 0568	20 Pin	.30	.25	.20
P 0569	20 Pin	.50	.45	.42
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Letters to the editor



Circuit voltages

Having constructed many of your projects over the years I was intrigued to read your article in the April issue entitled "If Your Project Won't Work". I agree with your basic precept, that most faults will be due to reversed components or incorrect values, but I almost laughed out loud when I read your advice to check voltages.

When has *Electronics Australia* ever published a kit design that identified, on the circuit diagram, the voltages that might be expected at various points? Note that I disregard such blindingly

basic voltage references as shown in the 1982 Function Generator schematic accompanying the article.

Lest I be accused of singling one magazine out, your competitor in Australia does not fare any better in this regard. And all this despite the fact that, given a working sample, such values could be established within 10 or so minutes, preferably with a cheap multimeter such as a hobbyist is likely to use.

B. Alison,
Mona Vale, NSW.

PS: Otherwise a great magazine.

Dummy load

Further to your article on the high power dummy load in the April issue, I would like to make the following points: (1) Everest Electronics is the Australian agent and importer of Arcol metal clad wire wound power resistors.

(2) Mayer Krieg & Co (NSW) are our NSW agents and the resistors used in the dummy load were supplied through them. The NHS100 8R resistors are a

stock line but the NHS100 4R units were specially ordered and supplied free for your use. We have a small stock on order in anticipation of a few loads being constructed.

Intending constructors in states other than NSW can obtain resistors from our agents as follows: Mayer Krieg & Co (Melbourne), 579 5722; Mayer Krieg & Co (Sydney), 684 1900; DGE Systems Pty Ltd (Broadmeadow, NSW), 69 1625; ECQ Electronics Pty Ltd

Video fires

I am writing in regard to the letters I have seen in your magazine concerning fires in TV sets and video cassette recorders. We own a VHS video recorder which is kept in our lounge room where it is out of the sun. On several occasions last summer the temperature reached 30°C and, in three instances the VCR switched itself on, placed itself in the record mode, and promptly started to record. On each occasion, the on/off switch was in the "off" position.

If it is possible that the switch is affected by heat enough to turn the unit on, or there is some other fault, then this type of machine may pose a major threat to the public. In the case of a short circuit, a fire may start or a shock could occur. At any rate, it is quite annoying to have a tape, with the record protect tab removed, erased by a faulty video. How about some projects for CB and amateur radio operators?

S. Lamshed,
Bairnsdale, Vic.

(Brisbane), 376 5677; Prospect Distributors (Perth), 362 5011; Anelco Electronics Pty Ltd (Adelaide), 294 2600.

R. Sedunary,
Everest Electronics,
Seaford, SA.

Problems with compact discs

In a recent editorial you defended, rather strongly, the compact disc system. Certainly, I have encountered the derogatory comments about compact discs which may well have been prompted by a vested interest in traditional LP disc equipment and the sale thereof.

However, contrary to your assertion, I am not convinced that all is yet as it should be with CD players. There may also be some problem with the discs themselves, although I am inclined to believe this is minor.

Late last year I bought a compact disc player. Although the sound quality and absence of background noise were all that I expected there were two problems. One was the dropping of the first few notes on a particular disc in rather more than 50% of starts. The other was random dropouts, probably averaging about one per disc but not necessarily on any one disc or on every play. Sometimes there would be no

dropouts at all; at others there would be three or four.

A complaint was promptly met by the manufacturer with an offer of a replacement unit which was accepted. The first problem mentioned above no longer occurred; no dropped notes after many, many starts. On the other hand, the incidence of dropouts (albeit of shorter duration) was increased about tenfold. While there was some variation in the average number of dropouts between discs, not one disc (of about 12) would ever play through without at least 3 or 4 dropouts while the highest number recorded for one disc was 27.

In the light of the comment in *Electronics Australia* about a year ago to the effect that one dropout in about 5000 years of normal playing was all that could be anticipated I felt satisfied that there was still a problem. Incidentally, I am more inclined to blame the player than the discs

because, although there is a variation between discs, the dropouts never occur twice in the same place and there was a very large difference in performance between the first and second players.

A further complaint to the manufacturer resulted in a visit to my home by the Service Manager to verify my complaint. Having satisfied himself on that score, a third unit was installed while the problem was referred back to Japan. This unit is perhaps the best so far although it has a few funny tricks of its own. Ultimately I expect I will end up with a unit which performs properly.

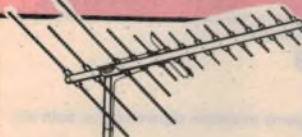
The whole thing is puzzling. I have not been aware of dropouts when CDs have been played on ABC FM. On the other hand I find it hard to believe that I am the only person to experience three faulty players.

Any comments you might care to make would be much appreciated.

A. Marsh,
South Turrumurra, NSW.

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Get ready for the Games!

Combined UHF/VHF antenna

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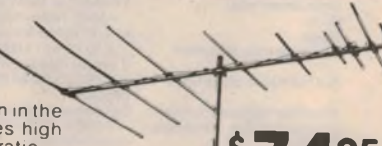
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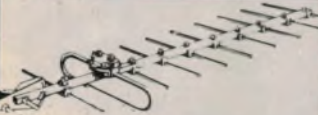
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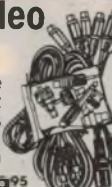


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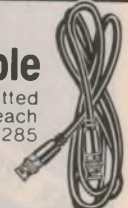
Now is the time to get your TV antenna system in tip-top condition... the Games start in just a few weeks. Wouldn't you be popular if...



Video to Video Cable Set

2m audio/video cable with phono plugs at each end. Adaptors to suit UHF (PL259), BNC, 6.5mm, 5 pin DIN & 6 pin DIN. **\$49⁹⁵**

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2m 75ohm coax fitted with BNC plugs each end. Cat W-1285


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Deluxe Video Processor

You won't believe the difference an enhancer makes to your video tape copies. Restores fine detail, lifts signal above noise level has inbuilt RF modulator so you can use with standard TV set.

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75 ohm TV Cable

2m 75ohm coax fitted with standard TV coax plugs. Cat L-4506

\$3²⁵




Mast Head Amplifier

Ideal for fringe areas. Designed to suit Australian TV & FM characteristics.

Cat L-4200 **\$49⁹⁵**

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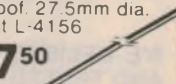
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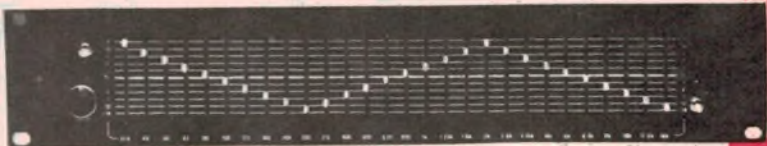
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REVIEWS OF RECENT

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SHOSTAKOVICH — Concerto No. 1.
KABALEVSKY — Cello Concerto No. 1.

Yo-Yo Ma (cello) with the Philadelphia Orchestra, Conducted by Eugene Ormandy.
CBS Masterworks Digital Disc D37840.

Two very different kinds of cello concertos are offered on this very well produced digital disc. The Shostakovich is a very serious work that needs knowing to be fully appreciated. Yo-Yo Ma, a 28 year old Paris born Chinese, starts the first movement with a typically cheeky Shostakovich tune, cello and orchestra beautifully mated.

The soloist and conductor both show the hands of masters and the digital processing is very clear and sharply recorded. The result is almost like a close-up of the music.

It is taken in the strictest time and I often found myself in my mind's eye marching to it.

The second movement is very luscious though the Philadelphia's strings lose a little of their gloss under the close-up of digital scrutiny. Ormandy, who uses the same strict treatment as in the first movement, loses a little of its lyricism in consequence. The main theme, cold at first, grows on you more and more as the movement goes on.

But the missing lyricism enters when Yo-Yo's cello sings out. His playing is peerless and the brilliantly scored orchestra is always in perfect balance. They blend together in a process Brillat-Savarin might well have called osmosis.

Towards the end the sound grows more compressed and the very high solo passages sound so far off key that they might be quarter tones.

But on the whole the movement is very lovely, different entirely from the jocose first one. There is a long cadenza treated with sensitive lyricism by Yo-Yo with a compelling crescendo built to fortissimo proportions by the player at speed.

Yo-Yo treats the daunting difficulties of the Finale with outstanding brilliance and at breathless speed. This has easily followed logic, and refers back cyclically to the first movement with here and there a hint of Stravinsky.

The Kabalevsky is much more accessible. Of lighter weight it sounds quite mellifluous after the Shostakovich. It starts with an easy swinging gait that makes great demands on the soloist. The engineering has the same close-up style of the reverse side with Yo-Yo's precision echoed everywhere in the orchestra. The second movement, marked *largo*, goes at much more like a *moderato tempo*. The composers' two styles couldn't be more different yet both are firmly Russian. Any sensuous sound is swept from the orchestra, leading to a long cadenza-like passage in meditative mood. The ending is full of charm.

The finale (*allegretto*) has the same easy-running style as a prelude to a faster strong Russian style that has the feet dancing. The movement runs along like a happy girl. Later, it is taken at a speed and clarity reminiscent of the old Heifetz finale to the Mendelssohn E. Minor. (J.R.)

CHOPIN

Waltzes No. 1 to 14. Claudio Arrau (piano). Philips stereo disc 9500 739.

One might be forgiven for thinking that a simple form like the waltz would have precluded any exercise of deep thought. Yet simple as it is, it has an astonishing number of different moods and styles. One has only to recall such variants as Liszt's Mephisto Waltzes, the Viennese Waltz, the serious and the flippant examples and finally this collection of Chopin.

One only has to hear the difference



between the Rubinstein performances and these of Arrau to appreciate this. One thing they share in common is an aristocratic style. Otherwise their readings are very different indeed. And much of this is due to the nature of Chopin's inspired writing.

The differences are striking right from the very first waltz recorded (and incidentally the first Chopin published), Op.34. Here Rubinstein's style is characteristically elegant; Arrau's is slower and much broader with fuller tone.

In Op.34 No.2, Arrau's darker mood is sharply contrasted by Rubinstein's brisker treatment. So, right at the beginning of the record, there is a difference between Rubinstein's salon elegance and Arrau's considerable delving into the construction of the pieces which, under his magic fingers, differ bewilderingly while always remaining true waltzes.

I must apologise here for the different spelling used in naming these pieces. Chopin used the French version *Valse*, but it is customary when discussing the form in English to use the German form *waltz*. I have tried to rationalise the problem but quite without success.

Op.42 is probably the finest of all these pieces (14 in all) and Arrau interprets it on a wider scale than his competitor, though Rubinstein suffers in no way by comparison. Perhaps the best example of the two artists' idiosyncracies is to be found in the C Sharp Minor *Valse* in which we have Rubinstein in typical mood and Arrau at his most meditative. Either versions of these delicious waltzes

should please everyone, but both would be better. (J.R.)

RACHMANINOFF

Symphony No. 1. Concertgebouw Orchestra conducted by Vladimir Ashkenazy. Decca digital disc SXDL 7603.

This symphony might be briefly described as a composer's love affair with the minor mode. But it is never lugubrious. At its first performance it suffered the fate of so many promising first pieces by a young composer — ridicule and condemnation.

Glazounov gave a disgracefully bad performance, not even taking the trouble to hide his dislike, so much so that the young (22) composer accused him of drunkenness. He had edited the symphony and made many alterations which it must be admitted were usually improvements. At any rate, young Rachmaninoff was so discouraged by its reception that he wrote nothing for some three years afterwards.

The recording is digital and some loss of lusciousness in the strings is compensated for by increased clarity of the scoring that otherwise tends to become congested. You won't hear any of the sensuous melodies you do in the piano concertos, though they are hinted at in plenty. After a rave introduction, the work continues very turbulently. The plainsong *Dies Irae* is featured — how often Rachmaninoff introduces it into its later works — and the splendid clarity of articulation at very fast speed in the cellos and basses is a joy. A very Russian-sounding second subject foreshadows the juicy tunes that will come later in the concertos and other works.

Next follows a fugato at great speed, faster than I have heard any other conductor take it — and none the worse for it. This leads to extended turbulence, played here with meaning and some pain. Ashkenazy has great panache and ease of manner in his handling of the very many abrupt changes of tempo. And the engineering provides a wide range of dynamics carefully not overdone. The second movement is scherzo-like but with some troubled Mendelssohnian speed. It is all enjoyable, the technique assured, with most of the movement so soft that loud bits bring with them some surprise.

The third movement is a larghetto which displays the promise of the composer's slow theme style with much reliance on the minor scale and some commonplace modulations from it and some decidedly not. The mood darkens

and remain sceptical. Ashkenazy shows much passion in the long quiet stretches and makes the whole very easy to listen to.

The stirring opening of the finale goes with splendid control of the many changes of syncopated rhythms. This is stunning playing at an exciting speed with the conductor pushing it along exuberantly. One can imagine his hair streaming in the wind he creates. But behind it all is exemplary refinement. Major struggles against minor in a stirring finish. Highly recommended. (J.R.)

HANDEL

Music for the Royal Fireworks. Water Music. The Academy of Ancient Music on authentic instruments conducted by Christopher Hogwood. Oiseau Lyre Stereo Disc DSLO 595.

The Royal Fireworks Music was written to celebrate the end of the War of the Austrian Succession. When it was arranged to hold the ceremony in the Green Park, and make a martial sounding outdoor affair of it, Handel first chose for his orchestration 16 trumpets and 16 French horns. George 2nd had also expressed the wish that there should be "no fiddles" and that oboes should be substituted. Handel disapproved of this, however, and later added "fiddles" and reduced the number of oboes and trumpets.

The Orchestration finally decided on consisted on 24 oboes, 12 bassoons, contra bassoons, nine horns, nine trumpets, side drums and three sets of timps. Serpents were also included but later removed from the score.

However, at the rehearsal everything went wrong. With 101 brass cannon, fireworks going off at the wrong time or failing to go off at all, rockets falling among the crowd, and a splendid pavilion that was to be the set piece catching fire, not much of the music could be heard.

The only conductor I know who tried to capture the original grand sound was Charles Mackerras many years ago on a Pye disc. He modified the first orchestration by using 26 oboes, 14 bassoons, four contrabassoons, two serpents, nine trumpets, nine horns, three timpanists and six side drums. And a grand row it all made.

The rehearsals took place in London after 11 o'clock at night, this being the only time that all the musicians needed would be free from engagements elsewhere. Anyway, they all loved it and made a joyous din and Mackerras told

me last year that Pye were thinking of re-issuing it.

Hogwood makes a fine fist of it using the present day compromise orchestration. At any rate, his music has an "authentic" sound, something like characteristic Handel. The problems caused by the recreation of Handel's first thoughts are more closely resembled by the Mackerras version but, in the meantime, the present one under review will do nicely.

The Water Music receives an excellent performance too, and I can recommend this disc as an entirely worthy compromise. But if the Pye re-issue of the Mackerras performance eventuates don't hesitate to acquire one. (J.R.)



STRAUSS

Eine Alpensinfonie (An Alpine Symphony); Richard Strauss. Herbert von Karajan conducting the Berlin Symphony Orchestra. DG compact disc 400 039-2.

The Alpine Symphony was composed between the years 1911 and 1915, with most of the actual orchestration being completed within the final three months. According to the booklet, Strauss did not particularly enjoy the task, although he saw the work as something of a musical tour-de-force, requiring an orchestra of 135-odd players, an organ, a wind machine and other possible effects.

Essentially a symphonic poem with a single movement lasting for just on 51 minutes, the Alpine Symphony describes a mountain-top climb, probably of the Zugspitze, which towered above the Strauss villa in the Bavarian Alps.

The work divides into 22 melodic episodes. It opens with the mountain shrouded in darkness ("Night") — barely audible strings: this is followed by "Sunrise", dramatic — and noisy! Then comes "The Ascent", followed by "Entering the Forest" . . . and so on to

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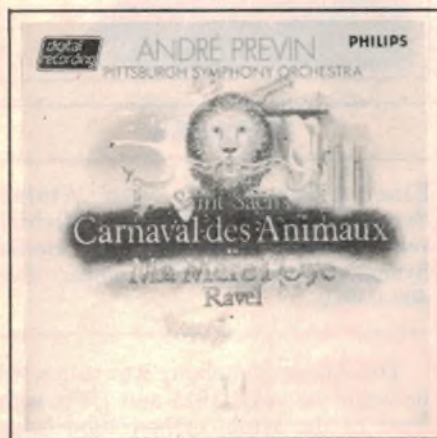
the complex emotions as the climbers reach the top: "Precarious Moments", "On the Summit" and "Vision".

The return journey is essentially the climb in reverse, except that it is interrupted by a fierce storm, complete with wind machine! But the storm subsides, the sun sinks from sight and an evening "Epilogue" ushers in another "Night".

The Berlin Philharmonic plays magnificently and Karajan's direction is equally notable. Some may feel that the climb has been scaled to epic proportions but this would be a quibble rather than a real criticism.

What I found really disappointing was the sound quality of the disc arising, I believe, from the difficulty of recording such a large group. Unless I miss my guess, DG engineers have relied too heavily on multi-miking and "spotting", leading to a confusion of sound, from which the violins in particular emerge in a quite strident fashion.

In short, the performance is fine but, by compact disc standards, I found the sound disappointing. (W.N.W.)



SAINT-SAENS, RAVEL

Carnaval des Animaux (Saint-Saens). Ma Mere l'Oye (Ravel). The Pittsburgh Symphony Orchestra conducted by Andre Previn. Philips compact disc 400 016 2.

Listening to Saint-Saens' Carnival of the Animals, I couldn't help but feel that this Philips release would be a worthwhile inclusion in any new domestic compact disc collection, where children (or grandchildren) are involved. To complement, say, Prokofiev's "Peter and the Wolf", Saint-Saens 14 miniatures depicting animals and what-nots would

provide the basis for a diverting and meaningful exercise in identifying orchestral themes.

The booklet which comes with the disc lists the subjects in this "Grande fantaisie zoologique" and adds a few jottings about the orchestration, which are probably sufficient for this popular and very transparent item. It's a fun performance.

By contrast, and despite its name, Ravel's "Mother Goose" suite sounds quite formal and the playing possibly does err in that direction. But it's a very competent performance, nevertheless.

My real quarrel is that the booklet notes on this "beautifully orchestrated" half-hour suite are lamentably brief — a mere 10 lines of English-language text, plus a list of six related ballet scenes — in French! It underlines an obvious problem in relation to compact discs produced for the European market: if you have to accommodate three languages in the usual small booklet, you can't say much in any of them!

A further point is that, with its potential for tuition and its 20 distinct subjects (14 in "Carnival" and 6 in "Mother Goose") the disc is a natural subject for detailed index and/or time encoding but there is no hint in the booklet of any such provision having been made. As far as the CD player is concerned, it simply registers two tracks and that's that. A pity!

The recording itself is fine, however and if the contents appeal, you can buy with complete confidence. (W.N.W.)

DEVOTIONAL

Restoration. A Prayer in Music for the Church. As expressed by Evie and Pelle Karlsson. Stereo LP Word WSB-8906. [From Word Records Aust, 18-26 Canterbury Rd, Heathmont, Vic 3135. Phone (03) 729 3777].

The devotional songs on this new album, all but one composed by Evie and Pelle Karlsson, reflect a strong personal faith and a deep concern of the Authors for the Christian Church — not for bricks and mortar but for the congregation of worshippers. Instead of the usual jacket notes, there is "An open letter to Christians everywhere", explaining their convictions.

In a program that runs for almost 40 minutes, Evie and Pelle present 15 of their songs, interspersed with occasional scripture quotations: Restore Your



Temple — Nehemiah's Prayer — Seek Me — Be Still and Hear — Sing to The Lord — Lord Most High — Your Glorious Throne — Rejoice and Sing — Touch Your People — Sanctify Yourself — Let There Be Fellowship — Jesus' Prayer — Authority — We Are The Church — Sanctify Yourself.

Featuring male and female vocal leads, Pelle and Evie Karlsson, chorus, organ and instrumental, the music should find wide acceptance — modern enough to appeal to a younger audience but not to the extent that would alienate the "oldies".

The lyrics appear in full on the liner and can be followed through from track to track. While the sound itself is good, the album should appeal to anyone whose interest goes beyond the mere music to the message which it carries. Have a look and a listen. (W.N.W.)



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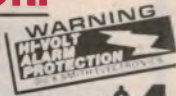
A real loud fire bell is great for scaring them off, too. This one is 12V operated, draws just 300mA and can be heard blocks away! Cat L-5280

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STOP PRESS
Just arrived: Swiss made Passive Infra-Red detector - top quality, no false alarms!
Cat L-5010 **\$119.00**

EXCLUSIVE

Your Home is on the 'hit list' - your valuable property maybe the gleam in a crooks eye tomorrow! You need help!!!

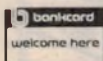
Here it is: our specially written guide to installing a fully professional alarm system - and it's free with any purchase of \$1.00 or more for June only! That's right: every home now needs protection - and we'll show you how to install an alarm that will deter even the most persistent pest.



FREE!

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See page 108 for full address details

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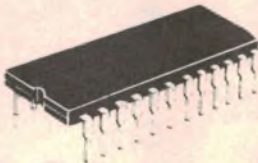
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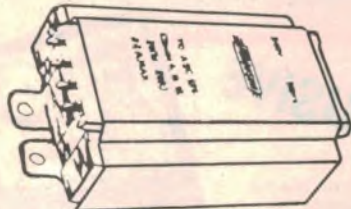


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1489	7107
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Records & Tapes

Whittaker and an oh-so-gentle orchestral accompaniment arranged by Chet Atkins.

My first reaction to the opening track was that Roger W is not as young as he used to be and that he was finding it just that much more difficult to match the flowing melody of the accompaniment. But the impression soon passes and a mood of relaxation takes over, which is obviously what Whittaker and Atkins had in mind.

In short, if you're a candidate for the greying generation, this is music to read by or knit by.

There are eight tracks on side one: Lara's Theme — Unchained Melody — Making Believe — Scarlet Ribbons — Red Sails in the Sunset — Red Roses for a Blue Lady — Red River Valley — Vaya Con Dios. Side two has 11 more but, without trying to list them all, they finish up with: "Eternally", "Tenderly" and "Stranger on the Shore".

Quality is no problem, if only because the even (who said "wallpaper"?!) sound obviates any worries with dynamic range. As I said: pure nostalgia! (W.N.W.)

POPULAR/CLASSICAL

Posh. Stereo LP. From Arika Records, PO Box 2, Pymble, NSW 2073.

The unlikely group name "Posh" is said to be short for "People of Sydney Harbour" but I'd take some convincing that it isn't a colloquialism to describe a

trio who, in part anyway, have their feet in the world of jazz, pop and rock, and their heads in the Conservatorium and the Opera House.

The basic group comprises:

Jane Rutter — flute, graduate of the Sydney Conservatorium High School, soloist with the Sydney Youth Orchestra, Sydney Symphony Orchestra, associate of the Australian Chamber Orchestra and lecturer at the Conservatorium.

John Huie — guitar and vocals, trained at Conservatorium High School, active composer, founder of two rock bands, studying overseas.

Hugh Fraser — double bass. Studied piano and clarinet at the Conservatorium High School, but became addicted to bass, studying and playing here and overseas, in the context both of classical and jazz.

Associated with them on this album are four other named players, playing cello, violin and congas.

The program is a mix, if ever there was one: "Lazy", humorous comment; "Can

You Imagine", a tribute to John Lennon; "Blackbird", adapted from Lennon-McCartney; "Terpsichore", "Go To Your Room" and "Gay Paris", classical/jazz fusion; "Telemann Vivace F Minor" and "Bach Bourrees", classically inspired; and others.

John Huie provides the novelty and variety with vocals and guitar but the whole program is tied together by the magnificent flute (and Piccolo) of Jane Rutter, and Hugh Fraser's no less magnificent bass. This is not loud music, because they rely on clarity and intimacy rather than amplification.


Posh has immediate and universal appeal and it is of no wonder that they are in such demand locally; or that they were invited to represent Australia in New York, at the International Off Broadway Festival, with other US engagements to follow.

Recorded at the Alberta St Studios and mixed at Sun Studios, the quality is first rate, with a very clean sound in the top and middle register and enough energy from the double bass to make your woofers wonder what hit them! Don't pass this one up because of the odd name! (W.N.W.)



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Simple One Hole mounting — no more expensive panel cutouts, brackets.

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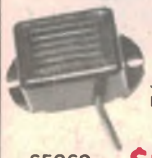
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Z0155.....	22c	19c	15c

MINI BUZZER 1.5-5V DC

SENSATIONAL LOW PRICE

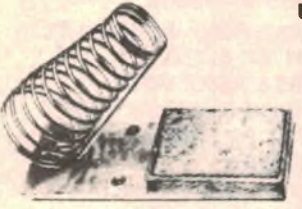
Handy little solid-state audio "Buzzer" or signalling device. Just the shot for communicator panels, or for timer alarms or in the car. Polarity conscious.



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Large Ferrite Magnet.
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Great for hobby projects.

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Dual Z 4/8 OHM
3 Watt RMS
Mounting hole centres
at 82mm.

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3 watt 8 OHM
Mounting Holes at
71mm centres.

C 0612... **\$4.75**
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3 Watt RMS
Mounting holes at
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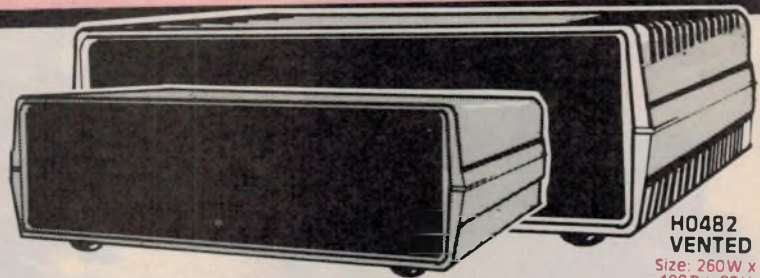
— naturally you won't have a clue as to whether they've got the items you need available. And of course, be prepared to wait, wait, patiently wait sometimes for weeks!
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H0480
Size: 200W x 160D x 70H

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Micronews

Apple IIc portable released



Apple Computer has released its second new product of the year, the Apple IIc portable, launched at the end of April. The IIc is a miniaturised, portable addition to the Apple family and is compatible with most of the vast range of software for the Apple II machines.

The basic unit consists of a 3.5kg keyboard console with a single built-in 13cm mini floppy disk drive, an external power supply pack and an RF modulator to enable the system to be used with a domestic TV receiver. A specially designed video monitor is also available, and a flat panel, 80 column by 24 line liquid crystal display (LCD) will be introduced for the IIc later this year, according to Apple.

Other features of the system include the use of the 65C02 CMOS version of the 6502 microprocessor, 128K bytes of RAM as standard, selectable 40 or 80 column text display (with video monitor) and three colour graphics modes (40 x 48 in 16 colours, 280 x 192 in 6 colours and 560 x 192 in 6 colours). A built-in sound generator and loudspeaker allows sound effects and music over a range of five octaves.

A range of new peripherals and software for the Apple IIc has also been announced, including a plain paper thermal printer, a "mouse" cursor positioning device, a modem, an external disk drive and a carrying case. The existing Apple joystick, hand controllers,

Imagewriter printers and Colour Plotter can also be used with the IIc.

To enable the new user to quickly learn how to use the IIc, Apple is including 20 hours of disk-based training in the form of an "interactive user's manual/computer literacy course" with each computer. "It's everything you need to get started in one box", says David Strong, managing director of Apple Computer Australia. "This allows consumers to buy, set up and use the system right away. The miniaturisation of the IIc architecture has resulted in a serious small computer that people can easily take from the home to the office or school and back again."

The Apple IIc will run most software written for the Apple II and IIe. The Apple programs that are incompatible are those which use non-standard copy protection and memory allocation schemes, and those which require the use of the CP/M operating system.

In fact, the "all-in-one" design of the IIc provides two RS-232C serial ports and a port for an external disk drive but no general-purpose expansion slots. There is no provision for a battery power supply making the IIc a "transportable" version of the Apple II rather than a challenger to "knee-top" computers such as the TRS-80 Model 100.

Price of the basic Apple IIc with one disk drive is \$1,775 including sales tax and an RF modulator.



Computer work-station from Meyertronix

Meyertronix has introduced a three tier computer work station called the "Computable" which is supplied as an easy to assemble kit. Features of the unit include three large shelves on an aluminium frame (available in a range of colours) and castor legs for moving the table about. Recommended retail price is \$199 (including sales tax).

Further information is available from Meyertronix, PO Box 65, Riverstone, NSW, 2765. Phone (02) 627 2510.

Software support for TI-99/4A

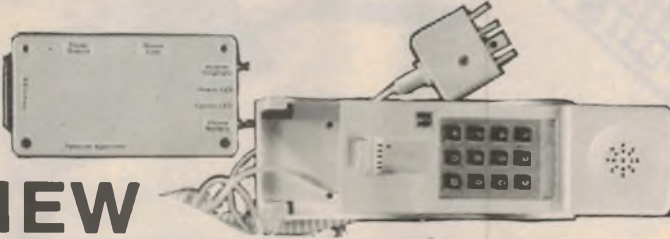
Imagic Australasia has joined forces with Texas Instruments to provide ongoing support for the TI-99/4A home computer. Since April, Imagic has been providing Australia-wide marketing and distribution services for TI software and peripherals for the 99/4A.

"Texas Instruments' policy is to provide long term support for the TI-99/4A" says Imagic's managing director Chris Milner. "We will have available the entire TI software range and will be carrying sufficient stock to support the system for over three years."

For further information contact Mr Don Dennis, Imagic Australasia Pty Ltd, PO Box 234, Dee Why, NSW, 2099. Phone (02) 981 2744.



1984 - BIG BROTHER MIGHT BE LISTENING... BUT WOULD YOU LIKE TO TALK BACK!



NEW AVTEK MINI MODEM

Possibly Australia's smallest Telecom approved (pending) MODEM. The **MINI MODEM** comes complete with a phone so that all you have to do is remove your standard phone and plug-in the **MINI MODEM**. It is so small that you can mount the **MINI MODEM** on the skirting board next to the phone socket and use the Modem phone all the time as your standard phone.

SPECIFICATIONS: ★ 300 Baud CCITT V.21 answer or originate full duplex ★ Power indicator LED ★ Carrier detect LED ★ Answer/originate switch ★ Modem/phone switch ★ Plug pack power supply ★ Size approximately 65x130x40mm overall - SIMPLE AND SMALL!!

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THERMISTOR SPECIAL 56R Philips type
2232-660-91009 - refer to Philips Catalogue for specs.
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SPECIAL - 1793 DISC CONTROLLER
WAS \$45.00 THIS MONTH ONLY \$25
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9" DISPLAY MONITOR FOR YOUR COMPUTER - GREEN (ORANGE) DISPLAY - ONLY \$279.00

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Designed for sanding - grinding - polishing - cutting - engraving - drilling - milling - erasing AC adaptor supplied

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This is for the hobbyist and is not approved for connection to Telecom lines. It is ideal for private line use and for the Amateur Radio operator for Packet Radio (See review EA January 1984). Complete kit to the last nut and bolt including pre-punched and silk-screened front and back panels.

ONLY \$249.00
MODEL MM2

This is a completely assembled and tested unit with a telephone hard wired into the Modem. It can be plugged legally into any phone socket to replace your standard phone

INTRODUCTORY PRICE \$329.00
MODEL MM3

This is basically the same model as MM2 but does not include the telephone but comes fitted with a data Telecom plug which means a dedicated socket must be installed by Telecom.

CONTACT AVTEK FOR PRICE
MODEL MM4

This unit is basically the same as model MM3 but does not have externally selectable Baud rate. The mode of operation is factory set. This is ideal for dedicated dial-up lines. This model also has hardware Auto Answer included.

CONTACT AVTEK FOR PRICE

SPECIFICATIONS FOR KIT, MM2, MM3 and MM4: □ Data Standards CCITT V.21 & V.23, Bell 103 & 202 □ Data Rates 300, 600 and 1200BPS □ Backward Channel 75BPS in conjunction with 1200BPS □ Computer Interface CCITT V.24 (RS232C) □ Power Requirements 240V AC 3 watts □ Front Panel Controls Mode Switch (12 position rotary - not MM4) Connect Switch (3 position toggle) Test Switch (3 position toggle) □ Front Panel Indicators Connect LED, DCD Data Carrier Detect, RXD Received Data, RTS Request to Send, CTS Clear to Send, TXD Transmit Data, RING Ring Detect, TEST Test Switch off normal, POWER NOTE: Models MM2, MM3, and MM4 will not be available until Telecom approval has been obtained.

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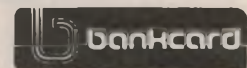


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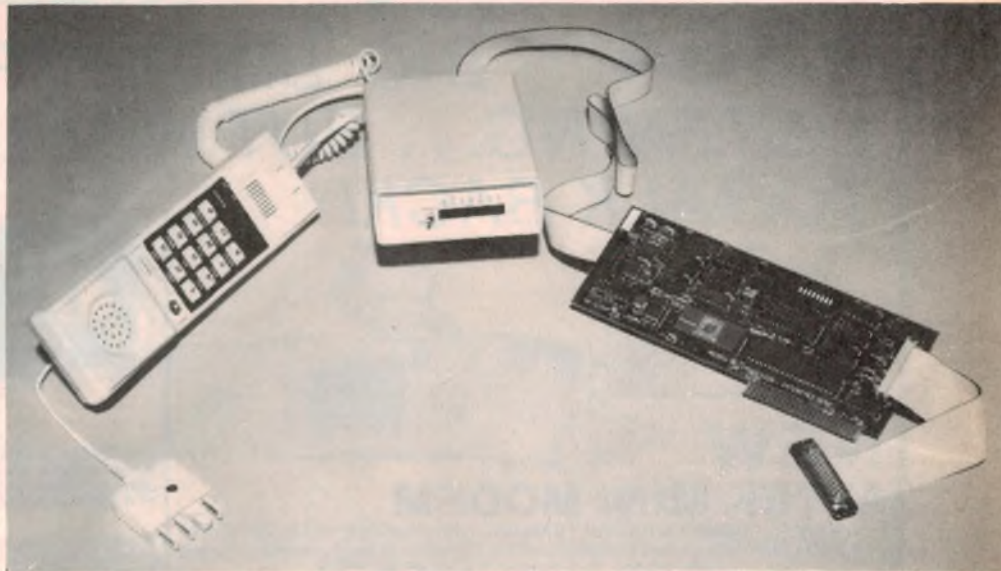
Micronews

Apple modem from NetComm Australia

NetComm (Australia) Pty Ltd has released a wholly Australian designed and built multi-function modem for Apple computers. The modem is the first in a range of modem communication products from the company and features Auto Dial, Auto Answer and Auto Disconnect facilities.

The unit can be preset with a series of hardware switches but can be re-configured under program control to provide either 300 baud asynchronous full duplex, 1200 baud synchronous half duplex or 1200/75 baud asynchronous Prestel formats. Thus the modem can be used to connect an Apple computer to virtually any remote computer service, including Prestel videotext, IBM 3270 systems, DEC, Prime and Wang minicomputer terminals, Dow Jones, The Source or CSIRONET.

Both CCITT (Australia) or Bell (USA) transmission standards can be supported, with the modem controlled by an on-board microprocessor with its own RAM and EPROM. A Telecom approved slim-



line phone handset is supplied with the modem and can be used for voice conversations or manual dialling. Automatic re-dialling is built-in.

The Auto-dial facility allows user programs to automatically establish a connection with their chosen data dial-up service, and the modem can be left in "auto answer" mode and will automatically alert the Apple program of an incoming call.

NetComm will also supply their Apple software package under a "third party developers" licence to allow the modem routines to be integrated into applications packages. Demonstration programs are currently available.

For further information contact NetComm (Australia) Pty Ltd, 8/33 Ryde Rd, Pymble, NSW, 2073. Phone (02) 498 5577.

Computers assist small business award winner

Systems and support supplied by a Commodore dealer have been a "large contributing factor" in the success story of one of the winners of the prestigious National Small Business Awards.

Paul Wright is a retired ballet dancer turned cobbler whose Brisbane-based company is one of only two national award winners from Queensland.

His company — Paul Wright Pty Ltd — makes a full range of dance shoes, including ballet and ballroom, and casual footwear. What started off as a "back of the garage" hobby 16

years ago, has today become a thriving concern, employing 50 people and producing 550 pairs of shoes a day.

Paul went computerised in July 1982 choosing a Commodore computer, one megabyte disk drive and 132-column printer from the 8000 Series.

Hardware was supplied by Commodore dealer Austcomp which also supplied Paul with standard Commodore accounting systems plus a specially written job-costing program.

"Our needs at that time were considerable," says Paul, "we had no costing control up to then and this was reflected in our profits.

"But from obtaining the systems, the company did a real turnaround."

Paul began his business purely as a hobby while touring with the Australian Ballet Company. Today his ballet shoes are used by dancers of both the New Zealand and Norwegian Ballet Companies and he has made shoes for women in the Queensland, Victorian and ACT police forces.

"I have always been ambitious but I would never have believed we could grow to such a degree and win this award," he says.



When is 180 CPS faster than 200 CPS?

When you have this little beauty on hand. **Through-put speed** is what counts: C.Itoh's new low profile dot matrix printer is a high speed performer, prints out with a throughput of 100 LPM (draft mode with pica character).

You'd expect to lose visual quality? No way! C.Itoh's print resolution is sharp, defined, unbeatable — throughout the print head's 100 million-plus character life.

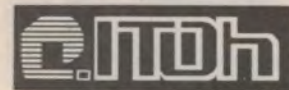
8510S is rugged, sturdy as it is fast, built to take the punishment with heavy duty castings and high quality metal parts throughout. Plastic parts are all high stress.

It's a colourful character: there's even a colour model which gives you up to seven colours, with high resolution graphics of 144 x 160 dots per square inch on all models.

And if you want to use all the features

of your IBM personal computer, C.Itoh has two special versions designed just for the IBM PC.

So make sure you ask the **throughput** of your new printer. And take a close look at C.Itoh. It answers all the questions.



For further information contact your Warburton Franki Data Products office.

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WF/RB1/84

MULTI SAVINGS!



NEW!

LCD Digital... it's the one with the lot!

Everything you've ever wanted in a multimeter
...and then some!

- ★ Semiconductor junction test
- ★ Hfe check for both NPN & PNP
- ★ Inbuilt buzzer for continuity
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- ★ 10A AC & DC ranges
- ★ 30 ranges
- ★ 0.5% accuracy

PLUS huge LCD display with auto polarity, low battery indication...all for less than \$150!! Isn't it time YOU updated your multimeter? Cat Q-1500

Includes a sturdy case for extra protection!

\$149⁹⁵

Amazing low price!



No tool case is really equipped... without an

LCD Multimeter

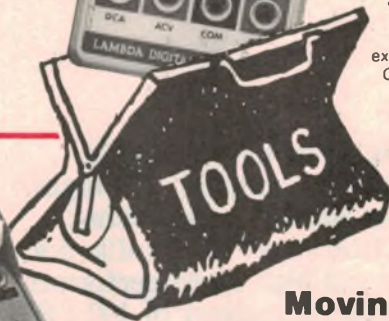
Where else but Dick Smith's could you find a quality digital LCD multimeter at this incredibly low price? We've cut no corners with this precision instrument. Features push button range selection, large 13mm LCD display, bench stand for easy reading, diode check facility and overload protection. With its 10A DC range, the Q-1444 represents excellent value for money! Complete with test leads and full instructions. Cat Q-1444

\$59⁵⁰

Budget Priced Moving Coil with Continuity Test!

A compact, reliable multimeter with an added bonus: a built-in buzzer for continuity testing! Also has a battery checker PLUS 10A DC range - not normally found on low-priced multimeters! On top of this, you get a high sensitivity (20,000 ohms per volt) meter mirrored scale and large banana plugs for sure contact. Cat Q-1022

\$29⁵⁰



Our Biggest Seller!

Almost a complete test bench in one package - no wonder it's our best selling multimeter! With 100,000 ohms per volt sensitivity and ranges to cover every test set-up, this outstanding meter is all the average hobbyist will ever need - and it's just as much at home on the service bench or in the lab! Measures transistors Ico and Hfe for both NPN & PNP (also good for diode testing) and has an inbuilt transistor oscillator for capacitance measurement. Cat Q-1140

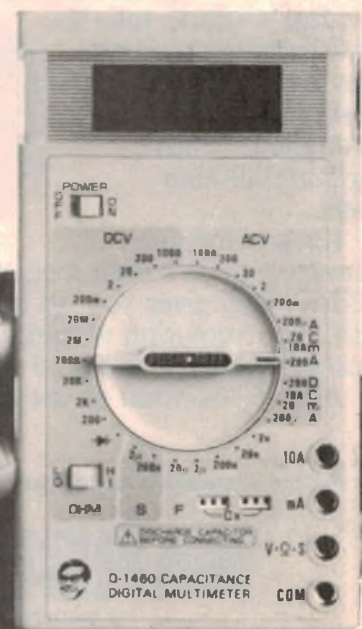
\$76⁵⁰

LCD Multimeter... that measures capacitance!

Yes! It not only features the normal ranges found on digital multimeters, it also has five ranges of capacitance checking, two ranges of conductance AND a diode check position! All this in a very accurate (less than 0.25% on DCV) and high impedance (10Mohm) instrument that is good enough for the designer's test bench, but has a low enough price for the hobbyist. All this plus overload protection, automatic polarity, 2.5cm LCD digits - and measurement to 10A AC & DC. Cat Q-1460

- ★ 32 ranges
- ★ Up to 1kV & 10A AC & DC
- ★ Capacitance, diode & conductance too!
- ★ Auto polarity

\$99



DICK SMITH ELECTRONICS



(See page 08 for address details)

A 763/GT

RMIT launches computer clearinghouse

The Royal Melbourne Institute of Technology has attracted 16 local and internal international computer companies to its Australian Micro-computer Industry Clearinghouse (AMIC), launched in April.

The Clearinghouse offers micro-computer owners, operators and potential users a range of services including access to hardware and software for evaluation, staff assistance and a variety of short training courses. Mr Don Schauder, the general manager of the Clearinghouse, predicted that the centre would appeal to individuals and businesses looking for somewhere to try out computers and peripheral equipment without sales pressure.

"As we don't sell computers, people using AMIC can be assured of total impartiality" he said. "People can book time on any of our machines for \$6 an hour. For students, the fee is \$3. Where the assistance of one of our 30 demonstrators is required, the hourly rate is from \$20".

AMIC already has an extensive range of hardware and software including the Tandy range of business computers, DEC Rainbow and Decmat and Hewlett-Packard's HP-150. Control Data has installed a CC638A microcomputer and ICL has three of its model 15 systems on display. Cromemco is represented by Insystems, and Futuretronics is expected to install six of its Atari computers at the centre.

Australian manufacturers, whose participation is sponsored by the Department of Science and Technology, are represented by Case Communications, Datacraft, Digital Electronics, Hartley, and SME. Other Australian firms will also be offered space.

AMIC occupies a suite of offices in Gateway Plaza, in Swanston Street, opposite the Royal Melbourne Institute of Technology and is open on weekdays and Sundays. Courses are conducted on most days, including 1½ hour breakfast sessions on specific products. Special programs on Sundays cater for family groups.



Pulsar Electronics expands

Pulsar Electronics Pty Ltd, the largest manufacturer of STD bus computer systems in Australia, has won status as a preferred supplier to the Victorian Education Department.

Pulsar Electronics manufactures a range of computer equipment, from single-user stand alone machines to Turbodos equipment designed for over 20 users. The company, which recently moved into larger premises at Tullamarine, also manufactures a range of ancillary STD boards to complement the Little Big Board which forms the heart of all Pulsar systems. These boards include a 256K RAM card, auto/dial auto answer modem board, hard disk interface, Turbodos slave processor boards, a six channel serial interface and four and 12-slot STD bus motherboards.

The company began trading in 1980

and developed various microcomputer products including display signs and a single board Z80 computer. In 1981 a project commenced to provide a high performance general-purpose computer, ultimately resulting in the Little Big Board.

All Pulsar products are 100% "open" with full details available on software and hardware. The flexibility and expansion possibilities of the Little Big Board in particular have made it a favourite with other computer manufacturers who base complete systems around Pulsar's board. Local support and manufacture means that products and assistance are readily available, without the problems of dealing with overseas suppliers.

Further information on Pulsar Electronics products is available from John Reardon at PO Box 10, Tullamarine Vic. 3043. Phone (03) 330 2555.

Commodore moves into IBM PC-compatible market

Commodore International Ltd, perhaps the most successful computer manufacturer in the home market, has made a significant move into the business area with the acquisition of an MS-DOS IBM PC-compatible portable computer. Previously the company has held off becoming involved with the IBM bandwagon, relying on sales of the VIC 20 and Commodore 64.

Commodore accomplished its bold shift of position with just two strokes of a pen, signing licenses to manufacture the Bytec Hyperion PC-compatible portable and to become a second source supplier of Intel's 8088 chip microprocessor, the heart of all IBM PCs and "workalikes".

The Hyperion, reviewed next month, is a substantially IBM compatible "transportable" computer with built-in

screen and dual disk drives. Commodore's acquisition of manufacturing licences places it squarely in IBM's market area.

Nor will the company be bedevilled by the chip shortages which have affected all manufacturers of IBM PC compatibles. One of the reasons for Commodore's profitability is that it makes all components for its own computers, including the 6502 and 6510 8-bit microprocessors. The second-source agreement with Intel is a major coup for Commodore, allowing the company to move into the 16-bit area with the same assurance of supply of vital components.

It may be some time before we see Commodore IBM compatibles in Australia, however. The company is moving to meet the huge demand for compatibles in Europe where Commodore is well established and has a larger share of the market than IBM. Supplies of the IBM PC itself have been delayed by shortages of chips.

Micronews

RTTY software for radio amateurs

Radio amateurs who have a Commodore computer can expand their activities with a software package just released by the Melbourne firm High Technology Computer Systems.

The new software, called simply "RTTY", is the brain-child of Mike Hamilton (VK3HM) and is designed to handle radioteletype, Morse code, and slow scan television (SSTV). It provides translation facilities for the Commodore VIC 20, '64 and series 8000 microcomputers.

Using the program requires a shortwave receiver. The receiver is connected directly to the computer and the package allows the user to monitor teletype traffic, Morse code and slow scan television, and to answer back with "Mailbox", an automatic response mode.

For the capabilities provided, the price seems very reasonable at \$59 on cassette or disk.

Further information is available from High Technology Computer Systems, 87 Swanston St, Richmond, Vic (03) 429 1966.

Sales promotions rely on computers

Those cash refunds, competitions and bonus offers included with products of all types are collectively known as "sales promotions" and are generally handled by a specialist company contracted to the distributor or manufacturer. One of the largest companies in the field is Purchase Point Pty Ltd, who claim that Australians can expect to see even more special offers in the years to come.

"Dozens of new companies will emerge in every capital city and sales promotion will rapidly escalate its massive penetration in press, radio, and TV media and in direct mail and point of purchase", says Robert Wentworth-Sheilds, Chairman of Purchase Point.

Computers are a real aid to success in the sales promotion field, according to the company. Purchase Point installed its first computer last year, choosing a Panasonic JB 3001 with a 10MB hard disk supplied by Amicron Computers.

The company ran up to 20 promotions simultaneously last year, involving thousands of cash refunds, hundreds of thousands of competition entry forms and hundreds of trade bonuses.

Sinclair launches 16-bit Quantum Leap computer

Clive Sinclair has definitely done it again with his QL computer. The first company to offer low-cost 8-bit systems, Sinclair has gone much further with the "Quantum Leap", a low-cost (\$US499) system based on the Motorola 68008 microprocessor. The 68008 has a 32-bit internal architecture and an 8-bit data bus, and is compatible with the 68000 in the same way that the 8088 is related

The QL offers a 65-key full-size keyboard, two built-in "micro tape" drives and 128K of RAM, expandable to 640K with an external cartridge. Word processing, business graphics, a spreadsheet package and database management software are included with the standard machine. Graphics resolution is 512 x 256 pixels in eight colours, with the powerful 16-bit processor allowing extremely detailed pictures to be constructed in a very short time.

The QL has the ability to run several programs simultaneously (called multi-tasking). Output from the various programs is displayed in different "windows" or sections of the screen. Sinclair's own version of

Basic, called SuperBasic, and a unique QDOS operating system are the keys to providing a powerful, easy to use system.

The tape cartridges used to store programs and data use narrow loops of video quality tape in plastic cartridges each the size of a book of matches. The tape is driven at around 50cm/second and each cartridge provides 100K bytes of storage, arranged in 50 data files.

In addition to the two tape drives built in, six others can be connected, for a total of 800K of storage. Average access time for a program on tape is 3.5 seconds.

At the rear of the console are connections for local area networking (allowing QLs to be connected together), colour and monochrome video monitors or a television set, a printer port, modem port and two joystick interfaces. Sinclair says that the add-on modem is still under development, as is a Winchester disk drive interface, a terminal emulator and other software. Up to 32K of ROM can also be plugged into the machine.

Barson Computers, who distribute Sinclair products in Australia, indicate that the QL will probably be available here later this year, at a price "under \$1000".

"We quickly reached the point where a computer was a necessity to compile correct statistical information quickly and efficiently," Mr Wentworth-Sheilds says. "Amicron was called in and they came up with a solution that met all our requirements. Our staff spent a day at Amicron's training centre and were given a further two days of training on site."

"The computer system runs under the MS-DOS operating system and uses a dBase II program written by Amicron and tailored to our exact requirements in sales promotion work."

The computer provides complete printouts of the number of consumer and/or trade entries for each promotion per state, per city, per store on a daily basis. The company is able to provide a completely detailed statistical breakdown of any promotion within hours of it finishing.

"It can make the difference between a promotion being an outstanding success or a dismal failure," says Wentworth-Sheilds.

For further information contact Amicron Business Systems, Suite 6, 281 Pacific Highway, North Sydney, 2060

News from the Clubs

- The Southern Districts Commodore Users Group meets on the first and third Wednesdays of each month at the API Hall, Kurrajong Rd. Preston. The group publishes a monthly newsletter and describes itself as a "family group" with activities and information for people of all ages. There is a joining fee of \$10 and an annual subscription of \$24.

Further information is available from the secretary, Lex Toms, 3

Lucille Cres. Casula. Phone (02) 602 8691.

- The Melbourne TI-99/4A Users Group meets monthly at the Victoria College, Burwood. The group publishes a bi-monthly newsletter and six program tapes per year, runs demonstrations, tutorials and a special interest group in Assembly language.

Further information is available from Wayne Worlidge, 123 Ashburn Grove, Ashburton, Vic. 3147. Phone (03) 25 1832.

'how I wun a pryze in a short storey competish-un fer gud English.'

While it's highly unlikely our **WordPlus** system ever would have to clean up a sentence such as the one above, it could without any trouble whatsoever.

Essentially, **WordPlus** is a computer programme that catches errors in spelling and other dictionary based tasks.

However, you are the one in control, you can over-ride its advice at your discretion.

Software Source also has another programme called **Punctuation and Style**. This system catches errors in punctuation and grammar and picks up phrases that are being misused and suggests alternatives. As you can imagine, both these systems can help your writing style considerably.

Correct grammar can cut down greatly the costly misunderstandings in business communication, so these programmes from Software Source may well be the best means a business has nowadays of cutting down the competition.

See Software Source for **Basic/z**, **C-86**, **Directory Sort**, **Modem 86**, **Spellbinder**, **Super Calc**, **VSpool** & **VEdit**.



Software Source Pty Ltd

P.O. Box 364, Edgecliff, N.S.W. 2027. Phone: 389 6388

Please send me full details of your **WordPlus** and **Punctuation and Style** systems.

Name _____
Company _____
Address _____

EA

551

Leave the kid's stuff to the kids...
YOU'RE READY FOR
FUN WAY 3

Now a whole new series of exciting projects - getting you into the fascinating world of **integrated circuits**.

No more kid's stuff: **Fun Way III** takes you straight into the big time. And while you're building, you're learning - what better way to understand what you're doing?

Look at the exciting range of projects to choose from...

There's something for everyone, from a mini amplifier and colour organ to games, binary electronics projects...even an electronic cricket (chirp!).

And if you're building a school project, we even include glossy labels to make your project look a million dollars (top marks!).

Don't miss a single one of these...



Mini Stereo Amp.

\$14⁹⁵

Just the shot for 'Walkie' stereo - now you can listen to it in your bedroom through speakers! Or make yourself a PA amplifier. Cat K-2667

Binary Bingo

\$19⁹⁵

A game of skill and reaction time - and a valuable teaching aid! It might sound pretty simple to play - but try it and see! Cat K-2668



Light and Sound

Another multi-talented project. Sound effects, flashing lights - continuity tester, Morse code oscillator - it's got the lot! Cat K-2665 **\$8⁹⁵**



Lil Pokey

It's a barrel of fun to play. And you don't risk losing your shirt like the real thing. Cat K-2662 **\$19⁹⁵**

THE BOOK

Fun Way III is for the advanced hobbyist: those who have worked their way through the projects in Fun Way I and Fun Way II. There are ten projects in Fun Way III and each one is based on integrated circuits. Because the projects are more complex than the previous Fun Way projects, they are dealt with in rather more detail. More explanation, more construction. So you learn more with Fun Way III. Cat B-2610

And best of all...

it's only
\$6⁹⁵

GET YOURS NOW!



Mini Colour Organ

Like a disco - but battery operated so it's safe! Connect to your radio, etc. for a LED lightshow. Cat K-2664 **\$12⁹⁵**



Combination Time Lock Switch

Make it into a game... or use as a real alarm component! It's that good! Just try getting into this one! Cat K-2666 **\$12⁹⁵**



Two Up

Australia's national game - now done electronically because King George pennies are hard to get! Cat K-2661 **\$9⁹⁵**



Minder

A multipurpose project for the car. 'Lights on' warning, 'door open' warning plus a pseudo burglar alarm. Cat K-2660 **\$7⁹⁵**

Cricket



Whaaa! Hide it in a dark room and it starts chirping. Turn the light on and it stops. It's infuriating! Cat K-2663 **\$9⁹⁵**



Mini Synth

Wow! A real musical synthesiser, with decay, frequency doubling & halving, tremolo... unique circuit uses YOU as the note generator! Cat K-2669 **\$19⁹⁵**

DICK SMITH ELECTRONICS



A 768/GT

(See page 108 for address details)

50 and 25 years ago...

"Electronics Australia" is one of the longest running technical publications in the world. We started as "Wireless Weekly" in August 1922 and became "Radio and Hobbies in Australia" in April 1939. The title was changed to "Radio, Television and Hobbies" in February 1955 and finally, to "Electronics Australia" in April 1965. Below we feature some items from past issues.

Wireless Weekly 30

June, 1934

New police radio: A complete new transmitting and receiving wireless station has been installed at the Redfern Police Barracks, for the purpose of keeping the police wireless patrol cars in constant communication with headquarters.

The equipment, which was designed and constructed by Amalgamated Wireless, is of the most modern pattern, and it will enable messages to be sent out both in the Morse code and by word of mouth.

The amplifier championship: This contest, announced several months previously and involving a good deal of preliminary judging to reduce the contestants to a short list, was finally held at the club rooms of the Royal Motor Yacht Club at Rose Bay.

Technical judges included Mr Len Schultz, Mr Keith Blackwell, and the technical editor Mr A. G. Hull. Musical Judges were Frank Hutchins and Howard Carr, both leading musicians of their day.

The Champion of Champions was Mr H. J. Carter, with Mr K. T. Boyle winning the technicians' choice.

Ratings system, 1934: Dr Nevil M. Hopkins, a lecturer in engineering at the New York University, has developed a device which he says "will revolutionise the radio broadcasting industry". Dr Hopkins calls it the "Televotes" and by use of this instrument a listener-in can, by pressing a button, immediately transmit to the station his reaction to the program.

The instrument, which would cost approximately one dollar, can utilise air waves or carrier current on an electric light or telephone wires.

Not bad for 30 lines: Television has advanced so far in England that a "looker-in" at Bradford was able to send the London transmitters an easily recognisable photograph of a televised artist. It is calculated that during the three seconds exposure necessary for the photograph, 37 pictures were formed on the television screen.

Most powerful transmitter: The new transmitter for WLW, WSAI, and W8XAL, the Crosley stations in the USA, will generate the most powerful radio signals ever broadcast. A 75 x 75 foot spray pond is part of the system which cools the tubes used in the transmitters.



June, 1959

Before the space probes: Radar contact with Venus, first achieved February 10 and again February 12, 1958, extended the range of radar to 28-million miles, more than 100 times the previous record, giving man his greatest DX. The contact gave us more accurate information on the size of the solar system, and may give us information about the surface of the planet.

The contact was made by scientists of the Massachusetts Institute of Technology Lincoln Laboratory, using equipment never before employed for radio-astronomical purposes and introducing techniques hitherto quite foreign to radio communications.

Where are they Neil? Some scientists believe that whoever wins the race to the moon might be rewarded with a fortune in diamonds.

Moon craters shaped like huge ice-cream cones could be an indication of diamond deposits, they believe.

Dr G. P. Kuiper, of Yerkes Observatory, Williams Bay, Wisconsin, has said the craters appeared similar to the funnel-like craters topping the Kimberley "diamond pipes" in South Africa.

Dr Harold C. Urey, Nobel Prize-winning scientist of the University of California, said pressures inside the moon were sufficient to create diamonds.

When TV was still a novelty: During the month, Australia's TV plans moved forward in two important particulars.

Firstly, initial programs as such were telecast in Adelaide, where thousands of people gathered around shop windows to watch, just as they did in Sydney and in Melbourne in 1956.

If anything, enthusiasm was greater in Adelaide, whose citizens have been long tantalised by reports of TV doings in other states.

There is no doubt that Adelaide, Brisbane and Perth will absorb TV even more rapidly.

Secondly, the Postmaster-General announced plans for extending TV into 13 country areas in the Capital Territory, Victoria, Queensland and Tasmania.

In doing so he emphasised that priority would be given to applicants representing local interests rather than those of the commercial stations already established, and that local commercial licences shall not necessarily be limited to one.

Our first coaxial cable: The £1,200,000 contract for the coaxial cable equipment for the Sydney-Melbourne six-tube coaxial system, which has been awarded to the Telecommunication Co of Australia Pty Ltd, is part of a huge program of expansion of Australian trunk telephone routes, using coaxial cable and wide-band radio systems.

New Radio, Television & Hobbies TV receiver: Our laboratory is currently developing a completely new television receiver for home construction. It uses the latest 110-degree deflection tubes and will fit completely within a modern slim cabinet. The emphasis is on simplicity of design, layout and construction, and it is anticipated that the total cost will be considerably lower than earlier designs. The new set will take either a 17-inch or a 21-inch tube, as desired.

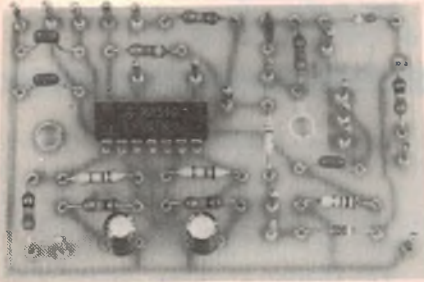
Watch for it in a forthcoming issue!

NEW KITS FOR THIS MONTH

FUNCTION GENERATOR ADAPTOR

EA JUNE 83

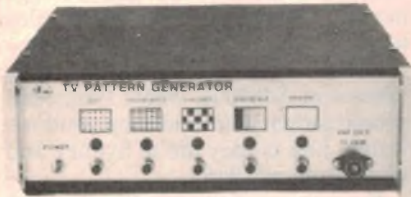
\$12



Add this enhancement to your Function Generator which lets it operate as a frequency meter improving the linearity of the coarse frequency control.

TV PATTERN GENERATOR

\$67.50



Anyone wishing to obtain the maximum performance from a colour TV receiver needs a pattern generator. Why not build this completely new design which provides five separate patterns: dot, crosshatch, checkerboard, grey scale and white raster.

ETI 477 MOSFET MODULE

\$63.50



Remember the great ETI 5000 power amp. With this module as the hub of the ETI 5000 and a transformer you get an amazing power output of 150W RMS.
Plus Power Supply (No Trans) \$49.00
Plus Transformer \$39.50

TRANSISTOR ASSISTED IGNITION

EA November 79



\$34.50

MUSICOLOR IV

\$84.00



Add excitement to parties, card nights and discos with EAs new Musicolor IV light show. This is the latest in the famous line of Musicolors and it offers features such as four channel "Color Organ" plus four channel light chaser, front panel LED display, internal microphone, single sensitivity control plus opto-coupled switching for increased safety. EA August 81

CRUISE CONTROL \$70

EA JUNE 83



Commercial Cruise Controls available on some new cars and on the aftermarket cost around \$200. This design can be built for less than half that figure. Price does not include windscreen wiper motor, brake cable or metal cases.

PROGRAMMABLE LIGHT CONTROLLER

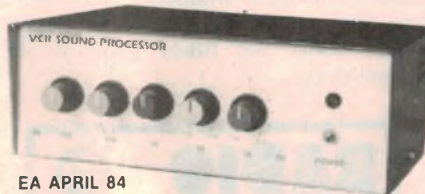
\$180



EA MAY 84

VCR SOUND PROCESSOR

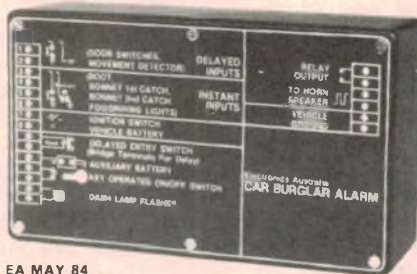
\$69.00



EA APRIL 84

Give the sound from your VCR a lift with this new VCR Sound Processor. Main features include an effective stereo simulator circuit, a 5-band graphic equaliser and noise filtering.

CAR BURGLAR ALARM \$70



EA MAY 84

AUDIO TEST UNIT FOR CASS DECKS

\$47.50



EA October 81

NOISE SIMULATOR \$30

\$30



EA JUNE 83

This Noise Simulator will provide a soothing noise, like rain on the roof or waves on the beach, to mask out those sounds that irritate. Cost does not include plugpack.



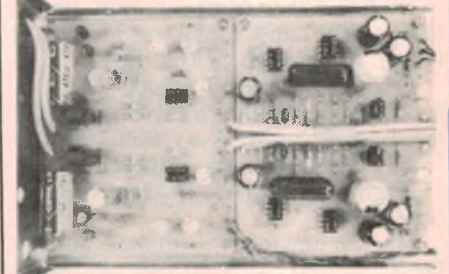
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EA MARCH 84

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CRYSTAL MARKER \$34.50 (INC 1MHZ X)

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PRE-STOCKTAKE SALE

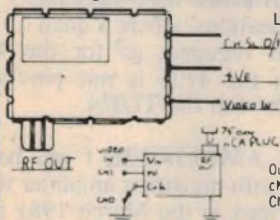
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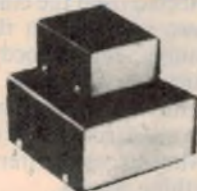


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Information centre

VCR SOUND PROCESSOR: I would like your help if possible in using the VCR Sound Processor (described in the April 1984 issue) as a graphic equaliser. I would appreciate it if you could give the formulas for changing the frequencies from those originally specified to 60Hz, 80Hz, 1kHz, 3.5kHz and 12kHz.

Would the same formulas be applicable to the graphic equaliser described in your May 1979 issue?

Also, what is the difference between the TL074, LF347 op amps and the uA4136 op amps used in the earlier graphic equaliser project? (MG., Woodbine, NSW).

● If you have a look at the capacitor values for the 500Hz, 1kHz and 2kHz gyrators (IC1d, 2c and 2, respectively), you will see that there is an inverse relationship between the size of the capacitors and the centre frequency. Essentially, you can shift the centre-frequency of the gyrators merely by scaling the size of the capacitors in inverse proportion to frequency value.

In simple language then, if you want to double the centre frequency, you halve the respective capacitor values and vice versa.

Unfortunately that is not the whole

story for it is evident that you also wish to change the spacing between the centre frequencies. This means that you have to adjust the Q value of the gyrators. We don't have the space to go into this subject here but there is a good outline in the National Semiconductor handbook in the section on Octave Analysers.

Note that having the centre-frequencies closely spaced at 60Hz and 80Hz requires a very high Q value for the gyrators otherwise there will be substantial overlap and hence, interaction between the two controls. It would be more practical to select more widely spaced frequencies.

The TL074 is a quad Fet-input op amp package. For convenience, it can be regarded as a considerably upgraded version of the old workhorse, the 741. Compared to the 741, the TL071, 072 and 074 family are much quieter, have superior bandwidth and better slew rate, meaning that they can deliver a higher voltage swing at high frequencies.

Apart from that, the TL07-series have Fet inputs. This means that they draw negligible input bias current. This has two advantages. First, it is easier to design this op amp into high impedance circuits and, second, noise due to input

currents is negligible.

The uA4136 is a quad low noise bipolar input op amp package. In fact, with the exception of the Signetics NE5533/34 family, the 4136 is the lowest-noise op amp package readily available.

For most general purpose circuits, it is difficult to go past the TL07-family and their equivalents. For reasonably low noise applications, where a quad op amp package is required, go for the 4136. Note that the 4136 is not pin-for-pin compatible with the TL074.

GUITAR AMPLIFIER: I am having problems with my guitar amplifier which was described in the March 1981 issue. The first point concerns the .0022 μ F capacitor connected from the collector of Q10 to the zero volt rail. In the Twin Twenty Five amplifier described in April '76, the same capacitor is shown connected to the equivalent transistor. Does this have an effect on the circuitry as I am drawing excess current and I can't find anything wrong.

Secondly, I cannot grasp the reason for the capacitors between the OV rail at the output and the tremolo cable sheathing to chassis ground as they are

TV antennas and steel conduit:

ANTENNA DESIGN: I was interested in your article on TV antenna design (How to Obtain Better TV Reception Pt 6). Would it be possible to use steel conduit, as used to encase wiring in old houses, as elements in the antenna?

It seems to be quite rigid and strong and would have nearly as good conductivity as aluminium tubing. More care would be needed to prevent corrosion, but are there any electrical problems with using steel conduit? (J.B., Oak Flats, NSW).

● You are right in suspecting that conductivity is not really important for receiving antennas although for transmitting antennas it is another matter.

Even so, there are several practical objections to the use of steel conduit for antenna construction. The first

you have already recognised as corrosion. Don't underestimate this problem. While it may be relatively easy to protect the surface of the conduit from rusting, the connections will probably be always prone to corrosion.

Second, there is the problem of weight. Steel conduit is considerably heavier than aluminium tubing. A large antenna array made of steel conduit could be well nigh unmanageable when it is being installed. Add to that the problem of windage (wind resistance). Since conduit has a diameter of about 20mm it will have considerably more windage than small diameter tubing.

All this means that you will need a considerably stronger mast to support your antenna. Add to that the fact that conduit is not as easy to cut as

aluminium tubing and it does not have a lot going for it.

In fact, the more we thought about this question, the less justification we could see for using the stuff. One justification could be having a pile of the stuff just waiting to be used but then it might be better to use it for tomato stakes.

Even as tomato stakes, conduit wouldn't be much good as it would rust out quickly. In fact, when you come to think about it, steel conduit isn't even any good for electrical conduit.

Since we have been so negative about the subject, we thought we should announce a competition for the best use for old steel conduit. Of course, in this case, the best use may not be the most obvious but it might be the funniest.

All right then, what would you do with steel conduit. The prize for the best answer will be \$15. Go to it.

already directly earthed at the inputs via the cable sheathing.

I could not procure a VPC14 choke so I wound one on a 100 ohm 1 watt resistor, winding as many turns of 22 B&S as I could get on it. If this is not satisfactory could you inform me as to the correct construction for this choke?

I have just about built everything myself including rewinding a C-core transformer secondary and the PC board etc.

I used a phenolic board to make my printed circuit and left as much copper as possible, so the tracks are very close. Could my problem be possible tracking through the phenolic? I am going to let my head go and splash out on a manufactured fibreglass board, hoping that this will cure the problem. (L.M., Tuncurry, NSW).

● It is highly unlikely that the .0022 μ F capacitor would be the cause of the fault. This capacitor rolls off the open loop gain of the power amplifier, as a stability measure. Of course if the capacitor was omitted or was open-circuit, it is quite likely that the amplifier would be unstable and would draw heavy current.

You have not quoted any DC voltage conditions nor have you mentioned whether you have tried to adjust the quiescent current so it is not possible for us to say whether you have a dc fault or not.

On the other hand, you have not used the correct 14 μ H choke in the output of the amplifier and you have made your own PC board, and probably varied the layout in the process, so it is quite likely the amplifier is unstable and oscillating supersessionally.

The 14 μ H choke is wound on a special grade of ferrite rod, 30mm long and 10mm in diameter. It is available from the mail order department of Dick Smith Electronics for 60 cents (cat. no K-6036).

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ADDRESS: All requests to the Assistant Editor, "Electronics Australia", Box 163, Chippendale, 2008.

The choke is wound using 15 turns of 18 B&S enamelled copper wire. Ordinary ferrite rod used for ferrite rod antennas is not suitable.

The capacitor connected between the chassis and the tremolo jack shield is to reduce hum which is otherwise picked up by the isolated socket.

VK POWERMASTER: I have constructed the VK powermaster supply described in March 1984 for the purpose of powering my Yaesu FT-77. The supply has one major drawback — no over-voltage protection. In the event of a collector-emitter short on one or more of the pass transistors, excess voltage is applied to the load, possibly doing untold damage.

By the simple addition of a 15V zener diode wired between the negative output rail and the base of Q7 (cathode to base) full over-voltage protection is provided. I

hope this information may be of use to readers. (M.B., Mt Warrigal, NSW).

● It is true that a faulty series pass transistor or other component failure could apply the full unregulated output of the Powermaster to the load. However, protecting against this condition is not an easy task. Your addition of a zener diode may activate Q7 and cause the undamaged series pass transistors to turn off but that is of little use if one series pass transistor is short-circuit.

In fact, if the regulator circuit is working at all, a short-circuit series pass transistor will immediately cause the other series pass transistors to turn off, as the circuit attempts to regulate.

In lower rated power supplies, such as our VK Powermate described in December 1983, it is possible to provide over-voltage protection fairly simply. We just connected at 15V 5W zener diode

Forum — continued from p43

preamplifier is judged to be "remarkably quiet for a tube design" — surely a somewhat left-handed compliment!

I was intrigued, too, with the subjective evaluation of the sound:

"... I found myself enjoying a preamp that fitted nicely in between the lush 'tubiness' of the Concordant and the more analytical sound of the Beard."

Perhaps I am a member of the old school of audiophiles, a Luddite questioning the sanity of the New Wave of reviewers (not my words) but I have the old-fashioned idea that a preamplifier should be neutral; should not have or impart a sound of its own. Simple logic seems to suggest that, if you have three supposedly prestige preamplifiers which

all sound subjectively different, then at least two of them must be suspect in terms of colouration. Maybe all three!

One more thing, and I promise to shut up:

When evaluating the Croft preamplifier, Ken Kessel says that he "switched it on and gave it a couple of hours to settle down" before proceeding to the listening tests.

In a previous article relating to the Audio Research D-70 power amplifier he explained how he had "let the D-70 warm up for four or five hours before spending any serious time with it".

Why, on earth?

If a preamplifier needs to "settle down" or a power amplifier needs to "warm up" for some hours before it can

give of its best, the owner faces a double problem:

● The valves need to re-absorb the occluded internal gas, electrolytic capacitors need to re-form, or the circuitry is thermally unstable for some other reason; and

● The extra switch-on time is likely to halve the practical service life of the valves.

It is true that rating procedures for the US market require that amplifiers be driven in a specified fashion for a specified time before readings are taken but this is intended, not to coax the best out of the amplifier, but to force it into thermal aberration, if it is prone to such.

Methinks that the "New Wave" of reviewers have a few things to sort out!

directly across the supply output. In the event of a failure the rising supply voltage will cause the zener to conduct heavily and blow the fuse. In the process the zener may be destroyed but provided the protection has worked and saved the equipment this is no great problem.

Such a simple method is not likely to be effective with the 25-amp VK Powermaster. Even a high-power zener is likely to be blown to pieces before the fuse blows. The solution is to use a more complicated "crow-bar" protection circuit. Such a circuit was published with our 5V/10A Minibrute power supply described in November 1977.

Briefly, the crow-bar circuit uses a zener diode to monitor the power supply output for over-voltage. If an over-voltage condition occurs, the zener conducts and uses a transistor to turn on an SCR. In turn this uses a heavy duty automotive relay to short out the unregulated supply rail and blow the fuse.

The beauty of this circuit is that it activates again if the fuse is replaced and no repair has taken place. The circuit could be easily modified to suit the VK Powermaster.

MOTOR-CYCLE INTERCOM: I have built the motor-cycle intercom that was published in your February 1984 issue but have a problem. Could you please help? The intercom works well when the

bike (the same model as in your article) is in the garage and engine running at 1,200rpm. With engine revs raised to say 1,500rpm slight interference occurs, but on the road conversation is impossible, with interference and voice distortion. When engine revs go back to tick-over it is possible to hear or just about.

All the cables used for the unit are the shielded type, have checked 7805 regular which is giving 9 volts. The only variation from your article is the case which you state plastic. I have used metal. (J.E., Campbelltown, NSW).

● We assume that you have connected the metal case to the chassis of the bike and thereby to the negative side of the battery supply. If so, we would expect the unit to give less trouble rather than more, as you have experienced.

We can only assume that the bike's electrical system is radiating interference which is being induced into the intercom wiring. With this theory in mind, it might be worth trying the effect of passing the supply leads several times through a fair-sized ferrite toroid. The same process could be tried on the two helmet leads, to try and reduce the common mode interference.

DREAM 6800: I am interested in building the Dream 6800 which was described in May 1979 and following issues.

At the moment I have some of the

appropriate chips including 6802 of which I wish to make the best possible use. Can you kindly supply me with the following information: Where can I purchase two 6802 compatible PC boards? If these are unavailable could you please supply me with the details of modification? Where can I get a complete list of the components and price list? Is there any additional documentation regarding software and hardware which may be necessary or useful for the development of the project?

M. A. Sallehpour,
1d/105 Cook Road,
Centennial Park, NSW 2021.

● Unfortunately we know of no supplier of Dream 6802 boards. It would also be quite a fiddly job to adapt the 6802 chip to the original 6800 board since the pinouts for the two devices are different. Perhaps one of our readers can help. We have published your name and address in full to that purpose.

Notes & Errata

SWEEP GENERATOR: (April '84, Circuit and Design Ideas): pins 2 and 3 of IC8 should be transposed while the wiper of S2 should go to -5V instead of ground. Note also that the auto and manual positions on S2 are shown transposed.

MODEL 175 AUTORANGING BENCH/PORTABLE DMM

KEITHLEY INSTRUMENTS



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The new Model 175 Autoranging Bench Digital Multimeter, from Keithley Instruments, Inc., combines the measurement capabilities of much higher-priced system DMMs with several new features to extend its utility, yet retain simplicity of use. Ideal for use as a bench meter in production or lab work, this 4-1/2 digit autoranging DMM also has a field-installable battery option, making it fully portable. Fast autoranging (up to 200ms per range change on DCV) enables the user to concentrate on getting the reading without worrying about choosing the appropriate range.

The Model 175 features digital calibration for reduced cost of ownership, as many users can now calibrate the meter in-house. With the Model 1753 IEEE-488 (GPIB) option, the 175 is the lowest-priced IEEE-interfaceable DMM available. Model 175's 100-point data logger monitors drifts, determines rates of change, and collects response curve data without a printer, output cables, or complicated hook-ups. The data logger has six different store rates from one reading/400ms to one reading/hour, and data recall is "push-button" easy.

Other features of the Model 175 include:

- 4-1/2 digit LCD display with annunciators for function, range, and feature indication
- 10 μ V/10m Ω /10nA sensitivity
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- 10A capability
- 100kHz bandwidth in AC
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- Relative reference
- Max/Min reading hold
- Safety input jacks
- Front panel accessible amps fuse

Next month in * Electronics Australia



Heat controllers

Save power this winter with one or both of these heat controllers. Use them for radiators in small rooms or for electric blankets. Zero voltage switching circuits are used for low electromagnetic interference.

Transceiver Power Supply

If you have built the UHF transceiver or want to build this month's VHF transceiver you'll also want a power supply housed in a matching cabinet. We publish an easy to build circuit.

Marantz CD-54 review

We check out the lowest cost CD player from Marantz, the CD-54. This compact machine stacks up well against the mounting competition from other low cost models.

Plus:

Our series on op amps continues; Hyperion computer review; and an antique SW receiver.

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Sensitivity	Narrow FM	0.3uV	12DB SINAD
	Wide FM	1.0uV	12DB SINAD
	AM	0.5uV	10DB S/N
Selectivity:	NFM	7.5KHz @6DB	20KHz @700B
	WFM	50.0KHz @6DB	250KHz @600B
	AM	5.0KHz @6DB	10KHz @700B
Spurious and image rejection	50DB		
Modulation Acceptance:	NFM	7.5KHz	
	WFM	50KHz	AM 100%
IF Frequencies:	1st IF 750MHz	SAW Filter	3rd IF 455KHz Ceramic Filter
	2nd IF 45.0275MHz	Crystal Filter	(WFM) 5.5 MHz Ceramic Filter
Reference Oscillator	(Synthesiser) Crystal Controlled		
Scanning Rate	Approx 5 Channels per Second		
Search Scanning Rate	Approx 6 Seconds per mega Hertz		
Scan Delay:	Normal	Approx 1 second	
	With Delay Option	Approx 2.5 seconds	
Search Delay:	Approx 2.5 seconds		
Priority Sampling Rate	Approx 2 seconds		
Audio Output	1W @10% or less Distortion		
Speaker (Internal):	8 Ohms		
Power Requirements	12V-14V DC		
Frequency and Message Readout:	LCD Type		
	Size	138mm Wide x 80mm High x 200mm Deep	
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WHAT'D HE SAY?
 SUPERMAN.
 SUPERSTUFF, STUPID.
 WHAT'S SUPERSTUFF?

THOUGHT YOU'D NEVER ASK, IT'S SYNTHETIC METALS. MORE CRITICAL THAN THE US OIL SHORTAGE IS IT'S METAL SHORTAGE—IT HAS TO IMPORT 22 OF THE 27 MOST IMPORTANT ORES ESSENTIAL FOR AERO-SPACE AND WEAPONS PRODUCTION.

IT'S HIGH-TECH STUFF, YA GREAT NEANDERTHAL, COMPLEX MOLECULES, POLYMERS, YA DILL.
 IT'S ON AGAIN.

THE MIX MISSILE NOSE CONE IS MADE OF SUCH A POLYMER AS STRONG AS STEEL BUT A FRACTION THE WEIGHT—ALSO SOME TENNIS RACKETS.

A TENNIS RACKET'S A WEAPON?
 IN JOHN MCENROE'S HANDS IT IS.
 HANG ON! WHAT'S THIS GOT TO DO WITH SATELLITES?
 I'M OFF.

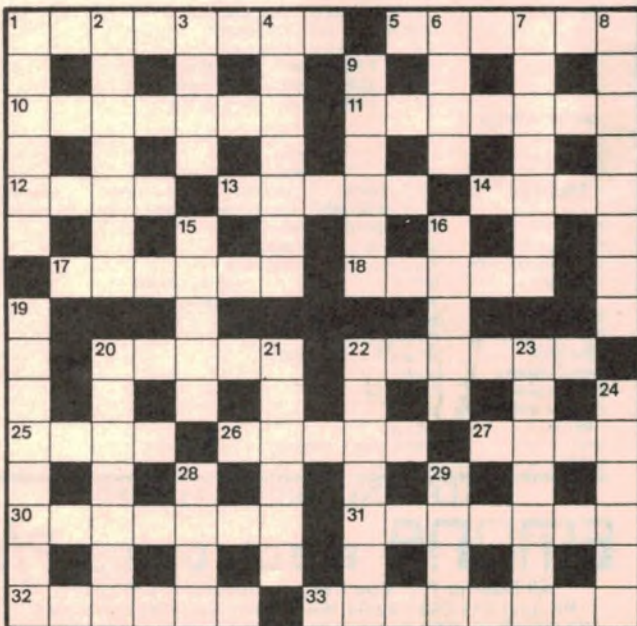
I'M GETTING TO THAT—SOME SCIENTISTS ENVISAGE GEOSTATIONARY SATELLITES TETHERED TO EARTH BY 38,000 KM SUPERSTRONG, SUPERLIGHT, SUPERSTRINGS, SUPERSTUFF, EH.

HELLO, WHERE DO I GET THIS SUPERSTRING STUFF?

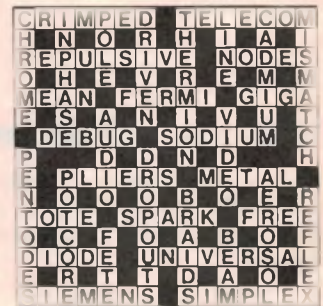
JUNE CROSSWORD

ACROSS

1. Computer storage capacity unit. (8)
5. Electronic device which enables you to make contact! (6)
10. This is found in a tilt version of 5 across. (7)
11. Type of key which is another version of 5 across. (7)
12. Sets up an antenna. (4)



SOLUTION FOR MAY



13. What a badly adjusted tonearm tends to do. (5)
14. The Crocodilian Connection? (4)
17. Electronics Australia's output. (6)
18. Ranging system. (5)
20. Another ranging system. (5)
22. Peaks. (6)
25. Type of aerial. (4)
26. Checks by 18 across. (5)
27. Prefix meaning "eight". (4)
30. Type of valve. (7)
31. Basic rule in electronics. (4,3)
32. Group of interconnected units. (6)
33. Electron accelerator. (8)

DOWN

1. Computer store. (6)
2. Openings for auto drivers. (7)
3. Component colour code for 6. (4)
4. Television coil structures. (1,1,5)
6. Erase a taped recording. (4)
7. Frequency multiplier. (7)
8. Type of filter. (4-4)
9. Part of an AC motor. (6)
15. Feature of a transformer. (5)
16. A circuit within a calculator. (5)
19. What 5 across possibly does to a circuit, etc. (8)
20. Removes ripple. (7)
21. Another type of 5 across. (6)
22. Electronic control panel. (7)
23. Kind of radio coil. (7)
24. Location with the call sign 8DN. (6)
28. Charge carrier. (4)
29. Colloquial radio operator's term, ack ----. (4)

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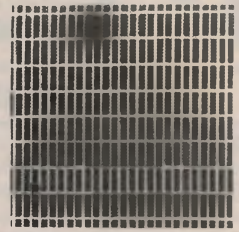
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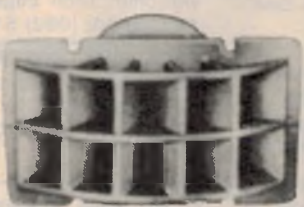
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Available from "Electronics Australia", 57 Regent St, Sydney. **PRICE \$4.50** OR by mail order from "Electronics Australia", PO Box 163, Chippendale, 2008. **PRICE \$5.40**

Yamaha CD player — continued from P37

problem, it appears that the hum is due to radiation from the unshielded transformer. A copper strap around the transformer could probably fix this.

Of course at any normal setting of the volume control, noise from the CD-X1 is virtually inaudible.


Listening tests confirmed that the CD-X1 is right up to the standards which we have come to expect from compact disc players.

The conclusion must be that Yamaha is on a winner with the CD-X1. At \$599 it is the lowest cost player available at the time of writing. We have raised a few quibbles but at this price they are just that — quibbles.

Further information can be obtained from hifi dealers or from the Australian distributors for Yamaha products, Rose Music Pty Ltd, 17-33 Market Street, South Melbourne, Victoria. (L.D.S.) 3

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267 1614.

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Carlingford 2118.
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115-117 Parramatta Road,
Concord, 2137.
Telephone 570 7000.

121 Forest Road,
Hurstville 2220.
Telephone 570 7000.

Radio Despatch Service,

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Telephone 211 0816.

RCS Radio Pty Ltd,

651 Forest Road,
Bexley, NSW 2207.
Telephone 587 3491.

Acetronics Printed Circuit Boards,

112 Robertson Road,
Bass Hill, 2197.
Telephone 645 1241

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Altronics,
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Jemal Products,
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