

NOVEMBER 1969 2s 6d

tape recorder

CONSTRUCTING A
CAPACITOR MICROPHONE

FIVE RULES OF MATCHING

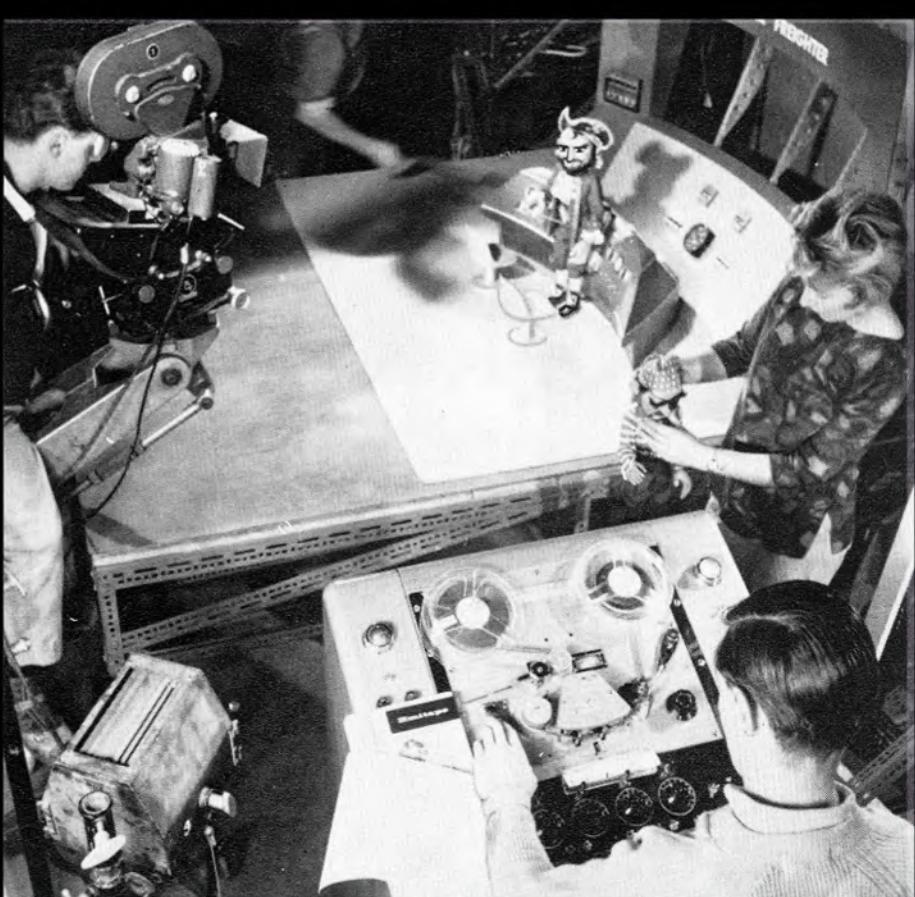
REVOX HS77 IEC
AND NAB REVIEWS

BLACK LIST

SO YOU WANT TO BE A
RECORDING ENGINEER?

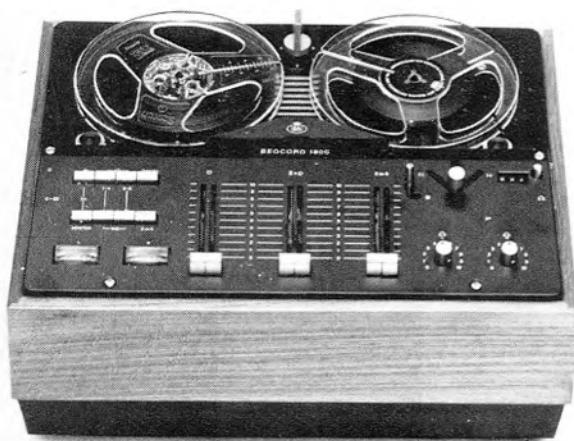
SYNCHRONISING TAPE
WITH FILM

AUDIO FAIR '69 PREVIEW





Two brilliant new additions to the Beocord range



BEOCORD 1800



BEOCORD 2400

Made by Bang & Olufsen for those who consider design and quality before price.

Whether you prefer to centre your High Fidelity system around a separate amplifier, or to base it on an amplifier integrated into one of the audio units, your needs for a tape recorder to complete your system can be satisfied by choosing one of these new Beocords. Both machines exceed the minimum requirements for DIN 45.500, and have operational facilities comprehensive enough to attract the semi-professional as well as the domestic user. These include a 3 digit tape counter with push button

reset. Foil operated auto stop plus thyristor controlled photo-stop for end of tape, tape break or programme scanning. Push button selection of A-B monitoring, sound on sound, echo, syncroplay, mono left, mono right, mixed mono, or stereo play. New hyperbolically ground tape heads with special patented machining give greatly improved contact between tape and tape head and less friction and noise during operation, resulting in less wear to tapes and tape heads.

The Beocord 1800 – designed for use with a High Fidelity amplifier such as the Beolab 5000 or Beomaster 1400.

Available in 2 versions: (a) $\frac{1}{2}$ track record and replay with extra switched $\frac{1}{4}$ track replay head, (b) $\frac{1}{4}$ track record and replay only. Sockets duplicated in DIN and phono type to simplify connection. Special amplifier and volume control for output to headphone sockets.

The Beocord 2400 – complete with its own stereo amplifier section giving 2×10 watts RMS output. $\frac{1}{2}$ track record and replay. 4 dual channel inputs in mixer section including a magnetic P.U. input. Bass, treble and split channel volume controls. Switched output for 2 pairs of speakers. The amplifier may be operated independent of the motor.

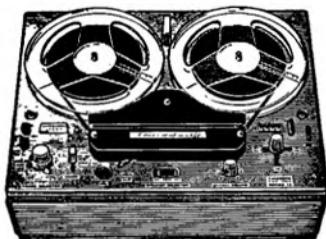
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B.A.S.F./PHILIPS/SCOTCH/GRUNDIG RECORDING TAPE

	Spool	Length	Suggested Retail Price	Our Price
STANDARD PLAY	4"	300'	14/6	11/2
	5"	600'	22/-	16/11
	5½"	900'	29/5	22/5
	7"	1200'	36/7	27/10
LONG PLAY	4"	450'	15/6	11/10
	4½"	600'	22/-	16/9
	5"	900'	29/2	22/2
	5½"	1200'	36/4	27/7
DOUBLE PLAY	4"	1800'	51/6	39/-
	4½"	600'	26/-	19/9
	5"	900'	31/-	23/6
	5½"	1200'	43/2	32/8
TRIPLE PLAY	4"	1800'	56/11	43/1
	5"	2400'	79/1	59/9
	5½"	900'	40/-	30/3
	7"	1200'	50/-	37/9
B.A.S.F. 'ROUND PACK'	5"	1800'	67/1	50/7
	5½"	2400'	91/4	68/10
	7"	3600'	116/8	88/5
	7" STD	1200'	OUR PRICE	21/6
	5" L/P	1200'	OUR PRICE	21/6
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	7"	1200'	21/-	subject to
LONG PLAY	5"	900'	16/-	2/6 package
	5½"	1200'	21/-	and postage.)
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RECOMMENDED: CASSETTES PHILIPS/B.A.S.F.

	Suggested Retail Price	Our Price	MAXELL CASSETTES (Philips Type)	Our Price
C-60 (Std.)	18/-	13/6	C-60	9/6
C-90 (L/P.)	25/6	19/6	C-90	13/9
C-120 (D/P.)	34/-	25/6	C-120	18/6



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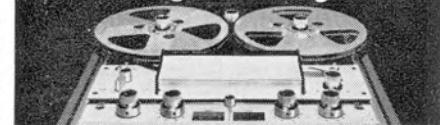
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- Single lever-knob deck operation with pause position.
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- Power output 10W per channel.
- Independent tone controls giving full lift and cut to both bass and treble each channel.
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5"	600'- 15/-	900'- 18/6d.	1200'- 28/6d.	1800'- 45/-
5½"	900'- 18/6d.	1200'- 22/6d.	1800'- 36/-	2400'- 57/6d.
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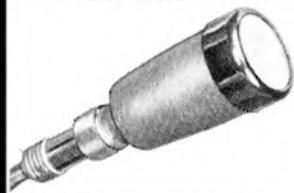
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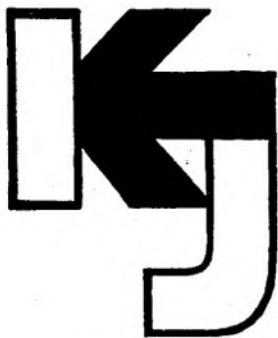
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hi-fi news



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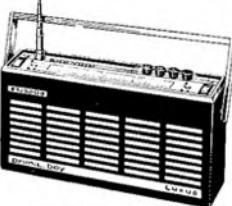


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tape recorder

NOVEMBER 1969 VOLUME 11 NUMBER 11

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SOUND AND CINE

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COVER PICTURE

The techniques of synchronising taped sound with cine film are discussed on page 444 of this issue by Richard Golding. A.P. Films of Slough had a third factor to contend with when producing the *Fireball XL5* children's television series: the electronic activation of each puppet's mouth. This and the later tape to 35mm film transfer were achieved with two EMI TR90's.

SUBSCRIPTION RATES

Annual home and overseas subscription rates to *Tape Recorder* and its associated journal *Hi-Fi News* are 30s. and 47s. respectively, U.S.A. \$4.30 & \$5.60. Six-month subscriptions are 15s. (*Tape Recorder*) and 24s. (*Hi-Fi News*), from Link House Publications Ltd., Dingwall Avenue, Croydon, CR9 2TA.

Tape Recorder is published on the 14th of the preceding month unless that date falls on a Sunday, when it appears on the Saturday.

WE SHALL BE in excellent company at this year's Audio Fair. Not only are we sharing part of Olympia with a handful of photographic dealers and manufacturers, we are also honoured by the presence of (wait for it) The Dairy Show. Eighty audio demonstration rooms and a prophesied 300 cattle under one roof could make considerable demands on the insulating properties of the 'Audio Studios' (to quote the official label), to say nothing of acoustic breakthrough between one room and another.

It may take more than 300 cattle to attract visitors from the recording industry to the 1969 Audio Fair. In past years, the Fair has been one of the few exhibitions catering even remotely for manufacturers of studio equipment and has been patronised by Studer, STC, AKG and the industrial divisions of Philips and Ampex. None of these companies will be represented this year. Studer (F.W.O. Bauch) and Ampex have switched their support to the APRS Exhibition; Philips (Pye TVT) have stayed out in the cold.

Four companies spanning both the industrial and domestic recording markets have also opted out of the Audio Fair this year: Reslo, Grampian, Chilton and Vortexon. At least one further company in this category is known to have been of two minds about exhibiting.

The result is an Audio Fair aimed more than ever at the gramophone record consumer. This division of recording and reproducing interests could be fortunate as it may herald increased support for next year's APRS Exhibition, a promising youngster that deserves solid backing from British manufacturers.

It is not so much his equipment as his attitude to recording which separates a domestic tape man from a professional. One studio engineer of our acquaintance produced a series of location recordings on a 4.75 cm/s cassette portable, dubbed them up to 38 and had them accepted for use by the BBC. Another bought himself a 38 cm/s Revox (the type reviewed on page 466) and declared it markedly superior to his employer's console equipment. This was no slur on the latter, which is several thousand pounds more reliable, but proves that professional results are within reach of the modestly wealthy individual.

Most readers will be aware of the trade restrictions that existed until a few years ago on the public circulation of commercial circuits. We have endeavoured to do our bit over the years in publishing circuits with service articles and reviews, and now claim that, where domestic recorders are concerned (the problem never arose with industrial equipment), few circuits are withheld from the general public.

Much the same situation exists, oddly enough, in the realm of microphone placing. Most London studios have evolved their own

ideas of 'good technique', some engineers treating them as trade secrets. This is fair enough, except that some of the secrets which leak out through reliable channels completely contradict each other. The situation may seem chaotic, but is in fact quite clear cut: microphone placing is not a science (yet), it is an art. It comprises a few basic rules relating to physical damage, stereo positioning, noise, frequency balance, instrumental balance, and reverberation, any or all of which may be ignored (by the pop producer at least) in favour of a new gimmick or effect. To quote Bob Fisher's* quite serious comment on pop techniques: 'If a microphone is placed inside a porcelain pot, then it is Right to place a microphone inside a porcelain pot'.

We recently played some stereo jazz recordings made on the editorial RE 301 (crossed cardioid pair) to a recording engineer specialising in classical music, and later to an engineer specialising in pop. Their comments, and we respect them both, may provide at least a grain of guidance to anyone disturbed by the 'subtle criticism' in record reviews. One considered the crossed-pair too far forward (the classical man) while the other (the multi-channel close-mike man) considered it too far back.

* Sales Engineer, STC.

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Power consumption AC 8 watts (max).

Reels 5 in. or smaller.

Tape speed $7\frac{1}{2}$ ips (19 cm/s), $3\frac{3}{4}$ ips (9.5 cm/s), $1\frac{7}{8}$ ips (4.8 cm/s).

Frequency response 30 Hz – 18 kHz at $7\frac{1}{2}$ ips; 30 Hz – 13 kHz at $3\frac{3}{4}$ ips; 30 Hz – 7 kHz at $1\frac{7}{8}$ ips.

Power output 1 watt.

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Line: sensitivity 0.055V, impedance approx. 100k ohms.

Remote control.

Speed tuning.

Output Monitor: standard output level 0.775V (load impedance 10k ohms).

Motor D-503F DC servo-motor.

Speaker $3\frac{1}{8}$ in x $6\frac{1}{4}$ in.

Battery life Up to $6\frac{1}{2}$ hours in continuous recording (with supplied batteries).

Dimensions $12\frac{1}{4}$ in. (w) x $4\frac{3}{16}$ in. (h) x $10\frac{1}{4}$ in. (d).

Weight 11 lb. 13 oz. with batteries.

Accessories Microphone (F-85 MTL), pre-recorded tape (5 in. tape), Sony reel (R-5A), connecting cord (RK-36), head cleaning ribbon, super batteries, magnetic earphone (ME-20).

Optional accessories Telephone pick-up (TP-4S), car battery cord (DCC-2AW), remote control (RM-6), microphone mixer (MX-600M), foot switch (FS-5), carrying case (CK-8B).



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ELECTRONIC MUSIC SOCIETY

DETAILS CONCERNING A survey of electronic music studios appeared in this column in July 1968. The survey was organised by the Arts Council of Great Britain and has resulted in a list of more than forty actively engaged in the preparation of electronic music. Partly as a result, the British Society for Electronic Music was inaugurated in February with a committee comprising Peter Maxwell Davis (chairman), Peter Zinovieff, James Murdoch, Don Banks, Tristram Cary and Hugh Davis. Its main aim is the foundation of a National Studio for Electronic Music though such a centre would be expected to cover a wider field. Its envisaged facilities will include:

1. Central processing rooms with sound generation equipment, a tape recording room, and several composing rooms, each a self-contained working unit but linked to the central system.
2. An acoustic research laboratory.
3. A lecture hall also suitable for small concerts.
4. A large recital hall linked (with the lecture hall) to a studio, projection and lighting equipment.
5. A library/archive of discs, audio tapes and video tapes.
6. Accommodation for composers.

The society has already organised one concert at the Royal Festival Hall and similar events will be held in the future. Further details of the society may be obtained from its administrator, John Woolf, SPNM, 29 Exhibition Road, London S.W.7.

DUPLICATING PLANT FOR SOUTH AFRICAN STUDIO

AN ORDER FOR high-speed duplication equipment has been won by Leevers-Rich from Manley Van Niekerk Studios (Pty) Ltd. of Johannesburg. The plant will handle the production of cassette and eight-track cartridge tape records for domestic tape players which are becoming increasingly popular in South Africa, particularly in cars. The contract, including installation supervision, is worth approximately £30,000.

BSI SPECIFICATIONS

A NEW BSI PUBLICATION relating to the use of magnetic tape recording and reproducing equipment in schools is now available, price 8s., from the BSI Sales Branch, 101/113 Pentonville Road, London N.1. The standard, BS 3499/8B, specifies safety, security, connectors, a warning light on mains powered equipment, wow and flutter limits, signal-to-noise ratio, distortion, frequency response at 19.05 and 9.53 cm/s (or 9.35 cm/s, the BSI press release was confused), and audio electrical output power. Bass and treble tone controls are recommended for equipment above a certain size, operating on replay only. Appendices deal with tape track positions (for '4-track' and '2-track'), storage and handling of recordings, and the information a supplier should forward to the purchaser. The importance of adequate servicing is emphasised in a foreword.

Also introduced is BS 3499/9C, concerned with electronic organs and priced 6s.

BBC 'USING A TAPE RECORDER'

A SERIES OF programmes for people using tape recorders for business, pleasure, or for education, will be broadcast by the BBC in December. 'Using a Tape Recorder' will be heard in Radio 3 on Tuesdays at 6.30 p.m. from December 2 to 30, and on Saturdays at 11 a.m., Radio 4, from January 3 to 17.

HOSPITAL BROADCASTS

THE ORGANISERS of 'Tyne Sound' would like to contact hospital broadcasting teams in the UK with a view to organising an exchange of programmes. Interested parties are asked to write to D. A. Morton, 31 Ridgewood Gardens, South Gosforth, Newcastle-on-Tyne 3.

PHILIPS 8mm FILM LOOPS

SOUND SERVICES LTD., Kingston Road, London S.W.19, have been appointed to distribute Philips 8 mm Film Loops. All loops in the series are animated, in colour, and available either in Standard 8 or Super 8. Prices are in the £3 10s. to £7 region. Crystallography, semiconductor physics, television and diffusion are covered by the present series which comprises 26 titles. All are available for ten day preview.

Stellavox SP7 professional stereo battery recorder described in last month's 'New Products'.

WORLD OF TAPE

APPOINTMENTS—LEEVERS-RICH

MR. N. V. NICHOLS has returned to Leevers-Rich after a period with Radford Electronics Ltd. and the EMI Group. He joins as Sales Engineer. Mr. Peter Richards, who has been with the company since 1959 and recently joined the board, has been promoted from Works Manager to General Manager.

STOLEN FERROGRAPH

A BRAND NEW Ferrograph 704W, Serial number 73215, was stolen on Sunday, September 28 from *Tape Recorder* contributor John Shuttleworth. Any reader coming across this serial number is asked to communicate with the Editor.



APPOINTMENTS—MULLARD

MR. T. ASPIN has been appointed Technical Manager of Mullard Ltd., Industrial Electronics Division. He will be responsible for establishing long term development policy in the fields of passive components, assemblies, semiconductors and ICs. Mr. Aspin joined Mullard in 1946 and was General Product Manager of the Consumer Electronics Division from 1966.

NEXT MONTH

JOHN FISHER DESCRIBES the construction of a 'dubbing box' providing tone control facilities between mixer and recorder or between recorders. Angus McKenzie contributes *Azimuthing with White Noise* while Alec Tutchings reviews the Akai X360 bi-directional stereo recorder and Foster FSA-1 stereo microphone system. David Kirk interviews Tom Reps (Managing Director, Magnetic Tapes Ltd.) on the problems of designing and manufacturing the Chilton 100s.

The Five Rules of Matching

Anthony Eden describes the simple arithmetic of connecting audio equipment

IN this article we shall be discussing some of the rules that apply when matching the output from one piece of equipment with the input of another. Then we shall consider some of the cases where these rules are broken and how matters can be remedied.

There are five basic rules to consider when matching one piece of equipment to another. It is important to remember that these rules apply only when *voltages* are being considered and another set of rules is required for *power* matching. All manufacturers quote input sensitivities and rated output levels in terms of voltage with the exception of loudspeaker matching which is invariably quoted in terms of power (i.e. watts). Power matching requires a different set of matching criteria.

Consider the case in which we have two units A and B and it is desired to feed the output from A into B (for example feeding a radio tuner into a tape recorder). The five rules to consider are:

- (1) The signal from A should be equal to or greater than the maximum input sensitivity of B.
- (2) The signal from A, as a general rule, should not exceed 5 times the input sensitivity of B.
- (3) The impedance of A should be equal to or less than that of B.
- (4) Any variation from a flat frequency response at the output of A is corrected for at the input to B. For example, it is no use feeding the output from a magnetic pick-up cartridge into the microphone socket of a tape recorder even though rules 1, 2 and 3 may be satisfied, since the recording characteristic of the disc is arranged to be frequency dependent and the input of B must be arranged to compensate for this.
- (5) When connecting unit A to unit B, be sure that no earth loop is created. If, for example, A is a mains powered radio tuner which is earthed at the mains and B is a tape recorder similarly earthed, any earth connection between the two units

will result in what is called an earth-loop and the recording may be seriously affected by hum.

A much simpler rule to remember is this: Connect up, switch on and only when trouble becomes apparent start a critical examination.

It may be remembered that rules 1, 2 and 3 also apply when matching a microphone to a tape recorder (February 1969 *Tape Recorder*), since a microphone is a voltage source. Let us now consider each of these rules in turn, and how problems may be overcome.

Rule 1 is a fundamental one and assuming that the manufacturers have stated the input and output voltages correctly (this is usually the case) we can readily ascertain if this rule is fulfilled. Insufficient voltage to drive the input of a tape recorder presented more problems when valves were used in tape recorders. It was quite frequent to find tape recorders with a radio input sensitivity of 250 mV and radio tuners with an output of only 150 mV thus presenting a matching problem. However with the advent of transistorised tape recorders the radio inputs to tape recorders have generally been increased to about 50-100 mV. Generally speaking, if a voltage increase is apparent in order to load the input of unit B fully, then only a small increase is called for and an amplifier with a 10 dB gain (3.2 times voltage gain) will in most cases be sufficient. A suitable low-noise amplifier fulfilling this specification is shown in fig. 1. The input to the amplifier can be any impedance up to 0.5 M without loss of bass response and any input up to 1 V maximum. The output impedance is very low and so can be fed into any impedance input. Such an amplifier is ideally suited where, for example, a radio tuner has an output of 100 mV at 250 K and is to be fed into a tape recorder of maximum input sensitivity 150 mV at say 50 K. The amplifier will step up the tuner output to about 300 mV which is then ideally suited for feeding into the tape recorder. It should be remembered that the output from an FM radio tuner can be quoted in one of several ways. If the output is quoted as 'up to 500 mV' this indicates that for 100% modulation of the carrier the output will be 500 mV. If the output is quoted as '250 mV for 50% deviation', this means that a typical transmission will deviate the carrier frequency by half its total permissible deviation and will in consequence be producing 250 mV which is half its total output. Hence the maximum output will be (2 x 250) mV, i.e. 500 mV. Ideally the output from unit A should be 1.5 to 3 times

the maximum input sensitivity of unit B, thus giving sufficient flexibility for variations of output and input.

Rule 2 considers the reverse problem of rule 1. Where the output from A is considerably larger than that of B it is quite possible for the input stage of unit B to become overloaded and distortion will result. For example, the average output from the Leak *Troughline* stereo tuner is about 80 mV, to be fed into a load of 50 K. The input to the Beocord 1100 is 2 mV at 50 K. Now to match these two units requires that the Beocord must stand more than a 40 times overload (32 dB). Whilst this could be a possibility it is a most undesirable state of affairs and some form of attenuation is required. Either a fixed potential divider or a variable potentiometer can be used. If the output from unit A requires a load of at least 100 K then the total value of the divider network ($R_1 + R_2$) in fig. 2 needs to fulfil this demand.

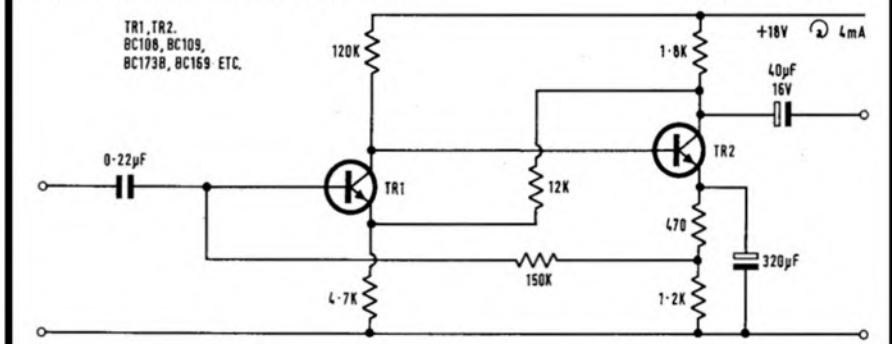
Thus $R_1 + R_2 = 100$ K and from the problem set above $V_{in} = 80$ mV and V_{out} has to be 2 mV. As the ratio of R_1 to R_2 alters so we alter the ratio of V_{in} to V_{out} and we find that:

$$\text{therefore } \frac{V_{out}}{80} \text{ approx.} = \frac{R_2}{100 \text{ K}}$$

Typical values for R_1 and R_2 respectively would be 100 K and 2.7 K. A quick glance back to our original rules will show that we have satisfied the output conditions for impedance matching, as well as ensuring that the input to the tape recorder is not overloaded.

Rule 3 considers a problem that we looked at with regard to microphone matching (February 1969). The same rules apply always when voltages are being considered. It is always advisable to load the output of unit A with as high a load as practicable even if the output impedance is quoted as 600 ohms. What this value refers to is the result of an analysis of the circuit and **not** the recommended load. Some manufacturers still quote the output impedance from their units as 600 ohms even though it has no relevance to practical matching problems. The value of 600 ohms was originally the value of impedance used for connecting broadcasting links to the Post Office land lines but it was important here to have impedance matching because power matching was used. The reason for this is that a land line

FIG. 1 LOW-NOISE AMPLIFIER (MULLARD)



can be considered as a continuous array of capacitative, inductive and resistive elements and assume a 'characteristic' impedance of about 600 ohms. These lines are so long that their impedance is independent of the connection at the far end and in order to obtain optimum energy transfer it is necessary to match the output from the broadcast unit with the characteristic impedance of the cable. It is easy to realise now why there is no point in making the output impedance of a unit 600 ohms, except to imitate the broadcasting authorities!

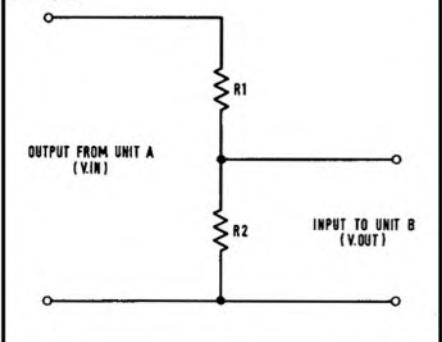
It is well to ask at this point how the frequency response and output voltage will be affected by placing a load across an output which has the same value as its output impedance. Consider first the effect on the frequency response. Normally the output coupling capacitor will cause a loss of bass response since the reactance of the capacitor would be appreciable with such a load. This problem was more apparent in the days of the valve driven cathode-follower circuit and an output coupling capacitor of much greater than $0.2 \mu\text{F}$ could be quite bulky. The Revox 736, for example, has an output impedance of about 1.3 K and the result of loading it with a 1.3 K load for various frequencies is shown in fig. 3.

A second problem also arises if a matched load is used. The output level drops significantly compared with the open circuit output. The result of this is shown in fig. 4, plotting output voltage against load at a frequency of 1 kHz.

The two graphs indicate the importance of not loading voltage output circuits more than is recommended by the designer.

One way of overcoming the impedance matching problem has already been described—namely that of using a potential divider network. This is excellent if we also wish to attenuate the signal being fed into unit B. However suppose that we have an output from unit A of 100 mV at 100 K which is being fed into unit B with an input sensitivity of 100 mV input at 2 K, how can we overcome this problem? Although this case is unusual, it can and does occur. The solution is not very simple and can only be successfully handled using an active impedance converter. An emitter-follower circuit provides one answer but a better solution was offered in 'Microphone Matching' (February 1969) using the compound emitter-follower circuit. This circuit has an input impedance up to 4 M and an output impedance of 70 ohms at unity voltage gain.

FIG. 2



Thus, we have now overcome most of the problems likely to occur with impedance matching. It should be remembered that if an **input impedance** is stated as 10 K it means that we can safely apply any input load up to this value without degrading performance. If there is sufficient feedback in the circuit it means that the value of the input impedance can well exceed the 10 K value without detriment to the circuit. However it is not advisable to work an amplifier under such conditions.

The above may be summarised in a table as follows:

Input Impedance

Input load: Up to but not exceeding the **input impedance**. Failure to observe this may result in a curtailment of the frequency response.

Output Impedance

Output load: As a guide should be 25 times greater than the output impedance. Failure to observe this may result in a reduction in the rated output voltage and a curtailment of the frequency response.

Rule 4 is self-explanatory and problems tend to occur where it is desired to feed the output from a pickup cartridge directly into the input socket of a tape recorder. Crystal and ceramic pickup cartridges are rather easier to feed into a tape recorder than magnetic cartridges. The crystal pickup will produce up to 500 mV output and the ceramic up to about 100 mV. If these pickups are fed into loads of about 2 M or greater, the frequency response of the cartridges approximately compensates for the recording characteristic of the disc. If the input is sufficiently sensitive to withstand it, a series 2.2 M resistor will ensure that a reasonably level frequency response can be obtained. However it should be remembered that if the input impedance to the tape recorder is low in comparison with the 2.2 M series resistor then the signal available at the input will be reduced

and we shall have the potential divider type network of fig. 2. Let us take an example. If we wished to feed the output from a ceramic cartridge type Sonotone 9TAHC into a Philips EL3575 tape recorder, the 9TAHC will typically produce about 100 mV output and the Philips tape recorder has a suitable input of 2 mV at 20 K. From the formula we find that $R1 = 2.2 \text{ M}$, $R2 = 20 \text{ K}$ and $V_{in} = 100 \text{ mV}$. Thus $V2 = 1 \text{ mV}$. Now, at peak output from the cartridge, it should be just about possible to fully load the input to the Philips tape recorder with this matching network.

The matching of magnetic cartridges cannot successfully be carried out for direct feed into a tape recorder unless either a special socket is available with the necessary equalisation (i.e. Beocord 2000 and Chilton 100 S) or the pickup is first fed into an amplifier providing the necessary correction, a corrected high level signal then being fed into the tape recorder.

Rule 5 is very often overlooked when connecting up separate units of equipment via the mains supply. A good general purpose rule is as follows: Where a number of units of equipment feed into a central amplifier, then this amplifier should be earthed and all the other units should be isolated from the earth lead. The converse problem can also arise where no earth connection is made and hum can result. This problem most often occurs with low voltage circuits such as magnetic pickup and microphone sources. Even if no hum problems are apparent it is a wise precaution to earth the equipment, both from an electrical safety viewpoint as well as ensuring that hum is kept to an absolute minimum.

This then concludes our study of inter-equipment matching. The same rules apply whether in mono or stereo, the only difference being that the left and right earthlead channels are normally commoned together and so obviously only one mains earthed lead is required. In conclusion, it is worthwhile using good quality screened cable for linking one piece of equipment with another.

FIG. 3 REVOX 736 ON OPEN CIRCUIT AND WHEN LOADED WITH 1.3K

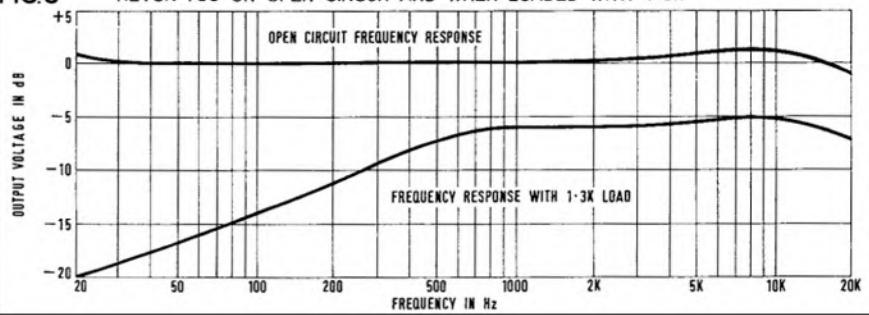
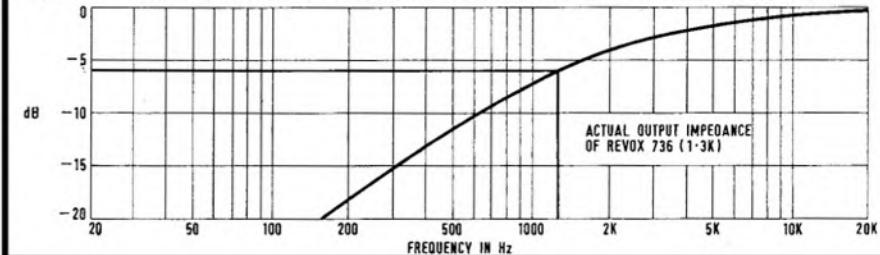


FIG. 4 REVOX 736 OUTPUT VOLTAGE AT 1kHz PLOTTED AGAINST LOAD TERMINATION



Synchronising Tape with Film

Part One A survey of current techniques and a close look at the Carol Cinesound
By Richard Golding

IN April this year, when it was made known that the Fairchild Model 900 8 mm sound recording camera was to be introduced into this country at a price around £425, it seemed that we British, at last, had recognized 8 mm as a serious film gauge. This was the single-system, sound-on-film magnetic stripe camera with electric drive and 62 m magazine. It could be used most efficiently with a portable transfer system such as the Siemens 8 mm double-band magnetic projector and appeared to be the answer to professional lip-sync on 8 mm. But like its predecessor the *Cinephonic 8*, the market was not quite ready. The objections made against it were that the pre-striped film

had a separation between sound and film that made cutting impossible and that the striped film had to be specially imported from America. With regard to the first point, 8 mm producers are obviously reluctant to go to the trouble and cost of extra prints and rerecorded sound whereas the Auricon people have been doing this for years on 16 mm. Secondly, the mere fact that 8 mm pre-striped film is readily available in America indicates that 8 mm single-system is taken seriously over there. Nine years ago when the *Cinephonic* first appeared prospects looked good for 8 mm sound on film. The Japanese and Americans were experimenting with 8 mm optical sound. The Eumig C5 Zoom-Reflex 8 mm camera

appeared. This was designed to start and to stop in conjunction with a small tape recorder carried over the shoulder. When the button was pressed, both units started together, but the synchronisation afterwards depended on the ability of each separate unit to keep up a constant speed. There were too, a very large number of sync units for controlling projection speed against tape speed, and there were some very good 8 mm stripe projectors on which post synchronisation could be carried out.

Since then there has been a great deal of movement in the design of cine cameras. 'Super 8' appeared and has been so successful (from the selling point of view at least) that there is only one manufacturer now who is



still making a standard 8 mm camera. It is all Super 8 now, with long range zooms, solid-state meter circuits, transistor speed control of the motor, fade shutters, and servo motors to operate the lens iris. You can pay up to £400 for a model in this gauge but, with the exception of the Pathe DS8 (this takes double Super 8), they will all be cartridge loading and thus incompatible with the design of a single-system magnetic stripe sound camera. The only Super 8 camera with a provision for sync-pulse operation with a small cassette recorder is the Zeiss-Ikon Moviflex S but this is not available in this country. Similarly, selling in France but not available here is the French made Phonimaj tape recorder. This is designed to operate with the Bauer D range of cine cameras and uses pulses fed through a multi-core cable to provide perfect synchronisation for 15 or 20 sequences on a 15 m film and to give synchronised sound to edited film and during editing, mixing or dubbing. The recorder is powered by six 1.5 V batteries; on location it is slung on a shoulder strap, the 8 cm spools being easily accessible at the top. Also in France, Pathe Movie Sonics offer the Erlson tape recorder originally designed to be used with the Pathe Webo 8 mm, 9.5 mm, and 16 mm cameras. A small impulse generator is mounted on a one turn to one picture shaft of the camera and relays its signals to a special control track on the recorder. A headset is supplied for monitoring on the spot, and for projection the pulse generator can be mounted on a 1-to-1 shaft on the projector. No more than two frames can slip at starting and this can be recovered almost immediately. The Erlson weighs less than 3 kg.

All very well for the French and Germans but what about us over here? Well, there is any amount of equipment that can be adapted for use with 8 mm providing that you have a budget to cover the cost. There are the Nagra and the Uher pulse-sync systems and the new generation Tandberg pulse-sync recorders that seem to be selling like hot cakes at the moment. There is also the fantastic (for me anyway) Perfectone with its crystal control (more about this later). But for those who want sync on 8 mm at very reasonable cost there are two very efficient units available, both British made, the Cinesound and the Synchronette.

The Synchronette, manufactured by *Films in Miniature Ltd., Romsey, Hampshire*, uses perforated tape to give automatic synchronisation between almost any electric drive camera, any gauge, any speed, and a mains or portable tape recorder. It can be used with a silent projector, to control its speed, and with a number of stripe projectors to provide automatic transfer of perforated tape to stripe. The scanning head of the Synchronette consists of a miniature exciter-lamp and a photo-electric cell. When the tape recorder is started, this scanning system reads the perforations and, by regulating the power supplied to the camera, automatically ensures that one frame of film moves through the picture gate for every tape perforation that passes through the scanning head. Thus camera and recorder are locked in sync. For sound editing, two other units may be added to the system, the *Editone* which plugs into the Synchronette and gives an automatic start and stop tone on the tape; and the *Edisync* which can be coupled to a sound or

silent projector or even to a film viewer.

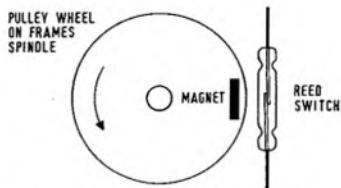
The Synchronette is only suitable for use with 16/18 f/s projectors, but it will control cameras at 24/25 f/s as well as 16/18 f/s; this will depend on the type of tape purchased. Prices of these units are: *Synchronette Mark II* £29 3s. 5d.; *Editone* £13 18s. 3d.; *Edisync* ½-track £48 10s. 3d.; *Edisync* ¼-track £50 18s. 11d. Slight modifications are needed to cameras and projectors. The camera needs to be fitted with two sockets for a simple plug-in lead from the synchroniser. The internal modification to the camera involves the fitting of a transmitter contact, driven by the camera's own mechanism. Films in Miniature can arrange for agents to carry out this conversion at a cost between £4 and £10, depending on the type of camera. The same with projector modification; the costs here being between £5 and £8.

The simplicity of the system is attractive. Editing is on a 'one for one' basis, i.e. one perforation of tape equals one frame of film so however many frames of film you remove, take the same number of tape perforations. With the addition of the Edisync you can have virtually professional editing facilities. Move the film backwards or forwards and the perforated tape follows it precisely, with every frame of tape locked to every frame of film. Also with the Edisync, accurate tape transfer is provided by means of a magnetic head wired to the miniature jack socket on the front panel. The Edisync will also synchronise a projector. All you have to do is to interrupt the film path through the projector by pulling out a loop of film ahead of one of the sprockets. This loop is threaded around the drive-sprocket of the Edisync which, in turn, drives the tape in perfect sync. Output from the Edisync may be fed into any amplifier and speaker system.

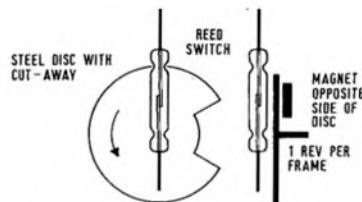
Synchropulse, pulse-sync, pilotton, neo pilot tone, call it what you will, gives greater flexibility than perforated tape and was invented and developed in this country by Norman Leevers who thus gave the film industry its first really portable sound equipment. Leevers-Rich synchropulse held sway for about ten years and then the two Swiss recorders, the Nagra and the Perfectone, the first all-transistor portable filmsound equipment, suddenly burst on the scene. These new recorders were designed mainly for newsreel work but they were soon recognised as being very suitable for many other kinds of sound filming and one or other of them became standard equipment on location, sometimes even being used for sync playback in the studios in place of the acetate disc. The first pulse-sync for the advanced amateur or small sponsored professional came in 1964 with the invention of the low cost, solid state, Carol Cinesound.

The Cinesound works on the following principle; if an electric motor is switched on and then off, the motor will obviously start running and then stop again, but if it is switched on and off continuously, then it will continue to run at a speed which will be slower than if it were fully switched on; if the time of this on/off cycle can be made to be in direct relationship to the frame speed of the projector, and the tape recorder made to perform the switching on and the projector the switching off, then the projector will run in 100% sync with the tape. (continued on page 473)

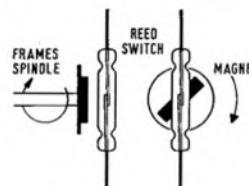
FIG. I TYPICAL METHODS OF PULSE GENERATION USING REED SWITCH AND MAGNET



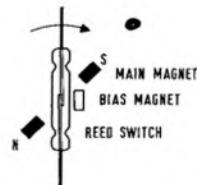
ROTATING MAGNET GLUED TO PULLEY WHEEL TO FORM A CAM SWITCH



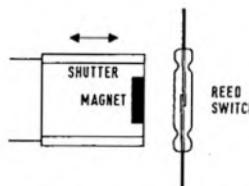
ROTATING SHUNT CAM SWITCH



ROTARY SWITCH WILL GIVE TWO PULSES PER FRAME

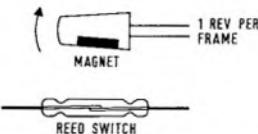


ROTARY SWITCH WITH BIAS MAGNET WILL GIVE ONE PULSE PER FRAME



MAGNET ON RECIPROCATING SHUTTER TO GIVE ONE PULSE PER FRAME

INCHING KNOB



MAGNET GLUED TO INCHING KNOB TO GIVE ONE PULSE PER FRAME



Model MR-990

Solid state mains stereo/mono tape recorder

Solid state, 14-transistor circuitry delivering 10 watts maximum music power per channel. 4-track monaural/stereo operation. 3 speeds controlled by single change lever. Greatest tape economy: 8 hours on one 7" reel at 4-track monaural operation. Varied applications: recording from tuner, turntable, or microphones. Playback through loudspeakers supplied or separate amplifier. Other facilities include sound-on-sound, sound-with-sound, pause control and automatic shut-off device. Line output socket and 5 pin DIN (rec./pb) socket. Headphone and speaker jacks on front panel.

SPECIFICATIONS

Recording system:

AC bias $\frac{1}{8}$ track

Erasing system:

AC erasing $\frac{1}{4}$ track

Tape speeds:

$7\frac{1}{2}$ ips (19cm/sec)

$3\frac{3}{4}$ ips (9.5cm/sec)

$1\frac{7}{8}$ ips (4.8cm/sec)

Wow & flutter:

$7\frac{1}{2}$ ips: 0.15% R.M.S.

$3\frac{3}{4}$ ips: 0.20% R.M.S.

$1\frac{7}{8}$ ips: 0.30% R.M.S.

Recording time:

96 min at $7\frac{1}{2}$ ips

(stereo 7" 1200ft. tape)

192 min at $3\frac{3}{4}$ ips

(stereo 7" 1200ft tape)

384 min at $1\frac{7}{8}$ ips

(stereo 7" 1200 ft. tape)

Level indication:

VU meter x 2

Output power:

Music: 10W x 2. Undistorted: 5W x 2

Frequency response:

$7\frac{1}{2}$ ips: 20-21,000 c/s

(± 3 db 30-16,000 c/s)

$3\frac{3}{4}$ ips: 30-13,000 c/s

$1\frac{7}{8}$ ips: 30-9,000 c/s

Signal-to-noise ratio:

45 db

Cross talk:

50 db (channel-channel)

Output impedance:

Ext. SP: 8 ohm x 2

Line out: 1k ohm x 2

Headphone: 10k ohm or 8 ohm

Microphone:

Dynamic microphone

Speakers:

4" (10cm) free edge permanent

dynamical speaker x 2

Monitor:

Headphone or speaker

Power source:

AC 100V, 117V, 125V, 220V, 240V

Dimensions:

Main unit 20" (w) x 10" (d) x 16" (h)

Speaker boxes: 9 $\frac{1}{2}$ "(w) x 5 $\frac{1}{2}$ "(d) x 16" (h)

Weight:

35.2 lbs. (17kg)

The MR-990 is available from the Sanyo dealer in your area, specially selected for first-class before-and-after-sales service. Or you can write for illustrated leaflet to :

Sanyo Marubeni (U.K.) Ltd.,
Bushey Mill Lane, Watford, Herts.
Telephone : 92 25355.

 **SANYO**

People the world over agree there's something about a Sanyo



... about local radio

From: Nigel Fell, BBC Radio Leeds, Merrion Centre, Leeds 2.

Dear Sir, I feel compelled to write in reply to the article 'Local Radio' in your September edition.

Mr Wright claims '... many amateur enthusiasts can claim a quality better than is possible in Local Radio'.

The signal transmitted by Radio Leeds is flat up to 18 kHz, as compared with the 9 kHz of Holme Moss. At 19 kHz a 35 dB attenuation is inserted into the circuit to prevent unwanted triggering of stereo decoders on domestic receivers.

The programmes are monitored in Studio 1 through a Goodmans *Tri-axiom* loudspeaker and I defy anybody to tell the difference between the Studio output and the check transmitter receiver.

Mr Wright finds it unwise to attempt anything musically ambitious. In Studio 2 we employ up to seven microphone channels plus additional facilities such as echo, reverberation, and double tracking. A response selection amplifier (RSA) is employed to give any desired effects which we might choose to use in pop music.

Monitoring in Studio 2 is carried out through an *LSU/10*, which is generally acknowledged as the finest unit of its kind in the world.

Successful recordings of pop groups of ten have been made. Four is common.

Other musical programmes are recorded on location, again using up to seven microphones, and the total output of local music amounts to over four hours a week of the best of jazz, country and western, folk, serious and popular music.

Yours faithfully,

... about a microphone amplifier

From: Anthony Eden, 1 Lambolle Road, Swiss Cottage, London N.W.3.

Dear Sir, With reference to F. C. Judd's article in the September issue entitled 'Pre-amplification and Mixing', I should like to make a few small points which I think may have slipped his attention.

1. The current consumption of the unit shown in fig. 1 is slightly under 4 mA not 2 mA as stated. The second stage alone consumes about 3.6 mA.

2. His statement 'It will operate with a 200

ohm microphone, but at reduced sensitivity' is misleading. Since the 200 ohm microphone is working into virtually open circuit, the sensitivity of the microphone cannot be reduced. The gain of the amplifier is independent of the input impedance and consequently its gain cannot be reduced. What then is operating at reduced sensitivity? What I think he means is that the output of a normal 200 ohm microphone is not sufficient to load fully the input to the amplifier without the introduction of considerable noise. A typical output from such a microphone is about 0.2 mV and this will reduce the signal-to-noise ratio to about 38 dB.

3. A typical signal input level of 3 mV will be amplified to 350 mV. It can be readily demonstrated that the overload point of the amplifier occurs at 2.1 V output. This means that the overload factor is $\frac{2.1}{0.35} = 16$ dB. This figure is far

too narrow for microphone operation and a figure of 30 dB at least is required if peaks from the microphone are not to be clipped. The only practicable solution is to use the amplifier with an input not exceeding 500 μ V. (i.e. from a microphone of 0.5 to 2 K impedance). The signal-to-noise ratio is then about 45 dB.

4. He quotes a signal-to-noise ratio of 60 dB and quotes an input impedance of 100 K so presumably the noise has been measured with this value of input resistor. Now, 60 dB below an output of 350 mV is 350 μ V. This means that, since it has been amplified 120 times, the noise of the input resistor will be less than 3 μ V (for a 0 dB NF Amplifier). However, the noise generated by a 100 K resistor measured on a 20 kHz bandwidth at 300°K is 5.5 μ V. Thus, as it stands, the value of 60 dB is meaningless and this indicates that either the measurement was made on a restricted bandwidth or with an input resistor of less than 100 K. I should be most grateful to know how the measurement was made.

5. He states '... slight changes in component value may be necessary for optimum performance. It is recommended that only the transistors specified are used'. What is optimum performance? You may like to criticise the following analysis, but as I see it the circuit is independent of the transistor parameters and depends solely on the feed-

back resistors R_4 , R_1 and R_3 . The equivalent circuit of fig. 1 may be represented as follows: Using Nodal Analysis we have:

$$\begin{aligned} Is &= (G_s + Y_{ie_1}) V_1 - Y_{ie_1} V_2 \\ 0 &= -G_s V_2 + Y_{fe_2} V_3 + (G_4 + G_L) V_4 \\ 0 &= -(Y_{ie_1} + Y_{fe_2}) V_1 + (Y_{ie_1} + Y_{fe_2} + G_4 + G_1) V_2 - G_x V_4 \\ 0 &= Y_{fe_2} V_1 - Y_{fe_2} V_2 + (G_2 + G_L) V_4. \end{aligned}$$

The ratio of $\frac{V_4}{V_1}$ is required for gain of the amplifier. This can be solved either by solving the above four equations or more elegantly by solving the equations using a determinant of the circuit. The result of this is that, to a reasonable approximation $\frac{V_4}{V_1} = 1 + \frac{G_1 + G_3}{G_4}$. Since $R_1 \gg R_3$ this approximates to

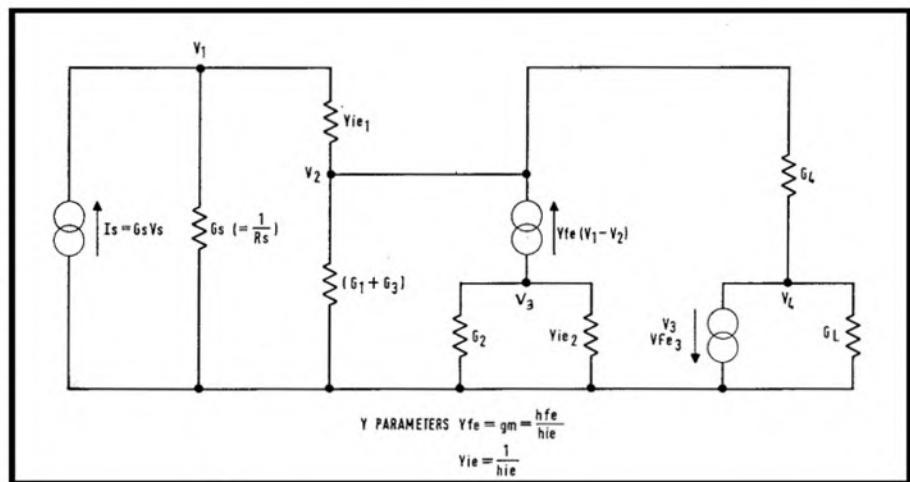
$$\frac{V_4}{V_1} = \frac{R_4}{R_3}$$

This means that, to a good approximation, the gain depends solely upon the values of R_4 and R_3 and is therefore 120 times or 41.6 dB. Therefore any transistor can be used that satisfies the DC operating conditions (almost all *n-p-n* silicon transistors) and in fact any good low noise transistor could be used. Close control of the values of R_4 and R_3 will closely control the performance of the circuit up to at least 20 kHz.

Basically, this type of 'voltage output-series input' circuit is one of the best and most stable circuits on the market except that the circuit has been incorrectly used as a microphone amplifier. Mullard in their manual describe better circuits from a matching, noise, and distortion point of view than the one Mr Judd described.

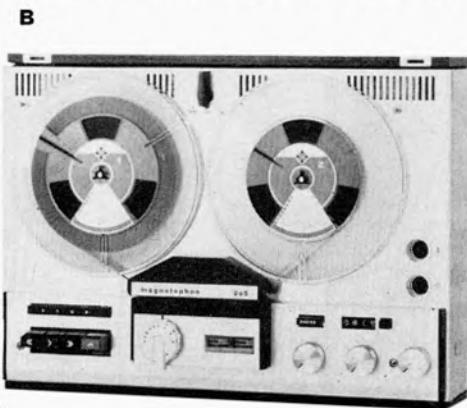
Yours faithfully,

A copy of this letter was forwarded to Mr Judd who offered no comment.—Ed.



AUDIO FAIR '69

A PREVIEW OF NEW RECORDING EQUIPMENT AT THE OLYMPIA INTERNATIONAL AUDIO AND PHOTO-CINE FAIRS 1969



A Sony 50 Compact Cassette recorder.
B Telefunken 205 stereo.
C Tandberg 6000X stereo tape unit.

THE largest exhibition of sound equipment ever launched in this country opens on Thursday October 16 at the London Olympia. Eighty-seven companies representing the audio industry are collaborating with fourteen from the photographic industry at the *International Audio and Photo-Cine Fairs 1969*.

The Audio Fair dates back to 1956, when an off-shoot of the British Sound Recording Association Exhibition was held at the Washington Hotel in Curzon Street. (The first BSRA Exhibition, for the record, was held in May 1948 at the St. Ermin's Hotel.) In 1957 the Audio Fair took place at the Waldorf Hotel and in 1959 at the Hotel Russell. But even this, seven floors spanning the full width of Russell Square, proved in the end too small for the thousands of visitors the fair attracted.

Moving to Olympia solves the space problem aggravated at the Russell by queueing in its narrow corridors. Demonstration room dimensions will be consistent, approximately 5 x 6 m,

each housing up to 30 seats set out in five rows of six.

The success of the 1969 Fair will depend largely on the effectiveness of the acoustic insulation provided by the demonstration room structures. A mixture of hardboard and plasterboard is being used for the walls, each ceiling being of hardboard alone. The flooring will be felt-covered concrete. Ventilation will rely on an extractor fan.

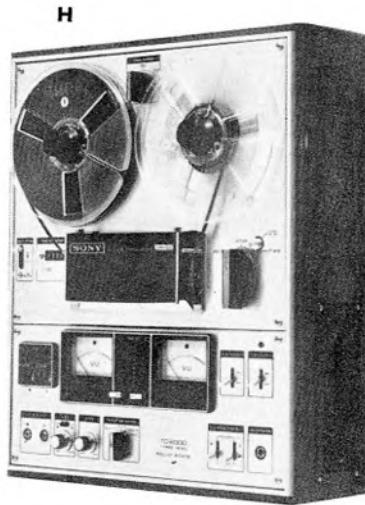
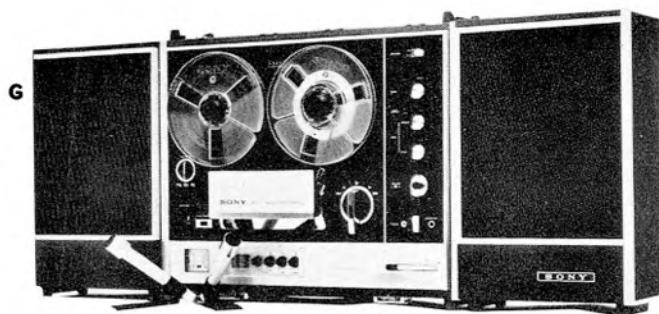
This will not be the first attempt to demonstrate audio equipment in a large exhibition hall. Some years ago, Daystrom set up a listening room at Olympia for the *Do It Yourself Exhibition*. The venture was not entirely successful we learn from the Editor of *DIY*, since the acoustic isolation failed to keep out extraneous noise, mainly from machine tools. These same tools created mains interference. Some visitors complained of inadequate ventilation. At Düsseldorf last year, however, prefabrication techniques were used

with much greater success in a 'one roof' audio exhibition. Ventilation there was shelved in favour of piped refrigeration.

The Russell Hotel Audio Fairs were aimed mainly at audio enthusiasts, tickets being circulated mainly through equipment retailers. This year, the exhibition is being aimed at a wider public through advertising on television and in non-specialist publications. Admission, previously free, is now 4s. per head, children 2s.

A trade and press preview from 10 a.m. to 4 p.m. precedes the public opening of the audio section, 4 p.m. to 9 p.m. on Thursday 16. Opening times are 10 a.m. to 9 p.m. on Friday 17, Saturday 18, and the following Monday, Tuesday and Wednesday. The exhibition will be closed on the Sunday.

An underground shuttle service will operate throughout the exhibition period between Kensington and Olympia. Bus routes passing the hall are 701, 702, 704, 705, 714, and 716 (green) and 9, 27, 28, 49, 73 and 91 (red).



D Brenell ST200 stereo.
E Sony 106.
F and J Melodium microphones.
G Sony 560 stereo.
H Sony 630D stereo tape unit.
I Sony 252D stereo tape unit.

A 'ten minute long explosion of sound' accompanied by colour pictures of London has been prepared by Agfa-Gevaert to demonstrate their new PE.36 LP, PE.46 DP and PE.66 TP low-noise tapes. These are being marketed alongside their standard range and cost 5% to 10% more.

Keith Monks (Audio) Ltd., exhibiting under the Audio & Design trade name, will display a range of Melodium microphones they are now importing from France. These range from a studio ribbon model at £45 to a Lavalier microphone at £9 4s. 3d.

Visitors to the BASF room will be invited to hear on headphones a selection of music 'For a City' and to take away a $\frac{1}{2}$ -track stereo copy. LP 35LH, DP 26LH and TP 18LH low noise tapes will be displayed alongside Compact Cassettes in the new KK8 container, described as ideal for tape correspondence.

Centrepiece of the Bang & Olufsen demonstration will be the new 2400, a $\frac{1}{2}$ -track stereo

recorder operating at 19, 9.5 and 4.75 cm/s. Hyperbolic heads and silicon transistor circuitry are claimed to contribute to a 60 dB signal-to-noise ratio at 19 cm/s with low noise tapes. Four pairs of slide potentiometers govern microphone, radio, gramophone and line inputs, a fifth pair controlling output level from the internal power amplifiers.

The recently introduced ST200 transistor stereo recorder will be demonstrated by Brenell. Retailing at £145 including tax, it operates at 19, 9.5 and 4.75 cm/s and accommodates spools of up to 21 cm diameter. Three outer-rotor motors are employed, the capstan motor being hysteresis synchronous. 19 cm/s specification includes 0.08% wobble, 40 Hz to 14 kHz ± 2 dB frequency response, 56 dB weighted signal-to-noise ratio, 60 dB crosstalk rejection (with HF bias on second track) and 3% third-harmonic distortion. Output power from the internal amplifier is 6 W RMS per channel, bass and treble controls providing -14 to +10 dB

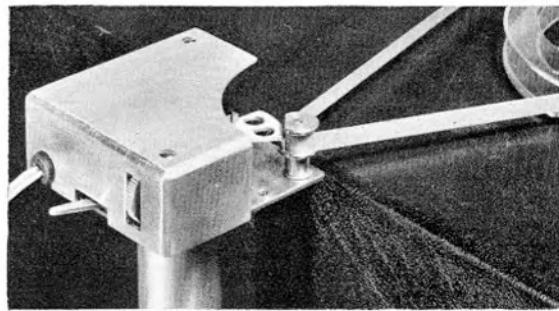
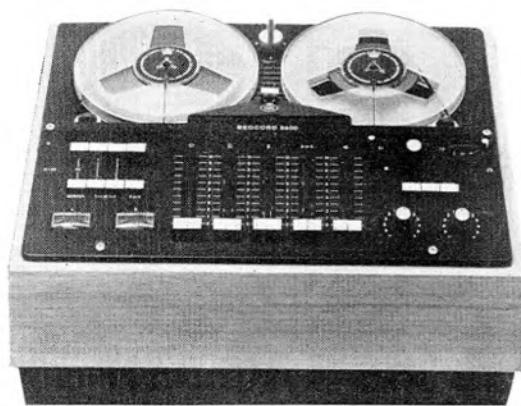
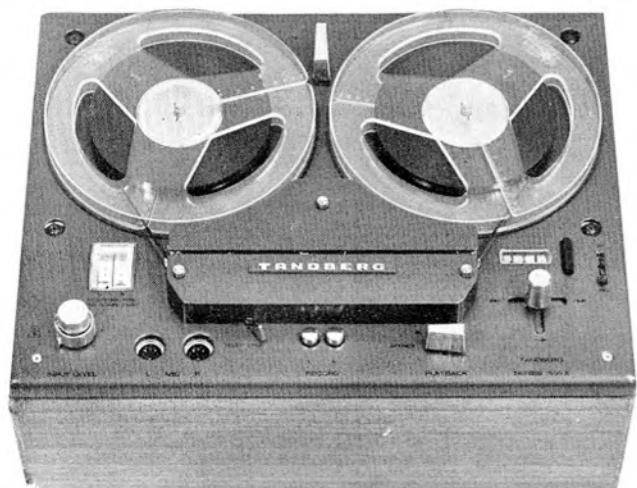
at 100 Hz and -18 to +5 dB at 10 kHz respectively. The tone controls operate during both record and play. Input sensitivities are 50 μ V at 200 ohms (microphone) and 40 mV at 220 K. Outputs are 200 mV into 47 K (external amplifier), 2 V at 100 ohms (headphones or external amplifier) and 15 ohms (external loudspeaker).

The presentation of British Amateur Tape Recording Contest prizes will be made at the Audio Fair by Mr. Douglas Brown.

A universal synchroniser for tape recorders and automatic relay-change slide projectors will be shown for the first time by Colton, in addition to a tape storage rack and an extensive range of gramophone accessories.

No new recorders are expected from Dual and the company's tape interests will be represented by the TG28 stereo tape unit. This relatively low-price design incorporates supply and take-up tension servos and operates at 19 and 9.5 cm/s.

(continued overleaf)



M

K Tandberg 1600X stereo tape unit.

L Trio TT-10 stereo tape unit.

M Bang & Olufsen 2400 stereo.

N Colton universal slide synchroniser.

N

A highlight of the 1968 Audio Fair for many visitors must have been the introduction of the Ferrograph *Seven* series of recorders. The series was not given a formal demonstration last year, the emphasis then being on encouraging visitors to see and handle the mechanism at close hand. Eight versions of the *Series Seven* are available, varying in price from £174 13s. 6d. to £212 7s. 6d. All carry tax though a tax free *Series Y* range is available for industrial application.

Eight recorders will be displayed and demonstrated by Grundig, including the C200, a cassette battery portable costing £36 17s. 6d. and a $\frac{1}{2}$ -track reel-to-reel machine, the £55 18s. 10d. TK149.

Two new stereo ribbon microphones, the 4-25 and 4-35, will be on show at the Lustraphone stand. Also to be displayed are the established *Series Four* ribbon and dynamic models, the noise-cancelling twin-ribbon 4-70, and a range of stands, mounts, booms and accessories.

Splicers for 6.25 mm and 12.5 mm tape will be seen on the Multicore stand. The Bib range of audio accessories also includes head cleaning kits, several permutations of fluid applicators,

brushes, tissues, polishers and anti-static fluid. Prices are from £3 9s. 6d., a kit intended for studios and service organisations, to 9s. 9d.

All six headphones in the American Koss range will be demonstrated by the importers, Tape Music Distributors Ltd. Model *ESP-9* incorporates capacitor transducers and, built into one earpiece, self-polarizing circuitry. This takes its energy from the audio signal itself or from a separate AC line. Claimed frequency response is 15 Hz to 15 kHz ± 2 dB with 0.2% THD at 110 dB SPL. The headphones work from 4 to 16 ohm amplifier power outputs and cost £69. Other Koss models, moving-coil, are the £45 *ESP-6*, £37 10s *ESP-7*, £23 *PRO-4A*, £16 10s. *KO727* and £12 10s. *K-6*.

A $\frac{1}{2}$ -track stereo recorder with a comparatively low price, £76 10s. including tax, will be shown by Philips. Designated the 4404, it operates at 19, 9.5 and 4.75 cm/s and accepts 18 cm spools. The 4407 costing £101 19s. 4d., has more elaborate tone controls and mixing facilities, independent level meters on each channel and greater output power. Most versatile of the Philips domestic range is the *PRO-12*, aimed

at the keen amateur and priced at approximately £235 including tax. Tape speeds are 19 and 9.5 cm/s.

Revox, who have hitherto specialised solely in recording equipment, will this year demonstrate the A.50 40 W continuous sine-wave per channel amplifier and A.76 FM IC/transistor hybrid stereo tuner. Prices are £103 19s. (A.50) and £156 9s. (A.76). The A.77 recorder in its domestic form varies from £187 19s. (stereo unit in wood or metal surround) to £223 13s. (internal amplifiers and speakers). NAB versions for studio/industrial applications start at £138 tax free. Visitors to the Revox room will be able to make their own recordings, monitoring on headphones.

Seven mains $\frac{1}{2}$ -track stereo recorders and a series of battery portable reel-to-reel and cassette machines are to be exhibited by Sanyo. Prices are £132 5s. (MR-990), £112 5s. (MR-939), £101 5s. (MR-999), £97 5s. (MR-929), £90 15s. (MR-151 stereo mains/battery and MR-800), £84 15s. (MR-910) and £79 15s. (MR-801).

No less than 13 new recorders will be

AUDIO EXHIBITORS

Trade Name	Manufacturer or Distributor	Location
Agfa-Gevaert	Agfa-Gevaert Ltd.	Upstairs North
Alwa	Alwa Co. Ltd.	Downstairs
Akai	Rank Organisation	Upstairs North
Arena	Highgate Acoustics	Downstairs
Armstrong	Armstrong Audio Ltd.	Upstairs South
Audio & Design	Keith Monks (Audio) Ltd.	Downstairs
Audio Packs	Tape Recorder Spares Ltd.	Upstairs South
Audio Record Review	Heathcock Press Ltd.	With Hi-Fi News
Audio Technica	Shiro (UK) Ltd.	Upstairs North
BASF	BASF (UK) Ltd.	Upstairs North
B & O	Bang & Olufsen (UK) Ltd.	Downstairs
B & W	Bowers & Wilkins Electronics Ltd.	Downstairs
Brenell	Brenell Engineering Co.	Downstairs
BBC	British Broadcasting Corporation	Downstairs
BSR	BSR Ltd.	Upstairs South
Bush	Rank Bush Murphy Ltd.	Upstairs North
Celestion	Rola Celestion Ltd.	Upstairs North
Colton	Colton & Co. (Lapidaries) Ltd.	Downstairs
Connoisseur	A. R. Sugden & Co. Ltd.	Upstairs North
Decca	Decca Record Co. Ltd.	Upstairs South
Diamond Stylus	The Diamond Stylus Co. Ltd.	Upstairs South
Dual	Dual Electronics Ltd.	Downstairs
Electrical & Electronic Trader	Illié Ltd.	With Wireless World
EMI	EMI Electronics Ltd.	Upstairs South
FBTRC	Federation of British Tape Recordists and Clubs	Downstairs
Ferguson	British Radio Corporation Ltd.	Upstairs North
Ferranti	Ferranti Ltd.	Upstairs North
Ferrograph	The Ferrograph Co. Ltd.	Upstairs South
Garrard	Garrard Engineering Ltd.	Upstairs North
Goldring	Goldring Manufacturing Co. Ltd.	Upstairs South
Goodmans	Goodmans Loudspeakers Ltd.	Upstairs North
The Gramophone	General Gramophone Publications Ltd.	Downstairs
Grundig	Grundig (GB) Ltd.	Upstairs North
Hacker	Hacker Radio Ltd.	Downstairs
Heathkit	Daystrom Ltd.	Upstairs North
HFDA	Hi-Fi Dealers Association	Downstairs
Hi-Fi News	Link House Publications Ltd.	With Tape Recorder
Hi-Fi Sound	Haymarket Press Ltd.	Upstairs North
High Fidelity Magazine	Billboard Publications Ltd.	Upstairs South
HMV	British Radio Corporation Ltd.	Upstairs North
Howland-West	Howland-West Ltd.	Downstairs
Jordan-Watts	Boosey and Hawkes (Sales) Ltd.	Downstairs
KEF	KEF Electronics Ltd.	Upstairs South
Koss	Tape Music Distributors Ltd.	Downstairs
Leak	H. J. Leak & Co. Ltd.	Upstairs South
Lowther	Lowther Manufacturing Co. Ltd.	Upstairs North
Lustraphone	Lustraphone Ltd.	Upstairs North
Lux	Shiro (UK) Ltd.	Upstairs North
Luxor	Highgate Acoustics	Downstairs
MB Microfonbau	Denham & Morley Ltd.	Downstairs
Metrosound	Metrosound Manufacturing Co. Ltd.	Upstairs South
Mordaunt-Short	Mordaunt-Short Ltd.	Upstairs South
Mullard	Mullard Ltd.	Downstairs
Multicore	Multicore Solderers Ltd.	Upstairs South
Ortofon	Metrosound (Sales) Ltd.	Downstairs
Peerless	P. F. & A. R. Holme Ltd.	Upstairs North
Perdio	Dansette Products Ltd.	Upstairs North
Philips	Philips Electrical Ltd.	Upstairs North
Philips Records	Philips Records Ltd.	Downstairs
Pickering	Highgate Optical & Industrial Co. Ltd.	Downstairs
Pioneer	Swisstone Ltd.	Upstairs South
Practical Electronics	IPC Magazine Ltd.	Downstairs
Practical Wireless	IPC Magazine Ltd.	With Practical Electronics
Quad	Acoustical Manufacturing Co. Ltd.	Upstairs South
Record Housing	N. & S. B. Field & Co.	Upstairs North
Records & Recording	Hansom Books Ltd.	Downstairs
Revox	Revox Ltd.	Upstairs North
Rotel	Rank Organisation	Upstairs South
Richard Allan	Richard Allan Radio Ltd.	Upstairs North
Sansui	Brush Cleelite Co. Ltd.	Downstairs
Sanyo	Marubeni-Ilda	Upstairs South
Scotch	Minnesota Mining & Manufact'g Co. Ltd.	Upstairs North
Shure	Shure Electronics Ltd.	Downstairs
Sinclair	Sinclair Radionics Ltd.	Upstairs North
SME	SME Ltd.	Upstairs North
Sony	Sony (UK) Ltd.	Upstairs North
Tandberg	Elstone Electronics Ltd.	Upstairs North
Tape Recorder	Link House Publications Ltd.	Downstairs
Tape Recording Magazine	Print & Press Services Ltd.	Upstairs North
Teac	B. H. Morris & Co. (Radio) Ltd.	Upstairs South
Telefunken	AEG (GB) Ltd.	Upstairs South
Teleton	Teleton Electro (UK) Ltd.	Downstairs
Thorens	Metrosound (Sales) Ltd.	Upstairs South
Toshiba	Hanimex (UK) Ltd.	Upstairs South
Transcribers	Transcribers Ltd.	Downstairs
Trio	B. H. Morris & Co. (Radio) Ltd.	Upstairs North
Uher	Bosch Ltd.	Upstairs North
Wharfedale	Rank Wharfedale Ltd.	Upstairs North
Whiteley	Whiteley Electrical Radio Co. Ltd.	Upstairs South
Wireless World	Illié Ltd.	Downstairs
Yamaha	Actina Ltd.	Downstairs

Constructing a Capacitor Microphone

John Penty describes an easily built omni-directional unit

TO produce a tape comparable in quality with that of a professional studio the advanced amateur recordist often lacks only one item of equipment—a high-grade capacitor microphone. His actual machine, although not as rugged and capable of giving day-in and day-out high quality performance as the studio equipment, is usually capable of providing a frequency response of 40 to 18 kHz ± 3 dB at a decently low level of distortion and noise. This frequency response is considerably better than most dynamic or ribbon type microphones in the £15 to £20 price bracket. It is true that capacitor microphones are available for less than £50 but the cost of the well-known makes is very much higher.

This constructional article is the outcome of many months of experiments to create a capacitor microphone using an FET head amplifier and powered from dry batteries. The results have proved that, with only a lathe, drilling machine, small tools and reasonable skill, such a microphone can be produced giving a performance very close to that obtained from the best professional models.

The case is a 4½in. length of ¼in. diameter copper water pipe, machined square at each end. The cap that holds the capsule is in two parts turned from 25mm brass rod. The short sleeve is bored to a push fit on the copper tube to the sizes shown in the diagram and a thread screw cut between 45 and 50 turns per inch, depending on the lathe wheels available. This is pressed and soldered to one end of the tube with 1/8in. of thread beyond the end of the tube. The cap is next machined to size and screw cut inside to an easy fit on the

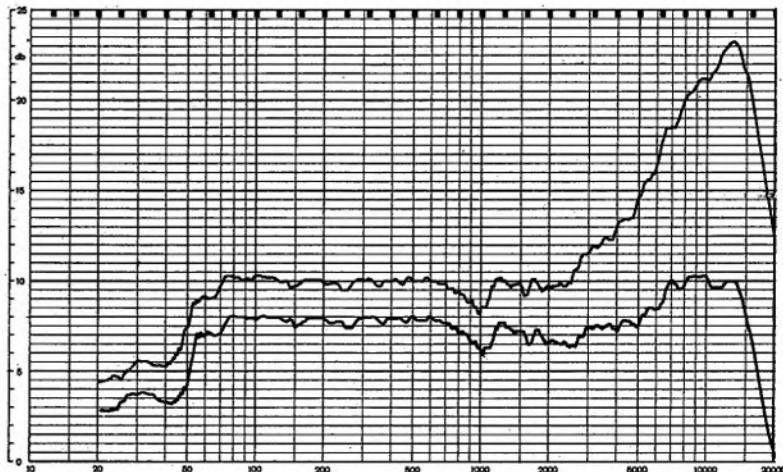
sleeve. When completed the capsule is gripped between cap and sleeve and this in turn holds the amplifier board, which is screwed to the back of the capsule.

To complete the case, the base ring is turned a sliding fit in the ¾ in. tube; this is then drilled to take a four-core screened cable, either standard or light gauge, or opened out to a press fit for a five-pin DIN socket, as shown in the photograph. The ring is held in place by a 10 BA screw. The cap is finished by fitting a disc of fine copper gauze in the front recess

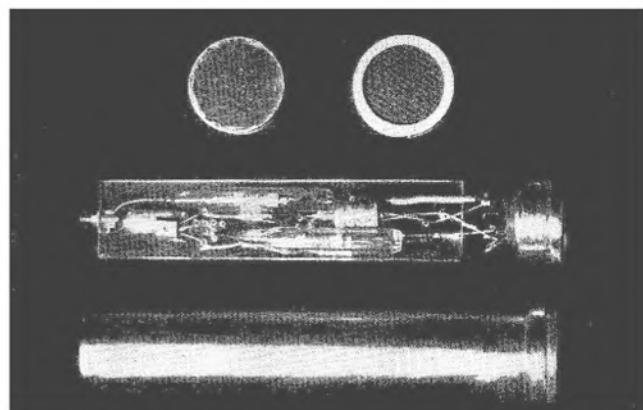
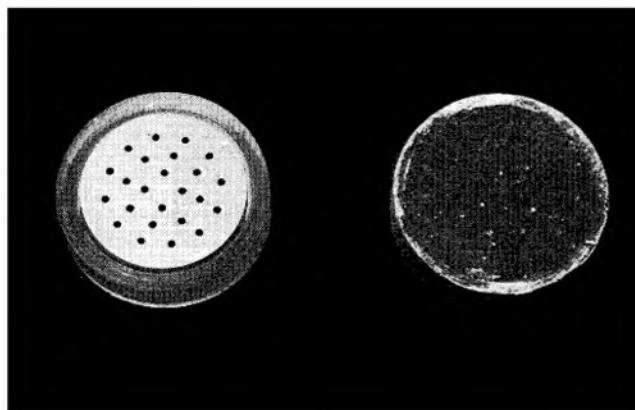
and securing with solder. The completed case can now be chromium-plated.

Making the capsule demands care, good machining and thorough cleaning. The back-plate is turned from Dural rod and after turning to size the positions for the acoustic holes are centre punched. These are indexed by employing a 24-tooth gear wheel on the lathe spindle or by a dividing head. With a 24-tooth wheel, every sixth, third or second tooth will index 4, 8 and 12 hole positions.

To centre punch accurately a simple punch



B & K frequency response traces with 0.25 μF capacitor at output (lower curve) and without capacitor.



Editor's Note : Readers wishing to construct capacitor microphones suitable for crossed-pair stereo recording to await Trevor Attewell's cardioid design which will be described in the January and February issues.

guide held in the tool post is required. This consists of a piece of $\frac{1}{8}$ in. square steel a few centimetres long drilled across one end with a $\frac{1}{16}$ in. diameter hole. The punch is 2in. of $\frac{1}{8}$ in. silver steel with a point ground at one end. This slides in the hole and the assembly is held in the tool post with the punch point level with the centre of the work. The top slide is now wound back $\frac{1}{16}$ in. and at each of the four hole positions a light tap on the punch will produce a clean and accurate mark for drilling. After repeating this operation for the middle and outer rings of holes, the blank is parted or sawn off and the back cleaned up and drilled and tapped to 10 BA. To drill holes of 0.035 inch diameter and $\frac{1}{8}$ in. deep requires a drill running at high speed fitted with a depth stop. Most electric drills can be adapted to do this.

As a broken piece of drill can rarely be got out of a hole, special care must be taken to avoid this happening. Use plenty of thin oil and withdraw the drill frequently to clear the flutes for each hole. The final finish on the backplate is obtained by grinding the face flat on either a new fine oilstone or on a piece of very fine wet and dry paper on a sheet of glass. When finished the face should be flat with a fine matt surface. All traces of dirt and grinding paste must now be cleaned away by washing in petrol or cellulose thinners, prodding each hole with a wire until quite clean. The Perspex ring is now turned to size and bored to a press fit for the backplate. At the same time as boring, a skin is taken across the front face of the ring, on which the diaphragm will be stuck. The backplate is now given a smear of Araldite

and pressed into the ring from the back. To set the gap at 37μ (1.5 thou.), a feeler gauge of this thickness is used to space the backplate from a piece of flat ground steel held across the front face of the capsule. Allow about 24 hours for this to set.

The diaphragm has now to be stuck on to the capsule. This diaphragm is a piece of 25 gauge Melinex aluminium sputtered on one side. As this material is only 6μ thick it is very difficult to handle, but the method now to be described has been found simple and straightforward in practice. Cut a $1\frac{1}{2}$ in. hole in a 2in. square of 18 or 20 gauge aluminium sheer, lightly coat around the hole with Evostik and attach a 2in. square of Melinex over the hole with the metallised side to the plate. When set this can be turned over and placed over the capsule, plain side to the backplate. Pressure with a weight of 4 oz. will now stretch the Melinex evenly and at the correct tension. A very thin and smooth film of Araldite is applied around the Perspex edge of the capsule after again checking for ingress of dust or dirt. Then press the capsule in the centre of the Melinex, turn over and apply the weight. Leave this assembly to set for at least 24 hours before trimming the edge with a razor blade and removing the capsule from the ring. When assembled the capsule circuit is completed by the aluminium sputtering on the outside of the Melinex being earthed by the cap.

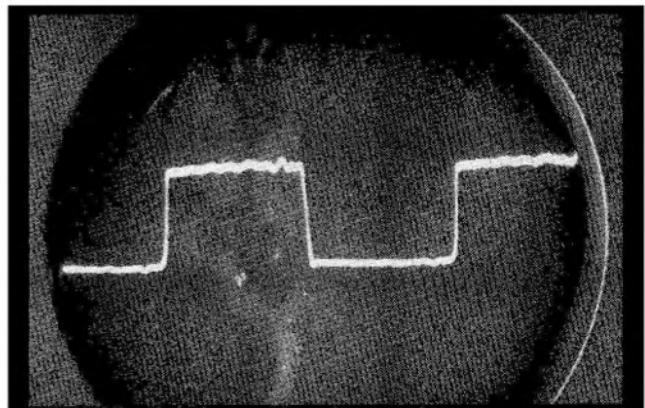
The head amplifier consists of a high input impedance FET followed by a *p-n-p* transistor as a cathode follower. The capsule capacity is about 50 pF giving it an impedance of over 60 M at 50 Hz. The amplifier input impedance

has, therefore, to be at least double this value. This calls for two high value resistors in the input. These are normally difficult to find and expensive. Fortunately, a supply of glass encapsulated resistors of values between 125 M and 1,000 M is available from Proops and any two of these resistors between the values stated seem to work well in this amplifier.

The insulation of all components in the input circuit, including the panel board has to be of a very high order to keep noise (hiss) to a minimum level. Therefore, $\frac{1}{8}$ in. Perspex is used for the components board. This is drilled and tapped 10 BA in the centre of one end and a 10 BA screw put in and the head cut off. A small brass solder tag is locked in place with a 10 BA nut and $\frac{1}{16}$ in. of thread left to screw into the capsule. The suggested layout for components (see sketch) has been found to work well and allow room for the completed board to slide into the $\frac{1}{8}$ in. diameter tube. The output impedance is about 100 ohms and the microphone feeds into a 200 ohm unbalanced line.

The microphone is powered by a 9 V PP4 battery for the amplifier and two 22.5 V and one 15 V flash-gun batteries for the capsule polarizing voltage. These can be mounted in any convenient box. A small panel with spring contacts to connect the flash batteries is required, with an Octal or DIN socket on this box to act as a switch and connector for the 2 m of four-core cable. A screened output lead from the box can be terminated with a jack plug to connect with further cable, if required.

First tests on samples of the completed
(continued on page 455)



New Tandberg 1600X stereo tape deck

4 tracks. Frequency response:
40 - 18,000 ; 40 - 14,000 ;
40-8,000 cycles \pm 2dB at $7\frac{1}{2}$,
 $3\frac{3}{4}$ and $1\frac{7}{8}$ i.p.s. respectively.
Signal - to - noise ratio better
than - 55dB - 53dB and - 52dB
at $7\frac{1}{2}$, $3\frac{3}{4}$ and $1\frac{7}{8}$ i.p.s. respectively.
Wow and flutter less
than 1 R.M.S., .15 R.M.S. and,
35 R.M.S. at $7\frac{1}{2}$, $3\frac{3}{4}$ and $1\frac{7}{8}$ i.p.s.
respectively. Cross talk better
than - 60dB. .9v output per
channel. Teak cabinet. £89.10.0

Send me full details

NAME

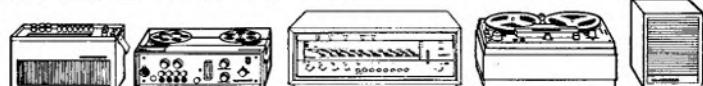
ADDRESS

Farnell - Tandberg Dept.TR5
Hereford House
Vicar Lane, Leeds 2



Cross-field bias head. Under £90

move up to **Tandberg**



Farnell-Tandberg Ltd., Hereford House, Vicar Lane, Leeds 2.

CAPACITOR MICROPHONE CONTINUED

microphone showed that the capsules had a rising HF response. This was confirmed later when, with the co-operation of friends with access to B & K frequency response recorders, some pen recordings were made in an anechoic chamber. Fortunately, the shape of the response was such that suitable correction only needed a 0.2 μF to 0.4 μF capacitor across the output of the head amplifier, the chosen value being dependent on the individual listening response obtained and personal preferences in sound quality. Incidentally, this capacitor is best housed in the battery container as it is unlikely that the microphone case can accept it.

The bass end is very flat right down to 30 Hz. Additional checks were made with electrostatic excitation* of the diaphragm and a 1 kHz. square wave displayed on a CRO showed the remarkably flat overall response.

The finished microphone has now been in regular use for several months and has been put into active service at a number of recording sessions. At these sessions, the opportunity was taken to compare its performance with other high-grade microphones from reputable manufacturers, including the STC 4038. The sound was monitored on a Quad ELS speaker and on A. R. Bailey's *Wireless World* design studio speaker system. The principal aural impression is one of extreme clarity and naturalness. Sounds with steep wavefronts, such as the triangle, the tympani, and certain instruments of the brass section, take on a vividly realistic presence when picked up by this capacitor microphone. Speech reproduction is natural with no excessive sibilance.

The finished microphone is robust and free from microphony and hum induction. If balanced line output is required, a 1:1 transformer can be fitted in the battery box.

In conclusion, I would like to extend my thanks to Mr. D. E. O'n. Waddington for the head amplifier circuit, which formed part of the sensitive FET Voltmeter design in *Wireless World*, May 1968.

**Electrostatic Excitation for Capacitor Microphones*; from "Acoustical Techniques and Transducers" by M. L. Gayford, Macdonald & Evans, 1961. (Appendix IV, page 349.)

COMPONENTS

Transistors:

T₁: 2N 3819 R₁: 250 M (from Proop Bros. Ltd.,
T₂: 2N 3702 R₂: 250 M 52 Tottenham Court
Road, London, W1 P0BA)
or any value between 125 M to 1,000 M

Resistors:

R₃: 12 K
R₄: 2.7 K (0.25 W, low noise)
R₅: 1.5 K

Capacitors:

C₁: 1000 pF Polystyrene
C₂: 50 μF 6.4 V Mullard Miniature Electrolytic
C₃: 0.2 μF approx. (to be determined by experiment)
Octal or DIN socket

Diaphragm Material:

25 gauge Vapcolex Metallised Melinex. One square foot (cost around 3s. 6d.) aluminized on one side, from

George M. Whiley Ltd.,
Victoria Road,
South Ruislip,
Middlesex.

FIG. 1 CAPSULE AND CASE LAYOUT

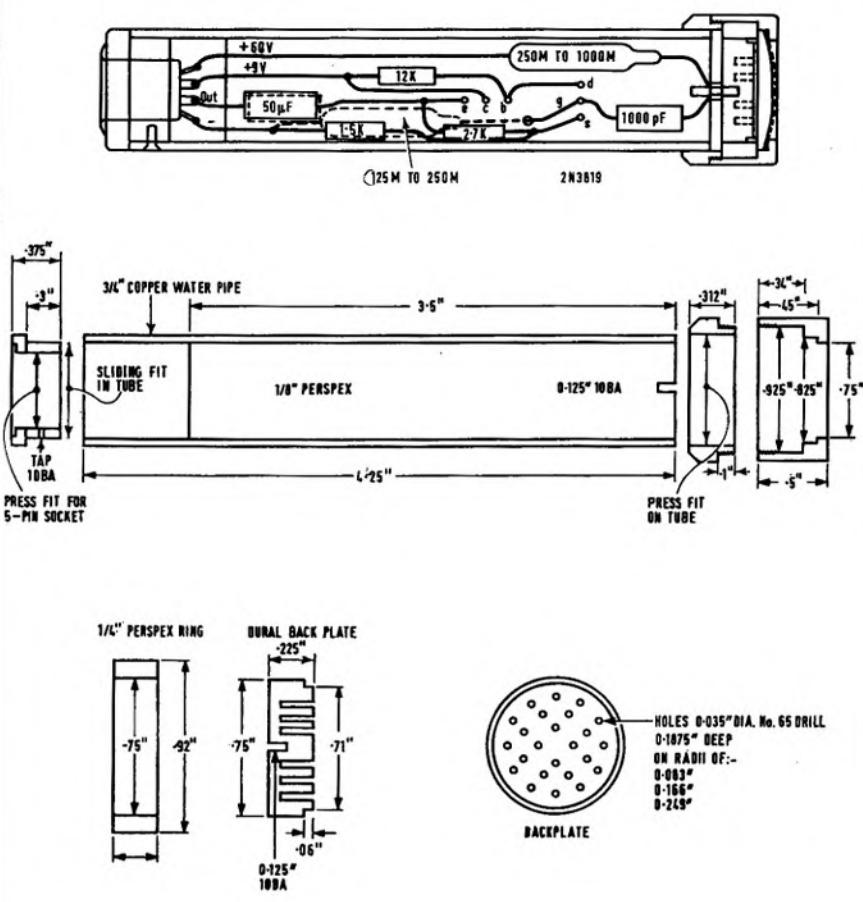


FIG. 2 AMPLIFIER CIRCUIT

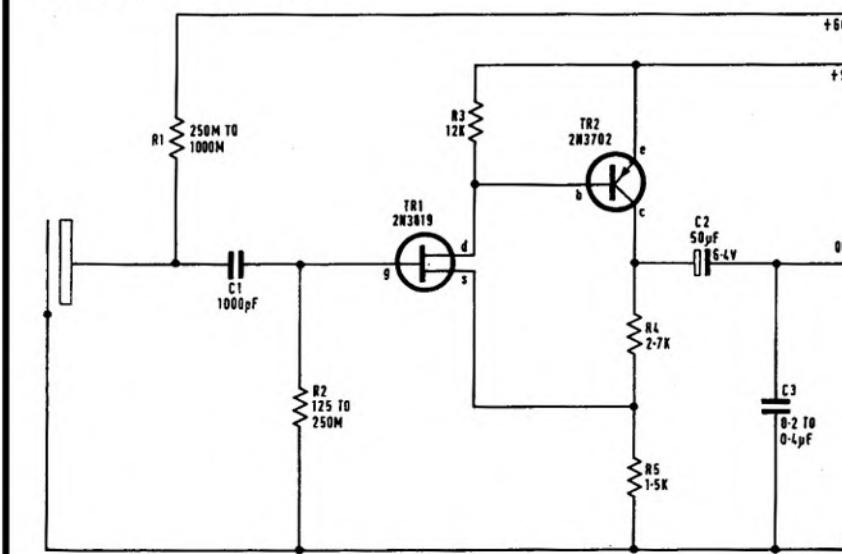
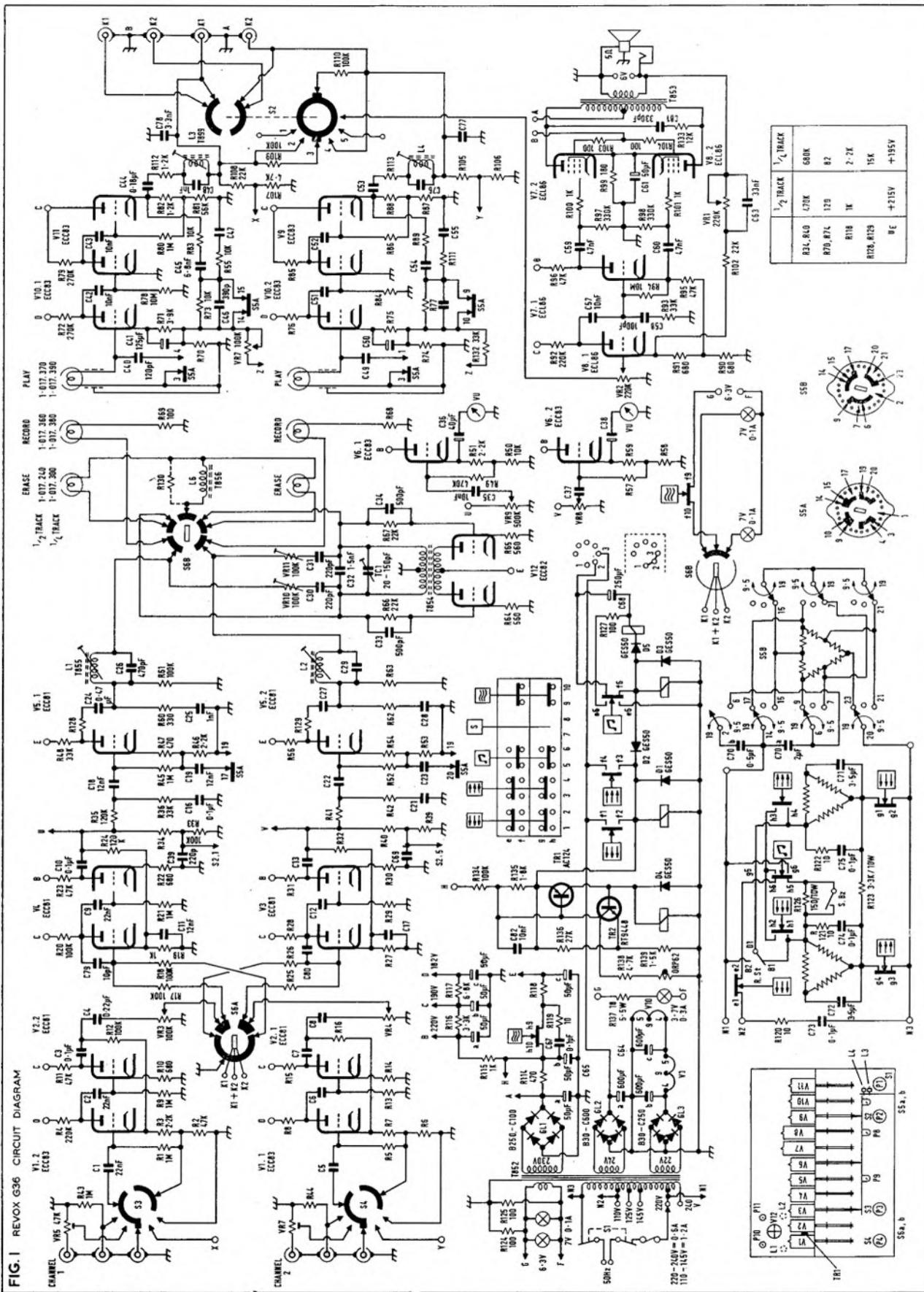
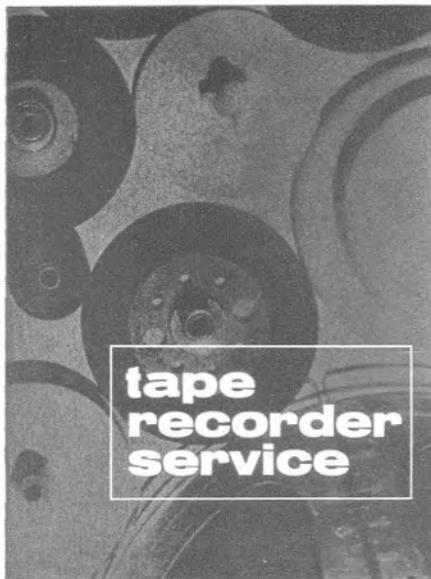


FIG. 1 REVOX G36 CIRCUIT DIAGRAM





tape recorder service

SOME GENERAL PROBLEMS

BY H. W. HELLYER

READER G. H. D. of Thetford, Norfolk, recently completed the construction of a Paraline loudspeaker from plans in *Five Speakers, How to Make Them*. On connecting the loudspeaker outlet of his Akai X4, he was disturbed by an immediate jump in hum level compared with the quality of the recorder's internal monitor. Investigation showed the mains unit to be responsible, since the hum vanished when operating from batteries. Hiss also worried G.H.D., whose letter ended with a frantic threat to tear his hair out. This is a case, I fear, of 'opening the window'. The plain answer is that the very much wider range (and higher electro-acoustic efficiency) of the Paraline is reproducing hum and hiss that was previously hidden by the inferior internal speaker. The Paraline cannot be blamed for doing its job properly and blame must lay at the door of the Akai. Hum in the power unit can sometimes be cured by replacing the large electrolytics and adding another filter section at the tape recorder connector end. If the transformer is at fault, however, there is little that can be done about it. Little, too, to do about hiss, which is excessive on many Akai models, short of redesigning the input stages.

W.P.T. of Scarborough purchased a Revox 736 in October 1967 and was from the outset bedevilled by a noisy capstan motor. Its rhythmic mechanical thudding was intermittent at first but rapidly deteriorated. The machine was eventually returned to the importer's northern representative who informed W.P.T. that the noise was caused by the spindle moving vertically in its seating. The offending bearing was packed with heavy grease and returned to its owner, but within a few days demanded further attention. This is in fact a legitimate method of reducing endplay and is effective for the lifetime of the motor if done properly. As the fault has recurred, I would suspect one of two things. First, a flaw in the bearing, causing overheating, subsequent loss of lubrication, and recurrence

of endplay. Alternatively, a drive fault that accentuates the endplay regardless of packing. In either case this warrants further investigation. I know at least two 736 owners who have put up with the noise for months, believing it to be inherent in the Papst motor design. This is far from being the cause, however, and the motor should develop no more than a soft whistle when in operation. The 736 does not take kindly to kitchen table transplants and persistent badgering of the importer is the only way to get things done. Hammonds care sufficiently about their reputation to replace an incurable motor.

There is nothing wrong with F.J.B. of Peterborough's Grundig TK120. The only problem is that he wishes to use the recorder in his boat and wonders whether a commercial vibrator would work effectively from a 12 V car battery. It is not in fact possible to run the TK120 from anything but a sinusoidal supply, either 110-117 V at 60 Hz or 200-240 V at 50 Hz. Vibrator supply units are not suitable for the synchronous motor in this

machine. Although there are electronic converter units on the market, notably those by Valradio Ltd., they are rather an expensive proposition and would cost more than a decent battery portable. The latter is the ideal solution, working from internal batteries or through a car battery adaptor.

F.A.B. of Cobham owns a Philips EL3586 battery portable which takes some four seconds to reach its 4.75 cm/s speed (who was it said tape recorders are like people, no two being the same?) and has to be helped by hand when rewinding. The root cause of this trouble is probably the motor, which is designed to work under very close tolerances and suffers from sluggish action if the drive conditions are incorrect. The pivot points and driving surfaces all have to be clean and correctly tensioned. This is no design on which to learn tape recorder servicing and I implore owners of the EL3586 and EL4200 to return faulty models to Combined Electronic Services (the Philips service network) or to a competent dealer. Sorry to be so damping.

S.E. of Llanelli bought himself a Bang & Olufsen 2000T some time ago and sent me a long angry letter detailing its faults (flutter, a stiff feed spool, an inoperative tape counter and a switch that didn't). The local B & O dealer from whom the recorder had been purchased delayed three months before collecting it and a further month before forwarding it to the B & O importer in Gloucester. Two months later, he was still awaiting its return. First, allow me to jump in quickly with a defence of B & O, and particularly of the 2000T. I can assert confidently, having bought one myself and maltreated it abominably, lugging it around the country in the boot of my car on various lecture-demonstrations: it has never given me any trouble and is a versatile match to any of the other equipment I care to couple to it. Small troubles can develop on anything. S.E. ended his letter by

(continued overleaf)

Editor's Note: We learn with regret that H. W. Hellyer is currently down with bronchitis and unable to contribute this month's column. To keep the flag flying in a series that has run non-stop for nearly seven years, we have assembled some of his recent correspondence on servicing matters with readers. Mac Hellyer has long been the backbone of our Advisory Service, in collusion with Graham Balmain and John Fisher, and the following notes have been a pleasure to prepare.

TAPE RECORDER SERVICE CONTINUED

promising to buy British in future, but I could make his hair stand with tales of faults I have experienced on new British equipment! But the dance he has been led was unforgivable and he was right to complain.

This illustrates one argument I have been making for a long time (granted, I have a vested interest, as Technical Director of a local Tape Recorder Centre). If you want good after-sales-service on domestic equipment, you simply *must* buy from the specialist. The little man down the road may be very helpful but he is not equipped to do repairs on elaborate and delicate equipment. It would not be economic for him to invest in a £500 'scope and £100 wobblemeter for two or three jobs a year. Don't blame him too much but nag him to get on to the distributors who should have given S.E. much better service.

C.C. of Sutton Coldfield was troubled by what he described as 'a gurgle on any note from middle-C up, especially sustained ones and complex tones like the tenor saxophone'. The fault was present in his Tandberg 64X which objected to new tape (*Dynarange* and others) but performed decently after the tape had been polished by a few runs. His final comment is, and I detect a musician's scepticism, 'to judge by the amount of miracle *Superlife* coating which sheds at the erase head during running-in, there is nothing wrong with the pad pressure'. It is quite true that tapes which have been 'polished' by a few preliminary runs give

better results than new reels, notably an extra two or three decibels around the 10 to 15 kHz mark. However, C.C.'s trouble seems more like the usual Tandberg trouble of erase head pressure-pad tensioning. Check the leaf spring and the surface of the pad itself. This surface should be quite soft, even fluffy, and it may be necessary to treat the pad in the usual way, with a drop of spirit lightly applied at the front end, ensuring that the spirit does not soak all the way through to the mounting to loosen it.

Check also that the back-bias head is not fouling on the front of the record head plates; I have had a couple of these with record heads very slightly lifted so that the bias head is ineffectively retarded.

Your remarks about oxide shedding at the erase head give the clue: really there should be an absolute minimum. I have found *Dynarange* the best bet on these machines, or the professional BASF *PES40*. C.C.'s letter suggested the commercial development of a bulk tape polisher, along the lines of a bulk eraser. The best bulk polisher is the contoured head of your machine!

Another Tandberg owner, this time of a conventionally biased Series 6, is B.S.A. of Ilford. His unit records happily but, on playback, the left-hand channel frequently diminishes to a low signal level, sometimes to nothing. Neutralising the replay control causes a static discharge through the left-hand (*Ditton 10*) loudspeaker. This fault is generally caused by a leaky interstage capacitor but, on rare occasions, can be instigated by valve trouble. Since the trouble occurs only on replay, the

cause is localised to the playback preamplifier. The two relevant valves are the *ECC82* and *ECC83* at the end of the playback printed board remote from the equalisation switch. The most likely cause is a leaky coupler between the first and second stages, a 0.22 μ F capacitor situated right beside the *ECC83*. This proximity is, I think, one reason why it fails.

E.B. of North Vancouver, British Columbia, sent in a service enquiry complete with a solution. He had been bothered with a persistent mechanical ticking in his Uher 4000S, so noisy that it was reaching the microphone. The noise ceased when he depressed the pause control, which led him to suspect the pinch-wheel. This was quiet enough when spun by hand, but two tiny spots of fine lubricating oil in its top bearing cured the fault completely. I have had troubles with ticking Uher battery portables and most of these have originated with the digital spool rotation counter. In fact, I have had to change one or two of these. Other persistent faults have been the spool drive belt (fortunately very easy to change), the motor (on early production runs), the zener diode in the regulator circuit, and the spring and collar (also, regrettably, the circlip) of the spool retainers. But these are minor matters when compared with the very fine performance of the 4000 design, especially when a good microphone is employed.

N.F. of St. Saviour, Jersey, owns a Stuzzi recorder and has been unable to contact the importers, Recording Devices Ltd., at their Kensington address. The company now lives at 274 Worton Road, Isleworth, Middlesex.

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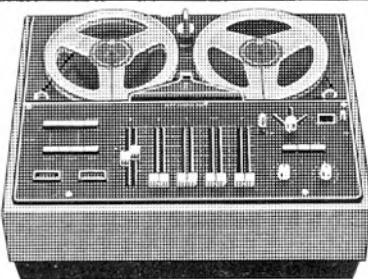
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HAVING left Part Two with a cliff-hanger we must plunge quickly into the subject of the multivibrator before getting involved in descriptions of practical circuits. We have followed the video input signal through its comparatively simple path to the modulator. Energising of the tape is by a frequency-modulated signal, for reasons we have already outlined. These generators can be formidably complicated pieces of hardware in high-powered transmitters but in the circuits of video tape recorders we are concerned with fairly straightforward examples and it may be wise to pause at this stage to make sure we are talking the same language.

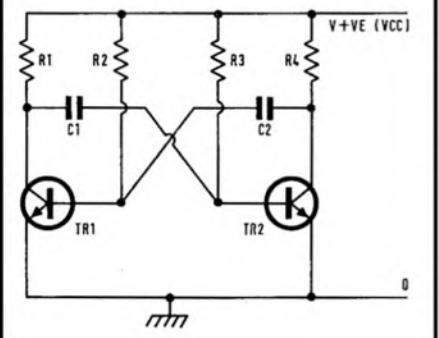
Multivibrators, especially in transistor designs, can take several quite different forms. Because of our familiarity with valve circuits, especially television timebases, we tend to speak of any two-valve or two-transistor circuit with regenerative action and switching between stable and quasi-stable states as 'a multivibrator'.

The genuine multivibrator has two quasi-stable states. The circuit oscillates between these two states in the absence of external triggering.

In its basic form, the transistor multivibrator circuit is like fig. 1, looking very like the familiar valve circuit with its characteristic cross-coupling. When Tr1 is bottomed, Tr2 is cut off and vice versa. At the moment of switching on, random current due to imbalance, which is practically inevitable, will cause one of the pair to take more current than the other, and regenerative action causes it to turn on fully while its opposite number switches off.

It is interesting to examine the voltage waveforms at base and collector of each of the pair through one cycle of operation. Presuming that Tr1 is switching on first, base current will flow through R2; collector current through R1. Knowing the specifications of the semiconductor, we can arrange that Tr1 is driven into saturation with a known base current and R1 is chosen to obtain this state. These are *n-p-n* transistors, so in fig. 2 we note that the cycle starts with base voltage at a value positive to the zero line and the collector voltage is at the saturation level, a little above zero. As Tr1 switches on, the charge on C1 takes the base of Tr2 negative. There is a little initial flip of collector current on the curve (c) where C1 reaches its charged state from switching on—an important short period for

FIG. 1 BASIC MULTIVIBRATOR CIRCUIT, FREQUENCY DETERMINED BY VALUES OF C AND R.

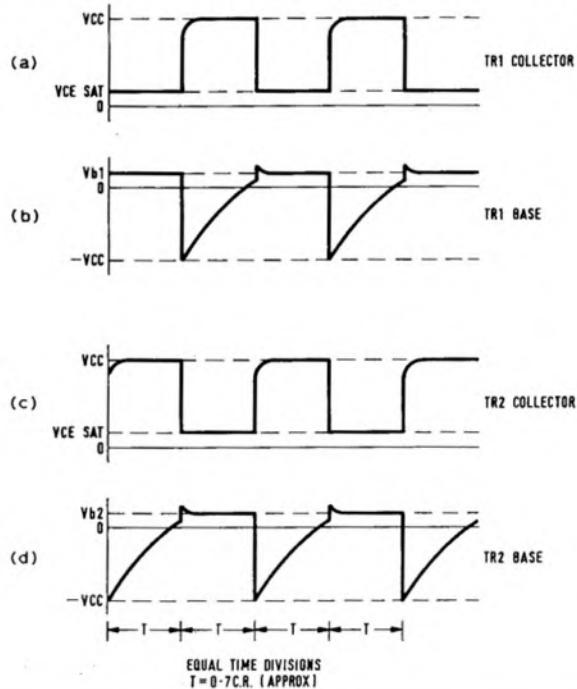


VTR CIRCUITRY

PART 3

BY HENRY MAXWELL

FIG. 2 VOLTAGE WAVEFORMS AT COLLECTORS AND BASES OF FIG. 1 TRANSISTORS



some applications, such as computer switching, but which need not concern us here.

C1 now discharges through R3 and the base of Tr2 is taken to a small positive value, and there is again a little twitch to the waveform as Tr2 turns on. The collector drops to saturation level and the opposite state of affairs occurs, with C2 discharging through R2 and C1 charging through R1. The time constant for the capacitors to charge through the collector loads is shorter than for their discharge through the base resistors. Regenerative action follows.

If the circuit is symmetrical, resistors and

capacitors for each of the pair equal, the time period for on and off states is the same. If one capacitor is larger than the other (this being a more convenient way of altering the time constant than changing a resistor, which alters DC conditions), discharge time is longer for the larger capacitor and the relevant transistor is held OFF longer. So one collector gives short positive-going pulses, the other gives relatively long pulses, also positive-going.

A circuit sometimes seen and not always fully explained is the diode loaded emitter configuration of fig. 3. Purpose of the diodes is to protect the transistor against breakdown, where the supply voltage of the circuit may be greater than the maximum reverse bias of the base-emitter junctions (fig. 2 b and d).

Diodes, and some additional components may also be met in circuits like fig. 4, where faster rise and fall times from the collectors are needed. Sharpening up the leading edges of pulses is a great design game: in this case, the diodes act as gates and the added resistors provide a charge path for the capacitors, alternatively to the collector loads. The circuit is used with high gain transistors.

We can divide our multivibrator circuits into three types; astable (free-running), monostable and bistable (flip-flop). The astable multivibrator switches repetitively between the two momentarily stable states. The monostable sets itself to one state when switched on and then resets to the other when triggered. It then stays in the switched state until the discharge period determined by the circuit values allow it to switch back again. But the flip-flop stays in the alternative switched state until again triggered. This is the fundamental difference between the three types and the main reason

(continued on page 461)

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why we cannot simply talk about 'a multivibrator' without defining it. We shall come across all three types in VTR circuits.

Our last reference (at the end of Part Two) was to an astable multivibrator, used as the generator of the Sony frequency modulation circuit, and having a free-running frequency determined by component values. Fig. 5 shows the basic circuit.

We can see that this circuit actually bears some resemblance to the theoretical circuits we have used to illustrate the point—an unusual circumstance, it seems, in this type of demonstration! Although every manufacturer or designer appears to have his own ideas about the putting of theory into practice, and much fun can be had with new circuits trying to trace out the purpose of apparently superfluous components. Sony employ a simple circuit, capable of easy adjustment, rock-steady in operation, and accessible.

We note that both the collector voltage and the emitter voltage for the matched transistors can be adjusted individually for balance. DC clamping has already been done, at the modulator. A varying DC is applied to the bases, in step with the incoming modulation and, as we have seen, slightly tailored. The base input voltage increase causes the output frequency to rise. We are, in effect, altering the value of R in the CR combination by altering the applied voltage to the base. There is nothing magical about the CR formula; all that happens is that in a given time the capacitor discharges (or charges) to alter the effective emitter-base voltage and turn the transistor on or off, providing the swing we need. So if we alter that base voltage ourselves, we can control the frequency.

This may help to explain why, as we saw last time, the carrier frequency setting is back in the modulator drive circuit, not on the generator itself. Actual setting up depends very much on the clamping of the modulator so that the black level of the video signal is exactly right. Then, excursions of the signal have reference to this level and frequency is stable about a set figure.

The basic oscillator in this circuit runs at 1.7 MHz, and this has to be quite carefully adjusted. Increase in basic frequency will cause a plasticity in the picture that is very

FIG. 3 DIODE LOADED Emitter CIRCUIT PROTECTS THE TRANSISTORS FROM BREAKDOWN WHERE SUPPLY EXCEEDS REVERSE Emitter - BASE JUNCTION BIAS.

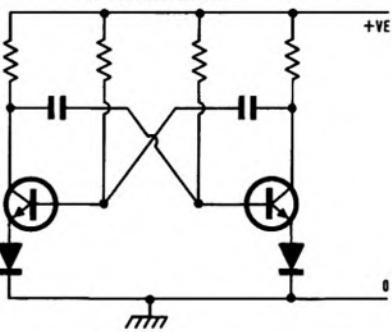
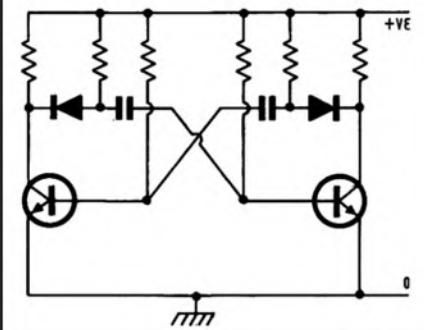


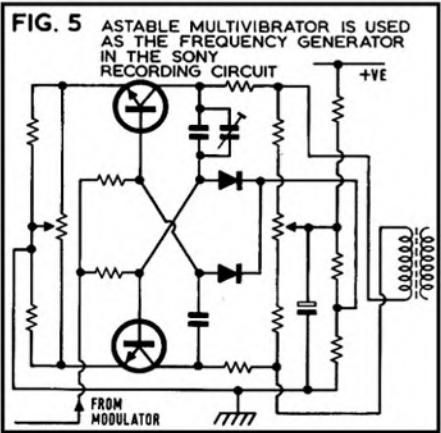
FIG. 4 GATING DIODES IN THE COLLECTOR CIRCUITS IMPROVE RISE TIMES



difficult to eradicate—and this is a general observation, not peculiar to the circuit we are examining at present. One of the troubles relevant to this appears to be the problem of carrier leak. At various parts of the circuit we find precautions taken against breakthrough of the carrier and there is always a temptation to alter the generator balance circuits to cure it. Indeed, in the Sony 2000, though certainly not so much in the 2100, it was sometimes necessary to touch up the generator balance controls and then go back over the whole clamping and clipping adjustment procedure and finally to check the modulation indication, which can be affected. All to get rid of a few wavering patterns on the screen!

Take-off from this kind of generator should be balanced, and Sony use a very special kind of coupling transformer with a floating primary. We shall revert to this point later. Before discussing any more processing of the circuit, however, it may be an idea to look at an alternative version, and the Loewe-Opta Optacord 600 series of video tape recorders, which have not yet received much mention, can provide us with good examples.

Once again, the free-running oscillator has its frequency controlled by alteration of the base voltage. Stabilisation of the drive voltage is obtained by the use of a zener diode (what did we do before these were developed I wonder?), and the take-off this time is across the balanced collector loads, again using a floating winding of a coupling transformer.



The interesting part about this circuit is that the basic oscillator frequency is 3.3 MHz and the adjustable input resistor, to whose slider the modulator couples the varying voltage for video drive, is set for minimum output of the second harmonic of the carrier frequency, i.e. 6.6 MHz. The resistor across the primary of the take-off transformer is set for correct depth of modulation, not for any relative frequency change. In practice it directly regulates the amount of modulating current through the video head.

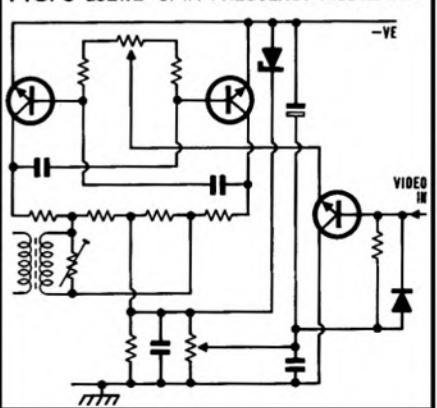
A brief word in general about the 600 series may help set the scene. It has not been possible to discuss it before as there was no circuit issued and I have, in fact, had to wait for the generosity of my friends in Dusseldorf before I could borrow one and discuss details, though practical information and my usual back-of-envelope scribbled notes were available in abundance.

This is a hybrid machine, a pair of PCL84 valves having crept into the circuit. Helical scan, using a single head, which traces a single field per revolution, while the tape moves past at 15 cm/s. This gives a relative motion of 19 m/s (metres per second) and permits a claimed bandwidth of 3 MHz. For recording and replay on the same machine, up to a hundred minutes performance may be accommodated but to ensure compatibility it is necessary to reduce this to 72 minutes.

One very useful feature is a variable speed fast rewind, from zero velocity to 60 times the recording speed. At low rewind speeds, the machine is still in the play mode and monitoring is possible. As an extension to this facility, still pictures can be displayed by setting to rewind and halting the machine. Later versions, the 603 range, automatically adjust for best scanning of the still frame and can be set to advance, frame by frame, giving a slow-motion effect. Tape width is 25 mm.

Continuous scan is achieved by a 360° wrap around the drum and helical systems as previously described. Head rotating speed is 3,000 r.p.m. and track width 0.15 mm. Synchronisation is by sampling of the vertical pulses and similar comparator systems to the Sony which we shall discuss in detail later. The two tape speeds, 15.22 cm/s for the single machine use, 21.5 cm/s for compatible use, are a novel VTR feature, and the relevant control circuitry will merit our future attention.

FIG. 6 LOEWE-OPTA FREQUENCY MODULATOR



A THEORETICAL alternative to pitch control by variable inductance is control by variable capacitance. It is, however, in practice so difficult economically to achieve adequate capacitance swing, that, notwithstanding advances such as variable capacitance diodes and gyrator circuit techniques, the method is still barely practicable.

The large family of R.C. oscillators contain a number of members which can be arranged to have adequate frequency stability. Control by variation of either resistance or voltage is feasible, and probably the most flexible and practicable means, currently, of managing the fine control of pitch is by the use of light dependent resistors. The light source must not be energised with A.C. or the tones will be modulated with mains frequency hum. Circuits of various R.C. oscillators are given in figs. 9 to 13.

So far we have considered only those instruments characterised by non-continuous tuning. Entirely different problems of pitch control arise if we decide that continuous sliding pitch is essential. The important point, however, is that an instrument capable of glissando must be capable of playing chromatically (i.e. in accurate semitone intervals) and it is necessary to fulfil this double requirement, while still providing for reasonable ease of accurate playing.

It is reasonable to enquire whether the faculties of glissando (which occurs very seldom in serious music) or portamento (which is more often a matter of expression than of the composer's intention and is often an artistic fault) justify the trouble of providing them. The answer to this question depends on the extent to which you are willing to compromise and the degree of difficulty in providing satisfactory control with continuous tuning.

A minor degree of portamento is, of course, available in the kind of arrangement already described but, even if the pitch variation range of each note is fully half a semitone on each side of the mean, so that there is a continuous frequency cover over the whole range of the instrument, neither full portamento nor smooth glissando is a practical possibility using the means suggested.

Gliding-tone circuits are very easily arranged and it is easy to design a single oscillator which will cover the required frequency range (about 1:10) in one sweep. Suitable frequency stability at any frequency within the range can also be achieved without much difficulty by stabilising

the synthesis of musical instrument tone

Part Two
By Robert M. Youngson

the power supplies and by good design. Among the simplest suitable circuits are relaxation oscillators using unijunction devices, in which the time constant of the charging circuit is varied by varying the resistive element (figs. 14 and 15) and emitter-coupled oscillators similarly controlled (fig. 16). Other suitable oscillators are shown in figs. 17 and 18.

It is when we come to the control of these oscillators that the trouble begins. In considering variable resistance control, the most obvious evolutionary step from a rotating control (which, however calibrated, is inherently quite unsuitable for this purpose) is an extended resistive element equal in length to the equivalent section of keyboard and having such a resistivity that the appropriate pitches are produced when contact is made at suitable points along its length. It is not actually necessary to employ an electrode held at the end of a flexible wire, since various methods have been developed to make contact at the point required. (see below)

Such a system, ignores the useful conventional orientation of accidentals and playing is

FIG. 9 TUNNEL DIODE VARIABLE FREQUENCY OSCILLATOR. THE TWO STATES OF THE DIODE ARE VOLTAGE DETERMINED.

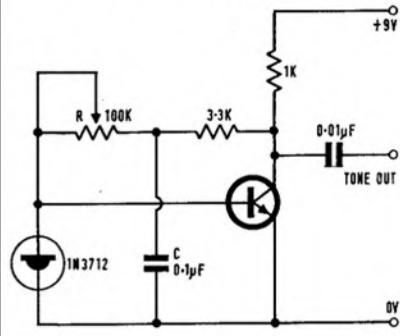


FIG. 10 PHASE-SHIFT RC OSCILLATOR
THIS CAN BE TUNED BY VARYING THE VALUE OF ONE RESISTIVE ARM.

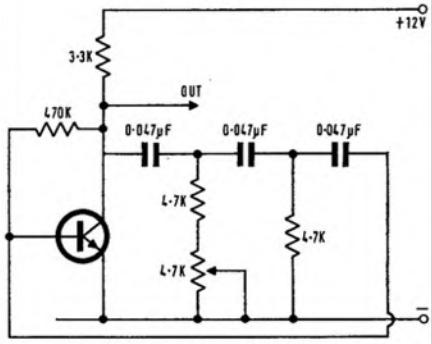


FIG. 11 WEIN BRIDGE OSCILLATOR

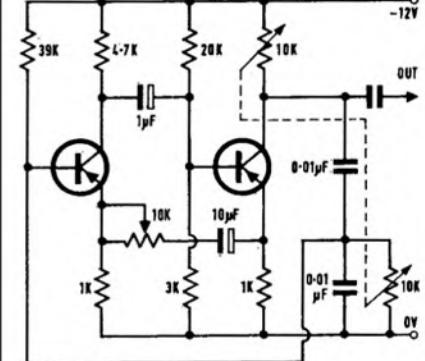


FIG. 12 TWIN-T FEEDBACK OSCILLATOR

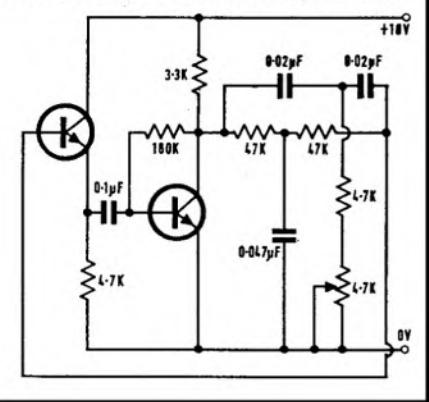


FIG. 13 WIDE-RANGE VARIABLE FREQUENCY SAWTOOTH RELAXATION OSCILLATOR USING AN N-P-N/P-N-P TRANSISTOR COMBINATION

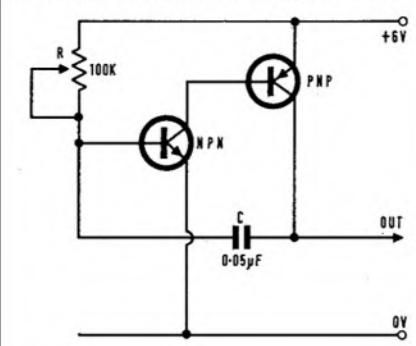
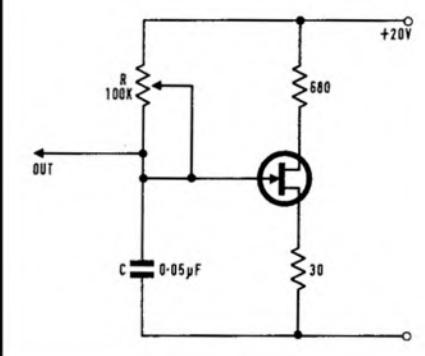


FIG. 14 SIMPLE UNIJUNCTION SAWTOOTH RELAXATION OSCILLATOR



made more difficult. A second resistive strip can, of course, be placed behind the first and both marked with the positions for the notes. In this case, much trouble is saved by providing a separate oscillator for each strip.

A major objection to the system lies in the difficulty of providing satisfactory contact arrangement. One approach is to arrange for a stretched flexible metal strip to lie just above each resistive line so that finger pressure at the appropriate point causes contact to be made. As may be imagined it is not easy with such a system to achieve accurate intonation since the breadth of a finger covers too large a proportion of the total length of the resistive strip. It is true that the resistance in circuit is only that part between one end of the strip and the

corresponding edge of the area of contact but, nevertheless, the accuracy of finger placement must approach that of the violinist. Vibrato can be managed, with a little practice, by rolling the finger in a manner similar to that of a string player.

Another possible approach is to provide a contactor which can be slid along a conducting guide to the appropriate position and then pressed down to make contact with the resistive element. Alternatively, the contact can be attached to the underside of a endless flexible metal tape which, while lying immediately above the tuning resistor strip, can be moved on rollers so that the contact can rapidly be brought to any desired position over it.

In any such system, contact resistance must be very low and must not vary with differences in finger pressure. If significant contact resistance occurs while the finger is descending, the note will be initiated at a lower pitch than the nominal and a quite unacceptable starting transient will result. A similar adventitious sound may occur at the end of the note when the finger is lifted. This difficulty is not easily overcome by improvement in the contact arrangements but can be solved by arranging for the oscillator to be switched on a few milliseconds after contact is made. This can be done by arranging for the variation in resistance to alter the time-constant, not directly but by changing the bias of a transistor through which the main tuning capacitor charges. The switch-on of this charging transistor can then be delayed by means of a second time-constant circuit (R_1, C_1 in fig. 19). This method has the additional advantage of

permitting controlled variation in the attack of the instrument by making R_1 variable, or alternatively by switching in different values for C_1 .

This type of continuous-tuning instrument, is capable of reasonable results, but it is inherently inferior to one having a separate oscillator for each note in the chromatic scale. Single oscillator instruments can, of course, be designed for use with a keyboard and some of the simplest and cheapest arrangements possible may thus be achieved. In these designs, the key switches bring in progressively changing values of capacitance or, preferably, resistance. Fine pitch control and vibrato is then most easily obtained by a separate control device acting directly, and independently, on the frequency of the oscillator, but you must see to it that the effect on frequency of a given movement of this control does not vary too much between one end of the gamut and the other.

One suggestion is given in fig. 20. The illumination of the LDR is via one fixed and one movable sheet of 'polaroid'. The latter is so articulated that lateral movement of the key switch button causes it to rotate slightly and thus change the intensity of light falling on the LDR. This will change its resistance and consequently the frequency of oscillation. As an alternative a simple shutter system may be used. The amount of control effected can be adjusted by shunting the LDR with a variable resistor.

In the design of musical instrument analogues one should remember that conventional means of pitch selection, such as keyboards, need not necessarily be the optimum. The factors which determined the present standard keyboard were not solely anatomical and physiological but also included the necessity to provide enough room to accommodate, within the breadth of each key, the required mechanical linkages or striking or plucking mechanism. Other factors, such as the standard depression distance and playing weight, may likewise be a compromise between convenience and practicability. Trained keyboard musicians have, of course, become so conditioned to the present arrangements that they are inclined to be intolerant of even minor changes and are understandably persuaded that these standards are absolutes.

There is little doubt that, on economic grounds alone, the present conventional

(continued on page 465)

FIG. 16 Emitter-coupled variable-frequency oscillator

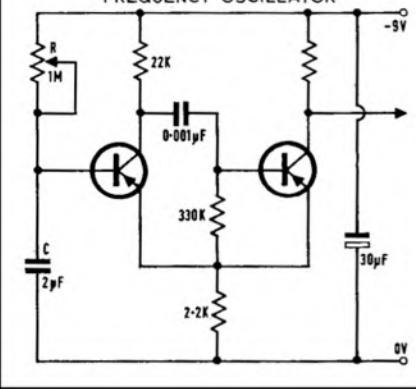


FIG. 17 Variable-frequency multivibrator

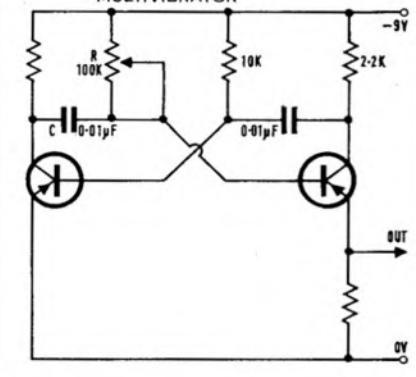


FIG. 18 Unijunction sawtooth oscillator with controllable linearity

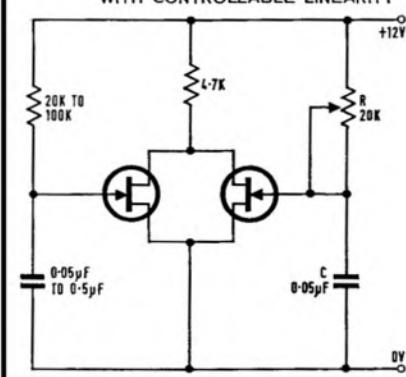


FIG. 19 Unijunction oscillator with controllable turn-on rate

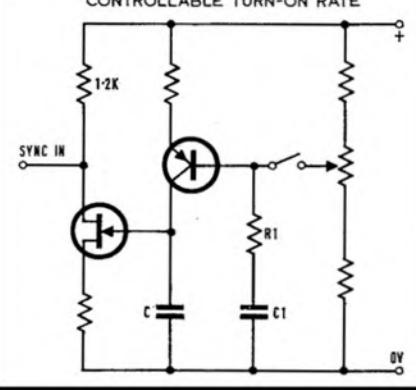


FIG. 20 Method of obtaining fine pitch control and vibrato of resistance dependent oscillators.

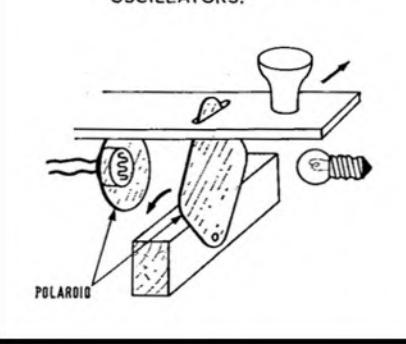
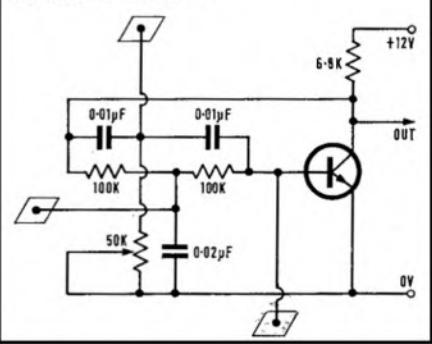


FIG. 23 Twin-T ringing oscillator

The circuit is shocked into brief oscillation by a touch on any one of the plates. Must be adjusted to be just below the threshold of oscillation



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Philips N4404	26 17 0	4 15 0	77 17 0	
Ferguson 3232	33 5 0	5 11 0	93 5 0	
Sanyo MR929	33 4 0	5 10 0	97 4 9	
Philips N4407	35 15 10	5 13 4	103 15 4	
Akai 1710W	37 15 7	6 2 1	111 0 5	
Sanyo MR939	38 13 6	6 2 3	112 0 2	
Sony TC230	40 11 9	6 15 0	121 11 9	
Telefunken 204TS	41 19 0	6 13 4	124 19 0	
Grundig TK247	45 10 9	7 2 4	130 18 9	
Sanyo MR990	44 18 0	7 5 0	131 18 1	
Philips 4408	46 19 5	7 8 9	136 3 10	
Sony TC530	49 12 3	8 1 8	146 12 3	
Tandberg 1241X	49 0 0	8 6 8	149 0 0	
Beocord 2000K	53 5 0	8 17 6	159 15 0	
Beocord 2000T	55 5 0	9 4 2	165 15 0	
National Console-Aire	62 0 0	10 5 0	185 0 0	
Akai M9	68 12 4	10 16 8	198 12 4	
Akai 1800SD	68 12 4	11 1 2	202 13 10	
Ferrograph 724	68 16 9	11 6 8	204 16 9	
Revox 1222/4	74 11 0	12 8 6	223 13 0	

4 TRACK MONAURAL

Fidelity Braemar	11 12 8	1 17 4	34 4 8
Fidelity Studio	15 17 10	2 10 2	46 0 10
Grundig TK144	16 10 1	2 11 11	47 13 1
Philips 4307	16 15 3	2 13 1	48 11 1
Ferguson 3228	16 16 8	2 13 4	48 16 0
Ferguson 3238	20 12 0	3 5 0	59 12 0
Philips 4308	20 14 2	3 5 7	60 0 10
Ferguson 3216	22 16 0	3 12 2	66 2 0
Tandberg 1541	28 0 0	4 10 0	82 0 0
Revox HW10-4T	28 16 9	4 11 2	83 10 1

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Sony TC355	34 2 6	5 10 0	100 2 6
Beocord 1500	42 10 0	7 0 0	126 10 0
Tandberg 62/64X	53 0 0	8 13 4	157 0 0
Beocord 1800	60 15 0	9 18 4	179 15 0
Revox 1102/4	63 19 0	10 6 8	187 19 0
Ferrograph 702/704	64 15 8	10 16 8	194 15 8

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MUSICAL TONE SYNTHESIS CONTINUED

musical instruments (and in particular polyphonic instruments) will give way to electronic. As they do there is likely to be a no less radical evolution in the process of pitch selection.

It is, of course, possible to play an electronic musical instrument without even touching it; beat frequency oscillators in which pitch alterations are achieved by changes in 'hand capacity' have been commonplace for many years and a modern example is given in fig. 21. Unfortunately, however skilfully the player may manage accurate intonation (and this is extremely difficult) such instruments can play discrete notes only by incorporating an interrupter switch which is, of necessity, independent of the pitch selection process. The separation of the two functions adds to the difficulty of playing but, if the switch can be

operated by the same hand which determines the pitch, a useful flexibility is achieved and the other hand is freed to operate dynamic and timbre controls, etc. This has the disadvantage that the playing hand must be connected to the instrument either by a wire or a radio or light link and some physical device, however small, must be held. An alternative is a foot-operated switch, but this is not very satisfactory in rapid passages. All in all, the method probably involves too many playing difficulties to become universally acceptable.

The most likely future method will involve simple light touch with the fingertips on small circular metallic elevations, the arrangement of which will be determined by ergonomic principles rather than by convention. Such a contact system can operate in two main ways, either by an actual flow of signal current

through the body of the player (the electrical resistance between the finger tips and any other part of the body is a mere $10\text{ k}\Omega$ to $50\text{ k}\Omega$ depending on the dryness of the skin)

(continued on page 469)

FIG. 15 OTHER UNIJUNCTION OSCILLATORS

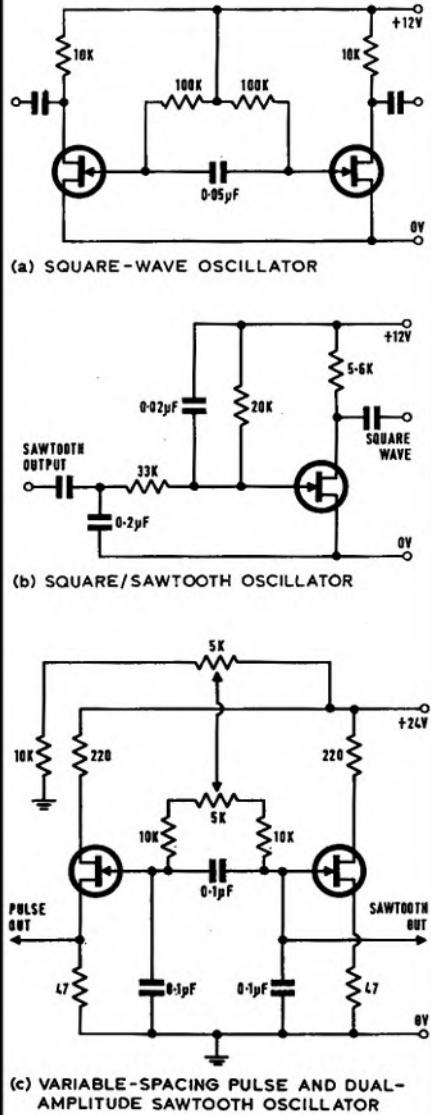


FIG. 22

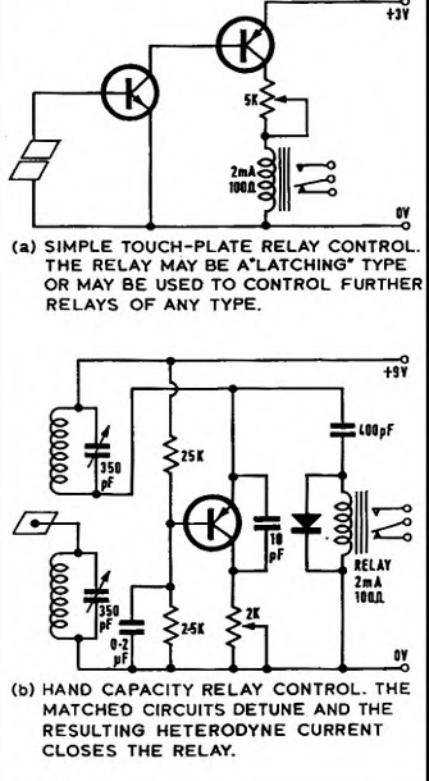


FIG. 25 BISTABLE MULTIVIBRATOR FREQUENCY DIVIDER, USING DIODE STEERING

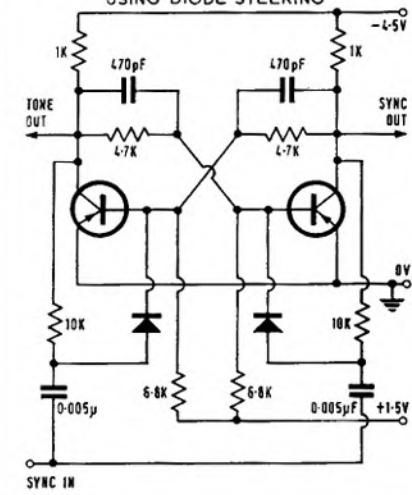


FIG. 24 NPN-PNP RELAXATION OSCILLATOR USED AS A FREQUENCY DIVIDER

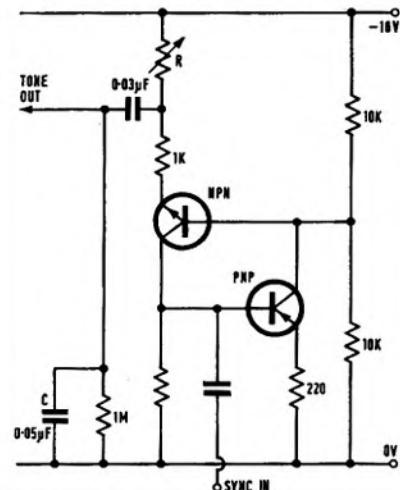
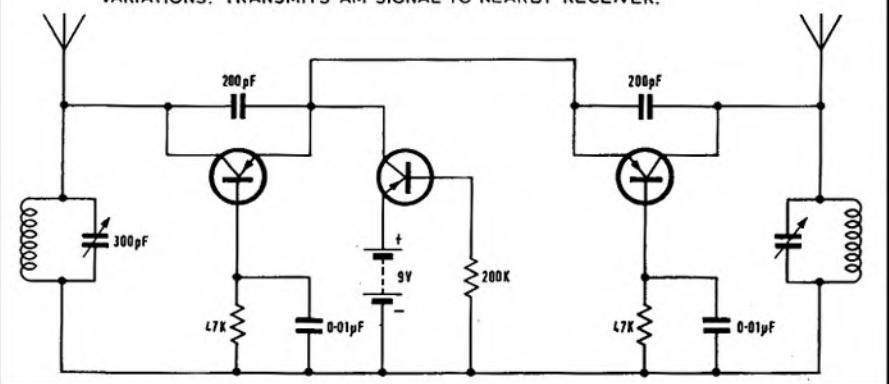


FIG. 21 'THEREMIN' BEAT FREQUENCY OSCILLATOR CONTROLLED BY HAND-CAPACITY VARIATIONS. TRANSMITS AM SIGNAL TO NEARBY RECEIVER.



equipment reviews



**REVOX HS77 NAB
AND IEC PROFESSIONAL**

MANUFACTURER'S SPECIFICATION (Agfa PE36 at 38 cm/s). Professional mains transportable stereo recorders with tachometer capstan motor speed control. **Tape transport:** Direct capstan drive, separate motors for fast forward and reverse wind. **Wow and flutter:** 0.04% maximum. **Tape slip:** less than 0.2%. **Spool capacity:** 26.5 cm, NAB hubs. **Frequency response:** 30 Hz-20 kHz ± 1.5 dB. **Distortion:** 2%. **Equalisation:** NAB or IEC to order. **Signal-to-noise ratio:** 60 dB. **Cross-talk (1 kHz):** 45 dB stereo, 60 dB mono. **Tape speeds:** 38 and 19 cm/s. **Bias frequency:** 120 kHz. **Inputs:** 0.15 mV at 50 ohms to 6 K or 2 mV at 100 K (*microphone*, switchable); 2 mV at 33 K (*radio*); 40 mV at 1 M (*auxiliary*). **Outputs:** 2.5 V at 600 ohms (*line*); 1.2 V at 2.5 K (*radio*). **Weight:** 15 kg. **Dimensions:** 359 x 215 x 413 mm (plus spool overhang). **Prices:** On application. **Manufacturer:** Willi Studer GmbH, CH-8105 Regensdorf, Zurich, Switzerland. **Distributor:** Revox Ltd, 90 High St., Windsor, Berkshire.

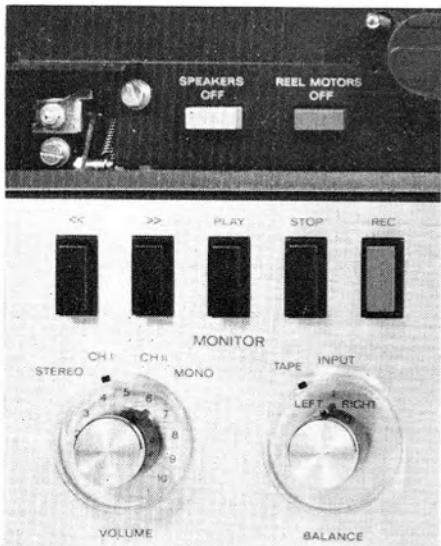


FIG. 1 REVOX HS77/NAB RECORD-PLAY WOW AND FLUTTER

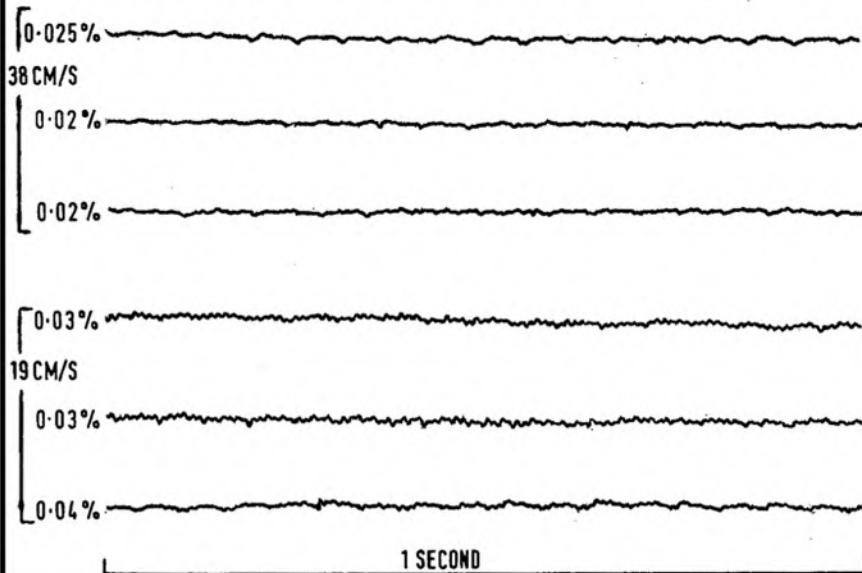
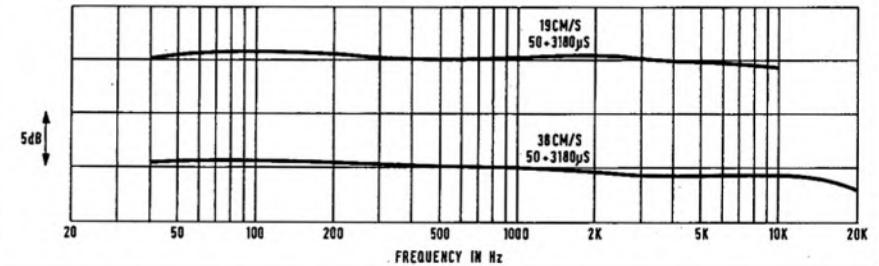


FIG. 2 REVOX HS77/NAB PLAY-ONLY FREQUENCY RESPONSE (TEST TAPES TO LINE OUT)



To meet the demand for a basic transportable professional recorder in this country, a number of A77 machines were modified by the distributor for 38 cm/s operation. This entailed a larger capstan diameter and alterations to the record and play equalisation to meet the 50 μ s NAB standards for both 38 and 19 cm/s. As I have access to several of these recorders, David Kirk asked me to prepare a review under the conditions suggested in his October Editorial, i.e. I was to be allowed to set the bias and equalisation for optimum performance on any given type of tape. As he forecast, such tests used up a vast amount of time as test tapes, for example, had to be checked one against the other to make sure that the published responses were as accurate as possible and did not include small errors in the calibration.

It was therefore with some consternation and considerable interest that we learned, only a few days before publishing deadline, that a

Swiss high speed recorder with a number of mechanical and electronic modifications had arrived in this country. This was an opportunity not to be missed and Revox Ltd. had it down to me within a few hours.

In the time available I was not able to repeat all the tests or optimise the bias and record equalisation for the best possible response with the different (IEC) equalisation. Nevertheless there were significant improvements in wow and flutter, signal-to-noise ratio and cross-erase which take the '77 design a further step towards perfection. The modifications to the Swiss machine listed were as follows:

- (a) Metal spool carriers to eliminate static charge on metal spools and (together with b) to give slightly faster and more even tape winding.
- (b) Roller bearing on left-hand tape guide to give lower friction and appreciably less wow and flutter.

FIG. 3 REVOX HS77/IEC PLAY-ONLY FREQUENCY RESPONSE (TEST TAPES TO LINE OUT)

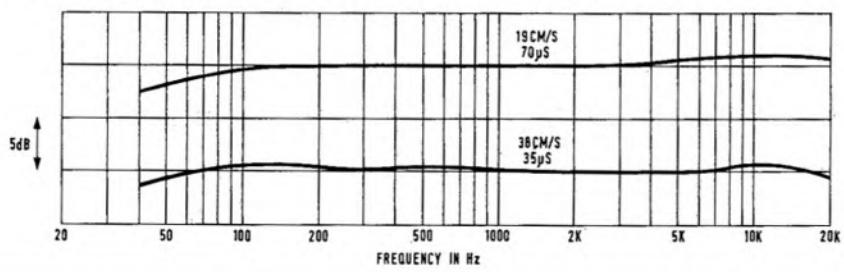


FIG. 4 REVOX HS77 (IEC AND NAB) PLAYBACK AMPLIFIER FREQUENCY RESPONSES

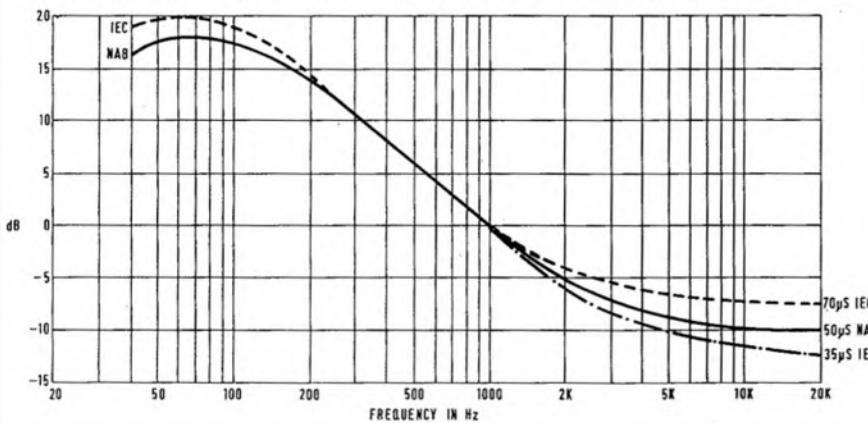
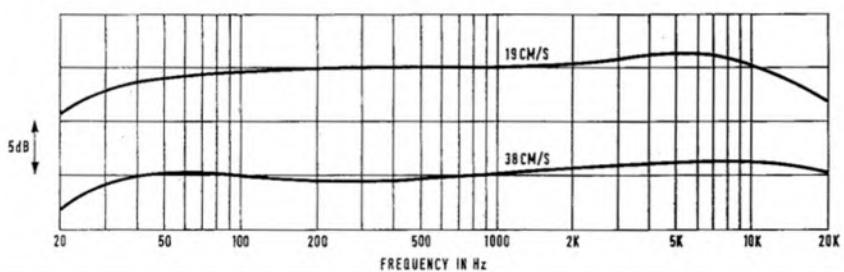


FIG. 5 REVOX HS77/NAB RECORD-PLAY FREQUENCY RESPONSE LINE IN, AGFA PE36, LINE OUT



(c) Damped transient absorber near left hand guide to give better starting.

(d) Wider pinch roller to reduce tape slip (my measurements on the width of the old and new pinch rollers showed them to be nearly identical, so perhaps this modification is yet to come).

Fig. 1 shows the pen recordings of cumulative wow and flutter at 38 and on the UK modified (HS77/NAB) recorder. At 19 cm/s the WHM fluttermeter reading remained steady at 0.03% RMS for long periods. Only occasionally did it rise to 0.04% as record and play speed fluctuations come into step for short periods. At 38 cm/s, the meter reading remained rock steady at 0.02% RMS with very occasional excursions to an absolute maximum of 0.025%.

On the Swiss machine, the 19 cm/s reading was 0.03% and I could not coax it any higher by slipping or phasing the tape for cumulative adding of any of the wobble components. At

38 cm/s we hit an all-time low of 0.015% RMS combined wow and flutter with occasional short rises to an absolute maximum of 0.02%.

Fig. 2 shows the responses at line output when playing 19 and 38 cm/s NAB test tapes with 50 μS high note pre-emphasis and 3180 μS bass pre-emphasis. It will be seen that playback equalisation is exact within 1 dB to 10 kHz at the lower speed, and to -15 kHz at 38 cm/s. The solid curve in fig. 3 shows the electrical equalisation as measured from head terminals to line output.

The HS77/IEC was tested with IEC 70 and 35 μS test tapes to give the play-only responses of fig. 4. These responses are level within 1 dB limits to 20 kHz at either speed with a very slight bass roll-off below 100 Hz at each speed.

The UK HS77/NAB was tested with the recommended Agfa PE 36 LP tape, bias and HF recording pre-emphasis was carefully adjusted at each speed to give the overall

responses of fig. 5 which are within the specified limits.

1 kHz 32 mM/mm reference tape level was recorded at +2 dB on the VU-meter scale. Total harmonic distortion at this level was 0.8%, mainly third harmonic. Unweighted system noise, with no tape passing the heads, was -56 dB on reference tape level. Weighting to the IEC 'A' response, which matches that of the ear at low listening level, gave a reading of -63 dB.

Bulk erased tape was 61.5 dB below reference and machine-erased tape was exactly 60 dB below 32 mM/mm 1 kHz reference tape level.

All the above distortion and noise levels were identical at 19 and 38 cm/s.

The Swiss HS77/IEC recorder was tested with the identical Agfa PE36 LP tape to give the overall frequency responses of fig. 6. It was obvious that the top track bias was a bit low at 19 cm/s, resulting in the rising high note response and very slightly lower mid and low frequency responses shown by the solid curve. The bottom track was nearer the optimum bias and pre-emphasis settings for the recommended Agfa tape as shown by the dotted response at 19 cm/s.

At 38 cm/s top and bottom tracks were almost identical and the response was within the specified limits from 30 to 20 kHz.

Unweighted system noise was -58 dB below reference tape level and weighting it to the IEC 'A' response gave the very low reading of -66 dB. This reading remained the same at 19 and 38 cm/s.

Bulk-erased tape noise was -62.5 dB at 19 and -64 dB at 38 cm/s.

Machine-erased noise was -60.5 dB at 19 cm/s and -62 dB at 38 cm/s.

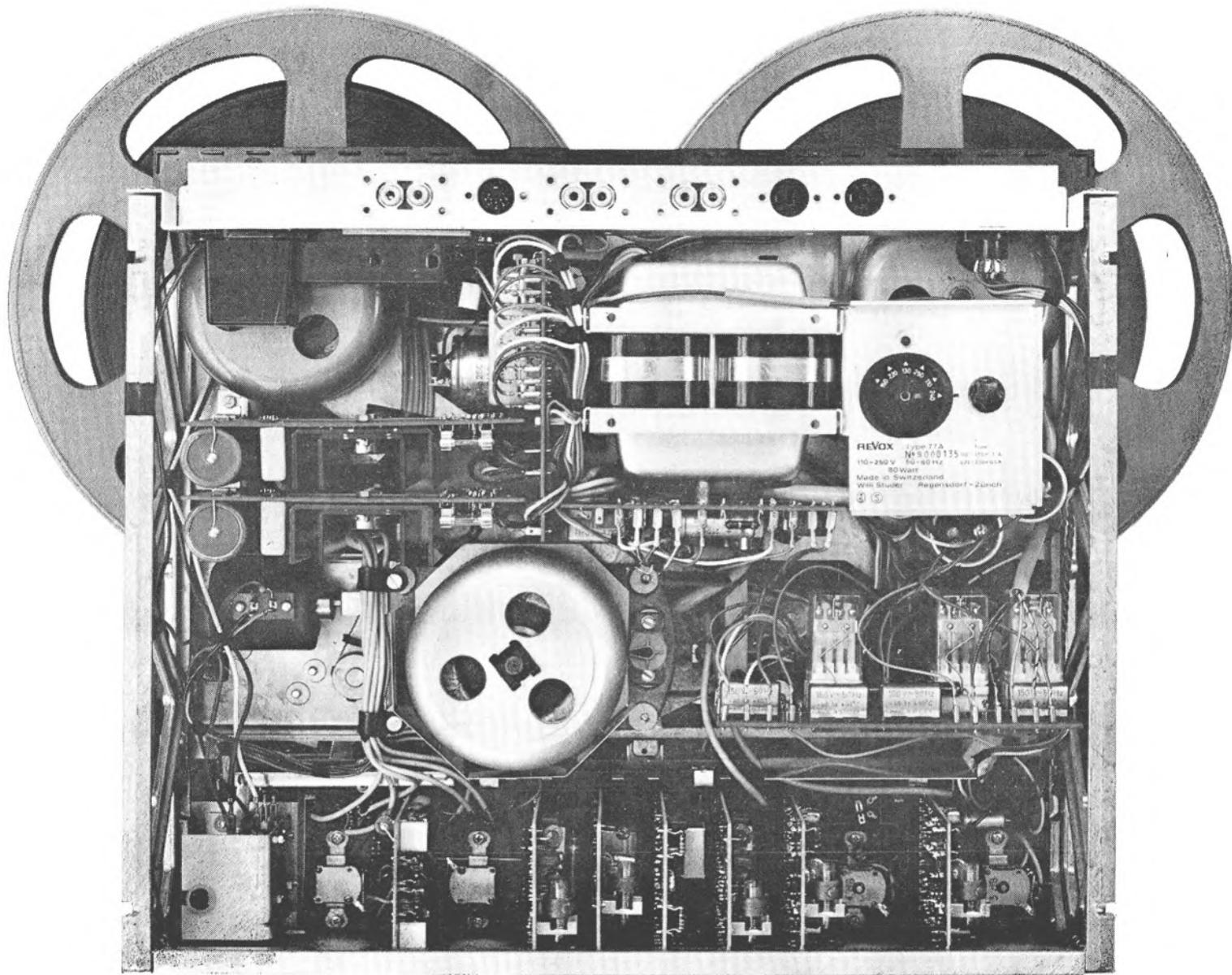
These noise differences with tape speed are mainly due to the change of extreme HF response as the playback equalisation is switched from 70 to 35 μS as shown in fig. 4.

The 19 cm/s 1 kHz harmonic distortion at 32 mM/mm was very slightly higher than the other recorder at 0.9% and it dropped to 0.75% at 38 cm/s. This could be due to the slight under biasing of the top track on which the measurements were made, or it could be due to the 3 dB difference in equalisation at 3 kHz (3rd harmonic) as again shown in fig. 2.

There was another small difference in the two recorders which could only be detected if the machines were used for industrial or scientific purposes, such as the production of test tapes, where 0.5 to 1 dB differences in extreme high note response were significant. If a mono recording of 10 kHz was recorded on the top track only of the NAB machine and erase and bias applied to the bottom track, either by switching heads or reversing the tape and leaving the bias and erase on the top track, then the 10 kHz signal dropped by 0.5 to 1 dB whenever the other track was erased. The trouble was traced to the erase head, as inserting a slip of paper between the erase head and the tape stopped the effect. It was also proved that the fault was not present on stereo recording.

Measurements showed that the voltage across each section of the erase head was 15 V on stereo recording, but rose to 25 V when

(continued on page 469)



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REVOX

HS77 IEC AND NAB REVIEWS CONTINUED

only one erase head was in use. This indicates that on mono the erase head is over powered and cross coupling within the head powers the unused head with 6 to 7 V which is sufficient to just begin to erase high frequencies on the unused track.

Screwing in the ferrite core of the dummy load coil L601 dropped the volts to 20, reducing the effect slightly, but this caused a change of volts on the record heads on switching from mono to stereo which could not be tolerated as the frequency responses were markedly altered.

On the Swiss *HS77 IEC* the fault did not show up at all, although the same change of volts appeared across the erase heads on switching from mono to stereo I can only assume that the impedance or depth of the gap in the erase head has been altered slightly as

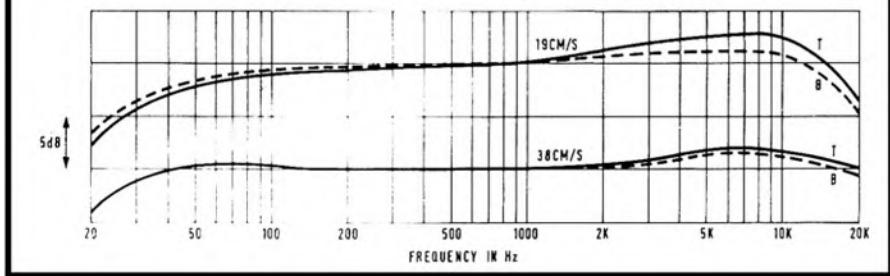
the type number has been changed from Z740 to Z940.

COMMENT

The last few paragraphs, showing concern over a 0.5 to 1dB difference in response, indicates that these *HS77* machines are in an entirely different class to the average domestic recorder and that testing and adjusting these machines to such high standards is a long and time-consuming job. It is made somewhat easier on these recorders by grouping all presets for bias, meter, record equalisation for each speed and track, etc., along the base of the recorder so that when it is removed from the cabinet they are fully accessible and well identified for adjustment with the recorder in a vertical operating position.

These recording instruments set new standards in wow, flutter, frequency response and signal-to-noise ratio which must ultimately benefit the design of transportable studio recorders.

FIG. 6 REVOX HS77/IEC RECORD-PLAY FREQUENCY RESPONSE LINE IN, AGFA PE36, LINE OUT



MUSICAL INSTRUMENT SYNTHESIS CONTINUED

or by means of switching and control circuits actuated by the capacitative changes occurring when the contacts are touched. There is virtually no limit to the range of control which can be effected in this way. Relatively simple capacitance or resistance switches can operate semiconductor gates each controlling as many signal lines as is desired, quantitative control can be exercised so that variations in finger pressure can determine dynamic changes, vibrato or tremolo can be produced by finger movements and so on. Three germinal circuits by which these controls can be achieved will be found in figs. 22 and 23, the first two being touch switches and the second an oscillator which is momentarily switched on by touching one of the points shown. Some useful 'attack' values can be produced by the latter.

Before leaving the subject of pitch determination, some mention must be made of frequency divider systems.

So far, I have dealt only with independent oscillators which are non-operative until switched on by the pitch selection device. When a large number of separate frequencies is required, as in an electronic organ or other polyphonic instrument, an economy, both in cost and space, can be achieved by providing only twelve separate independent oscillators (one for each semitone in the octave) and connecting each to a chain of synchronised, divide-by-two circuits equal in number to the number of octaves of tones required. Many different types of circuit capable of giving an

oscillatory output of frequency exactly half of the input frequency have been developed and most have been used in musical instruments. Two examples are given in figs. 24 and 25. The outputs from each divider stage are used both as basic signal currents and as a means of synchronising the stage below. These currents are usually of square or sawtooth form (but more of this in the section on tone quality).

While commercially of very great importance as a cheap means of constructing reasonable polyphonic musical instruments, frequency divider systems all suffer from the inherent disadvantage, as *polyphonic sources*, that all octavely-related notes are precisely in phase with each other. Furthermore, for any combination of notes to be available simultaneously, it is necessary that all the master-oscillators and all the divider stages should be operating continuously while the instrument is in use. The consequence of this is that *all* tones in the whole gamut are phase-related and much of the realism arising from the slight phase differences between discrete sources, however accurately tuned (which is the basis of our identification of them as individual sources), is lost.

This factor, which is a disadvantage in polyphonic instruments can, however, provide us with a most useful tool, in the synthesis of monophonic instrumental tone, if each master oscillator and its divider chain is regarded as a source of raw material for a single note. Phase-freedom is preserved and additional harmonic components made available for tonal synthesis. This is dealt with later.

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So you want to be a recording engineer?

By Gerald Chevin

THE sound recording industry in and around London is currently expanding at a considerable rate to meet the growing demand for gramophone records. This expansion has created new opportunities for potential recording engineers and tape machine operators.

The progression from 'tape jockey' to engineer depends on several factors, which vary between studios, but it can happen purely by luck. Perhaps the engineer due to balance a session fails to arrive because of illness or a traffic jam. It may well be left to the assistant to take charge and, if things go well, that particular producer may ask for the assistant to engineer his next session.

Firstly it must be stated that absolutely no glamour is attached to the position of 'tape jockey'. In fact it is hard work with little reward, financial or otherwise, and it means working very long hours. But if you are prepared to face the initial period, the hard slog will prove useful in furthering a career as a sound recording engineer.

The question is often raised—what educational qualifications are required for the job? So far there is no formula for the perfect engineer and many studios simply choose applicants with a musical background, electronics background, or a mixture of the two. Recording engineers can be split fairly easily into two categories, concentrating respectively on small groups and large orchestras. Rather more musical experience, including the ability to follow a score, is desirable for a classical recording engineer. For group work, on the other hand, the ability to mix with young people, and an ear for their kinds of music, are important. It is only fair to mention that age plays a substantial part since many groups prefer to see a young engineer at the controls, even though an older person might do a better job.

Being able to operate the tape machines quickly and efficiently is the first task most studio people learn. From there you branch out to editing and dubbing tapes, setting up for a session, and the big one—working overtime. The job should not even be considered if you are not prepared to work overtime, nights and weekends.

Finally, one should apply for a position by letter, stating qualifications, age and present job. Who knows, in a year or so, you too could be a recording engineer.

BLACK LIST

A REPLY TO PETER BASTIN'S 'THE OTHER SIDE OF THE COIN'

By H. W. HELLYER*

HE came into our shop, patently timid, weighed down by a portmanteau-sized tape recorder the manufacturer had slyly labelled 'transportable' when it was put on the market, well over a decade ago. He left, ten minutes later, a sadder and wiser man, taking his unrepairable burden.

Long experience in the trade has revealed that some makes and models are beyond economic repair. As enthusiasts—and some of us carry our daily work over into this absorbing hobby so that the border-line between work and pleasure can hardly be defined—we would love to be able to rip another of the old-timers to bits, to turn up new spindles on the lathe, to refashion bearings, strip down motors to their essentials and clean the running surfaces, and finally to add some modern refinements to the circuitry so that the veteran emerges as a piece of equipment that could compete for quality with any of its modern counterparts. As so many of these older machines were built to last as long as a battleship, the refurbishing would be worthwhile—but time costs money. Such a job would be a labour of love, and needs a good technical knowledge. Which is why, to quote from the June Editorial, so many enthusiasts 'curtail their creativeness in favour of chasing the latest transistor amplifier, the latest IC tuner, and the latest "Dolbyised" discs . . . who tolerate capstan sleeves and narrow tracks, plastic mics and miniature jacks, and then complain that their tape equipment is not as good as their gramophone'.

Which is why, also quoting the June issue,

*Technical Director, Bristol Tape Recorder Centre

people like F. W. Sutherland can earn our approbation by an intelligent improvement to a standard machine (*Extending an Akai M8*, page 235). His handful of parts may have cost shillings, and the knowledge would be current in the average workshop, but the time involved in doing the job would undoubtedly cost more than a casual customer is likely to tolerate.

Even the normal servicing processes can run up a considerable bill, when one of these veteran machines has to be tackled. If the service establishment wants to guarantee its work—and most of us do—it becomes necessary to inspect an old-timer more critically, to clean more thoroughly, to relubricate throughout and often to replace small parts that the owner may not have been aware of, let alone noted their depreciation. Otherwise, sad to say, one does a swift service job on one part of the machine and has the distasteful task later of convincing the owner that the subsequent breakdown was in no way related to the original repair.

First consideration is the availability of spare parts. Many firms have folded, others have been taken over with their new masters completely disowning earlier products. Even when the makers are still in business the stockpile of replacements will have long since melted away. If we know, as soon as our little fellow drags his equipment through the door, that certain bits and bobs are unobtainable and that some of the jobs on his ageing pet will take almost as long as building anew, then, sirs, we must fain refuse.

We do, in fact, publish a Black List, which has a copy under glass upon the counter by the till. It causes some raised eyebrows among the aficionados: 'What, you can't repair the old Thundergut? Best machine they ever made. Never goes wrong.'

Stifling our obvious rejoinder 'Why have you brought it in?' we say that yes, we agree it was good—accent on the past tense—but that even the makers have brought out new models and, though we hardly hope to be able to resell, nevertheless we would take a *Mark One* in part exchange . . .

It must seem unfortunate for us that the disappointed owner of the veteran seldom comes back to us to replenish his home rig. Too often, he goes along to the discount store, buys reduced rubbish and forswears 'hi-fi' forever.

There is no solution to the contrepoids. We must upset some in order to give good business to others. Our Black List remains, with many quite respectable names upon it: machines that have seen such good service that their owners can never accept their relegation to a scrapheap; others that came on the market like mayflies, to perish in a season, and a few, mostly foreign, whose agents and distributors have kept us waiting so long for spares that tape decks go rusty before they can be repaired.

There must be room in the fringe of the business for a service organisation willing to accept the audio jobs that nobody else is able to do. Our Editor could not have been thinking in these terms when he suggested in a leading trade magazine that audio service depots were an inevitable thing of the future. But among our readers we shall surely find one or two experts ready to have a go. What about it, lads?

Your Tape Dealer

SURREY (continued)

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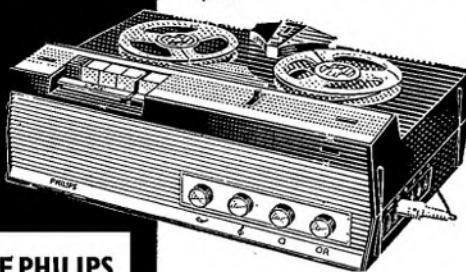
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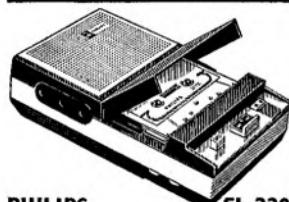


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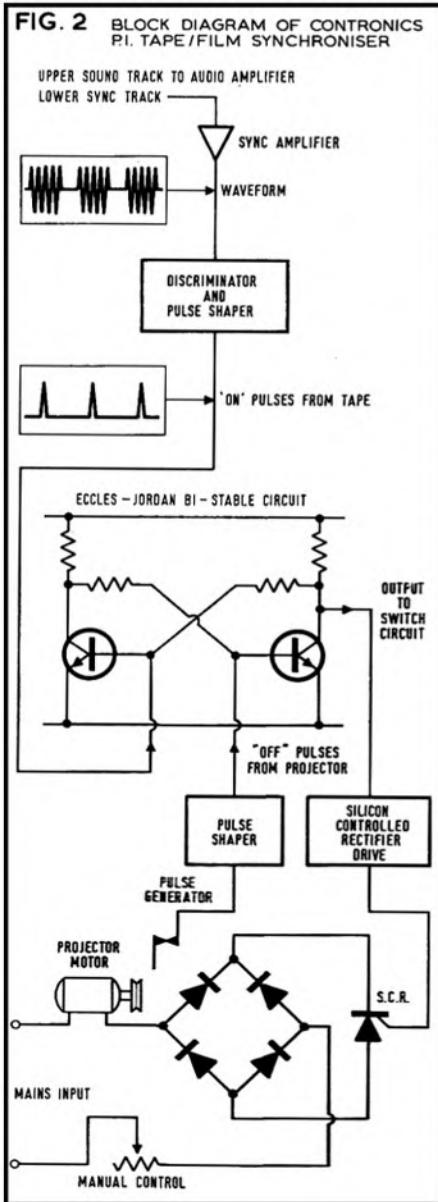
shorter time after the on pulses, and automatically correct the speed of the motor. In this manner the motor is electronically locked to the pulses on the tape by what is known as the mark space ratio of the pulses and, therefore, the projector remains in precise sync to the tape.

The pulses originate from the camera which needs a simple contact to produce one pulse per frame. As we are recording, in the first instance, for a projection system, we should bear in mind that an electric motor has inertia and if a very rapid on/off control is applied to it, it cannot immediately respond to any slight variations in the control. It requires finite time to slow down or to speed up. Slower or faster pulses may be used, but in practice, one pulse per frame is ideal for most 8 mm projectors. These pulses are recorded either on a stereo tape recorder or a 4-track machine that has been modified so that a feed can be taken from the bottom track, directly into the Cinesound without the necessity of additional amplifiers. The stereo machine could well be modified itself by adding an additional head between the sound tracks, thus allowing music and effects to occupy different tracks. The projector requires two small modifications, and these are fairly easy to carry out; the first is to fit a simple contact like a reed switch and a small magnet to the revolving shaft so that the reed relay makes and breaks once per frame when the magnet passes it; the second is to connect the synchroniser control leads into the motor circuit.

Primarily, the Cinesound is a pulse producing system ideal for 8 mm projection using a silent projector. The modifications needed are not difficult to effect, and full instructions are given in the very good handbook supplied by the manufacturers. The record unit RI which is attached to the camera is very small and light and costs £5 3s. 1d. The replay unit, PI, which is connected to the projector is again fairly small and costs £15 11s. 7d. Both electric and spring drive cameras may be used. There is a combined record/playback model CS/1 available which costs £33 0s. 5d. This unit incorporates a frames-per-second indicator, auto start switch, and circuits to accept different rates of pulse input. The Cinesound system may be used with perforated tape. This greatly assists editing but an electric camera-drive must be used with modifications to the camera motor wiring. It has no special merit for transferring to magnetic stripe as it is not desirable to try to control a magnetic projector's speed from the pulses on the recorder.

If the record unit is adapted for use with a 16 mm camera for ultimate transfer to 16 mm optical film, it must be remembered that most laboratories will only accept pulse-sync tapes that have been recorded to Nagra or Perfectone standard (i.e. two-track tape with the pulse recorded on the bottom track at *two pulses per frame* (one pulse per half-frame interval) at sound speed or 48 pulses for 24 f/s or 50 pulses for 25 f/s). The 16 mm camera, therefore, must be fitted with commutator and generator that can produce this rate and, ideally, an electric motor.

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Your own tapes transferred on to discs. Send for details: R. J. Foley Tape to Disc Service, 112 Beach Road, Scrabty, Great Yarmouth, Norfolk.

Graham Clark Records. Tape to disc pressings. 23 The Grove, Walton-on-Thames, Surrey. Tel. Walton 25627.

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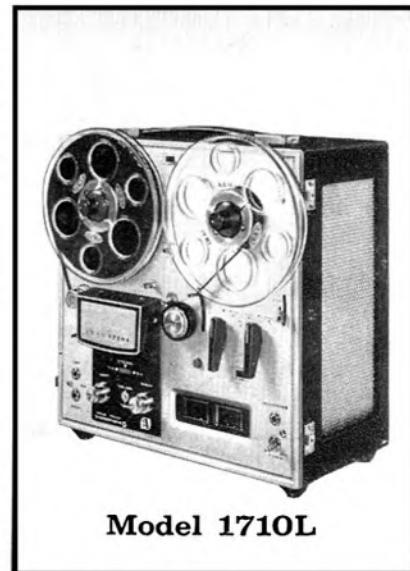
*4 track stereo/monaural recording and playback *2 speeds, 3 heads *All silicon transistorized pre-amplifier *Automatic shut off, Instant stop control *Tape cleaner *ONE MICRON GAP HEAD *Magnificent oil-finished wooden cabinet *For increased stereo enjoyment, use the matching AA-6000, 120 watt solid state amplifier and the matching speaker SW-130 (2 way, 25 watt input).

MIGNON STEREO TAPE RECORDER—1710L

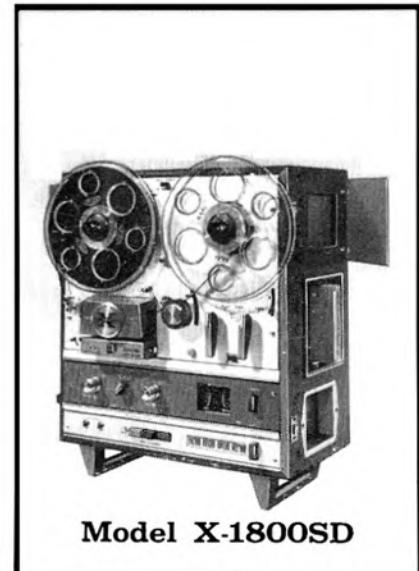
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Model 1710L



Model X-1800SD

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