

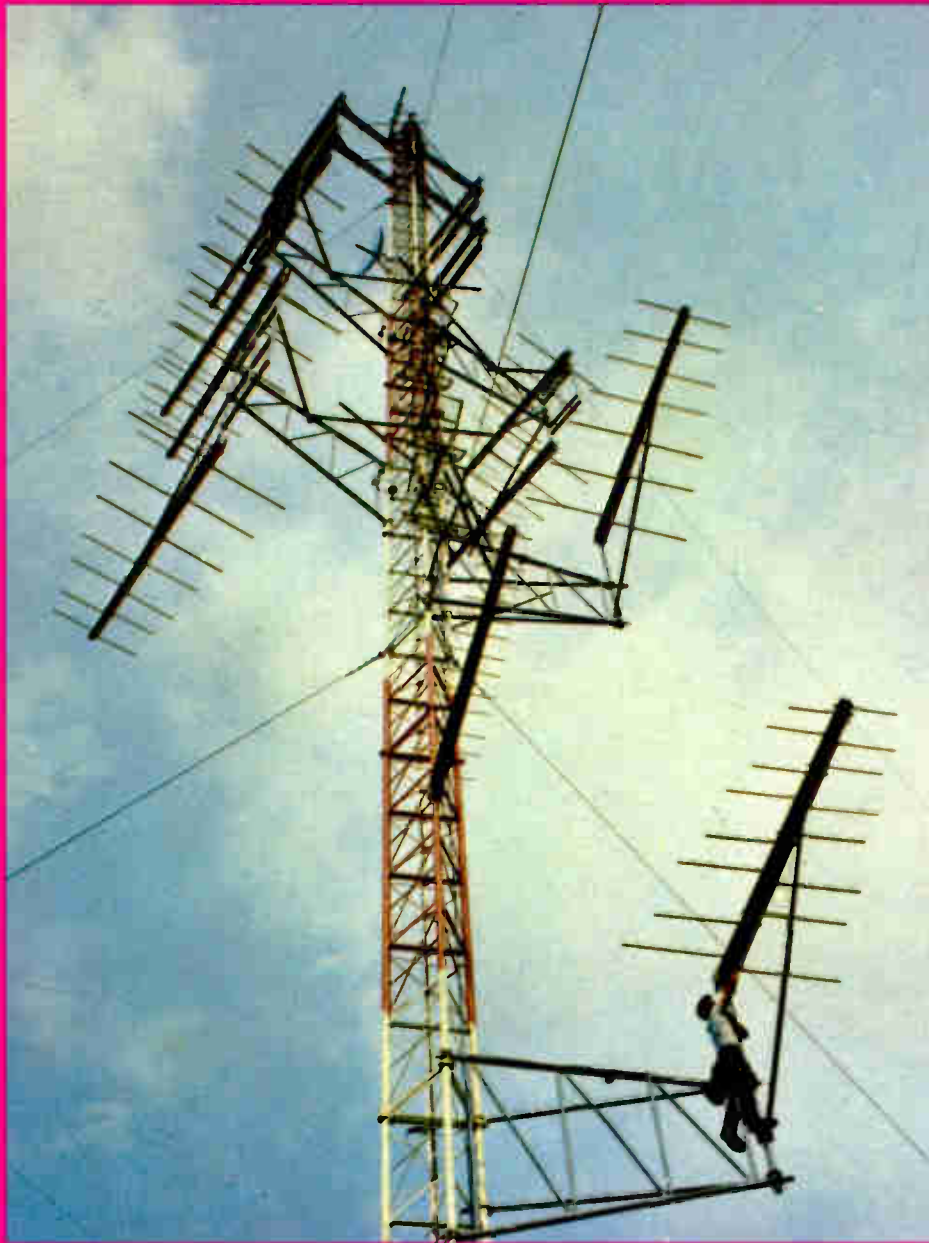
May/June '72 vol. 8/ no. 3

# ***CABLECASTING***

## ***Cable TV Engineering***



The official journal of the  
SOCIETY OF CABLE TELEVISION ENGINEERS



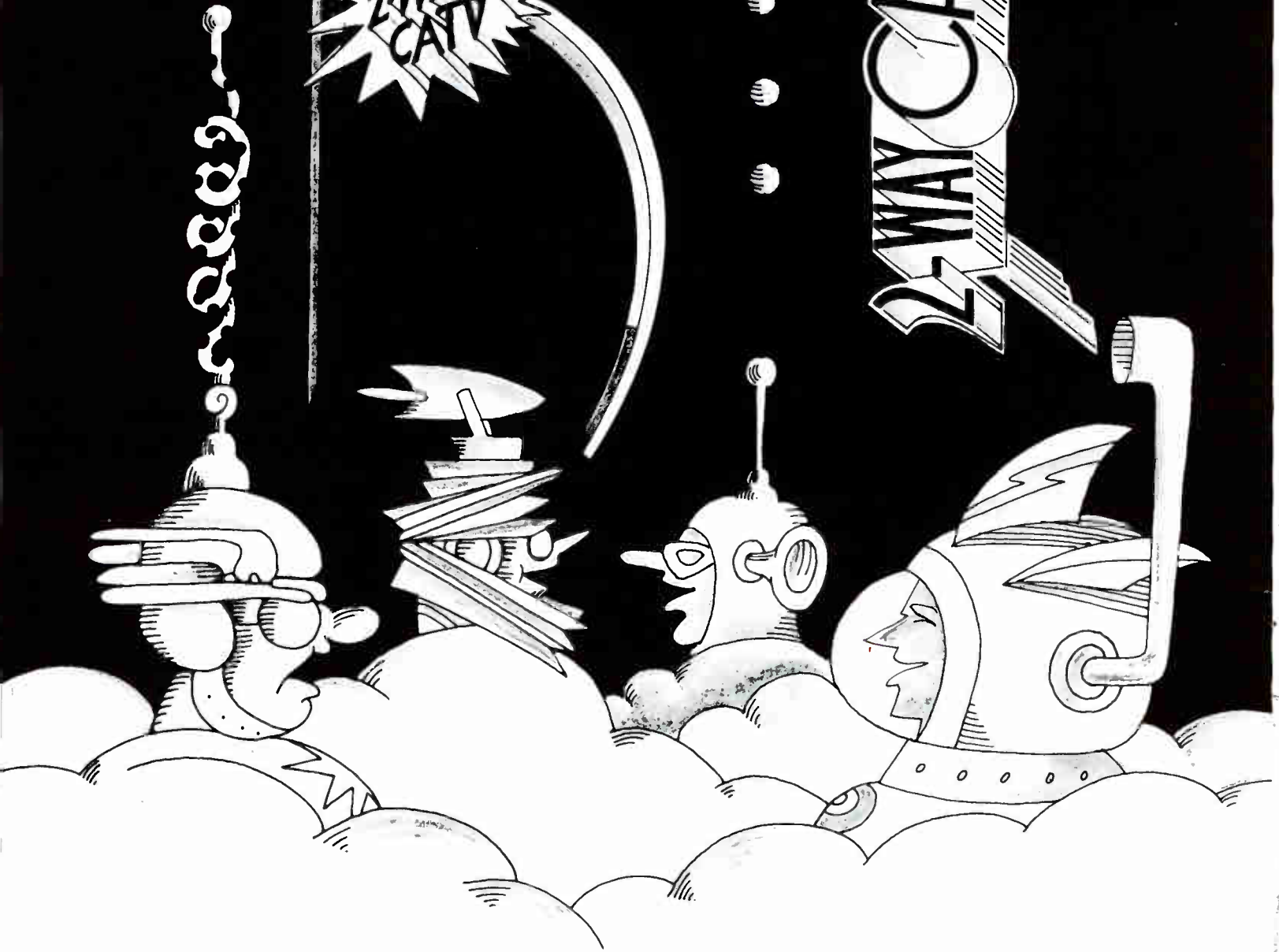
**ANTENNA RADIATION PATTERNS  
& CO-CHANNEL PROTECTION**

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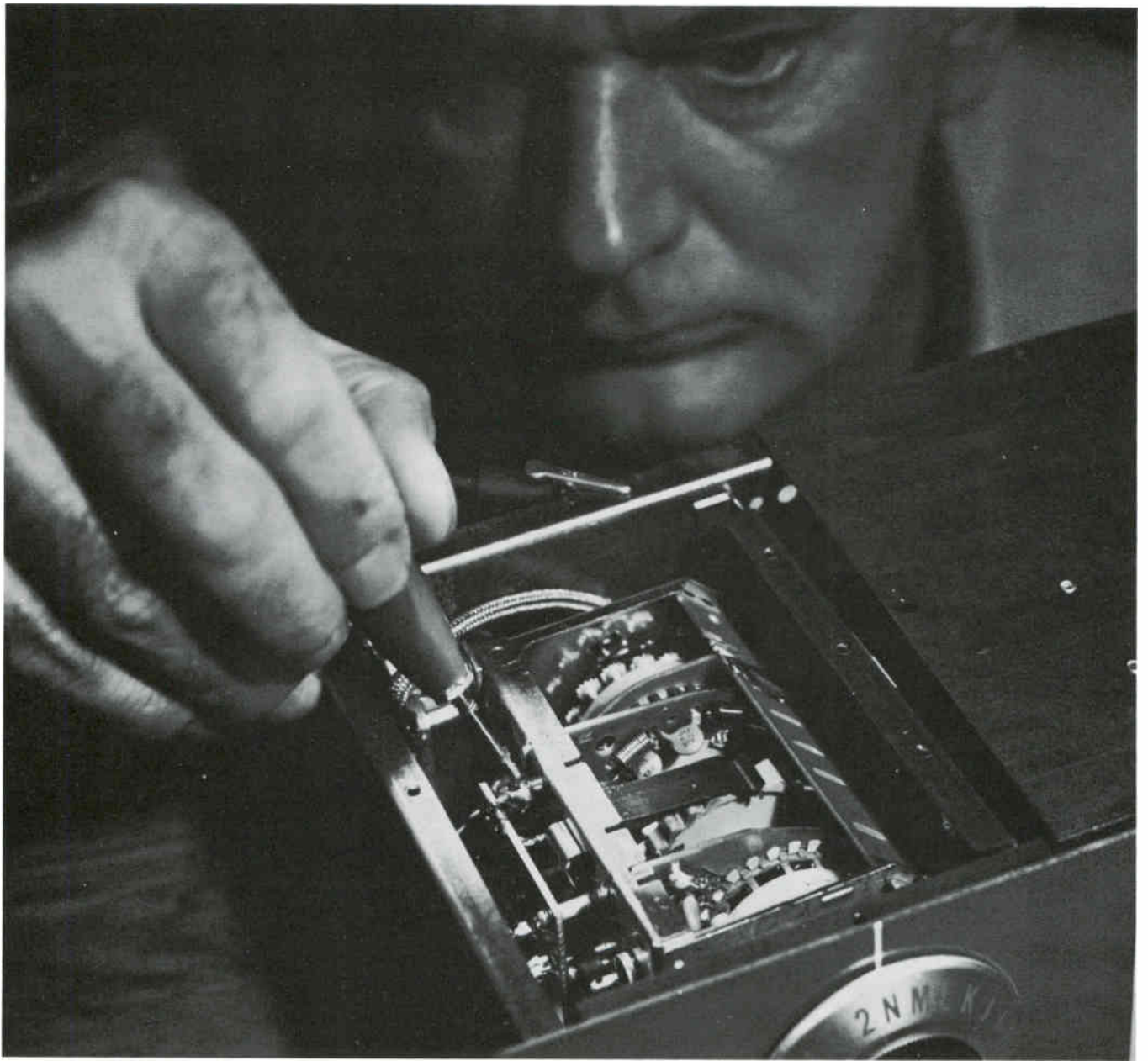
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# As We Go To Press

## CYPRESS COMMUNICATIONS CORP. SEEKS FRANCHISE FOR DAYTON IN COOPERATION WITH CITIZENS GROUP.

Cypress Cable TV of Dayton, Ohio, a subsidiary of Cypress Communications, has asked the City to authorize the construction of a \$5.5 million cable TV system to serve the urban center of the city. In addition, a jointly-owned firm in association with Citizens Cable Corp., a corporation owned solely by residents of a predominantly black area, will seek to build a \$2 million cable system in southwest Dayton. Breaking up the city in this way is in accordance with the recommendations of a report prepared by the RAND Corporation. Cypress will invest up to \$1.9 million in the southwest cable system for a 50% interest. The remaining 50% will be owned by Citizens Cable Corp. which will pay \$500,000 for its 50%; \$400,000 of that amount will be loaned to it by Cypress on a long-term, low interest basis. The minority owned corporation plans to finance the balance by a registered public sale of its voting stock, limited to persons residing in the service area of the cable network.

\*

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\*

CABLE TV COMPANY SUES SOUTHERN BELL FOR LEASEBACK SERVICE DAMAGES. Cable Television Co. of Charlotte, N.C., serving 7,000 subscribers, has entered a suit against Southern Bell Telephone Co. for damages resulting from their CATV leaseback service. In a recent interview, Sam Street, president of the managing company, stated that the defective leaseback plant is costing the cable TV company thousands of dollars in lost revenue and maintenance, plus hundreds of unhappy subscribers. The company owns 155 miles of CATV plant in Charlotte and leases an additional 145 miles of plant from the telephone company. In the complaint, Cable Television Co. alleges that the defective leaseback system will cost \$399,000 to rebuild.

\*

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\*

TVC TO ACQUIRE CYPRESS. TeleVision Communications Corp., a wholly owned subsidiary of Warner Communications Inc., has reached an agreement in principle to acquire Cypress Communications Corp. in an exchange of stock valued at about \$58.7 million. If and when the deal goes through, TVC's cable TV holdings will serve about 360,000 subscribers, making it number two to TelePrompTer. (which has about 620,000 subs)... MACLEAN-HUNTER CABLE TV BUYS 25% INTEREST IN EDMONTON SYSTEM. Subject to approval of the Canadian Radio Television Commission, Maclean-Hunter will have the 25% interest in QCTV Limited, which holds a cable TV license for the west half of the City of Edmonton, with a potential of some 75,000 homes in its area. The system presently serves about 1,500 homes and is in the first phase of its construction.

\*

\*

\*

WISCONSIN, GEORGIA SYSTEM COMPLETED. AEL Communications Corp., the CATV subsidiary of American Electronic Labs in Lansdale, PA., has just completed turnkey installation of dual cable plant in Racine, Wis., for Telecable of Racine (a division of Telecable Corp. of Norfolk, VA.). This system consists of more than 200 miles of plant. AEL has also completed a turnkey installation of a 200 mile plant in Columbus, GA. for Telecable of Columbus... TOCOM FILES FOR A PUBLIC STOCK OFFERING. TOCOM, Inc. (formerly CAS Manufacturing Co.) of Dallas has filed a Registration Statement for a proposed offering of 267,000 shares of common stock. Underwriters are McKinney, Rose & Co. of Dallas... John R. Woods, President of Systems Wire and Cable Inc. reported 1972 first half earnings of \$113,441, a 13% increase over the same period of 1971... General Instrument Corp. Chairman predicts CATV growth rate of 21% for the building and rebuilding of CATV systems. According to Mr. Moses Shapiro, the CATV market will go from \$145 million to \$255 million by 1974.

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## PEOPLE IN THE NEWS



**GEORGE L. FLETCHER** has joined Suburban Cablevision Inc. (Whippany, N.J.) as Manager of Field Engineering. In this newly-created position, Mr. Fletcher will be responsible for the technical performance of the com-

pany's CATV systems, assuring that they are in compliance with the new FCC regulations. Mr. Fletcher brings with him seven years of experience encompassing design, engineering and field sales.

• • •  
**DUANE CRIST** has been named Acting Sales Manager of the Theta-Com CATV Division (formerly Kaiser CATV). Mr. Crist joined Kaiser CATV in 1970 as manager of Special Projects after serving with Anaconda Electronics from 1967 to 1970 as Vice President-Marketing. Prior to that he was with Ameco.

• • •  
**ROBERT SCHENROCK** has been appointed Manager of the Allband CableVision system (of TeleVision Communications Corp.) in Olean, N.Y. Mr. Schenrock was super-



intendent of construction for TVC's Akron CableVision and before that for Cablevision of Savannah and for Jerrold.

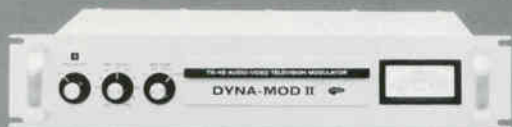
• • •  
**MELVIN GRAY**, who was a sales engineer in the New England area for Jerrold Electronics, has been advanced to Northeastern Regional Sales Manager by the firm. Mr. Gray is a communications graduate from Boston University; he joined Jerrold in 1957.

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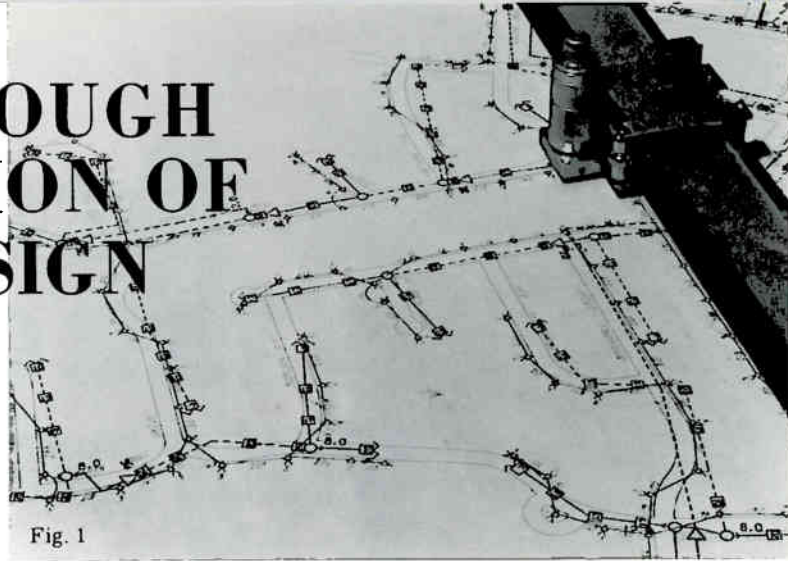
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# RELIABILITY THROUGH TOTAL AUTOMATION OF CATV SYSTEM DESIGN

by Ivan T. Frisch, Bill Rothfarb,  
& Aaron Kershenbaum

Network Analysis Corporation



In the July/August, 1971 issue of *Cablecasting* magazine, we described the principles of computer CATV system design. Since that time, we've made some changes in our operations and learned some things which we think may be of importance to cable television engineers interested in the application of computer technology to system design.

To augment its CATV design service NAC has recently completed an automated drafting program. With this new feature, layouts developed by NAC's design program are drawn as complete final construction maps by an automatic drafting machine under direct command of the computer. The specific advantages of automatic drafting are numerous:

**Elimination of Drafting Errors.** One time-consuming factor in the past has been the drafting and checking of maps. Once a human is introduced into the design-drafting process, errors are introduced and hence there is a need for a long checking process. To check a typical 100-mile system for every tap value and location, as well as all amplifiers, power supplies etc. takes a checker about one week, and still drafting errors slip by. With the automatic plotter, the layout is **drafted** exactly as designed. The net result is less headaches for construction crews and better systems for owners.

**Faster Layouts.** The 10 mile system shown in Figure 1 was drafted by the computer in 15 minutes, including all linework, symbols and lettering. A typical 100 mile system is drawn automatically at 200' to the inch, in about **four hours** of plotter time. In other words, the time to produce correct drawings has been reduced by a factor of 20 over the efforts of a draftsman and checker.

**Complete Flexibility in Drawing Modifications.** As any system designer knows, very few layouts remain untouched once they are completed. Strand changes are discovered. Telephone poles seem to move with a life of their own and people are found to live on unmapped streets. Often these sections are redesigned on the spot. The new information can then be fed to the program which will modify

the appropriate sections of layout or redraw a whole map, or a whole system as the user wishes.

**Complete Flexibility in Presentation.** The computer can make the drawings to any scale. You may want one drawing at 200' to the inch and another overview drawing at 400' or 1000' to the inch. Instead of resorting to microfilm and photo reduction methods, the plotter will simply produce the required drawing. It can isolate any section of the design and draw it to any required scale. For example, it can break out the trunk routing as a separate drawing.

**Complete Flexibility in Format.** The program has a library of symbols that can be used for any particular device. If the system owner wishes a different symbol, it can easily be added to the library. At present we have all the NCTA standard symbols in the library as well as many variations of these symbols in use by our clients.

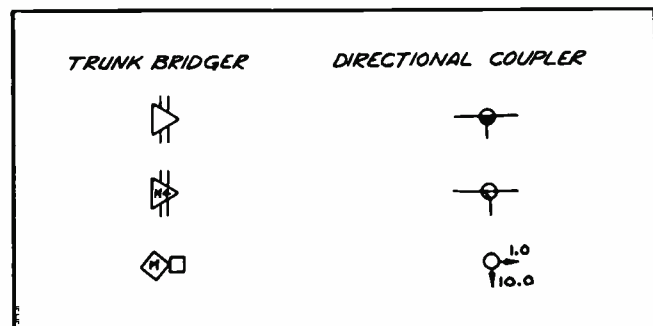
Thus, for example, the symbols for trunk bridgers and directional couplers shown in Figure 2, are all in the library, even though the last symbol for the trunk bridger is not a standard NCTA symbol.

In summary, automated drafting produces its results faster than humans without introducing drafting errors. The system owner does not have to choose speed or reliability; he gets speed and reliability.

## Reliability And Flexibility

One of the most persistent misconceptions fostered by manual designers is that they "overdesign"

Fig. 2. Some of the symbols in NAC's computer library of symbols.



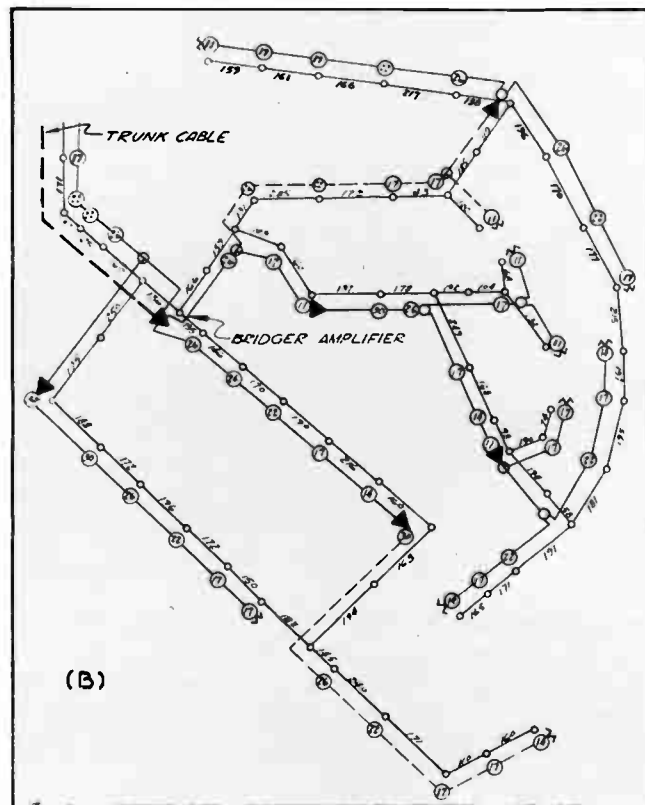
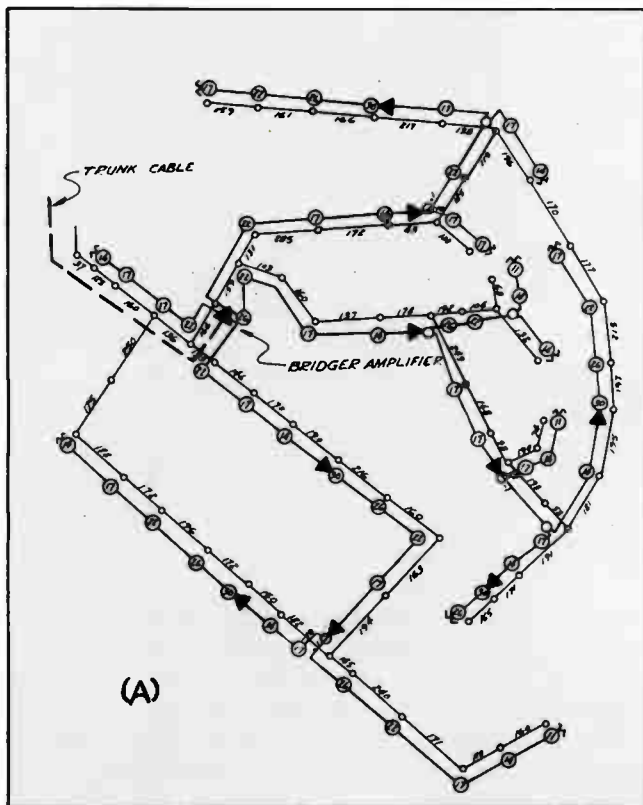


Fig. 3. Comparison of NAC's computer design with an industry manual design. (A) is industry design; (B) is NAC's computer design.

a system by putting extra amplifiers in so that they have more reliability and more slack for flexibility. **This is absolutely false.** There is indeed extra equipment and more cost. But, obviously, with more electronics there are more failure prone elements in the system and less overall reliability.

For example, the design in Figure 3A shows an industry manual design for one section of a larger 100 mile system. The computer design for the same section is shown in Figure 3B. The manual design has 4 more extender amplifiers than the computer design. Furthermore, there are 3 places where there are 3 extenders in cascade in the manual design whereas there are none in the computer design. The computer design is obviously more reliable. In general, if reliability data is available for different types of amplifiers, such as trunk and extender amplifiers, the computer will take them into account trading off amplifiers for the best design.

The claims for added slack and flexibility in manual designs also turn out to be patently false upon examination of the available evidence. As an example, the minimum input level to extender amplifiers in the designs in Figure 3 was 20 dBmV. For the computer design, signal levels are high enough so that the feeders could be extended or taps could be added if necessary without adding extender amplifiers. In the manual design, some of the end levels are tighter even though there are more amplifiers. Furthermore, the computer designed system is easier

to expand or change because there only two extenders in cascade.

The net result is that the manual design with more electronics is, in every sense, a poorer design--more expensive, less reliable and less flexible. **The manual design has wasted electronics** which in no sense adds to the system performance--only the system cost. The way to improve system reliability is to first adopt more rigid system specifications--and then find the most cost effective design meeting those specifications. With computerized design, it is actually possible to design to significantly tighter specifications with no additional cost over a more poorly performing manual design.

In addition to drafting errors and poor designs one of the primary hazards of manual designs to system owners, builders and users are good old-fashioned errors and blunders. Sometimes these are errors in bills of materials, but more often and more seriously, they are technical errors which make the system unreliable, or indeed, incapable in meeting contractual specifications.

### Manual Design Errors

The types of errors made by manual designers, of course, include every possible error that can be made. Some of the more prevalent and representative types that we have come across are shown in the examples below. Needless to say, the computer can not make these errors.

**Signal levels at subscriber taps.** In the portion of the industry design shown in Figure 4, the output levels of the taps are given. The required tap output level is 10 dBmV. Note that on one tap the signal level

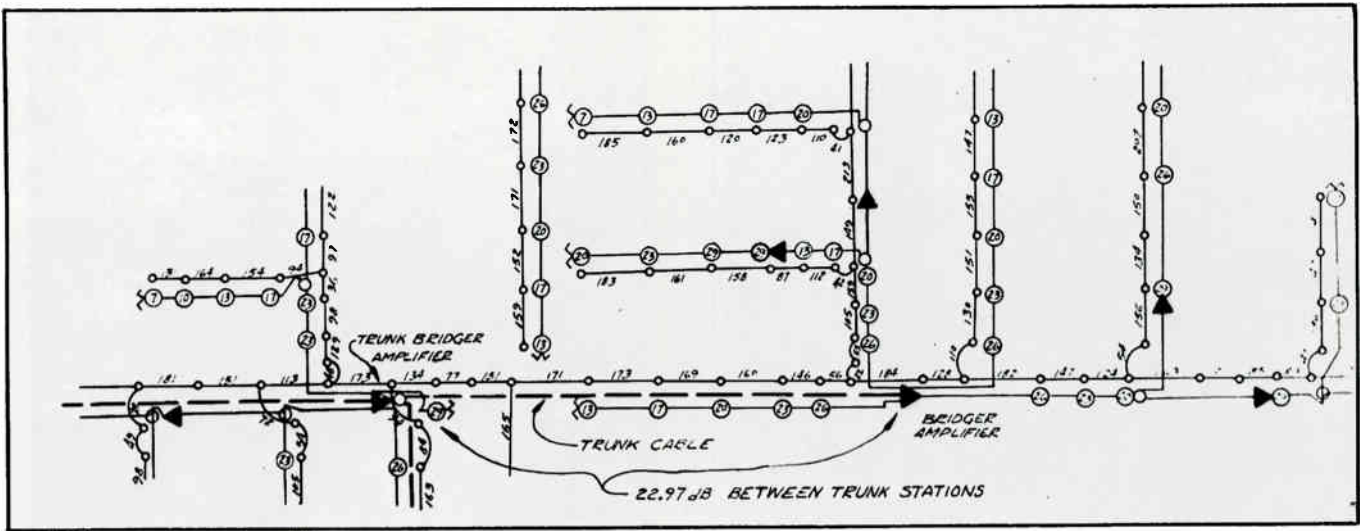


Fig. 5. A manual design in which trunk spacing violates system requirements.

is 3 db too low--the customer is receiving only one half his required signal power. This is one of the most persistent types of design fudges. In one design, the signal over 20 of the taps did not meet the required output level. With proper design this type of fudge is unnecessary.

**Trunk spacing.** In Figure 5 is a manual design in which the required 22 db trunk spacing is exceeded by .97 db. Errors on the trunk of this sort are truly unfortunate since the resulting distortion propagates throughout the remainder of the system. In major markets where cable signals are competing with off-the-air pickup, the resulting poor quality pictures are particularly serious.

**Power requirements.** Figure 6 shows an industry design with 6 extender amplifiers drawing power from one output of a trunk bridger amplifier thereby exceeding the power passing capability of the bridger. This means that subscribers will not be getting decent service until a section of the system is rebuilt.

Our experience has shown that these types of errors occur repeatedly in manual designs. Why are there so many errors in layouts produced by industry designers? There is probably no single reason al-

though there are obviously many critical factors.

The quality of designers in the industry varies greatly. A designer with five years experience is usually superior to a designer with one year of experience. With the rapid turnover of designers, and the rate of introduction of new lines of equipment, many designers don't get much experience with particular equipment. With those that do, the "Peter Principle" takes its toll: good designers don't usually end up being good designers--they end up being managers.

If the situation is bad now, there are indications that it will get worse. If the recent FCC rulings lead to a spurt in construction, the present designers are clearly going to be swamped. The typical design will be even poorer and may take longer to produce. The FCC decision makes the computer not only a useful tool but a vital one.

Fig. 6. A manual design in which power passing capability of a trunk bridger amplifier is violated.

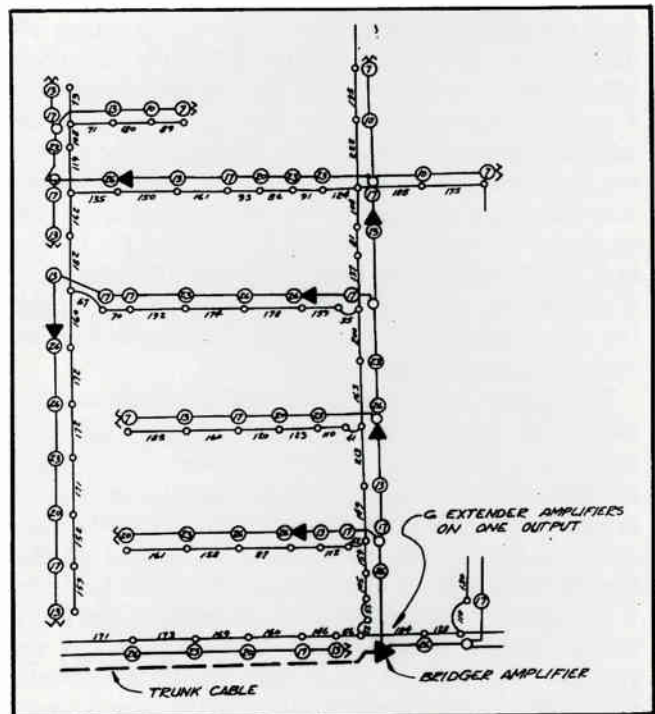
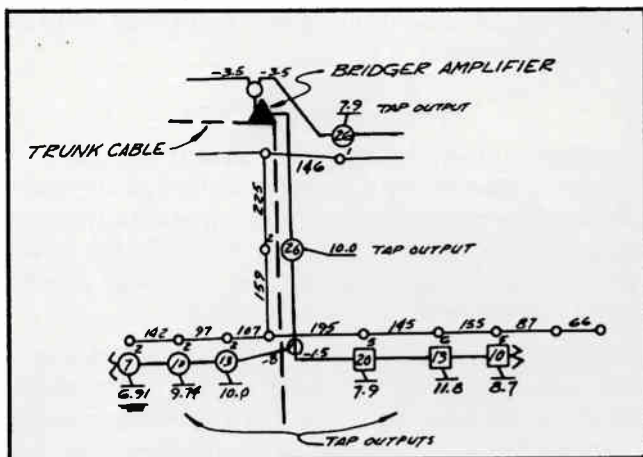


Fig. 4. A manual design in which tap output levels do not meet specifications.



# ANTENNA RADIATION PATTERNS & CO-CHANNEL PROTECTION

by Steven I. Biro

B-RO Antenna & Head-End Engineering

**A**ntenna manufacturers publish a more or less complete list of electronic parameters on their specification sheets, including: gain, bandwidth, input match, front-to-back ratio, beamwidth, etc. As far as co-channel protection is involved, specifications such as bandwidth, gain and match are **not** pertinent. What really counts is the antenna radiation pattern; not over-optimistic and over-simplified graphs, but the **actual** radiation patterns, as recorded on the antenna test range. Let's discuss the most important aspects about radiation patterns, and how to evaluate them.

## RADIATION PATTERN BASICS

Co-channel interference protection is basically an antenna radiation pattern problem. At one extreme, let's consider the turnstile type antenna. Exhibiting a horizontal omnidirectional pattern, Figure 1 (A), the antenna would receive stations from all directions, generating intolerable co-channel interference conditions.

On the other hand, the ideal CATV antenna array would exhibit a pencil beam radiation pattern, Figure 1 (B), receiving signals only from one direction, the direction of the **desired** station. This antenna would reject any other station operating on the same channel.

In the real world of CATV, where co-channel protection is primarily a **low-band** problem, pencil beam type radiation patterns are unattainable because the size of the array could easily approach the dimensions of a football field. Today's CATV arrays exhibit radiation patterns with a more or less narrow main lobe, and numerous side and backlobes. Should the antenna array create a null in the direction of the co-channel offender, protection is assured. If the antenna array happens to exhibit medium or even minor lobes in the direction of the co-channel station, the array will provide only **limited** protection.

Antenna manufacturers often publish vertical (H-plane) and horizontal (E-plane) beamwidth data, and radiation pattern displays. Since various co-channel

offenders arrive from different **azimuth** angles, the vertical radiation pattern information is irrelevant. Only the horizontal (E-plane) will fully describe the antenna performance as related to co-channel protection.

The horizontal radiation pattern of an antenna may be presented in polar or rectangular coordinates. Polar presentation is preferred in popular publications because this information gives an easy to understand picture of the received or transmitted power distribution. By contrast, the **rectangular** radiation pattern permits a presentation of much finer details, including precise angle and dB readings of peaks and nulls.

The radial deflections on the polar and rectangular charts may be arranged in:

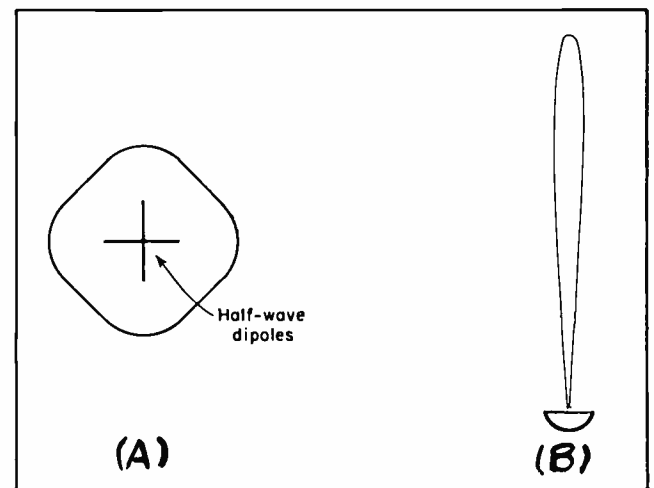
Linear scale

Power scale

dB scale.

The dB scale, presenting the received signals' logarithmic variations, is the most suitable for the

Fig. 1. Polar radiation patterns for a turnstile antenna (A), and an ideal CATV single channel array (B).



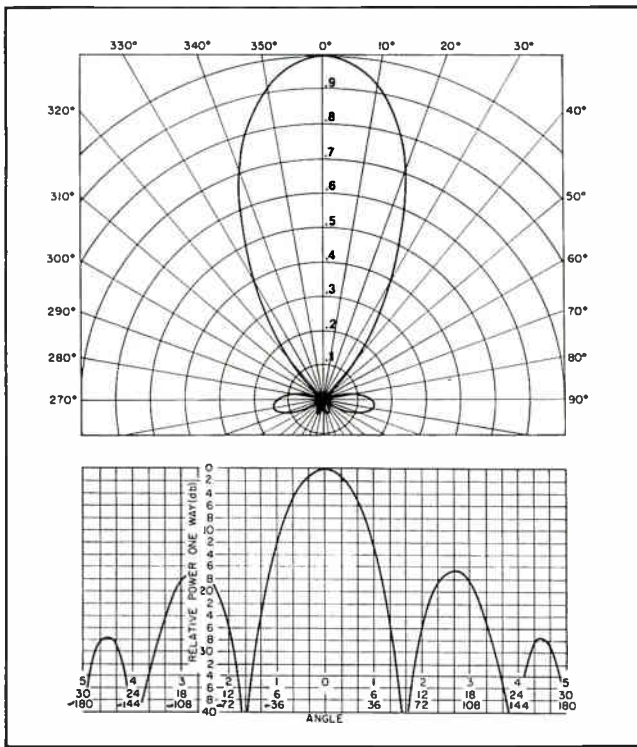


Fig. 2. Here the same antenna has been tested twice. Compare the readability of a polar and horizontal radiation pattern presentation.

examination of antenna array radiation. A dynamic range of 40 to 50 dB permits the evaluation of deep nulls and otherwise fuzzy sidelobes.

Figure 2 presents a polar and a rectangular radiation pattern taken from the same antenna. It should be noted that while location, depth, and width of the null of 168° is somewhat unclear on the polar pattern, the rectangular pattern offers good readability.

### RADIATION PATTERN ANALYSIS

There are a number of important factors determining the co-channel protection capability of an antenna-array, all readable from the radiation pattern:

- The exact azimuth angle of the nulls
- The depth of the nulls
- The width of the nulls
- The shape of the main beam.

Actual co-channel offenders should be identified by an on-site signal survey. The azimuth angles of these identified offenders may then be determined to the last 1/10° by computer controlled calculations. Thus the CATV engineer should be convinced that on the wanted channels, the radiation pattern nulls fall in such an angle.

If a standard antenna-array is used, such as a diamond array of L-P antennas with a fixed mechanical structure, the radiation pattern must be closely examined to see if it exhibits a null in the direction of

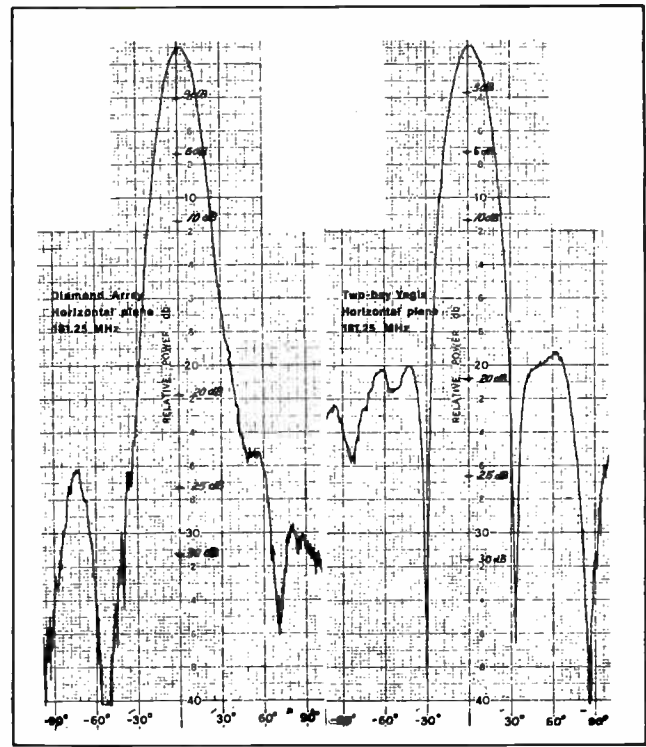


Fig. 3. Side-by-side presentation of radiation patterns of a standard diamond array and a custom-designed array of yagis. The co-channel interference was arriving from -30 degrees.

the identified co-channel interference. On the other hand, an antenna array may be custom designed to force nulls in the directions from which the interfering signals arrive. In these cases, actual radiation patterns may confirm whether the nulls are right on the target, and how deep they are.

Nulls exhibiting 20 dB depth cannot be considered adequate co-channel protection. 40 dB deep nulls are highly desired but seldom demonstrated on actual radiation patterns.

Figure 3 is a side-by-side presentation of the diamond array versus a phased yagi on Channel 8. Compare the co-channel protection results at -30° off from the main direction.

The depth of the radiation pattern nulls may also be conveniently identified from a rectangular radiation pattern with a dB scale, enabling the CATV technician to confirm manufacturers' specifications, or to discover over-optimistic claims.

Figure 4 illustrates the need for F/B ratio specification checks by radiation patterns. The manufacturer's specifications stated 30 dB protection from the back. The radiation pattern indicates that the array indeed provides 30 dB protection from 180°. However, the co-channel offender, arriving from 165° azimuth — and we can still call this "from the back" — will be attenuated only by 25 dB. This is 5 dB short of expectations based on "general" specifications.

The width of the null is an additional important characteristic with which to be concerned. From a dB scale rectangular radiation pattern, this parameter

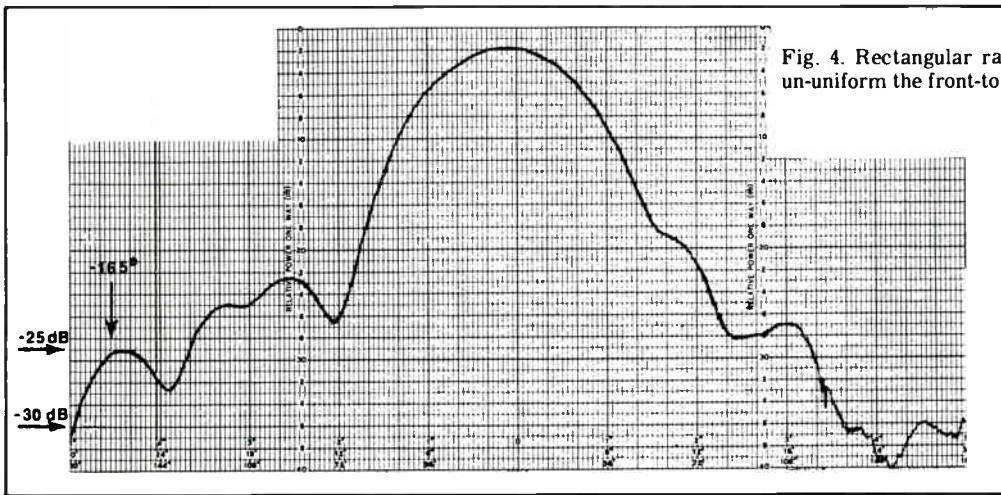


Fig. 4. Rectangular radiation pattern showing clearly how un-uniform the front-to-back ratio can be.

may be precisely measured at any null location. Very narrow ( $1^\circ$  to  $3^\circ$ ) nulls should warn the CATV technician of two possible problems:

1. It is difficult to orient a tower mounted CATV array with such accuracy due to normal working conditions.
2. Under medium to heavy wind conditions, the twisting of the CATV tower, combined with the movements of the antenna gates and pipes, could skew the nulls of the radiation pattern by several degrees, thus significantly decreasing co-channel protection.

Nulls of  $5^\circ$  to  $8^\circ$  width are considered optimum for CATV application.

It is not uncommon to encounter asymmetrical radiation patterns. A re-examination of the diamond array pattern and horizontally stacked two-bay pattern (Figure 3) shows a number of asymmetrical features. These include a missing null at  $-90^\circ$  on the two-bay pattern, and the development of a broad shoulder on the diamond array at  $+50^\circ$ . These are warning signs indicating that either the antenna test range or the constructed arrays have hidden faults. If co-channel conditions warrant the need for extreme caution, the radiation pattern testing should be repeated on a slightly altered test range, or with a different mounting, in order to identify the nature of the asymmetrical pattern performance.

Figure 5 is a classical example of a questionable radiation pattern, not to be accepted for evaluation

purposes. The radiation pattern of a log-periodic antenna is presented in this chart. Note that the signal level responses differ considerably at  $180^\circ$ , for no apparent reason. On the left side, the curve dips to  $-22$  dB, while on the right side it levels off at  $-13$  dB. The resulting 9 dB difference between the left and right side could indicate that the recording equipment is not working correctly, or that the transmitter/receiver suffers from instability.

The frequency of radiation pattern testing is also an important qualifying parameter. Co-channel beats are generated by the video carriers of two or more stations. Therefore, for co-channel evaluation, the radiation patterns must be tested on the respective video carrier frequencies. The pattern response may or may not change within a couple of mHz; however, the bearings of the nulls, the depth of the nulls, and their width may shift considerably, warranting on-video carrier testing.

Antenna arrays mounted on small diameter pipes on the top of the wooden test tower exhibit perfect radiation patterns with deep nulls. But mounted on metal antenna gates, in the vicinity of a 48" or 60" face tower, they may not perform as well. Reflections from the horizontal braces of the tower and the long horizontal pipes of the antenna gates will generate phase sensitive cancellations, filling in the deep nulls in the pattern, or causing null-shifts. There is little point therefore in publishing a "mast mounted" radiation pattern for a diamond array, if the array must be mounted on a CATV tower with 40" to 60" tower face.

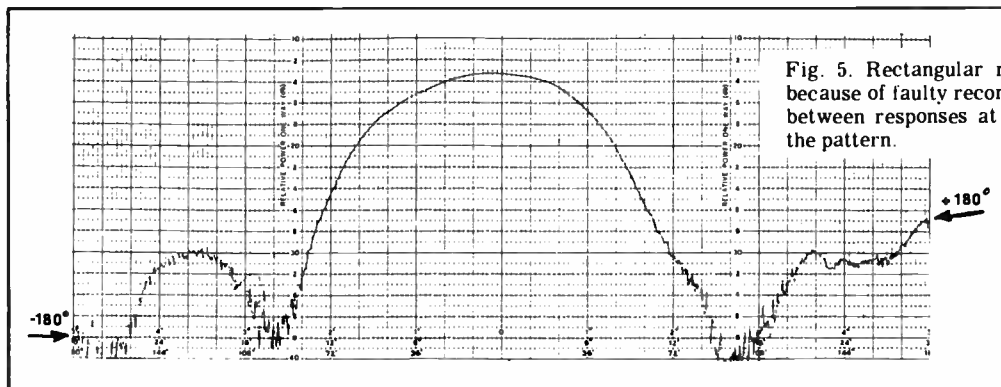


Fig. 5. Rectangular radiation pattern which is incorrect because of faulty recording equipment--note the discrepancy between responses at 180 degrees on the left and right of the pattern.

Monday, May 15th

# TECHNICAL SESSIONS of NCTA Annual Convention

**8:00 AM Eye Opener Workshop**  
*Bel Air Rm.*

Sponsored by the Society of Cable TV Engineers, this will be a free-wheeling discussion by experts regarding short haul microwave, led by Roger Wilson of TelePrompTer.

**10:15 AM Satellite/Cable System Engineering**  
*Williford Parkor B*

A conference Highlight — this session will present information on how the cable industry will be involved in the satellite experiments for distribution of high quality television to schools and homes. An analysis of the domestic satellite situation as it relates to cable will also be presented. Speakers will be Dr. Richard Marsten of NASA and Ralph Clark, consultant.

**2:00 PM Blue Sky to Cash Flow**  
*Boulevard Rm.*

There are a great many functions suggested for cable TV systems — some of them are even being performed. Dr. Peter Goldmark, John O'Neill of MITRE, John Ward of MIT, and Robert Behringer of Theta-Com will try to keep our feet on the ground in this guessing game.



**TUESDAY, May 16th**

**8:00 AM Eye Opener Workshop**

*Bel Air Rm.*

Sponsored by the SCTE, this discussion will cover technical training, and will be led by Jake Landrum of Commco Inc.

**9:15 AM Technical Rules and Standards**

*Williford Parlor B*

An unusually timely session, with the adoption of the new FCC rules and regulations, this session will present a discussion of the new technical standards, their interpretation, and techniques for conforming to them. A discussion of logical steps leading from a typical cable operation to complete compliance will be presented. Speakers are Sydney Lines of the FCC, Norman Penwell, Jerald Crusan of Jerrold, and Linley Grumm of Tektronix.

**9:15 AM Program Origination**

*Boulevard Rm.*

Featuring talks on audio techniques for TV by Bernard Wise of CCA, Privacy for Cable Services by Frank Eldridge of MITRE, and VTR selection by Ronald Hymas of Telemation.

**2:00 PM Cable Channel Allocations**

*Williford Parlor B*

This is a presentation on the next big industry requirement as it moves into operation with more than 12 services. Dr. Robert Powers of the OTP will talk on channel allocation options, Nate Levine of Sammons Communications will talk about the dilemma of mixed systems, I. Switzer will talk on carrier considerations, and Parker Ellsworth of Magnavox will describe subscriber terminal interface requirements.

**2:00 PM Cable System Operation**

*Boulevard Rm.*

The papers in this session will include presentations of valuable experience in many aspects of cable operation. They include discussions of a documentation process for CATV systems, of field strength monitors, and elimination of cross modulation. Also antenna site problems, surge protection and the use of retreaded aerospace engineers.

**Wednesday, May 17th**

**8:00 AM Eye Opener Workshop**

*Bel Air Rm.*

SCTE sponsored discussion on lightening protection, led by Robert Bilodeau.

**9:15 AM Two-Way System Experience**

*Williford Parlor B*

This session will present the real life experiences of those systems actually experimenting with two-way operation. In some cases, it will be the first public presentation of preliminary data on new systems. They will include the results of market and field tests to develop public reaction to various innovations in Norfolk and Reston Va.; Jonathan Village, Minn.; London, England; and Los Angeles.

**9:15 AM Advanced Techniques and Designs**

*Boulevard Rm.*

The papers in this session will discuss new or evolutionary concepts. These include improved reliability through automated system design, the application of digital transmission engineering for auxiliary services, and others.

**2:00 PM Underground Engineering**

*Williford Parlor B*

The municipal codes and regulations involved, installation techniques, trade-offs and costs, and reliability and maintenance factors.

**2:00 PM Multi-Channel, Microwave Distribution systems**

*Boulevard Rm.*

This session will present discussions of four different technical approaches to this operation. This will be an opportunity to make direct comparisons of key operating characteristics. Also, Douglas Milne of Varian Associates will talk about the new FCC proposed multi-point microwave service in the 2110-2113 MHz band.



## SOCIETY OF CABLE TELEVISION ENGINEERS

Since its founding in June, 1969, the Society of Cable Television Engineers has grown rapidly. On this and the next 11 pages are the names of the current members of the Society, listed by geographic region. In addition to these members, the Credentials Committee of the Society is now reviewing the applications of many other CATV engineers and technicians who have applied for membership.

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- Alfred J. Zimmermann, Comtec Inc., P.O. Box 747, Hilo 96720

## NEW ENGLAND CHAPTER

- Richard Blais, Paper City TV Cable, 215 Main St., Berlin, N.H. 03570
- Rex C.S. Chien, M. I. T. Lincoln Labs, Lexington, Ma. 02140
- Donald B. Fairbrother, Sanders Associates Inc., Daniel Webster Highway South, Nashua, N.H. 03060
- John A. Fergie, Springfield TV Broadcasting Corp., P.O. Box 2210, Springfield, Ma. 01101
- Albert K. Fowler, R F Systems, Inc., 155 King St., Cohasset, Ma. 02025
- John J. Guachione, Pittsfield/Dalton TV Cable, 301 North St., Pittsfield, Ma. 01201
- David E. Karrmann, Karrmann Assoc., Inc., Church Plaza, 129 Highland Ave., Cheshire, Ct. 06410
- Anthony S. Katona, Northwest Cablevision Inc., 110 Main St., Winsted, Ct. 06098
- John J. Kelleher, III, New England Telephone Co., 185 Franklin St., Rm. B-11-L, Boston, Ma. 02107
- J. J. Mueller, EMCO CATV, Inc., P.O. Box 646, Manchester, Vt. 05254
- Scott A. Ricci, Chesterfield Cablevision, Inc., P.O. Box 213, Spofford, N.H. 03462
- William M. Ruiz, Jerrold Electronics, 17 Sutton Pl., Agawam, Ma. 01001
- Richard K. Schroeder, New England Tel. & Tel. Co., Room 300, 260 Summer St., Boston, Ma. 02210
- Samuel A. Shearer, Cox Cablevision, 192 College St., Burlington, Vt. 05401
- Melvyn E. Shlank, Community TV Systems, Inc., 1326 Whalley Ave., P.O. Box 3023, New Haven, Ct. 06515
- Lloyd Tate, Community Management Corp., 6 Vista Way, Merrimack, N.H. 03054

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- Ronald A. Arbisi, Television Transmission Co., 301 Peru St., Peru, Il. 61354
- Richard Ashpole, Quincy Cablevision, Inc., 116 North Fifth St., Quincy, Il. 62301
- G. E. Baldwin, Lake Charlevoix Cable TV, Inc., 202 State St., Charlevoix, Mi. 49720
- Don Bertling, Valley Antenna Systems, 1625 Covington Ave., Piqua, Oh. 45356

- Cliff Beyersdoerfer, 1905 Warren St., Marion, Ill. 62959
- Chas. E. Birkett, Cox Cablevision, 1307 Columbus, Wabash, In. 46992
- Peter C. L. Boyce, Boyce Service Co., 604 Navajo Drive, New Albany, In. 47150
- Robert A. Brooks, J. C. Barnard & Associates, 10121 Manchester Rd., St. Louis, Mo. 63122
- Donald L. Brown, Cable Communications of Iowa, Inc., 57 South Court St., Fairfield, Ia. 52556
- Everett L. Burrows, Wisconsin CATV Inc., 415 S. Barstow St., Eau Claire, Wi. 54701
- T. G. Cady, Keokuk Cablevision, 409 Main St., Keokuk, Ia. 52632
- James Camsky, Wheeling Antenna Co., P.O. Box 1043, Wheeling, W.V. 26003
- Michael E. Charchenko, G-F Cable TV, 414 N. Washington, Grand Forks, N.D. 58201
- David W. Chase, Spencer Community Antenna System, Inc., 313 Grand Ave., Spencer, Ia. 51301
- Donald E. Clark, Logansport TV Cable, 214 South 6th St., Logansport, In. 46947
- Don Countryman, D. F. Countryman Co., 1821 University Ave., St. Paul, Mn. 55104
- G. W. Cummins, Full Vu Television, 1029 North 4th St., Vincennes, In. 47591
- Buell Daniel, Allegan Tele-Ception Inc., 114 Locust St., Allegan, Mi. 49010
- W. Dean Davis, El Dorado Springs Cable TV, Inc., 105 East Spring St., El Dorado Springs, Mo. 64744
- Harry G. Dawson, Jacksonville Cable T.V. Co., Lincoln Square, Jacksonville, Il. 62650
- D. R. Deveraux, LVO Cable, 715 S. Oakcrest, Casper, Wy. 82601
- G. Alfred Dodds, Applied Video Electronics, Inc. 4936 Caroline Drive, Cleveland, Oh. 44128
- Earl W. Drake, Arrow Electronics & Construction Co., 1610 West Main St., Kalamazoo, Mi. 49007
- Leslie E. Eakins, Tower Communications Inc., 811 South 3rd St., Ironton, Oh. 45638
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- Leo A. Engleman, Television Transmission Co., 301 Peru St., Peru, Il. 61354
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- Jake G. Frickel, Lincoln Tel. & Tel. Co., 1440 M St., Lincoln, Ne. 68501
- Douglas B. Fuller, St. Joseph Cablevision, 716 Francis St., St. Joseph, Mo. 64501
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- Dexter A. Hawkins, Jr., GT & E Communications Inc., Public Square, Angola, In. 46703
- Harold Hay, Telesystems Corp., 22 E. 3rd St., Peru, In. 46970
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- Jay K. Hubbell, Anaconda Electronics, Box 245, Wilmington, Il. 60481
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- William J. Lichtenberg, Mid American Cable Systems, Inc., 226 S. Kansas Ave., Olathe, Ks. 66061
- Edward G. Mattox, American Television & Communications Corp., 716 South 33rd St., Parsons, Ks. 67357
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- Thomas R. Ridley, Arrow Electronics, 303 North Ohio St., Fremont, Oh. 43420
- Stanley D. Rischman, Jerrold Electronics Corp., 9201 Moody Park Dr., Overland Park, Ks. 66212
- Clarence E. Ross, Midway Cable TV, 1413 Minnesota Ave., Kansas City, Ks. 66102
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- Leroy E. Savage, Automatic Electric Co., P.O. Box 42, Northlake, Il. 60164
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- Stephen H. Swarny, Tower Communications, Inc., 617 Tuscarawas Ave. N.W., New Philadelphia, Oh. 44663
- Nichole A. Tarraferro, Nick's TV & Appliance, 837 Peach St., Lincoln, Ne. 68502
- Bill R. Thomison, Spencer-Kennedy Lab., Inc., 120 Hackberry, Independence, Ks. 67301
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- Joseph D. Dugas, TelePrompter Cable TV, P.O. Box 1268, Brandon, Fl. 33511
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- Harold D. Edwards, Jr., Georgia Cablevision Corp., 1601 W. Peachtree, Atlanta, Ga. 30309
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- Donald H. Fissel, Suburban Cablevision, 163 E. Davis St., Culpeper, Va. 22701
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- Robert O. Frier, Highlands Cable TV, P.O. Box 229, Sebring, Fl. 33870
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Michel Rouleau, Transvision Cookshire Inc., C.P. 145, Cookshire

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Jacques Savoie, Cablevision Victoriaville, 298 rue Notre Dame East, Victoriaville

David A. Shefler, Vikoa of Canada, 8340 Mayrand, Montreal

John Steele, Laurentian Cablevision, 425 Blvd. St. Joseph, Hull

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Florian Thibault, Centre Electronic Thibault, 1646 St. Marc, Shawinigan

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- Bryan Boyko, Jerrold Electronics, 60 Wingold Ave., Toronto
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- Robert A. Elliot, Western Cable TV, 16 Graham St., Woodstock
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- John R. Pfeiffer, Grand River Cable TV, 48 Preston St., Kitchener
- Gordon E. Pigden, Hastings Cable Vision Ltd., P.O. Box 223, Madoc
- Peter Pillwein, Guelph Cable, 86 Scottsdale Drive, Priory Park, Guelph
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- Frank Verkaik, Rogers Cable TV Ltd., 51 Beverly Hills Drive, Downsview
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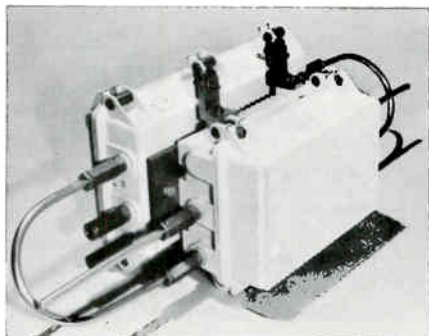
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# NEW PRODUCTS

## REVERSE AMPLIFIER KIT



Theta-Com CATV (P.O. Box 9728, Phoenix, Ariz. 85020) has developed a reverse amplifier for converting existing one-way single cable systems to two way. The Reverse Conversion Kit consists of a single housing containing a 5-30 mHz reverse amplifier and necessary filters for facilitating reverse operation. The Reverse Conversion Kit features on-site mechanical installation to trunk amplifiers. It will be in full production in late May, the company claims.

• • •

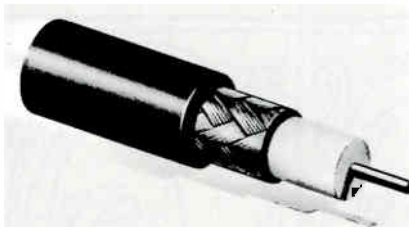
## CONVERTER WITH AFC



The CATV Division of Oak Electro/Netics Corp. (Crystal Lake, IL 60014) has announced a set-top converter with automatic frequency control. The new AFC feature will ensure frequency stability and reduce the possibility of the subscriber incorrectly tuning either the converter or the television set when normal frequency drift occurs. Deliveries begin in the summer, we are told. Some technical characteristics are: input and output impedance are 75 ohms, input and output VFWR are 2:1 maximum, typical

noise figure is 11 db, and cross mod is not visible on any channels over the specified operating range.

## DROP CABLE



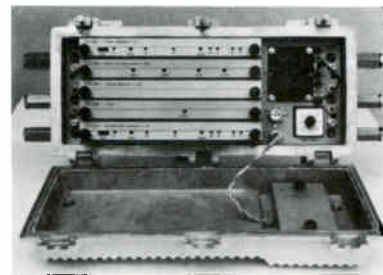
A new series of 97% braid shielded CATV drop cables has been announced by Cerro Wire & Cable of Freehold, N.J. Available in RG-59, RG-6, and RG-11 sizes, the new drop cables are made with tightly woven copper clad aluminum braid shields and copper clad steel center conductors for mechanical strength. They are available with either solid or foam polyethylene dielectrics, vinyl (PVC) or polyethylene jackets, with or without integral steel messengers, single and dual construction. Attenuation losses are from 2.3 db 100' @ Channel 13 for the foam RG-11 to 5.2 db/100' for solid RG-59.

• • •

## Classified

### WANTED SENIOR CATV TECHNICIAN

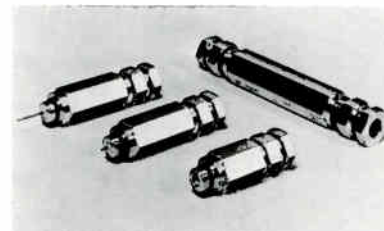
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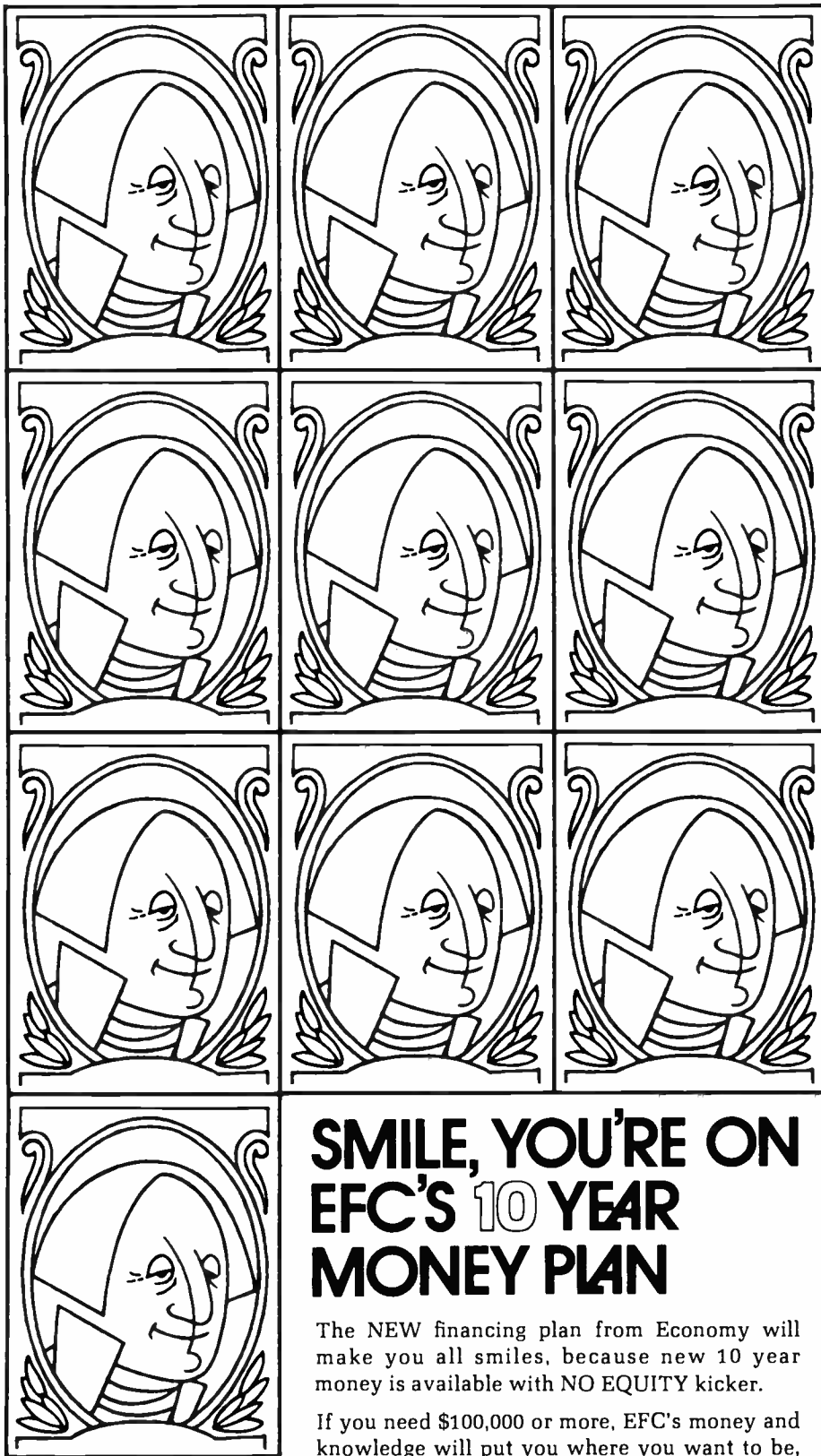
TOCOM, Inc. (P.O. Box 47066, Dallas, Tex. 75207) is offering its model 2000 amplifier series with push-pull trunk amplification with AGC; push-pull distribution amplification with one, two, three or four outputs; midspan bridger or terminal bridger with one, two, three or four outputs; status monitoring and bi-directional capability. The units are also available for either the "super trunk" concept or conventional system design. An external temperature probe senses atmospheric changes and compensates for cable attenuation changes due to temperature. Various thermal values are available. Other features include 30 or 60 volt tapped transformer, plug-in automatic reset circuit breakers on distribution ports, plug-in pad for cable spacing compensation, plug-in splitters and center-conductor seizing post integrated with test points to facilitate monitoring of all ports.

• • •

## COAX CONNECTORS



The Magnavox Co. CATV Division (133 W. Seneca St., Manlius, N.Y. 13104) announces its expanded line of high rfi integrity coaxial connectors, the 990 series. Now available for foam dielectric aluminum sheathed coax as well as standard cable in .412, .500 and .750 sizes, each family of models includes a splice and feed-thru and a short or long pin for chassis types. The connectors are constructed with extra-long sheath



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### SOUND EFFECTS



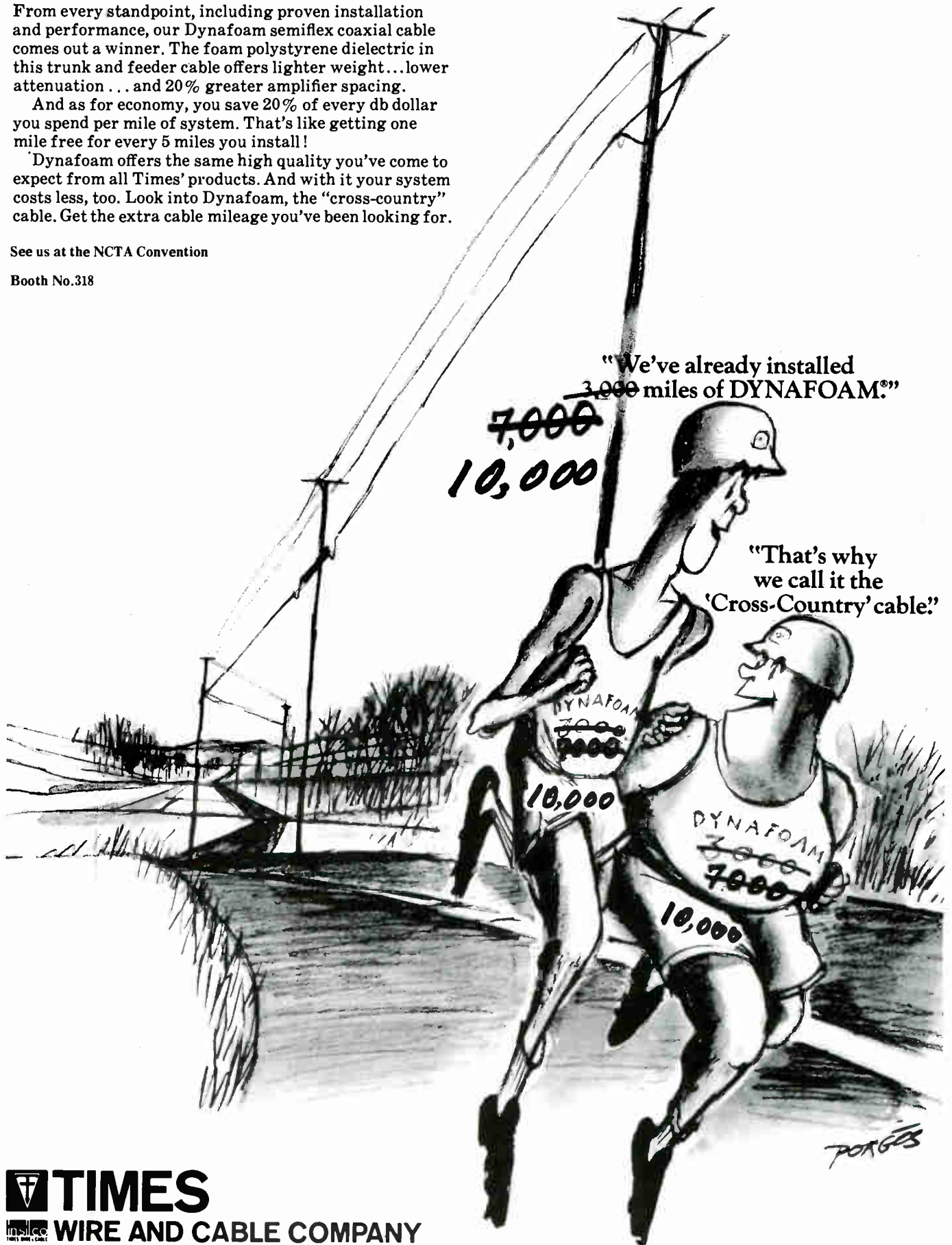
From every standpoint, including proven installation and performance, our Dynafoam semiflex coaxial cable comes out a winner. The foam polystyrene dielectric in this trunk and feeder cable offers lighter weight... lower attenuation... and 20% greater amplifier spacing.

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