

Thermistor Applicator

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 A S its name implies, the thermist-
or is a thermally-sensitive resistor. It is also a non-linear resist or. Although it is a 2 -terminal semi- conductor device, the thermistor is not a rectifier. It accordingly may be employed in either a-c or d-c circuits. Thermistors are manufactured
in a number of shapes, principally
beads, discs, and rods, and in varbeads, discs, and rods, and in various sizes including subminiature.

The basic property of the ther-

mistor is its change of resistance

with temperature. The temperature

change affecting it may arise exter-

nally or it may result from current

flowing through the thermistor. This property gives rise to the nonlinearity of the thermistor resistance characteristic.

Thermistor action may be employed in several ways to modify the behavior of electrical circuits. Many ap-
plications are rendered especially attractive by the simplicity of the thermistor and its compactness. A number of typical applications are described in this article.

Typical Characteristics

Figure 1 displays the non-ohmic $\frac{\text{from }-60 \text{ to } +150 \text{ degrees C}}{\text{variation of resistance}}$ variation of resistance with tempera-
tigure 2 shows the static E ture. From this curve, the resistance

Figures 1, 2, and 3 illustrate typicarease over a range of approximately cal thermistor characteristics. 2000 to 1 for a temperature increase of this particular unit is seen to de-

crease over a range of approximately
 $\frac{1}{2000}$ to 1 for a temperature increase
 $\frac{1}{2000}$ to 1 for a temperature increase
 $\frac{1}{2000}$ for $\frac{1}{200}$ for $\frac{1}{200}$ for $\$ from -60 to $+150$ degrees C.

 $\sqrt{\frac{1}{2}}$ $\sqrt{\frac{1}{2}}$ $\sqrt{\frac{1}{2}}$ ant first increases rapidly from zero plot reveals that as the current
through the thermistor is increased, the voltage drop across this componto a peak (T_0) and then decreases with further increase in current, finally falling to point $T₇$. Thus, the thermistor shows positive resistance from zero to T., but negative resist-
ance from T. to T_7 . Points T_1 to $T₇$ on the curve represent temperature levels at those points resulting from internal heating in the thermist-
or due to current flow.
Thermal lag prevents the thermist-

or temperature from increasing in-
stantaneously with initiation of current. A significant time interval thus elapses after application of voltage before the current through the thermistor reaches the magnitude expected from an examination of the voltage-vs-resistance charac-
teristic. Figure 3 illustrates this Figure 3 illustrates this time delay characteristic.

The slopes of the curves shown in Figures 1, 2, and 3 and the values of their coordinates will vary with thermistors of different types. However, the over-all configurations will remain substantially the same.

Figure 2 shows the static EI char- of the characteristics illustrated by teristic of the thermistor. This Figures 1, 2, and 3. These applica-Each of the wide range of ther-Figures 1, 2, and 3. These applica-

tions may be grouped further according to whether the thermistor is ining to whether the thermistor is in-
ternally or externally heated (that
 T externally heated (that
 T externally heated (that
 T externally heated (that
 T externally heated in T external that is, whether by current flow or am-
bient temperature). The temperature dependence of the thermistor persuare sensitivity. resistance has been utilized for the stabilization of circuit resistances in an environment of fluctuating teman environment of nuctuating tem-
perature. Thus, thermistors have negative measurement been employed to compensate indicating meters, fixed resistors, and bal-
ancing circuits; and, in the d-c bias net -works of transistor circuits, to stabilize operating points.

Illustrative Circuits

thermistor circuits. These have been will be required to indicate amperes selected to illustrate the wide range as well as milliamperes.

of applications possible with ther-

 \langle (\langle) \rangle

Temperature Measurement. The thermistor is applicable as a temperature sensing element of good
sensitivity. In this connection, a small thermistor may be mounted in perature measurement.

Figures 4 to 15 show representative with temperature, meter M probably In Figure $4(A)$, the thermistor (T) is connected in series with a d-c source, adjustable current-limiting resistor (R) , and a direct current graduated directly in degree
meter (M) . Reference to Figure 1 basis of such a calibration. shows that, since the thermistor undergoes a large resistance change Figure 4(C) shows one type of with temperature, meter M probably bridge circuit for checking tempera-
will be required to indicate amperes ture by measuring thermistor resist-
as well as m

The meter may be set to zero, or
to some other desired initial reading, by adjustment of R. As the temperature to which the thermistor is exposed rises, the meter deflection will increase. The deflection may be referred to a current-vs-temperature chart, or the meter scale may be graduated directly in degrees.

the nose of an exploring probe. Fig-
ohmmeter is employed to indicate In Figure $4(B)$, a conventional d-c the thermistor resistance as it
changes with temperature. The changes with temperature. meter deflection may be referred to a resistance -vs -temperature calibration or the instrument scale may be graduated directly in degrees on the

> bridge circuit for checking temperature by measuring thermistor resist-

When the switch is closed, load device RL_1 can operate almost instantaneously. The other load devices will be operated at later intervals, the time of each depending upon its resistance, since each is in series nected across the amplifier input ter-
with a thermistor which introduces minals where it forms a potentiometwith a thermistor which introduces minals where it form a time delay. By choice of appro- er with resistor \mathbf{R}_{1} . a time delay. By choice of appro- er with resistor R_s.
priate values of load resistances (or of the resist-
of individual external series resist-
thermistor is heated by this increased ances when each load device has voltage across its heater, and its re-
the same resistance) the devices may sistance decreases. By notentiomet. be caused to operate in a desired se- er action with R_n , the thermistor quence after the switch has been resistance then lowers the signal inclosed.

employing series thermistors.

In this circuit, when any switch is closed, that leg of the circuit draws current through a thermistor. By *Limiter*. The simple limiter or properly proportioning the series re- compressor circuit in Figure 13 sistor (R₁ Thyratron action, and to conduct as long as its switch is closed. When one leg is conducting, the current Because current through the ther-
draw through the common series re-
mistor increases rapidly while the sistor, R., sets up a voltage drop applied voltage is increasing slowly, across R. sufficient to reduce the line voltage too low for any other ther-
mistor to fire.
mistor to fire.

The result of this action is that when one leg of the circuit is in operation, all other legs are locked out. The latter will not operate when their switches are closed. Only when the switch in the conducting leg is the a particular type of the initial
opened will the circuit be restored will yield efficient limiting action
to the initial condition in which any minus the high distortion encountto the initial condition in which any other Leg may conduct.

Amplifier Feedback. The thermist-
or in Figure 12 is of the heater Expander. The opposite action is type (also called "directly -heated").

This thermistor has an internal heater element which is connected across the output terminals of the amplifier. The thermally-sensitive resistance element of the thermistor is connected across the amplifier input ter-

Lockout Switching System. Figure output. The amplifier output thus is
11 shows another switching system stabilized at a predetermined level When te signal output rises, the thermistor is thermistor increased voltage across its respective action with R_s , the thermistor put voltage, and in turn the amplifier
output. The amplifier output thus is state and largely by the ratio of R. adjustable by means of R..

> The simple limiter or compressor circuit in Figure 13 utilizes thermistor non-linearity in A small line ease in applied voltage
wory much the same manner as the (signal input) causes a large curvery much the same manner as the to obtain limiting action.

> mistor increases rapidly while the amplification is taking place. Ampliapplied voltage is increasing slowly, $\frac{1}{10}$ fication does not occur because the resulting voltage drop across the $\frac{1}{2}$ applitude of the input signal is not nal output voltage in this instance) is maintained constant while the amplitude of the signal input voltage fluctuates.

> Choice of resistances R_1 and R_2 for a particular type of thermistor will yield efficient limiting action minus the high distortion encount-
ered with simple limiters of some tance of the thermistor enables these other types.

obtained with the circuit shown in $\frac{power}{waves}$.

Figure 14. Here, the output signal is the voltage drop due to the flow of non-linear thermistor current through a series resistance (RL). A small increase in applied voltage rent to flow through RL, producing a large increase in signal output. We italicize the word "increase" here to prevent giving the impression that amplitude of the input signal is not increased by the circuit action, only its rate of change. In fact, the absolute amplitude is decreased by potentiometer action between R_1 , T , and RL.

U -H -F, Microwave Wattmeter. The thermistor bridge shown in Figure 15 is invaluable for measuring $a-c$ tance of the thermistor enables these measurements to be made anywhere in the frequency spectrum from low, power-line frequencies to micro-

The signal energy is applied to the thermistor only, through the isolating
capacitor, C. The radio-frequency capacitor, C. The radio-frequency
choke, RFC, prevents passage of this energy through the other arms of the
bridge. The signal current heats the thermistor and thus changes its re- sistance proportionately.

The thermistor resistance may be checked by adjustment of the bridge to null, whereupon $R = (R_1 R_2)/R_3$,
and this resistance value referred to
a resistance-vs-power calibration a resistance-vs-power curve to determine the signal watts. Or the scale of the indicating meter may be graduated directly in watts.

It is customary to employ a d-c
bridge supply, E, when measuring a-c
watts. When checking d-c watts with a thermistor bridge, capacitor C is omitted from the circuit and an a -c bridge supply and a-c meter may be employed.

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closure of the switch. The length of the time interval may be selected by adjustment of R.

Voltage Regulator. Within its power handling limitations, the thermistor may be employed as a voltage $Vacuum\ Gauge$. In Figure 8, there regulator, especially at low voltages, mistors T_a and T_b form two of the in the simple circuit of Figure 7, to stabilize an output voltage against input voltage variations.

 R_1 is a current-limiting resistor outsis
similar to the same resistor in a gas- Be-
eous-tube regulator circuit. The val- bridg ue of R_2 must be chosen, with respect to the EI characteristic of the the evacuation then progresses, ther-
type of thermistor in use, for max- mistor T., can dissipate its heat due type of thermistor in use, for maximum regulating effect.

The voltage regulating action results from the fact that current surthrough a thermistor, and therefore $air.$ Co the resultant voltage drop across it, increases at a rate somewhat great-
increases at a rate somewhat great-
of the bridge unbalances, and the meter
er than linearly with applied volt-
deflects. The meter scale may be ca age (voltage drop across the thermist-

or) thus results from a rather large change in input (applied) voltage.

A particular desirable feature of just described.
is circuit is that it may be used Here again, there is a 4-arm bridge this circuit is that it may be used to regulate either ac or dc.

Vacuum Gauge. In Figure 8, ther-
mistors T_1 and T_2 form two of the (T_1) is a arms of a Wheatstone bridge. Thermistor T_1 is placed inside the vac-
uum chamber, while T_2 is mounted the fluid outside.

the evacuation then progresses, therto current flow faster than can T_1 inside the chamber because T_1 is $\frac{unp_i}{whip_j}$ surrounded by progressively thinner $\frac{w_{\text{HIC}}}{w_{\text{HIS}}}$ air. Consequently, the resistance of the hotter T_1 differs from that of T_2 , deflects. The meter scale may be cal-

Sequence-Switching Circuit. In Fig-

Flow Meter. Figure 9 shows a flow

meter operating on somewhat the same principle as the vacuum gauge just described.

Before evacuating the chamber, the quiet, by adjustment of R_{0} . As the bridge is balanced (meter M nulled) by adjustment of resistor R_{0} . As beat due to current flow rapidly bewith thermistors in two of its arms. In this instance, one thermistor (T_1) is mounted so as to be directly (T_1) is mounted so as to be directly
in the flow of a fluid (liquid or gas), while thermistor T_2 is mounted in the fluid but outside of the flow. The bridge is balanced with the fluid quiet, by adjustment of R.,. As the cause of the surrounding flow. But T., becomes hot because of its quieter ambient. Consequently, the bridge unbalances, deflecting the meter which may be calibrated to read flow units.

> A similar thermistor circuit has been used as an anemometer.

ibrated to read chamber pressure. ure 10, several load devices, represented by RL_1 to RL_n , are connected across a line supplied by source E and controlled by switch S. All except R_{L₁} are connected in series with thermistors $(T_1$ to T_n).

mistor (T) forms one arm of the bridge, while the other three arms are conventional resistors. One resistance arm, R_2 , is made variable for nulling meter M or setting it to $\begin{vmatrix} \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot \end{vmatrix}$ some predetermined level at ambient temperature or zero degrees. As the | O thermistor resistance alters in re-
sponse to temperature, the bridge un-
balances and the meter is deflected. The bridge may be re-balanced and the thermistor resistance measured in terms of the bridge arms (that is: $R = (R_1 R_2)/R_3$. Or the meter scale may be graduated directly in degrees.

Temperature Control. In addition
to temperature measurement. a number of thermistor circuits are avail-
able for direct temperature control. Figure 5 shows a simple arrangement
utilizing the temperature-sensitive resistance of a thermistor in series with the coil of a control relay.

Rising temperature lowers the thermistor resistance, allowing the latter to pass more current to the relay which eventually is actuated. The supply voltage may be either ac or de, provided the relay is chosen ac- cordingly.

For greater sensitivity to small changes in temperature, a sensitive dicating meter in the bridge circuit in Figure $4(C)$.

REGULATED Time Delay. The thermistor delay
OUTPUT characteristic illustrated by Figure Time Delay. The thermistor delay 3 may be utilized to obtain time delay effects in a simple manner.

> In Figure 6, for example, a ther- mistor is connected in series with an a-c or d-c source and a corresponding relay coil. Resistor R limits current and accordingly modifies the current-time curve of the thermistor. When switch S is closed, the relay current gradually increases, according to the current-time curve of the thermistor-resistor combination. The current reaches a level sufficient to actuate the relay some time after

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