MWDX-6 Phasing Unit
Mark Connelly - WAIION - 12 SEP 1994

## Introduction

The MWDX-6 provides antenna phasing with improved signal-to-noise ratios at low-signal rural locations. Two BUF-A buffer amplifiers are used: one on each antenna input line. Active capacitivelycoupled (AC) and active inductively-coupled (AL) functions provide high gain and good coupling with a wide variety of input loads / antenna lengths. The passive capacitively-coupled (PC) function allows the MWDX-6 to be used at urban sites where amplification is not desirable. The unit also offers a bypass (BP) function which routes the antenna input around the tuned circuits. This is advantageous for rapid bandscanning / parallel-frequency checking, also the BP function is used when the output from a loop antenna supplies signal. The antenna coupling function is independently selectable for each of the two antennas. Usually the same function would be chosen for both lines; exceptions to this rule would be in loop-versus-wire or longwire-versus-shortwire phasing applications.

Future buffer card designs may be swapped into the unit later without changing other features. If amplifiers with substantially - better noise figures or superior intermodulation-distortion (IMD) specifications become available, such a swap would be desirable. As it stands, the current MWDX-6, with two BUF-A's, performs well. Two of the low-IMD whip amplifiers currently under design and evaluation by Dallas Lankford may suit this application.

Noise-reducing antenna considerations have been accommodated by the inclusion of two isolation transformers ( $\mathrm{T} 1, \mathrm{~T} 2$ ) on the inputs. When suitable "quiet" grounds or counterpoise wires are part of the antenna layout, one or both transformers can be switched in to reduce local electrical noise. The noisereduction (NR) input mode may be used for low-noise balanced antenna inputs as well. Remote-site noise-reducing matching-transformer / pad outputs can be connected via coaxial cable to J1/ / 3 or J2/ / 4 . If Input mode switches S1 and S2 are set to the Noise-Reduction (NR) mode, the phasing unit may be interfaced correctly with coaxial inputs from low noise antenna systems consisting of a wire antenna and a "field site" earth ground fed to the primary of a (field site) step-down transformer in the 4:1 to 12:1 range; either a Mini-Circuits T9-1-X65 or Nick Hall-Patch's home-brew version consisting of an Amidon FT5043 core with 35 turns primary / 11 turns secondary will work well. The lower impedance output of this field-site transformer is paralleled with 270 to 330 ohms; one secondary lead goes to the shield of the coaxial cable going to the operator's "shack" and the other secondary lead goes to the center conductor of this coaxial cable through a small series resistor in the 5 to 12 ohm range. The resistors form a low-loss matching pad to reduce the degree of mismatch. Excessive mismatch can compromise the shielding effectiveness of the coaxial cable. One such low-noise set-up can be phased against a loop or, even better, against a second low-noise antenna system with different directional properties. In any event, the "shack end" of a Line I low-noise coaxial feed is connected to JI (center) and J3 (shield) of the phasing unit; similarly, if such a coaxial feedline is to be used for Line 2, it should be connected to J2 (center) and J4 (shield).

For further discussion of noise-reduction schemes, the reader is advised to consult my articles "Another Look at Noise-Reducing Antenna Systems" (6 JUL 1992), "Bevmatcher" (15 JAN 1991), and "Antenna Experiments - Summer 1994"; also, check the Nick Hall-Patch / John Bryant article "Impedance Matching a Beverage Antenna to a Receiver" in Proceedings 1988, and the 1991 noise-reducing invertedL articles by Dallas Lankford and Denzil Wraight. The reader should be advised that the noise being reduced is LOCAL electrical noise of the type caused by TV sweep oscillator harmonics, light dimmer buzz, and the like. These antenna systems cannot, singly, reduce static from lightning bolts. Such noise CAN be nulled by phasing two antennas if it is coming from far enough away as to approximate a point source not having great incoming-angle variation over time (it is then treated as a "dominant signal" as if it were a broadcast station interfering with desired DX).

The MWDX-6 (unlike Super-MWDX-5) separates the noise-reduction / normal input mode selections from the coupling-function settings. This allows more versatile tuning of noise-reduced antennas.

Because butter amplifiers are used, there is no need for the series-tuned input configuration requiring the tuning capacitors to be isolated from chassis ground. The longer wires for which seriestuning worked best will tune quite efficiently in the active inductively-coupled (AL) function.

As with previous phasing units, nulls can be obtained which are difficult or impossible to obtain with a loop. Nulls created by phasing are often single-direction nulls; the directional pattern created thereby can approximate the cardioid or end-fire patterns most useful for international medium-wave DXing from the Atlantic and Pacific coastal areas of the USA and Canada. There are a few circumstances when a loop will do better. So it's advisable to have both a loop and a phased-wires (or loop-versus-wire) system available for optimum DXing results.

Wire antennas used should be at least $20 \mathrm{~m} / 66 \mathrm{ft}$. long. If two wires are used, there should be an MINIMUM angle of 45 degrees (horizontal and/or vertical) between them for best results. An exception to this rule can be made for Beverage-length (over $250 \mathrm{~m} / 820 \mathrm{ft}$.) wires, especially if of different length or if one is terminated and the other is "floating". Good nulls were obtainable by phasing two parallel Beverages during the October 1993 Newfoundland DXpedition.

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| Input / Output Connectors |  |  |  |
| :---: | :---: | :---: | :---: |
|  | =e=ewemer |  | memeremeremexem |
| left side | J1 | Line I wire input | banana jack |
| left side | 12 | Line 2 wire input | banana jack |
| left side | J3 | earth ground input 1 | banana jack |
| left side | J4 | earth ground input 2 | banana jack |
| left side | J5 | chassis ground | banana jack |
| right side | J6 | RF output | BNC jack |
| right side | J7 | $B+$ in | phono jack |

Table 2: S5 Bandswitch Settings Chart
Ranges are usually a bit greater than those shown. These ballpark values are for $50-\mathrm{m} . / 164-\mathrm{ft}$. wires. Wire length and coupling mode affect the ranges somewhat. Occasionally a lower or higher SS range setting will produce better tuning and nulling. A sharp, well-defined peak near the center of a giv tuning capacitor's adjustment range will yield better results than a lower- Q (less sharp) peak near the clockwise or counterclockwise (anticlockwise) end of the capacitor's mechanical adjustment range.

The MWDX-6 family of phasing units has frequency coverage characteristics as noted in the following table:
MODEL: standard MWDX-6 (LWBC: 130-285; MW: 430-1800)

| S5 | S5 Knob | Freq. | Max. Freq. | "Main" L ["Tap" L] <br> Tank Inductor Values |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pos. | "o'clock" | $\mathrm{kHz}$ | kHz | L\# | uH | Mouser Part \# |
| = | ==:= |  |  |  |  |  |
| 1 | 9:30 | 130 | 180 | LI,L13 | 4700 | 434-1120-473K |
| [* | - | - | - | L7,L19 | 1000 | 43LR103 |
| 2 | 10:30 | 180 | 285 | L2,L14 | 2200 | 434-1120-223K |
| [* | - | - | - | L8,L20 | 470 | 43LR474 |
| 3 | 11:30 | 430 | 630 | L3,L15 | 470 | 43LR474 |
| [* | $\because$ | - | - | L9,L2I | 100 | 43LR104 J |
| 4 | 12:30 | 630 | 880 | L4,L16 | 220 | 43LR224 |
| [* | . | - | - | L10,L22 | 47 | 43LR475 |
| 5 | 1:30 | 880 | 1260 | L5,117 | 100 | 43LRI04 |
| [* | - | . | - | L11,L23 | 22 | 43LR225 J |
| 6 | 2:30 | 1260 | 1800 | L6,L18 | 47 | 43LR475 |
| [* | $\cdots$ | - | - | L12,L24 | 10 | 43LR105 |
| MOD | MWDX-6A | \& MW: | 5-2700) |  |  |  |
| S5 | SS Knob | Min. | Max. | "Main" | L ["Tap |  |
| Pos. | Pointer | Freq. | Freq. | Tank I | ductor V |  |
| \# | "o'clock* | kHz | kHz | L\# | uH | Mouser Part \# |
| $=$ | = =:= | = $=$ | =e= | = $=1$ | 300 |  |
| 1 | 9:30 | 145 | 230 | L1,L13 | 3900 | 434-1120-393K |
| [* | 9,30 | . | . | L7,L19 | 820 | 43LR824 ] |
| 2 | 10:30 | 230 | 375 | L2,L14 | 1500 | 434-1120-153K |
| [* | 10.30 | - | . | L8,L20 | 330 | 43LR334 1 |
| 3 | 11:30 | 375 | 620 | L3,L15 | 560 | 43LR564 |
| [" | . | - |  | L9,L21 | 120 | 43LR124 |
| 4 | 12:30 | 620 | 1050 | 14,L16 | 220 | 43LR224 |
| [* | 12.30 | 62 | . | L10,L22 | 47 | 43LR475 |
| 5 | 1:30 | 1050 | 1600 | L5,L17 | 82 | 43LR825 |
| $1 \cdot$ | - | - | - | L11,L23 | 18 | 43LR185 |
| 6 | 2:30 | 1600 | 2700 | L6,L18 | 33 | 43LR335 |
| ${ }^{-}$ | 2.30 | 1600 |  | L12,L24 | 6.8 | 43LR686 |

$\begin{array}{lll}\text { MODEL: } & \text { MWDX-6B (extended LW: } \\ \text { S5 } & \text { 90-880) } \\ \text { SS Knob } & \text { Min. } & \text { Max. }\end{array}$

| S5 <br> Pos. <br> $\stackrel{\#}{=}$ | S5 Knob Pointer "o'clock" | Min. <br> Freq. <br> kHz | Max. <br> Freq. <br> kHz | "Main" L ["Tap" L] <br> Tank Inductor Values |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | LItant | uH | Mouser Part \# |
|  | = $=$ = |  |  | =axer | = | =134-1120-104K |
| 1 | 9:30 | 90 | 130 | L1,L13 | 10000 | 434-1120-104K |
| [" | $\because$ | - | - | L7,L19 | 2200 | 434-[1120-223K] |
| 2 | 10:30 | 130 | 180 | L2,L14 | 4700 | 434-1120-473K |
| [* | - | - | - | L8,L20 | 1000 | 43LR103 ] |
| 3 | 11:30 | 180 | 285 | L3,L15 | 2200 | 434-1120-223K |
| [* | I | . | - | L9,L21 | 470 | 43LR474 1 |
| 4 | 12:30 | 285 | 430 | L4,L16 | 1000 | 43LR103 |
| [* | - | - | - | L10,L22 | 220 | 43LR224 |
| 5 | 1:30 | 430 | 630 | LS,L17 | 470 | 43LR474 |
| [" | , | - | - | L11,L23 | 100 | 43LR104 |
|  | 2:30 | 630 | 880 | L6,L18 | 220 | 43LR224 |
| [* | , | - | - | L12,L24 | 47 | 43LR475 |


| MODEL: MWDX-6C (MW, tropical: 375-6500) - ${ }^{\text {a }}$ ( ${ }^{\text {a }}$ ( L |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { SS } \\ & \text { Pos. } \end{aligned}$ | SS Knob | Min. | Max. | "Main" L ["Tap |  |  |  |
|  | Pointer | Freq. | Freq. | Tank In | uctor Va |  |  |
| \# | "o'clock* | kHz | kHz | L" | uH | Mouser Par |  |
| $=$ | = =:= |  |  |  |  | 43LP564 |  |
| 1 | 9:30 | 375 | 620 | L1,113 | 560 | 43LRS64 | ] |
| [" | - | - | - | L7,L19 | 120 | 43LR124 | ] |
| 2 | 10:30 | 620 | 1050 | L2,L14 | 220 | 43LR224 |  |
| [* | - | - | - | L8,L20 | 47 | 43LR475 | 1 |
| 3 | 11:30 | 1050 | 1600 | L3,L15 | 82 | 43LR825 |  |
| [" | . | - | - | L9,L21 | 18 | 43LRI85 | 1 |
| 4 | 12:30 | 1600 | 2700 | 14,L16 | 33 | 43LR335 |  |
| [* | . | - | - | L10,L22 | 6.8 | 43LR686 | 1 |
| 5 | 1:30 | 2700 | 4000 | LS,L17 | 12 | 43LR125 |  |
| [* | - |  | - | L11,L23 | 2.7 | 43LR276 | ] |
| 6 | 2:30 | 4000 | 6500 | L6,L18 | 4.7 | 43LR476 |  |
| [* | . | - | - | L12,L24 | 1 | 43LR106 | ] |

MODEL: MWDX-6D (extended tropical, SWBC: 1260-12500)

| S5 | S5 Knob | Min. | Max. | "Main" | ["Tap |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pos. | Pointer | Freq. | Freq. | Tank 1 | uctor V |  |  |
| \# | *o'clock* | kHz | kHz | L\# | uH | Mouser Part |  |
| $=$ | = =:= | = | = $=$ =0 | =exa= |  |  |  |
| 1 | 9:30 | 1260 | 1800 | L1,L13 | 47 | 43LR475 |  |
| [* | - | - | - | L7,L19 | 10 | 43LR105 | 1 |
| 2 | 10:30 | 1800 | 2800 | L2,L14 | 22 | 43LR225 |  |
| [" | - | - | - | L8,L20 | 4.7 | 43LR476 | 1 |
| 3 | 11:30 | 2800 | 4000 | L3,L15 | 10 | 43LR105 |  |
| [* | - | . | - | L9,L21 | 2.2 | 43LR226 | 1 |
| 4 | 12:30 | 4000 | 6500 | L4,L16 | 4.7 | $43 \mathrm{LR476}$ |  |
| [* |  | - | - | L10,L22 | 1 | 43LR106 | ] |
| 5 | 1:30 | 6500 | 8800 | L5,L17 | 2.2 | 43LR226 |  |
| [* | 1:30 | - | . | L11,L23 | 0.47 | 43LR477 | ] |
|  | 2:30 | 8800 | 12500 | L6,L18 | 1 | 43LR106 |  |
| $1{ }^{1}$ | 2.30 |  | , | L12,L24 | 0.22 | 43LR227 | 1 |

## MODEL: MWDX-6E (reduced coupling efficiency) ( $90-8800$ )

Note: For this configuration, S5 is a 2-pole, 12 -position switch. The inductors on the S5A section (LI through LI2) are joined at "IN-1B" of Figure 4 and a 68 ohm resistor is connected to ground from this point (instead of the old S5C section). The inductors on the S5B section (L13 through L24) are joined at "IN-2B" of Figure 4 and a 68 ohm resistor is connected to ground instead of the old S5D section.


## Operating the MWDX-6

Figures 1 through 5 are the schematics of the MWDX-6. Please refer to them during the discussion of phasing procedure. See Tables 2 and 6 for physical positioning of switches.

Nulling procedures sound complicated at first, but are quickly executed once learned. The user should practice during non-skip daylight conditions on "graveyard" and regional channels having discernible subdominants to get familiar with operation of the controls before attempting night-time nulls of unsteady signals. As with a loop, solid nulls of skip stations closer than 500 miles $/ 800 \mathrm{~km}$, especially above I MHz , are difficult because of the rapid changes in vertical (and sometimes horizontal) arrival angles inherent in high-angle skip. Such nulls are better when using phased Beverages than when using a loop, loop versus loop, loop versus wire, or phased shorter wires.

### 1.0 MWDX-6 Two Wire Phasing Procedure

1.1 ** INITIALIZE CONNECTIONS AND CONTROLS **

JI: connect Antenna \#1 wire.
J2: connect Antenna ${ }^{12}$ wire.
33: if a noise reducing ground for Antenna \#1 is available, connect it; otherwise, no connection is needed.

J4: if a noise reducing ground for Antenna \#2 is available, connect it; otherwise, no connection is needed.

15: this may be connected to mains, earth, or vehicle ground if doing so improves signal-to-noise ratio. This would be done more often with portable receivers than with tabletop communications models having a metal case.

J6: connect, via coaxial cable, to the receiver input, or to the input of a tunable preselector between the phasing unit output and the receiver input.

J7: connect this to a DC power source of +11 VDC minimum, +25 VDC maximum. If you don't intend to use the active (AC or AL) functions, DC power will not be necessary.

SI: set to NORM unless using a noise-reduced input pair at J1 and J3 for Antenna \#1 (in that case, set SI to NR).

S2: set to NORM unless using a noise-reduced input pair at J2 and J4 for Antenna \#2 (in that case, set S2 to NR).

S3: set to Active Capacitively-Coupled (AC) (or to a different position, depending on experimentation that leads to having determined the best position for a given Antenna \#1, consistent with maximum usable signal with no spurious responses).

S4: set to Active Capacitively-Coupled (AC) (or to a different position giving best results for Antenna \#2).

S5: set for the correct frequency range, according to Table 2.
RI: set to fully counterclockwise (minimum attenuation).
R2: set to fully counterclockwise (minimum attenuation)
R3: set to center of mechanical adjustment range.
1.2 ** PEAK LINE 1 **

Set S 6 to (Line) I. Tune Line I by peaking desired-frequency signal strength with CI . At this time, leave Cl at its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe S-meter, if available, or note audible level).
[At this time, other positions of Line I Function switch S3 may be tried to see if greater signal transfer is possible. Re-adjustment of CI , and possibly SS , may be needed to re-establish a peaked condition. In any event, the peak should have reasonable Q (be well defined) and Cl should not be set too close to fully CW or fully CCW. If objectionable spurious responses are noted, adjust RI in a clockwise direction until the spurs are not noted with Cl peaked properly OR set S 3 to Passive Capacitively-Coupled (PC) function and re-peak Cl .]

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1.3 ** PEAK LINE 2 **

Set S6 to (Line) 2. Tune Line 2 by peaking desired-frequency signal strength with C 2 . At this time, leave $C 2$ at its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe $S$-meter, if available, or note audible level). The notes in Step 1.2 pertaining to S3, CI, and RI (for Line 1) may also be applied to $S 4, C 2$, and R2 as used on Line 2 .

## 1.4 ** EQUALIZE LINE 1 , LINE 2 LEVELS **

If the dominant-station signal level noted when peaking Line I with CI (Step 1.2) is comparable (within 3 dB on meter, or not audibly different) to the strength noted when peaking Line 2 with C 2 (Step 1.3), proceed to Step 1.5 .
$\ggg$ If the dominant-station signal level noted when peaking Line I with CI (Step 1.2) is noticeably greater than the strength noted when peaking Line 2 with C2 (Step 1.3), switch S6 between Line 1 and Line 2 while adjusting RI to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to Step 1.5. >>>

If the dominant-station signal level noted when peaking Line 2 with C2 (Step 1.3) is noticeably greater than the strength noted when peaking Line 1 with Cl (Step 1.2), switch S6 between Line 1 and Line $\mathbf{2}$ while adjusting R2 to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to Step 1.5.

## 1.5 ** initialize null **

Set S6 to Null-a and then to Null-b. If one of these positions shows noticeably-better reduction of the dominant signal, leave S6 at that setting and proceed to Step 1.6.
$\ggg$ If R1 and R2 positions are approximately the same (e. g. both fully counterclockwise), or R2 is closer to its initial CCW setting, set S 6 to Null-a and adjust CI for a null of the dominant station.

Do the same with S6 set to Null-b. Leave S6 at the position which gives the deeper, sharper null when you adjust CI . If there's little difference in null depth or sharpness between the two $\mathbf{S 6}$ null positions, select the S 6 position that results in Cl being set closer to the center of its mechanical adjustment range when a null is produced. Make a few small re-adjustments of Cl and RI to improve null depth. Then, proceed to Step 1.6. >>>

If R1 is closer than R2 to its initial CCW setting, set S6 to Null-a and adjust C2 for a null of the dominant station. Do the same with $\mathbf{S 6}$ set to Null-b. Leave $\mathbf{S 6}$ at the position which gives the deeper, sharper null when you adjust C 2. If there's little difference in null depth or sharpness between the two S6 null positions, select the S 6 position that results in C2 being set closer to the center of its mechanical
adjustment range when a null is produced. Make a few small re-adjustments of C2 and R2 to improve null depth. Then, proceed to Step 1.6 .
1.6 ** FINALIZE NULL **

Do the final null "touch-up" with an interactive adjustment of C1, C2, and R3.
2.0 MWDX-6 Loop-versus-Wire Phasing Procedure

NOTES:
The loop should be equipped with a Q -spoiling resistor of approximately $\mathbf{2 2 K}$ across its paralleltuned LC tank. A 50 K potentiometer (initially set to center) might be substituted; it can provide an added control over nulling if desired. The pot or fixed resistor should be easily removable (switch or clips) to facilitate stand-alone (high-Q) loop usage.

A loop used in a phasing application is usually oriented for best directivity toward desired DX signals, whether or not that position reduces the dominant. Sometimes orienting the loop for MAXIMUM dominant signal pick-up, or for dominant level equal to that from the wire, can actually help nulling.

## 2.1 ** INITIALIZE CONNECTIONS AND CONTROLS **

$\mathrm{JI}:$ connect Antenna \#I wire.
J2: connect center of coaxial cable from loop output.
J3: if a noise reducing ground for Antenna \#1 is available, connect it; otherwise, no connection is needed.

J4: connect shield of coaxial cable from loop output.
J5: this may be connected to mains, earth, or vehicle ground if doing so improves signal-to-noise ratio. This would be done more often with portable receivers than with tabletop communications models having a metal case.

J6: connect, via coaxial cable, to the receiver input, or to the input of a tunable preselector between the phasing unit output and the receiver input.

J7: connect this to a DC power source of +11 VDC minimum, +25 VDC maximum. If you don't intend to use the active (AC or AL) functions, DC power will not be necessary.

SI: set to NORM unless using a noise-reduced input pair at JI and J3 for Antenna \#1 (in that case, set SI to NR).

S2: set to NORM.
S3: set to Active Capacitively-Coupled (AC) (or to a different position, depending on experimentation that leads to having determined the best position for a given Antenna \#1, consistent with maximum usable signal with no spurious responses).

S4: set to Bypass (BP).
S5: set for the correct frequency range, according to Table 2.
R1: set to fully counterclockwise (minimum attenuation).
R2: set to fully counterclockwise (minimum attenuation).
R3: set to center of mechanical adjustment range.
2.2 ** PEAK LINE 1 **

Set S6 to (Line) I. Tune Line I by peaking desired-frequency signal strength with CI . At this time, leave Cl at its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe S -meter, if available, or note audible level).
[At this time, other positions of Line 1 Function switch S3 may be tried to see if greater signal transfer is possible. Re-adjustment of CI , and possibly SS , may be needed to re-establish a peaked condition. In any event, the peak should have reasonable $\mathbf{Q}$ (be well defined) and Cl should not be set too close to fully CW or fully CCW. If objectionable spurious responses are noted, adjust RI in a clockwise direction until the spurs are not noted with CI peaked properly OR set S3 to Passive Capacitively-Coupled (PC) function and re-peak CI.]

## 2.3 ** PEAK LINE 2 **

Set S 6 to (Line) 2. Tune Line 2 by peaking the loop's tuning capacitor. Leave the loop tuning capacitor à its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe S -meter, if available, or note audible level).
2.4 ** EQUALIZE LINE I, LINE 2 LEVELS **

If the dominant-station signal level noted when peaking Line I with Cl (Step 2.2) is comparable (within 3 dB on meter, or not audibly different) to the strength noted when peaking Line 2 with the loop tuning capacitor (Step 2.3), proceed to Step 2.5 .
$\ggg$ If the dominant-station signal level noted when peaking Line 1 with Cl (Step 2.2) is noticeably greater than the strength noted when peaking Line 2 with the loop tuning capacitor (Step 2.3), switch S6 between Line I and Line 2 while adjusting RI to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to Step 2.5. $\ggg$

If the dominant-station signal level noted when peaking Line 2 with the loop tuning capacitor (Step 2.3) is noticeably greater than the strength noted when peaking Line 1 with Cl (Step 2.2 ), switch S6 between Line I and Line 2 while adjusting R2 to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to Step 2.5 .

## 2.5 ** INITIALIZE NULL **

Set S6 to Null-a and then to Null-b. If one of these positions shows noticeably-better reduction of the dominant signal, leave S6 at that setting and proceed to Step 2.6.
$\ggg$ If R1 and R2 positions are approximately the same (e. g. both fully counterclockwise), or R2 is closer to its initial CCW setting, set S6 to Null-a and adjust CI for a null of the dominant station.

Do the same with S6 set to Null-b. Leave S6 at the position which gives the deeper, sharper null when you adjust C1. If there's little difference in null depth or sharpness between the two S 6 null positions, select the S 6 position that results in Cl being set closer to the center of its mechanical adjustment range when a null is produced. Make a few small re-adjustments of CI and RI to improve null depth. Then, proceed to Step 2.6. >>>

If R1 is closer than R2 to its initial CCW setting, set S6 to Null-a and adjust the loop tuning capacitor for a null of the dominant station. Do the same with S6 set to Null-b. Leave S6 at the position which gives the deeper, sharper null when you adjust the loop cap. If there's little difference in null depth or sharpness between the two $\mathbf{S 6}$ null positions, select the $\mathbf{S 6}$ position that results in the loop cap. being set closer to the center of its mechanical adjustment range when a null is produced. Make a few small readjustments of R2 and the loop capacitor to improve null depth. Then, proceed to Step 2.6.

## 2.6 ** FINALIZE NULL **

Do the final null "touch-up" with an interactive adjustment of Cl , the loop tuning capacitor, and R3. Slight physical re-positioning of the loop may also help to finalize the null.

If a 50 K pot (initially set to center, approximately 25 K ) had been installed across the loop coil (instead of the approximately-22K fixed resistor), it may also be touched up for null completion.

### 3.0 MWDX-6 Loop-versus-Loop Phasing Procedure

NOTES:
Each loop should be equipped with a Q-spoiling resistor of approximately 22 K , or a 50 K pot set to center ( 25 K ), across its paraliel-tuned LC tank. Q-spoiling components should be removable for normal stand-alone loop usage.

Two-loop phasing works best when the loops are aimed at bearings that are angularly separated by more than 60 degrees and less than 120 degrees. Orthogonal.( 90 degree) positioning is customary, with the bisector of the angle between the loops pointing towards the direction of interest. Example: To produce a cardioid pattern nulling west and peaking east (or, for that matter, nulling east and peaking west), Loop \#1 can be aligned northeast / southwest and Loop \#2 set to southeast / northwest. Loops should have comparable gains for best nulling results.
3.1 ** INITIALIZE CONNECTIONS AND CONTROLS **

JI: connect center of coaxial cable from Loop \#1 output.
J2: connect center of coaxial cable from Loop $\# 2$ output.
J3: connect shield of coaxial cable from Loop \#1 output.
J4: connect shield of coaxial cable from Loop ${ }^{2} 2$ output.
J5: this may be connected to mains, earth, or vehicle ground if doing so improves signal-to-noise ratio. This would be done more often with portable receivers than with tabletop communications models having a metal case.

J6: connect, via coaxial cable, to the receiver input, or to the input of a tunable preselector between the phasing unit output and the receiver input.

J7: no connection is needed.
SI: set to NORM.
S2: set to NORM.
S3: set to Bypass (BP).
S4: set to Bypass (BP).
S5: position is irrelevant.
RI: set to fully counterclockwise (minimum attenuation).
R2: set to fully counterclockwise (minimum attenuation).
R3: position is irrelevant.
3.2 ** PEAK LINE 1 **

Set S6 to (Line) I. Tune Line I by peaking desired-frequency signal strength with Loop \#1 Tune (the tuning capacitor on Loop \#1). At this time, leave Loop \#1 Tune at its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe S-meter, if available, or note audible level).

## 3.3 ** PEAK LINE 2 **

Set S6 to (Line) 2. Tune Line 2 by peaking Loop \#2 Tune (the tuning capacitor on Loop \#2). Leave Loop \#2 Tune at its peaked-signal position. NOTE THE SIGNAL STRENGTH (observe S-meter, if available, or note audible level).

## 3.4 ** EQUALIZE LINE I, LINE 2 LEVELS **

If the dominant-station signal level noted when peaking Loop \#1 (Step 3.2) is comparable (within 3 dB on meter, or not audibly different) to the strength noted when peaking Loop \#2 (Step 3.3), proceed to Step 3.5 .
>> If the dominant-station signal level noted when peaking Loop \#1 (Step 3.2) is noticeably greater than the strength noted when peaking Loop \#2 (Step 3.3), switch S6 between Line 1 and Line 2 while adjusting RI to make the observed signals equal on the S-meter (or not audibly different). Then, proceed to Step 3.5. >>>

If the dominant-station signal level noted when peaking Loop \#2 (Step 3.3) is noticeably greater than the strength noted when peaking Loop \#1 (Step 3.2), switch S6 between Line I and Line 2 while adjusting R2 to make the observed signals equal on the $S$-meter (or not audibly different). Then, proceed to Step 3.5 .

Set S6 to Null-a and then to Null-b. If one of these positions shows noticeably-better reduction of he dominant signal, leave S6 at that setting and proceed to Step 3.6.
$\gg$ If R1 and R2 positions are approximately the same (e. g. both fully counterclockwise), or R2 is closer to its initial CCW setting, set S6 to Null-a and adjust Loop \#1 Tune for a null of the dominant station. Do the same with S6 set to Null-b. Leave S6 at the position which gives the deeper, sharper null when you adjust Loop \#1 Tune. If there's little difference in null depth or sharpness between the two S6 null positions, select the S6 position that results in Loop \#1 Tune being set closer to the center of its mechanical adjustment range when a null is produced. Make a few small re-adjustments of Loop \#1 Tune and RI to improve null depth. Then, proceed to Step 3.6. $\ggg$

If R1 is closer than R2 to its initial CCW setting, set S6 to Null-a and adjust Loop \#2 Tune for a null of the dominant station. Do the same with S6 set to Null-b. Leave S6 at the position which gives the deeper, sharper null when you adjust Loop \#2 Tune. If there's little difference in null depth or sharpness between the two S 6 null positions, select the S 6 position that results in Loop \#2 Tune being set closer to
the center of its mechanical adjustment range when a null is produced. Make a few small re-adjustments of Loop \#2 Tune and R2 to improve null depth. Then, proceed to Step 3.6.

## 3.6 ** FINALIZE NULL **

Do the final null "touch-up" with an interactive adjustment of Loop \#1 Tune, Loop \#2 Tune, and whichever pot (RI or R2), is not set to a fully counterclockwise position. Slight re-positioning of each loop may also help to finalize the null. If either, or both, loops have a $50 \mathrm{~K} Q$-pot (instead of a fixed resistor) across its coil, touch such pots up for null completion.

## Building the MWDX-6 Phasing Unit

The documentation (schematics, assembly drawings, parts lists, hole lists, etc.) serves as the starting point. The following procedure should serve as an outline for the builder. This is NOT a beginner's project. Some experience in electronic "homebrewing" is advisable.

1. Gather all necessary parts (see Tables $2,4,5$ ). Prepare work area with appropriate tools.
2. Drill out chassis box, in accordance with Table 3.
3. Assemble the two BUF-A Buffer Amplifier Cards to be used for AI and A2. Refer to Figures 10 and 11 and Table 5.
4. Pre-wire the bandswitch ( S 5 ) per Table 2 and Figure 4.
5. Pre-wire S 3 and S 4 function switches in accordance with the detail in Figure 2.
6. Pre-wire the output switch (S6) in accordance with the detail in Figure 5.
7. Mount vernier knobs and tuning capacitors (C1, C2) per Tables 3 and 4 and Figures 6 and 9.
8. Mount the following components in the chassis box per pictorials (Figures $6,7,8$ ) and parts list (Table 4):

LEFT SIDE:
TOP SIDE:
J1, J2, J3, J4, J5, S1, S2, G1
RIGHT SIDE:
R1, R2, R3, G2, S5, S3, S4, S6
A1, J7, G3, J6, A2
Note that each grounding hardware assembly (G1, G2, G3) consists of a 4-40 X 0.375" screw, a \#4 solder lug, and a 4-40 hex nut. The lug and the nut are on the inside of the chassis box; the head of the attached screw is outside the box.
9. Install remaining electrical components and wiring inside the chassis box in accordance with the parts list (Table 4), the assembly pictorial (Figure 8), and the schematics (Figures 1 through 5).
10. Install knobs on R1, R2, R3, S3, S4, S5, and S6 per Figure 6 and Table 4.

## Table 3: MWDX-6 hole-drilling list

$\mathrm{X}=$ Horizontal distance, in inches, from the vertical centerline (VCL) on the side observed. Negative values of $X$ are left of VCL, positive values of $X$ are right of VCL.
$\mathrm{Y}=$ Vertical distance, in inches, from the bottom horizontal edge of the side observed.
$D=$ Hole diameter in inches.
Hole loci are first marked on the box with a scriber and are then drilled with a $.125^{\prime \prime}$ bit. Subsequently, as required, the holes are enlarged to the proper size by using progressively larger bits up to that corresponding to the final desired diameter.
Chassis Box = Mouser \#537-TF-782: 7" X 5" X 3" LEFT SIDE

| Hole \# | Comp. Desig. | Description | X | $\mathbf{Y}$ | D |
| :---: | :---: | :---: | :---: | :---: | :---: |
| - | --- |  | --.-- | --.- | -.-- |
| 1 | SI | Line 1 Input switch - shaft | -1.5 | 1.5 | 0.25 |
| 2 | SI | Line I Input switch - tab | -1.5 | 1.25 | 0.125 |
| 3 | J1 | Line I ant. -red banana jack | -1.5 | 0.5 | 0.3125 |
| 4 | J3 | GNDI In - black banana jack | -0.75 | 0.5 | 0.3125 |
| 5 | G1 | grounding H/W - internal lug | 0.0 | 1.125 | 0.125 |
| 6 | J5 | chas. GND-black banana jack | 0.0 | 0.5 | 0.3125 |
| 7 | J4 | GND2 In - black banana jack | 0.75 | 0.5 | 0.3125 |
| 8 | S2 | Line 2 Input switch - shaft | 1.5 | 1.5 | 0.25 |
| 9 | S2 | Line 2 Input switch - tab | 1.5 | 1.25 | 0.125 |
| 10 | J2 | Line 2 ant. -red banana jack | 1.5 | 0.5 | 0.3125 |
| TOP SIDE |  |  |  |  |  |
| Mounting holes on Cl \& C 2 must be tapped to 6-32 thread. |  |  |  |  |  |
| Hole | Comp. <br> Desig. | Description | X | Y | D |
| - | --.. | --.-.....-.......- | --...- | --. | --- |
| 1 | RI | Line I atten. pot - tab | -3.0625 | 4.0 | 0.144 |
| 2 | RI | Line I atten. pot - shaft | -2.75 | 4.0 | 0.3125 |
| 3 | R3 | Null vernier (Q) pot - tab | -3.0625 | 2.5 | 0.144 |
| 4 | R3 | Null vernier (Q) pot - shaft | -2.75 | 2.5 | 0.3125 |
| 5 | R2 | Line 2 atten. pot - tab | -3.0625 | 1.0 | 0.144 |
| 6 | R2 | Line 2 atten, pot - shaft | -2.75 | 1.0 | 0.3125 |
| 7 | (C1) | CI vernier knob - Mtg.H/W I | -1.64 | 3.25 | 0.125 |
| 8 | Cl | Line I Tuning Cap.-Mtg.H/W I | -1.463 | 4.125 | 0.144 |
| 9 | CI | Line I Tuning Cap. - shaft | -1.0 | 3.875 | 0.5 |
| 10 | Cl | Line 1 Tuning Cap.-Mtg.H/W 2 | -0.537 | 4.125 | 0.144 |
| 11 | (C1) | CI vernier knob - Mtg.H/W 2 | -0.36 | 3.25 | 0.125 |
| 12 | G2 | grounding $\mathrm{H} / \mathrm{W}$ - internal lug | -1.0 | 2.5 | 0.125 |
| 13 | (C2) | C2 vernier knob - Mtg.H/W 1 | -1.64 | 0.625 | 0.125 |
| 14 | C2 | Line 2 Tuning Cap.-Mtg.H/W 1 | $-1.463$ | 1.5 | 0.144 |
| 15 | C2 | Line 2 Tuning Cap. - shaft | -1.0 | 1.25 | 0.5 |
| 16 | C2 | Line 2 Tuning Cap.-Mtg. H/W 2 | -0.537 | 1.5 | 0.144 |
| 17 | (C2) | C2 vernier knob - Mtg.H/W 2 | -0.36 | 0.625 | 0.125 |
| 18 | S5 | Bandswitch - shaft | 0.75 | 2.5 | 0.375 |


| 19 | S5 | Bandswitch - tab | 0.75 | 2.0 | 0.144 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | S3 | Line I Function sw. - shaft | 1.5 | 4.0625 | 0.375 |
| 21 | S3 | Line I Function sw. - tab | 1.5 | 3.5625 . | 0.144 |
| 22 | S4 | Line 2 Function sw. - shaft | 1.5 | 0.875 | 0.375 |
| 23 | S4 | Line 2 Function sw. - tab | 1.5 | 0.375 | 0.144 |
| 24 | S6 | Output switch - shaft | 2.4375 | 2.5 | 0.375 |
| 25 | S6 | Output switch - tab | 2.4375 | 2.0 | 0.144 |
| RIGHT <br> Hole <br> \# | SIDE Comp. Desig. | Description | X | Y | D |
| - | $\cdots$ |  | $\cdots$ | $\cdots$ | $\cdots$ |
| 1 | A2 | Line 2 Buffer Amp. Card-H/W I |  | 2.2 | 0.125 |
| 2 | A2 | Line 2 Buffer Amp. Card-H/W 2 | -1.5 | 0.6 | 0.125 |
| 3 | 17 | B+ input - phono jack | 0.0 | 1.75 | 0.25 |
| 4 | G3 | grounding H/W -internal lug | 0.0 | 1.125 | 0.125 |
| 5 | J6 | RF out - BNC jack | 0.0 | 0.5 | 0.375 |
| 6 | AI | Line I Buffer Amp. Card-H/W I | 1.5 | 2.2 | 0.125 |
| 7 | AI | Line 1 Buffer Amp. Card-H/W 2 | 1.5 | 0.6 | 0.125 |

## Table 4: "upper level" parts list

NOTE: Inductors used on bandswitch S5 are itemized separately as shown by Table 2 and *: Note follows parts list.
Vendor codes for this and subsequent parts lists:
Figure 4.
AE = Antique Electronic Supply

GER $=$ Gerber Electronics
/ Tempe, AZ 85283
Trel. 1-602-820-5411
$/ 128$ Carnegie Row
/ Norwood, MA 02062
TTel. 1-617-769-4852, 769-6000
MCL $=$ Mini-Circuits Lab.
/P. O. Box 350166
/ Brooklyn, NY 11235-0003
/Tel. 1-718-934-4500
111433 Woodside Ave.
/ Santee, CA 92071
/Tel. 1-800-346-6873
/ Many locations worldwide

| $\begin{aligned} & \text { Item } \\ & = \pm= \end{aligned}$ | Designator | Description/Value | Vendor <br> = | Vendor Stock \# $\qquad$ | QTY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | - | chassis box 7X5X3" | MOU | 537-TF-782 | 1 |
| 2 | A1,A2 | BUF-A amp. card |  | (refer to text) | 2 |
| 3 | $(\mathrm{Cl}, 2)$ | vernier knob | MOU | 45KN100 | 2 |
| 4 | * | knob | RS | 274-416 | 7 |
| 5 | Cl, 2 | var. cap., 10-365pF | AE | CV-231 | 2 |
| 6 | C3,4,7,8,11 | capacitor, 0.1 uF | MOU | 539-CK05104K | 5 |
| 7 | C5 | capacitor, 10 uF | moU | 581-10K35 | 1 |
| 8 | C6 | capacitor, 0.01 uF | MOU | 539-CK05103K | 1 |
| 9 | C9,10 | capacitor, 36 pF | MOU | 21 CB 036 | 2 |
| 10 | G1,2,3 | solder lug, \#4 | MOU | 534-7311 | 3 |
| 11 | * | screw, 4-40 X.375" | MOU | 572-01881 | 7 |
| 12 | G1,2,3 | hex nut, 4-40 | MOU | 572-00484 | 3 |
| 13 | * | screw, 4-40 X .25" | MOU | 572-01880 | 8 |
| 14 | * | spacer, 4-40 X $5^{\text {- }}$ | MOU | 534-1450C | 4 |
| 15 | * | split lockwasher,\#4 | MOU | 572-00649 | 8 |
| 16 | * | screw, 6-32 X .25* | MOU | 572-01888 | 4 |
| 17 | * | split lockwasher,\#6 | MOU | 572-00650 |  |
| 18 | J1,2 | red banana jack | RS | 274-662 | 2 |
| 19 | J3,4 | black banana jack | RS | 274-662 | 2 |
| 20 | J6 | BNC jack | RS | 278-105 | 1 |
| 21 | 17 | phono jack | RS | 274-346 | 1 |
| 22 | R1,2 | pot., IK, linear | MOU | $31 \mathrm{CT301}$ | 2 |
| 23 | R3 | pot, 100 K , linear | MOU | 31 CR501 | 1 |
| 24 | R4 | resistor, 1 ohm | MOU | 29SJ500-1.0 | 1 |
| 25 | R5,6 | resistor, 20 ohm | MOU | 29SJ500-20 | 2 |
| 26 | S1,2 | switch, 3PDT,on-on | MOU | 10 TC 280 | 2 |
| 27 | S3,4 | switch/6pole/4pos.r | MOU | 10WR064 | 2 |
| 28 | S5 | switch/4pole/6pos.r | MOU | 10WR046 | 1 |
| 29 | S6 | switch/3pole/4pos.r | MOU | 10YX034 | 1 |
| 30 | T1,2,3 | RF transformer, 1:1 | MCL | T1-6-X65 | 3 |

## Misc. items: hook-up wire, buss wire, solder, labels "AS REQUIRED"

*Item 4 note: one each for S3, S4, S5, S6, R1, R2, R3
*Item 11 note: one each for G1, G2, G3; two each for C1 vernier knob, C2 vernier knob
${ }^{*}$ Item 13 note: two each for A1 mount, A2 mount, C1 vernier knob, C2 vernier knob
*Item 14 note: two each for C1 vernier knob, C2 vernier knob
*Item 15 note: two each for A1 mount, A2 mount, C1 vernier knob, C2 vernier knob
*Item 16 note: two each for C1, C2 - see Figure 9.
*Itern 17 note: four each for C1, C2 - see Figure 9.

Table 5: BUF-A Buffer Amplifier card parts list
Vendor codes per Table 4.
Schematic $=$ Figure $10 /$ Assembly $=$ Figure 11 .
Quantities are per-card. Double for total quantity required (A1, A2).

| $\begin{aligned} & \text { Item } \\ & =\pi=0 \end{aligned}$ | Designator | Description/Value | Vendor <br> == | Vendor Stock \# | $\stackrel{\text { QTY }}{==}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | BD | perfboard:1.2*X2.0* | RS | 276-1396 (cut) | 1 |
| 2 | CI | capacitor, 0.01 uF | MOU | 539-CK05103K | 1 |
| 3 | C2 | capacitor, 10 uF tant | MOU | 581-10K35 | 1 |
| 4 | C3 | capacitor, 0.001 uF | MOU | 539-CK05102K | 1 |
| 5 | C4,5 | capacitor, 0.1 uF | MOU | 539-CK05104K | 2 |
| 6 | H1,2 | screw, 4-40 X $25^{\prime \prime}$ | MOU | 572-01880 | 2 |
| 7 | H1,2 | spacer, 4-40 X $5^{\prime \prime}$ | MOU | 534-1450C | 2 |
| 8 | H1,2 | solder lug. \#4 | MOU | 534-7311 | 2 |
| 9 | PI-7 | flea-clip/ $.042^{\prime \prime}$ hole | MOU | 574-T42-1/C | 7 |
| 10 | R1,2 | resistor, 680 K | MOU | 271-680K | 2 |
| 11 | R3 | resistor, 100 ohm | MOU | 271-100 | 1 |
| 12 | R4,5 | resistor, 4.7 ohm | MOU | 295-4.7 | 2 |
| 13 | TI | RF transformer 4:1 | MCL | T4-6T-X65 | 1 |
| 14 | U1 | buffer amplifier IC | GER | (National)LH0033CG | 1 |

Table 6: control orientation conventions
Ensure that components are mounted and wired in accordance with this table; align knob pointers to clock positions indicated. Orientations are as viewed from outside the chassis box assembly.

| Side | Control | Orientation Conventions |
| :---: | :---: | :---: |
| left | S1 |  |
| left | S2 | NR = up; NORM = down NR = up; NORM = down |
| top | Cl | fully $\mathrm{CCW}=0$ on vernier knob |
| top | C2 | fully $\mathrm{CCW}=0$ on vernier knob |
| top | RI | $\mathrm{CCW}=$ maximum level $\quad$ (no attenuation) $=7: 00$ <br> $\mathrm{CW}=$ minimum level (maximum attenuation) $=5: 00$ |
| top | R2 | $\begin{aligned} & \mathrm{CCW}=\text { maximum level } \quad(\text { no attenuation })=7: 00 \\ & \mathrm{CW}=\text { minimum level }(\text { maximum attenuation })=5: 00 \end{aligned}$ |
| top | R3 | $C C W=$ maximum level/ $Q$ Line $1(\mathrm{~min}$. Line 2$)=7: 00$ <br> $C W=$ maximum level/Q Line $2(\min$. Line 1$)=5: 00$ |
| top | S3 | $P C=10: 30 ; A C=11: 30 ; A L=12: 30 ; B P=1: 30$ |
| top | S4 | $P C=10: 30 ; A C=11: 30 ; A L=12: 30 ; B P=1: 30$ |
| top | S5 | Refer to Table 2. |
| top | S6 | Line $1=10: 30$; Line $2=11: 30$; <br> Null-a = 12:30; Null-b = 1:30 |

## FIGURE 1: MWDX-G INPUT SECTION SCHEMATIC



FIGURE 2: MWDX-6 CENTRAL SECTION SCHEMATIC
(LINE 1)


FIGURE 3: MWDX-G CENTRAL SECTION SCHEMATIC
(LINE 2)


FIGURE 4: MWDX-6 TANK / BANDSWITCH COMPONENTS

BANDSWITCH INDUCTOR VALUES SHOWN ARE FOR
STANOARD (LWBC/ MWBC) VERSION. OTHER CONFGURATIONS
ARE POSSIBLE: SEE TABLE 2 OF ARTICLE.


FIGURE 5: MWDX-6 OUTPUT SECTION


FIGURE 6: MWDX-G CHASSIS PICTORIAL (TOP)


FIGURE 7: MWDX-6 CHASSIS PICTORIALS (LEFT, RIGHT SIDES)


FIGURE B MWDX-B ABSEMELY PICTORIAL (NOT TO BCALE)


NOTRS 1: FOR SS WIRING, SEE FIGURE 4 AND TABLE 2 2: JUNCTION L7 THROUGH L12, LIS THROUGH L2. 3: TP = TWISTED PAIR (INSULATED) WIRE

FIGURE 10: MWDX-6 PHASING UNIT (SCHEMATIC: BUF-A BUFFER AMPLIFIER CARD) one used for A1, one used for A2


FIGURE 9: MWDX-G PHASING UNIT
(C1,C2 VARIABLE CAPACTTOR / VERNIER KNOB MOUNTING)


## FIGURE 11: MWDX-6 PHASING UNTT

 (ASSEMBLY: BUF-A BUFFER AMPLIFIER CARD) one used for A1, one used for A2

