The 127E Transmitter is designed with features which make it universally applicable as a multifrequency transmitter for marine shipboard, marine shore, aeronautical ground and police services. A combination of high frequency and intermediate frequency operation, with the latter optional, covers most commercial requirements.

The 127E is completely housed in a compact sturdy cabinet of processed metal construction for protection against salt water atmosphere. Components are assembled on removable cast aluminum frames and decks. Electrical circuits are made by heavy duty automatic connectors and wiring is not disturbed when sections are removed through the front of the transmitter for inspection and service.

Collins Autotune System is operated by a ten position selector switch which completely retunes the transmitter, in six seconds or less, to any one of ten crystal controlled frequencies.

**Rated Power Output:** 500 watts A1 emission and 300 watts A2 and A3 emission.

**Frequency Range:** High frequency 2000 to 16,000 kc, Intermediate frequency 300 to 500 kc (optional).

**Modulation Capability:** 100%.

**Audio Frequency Response:** Uniform within plus or minus 2 db from 200 to 3000 cycles.

**Audio Frequency Harmonic Distortion:** Less than 10% R.M.S. total harmonics at any modulation level at 400 cycles.

**Carrier Noise Level:** More than 40 db below 100% modulation on A3.

**Keying System:** Allows full break-in operation. Antenna keyed on if. only. Antenna change-over relay provided for h-f operation. Keying speed of 60 w.p.m.

**Cabinet Dimensions:** 72" high, 21" wide, 22" deep. Shock mounting supplied when required.

**Power Source:** 115 volts, 60 cycle single phase a.c. A converter is supplied for operation from 110 volt d.c. when required.
A communications receiver—no matter how well constructed—is no better than in engineering. Each function in the SKYRIDER 23 was carefully analyzed from the most scientific approach before it was incorporated into the final circuit. (This page on drift characteristics from the Laboratory Data Book is an interesting example.) That is a vital reason why the "23" is one of the best receivers the Hallicrafters has built. Yes, it is available at your Distributors for only $23.10 down payment, less speaker. See it today. Try it tonight.

Back of the

the hallicrafters inc.
CHICAGO, U.S.A.
"LARGEST BUILDERS OF AMATEUR COMMUNICATIONS EQUIPMENT"
SKY BUDDY is an 18-feature communications receiver with continuous coverage from 44 MC to 545 KC with uniform sensitivity over the entire range. Electrical band spread. Beat frequency oscillator. Built-in line filter. Built-in rubber mounted speaker, etc. $29.50

Skyrider DEFIANT offers performance usually associated with more expensive receivers. Four bands cover from 43.5 MC to 545 KC. Frequency Meter tuning on 10, 20, 40, and 80 meter amateur bands. Controls include RF gain, Selectivity switch, Crystal phasing, Audio gain, Pitch control, Bandspread tuning, A.N.L. switch, BFO, etc., with crystal, $69.50

HT-4 (shown at right) is a high-powered amateur transmitter, giving 450 watts on CW and 325 watts on phone. Separate preamplifier allows remote control of volume, keying and standby. Transmitter may be set to any three of the 10, 20, 40, 80 or 160 meter bands. Like all Hallicrafters equipment, immediately available. Includes Pre-amplifier, coils and crystals for three bands $695

Super SKYRIDER SX-17 (illustrated at the left) is the finest communications receiver the Hallicrafters make. Has two stages of preselection, built-in Dickert noise limiter. Iron-core air tuned I.F. circuits provide wide range variable selectivity—from broad high-fidelity to single signal sharpness. 1000° Spiral bandspread dial. Plus numerous other quality features. With crystal, less speaker $13750

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"LARGEST BUILDERS OF AMATEUR COMMUNICATIONS EQUIPMENT"
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In acknowledging the tremendous popularity of Taylor's two Wonder Tubes, the T-40 and TZ-40, it is natural that Taylor Tubes salute the Helwig-Speer Carbon Company, whose fine Carbon Anodes have proved their stamina in the T-40 and TZ-40, by devoting this space to tell you —

WHY CARBON IS BETTER!

The ability of carbon to stand up and deliver maximum results under all working conditions — its better physical characteristics, make it truly a splendid anode material. Remember that the amount of power a tube will handle as an Oscillator — Amplifier — Doubler-Modulator or Rectifier — depends to a large degree on the ability of the anode to dissipate heat. Because carbon has an extremely high radiation emissivity, and high thermal conductivity, anodes made of carbon are superior. We list here some of the major reasons why carbon is a preferred anode material.

RADIATION EMISSIVITY

It is an established scientific fact that rough, black surfaces radiate heat many times faster than smooth metallic surfaces. This feature of carbon insures lower temperatures of all associated tube parts — adding to the tube’s ability to withstand overloads.

THERMAL CONDUCTIVITY

The high thermal conductivity of Helwig-Speer Carbon Anodes, produces quicker diffusion and a more uniform distribution of heat throughout the anodes. This feature prevents hot spots which result in warping and fusing of the anode material. Tubes using Carbon Anodes, can be made with smaller elements because carbon radiates heat at a faster rate. This means low inter-electrode capacities and permits successful operation at higher frequencies.

DEGASSING QUALITY

All known materials, usable as anodes, have a heat point at which all gasses will be expelled. In degassing a tube, tremendous heat is induced into the anode by Radio Frequencies while a series of vacuum pumps of special design carry away the gases being liberated. (It is interesting here to note that carbon has the highest melting point of all common anode materials. Carbon does not melt at temperatures under 3537°C while Tungsten has a 3370°C melt point, Tantalum a 2850°C melt point and Molybdenum a 2620°C melt point.) Regardless of the anode material used this process of degassing is always followed. A TUBE MADE “GAS-FREE” IN PRODUCTION REMAINS “GAS-FREE”. Helwig-Speer Processed carbon anodes have ideal degassing qualities and compare, in this respect, more than favorably with all other anode materials.
EXPERIENCE GAINED IN PRODUCING 20,000 T-40's and TZ-40's NOW MAKES POSSIBLE Increased Ratings

Over 20,000 of these Wonder Tubes have been made and sold in 20 months. Continued research and experiment have proved that in INTERMITTENT AMATEUR SERVICE our original Operating Ratings were extremely conservative. The new ratings shown below are still conservative and allow you true long life performance. The regular operating ratings remain the same for continuous commercial service, the new ratings for Intermittent Amateur Service.

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<th>Commercial</th>
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Class C Telegraph
Plate Volts 1500 V.
Plate Current 150 M.A.
Grid Current 38 M.A.

Class C Telephone
Plate Volts 1250 V.
Plate Current 125 M.A.
Grid Current 40 M.A.

The performance in actual service of the Wonder Tubes T-40 and TZ-40 over the past 20 months prove that Taylor's ratings are conservative. The husky Carbon Anode is rated at only 40 watts, yet it actually takes 70 watts plate dissipation to cause the anode to show color. That means your T-40 or TZ-40 can stand serious overloads without damage—a real safety factor. The complete Molybdenum Grid designed for heavy duty service withstands abnormal abuses. Taylor Tube filaments are designed as to diameter and length so that they provide the necessary surface area needed to furnish emission in amounts well beyond the requirements of maximum peak plate current with good emission efficiency in terms of filament power at safe temperature for long life.

When Taylor Tubes brought out the Wonder Tubes—T-40 and TZ-40—comparative types sold at $10.00. Amateurs the world over quickly recognized the outstanding value of the T-40 and TZ-40 and rapidly they have become the most popular of all Amateur Transmitting Tubes. Naturally the tremendous success of these Wonder Tubes has attracted competition—and we expect more. We ask you to remember that the experience gained in producing this large number of tubes is your best assurance of Better Performance and Top Value. Insist on Taylor's T-40's and TZ-40's—conservatively rated like all Taylor Tubes—and proved through use.

RECOMMENDED BY LEADING PARTS DISTRIBUTORS

"More Watts Per Dollar"

TAYLOR TUBES, INC., 2341 WABANSIA AVE., CHICAGO, ILLINOIS
### Section Communications Managers of the A.R.R.L. Communications Department

All appointments in the League’s field organization are made by the proper S.C.M., elected by members in each Section listed. Mail your S.C.M. on the 10th of each month a report of your radio activities for the previous 30 days. Tell him your DX plans for experimenting, results in phone and traffic. He is interested, whether you are an A.R.R.L. member or not, your DX plans at the newstands; he wants a report from every active ham. It is interested and qualified for O.R.S., O.P.S. or other appointments he can tell you about them, too.

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We make more different types of resistance units than any other company in the world — each having characteristics making it particularly suitable for a certain class of service.

There is naturally a temptation to devote this page to some new development in resistors or circuit application, but we should not neglect one of our old standbys — in fact, our Bread and Butter in the average ham shack — the cement-coated power wire wound resistors.

Their acceptance is no accident. In food mixers and Pullman cars, desk fans and submarines, furnace controls and dental equipment, in Peace and in War, they carry on their unspectacular task. They make no headlines but many headlines would not be made without them.

All the ingenuity we can muster in their design, all the care we give to their manufacture is to the end that you can install them, depend on them — and forget them.
The American Radio Relay League, Inc., is a non-commercial association of radio amateurs, bonded for the promotion of interest in amateur radio communication and experimentation, for the relaying of messages by radio, for the advancement of the radio art and of the public welfare, for the representation of the radio amateur in legislative matters, and for the maintenance of fraternalism and a high standard of conduct.

It is an incorporated association without capital stock, chartered under the laws of Connecticut. Its affairs are governed by a Board of Directors, elected every two years by the general membership. The officers are elected or appointed by the Directors. The League is non-commercial and no one commercially engaged in the manufacture, sale or rental of radio apparatus is eligible to membership on its board.

"Of, by and for the amateur," it numbers within its ranks practically every worth-while amateur in the nation and has a history of glorious achievement as the standard-bearer in amateur affairs.

Inquiries regarding membership are solicited. A bona fide interest in amateur radio is the only essential qualification; ownership of a transmitting station and knowledge of the code are not prerequisite. Correspondence should be addressed to the Secretary.
"IT SEEMS TO US—"

POSITION REPORT

As we write, in early October, we are keenly conscious that fast-moving developments in the international situation may make hash of what we write before the printer's ink is dry. It has been that way the past two weeks. We can only do our best.

We have just returned from Washington, where we talked over the position of the amateur with officials in every branch of the government concerned with radio. We still feel assured that there is no present room for uneasiness about our situation, provided that we continue to behave ourselves. Officials watchfully ponder the whole communications picture, but there are no deep and foul plans to do away with us. They don't know what may happen to alter America's position in the international picture; they don't know what steps may later become necessary to protect our country's interests. But stories that there are intentions to close us down are completely untrue. The nation needs its radio amateurs as it never has before, and that fact is realized.

In the month since we presented the A.R.R.L. neutrality code the ether has rung to the retelling of that story on every band. By now it must be known to every amateur. And by now it is clear that only our prompt and voluntary adoption of that code, and our ability to show Washington that we were taking care of our own house, saved the day for us during the early unsettled period. It continues to be of transcendent importance that we observe neutrality by refraining from discussing on the air any manifestation of the war and any subjects that might have military interest for an interceptor. To the extent that you value your right to operate, let that be your code, unfailingly!

ABOUT INTERCEPTING

We amateurs have trained ears and sensitive receivers, and our numbers blanket the nation. We are ready for any emergency job that might be entrusted to us. There have been reports in the press that amateurs were being appointed "radio detectives" — we're not sure what for — and some of us are simply bursting to get going on such an assignment.

Sorry, fellows, but there is nothing stirring. There are no such jobs. The press stories are incorrect. The League has offered our services to the appropriate government agencies but they are not needed. America is at peace with all the world. There is no situation existing that cannot be covered by the normal facilities of the government. The government says it wants no self-appointed vigilantes, no super-patriots going around chasing spies.

We are even less free than the ordinary citizen in such matters, for the secrecy provisions of radio law are still in full force. It is against the law to divulge the text of a message, or its general meaning, or even its existence. We must not appoint ourselves super-patriots and commence copying down everything that we can't understand, and reporting it. To do so will cause us about as much embarrassment as to violate neutrality ourselves. Frequency, calls and hours of course can be mentioned, but not the nature of a communication. Amateurs must not copy texts and send them to Hq. for study, because that constitutes divulging them. They may not send them to government agencies because these agencies have not requested and authorized it.

The foregoing refers to the authorized communications of government and licensed stations. The protection of the secrecy provisions does not extend to unlicensed stations operating in defiance of law. If amateurs hear an unlicensed station sending a message that violates U.S. neutrality, and if they are sure the station is unlicensed, they may report the matter in detail. But if it turns out to be the communication of an authorized station, the amateur is in great danger of being penalized for violating the secrecy provisions. (And — while it's an academic point — that would be true even if the text violated neutrality.) We would be praised for turning in an unlicensed station engaging in unauthorized activities, but there are surely not many such, and the risk is great that we would only be intercepting a routine military tactical drill and that the result would be a suspension for the reporter and a black eye for all of us.

Now under these circumstances, what should we do? We suggest that we "lay off." We may listen and keep our ears open but we counsel every amateur to sit tight unless he is dead sure what he's talking about. We repeat that there is no large situation needing our assistance. Existing agencies can deal with it. Let's stick to our own operating.

While amateur communications also have the protection of the secrecy provisions, this
doesn't bar an amateur from communicating by radio or mail with another ham who is "talking about the war," to call our code to his attention and ask his compliance. We request all hams to help us make sure that our house is clean as clean.

FORWARD!

Let's summarize: The period of jitters is over. If we'll only carry on as we were doing four months ago, before this war was imminent, we can do so indefinitely. Let us show calmness and restraint. Let us squash stories that anything is going to happen to amateur radio. We have a mighty busy and interesting winter ahead of us. Let us have only one big rule for ourselves: to ignore the w-r completely as a topic of conversation and action!

K. H. W.

* SPLATTER *

Of particular interest to the u.h.f. gang will be the description of WIXEH's coaxial antenna by Ed. Sanders. This antenna, besides being an original piece of design, is intriguing because it is right down the alley of a ham experimenter: a pair of tin shears and some gutter pipe, and you have the essentials for a highly effective general coverage radiator.

Phil "Gil" Gildersleeve, W1CJD, has been making QST cartoons for over a decade. In 1931 he did a series of cartoon strips depicting the maneuvers of the Podunk Hollow gang for QST covers. That this series was well liked is evidenced by the fact that fellows still ask, "When are you going to have some more cartoon covers?" For the past two years Gil has forsaken Gildersleeve-on-the-Connecticut for life among the banana boats, pounding brass and air-mailing cartoons between ports. We are indebted to W1DDB for a self-portrait that Gil made and exchanged with DDB, another artist, some years ago.

This design was made and produced by The Robbins Company and is one of the neatest we have ever seen. An award will be made to both c.w. and 'phone participants in every A.R.R.L. section.

FEEDBACK

Equation 2, p. 40, October QST

This equation should read:

\[ X_2 = \sqrt{R_1 R_2 - R_2^2} \]

P. 39, October QST

If there is anyone, besides the Managing Editor, who didn’t catch this one (a couple more states and we would have WAS), that halftone is upside down.

Our Cover

This is a rather shuffled array of gear comprising a portable station that was built by Clint DeSoto for the new Handbook, about to be released.
More Thoughts on Effective Antennas

Proven Designs for 14, 28 and 56 Mc.; Four-Element Beam Supports; Tuning the Array

BY ARTHUR H. LYNCH,* W2DKJ

For many years we have held the idea that amateurs generally were not taking full advantage of the better performance which could be obtained from a given transmitter and receiver by using antennas suitable for the particular job the station was intended to do. It has been a source of great satisfaction to find that the past few years have focused more and more attention on that subject. As most of us now know, it is easier to maintain contact between two given stations, with reasonably low power but equipped with suitable beam antennas pointed at each other, than it would be with several times the power and the older types of aerials — and very much cheaper.

Many of the commercial companies have been using large rhombic antennas to good advantage for some time, and the reports from those amateurs who are lucky enough to have the space available to duplicate them have been so glowing that the rest of us have burned up with envy. Since radio began, we have gone about our business by starting with something rather large and gradually cutting and trimming until much more efficiency has been brought out of equipment which, in many cases, is less than a quarter the size of the original. It is therefore with a feeling of confidence, founded on the solution of many knotty problems in the past, that some of the more pioneering souls among hams have attempted to produce small antennas which would approach the performance of the envied larger ones, but which could be used by those of us who are not blessed with many acres.

In presenting the following facts — and sufficient time has elapsed to be certain that they are facts — we make no claim for any particular originality, other than certain portions of the mechanical design which seem to contribute to the ease and the permanence of the final assemblies. As was the case with the former articles which we prepared for QST, the present one combines our own investigations with those of many others, and we trust that the present digest will bring the same hearty response which came from the past efforts.

*Managing Director, W2USA Radio Club, N. Y. World’s Fair, 1939.

Five Meters

Like many other amateurs whose property is not large enough to warrant extensive antennas on the lower frequencies, we have been confining our own investigations to the five- and ten-meter bands. It is fairly well understood that most of the conditions which obtain on the higher frequencies can be duplicated on the lower frequencies, giving due consideration to some of the important factors such as height above ground and freedom from other objects, when the dimensions are increased to produce similar results on the lower frequencies.

This is both an advantage and a handicap. It is an advantage for the reason that the adjustments become less critical as we go lower in frequency. Adjusting a matching stub on 112 megacycles is much more of a precise undertaking than doing so on an antenna designed for twenty-meter operation. It is a handicap for the reason that aerials approach in actual performance the theoretical only when they are sufficiently above ground and well in the clear, so far as other objects are concerned. The latter fact becomes more important as the natural radiation or absorption qualities of the objects within the field of the antenna increase. Well known as these facts are, they are sometimes forgotten.

Based upon the informative article on the “Extended Double-Zepp Antenna,” by Hugo Ro-

Besides giving some timely electrical dope on antennas useful in the 5-20 meter range, the author shows how, with a few simple changes, the framework described in a previous QST article can be adapted to support multielement rotary beams.
mander, W2NB, Frank Lester, W2AMJ, and Lawrence Cockaday, W2JCY have applied the same principles to five meters. Most of the Romander article had to do with horizontal aerials, while most of the five-meter activity is on vertical units. There was no reason to believe that the change of plane would change the overall results very much. Actual experiment, however, indicated that a very considerable change in the dimensions suggested by Romander would be necessary if the best results were to be obtained on five meters with a vertical antenna. This type of antenna has been used to better advantage by both Lester and Cockaday than any antenna they had previously used for five-meter operation. Equally improved performance has been the experience of all the other stations which have installed this very simple aerial, including the one which has been in use at W2USA ever since that station has been on the air, which will be nearly a year by the time this article is published. (The five-meter transmitter at the N. Y. World's Fair was operated as W2DKJ, until the issuance of the W2USA call.)

The arrangement shown in Fig. 1 is in use at W2USA at present. It is frowned upon by both Lester and Cockaday, for the reason that a twisted pair is used to feed it. They claim that the losses in that form of transmission line are too great. We agree that some gain in efficiency could be brought about by the use of a spaced transmission line on the high frequencies, but there are certain limiting factors over which we have no control, and we are forced to take the loss and like it. In spite of loss in the line, the convenience warrants its use in any number of places and we do know that we are getting better results than would be possible with a half-wave antenna delta-matched to an open line, a type commonly used for five-meter operation. That fact has been borne out at all of the stations which have made the change. Just how much better the open-wire arrangement would be, we cannot say, but we do everything we want to do with our present arrangement. All of the important dimensions (for the middle of the band) will be found in the drawings, and the picture of the antenna in use at W2USA indicates how it is done. Of course dimensions can be altered and standing waves can be eliminated in the usual manner. For all practical purposes, however, we know that the system may be set up just as shown and excellent results will be obtained.

The second figure gives all the necessary information for the use of an open line of the type used by both Lester and Cockaday. For the operator who is acquainted with antenna and transmission-line tuning and pruning, there will be no difficulty in bringing the whole system to peak performance; for operators who do not have such experience, we suggest the setup just as it is shown. Any number of installations have been made in just that manner with very gratifying results in every case.

**Beam Antennas**

There is an old saying: "You don't get something for nothing — for long." It is pretty well borne out in connection with the use of beam aerials for improving the performance of any radio station. We hear a lot of conversation on the air and we read much about the "gain" to be obtained from a given antenna system. To be sure, the use of a suitable antenna system will improve the performance of any station. But if the gain

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2. Depending upon the spacing of the open-wire line and the way in which it is brought from the antenna, radiation from the line may cause the radiation angle to shift upward, with consequent reduction of the effectiveness of the antenna on 56 Mc. This accounts for the superiority of the concentric line antennas over the "J," for example. Since radiation is negligible from a twisted pair, the overall performance of the system may not compare as unfavorably with an antenna fed by an open line as might be thought from consideration of the considerably higher losses in the rubber-insulated line. — Editor
for certain antenna systems were actually what is claimed for them, we should be well on the road to the solution of the perpetual motion problem.

The simplest way to understand why beam aerials are superior to the ordinary kind is to consider the analogy of an automobile headlight. An ordinary 32-candle-power bulb, if used without reflectors and hung directly from the ceiling of the ordinary room, would produce anything but good illumination. And, even in this case, there is a certain amount of reflection from the bright ceiling. But if we take the same bulb and place it in front of a good reflector, it can be made to produce a beam which will have the equivalent of several hundred candle power, in the direct line of the beam.

If we move the lamp toward or away from the central portion of the reflector, within certain limits, we will increase or decrease the width of the beam. As the width of the beam is increased the intensity of the light in the direction of the beam is cut down, and as the beam is sharpened the intensity is increased. It is easy to see that the light intensity at a distance of say thirty feet from the lamp would be much greater for a highly directive beam than for the lamp used without any reflector.

Additional increase in the luminosity of the beam is produced by the introduction of one or more lenses ahead of the lamp, as is done with the common flashlight. We know that we can operate an ordinary flashlight in a dark room without any reflector or lens and the light it produces will not bother our eyes, even if we look directly into it. The same bulb, with suitable reflector and lens, when properly adjusted to produce a sharp beam will give a blinding light at more than two hundred yards.

And so it goes with the radio beam. Our transmitter, tuned to the nth degree, may well be considered the flashlight battery; the regular antenna, or radiator, the flashlight bulb; the reflector remains the reflector and the lens of the flashlight is replaced by what we call the director.

We do not get any additional power from the use of suitably designed beams; what we do is use the available power more efficiently. We put it where we want it and where it will be useful, without having the light shining in other people's eyes. On the other hand, when similar antenna systems are used for receiving we have the advantage of receiving with greatest intensity from the desired direction, with great attenuation of signals coming from undesired directions.

Without delving into the complications of the underlying theory of antenna design we get right down to the details of an antenna system which has given remarkable results in the 14-Mc. band. Certain mechanical defects which showed up in an early model of this antenna have been overcome in the design shown in Fig. 3.

**Supports**

The "ladder" type of construction has given satisfaction with 14-Mc. beams when the number of elements has not exceeded three. However, when four elements have been used, there has been noticeable warping of the central structure, with resultant disalignment of the elements which in turn has brought about a serious reduction of the overall efficiency of the beam. In many instances the pattern, originally of a very fine character, has been so badly distorted that the front-to-back signal ratio has been more than cut in half, and signal strength off the ends, which would normally be almost zero, has come up to a point which competes with the other angles. It was with a view to preventing such warping, without going to a mechanical assembly which would be unduly heavy, that we developed the support shown in Fig. 3.

Retracing our steps to the framework we described in October, 1938, *QST*, and considering the additions we made to that original design to use it for a three-element beam, we decided that it would be a reasonably simple job to use the same design for two new supporting frames, one for a four-element 28-Mc. array and the other for a four-element 14-Mc. array.

For 14 Mc., it was only necessary to extend the length of "D," in our original Fig. 3, and add two additional "E" sections which are used to carry the two additional elements. Additional transverse struts have been added, similar to those shown as "F," in the first drawing. Extensive further modifications have been made to the concrete framework, and Fig. 3 shows the completed design. The framework for the four-element 14-Mc. beam, the lighter portions being the additions to the original frame described in October, 1938, *QST*. Shown in the author's yard prior to its installation at W2USA. W2BRI in attendance.
sion of the long arms of the beam is simplified by using single extensions instead of double rails, and this also has the effect of holding the weight down materially. The transverse struts have been made very much lighter than in the original design to hold the weight down, and both strength and rigidity are attained by the use of the raised guy wires. And that brings up a few points which are well worth considering.

**Guying**

In addition to providing unusual strength with very light weight, the use of the proper sort of guying arrangement gives us very satisfactory control over the positions of the outside elements. It is bad practice to run the guys through the central support and carry them to more than one of the outside points; each guy should be terminated at the central support. Then, by proper adjustment of the turnbuckles, we can raise or lower the outside elements with relation to the two central units and we can raise or lower the outside ends with relation to the central axis. Thus all the elements can be maintained in the same plane, even if a certain amount of "set" occurs after the beam has been completed. As all the turnbuckles are located near the center of the beam framework, suitable adjustments may be made before the assembly goes into the air.

In our own case, certain precautions were taken which we believe to be well worthwhile. For instance, we chose the National Type AA-5 compression-type strain insulators for making up the guys. They are very small and therefore offer very little wind resistance; furthermore, they are very light. For the guy wires we used No. 12 Copperweld. It is steel wire with a copper coating, and is also enameled. It is not the easiest wire to work with since it is very stiff, but a couple of pairs of gas pliers did the trick for us in good shape. The turnbuckles we selected are light, but well plated, so as to withstand the weather.

We found it convenient to use ringbolts for the guy terminations, as they served the purpose of holding the various portions of the framework together, along with their function of providing a suitable guy anchorage. Like all the other metal parts, they should be weather-resistant.

**Lengths and Spacings**

After long experience with various types of beam antennas, as well as from comparing notes with other workers, we have come to the conclusion that the formulas to be given constitute a very good starting point for the adjustment of any antenna. It must be borne in mind that no formula will apply under all conditions. The height of the aerial above ground, the proximity, as well as the character, of surrounding objects and other variables of a similar nature, will alter cases to a greater or lesser degree. The character of the ground above which the antenna is to be
erected will have a very important effect upon its final performance. None of these things can be determined with much accuracy in advance. So, while the tables which most of us are wont to mention so glibly are correct for a theoretically perfect group of circumstances, they will hardly fill the bill in the average case. For that reason we suggest them as nothing more than the starting point.

Since all the dimensions for the various portions of the 14-Mc. band are so much alike, it is possible to utilize a supporting framework with fixed spacing between the elements, compensating for any variations by the adjustment of the small tuning stubs, as outlined later on.

The formulas are:

\[ R = \frac{492,000}{f} \text{ (kc.)} \]
\[ A = 0.95R \]
\[ D = 0.925R \]
\[ R \text{ to } A = 0.1 \times 2R \]
\[ A \text{ to } D = 0.95 \times 0.1 \times 2R \]
\[ D \text{ to } D = 0.95 \times 0.1 \times 2R \]

All dimensions are in feet. \( R \) is the length of the reflector, found by dividing the constant 492,000 by the frequency in kilocycles; \( A \) is the actual antenna, or driven element; \( D \) and \( D \) are the directors. From these formulas we have the following approximate figures for the ends and center of the 14-Mc. 'phone band:

<table>
<thead>
<tr>
<th>Frequency (kc.)</th>
<th>( R )</th>
<th>( A )</th>
<th>( D )</th>
</tr>
</thead>
<tbody>
<tr>
<td>14,150</td>
<td>34' 9/16''</td>
<td>34' 8''</td>
<td>34' 6 1/4''</td>
</tr>
<tr>
<td>14,200</td>
<td>33'</td>
<td>32' 10 3/4''</td>
<td>32' 9 1/4''</td>
</tr>
<tr>
<td>14,250</td>
<td>32' 11/2''</td>
<td>32' 1 1/2''</td>
<td>31' 11 3/4''</td>
</tr>
</tbody>
</table>

\[ R \text{ to } A \] = 6' 11'' 6' 10'' 6' 9''
\[ A \text{ to } D \] = 6' 7'' 6' 6 1/2'' 6' 6''
\[ D \text{ to } D \] = 6' 7'' 6' 6 1/2'' 6' 6''

Except for slight differences in the lengths of the various elements, it will be seen that variations in the other portions of the assembly, for frequencies within the 14-Mc. 'phone band, are very small indeed. They may be neglected, as we have said, and compensated for by the adjustment of the stubs in the various elements.

**Tuning the 14-Mc. Four-Element Beam**

Although others have been able to get satisfactory results by tuning their four-element arrays while they were on the ground and then making slight adjustments to bring them "on the nose" when they got them into the air, we have never had much luck with that procedure. Then, too, we set about the job with misgivings for the reason that the portion of the short stub which is to be used is actually added to the center of the antenna system all the way down to the final tank transformer for the transmission-line, the radiator has been suitably adjusted. The method used to accomplish this is to set the radiator to the indicated length, which figure includes the length of the two halves plus fourteen inches. This latter figure is made up by considering the shorting bar to be half way down the stub, the two sides of which are two inches apart. That permits us to raise or lower the shorting bar six inches from the central position, which has proved to be amply. The stubs themselves consist of two separate wires, each a foot long.

While it is possible to do the tuning by having another person listen in for the signals from the beam to be adjusted, we believe the following will be much simpler and more satisfactory.

Considering that we are to use a delta matching transformer for the transmission-line, the radiator system all the way down to the final tank will have the general appearance of Fig. 4. The number of turns required to couple the line to the final amplifier will be determined by the impedance of the line; in the case of the 600-ohm line, four turns will do very well. If the center of the coupling coil is grounded, as indicated, very satisfactory lightning protection is provided. It will be seen that the wires which form the delta will be attached about 22 inches from the inner extremities of the two units which form the radiator. The equilateral triangle generally used seems to be thrown out of kilter, but if we consider that the portion of the short stub which is to be used is actually added to the center of the matching transformer, it will be seen that the proportions of the triangle are fairly well kept.

Now, we set up a good field-strength meter, a

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couple of wavelengths from the radiator. It is worth mentioning that the antenna used in conjunction with the field-strength meter, should be in the same plane as the antenna. However, it is not necessary to have it at the same height, though this is desirable. If we are using the antenna in a horizontal plane the field-strength meter should have its antenna in a horizontal plane, and vice versa.

Now, the radiator is energized with low power — just enough to provide suitable readings on the field-strength meter. Naturally, the radiator and the field-strength meter antenna should be parallel. The shorting bar is raised and lowered until the greatest reading on the field-strength meter is obtained. This adjustment is not too critical and may be accomplished by sliding the bar up and down by hand — though it is important, even with low power, to use gloves. This is just as true when we are working on other elements as it is when we are adjusting the directly-fed element.

Next, swing the beam around to a position where the reflector is between the radiator and the field-strength meter, attach the shorting bar to the reflector stub and adjust for the lowest reading on field-strength meter.

Now swing the beam around again so that it is pointing at the field-strength meter and manipulate the stub of the first director until the greatest field strength is indicated on the meter. In some instances it will be found, even when this adjustment is made with fifty watts or less going into the radiator, that the field-strength meter will have to be shunted to prevent its going off scale. Some experimenters advocate the reverse procedure, in which the reflector remains between the driven radiator and the field-strength meter and the director is adjusted until the lowest reading, indicating the greatest rejection, is obtained. Both methods will work.

Finally, coming to the second director, the stub of that element is adjusted until the highest reading is obtained on the field-strength meter. At this point, it will be found that the front-to-back ratio of the beam is tremendous and no further adjustments need be made. However, by trimming here and there, it will be found that even greater increase is made possible. There is no cheaper way of improving the efficiency of a transmitter. The power gain which these few, easy adjustments make possible is highly gratifying.

Standing Waves

Above, we mentioned that the field-strength meter should be a couple of wavelengths or more from the radiator. One important reason for this precaution is the fact that, with the transmission line tied to the antenna in the manner suggested for starting the tests, it is very likely to be out of adjustment as far as impedance match is concerned and will no doubt have some standing waves and may be somewhat unbalanced. If that is the case, and the field-strength meter is too close to the line, the meter will respond to radiation from the line in addition to that from the radiator, resulting in readings which are likely to be inaccurate.

Except for the misinformation they would give us with regard to the proper adjustment, it is doubtful if standing waves on the line would have any serious effect on the overall performance of the beam. However, they are very easy to eliminate and, if we are going to operate with high power in a congested area, the possibility of interference with broadcast reception can be reduced by eliminating them.

Six-volt flashlight bulbs coupled to the line by a loop of wire will do the trick. The amount of wire in each of the loops will depend on the amount of power in the line. In our case, a couple of inches was all that was necessary, with 500 watts input to the transmitter. First locate a point on the line where the bulb lights up brilliantly and clip one bulb there. Place a second bulb a quarter wavelength along the line from the first. This point is easy to locate by finding the spot where the bulb shows the least brilliancy.

Now it is only necessary to increase or decrease the distance between the points of the delta where they join the radiator until the brilliancy of the two bulbs is equal.

The 28-Mc. Beam

The only essential differences between the new four-element 28-Mc. beam frame and our original framework for a 14-Mc. W8JKK array are in the length of the longitudinal sections and the fact that we use single wooden supports for the ele-
W1XEH, the u.h.f. transmitter of WTIC, originally was installed a few years ago to provide a continuous 63.5-Mc. signal for recording at Harvard, in cooperation with the late Ross A. Hull's program for investigation of air-mass bending of u.h.f. waves. The antenna described here has given such satisfactory performance, in comparison to the conventional multi-element array, that it certainly warrants trial by amateurs interested in improving the strength of their 56-Mc. signals. Constructed of tinsmith's materials, its appearance is far from conventional.

A Novel Four-Element Collinear Array for 56-Mc. Work

The stacked coaxial radiator at W1XEH has four in-phase elements made of downspouting with sheet-metal sleeves. The downspouting serves as transmission line, part of the radiating system, and part of the phase-reversing stubs. It is all one piece — no insulated joints are necessary.

Stacking Coaxial Antennas

BY EDWIN R. SANDERS*

The original antenna at W1XEH was a bi-directional array toward New York and Boston, hung from a halyard between two poles. Arrays hung in this fashion must be light in weight and so are susceptible to damage by storms. Further, the insulators were located at voltage loops, so that rain and snow changed the characteristics of the antenna so much that the final stage was sadly detuned and mismatched in bad weather.

To overcome these defects a second antenna, an 8-element array 4 elements high and two wide, supported from a central lattice tower, was constructed. The phasing sections were made of 3/4-inch I.D. hard copper tubing and supported from the tower by standoff insulators near their centers where the voltage is low. The antenna elements were 1/2-inch I.D. hard copper tubing run vertically between the ends of the feeders. Since the phasing sections were very stiff no insulators were needed at the junctions with the antenna elements, and since there was no feeder

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A close-up of one section of the antenna.

November 1939
at the top or bottom of the array, the upper and lower elements were supported at their centers, where the voltage is low, from wooden crossarms and standoff insulator, as shown in the photograph.

The array was excited through an open line of 3/16 copper tubing spaced 4 inches. This was pulled tight with turnbuckles so that spans of 25 feet were permissible without the use of spreaders. The line was supported by metallic insulators consisting of 1/4-wave shorted stubs. A matching stub was used to couple the line to the middle of the center horizontal phasing section.

This antenna was a great improvement in the matter of changes because of ice and snow. However, the hurricane of 1938 took it down rather handily.

About this time the coaxial antenna \(^1\) was announced. We have long adhered to the principle that a high order of vertical directivity is needed at 5 meters. We decided to stack four coxials vertically.


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This is the 8-element array which the present coaxial antenna has replaced, giving as good signal in all horizontal directions as the directive system in its best direction.

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Fig. 1 — The constructional details are shown in this drawing. The cone standoffs are mounted about three inches up inside the sleeve for protection from rain; the inner ends are not fastened to the pipe but simply rest in the corrugations. The long piece of the feed-through insulator should be fastened to the wire at the right point before the wire is pulled through the pipe, so that the lead can be fished through the hole when the inner wire conductor is in place. This must be done before the sheet-metal sleeve is installed on the pipe.

The conductor pipe were "slipped" together to lap 8 inches and fastened with sheet metal screws. Since the spouting is only intended to lap a few inches, special treatment is needed here to get the longer lap which is necessary for good mechanical strength. The diameter of the pipe which is to be the inside member of the lap must be made smaller than normal for the length of the lap. This can be done by placing a thin piece of wood longitudinally in the bottom of the groove and hammering so that the grooves tend to "pinch" together slightly. Treat each groove similarly. The two sections of pipe can be slipped together by holding the inner one firmly and having a helper pound on the opposite end of the outer section, using a block of wood to prevent damage to the hammered end. The lap should be made so that the top section slides over the one below it to keep water out of the inside. A visit to the kitchenware department of the "5 and 10" will provide a cap for the top.

The lower half of each antenna element is a sleeve of galvanized iron 6 inches in diameter and 95\% of 1/4-wavelength long. The top end is slit and bent to fit around the conductor pipe where it is fastened with sheet metal screws and solder as shown in Fig. 2. A coat of roof cement of the asbestos-base variety keeps the inside dry. The bottom of the sleeve is spaced from the pipe by three standoff insulators fastened only to the outer sleeve and resting in the bottoms of the grooves in the pipe. The sleeves are so spaced on the pipe that the element length, bottom of one sleeve to bottom of the next, is 95\% of a half wave.

It is now apparent that we have a Franklin antenna (in phase collinear elements) in which the phase reversing stubs are coaxial instead of spaced, and the stubs are turned up inside the elements.

It is desirable to feed the antenna from the top to insure a maximum of energy in the top elements, since these are the most effective from a radiation standpoint due to their elevation. On
The electrical arrangement of the four-element coaxial antenna. The top element and the third from the top are directly driven. Dimensions in feet can be found by applying the factors given in the drawing to \( f_{\text{Mc}} \). The concentric line may be continued to the transmitter or matched into another line by any of the conventional methods suitable for the purpose.

On the other hand we were told of the excellent isolation of elements produced with coaxial stubs and we wanted some energy in the lower elements. We decided to feed both the top sleeve and the third from the top. Thus the top element is driven directly, while the second from the top can be considered to be excited as an end-fed half-wave element through an inverted quarter-wave stub at the top. The third and fourth sections duplicate the first and second.

Since all the elements are to be fed in phase and these two stubs are approximately one wavelength apart they may both be connected to the line and will be effectively in parallel. The pipe is used for a transmission line of about 220 ohms by stringing a No. 14 wire down its center. The wire is kept central by squares of bakelite panel cut to slide in the grooves of the pipe. These are fastened to the wire at 2-foot intervals by drilling two holes in the bakelite and feeding the wire in one and out the other, as shown in Fig. 2. Care in the use of sheet metal screws must be used to prevent fouling the groove for these spacers; that is, at least one pair of diametrically-opposite grooves must be clear of screws for the entire length of the antenna. The bakelite spacers should be cut slightly small so that they will pass through the laps without binding. In pulling the wire through the pipe, start from the proper end so that there is no danger that the spacers will catch on the edge of the inner pipe at a lap joint. The center wire is attached to the outer sleeve after going through a lead-through insulator in the side of the pipe. The point of feeder attachment to the sleeve is figured for about 440 ohms so the two loads in parallel will match the transmission line of 220 ohms. There is, of course, a slight mismatch on the last section of line, between the two directly-driven elements, but it is not serious.

The photographs show the 8-foot fir sticks used for guy wire insulators to help keep the guys out of the argument. The guys should be attached 2/3 of the way up and at a low-voltage point. The center of the second element from the top was used so there is 11 feet above the guys and 19 feet between the guys and the bottom braces shown in the photograph. The 3-inch pipe will stand a 70 m.p.h. wind before buckling.

Reports on the signal indicate that even though this antenna radiates equally well in all horizontal directions and has only half as many elements as the previously-used 8-element array, the signal strength is as high as that from the directional array on the center of its lobe of maximum radiation.

**Strays**

Minus the time to put up another antenna after a change of location, I hooked the bed-springs to antenna tank coil link coupled to the final. The final loaded up nicely and, with 100-watts input, K6OXJ gave me S7 on 40 in the daytime. Worked several others with good reports.

— W6NCO

**Silent Keys**

It is with deep regret that we record the passing of these amateurs:

- George J. Besnah, ex-W9GB, Appleton, Wis.
- Max Brown, W5FFI, Pine Bluff, Ark.
- Vincent L. Crawford, W5GVB, Texarkana, Ark.
- Clyde A. Gardner, W6KOT, Los Angeles, Calif.
- Wendelin J. Gunther, W9TOD, Des Plaines, III.
- James Lewis Haynie, W5GZE, Texarkana, Ark.
- Sullivan Herring, W5GHE-W4ESI, Clinton, N. C.
- Morris L. Hoag, W6KMA, Ogden, Utah
- Warren F. Jepson, W1NB, Melrose, Mass.
- Paul V. Mayer, W2JGO, West New York, N. J.
- George Robinson, W9MMU, Lombard, Ill.
- A. M. Venne, Jr., W9TCM, Hannibal, Mo.
A Simple Freqmeter-Monitor

Using Low-Drain Tubes for Low Drift

BY H. S. BRITT, W7CQE

The prime requisite for a good frequency meter is stability. However, there is one kind of instability that is very difficult to avoid with the ordinary heater-type tubes, especially when the tube and associated parts are enclosed in a metallic cabinet. This is the frequency drift due to the heat from the tube itself, which manifests itself as a quite rapid drift when the tube is first turned on and then more gradually as the heat is transmitted to other parts, so that the oscillator does not settle down for quite a time. In fact, the statement is made in some articles that, for greatest accuracy, the meter should be left running a half hour before taking readings.

Using a low-drain battery-type tube as an oscillator practically eliminates this drift. The filament power required is so low that the temperature rise of the tube is not noticeable, and the readings may be taken at once. Against this, of course, are the disadvantages of batteries, but in the freq-meter-monitor to be described, these disadvantages are minimized.

Referring to the diagram, there is nothing novel in the circuit itself. The oscillator uses the 1N5G, and filament supply for this tube is obtained from a single dry cell, while the remainder of the power requirements are satisfied by a separate external a.c. power supply. An ordinary dry cell should give something like 1000 hours of service here.

Construction

$L_1$ consists of 36½ turns of No. 22 enameled wire, wound on a 1½" coil form which sets in a separate ceramic socket. The length of winding is 1.4 inches and the cathode tap is 11.4 turns from the ground end. $L_2$ is 11.4 turns of No. 22 d.c., wound over the corresponding part of $L_1$. The grid end of $L_2$ is not taken out through the socket but is terminated at a small machine screw passing through a hole drilled in the form near the upper rim.

$C_1$ is a Centralab ceramic capacitor with a negative temperature coefficient to compensate for changes in temperatures. To determine the necessary coefficient, the meter should be put in operation without the compensator and a series of observations made to determine the change in frequency per degree of temperature change. From this the necessary compensation can be computed. (Data sheets on these capacitors may be obtained from the manufacturers which will give a convenient formula for working this out as well as other information for ordering.) For closest compensation, the capacitor should be ordered to the next even figure above the exact value worked out from the tests, then, if it is found that after putting the compensator in the circuit (as shown by the full lines in the diagram), the meter is over-compensated, the grid terminal of the compensator may be tapped down on the coil a few turns, until by trial the compensation is made as close as desired. These capacitors are very small, actually less than the size of a ¾-watt resistor, and hence are very easy to introduce into the circuit.

$C_4$ is a 35-μfd. variable, controlled by the small knob on the panel to the left of the tuning dial. This condenser's shaft extends about ½ inch back of the rear bearing. A collar on this shaft, held by a long set-screw, forms an adjustable stop, and it is set so that the capacity range of $C_4$ is slightly less than that of $C_3$, the main tuning condenser. When $C_4$ is set against the stop at maximum capacity, $C_3$ tunes over the lower half of the 1.75 and 3.5-Mc. bands, and over all of the other bands. Then by turning the knob against the stop at minimum capacity, the high-frequency part of the broad bands may be covered. By this means the band spread is approximately doubled, with a corresponding increase in

The simple freqmeter is built on a plywood base with aluminum shielding of the frequency-control unit. The knob on the front changes the range of the meter (see text) and the small screw above the knob permits initial setting of the tuning range.
One simple way to reduce the temperature effects in a frequency meter is to work everything near room temperature. The new dry-cell tubes allow this, and W7CQE describes a simple meter using the principle. Temperature compensation takes care of changes in room temperature.

accuracy in reading the tuning dial, and at the same time the meter can be quickly and accurately re-set.

The second movable element of C₄ is a "correction" attachment, for bringing the meter back to a previous calibration and thus compensating for slight changes which may occur over a period of time. It consists of a small plate (about 1 ½ inch square) soldered to one of the stator terminals of C₄. The end of a long screw passing through a hole tapped in the panel approaches this plate. Another small plate has a hole tapped at its center and is screwed on the end of the long screw with a lock nut behind it, to form the other plate of the condenser. A milled nut on the projecting part of the screw provides a means for locking the screw firmly in any desired position.

C₂ is a single bearing condenser, with ceramic insulation, mounted in the upper compartment by means of a bracket or angle fastened to the panel with its shaft vertical and with a slot cut in the end of the shaft so that it may be set by a screwdriver.

The oscillator section of the meter is mounted in an aluminum cabinet. The front panel of this cabinet is 7 inches by 8½ inches high, and the bottom, 6 inches by 6¾ inches wide, is raised 2⅛ inches from the bottom of the panel. The 56 tube and its associated parts are mounted on and under a base formed from a sheet of aluminum 4½ inches by 12 inches, with ends bent down to form 2¾-inch deep sides and top 4½ inches by 6¾ inches. A 2½-inch circular hole in this accommodates the dry cell. This base is located just back of the cabinet but separate from it to avoid heat transmission from the 56, both base and cabinet being fastened to a 7-inch by 11-inch plywood base. The cabinet rests on this base at only three points, to avoid possible distortion effects.

The dial is a 4-inch National Type A with a home-made vernier. No doubt a dial of the precision type would be better, but this one had been in use on another meter, and with a little care it can be read to ½ of a division or closer which, with the spread available, is accurate enough.

Switching arrangements are not shown in the diagram. The receiver output and B supply are brought into the freqmeter-monitor and, in transmitting, a three-pole double-throw switch switches from receiver to monitor, at the same time cutting the oscillator filament and receiver "B" in and out.

The meter is quite insensitive to voltage variations. At 7 Mc. a drop in oscillator filament voltage from 1.50 to 1.25 volts produced no perceptible change in frequency; a drop to 1.15 volts produced a change of about 400 cycles. Dropping the B supply voltage from 265 to 210 volts produced no perceptible change.

From experience so far with this meter, I believe that, with occasional checks from a frequency standard or from a broadcast station, it can be relied on within ½ kc. at 7 Mc., or to within about one part in 15,000. This may be much closer than is really necessary unless one is working very close to the edges, but the ability to measure frequencies to this degree of accuracy is a source of considerable satisfaction at all times and is very much worth while.

The type 1624 beam-power tube recently announced by RCA should be of unusual interest to those contemplating emergency or portable equipment. In characteristics, it is identical to the type 807 used so widely in portable gear, but has a 2.5-volt 2-ampere fast-heating filament which permits quick on-off operation with the possibility of a saving in filament-battery life.

Strays

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**WHAT THE LEAGUE IS DOING**

7-MC. POLL

It will be remembered that in July, at the instance of the A.R.R.L. Board, we took a poll of amateur sentiment on the question of whether the League should endeavor to get 7200-7500 kc. opened to phone work in the event this step was found necessary to enable us to combat foreign broadcast interference. About 82% of the replies favored such a course.


<table>
<thead>
<tr>
<th></th>
<th>Yes</th>
<th>No</th>
</tr>
</thead>
<tbody>
<tr>
<td>U.S.A. and Possessions</td>
<td>6858</td>
<td>81.9%</td>
</tr>
<tr>
<td>Canada</td>
<td>572</td>
<td>84.4%</td>
</tr>
<tr>
<td>Total</td>
<td>7430</td>
<td>82.0%</td>
</tr>
</tbody>
</table>

As we explained in July *QST*, the Board of Directors then proceeded to study these expressions in the light of the actual interference found to exist since September 1st. It was of course just then that Europe’s difficulties began. Whether the war has slowed up the occupancy of these frequencies for broadcasting abroad we don’t know; it seems likely. But at any rate, as every amateur knows, the actual interference situation has not been particularly bad. It may become so later in the winter, in which event the subject will be studied anew. But for the present the A.R.R.L. Board has decided it requires no action.

WASHINGTON NOTES

The minor changes in our regs mentioned last month, including authority for carrier-on operation above 112 Mc., are still pending before F.C.C. . . . Nobody sees how the Stockholm C.C.I.R. meeting can be held and its postponement is expected. However, the inter-American regional conference at Santiago, Chile, in January is still on the docket and preparatory work has begun. The League will be represented there by General Counsel Segal and Secretary Warner.

Recent interference statistics show numerous b.c.l. QR.M complaints caused by 28- and 56-Mc. operation. As much of the work in these bands is done by portable stations which do not have to report their whereabouts, the stations at fault are often hard to locate. The F.C.C. is contemplating extending to 60 Mc. the requirement to report in advance the locations where portable (but not mobile) work will occur.

MEMBERSHIP CONTACT

With the return of the active hamming season the officers of the League and Headquarters staff members have been getting around the country extensively, meeting with and speaking before our affiliated clubs and other membership gatherings. President Woodruff attended meetings in Montana and Washington and was the guest of honor at the Roanoke, Rocky Mountain and Northwestern Division conventions. Vice-President Bailey also attended the Roanoke Convention and, together with Secretary Warner, represented the League at the Hudson Division Convention. Communications Manager Handy found time from the rush of Fall activity to be present at the Vermont State Convention and the New Hampshire Hamfest.

Most of the League’s travel, of course, is to affiliated clubs, and the early Fall has seen a great deal of this type of contact. Assistant Secretary Budlong has just finished an 11,000-mile trip to the Coast and back, during which he attended meetings with fifteen affiliated clubs, visited League members in six additional cities and was present at the Rocky Mountain, Northwestern, the combined Pacific-Southwestern and West Gulf Division conventions; Assistant Secretary Huntoon completed a two-weeks’ trip through Eastern States for a total of nine club sessions, a hamfest, and the Central Division and Wisconsin State conventions; and Assistant Communications Manager Battey is now on a jaunt through the Midwest, which will take him to affiliated-club meetings in fourteen cities and to the Midwest Division and Kansas State conventions.

It’s a busy season!

WWV Schedules

Except for the special broadcasts of WWV using 20 kw, as described below, WWV is now running a continuous schedule (day and night) on 5000 kc. with a power output of 1 kw. This continuous transmission is modulated with the standard pitch in music, 440 cycles per second.

Each Tuesday, Wednesday and Friday (except legal holidays), the National Bureau of Standards station, WWV, transmits with a power of 20 kw. on three carrier frequencies as follows: 10:30 to 11:30 A.M., E.S.T., on 5000 kc.; noon to 1:30 P.M., E.S.T., on 10,000 kc.; 2:30 to 3:30 P.M., E.S.T., on 20,000 kc. The Tuesday and Friday transmissions are unmodulated c.w. except for 1-second standard-time intervals consisting of short pulses with 1000-cycle modulation. On the Wednesday transmissions, the carrier is modulated 30% with a standard audio frequency of 1000 c.p.s. The accuracy of the frequencies of the WWV transmissions is better than 1 part in 5,000,000.
Cathode Modulation

A complete telephone transmitter, including power supply and modulator, capable of delivering a 100%-modulated carrier of 60 watts. The two 6F6 tubes used to modulate the push-pull T20 amplifier can just be seen in back of the tank condenser. The crystal socket is just to the left of the 6V6 oscillator.

Combining Grid and Plate Modulation for Economy and Efficiency

BY FRANK C. JONES, W6AJF* AND FRANK W. EDMONDS, W2DIY**

Cathode modulation is a system of modulation which brings the advantages of high-power telephone operation to a much greater group of amateur operators than has heretofore been possible. By means of this system of modulation it is possible to modulate a high-power Class C amplifier with a surprisingly small amount of audio power, thus appreciably decreasing the size and cost of the modulation equipment.

This system of modulation, as the name implies, impresses the audio signal on the cathode circuit of the Class C stage, as shown in Fig. 1. Since the cathode circuit is common to both the grid and plate circuits of the Class C stage, cathode modulation is thus a combination of plate and grid modulation.

The audio power required for 100% cathode modulation is greater than that required for grid modulation, but considerably less than that needed for plate modulation. Cathode modulation is not attended by the difficulties of adjustment inherent in grid-modulated equipment, nor does it require the abundance of Class C r.f. grid drive necessary for plate modulation.

Whereas a plate-modulated Class C amplifier requires audio power equal to 50% of the Class C d.c. input power, the amount of audio power required for cathode modulation is between 5 and 15% of the d.c. input power, depending on the amplification factor of the Class C tube and on the degree of impedance mismatch between the modulator and cathode impedance. The impedance of the cathode circuit of the modulated stage will appear to be between 300 and 2000 ohms, depending on the characteristics of the tube or tubes. An impedance mismatch of 4 or 6 to 1 has little effect on the character of the modulation but will require the use of slightly more audio power, depending on the degree of mismatch. An average value of 500 ohms will be found satisfactory in most cases, and transformers designed to work into a 500-ohm load may be used for cathode modulation provided that the 500-ohm winding is sufficiently heavy to carry the Class C plate and grid current, and the size of the transformer is sufficient to permit dissipation of the additional heat due to the added iR losses involved. Transformers which are designed to permit a closer match of cathode impedance will, of course, result in greater modulation efficiency and hence less audio power will be required.

The mechanics of cathode modulation are as follows: The instantaneous negative peak voltage impressed on the cathode increases the instantaneous plate voltage, and at the same time decreases the grid bias, both of which factors cause

Any modulation system that requires only about one-fifth the audio power required for plate modulation and still allows the final amplifier to realize between 50 and 60% efficiency would seem to be destined for widespread application. It now appears that cathode modulation—known years ago as “center-tap modulation”—has been hiding its light under a bushel, since it is just such a system. Here’s your chance to get acquainted.
an increase in r.f. output. Similarly, an instantaneous positive voltage will cause a decrease in r.f. output due to a decrease in plate voltage and an increase of bias. Thus the grid and plate modulation is in phase and capable of 100% modulation.

The ratio of grid and plate modulation determines the efficiency at which the Class C stage may be operated. A Class B amplifier which is 100% grid-modulated usually runs at 30 to 35 per cent efficiency with no modulation. A cathode-modulated Class C amplifier can be adjusted to run at 60% efficiency. If the grid modulation is reduced to 70 to 75% of the total, the amplifier may then be adjusted to run at a resting efficiency of 50 to 60%, with resultant higher carrier output. The remaining 25% modulation may then be obtained in the form of plate modulation of the cathode circuit. The 25% plate modulation can be obtained with an audio power of approximately 4% of the d.c. plate input under ideal conditions. The power required for grid modulation of 60 to 70% is approximately equal to 1 to 2% of the d.c. plate input. Therefore, under average conditions, an audio power equal to 10% of the d.c. plate input will be sufficient for 100% cathode modulation.

Low-µ triodes should be used in the cathode-modulated Class C amplifier, since they are somewhat more suitable for grid modulation. Pentodes or tetrodes are not suitable because of their extremely high amplification factor, although triodes with a µ of 20 to 30 may be used with a slight sacrifice of carrier power. Bias may be obtained by means of a grid resistor, although a source of fixed bias voltage is preferable and will give better grid voltage regulation. The bias should be several times cut-off and, if obtained by a grid-leak resistor, the resistance should be several times greater than that used for c.w. or plate-modulated amplifiers. The grid-leak resistance should be bypassed for audio frequencies by a 1/2- to 1-µfd. paper condenser. If too much grid modulation is obtained, part of the grid resistance should be left without by-pass to limit the degree of grid modulation. It is advisable to use a variable grid resistance or variable-voltage bias pack in order to compensate for the varying r.f. drive and antenna loading on different bands, if the transmitter is to be used on more than one band. This is easily accomplished by using a number of resistors in conjunction with a rotary tap switch to cut in the required amount of grid resistance. In adjusting the bias resistance, the resistance should be increased until the monitoring 'scope shows full modulation is being obtained. If the resistance is too low, the carrier will not be fully modulated; if it is too high, over-modulation will result.

Too much r.f. drive will decrease the percentage of modulation obtainable, but will not seriously affect the output. Too little drive will reduce the available carrier and result in under-modulation. The antenna loading should be rather heavy, as is the case with a Class B linear amplifier. Too light loading will result in downward modulation. The Class C stage should be loaded to the point where a further increase in loading causes a decrease in antenna current, for proper operation.

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When the transmitter is properly adjusted, the cathode current will remain very nearly constant under modulation. Some slight change (5%) is not serious, however.

A 100-Watt Transmitter

A representative transmitter, employing cathode modulation, is shown in the photographs. This 100-watt transmitter is indicative of the space economy which may be obtained with a cathode-modulated transmitter. It is mounted on a standard 10” x 28” x 12” chassis which contains the three r.f. stages, two power supplies, and the speech amplifier and modulator.

The r.f. line-up is a 6V6 regenerative crystal oscillator, an 807 buffer, and a push-pull T20 power amplifier. In the audio, a 6SJ7 pentode feeds a 6C5 which is transformer-coupled to the p.p. 6F6 modulators. The modulation transformer is one which has been designed to match several impedances between 300 and 2000 ohms for proper matching to the cathode circuit of the Class C amplifier. The low-voltage supply furnishes power to the speech amplifier and to the oscillator and buffer. The Class C plate power is supplied from the high-voltage power supply at the left-hand end of the chassis. The 6SJ7 was

(Continued on page 102)
The U.H.F. Relay!

Eastern Messages Reach Chicago—W1HDQ-W3DBC Messages
Fastest—A Second U.H.F. Contest To Be Held November 4th-5th

BY F. E. HANDY, W1BDI

To the 56-Mc. adventurers who stuck by their transmitters through thick and thin goes the credit for the success of Number One Relay-and-Field-Day for the u.h.f. bands! A 'box' announcement credits the scores, or individual standings of the fellows who pushed the messages.

The Best Relay Route. East coast points to Chicago — 1000 miles via 56 Mc.!

and who reported the most outstanding number of contacts. Poor conditions were reported from some points, but that was the idea, to prove to the doubters that real communication can be accomplished on u.h.f. day in and day out, with average conditions — no exceptional lucky breaks required. It can.

Dozens of messages were flying about. If there were any disappointed hams, they were the ones that didn’t try to handle any. Credit is due many unreported fellows at isolated points, who like W6FYF—W4GAW—W4ELZ, etc., got on in Georgia, and Oklahoma, and far-flung states. Every district has now been covered by 5 meters. W9ZJB has even "worked all districts" as reported in detail last month. Many isolated fellows conscientiously tried to hear the stations they knew were on for the Relay. Hour after hour these men were on the job, and with a few "filler-in" stations we would have had many additional successful routes to surprisingly diverse sections of the country. Each relay to come should see progress, new routes made, old records shattered.

In this relay the record message, for distance and number of relays, was one started from W2GHV, Dumont, N. J., just a few miles from N. Y. C., which got through to W9VHG, Glenview, Ill., covering over 1000 miles (710 miles airline) between 7:40 P.M. September 9th and 10:37 P.M. September 10th by the following route:

W2GHV-W3BZJ-W3BKB-W3HWN-W8CIR-W8NYD-W8QDU-W8MDA-W8CVQ-W9VHG

A close competitor, was a message started from Wilmington, Delaware, which went 600 airline miles to the same destination, near Chicago:

W3CGV-W3BKB-W3HWN-W8CIR/W8CIR-W8NYD-W8QDU-W8MDA-W8CVQ-W9VHG

8:20 P.M. (9th) to 10:21 P.M. (10th) is good time for that many relays also, about two hours per hop, average. Both these messages were directed to "any west coast amateur." A chain of stations down through Indiana or So. Illinois and through Missouri, would have put these messages to our Oklahoma friends who were alert for any such opportunity.

A distance of 325 airline miles, with answer back, is also something to be proud of, for 56-Mc. performance. It isn’t done every day, though with all the gang on each weekend, it should be possible to keep things lined up by actually running such tests each week. For speed and efficiency we commend the following multi-hop relay to your attention: Addressed to Washington, D. C., this message actually went there, with answer returned! W1HDQ (Wilbraham, Mass.), W1LLL (Hartford), W1UJ (Madison), W2JCR/1 (Fairfield Beach), W1KTF (Stamford), W3FQS (Stony Creek Mills, Pa.), W3CGV (Wilmington), W3DBC (Washington, D. C.). The message was filed at 3:10 P.M. at the start of the relay, got to destination at 9:45 P.M., and the reply by the following route got back at 11:32 P.M.
(7 stns., 2 hrs., 24 mins.).

Other notable message routes:

One from W1JLI to W4DZJ, travelled W1JLI-W1HXP-W1KIK/1-W1HDQ-W1BDI-W1KLL-W1IJJ-W1CLLH-W3AC/3-W3HOH-W3FQS-W3CGV-W3GGR-???

One from W1KIK/1 to "any Florida station," travelled W1KIK/1-W1HDQ-W1LL-W1IJJ-W1CLLH-W3BZJ-W3CTV-W3GGR-???

One from W3FQS "to New Hampshire," travelled W3FQS-W3BZJ-W3AC/3-W1HDQ-W1AU-W1KIK/1-W1KXK (New Market, N. H.) 4:25 p.m., 10th. An answer, giving the time received, returned all the way to W3FQS: W1KXK-W1KIK/1-W1HDQ-W1IJ-W1CLLH-W3AC/3-W3HOH-W3FQS.

One travelled W3AIR-W3AC/3-W1AU-W1KIK/1-W1DEI (destination) W1DEI's message to W3AIR got most of the way OK: W1DEI-W1KLJ-W1IJ-W3AC/3-W3HOH-W3FQS (on hook at end).

A message to Hartford came all the way on "fi": W3NF/3-W3EUA-W3BYF-W3AC/3-W1KLJ-W1LLL-W1INF.

Bridging Gaps

As predicted, some stations set up at high points and mobiles at half-way places, were in a position to render invaluable assistance to the establishment of routes. The notable work of W1KIK/1, Mt. Wachusett; W1HDQ, Wilbraham Mountain, Mass.; W1KJI, Fall Mts., Bristol, Conn.; W8CVQ, Kalamazoo, Mich.; W3BZJ, Glenside, Pa., of W3AC/3, High Point Park, N. J., and the stations in the upper half of the score tabulation is due to the earnest efforts of those operators in organizing relay routes plus their strategic locations in some cases. W8CIR's planning was most noteworthy, since it made the 1000 mile relay success possible.

W8CIR/8 went mobile from Aliquippa to Tuscarora Summit near McConnellsburg in the Southern Central part of Penna. This location was decided upon in an effort to bridge the gap existing in the mountains of Central Penna. W8CIR at Aliquippa, Pa., 20 mi. N.W. of Pgh., Pa. (the home location), was to relay messages to W8SFF in Colver, Pa., near Altoona, an 85-mi. hop thence from Colver to McConnellsburg to mobile W8CIR — 65 mi., and then eastward. W8EUF also went mobile to try and place himself between Colver and McConnellsburg to break the 65-mi. hop between these two points. W8CIR in Aliquippa had no difficulty in giving messages to W8SFF in Colver. However, mobile W8CIR, mobile W8EUO and W8SFF could not hear each other. Mobile W8CIR in McConbrg., however, succeeded in working W3HWN, Harrisburg, Pa., 65 mi., and W3BZJ, Glenside, Pa., 150 mi., and heard W3RL, Herndon, Va., and W3BKB, York, Pa. After three messages for the west were taken from W3HWN conditions became worse with wind and rain. After midnight we decided to pull up stakes and go home, arriving there at 5 a.m. Sunday. Three messages were relayed by "Pony Express" the 150 mi. back to the home station (W8BHY kept vigils there) and then relayed by radio further west!

Equally commendable work was done by many stations. W3BZJ, who sent us 25 message copies,

Scores of Reporting Stations in the UHF Relay and F.D.

<table>
<thead>
<tr>
<th>W3AC/3</th>
<th>W3ETA/3</th>
<th>W1KIK/1</th>
<th>W3NQ</th>
<th>W3BZJ</th>
<th>W1HDQ</th>
<th>W1KLL</th>
<th>W1UJ</th>
<th>W3FQS</th>
<th>W3CH</th>
<th>W3GGR</th>
<th>W8MDA</th>
<th>W8CIR</th>
<th>W1CLL</th>
</tr>
</thead>
<tbody>
<tr>
<td>308</td>
<td>140</td>
<td>100</td>
<td>93</td>
<td>78</td>
<td>77</td>
<td>74</td>
<td>64</td>
<td>59</td>
<td>55</td>
<td>52</td>
<td>51</td>
<td>48</td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>W3FQS</th>
<th>W3CGV</th>
<th>W3GGR</th>
<th>W8MDA</th>
<th>W8CIR</th>
<th>W1CLL</th>
</tr>
</thead>
<tbody>
<tr>
<td>74</td>
<td>64</td>
<td>59</td>
<td>55</td>
<td>52</td>
<td></td>
</tr>
</tbody>
</table>

1 Each station worked counted 1, 2, 5 or 10 points for distances up to 50, 100, 300 miles and over, respectively. One test message originated counted 10 points, a point for receiving, and 2 points for relaying onward any test message. Stations in the field multiplied the sum of all points by two.

November 1939
Coil Chart for Quick Reference

BY L. C. GALLAGHER, W5FRE

When new transmitter tank circuits or tuning circuits for receivers are needed, much pad scratching and searching for formulas may be saved by reference to the handy chart shown on the opposite page. In this chart, the 45-degree diagonal lines — inductance and capacity — may be used with the vertical frequency lines to find the amount of inductance needed for tuning over a required range of frequencies with the capacity available. Once the inductance has been determined, the diagonal line corresponding to this value may be followed through its intersections with the lines for coil dimensions. The result of this step is found in the scale of turns per inch at the top of the chart.

As an example of the use of this chart, suppose that a tuned circuit for the 3.5-megacycle band is needed in the output of a r.f. amplifier using single-section condenser and center-tap grounded coil, and operating with 1250 volts at 100 ma. plate current. Reference to a table of capacity values for use with different plate voltage-current ratios\(^1\) gives a requirement of 80 micro-microfarads capacity for 3.5 megacycles under these conditions.

With the capacity value now determined, the chart on the opposite page is used to find the amount of inductance required for resonance. By following the 3500-ke. vertical line upward (actually, no line is shown at this exact frequency, but an imaginary line between the 3- and 4-megacycle lines is used), the point where it crosses the 80-micro-microfarad capacity diagonal is found. The inductance line passing through this point at a right angle to the capacity line indicates a value of approximately 25 microhenries needed for resonance. Suppose a coil of 2-inch diameter and 2-inch winding length is to be used. Following the 25-microhenry inductance line downward, a point is found where it crosses the line "T" (found in the table at lower right corner of chart to be the line for 2-inch coil). The vertical line to the top of the chart from this point gives a turns-per-inch figure of 13 for the 25-microhenry coil, or a total number of 26 turns for the 2-inch winding length. The line for a coil of 3-inch diameter and 4-inch winding length gives a point on the 25-microhenry line from which 6 turns per inch, or 24 turns total, are found to be required.

Other uses of the chart include determination of required capacity for tuning through a selected frequency range when a coil for the purpose is already available.

---

New Transmitting Tube

The 828 is a beam power tube designed particularly for Class-AB; modulator and a.f. power-amplifier service, but is also useful as an r.f. power amplifier, frequency multiplier, oscillator and grid- or plate-modulated amplifier. Two 828's in Class AB service are capable of delivering 300 watts of audio power with only one percent distortion. Maximum plate dissipation of the 828 for this service is 80 watts. Because of its high power sensitivity, the 828 can be operated in r.f. services to give full power output with very little driving power and, consequently, with a minimum number of driver stages.

Ratings and typical operating conditions are as follows:

<table>
<thead>
<tr>
<th>Rating/Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Filament voltage</td>
<td>10 volts</td>
</tr>
<tr>
<td>Filament current</td>
<td>3.25 ma.</td>
</tr>
<tr>
<td>Transconductance, for plate current of 43 ma.</td>
<td>4500 ohms</td>
</tr>
<tr>
<td>Interelectrode capacities:</td>
<td></td>
</tr>
<tr>
<td>Grid-plate (with external shield)</td>
<td>0.05 µµfd.</td>
</tr>
<tr>
<td>Input</td>
<td>13.8 µµfd.</td>
</tr>
<tr>
<td>Output</td>
<td>14.5 µµfd.</td>
</tr>
</tbody>
</table>

**Push-pull Class-AB, Modulator**

**Typical Operation**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>D.C. plate voltage</td>
<td>1700 volts</td>
</tr>
<tr>
<td>D.C. suppressor voltage</td>
<td>60 volts</td>
</tr>
<tr>
<td>D.C. screen voltage</td>
<td>750 volts</td>
</tr>
<tr>
<td>D.C. grid voltage</td>
<td>-120 ma.</td>
</tr>
<tr>
<td>Peak a.f. grid-to-grid voltage</td>
<td>240 volts</td>
</tr>
<tr>
<td>Zero-sig. d.c. plate current</td>
<td>50 ma.</td>
</tr>
<tr>
<td>Max. sig. d.c. plate current</td>
<td>248 ma.</td>
</tr>
<tr>
<td>D.C. suppressor current</td>
<td>9 ma.</td>
</tr>
<tr>
<td>Zero-sig. screen current</td>
<td>4 ma.</td>
</tr>
<tr>
<td>Max-sig. screen current</td>
<td>43 ma.</td>
</tr>
<tr>
<td>Plate to plate load resistance</td>
<td>16,200 ohms</td>
</tr>
<tr>
<td>Max. sig. power output</td>
<td>18,500 watts</td>
</tr>
<tr>
<td>Max. sig. power output</td>
<td>300 watts</td>
</tr>
</tbody>
</table>

**Plate-Modulated Class-C Telegraphy**

**Typical Operation**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>D.C. plate voltage</td>
<td>1000 volts</td>
</tr>
<tr>
<td>D.C. suppressor voltage</td>
<td>75 volts</td>
</tr>
<tr>
<td>D.C. screen voltage</td>
<td>400 volts</td>
</tr>
<tr>
<td>Screen resistor</td>
<td>26,000 ohms</td>
</tr>
<tr>
<td>Grid leak resistor</td>
<td>14,000 ohms</td>
</tr>
<tr>
<td>Peak r.f. grid voltage</td>
<td>230 volts</td>
</tr>
<tr>
<td>D.C. plate current</td>
<td>156 ma.</td>
</tr>
<tr>
<td>D.C. suppressor current</td>
<td>15 ma.</td>
</tr>
<tr>
<td>D.C. screen current</td>
<td>23 ma.</td>
</tr>
<tr>
<td>D.C. grid current approx.</td>
<td>10 ma.</td>
</tr>
<tr>
<td>Driving power approx.</td>
<td>2.1 watts</td>
</tr>
<tr>
<td>Power output approx.</td>
<td>100 watts</td>
</tr>
</tbody>
</table>

**Class-C Telegraphy**

**Typical Operation**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>D.C. plate voltage</td>
<td>1250 volts</td>
</tr>
<tr>
<td>D.C. suppressor voltage</td>
<td>75 volts</td>
</tr>
<tr>
<td>D.C. screen voltage</td>
<td>400 volts</td>
</tr>
<tr>
<td>D.C. grid voltage: From a fixed supply</td>
<td>-95 volts</td>
</tr>
<tr>
<td>From a grid resistor</td>
<td>7900 ohms</td>
</tr>
<tr>
<td>From a cathode resistor</td>
<td>415 ohms</td>
</tr>
<tr>
<td>Peak r.f. grid voltage</td>
<td>195 µµhos</td>
</tr>
<tr>
<td>D.C. plate current</td>
<td>180 ma.</td>
</tr>
<tr>
<td>D.C. suppressor current</td>
<td>22 ma.</td>
</tr>
<tr>
<td>D.C. screen current</td>
<td>35 ma.</td>
</tr>
<tr>
<td>D.C. grid current approx.</td>
<td>12 ma.</td>
</tr>
<tr>
<td>Driving power approx.</td>
<td>2.2 watts</td>
</tr>
<tr>
<td>Power output approx.</td>
<td>150 watts</td>
</tr>
</tbody>
</table>

---

*1508 So. Travis St., Sherman, Texas.

\(^1\) Fig. 825, *Radio Amateur's Handbook*, 1939 edition.
THE Naval Communication Reserve of the Sixth Naval District comprises units in Georgia, South Carolina, and North Carolina. Each of these states is represented by a section of the district organization and each state section in turn is made up of the several units of the Naval Communication Reserve in the respective state. The three sections are coordinated under the command of the Naval Communication Reserve, Sixth District Commander in Charlotte, N. C., and here the staff of the Naval Communication Reserve Commander is also located for the administration of the organization of the Sixth District.

All activities are directed from the staff headquarters at the Municipal Armory in Charlotte, and the only dependence placed upon the headquarters of the Sixth Naval District at this part of the country at their head. This organization comprises various units having headquarters in Savannah, Charlotte, Charleston, and Wilmington. The Sixth Naval District, as the headquarters of the Naval Communication Reserve, has its headquarters in the Municipal Armory in Charlotte. All drill schedules, training programs, courses of instruction, and material instruction are instituted by the staff headquarters in Charlotte. All activities are directed from the staff headquarters at the Municipal Armory in Charlotte, and the only dependence placed upon the headquarters of the Sixth Naval District at this part of the country at their head.

During the last year the Naval Communication Reserve of the Sixth District demonstrated its efficiency in time of local emergencies when a tornado hop-skipped in and about the city of Charleston in September. In addition to demolishing many historic buildings and leaving a heavy death toll in its wake, the "twister" made a complete job of putting down all telephone and telegraph lines connecting Charleston to the outside world. With all local power off for about 12 hours, and not available in some parts of the city for almost a week, Unit Five of Section One in Charleston was on the air to attend the regular Naval Communication Reserve drill ten hours after the tornado struck the city. Prior to checking in on the drill W4DFC had already been on the air for a couple of hours handling distress traffic, and after the drill his rig handled a good-sized load of personal distress messages until the wee small hours of the morning when the telephone and telegraph lines were partially restored. The emergency demonstrated the alertness of the Naval Communication Reserve to function under adverse conditions, and gave ample evidence of the new initiative spirit which promises to put the Naval Communication Reserve of the Sixth District up at the head of the other districts during the competition.

Another old-timer who is a regular caller on the ham bands and is still so enthusiastic with the Navy as to give up many a night for the administration of the units in North Carolina is W4BRT. Across the state line to the south is W4CE, another Section Commander who works for another Federal Government agency during the daytime and then spends his evenings in administering to the needs of the Naval Communication Reserve in South Carolina. No less a personage than the Federal Inspector himself looks out for the newest unit in Savannah. Over 30% of the members of the organization in this district have ham tickets, and the elementary instruction given in the various units has resulted in an increasing number of applications for amateur licenses.

A cursory glance at a call book will show a noticeable scarcity of hams in the Carolinas and Georgia. The recruiting problem, therefore, to fill the Reserve ranks with licensed amateurs has been a difficult one for the past several years. During 1938-39, however, this enlistment situation has been ameliorated by recruiting a number of young men who have utilized the instruction programs during regular Naval Communication Reserve weekly drills as a means toward qualifying for a ham ticket. At the same time such training for Navy operating has progressed from the fundamentals of Navy procedure on up to the point where the men are well qualified as watch standers by the time they obtain their amateur "tickets."

During the past year the Naval Communication Reserve of the Sixth District demonstrated its efficiency in time of local emergencies when a tornado hop-skipped in and about the city of Charleston in September. In addition to demolishing many historic buildings and leaving a heavy death toll in its wake, the "twister" made a complete job of putting down all telephone and telegraph lines connecting Charleston to the outside world. With all local power off for about 12 hours, and not available in some parts of the city for almost a week, Unit Five of Section One in Charleston was on the air to attend the regular Naval Communication Reserve drill ten hours after the tornado struck the city. Prior to checking in on the drill W4DFC had already been on the air for a couple of hours handling distress traffic, and after the drill his rig handled a good-sized load of personal distress messages until the wee small hours of the morning when the telephone and telegraph lines were partially restored. The emergency demonstrated the alertness of the Naval Communication Reserve to function under adverse conditions, and gave ample evidence of the new initiative spirit which promises to put the Naval Communication Reserve of the Sixth District up at the head of the other districts during the competition.

SWITCH TO SAFETY! QST for
Don't Miss the Tenth A.R.R.L. Sweepstakes

Nov. 11th-12th, 18th-19th—Awards to Section Leaders—Also CW and 'Phone Certificate in Each Club—Gavel to Winning Club—Use 'Phone or CW. Any Ham Band(s)

F. E. Handy* WIBDI

You can work more than 20 hours on one of the two 33-hour week-ends, but in no case will any entry more than 40 hours total operating in the two contest periods be accepted. Use any amateur frequency bands you choose. This timing plan permits the average ham to plan for his time for meals, for 8 hours' daily sleep, etc. Cross examination of logs makes it possible to check operating time. Every amateur active in any A.R.R.L. field organization section is cordially invited to take part.

Contest exchanges can be logged directly on the sheet that you send Hq. for a report. Paper work set forth for these things in handbook. Mimeographed contest forms will be sent gratis to anyone who sends a radiogram or drops a card for the same. Use of our sheets is not required nor is advance entry necessary. The purpose is to help participants keep a uniform log. Follow the arrangement or form shown with this announcement. Draw your own columns on your own paper if you like ... or ask us for a form.

In the annual "SS" telegraphing operators will contest and compete with other telegraphing operators. "Phone hams will compete with other "phone hams.

Many complete their QSL-card records and achieve "WAS" through each year's "SS." This is the best chance of the year to progress toward that objective.

The contest is to work as many stations as possible. The points from such work will be multiplied by the number of different A.R.R.L. Sections worked with at least a complete one-way exchange in the contest. All essential contest information is sent in the form of a standard preamble. Exchanges are for the record sent to Hq. New hams may also add to their knowledge of the way preambles to A.R.R.L. messages are sent and acknowledged, and files requested, accuracy of 'phone communication assured, etc., if they take part and follow the standard practices set forth for these things in The Radio Amateur's Handbook. Some emergencies of late years have found amateurs unfamiliar with good operating practices, resulting in delays, garbles, and inaccurate writing or taking a message in standard form. The "SS" builds operating keenness at the same time new station records are made. It's operating fun.

The new award for winners this year is a beauty. In addition to its utility (a chromium pin and tie holder) a neat, diamond-shaped charm is attached. On this diamond will be inscribed the personal and individual call designation of each winner. The c.w. winner, and the radiotelephone winner, for each A.R.R.L. Section will receive recognition through this award (see page 10).

The General Call
"CQ SS CQ SS CQ SS de W ... W ... W ..." is used by stations looking for contacts in the Sweepstakes. A single, snappy CQ SS will bring results!

---

THE CONTEST PERIOD

<table>
<thead>
<tr>
<th>Time</th>
<th>Start</th>
<th>Ends</th>
</tr>
</thead>
<tbody>
<tr>
<td>A.S.T.</td>
<td>Nov. 11 &amp; 18, 7:00 P.M.</td>
<td>Nov. 13 &amp; 20, 4:01 A.M.</td>
</tr>
<tr>
<td>E.S.T.</td>
<td>Nov. 11 &amp; 18, 8:00 P.M.</td>
<td>Nov. 13 &amp; 20, 5:01 A.M.</td>
</tr>
<tr>
<td>C.S.T.</td>
<td>Nov. 11 &amp; 18, 9:00 P.M.</td>
<td>Nov. 13 &amp; 20, 6:01 A.M.</td>
</tr>
<tr>
<td>M.S.T.</td>
<td>Nov. 11 &amp; 18, 4:00 P.M.</td>
<td>Nov. 15 &amp; 20, 1:01 A.M.</td>
</tr>
<tr>
<td>P.S.T.</td>
<td>Nov. 11 &amp; 18, 3:00 P.M.</td>
<td>Nov. 13 &amp; 20, 12:01 A.M.</td>
</tr>
</tbody>
</table>

Proof or QSO

At least one way complete six part exchange must be completed and acknowledged between two stations as "proof of QSO" before points or Sections can be claimed.

It is not essential that each station worked be taking part in the contest to make your points count. Any operator who needs information can be referred to this announcement. First, ask the operator to take your preamble and come through with like information in preamble form.

Power Factor and Scores

If the power input to the final stage (plate current times plate voltage — $E \times I$) is:

<table>
<thead>
<tr>
<th>Power Factor</th>
<th>Scores</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>100</td>
</tr>
<tr>
<td>2</td>
<td>200</td>
</tr>
<tr>
<td>3</td>
<td>300</td>
</tr>
</tbody>
</table>

* Communications Manager, A.R.R.L.

1 Including Cuba, Porto Rico, Hawaii, Alaska, P. L., etc.

2 See the complete list of the 71 Sections in the A.R.R.L. field organization, page 6 of this issue of QST.

November 1939
(a) Up to and including 100 watts — multiply score by 1.25.
(b) Over 100 watts — multiply score by 1.

Operating in both low- and high-power classes at different times is still permitted, but scoring rules do not permit Sections worked on high power to be used in the low-power classification. Points of some kind are credited for every QSO with a bona fide exchange, whether the station worked is a leading "SS" man or a ham outside the contest. If one breaks his power class, however, the Total Score is the sum of scores separately computed for each power class and added.

Scoring system in brief:

All contacts:
One point for each QSO when "receipt" is completed for an exchange one way.
Two points for each QSO when the required information is exchanged both ways.

For final score:
Multiply totaled points by the number of different A.R.R.L. Sections worked, that is, the number in which at least one bona fide S.S. point or exchange has been made.
Multiply this by 1.25 if you used 100 watts or less for transmitter input.

Additional Rules
1. Information in contest exchanges (six parts) must be sent in the order indicated, that of the A.R.R.L. message preamble. Incomplete exchanges or wrong order of sending justifies disqualification.
2. Entries should be (a) in the low-power class, or (b) high-power class, or submitted as the sum of separately computed work at one station falling in each class. Sections worked on high power do not count in the multiplier for low-power-score and vice versa. Logs must show the power used for each QSO or for groups of QSOs.
3. If the power was changed between (a) or (b) during the contest, separate scores must be kept for each power class, and the two added together for the total.

STATION W... SUMMARY OF EXCHANGES 10TH A.R.R.L. ALL-SECTION SWEEPSTAKES

<table>
<thead>
<tr>
<th>Band (mc.)</th>
<th>Time On or Off</th>
<th>NR.</th>
<th>SENT (1 point)</th>
<th>Time</th>
<th>RECEIVED (1 point)</th>
<th>Number of each Different New Section or Wk'd</th>
<th>Points</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.5</td>
<td>On 6:10 P.M.</td>
<td>1</td>
<td>WIAW 579</td>
<td>6:15</td>
<td>3 WIGME 650</td>
<td>Middlebury, Conn. 6:18 P.M. 12 1 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>2</td>
<td>489 W. Hartford, Conn. 6:26</td>
<td>6:18</td>
<td>7 WATEM 479</td>
<td>New Haven, Conn. 6:29 P.M. 12 1 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>3</td>
<td>587 W. Hartford, Conn. 6:40</td>
<td>6:29</td>
<td>2 W3BEZ 389</td>
<td>Chevy Chase, D.C. 6:45 P.M. 12 1 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>4</td>
<td>489 W. Hartford, Conn. 6:18</td>
<td>6:30</td>
<td>3 WSBEN 509</td>
<td>Rochester, N. Y. 6:31 P.M. 12 1 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>5</td>
<td>578 W. Hartford, Conn. 6:30</td>
<td>6:30</td>
<td>7 WTSV 589</td>
<td>Chicago, Ill. 1:15 A.M. 12 1 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>Off 3:00 A.M.</td>
<td>6</td>
<td>519 W. Hartford, Conn. 2:59</td>
<td>12</td>
<td>15 W9VEF 479</td>
<td>Minneapolis, So. Minn. 2:55 A.M. 13 5 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>7</td>
<td>WIAW 579</td>
<td>6:15</td>
<td>15 W8W5 479</td>
<td>Buriton, La. 1:05 P.M. 20 6 1</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>8</td>
<td>588 W. Hartford, Conn. 6:00</td>
<td>2:15</td>
<td>17 W5BDI 450</td>
<td>Houston, So. Tex. 2:20 P.M. 20 7 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>9</td>
<td>578 W. Hartford, Conn. 4:06</td>
<td>20</td>
<td>11 WIEWD 580</td>
<td>New Britain, Conn. 2:55 P.M. 20 1 2</td>
<td></td>
</tr>
<tr>
<td>(W5WG)</td>
<td>Off 3:00 A.M.</td>
<td>10</td>
<td>WIAW 347</td>
<td>6:30</td>
<td>16 WSMVK 439</td>
<td>Modesto, S. J. V. 4:31 P.M. 20 8 2</td>
<td></td>
</tr>
<tr>
<td>&quot;</td>
<td>&quot;</td>
<td>11</td>
<td>479 W. Hartford, Conn. 6:10</td>
<td>20</td>
<td>9 W4HT 579</td>
<td>Wheaton, III. 5:15 P.M. 20 8 2</td>
<td></td>
</tr>
</tbody>
</table>

Total: 22 points

Number and name of operators having a share in above work: W. Hartford, Conn.

I hereby state that in this contest I have not operated my transmitter outside any of the frequency bands specified on my station license, and also that the score and points set forth in the above summary are correct and true.

Signature

My Tube Line-Up

Number Different Stations Worked

Address

QST for
EXPLAINING CONTEST EXCHANGES

<table>
<thead>
<tr>
<th>Send</th>
<th>Like Std. Msg. Preamble</th>
<th>NR</th>
<th>Call</th>
<th>CK</th>
<th>Place</th>
<th>Time</th>
<th>Date</th>
</tr>
</thead>
<tbody>
<tr>
<td>In the “SS” Ex-</td>
<td>Number contest info, sent consecutively, 1, 2, 3, etc., a new nr. for each station worked</td>
<td>Send your own call</td>
<td>CK in RST report of station worked</td>
<td>Your city and Section</td>
<td>Send time of transmitting this “NR”</td>
<td>Send date of QSO</td>
<td></td>
</tr>
</tbody>
</table>

Purpose........ The QSO-nr tells how you are doing; aids HQ, checking | Identification | All stations exchange complete reports | The A.R.R.L. Section is vital contest data | Time and date must check in both logs and fall within the contest period to prove each point claimed

---

3. Reports must show operating time for each period spent on the air in the “SS,” and the total of such operating time.
4. Logs must be marked for “phone” or “C.W.” entry, grouping all work by either method together as one score.
5. All work must fall in the contest period.
6. Decisions of the award committee of C.D. staff members shall be accepted as final.
7. Reports must be received at A.R.R.L. Hq. from all stations except those in Alaska, Hawaii, and P. I. on or before noon, Dec. 22, 1939, to be considered for certificate awards. From outlying points, reports must similarly be received on or before Jan. 19, 1940.

Club Participation
Certificate awards (besides the ‘phone and telegraph Section awards) will be made through each club where three or more individual club members, or new hams invited and reported by such a club, in addition to sending a contest report have their club secretary write Hq., listing their individual calls and scores, and the total of such scores. Only the aggregate of scores confirmed by receipt here of Contest Logs shall count for the club. If there are both ‘phone and c.w. entries, A.R.R.L. will provide two certificate awards for the club to give its leading members. The sum of the scores of all club participants (‘phone and c.w.) confirmed by logs will be added by the secretary, to count for the club.

A genuine gavel, with engraved sterling silver band, is offered as an award to club whose officers or activities manager submits the greatest collective score from “SS” logs. Club members must send in full reports either direct or through the secretary to substantiate the club’s claim on the gavel award! A chance to win honors for your club and a valuable trophy for the club’s presiding officer to use at meetings!

Competition comes only from operators in one’s immediate Section. Awards are for the operator running up the best DX condition and operating opportunity. Fullest operating enjoyment is assured. See May QST for full details on the latest contest to avoid delay and insure that your results are credited and known through QST.

Support claims made in logs from other stations and receive credit in QST.

The highest individually-attained score of any one of the operators of amateur stations having more than one operator is the official score for such a station. The summary of scores must show all stations worked by all operators however, circling the entries of stations and/or Sections that cannot count in the official total. Awards will be based on the official total and will be made to the individual operator accredited with this total. To show the possible scores that can be built up by several operators at one station, such scores (all Sections listed by all points listed) may be shown parenthetically after the “official” score that counts toward a possible award.

---

**To A.R.R.L., West Hartford, Conn. as soon as the contest is over. Use the log form shown in the example.**

**All hams are requested to submit lists, even if they only show a small score, on a postal. By doing this they help list all operators whose work at your station is responsible for any part of the score.**

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**November 1939**
Pointers on Design and Adjustment of High-Efficiency Grid-Modulated Amplifiers

Experimental Transmitters Using the Terman-Woodyard System

BY CHARLEY W. WINKLER,* W9AKC

The high-efficiency grid-modulated amplifier realizes the high efficiency of plate modulation while still retaining the chief advantage of grid modulation — low audio power requirements. This type of amplifier can provide a carrier output approaching that obtainable in a Class-C amplifier plate modulated, and the initial cost of the equipment is low compared to the first cost of a plate-modulated transmitter.

The high-efficiency grid-modulated amplifier is similar in some respects to the Doherty high-efficiency linear amplifier, the principal difference being in the way modulation is applied. The Doherty amplifier is driven by a wave already modulated, while the audio signal is applied directly to the amplifier in the grid-modulation system. Another difference exists, however, which makes the high-efficiency grid-modulated-amplifier much more practical for the use of the amateur. Terman and Woodyard have developed a tuning method, and have shown the mathematical derivation for it, which greatly simplifies the problem of adjustment. The tuning of the high-efficiency grid-modulated amplifier is done by using only the conventional grid and plate meters to show correct adjustment.

The Plate Circuit

The most difficult adjustment to be made is that of the plate phasing network. We can visualize this part of the circuit quite easily, however, since it is similar to the pi-section matching network that amateurs have used for a long time to couple the output of a transmitter to an antenna (Fig. 1). The network is used in this application to provide impedance inversion. Consider a network of $X$ ohms characteristic impedance, terminated in resistance of $R$ ohms equal to $X$. The sending-end impedance will then be equal to $R$ ohms. If the terminating resistance is changed to $R/2$ ohms the sending end impedance will be $2R$ ohms. The phase through the network of Fig. 1-A will be retarded 90 degrees while that of Fig. 1-B will be advanced 90 degrees, and this phase shift will not be dependent upon the value of $R$. The sending end impedance is given by the relation

$$Z = -\frac{X^2}{R}$$

The inductive reactance of the phasing coil in the elementary circuit, Fig. 2, is made equal to the impedance the tube should look into as a Class-C amplifier when working at peak level (100% modulation conditions). This value is determined from the allowable plate dissipation, filament emission, and permissible direct plate voltage. The value of plate dissipation during

* Supervisor, KFAB Transmitter; 3811 J Street, Lincoln, Neb.


A top view of the experimental amplifier using HF-100's. The plate phasing coil projects through the baffle shield between the two stages. Amplifier tank coils are mounted on top of their respective condensers. The shield cans contain the grid coils.
modulation can be made somewhat higher than for Class-C telegraph conditions because the tube is operating at peak level only a small period of time. The value of direct plate voltage may be made higher than for plate modulation because the tube is not subjected to the voltages, on peaks of modulation, that it would encounter in plate modulation.

Operating Conditions

The following method can be used to obtain the general operating conditions. Assume that we want a total carrier equal to that which we would have by using two tubes, say, HF-100's, in a plate-modulated Class-C amplifier. The manufacturer's rating for one HF-100 plate modulated is 105 watts output. The c.w. telegraph rating, however, is 170 watts, so by permitting a small overload we may choose a total carrier power of 200 watts as the desired output from a high-efficiency grid-modulated amplifier. This as:

The particular operating conditions discussed here have the tube manufacturer's sanction, since the maximum plate current subsequently found is within the capabilities of the tube, while the average plate dissipation is very little, if any, above normal. The factors to be considered in determining the permissible power output from any of tube are the plate dissipation under modulation conditions, and the total emission of the filament. The peak demand on filament emission will depend upon the operating angle and the grid characteristics. A tube should be capable of a carrier output of twice its normal plate-modulated rating provided the increased output can be obtained without exceeding the maximum permissible plate dissipation. This requires fairly high plate efficiency, depending upon how the tube originally was rated. Demands on filament emission will be lessened by obtaining the increased input largely by an increase of plate voltage, rather than by increased plate current.

Experience in building and adjusting two 20-meter 'phone transmitters using the high-efficiency grid-modulated amplifier of Terman and Woodyard has given the author a practical background which makes the information contained in this article of real value. A careful reading will help in estimating the relative merits of the system, for particular ham problems, as compared to conventional plate modulation.
The value of plate current for carrier conditions is half the maximum value of 356, or 178 ma. This value of plate current will give a plate loss at carrier level which is less than rated plate dissipation. The carrier input is 175 x 1500, or 267 watts, which less the output of 200 watts, gives a plate loss of 67 watts.

If the plate loss were strictly limited to 75 watts and it were necessary to modulate continuously at 100% with a sine wave, the above values would be too high and a new value for carrier output would have to be used which would give a plate loss, under modulation, not exceeding the rating of the tube. It is permissible to use the tube under the conditions given above because average percentage of modulation over a period of time is considerably less than 100%.

Circuit Operation

Tank circuits 1 and 2 are detuned from resonance to provide a capacitive reactance equal to the reactance of the phasing coil. This detuning on 14 Mc. is very slight, being only a few µfd. for impedances from 2000 to 5000 ohms. The design of these tank circuits should take this into consideration, so that a reasonable variation of the tank condenser capacity can be secured before reaching either the maximum or minimum setting.

The two tank circuits provide the capacitive reactance are secured by detuning the tanks.

\[ P_0 \left(1 - \frac{1}{8} \frac{M}{S} - \frac{M^2}{4} \right) \]

where \( P_0 \) is the carrier output, \( e \) is the efficiency and \( M \) the modulation factor. For 75% efficiency and 100% modulation the plate loss is

\[ 200 \left(1 - 0.75 \frac{1}{0.75} + \frac{1}{\pi} - \frac{1}{4} \right) = 80 \text{ watts} \]

Fig. 2 — Essentials of practical circuits to produce the effect of the quarter-wave matching sections of Fig. 1. The tank reactances are secured by detuning the tanks.

Fig. 3 — Circuit diagram of an experimental transmitter using 807's. The carrier output secured was approximately 50 watts.

- \( C_0 \) — 3-6 µfd. midget variable.
- \( C_1 \) — 0.001-µfd. mica, 500-volt.
- \( C_2 \) — 100-µfd. mica, 500-volt.
- \( L \) — 36 turns No. 17 s.c.w. on 1½-inch form, close-wound. Conventional tank circuits are used.

- \( R_1 \) — 3000 ohms, 1-watt.
- \( R_2 \) — 35,000 ohms, 20-watt.
- \( R_3 \) — 10,000 ohms, 1-watt.
- \( R_4 \) — 90,000 ohms, 1-watt.
reactance which with the coil make up the quarter-wave line. Tube No. 1 is located at the sending end of the line and tube No. 2 at the terminating end. The resulting action of the combination is such that under carrier conditions tube No. 1 looks into an impedance of \(2R\) ohms, with the network of characteristic impedance \(X\) (equal to \(R\) ohms) terminated in \(R/2\) ohms. As modulation is applied, tube No. 1 looks into a gradually lowering impedance reaching the value of \(R\) at the up-peak of 100% modulation. The terminating impedance of the network consists of tank No. 2, loaded by the antenna or any useful load, with tube No. 2 in parallel. The effect here is that of a negative resistance shunted across the tank circuit, and as the power delivered by tube No. 2 increases, the terminating resistance also increases, thus causing the sending-end impedance to decrease. Modulating voltages are applied to tube No. 1 to lower its internal resistance so that as its load impedance decreases it can supply additional current to the load. At 100% modulation tube No. 1 is supplying twice carrier level at no increase of r.f. voltage (this was already at maximum under carrier conditions) so the increase in output is effected because of the increase of output current.

### Adjustment

The method of adjusting the plate phasing network as suggested by Terman and Woodyard is to place a load resistance of \(R/2\) ohms across tank No. 2 (with the filament of tube No. 2 disconnected but with this tube in its socket so that its capacitance will be present) with reduced plate voltage, normal excitation and normal bias on tube No. 1. Under these conditions the condenser of tank No. 1 is adjusted for minimum plate current and the condenser of tank No. 2 adjusted for maximum plate current on tube No. 1. The setting for \(C_1\) will be dependent upon the setting of \(C_2\) in much the same manner as the two condensers in a pi matching network are dependent upon each other. The correct conditions are achieved when any further adjustment of \(C_2\) will produce no further rise in plate current and the adjustment of \(C_1\) will produce no further decrease in plate current.

This procedure gives correct adjustment of the network but does not insure that it is of the correct characteristic impedance. To adjust for the correct value of impedance disconnect the phasing coil and place a resistance of \(2R\) across tank No. 1, which is tuned for minimum plate current with

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\(C_0 = 3.6 \mu\text{fd.}, \text{midget variable.}\)  
\(C_1 = 50-\mu\text{fd. (total) split stator, 0.07'' air-gap (Cardwell MT-100-Gd).}\)  
\(C_2 = 100-\mu\text{fd. mica, 1000-volt.}\)  
\(C_3 = 0.001-\mu\text{fd. mica, 2500-volt.}\)  
\(C_4 = \text{Neutralizing condenser, 10 } \mu\text{fd. max.}\)  
\(C_5 = 1-\mu\text{fd. paper (audio coupling).}\)  
\(C_6 = 50-\mu\text{fd. transmitting midget.}\)  
\(C_7 = 0.01 \mu\text{fd.}\)  
\(R = 10,000 \text{ ohms, 10-watt.}\)  
\(L = 30 \text{ turns No. 17 e.e.c close-wound on 11/8-inch form}\)  
\(L_4 = 12 \text{ turns No. 12, diameter 11/4 inches.}\)  
\(L_2 = 8 \text{ turns on 13/4-inch form.}\)  

Note: Inductance of tank coils adjusted (by varying turn spacing) to resonate at mid-scale on tank condensers.

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**Fig. 4** — Circuit of the transmitter using HF-100's.

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**November 1939**
While the idea of ganging a variable inductance and variable condenser is not new to the art, nothing much seems to have been done about applying it to ham transmitters. Here’s some dope on the performance of an experimental ganged unit which has given a good account of itself.

The variable-inductance coil ganged with the tuning condenser in the plate tank circuit of an experimental amplifier using RK-51’s at an input of 450 watts.

**Constant L/C Ratio; Switch-less Three-Band Tuning**

A Single-Control Wide-Range Tank Circuit

BY T. M. FERRILL, JR.* W1LJJ

Plug-in coils for transmitter tanks are marked not only by good efficiency and moderate cost, but also the inconvenience of external coils and the bother of getting into various stages of the transmitter to remove and replace them. Also, a full set of plug-in coils sometimes proves to be much more expensive than the associated tuning condenser.

Second in popularity to the plug-in coil tanks are those incorporating front-panel controlled turns-shorting switches. While a marked advance in operating convenience is provided by tanks of this type; efficiency, low stray capacities, circuit balance, and simplicity of loading are likely to be sacrificed.

In the ganged coil-and-condenser tuner shown at the left in the accompanying photograph, the shaft of a split-stator plate tuning condenser is mechanically coupled to the rotor coil of a unit somewhat resembling the old variometers. In contrast to the variometers used for early receiver and transmitter tuning, however, the number of turns on the rotor is less than half that of the stator section. In spite of the small number of rotated turns, an inductance range greater than 4 to 1 is provided by the variable inductance coil, so that with a condenser having an equivalent effective maximum-minimum capacity ratio a four-to-one frequency range can be covered.

In practical operation this combination of coil and condenser on a single tuning shaft has been highly satisfactory. It was expected at first that the variable inductance would reduce the plate tank efficiency, but actual tests indicated a high order of efficiency throughout the tuning range. Minimum plate current on the 1.75-, 3.5- and 7-Mc. bands with 1200 volts applied to the plates of the push-pull amplifier at constant rated grid excitation gave a minimum (unloaded) plate current of 20 ma. on each of the three bands.

The minimum plate current of an unloaded r.f. stage with fixed excitation, bias, and plate voltage serves as a good practical criterion of comparative tank-circuit efficiency, with high minimum current values usually indicating low tank efficiency, provided the comparisons are made between tanks having the same L/C ratio.

**Loading**

It was anticipated that a link output coil having the correct number of turns for loading on one band, with a fixed non-inductive load, would provide reasonably constant loading throughout the entire tuning range — that is, loading varying perhaps from 200 ma. to 300 ma. in a stage normally designed for 250-ma. plate current. Here again expectations were exceeded and the current values were found to vary only from 210 ma. to 250 ma.

This characteristic is an important one, since a single link coil may be wound on the final-amplifier tank coil to match similar transmission lines used for three antennas, with correct amplifier loading being provided automatically at the frequencies of the three antennas. Further-
more, with tanks of this type used for grid and plate circuits of link-coupled stages, one adjustment of the coupling turns at the grid and plate coils should serve for proper loading and excitation on three bands.

**Uniform L/C Ratio**

The mechanically-coupled coil and condenser system is inherently well suited to design of a tank with fairly constant L/C ratio. Capacity variation of most transmitter tuning condensers is almost linear with rotation, the greatest departure from linearity occurring at the very minimum-capacity end of the tuning range. Although the inductance variation is not linear, it is sufficiently near a straight line to hold the L/C ratio within close limits throughout the tuning range. Actually, the coils of the variable inductance could be proportioned for greater variation of inductance than of capacitance, or the reverse. The nearly constant ratio, however, is a very desirable feature. The constants given work out to a tank Q of 6 for the amplifier with which the tank is used.

**Balanced or Unbalanced**

The tank used in the plate circuit of the transmitter in the photograph is well balanced at all settings of the rotating coil. Neutralization remains fixed throughout the entire tuning range. The inductance unit used in this r.f. amplifier is suited also to use in a single-ended or unbalanced tank circuit, such as the usual plate tank arrangement for an r.f. pentode or beam-power tube. In such a single-ended tank, the connection to the center of the rotated coil would of course, be omitted.

**Construction**

Outer and inner coils of the variable inductance are "air-wound." Specifications are given in Fig. 2. A ¼-inch diameter bakelite shaft is passed through small semi-circular bends in the center turns of the coils. The shaft is supported and centered by the turns of the outer coil, and the turns of the inner coil rest on it, giving a pressure bearing for rotation of the inner coil. Connections between the center divided turn of the outer coil and the ends of the rotor are made by means of two pigtail connections running along the condenser end of the bakelite shaft. A third pigtail connection from the center of the rotor is carried through the back of the assembly for d.c. supply. This, of course, is a brief description of a unit built simply for experiments. More rigid and dependable construction for the rotating assembly is considered highly desirable for mechanical permanence, and readily could be devised.

The link coil is wound in usual fashion around the middle of the tank coil. Coupling is tightened or loosened by increasing or decreasing the number of turns in the link winding. For use in unbalanced circuits, with one end of the tank coil operated at ground r.f. potential, the link turns should be wound near the "ground" end of the coil rather than at the center. If a considerable amount of metal is used in the rotating mech-

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*Fig. 1 — As these drawings clearly show, the circuit arrangement is perfectly orthodox.*

*Fig. 2 — Practical circuit diagram using the ganged tank. The variable tank coil, L2, has 21 turns of No. 14 on the outer coil and 9 turns of No. 10 on the inner. Diameter of the outer coil is 4 inches, of the inner, 3½ inches. Both coils have a length of 2½ inches. The coil is ganged to a National TMA-2000D condenser, which has a maximum capacity of 200 µfd, per section with 0.077-inch spacing. Other circuit values will depend upon the tubes used. For the experimental unit shown:

- C1 — Grid tuning, 356 µfd, per section.
- C2, C3 — Disc-type neutralizing condensers.
- C4, C5 — 0.002-µfd. mica.
- C6, C7 — 0.01 µfd.
- C8 — 0.002-µfd. mica fixed, 5000-volt.
- RFC1 — 125-ma. r.f. choke.
- RFC2 — 600-ma. r.f. choke.
- T — Filament transformer.
- L1 — Center link plug-in grid coils (National AR16 series).*
The 1939 Canada-U.S.A. Contest was very well received and thoroughly enjoyed by the many participants. Scores reached new highs, although the contest duration was of fewer hours than in previous years. There was plenty of activity in the forty-eight hours of the April 14th–16th week-end. Logs were received from 119 VE's and 258 U.S. participants.

Certificates of Merit are being awarded the leader in each A.R.R.L. Section. Additional awards go to the highest-scoring of all participants in Canada and in U.S.A. Sections. The fifteen highest scorers among VE's and the fifteen highest W's follow:

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**Disqualifications**

We have verified carefully the reports of these stations and we have asked confirmation from numerous amateurs shown worked in their reports. Due to the declaration of a sufficient number of such operators certifying "no contact" on the dates in question, it has been deemed necessary to declare the following three stations disqualified, and therefore their scores do not appear: VE2EP, VE3QP, VE3AHV.

**Score Listings**

Scores are listed by Divisions and Sections, the winning station being first listed in each case.

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*Director of Survey, 1939 W/VE Contest Committee.

Les Amateurs Canadiens-Francais de la T.S.F., L'apaisement Nationale, 840 Cherrier Street, Montreal, Quebec.

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40 QST for
A Safety Kilowatt Transmitter

Some Ideas in High-Power Transmitter Construction

BY W. T. BISHOP, W9UI

Although the transmitter that is absolutely safe in the hands of a careless person has not yet been built, many steps can be taken to improve the present practice in the construction of amateur transmitters. One has only to read the past year's copies of QST to prove this point. The transmitter described here has been built with the express idea of seeing just what can be done with available equipment toward building a safe compact kilowatt. There are without doubt other precautions that could be incorporated; however, I believe the most important points have been protected with safety devices.

Of first importance is, of course, the housing of the transmitter in a steel cabinet, and the door to the cabinet must be provided with an interlock switch so that the a.c. line is broken when the cabinet door is opened. A Bud CR1772 cabinet was selected for the job, since it has room built in for door interlock switches. Another potential hazard that exists in the majority of rack-panel transmitters is the plate meters connected in the positive side of the high-voltage line. From the beginning it was decided to place all meters in the negative lead, and surprisingly few complications over the conventional system were encountered in doing so. In the oscillator and buffer-doubler stages, the meter was simply placed in the cathode circuit. This has the disadvantage that the meter reads the total plate, screen and control-grid current but it can easily be overlooked, since the control-grid current is small and the screen current is small when the plate current is increased upon loading. Resonance is indicated by a less pronounced dip in the current due to the screen current and control-grid current rising as the plate current dips. In the case of the driver and final stages there were two possible methods that could be used. Fig. 1A shows the method used in the oscillator and buffer-doubler stages. However, this method reads both grid and plate current and was considered a disadvantage in the case of a triode, since the grid current can so easily be separated from the plate current by one change in the connection, as shown in Fig. 1B. This method of metering not only makes the meter safe to the operator but also protects the meters from possible breakdown to ground. Although only 100 watts is dissipated in the bleeder, 200-watt bleeder boxes were used, with the idea of making them more dependable. Then, too, some allowance must be made for resistors mounted under the chassis, where the air circulation is not quite as good as it is in the open and the resistors cannot be used at full rating.

The Push-Pull TW-150 Amplifier

In keeping with modern practice, the transmitter was designed to work in the amateur bands from 3.5 to 30 Mc. This required careful selection of the tank condensers, since they had to have a low enough minimum capacity to tune to 10 meters and still be high enough on 80 meters. Spacing that would stand 3000 volts and 100% modulation was necessary in the condenser, but its size had to be such that it would fit on a standard chassis pan. The condenser finally selected was the Johnson 100DD90, which has a flashover per section of 9000 volts and is approximately 16½ inches long. This length dictated that the

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1Strictly speaking, this does not comply with the Safety Code principle that one side of all meters must be grounded. However, in this case the grid meter can only be above ground by the drop across the plate meter, which will be small unless the plate meter opens up. A 25-ohm 25-watt resistor across the plate meter would be an additional precaution. — En.
condenser be mounted parallel with the panel, since the cabinet is only 16 inches deep. The condenser fitted beautifully along the front of the chassis but this made it difficult to connect a dial to the condenser shaft. However, a bit of thinking revealed that this condenser, like many other makes of split-stator condensers, could be driven from the center by the use of suitable gears. The 100DD00 was partially disassembled and a mitre gear installed between the two rotor sections so that a similar gear would drive the shaft at the center. The operation was not difficult, and it could be done with only a hack saw, drill and a file, if a lathe were not available. The gears used were from the Boston Gear Works, catalog No. G465, and cost about one dollar. A small bracket, to hold the shaft of the driving gear, was fastened to one of the tie rods, and this bearing along with a standard panel bearing mounted on the front panel made a substantial mechanical assembly.

In order to increase the flashover point of the tank condenser, the d.c. was removed from across the condenser sections as described in the December, 1938, issue of QST. This required that the condenser be mounted on good stand-off insulators and that the shaft be well insulated from the panel and dial. One-inch steatite cone insulators were used to mount the condenser, and the tuning shaft was insulated with a Johnson No. 252 rigid ceramic shaft coupling.

The final tank-coil assembly, a B & W HDVL, was mounted directly on the panel so that the coils plug in horizontally. This resulted in a saving of some height and gave short leads to the
tank condenser. The neutralizing condensers, of the tubular type, were mounted horizontally in order to save lead length and to facilitate adjustment.

Another feature of the final amplifier is the provision for either individual or combined reading of the grid current. This was considered important because, although it is quite easy to have sufficient total grid current, it is useful to know that the current is dividing equally between the two tubes. To prevent loss of bias during switching, 100-ohm one-watt resistors are connected from each grid return to the positive side of the meter. The resistors are in shunt with the grid-current meter but cause a negligible error because the meter resistance is less than one ohm. The grid circuit consists of a B & W coil assembly tuned by a Johnson 100DD20 condenser. The BVL coils are split in the center which makes it very simple to meter the grid currents individually as mentioned above. The amplifier as shown is extremely stable on all bands. It will not oscillate even when operated with bias low enough to allow considerable plate current to flow.

A one-turn link is very loosely coupled to the plate tank coil and terminates at the base of the cabinet, where it can be connected to an oscilloscope for observation of the wave pattern. One side is grounded, eliminating any danger of the operator coming in contact with the tank coil via the oscilloscope pick up.

The Exciter Unit

The exciter consists of a T-21 oscillator, T-21 buffer-doubler, and a TZ-40 amplifier, and is band-switching from the front of the panel. Provision has been made for five crystals, one of which may be a variable type and adjustable from the panel. One of the five-prong sockets used for the crystals is connected so that a coil wound on a five-prong coil form with self-contained tuning condenser can be inserted and connected to an electron-coupled oscillator. This coil and condenser combination should be tuned to half the frequency of the crystal it replaces. This makes the oscillator act as a frequency doubler and eliminates the self-oscillation that would result from straight-through operation. The connections for this are shown in Fig. 2. All interstage coupling is capacitive, to facilitate band switching. The power supply for the two T-21 tubes is mounted on the same chassis and delivers 400 volts. The TZ-40 amplifier stage is connected as a balanced-output plate-neutralized amplifier and uses a B & W turret assembly in the output circuit. This allows the selection of three bands from the front of the panel. The plate voltage for the TZ-40 is obtained from the 1750-volt power supply primarily intended for the modulator. This voltage is reduced to the proper value by a series resistor and a cathode resistor. When the transmitter is being keyed the resting current of the high-mu TZ-40, with the bias secured from the cathode resistor, limits the plate dissipation to about 30 watts. This eliminates the need of a well-regulated bias supply in the transmitter, since the bias supply is needed only for the final amplifier. The TZ-40 operates with an r.f. choke in the plate and grid circuits and this caused the usual trouble of low-frequency parasitic oscillations. The plate choke becomes a low-frequency tank circuit and the grid choke allows sufficient excitation voltage to build up and start a weak oscillation. This type of parasitic is only troublesome when the excitation is removed, as when keying, so the proper approach toward elimination was to make the plate choke look like a poor tank circuit and at the same time not effect the operation on the operating frequency. This was done by placing carbon one-watt resistors across

If you have built or are building a high- or even medium-power job, you have probably run up against a few problems in design. This rig, designed primarily for safety, has some thoughts in it that are well worth passing along and may help you with your own troubles.
The switch panel unit includes all of the control switches except the high-low power switch for tuning. The metal block at the center of the panel is used to operate two toggle switches in the a.c. line simultaneously, since it was considered that one was not sufficient to handle the load. Three toggle switches handle local keying, phone or c.w. and plate on-off, while three others select the various plate supplies for tune-up purposes. A six-volt transformer to furnish current for the meter lights is mounted at the rear corner, next to the plate transformer relay.

the plate choke and gradually reducing the resistance until the oscillation stopped with the key open. 2000 ohms was found to be the proper value in our case. The rig is keyed by breaking both T-21 cathode circuits with a Guardian type K-100 relay. Six volts from the heater circuit is used to work the relay.

Switch Panel

The switch panel is located between the exciter and the final amplifier. The 110 volts a.c. is brought from the door interlock switch to this unit and is distributed to all chassis in the proper sequence. Two Bud No. 1269 d.p.s.t. 10-amperes toggle switches, which must carry the total 20-amperes load of the transmitter, are located in the center of the panel. These switches are operated in tandem by means of a block of metal machined to join the two handles. Throwing this switch turns on all filaments and the meter lights. The three switches on the right are connected in the individual plate primaries so that any or all may be cut out during adjustment. Three switches on the left are used to change from telephone to telegraph, close the keying relay locally, and to operate the plate primary relay locally. Parallel connections of the latter two appear at the base of the transmitter for remote operation. All wiring in the switching unit terminates in nine four-prong Amphenol bakelite sockets and an Amphenol 92-C5 receptacle. The plate primary relay, a Guardian K-100, and the meter light transformer are also located in this unit.

Modulator

Two 805's are used in the modulator. Experience has proven that they can modulate 1000 watts input very nicely if only voice is used and the plate-to-plate load made slightly lower than normal.\(^2\) It was debated whether to install a bias regulator or use battery bias, and the battery won out because it was simple and only 22½ volts bias was necessary, with 1750 volts on the plates. Input to the modulator is through a 500-ohm line-to-grid transformer. The modulation transformer is connected in the negative lead instead of the conventional positive lead. This was done so that an inexpensive relay could be used to short-circuit the secondary when using c.w. This method requires only 3000-volt insulation instead of 6000. This method does, however, raise

(Continued on page 106)


Fig. 3 — Wiring diagram of the final amplifier.

| C1 | 100-µfd. per section (Johnson 100DD20). |
| C2 | 100-µfd. per section (Johnson 100DD90). |
| C3 | 0.002-µfd., 1200-volt mica. |
| C4 | 0.002-µfd., 12,500-volt mica (C-D 22A-86). |
| C5 | 0.01-µfd., 600-volt paper. |
| L1 | 100-ohm 1-watt carbon. |
| L2 | 500-Ma. r.f. choke (Johnson No. 754). |
| S1 | D.p.d.t. toggle switch. |
| S2 | S.p.d.t. toggle switch. |
| A | Connectors (Amphenol 92-C5). |
| B | Connectors (Amphenol PCIM) A is for excitation; B is for connection to oscilloscope. |
| T1 | 10-volt 6-ampere filament transformer (Stancor P6139). |
| T.C. | Thermocouple for use with Ma. |
Link Coupling for the Rotary Antenna

A Three-Element Beam with Continuous Rotation in Either Direction

BY J. M. BURKE, JR.,* W5EME

After discarding several different types of sliding contactors in an effort to make a 3-element rotary beam antenna completely rotatable, a system of link coupling was worked out which is simple to adjust and is giving splendid results.

From the accompanying photographs it can be seen that a tuned tank circuit is mounted just above the rotating mechanism and centered around the rotating shaft. For 20 meters this pancake-type coil, a thought carried over from the old spark days, has four turns of \( \frac{1}{2} \)-inch copper tubing spaced approximately \( \frac{3}{10} \) inch, with a mean diameter of 10\( \frac{3}{4} \) inches. The 3-plate tuning condenser has a capacity of about 15 \( \mu \mu \)fd., with 0.2-inch spacing between plates. This tank is fed with an ordinary 600-ohm untuned open-wire line, using slightly less than one turn of the antenna coil itself as the coupling link. The other end of the 600-ohm line is linked directly to the plate tank by one or two turns placed around it. This keeps the d.c. plate voltage off the transmission line. Tuning these two link-coupled tanks is quite conventional. The one-turn antenna coupling link (10\( \frac{3}{4} \) inches in diameter) is attached to but insulated from the rotator shaft and turns with the beam. As shown in the photograph, this link is spaced approximately \( \frac{3}{8} \) inch from the pancake coil.

A short coaxial cable is used to current feed the driver radiator of the 3-element beam from the one-turn link. The impedance at the center of the radiator element is quite low, amounting to some 10 or 15 ohms. The cable shown in the diagram was constructed from two concentric tubes. The outer tube is 3\( \frac{1}{4} \)-inch thin-wall electrical conduit, measuring 0.82-inch inside diameter, and the inner tube is 3\( \frac{1}{2} \)-inch hard-drawn copper water pipe measuring 0.62 inch outside diameter. 1\( \frac{1}{4} \)-inch threaded studs are soldered to “center” in the shorter 3\( \frac{1}{2} \)-inch copper pipe and act as supports for the inner conductor. Johnson No. 45 feed-through insulators were used to insulate and space the tubes, using the short end with the glazed-porcelain cone tip. The gaskets supplied with the insulators were shellacked in place to keep out moisture and to keep the tube spacing correct. This cable has 1/10-inch air spacing and a much longer glazed porcelain insulation path. The energy transfer is good, with no noticeable heating at the 500 watts input used. The impedance figures to be about 16 ohms from the formula, which is a fair match for the low-impedance radiator.

The 3-element beam uses tenth-wavelength spacing for the reflector and 0.15-wavelength spacing for the director, as recommended in the

* 1315 South College St., Tyler, Texas.
Here is a straightforward solution to that bugaboo of rotary antennas: the feed problem. Inductive coupling, a simple reversible drive, and an easy-to-build direction indicator make this a worthwhile article for the 99% interested in rotatable antennas. The other 1% can learn something, too.

A close-up of the drive gear reveals the direction-indicator switch under the gear.

Premax Technical Bulletin H-3. Tuning of such a beam has been thoroughly covered in previous articles, and needs no further comment.

**Direction Indicator**

The direction indicator uses an A.R.R.L. radio map of the world, mounted on ¼-inch plywood with picture molding around it. Tyler, Texas, was located on the map, and a pin-hole made through into the plywood. The map was removed and a 16-inch circle drawn with this point as the center. Twelve points were located on the circle corresponding to the hour markings on the face of a clock, with 12 o’clock pointing due north. Holes were drilled at all these points to take 6.3-volt dial lights. The map was remounted and dial lights were inserted from the rear so as just to touch but not break the map paper. Red lines were then drawn on the map from the center (Tyler) through each light to the edge of the map. The lights are connected through a small filament transformer, and a 12-wire cable was run to the contactor on the rotor mechanism. The photograph shows the details of the contactor. The phosphor-bronze contactor bridges between contacts as it passes around, so that either one or two lights are always burning. This gives 12 single direction points on the map, and 12 additional

The antenna coil, its tuning condenser, and the one-turn pick-up loop can be seen at the top of the photograph. The gear drive for the shaft is shown at the bottom, belt-driven by two motors which allow rotation in either direction. In use, the whole unit is covered by a weatherproof housing.

Fig. 2 — The coaxial line from the pick-up coil to the antenna is made of thin-wall electrical conduit with a piece of ½-inch copper tubing running through the center. Parts of feed-through insulators support the inner conductor, and the line is made weatherproof by sealing at both ends.
Intermediate points when any two lights are burning. The dial lights shining through the map paper give a soft and pleasing effect.

The rotor mechanism uses two 1/4-hp. Emerson motors arranged so that the beam is reversible and continuously rotatable from the operating table. A grounded metal cover protects the mechanism from the weather.

Adjustment

Standing waves on the 600-ohm line were reduced to a near minimum by adjusting the coupling turns on each end of the line. A few inches of wire and a flashlight bulb were used as an indicator. The coupling was adjusted between the coil and the one-turn link (this link is located above the antenna coil and connects to the coaxial cable) until correct final amplifier loading was obtained. Naturally, there is some interlock, and it is necessary to tune first one and then the other. It is also well to choose a length of line which is not resonant at or near the frequency used.

Results have been very satisfactory both in transmitting and receiving; and many excellent reports have been obtained. Although tuned for the middle of the 14-Mc. 'phone band, it seems to work well from one end of the phone band to the other.

Photographs are by J. Heath Lamb, W5PH.

New Method of Rating Transmitting Tubes

Everybody knows that a tube doesn't immediately blow up when it's pushed a bit beyond the manufacturer's ratings, but the tantalizing question is: Just how far can the pushing be carried on? And, supposing the life is shortened thereby, how much more power can be taken from the tube before it becomes cheaper to buy the next larger tube rather than overload the small one?

A new system of dual ratings introduced by RCA Manufacturing Company, taking into account the difference between the kind of operating done by amateurs and that in commercial work, should help to answer some of these questions. We quote from a statement on the subject:

"Instead of one set of maximum ratings for each tube type, two sets of maximum ratings are given. These ratings are designated 'continuous commercial service' (CCS) and 'intermittent commercial and amateur service' (ICAS). The CCS ratings are essentially the same as the former maximum ratings. The ICAS ratings, however, are considerably higher, permit the use of much greater power input, and provide a relatively

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A New Method of Measuring A.C. Voltages

Applying the Cathode-Ray Oscilloscope to the Slide-Back Voltmeter

BY GEORGE S. WACHTMAN

This is an account of a method of measuring a.c. voltages with cathode-ray tubes of the electrostatic-deflection, medium- or short-persistence screen, type, with descriptions of the equipment needed and used in the experiments pertaining to the development of the method.

Theoretical Considerations

Considering a cathode-ray tube of the type described above, with the various electrode voltages adjusted to give a sharply defined spot on the screen and one vertical and two horizontal deflecting plates grounded; suppose a positive potential of 100 volts with respect to ground is applied to the free vertical deflecting plate as at A, Fig. 1. The spot will move up vertically away from its normal position near the center of the screen a distance proportional to the voltage applied to the plate.

Now, if a negative potential with respect to ground of 100 volts is applied in series with the positive potential and ground as at B, Fig. 1, so that the two voltages oppose one another, the spot will immediately move back to its exact original position. Therefore, the voltage necessary to deflect the spot back to its original position may be taken as an exact measure of the voltage necessary to move it away. This applies to either set of plates, of course.

It should be possible, theoretically, to measure the spot's distance at any point on the screen from its normal position in terms of the voltage necessary to deflect it back to this position. Practically, this is true except when the spot's position is indistinguishable from its position at any other point on the screen, such as in the case of a solid pattern or when the image or signal is of an irregularly recurrent or transient nature.

In case one or more a.c. voltages may be applied to either or both sets of plates, either separately or simultaneously, the important thing to remember is that any image that appears on the screen is caused by a more or less rapidly moving spot which, because of the persistence of vision of the eye, is caused to appear as a single image instead of a moving spot. Thus any point on any pattern appearing on the screen may be considered as a single spot which may be measured as before stated. If a linear-time base is used to sweep the spot along one axis, the voltage/time relation may be determined.

Equipment Needed

Three things are apparently necessary to make even the most rudimentary measurements by this method: First, of course, a cathode-ray oscilloscope of some sort or other; second, a source of variable d.c. voltage with which to bias or return the spot to normal or some other reference point; and third, a d.c. voltmeter with which to measure the variable d.c. voltage.

The oscilloscope may be of any type employing a cathode-ray tube of the electrostatic type, from the simplest composed of the CRT and its associated power supply to the most elaborate with its amplifiers and linear sweep, according to the kind of signal to be measured and the amount of information to be gleaned from it. However, there must be some means provided whereby a variable d.c. voltage can be connected in series with the free deflecting plate to which the signal...
If you own an oscilloscope and a halfway decent d.c. voltmeter, there's no reason why you can't measure a.c. voltages within normal ranges. The method described here gives you more accuracy than you could normally obtain.

to be measured is applied, usually the vertical one. Also, a transparent screen with at least two lines ruled on it at right angles to each other across the center is essential. This screen is placed in front of the tube's screen and the lines used as reference when biasing the spot during a measurement. It should be mounted so that one of the ruled lines is parallel to the horizontal or "X" axis of the tube, or the line drawn by the spot when it is deflected horizontally. The other line should then be parallel to the vertical or "Y" axis of the tube. Usually it is simply a matter of mounting the screen centrally before the tube and then rotating the tube until its axes and the screen's lines coincide. In some cases it is impossible to place the screen and the tube so that both lines are parallel to the axes of the tube, and in such a case it is best to place them so that the horizontal line and the horizontal axis coincide as most of the voltage measurements are made with the horizontal line as a reference. The vertical line is used in determining the voltage-time relation of a signal.

The source of variable d.c. voltage can be anything that is capable of delivering enough voltage to deflect the spot from one edge to the center (or vice versa) of the tube used, at a current of from 5 to 10 milliamperes and with very little ripple (1% or less). A potentiometer is used to vary the voltage. In some cases the centering controls on the oscillograph will serve as the source of variable d.c., provided there is enough range of voltage. In any case the output should be variable from zero up to as high as necessary.

Almost any good d.c. voltmeter with suitable ranges will serve as the measuring instrument. That is, one that is sensitive enough not to overload the variable attenuating control on the d.c. source.

Various combinations of these three units may be used. They can be combined in one unit or may be separate; other combinations may be used to suit individual needs. Obviously the single unit is to be preferred.

Equipment Used in Experiments
The equipment used in developing this method of measuring a.c. voltages was all straightforward. Fig. 2 shows the oscillograph and d.c. voltmeter set up to make a measurement.

The CRO is a home-built affair employing a 913 CR tube. It is self-contained, having its power supply, linear-time base, vertical amplifier, and CR tube contained in one unit. Its unusual feature is the shorting-type 'phone tip jack through which a variable d.c. voltage may be applied in series with the free vertical deflecting plate of the 913 and the vertical centering control. Fig. 3 is a schematic diagram of this feature. This same means of inserting a d.c. voltage may be used with the horizontal plates.

The 1- to 2-megohm resistor, R3, connected across the 'phone tip jack, is to keep the circuit continuous from centering control to plate when the jack is opened and in no way affects the accuracy of a measurement. The 0.5-µfd. condenser, C3, is necessary to by-pass any ripple that may appear in the circuit.

The d.c. measuring equipment is an 0-1-ma. meter. There are five ranges available through a selector switch. The ranges used in conjunction with the CRO and power supply are: (1) 100-volts peak, and through an auxiliary s.p.s.t. toggle switch, 100-volt r.m.s. direct-reading range; and (2) a 250-volt peak indirect reading range; i.e., on range 2 the scale of the milliammeter must be multiplied by 2.5 and the product taken as the voltage indicated by the instrument. This latter range is used only in making peak measurements between 100 and 150 volts.

A 4-prong tube socket is mounted on the back of the instrument case into which the cable outlet from a portable power supply is plugged when measurements are to be made. The output of the power supply is fed from this socket through an attenuating network which includes the potentiometer, the control knob of which may be seen in right center of the panel of the instrument. The variable d.c. output is taken from the negative end and the movable arm of the potentiometer. It is fed directly across these jacks through appropriate series dropping resistors on each of the two ranges by means of the range switch. Fig. 4 is a schematic diagram of the circuit showing the various parts of the instrument used in these two ranges, including the attenuating network and socket.

$S_{un}$ and $R_4$ are used only when reading r.m.s.
voltages of signals whose waveforms are sine- or very near sine-wave in character. Referring to Fig. 4, with $SW_1$ in position 1 and $SW_2$ closed, the meter is connected through a 99,700-ohm resistor, $R_2$, to the variable d.c. output jacks and reads directly the d.c. equivalent of the peak voltage of the signal. With $SW_2$ open, a 41,400-ohm resistor, $R_4$, is connected in series with the negative lead to the meter, and the meter reads directly the d.c. equivalent of the r.m.s. value of the signal. Because of this resistor the meter actually reads 70.7% of the voltage across the output terminals. For a full-scale deflection of 1 ma., 144.4 volts must be applied to the terminals; i.e., the output voltage is actually 1.414 times that indicated by the voltmeter, or the voltmeter indicates 0.707 of the voltage over the terminals, thus indicating the r.m.s. value directly in volts.

It is readily seen why this is so. Suppose we have a symmetrical sine-wave signal on the screen whose r.m.s. value is known to be 100 volts. Its peak value is, therefore, 1.414 times this value, or 141.4 volts. As it will take 141.4 volts d.c. to bias the upper tip of the image down to the upper edge of the reference line, and the meter reads 0.707 of the variable d.c. output from the d.c. source with $SW_2$ open, then $0.707 \times 141.4 = 100$ volts, the d.c. equivalent of the r.m.s. value. Biasing and adjustment of the image is explained later.

The d.c. source or power supply furnishes about 375 volts at 50 ma. Nothing further need be said about it except that it is quite well filtered; in all other respects it is similar to any other a.c. power supply.

**Practical Considerations**

We shall now consider the practical aspects of making measurements. After the CRO has been turned on and allowed to warm up for a minute or so, the first adjustment is to focus the spot on the screen. Too much care cannot be exercised in doing this — the spot should have a very definite sharp outline when properly focused. The size of the spot is immaterial so long as it is properly focused and only peak measurements are being taken. If measurements other than peak (those involving details of a signal) are to be made, the spot should be as small as practical yet bright enough to be seen without too much eye-strain.

If a horizontal sweep, either linear or otherwise, is to be used, the sweep should be applied and the line caused by the spot should be adjusted until it is of uniform width, and its upper and lower edges are sharply defined throughout its length.

Since when the spot is deflected horizontally, the spot or line has a finite width, it must be displaced enough to bring one of its edges even with one of the edges of the horizontal reference line on the transparent screen; upper edge even with upper edge, as at $A$, Fig. 5, if measuring the upper half, and lower edge even with lower edge, as at $B$, Fig. 5, if measuring the lower half of a signal as seen on the screen of the CR tube. This adjustment minimizes one of the chief sources of error. The necessary displacement of the spot or line is brought about by varying the vertical centering control by the correct amount.

This brings us to another point in question: whether to measure the positive or negative half of a signal. (The portions of the CR tube's screen in which the positive and negative halves of an image appear may be determined by applying a positive d.c. voltage to the free vertical deflecting plate and noting which half of the screen the spot is deflected into, in which case any portion of any image appearing in that half is positive and any portion appearing in the other is negative. In this case the horizontal reference line is used as the dividing line.) It is immaterial which half of a symmetrical signal is measured — either one will do — but the decision as to which half of an asymmetrical signal should be measured lies entirely with the operator and his judgment and depends on the requirements of the case.

The most important part of all entails the biasing of the spot or image. For example, suppose we want to measure the peak voltage of the upper half of an image or respective half of a signal. This may be done either with or without horizontal deflection of the spot. After the spot has been focused properly and adjusted as described before and the spot or line is adjusted upper edge to upper edge of the reference line,

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the signal is applied to the vertical plates, the voltmeter connected to the output of the d.c. power supply and the variable d.c. output connected to the shorting type phone tip jacks on the CRO. Now all that is necessary is to adjust the bias until the very upper tip of the line or image that appears on the screen is even with the upper edge of the horizontal reference line. This is done by adjusting the potentiometer on the instrument panel of the voltmeter; i.e., by varying the output of the d.c. supply, and then noting the voltage indicated by the voltmeter. This reading is equal to the peak voltage of the upper half of the image or the respective half of the signal. In case the image moves up instead of down when adjusting the potentiometer, reverse the leads connecting the variable d.c. voltage to the CRO.

The same procedure is carried out in reverse when measuring the peak voltage of any part of any image appearing in the lower half of the screen, i.e., the lower edge of the spot or line is adjusted until it is even with the lower edge of the reference line, and the signal is applied and biased until the very lower tip is again even with the lower edge of the reference line. The voltage can then be read from the voltmeter. Fig. 6 illustrates the various positions of the image, including its normal or unbiased position, when properly biased for peak measurements.

**Time Relations**

To locate the spot’s relation to time simply means to determine its position with respect to the beginning of a cycle, in electrical-time degrees. This may be done easily if a linear time-base is used to sweep the spot along the horizontal axis, the horizontal and vertical reference lines are parallel to the X and Y axes respectively, and a means is provided whereby a variable d.c. voltage can be applied in series with the plates to which the linear sweep voltage is applied. For example; if the conditions outlined above are met, it is then necessary to apply the linear-sweep voltage to the horizontal plates and make its amplitude as great as is consistent with good linearity. Next, the horizontal line created by the moving spot should be adjusted to the horizontal reference line as in taking a measurement of the peak voltage of a signal. The signal is then applied to the vertical plates and the sweep frequency adjusted until two or three cycles appear on the screen of the tube. After choosing one of the cycles to measure, the point at which it begins (i.e., one of the points at which the spot crosses the zero or horizontal reference line) is adjusted to the junction of the horizontal and vertical reference lines by means of the horizontal centering control and the variable d.c. voltage supply is connected in series with the horizontal deflecting plate and centering control of the CRO.

The tube is then biased until the end of the cycle, $P_1$, is at the same position on the screen as the beginning was before. The voltage indicated by the voltmeter, $V_1$, is noted. The point on the curve of the cycle whose position in electrical-time degrees is to be found, $P_2$, is selected, and the d.c. voltage on the horizontal plate is again varied until this point is even with the vertical reference line. The voltage, $V_2$, is read from the voltmeter and noted. The position of $P_2$ in electrical-time degrees is found by:

$$P_2 = \frac{V_2}{V_1} \times 360$$

To measure a point on the slope of a curve a linear time base should be used, the point adjusted to the vertical reference line, and then biased up or down to obtain the voltage.

**Percentage of Modulation**

To measure the percentage of modulation of an r.f. signal it is only necessary to follow the same general procedure for focusing and adjusting the spot or line as before and then measuring the voltages represented by $O$ to $D_1$, and $O$ to $D_2$, Fig. 7, by biasing $D_1$ and $D_2$ down to the horizontal reference line respectively. The percentage of modulation is then found by substituting in the equation:

$$\% \text{ Mod.} = \frac{D_2 - D_1}{D_2 + D_1} \times 100$$

A word about the accuracy attainable with this method of measurement. The accuracy of adjustment of the spot or line to the reference line may
be held within less than 1/100 inch or 1% of the diameter of the 913's screen. This figure may vary with different persons as it depends somewhat on the operator's eyes. In my own case, I have found my error in adjustment to be approximately 0.008 inch or 0.8% of the diameter of the screen. When measuring a signal of 100 peak volts this would be equal to an error of approximately 1.6%, as the measurement is made from one peak to the reference line at the center of the screen.\(^1\)

This is well within the 2% full-scale error which is the maximum guaranteed for the meter used as the indicating device in this case. The error in adjustment in per cent of signal is approximately inversely proportional to the size of the image or amplitude of the signal; for instance, if there is an initial error of 1.6% at 100 volts, this will rise to 2.5% at 50 volts, 5.25% at 20 volts, and approximately 10% at 10 volts. Therefore, the larger the amplitude of the signal the less the error of the measurement. As for the error due to the meter, this may be minimized by using a more accurate meter or by adding additional low voltage ranges, say 50-volt and 25-volt ranges, or both. On measurements below 10 volts the error of adjustment becomes too great to make such measurements practical.

As the impedance of \(G_i\), Fig. 3, varies with frequency it will introduce an appreciable error when measurements are made on the lower frequencies. The impedance of this condenser equals 5,400 ohms at 120 cycles, 10,800 ohms at 60 cycles, and 21,600 ohms at 30 cycles, introducing errors of \(-0.5\%\), \(-1.0\%\), and \(-2.0\%\), respectively.

There is one precaution to be observed when setting up the equipment to make a measurement, and that is to make certain that there is no direct connection between the CRO and the d.c. power supply other than the two connections to the 'phone jack in series with the free vertical deflecting plate and the vertical centering control. For instance, if the CRO chassis were directly connected to the negative side of the power supply while the two leads to the 'phone jack were connected, the centering voltage from the vertical centering control would be shorted to ground and the control would cease to function as such. In any case, whether the bias or d.c. source and the CRO are combined in one unit or are separate, they should be isolated from each other except for the two leads or connections in series with the free plate of the C.R. tube.

The voltage limits of the tube, a 913, may be extended by an attenuating network of the parallel element type in case voltages in excess of 150 volts peak are to be measured, and by amplifiers in case voltages lower than 10 volts are to be measured. When an amplifier is used it is necessary either to calibrate it or use it as a vacuum tube voltmeter. In the latter case the CR tube is used merely to indicate false zero.

Henceforth when measuring voltages with a CR tube it was necessary to know its deflection sensitivity, whereas it has very little effect on the accuracy and need not be known when using the method just described. There are several other advantages to the use of this method, chief among which is the greater accuracy than that obtained by using the older one of calibrating the screen of the CR tube in volts/inch or volts/mm. deflection. Once this system is mastered it is very easy to take measurements of almost any type of signal.

**U.H.F. Contest and Relay—**

**November 4th-5th**

**The** September relay was acclaimed. The gang asked for another. Here it is. And don't think we're not going on to have more fun. Five-meters, and 2½- are year 'round bands. A surprisingly large number of operators have u.h.f. gear along-side low frequency transmitters and are just looking for chances to test it out. Here's our chance!

**Scoring Contacts:** List all different stations worked in the contest period, which is November 4th (Saturday), 3 P.M. local time, to November 5th (Sunday), 11.59 P.M. local time. Beside the calls show the location of these stations, obtained as you work them, for points claimed. For stations:

- Under 50 miles, score 1 point
- 50 up to 100 miles, score 2 points
- 100 up to 300 miles, score 5 points
- Over 300 miles, score 10 points

For originating and sending a five-to-ten word test message, specifically addressed to remote sections of the country, as in September (one message only may be started per station) and mailing copy, with handling data to Hq., 10 additional points may be credited. Likewise, for relaying such messages away from the starting point and submitting copies, count 3 points each, \(1\) for receiving by radio, \(2\) for each relay onward. Operators subject to the difficulties and inconveniences of working at field locations under portable designation, may multiply the sum of their contact and relaying scores by \(2\).

**U.H.F. Certificate Award:** Each participant who sends a "station worked" list, with message copies attached, and a claimed score, will receive a special A.R.R.L. certificate showing his score and how many stations were worked, in this activity. It's a neat certificate that will be valued as

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(Continued on page 113)

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\(^1\) Since writing this story, Mr. Wachtman has found that the accuracy can be increased by using a larger tube. A 906 with 1000 volts on the number 2 anode gives only one-third the error of the 913. — Ed.
The Portable at W7AW

A Complete Low-Power 'Phone and C.W. Rig

BY I. VEE IVERSEN,* W7AW

This transmitter is the result of several years of operating portable transmitters of various kinds. I have tried to discard all of the undesirable features and retain only the good ones in the rig to be described.

Since I work portable a good portion of the time and have learned about what minimum power I can use and still get satisfactory results, I designed this transmitter by starting with the final stage and working backwards to the oscillator. I knew from experience that 14 Mc. was the best band for my operation because of antenna limitations and past experience with the other bands. For an antenna I selected a half-wave center-fed horizontal radiator made of fixture wire (the flexible kind used for wiring home-lighting fixtures), so that it can be put up and taken down with the least trouble.

For feed line I use the twisted-pair transmission line sold for use with b.c.l. all-wave antennas and, in spite of its reputation, I have never had any of this line break down from voltage or other causes, and some of it has been used for over two years in all kinds of weather. The antenna and transmission line are coiled up together when not in use.

I found the best dimensions for the "Y" match from the transmission line to the flat top to be 20 inches on each side of the triangle, for 14-Mc. operation. My antenna is seldom over 10 to 15 feet above the ground, but it gets out in good style, if the results obtained in operation are any indication.

The Circuit

An RCA 809 was selected for the output tube and, since this tube is not too easy to drive, I decided to use an 802 as a Tri-tet oscillator-buffer for c.w. operation. Using 7-Mc. crystals and doubling to 14 Mc. in the plate circuit, the 802 Tri-tet drives 20 mils grid current through the 3000-ohm grid leak of the 809.

I wished to have the final tank single-ended, to make it simpler to feed the twisted pair transmission line to the antenna, and this made grid neutralization necessary. I used one mesh of a pi network for combined final tank circuit and antenna feed, the condenser feeding the transmission line to the antenna being a fixed one. As I

*Officer of Chief Engineer, Northern Pacific Railway, St. Paul, Minn.
It takes more than spending most of his time away from home to reduce an old-timer's interest in amateur radio. This is the story of a portable for the traveler who has 110 volts a.c. available at his stops but not much else.

use the same antenna and run the 809 to full load all the time, the fixed capacity works out nicely and takes up less space than a variable. The harmonics seem to be attenuated greatly with this coupling network. The coupling condenser is mounted on GR banana plugs, so that it may be changed quickly or a variable condenser used. It may be shorted out if a coupling link is used or if some other type of antenna becomes available. In my case, to load the 809 to 100 mills this condenser is made up of five 0.00015 µfd. 5000-volt mica condensers in parallel. These condensers are operated in parallel to allow for the heavy circulating current they have to carry.

The grid and plate coils for the 809 are Decker coils that plug into five-prong sockets. The plate coil of the 802 is link-coupled to the grid coil of the 809, using nine turns for link coupling to the 802 and one turn on the grid coil of the 809, to give the greatest transfer of power. The plate coil of the 802 is a tapped coil wound on a five-prong plug-in coil form, wound ten turns to the inch and wound full. The tuning condenser should be tapped at about the center of the coil, just so the coil can be tuned. This gives the necessary high-impedance load for the 802 and increases the output of the tube considerably over what can be taken from a tank circuit that has the condenser across the whole coil. The cathode tank for a 7-Mc. crystal is 7 turns on a 1½-inch form.

Blocked-grid keying is used, the blocking voltage being taken from the power supply and, with the values of capacity and resistance used, all key clicks are eliminated. With 550 volts on the plate of the 802, a blocking voltage of 220 volts on the grid is necessary to cut off the plate current.

Since it is a high-µ tube no provision is made for blocking the grid of the 809 and, with excitation removed and full plate voltage applied, it draws only 20 mills, which will not harm the tube during periods of no excitation. All bias for the 809 is from the grid leak.

A switch is placed in the negative lead from the center tap of the power transformer secondary to ground, to cut the plate voltage to the tubes and still allow the filament of the 5Z3 to be heated. This method allows the use of a single-pole

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**Fig. 1** — Circuit diagram of the transmitter as used for c.w.

\[ C_1 = 0.1-\mu\text{fd., 1200-volt.} \]
\[ C_2, C_3 = 4-\mu\text{fd., 1000-volt.} \]
\[ C_4 = 24-\mu\text{fd., electrolytic, 450-volt.} \]
\[ C_5 = 10-\mu\text{fd., electrolytic, 250-volt.} \]
\[ C_6, C_7 = 0.1-\mu\text{fd., 400-volt.} \]
\[ C_8, C_9, C_{10}, C_{11}, C_{12}, C_{13}, C_{14}, C_{15}, C_{16}, C_{17}, C_{18}, C_{19} = 0.001-\mu\text{fd. mica.} \]
\[ C_{20} = 100-\mu\text{fd., 1000-volt.} \]
\[ C_{21}, C_{22} = 50-\mu\text{fd., variable.} \]
\[ C_{23} = 0.002-\mu\text{fd., 1000-volt mica.} \]
\[ C_{24} = 50-\mu\text{fd., each section split.} \]
\[ C_{25} = 10-\mu\text{fd., neutralizing condenser.} \]
\[ C_{26} = 0.006-\mu\text{fd., 5000-volt.} \]
\[ C_{27} = 0.00015-\mu\text{fd., 5000-volt.} \]
\[ C_{28} = 0.003-\mu\text{fd., 120-volt.} \]
\[ C_{29} = 0.001-\mu\text{fd., 600-volt.} \]
\[ C_{30} = 0.05-\mu\text{fd., 3000-volt.} \]
\[ C_{31} = 0.006-\mu\text{fd., 600-volt.} \]
\[ C_{32} = 0.00015-\mu\text{fd., 5000-volt.} \]
\[ C_{33} = 0.001-\mu\text{fd., 120-volt.} \]
\[ C_{34} = 0.006-\mu\text{fd., 600-volt.} \]
\[ C_{35} = 0.00015-\mu\text{fd., 5000-volt.} \]
\[ C_{36} = 0.001-\mu\text{fd., 120-volt.} \]
\[ R_1 = 60-ohm, 100 ma. \]
\[ R_2 = 5000-ohm, 10-watt. \]
\[ R_3 = 50,000-ohm, 50-watt voltage divider. \]
\[ R_4 = 10,000-ohm, 10-watt. \]
\[ R_5 = 50,000-ohm, 10-watt. \]
\[ R_6 = 60-ohm center-tapped, to carry 100 ma. \]
\[ R_7 = 7½-volt filament transformer. \]

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single-throw switch of the small toggle variety to be used to cut plate voltage. I feel it is much safer than using a double-pole switch to break the plate leads to the rectifier tube, as is sometimes done. The latter method puts a high voltage across the switch - in fact, twice that which will appear across the switch insulation as I have used it.

Due to the large variation in line voltage found in various parts of the country, I have used a 7.5-volt filament transformer with a rheostat in the primary, to allow me to have 6.3 volts for the 809 and the 802, even under very low supply-voltage conditions.

I found that by putting 24 µfd. of electrolytic condenser across the supply tap for the screen of the 802 Tri-tet, the output was raised an appreciable amount, and the note was greatly improved. The suppressor is run at 50 volts positive. In this regard, I wish to remind the reader that if cathode bias is used on a tube like the 802, it is sometimes almost impossible to make the tube deliver any load power even with 50 volts on the suppressor grid. The reason, of course, is that the voltage developed across the bias resistor may be of the order of 60 to 75 volts and with only 50 volts positive on the suppressor grid, it is obvious that the suppressor will actually be 10 to 25 volts negative with respect to the cathode. In order to run the suppressor grid positive with respect to the cathode, it is necessary to have it from 100 to 125 or 135 volts above ground, if cathode bias is used. This is a matter that I have found overlooked in a great many transmitters built around these pentodes. Bear it in mind when applying cathode bias to a pentode tube, when the suppressor is operated positive.

Another thing that is very often overlooked is the voltage on the neutralizing condensers, which causes arcing on closely-spaced condensers. You will notice that I have used parallel feed for my 809, and the neutralizing condenser is connected to the ground side of the blocking condenser, thus avoiding the plate voltage appearing across the neutralizing condenser, or on the tank coil or antenna. This will allow a smaller condenser with closer spacing to be used, and it will avoid arcing even under modulation.

Using a 7-Mc. crystal and doubling to drive the 809 on 14 Mc., the 802 as a Tri-tet does not give power enough to drive the grid of the 809 sufficiently for modulation, and I found it necessary to add an oscillator tube when I tried to modulate the 809. If phone operation is required, I would suggest using the 802 as a buffer and exciting it from another tube. This is also better practice, as it isolates the oscillator from the modulated tube. It is an easy change to make, for the crystal tube may be put in the socket used for the cathode coil of the Tri-tet and, by using one of the new crystal sockets that mount above the chassis, the added

**Fig. 2—Wiring of the transmitter when used for phone.**

- C4- 10-µfd. neutralizing condenser.
- C24, C25-4-µfd., 600-volt electrolytic.
- C25- Five 0.00015-µfd. mica in parallel.
- CH1-30-henry filter choke.
- CH2-5-henry filter choke.
- Ri- 100-ohm primary rheostat.
- Rs- 50,000-ohm, 50-watt voltage divider.
tube is an easy thing to achieve. With this tube added, it is easy to get the necessary 32 or 35 mils grid current on the 809.

The modulator used is designed to reduce all frequencies under 200 cycles and above 3000 cycles and, with a pair of 6F6G tubes operating class AB1, gives much more audio power than is necessary to modulate 100 per cent with voice.

Construction

The power supply and r.f. portion are all on one 10-inch by 17-inch by 3-inch chassis. The power supply is mounted along the back edge of the chassis and the r.f. components on the forward edge, all condensers being mounted under the chassis. This would seem to make for long leads, but the fact is that they are not long but quite direct and short.

The controls are as follows, from left to right: Cathode-tank tuning condenser for the Tri-tet, or crystal-oscillator plate tank when the separate tube for 'phone operation is used; d.c. high-voltage switch, key jack, tuning condenser for the 802 plate circuit, plate-current jack for the 802, grid-current jack for the 809, grid-tank tuning condenser for the 809, plate-current jack for the 809, 110-volt a.c. switch, plate-tank tuning condenser for the 809. Each inductance is mounted directly above its respective condenser.

This transmitter was built up of parts that have been around for years. Anyone building a similar one could save a great deal of space by using the new small oil-filled condensers in the filter. The condensers I used were many years old, and of the old paper overgrown size, as can be seen.

All wiring is conventional. The link between the 802 and the 809 was found to deliver much more power with two spaced wires than with a twisted pair, and it is made of a pair of No. 12 solid wires, spaced 3/8 inch.

The r.f. choke and blocking condenser for the 809 are mounted directly behind the socket of the 809 plate tank inductance, giving a short, direct lead to the plate cap of the 809 for both d.c. and r.f. All d.c. high-voltage leads were run in shielded wire, to prevent any stray coupling through the supply network. The 809 neutralizes nicely, and has no tendency at all to go off on its own.

For c.w. operation, the 802 Tri-tet is plenty of driver, and the arrangement makes a nice compact two-tube transmitter. For 'phone operation, the addition of the separate driver tube was found necessary. I chose a 41 type tube for crystal oscillator because of its small size and its being a pentode. The plate potential was taken from the tap for the screen grid of the 802 on the bleeder resistor. This gives 300 volts for the plate of the 41, and its screen grid is fed from a divider of 10,000 ohms and 20,000 ohms to ground. It oscillates very nicely and, with a 14- or 7-Mc. crystal, will deliver plenty of power with the drive for the 802 being tapped way down on the plate coil. This allows the oscillator to run lightly loaded and yet drive the 802 to plenty of output.

The number of turns on the tank coils are not given, for the reason that anyone building this transmitter will have to cut and try anyway. Any of the coils given in the Handbook will be a good starter. The Decker coils, of course, are pre-wound and will be correct if used.

The grid-tuning condenser for the 809 is the only split-stator one used. All condensers are mounted on the chassis with rotors grounded, with the exception of the neutralizing condenser. Small mica blocking condensers and the series feed tanks are used to accomplish this.

No provision was made to measure the plate current of the 41. The important thing is the r.f. crystal current, and a small pilot lamp is put in series with the crystal to indicate that current. The screen grids of both the 41 and the 802 are keyed. With
this arrangement, good keying is obtained, without key clicks.

It might be of interest to mention that I tried a small amount of cathode bias for the 809, but had to remove it because under modulation the increase in plate current raised the bias to such a value that downward modulation resulted. Removal of the cathode bias cleared it up.

Modulator

The modulator and its power supply are also built up on a 10-inch by 17-inch by 3-inch chassis. About the only thing of special interest in the modulator, which uses conventional AB1 output, is the method of hum and frequency discrimination used.

Since I operate portable most of the time, when often a good ground is almost impossible to obtain, I found that the only microphone I could use with any degree of success was a dynamic one with the low output impedance of 50 ohms. I bought a nationally-known input transformer, which was supposed to have hum-bucking windings and consequently a very low hum output. But the fact was that, regardless of where I mounted that transformer, or in what position, the hum was so bad that it could be heard with ease with a pair of phones across the secondary. I almost gave up trying to use it, and I was going to try using resistance coupling from the microphone to the first grid, but I thought I would play around with inverse feedback and cutting off the low frequency response for the amplifier, to see how far I could go by that method. This was very successful.

It is a practice in ham audio work to use high values of grid resistors, on the order of 500,000 ohms or more. This favors low frequency response. We have to change our habits and go the other way to get rid of hum. By using 50,000-ohm grid resistors, we can attenuate the low frequency; 100 cycles is cut out about 8 db by this low value of resistor. Then, by using 500,000 ohms or more in series with the grid, we can cut the lows some more. By using both, the hum frequency of 120 cycles is almost completely eliminated. Then, too, introducing inverse feedback to the input transformer as shown helped the hum trouble no end. By using coupling condensers of small values between stages, in addition to the above, the problem was solved. It was fun playing with this problem, and anyone interested can spend a pleasant afternoon with a few resistors and condensers.

In the final form, the hum is heard with the volume control full on, but it is not objectionable. With the control operated where it gives plenty of audio to modulate the transmitter, the hum is just visible on the oscilloscope and can be just barely heard.

The circuit is self-explanatory, but it might be a point to mention that I had to use the 200-ohm primary connection on the input transformer for the 50-ohm microphone and thereby was able to ground the center point of the primary and get a balance to ground on that winding. This will also allow the use of a single or double button carbon microphone. Anyone wishing to tackle the hum problem can lick it in this way.

I chose a 6E6 for the driver tube, as it is a low-µ dual-triode tube and works well enough with transformers designed for 45's. It is not a perfect match but is near enough to work well at voice frequencies. I would rather drive the modulator tubes with a transformer than with a resistance-coupled phase inverter. The 6E6 looked like the answer, since I had the push-pull transformers for 45's. It was. The driver trans-

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Fig. 3—Wiring diagram of the modulator unit.

- C1—0.001-mfd. mica.
- C2—0.01-mfd. paper.
- C3—10-mfd., 10-volt electrolytic.
- C4—50-mfd., 25-volt electrolytic.
- C5—0.1-mfd. paper.
- C6—0.001-mfd. mica.
- C7, C11—8-mfd. electrolytic.
- C8—0.25-mfd. paper.
- C9—24-mfd., 450-volt electrolytic.
- C10—16-mfd., 450-volt electrolytic.
- C11—20-henry filter chokes.
- C12—200-ohm, 1/2-watt.
- C13—200-ohm, 15-megohm.
- R1—50,000-ohm.
- R2—500-ohm, 1/2-watt.
- R3—1,000-ohm.
- R4—0.5-megohm volume control.
- R5—0.15-megohm.
- R6—50,000-ohm, 1/2-watt.
- R7—200-ohm, 1/2-watt.
- R8—2,000-ohm, 1/2-watt.
- R9—400-ohm, 2-watt.
- R10—200-ohm, 2-watt.
- R11—50,000-ohm.
- R12—5,000-µfd. paper.

Resistors are 1-watt except where otherwise specified.

- T1—Microphone input transformer.
- T2—Push-pull input interstage transformer.
- T3—Driver transformer (45's to Class-B 10's).
- T4—Modulator output transformer.
- T5—Plate supply transformer 350-0-350 volts at 150 ma.
former used was for 45's to class B 10's. Using it for the 6F6G's in class AB1 works nicely, and this saved the cost of a new driver transformer.

By "trying," one finds that the equipment around the shack will sometimes work, but not always. By this time the reader has seen that the transmitter and modulator are in reality junk-box creations in great part. They do the work, however, and for my use this is the best answer to the question of what is the best portable transmitter. As do all hams, I realize that the answer will change as time comes and goes; but for now, at any rate, it is the answer, and I hope it will be for some time to come.

Credit should be given to Les Grube, W9LEX of Saint Paul, Minnesota, for the mechanical work and mounting of equipment in the transmitter and modulator, as well as a good part of the wiring of the modulator. This equipment is the joint brain-child of W9LEX and W7AW.

Model Three-Element Beam Demonstrated at Pacific-Southwestern Division Convention

One of the most interesting talks at the Pacific-Southwestern Divisions A.R.R.L. Convention held at San Francisco was the practical demonstration of a model 3-element rotatable antenna by Clayton Bane, W6WB. The 100-Mc. 3-element beam was supported on the top of a 6½-foot tower and could be rotated in the horizontal plane and tilted slightly in the vertical plane. The antenna element was fed by a twisted pair, delta-matched at the antenna.

A field-strength meter, designed by Francis Wells, W6QUC, and consisting of a half-wave antenna for pickup and a 30 tube working as a diode rectifier, was used to indicate the signal intensity. It was placed several wavelengths from the transmitting antenna, and a large meter was used so that the audience could easily see the effects of changes in the transmitting antenna.

The power from the transmitter was adjusted so that, with the beam pointed at the field-strength meter, nearly full-scale deflection was obtained on the 0–1 ma. meter used. Rotating the antenna about 30° dropped the meter indication to 0.5 ma., and at 45° rotation the needle was practically at zero. As the antenna was rotated, the needle remained practically at zero until at the back a little radiation showed up, just enough to be readable on the meter. With the beam pointed at the pick-up antenna, a tilt of 20° showed a marked reduction in signal, indicating the sharp vertical pattern of the antenna. Mr. Bane demonstrated the effect of near-by objects by placing his hand near the field of the antenna. The reduction in signal strength showed the im-

![Diagram of Field-Strength Meter](image1)

Fig. 1 — Wiring diagram of the simple field-strength indicator.

- $C_1 = 0.00025 \mu$fd. midget mica.
- $I_1 = 8$ turns No. 14 tinned copper, wound self-supporting with diameter of $\frac{1}{2}$ inch and spaced the diameter of the wire. Opened at center to take $I_2$.
- $I_2 = 1$ turn No. 14, $\frac{1}{2}$ inch diameter.
- $M = 0.1$ ma.
## WAR

It will be the duty of this department during such period as there exists a state of war in Europe, while remaining completely neutral in all respects, to be as complete and accurate as possible a reporter of international events affecting amateur radio.

In these troubled times, when rumors fly fast and even facts change from day to day, it is not feasible to label any international data as correct or complete. However, we have compiled from a myriad of various sources the information appearing below. We emphasize that these may not be facts, but are merely abstracts of current available data at the time of publication.

The following countries are off the air as belligerents: G, GI, GM, GW, F, SP, VE, VK, YM and ZL. All the innumerable colonial possessions of the British and French empires are also off. Apparently purely as a precautionary measure, ON and PA hams have been closed down; in fact, the Belgians seem to have been the first amateurs to be put off. Portuguese amateurs received orders to close down September 12th, except that the Swiss amateurs have been closed down; in fact, they hope and expect to continue in the normal way. With the exception of Cuba and Haiti and possibly colonial possessions of belligerents, all of South and Central America are unaffected. In Canada, amateurs are completely mobilized. We assume that amateurs were generally interfering with broadcast stations and using excessive power, and was represented as not related to the war situation. Haitian amateurs were closed September 13th, "to prevent any possible violation of neutrality." Advice is that the closing is temporary, to provide time to look the licensees over; most of them are expected to reopen soon "under certain restrictions."

South African amateurs remain on the air in full force. They tell us their government has simply taken no action towards them and that they hope and expect to continue in the normal way. With the exception of Cuba and Haiti and possibly colonial possessions of belligerents, all of South and Central America are unaffected. In Canada, amateurs are cooperating with their government in monitoring activities - not the amateur bands alone, but an extensive portion of the spectrum. They are also assisting in the construction and operation of radio stations. Word comes that the Swiss amateurs have been completely mobilized. We assume that amateurs in all belligerent nations are in some manner serving their countries.

We are mildly surprised at the scarcity of news from our members. We had expected some delay in the handling of international mail, but not the complete lack of it. Outside of the item next below, we are appallingly devoid of news on the activities of our European member-societies since the first of September.

### R.S.G.B.

We welcome the news that the Council of the Radio Society of Great Britain unanimously voted for continuance of the organization even in the face of present disrupted conditions. It is planned to continue monthly publication of the society's journal on a small scale. The QSL were generally interfering with broadcast stations and using excessive power, and was represented as not related to the war situation. Haitian amateurs were closed September 13th, "to prevent any possible violation of neutrality." Advice is that the closing is temporary, to provide time to look the licensees over; most of them are expected to reopen soon "under certain restrictions."

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### R.S.G.B.

We welcome the news that the Council of the Radio Society of Great Britain unanimously voted for continuance of the organization even in the face of present disrupted conditions. It is planned to continue monthly publication of the society's journal on a small scale. The QSL were generally interfering with broadcast stations and using excessive power, and was represented as not related to the war situation. Haitian amateurs were closed September 13th, "to prevent any possible violation of neutrality." Advice is that the closing is temporary, to provide time to look the licensees over; most of them are expected to reopen soon "under certain restrictions."

South African amateurs remain on the air in full force. They tell us their government has simply taken no action towards them and that they hope and expect to continue in the normal way. With the exception of Cuba and Haiti and possibly colonial possessions of belligerents, all of South and Central America are unaffected. In Canada, amateurs are cooperating with their government in monitoring activities - not the amateur bands alone, but an extensive portion of the spectrum. They are also assisting in the construction and operation of radio stations. Word comes that the Swiss amateurs have been completely mobilized. We assume that amateurs in all belligerent nations are in some manner serving their countries.

We are mildly surprised at the scarcity of news from our members. We had expected some delay in the handling of international mail, but not the complete lack of it. Outside of the item next below, we are appallingly devoid of news on the activities of our European member-societies since the first of September.
Bureau will now be handled by Arthur O. Milne, 29 Kechill Gardens, Hayes, Bromley, Kent, to whom all cards confirming past contacts with English amateur stations should be sent. The registered address of the society will continue to be 53 Victoria St., London, S. W. 1, to which all correspondence should be sent, but actual headquarters operations will be carried on from the private home of the secretary-editor. It is unfortunate that the extended plans for the 1939 convention had to be cancelled.

**KIEL CONVENTION**

The D.A.S.D. were more fortunate than the British society in that their convention was scheduled in May of this year. The primary purpose was to provide those interested in amateur radio, especially the officers of the various local clubs, with an opportunity to become familiar with recent technical developments and to familiarize anyone who might be interested with the details of naval and marine transmissions. Organizational details, it was pointed out by the president, which had required so much time in the past year, were now completed and members could in the future again devote their time to the technical aspects of short-wave communication — the primary purpose of the society. Encouragement was given to all those interested in ultra-short-wave transmission to carry on experimental work. A committee was organized to aid all amateurs interested in television.

**NEW GUINEA**

In this "world's largest island" is a little group of amateurs who formed the New Guinea Amateur Radio League as an affiliate of the W.I.A. From an interesting letter, we learn that the country is very volcanic and mountainous; rainfall is quite heavy and in some districts reaches as high as 200 inches annually. This makes road construction difficult and landslides make it expensive, so that most of the transport about the interior is by air. The fact that the amateurs are so scattered and that normal communications services between districts are scarce — no roads, telephones or telegraph — makes amateur radio extremely valuable. The 40-meter band is the only one useful to them for local work, as 20 is out on account of skip usually and 80 and 160 mostly unworkable on their low power owing to QRN. Says President Williams, "There are only a few of us, we are widely scattered about the countryside, and when the 'wind' is with us we go over your way. In addition, we QSL 100%." Too bad that all this now has to be written in the past tense.

**W.A.S.**

The W.A.S. award is no easy accomplishment for American amateurs, and it becomes a mark of special distinction when a foreign station achieves it. We publish below a list of stations, excluding those on the North American continent, who have received the award. Italics indicate all contacts made by radiotelephone:


**SWL BUREAU**

The territory announced in our last issue as being covered by Mr. Mayes is now being handled by Edwin Goodbout, 503 N. Genessee St., Waukegan, Illinois.

**Wide-Range Tank Circuit**

(Continued from page 39)

This general type of inductance-and-capacitance variable tank may be useful for crystal oscillator plate circuits, grid and plate tuning of the r.f. amplifiers and frequency multipliers, and for some types of antenna tuning as well. It need not be limited to the three bands mentioned above, but no doubt could be adapted to any three consecutive bands except possibly in the u.h.f. range.

**Strays**

Grooved forms for space-wound high-frequency chokes can be easily made by running a half-inch die or threader over half-inch hard-rubber tubing.

-W8PUY

**November 1939**
DIRECTION FINDING WITH R.C. PORTABLES

Here is an idea that I think might be of interest to those amateurs who also enjoy boating. The recent trend toward the carry-about radio has produced a receiver having characteristics desirable for a direction finder on board small water craft. Any of the several makes of these self-contained receivers may be used to take bearings on broadcast stations to determine position while at sea. To do the job, the receiver is mounted on a rotatable platform up above any surrounding metal objects. On top of the receiver is mounted a good compass the case of which is fastened so as to rotate with the receiver. Watch out for the speaker field.

To calibrate first the apparatus it will be necessary to determine accurately the directions from your port to two or three local broadcast stations. After doing this, tune in one of those stations and rotate the receiver until the signal is absolutely the weakest and set the compass case to read in the same direction as the known direction. Check two or more stations in other directions and make corrections if necessary.

These receivers are bi-directional and sometimes will not work the same off both sides so always remember to use the same side of the receiver when taking bearings as used when calibrating the compass. Don’t try to navigate by dx stations because their signal paths often are not in the true direction of the antenna. With accurate bearings it is possible to determine your position within ¼ mile from signals 70 to 100 miles away.
—— Francis L. Sherwood, W8NCM

ROTATABLE ANTENNA SUPPORT FROM AUTOMOBILE PARTS

In March QST, W5EOW described a bamboo fishpole rotating antenna for 20 and 10 meters. One was constructed and found to perform admirably as far as contacts were concerned, but it did not stand up in heavy northern weather as well as it might have. After considerable experimental changing, a welded steel channel support was developed to hold the bamboo poles instead of the original wooden platform; also a short center pole was added. Both of these changes effectively increased the rigidity and strength of the unit without exceeding by more than $5.00 the original cost or impairing the performance in any way.

A Model-A Ford front wheel brake drum (welded steel, not cast-iron type) with associate roller bearings, races and spindle was selected for the foundation. Thus, with one trip to the junk yard, half the work in the antenna is completed and you have no worries about this strong, easily rotated assembly when the winds blow. All that remains are the four bamboo poles (18-ft. poles are used instead of the 22-ft. length), a bamboo pole 9 ft. in length for the center support, four steel channels 1½" by ½" by ¾", each 2 ft. long; about 6 feet of ⅛" by 1" steel band for braces; two pieces of wood 1" by 2¼ 4 ft. long for the center pole, miscellaneous bolts and nuts, rope, antenna wire and insulators. The channel size is correct for bamboo poles up to 1½" diameter. The poles are lashed with wire to the channels in two places. Strap bolts can be used but are not necessary. When purchasing the brake drum and spindle, be sure to include the spindle nut and the dust cover for the drum housing.

The big job and the heart of the antenna is the brake drum. The sketches of Fig. 1, A and B show how the channels and associated parts are orient-
tated, braced and welded. Cut the channels to a length of 2 ft., weld the 4" separators, then weld to the brake drum. After welding, bend the channel about 3 inches away from the drum with an acetylene torch. Raise the channel to the proper angle by holding a wood block 6 inches long under the ends of the channel and at the same height as the top of the drum. This method enables you to gauge the bend of the channel while heating, and is simpler than bending all four channels before welding to the drum. The rise of the channels given is the best for holding the bamboo poles in position and should not be raised or lowered without changing the height of the center pole. Measure, cut and weld the long 1½" by 1" steel braces after the channels are bent into position. Electric weld all parts to the hub if possible, otherwise use an acetylene torch. The channels are bent with the acetylene torch. While at the welder, have the lugs burned off the spindle. This sounds like a lot, but your bill should not run over $3.00 for welding. Also include the two 6" pieces that hold the center pole. Drill the holes before welding. A third piece, same size, is welded to the drum. The piece is used to hold a short length of 1" by 2" that keeps the feeders away from the drum. If you prefer, slip rings could be welded on the hub of the drum. It is a good idea to use a dirt cover (hub cap) over the spindle. Assemble the center pole and support first. At this point the bamboo poles are raised and laid in the channels. They can be moved up or down the channels or rotated to get all uniform and can then be lashed securely to the channel with wire.

The antenna can be rotated by means of a turn of rope around the drum or by two ropes attached to the ends of the channels. The choice depends on the location and to what extent you wish to go with the controlling mechanism. Only 180-degree rotation is required.

Two coats of paint are recommended for the steel drum and other parts. The bamboo poles should last several years if kept varnished each year, or you won’t have to worry about them if you don’t care about a 25-cent replacement once a while. All changes can be made at the center of the antenna so if your mast is sturdy enough to climb, a new bamboo section can be wired in place in a few minutes.

— Edward E. Schultz, Jr., W9UHA

MEASURING RADIO-FREQUENCY POWER OUTPUT

Of the several available methods for measuring power output from a radio transmitter, only one has received any considerable attention in the literature of amateur radio. Most “hams” are familiar with the use of incandescent light bulbs, in conjunction with a calibrated photometer or a visual estimation of “normal brilliance,” for the approximate determination of power output. Our experience with the difficulty of getting an impedance match between the output of the transmitter and the lamp bank load, with the inaccuracy of visual estimation of brilliance, and with the expense of photometric indicators, led us to try an alternative method for measuring the power output from our transmitter.

The theory of the method is based on the fact that there are quantitative relations (1) between the power output of the transmitter and the rate at which it produces heat in a resistive load, and (2) between the rate of heat production in the load and the rate of temperature rise of the load. The first of these relations is expressed by the formula, \[ W = 4.18 C_2 T_c \] where \( W \) is the power output in watts, and \( C_2 \) is the rate of heat production in calories per second. The second relation is expressed by the formula, \[ C_2 = \frac{M_T}{60} T_c \], where \( C_2 \) is as above, \( M_T \) is the equivalent mass of the heat absorbing system in grams, and \( T_c \) is the rate of temperature rise in degrees centigrade per minute. The equivalent mass of the heat absorbing system is found by multiplying the mass of each component of the system which absorbs heat by its specific heat, and adding the separate products. The two formulas may be combined into the following, \[ W = \frac{4.18 M_T}{60} T_c \]. The application of this formula will become clearer when we trace its use in a specific problem.

The apparatus used for making the power measurements is shown in the photograph. The calorimeter cell on the left is a pint fruit jar. It is

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covered with a rubber cap, which is sold in dime stores for opening fruit jars. Holes drilled through the cap fit snugly about the thermometer and electrodes, holding them in position. The stirrer, of course, moves freely. A dime store Fahrenheit thermometer may be used, provided that the temperature changes indicated on it are multiplied by .56 to convert them to centigrade changes. Arc carbon electrodes are preferable to metallic electrodes because of their freedom from electrolytic attack. A second rubber cap, cut in quarters, tacked to the baseboard, and bound at the circumference with friction tape, forms the support of the jar.

The fluid in the jar is water. Its impedance is varied to match the loading of the antenna by varying the amount of dissolved salt or mineral matter it contains. Our first thought was to match the impedance by raising or lowering the electrodes, but we found that the variation obtainable by that method was very slight. Since our transmitter works into a voltage-fed antenna, the impedance of the cell had to be kept rather high. For measurements on 20 meters, we found that city water, plus a little salt, would do the job nicely. On 40 meters it was necessary to add some distilled water to the tap water, and on 80 meters, almost pure distilled water was necessary. The cell as constructed has a capacity of about 50 µfd. In order to make it present a purely resistive load to the transmitter it was necessary to connect a parallel resonant circuit across it. The circuit is adjusted by tuning the condenser for minimum plate current. If you have a suitable condenser in the junk box, the entire apparatus can be constructed for less than one dollar.

In order to understand the use of this apparatus let us follow through an actual case of power measurement on 20 meters. The grocer’s scale tells us that the jar, stirrer and electrodes weigh about 12.8 ounces. (We let the exposed portions of the stirrer and electrodes make up for the immersed part of the thermometer, in figuring the weight of the heat absorbing materials.) Since one ounce equals about 28.3 grams, we figure the weight of the jar and accessories to be 362 grams. Taking 0.16 for the specific heat of the jar and accessories, we get approximately 58 grams (362 × 0.16) for the equivalent weight of the jar, stirrer and electrodes.

A convenient volume of water to use in a pint fruit jar is 12 ounces. (The XYL’s kitchen equipment comes in handy for measuring this.) One ounce of water weighs about 29.6 grams. This gives us 355 grams for the weight of the water. Since the specific heat of water is 1, its equivalent weight remains 355 grams. Adding this to the 58 grams previously obtained, we have 413 grams for the equivalent mass (M_r) of the heat absorbing system.

When this value is substituted in the formula

$$ W = \frac{4.18 M_r T_r}{60} $$

and the expression simplified, we get

$$ W = 28.8 T_r $$

This formula can now be used for each measurement made, without repeating the preceding calculations.

We are now ready to make the actual measurements. By adding salt to the tap water, the resistance of the cell is adjusted so that the plate current in the final with the watt meter connected is the same as when the antenna is connected. The cell is then cooled in running water or in the refrigerator until it is five or ten degrees cooler than room temperature. By continuing the measurement until the temperature in the cell is five or ten degrees warmer than room temperature, we balance out the effect of loss or gain of heat from the surrounding air.

With the cooled cell back in place, the transmitter is turned on and the initial readings of time, temperature and plate current are taken. When the temperature has risen to about five degrees above room temperature, we take the final reading of temperature, time and plate current. Here are the results:

<table>
<thead>
<tr>
<th>Time</th>
<th>Initial</th>
<th>Final</th>
</tr>
</thead>
<tbody>
<tr>
<td>Temperature</td>
<td>8:47</td>
<td>8:52</td>
</tr>
<tr>
<td>Plate Current</td>
<td>147</td>
<td>155</td>
</tr>
</tbody>
</table>

Since the temperature changed 12.7 degrees in five minutes, $T_r$ equals 2.54. Placing this in the formula $W = 28.8 T_r$, we obtain 73.2 watts for the apparent power output. One correction needs to be applied to this value to get the true power output. Not all of the power output has gone into

(Continued on page 108)
IT REALLY WORKS!

Ruthilda, Sask.

Editor, QST:

It only interest you to know that, through extensive experiments carried on in our laboratory, we have finally developed an entirely new system of radio transmission, one that is notable because of its simplicity and economy.

Briefly, the system requires but a few parts to put into operation, as follows: (A) one tomcat, (B) one neon bulb, (C) a system of exciting tomcat. Procedure is as follows: Stroke tomcat at a steady rate of fifteen strokes per minute, and apply neon light to tomcat's nose. Considerable r.f. will be obtained. Connect resonant antenna to cat's tail, with key in series. If cat is properly excited resulting note will be quite similar to some heard on the amateur bands. Two tomcats in pushpull would be more desirable, but perfect match must be had. Power output goes up as speed of stroking increases, but excitement must be controlled.

Room lighting effects may also be obtained through this same system of applied neon light. A very peaceable cat must be obtained, however, otherwise results may be varied.

H. A. Walker, VE4BN, and W. N. Veale, VE10Q

CUT-THROAT COMPETITION

920 Eighth Ave., Brooklyn, N. Y.

Editor, QST:

During recent years which have brought great developments and technical advances in radio, and at the same time the most severe depression in American history, I have regretfully watched the art being exploited by a few to the detriment of all. Cut-throat competition is the most common way of referring to the practices I mean, though I feel that the expression does not begin to paint a full picture of such practices, or their far-reaching consequences.

One manufacturer will bring out a piece of equipment, a receiver, for example, which will do something that no other receiver has ever done; it has wider frequency response, it tunes with a single control, it receives short waves, or perfect match must be had. Power output goes up as speed of stroking increases, but excitement must be controlled.

Room lighting effects may also be obtained through this same system of applied neon light. A very peaceable cat must be obtained, however, otherwise results may be varied.

H. A. Walker, VE4BN, and W. N. Veale, VE10Q

WHO HAS THE DOPE?

Bruni, Texas

Editor, QST:

How many of us have at one time or another thumbed through our lengthy files of QST in search of a remedy for either transmitter or receiver trouble? I should judge a great many more than there are members of the League.

I am eighteen miles from any commercially-available a.c. My power supply consists of a 5-kw. single-cylinder engine coupled to a 3-kw. a.c. generator with several VS fan belts. The voltage stays on the mark, and an electric clock keeps time.

But someday my 110-volt a.c. will fail. Someday I'm going to need help when the exciter or the generator "goes soft." No doubt I will again resort to my old thumb-worn copies of QST for a cure.

Surely some ham knows how to re-wind generators, or what to do when brushes start cutting the collector rings. Or has found that taking the end play out of the shaft will cure QSN.

And you fellows in the A.R.R.L. Emergency Corps — if the armature gets soaked, just how long will you have to bake it, and how hot do you dare get it? Let's not keep such an art a secret. If the solutions to my problems can't be found in QST, I'm sunk. I can't run and ask Charlie; I've had only one personal QSO with a ham in five years, and he didn't understand generators.

Let's have some dope.

D. A. Nightingale, W5EGV — ex-W5ETH

PRIDE

Bethany, W. Va.

Editor, QST:

Enclosed find check for membership in A.R.R.L. I am a new ham and hope that I may uphold the traditions and practices of the League. I happen to be a college professor and mayor of the city, but I am more proud of my ham ticket than any honor I have ever received. Guess I appreciate it because it really took hard work to get it. (Teaching college biology does not help one much with code and radio theory.) Well, I now have the old ticket and hope that I can take my place among the fine bunch of fellows on the air.

W. J. Swanspetine, W3TID

November 1939
Current Activities. Operating features arranged by A.R.R.L. are open to every licensed amateur. The opportunity offered in the 2ND U.H.F. CONTEST, November 4th and 5th, is given full announcement elsewhere in this issue. S.C.M.'s are taking steps to have u.h.f. stations on the air these dates in every part of the country... a chance for everybody to make new contacts, which in turn gives everybody a score. THE 10TH A.R.R.L. SWEETSTAKES (November 11th-12th and 18th-19th) also announced in this issue, needs no introduction! Long a major activity, the all-Section opportunities create unparalleled W.A.S. opportunity. Many who find the DX bands less intriguing, with amateurs of so many countries off the air due to the war, will find a new high in operating success and fraternality through the "SS."

The Navy Day Receiving Competition will be well worth the attention of every real amateur, too. Announcement was on page 20 of last QST. Be at your receiver on the early evening of October 27th. We'll look for your reports on all the above.

Neutrality Responsibilities of Radio Amateurs. The subject that transcends all others to us amateurs in importance is that of our special responsibilities not alone in keeping neutrality in operating, but also in conducting our radio operating so it is constantly above suspicion, requires no investigating of visitor-talk or other activity, and is completely in accord with F.C.C. regs. The President has proclaimed a limited national emergency with life-and-death powers (almost) over many things that are important to the whole country, and this power, if necessary, may touch us. The President said to Congress, however, that there was no need for further executive action at this time. Only if and when conditions justify and force such government steps, we are told, will the government feel obliged to adopt special restrictions on communications. The League must warn amateurs, however, that the full continuance of our amateur radio depends on our perfection in adhering to our regulations, at the same time we are watchful of the neutrality content of our communications.

F.C.C. Warning. The Federal Communications Commission has announced the suspension of two amateur operator licenses (Bruce A. Koppenhaver, W3FSU, Pottstown, Pa., and Albert E. Chatel, W1DIF, Wales, Mass.) and with these suspensions for communicating with an unlicensed station in one case, and for permitting unlicensed operators to use equipment in another, the F.C.C. issued a warning to this effect: That any further unauthorized activities by amateur stations during the period of the European war may tend to bring about the curtailment of amateur operation generally, that the Commission now regards it doubly necessary that United States amateurs observe their regulations closely, and the Commission urged all amateurs to take steps at once to prevent any new deviations from regulations. We might add that the F.C.C. imposed heavier than usual penalties in these cases.

The continuance of amateur radio in the United States apparently depends on perfect observance of all F.C.C. regulations and strict observance of neutrality. Our A.R.R.L.-amateur neutrality code has been published. All amateurs must make it their personal business to notify and warn any operator mentioning matters related to war, or engaging in any improper or irresponsible radio work or action. A neutrality code is not alone enough assurance that restrictions will not be invited by amateur stations. There must be perfect compliance with every F.C.C. regulation. Each licensee must show himself truly a highly responsible operator and citizen. The F.C.C. stated that in one case of suspension the licensee "willingly and knowingly allowed an unlicensed operator the use of his station." In the other case the amateur "communicated with an unlicensed station" (not permitted under Sec. 152.14, F.C.C. regulations). Why are these examples emphasized by the F.C.C.'s warning? What practices might be especially dangerous while we maintain our war neutrality?

As we see it, our government knows that we have passed tests of citizenship and technical qualifications. But if, contrary to our regulations, we work "uncertified" people who may not be citizens or persons whose responsibility has been certified by a government, the responsible agencies may feel obliged to check into what is going on. Radio communication, remember, jumps over county, state, national, and continental boundaries. It is international in its potential effects.

There is surveillance. Every communication we make, every station we contact, is subject to surveillance by designated agencies. At all times when operating we should bear this in mind. Common sense requires that no amateur shall allow anybody without proper license to use his set. No sensible amateur wants to personally receive heavy penalties, or be responsible for a government order that injures all of amateur radio.

It is recommended that two-way work with European, and especially belligerent nations' amateurs (in any continent) be avoided. We urge that amateurs not quibble over technicalities to

QST for
justify border line work. We should avoid provocation of suspicion by refraining from even harmless work with unauthorized or neutral stations. It is best not to work any D's, F's etc. heard intermittently on the air. We recommend that you do not. The steps to adopt a neutrality code have already paid dividends in “safety” and it seems to me that as the situation worsens in continued months of war increasing the strains on neutrality, we must sensibly follow additional reasonable precautions as above recommended.

The international situation changes rapidly from day to day. Sinkings, propaganda scares, military reports follow one another. Reports will yet concern illicit radio activity, and we amateurs do not wish to be even remotely mixed up with such. We have had our warning. Let us remember there is surveillance, be watchful, and be completely law abiding amateurs.

It is also especially important to limit anything unlicensed persons may say over one’s mike! Keeping strictest neutrality is of vital importance to our country and our own future. These are in reality war times. If any actions of any amateur are of a type indicating potential danger to our security as a people, or positive un-neutrality, the government may be expected to live up to its advance warning, to prevent repetition of such incidents. See that your contacts are not with questionable stations, or provocative of suspicion or investigations, but that in every operating word and act, your hamming does comply to the letter with regulations, and will bear closest scrutiny or surveillance.

The other day an S.C.M. wrote us that an amateur in his jurisdiction allowed a stranger entirely clear of 'em! It got the entire concept of asking us to violate our neutrality code. To a belligerent, directly or otherwise, and had best keep with a foreign tongue, which he admitted he could not understand, to work direct by voice with a foreign country (South America) for some time. This fellow sincerely regretted his action, when the possible criticism of his individual operator's judgment was pointed out to him, and he of course promised full cooperation with the S.C.M. (W2GVZ). There is a job to be done in proper advising every operator who has not yet got the entire concept of his responsibilities in these times.

--- F. E. H.

BRIEF

One F-station heard in the amateur band was reported as a propaganda-giving station. Just as we go to press it becomes apparent that two legitimate-sounding L-stations that have been working two-way with U.S.A. in our band are apparently stations of government agencies. They ask those they work about the war, pump for information on public reactions, feelings, etc. In other words they are asking us to violate our neutrality code. We must watch and have nil to do with any such. We must not give information to a belligerent, directly or otherwise, and had best keep entirely clear of 'em!

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PRIZES FOR BEST ARTICLE

The article by Mr. Carl C. Drumeller, W9EHC * wins the C.D. article contest prize this month.

Each month we print the most interesting and valuable article received marked “for the C.D. contest.” Contributions may be on any phase of amateur operating or communication activity (DX, phone, traffic, rag-chewing, clubs, fraternalism, etc.) which aids constructively to amateur organization work. Prize winners may select a 1939 bound Handbook, QST, Binder and League Emblem, six logs, eight pads radiogram blanks, DX Map and three pads or any other combination of A.R.R.L. supplies of equivalent value. Try your luck. Send your contribution to-day.

How to Operate Well

BY CARL C. DRUMELLER, W9EHC *

1. Before the call:
Listen over the band, especially in the half (low-frequency or high-frequency) of the band in which your transmitter is located. Your chances of making a contact are better if you answer someone's CQ than if you send out a CQ yourself. If you have a low-powered transmitter and a good receiver, do not waste your time and cause interference by calling weak stations. Make sure that you will not interfere with any local station that is already operating; be courteous.

2. The call:
A. In answering a CQ, time the length of your call by these factors:
   a. The number of stations that can be heard in your end of the band; the more stations, the longer your call should be so that the station will have time to tune you in.
   b. The nearness of your frequency to the edge of the band. The other operator will start tuning from the edge of the band nearest his frequency; therefore if his frequency is near the high-frequency edge of the band and yours is very near the high-frequency edge, a very short call should be all that is necessary. If the station does not reply to you or any one else immediately, call again with a short call. Remember that farther your frequency is from an edge of the band, the longer a call you have to make. Do not make your calls too long, for the other operator will get disgusted and tune away.

B. In making a CQ, I recommend a form rather than haphazard calling; it is this:
   CQ QO CQ QO CQ QO DE W9EHC
   CQ QO CQ QO CQ QO DE W9EHC W9EHC
   CQ QO CQ QO CQ QO DE W9EHC W9EHC W9EHC K

I personally use dit dit dit dit between the sections of the call. Most stations merely pause before a repetition of a call sequence. It is not proper to use the "fractional bar," the "break," or the "understand" signal or SI between the identifying call sign and the next CQ group. Note that only the "go ahead" (K) signal follows the call; do not use the "end of message" (AR) signal here; nor should one be guilty of the Hildeman of sending "TWT." However, it is very good form to end up something like this: ... W9EHC ORS COLO QHM K — meaning that the station is an Official Relay Station located in Colorado and that the operator will tune from the high-frequency end of the band to the middle of the band. These signals give the listening operators some definite information that aids in making a reply. The "ORS" means that the

SCM Colorado, 219 East Dale St., Colorado Springs, Colo.
The sign-off: means that the station will handle traffic for that state with a minimum loss of time: the QHM means that it is a station that is reliable and will handle traffic: the “COLO” frequency is in the low-frequency end of the band, he need not waste time calling. Send your CQ at a speed no faster than you can copy solid, for the answering operator will reply at the same speed you use, unless he is otherwise instructed. The A.R.R.L. operating booklet reads (on the subject of calls) as follows: “The general inquiry call (CQ) should be sent not more than five times without interspersing one’s station identification, and the length of repeated calls carefully limited in intelligent amateur operating.”

3. The contact:
After you have contacted the other station by answering its CQ call or by a scheduled call, it is not necessary to make a long call; each station has its receiver tuned to the other’s frequency, and calls can be very short — W9FXQ DE W9EHC — or else omitted. Just remember that you must sign your call at least once every ten minutes or at the end of every transmission (after the SK).

In the context of the first transmission after contact is effected, there is considerable variation. However, there are a few fundamentals to be observed. The call should be separated from the context by a “break” signal (BT): W9FXQ DE W9EHC BT R TNX FER THE CALL OM RST 579X QTH COLORADO SPRINGS COLO BY BT QST OR QST OR QST OR W9EHC K OR: W9FXQ DE W9EHC BT R GLAD TO MEET U OM RST 579X HR IN COLORADO SPRINGS COLO BY BT QST OR QST OR QST OR W9EHC K. One can separate his thoughts into paragraphs by insertion of BT at appropriate intervals. Note that it is not at all necessary (nor is it good form) to send “UR SIGS” before the RST report. It is a matter of politeness to give the other operator an answer to any question, or phone, and let the sign-off take up several exchanges. After you send SK, don’t come back to the other station with anything more than a “ditdid” to let him know that you heard his sign-off. Here’s a sample sign-off: . . . , W2 QST OM JAF DE W9EHC. We call ours the Rebel Net, first because of the historical state, the C.W. sectors of the band at least at “full up.”

We call ours the Rebel Net, first because of the historical state, the C.W. sectors of the band at least at “full up.”

The Kentucky Section

Section Nets Urged to Use “160”

It has been the practice of A.R.R.L. for some years to “register” the frequencies of all operating amateur nets, inviting inquiries from Route Managers, Phone Activity Managers and others, and advising all concerned promptly by advice on frequencies in use, so that all conflicts between Trunk Tones, and A.A.R.S. and N.C.R. or other group frequencies might be avoided in advance choices insofar as possible, and by time-of-operation changes, to avoid mutual QRM. There may be room for one or two spot-net additions to existing nets, but from a practical standpoint, the trunked net will do the job. W9BAZ adds this interesting comment: We call ours the Rebel Net, first because of the historical state, the C.W. sectors of the band at least at “full up.”

W9BAZ adds this interesting comment: We call ours the Rebel Net, first because of the historical state, the C.W. sectors of the band at least at “full up.”

The Kentucky Section is first to set the example by a move to the 160-band. It’s from practical Kentucky operations that we are advised, as above, that a 6L6 and a new rock will do the job.

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W1AW Operating Schedule

OPERATING-VISITING HOURS
3:00 P.M.-5:00 A.M. E.S.T. daily, except Saturday-Sunday.
Saturday — 8:30 P.M.-2:30 A.M. E.S.T.
Sunday — 7:00 P.M.-1:00 A.M. E.S.T.

OFFICIAL BROADCAST SCHEDULE (for sending addressed information to all radio amateurs).

Frequencies
C.W.: 1762.5-3825-7280-14,254-28,600 kc. (simultaneously)

Starting Times (P.M.) Speeds (W.P.M.)

<table>
<thead>
<tr>
<th>E.S.T.</th>
<th>C.S.T.</th>
<th>M.S.T.</th>
<th>P.S.T.</th>
<th>T W</th>
<th>F</th>
<th>Sat</th>
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<td>9:00</td>
<td>8:00</td>
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</table>

PHONE: 1806, 3950.5, 14,237, 28,600

For sending to GENERAL

OPERATING-VISITING HOURS
devotes the following periods, except Saturdays and Sundays to GENERAL

OPERATING-VISITING HOURS

MARKER FREQUENCY TRANSMISSIONS

Sunday- 7:00 P.M.-1:00 A.M.
Saturday — 8:30 P.M.-2:30 A.M.

10:30 P.M.-11:30 P.M., Nat'! Trunk NCS 3670 kc.
8:00 P.M.- 8:30 P.M., Skeds on 80 meters.
6:00 P.M.- 6:30 P.M.
4:30 P.M.- 5:00 P.M.
3:00 P.M.- 3:30 P.M.
2:00 P.M.- 2:30 P.M.
1:00 P.M.- 1:30 P.M.
11:30 AM-12:00 A.M.
10:00 A.M.-10:30 P.M.
9:30 P.M.-10:00 P.M.
9:00 P.M.- 9:30 P.M.
8:30 P.M.- 8:30 P.M.
8:00 P.M.- 8:00 P.M.
7:30 P.M.- 8:00 P.M.
7:00 P.M.- 7:30 P.M.
6:30 P.M.- 7:00 P.M.
6:00 P.M.- 6:30 P.M.
5:30 P.M.- 6:00 P.M.
5:00 P.M.- 5:30 P.M.
25 15 20 20 15 15 25 15 20 15 15

Each code transmission will be followed in turn by voice frequencies.

The station is not operated on legal national holidays.

GENERAL OPERATION:

Besides special schedules in different bands, W1AW devotes the following periods, except Saturdays and Sundays, to GENERAL work in the following bands:

Time, E.S.T.
Frequency
4:30 P.M.- 5:00 P.M. 28,600 kc. Fone/CW
6:30 P.M.- 6:30 P.M. 14,237 kc. Fone
6:30 P.M.- 7:00 P.M. 14,254 kc. CW
8:00 P.M.- 8:30 P.M. 14,264 kc. CW
9:30 P.M.-10:00 P.M. 3950 kc. Fone
10:00 P.M.-10:30 P.M. 14,237 kc. Fone
11:30 P.M.-12:00 A.M. 1702/1806 kc. CW/Fone
1:00 A.M.- 2:00 A.M. 3852 kc. CW
2:00 A.M.- 3:00 A.M. 7280 kc. CW
7:00 P.M.- 8:00 P.M. Schedules on 80 meters.
10:30 P.M.-11:30 P.M. Nat'l Trunk NCS 3670 kc.

Effective Nov. 1, 1939

At other times, and on Saturdays and Sundays, operation is devoted to the most profitable use of bands for general contacts and to participation in special week-end operating activities. The station is not operated on legal national holidays.

Give W1AW a call for an accurate frequency measurement. To communicate with any department of A.R.R.L., to rag-chew when time permits, or to pass a message to ham friends on other places or on other bands.

W1AW is installing what may be amateur radio's largest oven for temperature control of crystals, prepared for starting a schedule of Marker Frequency Transmissions near amateur-band edges. Three of the eight special Bliley BC10 units are shown in front of the thick balsa wood oven to which the General Radio temperature-control equipment will be attached. The control oscillator is in the 1/4" aluminum double-box.

This control unit will be located in one of the completely enclosed racks, near the G.R. 100-kc. standard. From this box a "battery" of 807 frequency doublers feeds the control and exciting r.f. voltage, through links to each of the 1000-watt transmitters. The Headquarters station schedule of Marker Frequency Transmissions will be announced as soon as adjustments of the frequencies are completed for all bands.

---

Puerto Rican Certificate Available!
The Puerto Rico Amateur Radio Club will issue a CERTIFICATE to every amateur having worked twenty-five (25) K4's.

Send complete sets of 25 K4's verification cards with only enough return postage and this certificate will be yours by return mail. Address all communications as follows:

Puerto Rico Amateur Radio Club, P. O. Box 15, HATO REY, Puerto Rico

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Brass Pounders' League

(August 16th - September 15th)

<table>
<thead>
<tr>
<th>Call</th>
<th>Orig.</th>
<th>Del.</th>
<th>Rel.</th>
<th>Credit</th>
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<td>114</td>
<td>290</td>
<td>1174</td>
<td>273</td>
<td>1851</td>
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<tr>
<td>W4PL</td>
<td>15</td>
<td>110</td>
<td>1680</td>
<td>29</td>
<td>1832</td>
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<td>261</td>
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<tr>
<td>W3CIL</td>
<td>52</td>
<td>138</td>
<td>222</td>
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<tr>
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MORE-FROM-ONE-OPERATOR STATIONS

<table>
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<th>Call</th>
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<td>1006</td>
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<td>334</td>
<td>123</td>
<td>40</td>
<td>110</td>
<td>607</td>
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<td>W2SC</td>
<td>22</td>
<td>107</td>
<td>292</td>
<td>103</td>
<td>524</td>
</tr>
</tbody>
</table>

These stations "make" the B.P.L. with total of 500 or over. One hundred deliveries + Ex. Del. Credits also rate B.P.L. standing. The following one-operator stations make the B.P.L. on deliveries. Deliveries count.

W4NLI, 390
W3JMJ, 131
W6JON, 104
W3JH, 105
W6VQI, 108
W4BAS, 129
W1AIW, 129
W3QPY, 254
W9FLC, 111
W3QSC, 122
W9QIL, 129

A total of 500 or more or 100 deliveries Ex. D. Cr. will put you in line for a place in the B.P.L.

---

*Puerto Rican Certificate Available!*
HOW:  

That crack we made last month about changing the name to "Where's DX?" isn't very funny about this time, what with the pickings getting slimmer every day and the answer coming back "What DX?" But carry on, ladles, and we'll tell you what the gang has been doing, if at all.

First, though, let's take a look-see at the set-up across the drink and elsewhere. The OZ's were closed down on October 1st, and HH has been off since September 13th. CO-CM, reported off last month, are expected back on shortly --- their absence is explained by the fact that the regulations are being revised down there and new licenses will be issued. We have heard a rumor that all HB's have been called into service. WIEH worked D&BV the second week in September and was told that not all D's had had their licenses "taken in" but that it was expected --- more surprising was the information that ex-OB and ex-OQ amateurs were being issued D calls, but in Slovakia OK calls still stand.

One PJ, writing to explain why he is off the air, says, "Transmitting is not allowed in time of peace, but now I thought, you know. We W's have to do just the same thing, according to WIWV, but W9HLF tells us the society is branching out to include chapters in Guam (TWG), China (TWC), KA (TWP), etc. . . . HX2GK was in Switzerland right under G"E3AG, one evening around October lat, and HR was talking about chapters in Guatemala (TWG), China (TWC), KA (TWP), etc. . . .

WHERE:

A busy DX month, for the coup DX of the month goes to W2BIIW and W2GVZ for knocking off ACAJS (14,400 T9), right under CB3AG, one evening around 7 P.M. The fellow is sure enough in Tibet and is even DX for W0GRL. First thing you know, the TWA (Tibet Workers of America) will need a bigger club room. While we're on the subject, Wuhl, proxy of the TWA, tells us the society is branching out to include chapters in Guam (TWG), China (TWC), KA (TWP), etc. . . . HX2GK was in Switzerland . . . . . . KGBRZ (14,385 T9) is taking over KB9ILT, according to W1WV, but W9HLF tells us that IIT, RWZ and KB9RSJ (14,385 T9) take turns using RWZ' new receiver, and that IIT is going on 'phone soon . . . . . . W7AYO gives the address of M6W (14,300 T9) as 65, Line Tabogs, P. O. Box 30, Shinkyo, Manchuko. Incidentally, all MX cards can go there for QSP . . . . . . ZL2JQ fooled us again, this time with ZXIA off South America . . . . . . W1BF tells us that, until further notice, all HK's must conduct all QSO's in Spanish. We don't know if this carries over to C.W. and the 5R/7-code type of conversion, but you'd better brush up on your hoohah, just in case . . . . . . This Y6ZC (14,300 T6) has been giving the boys a time. No, we don't know either . . . . . . W2IYO will be glad to QSP your cards to TF3MX (14,350 T3) who QSL's.  

The rig at VU7BR is a GL-907 job running at 28 watts input. The 807 acts as a doubler on either 20 or 10 and, through a matching network, feeds a Zepp with a 200-foot top. The receiver is an HRO.
DANA BACON’s article in last month’s QST on his noise limiter has caused a lot of interest, judging from our mail. One amateur reported that he had installed the limiter in his receiver, and it worked FB. He must have stayed up nights doing it, for his letter was postmarked only a few days after QST appeared.

However, installing a limiter is not a task to be undertaken lightly, and we do not recommend that you attempt it unless you have excellent laboratory equipment and plenty of experience. The difficulties are not just with the noise limiter itself. The performance of the receiver is apt to suffer in other respects when the changes are made unless care and skill are used.

All new receivers of the NC-100 series will be equipped with the new noise limiter. We will install it in older receivers of this series at the factory for a nominal price. Just when this can be done, and what the price will be, we cannot say at this time. We will let you know shortly.

What with the World’s Fair and all, we have had a lot of visitors at our plant this Summer. They are always very welcome, and we hope that any amateurs who find themselves near our plant will drop in to see us. As a matter of fact, you can get a pretty good bird’s eye view of radio manufacturing within our plant, because we make many of the parts we use. This includes almost everything except tubes, resistors and bypass condensers.

If you have any curiosity as to how bakelite moldings are made, or how a high speed winding machine puts the coils on an R-100 choke, this is a golden opportunity to find out. If you want to see a power press blank out the chassis of an NC-100 at a single blow, there it is. If you have wondered what we meant when we said every receiver had laboratory test and alignment, you can see for yourself. You can see the whole works, from research laboratory to shipping room.

You have probably gathered by this time that we are rather proud of our plant. Sure we are. We remember when it was one room about 20 by 20 feet. That was twenty-five years ago (October was our 25th Anniversary). We did not make radio equipment at first, but we were in it among the first. Remember the old Velvet Vernier dial (still going strong) and the DX condenser? Since then, steady growth has brought many changes, and we would like to show you what we have. One reason is that we are proud of it. The other is that we think it will give you a new respect for National Products to see how they are put together.

W. A. READY
For the Finest in Switches
it's
MALLORY-YAXLEY

Yaxley Push Button switches are ideal for meter shunt service as well as for test analyzers, tube checkers and other test equipment.

Here are just two of the many types of switches perfected by Mallory-Yaxley. Each type offers outstanding advantages for circuit application.

This Mallory-Yaxley Hamswitch No. 151, permits the use of a single meter to measure currents or voltages on up to and including five circuits in an amateur transmitter.

P. R. MALLORY & CO., Inc.
INDIANAPOLIS, INDIANA
Cable Address - PELMALLCO

WHAT:
ONE has to be very careful these days before accepting an idea. For example, W3DPA suggests something that, at first glance, looks like a swell thought. Jack thinks it would be a fine thing if we all got together on a "National Non-CQ Week" in the DX bands. This would mean that no W would call CQ on 10 or 20 (we couldn't hope for such a thing on 40!) during that week. Lots of talk has been made about the folly of calling CQ DX, but this would bring it home to those fellows who have been guilty of the waste of time, since they'd have to listen for a change and then they'd begin to work the stuff.

We're against it! Why should we cut our own throats? If the poor guys want to pass up the DX by calling CQ all day long, let them do it. It would just make it tougher for the rest of us if some of those CQ-hounds ever got wise to the fact that they could work ten times as much stuff if they'd listen and call instead of call and listen. If they're too dumb to realize it, we aren't going to tell them. As a matter of fact, Jeffes and I call CQ DX every once in a while, just to throw the others off the track. Say -- maybe that's the way. Let all the DXCC gang keep the air filled with "CQ DX" -- then the others will think that's the way it's worked and they'll never learn, leaving all the choice stuff to us old smarties who have been sneaking a listen all the time.

PHONE:
WIL reports K6ACG (398?) coming through consistently around 6 a.m., and XE6FCG (3934) around midnight, for those who hunt it on 75 . . . . 10 is picking up, and first evidence for the defense is submitted by W6PQW and his QSO with K2KN (28,700). Further evidence is presented by W1WV, who reports K4KOP, K4FOW, ZS6CD and ZS4AA. W1EWH also reports South Africans coming through very well on 28 Mc.

W1LFE has some swell dopes on 20, with stuff like CP1IBA (14,035), OQ5AA (14,060), ZS5Q (14,050), ZS6UY (14,080), W1UQV (14,400), K7BQ (14,210), YU7B (14,400), ZS6AD (14,070), K2KN (14,080) and JSCW (14,075) all tucked away. Heard but not gloomed on to were IMZ (14,080), KAEF (14,095), PK4K (14,095), K4RI (14,100), W6KP (14,100) and K7BQ (14,210) . . . . W2KLV says that the F3GO you heard on, after all the 'J' stations had quit, was really quite OK, having been given special permission by the government to police the DXCC over there. Lew says there is a n.g. F3IC on the air . . . . WI7KX has been knocking it over, too, with ES4G (14,080), OQ5RT (14,035), CX2BK (14,115), H33B (14,100), I1TKM (14,015) and others in the bag. ED would like to see more dope on 'phone in this pillar, duplicating our sentiments exactly, only we have to depend on others sending in the stuff and, no sendee - no DX Contest in spite of some of the countries being inactive.

WHO:
W6QD plans to go through with the November DX Contest in spite of some of the countries being inactive. It should be an interesting contest, since this is the first time that a major one has come around at this time of the year.

The dates, you know, are November 25th-27th and December 2nd-4th, starting and ending at 02 GMT, But don't send your logs to us - send them to Herb and make sure they're postmarked not later than December 15th. Good luck lads will all get cards in time - if they have patience.

K4FCV is up to 104 counties, U9AW giving him the e.g.o. He tries to work as many as possible, but the men . . . . . . WAC, working O22AU, ZS6J, J6CD, W7FMP/7, KAI9H and FY1FM in that time one morning around 2 . . . . . . K4FCV is up to 104 countries, U9AW giving him his latest . . . . . . W6KP tells us he's through down there, but the lads will all get cards in time - if they have patience. He's shutting down because of conditions, and he doesn't mean weather! . . . . . . XU7M1, via W1AB and W1APA, says to please ask the gang to lay off breaking up his QSO's with the a.e.o. He's trying to work as many as possible, but the silly calling on top of a station he's working just slows up everyone. 8M1 has lost several important messages because he hasn't been allowed to finish. We could put in our two cents' worth regarding what we think of monkeys that bust

62
HIGH SENSITIVITY in a communications receiver is only usable when the proper degree of selectivity is also available. If selectivity is not sufficient, no amount of sensitivity will permit satisfactory reception. Here, the new Series 200 “Super-Pro” stands supreme. The extremely high sensitivity available in the “Super-Pro” is always usable because of the continuously variable selectivity characteristics. The I.F. band width control varies the selectivity from approximately 3 kc. to 16 kc.; in addition to this feature, the variable selectivity crystal filter permits the selectivity to be varied from 2½ kc. down to better than 100 cycles. The operator can adjust the selectivity of the new “Super-Pro” to a point where interference is reduced sufficiently to permit reception of the desired signal. This optimum point of selectivity permits the greatest possible fidelity without interference. The selectivity of the I.F. amplifier in the new “Super-Pro” is varied by mechanically changing the coupling between the primary and secondary of the I.F. transformers. This method provides a smooth control of selectivity.

In addition to the above features, the operator of a “Super-Pro” has available such other refinements as: noise limiter; continuous band spread; an AVC system designed for greatest effectiveness; a new adjustable “S-Meter”; two stages of tuned radio frequency amplification which practically eliminate images, and many others. If you want the best, get a “Super-Pro”.

MAIL COUPON TODAY

Hammarlund Mfg. Co., Inc.
492-498 W. 33rd St., N. Y. City
Please send New “Super-Pro” Data.

Name .................................................................
Address ..............................................................
City ................................................................. State

Canadian Office: 41 West Ave.
No., Hamilton, Ont.

Above: Three important selectivity controls. The use of these controls permits the operator to adjust the band width of the receiver to conform with receiving conditions.
THE A.R.R.L.
ANTENNA BOOK
HAS WHATEVER YOU WANT!

Chapters:
1. Wave Propagation
2. Antenna Fundamentals
3. Ground Effects
4. Feeder Systems
5. Half-Wave Antennas
6. Long Single Wires
7. Multiband Antennas
8. Driven Arrays
9. Parasitic Arrays
10. "V" Antennas
11. Rhombic Antennas
12. Antennas for 160 Meters
13. U.H.F. Antennas
14. Special Antenna Systems
15. Finding Directions
16. Supports and Construction
17. Rotating Mechanisms
18. Receiving Antennas

144 pages, in "QST" format.
50 cents, postpaid. No stamps, please!

A.R.R.L.
WEST HARTFORD CONN.

Colorado Hams Make
112-Mc. History!

A two-hour two-way QSO on 2 ½ meters over an air-line distance in excess of 120 miles is an u.h.f. accomplishment in anybody's language. "Bob" Swanlund of W9WYX and his partner in radio, "AI" Suedekum, W9VTK, made this record on August 19, 1939, after some months of planning and testing. During early summer, two transceivers were built, and other local hams, W9DTA and W9VGC, were interested. The whole group had a pile of fun working from house to house, and then from Mt. Genezee to the shack, about 20 miles. There was no trouble working from any place where 56 Mc. had been tried before. In July, W9CKO, an old u.h.f. hand, joined the experimenters.

August 19th "Doo," W9CKO, took his 76-42 rig to Genoa, Colo., a town 105 miles east of Denver, while W9VTK went up Mt. Genezee, W9WYX remaining in Denver, all to run a series of transmitting and listening schedules. W9VTK and W9WYX communicated successfully. All setups were using straight half-wave doublet fed by twisted-pair lamp cord. W9VTK didn't hear W9CKO, but W9CKO heard W9VTK (76-6F6) whistling his call. A review of the results indicated that better antennas might up trans-Pacific traffic, but this paper wouldn't take it, unless they've added more asbestos to it. . . . . I.L.D writes to assure us that I7AA is actually in Ethiopia, in spite of what some of the W's think. Some get the idea that, because I.L.D has been handing the cards for I7AA, they were one and the same station. Frankly, if it hadn't been for I.L.D, none of us would have our I7AA cards. So give him a break, boys, and don't accuse him of putting one over on us. Personally, we know I7AA is in Ethiopia — get W1SE to tell you how we know . . . . . . WSQFL was ZC6JW's first W contact . . . . . Oh, well, if DX keeps up like this we can always change the title to "Remember When." But our grandchildren will never believe us unless we can produce the cards.

— W1JPR

The Tower, location for W9WYX's 120-mile, 2 ½-m. work from Genoa.
There's a good reason for the high signal-to-noise ratio in the "HQ-120-X". The first tuned circuit of any receiver controls the signal-to-noise ratio. When an antenna is coupled to this very important circuit, there is usually a detuning effect. This detuning effect lowers the signal-to-noise ratio. The antenna compensator on the "HQ-120-X" provides a control for restoring resonance, regardless of the effects of the antenna system. In high gain, highly selective circuits this control becomes a necessity if peak performance is to be had. Try an "HQ-120-X" and note its superior signal-to-noise ratio.

An improved highly efficient noise limiter; accurately calibrated main dial; band spread dial calibrated for 80, 40, and 20 meter amateur bands; sensitive "S-Meter" and variable selectivity crystal filter are a few of the other features which have made the "HQ-120-X" one of amateur radio's most popular receivers.

Write for booklet
Short wave reception really means something these days . . . and when it is a bit "frazzly" on the higher frequencies the Radio Serviceman comes into his own. The wise brothers carry Centralab "spares" for satisfactory replacement service, and please the most critical cash customers. So, if you would glean the golden harvest these days . . . see your jobber for sufficient Centralab replacement parts.

**CERAMIC CAPACITORS**
Where permanence of temperature compensation insure and retain stability of frequency in oscillator circuits.

**VOLUME CONTROLS**
In standard or midget . . . a low noise level and smooth attenuation insure reception of faint signals.

**WAVE CHANGE SWITCHES**
Multi-point switching for wave change or tone control . . . with positive low resistance contact.

**TOGGLE SWITCHES**
In communication receivers . . . with crystal filters and wherever delicate supplemental tuning is involved.
The new Hammarlund "HFB" condenser offers the amateur a solution to many difficult problems. The "HFB" is radically different in design from the usual transmitting condenser. The use of isolantite end plates and an insulated control shaft provides greater personal safety to the operator and permits the use of higher circuit voltages for a given plate spacing. This new condenser was especially designed for the circuit shown in the illustration. This circuit was introduced by Ferrill in December 1938 "QST".

All superfluous metal framework has been eliminated in the new "HFB" making it ideal for high frequency operation. Losses are reduced to a minimum through the use of soldered brass plates, cadmium plated. There is no staking, riveting, or clamping to introduce the danger of high resistance contacts. Every joint is securely soldered. The compactness of the "HFB" is another of its many desirable features. The "HFBD-65-D," illustrated, is only 5" long x 1 13/16" square, and is suitable for use in circuits with 3,000 volts applied to the tubes.

See page 38 of October "QST" for an amplifier using the new "HFB". Our 1940 catalog describes a complete line of these new condensers.

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No., Hamilton, Ont.
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40th EDITION OF THE AMATEUR'S BOOK IS READY! $1 POSTPAID

(ILLUSTRATION OF A BOOK BEING HELD)
CATHODE MODULATION

KENYON takes pleasure in offering a series of three low price CATHODE DRIVE modulation transformers. These new and extremely flexible units are designed to match 6V6’s, 2A3’s, 6L6’s, etc. to various class “C” loads between 40 and 3,000 ohms. Impedance matching is not critical and a rather wide variation from the above values will give satisfactory results. This new method of economical modulation was described in the October issue of Radio and should be attractive to those amateurs who have long wished to operate on phone but who have been held back because of the high cost of plate modulation.

<table>
<thead>
<tr>
<th>Type</th>
<th>Max. Sec.</th>
<th>Audio Tubes</th>
<th>Amateur Net Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>T-471</td>
<td>200 M.A.</td>
<td>Single 6F6</td>
<td>$2.40</td>
</tr>
<tr>
<td>T-472</td>
<td>300 M.A.</td>
<td>PP 6V6 or 2A3</td>
<td>$3.00</td>
</tr>
<tr>
<td>T-473</td>
<td>450 M.A.</td>
<td>PP 6L6’s — AB1 or AB2</td>
<td>$3.60</td>
</tr>
</tbody>
</table>

Send today for complete sheet showing various combinations possible and complete technical information. Catalog free upon request.

KENYON TRANSFORMER CO., INC.
240 BARRY STREET • NEW YORK, N. Y.

Oahu Outing

On Sunday July 23rd, the Oahu Amateur Radio Club held an outing at the home of Paul McGauley, K6DTT, in

MEMBERS, DX CENTURY CLUB
The successful use of RCA Transmitting Tubes at far above their specified ratings is an old story to hundreds of experienced amateurs. Such "overloading" has been readily possible because RCA ratings were based, not on intermittent use, but on hard, constant operation in the world's most exacting commercial applications.

Now, thanks to the new "Dual Rating" system for many of the most popular RCA Air-Cooled Transmitting Tubes, you can take complete, fully-informed advantage of the big, extra measure of quality for which these tubes have long been famous. No guesswork. You simply choose the rating most closely approximating your own individual operating conditions and benefit accordingly.

This new RCA System recognizes that amateurs and many other users seldom operate power amplifier tubes under anything like the constant "key-down" conditions on which RCA Class C Telegraphy ratings have been based.

Two sets of maximum ratings are given for each tube, one designated as "Continuous Commercial Service" (CCS) and the other, much higher ratings, as "Intermittent Commercial and Amateur Service" (ICAS).

The CCS (continuous) ratings are essentially the same as the old maximum ratings. They are based on continuous, 18-hour-a-day-or-better service. The ICAS ratings permit much greater power input and a relatively large increase in useful power output for intermittent services. They take full account of the rapid progress in tube and transmitter design, and in tube manufacture and operating technique. ICAS ratings are suitable, for example, for use by the average amateur, who has his transmitter on the air not more than 300 hours a year.

Careful investigation of tube life under these higher ICAS ratings shows decidedly satisfactory results. A tube lasting several thousand hours at the CCS ratings may reasonably be expected to give in amateur service at least several years of trouble-free operation at ICAS ratings.

Thus, the new RCA Dual Rating System represents a big forward step. The new ratings pave the way for the finest tube buys on the market today. They are your keynote to low initial cost with maximum power output PLUS the utmost in real dependability.

POWER TO FIT YOUR NEEDS . . . at Prices to Fit your Rig Budget!

These typical examples indicate the money-saving opportunities in the new ICAS (Intermittent) Class C Telegraph Ratings on popular RCA Tube types:

- **802-R-f amplifier pentode.**
  - Max. plate voltage: 600 V.
  - Max. d-c plate input: 33 W.
  - Grid driving power: 0.3 W.
  - $3.50 Amateur Net

- **804-R-f amplifier pentode.**
  - Max. plate voltage: 1500 V.
  - Max. d-c plate input: 150 W.
  - Grid driving power: 2.2 W.
  - $15.00 Amateur Net

- **806-Tantalum Plate triode.**
  - Max. plate voltage: 3300 V.
  - Max. d-c plate input: 1000 W.
  - Grid driving power: 53 W.
  - $22.00 Amateur Net

- **807-Beam power tetrode.**
  - Max. plate voltage: 750 V.
  - Max. d-c plate input: 75 W.
  - Grid driving power: 0.32 W.
  - $9.50 Amateur Net

- **808-High-mu triode.**
  - Max. plate voltage: 2250 V.
  - Max. d-c plate input: 620 W.
  - Grid driving power: 12 W.
  - $18.50 Amateur Net

- **809-Beam power tetrode.**
  - Max. plate voltage: 1500 V.
  - Max. d-c plate input: 225 W.
  - Grid driving power: 1.5 W.
  - $17.50 Amateur Net

RCA 811 and RCA 812—For details on these amazing new triodes see the RCA announcement on the back cover of this issue.

![RCA Manufacturing Co., Inc., Camden, N.J., a subsidiary of the Radio Corporation of America](image)
It's to your advantage to get the plus performance and extra value of Ohmite Parts for your rig. They do the job right, even under severest operating conditions. That's why they're so widely used in amateur, commercial and broadcast transmitters and receivers the world over.

NEW TAP SWITCHES — For high-current circuit switching. Compact, all-enclosed ceramic construction. 4 sizes from 10 to 75 amperes — 240 V.A.C. ★ POPULAR "BROWN DEVIL" RESISTORS — For voltage dropping, bias units, bleeders, etc. ★ DIVIDOHM ADJUSTABLE RESISTORS — Easily adjustable to resistance you want — or tapped where needed. Ideal voltage dividers. ★ And, of course, there's the Ohmite Dummy Antenna, Parasitic Suppressor, Band Switch, R.F. Plate and Power Line Chokes, etc.

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Write today for Free Catalog 17

—-—

"Contender" Uses Amateur Frequency in Gale

Leaving Saturday, September 23rd, forty-three men, whose interest is in radio, chartered the Yacht Contender (first in the Honolulu race) for a weekend trip to Catalina Island. Three licensed amateurs were aboard, W6ZAA, Garrett Arnold; W6DEP, Larry Lynde, and W6AM, Don Wallace. There was also Dean Hoffman, to go up for license soon, and ten with previous amateur experience. The transmitter aboard the Contender, KLRL-6, was intact from the race, and F.C.C. had been notified of portable locations for use of W6AM for the weekend, with September 25th indicated for good measure (a fortunate bunch). On the trip to Catalina the gang had a wonderful time, and successful 10-meter communication. The 350-watt transmitter also worked on the harbor 'phone frequency of 2738 kc., connected with shore on 2176 kc., and was open to public service on 'phone, c.w.

From our fixed location, amateurs in all districts but two were worked on 10 and 20 meters, including K7PQ (Alaska) on 10. Beams, an Alford array staked to 100 feet above the water line, eleven antennas in all, were available.

Sunday we noticed storm warnings over the weather services just before the scheduled leaving. Captain Dick Loynes, careful skipper that he is, decided to wait for further bulletins. When the gale came from 300 miles at sea there was a battle to save the 75 or more small boats in the harbor. Heavy winds and seas reached tremendous proportions; anchors dragged. When the harbor 'phone and Coast Guard stations could not be heard from it seemed best to look for amateurs to assist us.

We raised W6NCR, 15 miles from L. A., and kept a 100-meter schedule thereafter. His telephone was out of service together with some 30,000 others in southern California. He helped us get W6NZZ (Long Beach) and W6SAL (Compton), who worked Pasadena, so our crew could send messages ashore. Twenty hours of tremendous wind and storm resulted in dozens of missing craft, many dead and unreported, and an estimated million loss due to property damage. Our crowd went from breakfast to breakfast with- out a meal, and few had any sleep during that 24 hours. The Navy in such times of trouble renders greatest assistance to those who may need it. Our first mate asked us to get hold of the destroyer anchored nearby to see if it was advisable for us to return.

W6NZZ (1950-ke. 'phone) got in touch with San Pedro, and the destroyers were asked to guard 8300 kc. for us. NISX, the U.S.S. Arpoe, and NATF, the U.S.S. Wilson, answered our call. Every time we touched the key plenty of answers were forthcoming, as they readily granted our frequency. The channel was reported open for large craft such as the Contender, but smaller ships were advised to stay under cover. KLRR sent some paid traffic through KPH, the RCA station in S. F., using all forms of radio possible around the yacht. Many other yachts, nearby, got radio weather information from us, and copies were even posted on the bulletin boards ashore.

A.E.C. Hams Fight Forest Fire in Black Hills

The sheer indispensability of training in a communications emergency was sharply underscored during July, when, faced by the most devastating forest fire in the history...
NW DIAL. The six-inch NW Dial has an engine divided scale and vernier of solid nickel silver. The vernier is flush with the scale. The variable ratio drive is unusually powerful at all settings. No. 2, 3, 4 or 5 scale.
Type NW. List Price, $15.00

N DIAL. The four-inch N dial has an engine divided scale and vernier of solid nickel silver. The vernier is flush with the scale. The planetary drive has a ratio of 5 to 1. No. 2, 3, 4 or 5 scale.
Type N. List Price, $6.75

B Dial. "Velvet Vernier" Dial, Type B, provides a compact variable-ratio drive that is smooth and trouble free. The mechanism is enclosed in a black bakelite case, the scale being read through a window. No. 1 or 5 scales.
Type B. List Price, $2.75
Illuminator. List Price, $.50 additional.

O DIAL. The Type O Dial is 3½" in diameter and mounts directly on ¼" shafts. The scale is solid nickel silver, and is heavily insulated from the hub. A metal brush for grounding the dial is supplied. No. 2 scale.
Type O Dial. List Price, $1.50

O DIAL LOCK. The Type ODL locking device has a thumbscrew control for clamping the Type O Dial. It is ideal for transmitter applications. Not illustrated.
Type ODL. List Price, $.50

O DIAL DRIVE. The O Dial Drive device, illustrated at the left, is a useful accessory where fixed tuning is desired.
Type ODD. List Price, $.60

HRO DIAL. The HRO Dial is 1½" in diameter and fits 1¼" shafts. The etched nickel silver dial is numbered from 0 to 10 over 180°. The dial is not insulated from the shaft on which it mounts.
Type HRO Dial. List Price, $.75

HRP KNOB. The HRP Knob is similar to that used on the HRO Dial above. It is 1¼" long and ½" wide.
Type HRP. Less pointer.
List Price, $.25

Type HRP-P. With pointer.
List Price, $.35

SHAFT BUSHING. The use of this bushing is recommended wherever long shafts require an extra bearing. It is particularly suitable for use in panels. Fits ¼" shafts.
Type SB.
List Price, $.25

[Table: DIAL SCALES]

<table>
<thead>
<tr>
<th>Scale</th>
<th>Divisions</th>
<th>Rotation</th>
<th>Direction of Condenser Rotation for increase of dial reading</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0-100-0</td>
<td>180°</td>
<td>Either</td>
</tr>
<tr>
<td>2</td>
<td>0-100</td>
<td>180°</td>
<td>Counter Clockwise</td>
</tr>
<tr>
<td>3</td>
<td>100-0</td>
<td>180°</td>
<td>Clockwise</td>
</tr>
<tr>
<td>4</td>
<td>150-0</td>
<td>270°</td>
<td>Clockwise</td>
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<tr>
<td>5</td>
<td>200-0</td>
<td>360°</td>
<td>Clockwise</td>
</tr>
<tr>
<td>6</td>
<td>0-150</td>
<td>270°</td>
<td>Counter Clockwise</td>
</tr>
</tbody>
</table>

HRK KNOB. The HRK Knob is used on the O Dial, the PW condenser and on various receivers. Its comfortable grip and handsome appearance has made it popular on fine instruments. Fits ¼" shafts.
Type HRK.
List Price, $.85
P.O.C.K.E.T  S.I.Z.E
A.C.  a.n.d  D.C.
V.O.L.T-0.H.M-MI.LL.I.A.M.M.E.T.R.E

MODEL
666-H

Size:
3 1/16" x 5 3/8" x 5 1/4"

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Net Price

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THERMO AMMETERS

• Model 446 with Front Illumination. Four-inch square modernistic instrument featuring extra-long scale. Same case available for ammeters, milliammeters, microammeters, voltimeters, millivolts, etc., AC and DC.

WRITE FOR CATALOG

SECTION 2511

HARMON AVE.

THE TRIPLETT ELECTRICAL INSTRUMENT CO.
Bluffton, Ohio

of the South Dakota Black Hills, forestry service officials turned for the first time to A.R.R.L. Emergency Corps bands for auxiliary radio operators in the fire area — and were "entirely satisfied with results."

The fire, well away from the Mt. Rushmore memorial, broke out late on the afternoon of July 10th. Fanned by a 30-mile wind the blaze quickly developed into a "crown" fire, the type most dreaded by foresters, racing from treetop to treetop, and overnight threatening several mining towns in the area.

As soon as the seriousness of the blaze was apparent, Emergency Coordinator Wallace Koppmann, W9YOB, telephoned Forestry Service Headquarters and offered the services of the Rapid City A.R.R.L. Emergency Corps. Within a matter of minutes Peyton Nelson, W9YJX, and Glen Catch, W9APT, were on their way to the fire lines, to be joined later by Jesse White, W9KVN, Richard Probs, W9CVR, and Victor Fite, W9SW.

The forestry service furnished the rigs. Fortified by monthly emergency drills (every licensed member of the Rapid City club is a member of the A.R.C.,) the boys were equal to every demand. In previous fires trained operators had been sent to the lines with simple phone rigs and brief instructions, and results had been haphazard and unsatisfactory.

Efficient communications were a major factor in the low loss of life during the fire. There were only two casualties; one of the crew was killed by lightning while on fire duty, and a salesman was killed in an auto crash attributed to traffic congestion in the fire area. Fifty children were safely evacuated from Camp Wanzer, state tuberculosis camp, and citizens of Hill City and Mystic were warned to be ready to leave those towns on short notice. With the shifting wind, the direction of fire progress was uncertain from hour to hour, and without efficient communication the danger of a shift trapping a section of the fighters would have been grave. Telephone communication in the area was completely paralysed. Approximately 1100 messages were handled during the fire and the "mopping-up" period afterward.

The boys operated on 3155-KC, using as calls the serial numbers of the rigs they were using. W9YJX operated SPF 404 from July 11th through July 17th, W9APT SP 234, SPF 402 and SP 232 from the 11th through the 18th, W9KVN SPF 402 from the 14th through the 17th, and W9CVR SP 402 through the 18th. W9SWV acted as radio liaison between Forest Service Headquarters and Superintendents of South Dakota's vacationland might conceivably be a smouldering, blackened ruin. "It can't happen here!" That's what the boys in Rapid City thought, too — but when it did happen, they were ready. "Nuff said!"

RESULTS OF THE 1939 INTERNATIONAL DX CONTESTS
ESTABLISH THESE SIX IMPORTANT FACTS

1. Of all the DX phone (VE & W) winning contestants use Eimac tubes.

2. Two of the three highest scores in the CW Contest use tantalum plates. As listed in Oct. QST.

3. Of all the DX c.w. (VE & W) winning contestants use Eimac tubes.

4. Tubes with tantalum plates are far superior when it comes to actual performance. First, second and third winners and four out of seven of the entire list of winners used tubes with tantalum plates.

5. Eimac tubes are first choice by the majority of the leading amateurs. Five of the first six winners and five out of every eleven of the winning (VE & W) list use Eimac tubes.

6. Six out of every ten of the (W) sectional winners, as listed in October QST, used tantalum plate tubes and Eimac tubes lead the field in this group five to one.

The fact that 44% of all the winning amateurs in the phone and CW contests use Eimac Tubes should indicate to you that...where performance and dependability are a factor...Eimac Tubes are first choice. (See lists in your October QST.)

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MANUAL
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The 1940 Sylvania Technical Manual is bigger and better than ever with a new easy-to-use arrangement. It has 264 pages packed with vital tube information for servicemen, radio technicians, engineers and amateurs.

It gives you complete data and tube diagrams for 344 types of tubes all now listed in numerical-alphabetical order for quicker reference. Operating conditions, characteristics and circuit applications for standard glass tubes, "G" types, "GT" types, Loktal, Metal, Majestic and special types. Full information, too, on Sylvania's complete line of panel lamps.

The new Manual also includes data on special tubes for particular applications in television amplifiers, cathode-ray tubes, etc., with new circuit information and diagrams covering the latest type tubes.

Send the coupon below for your copy! This new edition is a bargain at only 35c.

W-VE Contest Scores
(Continued from page 41)

<table>
<thead>
<tr>
<th>Score</th>
<th>Preambles</th>
<th>Contacts</th>
<th>Sections</th>
<th>Received</th>
<th>Confirmed</th>
<th>Worked</th>
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<td>DAE</td>
<td>1800</td>
<td>20</td>
<td>20</td>
<td>16</td>
<td>5</td>
<td>7</td>
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<td>ROX</td>
<td>700</td>
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<td>12</td>
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<td>GQX</td>
<td>594</td>
<td>11</td>
<td>11</td>
<td>9</td>
<td>3</td>
<td>7</td>
</tr>
<tr>
<td>BMX</td>
<td>270</td>
<td>5</td>
<td>5</td>
<td>3</td>
<td>2</td>
<td>7</td>
</tr>
</tbody>
</table>

Wisconsin

| W9YDS | 19467 | 103 | 103 | 63 | 7 |
| EYH   | 18144 | 96  | 96  | 58 | 7 |
| RFI   | 13135 | 70  | 70  | 41 | 7 |
| RGM   | 9450  | 50  | 50  | 34 | 7 |
| MBDX  | 7812  | 62  | 62  | 38 | 7 |
| YMG   | 3780  | 30  | 30  | 20 | 7 |
| SKF   | 1530  | 17  | 17  | 14 | 5 |

Dakota Division:

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<thead>
<tr>
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<tr>
<td>W9VJH</td>
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<thead>
<tr>
<th>South Dakota</th>
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<tbody>
<tr>
<td>W9MR8</td>
</tr>
<tr>
<td>YOB</td>
</tr>
<tr>
<td>WUO</td>
</tr>
</tbody>
</table>

Northern Minnesota

| W9VOR | 15876 | 84    | 84    | 54   | 7 |
| DNY   | 1890  | 14    | 14    | 6    | 5 |
| WUQ   | 729   | 9     | 9     | 7    | 3 |

Southern Minnesota

| W9XXO | 12948 | 71    | 71    | 45   | 7 |
| VIP   | 5184  | 32    | 32    | 20   | 6 |
| TVE   | 1440  | 20    | 20    | 4    | 6 |
| KDU   | 769   | 9     | 9     | 7    | 3 |

Delta Division:

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<tbody>
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<td>W5KCK</td>
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<tr>
<td>EJ DK/5</td>
</tr>
<tr>
<td>HTG</td>
</tr>
</tbody>
</table>

Mississippi

| W5FIT   | 2918  | 18    | 18    | 14   | 4 |

Tennessee

| W4FDT   | 1620  | 12    | 12    | 10   | 5 |

Hudson Division:

<table>
<thead>
<tr>
<th>Eastern New York</th>
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<tbody>
<tr>
<td>W2JRG</td>
</tr>
<tr>
<td>EWO</td>
</tr>
</tbody>
</table>

New York City and Long Island

| W2IOP           | 30429 | 161   | 161   | 92   | 7 |
| EGG              | 18711 | 99    | 99    | 60   | 7 |
| IRV              | 14553 | 77    | 77    | 52   | 7 |
| KRU              | 13419 | 71    | 71    | 50   | 7 |
| HUDO             | 11539 | 63    | 63    | 50   | 7 |
| KVY              | 6986  | 44    | 44    | 27   | 6 |
| CRQ               | 3717  | 30    | 30    | 23   | 7 |
| AOD              | 2700  | 25    | 25    | 19   | 6 |
| AQG              | 918   | 17    | 17    | 13   | 5 |
| LFP              | 354   | 11    | 11    | 10   | 7 |
| LPE              | 216   | 4     | 4     | 3    | 2 |
| KWB              | 27    | 1     | 1     | 1    | 7 |

Northern New Jersey

| W2JKE            | 2403  | 127   | 127   | 71   | 7 |
| WC                | 16159 | 85    | 85    | 58   | 7 |
| GSA               | 13041 | 69    | 69    | 60   | 7 |
| HTG               | 7749  | 42    | 42    | 40   | 16 |
| LMM               | 7560  | 40    | 40    | 26   | 7 |
| DRY               | 7036  | 38    | 38    | 34   | 7 |
| HZN               | 4758  | 38    | 38    | 17   | 7 |
| LXT               | 3993  | 37    | 37    | 27   | 6 |
| LUE               | 3560  | 22    | 22    | 15   | 6 |
| JJE               | 2673  | 34    | 34    | 20   | 3 |
| CW                | 2349  | 29    | 29    | 17   | 3 |
| BAC               | 2187  | 14    | 14    | 8    | 8 |
| DZB               | 1855  | 17    | 17    | 10   | 6 |
| JFJ               | 1512  | 14    | 14    | 9    | 3 |
| INJ               | 1080  | 10    | 10    | 4    | 4 |
| KDB               | 540   | 10    | 10    | 5    | 2 |
| JRU               | 270   | 5     | 5     | 4    | 3 |
| HBN               | 216   | 4     | 4     | 3    | 2 |

Midwest Division:

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<tbody>
<tr>
<td>W9QFB</td>
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<tr>
<td>LDD</td>
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<tr>
<td>YQY</td>
</tr>
</tbody>
</table>

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Set-Tested Radio Tubes

HYGRADE SYLVANIA CORP. Q 119
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Here is 35c. Please send me a copy of the bigger and better Sylvania Technical Manual.

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86
The experienced amateur will see quickly enough what we mean by our slogan, "Designed for Application" when he studies the many new and different parts illustrated and listed in our new catalog. If you don’t have a copy yet, be sure and get one from your dealer while his supply lasts. In it you will find new types of sockets that can’t flash over between contacts, that are easy to mount, and that have contacts that will really stand up in hard service! You will also find new types of dials, midget condensers, radically different designs of transmitting condensers, safety terminals, A.C. terminal blocks, Isolantite rectifier tube plate caps, Isolantite bushings, flexible couplings, transmission line spreaders, and a host of other novel, better performing and easier to use component parts.

This remarkable material has made possible, in our No. 15001 neutralizing condenser, a design that is within reason relative to the size of the tube with which it is to be used as well as much less expensive to manufacture and sell.

For instance, the little No. 15001 condenser is ideal for use with such low capacity tubes as the 3ST, the HK24, the HK54, the 907, the 1E3, the T40, the T20, the HY40 and the HY25. For the higher-capacity tubes the No. 15002 takes care of about everything. It actually has a low enough minimum (0.5 µf) to neutralize 6L6s and a maximum of 13.5 µf which is a ratio of 27 to 1!!! Incidentally, though conservatively rated at 6000 v. breakdown, the No. 15002 in a recent test in one of the large Eastern technical college laboratories, took 30,000 volts A.C. to cause a flashover to ground! Even then the polystyrene insulation was not punctured!!!

Aside from the QuartzQ neutralizing condensers and the centre mounted transmitting condensers, the most spectacular item in our line as yet, is the HETROFIL. Ray Woodward’s article in the September issue, plus the illustration at the right, tells the story. Since writing the QST article, Dr. Woodward has done considerably more laboratory work which is incorporated in the commercial model of the HETROFIL. One of the changes pertains to the use of different values for the fixed resistors and condensers so as to eliminate the necessity for the dual range and the consequent complication of switching. Yes, the advertisements last month were correct — the price is only $3.50!!!
WON'T DO

Many times an otherwise f.h. rig will fail to function as it should because of neglect at some minor detail. You can depend on JOHNSON plugs and jacks. Proved by years of acceptance, they always do the job. They love contacts, slide together smoothly, hold tenaciously, release readily.

JOHNSON “Banana Spring” plugs are made in wide variety, from the smallest, No. 75D (with beryllium copper spring, specified for exacting Government requirements), to the heavy duty 77 series. Note the new insulating handles, of generous size, in polished black or red plastic. JOHNSON “Spring Sleeve” types (lower views) are exceptionally rugged, stand heavy currents. Learn more about these and other dependable JOHNSON products.

Ask your Jobber or write for new 2 color Catalog 966J.

E. F. JOHNSON CO.
WASECA, MINNESOTA
MANUFACTURERS OF RADIO TRANSMITTING EQUIPMENT

88
IT is the largest-selling Plate Supply Transformer in the world—the THORDARSON T-19P56! Ten pounds of the most scientifically engineered iron and copper—built with the ruggedness of Gibraltar, to give amateurs dependable service for years. Your favorite Parts Jobber has just the THORDARSON transformer you need for any purpose—transmitter or receiver. Ask your Parts Jobber for Catalog 400-D.

THORDARSON

Elec. Mfg. Co., Chicago

"THERE IS 44 YEARS OF EXPERIENCE BUILT INTO EVERY THORDARSON TRANSFORMER"
Not satisfied with “GOOD ENOUGH”...

There’s a healthy mixture of “experimenter blood” in our organization, and a large portion of the time our lab is devoted to “monkeying around” with new ideas. This notwithstanding the fact that our test equipment units are now recognized as “TOP QUALITY”... every instrument being checked and calibrated against laboratory standards.

Our facilities provide complete facilities for obtaining all measurement requirements for Amateur, Service, Laboratory, Television and industrial users. You are sure to find one to satisfy you... at a price that makes it “tops” in value.

New Precision Series 844—34 Range
AC-DC Volt-Ohm-Decibel-Milliammeter
including ranges of
6,000 Volts AC-DC
10 Megohms
12 Amperes

* SIX A.C. and D.C. VOLTAGE RANGES at 1000 ohms per volt: 0 to 120/300/600/1200 and 2400 volts.
* SIX D.C. CURRENT RANGES: 0/12/120/300/600/1200 MA; and 1/12 Amperes.
* SIX DECIBEL RANGES from 12 to +100 DB.

$44-L Walnut finished hardwood case with carrying handle. (7 x 8 x 4). Less batteries and test leads. Net...
$24.95

DC Volt-Ohm-Milliammeter
Large 3-inch modern D’Arsonval type meter. Wire wound shunts and matched metalized multipliers of 1% accuracy.

* FOUR RESISTANCE RANGES: 0-400; 0-1000; 0-5000; 0-25000 ohms.
* Provisions for mounting Ohmmeter Batteries (4½ and 45 volts) on inside of case.
* SIX OUTPUT RANGES: 0 to 120/300/600/1200 and 6000 volts.

$40.95

* FIVE D.C. voltage ranges at 1000 ohms per volt: 0-10; 0-100; 0-250; 0-500; 0-1000 volts.
* FOUR D.C. current ranges: 0-1; 0-10; 0-100; 0-250 MA.
* Two resistance ranges: Low Ohms (shunt method ½ to 300 Ohms). High ohms 300-500,000. Ohmmeter ranges are powered by self-contained supply. See these two as well as other popular PRECISION Test Equipment models on display at all leading radio parts distributors. Fifteen types and combinations of Math-Maxx Testers and Set Testers... Signal Generators, too... Ask for your 1940 catalog.

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Brooklyn, New York

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W5AQE 9460 50 50 31 7
C3Y 6615 53 53 34 7
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CARDWELL condensers are always "well represented".

CARDWELL condensers never fail to justify their choice for finest commercial equipment, reflecting the prestige of the product of which they become a part.

THE ALLEN D. CARDWELL MANUFACTURING CORPORATION
85 PROSPECT STREET, BROOKLYN, NEW YORK
These Crystals FLUNKED their FINALS!

Somewhere along the line—in perhaps just one particular test, these crystals failed to meet the Monitor quality requirements. They received four tests on activity, four on drift, and four on frequency. They were checked for dimensional activity (which influences output) and against twin peaks. In addition to all these, most Monitor crystals receive ten special examinations for determining characteristics known only to Monitor engineers. Each crystal must pass every single one of these tests before Monitor accepts it.

Most of the crystals above would probably operate satisfactorily in your rig, but, to assure you the finest possible performance, every Monitor crystal must pass above a certain set standard in each of the many tests subjected to it. That's why every Monitor crystal is of the highest possible quality.

By detailed examination of their product, Monitor engineers have won an unmatched position for crystal dependability. That's why commercial interests the world over have specified Monitor crystals for nearly ten years for aviation, marine, and police work. With any of the complete line of Monitor crystals, you are guaranteed better performance, trouble-free operation, and quality higher than the price!

Available at your dealer's or write direct to us.

New Transmitting Tube Ratings

(Continued from page 48)

large increase in useful power output. For example, the a.f. power output of two 809's in Class B is 100 watts at the old maximum plate-voltage rating of 750 volts. At the new ICAS rating of 1000 volts, the power output is 145 watts—an increase of 45 per cent. In plate-modulated telephony service, the r.f. output of the 809 is 38 watts with the CCS ratings and 55 watts with the new ICAS ratings—an increase of about 45 per cent. Complete operating data, including both CCS and ICAS ratings, have been prepared for RCA types 802, 804, 806, 807, 809, 810, and 814, as well as for the new 811, 812, and 828, and can be obtained on request.

"The new system provides transmitting-tube ratings which recognize the diversified design requirements of modern transmitter applications. For example, there are numerous applications where the design factors of minimum size, light weight, low initial cost, and maximum power output are far more important than extremely long tube life. In such cases, the set designer may very properly decide that a small tube operated with ICAS ratings better meets his requirements than a larger tube operated with CCS ratings.

"It is self-evident, of course, that the harder a tube is worked the shorter will be its useful life. Although no rule can be set up which will accurately predict the life performance of an individual tube under specified operating conditions, it is practical to make an estimate of tube life on the basis of average results from a large number of tubes. In average amateur service, a tube operated at the higher ratings can normally be expected to give about 50 per cent of the life obtainable with CCS ratings.

"It has been estimated that an active amateur does not have his carrier on the air more than 300 hours per year. Therefore, a tube lasting 1000 to 1500 hours when used with CCS ratings would give him at least 3½ to 5 years of service. The amateur, because he is usually most interested in low initial cost and maximum power output, may consequently decide that the ICAS ratings are better suited for his purpose.

"The engineer designing a broadcast transmitter has quite a different problem. A broadcast station may operate tubes on an average of 18 hours a day. Tube failures are expensive both in themselves and in advertising revenue lost because of interrupted programs. Consequently, since reliability is his main concern, he should operate tubes at the CCS ratings, or perhaps even lower. Only in this way can he obtain the long tube life required for continuous commercial services.

"In view of the fact that the ICAS ratings are considerably higher than the former maximum ratings, an explanation of the basis on which these new ratings are established is desirable. The old method of rating transmitting tubes has been based on the assumption that tubes would always be used under the most severe operating conditions possible for each class of service. Although..."
THE FOURTH EDITION HAMANUAL
THOROUGHLY DESCRIBES A HOST OF
NEW TRANSMITTERS AND AMPLIFIERS...

INCLUDING THESE TWO:

STANCOR 12-E EMERGENCY TRANSMITTER

The logical answer to the emergency problem.
Low drain operation from a 6 volt DC source.
Crystal control on 1.7, 3.5, and 7 MC bands.
12 watts input to R.F. Amplifier.
Universal antenna coupler — self-contained.
Easy hand shift — phone or CW.

Approximate net price, less coil, tubes, crystal, dust cover and Vibrapack.

$14.50

STANCOR 10-P TRANSMITTER

Unparalleled versatility in a low power rig.
Five band operation (10-160 meters) with but three crystals.
R.F. Amplifier Input — 12 watts phone, 20 watts CW.
Four tubes — only one tuned circuit.
High level modulation — break-in for CW.
Price includes cabinet, escutcheon, etc.

Approximate net price, less tubes, coil, crystal and meter.

$21.00

STANCOR HI-FI TRANSFORMERS

A most exacting transformer in performance and appearance. High Fidelity that really means ultimate in tone quality. A precision product from start to finish. See it at your dealers.

STANDARD TRANSFORMER CORPORATION
1500 NORTH HALSTED STREET
CHICAGO

STANCOR THOROBRED
America’s first safety plate transformer. The only transformer of its kind — anywhere. Your Stancor Jobber has it — be sure to see it.
THAT this expensive bridge
type construction with soft
iron pole pieces could be used in
instruments priced no higher than
the ordinary kind, has been the
marvel of those who know instru­
ment construction.

This finer movement is the
heart of the "Hammer"—the first
self-contained pocket-size tester
built expressly for your needs.
Notice the ranges of this tester
listed opposite. Both A.C. and D.C.
ranges have resistance of 1,000
ohms per volt. It is shock-proof
throughout—test cables are insu­
lated for 5,000 volts; tips and clips
are also heavily insulated. Mea­
suring only 5 1/2 x 2 1/2 x 1 1/4 inches,
and weighing only 20 ounces, the
Hammer is the answer to every
need. When you see it, you will
be all the more astonished at its
low price.

PANEL INSTRUMENTS WITH THE
SIMPSON MOVEMENT COST NO MORE
You pay no more for panel instruments having the Simpson
Bridge Type Movement with soft iron pole pieces. Here are
typical values:

**R.F. AMMETERS**—Internal, thermo-couple radio frequency am­
eters (1 1/2, 2, 2 1/2, 3 or 5 Ams).
Your net price

**HIGH RANGE VOLT METERS**—D.C. plate voltmeters, complete
with external resistors, (1.000 - 1.500 - 2.000 - 3.000 - 5.000
or 10,000 volts).
Your net price

**DECIBEL METERS**—Rectifier type volume
level indicator (—0 to 6 db (200 ohm line; 8 M.W.)).
Your net price

**OTHER OUTSTANDING VALUES ARE**:
D.C. plate milliammeters (all popular ranges
from 0-5 to 0-1,000 milliamps).
List $7.95. Your net price

A.C. filament voltmeters (0-10 or 0-15 V.).
List price $9.65. Your net price

Illuminated dials for all popular ranges, in­
cluding 6 V. lamp, 50c net additional.

SIMPSON ELECTRIC CO.
5210 Kinzie St., Chicago, Ill.

**SIMPSON**
INSTRUMENTS THAT STAY ACCURATE
they may look alike

but

... put to the test, all capacitors are *not* alike. They differ in life span, in number of advanced features, in dependability. Unfortunately the eye cannot see these important differences. There is a way, however, that you can be sure you're getting the all-around tops in capacitor value. Look for the name CORNELL-DUBILIER on the label. Only capacitors bearing this name are backed by the specialized experience of 29 manufacturing years and by laboratory *life tests* for performance—a guarantee of outstanding performance on the job.

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WET & DRY ELECTROLYTICS

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CORNELL-DUBILIER
a great name in capacitors

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1013 Hamilton Boulevard, South Plainfield, New Jersey
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ABBOTT • DK2 •
2½ METER TRANSCEIVER
For a change try 112 mc. You will enjoy it
List Price $27.50
Less Tubes and Batteries
40% Discount to Amateurs
GENERAL: The DK2 is a completely self-contained 112 mc \radio\transceiver\ and receiver, for use in your car, plane, boat, or while being carried, for portable work. It is very simple to operate. The working range is between 2 to 30 miles depending on the location. Astonishing results have been obtained.

SPECIFICATIONS
CASE: Size 11½" long x 9½" high x 64/" wide, grey wrinkle finish metal, heavy leather handle. All batteries are self-contained in case. Removable side panel for easy access to the batteries and tubes.
FREQUENCY: Will cover 112 mc to 118 mc (amateur 2.5 meter band).
BATTERY REQUIREMENTS: Three 45 volt B batteries like Burgess 55308 and four No. 6 dry cells, or two Burgess 2P2H batteries.
TUBES USED: One type 6J5GTX, one type 6G6G.
SHIPPING WEIGHT: 12 pounds.

ORDER FROM YOUR NEAREST DISTRIBUTOR — IF NOT STOCKED CALL 888-444-6868

ABBOTT INSTRUMENT, INC.
51 Vesey Street
New York City

The U. H. F. Relay

(Continued from page 87)

worked hard prior to the relay lining up routes westward. He heard W8QDU using c.w., but was unable to raise him Saturday evening. W8CFD was heard briefly. W1KIK/1 heard W3AC/3 and W3AIR direct and handled a nice bunch of traffic. Between June and August W1KII/1 has worked 134 different 5-meter stations in 18 states (seven districts). The important route from Detroit to Chicago was open for the entire relay period. Messages were exchanged by 5-meter amateur radio between the respective F.C.C. offices. W8CVQ (Kalamazoo) worked W9VHG six times, W8MDA (Ann Arbor) seven times and W8QDU (Detroit) eleven times in the relay. W8CIR's longest relay was Aligquipa-Detroit (200 miles), using 200 watts to a 7-element Yagi beam. He used a 4-tube acorn converter and RME69.

It has been fascinating and interesting to see the message copies roll in to be clipped together to make a complete record of each route. We regret some of the gaps that cannot be filled because a few fellows failed to report. There were dozens of messages, and since many wonder how they progressed, we include information relating us. W3EBH's message to Maine got as far as W1KIK/1. W1KUD's, W1SL's and W1KEE's have been traced as far as W3HOH. One from W1UJ, Sanford, Maine, likewise. Another started by him got to W1KII/1 and W1LL. W1ERT's got to W3AC/3, W1EHT's, W3ETA/8, W2ADW's, W3EUA's and W1AUN's got as far as W3GGR/5. We never got beyond W8NPD in tracing those from W8MDA, W8SMP, W8QQS, W8QDU, W8LQ, W8RKE, W8TNB/8 and W8RFW. W3IDS, W1KII and W1HXU got messages as far as W1EKI, after which no further reports. W8HPD, W1UUU and W1JSV messages got to W1KIK/1. W2MGEU got a message through to W1HDQ, W3AC/3, W3HHC's and W3HPD's got to W3ETA/8. W3HSN got to W3DBC. W2LEG was delivered at W3BYF. W2NFE's, W3FJI's, W1CLH's and W1B1DI's got to W3KBK en route west.

The spirit of all participants was high. It was great fun, and a thrill of accomplishment to hear about the routes being set up, and pass along messages to well known friends or hear them on their way.

Typical comment: “Orchids to W8CIR for his fine work in attempting to bridge the gap west during the contest.”—W3FQS. “Everyone taking part had the time of his life. . . . Used a beam with eight half-wave elements here.”—W8CVQ. “Heard W5EIM testing on 56.2 Mc. and am reporting this to him.”—W3EUA. “More activity on the band than for many a day.”—W1IJ. “Relay work is the answer to keeping five meters open. The messages slid up and down the coast as if ‘five’ had been used for this purpose for years. Don’t let anyone tell you the boys on this band cannot handle traffic.”—W1I. “Most activity at the start and at the end.”—W3H0H. “Will stay on throughout the winter. All set for all districts, and
Here's the buy!

11 Tube COMMUNICATION RECEIVER

$69.98

Amateurs Net
Wired with Tubes

Every year ONE communications set pushes out in front . . . because it has what it takes, in performance and Extra Value. We believe that during the coming year it may well be the GUTHMAN 11-tube U-50 SUPER.

Complete with new Gun-Sight Tuning Pre-Selection Stage, this new receiver provides quiet DX thru controlled regeneration, and socket provision for adding 100 kc. oscillator giving in-built frequency check.

U-50K SUPER, assembled, ready-to-wire, less cabinet, tubes, speaker ............. $83.25 list $49.95 net
U-50W SUPER WIRED, less cabinet, tubes, speaker ... 95.75 list 57.45 net
U-51 Hinged top Cabinet .................. 5.84 list 3.50 net
U-62 10" Speaker and Cabinet ............ 16.50 list 9.90 net
U-53 Tube Kit ............................ 15.05 list 9.03 net

See it at your jobber's today, or order direct, giving jobber's name if out of stock.

EDWIN E. GUTHMAN & CO., INC.
400 S. PEORIA ST. CHICAGO, U.S.A.

CHECK THESE FEATURES
• Six bands, 525 to 62,000 kc.
• Gun-Sight Tuning, Illuminated and Magnified 2½ times
• Socket Provision for 100 kc. Oscillator to be added
• Controlled Regeneration
• R.F. Stage (3-gang condenser)
• Improved Noise Silencer
• Calibrated S-Meter
• Antenna Trimmer
• 12 Watts Output
• Matched Dynamic 10" Speaker
• AND every other Vital Control
Low-cost dual-section midget electrolytics.

• Extremely compact for tight spots.

• 25, 50, 150, 200 and 450 v. D.C.W.

• 8-8 to 20-20, various popular combinations.

• Center strap mounting. Polarity-colored leads.

These dual midget-type electrolytics are now listed in the 1940 AEROVOX catalog, along with many other new items.

Ask your local jobber for your copy. Or write us direct.

MORE DX LESS NOISE!

WITH THE AMAZING NEW BROWNING PRESELECTOR

W2APT says . . . “In the past 15 days I have logged 23 Asiatics, working 19 of them . . . couldn’t even be heard without the preselector. . . . Extremely grateful for wonderful performance of this unit . . . .”

This new Preselector is GUARANTEED to improve the performance of any Receiver. Available in kit form at $15.50 or wired and tested with Filament Transformer $19.50. Uses new 1852 tube in High-Cain circuit. Range from 5 to 150 meters bandswitching. Buy one today on money-back if-not-satisfied basis at your local Ham Supply House, or write direct. Free Bulletin upon request.

NEW BROWNING VISUAL FREQUENCY MONITOR

The new Browning Visual Frequency Monitor compares favorably with $400 models. Exceptionally accurate and indispensable for logging DX stations and working “close to the edge” of the band. Ideal when used with R.C. operation. Many outstanding features, Amateur net price (Less 5 tubes) only $74.65.

Always Be Careful

(A) Kill all transmitter circuits completely before touching anything behind the panel.

(B) Never wear ‘phones while working on the transmitter.

(C) Never pull test arcs from transmitter tank circuits.

(D) Don’t shoot trouble in a transmitter when tired or sleepy.

(E) When working on the transmitter, avoid bodily contact with metal racks or frames, radiators, damp floors or other grounded objects.

(F) Keep one hand in your pocket.

(G) Develop your own safety technique. Take time to be careful.

Death Is Permanent!
**SWITCH TO SAFETY**

Buy Quality Sets and Parts from NEWARK

- Send 20% down payment with your order
- Add 6% carrying charge to the balance
- Divide into 12 monthly payments or less

**NATIONAL**

**NC101X or NC101XA**

**$25.80**

Choice of Direct Reading or Micrometer Dial. Cash Price .................. $129.00

**OTHER RECEIVERS AVAILABLE ON OUR FAMOUS 6% TIME PAYMENT PLAN**

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<thead>
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<th>NATIONAL</th>
<th>Cash</th>
<th>Down</th>
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</thead>
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<tr>
<td>NC101X...</td>
<td>$142.50</td>
<td>$78.50</td>
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<tr>
<td>NC101....</td>
<td>99.00</td>
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<tr>
<td>RHO D.C....</td>
<td>179.70</td>
<td>35.94</td>
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<td>RME 70....</td>
<td>138.00</td>
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<td>7DDBX Combination...</td>
<td>181.80</td>
<td>36.36</td>
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<tr>
<td>HAMMARLUND HQ120...</td>
<td>129.00</td>
<td>25.80</td>
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**HALICRAFTERS**

- SX 24.... | 81.50    | 16.30     |
- SX 25.... | 127.50  | 25.50     |
- Sky Buddy... | 39.50  | 8         |
- Sky Champion.... | 49.50  | 10.99     |
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**FREE!**

NEWARK'S BIG NEW

84 page Catalog

**HERE'S A REAL CABINET BARGAIN!**

Again NEWARK scores with this smash value - proud of NEWARK'S "On their toes" look-out for items of merit for the Amateurs. Here's a black crackle finish heavy gauge metal Cabinet with hinged top door, 12½" high, 19¾ wide, 11¾ deep. Just the right cabinet for a B B table model rig or for that mobile job. We guarantee you'll like this cabinet and it's priced at a real saving. Shipping weight 16 lbs.

NO. PX-1. - Complete with front panel to match ........... $2.00

Classic to fit this Cabinet, 19¾" x 17½" x 3½" .............. $9.90

**NEW NATIONAL NC44A**

**NOW IN STOCK**

- $49.50

**MIMS SIGNAL SQUIRTER**

on Easy Terms

- only 20% Down

Add 6% carrying charge to 12 months.

Write for Prices

**39 YEARS TOTAL EXPERIENCE**

and consistent amateur activity

ADDED TO NEWARK'S TECHNICAL STAFF

A. D. Middelton

"MID" W9AOB

Original ORS party king and competition winner, former S.O.M. Kentucky. Member USRA

G. W. Mossbarger

"MOSS" W9AUN

Original ORS party king and competition winner, former S.O.M. Kentucky. Member USRA

Newark is proud to announce that these two men have been added to their technical staff and are now at your service in helping solve your amateur radio problems. Write to them.

**AEROVOX "HYVOL"**

Oil-Impregnated and Wax-Filled in Rectangular Metal Cans

Discontinued by Aurovex. Closing out at these low Prices While Stock Lasts!

Recommended for use where economy is a necessity. Comes Complete with Universal Mounting bracket illustrated.

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  Mfg. L.W.D. Net
  N 11½ x 12½/16 x 1 1/16 $1.85
  2 11½ x 12½/16 x 1 1/16 4.47
  4 11½ x 12½/16 x 1 1/16 1.36

- Type 1511 - 1500v. D.C.W.
  Mfg. L.W.D. Net
  2 11½ x 13½/16 x 1 1/16 $1.43
  4 11½ x 13½/16 x 1 1/16 1.96
  8 11½ x 13½/16 x 1 1/16 3.18

- Type 2011 - 2000v. D.C.W.
  Mfg. L.W.D. Net
  2 13½ x 14½/16 x 1 1/16 $1.72
  4 13½ x 14½/16 x 1 1/16 4.20
  8 13½ x 14½/16 x 1 1/16 4.56

- Type 3011 - 3000v. D.C.W.
  Mfg. L.W.D. Net
  2 14½ x 15½/16 x 2 1/16 $2.65
  4 14½ x 15½/16 x 2 1/16 4.95

**99**
NEW ENGLAND DIVISION

 CONNECTICUT — SCM, Frederick Ellis, Jr., W1CTI — Nutmeg Net; 3640 kc. 6:45 p.m. daily except Sunday. JTD, with an input of 290 watts, has a total of 71 counties to his credit. On Sept. 17th EAO worked with KXM/1, KDFE, GAG and EHT/1, reporting rifle match at Hartford. Connecticut A.A.R.S. Net opened on Sept. 11th, with most of the old gang on hand and KXQ as new member. Sorry to hear that AIB will be inactive this year. Recid will be missed by both A.A.R.S. and Nutmeg Net. The Wilsonite, having had a temporary handover at Trumbull, 1/2 is on 3464 kc., Mon., Wed. and Fri., from 6:30-8 p.m., looking for traffic. DWP now has an 810 final. Nominations for club officers are being held at GB. KEN has band-switching and plans a new 3.5-Mc. antenna. AVC attended DX Round-up in Springfield, Mass., with APA. ADV is building new home in Easton, and will have 1 kw. on the air when he gets moved. JBIJ has completed new modular using a pair of RCK2's. RW wrote in that he had a very happy birthday, B.A.R.A. made an excellent showing in June Field Day. More reports from Connecticut amateurs would be appreciated. Reports from all licensed amateurs are welcomed and should reach the A.A.R.S. Net. In the GB District the GB District Committee attended the Manchester, N. H., Convention. Twelve members of the Nutmeg Net were present at a get-together held in the club rooms of N.H.A.R.A., W1GB, Sept. 23rd. A fine spirit of interest and activity was evident, which indicates that interest and activity was evident, which indicates that you fellows are maintaining the Nutmeg Net, this year. Our thanks to the N.H.A.R.A. for its fine hospitality.

 TRISTAN (WILM 29) EAO 26 JXP 15 BDJ 6 KYQ 5 T4-DWP-KFN 2 GB-CTI 1.

 MAINE — SCM, H. W. Castner, W11EB — Your S.C.M. has been appointed on the "Planning Committee" of 75 amateurs, which is making a study of present usage and future recommendations of all our bands and privileges. The opportunity has arrived for you to write me all about what needs to be changed, improved or corrected in all our operation. A.R.K. has set up this study in such a way that every recommendation will be filed. If you have a comment or a suggestion, please write me.

 Maine A.R.S. is hard at work on a new project that will be of great interest to the public. Now that the weather is getting colder and it is getting harder to get outside, the opportunity to see the moon and stars is almost non-existent. The Public Service Board has given permission to use the old military building at the Naval Air Station in Portland for a public observatory. The observatory will be open to the public on Saturdays from 2 p.m. to 5 p.m. The observatory will be staffed by volunteers who will be on hand to answer any questions you may have about the night sky. The observatory will be open to the public on Saturdays from 2 p.m. to 5 p.m. The observatory will be staffed by volunteers who will be on hand to answer any questions you may have about the night sky.

 STATION ACTIVITY

 The Station Activity section of the QST magazine is a valuable resource for amateur radio operators. It provides information on station activity throughout the country, including the latest news and events. The section includes details on new stations, changes in station operation, and news about equipment and accessories. It is an important source for operators looking to stay up-to-date with the latest developments in the world of amateur radio.

 This section is also a great place to find information on upcoming events and activations. Operators can use the information to plan their own activities and to interact with other operators in their area. The Station Activity section is a must-read for anyone interested in amateur radio, and it is an excellent resource for operators looking to expand their knowledge and skills.

 In conclusion, the Station Activity section of the QST magazine is an invaluable resource for amateur radio operators. It provides up-to-date information on station activity throughout the country, including details on new stations, changes in station operation, and news about equipment and accessories. It is a great place to find information on upcoming events and activations, and it is an excellent resource for operators looking to expand their knowledge and skills.
JJY is active with traffic and lining up Emergency Coordination. JRC is now on 28-Mc. 'phone. MFO, ex-3GZK, is most welcome addition to E. Mass. KFJ says no more J.P.L., as VO3A is now off. LNS reports ASA and MEZ on 1.75 Mc. BFR is now first-class telephone op. LXX sends first report. QW reports general overhaul for winter season. KZK, LDI and JNO have new 14-Mc. verticals built up. AAT, LXY, JEF, HJU, IFJ, BTV, LBS, KJA, IYW and LWH are on 28 Mc. 'phone and in around Beverly. Let's go for a real season, gang. Please report all activity. 73 from Larry, Kay and Bob.

WESTERN MASSACHUSETTS — SCM, William J. Barrett, W1JAH — LTV and LJJ are new O.P.S. HDQ is new O.P.S. IDQ applied for O.O. O.L. leads the traffic reports in and out. BIY is waiting full swing in A.A.R.S. JAH visited BTV, KUW and BIV. AZW applied for O.R.S. DUZ and FOI keep the 'phone represented in the traffic column. DUZ reports that the West Mass. A.A.R.S. Phone Net is now set for the active season. E.N. is active with 14-Mc. w.t., K.O. has been concentrating on rebuilding in preparation for the coming winter. CO1 took down rhombic antenna to make way for new rotary. How about some reports to help fill this column, fellows.

Traffic: W1LVY 120 BIV 87 JAH 54 (WLGE 9) BVR 17 (W1GZ 138) FOI 12 DUZ 4.

NEW HAMPSHIRE — SCM, Carl B. Evans, WIBFT — DQ is the life behind this section. DUZ has put forward a request for some interested fellows to line up some schedules with him to facilitate the delivery of traffic over New Hampshire. Drop DLX or your S.C.M. a line, and if interested, DUZ has line up an active schedule beginning at 9 a.m. (Continued on page 104).

Traffic: W4AKC 166 DLX 15 DSY 101 KJG 23 KXY 4 FSV 36.

ROANOKE DIVISION

NORTH CAROLINA — SCM, W. J. Worthington, W4CYB — The A.A.R.S. got off to a good start, and various networks have been functioning in the state. SCM has put forward a request for some interested fellows to line up some schedules with him to facilitate the delivery of traffic over North Carolina. Drop DLX or your S.C.M. a line, and if interested, DUZ has line up an active schedule which is beginning to function. FLC, new O.R.S., is ready for action DQ is installing new skywire. DXY rag chew most of the time. BV has new speech equipment. MR is working 1.75 and 28-Mc. rig on 1936 kc. TJ returned to 3.9 Mc. after his having permanently moved to 14 Mc. CPV sends nice list of DX. AK0 leads State in traffic this month. BIY, Joe, FCB reports from Schofield Barracks as a portable K6 and worked PN with KQ0U. FEA has new modulator for checking rig located in attic. EIZ is building portable for use at Duke Univ. EYF and DLX have emergency transmitters. New members in Emergency Corps are FYY and DXY. How about sending in some of the blanks given out in Greensboro? We have been asked by BMR to retract our last month's statement to the effect that he had four 250TH's in P.L. parallel. Our apologies for an incorrect statement. DGY enjoyed trip to YUBA and up into Canada. ANU has new combination 14.5 Mc. antennae, A1U returned to 3.9 Mc. We want to thank the gang over in Greensboro for the nice hamfest held September 2nd. Prepare now to go to Charlotte, November 6th.

Traffic: W4AKC 166 DLX 15 DSY 101 TJ 2 DGY 1.

SOUTH CAROLINA — SCM, Ted Ferguson, W4BQG/ AN— AXT is active on 3.9-Mc. 'phone. DFE reports rig working 2B on 1023 kc. F.S. II adds a new 14-Mc. regular schedule with DX, CE has line up a neat rig on 7-Mc. final, both 'phone and e.w. COL has returned to Clemson. GAR changed QTH to Denmark. CXX is rebuilding for 14-Mc. 'phone. PFO changed QTH to Clemson. EJZ is active in 1.75-Mc. 'phone net and makes nice report of the activity up-state. Thanks, OM, FYL and EIZ attended the 'fest at Athens, Ga., and report nice time. GCW returned from Michigan. FNC and EJK are old standbys on the 1.75-Mc. net. OSP operates 1.75-Mc. 'phone. YVF has a new Jr. op. Congrats, OM. WPS is active on 22-Mc. band at Greenville. Nice going, fellows, EDQ changed QTH to Greenville. EWI is active on 1.75-Mc. 'phone. EJZ can be heard on 7-Mc. e.w. and 1.75-Mc. 'phone. CZA reports activity in the A.A.R.S. and T.L. "O", 


VIRGINIA — SCM, Charles M. Waff, Jr., W3UVA— R.M.'s: 3GZV, 3IDQ, P.A.M.'s: SAI, SGW, FHF plans to be on 4-Mc. 'phone. O.R.S. H5G, for the Old Dominion Radio Ass'U. HAB reports the Norfolk Radio Club very active. John Hunton, LVQ, of A.A.R.R. HQ's staff, visited Petersburg, Richmond and Norfolk clubs. We have word
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"United" won the Aviation Maintenance Award for 1938. And, here's one of the precautions that typifies the Air Lines' safety mindedness.

The picture shows Al Otvos, radio mechanic, installing a No. 3T10 Burgess Battery on a DC3 Mainliner's Emergency Radio. This set is a 4-tube, tuned frequency model which is standard equipment on all United's planes.

A letter from the company says, "The importance of the emergency radio is obvious . . . The possibility of failure cannot be risked on any occasion—and that is why Burgess batteries were selected."

Again Burgess batteries have been chosen for their dependability. Whatever your requirements are, you too will be safe with Burgess.

BURGESS BATTERY COMPANY
FREEPORT, ILL.
A new appointment: LKQ O.R.S., JQJ O.B.S. KJY reports from L.A., where he is operating portable from the trailer, "Continental Clipper," which carries radio WLSV, MMC is a new station at 425-430 M.C.R. 9:15 P.M. Starting, FXW is now located at 750 W. 148th St., Flushing. EXR's new QTH: 1010 McGraw Ave., Bronx. JYR is now at 1303 Dean St., Brooklyn, but will be operating portable from Syracuse for the rest of the year. A.A.R.S. is looking for members in the portable area. FB with the new rig. MCI operates on 7-Mc. Traffic Net. LTG is giving 14 Mc. a try. KYO received his A-1 operator's certificate. JU is building for 28-Mc. phone. KMZ is using a second-class telegraph ticket. LNN received his Class "A" ticket. Ki is ready for big season. ELK's new transmitter is all built, with the latest safety devices. LGO did a lot of 86.-Mc. DX listening. Both KHH and KMZ are working on 86.-Mc. LJP is interested in getting his QSO on the F.S.S. with AEU. L JR is official F.S.S. BC station and is on every Friday at 7:30 P.M. E.S.T. on 7200 kc. DBQ is looking for members for A.A.R.S.-7-Mc. Net. EC reports that 8 A.-P. trunk line is now operating on third-class-telegram ticket. LNN received his Class "A" ticket.


Traffic: W2LSD 154 KWG 64 LU 47 MHW 6 DVC 3.

Hudson Division

Eastern New York — SCM, Robert E. Haight, W21B, PO Box 150, Hartsdale, New York. SCM is the gourm tort FTS, working approximately 182 stations on F.T.S. schedules. KGW continues keeping West Point on the air. Lu is on 3530 kc. looking for E.N.Y. stations. MHW is working W.N.Y. and E.N.Y. traffic nets on 3720 kc. D.V.C. sports new Howard. KGW's new 15-W. Lucie, will be back on 3720 kc. Lu reports total of 55 contacts. MHW, new O.R.S., reports GTM at sea operating on Liner "Cerise." LOR is overhauling rig while KGW rebuilds his station receiver. KGW, pinch-hitting at WKO and W2AH, POBox 79, Flushing, said Lu is busy, discussing E.C. activities in his district. EMK is now O.R.S. KGW has been doing a swell job at 2USA. E.N.Y. is proud to have KGW in our Section.

Traffic: W2EBS 12 14 DVC 8 KJH 8.

New York City and Long Island — SCM, E. L. Baunach, W2AZV — New appointments: LKQ O.R.S., JQJ O.B.S. KJY reports from L.A., where he is operating portable from the trailer, "Continental Clipper," which...
Advise 3AQN of your schedules. 3BES has new QTH. 3BES is building a 200-watt e.c.o. from new QTH.

From Jacksonville, Fla. to Dexter Hill, Pa., and back in five minutes is a traffic record set by 3PML. FB! 3FR1, vigilant O.S., is on 14 Mc. E.O. has low-power rig on 3.9 Mc. FB1 likes his O.S. so well he has signed up for his fourth year. 3HID is nearing his goal of Century Club.

3GHN has started training for the Sweepstakes. 3GKO is in the market for a new beam. 3CHH aBXE, O.R.S. of old, is at it again, this time with an 809. JGRF. 3AGV received RR's e.c.o. has boosted his training in spite of curtailed fourth year. GHD is nearing his goal of Century Club.

"And reports "F.B." FUM began operations with the AP. 3CHH 5 3EML 1851 3FLH 3 3FRY aBWT. HGQ will accompany Admiral Byrd on his expedition to the South Pole, and will try to work U.S.A. 14-Mc. 'phone; he now has 20 watts. Unit 3, Section V, U.S.N.R., 3GHN has started training for the Sweepstakes. 3GKO's e.c.o. has boosted his training in spite of curtailed fourth year. GHD is nearing his goal of Century Club."

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A Safety Kw. Transmitter
(Continued from page 45)

one side of the filter condenser to 6000 volts above ground on modulation peaks, but this is of no consequence with good filter condensers. An underload and overload relay are connected in series with the secondary of the modulation transformer and in the grounded side. Should the final amplifier plate current drop below a predetermined value the underload relay will open the 500-ohm line to the input transformer and stop modulation and possible damage to the output transformer. If the current of the final amplifier exceeds a predetermined value, the overload relay will disengage the primary of the final amplifier plate transformer. An additional relay is used to short-circuit the coil of the underload relay when the modulator filaments are turned off during telegraph operation. Turning off the modulator filaments also automatically shorts the Class-B transformer secondary, and the switching panel is so connected that it is impossible to key the transmitter when the modulator filaments are lighted.

A condenser and resistor network is connected to the secondary of the Class-B transformer to provide a source of audio voltage for a trapezoid pattern on an oscilloscope.

The bias supply is also located on the modulator chassis and is used for the final amplifier only, hence no low resistance bleeder is necessary in order to provide good regulation. In fact, a bleeder of sufficient resistance was used so as to act as a grid leak as well. With no grid current flowing, there is sufficient bias to cut off the final amplifier plate current. When normal grid current is flowing, the voltage across the bias supply bleeder resistance rises to the normal value for Class-C telephone operation. Either this method or a combination of grid leak and well regulated bias supply is recommended for best linearity in a plate-modulated telephone transmitter.

Power Supply

The plate transformers for a 1000-watt transmitter are extremely heavy and do not lend themselves to conventional chassis mounting. In this transmitter both the 3000- and 1750-volt transformers are mounted on the base of the relay rack cabinet. Two pairs of 866 rectifiers, two input chokes, and two 4-µfd. filter condensers are mounted above the plate transformers, comprising the rectifier and filter for both high-voltage power supplies. Only single-section filters have been used, since this was considered sufficient and results in a considerable saving of space. In keeping with government regulations, a 0-4000 volt-meter is used to measure the final amplifier plate voltage at all times. The meter is mounted on the modulator panel. During tuning, the plate voltage to the final amplifier is reduced by taking advantage of the double primary on the 3000-volt transformer, a d.p.d.t. switch connecting the windings either in series or parallel.

The interconnecting cables for the units are neatly formed to fit in the rear corners of the

[Adaptation of text from the original to fit the context of each part]
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If your Class-B output transformer doesn't come equipped with a safety gap, the attachment of such a gap across the secondary output terminals may save the transformer in case the Class-C load is lost. The gap should be adjusted so that no arc occurs during normal modulation or slight overmodulation.

W6LNS

Ceramic coil forms may be drilled in a drill press with a short piece of copper tubing of the right diameter in the chuck. Use valve-grinding compound and lots of water on the edge of the tubing, never allowing the water to become hot.

W2ALP

High-Efficiency Grid-Modulated Amplifiers
(Continued from page 87)

normal plate voltage, and the plate current noted. The phasing coil is then reconnected, with tube No. 2 filament still open, the resistor across tank No. 1 removed, and the resistance R/2 placed across tank No. 2. On retuning the network the plate current should be the same as before, if the size of the phasing coil is correct. If, under these conditions, tube No. 1 draws too much plate current the phasing coil has insufficient inductance and if the plate current is too low the phasing coil has too much inductance. In general, the calculated value will be very close to the correct cabinet and laced tightly with armature twine. The cables can best be made on a work bench by laying out a scale drawing of the rear view of the transmitter on wrapping paper. Nails can be driven to form a temporary channel to lay wires in and to form the bends for the various branches of the cable. All chassis are connected together by a half-inch copper strip running along the side to furnish a common ground. Three-quarter-inch diameter holes were drilled in each rear corner of the bottom of the cabinet for the cabling for remote control connections. An eight-contact plug is mounted on the left side in the rear of the base and handles the 500-ohm line, key, plate-primary relay, audio voltage for the oscilloscope, and ground. Next to this is mounted an Amphenol 92-C receptacle for the 110-volt a.c. Alongside the power receptacle is a four-prong socket which is connected to the switch panel so as to provide a green signal light on the operating desk when filaments are on and a red light when the carrier is on. On the right side of the rear of the base are mounted three Amphenol type PCM connectors which handle the external e.c.o. voltage, the r.f. from the final amplifier tank circuit for the oscilloscope, and the receiving antenna connection from the change-over relay. Amphenol small size flexible co-axial cable, No. 76-22S, was used for all interconnecting links carrying r.f.

Strays

If your Class-B output transformer doesn't come equipped with a safety gap, the attachment of such a gap across the secondary output terminals may save the transformer in case the Class-C load is lost. The gap should be adjusted so that no arc occurs during normal modulation or slight overmodulation.

W6LNS

Ceramic coil forms may be drilled in a drill press with a short piece of copper tubing of the right diameter in the chuck. Use valve-grinding compound and lots of water on the edge of the tubing, never allowing the water to become hot.

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High-Efficiency Grid-Modulated Amplifiers
(Continued from page 87)

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value and in most instances will not require much adjustment. Finally, the filament of tube No. 2 is closed and voltages applied (tube No. 2 is biased approximately to cut-off so takes negligible plate current). Then the load on tank No. 2 is adjusted to bring the plate current on tube No. 1 to the same value as before.

The network of Fig. 1-B is inserted in the grid circuit of tube No. 1 to advance the phase 90 degrees so that the r.f. currents from the two tubes will be additive in tank No. 2. This network, in comparison, is not very critical. The series condenser is chosen so that its capacitive reactance will have a value approximately equal to the grid input impedance. Tank No. 1 of the grid network is tuned to resonance and tank No. 2, with the network loosely coupled to the driver, adjusted for maximum plate current on the driver. This adjustment should correspond to minimum plate current on No. 2 tube and maximum grid current on tube No. 1. Maximum loading on the driver results because as proper adjustment is reached the effective inductance of tank No. 2 is series resonant with the series condenser Cₙ, and so effectively lowers the load impedance on the driver.

Final adjustment of the grid phasing network should not be made until both tubes have been neutralized. Neutralization may be accomplished using the conventional methods.

It might be wise to point out that tank No. 1 of the grid phasing network may be used either as the tank circuit of the driver stage or as a separate tank, link-coupled to the driver. In this latter case, however, maximum loading on the driver as tank No. 2 is varied may not necessarily hold because of reflected reactance to tank No. 1 from the link. In this case the more certain indication of correct adjustment is that of tuning tank No. 2 for minimum plate current on tube No. 2.

Driving power required is about the same as that for a conventional Class-C amplifier. Considering losses in the various tank circuits, the driver output required will be about four or five times the rated driving power for one tube.

Fig. 3 shows the diagram of a transmitter built shortly after the appearance of the paper by Terman and Woodyard. Fairly good results were obtained with it; the quality was good, and an output of 50 watts from the two 807 tubes was reached. The output was measured by using a Weston 0-500-ma. r.f. meter and an Ohmite dummy antenna.

The adjustment of excitation and bias was more critical than was desired and it would appear that it would be easier to make this adjustment on triodes than on pentodes.

It was difficult to obtain non-inductive resistors to use in the adjustment of the plate phasing network as suggested by Terman and Woodyard. Final adjustment was reached by changing the coupling to tank No. 2 and trying several different values of inductance for the phasing coil for correct plate current on tube No. 1. If correct plate current did not result a new value of coupling was chosen and the testing repeated. It is possible to get the wrong value of coupling and...
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Let me help you get the right one.

Bob Henry, W9ARA

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Standard Construction
Fully Guaranteed
2½ Volts 10 Amps
10,000 Volts insulation
6.3 Volts 6 Amps
2500 Volts insulation

These transformers bear the same warranty as when formerly sold at full price.

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New LOW PRICE on VF-1 Variable Frequency, Low Drift crystals. Your choice of frequency in 40 or 90 meter bands. $6.60
Bliley Harmonic Chart in colors on heavy cardboard. Suitable for mounting.

Free for the asking.

General Rotary ANTENNA ELEMENTS
are selling like WILD-FIRE
Construct your own Rotary Beam at small cost.
General elements are constructed of light, durable seamless tubular steel—both copper and cadmium plated. Due to unusual construction—suitable for mounting.

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General elements are constructed of light, durable seamless tubular steel—both copper and cadmium plated. Due to unusual construction—suitable for mounting.

B & W Baby Switching Turret—5 band low power switching; Taylor TW-150 Tubes—Thin Wall Carbon Tubes; Guthman U-35 Keytomer—Learn code rapidly—Melssner Television Components—Special television chokes and coils—Hytron GTX Ceramic base receiving tubes.

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still have the correct plate current on tube No. 1 if the size of the phasing coil is far off, but this will be indicated by the reluctance of tube No. 2 to increase its plate current with modulation, as it would be if its load impedance was too high.

It was very difficult to get enough coupling to tank No. 2 so that it would present the proper terminating impedance for the network. The desired value was about 675 ohms. The L/C ratio was about 320,000 so the coupled resistance necessary was about 475 ohms.

The second transmitter, shown in Fig. 4, uses HF-100's. Split tank circuits were used here to provide easy neutralization. The L/C ratio in this case was about 330,000 and the coupled resistance needed is only about 75.5 ohms. The inductance of the plate phasing coil is 24 microhenrys and it has a reactance of 2100 ohms.

D.c. bias on tube No. 1 is all grid leak bias—a bias resistor of 10,000 ohms and a grid current of 20 ma. provide a bias of 200 volts. Bias on tube No. 2 is all fixed bias and is supplied by a small bias rectifier capable of delivering 300 volts.

Power output from this transmitter is 200 watts, and the general results obtained with it have been very satisfactory.

Shunt feed was used in this transmitter to reduce the danger to the operator which might be present if d.c. plate voltage appeared on the tank coils and the phasing coil.

With this type of amplifier it is interesting to note that as the antenna coupling is increased the plate current of tube No. 1 decreases. This is in accord with the theory of the network but presents a somewhat different view than that to which we are accustomed. Conversely, as coupling is decreased the plate current of tube No. 1 will increase and with no coupling may become dangerously high.

Linearity, during modulation, is dependent to a considerable extent upon the relation between the applied audio voltages, bias and excitation and can best be determined by experimentation. An oscilloscope will be helpful. In general, tube No. 2 requires one-half to three-quarters the modulating voltage applied to tube No. 1. Excitation is about the same on both tubes, with tube No. 2 biased so that it will draw essentially no plate current at carrier level.

By installing audio chokes in the grid leads, the audio requirements were lowered considerably as compared to the method shown in Fig. 4, because without them the modulator is terminated by the bias resistor as well as the internal grid impedance of the tube. An alternative arrangement would be to feed the audio voltage in series with the bias, with the grid leak and bias supply by-passed for audio frequencies. This would necessitate placing both sides of the fixed bias supply above ground for audio frequencies, unless separate secondaries are available on the a.f. output transformer.

The author wishes to express his appreciation of the help and encouragement given him by Mark W. Bullock, Technical Supervisor for the Central States Broadcasting Company, and by Burt E. Davis, WOZE.
CIRCULAR A-7 describes the complete line of BLILEY CRYSTAL UNITS For Amateur Frequencies

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W3 - Maurice Downs, W3WU, 1311 Sheridan St., N. W., Washington, D. C.
W4 - G. W. Hoke, W4D.YB, 328 Mell Ave., N. E., Atlanta, Ga.
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K5 - Norman F. Miller, K5AF, 15th Air Base Squadron, Albrook Field, Canal Zone.
K6 - James F. Pa, K6LBH, 1416D Lunallio St., Honolulu, T. H.
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KA - George L. Rickard, KA1GR, P. O. Box 848, Manila, P. I.

**Effective Antennas**

(Continued from page 16)

ments, in place of the double supports for the 14-Mc. elements. The latter is made possible because of the lighter weight of the elements. Also, the smaller size Johnson insulators, type 66, may be used throughout.

Halving the 14-Mc. dimensions when we double the frequency will do quite nicely, and from that we find that a total overall length, for the longest
New Model Dynamic Microphone

In presenting this new Model "DN" Dynamic Microphone, Astatic Engineers give to amateur and other fields of usage, an instrument of exceptional dependability, high in efficiency, sturdy in construction and low in cost.

Incorporated among its many outstanding features is Astatic's new UNITARY MOVING COIL SYSTEM, a correctly designed magnetic structure with ALNICO Magnet and carefully proportioned ACOUSTIC CIRCUIT to highly damp natural resonance of the moving system and provide a response characteristic substantially flat from 50 to 7,000 cycles.

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The only difference between tuning the four-element 28-Mc beam and the procedure outlined above for use on 14 Mc, comes from the fact that the elements are so short that it is desirable to adjust them from the two ends rather than by means of the short matching stubs. Therefore it is desirable to leave the elements off the framework until it is time actually to use them. The radiator is set up first and tuned, as outlined. Then, and not until then, the reflector is set in place and tuned. Then the first director and lastly the second director. Similar minor adjustments may also be made to bring the beam into its most efficient state. The same procedure with relation to the elimination of standing waves may also be followed.

While the original W8JK type of beam remains our favorite for regular communication, there is no doubt about the greater gain, in a given direction, of the two-, three- and four-element unidirectional rotaries, when they are properly tuned. Of course, much of the ability to get real distance from any of these beams comes from setting them at the correct height above ground. That is a factor which is extremely difficult to figure for a group of circumstances, and on it will depend the ultimate performance of any beams of this type. However, without changing the height at all, both receiving and transmitting are improved very greatly. Well worth getting, to be sure!

U.H.F. Relay
(Continued from page 68)

the years roll along, proving your earlier u.h.f. work, and for once we can guarantee every participant who reports one of 'em. We want to hear from every ham on 23½ and on 5-meters on these dates. Such a certificate is shown below:

After you get your test message off, your aim is to see how many you can work, what u.h.f. DX you can hear and raise, how many test messages you can push along, etc. For examples of message and information on handling data see page 33 of September QST.

U.h.f. conditions were fine last November, and we expect to see many states represented in the next report that did not get in on the September activity. Any u.h.f. bands can be used, 56, 112, or 224 Mc, etc., as you choose, and we'll report back to all who take part the full extent of the success in each frequency band group. Terminal stations, each starting an u.h.f. "msg," and each holding one or more that cannot be relayed on, at the end of the relay, are especially urged to see that we get reports of these promptly, so that full message histories may be made up . . . and once again we'll report to you on the routes of the most successful messages. Luck and b.c.n.u. in the Contest.

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40-watt beam-power amplifier having thoriated-tungsten filament—Phone ratings 50% greater than cathode type—Reduces battery drain in portable-mobile xmitters—Mechanically rugged, electrically ideal.

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- R.F. output at max. input: 42 approx. watts
- The HY69 is fully shielded for use in all radio frequency circuits—no neutralizing needed. Full ratings up to 60 megacycles.

Uses
- Mobile transmitters...Class A or AB-2 modulators...
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- Use the HY69's in your main rig—transfer them to your portable unit when you take a trip—swap them to your emergency rig if necessary.
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Type 16P00 — Delivers 650 or 500 D.C. volts @ 200 ma. Completely shielded.
Wt. 8¾ lbs. Your cost........ $2.69

Type 16P03 — Will furnish 1250/1000 volts D.C. at 300 mills. Cased as illustrated. Wt. 30½ lbs.
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Primary.................. 115 Volts, 50-60 cycles
Secondary No. 1........ 1200 Volts C.T. @ 200 MA.
Secondary No. 2........ 6.3 Volts @ 4 A.
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Heavy filter units rated at 1 mfd. — 2000 volts and 2 mfd.s. — 1000 volts.
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Skyrider Defiant (SX24) ...... 69.50
National NIU receiver ...... 165.00
Staco antenna relay .......... 3.45

Three-Element Beam Demonstration

(Continued from page 69)

The importance of keeping the antenna away from other objects.

Probably one of the most striking parts of the demonstration was that showing the importance of the correct length of the elements. With the beam pointed away from the field-strength pick-up, the reflector element length was varied by a relatively small amount and whom! The meter needle flopped over almost to the pin, demonstrating quite vividly to everyone present the absolute necessity for careful tuning of the array for optimum results.

The transmitter used was of considerable interest to the u.h.f. men present. A 6V6 crystal oscillator, with a 5.5-Mc. crystal, doubled in the plate circuit to drive an 807 tripler which in turn drove a pair of HK24's in push pull. The push-pull amplifier was tuned to the third harmonic in the plate circuit, using a linear tank. With only 750 volts on the plates, 20 watts at 100 Mc. was obtained in the output. — B. G.
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WARD LEONARD RADIO SPECIALTIES
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Relays * Resistors * Rheostats
The oldest and most complete line on the market for service and amateur use. Proven dependability and conservative ratings. You are not experimenting when you install Ward Leonard items ... you know they are right.

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RADIO MAN’S GUIDE
TO WHAT EVERY
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Information in a handy form covering modern Radio & Television in theory and practice. An entirely New Book that Points the Way to Success in Radio & Television—JUST OUT!


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HELP FOR YOU COMPLETE "PAY $1 A MQ.

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(5) Provisions of paragraphs (1), (2), (3) and (4) apply to all advertising in this column regardless of which rate may apply.

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CALLBOOKS—all editions now on sale containing complete quartz suitable for making piezo-electric crystals. W3DQ, Wilmington, Del.

CRYSTALS, mounted 80-100, $1.25; 200-400, v-cut 40, $2.25. R9 Quartz Murray Ave., Arnold, Pa.

QSL'S, SWL's, 100 — 3 color — 75¢. Lapco, 544 W. 39th, Indianapolis, Ind.

MACAUTO code machines: long monthly rental 50,000 words practice tapes. Write N. C. Ayers, 711 Boylston St., Boston, Mass.


COMPLETE stock ham supplies. New and used communication receivers. Amarelo Electric, W5X, Amarelo, Texas.

QSL'S, all colors, cartoons, snappy service. Write for free samples today. W1BEF, 78 Warren Ave., Springfield, Mass.

STANDS for all types of microphones. Tri-ped, Jr. desk model, chrome or walnut, $1.50. Ellis Lab., 189-Q W. Madison St., Chicago.

MICROPHONES—The best carbon microphones at anywhere near the price. Hand model $5.75; stand model $5; suspension model $3.50; repairs. Ellis Lab., 189-T W. Madison St., Chicago.

CRYSTALS in plug-in heat dissipating holders. Guaranteed good oscillations, $1.25; (no Y cuts) $1.50; 85M Vari-freq. complete, $2.95. Salesman frequency desired. C.O.D.'s accepted. Pacific Crystals, 1042 S. Hicks, Los Angeles.


BEST place to get amateur receivers is from W9ARA. Best trades, best terms (financed by myself), ten-day trial of all receivers. Prompt shipment from world's complete stock of amateur receivers. Shipments from factory if you prefer. Write now for fully descriptive literature. AMATEUR R. F.晶体, 123 W. Madison St., Chicago.

BARGAIN 150 watt remote controlled push-to-talk modern rack and panel mixer, W6WPQ, Auburn, Ind.

HEALFUFL baked gray wrinkle and black crackle Masonite panels. Sizes to 27" x 47". Get prices. Panels, chassis, racks. Lynch, 970 Calamos, Los Angeles, Calif.


NEW: Complete 40 watt receiver. $25.00. Included in this price are antenna and transmitters. Ten days free trial. Nearly all models cheap. Terms. List free. Write W9ARA, Butler, Mo.

CRYSTALS: famous F-K., mounted in latest Admirai 35 hold $3.50. 20-meter PR-20, $4.50; unconditionally guaranteed. Immediate shipment. Wholesale Radio Labs., Council Bluffs, Iowa, WOCR.


CHRISTMAS POLAROID flashlights, lamp, and amateur frequencies. Descriptive catalog. Ham Crystals, 1104 Lincoln Place, Brooklyn, N. Y.

WHY not get better deal? Tried receiver list free. W9RA, Chicago, Ill. CHICAGO: Poland for amateur lamps and amateur frequencies.

QSL'S: 1938 Super Skyrider, crystal, speaker. Best offer. W2FBH, 53—128 63 St., Mapleth, L.L.

QSL'S: RCA 3" oscillograph TVM-122-B, $40; dynamotor 24 v 111/200 v. $215. W2FBH, 534 Vanderhey St., Queens Village, N. Y.

QSL'S, SWL's, stationery, job printing. Free samples. WSDD, Holand, Mich.

ADS: W6BUK, marine, broadcast. Transmitters, receivers, frequency meters, coils, condensers. Stock designs or built to any specifications by the oldest designers of short-wave apparatus. Also blueprint plans, specifications for any type transmitter or radio compass. Prices on request. Ensal Radio Lab., 1053 Kenilworth Ave., Warren, Ohio.

QSL's: Utah transmitter, Premuz antenna, $3.1, Dalton Harrow, Frederic, Md.

COMPLETE line Arvin radios at special Jobbing prices. Loughnane & Co., Desatur, Ill.

QSL'S. Samples, W6HR Radio Press, F. O. Box 202, Clam, California.

WANTED 10 to 100 watt output transmitter factory built for 2118 and 2738 kc. 110 volt a.c. supply or marine transmitter.

Dr. Young, WDG, Minneapolis.

GENERAL Electric dynamotors 24/750 volts 150 watts, $15. W3TWC, 16-18 12th street, Dallas, Texas.

QSL'S. Newest design. W2YDB, Mason, Ohio.

TRADE: complete 175 watt 20 meter phone transmitter for Filmo S camera and Filmo 8 projector. For details write or wire W4ENQ, Rome, Ga.

WANTED: commercial sidewriter or cote key in good condition. Write W5CJ, Decatur, Ill.

SELLING out station — list — W2ZBS.

TELEPLEXES, Instructographs, omniographs bought, sold, traded. Ryan's, Hamilton, Mo.

QSL'S. New free samples. Maleco, 1805 St. Johns Place, Brooklyn, N. Y.


FOR sale: complete 400 watt rack and panel phone transmitter, $295. Charles Bartlett, 100 Park St., Portland, Me.

RMI—99—excellent condition — $85.50. W9IYA.

QSL'S. Samples, W9RUJ, Auburn, Neb.

BARGAIN 150 watt remote controlled push-to-talk modern rack and panel mixer, W6WPQ, Auburn, Ind.

LOOK: unbreakable feeder spacers. High dielectric and tensile strength. $1 per dozen six inch. W9HDH, Wisconsin, Neb.


HAROLD & MARGUERITE Super Pro, world’s finest receiver, xtal model, like new, cost me $261 but I’ll sell it for $150.00. I paid $10 in U. S. 1 year guarantee. Write W9IXR, Rice Lake, Wis.

LOOK—newed universal modulation transformers. MORE audio watts for less dollar. W6BDQ, Waukenth, Wis.

QSL'S—By W3NOS—18 Swan St., Buffalo, N. Y.
SALE: 250 watt phone transmitter. Whole or in parts. 50% off.

W1LLB.

NEW Hammarlund AFC100 condensers, 604. Extraordinary bargains — power, audio transformers, chokes, gang condensers, dials, shield cans, parts, Radiator, Hyde, Pa.

FOR sale — 5 amperes, 2 wire, 100 volt, 60 cycle, single phase, Westinghouse Type OA. 750 volt transformer, 4 mmf. 1000 v. condenser all for $33. 250 line - cost over $135. W9BRN, Butler, Mo.

SELL complete transmitter, 400 watt phone, CW completely enclosed, two cabinets, remote control. W2AEB.

SELL: HIQ like new, reasonable. W8JAH.

SALE or trade — High quality complete phone — CW transmitter 100-150 watts. Also Thordarson dual power supply. Money offer. W2IKV.

NEW Hammarlund AFC100 condensers, 604. Extraordinary bargains — power, audio transformers, chokes, gang condensers, dials, shield cans, parts, Radiator, Hyde, Pa.

FOR sale — 5 amperes, 2 wire, 100 volt, 60 cycle, single phase, Westinghouse Type OA. 750 volt transformer, 4 mmf. 1000 v. condenser all for $33. 250 line - cost over $135. W9BRN, Butler, Mo.

SELL complete transmitter, 400 watt phone, CW completely enclosed, two cabinets, remote control. W2AEB.

SELL: HIQ like new, reasonable. W8JAH.
Your Nearby Dealer Is Your Best Friend

Your nearby dealer is entitled to your patronage. He is equipped with a knowledge and understanding of amateur radio. He is your logical source of advice and counsel on what equipment you should buy. His stock is complete. He can supply your needs without delay. His prices are fair and consistent with the high quality of the goods he carries. He is responsible to you and interested in you.

One of these dealers is probably in your city—Patronize him!

<table>
<thead>
<tr>
<th>ATLANTA, GEORGIA</th>
<th>NEWARK, N. J.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radio Wire Television Inc.</td>
<td>Radio Wire Television Inc.</td>
</tr>
<tr>
<td>265 Peachtree Street</td>
<td>24 Central Avenue</td>
</tr>
<tr>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
</tr>
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</table>

<table>
<thead>
<tr>
<th>BALTIMORE, MARYLAND</th>
<th>NEW HAVEN, CONNECTICUT</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radio Electric Service Co.</td>
<td>Harty &amp; Young, Inc.</td>
</tr>
<tr>
<td>3 N. Howard St.</td>
<td>1172 Chapel Street</td>
</tr>
<tr>
<td>Everything for the amateur</td>
<td>National, Taylor, Kenyon T Line, Radiotron, Howard, etc.</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>BOSTON, MASS.</th>
<th>NEW YORK, N. Y.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radio Wire Television Inc.</td>
<td>Radio Wire Television Inc.</td>
</tr>
<tr>
<td>110 Federal Street</td>
<td>100 Sixth Avenue</td>
</tr>
<tr>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
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<tr>
<th>BRONX, NEW YORK</th>
<th>NEW YORK, N. Y.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Radio Wire Television Inc.</td>
<td>Harrison Radio Company</td>
</tr>
<tr>
<td>542 East Fordham Road</td>
<td>12 West Broadway</td>
</tr>
<tr>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
<td>Harrison Has It! Phone WOrth 2-0276 for information or rush service</td>
</tr>
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<table>
<thead>
<tr>
<th>BUFFALO, NEW YORK</th>
<th>PHILADELPHIA, PENNSYLVANIA</th>
</tr>
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<tbody>
<tr>
<td>Radio Equipment Corp.</td>
<td>Eugene G. Wile</td>
</tr>
<tr>
<td>326 Elm Street</td>
<td>10 S. Tenth Street</td>
</tr>
<tr>
<td>W8PMC and W8NEL — Ham, service and sound equipment</td>
<td>Complete Stock of Quality Merchandise</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>BUFFALO, NEW YORK</th>
<th>PROVIDENCE, RHODE ISLAND</th>
</tr>
</thead>
<tbody>
<tr>
<td>Dymac Radio</td>
<td>W. H. Edwards Company</td>
</tr>
<tr>
<td>1531 Main Street — Cor. Ferry</td>
<td>85 Broadway</td>
</tr>
<tr>
<td>Open Evenings</td>
<td>National, Hammarlund, Hallicrafter, Thordarson, Taylor, RCA</td>
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<table>
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<tr>
<th>HOUSTON, TEXAS</th>
<th>RICHMOND, VIRGINIA</th>
</tr>
</thead>
<tbody>
<tr>
<td>R. C. &amp; L. F. Hall</td>
<td>The Arnold Company</td>
</tr>
<tr>
<td>4091 Huey Street (W 9-9713)</td>
<td>Broad at Harrison St.</td>
</tr>
<tr>
<td>&quot;Specialists in Amateur Supplies&quot;</td>
<td>W3EOQ — &quot;The Virginia Ham Headquarters&quot; — W3FBL</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>JAMAICA, L. I., NEW YORK</th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Radio Wire Television Inc.</td>
<td></td>
</tr>
<tr>
<td>90-08 166th Street (Merrick Road)</td>
<td></td>
</tr>
<tr>
<td>&quot;The World's Largest Radio Supply House&quot;</td>
<td></td>
</tr>
</tbody>
</table>
YOU CAN BE SURE WHEN YOU BUY FROM QST ADVERTISERS

"Advertising for QST is accepted only from firms who, in the publisher’s opinion, are of established integrity and whose products secure the approval of the technical staff of the American Radio Relay League."

Quoted from QST's advertising rate card.

Every conceivable need of a radio amateur can be supplied by the advertisers in QST. And you will know the product has the approval of the League's technical staff.
Who could have believed that RME receivers built five years ago would still be quite up-to-date today?

Our old RME-9D SIX YEARS AGO incorporated as standard—handswitching, crystal filter, panel control of beat oscillator, automatic volume control, tuned RF stage ahead of the first detector, direct reading R-meter, and resonating control; and all this in a day when those features were scarcely out of the laboratory.

Today we are building not one, but two, fine communication receivers—both of which, from all indications, are living up to the standards set by their predecessor of six years ago.

These models, known as the RME-69 and 70 have been designed and constructed with the same thoroughness which has given the older equipment such lasting qualities.

New parts, new tubes, and new circuits have been incorporated in RME receivers as rapidly as they have been developed, so that today, with their noise suppressors, high gain circuits, and stable characteristics they are extremely modern.

If the present RME receivers live up to the standard of longevity set by the 9D (and we think they will) they should still be in active service five years and even longer from now. Invest in a receiver which will give you years of continued satisfactory operation.

The new 12-page catalog is mailed to you on request.
UTC SPECIAL SERIES
of TRANSFORMERS for
AMATEUR APPLICATION

MAXIMUM VALUE AT LOW COST

FILTER, SWINGING, AND AUDIO CHOKES

<table>
<thead>
<tr>
<th>Type No.</th>
<th>Service</th>
<th>Inductance</th>
<th>Current</th>
<th>Resistance</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>S-23</td>
<td>Audio</td>
<td>500 Hz.</td>
<td>5 Ma.</td>
<td>6000 ohms</td>
<td>$1.35</td>
</tr>
<tr>
<td>S-24</td>
<td>P.P.</td>
<td>500 Hz.</td>
<td>3 Ma.</td>
<td>4000 ohms</td>
<td>1.50</td>
</tr>
<tr>
<td>S-25</td>
<td>Filter</td>
<td>30 Hz.</td>
<td>30 Ma.</td>
<td>900 ohms</td>
<td>1.80</td>
</tr>
<tr>
<td>S-26</td>
<td>Filter</td>
<td>15 Hz.</td>
<td>60 Ma.</td>
<td>330 ohms</td>
<td>1.90</td>
</tr>
<tr>
<td>S-27</td>
<td>Filter</td>
<td>30 Hz.</td>
<td>75 Ma.</td>
<td>160 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-28</td>
<td>Filter</td>
<td>20 Hz.</td>
<td>100 Ma.</td>
<td>350 ohms</td>
<td>1.65</td>
</tr>
<tr>
<td>S-29</td>
<td>Filter</td>
<td>10 Hz.</td>
<td>175 Ma.</td>
<td>95 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-30</td>
<td>Swinging</td>
<td>5/25 Hz.</td>
<td>175 Ma.</td>
<td>95 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-31</td>
<td>Filter</td>
<td>30 Hz.</td>
<td>300 Ma.</td>
<td>90 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-32</td>
<td>Filter</td>
<td>15 Hz.</td>
<td>400 Ma.</td>
<td>85 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-33</td>
<td>Swinging</td>
<td>5/25 Hz.</td>
<td>225 Ma.</td>
<td>120 ohms</td>
<td>2.10</td>
</tr>
<tr>
<td>S-34</td>
<td>Filter</td>
<td>20 Hz.</td>
<td>225 Ma.</td>
<td>120 ohms</td>
<td>2.10</td>
</tr>
<tr>
<td>S-35</td>
<td>Filter</td>
<td>10 Hz.</td>
<td>300 Ma.</td>
<td>90 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-36</td>
<td>Swinging</td>
<td>5/25 Hz.</td>
<td>300 Ma.</td>
<td>90 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-37</td>
<td>Filter</td>
<td>30 Hz.</td>
<td>350 Ma.</td>
<td>85 ohms</td>
<td>2.00</td>
</tr>
<tr>
<td>S-38</td>
<td>Swinging</td>
<td>5/25 Hz.</td>
<td>350 Ma.</td>
<td>85 ohms</td>
<td>2.00</td>
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</table>

SINGLE SECONDARY FILAMENT TRANSFORMERS

Primary Tapped 105, 115 Volts — 50/60 Cycles

<table>
<thead>
<tr>
<th>Type No.</th>
<th>Secondary Volts</th>
<th>Secondary Current</th>
<th>Insulation</th>
</tr>
</thead>
<tbody>
<tr>
<td>S-53</td>
<td>2.5 VCT</td>
<td>10 A.</td>
<td>1500 V.</td>
</tr>
<tr>
<td>S-54</td>
<td>5 VCT</td>
<td>4 A.</td>
<td>2500 V.</td>
</tr>
<tr>
<td>S-55</td>
<td>6.3 VCT</td>
<td>3 A.</td>
<td>1500 V.</td>
</tr>
<tr>
<td>S-56</td>
<td>7.5 VCT</td>
<td>3 A.</td>
<td>1500 V.</td>
</tr>
<tr>
<td>S-57</td>
<td>9.5 VCT</td>
<td>10 A.</td>
<td>10,000 V.</td>
</tr>
<tr>
<td>S-58</td>
<td>9.5 VCT</td>
<td>20 A.</td>
<td>10,000 V.</td>
</tr>
<tr>
<td>S-59</td>
<td>5 to 5.25 VCT</td>
<td>13 A.</td>
<td>5000 V.</td>
</tr>
<tr>
<td>S-60</td>
<td>5 to 5.25 VCT</td>
<td>22 A.</td>
<td>10,000 V.</td>
</tr>
<tr>
<td>S-61</td>
<td>7.5 VCT tapped</td>
<td>8 A.</td>
<td>3000 V.</td>
</tr>
<tr>
<td>S-62</td>
<td>10 VCT</td>
<td>10 A.</td>
<td>3000 V.</td>
</tr>
<tr>
<td>S-63</td>
<td>14 VCT tapped</td>
<td>10 A.</td>
<td>5000 V.</td>
</tr>
<tr>
<td>S-64</td>
<td>11 VCT</td>
<td></td>
<td></td>
</tr>
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MULTIPLE SECONDARY FILAMENT WINDINGS

Primary Tapped 105, 115 Volts — 50/60 Cycles

<table>
<thead>
<tr>
<th>Type No.</th>
<th>Fil. 1</th>
<th>Fil. 2</th>
<th>Fil. 3</th>
<th>Insulation</th>
<th>Net Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>S-64</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-5A</td>
<td>5 VCT-6A</td>
<td>3800 V.</td>
<td>$2.40</td>
</tr>
<tr>
<td>S-65</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-5A</td>
<td>5 VCT-6A</td>
<td>3800 V.</td>
<td>2.40</td>
</tr>
<tr>
<td>S-66</td>
<td>2.5 VCT-10A</td>
<td>7.5 VCT-5A</td>
<td>10 VCT-6A</td>
<td>3800 V.</td>
<td>2.40</td>
</tr>
<tr>
<td>S-67</td>
<td>5 VCT-6A</td>
<td>6.3 VCT-5A</td>
<td>10 VCT-6A</td>
<td>3800 V.</td>
<td>2.40</td>
</tr>
<tr>
<td>S-68</td>
<td>5 VCT-6A</td>
<td>6.3 VCT-5A</td>
<td>10 VCT-6A</td>
<td>3800 V.</td>
<td>2.40</td>
</tr>
<tr>
<td>S-69</td>
<td>6.3 VCT-5A</td>
<td>7.5 VCT-6A</td>
<td>5 VCT-6A</td>
<td>3800 V.</td>
<td>2.70</td>
</tr>
<tr>
<td>S-70</td>
<td>6.3 VCT-5A</td>
<td>7.5 VCT-6A</td>
<td>5 VCT-6A</td>
<td>3800 V.</td>
<td>2.70</td>
</tr>
<tr>
<td>S-71</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-12A</td>
<td>10,000 V.</td>
<td>4.50</td>
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<tr>
<td>S-72</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-5A</td>
<td>2.5 VCT-6A</td>
<td>5000 V.</td>
<td>3.00</td>
</tr>
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</table>

UNIVERSAL DRIVER TRANSFORMERS

(See Modulator chart for tube types)

<table>
<thead>
<tr>
<th>Type No.</th>
<th>Application</th>
<th>Net Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>S-8</td>
<td>Single driver plate to pushpull grids</td>
<td>$1.65</td>
</tr>
<tr>
<td>S-9</td>
<td>Pushpull driver plates to grids of class B tubes up to 400 watts output.</td>
<td>2.25</td>
</tr>
<tr>
<td>S-10</td>
<td>Pushpull 56, 6C6 triode, 6C5, or similar plates to 45's, 2A3's or 6L6's, self or fixed bias.</td>
<td>2.10</td>
</tr>
</tbody>
</table>

UNIVERSAL OUTPUT TRANSFORMERS

Any modulator tubes to any RF load

<table>
<thead>
<tr>
<th>Type No.</th>
<th>Audio Power</th>
<th>Net Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>S-18</td>
<td>12 watts</td>
<td>$2.10</td>
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<tr>
<td>S-19</td>
<td>30 watts</td>
<td>2.85</td>
</tr>
<tr>
<td>S-20</td>
<td>55 watts</td>
<td>3.90</td>
</tr>
<tr>
<td>S-21</td>
<td>110 watts</td>
<td>6.00</td>
</tr>
<tr>
<td>S-22</td>
<td>250 watts</td>
<td>8.40</td>
</tr>
</tbody>
</table>

UNITED TRANSFORMER CORP.
Write: COMMUNICATIONS DIV. * 150 VARICK ST. * NEW YORK, N. Y.
Export Division: 100 Varick Street NEW YORK, N. Y. Cables: "ARLAS"

QST for November, 1939, EASTERN Edition
READY TO GO

Equipped with the advanced noise limiter circuit described in October OST, the NC-101XA is ready to hang up new records. All the fine features, all of the outstanding performance of the older models have been retained, but to them have been added a noise limiter of truly remarkable effectiveness. The NC-101XA is master of adverse operating conditions. Combined with the NTE Exciter-Speech Amplifier, it forms the heart of a superb station.

NATIONAL COMPANY, INC., MALDEN, MASS.
Think of it! 225 watts power input to a $3.50 tube! Or, with a pair of the new RCA-811's or RCA-812's, you can use an input of 450 watts. That's real power plus real economy in any language.

This outstanding performance results largely from RCA's development of the Zirconium-coated anode, an exclusive RCA feature. These anodes mark an important forward step in the production of high-pervenance, high-power tubes at hitherto unheard of low costs. They run cooler. They do a better job of absorbing gases, even under high overloads. Other exclusive features of these tubes include the new low-loss RCA Micanol base, now available for the first time. Summed up, they answer the need for high power output with low driving power and moderate plate voltages—at a tube cost within the reach of all!

**Bulletin free upon request**

Class "C" Telegraphy Maximum Ratings

<table>
<thead>
<tr>
<th>*ICAS</th>
<th>*CCS</th>
</tr>
</thead>
<tbody>
<tr>
<td>1,500</td>
<td>D. C. Plate Voltage</td>
</tr>
<tr>
<td>150</td>
<td>D. C. Plate Current</td>
</tr>
<tr>
<td>225</td>
<td>Plate Input</td>
</tr>
<tr>
<td>55</td>
<td>Plate Dissipation</td>
</tr>
</tbody>
</table>

**NEW RCA DUAL RATING SYSTEM ANNOUNCED**

Ratings given here are the new RCA Intermittent Commercial Amateur Service (ICAS) and Continuous Commercial Service (CCS) ratings described in detail on Page 81 of this issue.