

NEW IRC® Distributed Parameter Delay Lines

FEATURE UNIFORMITY, STABILITY AND LOW COST

IRC's extensive mass production experience and technique in the manufacture of continuous lengths of wire wound resistive elements have now been utilized to produce a uniform high-quality, low-cost, distributed-constant delay line. Simplicity of design permits close control of electrical characteristics even to providing, in many applications, unusual phase characteristics to meet customers' special requirements.

> Encapsulation in phenolic impregnated rigid tubes with axial leads assures good stability under adverse environmental conditions. These delay lines are well suited for either point-to-point wiring or printed board applications.

> > If you have an application for distributed constant delay lines, we will be pleased to review your requirements. Send coupon for full details.

Features

TIME DELAY 0.2 to 1.0 microseconds IMPEDANCE 500 to 2500 ohms standard; higher and lower are available on special request

BANDWIDTH 3.5 MC and greater as required

TEST VOLTAGE 300 volts OPERATING TEMPERATURE 65°C

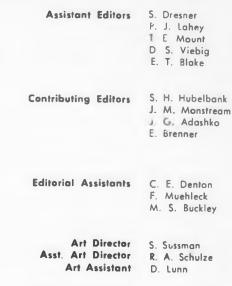
INTERNATIONAL RESISTANCE CO.

Dept. 266, 401 N. Broad St., Phila. B, Pa. In Canada: International Resistance Co., Ltd.,

Toronto, Licensee Send technical data and prices on the new IRC Distributed Parameter Delay Lines.

| COMPANY | |
|---------|--|
| ADDRESS | |
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CIRCLE 1 ON READER-SERVICE CARD FOR MORE INFORMATION



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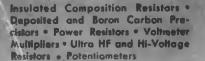
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Wherever the Circuit Says

Low Waltage Wire Wounds • Resistance Strips and Discs • Selenium Rectifiers and Diodes • Hermetic Sealing Terminals • Insulated Chokes • Precision Wire Wounds • Attenuators



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ELECTIONIC DESIGN . July 15, 1957

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G-V Hot Wire Time Delay Relays





WRITE for Publication No.35complete engineering data and drawings.



Designed for delay intervals which are longer than those produced by magnetic relays and shorter than can be produced by the usual types of thermal relays, these G-V Hot Wire Time Delay Relays make possible many simplified, lightened and improved designs.

How They Operate: G-V Series H Time Delay Relays employ a group of nickel-chromium alloy wires, 8 to 20 strands electrically in series and mechanically in parallel, as the actuating element. A mechanism holds these wires under tension and when the energizing current passes through these wires, heating them and causing elongation, the mechanism multiplies this and moves the contacts into or out of engagement.

Over two years of successful field service in electronic, aeronautical and industrial equipment prove these new G-V relays to be dependable, efficient and accurate.

ADJUSTABLE DELAY even though hermetically sealed DC or AC of any frequency for energization SMALL AND LIGHT. 1/4" diameter, 23/6" length. Weight: 1 oz. WIDE AMBIENT RANGE compensated from -70 C to 100 C or higher CONTINUOUS ENERGIZATION without damage AVAILABLE in 7-pin Plug-in and Flanged designs



18 Hollywood Plaza, East Orange, New Jersey

CIRCLE 2 ON READER-SERVICE CARD FOR MORE INFORMATION

Now, your choice of SILICON RECTIFIERS

from one reliable source (All available in production quantities)



Diffused junction STUD RECTIFIERS

Vie" Hex

Actual

Temperature Range, minus 65°C to plus 165°C

| AVE | RAGE CHA | RACTERIS | TICS |
|-------|---------------------------|--|--|
| Туре | Peak Inverse Volts* | Average Rectified Current** Amps. | Reverse Current (max.) at PIV mAdc at 25°C |
| CK846 | 100 | 1.0† | 0.002 |
| CK847 | 200 | 1.0† | 0.002 |
| CK848 | 300 | 1.0† | 0.002 |
| CK849 | 400 | 1.0† | 0.002 |
| CK850 | 500 | 1.0† | 0.002 |
| CK851 | 600 | 1.0† | 0.002 |
| 1N253 | 95 | 1.0‡ | 0.010 |
| 1N254 | 190 | 0.4‡ | 0.010 |
| 1N255 | 380 | 0.4 ‡ | 0.010 |
| 1N256 | 570 | 0.2 ‡ | 0.020 |

† Rated at 150°C ‡ Rated at 135°C



Diffused junction WIRE-IN RECTIFIERS

| AV | ERAGE C | HARACTER | ISTICS | | | |
|---------------|---------------------------|--|--|--|------|--------|
| Туре | Peak Inverse Volts* | Average Current 150°C Ambient | Rectified Amps. 100°C Ambient | Reverse Current (max.) at PIV mAdc at 25°C | | |
| 1N537 (CK840) | 100 | 0.25 | 0.5 | 0.002 | | |
| 1N538 (CK841) | 200 | 0.25 | 0.5 | 0.002 | 1000 | Actual |
| 1N539 (CK842) | 300 | 0.25 | 0.5 | 0.002 | 1000 | Size |
| 1N540 (CK843) | 400 | 0.25 | 0.5 | 0.002 | | |
| CK844 | 500 | 0.25 | 0.5 | 0.002 | | |
| CK845 | 600 | 0.25 | 0.5 | 0.002 | | |



POWER RECTIFIERS

Temperature Range, minus 65°C to plus 165°C

| | | MAXIMUM R | ATINGS | | | |
|---------|--------------------------|---|--------------------------|----------------------------------|-------------------------------------|-----|
| | | 125°C Case Tem | 125°C Case Temperature | | emperature | 1 |
| Туре | Peak Inverse Volts | Average Rectified Current** Amps. | Peak Current Amps. | Forward Voltage at 5 amps. | Reverse Current (max.) at PIV | W |
| CK774 | 25 | 5 | 15 | 1.5 | 5 mA | |
| CK775 | 60 | 5 | 15 | 1.5 | 5 | 1 |
| CK775-1 | 125 | 5 | 15 | 1.5 | 5 | 1 |
| CK776 | 200 | 5 | 15 | 1.5 | 5 | 8 |
| CK777 | 325 | 5 | 15 | 1.5 | 5 | Act |

*PIV ratings apply from -65°C to +150°C **Average rectified current into inductive or resistive lo

(RAYTHEON)®

SEMICONDUCTOR DIVISION

Silicon and Germanium Diodes and Transistors • Silicon Rectifiers

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CIRCLE 3 ON READER-SERVICE CARD FOR MORE INFORMATION

Editorial

Transistor Noise

Special issues generally run the risk of offering nothing of interest to a number of readers. Not so with transistors. All circuit and equipment designers are interested. The promise of unlimited life is a feature which can't be overlooked.

This is not to say transistors threaten the existence of vacuum tubes. Metal and ceramic tubes are available to operate at 500 to 800 C. The present target for top transistor operation is 500 C. By the time this is achieved, tubes will probably have exceeded 1000 C. Tubes are still well out front with regard to power, frequency response, high-temperature operation and tolerance to radiation. We expect transistors to catch up. According to Dr. Hebb of General Electric, there is every reason to expect improvements in the first three areas. Except for possible inherent limitations in radiation tolerance, Hebb finds no theoretical reason why transistors cannot match many types of tubes.

What seems to be needed is more competition. This may seem paradoxical in view of the fact that there are 430 different types in our fifth Transistor Data Chart, compared to 270 for last year. (These are types commercially available.) This impressive quantity belies the real situation. Only in a few cases do different manufacturers make the same or interchangeable types. (In only five cases are RETMA types made by more than one manufacturer.) Military designers in particular are reluctant, or may find it impossible, to specify transistors if there is only a single source available.

What may be needed is standardization of user demands. The perennial cry has been that manufacturers don't standardize. It will be a long time before there is or can be any standardization of manufacturing processes. Until that time, there will be few identical types. In the meantime, transistor manufacturers will put out many new types, more or less sampling the market. Those that look like they can be sold profitably will be manufactured. This means the designer's requirements and demands can influence what is made.

User criticisms about too many types but no similar types are worthless until there is an effort on the part of users to guide manufacturers intelligently. Tantalizing both users and manufacturers are valid accelerated life tests. Thwarting concentrated effort to take stock of what might be best for the future of the transistor industry is the celerity of manufacturers turning out better units and the frantic effort of users trying out all the new items. But such activity almost guarantees progress.—JAL

Next issue watch for the first of a two-part s ries on transistor network design. **Engineering Review**

For more information on developments described in "Engineering Review," write directly to the address given in the individual item.



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Two of the portable microwave stations are placed back to back to form a link. Each station can be broken down into individual units that can be carried on a man's back. The amount of time it takes to erect one of these stations is about five minutes.

Weighing less than 46 lbs per unit, a microwave communications system has been developed which should prove highly applicable to a multitude of military, emergency and industrial situations. Designed in Paris, France, by the Compagnie Generale de Telegraphie Sans Fil, the system is being marketed in this country by International Electronics Corp. of Mineola, Long Island, N.Y.

The purpose behind the design of the equipment was to furnish a system that could be carried piecemeal on men's backs and could be quickly and easily installed. As it turned out, one link of the MX-641 microwave system can be erected in approximately five minutes. The equipment is also waterproofed to allow floating it across bodies of water.

One of the components which gives this system a somewhat distinct appearance is the cigar-shaped antenna. Consisting of a disc-loaded aluminum rod, with the discs slightly varying in diameter and spacing according to frequency demands, the antenna has considerable advantages over parabolic designs in being quite light in weight and in having less wind resistance. Capable of producing a gain of about 18 db, the antenna can be easily attached to whatever offers itself, such as trees, telephone poles and the like. For the ordinary situation, a pneumatic mast permits raising of the antenna to a height of 22 ft. The length of the antenna is not critical; however, by making it longer, it becomes more directional.

A 2000 mc band was chosen in preference to a higher frequency so that rather long feeders to the antenna could be used without a crippling loss of power. Thus antennas can be set at considerable heights to achieve the required line of sight.

A terminal station, consisting of eight units, can be transported in a jeep, small trunk or by three



The microwave antenna with the new look can also be attached to trees and telephone poles. Offering less wind resistance than the parabolic type, the discloaded aluminum rod has a gain of about 18 db. men over terrain inaccessible to vehicles. Voltages from 105 to 240 ac v can be used for power. A switch permits selecting the proper transformer connection for the supplied voltage. A test meter for monitoring and adjusting all the important circuits in both the radio and pulse chassis is also included. Simply by juxtaposing two terminal stations, a relay station can be established. Links up to 180 miles are possible by means of such stations placed about 30 miles apart.



The Seagoing Air Force: In order to fill a missile tracking gap in the 5000 mile test range off the coast of Florida, the Air Force ARDC has taken to the water in ships obtained from no one other than the Army. Six cargo vessels were converted into telemetry ships, which will receive data from missile test flights over the Atlantic ocean and transmit this data back to Cape Canaveral, Florida.

Engineering Review

Color TV Studies Missile Takeoff

The color of flash and flame spurting from a missile during and shortly after takeoff can disclose considerable information concerning the missile's flight characteristics. Closed-circuit color TV will make the recording of such information possible, an accomplishment which was almost impossible previously without such a system. Required safety precautions and the variations in the brightness of the flame made it extremely difficult to observe its color.

The closed-circuit TV is being purchased by the Army from General Electric Co. The contract calls for delivery this month, and the system will be put to use at the Army's Missile Test Center at Cape Canaveral, Fla.

Lots of Juice

In 1963, 450 billion kw-hrs of electrical power will be required by American industry, according to Westinghouse Vice President A. C. Monteith. The figure is 12-1/2% higher than the estimate made in 1954.

Doped Gold Transistors

The development of doped gold processes, utilizing group 3 and 5 elements, for use in germanium and silicon semiconductor applications, is expected to eliminate major shortcomings of conventional materials by operating at room temperatures, and producing bright, uniformly distributed gold deposits in required thicknesses, directly from the bath. Doped with antimony or other elements, depending on the desired physical properties, the process is the result of work done by Precious Metals Division, Sel-Rex Corp., Nutley, New Jersey.

Although the electronics industry has taken advantage of gold's unique properties for years, gold processes containing small percentages of group 3 and 5 elements have not been reliable in proprietary salts or solutions, heretofore.

CIRCLE 4 ON READER-SERVICE CARD ►

Τ.

SILICON

FEATURE:

- Recovery times under .15 µsec
- High voltage ratings
- Operation up to 200°C
- High Inverse Resistance
- Subminiature size

MILITARY AND HIGH CONDUCTANCE TYPES

RATINGS AT 150°C AMBIENT

| Туре | Maximum Inverse Operating Voltage (volts) | Maximum Average Forward Current (ma) | Maximum Inverse Current (µa) @ V | | |
|------------|---|--|---|--|--|
| IN457* | 60 | 25 | 5 @ 60 | | |
| N458* | 125 | 25 | 5@ 125 | | |
| IN459* | 175 | 25 | 5 @ 175 | | |
| IN486A | 225 | 50 | 25 @ 225 | | |
| IN488A | 380 | 50 | 25 @ 380 | | |
| ALAM Tomas | | | | | |

*JAN Types

HIGH FREQUENCY AND FAST SWITCHING TYPES

| RATINGS AT 25°C | | | | | | | |
|-----------------|---|--|---------------------------------------|--|--|--|--|
| Туре | Maximum Inverse Operating Voltage (volts) | Maximum Average Forward Current (ma) | Inverse Recovery Time (µsec) | | | | |
| IN251* | 30 | 75 | .15 | | | | |
| IN252 | 20 | 100 | .15 | | | | |
| SG213 | 200 | 30 | .3 | | | | |
| SG223 | 200 | 55 | .5 | | | | |
| SG228 | 200 | 80 | t | | | | |
| JAN Types | | | | | | | |

Write for Bulletin TE1350

GERMANIUM DIODES

FEATURES

- Complete Reliability
- Superior Forward Conductance
- Higher Inverse Resistance
- More Uniform Characteristics
- Greater Ruggedness

| Туре | Forward Current at + IV (ma) | Inverse Current at Specified Voltage (μa @ V) | Max. Oper. Voltage (volts) | Description |
|------------|---------------------------------------|---|----------------------------------|----------------------|
| IN270 | 200 | 100 @ - 50 | 80 | |
| IN277 | 100 | 250 @ -50 75 @ -10 @ 75° | c ¹⁰⁰ | |
| IN276 | 40 | 100 @ - 50 | 70 | |
| IN281 | 40 | 500 @ - 50 30 @ - 10 | 60 | JAN TYPES |
| IN126 | 5 | 500 @ - 50 30 @ - 10 | 60 | |
| IN127 | 5 | 300 @ 50 25 @ 10 | 100 | |
| IN 198 | 5 | 250 @ -50 75 @ -10 @ 75° | C 50 | |
| IN283 | 200 | 20@-10 | 20 | COMPUTER |
| TIG | 40 | 100 @ - 50 20 @ - 10 | 60 | COMPUTER TYPES |
| IN278 | 20 | 125 @ - 50 @ 75° | C 50 | HI- |
| T22G | 40 | 20 @ - 10 @ 75° | | TEMPERATURE TYPES |
| T9G | 100 | 20 @ - 50 2 @ - 10 | 60 | HI- |
| IN67A | 5 | 50 @ -50 5 @ -5 | 80 | RESISTANCE TYPES |

Other JAN types: IN38A, IN69, IN70, IN81, IN128 Write for Bulletin TE1300 & TE1319

Irans

SILICON Power

FEATURES

- Reliability at High Temperature
- High Power Handling Ability
- High Efficiency
- Rugged Construction
- Hermetically Sealed

MINIATURE TYPES

| | RATINGS | AT | 150°C | AMBIENT | |
|-------|---------|--------------|-------|--|---------------------------------------|
| Туре | | Inve Volt | rrent | Maximum Average Forward Current (ma) | Maximum Inverse Current (ma) |
| TJIOA | | 10 | 0 | 200 | .5 |
| TJ25A | | 25 | 0 | 200 | .5 |
| TJ40A | | 40 | 0 | 200 | .5 |

SILICON RECTIFIER STACKS

| RATINGS AT 125°C AMBIENT | | | | | | | | |
|--------------------------|--------------------|-------------------|----------------------|--|--|--|--|--|
| | DC O | utput | | | | | | |
| Circuit | Voltage (volts) | Current (amps) | Stack Designation | | | | | |
| 6 ø Star | 150 | 30 | TL6SIAI/TR352 | | | | | |
| 3 ø Bridge | 325 | 18 | TL6FIAI/TR352 | | | | | |
| 3 d Halfwave | 1120 | 1.2 | TDI2Y6BIA4 | | | | | |
| I ø Bridge | 748 | 1.2 | TD1284CIA3 | | | | | |
| I & Center Tap | 250 | 3.0 | TD12C4C3A2 | | | | | |

SILICON VOLTAGE REGULATORS and REFERENCES

FEATURES

- Excellent long-term stability
- High current handling ability
- Operation to 150°C
- Extended operating current range
- Small size, easy mounting
- Hermetically sealed

Reference assemblies are available with temperature coefficients to .002%. They are also available with voltage tolerances to 1% from 10 to over 100 volts. The assemblies are encapsulated in a miniature axial lead package.

"Leadership in semiconductors"

itron

RECTIFIERS

| | Peak Recurrent | Maximum | Maximum |
|--------|-------------------|-----------|---------|
| | Inverse | Forward | Inverse |
| | Voltage | Current | Current |
| Туре | (volts) | (ma) | (ma) |
| | MILITARY | TYPES | |
| N253 | 95 | 1000 | .1 |
| N254 | 190 | 400 | |
| N255 | 380 | 400 | .15 |
| N256 | 570 | 200 | .25 |
| | STUD MOUN | TED TYPES | |
| TM47 | 400 | 3000 | .5 |
| TM64 | 600 | 1000 | .5 |
| | MEDIUM PO | WER TYPE | 5 |
| | | (amps) | |
| IN250A | 200 | 20 | 5 |
| TR30I | 300 | 10 | 5 |
| TR402 | 400 | 20 | 2 |
| | HIGH POW | ER TYPES | |
| | | (amps) | |
| | 100 | 35 | 5 |
| IN412A | 400 | 35 | 5 |

| Туре | Voltage Rang (volts) | Maximum Dynamic e Resistance (ohms) | Maxim Curre @ 25°C (ma) | |
|---------|-------------------------|--|----------------------------------|-------|
| Submini | iature | | | |
| 5V-5 | 4.3- 5.4 | 55 | 50 | 10 |
| SV-7 | 6.2- 8 | 8 | 30 | 6 |
| SV-II | 9.0-12.0 | 50 | 20 | 4 |
| SV-15 | 13.5-18 | 120 | 14 | 3 2 |
| SV-24 | 20 -27 | 300 | 10 | 2 |
| Miniatu | re | | | |
| SV-804 | 4.3- 5.4 | 55 | 150 | 30 |
| SV-806 | 6.2-8 | 8 | 90 | 18 |
| SV-810 | 9 -12 | 50 | 60 | 12 |
| SV-815 | 13.5-18 | 120 | 40 | 8 |
| SV-824 | 20 -27 | 300 | 27 | 5 |
| Power | | | 55°C (amps)* | (ma)* |
| SV-904 | 4.3- 5.4 | .5 | 2.0 | 500 |
| SV-906 | 6.2- 8 | .8 | 1.2 | 300 |
| SV-910 | 9 -12 | 1.5 | .8 | 200 |
| SV-915 | 13.5-18.0 | 3 | .6 | 150 |
| SV-924 | 20 -27 | 8 | .4 | 100 |

TE-1 352

TRANSISTORS HIGH FREQUENCY TYPES FEATURES • Low Icer typically under .02 µa Operation to 175°C Power Ratings of 200 mw

- **High Frequency Operation**
- Welded Hermetic Seal

SILICON

| Гуре | Minimum Common Emitter Current Gain B | Maximum Collector Voltage Vre Peak (volts) | Typical Cut-off Frequency (mc) | Maximum Collector Cut-off Current @ 25°C @ Vo Max. (µa) |
|------|--|--|---|--|
| STI2 | 40 | 15 | 16 | .5 |
| ST32 | 40 | 30 | 16 | .5 |
| STIL | 20 | 15 | 13 | .5 |
| ST3I | 20 | 30 | 13 | .5 |
| STIO | 10 | 15 | 9 | .5 |
| ST30 | 10 | 30 | 9 | .5 |

Write for Bulletin 781353

GERMANIUM Power TRANSISTOR

FEATURES

- Operation to 85°C
- Linearity at High Currents
- Up to 10 watts Dissipation
- Low Thermal Resistance
- **Small Size**
- **Hermetically Sealed**

| TYPE | Minimum DC Common Emitter Current Gain (B @ lc) | Voltage | Collector Current | Maximum Power Dissipation (watts) |
|-------|--|---------|----------------------|--|
| 2N83A | 8 @ I.0A | 60 | 3 | 10 |
| 2N83 | 8@ .5A | 60 | 2 | 10 |
| 2N84A | 12 @ 1.0A | 45 | 3 | 10 |
| 2N84 | 12 @ .5A | 45 | 2 | 10 |

Write for Bulletin TE1320

electronic corporation



Modified Matador

The Matador ground-to-ground tactical missile designed by Martin Co. and presently in operational use is being replaced by an improved version. Designated the TM-61C, the missile incorporates an improved guidance system developed by the Martin Co. Range of the TM-61C Matador will be substantially increased over the original version, and traffic capabilitiesthe ability to control more than one missile in the air at the same time-will be greater, thus making the firepower of a missile squadron much stronger.

One of the most important improvements in the TM-61C guidance system is stated to be the high resistance to electronic countermeasures. As in other Matador missiles, the TM-61C can be launched from rough terrain through the use of mobile launching platforms. The TM-61C is 39.6 ft long, 54 in. in diam and has a wing span of 28.7 ft. Operating at speeds of more than 650 mph, the missile is capable of altitudes over 35,000 ft.

High Altitude Altimeter

A new type altimeter, accurate in the ranges of from 75,000 ft to 225,000 ft, is being produced by Hastings-Raydist, Inc. of Hampton, Virginia. The altimeter operates on 115 v ac is unaffected by ambient temperature changes, and provides continuous direct altitude reading or recording. The instrument measures altitude by means of a transducer, which consists of a noble metal thermopile. At the higher altitudes it becomes much more sensitive than the usual bellows or capsule types of pressure indicators. Maximum sensitivity is in the range of a few mm of mercury.

These thermopile elements are compensated for ambient temperature and change of temperature. The transducer elements are designed using only metal to glass and have been operated satisfactorily through a range of temperature extending from -300 to +300 F. The elements react very rapidly to changes in pressure and altitude, having a lag of only a few hundredths of a second.

CIRCLE 4 ON READER-SERVICE CARD

Transitron

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Lightweight Radio Relay for Military

In line with the new Marine concept of helicopter assault operation. a new lightweight radio communications relay set that can be carried on a man's back to otherwise inaccessible battlefield locations is now available. Developed by Raytheon Manufacturing Co., Waltham, Mass., the set operates in the super high frequency range making it possible to reduce the diameter of the antenna to 2-1/2 feet.

The radios have a point to point range up to 10 miles or they may be linked in chain fashion to transmit up to 40 miles. Eight messages may be sent or received simultaneously. The complete radio and all auxiliary parts can be carried by a team of five men, the heaviest unit weighing about 55 lbs. Total weight of the entire unit is about 250 lbs.

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Science Faculty Fellowships

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The National Science Foundation announced that applications will be accepted after June 10, 1957, for a second group of Science Faculty fellowship awards to be made in this calendar year. Closing date for receipt of applications is Sept. 3, 1957. The primary purpose of these awards is to provide an opportunity for college and university science teachers to enhance their effectiveness as teachers. Fellowships are offered for study in the mathematical, physical, medical, biological, engineering, and other sciences.

The foundation's awards will be adjusted so that the combined supportfrom the Foundation and other sources-will not exceed \$10,000 per annum. Selection will be based on letters of recommendation, academic records, and other appropriate evidences of professional activity and competence. Application materials may be obtained from the Division of Scientific Personnel and Education, National Science Foundation, Washington 25, D. C. Completed materials must be received not later than September 3, 1957. Selections will be announced on October 18, 1957.

← CIRCLE 12 ON READER-SERVICE CARD

Data sheet on Lab-type Power Supply

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Data sheet on Stroboscope Unit

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| | Western Gear | [|
| | Corporation | 1 |
| | ENGINEERS AND MANUFACTURERS | 100 |

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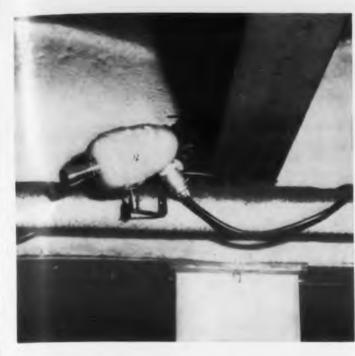
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Data sheet on Voltage Regulator



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Policing Via TV: An experimental closed-circuit TV system is being used by the New York Transit Authority to study the possibilities of increased efficiency in subway operations. Installed by General Precision Lab., N.Y., a small camera is mounted on a ceiling beam and focused on subway exit gates to prevent riders without passes from entering. A picture of the area is transmitted by coaxial cable to a monitor screen located nearby. The use of television cameras to police entire subway platforms as a further deterrent to crime is also being considered.



More Powerful Radar: Turret-like radar antennae located behind the Terrier missiles aboard the cruiser USS Canberra will be used for long range missile guidance. Developed for the Navy by Sperry Gyroscope Company, of Great Neck, N. Y., the AN/SPQ-5 radar systems came into fleet use after several years of testing. The two systems aboard the Canberra combine several radar functions in each unit. Either system can control the missiles from a single launcher or battery, or both radars can track different target groups simultaneously.

The systems include flexible modes of scanning and provide the advantage of early warning.

TUNG-SOLGERMANIUM COMPUTER

cracking the glass!

Here's the answer to the problem of how to make computer diodes so the lead wires can be sharply bent close to the glass body without cracking the end seal. It's the "ring seal" design, an exclusive Tung-Sol construction feature embodying a metal collar fused into the end-seal. The collar absorbs the strain of lead wire bends, thereby preventing damage to the diode enclosure

During its more than fifty years of lamp, electron tube and semiconductor manufacturing experience, Tung-Sol has had to over-come countless problems in glass to metal bonding. Almost every new product development and design improvement thru the years has presented new technological challenges. The resulting stockpile of experience in sealing glass to metal is one of the reasons for the



TYPICAL DIODE CHARACTERISTICS; Peak Inverse Voltage 75 volts Forward Current At 1.0 volt 75MA Reverse Currents At –50.0 volts 50 Microamperes Recovery Time Less Than 1.0 Microsecond

CIRCLE 6 ON READER-SERVICE CARD FOR MORE INFORMATION

high quality standards enjoyed by Tung-Sol

tubes and semiconductor products. Tung-Sol Diodes with "ring seal" construc-tion will be supplied in the standard RETMA or JAN types. The Tung-Sol junction-forming technique features an electronicallycontrolled bonding cycle. The result is a con-sistently accurate bond which assures maximum uniformity of electrical characteristics. ADDRESS INQUIRIES TO:

SEMICONDUCTOR DIVISION, Tung-Sol Electric Inc., 95 Eighth Avenue, Newark 4, New Jersey. BALES OFFICES:

Atlanta, Ga.; Columbus, Ohio; Culver City, Calif.; Dallas,Texas; Denver, Colo.; Detroit, Mich.; Irvington, N.J.; Melrose Park, Ill.; Newark, N.J.; Seattle, Wash. SPECIAL INFORMATION SERVICE :

Your name will be added to our Special Mailing List to automatically receive new data as it becomes available.

ELEC RONIC DESIGN . July 15, 1957

Engineering Review

Bombed Again

The ARDC has just disclosed for immediate publication its Talking Bomb which, when parachuted above the heads of enemy troops, will successfully talk them into surrendering. Judging from the number of news releases received during the past year on this aerial brainwasher, it would seem that it is the century's answer to the atom bomb. Possibly, the ARDC is carrying on an intensive investigation of the effects of psychological warfare. Hearing the same thing over and over again does have its effects, and we are duly impressed by the success of these always new but identical releases from the ARDC in causing frenzied distraction among our ranks. But before we throw down our pencils and surrender, we offer this last resistance as token of our firm belief that words can still be fought with words, without recourse to swords, bombs or other devices.

Resilient Mounts: a "Crutch"

When approaching the problems of vibration and isolation of airborne equipment, resilient mounts should be used if all other solutions have been investigated and appear impractical. According to a paper delivered at the AIEE Air Transportation Conference, isolation should always be regarded as a crutch, and all possible means should be used to obtain compatibility of equipment with environment without using resilient mounts.

The engineer was advised to proceed directly to the solution of resilient mounts only when the level of shock transmitted by the structure to the equipment supports is sufficiently greater than the fragility level, removing all doubt that no other means is practical. In short, this implies that a vibration specialist should be employed to translate environment level into terms comparable to fragility level. The engineer would then be able to consider the fragility factor in realistic terms, and therefore maintain better design control.



TWIST WIRES



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DIP IN SOLDER ...

Anaconda announces AnalaC an improved solo

New Analac* film-insulated, solderable magnet wire can be used similarly to Formvar or Plain Enamel—except that it is solderable without stripping!

Soldering by dipping, iron or gun produces a perfect joint—in just one second in finer sizes—without prior removal of the insulation. Analac reduces labor, saves time and money wherever many soldered connections are made, or where small diameter wire makes other means of insulation removal hazardous to the insulation or wire.

Not only this, Analac has the excellent abrasion resistance and other good mechanical properties of the enamel wire you're now using. It handles readily, performs well in high-speed winding.

Analac is colored a bright red with stable dve used many years for identical applications—making it highly visible even in finest sizes. This helps operators feel more secure, results in higher quality work. Distinctive color simplifies its identification, too, from nonsolderable wires

Analae is available in an exceptionally large range a sizes. The Man from Anaconda will be glad to give you more information and help with a production run in your plant. See "Anaconda" in your phone book—in most principal cities—or write: Anaconda Wire & Cable Ce opany Magnet Wire Headquarters, Muskegon, Michigan outer. U. S. Pat. of



OINT IS COMPLETED WITHOUT TRIPPING WIRE with Analac wire dipped in 50-50 tin-lead solder at 360°C (680°F). The insulation is noved at the temperature of molten solder.

ed solderable magnet wire



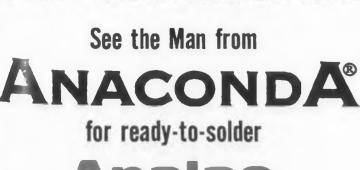
STRONG JOINTS—as strong as the same joints made in bare copper wire—are produced. Here in laboratory test, joint holds under high stress.



2. **EXCELLENT ABRASION RESISTANCE** of Analac is shown in this test. It has the same high windability normally associated with Formvar, Plain Enamel.



MOLDED-PLASTIC CASES – designed and developed by Anaconda–protect spools of Analac from damage during shipping. Result: no breaks due to bent spools.



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NEW CATALOG ON ANALAC Yours for the asking. Mail coupon for your copy. ANACONDA WIRE & CABLE COMPANY Magnet Wire Headquarters, Muskegon, Michigan. Please send me catalog C-95A on Analac ready-to-solder magnet wire.

| COMPANY | |
|-------------------|--|
| ADDRESS | |
| CITY. ZONE. STATE | |

Automatic Ferrite Memory Core Tester

An Automatic Ferrite Memory Core Tester, with the ability to test, select and reject cores according to the customer's specifications three times as fast as was formerly possible with most semi-automatic devices has been developed. Currently in operation at the RCA Components Division, Camden, N. I., the core tester couples a mechanical handling device with an electronic pulse program generator and electronic measuring and evaluating circuits. The device hopper-feeds 0.050 I.D. x 0.080 O.D. x 0.025 thick ferrite memory cores through the Tester. Each core is tested for its one output on a Go-No-Go basis. The Tester also examines each core for Disturbed Zero output, then classifies the test run into five groups according to value. In addition to its high-speed fully-automatic operation, it features the ability to segregate cores.

Retreat of Transistor Heat Barrier

Experimental use of new compound semi-conductors in place of germanium or silicon has led to laboratory types of transistors and diodes that can operate efficiently over a broad range of frequencies at temperatures as high as 850 deg F.

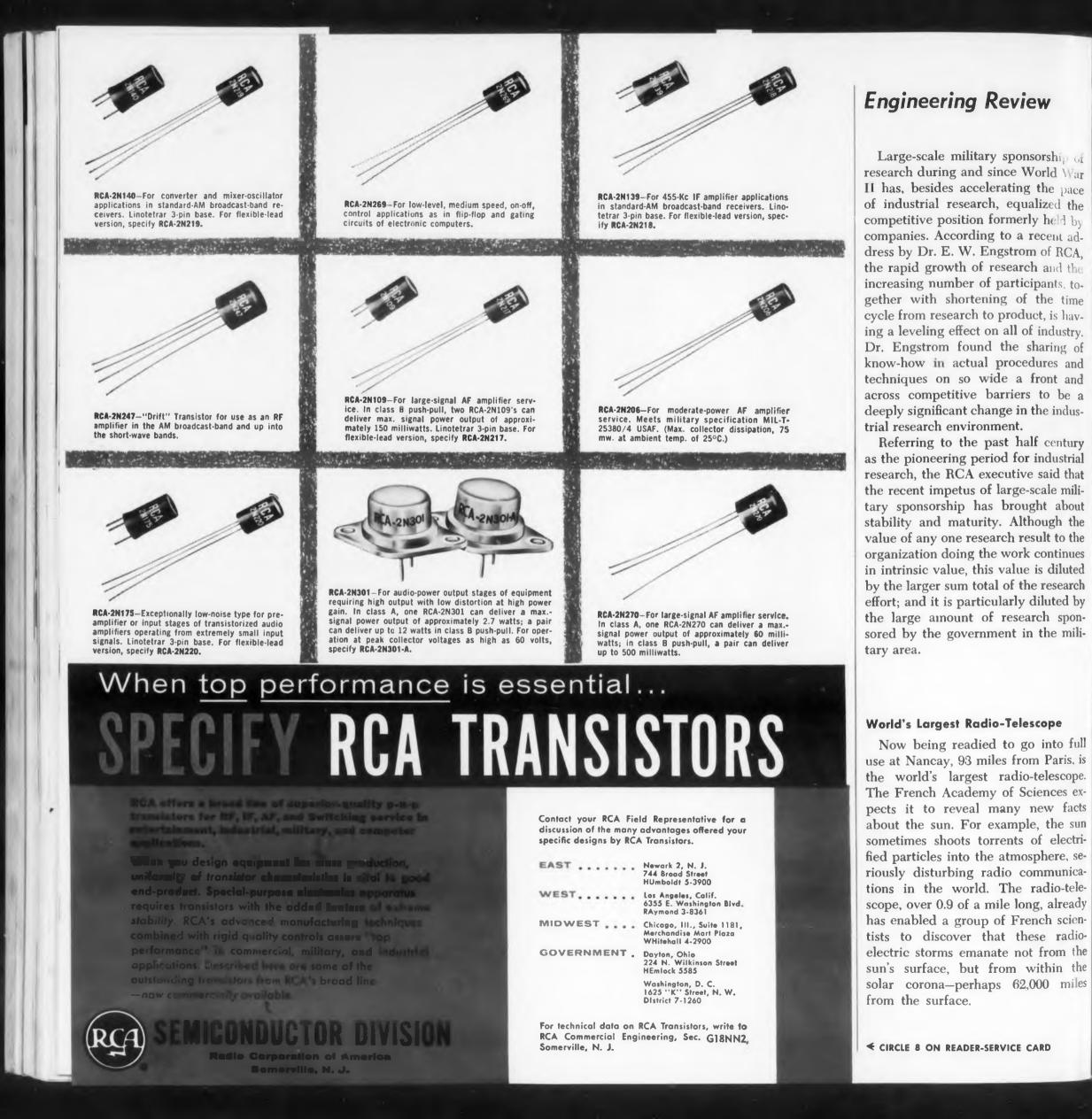
Describing recent work at RCA labs, Princeton, N. J., Dr. Dietrich Jenny noted that efforts to combine in a single material the best features of both germanium and silicon have now resulted in new experimental devices employing various compound materials, notably gallium arsenide. Germanium is most useful for its high frequency properties, silicon greater efficiency at higher temperatures.

Correction

In "Resistor Performance Levels," ED, June 15, 1957, the symbols for Composition Resistors and the New Pyrolytic General Purpose Resistors in the bar graph of Performance Characteristics (Fig. 6) were accidentally reversed. This leaves the erroneous impression that the performance of the new pyrolytic resistors was worst in the comparison, whereas—it was indeed the best.

CIRCLE 7 ON READER-SERVICE CARD

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combination of an automatic ator, a sonic altimeter, and a navi path indicator enables helicopglid ter lots to take off, fly to any spot insich a 100-mile area, make an instrui int approach to within 10 ft of the round and then land without ooking outside the helicopter cabin. The navigator system, developed originally by Decca Navigation Co. Ltd. of England, but being built for use in this country by Bendix-Pacific Corp uses transmission of radio signals from three ground stations to receiving equipment in the aircraft. The airborne unit, which weighs 40 lb, can pinpoint the helicopter's location with 25-ft accuracy. The triangular arrangement of stations creates a pattern of precisely known and stable geographical positions.

Position information is computed and displayed by decometers or by plotting boards. Pilots can follow the navigation-position lines displayed on the board, deviating from one line or direction to another as necessary, similar to the way one follows a road map from one city to another. The sonic altimeter weighs 16 lb and measures absolute altitude from 0 to 150 ft, with an accuracy of less than 6 in.

3-D TV?

A television screen, developed by the Naval Research Lab., may lead to three-dimensional television. In its present state it offers a simplified approach to color TV. The basis for the new screen is a process for depositing phosphor on the face of the TV tube in the form of thin, transparent films, instead of the opaque white powders now in use. Films that create different colors may be deposited on top of each other and may be lighted separately or mixed by controlling the speed or the direction of the electrons in the tube. By using one film of each of the three primary colors, the ciencomplete color spectrum can be obtained by proper mixing. The process n the has been successfully demonstrated in the a full range of colors. miles

how large is small?

DAVEN'S NEW MINIATURE WIRE WOUND RESISTORS PROVIDE AS **MUCH AS 400K RESISTANCE IN** 1/4 " x 5/16" SPACE

DAVEN's fully encapsulated, miniature, precision wire wound resistors offer the design and development engineer the solution to critical space limitation problems. DAVEN's advanced techniques provide the needed resistance value in a minimum of space, without sacrificing reliability. Where space conservation is a prime factor in your design, specify DAVEN miniature wire wounds.

Types and Specifications

| Туре | Dia. | Length | Max. Ohms | Max. Watts |
|-------|------|--------|--------------|---------------|
| 1274 | 3/16 | 3/8 | 100K | 0.25 |
| 1273 | 1/4 | 5/16 | 400K | 0.25 |
| 1283 | 1/4 | 5/16 | 400K | 0.25 |
| 1284 | 1/4 | 27/64 | .5 Meg. | 0.25 |
| 1250 | 1/4 | 1/2 | 900K | 0.33 |
| 1170A | 7/16 | 1/2 | 1.2 Meg. | 0.50 |
| 1170 | 1/2 | 1/2 | 1.8 Meg. | 0.50 |

· Fully encapsulated · Meet and exceed all humidity, salt water immersion and cycling tests as specified in MIL-R-93A, Amendment 3 • Operate at 125°C continuous power without de-rating . Can be obtained in tolerances as close as $\pm 0.02\%$ • Standard temperature coefficient is ± 20 PPM/°C.





Special temperature coefficients can be supplied on request. Write for our new resistor catalog.

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Engineering Review

Sperry is Superclean and Ultraprecise

Ultraprecision machining to 25 millionths of an inch has been achieved on a production basis by Sperry Gyroscope Co. for "floating" integrating gyros used as "stable tables." Cleanliness is a major problem in manufac. turing inertial navigation equipment. as specks of dust or bacterial organisms might cause errors of miles at the end of 5000-mile flights.

What is tolerable in the way of foreign particles and what constitutes a cleanliness hazard is not fully known. To be on the safe side, Sperry considers the assembly room the key to the problem. Sperry assemblers. that put floating integrating gyros and accelerometers together, work in what has been judged the cleanest place on earth. This pure environment is 5000 sq ft in size. Ceilings, walls and floors are vinyl covered. The skilled workers are carefully screened for desirable skin conditions, and are clad from head to toe in special nylon gowns, caps and boots (of different colors for psychological reasons). The uniforms prevent microscopic dust or lint from clothing from reaching the ultrasensitive elements put together under 45power microscopes. No paper is allowed in these rooms-"blueprints" are plastic sheets.

Sperry's all-out effort to design and analyze inertial components of extreme accuracy has resulted in the development of new supersensitive test devices. Reaction torques less than 0.05 dyne-cm and output torques accurate to 1/10 dyne-cm can be measured. Heavy seismic blocks for testing are completely isolated from the building floor.

Fabrication of the high-precision gyros on a production basis with needed accuracy and ruggedness is considered a manufacturing breakthrough. In addition to machining and cutting gears to 25 millionths of an inch, special deburring processes are used. Relatively new electropolishing techniques and dental polishing tools are used. A leak detector can note 2/10,000 micron per cu ft per hr.

CIRCLE 10 ON READER-SERVICE CARD

CIRCLE 11 ON READER-SERVICE CARD >

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NEW: from Beckman[®]

Berkeley

- Variable Time Base Universal EPUT[®] Meters
- For Direct Digital Readout Without Conversion!



NEW MODELS 7351

(shown on preceding page) and 7361

With their variable preset "count down" time bases, Models 7351 (100 kc) and 7361 (1 mc) Preset Universal EPUT* Meters are unique multipurpose instruments. Regardless of transducer conversion factors, results may be read in direct digital form by merely selecting the proper time base. These instruments will measure time intervals of any number of periods from 1 to 10,000 over the frequency range 0 to 10 kc, totalize a selectable sequence of events, divide frequency, function as single preset counters, generate pulses of varying frequency.

Applications include precise measurement of velocity, pressure, flow, viscosity, low and high frequency, frequency ratio and period, and tachometry.



NEW MODEL 5230 PORTABLE UNIVERSAL EPUT* METER

Combines many features of the popular Beckman/ Berkeley 7000 series in a new, light-weight portable instrument to perform the functions of a counter, timer, time interval meter, EPUT* meter, frequency, frequency ratio or period meter. Printed circuitry contributes to compact design, increased reliability and economical cost.

MODELS 7350 and 7360 UNIVERSAL EPUT* METERS

DESCRIPTION – These truly universal instruments combine high-speed electronic counting with a precision time base in multi-purpose circuitry. They function as counters, timers, time-interval meters, EPUT* meters, frequency, frequency ratio or period meters, or as secondary frequency standards.

All models have provision for standardization against WWV and may be coupled to external frequency standards. Connections are provided for driving Berkeley digital printers, data converters, or in-line remote readout units.

FEATURES

CESSORIES

- **1** 0.1 v rms sensitivity
- 2 Step attenuators; trigger-adjusted noise discriminators
- 3 More stable frequency dividers
- **4** Electronic (not relay) reset
- 5 External frequency standard input connection
- 6 AC or DC coupling of all input circuits; 10 megohm input impedance
- 7 Multivoltage accessory socket to power photocells, etc.
- 8 Binary-coded output with direct connection to digital printers, data converters, inline readouts, etc.
- 9 Crystal-controlled time marker output
- **10** Unitized modular design
- 11 Larger, brighter readout numbers
- **12** Modern-styled all-aluminum cabinets



MODEL 1452 DIGITAL PRINTER

Automatically and permanently records information from any Berkeley 5571 or 7000 Series instrument, prints data in digital form on standard adding machine tape from printer and scanner in one compact unit. May be modified to print "Time" or "Code" information simultaneously with data. Rack or bench mounted: available in up to B digits. One printout every 0.85 seconds. Price (6-digit), \$950.00.



MODEL 5916 IN-LINE READOUT

Large, illuminated in-line IN-PLANE figures reduce fatigue and error. Ideal for remote observation of data. Connects directly to any Berkeley 5571 or 7000 Series instrument. Presentation rate up to 15 per second; accepts binary voltages. Price (six digit unit), \$775.00.

TRANSDUCERS

A large number of transducers especially designed for use with Berkeley counting, timing, and frequency measuring equipment are available. These include tachometer pickups, photocells, and light sources. Specifications and technical description on request.

| RANGES-FREQUENCY | 0 cps to 100 kc | 0 cps to 100 kc | 0 cps to 100 kc | 0 cps to 1 mc | O cps to 1 mc | | |
|--|--------------------------|--|--------------------------------------|--|--------------------------------------|--|--|
| TIME INTERVAL | 100 µsec to 10' sec | 10 μsec to 10" sec | 10 μsec to 10 ² sec | 1 μsec to 10 ⁷ sec | 10 μsec to 10 ³ sec | | |
| PERIOD | O cps to 10 kc | 0 cps to 100 kc | O cps to 10 kc | O cps to 1 mc | 0 cps to 10 kc | | |
| TIME BASES | 0.1 and 1 sec | 10 µsec to 10 sec | Time Interval* Generator | 1 μsec to 10 sec | Time Interval Generator | | |
| COOED OUTPUT FOR DRIVING DIGITAL RECORDER, ETC. | \$30.00 extra | yes | yes | yes | yes | | |
| COUNT CAPACITY (READOUT) | 4 digit | 6 digit | 5 digit | 7 digit | 6 digit | | |
| ACCURACY | | ± 1 | count, \pm oscillator stab | ility | | | |
| OSC. STABILITY | 1 part in 10' per day | 3 parts in 10 st per week | 1 part in 10 ⁴ per day | 3 parts in 10 ⁶ per week | 1 part in 10 ⁴ per day | | |
| INPUT SENSITIVITY | 0.25 v rms | 0.1 volt rms** | | | | | |
| INPUT IMPEDANCE | 1 megohm, direct | | 10 megohm, dc | or ac coupled | | | |
| TRIGGER SLOPES | | | Positive or negative | | | | |
| CABINET DIMENSIONS | 12"H x 8"W x 14"D | 10¼" H x 20¾" W x 16½" D (Rack Panel — 8¾" x 19") | | | | | |
| APPROX. SHIPPING WT. LBS. | 30 | 60 | 50 | 60 | 50 | | |
| PRICE: (F.O.B. FACTORY) | \$575.00 | \$945.00 | \$1295.00 | \$1245.00 | \$1445.00 | | |

Complete technical specifications on Beckman/Berkeley Universal EPUT* meters and accessories are available promptly on request. Please address Dept. D-7.

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Berkeley Division

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Berkeley's world-wide staff of factory trained engineering representatives work closely with our sales office and the customer. They help the customer set up newly-purchased equipment, acquaint personnel with its operation and application, and make sure that it stays in operating order. The representative's job is not completed until he has "followedup" to insure that the customer receives maximum use from his instruments. These men will be glad to give you personal assistance at any time. A list of Berkeley representatives follows.

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DALLAS 9, TEXAS John A. Green Co. 6815 Oriole Drive Phone: Fleetwood 2-9918

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KANSAS CITY 14, MO. Leemark Associates 706 E. 73rd St. Phone: Jackson 3-9299

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ALBERTA & BRITISH COLUMBIA Hawthorne Electronics 107 Administration Bldg. Boeing Field, Seattle Phone: Wohawk 3962

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MIAMI 43, FLORIDA Murphy & Cota 11375 S.W. 46th St. Phone: Mohawk 5-1563

MINNEAPOLIS 3, MINNESOTA Pinkney & Hine 1925 Nicollel Ave. Phone: Federal 8-0523

NEW HAVEN 10, CONNECTICUT Broger Instrument Sales Co., Inc. 42 Church Street Phone: Spruce 7-6279

PHILADELPHIA, PENNSYLVANIA Gawler-Knoop Co. 835 Glenside Ave., Wyncote, Pa. Phone: Waverly 7-1820

PORTLAND 14, OREGON Hawthorne Electronics

700 S. E. Hawthorne Blvd. Phone: Belmont 4-9375

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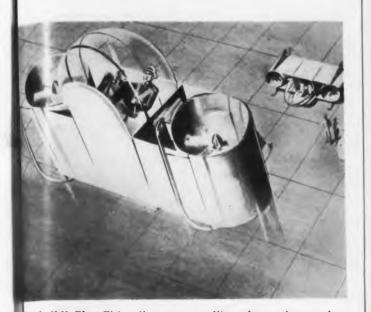
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tock N' Fly: This all-purpose utility plane, that rocks on take-off and landing, combines the aero-dynamic principles or ting wings, ducted propulsion and elevons. It rests on the ground horizontally and is rocked back into vertical take-off position with partial power. The alane lands the same way, backing down to the ground, then forward to rest. Designed by M. A. Novosel, the plane is one of the eighteen designs selected for awards in Mars Drafting Pencils Design Series. Another contest s planned for next season.

ramic-vs-Glass Tubes

Electron tubes made of ceramics will prove of rat value in atomic-powered and other high red aircraft according to Electronic Products, In a paper delivered before the Boston Chapof an IRE Group on Electron Devices, it was ited that ceramic materials can endure intense clear bombardment far better than the glass mponents of conventional tubes, making it posto remove considerable shielding weight from electronic systems of nuclear-powered planes. The construction of a stacked tube which uses mic parts extensively even for the envelope described. The tube parts are stacked one on the other in a radical departure from ordim assembly methods. While possessing electricharacteristics comparable to conventional bes, the ceramic stacked tubes are smaller than unterparts. The unusually stable life performwe of stacked tubes under conditions of shock, bration, and high ambient temperatures was inted out. This performance was attributed to resiliency of the ceramic material, the stacked ustruction, and the high-temperature outgassing t can be employed in the manufacturing procof the tubes.

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LOWELL CONSOLES

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 Located
- Equipment is Well Protected
 Single, Deuble and Triple Ped-
- estal Units With Turrets
- Handsome Styling
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LOWELL RACKS

- Versatility
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- Durability
- Transmitter Racks for 19", 24", and 30" Panels—181/2" and 24" Deep
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For Industry . . . Schools . . . Airports . . . For Broadcasting . . . Recording . . . Testing Apparatus

. . .

Lowell has a complete line of electronic housings and equipment over 200 models. Write for complete catalog and specifications.

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MANUFACTURING COMPANY

3030 Laciede Station Road, St. Louis 17, Missouri In Canada: Atlas Radio Corp., Ltd., 50 Wingold Ave., Toronto 10, Ontario

CIRCLE 5 ON READER-SERVICE CARD FOR MORE INFORMATION

Washington Report

Herbert H. Rosen

Wilson Directives to Curtail Defense Spending

Now that we are into the Government's new fiscal year, some of the pressure on cost-saving in defense projects may be somewhat relieved. However, the effects of three recent Wilson directives on spending are expected to have far-reaching effects on the future of electronics. One directive concerns overtime work. It is merely a reaffirmation of existing ASPR regulations governing the authorization of overtime on defense contracts. The final decision on whether a project is of sufficient importance to warrant overtime engineering and labor will rest chiefly with the Government's project engineer. He has been given instructions that will help guide him to his decision.

Another order was designed to lop off some \$500 million from the Fiscal '57 spending budget just passed. But the order seems to have come a little too late to be wholly effective, as was hoped. The inertia of Government projects just does not allow a cut of this magnitude in so short a time.

The third order restricts the services from letting a contract for a project or program until all of the money required for their completion is in the "bank." This means the services cannot order 100 widgets, pay for 20, and hold up delivery on the remaining 80 for some later date when and if the money is made available.

In terms of the future, these directives mean that the defense effort, especially in electronics, is stretched out for an undetermined length of time. Sec'y of the Air Force Douglas estimates that the directives mean an ultimate cut of over \$3.5 billion from the AF's purchasing ability. Some programs that have been marginal for lack of conclusive data may now very well be discontinued until more money becomes available—if it ever will.

But of particular importance, the element of time is severely sacrificed. No one has been able to figure out just how bad a sacrifice this will eventually be. Another factor obviously overlooked is that much of the huge spending in '57 and '58estimated at about \$42 billion-is the result of two or three year old programs coming into fruition. In all, some severe economies will have to be instituted by the electronic industries. From here on the cry will be for the same or better gear as before at a lower price. It will be up to the design engineer to give his company that equipment.

Is Automation Passe?

A meeting in Washington of the IRE Professional Group on Production Techniques seemed to prove one thing: There's reasonably little that's new in

LOW VALUE CAPACITORS

Simplest, most economical fixed composition types yet produced. Color-coded values from 0.10 to 10.0 µµf. Bulletin GA.

New! CERAMIC PERMANENT MAGNETS

The permanent magnets that are really permanent! Made from non-critical, lowcost ceramic powders. Write for new Stackpole Ceramagnet[®] Bulletin RC-10A.

CERAMAG[®] FERRO-MAGNETIC CORES

Characteristics of Stackpole Ceramag Cores are maintained with remarkable uniformity regardless of size or shape. Standard deflection yoke, "U," cup and threaded screw types. Complete facilities for special types. Ask for Bulletin RC-9A.

MOLDED COIL FORMS

Molded of high-resistance powdered iron with firmly-anchored, easy-to-solder wire leads. Bulletin RC-10C.

FIXED COMPOSITION RESISTORS

1/2-, 1- and 2-watt composition types in all standard RETMA ranges. Low noise level... unsurpassed humidity protection ... easily-soldered, firmly-anchored leads.

VARIABLE COMPOSITION RESISTORS (Controls)

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LINE SWITCHES

Types to provide practically any desired switching arrangement for Stackpole Variable Resistors. Ask for Bulletin RC-10B.

SLIDE SWITCHES

1/2 to 3 amp. UL approved types for maximum switching versatility and convenience in appliances, TV and radio sets, instruments, toys, etc. Bulletin RC-10D.

POWDERED IRON CORES

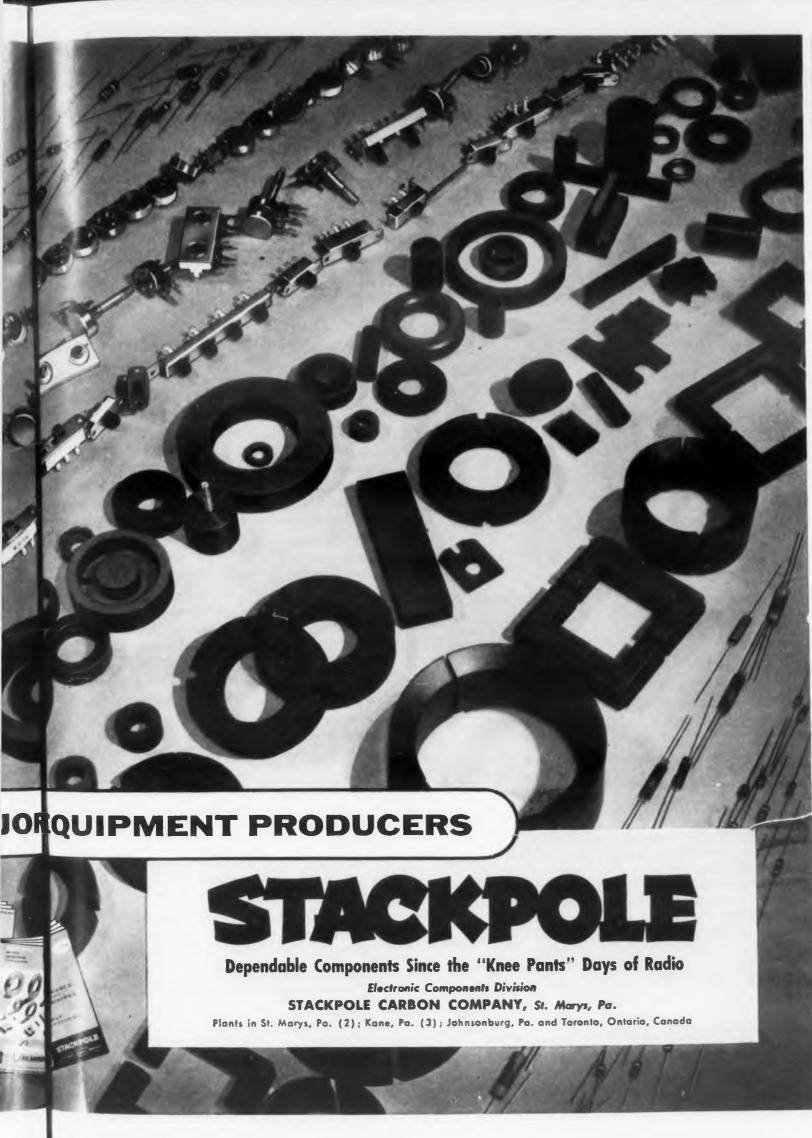
Insert, cup, sleeve, threaded, choke coil, sidemolded and plain core types. Also Stackpole preferred type "EE" Cores for maximum economy. Bulletin RC-10C.

A MAJOR COMPONENT SOURCE...for MAJOR

Bulletin RC-10B Variable Resistors and Line Switches Bulletin RC-10C Powdered Iron Cores and Coil Forms Bulletin RC-9A Ceramag^(P) Ferromagnetic Cores Bulletin RC-10D Slide Switches Bulletin RC-10A Ceramagnet^(P) Permanent Magnets Bulletin GA Low-Value Capacitors



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1957 ELECTRONIC DESIGN . July 15, 1957

the field of automatic production. Further, that while the electronic industries are and will be to a greater extent responsible for automation in other industries, the "art" is a long way off for itself. True, mechanization may become more highly refined. But the day of automatic feedback loops and computer directed mechanization that will control the assembly of a piece of electronic gear is far off.

The meeting did demonstrate one important concept to the design engineer. The concept of standardization. From here on in there will be greater and greater emphasis on cost coupled with reliability. And it seems that the only way to achieve these two factors simultaneously is by standardization.

One step in this direction is RETMA standard RS-188. This lays down the recommendation that "dimensions which must be controlled for automatic purposes be multiples of 0.025 inch." The standard also represents an early attempt to bring about an era of mechanical standardization. It also means that if an end assembler hopes to mechanize any of his production capability, his design engineers may have to design the end equipment around these suggested standards.

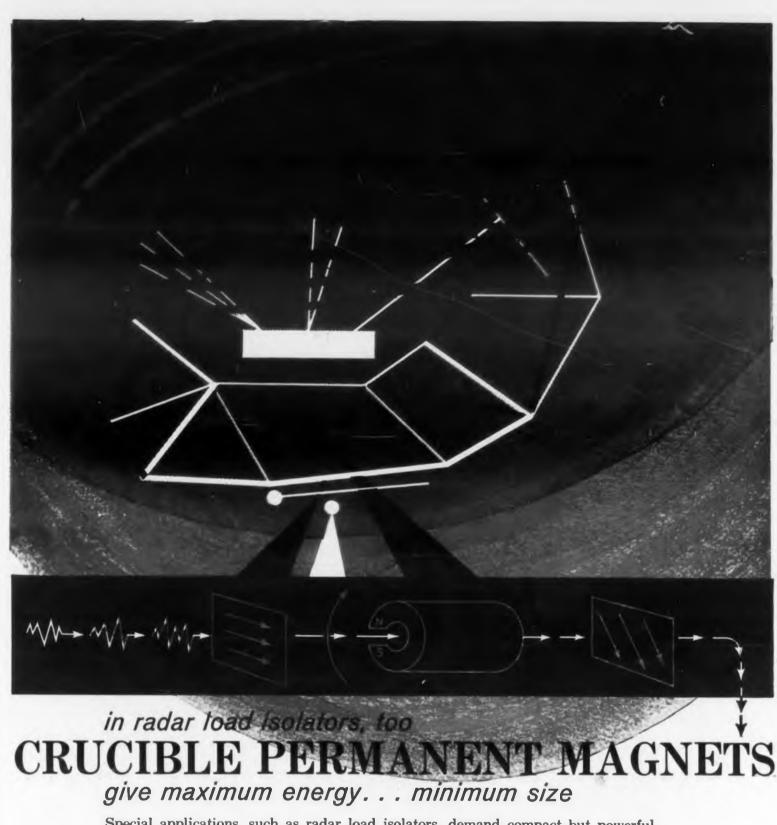
Another document disclosed at this meeting concerns itself with design requirements for printed wiring used in electronic equipment produced for the Signal Corps. It lays down suggested ground rules for circuit design, packaging, printed wiring boards, component mounting, modular dimensions.

Anticollision Study

Bendix Aviation has been awarded a small Air Force contract to help defray their costs for developing a device to give proximity warning and avoid collision of airplanes. The company has been working on the problem for about 2 years and have reached the point of proving their mathematical hypotheses. The Air Force has asked Bendix to study the problem, first, from the standpoint of defining the proximity and collision problems. Once this has been done, possible technical approaches to the solution of the defined problems are to be suggested. Finally, Bendix is to build a research model of the instrument that is supposed to do the job. Deadline for the project is March 1958.

Behind all of this activity is a minimum market worth \$10 million. This is the value set by the airlines industry on what they—as a combined group would pay to equip their airliners.

And still in the realm of air safety and navigation, the Department of Defense has finally declassified four types of Doppler radar. Generally, these units are self-contained navigation aids and fit in ideally with the space and power limitations of a commercial airliner. By type numbers, the equipments released are AN/APN's 66, 78, 105, 79, and 67. A commercial version of the APN-66, called the RADAM, is supposed to be turned over to ATA by General Precision Laboratories via the Air Force.



Special applications, such as radar load isolators, demand compact but powerful magnet assemblies. And this is but one of the many places where the *consistently* higher energy product provided in Crucible Alnico magnets pays off.

These Crucible Alnico permanent magnets can be sand cast, shell molded, or investment cast to exact size, shape or tolerance requirements... and in any size from a mere fraction of an ounce to hundreds of pounds.

The design and production of permanent magnets has been a Crucible specialty ever since Alnico alloys were discovered. It's one of the good reasons why so many people bring their magnet applications to Crucible. Why don't you? Crucible Steel Company of America, The Oliver Building, Mellon Square, Pittsburgh 22, Pa.

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Steel

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Printed Circuit Board Problems

Gentlemen:

I found your editorial appearing in the January 15th issue of ELECTRONIC DESIGN to be very timely As of this date, we are experiencing considerable difficulty with one of our suppliers who builds a piece of airborne electronic equipment for us, due to printed circuit board problems. Certainly, you indication that evidence is accumulating showing that plated through holes on printed circuit boards are oft times troublesome is disturbing to us, since we plan a change to "plate-through" holes as a solution to some of our problems. Specific information that you may have concerning types and frequency of failures would be of immediate interest.

Noting that an association of manufacturers is now being set up to establish standards for printed circuits, I would appreciate being advised as in the membership of this group with the thought in mind of contributing our experience as well a requirements to assist in their undertaking.

W. E. Shannon Electrical Design Group Allison Division General Motors Corp. SU

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> The technical problem seems to be with soldering plated-through holes. See article on p 40, April 1 ELECTRONIC DESIGN for an hourglass hole configuration which may be a solution. We have received many such letters from people expressing concern about the problem.

Our latest word is that the manufacturers association is not yet officially formed. According RETMA, Committee 40C on Printed Circuits has recently been reorganized into subcommittees more efficiently consider printed circuit problems Subcommittees are: 40C2, Industrial Standard Survey; 40C3, Conductivity and Temperature Rise 40C6, Arc and Flame Resistance; 40C7, Insulation Resistance; 40C8, Adhesion and Solderability; 40C1 Definition and Register; 40C10, Contamination 40C13, Mechanical Consideration; and 40CH Hardware.

Crucible

Letters to the Editor

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The Russian translation starting on page 180 of your March 1st issue describes "A new photoconductive pickup tube of the Vidicon type. . .recently developed in Russia. . . ," employing SB_2S_3 .

It may be of interest to recall here that an SB_2S_3 Vidicon of very high sensitivity was rather extensively described back in September, 1951 in this country in the RCA REVIEW article "Properties of Some Photoconductors, Principally Antimony Trisulfide" by S. V. Forgue, R. R. Goodrich and A. D. Cope.

One of our modifications of SB_2S_3 having good speed of response has been commercially available for several years in the RCA 6198 Vidicon.

> Stanley V. Forgue RCA Laboratories Princeton, N.J.

> > (2)

16"

Type K1328

11⁄4" Type 6467 5"

Type 6364

Type 6292

• It's comforting to know the U.S.S.R. is five years behind, in this instance at least.

Correction

In the article, "Cooling Packaged Electronic Equipment," Part I, May 15, equation (2) should read:

$$h_p = \frac{h_1}{[1 - e^{-(t_l/T)}]}.$$

The expansion of the exponential should read:

$$t^{-(t_1/T)} = 1 - \frac{t_1}{T} + \frac{t_1^2}{2!T^2} - \frac{t_1^3}{3!T^3} + \dots$$

Correction Please!

Martin Berger of Minitran Corp., 5 Oliver St., Newark, N.J., was the unidentified author of "Transformer Design Nomograph-III" appearing on page 36 of the June 1st issue. Minitran Corp. manufactures miniaturized transformers. We regret that the by-line was omitted.

Precise

PHOTOELECTRONICS*

* The conversion of light input to highly magnified electrical output in a dependable, precise relationship.

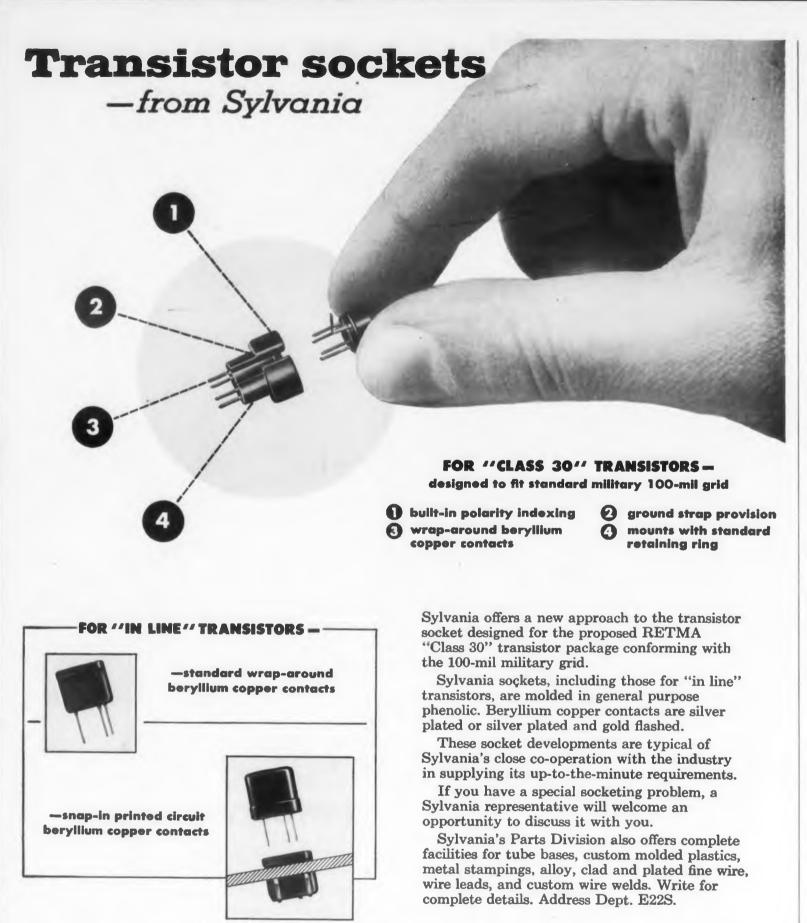
Depend on Du Mont Multiplier Phototubes for precise quantitative and qualitative measurements. Available in a wide selection of sizes and electrical characteristics for every photoelectronic need.

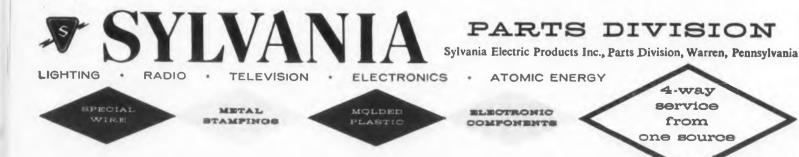


Type 6363

Type 6365

Industrial Tube Sales, ALLEN B. DU MONT LABORATORIES, INC. 2 Main Ave., Passaic, N. J. CIRCLE 16 ON READER-SERVICE CARD FOR MORE INFORMATION





CIRCLE 17 ON READER-SERVICE CARD FOR MORE INFORMATION

Meetings

Aug. 7-9: Sixth Annual Conference on Industrial Applications of X-Ray Analysis

Albany Hotel, Denver, Colo. Sponsored by the Denver Research Institute Metallurgy Div. Twentythree papers will be presented. For further details write to the Metallurgy Div., Denver Research Institute, Univ. of Denver, Denver 10, Colo.

Aug. 20-21: Third Biennial Electron Beam Symposium

General Electric Co. X-Ray Dept., Milwaukee, Wis. There will be reports on radiation equipment, applications of radiations, and economic evaluation of processes and methods. Chemical, plastic and petroleum applications are to be stressed. A conducted tour of GE facilities for fabricating electron beam generators and linear accelerators will be offered. More information may be obtained from J. J. Ludwig, General Electric Co., X-Ray Dept., 4855 Electric Ave., Milwaukee 1, Wis.

Aug. 20-23: Wescon (Western Electronic Show and Convention)

Cow Palace, San Francisco, Calif. Sponsored by the San Francisco and Los Angeles Sections representing the Seventh Region IRE and West Coast Electronic Manufacturers Association. For more information write to Don Larson, Business Manager, 342 N. LaBrea Ave., Los Angeles 36, Calif.

Aug. 29-30: Fourth Annual Symposium on Computers and Data Processing

Albany Hotel, Denver, Colo. Sponsored by the Denver Research Institute. Technical papers on components, devices, systems organization, analysis techniques, and design techniques will be presented. For further information write to J. Marshall Cavenah, Electronics Div., Denver Research Institute, University of Denver 10, Colo.

Sept. 4-6: Special Technical Conference on Magnetic Amplifiers

Penn Sheraton Hotel, Pittsburgh, Pa. Sponsored by the AIEE and the IRE. The program's four sessions will deal with New Circuits and Techniques, Analysis and Design, and Applications. For more information, write to D. Feldman, Bell Telephone Labs.

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Sept 8-13: Second Annual Course on Investment Cas gs

MI Cambridge, Mass. Sponsored by the Invest-Casting Institute. Lectures, laboratory men trial exercises and demonstrations will be offered on invesment materials; melting; gating, risering, the solidication and heat transfer; metal and alloy entysystems; defects in castings; and consideration of tails new investment and allied processes. For further information, write Harry P. Dolan, Investment Casting Institute, 27 E. Monroe St., Chicago 3, Ill.

Sept. 9-13: Twelfth Annual Instrument-Automation **Conference and Exhibit**

Cleveland Auditorium, Cleveland, Ohio. Sponsored Wis. by the JSA. Organized under the unifying theme, ap "Instrumentation for Systems Control," the confern of ence will open with formal sessions devoted to data and handling and instrument terminology. Following conthese there will be individual workshop sessions in tron limited discussion groups covering such topics as 1 be aircraft and missiles (excluding propulsion), wind from tunnels, flight propulsion systems, process indusept., tries, power generation and distribution, meteorological, nuclear, medical, geophysical exploration and general industrial laboratories. Some 100 papers will be presented at the technical sessions. There will be about 500 exhibits. For details of the techand nical program write to Herbert S. Kindler, Director of Technical Programs, ISA, 313 Sixth Ave., Pittsv the burgh, Pa.

Sept. 17-18: RETMA Symposium on Numerical Connfortrol Systems for Machine Tools , 342

Ambassador Hotel, Los Angeles, Calif. For details write to RETMA, Room 650, 11 W. 42nd St., New York 36, N.Y.

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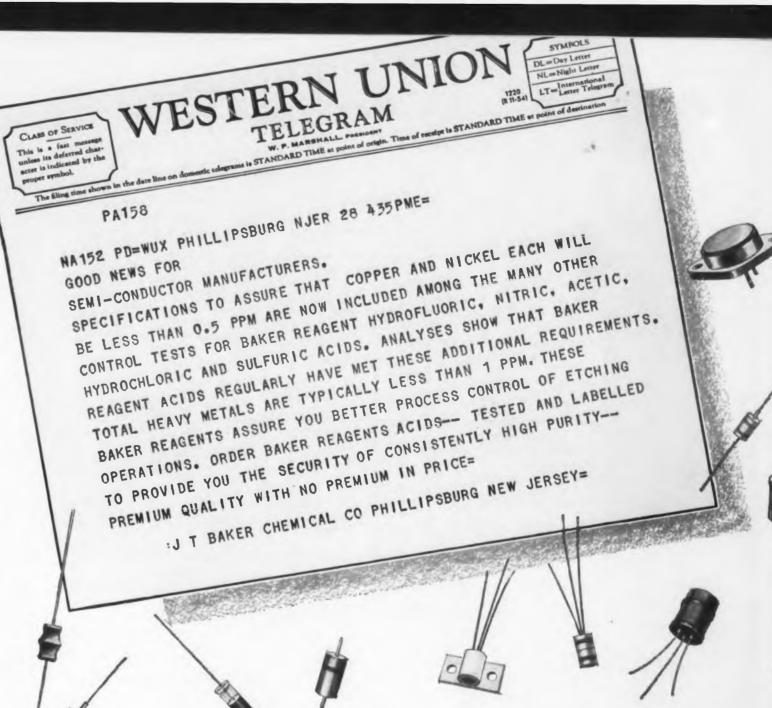
Sept. 24-25: Sixth PGIE Symposium on Industrial Electronics

Morrison Hotel, Chicago, Ill. Sponsored by the IRE s on Professional Group on Industrial Electronics and lysis AIEE. The main theme for the conference will be prethe characteristics, use and integration of transshall Instiducers into complete systems to measure and control complete processes. For further details, write ^{to} J. N. Banky, 628 West 18th Street, Chicago, Ill.

Oct. 16-18: 1957 IRE Canadian Convention Aagand Exposition

Automotive Building, Exhibition Park, Toronto, d by Canada. Sponsored by the Canadian Sections of the sions IRE. For information write to Grant Smedmor, IRE naly-Canadian Convention, 745 Mt. Pleasant Rd., Tomaronto 7, Canada.

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SEMI-CONDUCTOR CHEMICALS

Acetic Acid, Glacial Acetone Ammonium Hydroxide Carbon Tetrachloride Chloroform Ether, Anhydrous Hydrochloric Acid Hydrofluoric Acid

Hydrogen Peroxide 30% Solution Methanol Nitric Acid iso-Propyl Alcohol Sodium Carbonate Sodium Hydroxide Sulfuric Acid **Xviene**

OTHER ELECTRONIC CHEMICALS

Acetic Acid **Aluminum Nitrate Aluminum Sulfate** Ammonium Carbonate Ammonium Chloride Ammonium Phosphate Antimony Trioxide Barium Acetate Barium Carbonate Barium Fluoride Barium Nitrate Benzene Boric Acid Cadmium Chloride Cadmium Nitrate **Cadmium Sulfate** Calcium Carbonate Calcium Chloride Calcium Fluoride Calcium Nitrate Calcium Phosphate Ether, Petroleum Hydrochloric Acid Lithium Chloride

Lithium Carbonate Lithium Nitrate Lithium Sulfate Magnesium Carbonate Magnesium Chloride Magnesium Oxide Manganous Carbonate Methanol Nickelous Chloride Nickelous Nitrate Nickelous Sulfate Nitrate & Oxide **Nitric Acid** Potass. Dichromate Potass. Hydroxide Radio Mixtures Silicic Acid Sodium Chloride Sod. Phos. Dibasic **Strontium Nitrate** Sulfuric Acid Toluene Triple Carbonate Zinc Chloride

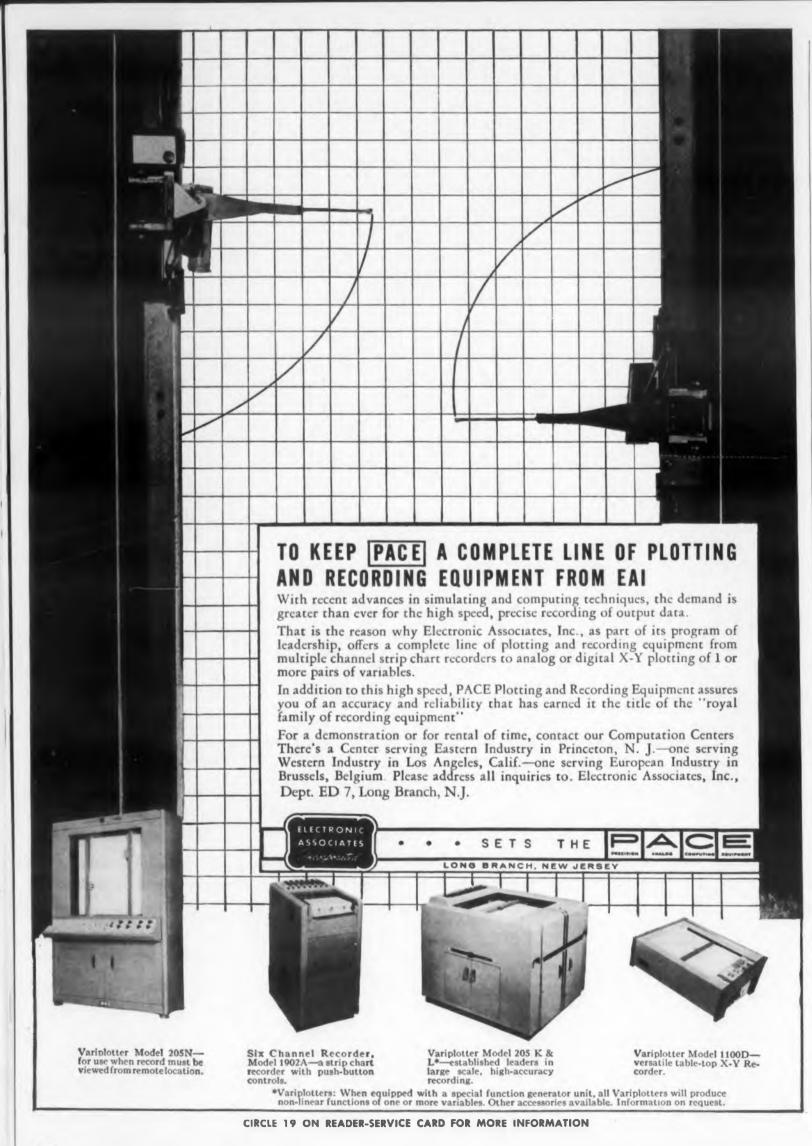
FOR SEMI-CONDUCTORS

These new control tests for copper and nickel have a double significance for the manufacturers of electronic components. They prove that:

- 1. Baker reagent purity regularly offers the qualityplus needed for semi-conductor manufacture.
- 2. As the electronics industry is able to define its needs more precisely, Baker will continue to provide material meeting the required specifications.

Listed at the left are some of the other Baker high purity chemicals of particular importance to electronic manufacturers.





Oct. 31-Nov. 1: Third Annual Technical Conference Nor of the Professional Group on Electron Devices, IRE. on

Shoreham Hotel, Washington, D.C. Those interested in submitting papers should check the paper deadlines at the end of this section. For more information, write W. M. Webster, RCA Semiconductor Div., Somerville, N.J.

Nov. 6-8: Tenth Annual Conference on Electronic Techniques in Medicine and Biology

Boston, Mass. Sponsored by ISA and AIEE. Further details and advance programs may be obtained from H. S. Kindler, Director of Technical Programs, Instrument Society of America, 313 Sixth Ave., Pittsburgh 22, Pa.

Nov. 6-8: Third Aero-Com Symposium

Hotel Utica, Utica, N.Y. Sponsored by the IRE Professional Group on Communications Systems. The conference will deal with systems, equipment design, techniques, antennas, spectrum conservation, air traffic control, management and other topics. For the presentation of confidential material, there will be a classified session on Nov. 8. For more information, write to R. C. Benoit, 138 Riverview Pkwy., Rome, N.Y.

Nov. 11-13: Third Annual Instrumentation Conference

Biltmore Hotel, Atlanta, Ga. The theme of this conference will be "Instrumentation for Data Handling" with special symposiums on electronic instrumentation as applied to medicine and the sales and purchasing aspects of electronic instrumentation. Papers should be submitted to Lamar Whittle, Federal Telecommunications Lab., 1389 Peachtree St., N.E., Atlanta, Ga. For more information write B. J. Dasher, School of Electrical Engineering, Georgia Institute of Technology, Atlanta, Ga.

Nov. 13-14: Mid-America Electronics Convention

Municipal Auditorium and Hotel Muehlebach, Kansas City, Mo. Sponsored by the Kansas City Section of the IRE. There will be exhibits and twelve technical sessions. Approximately thirty papers will deal with medical electronics, airborne electronics, instrumentation, engineering management, electronics in nucleonics and a diversity of other subjects. Persons who want to submit papers should contact the Technical Papers Chairman, MAECON, 5109 Cherry St., Kansas City 10, Mo. The deadline for submissions is Aug. 15. For more information write Richard L. Clarke, 425 Volker Blvd., Kansas City 10, Mo.

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Nov. 13-15: Eighth National Conference ence on Standards IRE.

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St. Francis Hotel, San Francisco, Calif. Sponsored by the American Standards Association. Emphasis will be on standards as a key to progress and profits. Sessions will cover radiation exposure, electronics, industrial preparedness, motion pictures and television, purchasing, company standards, technical communications, government standards and safety. For more information, write to D. E. Denton, ASA, 70 E. 45th St., New York 17, N.Y.

Dec. 9-12: Seventh Eastern Joint Computer Conference and Exhibit

Sheraton-Park Hotel, Washington, D.C. Sponsored by the IRE, Association for Computing Machinery and AIEE. "Computers with Deadlines to Meet" will be the central theme. Papers will be presented on record keeping, materials handling, traffic, deadline data reduction, communication, flight simulation, and other computer deadline areas. For more details, write to Malcolm B. Catlin, Council for Economic and Industry Research, Inc., Arlington 2, Va.

Jan. 6-8: Fourth National Symposium on Reliability and Quality Control

Hotel Statler, Washington, D.C. Sponsored by the IRE, ASQC and AIEE. Covering fields of reliability in the electronic industries, the symposium will encompass the following topics: reliability organization and management; theory and mathematical techniques; application of these techniques; design information; and education and training for reliability. For detailed information, contact Richard M. Jacobs, RCA Bldg. 108-2, Moorestown, N.J.

Paper Deadlines

Nov. 1: Deadline for papers to be presented at the 1958 IRE National Convention. The convention will be held March 24-27 at the Waldorf-Astoria h, Kanand the New York Coliseum, New York, N.Y. Pros-Section e techpective authors should submit a 100-word abstract rs will and a 500-word summary. Both must be in triplicate with the title of the paper and the name and adtronics, dress of the author. The technical field in which electhe paper falls must also be indicated. Only papers er subnot published or presented prior to the convention should will be considered. Military or company clearance ECON, eadline must be obtained before submittal. Address all mation naterial to Dr. George L. Haller, Chairman, 1958 Technical Program Committee, IRE, 1 E. 79th St., Kansas New York 21, N.Y.

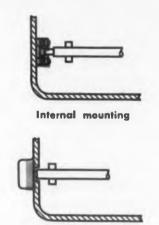
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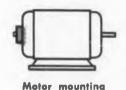
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NESTON *bearingless* Tachometer Generators



ITED STATOR

Pad mounting



Now . . . design engineers are achieving more efficient, more flexible speed indications and control without external generator attachments. The new Weston bearingless tachometer generator is so compact and light in weight it can be built right into equipment, or mounted on rear motor shafts. The cost is far less than for the conventional tachometer installation; and due to design simplicity, maintenance-free service is assured. Can be used with individual indicators, or with duplicate or remote indicators, calibrated in any function of the R.P.M. . . . as well as with Weston potentiometer recorders. For speed alarm or control, Weston sensitive relays are available. Speed ranges from low as 500 up to 100,000 R.P.M. full scale. Engineering assistance is available to original equipment manufacturers on all tachometer problems. Literature on request ... Weston Electrical Instrument Corp., 617 Frelinghuysen Avenue, Newark 12, N. J.





CIRCLE 20 ON READER-SERVICE CARD FOR MORE INFORMATION



What is the Status of Transistors?

Bernard Reich

U. S. Army Signal Corps Eng. Labs. Ft. Monmouth, N. J.

THIS report covers the current status of transistor development. Specific areas of transistor development are discussed; power, high frequency, and switching.

Over the last three years, the state of the transistor art has progressed quite rapidly. During this period new advances were made to allow operation at higher temperatures in germanium devices, and to remove existing frequency barriers; however, the designer interested in developing equipment utilizing transistors has the primary problem of securing devices which are available and reliable. Because of the nature of the industry, the availability and reliability of devices has not been defined. [The Transistor Data Chart section lists the types reported by manufacturers as being available.] This lack of definition regarding the current status of transistor development requires amplification. It is the purpose of this paper to clarify, as much as possible, the status of transistor developments and the extent of availability. The statements set forth are based on the experience of the writer in his contacts with the transistor industry.

Power Transistors

Two to three years ago the upper limit for germanium power transistors was 10 to 15 w. These ratings were attainable under the most optimum conditions and very limited numbers were available. Maximum operating junction temperatures of 80 C were quoted; however, the reliability of most devices at this temperature was not defined, or may not have been known. By the spring last year most power transistors were rated at 85 C operating junction temperature. Many manufacturers sold units meeting this specification; but often poor hermetic seals caused device failure during operation. Although the effects of moisture on junctions was well known at the time, apparently no short-term test was available to remove leaky devices. Experiments performed at these Laboratories indicated a definite correlation between operating failures and non-moisture resistant transistors.

During the last year, the power transistor demand has increased many-fold by the inclusion of the devices in the audio output stages of automobile receivers. With this requirement on the transistor industry has come the fabrication of devices capable of operating at junction temperatures to 100 C. In some instances, devices manufactured to these specifications are guaranteed a minimum of 1000 hours of reliable operation. The transistors utilized in radio applications have collector-to-base or collector-to-emitter voltage ratings of the order of 40 v, and thermal resistances of 1 to 4 deg C per watt. There are approximately eight suppliers of this type of device, and most of the suppliers use the same type of package indicating semi-standardization in power transistors.

In limited instances, the above devices are suitable for military applications; however, provisions must be made for higher voltage operation. Units have been manufactured with the required voltage ratings by approximately six suppliers. Of the higher voltage units, one is presently covered by a Signal Corps specification.

Other units are available with thermal resistances of 1 deg C per watt or less; however, the number of manufacturers is limited to two or three.

The impetus of the automobile radio business, and the requirements for power transistors in power supplies have caused the number of power transistor suppliers to increase. Because of the competition involved, the yields in manufacture have increased, making available power transistors for other uses.

The discussion on power transistors thus far has been limited to germanium devices. Some applications require silicon because of the temperature limitations on germanium. Some power transistors (approximately one-watt devices) have been fabricated in silicon by grown-junction techniques. Grown junction silicon transistors and some early development alloy silicon power transistors have been fabricated. One of the major problems is the alpha vs. I_r response of these devices leading to high output harmonic distortion in audio circuits. It appears that the upper operating junction temperature of silicon devices presently available is in the neighborhood of 150 C. t.

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Future developments in silicon power devices will include fabrication by diffusion techniques. At this time, it is difficult to see whether any startling operational differences will be noted. This can be explained by the lack of information on the nature of the silicon material and associated surface conditions. In addition, high temperature materials associated with the fabrication of silicon devices must be developed. Eventually, silicon power devices will be available with operating junction temperatures of 200-300 C. Much research and development work is still necessary before the full benefits of silicon transistors will be realized.

Switching Transistors

The potentiality of transistors will be fully exploited in the switching applications area. Computers utilize many transistors and other semiconductor devices. Long life under mild operating conditions are requirements.

For low-speed switching applications such as de to de converters, many germanium audio devices in various power ranges exist. With the additional specification of the key-parameters requisite of a switching transistor, devices normally used as audio amplifiers can be employed. As with all audio devices fabricated by alloying techniques, p-n-p transistors are more available than the n-p-n variety. Some n-p-n germanium transistors fabricated by grown-junction techniques do exist; however, these devices bear the characteristics resulting from fabrication by this method. It appears, at present, that there are many different types of p-n-p devices for w-speed switching applications. Some of these vices are covered by military specifications, while many others are commercially available. A few of the n-p-n units are comparable to the p-n-p counterparts.

In the low-power medium-speed switching range, many alloy germanium p-n-p devices exist. In general, the availability of this type of device is consubered fair. There are some n-p-n switching devices in this area manufactured by three suppliers. The overall availability of these units is considered poor to fair, mainly because of fabrication problems.

Core switches developed for computer use also fall into this same general frequency area. Some limited operation core switches are available commercially. The Signal Corps, at present, is developing both germanium and silicon core drivers. A very limited number of feasibility samples have been evaluated. In coming months, state-of-the-art samples will become available. Approximately one year hence, pilot-line production quantities are expected. Summarizing the core switch situation, some commercial units are presently available; however, more units should appear in about one year.

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New developments are occurring in the highspeed switching area where rise times in the order of a few millimicrosec are required. Already an extremely limited quantity of devices have been evaluated with rise, storage and fall times in the neighborhood of 10 millimicrosec. These devices are being fabricated by diffusion techniques. It is believed that in the next 18 months, many more units should be available for circuit evaluation, and limited numbers for equipment models.

High-Frequency Transistors

The development of high-frequency transistors will open new areas of application in communications equipment. A year ago, alloy or surface barrier homogeneous base transistors were being used. In addition to these triode devices, some tetrodes were and are still used in high-frequency applications. At that time, some devices were available for operation as radio-frequency and intermediate frequency amplifiers up to about 10 mc.

With the advent of the p-n-i-p and drift transistors, the limiting frequency barrier was lifted. The possibility of operating transistors to 3000-5000 mc is now feasible. It is known that many interested device manufacturers are utilizing the advantages of the p-n-i-p and drift structures.

At present, the supply of diffused-base high-frequency transistors is quite limited; however, it is expected that within the next 12 to 18 months more units will be available for advanced circuit design and development. At that time, 200 mc amplifiers and oscillators should be available.

Silicon Transistors

At present, for operating junction temperatures of over 100 C, it is necessary to use silicon transistors. Most silicon transistors available are of the grown type and are supplied mainly by two manufacturers. For high-power, high-current operation, silicon transistors are practically non-existent. [For a new type see ED, June 15, p 42.] Most silicon devices suffer from high saturation resistance and low current gains at higher current levels.

The operating temperature potential of silicon should be in the range of 200-300 C. At present, available devices are rated to about 150 C. The technology of preparing silicon is not understood as well as is necessary for the fabrication of better devices. Injection efficiencies of the emitter diode must be improved to improve current gain. Silicon surfaces require study in order to be understood. It is also difficult to predict when silicon transistors will become as available as comparable performing germanium devices.

In summarizing, it can be stated that germanium audio devices of various power levels are available. One of the major problems in this area, which should be overcome within the next year, is standard packaging.

Low and medium-frequency p-n-p switching transistors are in fairly good supply. The n-p-n varieties, especially the alloy type, are not as available. High-speed switching devices are in extremely limited supply.

High-frequency p-n-i-p or drift types are, at present, in extremely limited supply. It is expected that this type will blossom within the next 12 to 18 months.

The advances to be made in silicon transistor fabrication are difficult to estimate because of the status of very basic material problems.

New Frontiers in Solid-State Physics



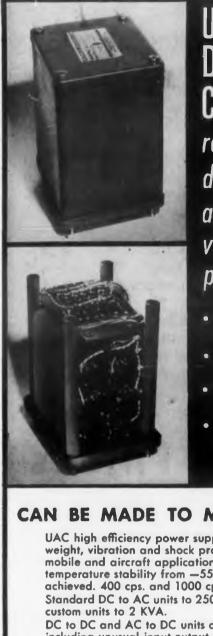
Dr. Malcolm H. Hebb Manager, General Physics Research General Electric Research Laboratory Schenectady, N. Y.

M UCH of industry's interest in solid-state science is related to the importance of solid-state devices to automation. Those who have made the most careful studies of tomorrow's population trends and production requirements describe automation not as a problem of the future but rather as the only solution to a problem of the future. A key function of electronics in automation is control, and the key requirement for control elements is reliability. Solid-state devices give every promise of providing the ultimate in long life, low maintenance, and reliability that will be required if automation is to be a dependable servant instead of a sick relative requiring constant nursing and medication.

Included in control-whether control of a chemical process, control of a manufacturing operation, control of inventory or of distribution-are three functions: 1) sensing the actual state of affairs, 2) processing the information so obtained with such aids as computers and instructions stored in memory devices, and 3) finally the execution of the control. For all of these control tasks, and particularly for the first two, solid-state devices are being developed at an ever-increasing pace. For sensing elements there are tiny devices that see (photo detectors), hear (piezoelectric materials), feel (magnetic materials), and smell (leak detectors). A solid that tastes is not known to the author, but it might be made if there were sufficient demand for it. There are many forms of solid-state substitutes for brain cells, although none thus far that could reproduce the complexity of the human brain in anything smaller than a warehouse packed with approximately ten billion transistors, ten billion transformers, ten billion solid-state memory cells, and more wire than anyone-even a machine-would want to think about. Solid-state devices can *talk* and they can *do*. And best of all, by performing these functions in solids, we can foresee the day when all of these devices can be built to last a lifetime, using very little power to operate them, and requiring no maintenance at all.

An example of how the transistor may turn up in some unexpected places in tomorrow's world is the report that automobile designers are working on a transistorized fuel-injection system. This appears to be an application never considered for the vacuum tube, however, most ideas for the use of transistors involve putting them in places now occupied by vacuum devices.

One can look forward to developments in another direction. Of particular interest are devices comprising more than one or two rectifying junctions. An example is a rectifier—somewhat like a hook



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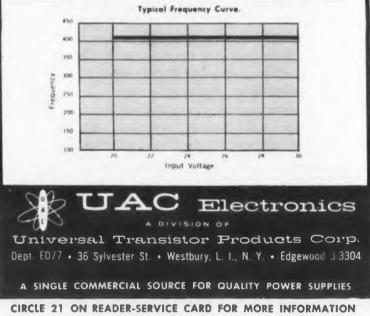
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|----------------|-------|----------------|-----|------------------|--------------------|-----------|---------------|
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| 10VA/115-400 | 10VA | 115-400 | CPS | .1 | 31/32x219/32x41/32 | 2 lbs. | 200.00 |
| 100VA/50-1000 | 100VA | 50-1000 | CPS | 2 | 32% x 311/12 x 5% | 31/2 lbs. | 300.00 |
| 100VA/115-1000 | 100VA | 115-1000 | CPS | 1 | 32% x 311/32 x 5% | 31/2 lbs. | 300.00 |



transistor-that might "fire" over a controlled part of the electrical cycle in the manner of a thyratron.

Photoconductors

The previous mention of solid-state devices that "see" was a reference to a whole family of photo detectors-photoconductors, photo diodes, photo transistors. Because they are relatively inexpensive and have high output, the photoconductors are coming in for a large share of scientific attention. Recently RCA announced it is making a photo conductive cell for use in a headlight dimmer for automobiles. General Electric's X-ray Department uses photoconductor detectors in an x-ray system that "looks" through beer cans to ensure that they are completely full before they leave the brewery. This way is faster than detecting a light can by its weight. Improved photoconductors would also extend the usefulness of the vidicon, that is now limited mostly to industrial TV applications because of low sensitivity and speed of response.

Tiny germanium-junction photoelectric cells recently announced by Standard Telephones and Cables Limited in Great Britain are less than a tenth of an inch in diameter and are designed specifically for scanning operations in punchedcard and perforated-tape machines. They speed operations by eliminating certain machined and other intermediate steps involved in storing information from punched-card systems.

Electroluminescence

Solid-state devices can be light-producing as well as light-sensitive. Electroluminescence-the well-publicized "wall of light" phenomenon to which important contributions have been announced recently by Sylvania and Westinghouseis essentially the direct conversion of electrical energy into light energy in a solid phosphor film. There is no question but that-with improvements in efficiency-electroluminescence will have an important place in the lighting techniques of the future. We should not forget, however, that even if it can become an economically efficient producer of light, the "wall of light" has certain limitations. One of the author's associates, tongue in cheek, has suggested that if Edison had invented electroluminescence instead of the light bulb, every research laboratory would be knocking itself out trying to produce a different kind of electric light source, one that wouldn't take up the whole wall and could be put in some compact form-maybe even in a little glass sphere.

Junction Light Sources

Solid-state research may have an answer to the need for more efficient light sources that also are compact. Some semiconductor junctions emit light when a current is passing through them. Although this phenomenon has been useful in clarifying certain theories of "breakdown" in transistors, it has not yet been evaluated as a useful source of jigh because of the extremely poor efficiency. Some the solid-state theoreticians at G.E.'s Research Laboratory, however, have ventured that the junc tion light source just might be the key to getting closer to the theoretical 200 lumens from ever watt of electricity instead of the approximately 2 lumens per watt produced by a good incandescen bulb and the 60 lumens per watt of fluorescen lamps.

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"Light-carrier" Amplifier

An interesting combination of the two solid-state been phenomena just discussed-light sensitivity and light production-is involved in a method of controlling electric currents in a manner that cannot be accomplished by ordinary relays or amplifiers In this system, electrical energy is converted into light by a form of electroluminescence; the light therefrom falls on a light-sensitive photoconductor. producing an electrical current. This sounds like a complicated method of starting out and ending up with the same thing-electrical energy-but it oflers certain opportunities for control that might not be possible by more straightforward methods.

New Light Amplifier

The converse of the above system would be to use light to control an electric current through a photoconductor and then convert the electric energy back into light by electroluminescence. A number of systems of this type have been developed under the general description of "light amplifiers." G.E. has developed another method of light amplification that is unique because the amplification and conversion (in this case the conversion of one kind of light energy directly into another kind of light energy) all takes place in a single solidstate layer of phosphor. The most appealing application at the present time appears to be in x-ray fluoroscopy, where amplification and conversion in a simple, thin device would combine a brilliant image for the doctor and minimum exposure for the patient.

The Cryotron

The Cryotron appears to be the first practical application of the phenomenon superconductivity Superconductive materials actually have no electrical resistance at all at extremely low temperatures-within a few degrees of absolute zero. The Cryotron is an amplifying device that makes use of the superconducting properties of tantalum when cooled in liquid helium. Because it is compact, simple, and inexpensive in construction-and consumes very little power apart from the modest power needed to create the very low temperatures -the Cryotron may play an important role in computers.

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"Maser" stands for Microwave Amplifier by Stimulated Emission of Radiation. Not all of the Masers developed to date are solid-state devices, although the solid-state Masers appear-obviouslyto have conspicuous advantages. Applications of the Maser are expected to be principally in the amplification of radar signals and in scatter communication.

Purity—Needed Breakthrough

Thus far devices, applications-even gadgets have id-state been discussed. Now let us turn to one fundamental that is important to the future of solid-state physics -purity. Purity has one meaning to a preacher, of concanno another to a water commissioner, but to the solidplifiers state scientist purity has a meaning that is difficult ed into to visualize. Semiconductors demand the extreme in e light freedom from chemical impurity and freedom from ductor, structural imperfections such as misplaced atoms. ; like a Germanium and silicon are routinely prepared with ling up no more than one part per billion of electricallyit oflers active impurities. They have been prepared with not be no more than one part per trillion. Some concept of this last number is given by noting that it is less than one counterfeit dollar in the national debt.

> This critical need for purer materials seems somewhat paradoxical since almost all semiconductor devices require eventually that certain impurities be intentionally introduced. However, other impurities must still be vigorously excluded, and to improve practical devices we must have the understanding that comes from studying extremely pure materials.

Eventually these efforts may produce the materials or the knowledge that can lead not only to important devices for industry and defense but even to cheaper and better lighting, or to babysitting TV sets, or to electronic computers that do most of the household chores automatically. Everyday use of solid-state electronic helpers "at home" will demand low-cost devices, and learning how to make power materials is closely tied to making electronics less expensive.

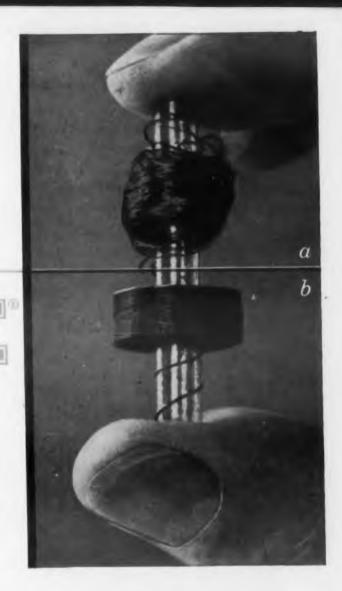
To accomplish some of the new things mentioned it will be necessary to extend the technology now available for silicon and germanium to other materials. It will require the talent and cooperation of several scientific disciplines: physics, metallurgy, chemistry, and others.

Keep an eye on the fundamental efforts to produce purer, cleaner materials for solid-state research. This is the "breakthrough" that is needed to produce many of the fantastic electronic devices that have been promised for the future.

Adapted from a talk at the 1957 IRE National Convention for use by ELECTRONIC DESIGN.

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Coils wound with (a) conventional film wire; (b) Grip-eze. Note clean pattern of Grip-eze as compared to fall-down of conventional film wire.

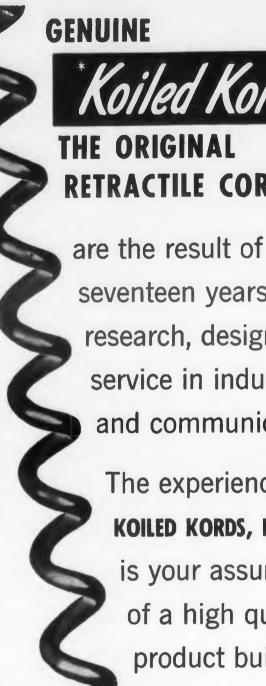
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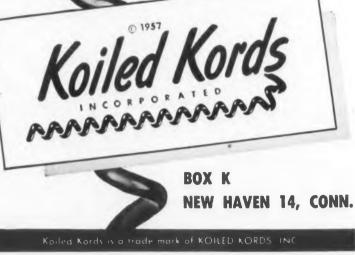


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Analysis of **Nuclear Radiation Effects** on **Transistors**

D. B. Kret

Defense Electronics Products Radio Corporation of America Camden, N. J.

URRENTLY available silicon transistors seem to stand up under radiation better than audio frequency germanium devices but not as well as high-frequency germanium devices.

For most polycrystalline materials, thermal neutron capture or transmutation is more important as a cause of damage than fast neutrons. However, in transistors, where regular single crystal structure is essential for the proper operation of the device, fast neutrons are the chief cause of damage.

Gamma rays must also be considered. Low energy gamma rays generally cause photoelectric effect to which most semiconductors are relatively sensitive. However, except under prolonged or intense low energy gamma radiation, generated photo emf's are of secondary importance and not a cause of permanent damage.

Another important consideration is Compton effect or Compton scatter-a process in which a

gamma ray is captured with a subsequent release of a high energy electron. Thus, although electrons themselves are not capable of penetrating the case used for a transistor, they may be generated inside of the transistor package itself.

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These particles are capable of causing crystal damage in the same manner as fast neutrons. All gamma ray with a certain minimum energy are capable of breaking chemical bonds in such a manner as to change the nature of the bombarded material. Silicone grease or oil may in this manner be vulcanized to rubber. Long chain type organic molecules decompose into smaller more stable compounds possibly with the evolution of Hydrogen gas. In transistors, this is very important, since at the surface of the crystal, various types of chemical bonds exist and various susceptible materials are used as fillers and capsulents.

The radiation effects on transistors can be recognized as primarily two discrete types, surface effects generally induced by gamma rays and damage to the crystal lattice primarily due to fast neutrons. Compton scatter electrons and thermal neutron capture may be regarded as second order sources of damage. The surface effects may be recognized by charges in surface recombination velocity, while bulk damage relates directly to decreases in minority carrier lifetime. The most sensitive design parameters relating these fundamental characteristics are:

beta(common emitter current gain) Ico (leakage and saturation current)

Typical gain curves are shown in Fig. 1 for transistors subjected to nuclear radiation. There are three modes of change. Curve A which indicates little change in gain hence, the most desirable characteristic occurred only on some of the highest frequency devices. This is due primarily to their much narrower base width as compared to lower frequency devices. Curve A on a somewhat different time base would take on the character of Curve C if the test had been continued for sufficient dura-

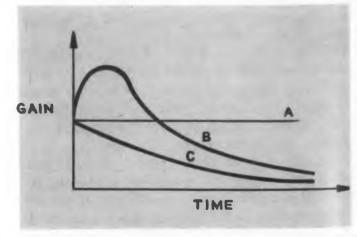


Fig. 1. Gain curves for transistors subjected to nuclear radiation. Curve A is that exhibited by most high-frequency transistors. Curve C is the usual curve for most transistors with a few following curve B as explained in the text.

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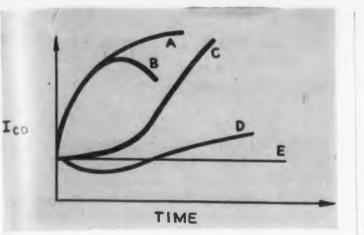


Fig. 2. Typical I_{co} vs Time curves for various transistors tested in presence of nuclear radiation. Most transistors followed curves A or C.

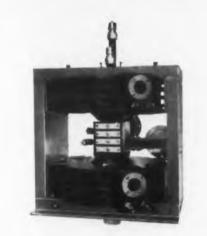
tion. While most transistors exhibit the predicted hyperbolic deterioration in gain as a function of time as depicted in Curve C, a fair number of them had the type of characteristic shown in Curve B. Most of these are p-n-p alloyed junction types in which the initial increases in gain are attributable to surface changes which tended to improve them by decreasing surface recombination velocity. The majority of units, however, show an initial deterioration of gain that might be expected due to bulk effects alone. Devices that initially have relatively low beta exhibit the same type of gain deterioration except that the percentage change is much less since they start so much lower down on the hyperbolic curves.

A composite of the variation I_{co} is shown in Fig. 2. Analysis is not as simple or straight forward as that for changes in gain. The initial I_{co} variations are primarily gamma induced surface changes while the long term increases are bulk induced, the former due to leakage current, the latter due to saturation current. Most transistors follow Curve A or C. Some of the units which exhibit the E characteristics had relatively high I_{co} initially. Units of a single type from one manufacturer produced in the same lot exhibited different types and amounts of L_o changes as a function of irradiation and time. This suggests an immediate expedient for obtaining reasonable radiation resistant devices for use in current equipment until more highly radiation resistant types are made by design. A simple screening process whereby all units required for an equipment design which would be exposed to a medium intensity gamma source for a relatively short period of time while the Ico changes are being monitored. All units exhibiting large Ico deterioration or instability would be eliminated and the balance could then be expected to be deteriorated as predicted by the bulk damage due to neutron flux only.

Most transistors recover or anneal to some extent after removal from radiation flux. Two distinct types



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The VA-804D (4.85—5.0 kMc) mounted in its focusing magnet, the VA-1504. A vital component of the new Canadian Westinghouse SHF scatter transmitter, now being operated in a "proving ground" circuit between Hamilton and Kinmount, Ontario, is the Varian VA-804 klystron amplifier, designed specifically for forward scatter communication service. The now familiar qualities of all Varian klystrons — remarkable efficiency (see below), economy, reliability, and proved performance — made this tube the logical choice for Westinghouse.

Electrical Characteristics:

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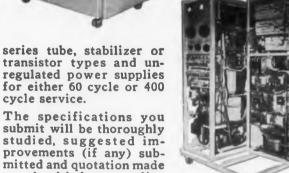
KLYSTRONS, TRAVELING WAVE TUBES, BACKWARD WAVE OSCILLATORS, LINEAR ACCELERATORS, MICROWAVE SYSTEM COMPONENTS, R. F. SPECTROMETERS, MAGNETS, MAGNETOMETERS, STALOS, POWER AMPLIFIERS, GRAPHIC RECORDERS, RESEARCH AND DEVELOPMENT SERVICES

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FORWARD DIODE **CHARACTERISTIC** PRE-I, IRRADIATION POST-IRRADIATION

Fig. 3. Diode characteristic-before and after being subjected to nuclear radiation.

of annealing are important, bulk and surface. Both of these processes are temperature and time dependent. While bulk annealing of germanium at 25 C is negligible, it becomes appreciable and increases rapidly above 100 C. Hence, devices might be rejuvenated by a high temperature baking process. Complete recovery could not be achieved at temperatures which would not destroy currently available germanium transistors due to the temperature limitations of other materials employed in fabrication. Although currently available silicon transistors have an upper limit of 200 C, it is now conceivable that they could be made in a manner that would permit baking at temperatures in excess of 500 C.

Surface recovery is not as clearly understood as bulk annealing. We believe it is so however, to predict that an exact repetition of the manufacturer's surface preparation technique could remove all traces of radiation effects from the surface. Radiation induced surface changes may cause either improvement or deterioration of device characteristics. Annealing reverses this process such that in some instances slight deterioration was noticed after removal of the units from the radiation environment, and in one exceptional instance the characteristics after annealing were markedly better than before the radiation test by a ratio of about six to one. This was however a very poor device

initially and was rejectable on the basis of manufacturers specifications. Generally, most commercially available devices can be expected to deteriorate due to surface changes during irradiation and recovered partially as a function of time and temperature after removal.

Effects Noted

In Fig. 3 is shown a diode characteristic before and after irradiation. The input impedance and saturation resistance of diodes, which have a linear relationship with common base and common emitter transistor circuits, should increase as a function of bulk deterioration. These changes will generally be relatively slight.

The output characteristics of a transistor are shown in Fig. 4 with the collector voltage plotted against the collector current and with the base current as the independent variable. The solid lines are pre-irradiation, and the dotted lines are pre-irradiation. The changes predicted on the basis of the forward diode characteristic are clearly apparent. In addition, from this it can be seen that the output impedance will generally decrease. The change being attributable to surface effects. In rare cases the converse might be true.

Maximum breakdown voltage should generally be decreased due to surface effects. Breakdown voltage which is generally a function of restivity will not be noticed before the device is virtually destroyed due to the deterioration of minority carrier lifetime except possibly for extremely narrow base width units.

Noise figure will increase as a function of surface deterioration. Discrete noise pulses due to incident particles and rays are insignificant except possibly in the presence of an intense cosmic shower. The probability of which is insignificantly small up to altitude in excess of 250 miles.

Improved silicon devices will show a greater sensitivity to nuclear radiation damage than equivalent germanium devices by a factor of two to five.



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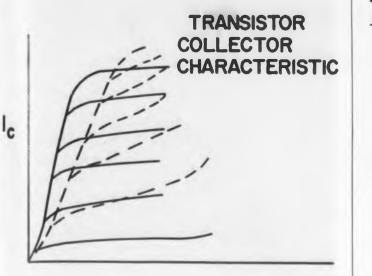
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Fig. 4. Transistor output characteristics curves—before (solid) and after (dotted) subjection to radiation fields.

Information is currently available for the initiation of development of devices specifically intended for use in radiation environments. Much work has yet to be done in this area, surface preparation and capsulating materials which can readily be analyzed and tested might be a fruitful area for work. More radiation resistant surfaces could be manufactured by design, but in the interim (by the screening technique suggested previously) highly resistant devices can be selected to be satisfactory for most requirements.

All the tests that have been conducted so far have been with very intense radiations such as are found in the heart of a reactor or under extremely intense gamma sources. The transistors tested were capable of lasting specific lengths of time. Some gave indications of little or no deterioration under very intense gamma flux; others under the most severe atomic pile conditions gave appearances of useful life in the order of hundreds of hours. Under these conditions, human beings could not be expected to survive after a fraction of one percent of this time. Due to their single crystalline structure, transistors are somewhat more sensitive to radiation damage than other conventional components, with a few exceptions.

This article is based on a talk given by Mr. Kret at the Electronics Components Symposium in Chicago, May 1-3, 1957.

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If you are a manufacturer of silicon devices or are planning to manufacture semiconductors, there is sufficient production capacity for Du Pont Hyperpure Silicon to meet anticipated requirements and assure you of an uninterrupted supply. Technical information on the growing of single crystals and the measurement of their properties is available to you. Get in touch with us about your silicon problems. We will be pleased to help you.



DU PONT HYPERPURE SILICON is available in three polycrystalline forms—needles, dense lumps and cut rods. At the Du Pont laboratories, a singlecrystal ingot, such as those shown at left, is grown from each lot of polycrystalline Hyperpure Silicon.

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Part of this characterization crystal is included with each shipment of a full lot of silicon. It may be used by the manufacturer as a seed to initiate the growth of single crystals and also as a resistivity reference to check the purity of single crystals grown from the lot.

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... THROUGH CHEMISTRY

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capacitors

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| | REPRESENTATIVE TYPES | PICAL | SIZ | E COMPARISONS |
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| | BOOLE Mylar dielectrie winding auto to | cap. | Volts | Diam. Lgth. |
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| | the resisting Epoxy. | .1 | 50 | .438 x 1-3/16 |
| | Contrast to the second s | .47 | 50 | .562 x 1-15/16 |
| | 663UW Mylar dielectric winding with tough plastic film | | | |
| | case and thermo-setting end seals. | .01 | 50 | |
| GODD-ALL | | .1 | 50 | .281 x 15/16 |
| DOD-ALL | | .47 | 50 | .437 x 1-15/16 |
| | 613C Mylar dielectric winding, extended foil construc- | | | |
| | tion, hermetically-sealed metal housing. | | | .173 x 23/32 |
| | tion, nermeticany-sealed metal housing. | -1 | 50 | .313 x 27/32 |
| | | .47 | 50 | .50 x 1-3/16 |
| RADIAL LEAD | SOORE This novel design combines features of conven- | | | |
| | tional tubular capacitors and upright mounting types. The | | | |
| GOOD-ALL | mylar dielectric winding is completely encapsulated in | .01 | 60 | 250 - 11 /10 |
| BUUD-ALL | Epoxy. In addition to its attractive glossy red appearance | .1 | | .250 x 11/16 .375 x 15/16 |
| | the Epoxy formulation developed by Good-All yields a tough, | .47 | 50 | .50 x 1-3/4 |
| | durable coating with excellent dielectric strength. | | | |
| RIGHT MOUNTING | | _ | _ | |
| NIGHT MOUNTING | BOOUPE Mylar dielectric winding molded in dense, mois- | .01 | | |
| | ture-resisting Epoxy. | .01 | 50 | .438 x 15/16 |
| | | .47 | 50 | .562 x 1-3/16 .688 x 1-15/16 |
| 600D-ALL | | | | |
| 8 | 620UPB Mylar dielectric winding with molded bakelite | .01 | 50 | .375 x 1 |
| 8 | housing and thermo-setting plastic end seal. | 1 | | .375 x 1-1/4 |
| F | | 47 | 50 | .625 x 1-7/8 |
| | 620PM Mylar dielectric winding encapsulated in a plas- | | | |
| | tic impregnated paper tube. | .01 | | .343 x 15/16 |
| | tio impregnated paper (une. | .1 | | .410 x 1 |
| | | .47 | 50 | .562 x 1-3/4 |
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Write or phone for consultation on specific design problems or to secure detailed specifications on the various capacitor types shown.



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Airborne El Telemetering C

SED FOR telemetering information in air-U craft and missiles, this electronic commutator can be expected to have a life of 5000 hours. Twenty-eight data channels are switched without recourse to moving parts. The unit, consisting of a transistorized pulse generator, a silicon diode switching matrix and a sequential counter, is contained in a package 3 in. diam x 5 in. long and weighs 2 lb.

The commutator, manufactured by Arnoux Corp., 11924 W. Washington Blvd., Los Angeles 66, Calif., is designed to operate at fixed speeds from 2-1/2 to 30 cps and to handle input signals over the range 0 to 5 v with a 25 K source impedance. One of the 28 input channels is used for frame synchronizing purposes. With an input signal between 0 and 5 v applied to this channel, the device produces a frame synchronizing pulse in the output equal in width to three on periods and two off periods. Output amplitudes are from 5 to 7 v with a 5 v input, constant to ± 5 per cent.

Electronic commutator containing parts, consists of a transistorized pulse generator, silicon diade switching matrix and sequentiat counter, is contained in a 47 cu in volume.

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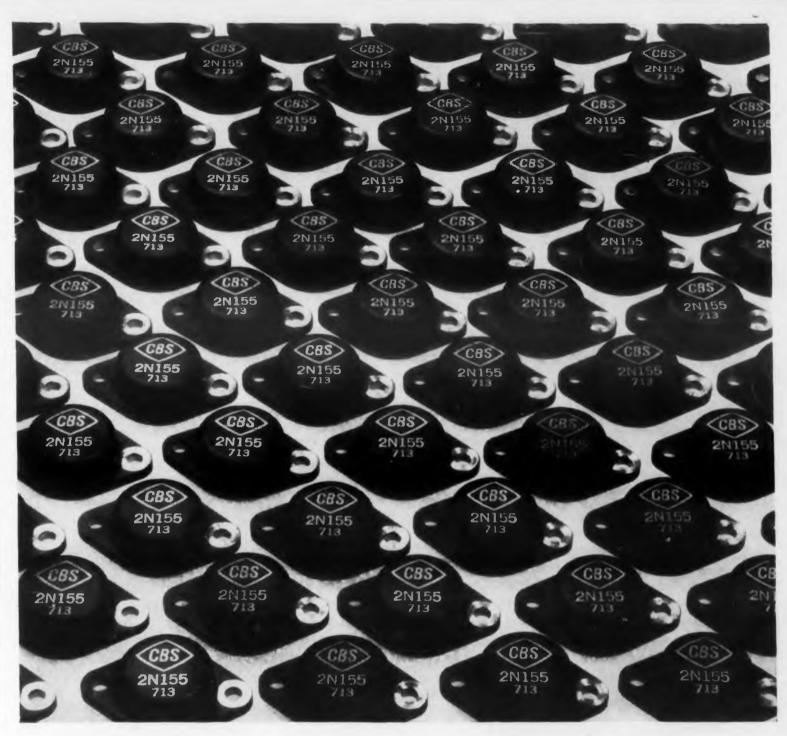
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The variation in output pulse level corresponding to inputs between 0 to 5 v is less than 10 per cent of the pulse width, while the peakto-peak noise level on the output pulse train is less than half a per cent of the full scale range. Cross-talk between channels is less than 0.25 per cent of the full scale range. With equal inputs to all channels-0 to 5 v-the variation in pulse levels between channels is again plus or minus half a per cent of the full scale range.

Designed to operate from $+150 \pm 5$ v dc, the unit requires 2 w. It will operate between -65and 185 F, sea level and 80 kilofeet.

The electronic commutator was developed to fulfill a need left by mechanical switches that wear relatively quickly when a common wiper makes contact with the data channel contacts at speeds from 150 to 1800 rpm.

For more information on this electronic commutator, turn to the Reader's Service Card and circle 33.



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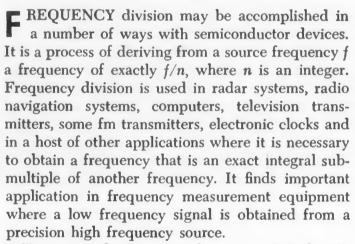
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ELECTRONIC DESIGN . July 15, 1957

Background for Designers_

Frequency Division with Semiconductor Devices

A William Carlson Transistor Applications, Inc. Boston, Mass.



Frequency division may be accomplished with semiconductor devices by use of:

- Blocking oscillators
- Multivibrators

• Devices showing negative resistance (double base diodes, point contact transistors, negative resistance diodes, avalanche transistors, combinations of junction transistors)

• Counter circuits (binary counters and ring counters)

Regenerative frequency dividers

• Circuits in which increments of charge are added to a capacitor which is then discharged at a given count (an integrating type of counter)

A junction transistor blocking oscillator is shown in Fig. 1a. This circuit is similar to one often used with vacuum tubes. The operation of the circuit may be explained by assuming that a negative pulse has just driven the base negative, causing the col-

34

lector to conduct and the voltage at the collector to swing positive. The transformer secondary in the base circuit inverts the voltage across the primary in the collector circuit and drives the base more negative causing the transistor to conduct more heavily. This action is regenerative and rapidly drives the transistor to full conduction. The duration of the pulse is a function of the size of the coupling capacitor in the base circuit and the mutual inductance of the transformer, among other things.

When the voltage across the capacitor begins to change, and when the voltage across the transformer starts to drop, the voltage at the base begins to decrease, causing a decrease in collector current. This initiates regenerative action in the other direction and the transistor is rapidly turned off. Because of the charge placed on capacitor C during the conduction interval the base is now biased positively and the transistor will remain in the cut-off condition until the capacitor discharges to zero or a pulse drives the base negative.

The base wave form is shown in Fig. 1b. The capacitor discharges with a time constant determined mainly by C and R_3 in series with the parallel combination of R_1 and R_2 . When the transistor is turned off, the impedance looking into the base is very high. If the transistor did not conduct when the base voltage became negative the capacitor would discharge to $-V_{cc} R_2/(R_1 + R_2)$.

Fig. 1b illustrates division by four. The negative pulses are too small to drive the base negative until

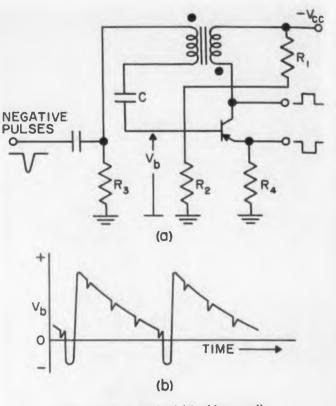


Fig. 1. a) A typical blocking oscillator b) Base voltage waveforms

base voltage has dropped to the point where the fourth pulse triggers the circuit. The free-running period of the circuit is longer than the triggered period. By placing R_4 in the emitter circuit a negative pulse is available to drive another similar dividing circuit. A positive pulse is available at the collector.

Blocking oscillator circuits take different forms. In Fig. 2a the RC circuit controlling the frequency is placed in the emitter circuit. A negative output is available from a transformer winding and a positive pulse is obtained at the collector. In Fig. 2b the transformer secondary and the RC circuit are in the emitter circuit, with a positive pulse available at the collector.

Multivibrators

A junction transistor multivibrator and the associated waveforms are shown in Fig. 3. The parameters R_{b1} , R_{b2} , and C_2 may be adjusted for the desired conduction periods. The circuit may be modified by returning R_{b1} and R_{b2} to voltages other than $-V_{cc}$. Every third pulse applied to the base of transistor 1 causes triggering in the example shown.

Negative Resistance Devices

Semiconductor devices capable of producing negative resistance characteristics include point contact transistors, double-base diodes, avalanche transistors and combinations of junctions transistors. A typical negative resistance curve is shown in Fig. 4a. If a load resistance R_L is used with a

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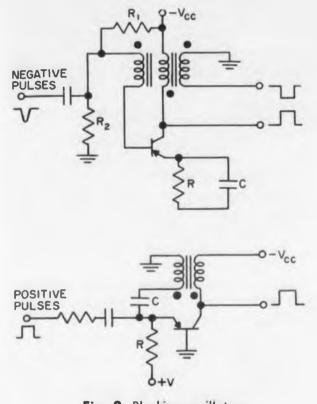


Fig. 2. Blocking oscillators using junction transistors

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voltage V_s to bias the device in the negative resistance region and a capacitor is placed across the input as shown in Fig. 4b, relaxation oscillations will result. The voltage appearing across the capacitor is shown in Fig. 4c where division by three is shown. The path of the operating point is shown by arrows in Fig. 4a. Operation of the circuit may be explained by assuming that the device is initially in the cut-off region. The capacitor charges towards V_s through R_L until the peak point V_p of the negative resistance curve is reached.

Upon reaching the peak point voltage, the operating point switches rapidly to the conduction region where the capacitor is quickly discharged to the valley point voltage V_v at which point the device is turned off and the cycle repeats. By superposing small timing pulses as indicated in Fig. 4b and 4c frequency division may be accomplished.

The negative resistance curve of Fig. 4a is typical of the V-I characteristics obtainable with the devices mentioned above except that the location of the curve in the V-I plane may differ. All the devices mentioned are three terminal devices with the exception of the negative resistance diode. The diode is not available on the market but a great deal of research is being carried on, as indicated at a recent conference on semiconductor devices where one-third of the papers presented were on the subject of negative resistance diodes.

The negative resistance diode is capable of very high frequency operation. Relaxation oscillators at

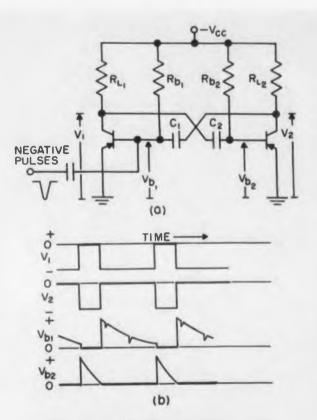


Fig. 3. A junction transistor multivibrator and the associated waveforms

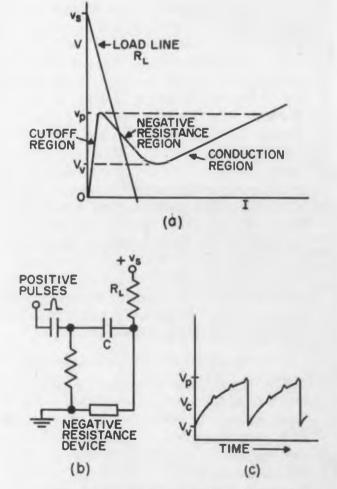


Fig. 4. a) A typical negative resistance curve b) A negative resistance frequency divider c) Voltage across the capacitor of Fig. 4b for division by three



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30 mc have been obtained. Fig. 4b gives a fair indication of the simplicity of a relaxation oscillator using a two-terminal negative resistance diode. For a three-terminal device, the block in Fig. 4b represents the two terminals across which negative resistance characteristics appear. In three-terminal devices, the third terminal may be used for a signal output.

Fig. 5 illustrates some other circuits having a negative resistance characteristic. The combination of a PNP and an NPN transistor as shown in Fig. 5d is equivalent to a point contact transistor except that the current gain is higher. The avalanche transistor is not shown but consists essentially of an ordinary junction transistor operated at higher than normal collector voltages where heavy conduction occurs due to avalanche multiplication at the collector. This "breakdown" current may be controlled by base current and the transistor may be used in circuits similar to those used with point contact transistors. The remarkable feature of the avalanche transistor is that a switching time of a fraction of a microsecond may be obtained with low frequency audio transistors.

Counters

Binary counters and ring counters may be used for frequency division. They differ from the frequency divider circuits previously mentioned in that they are not free-running and are not as sensitive to trigger pulse, supply voltage, or circuit parameter variations. They are, however, more

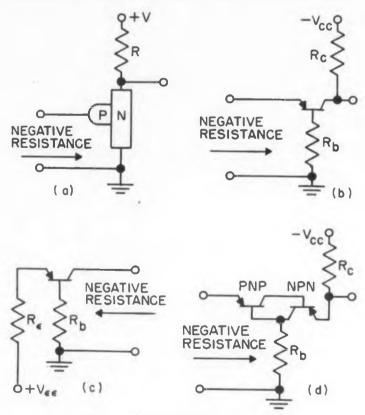
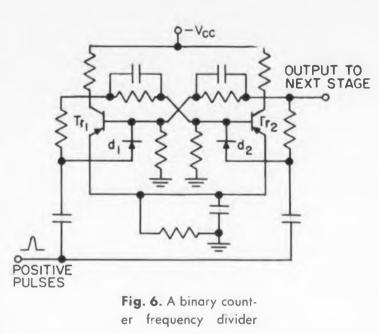


Fig. 5. Circuits having negative resistance characteristics a) Double base diode b) Point contact transistor c) Point contact transistor d) Combination of junction transistors



complicated than the free-running circuits. If the counter accepts n pulses before returning to its original state, it will produce an output pulse once for each n input pulses. The counter may be constructed with transistors of either the point contact or junction type and may be either a ring counter or a binary type made up of a number of binary flip-flops. Fig. 6 shows a typical binary counter stage using junction transistors.

Ring counters may be constructed to divide by any integer. Binary counters normally count in powers of two but may be used with feedback circuits to reset at the desired count and thus may also be used to divide by any integer. The binary counter of Fig. 6 operates as follows. If Tr_2 is 'on' a positive pulse applied to the flip-flop will pass through d_2 to the base of Tr_2 and turn it 'off' and at the same time turn Tr_1 'on', (diode d_1 is reversebiased by the negative collector voltage of Tr_1).

The next positive pulse will turn Tr_1 off and Tr_2 on producing a positive going voltage at the collector of Tr_2 which may be applied to another binary stage for further division. Thus every other input pulse applied to the flip-flop returns it to the same state. In a ring counter an 'on' condition is transferred from one stage to the next at each input pulse with the frequency division determined by the number of stages in the counters.

Regenerative Frequency Dividers

The regenerative frequency divider shown in Fig. 7 is similar to the counter types in that it is not free-running, but differs in that it is essentially a sine wave circuit. Fig. 7a shows a block diagram of the regenerative frequency divider. To understand the operation of the circuit, assume the system is in operation with an input frequency f and an output frequency f/n. A signal of frequency f/n is applied to a harmonic generator tuned to the (n-1)th harmonic of the f/n signal and thus has an output frequency of (n-1)f/n which is applied to the mixer.

The mixer output circuit is tuned to the difference frequency of the two signals coming into the mixer, f and (n-1)f/n, this difference frequency being the desired output frequency, f/n. Fig. 7b illustrates how the circuit might be realized with junction transistors.

Integrators

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Fig. 8a shows a counter in which an increment of charge is added to a capacitor each time a pulse is applied to the circuit. After a desired number of pulses the negative resistance circuit discharges the capacitor. In explaining the operation of the circuit it will be assumed that the negative resistance device has a V-I characteristic similar to that in Fig. 4a. The transistor is normally 'off' and a negative pulse is assumed to drive the transistor fully 'on' so that the collector goes nearly to ground potential during the pulse. C_1 is much smaller than C_2 . Assume that the negative resistance device has just discharged C_2 at time t_0 . C_1 is charged to a voltage of nearly $-V_{cc}$ (the voltage at the collector when cut off). When a short negative pulse arrives it drives the transistor to full conduction, the collector approaches ground potential, and C_1 transfers most of its charge to C_2 through diode D_2 causing a positive step of voltage to appear across C_z as shown in Fig. 8b. After the trigger pulse disappears, C_1 charges again to $-V_{ec}$ through R_L and diode D_I . The next trigger pulse to arrive results in another transfer of charge from C_1 to C_2 and another jump in voltage across C_2 . The process continues until the

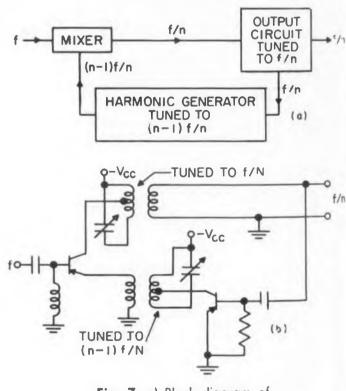
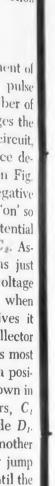


Fig. 7. a) Block diagram of a regenerative frequency divider b) Circuit of a regenerative frequency divider erence Diixer ng the strates nction



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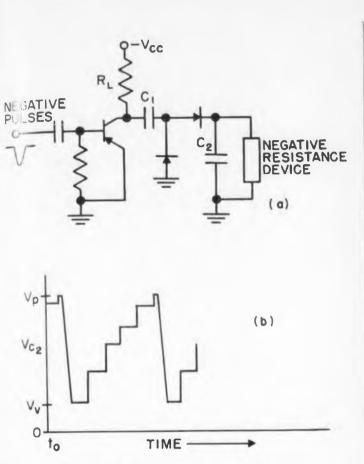


Fig. 8. a) An integrating type of frequency divider b) Associated waveform

voltage across C_2 reaches the peak point of the negative resistance device causing it to fire, at which time the cycle of events repeats. It is assumed that the back resistance of the diodes and the cut-off resistance of the negative resistance device is high enough so that C_2 does not discharge appreciably between trigger pulses. The negative going waveform appearing when C_2 is discharged could be used to operate another similar counter circuit. Fig. 8b shows frequency division by five.

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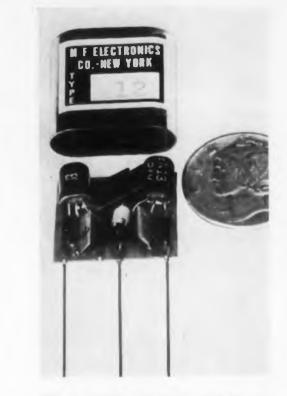
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Fig. 1. Stable 400 cycle multivibrator

OCCUPYING less than one fifth of a cubic inch, these minute transistorized circuit assemblies provide remarkable performance for their size. They operate within specifications from -25 to +50 deg C, and may be stored safely from -40 to +70 C. The units are particularly suitable for use in missiles, portable equipment, telemetering, balloons, and other ap-

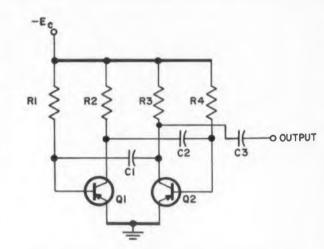


Fig. 2. Schematic of tiny 400 cycle multivibrator

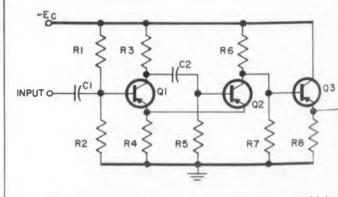


Fig. 3. Schematic of one-shot multivibrator which occupies less than one-fifth of a cubic inch

ELECTRONIC DESIGN • July 15, 1957

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An accessory that consists of coupler and an adapter has been recently perfected by Cannon to provide quick connect and quick disconnect characteristics The adapter is designed to screw over the coupling threads of a standard AN receptacle, and contains an **Ouick-Disconnect** external locking groove which receives the formed ends of the coupler latch when fully engaged. The entry of the coupler latch into this groove permits a compression spring to move the coupler sleeve forward, locking the parts securely. A simple straight pull back on the sleeve releases the latch **Accessories for AN-Plugs** and permits disconnection. The coupler consists of a special spring latch assembly, and is designed to replace the coupling nuts on Cannon AN3106A and AN3106B plugs. CA06BQ Plug **CA02AQ** Receptacle

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CIRCLE 42 ON READER-SERVICE CARD FOR MORE INFORMATION

Tiny Transistor Assemblies

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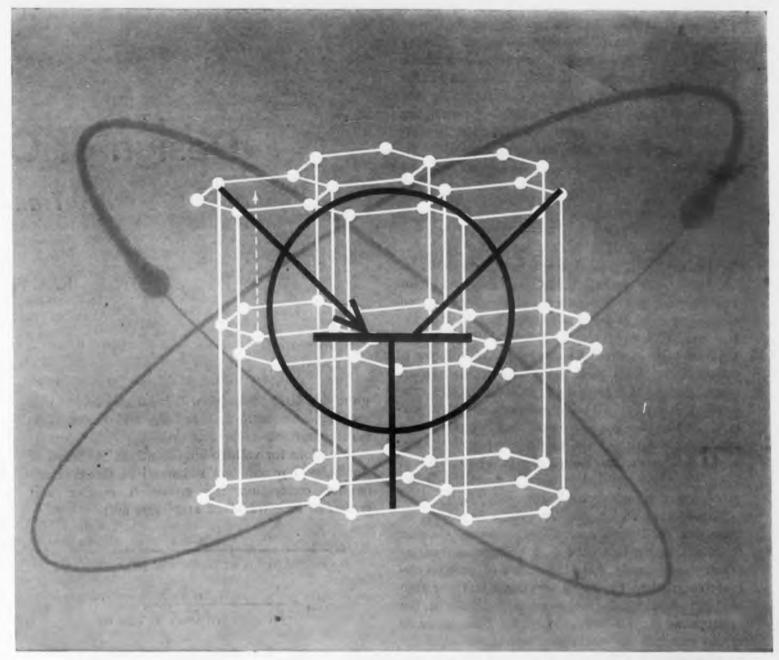
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plications where reliability is of prime importance. Circuit configurations currently available are a two-stage audio amplifier, three db down at 40 cps and 60 kc with a minimum voltage gain of 30 db; a 400 cycle multivibrator; a one-shot multi; a flip-flop which can be triggered at rates up to 20 kc; and a bootstrap sawtooth generator. These minuscule assemblies are designed and manufactured with emphasis on reliability. The manufacturer, M F Electronics Co., 122 E. 25th St., New York 10, N.Y., includes testing as one of a major series of operations in their fabrication. The units are subjected to exhaustive tests, first at the mock-up stage, again prior to potting, then once again after the units have been potted and set for several days. In addition temperature runs are made on representative units to insure that the specified temperature requirements are met. The 400-cycle multi, which may be used, typi-

cally, to drive a gate, act as a pulse source, or drive a counter, is shown in Fig. 1, and its schematic in Fig. 2. Critical components RI, R4, C1, and C2 are chosen to be the most stable components available. 5 v peak to peak are available, using a 6 vdc supply providing 3 ma. Even more impressive from the viewpoint of space economy is the three-transistor one-shot multi whose schematic is shown in Fig. 3.

These Lilliputian circuits are encapsulated with epoxy resin in drawn nickel silver cases, offering complete protection from humidity—even operation under water. The container measures 0.75 in. h. x 0.717 in. w. x 0.312 in. t., and the complete assembly weighs less than one-third of an ounce. For more information about these tiny circuits, turn to the Reader's Service Card and circle 28.



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CIRCLE 34 ON READER-SERVICE CARD FOR MORE INFORMATION

Editors Note: Use of conductance curves¹ for designing electronic circuits has been the subject of many articles by Mr. Pullen. In this article he points out some interesting conduction ratios which can be used in the design of oscillators. Part I, which appeared in the July 1 issue, discussed the design of vacuum tube oscillators using conductance values. Part II extends these techniques to a variety of transistor oscillators.

TRANSISTORS are excellent active elements for low-power oscillators. High stability and almost unbelievable economy can be attained when transistors are used in design of oscillators. In Part I of this article, the principals involved in design of vacuum tube oscillators were analyzed in terms of practical problems of design. Conductance values were used in the analysis to coordinate the tube (active element) with other components in the circuit. Design techniques were considered from a small signal point of view with emphasis on sinusoidal oscillators. The techniques developed in Part I will now be extended to include practical design problems of transistor oscillators.

The factors which are important in design of transistor oscillators are: (1) the active element functions best when used in a voltage control, or conductance mode. (2) Impedance of passive circuits coupled to the input terminals of the active element should satisfy the relation gZ < 1 at the appropriate port or terminal pair. (g is conductance of the active device, and Z source impedance of the passive circuit). (3) Loading of the feedback network should have a negligible effect on the output voltage of the active device. (4) Loop amplification should exceed unity for proper starting. (5) When good frequency stability is necessary, circuit feedback must be sufficiently small to prevent amplitude limiting as a result of clamping.

Each of these requirements are elaborated upon in the discussion which follows.

Operating Conditions

The first step in the practical design of transistor oscillators is establishment of operating conditions which will provide amplitude limiting. The high degree of current gain constancy in transistors prohibits the use of constant current conditions—starting is too hard to obtain in sinusoidal oscillator circuits. Amplitude control is readily obtained when the transistor is used in a conductance mode of operation (constant input voltage). Thermal stability requires that either base or emitter current be held approximately constant. Base current is held constant when a common emitter connection is used. Emitter current is held constant with a

Design of Oscillators-II

Transistor

K. A. Pullen, Jr. Ballistic Research Laboratories Aberdeen Proving Ground, Md.

grounded base connection. It is for this reason that starting base current is call I_{bo} and the starting emitter current I_{eo} in this article.

Equations for voltage amplifications^{*} in terms of small-signal parameters measured at the common emitter connection for grounded emitter and grounded base transistor amplifiers are:

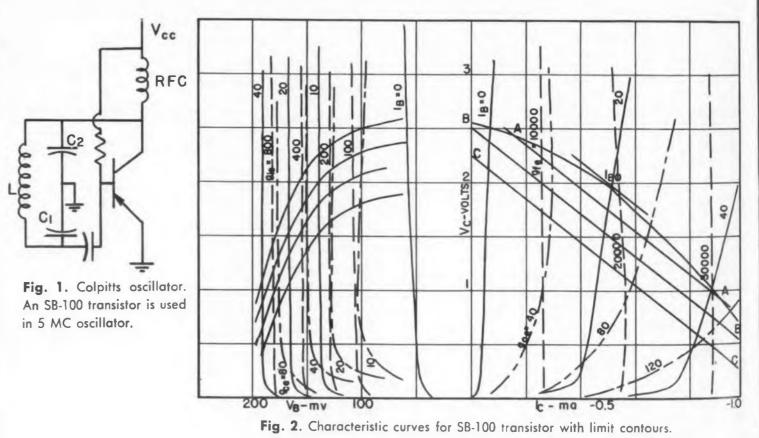
$$K_{ve} = \frac{-g_{fe} R_L}{1 + g_{ie} (R_i + r_b') + g_{oe} R_L + g_{ie} g_{ce} (R_i + r_b') R_L} (1)$$

$$K_{vb} = \frac{g_{ie} + g_{fe}}{1 + (g_{ie} + g_{fe}) (R_i + r_b) + g_{oe} R_L}$$
(2)

Two conclusions can be drawn from these equations: the first is that if R_i (or r_b') is sufficiently large, variations of K_v are difficult to obtain since R_L and R_i are constants; the second is that available values of amplification are relatively small.

Input admittance of a transistor is rather large compared to that for a tube. The reason is evident when the significance of g_{ie} is considered. The design technique used to compensate for capacitive charging current in the input circuit of a tube is to arrange the input circuit to provide the required

*Notations used in the equations are described in the transistor data chart.



charging current without upsetting impedance relations. The same technique may be used with transistors.

Input conductance of a grounded emitter transistor is approximately equal to g_{ie} , and for a grounded base transistor it is approximately $(g_{ie} + g_{fe})$. Complete equations for input admittances of common emitter and degenerative emitter amplifiers are:

$$g_{in} = \frac{g_{ie} (1 + g_{ce} R_L)}{1 + g_{ie} (R_i + r_b') + g_{oe} R_L + g_{ie} g_{ce} (R_i + r_b') R_L}$$
(3)
$$g_{id} = \frac{g_{ie} [1 + g_{ce} (R_e + R_L)]}{1 + g_{ie} (R_i + r_b + R_e) + (g_{fe} + g_{oe}) R_e + g_{oe} R_L + g_{ie} g_{ce}}{[(R_i + r_b) + (R_e + R_L) + R_e R_L]}$$
(4)

Equation 4 is of particular importance in the design of phase-shift oscillators. Without emitter degeneration input admittance can not be made sufficiently small to function with the phase-shift network.

Colpitts Oscillator

Design procedures discussed in the first part of this article^{••} will now be applied to a transistorized Colpitt's oscillator (Fig. 1). The following relations apply in a well-designed oscillator. For the output circuit:

$$g_{oe} Z_L < 1$$

and the input circuit:

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$$g_{ie} R_i = g_{ie} (C_2 / C_1) \, {}^2 Z_L < 1 \tag{6}$$

**Design of Oscillators-I, Electronic Design pp. 52 to 55 July 1, 1957

Feedback gain is:

$$\mathbf{k}_f = C_2/C_1$$

and the loop gain is approximately:

 $K_L = K K_f = g_{fr} Z_L (C_2/C_1 \ge 1$ (8) For oscillation to start, the terms in (8) should be selected so that the product is equal to at least 1.5.

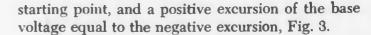
(7)

A 5 mc transistor Colpitts oscillator will be designed to illustrate equations 5 through 8. The transistor selected is an SB-100 (Fig. 2). A trial collector supply voltage of -2v with a collector current of 0.5 ma is used as starting point for design. Since g_{ic} has a value of 550 micromhos, $(C_2/C_1)^2 Z_L$ must have a value of about 1,000 to satisfy eq. 11. Taking $C_z/C_t = 0.1$, gives value of Z_L in the neighborhood of 2500 ohms. Since the value of g_{le} at the starting point is 0.018 mhos, a value of 0.05 for C_2/C_1 and 2000 ohms for Z_L gives a K K_l of 1.8. The approximate impedance of the circuit which supplies the base is $(0.05)^2 \times 2000$, or five ohms. A typical value for g_{oe} is 60 micromhos. Substituting in eq. 5 gives $g_{oe} Z_L = 0.12$, indicating that the effect of collector loading can also be neglected.

Assuming a Q of 100 for the overall tuned circuit, the reactance of the collector circuit is 20 ohms, giving a capacitance C_2 of 1600 µµfd, and $C_1 =$ 3200 µµfd. The required inductance L is 0.67 microhenries.

The next step is to plot limit contours on the transistor characteristic curves, Fig. 2, and locate the amplification limit conditions. Operating limits along any load line are determined by finding the set of points which will simultaneously give the same average base current as that chosen at the

phase of the feedback.



Two points are taken along the load contour drawn on the base family. The points represent equal changes of base voltage, one positive, ΔV_{bp} , and the other negative ΔV_{bn} .

$$\Delta V_{bp} + \Delta V_{bn} = 0$$

The base current is averaged by the equation:

$$I_{ba} = (I_{bp} + 2I_{bs} + I_{bn}) / 4 \tag{9}$$

where I_{bp} is the most positive base current, I_{bs} the base current at the intersection of the static and dynamic load lines, and I_{bn} the most negative base current. This equation is valid as long as the sum of I_{bp} and I_{bn} is approximately twice I_{bs} . If this condition does not exist, a more complex method of averaging is required. The current I_{bs} has a smaller magnitude than I_{bo} , the starting base current. Either I_{bp} or I_{bn} must be very large, otherwise the average will not limit to a value of I_{ba} equal to I_{bo} . Trial changes in base voltage amplitude are increased until the proper value of I_{ba} is obtained. The resulting points represent the positive and negative limits along the individual load contour. The calculation may be repeated along each load line.

When the limit contours have been located and plotted, loop amplifications at the static point and at the limit points can be calculated for each of the load contours. The average amplification, assuming that no sharp breaks in the plot of K as a function of e_b are encountered, is given by the equation:

$$K_a = (K_p + 2 K_s + K_n)/4 \tag{10}$$

and the loop gain by

$$K_a K_f = K_L \tag{11}$$

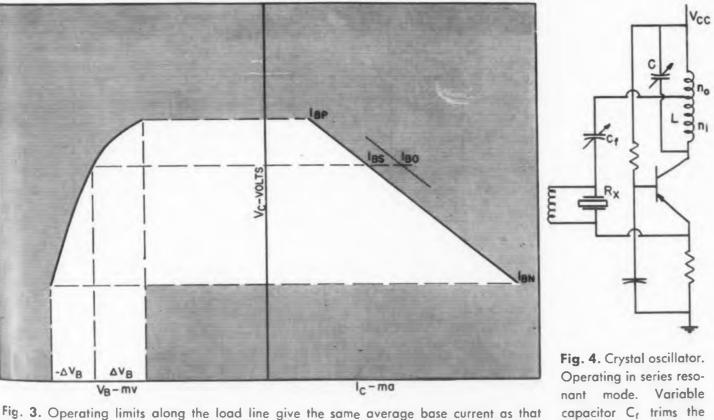
As always with oscillators, the load contour giving a value of unity for K_L is the one which represents the limit cycle.

The limit contours shown in Fig. 2 show that the operating point has not been properly selected (or the wrong load impedance has been selected), causing the transistor to cut off for part of the cycle. The average amplification for the load line at which the minimum base current reaches zero is 1.4, indicating that eq. 10 does not give accurate results. Linear operation can be obtained by changing the value of K_l from 0.05 to 0.033 or changing both K_l and Z_L to provide better characteristics.

Crystal Oscillator

An excellent crystal-controlled oscillator can be constructed using the SB-100 transistor. The circuit is shown in Fig. 4. The crystal is used in the series resonant mode and has the variable capacitor C_{f} in series with it to trim the phase of the feedback. A coil in parallel with the crystal is used to tune out the shunt capacitance of the crystal and its holder.

When a transistor is used as a grounded base



(5)

Fig. 3. Operating limits along the load line give the same average base current as that chosen at the starting point and equal positive and negative excursions of the base voltage.

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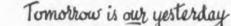
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oscillator, an impedance stepdown (current stepup) is required to provide the current gain needed to make the necessary emitter signal current available. The very low input impedance of the emitter also makes a voltage step-down necessary. Maximum turns ratio in the inductance L is given by:

$$n_i/n_o = g_{fe} Z_L / [1 + (g_{ie} + g_{fe}) R_x]^2$$
 (12)

where R_x is the series resistance of the crystal, n_i is the total number of turns in L, and n_o the number of turns from the collector supply to the feedback tap. A ratio value about half the maximum given by eq. 12 should be used to assure effective starting with average transistors. For a crystal having a series mode resistance of 100 ohms, a typical value for the complete denominator would be between ten and twenty, since $(g_{ie} + g_{le})$ has a value between 0.02 and 0.03 mhos. The maximum value of the ratio n_i/n_o is between two and twenty, depending on the crystal used.

Current limiting in a grounded base oscillator is obtained in a manner similar to the method described for a Colpitts oscillator except that limiting is on the emitter current instead of the base cur-

Fig. 5. Magnetic coupled

rent. Exactly the same technique is used to average the emitter current, which is the sum of the base and the collector currents. The limit points are points having equal changes of base to emitter voltage with reference to the static voltage. (If the crystal impedance is very high, the emitter current changes will be equal rather than the voltages).

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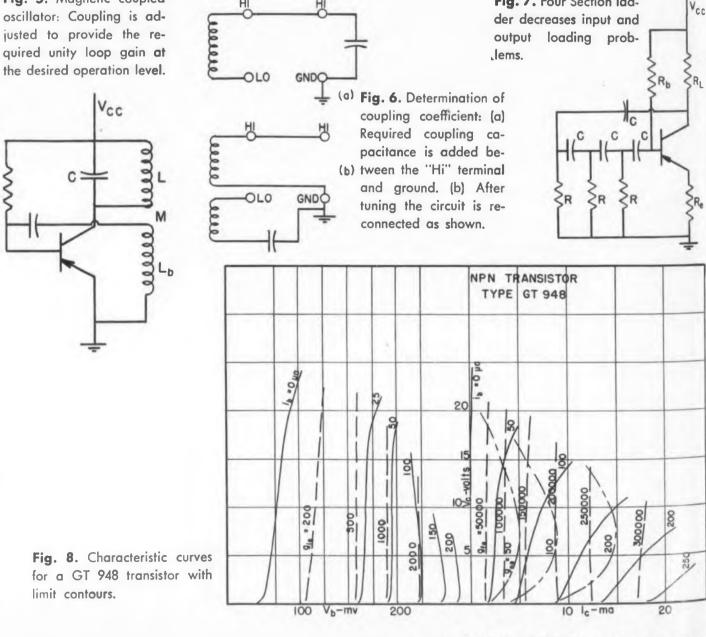
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An oscillator can be built around the static conditions used for the Colpitts oscillator just discussed. With $Z_L = 2000$ ohms, and resistance of the crystal. 50 ohms, the feedback ratio should be approximately four. Use of a coil with several taps is desirable. since measurement of the series resonant resistance of the crytal is quite difficult with ordinary equipment.

Magnetic Coupled Oscillators

Transistorized oscillators using magnetic coupling in the feedback path are constructed with the tuned circuit in the collector rather than in the base circuit. Otherwise oscillator starting and frequency stability will be difficult to obtain. Impedance of the base coil, L_b in Fig. 5, is adjusted so that $g_{ie} X_b < 1$. where X_b is the reactance of the base coil L_b . Cou-

Fig. 7. Four Section lad-



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pling is adjusted to provide the required unity loop gala at the desired operation level.

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The main design advantage of a magnetic coupled oscillator is the additional degree of freedom—the coupling factor. The reactance in the base circuit is first adjusted to be small compared to the input conductance. Inductance of the base coil should also be low enough so that $\omega^* L_b C_b < 0.2$, where ω is the angular frequency at which the oscillator operates, L_b is the inductance, and C_b is the capacitance of the base circuit, including, if necessary, the effective capacitance from base to collector.

The impedance level of the tuned circuit serving as the collector load impedance should be sufficiently small to permit stable operation. A practical value is 2000 ohms. The equation for this relation is written:

$$Z_L = Q X_c = 2000 \text{ ohms} \tag{13}$$

where X_c is the reactance of the capacitor C, and Q is the overall Q of the collector circuit.

Coupling Adjustment

Experimental adjustment of the coupling can be accomplished with a Q meter. First the collector inductance L is connected to the Q meter, Fig. 6a, and the required capacitance obtained by adding fixed mica capacitors between the "HI" terminal and ground to tune the circuit to the proper frequency. (At one megacycle a C of about 5600 µµfd is required). The Q of the combination is read, and the circuit reconnected as shown in Fig. 6b. The position of the coil L_b is adjusted until the new reading on the Q scale satisfies the relation:

$$K_f = Q_b/Q_c \tag{14}$$

where Q_b is the reading with L_b connected to the "HI" terminal (Fig. 6b), and Q_c the reading when the tuned circuit L-C is connected to the "HI" terminal, (Fig. 6a). If, after the adjustment is made, the transistor gain satisfies the relation

$$K_a = g_{fe} Z_L > 1/K_f \tag{15}$$

oscillation will result. (At very high frequencies g_{fe} may be reduced below the dc value, with the result that near cutoff frequency K_f may have to be larger than calculated).

Transistor R-C Oscillators

Transistor R-C oscillators are more difficult to design than their vacuum tube equivalents because of the relatively high values of g_{ie} characteristics of transistors. As a consequence, a design which may appear to be excellent on paper may not function properly even when loop gain and phase appear to be correct. A circuit, such as shown in Fig. 7, requires considerable emitter degeneration to function as an oscillator. Without the four-section ladder, input and output loading become difficult to design problems.

Collector load impedance should not be greater than 1500 ohms with a GT-948 transistor operating at point A, Fig. 8. Since forward conductance of the transistor is 0.075 mhos at point A, the maximum permissible value of R_e is 82 ohms. Amplification is therefore about 15. Emitter resistance also increases the input impedance of the transistor through emitter degeneration.

The approximate input conductance for a degenerative transistor amplifier $(g_{ie} \text{ and } g_{fe} >> g_{oe}$ and $g_{ce})$ is:

$$g_{id} = \frac{g_{ie} \left(1 + g_{ce} \left(R_e + R_L\right)\right)}{1 + \left(g_{ie} + g_{fe}\right) R_e + g_{oe} R_L}$$
(16)

Since the forward amplification is

$$K = \frac{-g_{fe} R_L}{[1 + (g_{ie} + g_{fe}) R_e + g_{oe} R_L]}$$
(17)

the loop amplification, assuming proper termination on the ladder is:

$$K_{L} = \frac{g_{fe} R_{L}}{13 \left[1 + (g_{ie} + g_{fe}) R_{e} + g_{oe} R_{L}\right]}$$
(18)

As a result, the effective value of g_{te} is reduced by 13 by the feedback net, lowering correspondingly the permitted value of g_{ie} ; A correspondingly larger value of beta is required in a transistor for a phaseshift oscillator.

The ladder network must simultaneously have negligible effect on the load impedance in the collector circuit, and an output impedance which is at most equal to the input impedance of the transistor. If input conductance of the transistor is used as the output shunt element of the ladder, the input resistance of network reduces the load impedance just enough to give a marginal operation with transistors having betas less than 100.

Design of oscillators using transistors is slightly more complicated than with vacuum tubes. For low power requirements the excellent results obtained are easily worth the effort. As was pointed out in the opening paragraph, transistors are highly stable elements and offer considerable savings in equipment cost.

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Design of Oscillators-Part I, K. A. Pullen, Jr. Electronic Design, July 1, 1957, pp. 52-55; Designing Cathode-Coupled Amplifiers with Conductance Curves, K. A. Pullen, Jr., Electronic Design, Jan. 15, 1956, pp 24-27; Designing Cascode Amplifiers with g-Curves, K. A. Pullen, Jr., Electronic Design, May 1, 1956, pp 26-27; Transistor Contour Curves, K. A. Pullen, Jr., Electronic Design July 1, 1956, pp 40-43; Design Techniques Using Conductance Curves, Pentode Degenerative Amplifier and Cathode Follower, K. A. Pullen, Jr., Electronic Design, Oct. 1, 1956, pp 32-35; Oscillator Design Techniques Using Conductance Curves, K. A. Pullen, Jr., Electronic Design, May 15, 1957, pp 34-37.



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Analog-to-Digital and Digital-to-Analog Converter

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The Multiverter, developed by Packard-Bell Computer Corp., Los Angeles, Calif., is the first commercially available high speed converter to be fully transistorized. The principles involved in design permits the construction of digital-to-analog converters which are about the size of a pack of cigarettes. At the electronic speeds with which the Multiverter operates-over 15,000 analog-todigital conversions per sec and 300,000 digital-toanalog conversions per sec-the 0.01 per cent ac-

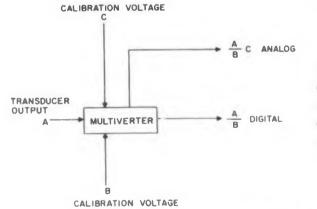


Fig. 1. Multiverter used for reading transducers. Calibration voltages B and C may represent temperature, barometric pressure or any other correction that must be applied to transducer output.

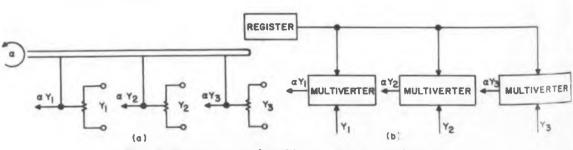


Fig. 2. Employment of Multiverter in a control system.

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all he otl curacy of the rack-mounted version is better than any previous converter. Greater accuracy has been obtained before, but only with relays or other electro-mechanical devices.

When used to convert a number n to a voltage, the product nx is formed simply by supplying the variable voltage x. When used to convert a voltage a to a digital number, the quotient a/v in digital form is effected by supplying the unit with a second voltage v. Multiverters are also available which will form aw/v as a voltage where wis a third variable voltage input.

The importance of being able to perform multiplication and division in the process of conversion can be gauged by considering Fig. 1 & 9

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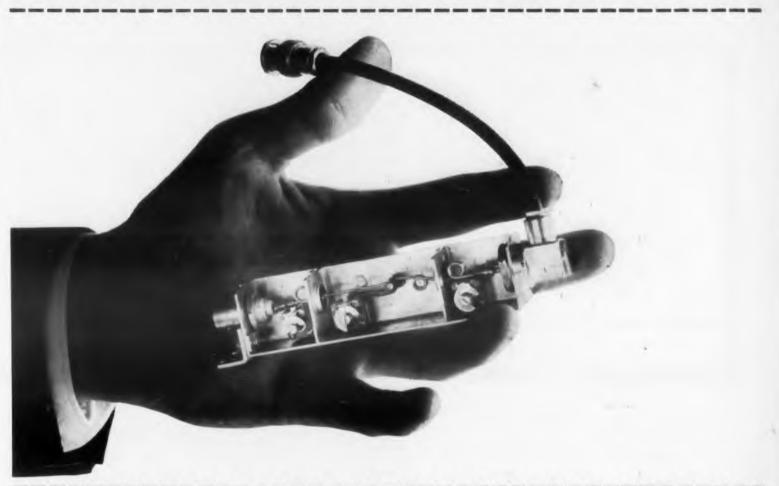
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Fig. 1 is a configuration that occurs in the reading of transducers. B and C are calibration voltages. They may represent temperature, barometric pressure or any other correction that must be applied to the transducer output. An analogous situation—not shown—arises in employing an analog plotter for plotting digital information. The converter in this case can introduce scale changes and other corrections during the process of conversion.

Fig. 2 illustrates the employment of the Multiverter in a control system. Common practice in an analog control system is to produce some of the outputs as shaft rotations and to couple to each shaft several potentiometers to effect a series of multiplications Fig. 2 (a).

Often a digital computer is used to replace a portion of the control system. When multiplication is to be performed digitally and the result take the form of a control voltage, two conversions are necessary. A single conversion and an analog multiplier are required when the multiplication is performed analogwise. In addition to eliminating the difficulties involved in conversion and multiplication, the Multiverter permits a digital output and an analog voltage to be multiplied directly Fig. 2 (b).

Accuracy requirements of most computing systems vary inversely with the frequency content of the data. This is because the contribution of higher frequencies to the over-all operation is proportionally small in most physical systems. Since speed and accuracy can be interchanged in the Multiverter, it will adjust to varying speed and accuracy requirements. This is particularly important in incremental conversion. Speed can be increased by a factor of several hundred in those portions of a solution where only low accuracies are needed. Because the adjustment of accuracy to frequency can be automatic, it is possible to use a single converter for both high and low frequency regions without manual intervention. For further information on this converter, turn to the Reader's Service Card and circle 38.



New Rev low pass filter squeezes max. performance into min. space

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R/C low pass filters owe their small size to a unique capacitor, the Series 75 air dielectric trimmer recently introduced by Radio Condenser. Perhaps the smallest air trimmers ever made in the U.S., they're finding wide application wherever space is a problem. Outstanding insulation resistance, "Q", and thermal stability make miniaturization a much easier job, on filters, i-f transformers, printed wiring boards, and conventional chassis of every description.

Originally designed for defense effort use, this filter is now in quantity production at R/C... and modifications are available to meet special performance requirements as they arise.

Additional information on R/C low pass r-f filters is provided in Engineering Bulletin FL-462. Trimmers are covered in Bulletin TR-123. Both are available on request to Radio Condenser Company.



0 20 8 40 60 80 300 400 500 600 700 800 900 1000 200 FREQ-MC

Electrical Specifications

| max. insertion loss, 200-400 mc | 5 db |
|-------------------------------------|---------------|
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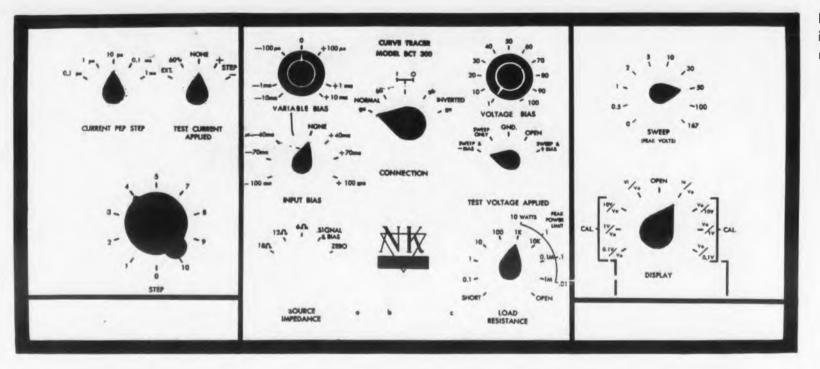


Fig. 1. A transistor analyzer showing the controls for biasings, etc. not found on a simple curve tracer.

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Norman B. Saunders Circuit Engineering Consultant Weston, Mass.

Using A Curve Tracer for Transistor Circuit Design

A TRANSISTOR curve tracer supplies stepped input current and swept output voltage to the device under test. It uses an oscilloscope face to compare families of curves with a calibration grid. It is superior to other methods of measurement in that it checks transistors over the full range of their characteristics giving more data, more accurately, faster, and with less chance of damage to the transistor if the tracer is properly designed and used.

Good circuit design requires that biases applied to the transistor be no larger than necessary to handle the expected signals with adequate margins. But at small biases gain goes down, feedback goes up, and distortion is introduced. The biases to give a reasonable compromise are determined on the collector family plot of the curve tracer. The relations are expressed quantitatively. The collector family curves are also used in determining cutoff current variation with voltage and the constant and temperature dependent portions of this current. The exponential relation between junction voltage and current simplifies some of the measurements and makes others almost unnecessary. The small signal coefficients are read on the displayed curves by slopes or intercepts. Translation of the display facilitates this.

A transistor analyzer is a curve tracer with input and output biases also supplied. The controllable biases allow interpolation between the steps and sweeps and permit direct reading of the small signal coefficients as on a meter. At frequencies high enough for reactive effects to be significant, the alternating current measurement is necessary for accuracy. The biases from the analyzer are also used to power a breadboard of the stage as designed for check of the design.

The data taken with the curve tracer is adapted to design by the method of successive approximations. In general, as the coefficients become difficult to measure they become unimportant in practical application. The complete consideration of the effect or reverse (feedback) voltage ratio is too extensive to be treated in this paper.

The manufacturer's published data on transistors has a limited number of coefficients given, usually at one bias or other parameter value. The range of the individual coefficients is seldom given. A transistor analyzer is generally the best instrument to supply the additional data necessary to design the individual transistor stage. A tracer having a full calibration grid is more accurate than the inexpensive transistor tester, and faster in a survey of the operating area than a precision small signal tester.

Setting Up the Curve Tracer

The full face of the oscilloscope should be checked for linearity and calibration by using the internal calibration circuits of the tracer. Check of just two axii across the face of the oscilloscope is inadequate to show up some of the weird types of deflection found too often even in the best of oscilloscopes. The cathode ray tube acts as an interpolating surface and a transfer device between the transistor curves displayed and the calibration grid. The scopeface calibration need only be made once a day and takes only a few seconds. The check of the origin (no deflection voltage in either direction) should be made every few minutes because most all oscilloscope amplifiers show appreciable zero drift.

The tracer should be set to limit the power into the transistor that is to be tested to its rated or other safe value. This protects the transistor having unexpectedly high leakage current or current gain, and also that incapable of withstanding normal voltages. If the tracer is capable of supplying the large power needed to test some transistors, only the operator can be sure it is set so as to protect those with lesser capabilities.

The Small Signal RC Coupled Stage

It is possible to operate a transistor just at the bias values at which the manufacturer choses to give its characteristics, but for small signal work this is seldom advisable. Power generally needs to be conserved to lengthen the life of the battery supply. Even with unlimited power available, limiting the power into the stage to the amount required is good design procedure. It limits the heating within the transistor, and increases the range of temperatures over which the circuit will operate, the stability of the circuit, and the life of the transistor. The desirability of keeping the temperature low to minimize I_{CO} is adequately discussed elsewhere.

On the other hand, operation at miniscule powers is seldom advisable. At low currents the current gain of the transistor is quite small, and it is also small at low voltages. Note the region below 0.2 volts in Fig. 2. Furthermore, the high frequency performance suffers. In Fig. 3 the apparent alpha cutoff frequency is plotted against collector voltage at two current levels. The apparent alpha cutoff frequency is taken as the common emitter current gain multiplied by the frequency of its measurement where the frequency of measurement is so chosen that the current gain is greater than unity and less than half of its low frequency value. Such an estimate may be low by one part in ten. The collector capacitance also increases at low voltages thus reducing high frequency power gain. Fig. 4, which shows the collector susceptance, was made with an adapter for the BCT 300 which allows measurement of the high frequency small signal output and reverse transfer coefficients ho and hr.

The maximum peak signal excursion is an obvious limit to the reduction in bias that is permissible. In the RC coupled stage the greatest distortion is probably introduced where the signal is from a voltage source. The distortion arises because of the exponential characteristic of the input impedance of the transistor. For a signal of ten millivolts peakto-peak the second harmonic at the output is onefifth of the signal or 0.2 fractional and the third 0.08 fractional. The fraction of second harmonic decreases directly as the signal decreases, while that of the third decreases as the square of the signal.

The first purpose of the transistor curve tracer is to set forth the family of collector-current collectorvoltage curves so that an operating region and bias point can be selected to give a reasonable compromise between these conflicting demands. As the preceding photographs show, the curve tracer allows one to pick an operating point such that any desired fraction of the possible current gain or other criterion is achieved. A more useful selection of the operating point is based upon an allowance for operating point or characteristic shift, say by a factor of two, in any direction. From the plots on the curve tracer the bias boundaries for the minimum performance of the stage are determined. The operating point is then chosen to differ from the bias at these boundary-of-performance points by the safety factor (see references 1 and 2).

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The collector cutoff current I_{CBO} (see reference 3) is given by the curve of collector current versus collector voltage with the emitter open. This is

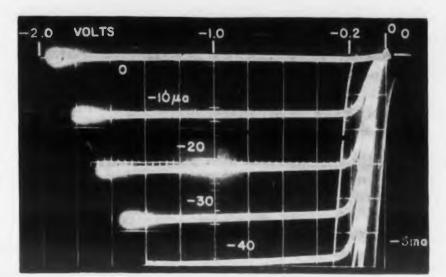


Fig. 2. Curve tracer display of collector current at 1 ma/cm as a function of collector voltage at 0.2 v cm. Input current of 10 μ a per step to a GT 92 transistor with common emitter. Note how the current gain beta falls below 100 at voltages below 200 mv.

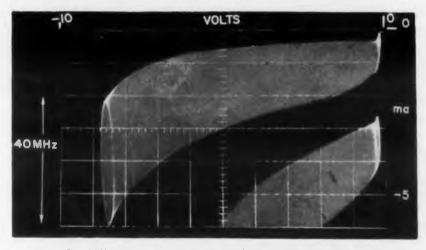


Fig. 3. Collector current at 1 ma/cm and collector voltage at 1 v/cm. A GT 764 with 100 µa peak to peak at 1 mc per second applied to base superimposed on two fixed input biases and collector voltage sweep. Emitter is common. The indicated frequency of alpha cutoff at 8 v is approximately 40 MHz.

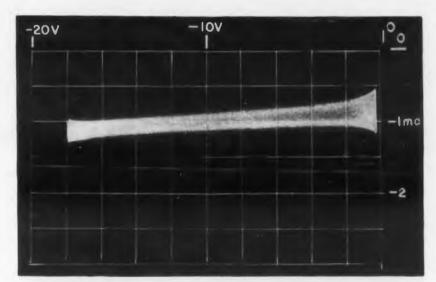


Fig. 4. Collector family for GT 222 with 1 v p-p of 1 MHz applied to the collector. Common emitter. 500 μ a/cm and 2 v/cm.

shown in Fig. 5 together with the saturation current, I_{CBS}, and the common emitter cutoff current ICEO. The scale for the latter is ten times that of the others. Note that I CBO consists of a constant portion plus a portion increasing linearly with voltage plus a portion increasing almost exponentially with voltage. The constant portion ICBOO may be measured at small voltages, is the current that should theoretically flow, and is the component that doubles every nine Celsius degrees. The proportional current IL is measureable by the slope on the display of the curve tracer and varies but little with temperature. This is the leakage current. The curve tracer allows these components of ICBO (ICO) to be determined separately so that its value at any temperature and voltage can be forecast by the equation $I_{CBO} = I_L \times V_C + I_{CBOO} exp(C^{\circ}/9)$.

When the collector cutoff current is too small to measure with the oscilloscope or meter at hand, it can be measured indirectly. The transistor is put into the common emitter connection and reverse base current applied and increased until the collector current no longer decreases at the voltage of interest. The collector current and base current are now each very nearly equal to the collector cutoff current. The value is read from the dials setting the input current to the transistor under test. With silicon transistors, and a few germanium units, the constant portion may be found more easily by calculating it from the saturation current. $I_{CBOO} = I_{CBB}$ $(1-h_{F0}h_{RF0})$ The saturation current, if not measureable directly, is determined from the fact that it increases tenfold for each input bias voltage increase of roughly 60 millivolts. With the Norden-Ketay BCT 300, thermally compensated resistors to set multiples of this voltage into the base are available. The transistor is measured in the inverted connection to put the applied bias across the collector junction. Ten or 100 milliamperes of nominal input current are applied to the resistor to produce the junction voltage giving the appropriate multiple of collector current. The output current is read, with its decimal shifted appropriately, as the saturation current ICBS. This method is a last resort; as it becomes most useful it also becomes most sensitive to voltage bias errors. The exponential relationship between junction voltage and current that makes this method of measurement possible also causes the error sensitivity.

The exponential relation also determines the large and small signal input impedances. The input bias voltage is proportional to the logarithm of the ratio of the operating emitter current to the emitter diode saturation current. The input bias voltage at the operating current is read with the curve tracer by switching to the display of input voltage.

With the curve tracers having a floating sweep voltage power supply, proper termination for the hybrid coefficients h_o and h_r will generally exist. Proper termination for measurement of h_1 and h_2 requires a collector load resistance that is small. The load resistance is satisfactory when (for full display of the collector characteristics) the sensitivity of the oscilloscope for the current axis is one hundred times as great as for the voltage axis.

Small Signal Coefficients

Next the small signal coefficients are determined in the vicinity of the chosen operating or bias point. The forward current gain is determined directly from its definition as the increment in collector current for a unit increment of base current at a constant collector voltage. At the voltage under consideration, the increment in collector current is read directly on the face of the oscilloscope. If the deflection system of the oscilloscope is uniform and linear, the pattern may be offset for convenience in reading. This is shown in Fig. 6. Restore the nosignal display point to the zero-zero scale point immediately after reading.

Reading of the small signal current gain at a given operating point can be made more simply or more accurately by the use of an analyzer. See Fig. 1. With this, the stepped and swept biases are removed and potentiometers used to set in biases to the chosen operating point. A smaller increment of stepped input current can now be superimposed, or a power frequency sine wave, or an alternating current wave of most any form at the frequencies of interest (superimposed from an external oscillator). High gain ac coupled amplifiers may now be used in the indicating oscilloscope or voltmeter. The alternating current is calibrated by switching it directly into the precision load resistor instead of through the transistor. The gain of the system is adjusted to give unit indication. A flick of the switch and the transistor is inserted into the circuit between the voltage dropping resistor and the load resistor, so that the meter now reads the current gain. These alternating current techniques are necessary where the heating of the transistor at its operating point causes drifts that would invalidate the curve-to-curve measurements, and also where the frequency of interest is high enough so that the transistor's coefficients differ from their low frequency and direct current values.

Cascaded RC Coupled Stages

In cascaded RC coupled stages the overall current gain is but little less than the product of the current gains of the individual stages. The amount by which the current gain of each cascaded stage falls short of the transistor current gain can be expressed by a correction factor, F, multiplying the current gain, B, of the transistor. The overall current gain of a four stage amplifier is then $B_1F_1B_2F_2B_3F_3B_4F_4$. Other loading effects and losses can be similarly accounted for. This is the method of successive approximations. The first approximation to the gain of the amplifier is the product of the current gains of the individual transistors. For the interstage coupling the second approximation correction factor is factored into that existing because the collector load resistors are only finitely larger than the input impedance of the following stage and that existing because of effects contributing still smaller losses. The third approximation is in the assumption that the output impedance of the transistor is large relative to the load resistor, R_L, and the input impedance in the same interstage network. The correction for this approximation is often unnecessary and the correction for the residual losses is usually unnecessary. It is easier to calculate the corrections separately and insert them if they are large enough to warrant than it is to solve the complete network equations. The factor F_2 in the above example is then made up of

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Input Impedance

At low frequencies the input impedance of a transistor is most easily found by calculation. For either base or emitter input the resistance is given by the thermal voltage divided by the input current. (proof supplied on request). The thermal voltage V_{θ} is defined as kT/q and is about 25 millivolts at room temperature. In the common emitter connection the collector cutoff current is part of the input current to be used in this calculation, and must be added to the external input current. The input current is best found by dividing the collector current by the current gain. The transistor input resistance is then given by; $h_i = V_{\theta} h_U I_c$. The curve tracer is used to check this value by setting the display to show the transistor input voltage V_1 and stepping the input current. The input voltage increment for unit input current increment at constant output voltage is by definition the input resistance, h_i. This may be difficult to read on the face of the oscilloscope or may be wanted at a frequency at which it is different from the dc value. The methods used for h_f apply here with the substitution of input voltage for output current. The analyzer is particularly useful if a measured value of h_1 or h_0 is desired.

Output Impedance

The correction for the output impedance being less than infinite requires the measurement of it. Restated in terms of the hybrid coefficients, "the correction for the output admittance being greater than zero." The small signal ouput admittance is the increment in output current for a unit increment in output voltage with the input current held constant. The measurement is made on the family of collector current as a function of collector voltage curves. The measurement is made along the tangent to the curve of constant base current passing through the point of interest. See Fig. 6. The portion of the curve intercepted by a unit increment of collector voltage is noted and the increase of collector current from one end of this segment to the other is the output conductance h_0 . One saving factor for the curve tracer is that as this measurement becomes more difficult to make because of the small size of it, the need for accuracy in the measurement de-

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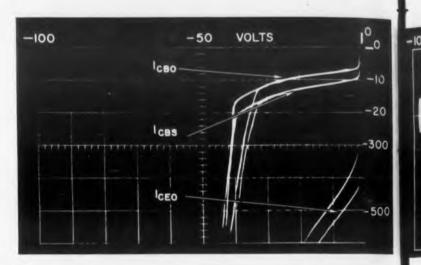


Fig. 5. Collector family GT 222 with 10 μ a/cm for I_{CBO} and I_{CBS} but 100 μ a/cm for I_{CEO}. For all, 10 v/cm. Collector cutoff current is the smallest of these three. Subtract 1 μ a/10 v from all curves to allow for the input conductance of the oscilloscope.

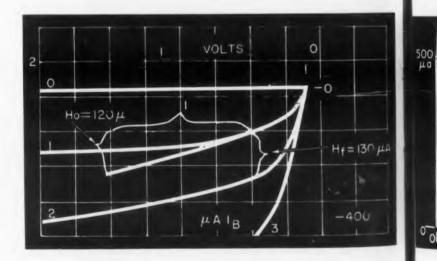
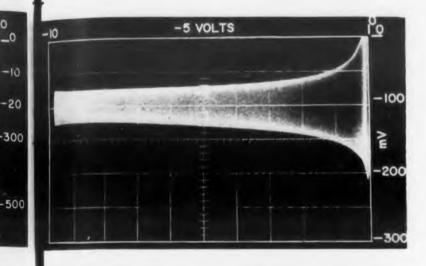


Fig. 6. Offset of the zero point for ease in reading small signal values by increments.

creases. The correction factor for it approaches unity. If a measurement is essential in any case, the analyzer allows it to be made by applying steady input and output biases to put the transistor at the operating point. A small sweep voltage is superimposed on the collector bias voltage and the collector current that results observed.

Observing the input voltage under these conditions gives the reverse voltage transfer ratio hr. The foregoing design procedure has assumed that the ef-



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Fig. 7. A plot of input voltage at 50 mv/cm as a function of output voltage at 1 v/cm for a GT 222 with 1 v p-p of 1 MHz applied to the collector and base common.

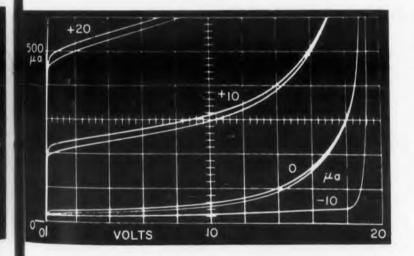


Fig. 8. Collector family 100 µa/cm and 2 v/cm for damaged GT 949 in common emitter with -10, 0, 10, 20 and 30 µA applied to the base. Overheating has reduced the saturation voltage to 18 v but the characteristics below 10 v are little changed.

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fect of this reverse voltage transfer is negligible. This is often the case. If it must be considered the first approximation is to add a correction factor which is close to but may be greater or less than unity. A plot of h_r as a function of collector voltage at intermediate frequency is shown in Fig. 7. The considerations in the incorporation of this correction supply material enough for two or more articles.

If the stage gain arrived at in this fashion is too large either local or overall feedback may be used to reduce it. Alternatively and if it is too small, the transistor type can be changed.

The final circuit design is then haywired and connected to use the analyzer current and voltage power supplies to power it. A selection of transistors at the limits of the manufacturers' range of production can then be plugged in to check the adequacy of the margins set up.

When the engineering model of the circuit has been built, the tracer is very convenient for checking transistors suspected of damage. The curve tracer has the advantage of quickly showing all of the transistor's useful operating region. Damage to a transistor may render it unfit for use in a particular cicuit but still not show up on a beta checker. An example is shown in Fig. 8. The transistor shown is a GT 949 rated at 30 volts and 100 milliwatts. A bit more than double the rated power applied momentarily reduced the sustaining voltage to twenty volts (as shown) with no apparent change in the characterestics at lower voltages, where most single point testers operate. The curve tracer has the further advantages that the average power applied is only one-fourth to one half of the peak power and of showing momentary variation in the transistor's characteristics. An example of such a variation is failure of the retrace to fall on top of the sweep. An upward drift of current is caused by continuous heating. A smooth gross deviation repeating each sweep occurs when the transistor is overheated in each single sweep. A jittery and irregular lack of superposition is indicative of an improperly processed or subsequentially damaged transistor. Such a transistor is likely to soon show excessive noise, leakage current, and short life.

Having designed the circuits of commercial wide band, precision small signal, and inexpensive testers, the author's preference is for a circuit analyzer due to its versatility. As a curve tracer it has the highest information rate for characteristics from transistor to operator.

References:

1. Norman B. Saunders, "Designing Reliable Transistor Circuits" Electronic Design, Vol. 3, No. 3, March 1955, pp. 24-27 and No. 4, April 1955, pp. 36-39.

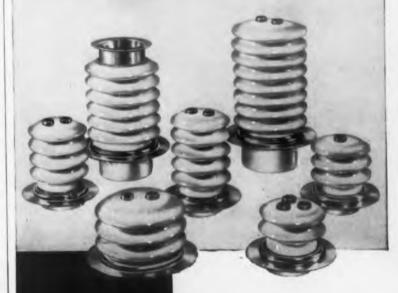
2. Keats A. Pullen, "Using Contour Curves in Transistor Circuit Design", Electronic Design, Vol. 3, No. 7, July 1955, pp. 22-25.

3. "IRE Standards on Letter Symbols for Semiconductor Devices, 1956" Proc. IRE, Vol. 44, No. 7, July 1956, pp. 934-7.

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Recent advances in the semiconductor field have resulted in the commercial availability of transistors designed specifically to handle large amounts of power. These "power transistors" are capable of dissipating up to several watts and are particularly suitable for use in audio-frequency power amplifiers. Circuit-design considerations for the application of pnp alloy junction power transistors to audio-frequency power outputstages are presented, along with a discussion of the effects of source and load impedances on distortion. Methods of obtaining a desired degree of bias stability with temperature variations are also outlined. Although a specific application is described in this article, sufficiently general remarks are made which are applicable to a wide variety of transistor power amplifiers.

Class A Transistor Power Amplifier Design

Robert Minton Semiconductor Div. Radio Corp. of America

(2)

•HE CHOICE of class A or class B push-pull operation depends upon several factors, including the amount of power output and power efficiency required. The object is to obtain as much power output as possible with a minimum distortion. A single power transistor can be used in a class A circuit for moderate output. The output is developed such that collector current flows continuously throughout the cycle. Because maximum power is dissipated in the transistor at zero input signal, the maximum possible output power is one-half the maximum rated dc power dissipation, $P_{max}(dc)$.

In audio power amplifier design, the most important consideration is of course the power-dissipation capability of the transistor. The maximum power that can be dissipated before "thermal runaway" occurs depends heavily on how well the heat generated within the transistor is removed. When it is removed by conduction, the ability to do so is measured by the thermal resistance. The lower this figure, the greater the power-handling capability. Other factors which determine the maximum powerdissipation capability are the collector-voltage rating, reverse collector saturation current, circuit stability factor, and maximum ambient temperature. The maximum permissible dissipation, P_{max} , of a germanium transistor is given by:

$$P_{max} = \frac{12.5}{\Theta} \times ln \left[\frac{12.5}{\Theta s_f V_{ce} I_{cs}} - \frac{(T_a - T_{25})}{\Theta} \right] \quad (1)$$

Where Θ is the total thermal resistance of the transistor and chassis in deg C per w,

 V_{ce} is the collector-to-emitter voltage in volts, I_{cs} is the reverse collector saturation current at

25 C,

 s_{l} is the circuit stability factor, and

 T_a is the maximum operating ambient temperature in deg C^{1, 2}.

In circuits having low values of $s_i V_{ce}$, P_{max} as computed may be greater than the power which can be obtained in practical circuits. The actual power dissipation possible in a practical circuit design is limited by the maximum safe collector-junction temperature at which the power transistor can be operated without appreciable alteration in its electrical characteristics or a decrease in its life expectancy. For most germanium transistors this is below 100 C. The maximum power-dissipation capability can be expressed in terms of the allowable junction temperature as follows:

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$$P_{max} = \frac{T_j - T_a}{\Theta}$$

transistor. "Thermal Runaway" occurs

at any point above the sloping lines.

Where T_i is the maximum allowable junction temperature in deg C, T_a is the ambient temperature in deg C and Θ is the total thermal resistance of chassis and transistor in deg C per w.3 The two equations for P_{max} can be used together to obtain powerrating curves for a given transistor provided that CI

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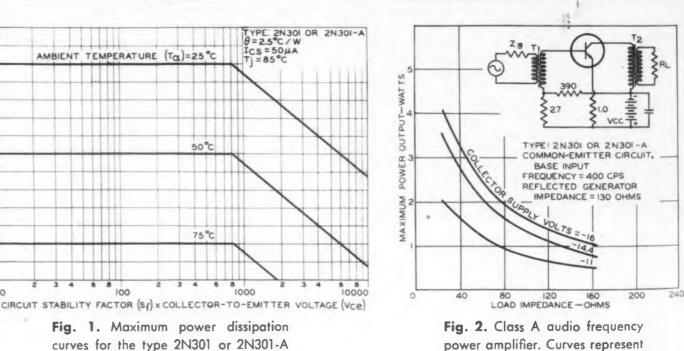
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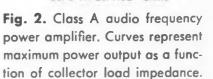
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• when the allowable power dissipation obtained from eq (1) is greater than that calculated from eq (2), the maximum allowable collector-junction temperature rise is the limiting condition for dissipation; and

• if the allowable power dissipation calculated from equation (1) is less than that found by equation (2), then thermal runaway is the limiting factor.





ig. 1 shows a set of maximum power-dissipation curves for the 2N301 or 2N301-A power transistor. The horizontal lines represent the maximum power difficult pation for various ambient temperatures when the limiting factor is maximum collector-junction temperature rise. The sloping portion of the curves represents the maximum power dissipation before run way occurs. The maximum power dissipation can be obtained for any value of $S_t V_{ce}$.

Class A Power Amplifiers

Fig. 2 shows a typical class A audio-frequency power amplifier for use in an automobile receiver output stage, together with curves of maximum power output as a function of collector load impedance. For the supply voltages shown, the load impedance must be kept low if large amounts of power output are to be obtained. Consequently, the possibility of impedance matching for maximum power transfer is eliminated; distortion becomes the limiting factor in selecting the output load value. In the case of output stages for automobile receivers, a maximum value of 10 per cent total harmonic distortion is usually acceptable, which the curves shown in Fig. 2 represent.

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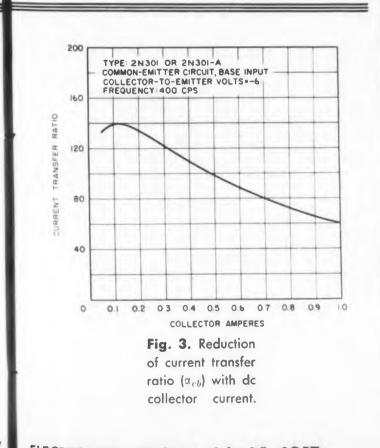
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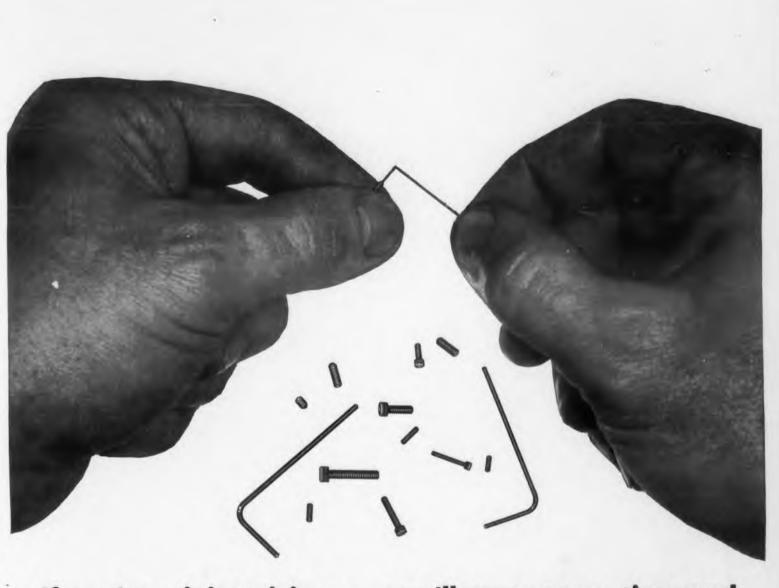
The power gain of a junction-transistor class A amplifier is a function of input resistance, load impedance, and ac large-signal current transfer ratio, and can be expressed as follows for the commonemitter circuit:

Power Gain = $\alpha_{cb}^2 \frac{R_1}{R_{in}}$

(3)

Where α_{eb} is the ac large-signal current transfer ratio,





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 R_{I} is the collector load impedance in ohms, and R_{in} is the ac input resistance of the transistor in ohms, i.e., r_{bb} plus the product of α_{cb} and the external emitter resistance.

At the high values of emitter current, the resistance of the emitter junction is very low and the input resistance of the transistor is approximately equal to the resistance r_{bb} . When an unbypassed external emitter resistor is used, the resultant input resistance of the transistor is approximately equal to r_{bb} plus the product of the current transfer ratio (α_{cb}) and the emitter resistor. If this resistance is greater than the load impedance, the power gain of the class A stage will again be low unless the transistor has a high α_{cb} . Fig. 3 shows the reduction of α_{cb} with dc collector current.

Efficiency of Class A

The efficiency of a class A transistor power amplifier is defined as the ratio of the power output that can be developed with only moderate distortion to the dc power supplied to the collector circuit. A class A power amplifier has a maximum theoretical efficiency of 50 per cent. In practice, the over-all efficiency depends upon the efficiency of the output transformer and the amount of power lost in the bias network. The collector-circuit efficiency is greatest at full rated power output and decreases as the power output is reduced.

Distortion is principally a function of supply voltage, power output, nonlinearity in transfer characteristics, and source impedance. When the input (base) current is sinusoidal, the nonlinearity in the current transfer characteristic is small at low signal levels. The output current is fairly linear and low in harmonics. As the signal level increases, the input current traverses a greater portion of the nonlinear region of the transfer characteristic and the harmonic content of the output current increases considerably. Fig. 4 shows the total harmonic distortion as a function of power output for different supply voltages. The increase in distortion with increasing power output is due primarily to the nonlinearity in the base-to-collector current transfer characteristic. Clipping is the cause of the rapid change in slope of the distortion curve.

Source Impedance Distortion

The source impedance presented to the input of a class A stage which uses an interstage transformer depends on the type of driving device used and the impedance transfer ratio of the driver transformer⁴. When the transferred driver output impedance is much less than the input resistance of the transistor, the class A stage is considered to be operated from a constant-voltage source. When the reflected driver output impedance is much greater than the input resistance of the transistor, the stage is considered to be operated from a constant-current source. Fig. 5 shows the variation in total harmonic distortion as a function of the ratio of reflected source impedance (Z_q) to the input resistance of the transistor. The total harmonic distortion increases appreciably as the ratio $Z_{g}R_{i-n}$ is increased, partly because of the higher degree of nonlinearity in the current transfer characteristic. The lowest feasible value of source impedance should be used in a class A power amplifier to minimize distortion.

In some applications, it may be necessary to use negative feedback to reduce the total harmonic distortion. One method of obtaining degenerative feedback is by the insertion of resistance in the emitter lead. The amount of emitter resistance that can be used is normally limited by the power-gain requirements of the output stage.

Temperature Considerations

The effects of temperature changes on transistor behavior are due primarily to changes in reverse collector current, I_{co} , and the dc input conductance. These parameters are highly sensitive to temperature changes, and may cause a shift in operating point. In a class A circuit having low dc load resistance, the collector voltage is relatively constant, but the collector current will increase with temperature due to variations in I_{co} and dc input conductance. The resulting increase in dissipation may cause operation beyond the maximum power ratings of the transistor. For satisfactory operation over a wide range of temperatures, some form of stabilization must be used.^{5, 6, 7}

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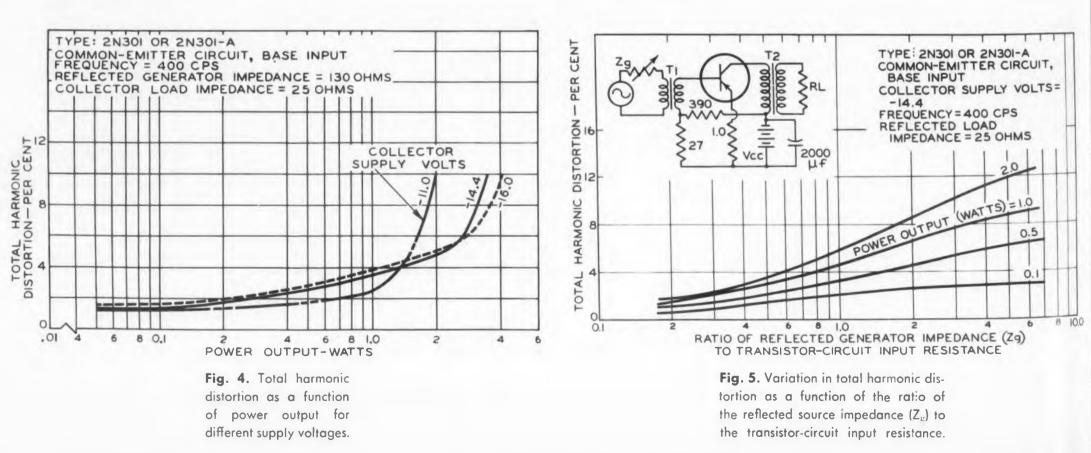
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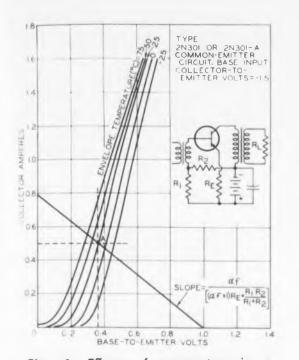
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The transfer characteristic curves shown in Fig. 6 illustrate the effects of temperature upon the



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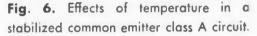
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transistor in a stabilized common-emitter class A circuit. The operating point is designated by point A on the 25 C curve. If this common-emitter circuit were operated with a constant base-to-emitter bias voltage, an increase in temperature would cause an appreciable increase in quiescent collector current and a consequent increase in power dissipation. In the circuit show, however, the bias voltage is determined by the voltage drops across the emitter resistor, R_e and the parallel combination of R_1 and R_{2} . The voltage drop across the emitter resistor is essentially proportional to the collector current, and tends to stabilize the collector current by applying a reverse bias to the transistor. For a given value of emiter resistance, therefore, the stability of the operating point is largely dependent on the resistance of the parallel combination of R_1 and R_2 . Decreasing the resistance of the parallel combination of R_1 and R_2 results in an increase in stabilization

This is the first of a series of two articles on circuit considerations for audio-output stages using power transistors. The second article will deal with class B push-pull power amplifiers.

References

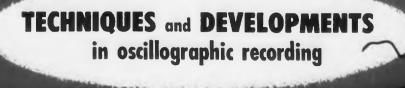
L. "A 20 Watt Transistor Audio Amplifier" by H. C. Lin, Transistor I, RCA Laboratories, pp 536-537, March 1956. 2. "Private Communications" by C. F. Wheatley, April 1956.

3. "Some Aspects of the Design of Power Transistors" by N. H. Fletcher, Procedings IRE, Vol. 43 pp 558-559, May 1955.

4. "Design Principles for Junction Transistor Audio Power Amplifiers" by D. R. Fewer, IRE Transactions on Audio, Nov-Dec 1955.

⁵. "Temperature Effects in Circuits Using Junction Transistors" by H. C. Lin, Transistor I, RCA Laboratories, pp 309-402, March 1956.

6. "Power Transistors for Audio Circuits" by L. T. Giacoletto, Electronics Vol 27 pp 144, January 1954. 7. "Bias Stabilization" by R. F. Shea, Principles of Transistor Circuits, John Wiley & Sons, Inc. pp 102-108.





DESIGN PRINCIPLES AND SOME APPLI-CATIONS OF A PREAMPLIFIER FOR LOGARITHMIC MEASUREMENTS

THE Model 150-1400 Log Audio Preamplifier (Figure 1), one of eleven plug-in "front ends" now available for 150 Series systems, permits measurements involving logarithmic or exponential functions. The "Log Diode" circuit (shaded portion

of circuit block diagram in Fig. 2) is the heart of this instrument, and is based on the logarithmic relationship between the voltage across a thermionic diode and the cur-

Fig. 2

Fig. 1

rent through it. If R is large, the current through the diode i_1 becomes proportional to the voltage e_1 , and the logarithmic relationship of e_2 and i_1 is transformed into a logarithmic relationship between e_2 and e_1 . Circuit constants for this Preamp were chosen to provide an accurately logarithmic relationship between e_2 and e_1 , over the range of 200 to .63 volts for e_1 . This is a 50 db spread, and the gain of the DC output amplifier (fed by e_2) is arranged so that a 50 db variation in e_1 produces a 50 mm stylus deflection. In audio or AC measurements, e_1 is derived from a peak reading type rectifier-filter circuit, which follows a high quality 20 cycle -20 KC audio amplifier. With an input of 100 mv RMS, this amplifier will produce a 200 volt output from the rectifier. The 50 db chart, therefore, corresponds to a variation in AC input voltage of 0.316 to 100 mv.

In DC measurements, the audio amplifier is bypassed and the input applied to the diode circuit. Since the diode itself is a rectifier, used in the forward direction with its cathode near ground, the DC input must be polarized with the high side positive.

One broad area of application for the Log Audio preamplifier is audio level recording. For example, room reverberation time can be measured by recording sound level decay after the sound source is suddenly turned off, the reverberation time considered the period required for a 60 db decay to occur. Another example of audio signal recording is the plotting of frequency response curves of audio equipment such as microphones, filters, loudspeakers, etc. A multi-channel recording system with appropriate filters also makes possible audio spectrum analysis.

A second major type of application of this Preamp is the recording of DC voltages on a db basis. If the signals are small, a chopper can be used to convert DC to AC, thus taking advantage of the Preamplifier's audio amplifier. With an impedance matching transformer added to such an arrangement, the system becomes a logarithmic DC millivoltmeter or logarithmic DC microammeter of extreme sensitivity. Such a device could be used for plotting the volt-ampere characteristic of a germanium diode, which might be very helpful in selecting matched pairs of diodes. Another possibility is plotting the output of a fixed gain radio receiver and linear detector to a db scale, to rapidly record antenna performance data.

A comprehensive discussion of the design and these applications of the Log Audio Preamplifier is contained in an article by Dr. Arthur Miller, Chief Electrical Engineer of Sanborn Company, published in the Sanborn RIGHT ANGLE. Copies are available on request.

Which Oscillographic Recording "PACKAGE" fits your needs?

SANBORN "150's" are housed, basically, in either of two ways: a vertical mobile cabinet, or separate portable cases for amplifier and recorder units. This in itself provides a number of "packaging" possibilities, but the number is greatly increased by various other alternate,

and sometimes special, housings. For example, an entire six- or eight-channel recording assembly is available in an extremely compact, mobile cabinet only 45'' high; or the same recorder can be portably housed in a $22'' \times 21'' \times 23''$ case. If field use of "150's" is planned, individual units in cases fitted with removable covers

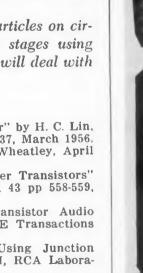
Detailed information, and assistance with your particular recording problem, is always available from Sanborn engineers.

and carrying handles, connected by patch cords, may be the best answer. Occasionally only a "special" adaption will meet a specific need.

But whatever the "150" oscillographic recording "package" you use, you're assured of basic Sanborn "150" advantages: inkless recordings in true rectangular coordinates; 1% linearity, resulting from high torque galvanometers and current-feedback driver amplifiers; numerous chart speeds, from 0.25 to 100 mm/sec.; choice of single to 8-channel systems, readily adapted to new requirements by plug-in Preamplifiers selected from 11 presently available types.

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SIMPLE HERMETICALLY-SEALED time element . . . long life stability. Not subject to aging or fatigue.

LOW COST as a unit; even lower considering simplified installation.

Extension and **Adapter Sleeves**

and alarm spring.

E XTENSION and adapter sleeves, which provide more enclosed space in the backshell area of connectors, and which permit the use of proper AN clamps with any given size cable and connector, increase the reliability of the electrical circuits to which they are attached.

Enclosure of wires in the standard backshell is, in many cases, possible only by crowding the wires, wherein strain and insulation damage may result. The extension sleeve replaces the stand. ard backshell increasing the space for wire terminations at the connectors.

There is only one clamp to fit a given size connector and very often it is too large or too small to fit the cable. The adapter has provisions for stepping up or stepping down the thread size for attaching the clamp. The adapter mates with the connector and permits the use of any of the AN clamps with a given connector.

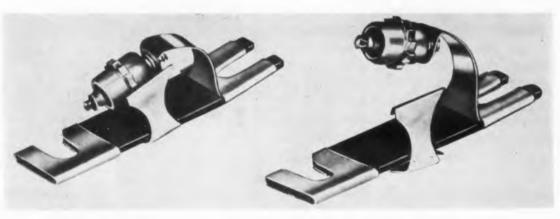
Developed by Pacific Automation Products, Inc., Glendale 1, Calif., the devices are threaded and fabricated of aluminum with an anodized finish. For more information on these extension sleeves fill out the Reader's Card and circle 44.

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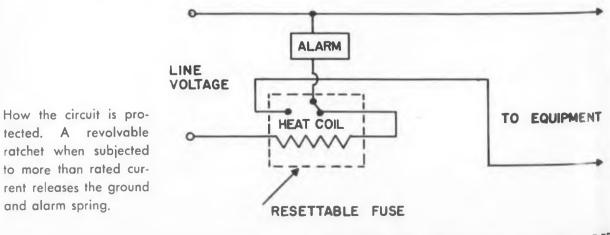
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Resettable Grasshopper Fuse



Resettable grasshopper fuse. At left contact is made when operating within normal rating of fuse. At right the contact is broken and alarm circuit is closed.



ELECTRONIC DESIGN . July 15, 1957

Bulletin T-5002 gives details. It's yours upon request.

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ELECTRIC COMPANY 156 Plum St., Trenton 2, N. J. CIRCLE 43 ON READER-SERVICE CARD FOR MORE INFORMATION

Time delays . . . from 1/4 to 120 seconds Small size . . . Overall dimensions: 21/16" x 2" x 1%16"... Weight 3 ozs. Contact capacity . . . 3 amp. at 120 volts AC (Non-inductive load) . . . D.P.D.T. High Speed actuation . . . positive contact

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D Y COMBINING the familiar grasshopper **D** fuse with a heat coil, a new economical and positive acting fuse, arc free, and with accurate operation time results.

Heat coil operation is simple and positive. When subjected to more than the rated current, the ratchet, which is permitted to revolve, releases the ground and alarm spring. After the trouble has been cleared, and the current flow is normal, the fuse can be reset manually by the ratchet which is again locked into position. In the case of abnormal overload or potential where the nichrome wire coil has been damaged, the heat coil can be unscrewed and easily replaced without disturbing the grasshopper fuse base.

Heat coils are manufactured to a range of ratings, notably a three hour current carrying capacity of from 0.1 amp to a 0.055 amp. The fuse will operate in 210 sec, when there is a current of 0.18 amp in the coil rated at 0.1 amp, and a current of 0.11 amp in the 0.055 amp rated coil. The grasshopper fuse bases are made to accommodate varied mountings and screw sizes. The fuses were developed by Cook Electric Co., 2700 Southport Ave., Chicago 14, Ill.

These grasshopper fuses are ideal for actuating alarm circuits or grounding out stray or excessive currents. For additional information about this resettable grasshopper fuse, fill out the enclosed Reader's Service Card and circle 45.

PRECISION TRANSISTOR ANALYZERS

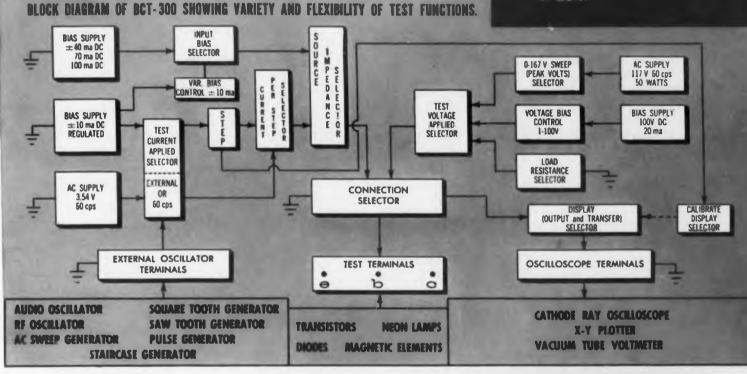
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- 1. Full Family Curve Tracing plus scope calibration.
- 2. Input impedance and current gain versus frequency can be read directly on a meter.
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PERFORMANCE ADVANTAGES

- Tests all PNP and NPN transistors in either grounded base or grounded emitter configuration.
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- Sweep circuit provides 270 volts, 10 amperes, or 20 watts.
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Wide Range **Parameter Testing BTS-400** 1. Provides direct meter reading of all hybrid parameters in grounded base or grounded emitter configuration.

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- 4. This is the only test unit made with an input impedance parameter range of 10 to 100,000 ohms.
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The curve shown above on the 55 watt Delco 2N174 was obtained with Norden-Ketay **BTS-400** Test Set.

Write for Bulletins containing full data on these transistor measuring devices to:

Norden-Ketay Corporation, Instrument & Systems Division, Wiley St., Milford, Conn.

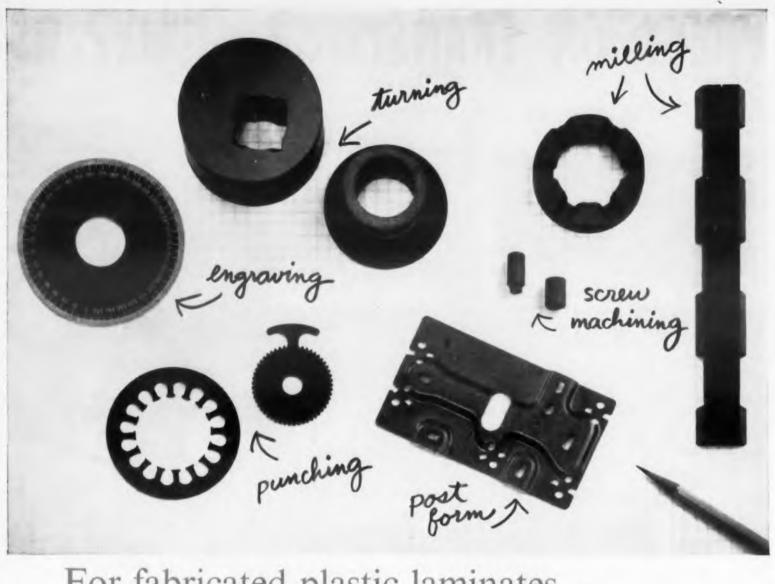
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A Voltage Gain Nomogram for Transistor Circuit Design

A S AN aid to rapid design and application of transistor circuitry to electronic systems, these two nomograms can be used to determine gain variations when changes are made in various circuit values.

The Transistor Voltage Gain Nomogram described will enable gain variations to be easily determined. It also permits the rapid design of common-base and common-emitter amplifiers for any desired gain. Any adjustment of either the load impedance (R_L) or the external emitter resistance (R_E) will automatically plot the course that the voltage gain (VG) will take. By the same token, if any two of the values are known, the other may be found.

The nomograms are based upon the approximation formula:

$$VG \cong \frac{\alpha R_L}{R_E + re + rb(1-\alpha)}$$
 (1)

Which assumes:

$$R_L \ll rc$$
$$R_E + rc + rb \ll rc$$

The approximation is for all practical purposes correct if $R_L \ll rc$ by two or more orders of magnitude. In general, $rc \cong 1$ megohm for junction transistors.

$$rc = \frac{V_{CB}}{I_{ce}} \tag{2}$$

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As R_L increases and approaches rc, the inaccuracy of equation (1) and of the nomograms increases. Generally, however, R_L remains lower than (0.01)rc. An error of 1 per cent may be expected if $R_L = (.001)rc$; and approximately 10 per cent as R_L approaches (.01)rc. For strict applications, and particularly where

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tight tolerances, great accuracy, and higher load impedances than $R_L = (0.01)rc$ are to be used, the exact expressions for VG should be used.

Nomogram Operation

Nomogram II functions with a denominator resistance R_D , where:

 $R_D = R_E + re + rb(1-\alpha)$

(3)

(4)

(6)

(7)

(8)

Parameters re and rb may be found in the specifications for a particular transistor. As an aid, Nomogram I lists the transistor's alpha with its $(1 - \alpha)$. A straightedge from $(1 - \alpha)$ to the *rb* scale will quickly determine the $rb(1 - \alpha)$ read from the center scale. Adding $re + rb(1 - \alpha)$ mentally, one gets the value of R_D .

 $R_D = re + rb(1-\alpha)$

However, if in grounded-emitter orientation an external emitter resistor, R_E , is further added, then the combined total becomes R_D , as in equation (3).

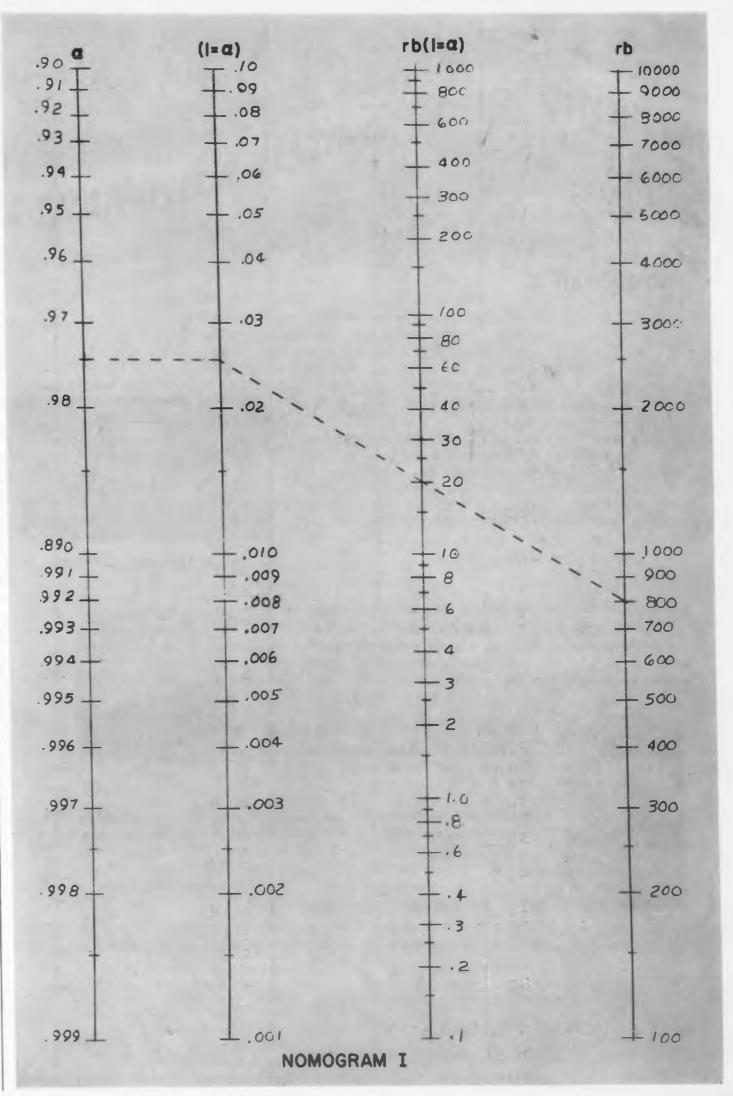
When $re + rb(1 - \alpha) \ll R_E$, in example by approximately two orders of magnitude, then:

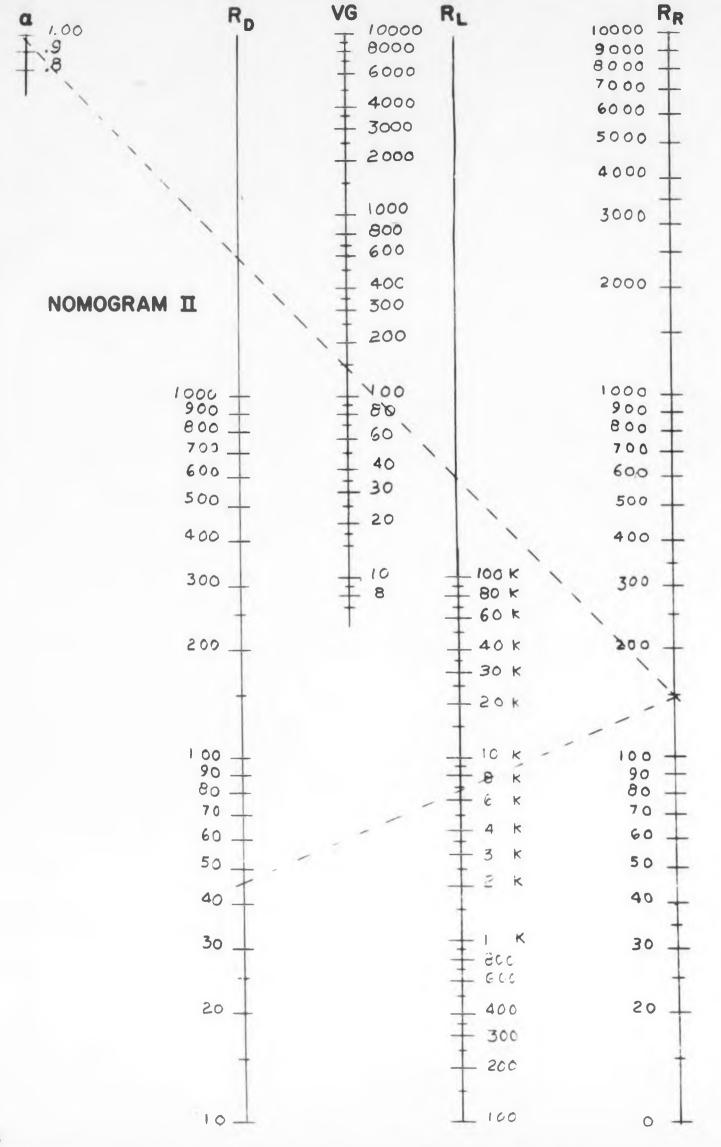
$$R_{D} \cong R_{E}$$
(5)

$$VG \cong \alpha \frac{R_{L}}{R_{D}}$$
(6)
Where the resistance ratio $R_{R} = \frac{R_{L}}{R_{D}}$ (7)

Then: $VG \cong \alpha R_R$

Set a straightedge on Nomogram II, from the value of denominator resistance on the R_D scale to the value of load impedance on the R_L scale, and note the value of the resistance ratio on the R_R scale. Now set the straightedge from the R_R value to the known alpha on the α scale and read the voltage gain direct on the VG scale.





The reverse procedure may also be used, by setting the straightedge from α to the desired value of VG and noting the R_R obtained. If R_L is known, then R_D may be found. Knowing the value of the parameters, *re* and *rb*, from the specifications previously employed, these parameters may be subtracted from R_D , the result being the value of the external emitter resistance, R_E , which should be placed in the emitter leg.

Sample Problem

(Using a 2N35-n-p-n in grounded-emitter) 1. List the values of re, rb, rc and α from the specifications: re = 26 ohms rb = 800 ohms rc = 2 megohms $\alpha = 0.975$ 2. Find the value of $rb(1 - \alpha)$ from Nomogram I. $rb(1 - \alpha) = 20$ ohms 3. Substitute the value of re and $rb(1 - \alpha)$ into Equation (4): $R_{\nu} = re + rb(1 - \alpha)$ (4) = 26 + 20 = 464. Note the value of R_E to be used, and compare with Equation (4):

 $R_E >> re + rb(1 - \alpha)$ by approximately 100 times.

5. If the comparison above is true, then substitute R_E into equation (5):

$$R_D \cong R_E \tag{5}$$

If not true, then substitute R_E into equation (3):

$$R_D = R_E + re + rb(1-\alpha) \tag{3}$$

If no R_E is used, then continue using equation (4):

$$R_D = re + rb(1-\alpha) \tag{4}$$

6. Assuming that an external emitter is used, resistance of $R_E = 500$ ohms, then the comparison of $R_E >> re + rb(1 - \alpha)$ would be true: $R_E >> 46$ by approximately 100 times.

Substituting into equation (5):

$$R_D \cong R_E$$

$R_D \cong 500 \text{ ohms}$

7. Note the value of R_L to be used and substitute into Equation (7): (Let R_L be 6000 ohms)

$$R_R = \frac{R_L}{R_D} \tag{7}$$

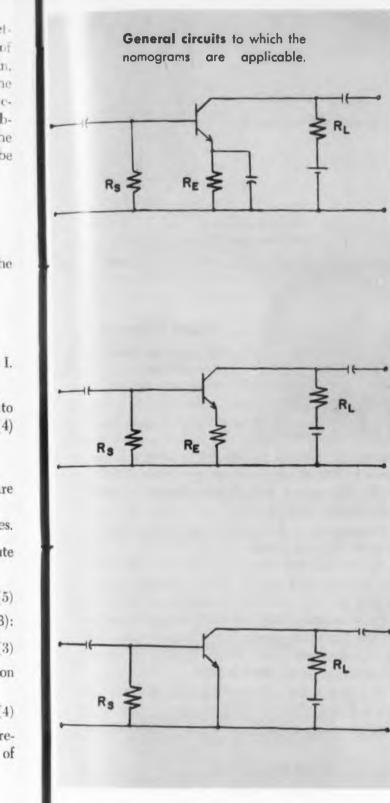
8. Since $R_L \ll rc$ (6500 \ll 2 megohms), less than 10 per cent error may be expected by use of the Nomogram.

9. Find the value of R_R from Nomogram II and substitute into equation (8):

$$\begin{array}{l}
VG \cong \alpha R_R \\
VG \cong \alpha(13)
\end{array}$$
(8)

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10. Lastly, knowing the value of alpha and R_R , find VG on Nomogram II.

$VG \cong 12.7$

Had no emitter resistance been used, R_R would have been 140 and VG equal to 136. For a reprint of this article, turn to Reader

Service Card and circle 499.

References

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F. R. Stansel: Transistor Equations: ELECTRONIC DESIGN: March 1953: page 156.

Nomogram for Some Transistor Parameters, H. Lefkowitz, Electronic Design, 15 Oct. 1956, p.

Principles of Transistor Circuits, R. F. Shea, John Wiley and Sons, Inc., 1953.

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TRANSISTOR TEST SET — The transistor tester that is rapidly becoming the standard of the industry ... for h parameters and equivalent T coefficients ... NPN and PNP junction and surface-barrier transistors ... grounded-base or emitter circuits . . . alpha and beta cut-off $\ldots I_{co}$ and C_c . Test frequency from 100 cps to 1 mc.



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Transistor Transformers

Seven Types



Seven additional types of ultra-miniature DO-T transistor transformers are available. These units weigh one-tenth ounce and are fully hermetically sealed. Included in this group are a number of 500 mw units designed for pushpull transistor to 600 ohm line, a chopper input transformer, transistor interstage transformer, and a line to line matching transformer.

United Transformer Corp., Dept. ED, 150 Varick St., New York 13, N.Y.

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Spectrum Analyzer 10 Cps Resolution



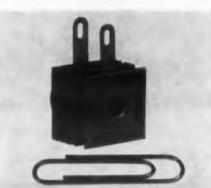
Designed for applications requiring extremely high resolution, such as investigation of side bands caused by low modulating frequencies, single sideband transmissions, teletype, etc. The SB-12 Panalyzor can be used to observe signals anywhere in the spectrum up to 1000 mc by means of an external signal generator and an internal aperiodic mixer which translate the spectrum segment to be analyzed down to the 450 to 550 kc input band of the Panalyzor. Offering the advantages of wide scan spectrum presentation, the SB-12 at the same time permits examination of signals so closely adjacent in frequency that their corresponding deflections normally tend to merge together or completely mask one another in wide scan displays. Maximum sweepwidth is 100 kc continuously reducible to 0 kc. Scan rate is adjustable in steps of 30, 5, 1 and 0.1 cps. Resolution ranges from 3.2 kc to 10 cps. Afc is provided for narrow sweepwidths.

The unit can be used to investigate pulsed rf signals, analyze am and fm transmitters, spot spurious oscillations and modulation, monitor communications bands, test industrial rf equipment, diathermy and electrosurgical instruments, and is applicable to other laboratory and production test problems.

Panoramic Radio Products Inc., Dept. ED, 10 S. 2nd St., Mount Vernon, N.Y.

CIRCLE 50 ON READER-SERVICE CARD FOR MORE INFORMATION

Selenium Rectifier 65 Mil



Designated Type 1263-A for standard mounting, and 1262-B for bracket mounting, this 65 mil selenium rectifier is for use in small electronic equipment. The rectifier has the following characteristics for single phase capacitive loads: Max rms input v of 130 v; max peak inverse v of 380 v; max peak current of 650 ma; max rms current of 175 ma; max dc current of 65 ma; approx rectifier voltage drop of 7 v; min series resistance of 22 ohms, and the max plate operating temp is 85 C.

Federal Telephone and Radio Co., Dept. ED, 100 Kingsland Rd., Clifton, N.J.

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This rotary solenoid is claimed to have a life expectancy of 300,000 snap-action operations at 500 F. It is able to operate with high wattage inputs to produce higher torques. Eight basic sizes are available, ranging from 1 to 3-3/8 in. diam. Starting torques for 45 deg. stroke range from 0.2 to 54.0 lb-in. Special magnet wire and coil insulation, lubrication, bearing and return spring materials were developed for the product. Operation is identical with the standard rotary solenoid. Magnetic action moves the armature along the solenoid axis. This action is converted into a rotary motion by means of ball bearings on inclined races.

G. H. Leland, Inc., Dept. ED, 123 Webster St., Dayton 2, Ohio.

CIRCLE 52 ON READER-SERVICE CARD FOR MORE INFORMATION

5 Mc Crystal High Stability



Type BG61A-5 is a glass mounted, optically polished, gold plated quartz crystal operating on the 3rd overtone mode at 5 mc. The temperature coefficient of the unit is less than 0.1 ppm over a 1 C range at the preferred operating temperature (75 C or 85 C). When used with temperature control adequate to maintain \pm .01 C, the resultant crystal stability is 1 part per billion at 5 mc.

Bliley Electric Co., Dept. ED, Union Station Bldg., Erie, Pa.

CIRCLE 53 ON READER-SERVICE CARD FOR MORE INFORMATION



Dish Antenna Simplified Mounting

A one-piece, four-foot dish antenna designed for tubular mast mounting is secured to 4 in. IPS tubular masting by two heavy-duty clamps. The clamps are designed to produce an even, tight connection assuring positive orientation under extreme wind loads.

This model is constructed on a ring principle. The basic ring is a circular heavy-weight aluminum disc supporting cantilever aluminum arms, which extend to the perimeter. The parabolic surface is covered with expanded aluminum mesh, inert arcwelded to the supporting arms. The antenna is designed to operate in the range of 1000 through 4000 mc. Standard drivers are of the dipole and horn type.

Technical Appliance Corp., Dept. ED, Sherburne, N.Y.

CIRCLE 55 ON READER-SERVICE CARD FOR MORE INFORMATION



surface barrier transistors from SPRAGUE

2N346/SB103

for High Frequency

Oscillators

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60 90

hfe

Min. Typ. Max.

- -

2N345/8B102 for High Gain Amplifiers Min. Typ. Max. hfe 25 40 110 fmax 30 45 -

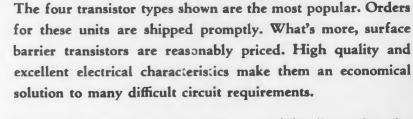
 American
 American

IN VOLUME PRODUCTION MOW!

actual

size

For general high frequency applications, and for high speed computer switching circuits, design around Sprague surface barrier transistors. They are available now in production quantities from a completely new, scrupulously clean plant, built from the ground up especially to make high quality semi-conductor products.



Sprague surface barrier transistors are fully licensed under Philco patents. All Sprague and Philco transistors having the same type number are manufactured to the same specifications and are fully interchangeable. You have *two* sources of supply when you use surface barrier transistors!

WRITE FOR COMPLETE ENGINEERING DATA SHEETS ON THE TYPES IN WHICH YOU ARE INTERESTED. ADDRESS REQUEST TO THE TECHNICAL LITERATURE SECTION, SPRAGUE ELECTRIC CO., 347 MARSHALL ST., NORTH ADAMS, MASS.

TRANSISTORS • RESISTORS • MAGNETIC COMPONENTS CAPACITORS • INTERFERENCE FILTERS • PULSE NETWORKS HIGH TEMPERATURE MAGNET WIRE • PRINTED CIRCUITS



CIRCLE 57 ON READER-SERVICE CARD FOR MORE INFORMATION

Insulation Tester

High Speed



This instrument will detect, totalize, and record insulation faults in material travelling at 400 ft. per min. with 1-in. long electrode. It will detect pinhole invisible to the naked eye at this speed.

The tester will detect and register every fault, since it does not have the inherent limitations of 60 cps testers and fault relays which do not register faults if they occur too close together in time.

Testing is non-destructive. It will not burn insulation. nor mark it in any way. The output is nonlethal. At 10 kv de the maximum short circut current is 4 ma.

Peschel Electronics, Inc., Dept., ED, 13 Garden St., New Rochelle, N.Y.

CIRCLE 56 ON READER-SERVICE CARD FOR MORE INFORMATION



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Simpson WIDE-VUE panel instruments mannan DC MILLIAMPERES Simpson 41/2' 31/2" MILLIAMPERES

concept

styling and visibility

The clean, graceful lines of these "Wide-Vue" panel instruments add two plus values to your equipment. First, style-ultramodern beauty that blends with the advanced design of today's panels. Second, functionalism-longer scales together with wide-angle readability. The $2\frac{1}{2}''$ size, for example, has the same scale length as a conventional $3\frac{1}{2}''$ panel instrument. The durable, plastic cover is formed in one piece, and can be supplied with black or color finishes. Custom-built in $2\frac{1}{2}$ ", $3\frac{1}{2}$ ", and $4\frac{1}{2}$ " sizes. External magnet type movement or self shielded core magnet meter movement.

21/2"

COMPANY ELECTRIC 5200 W. Kinzie St., Chicago 44, Illinois Phone: EStebrook 9-1121 In Canada: Bach-Simpson Ltd., London, Ontario

New Products

1500 F Insulating Fabrics

Also Used for Leak Detections

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Two types of high temperature insulating fabrics for service up to 1500 F have been announced. Made of fiberfrax ceramic fiber, these fabrics are available in various widths or thickness for positive high tempera. ture insulation. In addition, they are also supplied as instrumentation tapes for both insulation and leak detection. The high temperature tapes consist of two stranded Chromel wires covered with reinforced ceramic fiber. When wrapped around pipes carrying metallic or radioactive fluids, the tape both insulates and quickly causes an alarm-sounding short circuit in the event of a leak. This tape is designed to withstand 1500 F for 1500 hr, and is flexible enough to be wrapped in spiral form around pipe of 1/2 in. diam. The fabrics can be treated with silicone rubbers, epoxy resins or can be impregnated with phenolic resin and molded into various shapes. If desired, they can be woven in tubular form.

The Russell Mfg. Co., Dept. ED, 255 E. Main St., Middletown, Conn.

CIRCLE 58 ON READER-SERVICE CARD

Arc Resistance Tester Quality Control for Plastics

An arc resistance tester has been designed to evaluate the arc and track resistance of plastic materials. The Model 126 is employed in measuring the resistance of insulating materials to high voltage-low current arcs. The instrument has a built-in timer to indicate arc resistance time and a specimen holder which automatically levels and sets the correct electrode pressure. The electrode enclosure permits visibility and prevents drafts from disturbing the arc during the test.

Delsen Corp., Dept. ED, 719 W. Broadway, Glendale 4, Calif.

CIRCLE 59 ON READER-SERVICE CAR

← CIRCLE 60 ON READER-SERVICE CARD

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Stock Drawing Forms

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A ringe of stock drawing forms are available for immediate delivery in small or large quantities. Drawing forms in stock are: A size-8-1/2 x 11 in., B size-11 x 17 in., C size-17 x 22 in., and D size-22 x 34 in.

PIC Design Corp., Dept. ED, 477 Atlantic Ave., East Rockaway, N.Y.

CIRCLE 62 ON READER-SERVICE CARD

Stagnation Temperature Probe For Flight Applications

The WCRC temperature probe provides stable measurement of stagnation air temperature. The probe has a high degree of internal, thermal equilibrium in dynamic measurement of total temperature. Heat transfer between probe and mounting is stabilized for wide temperature differentials. The aerodynamic design provides for steady-state readings from subsonic to supersonic speeds. Recovery factor is relatively insensitive to speed. Sensing is accomplished by a resistance element, a thermocouple, or a thermistor, depending on specified input impedance.

West Coast Research Corp., Dept. ED, 2371-1/2 Westwood Blvd., Los Angeles, Calif.

CIRCLE 63 ON READER-SERVICE CARD

Thyratron

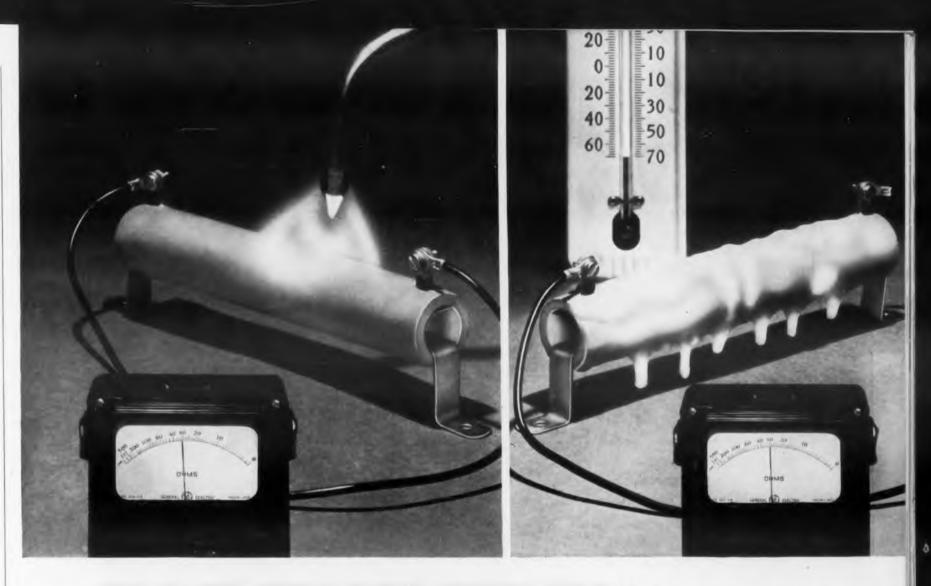
Average Rating of 1 Amp.

The Xenon-filled XR-764, 3-1/2 in. high, has an octal base and top cap and a 10 v drop in use. Filament voltage and current is 5 v and 3 amp respectively, with a heating time of 120 sec. Peak forward and inverse voltages are 500 v dc, start (plus 3 v grid) is 25 v, with 25 v emission at 30 amps. De-ionization time is 200 usec or less. The tube is claimed to be unusually rugged.

Continental Electric Co., Dept. ED, ⁶ N. Michigan Ave., Chicago 2, Ill.

CIRCLE 64 ON READER-SERVICE CARD

CIRCLE 65 ON READER-SERVICE CARD >



TESTS ON NEW GENERAL ELECTRIC RESISTORS PROVE ...

Stable operation from $+700^{\circ}$ to -70° F

Under searing heat or sub-zero cold, General Electric resistors maintain their rated ohmic values. Actual laboratory tests have proved that these vitreousenameled resistors hold their rated resistance under ambient temperatures from +700 F to -70 F.

These General Electric resistors are available in over 1400 combinations of ratings (5 to 200 watts), types, and mountings. Stable operation is but one of their outstanding qualities: They have sufficient terminal strength to hold up to 21 pounds of right-angle pull, and special terminals are available to hold up to 34 pounds. Their vitreous-enamel coating provides resistance to adverse atmospheric conditions.

Like to know more? Ask your General Electric salesman for a free set of sample resistors and test them yourself! And mail this coupon today for the new 36-

page catalog containing complete information on ratings, dimensions and ordering directions.

Industry Control Department, Roanoke, Virginia.

SEND TODAY FOR FREE **RESISTOR CATALOG**

Section 8784-8

General Electric Co., Schenectady, N. Y.

Please send a copy of GEA-6592, G-E Resistor Catalog.

| NAME | |
|---------|-------|
| COMPANY | |
| ADDRESS | |
| CITY | STATE |

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WELL I'LL BE DIPPED...better ...because the NEW AND SNAPIN

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AMP

- Gets leads to the printed circuit board in one assembly operation;
- Eliminates an investment in expensive automation equipment;
- Can be applied to solid or stranded wires;
- Eliminates danger of shorts due to "solder-bridging" of insecure leads;
- Has construction details that promote good capillary flow of solder during the dipping process;
- Is self-retaining, with no damage to the printed circuit board during preassembly operations;
- Is self-aligning—no further positioning or deformation is required.

Write today for additional information on the NEW A-MP SNAPIN, the AMP-EDGE Connector and other A-MP products designed for printed circuit applications.

AMP INCORPORATED

GENERAL OFFICE:

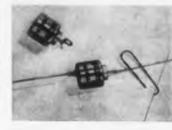
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Distributor in Japan: Oriental Terminal Products Co., Ltd., Tokyo, Japan

CIRCLE 66 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products



Miniature Tantalum Capacitors 175°C

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Miniature tantalum electrolytic capacitors an available for operation over a temperature range from -55 to 175 C. Known as the X T M line, the are being manufactured in six capacities, from 4 to 40 mfd, at nominal working ratings from 40 to 360 v. The body diameter of the metal case (all capacitors) is 5/8 in. with case lengths from 9/16 to 1-25/32 in. All capacities employ a metal-to-glass hermetic seal and offer a choice of 2-1/4 in. axia leads or solder-tab terminals.

P. R. Mallory & Co. Inc., Dept. ED, Indianapolis Ind.

CIRCLE 67 ON READER-SERVICE CARD FOR MORE INFORMATION

Frequency-Period Counter

0 cps-1 mc



This frequency-period counter, model 203A, offers 0 cps to 1 mc direct reading operation for frequency and period (1 freq.) measurement. The counter also serves to measure pressure, temperature, velocity, acceleration, flow, rps, rpm, and displacement with the use of suitable transducers. The instrument may also be used as a secondary frequency standard. It features a continuously adjustable trigger level control which permits ful rated sensitivity at any voltage level between -300 and +300 v. Small voltage increments ordinarily masked by attenuators are easily selected. Simplified color-coded controls and direct read-out in kc, mc, sec, or usec, with automatic decimal point indication are incorporated. Oscilloscope marker signal facilities trigger level adjustment for amplitude discrimination in frequency or period measurement. The counter has a time base range of 10 usec to 10 sec in decade steps (frequency), 1 and 10 cycles (period).

Computer-Measurements Corp., Dept. ED, 5528 A Vineland Ave., No. Hollywood, Calif. Ave

CIRCLE 68 ON READER-SERVICE CARD FOR MORE INFORMATION CIRCL

Magnetic Tape Recorder 300 KC Bandwidth

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Series 3000 Multi-Channel Magnetic Tape Recording System features a 300 kc Band Width. The system accommodates reel sizes up to 14 in. as standard equipment and has a single switch on the front panel which selects any of the six standard speeds up to 60 in. per sec. Module housings provide plug-in facilities for amplifiers, permitting instant selection of direct fm or PDM recording or playback in any combination.

American Electronics, Inc., Dept. ED, 655 W. Washington Blvd., Los Angeles 15, Calif.

CIRCLE 69 ON READER-SERVICE CARD FOR MORE INFORMATION

Ultrasonic Cleaning 50-250 W output



A series of ultrasonic cleaning units ranging in capacity from two quarts upward is available.

Power output ranges from 50 to 250 w. Designed for continuous commercial use, the generator supplies the rated output of electrical energy to a barium titanate transducer. Generators are designed to permit use of two cleaning transducers alternately. One tank may be used for removal of excessive amounts of contamination, and the other tank for final cleaning.

Alcar Instruments Inc., Dept. ED, 17 Industrial Ave., Little Ferry, N.J.

CIRCLE 70 ON READER-SERVICE CARD FOR MORE INFORMATION

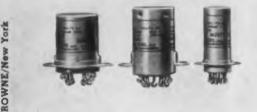


for Air-borne Power Supplies and Other Military and Industrial Applications



Hoffman

CIRCLE 71 ON READER-SERVICE CARD FOR MORE INFORMATION





EXCLUSIVE WITH FILTORS, INC.

PRECISION MACHINED ROTARY REL

STAMPED PARTS IN THE MOTOR. MACHINED PARTS-ONLY ONE OF THE ADDITIONAL QUALITY CONTROL STEPS TAKEN BY FILTORS THE MANUFACTURE OF HERMETICALLY SEALED SUB-MINIATURE RELAYS ... YOUR ASSURANCE OF GREATEST RELIA

WRITE FOR CATALOG, FILTORS, INC., PORT WASHINGTON, LONG ISLAND, NEW YORK, PORT WASHINGTON 7-3850

New Products

Flying Spot Scanner For Test Equipment

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A 5 in. flying spot scanner tube for use in television receiver test equip. ment has been developed. Desig. nated type 5BNP16, the tube employs low voltage electrostatic focus, an aluminized screen of very short persistence, and operates without ion trap for simplified installation. Compared to other tube types designed for studio flying spot scanning pickup equipment, the 5BNP16 is less expensive, approximately 4 in. shorter in over-all length, and operates at lower anode voltages.

Sylvania Electric Products, Inc., Dept. ED, 1740 Broadway, New York 19, N.Y.

CIRCLE 106 ON READER-SERVICE CARD

Cap Nuts

Made of Nylon

A line of cap nuts fabricated from black Nylon comes either knurled or slotted, and may be used with rods or screws or serve as knobs. Nylon fabrication makes the nuts particularly useful where dielectric strength and resistance to corrosion are important. A range of sizes with American Standard threads includes 6-32, 8-32, 10-32 and 1/4-20.

usual Weckesser Co., Dept. ED, 5701 Northwest Highway, Chicago 30, Ill. Fulto

CIRCLE 107 ON READER-SERVICE CARD

Wide-Field Magnifier

For Parts Inspection

A magnifier has been developed that allows the small parts inspector to use both eyes and thus maintain a high degree of efficiency. The widefield magnifier consists of a large oilfilled, plastic-cased lens. The lens is very clear and free of distortion from edge to edge. It will not discolor or become cloudy with age. The magnifier permits an inspector to sit comfortably while the item to be inspected is passed beneath the lens.

Curry & Paxton, Inc., Dept. ED, 866 Willis Ave., Albertston, Long Island, N.Y.

CIRCLE 108 ON READER-SERVICE CARD

CIRCLE 109 ON READER-SERVICE CARD

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Precision Fine Wire 0.004 In. Diam.

Through new methods developed using a centerless grinder, wire can he ground as fine as 0.004 in. diam eliminating the problem of lateral die e for marks which are present in most drawn wire. This is extremely important for electronic tube elements. ploys instrument movements, and similar applications. per-

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The TB-12 centerless grinder used ion Comfor the process will production grind tungsten carbide, titanium, glass, gned wood, hard rubber, ceramics, cork, ickup and other materials. s ex-

Royal Master Inc., Dept. ED, State orter Highway No. 23, Riverdale, N.J.

CIRCLE 110 ON READER-SERVICE CARD

Brazing Alloys

High Purity

Vacuum-tube grade silver and gold brazing alloys have been designed specifically for brazing electronic components in which the concentrates of metallic impurities must be kept to an absolute minimum. The alloys are carbon-free and meet all applicable industry specifications on maximum content of cadmium, zinc and other volatile elements not allowable for vacuum-tube work. They are supplied in wire, strip and sheet form in all the usual gages.

Handy & Harman, Dept. ED, 82 Fulton St., New York 38, N.Y.

CIRCLE 111 ON READER-SERVICE CARD

Reinforced Plastic Sheet Flexible

A flexible grade of reinforced plastic sheet, 1/32 in. thick, with characteristics which make it suitable for such application as transformer layer insulation, is in production. Known as Grade EEF, this insulating material is expected to have use in other components besides transformers. Bulletin No. 101 containing product characteristics is available.

Reinforced Plastics Div., Dept. ED, Hays Mfg. Co., Erie, Pa.

> CIRCLE 112 ON READER-SERVICE CARD CIRCLE 113 ON READER-SERVICE CARD >

OHMITE

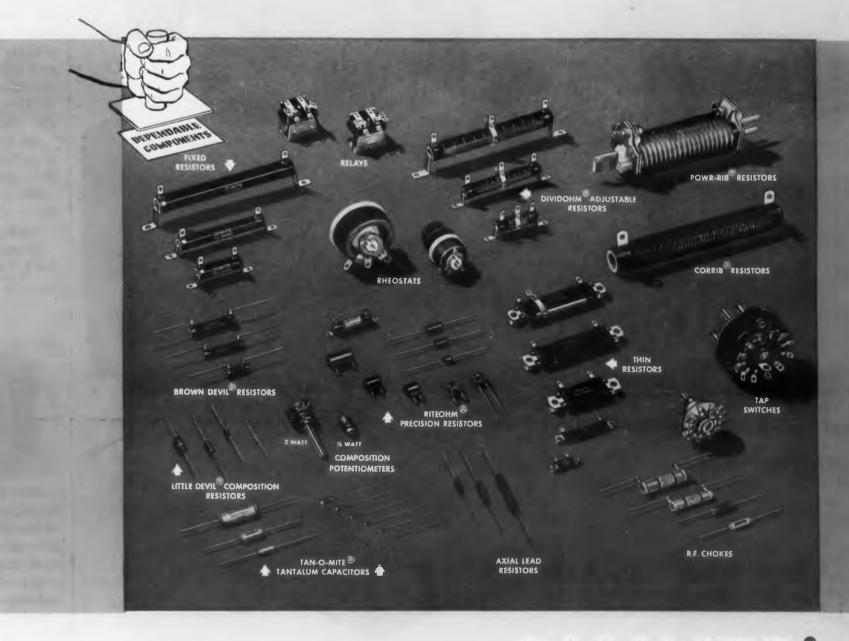
develop more efficient manufacturing processes. All this plus the fact that Ohmite is the world's leading specialist the complete in the manufacture of power-type resistance components -high quality rheostats and wire-wound resistors in the most complete range of sizes and types available to industry. Reliability is also characteristic of Ohmite tap switches, precision wire-wound resistors, molded composiline of tion resistors and potentiometers, general-purpose relays, subminiature tantalum capacitors, and R. F. chokes. Write on company letterhead for the complete Ohmite Catalog and Engineering Manual. industry-preferred COMPONENTS

Long life and dependability are synonymous with the name Ohmite. When you specify Ohmite components ...

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RHEOSTATS • RESISTORS • RELAYS • TAP SWITCHES • TANTALUM CAPACITORS

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thousands of combinations for **REMOTE CONTROL** SWITCHING

rotary SOLENOIDS*

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The variety of Oak switches is almost limitless. Combined with Oak rotary solenoids, they provide an assortment of Rotary Selectors that covers almost any low-current applicationsimple or complex, military or commercial. Oak Rotary Selectors give a positive stepping action, even under severe vibration and shock. To help you get the exact remote-control unit you require, Oak engineers will be glad to work out special recommendations. Write for copies of the Oak switch catalog and rotary solenoid bulletin with time-saving layout sheets.

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low-current

SWITCHES

1260 Clybourn Avenue, Dept. D., Chicago 10, Illinois Phone: MOhawk 4-2222 CIRCLE 78 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Remote Size and Position Indicator Accuracy of 1 Per Cent



Remote indication of position, size, tension. strain, thickness, and other quantities which can be related to minute displacement of a feeler probe, is accomplished with the Model 100 displacement transmitter used with the Model 300 displacement indicator. The system offers accuracy of 1 per cent of scale with three calibrated ranges of ± 0.1 , 0.01, and 0.001 in. full scale. Drift errors are virtually eliminated by a constant current excitation system, stabilized amplifier circuitry, and integral zero and gain checking features.

An auxiliary electrical output is available which is suitable for direct operation of standard strip chart recorders. A wheel attachment is available for continuous thickness measurements of moving material. Operating temperature range is -65 to +200 F.

Daytronic Corp., Dept. ED, 216 S. Main St., Dayton 2, Ohio.

CIRCLE 79 ON READER-SERVICE CARD FOR MORE INFORMATION



Voltage Regulator 400 Cycle, Single Phase

This automatic voltage regulator for 400 cycle, single phase service gives instantaneous correction of line voltage variations with 0.25 v bandwidth for line voltage variations and 0.35 v bandwidth for load current and load power factor changes. The unit is designed for an input of 95-130 v for nominal output voltage of 115 v, adjustable from 110-120 v and a load of 1.0 kva. It has a waveform distortion of 3.5 per cent max at 400 cycles. The power factor rating is from 0.7 lagging to 1.0. The size of the regulators is 7-3/4 x 5 x 14-3/8 in. including front panel handles.

The Superior Electric Co., Dept. ED, 83 Laurel St., Bristol, Conn.

CIRCLE 80 ON READER-SERVICE CARD FOR MORE INFORMATION

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Step Input Unit

Plots Bar Graphs



Data plotting at any number of pre-set increments up to 999 steps along one axis is possible with the model 51 Step Input Unit. The unit provides means for producing bar-type graphs to any scale on standard or non-standard graph paper and visually displays by means of illuminated numbers the content of the mechanism at any point in a test series thus facilitating start and stop operations without losing track of position at any time. Calibration to any scale factor is possible by adjusting both size and number of steps to conform to the data being plotted. Zero may be set at any point.

F. L. Moseley Co, Dept. ED, 409 N. Fair Oaks Ave., Pasadena, Calif.

CIRCLE 81 ON READER-SERVICE CARD FOR MORE INFORMATION

Cannon Electric reduces laminate rejections by 54%

Cannon Electric engineers tested many XXX-P laminates before they chose G-E Textolite 11570 for the insulators in their LK-A53 connectors. By using this laminate the percentage of rejections was reduced from approximately 55% to 1%. This insulator is the most difficult punching part at Cannon. The dimensions—1.998" in diameter, 1/8" thick, 49 holes .067" diameter and 4 holes .128 diameter. The report is superior punching with no cracking between holes, no delamination around holes, and no dimensional change in parts.



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Coaxial Turret Attenuators 30 db

Three new coaxial turret attenuators, Models 705, 706, and 707 offer twelve steps of attenuation in the uhf range from dc to 1500 mc. A single unit can give a maximum of 30 db. Two units can also be used in series to permit a wide range of control in small steps. Designed for either bench use without further mounting, or for mounting into a test equipment package, the turret attenuators are housed in a cast case which is provided with tapped mounting holes. All models use type BNC connectors and have twelve snap-in attenuator pads in a convenient turret arrangement. The units have a zero insertion loss position for use in applications where it is necessary to obtain the full output of the signal source into the load. This zero insertion loss position also provides a convenient point for calibration without physically removing the attenuator. A spring-loaded detent assures alignment of the pad selected. An engraved dial indicates the attenuation values.

Narda Corp., Dept. ED, 160 Herricks Rd., Mineola, N.Y.

CIRCLE 82 ON READER-SERVICE CARD FOR MORE INFORMATION

Textolite 11570 COLD PUNCH LAMINATE

> General Electric Textolite 11570 is a XXX-P, high IR paper-base laminate that can be punched clean in a temperature range of 80° F. to 130° F. This cold fabricating quality, plus outstanding product uniformity, eliminates dimensional variations from piece to piece . . . permitting the use of automatic assembly techniques. The superior electrical and mechanical properties of G-E Textolite 11570 offer many design opportunities to both electrical and electronic manufacturers.

| General Electric Co. Laminated Products Dept. Sec. EDL-77, Coshocton, Ohio | Please send me details of the Cannon Electric Company tests of G-E Textolite® 11570 laminate |
|--|--|
| Please have your representativ | ve call. |
| Name | |
| Title | |
| Firm | |
| Street | |
| | |



CIRCLE 83 ON READER-SERVICE CARD FOR MORE INFORMATION

ALLEN-BRADLEY QUALITY variable resistors

When successful circuit operation depends upon a variable resistor that is not affected by moisture, heat, cold, or age... the Allen-Bradley units are the answer. The solid "one piece" hot-molded structure has insulation, terminals, faceplate, and threaded bushing imbedded in the plastic body. With the resistance element as an integral part of the mold—not an added film or paint —it can be made to satisfy any resistance-rotation curve. Write for full details, today.

Sectional view showing how elements are molded in one integral unit

mmm

HOT-MOLDED

SOLID

in one integral structure

for long life and low noise level

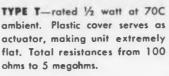
TYPE J—rated 2 watts at 70C ambient. Total resistance values from 50 ohms to 5 megohms. Available in single, dual, and triple units with various types of adjusting shafts, and with built-in line switch.



Allen-Bradley Co., 1344 S. Second St. Milwaukee 4, Wis. In Canada: Allen-Bradley Canada Ltd., Galt, Ont.



TYPE H—rated 5 watts at 40C ambient. Total resistance values from 50 ohms to 2.5 megohms. Good for over 100,000 cycles with no appreciable resistance change. Max. voltage 750 v, d-c.





TYPE F—rated ¼ watt at 70C ambient. Diameter ½". Standard tapers. Slotted shaft. Designed for printed circuits.



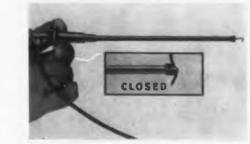
TYPE G—rated $\frac{1}{2}$ watt at 70C ambient. Diameter $\frac{1}{2}$ ". Plain or lock-type bushings; plain or slotted shaft. Available with line switch (right).

ALLEN-BRADLEY RADIO, ELECTRONIC, AND TELEVISION COMPONENTS

CIRCLE 84 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Test Probe Grips Wires



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The Griprobe is a test probe of durable plastic for gripping terminals, tube sockets, lugs, and wires thus freeing the hands of the operator to handle other tools or test equipment. It features an interior spring mechanism which by pressing the thumb, opens the hook-shaped metal probe and, by removing the thumb, closes it in a self-lock grip.

Standard Electronics, Inc., Dept. ED, 5523 Satsuma Ave., Burbank, Calif.

CIRCLE 85 ON READER-SERVICE CARD FOR MORE INFORMATION

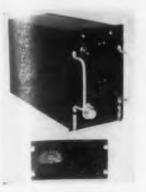
Brushless Converter 1 KVA - 10 KVA



Nobrush, a 40-pole, brushless, 400 cycle converter operates from standard 60 cycle supply. The unit employs a generator, direct coupled to 1200 rpm, 60-cycle synchronous motor. The generator is direct mounted on motor, making the unit two-bearing. With input variation up to 15 per cent, output for steady load, without regulator, will remain within 1 per cent. Any standard voltage, single or three phase, can be supplied. Three phase machines can be loaded asymmetrically, without impairment of performance. For unity power factor, voltage will depart no more than 2-1/2 per cent from slated value for any load within rating of machine. With correction of power factor to high leading value, voltage will hold within better than plus or minus 1 per cent. For other load conditions, or for closer regulation, regulator can be supplied, holding voltage within 1/2 per cent for all conditions of load. Units from 1 KVA to 10 KVA are available.

Georator Corp., Dept. ED, Manassas, Va.

CIRCLE 86 ON READER-SERVICE CARD FOR MORE INFORMATION



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Aircraft Safety Device Monitors Critical Temperatures

Model CTI-10D is powered and operated entirely by magnetic amplifier circuitry, monitoring up to 10 channels of temperature, simultaneously. Balance and sensitivity adjustment enable each channel to be set for any desired critical temperature range and trip point. This point may be set accurately to within 1 per cent of the operating range established. Units comprising a complete temperature-monitoring system are: indicator panel, for mounting in a convenient location clearly visible to pilot or flight engineer; balance and power unit; temperature probes; and interconnecting cabling. Power requirements are 105-125 v, 380-420 cps, 25 w. System accuracy is ±1 per cent under specified environmental conditions. The warning panel measures 5-3/4 x 3 x 3 in.; the balance and power unit, 5-1/8 x 9-1/4 x 19 in.; the total system weighs 15 lbs. The device meets MIL-E-5272 for temperature, acceleration, vibration, altitude and humidity.

Armoux Corp., Dept. ED, 11924 W. Washington Blvd., Los Angeles 66, Calif.

CIRCLE 87 ON READER-SERVICE CARD FOR MORE INFORMATION



Thyratron Xenon Filled

A Xenon filled, 18 amp dc thyratron provides quick starting and wide temperature limits. It is especially designed for motor speed control, resistance welder control, and incandenscent light control. Designated as the NL-5665/C16J, its ratings are: filament volts, 2.5; filament current, 31 amp; maximum peak inverse volts, 1250; maximum peak forward volts, 1000; average anode current, 18 amp; peak anode amp, 100 amp; anode current averaging time 4.5 sec; and filament heating time, 60 sec.

National Electronics Inc., Dept. ED, Geneva, Ill.

CIRCLE 88 ON READER-SERVICE CARD FOR MORE INFORMATION



NATIONAL SCENE

REEFING "ELECTRONIC BRAINS" FROM LOSS OF MEMORY. One of science's greater marvels is IBM's 705 Electronic Data Processing Machine—which makes intricate calculations and logical decisions in millionths of a second. Heart of this electronic "wizard" is its main magnetic core memory. Designed for use with the machine's high-speed printer is the IBM 760 Control and

Storage Unit containing its own core memory of 1,000 positions which allows central processing to continue in the 705 while other data are being printed. Helping the 760 remember what information is to be printed is a job for PHENOLITE® Laminated Plastic. PHENOLITE's unique combination of properties makes it ideal for this application.

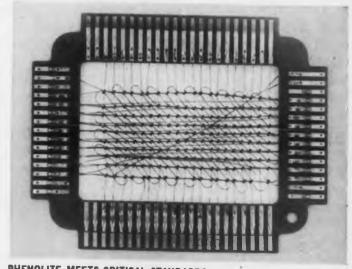


MOST ADVANCED FORM OF ELECTRONIC STORAGE. The 1,000-position core memory for the IBM 760 Control and Storage Unit—a portion of which is shown here—consists of pinhead size cores strung on copper-wired frames of PHENOLITE. Electrical impulses, passing through wires, alter the magnetic state of cores so that a group of them stands for a word or figure. Reversing the process recalls information from storage. PHENOLITE frames safeguard the circuit and permit stacking of core planes as shown.

NATIONAL CAN HELP YOU reduce unit product cost or improve product performance at no added cost. Here's why... You can select the "one best material" from over 100 grades of PHENOLITE, Vulcanized Fibre and National Nylon—without compromise in properties or cost. You can simplify production and purchasing with the timed delivery of 100% usable parts—from a single reliable source. You gain competitively with National's new materials and grades—the direct result of programmed materials-research.

You benefit by calling National first. Check Sweet's PD File 2b/Na, the Telephone Directory Yellow Pages, or write Wilmington 99, Delaware. Dept. E-7.

CIRCLE 89 ON READER-SERVICE CARD FOR MORE INFORMATION



PHENOLITE MEETS CRITICAL STANDARDS. Core frames like the one shown are punched out of laminated PHENOLITE by IBM. Each frame has printed circuit type terminal strips and soldered connections. PHENOLITE proves an ideal material for this application because it is mechanically strong and stiff, punches cleanly, etches well, remains flat, has high dielectric properties and withstands the heat of dip soldering.



NATIONAL FIBRE CO. OF CANADA, LTD., Toronto 3, Ont.

1957

New Products

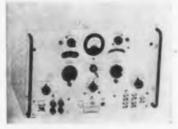


Hexagon Nut Drivers

Miniature Sizes

Starting where normal size nut drives leave off and going down to the no. 00 hexagon nut, this set of nut drivers is available in sizes, measuring across the flats, of 5/64, 3/32, 7/32, 1/8, 5/32 and 3/16 in. Approximate overall length of the nut driver is 2-1/2 in. Drivers are available in sets containing their individual permanent plastic handles, and also in replaceable sets with a swivel type jewelers handle.

Hunter Tool, Dept. ED, Box 564, Whittier, Calif. CIRCLE 90 ON READER-SERVICE CARD FOR MORE INFORMATION



Signal Generator 900-2100 Mc

The SHF Signal Generator (Model SG-161) operates over a frequency hand from 900 to 2100 mc, with an accuracy of better than 1 per cent, providing signals for a variety of measurements on radar and communications receivers. It can be used to energize slotted lines for vswr measurements and to measure conversion gains of receiver front ends, while its low residual rf leakage makes possible overall receiver gain measurements at fractional microvolt levels. Either cw or pulse modulated output may be obtained and the output continuously varied between 0.2 and 200,000 mv into a 50 ohm load. The signal generator provides for a choice of either internally or externally generated pulses for modulation of Klystron oscillator tube. Circuits and controls are included for adjusting the repetition rates and width of pulsed rf signals when such signals are derived from the internal modulator. The internal modulator may be operated either free running or synchronized with pulse or sine wave signals from an external source. In addition to the rf output signal, the SG-161 also provides two separate output synchronizing signals for external use in synchronizing pulsed rf signals with external equipment.

Transitron, Inc. Div. of Van Norman Indus., Dept. ED, 186 Granite St., Manchester, N.H.

CIRCLE 91 ON READER-SERVICE CARD FOR MORE INFORMATION

MICROWAVE PROGRESS

At this time, in place of our usually scheduled scientific discussions, we'd like to introduce our specially skilled field representatives to you. These men are highly qualified engineers, capable and willing to sit down with you to discuss any microwave equipment problems you may have. They'll see to it that your problems are answered promptly and completely.

Washington State J. K. Dooley Co. 3215 Western Avenue Seattle 1, Washington Murdock 8313

Mid-Atlantic Gawler-Knoop Co. 178 Eagle Rock Avenue Roseland, New Jersey Digby 4-2997

> 835 Glenside Avenue Wyncote, Pennsylvania Waverly 7-1820

8726 Colesville Road Silver Spring, Maryland Juniper 5-7550

Rocky Mountains Elton Kelley 336 East Fourth Street Loveland, Colorado Normandy 7-1376

Midwest Kenneth W. Meyers 1 South Northwest Highway Park Ridge, Illinois

Talcott 3-3174 New England and Upstate New York Technical Instruments, Inc. 971 Main Street Waltham 54, Mass. Twinbrook 3-1400

> 218 Harrison Street Syracuse, New York Granite 1-7870

174 Grayton Road Buffalo, New York Atwater 5095

119 Ann Street Hartford, Conn. Jackson 5-4846 PRD West Coast Sales Office 737-41 North Seward Street Suite 7

Hollywood 38. California Hollywood 5-5287 TWX LA1101



We've expanded our production runs to fill the increasing demand

for our catalog products. Delivery on these items can now be made within 30 days (at the outside) from receipt of order.

The listing on the opposite page is a partial rundown of the PRD items in stock and available for immediate delivery.

If you don't see the product you want, contact our Engineering Representative nearest you (see Microwave Progress column), or write directly to us.

P.S. We will always maintain the same high standards of product quality that started this increasing demand in the first place.

Be sure your name's on our mailing list for:

- PRD Catalog . . complete descriptions and specifications on PRD's microwave equipment. NEW CATALOG COMING SOON!
- PRD Reports ..., internationally famous, authoritative professional papers that give practical information on virtually every aspect of microwave research and engineering.

CIRCLE 92 ON READER-SERVICE CARD FOR MORE INFORMATION

PRD MICROWAVE TEST EQUIPMENT READY FOR IMMEDIATE DELIVERY!

| PRODUCT | PRD TYPE # | FREQUENCY RANGE (kmc/sec) |
|---|-------------|------------------------------|
| Vaveguide Termination | 116-A | 8.2 to 12.4 |
| ixed Coaxial Attenuator | 130 Series | 2.0 to 10 |
| ixed Coaxial Attenuator | 1100 Series | DC to 4.0 |
| oaxial Termination | 145-A | 0 to 4.0 |
| recision Dial-Gauge Attenuator | 185-B | 7.0 to 10.0 |
| recision Dial-Gauge Attenuator | 192-A | 26.5 to 40.0 |
| recision Dial-Gauge Attenuator | 195-B | 8.2 to 12.4 |
| hielded Uncalibrated Variable Attenuator | 154-A | 8.2 to 12.4 |
| recision Dial Attenuator | 196-C | 8.2 to 12.4 |
| recision Dial Attenuator | 196-D | 8.5 to 9.6 |
| ariable Cutoff Attenuator | 180-A | 8.2 to 10 |
| Precision Coaxial Slotted Section | 200-C | 1.0 to 4.0 |
| Precision Coaxial Slotted Section | 205-A | 4.0 to 10.0 |
| Precision Waveguide Slotted Section | 201-A | 3.95 to 5.85 |
| Precision Waveguide Slotted Section | 203-E | 8.20 to 12.4 |
| Precision Waveguide Slotted Section | 212-A | 26.5 to 40.0 |
| totary Standing Wave Detector | 219 | 100 to 1.000 mc/s |
| Broadband Probe | 250-A | 1.00 to 12.4 |
| Standing Wave Amplifier | 277 | 350 to 2500 cycles |
| Vaveguide Slide Screw Tuners | 303-A | 8.2 to 12.4 |
| Double Stub Tuner | 306-A | 2.0 to 10.0 |
| -H Tuner | 313-A | 18.0 to 26.5 |
| Naveguide-to-Coaxial Adapter | 354-B | 8.2 to 12.4 |
| Naveguide-to-Coaxial Adapter | 356-A | 5.4 to 8.2 |
| Directional Coupler | 401 | 7.05 to 10.0 |
| Directional Coupler | 402 | 8.5 to 9.6 |
| -Plane Bend | 462 | 8.2 to 12.4 |
| I-Plane Bend | 463 | 8.2 to 12.4 |
| Frequency Standard Multiplier | 500 | 3.25 to 10,000 mc/s |
| Heterodyne Frequency Meter | 504 | 100 to 10,000 mc/s |
| Precision Direct Reading Frequency Meter | 559 Series | 8.20 to 10.0 |
| Precision Direct Reading Frequency Meter | 570 Series | 26.5 to 32.0 |
| Calibrated Precision Frequency Meter | 560-S1 | 2.7 to 3.7 |
| Calibrated Precision Frequency Meter | 583-D | 2.4 to 3.7 |
| Direct Reading Frequency Meter | 585 Series | 8.2 to 10.0 |
| Tunable Crystal and Bolometer Mount | 621-A | 18.0 to 26.5 |
| Bolometer | 610-A | 0 to 12.4 |
| Coaxial Tunable Crystal and Bolometer Mount | 612-A | 1 to 10 |
| Broadband Coaxial Bolometer Mount | 627-A | 0.5 to 10 |
| Broadband Coaxial Bolometer Mount | 628-A | 0.5 to 10 |
| Broadband Bolometer | 631 Series | 0.5 to 10 |
| Waveguide Thermistor Mount | 643-A | 8.2 to 12.4 |
| Waveguide Thermistor Mount | 646 | 5.4 to 8.2 |
| Universal Power Bridge | 650-B | |
| Shielded Tube Mount | 702 | 8.50 to 9.66 |
| Universal Klystron Power Supply | 801-A | |
| Klystron Power Supply | 809 | |
| VHF-UHF Noise Generator | 904 | 30 to 1000 mc/s |

Polytechnic Research & Development Co., Inc.

202 Tillary Street • Brooklyn 1, N. Y. • Tel: UL 2-6800 Cable Address: MICROWAVE, NEW YORK Teletype: Home Office: NY-23157 • Western Office: LA1101

CIRCLE 92 ON READER-SERVICE CARD FOR MORE INFORMATION



Subminiature Relay High Contact Rating

This subminiature relay has full 1/8 in. silver or palladium contacts, which handle 3 amps resistive load standard and 4 amp intermittent. The basic design incorporates a permanent magnet in an electro-magnetic circuit of high efficiency and performance. This arrangement provides the extra armature torques necessary to overcome high contact pressures and actuate large contacts. Relay is constructed with a balanced armature having no pivots, hinges or bearings.

Three types are available. Model M-1000A is a dc spdt relay with standard pull-in 1/2 w. Vibration resistance is 10 g to 2000 cps. Greater sensitivity can be achieved by derating the vibration resistance to 500 cps. The standard coil for 24 v operation has a 550 ohm resistance, with special coils available up to 10,000 ohms. Model M-1000AA has identical characteristics except that pull-in power is 2/3 w, and vibration resistance is 30 g to 500 cps and 20 g to 2000 cps. Model M-1000P is a twoposition de polarized relay for use as a versatile control element. This relay provides sensitivities from 15 mw to 500 mw, and 2 to 3 amp contact rating. Vibration resistance is 10 g's to 2000 cps with 500 mw models and 10 g to 500 cps with the more sensitive models. Coils are available to 10,000 ohms.

Luther Mfg. Co., Dept. ED, 7312 Varna Ave., No. Hollywood, Calif.

CIRCLE 93 ON READER-SERVICE CARD FOR MORE INFORMATION



Precision Gears For Servo Systems

Spur, spring and clutch gears, and bevel and miter gears are among the types available, especially for servomechanism use. Presently in stock for immediate delivery are 48- and 64-pitch spur gears, in tooth multiples of 8 and 10, with 14-1/2 deg pressure angle, and minimum and maximum pitch diameters of 9/16 in. and 4 in. respectively. Stock gears have clump hubs with 1/4 in. bores.

Helipot Corp., Dept. ED, Newport Beach, Calif. CIRCLE 94 ON READER-SERVICE CARD FOR MORE INFORMATION





... specify Centralab Metallized Ceramics

Centralab offers you unmatched facilities and experience to produce fired or pressed-on metallized components for all your mechanical and electrical uses.

Steatite bodies with low-temperature seals or High Alumina components with special high-temperature alloy seals are available.

Properly matched metal-ceramic combinations facilitate brazing . . . prevent bake-out. And integrally formed metals and ceramics minimize destructive motion and vibration, maintain close tolerance, and provide excellent electrical characteristics.

Centralab offers you modern facilities and the services of ceramics specialists to help improve your product's efficiency.

Send your inquiry to Centralab today. And ask for Bulletin 42-221 showing complete facilities.

Centralab

A DIVISION OF GLOBE-UNION INC. 960G E. Keefe Ave. Milwaukee 1, Wis. In Canada: 804 Mt. Pleasant Road, Toronto, Ontario

Discuss your special requirements with your Centralab representative CIRCLE 95 ON READER-SERVICE CARD FOR MORE INFORMATION

74

New Products

Floated Integrating Gyros Measuring 1 In. Diam



Known as series 101G, these gyros retain all of the precision construction of the larger series of the company's floated gyros, the 2-in. 201G and the 3-1/2-in. HIG-5. Measuring 1 in. in diam, the new gyros are fully floated to keep friction and uncertainty torques to low levels and to give the unit resistance to vibrational shock. Trimmed drift rates as low as 0.1 milliradians/sec can be expected. Both signal generator and torque generator are provided for use in closed-loop operation, and a range of impedances and sensitivities are available to meet specific requirements.

The unit is arranged in a flanged housing for easy mounting, with the input axis located by a notch in the flange. Power requirement is less than 1/3 w. Connections are made through 11 pin plugs at each end of the gyro. Total weight exclusive of connectors is 3-3/4 oz.

Reeves Instrument Corp., Dept. ED, 215 E. 91st St., New York 28, N.Y.

CIRCLE 96 ON READER-SERVICE CARD FOR MORE INFORMATION



Measuring 3 4 in. diam x 3/4 in. long, this 2 w precision wirewound potentiometer is composed of a one piece anodized aluminum housing securing a low loss phenolic terminal board and winding assembly. Shaft torque is 0.05 oz-in. standard, 0.02 ozin. on special request. Independent linearity of 1 per cent is standard, better linearity can be provided. The precision potentiometer is available in a servo mounting, 75-M27, or threaded bushing, 75-M7, with a selection of shaft lengths.

Maurey Instrument Corp., Dept. ED, 7924 S. Exchange Ave., Chicago 17, 11.

CIRCLE 97 ON READER-SERVICE CARD FOR MORE INFORMATION

GREATER VERSATILITY IN SUMMING ANGULAR SHAFT POSITIONS. The Hollow Shaft design reduces bread-board and production costs by eliminating the need for stocking custom shaft lengths. Can be installed or removed without disassembly of differential or instrument. Small size, low inertia, high accuracy. Write for complete specifications.

Hollow Shaft Differential



Librascope Mechanical Computer Components

Sine-Cosine Mechanism

INSTANTANEOUS, ACCURATE ANGLE RESOLVER FOR ANA-LOG COMPUTERS. The Sine-Cosine Mechanism is a precision device that permits the conversion of angular motion into a linear displacement. This displacement is proportional to the sine or cosine of the angle of input rotation. It is designed to solve range, beating and vector resolution computations. Its features include low friction, high accuracy, and simplicity of installation. Write for complete specifications.

IBRASCOPE

Librascope, Inc. 808 Western Ave. Glendale, Calif.

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CIRCLE 99 ON READER-SERVICE CARD

HOW PRINTED CIRCUITRY BECAME A MAJOR PRODUCT AT CRONAME

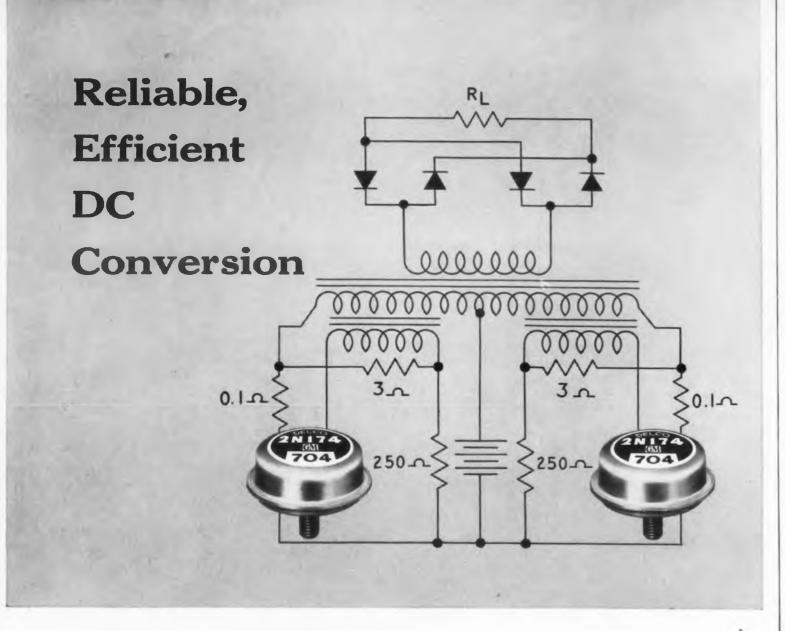
A few short years ago circuitry was confined to our research laboratories. NOW, EVERY DAY thousands and thousands of etched and plated circuits are produced at CRONAME for America's leading radio, television, electronic, instrument, automotive and appliance manufacturers. For over 50 years CRONAME has been accepted by industry as a superior source for decorative metal and glass parts, nameplates, grilles, control panels, bezels, escutcheons, jack covers, TV masks and assemblies. With the advent of Printed Circuitry, CRONAME'S vast experience in precision etching, plating, silk screening and lithographing on metal was called upon to lead the way for a new electronic era.

This experience has met the challenge. Our precision quality and service in the infant Printed Circuitry industry has brought an acceptance of our circuits exceeding many of our older products. Our new Printed Circuitry Division geared for volume production will share a major portion of our new facilities now under construction. Your acceptance of our products has made this expansion inevitable. We would like to help you improve your product now. Write for literature.



1957

CINCINNATI · CLEVELAND · CHICAGO · DETROIT · INDIANAPOLIS · LOS ANGELES · LOUISVILLE · MINNEAPOLIS · NEW YORK · PHILADELPHIA · SYRACUSE · CRONAME (CANADA LTD., WATERLOO, QUEBEC



Industry's Highest Power Transistors

Low saturation voltage of Delco Radio 2N173 and 2N174 opens new opportunities for converter economy, efficiency and reliability

The excellent electrical characteristics of Delco High Power transistors permit the conversion of low DC voltage to higher DC voltage-with a high degree of efficiency-in a wide range of applications. This proved performance offers greater reliability than will be found in corresponding vibrator circuits.

The low saturation voltage of Delco 2N173 and 2N174 transistors also reduces their internal power dissipation in conversion applications to an insignificant degree so that little selfheating is apparent. The result is an overall economy which permits converters of smaller size . . . important in many applications.

DELCO RADIO

| Alpha cutoff frequency | 0.4 | 0.4 |
|---|------|------|
| Power dissipation | 55 | 55 |
| Thermal gradient from junction to mounting base | 1.2° | 1.2° |
| Distortion (Class A, 10 watts) | 5% | 5% |

TYPICAL CHARACTERISTICS

2N173 2N174

12 Volts 28 Volts

12

80

0.7

38

0.4

12

60

0.7

38

DIVISION OF GENERAL MOTORS KOKOMO, INDIANA

Properties (25°C)

Maximum current

Maximum collector voltage

Saturation voltage (12 amp.)

Power gain (Class A, 10 watts)

CIRCLE 100 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Explosion-Proof Cases

For Airborne Equipment



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This line of explosion-proof cases, to house air. borne electronic equipment, is designed for use in an environment of explosive atmosphere. Flame and explosion arresting characteristics meet test procedure 2 of Military Specification MIL-E-5272A. Weighing about 10 per cent more than standard MIL-C-172B cases, these units fit shock mounting racks listed on military standard sheet MS91405 of the same specification. Thirteen case volumes are available.

Churchill Lighting Corp., Dept. ED, 344 Franklin St., Melrose 76, Mass.

CIRCLE 101 ON READER-SERVICE CARD FOR MORE INFORMATION



Oscillogram Reader For Data Reduction

This Oscillogram Reader reads opaque or translucent oscillograms, automatically correcting for nonlinearity in the record, and prepares data for recording by plotting, type-writing, tap-perforating, or card-punching devices. Either linear or nonlinear calibration is possible without overlays. Curves may be quickly and accurately traced. Editing, notating, and reading are all possible over the entire area of the exposed record. X and Y motions are separately inhibitable. This equipment is incorporated into a desk-type console 54 in. wide and 59 in, high and constructed of walnut and formica panels on a metal frame. The 12 x 14 in. exposed reading area accommodates records 13 in. wide with a roll diam of 6 in. Other specifications include a 40-400 count per inch resolution, total travel ± 999 counts, and accuracy calibrated to ± 0.010 .

Telecomputing Corp., Dept. ED, 16217 Lindbergh St., Van Nuys, Calif.

CIRCLE 102 ON READER-SERVICE CARD FOR MORE INFORMATION



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Wire-Wound Resistors Vitreous Enamel

These wire-wound axial-lead resistors offer compact size and are designed to withstand high temperatures. A vitreous enamel coating affords environmental protection. Standard tolerances are ± 5 per cent for 50 ohms and higher and ± 10 per cent for below 50 ohms. Power ratings are based on temperature rise of 300 C in free air with ambient temperature of 40 C. Available in 3, 5 and 10 w ratings for up to 50 K.

Hardwick Hindle Inc., Dept. ED, 40 Hermon St., Newark 5, N.J.

CIRCLE 103 ON READER-SERVICE CARD FOR MORE INFORMATION



Coaxial Switch Direct Scope Measurements

This coaxial switch transforms an ordinary oscilloscope into an instrument that takes accurate, quantitative measurements, offering the simultaneous display of two channels or voltages on an oscilloscope. The high-speed switch unit utilizes two Clare "Mercury-Wetted" switch elements mounted in a coaxial circuit. The switching unit has a maximum current rating of 5 amp at 500 v and can be supplied for either 50 or 75 ohms with a vswr of less than 1.08 from 0 to 250 mc. The switching functions are controllable by circuitry at a 30, 15, or 10 cps rate, locked with the 60 cycle line. A phase reverse switch and a phasing control are provided for adjusting the phase in respect to the line. By switching rf energy up to 250 mc, it is possible to use one detector for the reference circuit, as well as for the unit being tested. This avoids the possibility of error caused by non-identical detectors. Suggested applications for the unit are: measurement of attenuation-0 to 250 mc; measurement of amplifier gain-0 to 250 mc; measurement of return loss (vswr); comparison of production unit with standard-up to 250 mc; general purpose oscilloscope switch; display of diode or transistor characteristics; square wave generator.

Jerrold Electronics Corp., Dept. ED, 23rd & Chestnut Sts., Philadelphia, Pa.

CIRCLE 104 ON READER-SERVICE CARD FOR MORE INFORMATION

MANY FACTORS CONTRIBUTE TO LOW INSTALLED COST OF SOUTHCO DRIVE RIVETS...

ECONOMICS OF FASTENING COVERS FULL CYCLE FROM INVENTORY REQUIREMENTS TO FINISHED PRODUCT

Designers who specify fasteners realize the many considerations that enter into cost determination. While ease of installation is often the most important feature, other factors affect costs. It may be difficult to put a dollar value on availability, for example, but serious financial losses do occur when production is held up or shipping dates are missed because of a slow fastener delivery. Being able to ship from stock, as Southco does, helps avoid production delays.

ELIMINATION OF SPECIAL TOOLS



QUICKLY SET



To install, Southco Rivets are placed in drilled hole. The pin is then driven with a hammer. Installation is complete. No bucking is required.

Down time due to special tool

failure and maintenance of special

fastening tools are two fastening

costs which are eliminated by Southco Drive Rivets. The only

tool required is a hammer . . . any kind of a hammer . . . claw or ball,

and size is not important. The

number of men on a Southco

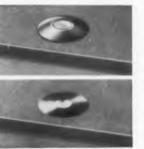
riveting job is never limited by the

number of special tools on hand

and in working order.

Expanded prongs force parts together. Pin is locked securely into rivet by displaced metal filling unique grooves. Compression forces are utilized for greater strength,

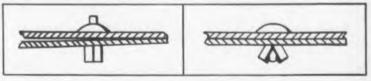
NO FINISHING OFF, NO WASTE



©1957

Impact of hammer seals pin neatly in rivet. No part of the rivet is cut off and discarded. No time-consuming filing, grinding or polishing is necessary. No scrap to clean up.

AUTOMATIC "PULL-UP" ACTION ASSURES TIGHT JOINT



Even when adjacent surfaces are separated, parts are forced together by Southco Rivet action, then held tightly in compression.

WIDE RANGE OF APPLICATION



Southco Drive Rivets are used to secure metal to metal or metal to wood. They are equally adaptable to blind or open applications. In each, they are quickly set and grip tightly. New PLY-HEAD* rivet permits higher loading of "soft" materials such as plywood, plastics and composition.

AVAILABLE IN ALUMINUM OR STEEL

Southco Rivets are supplied in aluminum or cadmium plated steel. The aluminum rivets have either cadmium plated or stainless steel grooved pins. The steel rivets have cadmium plated steel grooved pins.

Standard head designs are Universal or Countersunk. Full Brazier heads are available in popular sizes. New PLY-HEAD river rounds out line.

| DIAMETERS | LENGTHS | NOMINAL GRIPS |
|-----------|----------------|---------------|
| 1/2 " | 1/a " to 1/2 " | 1/22" to 1%2" |
| 5/32 m | 7/12" to 3/4" | 1/16" to 5/2" |
| 3/16 " | 1/a " to 3/4 " | 1/2" to 5/8" |
| 1/4 H | 7/12" to 3/4" | 1/16" to 5/8" |

| DIAMETERS | LENGTHS | NOMINAL GRIPS |
|-----------|----------------|--|
| 1/8 " | 1/8 " to 1/2 " | ½ [#] to ¹³ ½ [#] |
| 3/16 " | 1/4 " to 3/4 " | ³ ½ [#] to 5⁄8 [#] |
| 1/4 " | 1/4 " to 3/4 " | ³ ∕2 [#] to 5∕8 [#] |

FREE FASTENER HANDBOOK ... Send for your free copy of Fastener Handbook No. 7, just released. Gives complete engineering data on these and many other specialty fasteners. 52 pages, in two colors. Write on your letterhead to Southco Division, South Chester Corporation, 235 Industrial Highway, Lester, Pa.



CIRCLE 105 ON READER-SERVICE CARD FOR MORE INFORMATION

PROBLEM:

Provide a reliable memory storage facility for digital computers . . . high speed, absolute dependability, compact size essential.

SOLUTION:

Magnetic Core Memory Planes by General Ceramics . . . far exceeded the requirements, won immediate acceptance of leading computer manufacturers.

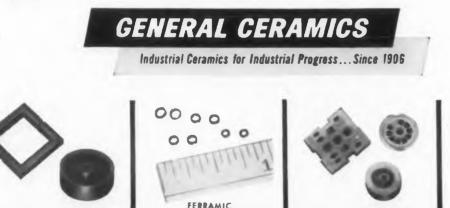
Completely Assembled Coincident-current Magnetic Memory Planes for Computers, Switching and Automatic Control Systems

General Ceramics

FERRAMIC[®] MAGNETIC MEMORY PLANES

Utilizing Ferramic Magnetic Memories resulted in important increases in reliability, speed and accuracy in actual operation. In addition, designers found space requirements sharply reduced. Lower power consumption, lighter weight, elimination of heat dissipating devices and greatly reduced maintenance were other significant improvements.

General Ceramics Magnetic Memories offer a solution to similar problems in automatic control systems for conveyors, elevators, telephony, production machines, processing equipment and signalling. For further details, write General Ceramics Corporation, Keasbey, New Jersey. Please address inquiries to Dept. ED.



FERRAMIC CORES





TEMPERATURE SEALS CIRCLE 72 ON READER-SERVICE CARD FOR MORE INFORMATION



Completely assembled standard type memory frames available from stock. Memory Frames of special design can be produced to your specifications.



SOLDERSEAL TERMINALS

Digital Clock

New Products

Time Source



This digital clock is a multiple output unit designed to serve as a time source for data loggers, data handling systems, computers, digital time displays and other applications where a digital representation of time is required. It also functions as a twenty-four hour program controller, providing a contact closure for every minute of the day. The output is a parallel, decimal contact closure pattern, based upon twenty-four hour time, i.e., 2:26 PM is represented as 14:26. As many as three completely independent parallel outputs can be supplied in one unit. Designed for 19 in. wide relay rack mounting, the digital clock requires 3 1/2 in. of panel height. The depth behind the panel is 12 in. Top and bottom covers are removable, permitting full access to all components. The clock utilizes printed circuit techniques for the digital circuitry; no stepping switches are used.

Supply voltage is 110-120 v, 60 cycle, as standard; other voltages and frequencies are available. Power consumption is 6 w continuous with peak power requirements of 200 w. Average power is about 7 w.

Chrono-Log Corp., Dept. ED, P.O. Box 4587, Philadelphia 31, Pa.

CIRCLE 73 ON READER-SERVICE CARD FOR MORE INFORMATION



Battery Eliminators 6 v or 12 v

The model "A" Battery Eliminator is designed for use with transistor or vibrator operated auto radio sets. It provides 6 v or 12 v dc output operation at negligible ripple current, featuring 8 position voltage control voltmeter, ammeter, and completely automatic operation.

American Television & Radio Co, Dept. ED. 300 E. 4th St., St. Paul, Minn.

CIRCLE 74 ON READER-SERVICE CARD FOR MORE INFORMATION

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Delay Line 100 µsec Delay

The model F-186 delay line has a delay of 100 μ sec with low attenuation and is tapped every 2 μ sec. At the full delay of 100 μ sec, the risetime is 5.5 μ sec and the attenuation is 1.4 db. The characteristic impedance is 2000 ohms. The unit comes in a hermetically sealed box with dimensions of 10-1 2 long x 4 wide and 6-3/8 in. high. Twenty-five tap terminals are brought out on each of the 10-1 2 x 6-3/8 in. sides for total of 50 taps. The d.lay line can be cascaded with additional units to provide longer delays. Four such units will provide a delay of 400 μ sec with a risetime of 17 μ sec and an attenuation of 6 db. The unit is provided with study for mounting.

Control Electronics Co., Inc., Dept. ED, 1925 New York Ave., Huntington Station, N.Y.

CIRCLE 75 ON READER-SERVICE CARD FOR MORE INFORMATION



Phase Angle VTVM Measures Phase and Magnitude

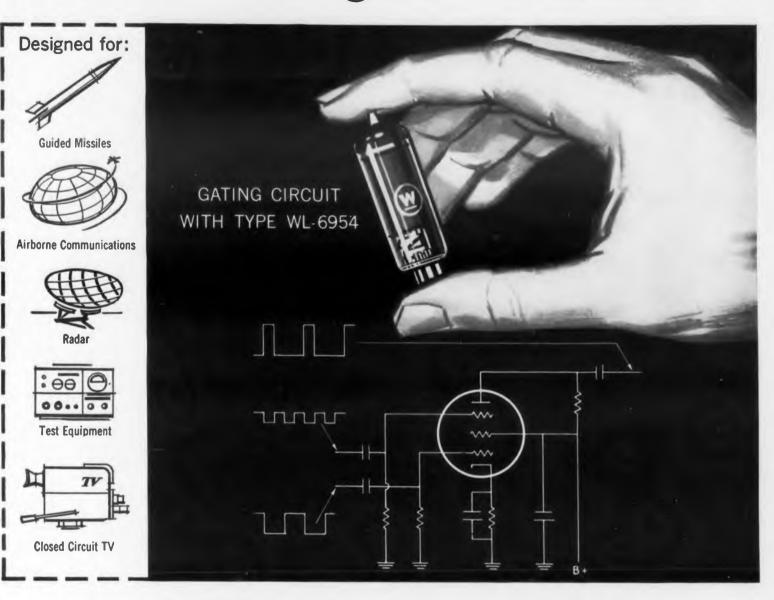
This VTVM includes a phase sensitive rectifier which can measure both magnitude and phase of a signal as well as perform other test functions. It permits measurement of 400 cps signal phase angles, $E \cos \Theta$, $E \sin \Theta$ and vector sum. Measurements are unaffected by quadature. Total harmonic rejection can be obtained by optional filters in signal and/or reference channels. Factory modifications adapt the instrument to 60, 1000 cps and other frequencies. Major applications are phase sensitive null indication, testing synchros, servo-mechanisms, magnetic amplifier carrier amplifiers, notch networks and transducers.

As a conventional VTVM, measurements are 1 mv to 300 v full scale at frequencies of from 10 cps to 50 kc.

North Atlantic Indus., Dept. ED, Instrumentation Div., 603 Main St., Westbury, L.I., N.Y.

CIRCLE 76 ON READER-SERVICE CARD FOR MORE INFORMATION

Now! Simplify pulse-forming circuits with new Westinghouse **WL-6954**



NEW SHARP CUT-OFF DUAL-CONTROL PENTODE OFFERS EXCEPTIONALLY HIGH TRANSCONDUCTANCE

The new Westinghouse WL-6954 is a 7-pin miniature pentode designed for application in Military and Industrial equipment as a gating, coincidence, mixing or delay tube.

Built to high standards of reliability, it meets MIL-E-1C vibration test specifications. It permits simplification of pulse-forming circuits and has the advantage of high transconductance from Grid 3 to Plate.

The WL-6954 is available in production quantities



CIRCLE 77 ON READER-SERVICE CAR

ELECTRONIC TUBE DIVISION . ELMIRA, N. Y.

for immediate delivery. It's one more reason why when you want highest quality tubes for Military or Industrial purposes—you'll find it wise to check Westinghouse.

| | al Eng. Dept., Electronic Tube Div. Duse Electric Corp., Elmira, N. Y. |
|--------------------------|---|
| Please send WL-6954 p | l me complete data on your new sentode. |
| NAME | |
| COMPANY. | |
| ADDRESS_ | |

79



Bring transistor circuits to life in a matter of minutes with the Sprague LF-1 Transimulator. This new instrument lets you simulate any amplifier stage, a-c or direct-coupled, short of high power audio output; also multivibrator, switching, phasing, push-pull, Class A and B, and many others using cross-coupled Transimulators ... whether the circuit is common or grounded emitter, base, or collector ... whether the transistors are PNP, NPN, or Surface Barrier. You can simulate circuits stage-by-stage for cascade operation ... or use a separate Transimulator for each stage to get simultaneous multi-stage operation.

Bring Circuit Diagrams To Life In Minutes

Everything you need for RC amplifier circuits is built right into the LF-1, including coupling capacitors bias and load resistors ... battery voltage supplies Base Collector-Voltage Divider stabilization circuits ... 5-way binding posts for transformer coupling and metering.

Whether you're designing audio circuits or switching circuits, you'll get a true picture of operating parameters minutes after you've drawn the circuit diagram ... without wasting valuable time with breadboard and soldering gun.

Pays For Itself In A Matter Of Weeks

An ideal laboratory instrument, Transimulators are inexpensive enough to justify several on every bench. You can even use the LF-1 to test transistors in the circuit... the only real proof of design parameters. And a complete step-by-step instruction manual makes operation fast, simple, and easy.

CIRCLE 114 ON READER-SERVICE CARD FOR MORE INFORMATION

FEATURES OF THE LF-1 TRANSIMULATOR

- TRANSISTORS—PNP and NPN Junction, and Surface Barrier.
- CIRCUITS Common or Grounded Emitter, Base, Collector.
- RANGE-Audio, up to 100 kc.

output, almost any con-

nection required.

- TRANSISTOR POWER—Through medium power audio output. • BATTERY SUPPLY—Separate bias and load. 1.5, 3, 4.5,
- 6 volts d-c. Polarity Reversing Switch. COUPLING—2 µf and 20 µf Direct, and Ext. C. posts,
- on both Input and Output.
- BIAS RESISTANCE-Up to 555,000 chms continuously variable
- . LOAD RESISTANCE-Up to 277,500 ohms continuously
- variable. • EMITTER RESISTANCE—Up to 2,500 ohms variable. Series resistor and bypass capacitor can be added.
- BASE COLLECTOR STABILITY-Up to 250,000 ohms variable. Series resistor and bypass capacitor can be added.
- VOLTAGE DIVIDER STABILITY Up to 50,000 ohms variable.
- 5-WAY BINDING POSTS—For meters, transformer coupling, external supply voltage, degeneration, bypass, coupling, signal input and



SPRAGUE PRODUCTS COMPANY, NORTH ADAMS, MASSACHUSETTS

New Products

Slide-Back VTVM 0.05 Per Cent Accuracy



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The TS-E6 is a slide-back VTVM which meas ures dc voltages in two ranges. The first range from 0.01 to 110 v, and the second range from 110 to 1100 v. An accuracy of 0.05 per cent is maintained on both ranges. The equipment operates equally well on 60 cps and 400 cps at 110 v ac. The maintenance and cycling time on the TS-E6 is held to a minimum because the meter contains a built-in standard cell for instant on-the-spot calibration. This unit contains no motor or stepper-switches that can burn out and complicate maintenance problems.

Accuracy of measurements is in no way dependent upon the deflection sensitivity of the meter movement, since it is a zero current operated device; the meter is used strictly as a null indicator.

George Vincent McMahon, Dept. ED, 381 W.7th St., San Pedro, Calif.

CIRCLE 115 ON READER-SERVICE CARD FOR MORE INFORMATION



Digital Tachometer Accurate to 0.001 RPM

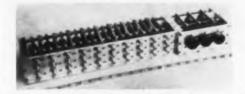
Accuracy of this instrument is only limited by read-out method employed, and can be better than 0.001 rpm, with a scale of zero to 10,000 rpm. Output can be by sharp pulse or sine wave with signal set 1 to 100 per revolution. The tachometer is available with either single-ended or feed-through shafts, for mounting on drive pads.

Nacimco Products, Inc., Dept. ED, 2300 National Ave., National City, Calif.

CIRCLE 116 ON READER-SERVICE CARD FOR MORE INFORMATION



Video and Pulse Switch Up to 4.5 Mc



This rotary switch, No. 5583, is designed for use at frequencies up to 4.5 mc, and is intended for video and pulse switching. The electrical characteristics of this switch call for DPDT operation of 10 separate circuits with very strict isolation requirements. The 10 rear decks of this switch are all completely isolated from each other by the use of sectional shielding and rf grounding fingers. Each of these 10 decks is also designed to eliminate capacitive or inductive coupling effects within each deck. The three front decks of this unit are used for switching filament voltages, line voltages and B plus voltages, etc. The entire switch is silver plated; all contacts and wipers are of coin-silver to minimize contact resistances. Overall dimensions are 4 1/2 x 3 x 22 in.

The Daven Co., Dept. ED, Livingston, N.J. CIRCLE 117 ON READER-SERVICE CARD FOR MORE INFORMATION

Programmer Counter Control of Test Limits

The Programmer Counter is used to turn on and off test apparatus whose limits are sensed by strain gages, thermocouples or any other transducers that have a maximum output not exceeding 100 mv dc. The unit eliminates the need for manual control of test cycling and simplifies the setting up of equipment each time a test is to be made. It is a precision, millivolt electronic relay having adjustable energizing and release thresholds and DPDT 15 amp contacts. Its two adjustable, stable thresholds provide for precise selection of upper and lower operating limits and a counter, which may be of the preset type, registers each cycle. The instrument operates on 110 v ac. Other models provide up to ⁵ sets of adjustable limits with automatic switching by preset counters. A signal of a flashing light or ringing bell can be supplied to indicate when the counter is registering.

Spar Eng. & Devel. Inc., Dept. ED, Wyncote, Pa. CIRCLE 118 ON READER-SERVICE CARD FOR MORE INFORMATION

NICKEL PINS-GOLD PLATED FOR LOW CONTACT RESISTANCE AND FREEDOM FROM CORROSION. BUTTON STEMS-STRENGTH IN ALL. PLANES WHY BENDIX* HY-G-300 ELECTRON TUBES ARE BEST FOR EXTREME SHO

| WHY BENDIX* HY-G-300 ELECTRON | TUB | ES ARE | | 0 | E FRO | M ST | OCK |
|---|-------------------|------------------------------|------------------|-------|------------------------|--------------|-----------------------------|
| | Bulb Size | Dbl. Triodes Volt Amp. | R.F. Pentodes | Gate | Rectifiers FullWave | Beam | Power Triodes Passing |
| TUBES ARE BEST FOR EXTREME SHOCK, | T-12 | - | - | - | - | - | 6080WB 6082A |
| | T-11 | - | - | - | - | 6384 6889 | - |
| WIDDATION AND TEMPEDATUDEOL | T-9 | - | - | - | 6853 | - | - |
| VIBRATION AND TEMPERATURES! | T-6½ | 6851 6854 6900 | 6582A | 6486A | 6754 | 6094 | 6877 6900 |
| | Retma Type No. | Retrofit For | Generic Type | Ę | 14 | Bulb | Bendix Type No. |
| From the standpoint of design features (see above), these reliable hard glass tubes | 6080WB | 6080 6080WA | 6080 | 6.3 | 2.5 | T-12 | TE-46 |
| offer the superior quality needed to survive today's severe environmental demands. | | - | 6AQ5- 6005 | 6.3 | 0.6 | T-6½ | TE-18 |
| Specifically, Bendix HY-G-300's are designed to withstand the following environmental conditions—bulb temperatures up to 300° C; vibration up to | 6853 | 6106 5Y3 | 5Y3 | 5.0 | 1.7 | T-9 | TE-45 |
| 20G's over the range of 5-2000 cycles; and shock of 200G's having 20-millisecond | 6384 | 6AR6 6098 | 6AR6 | 6.3 | 1.2 | T-11 | TE-27 |
| duration. | 6854 | 6385 | 2C51 5670 | 6.3 | 0.5 | T-6½ | TE-47 |
| For full information about the HY-G-300 line the surest answer to electron | 6486A | 6486 | 6AS6 | 6.3 | 0.25 | T-61/2 | TE-43 |
| tube applications in jet aircraft, missiles and rockets write RED BANK DIVISION, | 6582A | 6582 | 6AK5 | 6.3 | 0.25 | T-6½ | TE-44 |
| BENDIX AVIATION CORPORATION, EATONTOWN, NEW JERSEY. *TRADEMARK | 6754 | 412A | - | 6.3 | 1.0 | T-61/2 | TE-36 |
| West Coast Sales and Service: 117 E. Providencia, Burbank, Calif. * Export Sales and Service: Bendix | 6851 6877 | 5751 | Half of | 6.3 | 0.5 | T-61/2 | TE-42 TE-48 |
| International Division, 205 E. 42nd St., New York 17, N. Y Canadian Affiliate: Aviation Electric, | 6900 | 5687 | 6080 5687 | 6.3 | 0.9 | T-61/2 | TE-54 |
| Ltd., P. O. Box 6102, Montreal, Que. | 6889 | - | 1001 | 6.3 | 1.2 | T-11 | TE-54 |
| | 6082A | 6082 | 6082 | 26.5 | 0.6 | T-12 | TE-55 |

Red Bank Division



CIRCLE 119 ON READER-SERVICE CARD FOR MORE INFORMATION

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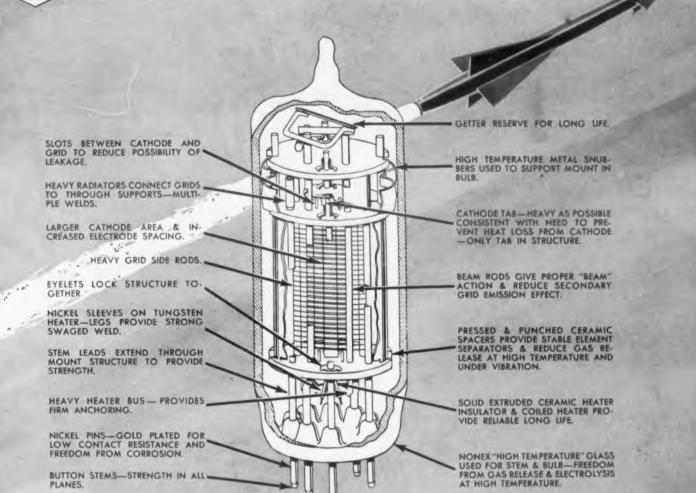
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1957

ELECTRONIC DESIGN . July 15, 1957

ELECTRON TUBES FOR SURVIVAL



Do your transistors have temperature problems?

... solve them with



thermistors



Minimize Ico variation and prevent thermal runaway by using Globar thermistors. They are available in a wide range of resistance values and temperature coefficients to meet most transistor circuit requirements.

Globar Thermistor Test Kits are available for general evaluation in transistor circuits. If you have a specific transistor temperature problem, submit details to GLOBAR Division, The CARBORUNDUM Company, Dept. ED 87-711, Niagara Falls, New York. Ask for Technical Bulletin GR-3... describes physical and electrical characteristics of GLOBAR Thermistors.



Over 30 years' experience in the field of special ceramic resistance devices CIRCLE 120 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Variable Power Supply 0.01 Voltage Variation



Model 700-A 1.5 amp power supply, features less than 500 mv ripple, less than 0.01 output voltage variation from no load to full load, and uses 5-1/4 in. of rack height. Voltage across the series tubes is kept constant by a secondary feedback loop, while the primary feedback loop controls the output voltage. Varying the line voltage, changing the load, or manually varying the output voltage does not affect the average series tube dissipation. As a result, the regulator does not lose regulation with a full 1.0 amp step change in load.

Harrison Labs. Inc., Dept. ED, Berkely Heights, N.J.

CIRCLE 121 ON READER-SERVICE CARD FOR MORE INFORMATION



Salt Spray Test Chamber Lucite Construction swit

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An All-Lucite test chamber is used for determining salt fog corrosion resistance of materials and components. The chamber, when connected to a low pressure air supply produces fine mist, and reaches test conditions within 15 min. Specimens to be tested are then suspended from Lucite hanger rods which are supplied with the chamber. Bulkier components can be placed on the bottom of the chamber supported by rods to avoid contact with the salt solution. The Lucite construction assures complete visibility from all angles of the test in progress. The unit is equipped with temperature controllers and indicators for both the chamber and the air saturation tower. Dimensions of the chamber are 20 x 20 in.

Assoc. Testing Labs., Dept. ED, 412 Clinton Road, Caldwell, N.J.

CIRCLE 122 ON READER-SERVICE CARD FOR MORE INFORMATION

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Waveguide Switches Rotary Channel Type

This miniature waveguide switch provides switching of signals from any one of three positions te either of the remaining two and will not change to another position upon failure of its power supply. The characteristics of the 1 x 0.5 in. OD size switch include a frequency range of 8500 to 9600 mc with a maximum vswr of 1.10 and a minimum isolation of 40 db. The maximum switching time is 0.25 sec. for 240 deg operation and 0.15 sec. for 120 deg operation. It operates at 3 amp maximum at 28 v dc nominal and employs 20 lb of pressurization throughout. Available in Xs and X_L band series, Airtron switches are of the rotary channel type using a circular bend in the rotor and a broadband internal choke design. Other frequency bands and special designs can be supplied. The three position switch can be designed with the circular bends in the H plane on special order.

Airtron, Inc., Dept. ED, Linden, N.J. CIRCLE 123 ON READER-SERVICE CARD FOR MORE INFORMATION

Packaged Filter & Blower Reduced Size



Packaged blowers are available in several sizes to utilize the minimum of valuable panel height in an electronic rack by designing the filter and blower section to protrude into the normally unused base section of the rack. The blower is normally the bottom component on a relay rack. Models 2P408 and 2Q408 require 5 1/4 in. of panel height but have the performance of Model 2E408 blower which is 7 in. high throughout, and will dissipate at 1.5 kw heat load with an air temperature rise of 10 C. A total of 25 models are available.

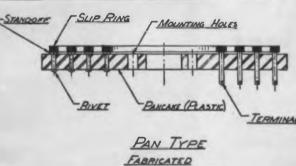
McLean Engineering Labs., Dept. ED, 70 Washington Rd., Princeton, N.J.

CIRCLE 124 ON READER-SERVICE CARD FOR MORE INFORMATION

SLIP RING ASSEMBLIES



General Purpose Slip Ring Assemblies are those which are used in relay, lighting and power supply circuits. These circuits are characterized by lack of sensitivity to external electrical influence induced by electro static or electro magnetic fields from other circuits. Another usual characteristic of these assemblies is their limited power handling require-



ments. For higher current and power requirements, the rings are usually classified as power rings.

Design techniques have been developed for small size and light weight. These are drum type, pan type, and electro formed assemblies.

The drum type are brushed on the surface bounded by the outside diameter. Another drum type ring is brushed on the flat surface. In this instance the brushes project between the ring surfaces.

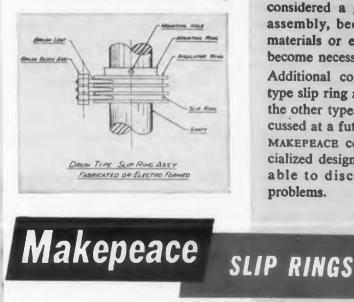
Pan type construction consists of a concentric, nested set of rings on one plane.

It is relatively easy to make electro formed rings of the first mentioned drum type and the pan type, and they perform well as general purpose rings. However, choice of materials is limited. The fabricated type construction will be superior and will surpass all the usual requirements of general purpose rings over the electro formed construction for universal applications.

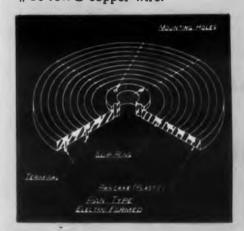
Fabricated ring stacks are metal rings separated by plastic laminate insulators. The plastic laminate should be treated with an insulating varnish to seal the machined edges against the entrance of moisture. The rings may be continuous and machined from plate stock or stamped from sheet. The standard hardness for the rings is 125 BHN minimum.

> Brush contact materials for slip rings are usually sintered silver-graphite; the silver provides the low contact and brush resistance, and the graphite provides lubrication for long wear.

As the brush moves with respect to the ring, and with current flowing from brush to ring



(or vice versa), there are variations in current flow resulting from the imperfect contact between the moving elements of the circuit. Even for general purpose slip ring applications, this current variation is kept to a minimum by proper selection of compatible materials. The resistance variation seldom exceeds .005 ohms for double contacts on a ring. This is equivalent to about 1 ft. of #16 AWG copper wire.



General purpose rings are usually limited to slow rotating speeds, not more than 1,000 rpm or less than 1,000 feet/minute. If this speed is exceeded, the assembly is no longer considered a general purpose ring assembly, because special brush materials or even air cooling may become necessary.

Additional considerations for this type slip ring assembly come under the other type assemblies to be discussed at a future time.

MAKEPEACE complete staff of specialized design engineers are available to discuss your slip ring problems.

CIRCLE 125 ON READER-SERVICE CARD FOR MORE INFORMATION

D. E. MAKEPEACE COMPANY Attleboro, Mass.

ENGELHARD INDUSTRIES

ELECTRONIC DESIGN . July 15, 1957

83

"Normalizing" relieves internal stresses, prevents core movement and physical damage such as spreading at the butt joint when subjected to high-temperature operation or encapsulation.

"Normalizing" Hipersil[®] Cores holds magnetic values constant

Westinghouse has licked the bugaboo of heat in transformer treatment and operation. "Normalizing," a process exclusive with Hipersil cores, relieves internal stresses in the core structure.

Both exciting current and inductance "stay put" when a transformer is built around a "normalized" Hipersil core. Thus, magnetic values remain constant (within practical limits) even when the transformer is cast or encapsulated in high-temperature resin, or operated at high temperatures.

Electronics industry demands are ideally met with Hipersil cores. Smaller, lighter transformers result from such revolutionary core properties as oriented grain direction, with 100% coincidental flux; lowest possible core volume for high-temperature transformers; highest permeability, lowest loss; and 100% flux-carrying activity. These values, plus the extra magnetic stability added by "normalizing" make Hipersil the preferred core for more efficient, compact transformers... at lower cost.

Also available from Westinghouse: a complete line of both Hipermag* and Hiperthin* cores for every electronic application.

For extra profits from your production, send for the Type "C" Hipersil Core Design and Application Manual. Write to Westinghouse Electric Corporation, P. O. Box 868, Pittsburgh 30, Pennsylvania. ^{•Trade-Mark}J-70799







Both "normalized" and un-"normalized" cores record the same exciting current before encapsulation in high-temperature resin.



"Normalized" Hipersil core shows exciting current unchanged after encapsulation.



Un-"normalized" core, with the same applied voltage, records considerably higher exciting current after encapsulation.

New Products



Wiring Duct Snap Slot

This plastic wiring duct, which requires no special fasteners, features a snap-in open slot design allowing wires to be installed in the duct with lugs already attached. The snap-in design eliminates operation of threading wire through duct holes. To insert a wire, the plastic finger separating the slots is pulled out, laid in the duct, and the finger released. A duct cover is snapped in place on the duct after wires are laid. The duct is also available in an overlapping closed-slot design which allows wire insertion over full length of the duct with no dead spots. Duct and cover are non-flammable dark grey vinyl plastic meeting J.I.C. specifications. Cutting is easily accomplished with snips or ordinary wood cutting tools.

Panduit Co. Dept. ED, 10132 S. Washtenaw Ave. Chicago 43, Ill.

CIRCLE 127 ON READER-SERVICE CARD FOR MORE INFORMATION



Miniature Magnetic Pickup No Physical Contact

A magnetic pickup, Model 3055, provides minimum weight and size with a maximum voltage output. Weighing about 4 grams, the pickup is a sensitive transducer which translates the movement of ferrous objects, without physical contact, into measurable ac voltage. The output, proportionate to the rate of the object's movement, can indicate motion, torque, rpm and vibrations.

Heart of the pickup is an Alnico magnet which energizes a pole device surrounded by a coil of wire. The pickup creates an external magnetic field, which when interrupted or distorted by the movement of an external ferrous metal object, generates the ac voltage. Operable in temperatures up to 250 deg F., the pickup has a 7/8 in. overall length and 1/4 in. diam. Six inch output leads are provided. The mounting end of the pickup has been threaded to screw into a 1/4 in.-40 NFS tapped hole.

Electro Products Labs., Inc., Dept. ED, 4501 N. Ravenswood Ave., Chicago 40, Ill.

CIRCLE 128 ON READER-SERVICE CARD FOR MORE INFORMATION

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Magnetic Potentiometer 0.5 Per Cent Linearity

A magnetic potentiometer for transmitter and/or receiver in servo systems. Directly interchangeable with may for models of synchro's for increased reliability, and offering infinite resolution. No electrical contacts, slip rings, etc. Output is linear with shaft rotation to better than 0.5 per cent. One to ten turn models are available in standard servo mountings from 0.937 in. and larger.

Instrol Inc., Dept. ED, 722E. Gutierrez St., Santa Barbara, Calif.

CIRCLE 168 ON READER-SERVICE CARD FOR MORE INFORMATION



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Sub-Miniature Terminals Direct Assembly to Panels

The terminals, measuring 0.17 in. diam x 1/4 in. outside height x 1/16 in. inside height, have a Teflon coated outer insulator, and are available in either feed-through or turret head styles. They can be assembled directly to the panel, thereby allowing unlimited patterns and eliminating the necessity of soldering in headers.

Sphere Co. Inc., Dept. ED, Eagle Rock Bldg., 25 Amity St., Little Falls, N.J.

CIRCLE 169 ON READER-SERVICE CARD FOR MORE INFORMATION



Analog to Digital Converter 70 Counts per Sec

Model 100A has an accuracy of ± 1 count and readings as high as 70 per sec. Input is 0 to 130 v. Unit supplies power for external scale changing amplifier. It can be used as a counter, timer or an events per unit time instrument. Contains decimal point locater and both decimal and binary coded output. Four digit 0.01 per cent accuracy models are also available.

Electronic Computer Co., Dept. ED, 6191 Ridge Ave., Philadelphia 28, Pa.

CIRCLE 170 ON READER-SERVICE CARD FOR MORE INFORMATION

Regulated dc power supplies

with unique features that simplify and speed research

model 3-150B

FITS INTO SMALL AREA OF

Size: 51/4"x19" panel-9"

Output: 0-300 V.D.C. continu-

Regulation: 105-125 V. line: 0.15%; NL to FL: 100 MV change.

150W...SMALL SIZE, WIDELY

Output: 500 V.D.C. at 300 MA

Regulation: 105-125 V. line:

Ripple: 0.1% change below 10 MV RMS for any rated

Size: W: 5"; L: 121/2"; H: 53/8"

ternal changes.

0.5%; NL to FL:

voltage or load.

above deck.

- adjustable by simple in-

ously variable without

switching. Current: 0-150

bulletin 1020

RELAY RACK

depth.

MA.

model 5-300XA

ADJUSTABLE

model IK-500B



WIDE RANGE, HIGH PERFORMANCE Output: 3-1000 V.D.C. continuously variable without switching. Current: 0-500 MA. Output current needs no derating throughout full range. Regulation: 105-125 V. line: 400 MV change; NL to FL: 800 MV change. bulletin 1021

model .6-IMB



FOR TRANSISTOR AND STRAIN GAUGE CIRCUITRY Output: 0-60 V.D.C.; current: 0-1 amp. Provides full output current throughout entire range with no derating. Regulation: 105-125 V. line: 0.1%; NL to FL: 20 MV change. Recovery: NL to FL: 0.5 millisecond; FL to NL: 0.25 milli-

second.

bulletin 1024

model D3-300E



| | MANY POWER SUPPLIES IN A COMPACT PACKAGE |
|---|--|
| | Outputs: 0-300 V.D.C. at 0-300 MA; 0-300 V.D.C. at 0-150 MA—both continuously vari- able without switching. |
| | Bias voltage 0 to -145/155 V.D.C. at 0.5 MA. Low ripple on D.C. outputs. 0.10 V.A.C controlled by Powerstat. |
| | Size: 8 ³ / ₄ " x 19 " panel – 17" depth. |
| _ | bulletin 1022 |

model .28-5MXR



28-V.D.C. -- 5 AMPS -- **REGULATED BY MAG. AMPL** You get the dependability and

long life of a magnetic amplifier in this unit. Regulation for 105-125 V. line: \pm .25V.; NL to FL: \pm 0.5V. Size: 4" wide, 12¹/₂" long, 7" high.

bulletin 1019

Each unit features simplified design, highest quality components, easy-to-trace wiring, and ample working room under the chassis. Components are derated to run cool and last longer. Write for literature on any or all models.

bulletin 1017



CIRCLE 171 ON READER-SERVICE CARD FOR MORE INFORMATION

Important leurt FROM TRANSISTOR CENTER, U.S.A.

PHILCO Transistors

| ALL DECK | - | |
|----------|--------------------------|--|
| | | MINIATURE LOW LEVEL AUDIO TRANSISTORS (25 mw) |
| P | 2N207 | general purpose micro-miniature low level transistor, typical beta of 100, 15 db maximum noise figure |
| ACTUAL | 2N207A | 10 db maximum noise figure version of 2N207 |
| JILL | 2N207B | 5 db maximum noise figure version of 2N207 |
| | T0031 | 50 volt version of 2N207 |
| _ | | Special versions of the 2N207 to selected beta ranges are available. |
| | | HIGH FREQUENCY, HIGH GAIN (MICRO ALLOY) TRANSISTOR |
| | T1166 | combines high frequency response with high gain for general purpose high frequency applications and switching circuits, typical f_{max} 60 \mbox{mc} |
| | | HIGH FREQUENCY SILICON TRANSISTORS (150 mw) |
| | T1025 | general purpose, 10 mc silicon transistor |
| a | T1159 | high speed silicon switch for speeds up to 5 mc characterized by ex- tremely low switch resistance |
| | | HIGH FREQUENCY SURFACE BARRIER TRANSISTORS |
| ACTUAL | SB100 2N344/ SB101 | general purpose, minimum $f_{max} = 30$ mc, beta over 10.5 general purpose, good beta control (11-33) |
| | 2N345/ SB102 | general purpose, higher beta (25-110) |
| 11 | 2N346/ SB103 | general purpose, higher minimum f _{max} (60 mc) |
| | 2N128 | general purpose, with military specifications, beta 19-66, minimum f _{max} 45 mc |
| | 2N129 | general purpose, with military specifications, beta over 11.5 |
| | 2N240 | switching transistor, $f_{\alpha b} > 30$ mc |
| | 2N299 | for tuned amplifiers, military specifications, 20 db minimum power gain at 10 mc, minimum f _{max} 90 mc |
| | 2N300 | for video amplifiers, 50 mc minimum current gain bandwidth product, f_{max} over 85 mc |
| | T1050 | high frequency transistor for 50 mc oscillator mixers and 10-15 mc bandpass amplifiers, 22 db typical power gain at 10 mc |
| | | Other types with special parameter controls are available. |
| n – | | MEDIUM POWER ALLOY JUNCTION AUDIO TRANSISTORS (100 mw) |
| | 2N223 | 39-120 beta driver transistor |
| ACTUAL | T1000 | 45-85 beta version of 2N223 |
| SIZE | T1001 | 70-120 beta version of 2N223 |
| | 2N224 | high gain output transistor, 2N225 is a matched pair |
| | 2N226 | medium gain version of 2N224, 2N227 is a matched pair |
| 11 | | Versions of the 2N224 with various beta ranges and higher betas are available singly or in matched pairs. |
| D | | AUDIO POWER TRANSISTORS |
| | T1040 | 40 volt, 7 watt power transistor, thermal drop 3°C/w maximum |
| | T1041 | 40 volt, 10 watt power transistor, thermal drop 2.5°C/w maximum |
| 1 | LI 167 | 60 volt, 12.5 watt power transistor |
| 1000 | T1168 | · · · |
| | 11106 | B0 volt, 12.5 watt power transistor |

Proven performance of Philco Hermetically Sealed Transistors has made them the basis for design in commercial and military applications where reliability is the major consideration. Philco transistors range from the world's smallest germanium transistors now in production to silicon transistors with excellent performance at temperatures from -60° C to $+150^{\circ}$ C.

Philco produces a wide range of transistors designed for special applications in accordance with customer requirements. The Philco Micro-Alloy Transistor is in production. Specifications and design quantities are available. New and exciting transistor types, such as the Philco Micro-Alloy Graded Base Transistor, are now in development. In keeping with our policy, specifications will be made available as soon as these units reach pilot production and are available in design quantities.

Make Philco your prime source for complete transistor application information... write to Lansdale Tube Company, Dept. 1-2, Lansdale, Penna.

Regional offices—Merchandise Mart Plaza, Chicago 54, Ill.—10589 Santa Monica Blvd., Los Angeles 25, Calif.

New Products

Twin Triode Oscillator 470 to 890 Mc Use

The 3AF4-A is a medium-mu twin triode of the seven-pin miniature type designed especially for use as an oscillator in tuners of uhf television receivers, covering the frequency range from 470 to 890 mc. It is like the popular 6AF4-A but utilizes a 3.2 v/450 ma heater having controlled warm-up time. The 3AF4-A features a small mount structure with small elements to provide low interelectrode capacitances; short internal leads to reduce lead inductance and resistance; silver-plated base pins to minimize losses caused by skin effect at the ultra-high frequencies; and double base-pin connections for both plate and grid. The double connections are arranged so as to facilitate use of the 3AF4-A with either series of parallel resonant lines.

Radio Corporation of America, Dept. ED, Electron Tube Div., Harrison, N.J.

CIRCLE 132 ON READER-SERVICE CARD

Strain Gage Bridge

Operates Off Line Voltage

Indicators and recorders available in the 10 my range work in well with the B-1 bridge without the need for further amplification. Because the B-1 operates off the line rather than batteries, there is power to drive higher resistance gages fully and thereby get increased sensitivity. The bridge handles SR-4 strain gages and similar transducers, and drives indicators, recorders, and oscilloscopes. Dc power on the bridge is regulated. One feature of the B-1 is the use of higher resistance internal bridge arms. These go in series with the external gages on the two arm connection, and thereby give practically double the output for the same gage current that would be obtained with the internal arm equal to the resistance of the external arm.

Ellis Associates, Dept. ED, Box 77, Pelham, N.Y.

CIRCLE 133 ON READER-SERVICE CARD

← CIRCLE 134 ON READER-SERVICE CARD

LANSDALE TUBE COMPANY DIVISION

O CORPORATI

LANSDALE, PENNSYLVANIA



General Purpose, Low Frequency

| | | | | imum Re | | | |
|--------------------------|--|------------------------|-----|--------------------|-------------------|------------------------|------------|
| Manufacturer and Type | Class and Application | W _c (mw) | | (a)mw/C (b)C/mw | | l _c (ma) | βοια |
| Amperex Electroni | c Corp., Hicksvillo, N. T. | | | | | | |
| 2N284 | p-n-p, alloy, hi-current switch | 1671 | 75 | | 32 | 250 | 45 |
| 2N284A | p-n-p, alloy, hi-current switch | 1671 | 75 | | 60 | 250 | 45 |
| OC65 | p-n-p, alloy, hearing aid | 50 | 1 | 1.54(a) | 10 | 10 | 30 |
| 0666 | p-n-p, alloy, hearing aid | 50 | | 1.54(a) | 10 | 10 | 47 |
| 2N109/2N217 | p-n-p, alloy, audio driver, out. | 125 | | 2.5(a) | 32 | 70 | 70 |
| 2N279 | p-n-p, alloy, audio pre-amp. | 1 | | 2.5(a) | 30 | 10 | 40 |
| 2N280 | p-n-p, alloy, audio driver | | | 2.5(a) | 30 | 10 | 75 |
| 2N281/2N2822 | p-n-p, alloy, audio output | 167 | | 3.33(a) | 32 | 125 | 70 |
| 2N283 | p-n-p, alloy, audio | | | 2.5(a) | 32 | 10 | 55 |
| | uston Export Co., Ltd. | | | | | | |
| Rugby, Warwickshi | re, England | | | | | | |
| GT1 | p-n-p, alloy | 50 | 654 | 1.25(a) | -9 | -10 | |
| GT2 | p-n-p, alloy | 50 | 1 | 1.25(a) | 1 | 1 | |
| GT3 | p-n-p, alloy | 50 | | 1.25(a) | | | |
| GT11 | p-n-p, alloy | 25 | | 0.75(a) | | | |
| GT12 | p-n-p, alloy | 25 | | 0.75(a) | | | |
| GT13 | p-n-p, alloy | 25 | | 0.75(a) | | | |
| CBS-Hytron, Lowell | , Mass. | | | | | | |
| 2N180 | p-n-p, alloy, gen. purp. | 2505 | 75 | 3(a) | -30 | | 60 |
| 2N181 | p-n-p, alloy, gen. purp. | 250 | 75 | 5(a) | -30 | | 60 |
| Fratco Inc., Pittsbur | gh, Pa. | | | | | | |
| 2N34 | p-n-p, fused, lo-pwr., lo-freg, | 50 | 30 | | -25 | +8 | 0.98 |
| 2N35 | n-p-n, fused, lo-pwr., lo-freg. | 1 | 1 | | +25 | -8 | 0.98 |
| 2N36 | p-n-p, fused, lo-pwr., lo-freg. | | | | -25 | +8 | 45 |
| 2N37 | p-n-p, fused, lo-pwr., lo-freq. | | | | 1 | 1 | 30 |
| 2N38 | p-n-p, fused, lo-pwr., lo-freq. | | | | | | 15 |
| General Electric Co | ., Syracuse, N. Y. | | | | | | |
| 2N43 | p-n-p, fused, audio | 150 | 100 | 2(a) | -20 | 50 | 50 |
| 2N43A | p-n-p, fused, audio | 1 | 1 | _(u) | Ĩ | 1 | 50 |
| 2N44 | P-n-p, fused, audio | | | | | | 22 |
| 2N45 | p-n-p, fused, audio | | | | | | 12 |
| 2N186 | p-n-p, fused, audio out. | 75 | 85 | 1.25(a) | -25 | 200 | 24 |
| 2N186A4 | p-n-p, fused, audio output | 180 | 85 | 3(a) | -25 | 200 | 24 |
| 2N1876 | p-n-p, fused, audio output | 75 | 1 | 1.25(a) | 1 | 1 | 36 |
| 2N187A4 | p-n-p, fused, audio output | 180 | | 3(a) | | | |
| 2N1884 | | | | | | | 36 |
| 2N188A4 | p-n-p, fused, audio output p-n-p, fused, audio output | 75 180 | | 1.25(a) 3(a) | | | 54 54 |
| 2N189 | p-n-p, fused, audio driver | | | 1.25(a) | -25 | 50 , - | |
| 2N190 | p-n-p, fused, audio driver | 75 | 03 | 1.23(a) | -25 | 50 15 | - 24 36 |
| 2N191 | | | | | | 3 | |
| 2N191 | p-n-p, fused, audio driver | 1.4 | | | | | 54 |
| 2N192 2N241 | p-n-p, fused, audio driver p-n-p, audio | 100 | | 3(a) | | 200 | 75 73 |
| 2N241A | | | | | 1 | | |
| | p-n-p, audio | 180 | 85 | 3(a) | -25 | 200 | 73 |
| 2N265 | p-n-p, alloy, audio | 75 | | 1.25(a) | -25 | 50 | 110 |
| 2N319 | p-n-p, audio | 200 | | | -20 | 200 | 36 |
| 2N320 2N321 | p-n-p, audio | 200 | 85 | | -20 | 200 | 54 |
| | p-n-p, audio | 200 | 85 | | -20 | 200 | 73 |
| 2N322 2N323 | p-n-p, audio p-n-p, audio | 75 | 85 | | -16 | 50 | 36 |
| 4JD1A17 | | 75 | | | -16 | | 54 |
| 2N324 | p-n-p, fused, audio p-n-p, audio | 150 75 | | | -20 -16 | | 40 75 |
| General Electric Co | | | | | | | |
| London, England | op = 140 op | | | | | | |
| GET3 | p-n-p, alloy, audio | 150* | 55 | 5(a) | -12 | -50 | 50 |
| GET4 | p-n-p, alloy, audio | 1 | 1 | 1 | -30 | 1 | 1 |
| WHI- | | | | | | | |
| GET6 | p-n-p, alloy, audio | | | | -12 | | |
| | | 200 | | 1 | | 350 | 40 |
| GET6 | p-n-p, alloy, audio p-n-p, alloy, audio p-n-p, alloy, switch | 200 250 | | 1 | -12 -30 -40 | 350 500 | 40 15 |

| Char I _{co} (µa) | nacter NF (db) | istics C _c (μμf) | f _{co} (Mc) |
|---|--|-----------------------------------|--|
| 4.5 4.5 5 4.5 5 4.5 4.5 4.5 2 | 15 15 9 9 15 10 8 15 4 | | 0.35 0.35 0.45 0.47 0.35 0.3 0.3 0.3 0.35 0.5 |
| -5 | 12 12 12 | | 0.8 ³ 0.9 1 4 6 9 |
| 10 10 | 12 12 | 25 25 | 0.6 0.6 |
| -12 | 50 50 40 | | 0.27kc |
| 15 | 22 10 22 22 15 | 40 | 1.0 |
| 16 | 15 10 10 10 | 35 35 35 25 35 | 0.8 1.0 1.0 1.2 1.2 |
| 16 | 15 | 35 | 0.8 1.0 1.2 1.5 1.3 |
| 16 16 16 | | 35 35 35 | 1.3 1.3 3 3 3 |
| 16 | | 35 35 40 35 | 3 3 1 3 |
| 67 | 9 9 6 | 60 42 | 1.5 1.3 |

A Survey of Transistor **Characteristics**

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N THE past eight years since the discovery of transistors at the Bell Telephone Laboratories, great strides have been made in raw material handling and transistor production techniques. This survey of the present state of junction transistor technology is a digest of many reports present in the literature.

Available Gain Per Stage

The amplification from a transistor depends upon the configuration in which it is operated. The transistor may be used as a voltage gain device (grounded base), as a current gain device (grounded collector), or as a power gain device (grounded emitter). These gains per stage, neglecting interstage loss, are approximately as follows:

| grounded base | 30 db |
|--------------------|-------|
| grounded collector | 20 db |
| grounded emitter | 40 db |

The grounded base configuration is essentially a voltage gain device; the grounded collector configuration is a current gain device; while the grounded emitter configuration must be considered a power gain device.

The input and output impedance of the three configurations are radically different and may therefore be used for impedance matching. The order of magnitude of these impedances are listed in Fig. 1.

These impedances vary with the termination at the other end and may be varied over approximately an order of magnitude. The impedance levels may also be adjusted with the proper use of feedback.¹ An unbypassed emitter resistor in the grounded emitter configuration will increase both input and output impedances. A feedback path from collector to base in this configuration will de-

¹Riddle, R. L., "Hybrid Parameters for Grounded Emitter Amplifiers with Feedback," Electronic Design, April 1, 1956.

With heat sink at 25 C.
 Matched pair of 2N281's.

6 v.

3. Grounded base. 4. Storage. 5. With heat sink.

7. At $V_c =$ 8. At 25 C.

42 1.3 65 1.0

ELECTRONIC DESIGN • July 15, 1957

6. Matching not required for class B push-pull.

4t - 1

R. L. Riddle Haller, Raymond and Brown, Inc.

State College, Penn.

crease both input and output impedances. A combination of these forms of feedback may be used for impedance stabilization.

Frequency Response

There are two effects in a transistor which tend to limit the upper frequency response. They are the transit time of minority carriers across the base region, and the capacity of the collector junction. The capacity of the collector junction is similar to the plate capacity of vacuum tubes and may be compensated for to a certain extent by external circuitry. The transit time for minority carriers across the base region is similar to the transit time for electrons from cathode to plate in a vacuum tube. External circuitry can do little to help the situation and a different design of the transistor is required to improve the frequency response.

There are many designs which tend to extend the upper frequency at which amplification may occur. These are listed below with their approximate upper cutoff frequencies, $f\alpha_{b}$.

| Conventional n-p-n or p-n-p: | 5 to 10 mc |
|------------------------------|---------------|
| N-p-n or p-n-p with very | |
| thin base regions: | 50 mc |
| Surface barrier transistor: | 200 mc |
| Double base transistor: | 200 mc |
| Diffused base transistor: | 1000 mc |

Power and frequency response seem to be inversely related. Plotting frequency versus power handling (see Fig. 2) reveals approximately a straight line relationship. The low frequency re-

| 1 | Maximum. | |
|-----|---|------------|
| | Matched pair of 2N224's. | 50 |
| | Matched pair of 2N226's. | all of the |
| | Cob | |
| | | |
| | Maximum at 12 v, 2N223 at 9 v. | |
| | $V_{cb} = 30 v, T_i = 30 C.$ | |
| | Junction to case. | |
| | Matched pair. | |
| | Sensitivity 0.3 A/lumen. | - 10 |
| 10. | Grounded base. | |
| 11. | $V_{c} = 4.5 v.$ | |
| 12. | Same type, flexible leads. | |
| 13. | Military type. | |
| 14. | Current transfer ratio, common emitter. | |
| 15. | Large signal. | |
| 16. | At -12 Vcb, common emitter. | |
| | Chic | |
| | Common base. | |
| 19. | At -25 Vcb. | |
| | Common base circuit. | |
| | All data referred to common emitter circu | it. |
| | | |

57

General Purpose, Low Frequency (cont.)

| Manufacturer | Class and Application | 1 | | imum Ra | | | 8 | Chard | | | |
|-------------------------------|--|------------------------|----------|--------------------|----------|------------------------|---------------------|-------------------------|------------|-------------------------|-------------------------|
| and Type | Class and Application | W _c (mw) | (C) | (а)mw/С (ь)С/mw | | l _c (ma) | β or α | Ι _{co} (μα) | NF (db) | С _с (µµf) | f _{co} (Mc) |
| General Transistor | Corp., Jamaica, N. Y. | | | _ | | | | | - | | |
| GT14 | p-n-p, alloy, audio | 125 | 85 | | 25 | 100 | 2821 | 6 | 16 | | |
| GT20 | p-n-p, alloy, audio | 11 | 1 | | | | 4221 | | 16 | | |
| GT34 | p-n-p, alloy, audio | | | | | | 1 521 | | 16 | | |
| GT74 | p-n-p, alloy, audio | | | | | | 7521 | | <12 | | |
| GT7 5 | p-n-p, alloy, audio | | 1 | | 1 | 1 | 1 5021 | | <12 | | |
| GTE 1 | p-n-p, alloy, audio | 125 | 85 | | 25 | 100 | 7521 | 6 | 16 | | |
| GT81H5 | p-n-p, alloy, audio | 150 | 1 | | 1 | 1 | 12021 | | 1 | | |
| GT82 | p-n-p, alloy, audio | 125 | | | | | 15021 | | | | |
| GT109 | p-n-p, alloy, audio | 11 | | | | | 12021 | | | | |
| GT222 | p-n-p, alloy, audio | | 1 | | 12 | | 1 2021 | | 30 | | |
| GT14H | p-n-p, alloy, hearing aid | 90 | 75 | | 12 | 50 | 2821 | 6 | 12 | | |
| GT20H | p-n-p, alloy, hearing aid | 1 | 1 | | 1 | 1 | 4221 | 6 | 12 | | |
| GT81H | p-n-p, alloy, hearing aid | | | | | | 8021 | 6 | 12 | | |
| GT210H | p-n-p, alloy, hearing aid | | | | | | 25021 | <25 | >29 | | |
| GT35 | n-p-n, alloy, audio | 100 | 75 | | 25 | 100 | 4021 | 12 | 16 | | |
| 2N43A13 | p-n-p, alloy | 150 | 85 | | 45 | 50 | 6521 | 10 | <20 | | >0.4 |
| 2N44 ¹³ | p-n-p_ alloy | 150 | 85 | | 45 | 50 | 3221 | 15 | <33 | | >0.4 |
| Intelex Systems In | nc., New York, N. Y. | | | | | | | | | | |
| T51 | p-n-p, alloy, low freq. | 50 | | | 1.5 | 2 | >10 | 10 | 15 | | 0.5 |
| T52 | p-n-p, alloy, low freq. | 1 | | | 1 | î | >30 | 1 | ĩ | | 1 |
| T53 | p-n-p, alloy, low freq. | | | | | | >50 | | | | |
| TJ1 | p-n-p, alloy, low freq. | 200 | | | | | 10 | | 25 | | |
| TJ2 | p-n-p, alloy, low freq. | 1 | | | | | >30 | | 25 | | |
| ELT | p-n-p, alloy, low freq. | | | | | | /30 | | 23 | | |
| | | | | | | | | | | | |
| 2N207 | p-n-p, alloy, low pwr. audio | 50 | 65 | 0.8(Ь) | -12 | -20 | 100 | 1.5 ¹ | 5 | | 2 |
| 2N207A | p-n-p, alloy, low pwr. audio | 1 30 | 05 | 0.8(6) | -12 | -20 | 100 | 101 | 2 | | î |
| 2N207B | p-n-p, alloy, low pwr. audio | | | | | | | 101 | 2 | | |
| 2N223 | p-n-p, alloy, audio driver | 100 | 65 | 0.12(Ь) | -18 | -150 | 95 | 205 | 10 | 904 | 0.8 |
| 2N224, 2N225 | | 150 | 75 | 0.12(0) | -25 | -150 | 75 | 255 | 10 | 1254 | 0.5 |
| | ³ p-n-p, alloy, audio output | 100 | 65 | | -25 | | | 255 | | 1404 | 0.4 |
| Motorola Inc. Sa | miconductor Product Div., | | | | | | | | | | |
| Phoenix, Arizona | miconductor product Div., | | | | | | | | | | |
| MN13A | p-n-p, fused, aud. driv., sw. | 350 | 90 | 14.3(a)7 | 40 | 150 | 15 | 304 | 32 | | 0.01 |
| MN13B | p-n-p, fused, aud. driv., sw. | | 1 | 1 | | | 30 | | 1 | | |
| MN13C | p-n-p, fused, aud. driv., sw. | | 1 | 1 | 1 | 1 | 60 | | 1 | | |
| | onal Electronic Corp.), | | | | | | | | | | |
| New York, N. Y. | n - n - Herr He | 0.5 | | 0.411 | 10 | 10 | 20 | E | 10 | | 10 |
| 0070 | p-n-p, alloy, audio | 25 | 45 | 0.4(b) | 10 | 10 | 30 | 5 | 10 | | 10 |
| 0071 | p-n-p, alloy, audio | 25 | 45 | 0.4(b) | 10 | 10 | 50 | 4.5 | 10 | | 10 |
| 00721 | p-n-p, alloy, audio | 100 | 75 | 0.3(b) | 16 | 125 | 55 | 4.5 | 15 | | 12 |
| 0073 | p-n-p, alloy, audio | 25 | 65 | 0.4(b) | 30 | 10 | 40 | 4,5 | 10 | | 10 |
| OC76 OCP71 | p-n-p, alloy, converters p-n-p, alloy, photo ⁹ | 50 25 | 65 55 | | 30 25 | 125 10 | | | | | |
| | | | | | | | | | | | |
| Pye Indust. Electr V10/15A | onics, Ltd., Newmarket, England p-n-p, alloy, audio | 100 | 75 | 2(a) | -10 | -30 | 20 | 1011 | 16 | | 0.610 |
| V10/30A | p-n-p, alloy, audio | 1 | 1 | 1 | 1 | 1 | 40 | 1 | 1 | | 0.710 |
| V10/50B | p-n-p, alloy, audio | | | | | | 75 | | | | 1.210 |
| RCA, Somerville, I | N. J. | | | | | | | | | | |
| 2N77 | p-n-p, alloy, audio | 35 | 85 | | -25 | -15 | 5514 | -1016 | 6.5 | 4017 | 0.720 |
| | ¹² p-n-p, alloy, audio | I | 1 | 2.5(a) | -30 | | 4414 | -1016 | 12 | 3617 | 0.720 |
| 2N105 | p-n-p, alloy, audio | | | | -25 | | 5514 | -516 | 16.5 | | 0.7 520 |
| | ¹² p-n-p, alloy, Ige. sig. audio | 50 | | | -25 | _ | 7014 | | | | |
| 2N175/2N220 | | 20 | | | -10 | | | -1219 | | 3617 | 0.8520 |
| 2N20613 | p-n-p, alloy, class A | 75 | | 3.3(a) | -30 | | | -1016 | 2 | 3517 | 0.782 |
| | E bl anall ana | | | / | | | | | | | |

General Purpose, Low Frequency (cont.)

| Manufacturer and Type | Class and Application | W _c (mw) | Ti | (а)mw/С (ь)С/mw | Vc | l _c (ma) | β or α | Char I _{co} (µa) | Acter NF (db) | istics C _c (μμf) | f _{co} (Mc) |
|--|--|------------------------|-----|--------------------|------------|------------------------|---------------------|---------------------------------|---------------------|-----------------------------------|-------------------------|
| Raytheon Mtg. Co. | Newton, Mass. | | | | | | | | | | |
| 2N63 | p-n-p, fused, audio, low rf. | 100 | 85 | | -22 | -10 | 22 | 6 | 15 | | |
| 2N64 | p-n-p, fused, audio, low rf. | 1 | 1 | | -15 | 1 | 45 | 1 | 13 | | |
| 2N65 | p-n-p, fused, audio, low rf. | | | | -12 | | 90 | | 11 | | |
| 2N106 | p-n-p, fused, audio, low rf. | | | | -6 | | 45 | | 4.5 | | |
| 2N130 | p-n-p, fused, audio, rf. | 120 | | | -22 | | 22 | 1 | 15 | | |
| 2N131 | p-n-p, fused, audio, rf. | 120 | 85 | | -15 | -10 | 45 | 6 | 13 | | |
| 2N132 | p-n-p, fused, audio, rf. | 1 | 1 | | -12 | 1 | 90 | 1 | 11 | | |
| 2N133 | p-n-p, fused, audio, low-noise | | | | -15 | | 45 | | 4.5 | | |
| 2N130A | p-n-p, fused, audio, rf. | 100 | | | -22 | | 22 | | 15 | | |
| 2N131A | p-n-p, fused, audio, rf. | 100 | | | -15 | | 45 | | 13 | | |
| AN 3 3 A 4 | m m m for all multiple | 100 | | | 10 | -10 | 90 | 6 | 11 | | |
| 2N132A | p-n-p, fused, audio, rf. | 100 | 85 | | -12 -15 | | | 0 | 4.5 | | |
| 2N133A | p-n-p, fused, audio, low-noise | 100 | | | | 1 | 45 | | 4.5 | | |
| 2N138A | p-n-p, fused, audio output | 130 | | | -12 | -100 | 140 | | | | |
| CK751 | p-n-p, fused, audio output | 240 ² | | | -12 | -100 | 140 | | 10 | | |
| 2N272 | p-n-p, fused, audio, rf. | 150 | | | -20 | -100 | 90 | | 12 | | |
| 2N273 | p-n-p, fused, audio output | 150 | 1 | | -12 | -100 | 140 | | | | |
| CK870 | p-n-p, fused, audio, sw. | 130 | 85 | | -25 | -100 | 10 | 6 | | | 0.4 |
| CK871 | p-n-p, fused, audio, sw. | 130 | 85 | | -20 | -100 | 15 | 6 | | | 0.5 |
| 2N327 | p-n-p, fused, Si, audio, sw. | 150 | 160 | | -50 | -50 | 14 | 0.005 | 18 | 601 | 0.3 |
| 2N328 | p-n-p, fused, Si, audio, sw. | | | | -35 | | 24 | | | 1 | 0.3 |
| 2N329 | p-n-p, fused, Si, audio, sw. | | | | -30 | | 50 | | 1 | | 0.6 |
| 2N330 | p-n-p, fused, Si, low-noise | | 1 | | -45 | 1 | 30 | 1 | 12 | 1 | 0.5 |
| prague Electric Ca | ., North Adams, Mass. | 1 | | | | | | | | | |
| 10A | p-n-p, alloy, audio driver | 180 | 70 | 4.5(a) | 50 | 100 | 33 | 5000 | 20 | 35 | 1.2 |
| 108 | p-n-p, alloy, audio driver | | | | | | 53 | 5000 | 1 | | - 1 |
| 100 | p-n-p, alloy, audio driver | | | | | | >53 | 5000 | 1 | 1 | 1 |
| 8F | p-n-p, alloy, audio | 100 | 80 | 2(a) | -45 | -50 | 15 | 16 | 20 | 28 | 0.7 |
| 88 | p-n-p, alloy, audio | | | | | | 30 | | | | - 1 |
| 8 D | p-n-p, alloy, audio | | | | | | 99 | | | | |
| 86 | p-n-p, alloy, audio | | 1 | | 1 | 1 | >100 | 1 | 1 | | 1 |
| iyivania Elec. Prod | ucts Inc., Woburn, Mass. | | | | | | | | | | |
| 2N229 | n-p-n, alloy, gen. purpose | 50 | 75 | 1(a) | -103 | 40 | 0.96 | 200 | | | 0.5 |
| 2N306 | n-p-n, alloy, low freq. | 1 | 1 | 1 | -203 | | 0.96 | 1 | | | |
| 2N34 | p-n-p, alloy, low freq. | | | | -403 | 100 | 0.975 | | | 15 | 0.3 |
| 2N35 | n-p-n, alloy, low freq. | | | | 403 | | 0.975 | | | 18 | 0.6 |
| 2N213 | n-p-n, alloy, audio driver | | | | | 1 | 150 | | | | |
| 2N214 | n-p-n, alloy, audio output | 125 | | 2.5(a) | 25 | | 70 | | | 15 | 0.6 |
| 2N228 | n-p-n, alloy, audio output | 50 | 1 | 1 (a) | 25 | | 7.5 | | | 15 | 0.0 |
| oxas Instruments | Inc., Dallas, Texas | 1 | | | | | | | | | |
| 2N185 | p-n-p, alloy, audio amp. | 150 | 50 | | -20 | 150 | 35 | 8 | | | |
| 2N238 | p-n-p, alloy, audio amp. | 50 | 60 | | -20 | | | 8 | | | |
| 2N291 | p-n-p, alloy, audio amp. | 180 | 50 | 0.25(Ь) | -25 | 200 | 30 | 10 | | | |
| lung-Sol Electric in | c., East Orange, N. J. | | | | | | | | | | |
| T5616 | p-n-p, alloy, med. pwr. audio | 200 | 85 | 0.2(b) | -25 | 200 | 365 | 8 | | | |
| T5617 | p-n-p, alloy, med. pwr. audio | 1 | 1 | 1 | 1 | 1 | 545 | 1 | | | |
| T5618 | p-n-p, alloy, med. pwr. audio | | - 1 | | | | 725 | | | | |
| T5620 | p-n-p, alloy, low-noise | 100 | | 0.35(Ь) | | 50 | 0.98 | | 8 | 50 | 1.0 |
| T5621 | p-n-p, alloy, low-noise | 100 | | 0.35(Ь) | | 50 | 0.99 | | 8 | 50 | 1.0 |
| SN63T | p-n-p, alloy, audio | 100 | 85 | 0.35(ь) | -25 | 25 | 0.96 | 8 | 25 | 50 | 0.6 |
| 2N64 | p-n-p, alloy, audio p-n-p, alloy, audio | 100 | 05 | 0.33(0) | 1 | Ĩ | 0.98 | 1 | 22 | 1 | 0.8 |
| 2N65 | p-n-p, alloy, audio | | | | | | 0.98 | | 20 | | 1.2 |
| 2619 | | | | | | 50 | 50 | | žU | | 1.4 |
| 5615T | p-n-p, alloy, driver amp. p-n-p, alloy, hi-volt, amp. | | | | -45 | 50 | 0.98 | | 22 | | 1.0 |
| | | 1 | | , | | | | 1 | | | |
| Vestern Electric Co 1N85 ⁶ | p.n, grown, photo, coding | 50 | 85 | | -90 | -1 | | 67 | | 5 | 0. |
| 2N294 | | | 85 | 2.0(a) | 35 | 100 | | 4 | 15 | э 8.5 | 2.0 |
| | n-p-n, grown, linear audio | 120 | | | | | 0.00 | | | | |
| GA528294 | p-n-p, alloy, gen. purpose p-n-p, alloy, gen. purpose | 120 120 | 85 | 2.0(a) | -65 | 50 | 0.98 | 4.5 | <10 | 17 22 | 3.0 |
| GA53149 ⁶ | | | 85 | 2.0(a) | -65 | -50 | | 4.5 | 10 | | |

sponse of transistor amplifiers depends upon pas. sive elements in the circuit and therefore may h controlled at the designer's discretion.

Power

Ξ

Fig.

for (

WATTS

Fig. for

Fig.

Curv

The maximum power dissipation of a commencially available transistor is about 25 watts. Experimental transistors have been constructed which dissipate over a hundred watts. Power handling capabilities of typical transistors are presented in Figs. and 3. It is noticed that $f\alpha_b$ (Fig. 2) decreases with increasing power handling capabilities and that h (grounded emitter current transfer function) de creases in a somewhat similar manner (Fig. 3),

The main drawback to large power handling capabilities is the internal temperature rise within the transistor. When a junction temperature of about 100 C is reached, a germanium transistor will not operate correctly (see section on temperature). Silicon is slightly better in this respect. A junction temperature between 150 and 200 C may be achieved.

Transistors are usually de-rated linearly in power as the temperature increases such as,

$$P_T = P_r \left[1 - K(T - T_r) \right]$$

where

 P_T = power dissipation at temperature T,

 $P_r =$ power dissipation at room temperature,

 $T_r = \text{room temperature, 25 C},$

K =de-rating constant.

The higher current density across the emitter to base junction affects the emitter efficiency, thereby reducing the parameter alpha, which in turn reduces the gain of the device. Therefore, power transistors usually have lower gain capabilities than transistors of other types (see Fig. 3).

Noise

Although noise is a drawback of point contact and early types of junction units, the noise figure of present junction transistors is as low as 4.5 db measured for a one-cycle bandwidth at 1 kc. Typical commercial units specify 10 to 12 db maximum noise figure.

| Impedance | grounded base | grounded emitter | grounde collecto |
|-----------|----------------------------------|---------------------|---------------------|
| Input | 100 ohms | 1500 ohms | 30,000 oh |
| Output | 100,000 ohms | 20,000 ohms | 100 oh |
| | Fi | g. 1 | |
| The | 1. Maximum. 2. With heat sink | | |

2. With heat sink 3. V_{cb}

4. Alpha, minimum,

5. $I_c = 150$ ma.

6. Military Type. 7. Dark current. Sensitivity—0.35 μα/mw.

ELECTRONIC DESIGN • July 15, 1957

iv

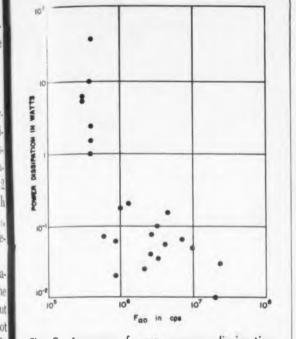
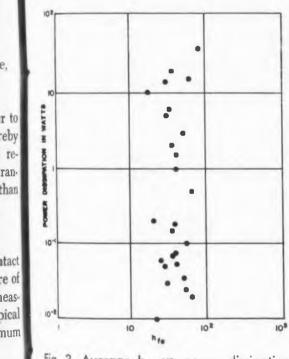


Fig. 2. Average fare vs. power dissipation for commercially available transistors.





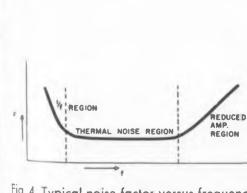


Fig. 4. Typical noise factor versus frequency curve for transistors.

1957

CIRCLE 501 ON READER-SERVICE CARD

F-I-a-s-h!...from Transistor Center, U.S.A.



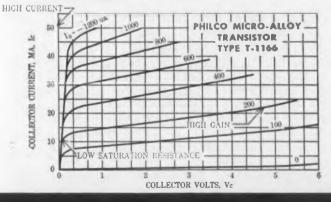
Announcing a new transistor class . . . The PHILCO Micro-Alloy Transistor (MAT)*



CHECK THESE UNEQUALLED FEATURES

• Excellent High Speed Switching characteristics.

- Low Saturation Voltage (low impedance)
- Excellent high frequency amplification.
- Excellent low-level amplifier over entire
- frequency range from D.C. to Megacycles.
- Exceptionally Long Life (hermetically sealed)
- Permits high speed computer design with Fewer Stages.



...world's first production transistor with exceptionally high <u>frequency</u> and high gain ... plus low saturation resistance!

This newest development from Philco Transistor Center features the characteristic high frequency response obtainable with extremely precise base width control. Designed for low voltage operation, the new MAT transistor is especially well suited for high speed applications where low saturation resistance (reduced power consumption) is necessary.

To combine high gain at high currents with high frequency response, the new MAT transistor employs a gallium doped alloy junction for the emitter electrode.

A special short-alloying cycle, combined with precise electro-chemical production techniques (pioneered and developed at Philco Transistor Center for production of SBT), results in the micro-alloy contact for exceptionally high injection efficiency. This new process assures higher gain, and permits operation at higher current. Beta linearity is excellent over the entire range of operating currents ... up to 50 milliamperes.

• Write for complete information and specifications. Make Philco your prime source of information for high frequency transistor applications. Visit The Unique Philco Transistor Display at WESCON Show, San Francisco Cow Palace, August 20-23, Booth #2217-2218.

*Patent Applied For

LANSDALE TUBE COMPANY DIVISION LANSDALE, PENNSYLVANIA

O CORPORA

General Purpose, Low Frequency (cont.)

| Manufactu and Typ | | ₩ (mw) | T _i (C) | (a)mw C (b)C mw | Vc | l _c (ma) | β or α | Char I _{co} (µa) | NF (db) | C _c (μμf) | f _{co} (Mc) |
|----------------------|---|-----------|-----------------------|--------------------|-------|------------------------|---------------------|---------------------------------|------------|-------------------------|-------------------------|
| - | Electric Corp., Youngwood, Pa. 5082 p-n-p, fused, switch, amp. | | 85 | | -35 | - | 481 | | | | 0.01 |
| 2N59 | p-n-p, fused, class B audio out. | 150 | Ĩ | 3.25(a) | -25 | -150 | 80 | 10 mg | 15 | 40 | 1.0 |
| 2N60 | p-n-p, fused, class B audio out. | 1 | - 1 | 1 | 31 | 1 | 66 | 1 | 1 | 1 | 1 |
| 2N61 | p-n-p, fused, class B audio out. | | | + | | | 45 | | | | |
| 2N403 | p-n-p, fused, class A audio out. | | | | | | 50 | | | | |
| 2N402 | p-n-p, fused, audio driver | | 1 | 1 | ·] . | 50 | 50 | 1 | 1 | | 1 |
| Bogue Elec. M | fg. Co., Paterson, N. J. | | | | 6.00 | | | | | | |
| 2N347 | n-p-n, grown, Si, audio, servo, sw. | 750 | 175 | 3.0(a) | 60 | 60 | 20 | | 24 | 10 | 0.2 |
| 2N348 | n-p-n, grown, Si, audio, servo, sw. | 1 | | | 90 | 50 | 1 | | 1 | 1 | 1 |
| 2N349 | n-p-n, grown, Si, audio, servo, sw. | | | | 125 | 40 | | | | | |

High Frequency, Switching

| Amperex Elect | ronic Corp., Hicksville, N. Y. | | | | | 1 | | | | | |
|------------------|---|-----|-----|---------|------------------------|------|-------|------|----|-----|------|
| 0044 | p-n-p, alloy, rf conv. | 100 | 75 | 2.0(a) | 15 | 10 | 100 | 0.5 | | 40 | 15 |
| 0C45 | p-n-p, alloy, if amp. | 100 | 75 | 2.0(a) | 15 | 10 | 40 | 0.5 | | | 6 |
| Bogue Elec. Mf | g. Co., Paterson, N. J. | | | | | | | | | | |
| RD316 | n-p-n, grown, Si, audio, comp. servo | 100 | 175 | 1.0(a) | 20 ² | 20 | 10 | 0.5 | 25 | 10 | 2 |
| 2N160/2N1 | 60A ³ n-p-n, grown, Si, audio, comp. servo | 150 | 1 | | 40 ² | 25 | 15 | | 1 | | 4 |
| | 61A ³ n-p-n, grown, Si, audio, comp. servo | 1 | | | | | 30 | | | | 5 |
| | 62A ³ n-p-n, grown, Si, audio, comp. servo | | | | | | 35 | | | | 8 |
| 2N163/2N1 | 63A ³ n-p-n, grown, Si, audio, comp. servo | | | | | | 50 | 1 | | | 6 |
| 2N97 | n-p-n, grown, audio, if, osc. comp. | 50 | 75 | 2.0(a) | 30 | 10 | 0.93 | 2 | 15 | 14 | 1.0 |
| 2N98 | n-p-n, grown, audio, if, osc. comp. | | | | 40 | 11 | 0.975 | | | 10 | 2.5 |
| 2N99 | n-p-n, grown, audio, if, osc. comp. | | | | 40 | | 0.975 | 1 | | | 3.5 |
| 2N103 | n-p-n, grown, audio, if, osc. comp. | 1 | 1 | 1 | 35 | 1 | 0.80 | 5 | 1 | 1 | 0.75 |
| CBS-Hytron, Lo | owell, Mass. | | | | | | | | | | |
| 2N182 | n-p-n, alloy, switch | 100 | 75 | 2.0(a) | 25 | | 25 | 3 | | 10 | 5 |
| 2N183 | n-p-n, alloy, switch | 1 | 1 | 1 | 1 | | 40 | | | 1 | 10 |
| 2N184 | n-p-n, alloy, switch | 1 | 1 | 1 | 1 | | 60 | | | | >10 |
| Fretco Inc., Pit | ttsburgh, Pa. | | | | | | | | | | |
| 2N32 | pt. contact, pulse, osc., sw. | 50 | 30 | | -40 | -8 | 2.2 | -12 | 40 | | 50 |
| 2N33 | pt. contact, pulse, osc., sw. | 30 | 30 | | -85 | -7 | | -12 | 40 | | 50 |
| General Electr | ic Co., Syracuse, N. Y. | | | | | | | | | | |
| 2N78 | n-p-n, grown, hi-gain rf-if | 65 | 85 | 1.1(a) | 15 | 20 | 40 | 5 | 12 | 2.4 | 8 |
| 2N123 | p-n-p, alloy, hi-fi switch | 100 | 1 | 1.67(a) | -15 | 125 | 50 | | | 15 | 8 |
| 2N164A | n-p-n, grown, mixosc., if | 65 | | 1.1(a) | 15 | 20 | 40 | 5 | | 2.4 | 8 |
| 2N165 | n-p-n, grown, if | 55 | 75 | 1 | 15 | 20 | 72 | 5 | | 2.4 | 4 |
| 2N167 | n-p-n, switch | 65 | 85 | 1 | 30 | 75 | 36 | 1.5 | 8 | 4 | 8 |
| 2N168A | n-p-n, grown, if | 65 | 85 | 1.1(a) | 15 | 20 | 40 | 5 | | 2.4 | 8 |
| 2N169 | n-p-n, grown, if | 55 | 75 | 1 | 15 | 1 | 72 | 1 | | 1 | 4 |
| 2N169A | n-p-n, grown, if | 55 | 75 | | 25 | | 72 | | | | 5 |
| 2N292 | n-p-n, grown, if | 65 | 85 | | 15 | | 25 | | | | 5 |
| 2N293 | n-p-n, grown, if | 65 | 85 | 1 | 15 | 1 | 25 | 1 | | 1 | 8 |
| 2N313 | n-p-n, grown, if | 65 | 85 | 1.1(a) | 15 | 20 | 25 | 5 | | 2.4 | 5 |
| 2N314 | n-p-n, grown, if | 65 | 1 | 1.1(a) | 15 | 20 | 25 | 5 | | 2.4 | 8 |
| 4JD183 | P-n-p, switch | 200 | | | -30 | 1000 | 15 | 20 | | 45 | 0.8 |
| 4JD184 | p-n-p, switch | 200 | | | -30 | 1000 | 20 | 20 | | 45 | 0.8 |
| 4JD4A2 | n-p-n, Si, hf | 150 | 150 | 1.0(a) | 15 | 20 | 14 | 0.15 | | 14 | 25 |
| 4 J D 4 A 3 | n-p-n, Si, low-level sw. | 150 | 150 | 1.0(a) | 10 | 20 | | 0.15 | | 14 | 25 |
| 4JD4A4 | n-p-n, Si, hf amp. | 1 | 1 | 1.0(a) | 15 | 1 | 15 | | | 1 | 1 |
| 4JD4A5 | n-p-n, Si, hf, amp. | | | 1.0(a) | 15 | | 40 | | | | |
| 4JD5A1 | n-p-n, Si, unijunction | 250 | | | 454 | 504 | | 504 | | | |
| 3N29 | n-p-n, tetrode | 50 | 85 | | 75 | 20 | | 25 | | 4.2 | 40 |
| 3N30 | n-p-n, tetrode | 1 | 1 | | 1 | 1 | | | | 5 | 80 |
| 3N31 | n-p-n, tetrode | | | | | | | | | 3.1 | 20 |

The typical noise figure characteristic (see Fig. 4) of a transistor has a 1/f characteristic at low frequency; is flat over the intermedaite range; and increases at the higher frequency. The 1/f noise at low frequency is predominantly semiconductor and surface recombination noise. The middle range is thermal noise, and the increase in noise figure at high frequencies is due to the decrease in amplification of the device.

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Reliability

When transistors were first produced in any quantity their reliability was very questionable. The effects of humidity and temperature were very disheartening. However, today with hermeticallysealed units the effects of humidity have been eliminated.

The most recent reports on reliability indicate that for transistors operating in computers and hearing aids, the number of unit-hours per failure is of the order of 10^5 to 10^6 . If this rate of failure continued, the average life of a transistor would be from 10 to 100 years. This sounds slightly fantastic but is not impossible.

The effects of vibration and shock on transistors are almost negligible. They will hold up as well as passive circuit elements.

Temperature

Temperature, however, still has a detrimental effect upon transistor operation. At the present time the upper operating temperature limit on germanium devices is approximately 85 C. The devices must be de-rated as mentioned earlier. Silicon transistors have an upper operating temperature limit of approximately 150 C. The factor controlling the upper temperature limit is the width of the forbidden region in the energy band structure of the material from which the transistor is fabricated. The reason silicon is better is because it has an energy gap of 1.1 volt as compared to germanium with 0.7 volt. An inter-metallic compound, e.g., Gallium Arsenide, has a larger energy gap than either germanium or silicon and thus should work at higher temperatures, if and when suitable single crystals are made.

With proper circuit design the effect of temperature upon I_{co} may be swamped out. That is, if the current flowing in the collector is large with respect to any expected I_{co} change, the operating point will not change appreciably.

1. I_c=1.5 A, V_{ce} = 2v.
2. 1 v emitter voltage.
3. Same as basic type, but emitter voltage 5 v.
4. V_{bb}, Ie, I_{eo}
5. V_{cb}

Irradiation Effects

Another environment besides high temperature that is detrimental to transistor operation is that of a gamma or neutron flux field.

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Neutrons react on transistors by producing imperfections in the crystal structure of germanium or silicon from which the transistor is fabricated. These imperfections appear as p-type impurity centers in germanium. After prolonged irradiation n-type germanium has been converted to p-type; p-type germanium remains p-type. The imperfections produced reduce the mobility and lifetime of the carriers in either type of material. In silicon the defects produced appear at an energy level in the center of the forbidden region. This material thus tends to become intrinsic under irradiation. The effects on mobility and lifetime are also present.

The general figure reported to date for the amount of integrated flux that a transistor will withstand is in the order of 10^{12} to 10^{13} nvt. This is the region in which the parameters of the transistors start to deteriorate. With the aid of feedback the useful range on a transistor amplifier might be extended an order of magnitude higher in integrated flux.

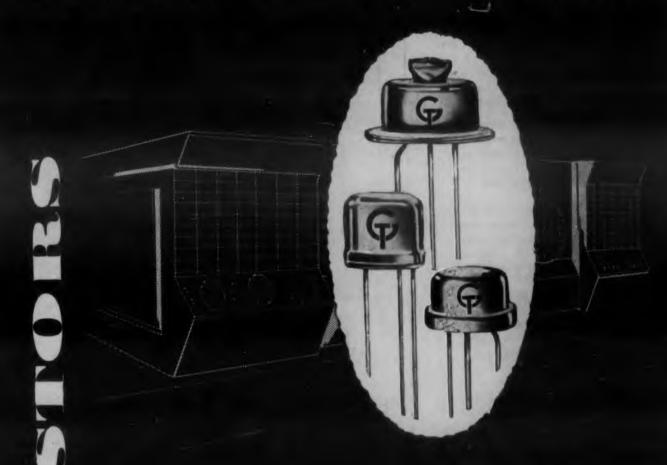
There is some evidence that indicates that it is the fast neutrons that do the majority of the above damage. Thermal neutrons are thought to produce substitutional impurities by K capture and beta emission. For the isotope ${}_{32}\text{Ge}^{70}$, this process is: ${}_{32}\text{Ge}^{70}$ plus thermal neutron transmutes to ${}_{31}\text{Ga}^{71}$ by K capture. For the case of the germanium isotope ${}_{32}\text{Ge}^{74}$, the process is: ${}_{32}\text{Ge}^{74}$ plus thermal neutron transmutes to ${}_{33}\text{As}^{75}$. The half-life of ${}_{32}\text{Ge}^{71}$ is 11.4 days, and for ${}_{32}\text{Ge}^{75}$ the half-life is 82 minutes.

This would indicate a gradual degradation in characteristics after irradiation, which does not seem to be present. In fact, improvement in the parameters after irradiation is stopped is more often noticed. This is explained by an annealing process which can occur even at room temperature. The annealing process results in removal of interstitials or other lattice defects by thermal vibration.

Camma irradiation produces interstitial defects as well as ionized atoms within the crystal structure. The ionization appears as an increased temperature with its resulting degradation in transistor performance.

Transistors have now taken their place alongside vacuum tubes as a useful tool for designers of electronic equipment. With careful design based upon the known limitations of transistors, reliable operation of transistor circuitry may be obtained.

VERSATILITY OF DESIGN



G.T. computer transistors

• MINIATURIZATION

• PORTABILITY

• RELIABILITY

• EXTENDED LIFE

Simplifying and miniaturizing circuitry with GT germanium alloy type transistors, control engineers are now able to design lighter weight, portable, more reliable units than by previous methods with conventional components. General Transistor's PNP and NPN transistors are playing a vital role in advancing the designs of control systems

Versatility of design is now available write today for Bulletin G-100 containing all types list and dimensional drawings.

Typical Applications

- Relay Amplifier
- Direct Current Swit
- Photoelectric readout & control
- Micro and millisecond switching
- Servo driver applications
- Control lighting
 - Phase detector circuit
- Low level modulation

GENERAL TRANSISTOR CORPORATION

CIRCLE 502 ON READER-SERVICE CARD FOR MORE INFORMATION

High Frequency, Switching (cont.)

| Manufacturer and Type | Class and Application | W _c (mw) | Ti | imum Ra (а)mw/C (ь)C/mw | Vc | l _c (ma) |
|------------------------------------|--|------------------------|-----|-------------------------------|------|------------------------|
| General Transistor | Corp., Jamaica, N. Y. | | | | | |
| G1759R | p-n-p, alloy, rf-if | 90 | 75 | | 12 | 100 |
| GT760R | p-n-p, alloy, rf-if | | | | 10 | 1 |
| GT761R | p-n-p, alloy, rf-if | | | | 10 | |
| GT762R | p-n-p, alloy, rf-if | | 1 | | 6 | 1 |
| GTE 3 | p-n-p, alloy, lo-speed comp. | 125 | 85 | | 25 | 200 |
| GT87 | p-n-p, alloy, lo-speed comp. | | 1 | | | |
| GT88 | p-n-p, alloy, lo-speed comp. | | | | | |
| GT122 | p-n-p, alloy, lo-speed comp. | | | | | |
| 2N311 | p-n-p, alloy, lo-speed comp. | 100 | 1 | | 15 | 1 |
| GT758 | p-n-p, alloy, lo-speed comp. | 100 | 85 | | >20 | 200 |
| GT123 | p-n-p, alloy, hi-speed comp. | | | | >20 | 1 |
| GT153 | p-n-p, alloy, hi-speed comp. | | | | >30 | |
| GT269 | p-n-p, alloy, hi-speed comp. | | | | 25 | |
| GT759 | p-n-p, alloy, hi-speed comp. | | 1 | | >20 | |
| G1760 | p-n-p, alloy, hi-speed comp. | 100 | 85 | | 15 | 50 |
| GT761 | p-n-p, alloy, hi-speed comp. | | 1 | | 15 | 50 |
| 2N356 | n-p-n, alloy, switch, comp. | | | | >30 | 200 |
| 2N357 | n-p-n, alloy, switch, comp. | | | | | 1 |
| 2N358 | n-p-n, alloy, switch, comp. | | 1 | | | |
| 2N312 | n-p-n, alloy, switch, comp. | 100 | 85 | | 15 | 200 |
| GT792 | n-p-n, alloy, switch, comp. | | 1 | | 20 | 100 |
| GT903 | n-p-n, alloy, switch, comp. | | | | 1 | 200 |
| GT904 | n-p-n, alloy, switch, comp. | | 75 | | | 1 |
| GT905 | n-p-n, alloy, sw tch, comp. | | 85 | | | |
| GT947 | n-p-n, alloy, switch, comp. | 100 | 85 | | 15 | 200 |
| GT948 | n-p-n, alloy, switch, comp. | | 1 | | 20 | 1 |
| GT949 | n-p-n, alloy, switch, comp. | | | | 30 | |
| G1762 | p-n-p, alloy, hi-speed comp. | | | | 6 | 50 |
| GT763 | p-n-p, alloy, hi-speed comp. | | | | 6 | 50 |
| GT764 | p-n-p, alloy, hi-speed comp. | 100 | 85 | | >20 | 200 |
| 2N315 | p-n-p, alloy, switch, comp. | | 1 | | 20 | 1 |
| 2N316 | p-n-p, alloy, switch, comp. | | | | | |
| 2N317 | p-n-p, alloy, switch, comp. | | | | 1 | |
| GT167 | n-p-n, alloy, switch, comp. | | 1 | | 25 | 1 |
| GT229 | n-p-n, alloy, experimental | 100 | 85 | | >10 | 200 |
| GT345 | p-n-p, alloy, bi-directional | 125 | | | 40 | |
| GT34N | p-n-p, alloy, neon light | 125 | | | 100 | |
| GT34HV | p-n-p, alloy, hi-voltage | 150 | | | 50 | 1 |
| 2N318 | p-n-p, alloy, photo ¹ | 50 | 1 | | 12 | 20 |
| | ic., New York, N. Y. | | | | | |
| TP1 | n, point contact, switch | 150 | | | -30 | 30 |
| TP2 | n, point contact, amp., osc. | 150 | | | -30 | 30 |
| Lansdale Tube Co. Lansdale, Pa. | Div. of Philco Corp. | | | | | |
| T0031 | p-n-p, alloy, Ne ind., rel. driv. | 25 | 65 | | -50 | -10 |
| T0033 | p-n-p, alloy, 'f switch | 50 | 85 | 0.8(ь) | -20 | -20 |
| 2N1282 | p-n-p, sbt, rf, video | 30 | 1 | 0.75(ь) | -10 | -5 |
| 2N1292 | p-n-p, sbt, rf, if | 30 | | | -10 | -5 |
| 2N2992 | p-n-p, sbt, rf tuned amp. ⁷ | 40 | | | -7 | -20 |
| 2N3002 | p-n-p, sbt, video amp. ⁷ | 40 | 1 | 1 | -7 | -20 |
| 2N344/58101 | p-n-p, sbt, hf | 20 | 55 | 0.75(ь) | -59 | -5 |
| 2N345/5B102 | p-n-p, sbt, hf | | 1 | | 1 | |
| 2N346/SB103 | p-n-p, sbt, hf | | | | 1 | |
| 2N240 | p-n-p, sbt, hf switch | 10 | | 1 | -6* | -15 |
| 2N393/T1166 | p-n-p, microalloy, hf, switch | 50 | 85 | | -6* | -50 |
| 2N354/T1025 2N355/T1159 | p-n-p, alloy, Si, hf amp. | 150 | 140 | | -25* | |
| - | p-n-p, alloy, Si, hf switch | 150 | 140 | 0.77(Ь) | -109 | 1 |
| T1164 | p-n-p, alloy, sym. switch | | | | | |

| | C 1 | | | | Fifth Annual | | |
|---------------------|------------|------------|-----------------------------|-------------------------------------|---|----------------|---------|
| β or α | | NF (db) | C _c $(\mu\mu f)$ | f _{co} (Mc) | | sistor | D |
| | | | | | | | - |
| 25 | 6 | | | 2.5 | | | |
| 40 70 | | | | 5 | | | |
| 120 | | | | 11 17 | | | |
| 49 | 10 | 16 | | <07 | | | |
| 38 80 | | | | 0.5 | Contents | | |
| 80 | <60 | 1 | | 1.5 | | | si |
| 15 | <5 | 16 | | <0.5 | | | rc |
| 150 | <6 | | | >5 | | | si |
| >20 | <5 <4 | | | >4 | Low Frequency Transistors | 2, 3, 4 | el |
| >20 | <5 | 16 | | 3 | High Frequency Transistors | 6, 8, 10 | al |
| 40 75 | 1.0 1.0 | 16 16 | | 5 10 | Power Transistors | 12, 14, 16 | eı p |
| | <5 | | | 3 | | | 0 |
| | | | | 6 | Switching Transistors | 13, 14 | 0 |
| | 10 | | | , | A Survey of Transistor | | c u |
| | <60 6 | | | 4.8 | Characteristics, Robert H. Riddle | 2 | с |
| | <25 | | | >4 | Transistor Parameter Conversion | | d |
| | 1 | | - | >* | Tables | 10 | Si |
| | <25 | | | | Transistor Test Equipment, | | С |
| | <20 <25 | | | >4 >0.7 | Soren C. Ibsen | 18 | ł |
| 100 | 1 | 16 | | 20 | JUICH G. IBJEN | 10 | U V |
| 120 | 1 <5 | 16 16 | | 30 >25 | Curve Tracers | 19 | f |
| 200 | 1.0 | 10 | | 5 | Portable Test Sets | 20 | I |
| | 1.0 1.0 | | | 12 20 | | | i |
| >25 | <10 | | | >5 | Parameter Analyzers | 22 | 1 |
| >10 15 | <10 15 | 30 24 | | | Misc. Test Equipment | 22 | 1 |
| 18 | <450 | | | | Transistor Cross Index | 21 | |
| 10 100 | 10 10 | 16 20 | | | | | |
| >2 | lma | | | | | | |
| 5 | 2 ma | | | 2 | | | |
| | | | | | | | |
| 100 | 15 10 | 5 | | 2 | | | |
| 35 | 35 | 9 | 34 | 653 | | | |
| 25 | | 9 84 | | 60 ³ 105 ³ | | | |
| 0.94 | | 84 | | 1053 | *All characteristic data for Generation | -I Transistor. | |
| 22 | 3 | 41 | 3.5 | 50 ³ | Colp. is relative to CE operation. | | |
| 35 | | 1 | | 50 ³ | Sensitivity 0.16 v/ft candle. Military type. | | |
| 30 32 | | 1 | | 753 553 | Max. freq. of oscillation. 4. Cob | | |
| 155 | 5 | 3.5* | 3.5 | 603 | 5. Max. at $V_c = -5 v_c$ | | н. |
| 18 | 0.1 | | 7 | 153 | At 10 MC. Characteristic data given for G | B circuit. | н |
| 18 | 0.1 | | 7 20 | 25 ³ 0.8 | 8. At 1 MC. 9. V _{ce} | | |
| | | | 20 | 0.8 | 9. V _{ce} | | |

Data Chart

This year's data chart has been designed as a quick and comprehensive reference for the transistor circuit designer. Only the most significant characteristics have been tabulated in an effort to keep the chart within reasonable proportions. Each transistor's operating characteristics depends on a particular circuit used, the frequency of operation, the temperature, and other conditions so that the operating characteristics given are typical ones, usually for the grounded emitter circuit. A general idea of operation under varying conditions can be had by scanning the maximum ratings.

Transistors fall easily into three categories: Low Frequency, High Frequency, and Power. A cut-off frequency of 1 Mc is used as a rough dividing line between high and low frequency units, and a collector dissipation of 1 w or more can define a power transistor. In addition, many transistors are recommended for switching purposes, both power switching and high frequency switching, and their operating characteristics are given in two separate tables. The new class of silicon transistors are not easily characterized since many of them are capable of high frequency power applications, as well as switching.

A total of about 430 different types of transistors are available this year, as compared to about 270 last year. Many new manufacturers have entered the field including many European firms and some Japanese. Most companies have given their own designation to their transistors, and may also have a RETMA number. In the cross-index, equal or equivalent types are listed after the type number designated by the company. For an addilional copy of this chart, turn to the Reader Service Card and circle 500.

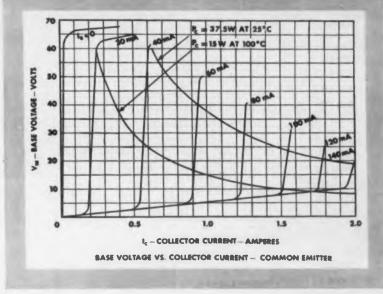


now you can get 15 watts at 100°C Example

NEW silicon high power transistor

For your audio servo uses – and many other applications, you can reach new transistor highs – in power, temperature and gain with low distortion and the stability and reliability you expect from silicon transistors. In Class B push-pull operation, two new TI Type 2N389 silicon diffused junction transistors provide 15 W power output at 100°C ... with distortion of less than 10% and typical beta cutoff frequency of 300 kcps. This new transistor is the first high power silicon transistor and the latest addition to the TI silicon line... widest in the industry.

Now! 37 TI silicon transistor types — your widest choice



absolute maximum ratings

| Power Dissipation at 100°C | | | | | | | 15 | Watts |
|------------------------------|---|---|--|----|---|----|-------|---------|
| 25°C | | | | | | | 37.5 | Watts |
| Collector to Emitter Voltage | | | | | | | +60 | Volts |
| Base to Emitter Voltage | | | | | | | -2 | Volts |
| Collector Current | | | | | | | 2 | Amperes |
| Saturation Resistance | | | | | | | 6 | Ohms |
| Base Current | | | | | | | 0.5 | Ampere |
| Storage Temperature | • | • | | -6 | 5 | to | +150° | С |

957

High Frequency, Switching (cont.)

| Manufacturer and Type | Class and Application | W _c (mw) | Ti | imum Ra (a)mw/C (b)C/mw | Vc | l _c (ma) |
|--------------------------|--|------------------------|-----|-------------------------------|-----|------------------------|
| Mullard (Internatio | onal) Electronic Corp. | | | | | |
| New York, N. Y. | | | | | | |
| 0C44 | p-n-p, rf conv. | 100 | 75 | 2.0(a) | 15 | 10 |
| OC45 | p-n-p, alloy, if amp. | 100 | 75 | 2.0(a) | 15 | 10 |
| Pye Industrial Elec | tropics 14d. | | | | | |
| Newmarket, Engla | | | | | | |
| V6/R2 | | 26 | 75 | 0.5(a) | | -12 |
| V6/R4 | p-n-p, alloy, if amp. p-n-p, alloy, if, oscmix. | 25 | 13 | 0.5(a) | -6 | -12 |
| V6/R8 | p-n-p, alloy, if, oscmix. | | | | | |
| | | | 1 | 1 | 1 | 1 |
| RCA, Somerville, N | | | | | | |
| | p-n-p, alloy, 455 kc if amp. | 35 | 85 | | -16 | -15 |
| | p-n-p, alloy, 540-1640 kc conv. | | | | -16 | -15 |
| 2N247 | p-n-p, alloy drift, class A rf | | | | -35 | -10 |
| 2N269 | p-n-p, alloy, lo-level switch | | 1 | | -20 | -100 |
| Raytheon Mfg. Co. | , Newton, Mass. | | | | | |
| 2N111 | p-n-p, fused, if-rf | 150 | 85 | | -30 | -200 |
| 2N111A | p-n-p, fused, if | 1 | 1 | | | |
| 2N112 | p-n-p, fused, if-rf | | | | | |
| 2N112A | p-n-p, fused, if | | | | | |
| 2N113 | p-n-p, fused, rf, switch | | | | | |
| 2N114 | p-n-p, fused, rf, switch | | | | | |
| 2N271 | p-n-p, fused, mixconv. bdcst. | | | | | |
| 2N271A | p-n-p, fused, if | | | | | |
| CK7da | p-n-p, fused, if-rf | 150 | 1 | | - | -100 |
| Sprague Electric Co | o., North Adams, Mass. | | | | | |
| 2N159 | n, point contact, pulse, sw. ⁵ | 100 | 80 | 2,0(a) | -50 | -40 |
| PC6 | n, point contact, comp. sw. ⁵ | 150 | 80 | 3.0(g) | -80 | -60 |
| SB101 | p-n-p, sbt, if-rf osc., amp. | 10 | 85 | 0.18(a) | -5 | -5 |
| 58102 | p-n-p, sbt, if-rf osc., amp. | 1 | 1 | 0.18(a) | 1 | 1 |
| 58103 | p-n-p, sbt, if-rf osc., amp. | | | 0.18(a) | | |
| SB5122 | p-n-p, sbt, hi-speed switch | | 65 | 0.28(a) | -6 | -15 |
| Svivenia Electric B | roducts, Inc., Woburn, Mass. | | | | | |
| 2N94 | n-p-n, alloy, hf | 50 | 75 | 1.0(a) | 20 | 50 |
| 2N94A | n-p-n, alloy, hf, switch | 1 | í | 1.0(0) | 20 | 1 |
| 2N193 | n-p-n, alioy, hf osc. | | | | 15 | |
| 2N194 | n-p-n, alloy, hf mixer | | | | 25 | |
| 2N211 | n-p-n, alloy, hf osc. | | | | 10 | |
| | | | | | | |
| 2N212 | n-p-n, alloy, hf mixer | 50 | 75 | 1.0(a) | 10 | 50 |
| 2N216 | n-p-n, alloy, if amp. | | | | 15 | |
| 2N233 | n-p-n, alloy, hf | 1 | I | 1 | 10 | |
| 2N377 | n-p-n, alloy, hf, switch | 150 | 85 | 2.5(a) | 20 | 200 |
| 2N385 | n-p-n, alloy, hf, switch | | | | 25 | |
| 2N388 | n-p-n, alloy, hf, switch | 1 | 1 | 1 | | 1 |
| Texas Instruments | Inc., Dallas, Texas | | | | | |
| 2N332' | n-p-n, grown, Si, gen. purpose | 150 | 175 | 0.116(b) | 45 | 25 |
| 2N333' | n-p-n, grown, Si, gen. purpose | | | 1 | | 1 |
| 2N334' | n-p-n, grown, Si, gen. purpose | | | | | |
| 2N335' | n-p-n, grown, Si, gen. purpose | | | | | |
| 2N336' | n-p-n, grown, Si, gen. purpose | | | | | 1 |
| 903' | n-p-n, grown, Si, gen. purpose | 150 | 175 | 0.116(b) | 30 | 25 |
| 904' | n-p-n, grown, Si, gen. purpose | 1 | 1 | 0.110(5) | 1 | ĩ |
| 904A' | n-p-n, grown, Si, gen. purpose | 1 | 1 | | | |
| 905 | n-p-n, grown, Si, gen. purpose | | | | | |
| 910' | n-p-n, grown, Si, gen. purpose | | | | | |
| | | | | | | 1 |
| 2N263' | n-p-n, grown, Si, switch | 125 | 150 | 0.166(b) | 40 | 20 |
| 2N337' | n-p-n, grown, Si, switch | | | | | |
| 2N338' | n-p-n, grown, Si, switch | | | | 1 | |
| 925' | n-p-n, grown, Si, hi-freq. | | | | 30 | 10 |
| 926' | n-p-n, grown, Si, hi-freq. | | | | | |
| 3N32' | n-p-n, grown, Si, hi-freq. | | | | | |
| 3N33' | n-p-n, grown, Si, video, rf | | | | | |
| 3N34' | n-p-n, grown Si, video, rf | | | | | |

| βοια | Char I _{co} | acter NF | istics Cc | fco | Transistor |
|---------------------------------------|------------------------------------|-------------|------------------|--------------|--|
| | (μα) | | (μμf) | (Mc) | Parameter |
| 100 | 0.5 | | 40 | 15 | |
| 40 | 0.5 | | 40 | 6 | E. K. Novak |
| 25 | 1.0 | | 35 | 3 | |
| 50 80 | | | | 5.5 10 | |
| 00 | | | | 10 | T RANSISTOR characteristics are usually now given |
| 482 | -6 | 4.5 | 9.53 | 4.74 | by most manufacturers in h parameters. Occasion. |
| 48 ² 60 ² | -6 -16 | | 9.5 ³ | 74 304 | ally however, characteristics are available only in r |
| 80- | 2.5 | | 1.7* | 44 | parameters. Also, in some transistor circuit design problems, a more familiar physical representation of the transistor is permitted if the small signal param. |
| 25 | 1.0 | 10 | 12 | 3 | eters of the transistor are expressed as resistances, |
| 25 30 | | 10 | | 3 5 | Both systems of representation are useful and a typi- |
| 30 | | 10 | | 5 | cal design problem usually requires the application of |
| 45 | | 10 | | 10 | both h and r parameters. The time required to per. |
| 75 45 | | 10 | | 20 10 | form these conversions may be considerably reduced |
| 45 | | | | 10 | by application of these tables. All equations given are in the exact form and are derived from the basic equiv. |
| 20 | 1 | | 15 | 2.5 | alent circuits given in Fig. 1. The r parameters are |
| | | | | | given for the common base, common emitter and |
| 3 | 0.5 ma 1.0 ma | 43 43 | 0.5 0.5 | 5 5 | common collector connections; the z and h parameters |
| 23 | 500 | 20 | 3.5 | 45 | are given in their general form and will represent the |
| 40 | | | | 45 | CB, CE or CC connection when the subscripts b , e or |
| >6 | 1000 | 1 | 1 | 60 | c, respectively, are added to each parameter. For example, the input impedance in the general four terminal network h parameters form is h_{II} ; h_{IIb} is the input |
| 0.97° | 507 | | 10 | 2 | impedance for the common base connection, h_{11e} is |
| 0.98 ⁶ 7.5 ⁶ | 50 ⁷ 40 ⁷ | | 10 | 5 2 | the input impedance for the common emitter connec- |
| 8.04 | 407 | | 11 | Î | tion, \hat{h}_{11c} for the common connector. |
| 106 | 207 | | 10 | | The h parameters are given by manufacturers in |
| 106 | 207 | | 10 | 4 | either of the two following forms: |
| 7.5 ⁶ 4.5 ⁶ | 407 1507 | | 11 | 2 | For common base: |
| 30* | 207 | | 15 | 4 | $h_{11b} = \text{input impedance} = h_{a}$ |
| 608 | 357 | | 15 | 4 | h_{12b} = reverse transfer, or feedback voltage ratio = h_{ib} h_{21b} = forward, or current transfer ratio = h_{ib} |
| 808 | 207 | | 15 | 8 | h_{22b} = output admittance = h_{ob} |
| 0.925 | 4 | 20 | 710 | 4 5 | Since the majority of the literature is written in the nomenclature of the left hand column it is used in |
| 0.975 | | | | 8 | these tables. |
| 0.980 | | | | 6 | Use of the tables is illustrated by the following |
| 0.990 | 1 | 1 | -10 | 7 | simple example. |
| 0.925 | 0.1 | 25 34 | 710 | 4 | The characteristics of a Type 903 grown junction |
| 0.975 | | 25 | | 8 | |
| 0.980 | | 25 20 | | 6 7 | |
| 0.990 | 1.0 | 20 | 3 | 30 | 1. Has flexible leads. |
| 0.975 | | | 3 | 20 | 2. Current transfer ratio, common emitter circuit. |
| 0.975 | 1.0 | | | 30 | 3. Cb _{rc} 4. CB circuit. |
| | 0.2 | | 1.8 1.8 | 12.5 | All characteristic data for Grounded Base circuit. h_{fe}—small signal current gain. |
| | | | | 4.3 | 7. Maximum, emitter open. |
| 1 | | | | 12.5 30.0 | 8. hfe—dc current gain. 9. All characteristics given for design center, grounded base. 10. 1[MC design center. |
| | | | | | |

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s s

1

te Conversion Tables

silicon transistor are given in the manufacturer's data sheet as follows:

| $h_{11b} =$ | 42 ohms |
|-------------|------------------------|
| $h_{12b} =$ | $120	imes10^{-6}$ |
| | -0.925 |
| $h_{22b} =$ | $0.4	imes10^{-6}$ mhos |

Since these parameters are given for the common base connection, calculation of the characteristics of a common emitter amplifier, for example such as in Figure 1c, requires conversion of the given values to their common emitter equivalent. Using Table I:

> $h_{11e} = \frac{h_{11b}}{(1 + h_{21b}) (1 - h_{12b}) + h_{11b} h_{22b}}$ = 560 ohms

similarly:

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 $= h_j$

 $= h_o$

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base

1957

 $h_{12e} = 104 \times 10^{-6}$ $h_{21e} = 12.3$ $h_{22e} = 5.33 \times 10^{-6}$ mho

Also from Table I, the common collector h parameters are:

| $h_{11c} = 560 \text{ ohms}$ |
|--------------------------------------|
| $h_{12c} = 1.0$ |
| $h_{21c} = 13.3$ |
| $h_{22c} = 5.33 \times 10^{-6}$ ohms |

When calculations in terms of r parameters are required, Table II and the above results give:

| r_b | = | 300 ohms |
|---------|---|---------------|
| r_c | = | 2.5 megohms |
| r_d | = | 0.187 megohms |
| r_{e} | = | 19.5 ohms |
| r_m | = | 2.3 megohms |
| | | |

Other conversions are carried out similarly. For the transformation of g parameters, the following relations can be used in conjunction with the tables:

$$h_{11} = \frac{1}{g_{11}}, h_{21} = \frac{g_{21}}{g_{11}}$$
$$h_{12} = \frac{-g_{12}}{g_{11}} = \frac{(g_c - g_{22})}{g_{21}}$$
$$h_{22} = g_c = \frac{1}{r_{22}}$$

Continued on page 12



New Clevite Germanium - Silicon Alloy Gold Bonded Glass Diodes, now available for immediate delivery.

Better high temperature performance than germanium.

Higher forward conductance at lower voltages than silicon.

All germanium RETMA specifications can now be met at higher temperatures with these new Germanium-Silicon alloy diodes... plus increased reliability at all temperatures.

For complete information write or phone for Engineering Bulletin B-215.







A Division of Clevite Corporation

CIRCLE 505 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN . July 15, 1957

High Frequency, Switching (cont.)

| Manufacturer and Type | Class and Application | W _c (mw) | Ti | (a)mw/C (b)C/mw | Vc | l _c (ma) |
|--------------------------|--------------------------------|------------------------|-----|--------------------|------|------------------------|
| Texes Instruments | Inc. (cont.) | | | | | |
| 2N252 | p-n-p, grown diff., conv. | 30 | 55 | | 16 | 5 |
| 2N308 | p-n-p, grown diff., if amp. | | | | 20 | |
| 2N309 | p-n-p, grown diff., if amp. | | | | 20 | |
| 2N310 | p-n-p, grown diff., if reflex | 1 | 1 | | 30 | |
| 2N172 | n-p-n, grown, conv. | 65 | 75 | 0.7(ь) | 16 | 5 |
| 2N145 | n-p-n, grown, 455 kc if | | 1 | 1 | 20 | |
| 2N146 | n-p-n, grown, 455 kc if | | | | 1 | |
| 2N147 | n-p-n, grown, 455 kc if | | | | | |
| 2N148 | n-p-n, grown, 262 kc if | | 1 | 1 | 32 | 1 |
| 2N149 | n-p-n, grown, 262 kc if | 65 | 75 | | 32 | 5 |
| 2N150 | n-p-n, grown, 262 kc if | 1 | 1 | | 32 | 1 |
| 2N253 | n-p-n, grown, 455 kc if | | | | 12 | |
| 2N254 | n-p-n, grown, 455 kc if | | 1 | | 20 | |
| Transitron Electror | nics Corp., Melrose, Mess. | | | | | |
| STIO | n-p-n, grown, Si, gen. purpose | 200 | 175 | | 15 | |
| ST30 | n-p-n, grown, Si, gen. purpose | | 1 | | 30 | |
| 5T40 | n-p-n, grown, Si, gen. purpose | | | | 45 | |
| STII | n-p-n, grown, Si, med. gain | | | | 15 | |
| ST31 | n-p-n, grown, Si, med. gain | | | | 30 | |
| 5741 | n-p-n, grown, Si, med. gain | | 1 | | 45 | |
| ST12 | n-p-n, grown, Si, hi gain | 200 | 175 | | 15 | |
| 5T32 | n-p-n, grown, Si, hi gain | | 1 | | 30 | |
| ST42 | n-p-n, grown, Si, hi gain | | | | 45 | |
| ST13 | n-p-n, grown, Si, hf | | | | 15 | |
| 5733 | n-p-n, grown, Si, hf | | 1 | | 30 | |
| Western Electric C | e., New York, N. Y. | | | | | |
| 2N673 | point contact, switch | 100 | | | -50 | -50 |
| 2N1103 | point contact, switch | 200 | | 3.3(a) | -50 | -50 |
| 3N223 | n-p-n, grown, video amp. | 30 | | | 10 | 3 |
| GA528293 | p-n-p, alloy, gen. purpose | 120 | 85 | 2.0(a) | -65 | -50 |
| GA528303 | p-n-p, alloy, core-driver | 500 | 80 | | -40 | -500 |
| GA530803 | point contact, switch | 250 | | | -100 | -50 |
| GA532423 | p-n-p, alloy, switch | 500 | 80 | | -40 | -500 |
| GA531493 | p-n-p, alloy, gen. purpose | 120 | 85 | 2.0(a) | -65 | -50 |
| GA532333 | p-n-p, diffused, vhf osc. | 200 | 1 | 5.0(a) | -35 | -30 |
| GA532703 | n-p-n, alloy, gen. purpose | 120 | | | 30 | 30 |

Power Transistors

| | Class and Application | Maximum Ratings | | | | | |
|--------------------------|------------------------------|------------------------|-----|------------------|---------------------------|--------------------------|--|
| Manufacturer and Type | | W _c (W) | | (а)W/С (ь)C/W | V _c (volts) | l _c (amp.) | |
| Bendix Aviation Ca | orp., Red Bank Dive | | | | | | |
| Long Brench, N. J. | | | | | | | |
| 2N235A | p-n-p, alloy, audio pwr. | 254 | 90 | 2(a) | -40 | 3 | |
| 2N234A | p-n-p, alloy, pwr. | | 90 | | -30 | 3 | |
| 2N285A | p-n-p, alloy, hi-gain audio | | 95 | | 40 | 3 | |
| 8-114 | p-n-p, alloy, audio pwr. | | 100 | | 40 | 3 | |
| X-140 | p-n-p, alloy, audio pwr. | | 95 | | 40 | 3 | |
| X-119 | p-n-p, alloy, class B audio | | 90 | | 40 | 3 | |
| X-145 | p-n-p, alloy, class B audio | | 90 | | 40 | 3 | |
| X113 | p-n-p, alloy, hi-current sw. | | 100 | | 70 | 4 | |
| X133 | p-n-p, alloy, hi-current sw. | | 1 | | 80 | 5 | |
| X134 | p-n-p, alloy, hi-current sw. | 504 | | 1.5(a) | 40 | 12 | |
| X137 | p-n-p, alloy, hi-current sw. | 504 | | 1.5(a) | 80 | 12 | |

| | | | | | Basic Equivalent Circuits | |
|--|-----------------------------------|-----------------|----------------|-------------------------|---|----------|
| | Char | acteri | stics | | (Small Signal Parameters) | |
| β or α | Ι _{co} (μα) | NF (db) | C _c | f _{co} (Mc) | (7-77-) | |
| | 10 3 | | 6' | | $ \begin{array}{c c} & z_{22}z_{12} \\ & z_{12} \\ &$ | Bei J |
| 25 | 3 0.005 ² | 22 | 7 | 9 | | Bo |
| 45 45 45 | | 20 20 20 | | 13 13 13 | | CB |
| 40 | 0.005 ² | 19 | 7 | 16 | $\begin{array}{c c} & & & \\ &$ | CI |
| 60 60 | | | 10 10 | 17 17 | | W |
| | 450 | | | 10 | | |
| 0.98 | 1300 1.0 4.5 | <10 | 2 17 | 10 20 3 | ie re - + re ic | K |
| | 10 | | 40 | 4 | | |
| | 1000 10 | | 40 | 15 | ve Zrb vc | |
| | 4.5 | 10 | 22 | 3 | | G |
| | 13 3 | 4.5 | 4 20 | 500 3 | r PARAMETERS-CB | L |
| | | | | | (d) | L |
| | Cha | racter | istics | | | |
| β or α | | f _{co} | pwr. gain | pwr. out. | | |
| pora | l _{co} (ma) | (Mc) | (db) | (W) | ·• >·• | |
| 60 | 1.0 | 0.007 | 35 | 2 | r PARAMETERS -CE (e) | |
| 30 100 | | | 30 38 | 2 | Continued on page 15 | |
| 50 | | | 34 | 5 | | |
| 100 50 | | 0.008 | 34 25 | 6 96 | | I |
| 40 40 ⁵ 40 ³ 15 ⁵ 15 ⁵ | I | 0.008 | 27 | 56 | Coe design center. At 6 v, 25 C. Military Type. With heat sink. hfe dc Beta. Two units. | |
| | | | | | ELECTRONIC DESIGN • July 15, 1957 | 1 |

Typical Switching Operation

| Manufact | | Rise | Stor- age Time | Fall Time | | Leak Cur. | |
|-----------------|---------------|-------|----------------------|--------------|------|--------------|-------|
| and Ty | pe | (μs) | | (μs) | | (µa) | |
| Bendix Aviatio | | | | | | | - |
| Long Branch, I | N. J. | | | | | | |
| X110 | pwr. | 100 | | 200 | 2 | 1000 | 40(a) |
| X113 | pwr. | | | | 2 | 8000 | 40(a) |
| X133 | pwr. | | | | | 2000 | 40(a) |
| X134 | pwr. | | | | | 4000 | 15(a) |
| X137 | pwr. | | | | | 4000 | 15(a) |
| Bogue Elec. Mi | | | | | | | |
| Paterson, N. J | | | | | | | |
| RD316 | | | | | 2.5 | | 10(a) |
| 2N160 | | 0.3 | | 0.4 | 1.25 | | 15(a) |
| 2N161 | | 0.3 | | 0.4 | | | 30(a) |
| 2N162 | | 0.2 | | 0.3 | | | 35(a) |
| 2N163 | | 0.25 | | 0.35 | | | 50(a) |
| XJOA | pwr. | | | | | | 12(a) |
| X31A | pwr. | | | | | | |
| X32A | pwr. | | | | | | 1 |
| CBS-Hytron | | | | | | | |
| Lowell, Mass. | | | | | | | |
| 2N182 | | 0.7 | 8.0 | 0.5 | 0.15 | 7.5 | 25(Ь) |
| 2N183 | | 0.5 | 0.7 | 0.3 | | 120 | 50(Ь) |
| 2N184 | | 0.3 | 0.6 | 0.2 | | 180 | 100(b |
| Clevite Transis | stor Prod. | | | | | | |
| Waltham, Ma | | | | | | | |
| 2N257 | pwr. | | | | | 2000 | 100(a |
| 2N268 | pwr. | | | | | 2000 | 100(a |
| 2N297 | pwr. | | | | 1.0 | 3000 | 100(a |
| CTP117 | pwr. | 1 | | | | 2000 | 60(a |
| Deico Radio | | | | | | | |
| Kokomo, Ind. | | | | | | | |
| 24278 | pwr. | 50 | | 80 | 0.6 | 15ma | 80(b) |
| 2N277 | pwr. | 50 | | 80 | 0.6 | 1.5ma | 80(b |
| 2N174 | pwr. | 60 | | 100 | 0.6 | 1 5 ma | 50(b |
| 2N173 | pwr. | 50 | | 80 | 0.6 | 1.5ma | 80(b |
| General Elect | ric Co. Ltd. | | | | | | |
| London, Engle | and | | | | | | |
| GETIO | | 1 | 3.5 | 4.5 | 40 | 6 | 40(a |
| Lonsdale Tub | e Co. (Philco | ») | | | | | |
| Lansdale, Pa. | | | | | | | |
| 2N352 | pwr. | | | | 0.47 | | 65(a |
| 2N353 | pwr. | | 0.5 | | 1 | | 90(a |
| 2N386 | pwr. | | | | | | 85(a |
| 2N387 | pwr. | | | | | | 85(a |
| 2N224 | | | | 0.29 | 0.25 | | 75(a |
| 2N226 | | | | 0.36 | 0.25 | | 55(a |
| 2N240 | h.f. | | | | 0.06 | | 65(a |
| 2N393 | h.f. | | | | 0.05 | | 93(a |
| 2N355 | h.f. | 0.038 | 3 | 0.09 | 0.08 | 1 | 50(a |
| T1164 | | 9 | | | | | 20(c |
| Minneapolis- | Honeywell | | | | | | |
| Minneapolis, | | | | | | | |
| HS | pwr. | 4 | 3 | 1 | 0.36 | - 500 | 30(c |
| H6 | pwr. | 1 | 1 | 1 | 1 | 1 | 42(c |
| H7 | pwr. | | | | | 1 | 60(c |
| | - | | | | - | - | |

D

e 15

957

H3A

H4A

H10

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| | Peak Re- current | Forv Volt | mum vard tage 5°G Its) | Max | imum Inv Current (Jua) | rorso | Forv | vard |
|---------------|------------------------|--------------|------------------------------------|------|------------------------------|-----------------|------|-------|
| 1-1 | Voltage (volts) | 100ma | 200ma | 25°C | 150°C | Test Voltage | 25.0 | 150-0 |
| PS 606 | 80 | 1.1 | 2 | .250 | 30 | - 70 | 125 | 50 |
| PS 611 | 80 | | 1.0 | .025 | 5 | - 70 | 200 | 100 |
| PS 618 | 200 | 1.1 | | .250 | 30 | - 180 | 125 | 50 |
| PS 623 | 200 | 1 C | 1.0 | .025 | 5 | - 180 | 200 | 100 |
| PS 630 | 330 | 1.1 | | .250 | 50 | - 300 | 125 | -50 |
| PS 633 | 330 | | 1.0 | .100 | 25 | - 300 | 200 | 100 |
| PS 634 | 420 | 1.1 | - | .250 | 50 | - 380 | 125 | 50 |
| PS 637 | 420 | | 1.0 | .100 | 25 | - 380 | 200 | 100 |
| | | | | | | | | |
| - | | | | | - | - | - | |

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ELECTRONIC DESIGN . July 15, 1957

pwr.

pwr.

pwr.

150

150

1000

12(a)

22(a)

20(a)

xiii

Power Transistors (Cont.)

¥.

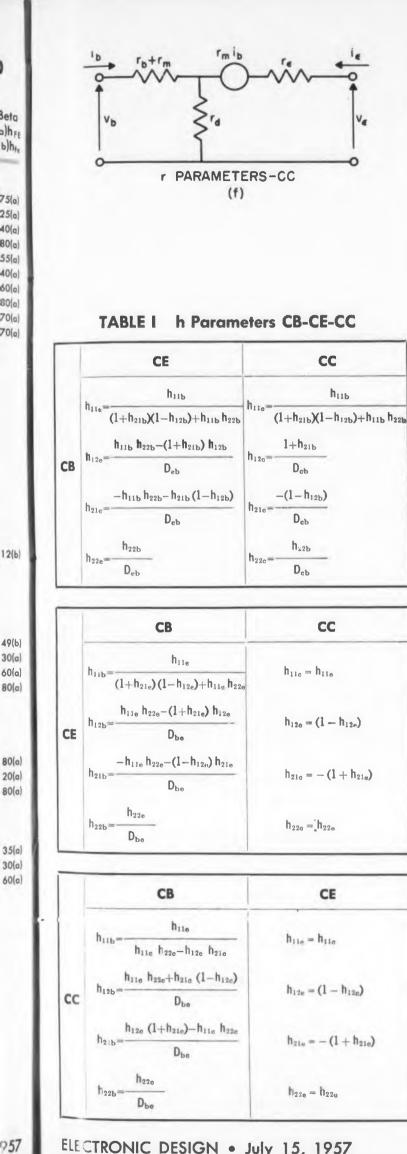
Maximum Ratings

| Manufacturer and Type | Class and Application | ₩. (₩) | т (С) | (а)W/С (ь)С/W | V _c (volts) | l _c (amp.) |
|------------------------------------|--|-----------------------------------|----------|------------------|---------------------------|--------------------------|
| Bogue Electric Mfg. | Co., Paterson, N. J. | | | | | - |
| XJOA | n-p-n, grown, Si, audio, servo | 81 | 175 | 0.1(a) | 40 | 0.20 |
| X31A | n-p-n, grown, Si, audio, servo | 101 | | | 80 | 0.16 |
| X32A | n-p-n, grown, Si, audio, servo | 101 | l | | 125 | 0.14 |
| BS-Hytron, Lowel | l, Mass. | | | | | |
| 2N155 | p-n-p, alloy, pwr. | 8.51 | 8.5 | 0.14(a) | -30 | -3 |
| 2N156 | p-n-p, alloy, pwr. | 8.51 | 1 | 0.14(a) | -30 | 1 |
| 2N158 | p-n-p, alloy, pwr. | 8.51 | | 0.14(a) | -60 | |
| 2N255 | p-n-p, alloy, pwr. | 6.251 | | 0.10(a) | -15 | |
| 2N256 | p-n-p, alloy, pwr. | 6.25 ¹ | 1 | 0.10(a) | -30 | 1 |
| Clevite Transistor F | Products, Waltham, Mass. | | | | | |
| 2N257 | p-n-p, alloy, pwr. amp., sw. | 371 | 90 | 0.5(a) | 40 | 3 |
| 2N268 | p-n-p, alloy, pwr. amp., sw. | 371 | 90 | 0.5(a) | 80 | 3 |
| 2N2972 | p-n-p, alloy, pwr. amp., sw. | 151 | 85 | 0.25(a) | 60 | 3 |
| CTP1117 | p-n-p, alloy, pwr. amp., sw. | 431 | 90 | 0.67(a) | 40 | 6 |
| Delco Radio, Kokor | no, Ind. | | | | | |
| 2N278 | p-n-p, alloy, pwr. | 701 | 95 | 1(ь) | 50 | 13 |
| 2N277 | p-n-p, alloy, pwr. | 1 | 1 | 1 | 40 | 1 |
| 2N174 | p-n-p, alloy, pwr. | | | | 80 | |
| 2N173 | p-n-p, alloy, pwr. | 1 | 1 | Ţ | 60 | 1 |
| General Electric Ca | . Ltd., London, England | | | | | |
| GET7 | p-n-p, alloy, dc conv. | 141 | 75 | 1.5(b) | -15 | 8 |
| GETS | p-n-p, alloy, audio output | 1 | | | -30 | 1 |
| GET9 | p-n-p, alloy, volt. reg. | 1 | l | | -60 | 1 |
| ansdale, Pa. | Div. of Philco Corp., | | | | | |
| 2N352/T1040 | p-n-p, alloy, audio out., sw. | 71 | 100 | З(Ь) | -40 | -2 |
| 2N353/T1041 | p-n-p, alloy, audio out., sw. | 101 | 100 | 2.5(Ь) | -40 | -2 |
| 2N386/T1167 | p-n-p, alloy, servo, pwr. sw. | 12.51 | 100 | 2(b) | -60 | -3 |
| 2N387/T1168 | p-n-p, alloy, servo, pwr. sw. | 12.51 | 100 | 2(ь) | -80 | -3 |
| | well Regulator Co., | | | | | |
| Minneapolis, Minn. | | | | 0.0(1.) | | |
| N5* | p-n-p, alloy, servo, dc conv. | 204 | 95 | 2.2(b) | -80 | -3 |
| H6* H7* | p-n-p, alloy, servo, dc conv. | 206 | | 2.2(b) | -80 | -3 |
| H7* H3A* | p-n-p, alloy, servo, dc conv. | 20 ⁶ 3 ⁶ | | 2.2(b) | -80 | -3 |
| H3A" H4A" | p-n-p, alloy, servo amp. p-n-p, alloy, servo amp. | 30 | | 14(b) 14(b) | -60 -60 | -3.5 -0.5 |
| H10 | p-n-p, alloy, servo amp. p-n-p, alloy, dc conv. | 55 | | 0.8(b) | -60 -60 | -0.5 -15 |
| Motorola Inc., Sem | iconductor Product Div., | | | | | |
| Phoenix, Arizona | | | | | | |
| 2N176 | p-n-p, fused, audio pwr. | 10 | 90 | 1 (m) | 40 | 3 |
| MN21 | p-n-p, fused, high-volt. | 1 | 1 | 1 | 80 | |
| MN24 | p-n-p, fused, audio pwr. | | | | 40 | |
| MN25 | p-n-p, fused, audio pwr. | | | | 40 | |
| | p-n-p, fused, audio pwr. | | | | 40 | |
| MN26 | | | | | 30 | |
| MN28 | p-n-p, fused, audio pwr., sw. | | | | | |
| | p-n-p, fused, audio pwr., sw. p-n-p, fused, audio pwr., sw. | 1 | I | Į. | 40 | 1 |
| MN28 MN29 Nucleonic Products | p-n-p, fused, audio pwr., sw. s Co., Los Angeles, Calif. | 1 | l | I | 40 | 1 |
| MN28 MN29 | p-n-p, fused, audio pwr., sw. | 10 | 90 |] 1(a) | 40 -40 | 3 |

Typical Switching Operation (cont.)

| | Char | acteri | stics | | | | | - | | | | |
|---------------------|-------------------------|-------------------------|----------------------|---------------------|---|--|--------------|------------------------------|---------------|----------------------|----------------------|-------------------------|
| β or α | l _{co} (ma) | f _{co} (Mc) | pwr. gain (db) | pwr. out. (W) | Manufacturer and Type | | Rise Time | Stor- age Time (µs) | Time | Sat. Volt. (V) | Leak Cur. (µa) | (a)he |
| | | | | | Motorola Inc. | 1 | | | | | | - |
| 15 | | | 32 | 2 | Phoenix, Ariz. 2N176 MN13A MN13B | pwr. | 50 7 | 10 2 | 80 9 12 | 0.6 0.2 | 1000 30 | 75(a) 25(a) 40(a) |
| | | | | | MN13C MN21 | | | 1 | 12 | | | 80(a) |
| 10 | 0.40 | 0.145 | | | MN24 | pwr. | 50 | 10 | 80 | 0.6 | 1500 | 55(a) 40(a) |
| 40 | 0.42 | 0.145 | 33 33 | 2 | MN25 | pwr. | | | | | 1 | 60(a) |
| 41 | 0.26 | 0.180 | 37 | 2 | MN26 | pwr. | | | | | | 80(a) |
| 30 | | 0.145 | 19-26 | 1 | MN28 | pwr. | | | | | 2000 | (9) |
| 30 | | 0.145 | 22-29 | 2 | MN29 | pwr. | 1 | 1 | 1 | 1 | 2000 | 70(a) |
| | | | | | RCA | | | | | | | |
| | | | | | Somerville, N | . J. | | | | | | |
| | 2 | 0.33 | 33 | 2.5 | 2N269 | | | | | 0.15 | -4 | |
| | 2 | 1 | 31 | 2.5 | | | | | | | | |
| | 3 | | | | Raytheon Mfg | | | | | | | |
| | 2 | 1 | 33 | 5.0 | Newton, Mass 2N113 | ₿. b.f. | 0.1 | | 0.14 | | | |
| | | | | | 2N113 2N114 | h.t. h.f. | 0.1 0.05 | | 0.15 | | | |
| | | | | | P1194 | п.т, | 0.05 | | 0.15 | | | |
| | | 0.34 | 40 | | Sprague Elec. | Co. | | | | | | |
| | | 0.34 | 40 | | North Adams, | | | | | | | |
| | | 0.154 | 38 | | 2N159 | | 0.12 | 1.5 | 0.5 | | | |
| | | 0.34 | 40 | | PC6 | | 0.05 | 1.0 | 0.5 | | | |
| | | | | | 5B5122 | | 0.015 | 0.065 | 0.015 | -0.1 | -200 | 12(Ь) |
| | | | | | Sylvania Elec. | Prod. | | | | | | |
| 20 | .062 | 0.25 | 46 | 20 | Woburn, Mas | | | | | | | |
| | | | | | 2N34 | | 1.0 | 2.0 | 2.0 | | | |
| | 1 | 1 | 1 | | 2N35 | | 1.0 | 1.5 | 2.0 | | | |
| | | | | | 2N94A | h.f. | 0.3 | 0.4 | 0.6 | | | 49(b) |
| | | | | | 2N377 | h.f. | 1 | 1 | 1 | 0.75 | | 30(a) |
| | | | | | 2N385 | h.f. | | | | 0.75 | | 60(a) |
| | 3 | 0.0165 | 36 | | 2N388 2N325 | h.f. | 0.6 5 | 0.6 10 | 0.6 5 | 0.75 0.6 | | 80(a) |
| | 3 | 1 | 36 | | 211323 | pwr. | Э | 10 | 5 | 0.0 | | |
| | 5 5 | 1 | 33 33 | | Texas Instrum Dallas, Texas | | | | | | | 00(1) |
| | | | | | 2N263 | | 0.06 0.05 | 0.02 | 0.14 | | | 80(a) 20(a) |
| | | | | | 2N337 2N338 | | 0.05 | | 0.08 | | | 20(a) 80(a) |
| 50° | -0.5 | >0.008 | 31 | 10 | 1.1.000 | | 0.00 | | 0.14 | | | |
| 759 | -0.5 | >0.008 | | 10 | Tung-Sol Elec | . Inc. | | | | | | |
| 140° | -0.5 | | | 10 | East Orange, | N. J. | | | | | | |
| 12' | 0.1510 | | 21 | 2 | T5612 | pwr. | 25 | | 40 | 1.0 | | 35(a) |
| 159 | 0.1510 | | 23 | 3 | TS613 TS614 | pwr. | | | | | | 30(a) 60(a) |
| | | | | | 13014 | | 1 | | 1 | 1 | | 00(0) |
| | | | | | Western Elec | tric Co. | | | | | | |
| | | | | | New York, N | . Y. | | | | | | |
| | | | | | 2N110 | | 90 | | 1.7 | | | |
| 45 | <1 | 0.007 | 34 | 2 | GA52830 | | 0.45 | | 0.6 | | | |
| 65 | 1.5 | | 37 | 5 | GA53242 | | 0.45 | 1.1 | 0.6 | | | |
| 40 | <1 | | 31 33 | 4 | - | | | | | | - | |
| 80 | <1 | | 35 | 4 | | 1. With he | mt atal. | | | | | |
| 60 | 2 | | 31 | 2 | - 1 | 2. Military | | | | | | |
| 60 | 2 | | 33 | 2 | | 3. Commo | n base ci | | | | | |
| | | | | | | 4. Ground 5. β _{co} , gro | | | | | | |
| | | | | | | 6. At a ma | ounting b | ase tem | | | | |
| 60 | 3 | 0.006 | 33 | | | 7. Two unit | | push-p | ull, com | mon en | nitter. | |
| 50 | 0.3 | | | | | 8. DC beta 9. I _{cbo} at a | | | | | | |
| | | | | | | | | | | | | |

ELECTRONIC DESIGN . July 15, 1957



"SOMEBODY STOLE MY 126"*

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Technical Data Immediately Available

AMERICAN ELECTRONIC LABORATORIES, INCORPORATED

121 N. SEVENTH STREET PHILADELPHIA 6, PENNSYLVANIA



CIRCLE 507 ON READER-SERVICE CARD FOR MORE INFORMATION

Power Transistors (Cont.)

Maximum Ratings

| Manufacturer and Type | Class and Application | ₩ _c (₩) | T _i (C) | (а)W/С (ь)C/W | V _c (volts) | l _c (amp. |
|--------------------------|--|-----------------------|-----------------------|------------------|---------------------------|-------------------------|
| Pye Industrial Elect | ronics, Ltd., | | | - | | |
| Newmarket, Engla | nd | | | | | |
| V15/10P | p-n-p, alloy, pwr., óv dc conv. | 102 | 75 | 0.2(g) | -15 | -3 |
| V15/20P | p-n-p, alloy, pwr., 6v dc conv. | I | 1 | 1 | -15 | 1 |
| V15/30P | p-n-p, alloy, pwr., óv dc conv. | | | | -15 | |
| V30/10P | p-n-p, alloy, pwr., 12v dc conv. | | | | -30 | |
| V30/20P | p-n-p, alloy, pwr., 12v dc conv. | | | | -30 | |
| V30/30P | p-n-p, alloy, pwr., 12v dc conv. | | | | -30 | |
| RCA, Somerville, N. | . J. | | | | | |
| 2N3014 | p-n-p, alloy, Ige. sig. audio pwr. | 122 | 85 | | -40 | -2 |
| 2N301A4 | p-n-p, alloy, Ige. sig. audio pwr. | 122 | 85 | | -60 | -2 |
| Sylvania Electric Pr | oducts Co., Woburn, Mass. | | | | | |
| 2N68 | p-n-p, alloy, pwr. | 42 | 75 | 0.08(a) | -30 | 1.5 |
| 2N95 | n-p-n, alloy, pwr. | 1 | 1 | 1 | 1 | 1 |
| 2N101 | p-n-p, alloy, pwr | | | | | |
| 2N102 | n-p-n, alloy, pwr. | | | | | |
| | | | | | -10 | 0.0 |
| 2N141 | p-n-p, alloy, pwr. | | | | -60 | 8.0 |
| 2N142 | n-p-n, alloy, pwr. | | | | 60 | |
| 2N143 | p-n-p, alloy, pwr. | | | | -60 | |
| 2N144 | n-p-n, alloy, pwr. | 1 | 1 | | 60 | 1 |
| 2N155 | p-n-p, alloy, pwr. | 8.5 ² | 85 | 0.14(a) | | 3 |
| 2N176 | p-n-p, alloy, pwr. | 102 | 90 | 1(a) | | 3 |
| 2N235A | p-n-p, alloy, pwr. | 5 ² | 85 | 0.5(a) | -40 | 2 |
| 2N242 | p-n-p, alloy, pwr. | 25 ² | 100 | 0.33(a) | -45 | |
| 2N250 | p-n-p, alloy, pwr. | 122 | 80 | 0.22(a) | -30 | 1 |
| 2N257 | p-n-p, alloy, pwr. | 25 ² | 85 | 0.41(a) | -40 | |
| 2N296 | p-n-p, alloy, pwr. | 2.5 ² | 100 | 0.33(a) | -60 | 2 |
| 2N307 | p-n-p, alloy, gen. purp. pwr. | 1 5 ² | 75 | 0.3(a) | -35 | 1 |
| 2N325 | p-n-p, alloy, pwr. | 122 | 85 | 0.2(a) | -35 | 2 |
| 2N326" | n-p-n, alloy, pwr. | 72 | 85 | 0.12(a) | 35 | 2 |
| lexas Instruments i | inc., Dallas, Texas | | | | | |
| 95110 | n-p-n, grown, Si, med. pwr. | 0.75 ² | 150 | 116(Ь) | 50 | .060 |
| 952 ¹⁰ | n-p-n, grown, Si, med. pwr. | | 1 | | 80 | .050 |
| 95310 | n-p-n, grown, Si, med. pwr. | | | | 120 | .040 |
| 2N24310 | n-p-n, grown, Si, med. pwr. | | 1 | | 60 | .060 |
| 2N24410 | n-p-n, grown, Si, med. pwr. | | | 1 | 60 | .060 |
| 2N33918 | n-p-n, grown, Si, med. pwr. | 1.0 | | | 55 | .060 |
| 2N34010 | n-p-n, grown, Si, med. pwr. | 1.0 | | | 85 | .050 |
| 2N34110 | n-p-n, grown, Si, med. pwr. | 1.0 | 150 | 116(ь) | 125 | .040 |
| 2N34210 | n-p-n, grown, Si, med. pwr. | 1 | 1 | 1 | 60 | .060 |
| 2N34310 | n-p-n, grown, Si, med. pwr. | | | | 60 | .060 |
| 97010 | n-p-n, grown, Si, power | 8.75 | | 166(b) | 120 | .140 |
| 2N38910 | n-p-n, grown, Si, power | 37.5 | | 166(b) | 60 | |
| 2N250 | p-n-p, alley, audio amp. | 25 | 85 | 1.1(b) | -30 | 3.0 |
| 2N251 | p-n-p, alloy, audio amp. | 25 | 85 | 1.1(b) | -60 | 3.0 |
| fransitron Electron | ic Corp., Melrose, Mass. | | | | | |
| 2N83 | p-n-p, pwr. amp. | 10 | 85 | 0.16(a) | -66 | 2 |
| 28636 | p-n-p, pwr. amp. p-n-p, pwr. amp. | 1 | 1 | 0.10(0) | -66 | 3 |
| 2N84 | | | | | -50 | 2 |
| 2N84A | p-n-p, pwr. amp. p-n-p, pwr. amp. | | | | -50 | 3 |
| Tung-Sol Electric | nc., East Orange, N. J. | | | | | |
| TS176 | p-n-p, alloy, audio pwr. | 102 | 85 | 3(b) | -30 | 2 |
| T5612 | p-n-p, alloy, audio pwr. p-n-p, alloy, pwr. sw. | 1.52 | 1 | 5(5) | -30 | 3 |
| | | 1.52 | | | -40 | 3 |
| T5613 | p-n-p, alloy, pwr. sw. | 1 | | | | |
| T5614 2N307 | p-n-p, alloy, pwr. sw. p-n-p, alloy, audio pwr. | 1.52 | | 5(ь) | -60 -35 | 3 |
| Western Rissanta A | ., New York, N. Y. | | | | | |
| | | | | | | |

| | | | | | | TABLE II h P | arameters | to r Pa | rameters |
|------------------------------------|-------------------------|------------------------------|-------------------------------------|--------------------------------------|----------------|--|---|--|---|
| - | | acter | pwr. | pwr. | | СВ | CE | | cc |
| ora | l _{co} (ma) | f _{co} (Mc) | gain (db) | out. (W) | | $h_{11b} h_{22b} - h_{12b}(h_{21b} + 1)$ |) h _{12e} | | $1 - h_{\scriptscriptstyle 12e}$ |
| | | | | _ | re | h _{22b} | h _{22e} | | h _{22e} |
| 18 | 0.03 | 0.1 | | 121 | | h _{12b} | h _{11e} h _{21e} -h _{12e} | (h _{21e} +1) h ₁₁ | $h_{22e} + h_{21e}(1 - h_{12e})$ |
| 24 38 | | | | | r _b | h _{22b} | h _{22e} | | h _{22e} |
| 18 24 | | | | | | $1-h_{\rm 12b}$ | $1 + h_{2}$ | le | - h _{21e} |
| 38 | 1 | , | | 1 | r _c | h _{22b} | h _{22e} | _ | h _{22e} |
| 703 | -0.22 | | 305 | 125 | rd | $1+h_{\rm 21b}$ | $1 - h_1$ | le | h _{12e} |
| 70 ³ | -0.2 | | 305 | 125 | · a | h ₂₂₆ | h _{22e} | | h _{22e} |
| 406 | 5 | 0.4 | 23 | 0.6 | r.m. | $-\left\lceil \frac{h_{12b}+h_{21b}}{2}\right\rceil$ | $h_{12e} + h$ | 21e | $\begin{bmatrix} h_{12e} + h_{21e} \end{bmatrix}$ |
| | | | | | | h _{22b} | h _{22e} | | h ₂₂₀ |
| | | | 26 | | | TABLE IV | z Parame | tors CB. | CE-CC |
| | | | | | Г | | | | |
| 607 | 1 3.0 | 0.145 | 33 32 | 2 | | CE | | | сс |
| 607 | 2 5 | 0.007 | 35 35 | 2 2.5 | | $Z_{11e} = Z_{11b}$ $Z_{12e} = Z_{11b} - Z_{11b} - Z_{11b}$ | 7 | $Z_{11c} = Z_{22b}$ | |
| 507 | 1 | 0.006 | 33 | 1.5 | | $Z_{12e} = Z_{11b} = Z_{21e} = Z_{11b} = Z_{21e} = Z_{11b} = Z_{1$ | | $Z_{120} = Z_{22b}$ $Z_{210} = Z_{22b}$ | |
| 276 | 2 0.2 | 0.007 0.004 | 30 | | | $Z_{21e} = Z_{11b} = Z_{22e} = Z_{11b} = Z_{1$ | | | $- z_{12b}$ $- Z_{12b} - Z_{21b} + Z_{22b}$ |
| 257 | 15 | 0.003 | 20 | 3° | | 2220 - 2116 - | 2216 T 2226 | 2220 - 2116 | - 2126 - 2216 + 222 |
| 40 ⁶ 40 ⁶ | 0,5 0,5 | 0.1 <i>5</i> 0.1 <i>5</i> | 28 28 | 39 | - | 1 | | | |
| | | | | | | CI | B | | СС |
| .9411 | .005 .006 | | 30 | | | $Z_{11b} = Z_{11}$ | e | $Z_{11c} = Z_{11c}$ | $z_{12e} - Z_{21e} + Z_{22e}$ |
| | .008 .001 | | | | | $Z_{12b} = Z_{11}$ | $1_{0} - Z_{12_{0}}$ | $Z_{120} = Z_{220}$ | $- Z_{126}$ |
| .9711 | .001 | | | | | $Z_{21b} = Z_{11}$ | ie - Z _{21e} | $Z_{210} = Z_{220}$ | - Z ₂₁₀ |
| .9411 .9411 | .001 .001 | | | | | $Z_{22b} = Z_{22}$ | $z_{e} - Z_{21e}$ | $\mathbf{Z}_{220}=\mathbf{Z}_{220}$ | 9 |
| .9411 | .001 | | 30 | | - | 1 | | _ | |
| .9411 | | | | | | C | B | | CE |
| 312 1012 | .01 .01 | | 2813 | | | $Z_{11b} = Z_{11e} - Z_{1}$ | $z_{20} - Z_{21c} + Z_{220}$ | $Z_{11e} = Z_{11e}$ | $z_{12c} - Z_{21c} + Z_{21c} + Z_{22c}$ |
| 30 | 0.3 | .01214 | 31 | 1.5 | 0 | $Z_{12b} = Z_{11c} - Z_{2}$ | 21e | $\mathbf{Z}_{12e}=\mathbf{Z}_{22e}$ | - Z ₁₂₀ |
| 30 | 0.3 | .01214 | 31 | 1.5 | | $Z_{21b} = Z_{11c} - Z_{11c}$ | 12e | $\mathbf{Z}_{21e}=\mathbf{Z}_{22}$ | z_{21c} |
| 18 | 0,1 | 0.35 | | | | $Z_{22b} = Z_{11c}$ | | $\mathbf{Z}_{22e}=\mathbf{Z}_{22e}$ | |
| 17 | 0.08 | 0.4 | | | - | 1.0 | | | |
| 21 20 | 0.11 0.09 | 0.4 0.45 | | | 6 | 2. With | pull class B on heat sink. | | |
| | | | | | | 4. All ch | signal current t aracteristics for | CE operatio | |
| 50 | 0.3 | 0.009 | 32 | 2.5 | | 6. hfe cu | ransistors class B rrent gain. | push-pull. | |
| | | | 24 ¹ 23 ¹⁵ | 2615 | | | ry Type. | | |
| | | | 2915 | 52 ¹⁵ 54 ¹⁵ | | | aracteristics for | grounded b | 056 . |
| 20 | 15 | | | | | 11. Alpha 12. DC b | a design center. eta (min.) | | |
| | | | | | | 13. Comm 14. Desig | non emitter, 1 w n center. | out at 100 | С. |
| | 0.07 | 0.2 | | | | 15. Switch | h. | | |
| | | | | | | ELECTRO | NIC DESI | | |

ELECTRONIC DESIGN • July 15, 1957

h1

h,

h2

h

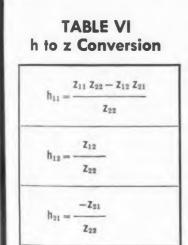
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***ABLE III** r Parameters to h Parameters

| | СВ | CE | СС |
|-----------------|---|--|---|
| h11 | $h_{11b} = r_{e} + r_{b} \left[\frac{r_{e} - r_{m}}{r_{e} + r_{b}} \right]$ | $h_{11e} = r_b + r_e \left[\frac{r_d + r_m}{r_d + r_e} \right]$ | $h_{11e} = r_b + \left[\frac{r_e r_e}{r_d + r_e} \right]$ |
| h ₁₂ | $r_{b} = \frac{r_{b}}{r_{c} + r_{b}}$ | $h_{12e} = \frac{r_e}{r_d + r_e}$ | $h_{12o} = \frac{r_d}{r_d + r_o}$ |
| h ₂₁ | $h_{21b} = -\left[\frac{\mathbf{r_m} + \mathbf{r_b}}{\mathbf{r_e} + \mathbf{r_b}}\right]$ | $h_{21e} = \frac{r_m - r_e}{r_d + r_e}$ | $h_{21e} = - \begin{bmatrix} r_e \\ \hline r_d + r_e \end{bmatrix}$ |
| h ₂₂ | $h_{22b} = \frac{1}{r_e + r_b}$ | $h_{22e} = \frac{1}{r_d + r_e}$ | $h_{22e} = \frac{1}{r_d + r_e}$ |

TABLE V r Parameters to z Parameters

| | СВ | CE | CC |
|-----------------|---------------------------------|---------------------------------|--------------------------------|
| z ₁₁ | $r_{b} + r_{e}$ | ſ _b + ſ _e | r _e +r _b |
| Z ₁₂ | ٢ _b | ľø | ۲ _d |
| Z ₂₁ | $r_m + r_b$ | r _e – r _m | ٢٥ |
| Z22 | r _o + r _b | $r_{e} + r_{d}$ | $r_e + r_d$ |



1

Z22

 $h_{22} = -$

TABLE VII z to h Conversion

4

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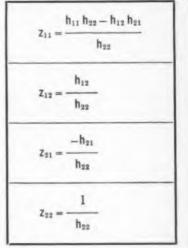


TABLE VIII z Parameters to r Parameters

| | CB | CE | СС |
|----------------|-------------------------------------|-------------------------------------|-------------------------------------|
| r. | $Z_{11b} - Z_{12b}$ | Z ₁₂₀ | Z ₂₂₀ - Z ₁₂₀ |
| r _b | Z12b | Z ₁₁₀ - Z ₁₂₀ | Z ₁₁₀ - Z ₂₁₀ |
| r _c | Z _{22b} - Z _{12b} | $Z_{22e} - Z_{21e}$ | Z ₂₁₀ |
| r _d | Z _{22b} - Z _{21b} | $Z_{22e} - Z_{12e}$ | Z120 |
| r _m | Z _{21b} - Z _{12b} | Z ₁₂₀ - Z ₂₁₀ | Z ₂₁₀ - Z ₁₂₀ |

957

h12e)

+ Z_{22b}

- Z_{22e}

- Z220

ELECTRONIC DESIGN . July 15, 1957

Types: IN536 thru IN540, IN1095

Hoffman

Types: IN456 thru IN459, IN461 thru IN464, IN482 thru IN488, A and B

Types: IN137A, IN138A, IN200 thru IN222, IN431, IN465 thru IN470, ZA8 thru ZA125. Double anode types IN471 thru IN475, IN225 thru IN235. (Silicon Junction Diodes will also be available in axial glass package)

Type: IN429

Types: IN430, IN430A, IN430B

Types: HMP1 thru HMP5 and 1A thru 5A; HDMP4 thru HDMP10 and 4A thru 10A

Tymes HFWRI thru HFWR3

Types: HZPR in Zener Voltage, voltages between 10 and 100 volts

 (\mathbf{H})

CIRCLE 508 ON READER-SERVICE CARD FOR MORE INFORMATION

Curve Tracers

| Manufacturer and Model | Maximum Base Current | Max. Collector Sweep Current and Frequency | Max. Coll. Sweep Power | Min. Load Resistance | Max. Sweep Volts | Auxillary Equip. Needed | Characteristics Displayed | internai Calib. | Accuracy | Price and Delivery | Size and Weight |
|-----------------------------------|----------------------------|--|------------------------------|-------------------------|------------------------|-------------------------------|------------------------------|--------------------|----------|-----------------------|--------------------|
| | | | | | | | | | | | |
| American Electronic Lab. | | | | | | | | | | | |
| 121 North Seventh Street | | | | | | | | | | | |
| Philadelphia 6, Pennsylvania | | | | | | | | | | | |
| 126H | 600 ma | 3 a | 30 w | | 150 v | Scope | Output, Input | Yes | | \$1,090.00 | 19" x 21" x 32" |
| 126R | (00 | 60 cps | | | | | | | | 4 weeks | 150 pounds |
| 1208 | 600 ma | 15 a | 200 w | | 200 v | Scope | Output, Input | Yes | | \$1,250.00 | 19" x 21" x 32" |
| | | 60 cps | | | | | | | | 10 weeks | 170 pounds |
| Cubic Corporation | | | | | | | | | | (Oscilloscope | |
| 5575 Kearney Villa Road | | | | | | | | | | \$425 extra) | |
| San Diego, 11 California | | | | | | | | | | | |
| 504 | .7 mu | 1/30 a | 1/2 w | | 18 v | 6 | 0.44 | | | | |
| | ., | 600 cps | 72 W | | 10 4 | Scope | Output | No | | \$325.00 | 2" x 3" x 8" |
| | | | | | | | | | | 30 days | 1 pound |
| ounn Engineering Associates, Inc. | | | | | | | | | | | |
| 186 Massachusetts Avenue | | | | | | | | | | | |
| Cambridge 39, Massachusetts | | | | | | | | | | | |
| 331 | l ma | 250 cps or 25 cps | | 1,300 ohm | 50 v | Scope | Output, Transfer | Yes | 3% | \$750.00 | 21" x 11" x 14 |
| | | Triangular Waveform | | ., | | ocope | | 163 | 5 % | 1 week | 65 pounds |
| | | | | | | | | | | IWECK | 00 poonds |
| airchild Guided Missiles Div. | | | | | | | | | | | |
| Wyandanch, L. I., New York | | | | | | | | | | | |
| 103A | 10 ma | 1/4 a | 2.5 w | | 100 v | Scope | Output, Transfer | Yes | 5% | \$650.00 | 19" x 13" x 10 |
| | | 60 cps | | | | | | | - /0 | 30 days | 35 pounds |
| | | | | | | | | | | | |
| Magnetic Amplifiers | | | | | | | | | | | |
| 632 Tinton Avenue | | | | | | | | | | | |
| New York 55, New York | | | | | | | | | | | |
| 200A | 10 ma | 1/10 a | 2 w | 100 ohm | 100 v | Scope | Output, Transfer | Yes | 21/2% | \$685.00 | 16" x 10" x 8" |
| 300A | | 60 cps | | | | | | | | 10 days | 18 pounds |
| 300A | 200 ma | 2 a | 5 w | l ohm | 100 v | Scope | Output, Transfer | Yes | 21/2% | \$785.00 | 16" x 10" x 13 |
| | | 60 cps | | | | | | | | 45 days | 28 pounds |
| Norden-Ketay Corporation | | | | | | | | | | | |
| Instrument and Systems Division | | | | | | | | | | | |
| Wiley Street | | | | | | | | | | | |
| Milford, Connecticut | | | | | | | | | | | |
| BC T-300 | 110 ma | 8 a | 20 w | 1/10 ohm | 267 v | 6 | 0.44.7 | | - 77 | | |
| | i to ind | 60 cps | 20 W | 1/10 onm | 20/ V | Scope | Output, Transfer | Yes | 2% | \$795.00 | 19" x 9" x 14" |
| | | 00 663 | | | | | | | | 30 days | 35 pounds |
| olyphase Instrument Company | | | | | | | | | | | |
| East Fourth Street | | | | | | | | | | | |
| Bridgeport, Pennsylvania | | | | | | | | | | | |
| TA-3A | 1.2 ma | 1/10 a | 10 w | | 150 v | Scope | Output, Input | Yes | | \$645.00 | 19" x 19" x 10 |
| | | 120 cps | | | | ocope | corbert when | 103 | | 6 weeks | 50 pounds (appro |
| TA-13 | 450 ma | 10 a | 1,560 w | Less than 1 ohm | 150 v | Scope | Output, Input, | Yes | | \$3,600.00 | 19" x 60" x 15 |
| | | 60 cps | | | | | Transfer | | | \$3,000.00 | 250 pounds (appr |
| | | | | | | | | | | | The becker (abb. |
| TA-11 | | 20 a | 3000 w | | 150 v | Scope | Output, Transfer | Yes | | \$1,450.00 | |
| R. C. A. | | | | | | | | | | | |
| | | | | | | | - | | | | |
| Harrison, New Jersey 811C-1 | | | | - | | | | | | | |
| 6116-1 | 1,000 ma | 1 a, 60 cps | 300 w | | 1,000 v | None | Output, Transfer | Yes | | \$6,500.00 | 19" x 21" x 32 |
| | | 1/2 wave | | | | | | | | 10 months | 140 pounds (appr |
| Tektronix | | | | | | | | | | | |
| Portland 7, Oregon | | | | | | | | | | | |
| 575 | 0 100 | | | | | | | | | | |
| | 2,400 ma | 10 a | 200 w | 1 ohm | 200 v. | None | Output, Input, | Yes | 3% | \$925.00 | 13" x 17" x 24 |
| onex, Incorporated | | 60 cps | | | | | Transfer | | | 6 months | 70 pounds |
| 73 S. State Road | | | | | | | | | | | |
| Upper Darby, Pennsylvania | | | | | | | | | | | |
| CT-103 | 0.5 ma | 15 | 1.5. | | 100 | 6 | 0 | | | | |
| | U.J ma | 15 ma | 1.5 w | | 100 v | Scope | Output | Yes | 5% | \$135.00 | 10" x 8" x 8' |
| | | 60 cps | | | | | | | | immediate | 13 pounds |

Transistor Test Equipment Survey

Soren C. Ibsen Norden-Ketay Corp. Milford, Conn.

THE TRANSISTOR test equipment field is keeping abreast of the dynamic semi-conductor growth by providing a large variety of instruments. The equipment power handling capabilities have a spread of 1/2 watt to 1560 watts; whereas, the weight of the instruments have extremes of 1 pound to 250 pounds. The units vary in price from \$125.00 to \$6,500.00. This variety has been dictated by the exponential growth of transistors themselves. Point contact types have been replaced with junctions and other transistors. Power transistors with dissipation ratings above 50 watts have outclassed their predecessors.

This power handling capability is the strongest underlying trend in Transistor Test Equipment for 1957. This high power need is met by some manufacturers by offering two separate models while others have upgraded their equipment to cover the entire span.

The 33 commercially available models built by 21 manufacturers tend to align themselves into four general categories: Curve Tracers, Parameter-Analyzers, Portable Test Sets, and Miscellaneous types. In each category, many performance differences are found among the instruments and they should be compared as to their individual merits.

Curve Tracers usually employ 60 cycle sweep power to produce the transistor characteristic curves for oscilloscope display. Sweep power varies greatly among units. If large power is available in the sweep circuit, then small transistor load resistance is necessary for the proper hybrid impedance termination. On the other hand, high sweep voltage is vital for transistor breakdown measurements and a transistor collector voltage of above 250 volts may be required. The accuracy specification should be evaluated with the oscilloscope tolerance included.

Parameter-Analyzers generally operate by small signal measuring techniques. Metered input and output bias supplies provide the transistor dc operating point under consideration. The transistor is connected in either the grounded base or grounding emitter configuration, with bias approriate for pnp or npn types. A small internal audio test signal is properly applied to the transistor, detected, and converted to

HIGH QUALITY DIODES AND TRANSISTORS MUST HAVE CONSISTENTLY HIGH QUALITY WELDS

Raytheon subminiature precision welding systems provide extremely uniform production—from the 1st to the 1,000,000th unit.

The four difficult welds shown here are being performed with Raytheon precision welding equipment at the rate of 25,000 units a day by the diode division of a major electronics manufacturer.* In addition to joining the components of these diodes, the welding also seals them hermetically. Statistical sampling of production runs consistently meets JETEC specifications for high quality welds.

Raytheon AC and DC power supplies, controls, welding heads and transformers have been proved in applications where high speed, low cost, precision welding is required. Millions of tubes, transistors, diodes. relays. instruments, capacitors and resistors have been produced with Raytheon welders—designed and produced by *electronic* engineers for use in electronic manufacture.

Learn how Raytheon can help you solve your production problems; have your own samples processed in our Welding Application Laboratory. Write Dept. 6120ED.

*Name on request

TYPICAL DIODE ASSEMBLY four welds performed with Raytheon precision welding equipment

.010" diam. soft annealed nickel wire to tungsten spike Pinch-off weld joining .010" diam. annealed nickel wire, .032" diam. tinned copper wire and hermetically sealing both in Kovar tube

.032" diam. tinned copper butt weld to Kovar disk

RAYTHEON MANUFACTURING COMPANY

Commercial Equipment Division

Kovar disk hermetically

sealed to plated mild steel

case

Waltham 54, Mass.

Raytheon production equipment for the electronic industry - AC and DC welding equipment . Automatic welding systems . Magnetizers . Ultrasonic Impact Grinders

CIRCLE 509 ON READER-SERVICE CARD FOR MORE INFORMATION

Excellence in Electronics



957

hybrid parameters for meter readout. Microampere test signals and true hybrid ac termination are manudatory for precision measurements with accuracy of better than ± 5 percent.

Analyzers vary in that some require external signal generators and vtvm detection while others are selfcontained. The dc bias capability is an important variation when high power transistors are to be measured. The range of parameter measurement is vital if the instrument is to test all transistors commercially available. One instrument has combined the parameter analyzing with that of curve tracing to provide a highly versatile Transistor Test Set.

Portable test sets are generally simplified parameteranalyzers in that the units provide only one or two parameters with the primary function of go-no-go testing. Some units are only dc static test instruments. The input bias current is limited and collector voltage is low. Battery operation is standard. The accuracy is normally not better than ± 5 percent.

How should a transistor be evaluated? The actual transistor user is the best judge as to what transistor characteristics are vital to his particular applications. He must further compromise as to whether a curve display is superior to a meter reading. Then questions as to instrument range, accuracy, flexibility, completeness and price become deciding factors.

| | | | Portable | Test Sets | | | | | |
|--|----------------------------|---------------------------------|--|---|----------------------------------|----------|---------------------|------------------------------|-----------------------|
| Manufacturer Model No. | Maximum DC Base Current | Maximum DC Collector Voltage | Test Frequency | Characteristics Displayed | Maximum Beta Range | Accuracy | Battery Operated | Size and Weight | Price and Delivery |
| Baird Atomic, Incorporated Cambridge, Massachusetts KT-1 | 10 ma | 7½ ∢ | 1 kc | Beta, H ₁₁ , I _{co} | 200 | 3% | Yes | 6″ x 5″ x 11″ | \$175.00 30 days |
| G. Electronics 305 Dallas Street Albuquerque, New Mexico TR-2 | 10 ma | 12 v | 1 kc | Alpha, Beta, I _{co} | 1 000 | - | Yes | 4" x 4" x 8" 3 pounds | \$124.50 15 days |
| ilectronic Research Associates, Inc. 67 East Centre Street Nutley, New Jersey AT-10 | 10 ma | 100 ¥ | 240 cps (External Oscillator to 5 mc) | Alpha, Beta | 100 | 5% | No | 8″ x 11″ x 8″ 17 pounds | \$385.00 60 days |
| Davenco, Incorporated 150 Broadway New York 38, New York TT-1 | - | <i>4</i> ½ ∨ | 270 срз | Beta | 100 | | Yes | 9" x 6" x 6" 9 pounds | \$125.00 8 weeks |
| Measurements Corporation Boonton, New Jersey 505 | 70 ma | 12 v | DC | lco, Beta, Gm, H ₁₁ | 200 | - | Yes | 10" x 14" x 7" 9 pounds | |
| Aetronic, Incorporated Mill Lane Waterford, Connecticut 545 | 100 ma | 5.2 v External to 25 v | 1 kc | Beta, I _{co} | 250 | 3% | Yes | 7" x 11" x 7" 8 pounds | \$210.00 4 weeks |
| ionex, Incorporated 73 S. State Road Opper Darby, Pennsylvania TT-205 | 2 ma | 20 v | 1 kc (External Osc. 0.25 to 5 kc) | Beta, I _{co} , Rc | 150 (Larger as calibrated) | 5% | Yes | 14" x 8" x 8" , 19 pounds | \$155.00 immediat |
| Auantum Electronics, Incorporated 1921 Virginia Street Albuquerque, New Mexico Mod. V | 100 ma | 5.36 v | 2 kc | l _{co} , Beta | 1,000 | 5% | Yes | 5″ x 7″ x 10″ 5½ pounds | \$295.00 90 day |
| Durson Company 10416 National Blvd. Los Angeles 34, Calif. 201 | 10 ma | 5 v | | Beta, I _{co} | 500 | - | Yes | 10" x 7" x 5" 10 pounds | \$190.00 |

Portable Test Sets

DOCC INDEN

CCur-

ctual sistor

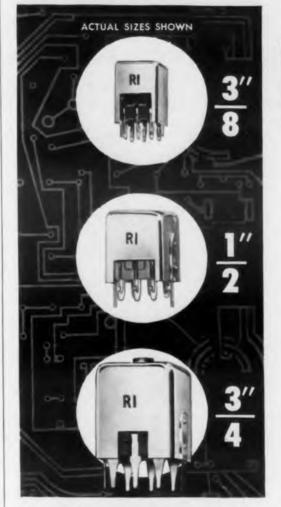
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plete-

| | CRO | OSS | INDEX |
|-------------------------------|---|--|---|
| General General General | Amperex Bendix Bogue Thomson Houstor 35-Hytror Clevite Delco Fretco I Electric Co, Ltd Transisto System Jale Tube (Philco | Be Bo BTH CBS C C C C C C C C C C C C C C C C C C | Minneapolis- Honeywell MH Motorola Mo Mullard Mu Nucleonic Nu PYE Electronics PYE Raytheon Ra Sprague Sp Sylvania Sy Texas Instrument TI Transitron Tr Tung-Sol TS Western Electric WE Westinghouse Wh |
| | Bo RCA RCA Ra 2N217 WE Ra | Am,RCA | 2N123 GE 2N128 LT 2N129 LT 2N130 Ra 2N130A Ra 2N131A Ra 2N131A Ra 2N132 Ra 2N132 Ra 2N132 Ra 2N132 Ra 2N133 Ra 2N133 Ra 2N133 Ra 2N133 Ra 2N133 Ra 2N133 Ra 2N134 Ra 2N135 Ra 2N134 Ra 2N135 RCA 2N140 RCA 2N141 Sy 2N142 Sy 2N143 Sy 2N144 Sy 2N145 TI 2N145 TI 2N145 TI 2N147 TI 2N148 TI 2N149 TI 2N155 CBS, Nu, Sy 2N166 CBS 2N161 Bo |

for your transistorized circuits . . .



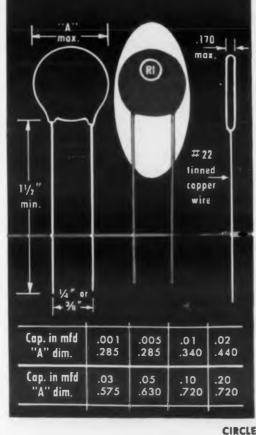
I.F. TRANSFORMERS

custom-built to the Q you require with the low cost advantages of mass production in 3/8", 1/2" and 3/4" sizes

Whether your circuit requires a high Q for performance or a low Q for greater stability, Radio Industries will engineer and manufacture I.F. transformers to meet any specific level you require, up to 200 for the 3/4" and 1/2" and up to 140 for the 3/4". RI transformers have the shunt capacitors built in to meet your requirements.

Available in a variety of terminal styles for wired and printed circuits.

for your transistorized circuits



ceramic **DISC CAPACITORS**

unique copper plating process lowers production costs

The Radio Industries patented Kemetal copper plating process provides copper electrodes that assure greater adhesion and freedom from migration. Another special RI process makes possible the unusual thinness of these capacitors, to meet the need for increased capacitance in a smaller size.

With a power factor of 3% maximum at 1 KC, RI caps have a working voltage of 30 volts DC with a minimum I.R. of 1000 megohms contingent upon capacity values. Capacitance tolerances are available in +100% - 20%, $\pm 20\%$, $\pm 10\%$.

> Write for complete description and details DIO

INDUSTRIES, INC. 5225 no. ravenswood ave. • chicago 40, illinois 3 modern plants: Chicago, Des Plaines, and Marshall, Ill.

CIRCLE 510 ON READER-SERVICE CARD FOR MORE INFORMATION

2N114 Ra

2N180 CBS

Parameter Analyzers

| Manufacturer and Model | Max. DC Base Current | Max. DC Collector Power | | Parameters Measured (gb and ge, NPN and PNP) | Range of Measurement | Transistor Bias Terminations (Output) | Maximum Frequency Range | | External Iquipment Required | Size and Weight | Battery Oper- ated | Price and Delivery |
|---|----------------------------|-------------------------------|-----------------|--|--|--|--|-------|-----------------------------------|-------------------------------|--------------------------|--------------------------|
| Baird Associates 73 University Road | | | | | | | | | | | | |
| Cambridge, Massachusetts | | | | | | | | | | | | |
| GP-4 | 5 ma | 1/2 w | 45 v | H ₁₁ , H ₁₂ , H ₂₁ , H ₂₂ , I _{co} | H ₁₁ to 3K ohm | | (ge) - 200 kc | 5% | Osc VTVM | 22" x 10" x 13" | Yes | \$475.00 |
| | | | 5 ma | | H ₂₁ to 1,000 | + | (gb) -1 mc | 0,0 | | 70 pounds | | 30 days |
| KP-1 | 200 ma | 30 w | 100 v 300 ma | H ₁₁ , H ₁₂ , H ₂₁ , H ₂₂ , I _{co} | H ₁₁ to 3K ohm H ₂₁ to 1,000 | | 200 kc | 5% | Osc. VTVM | 22" x 22" x 15" 100 pounds | No | \$795.00 90 days |
| Quantum Electronics 1921 Virginia Avenue Albuguerque, New Mexico | | | | | | | | | | | | |
| PTA #3 | 1,500 ma | 75 w Regulated) | 32 v 15 a | H ₂₁ , (ge only) | H ₂₁ to 1,000 | | DC Tests | - | None | 47" x 21" x 24" 200 pounds | No | \$3,475.0 120 days |
| Norden-Ketay Corporation Instrument & Systems Division Wiley Street Milford, Connecticut | | | | | | | | | | | | |
| BCT-300 (See Curve Tracer) | 10 ma | 2 w | 100 v 20 mg | H ₂₁ , H ₁₁ | H ₁₁ to 10K ohms H ₂₁ to 1,000 | 100 ohm | l mc georgb | 3% | Osc. VTVM | 19" x 8" x 14" 35 pounds | No | \$795.00 30 days |
| BTS-400 | 1,000 ma | 60 w | 150 v 6 a | H ₁₁ , H ₁₂ , H ₂₁ , H ₂₂ (Real and Imaginary) I _{co} , I _{ceo} , I _{ces} | H ₁₁ to 100K ohms H ₂₁ to 1,000 | 1 ohm | 2 mc with external Oscillator, ge or gb | 2% | None | 19" x 14" x 15" 80 pounds | No | \$2,495.0 6 months |
| Owens Laboratories 55 Beacon Place | | | | 'cor 'ces | | | | | | | | |
| Pasadena, California | 71/2 mg | | 75 v | No. Hos Hos Hos I | H ₁₁ to 1K | 5 ohms | 1 mc with external | E (77 | N. | 15" x 13" x 4" | No | £ 475 O |
| 210 | 772 ma | | /5 • | H ₁₁ , H ₁₂ , H ₂₂ , H ₂₁ , I _{co} | H ₂₁ to 1,000 | 3 onms | Oscillator, VTVM | 5% | None | 18 pounds | NO | \$475.00 30 days |

Miscellaneous Test Equipment

2N181 CBS 2N218 RCA Manufacturer **Price and** 2N182 CBS 2N219 RCA Model Description **Test Performed** Delivery 2N220 RCA 2N183 CBS 2N223 LT 2N184 CBS 2N224 LT **Electronic Measurements** 2N185 TI Power Pack for Transistors. Provides voltage to 100 v and 2N225 LT 2N186 GE **Lewis Street** 3000 ma regulated to 1/10 ohm 2N186A GE 2N226 LT Eatontown, New Jersey output impedance. Input modula-2N227 LT 200 Series 2N187 GE tions jacks available for coefficient 2N228 2N187A GE Sy measurements. 2N229 2N188 GE Sy 2N233 Sy 2N188A GE **Electronic Research Assoc.** Range of 60 db at 1000 cps with \$775.00 Transistor Noise figure meter. 2N189 GE 2N234A Be Incorposated 1 cycle band-width. DC input bias 4 weeks 2N235A Be, Sy **69 East Center Street** 2N190 GE to 10 ma. 2N237 TI 2N191 GE Nutley, New Jersey 2N238 TI NET 2N192 GE 2N240 LT 2N193 Sy Kay Electric 2N194 2N241 GE Sy DC input bias to 10 ma. Output \$1,595.00 Alpha versus frequency Curve 2N241A GE Maple Avenue Tracer. Combine bias controls bias 25 ma and 50 volts. Auxiliary 2N206 RCA 60 days 2N242 Sy 2N207 LT Pine Brook, New Jersey with "Mega-Sweep" generator Oscilloscope required. 2N243/2N342 TI 970A 2N207A LT (50 mc). 2N244/2N343 2N207B LT 2N211 Sy 2N247 RCA Polyphase \$1,225.00 Alpha and Beta versus input cur-DC input bias to 15 ma. Output 2N250 Sy, TI **East Fourth Street** rent Curve Tracer. Metered Beta, bias to 30 ma and 100 v. 4 weeks 2N212 Sy 2N213 Sy 2N251 TI Bridgeport, Pennsylvania Alpha and Ico. 2N252 TI **TA-16** 2N214 Sy 2N253 TL 2N215 RCA 2N216 Sy 2N254 TL TA-10 \$395.00 Unijunction transistor or diode Interbase or power pack, 0-100 v, 2N255 CBS curve tracer; power supply. 0-100 ma. Emitter to 150 v. Scope 2N217 RCA

required.

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| 271256 CBS | 2N348 Bo |
|----------------------------------|--|
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| 21263 TI | 2N350 Nu |
| 21 265 GE | 2N352/T1040 LT 2N353/T1041 LT |
| 2N 268 C | 2N354/T1025 LT |
| 2N269 RCA | 2N355/T1159 LT |
| 2N270 RCA | 2N356 GT |
| 2N271 Ra 2N271A Ra | 2N357 GT |
| 2N272 Ro | 2N358 GT |
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| 2N325 Sy | 970 TI |
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| 2N328 Ra | 10C Sp |
| 2N329 Ra | B114 Be |
| 2N330 Ra | CK751 Ra |
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| 2N333 TI | |
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MOTOROLA TRANSISTORS

This battery of mechanized furnaces, developed by Motorola, produces crystals of extreme quality . . . in quantities necessary for Motorola's mass production of transistors. Crystals are outstanding in uniformity of structure and characteristics --- contributing to exceptional transistor performance.

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More rugged, more compact, more flexible-specifically designed for the following applications:

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- Amplifier for Servo Motors-for control motors or indicator motors

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WHERE miniaturization is vital, yet high power is still required, Honeywell's complete line of Weld-Seal Transistors is your best answer.

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CHICAGO **IRving 8-9266** 7350 N. Lincoln Ave.

BOSTON ALgonquin 4-8730 1230SoldierFieldRd. 2749 4th Ave. So. LOS ANGELES RAmond 3-6611 or

PArkview 8-7311 6620 Telegraph Rd.

MINNEAPOLIS

FEderal 2-5225

CIRCLE 512 ON READER-SERVICE CARD FOR MORE INFORMATION

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| l Weld-Seal H6 Transistors make this 48-watt, 14 C. Power Converter more compact than any other. |
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| e these new specifications—developed with |
| the design engineer in mind |
| H5 H6 H7 |
| istance 24—48 ohms 27— 54 ohms 30— 60 ohms |

Honeywell ounce D.

| Note these new specifications—developed with the design engineer in mind | | | | | | | | |
|--|---|---|--|--|--|--|--|--|
| H5 | H6 | H7 | | | | | | |
| 24-48 ohms | 27-54 ohms | 30— 60 ohms | | | | | | |
| 17.5-52 mhos | 35—105 mhos | 71-213 mhos | | | | | | |
| 30 | 40 | 60 | | | | | | |
| (At a collector current of 2 amps.) | | | | | | | | |
| The H6 and H7 Transistors are available for immediate delivery. | | | | | | | | |
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| | design engin H5 24—48 ohms 17.5—52 mhos 30 a collector curre | design engineer in mind H5 H6 24—48 ohms 27— 54 ohms 17.5—52 mhos 35—105 mhos 30 40 a collector current of 2 amps.) | | | | | | |

Honeywell

First in Controls

| INDE) | (Cont.) |
|-------------------------------------|----------------------------------|
| GET8 GL | 0C45/2N140 M |
| GET9 GL | OC65/2N130 An |
| GET10 GL | OC66/2N131 An |
| GET15 GL | 0C70 Mu |
| GTI BTH GT2 BTH | 0C71 Mu 0C72 Mu |
| GT3 BTH | 0C73 Mu |
| GTIL BTH | OC76 Mu |
| GT12 BTH | OCP71 Mu |
| GT13 BTH | PC6 Sp |
| GT14 GT | RD316 Bo |
| GT14H GT GT20 GT | SB101/2N344 Sp SB102/2N345 Sp |
| GT20H GT | SB103/2N346 Sp |
| GT34 GT | SB5122/2N240 |
| GT34HV GT | STIO Tr |
| GT34N GT | ST11 Tr |
| GT34S GT | ST12 Tr |
| GT35/2N35 GT GT74 GT | 5T13 Tr 5T30 Tr |
| GT75 GT | ST31 Tr |
| GT81H GT | ST32 Tr |
| GT81 GT | CT22 T, |
| GT81HS GT | 5T40 Tr |
| GT82 GT | ST41 Tr |
| GT83 GT GT87 GT | 5T42 Tr T0031 LT |
| GT88 GT | T0033 LT |
| GT109/2N109 GT | T1164 LT |
| GT122 GT | TJI IS |
| GT123 GT | TJ2 IS |
| GT153 GT | SI ST |
| GT167 GT GT210H GT | TP1 IS TP2 IS |
| GT222 GT | TSI IS |
| GT229 GT | TS2 IS |
| GT269 GT | TS3 IS |
| GT758 GT | TS176/2N242 T |
| GT759 GT GT759R GT | TS612/2N378 T TS613/2N379 T |
| GT760 GT | TS614/2N380 T |
| GT760R GT | TS615/2N44 TS |
| GT761 GT | TS616/2N381 T |
| GT761R GT | TS617/2N382 T |
| GT762R GT | TS618/2N383 T |
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| GT947 GT | V10-30 PYE |
| GT948 GT GT949 GT | V10-50B PYE V15-10P PYE |
| H38 MH | V15-20P PYE |
| H4A MH | V15-30P PYE |
| H5 MH | V30-10P PYE |
| H6 MH | V30-20P PYE |
| H7 MH | V30-30P PYE |
| HIO MH | X30A Bo |
| MN13A Mo MN13B Mo | X31A Bo X32A Bo |
| MN13B Mo MN13C Mo | X110 Be |
| MN13C Mo MN21 Mo | X113 Be |
| MN21 Mo | X119 Be |
| MN25 Mo | X133 Be |
| MN26 Mo | X134 Be |
| MN28 Mo | X137 Be X140 Be |
| MN29 Mo | X140 Be X145 Be |
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Color Drafting Pencils

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Draw 'ermanent or Temporary Lines

The first of these pencils is called the Non-Print. Its translucent, colored lead not kes a line that drops out when a transacent original or master is reproduced by processes such as blueprint, brownprint, and Ozalid. The pencil provides freedom to sketch and make notes on drawings without having to worry about cleaning up before the drawings are reproduced. The pencil has a fine point and supplies a contrasting color that will not fade or smear. The function of another model, called the Lumochrom, is entirely different. The Lumochrom comes in 24 colors, including white, and all of its colors reproduce perfectly. Because of this it enables draftsmen to distinguish quickly between numerous different elements shown on their masters by means of their color contrast. J. S. Staedtler, Inc., Dept. ED. Hackensack, N.J.

CIRCLE 136 ON READER-SERVICE CARD

Pen-Size Oiler

For Exact Lubrication

Designed like a fountain pen, this oiler delivers exact amounts of oil as small as a fraction of a drop. It operates in holes up to 7/8 in. in depth and other out-of-the-way places ordinarily difficult to reach. The oiler can be used either vertically or horizontally for both holes and surface application. The oil supply is clearly visible in the transparent reservoir, and one filling provides a supply for long periods. In operation, the spring controlled steel point of the unit is pressed against the spot to be oiled, then released. A fraction of a drop is thus automatically ejected, and if more is required, repeated pressing will deliver the exact amount.

Dill Mfg. Co., Dept. ED, 700 E. 82nd St., Cleveland, Ohio.

CIRCLE 137 ON READER-SERVICE CARD

7

INSURING RF SIGNAL RECEPTION AND TRANSMISSION IN THE LOCKHEED X-17 TEST MISSILE

The Rheem REL-09 Miniature RF Power Amplifier has been used in the X-17 test missile since the inception of the project.

The REL-09 provides power amplification over the 215-235 mc telemetering band. With 1.4 watts input drive, it will deliver an 11-watt output to a 52-ohm load. Grid and plate tuning controls are accessible from the front plate. Automatic protection is provided against damage resulting from loss of drive or plate power. Power leads contain 84-db attenuation filters. No cooling or shock mounting is required.

For further information, write direct to Rheem or contact your area sales representative:

North Central

Sam Robbins, Inc. 230 East 1st Street, Flint 2, Michigan Florida Arthur H. Lynch & Associates P.O. Box 466. Fort Myers, Florida New England and New York State Electronics Associates, Inc. 200 5th Street, Stamford, Conn. **Central East Coast** F. R. Jodon, Inc. 8510 Beech Tree Road, Washington 14. D.C. Southwest, Rockies and State of Washington George E. Harris & Co., Inc. 3241 East Douglas, Wichita 8. Kansas



ELECTRONICS DIVISI RHEEM MANUFACTURING COMPANY THE LOCKHEED X-17 TEST MISSILE The X-17 provides information on the problems which arise when the warhead of a ballistic missile re-enters the earth's atmosphere at high speed.



7777 Industry Avenue, Rivera, California

NO MORE EXTERNA BOOSTER AMPLIFIE

Amplifier No. 1

2 Booster Amplifier No. 2

with the new combination resolver-booster

L Resolver R151

by Reeves

An outstanding advance in MINIATURIZATION without sacrifice of performance or precision.

Shown FULL SIZE in the illustration above, this latest Reeves achievement in miniaturization for airborne applications takes up a fraction of the space occupied by a conventional resolver with external boosters. Yet performance, accuracy and dependability are in every way equivalent or better.

The new Reeves Combination Resolver-Booster consists of the time-proven R151 Precision Resolver with two PLUG-IN TRANSISTORIZED BOOSTER AMPLIFIERS built onto it as shown. The amplifiers provide standardization for transformation ratio and phase shift over a wide range of temperatures. Specifications given are maintained for production units without culling. Additional data on request.



Actual

Size

REEVES INSTRUMENT CORPORATION A SUBSIDIARY OF DYNAMICS CORP. OF AMERICA, 223 EAST 91st ST., NEW YORK 28, N. Y. CIRCLE 140 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Thermocouple

Higher Voltage Output

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The Super-Clad thermocouple is said to generate greater electrical output than standard thermocouples. The unit, which is interchangeable on all standard pilots, is designed to eliminate service calls caused by pilot outages and to insure positive holding action. Improved thermo-electric alloys are used to gain increased voltage output. The plating protects the copper from heat and prevents oxidation. The unit has 24 cooling fins to create a greater temperature differential. Tin plating on the contact end provides good electrical conduction.

Robertshaw-Fulton Controls Co., Dept. ED. Grayson Controls Div., Long Beach 5, Calif.

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Wire Markers Aluminum Foil

Speedy Marx, aluminum foil wire markers, are furnished on quick-release dispensing cards which have been precut for easy handling, and can be applied instantly without tools. Flexible aluminum markers offer users double sticking action. A thermosetting adhesive retains its bonding action up to temperatures of 350 F, and the mechanical action of the aluminum as it wraps around wiring will remain unaffected by solvents, grease or coolants. Large diameter wire and cable, or pipe and tube, can be coded with aluminum markers. A transparent plastic coating is applied to marker surfaces after imprinting to protect symbols against abrasions. water or dirt. Two sizes are available: 1-1/2 in. markers for wires over 1/4 in. OD, 3/4 in. markers for wires under 1/4 in. OD. Special sizes, shapes and colors can also be furnished.

North Shore Nameplate, Inc., Dept., 214-27 Northern Blvd., Bayside 61, N.Y.

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specifications

Transformation ratio: 1.000±.001 Phase shift: 0°±3' Functional accuracy: 0.1% Input impedance: over 8 megohms Frequency: 400 c.p.s.±5% Max. amplitude: 14 V. r.m.s. Temp. range: --55° C. to 80° C. Power requirements: 30 V. d.c. @ 6 ma. per amplifier



Provides continuous 360° check on resolver functional accuracy, and yields permanent record of results.



Pulling Elbow For Corner Wiring

The Pulling Elbow permits easy wiring. Wires are slipped straight through conduit and out one hub. A big loop of wires is made and again pushed through hub and conduit. The wires are pulled out from the other end of system. The cover attaches quickly with big screws and will open erate easily. The Elbow is made of top quality malleable ermoiron with heavy cadmium plated finish. Full neon all prene gaskets and large cover screws designed to calls fit snugly in opposed corners without protruding inside. In addition, the cover is domed for greater rigidity and provides more wire area inside elbow. Smooth ground surfaces provide better cover and gasket seal. Hubs have precision tapered pipe threads and are positioned exactly 90 deg from center. The smooth inside surfaces eliminate the ED. possibility of skinning insulation on wire when it is pulled through electrical system.

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Ideal-Simplet Fittings, Inc., Dept. ED, 5098 Park Ave., Sycamore, Ill.

CIRCLE 144 ON READER-SERVICE CARD FOR MORE INFORMATION

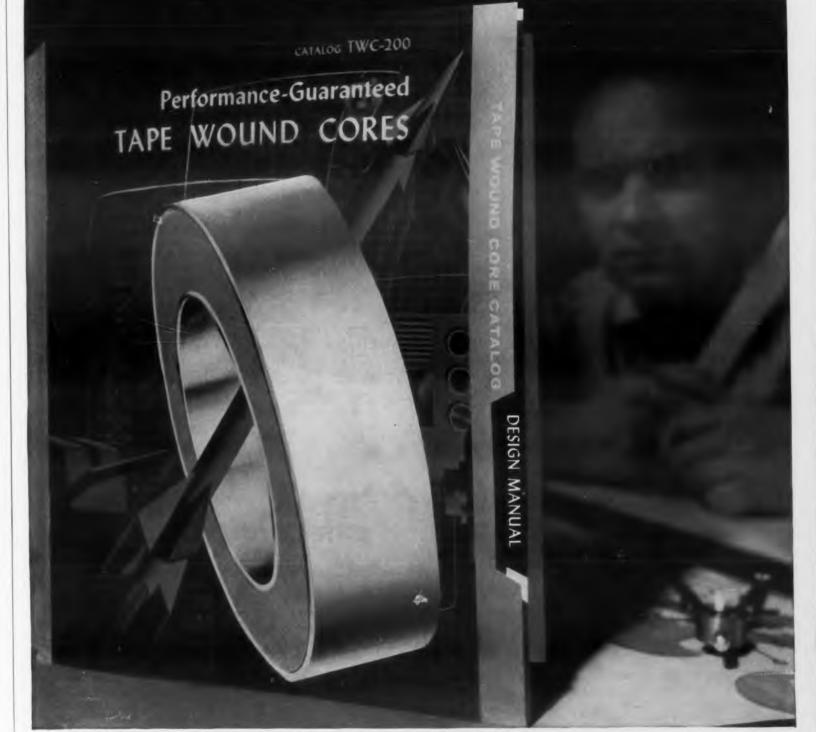
Sweeping Oscillator Sweeps I-F's to 280 Mc



A broadband sweeping oscillator with six switched bands, the Rada-Sweep Sr. has 24 precise crystal markers set at customer specified frequencies. Center frequencies are from 1 to 260 mc. The instrument is designed and built for sweeping radar i-f units up to 280 mc.Rf output: 0.5 v rms into nominal 70 or 50 ohms. Higher for lower frequency units. Output held constant to within ± 0.5 db over widest sweep by agc circuit. Attenuators: switched 20 db, 10 db, 2 db plus continuously variable 6 db. A true zero base line produced on the oscilloscope during retrace time. Sweep output: sawtooth synchronized with sweeping oscillator.

Kay Electric Co., Dept. ED, 14 Maple Ave., Pine Brook, N.J.

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Here's the first design manual for your work with tape wound cores

Because engineers have expanded high permeability magnetics into a host of new uses, Magnetics, Inc. has combined its new tape wound core catalog with the industry's first design manual. If you and your staff need a working familiarity with magnetic equations, characteristics and terminology, this 28-page book will be of unusual value.

This design manual has been compiled under the direction of our laboratories. It contains basic units and conversion factors, methods of testing (dynamic, EI loop and d-c), properties and magnetic values of nickel-iron alloys, and many pages of curves showing the variation of magnetic properties with temperature and of core loss with frequency. This fact-packed catalog and design manual also describes in detail the tape wound cores and bobbin cores which we manufacture. It will enable you to design around and specify the industry's only Performance-Guaranteed Tape Wound Cores. Should your engineering departments feel that more than one copy would be of value, please write for TWC-200 on company letterhead, giving full names and titles. Magnetics, Inc., Dept. ED-40, Butler, Pa.



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| | Meets A.C.S. Spec | ifications |
| A | Assay (HF) | |
| | Maximum Limits of | Impurities |
| | Fluosilicic Acid (H2SiF6) | |
| | Residue after Ignition | |
| 1 | Chloride (Cl) | |
| | Phosphate (PO4) | |
| ELECTRONIC B | Sulfate (SO ₄) | |
| | Sulfite (SO3) Arsenic (As) | |
| B'A | Copper (Cu) | |
| ACID | Heavy Metals (as Pb) | |
| TOROFLUORIC, A | | |
| Code 2753 (T) | Iron (Fe) | 0.0001 % |

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CIRCLE 148 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Subminiature Capacitors High Temperature



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Deltaply 165 subminiature capacitors operate reliably over the temperature range -65 C to +165 C. As an example of the size, a 1.0 mfd., 200 v unit requires 3.8 cubic inches. The same unit in teflon requires 6.4 cubic inches. Capacitance change over the full temperature range will amount to less than 9 per cent. Insulation resistance in megohms x microfarads varies from 200,000 at 250 C. The selfhealing, metallized, plastic film provides unusually long life at 165 C with no voltage derating. Capacitance values from .001 to 10.0 mfd., may be obtained in hermetically sealed metal tubes or doublelock seal tubular cans. The smaller sizes are also available uncased. Standard voltage ratings are 200, 400 and 600.

Dearborn Electronics Labs., Dept. ED, 1421 N. Wells St., Chicago 10, Ill.

CIRCLE 149 ON READER-SERVICE CARD FOR MORE INFORMATION



Inductor Timing Motor 30 Oz-In. at 1 Rpm

A permanent-magnet synchronous motor with guaranteed torque of 30 oz-in. at 1 rpm and 60 cps is designed for a variety of timing applications. Basic features include: total enclosure to seal out dust, dirt and other breakdown materials; a controlled lubrication system; and the ability to operate in any position. Rotor speed of 450 rpm makes it possible to reduce the gear train and insure quieter operation and durability. The inductor motor is available with output shaft speeds from 1 to 60 rpm, for 120 and 240 v operation at 50 and 60 cps. Models for either clockwise or counterclockwise rotation can be supplied.

Haydon Mfg. Co., Dept. ED, 245 E. Elm St., Torrington, Conn.

CIRCLE 150 ON READER-SERVICE CARD FOR MORE INFORMATION





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1 KVA Voltage Regulator **Magnetic Type**

Type TM7101 has an accuracy of 1 v band for line voltage variations and/or load magnitude or power factor changes. Load is rated at 1 kva. Input is 95 to 135 v, single phase, 60 cps, and output is 115 v nominal, adjustable from 110 to 120 v. It is suited for applications where little or no attention is possible, such as microwave relay stations and remote installations, where a tube or transistor malfunction and replacement can be costly or not immediately possible.

Cabinet model is a self-contained portable assembly that can be carried to laboratory test apparatus or factory operation.

The Superior Electric Co., Dept. ED, 83 Laurel St., Bristol, Conn.

CIRCLE 152 ON READER-SERVICE CARD FOR MORE INFORMATION



Speed/Torque Unit 1-6 Output Speeds

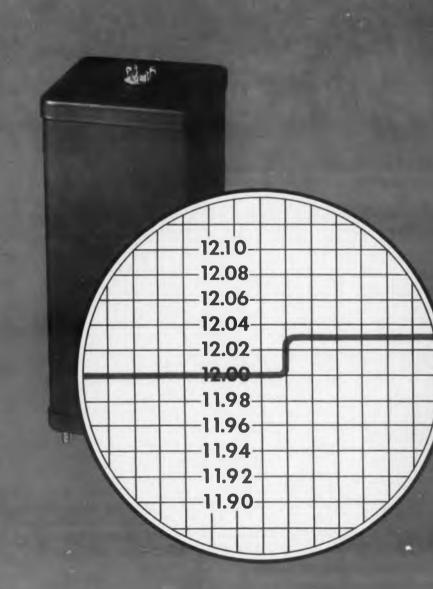
The new Servo-Speed/Torque-Unit, an experimental gear set, may be used with the manufacturer's Servo-Kit and other servo equipment. A complete set of change gears is supplied which enables the user to select any one of six output speed and torque values. There are two models, one for each of the two Barcol motors which are supplied with the Servo-Kit. Provision is made for mounting a 3/8 in. bushing mount potentiometer, coupled directly to the output shaft. Mounting adapters can be furnished so that the units may be used with any of the other popular makes and types of servo motors and transducers.

Servo Systems Co., Dept. ED, 55 Meeker Ave., Newark 12, N.J.

CIRCLE 153 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN . July 15, 1957

TRANSISTORIZED **REGULATED POWER SUPPLIES**



TSO BOULEVARD. KENIEWORTH. NEW JERSEY

WITH ZERO LINE TRANSIENT

Immediate Delivery

Transistor Devices, Inc brings to the design engineers a line of high performance, fully transistorized regulated power supplies. Units are all hermetically sealed and are available FROM STOCK in 0 to 30 volts range. These TDI power supplies also offer in-stantaneous and non-microphonic operation.

The scope trace as shown indicates a 12V unit taken from stock and checked before shipping — the result as in all previous tests showed a zero line transient.

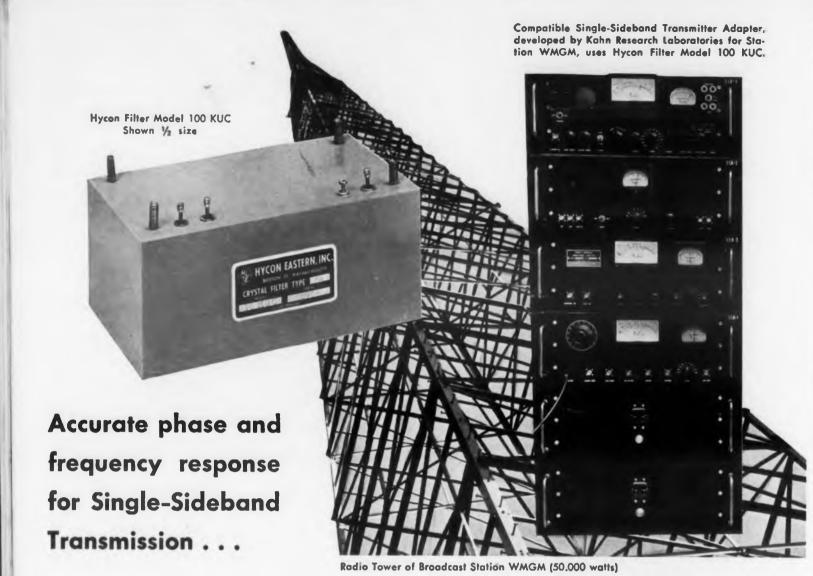
If you need compact reliable regulated power supplies — call on TDI for high performance at quantity production prices.

Compare these specifications

Compare these spectrications Model 12E200 Input 115 V \pm 10% 60 cycles Output 12 V D.C adjustable \pm 10% Load regulation 0 to .2 amps \pm 0.1% Line regulation 103.5 to 126.5 V \pm 0.2% Output impedance 1 ohm, 20 cycles to 10 KC. Ripple less than 1 millivolt Transient for 50% load step 0.4% Load regulation 200 microsecond Load transient recovery time 200 microseconds Transient for 10% line step 0.0%!!! Instant operation Non microphonic Hermetically sealed Only 2% x 3 x 6 inches Available models for other outputs For informative literature write

CIRCLE 154 ON READER-SERVICE CARD FOR MORE INFORMATION

ANSISTOR DEVICES, INC.



another problem solved by **HYCON FILTERS**

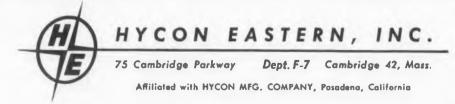
The first domestic broadcast installation of the Compatible Single-Sideband Modulation Method has recently been completed by Broadcast Station WMGM of New York City on an experimental basis. Advantages of this system are improved fidelity, improved range in the presence of co-channel interference, resistance

| ELECTRICAL SPECIFICATIONS (Model 100 KUC) |
|---|
| Carrier Frequency: 100 KC |
| Attenuation at carrier +300 cps: 2 db maximum |
| Attenuation at carrier +6000 cps: 2 db maximum |
| Attenuation at carrier - 300 cps: 60 db minimum |
| Insertion Loss: 10 db maximum |
| Passband Response Variation: $\pm \frac{1}{2}$ db |
| Impedance: 8200 ohms |
| Dimensions: 5 % " x 3" x 2 % |
| ALSO AVAILABLE: Model 100 KLC—Lower Sideband Model 100 KPA—Carrier Selection |

to fading and reduction in spectrum space. Because of their ability to meet the stringent requirements for the SSB frequency selective networks, Hycon Filters were chosen for this installation by Kahn Research Laboratories, designers of the CSSB Transmitter Adapter.

Whether your selectivity problems are in transmission or reception, AM or FM, mobile or fixed equipment, Hycon quartz crystal Filters offer you these advantages: LOW COST standard models; LOW DISTORTION—passband uniformity within $\pm \frac{1}{2}$ db; HIGH STA-BILITY — inherent in crystal resonators, also freedom from microphonic behavior; ZERO MAINTENANCE — hermetically sealed, requiring no realignment or readjustment. Hycon Eastern, Inc. can assist you in the selection of filter characteristics best suited to your needs. Write for Crystal Filter Bulletin.

"Bridging the Gap Between Science and Technology through Electronics"



Manufacturers of: Crystal Filters, Ultra Stable Oscillators, and Magnetic Tape Indexing and Search Units CIRCLE 156 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products



Equipment Mount Temperature Resistant

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This mounting features load capacitance above 60 lb, temperature resistance from -80 to +250 F, vibration isolation in severe operating conditions. The Temproof mounting is designed to meet the requirement of MIL-C-172B and is self damping in its resonant range. Mountings support loads in either the upward or downward direction.

Lord Manufacturing Co., Dept. ED, Erie, Pa.

CIRCLE 157 ON READER-SERVICE CARD FOR MORE INFORMATION



Resolver 1.062 In. Diam

Measuring 1.062 in. diam, size 11 resolvers are offered with a functional accuracy of better than 0.1 per cent. Compensated units are provided for use in systems performing over a wide temperature range. Both compensated and uncompensated resolvers are available in a range of 400 to 16 cps models.

Reeves Instrument Corp., Dept. ED, 207 E. 91st St., New York 28, N.Y.

CIRCLE 158 ON READER-SERVICE CARD FOR MORE INFORMATION



Transistor Clip Beryllium Copper

This transistor clip is designed to retain all popularly used transistors under conditions of severe acceleration, deceleration, shock and vibration. Made from tempered beryllium copper, the transistor clip performs a dual function of retention and heat dissipation. Offered in a choice of cadmium, black ebanol or silver plate, clips are available in many sizes and modifications.

The Birtcher Corp., Dept. ED, 4371 Valley Blvd., Los Angeles 32, Calif.

CIRCLE 159 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN • July 15, 1957



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Bolometers and Thermistors Broadband Disc Type

Two broadband disc bolometers for coaxial detectors. Models N603 and N603-4.5, covering the frequency range of from 500 to 10,000 mc, and a broadband disc thermistor, Model N335, covering the same frequency range, have been developed. The Model 603 bolometers consist of two 100-ohm Wollaston wire bolometer elements mounted on a mica disc. The mica discs incorporate the rf bypass capacitor for the ungrounded end of the bolometer as well as a blocking capacitor at the central junction between the 100-ohm elements. This provides rf contact to the transmission line center conductor while blocking the bias current. The elements are in series to present a 200-ohm resistance to the external dc or af bias circuits and are arranged to be in parallel in the rf transmission line, thus acting as a 50-ohm termination.

The Model N335 thermistor is specifically designed for use with the Model 561 coaxial bolometer mount for microwave power measurements. The thermistor is used with microwave power meters capable of supplying the necessary 12 to 15 ma bias to measure power levels from 0.01 to 10 mw. Because of the long time constant, approximately 1 sec, the thermistor is particularly suited to measurement of pulsed signals. It is not susceptible to burnout, but in any case is readily replaceable and does not require tuning.

The Narda Corp., Dept. ED, 160 Herricks Rd., Mineola, N.Y.

CIRCLE 160 ON READER-SERVICE CARD FOR MORE INFORMATION



RF Preamplifier 35 and 50 Db Gain

Model 1 provides a gain of 35 db at band center and Model 2 provides 50 db, both with a maximum noise figure of 3.5 db. Frequency response is within 3 db over the band of 215-247 mc. The unit occupies a volume of 1/3 cu ft and weighs less than $3\cdot1/2$ lb.

Radiation, Inc., Dept. ED, P.O. Box 37, Melbourne, Fla.

CIRCLE 161 ON READER-SERVICE CARD FOR MORE INFORMATION

Servo Motors For Transistorized Operations

Meets MIL-E-5272 -65°C to +125°C temperature range.

| | SIZE 8 | SIZE 10 | SIZE 11 | SIZE 15 | SIZE 18 |
|--|-------------|-------------|--|-----------------------|------------|
| Oster Type | 8-5001-00 | 10-5052-00 | 11-5101-00 | 15-5153-00 | 18-5201-00 |
| Electrical Characteristics | | | and the second s | and the second second | ALC: NOT |
| Frequency (cps) | 400 | 400 | 4.00 | 400 | 400 |
| Torque at Stall (oz. in.) | .15 | .30 | .63 | 1.45 | 2.35 |
| No Load Speed (rpm) | 6500 | 6500 | 6500 | 5200 | 5200 |
| Speed at Half Torque (rpm) | 4000 | 4000 | 4000 | 3200 | 3200 |
| Time Constant (sec.) | 0.03 | 0.015 | 0.016 | 0.017 | 0.013 |
| Reversing Time (sec) | 0.051 | 0.025 | 0.028 | 0.030 | 0.022 |
| Theo Acceleration at Stall (rad sec ²) | 22500 | 45000 | 41500 | 31000 | 40000 |
| Operating Temp Range (°C.) | -54 to +125 | -54 to +125 | -54 to +125 | -54 to +125 | -54 to +12 |
| Slot Effect | 1.6v/26v | 1.0v/36v | 1.0v/40v | 1.0v/40v | 1.0v/40v |
| Duty Cycle | Cont. | Cont. | Cont. | Cont. | Cont. |
| Fixed Phase | | In a set | | | - |
| Voltage | 26 | 115 | 115 | 115 | 115 |
| R (Stall) Ohms | 196 | 1270 | 1250 | 490 | 280 |
| X (Stall) Ohms | 183 | 1560 | 1780 | 890 | 570 |
| Z (Stall) Ohms | 268 | 2210 | 2175 | 1030 | 640 |
| P F (Stall) | 0.73 | 0.57 | 0.58 | 0.49 | 0.45 |
| Effective R (Stall) Ohms | 366 | 3840 | 3800 | 2160 | 1460 |
| Parallel Tuning cond. for unity P.F. (Stall) Mfd. | 1.0 | 0.13 | 0.15 | 0.33 | 0.55 |
| Control Phase | - | 1 | | - | - |
| Voltage | 40/20 | 40/20 | 40/20 | 40/20 | 40/20 |
| •R (Stall) Ohms | 480 | 124 | 145 | 58 | 39 |
| •X (Stall) Ohms | 445 | 215 | 204 | 103 | 77 |
| *Z (Stall) Ohms | 660 | 248 | 250 | 118 | 86 |
| •PF (Stall) | 0.73 | 0.50 | 0.58 | 0.49 | 0.45 |
| •Effective R (Stall) Ohms | 910 | 495 | 430 | 240 | 190 |
| Parallel Tuning cond. for unity P.F. (Stall) Mfd | 0.4 | 1.4 | 1.3 | 2.9 | 4.1 |
| Mechanical Characteristics | - | - | | | |
| Rotor Inertia (gm. cm²) | .47 | .47 | 1.07 | 3.3 | 4.0 |
| Weight (oz.) | 1.2 | 2 | 4.5 | 8 | 14 |
| Mounting Type | Synchro | Synchro | Synchro | Synchro | Synchro |
| Motor Length | .863 | .672 | 1.703 | 1.625 | 2.03 |
| Type Shatt | Pinion | Pinion | Plain | Plain | Plain |
| Shaft Extension | .375 | .218 | .437 | .540 | .540 |
| Outside Diameter | .750 | .937 | 1.062 | 1.437 | 1.750 |
| Lype Connection | Leads | Terminals | Terminals | Terminals | Terminals |



Size 8



Size 10



Size 11



Size 15

Size 18

*For 40v connection

This complete line can be varied by Oster specialists to your precise requirement. Write today for further information, enclosing detailed data on your needs.

Other products include motorgear-trains, synchros, AC drive motors, DC motors, servo mechanism assemblies, motor tachs, servo torque units, reference and tachometer generators, actuators, motor driven blower and fan assemblies and fast response resolvers.

BURTON BROWNE ADVERTISION



Engineers For Advanced Projects:

Interesting, varied work on designing transistor circuits and servo mechanisms. Contact Mr. Zelazo, Director of Research, in confidence.

CIRCLE 162 ON READER-SERVICE CARD FOR MORE INFORMATION



Sylvania...your only source for both semiconductor materials

LF YOU NEED MATERIALS for transistors, diodes, or other semiconductor devices ... Sylvania is your only dependable source of both germanium and silicon.

The following forms of Sylvania germanium products are available; spectrographically pure germanium dioxide; polycrystalline as-reduced ingots; polycrystalline purified ingots; and undoped single crystals. All Sylvania germanium is n-type, and—in the purified ingot or single crystal form—has a resistivity greater than 40 ohm cm.

Diode and transistor manufacturers report that Sylvania germanium makes it possible for them to use the same doping schedule from shipment to shipment. They report higher yield in the growth of doped single crystals. For growing doped crystals horizontally, Sylvania germanium ingots are purified in five standard shapes, or to your specification. Cut pieces, which require no further cutting or etching, are supplied to fit your crucible for vertical crystal growing.

Sylvania silicon is available in the form of polycrystalline stalagmitic rod; average density is 2.2 g/cc. The standard diameter for stalagmitic rod is $1\frac{1}{2}$ in., and it is available in pieces or crucible charges to your specification.

If you have special requirements, our engineering department will gladly consult with you. Send for technical literature on Sylvania germanium and silicon. Write to:

SYLVANIA ELECTRIC PRODUCTS INC. Tungsten and Chemical Div., Towanda, Penn.

TUNGSTEN . MOLYBDENUM . CHEMICALS . PHOSPHORS . SEMICONDUCTORS



LIGHTING

RADIO ELECTRONICS TELEVISION CIRCLE 164 ON READER-SERVICE CARD FOR MORE INFORMATION ATOMIC ENERGY

New Products

Electromechanical Counter

300 Million Counts



A life of 300 million counts, count rate up to 60 per sec, either electrical reset or manual reset by a single-stroke push bar, and switch readout circuitry are features of an electro-mechanical counter. The unit adds, subtracts, and totalizes. If add and subtract pulses are received simultaneously, a zero count results. It is not necessary to have any specific sequence of add or subtract impulses, nor will the counter jam from an incomplete pulse. The totalizer will operate best with a counting-pulse ratio of 50 per cent on, 50 per cent off. While a square wave pattern for the pulse shapes is best, the totalizer will handle a wide variety of pulse shapes providing the leading edge of the wave is reasonably steep.

Autron Engineering, Dept. ED, 1254 W. Sixth St., Los Angeles 17, Calif.

CIRCLE 165 ON READER-SERVICE CARD FOR MORE INFORMATION



Sampling Switch High Speed For as a

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CIRCLE

A precision switch having radial terminals designed for military and commercial applications is available with one or two poles and up to 120 shorting channels or 60 non-shorting channels per pole. The switch is easily adapted to a variety of motor drives. It is equipped with a precision machined ball bearing output shaft, constant force perma brushes and lifetime semi-molded contact plates for long service free life. Approximate dimensions are 2.620 in. diam x 1.332 in. length plus hub extension 3/4 in. diam by 1/2 in. length and shaft 1/4 in. diam by 3/4 in. length. Applications include special oscilloscope displays, error indicating systems, and multichannels data systems.

General Devices, Inc., Dept. ED, P. O. Box 253, Princeton, N.J.

CIRCLE 166 ON READER-SERVICE CARD FOR MORE INFORMATION

VHF Directional Antenna

Gain of 23 Db



For 100 to 500 mc use, this directional antenna has a low vswr at any frequency in the band, accomplished through a rear adjusting balun and reflector assembly. The model CF-121M is a 12 ft. diam. antenna and utilizes a dipole exciter. Gain is 23 db or better at 500 mc, with minimum side lobes and cross polarization of 20 db or better. The antenna is of lightweight, all-aluminum mesh construction, fully weatherized and corrosive resistant. It is available in both the 12 ft. diam model CF-121M, and a 14 ft. diam model CF-141M. Ainslie Corp., Dept. ED, 312 Quincy Ave.,

Quincy, Mass.

CIRCLE 129 ON READER-SERVICE CARD FOR MORE INFORMATION



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X-Band Stabilization System High Short-Term Stability

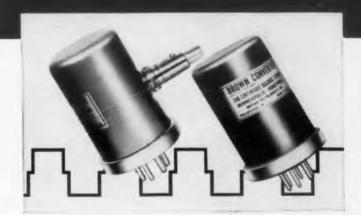
In combination with the VA-201B Klystron, the BA-1280B Stalo Cavity achieves a short term frequency stability of better than one part in a billion. The stabilization factor of the cavity is completely independent of the oscillator fluctuations or external disturbances. According to the manufacturer, this feature provides an advantage over stabilization systems utilizing the feedback principle. The elimination of all electronic components except the klystron oscillator provides reliability and longer life. The cavity tunes over the range of 8200 to 10,000 mc, depending on the klystron used. A method is utilized to suppress all undesired modes within this fance.

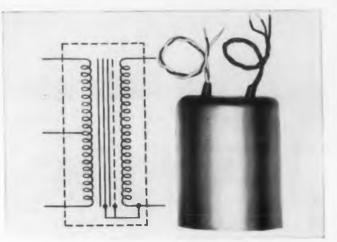
Varian Assoc., Dept. ED, 611 Hansen Way, Palo Alto, Calif.

| ION | CIRCLE 17 | O ON | READER-SERVICE | CARD FOR | MORE | INFORMATION |
|-------|-----------|------|----------------|----------|-------|-------------|
| 1 m m | | | READER-JERVICE | CARD FOR | NUCKE | INFORMATIO |

Use high-quality, dependable BROWN COMPONENTS

in your measuring circuits and servo loops







For additional details, call your nearby Honeywell sales engineer. He's as near as your phone.

MINNEAPOLIS-HONEYWELL REGULATOR Co., Industrial Division, Wayne and Windrim Avenues, Philadelphia 44, Pa.—in Canada, Toronto 17, Ontario.

CONVERTERS—Handle d-c signals as small as 10-8 volt. SPDT switching action. Sensitive, stable performance. Ideal for computers, servomechanisms, balancing circuits. Available with special features such as fungus proofing, grounded housing, mica-filled base, various contact percentages. Weight: 10 ounces. Driving coils in 60, 40 and 25 cycle converters are energized by 6.3 volt a-c. 400 cycle uses 18 volts. Other coil ratings as follows:

| Converter Type | Impedance | D-C Resistance | Power Consumption | Current Drain |
|--------------------------|-----------|-------------------|----------------------|------------------|
| 60 cycle | 125 ohm | 110 ohm | .3 watts | .05 amps |
| 25 and 40 cycle types | 65 ohm | 55 ohm | .60 watts | .10 amps |
| 400 cycle | 191 ohm | 110 ohm | 1.7 watts | .094 amps |

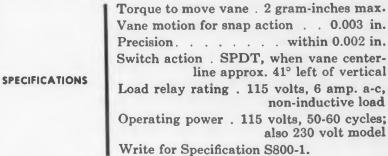
Write for Specification S900-2.

INPUT TRANSFORMERS—Handle low-frequency a-c, or choppermodulated d-c signals from .005 to 200 millivolts, such as generated by thermocouples or other transducers. Designed with highly efficient shielding. Measure $1\frac{5}{8}$ " in diameter, $2\frac{3}{12}$ " high.

| Choose from three models | | 355567-1 | 356326 | 35567-2 | |
|--------------------------------|---|--|--|--|--|
| Primary (center- tapped) | turns (½ primary) Resistance (approx.) 60 cps impedance Impedance, full pri. | 600 30 ohms 1,300 ohms 5,200 ohms | 1,094 450 ohms 7,500 ohms 30,000 ohms | 3,400 750 ohms 30,000 ohms 120,000 ohms | |
| Secondary | turns Resistance (approx.) Capacity to tune to 60 cycles | 9,600 2,500 ohms .015 mfd. | 17,500 5,800 ohms .001 mfd. | 12,000 3,400 ohms ,003 mfd. | |
| Weight | | 5.7 oz. | 7.1 oz. | 6 oz. | |

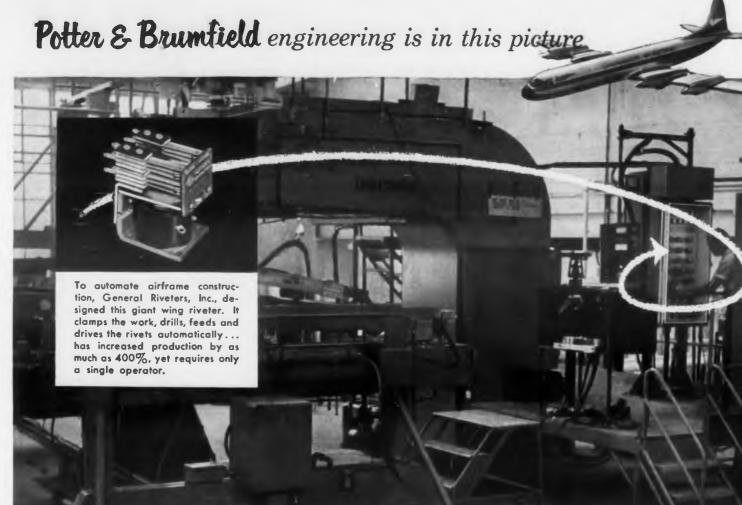
Write for Specification S900-1.

ELECTR-O-VANE CONTROL UNIT—A torque of 2 gram-inches or less actuates this precision switch. Use it as a limit switch to operate valves, lights or hopper openings, in response to motion of weighing beams or other members. Use it to sense other mechanical movements—to operate protective devices when a diaphragm is bulged or near rupture, for example.





57 ELECTRONIC DESIGN . July 15, 1957



P&B RELAYS AUTOMATE THIS GIANT RIVETER for new Lockheed Electra Wings

This new automatic riveter will be used to make wings for the new Lockheed Electra, a prop-jet luxury liner, as well as many other modern aircraft. The heart of this riveter is a relay circuit that "takes orders" from a pattern of holes punched in 35 mm film strips.

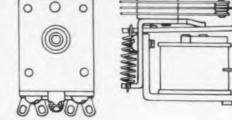
General Riveters, Inc. selected the GA Series P&B relay for the control circuits of this riveter because of its unusual dependability and versatility. In adapting this relay to a specific application, P&B's engineers again demonstrated how 25 years of creative engineering can pay off by providing a standard type or completely new relay to solve your particular problem. Write today for new compact catalog or engineering consultation.

P&B Standard Relays are available at your local electronic, electrical and refrigeration distributors



PRINCETON, INDIANA Subsidiary of AMERICAN MACHINE & FOUNDRY COMPANY Manufacturing Divisions also in Franklin, Ky. and Laconia, N. H. CIRCLE 172 ON READER-SERVICE CARD FOR MORE INFORMATION

ENGINEERING DATA GA SERIES RELAY Multiple Leaf AC or DC 0



CONTACTS

Material: 3/16" fine silver (other contact materials can be furnished for specific applications)

Rating: 5 amp. 115 V. 60c non-inductive load Arrangements: 4 Form C Max., AC; 6 Form C Max., DC Breakdown: 1000 V. RMS between all elements

COIL

Resistance: 30,000 ohms max.

Power req'd: 6 W. max., 2 W. min. DC at 25° C. ambient V range: DC to 110 V.; AC to 230 V.

DIMENSIONS, MAX. 123/32" L. x 11/16" W. x 125/32" H.

MOUNTING DATA

4 tapped #6-32 holes, .750" x .875" o.c. 1 tapped #8-32

core **ENCLOSURES**

Hermetically sealed, octal plug: 21 7/12" x 129/12" x 125/12" Multiple solder header and miniature plug-in: 215/12" x 129/12" x 125/12"

- Special container required for 6 Form C
- TERMINALS Contacts: two #16 AWG wires

Coil: two #20 AWG wires See our catalog in Sweet's Product Design File

New Products

TEFLOI LAMEN BRAID

Air Dielectric Cable Low Capacitance

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This Teflon-air dielectric coaxial cable has a nominal overall diameter of 0.22 in. The conductor is No. 30 AWG, 7/38 silver plated copperweld. A choice of outer jackets include Teflon, lacquered nylon braid, and Teflon or silicone impregnated glass braid. The low attenuation of the 10 µµf cable makes it useful for high frequency, low level applications and as a low capacitance probe. Capacitance values of less than 10 µµf, with somewhat larger overall diameters are also available on request.

Flexibility is one of the features of the coaxial cable. Among the other characteristics are solderability, light weight, small size, and ready adaptation to a variety of connectors.

Tensolite Insulated Wire Co., Inc., Dept. ED, 198 CIRCL Main St., Tarrytown, N.Y.

CIRCLE 173 ON READER-SERVICE CARD FOR MORE INFORMATION



DC Power Supply 200 to 325 v, 0 to 100 ma

Continuously variable output from 200 to 325 v de for load currents of 0 to 100 ma can be obtained from the Model 3. Regulation is better than 1 per cent for loads of 0 to 100 ma and line voltage variations from 105 to 125 v. Ripple is less than 10 mv rms. Both positive and negative sides of the ouput are isolated from ground. Either side may be grounded or the output may be left floating. An isolated output of 6.3 volts ac at 3 amp is available at the output terminal connections. Net weight is approximately 20 lb, and it measures 5 wide, 7 high, and 16 in. deep.

Associated Specialties Co., Dept. ED, 1751 Main St., Orefield, Pa.

CIRCLE 174 ON READER-SERVICE CARD FOR MORE INFORMATION



able ce

Snap-In Vise For Connectors

Round connectors are securely held during sollering operations by the Model V-3 Snap-in Vise. spring loaded jaw provides the necessary presmure to hold the connector. Adjustment of the vise nomi- for any desired diameter may be done quickly. Once is No. this adjustment is made, slight pressure on a lever choice engages or disengages the connector from the vise. nylon This feature is especially useful in production asglass sembly where repetitive operations are carried out. Jaws are covered with a tough non-skid cork and nakes synthetic rubber compound which protects threaded ations values portions from damage. The vise can be adjusted all di- anywhere within an arc of 180 deg. Connectors up to 2 in. in diam, are tightly held in the vise. Screws oaxial are provided for easy mounting on a work bench older. or plywood base.

Western Electronic Prod. Co., Dept. ED, 655 lapta-Colman St., Altadena, Calif.

), 198 CIRCLE 176 ON READER-SERVICE CARD FOR MORE INFORMATION



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Standard and Null Meter Model 301

This variable DC standard and null meter, Model 301, utilizes a chopper stabilized circuit which con-325 v stantly compares the output with an internal standained ard cell to provide stability and accuracy. Direct-1 per reading, calibrated dials provide instant voltage variaselection. Power supply output voltage is 1 to 501 v 0 mv at up to 20 ma. It has 4 decaded null meter ranges ouput from 50 v to 501 mv full scale. The meter can also y be be used to read input voltage or the output voltage n isoof the supply. The unit features 0.01 per cent stable at bility, 0.2 per cent accuracy, 0.022 per cent line and load regulation, less than 100 mv ripple, 0.2 msec response time, and less than 0.01 output impedance. Kin Tel, Dept. ED, 5725 Kearny Villa Rd, San

Main Diego, Calif.

CIRCLE 177 ON READER-SERVICE CARD FOR MORE INFORMATION

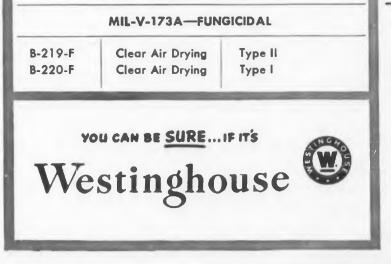
Now NEAR THIS ! THIS ! HEAR THISI

DESIGN ENGINEERS! ELECTRICAL ENGINEERS! REPAIR SHOP FOREMEN! LOOKING FOR A LINE OF U. S. NAVY-APPROVED INSULATING OR FUNGICIDAL VARNISHES?

HERE IT IS!

A Complete Westinghouse Leadership Line of Military-Approved Insulating and Fungicidal Varnishes for Original Equipment Manufacturers and Repair Shops.

| MIL-V-1137A—INSULATING | | | | |
|------------------------|------------------|----------------------|--|--|
| GRADE | ТҮРЕ | MILITARY DESIGNATION | | |
| B-161 | Clear Baking | Grade CB, Type M | | |
| B-163-N | Clear Baking | Grade CB, Type M* | | |
| B-166-1 | Clear Baking | Grade CB, Type M | | |
| B-222-N | Clear Air Drying | Grade CA, Type M* | | |
| B-340-N | Black Baking | Grade BB, Type M* | | |
| B-451-N | Black Air Drying | Grade BA, Type M | | |



Whether you're designing, manufacturing, or repairing military electrical apparatus, or whether you simply need quality insulating or fungicidal varnishes or enamels for critical applications, you can't do better than the Westinghouse Leadership Line of insulation materials, field proven in over 100 million applications!

The chart at left shows some of these remarkable products, approved by the U.S. Navy. For complete information, call your nearest Westinghouse branch or write for your free copy of the 8-page Leadership Line Catalog of insulating materials. Just fill out the coupon below. **J-0665**9

ED-7-57 Westinghouse Electric Corporation **Benolite Plant**

Manor, Pennsylvania

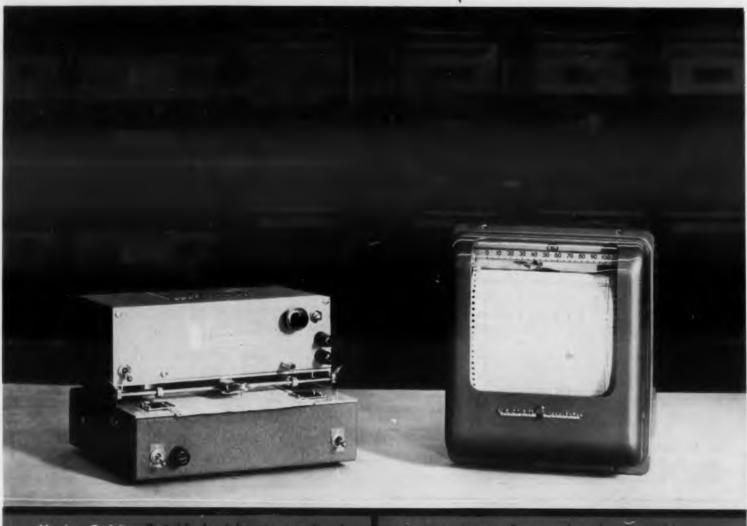
Please send free copy of Leadership Line Catalog.

| Name | | | |
|---------|------|-------|--|
| Title | | | |
| Firm | | | |
| Address | | | |
| City | Zone | State | |
| City | Zone | State | |

CIRCLE 178 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN • July 15, 1957

Varian Strip Chart Recorders POTENTIOMETER PERFORMANCE* AT MODERATE COST



Varian G-10 — Particle for laboratory or bands as where chart accessibility is of prime importance. Take price \$340. Varian G-11 – For panel, rack or poriable user designed for OEM, lab or field for long-term maniforing. Base price \$450.

*

The servo-balance potentiometer method has long been used in expensive recorders to achieve superior stability, sensitivity, ruggedness and high input impedance. Use of servo balancing systems assures full realization of these inherent advantages by providing ample power independent of the source being measured. Now Varian offers you recorders of moderate cost using this time-proven principle.

> Varian recorders are sold and serviced throughout the free world by representatives in principal cities.

VARIAN SPECIFICATIONS:

- Spans as low as 10 mv
- Limit of error 1 %
- Maximum source resistance 50K ohms or higher
- Balancing times: 1 second or 2.5 seconds on G-10; 1 second on G-11

WRITE TODAY FOR COMPLETE SPECIFICATIONS



PALO ALTO 21, CALIFORNIA

Varian Associates manufactures Klystrons, Traveling Wave Tubes, Backward Wave Oscillators, Linear Accelerators, Microwave System Components, R. F. Spectrometers, Magnets, Magnetameters, Stalos, Power Amplifiers and Graphic Recorders and offers research and development services.

CIRCLE 180 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products



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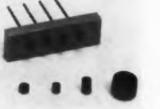
La

CIRC

Known as the Golden Gnat Rate Gyro, Type GM has the following features: size of 1 in. diam, 2-14 in. length; weight of 3.8 oz; range of full scale rates up to 600 deg per sec; threshold and resolution of 0.01 deg per sec; inertia ratio of 0.00045 sec (ratio of gimbal inertia to angular momentum); temperaturecompensated viscous damping for controlled dynamic performance; variable reluctance pickoff for high signal-to-noise ratio with infinite pickoff resolution; linearity of 0.1 per cent of full scale to 12 range, within 2 per cent to full range; ambient temperature range of -55 to +85 C; linear vibration of 10 g peak, 0 to 2000 cps; linear acceleration up to 100 g depending upon range; and shock up to 100 g depending upon range.

Minneapolis-Honeywell Regulator Co., Dept. ED. Boston Div., 1400 Soldiers Field Rd., Boston 35 Mass.

CIRCLE 181 ON READER-SERVICE CARD FOR MORE INFORMATION



Ceramicite For Hermetic Seals

Ceramicite is a leak-tight ceramic hermetic seal used in relay bases, transformer bases, transistor bases, diode closures and other such component in continuous operation at temperatures up to 700 F. The heating required by the sealing process causes changes in the linear expansion properties of the materials resulting in a common coefficient permitting crystalline migration between interfaces of the materials involved during the cooling cycle. Thus an actual molecular bond exists between the metal and the Ceramicite. Ceramicite is available in two forms: as pre-formed pieces, ready for firing by the user in fabrication of seal components and as completed seal components, such as single and multiple pin terminals and headers.

Consolidated Electrodynamic Corp., Dept. ED. 300 N. Sierra Madre Villa, Pasadena, Calif.

CIRCLE 182 ON READER-SERVICE CARD FOR MORE INFORMATION



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Punched Card Sensor Multiple Switching Device

This static reader for punched cards, a multiple switching device that simultaneously senses the entire card, is adaptable to any combination of 540 switching operations. The card reader accepts a standard punched-card with 540 holes, arranged 12 wide by 45 high, which is read or sensed when the handle is closed. In each hole position is a spring-loaded pin and a corresponding normally closed switch with each side isolated. The pin remains static where there is a hole in the card. Where there is not a hole in the card the pin moves forward and opens the corresponding switch. The card reader measures approximately $6-1/4 \times 10-1/4$ $\times 9$ in., and weighs 18 lb. It may be installed in any circuitry by means of standard connectors.

Metron Corp., Dept. ED, Union and Elm Sts., Lambertville, N.J.

CIRCLE 184 ON READER-SERVICE CARD FOR MORE INFORMATION

Variable Delay Line

Model 502

This continuously variable delay line, Model 502,

is designed for use as a component or as test equip-

ment in advanced computer and radar systems. The

entire delay range, from zero to maximum delay, is

covered by a single control shaft, in ten turns. The

unit may be locked at the desired delay by a

locking device which is available from the manufac-

turer. It can then be used as a component in equip-

ment with a fixed delay, or as a continuously vari-

able test unit. Attenuation in the new unit is 1.2 db.

Resolution is better than 1/1000 of maximum delay.

Termination is external. Maximum delay is 2.0 µsec.

Maximum rise time is 0.38 usec. Impedance is 470

ohms. Outside dimensions are 7 1/4 x 1 x 1 5/8 in.

Four other variable delay lines which feature max-

imum delays from 0.9 to 15.0 µsec., Maximum rise

times from 0.18 to 2.8 µsec., and impedance from

ESC Corp., Dept. ED, 534 Bergen Blvd. Pali-

CIRCLE 185 ON READER-SERVICE CARD FOR MORE INFORMATION



FROM SPECS TO PROTOTYPES---FAST

Globe Industries makes to special order all of the miniature motorized devices shown on this page. But so do a lot of other companies. The difference lies in your design freedom.

At Globe you can set the specs and get prototypes in a few weeks. Our special order department builds these under the direction of the engineering department. And production orders are delivered in a few months because Globe maintains enormous inventories around which most custom designs are based.

Globe's broad base of standard parts has helped earn a reputation for earliest prototype delivery, fast production, reasonable price, aircraft standards, and repeat-business quality. Parts for your servo, timing, control, power, or air moving systems may be in Globe's inventory now. MIL specs and special development (including temperatures to $+500^{\circ}$ F.) are routine at Globe Industries.

Catalog sent to qualified firms; please request it on your letterhead. Inquire now about products which interest you. Get a Globe proposal on your next design.

1. GEAR REDUCED MOTORS

6 basic AC and DC motors, 2 basic gear types with 112 odd and even ratios, as well as various brakes, clutches, shafts, governors, windings and mountings. Above unit powered by SS motor. Inventoried parts for SS motors can be combined in $6x10^{17}$ different ways.

2. RATE GYROS

5-10 cps. is natural frequency. Provides adjustable damping and control contacts, withstands 60Gs for 11 milliseconds repeatedly. Above unit powered by MM motor. Inventoried parts for MM motors can be combined in 10¹⁹ different ways.

3. TIMERS

AC or DC operated timing cycles to order, from a few seconds to many minutes, adjustable or non-adjustable. multiple switching actions. Can be powered by any motor, such as the LL. Inventoried parts for LL motors can be combined in 8x10¹⁷ different ways.



GLOBE INDUSTRIES, INC.

Dayton 4, Ohio • Phone: HEmlock 3741

CIRCLE 186 ON READER-SERVICE CARD FOR MORE INFORMATION

4. CENTRIFUGAL BLOWERS

Many standard models with typical alr delivery of 22 cfm. at 1" back pressure. Unit above is SC. Inventoried parts for SC motors can be combined in 10^s different ways.

5. AXIAL BLOWERS

Many standard models with typical air delivery to 58 cfm. in above configuration and over 300 cfm. with open axial fan. Above unit powered by MC motor. Inventoried parts for MC motors can be combined in 12×10^4 different ways.

6. ACTUATORS

3 standard models around which custom units are designed, with intermittent torques up to 2500 oz. in. Above unit powered by FC motor. Inventoried parts for FC motors can be combined in 10^s different ways.

ELECTRONIC DESIGN . July 15, 1957

56 to 1000 ohms are available.

sades Park, N.J.

polystyrene capacitors

worth their weight in GOLD!

Dearborn

You'll find Deltaply "85" capacitors ideal for applications involving such critical factors as small uniform capacitance change with temperature . . . high Q . . . very high insulation resistance . . . very low dielectric absorption . . . and high stability. The "85" offers exceptional electrical properties in temperature range -55°C to +85°C. Temperature-capacitance co-efficient is -120 PPM/°C and is very nearly linear. Insulation resistance in megohms x mfd. varies from 10 million at 25°C to 200,000 at 85°C.

Capacitance values from .0001 to 10.0 mfd. are available in hermetically sealed metal tubes or CP-70 cans in six standard voltage ratings from 50 to 1000 volts.

WRITE FOR BULLETIN RL-1

DEARBORN ELECTRONIC LABORATORIES 1421 NORTH WELLS STREET • CHICAGO 10, ILLINOIS



CIRCLE 188 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

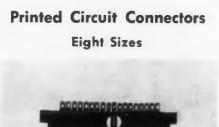


Packaged Power Supply **Hermetically Sealed**

These hermetically sealed high voltage power supplies are convenient means of supplying high voltage to devices such as cathode ray tubes, oscilloscopes, TV equipment, and precipitators. The units are made by hermetically sealing all components in a metal can with suitable insulating oil. The advantages of this unitized power supply are greater reliability, long use life, more compactness and greater convenience. Different models give output voltages of 2 kv at 2 ma, 5 kv at 5 ma, 10 kv at 1 ma, 15 kv at 1 ma, 30 kv at 1 ma, and 50 kv at 1 ma.

Laboratory for Electronics, Inc., Dept. ED, 75 Pitts St., Boston 14, Mass.

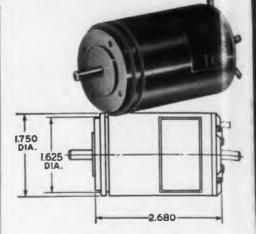
CIRCLE 189 ON READER-SERVICE CARD FOR MORE INFORMATION



These printed circuit connectors are available in eight different sizes, 6, 8, 10, 12, 15, 18, 22 and 38 and feature .058 wide coined beryllium copper contacts, heat treated to retain contact force after hundreds of insertions. Wide contact pads insure minimum abrasion under maximum contact force. Excessive contact mass insures lower heat rise at rated loads. Barriers between terminals insure high voltage break down ratings exceeding 2500 v rms at sea level and 700 v rms at 60,000 ft. Present models are available for printed circuit board thicknesses from .061 to .071. Polarizing pins may be located in any slot desired. Materials and construction match requirements called out in MIL-C-8384.

Gorn Electric Co., Inc., Dept. ED, Gorn Electronics Div., 845 Main St., Stamford, Conn.

CIRCLE 190 ON READER-SERVICE CARD FOR MORE INFORMATION



FOUR NEW VERNISTAT POTENTIOMETERS

WITH HIGH LINEARITY LOW PHASE SHIFT LOW OUTPUT IMPEDANCE

There is a Vernistat a. c. potentiometer to meet your requirements. Uniquely combining the functions of an auto-transformer with an interpolating resistance, the Vernistat potentiometer offers low output impedance and precise linearity plus long term stability.

The Model 2B Vernistat potentiometer is available in five versions. Check these specifications:

Model 2B

Output impedance (max) - 130 ohms Linearity - ±0.04% Max. input voltage - 130 Output quadrature (max) - 0.50mV/V

Model 2B1

Output impedance (max) – 470 ohms Linearity – ±0.03% Max. input voltage – 130 Output quadrature (max) – 0.13mV/V

Model 2B2

Output impedance (max) — 45 ohms Linearity — ±0.05% Max, input voltage — 65 Output quadrature (max) — 0.47mV/V

Model 2B3

Output impedance (max) — 130 ohms Linearity — ±0.03% Max, input voltage — 65 Output quadrature (max) — 0.16mV/V

Model 284 Output impedance (max) – 470 ohms Linearity – ±0.02% Max. input voltage – 65 Output quadrature (max) – 0.06mV/V

For additional information write:



division PERKIN-ELMER CORPORATION Norwalk, Connecticut CIRCLE 191 ON READER-SERVICE CARD

ELECTRONIC DESIGN • July 15, 1957

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Protective Coating

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A strip-off plastisol coating for the rotection of metal parts and products an be applied by heating the parts nd dipping them in the plastisol. The lastisol can be peeled off readily by and and serves as a protective coatng for any metal parts which are subect to rust, corrosion, dirt or damage while in storage or transport. The oating provides resilient cushioning which reduces shock and breakage, nd is a defense against nearly all hemicals including most acids, alalis and solvents. It also has high hermal and electrical insulating ualities and is completely unaffected by extreme cold or hot weather. It esists mold, mildew, salt air and water and is not deteriorated by ime or exposure.

Auburn Button Works, Inc., Dept. ED, Chemical Div., Auburn, N.Y.

CIRCLE 193 ON READER-SERVICE CARD

Teflon Film

Thin Film Laminate

Type CSC cast Teflon film is a cured, semicured film or Teflon in its intered and partially sintered forms. It is comprised of a composite laminate of a minimum 2 mils of fullycured cast Teflon superimposed by a 0.25-mil layer of semicured Teflon in particulate form bonded together to resist normal handling. Final insulation thickness is maintained after fusion because of the use of fullycured Teflon. It is also offered in a 1.25-mil thickness. Suggested applications may include high-temperature wire insulation or the construction of thin-wall flexible Teflon tubing. Available in continuous roll lengths of 100 and 500 ft, in widths from 1/4 to 1 in. in increments of 1/16 in. Packaged on 3-in. ID cores.

Dilectrix Corp., Dept. ED, Allen Blvd. and Grand Ave., Farmingdale, N.Y.

CIRCLE 194 ON READER-SERVICE CARD

CIRCLE 195 ON READER-SERVICE CARD >

TRANSISTORIZED



Input: 105-125V, 60-500 cps, approximately 3A. Output: 100-150V, 0-1.5A. Ripple: ONE MILLIVOLT RMS. Regulation: Line, 0.1%, 105-125V. Load, 0.1%, NL-FL. Transient Response: ZERO-LAGGED for \pm 10% line transient or \pm 25% load transient. Output Impedance: 0.06 ohms at dc. Less than 0.5 ohms, DC-500KC. Meters: 0-150 volts, 0-2 amperes, 4½" rectangular, 2%. Size: Standard 19" panel, 5¼" high, 14¾" deep behind panel. Duty: Continuous, between -20°F and 110°F, 100% humidity, 0 to 10,000 feet.

Polarity: Reversible and floatable to 500V peak from chassis ground.

Price: \$465. f.o.b. Kenilworth, New Jersey. Generous quantity discounts. Delivery 15 days.

solid state power supplies have Everything!

ULTRA COMPACT-More power supply per inch of panel height than ever before!

COOL—Throws less heat into the cabinet than any other type of supply ... 1/10th the heat generated by vacuum-tube equivalents.

FULLY TRANSISTORIZED—Semi-conductor rectifiers, zener-diode reference standards, transistor series regulators, transistor loop amplifiers.

CA

HIGH STABILITY-Improved high-gain balanced PNP amplifier-prestabilized zener reference.

LOWER PRICE-As much as 30% less than inferior vacuum-tube equipment.

TEN MODELS—Covering 0-300V at 0-1.5 amperes for every plate, bias, and clamp application.

Write for our Solid State Catalog.



Corporation Electronic Development & Manufacturing

RNEGIE AVENUE, KENILWORTH, NE

Competent Engineering Representation Everywhere

hot's some on up there? American Electronic's new 300 KC Band Width **RECORDATA** magnetic recording system gives an accurate, permanent record.

projects where extreme accuracy is required, RECORDATA offers a new concept in reliability and versatility. This exteen channel system with its modular construction offers many unique features. For example, the six standard tape speeds of 17s, 334, 732, 15, 30 and 60 inches per second can be instantly selected with a single switch without changing belts or pulleys. Special speeds to 240 inches per second are also available. Automatic controls assure constant tape tension from beginning to the end of the reel, regardless of size.

of the reel, regardless of size. Quickly interchangeable tape guides accommodate ¼" ½" or I" tapes. The plug-in magnetic head assemblies are extremely accurate and provide data tracks with the best electrical uniformity. Where fidelity and reliability are necessary in a data recording system you can depend on RECORDATA ...manu-factured by American Electronics whose Concertone Hi-Fi tape recorders have been famous as quality leaders. Write to Dept. Jy34 tor complete techni-cal information. al information.



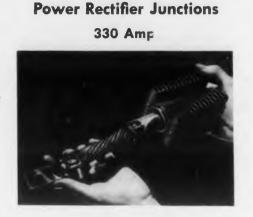
AMERICAN ELECTRONIC

655 W. Washington Blvd. INC. Los Angeles 15, California

Have you heard about the wonderful Engineering opportunities at AMERICAN?

CIRCLE 197 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products



This 330 amp germanium power rectifier junction is one of a series of six rated at 330 amps rectified output current with voltage ratings from 20 to 66 v rms. These low current density high capacity junctions have corrosion and moisture resistant castaluminum housings with airfoil type cooling fins for maximum heat dissipation. The unit size is 4 3/32 x 3 x 3 1/4 in. Six 330 amp germanium junctions connected in a three-phase bridge circuit will deliver 85 kw, (1,000 amps @ 85 v) while occupying 1/2 cu ft of space. Its efficiency rating is to 98.5 per cent.

International Rectifier Corp., Dept. ED, 1521 E. Grand Ave., El Segundo, Calif.

CIRCLE 198 ON READER-SERVICE CARD FOR MORE INFORMATION

Double Stub Tuner Locking Collets

This double stub tuner, Model DS-1-12, has an impedance of 50 ohms and a frequency range of 1000 to 12,000 mc. A pair of collets locks the tuner securely in any pre-set position. The device employs silver plated contact springs, rugged stub junction construction and smooth acting, non-slip tuning elements. The tuning elements can be furnished with or without collet-type locking caps. The hex shaped body of the tuner facilitates holding or mounting in any position.

Uniwave, Inc., Dept. ED, 2 Marine St., Farmingdale, N.Y.

CIRCLE 199 ON READER-SERVICE CARD FOR MORE INFORMATION



Application-engineered microwave parts and complex assemblies are our specialized field. We'll manufacture components to your prints ...or we will design and integrate them into your application.

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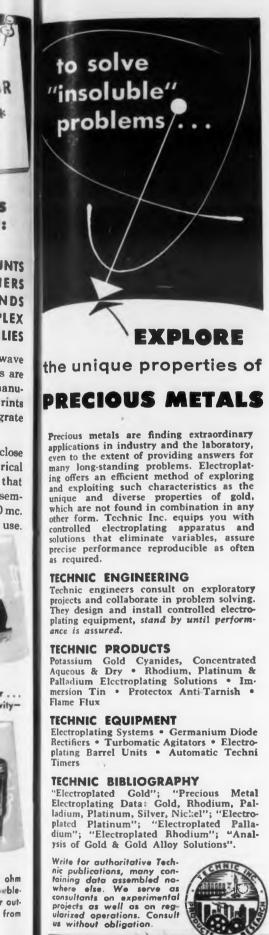
You can depend on J-V-M for close coordination, guaranteed electrical performance and "know how" that is attested by innumerable assemblies ranging from dc. to 40,000 mc. now in industrial and military use.



ELECTRONIC DESIGN . July 15, 1957

(Chicago Suburb)

CIRCLE 200 ON READER-SERVICE CARD



Phasemeter 60 Cps-20 Kc

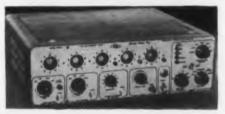
The PM-1B Phasemeter offers accurate measurement and calibration of phase relationships in complete systems and in electronic instrumentation at audible and supersonic frequencies. Featuring a passive system utilizing neither tubes nor semiconductors, the PM-1B phasemeter will retain its calibration accuracy of better than \pm 1/2 deg for very extended periods. The meter is available in two models: a single frequency unit which can be provided for any single frequency between 60 cps and 20 kc; and a three frequency unit which can be provided for any three selected frequencies between 60 cps and 20 kc. Continuous measurement of the phase angle from 0 to 360 deg may be obtained, while lead and lag angles may be measured directly from any reference desired. High impedance input with low impedance output; a large direct reading dial with adjustable zeroing and a constant amplitude output are other features.

The size of the unit is $7 \times 7 \times 7 \times 1/2$ in. and it weighs approximately 6 lbs.

Statham Development Corp., Dept. ED, 12411 W. Olympic Blvd., Los Angeles 64, Calif.

CIRCLE 203 ON READER-SERVICE CARD FOR MORE INFORMATION

Frequency Interval Meter Period and Time



Model 7550B features only one glow transfer counting tube per decade for both counting and indication, 200 mv input sensitivity, a self-test function switch for checking internal time base and counter decades, measuring capacities from 0.1 to 100 kc and 10 µs to 1.5 days, and a counter tube life expectancy of over 10.000 hours. Applications include flow measurement, filter characteristic determination, oscillator calibration, rpm monitoring, and timing of physical events.

Electro-Pulse, Inc., Dept. ED, 11861 Teale St., Culver City, Calif.

CIRCLE 204 ON READER-SERVICE CARD FOR MORE INFORMATION

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1957 ELECTRONIC DESIGN • July 15, 1957

39 Snow Street, Providence, R 1.

JAckson 1-4200

Chicago Office-7001 North Clark Street

THE LARGEST ENTERPRISE OF ITS KIND IN THE WORLD

CIRCLE 202 ON READER-SERVICE CARD

TECHNI

AMERICAN ELECTRONICS, INC.





...a revolutionary system for detecting leaks in transistors, diodes and other sealed units **for pennies each!**

RADIFLO offers a vast improvement over present leak detection methods because it measures the leak after the final sealing operation is completed. RADIFLO eliminates most of the expensive labor cost... yet gives the same or greater accuracy in a fraction of the time!

Here is how RADIFLO works. One or many parts are immersed under pressure in an inert, non-toxic radioactive gas. After air washing, the parts are passed over a scintillation counter which measures the molecular leakage to a normal sensitivity of one cc per 500 years.

Tests have shown that transistors can be checked at a cost as low as two cents each with corresponding savings on other types of parts. RADIFLO can also be easily set up on an assembly line for automatic parts inspection.

Even the initial cost of RADIFLO is low. Why not write today for complete technical information to Dept. No. 734Jy.





AMERICAN ELECTRONICS, INC. 655 W. Washington Blvd. Los Angeles 15, California

Have you heard about the amazing engineering opportunities at AMERICAN?

CIRCLE 205 ON READER-SERVICE CARD FOR MORE INFORMATION



... Designed especially for your applications



LIGHTWEIGHT because they are made of aluminum or magnesium castings produced in Joy's own foundries.

COMPACT design—with motor mounted inside the fan—permits installation anywhere...even inside a duct.

EFFICIENT vaneaxial design provides more air per given size than any other type fan.

AVAILABLE on a production line basis ... Joy has over 250 standard models with 1300 designs available to your specs ... from 1/500th horsepower up.

RUGGED because of simple design... the outer casing, the vanes and motor mounts are cast in one piece ... vibration free.

Get more information from the world's largest manufacturer and supplier of vaneaxial fans to companies like G.E., Hallicrafters, Lear, R.C.A., Motorola, Raytheon, Sylvania.

Write to Joy Manufacturing Company, Oliver Building, Pittsburgh 22, Pa. In Canada: Joy Manufacturing Company (Canada) Limited, Galt, Ontario.









Write for FREE Bulletin 135-57 WORLD'S LARGEST MANUFACTURER OF VANEAXIAL-TYPE FANS

CIRCLE 207 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

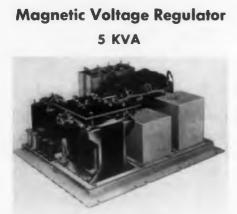


Concentric Dial Assembly Separate or Geared Inputs

This low inertia concentric dial assembly may be mounted so that the dial face is either parallel or perpendicular to the mounting surface. Input can be made perpendicular to the axis of rotation of the dial by the incorporation of a pair of miniature spiral mitre gears. Separate inputs to the two dials are provided permitting the comparison of two separate readings. Gears used are AGMA Class II. A hair-line indicator ensures accurate dial reading The dial assembly is a two-speed indicator, with standard ratios of 10:1 or 36:1 available. Other ratios are available on special order.

Reeves Instrument Corp., Dept. ED, 207 E. 91st St., New York 28, N.Y.

CIRCLE 208 ON READER-SERVICE CARD FOR MORE INFORMATION



The 5 kva automatic voltage regulator type TM7105 is designed for an input of 95-135 v, and an output of 115 v nominal, adjustable from 110-112 v. The accuracy of the unit is 1 v band for line voltage variations and/or load magnitude and power factor changes. It has a waveform distortion of 4 per cent maximum and a response time of less than 1/2 sec for ordinary line and/or load changes. The size is 21-9/16 x 19 x 12-3/16 in., weighing 215 lbs. Both input and output connections are made to the terminal board inside the cabinet.

Superior Elec. Co., Dept. ED, 83 Laurel St., Bristol, Conn.

CIRCLE 209 ON READER-SERVICE CARD FOR MORE INFORMATION

HIGH VOLTAGE TEST BREAKDOWN . . proves Johnson tube sockets are built to take it! Eliminate special set-up charges! End Pick the tube socket you need from sem Johnson's 3 basic grades ... tion Qua STANDARD—These are commercial grade socksh for general requirements. Bayonet Sockets equipped with porcelain bases, glazed top and sides. Phosphor bronze contacts .0002 cadmium plated. Nickel-plated hardware. Bayonet shells are etched aluminum. Water Sockets equipped with glazed steatite base—DC200 treated. Contacts are plated bross with steel springs. Shielded types equipped with etched aluminum blads mac Sha fast sem Shielded types equipped with etched aluminum shields. DTO wit INDUSTRIAL—Superior in quality to "Star types, equipped with glazed steatite bases, DC200 treated. Phosphor bronze or beryllium copper contact and springs, .0005 silver-plated. Fungus resistant cushion washers under contacts. Aluminum bayonet shells and shields for wafer types, fridite No. 14 treated. Ovi hec MILITARY—Top quality for military requirements. Glazed L4 steatite bases, DC200 treated, Bayont Sockets equipped with beryllium copper contach .0005 silver-plated. Hot tin-dipped solder terminals – brass bayonet shells, .0003 nickel-plated. Threaded brass bayonet shells, .0003 nickel-plated. Threaded hardware.0002 nickel-plated—unthreaded hardware .0003. With fungus resistant cushion washers under contacts. Wafer Sockets equipped with phosphor bronze contacts and beryllium copper springs, silverploted .001. Hot tin-dipped solder terminals, Engu-resistant, glass base melamine cushion washers under contacts. Aluminum shields on shielded types, No. 14 Woo Iridite treated. Entire socket protected for 200 how Screv salt spray test. Roll Balt Complete specification: Write for your copy of Socket Standardization Booklet 536, today1 E.F. Johns any a Comp 3412 Second Ave. S.W. . Waseca, Minner War CIRCLE 210 ON READER-SERVICE CARD ELI ELECTRONIC DESIGN • July 15, 1957

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End the bottleneck on your assembly line by precision application of fasteners. Southern Quality fasteners are precision made for precision production. Sharp pointed, threaded to start fast, hold tight. They speed assembly, lower rejects. Give your product Permanence and Quality with Southern Screws!

Over one billion fasteners stocked — in wide variety of finishes, heads, sizes and styles.

Your order filled in moments after receipt, if requested.

For free samples and Stock List write Box 1360-ED, Statesville, N. C.

Wood Screws • Stove Bolts • Machine Screws & Nuts • A, B & F Tapping Screws Roll Thread Carriage Bolts • Hanger Bolts • Dowel Screws • Wood & Type U Drive Screws



CIRCLE 212 ON READER-SERVICE CARD



Low Voltage Power Supply Regulation ± 0.2 Per Cent

These telemeter and strain gauge power supplies are designed for 400 cps operation, but are also available for 60 cps circuits. Hermetically sealed, the supplies have no moving parts and are self-protected for shorted output. Characteristics include a regulation of ± 0.2 per cent, ripple of 1 per cent rms, recovery time of 0.5 sec, and a variety of outputs. Gulton Industries, Inc., Dept. ED, Engineered Magnetics Div., Metuchen, N.J.

CIRCLE 213 ON READER-SERVICE CARD



Modulators and Demodulators For Tape Systems

FM-1A Modulators and FD-1A Demodulators are available for use with the modulator tape recording systems. The modulator produces an fm carrier suitable for magnetic tape recording and data transmission from a low-frequency signal. Each unit requires less than 6 ma at 180 v dc and 0.6 a at 12 v dc. Carrier output level is 100 v across 100,000 ohms; demodulator output level is 1 v across 20 K.

Electrodynamic Instrument Corp., Dept. ED, 2508 Tangley Rd., Houston 5, Texas.

CIRCLE 214 ON READER-SERVICE CARD



High Voltage Terminals 15 Kv to 50 Kv

Terminals in the 15 kv to 50 kv range have been developed. In addition to standard items, complete facilities to build custom terminals are in operation. The terminals are all twist-free, gasket type, and feature oil-filled design. Emphasis has been placed on raising the corona threshold.

Sphere Co. Inc., Dept. ED, Eagle Rock Bldg., 25 Amity St., Little Falls, N.J.

CIRCLE 215 ON READER-SERVICE CARD

957 ELECTRONIC DESIGN • July 15, 1957





MANUALLY OPERATED -- same contact arrangement and R F head as the 1460 Series. For chassis or panel mounting.

COAXIAL SWITCHES





PROJECT ENGINEER OPENING FOR R. & D. ELECTRONICS

Engineer on Microwave Antenna Systems with Southern California leader in Avionics. Excellent company benefits. Address inquiries to Personnel Director.

-they simplify design of RF systems

With TRANSCO switches, you can cut down the number of components in a system—one switch handles up to 6 circuits. TRANSCO switches are small, and light in weight. Each is supplied in a choice of configurations to simplify installation.

Adds versatility to a system. All channels on a TRANSCO can be operated independently, and there's a wide variety of make-and-break arrangements available. TRANSCO switches operate through 11,000 MC -a standardization which cuts your stocking requirements to only one switch for this entire R F band width

High-efficiency switching is due to minimum insertion loss, low VSWR, and high isolation between channels. TRANSCO units are qualified to applicable military specifications. Performance has been fully confirmed in the field, where thousands of units are giving dependable service.

Technical data on any unit or the complete line sent on request. Send us your coaxial switching problems.

PRODUCTS, INC.

The Finest in R F System Components 12210 NEBRASKA AVENUE, LOS ANGELES 25, CALIFORNIA REPRESENTATIVES IN MAJOR AREAS CIRCLE 227 ON READER-SERVICE CARD FOR MORE INFORMATION

50



Specify.... Kesinite EP-93

For aircraft, airborne components, missiles and guidance systems – wherever specs call for MIL-I-7444A(2), or for any application where a dependable low temperature vinyl insulation sleeving is required, specify Resinite EP-93.

Not only does this outstanding material remain flexible at -90°F, it withstands 185°F continuously, an unusually wide operating range. It also offers exceptional flame, fungus and corrosion resistance. Available in all 3 size ranges.

EP-93 is just one of many fine insulation materials that have made Resinite the leading supplier of specification sleeving to the aircraft and electronics industries.

Write us your requirements and we'll submit samples and performance data on appropriate sleevings, tapes or lacing cords.



SPECIALISTS IN VINYL SLEEVING AND TUBING FOR THE AIRCRAFT, ELECTRONICS, ELECTRICAL AND PHAPMACEUTICAL FIELDS CIRCLE 217 ON READER-SERVICE CARD FOR MORE INFORMATION

New Products

Logarithmic Counter

5 Decades



This logarithmic count rate meter, based on the Cooke-Yarborough circuit, is a wide-range instrument for use with all types of radiation detectors. Typical applications include gamma monitoring with scintillation counter, beta-gamma monitoring with Geiger counter, and gamma ray spectrometry. It incorporates a Schmidt trigger circuit for discrimination. The meter eliminates the necessity of manual or electro-mechanical switching as is required in linear-type rate meters. The meter circuit consists of a series of diode pump circuits where the signal is fed into a coupling condenser which charges through one diode and discharges through another into an integrating capacitor once each cycle. Range is from 10 to 1 million counts per min. in 5 decades on a single scale. Accuracy is within ± 2 per cent over the entire decade and is better than 1 per cent in the vicinity of the calibration point. Drift is less than 1 per cent in 24 hours. The unit operates on 150 v, 60 cycles and draws 135 w. Relay rack panel is $8-3/4 \times 19$ in. and shipping weight is 60 lb.

The Victoreen Instrument Co, Dept. ED, 5806 Hough Ave., Cleveland 3, Ohio.

CIRCLE 218 ON READER-SERVICE CARD FOR MORE INFORMATION



Utility Oscillator 4.5 to 220 Mc Range

Incorporating self-contained attenuators, power supply and output meter, the Utilator provides a high level rf output agc controlled for ± 0.5 db flatness over the 4.5 to 220 mc range. A direct reading frequency dial is accurate to ± 1 per cent. Rf output is 0.7 v rms into nominal 75 ohms. Attenuation is produced by switched steps of 20, 10 and 6 db, plus continuously variable 6 db. The instrument weighs 19 lb.

Kay Electric Co., Dept. ED, 14 Maple Ave., Pine Brook, N.J.

CIRCLE 219 ON READER-SERVICE CARD FOR MORE INFORMATION



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in a Nutshell...

You may never build a circuit on or in a nutshell, but you and a lot of other manufacturers —do have miniature and subminiature designs to contend with as a part of the modern electronic trend.

Mallory sub-miniature components help make these tiny circuits possible. Mallory, for example, pioneered the Mercury Battery—known 'round the world for its ability to perform ... for its tiny size ... and for its constant-voltage discharge rate, ideal for transistor circuitry.

Mallory manufactures four distinct lines of sub-miniature capacitors—from premium grades for performance under the most exacting conditions to the newest TT series, lowcost aluminum-cased electrolytics, ideal for commercial applications. The new tiny TNT Capacitors measure .145" dia. by only $\frac{5}{16}$ " long!

When your problems are "small" —in physical size, look to Mallory for sub-miniature components. Ask the Mallory application engineers for capacitor specifications and assistance.

P. R. MALLORY & CO. INC. Indianapolis 6, Indiana



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TRANSISTOR CIRCUIT ENGINEERING

RANSISTOR CIECUIT ENGINEERING

Edited by RICHARD F. SHEA. Eight co-authors, all of the General Electric Company.

Provides you with the necessary tools to lo actual circuit designs, and develop isable circuits in *all* potential fields of ipplication. It shows you how to build necessful audio amplifiers, radio frequency amplifiers, etc. using available transistors—and how to combine these elements into radio receivers, television sets, and high fidelity audio systems.

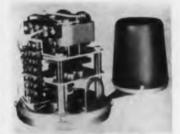
Written by a team already famous as pioneers in the field of transistor electronics, the work contains a great deal of brand new material, plus up-to-date information on recently-introduced devices and their applications in everwidening fields. Greatest emphasis is placed on the practical engineering aspects of the subject.

Chapter headings:

Characteristics and Characteristic Curves —Equivalent Circuits—Bias and Its Stabilization—Audio Amplifiers—DC Amplifiers and Their Applications— Tuned Amplifiers—Video Amplifiers— Oscillators—Modulation, Mixing and Detection—Transient Response and Pulse Circuits—Systems—Special Circuits.

Just out 468 pages 104 illus. \$12.00 Send for your ON-APPROVAL copy lodgy!

ED-77 JOHN WILEY & SONS, Inc. 440 Fourth Ave., New York 16, N. Y. Please send me a copy of TRANSISTOR CIRCUIT ENGINEERING to read and examine ON APPROVAL. Within 10 days I will return the book and owe nothing, or will remit \$12.00, plus postage. Name Address CityZone....State..... SAVE POSTAGE! Check here if you ()ENCLOSE payment, in which case we pay postage. Same return privilege, of course. CIRCLE 222 ON READER-SERVICE CARD



Control Gearmotor Built-In Potentiometer

Shaftrol, shaft mounted gear motor includes a built-in potentiometer that provides remote control for valves, variable speed drives, gates, jacks, and variable displacement pumps. The potentiometer may also serve in bridge circuits of automatic control systems. Control may be by dial control, by push button or it may be automatic from limit switches, controllers or proportioning devices. The mounts on shafts from 1/4 to 1 in. in diam. A wide range of operating speeds and torques can be had by specifying the desired ratio of the 3 or 4 stage reduction gearing. A variety of potentiometer gear ratios may also be had so that full scale deflection of the calibrated meter may be obtained for rotation of the driven shaft from 1/6 revolution to 40 or more. Limit switches, which are optional, may be set to limit travel to any desired amount. Shaftrols can be furnished with built-in single or multi-turn precision potentiometers having a wide range of specifications. When the potentiometer is used as a part of a bridge circuit, the standard Shaftrol provides follow-up accuracies of plus or minus 1/5 per cent of full scale. With precision multi-turn potentiometers accuracies of 1/25 of 1 per cent can be had with counter read out if preferred. Shaftrols are available for use on single or 3 phase circuits with drip proof, totally enclosed or explosion proof enclosures.

Jordan Co., Inc., Dept. ED, 3235 W. Hampton Ave., Milwaukee 9, Wis.

CIRCLE 223 ON READER-SERVICE CARD FOR MORE INFORMATION



Spin-Lock Nuts Will Not Loosen

Spin-lock unts combine the function of nut and lock washer in one piece. Available in sizes ranging from no. 8 to 1/2 in., the nut provides a rachet-like structure on its base which bites into the bearing surface of the metal to be joined, resisting any tendency to loosen. The teeth provide excellent contact for electric equipment. The nuts are hardened to make them capable of carrying heavy loads, and the teeth are not deformed by use.

Russell, Burdsall & Ward Bolt and Nut Co., Dept. ED, Port Chester, N.Y.

CIRCLE 224 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN • July 15, 1957

AN OPPORTUNITY AND A CHALLENGE FOR COMPONENT AND SYSTEMS DESIGNERS

SIMPLIFY AND INCREASE SYSTEM RELIABILITY BY DESIGNING TO CHARACTERISTICS OF LOW IMPEDANCE A-C DIFFERENTIAL TRANSFORMERS

infinite resolution • no sliding contact nor bearings frictionless • unlimited life, nothing to wear out temperature stable • high signal to noise ratio small, compact, lightweight

Recommended for hydraulic servo valve feedback, rate gyros, accelerometers, hydraulic servo motors, pressure, flow, position and level detectors, Atcotran Differential Transformers are setting the pace for improved reliability of components in existing systems by replacement of sliding contact pickups.

New systems designs incorporating the full advantage of inherent characteristics of these transducers promise outstanding benefits:

1) The low impedance characteristics of differential transformers can reduce or eliminate the need for filter circuits.

2) Ratio winding techniques and simple interconnection for algebraic functions frequently can be accomplished without intermediate components.

3) The reliability and precision of differential transformers makes possible a new order of performance. EXPERIMENTAL KIT

To enable designers to familiarize themselves with the application of differential transformers in the laboratory, the Atcotran Differential Transformer Experimental Kit has been made available. It contains seven standard coils of various characteristics, a flexure plate and clamp, a demodulator and a 32-page HANDBOOK containing theory and application data on differential transformers.

A \$324.00 value specially priced at only \$189.50 for lab investigation. Start exploring this new opportunity now. Order your kit today.

| THE WORLD'S LEADING DESIGNERS AND MANUFACTURERS OF LOW IMPEDANCE DIFFERENTIAL TRANSPORMERS | AUTOMATIC TEMPERATURE CONTROL CO., INC. SUBSIDIARY OF SAFETY INDUSTRIES, INC. 5239 Pulaski Avenue, Philadelphia 44, Pa. Please send me an Atcotran Differential Transformer Experimental Kit and invoice \$189.50 against our purchase order No |
|---|--|
| | NAME COMPANY ADDRESS CITY |
| FOREIGN SALES: ATC EXPORT DE | PARTMENT, 1505 RACE ST., PHILA. 2, PA. |

CIRCLE 225 ON READER-SERVICE CARD FOR MORE INFORMATION

NEWEST

MINIATURIZED CONNECTORS!

AMPHENOL'S super-reliable Micro-Ribbons are now available in cable-to-chassis mountings. Providing all of the remarkable Micro-Ribbon advantages for this needed application, these new types feature cadmiumplated brass shells with clear chromate treatment, gold-over-silver plated contacts, diallyl phthalate dielectrics.

If you are cramped for space, here is how these connectors work for you. The *largest* cable-to-chassis pair contain 50 contacts—yet, mated, measure only 3.8 square inches!

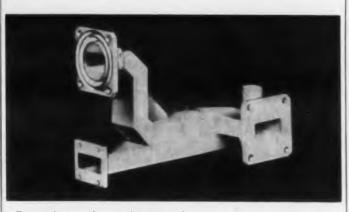
At 5 amps Micro-Ribbon connectors are rated at 700 Volts D. C. at Sea Level, 200 Volts D. C. at 70,000 feet. They are available in 14, 24, 36 and 50 contacts.

> AMPHENOL ELECTRONICS CORPORATION chicago 50, illinois "BUILDING TO THE FUTURE OF ELECTRONICS" AMPHENOL CANADA LIMITED toronto 9, ontario

Services for Designers

Flux-Dip Brazing of Aluminum Assemblies

Flux-dip brazing, a new technique for joining complex, multi-joint aluminum assemblies in one operation, is now available through Waveline, Inc., of Caldwell, New Jersey. This revolutionary process eliminates the many drawbacks of hand brazing, and assures unmatched high volume, low cost production. The major benefits of flux-dip brazing are: Mechanical accuracy, due to controlled uniform heating, warp and distortion of the assembly are eliminated; close tolerances are maintained; high strength, quality finish, and economy. Flux-dip brazing has proven ideal for brazing waveguides, antennas, chassis and microwave assemblies. It also has found application in the aviation, missile and instrument industries. Additional information may be obtained by writing to Mr. John Morris, Production Engineer in charge of development, Waveline, Inc., Caldwell, N.J.



Typical complex multi-joint aluminum assembly flux-dip brazed in one operation.

Research and Development Laboratory

A new laboratory which offers research and development services on a contract basis has been established in Madison, Wisconsin by Trionics Corporation, P.O. Box 548. The services of the laboratory are available to both industrial and government sponsors. It will employ more than 30 persons at the Madison laboratory and plans call for an increase in staff to more than 70 persons.

The research program of the new laboratory is primarily designed to develop new and improved materials to meet the requirements of specific technological advances. Special fields in which the laboratory will be active include high and low temperature resistant materials, magnetic materials, ceramics, coatings and surface treatments, plastics, electronic component materials, high strength-low weight materials, packaging materials, corrosion inhibition, metallurgy, radiochemistry, and microwave physics.



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GUDEBROD BROTHERS ARE PIONEERS IN FLAT & BRAIDED TAPES OF NYLON, DACRON, TEFLON. WAX-COATED, FUNGUS-PROOF, HEAT-RESISTANT.

Gudebrod flat braided lacing tapes hold harness securely no bite-through or slip, yet are easy on the hands. Some resist high temperature, some are color-coded... and they come wax-coated or wax-free ... rubber-coated ... or with special coating. Gudebrod makes many tapes for many purposes, including defense work. Send us your lacing problems or your specifications ... we can supply the answer to both.

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GUDEBROD BROS. SILK CO., INC. ELECTRONICS DIVISION 225 W. 34th St., New York 1, N. Y. EXECUTIVE OFFICES 12 South 12th St., Philadelphia 7, Pa.

CIRCLE 228 ON READER-SERVICE CARD

ON THE SHELF! SINGLE SPIDER **GEAR DIFFERENTIALS** by FORD INSTRUMENT **AVAILABLE IN FOUR SIZES:** 1/8", 36", 1/4", and 3/6" Shaft Diameters NOTE! Prices of 1/8" units have been drastically reduced. GUARANTEED SHIPMENT WITHIN: TYPE (WITHOUT END GEARS) for units with set shaft 1 WEEK lengths* **3 WEEKS** for units with shaft lengths to customer B specs (WITH END GEARS) WEEKS for units with stock end gears WEEKS for units with end gears D to customer specs (SUBJECT TO PRIOR SALE) *Note: 54" units are not stocked with set shaft lengths. Ford Instrument produces single spider gear differen-tials to highest military and commercial standards, for extreme accuracy in addition and subtraction, and in servo loop applications. Seven ways superior. Call or wire W. Mohr, Component Sales Division (STillwell 4-9000) for prices, or check and mail coupon below, stating quantity. Data bulletin with performance curves and characteristics will be sent with the prices. **Component Sales Division ED** FORD INSTRUMENT COMPANY DIVISION OF SPERRY RAND CORPORATION 31-10 Thomson Avenue, Long Island City 1, N. Y. Please send me prices on the following: Circle size of unit desired: 36" 1/8" 36" 1/4" Circle category for type of units needed: (Check (wo if both apply) B С Δ D ____ (number) units: I want ____ Position ... Company___ Street City_ _State_ CIRCLE 232 ON READER-SERVICE CARD

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Physics Research and Consulting Service

A privately-financed organization to offer fullscale physics research and consulting service based on use of a Van de Graaff particle accelerator has completed installation of its "atom smasher." The new company, Texas Nuclear Corp., Austin, is initially using its 2-million-volt positive-ion accelerator in programs dealing with elastic and inelastic scattering of neutrons.

The company is now staffed and equipped to provide complete coverage in such programs as analysis of compounds by nuclear methods, neutron activation cross section studies, investigation of radiation damage, study of radiation damage by electrons, electron sterilization and well-logging research. A 3600 square-foot facility has been constructed to house the Van de Graaff accelerator, and auxiliary equipment including a multichannel analyzer and related specialized counting and recording devices.

Plastic Coating Operation

The Polymer Corporation, Reading, Pa., announces the establishment of a plant at 3030 Oak Street, Santa Ana, California, to perform custom coating by the new Whirlclad coating process. The process is a new coating technique which primarily involves dipping preheated articles into a bed of finely divided dry powders which are fluidized by ascending currents of gas or air. The powders heat fuse to form the coating.

The process permits use of a wide range of plastic materials such as nylon, polyethylene, cellulosics, epoxies and polyethers to be applied to metals and other base materials. Materials such as nylon and polyethylene, can be utilized. The single dip technique applies coatings for chemical and corrosion resistance, wear resistance, electrical insulation and decorative purposes. The new Santa Ana operation is expected to provide new availability of coatings to the aircraft, electronics, and other West Coast industries.



Preheated metal parts being dipped into a tank containing fluidized coating powders.

ELECTRONIC DESIGN • July 15, 1957

What makes a relay RELIABLE?

BASIC DESIGN

UNION engineers have been designing relays noted for highest reliability for more than 75 years. This experience has been applied to miniature relay design with outstanding success.





To obtain reliable performance in every relay, UNION has developed excellent techniques for precision manufacture on a high-volume basis. Workers are provided with ingenious tools, jigs and fixtures for consistent accuracy. Special processes such as high-temperature baking and hermetic seal by welding of steel cases assure top relay performance.



Scientific quality control practices and 100% testing to critical Military Specification requirements, including a hermetic seal test by mass spectrometer, assure standard quality in every relay.

See our exhibit at the Wescon Show, Booths 810-811



CIRCLE 233 ON READER-SERVICE CARD FOR MORE INFORMATION



MECHANICAL CHARACTERISTICS

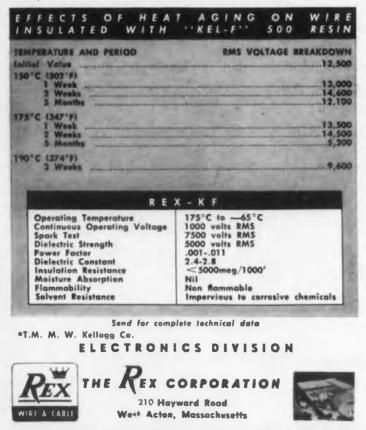
- Good abrasion resistance
- Excellent resistance to cold flow
- Extremely flexible
 Smaller O.D. than wires of comparable values

ELECTRICAL PROPERTIES

- Dielectric constant between 2.5 and 3.0
- Good arc resistance
- Zero moisture absorption
- Resists wetting and high humidity

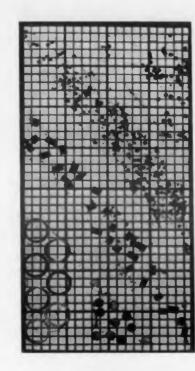
Available from stock in 17 solid colors — AWG sizes 10 through 30, also in 1, 2 or 3 stripes in any combination of 10 colors for almost unlimited color coding. Can also be supplied with braided shielding for special requirements.

Complete facilities for twisting single, insulated conductors in pairs, triplex or quads, cabling 808 conductors into a single core, and, for layer or sector type cabling are available. Application of braided shielding or spiral tape shielding over the core before jacketing a specialty. Jacketing done in polyethylene, vinyl, nylon, or Kel-F.



CIRCLE 237 ON READER-SERVICE CARD FOR MORE INFORMATION

New Materials_



Microforms for Semiconductors

Herbert Drapkin Anchor Metal Co., Inc.

Liquidus

a + B

-wt. %->

Gallium

a + Lia

Indium

THE CHOICE in semiconductor devices at present are germanium for its high frequency properties, and silicon for its greater efficiency at higher temperatures. Experimentally other compounds show the high frequency properties of germanium at the temperatures where silicon devices work best, but for the purpose of description these two basic elements are used as examples.

Microforms of pure germanium and silicon are cut from single long crystals grown from zone-purified metals. The crystals are first started as seeds and pulled from their melts at about 1 mm per min. Purified germanium, or silicon, must be innoculated during crystal growth with precise amounts of doping elements, which either donate electrons to crosssections of the growing crystal or take electrons out. Donor dopes include antimony, arsenic, bismuth phosphorus. Acceptors include boron, gallium, indium.

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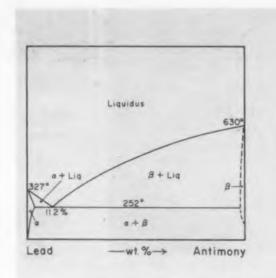
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Junctions of types p or n are created in the crystal by letting pellets or spheres of the appropriate innoculant slide down a tube into the melt intermittently. Microforms cut from such doped germanium or silicon crystals grown by this method have either n or p, or both, junctions grown into them.

Other devices use microformed wafers of pure germanium or silicon to which the impurity is fused. For example, a pellet of indium is placed on a wafer of n-type germanium. The unit is slowly heated. At 156 C, the indium melts into a tiny blob. As the temperature continues to rise the spot of germanium on which the indium rests begins to melt and dissolve



Typical equilibrium diagrams show the proportional weight of each element of a binary alloy as it passes from the liquid to the solid phase.

ip into the molten indium, making an indium-germanium alloy. At 500 C, heating is stopped and the unit allowed to cool slowly. The germanium settles out of the alloy and grows back into its original n-type crystal base. But the regrown spot of germanium is now p-type because it is contaminated with some atoms of indium, and the whole germanium wafer includes a p-n junction. The re-solidified indium blob on top makes an excellent connection to the junction.

Microforms used to alloy, solder, seal and otherwise serve in semiconductor devices must be extremely precise in the quantities of elements of which they are made. Most must be so small that they can be manipulated only under magnifying glasses. A few of the shapes in demand are discs, pellets, spheres, washers. These measure from 0.001 in to 0.04 in. in thickness, from 0.1 in. up in diameter. In, say, antimony-doped germanium an impurity diffusion layer can be created 1.5x10⁻⁴ cm thick.

muth In addition to the simple elements many alloys m, inheretofore scarcely known and still incompletely understood are being used in research, engineering erystal and development. Such alloys, to list only a few te inbinary ones, include indium with gallium, tin, lead, ermit. germanium, gold, silver, zinc and cadmium; lead anium with arsenic and antimony; aluminum with gallium, either and indium; tin with gallium, lead, bismuth, antimony, gold, silver and arsenic; silver with arsenic pure and copper; gold with arsenic, antimony and galfused. lium

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To produce the alloy prescribed for a particular ed. At use the metallurgist must know the proportions of the elements at the temperatures where their mixtures solidify out of the melts. This data has been recorded as precisely as possible for many binary, ternary and quatenary alloys, and charted as equilibrium diagrams.

> Equilibrium diagrams for the systems lead-antimony and indium-gallium are shown. At 327 C lead starts to settle out of the Pb-Sb liquidus (melt). This is the alpha phase of the solidifying alloy. Antimony, as shown at the other side of the diagram, has already been settling out of the liquidus as it cooled below 630 C. This is the beta phase. At 252 C the alloy is all solid. It is a homogeneous mixture containing 11.2 per cent lead with 88.8 per cent antimony. Similarly, the In-Ga system solidifies at 15.7 C with 75.6 per cent gallium. Such equilibrium diagrams are considered guides to the engineer in calculating the quantities of the elements in the microform that he requires in the design of his semiconductor devices.

GUDEMAN Capacitors

Bathtub Type Military Capacitors MIL-C-25 Types CP53, CP54, CP55 Case Styles Temperature Ranges: -55°C to +85°C -55°C to +125°C

Military Capacitors MIL-C-25 Types **CP70** Case Styles Temperature Ranges: -55°C to +85°C -55°C to +125°C



Tubular Laminated Cardboard Capacitors The 633 series gives extra protection in extremely high humidity applications. Paper Dielectric: Wax or Oil Impregnated **Resin End Seals** Temperature Range: -40°C to +85°C



"XC" Plastic Film Dielectric Capacitors The development of the Gudeman "XC" capacitors provides high temperature capacitors that have exceptionally high insulation resistance, low power factor and low dielectric absorption. No voltage derating is required when used within a temperature range from -65°C to +165°C. Bathtub and rectangular case styles also are available.



Miniature Feed-Through Capacitors The Gudeman Feed-Thru Capacitor, Types 271 and 272 is a three-terminal component designed to be used for R. F. Interference suppression in a manner similar to a low pass filter. The typical insertion loss characteristics for these Feed-Thru Capacitors when measured in a 50 ohm line are in accordance with MIL-Standard 220.

TRILL

Dry Electrolytic Capacitors MEand Printed Circuit Types High Purity (99.99%) Aluminum Foil Low Leakage Temperature Range: -30°C to +85°C

GUDEMAN COMPANY THE

Write for latest technical data Main Plant & General Offices

340 West Huron St., Chicago 10, Illinois, Mfg. Branches: Chelsea, Mich.; Sunnyvale and Monrovia, Calif.; Terryville, Conn. Manufacturers of Electronic Components for Military and Commercial Applications. CIRCLE 239 ON READER-SERVICE CARD FOR MORE INFORMATION





112

CIRCLE 242 ON READER-SERVICE CARD FOR MORE INFORMATION

preformed to your specifications . . .

Indium or indium alloys in ingots, sheets, wire,

powder, ribbon, and pellets (disc or spherical) are

supplied by us to leading U.S. manufacturers of elec-

tronic equipment. These and other forms prepared to

your own requirements are available in two grades: Tadanac High Purity - approximately 99.999% In Tadanac Standard Grade - guaranteed 99.97% In As one of the world's leading primary producers of indium, we apply the services of our Research and Development Division to assist our customers in obtaining the full benefits of this most versatile metal.

Other high purity TADANAC BRAND METALS

Silver - 99.9999 %

For further information or quotations contact:

THE CONSOLIDATED MINING & SMELTING COMPANY OF CANADA LIMITED.

Metal Sales Division 215 ST. JAMES STREET WEST, MONTREAL, CANADA

Our prices include custom's duties, and we handle

Lead - 99.9998%

5762-ME

Cadmium - 99,9999%

Zinc - 99.9995%

Bismuth - 99.9998%

all customs procedures.

New Materials

Ferroelectric Material

Permits Low Voltage Switching

Exploration in the field of ferroelectrics has resulted in the discovery of a new ferroelectric material at Bell Telephone Laboratories. Known a triglycine sulphate, the material has a rectangular voltage hysteresis loop and other desirable properties which make it promising for switching circuits and memory devices.

The most popular ferroelectric crystal previously investigated was barium titanate. Triglycine sulphate is superior in that it has a much lower coercive field, 220 v per cm, thus permitting switching with a lower voltage. Its polarization results in a lower output pulse when switched, but the size of the pulse can be increased by increasing the area of the switching electrodes.

Triglycine sulphate is stable chemically and does not decompose when exposed to moisture or to the atmosphere. It has adequate mechanical strength to permit handling in thin sheets. Large single crystak can be grown quite easily, and a number of large area slices can be cut from each crystal.

Repeated switching does not cause any fatigue, and a given area will retain a given polarization indefinitely without deterioration. Although heating beyond the Curie point causes the material to lose its ferroelectric properties, these properties are regained in full when it is cooled.

The Curie point of the material is about 47 C. However, by replacing some of the hydrogen atoms with deuterium, easily accomplished when the crystal is grown, the Curie point can be raised to 60 C. Switching time is of the order of 1 to 2 μ sec. Electrodes can be applied to a slice cut from a single crystal by evaporating thin strips of metal on each side of the slice, the strips on one side



Triglycine sulphate, a new ferroelectric, provides a low switching voltage level as well as other qualities favorable for use in switching circuits.

ELECTRONIC DESIGN • July 15, 1957

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bein perpendicular to those on the other. Using this chnique, thirty or more strips per inch can be applied, resulting in a memory or switching device capable of storing 900 or more bits of inform tion on a square inch of crystal.

Custom-Shaped Sapphire

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Melting Point of 2040 C

roper. Advances in synthetic sapphire growing techniques have produced large single crystals comrcuits netitive in price with sintered aluminas and quartz. ioush A wide variety in sizes and shapes of rods, disks, e sul tubes, domes and balls of sapphire are now availcoer. able.

tching Properties include extreme hardness (next to diamond); resistance to acids and alkalies even at elevated temperatures; excellent electrical insulasize of e area tion; strength at high heats; melting point of

2040 C; excellent transmission characteristics of does ultra-violet and infra-red wave lengths. These to the properties, together with the variety of shapes gth to and sizes, allow such uses as windows and domes ystak for infra-red systems and spacers and supports for large. electron gun structures.

Linde Air Prod. Co., Dept. ED, Div. Union Cartigue. bide, 30 E. 42nd St., New York 17, N.Y.

CIRCLE 244 ON READER-SERVICE CARD FOR MORE INFORMATION

Zirconium

Uses and Properties

Some sources of information pertaining to the applications and the electrical, chemical and nuclear properties of zirconium and its alloys have been collected for those who may be considering the use of zirconium. Comprehensive sources of information are the following books and pamphlets: American Society for Metals, Zirconium and Zirconium Alloys, Cleveland, Ohio, 1953.

U. S. Atomic Energy Commission, Zirconium, A Bibliography of Unclassified Report Literature (TID. 3304), Oak Ridge, Tenn., 1956.

H. K. Adenstedt, Physical, Thermal, and Electrical Properties of Hafnium and High Purity Zirconium, Trans. A.S.M., 44, 949, 1952.

George A. Espersen, Zirconium for Electron Tubes, Foote Prints 18 (1), 3-7, 1946.

L. B. Golden, The Corrosion Resistance of Zirconium and Zirconium Alloys, A.S.M. Symposium on Zirconium and Zirconium Alloys, 305-326, 1953.

W. J. Kroll and H. L. Gilbert, Melting and Casting Zirconium Metal, Journal of Electrochemical Society, 96, 156, 1949.

C. F. Squire, and A. R. Kaufman, The Magnetic Susceptibility of Titanium and Zirconium, J. Chem. Phys., 9, 673, 1941.

Courtesy of Columbia-National Corp., 70 Memorial Drive, Cambridge 42, Mass., from whose bibliography on zirconium the above list was selected. NEW

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The same company, the same engineering and manufacturing facilities, the same world-wide staff of field engineers, but a new name more descriptive of the Company and its products.

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Representatives in all major cities

ABSOLUTE DC POWER BROADCAST TELEVISION SUPPLIES AND EQUIPMENT METER CALIBRATORS

On these and many other electronic products the name KIN TEL means outstanding instruments and television equipment.

105

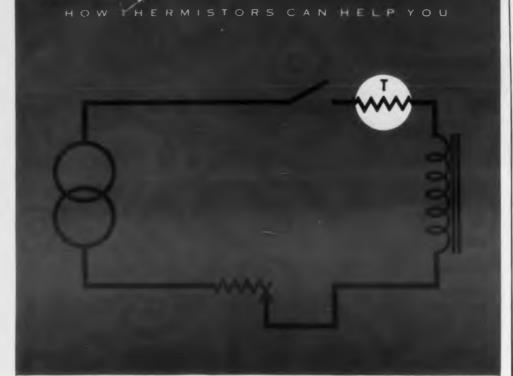


Write, wire, phone today for demonstration

CONTROL ELECTRONICS FOR COMMUNICATION

5725 KEARNY VILLA ROAD · SAN DIEGO 11, CALIFORNIA · BROWNING 7-6700 CIRCLE 245 ON READER-SERVICE CARD FOR MORE INFORMATION





Effecting Time Delay with GLENNITE® Thermistors

An extremely effective time delay can be accomplished using Glennite Thermistors. This method shows distinct advantages over conventional time delay methods because of Glennite Thermistors' small size, long life, ruggedness and the elimination of moving parts.

The Glennite Rod Thermistor in the above schematic regulates current flow resulting in variable or fixed delay due to resistance change in the thermistor. Variable time delay can be obtained from a fraction of a second to several minutes.

Glennite Thermistors are available in bead, probe and wafer units, too — with some units offering temperature coefficients up to 7% per °C.

> Complete technical specifications and typical applications are in the Brochure T-100 . . . write for your copy.

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CLEMENT.

FROM RAW MATERIALS TO COMPLETE SYSTEMS ...

Gulton Industries, Inc.

CIRCLE 248 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Electromagnetic Controls

249

Various types of electromagnetic controls are discussed in a series of seven catalogs recently released.

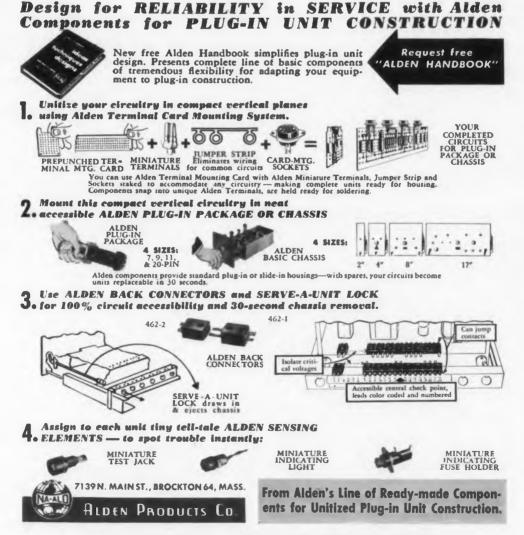
The booklets cover the following items: complete information on automatic transfer switches (mechanically or magnetically held) (Catalog 57-S1); remote control switches which are used to control power and lighting circuits (Catalog 57-S2); magnetically held contactors available for all normally open and closed classes of load (Catalog 57-S3); relays (Catalog 57-S4); AC and DC Solenoids (Catalog 57-S5); electric plant controls. Material includes complete systems, paralleling, changeover and alternating panels, load demand controls, battery chargers and adapter units (Catalog 57-S6); and Catalog 57-S is the complete electromagnetic control catalog. which combines the information on Cata. logs 57-S1 through 57-S6. Automatic Switch Co., Florham Park, N.I.

Electrolytic Capacitors

Catalog 1165 presents 12 pages of data on electrolytic capacitors. It also describes a long life capacitor which eliminates the excessive leakage current and rapid shelf aging problems of conventional electrolytic units. Industrial Condenser Corp., 3243-65 N. California Ave., Chicago 18, Ill.

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CIRCLE 251 ON READER-SERVICE CARD FOR MORE INFORMATION

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Screw-Lock Inserts

S₁ cifications on a complete line of screw-lock inserts, including miniature size 4.40 inserts are listed in Bulletin 738. The eigh page booklet contains screw-lock selection tables with thread sizes, insert num ers and sizes, and complete information on drilling, tapping, gaging and installation. Line drawings and photographs illustrate proper installation of the inserts in both blind and through holes. Also presented are basic engineering design data, military specifications, classes of fit, and assembly proportions. A variety of costcutting applications are cited. Heli-Coil Corp., Danbury, Conn.

Servomotor-Rate Generator 259

Data Sheet 866 covers details of the model 18 MG 690/660, a 60-cy, 115-v size 18 servomotor-rate generator. The sheet contains specifications, characteristics and other design information. It is illustrated with dimensional drawings, a schematic and a torque-speed curve. Beckman/Helipot Corp., Newport Beach, Calif.

Precision Ball

258

Catalog that serves as guide to quick and simple selection of precision balls for practically any requirement and material specification has been released. Included is comprehensive data on such items as balls of aluminum, brass and bronze, carbon steel etc., as well as information on balls of special materials.

It also includes material characteristics, type analysis, mechanical properties, temperature characteristics, corrosion resistance factors, machinability, finish, hardness, accuracy, size, weight, and quantities per pound and per shipping container.

A special feature is the Quick Ball Selector Chart that provides a comparative reference for all ball types. Hartford Steel Ball Co., 12 Jefferson Ave., W. Hartford, Conn.

Slip Ring Assemblies

Custom built slip ring assemblies are the topic of Bulletin S-2056. The four-page illustrated text describes complete ring assemblies, brush holder assemblies and brush contacts. Superior Carbon Products, Inc., 9115 George Ave., Cleveland 5, Ohio.



250

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261



Among the many requirements for heat elements in industry today are those demanding virtually one-of-a-kind design.

Since such requirements normally cannot be met by loom weaving, Safeway technicians fabricate odd-shaped elements individually. Circles, half circles, cutouts, tapers and compound shapes are just a few of the elements fabricated in this fashion and produced in quantity.

Insulation, too, must provide for the characteristics of specialized applications. Safeway produces a wide variety of elements insulated with neoprene rubber, silicone rubber or reinforced plastics.

If you have a problem that requires heat, let Safeway engineers study your requirements and—without obligation to you—submit an appropriate recommendation.

For your copy of a fact-filled folder, write to:

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HEAT EMENTS

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| S.T.A | | acitors |
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| STA | Stabl | e** |
| Series 200 | Large | e Capacity*** |
| *How Small? | | Series 100 |
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| **How Stable? | | |
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| | Series 300 | 5 mfd at 35 volts 20 mfd at 35 volts |
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| SEE US AT WESCON | | 21.1222 |

New Literature

Rectifiers and Capacitors

ReCap, a new bimonthly journal of information on rectifiers and capacitors is now available, free, to interested engineers. The first issue, a four pager, featured an article on types and characteristics of silicon rectifiers and contained other interesting material on capacitors and rectifiers. Rectifier-Capacitor Div., Fansteel Metallurgical Corp., North Chicago, Ill.

Aluminum Bus Conductor Handbook 270

"Alcoa Aluminum Bus Conductor Handbook," a comprehensive work of 280 pages, presents facts and figures relative to the engineering and maintenance of bus installations. It contains 69 graphs, tables and photographs and presents essential information. These is comparatively little text. Introductory material traces the development of aluminum's use and its properties as a conductor. Subsequent chapters deal with conductor shapes, design, reactance, capacities, deflections, joints and shortcircuit conditions, and the final sections explain important fundamentals of installation. A comprehensive bibliography refers the user to technical articles on related subjects. Copies of the handbook may be obtained by writing on company letterhead to Aluminum Co. of America, 793 Alcoa Bldg., Pittsburgh 19, Pa.

Data Sheets for Motors & Timers

To assist customers in ordering special timers or motors, two bulletins have been released.

Bulletin MS101-Applications data sheet for motors and elapsed time indicators and Bulletin MS102—Applications data sheet for repeat cycle timers and time delay relays. These bulletins are designed to aid customers in organizing their thinking when ordering or requesting information on any special units. All pertinent information is itemized with ample space to insert required values of current, voltage or life. In many cases these bulletins can be used to replace lengthy problem statements.

These bulletins will help considerably in saving time and money for the customers, since much correspondence can be eliminated by averting the omission of important details in the initial description of a timer.

The bulletin sheets are clearly blocked out with readable size type and check-off blocks and charts for laying out timing programs. A. W. Haydon Co., Waterbury, Conn. you can depend upon **Outomotic** coaxial SWITCHES and RELAYS

Custom engineered to your specifications

Unsurpassed accuracy and dependability, based on over 15 years experience in producing precision parts for the Army, Navy, Air Force, and Atomic Energy Commission.

AUTOMATIC'S Coaxial Switches and Relays are available in the following types:

SPDT, DPDT, Crossover, Resistor Terminated, Multiple Position, and Rotary—both continuous and index type.

All switches available for both manual and relay operation, and may be ordered with all standard and sub-miniature fittings.

AUTOMATIC'S Switches and Relays are small in size...light in weight... low in cost...and have excellent electrical characteristics.

Our engineers are always ready to discuss your special requirements.

WRITE, WIRE, OR PHONE FOR FREE TECHNICAL INFORMATION



319 Barry Street, Bracklyn 11, N. Y. • EVergreen 8-0364 CIRCLE 272 ON READER-SERVICE CARD

269

271



Industrial Materials

This new industrial materials selection chart lists application and descriptive data on adhesives, coatings and sealers. The chart, divided into six sections, includes reclaim rubber, synthetic rubber, latices, plastics, epoxy resins, and caulkings. Miracle Adhesives Corporation, P.O. Box 466, New Philadelphia, Ohio.

High Density Felts

280

High density felts called Feutron "63," are discussed in Technical Data Sheet No. 19-a 2-page comprehensive presentation now available.

The data sheet describes the general characteristic of the new high density felts and diagrams their physical properties. Feutron "63" line felts provide an opportunity for technological advances in a wide range of applications, particularly where severe mechanical operating conditions are encountered.

Among the general characteristics of the new high density felts are high tensile strength, exceptional abrasion resistance and isotropic structure.

The bulletin declares that "special chemical and heat resistant properties are identified with the particular synthetic fiber of which the felt is composed.

A table in the data sheet refers specifically to the physical properties and performance characteristics of four representative samples included in the bulletin, which are illustrative of this class of mechanically interlocked and chemically shrunk materials. American Felt Co., Eng. & Research Labs., Glenville, Conn.

SRI Journal

The Stanford Research Institute has announced the first issue of its quarterly SRI Journal. The new publication will present scientific and economic subjects in comparatively nontechnical language. It is designed primarily for research directors and key executives in business, industry and government. Editor of the new magazine is Charles Scarlott, manager of the Institute's Publication Department. The Journal will feature articles by staff members and guest contributors. It will contain selected papers presented at SRI-sponsored meetings. Interpretive summaries of research projects will also be offered. The first issue contains illustrated articles on guided missile research; techniques for machine reading of Arabic characters printed in magnetic ink; the problem of X-ray crystal analyses and a new computer to shorten computation time; and other subjects. The Journal may be obtained for \$1.00 a copy or \$4.00 a year from the Editor, SRI Journal, Stanford Research Institute, Menlo Park, Calif.

279

A B S E E L LICON TIFIERS Small* Wide Range** High Performance

Available in peak Inverse vollage astings from 50 through 350 yolts

Relat at 550 millionpo without boot sive



How Small?

How Wide?

How High?

NSTEEL METALLURGICAL CORPORATION North Chicago, Illinois, U.S.A.

Tall Us Aband Tour Requirements

CIRCLE 281 ON READER-SERVICE CARD FOR MORE INFORMATION





NEW AM-100





Now Bulova pioneers an entirely new, ultra-simplified means of temperature compensation...the "multi-purpose" AM-100 oven.

The AM-100 is designed to yield exacting temperature control of more than just crystals. Now entire circuits, components and/or complete sub-assemblies can be housed in one, low cost unit...the highly stable AM-100.

By eliminating costlier, less dependable, heavier and more complex temperature compensating factors, hundreds of design hours can be saved...circuits can be simplified and more dependable, and have a far wider operating range.

THE AM-100 FEATURES: Rugged lightweight construction (less than $7\frac{1}{2}$ oz.); Long life expectancy due to triple insulation on heater winding; High stability \pm .1°C.; Standard octal plug-in (stud mounting available); The unit draws 20 watts on initial warm-up, with average dissipation of less than 5 watts after warm-up; Meets vibration tests per MIL-E-5272; Overall 3" diameter x 5" high - cylindrical cavity 1%

A complete line of precision Bulova ovens are available in quantity, with custom designed units available on request.



watch company

Electronics Division Woodside 77, N.Y. Write Dept. A-765 Full Information and Prices on Ovens

CIRCLE 288 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Zinc Brightener

289

The advantages of a zinc brightener used in plating parts by the barrel method are discussed in data sheet released recently.

The new brightener makes zinc barrel plating more dependable and reduces cost by eliminating subsequent bright dipping. Smoothex, Inc., 10705 Briggs Rd., Cleveland 11, Ohio.

Angle Meters

290

Various 250 deg. arc angle meters are discussed in a 6-page folder, Form 250 now available. The illustrated folder describes meters which feature scale lengths up to 2-1/2 times as long as conventional meters and are accurate up to one per cent of full scale deflection. The meters are available from 2-1/2 in. up in ruggedized, shockproof and sealed cases. Long scale aircraft and special purpose meters are also illustrated. Hickok Electrical Instrument Co., 10525 Dupont Ave., Cleveland 8, Ohio.

Battery Connectors

decad GB6 is a catalog with 32 pages of infor. 10 mg mation on battery connectors, power conspeed nectors, and heavy-duty connectors for in. dustrial and allied applications. Several series for aircraft, sound equipment, tele. vision and other uses are described Individual units are listed with short specifica. tions, dimensional drawings and photo. graphs. The booklet also contains explicit ordering information. Cannon Electric Co., 3208 Humboldt St., Los Angeles 31, Calif.

Special Transformers

In a 4-page brochure, a line of military and special commercial transformers is described. High power pulse, hermetically sealed military and open type military, subminiature binary and toroids are some of the types discussed and illustrated. Manufacturing facilities are also outlined. Laboratory for Electronics, Inc., 75 Pitts St., Boston 14. Mass.



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CIRCLE 293 ON READER-SERVICE CARD FOR MORE INFORMATION

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ELECTRONIC DESIGN • July 15, 1957

Electionic Counters

298

A four-page illustrated brochure shows a line of electronic counters. Described are a decade scaler with a counting speed of 10 mc and a binary scaler with a counting speed of 20 mc. Other decade scalers covered have counting speeds of 20 kc, 40 kc. 100 kc and 1 mc. Three preset scalers of 20 kc, 40 kc and 100 kc counting speeds are also presented. Laboratory for Electronics. Inc., 75 Pitts St., Boston 14, Mass.

Miniature Lighting Assemblies 299

Miniature lighting assemblies, lampholders and components are covered in 16page catalog just released. The catalog gives full application and dimensional data on the numerous units and parts, with detailed illustrations and full information on special variations and modifications of standard assemblies.

In addition, a general discussion of the purposes and construction of the component parts of assemblies is included, in order to facilitate the selection of the right unit for a given application. Drake Mfg. Co., 1713 W. Hubbard St., Chicago 22, Ill.

Regulated Power Supplies

Magnetically regulated power supplies are the topic of a recent catalog. The fourpage folder describes and illustrates filament power supplies, telemetering and strain gage power supplies, computer power supplies, and miniature magnetic amplifier power supplies. Also discussed is a transistorized line which includes dc voltage regulators and inverters. Gulton Industries, Engineered Magnetics Div., 212 Durham Ave., Metuchen, N.J.

300

Tiny Tantalytic Capacitors 301

GEA-6065C is a 4-page booklet on microminiature tantalytic capacitors for lowvoltage, dc applications where high capacitance is needed. It contains a discussion of the units' features, construction, uses and specifications. A table shows ratings and dimensions. Photographs and dimensional diagrams provide illustration. The brochure also contains photographs and short descriptions of other capacitor types together with the numbers of bulletins where they are more fully treated. General Electric Co., Schenectady, N.Y.



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957 ELECTRONIC DESIGN • July 15, 1957

NEW MODULAR DESIGN PRECISION POTENTIOMETER



FEATURES OF CUSTOMIZED STANDARD POTS

- ► High Temperature Operation . . . to 145 deg C
- ▶ Independent Linearity of ±0.25%
- ► Non-linear Functions

The newly developed TIC Type PVR-09 incorporates modular design for choice of cup depth, mounting, and number of taps. Modular design, a new concept in manufacturing, makes available all mounting types — servo, tapped hole, and threaded bushing ... and, in addition provides extreme flexibility in customizing the standard PVR-09 design to the individual application.

Ganging up to 15 cups, without external clamps, and each individually phased at the factory also provided by the modular design technique. Up to 9 taps are available in a standard unit — others on special order. Ball bearing construction provides low torque.

With our new plant facilities and unique modular design techniques you now can get <u>customized</u> design without delay. Complete spec's on request.

PERTINENT CHARACTERISTICS:

- STANDARD RESISTANCES: 100 ohms to 150K
- ACCURACY OF TOTAL RESISTANCE: ±5% on standard, to ±1%
- on special linear functions • INDEPENDENT LINEARITY: $\pm 0.5\%$ of total R above 5K standard, $\pm 0.25\%$ on special
- POWER RATING: 1.25 watts at 85°C
- RESISTANCE FUNCTIONS: Can be provided with a variety of non-linear functions
- TAPS:
- Up to 9 taps . . . with 10 deg • TEMPERATURE RANGE :
- -55 to +145 deg C • MILITARY SPECIFICATIONS :

P.O. BOX 3941, NORTH HOLLYWOOD, CALIF.

Tested to MIL-E-5272A

555 MAIN STREET, ACTON, MASS.

<u>Y INSTRUMENT CU</u>

CIRCLE 303 ON READER-SERVICE CARD FOR MORE INFORMATION



New Literature

Network Components

309

Manufacturers of communications networks components recently established a regular monthly periodical entitled the Burnell Bulletin. The bulletin will contain, in addition to information about its progress, background material on the development and application of their products. Burnell & Co., Yonkers, N.Y.

Part Winding Starters

310

Bulletin GEA-6606 is a 4-page discussion of part winding starters. It points out the advantages of two-thirds part-winding starting and gives application data and part-winding characteristics of a typical motor. It also gives nomenclature and price information on the CR7050 starter designed for either one-half or two-thirds part-winding starting of standard motors or special part-winding motors for reduced kva inrush. The booklet is illustrated with connection diagrams and photographs. General Electric Co., Schenectady 5, N.Y.

Metal Instrument Cases

Deep-drawn and fabricated metal instrument cases, boxes and military cases are a ph listed in a 62-page catalog. Photographs Brev specifications and descriptions are provided New for a line encompassing more than 1400 stock sizes and shapes. The catalog has a section detailing plant facilities, among them product design, tooling, hydraulic presses, heliarc and spot welding, metal finishing, stamping and assembly. Zero Mfg. Co., 1121 Chestnut St., Burbank, Calif.

Control Cables

Publication of a brochure on supervisory and station control cables is announced The illustrated literature introduces applications and gives complete technical information and engineering specifications. It comes in a loose-leaf cover binder to which supplemental data can be added. For copies write on company letterhead to Ansonia Wire & Cable Co., 111 Martin St., Ashton. R.I.

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CIRCLE 312 ON READER-SERVICE CARD FOR MORE INFORMATION

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Slow Worm Motor

A me-page sheet is devoted to a slowmotion worm motor. Standard specifications on speed, rotation, shaft length, and type if application (continuous or intermittent) a philograph and a dimensional drawing. Brevel Products Corp., 601 W. 26th St., New York I, N.Y.

VHF Transmitter

319

320

318

The Type T-20 building block 20-channel vhf transmitter is described in Brochure ARCBR-T20-1. The unit is designed to operate with either the ARC Type R-15 (108 to 135 mc) or ARC Type R-19 (118 to 145 mc) receiver to provide a 2-way vhf radio set. Aircraft Radio Corp., Boonton, N.J.

Industrial Heating

Bulletin 1331, a reprint of article entitled "How To Braze Stainless" by H. M. Webber, is now available. It discusses filler metals, wetting, fixtures, distortion, protective atmospheres, and other aspects of furnace brazing on stainless steels. General Electric Co., Schenectady 5, N.Y.

TYPE 751

Pulse Burst Generators

The operation, specifications and uses of the Models 2130A and 2150A pulse burst generators are comprehensively treated in a bulletin of two pages. The text is illustrated with a diagram and a photograph. Electro-Pulse, Inc., 11861 Teale St., Culver City, Calif.

Epiradiator

An epiradiator for remote evaporating and drying for infrared radiation is described in folder just released.

The folder gives complete description of the model as well as specifications and characteristics of the item. Quartz Products Corp., P.O. Box 628, Plainfield, N.J.

Ballast Heating

Basic heat problems and what causes overheating in fluorescent lamp ballasts are discussed in Bulletin 3328 entitled "Let's Talk About Ballast Heating" now available.

The 8-page two-color booklet tells what happens to an overheated ballast and gives steps to avoid ballast overheating and associated problems. General Electric Co., Schenectady 5, N.Y.

Fairchild miniature precision potentiometers meet applicable portions of MIL-E-5272A. These units, in %" and 1%" diameters, are available in standard or high temperature versions rated to 150° C. They are miniaturized without sacrificing performance meeting the same requirements for accuracy and reliability as most standard precision units up to 2" in diameter.

MINIATURE PRECISION POTENTIOMETERS linear and nonlinear

Precision in linear and nonlinear functions is assured with each of these Fairchild miniature potentiometers. 0.5% standard accuracy, 0.25% special accuracy available. Type 751 (%" dia.—weight .57 oz.) has a resistance range up to 75K ohms in mandrel, and 100K ohms in card-type windings. Type 741 (11%" dia.—weight .77 oz.) has a resistance range up to 100K ohms in mandrel and 150 ohms in card-type windings. New external flush clamp bands, increasing the coupling strength of ganged units by 200% over previous designs, permit ganging up to six standard units without increasing the overall diameter.

Write for complete specifications. Dept. 140-83N, Fairchild Controls Corporation, Components Division:

EAST COAST 225 Park Avenue Hicksville, L.I., N.Y. WEST COAST 6111 E. Washington Blvd. Los Angeles, Calif. TYPE 741

PRECISION POTENTIOMETERS

CIRCLE 324 ON READER-SERVICE CARD FOR MORE INFORMATION

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WIRE WITH 400 LIVES

New "High Strength" wire with 400% longer "flex-life"

25% greater "tensile strength"

THE PROBLEM: Stranded hook-up wire users are experiencing excessive, costly and often dangerous conductor breakage, especially in the smaller, more susceptible conductor sizes (32 AWG to 24 AWG).

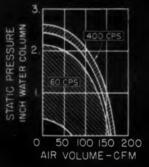
THE SOLUTION: A brand new mechanically improved, non-magnetic conductor, called "High-Strength" wire, has been developed by Hitemp Wires, Inc. Exhaustive tests of the new wire, which meets the requirements of MIL-W-16878, show tremendous improvement over conventional stranded wire...a truly amazing average of 400% longer "flex-life" and 25% greater "tensile strength." Another giant step by Hitemp to meet the growing needs of America's industrial and defense requirements.

Write today for full information!

HITEMP WIRES, INC. 26 Windsor Avenue, Mineola, New York CIRCLE 325 ON READER-SERVICE CARD FOR MORE INFORMATION

Cool Magnetrons and Power Tubes with Model D Blowers

INVERTED TYPE 505



41/4"

Shown is one of a family of high-pressure blowers designed for turbulent cooling in Commercial and Military Electronic applications where space is at a premium and long trouble-free life is mandatory.

Ator

10"

OPTIONAL AIR INLET & OUTLET ADAPTORS & MOUNTING SURFACES

SEE Catalog Sheets: 40102-31 40102-32 30102-3



CIRCLE 328 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Erasing Machine

329

Superior electric erasing machine developed for the engineer and draftsman for faster erasing with minimum fatigue is described in data sheet now available.

This new meahine "Sovereign," operates cool under heavy work conditions, has minimum torque and automatic stall control to protect drawings against damage from too heavy pressure. The machine is lightweight and easy to handle according to the data sheet. Frederick Post Co., 3650 N. Avondale Ave., Chicago 18, Ill.

Components and Test Equipment 330

In Short Form Catalog 57-BG, all company products are listed: pulsed and CW magnetrons, TR and ATR duplexing tubes, microwave silicon diodes, silicon power rectifiers, flange-mounted and solderable waveguide pressure windows, waveguide components, and test equipment. Operating characteristics are tabulated for a majority of the products. Microwave Associates, Burlington, Mass.

Reversible Geared Motors

Four pages of details on type TYAZ-CE reversible geared motors are available in Catalog GR2. Attention is given to construction, mounting, base motors and duty cycles. Standard gear reductions and control circuits are also considered. Tables show the performance characteristics of individual units. Photographs illustrate the motors and drawings show dimensions and circuits. Barber-Colman Co., Small Motors Div., 1400 Rock St., Rockford, Ill.

Miniature DC Solenoids

Reference material on representative miniature and subminiature dc solenoids is available. It is designed to aid in solenoid selection by type, size, voltage range, temperature range, force, weight and similar characteristics. The illustrated reference sheets give detailed data on nine units for data processing and memory units, computers, avionics and other applications. PSP Engineering Co., 6058 Walker Ave., Maywood, Calif.

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Precision Potentiometers

Recent modifications in specifications for the series AN and CN multi-turn potentiometers are noted in Data Sheet 54-12. Issued to supersede Data Sheet 54-11, the 2-page leaflet presents detailed technical information and illustrations to show dimensions and construction. Helipot Corp., Newport Beach, Calif.

usec Coaxial Cables

339

1957 catalog describing line of microminiature coaxial cables and connectors is available. The 32-page catalog gives specifications and applications of the items included in the catalog. Microdot, Inc., 220 Pasadena Ave., So. Pasadena, Calif.

Coaxial Terminations

340

The Model 369 Series of high power coaxial terminations are the subject of a onepage data sheet. The leaflet presents photographs, power ratings, specifications, special features and prices. The Narda Corp., 160 Herricks Rd., Mineola, N.Y.

Shaft Angle Converters

Shaft angle converters for binary decimal coding are the topic of a four-page folder. The instruments' features are discussed with special attention to code drums, brush blocks, and drive systems. Also provided are application suggestions, detailed performance data, and a table showing specific characteristics of available models. The folder is illustrated with photographs and dimensional drawings. Instrument Development Labs., Inc., 67 Mechanic St., Attleboro, Mass.

341

Lubricant Testing Machines 342

Operating information on Model LFW-1 Lubricant-Friction-Wear testing machine are included in revised bulletin 106 now available.

Included in the bulletin is a more complete description of the machine's operation as well as a revised list of specifications in the English and Metric systems.

The details of the specimen holder and lubricant reservoir are shown in photograph. Alpha Molykote Corp., 65 Harvard Ave., Stamford, Conn.



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CAMLOC low cost/light weight

Camloc's new small, lightweight 5F Series features high strength-weight ratio plus the quick-operating advantages of a ¼-turn fastener... in a size and weight that offers new design possibilities to original equipment manufacturers! Particularly adaptable to thin materials and miniaturized equipment like airborne electronics, small electro-mechanical and computing devices and communications components. Ideal for attaching lightweight components in "packaged" equipment or for holding access panels on everything from washing machines to radar units.

series

Offered in many different head styles. Complete specifications will be sent to you on request.



FASTENER CORPORATION 61 Spring Valley Road, Paramus, N. J.

WEST COAST OFFICE: 5410 WILSHIRE BLVD., LOS ANGELES, CAL. FORT WORTH OFFICE: 2509 W. BERRY ST., FORT WORTH, TEXAS CIRCLE 344 ON READER-SERVICE CARD FOR MORE INFORMATION

PICTURE OF AN ANGLE

Using the new DIEHL Precision Phase-Shifter, any shaft angle can be converted into an accurate *digital* presentation like the pulse

train shown above. In such use, a separate high frequency counting signal is triggered by the reference wave and shut off by the phase-shifted wave, thus identifying a shaft angle with a finite number of pulses. Small size and simplicity make this Phase-Shifter ideal for use as an Analog-to-Digital Converter component.

This is only one of many applications for the DIEHL Precision Phase-Shifter which can now be provided for any fixed frequency between 60 cps and 4 megacycles.

By combining the very accurate DIEHL Size 11 Resolver with the appropriate circuitry, accuracies of better than $\frac{1}{4}$ of a degree have been attained at frequencies up to 100 Kc. Phase shift is continuous through 360° and variation of output amplitude is held to a minimum.

To insure that the accuracy of the Phase-Shifter is not influenced by external loading, a cathode follower circuit is incorporated in the network to isolate the unit.

Send for additional engineering data.

DIEHL MANUFACTURING COMPANY Electrical Division of THE SINGER MANUFACTURING COMPANY

Finderne Plant, SOMERVILLE, N. J.

other available components

AC SERVOMOTORS
 AC SERVOMOTORS WITH AC TACHOMETERS
 AC SERVOMOTORS WITH DC TACHOMETERS
 AC AND DC TACHOMETERS
 RESOLVERS

CIRCLE 348 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Transfer Storage Counter

"The Counter with a Difference" is a 6page booklet about the Model TS-204 transfer storage counter and two of its accessories. The text explains what the counter can do and how it operates. The accessories described are the RR-40 relay readout and the TS-204P power supply. The booklet is illustrated with photographs and a block diagram. A list of specifications is provided for all three units. Burroughs Corp., Electronic Tube Div., Plainfield, N.J.

Ferrites

350

349

The magnetic properties of three ferrite materials, Ferramic O-2, Ferramic Q and Ferramic H, are discussed in separate 2page catalog sheets. The ferrites are used as component parts in radio and TV sets, computers, automatic controls and related electronic equipment. Pertinent information is presented in tables and graphs. Photographs are provided for illustration. General Ceramics Corp., Keasbey, N.J.

Systems Manufacture

Facilities for systems manufacture are outlined in an illustrated brochure of eight pages. The booklet stresses the importance of systems to technological progress and names some areas where they have contributed immeasurably. It also cites a number of specific systems that the company has pioneered and supplied. McGraw-Edison Co., Thomas A. Edison Instrument Div., West Orange, N.J.

Vacuum Tube Test

A 16-page technical brochure deals with a quality test used in the production of power vacuum tubes. Entitled "A Positive Grid Voltage-Space Current Division Test for Power Vacuum Tubes," the paper was originally delivered by James A. Jolly at the 1957 IRE Convention. Existing test techniques and their limitations are discussed along with the new one. The description of the subject method is supported with sample data. Eitel-McCullough, Inc., San Bruno, Calif.

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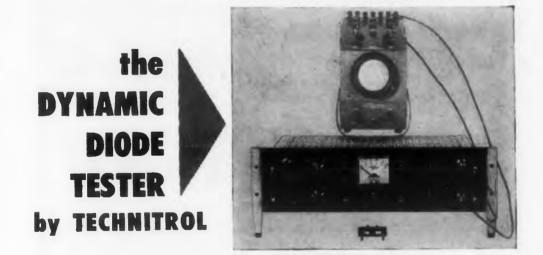
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This moderate-price instrument provides an invaluable means for the rapid, accurate checking of semiconductor diodes for instability and irregularities. The dynamic curve, far more revealing than static testing, is quickly apparent on a scope screen, and is readily adapted to volume testing. In addition, the easy portability of this 16-pound instrument makes



it ideal for field work as well as bench or rack installation.

Designed for use with a D.C.-coupled oscilloscope, the Technitrol Diode Tester provides for a variety of back and forward voltages, as well as independentlycontrolled ranges for back and forward currents.

CALIBRATED RANGES:

• Reverse current0—1 ma.

CIRCLE 353 ON READER-SERVICE CARD FOR MORE INFORMATION

Vire Twister

A 1957 catalog and price list for the M-80 ire twister is now available. The catalog fully illustrated and contains complete pecifications. The patented action of the ire twister is shown by a motion-picturete sequence of 9 photographs. Ralph C. obinson Co., 2516 Crosby Way, N. Sacraento 15, Calif.

uick Reference Catalog

359

358

A 16-page, 3-color Quick Reference Cataog which summarizes electrical and physial data is now available. It gives this inormation in a handy tabulated form for ach line of triodes, tetrodes, pentodes, lystrons, heat dissipating connectors and thers. Eitel-McCullough, Inc., San Bruno, alif.

Aulti-Turn Potentiometers 360

Two series of multi-turn precision potenometers with linearity tolerances of ± 0.01 er cent are specified in Data Sheet 54-23. The 2-page treatment is illustrated with a hotograph, dimensional diagrams and a ibeled cutaway. Helipot Corp., Newport leach, Calif.

Pulse Generator

The Model 2125B pulse generator is featured in a revised two-page bulletin. Illustrated with photographs and lock diagrams, the text provides design and construction data and detailed specifications. Electro-Pulse, Inc., 11861 Teale St., Culver City, Calif.

Thermostats

Two thermostats, the Model D1 for ac systems and the D10 for dc systems, are featured in Bulletin RT-803. Illustrated with photographs and diagrams, the fourpage folder contains application and installation information. Robertshaw-Fulton Controls Co., 110 E. Otterman St., Greensburg, Pa.

Plastics: Fibre and Thermosetting 363

Various parts used in a wide range of industries are included in a folder entitled "Applications for Wear" now available.

The illustrated pamphlet gives a complete description of the parts, such as retainers, washers, bearings and rubbing blocks and bushings. Spaulding Fibre Co. Inc., Tonawanda, N.Y.

MODEL 1852

CINTEL MUTUAL and SELF INDUCTANCE BRIDGE

Coverage: 0.001 μH to 30mH in 12 ranges 100μ Ω to 3000 Ω

Accuracy: ± 1% of full scale on all ranges

Frequency: 1592 cps (ω = 10,000)

Price: \$625.00 f.o.b. N.Y.C.

Features:

- Direct reading of either mutual or self inductance.
- All measurements in form of 4-terminal network.
- Also measures very low resistance.
- Maintains accuracy at low values.
- L & R balances are independent.
- Built in oscillator and visual detector.

CINTEL bridges simplify intricate measurements and all have wide range and high accuracy. Watch for future ads. Detailed specification on request.

Exclusive Sales and Service in U.S.A.

MARCONI Instruments 44 New Street • New York 4 CIRCLE 364 ON READER-SERVICE CARD FOR MORE INFORMATION 362

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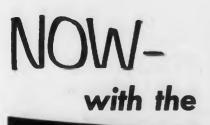
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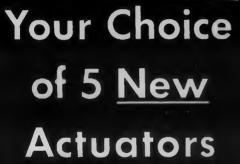
ACRO SUBMINIATURE SWITCH



ACTUAL SIZE

CIRCUIT ARRANGEMENTS

COM C O O CC O



With its small size, high capacity, and newlydesigned actuators, the Acro Subminiature Switch meets an exceptionally wide range of design requirements . . . provides many new development possibilities for subminiature assemblies.

The electrical rating of this precision Acro Snap-Action Switch—10 amperes at 125 or 250 volts A.C. or 28 volts D.C.—is over four times that of most switches this size. It will operate within a temperature range of from $+350^{\circ}$ to -80° F., and its terminal arrangement permits wiring double circuits.

Switching mechanism is enclosed in a durable plastic case which can also be adapted to various types of present actuators and mountings not shown.

Write for literature, engineering datal



FAF



CONTROLS COMPANY ACRO DIVISION Columbus 16, Ohio

In Canada: Robertshaw-Fulton Controls (Canada) Ltd., Toronto CIRCLE 365 ON READER-SERVICE CARD FOR MORE INFORMATION



Computer - Measurements Model 226A

new

UNIVERSAL COUNTER-TIMER



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- ★ Three independent, adjustable trigger level controls permitting <u>full rated</u> <u>sensitivity</u> at any voltage level between <u>300</u> and <u>300</u> volts.
- ★ Small voltage increments ordinarily masked by attenuators are easily selected.
- Simplified color-coded controls and direct read-out in kc, mc, sec, or millisec, with automatic decimal point indication.
- Oscilloscope marker signals facilitate start and stop trigger level adjustment for time interval measurement of complex waveforms.

A brand new, multi-purpose instrument provides precision measurement of frequency, frequency ratio, period (1 frequency) and time interval Pressure, velocity, acceleration displacement, flow, RPS, RPM, etc., may also be measured with suitable transducers. The 226A may be used as a secondary frequency standard

price \$1,100.00

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SPECIFICATIONS:

FREQUENCY MEASUREMENT

Frequency Range: 0-1,000,000 cycles per second Input Sensitivity: 0.2 volt rms. Direct-coupled input Time Bases: 0.00001, 0.0001, 0.001, 0.01, 0.1, 1 and 10 seconds. Also can use external 0-1 mc standard

PERIOD MEASUREMENT

Period Range: 10 microseconds to 1,000,000 seconds Frequency Range: 0.000001 cps to 100 kc Input Sensitivity: 0.2 volts rms. Direct-coupled input Timee.

Gate Times: 1 and 10 cycles of unknown frequency Standard Frequency Counted: 1 mc; 100, 10, 1 kc; 100, 10, 1 cps; external 0-1 mc.

TIME INTERVAL MEASUREMENT

Range: 3 microseconds to 1,000,000 seconds Start and Stop: Two independent or common channels Positive or negative slope Input Sensitivity: 0.2 volts rms. Direct-coupled input Standard Frequency Counted: 1 mc; 100, 10, 1 kc; 100, 10, 1 cps; external 0-1 mc.

GENERAL Stability:

Short Term: 1 part in 1,000,000 (temperatureregulated crystal)

Long Term: 3 parts per million per week Display Time: Automatic: Continuously variable 0.1 to 10 seconds Manual: Until reset Input Impedance: 1 megohm and 50 mmf Trigger Level: Continuously adjustable from -300 to +300 volts Accuracy: ± 1 count \pm stability Secondary Frequency Standard: 1 mc; 100, 10, 1 kc; 100, 10, and 1 cps Dimensions: 17" W x 8¾" H x 13½" D approx. Weight: 50 lbs. approx.



MODEL 225A 0 cps-100 kc UNIVERSAL COUNTER-TIMER Similar to the 226A in design.

Similar to the 226A in design. Featuring Oscilloscope Trigger Level Marker Signals; Three Direct-Coupled Inputs of 70 mv sensitivity; Direct Reading, Automatic Illuminated Decimal Point. Easily portable. Price: \$840.00

Data Subject to Change Without Notice – Prices F.O.B. Factory Write for complete specifications on the new 226A and the 225A models and the complete CMC line of electronic counting and controlling equipment.

Computer-Measurements Corporation

5528 Vineland Avenue, North Hollywood, Calif. Dept. 76-G CIRCLE 368 ON READER-SERVICE CARD FOR MORE INFORMATION

CC-30

New Literature

Aluminum Foil Wire Markers

A line of aluminum foil wire markers are shown in a two-page, three color bulletin now available. The bulletin illustrates two sizes of foil markers furnished on quick-release dispenser cards: 1-1/2 in. markers for wire over 1/4 in. O.D. 3/4 in. markers for wire under 1/4 in. O.D.

Special properties of instant-sticking aluminum wire markers are listed: resists temperatures to 350 F; precut, fits and sticks to any wire diameter; resistant to soil, grease and water; protected by transparent coating against rubbing and abrasion, and no tools required.

Although any size, shape, color or symbols can be specified, a large stock of items for immediate delivery are listed. These include solid numbers, letters, symbols and machine tool control symbols; consecutive numbers or letters; or consecutive numbers or symbols repeated in sequence.

The catalog also contains ordering information, list of prices and delivery time. North Shore Nameplate Inc., 214-27 Northern Blvd., Bayside 61, N.Y.

CURTISS

3130

Multi-Channel Oscilloscopes

369

A 28 page catalog describing complex line of standard 2- and 4-channel oscilla scopes, strainalyzers and related dc ampl fiers has been issued.

A number of new items are feature including a 2-channel scope with a vertice frequency range from dc to 15 Mc, and 4-channel recording oscilloscope and may ter strainalyzer for which input information may be either differential or single-ended

A portion of the catalog is devoted explaining the advantages of multi-channel oscillography in which non-recurring event may be triggered and the resulting open tional phenomena recorded simultaneous from different points. In addition to the 2- and 4-channel units described in the catalog, other types including oscilloscope providing up to 8 channels or beams on single-tube face are described. The catalog lists multi-gun cathode ray tubes in 2-, 3 4-, 5-, 6-, 8- and 10-gun types. DC powe supply units are likewise included. Elec tronic Tube Corp., 1200 E. Mermaid Lan Philadelphia, Pa.



Computers, broadcast equipment, motors, lighting systems, missiles, industrial controls — for electrical circuit appli-cations involving time delay that demand unfailing action cations involving time delay that demand unfailing action in every control phase, more and more design engineers specify "SNAPPER" Relays by Curtiss-Wright. These reliable relays eliminate chatter with *positive* snap action, have single-pole double throw contacts and a wide temper-ature range ($-65^\circ + 100^\circ$ C). Preset time delays from 3 seconds to 3 minutes are now available in metal envelope and from 5 to 60 seconds in glass envelope. Write for our new detailed data sheet with complete application in-formation formation.

ELECTRONICS DIVISION

Component Sales Department

CIRCLE 371 ON READER-SERVICE CARD FOR MORE INFORMATION

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RELAYS

—thermally operated bi-stable time delay relays with two sep-arate heater circuits.

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xparision Joints

Rubber, neoprene and Teflon-lined exansion joints, their construction, sizes and ses are fully explained in Bulletin AD-137 ow available. The bulletin describes the haracteristics and limitations of seven tyles of expansion joints and flexible coulings; 1 spool-type expansion joints; 2 rec-

378

ingular-type expansion joints; 3 U-type pints; 4 all-Teflon expansion joints; 5 allreflon flexible couplings; 6 full-faced Teflon ined rubber expansion joints; 7 expansion pints for use on piping and flanges.

It also explains that rubber expansion pints are suitable for handling hot or cold vater, mild acids, mild caustic solutions, prine, air or exhaust steams, at temperaures to 180 F.

Rectangular type expansion joints as decribed in the bulletin are available for pplication in pressure and vacuum lines. These joints are frequently used as a flexble connection between a turbine and a condenser.

Metal retaining rings made of galvanized teel to be placed behind and directly

new ...

against the inner face of each of the rubber flanges at the ends of the joints, as well as Teflon expansion joints and flexible couplings for fluid process piping handling strong acids, caustics, foods and halogenated solvents are outlined in the bulletin. Garlock Packing Co., 408 Main St., Palmyra, N.Y.

379

Aircraft Thermocouples

MC-153 is a four-page brochure on thermocouples for aircraft gas turbines and related aviation applications. It describes and illustrates the four basic junction tips-exposed junction, twisted-exposed junction, stagnation tip and sampling tip--which provide the starting point for hundreds of model variations. Performance data and accuracy limits for the thermocouple wire material at temperatures up to 2000 F are listed. Also illustrated are the various design features which assure the reliability and accuracy of the thermocouple series in aviation service. Fenwal Inc., Aviation Products Div., Ashland, Mass.

when ordinary instruments are too big or inadequate . . .

trio

trio

low-level BUILD-IN AC VTVM

with BUILT-IN ISOLATION

ardes.

panel-mounting, new model 109-1 reads down to 20 microvolts on its 1 MV range with 2% full-scale accuracy, 10 megs input impedance, response 20-80,000 cps . . . features signal & power circuits and mounting panel all isolated from each other ... extreme stability - wide line variations do not affect accuracy . . . calibration of gain and frequency response without removal from panel . . . feedback and printed circuitry for exceptional reliability and simple maintenance . . . size 5¼" h x 9½" w x 9¾" d -panel fits standard modular-type consoles. Price \$199.50 Write for FREE "how-to" ENGINEERING GUIDE on Trio's complete line to Dept. ED-7, Trio Laboratories, Inc., Seaford, N.Y.

Designed especially for

CIRCLE 380 ON READER-SERVICE CARD FOR MORE INFORMATION

ELECTRONIC DESIGN • July 15, 1957

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1957

Between Concept and ConfigurationSave Time and Money with

PHILBRICK PLUG-IN DC

Shown 1/2 size

AVAILABLE FROM STOCK

For a wide variety of instrumentation and control problems, you can facilitate rapid set-up with either one or both of these octal-based, plug-in Philbrick Amplifiers. Operational Amplifier, Model K2-W, features balanced differential inputs for minimum drift and maximum utility. In conventional applications, overall amplifier characteristics are affected solely by the feed-back networks, since the two inputs can be maintained at nearly equal potential with appropriate feed-back circuitry.

For more critical applications where long term drift must be reduced to sub-millivolt levels, Stabilizing Amplifier, Model K2-P, is paired with Model K2-W. Write for free 28 page Plug-In Amplifier Applications Manual-13.

MODEL K2-W

GAIN: 15,000 dc, Open Loop POWER REQUIREMENTS: 4.5ma @ ±300 vdc, 0.6 amps. @ 6.3v OUTPUT RANGE: +50v. to -50v. at 1 ma RESPONSE: 2 Microseconds rise time, 100 Kc with unity feed-back PRICE: \$24.00 Postpaid

· MODEL K2-P

GAIN: 1,000 dc

POWER REQUIREMENTS: 2.4 ma @ +300 vdc, 0.45 amps. @ 6.3 vac, 60 cps

INPUT IMPEDANCE: 1 Megohm STABILITY: Below 100 Microvolts PRICE: \$60.00 Postpaid



230 Congress Street, Boston 10, Massachusetts HUbbard 2-3225 CIRCLE 381 ON READER-SERVICE CARD FOR MORE INFORMATION

Acetrim^{*} sub-miniature

precision TRIMMERS for PRINTED CIRCUITS

Here is another new development from Ace...sub-miniature precision wire-wound trimmers especially for printed circuits. Designed and produced to meet your tightest specifications, the new Acetrim has flat or round tabs to facilitate production assembly. Just plug into printed circuit board, secure, and dip solder.

New

Ace delivers reliability

Featuring

- 1/2" size
- 10 ohms to 150 K
- weight 1/4 ounce
- power 2 w. @ 60° C. max.
- temperature to 125° C.
- sealed, moistureproofed, anti-fungus treated
- withstands severe shock, vibration, acceleration
- meets applicable Military specs

Modern mass production techniques assure delivery to meet your schedules . . . rigid quality controls assure highest standards of performancereliability.

Acetrim — write for Technical Data Unit #563.

Acopot — $\frac{1}{2}$ " sub-miniature precision wire-wound linear potentiometers from 10 ohms to 250K. $\pm .3\%$ standard. Write for Technical Data Unit #564.

Nonlinear Acepot — precision wirewound nonlinear potentiometers for

•trademarks applied fo

sine-cosine and square-law functions and other applications. High resolution, close conformity. Write for Technical Data Unit # 572.

X-500 Acepot — ½" sub-miniature precision potentiometers for extreme temperatures of --55° C. to 150° C. 10 ohms to 250K. Write for Technical Data Unit #571.



Telephone: SOmerset 6-5130 Engineering Representatives in Principal Cities C.RCLE 388 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Plastic Molding Presses

The redesigned 741 series of fully automatic compression presses for plastic molding is described in the 12 pages of Catalog 200. Complete specifications are given for the series' four models of 50, 75, 125, and 200 tons capacity. Photographs illustrate the 741 presses and a variety of other equipment. F. J. Stokes Corp., 5500 Tabor Rd., Philadelphia 20, Pa.

Antenna Systems

390

389

Engineering improvements to existing antenna systems equipment are noted in a 32-page new product supplement. Illustrated and described are a 9-in. uhf transmission line, a 3 1/8-in. uhf coaxial switch and an expanded line of microwave and communication antennas. Full specifications are given for all items. The booklet also contains ordering information and a price list for all available products. Andrew Corp., 363 E. 75th St., Chicago 19, Ill.

Bimetal Thermostats

Snap-acting Type M bimetal thermost are the subject of Bulletin 6000. Herme cally sealed and semienclosed types for usin appliances, fire alarms, television restations and communications equipmentail. are described. The 2-page bulletin cove principles of operation, construction [don tures and ratings. It is illustrated with photographs showing different types available terminal arrangements and closures. Stevens Mfg. Co., Inc., Lexington Ohio.

Electric Brake

An electric brake for ac motors is externation wid sively discussed in a folder of 4 pages. advantages, operation, performance, specare fications and uses are covered. Typic performance curves and a labeled phone graph showing construction are among the illustrations. American Rectifier Con Selenibrake Div., 95 Lafayette St., Ne York 13, N.Y.

for maximum reliability



SIZES Available in sizes and modifications to retain all popularly used transistors.

Write for catalog

under severe conditions of shock and vibration. In addition they provide an excellent heat path to drain off heat into chassis or heat sink.

| THE BIRTCHER CORPORATION | | | |
|--------------------------|------------------------|--|--|
| INDUSTRIAL | 4371 Valley Bivd., | | |
| DIVISION | Los Angeles 32, Calif. | | |

CIRCLE 393 ON READER-SERVICE CARD FOR MORE INFORMATION

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bCT ming Motors

Bulletin AWH MO 805, a 2-page insert 30 or a current catalog, contains information termost for a current catalog, contains into the function of the three basic dc timing Hermonotors. The construction of the 5300, 6300 es for and 7600 series motors are analyzed in de-sion result Featured is a cutaway view of the moail. Featured is a cutaway view of the moquipm or which shows the rotor construction and in cove elf-contained gear train. The A. W. Hayction fe don Co., Waterbury, Conn. ted wi

Chopper Circuit Residual Noise 399

exingto Availability of a four-page technical paper, "Measurement of Residual Noise in Chopper Circuitry," is announced. The 39 article covers the theoretical as well as the is exterpractical evaluation of residual noise in a pages h wide variety of chopper circuitry. Included ce, spectare graphs and information helpful to de-Typic sign engineers. James Vibrapowr Co., 4050 M. Rockwell St., Chicago 18, Ill. d phot

Com Design Services

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Electronic research and development, quipment and systems designing, production engineering, and pilot model building are among the services announced in Bulletin 571. The four illustrated pages also give details on facilities and on completed projects. Strand Engineering Co., 1354 N. Main St., Ann Arbor, Mich.

Magnetic Tape Recorders 401

An entire line of professional magnetic tape recorders is listed in a catalog of 15 pages. Complete specifications and pertinent information are presented for all models. Also described with specifications are a variety of accessories and modification kits. Photographs are provided for illustration. Magnecord, Inc., 1101 S. Kilbourn Ave., Chicago 24, Ill.

Centerless Grinder

The TG-12 centerless grinder is the subject of a 4-page illustrated brochure. To a detailed description of mechanical features is added a complete specifications table which gives data on capacity, equipment and accessories. Various types of grinds are illustrated. Royal Master, Inc., State Highway No. 23, Riverdale 1, N.J.

402





for military and industrial applications. Illustrated are some of these units . . . any can be modified to meet your specific requirements if the basic design is not adequate.

Shown below is the new catalog of the A. W. Maydon Company describing all of the basic types of units available and many of the "speciah". Included in this 25-page catalog are 60 photographs of timers, 30 d im en sien a 1 drawings, and 50 charts and diagrams. This



complete log will be plied on req catae sup-quest.

•

Long a pioneer in the timing field, The A. W. Haydon Company is prepared to assist you in solving your timing and control problems. When a solution to your problem has been reached, The A. W. Haydon Company is pre-• . pared to follow through with production geared to meet your requirements whether a basic ø timing unit or a highly specialized device is required.

W. HAYDON COMPANY the A. 227 NORTH ELM STREET WATERBURY 20, CONNECTICUT Design and Manufacture of Electro-Mechanical Timing Devices

CIRCLE 403 ON READER-SERVICE CARD FOR MORE INFORMATION

LECTRONIC DESIGN • July 15, 1957

NEW PHAOSTRON EXPANDED SCALE AC Voltmeter

Available now from distributors in 90V to 130V Range, AC Rectifier Type in all custom styles and sizes.

> 3½" or 4½" rectangular meter

> > NOW!...all the time-tested proven Phaostron features PLUS UP TO TEN TIMES GREATER READABILITY

adautoutoutout

OLTS

for greatly increased accuracy!

2½" or 3½ square meter



6" rectangular meter



All meters available with illuminated dial on special order Phaostron has squeezed down that under 90V portion of the scale, where you don't need it, and expanded the section where you need it most—between 90 and 130V. Precisely calibrated 1 volt scale increments provide greater reading accuracy. Wide frequency range linearity—true rms reading and Phaostron craftsman construction.

Phaostron Custom Panel Meters, with expanded scale, 90V to 130V AC rms, are available in nine types at your Parts Distributor. For special requirements for AC or DC expanded scale meters, write to Product Development Dept. for practical recommendations.



PHADSTRON INSTRUMENT & ELECTRONIC CO., 151 PASADENA AVE., SOUTH PASADENA, CALIF. CIRCLE 404 ON READER-SERVICE CARD FOR MORE INFORMATION



RCA RELAYS

RCA Relays . . . for outstanding performance in high-speed, highaltitude missile and airborne applications, and critical requirements in industry.

Miniaturized . . . hermetically sealed . . . RCA Relays are highly reliable under the most severe operating conditions. RCA Relays meet and exceed the electrical and mechanical requirements of MIL-5757C and MIL-R-25018 (USAF).

GENERAL FEATURES

• Rated for operation up to 80,000 feet. • Insulation resistance better than 1,000 megohms after life test. • Balanced rotary motors for utmost stability. • EXCLUSIVE— Specially crimped mounting flanges provide positive contact at four points on the mounting surface!

Use the coupon for more information about RCA Relays.



RCA Type 203W2—A 6 PDT miniaturized DC relay weighing less than $4\frac{1}{4}$ ounces. Withstands 50g deceleration shock for 11 milliseconds, and 10g vibration shock from 5 to 2,000 cps. 26.5 volts DC coil. Contact rating 2 amperes. Life 100,000 cycles plus! Contact resistance less than .050 ohm. Contact Bounce less than 300 microseconds. R.F. Capacitance less than 3 $\mu\mu$ f. Temperature Range -55° C to $+85^{\circ}$ C.

RCA Type 204W1—Same as the 203W2 except: Temperature Range -65° C to $+125^{\circ}$ C. Uses a "getter" which absorbs organic vapors and keeps contact clean—contact resistance will be lower *after* life test than *before* life test.





RCA Type 206W1—A 2 PDT miniaturized DC relay weighing less than 0.9 ounces. Temperature Range -65° C to $+125^{\circ}$ C. Like the 204W1 uses a "getter" to keep contacts clean. All other characteristics the same as the 203W2 except resistance to vibration shock from 5 to 2,000 cps is 15g.

ILLUSTRATIONS ARE TWO-THIRDS ACTUAL SIZE.



RADIO CORPORATION of AMERICA

COMPONENTS DIVISION

CAMDEN. N.J.

MAIL NOW FOR RCA RELAY DATA

| RCA Components Division, Sect. E-84-PP, Camden, N.J. | | | | | |
|--|----------------|-------------------------------|--|--|--|
| Bulletin 204W1 | Bulletin 206W1 | Have RCA Rep call | | | |
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| | | Bulletin 204W1 Bulletin 206W1 | | | |

CIRCLE 408 ON READER-SERVICE CARD FOR MORE INFORMATION

New Literature

Hardener for Epoxy Potting

An epoxy hardener, for potting and encapsulation of electrical and electronic components, that gives good heat distortion temperature, excellent toughness, and long pot life is described in bulletin No. 13.

The physical properties of Sonite No. 41 and the physical and electrical properties of epoxy resins cured with this material are discussed.

Bulletin No. 13 gives detailed aspects of the properties, handling, mixing, pot life, and curing procedures when using Sonite 41. In addition physical properties of the cured castings, such as flexural strength, tensile strength, and resistance to impact, and electrical properties at various temperatures, such as surface resistance and volume resistivity. The physical data concerned with using Sonite 41 in glass cloth systems are also included. laminate Smooth-On Mfg. Co., 572 Communipaw Ave., Jersey City 4, N.J.

AC Output Accelerometer

409

Technical Data Sheet No. 20 provide tures engineering data, illustrations and inforture, mation on special design and operational features of the Model GAL ac output accelerometer. The four-page bulletin also describes a modified version of the instrument, designated the Model CHL, which contains an internal thermostatically-oper ated heater for extremely close damping control. Genisco, Inc., 2233 Federal Ave mac Los Angeles 64, Calif.

Electronic Parts Catalog

a 19 A 1957 electronic parts catalog has been released. Prepared by Electronic Publish on ing Co., Inc., the catalog contains 224 page bly listing components, equipment and other mer inje electronic products for industrial and senice use. Warren Radio Co., 1002 Adam Toledo, Ohio.



For exacting, high-temperature applications... **CERAMASEAL LEAK-TIGHT TERMINAL**

Assuring you savings in installation and operation, these Ceramaseal high-temperature terminals are 100% leak-tested and guaranteed leak-tight when shipped. High-alumina ceramic and metal parts of Ceramaseal terminals are joined by an exclusive process to form a high-strength, long-life molecular seal.

Brazing, welding or soldering techniques can be used for installation, without resulting damage to the seal, thus eliminating costly rework or replacement. For brochure and spec sheets, or complete information on special high-temperature terminals, write: Ceramaseal, Inc., Box 25, New Lebanon Center, New York.

Supplying High-temperature, Quality Terminals for Five Years



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411

Load Calculating Nomograph

A load calculating nomograph has been developed to help figure cooling requirements for electronic equipment mounted in trailers, vans, consoles or stationary structures. When the type and size of a structure, the internal load, operating temperature and occupancy are selected, this nomograph will provide the required cooling load in BTU's per hour, and select the correct capacity for air conditioning equipment designed to meet rigid military specifications. The nomograph is printed on paper easily copied by any reproduction machine. Ellis and Watts Products, Inc., Monroe at Spencer, Cincinnati 36, Ohio.

Custom Molded Plastics

419

418

"Custom Molded Plastics for Industry" is a 12-page booklet with illustrated sections on molding facilities, finishing and assembly of components, research and development, and quality control. Chapters on injection molding, compression molding d othe id serv and transfer molding list examples of auto-Adam matic equipment used in molding of thermoplastic and thermosetting materials. Sylvania Electric Products Inc., Warren, Pa.

Electronics—Key to Control 420

Applications of electronic temperature controls for the heating, ventilating and air conditioning field are described in colored four page bulletin, F-2287-4 now available. It explains all the features, functions and advantages of an electronic system which provide efficient and economical control for any type of heating and air conditioning equipment. All components and accessories, used in the various types of electronic systems, are illustrated and specific applications of each are discussed. Barber-Colman Co., Temperature Controls, 1400 Rock St., Rockford, Ill.

Current Limiting Fuses

The eight pages of Bulletin GEA-6319B describe a line of CLF current limiting fuses capable of interrupting short circuit currents up to 200,000 rms symmetrical amperes. The operation and application of the fuses are outlined and dimensions and ratings are given. The booklet is illustrated with photographs and also graphs showing current characteristics. General Electric Co., Schenectady 5, N.Y.

421



ELECTRONIC DESIGN • July 15, 1957 1957

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as bee Publish 4 page

41

A New Broad Band Kearfott



Use this Ferrite Isolator in your microwave setup for maximum frequency stability.

CHECK THESE FEATURES:

Broad Band --- Usable from 8.2 to 10.2

High Isolation - A minimum of 25 db

Flanges — Cover type. Mates with UG39/U flanges. Will absorb up to

For custom-made isolators for

specific radar & microwave appli-

cation, you can depend on the skill

Kearfott, Western Division, has

complete facilities for waveguide

production, with qualified experts

to assist in solving your problems.

MICROWAVE DEPARTMENT 14844 OXNARD ST. . VAN NUYS. CALIF.

COMPANY, INC. FALLS, NEW JERSEN TERN DIVISION

of the Kearfott organization.

10 watts reflected power Price-\$135.00 each f.o.b., Van Nuys,

Insertion Loss - Less than 1 db Small & Compact - Only 21/2 inches long-weighs only 11/2 lbs.

KMC

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Delivery-From stock

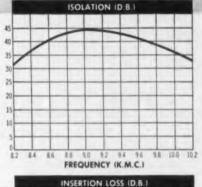
Let us help you.

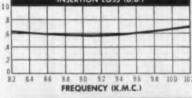
Order - Model W177-2C-1

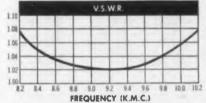
over the band

Model W177-2C-1

Typical Performance Curves







For detailed information, ask for bulletins on new Ferrite Isolators and Radar Test sets.

A SUBSIDIARY Eastern Office: 1378 Main Ave. Clifton, N.J.

Midwest Office:

SALES OFFICES 188 W. Randolph St. Chicago, Ill.

WES

South Central

Western Area Office: Office: 6115 Denton Drive Dallas, Texas Office: 253 Vinedo Ave. Pasadena, Calif.

CIRCLE 423 ON READER-SERVICE CARD FOR MORE INFORMATION



Transistor Beta Tester

A simple, inexpensive instrument for measuring the β of a wide variety of transistors has been developed by the National Bureau of Standards. The device measures the common-emitter short-circuit current gain of pnp or npn transistors at low audio frequency. In operation, the transistor is plugged into the instrument and a dial is adjusted to the point where a tone is heard from a loudspeaker. The β is then read directly from the dial. Properly calibrated, the instrument can measure β accurately over a range of 10 to 170.

The circuit is similar in principle to one used for measuring vacuum tube transconductance. In such a tube circuit, part of the plate voltage is fed back into the grid through resistor and transformer coupling to cause oscillation. Similarly, with the circuit for measuring transistor gain, the output is fed back into the input through a variable resistor and a transformer; when the resistor is properly adjusted, the circuit begins to oscillate at an audio frequency. The dial on the variable resistor can be calibrated through a substitution method.

To reduce the number of controls to a minimum, circuit parameters are chosen so that the transistor will adjust itself to a specified dc operating point. The resistors in the circuit were selected to fix this

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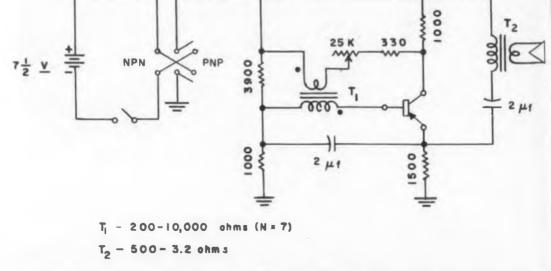
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Circuit diagram of transistor β tester. When the 25K pot is properly adjusted for a given transistor, the circuit oscillates at an audio frequency. Tone can be heard from loudspeaker.

ELECTRONIC DESIGN • July 15, 1957

Get S to jo made Full i taine Get \$10.00 plus a by-line for the time it takes you to jot down your clever design idea. Payment is made when the idea is accepted for publication. Full information and an "entry blank" can be obtained by circling 548 on the Reader's Service Card.

point at about 5 v collector potential and 1 ma collector current. For any transistor whose β falls within the measuring range of the instrument, these dc values will be closely approximated when the transistor is plugged in.

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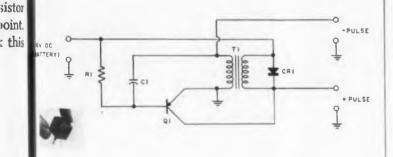
957

The frequency at which oscillations begin depends upon the characteristics of the transformer and the phase shift of β . The current ratio of the audio transformer has a broad maximum centered at 1 or 2 kc, and if the phase shift of the transistor is sufficiently small, oscillation begins at a frequency near this maximum. However, the transistor gain required to produce oscillation for a given dial setting is not a particularly sensitive function of frequency. Measurements accurate to within a few

per cent of full scale can be expected.

Encapsulated Blocking Oscillator

Encapsulated with epoxy resin within a 3/4 in. cube shown is a complete blocking oscillator circuit which includes a subminiature pulse transformer, transistor, capacitor, resistor and crystal diode. The circuitry shown produces triggering electronic



pulses identical to those obtained from larger, more expensive pulse generators.

Designed by engineers of Allen B. DuMont Labs. Inc., a pulse of 3 µsec duration with a rise time of 0.06 usec is obtained. The repetition rate is 25 kc. Power requirements are furnished by a miniature 6 v mercury cell which lasts approximately 1000 hours. Amplitude of pulse is from +6 to -3 v peak. The "pulse cube" can be obtained from DuMont with a fixed repetition rate of 1 kc if desired, or a variable repetition rate from 400 cps to 24 kc. It can also be obtained as a free-running blocking oscillator or for external triggering. Operating temperature range is from -55 to 60 C.

FOUR NEW G-E TRANSISTORS

 Operation below zero and up to 150°C

• 25 mc alpha cutoff

• Low leakage current

 Easy automatic insertion in printed circuit board

DESIGN FEATURES

High Temperature Performance . . . maximum ambient operating temperature 150°C, storage temperature up to 200° C

TYPES

4JD4A2

4JD4A3

4JD4A4

4JD4A5

New Package Design ... for automatic insertion in printed circuit boards

Package Hermetically Sealed ... no moisture seepage from outside air

Package Seams Are Welded for great strength, long wear

Long Life and Stable Performance . . . when used within specified ratings

Small Size . . . extremely compact design provides added flexibility for most applications

Here are just a few typical applications for the NPN silicon triode transistors: wide band and d-c amplifiers, oscillator circuits, computer switching.

And now all General Electric transistors are a better buy than ever. Because of mechanized production lines, G-E transistors are made in less time and at a lower cost than before. Thus you benefit from lower prices. Besides, machine methods used on the General Electric production lines promote the strictest adherence to top quality standards. As a result, characteristics are controlled and narrow limits are built into the production transistor for a more uniform product. Therefore, General Electric is able to give a one-year written warranty.

For specifications and application engineering assistance, call your G-E Semiconductor District Sales Manager, your G-E Semiconductor distributor, or write the General Electric Company, Semiconductor Products, Section S2377, Electronics Park, Syracuse, N. Y.



ECG-126

CIRCLE 429 ON READER-SERVICE CARD FOR MORE INFORMATION

aker

ELECTRONIC DESIGN • July 15, 1957

133

GYROS for every application

The Kearfott miniature 4 Gimbal 3 Gyro, stable platform, provides precise azimuth, pitch and roll information-irrespective of the airframe attitude. It is hermetically sealed for environmental protection. Because of its rapid warmup characteristic, this unit is fully operational in less than five minutes. This platform provides the features of a magnetic slaved or a latitude corrected directional gyro for heading reference. Dependable, accurate single purpose Kearfott Gyros also available.

> VERTICAL GYROS

> > FREE GYROS

KEARFOTT COMPONENTS INCLUDE:

Gyros, Servo Motors, Synchros, Servo and Magnetic Amplifiers, Tachometer Generators, Hermetic Rotary Seals, Indicators and other Electrical and Mechanical Components.

KEARFOTT SYSTEMS INCLUDE: Directional Gyro Compass Systems, 3 Gyro Stable Platform Systems and Inertial Naviga-

tional Systems.



Suitable for use in both missile and aircraft, random drift rate 1° per hour in azimuth and 3° per hour in vertical. Measures only 8" Diam. x 8^{3_4} " High, weighs but 23 lbs.



RATE GYROS



FLOATED RATE

Send for bulletin giving data of components of interest to you.



GENERAL PRECISION EQUIPMENT CORPORATION

KEARFOTT COMPANY, INC., LITTLE FALLS, N. J.

Sales and Engineering Offices: 1378 Main Avenue, Clifton, N. J. Midwest Office: 23 W. Calendar Ave., La Grange, Ill. South Central Office: 6211 Denton Drive, Dallas, Texas West Coast Office: 253 N. Vinedo Avenue, Pasadena, Calif.

CIRCLE 430 ON READER-SERVICE CARD FOR MORE INFORMATION

Ideas for Design

Quick-Release Fastener

The clamp design shown eliminates or minimizes the tedious and time-consuming manual manipulations of the available non-standard component clamps and at low cost.

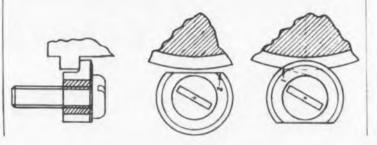
The clamp is a powdered metal casting of stainless steel with a core of plastic partially threaded. When assembled with a screw, the remainder of the thread is cut making a tight-fitting casting on the screw threads.

This captive sub-assembly is screwed into its mounting hole until it bottoms, and it is then backed off until the flat is opposite the diameter as shown. After three clamps are set, the component is mounted with the clamps in the open position, shown in the sketch. With a screw driver, the screw is turned until the clamp is in the locked position. The integral shoulder (1) stops the clamp in its strongest holding position.

Further tightening of the screw does not turn the clamp, but it is pulled down to its clamping position. In allowing the screw to continue to turn, while the clamp is stationary, the plastic permits the unit



Device held by "Synclamps". Below center, clamp is in unclamped position; at right, in clamped position; left, a side view. A half-turn with a screwdriver "does the trick."



No waveform distortion

from G-E Inductrol* Voltage Regulators

Unlike many other types of voltage regulators, General Electric Inductrols introduce no waveform distortion.

Featuring drift-free controls, Inductrols maintain the a-c or d-c voltage powering electronic circuits within $\pm 1\%$; are small and light.

They have long life and require little maintenance because they use no brushes!

For more information, write Section 425-6, General Electric Co., Schenectady 5, N. Y., or contact your G-E sales office or agent.

*General Electric Trade Mark for Induction Voltage Regulators.

Progress Is Our Most Important Product GENERAL B ELECTRIC CIRCLE 431 ON READER-SERVICE CARD

ELECTRONIC DESIGN • July 15, 1957

ELF

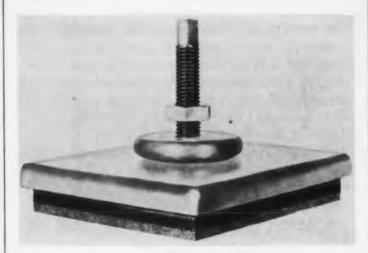


to phase itself to the pilot diameter and its own tapped hole. Seemingly, by this action, the plastic thread is stripped. However, with just a half-turn the clamp is lifted up and around to the open position, being stopped by the flat (2).

The tight fit of the plastic on the screw threads is unchanged by the "stripping" action, and may be operated indefinitely. This tight fit also gives a stop-nut action by making the screw and clamp act as a unit. It is prevented from turning by the friction at the clamping point, giving a longer moment of arm. Timber-Top Inc., P.O. Box 14, Freeport, New York.

Shock Mount Provides Mobility

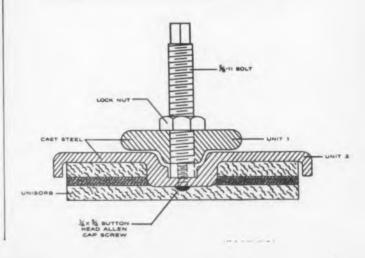
Through the use of a vibration dampener pad under a heavy steel plate, as shown, the Felters Co. of Boston has produced an equipment mount that permits ready mobility. At the same time, the equipment will remain firmly in position under vibration.



As illustrated in the cross-sectional view, leveling is readily accomplished by rotating unit 1, then locking in position with the lock nut. Unit 2 is a steel base plate which rests on the "cushion" of Unisorb.

Mounts of this type are standard for loads from 800 to 7500 lb per mount, and in sizes from 4 to 10 in. square.

The Unisorb cushion will reduce transmitted vibration by as much as 85 per cent and is impervious to cutting fluids and cleaning compounds.



ELECTRONIC DESIGN . July 15, 1957

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CONNECTORS

for MILITARY-INDUSTRY

THAT MEET AND EXCEED PERFORMANCE REQUIREMENTS OF CLASS A, B, C AND E OF SPECIFICATION MIL-C 5015B

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INSULATION SANDWICH

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connectors

Plugs and Receptacles

featuring the SILICONE

THE PYLE-NATIONAL COMPANY WHERE QUALITY IS TRADITIONAL

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CIRCLE 433 ON READER-SERVICE CARD FOR MORE INFORMATION



This new Speer Packaged Assembly Circuit offers you a wide variety of custom, preassembled units of high-quality components for use in conjunction with printed board applications.

P.A.C. permits the insertion, as a group, of a full range of capacitors and resistors in simple or complex circuitry. Each P.A.C. is based on components of uniform dimensions, $\sqrt{6}$ diameter and $\sqrt[5]{6}$ long. Component availability includes Jeffers tubular ceramic capacitors and Speer fixed composition resistors, providing wide circuit flexibility in a single P.A.C. unit.

ADVANTAGES OF SPEER P.A.C.

- Simplifies chassis design and assembly
- Reduces printed circuit board area and insertion operations
- Permits easy and low-cost component change-over to accommodate circuit revisions
- Broad choice of characteristics—low capacitance temperature compensating units and high capacitance bypass capacitors mounted in same P.A.C. unit
- Isolation of individually mounted units provides low shunt capacitance across resistors
- Pretested components achieve unusually close tolerance assembly

Learn more about the new Speer P.A.C. For information write to:

JEFFERS ELECTRONICS DIV.



Speer Carbon Co. Du Bois, Pennsylvania CIRCLE 434 ON READER-SERVICE CARD FOR MORE INFORMATION

Ideas for Design

Regulated Radio-Interference Free Generator

Described here is a generator of radio-interference-free design which produces a conventional voltage regulated output without requiring brushes, slip rings or commutator. As a result of the design, there are no sliding or arching contacts to initiate radio interference. The unique feature is the manner in which regulated excitation is supplied to the rotating field.

Brushless generators are not new. However, a machine was required which was suitable for all normal power and lighting applications and which produced a well-regulated 60 cps voltage supply. This requirement made it necessary for the generator to have a regulated dc field.

A standard engine generator set was modified for brushless, voltage regulated operation. The generator was a 30 kw., 0.8 power factor, 60 cps, 120/208/416 v, 1200 rpm diesel generator. The generator was a common type with a static armature, rotating field, and overhung dc exciter (Fig. 1). Voltage control was obtained by taking the commutated output of the exciter off through a set of brushes and feeding the dc excitation through slip rings into the main generator field. Control of the exciter output was exercised through the ex-

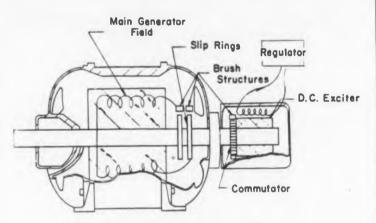


Fig. 1. Generator before modification.

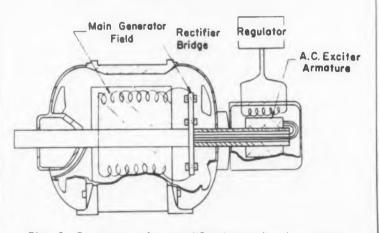


Fig. 2. Generator after modification to brushless type.

DUAL PURPOSE

TRANSISTORIZED ELECTROMETER

combined preamplifier and dc vtvm has 10¹⁴ ohms input, 1 mv sensitivity

HIGH input impedance is only part of the story with the new Keithley Model 220. As a sensitive dc vtvm, it's especially conveni when measuring voltages of transistors, dc amplifiers and computers, as well as many electrochemical and biological tests. In its alternate role as a dc preamplifier, the 220 has gains of 0.05 to 167 with suitable outputs. Uses include recording the variations in piezo-electric and pH voltages; currents in photocells, vacuum tube grids and ion chambers; and other long-term monitoring functions.



KEITHLEY Model 220 DC VTVM

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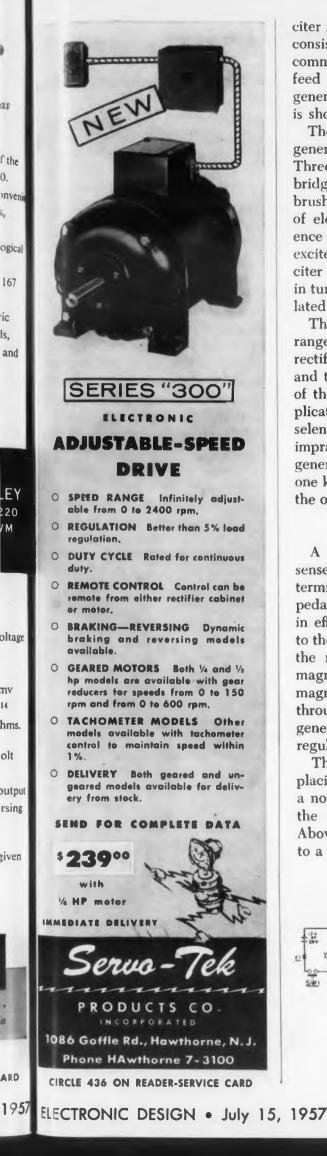
LINE-OPERATED, the 220 has 8 voltage ranges from 30 millivolts to 100 volts full scale. With added accessories, the instrument measures voltages from 1 mv to 20 kv, currents from 10^{-3} to 5 x 10^{-14} ampere, resistances from 10^4 to 10^{16} ohms.

USEFUL FEATURES include a 5-volt unbalanced output for amplifiers and oscilloscopes, and a one-milliampere output for sensitive recorders; a polarity reversing switch; and zero drift below 3 mv/hr.

DETAILS about the Model 220 are given in Keithley Engineering Notes, Vol. 5 No. 2. A request on your company letterhead will bring a copy promptly.



ELECTRONIC DESIGN . July 15, 1957



citer field. The modification made on the generator consisted of eliminating the two sets of brushes, the commutator, and the slip rings, and arranging to feed controlled dc excitation to the rotating main generator field. A sketch of the modified generator is shown in (Fig. 2).

The exciter armature, rectifier bridge, and main generator field are all rotating on the same shaft. Three phase ac exciter output is rectified in the bridge and delivered to the main field without brushes, commutators or slip rings. Thus all sources of electrical sparking and resulting radio interference have been eliminated from the generator and exciter. Control is exercised through the static exciter field which governs the exciter output, which in turn varies the main generator field to give regulated voltage output at the generator terminals.

The key development which has made this arrangement possible is the perfecting of the silicon rectifier. The relatively small size per unit of power and the more desirable temperature characteristics of the silicon rectifiers makes their use in this application very advantageous. The space required by selenium or copper oxide rectifiers would make it impracticable to mount them on the shaft of the generator. These small rectifiers will handle about one kw each. Their mass is about 1 per cent that of the old selenium or copper oxide type.

Voltage Regulation

A static type voltage regulator is used which senses the voltage output of the main generator terminals. This voltage is impressed upon two impedance type circuits in the regulator, which are in effect a voltage standard. A signal proportional to the difference between the generated voltage and the regulator voltage standard is delivered to a winding, magnetic-amplifier control and the magnetic-amplifier output is fed to the exciter field through rectifiers in such an amount as to bring the generator terminal voltage in balance with the regulating standard.

The regulating voltage standard is developed by placing across the generator terminals a linear and a non-linear circuit. There is one voltage at which the currents drawn by these circuits are equal. Above this voltage they deliver a different current to a control magnetic-amplifier in such a way as to

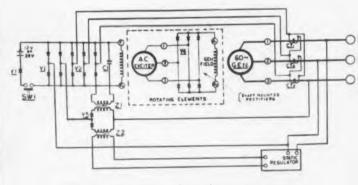


Fig. 3. Schematic of Brushless Generator.

SAVE PANEL SPACE

TRIC-SHAFT

with these

PRECISION POTS

CONCEN

You can put twice as many precision controls in the same panel space with Waters' new concentric-shaft potentiometers.

Two precision pots \cdot in $\frac{7}{8}$ " or $1\frac{1}{8}$ " size \cdot assembled in tandem \cdot for single-hole or servo mounting \cdot and control by one dual knob \cdot with stops, or for continuous rotation of either or both elements \cdot save vital space \cdot and simplify your designs.

Concentric-shaft, tandem precision potentiometers can be furnished to meet substantially the same specifications as the standard line of Waters RTS 7/8 and AP11/8 pots.

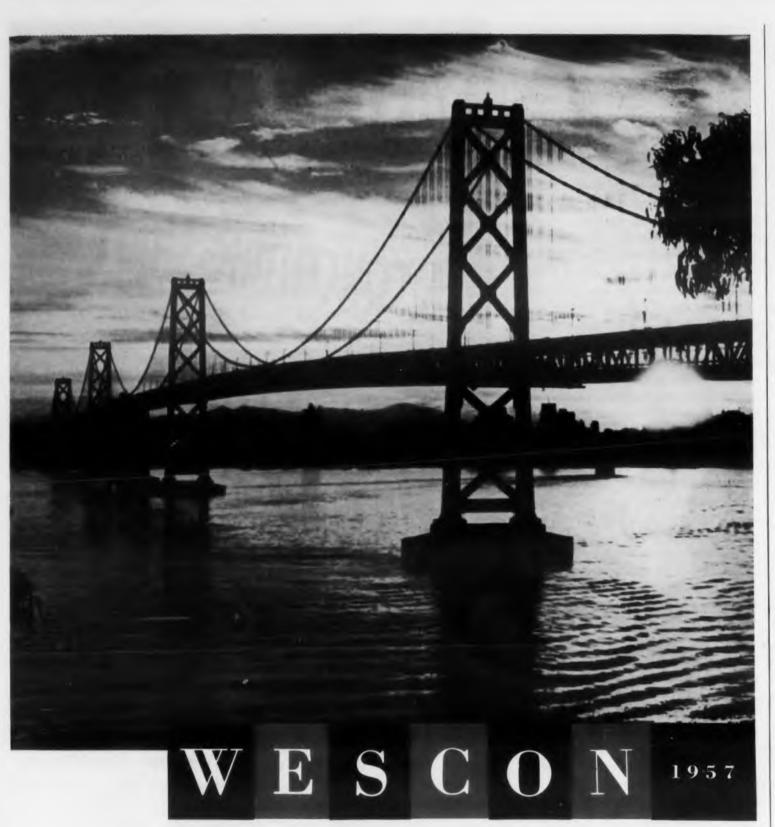
Write today for further information, or see your Waters representative.

UFACTURING.



CIRCLE 437 ON READER-SERVICE CARD FOR MORE INFORMATION

APPLICATION ENGINEERING OFFICES



An all time high, both in papers presented, and in number of exhibits, has been reported by the management of this year's WESCON.

Once again (August 1 issue) Electronic Design will cover design progress at WESCON from the standpoint of the practical, working engineer.

If you would like an opportunity to publish your own practical design ideas, achievements, etc., not to a few, but to all of your 25,000 fellow engineer subscribers, be sure to look for us at the show. Our editors will be on hand to meet and talk to you.

> a HAYDEN publication 19 East 62nd Street • New York 21, N.Y.

Ideas for Design

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they deliver a difference current which increase excitation. The magnetic-amplifier receives It's cal power from the 60-cycle output of the main genera tor and delivers its rectified output to the stationard sitive down field of the exciter. The regulator is frequency com pensated to hold voltage within ± 2 per cent with e Signa engine speed changes of ± 5 per cent. from 0.2

decrease generator excitation. Below this voltage

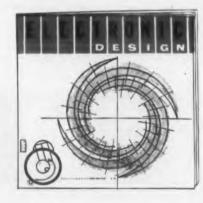
In order to provide fast response and ample e violet to frared v citation current for motor starting loads and fo ity at 2.2 short-circuit relay tripping conditions, the excita tion system is strengthened by using current trans • They plex ar formers in the output of the main generator. Whe mosaics. load or fault current flows from the main generate e Signa the current back through a three phase rectifie • Vibro bridge directly to the stationary field winding of the ac exciter. Thus on motor starting loads or unde • Eleme fault conditions, which are low power factor d To get mands, the current transformers maintain excitation at a value which will sustain the generator voltage This arrangement insures that there will be su EAST ficient current flow under fault conditions to tri Roches the circuit breakers. A schematic wiring diagram of the generator and regulating system is shown i Fig. 3. A. M. Brown, U.S. Naval Civil Engineering Research and Evaluation Lab., Construction Ba talion Center, Port Hueneme, Calif.

New Shock Mounting

Robinson Aviation, Inc. of Teterboro, manufacturers of all-metal vibration and shock mounting systems, recently developed a Met-L-Flex centerof-gravity mounting for a pressure ratio transmitter unit developed by Minneapolis-Honeywell for airborne applications.



ELEC ELECTRONIC DESIGN • July 15, 1957





It's called a Kodak Ektron Detector, the photosensitive substance is lead sulfide, and it can be laid down in any pattern.

 Signal response extends from 0.25 microns in the ultraviolet to 3.5 microns in the infrared with maximum sensitivity at 2.2 microns in the infrared.
 They are available in com-

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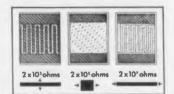
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moraics.



• Signal-to-noise ratio is excellent, particularly in the infrared.

• Vibration doesn't affect them.

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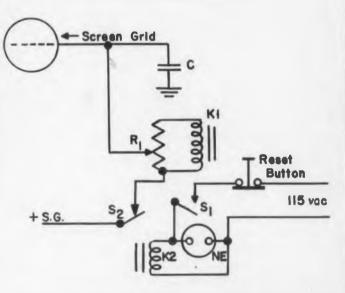
This specialized mounting system shown incorporates pressure and electrical connectors as part of the supporting structure of the mounting. It provides for ease of installation and in effect combines the equipment and mounting into an integral package.

Constructed of aluminum and steel throughout, the lightweight mounting system is a permanent type mounting unaffected by adverse operating conditions. The incorporation of Met-L-Flex resilient elements, located in the plane of the center-ofgravity, provides Model 1323 with environmental tolerance from vibration and shock, thereby insuring equipment reliability.

The high percentage of inherent damping displayed by the mounting system results in the reduction of resonant peaks and the quick dissipation of transient forces. The natural freqency of Model 1323 is between 6 to 11 cps while the amount of vibration provided is approximately 90 per cent at 40 cps. Designed in accordance with military specifications MIL-E-5272A, MIL-C-5541 and QQ-P-416, this mounting system is readily adaptable to military applications.

Tube Protection Scheme

A solution is given here to the problem of finding a reliable method of protecting the screen grids of high-power beam tetrodes and pentodes in event of bias, excitation or plate supply failure.



A very sensitive relay (k_1) of 10,000 ohms is used. When I_{sg} exceeds a predetermined value, the voltage drop across R_1 pulls in the relay K_1 . S_2 closes, energizing K_2 , which opens S_2 . K_2 has a holding contact which prevents reapplication of screen voltage until the reset button is pushed, again closing S_2 . The neon lamp across the coil of K_3 gives visual indication of the overload. Stephen J. Goch, Director Research, G & G Electronics Labs., 1062 Virginia Ave., Bronx 72, N.Y.



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Report Briefs

Traveling Wave Tubes

Two-helix and three-helix backward-wave amplifiers of the cascade type were studied, and the latter found to have a higher gain-bandwidth product. An experimental model of a two-helix mixer in which one helix is a backward-wave amplifier and the other a backward-wave oscillator gave conversion efficiencies up to 0.57, and it is believed that the design could now be improved. Interaction between several space harmonics, originally believed to be orthogonal, was observed on the multi-helix tubes, and several studies were conducted to determine the source of the interaction. A velocity and current analyzer for the backward-wave tubes was also designed. Several studies in crossed-field tubes are described, including measurements on a forward-wave amplifier using a zig-zag slow-wave structure, and the design of a two-circuit backward-wave crossedfield tube. Several gun studies, especially on guns of the shielded type, were made. Electrostatic focusing of electron beams was studied analytically and experimentally, and attempts were made to combine rf interaction with an electrostatically focused beam. Analyses of the noise problem and the largesignal problem are discussed. Experiments were made on several novel high-density emitters, including a metallic arc, a Phillips ion gage discharge, and a shielded field emitter. PB 123983 Traveling Wave Tubes and Related Studies, David H. Sloan, John R. Whinnery and John R. Woodyard, California Univ. Order from Library of Congress, Photoduplication Service, Publications Board Project, Washington 25, D. C. Dec. 1955, 26 pp. Microfilm \$2.70. photocopy \$4.80.

Low Frequency Propagation

Study of Loran signals showed that E-layer fading rates are not always the same as those in the Dlayer. Wide band multichannel equipment for the study of various kinds of atmospherics was designed and constructed. An improved intervalometer was constructed. From whistler data obtained in Seattle and Stanford during 1951 and 1952, it was found that approximately 22 per cent of the whistlers that occurred at either location were received at both locations. This result provides support for Storey's theory of whistlers. Simultaneous whistler observations made at Stanford and on the U.S.S. Atka of the Navy Antarctic Expedition in Dec. 1954 were analyzed. PB 122359 Low Frequency Propagation Studies, Robert A. Helliwell, Stanford University, Radio Propagation Lab., Stanford, Calif., Library of Congress, Washington 25, D.C. Sept 1955, 61 pp. Microfilm \$3.90, photostat \$10.80.



Type M1000. shown actual size

Contacts in this tiny, sealed unit are $\frac{1}{6}$ " solid silver or palladium, handling up to 3 amperes. Use of a permanent magnet in the magnetic circuit gives exceptional efficiency. Units available in production quantities, with solder lugs or printed circuit leads ... for polarized or non-polarized operation. Immediate sample delivery. Write for literature.

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ELECTRONIC DESIGN • July 15, 1957

957

Anisotropic Particle Lattice

The dielectric properties of lattices composed of identical metallic or dielectric elements of various geometries, such as spheres, discs and strips have been investigated from a molecular point of view. The main objective of this note is to extend the treatment to general uniform lattice structures made of identically shaped and oriented particles of general constitutive characteristics. Thus, it includes the most general case of a uniform lattice with structural anisotropy and both element isotropy and anisotropy at the lattice points. PB 124171 Dielectric Properties of a Lattice of Anisotropic Particles, Zohrab A. Kaprielian, California Institute of Technology, Electrical Engineering Dept., Library of Congress, Washington 25, D.C. June 1955, 29 pp. Microfilm \$2.70, photostat \$4.80.

Radome Design

This report presents a general discussion of the design information which has been gathered by investigators and fabricators in developing various sizes and modular configurations of rigid radomes. The design information which is included pertains to the aerodynamic, structural, and thermodynamic analyses. Test data are given concerning climatic studies, wind-simulated loading tests, transmission tests, and installation tests. A discussion is also included on the parameters and problems involved in material selection and fabrication procedures. The applicability of the collected design and test data to Air Force requirements is discussed and conclusions and recommendations are presented. PB123976 Design Considerations for Rigid Radomes, J. R. O'Donnell. U. S. Air Force, Air Research and Development Command, Rome Air Development Center, Griffiss Air Force Base, Rome, N.Y., Library of Congress, Washington 25, D.C. June 1956, 73 pp. Microfilm \$4.50, photostat \$12.30.

Low-Power Pulse Transformers

Analysis and design procedures are derived for application to low-power pulse transformers including, in particular, the types expected to be employed in many circuits of the electronic digital computer of Project Whirlwind. Pulse lengths considered are between a twentieth and a quarter usec. Although optimum reproduction of pulse shape is assumed to be a leading requirement, the procedures given are presumably general enough to be extended to applications for which faithful reproduction of input voltage or current waveform is not necessary. PB 124199 Low-Power Pulse Transformer, Thomas F. Wimett, Mass. Institute of Technology, Servomechanisms Lab., Cambridge, Mass., Library of Congress, Washington 25, D.C. Dec 1947, 114 pp. Microfilm \$6.00, photostat \$18.30.



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Report Briefs

Snow Measurement

Intensities of the snow echoes obtained by a zenith-pointing radar from 180 different contributing regions are compared with suitably chosen thresholds. The probability of the intensities exceeding such a threshold and the frequency with which two intensities separated in time straddle it, are used to deduce the autocorrelation coefficients of the signals. The autocorrelation coefficient, after correction for receiver noise, is shown to be the product of three partial coefficients due to the differential settling of the particles, to a uniform wind driving the particles across the beam, and to turbulence. To the extent that differential settling and cross-wind are known, turbulence can be deducted from the measured coefficient of the signal. Considerations based on the theory developed suggest that measurements of turbulence in rain or snow in the horizontal beam of a high-resolution radar at close range should be feasible. Appendix 1: Correlation coefficients of the signal intensity, and of the amplitude components; the Wiener-Khintchine theorem. Appendix 2: Auto correlation coefficients are "multiplicative." PB 124560 Measurement and Calculation of Fluctuations in Radar Echoes from Snow, Walter Hitschfeld and Arnett S. Dennis, Mc-Gill University, MacDonald Physics Lab., "Stormy Weather" Research Group, Montreal, Canada, Library of Congress, Washington 25, D.C. 53 pp. Microfilm \$3.60, photostat \$9.30.

M Type BWO

A field theory of electron beams focused by crossed electric and magnetic fields is given. The theory is basic to the understanding of the small signal behavior of crossed field electron devices. It is applied to explain the slipping stream, or diocotron, effects as a coupling of two surface waves of the electron beam, and to derive the start-oscillation conditions of the M-type backward wave oscillator. It is found that the slipping stream effect can reduce the starting current by an appreciable factor. The results are compared with the thin beam theory which neglects space charge effects. An analysis of a loaded strip transmission line is given, from which a method of representing space harmonic slow wave circuits by a surface admittance boundary condition is obtained. Forward and backward space harmonic interaction may be treated equally well. PB 123973 Field Analysis of the M Type Backward Wave Oscillators, Roy W. Gould, Calif. Institute of Technology, Electron Tube and Microwave Lab., Pasadena, Calif., Library of Congress, Washington 25, D.C. Sept 1955, 108 pp. Microfilm \$5.70, photostat \$16.80.



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Magnetic Amplifiers with Feedback

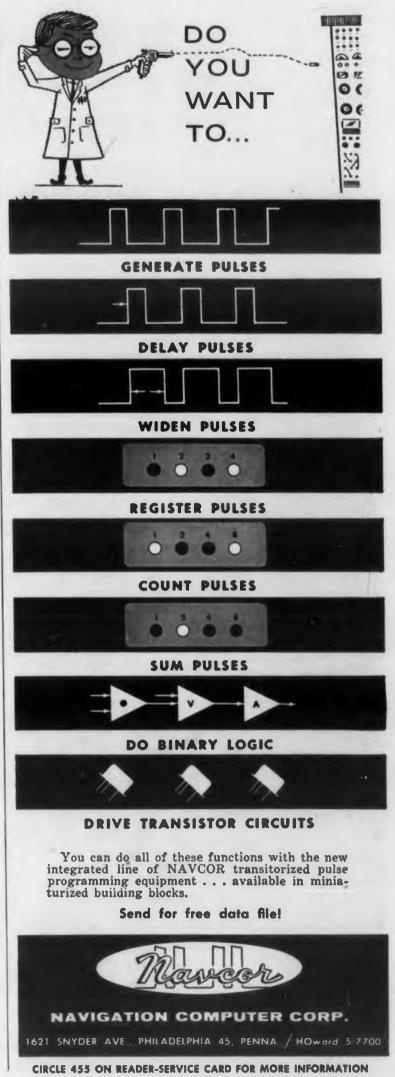
Tests made on magnetic amplifiers excited by a sine-wave carrier were conducted to determine if the figure of merit could be improved by means of feedback techniques. The results are presented schematically and mathematically. In general, the investigations reveal that the power gain of the magnetic-amplifier device can be increased to an unlimited point, but that with this increase a finite rise time remains. Under these conditions the figure of merit, as it is ordinarily defined, becomes meaningless. However, investigations reveal that even under conditions in which feedback techniques are employed, the voltage-gain to magnetic-amplifier rise time ratio remains essentially constant and results in a useful figure of merit. PB 123403 Investigations of Magnetic Amplifiers with Feedback, Remington Rand Univac, Order from Library of Congress, Photoduplication Service, Publications Board Project, Washington 25, D.C. Mar. 1956, 20 pp. Microfilm \$2.40, photocopy \$3.30.

RFI in Communication

A simple method for measuring densitization of receivers caused by radio interference is presented. The use of this method for obtaining true signal to noise ratio measurements at the output of a receiver is discussed. A standard speech test signal is suggested for intelligibility evaluation by means of the concept of articulation index. PB 123076 Evaluation of Interference Effects on Speech Communications, Arthur Gottfried and Kurt Ikrath, U. S. Signal Corps Engineering Labs., Fort Monmouth, N.J., Library of Congress, Washington 25, D.C. Mar 1956, 18 pp. Microfilm \$2.40, photostat \$3.30.

Traveling-wave Tube Theory

Propagation constants have been calculated for a lossy traveling-wave tube by means of a field theory. These results have been applied to the prediction of an attenuator power loss of the order of 2 or 3 db. compared to attenuatorless operation. It is shown that the gain of the higher order modes is negligible. Admittance matching by means of radial admittance transformation is the underlying method used throughout. The Pierce-Fletcher theory in common use at this time is examined in some detail to determine its range of validity. The effects of space charge bunching on saturation has been treated. Criteria have been set for determining whether bunching is important or not in determining saturation. PB 123173 Field theory of travelingwave tubes with application to the study of attenuator saturation effects, William Buchman, California Institute of Technology, Electron Tube and Microwave Laboratory, Pasadena, Calif. LC. Washington 25, D.C. 136 pp. \$21.30.



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| DC Output Voltage (three ranges) | 0-10 0-25 0-50 | 0-10 0-25 0-60 | 0-25 0-50 0-120 |
| Output Current (amps.) | 0-1.5 | 0-5 | 0-2.5 |
| Regulation, line: 105-125 V For wider input | | ±0.5% ±1.0% | ±0.5% ±1% |
| Internal Resistance, typical (ohms) | / | | ~ 70 |
| low-voltage range middle range high range | | 0.35 0.55 1.0 | 1.3 2.0 4.0 |
| | 50 max. | 50 max. | 50 max. |
| (line) (load) | | | |
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Patents

Phase-Shift Oscillator

Patent No. 2,777,952 B. F. Spencer (Assigned to Sperry Rand Corporation)

Phase-shift oscillators as heretofore designed have required more than two phaseshift networks in the plate circuit of the oscillator tube in order to secure the 180 deg phase-shift necessary for sustained oscillations. Oscillators must have enough gain to overcome circuit losses for sustained oscillations. In the usual phase-shift oscillator, the cathode circuit includes a resistor and a condenser of large value in shunt with the resistor with the result that the phase-shift achieved in the cathode circuit is negligible. As a consequence an additional phase-shift network is required in the grid plate circuit to secure the necessary 180 deg phase-shift.

In the phase-shift oscillator shown in the figure, oscillations are secured with two phase-shift networks 17 and 19 in the plate to grid connection. The networks shown are of the L type using capacitors C17 and C19 in series between plate and grid. These two networks secure a phase-shift of sub stantially less than 180 deg. The additional of prophase-shift necessary to achieve 180 de grees of phase-shift is secured from the re- unction actance network K in the cathode to ground ally co circuit. The shunting capacitor C21 has a ance value that provides sufficient phase-shift to electro achieve the 180 deg phase-shift for maintaining sustained oscillations.

It will be noted, therefore, that the phase Paten shift network in the plate-grid circuit pro Vicke vides substantially less than 180 deg phase shift and that the additional phase-shift required is provided by the cathode net work. As a consequence, a reduction in the number of phase-shift networks necessar to secure sustained oscillations is secured In addition, the gain of the circuit for se curing sustained oscillations is reduced to a minimum since circuit losses are less. The circuit described and illustrated has good stability. The patentee illustrates two othe forms of the phase-shift oscillator circuit with results comparable to the results se cured with the circuit illustrated.

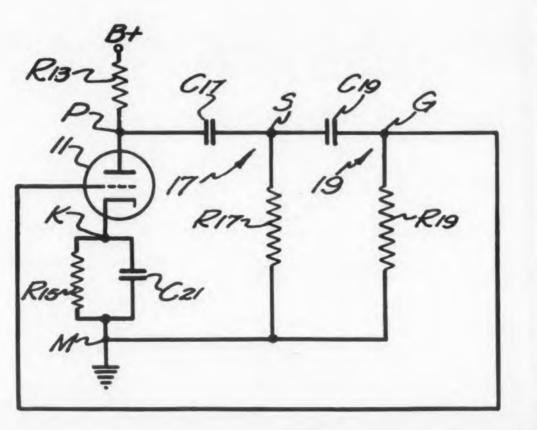
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Semi-Conductor Network

Pateil No. 2,780,752 R. W. Aldrich et al (Assigned to General Electric Company) The network has a semi-conductor provided with spaced electrodes which are predominantly bilaterally conducting. A unction electrode having unilateral conneting properties contacts the semi-conductor in a region which is influenced by f sub potential applied between the spaced biaterally conducting electrodes. A potential tional of proper value is applied between these 0 de naced electrodes. A capacitor connects the he re-function electrode with one of the bilaterround lly conducting electrodes, and an impedhas a nee connects the other of the spaced hift to electrodes and the junction electrode. main.

Self-Saturating Reactor Circuits

phase Patent No. 2,780,772 B. Lee (Assigned to t pro Vickers Incorporated)

chase The magnetic amplifier has the usual ine-shill out and output circuits. A saturable reactor e net has its reactance winding in series with a half-wave rectifier between the input and essan output circuits for self-saturation. A second eured reactor winding connects with a source of alternating control current. A shunt circuit is provided across the second winding. The circuit includes a second half-wave rectifier so that induced current flow in the second winding flows in a direction to generate magnetic effects in the reactor which are oppositely related to the magnetic effects produced by current flow through the first rectifier.

UHF Signal Generation

Patent No. 2,777,062. R. J. Hannon. (Assigned to Standard Coil Products Co., Inc.)

The high frequency oscillator of the patent uses an electron tube having a plurality of electrodes. The effective inductance of certain of the leads to the electrodes is resonated by means connected between the plate and the grid terminals of the tube in order to establish the frequency of oscillation. Compensation is provided for the effective inductance of the other electrode leads, as well as a parallel non-resonant LC circuit in series with the compensating circuit element for providing a high frequency output signal. This series circuit is between the plate terminal of the tube and ground.





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Patents

Switching System

Patent No. 2,782,303 E. A. Goldberg (Assigned to Radio Corporation of America)

Electronic switching circuits employing semi-conductor materials are coming into increasing use since they require no filament supply and the overall circuit is simplified. The semiconductor materials are particularly desirable when there is no need for amplification of the switched signals. Switching circuits, as presently designed, are subject to two difficulties in particular. One difficulty is that of maintaining the level of the signal being switched because of losses arising in overcoming a blocking bias. Another difficulty is that occasioned by the capacity of the wiring which prevents rapid transmission of the switched signal required with electronic equipment.

The circuit in its simplest form is illustrated in the figure. The positive signal to be switched is applied to the input terminal EA and a negative signal is applied to the input terminal EB. The positive signal passes through the diode 30 and resistor 38 under the control of a switching signal which is applied through the diode 50. Upon the application of a positive switching control signal through the diode 50, the cathode 32 of the diode 30 is biased to nonconduction and consequently the input signal is not transmitted. A negative control signal applied through the diode 50 will render the diode 30 conducting and the signal will be transmitted. In similar manner, a positive or negative control switching signal applied through the diode 80 biases the diode 60 to non-conduction or conduction so that the negative signal is blocked or transmitted. swi c the d a n

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Biasing of the diode 30 so that it becomes conducting affects the current flow through the resistor 92 and diode 40 so that the input signal appears at the output terminal 90. Similarly a signal conducted through the diode 60 affects the current flow through the resistor 92 and diode 70 and results in the negative signal appearing at the output terminal 90. With the circuit illustrated, the diode power losses in diode 30 and 40 are equal and opposite so that the two losses compensate for each other. The output signal appearing at the terminal 90 is of the same value as the input signal being



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switched or transmitted. The connection of the diodes through resistors 38 and 68 with a n gative source of potential permits any potentials occurring as a consequence of capacitive effect of the connections to leak off and enables a high speed switching operation to be secured with the circuit.

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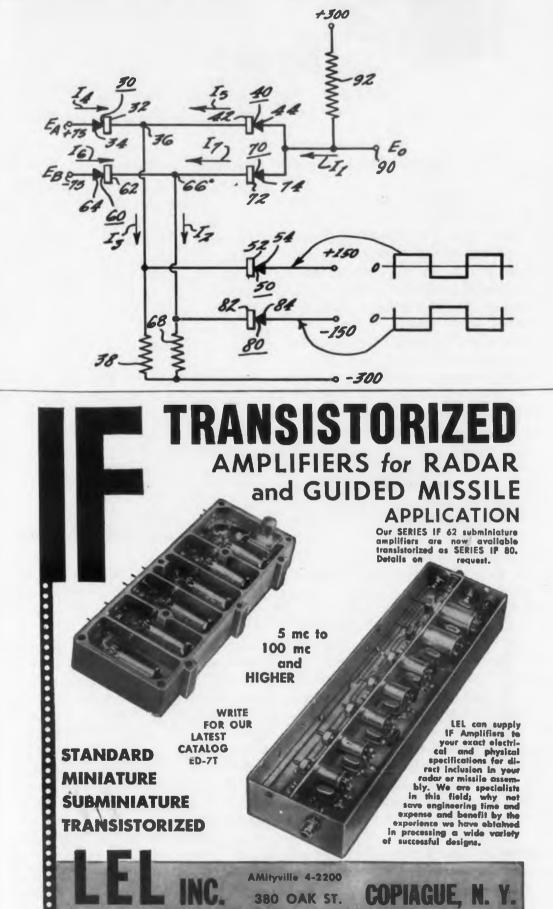
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There are two other forms of the circuit illustrated and described in the patent. In one circuit the resistor 92 is replaced by a vacuum tube and the resistors 38 and 68 also may be replaced by vacuum tubes. The other modified circuit is a refinement of the circuit illustrated herein.



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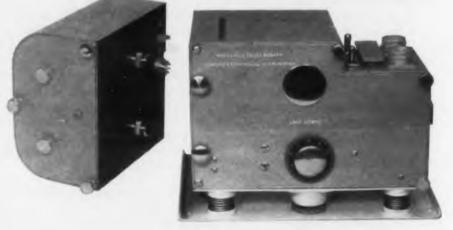
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Annual Report 1956, National Bureau of Standards.

U. S. Dept. of Commerce, Washington 25, D.C., 15 pages, \$.60.

The National Bureau of Standards Annual Report on its research and development activities in the physical sciences contains brief descriptions of the accomplishments in each area of the Bureau's responsibilities. Such subjects as the maintenance of basic standards, determination of physical constants and properties of matter, development of methods and instruments of measurement, and the provision of calibration, testing and scientific advisory services are covered.

During the past year, significant results were achieved in programs dealing with electronic computers, electronic instrumentation and the properties of matter and materials. Development work was successfully completed on a micro-image data storage and retrieval device which provides rapid access to any one of 10,000 microfilmed images located on a 10 in. square sheet of film.

The Bureau also developed a technique for capturing and storing large numbers of free radicals—highly reactive molecular fragments—at temperatures near absolute zero. In the field of optics and metrology, the Bureau completed a comprehensive dictionary of color names, which lists some 7500 individual color names and defines them in simple accurate terms easily understood by workers in different fields. A study of the effect of crystal orientation of fatigue crack initiation in metal was also completed.

Engineers in foreign countries ordering the publication must send remittances in U. S. exchange and should include an additional 1/4 of the publication price to cover mailing costs.

Semiconductor Abstracts

Battelle Memorial Institute, John Wiley & Sons, Inc., 440 Fourth Ave., New York 16, N. Y. 322 pages, \$10.00.

As with previous issues, the principal source of information for this volume is abstract journals. Some original articles, however, have been reviewed in cases where they add to the completeness of coverage. Numerical results are included in many of the abstracts.

The engineer working in the field of semi-conductors will find these abstracts an excellent directory of the literature released during the past year. They will give him an "even chance" of keeping up with the contributions from the many branches of science which are encompassed by activities in the semiconductor field.

Television Engineering Principles and Practice

Vol. 3-Waveform Generation, S. W. Amos & D. C. Birkinshaw Philosophical Library. 15 East 40 St., New York, N.Y., 226 pages, \$15.00.

A comprehensive survey of modern television principles and practice is compiled in this third volume of the four volume series. The application in television of sinusoidal, rectangular, sawtooth and parabolic waves and the mathematical relationship between them, is described. The text is devoted to the fundamental principles of the circuits commonly used to generate such signals. Treatment of the subject is primarily descriptive and considerably less mathematical than that of the previous volume. Although written primarily for the television engineer the book should prove useful to engineers interested in refreshing their knowledge on the fundamentals of pulse circuitry.

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Digital Computer Programming

D. L. McCracken, John Wiley & Sons, Inc. 440 ourth Ave., New York 16, N. Y. 253 page, \$7.75.

Digital programming is discussed on a practical level. Details involved in actually working with digital computers are presented in a lucid, comprehensive treatment. Many of the problems which are specially troublesome to beginners are discussed in a presentation of basic programming fundamentals.

Coverage is more comprehensive than that provided by instruction manuals for specific computers, yet it is on a more practical level than broad treatments written primarily for non-users of computers. To implement his approach Mr. McCracken has devised a mythical computer combining elements from a number of different models currently on the market. This approach makes the book suitable for study even though a computer might not be available for practice or demonstration. When a specific machine is available, the applicable parts of the book can be read with profit, along with the large portion of text material that is relevant to any machine. Mr. McCracken's book should prove val-

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hing s of uable for people with no previous knowledge of computing who want to know how to prepare detailed "instructions" for a computer, as well as for people whose work is so closely related to computer applications that they need to know what is involved in programming.

Transistor Circuits and Applications

John M. Carroll. McGraw-Hill Book Co., Inc., 330 West 42nd St., New York 36, N.Y., 283 pages, \$7.50.

Articles on transistors and transistor applications have been edited and compiled by Mr. Carroll into a somewhat textbook form. Many of the articles contain typical circuits with component values. The design engineer will find this information useful as background material and for comparison with his own designs and techniques. Military, industrial and home-entertainment transistor circuits are covered in the various articles. Typical transistor operating characteristics, important circuit parameters, transistor types, problems of temperature and gain stabilization, and a large number of typical transistor circuits are also included.



P57 ELECTRONIC DESIGN • July 15, 1957

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CIRCLE 465 ON READER-SERVICE CARD FOR MORE INFORMATION

Russian Transistors

J. George Adashko

Construction features and electrical properties of Russian semiconductor devices are presented in "Parameters and Construction of Russian Transistors" by A. V. Krasilov, (8 pp, 9 figs, 3 tables). The article appeared in *Radiotekhnika i Elektronika*, No. 8, 1956, whose contents were reviewed in *ED*, May 15, 1957. These features are abstracted here in picture caption form. Also presented in the article are three tables giving the salient parameters of Russian point-contact and junction transistors.

The columns marked "80% limits" of Tables 1 and 2 show the limits, in which up to 80 per cent of the transistors of the corresponding types have been issued. The current amplification coefficient, α , is measured at audio frequency. The indices 0.5, 1.5, 5, and 10 in Table 1 indicate that the measurements

were carried out respectively at 0.5, 1.5, 5, and 10 mc. I_c limit of Table 3 indicates the minimum collector current at which the gain, $\beta = \alpha/1 - \alpha$ still exceeds 2 for a given type of transistor.

The tables show that the spread in transistor parameters is quite large. The article claims that one of the reasons for this is the inhomogeneity of the presently used germanium.

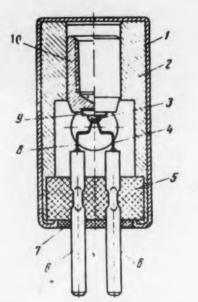


Fig. 1 Construction of point-contact transistor (types C1 and C2). 1—nickel envelope, 2 brass shell, 3—lacquer, 4—emitter, 5—plastic insulator, 6—nickel pin, 7—potting lacquer, 8 collector, 9—germanium base, 10—crystal holder.

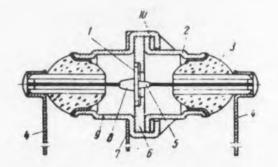


Fig. 3 Construction of junction-type transistor (types P1 and P2). 1—germanium base, 2—shell, 3—glass insulator, 4—terminal, 5—emitter, 6—crystal holder, 7—terminal, 8—collector, 9—shell, 10—lead lining.

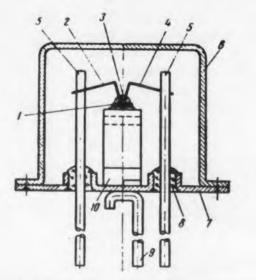


Fig. 2 Construction of hermetic point-contact transistor. 1—germanium base, 2—emitter, 3 lacquer, 4—collector, 5—pin, 6—shell, 7—mount, 8—glass insulator, 9—pin, 10—crystal holder.

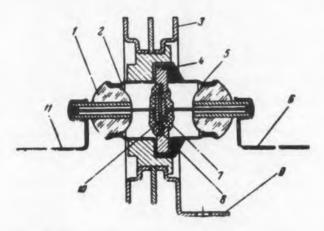


Fig. 5 Construction of P3 junction-type transistor. 1—insulator, 2—shell, 3—radiator, 4—crystal holder, 5--shell, 6—emitter terminal, 7—emitter electrode, 8—germanium crystal, 9—base terminal, 10—collector electrode, 11—collector terminal.

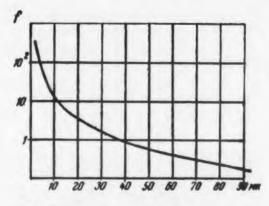


Fig. 4 Dependence of limiting frequency *f* of a junction-type transistor on distance between the emitter and collector.

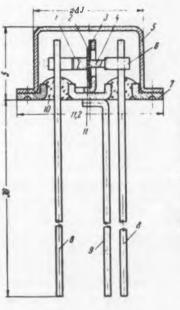


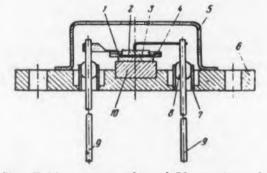
Fig. 6 New construction of P1 transistor. 1—collector, 2—tin ring, 3 nickel crystal holder, 4 emitter, 5—shell, 6 nickel lug, 7—mount, 8, 9—terminals, 10—glass insulator, 11—germanium base.

| | _ | _ | _ | 4 | | | | _ | Par | amet | ers | (grou | nde | ed-ba | | ircui | | with (| t = #2 | 0 2 5 | deg (| | | | | | Measu Condi | tions | | Peak Value | | |
|------|-----------------------------|------------------------------|--|----------------------------------|------------------------|----------------|----------------------------|----------------------------|--------------------|------|-------------|-------|-----|---------------|-------|-----------|----------------|--------|--------|------------|-------|----------------|---------------------|------|---|--------------------------------|--|--|---|---|---|--|
| Туре | _ | R ₁₁ Ohm | | | R ₁₁ Ohm | _ | K | R ₂ | n | | C | | | *0,5 | - | «1, | 5 | | æ s | | E10 | 1 | K.v. | | K _m (power R ₂ = 500 c Rload = 10 | ohm, | le ma. | Ue v. | l _e ma. | I _c ma. | U _c v. | P _c mw |
| TÀbe | norm | 80 lira | | norm | 80 lim | | maon | 80 1im | | norm | 80% limi | | | 80% limite | LIOTM | 80 lin | % nits | norm | | 0% hits | norm | norm | 80 lim | | Not | rm | | | norm | norm | norm | mroa |
| | màx. | min. | max. | max. | min. | max. | mim. | min. | max. | min. | mim. | max. | | min | min. | min. | max. | min. | min. | max. | min. | min. | min. | max. | min. | màx. | | | max. | max. | max. | max. |
| S1A | 750 1500 1500 1500 | 300 350 300 350 | 500 500 500 600 800 900 | 200 200 200 200 1000 | 30 60 50 150 | 120 180 | 7 7 7 7 7 7 | 10 10 10 10 10 | 20 20 20 | 1,5 | 62 | 5 | | .32 | 1. | 21,5 | 32,1 53 | | | 3 1 3,5 | | 50 50 30 1 1 1 | 75 100 50 | 150 | 15 18 | 19 22 19 22 22 | 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0,3 | 20 20 20 20 20 20 10 10 10 10 | +10 +10 +10 +10 +10 +10 +10 +10 +10 | -6 -10 -6 -6 -10 -6 -10 -6 -6 -6 | -40 -40 -40 -40 -30 -20 -20 | 50 100 50 50 50 50 100 50 50 50 50 50 |

Table 1 Summary table of parameters of point-contact transistors

Table 2 Parameters of low-power junction transistors

| - | | | | | | | | | | | | | | | P | A | R | A 1 | ME | T | E | R | S | , | | | | | | Condition | | nt | | rmissible mits | |
|---|------|-------------|--|--|---------------------------------|-----------------------|------|---------------------------|----------------------------------|------|-----------------------------------|--|---------------------------|----------------|----------------------------------|----------------------------------|--------------|------------------------|---|--|--------------|----------------------------------|----------------------------|-------------------|--|--|---------|--|---|--|--|--|----------------|--|--|
| | | | æ. | | | P | Ъ | | | Rc | | | pow | K _m | zain) | | | f _{lin} kc | n | | nois | - | wer | C | | | (Uc) | 10 v.) | Le | Uc | Rgen | Rload | 1 _c | U _c peak | Pc |
| | | _ | | | | | | | | | | | - | db | | _ | | | | | - | в | _ | | | _ | ua | | ma | v. | ohm | tilohm | ma | v. | mw |
| Type | - | ified rm | | % nits | Sp | ec. rm | | 0% mits | Spe | | 80 lim | | Spe | | 809 limi | | Spec Norn | | 80ª limi | | Spec Norn | | | Spec. Norm | | | | | | | | | | | |
| | min. | max. | min. | max. | min. | max. | min. | max. | min. | mæx. | min. | max. | min. | max. | min. | max. | min. | max. | min. | max. | max. | min. | max. | max. | min. | max. | min. | max. | | | | | | | |
| PIA PIB PIV PIG PID PIE PIZ PIZ PII | 0,93 | | 30,9 70,93 70,93 0,96 0,94 0,96 0,96 | 0,9 0,9 0,9 0,9 0,9 0,9 | 7 — 7 — 9 — 9 — 9 — | 400 400 600 | 250 | 400 350 350 1500 | 1000 500 500 300 300 | - | 500 1200 700 1200 300 | 3000 1200 4500 4500 4500 4500 4500 | 33 37 37 33 — | 11111 | 35 38 38 35 33 35 | 42 45 45 45 45 45 | 100 465 | | 150 100 200 200 500 1000 | 400 400 400 400 1000 1600 | 18 | 15 15 15 15 15 15 | 40 40 14 40 40 | - - - 40 | 20 20 20 20 20 20 20 20 | 35 35 35 35 35 35 35 35 | 5555555 | 25 20 15 20 15 25 25 20 20 | 111111111111111111111111111111111111111 | $\begin{vmatrix} -10 \\ -1$ | 600 600 600 600 600 600 600 600 | 30 30 30 30 30 30 30 30 30 30 30 | 5555555 | 20 20 20 20 20 20 20 20 20 20 | 50 50 50 50 50 50 50 50 50 |



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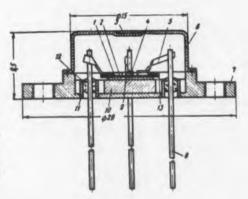
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Fig. 7 New construction of P3 transistor. 1germanium base, 2-emitter, 3-collector, 4base, 5-shell, 6-mount, 7-cover sleeve, 8glass insulator, 9-terminal, 10-copper disc.

Fig. 8. New construction of P2 transistor. 1-germanium base, 2-emitter, 3-sealing (hermetic) lining, 4central base, 5-nickel lug, 6-shell, 7-mount, 8-terminal, 9-collector, 10-copper disc, 11-cover sleeve, 12-glass insulator, 13-annular base.

Table 3 Parameters of high-power junction transistors

| | 1 - | | | 1, | 0 | | _ | | | | | | |
|---------|---------------|-----------------------|--------------|--------|--------|----------------------|----------|-------------|-------|----------|----------------------|----------------|--------|
| Plane a | Pout Watte | Km | Ic lim. | ma. | ma. | | T | est Condit | ions | | Limi | ting Values | |
| Туре | min. | (power gain) db | (β=2). ma | -10 v. | -50 v. | I _c ma | Uc v. | Rgen ohm | Rload | f cps | l _c ma | U _c | Pdiss. |
| P2A | 0,1 | > 17 | - | 0,03 | 0,2 | 5 | 50 | 100 | 10000 | 1000 | 10 | 100 | 0,250 |
| P2B | 0,1 | > 17 | - | 0,03 | 0,2 | 10 | 25 | 25 | 4000 | 1000 | 15 | 50 | 0,25 |
| P3A | 1 1 | 17-20 | · 150 | - | - | 130 | 25 | 5 | 220 | 1000 | 150 | 50 | 3,5 |
| PJB | 1 1 | 20-25 | 250 | 0,25 | 5 | 130 | 25 | 5 | 220 | 1000 | 250 | 50 | 3,5 |
| P3V | 1 1 | 25 30 | 450 | 0,25 | 3 | 130 | 25 | 5 | 220 | 1000 | 450 | 50 | 3,5 |
| P4 | 10 | 13-20 | 1500 | 0,5 | - 1 | 1000 | 26 | 3 | 85 | 1000 | 2000 | 55 | 30 |



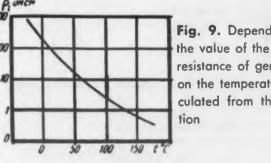


Fig. 9. Dependence of the value of the intrinsic resistance of germanium on the temperature, calculated from the equa-

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What the Russians Are Writing

J. George Adashko

RADIO ENGINEERING AND ELECTRONICS

(Contents of Radiotekhnika i Elektronika No. 11, 1956) TRANSISTOR CIRCUITS

HF Transistor RC Oscillator, L. N. Kaptsov, (6 pp, 5 figs, 2 tables).

A grounded-base point-contact transistor amplifier with greater than unity gain may have negative input and output resistances and may serve as a relaxation or harmonic oscillator. Such a circuit, (essentially a multivibrator,) is analyzed in this article on the basis of the equivalent circuit of Fig. 2 over a range of frequencies comparable with the critical current-gain frequency. Fig. 3 shows the frequency and amplitude dependance on emitter current for several transistors.

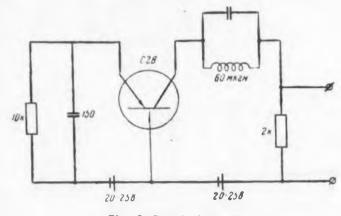
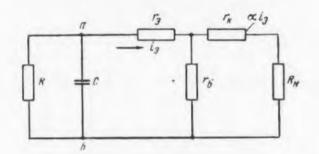


Fig. 1. Practical circuit of RC-oscillator using a type C2B transistor.





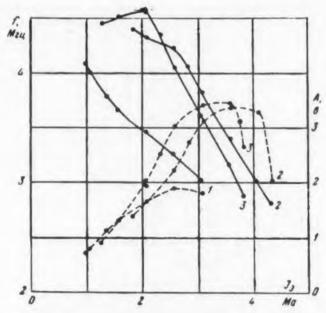


Fig. 3. Plots of frequency (solid) and output amplitude (dotted) vs. emitter current. Curves 1 and 2 are for two C2B transistors, Curve 3 is for the non-standard No. 577 transistor.

Voltage Gain of Tuned Point-Contact Transistor Amplifiers, E. F. Vorob'eva, (12 pp, 9 figs, 2 tables).

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This is a simple approximate calculation applicable to common-base transistors, taking into consideration the effect of the frequency dependence of the transistor parameters and of the internal feedback on the resonant voltage gain. The analysis of the equivalent circuit leads to a set of gain vs. frequency curves for various degrees of mismatch at the input. Experimental verification of the analytical results is cited.

Study of Transients of a Triggering Circuit Using Point-Contact Transistors and Shaping of Pulses from a Sinusoidal Voltage, V. A. Kuz'min, (7 pp, 8 figs).

The study begins with the computation of the duration of the leading edge of the ouput pulse in response to an arbitrary input voltage. This is followed by computation of the part of the trailing edge of the output pulse that corresponds to the transition through the active region under the influence of the negative voltage drop. Shaping of sinusoidal voltages into pulses with the proposed trigger system is then studied. The amplitude, duty cycle, and duration of the forward front of the output pulses are calculated, and the circuit parameters are evaluated. The analysis is checked experimentally. Refers to A. W. Lo, "Transistor Trigger Circuits," Proc. IRE, 1952, 40, 11, 1531, and Lebow and Baker, "The Transient Response of Transistor Trigger Circuits," Proc. IRE, 1954, 42m 6, 938.

T W OSCILLATORS

generation of Electromagnetic Oscillations by Travling Nave Tubes with Double-Spiral Coaxial Lines, 5. Mikhalevski, A. G. Dolganov, V. D. Ivanova, 11 pp, 13 flgs).

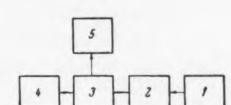
A theoretical treatment of the dispersion properies of the double-spiral coaxial line was reported v V. S. Mikhalevski in the October 1956 issue of adic ekhnika i Elektronika (ED June 15, 1956). the present article gives extensive experimental reults on the effects of the geometry, winding direcion, winding connections, and operating modes on he performance of the traveling-wave tube as an scillator.

MEASUREMENT

Waveguide Methods for High-Temperature Measarement of Dielectric Properties of Materials, V. I. Aksenov, M. Ia. Borodin (9 pp, 6 figs).

The open-circuit method is used to determine the dielectric properties of materials at a wavelength of 3.2 cm in the 20-200° range. Equations are derived for ε' and ε'' ($\varepsilon^{\bullet} = \varepsilon' - j\varepsilon''$) and the temperature dependence of ε' and tan δ of several polymers s obtained from the measurements and these equa-

Fig. 4 shows the block diagram of the test setup, while Fig. 5 shows a waveguide section used in the neasurement.



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Fig. 4. Block diagram of test setup. 1-oscillator, 2-decoupling attenuator, 3-slotted line, 4-electricallyheated waveguide section, 5-amplifier.

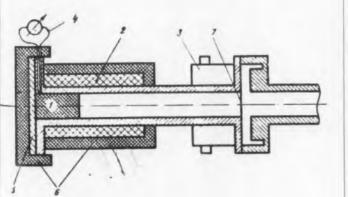


Fig. 5. Waveguide section. 1—specimen of dielectric, 2-electric heating coil, 3cooling jacket, 4-thermocouple, 5-shortcircuiting plate, 6-thermal insulation, 7styroflex film.



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Russian Translations RADIO ENGINEERING AND ELECTRONICS, Cont.

New Measurement Method for the Parameters of Magnetized Ferrites at Centimeter Waves, V. N. Vasil'ev, (17 pp, 14 figs).

A ferrite specimen in the form of a slab is inserted in the center section of a rectangular cavity. The mode and direction of the constant magnetic field are varied to make the resonant frequency and the Q of the cavity depend only on one or two unknown parameters (such as the complex dielectric constant or the permeability tensor), which are then calculated from the changes in the frequency in the resonator Q.

The method is applicable in the 0.8–20 cm range. The necessary equations are derived and experimental results are given for several ferrites. The real components of the permeability tensor and of the dielectric constant are obtained with an accuracy of 3 per cent. The accuracy of the imaginary components depends on the losses and ranges from 7 to 30 per cent (the accuracy increases with the losses.)

MISCELLANEOUS

Systems with Centrifugal-Electrostatic Electron-Beam Focusing, Z. S. Chernov (7 pp, 11 figs).

Describes a new electrostatic electron-beam shaping and focusing system, with the electrons moving in a spiral orbit within the beam. The new system eliminates many of the shortcomings of the usuallyemployed solenoids or permanent magnets such as high power consumption, heavy and cumbersome magnetic systems, the need for precise tuning, and short life.

Based on the stable motion of electrons in the field of cylindrical capacitor, the Institute of Radio Engineering and Electronics of the USSR Academy of Sciences developed new travelling-wave or doublehelix tubes (called "spiratrons") employing this new system and requiring no magnetic focusing.

Figs. 6 and 7 show two types of electron guns to produce a spiralling electron beam. In Fig. 6 the electron beam is shaped into a ribbon and enters the space between two coaxial cylinders at an angle. The inner cylinder is at a higher potential than the outer one. The electrons leave the cathode with both axial and tangential velocity components, and when the centrifugal force is balanced by the electrostatic field strength, they move in spiral trajectories.

In Fig. 7 an annular cathode is contained between cylindrical focusing electrodes, and a cylindrical anode is placed in front of the cathode. Since all electrodes have spiral cross sections, the electrodes have spiral cross sections, the electron leaving the cathode acquire an initial angular mentum and form a solid tubular beam w th spirajectories upon entering the field of the collindric capacitor.

Two spiratron prototypes are illustrated in F 8 and 9. Experimental data are given on their for ing properties and on their high-frequency behavior

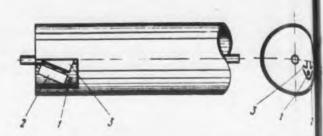


Fig. 6. Centrifugal electrostatic focusing system w flat gun 1—cathode, 2—focusing electrode, 3—and

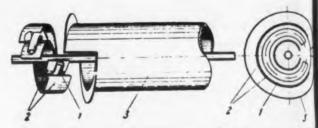


Fig. 7. Centrifugal electrostatic focusing system w spiral gun 1—cathode, 2—focusing electrode, 3 anode.

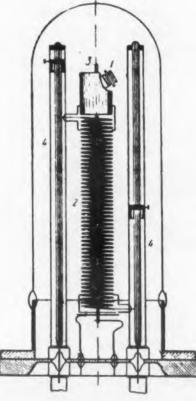


Fig. 8. Demountail construction of trave ling wave type of spiratron (100-300 m 1—electron gun, 2helix, 3— focusin rod, 4—coaxial line

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Automatic, instantaneous, $\pm 1\%$ voltage regulation for 6.3v electronic tube filaments is now available in the output-rating range of up to 25 amperes. For the first time, sizeable banks of these tubes may be served by a single constant voltage transformer. Also, loadings within 75-100% of the transformer's

full load current rating give tube filaments the starting inrush protection afforded by the current limiting effect inherent in Sola design.

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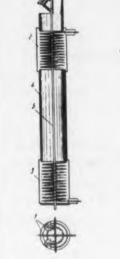


Fig. 9. Construction of double spiral spiratron (tested at 100-300 mc). 1-elecgun, 2-entron trance spiral, 3 exit spiral, 4—drift tube, 5-focusing rod.

Reception of Pulses of Arbitrary Waveform with Super-regenerative Receiver, L. R. lavich, (9 pp, 9 figs).

The principle of superregeneration has been in use for more than 30 years, yet many of its theoretical aspects still remain to be explained. This pertains in particular to non-stationary processes which have lately come into prominence by virtue of the use of superregeneration for pulse reception. The author uses the slowly-varying amplitude method to analyze reception of pulses of any waveform with a superregenerative receiver having a separate heterodyne. It is shown that the pulse area can serve as a criterion of the effectiveness of pulses of different waveforms and durations.

ELECTRICAL COMMUNICATIONS

(Contents of Elektrosviaz' No. 11, 1956)

RADIO RELAY

Type FN-675 Radio Relay Apparatus, N. N. Kamenski, (10 pp, 5 figs).

Description of a French (CSFR) system, capable of handling up to 6 trunks, each accommodating 600 telephone channels or one TV (video plus audio) channel over distances up to 2000-3000 km.

Choice of Standby System of Radio Relay Lines, V. V. Petrov, M. V. Brodski, V. D. Shoshenkov, (9 pp, 4 figs).

Probability-theory aspects of square channels and of automatic switching.

NEGATIVE FEEDBACK

Modulation Negative Feedback in Radio Transmitter Installations, V. A. Khatskelevich, L. M. Shur, (10 pp, 5 figs).

A thorough discussion of the factors that limit the amount of feedback that can be used in transmitter circuits. The rigorous treatment is based on Bode's theories.

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- Curve Tracer
- a-B Meter
- Analyzes Transistors rated up to 100 watts

Russian Translations Electrical Communications (continued)

PULSE SYSTEMS

On the Theory of Linear Pulse Systems with Variable Parameters, G. P. Tartakovski, (12 pp, 2 figs).

Introduces the concept of a time-dependent transfer function of a pulse system with variable parameters. Shows, in analogy with the constant-parameter case, that this function yields the response of the system to any pulse sequence. Treats variable parameters of the linear portion of the system, variable sequence periods, and variable pulse durations. Gives examples of communication systems and elements normally subjected to pulse sequences. Refers to Zadeh's "Frequency Analysis of Variable Networks," Proc. IRE 38, No. 3, 1950, and "Time-Dependent Heaviside Operators," J. Math. & Phys. vol. 30, No. 2, 1951.

INTERFERENCE

Prevention of Interference in Steel Conductors from Other Steel Conductors or from Toll Lines, P. K. Akul'shin, (8 pp, 1 fig).

Continuation of work by the same author, reported in the January and April 1956 issues of Elektrosviaz' (*ED* May 15, and November 1, 1956).

MISCELLANEOUS

"Calculation of Errors Introduced by Speed Differences in Telegraph Start-Stop Apparatus," N. B. Zeliger, (13 pp, 8 figs, 1 table).

"Conditions under which Communication Aerial and Cable Lines can Parallel High-Voltage DC Transmission Lines," M. I. Mikhailov, K. K. Nikol'ski, (11 pp, 10 figs). (The Russians are planning power transmission at 400-800 kvdc. The inductive interference of the dc ripple with low frequency communication lines is therefore of more than theoretical interest.)

"Concerning the Mechanism of Communication-Line Loss under Icing Conditions," I. M. Metter, (2 pp, 2 tables).

AUTOMATION AND TELEMECHANICS

(Contents of Avtomatika i Telemekhanika No. 12, 1956)

SERVO SYSTEMS

Investigation of the Steady State of Pulse Servo Systems, Ia. Z. Tsypkin, (13 pp, 10 figs).

Pulse servo systems are frequently used to convert discrete (digital) data into a continuous (analog)



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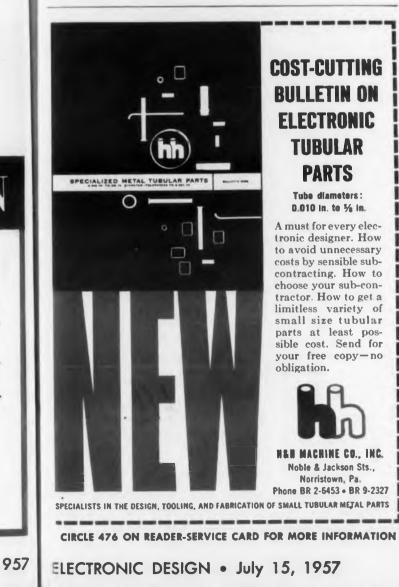
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function, i.e., to interpolate between adjacent discrete values. To minimize the steady-state error it is necessary to improve on the customary straight-line interpolation, using suitable interpolating functions or polynomials (see Porter, Stoneman, and Lowden, "A New Approach to the Design of Pulse-Monitored Servosystems," Proc. IRE, part II, vol 97, 1950). The author gives an analytic expression for the steadystate error and discusses the transfer functions of a simple suitable system.

On the Theory of Nonlinear Solution Elements Employing Piecewise-Linear Approximation, B. Ia. Kogan, (11 pp, 7 figs).

Diode functional converters, described in an article by Talantsev in the February 1956 issue of Avtomatika i Telemekhanika (ED August 1, 1956) are used in conjunction with a solution (operational) amplifier to approximate a variety of nonlinear functions. The article derives some fundamental relationships for a solution amplifier employing stepwise-linearized nonlinear conductances. The relationships obtained between the slope of the original non-linear function and the slopes of the current curves of diode networks connected both in the amplifier input and in the external feedback loop. Several methods of synthesizing functional converters employing diodes are given.

The methods given make it possible to reduce the errors inherent in the functional converter and make it possible to reproduce a greater variety of functions. The article also shows how the current characteristics of the diode circuits can be plotted.

MEASUREMENT

Regenerative Measuring Transmitters, L. L. Dekabrun, (9 pp, 12 figs, 1 table).

Regenerative transmitters are vacuum-tube oscillators used to measure, say, small variations in conductivity of semiconductors by determining the change such a semiconductor introduces in the Q of the oscillator tuned circuit. A theoretical analysis of such a circuit is given, and some experimental installations are described. Reference is made to work by Trott (Journal of Scientific Instruments, No. 7, 1952) and Malling (Electronics, April 1953).

Other Articles In This Issue

"Electronic Flow Meter," D. A. Agaikin, A. A. Desova (4 pp, 7 figs). (Description of two types of electromagnetic flow meters for conducting liquids. Refers to several American designs.)

"Coding of Remote-Control Signals by Using Pulse Identification," M. A. Gavrilov, (22 pp. 18 flgs). (Abstract switching theory.)

"Investigation of a Turbine-Drilled Well as an Object of Regulation," Ia. B. Kadymov, (11 pp. 8 figs).

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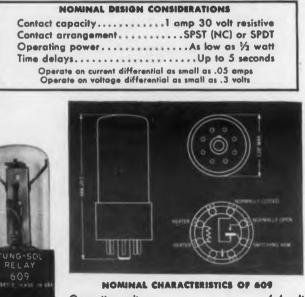
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German Abstract_

Feedback T

THE ADVANTAGES of feedback which are realized with vacuum tube circuits are also achieved in transistor circuits; i.e. stability and flexibility of input and output impedance values are possible. A systematic analysis of four basic resistancefeedback arrangements yield general results which can be of value to the designer.

In Fig. 1, four basic feedback circuits are shown. The calculations are particularly simple if the circuit description of the transistor is selected to suit each type of connection.

```
For Fig. 1a choose

v_1 = r_{11}i_1 + r_{12}i_2

v_2 = r_{21}i_1 + r_{12}i_2

For Fig. 1b choose

i_1 = y_{11}v_1 + y_{12}v_2

i_2 = y_{21}v_1 + y_{22}v_2

For Fig. 1c choose

v_1 = h_{11}i_1 + h_{12}v_2

i_2 = h_{21}i_1 + h_{22}v_2

For Fig. 1d choose

i_1 = g_{11}v_1 + g_{12}i_2

v_2 = g_{21}v_1 + g_{22}v_2

The quantities of interest are the voltage gain, \beta;
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the current gain α ; the input resistance R_e ; and the output resistance R_a . In addition, assuming that the input terminals are fed from a source of resistance R_q and the load resistance is R_L , optimum values of input and output resistance are defined as those values which match source and load resistance respectively. (These optimum values result in maximum power gain.)

The results of the analysis are summarized in Table I. The notation used in this tabulation uses the superscript zero with reference to a quantity with feedback. In addition

 $R_{ek} = input resistance with shorted output terminals$

- $R_{\mbox{\tiny ak}} = \mbox{output}$ resistance with shorted input
- $\alpha_k = current$ gain with shorted output
- $R_{a1} = output resistance with open input$
- $r_o = r_{11} + r_{22} r_{12} r_{21}$, other zero subscripts have analogous meaning.

Graphically these results are presented (qualitatively) in Fig. 2. The various significant ratios of characteristic value with feedback to value without feedback are shown (not on a linear scale) for the emitter connection. (Abstracted from an article by W. Glaser, Nachrichtentechnik, Vol. 7, No. 4, April 1957, pp. 159-162.)

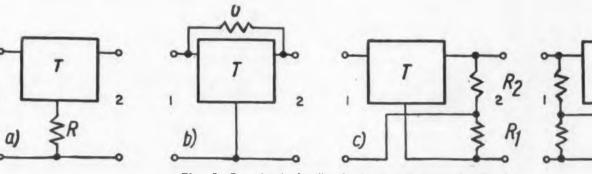


Fig. 1. Four basic feedback circuits: a) Series feedback b) Parallel feedback (G = 1/R) c) Series-Parallel feedback $[R_1 = k(R_1 + R_2)]$ d) Parallel-Series feedback.

| ra | E. Brenner | | | |
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| Fi - | g. la Fig. lb F | Fig tion ters | 2. Varia- of parame- for the dif- ent connections. | |
| | Table 1. Char | racteristic values of the four | types of transistor feedback (| circuits. |
| • | Table 1. Char Fig. 1a | racteristic values of the four Fig. 1b | types of transistor feedback o | fircuits. Fig. 1d |
| a* | Fig. la | | Fig. 1c | |
| | Fig. 1a $\frac{a_k R_{al} - R}{R_L + R_{al} + R}$ | Fig. 1b $\frac{\frac{a}{R_{ek}} - 0}{\frac{1}{R_{ek}} + 0 + R_L \left(\frac{1}{R_{ek}R_{al}} + y_* \theta\right)}$ | Fig. 1c | Fig. 1d $\frac{a_k \frac{R_{a,k}}{R_{e,k}} + k}{\left(\frac{1}{R_{e,l}} + \frac{1}{R}\right)R_L + \frac{R_{a,k}}{R_{e,k}} + kg_e}$ |
| ₿• | Fig. 1a $\frac{a_k R_{al} - R}{R_L + R_{al} + R}$ | Fig. 1b $\frac{\frac{a}{R_{ek}} - G}{\frac{1}{R_{ek}} + G + R_L \left(\frac{1}{R_{ek}R_{al}} + y, G\right)}$ $-\frac{R_L \left(\frac{a_k}{R_{ek}} - G\right)}{1 + R_L \left(\frac{1}{R_{ak}} + G\right)}$ | Fig. 1c $\frac{a_k + k}{1 + \frac{R_L}{R_{al}} + \frac{R_L}{R}}$ $\frac{R_L (a_k + k)}{R_{ak} + R(k - k^a) + R_L \left(\frac{R_{ak}}{R_{ak}} + kh_a\right)}$ | Fig. 1d $\frac{a_k \frac{R_{ak}}{R_{ek}} + k}{\left(\frac{1}{R_{el}} + \frac{1}{R}\right)R_L + \frac{R_{ak}}{R_{ek}} + kg_*}$ $- \frac{R_L \left(a_k \frac{R_{ak}}{R_{ek}} + k\right)}{R_L + R_{ak} + R(k - k^*)}$ |
| β° R_{s}^{0} $R_{s}^{0.2}$ | Fig. 1a $\frac{a_k R_{al} - R}{R_L + R_{al} + R}$ $-\frac{R_L(a_k R_{al} - R)}{R_L(R_{el} + R) + R_{ek} R_{al} + r_e R}$ $\frac{R_L(R_{el} + R) + R_{ek} R_{al} + r_e R}{R_L + R_{al} + R}$ $\frac{R_{el} + R}{R_{al} + R} (R_{ek} R_{al} + r_e R)$ | Fig. 1b $\frac{\frac{a}{R_{ek}} - G}{\frac{1}{R_{ek}} + G + R_L \left(\frac{1}{R_{ek}R_{al}} + y_e G\right)}$ $-\frac{R_L \left(\frac{a_k}{R_{ek}} - G\right)}{1 + R_L \left(\frac{1}{R_{ak}} + G\right)}$ $\frac{1 + R_L \left(\frac{1}{R_{ak}} + G\right)}{\frac{1}{R_{ek}} + G + R_L \left(\frac{1}{R_{ek}R_{al}} + y_e G\right)}$ $\frac{\frac{1}{R_{ek}} + G}{\frac{1}{R_{ek}} + G} \frac{1}{\frac{1}{R_{ek}R_{al}} + y_e G}$ | Fig. 1c $\frac{a_{k}+k}{1+\frac{R_{L}}{R_{al}}+\frac{R_{L}}{R}}$ $\frac{R_{L}(a_{k}+k)}{R_{ak}+R(k-k^{2})+R_{L}\left(\frac{R_{ek}}{R_{ak}}+kh_{e}\right)}$ $\frac{R_{ek}+R(k-k^{2})+R_{L}\left(\frac{R_{ek}}{R_{ak}}+kh_{e}\right)}{1+\frac{R_{L}}{R_{al}}+\frac{R_{L}}{R}}$ $\frac{R_{ek}+R(k-k^{2})+R_{L}\left(\frac{R_{ek}}{R_{ak}}+kh_{e}\right)}{\frac{1+\frac{R_{L}}{R_{al}}+\frac{R_{L}}{R}}{\frac{R_{ek}}{R_{ak}}+kh_{e}\right)}$ | Fig. 1d $\frac{a_k \frac{R_{ak}}{R_{ek}} + k}{\left(\frac{1}{R_{el}} + \frac{1}{R}\right)R_L + \frac{R_{ak}}{R_{ek}} + kg_s}$ $-\frac{R_L \left(a_k \frac{R_{ak}}{R_{ek}} + k\right)}{R_L + R_{ak} + R(k - k^s)}$ $\frac{R_L + R_{ak} + R(k - k^s)}{\left(\frac{1}{R_{el}} + \frac{1}{R}\right)R_L + \frac{R_{ak}}{R_{ek}} + kg_s}$ $\frac{R_{ak} + R(k - k^s)}{\frac{1}{R_{el}} + \frac{1}{R}} \frac{1}{\frac{R_{ak}}{R_{ek}}} + kg_s$ |
| α* β* R ⁰ _e ε opt | Fig. 1a $\frac{a_k R_{al} - R}{R_L + R_{al} + R}$ $-\frac{R_L(a_k R_{al} - R)}{R_L(R_{el} + R) + R_{ek} R_{al} + r_e R}$ $\frac{R_L(R_{el} + R) + R_{ek} R_{al} + r_e R}{R_L + R_{al} + R}$ $\frac{R_{el} + R}{R_{al} + R} (R_{ek} R_{al} + r_e R)$ | Fig. 1b $\frac{\frac{a}{R_{ek}} - G}{\frac{1}{R_{ek}} + G + R_L \left(\frac{1}{R_{ek}R_{al}} + y_e G\right)}$ $-\frac{R_L \left(\frac{a_k}{R_{ek}} - G\right)}{1 + R_L \left(\frac{1}{R_{ak}} + G\right)}$ $\frac{1 + R_L \left(\frac{1}{R_{ak}} + G\right)}{\frac{1}{R_{ek}} + G + R_L \left(\frac{1}{R_{ek}R_{al}} + y_e G\right)}$ $\frac{\frac{1}{R_{ek}} + G}{\frac{1}{R_{ek}} + G} \frac{1}{\frac{1}{R_{ek}R_{al}} + y_e G}$ | Fig. 1c $\frac{a_{k} + k}{1 + \frac{R_{L}}{R_{al}} + \frac{R_{L}}{R}}$ $\frac{R_{L}(a_{k} + k)}{R_{ok} + R(k - k^{a}) + R_{L}\left(\frac{R_{ok}}{R_{ak}} + kh_{o}\right)}$ $\frac{R_{ok} + R(k - k^{a}) + R_{L}\left(\frac{R_{ok}}{R_{ak}} + kh_{o}\right)}{1 + \frac{R_{L}}{R_{al}} + \frac{R_{L}}{R}}$ | Fig. 1d $\frac{a_k \frac{R_{ak}}{R_{ek}} + k}{\left(\frac{1}{R_{el}} + \frac{1}{R}\right)R_L + \frac{R_{ak}}{R_{ek}} + kg_s}$ $-\frac{R_L \left(a_k \frac{R_{ak}}{R_{ek}} + k\right)}{R_L + R_{ak} + R(k - k^s)}$ $\frac{R_L + R_{ak} + R(k - k^s)}{\left(\frac{1}{R_{el}} + \frac{1}{R}\right)R_L + \frac{R_{ak}}{R_{ek}} + kg_s}$ $\frac{R_{ak} + R(k - k^s)}{\frac{1}{R_{el}} + \frac{1}{R}} \frac{1}{\frac{R_{ak}}{R_{ek}}} + kg_s$ |

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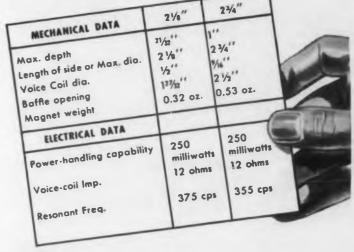
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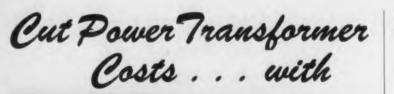
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Standards and Specs

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Connectors

MIL-C-3989, CONNECTORS, COAXIAL, RADIO FRE-QUENCY, AND ASSOCIATED FITTINGS, SERIES C, 14 MARCH 1957

This spec covers weatherproof series C connectors, having a nominal impedance of 50 ohms, and associated fittings. Qualification inspection is not required. Supplement 1 references the following connectors which are part of this spec: Plug UG-709A/U; Receptacle UG-704/U; Plug UG-707A/U; Right-Angle Plug UG-710A/U; Plug UG-707A/U; Plug UG-708A/U; Bulkhead Receptacle UG-706/U; Bulkhead Adapter UG-701/U; and Bulkhead Receptacle UG-705/U.

IEC PUBLICATION 83, STANDARDS FOR PLUGS AND SOCKET OUTLETS FOR DOMESTIC AND SIMILAR GEN-ERAL USE

This 32-page publication gives the dimensions of plugs and outlets for three electrical systems throughout the world. These three systems are: standards approved by ASA and used in Canada and the United States; standards of the British Standards Institution and used in India and the United Kingdom; and standards of the International Commission on the Rules for the Approval of Electrical Equipment and used in Belgium, Denmark, France, Germany, Italy, Japan, The Netherlands, Norway, and Sweden. Copies of this publication may be obtained for \$2.40 from ASA, 70 East 45 Street, New York 17, N.Y.

Resistors

MIL-R-19A, RESISTORS, VARIABLE, WIREBOUND (LOW Operating Temperature), General Specification for, 9 November 1956

Style RA10 has been added. It is a miniature type with a body diameter of 3/4 inch and is rated at 1 watt. Style RA25 has been deleted. The three styles, RA10, RA20, and RA30 are specified on detailed Military Specification Sheets MIL-R-19/1, 2, 3 respectively. Resistance tolerance of $\pm 5\%$ has been deleted, and only a tolerance of $\pm 10\%$ is now specified. Round shafts have been deleted. The number of flatted-shaft lengths has been reduced to one-2 1/2 inches. A moisture resistance test has been added to replace the humidity test. Low-temperature operation, low-temperature storage, acceleration, shock, and high-frequency vibration tests have been added. This spec supersedes JAN-R-19 and Amendment 7 thereto.





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American Standards

American Standards Association has announced that the following standards have been recently released or approved:

ELECTRICAL TERMS, DEFINITIONS OF, GROUP 35, TRANSMISSION AND DISTRIBUTION, C42.35-1957

ELECTRICAL TERMS, DEFINITIONS OF, GROUP 65, COMMUNICATIONS, C42.65-1957

METHODS OF MEASUREMENT OF PULSE QUANTITIES, C16.28-1956

COLOR CODING FOR NUMERICAL VALUES OF COMPO-NENTS FOR ELECTRONIC EQUIPMENT, C83.1-1956

NOMENCLATURE AND DIMENSIONS FOR PANEL MOUNT-ING RACKS, PANELS, AND ASSOCIATED EQUIPMENT, C83.9-1956

REQUIREMENTS FOR RECTANCULAR WAVEGUIDES. C83.10-1956

REQUIREMENTS FOR METAL-ENCASED FIXED PAPER DIELECTRIC CAPACITORS FOR D-C APPLICATION, C83.11-1956

REQUIREMENTS FOR CABLE CONNECTORS FOR AUDIO FACILITIES FOR RADIO BROADCASTING, C83.12-1956 **REQUIREMENTS FOR WIRE-WOUND POWER-TYPE RHE-**OSTATS, C83.13-1956

REQUIREMENTS FOR RIGID COAXIAL TRANSMISSION LINES-50 OHMS, C83.14-1956

REQUIREMENTS FOR ELECTROLYTIC CAPACITORS (FOR USE PRIMARILY IN TRANSMITTERS AND ELECTRONIC INSTRUMENTS), C83.15-1956

Indicators

MIL-L-3661, LAMPHOLDERS AND LIGHTS, INDICATOR; BAYONET BASE, MINIATURE AND CANDELABRA, Amendment 2, 19 March 1957

The type designation letter for jewel lens D now designates plain, polaroid dimmer. A new letter designation M has been added to cover the plain, shutter dimmer type. Requirements for solder-lug wiring terminals have been added. Additional requirements have been established for packaging and metal parts. Three MS sheets have been revised.

RETMA Standards Proposals

The following Standards Proposals are being circulated by RETMA for standardization approval: S.P. 537, MICROWAVE TOWERS

S.P. 538, MECHANICAL CHARACTERISTICS FOR MICRO-WAVE ANTENNAS AND PASSIVE REFLECTORS

S.P. 539, Recommended Practice for Preparation OF OUTLINE DRAWINGS OF ELECTRON TUBES AND BASES (REVISION TO RETMA ET-102-B)

S.P. 540, DESIGNATION SYSTEM FOR CATHODE RAY TUBES (REVISION TO RETMA ET-111-A)



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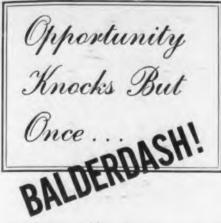
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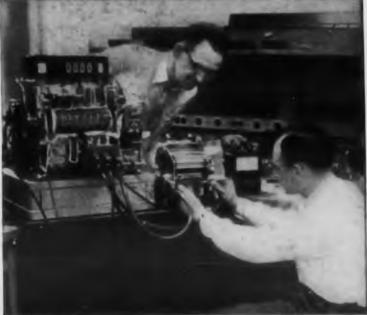
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To conceive, analyze and develop new systems for detecting and neutralizing military targets using electronic techniques available in any part of the electromagnetic spectrum.

Problems in both areas have application from zero velocity of VTOL craft to ballistic and hypersonic glide vehicles and weapons.

Men able to take the holistic approach—and able, as well, to keep practical objectives always in mind—will discover these staff openings offer excellent reward and opportunity for continued professional growth with the creators of the XF-103 and the F-105B Thunderchief...most powerful supersonic fighterbomber—designed and built under the Weapons System Concept. Graduate engineers with various ranges of experience will find work levels commensurate with training and ability.

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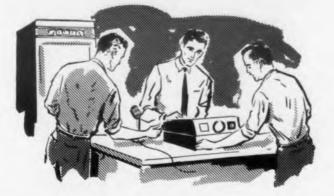
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- V Our electronics engineering staff has grown 12 times since 1953!

OUR FUTURE:

OUR PRESENT:

- ✓ Continued rapid, orderly growth, with increasing opportunities for engineers.
- If you want to link your future with ours
- and grow with us, here's a check list for you! \checkmark Name, address, home telephone number
- V College, degree
- Electronics experience
- / Other experience
- / Preferred field of work

CIRCLE 553 ON READER-SERVICE CARD FOR MORE INFORMATION

- Sales Engineering
 - Systems Test Equipment
 - Transistor Engineering
 - Writers—Technical

15, 1957

- Communication Systems
- Components and Specifications
- Countermeasures
- Data Systems
- Digital Techniques
- Field Engineering
- Infrared
- Mechanical Design
- Microwave Circuits
- Missile Guidance
 Systems
- Radar
- Sonar

NEW ELECTRONIC GALVANO



Sensitive - Rugged - Versatile

Functionally equivalent to suspension galvanometers, but with far greater versatility, the Model 204A is the ultimate for DC null detection in low level bridge and potentiometer circuits. KIN TEL's chopper stabilized, all transistor design provides extreme sensitivity and rugged durability superior to conventional moving coil or electronic galvanometers.

Immune to overload and shock, the current sensitivity of the Model 204A is 20 times greater than the sensitivity of high quality, mechanical current galvanometers. As a voltage galvanometer, the extremely high power sensi-tivity of the Model 204A makes it superior to low impedance moving coil instruments. This reliable, general purpose unit is ideal for use as a direct reading indicator for strain gage thermocouple and other current or voltage measurements in industry or laboratory. The 204A's simplicity of operation makes it the key to efficient production line testing. Its unequalled stability makes it ideal for low level DC amplification to extend the range of recording and other measurement instruments.

Representatives in all major cities.



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(KAY LAB)

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| ANOMETER dc null detector | Gee Lar Mfg. Co.156PiGeneral Chemical Div. Allied Chemical & Dye Corp.90General Ceramics Corp.78General Electric Co., Apparatus Sales Dept.134General Electric Co., Industry Control Dept.63General Electric Co., Industry Control Dept.63General Electric Co., Light Military Div.165General Radio Co.139General Transformer Co.160RGeneral Transformer Co.Globe Industries, Inc.99R. Gudebrod Bros. Silk Co.108Gudeman Co., The111R. Gulton Industries114 |
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| micro-microammeter | H & H Machine Co 157 Harrison Laboratories, Inc |
| microvolt level dc amplifier microvoltmeter | Hart Manufacturing Co.157FillHaydon, A. W. Co., Inc.129Heinemann Electric Co.54Heminway & Bartlett Mfg. Co.141Hermetic Seal Products Co.146Hewlett-Packard Co.171Sa171HiTemp Wire, Inc.121Sa65, Insert XVIIHycon Eastern, Inc.92SiInsuline Corp. of AmericaInternational Resistance Co.2 |
| A dozen good reasons why KIN TEL's Electro-Galvo solves your low- level dc measurement problems | J-V-M Engineering Co. 102 Johnson, E. F. Co. 104 Joy Mfg. Co. 104 S 104 Kay Lab (see Kin Tel) S |
| 1 20 Micro Microamps Per Division Sensitivity 2 ± 10 Microvolts to 10 Volts or ± | Kearfott Co., Inc. Little Falls Div. 134 S Kearfott Co., Inc. Western Div. 131 S Keithley Instrument Co. 136 S Kester Solder Co. 161 S Kin Tel ((Formerly Kay Lab) 113, 170 S Koiled Kords, Inc. 28 S Kulka Electric Mfg. Co. 139 S |
| 0.001 Microamp to 1 Milliamp Full Scale Sensitivity 3 Withstands Extreme Overload with No Zero Offset | L E L, Inc |
| ⁴ Transistorized — Rugged — Insensitive to Shock, Microphonics, Position ⁵ Floating Input ⁶ 7 Voltage or Current Ranges ⁷ 10,000 Ohm Input Resistance ⁸ 10⁻¹⁴ Watts Full Scale Power Sensitive | Magnetics, Inc. Components Div.89Makepeace, D. E. Co.83Mallory, P. R. & Co.106Mansol Ceramics Co.157Marconi Instrument Co.125Mica Insulator Co.56Microtran Co.146Millivac Instrument Corp.42Minneapolis-Honeywell Regulator Co., Industrial Div.95Minneapolis-Honeywell Regulator Co., Transistor Div.112Motorola, Inc.168Motorola, Semi-Conductor ProductsInsert XXIIIMotorola, Western Military Electronics Div.167 |
| tivity 9 Equivalent Built-in Ayrton Shunt — No Accessories to Buy 10 Use as Stable DC Amplifier with 1 Volt | NJE Corp.101National Cash Register Co.163National Vulcanized Fibre Co.71Natvar Corp.35Navigation Computer Corp.143Norden-Ketay Co.55 |
| at 1 ma Output 11 Less than 2 Microvolts Drift | Oak Mfg. Co. 68 Ohmite Mfg. Co. 67 Oster, John Mfg. Co. 93 |
| 12 Less than 1 Microvolt P-P Noise Model 204A Price \$325.00 | Pacific Semi-Conductors, Inc. Insert XIII Perkin-Elmer Corp., Vernistat Div. 100 Phaostron Co. 129 Phelps Dodge Copper Products 27 Philco Corp., Lansdale Tube Div. 86, Insert V Philbrick Researchers, George A 127 |
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| Px echnic Research & Development Co. Pc r & Brumfield Pr ier Metal Products Co. Px National Co., The | |
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| R a Condenser Co R > Corp. of America R > Corp. of America, Components Div R - Industries, Inc. R - Wooldridge Corp. R - Heon Mfg. Co., Industrial Div. R - theon Mfg. Co., Personnel R theon Mfg. Co., Semi-Conductor Div Reves Instrument Corp. - E ungton Rand, Inc. Univac Rentwandt, Inc. - Republic Aviation Corp. - Recem Mfg. Co. - Rheem Mfg. Co. - Retorn Mfg. Co. - Republic Aviation Corp. - Retorn Mfg. Co. - </td <td>12, 172 130, 159 130, 159 130, 159 165 165 Insert XXII 164, 166 4 88 162 157 164 110 87 122</td> | 12, 172 130, 159 130, 159 130, 159 165 165 Insert XXII 164, 166 4 88 162 157 164 110 87 122 |
| Safeway Heat Elements, Inc. Sanborn Co. Servæ-Tek Products Co., Inc. Simpson Electric Co. Sola Electric Co. Southern Screw Co. Southern Screw Co. Southern Div., South Chester Corp. Speer-Carbon Co., Jeffers Electronic Div Sprague Electric Co. Stackpole Carbon Co., Electronic Compo Standard Pressed Steel Co. Statkam Development Corp. Statham Laboratories, Inc. Stavid Engineering Steafix Stewart Warner Electronics Stromberg-Carlson Co. Stuttevant, Co., P. A. Superior Tube Co. Sylvania Electric Products, Parts Div. | 38 137 62 155 144 105 77 136 61, 80 nents Div. 16, 17 141 142 118 135 167 149 166 169 154 143 20 |
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| Waters Mfg. Co. Weckesser Co. West Coast Electrical Mfg. Co. Western Gear Corp.' Westinghouse Electric Corp., Industrial T Westinghouse Electric Corp., Semi-Cond Westinghouse Electric Corp. Westinghouse Electric Corp. Weston Electrical Instrument Co. Wiley & Sons, John, Inc. Wilmad Glass Co. | 140 119 8 'ube Div. 79 ductor Div. 153 84, 97 23 107 |
| 7 °0 Mfg. Co. | |

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LECTRONIC DESIGN • July 15, 1957

SPECIFICATIONS

Sweep Range: 0.02 "sec/cm to 15 sec/cm.

Calibration: 24 sweeps: 1-2-5-10 sequence, 0.1 µsec/cm to 5 sec/cm. 3% accuracy.

Triggering: Internal, line voltage or external 0.5 v or more. Pos. or neg. slope, -30 to -30 v trigger range.

Preset Trigger: Optimum setting for automatic stable triggering.

Horizontal Amplifier: Sweep magnification 5, 10, 50, 100 times. Vernier position control selects any 10 cm⁺part of sweep. External input pass band dc to over 500 KC. Sensitivity 200 niv/cm to 15 v/cm.

Vertical Amplifier: Fass band dc to 10 MC Optimum transient response and rise time less than 0.035 usec. Signal delay of 0.25 usec permits leading edge of triggering signal to be viewed

Amplitude Calibration: 18 calib. voltages, 1-2-5-10 sequence, 0.2 mv to 100 v peak-topeak. Accuracy-3%, Approx. 1 KC square wave, rise and decay approx. 1.0 usec.

Prices: -hp- 150A High Frequency Oscilloscope, \$1,100.00 -hp- 151A High Gain Amplifier, \$200.00 -hp- 152A Dual Channel Amplifier, \$250.00

-hp- 150A HIGH FREQUENCY OSCILLOSCOPE

New reliability • New convenience DC to 10 MC. Plug-in preamplifiers 24 direct reading sweep times Sweeps 0.02 µsec/cm to 15 sec/cm "Universal" automatic triggering New, ultra-conservative design

New Model 150A is not a "warmed-over" imitation of previous oscilloscopes. Instead it is a totally new kind of instrument whose radical design approach obsoletes old standards of oscilloscope versatility, simplicity and dependability.

Specifications given here spell out the 150A's unique usefulness. Its simplicity and reliability stem from such unique features as: Unitized circuits, easily isolated for testing or service, etched and mounted on translucent plastic. Highest quality components, operated well below ratings. Concentric, colorcoded, functionally-grouped controls. Direct sweeptime selection; no mental gymnastics. Universal automatic triggering system wherein one preset adjustment provides optimum triggering for almost all conditions.

Wouldn't you prefer a *really new, convenient* oscilloscope? Call your -*hp*- representative today for the complete story. Or, write direct.

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also offers -hp- 130A Low Frequency Oscilloscope, dc to 300 KC, sweeps 1 µsec/cm to 12.5 sec/cm.

CIRCLE 490 ON READER-SERVICE CARD FOR MORE INFORMATION

He "reads" his radar data... IN BRIGHT DAYLIGHT

No hood needed for this presentation, because the RCA-6866 Display Storage Tube pictured here produces an average display brightness of 2750 foot-lamberts —brilliant enough to view directly in bright daylight!

In addition to its application in military electronics, RCA-6866 offers many exclusive features of special interest to equipment designers in the field of electronic data processing. For example, RCA-6866 can present non-flickering display of electronic information—for as long as 60 seconds after writing stops. It can "write" at speeds as high as 300,000 inches per second-fast enough to "freeze" microsecond transients for visual or photographic examination.

Are you working with airplane-cockpit radar-fire-control radar-airport surveillance-transient studies-data transmission, including half-tones-visual communications via narrow-bandwidth transmission? If you are, then don't overlook the unique advantages of the RCA-6866.

Tube Division

Harrison, N. J.

For technical bulletin on the 6866, write RCA, Commercial Engineering, Section G-18-Q-2, Harrison, N. J. For sales information on this and on other RCA display storage tubes now in development...contact the RCA Field Office nearest you.

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