

Electronic Design

FOR ENGINEERS AND ENGINEERING MANAGERS

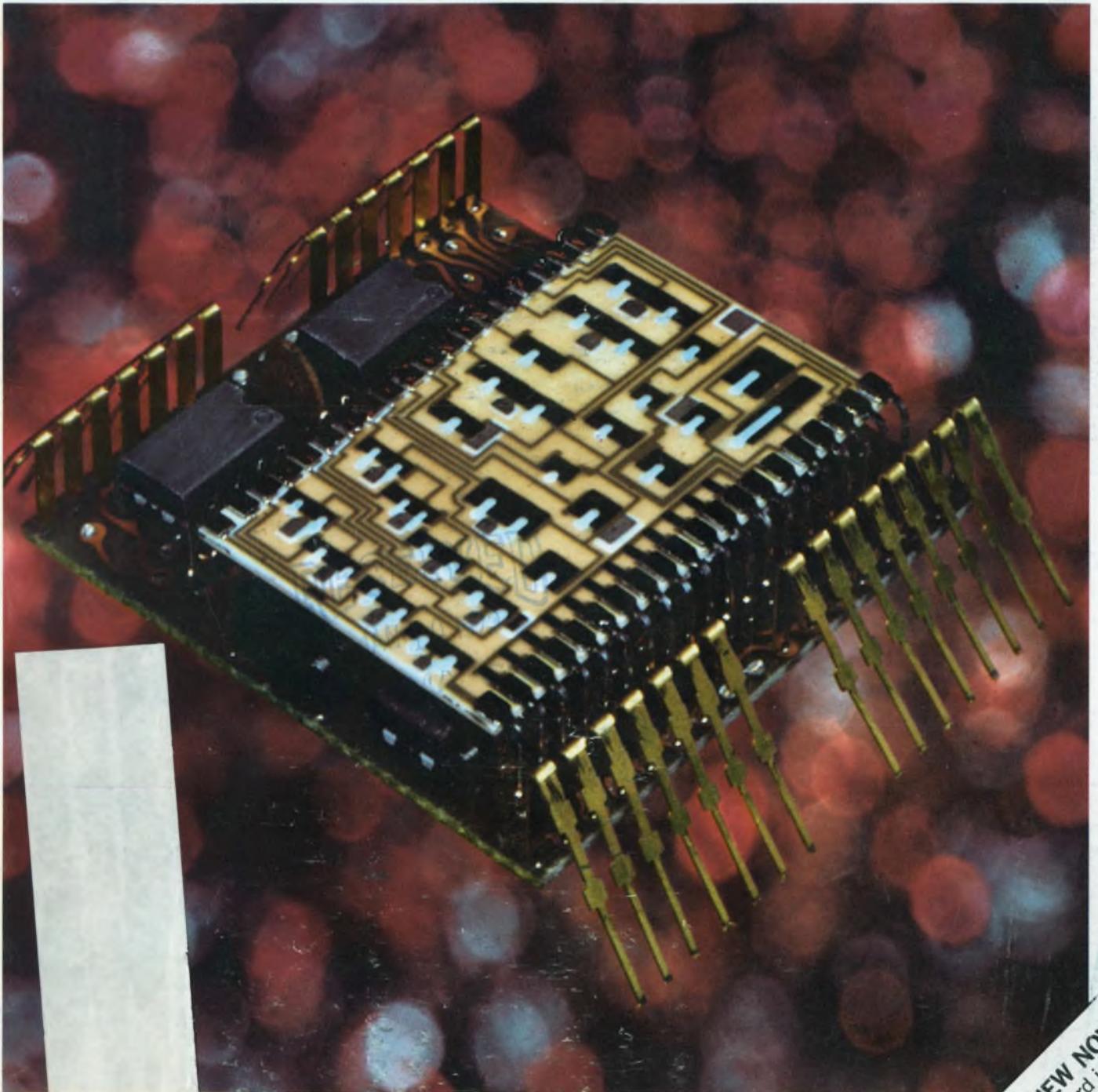
VOL. 21 NO.

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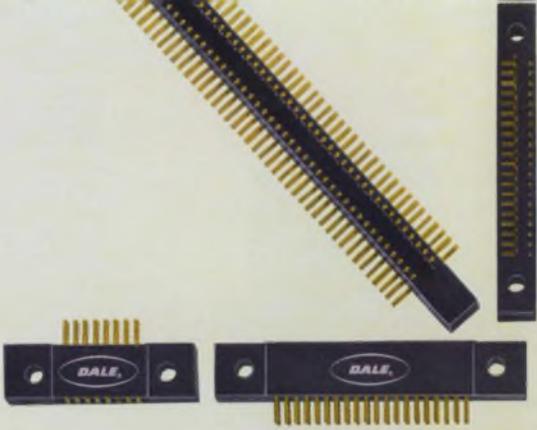
JAN. 4, 1973

A/D and D/A converters unite the worlds of the analog and digital design engineer. However, familiar specs are hard to find. Conversion time, resolution and

coding are mixed with settling time, accuracy and linearity. The converters come in many shapes and sizes. To clarify an often confusing subject, turn to p.56.



RENEW NOW!
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front cover



digital readout connectors



...custom tailored to your case at standard prices

Don't let a connector dictate your case design. Dale *Customline* .050" and .100" edgeboards give you extra design flexibility to cope with case contours. They'll help you produce an easy-to-read product with lots of eye appeal whether you're working with a calculator, a panel meter, a counter ...or other digital display application. Our unique design and manufacturing process lets us deliver custom body and contact configurations *below* the price of conventional high density edgeboards. And, if you're talking about any volume at all, the tooling will be amortized in the bargain. This is no

theoretical system. Dale *Customline* edgeboards are in use now mounting liquid crystal and LED displays in high volume calculator and panel meter applications. They're not limited to digital displays, either. They'll give you budget and design freedom wherever a low cost, reliable high density edgeboard is called for...the new leadless ceramic MOS packages, for example.

Make us prove it. Write for *Customline* Design Folder or call 605-665-9301 for Application Engineering Assistance.

INFORMATION RETRIEVAL NUMBER 242



TO: Dale Electronics, Inc., East Highway 50, Yankton, S. D. 57078

Send Custom Edgeboard Design Outline
 Information on Standard Edgeboards Have Representative call.

NAME _____ TITLE _____ COMPANY _____
 CITY _____ STATE _____ ZIP _____



Until you try HP's new IC Troubleshooting Partners, you'll never know how simple logic circuit testing can be.

Just push a button on the Pulser on the left, and let the Probe on the right automatically monitor the response downstream.

How? HP's new 10526T Logic Pulser injects a single 300 nanosecond pulse anywhere in your TTL and DTL circuitry. Low nodes are momentarily forced high, high nodes automatically pulled low. There's no unsoldering or trace cutting. Just press the button and the pulse is there. \$95.

And HP's new 10525T Logic Probe checks the result. A single, unambiguous light at your fingertips tells you exactly what's going on. If no pulse is detected, something's wrong.

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For other applications, the HP 10528A Logic Clip monitors all pins of DIP TTL/DTL IC's simultaneously. Use the Clip with the Pulser — the Pulser injects clocks, transfers, shifts, etc. HP 10528A Clip, \$125.

All three troubleshooters team up as the 5015T Troubleshooters Kit for \$285 which gives you a 10% discount and a handy carrying case to boot.

For more information on these and other IC Troubleshooters call your local HP field engineer or write Hewlett-Packard, 1501 Page Mill Road, Palo Alto, California 94304; Europe: P.O. Box 85, CH-1217 Meyrin 2, Geneva, Switzerland; Japan: Yokogawa — Hewlett-Packard, 1-59-1, Yoyogi, Shibuya-Ku, Tokyo, 151.

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02206

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**TELEDYNE
RELAYS**



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Cover: Photo of 12-bit DAC, the ZD 432, by Concord Photography Studio, courtesy of Zeltex Inc., Concord, Calif.



hp 34740A
DISPLAY

OFF ON

19.999

hp HEWLETT • PACKARD

34702A MULTIMETER

INPUT V HI

1000V MAX

DCV

ACV

OHM

INPUT Ω

350V MAX

LO

100V MAX

100Ω

1

10

100

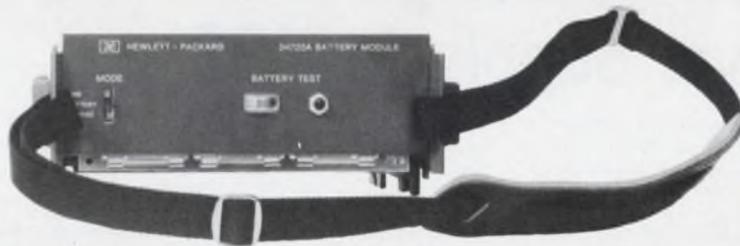
1000

10MΩ

500V MAX

V/kΩ

The New Snap-On...



Low-Cost, 4-Digit Measurement System 3470.

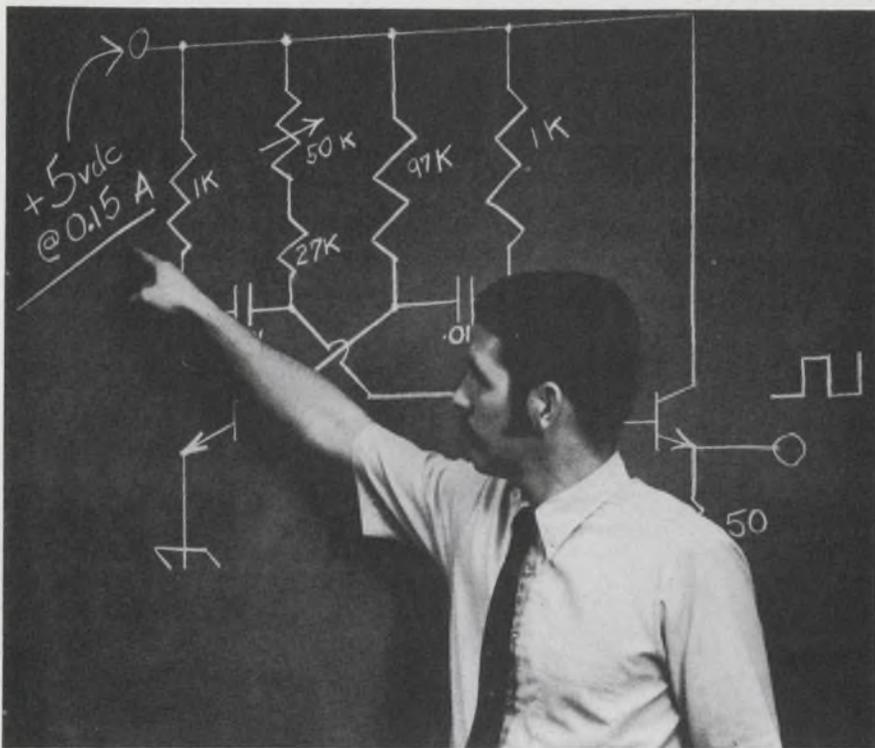
- Bright LED Display section has 100% overranging.
- AC/DC/OHMS snap-on with display. (\$600 complete)
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If you need one of these low-cost DMM's, there's no time like the present. Pick up the phone and call your nearest H-P Representative, now. Or, write to Hewlett-Packard, Palo Alto, California 94304; Europe; P.O. Box 85, CH-1217 Meyrin 2, Geneva, Switzerland. In Japan: YHP, 1-59-1, Yoyogi, Shibuya-Ku, Tokyo, 151.

HEWLETT  PACKARD

DIGITAL VOLTMETERS
INFORMATION RETRIEVAL NUMBER 4



How to Design Your Power Supply for \$83

You get the **complete schematic diagram, and parts list** with operating and installation instructions when you spend \$83 for an Abbott Model "R" power supply. Two years in development, this model represents the latest state of the art in power module design. It features close regulation ($\pm 0.05\%$), low ripple (0.02%), automatic short circuit and complimentary overvoltage protection and continuous operation in a 160°F ambient.

Abbott Engineers followed specific design criteria in engineering these modules. First, the electrical design was carefully engineered to insure that all components operate well within their limits, under "worst case" operating conditions. Second, the thermal design, including case construction, was carefully made to insure that the maximum temperature limits of all components are never exceeded. Then the size and weight of these modules were controlled to a minimum, without sacrificing reliability. Finally these units were thoroughly tested to make certain that all design and performance specifications were met.

So, you can build your own power supply using our schematic diagram if you want to—but we think we can build it more

reliably and for less cost, simply because we have been doing it for ten years. Put our power supply in your system first and try it. Examine its performance. We think you will be pleasantly surprised at the quality, adherence to specifications, and the reliability you find in the Abbott Model "R"

Any output voltage from 5 to 100 volts DC with current from 0.15 to 20 amperes is available. *Many of the popular voltages are carried in stock for immediate delivery.* Please call us for attractive O.E.M. discount prices.

Abbott also manufactures 3,000 other models of power supplies with output voltages from 5.0 to 3,650 volts DC and with output currents from 2 milliamperes to 20 amperes. They are all listed *with prices* in the new Abbott catalog with various inputs:

- 60 A to DC, Hermetically Sealed
- 400 A to DC, Regulated
- 28 VDC to DC, Regulated
- 28 VDC to 400 A, 1 ϕ or 3 ϕ
- 24 VDC to 60 A, 1 ϕ

Please see pages 618 to 632 of your 1971-72 EEM (ELECTRONIC ENGINEERS MASTER Catalog) for complete information on Abbott modules.

Send for our new 56 page FREE catalog.

abbott transistor

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across the desk

Printer/plotter article ruffles some feathers

The article "Need a Hard-Copy Peripheral?" (ED 18, Sept. 2, 1972, p. 54) should be useful to the prospective printer/plotter customer, but a potential buyer of an electrostatic plot device should consider several points not mentioned.

The electrostatic plotter is, by its design, limited to paper movement in one direction only. Thus a plot must be completely composed and stored prior to the output of the "picture"—not as coordinate pairs but as a binary bit for each spot. An 8 × 10-in. plot with 80/in. resolution requires 32,000 16-bit words of mass storage.

The "up to 10 seconds" figure quoted as time to produce a typical plot is apparently output time only. Not mentioned was the core-time required to convert program-supplied data into picture data—a factor not present in direct pen plotters. The inclusion of required compute time into this figure considerably reduces the time savings claimed for the electrostatic devices.

I recently completed a real-time software package for an electrostatic plotter/printer (the Varian Statos 21) on the CDC 1700. A comparison of start-to-finish times for this device and a standard direct pen plotter show time savings factors of from 5 to 10. Disc storage is used for picture data and plots over 200 in. long may be generated. The programming effort was extensive.

Tom Markle

Computer Sciences Corp.
3065 Rosecrans Pl.
San Diego, Calif. 92110.

The author replies

Mr. Markle is correct in his general statements about generating plots on large computers for elec-

trostatic printer/plotters; however, other methods are available to generate plots. Both pen and electrostatic plotters require the same routines and computer time, except that pen-plotter routines must also include mechanical pen positioning instructions (pen up, down, etc.). But Mr. Markle's "core-time required to convert program-supplied data into picture data" can virtually be eliminated for electrostatic plotters. Varian has developed software for use in 16-bit minicomputers that sorts, by magnitude, the same vector-end-point data used by pen plotters, then converts the data to raster format and starts the output through an on-line electrostatic printer/plotter within a few seconds. This software can typically maintain plot output at rates comparable to 10 sec. for an entire 8-1/2 × 11-in. plot. Plot speed, of course, varies inversely with plot density. In addition Fortran vector generation routines are available to generate complete plots with a minicomputer of only 12-k memory.

The article "Need a Hard Copy Peripheral?" contains obvious factual errors and is laced with advertising in favor of electrostatics. The A.B. Dick Videojet series of ink-jet printers have been on the market since 1968. Models are available at 250 characters/sec. and 750 characters/sec. Both employ a single nozzle. These facts were ignored by the author, who would have your readers believe that single-jet devices are speed-limited at 100 characters/sec. and that less reliable, multiple-jet systems are needed to reach speeds of 200 characters/sec.

The author writes with equal "expertise" and accuracy about imaginary problems that plague jet systems. She alludes to environmental conditions that make lit-

(continued on page 16)

Electronic Design welcomes the opinions of its readers on the issues raised in the magazine's editorial columns. Address letters to Managing Editor, Electronic Design, 50 Essex St. Rochelle Park, N. J. 07662. Try to keep letters under 200 words. Letters must be signed. Names will be withheld on request.

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ACTUAL SIZE



THIN-TRIM capacitors are a new development in miniaturized variable capacitors for application in circuits where size and performance is critical. The Thin-Trim concept provides a variable device to hybrid circuit designers which replaces fixed tuning techniques and cut and try methods of adjustment.

FEATURES

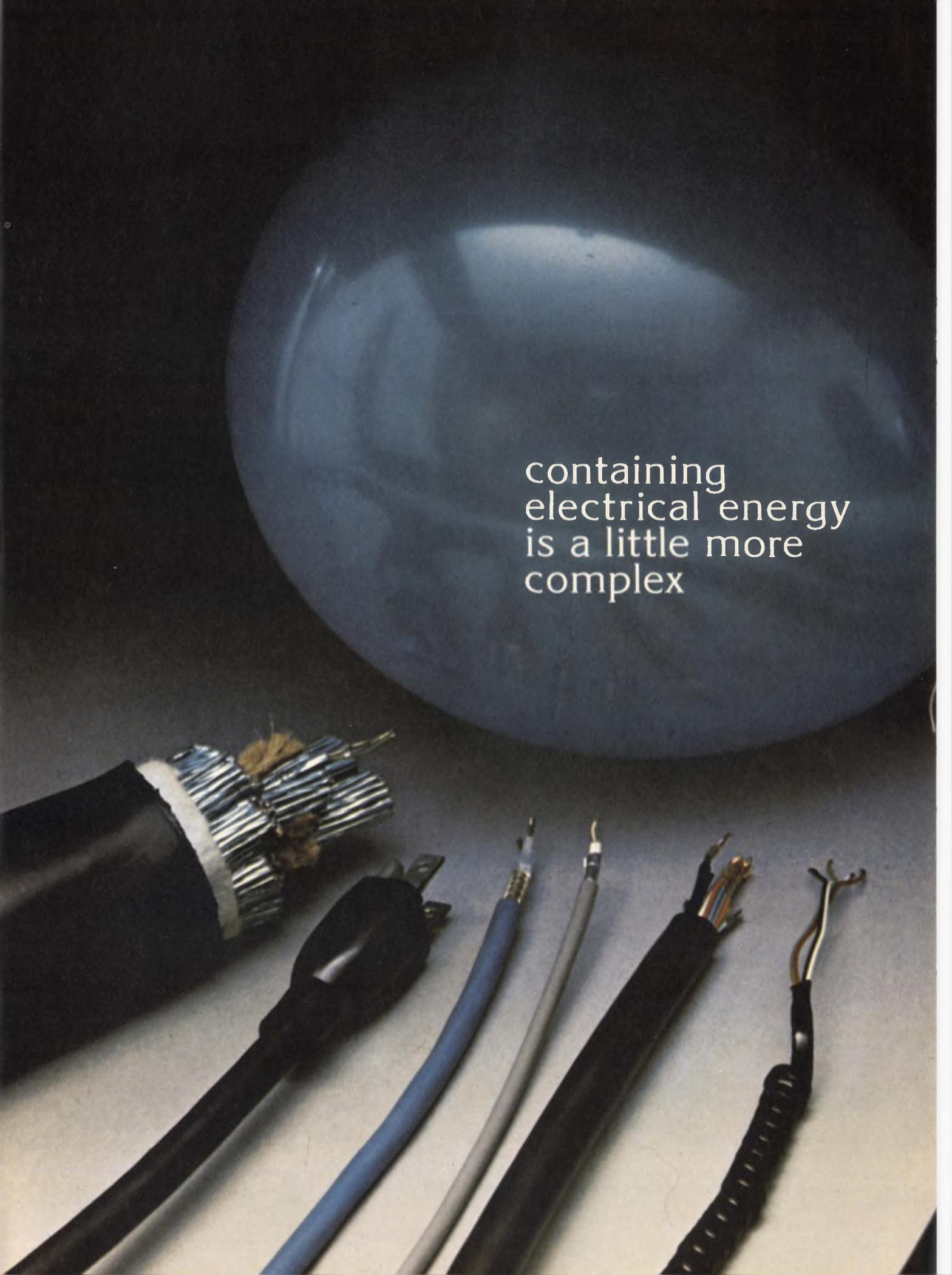
- Low profile for HYBRID CIRCUIT applications.
- High capacity values for BROADBAND applications.
- High Q - low capacity values for MICROWAVE applications.

U.S. Patent 3,701,932

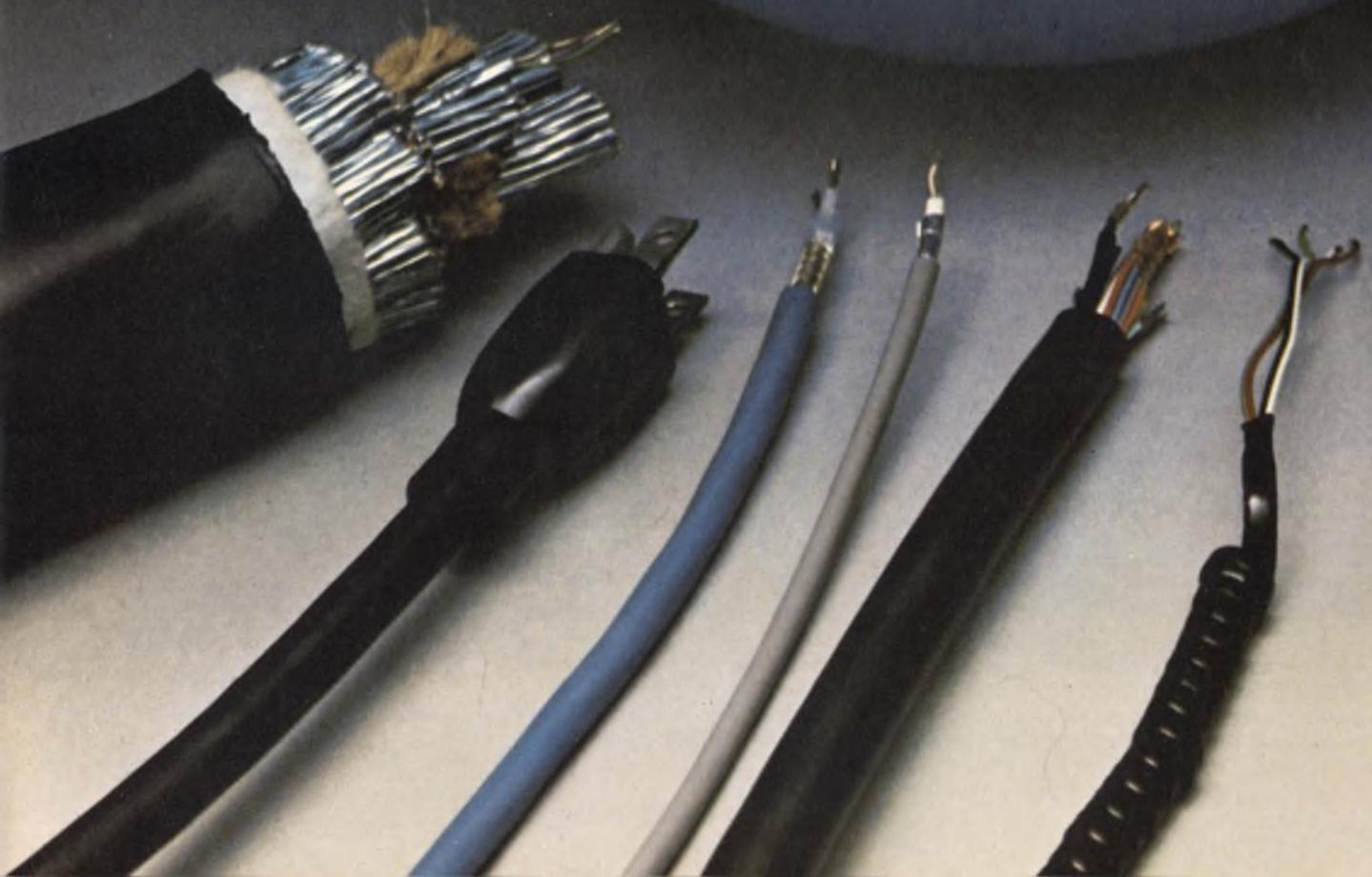
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electrical energy
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complex



How a cable copes with the problems of voltage safety; frequencies; current; attenuation; capacitance; velocity of propagation; inductance; electrostatic and electromagnetic interference, depends heavily on what surrounds the conductors:

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Write for a copy of the Belden Electronic Wire and Cable Catalog. Belden Electronic Division, P.O. Box 1100, Richmond, Indiana 47374. Phone (317) 966-6681.

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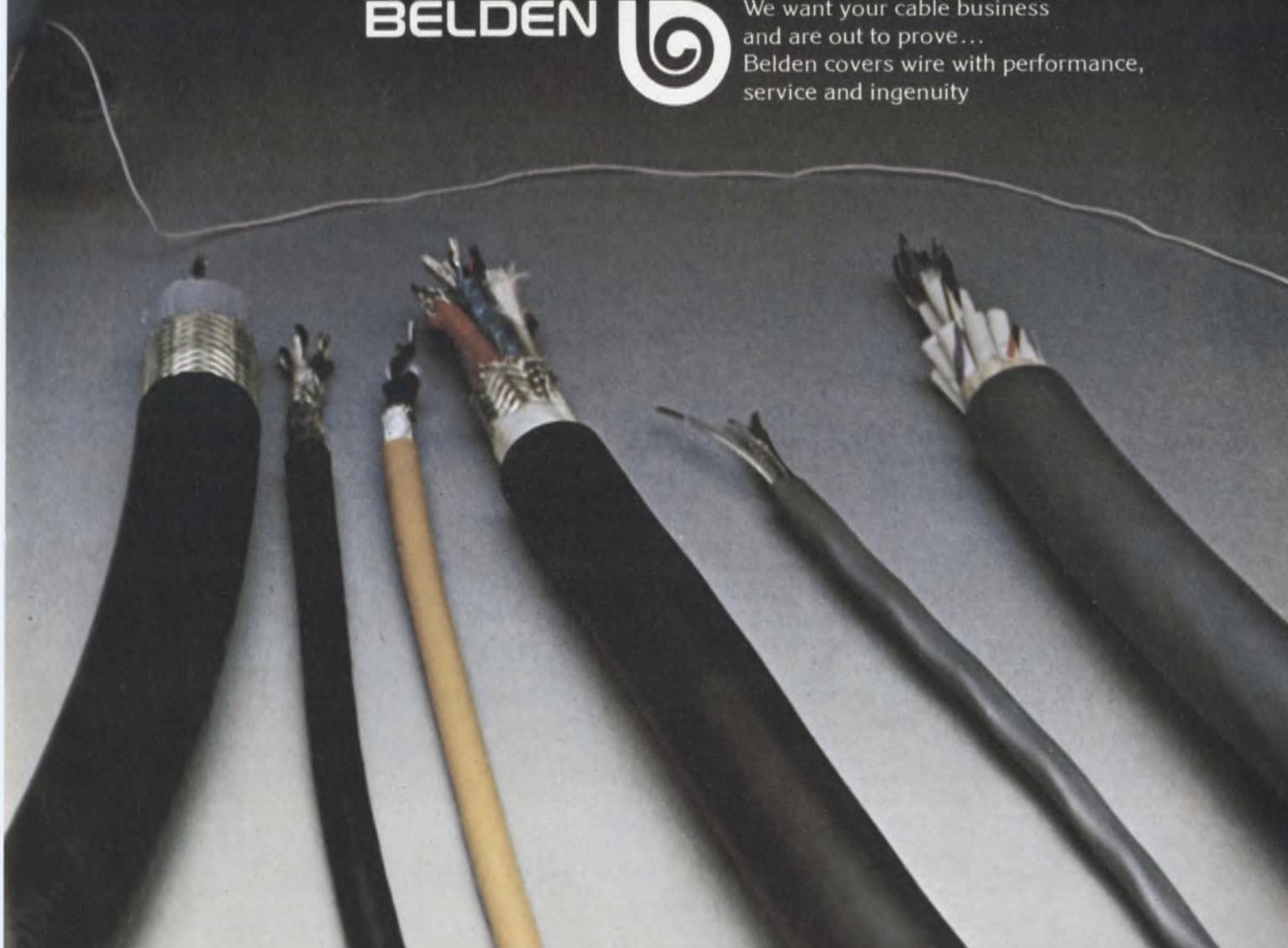
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BELDEN



We want your cable business
and are out to prove...

Belden covers wire with performance,
service and ingenuity



If you thought you had an MPF headache...

calm down

No need to redesign! General Instrument's new MEM 620/621/622 Plastic RF MOSFETS are direct pin-for-pin replacements for our competition's MPF 120/121/122's.

And our MEM's offer superior performance, lower cost, and most importantly, are available now . . . and from now on. So, calm down.



If you're outside New York State and want an evaluation sample and data sheets (you won't need the aspirin), or if you want any information on the subject of MOSFETS, ours, or other people's, call

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If you're in New York State call collect: 516-733-3037 or write: Dept. MOST, General Instrument Corporation, 600 West John Street, Hicksville, N.Y. 11802, or call, in New York: 516-733-3333; in Chicago: 312-338-9200; in Los Angeles: 213-641-7411. In Canada, call or write: General Instrument Canada, Ltd., 61 Industry Street, Toronto 337, Ontario, Canada, Tel: 416-763-4133. In Europe, write: General Instrument Europe S.P.A., Piazza Amendola 9, 20149 Milano, Italy. In the U.K., write General Instrument Microelectronics Ltd., 57/61 Mortimer Street, London, W1N7TD, England: In the Far East, write General Instrument of Taiwan Ltd., P.O. Box 22226, Taipei, Taiwan.



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INFORMATION RETRIEVAL NUMBER 7

INFORMATION RETRIEVAL NUMBER 8 ►



PACKS TWICE THE CONTACTS IN THE SAME SPACE AT ABOUT HALF THE COST

Elco's solution to the escalating packaging squeeze and packaging costs in electronic circuitry. A line-up of I/O rack and panel and cable-to-cable connectors with contact spacing on .100" and .125" centers.

On a performance/price basis, these high density connectors are your best buy. Quality is equal to or better than, and published prices are much less than those of their pin-and-socket counterparts.

Take the Series 8026 R/P and cable-to-cable connector that's equipped with the Elco high-reliability crimp-and-insert mini Varilok™ contact. Team a Series 8026 117-contact plug with its corresponding receptacle, and you have a 117-contact connector that's in the same envelope as a 56-contact connector on .150" spacing. But packing more than twice the contacts in the same space.

The 75-contact 8026 connector will fit in the same space as a 38-contact connector on .150" spacing. And the 8026 33-contact connector is one of the smallest 33-contact R/P connectors you've ever seen. For back-up, we offer Series 8026 connector with 55 and 79 contacts on .125" square grid.

For full details on these new connectors from Elco, contact your local Elco representative or distributor, or: Elco, Willow Grove Division, Willow Grove, Pa. 19090, (215) 659-7000 • Elco, Pacific Division, 2200 Park Place, El Segundo, Calif. 90245, (213) 675-3311.

For your I/O back-panel applications, Elco Series 5540 connectors are available in the same sizes as the 8026, but use the field-proven Varicon™ contact with .025" square wire-wrappable posts. They incorporate—as do the 8026's—a new female turnable jackscrew that eliminates any possibility of damage to plate contacts in difficult or blind mating situations. Both series use standardized polarizing and keying hardware to prevent unmatched plugs and receptacles from being mated.

And by no small coincidence, hardware standardization and using one contact for both sides lets you minimize your in-house and field stocking requirements, and allows you to use the same manufacturing set-up to assemble all sizes.

Besides helping you cope with your close-order circuits, these connectors will help you effect other cost economies. Like using your existing 8016 panel punches. Reducing inventory because they can do duty in R/P and cable-to-cable applications as well as be used as an I/O.

There's one more bonus. Immediate availability. Both series. All sizes. Another service in keeping with CONNECTRONICS, Elco's Total Connector Capability.



Series 5540 input-output plate receptacles with or without polarizing hardware. On .100" grid with 33, 75 and 117 contacts. On .125" grid with 55 and 79 contacts.



Polarizing hardware provides 36 polarization combinations per connector pair.



Metal covers for 33, 55, 75, 79 and 117-contact connectors have top and side cable entries.



Cable strain relief clamps are adjustable for small and large cable bundles, can be mounted on plug and/or receptacle.



ELIMINATE RESISTOR STOCKPILES

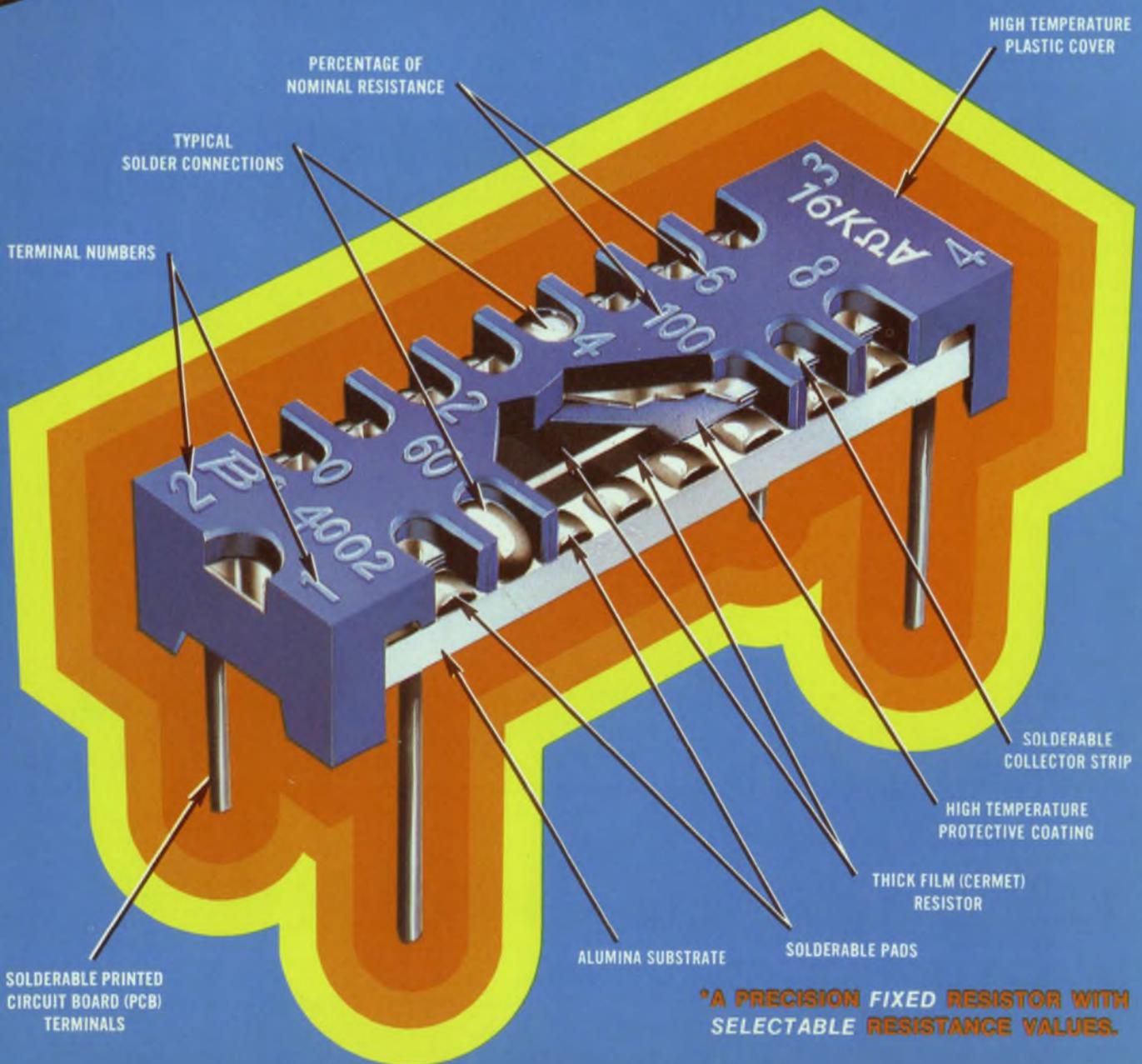
WITH... BOURNS

SFR™

SELECTABLE FIXED RESISTOR*

90 SELECTABLE RESISTANCE VALUES IN **1** TINY UNIT.

Model
4002



*A PRECISION FIXED RESISTOR WITH
SELECTABLE RESISTANCE VALUES.

BOURNS NEW... UNIQUE CONCEPT IN RESISTIVE COMPONENTS ALSO OFFERS

- * 33 ohm to 1.25 megohm combined resistance range over 15 units
- * Selectability within $\pm 1\%$ of required resistance value over the entire range

BOURNS
SFR™
 SELECTABLE FIXED RESISTOR

- ... IS A STABLE, THICK-FILM, FIXED RESISTOR WITH ADJUSTABILITY OF $\pm 1\%$ OR BETTER
- ... REPLACES STANDARD FIXED RESISTORS IN APPLICATIONS WHERE FINAL RESISTANCE VALUE REQUIRED CAN'T BE PRECISELY DETERMINED AT THE DESIGN STAGE
- ... REPLACES "ONE-TIME ADJUST" VARIABLE RESISTORS IN APPLICATIONS REQUIRING LONG-TERM STABILITY
- ... RESISTANCE VALUE IS SELECTED, THEN PERMANENTLY, RELIABLY SET BY SOLDERING

LOOK AT THE \$\$ YOU SAVE ON INVENTORY!!

FOR EXAMPLE: Your application requires selection of individual resistance values from 550 ohms to 1000 ohms, or 40 different resistors at 10¢ each. One Model 4002 provides the same resistance selection within $\pm 1\%$ at 76¢*.

Result: 40 different resistor values: 40 x 10¢ = \$4.00
 One Model 4002: 1 x 76¢ = .76

YOU SAVE... \$3.24!!

* 1,000 piece quantity price U.S. dollars, F.O.B., U.S.A.

it's easy to use

After mounting on PCB; probe the COARSE and FINE adjustment taps (Figures 1 and 2) to determine the precise resistance required. Solder the selected taps (Figure 3) and the SFR RESISTOR is permanently set.

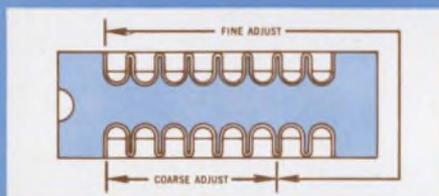


Figure 1



Figure 2



Figure 3

FOR COMPLETE DETAILS AND A BROCHURE:

- CALL SFR RESISTOR SALES COLLECT (714) 781-0270
- CONTACT YOUR LOCAL BOURNS REPRESENTATIVE.

FOR A FREE SAMPLE... write to the factory answering the following on your company letterhead.

- (a) My application for the Bourns SFR Resistor is . . .
- (b) It will replace (number) of fixed resistors in my inventory
- (c) Approximate anticipated annual quantity usage: (number)

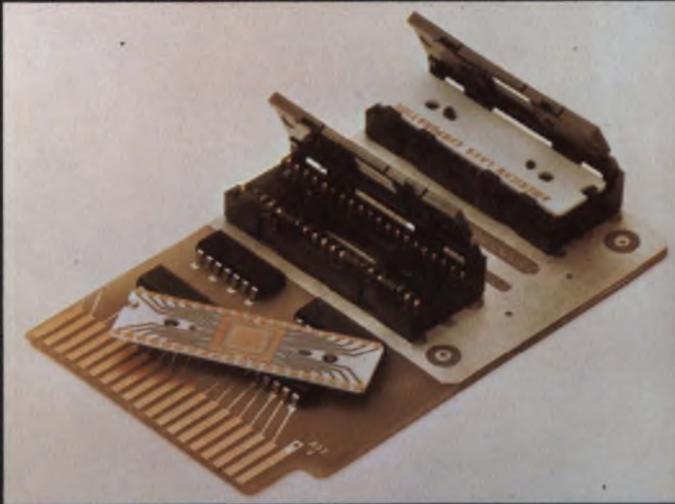


"SFR" is a trademark of Bourns, Inc. Patents Pending

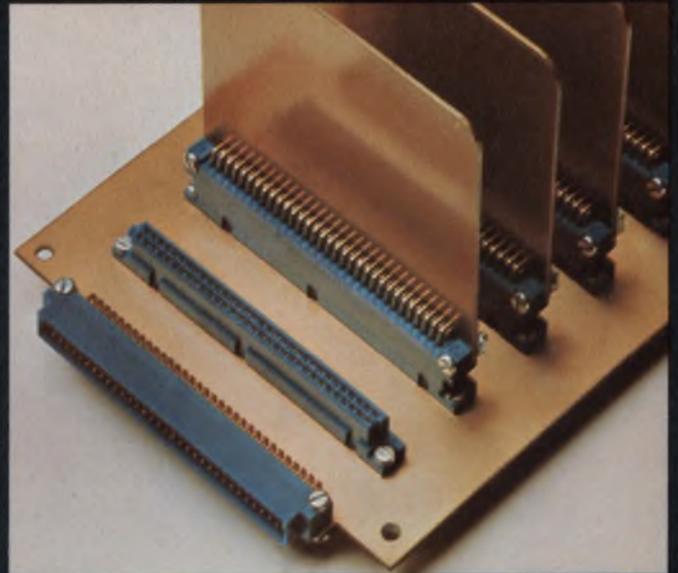
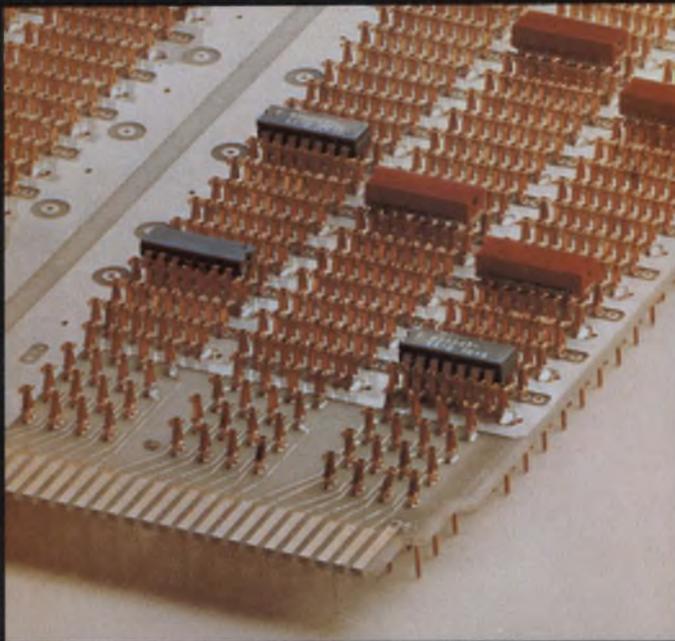
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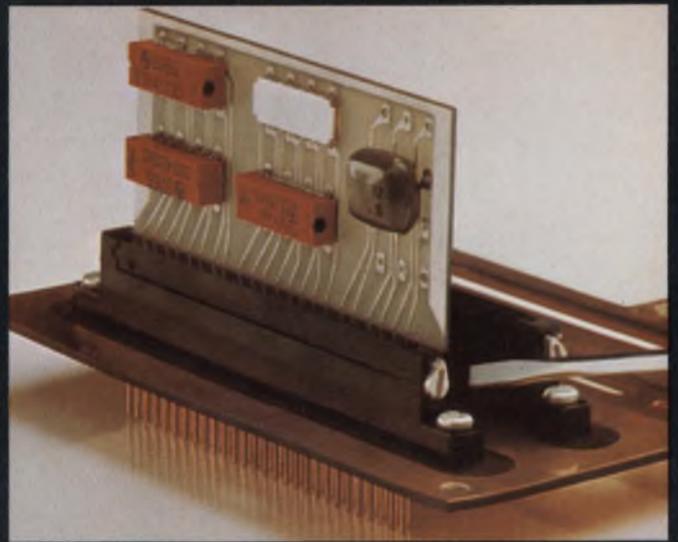
New from Amphenol's Spectrum



level 1 MOS/LSI Planar Plug-In connectors (above) for leadless, flat mount ceramic substrates. Permits fast, easy replacement of IC package, no screws, has snap-down lid. ■ Free-standing terminal (below) terminates IC's to PC boards for lowest total systems cost.



level 2 Box contact connectors (above) intermate with .025" square or round contacts. Low insertion force. Terminations for crimp, wire wrapping or wave solder. ■ Zero insertion force connectors (below) improve PC board and connector life by eliminating strain and wear.



Above are seven new ideas from Amphenol Industrial Division's Spectrum of interconnection capability.

Amphenol's SPECTRUM offers you *all four* levels of interconnections from our unmatched breadth of product line:

Level 1 . . . DEVICE TO BOARD OR CHASSIS. We offer interconnections for components such as tubes, relays, transistors, IC packages, trimmers, resistors or capacitors to a PC board or chassis.

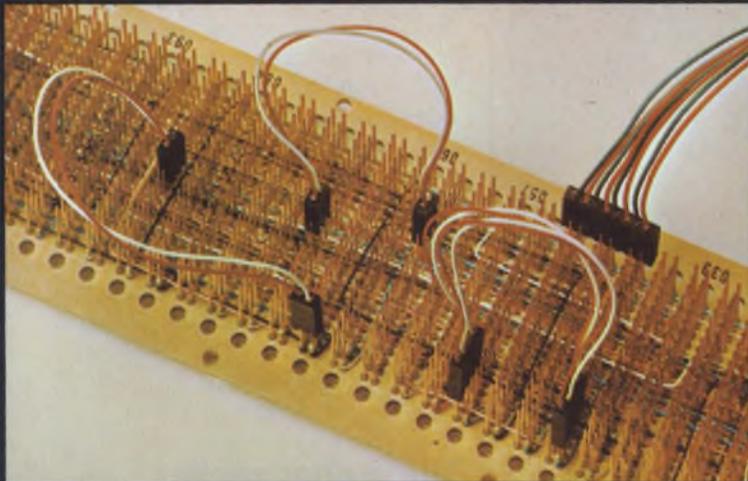
Level 2 . . . BOARD TO MOTHERBOARD OR BACK PLANE. We offer interconnections for PC boards or

other sub-circuit modules to a motherboard or to a back plane.

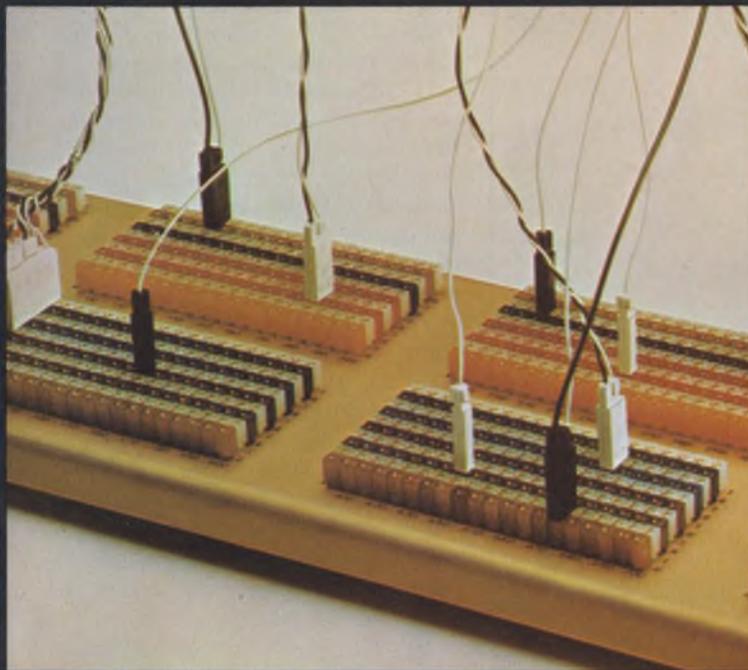
Level 3 . . . MOTHERBOARD OR BACK PLANE WIRING. We offer interconnections for levels to each other and to other sub-circuits with multi-layer circuit boards, wire wrapping, clip terminations, jumper techniques and dip-soldering.

Level 4 . . . INPUT/OUTPUT CONNECTIONS. We offer interconnections for power and signals to and from a system. This interface may be between sub-assemblies within the same enclosure or between individual units.

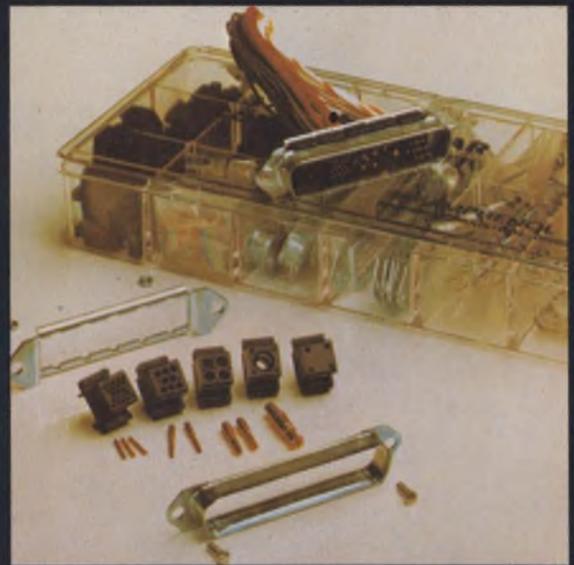
of interconnections.



level 3 Low cost strip connectors (above) are used as jumpers in back plane wiring. Intermates with .025" square or round posts. ■ Circuit Concentration Bay (below) consists of wire wrappable panels that are five times as compact as the telephone distribution frames they replace.



level 4 Modular Integral Connector concept lets you make your own pin & socket connector to fit your needs. Five contact sizes, thousands of combinations. Sufficient components for six connectors in handy MIC-KIT. Design and assemble your own prototypes.



From the simple tube socket—to a myriad of electrical/electronic connectors—to complete and complex termination systems . . . SPECTRUM.

But SPECTRUM is far more than products. It is a depth of capability in engineering, manufacturing and quality control. Amphenol's SPECTRUM is a new height of service, availability and distribution backed by seven Amphenol interconnection-oriented divisions.

Amphenol can fulfill your total interconnection requirements because we are not limited to specifics such as one or two product lines, one or two levels.

Therefore we approach your interconnection needs with complete open-mindedness.

For more new ideas and specific information, write for your copy of "SPECTRUM." Amphenol Industrial Division, Bunker Ramo Corp., 1830 South 54th Ave., Chicago, Illinois 60650.

**BUNKER
RAMO**

AMPHENOL



When it comes to Synchro Converters, if we don't make it... you won't find it.

Fact is, we've got the broadest line of synchro converters on the market. Single and "building-block" modules with errorless tracking . . . single and multi speed converters of high resolution . . . multiplexed converters going D/S or S/D . . . synchro to linear converters . . . DC angle or invariant sin/cos. Chances are, the very device you need is sitting right here on the shelf. But let's face another fact. Could be, you've got a problem application that a standard product won't meet. That's where our technical staff comes in. Ready to work with you. To design an individual module, or a total system to solve your digital or analog interface requirement. And more times than not, simple modification of existing products will do the job.

You see, if we don't have it, we'll make it. That's the attitude that made us "Number One" in the Synchro Conversion field.

For product or technical applications information, write or call Steve Muth or Jim Sheahan. They're engineers, so they talk your language.



ILC DATA DEVICE CORPORATION
100 TEC STREET, HICKSVILLE, N. Y. 11801 • PHONE: (516) 433-5330

ACROSS THE DESK

(continued from page 7)

tle sense—for example, "humidity can shift dots"—and are not experienced in the field. She ignores the fact that ink-jet printers are the only nonimpact printers available commercially that utilize inexpensive and widely available plain paper. She conveniently glosses over the disadvantages of electrostatics—proprietary paper that is expensive and needs a liquid for image developing.

George E. Marton
Marketing Manager

A.B. Dick Co.
5700 W. Touhy Ave.
Chicago, Ill. 60648.

The author replies

No specific Videojet information was at my disposal when the article was written. A very recent article from *IEEE Transaction on Computers* (Ernbo, Arne, September, 1972, No. 9, Vol. c-21, pp. 942-947) only hints at speeds of 250-750 characters/sec. for single jet units. Therefore my article rated ink jets at 15-300 characters/sec. in the table on p. 59. But the higher speed hardly affects the ink-jet devices' relative over-all position compared with the other techniques. Not delving into Videojet details—which is obviously state of the art—was surely an oversight on my part.

As for those "imaginary" problems plaguing jet systems, CRT-type aberrations and air-current-induced dot shifts were very real to members of Varian's engineering staff who viewed them—admittedly on another manufacturer's device, an Inktronic unit—at a recent trade show.

Mr. Marton is correct in pointing out that the article failed to mention that ink-jet devices can use inexpensive, plain paper.

Jill Peters

Varian Data Machines
611 Hansen Way
Palo Alto, Calif. 94303.

The joys of starting a company extolled

Congratulations on the editorial "Get Enriched (If Not Rich) with
(continued on page 21)



Just born. The littler trimmer.

Meet our new microminiature ceramic variable capacitor.

It provides maximum adjustable capacity for a given size—plus high reliability at low cost.

The DVJ5014 trimmer, with a height of .070 inches above the mounting surface, is only .245 inches in diameter yet matches the electrical performance of other capacitors many times its size. This trimmer features a slotted adjustment head.

Also available is the DVJ5009 series (with a height of only .045 inches above the mounting surface) featuring a flush adjustment head. In applications where cost rather than height is the prime consideration, use of the DVJ5014 is recommended.

Rotors for both models are constructed with a monolithic embedded electrode in a special pro-

prietary ceramic material and a stator body made from high alumina ceramic. These features provide a larger ΔC , and higher reliability than previously available, as well as complete environmental stability.

The new JFD microminiature ceramic variable capacitors are well suited for printed or hybrid circuit mounting as well as other applications involving ceramic substrates, microminiature crystal oscillators, stripline assemblies, multiplex transceivers, telemetry oscillators and transmitters, frequency multipliers, and other subminiature electronic circuits.

That's quite a lot for a little trimmer.

Why trade off performance to get lower prices? For full details write or call us or your local JFD field engineer.

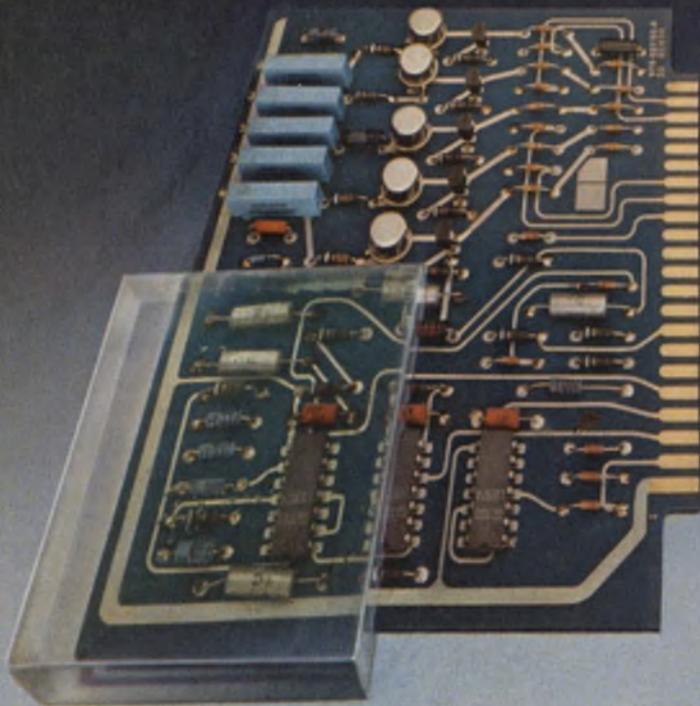
DVJ5009	ACTUAL SIZE	DVJ5014
Model		Capacitance Picofarads Min.-Max.
DVJ5009/10		3-10
DVJ5014/10		
DVJ5009/15		3.5-15
DVJ5014/15		
DVJ5009/20		4-20
DVJ5014/20		
DVJ5009/30		5-30
DVJ5014/30		

No special tools required for adjustment.

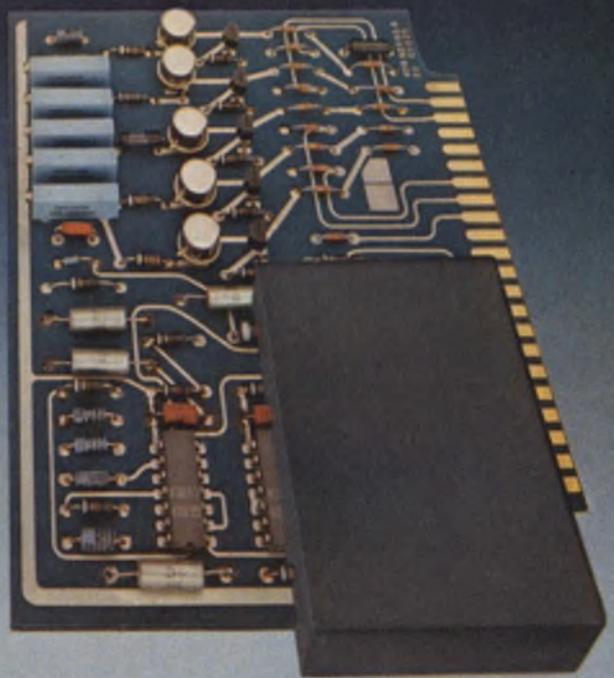
JFD

A Riker-Maxson Subsidiary
JFD Electronics Corporation
 18th Ave. at 82nd Street
 Brooklyn, N.Y. 11218
 Phone (212) 331-1000

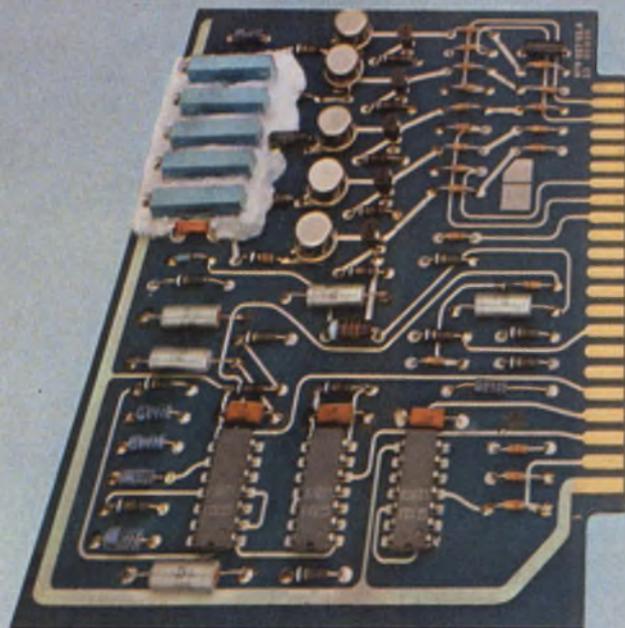
As components become more sophisticated, the versatility of silicones is more evident.



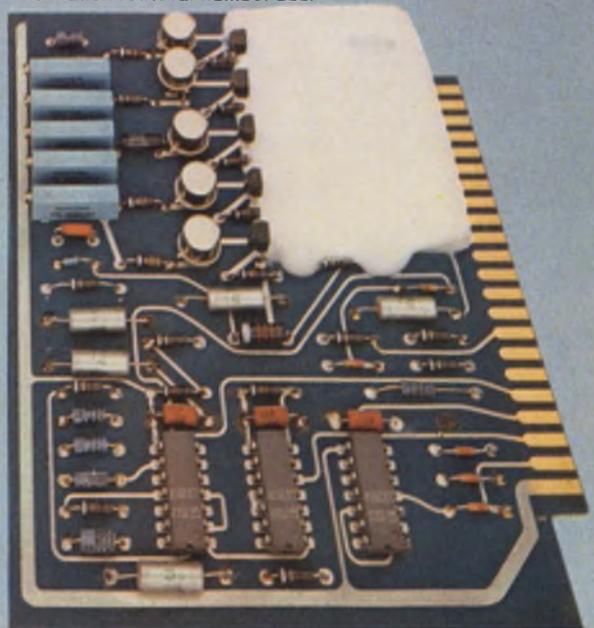
For see-through protection, encapsulate with this clear, resilient silicone resin. Self-extinguishing, it guards against humidity, heat, cold, radiation, thermal shock and vibration. Information retrieval number 221.



For added safety, specify this flame-retardant, pourable silicone elastomer. Uses for this low-cost packaging material include coating, potting and encapsulating. Information retrieval number 222.



For excellent adhesion to corrosion-prone metals such as copper, use this new noncorrosive, one-part Dow Corning sealant. Cure mechanism produces no exothermic heat or acetic acid. Information retrieval number 223.



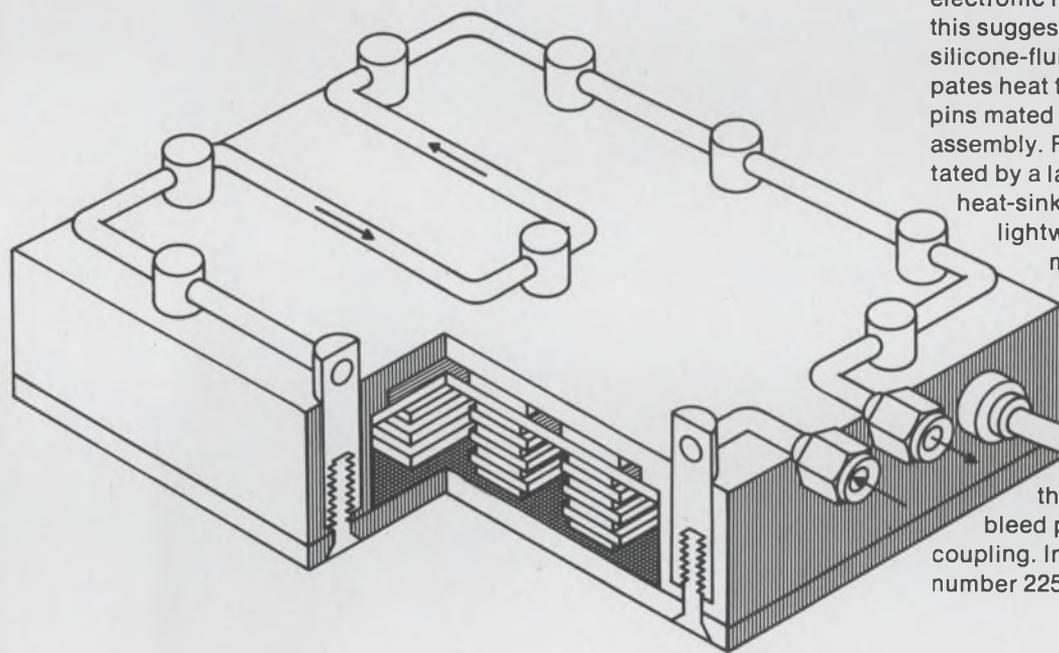
For protection against moisture, dirt, ozone, radiation and many solvents and chemicals, select this conformal coating. It flows on easily and cures at room temperature to a tough silicone rubber with excellent dielectric properties. Information retrieval number 224.

Silicones are unusual in the number of ways they protect. They resist change in hostile environments where other materials are unstable. They have excellent dielectric properties. With the electronic industry's concentration on higher performance and smaller components, the application areas where only silicone materials

can ensure design integrity have increased dramatically. Here are some of the newest examples. Many others are described in our Silicone Electronic Materials brochure available from your Dow Corning distributor. His name appears on the following page. Or write Dept. A-2202, Midland, Michigan 48640.

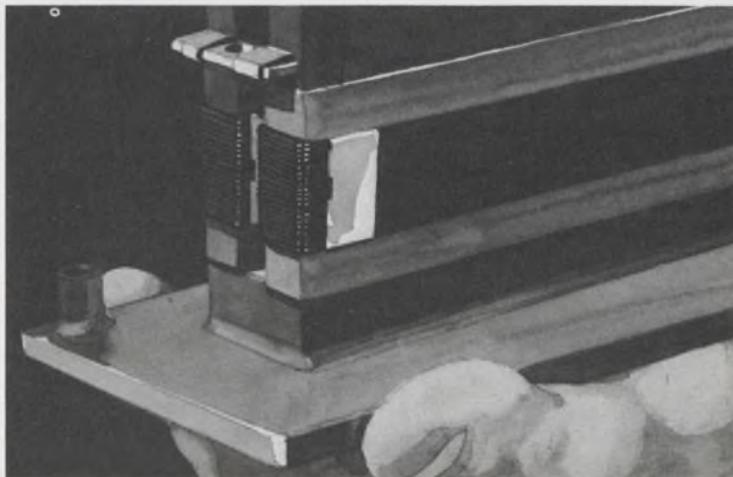
Electrical/electronic materials from

DOW CORNING



Silicones for cooling high-density modules. More efficient cooling of electronic modules is possible with this suggested assembly design. A silicone-fluid-filled coolant tube dissipates heat transferred to it from dowel pins mated to holes in the module assembly. Further conduction is facilitated by a layer of Dow Corning® heat-sink compound between a lightweight cold plate and module base. Silicone fluids have excellent heat-transfer properties and maintain constant viscosity over a wide temperature range. The heat-sink compound has high thermal conductivity and low bleed properties for long-term coupling. Information retrieval number 225.

Silicones add durability to Ominimite* transducer. This magnetostrictive device converts electrical energy into sound for ultrasonic cleaning systems. It is insulated with Dow Corning silicones. Bendix Instruments and Life Support Division uses coil forms fabricated from a Dow Corning silicone resin bonded glass laminate. Finished coils are dipped in Dow Corning® 997 varnish and baked. Silicones help add the physical and electrical stability required for long-term performance. Information retrieval number 226.



*TM, Bendix Corporation

This is no time for popcorn noise...



In fact, no time is acceptable for Popcorn (burst) noise, if you're designing a system to handle extremely small signals.

So RCA is announcing a new micropower, low noise operational amplifier. It's a designer's dream.

Our unique process gives you a monolithic silicon op amp that not only exhibits low burst noise but operates from a single 1.5-volt cell with a power consumption of 1.5 microwatts.

How low is the noise? Every CA6078AT op amp that leaves RCA must operate with equivalent

input burst noise less than 20uV (peak) at $R_s=200,000$ ohms.

That's not all, the CA6078AT features output short-circuit protection through built-in output resistors, input voltage range ($\pm 15V$ max. for $\pm 15V$ supply) wide dif-mode range ($\pm 6V$), and low offset-voltage nulling capability.

So go ahead! Design the CA6078AT into your system... and relax. Because you can be certain that with the new RCA micropower op amp, no time is acceptable for popcorn (burst) noise.

Want more data on the
INFORMATION RETRIEVAL NUMBER 192

CA6078AT or CA3078AT (the low cost version of the CA6078AT for less critical applications) or the CA6741T, RCA's low-burst-noise 741? See your RCA Representative or Distributor and ask for Technical Bulletins, File No. 530 and 592 and Application Note ICAN-6732. Or write RCA Solid State, Box 3200, Somerville, N.J. 08876. Phone (201) 722-3200.

RCA Solid State
products that make products pay off

Silicone Protectors

A full line of silicone encapsulating, insulating, sealing, coating and dielectric materials is available from Dow Corning Distributors at the following warehouse locations:

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Centralab perspectives

FOR USERS OF ELECTRONIC COMPONENTS



CENTRALAB

Electronics Division
GLOBE-UNION INC.

5757 NORTH GREEN BAY AVENUE
MILWAUKEE, WISCONSIN 53201

Covering Detroit's needs for thick film hybrids is a big order.

Whether you're in autos, computers, music, data processing, business machines, telecommunications or industrial electronics . . . Centralab can now provide the thick film hybrid circuits you need.

Tight schedules. Exacting specs. Volume orders for millions of pieces. Anyone who has supplied the nation's auto manufacturers with component parts knows this is the kind of mission he faces.

Centralab has run this fast track for some years, providing assembly plants throughout the U.S. with thick-film hybrid circuits for Detroit end use. These have included circuits for car radios, stereo tape players, fuel controls, headlight dimmers and dashboard instrumentation such as tachometers and sequential turn controls.

Why Centralab hybrids? Obviously, the auto makers are getting the high performance specs they ordered, and in the enormous quantities they demand.

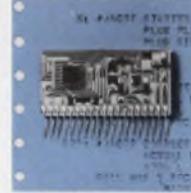
Take the specs, for example. Package power up to 4 watts per square inch. Rugged ceramic substrates with special form factors. Compare resistor tolerances as low as $\pm 0.5\%$ and TC of 0 ± 100 PPM/ $^{\circ}$ C and you get an idea of the customized circuitry Centralab thrives on. Capacitor dielectrics range through NPO & N5250 to Hi K. Designs include plastic and glass encapsulated transistors and diodes, as well as chip devices.

Happily, this type of spec is also

required in other industries. Manufacturers of musical instruments, sound equipment, radio and TV come regularly to Centralab for custom hybrids. Typical circuits produced are tuner, IF, color and audio-circuitry. Electronic organ manufacturers are using Centralab thick-film circuits for staircasing networks, passive filters, keyers, frequency dividers, amplifiers, MOS protection and tone control circuitry.

Among the fastest growing fields is data processing. Here Centralab has produced such circuits as pull-up networks, voltage regulators, dis-

play drivers, one shot, multi-vibrators, hammer drivers and interface devices.



Centralab's programmed for thick-film usage in computers.

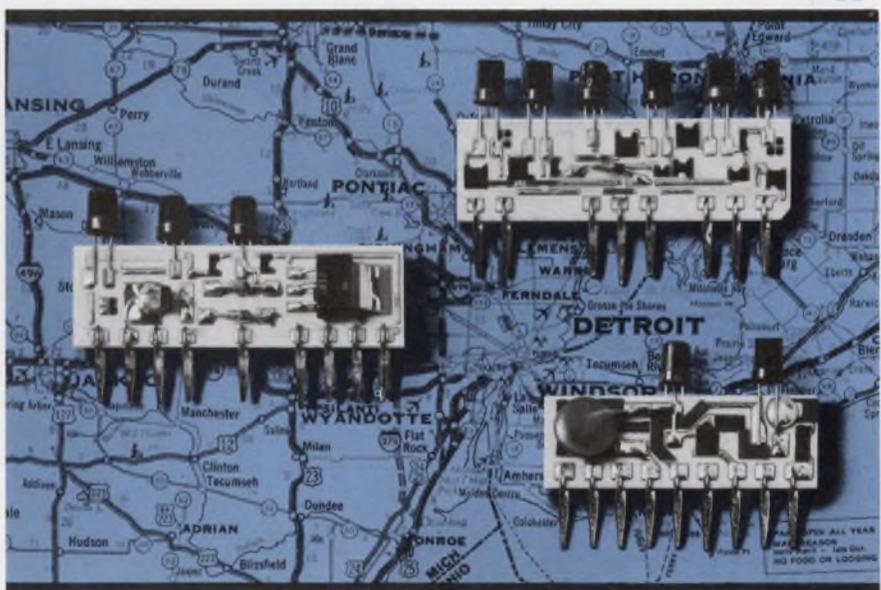
Also worth singling out are business machine and point-of-sale equipment manufacturers who specify circuits such as clock drivers, video amplifiers, high voltage bleeders, and motor speed regulators.

The list goes on and on. Telecommunications and the requirements for attenuator pads, passive filters and mixing networks. Industrial electronics and circuits such as motor speed control, solid state switches and frequency control networks.

But you get the idea by now. You set the spec. Centralab will set the precedent. It's virtually that easy when you deal with a leader. If you've a special application for hybrids, or you'd like to consider their adoption in your line, get in touch. Write A. R. Wartchow, Marketing Manager, Electroceramic Products. Ask for Centralab Bulletin No. 1429H.

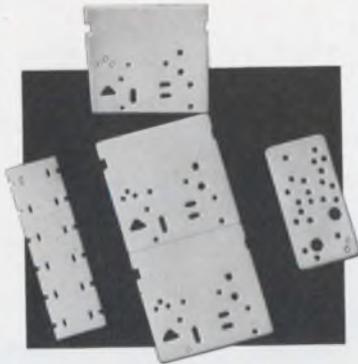


Hybrids sound good to music makers, too.



Centralab
perspective:

**Ceramic
Substrates/
ScoreStrates.®**



**Get your circuits
started right.**

Need ceramic substrates for your hybrid circuits? For resistor networks? Capacitor networks? Centralab's got them in every shape and size. In aluminas of 99.5% and 95%. Plain or metallized. With holes, slots, notches, scorelines or plain. With accurate dimensions and a surface finish compatible with your particular needs.

The pay off with Centralab is high performance reliability right from the start. So start right and specify Substrate/ScoreStrate ceramics from Centralab. You'll end up with the same high reliability substrate found in Centralab thick-film circuits (we're using them at the rate of 50 million per year).

For assistance on specifications, price and delivery, call Chuck Thompson, 414/228-2942 or write Centralab for Bulletin No. 1057TC.



Centralab
perspective:



Combination potentiometer and push button switch.

ULTRA-ONE™ pots.
The quiet one
is also
the quick one.

One look inside the Ultra-One $\frac{5}{8}$ -inch potentiometer tells you why it's the quiet one. The improved resistor system uses a smooth *conductive plastic element* and a *multi-fingered contact*. Result: CRV is virtually immeasurable throughout the long life of the pot.

The Ultra-One industrial potentiometer sets a new standard for design flexibility. The Quiet Pot. Quick delivery. Quite a combination! Other features include:

- 0.5% maximum noise through 100,000 \sim
- ± 250 PPM/ $^{\circ}$ C
- $\frac{1}{2}$ watt at 40 $^{\circ}$ C
- 500 volts DC
- $\Delta R < 10\%$ after load life
- $\Delta R < 10\%$ after 100,000 \sim

Write Centralab for Bulletin No. 1526P.



Centralab
perspective:

**Ultra-Kap™
capacitors.**
Low dissipation.
High insulation.



A dissipation factor as low as 3 percent maximum and high insulation resistance up to 1,000 megohms are only two critical design parameters met by Centralab Ultra-Kap capacitors. Also important is Y5F stability which is a maximum capacitance change of $\pm 7.5\%$ from +25 $^{\circ}$ C over a temperature range of -30 $^{\circ}$ C to +85 $^{\circ}$ C.

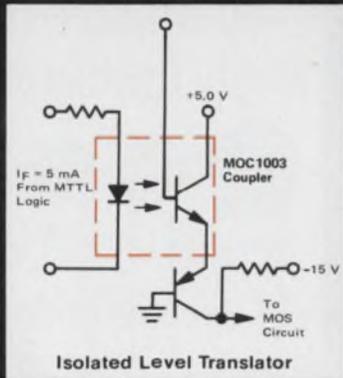
Centralab Ultra-Kap capacitors cost far less than Mylar® and multi-layer monolithic types. With all the function you want. In substantially smaller space, too. For example, you can get a .05 μ FD, 16 V capacitor in a .375 diameter disc.

Ultra-Kap capacitors are available in voltage ratings of 3, 12, 16, 25, and 50 V, with a choice of lead size and configuration, and in a selection of coating controls. Ask about the ratings, sizes and shapes you need.

Write Centralab for Bulletin No. 1106CA.

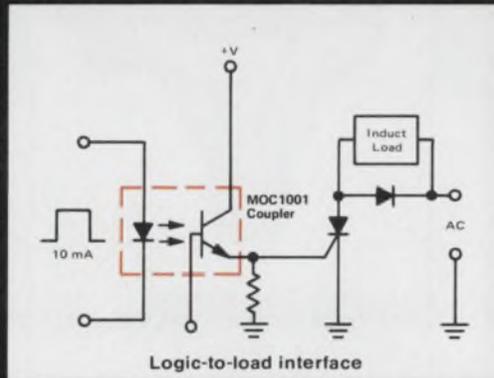


If you can't find the lowest-cost optical coupler, relay, switch, translator or interface you want here...



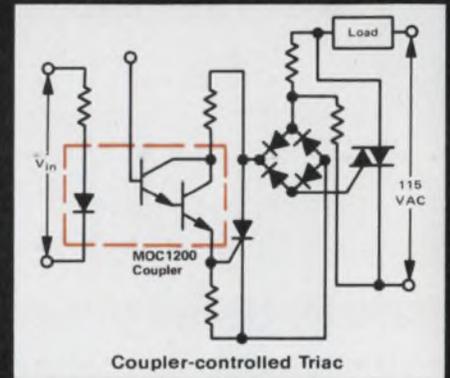
Isolated Level Translator

Type: MOC1003 Coupler
 Price: 99¢
 Features: 500 V Isolation
 30% Transfer Ratio



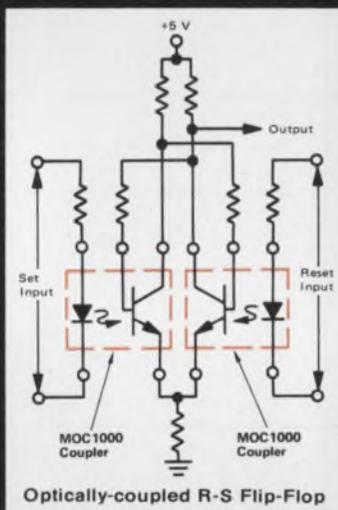
Logic-to-load interface

Type: MOC1001 Coupler
 Price: \$1.95
 Features: 2,500 V Isolation
 60% Transfer Ratio

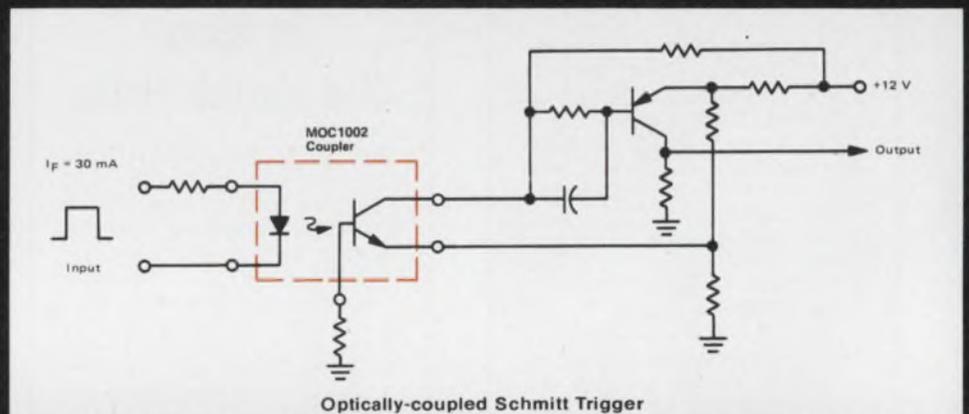


Coupler-controlled Triac

Type: MOC1200 Darlington Coupler
 Price: \$1.95
 Features: 1,500 V Isolation
 200% Transfer Ratio



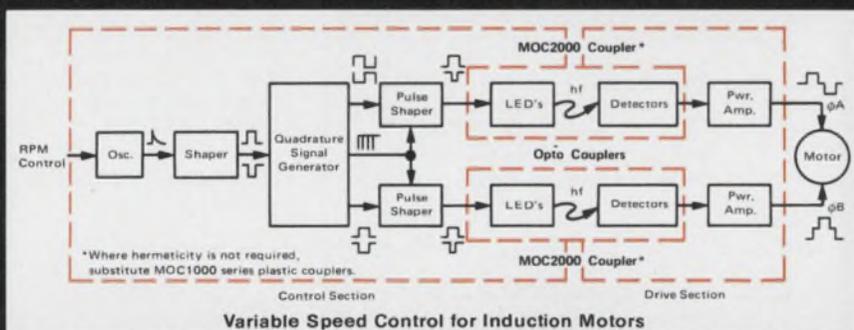
Optically-coupled R-S Flip-Flop



Optically-coupled Schmitt Trigger

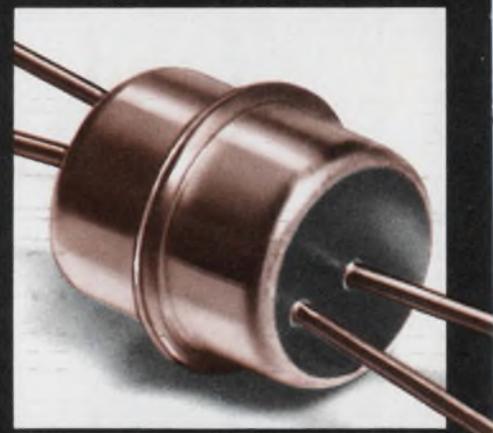
Type: MOC1000 Coupler
 Price: \$1.75
 Features: 1,500 V Isolation
 60% Transfer Ratio

Type: MOC1002 Coupler
 Price: \$1.50
 Features: 1,500 V Isolation
 30% Transfer Ratio



Variable Speed Control for Induction Motors

Type: MOC2000 Hermetic Coupler
 Price: \$3.10
 Features: 1,500 V Isolation
 3.0% Transfer Ratio



better have your isolation examined.

Optical couplers offer design engineers new freedom in designing circuits and systems. They're the only devices around that transfer, relay, couple, switch or isolate an electrical signal through the medium of light. They offer excellent input/output isolation . . . 100 billion ohms . . . and up to 2,500 V isolation voltage.

Call them what you will, they're versatile, quick, simple, reliable. And more economical than ever — Motorola prices now start at just 99¢, 100-up!

Problems such as ground loop isolation, common mode noise rejection, voltage level translation and many more can be solved or simplified using couplers.

In electro-mechanical relay replacement they offer unbeatable advantages. With no contacts,

they're immune to arcing and pitting and provide half the size and 1,000 times the speed of relays. There's no shock or vibration problems and they can be mounted in any position. Their inherently high isolation voltage permits operation in interface systems at different voltage levels and they're compatible with integrated circuits such as MOS, TTL, op amps and regulators.

Various responses can be achieved through linear modes of operation with feedback possible for inductive and reactive loads such as make/break timing designs. And with non-degrading solid-state operation, they're truly lifetime circuit performers.

Although of closed construction, they're simplicity itself. Coupler input is connected to a light emitter

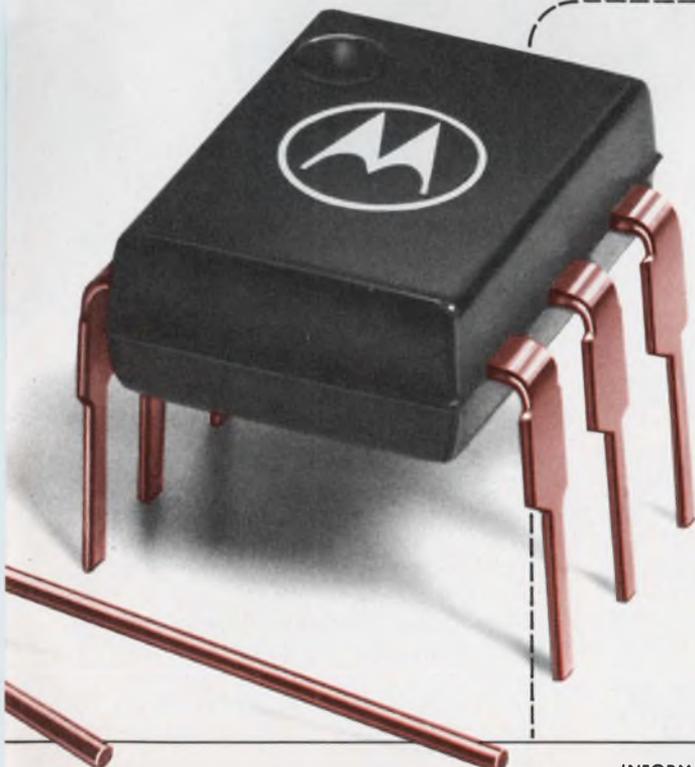
and the output is a photodetector transistor. The elements are separated by a transparent insulator and housed in a light excluding package. Once assembled, the device is completely electronic in nature, eliminating the designer's need for knowledge of optics.

For information about how they can fit into your system designs, write on your company letterhead to Motorola Semiconductor Products Inc., Box 20912, Phoenix, AZ 85036. We'll send three just-published design aids: OPTOELECTRONICS AT WORK, AN571 — Isolation Techniques Using Optical Couplers and AN575 — Variable Speed Control System For Induction Motors. Circle the reader number for data sheets.

All prices shown are 100-999.



MOTOROLA COUPLERS *— lighten your industrial load*



1 FREE OPTICAL COUPLER

. . . is yours when you contact the Motorola distributor nearest you. Call him or send the coupon for a free MOC-1003 optical coupler ready for evaluation and prototyping — do it now!

To (distributor) _____

Send me my free Motorola MOC1003 optical coupler immediately!

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(Offer expires January 31, 1973)

There's more to a Unimax product than meets the eye.



More quality. More reliability. More choice. More service.

When it comes to switches, you'll find that our models cover almost any conceivable snap-acting switch requirement.

BASIC PRECISION switches that are the first choice of the volume OEM users.

The most complete GENERAL PURPOSE line in the industry.

All styles of MINIATURE, SUBMINIATURE, and MINIATURE SUBMINIATURE types.

Big, rugged, METAL-CASED LIMIT

switches. Thousands of specials in minimum turn-around time, at minimum cost.

And to see the light, ask about our ILLUMINATED PUSHBUTTON CONTROLS. They offer you the broadest variety of styles in the business—in the widest choice of displays, colors, illuminations and actuations. From simple pilot light applications to the most

sophisticated multi lamp—multi switch—multi legend control, you'll find a Unimax LPB to meet your requirements. At a competitive price.

You'll also find special key lock or mushroom cap models. Mountings that are simplicity itself. Electrical and mechanical performances that are uniformly high.

Let us give you more. Write for detailed information concerning your applications to Unimax Switch Corporation, a Riker-Maxson Subsidiary, Ives Road, Wallingford, Conn. 06492. Or call (203) 269-8701.

 **Unimax**
We give you more.

INFORMATION RETRIEVAL NUMBER 198

If you're trying to create logic functions with your own hardwired circuitry, there's an easier way to go. Don't look now, but minicomputer state-of-the-art (and state-of-the-price) just caught up with your application.

The Naked Mini 8 is a computer that's a component. A powerful, fully-operational, byte-oriented, 8-bit computer. Completely tested and easy to interface. Ready to drop into your system like a simple component.

All you add is the power supply and control panel. Everything else is already there. A 1600 nanosecond cycle time, 4K core memory (expandable to 32K), fully-parallel broad-

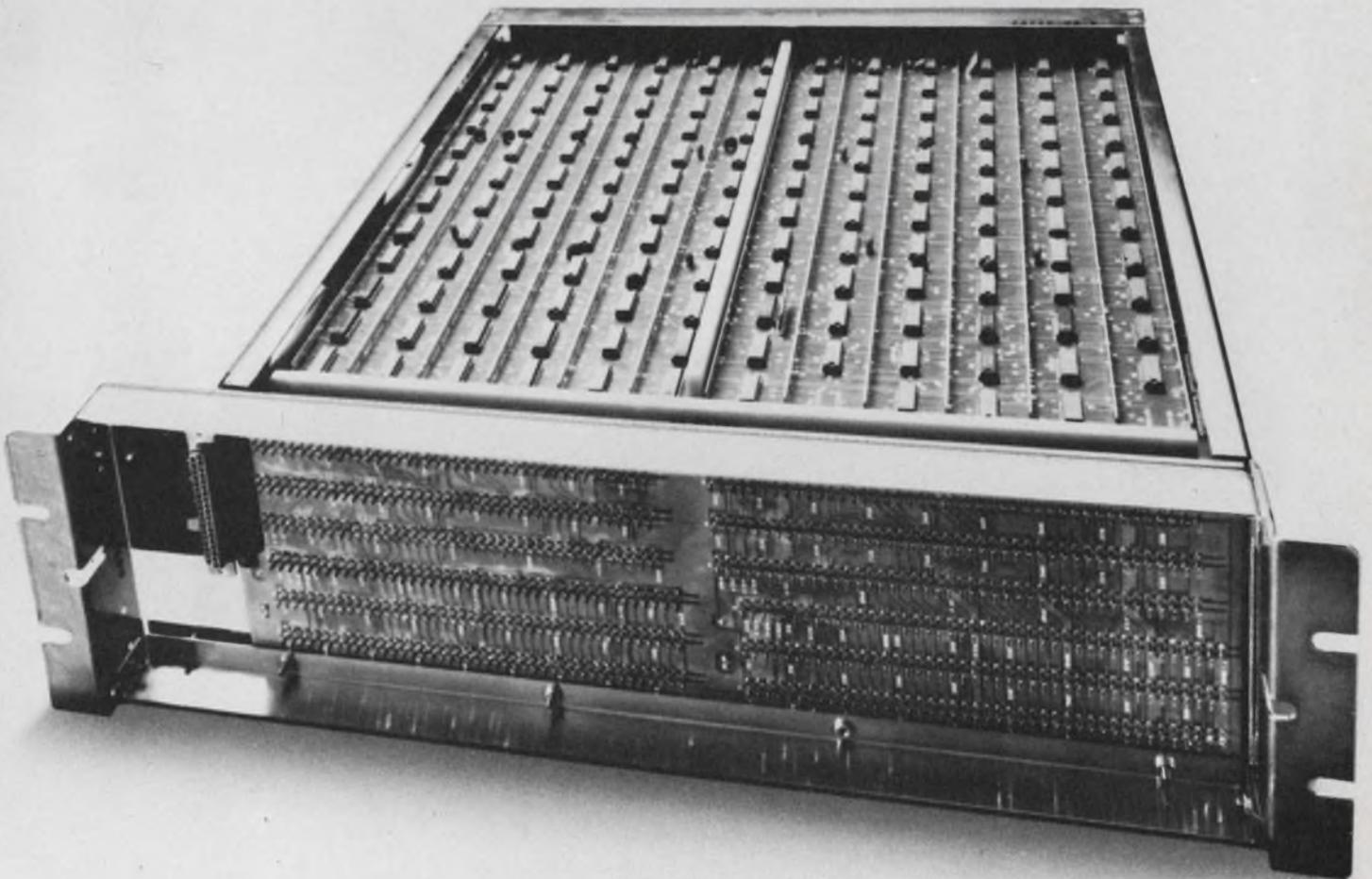
side I/O, three vectored priority interrupts, two direct memory channels, and an unconditional one-year warranty — the longest in the business.

In 200 unit OEM quantities, you get all of this and more for \$1450. For full specs and price lists, write today: Computer Automation, Inc., 18651 Von Karman, Irvine, California 92664. (714) 833-8830. TWX 910-595-1767.



COMPUTER AUTOMATION, INC.
the NAKED MINI company

The computer that's a component.



The NAKED MINI,TM \$1450.

Model 501

5MHz Function Generator with trigger/gate.

\$395



If you find that hard to believe, you know a lot about function generators.

But do you know about our modular solid state Model 501? And what it can do? It can make sine waves, square waves or triangles with variable offset or with DC. With symmetry control it can make pulses or ramps — and at rates to 5 MHz with our 1000:1 voltage generator control.

You can start and stop Model 501 as you choose with trigger / gate for one-pulse, tone bursts or synchronous timing. And you can add in your own signals to our built-in, input-summing, high-output wide-band amplifier.

What more could you ask for \$395?

If you're skeptical, that's fine. Because we'd like you to take Model 501 home with you and test it till your heart's content. Write or call today. Find out what Model 501 can do for you. And if you'd like the complete story on function generators, write for our "Free-folding, function generator guide."

We're making this offer because we have a theory—the more you know about function generators, the better for us.

WANT TO TEST MODEL 501? WRITE OR CALL AILTECH TODAY.

THE GOLD LINE SERIES FROM

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INFORMATION RETRIEVAL NUMBER 200

OTHER SOLID GOLD PRODUCTS FROM AILTECH INCLUDE SPECTRUM ANALYZERS, NOISE MEASUREMENT EQUIPMENT, RF POWER SOURCES, OSCILLATORS AND TRANSDUCERS.

Fluke problem solvers

The new multimeter with advanced L.S.I. for more function power. 26 ranges, 5 functions.



\$299... Fluke's new 8000A, Try one for fifteen days, no obligation.

Now you can put the unmatched quality of Fluke instrumentation to work for you at the price of an ordinary multimeter.

Here's the DMM with more function power. Its got 26 ranges, including five ranges of ac and dc volts, five

ranges of ac and dc current, and six ranges of resistance. Push button control gives you the simplest most reliable error-free operation possible. The new Fluke 8000A is the only multimeter using an A-to-D converter with inherent self-zeroing to com-

pletely eliminate offset uncertainty.

More details are on the next page, but we think you'll want to try this low-priced measurement system now. Fill in the coupon; we'll do the rest.

Circle 240 for more information

Ship me a Fluke 8000A for \$299 plus \$_____ for additional options checked below. I prefer the following payment option:

Charge my Master Charge, BankAmericard, or American Express account for the full amount plus \$5 shipping and handling.

If using Master Charge, please indicate the 4 digit number appearing above your name

Bill against the attached company purchase order for the full amount plus \$5 shipping and handling.

Cash Order. My check for the full amount is enclosed. Fluke pays shipping and handling.

(Washington state residents add 5% sales tax.)

Return within 15 days for full refund if not delighted.

Add the following options:

- | | |
|---|---|
| <input type="checkbox"/> Rechargeable Battery — \$50* | <input type="checkbox"/> Carrying Case — \$15 |
| <input type="checkbox"/> BCD Data Output — \$75* | <input type="checkbox"/> Dust Cover — \$8 |
| <input type="checkbox"/> RF Probe — \$75 | <input type="checkbox"/> Rack Kit-Center — \$30 |
| <input type="checkbox"/> AC Probe 20A & 200A — \$50 | <input type="checkbox"/> Rack Kit — 1/2 Rt or Left — \$30 |
| <input type="checkbox"/> HV Probe — \$25 | <input type="checkbox"/> Send me literature only |
| <input type="checkbox"/> Deluxe Test Leads — \$5 | |

*Choose BCD data output or battery pack; both cannot be ordered in the same instrument.

Name _____

Company/Institution _____

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City & State _____ Zip _____

Credit Card No. _____ Phone _____

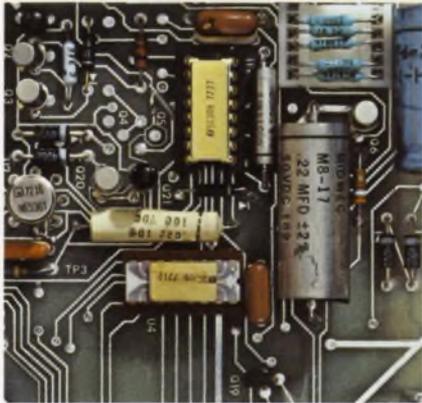
(Signature authorizing charge to credit card) _____

For even more convenience, let your nearby Fluke sales office handle the details. For location, dial toll-free 800-426-0361.



When you look inside you'll find the same high technology and quality we put in our \$3000 DVM's.

Take a look inside. The LSI chips, equivalent to over 3,000 circuit elements, are the most advanced proven semiconductor devices on the market today. Fluke is the only manufacturer using **both analog LSI and digital LSI** to give you increased reliability at lower cost with fewer parts. The Fluke 8000A has only 1/3 the number of parts used in a typical 3 1/2 digit multimeter.



A simple guarantee

You can understand our 12-month guarantee. It's straightforward and honest. And you can believe we live up to it. If anything happens to your 8000A, take it or send it to your nearest factory service center. We'll give you 48-hour turnaround service in the U.S., Canada, Europe and the Far East.

Specs to work by

The new Fluke 8000A has a dc accuracy of 0.1% when you buy it. We guarantee it will still measure within that accuracy without recalibration a year later.

The case is rugged and tough. Drop this multimeter from a bench. Nothing happens to the works inside. We guarantee it.

Wide range of measurements

Measurement flexibility is broad enough to meet all the situations you're likely to encounter. The Fluke 8000A gives you 26 ranges to measure ac and dc voltages from 100 microvolts to 1200 volts, currents from 100 nanoamps to 2 amperes; and resistance from 100 milliohms to 20 megohms.



Wide choice of options

For a few dollars more, you can add a rechargeable battery pack to give you completely portable operation for over eight hours. And when you're back on the line, the batteries will recharge automatically. Other options include digital printer output, deluxe test leads, high voltage probe, rf probe, 200-amp ac probe, carrying case and rack mount kits.



A complete digital multimeter

But with or without options, the Fluke 8000A comes complete with test leads and spare fuses. It all adds up to an instrument you can count on day after day, year after year. Isn't this what you want in a digital multimeter at any price? Fluke thinks so.

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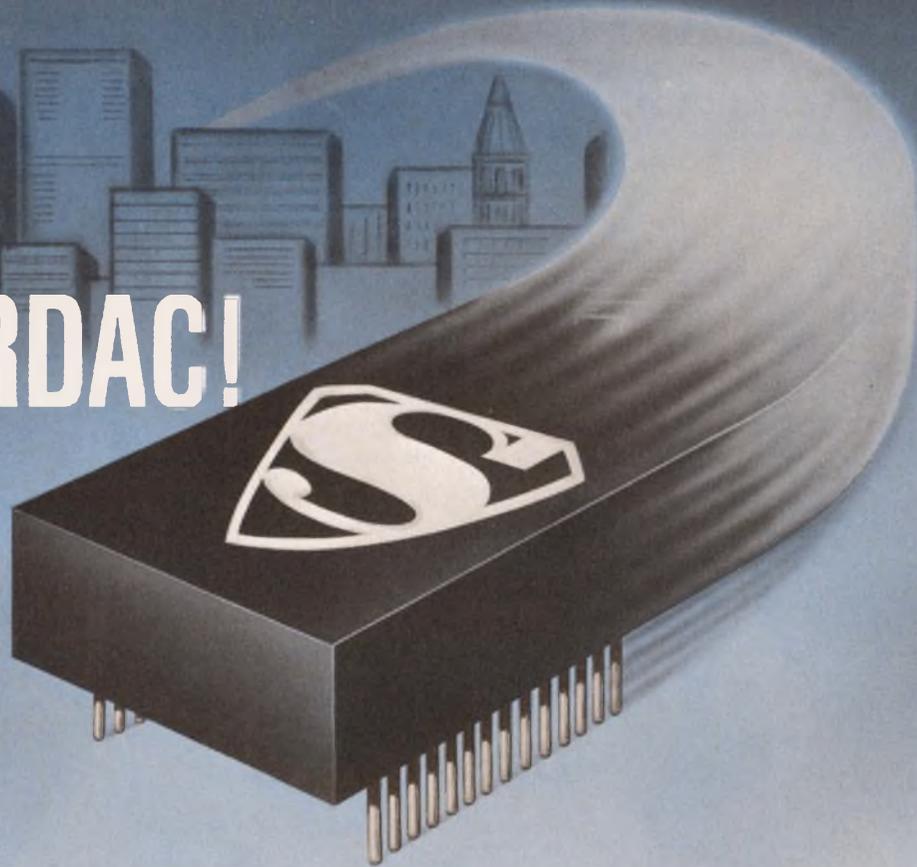
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...it's SUPERDAC!



There are quite a few manufacturers of D/A Converters today. Some large, some small. They come and they go. But there aren't many who can give you the benefits of seven years of experience in this technology . . . benefits such as reliability, long life, stability.

Sprague SUPERDACs from 8 to 12 bits with settling times to 2 μ s are in full production. Reference voltage adjustable to +18V. They're priced competitively with discretely—with this difference: the performance, precision, and stability inherent in a well-engineered product are free. Here's your chance to gain from Sprague's sophistication in D/A Converter design and manufacture.

UP WITH PERFORMANCE . . . All internal devices hermetically-sealed and designed to meet the most stringent environments or exceed MIL-STD-883 requirements.

UP WITH PRECISION . . . Voltage offsets less than 5 mV. Resistors laser-adjusted to achieve typically $\pm 0.1\%$ resistance tolerance and matching to within $\pm 0.01\%$. Proprietary monolithic IC ladder switches and buffer amplifiers are also featured.

UP WITH STABILITY . . . Operating temperatures are -55 C to $+125$ C for ± 1 LSB accuracy, or -25 C to $+100$ C for $\pm 1/2$ LSB accuracy.

. . . AND AWAY WITH DISCRETE PRICES . . . Compare Sprague's price/performance/size with those of any other manufacturer. Prices are as low as \$2.50/bit. Then choose SUPERDAC . . . for signal processing, servo position, process control, and modems, to name a few applications.

Sprague Catalog Number	Resolution	Settling Time to $\pm 1/2$ LSB (μ s)	External Reference Voltage	Full Scale Output	Temp. Coeff. (1) (ppm/ $^{\circ}$ C)	Unit Price (1-24)
FIXED REFERENCE						
UHM-532A	12-bit/3-digit	15	-10	-10	1	\$42.20
UHM-533A ⁽³⁾	12-bit/3-digit	15	-10	± 10	3	50.40
UHM-503A	10-bit	2	-10	-10	1	36.00
UHM-506A ⁽³⁾	10-bit	2	-10	± 10	3	42.20
UHM-523A	8-bit/2-digit	2	-10	-10	1	28.80
UHM-526A ⁽³⁾	8-bit/2-digit	2	-10	± 10	3	36.00
4-QUADRANT MULTIPLYING^{(2) (3) (4)}						
UHM-412	12-bit/3-digit	20	$\pm 10V/20V$ p-p	± 10	3	86.33
UHM-409	10-bit	20	$\pm 10V/20V$ p-p	± 10	3	71.92
UHM-408	8-bit/2-digit	20	$\pm 10V/20V$ p-p	± 10	3	57.53

(1) $\pm 1/2$ LSB Linearity
(3) Includes Op Amp

(2) DTL/TTL/CMOS (Neg. Logic) Input Compatible

(4) Multiply D/A Output Swing Adjustable to $\pm 18V$ Max.

Standard Size: $1\frac{1}{2}$ " x 2" (1 " x $1\frac{1}{2}$ " Available on Special Order).

Inputs Available: Binary, BCD and on Models with Op Amp, Offset Binary.

Power Supply: $\pm 15V$ (Fixed Reference DACs Available with +4, -20V supply), Multiply D/A Accept Reference Variable to $\pm 18V$.

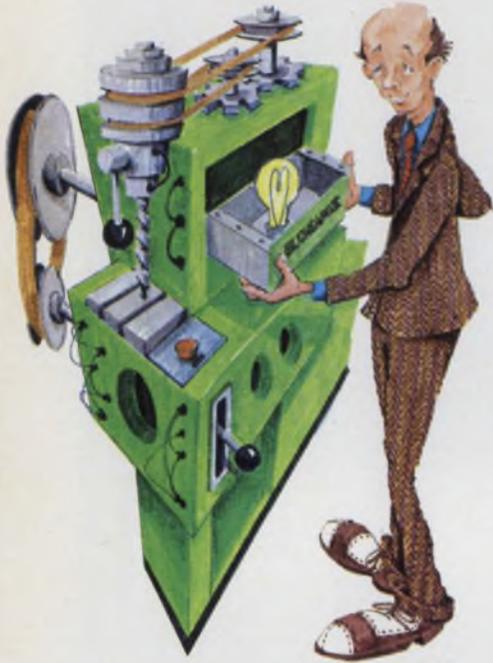
The same technology that makes this series provides a complete family of successive approximation A/D converters, with current-summing capability and custom engineering as well.

For complete information, call or write Ron Beck, Semiconductor Division, Sprague Electric Co., 115 Northeast Cutoff, Worcester, Mass. 01606. Tel. 617/853-5000.



Analog Products for Signal Processing

What the industry taught us about cheap OEM minicomputers.



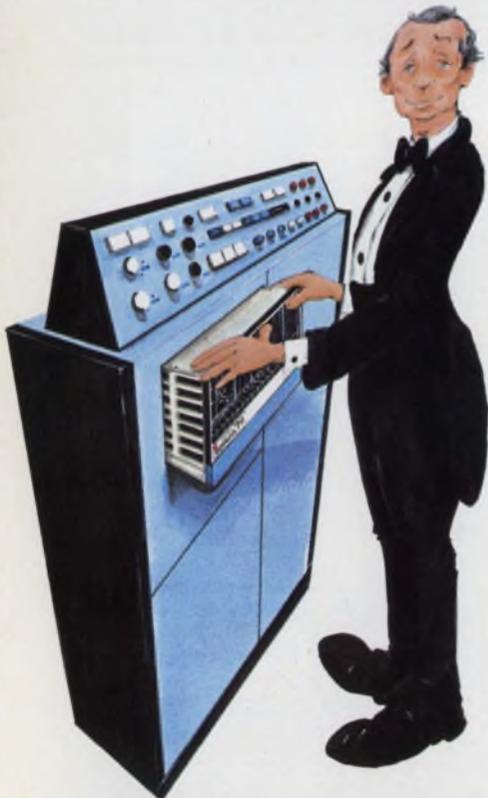
Stripped for action.

Here's a familiar approach. El Cheapo II. In reality, it's the good old Mod X stripped of all the stuff that made the old Mod X good. Instructions. Memory. I/O facilities. Everything. But it's cheap. It's really cheap. Only the hum remains.

Dressed to kill.

Here's the same machine in disguise. Now it's hiding behind all the things you have to hang on it to make it work. Like a power supply and a memory and some sort of I/O kluge so your system can talk to it.

Also hidden, of course, is the cost. And it isn't so cheap any more.



Introducing the \$3600 Interdata Model 74. What you need is what you get.

Here's a new approach.

A \$3600* general-purpose OEM minicomputer with the much-copied third generation architecture of the Interdata New Series family of minicomputers.

And that \$3600 — lowest in its class — includes hardware multiply/divide, 16 general registers, directly addressable 8KB core expandable to 64KB, an 80-ns solid-state Read-Only-Memory and a multiplexor that provides an I/O system for communicating with up to 255 peripheral-oriented device controllers.

We've even made the display panel optional because most OEMs don't need it. And what you need is what you get.

At \$3600, maybe we'll teach the industry a thing or two.

INTERDATA

2 Crescent Place, Oceanport, New Jersey 07757 (201) 229-4040. Atlanta — (404) 288-7000. Boston — (617) 890-0557. Chicago — (312) 437-5120. Dallas — (214) 238-9656. Detroit — (313) 356-5515. Houston — (713) 783-1830. Los Angeles — (213) 640-0451. Palo Alto — (415) 969-1180. Washington — (703) 525-4806. Toronto — (416) 678-1500. United Kingdom — Uxbridge 51483. Sydney — NSW 439-4155. West Germany — 0811/160031. Tokyo — 270-7711.

*Basic 8KB Model 74 list.
With OEM discount, quantity of 18 — \$2,520.00.

(continued from page 16)

those High Flyers," (ED 23, Nov. 9, 1972, p. 51). As one of the guys you're talking about in a fledgling company, it is easy to verify your remarks.

During the last two years many engineers have been crying about unemployment, loss of pension rights when changing companies and other things of a less critical nature. For people who had to work long and hard to get that paper attesting that they are engineers, it seems they have lost their drive. Your editorial points out an experience they should have: There is no better way to gain an understanding of the problems of management than to get into the thick of the battle to start and mature a new company.

The easy thing is to complain. From personal experience, it is much harder to crack the nut of a new company.

Harold F. Shultz

Vice President, Marketing

Emhiser Rand Industries

7721 Convoy Court

San Diego, Calif. 92111.

About those keyboards by Donnelly Mirrors . . .

Your article on keyboards in the Nov. 9 issue ("Focus on Keyboards," ED 23, p. 54) made reference to Donnelly Mirrors keyboards as an elastic diaphragm type with high contact resistance and a spongy touch. It also related them to low-cost pocket and desk-top calculators.

In fact, Donnelly Mirrors keyboards employ gold-plated, hard contacts with their associated low contact resistance, have a touch comparable to the most expensive solid-state keyboards and have application mostly in computer-related equipment. The keyboards do employ an integral, laminated switch structure, from which they gain their low profile and competitive price.

Derek J. Hatley

Manager of Electronic Development
Donnelly Mirrors, Inc.
Electronics Div.
611 Ottawa Ave.
Holland, Mich. 49423.



Stacked...with beautiful curves!

(stacked-foil construction with ultra-low impedance, ultra-low ESR, ultra-low inductance)

Revolutionary new Type 432D COMPULYTIC® Aluminum Electrolytic Capacitors offer capacitance values to 100,000 μ F with equivalent series resistance of typically less than 0.001 ohm and inductance of only 1 nH in a 3" x 5½" case. This same capacitor will handle 93 amperes of ripple current at 65 C and 1 kHz.

Impedance limits at 10 kHz are as low as 0.001 ohm with typical values of only half of the specified limits.

Terminals are ideal for use with laminated-bus power distribution systems found in modern EDP equipment, where the low ESR and impedance of Compulytic capacitors help insure continued operation of logic circuits even during momentary power outages.

Sprague Type 432D Capacitors are available in nine voltage ratings from 5 to 50 volts d-c, and are designed for operation over the temperature range from -40 to +85 C.

For complete technical data, write for Engineering Bulletin 3443 to: Technical Literature Service, Sprague Electric Co., 347 Marshall St., North Adams, Mass. 01247.

THE BROAD-LINE PRODUCER OF ELECTRONIC PARTS



INFORMATION RETRIEVAL NUMBER 14

SCHOTTKY ON



One-stop TTL shopping for 74S MSI, SSI...

At last. Available now, all in one place. The whole mix in Schottky logic—to match every high speed TTL function in demand today. Signetics

broad line of 74S circuits. Plus our compatible 82S series of enhanced MSI devices that help Schottky give you a competitive step-up in speed, in design-ease, in versatility... and of course, in MSI complexity.

And you get it where you want it, when you want it. Fast service directly from distributor stock. Signetics knocks off the waiting list tie-ups, the multi-stop shopping. After all, how can we encourage you to boost system speed by replacing TTL with Schottky equivalents, if you can't get the circuits to work with? All the parts you need—without delays, without runarounds, without making six calls when one should do the job.

Here's where Signetics makes the difference. One call does the job. Completely. SSI Schottky to cover full function range:



SSI SCHOTTKY 74S TTL

74S00	Quad 2-Input NAND Gate
74S03	Quad 2-Input NAND Gate (Open Collector)
74S04	Hex - Inverter
74S05	Hex - Inverter (Open Collector)
74S10	Triple 3-Input NAND Gate
74S11	Triple 3-Input Positive AND Gate
74S15	Triple 3-Input Positive AND Gate (Open Collector)
74S20	Dual 4-Input NAND Gate
74S64	4-2-3-2-Input AND/OR/INVERT Gate
74S65	4-2-3-2-Input AND/OR/INVERT Gate
74S74	Dual D-Type Edge-Triggered Flip-Flop
74S112	Dual J-K Edge-Triggered Flip-Flop
74S113	Dual J-K Edge-Triggered Flip-Flop
74S114	Dual J-K Edge-Triggered Flip-Flop
74S40	Dual 4-Input NAND Buffer
74S140	Dual 4-Input NAND Line Driver

You can make the same call encompass MSI too. Signetics 74S MSI circuits offer the same volume availability as SSI, as well as the same total TTL compatibility—pin-for-pin fits with standard TTL and low-power Schottky. Ten MSI devices in stock now, with more to be announced in the next few months.

MSI SCHOTTKY 74S TTL

74S151	8-Input Data Selector/Multiplexer
74S153	Dual 4-Input-to-1-Line Selector/Multiplexer
74S157	Quad 2-Line-to-1-Line Data Selector/Multiplexer
74S158	Quad 2-Line-to-1-Line Selector/Multiplexer (Inverting)
74S174	Hex D-Type Flip-Flop w/Clear
74S175	Quad D-Type Flip-Flop w/Clear
*74S181	Arithmetic Logic
*74S194	4-Bit Bidirectional Shift Register
*74S195	4-Bit Parallel Access Shift Register
74S251	8-Input Data Selector/Multiplexer w/tri-state
74S253	Dual 4-Input-to-1-Line Selector/Multiplexer w/tri-state
74S257	Quad 2-Line-to-1-Line Data Selector/Multiplexer w/tri-state outputs
74S258	Quad 2-Line-to-1-Line Selector/Multiplexer (Inverting) w/tri-state

*January-February announcement

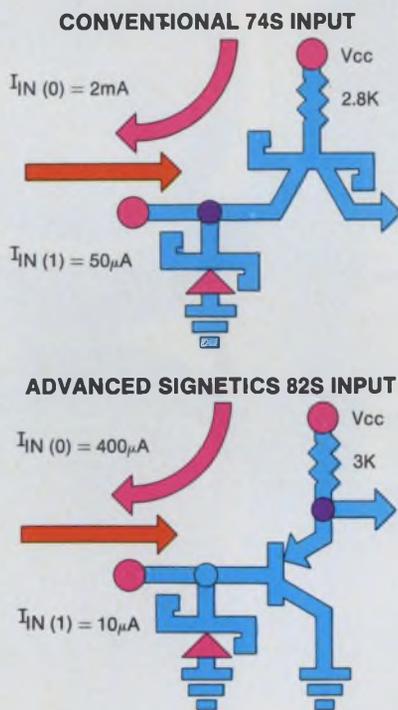
Complementing 74S, Signetics 82S series MSI circuits offer significant advantages in sophisticated Schottky systems designs. The conventional TTL input circuit found in all Schottky logic, other than Signetics 82S, suffers from low input impedance.

Signetics advanced PNP structure produces significantly higher input impedance. You can drive far more devices from one output since input current is one-fifth that of standard Schottky inputs. With Signetics 82S MSI you need not worry about noise when driving long lines since, in addition to 10 PNP loads, a termination resistor can be accommodated when needed without fan-out reduction.



THE DOUBLE.

...and now optimized 82S MSI too.



The growing line of 82S includes ultra high speed pin-for-pin replacements for the popular 8200 series MSI. In addition, the 82S90/91 100 MHz counter will replace the 74196/197, and the 82S70/71 70 MHz shift register will replace the 74178/179 in systems requiring improved speed performance.

The BCD arithmetic unit 82S82 replaces at least six MSI packages previously needed for the same function while at the same time operating speed is improved by a factor of 3. For BCD applications that only require addition, the 82S83 adder will replace three MSI circuits, and double operating speed. The 82S62 parity generator/checker is unsurpassed in speed.

Of course the 82S MSI line interfaces with 74S logic directly, operating in the same design environment as all 7400 circuitry but with the added advantage of direct replacement without violating fan-out rules.

MSI SCHOTTKY 82S TTL		SPEED
82S30/31/32	8-Input Digital Multiplexer	15 ns
82S33/34	2-Input, 4-Bit Digital Multiplexer	15 ns
82S41/42	Quad Exclusive-OR/Quad Exclusive-NOR	5 ns
82S50/52	Binary-to-Octal/BCD-to-Decimal Decoder	12 ns
82S62	9-Bit Parity Generator / Checker	17 ns
82S66/67	2-Input, 4-Bit Digital Multiplexer	15 ns
82S70/71	4-Bit Shift Register	70 MHz
82S82	BCD Arithmetic Unit	20 ns
82S83	BCD Adder	20 ns
82S90/91	Presetable Decade/Binary Counter	100 MHz

74S/82S Schottky TTL. Just one call to one of our distributors, reps or salesmen. And Signetics puts it on the line. Your line.

Signetics-Schottky 811 East Arques Avenue Sunnyvale, California 94086		
High speed response requested on Schottky TTL data, specs, applications and delivery for 74S SSI, 74S MSI and 82S MSI.		
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Company		
Address		
City	State	Zip
Telephone		
<small>Signetics Corporation, a subsidiary of Corning Glass Works.</small>		

signetics

The 5 fastest ways to make better inverters.

1 The new 81RM — fastest 125 Amp inverter SCR around.

It has $20\mu\text{S}$ turn-off, through 1000V, with efficiency that cuts filtering, commutating and snubbing costs up to 30% in new designs. Plugged into existing circuits, it can increase overload capability or power rating by 50%. Its 30% lower switching losses let you operate efficiently at 10KHz. And for today's circuits, a guaranteed turn-off time of $25\mu\text{S}$ with an antiparallel diode gives unequalled speed. The best "soft recovery" in the business assures the lowest RFI generation, minimizes false triggering and improves reliability. Voltage ratings from 100-1000V. dv/dt is $200\text{V}/\mu\text{S}$, and di/dt is $800\text{A}/\mu\text{S}$.

2 New 35 Amp IR140/141's. None faster. Lowest switching losses.

At $15\mu\text{S}$ and $10\mu\text{S}$ turn-off, there are no faster SCRs in their range. But what really sets them apart is the 30% lower switching loss for unequalled efficiency at high frequencies. No derating to 4KHz, and 50% of the rated current at 20KHz. Excellent as commutating SCRs. Conforms to JEDEC 2N3649-58. Reapplied dv/dt is $200\text{V}/\mu\text{S}$, and di/dt is $400\text{A}/\mu\text{S}$. Voltage ratings: 50-400V.

To get our Inverter SCR "Data pack" fast, write Dept. ED

International Rectifier
233 Kansas Street
El Segundo, CA 90245

New — The fastest Turn-Off ($10\mu\text{S}$) high-current inverter SCRs available!

These low-frequency inverter SCRs turn off four times faster than others at their power level. You can reduce commutating component size and cost $\frac{1}{3}$ and still increase inverter ratings with greater reliability. Higher surge ratings give you bigger safety margins, easier fuse selection. To top it off, you can choose from three package types in 50-600V ratings to optimize your design.

3 New 430 Amp (RMS), 275RF Series. The only stud-mounted 430 Amp (RMS) inverter SCR available. 7000 Amp surge rating. $200,000\text{A}^2\text{Sec}$. I^2t rating.

4 New 710 Amp (RMS), 450PF Series. Rated 710 Amp (RMS), this ceramic "Hockey Puk" has a surge rating of 9000 Amps and I^2t of $340,000\text{A}^2\text{Sec}$.

5 New 710 Amp (RMS), 451PF Series. For maximum economy, the first and only plastic encapsulated 710 Amp (RMS) "Hockey Puk" SCR. Surge rating: 9000 Amps. I^2t is $340,000\text{A}^2\text{Sec}$.



International Rectifier

... the innovative power people 

Kurz-Kasch Digital Logic Instruments*



... complete logic systems analysis through the logic-probe concept

Rugged, all solid-state, Kurz-Kasch logic probes are designed for fast, accurate testing of logic levels in all types of integrated circuit systems. A simple readout system indicates "true", "zero", or "pulse" readings precisely through color-coded visual electronic readouts in the probe tip. Absence of logic levels is indicated by all readouts remaining OFF.

Applications Logic levels can be accurately tested in virtually any (DTL, TTL, RTL) IC system including desk calculators, business machines, N/C devices, computers or telephone systems. Power is derived from the unit under test allowing use in the field or in the lab.

Specifications

Readout Light Red = Logic "1"
Readout Light White = Logic "0"
No Readout Light = "infinity"

High input impedance prevents loading of circuit under test.
Size $\frac{3}{16}$ " dia., 6" long, 26 $\frac{3}{4}$ " leads with pin terminals

A pulse detection feature is available on most models of logic probe. A third readout is provided to display high speed pulse trains or a single cycle pulse of less than 50 nanoseconds on the standard Model LP-520. Overload protection to +50, -20 volts DC is also available.

Standard Probes Logic probes are presently available in five standard models. MODEL LP-500 for use in testing 4.75-5.0 V DC logic systems. MODEL LP-510 for testing 4.75-5.0 V DC systems . . . includes overload protection to +50, -20 V DC. MODEL LP-520 . . . for 4.75-5.0 V DC logic systems . . . includes overload protection and pulse detection features. MODEL LP-530 for testing of 12-15 V DC logic systems . . . includes overload protection to +50, -20 V DC. MODEL LP-540 . . . for 12-15 V DC systems . . . includes overload protection and pulse detection features.

Add these options: G-S-M: Gating Feature (-G)— 3 Channel input for timing. Pulse indicator displays only when probe tip and gate/gates are in coincidence. **Memory & Stretch (-M)**— Push-pull switch for selecting stretch or latch mode. Stretch mode detects high speed pulse and displays blue "P" lamp for 200 mS. Latch mode captures high speed pulse/trains and latches blue "P" on until reset. **5 Nano-second capability (-S)**— Allows detection of pulses up to 10 x faster than standard probes. Each option \$10.00.

Special Probes As a routine service, Kurz-Kasch will custom design logic probes to user specifications. Custom designs can include: both positive and negative logic levels from 50 to 30 volts . . . special pulse detection characteristics . . . floating or grounded cases . . . custom power supply requirements . . . power lead reversal protection . . . and your choice of logic crossover parameters.

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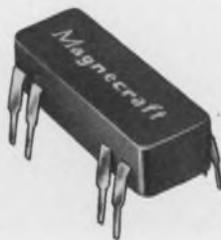
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Which semis for cars? Panel to debate issues

It's widely predicted that the automobile industry will be using semiconductors in voluminous quantities before long. But what kind of semiconductors—custom or off-the-shelf, digital or linear? Questions like these will stir controversy next month at a panel discussion at the 1973 IEEE International Solid-State Circuits Conference.

One member of the panel—Tom Frederiksen, head of National Semiconductor's Automotive Linear Integrated Circuit Dept. in Santa Clara, Calif.—says that off-the-shelf building blocks are a logical choice. Because of legislative and competitive pressures and because system design is subject to change during the development cycle, he notes, such standard ICs offer flexibility and short turn-around times that would be difficult to achieve with custom devices.

Another panel member—Peter Ansbro, manager of automotive programs for Philco-Ford, Dearborn, Mich.—disagrees. While conceding longer turn-around times and less flexibility, he argues that the advantages of custom ICs outweigh the disadvantages. He cites lower cost, easier assembly and a lower parts count.

Ansbro sees the building-block technique being used only as a stopgap for optional equipment. But once a feature becomes standard equipment on all cars, it is a lot cheaper to develop a custom IC to do the job, Ansbro asserts.

As far as which semiconductor technology to use—bipolar or CMOS—Ansbro says the automobile manufacturer doesn't really care: He merely orders a "black box" that meets certain requirements and either of the two competing technologies are satisfactory.

Whatever technology is used, the

potential size of the automotive market is staggering, Frederiksen says, "Even if all the semiconductor manufacturers got along well and cooperated to the fullest," he notes, "it would be hard to meet the volume demand of the automotive industry."

Quoting generally accepted estimates of the number of cars produced annually and estimating 10 ICs per car, Frederiksen predicts that about 120 million ICs will be needed each year—two to four times what the semiconductor industry is producing today. This means, he points out, that a tremendous expansion must take place.

Another topic that the panel will investigate is how to achieve compatibility between the emerging electronics and the noisy electrical environment of the car. The chairman of the session—Will Steffe of Fairchild Semiconductor, Mountain View, Calif.—favors a systems engineering approach. This way, he says, problems such as 250-V transients which are sometimes produced by the alternator can be eliminated at the source and not at each individual piece of electronic equipment.

Ansbro agrees and says that a systems approach will likely emerge in two to three years.

The conference is being held Feb. 14-16 in Philadelphia, and the panel discussion the evening of Feb. 14.

AF automates watch on celestial events

To speed predictions of celestial events that can disrupt or black out military communications around the world—like solar flares—the Air Force has acquired a new Automated Astrogeophysical Data Processing System.

The new system, developed by the Air Force Cambridge Research Laboratories scientists and the Air Weather Service, uses 26 programs that have taken several years to write. The system will be used at the Global Weather Central Station, Offutt Air Force Base, Nebraska, to sort, decode, analyze and display the outputs of many space monitoring instruments.

"By eliminating many of the manual plotting and updating chores, the forecaster will be free to analyze the data more accurately and react faster to critical conditions," says Robert A. Skrivanek, a member of the space forecasting group who helped prepare the new program at the Cambridge Laboratories.

A basic problem with previous forecasting of celestial events has been that data from observation stations and ground-based sensors have been delivered in widely varying forms of time and magnitude not related to one another. By the time forecasters have been able to decipher and evaluate the data and reduce it to meaningful form, the event may already have passed.

Among the diverse information that the new system will digest are X-ray and particle data from monitors on the Vela satellite, ground-based optical data from telescopes monitoring the sun and from telescopes, and data from ionosons, or ground-based sounders, that indicate the state of the ionosphere.

UV process speeds photoresist removal

A new "ultraviolet depolymerization" process is reported to speed and simplify the removal of plastic photoresist material from semiconductor wafers.

Current widely used methods for removing photoresists call for either soaking the polymer film in a solvent that causes it to swell, after which it is shaken or abraded off, or dipping the film in an acid solvent, which destroys it.

In many cases, however, a semiconductor manufacturer would prefer to remove the photoresist without subjecting the substrate to solvents or acids. This is particularly important where soft metal

overlays are present and they would be damaged by abrasion or corrosive solvents, or where carbon contaminants would interfere with subsequent fabrication steps.

The new process developed by Dr. Donald A. Bolon, a scientist at the General Electric Research and Development Center in Schenectady, N.Y., uses intense ultraviolet light in the presence of air to break down and vaporize the photoresist material.

A typical plastic film—depending upon the composition and thickness—can be completely removed from a semiconductor wafer in 25 to 30 minutes, according to Bolon.

This process, he notes, is the first that lends itself to the continuous removal of excess photoresist. All other known techniques require the processing of wafers in batches and are therefore inherently slower. Also, Bolon says, his is the first dry-process technique that operates at atmospheric pressure and at modest temperatures (about 250 C).

Tests at the GE Research and Development Center show that ultraviolet removal of photoresists proceeds at a rate of about 1000 Å per minute. However, Dr. Bolon points out, the process can be made to operate 10 times faster by the injection of about 2% ozone gas into the processing chamber.

Laser airspeed meter being tested by NASA

A laser airspeed indicator accurate to within 0.1%—10 times more precise than the best systems now in use in commercial aircraft—is being tested by the National Aeronautics and Space Administration at its Ames Research Center, Mountain View, Calif. It will be used in aircraft research programs where small performance changes caused by subtle design changes must be evaluated.

The system, developed by Honeywell's Systems and Research Center in Minneapolis, focuses a carbon-dioxide laser beam 20 meters ahead of the aircraft, where the air is undisturbed by the bow wave of the fuselage. The system's infrared sensor detects backscatter from aerosols—particles of moisture—in the atmosphere and measures a

doppler shift in frequency that is proportional to the aircraft speed.

Tests conducted in clear air with a visibility of 30 miles gave accurate readings at speeds of 10 to 520 mph at altitudes up to 10,000 feet.

The system itself consists of the carbon-dioxide laser, an optical system made up of a co-linear transmitting and receiving telescope, an infrared window, an infrared detector and electronics for tracking the frequency shift and presenting results digitally.

BART system problems under close scrutiny

Hearings are currently underway at the California Public Utilities Commission to get to the bottom of allegations that Bay Area Rapid Transit (BART) system is unreliable and unsafe. The hearings come two months after the accident last October 2 in which a BART train ran off an embankment.

Critics of BART have noted that the system seems to have insufficient redundancy or backup capability and is incapable of detecting a "dead" or disabled car on the track.

Although, not part of the contract, dead car detection is currently under study by the prime contractor for train control on Bart, Westinghouse Electric Co. of Pittsburgh.

Contacted by ELECTRONIC DESIGN, Howard Miller, the division engineering manager for Westinghouse in Emeryville, Calif., admitted: "We have had some problems with reliability in the train control, propulsion and other electronic systems. Besides the malfunctioning crystal that caused the accident, we've found several other minor problems that are now being corrected. As in all electronic systems, problems pop up that were never anticipated theoretically and in laboratory tests."

Miller pointed out that typical of the problems is a diode used for transistor protection which has been burning out due to noise spikes. This diode is being replaced.

Other problems have involved connectors shielding and various other components. Miller emphati-

cally states that none of the problems so far detected, other than the malfunctioning crystal that caused the train accident, can compromise system safety.

Inability to detect a dead car—one that is drawing no third rail power—results from a rust film buildup on the wheels of the car and on the tracks. This film increases the shunt impedance that the car presents across the track from a few milliohms to a few ohms.

Car detection is by a conventional fixed block technique, a block being a given number of feet of track. At the beginning of the block a transmitter sends a coded ac signal down the track to a receiver at the end of the block. A train in the block shunts the track and keeps the signal from ever reaching the receiver. Since the ballast impedance of the track can be as low as 5 ohms in certain types of weather, the train must present an impedance substantially lower than that. The standard in the industry is 0.06 ohms.

Miller told ELECTRONIC DESIGN that several types of corrections are being considered. They include: scrubbers on the wheels to clean the rust off; stainless steel beads on the track to increase the surface area of the wheel-track interface and an additional contact that would drop from the car to the track in case of power failure.

Extra line feeds speed telescope's data input

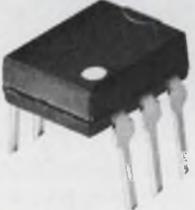
The National Science Foundation has increased the data-handling capabilities of its 1000-foot-diameter radio telescope near Arecibo, Puerto Rico, by connecting 10 line feeds to the telescope instead of the usual one. The speed of data collection has been increased by a factor of 10.

This technique cannot be used on all radio-telescopes, however—only on those that are spherical in shape. A spherical reflector can have many simultaneous feeds, each mounted on a different radial line.

The feeders for the Arecibo telescope are arranged in two rows of five lines each and operate at 611 MHz.

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THE OUTLOOK FOR 1973

With LSI, you'll get more instrument punch in a much smaller package at a lower price

Stanley Runyon
Associate Editor

This year will be the year of the miniature, low-cost instrument. The reason? The use of LSI, introduced in instruments last year, should increase dramatically in 1973. And just in time, too. Soaring sales of digital, data-processing, communication and medical and industrial electronics equipment have increased demands for field service and for small, portable instruments.

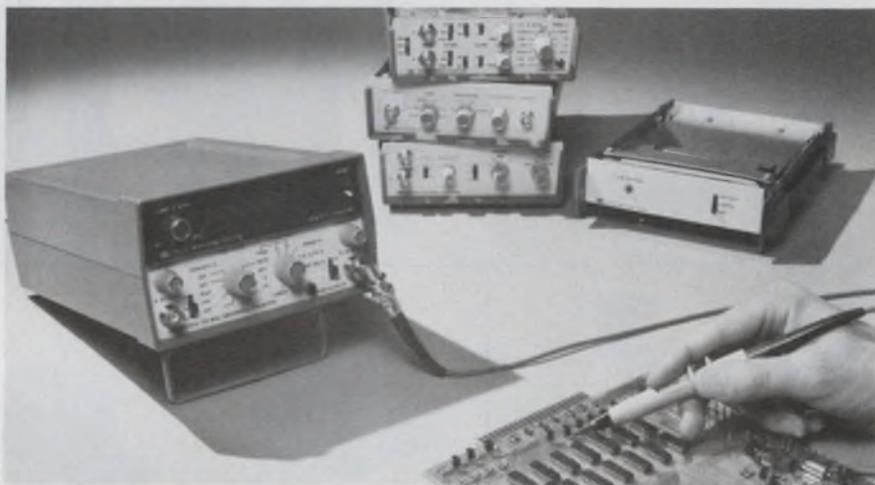
At the same time executive engineers in the industry see major growth at the opposite end of the size/cost scale—in instrument systems.

John Zevenbergen, president of the Fluke Manufacturing Co., Seattle, says his company is incorporating LSI in instruments wherever practical. He feels that in addition to portability LSI offers the best of two worlds: lower cost and increased performance. And with the newer commercial and industrial markets demanding better field service, Zevenbergen says that LSI offers another benefit—greater reliability.

John Young, vice president and executive head of the Hewlett-Packard Electronic Products Group, Palo Alto, Calif., agrees that increased use of LSI plus other new technology—such as CMOS—will contribute to important changes in instrument design.

Young expects a growing need for instrument systems to replace technicians. Such systems, he suggests, can start out as compatible,

The 1973 outlook for military, space and industrial electronics will appear in the January 18 issue of *Electronic Design*.



Measuring system typifies current trends in instrument design: LSI circuitry, solid-state displays, small size and easy servicing.

calculator-based units and be upgraded or integrated into larger computer-based systems.

William Walker, vice president of engineering at Tektronix, Inc., in Beaverton, Ore., agrees. He sees growth of the systems concept as one of two major instrument trends. The second trend, he says, is toward simpler instruments.

Two types of systems

Walker splits systems into two categories: The first is the large, dedicated system with at least a PDP 11 either chewing up the measurement information or controlling the system. At the opposite end of the spectrum is Tek's integrated systems concept, which first ties together various measurement functions—such as counters, DVMs and scopes—and then adds a calculating or computing capability.

Spurring the trend toward systems, Walker continues, is the fact that a United States advisory committee is reported close to agreement on a standard for interfacing

that will enhance instrument use in data-acquisition systems. The standard, to be adopted by the International Commission for Electrical Standards, is basically a byte-serial, bit-parallel scheme that permits interconnection of instruments by plug-in cables.

Walker also sees increasing use of LSI. "It lends itself to doing a lot more for less cost," he explains. "Whenever you can use, say, MOS LSI in a particular section of instrumentation, the prices come rolling down."

A few years ago, when Government contracts were in abundant supply, engineers were buying more sophisticated instruments than they really needed to do the job. Today there is a tight check-rein on this tendency. Walker, HP's Young and Zevenbergen of Fluke agree that instrument buyers have become more cost-conscious. They want simplicity in instruments and just enough accuracy to do the job well.

In addition many new markets for instruments—vocational education, automobile manufacturing

and servicing and the medical field—can't stand long down-times, Zevenbergen notes; the new instruments must be geared for fast service.

What specific new instruments will we see in 1973? The instrument makers aren't saying. But HP's Young suggests a broad area that is under investigation:

"The trend to digital has produced large-scale troubleshooting problems. When a fault develops on a circuit board with something

like 60 IC packages on it, you can't afford to discard it, and maybe you can't afford a duplicate while the factory finds the fault for you. When something like that happens on a circuit under design, you need a way to find out if the fault is in the over-all design or on a chip somewhere."

Tek's Walker expects a trend toward getting more out of a measurement. He says: "There will be some major steps taken to deal with waveforms and signals to ex-

tract more information from them." When asked if this meant a possible tie-in with a computer, he replied: "That could be a piece of it, but not all of it."

Tektronix, Walker continues, is also taking a look at some measurements now made mechanically with transducers. It hopes to come up with instruments that will see what's going on in real time. Thus, Walker hints, the user will be able to see pressure, temperature, force or strain in a transient way. ■■

NMOS and CMOS are surging forward in drive to dominate semiconductor scene

Edward A. Torrero
Associate Editor

While complementary MOS (CMOS) will continue to make major inroads in applications once dominated by TTL—especially where low power is required—n-channel MOS (NMOS) should come into its own this year with the introduction of 4-k RAMs.

It figures: In virtually every year since the invention of the transistor, components have tended to become smaller—and therefore denser—and faster.

Most industry observers believe the 4-k RAM will become the next standard RAM, following the 1-k 1103 (originally introduced by Intel). In the competition between semiconductor memories and core, the 1103 signaled that memory chips were available with the right density and speed for mainframe applications.

Two companies are offering random-access memories with 4096-bit, n-channel chips as the basic building block. Microsystems International Ltd. of Quebec, Canada, has a memory system—the RAM 4A—that consists of ten 4096 chips on a single card. It consumes just 150 μ W/bit, compared with 1 mW/bit for equivalent core and 300 μ W/bit for 1103 types. The RAM 4A's initial price is 1¢/bit, but the company says it expects to cut this in half within two years.

Standard Microsystems of Sunnyvale, Calif., has the other entry: its COPLAMOS process. The com-

pany is reporting speed/density advantages over the standard n-channel process and says it has achieved a read access time of 180 ns. Other companies believed to be working up a 4-k, n-channel RAM are Intel, Mostek, American Microsystems and Motorola.

Meanwhile CMOS will also continue to enter new markets. Though RCA's CD 4000A series should still predominate, the ICs of other manufacturers will probably penetrate such areas as the automotive industry.

In fast logic, Schottky TTL and ECL 10,000 will continue to compete. But watch for more second-sourcing of Motorola, TI and Fairchild fast logic.

Bipolar MSI logic gains

Though MOS will continue to grow in use, Advanced Micro Devices of Sunnyvale, Calif., expects bipolar MSI logic to outsell any other type of logic. The use of PROMs should also increase.

Digital subsystems on a chip are continuing their drive toward higher complexity in 1973, filling demands in areas other than calculators and microprocessors.

Linear ICs should also grow in complexity and number of functions. The faster comparators that will be appearing will be TTL as well as ECL-compatible. The quad op amps from Motorola in Phoenix, Ariz., and National Semiconductor of Santa Clara, Calif., will be better and faster than discrete op

amps, and they will lower the price of a single op amp to a new low.

Refinements in the manufacturing processes of components will contribute to density increases. Fairchild's Isoplanar, Raytheon's V-ATE and Motorola's VIP processes—now turning out bipolar ICs—may be expanded to MOS. Fairchild is reported working on an Isoplanar process for MOS devices.

The action in passive components is focusing on thick-film and hybrid circuits. Thick films will expand in function from continuously variable resistors to quasi-active switches and other areas. Hybrids will penetrate the automotive industry and other markets as better manufacturing techniques lower their cost. And more ion implantation is foreseen.

Ceramic thermal switches will appear during 1973 for de-current control applications. Avalanche devices will control large currents of several amps compared with only microamps at present. The new devices are expected to threaten relays.

Because of their attractive price, more molded tantalum capacitors will be used in 1973, according to Sid Chertok, manager of information services for Sprague in North Adams, Mass.

And connectors will seek to match the improved density and cost of components. Watch for non-noble contact platings to become more popular. ■■

(continued on page 32)

The new minicomputers: Faster, sophisticated and a choice of MOS or bipolar memories

Jim McDermott
Eastern Editor

"The emphasis in the minicomputer industry has traditionally been on price and performance, but today the industry is developing faster electronics."

That's one major trend that Andrew Knowles, vice president of the Digital Equipment Corp. in Maynard, Mass., sees for 1973. Others he says, include these:

- Faster logic.
- Both MOS and bipolar memories.
- Multiple bus systems.
- Multilayer boards.
- MSI and LSI in microprogramming.
- Increasing manufacturer costs, and emphasis on software rather than hardware.

As an example of developments aimed at increasing computer speed, Knowles points to the DEC 1145.

"This machine," he says, "uses the highest-speed TTL that we could find—Schottky devices from Texas Instruments."

The 1145 also uses both MOS and bipolar memories, the latter to accommodate the fast memory.

"In addition," Knowles explains, "the 1145 is a multibus unit. It has a fast-memory bus, a slow-memory bus and an in-out bus that is combined with the slow-memory bus."

This type of design, he points out, reflects the tendency of computer manufacturers to distribute the computer power among several buses—much as they did with the advent of the third and fourth generations of large systems, when they used multibuses and multipoint memories. The development of minis is toward the architecture of larger systems and faster equipment.

One of the newest design features is that of multilayer boards. "Instead of simple two-sided boards," Knowles notes, "we're

using multilevel boards of three and four discrete layers."

The use of microprogramming techniques is definitely on the increase in the minicomputer field. Here, Knowles says, the minis are making heavy use of MSI and LSI either for the execution of the instruction set or for user microprogramming.

The result, the DEC president points out, is better performance with lower costs.

With such microprogramming substituting in many cases for additional hardware, the emphasis in mini system design is more and more on software instead of hardware, Knowles says.



Next year's minicomputers are expected to offer faster logic and supporting electronics along with MOS and bipolar memories.

The tendency among mini manufacturers now, he believes, is to spend more money on systems monitors that allow the peripherals to interplay with the central processor and thereby handle much traffic and scheduling formerly done by the programmer.

As a result, operation of the machines is becoming substantially simpler. Originally, Knowles points out, a programmer had to be a near scientist; now grammar-school

children can program these machines. But software costs are gradually rising higher than the hardware as a result, the DEC executive says.

While today the so-called virtual memory is associated with large computers, like IBM and Burroughs machines, Knowles predicts that minicomputers will use the technique eventually.

The virtual memory is provided essentially by the use of rotating memories, like discs, to store address information ordinarily considered to be in the main core memory. When the user runs out of address space in the core, the disc file provides added memory space that can be accessed faster.

"When our miniprogramming and our monitors run out of core," Knowles notes, "then virtual programming will be the next step."

No spectacular breakthroughs are likely in peripherals this year, according to Robert Schuck, director of OEM marketing for the Mohawk Data Sciences Corp., King of Prussia, Pa. He sees the present third generation of peripherals—those with the latest mechanical approach and full TTL electronics—going through a refinement.

More efficient tape drives

Tape drives are becoming more efficient and easier to service, he says, pointing to the Mohawk 4025, which provides a tape speed of 125 inches per second in a rack mount.

For both printers and card readers, the trend, Schuck says, is toward greater reliability and easier maintenance. Cassette cartridges, for example, are headed for greater use as memories. Mohawk has chosen the 3-M cassette, Schuck reports, because data can be loaded onto it at about 1600 bpi, with a resolution of at least one bit in 10^8 . This performance is produced on 1, 2, 3 and 4-track recordings. ■■

(continued on page 34)

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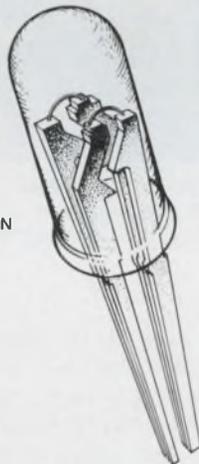
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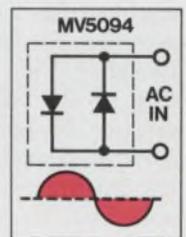


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INFORMATION RETRIEVAL NUMBER 20

Color television swinging to in-line tubes as complex ICs widen consumer market

Jim McDermott
Eastern Editor

Greater use of new short, in-line-gun color tubes, the inclusion of more automatic circuits and increased emphasis on all-electronic varactor station tuners are developments in color television that Dan Schuster, Sylvania's vice president of engineering in Batavia, N.Y., sees over the next two years.

An increasing number of portable color TV sets will incorporate the in-line tubes, Schuster says. The reason? Lower ultimate costs. While the in-line tubes cost about the same as present comparable units, the in-line system permits simplification of the convergence circuitry. In-line tubes are also shorter, so a slimmer cabinet can be used. And Schuster notes that these tubes can be more easily adjusted at the factory and in the field.

For consumer entertainment sound systems, Richard F. Wood, engineering manager of electroacoustics for the Philco-Ford Corp., Lansdale, Pa., looks for incorporation of the SQ (Columbia Broadcasting System) type of quadasonic decoder system this year. The SQ hardware is now readily available, he notes, and there are a relatively large number of SQ records on the market.

But within two or three years, Wood feels, discrete four-channel recordings and playback systems will be the next step.

Increased use of ICs seen

Norman Doyle, consumer applications manager for Fairchild Semiconductor, Mountain View, Calif., says that the next area of development in ICs for television will be that of the video channel. In AM/FM radios and sound systems, he sees many different IC circuits being produced. And Doyle sees ICs being used in systems for the new video recorder-players.

Automobile and camera manufacturers will be using newly developed ICs this year, Doyle continues. Predictions are, he notes, that by 1980 the automotive IC market will be worth \$1-billion annually, while cameras will account for more than \$300-million in sales.

The trend, Doyle points out, is toward more complex ICs. "Our customers want more and more of the external components built onto one chip," he says. As a result, chip sizes are increasing. For consumer ICs, Doyle notes, Fairchild now has 10,000-square-mil chips.



Television receivers are assembled on the production line at RCA's TV facility in Bloomington, Ind.

Power is an important area in which IC barriers are being pushed back, Doyle says. "Right now," he reports, "we can make 10-W audio ICs. But that's probably as high as we're going to go in the foreseeable future."

Frequency response is also being increased, Doyle says. For present devices, the gain-bandwidth product is about 150 MHz. "But by applying the isoplanar process to ICs," Doyle says, "we can see an increase in the bandwidth product by an order of magnitude. And another advantage is that this process

gives increased circuitry density on a chip, leading to a more cost-competitive end product."

Arthur M. Liebschutz, market planning manager for RCA's Solid State Div. in Somerville, N.J., sees 1973 as the year in which high demand for ICs will curtail their development. Semiconductor manufacturers will be too busy filling orders to divert too much effort to R&D, he explains.

The reasons for high demand, he says, include these:

- Overseas markets are expanding.
- The use of automotive ICs in large quantities is beginning, with ICs to be used in seat-belt sensor systems for 1974 cars.
- ICs in television receivers are on the rise.

The replacement of conventional off-the-line ac power supplies with miniature, high-frequency supplies is not far off, says Leo Lehrer, product manager for power transistors at Motorola Semiconductor in Phoenix, Ariz. He sees what he calls the "20-kHz revolution."

He expects these low-voltage, high-current power supplies to replace high-voltage, low-current supplies in solid-state entertainment products.

Within five or six years, Lehrer says, 5-V, 200-A supplies delivering 1 kW may operate toasters. Shock hazards will be substantially reduced.

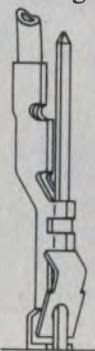
In electronic watches—a rapidly growing consumer area—there will be more of an evolution than a revolution, according to Richard Kaury, marketing product manager for Micro Power Systems, Inc., Santa Clara, Calif. For power sources, he sees production use in a few years of 1.5-V and 15-V lithium batteries. The 15-V unit, he says, will be able to operate liquid-crystal displays directly, thus eliminating the step-up converter now required with 1.5-V batteries ■■

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3 years after birth, CCDs head for first commercial applications

Charge-coupled devices (CCDs) have always been a technology to watch. Because they have a minimum of diffusions and metal substrate contacts, they are capable of high packing densities, low power dissipation, high yields, increased complexity and low costs.

Jules H. Gilder
Associate Editor

According to most experts in the field, 1973 will see significant CCD developments and the first commercial applications of these devices. Since their introduction in 1970, much has been written about their promise, but only with recent advances in CCD technology has it been possible to turn the promise into reality.

Among the advances expected

this year are these:

- Commercially available CCD image-sensor arrays.
- Inexpensive black-and-white television cameras for use in security and surveillance systems.
- High-quality black-and-white and color television cameras for broadcasting studios.
- CCD serial computer memories.
- CCD analog signal processors.

Much of the work being done on charge-coupled devices is in the area of imaging. This has been spurred by support from the military, which is interested in low-light television applications.

Brown Williams, manager of the electro-optics laboratory in the RCA Electronic Components Div., Princeton, N.J., says that CCD image sensors will be used not only to replace electron-beam-scanned camera tubes but also to replace other solid-state imagers. And, because they will be relatively inexpensive, CCD sensors will turn up in home-security and home-entertainment systems, he adds.

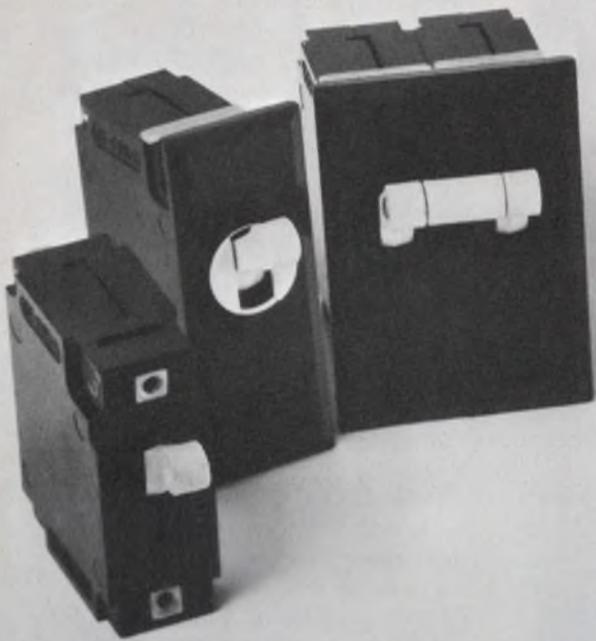
In pointing out the advantages of CCD imagers, Williams compared them with the presently used image sensors. He noted that vidicons—the most widely used device—need a high voltage to operate and have many bulky components, such as deflecting coils. In addition they are fragile.

CCDs, Williams points out, can operate from low voltages—10 to 15 V typically—and since the sensors are inherently self-scanning, there is no need for bulky deflecting coils. This self-scanning property also gives CCDs an edge over silicon-diode-array image sensors, which require complex scanning circuitry.

Another advantage of CCDs over silicon diodes is that they are easier to manufacture, Williams



Color image formed by Bell Labs' CCD television camera reveals that the principle is sound but the resolution is poor. Higher-resolution cameras are expected to be available before the end of the year.

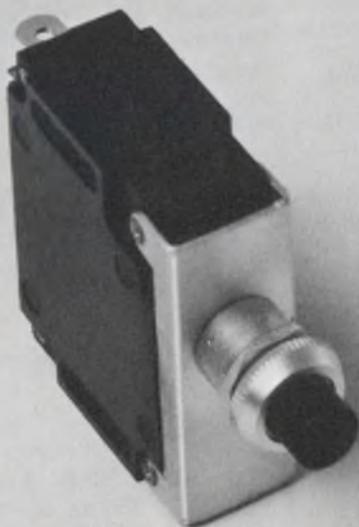
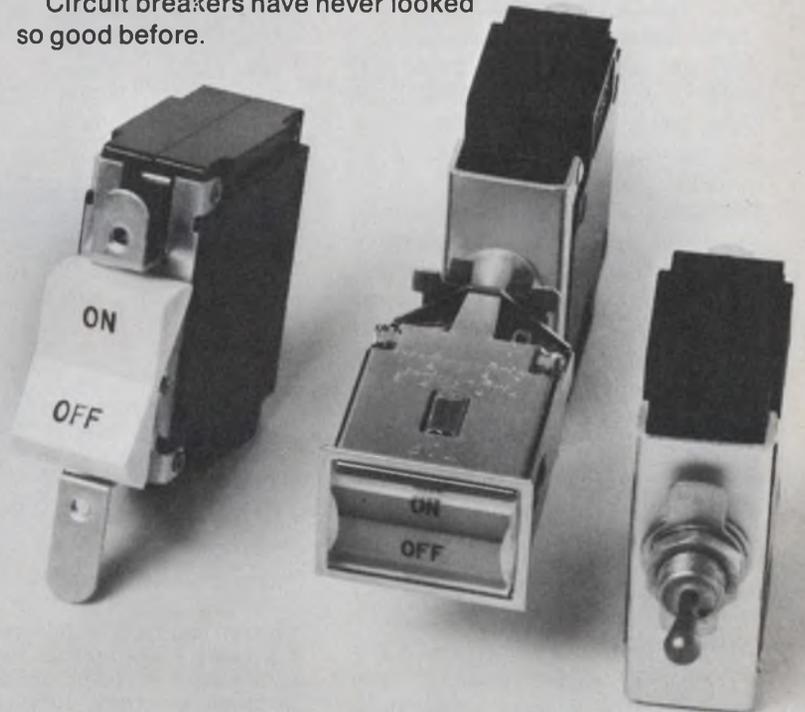


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says. The charge-coupled devices do not require any diffusions to form the sensing elements, whereas silicon diode arrays require a few hundred thousand diffusions.

Last year both Bell Telephone Laboratories and RCA demonstrated that it was technically feasible to build television cameras with charge-transfer devices.

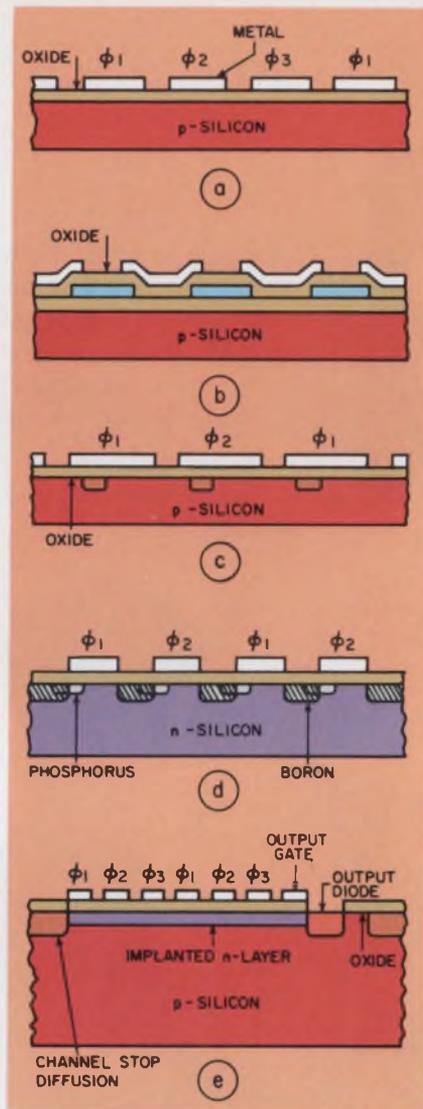
The approach taken by Bell used charge-coupled devices to produce a color television camera, while RCA used a bucket brigade—another type of charge-transfer device—to construct a black-and-white television camera.

The bucket-brigade sensor, however, has limitations that may not make it as popular as the CCD. To begin with, bucket brigades have a lower charge transfer efficiency—99.9% vs 99.999% for CCDs. They also have a lower maximum operating frequency. In addition, notes RCA's Williams, the bucket brigades require four diffusions for each element, whereas CCDs require none. The bucket brigade does have one advantage, however: Since it is essentially an integrated version of a discrete circuit, any company capable of manufacturing MOS integrated circuits would have very little trouble making them. The devices will probably find application in filters and delay lines, Williams says.

RCA, like General Electric, Westinghouse, Texas Instruments, Fairchild and others, sees an enormous market for CCD imagers in the next two years. These manufacturers believe that home-entertainment systems, such as portable video tape cameras, will use large quantities of the devices. One company goes so far as to say that in two years it expects to see a repeat of the calculator craze, with everyone buying miniature television cameras this time.

In an attempt to capture a large share of the CCD imager market, General Electric at Schenectady, N.Y., has switched its operations from memory-oriented devices. William Engler, a member of GE's research and development staff, says the company will have a CCD imaging chip on the market before the end of the year.

While most industry estimates indicate that CCD television cameras with commercial resolution



Several methods of fabricating CCDs are being investigated. The first (a) is a simple three-phase device, but the close electrode spacings are difficult to produce. Two-level metalization CCDs, either two-phase or four-phase devices, (b) eliminate spacing problems. Two-phase operation can also be obtained by using an ion-implanted-barrier CCD (c). And an improvement over the implanted-barrier device is the conductively connected CCD (d) which also alleviates the spacing problem. The buried-channel CCD (e) eliminates the trapping effects of interface states and promises a more efficient device.

will be available in two years, at least one manufacturer is pushing to have one developed by the second half of this year.

Most of the funding for current work in CCD imagers is being done by the military. Edwin N. Myers, staff specialist in electronic science for the Director of Defense Research and Engineering in the Pentagon says:

"We'd like to have a completely

solid-state imager that is within a factor of 10 as sensitive as the intensified silicon-diode camera tube used in low-light-level TV."

He adds: "We would like a spectral response that would enable us to pick up neodymium laser illumination."

The Navy Electronics System Command is coordinating all military CCD work. Plans are to invest a total of \$3-million for research and development of CCD imagers. Fairchild, RCA and Texas Instruments are the recipients of the Navy money and each must deliver a 100-by-100 element array and a 500-by-1 element array by March.

Progress in CCDs is advancing so rapidly, however, that by the time these devices are delivered, it's possible that larger devices will be near completion. Both Fairchild and RCA are working on larger devices that should be finished by the second half of 1973.

CCDs challenge serial memories

It looks as if CCDs will provide some tough competition for computer memories, says Dean Toombs, director of group engineering for Texas Instruments in Dallas. Since the devices are basically shift registers, he notes, their applications in memories will be limited to serial memories.

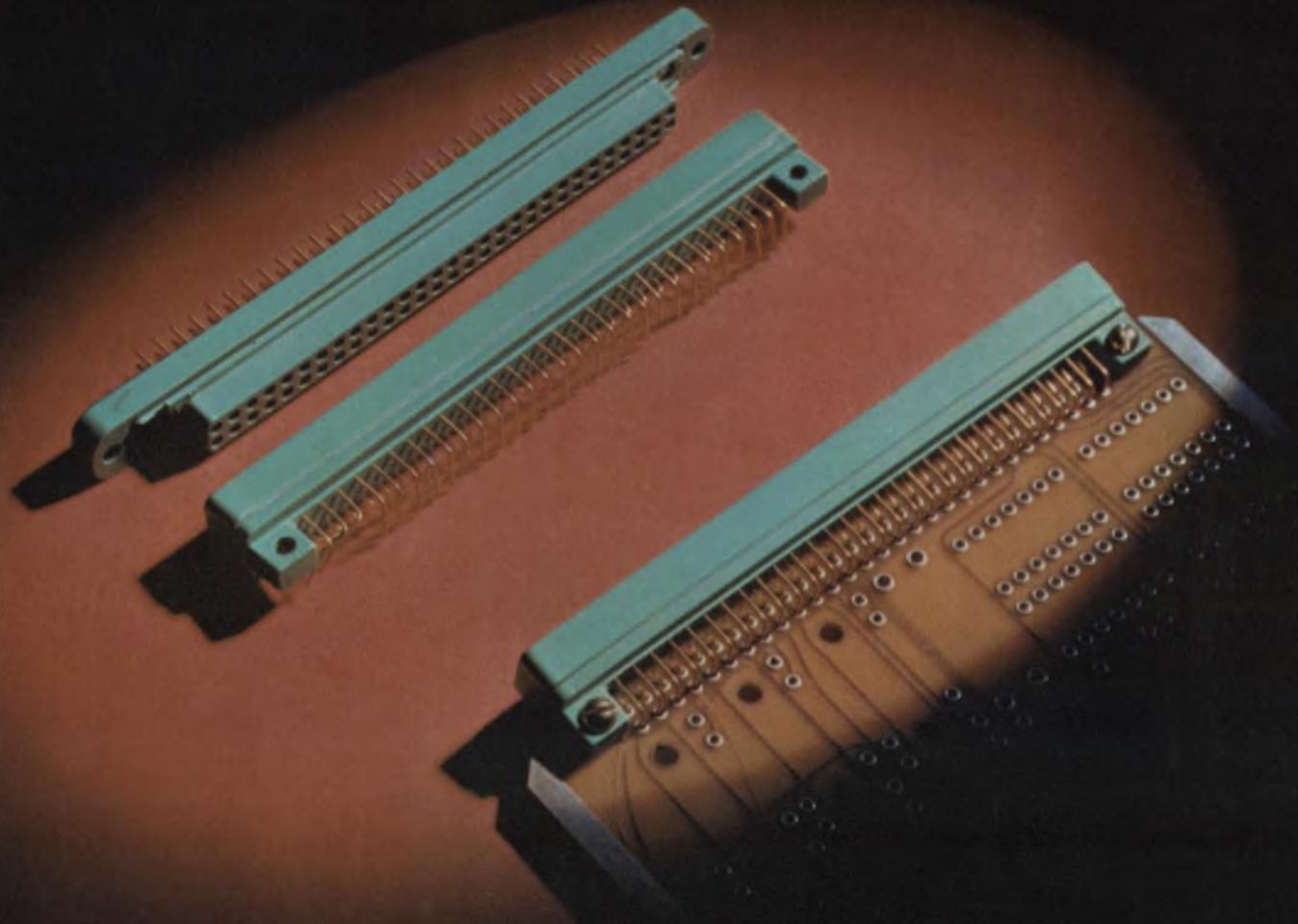
Toombs points out that CCD memories are potentially cheaper than presently available systems, and he sees them finding application as replacements for disc and drum types. CCDs, he says, can be used wherever MOS shift registers are presently in use.

The advantages of CCDs, notes Toombs, are a two to fivefold increase in density, simpler processing and lower cost.

IBM agrees that CCDs have great potential in memory applications, and it has even constructed an experimental memory using them (see "Charge-Coupled Devices Await Mass Application by Industry," ED 6, March 16, 1972, p. 27).

More recent work by IBM has shown that with conventional processing, high density, very long (128-bit) p-channel CCD structures can be produced. These devices are capable of being clocked

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in the 10 to 20 MHz range. One major problem noted by IBM researchers is that very large, high-density CCD arrays require driving power densities that are difficult to provide. As a result, the development of a nonoverlapped-electrode, gapless CCD may be integral to the density-performance capability of these devices.

James Carnes, a member of the

technical staff at RCA, says that for CCD memories to be viable, they must break the 0.1-cent-per-bit barrier. The area required for each bit should also be less than 1 square mil per bit, he adds.

In visualizing the size of future CCD memories, Carnes says that a 200-by-200-mil chip should contain a memory of between 30 and 50 kilobits, while a 500-by-500-mil

chip should be able to accommodate memories of 250 kilobits.

An interesting point made by Carnes is that the same basic masks used to make an imager can be used to make a memory device.

When asked when he thought CCD memory chips would be available, Carnes said that they probably would be developed by the end of 1973. ■■

The CCD and the BBD: They're unlike semiconductors

Charge-transfer devices are fundamentally different from the semiconductors that most engineers are familiar with. They use the controlled movement of electric charge to perform their functions, and they are generally classified two ways: as *charge-coupled* devices and as *bucket-brigade* devices. The general operation of both is similar, but there are important differences in fabrication.

Charge-coupled devices (CCDs) are simple in structure and consist of three layers: the semiconductor material, an oxide layer and the metal electrodes. They are basically junctionless devices, except for small, diffused p-n junctions at the input and output of the CCD shift register. In addition long registers may contain refresh cells, which also require diffusions.

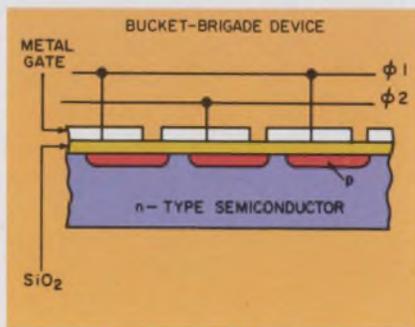
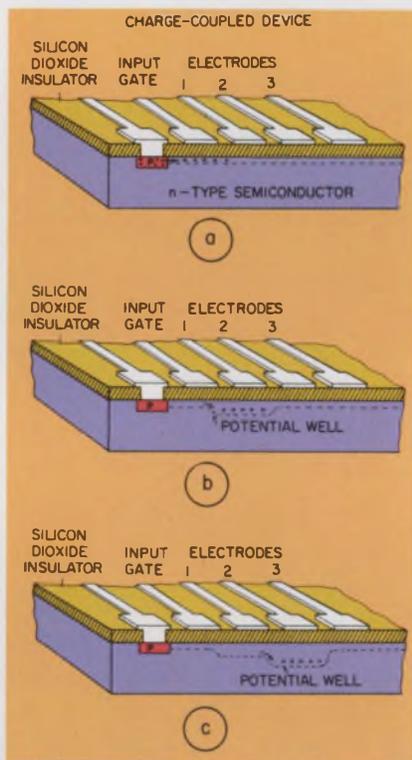
The operation of a CCD requires that electrical charge in the form of minority carriers be transferred from the region under one electrode to another. The charge represents information and is moved by control of the voltage applied to the electrodes.

When information (negative voltage) is applied to the input gate, a channel in the n-type material opens up and draws positive charges from the input p-n junction to the region under the gate (Fig. a).

When a negative voltage is applied to electrode 1, evenly distributed electrons in the n-type material are driven downward, away from the electrode, leaving a region of depleted electrons just below the oxide

layer. This depletion region produces a potential well (Fig. b).

Positive charges passing through the channel under the input gate are drawn to electrode 1 and stored in the potential well, provided that the electrodes are close enough to allow coupling.



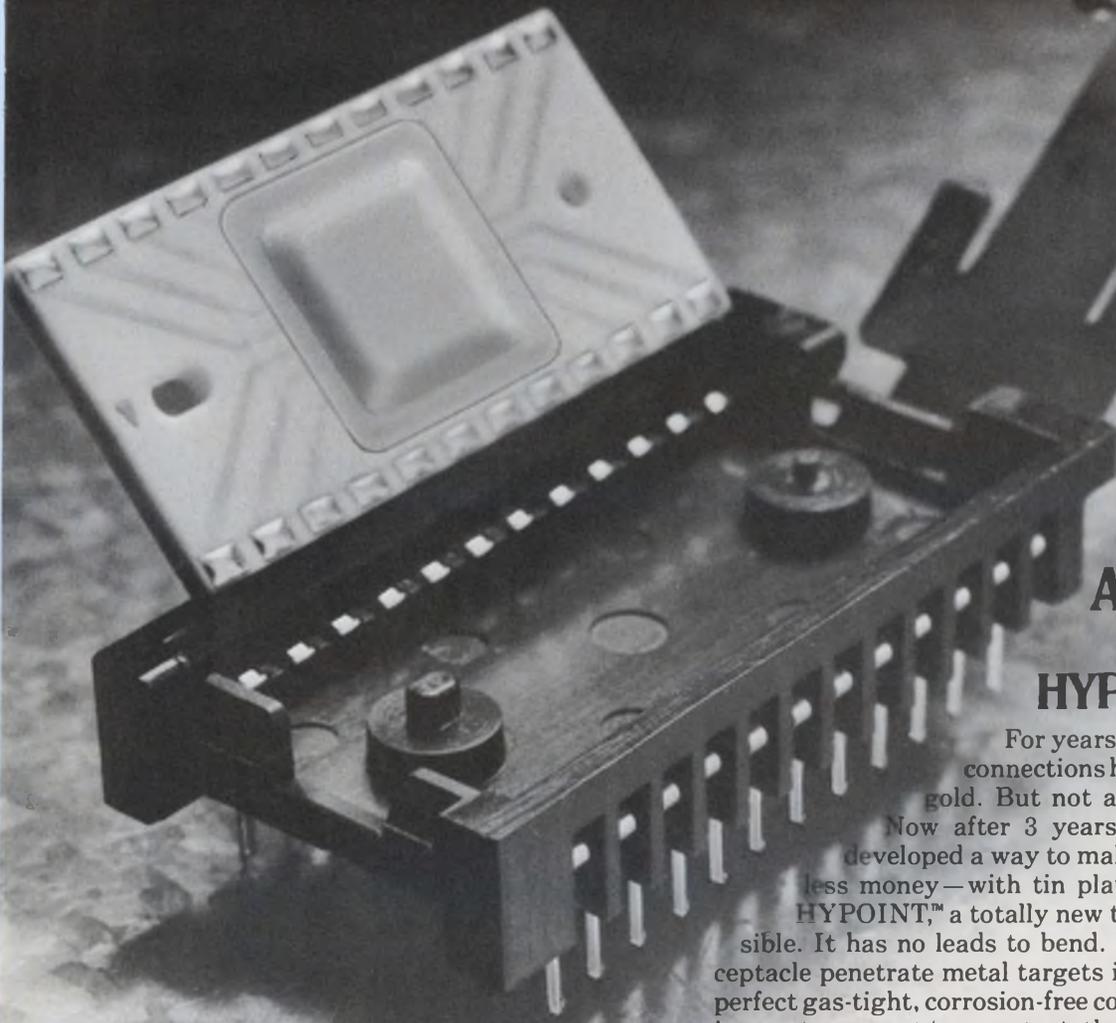
The information—positive charge—can be transferred from electrode 1 to electrode 2, by application of a negative voltage to electrode 2 and reduction of the voltage on electrode 1. This transfer voltage forms a deeper potential well under electrode 2, and the information flows to the well under electrode 2. Thus by proper manipulation of electrode voltage, information can be transferred (Fig. c).

The simplest CCD is a three-phase device in which electrodes 1, 2 and 3 form a single memory cell. Information is stored under only one electrode while the two others provide isolation.

Bucket-brigade devices differ from the CCDs in that they can be constructed from discrete components. Information is stored as majority carriers and transferred as minority carriers. Storing occurs in an array of capacitors as charge deficit. Charge-transfer circuits consisting of MOS transistors allow the charge deficit to move from one capacitor to the next.

The structure of the bucket brigade (lower figure) reveals that charge is stored in offset p-regions under MOS capacitors and that it is a two-phase device. When a negative voltage is applied to an electrode, the diffused area underneath it becomes reversed-biased and inverts the channel between this diffusion and the next one. By application of the appropriate clock signals to the device, excess charge is transferred from the source of one FET to the drain of the next via the inverted channel.

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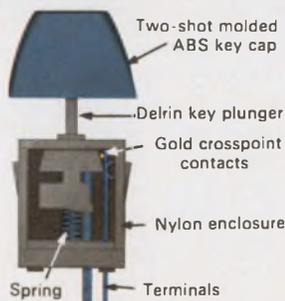
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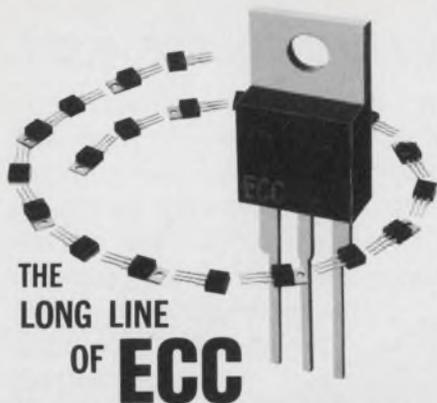
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The effectiveness of radio-frequency systems for pinpointing the position of aircraft and for guiding helicopters and vertical takeoff craft to safe landings in bad weather is being investigated by the Royal Aircraft Establishment, Farnborough, England. A Honeywell 316 minicomputer is part of a system set up for the studies. Using an rf interferometer, the system can cover a complete hemisphere rather than just a narrow sector. As a result, it can produce curved-line profiles needed to guide helicopters and vertical takeoff aircraft. To eliminate ambiguity of position, the interferometer incorporates additional pairs of antennas that uniquely define a position in space.

CIRCLE NO. 201

A complete AM radio receiver on a single silicon chip, using collector-isolation-diffusion processing techniques, has been produced by Ferranti of England. The circuit, which is packaged in a standard three-lead transistor, can incorporate an agc network. The receiver operates over the frequency range of 200 kHz to 1.5 MHz. The radio is completed by the addition of a battery, antenna, two resistors, a variable capacitor, two fixed capacitors and a loudspeaker. The power requirement is 1.5 V at 0.5 mA. Over-all gain is on the order of 70 dB.

CIRCLE NO. 202

A system that permits television receivers to display on demand information such as weather reports, motoring and travel news, sports results, and stock market prices is being developed by the British Broadcasting Company. The system will superimpose the data on the regular TV signal.

The information will be removed from the picture by a data collection and storage unit at the receiver. The information will be stored in the form of pages that will be updated upon receipt of new information. The viewer, upon selecting a page of information, will be able to override the TV picture and present the page on the TV screen. A demonstration is to be held by mid-1973 in addition to field trials to evaluate different methods of instrumentation for the system.

CIRCLE NO. 203

A high-frequency monolithic quartz crystal filter with reduced volume and improved aging stability has been developed by AEG-Telefunken of West Germany. The filter consists of a quartz disc with several acoustically coupled resonators, plus a capacitor chip. The center frequencies of these filters are 10.7 and 15.3 MHz. Nominal bandpass is 20 to 25 kHz. The ultimate limit for the new design is calculated to be about 300 MHz.

CIRCLE NO. 204

A miniature synchronous motor reported to be of lower cost and several times more power than any previous unit of its kind has been produced by collaboration between the Electric Remote Control Co., the National Research Development Corp. and Sheffield University, all of Britain. The mini-motor, which is 32 mm in diameter by 16 mm deep, rotates at 375 rpm with 50 Hz excitation. Maximum running torque is 9400 gm-cm. Its ferrite rotor has 16 poles. The stator is composed of soft-steel precision stampings. The stator winding is embedded in glass-filled polyamide plastic.

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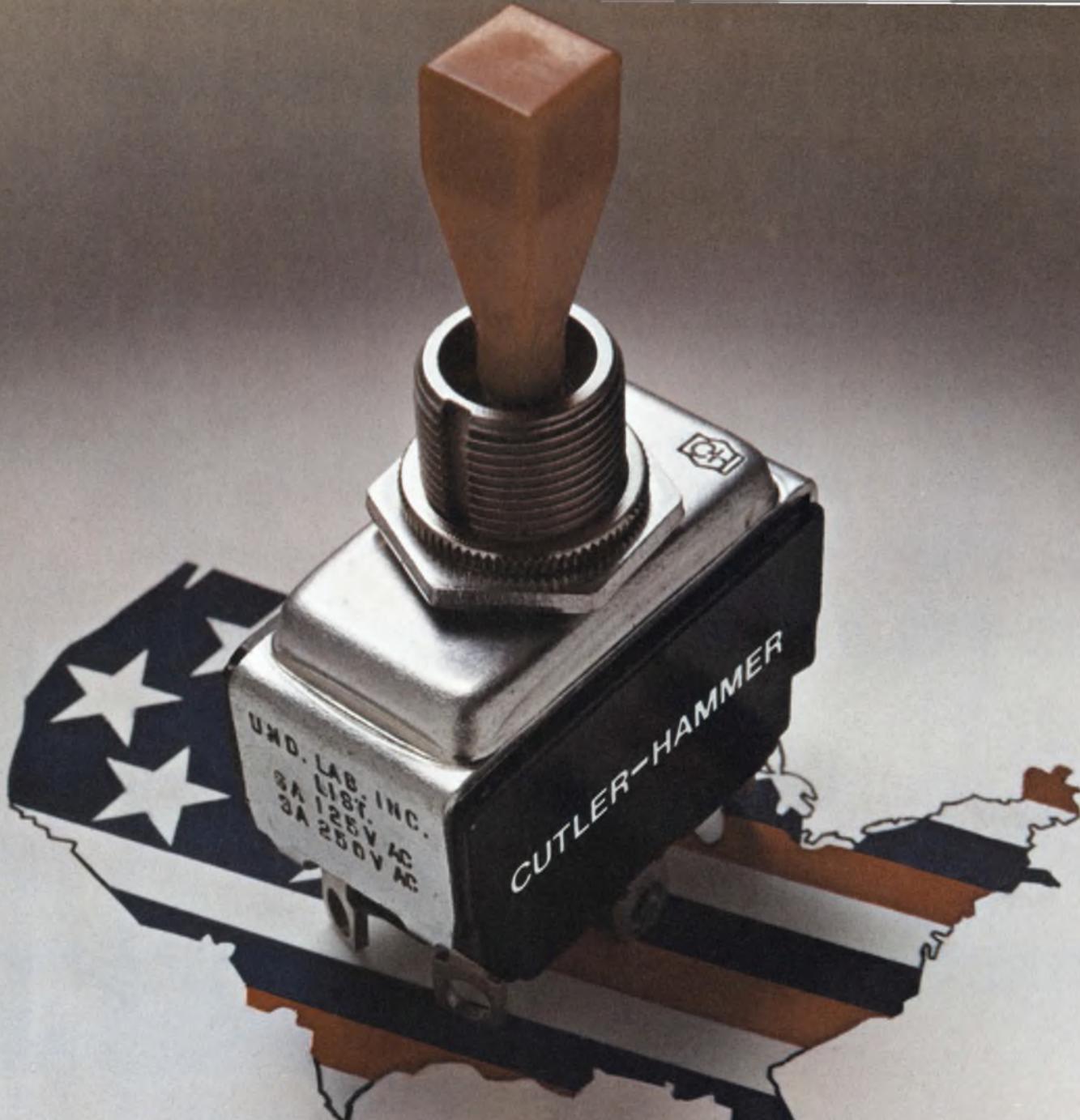
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washington report



Heather M. David
Washington Bureau

Congress tackles the F-14 problem

The Navy-Grumman dispute over whether or not the company should be held to its contracted cost figures for the F-14 carrier aircraft has moved to the Congressional arena. Hearings have begun on the cost of the fighter plane's weapons systems before Senator William Proxmire's (D-Wis.) joint economic subcommittee, and investigations are planned in the House and Senate Armed Services and Appropriations Committees. New York State's Senators, Jacob Javits and James Buckley, both say they will introduce legislation to keep Grumman from going out of business.

Congressional reaction thus far is mixed, some influential military-affairs committee members are tired of rising costs in weapons and fearful of an avalanche of contractor defaults if Grumman's plea to renegotiate fees is heeded. Privately these Congressmen indicate they are in favor of canceling the F-14 program. Others, with strong Navy ties, are expected to back Grumman, since the F-14 is seen as the major justification for the Navy's aircraft-carrier fleet.

Insiders say that actually Grumman will not be in default of its contract for at least a year and that the current announcements by the Navy and the company are designed to smoke out Congressional opinion and force action on the problem. The F-14 reportedly is performing well in tests, including its AWG-9 weapons fire-control system, built by Hughes Aircraft.

FTC vs Xerox: A hearing seems likely

The next step in the battle between the Federal Trade Commission and the Xerox Corp. over the FTC's allegation that the company has illegally monopolized the office-copier machine industry apparently will be a hearing before an administrative law judge of the commission. Xerox officials say they will fight the FTC charge and take the suit to a Federal Court if the hearing judge rules against the company. Among other things, the Federal agency is considering punitive action to force Xerox to give free licenses on all present patents as well as any developed in the next 20 years.

A ruling due on television-tube dumping

The Tariff Commission will report to the Treasury Dept. this month as to whether the U.S. television-tube industry has been injured by Japanese dumping. If the answer is yes—and the Electronic Industries Association has testified to that fact—the Treasury Dept. will begin examining re-

cords to assess levies. The department is now collecting levies on an earlier antidumping decision against Japanese color-television imports. Meanwhile Japanese manufacturers of electronic consumer goods have voluntarily moved to limit the export of such items as stereos, monochrome and color-TV tubes, tape recorders and civilian communications equipment.

On the other side of the import-export coin, the National Export Expansion Council's Industry Advisory Committee has called for elimination of domestic and foreign impediments to the export of computer equipment and office machines. The committee says it doesn't need Federal curbs on imports, just less restrictions on sales abroad.

Postal Service to expand its electronic aids

The U.S. Postal Service will invest in some new electronic equipment in the near future and will be looking for contractors to bid on 28 multi-position machines. The units will have solid-state computer equipment to sort mail for the 277 Zip Code destinations in the United States. The Postal Service has been buying equipment to automate the handling of packages, but it finds the electronic handling of letters a more difficult problem. The service will commit about \$102-million in R&D funds this fiscal year, including \$15-million for general research, \$59-million for applied research, \$23-million for engineering and \$4-million for administrative support.

U.S. help for budding investors on the way

The National Science Foundation has started an experimental R&D incentives program to enable designers of technical inventions to have their designs verified in Government laboratories. The program is aimed at encouraging innovations in the civilian sector. Laboratories of the National Aeronautics and Space Administration and the Dept. of Defense will be the first to participate in the program. Foundation officials say the tests should help successful inventors attract venture capital to their projects by proving the feasibility of their ideas. To apply to have an original design verified write for instructions to the NSF Project Officer, Mr. Evan D. Anderson, National Science Foundation, 1800 G. St. NW, Washington, D.C. 20550.

Capital Capsules: U.S. industry R&D expenditures will increase 25% between 1972 and 1975, to a record \$14-billion, according to the National Science Foundation. Employment of scientists and engineers also will rise, from 240,000 last year to 260,000 in 1975, the foundation predicts. . . . **The uptrend in business capital expenditures will continue in 1973**, the Commerce Dept. says. A survey by the Bureau of Economic Analysis says the communications industry will have an increase in investment of more than 10%. . . . The General Accounting Office's latest tally of defense weapons systems shows that 47 major systems had a cost growth of \$1-billion in the three-month period from March to June. . . . The Electronic Industries Association continues to expand its trade activity. It has appointed **Ralph E. Van Hoorn** of ITT to head the association's new International Business Council. . . . The Air Force recently demonstrated a radio-controlled balloon system that, it says, could be used to carry instruments for a number of electronic missions.

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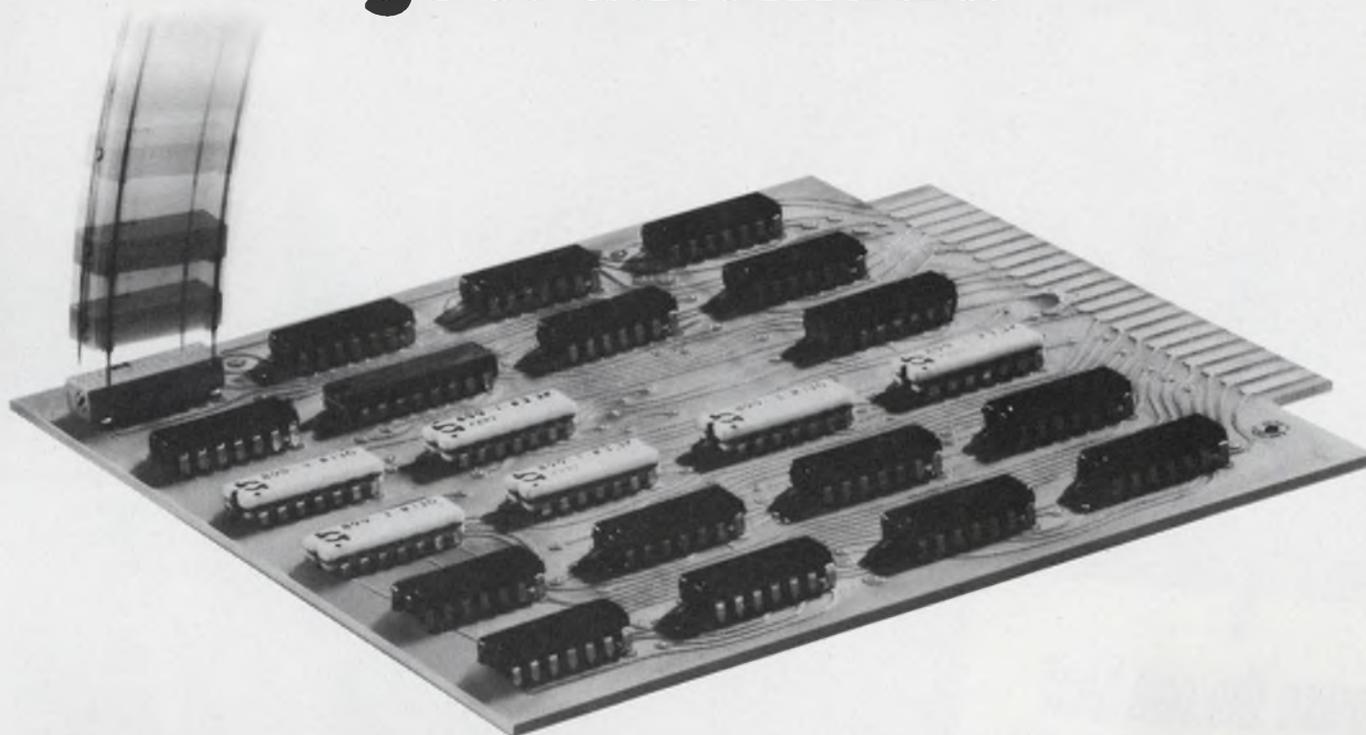
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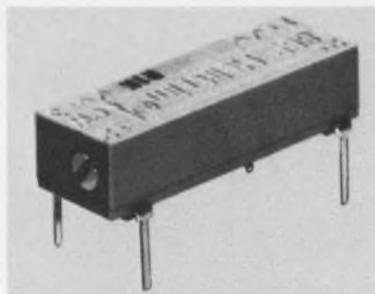
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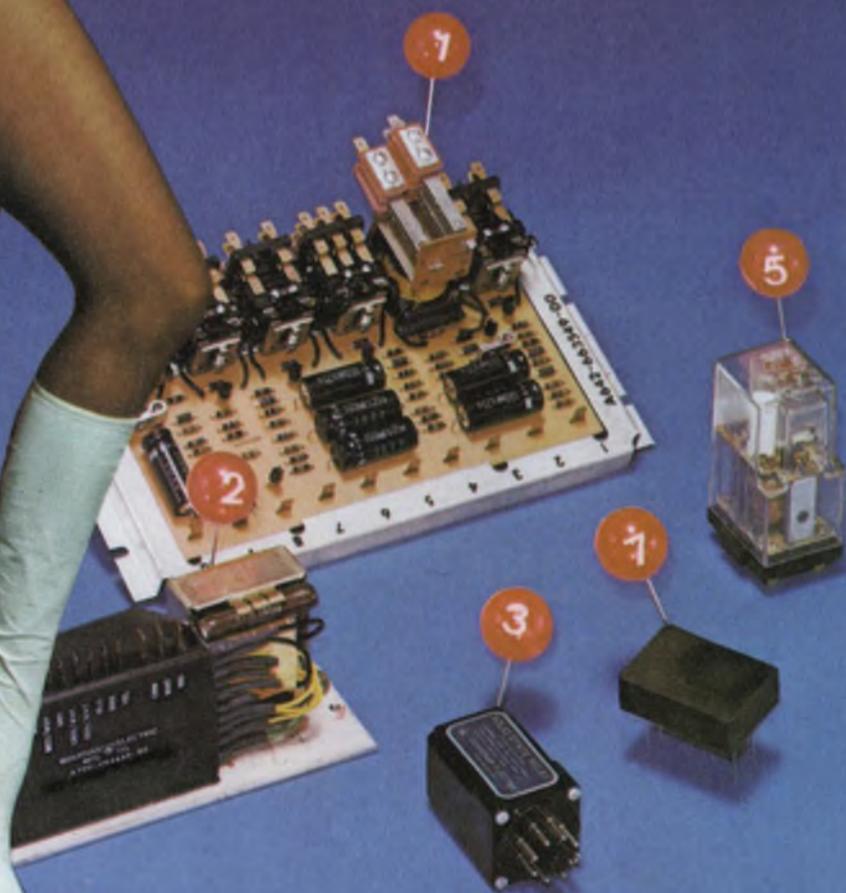
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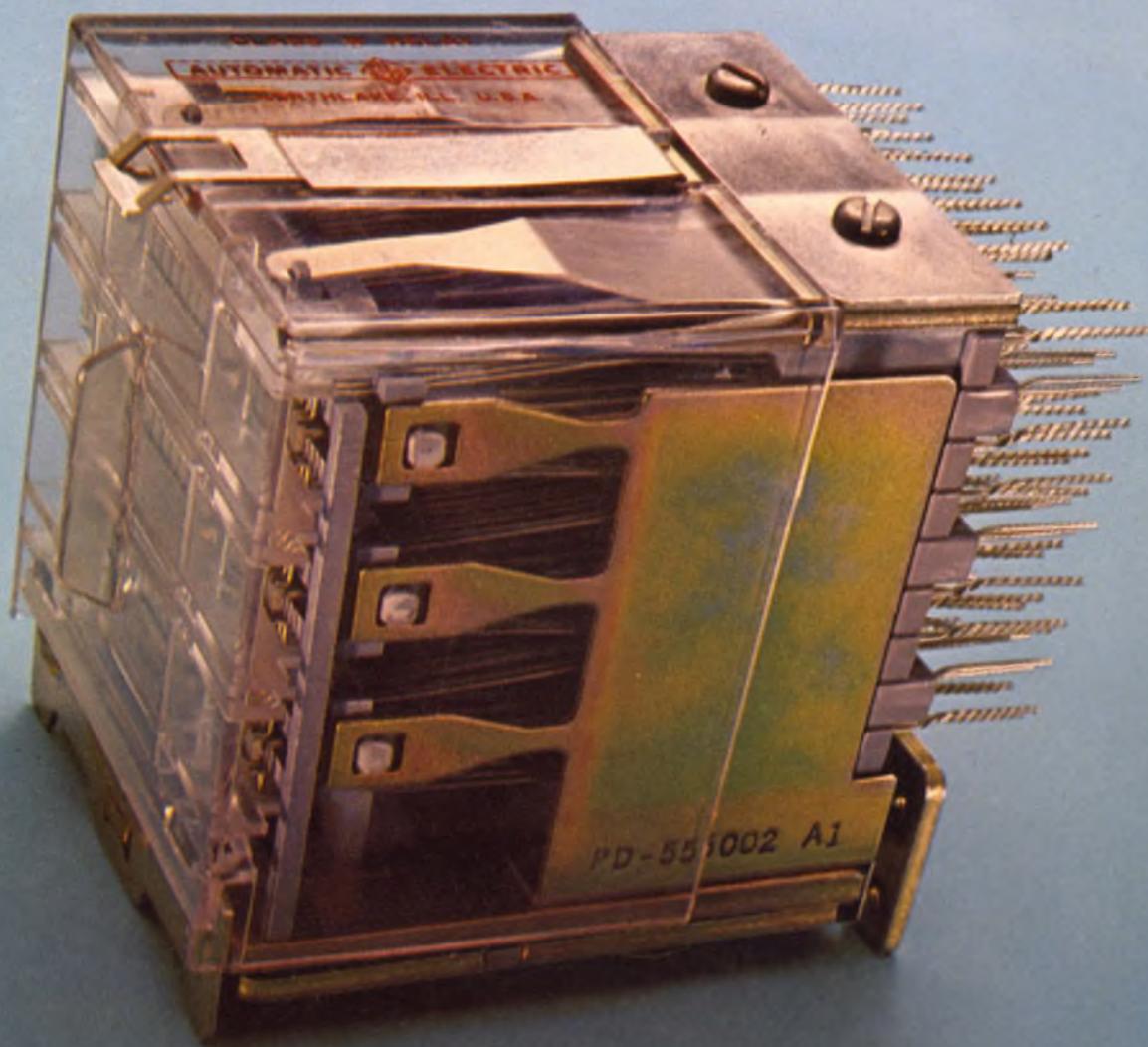
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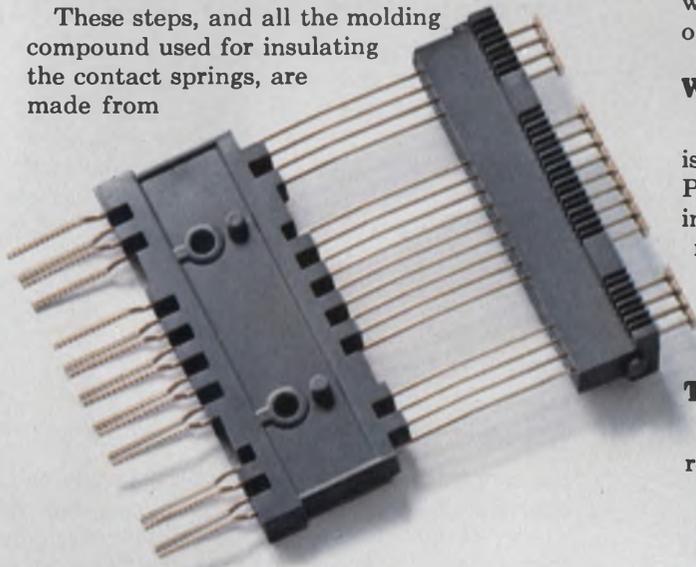
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diallyl phthalate. (They call it DAP for short.) It has great insulating properties and it wears like iron. Even if the humidity is high, you have excellent protection.

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We're for independence.

Our springs are longer, because the longer the spring, the more independent they get. And the better contact they make. Don't forget, the wire-spring relay is the most reliable way to get a permissive make or break contact. You can rely on it.

The middle contact springs have to be stationary. To make sure they stay that way forever, we actually mold them between two thick pieces of DAP on both ends. Just try to move one.

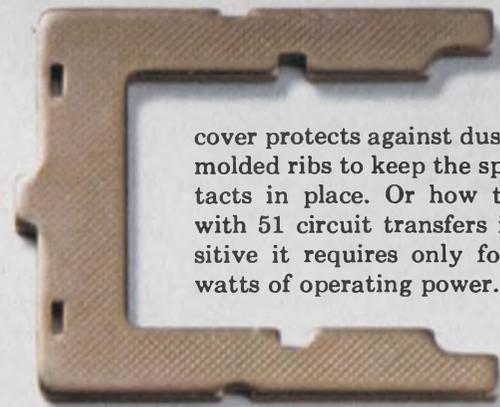
When we say flat, it's flat.

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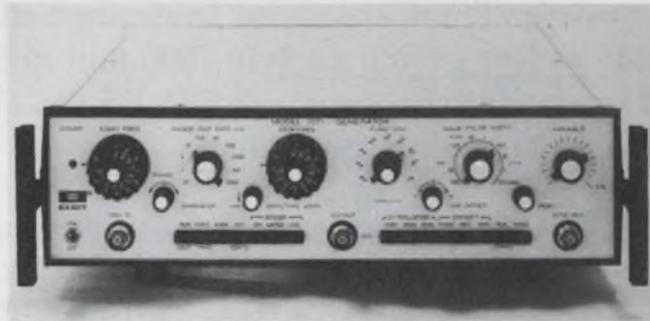
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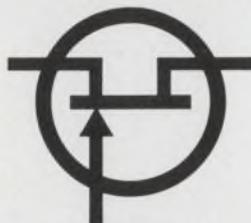
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INFORMATION RETRIEVAL NUMBER 31

ELECTRONIC DESIGN 1, January 4, 1973

Stop the computer. I want to get off.

There's something impressive about a computer that helps us land guys on the moon. I'm even impressed by a machine that can tell me in New York, within seconds, that seat 14A is available on the 2 p.m. United Flight from Denver to Seattle next Tuesday. But most of us are so jaded that we take such accomplishments for granted. We accept them as casually as we accept flying across the country in five hours—and finding our baggage on the other end.

And there's the trap. We're so casual that we may give the computer too much authority. At some point when we're not looking we may unwittingly let it take over—despite warnings from the science-fiction writers. I'm not an alarmist, but I sometimes wonder if it's not beginning.

When I was younger, everybody in my neighborhood would always say, "Let George do it." Today everybody's saying, "Let the computer do it." That's understandable because the computer has a sensational batting average. It processes millions of payroll checks with hardly an error. It zips through millions of bank statements with scarcely a slip.

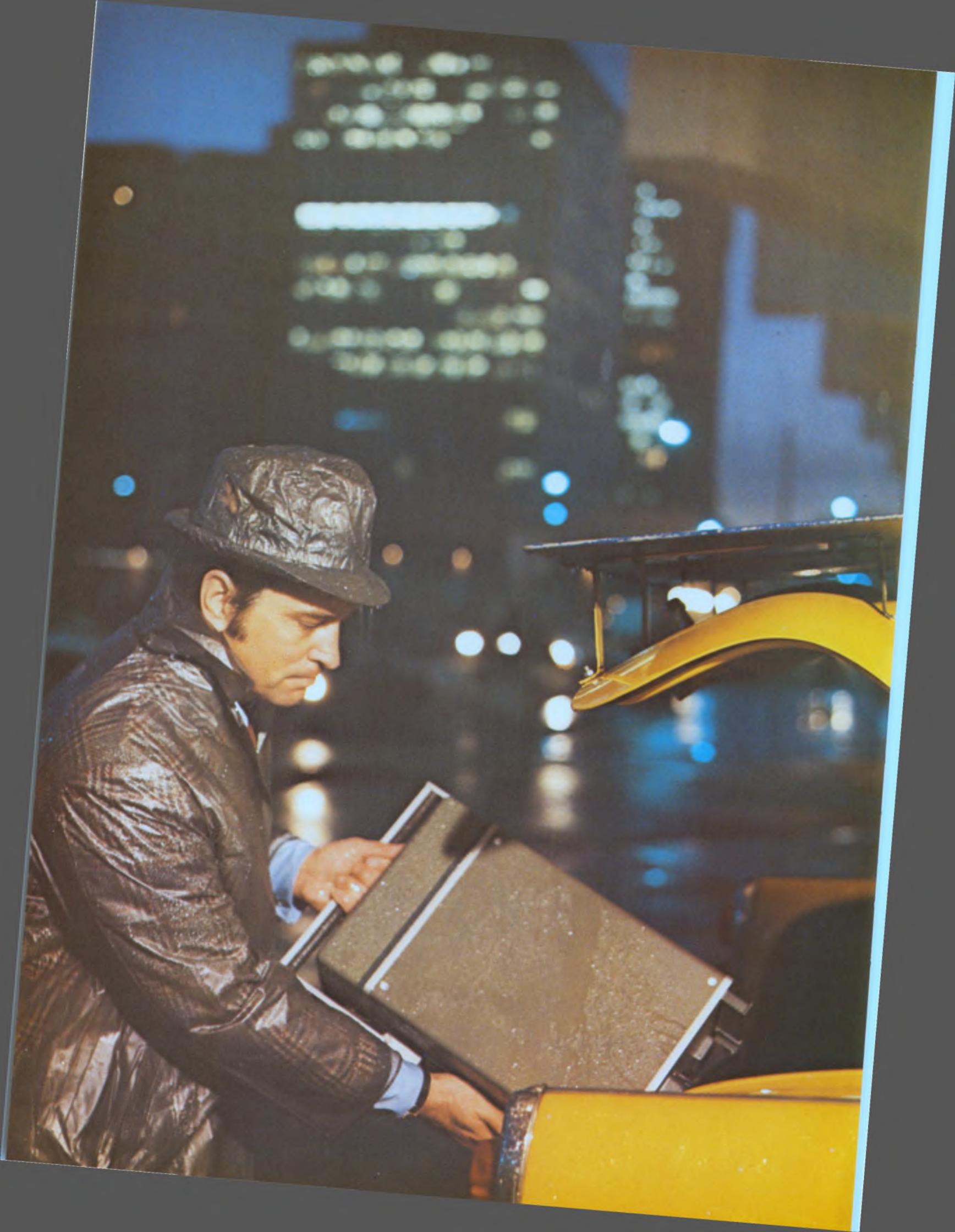
But when it slips, it can really pull a corker—one that's not easily undone. In the old days, when your grocer sent you the wrong bill, you could call and say, "Hey Jack. You sent me Mulligan's bill by mistake." And he'd say, "Gosh, I'm sorry. I'll fix it right away." Try to get that kind of action today if you find an error on your credit-card statement. It can take months to get a computer to admit it made a mistake.

Often it's not the computer's fault. It's ours. We design for the convenience of the machine instead of man. The whole mess hit me one night in Philadelphia when I needed a room. I telephoned the nearest hotel—the Sheraton—and got a friendly chap who said: "Sorry, we can't book you. Call our toll-free number in St. Louis and get your room through our computerized reservation system." I didn't mind; it wasn't my nickel. IT&T (Sheraton's parent) paid AT&T for the call. But it did seem ludicrous to place a 900-mile call to book a room half a mile away. Are we going to get sillier?



A handwritten signature in cursive script that reads "George Rostky". The signature is written in dark ink and is positioned above the printed name.

GEORGE ROSTKY
Editor-in-Chief



Think Twice:

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They're tough go-anywhere scopes: weatherproof, dustproof, completely self-contained. Not the kind of "portable" that's gently moved from bench to bench, trailing a power cord. With a 1700 Series scope you don't worry about the rain. Or the rough ride. Or whether, when you get there, you'll find ac or dc power—or no line power.

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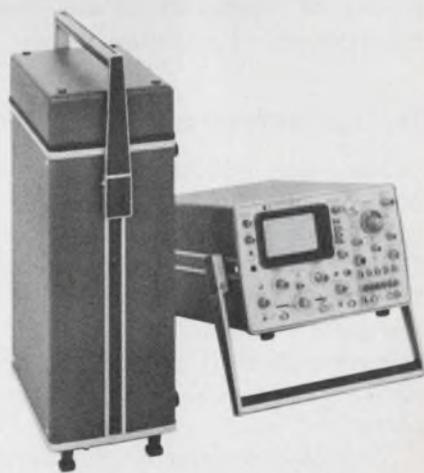
But that's just the beginning. Then the 1700 Series allows you to pick the specific features you need for your field service application: conventional or variable-persistence storage CRT; bandwidths of 35, 75, or 150 MHz; sweep speeds as fast as 2 ns/div; delayed or non-delayed sweep; selectable input impedance; bright-scan viewing mode; and a built-in rechargeable bat-

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083/1

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FOCUS

on
A/D and D/A
converters

Analog and digital circuit designers live in two different worlds.

Analog-to-digital (a/d) and digital-to-analog (d/a) converters bridge the gap between those worlds. Suddenly digital designers have to cope with specifications like linearity, offset voltage, settling time and slew rate. Likewise analog designers must grapple with quantizing error, switching time and bit resolution.

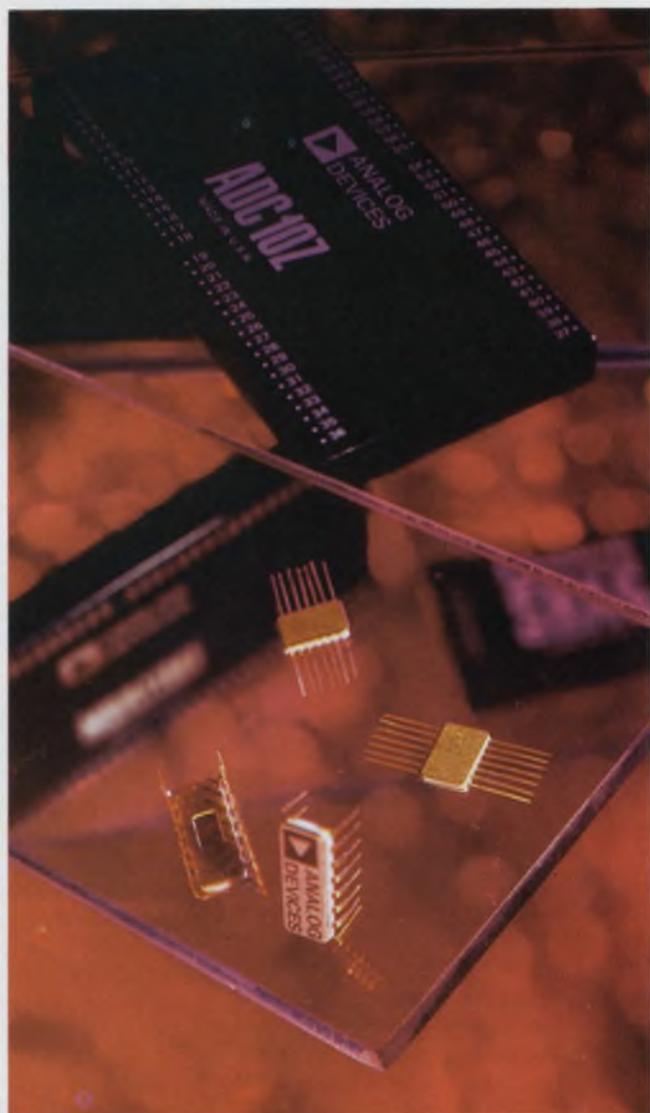
That wouldn't be so bad if the a/d and d/a manufacturers used standardized definitions for converter specs. Not only don't the specs always mean the same thing; often they don't even appear on data sheets.

Converters come in many forms: monolithic or hybrid integrated circuits, potted modules, circuit boards or rack-mounted instruments. Each class also comes in versions for several different modes of operation. Each mode has its own peculiar set of advantages and disadvantages.

The d/a converter and how it works

The vast majority of d/a converters on the market today use two basic circuits: the weight-resistor network and the R-2R configuration. Both terms relate to the type of resistive ladder network used in the converter. These two types are most conveniently described for the case of a voltage-output d/a—that is, the case where a digital input yields a discrete voltage level at the output.

Weighted-resistor d/a converters include a reference voltage source, a set of switches, a set of binary-weighted precision resistors and an operational amplifier. Each binary bit of the digital input word controls its own switch. If the bit value is a binary ONE, the switch closes. If it is

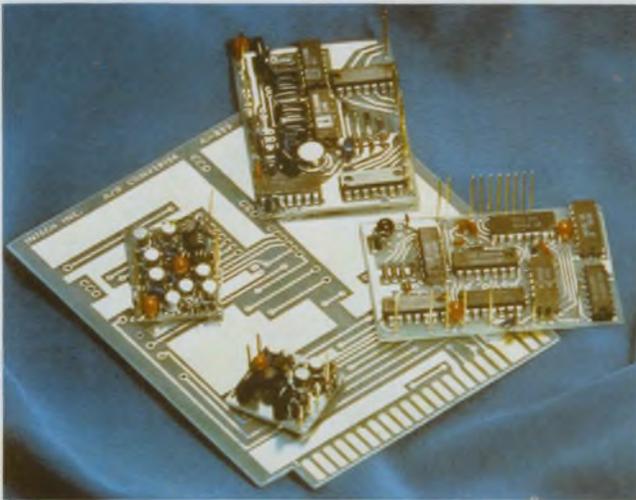


Analog Devices' high-speed, low-cost a/d converter is called the ADC-10Z. It is a 10-bit, 18- μ s, device. The company will soon have IC a/d's.

David N. Kaye
Senior Western Editor

a binary ZERO, the switch stays open. When the switch closes, the reference voltage is impressed across the weighted resistor in series with the switch, and a current flows into a summing bus. When the currents from all of the legs of the weighted-resistor ladder network are summed in the amplifier, the output voltage of the amplifier is proportional to the total current and therefore to the value of the digital input code.

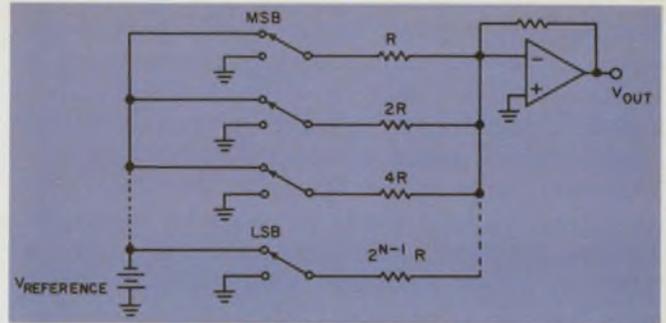
The R-2R d/a converters also contain a reference voltage source, a set of switches and an op amp. However, instead of a set of binary-weighted resistors, they contain two resistors per bit. One in series with the bit switch, and the other, valued at one-half the series resistor, is in the summing line, so that the combination forms a pi network in conjunction with succeeding stages (Fig. 2). With the least significant bit (LSB) of the digital input code farthest from the amplifier and the most significant bit (MSB) closest, it



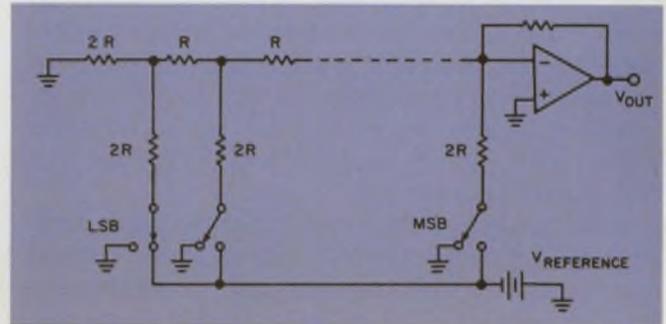
Intech's A-852, 12-bit a/d converter has a 4- μ s conversion speed, an accuracy tempco of ± 10 ppm/C and a price tag of \$420 in 1-9 quantities.

can be seen that current flowing in any leg of the ladder gets divided by two at each junction of the ladder on its way to the amplifier. Of course, all other legs of the ladder should be grounded through their respective switches at the time each bit current flows.

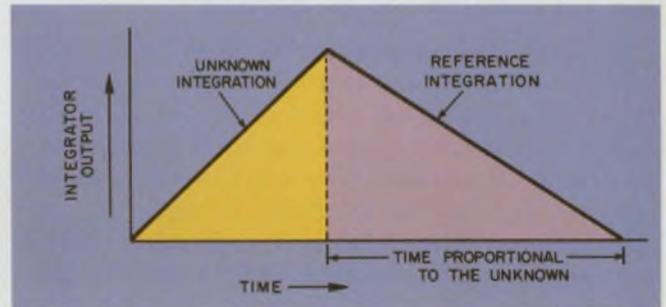
Weighted-resistor d/a converters are in general, easier to make than R-2R converters. In the R-2R all resistors and switches must be perfectly matched and must track each other over temperature. The R-2R is best made by monolithic integrated-circuit techniques, and its main advantage is that only two values of resistance are needed. The weighted-resistor converter requires a different value of resistance for each bit of the input digital code. Since the resistance values are binary weighted, the range of resistance values



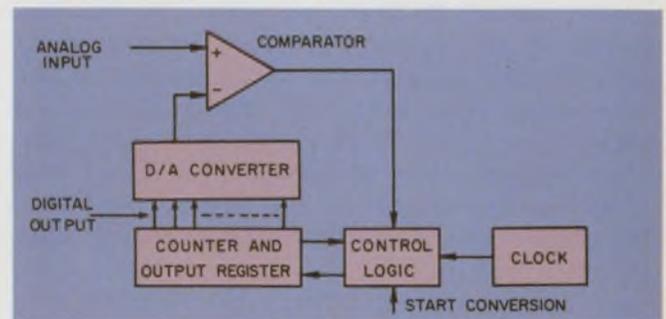
1. Weighted-ladder d/a converter uses binary weighted resistors in each bit line and sums the currents in an output amplifier.



2. R-2R D/A converter has the same current in each bit line. But as the current moves to the amplifier, it gets divided by two at each node.



3. Dual-slope integration requires that the unknown signal be integrated for a fixed time. An opposite-polarity reference is then attached, and the time it takes the integrator output to return to zero is proportional to the value of the unknown.



4. Successive approximation a/d converters work in a fashion similar to a chemical balance. They weigh each bit against the unknown, starting with the most significant bit and working down to the least significant.

becomes very large as the size of the digital word increases beyond eight or 10 bits. For example, a 12-bit d/a would require a range of resistance values of 4096:1. In a practical converter this would mean a range of about 10 k Ω to 40 M Ω . This wide range makes thick and thin-film resistor deposition impractical and requires the use of discrete resistors. For large converters—of 16 bits and up—a cascaded quad approach seems more feasible. It cascades individual four-bit converters via 16:1 current attenuators. The result is up to 16 bits of resolution in four-bit increments.

Other d/a configurations use similar types of ladder networks. One important type of d/a is the multiplying converter, which generates an output that is proportional to the product of the input digital code and a time-varying reference voltage. These converters do not include an internal reference source and can be implemented either with ladder network techniques or with taped autotransformers.

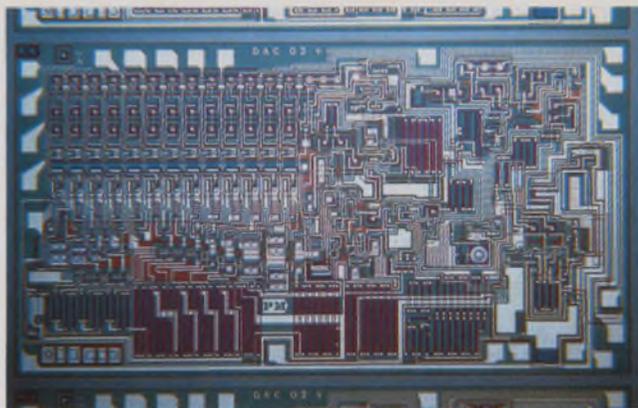
D/a converters find application in such areas as analog display driving, digital motor control, computer-controlled testing and programmable instrumentation. The multiplying d/a seems well suited to such applications as graphic displays, where vector multiplications must often be generated.

The a/d converter and its operation

As with d/a converters, the vast majority of a/d converters on the market comprise two basic types: the dual-slope integration a/d converter and the successive approximation a/d converter. Each takes a voltage input and puts out a digital code proportional to the input voltage.

Dual-slope integration a/d converters contain an integrator, some control logic, a clock, a comparator and an output counter. The unknown voltage is fed into the integrator for a predetermined period of time, as measured by the clock. Then a reference input voltage of opposite polarity is switched to the integrator. As the integrator processes the reference voltage, the output of the integrator decreases from the unknown voltage level to zero (Fig. 3). The duration of the second period of integration is automatically proportional to the average of the unknown signal level over the predetermined integrating period. A digital counter then measures the reference integration period and provides the digital code at the output. Dual-slope integration a/d converters offer excellent noise rejection and linearity, but they are fairly slow.

Successive approximation a/d converters contain a comparator, a d/a converter, a shift register, an output register and some control logic (Fig. 4). The input voltage is fed to one input of the comparator, while the output of the inter-



Precision Monolithics' MonoDAC-02 is the first 10-bit monolithic d/a to hit the market. It has a diffused R-2R network and dissipates only 500 mW.



The Milliverter II, produced by Data Technology as an amplifier-per-channel data-acquisition system. A 15-bit a/d for automatic test systems is included.

nal d/a converter goes to the other input. Each bit line in the d/a converter corresponds to a bit position in the output register. When a conversion command is applied, the converter is cleared and the MSB output of the d/a is fed to the comparator to be tried against the unknown input level. The MSB output is, of course, equivalent to one-half the converter's full-scale range. If the unknown is greater than the MSB, a ONE is inserted in the MSB position in the output register. If the unknown is less than the MSB, a ZERO is inserted. Then the circuit tries the next bit in the d/a. If this bit doesn't exceed the input, a ONE goes into its position in the output register. If it does, a ZERO is positioned. The procedure continues through to the LSB, at which stage the conversion is completed. The procedure is similar to a chemical balance in which one weight is added at a time. The main advantage of the successive approximation a/d is speed. Accuracy is primarily determined by the accuracy of the internal d/a.

In addition to the two most widely used

schemes, there are many other types of a/d converters on the market. These include single-slope integrator, triple-slope integrators, voltage-to-frequency converters, voltage-to-pulse rate converters, parallel-series converters and straight parallel converters.

The various types of a/d converters are used primarily in data-acquisition systems and modems. Parallel-series and straight parallel converters are used primarily where extremely high speed is required.

Specmanship and the d/a

Almost all manufacturers give typical specs and sometimes maximum or minimum room temperature—either 25 or 23 C. And most give all specs at nominal power-supply voltages. Temperature range and response to power-supply variation are two of the most important factors to consider in d/a's and a/d's. Temperature coefficients are usually given only for a few specs and sometimes not given at all. Susceptibility to power supply variations is only rarely stated, and often in confusing terms.

The most easily misunderstood d/a specs are resolution, accuracy and speed. Resolution is almost always stated in terms of bits—6, 8, 10, 12 or 16. This is immediately misleading. Resolution is an output quantity that refers to the difference between two voltage levels generated by the application of adjacent input digital codes, such as 000001 followed by 000010. Therefore resolution should be stated as a voltage, generally in mV. It is derived by taking the full-scale voltage range and dividing it by 2^n , where n is the number of bits accepted in the input digital code. Thus if the full-scale range is 10 V and the converter accepts a 10-bit code, the resolution would be $10/1024$, or 9.75 mV. Another way of looking at resolution is to regard it as the voltage value of one LSB.

When figuring a converter's resolution distinguish carefully between full-scale range, full-scale voltage and just "full-scale." In a bipolar converter with, for example, an output range of ± 10 V, the full-scale range is 20 V, the full-scale voltage is 10 V, and full scale is whatever makes the manufacturer's spec sheet look better. Some manufacturers have been known to use full-scale range on one data sheet and full-scale voltage on another.

Accuracy is often confused with resolution. In fact, the two specs are only loosely related. Whereas resolution gives the size of an output step, accuracy gives the relationship of the specific voltage of any given step to the National Bureau of Standards standard volt. This figure is occasionally called absolute accuracy.

Sometimes accuracy is stated in terms of the

relationship of the actual value of the voltage to the resolution. When so defined, it is usually quoted as a portion of an LSB. A widely quoted, but misleading, figure is $\pm 1/2$ LSB. This merely guarantees that the voltage at the output of the converter at some nominal temperature, like 25 C, is somewhere within the resolution of the converter. It doesn't say anything about what happens if the temperature varies. Accuracy is rarely stated for a temperature range; either the manufacturer says nothing about temperature or he gives a separate temperature coefficient accuracy (tempco). With fragmented specs, the user must do the calculation to find out how much the temperature must move before the $\pm 1/2$ LSB figure no longer holds. This temperature range may be only a few degrees.

Since accuracy relates to an analog quantity, it would be better stated as percentage deviation. Also, purists point out that it should really be called "inaccuracy."

When a tempco is given, it should also be given in percent per degree centigrade. This would allow the engineer to calculate easily the variation in accuracy over a temperature range. Unfortunately most manufacturers prefer to give the figure in ppm (parts per million) Centigrade. This is quite easily converted to percent per degree C, but why should it be necessary to convert? Specs should be given consistently in the first place. Note also that specified tempcos are often just typical figures. Few manufacturers take the trouble to measure it accurately for many units and to come up with a reliable maximum tempco figure.

Absolute accuracy consists of several components. Included are scale factor, linearity, offset voltage and power-supply rejection, to name just a few of the most important. Scale factor relates to the actual output voltage when the input calls for a full-scale output. The deviation from the desired level is the scaling error. This should be given as a percentage of full scale, but it rarely is. When a line is drawn from the actual full-scale value down through zero, the deviation from that line is sometimes called the relative accuracy. It is also sometimes called the linearity of the d/a, but shouldn't be because when the input code calls for zero output, the resulting output is usually a finite voltage. The latter is called the offset voltage.

To get true linearity—or, more correctly, non-linearity—of the converter, the line should be drawn from the actual full-scale reading to the offset voltage. Now, deviations from that line are the true nonlinearity of the converter.

Power-supply voltage changes will often cause the full-scale voltage to vary. Thus the linearity—and, in turn, the accuracy—will vary. Sometimes, but not often, a term called power-supply

rejection is offered. It is usually in terms of “% per %.” Only in rare cases is the engineer told exactly what this means. It usually means percent change in scale factor for a 1% change in power-supply voltage. Sometimes, though, it means percent change in accuracy for a 1% change in power-supply voltage. It is also sometimes called power-supply sensitivity. This particular spec appears more commonly in a/d converter data.

Since accuracy is made up of all of these factors, it could be important to know how each varies. Variations occur with both temperature and time. Sometimes scale-factor errors and offset voltage can be nulled with external potentiometers. But other error sources aren't so easily corrected.

Linearity is the most important individual spec. Unless it is always within $\pm 1/2$ LSB, the converter may be nonmonotonic—that is, when the input code calls for a small increase in the output, the output may go down instead. Most users of d/a's are in bad shape if their converters aren't monotonic. Bad things happen—like oscillation in feedback systems.

Each factor affecting accuracy varies differently with temperature. A well-written spec sheet will give separate tempcos at least for linearity, scale factor and offset voltage. Also the tempcos should be maximum figures, not typical. In fact, max/min figures should be given for all specs. “Typical” figures have been the cause of many cost overruns. If the d/a has a zener-diode reference—and not all do—the reference voltage must be recalibrated occasionally. It varies with time, causing variations in the scale factor. But how often it should be calibrated is rarely indicated on data sheets.

Long-term linearity variations are caused by variation in the resistive ladder network. Thick-film resistors can change as much as 0.1% a year. Wirewound resistors are better, but they cost more and respond slower. In addition resistor values can be affected by thermal and electrical stress during use. Variation of specs with time affects the repeatability of the d/a. Some d/a's carry the term “precision.” Precision means repeatability. Yet few manufacturers give the engineer any way of knowing how their converters will respond to the same code a day later, a month later or a year later.

Over-all accuracy specs are usually averages of the various classes of error. Sometimes the “accuracy” is an RMS average. Sometimes it is a measured value.

Many users expect a 12-bit d/a to be accurate to 0.01% over the full quoted temperature range of the converter. This is $\pm 1/2$ LSB for 12 bits. More likely it will be accurate to $\pm 1/2$ LSB for some window around 25 C and then accurate to



A two-channel d/a made by Perkin-Elmer, the only company to produce a multiplying d/a that uses an auto-transformer rather than a resistive ladder network.

$\pm 1/2$ LSB for 11 bits for a while and then 10 bits and then nine bits.

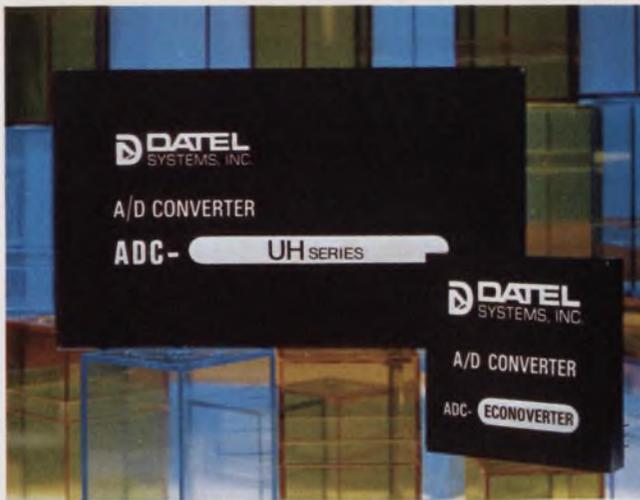
For some applications, this may be all right. But, when it isn't, the engineer doesn't find out until it's too late. It is possible for a 12-bit d/a to have only 10-bit accuracy to $\pm 1/2$ LSB, and it is possible to have 14-bit accuracy to $\pm 1/2$ LSB. Remember, resolution and accuracy are independent quantities. In most feedback control systems, resolution and monotonicity are much more important than accuracy. If they are for you, tell the vendor. He can usually get you a cheaper unit.

Settling time vs slewing rate

Do d/a's settle or slew? In fact, they do both. Both are often specified, and they should be, so the designer can know how fast the d/a actually converts.

Settling is often given as the time that it takes the output voltage to move from one stable level to the next, to within $\pm 1/2$ LSB, while the input changes from one code to the next adjacent one. At other times it is given for a change from zero to full scale on the output when the input code calls for the change. The time required for a full-scale change is the maximum conversion time and the more important of the two. Sometimes both figures are given. If settling time is given only for a one-LSB change, the converter will seem to be much faster than it actually is. Settling time may also vary, depending upon whether the unit is a voltage-output d/a or a current-output d/a. Additional confusion is caused by the fact that settling time is often specified to within 0.1%, 0.05% etc., of full scale. These figures may or may not correspond to $\pm 1/2$ LSB.

Slewing rate is the rate of change in $V/\mu s$ that the output is capable of attaining. It is controlled by the output amplifier.



Datel's ADC-UH8B an eight-bit a/d, has a conversion rate of 10 MHz. The ADC-Econoverter is a six-bit a/d that sells for only \$22.95.

Sometimes switching time is given. This is the settling time less the period of damped oscillation after the output has completed its initial ramp and overshoot the desired value.

Noise a problem with high resolution

As the quoted resolution of the d/a converter gets above 11 or 12 bits, noise becomes of considerable concern. It takes two forms: internally generated noise in the converter and external noise picked up from the power supply or other adjacent circuitry. Internal noise can be specified by the manufacturer as either an rms value, $3\text{-}\sigma$ noise or peak noise over the bandwidth of the converter. It rarely is given for d/a's, but sometimes is given for high-resolution a/d's.

Sometimes common-mode, or normal-mode, rejection are given as well. These specs relate mainly to external noise. Often there is enough pickup from the power supply to throw the converter out of its rated accuracy. An even more common problem, once the resolution gets up to 16 bits, is caused by the resistance of even short runs of conventional wiring. For example, consider the case of a 16-bit d/a with a 10-V, full-scale range. Just 15 mA—the full scale current output of a typical d/a of this type flowing through two feet of 18 gauge wire—will drop approximately $165\ \mu\text{V}$, or the equivalent of slightly more than 1 LSB for this converter. This raises the entire converter to a finite common-mode voltage—large enough to seriously degrade the converter's accuracy.

Noise problems such as these can be relieved by careful shielding of the converters, the use of decoupling networks at the power-supply ports of the converter and other techniques of careful circuit design. Some manufacturers build in such features; others don't. The only sure way to



A differential d/a, the Model 840, made by Computer Central. It gives an analog-signal output that is proportional to the difference between two parallel BCD inputs.

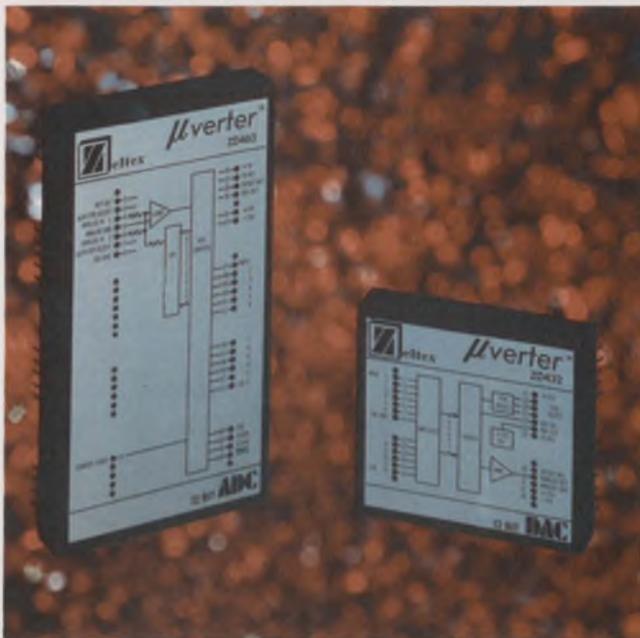
know whether a converter will work in your equipment is to get one and try it.

A slightly different type of noise problem in d/a's is that of voltage spikes on the output caused by the closing of the switches within the converter. These glitches can easily be several LSBs in magnitude, and they can cause problems in the external circuitry. Some converters have built-in deglitchers—sample-and-hold circuits that hold the output of the converter constant during each switching period and then let it go to the next value. But these circuits add to the price of the converter and are not necessary in many applications.

Many options are available with d/a's. You can usually specify the input code to the converter. Most popular of the available codes are straight binary, binary-coded decimal, gray, ONEs-complement binary, TWOs-complement binary, sign-magnitude, offset binary and a variety of other modified or complementary codes. The converter may or may not have an output buffer amplifier. It may or may not have an internal reference; for very high accuracy, it is better to provide your own external reference. The converter may have a variety of output voltage or current ranges. Finally it may come with a variety of operating temperature ranges. When comparing prices, make sure the options are all the same.

A/d specs are similar to d/a specs

Most everything said for d/a specs also holds for a/d specs. These also are often typical rather than max/min specs, and they may be given only at a nominal temperature and power-supply settling. A main difference is that the output of an a/d is a series of digital codes. Therefore accuracy and resolution, as well as most other specs, should be given in digital terms rather than ana-



A pair of economy 12-bit products produced by Zeltex. The ZD462 is an a/d that sells for \$99 (1-99). The ZD432 is a d/a that sells for \$49 (1-99).

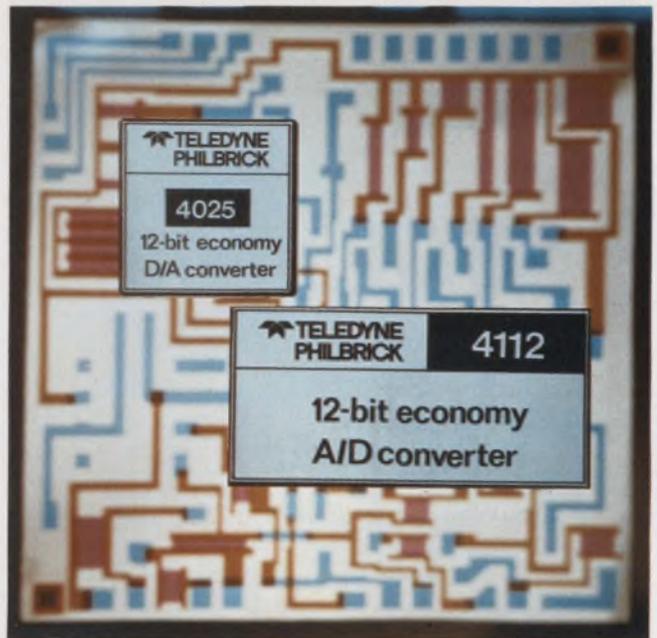
log. For example, resolution is in bits. Since the number of bits defines the number of discrete output codes that the input analog signal can be broken into, it is fair to talk of an 8, 12 or 15-bit a/d converter.

Accuracy must also be given in terms of bits. Therefore the terminology $\pm 1/2$ LBS is fair. Four additional factors enter into accuracy that are not called out for d/a converters. They are quantizing error, missing codes, aperture error and differential linearity.

Quantizing error refers to the fact that a range of analog voltages are represented by a discrete digital code. The width of that range is 1 LSB. Since an a/d converter inherently breaks up a linear signal into discrete steps, it is quantizing the signal. The inherent quantization error of every a/d converter is $\pm 1/2$ LSB. This is over and above any other errors that contribute to the inaccuracy of the converter.

Missing codes come about when the input voltage passes through a range that is supposed to be represented by a particular code and that code is not there. In its place is the code either directly before or directly following the desired one. Some converters guarantee no missing codes; most do not. If missing codes can exist, the stated resolution of the converter is also in question.

Aperture error arises from converter indecision as to the proper input voltage to convert, if the input varies by more than equivalent 1 LSB during the conversion time of the converter. For example, should the output code represent the signal at the beginning of the conversion time or the signal just before the end of the conversion time? Most converters give the code cor-



Teledyne-Philbrick's pair of economy 12-bit units. The 4112 is an a/d that sells for \$109 (1-9). The 4025 is a d/a that sells for \$69 (1-9).

responding to the signal at the beginning of the conversion time. Others do not. Only a very few manufacturers acknowledge aperture error with a spec on the data sheet.

Differential linearity is the difference in the size of the quantum steps represented by the digital output codes. For example, if one code represents 10-mV of input range and another only 8-mV, the differential linearity is 2 mV. If an LSB is 10 mV, the differential linearity would probably be stated on the spec sheets as $\pm 1/10$ LSB. This is fair, since the output of the converter is digital and errors in it should be expressed digitally.

Other errors—such as linearity, offset voltage and scaling or gain error—also exist. The same problems occur with a/d's as, we saw earlier, with d/a's. This is true for errors, tempeos and noise.

How fast an a/d?

Speed in an a/d converter is really the number of conversions that can be made in a unit time. It is best given as a conversion rate or throughput rate. Sometimes speed is given as a conversion time. This is misleading. There is a necessary dead period between conversions called the reset time. It is the time that it takes the system to absorb a conversion and reset its amplifiers. This is rarely given, but usually it is on the order of a few hundred nanoseconds. It must be added to the conversion time before the reciprocal can be taken to derive the conversion rate.

Similar options exist for a/d's as for d/a's. The differences lie in the fact that voltage ranges

apply to the input, while the output is a digital code. An additional option that is sometimes offered is a parallel-serial converter for the output. Most a/d's do not have input buffer amplifiers, but they are offered as options.

What's available in the field

There are so many manufacturers of d/a's and a/d's that it is difficult to pick out the best unit for an application. No monolithic a/d's are on the market yet. However, several manufacturers make six or eight-bit monolithic d/a converters, among them Precision Monolithics, Harris Semiconductor, Motorola, Fairchild and Siliconix. Only Precision Monolithics, with its Mono DAC-02, has a 10-bit monolithic DAC on the market at present. This unit has a diffused R-2R ladder network and a settling time to $\pm 0.05\%$ of $1.5 \mu\text{s}$. Analog Devices will soon introduce a competing 10-bit d/a that will also be monolithic and will feature a thin-film R-2R network. Motorola is offering six and eight-bit multiplying d/a's. These monolithic units can usually be specified over a MIL temperature range of -55 to $+125$ C.

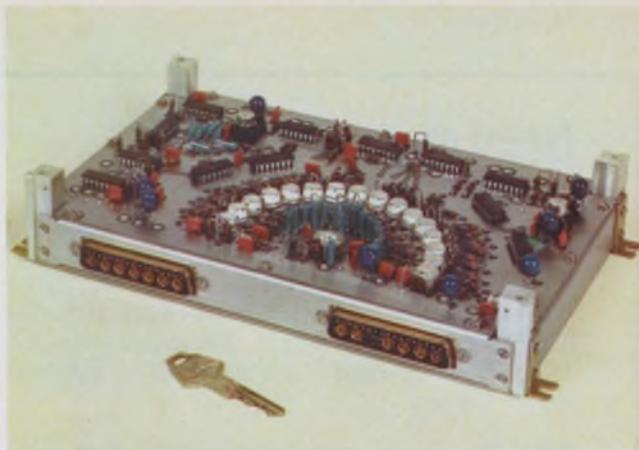
Most commercial units are for the range of 0 to 70 C. Aside from the monolithic units and some of the hybrid, few converters will work over the full MIL temperature range.

Among the fastest d/a's on the market are the eight-bit DAC 371-8 from Hybrid Systems, which settles in 950 ns; 10-bit MDS-1020 from Computer Labs which settles in 20 ns; 14-bit MP-1914A from Analogic, which settles in $3.5 \mu\text{s}$; 15-bit 1535 from Tustin, which settles in $1 \mu\text{s}$; and 16-bit 20255 from Lancer, which settles in $15 \mu\text{s}$. Other manufacturers with very fast d/a converters include Analog Devices, Burr-Brown, Inter Computer Electronics, Optical Electronics, Zeltex, Function Modules, Cycon and Data Device Corp.

Many manufacturers also produce economy d/a converters that don't have outstanding specs but are cheap. Some examples of these are the 12-bit 4025 from Teledyne-Philbrick, which sells in small quantities for \$69; eight-bit 371-8 from Hybrid Systems, \$9.90; 12-bit ZD432 from Zeltex, \$49. Of the 16-bit DACs on the market, one of the cheapest is the DAC 45 from Burr-Brown, at \$350. Several other manufacturers are aggressively promoting low-cost d/a converters—Datel, Function Modules, Cycon, Analog Devices and Micro Networks.

A/d's come in all shapes and sizes—from rack-mounted instruments like the Data Technology 15-bit Milliverter II, and comparable units from Xerox and Preston Scientific, to economy modules and hybrids from Zeltex, Datel and Hybrid Systems.

Among the more unusual converters on the



The MOD-4100, four-bit a/d made by Computer Labs is a parallel unit with a 100-MHz conversion rate. It sells for about \$2000 and is the fastest a/d on the market.



Singer-Kearfott's SKC-2950 is an eight-bit militarized a/d converter. It features a 25-ns conversion time and has two channels.

market are the DD/A 840 from Computer Central. It is a differential d/a that gives an analog output proportional to the difference between two parallel BCD inputs.

Another interesting product is the Perkin-Elmer Varidac series—one, two and four-channel d/a converters that do not use a resistor network but taps on an autotransformer for extremely stable operation over a wide temperature range. These d/a's are of the multiplying type.

D/a's and a/d's are getting faster, smaller and cheaper. The trend seems to be towards packing more and more electronics into small packages. Instead of just getting an a/d in a module, you can now get a whole data-acquisition system, including a/d, multiplexer, sample-and-hold amplifier and logic. Often even memory and buffer amplifiers are included. This field is still in its infancy. As it matures, a more standard means of specifying converters may appear. ■■

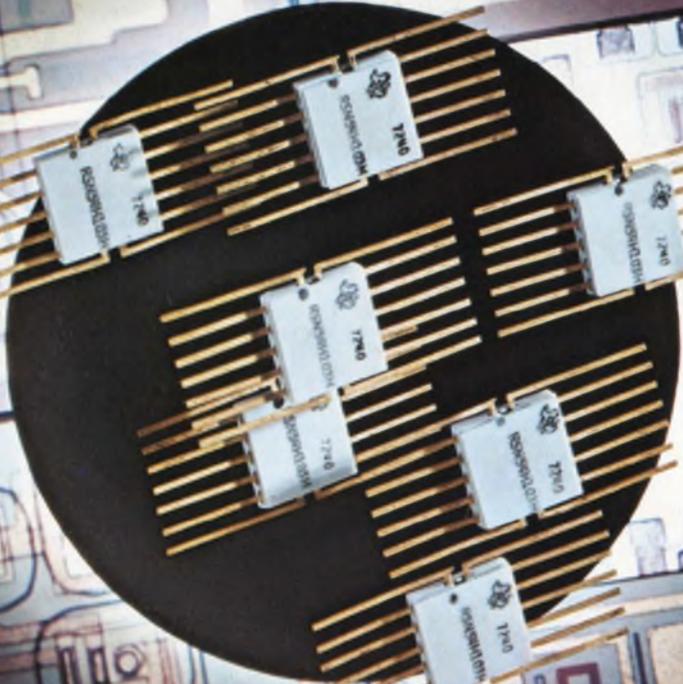
(continued on page 64)

Need more information?

The products cited in this report have, of necessity, received only cursory coverage. And they don't represent the vendors' full lines. Readers may wish to consult the manufacturers listed here for more details. For quick response, circle on the retrieval card the boldface numbers shown below:

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- ALL, Div. Cutler Hammer, Inc., Comac Rd., Deer Park, N.Y. 11729. 595-6471. (John McMurray, Business Development). **Circle 318**
- Aim Electronics, Ltd., the River Mill Stives, Huntingdonshire, England. **Circle 319**
- American Astrionics, 291 Kalmus Dr., Costa Mesa, Calif. 92626. (714) 557-8480. (Phillip Harms, Project Engineer). **Circle 320**
- American Electronic Laboratories, Inc., P. O. Box 552, M/S 1123, Lansdale, Pa. 19446. (215) 822-2929. (A. Rosset, Manager Advertising). **Circle 321**
- Analog Devices, Inc., P.O. Box 280, Norwood, Mass. 02062. (617) 329-4700. (Martin Dross, Sales Manager). **Circle 322**
- Analogic Corp., Audubon Rd., Wakefield, Mass. 01880. (617) 246-0300. (Fred Molinari, Director of Marketing). **Circle 323**
- Applied Devices Corp., 60 Plant Ave., Hauppauge, N.Y. 11787. (516) 234-4000. (Saul Seigel, Director of Engineering). **Circle 324**
- Astro-Systems, Inc., 6 Nevada Dr., Lake Success, N.Y. 11040. (516) 328-1600. (N.I. Wheatcroft, Vice President Marketing). **Circle 325**
- Austin Electronics, 450 First Ave., Roselle, N.J. 07203. (201) 241-3300. (J. F. Donnelly, Sales and Estimation). **Circle 326**
- Baldwin Electronics, P.O. Box 3838, Little Rock, Ark. 72203. (501) 375-7351. (Herb Welse, Advertising Manager). **Circle 327**
- Beckman Instruments, Inc., 8475 Artesia Ave., Buena Park, Calif. 90620. (714) 521-3700. (Lyle Pittroff, Sales Supervisor). **Circle 328**
- Burr-Brown Research Corp., International Airport, Industrial Park, Tucson, Ariz. 85706. (602) 294-1431. (Tom Fern, Vice President Marketing). **Circle 329**
- CAE Electronics Ltd., Box 1800, Montreal, Quebec. **Circle 330**
- California Instruments Corp., 5150 Convoy St., San Diego, Calif. 92111. (714) 297-8620. (Walt Hanford, Product Manager). **Circle 331**
- Canadian Research Institute, 85 Curlew Dr., Don Mills, Ontario. **Circle 332**
- Canberra Industries, 45 Gracey Ave., Meriden, Conn. 06450. (203) 238-2351. (Ben Compo, Assistant Marketing Manager). **Circle 333**
- C & A Products, Inc., 28-17 33th St. Astoria, N.Y. 11102. (212) 721-6220. (R. Bogin, Sales Manager). **Circle 334**
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- Dynamco, Div. DCA, East Mains Industrial Estate, Broxburn, W. Lothian, Scotland. **Circle 354**
- Dynamic Systems Electronics Corp., 1310 W. 23rd St., Tempe, Ariz. 85281. (602) 272-6489. (Brad Ormsby, Operations Manager). **Circle 355**
- Dynatronics Instruments, 4800 Evanswood Dr., Columbus, Ohio 43229. (614) 885-3303. (Robert Rush, Office Manager). **Circle 356**
- E-H Research Labs, Inc., P.O. Box 1289, Oakland, Calif. 94604. (415) 834-3030. (Earl Olsen, Systems Sales Manager). **Circle 357**
- Electronic Associates, Inc., 185 Monmouth Parkway West, Long Branch, N.J. 07764. (201) 229-1100. (Ken Craven, Senior Market Support Engineer). **Circle 358**
- Electronic Processors, Inc., 5050 S. Federal Blvd., Englewood, Colo. 80110. (303) 798-9305. (Robert C. Derschang, Vice President Marketing). **Circle 359**
- EMI Electronics & Industrial Operation Blyth Rd., Hayes Middlesex, England. **Circle 360**
- EMR Telemetry, Box 3041, Sarasota, Fla. 33578. (813) 958-0811. (S. D. Bass, Marketing Manager). **Circle 361**
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- Fairchild Semiconductor, 464 Ellis Dr., Mountain View, Calif. 94040. (415) 962-2211. (Bob Ricks, Marketing Manager). **Circle 363**
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- Ferranti, Ltd., Hollinwood, Lancashire, England. **Circle 365**
- Fifth Dimension, Inc., P.O. Box 483, Princeton, N.J. 08540. (609) 924-5990. (John Pohlke, Manager Telemetry Sales). **Circle 366**
- Flight Research, Grotel Co., P.O. Box 1-F, Richmond, Va. 23201. (703) 222-0163. (Melvin Swartz, Marketing Manager). **Circle 367**
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- Nuclear-Chicago, 2000 Nuclear Dr., Des Plaines, Ill. 60018. (312) 298-6600. (Dick Beers, Advertising Manager) **Circle 407**
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- Precision Monolithics, 1500 Space Park Dr., Santa Clara, Calif. 95050. (408) 246-9225. (Jerry Zis, Product Marketing Manager) **Circle 414**
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- Ragen Precision Industries, 9 Porete Ave., North Arlington, N.J. 07032. (201) 997-1000. (James Hobbs, Marketing Manager) **Circle 417**
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- Teledyne Philbrick, Allied Dr. at Route 128, Dedham, Mass. 02026. (617) 329-1600. (Walter Patstone, Product Manager) **Circle 435**
- Teledyne Systems Co., Lewisburg Div., Industrial Park, Lewisburg, Tenn. (615) 359-4531. (Ralph Mann, Manager of Future Programs) **Circle 436**
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- TRW Systems Group, BCRI Space Park, Redondo Beach, Calif. 93278. (213) 536-1977. (Hank Dimond Program Development) **Circle 443**
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- Varian, 611 Hansen Way, Palo Alto, Calif. 94303. (415) 326-4000. (Joe DePaolo, Product Manager) **Circle 445**
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A circular silicon die is shown in the center, with numerous gold wire bonds extending from its perimeter. The die is mounted on a printed circuit board (PCB) with a complex, multi-layered circuit pattern in shades of blue, green, and gold. The background is a close-up of the PCB's intricate circuitry.

More TI integrated circuits are used in today's electronic systems than any other brand in the world. And for the reasons you'd expect: Technology. Volume. Price. Breadth. Dependability. Service. Quality. Weigh them all when you buy radiation-hardened IC's.

RAD-HARD IC'S

If your system calls for radiation-tolerant ICs, TI can provide full-service support.

**49 standard digital and linear functions.
Custom capability backed by more than a decade
of "rad-hard" R&D and production experience.
Computer-aided design. Comprehensive documentation.**

Full service.

From materials technology to product design, manufacturing experience and capability, support data and program management—Texas Instruments can supply everything you need to meet the most challenging system and program requirements.

TI has been solving radiation effects problems for more than 10 years...and is a major supplier of radiation-hardened devices for strategic defense systems.

Technological strength— now and in the future

TI is thoroughly experienced in all technologies basic to radiation-tolerant integrated circuits, including dielectrically isolated substrates, thin-film resistors, minimum-size transistor geometries, narrow base widths, various packaging options and photocurrent compensation, where required.

Computer-aided design is now a matter of routine for both the design and layout of TI radiation-tolerant integrated circuits.

And TI will continue to extend its technological capability by combining radiation-hardening expertise with in-depth knowledge of MSI, beam leads and low-power Schottky TTL. (In addition, TI has depth experience in "rad-hard" discrete devices—both power and small-signal—and offers a broad line.)

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In addition to its standard rad-hard line, TI has complete facilities, personnel and know-how—including all necessary R&D back-up—for the design of radiation-tolerant devices to your specifications and program requirements. A top-secret facility and storage security clearance, as well as provisions for comprehensive documentation, further strengthen TI's ability to provide full-service support.

Industry's broadest standard line

TI today offers industry's broadest line of standard rad-hard ICs—49 digital and linear functions, with more to come.

Digital ICs

	1mW/30ns	10mW/10ns	20mW/7ns	DTL
	TTL	TTL	TTL	
Quad 2 NAND	RSN54L00	RSN5400	RSN54H00	-
Hex inverter	-	RSN5404	RSN54H04	-
Triple 3 NAND	RSN54L10	RSN5410	RSN54H10	RSN15962
Dual 4 NAND	RSN54L20	RSN5420	RSN54H20	RSN15930
Single 11 NAND	-	RSN5431	RSN54H31	-
Dual 4 buffer	-	RSN5440	RSN54H40	RSN15932
Dual 4 power gate	-	-	-	RSN15944
Dual 2-wide AOI	-	RSN5456	RSN54H56	-
Single 4-wide AOI	RSN54L57	RSN5457	RSN54H57	-
Single 2-wide AOI	-	RSN5458	RSN54H58	-
Dual 3-2 AOI	-	-	RSN54H66	-
RS flip-flop	RSN54L71	-	-	-
JK flip-flop	RSN54L72	-	-	RSN15945
Dual D flip-flop	RSN54L74	RSN5474	RSN54H74	-
Dual J-K flip-flop	-	-	RSN54H103	-
One shot	RSN54L122	-	-	-
Dual 3 NAND	RSN54L130	-	-	-
Dual 3 NAND w/expander	RSN54L131	-	-	-
3-to-8 decoder	-	-	RSN54H149	-

Linear, Interface ICs and Monolithic Arrays

Standard operational amplifier	RSN52709
High-performance operational amplifier	RSN52800
2-channel/capacitor-coupled plated-wire sense amplifier	RSN55900/55910
4-channel/DC-coupled plated-wire sense amplifier	RSN55920
Dual 500mA word switch	RSN14026
Quad JFET interface driver	RSN21890
7-diode array	RSN14925
16-diode array	RSN14097
Quad 30mA NPN transistor array	RSN21885
Quad 100mA NPN transistor array	RSN21886

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For price and availability, call your local TI sales office. Or call Gerd Noebel, in Dallas, (214) 238-3025. For a copy of TI Bulletin CB-146, "Radiation and Semiconductors," circle 250 on the Reader Service card. Or write Texas Instruments Incorporated, P. O. Box 5012, M/S 308, Dallas, Texas 75222.



TEXAS INSTRUMENTS
INCORPORATED

Engineering jobs: What, why and where?

All indicators point to more jobs, more money and a major shortage of engineers in the near future.

Richard L. Turmail, Management Editor

Like the sign of the absentee merchant, "Back in ten minutes—already been gone five," engineering employment seems to be returning almost before it left. Despite impressions to the contrary, a number of jobs are unfilled in the electronics industry, according to a recent survey by **ELECTRONIC DESIGN**.

From this study of 30 representative companies and from other sources, the following highlights emerge:

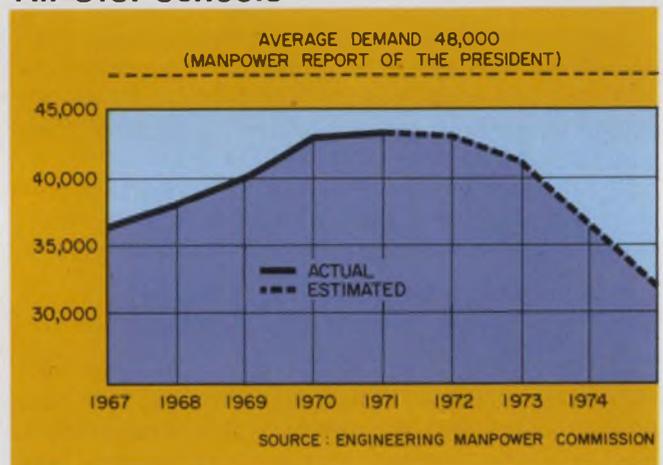
- Four of every five electronics companies surveyed by **ELECTRONIC DESIGN** reported many openings for engineers.
- The demand for engineers and scientists has nearly doubled in the last year.
- A major shortage of engineers is expected in three to four years, with shortages reported even now in some fields.
- Some 1500 job openings for aerospace engineers, and 12,200 electrical engineers in general are expected annually throughout the decade.
- Company reservations for college recruiting are up after a two-year decline.
- The over-all rate of unemployment among engineering graduates is only about 3%, or about half the national average.

Survey reveals job openings

The employers in **ELECTRONIC DESIGN**'s survey, which was conducted in the last quarter of 1972, reported job openings in a wide variety of engineering disciplines, with logic, digital and circuit designers, processor engineers and systems and industrial engineers leading the demand. Digital Equipment Corp. of Maynard, Mass., reports that it is becoming a total systems house and will need 600 domestic field-service engineers over the next year.

Specialized engineering skills, including designers of biomedical, spacecraft-power and command and control systems, are also in demand but on a smaller scale. Few of the companies sur-

Bachelor's Degrees in Engineering, All U.S. Schools

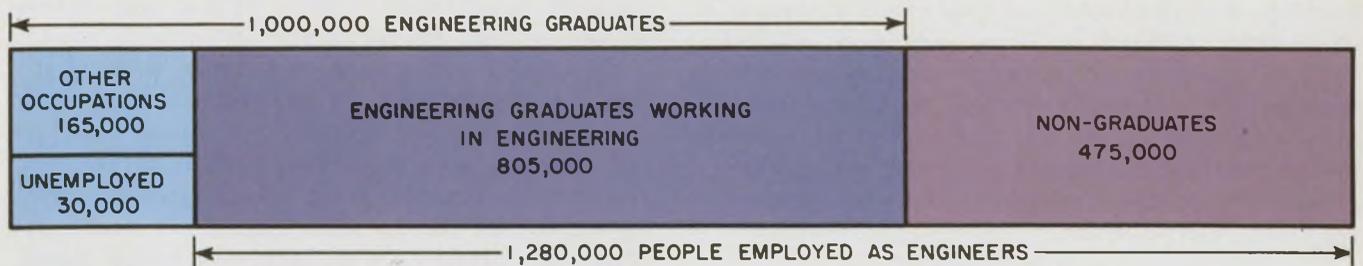


veyed, perhaps one in 10, reported that they were phasing out engineering disciplines. For the industry as a whole, there does not appear to be any engineering category that is obsolete.

Following is a breakdown of engineering openings turned up by the **ELECTRONIC DESIGN** survey. Salary ranges are included where reported. The companies were asked what jobs would be available now and in the next six months. Most indicated that most of the jobs would be available through March, 1973:

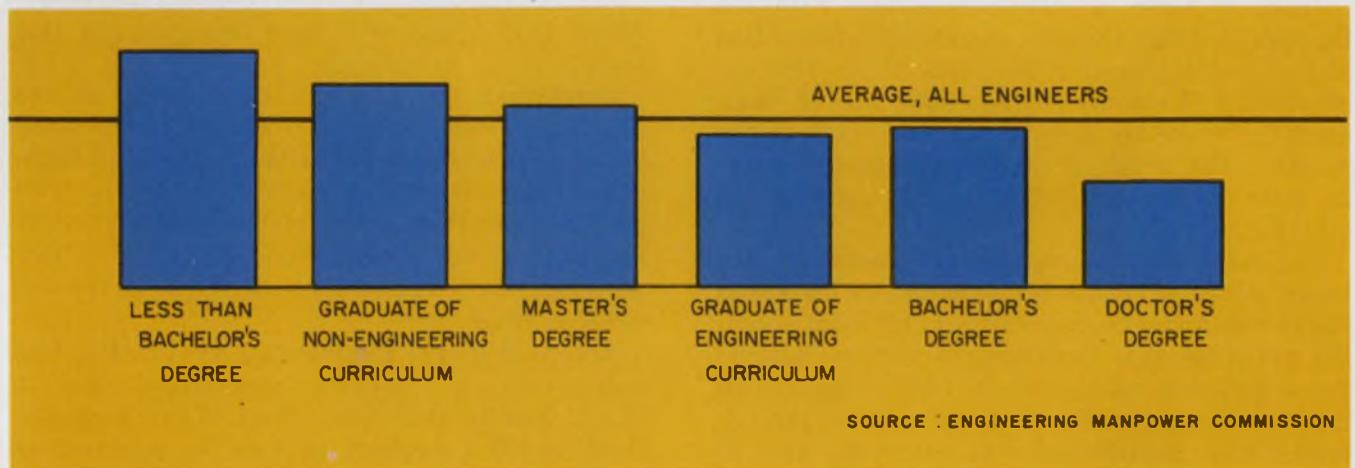
- Computer Products, Fort Lauderdale, Fla. (computers): Digital design engineer (10 to 15 k); project engineers (14 to 18 k); field engineer (9 to 12 k).
- Digital Equipment Corp., Maynard, Mass. (computers): Electronic engineers; logic and circuit design engineers; field engineers.
- Data General, Southboro, Mass., (computers): Logic designers; power supply engineers; circuit designers; memory-core engineer.
- North Electric Co., Galion, Ohio (communications): Systems test engineer; principal engineer; switching design engineer.
- Fairchild Semiconductor Products, Mountain

A Model of Engineering Employment—1972



SOURCE: ENGINEERING MANPOWER COMMISSION

Engineering Unemployment as a Function of Education



SOURCE: ENGINEERING MANPOWER COMMISSION

View, Calif.: Digital and linear circuit designers; process engineer; product engineer (all 12 to 20 k).

■ Motorola Semiconductor Div., Phoenix, Ariz.: Product engineers; process engineers: R&D staff members (all 12 to 20 k).

■ Teradyne, Boston, Mass. (test measurement): Field-service engineers; test engineers; applications engineers; circuit designer; hardware-oriented EEs; software development engineers.

■ Jet Propulsion Laboratory, Pasadena, Calif.: 10 openings for EE, ME, math or physics (12.6 to 16.3 k).

■ Stanford Research Institute, Menlo Park, Calif.: Senior systems engineers; senior research engineers.

■ Computer Identics Corp., Westwood, Mass. (systems): Project engineers, logic design and minicomputer interface (10 to 12 k).

■ Trump/Ross Industrial Controls, North Billerica, Mass. (systems): Senior electromechanical engineer (14 to 18 k).

■ Corning, Corning, N.Y. (consumer): Electrical process engineer; control engineer.

■ Du Pont, Wilmington, Del. (consumer): Engineers of all technologies.

■ RCA, New York, N.Y. (consumer): Telephone engineers (up to 15 k); satellite engineers (up to 18 k); solid-state engineers (up to 20 k); circuit-design engineers (up to 20 k); industrial engineers (up to 14 k); test equipment engineers (up to 18 k).

■ Burr-Brown, Tucson, Ariz. (components): Hybrid lab manager (16 k); applications engineer (16 k).

■ Electro Scientific Industries, Portland, Ore. (components): Product manager (13 to 18 k); programmer; EE.

■ Ballantine Laboratories, Boonton, N.J. (instruments): Circuit design engineer (10.5 to 15 k); product engineering section manager (13.6 to 17 k).

■ Hewlett-Packard, Loveland, Colo. (instruments): BSEE or MSEE, R&D (10.5 to 13.2 k); BSEE, R&D circuit-design production; BSME, R&D; process engineer.

■ Delco Electronics, Kokomo, Ind. (instruments): Semiconductor process engineer; integrated-circuit product engineer.

▪ Ground Data Corp., Fort Lauderdale, Fla. (instruments): EE (14.5 k); junior engineer (12 k); design/draftsman (13 k).

▪ North American Rockwell, Anaheim, Calif. (aerospace): Electronic engineers; electro-optical engineers; infrared systems engineers; digital design engineers; microwave engineers; communications systems; electronic countermeasure engineers; thick and thin-film circuit engineers; radar circuit design and radar systems engineers; laser field; microminicomputer memory engineers (15 to 30 k).

Recruitment up—enrollment down

With so many jobs available, why does it seem that engineering jobs are scarce?

John D. Alden, a manpower expert with the Engineer's Joint Council, a nonprofit federation of national engineering societies, offers this explanation: There are enough jobs for all engineers but they are not distributed evenly in the country. The result is pockets of unemployment in some areas and scarcities of engineers in others.

The hard core of engineering unemployment today, Alden says, has been created by layoffs in the recent recession and shifts in national spending priorities that have created serious regional supply-demand imbalances in certain specialized fields and in some localities. In addition the following have contributed: the advancing ages of some engineers, technological obsolescence, the lack of mobility of many engineers who lost their jobs and a lack of formal educational credentials. Few engineering graduates of 1971 and 1972 have been unable to find suitable jobs, Alden says.

The Newark College of Engineering in New Jersey reports, for instance, that of the students who registered for placement services last year, 72.5% found suitable employment by June 30.

"We had good job openings in the summer for the rest of the graduates," says Richard Albers, the college's director of placement, "but we've discovered that a small, but consistent, group of students is not sure of their future and choose to 'look around' instead of actively seeking work."

Electronics jobs were reportedly hardest to find, but the referral list has increased.

Albers says that company recruiting reservations are up over last year, with a notable increase in the number of electronics concerns seeking employees. He also notes that while senior engineering students are no longer receiving three, four and even five job offers, as was often the case prior to the recent recession, the number of openings is expected to be higher than in the last couple of years.

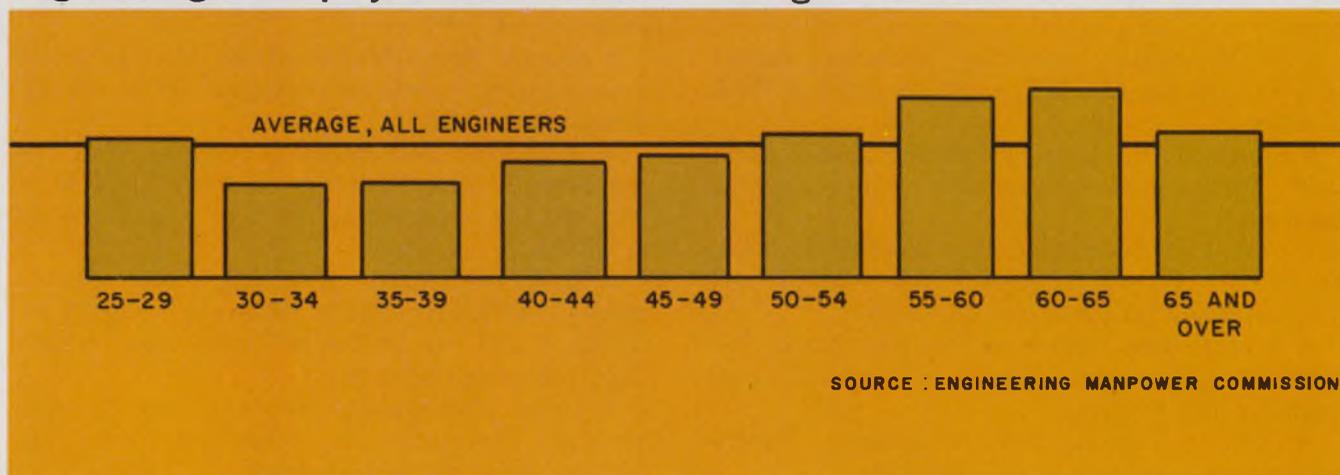
"Those companies with two openings last year," Albers says, "may well have five openings this year."

Enrollment for graduate engineering at the Newark College is up 4% over last year's total, but student interests are shifting. There's a higher percentage in environmental work and the computer sciences than before. However, in the undergraduate school, enrollment is up only fractionally. But that's better than the drop of the national average.

According to the Engineer's Joint Council, this year's national freshman engineering class is 13.6% smaller than last year's 58,566 students. Only 43,000 bachelor's degrees in engineering were awarded in 1972, and with normal attrition, fewer than 29,000 engineers will be graduated in 1976—a total far short of the 48,000 that the Presidential Manpower Commission has predicted will be the yearly need through the end of the decade.

The U.S. Labor Dept.'s Bureau of Labor Statistics agrees that engineering opportunities for the college graduate are growing, and that in-

Engineering Unemployment as a Function of Age



cludes career shifts and advancement to managerial spots.

According to the bureau, the long-run outlook in aerospace is favorable, but the 1500 annual openings it predicts over the next seven years may fall short of the number of engineers who are seeking employment in that field. Helping to pick up the slack, the bureau says, will be about 12,200 openings annually for electrical engineers in the rest of the industry.

Why there are openings

Note, too, that engineering graduates are eligible for such related jobs as industrial designers, programmers, systems analysts, technical writers and urban planners. Others use their engineering background to enter the professions of patent law, medicine, business administration, science and college teaching.

Helping to spur growth in engineering employment is the demand for electrical equipment to automate and mechanize production processes, especially for such items as computers and numerical controls for machine tools. Demand for electrical and electronic consumer goods is up, too.

And even though the Government has cut back on its massive effort in aerospace, the Defense Dept. budget for fiscal 1973 is shaping up as comparable to the one in 1972. There's still a great deal of funding for such projects as the Trident submarine, the B-1 bomber, the F-14 and F-15 aircraft, the space shuttle and the usual R&D for weaponry.

The job situation is also brightened by a recent College Placement Council report that starting engineering salaries in 1972 increased for the first time in years by nearly 2% over those of the previous year. The average starting salary for an electrical engineer is \$888 a month. Engi-

Average starting salaries, 1972 graduates

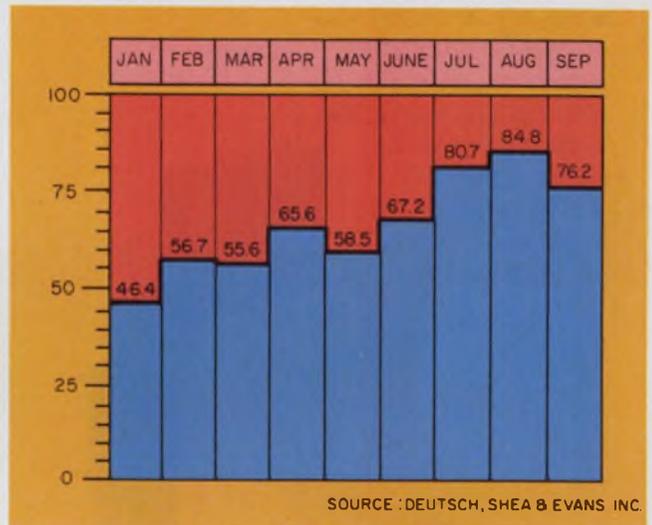
Degree level	% Change from 1971	Dollars per month
Associate Degree in Technology (ECPD Schools)	+1.6	\$ 647
Bachelor's Degree in Technology	+1.9	\$ 825
Bachelor's Degree in Engineering	+1.7	\$ 892
Master's Degree in Engineering	+1.4	\$1024
Doctor's Degree in Engineering	+4.2	\$1396

Source: Engineering Manpower Commission

neers topped practically all other occupations in starting salaries reported by the council.

What about engineering jobs this year and beyond? A quick look at engineer demand figures of recent years shows that 1961 was a more or less normal year of demand. Deutsch, Shea & Evans, Inc., a technical manpower agency, uses it as a median of 100 in an employment index that it keeps. Its engineering-scientist demand index

Engineers Demand Index—1972



The big picture to 1980, as painted by the U.S.

The following assumptions are made by the Bureau of Labor Statistics in arriving at its job projections to 1980:

The international climate will improve. The United States will no longer be fighting a war, but guarded relations between the major powers will permit few major reductions in armaments.

The strength of armed forces will drop to about the same level that prevailed in the pre-Vietnam escalation period.

The institutional framework of the American economy will not change radically.

Economic, social, technological and scientific trends—including values placed on work, education, income, and leisure—will continue.

Fiscal and monetary policies will achieve a satisfactory balance between unemployment and relative price stability without reducing long-term economic growth.

All levels of government will join to meet a wide variety of domestic requirements, but Congress will channel more funds to state and local government.

There will be fewer births in the country than there have been in the recent past.

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INFORMATION RETRIEVAL NUMBER 32

is based on a study covering over 40 publications in 20 major markets and technical journals.

The demand for any particular kind of manpower is made of three major components—replacement, transfer and growth. The demand for engineers and scientists in the U.S. reached a peak in the second and third quarters of 1966 that may never be equaled, according to Deutsch, Shea & Evans. After swooping to a precarious perch of 219 in May, 1966, the demand for engineers over the next half dozen years dived to a low of 37.4 in January, 1971. For 18 months—from mid-1970 to the end of 1971—the demand figure hovered around 40 to 45.

Now Deutsch reports an increasing demand for engineering talent in 1972. The average of 65.7 for the first nine months of 1972 is some 25 points higher than the 1971 average of 41. A year ago the demand figure was stagnating at 46.4—less than half the annual demand figure of 108.5 for 1969, the last year before the recent recession. According to Deutsch, the demand figure started to rise in earnest six months ago, and by last September it had risen 30 points since the start of 1972.

The scenario for jobs to 1980

Technical recruiting, then, is definitely up. More companies are hiring more engineers. According to Deutsch, technical employers are placing a smaller total of recruitment ads than, say, a year ago, but they're buying more space, indicating perhaps a multiple listing of available jobs.

As for demand for technical employees beyond 1973, there are two views really, and they both hinge on what the Government does or doesn't do. A spokesman for one company covered in the ELECTRONIC DESIGN survey thought that the future depended largely on the ability and willingness of the Government to stimulate R&D work. He said that most electronics companies could not support new development work out of earnings, given the present tax and investment climate. To put it another way, fewer and fewer private investors are willing to subordinate present earning to future possibilities. He concluded that in the absence of greater incentives for private R&D, the implications for the electronics engineer could be ominous.

In some areas companies are starting to plan products that will not be dependent on Government R&D and Government contracts. Such companies, planning to compete in both the domestic and international marketplace, should be in a position to offer employment to engineers without the hidden guarantee of a layoff every three to seven years. ■■

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SUPER CONTESTS
FOR**

(1) Electronic Design READERS

(2) ADVERTISERS & THEIR ADVERTISING AGENCIES

Electronic Design's

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WOULD YOU LIKE A CAREFREE WEEK FOR TWO IN THE BLUE CARIBBEAN?

Relax or lend a hand, swim, scuba dive, or just put your feet on the rail. Visit exotic tropical islands and foreign ports. It's the vacation for thinking people with a spirit of adventure. Sail in air conditioned comfort on big, safe windjammers. Choice of Bahamas, Virgin Islands, Windward or Leeward islands cruises. Pick your own departure dates. It's a trip you'll always remember. AND it's only part of the big first prize offered this year.

PLUS: \$1,000 IN CASH!

Everyone can use some extra money—especially on a cruise. Use it for babysitters, tropical clothes, shop the free ports, bank it or spend it. It goes along as an extra bonus to the lucky first prize winner who picks the Top Ten ads in the January 4 issue.



LAST YEAR'S TOP PRIZE WINNERS TELL HOW TO DO IT



Ronald S. Newbower
*Bio Engineering Division
Harvard Anesthesia Center
Massachusetts General Hospital*

Dr. Newbower looked through the contest issue with particular attention to general interest advertisements. He assumed that those ads with appeal to a large fraction of readers would place in the Top Ten. He also tended to choose ads for products that were (a) new (and of general interest), or (b) had their logos emphasized. The result: Dr. Newbower sailed off with first prize. He and his wife enjoyed their windjammer cruise; sent *Electronic Design* an enthusiastic note from the Caribbean island of Saint Lucia.



William R. Austin
*Senior Engineer
Singer, Simulated Products Division
Binghamton, New York*

Mr. Austin selected 37 ads which he considered potential winners. Then he made a chart, assigning points to each ad for esthetic appeal, copy approach, usefulness, etc. — six rating categories in all. The final results were then modified using a purely subjective approach. His system must be a good one. Two or three hours of work paid off with second prize.



Arthur L. Moorcroft
*E.E.
Naval Underwater Systems Center
New London, Connecticut*

Mr. Moorcroft first selected the 15 to 20 ads that he considered exceptional. Then culled them to pick the Top Ten. He leaned heavily toward new advertisements, new products, or new features in making his choices. The system worked well enough to make him one of the three big reader winners in last year's contest.

Electronic 1973 SUPER TOP

TRY YOUR LUCK — ENTER THE CONTEST —

AND: FREE JET TRANSPORTATION

This really makes the 1st prize complete. Think about it! The cruise . . . the \$1,000 in cash, AND free round-trip tickets for two on



regularly scheduled jets to the cruise's point of departure. It all adds up to the vacation of a lifetime. AND, you can be the lucky winner!

AND: YOU CAN WIN VALUES UP TO \$4,500—OR MORE— FOR YOUR COMPANY

Another big feature of the Top Ten Contest is the free advertising you can win for your company. Here's what your company can win if it has an ad in the January 4 issue:

A FREE RERUN . . . for each of the ads that are voted in the Top Ten by *Electronic Design's* readers.

A FREE RERUN . . . if one of your company's engineers wins any one of the first 3 prizes — whether or not your ad placed in the top ten.

A FREE RERUN . . . if one of your company's advertising or marketing people, or your advertising agency, wins any of the first 3 prizes.

Suppose you are one of the first three prize winners. If your company has a full page, 2-color ad in the January 4 issue, your company will receive a free rerun worth \$2,165. But suppose it is a 4-color spread. You've just racked up space worth \$4,500 for your top brass.

Be sure to alert your advertising or marketing manager to these possibilities. Urge him to schedule your company's ad in the January 4 issue . . . It's an opportunity no company can afford to miss.

PLUS 99 OTHER VALUABLE PRIZES

There are two separate Top Ten Contests, one for *Electronic Design's* engineer-readers, and one for advertisers and their advertising agencies.

PRIZES (Reader Contest)

- 1st Prize: Windjammer cruise for two.
Jet transportation for two.
\$1,000 cash.
Free ad rerun.
- 2nd Prize: Portable color TV.
Free ad rerun.
- 3rd, 4th & 5th Prizes: Bulova timepieces.
Free ad rerun (3rd Prize only).
- 6th thru 100th Prizes: Technical books.
(Title to be announced.)

PRIZES (Advertiser Contest)

- 1st Prize: Windjammer cruise for two.
Jet transportation for two.
\$1,000 cash.
Free ad rerun.
- 2nd Prize: Portable color TV.
Free ad rerun.
- 3rd Prize: Bulova timepiece.
Free ad rerun.

NO STRINGS, NO GIMMICKS ... HERE'S ALL YOU HAVE TO DO TO ENTER

- (1) Read the January 4th issue of *Electronic Design* with extra care.
- (2) Select the ten advertisements that you think will be best remembered by your 78,300 fellow engineer readers.
- (3) Identify the advertisements by company name and *Information Retrieval Number* (Reader Service Number) on the entry blanks bound in the issue. Mail before midnight February 15.

THIS IS THE CONTEST ISSUE LOOK FOR RULES ON PAGE 178

Entry blanks are bound inside the front and back covers of this issue.

Design

TEN CONTEST

COMPLETE INSTRUCTIONS ON PAGE 178

Get perfect linearity in CRTs when using resonant-recovery circuits with large screens and large deflection angles. A straightforward circuit provides the correction.

With rapidly rising demand for precision graphic and alphanumeric CRT displays, the linearity of CRT deflection amplifiers becomes more important. While for small deflection currents class-A deflection amplifiers are quite adequate, their low efficiency precludes their use with the larger CRTs; so-called resonant-recovery deflection circuits must be used. A problem here is that the inherent waveform of most resonant-recovery circuits does not meet even modest CRT linearity requirements. The solution is to correct the waveform.

This can be done with a relatively straightforward circuit that achieves high resolution and linearity. The resonant recovery and the correction circuit will put out the S-shaped deflection current needed to produce linear spot deflection.

Why S-shaped current is needed

Magnetic deflection of a CRT beam inevitably produces some degree of geometric distortion, or so-called "pincushion distortion," especially if the CRT has a flat face. For example, the pin-cushion error at the edge of a flat-faced CRT with

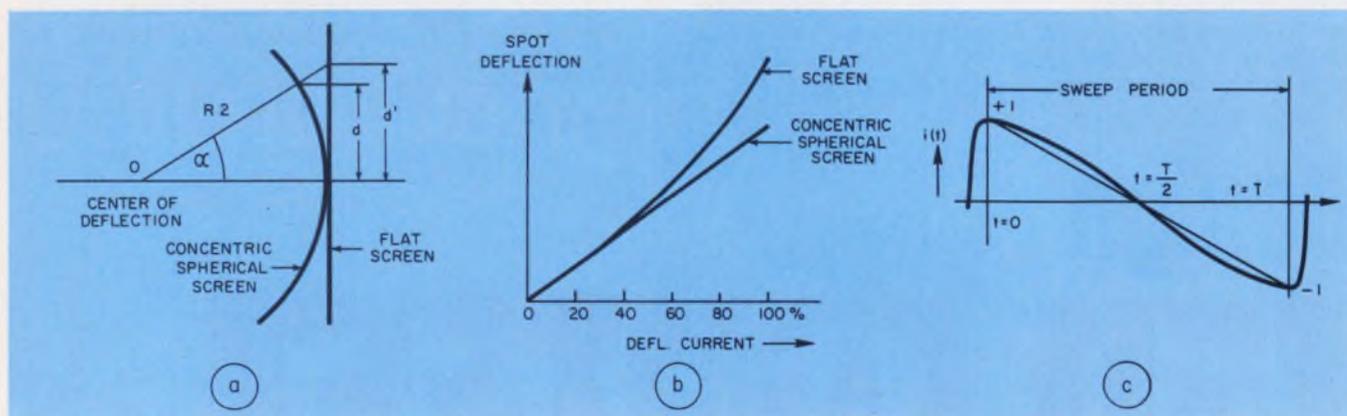
a $\pm 35^\circ$ deflection angle is $\pm 18\%$ at full deflection.

Figure 1a indicates why a linear deflection current produces nonlinear spot deflections for any CRT that has other than a spherical face. Figure 1b shows that the deflection current must be nonlinear to produce linear spot deflection. And Fig. 1c depicts the deflection-current waveform—an elongated S-shape that produces a linear spot deflection.

In general, perfect linearity correction at all CRT screen locations requires a cross connection between the horizontal and vertical deflection amplifiers so that a small portion of the corrected vertical deflection signal is added to the horizontal input and vice versa. This approach, however, is both costly and complex. A more practical solution is to use electrical means to provide accurate on-axis correction in the horizontal and vertical directions, and to use external magnets to correct for off-axis distortion.

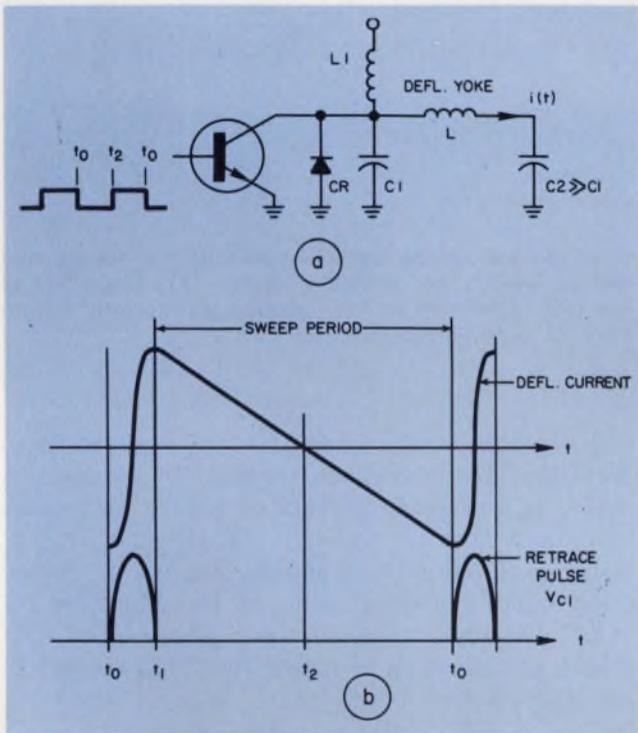
In TV displays the vertical deflection is relatively slow and requires relatively low currents. In this case a class-A amplifier can be used. The horizontal deflection, however, requires high speed at high currents, and it is here that the resonant-recovery system can be used to best advantage. In the following analysis, it is assumed that the purpose of correcting the linear resonant-recovery waveform is to provide an on-

Alfred E. Popodi, Fellow Engineer, Westinghouse Electric Corp., Baltimore, Md. 21203.

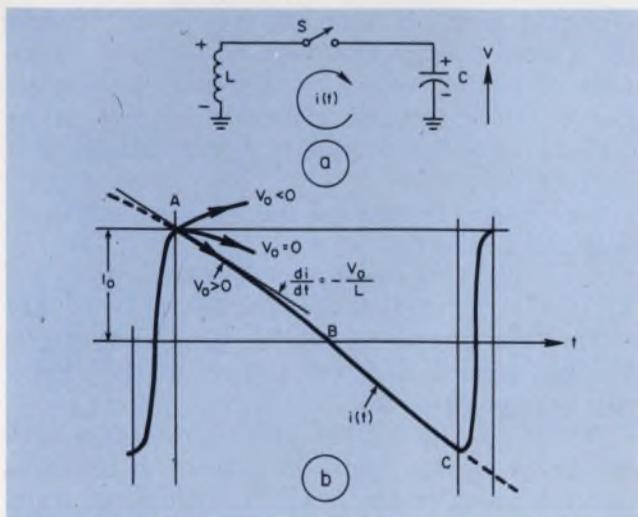


1. Large linearity errors caused by radius changes, occur in CRTs that have any screen other than a sphere (a). The nonlinearity in the spot deflection is illustrated

in b. The ideal S-shaped deflection current waveform needed to produce linear spot deflection in a CRT is demonstrated in c.



2. The basic resonant-recovery sweep circuit is simple and functional (a), but the waveform that it produces is linear (b) and doesn't correct scanning errors.



3. Operation of the resonant-recovery circuit becomes clear when we analyze its lossless equivalent circuit (a). The latter circuit produces a waveform that is slightly S-shaped (b) to produce linear deflection.

axis, S-shaped current waveform:

For a flat-faced, magnetically deflected CRT, the linearity correction factor, k , is defined by¹

$$k = i_c/i_u = 1/\sqrt{1 + p^2 \tan^2 \alpha}, \quad (1)$$

where i_c is corrected deflection current, i_u is uncorrected deflection current, α is maximum deflection angle at the tube edge,

and p is relative input amplitude varying between zero and one.

Thus the expression for a time-varying deflection current that is linearity corrected and that varies between $-I$ and $+I$ during the sweep is

$$i(t) = \frac{I_0 [-(2t - T)/T]}{\sqrt{1 + [(2t - T)/T]^2 \tan^2 \alpha}}, \quad (2)$$

where T is sweep time

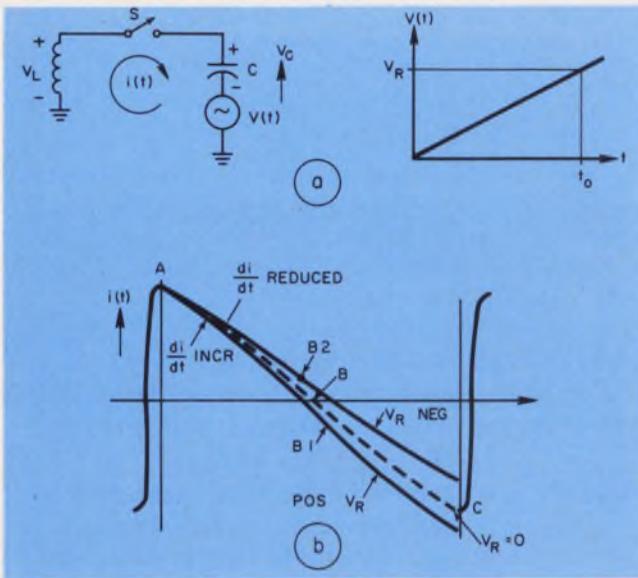
and I_0 is the uncorrected deflection current at time $t = 0$.

The curve shown in Fig. 1c is a plot of Eq. 2, and it represents the ideal, on-axis waveform of the deflection current corrected for pincushion distortion. The sweep generator must ultimately deliver current that has this waveform to the deflection yoke, if a linear spot deflection is desired.

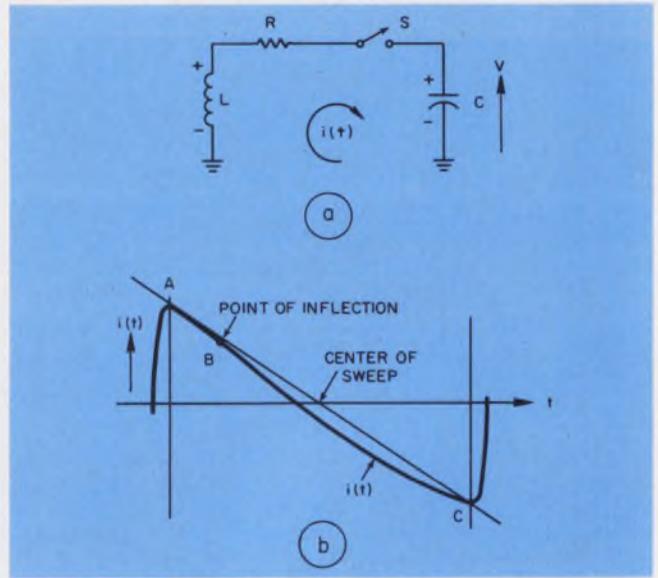
Analyze the resonant-recovery circuit

The basic resonant-recovery circuit (Fig. 2a) consists of the deflection yoke, L ; a retrace capacitor, C_1 ; an S-curve correction capacitor, C_2 , and a damper diode, CR . Inductor L_1 is a charging choke with high inductance. The switching signal at the base of the transistor controls the timing.

Figure 2b depicts the characteristic current and voltage waveforms of this circuit. During the second half of the sweep period the transistor conducts and C_2 acts as the energy source. When at time T_0 (end of sweep) the deflection current reaches its negative peak, the transistor is cut off and the retrace period begins. The stored energy in the yoke inductance builds up a sinusoidal voltage of several hundred volts across the small retrace capacitor, C_1 . When this voltage reaches zero (at time t_1), diode CR begins to conduct and the actual sweep begins. The energy



4. One way to correct the resonant-recovery waveform is to add a time-varying voltage source in series with the deflection coil (a) and thus gain control over the current-waveform slope (b).



5. A realistic resonant-recovery circuit has losses that can be lumped into a single resistor (a). The effect of this loss component on the idealized waveform is to produce an asymmetrical S curve.

source is again the deflection yoke. At time t_2 current polarity reverses, the diode stops conducting, and the transistor starts conducting until the end of the sweep. Capacitor C_2 is now the energy source until time t_0 .

When, at time t_1 , the sweep begins, the equivalent lossless circuit of the sweep generator is as shown in Fig. 3a. The deflection current is a maximum at time t_1 (Fig. 2a) with the inductor acting as the energy source. Capacitor C has a positive charge that opposes the current flow (hence the open switch in Fig. 3a). The lower terminal of choke L_1 can be assumed to be at ground potential during the sweep, since either the diode or the transistor conduct during this time.

When switch S closes, the voltage across capacitor C is $V = V_0$, and the current is $i(t) = I_0$. Since the inductor L is the energy source, we have

$$V = -L(di/dt)$$

and

$$i = C(dV/dt).$$

Thus, if we omit the well-known intermediate equations, we can write the final expression for the current:

$$i(t) = I_0 \cos \omega t - [(V_0/Z) \sin \omega t], \quad (3)$$

where $Z = \sqrt{L/C}$.

The plot of Eq. 3 indicates (Fig. 3b) that the current varies sinusoidally from A to C with the initial slope $(di/dt) = (V_0/L)$. The slope is independent of the capacitor size. Zero-crossing point B lies exactly at the midpoint between A and C . If V_0 is more positive, the current will decay faster. If $V_0 = 0$, the initial tangent, di/dt ,

is horizontal. If V_0 is negative, the current rises. Note that the waveform in Fig. 3b between A and C is the center portion of a very large sine wave and that its linearity is directly proportional to the amplitude of this sine wave. On the other hand, a smaller value of the capacitor results in a more pronounced S shape. For this reason capacitor C_2 is called the S-curve correction capacitor.

Add a correction voltage to resonant recovery

As was briefly mentioned earlier, the current waveform of a resonant-recovery circuit must be corrected with an external voltage to produce the desired S-shape curve. To understand the effects of adding such a voltage source, consider Fig. 4a. Here a voltage source in series with the capacitor produces a linearly rising voltage, $v(t) = V_R(t/t_0)$.

Once again, if we omit the intermediate equations, we can write

$$i(t) = I_0 \cos \omega t - [(V_0/Z) \sin \omega t] - [(CV_R/t_0)(1 - \cos \omega t)]. \quad (4)$$

The first two terms are the same as in Eq. 3. The last term describes the effect of the correction voltage (Fig. 4b).

If V_R is positive—that is, the correction voltage increases with time—the slope di/dt increases faster between points A and B , enhancing the S shape during the first half of the sweep. The point of inflection, B_1 , lies now below the zero-current line, and the waveform is no longer symmetrical. The second part of the sweep be-

comes more linear.

If V_R is negative, the first part of the sweep is more linearized and the second part more S-shaped. The point of inflection, B_0 , is now shifted above the zero-current line.

This illustrates how the current waveform can be shaped by a time-varying signal that is injected into the resonant-recovery circuit. The actual waveform of the correction signal depends on the desired current waveform. In general, a positive correction signal causes a faster increase of di/dt of the deflection current. A constant dc level will have no effect on the current waveform.

We can now turn our attention to a more realistic case—a resonant-recovery circuit with normal circuit losses. If we assume that all the circuit losses can be represented by the resistor, R , the equivalent circuit is as shown in Fig. 5a. When the switch is closed, the voltage across the capacitor is $V = -L(di/dt) - iR$, so that

$$i(t) = -LC(d^2i/dt^2) - RC(di/dt). \quad (5)$$

Solving this equation, we get

$$i(t) = (e^{-t/2T_L}) \{ I_0 \sin[\omega \sqrt{1 - (T/4T_L)t + \psi}] - (V_0/Z) \sin \omega \sqrt{1 - (T/4T_L)t} / \sqrt{1 - (T/4T_L)} \}, \quad (6)$$

where $T = RC$

$$T_L = L/R$$

$$\omega^2 LC = 1$$

$$Z = \sqrt{L/C}$$

$$\sin \psi = \sqrt{1 - \xi^2}$$

$$\xi = R/2Z, \text{ and } \xi > 90^\circ.$$

The term in the figure brackets represents a symmetrical, sinusoidal currents waveform, just as in the lossless case. When this term is multiplied by an exponentially decaying function, the result is an asymmetrical waveform with the point of inflection to the left of center (Fig. 5b). The first portion of the sweep looks like a straight line, with the slope gradually decaying towards the end of the sweep. In terms of display linearity, this means that the CRT spot velocity in the first half of the sweep is too high compared with the second half. This results in expansion of the video image in the first half and compression in the second half. And this is the inherent waveform of a resonant-recovery circuit. It deviates considerably from the ideal, symmetrical S-shaped curve.

Choosing the right correction method

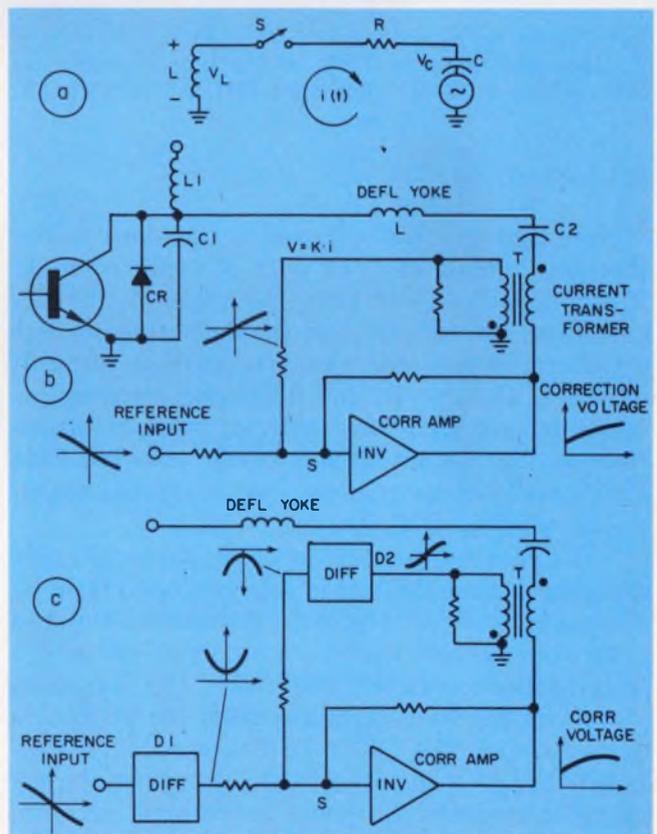
Whenever a resonant-recovery sweep generator is used, the purpose of the waveform correction is not only to correct for the unsymmetrical waveform of the sweep generator but also to provide the S-shaped current needed for the pincushion correction. The most accurate method is to compare the differentiated deflection current with the differentiated reference input that has

been shaped to correct for the pincushion error.

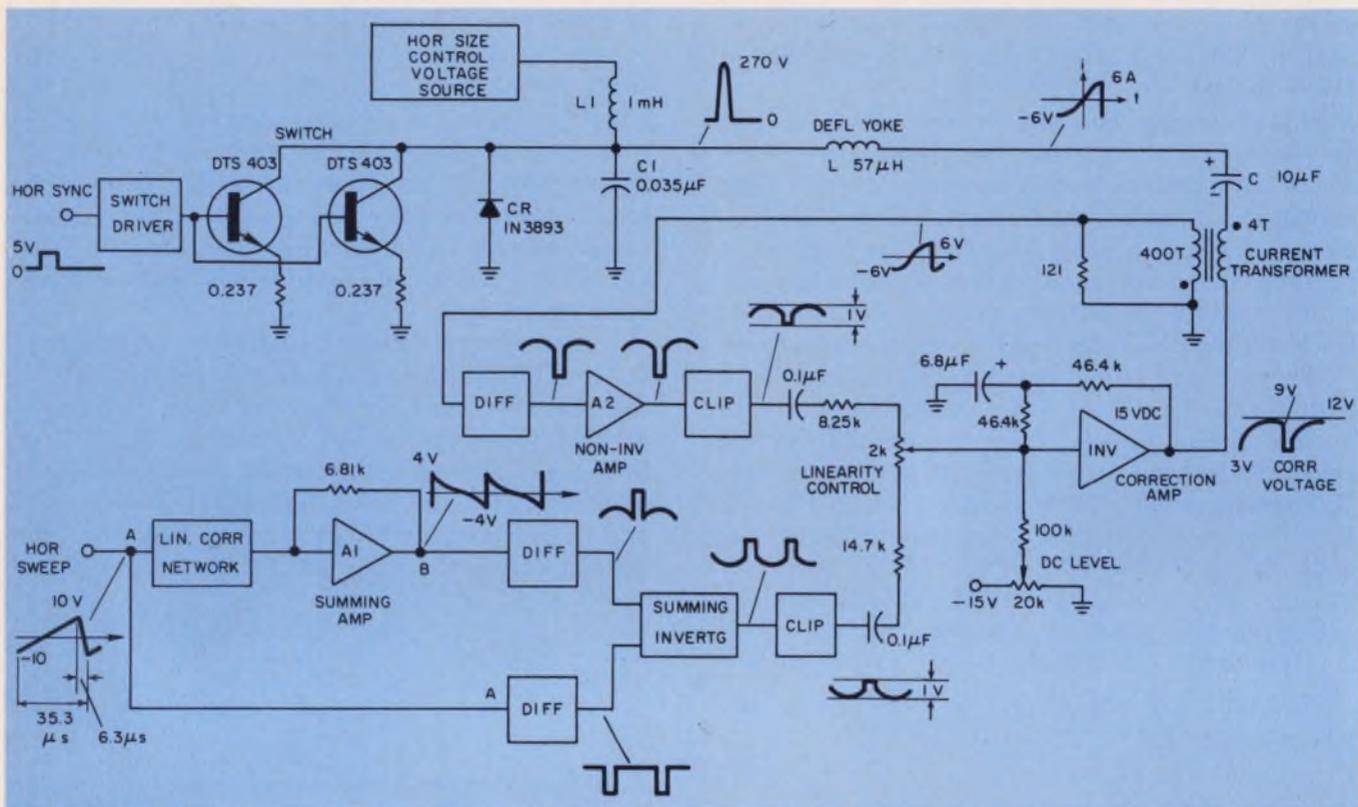
Depending on the linearity requirements, one of these four methods can be used:

1. *No correction amplifier.* For tubes with small deflection angles or in cases where the linearity needs are not very demanding ($\pm 5\%$), a correction signal can be generated externally and added to the sweep circuit with a transformer. Another way is to use a properly biased saturable reactor in series with the deflection yoke (or with a transformer) to partly restore waveform symmetry.

2. *Open-loop correction amplifier.* In this case better CRT linearities can be obtained than with the previous method. The correction voltage is derived from the deflection current itself. For instance, a current transformer can be connected in series with the yoke. Its output is amplified and is added to the sweep circuit (Fig. 6a). The voltage across the yoke is given (with use of the



6. The desired degree of linearity determines the type of correction method to be used. A not too stringent system can use a scheme in which a correction voltage is derived from deflection current and then injected in series with the deflection coil (a). Adding a first-order feedback (b) improves the degree of linearity obtainable. The most accurate correction scheme uses a second-order feedback system in conjunction with a correction amplifier (c). Waveforms are shown for key points.



7. Linearities of up to 0.2% of the tube diameter are obtained for a 22-inch, flat-faced CRT with this circuit.

Without correction circuits, total linearity error (pin-cushion plus the sweep-circuit distortion) was 54%.

notation of Fig. 6a) by

$$v_L = i(R + k) + v_c \quad (7)$$

Note that the final solution is the same as for the lossy circuit (Eq. 6) with R modified by k . If k is negative (positive-going voltage), the circuit losses are reduced and the deflection current waveform approaches the symmetrical, sinusoidal case. If $k = R$, the deflection current becomes a pure sine wave with its point of inflection in the middle of the sweep interval. This sine wave is in many cases a good approximation to the required S shape.

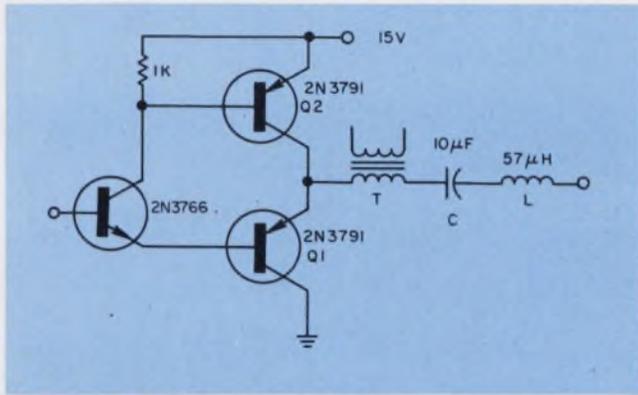
3. *First-order feedback with amplifier.* In this case the actual deflection current waveform is compared with a reference waveform, and the difference between the two is amplified and added to the deflection circuit (Fig. 6b). The reference waveform can be determined from the geometric properties of the CRT. In the case of a flat-faced CRT, for instance, Eq. 2 describes the required waveform. It should be pointed out here that this is not a true feedback system, since the correction signal is not required for the sweep generation; it only modifies its waveform.

Referring to Fig. 6b, we see that the reference signal and the feedback signal must have opposite phase at the summing point, S, of the inverting op amp. The reference input is larger than the feedback input. Since the correction sig-

nal must be positive-going, the reference input must be negative-going.

The drawback of this circuit is the time lag between the correction signal and coil current, because the latter is proportional to the integral of the applied voltage. Now assume that, because of a parameter change in the deflection circuit, a sudden slope change occurs. With plain current feedback, the correction voltage changes its slope. A slope change of the correction voltage, however, cannot correct for a slope change in current. Only a step function can do this, and it is not provided by this circuit. Thus this approach is useful for many applications but not for large deflection angles.

4. *Second-order feedback with amplifier.* In a second-order feedback system (Fig. 6c), a sample of the differentiated deflection current is compared with the differentiated reference input, and the difference between the two is amplified, inverted and applied to the sweep circuit. This provides time-lag-free correction with better accuracy than the other methods, and it is satisfactory for large displays with stringent linearity requirements (better than $\pm 0.5\%$). The differentiators can be simple RC networks followed by a single-stage amplifier. The output of the current transformer is a voltage that is proportional to the deflection current. This voltage is then differ-



8. The correction-amplifier output stage must be able to handle full deflection current. This is achieved by letting each output transistor conduct during alternate halves of the sweep cycle.

entiated in D_2 . Both the transformer and D_2 can be replaced by a differentiating voltage transformer.

A complete and more detailed functional horizontal deflection circuit is shown in Fig. 7. The reference input at point A is a linear ramp. The linearity correction network is a function generator consisting of biased diodes and resistive voltage dividers. Its output current is converted into voltage by an op amp, A_1 . After the signals are differentiated, they are added, clipped and applied to the comparator via the linearity control potentiometer.

The correction amplifier has low gain, and its output stage must be capable of absorbing the full deflection current (Fig. 8). During the first half of the sweep, when the yoke is the energy source, transistor Q_1 conducts; during the second half, transistor Q_2 conducts.

The circuit of Fig. 7 was used with a 22-inch, flat-faced CRT having $\pm 35^\circ$ deflection angle. The horizontal-deflection yoke inductance is 57 μ h, and the deflection current is ± 6 A. Non-linearity due to the CRT geometry was originally 18% at the edge of the tube. The total sweep nonlinearity due to this pincushion error and sweep-waveform distortion was 54%. After application of the correction circuit in Fig. 7, the maximum on-axis deviation from linearity became less than 0.2% of the CRT diameter. The linearity was measured by comparing a digitally generated video grating pattern with an accurate overlay. The output swing of the correction amplifier is only 6 V peak to peak. ■■

Acknowledgement

The author wishes to thank J.W. Ensor for his contribution.

References:

1. Popodi, A. E., "Linearity Correction for Magnetically Deflected Cathode Ray Tubes," *EDN*, January, 1964.

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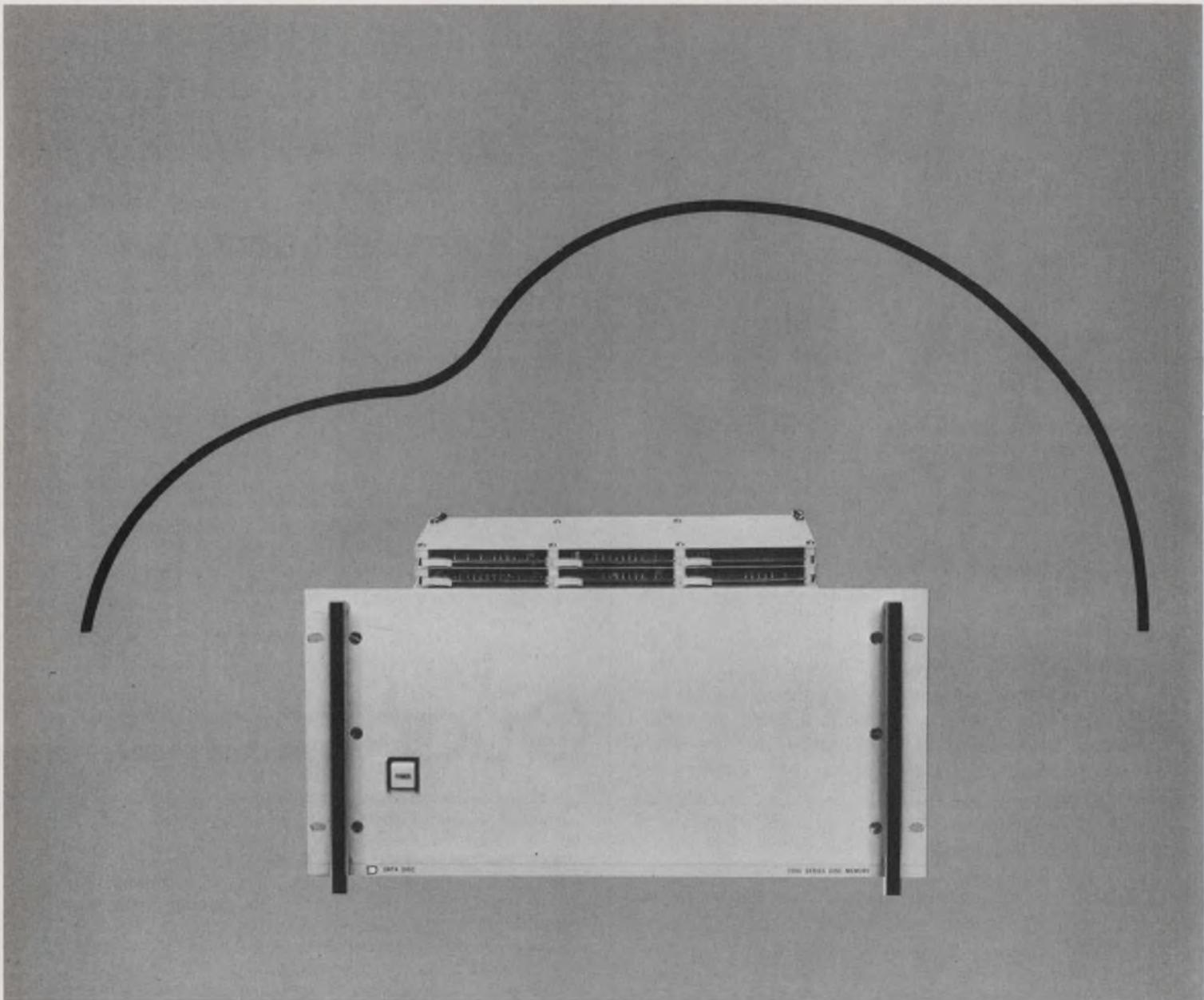
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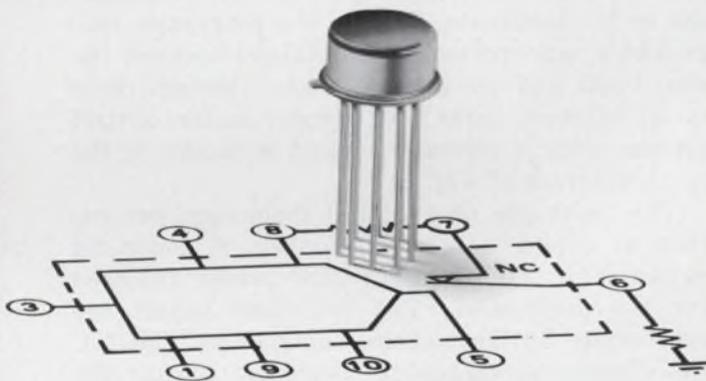
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The celerator (from "acceleration" and "deceleration") causes the stepper motor to accelerate or to decelerate. This is the maximum rate at which synchronism is maintained between the step input and the motion output (though there is an inherent delay). A stepper-motor control system using a celerator circuit is shown in the block diagram of Fig. 1.

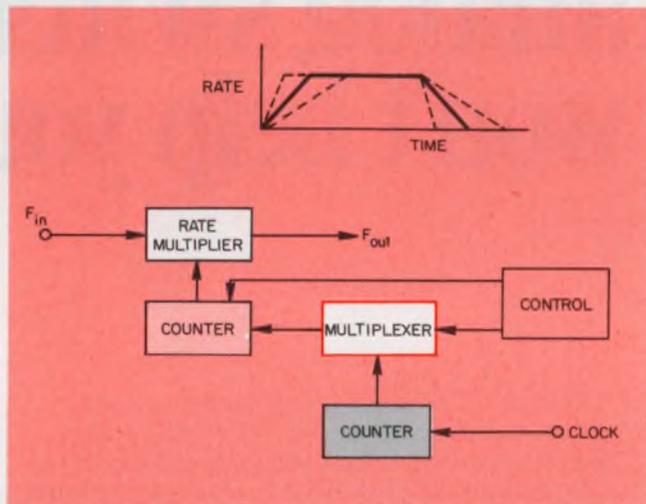
The technique uses digital frequency generation to obtain a specific number of command pulses with the frequency-time profile required for the application. The command pulses are synthesized by the machine-control unit (MCU). An alternative technique would be to use the arithmetic approach of digital differential analysis (DDA). Frequency generation is preferred because it makes the internal data representation identical to the external representation. It is also remarkably easy to do.

Use a digital rate multiplier

All machine-control units that generate frequencies digitally use a common logic element—the digital rate multiplier—at the heart of the design. The rate multiplier generates an output frequency that is the product of the input frequency and a digital fraction determined by the binary-coded multiplier. The rate multiplier converts a binary or BCD data-input word to a frequency representation.

Subfrequencies of the input frequency, generated by a counter, are selectively combined as controlled by the multiplier. The net effect is a periodic removal of pulses from the input stream. The period of any cycle is thus not constant. But the average of all cycle periods is.

If a more uniform output is desired (to approach spectral purity in the frequency domain), the output can be initially generated at a higher



1. Linear celerator allows stepper motor to be accelerated or decelerated, thus providing higher average speeds without loss of accuracy. A rate multiplier is programmed to produce the required linear ramps in the output pulse rate.

frequency than desired and then divided down. The divider, or counter, then acts as a low-pass filter. The amount of remaining jitter, or side bands, is expressed by:

$$\frac{F_{IN}}{2N}, \quad (1)$$

where F_{IN} is the maximum stepping frequency, and N is the cycle set of the counter. Suitable digital rate multipliers are available as ICs. The one used in the circuit of Fig. 2 is the SN7497 binary rate multiplier.

How the celerator circuit works

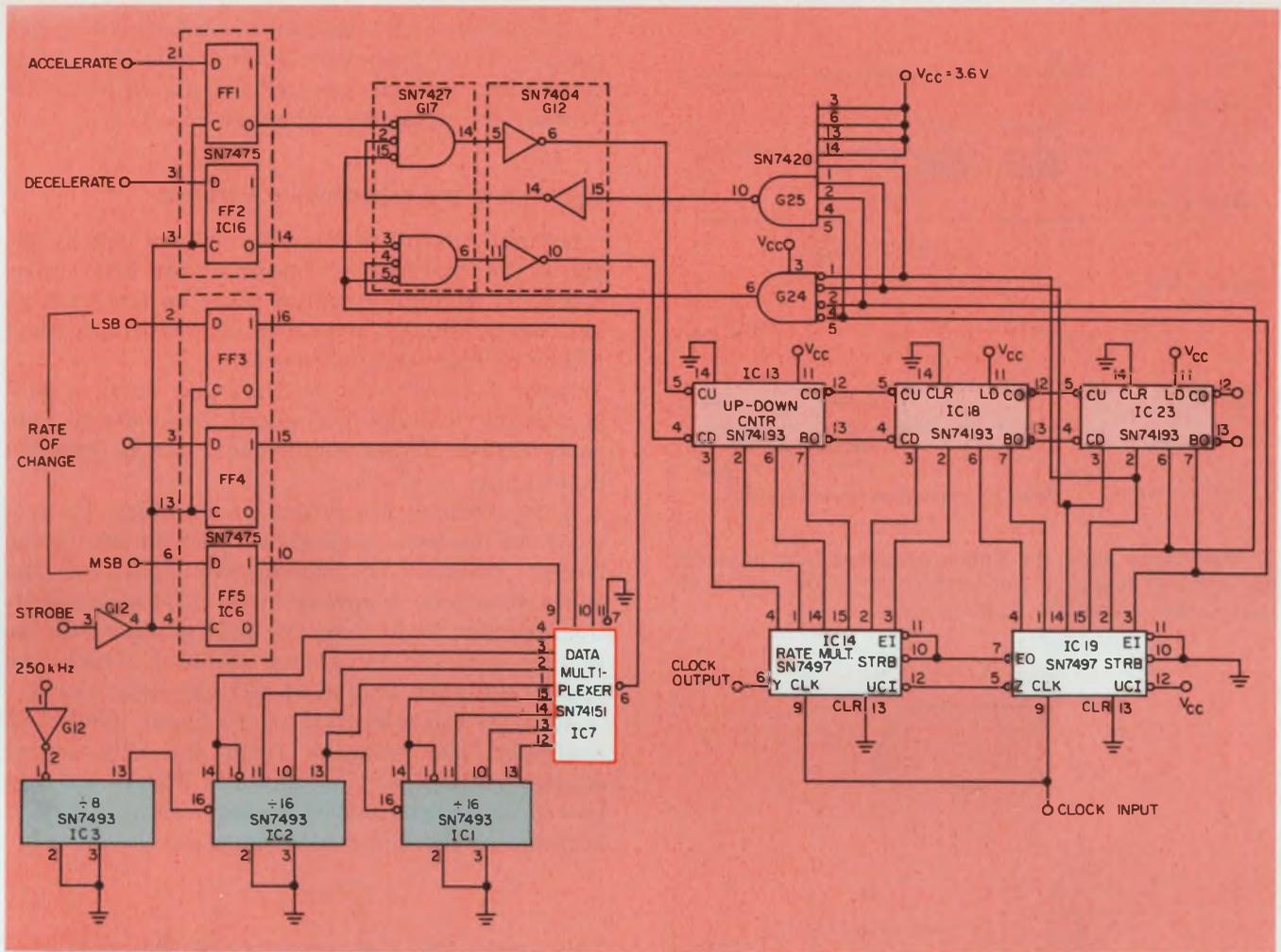
The celerator circuit is basically a rate multiplier controlled by an up-down counter. Additional rate multipliers in the celerator may be cascaded to provide greater output resolution.

If the binary inputs are labeled A through F, for the least to the most significant, the relationship of the output to input rates is given by the expression

$$F_{OUT} = F_{IN} \frac{2^6F + 2^4E + 2^3D + 2^2C + 2B + A}{64} \quad (2)$$

To illustrate how frequency generation is typically used, consider a situation where a digital

T. A. Seim, Computers and Control Section, Battelle, Pacific Northwest Laboratories, Battelle Blvd., Richland, Wash. 99352.



2. The complete linear celerator circuit uses two cascaded rate multipliers, IC₁₄, and IC₁₉, which are driven

by up-down counters IC₁₃, IC₁₈, and IC₂₃. Counters IC₁, IC₂ and IC₃ generate the different clock rates.

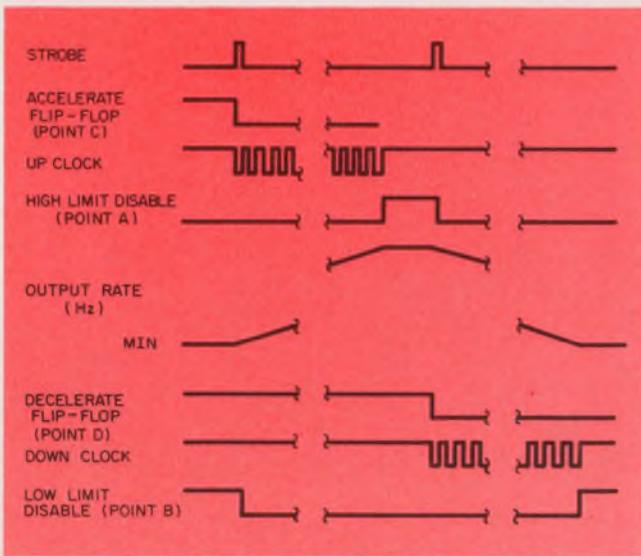
command causes a linear rise or fall in the output frequency at a rate that is also under digital command. Fig. 1 shows the logic needed to perform this function. Rate F_{IN} is the maximum stepping frequency, and F_{OUT} is the rate applied to the stepping motor translator.

Up-down counters IC₁₃, IC₁₈ and IC₂₃ (Fig. 2) generate the linear ramp required to produce constant celeration, and this is then multiplied by the input rate. A second series of counters, IC₁, IC₂ and IC₃, together with multiplexer IC₇, generates the different clock rates needed to select the ramp slope. Gates G₁₂, G₁₇, G₂₄ and G₂₅, driven by the counters, inhibit the up-down clock, IC₇, preventing the counter from overflowing or underflowing. Figure 3 shows the timing of the pulse trains and their effect on the output rate.

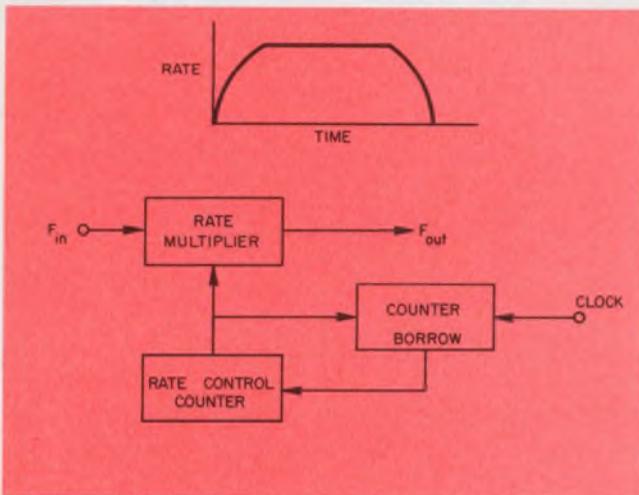
The multiplexer, IC₇, selects the counting rate, which is directed through gating to either the up or down clock input of three cascaded SN74193 binary counters. Gating decodes the four most significant bits to halt celeration at the required limits, so that the ratio between the high and low limits is about 16 to 1. Note that the counting rate does not go to zero, but it

can be made to do so by further decoding. The lower limit can be set to any value, including zero, provided that it is algebraically less than the high limit. In the circuit of Fig. 2 the lower limit is not zero because only the four most significant bits are decoded. Thus the binary counters stop at binary 000011111111, which is convenient for an application in which the stepper motor continues moving regardless of the state of the celerator. If the application requires the stepper motor to stop when the celerator so dictates, the limit should be made zero.

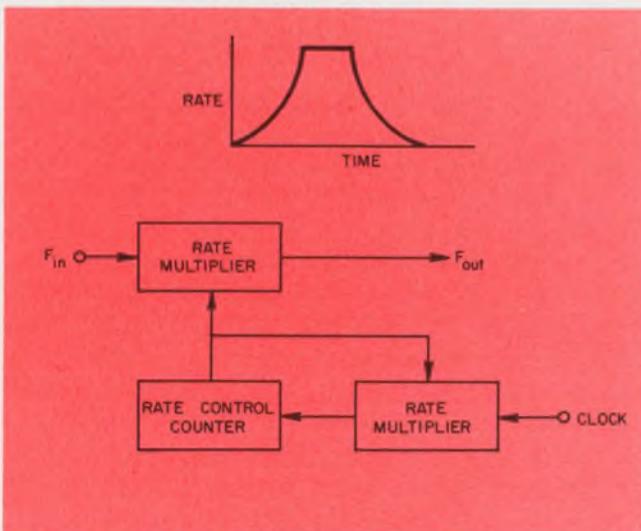
Celeration is initiated by strobing the control register, which is composed of five D flip-flops, FF₁ to FF₅. To select celeration direction, set either the accelerate (FF₁) or decelerate (FF₂) flip-flop. Also program rate-of-change, using the three other flip-flops (FF₃ to FF₅). With 250-kHz as the clock rate, the time allowed for full-scale celeration varies from 0.25 to 33 s. Celeration occurs until either a limit is reached or the control flip-flops are reset. This allows the celeration to be halted at any point within its range (at any clock rate between maximum and minimum). This feature can conceivably be used in a feedback control-loop application.



3. Waveforms show the timing sequence that produces the required trapezoidal characteristic for the output bit rate. Linear ramps are thus formed.



4. Logarithmic celerator is obtained by adding feedback from the rate control counter to the clock that drives it.



5. Exponential celerator uses feedback, as in the logarithmic case, but with the clock counter replaced by a rate multiplier.

The output of the up-down counters is the frequency of the output in binary code. If decade devices are used, the counter outputs will be BCD—ready for readouts and other uses.

Logarithmic and exponential celerators

Optimal control of stepping motors usually requires that the rate-of-change of the drive-pulse frequency at high stepping rates be less than at low ones. This is because of the diminished torque at high slewing speeds.

Large inertial loads, on the other hand, should be brought to their final speed gradually to prevent ringing. Either requirement can be handled by a digital celerator.

A logarithmic celeration curve (Fig. 4) provides the optimal characteristic for all except the largest motors. The deceleration part of the curve should be a mirror image of the acceleration portion. The characteristic is thus similar to that achieved by analog circuits, which are usually designed around an RC rise-delay curve.

To make the celeration curve linear instead of nonlinear, use feedback from the rate-control counter to the clock that drives it. Figure 4 shows how this is accomplished. A logarithmic solution is found to the differential equation:

$$\frac{dR}{dt} = \frac{k}{R} \quad (3)$$

This means that the derivative of the count-rate function R is proportional to its inverse. So the clock rate applied to the counter must be multiplied by a factor inversely proportional to the counter's contents. This is easily handled by a presettable counter whose set inputs are the outputs of the rate-control counter.

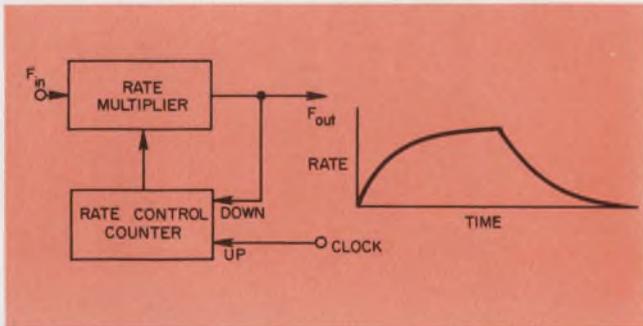
A problem arises if you want the rate-control counter to go to zero where the logarithm is undefined. A simple solution is to add a small constant factor to the value of the rate-control counter, such as by connecting the least significant bit of the clock counter to a logic HIGH.

The same basic concept can be used for an exponential celerator with a characteristic (Fig. 5) suitable for driving large inertial loads without overshoot. For this circuit, we substitute a rate multiplier for the clock counter used in the logarithmic version. The mathematical relationship for this version of the circuit is the differential equation

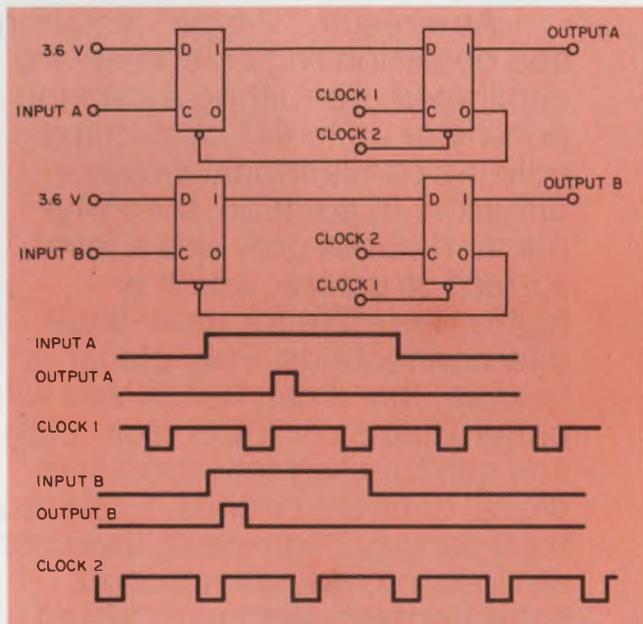
$$\frac{dR}{dt} = kR \quad (4)$$

In this case, the derivative of the clock rate function is directly proportional to the function itself. The solution is an exponential function.

For applications requiring asymptotically converging rates, Fig. 6 shows how the output rate itself is used as feedback to the control counter.



6. For an asymptotic celerator, the output rate itself is used as feedback to the rate-control counter.



7. To insure anticoincident clocks, provided they are asynchronous, this flip-flop circuit works when the phases have noncoincident edges and a frequency at least twice that of the inputs.

The final stepping rate, including zero, is determined by the input clock. The input clock does not control the rate of change, as in the previous cases.

If the stepping rate of Fig. 6 is altered from a steady-state value, the higher rate predominates. This causes the counter to change the output rate so it converges on the control rate. But as the difference in rates becomes smaller, the net change of the counter slows.

The time constant of the asymptote depends on the maximum clock rates and the number of stages in the counter. The output rate can be converted to any constant multiple of the control rate by the insertion of rate multipliers in either or both feedback legs.

One constraint not obvious in the circuit of Fig. 6 is that the two clocks must be anticoincident—they cannot overlap. If the clocks are asynchronous, the circuit of Fig. 7 takes care of the problem. The only precautions are that the phases have noncoincident edges and be at least twice the frequency of the inputs. ■■

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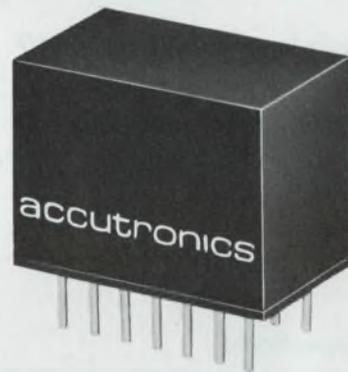
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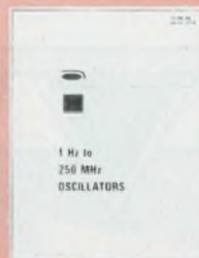
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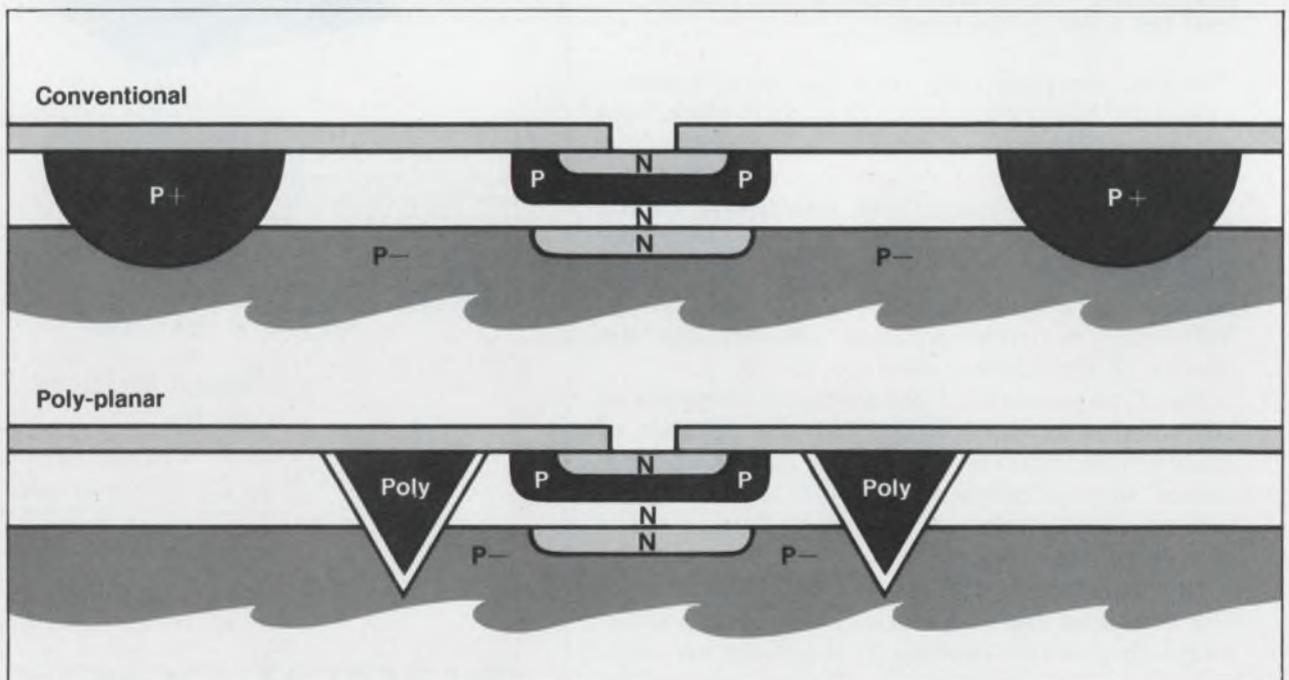
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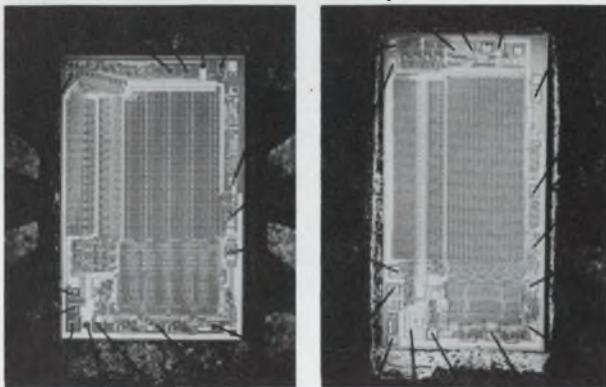
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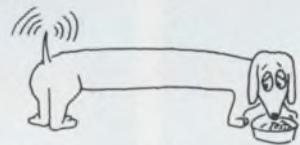
Here is a master checklist that can save you time and money. Check your designs against it. Better yet, refer to the list during each phase of your design. One corrected item—an item that might have gone unnoticed without the checklist—can sometimes save a project from disaster.

No list like this can be all-inclusive. But it does present often-overlooked points of broad interest. You may wish to add your own entries based on your specialty.

James C. Breese, 1405 Amherst St., W. Los Angeles, Calif. 90025.

Amplifiers

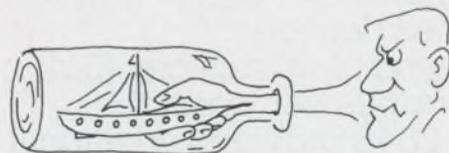
1. Are inputs and outputs physically and electrically separated as much as possible?



2. Are power sources decoupled close to high-gain, wide-bandwidth devices? Does each device have its own decoupling circuit?

General

1. Have U.L. requirements been considered, and do the designs conform?
2. Have all of these factors been considered in the design:
 - Power consumption?
 - Weight?
 - Size?
 - Cost?
 - MTBF, MTTR?
3. Are there anticipated requirements or options that may be satisfied by minor changes easily incorporated now? For instance, components that might be needed later can be put on the PC art work now. The parts can be left out and mounted when needed.
4. Is the module easily tested? Has test equipment been designed? Have test personnel examined the design?
5. Are parts selected from the company's standard parts list where possible? Are parts available from second sources? Are the parts in this design in common use in other products of the company?
6. Has producibility been considered? Has production seen the design?
7. Has the module been "operator proofed" against the following:
 - Simultaneous and contradictory commands?
 - Damage from insertion or removal with power applied?
 - Backward power connections?Use your imagination here. The operator certainly will.
8. Are assemblies easily removed and replaced?
9. Does failure of a module cause "domino" failures elsewhere?
10. Can interlocks be defeated accidentally?



Capacitors

1. Are surge currents within the rated limits of the capacitor? Can associated components safely handle the surge?
2. Are capacitors operated at less than half rated voltage for maximum MTBF?
3. Are electrolytics bypassed for high fre-

quencies with a small, solid-dielectric, noninductive capacitor?

4. Are large capacitors bypassed by bleed-resistors?
5. Are capacitors operated within their temperature limits?

3. Can linear amplifiers be driven into non-linear modes and do they automatically restore to linear operation?
4. Do nonlinearities generate sidebands that remain and appear as distorted data?
5. Have the effects of offset, bias voltages and currents to op amps been considered?
6. Is the slew rate adequate for high-frequency and fast-switching performance? Is the maximum output swing available at the highest signal frequency?

Interfacing

1. Are standardized nomenclatures and pin assignments used?
2. Are decoupled power busses clearly identified and separated from the regulated but noisy power busses?
3. In the layout of the PC board have pins not assigned to standard and critical circuits been left unassigned to permit layout flexibility?
4. Can the interfacing cables be driven without degrading performance? Have sufficient steps been taken to protect against noise pickup on the cables?



Cost

1. Is the circuit free of special parts (custom transformers, specially machined sinks, special specification op amps, selected resistors, etc.)?
2. Is the variety of parts at a minimum?
3. Is the module easy to assemble and test? Is it easy to repair?
4. Are low-cost parts used where possible?
5. Are ICs, LEDs, ROMs, and other parts with declining prices being used where possible?
6. Have expensive parts been submitted for competitive bidding?
7. Is hand-wiring eliminated where possible? Does the design use PC boards as male connectors, group I/O connections for flat cable wiring and wave soldering?

(Plastic power transistors can be mounted so that they overhang the PC card, thereby allowing transistors to be fastened to heat sinks with single screws.)

5. Are all loads compatible with their sources?
6. Will failure or the disconnecting of one or more power sources cause damage? If yes, what steps have been taken to prevent damage?
7. Is any special sequence required for removing or applying power?
8. Are interlocks provided to insure against improper power sequencing?
9. Can an open or shorted lead produce a harmful action? Is the circuit behavior fail-safe when an interface lead is opened or shorted?
10. Is circuit initialization—an automatic or manual reset or a warm-up time delay—required?
11. Have time race conditions been designed out of the circuits?

Semiconductors

1. Have both voltage and current thyristor rate effects been considered in designing with thyristors?
2. Are transistors operated at less than 80% V_{ce} and V_{be} ? Are power limitations observed? Are capacitive and inductive loads properly treated?
3. Is the thermal impedance to the heat sink and to the ambient air low enough?
4. Are matched pairs used where needed? Are they adequately coupled thermally?
5. Are spare circuits identified on the schematic?
6. Have multitransistor arrays been considered to reduce cost or save PC space?
7. Are FET leads properly connected? (The gate is often not in the middle.)

Inductors and transformers

1. Can the unit support the highest possible input voltage at the lowest possible frequency without saturation?
2. Is dc current carried by the unit? If yes, is the core large enough to withstand saturation and consequent reduction in inductance?
3. Is protection provided against voltage spikes from sudden field collapse? Does this protection prevent proper high-speed operation?
4. Have the effects of magnetic and thermal orientation of the unit within the assembly and in the next higher assemblies been considered?
5. Can worst-case core and copper losses be dissipated?
6. Are taps provided for required impedances or drive voltages?

Resistors

1. For reliability, are all resistors operated at less than 75% of their rated power? Are they operated within their voltage rating?
2. Are noninductive resistors used in high-frequency and high-speed circuits?
3. Have the needs for precision, stability, linearity and noise-free performance of resistors been evaluated?

Noise

1. Are critical component positions and sensitive cable routings securely fixed in place?
2. Is rf decoupling used in each module?
3. For low-level critical signals, are power driver and receiver circuits used with twisted, shielded-pair lines?
4. Are high-current, noise producing leads, such as those to motors and solenoids, isolated and shielded from signal circuitry?



5. Are the signals used for edge-triggering "clean" and free of multiple transitions?
6. Are filters used for both reducing line noise pickup and preventing noise broadcasting?
7. Are all wires large enough to carry worst-case loads?
8. For critical signals, has the common-mode-rejection method of reducing response to noise been considered and properly implemented? Are low-level leads as short as possible?
9. Are grounds returned to a single point? Are separate ground leads provided for low-level signals and kept separate from high-current and high-frequency ground leads?

Testing

1. Are tests points provided so they are still accessible in the final assembly?
2. Can test points be shorted to ground without circuit damage?
3. Are test points labeled and conveniently placed for any corresponding adjustments?
4. Has a test specification and procedure been prepared?

Adjustable components

1. Is the adjustment really necessary?
2. Are adjustments adequately labeled? Do clockwise adjustments produce an increase in the controlled quantity or move the operating point to the right in visual displays?
3. Is each adjustment independent of other adjustments? Are adjustments independent of power supply levels?
4. Is there sufficient range and resolution in the adjustment? Are the adjustment end stops strong enough to protect against overzealous turning?
5. Are adjustments still accessible when the module is mounted in the full assembly? Can the adjusted parameter be monitored from the module's final position?
6. Are factory-adjusted components sealed? Are they mounted so that tampering is discouraged?
7. Are variable resistors wired with the wiper connected to one end, thus preventing a completely open circuit should the wiper contact fail?

PC cards and packaging

1. Are PC cards keyed and does the keying prevent reversed insertion?
2. Are power and ground busses labeled on the art work? Are diode directions shown? Are capacitor polarities marked?
3. Are pin-number labels provided for connectors, ICs and transistor sockets?
4. Are standardized pins used for power and ground? Are alternate pins left blank where possible to minimize accidental shorts while troubleshooting?
5. Are the adjustable components labeled?
6. Are sockets used for fuses and lamps?
7. Are low-level signal runs as short as possible? Are high-current conductor widths on PC boards wide enough?
8. Are hot components raised above the card, for cooling and card protection?
9. In difficult or dangerous environments, has hermetic sealing been considered for the package design?
10. Are metal-cased parts protected so they don't cause accidental shorts?
11. Is some room allowed for future growth?
12. Does the module carry its part number and name in a visible area?

Relays

1. Has the relay driver been protected against voltage spikes? Does the protection increase dropout time too much?
2. Have operate, release and bounce times been considered?
3. Is arc suppression necessary. If yes, has it been tested for effectiveness?
4. Are contacts designed for the nominal load only? In "dry" circuits, are the proper contacts used? Have solid-state relays been considered?
5. Has circuit and contact timing been studied to eliminate sneak paths and momentary bridging of contacts?
6. Has the duty-cycle of the relay coil been considered?

Temperature

1. Is sufficient cooling airflow provided? Is cooling still present with the drawers pulled out? Can airflow be impeded by operator negligence, such as stowing manuals on the cabinet top? (A good rule of thumb is: $\text{Temperature Rise } (^{\circ}\text{C}) = \frac{1.7 \times \text{Power Dissipated (Watts)}}{\text{Airflow Rate (CFM)}}$)
2. Has the performance of the cooling system been checked?



3. Are personnel protected from contact with hot parts?
4. Are heat-sensitive parts (transistors, capacitors) protected and kept away from heat sources?
5. Are PC cards and other materials that easily discolor protected from contact with hot parts?
6. Are components still properly cooled when installed in the final assembly?
7. Has power dissipation been checked under worst-case conditions? (For instance, check zener regulator circuits with the load removed.)

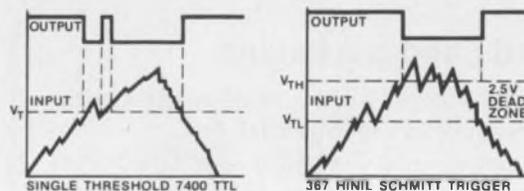
Schmitt, the name that made the trigger famous, now makes HiNIL universal.

Schmitt is Teledyne's new HiNIL 367, noise-proof line receiver. It's the new way to go for a universal input-port to logic blocks. In industrial applications, for example, most inputs are either a switch or a relay closure. They usually cause contact bounce. But the most amazing thing about the 367 is that it has a truth table that simply eliminates contact bounce by definition.

And by the way, the noise immunity of the 367 is more than enough to handle any long lines between the logic and input. It has a 5.0 volt worst-case noise immunity and an additional 2.5 volt dead-zone Schmitt Trigger margin.

Because the 367 is a Schmitt Trigger, it holds that 2.5 volt noise immunity *even* during logic transition. Slow-down

capacitors, as you all know, do not provide true noise immunity during switching. But, with the 367 in there, you can use those slow-down capacitors at the rate of 4msec/uFd *and* achieve a high guaranteed noise immunity too.



For fussy people, we put an inhibit pin on the 367 that allows information to be accepted only at times of low noise.

The new Quad Schmitt 367 is available now at \$2.98 in 100 up quantities. Order now or get in line.

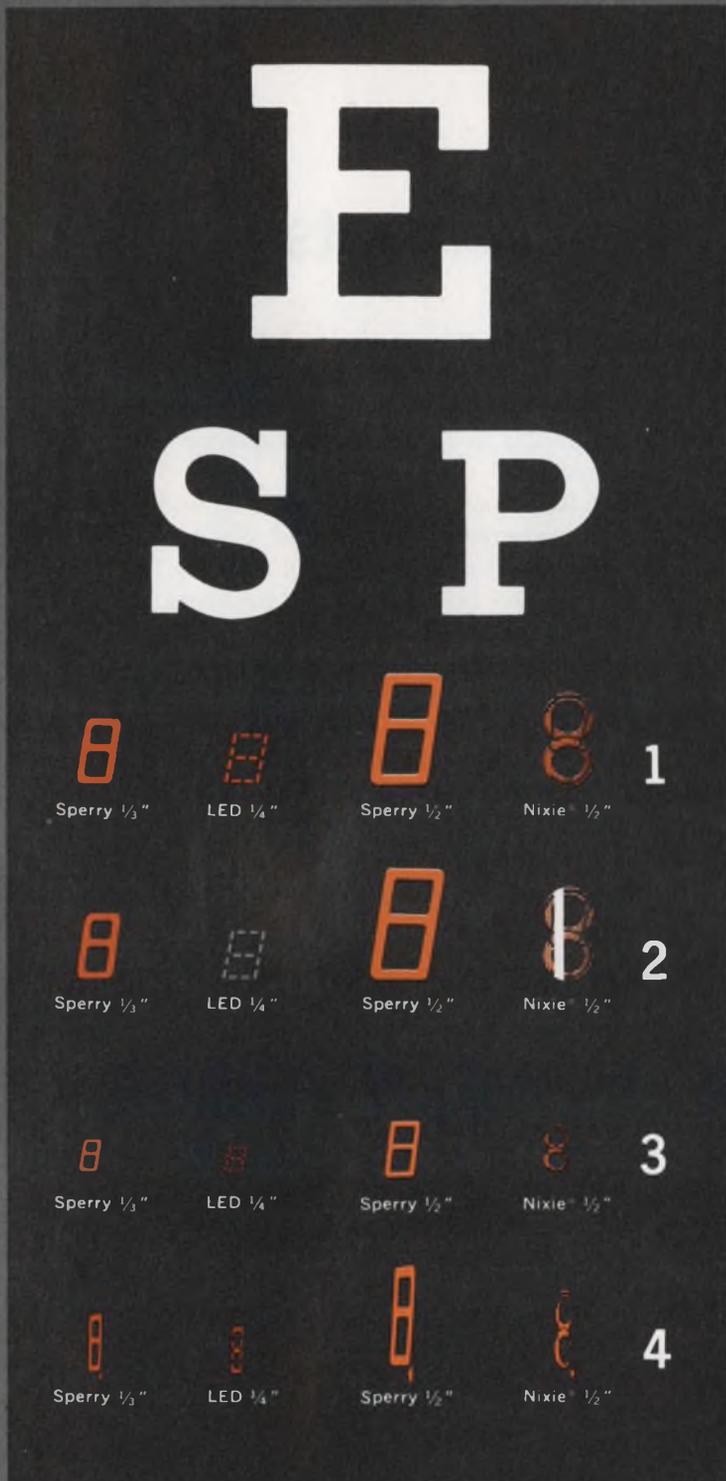
the challenger

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INFORMATION RETRIEVAL NUMBER 42

The Sperry eye test for display equipment buyers



The old saying "what you see is what you get" certainly applies to the purchase of equipment incorporating displays — panel meters, DVM's, multimeters, counters, instruments, calculators and other equipment. If you can't clearly and easily read the information being displayed then you're not getting full product value. And, you're obviously not getting equipment supplied with advanced Sperry planar displays†.

How do you tell if they're Sperry displays? Simply take the Sperry eye test.

1. Do the displays appear as uniformly bright, continuous characters with no irritating gaps or filaments and screens to reduce readability?
 YES NO
2. Do the displays remain bright and clearly legible with no glare or appreciable fading even under direct sunlight conditions?
 YES NO
3. Can you quickly, easily and accurately read the displays from 20 to 40 feet away?
 YES NO
4. When the unit is positioned within a 130° viewing angle, can you still clearly read the displayed characters?
 YES NO

If you answered YES to all four questions, you already have your eyes on equipment featuring preferred Sperry displays.

If you answered NO to any of the questions, you owe it to yourself to take a comparison look at products equipped with superior Sperry displays.

FREE BUYER'S GUIDE —

To help you make the right equipment selection, Sperry offers the handy "Buyer's Guide for Equipment featuring Electronic Displays". It's yours for the asking. Order your copy today by checking the reader service card or phone or write: Sperry Information Displays Division, P.O. Box 3579, Scottsdale, Arizona 85257, telephone (602) 947-8371.

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Sperry 1/2"

units are available for use with red filters

The above is a printed interpretation of the appearance of the more popular displays. You are encouraged to make the same comparison with actual devices.

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† Patents Pending
* NIXIE is the registered trademark of The Burroughs Corporation.

INFORMATION RETRIEVAL NUMBER 236

Integrate-and-hold circuit gives electrochemical measurements

Operational-amplifier integration techniques can provide input-signal and time ranges comparable with those obtained from electrochemical cells. A FET peak-holding circuit holds the largest voltage reached by the integrator's output. More important, the value is held for a period up to three times longer than could be expected for the integrator capacitor alone.

With switch S_1 in the Integrate position (Fig. 1), the integrated signal from A_1 is fed to the peak-holding circuit comprised of amplifier A_2 , low-leakage capacitor C_2 , diode CR_1 , and FET Q_1 .

The high input impedance of FET Q_1 and the use of a voltage-follower circuit provide isolation between the integrator and output meter, thus minimizing leakage from the integrating capacitor, C_1 .

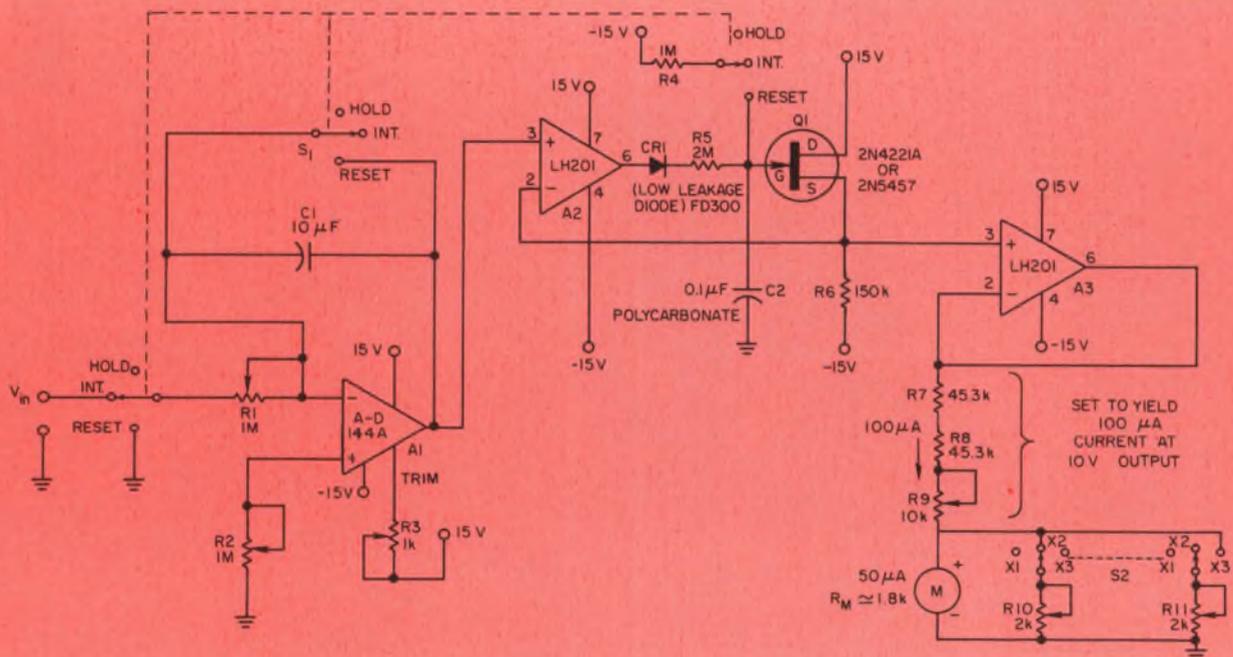
The meter reads directly in coulombs when S_2

is set in the X1 position and when the input scale factor is 1 V/A. Switch S_2 should be set to the X3 position to avoid off-scale meter readings, if the unit is to be unattended during an integration cycle.

The Reset position of S_1 clears C_1 and C_2 . When the measurement is completed, S_1 is switched to the Hold position. This disconnects the input signal from the integrator and prevents a loss of charge from capacitor C_1 .

The coulombmeter shown has a range of 0 to 128 coulombs, with the upper limit resulting when one or more internal amplifiers reach saturation. The peak-holding circuit will limit the output droop to about 0.7 coulomb/min., for an indication of 120 coulombs on the meter.

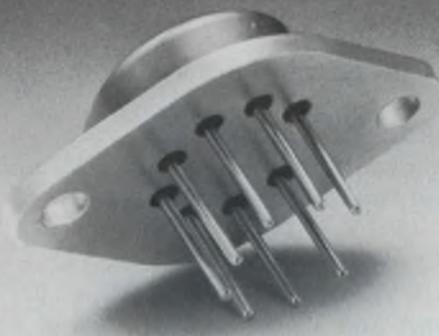
Robert G. Warsinski, Ford Motor Co., 24500 Glendale, Detroit, Mich. 48239. CIRCLE NO. 311



The peak value of the integral of the input voltage is read out directly on the microammeter, M,

which is calibrated to read in coulombs for an input scale factor of 1 V/A.

THE BEST WAY TO SWITCH HIGH POWER LOADS FOR PRECISELY TIMED INTERVALS.



□-LINE ONESHOT POWER PULSERS

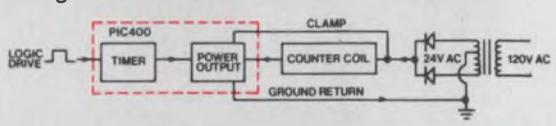
The Unirode Power Pulser is a hybrid circuit available in two series optimized for switching loads up to 500 watts (60V) for 0.5 to 50ms. Output pulse width tolerance is within 1% of the internally preset time with a temperature coefficient of $-0.04\%/^{\circ}\text{C}$ from 0°C to 125°C . It is a complete, ready-to-use thick film circuit in a compact TO-3 package.

VOLTAGE SWITCH – PIC400

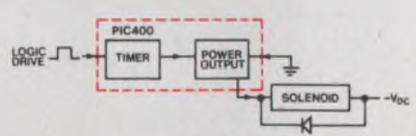
Upon actuation by an input pulse from an IC logic gate, the output of the PIC400 will switch the supply voltage across the load independent of the shape or duration of the input. No external components are necessary. The load may be placed in either the collector or emitter of the darlington output and may be driven from either a positive or negative supply. A wide variety of options are available, including 1800W switching capability (15A, 120V), extended pulse width range (from a fraction of a millisecond to several seconds), and controlled rise and fall rates. The two applications listed below illustrate the versatility of the PIC400.

TYPICAL PIC400 SERIES APPLICATIONS

1. Driving electro-mechanical counter from 24V AC.



2. Solenoid actuation from negative power supply.



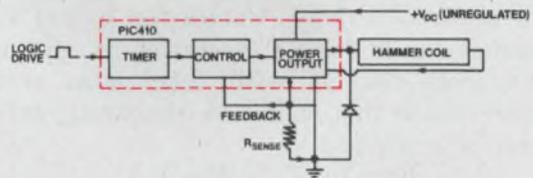
REGULATED CURRENT SWITCH – PIC410

The PIC410 is a more sophisticated version of the PIC400. The output pulse is current regulated to within 1% of an externally preset value by means of a switching regulator in the output circuitry. This insures substantially lower internal power losses and higher efficiency than could be obtained with a series

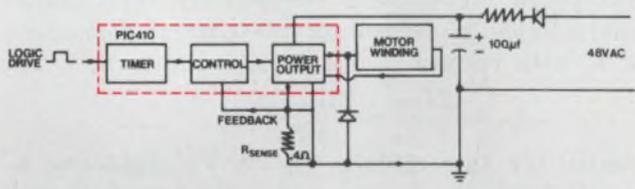
regulator. A rapid turn-off circuit insures the fastest possible current decay upon termination of the output pulse. The range of options available for the PIC410 are the same as for the PIC400. Two typical applications follow.

TYPICAL PIC410 SERIES APPLICATIONS

1. Constant current switching of high speed print-hammer from unregulated supply.



2. Driving high-speed stepper motor (with 5A constant current pulse) from 48V AC.



For more specific information call Vinnie Savoie – collect – at (617) 926-0404, or return the coupon to Unirode Corporation, 580 Pleasant St., Watertown, Mass. 02172.

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PIC400 PIC410
 Application Note Power Darlington

My application is: _____

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See EEM Section 4800 And EBG Semiconductors Section for more complete product listing



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Analog multiplication or amplitude modulation are provided by a single MOSFET

A single n-channel, dual-gate MOSFET can be made to perform analog multiplication if one of the gates is used to vary the device's transconductance and the other is used for signal input. The resulting drain-current variation can be expressed as the sum of two terms—one proportional to the signal and control voltage. Removal of the signal term by subtraction of a portion of the input signal leaves just the product term.

As shown in Fig. 1, the input signal, V_s , is fed to gate G_1 , while the control signal, V_c , goes to gate G_2 . If $V_c \gg V_s$, then the drain voltage can be expressed by

$$V_o = -(k_1 + k_2 V_c) R_1 V_s.$$

The expression in the parenthesis is the small-signal MOSFET transconductance, g_m , and R_1 is the drain-load resistor. Values for k_1 and k_2 are computed for MOSFET operation in the depletion region—that is with both gates reverse-biased. Under this condition the drain current, I_D , can be expressed by

$$I_D = I_{DSS} (1 - V_{GS}/V_p)^2.$$

I_{DSS} and V_p are the short-circuit drain current and pinch off voltage, respectively. The transconductance is defined as the partial derivative of I_D with respect to V_{GS} . It is found to be

$$g_m = \frac{2I_{DSS}}{-V_p} + \frac{2I_{DSS}V_c}{V_p^2}$$

where, for this circuit, $V_{GS} = V_c$. Equating k_1 and k_2 with the previous equation, we find that

$$k_1 = \frac{2I_{DSS}}{-V_p}$$

$$k_2 = \frac{2I_{DSS}}{V_p^2}$$

Multiplication of the terms in Eq. 1 gives the output voltages as

$$V_o = -(k_1 R_1) V_s - (k_2 R_1) V_c V_s.$$

In the circuit shown, amplifier A₁ sums V_o and V_s so as to cancel the first term and leave

$$V_{out} = -(R_f/R_{s1}) (k_2 R_1) V_c V_s,$$

provided that

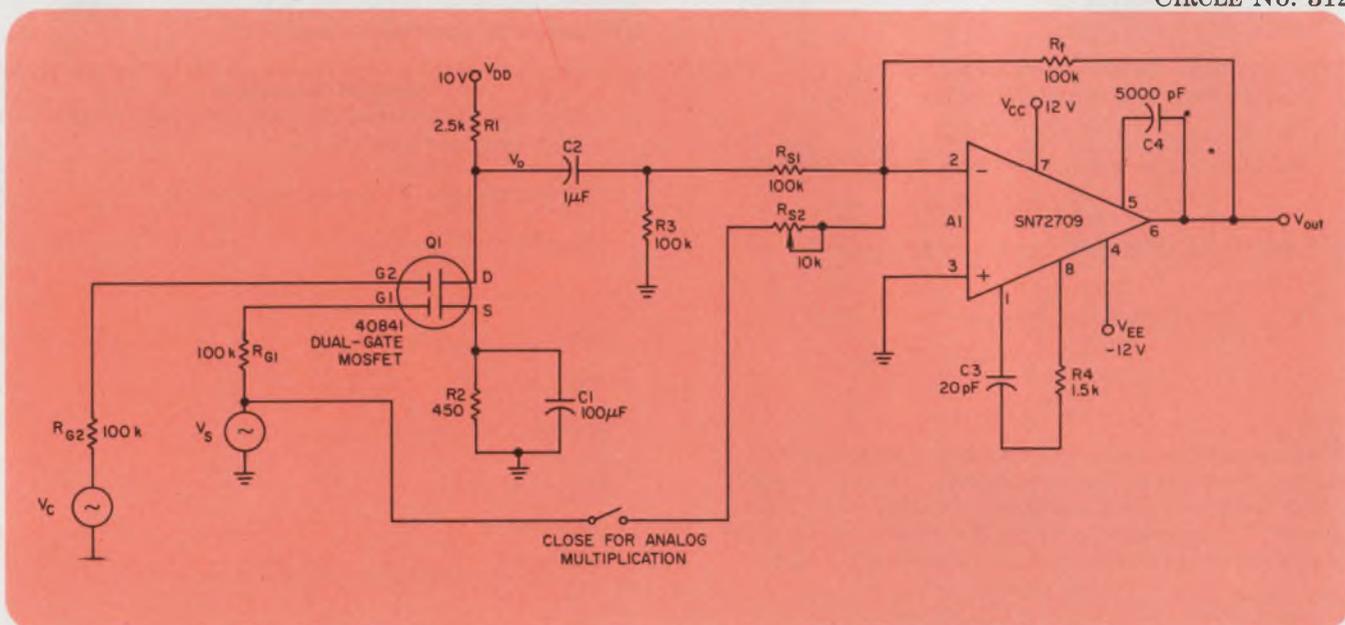
$$-(R_f/R_{s2}) V_s + (R_f/R_{s1}) (k_1 R_1) V_s = 0.$$

With $I_{DSS} = 4$ mA and $V_p = -1.5$ V, V_s and V_c are restricted to voltage swings of 0.3 and 1 V, respectively, to avoid saturation or pinch-off. For these operating conditions, $k_1 = 5.32$ mA/V and $k_2 = 3.56$ mA/V². Since $R_f = R_{s1}$, and R_{s2} is adjusted to cancel the V_s term, $V_{out} = 8.9 V_c V_s$.

In practice, the highest operating frequency is restricted to 100 kHz by the low-frequency response of the op amp. If required, amplitude modulation can be obtained by omitting R_{s2} . However, without filtering, the modulation depth is limited to 60%. Above this V_c and V_s are of the same order of magnitude, causing the transconductance to be a function of both signals with consequent generation of spurious harmonics.

Dr. W. V. Subbaro, Assistant Professor, North Dakota State University, College of Engineering and Architecture, Fargo, N.D. 58102.

CIRCLE NO. 312



The drain circuit of MOSFET Q_1 contains the product of signal voltage V_s and control voltage V_c .

The first-order term in V_s is nulled by R_{s2} , leaving only the product term at the output.

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INFORMATION RETRIEVAL NUMBER 45

Increase bandwidth of cascaded synchronous counters to 35 MHz

With the addition of a Schottky TTL flip-flop and a three-input AND gate to a Signetics 8284 synchronous counter, it's possible to cascade up to 12 such counters and achieve frequencies of up to 35 MHz. The technique (Fig. 1) overcomes the usual delay that occurs with two or more cascaded 8284s. The delay occurs primarily at the Carry-Out output of the first stage in the conventional synchronous configuration.

To increase the bandwidth, the Carry-Out (CO) output of the first counter must be anticipated. Even though a single counter may work at over 40 MHz, its CO output—used to enable the following stages—has a typical delay of 30 ns from the clock pulse. After this delay is added to the typical 15-ns setup time for Count-Enable (CE), the minimum period of the clock becomes 45 ns—which corresponds to a frequency of 22 MHz. (A frequency of 23.6 MHz has been obtained in practice with the conventional configuration.)

To anticipate the CO output of the first counter stage, the circuit uses two Schottky clamped ICs having a typical total propagation delay of 5 ns. The first Schottky circuit is a three-input AND gate, G_1 , and the second a JK flip-flop, FF_1 . The typical setup time is 3 ns.

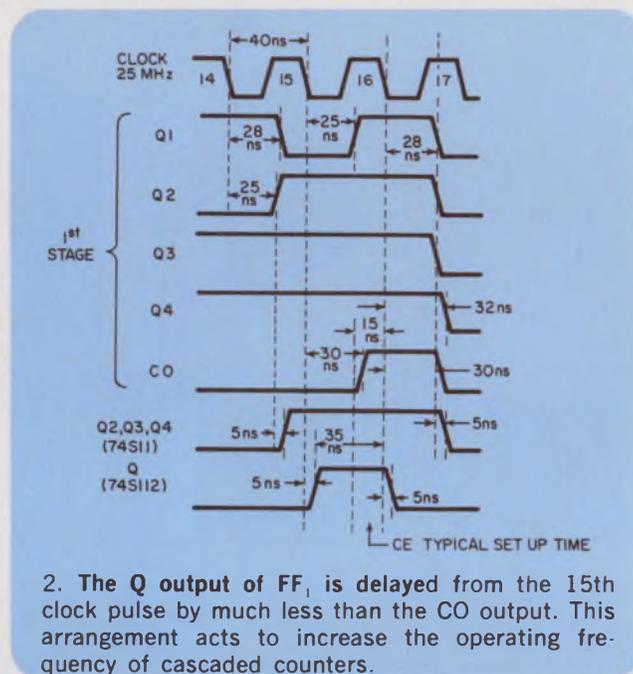
When outputs Q_2 , Q_3 and Q_4 of the first counter stage coincide, the J input of FF_1 is enabled for the 15th and 16th clock pulses. With the K input of FF_1 at V_{cc} , the Q output of the flip-flop will be a positive pulse. The leading edge of the pulse coincides with the trailing edge of the 15th clock pulse, and the pulse's trailing edge is synchronized with the trailing edge of the 16th clock pulse. The flip-flop output is then identical to the CO output of the first FF counter, but with a delay

relative to the clock pulse of 5 ns instead of 30 ns.

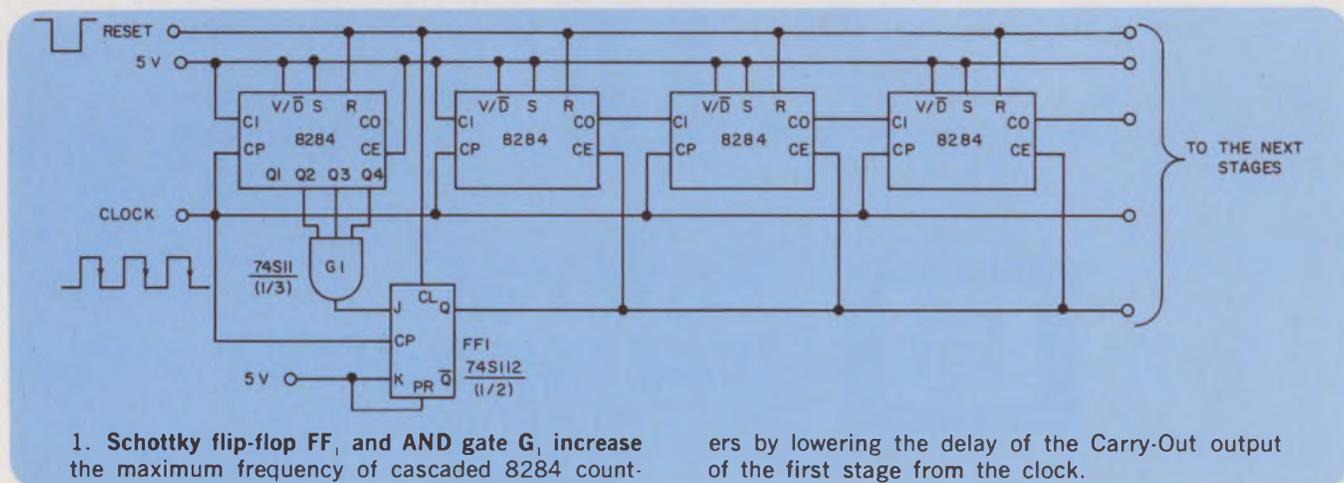
The timing diagram of Fig. 2 is for a 25-MHz clock. During the 30-ns delay of CO from the 15th clock pulse, the Q output of FF, provides a setup time of 35 ns. This is considerably longer than the typical setup time of 15 ns that is typically required. The setup time allows the circuit of Fig. 1, with the Q output of FF_1 as the CO, to achieve frequencies of up to 35.3 MHz.

Boris Bertolucci, Electronics Instrumentation Group, Stanford Linear Accelerator Center, P.O. Box 4349, Stanford, Calif. 94305.

CIRCLE No. 313



2. The Q output of FF_1 is delayed from the 15th clock pulse by much less than the CO output. This arrangement acts to increase the operating frequency of cascaded counters.



1. Schottky flip-flop FF_1 and AND gate G_1 increase the maximum frequency of cascaded 8284 count-

ers by lowering the delay of the Carry-Out output of the first stage from the clock.

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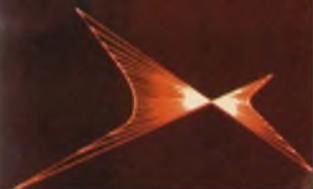
Long term moisture like 500 to 5000 hours in a humidity chamber can be even more destructive than boiling. If you put Vactec to this test, be sure to include some competitive cells for comparison.

You simply can't buy a better photocell *anywhere*, and Vactec is competitive with import prices because of automated processing, assembling, and testing. Take advantage of Vactec engineering, research, and manufacturing in the heart of America. Because Vactec has 249 different types of cells in stock, we can ship before your order reaches an overseas supplier. Included is a complete line of visible detectors: photoconductors (CdS and CdSe); photovoltaic cells (Se and Si); couplers of LED's or lamps and photoconductors called Vactrols. Vactec also has a photometer which measures from .0002 to 10,000 fc, for as little as \$300.00.



VACTEC, INC.

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Retriggerable one-shot prevents false triggering of PLL tone detector

By adding a retriggerable one-shot multivibrator and a transistor to a phase-locked-loop tone detector, you can prevent false triggering by radio noise.

The circuit of Fig. 1 discriminates between noise and the input tone by measuring the interval of time that the tone is present at the input of the detector. Since in-band frequency components of radio noise are shorter than the duration of a tone command signal, the circuit can be made insensitive to triggering by radio noise.

The 5-V logic level at the tone-detector output, point A, keeps transistor Q_1 in saturation. But when a tone is detected, point A switches to ground potential, thereby triggering one-shot MM1. The triggering of MM1 raises the one-shot output, point B, from ground to 5 V. The 5-V level at point B keeps transistor Q_1 saturated until the one-shot times out. Point B then returns

to ground potential.

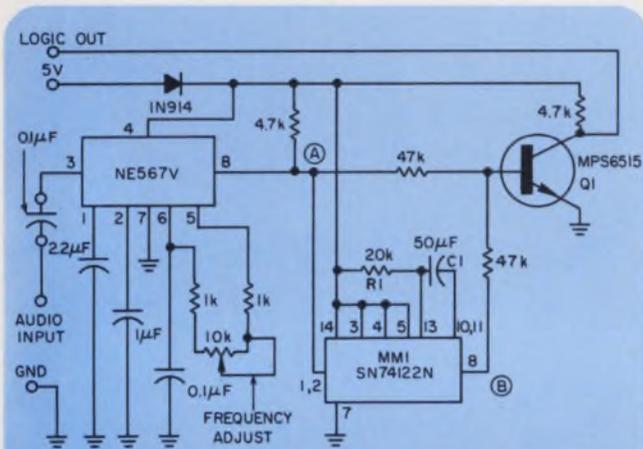
If the tone is still present after point B returns to ground—as occurs for a valid signal—both points A and B will be at ground potential. Transistor Q_1 is thus cut off, providing a logic ONE at the output.

If the tone is no longer present—as when the detector is triggered by noise—point A will be at 5 V and point B at ground. Transistor Q_1 stays saturated, and the output remains at ZERO.

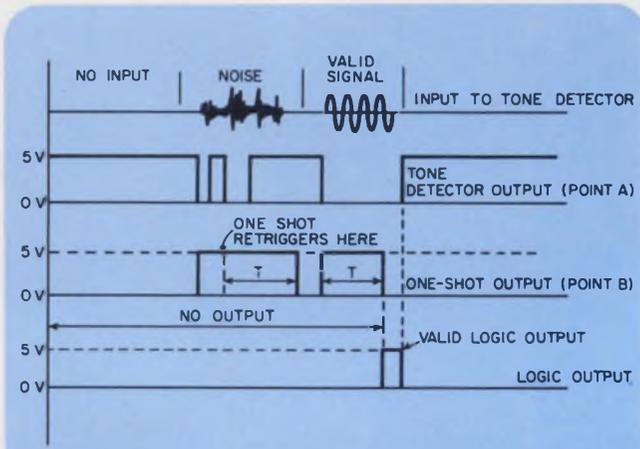
Resistor R_1 and capacitor C_1 control the timing (Fig. 2) of MM1. The R_1C_1 time constant should be chosen to be about five times longer than the longest noise component expected on the particular transmission channel. About 100 ms is adequate in the hf spectrum.

Edward I. Levy, Dade Div., American Hospital Supply, P.O. Box 672, Miami, Fla. 33152.

CIRCLE NO. 314



1. One-shot MM1 and transistor Q_1 prevent radio noise from falsely triggering the NE 657V tone detector.



2. False triggering of the tone detector or one-shot does not produce a logic output, as indicated by the three output waveforms.

IFD Winner of September 2, 1972

Peter Himmelheber, Senior Project Engineer and Stanley Thomas, Project Engineer, Naval Electronic Systems Test and Evaluation Facility, St. Inigoes, Md. 20684. Their idea, "Digital sweep generator maintains constant output voltage at specified time" has been voted the Most Valuable of Issue Award.

Vote for the Best Idea in this issue by circling the number for your selection on the Information Retrieval Card at the back of this issue.

SEND US YOUR IDEAS FOR DESIGN. You may win a grand total of \$1050 (cash)! Here's how. Submit your IFD describing a new or important circuit or design technique, the clever use of new component or test equipment, packaging tips, cost-saving ideas to our Ideas for Design editor. Ideas can only be considered for publication if they are submitted exclusively to ELECTRONIC DESIGN. You will receive \$20 for each published idea, \$30 more if it is voted best of issue by our readers. The best-of-issue winners become eligible for the Idea of the Year award of \$1000.

ELECTRONIC DESIGN cannot assume responsibility for circuits shown nor represent freedom from patent infringement.

To celebrate our 50th Anniversary—1923-1973



See this beauty at the Struthers-Dunn exhibit during the 1973 Design Engineering Show, Philadelphia, Pa. April 9, 10, 11, 12.

This 1923 Model T FORD as GRAND PRIZE for your most unusual relay application!

Second 50th Anniversary prize: TEN \$50.00 U.S. Savings Bonds.
Third Prize: FIVE \$50.00 U.S. Savings Bonds.

ALL entrants will receive a 9" x 12" four-color print of this photograph by contest end. Perfect for framing.

Yes! A beautifully restored Model T Ford Station Wagon from the same year the first Struthers-Dunn relays came out! It could be yours for telling us about your most unusual or interesting relay application, as detailed in the rules below. You and the car will be the talk of your town from the day it is delivered. Start writing or thinking about your application today! Note those second and third prizes, too! *Be sure to follow the rules below.*

CONTEST RULES

- (1) Entrants must give a clear and complete description of an unusual, but practical and operating, relay application or solution of a relay problem, using electromechanical or reed relays of any make or price. *Entries must contain nonconfidential matter only.* No purchase necessary.
- (2) Winning entries will be judged on basis of the most unusual applications and/or imaginative thinking of widest interest to relay specifiers.
- (3) The three judges, familiar with design and use of relays, will be from the editorial departments of technical trade publications, and their decision will be final.
- (4) Brevity, clarity and completeness will count. Be formal or informal. Schematics welcome.
- (5) No limit on entries, but keep each entry to one application.
- (6) Entries must be postmarked no later than midnight May 15, 1973. Address: 50th Anniversary Contest, Suite 1500, 1201

Chestnut Street, Philadelphia, Pa. 19107. Do not send entries to Struthers-Dunn or its distributors.

- (7) For anonymity in judging, entries will be coded and identification removed insofar as possible.
- (8) Winning entrants will be notified by July 1, 1973 and publicly announced and identified shortly thereafter.
- (9) Grand prize will be delivered to winner's home.
- (10) All entries become property of Struthers-Dunn, Inc. and none will be returned. Struthers-Dunn reserves the right to use all entries in its advertising and promotion on an anonymous basis, but entrants will be paid \$50.00 for each entry used.
- (11) Contest void where prohibited, regulated or limited by law. Winners will be responsible for taxes, if any, on prizes.
- (12) Employees of Struthers-Dunn, Inc., its sales affiliates, distributors, advertising agencies, contest judges and members of their families are not eligible.



STRUTHERS-DUNN, INC.

PITMAN, NEW JERSEY 08071

Canada: Struthers-Dunn Relay Div., Renfrew Electric Co., Ltd.

INFORMATION RETRIEVAL NUMBER 47

“Scotchflex” Flat Cable Connector System makes 50 connections at a time.



“SCOTCHFLEX” IS A REGISTERED TRADEMARK OF 3M CO.

Build assembly cost savings into your electronics package with “Scotchflex” flat cable and connectors. These fast, simple systems make simultaneous multiple connections in seconds without stripping or soldering. Equipment investment is minimal; there’s no need for special training. The inexpensive assembly press, shown above, crimps connections tightly, operates easily and assures error free wiring.

Reliability is built in, too, with “Scotchflex” interconnects. Inside of connector bodies, unique U-contacts strip through flat cable insulation, grip each conductor for dependable gas-tight connections.

“Scotchflex” offers you design freedom, with a wide choice of cable and connectors. From off-the-shelf stock you can choose: 14 to 50-conductor cables. Connectors to interface with standard DIP sockets, wrap posts on standard grid patterns, printed circuit boards. Headers for de-pluggable connection between cable jumpers and PCB. Custom assemblies are also available on request.

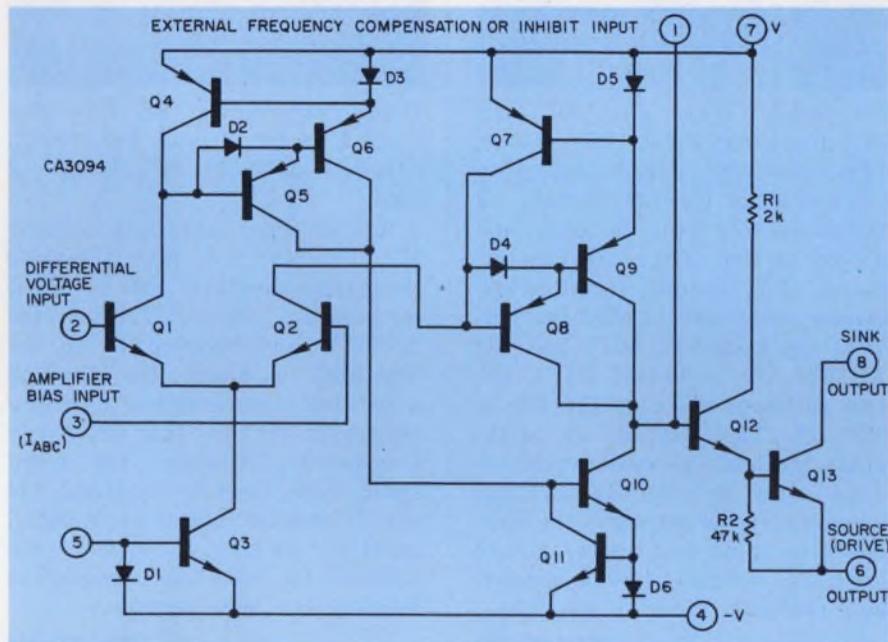
For more information, write Dept. EAH-1, 3M Center, St. Paul, Minn. 55101.



“Scotchflex”.
**Your systems approach
to circuitry.**

new products

Flexible power switch/amp IC delivers 10 W of peak power



RCA Solid State Div., Route 202, Somerville, N.J. 08876. (201) 722-3200. P&A: See below.

Consisting of a high-gain differential-input preamplifier driving an output power amplifier, RCA's monolithic CA3094 offers design flexibility for control and general-purpose applications. It can be used as an op amp or a power switch, delivering up to 3 W of average power or 10 W of peak power to an external load. And the device may be operated from either a single or dual power supply. Strobing, gating and squelching, as well as agc, are all programmable.

In single-ended class-A amplifier applications, the CA3094 can deliver 0.6-W output, with 1.6 W dissipation in the device. Total harmonic distortion at 0.6 W in class-A operation is typically 1.4%.

The new IC has the generic characteristics of RCA's popular CA3080 op amp directly coupled to an integral Darlington power transistor that is capable of sinking or driving currents of 100 mA average or 300 mA peak. This sig-

nal level is said to be sufficient to drive directly high-current thyristors, relays, dc loads or power transistors.

The gain of the differential input stage is proportional to the amplifier bias current, I_{ABC} , permitting programmable variation of the IC sensitivity with either digital or analog signals. With an I_{ABC} of 100 μ A, for example, a 1-mV change at the input changes the output from 0 to 100 mA (typical).

Despite its high power ratings, the CA3094 can be programmed to idle at microwatt power levels. And because input impedance can also be programmed, the IC can be used in timers to give delays in excess of four hours.

Versions of the CA3094 come in the eight-lead TO-5 package and differ only in supply-voltage ratings. The models available are rated at 24 V (suffix T), 36 V (suffix AT) and 44 V (suffix BT).

A major use of the CA3094T is expected in automotive equipment and other applications where operation up to 24 V is a primary de-

sign requirement.

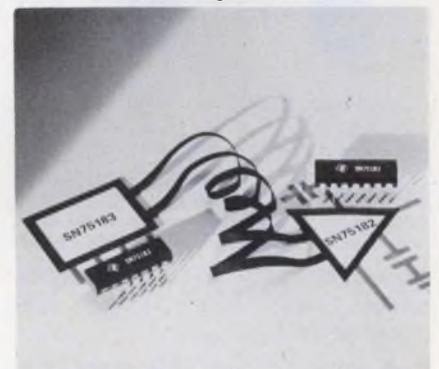
The CA3094 may also be obtained with formed leads corresponding to the eight-lead DIP or Mini-Dip. These models are designated with suffixes S, AS and BS, corresponding to the CA3094T, CA3094AT and CA3094BT, respectively.

Pricing for 100 to 999 quantities is 75¢ (suffixes T and S), \$1.19 (suffix AT and AS) and \$1.67 (suffixes BT and BS).

For more information

CIRCLE NO. 251

Driver-receiver good for twisted pair line



Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. SN75182N: \$3.14; SN75183N: \$3.48 (100 up); stock.

A line driver and receiver combination can be used in digital systems connected by twisted pair lines. The dual differential line receiver—the SN55/75182—replaces the DM7820A/DM8820A while the dual differential line-driver—the SN55/75183—replaces the DM7830/DM8830. The 182 receiver has two independent units. The input stage rejects large common mode signals while responding to small differential signals.

CIRCLE NO. 252

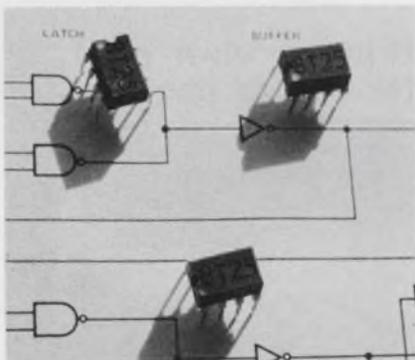
4k RAM emerges from Coplomar process

Standard Microsystems Corp., 35 Marcus Blvd., Hauppauge, N.Y. 11787. (516) 231-5151.

A 4096-bit electrically alterable RAM with decoding and sensing contained on a single monolithic silicon structure offers twice the speed of standard RAMs, according to the manufacturer. Called the SMC N-4412, the memory uses the company's Coplamos process. With a silicon die that's comparable in size to current 1024-bit configurations, the new memory has an access time of less than 180 ns. Production pricing is expected to eventually reach 0.25¢/bit.

CIRCLE NO. 253

Dual amp senses low-level MOS signals

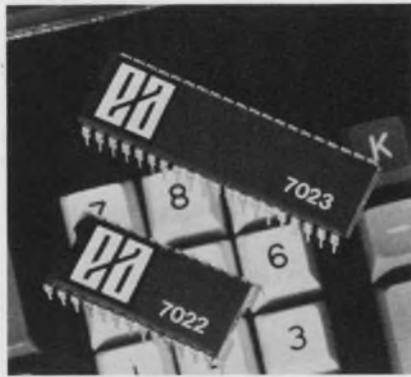


Signetics, 811 E. Arques Ave., Sunnyvale, Calif. 94086. (408) 739-7700. \$2.85 (100 up).

A dual MOS-to-TTL sense amplifier, for MOS RAMs—the 8T25—performs the same functions as two 75107 line receivers and either one-half of an 8275 quad bi-stable latch or a third of an Intel 3403 hex latch, according to Signetics. Thus one tiny eight-pin IC replaces two 16-pin packages and more. Another feature of the device is that it's bus-ORable—the tri-state outputs permit interface from the MOS memory directly onto a bus. Data inputs are current-sensitive, with a threshold of 300 mA. In the HIGH level, the voltage of the driving source must be greater than 1.6 V.

INQUIRE DIRECT

Calculator system on two ICs



Electronic Arrays, Inc., 501 Ellis St., Mountain View, Calif. 94040. (415) 964-4321. \$32.50 (100).

Two MOS circuits contain all the calculating logic, the clock, and a good portion of the interface circuitry of a 12-digit, four-function memory calculator. Called the EA-7022 (in a 28-lead DIP) and the EA7023 (in a 40-lead DIP), the two packages make up the EA S-129 set. They include an arithmetic/algebraic processor with 12-digit entry and display capacity, an accumulator memory, the keyboard scanning and display control logic, an internal clock generator, and power-on clearing circuitry.

CIRCLE NO. 254

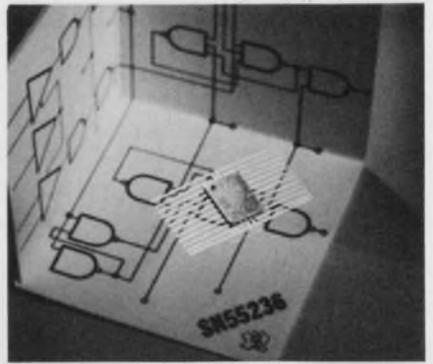
M119 dual comparator series offered

National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, Calif. 95051. (408) 732-5000. LM-119: \$13.95; LM219: \$8.50; LM-319: \$3.95 (100 up); stock.

The LM119 series precision dual comparator is designed for operation with a single 5-V power supply to ± 15 -V supplies. It has improved specs over older comparators, according to the manufacturer. Special features include bias current of 500 nA, response time of less than 100 ns and gain of 40,000. Both the inputs and outputs of the LM119 can be isolated from system ground and as much as 25 mA output current is available from each comparator. With large overdrive, the response time of the LM119 is substantially less than 100 ns.

INQUIRE DIRECT

Sense amp/data register has ± 2 -mV sensitivity



Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. \$23.17 (100 up); 8 wks.

A dual sense amp/data register IC features ± 2 mV threshold sensitivity over the -55 to 125 C temperature range. Termed the SN55236 and believed to be the first MSI sense amp, the IC offers a two-times improvement in threshold sensitivity over that previously announced. Designed for high-speed core memory systems, the new IC detects bipolar differential input signals from the memory and provides the interface between the memory and logic section.

CIRCLE NO. 255

Fast rectifiers go to 20 A, 600 V

RCA Solid State Div., Route 202, Somerville, N.J. 08876. (201) 722-3200. TA8411, TA8411R: \$1.49; TA8415; TA8415R: \$2.00; TA-8419, TA8419R, \$2.80 (1000 up); stock.

Twelve 100 to 600-V fast-recovery silicon rectifiers, available in forward and reverse-polarity versions, have current ratings of 6, 12 and 20 A. Series TA8411 through TA8414 are 6-A, forward-polarity types (cathode connected to stud), while Series TA8415 through TA-8418 are rated at 12 A. The Series TA8419 through TA8422 covers 20-A applications. Repetitive peak reverse voltage ratings are 100 V for TA8411, 15 and 19; 200 V for TA-8412, 16 and 20; 300 V for TA-8413, 17 and 21; and 600 V for TA8414, 18 and 22. All twelve devices have reverse-polarity versions (like numbered with suffix R) that are anode connected to stud.

CIRCLE NO. 256



Two New Opto-Isolators Featuring LEDs with CdS Cells...

Offering high reliability at low cost, PHOTO-MOD[®] opto-isolators, series CLM-6000 and CLM-8000, are now available for immediate delivery from Clairex. Using solid-state lamps and Clairex photoconductive cells, reliability and ruggedness are inherent in the design.

CLM-6000 is a miniature, low power, low resistance, isolator offering noiseless switching and

complete isolation for TTL to TTL interfaces.

CLM-8000 provides a hermetically sealed CdS cell and an LED. Operates on line voltage to drive SCRs and Triacs from TTL outputs.

For complete data or special assistance with your isolation problems, call (914) 664-6602 or write Clairex[®], 560 South Third Avenue, Mount Vernon, New York 10550.

CLAIREX ELECTRONICS
A DIVISION OF CLAIREX CORPORATION

Reliability. Our patented Grand Prix sleeve bearing design is rated at 12 years operating life (at 54°C). It's cool running and quiet. A unique capillary seal eliminates lubricant seepage. Rugged all-metal construction won't warp, resists breakage and acts as an effective heatsink.

Cooling power. PeWee delivers more air at higher back pressures — 22 cfm at .10 inches of water, 30.5 at .06 inches, 36 cfm in free air.

Whatever the equipment — rack panel, tape deck, power supply, counter, or memory stack, where space is at a premium and cooling critical, PeWee Boxer performs.

Other airmovers? Of course! Send for our full-line catalog No. ND4r. It's free, and contains performance data, electrical and mechanical specifications on more than 100 units. Valuable application information too.

For immediate service, contact us at **IMC Magnetics Corp., New Hampshire Division**, Route 16B, Rochester, N.H. 03867, tel. 603-332-5300. Or the IMC stocking distributor in your area. There are more than 50 nationwide and overseas. **IMC. We're reliable.**

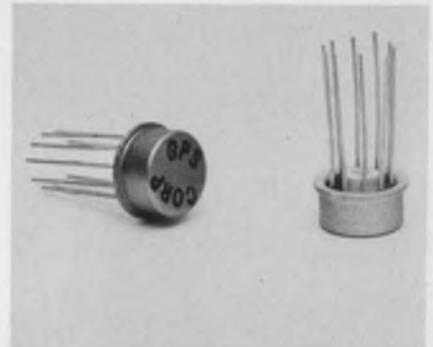
The Tiny Giant. It's 3 1/8 inches square by 1.655 inches slim. The only fan its size delivering 36 cfm. IMC's PeWee Boxer.



INFORMATION RETRIEVAL NUMBER 50

ICs & SEMICONDUCTORS

4-quadrant multipliers boast 0.5% accuracies



GPS Corp., 14 Burr St., Framingham, Mass. 01701. (617) 875-0607. Stock.

The 4100 Series four-quadrant multipliers are tiny hybrids that have accuracies of up to 0.5%. Other features of the line include a full power response of 800 kHz, bandwidth of 1 MHz and slew rate of 45 V/μs. Wide bandwidth operation, wide temperature range and the increased versatility of the 4100 Series make it ideal for all multiplier applications in control and instrumentation systems, according to GPS Corp.

CIRCLE NO. 257

'Calculator-on-a-chip' line expands to 9 ICs

Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. 8-digit chips: \$38.15; 10-digit chips: \$41.97 (100 up); stock.

The TMS0100 family of "calculator-on-a-chip" MOS/LSI ICs has been expanded to nine standard off-the-shelf circuits. The TMS0101 and TMS0103 are preferred eight-digit circuits, while the TMS0106 and TMS0118 are preferred ten-digit versions. The TMS0101 has floating or fixed-point result, chain operation, constant operation and protection of result in overflow; it uses algebraic keyboard entry. The TMS0103 provides four operations, floating or fixed decimal point and constant or chain operation; it's ideal for desk-top machines. The TMS0106 and TMS0118 feature a three-position selectable round-off.

CIRCLE NO. 258

INFORMATION RETRIEVAL NUMBER 51 ►

Bright Tape Decks

...for those who
expect to get more
when they pay more.



Bright tape decks cost more than other tape decks. They cost more because more goes into them—more quality in the materials, more care in design and manufacturing.

But this quality and care wouldn't be worth the extra you pay for it unless it meant greater reliability and freedom from the problems you accept as routine with other tape decks.

Bright quality pays for itself.

Bright tape decks have a rigid cast front panel. A front panel that can't come out of alignment so the tape always runs true, and tedious adjustments are unnecessary. Also, by conservative design, all electronic adjustments have been eliminated. The only maintenance is a simple bit of clean-up; there's virtually no downtime.

Even a seemingly insignificant part like a constant tension spring on the buffer arm received our attention. Because of this spring, you

can be sure that your tape will run at a constant speed and stack on the reel uniformly; when the tape is uniform on the reel, it won't stretch in storage.

And to insure uniform data density and perfect IBM compatibility, the timing, spacing, and tape speed are tied directly to the capstan encoder.

Available in either 8½ inch or 10½ inch models, you can buy Bright tape decks configured to suit your needs. Construction is completely modular with small, functionally organized circuit boards. You can order anything from the bare necessities to fully buffered electronics and interfaces for your application.

It's true that Bright tape decks cost more (about 10%), but you get what you pay for—a tape deck that is truly impressive in your system.

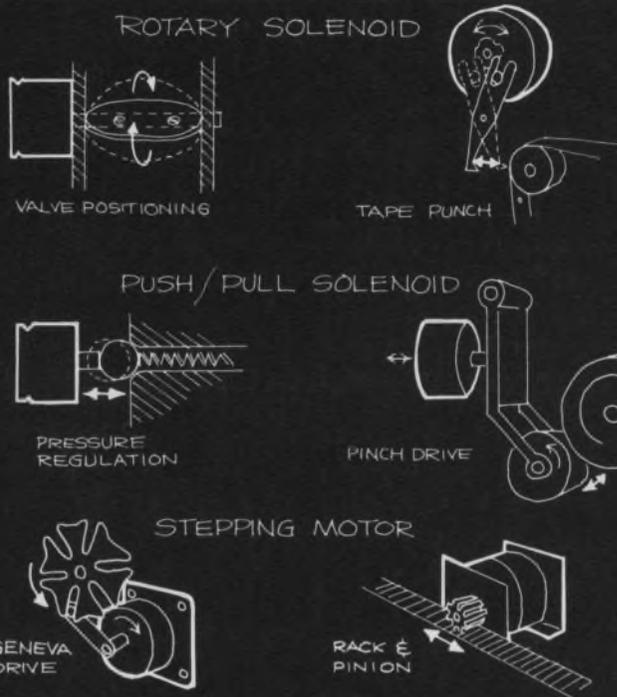
For more information write to Bright Industries, Inc. 686 West Maude Avenue, Sunnyvale, California 94086, (408) 735-9868.

Bright

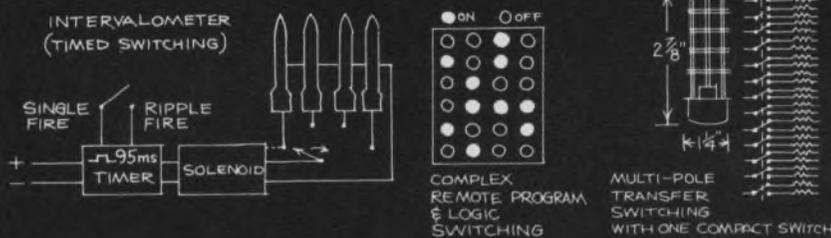
INDUSTRIES INC.

A Subsidiary of Data Disc, Inc.

When you've got a load to move,



or circuits to switch . . .



Ledex Rotary Solenoids give you fast, direct rotary motion. There's a family of eight sizes with torque all the way up to 117 pound inches. For linear loads, our **Push/Pull Solenoids** respond in less than 10 ms. Both have a compact form factor and there are over 350 stock models to get your prototype off the board and into the shop fast.

Ledex Stepping Motors position loads remotely in predetermined increments over 360°, cw, ccw, or both. You can add a knob for manual positioning. Attach a load on either or both ends. And our newest 12-position model has built-in pulsing circuitry, so it self-steps; needs no logic circuitry.

You'll find versatile **Ledex Switches** everywhere . . . in aircraft controls, laboratory instruments, business machines,

even amusement games. They take up very little space to control, transfer, program and check out complex circuits.

For a neat **Packaged Control Solution** to your most complex switch problems, we'll deliver the answer in a small black box, ready to plug in. Chances are, the Ledex combination of people and products have solved an actuating or switching problem much like yours already. Just send us an outline of your problem. Or ask for:

Catalog A-9500
Over 400 ways to turn . . . push . . . pull . . . step . . . and switch plus new micro-electronic interface circuits.



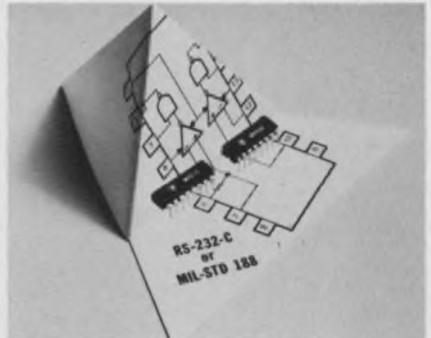
LEDEX the total technology people

LEDEX INC.
123 Webster Street
Dayton, Ohio 45401
(513) 224-9891

POSITIONING · SWITCHING · MICROELECTRONICS
INFORMATION RETRIEVAL NUMBER 52

ICs & SEMICONDUCTORS

Line receiver IC meets standard specs



Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. \$5.40 in plastic; stock.

A dual line receiver IC meets RS-232-C or MIL-STD-188C specs without requiring external components. Designated the SN75152, this interface IC features a ± 25 V input common-mode range, 25 V differential input capability and continuously adjustable hysteresis with external resistors. Input hysteresis for the SN75152 remains approximately fixed for power supply and/or temperature variation. This receiver operates on ± 12 V power supplies and over the 0 to 70°C industrial temperature range.

CIRCLE NO. 259

1024-bit static MOS RAM easy to use

Intel Corp., 3065 Bowers Ave., Santa Clara, Calif. 95051. (408) 246-7501. \$35 (100 up); stock.

A 1024-bit n-channel silicon-gate static MOS RAM connects to TTL logic without any interface circuits. Termed the 2102, it runs on a single 5-V supply, accepts standard TTL inputs and generates a standard TTL output. Because the RAM is fully decoded and static, it requires no external decoding circuits, no refreshing circuits and no clock. Other features include an access time of 1 μ s, power dissipation of 0.15 mW/bit and input capacitance of only 5 pF. It has a 3-state output for OR-tie capability and a chip-enable input to facilitate simple memory assembly and expansion.

CIRCLE NO. 260

WINDJAMMER

FREE

barefoot adventure

**SOMETHING TO
STIMULATE YOUR
EROTIC PREOCCUPATION**

We have a book with color pictures. It's nothing pornographic. But somehow it tends to stimulate erotic thoughts. Especially if you're a free thinking, uninhibited person who wants to be turned on to an unusual vacation experience.

We sail adventurous schooners to several slightly uncivilized islands in the Caribbean. Places like Grenada, Saba, Monserrat, St. Maarten and Antigua. Fortunately these are the few islands that haven't been overrun by jaded tourists.

So you can find a deserted beach and stretch without being seen. Or you can strip down and play under a waterfall. Or you can get into the local color on each island.

And we haven't let our Windjammer cruises become a luxury. We keep things basic. Nice, clean cabins. Good hearty food. And an uninhibited crew that will entertain you until dawn with wild native music. The rest is up to you. There are no formalities, no social pressures, no restrictions. Fish, skin dive, soak up the sun and communicate with real people in an unhampered, natural setting.

A 10 day Windjammer cruise starts at \$245 per person. Write for our free book today. It will give you something good to think about.



Windjammer Cruises.
P.O. Box 431, Main Office Department 550 Miami, Florida 33101

Yes, send me the book.

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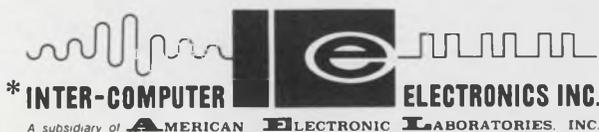
Zip _____

few major
companies
can give you
this type of
recorder.



**Our Recorder
is the one with
greater accuracy
and efficiency.**

- With a larger memory bank . . .
41% larger . . . for more on-line processing
before the memory has to be cleared again.
 - Greater accuracy in system stability and recording.
 - With these pluses and more,
our Pulse and Transient Recorder costs less.
- Add to this an unheard of ease of operation,
a compatibility with all types of recording devices
and a flexibility that makes its applications seem endless,
and you've got the one that fulfills your recording needs best.
- Ask for the whole story, ask for the literature
on the *ICE Pulse and Transient Recorder.
The better one.



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INFORMATION RETRIEVAL NUMBER 54

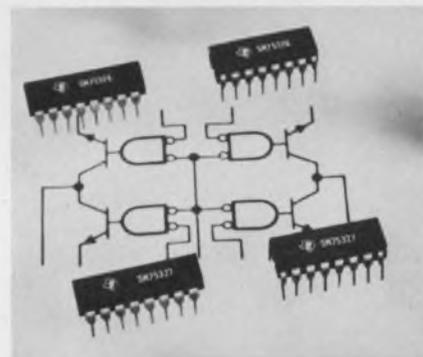
UV silicon photodiodes spec'd at 90 mA/W

EG&G, Inc., Electro-Optics Div., 35
Congress St., Salem, Mass. 01970.
(617) 745-3200.

A UV series of photovoltaic silicon photodiodes are optimized for analytical instrument applications. Special features include a spectral responsivity at 230 μm of 90 mA/W; spectral stability at 230 μm of 0.13%/°C; equivalent Johnson noise current in the range of $2\text{-}5 \times 10^{-14}$ A per root hertz; and a linearity response within 1% over seven decades of irradiance. Available stock items are the UV-100 with an area of 0.051 cm^2 ; the UV-444A with active area of 1.0 cm^2 ; the UV-800A with active area of 3.14 cm^2 ; and the HUV-1000 op amp/photodiode, which combines the UV-100 and a low noise, FET input op amp in a TO-5 package.

CIRCLE NO. 261

Driver ICs good for magnetic memories

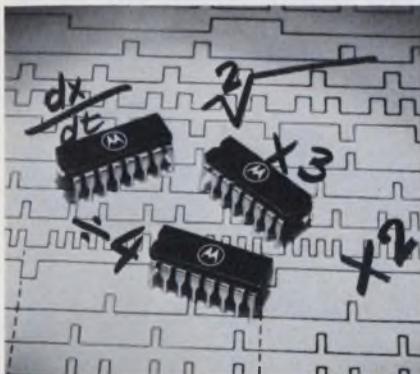


Texas Instruments Inc., P.O. Box
5012, M/S 308, Dallas, Tex. 75222.
(214) 238-3741. SN75326N and
SN75327N: \$4.20 (100 up); stock.

Two versatile memory driver ICs, termed the SN55/75326 and the SN55/75327, are compatible with high speed magnetic memory systems. These quad bipolar memory drivers accept standard TTL/DTL decoder input signals and create high current, high-voltage output levels suitable for driving magnetic memory drive lines. Output transistor selection is determined by four separate address inputs and common timing strobe.

CIRCLE NO. 262

CMOS rate multiplier does arith functions



Motorola Semiconductor Products Inc., P.O. Box 20924, Phoenix, Ariz. 85036. (602) 273-3466. MC-14527CL: \$6.60; MC14527AL: \$11.85 (100-999).

The MC14527 BCD rate multiplier, a CMOS (CMOS) device, performs arithmetic, algebraic and differential-equation functions. The output of the multiplier has a pulse rate based on a BCD input number. This device is the first low power—0.25 μ W (quiescent)/package at 5 V dc—and high noise immunity (45% of V_{DD} typ) BCD rate multiplier. Previous digital rate multiplier functions have been available only in TTL devices.

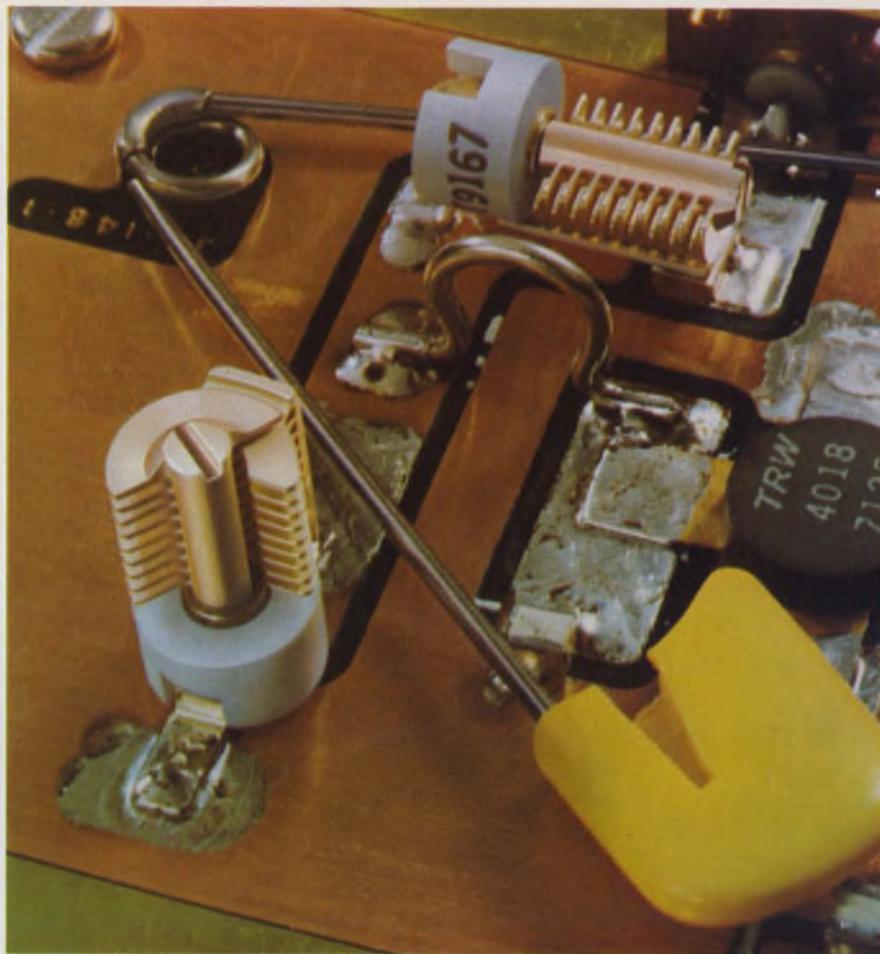
CIRCLE NO. 263

Programmable processor system

Fairchild Semiconductor, 464 Ellis St., Mountain View, Calif. 94040. (415) 962-3816

A family of microprogrammed MOS/LSI data processor circuits can be developed into a wide variety of small programmable digital processing systems. Called the PPS-25 (for Programmable Processor System), the system consists of a kit of six basic building blocks: the 3807/3803 keyboard circuits, 3805 arithmetic unit, 3806 function and timing unit, 3808/3809 serial memory registers, 3810 ROM and the 3811 output device. Although the kit comprises standard devices, it can be adapted to individual system requirements by microprogramming the 3810 ROM.

CIRCLE NO. 264



The smallest 180° tuning air variable capacitors just had babies!

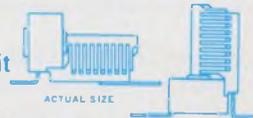
Right. Johnson's exclusive subminiature type "T" air variable capacitors (PC mounts) now come with stripline terminals for microwave applications, either vertical or horizontal tuning.

These space-savers are only about 1/3 the volume of a "U" capacitor, but they offer extraordinarily high mechanical and electrical performance for critical applications.

Rotors and stators are as stable and uniform as precision machining from solid brass extrusion can make them. A high 1 1/2 to 8 ounce-inches torque holds the rotor securely under vibration.

Temperature coefficient is very low plus 30 ± 15 ppm/° C. Q is high, typically 1800 at 200 MHz. Three capacitance ranges span from 1.3 pF to 15.7 pF.

Our 45 years of experience really shows up in these new capacitors. But why take our word for it when a stamp will get you a couple of freebies and you can check them out for yourself.



E. F. JOHNSON COMPANY / 3301 Tenth Ave., S.W. / Waseca, Minnesota 56093

Check type and range of sample(s) needed:	Capacitance range	1.3 to 5.4	1.7 to 11.0	1.9 to 15.7
Horizontal tuning		<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>
Vertical tuning		<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>

Name _____ Phone _____

Firm _____ Title _____

Address _____

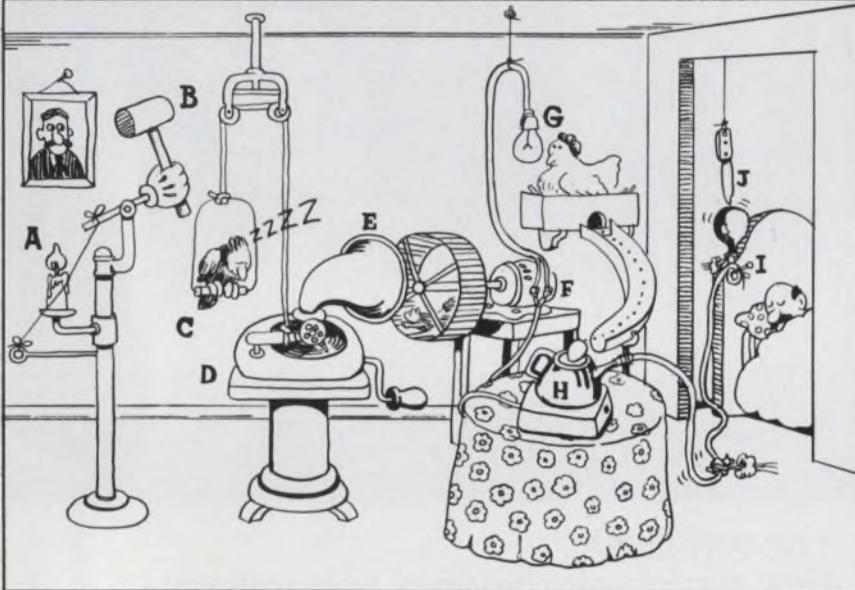
City _____ State _____ Zip _____



E. F. JOHNSON COMPANY

INFORMATION RETRIEVAL NUMBER 55

WHILE SPENDING LONG SUNLESS DAYS IN ALASKA, PROFESSOR FLAKE CAME UP WITH THIS INGENUOUS INVENTION WHICH HE CALLS "THE COMBINATION CHICKEN-FOOLER AND THREE MINUTE EGG ALARM. CANDLE (A) BURNS DOWN TO THE POINT WHERE STRING BREAKS. THIS ALLOWS HAMMER (B) TO FALL KNOCKING SLEEPING BIRD (C) OFF SWING. REMOVAL OF BIRD'S WEIGHT ALLOWS PHONOGRAPH ARM TO FALL ON RECORD (D) AS RECORD PLAYER (E) BLASTS OUT "JADA," SQUIRREL THAT HAS BEEN TRAINED TO RESPOND, TURNS TREADMILL ATTACHED TO GENERATOR (F). GENERATOR LIGHTS BULB (G) AND CHICKEN, THINKING IT IS SUNRISE, LAYS EGG WHICH ROLLS INTO TEAKETTLE ON ELECTRIC HOT PLATE (H). STEAM FROM TEAKETTLE TRAVELS THROUGH HOSE ATTACHED TO BED (I). AS STEAM INFLATES RUBBER BALLOON, IT PRESSES AGAINST POINT OF KNIFE (J) AND IS PUNCTURED. THE RESULTING NOISE AWAKENS SLEEPING MAN JUST IN TIME TO RETRIEVE THREE-MINUTE EGG FROM TEAKETTLE.



There's a better way to time yourself. Send for our E-Cell™ Kit.

A \$30 value to introduce you to the wide range of timing, counting, integrating, delaying, monitoring, sequencing and measuring capabilities of this remarkably useful electronic device. Ten functioning E-Cell components, ready to use, with schematics for circuit assembly. Full specifications. Applications Notes and Plug-in sockets. The whole works for only \$9.95.

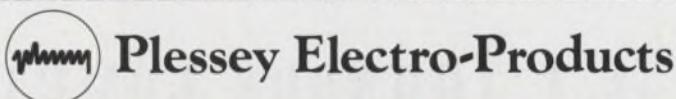


actual size

Plessey Electro-Products
3860 Centinela Avenue, Los Angeles, California 90066

Enclosed is my check or money order for \$9.95.
Please send my E-Cell Applications Kit to:

Name	
Title	Company
Street	City
State	Zip



INFORMATION RETRIEVAL NUMBER 56

Fast multipliers give 8 bits in 40 ns



Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. SN74284N and SN74285N: \$8.10 (100 up); stock.

Two TTL/LSI ICs can be used together to generate an eight-bit binary product in 40 ns. Designated the SN54/74284 and SN54/74285, these four-bit-by-four-bit parallel binary multipliers each contain the equivalent of over 200 gates on a monolithic chip. Used with the SN54H/74H183 carry-save adder, the SN54S/74S181 arithmetic logic unit, and the SN54S/74S182 look-ahead generator, expandable n-bit-by-n-bit applications are possible.

CIRCLE NO. 265

Waveform gen/VCO has 50 ppm/°C stability

Intersil, 10900 N. Tantau Ave., Cupertino, Calif. 95014. (408) 257-5450 8038A: \$9; 8038B: \$4; 8038C: \$2.50 (100 up).

A monolithic IC waveform generator and voltage controlled oscillator, termed the 8038, produces simultaneous sine-wave, square-wave, and triangular-wave outputs with minimum amplitudes up to 6 V, 28 V and 10 V pk-pk, respectively. The 8038C has a typical temperature drift stability of 50 ppm/°C. Other versions have typical drift specs of 10 ppm/°C (8038A) and 20 ppm/°C (8038B). All outputs may be made TTL compatible and output frequency is tunable from 0.001 Hz to 1.0 MHz.

CIRCLE NO. 266

SUPER BOWL



... and what a line-up—depth in every position! A rugged team of general purpose relays from 1 to 20 amps, AC and DC, 1 to 6PDT, with ratings to 110 VDC and 250 VAC. At the corners, dry reed and mercury-wetted DIP; on the line, open frame and covered units, plug-in and axial lead, Forms A, B and C, with ratings to 2 amps, 50 watts and 500 VDC. And in line backer slots, a new series of electromechanical and solid state industrial timers and sensors with delays of 0.01 to 360 seconds, voltages to 220 VDC and 400 VAC, and frequencies to 440 Hz.

Whatever signals you call, you're the coach with the Babcock team. Call your own "audibles" with our general purpose units; they're completely interchangeable with other models. They'll plug right into your PC board or socket with no time out. And there's never a fumble on delivery—the entire Babcock team is available "off the bench". If you have a design problem, huddle with us on it.

too; our applications engineering staff is ready to join your team.

Send for your FREE program today—our new short form lists all the players...with some very interesting numbers. Write or call Babcock Electronics Corp., Unit of Esterline Corp., 3501 No. Harbor Blvd., Costa Mesa, Calif. 92626; Tel: (714) 540-1234.

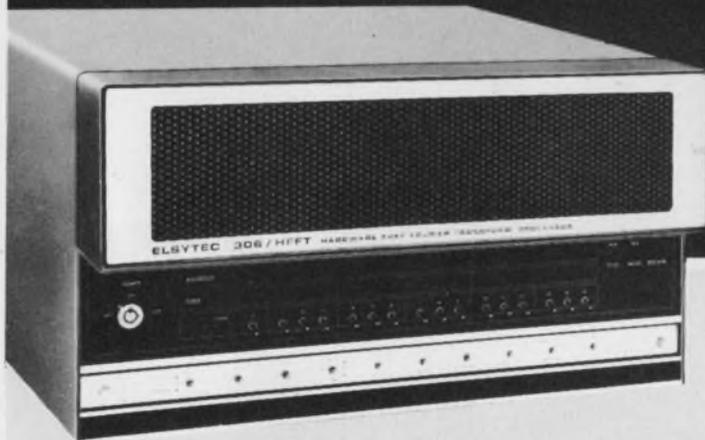


BABCOCK

A UNIT OF ESTERLINE CORPORATION

INFORMATION RETRIEVAL NUMBER 57

Hardware Fast Fourier Transform Processor



The 306/HFFT is a digital processor that performs forward or inverse Fourier Transforms of time or frequency domain data. It is contained within the mainframe of its host NOVA 800 computer for efficiency, smaller size and cost saving.

FEATURES

- Basic Fast Fourier Transform time of 9.5 ms for 512 complex points (1024 real points).
- Real-Time to 25 KHz for 1024 real input points, 18 ms total processing time including all requisite procedures.
- Transform from 16 to 16384 real points.
- Full 16 bit accuracy.
- Polar coordinate output standard.

APPLICATIONS

- | | | |
|-----------------------|------------------------|-----------------|
| Underwater acoustics | Speech recognition | Biomedicine |
| Mechanical vibrations | Noise identification | Geophysics |
| Digital filtering | Doppler radar analysis | Nuclear physics |

EXPAND to a complete Fourier Spectrum Analyzer by field addition of:

- A single or dual Input Channel.
- Anti-aliasing filters
- Operation oriented Control Panel
- Output displays

Delivery is 90 days ARO.

For further information, contact your local representative or the factory directly.



212 MICHAEL DRIVE, SYOSSET, N.Y. 11791
(516) 364-0560

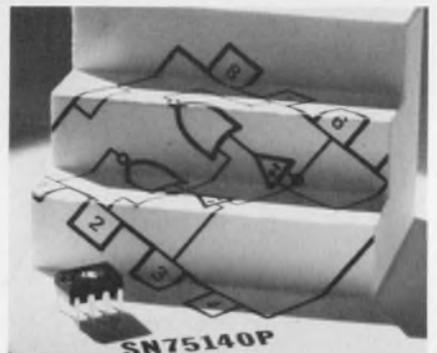
High threshold logic line expands

Motorola Semiconductor Products, Inc., P.O. Box 20924, Phoenix, Ariz. 85036. (602) 273-3466. MC684P, MC685P and MC686P: \$4.05; MC688P: \$2.10.

The company's high threshold logic (HTL) line expands by four new devices: the MC686, a four-bit shift register (the first shift register offered in MHTL Series); the MC684, a decade counter, and the MC685 binary counter (first two counters in the series) and the MC688, a dual J-K flip-flop in a 16-pin package. All MHTL devices operate on a +15 V power supply. Switching threshold voltage is typically +7.5 V, while dc noise margin is typically 6 V.

CIRCLE NO. 267

Dual line receiver features ± 100 mV input

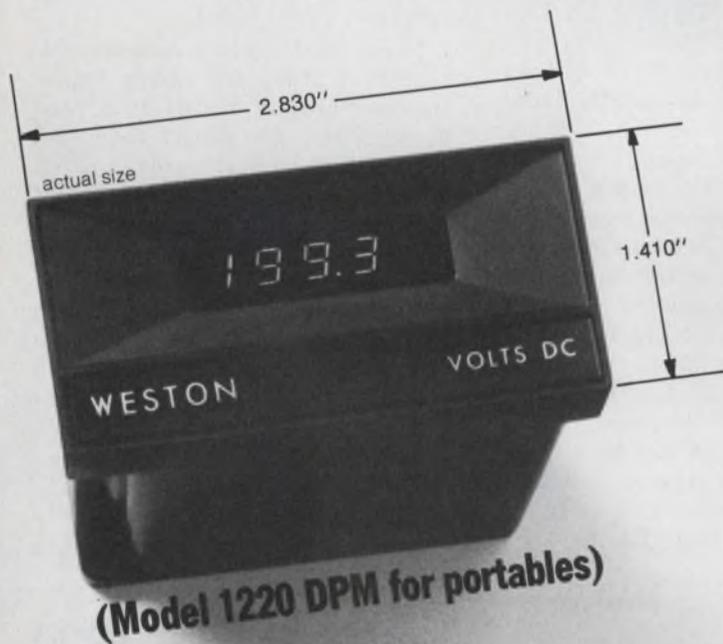


Texas Instruments Inc., P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. P: See below.

A versatile and economical dual line receiver provides a low-input current of less than 100 μ A. This allows the receiver, designated the SN75140P and priced at \$2.52 (100 up), to be used in bus-organized systems. As many as 100 receivers may be used per line. The device comes in an 8-pin plastic DIP and features a guaranteed ± 100 mV input sensitivity for higher noise margins. Also, threshold voltage is externally adjustable from 1.5 to 3.5 V.

CIRCLE NO. 268

WESTON presents a small achievement.



At last—a truly tiny DPM, with all the features you need for portable equipment.

A full 3½-digit meter. Weighs only 4 ounces. Takes up less than 4 square inches of panel space. Or, if that's too much, you can flush-mount it with only the readout showing.

But, power requirements are the big story of the 1220. 5.5V ± 10% is all the DC it needs. Use four Nicad C cells for up to 18 hours continuous operation—with all segments lit. Or, draw from equipment DC power supply. The 1220 uses less than .75 watt with all digits working. And, digits not in use are

automatically blanked out to conserve power.

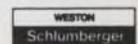
And that's not all. The 1220 features a plug-in bi-polar LED display, reliable printed circuitry built around a plug-in LSI chip, and is designed to conform to vibration spec. MIL-M-10304. External display check feature lets you illuminate all segments of the display. And, of course, it needs no warmup. Accuracy is guaranteed from the moment you turn it on! Ten variations of the 1220 are available to give you a choice of full-scale ranges from 100MV to 1000V, 10µA to 100MA.

Sound like a lot? Here's the best part. The Model 1220 is less than \$100 each in OEM quantities. For line operation only, order Model 1221.

To see our new Model 1220 DPM, call your nearest Weston distributor. He'll be glad to go anywhere to show you the "go-anywhere" DPM. Or, call us direct at (201) 243-4700. Weston Instruments, Inc., 614 Freylinghuysen Ave., Newark, N.J. 07114.

We're either first or best. Or both.

WESTON®



Recorder provides copy from CRT terminals



Alden Electronic & Impulse Recording Equipment Co., Inc., Alden Research Center, Westborough, Mass. 01581. (617) 366-8851. \$2400 (unit qty.); \$1830 (100 up).

The Alden 600 "Push to Print" OEM recorder provides paper records from graphic CRT display terminals. A flying-spot technique is used to write on electrosensitive paper at 30 lines/s—a 600-line frame takes 20 s. Recordings are visible immediately and require no further processing. No toners, developers and fixers are used, and the cost of supplies is less than one cent per frame. A sweep-trigger output pulse is supplied by the unit. The user supplies X-Y voltages and a CRT target "read" signal to the unit. Space and power are available for the addition of a customer's circuitry within the housing.

CIRCLE NO. 269

CPU chip offers 12.5 μ s instruction cycle

Intel Corp., 3065 Bowers Ave., Santa Clara, Calif. 95051. (408) 246-7501. \$90 (100 up); stock.

Model 8008-1, a faster version of the Model 8008 CPU, is designed for direct addressing of up to 16 k, eight-bit words. Model 8008-1 contains an eight-bit parallel adder, six 8-bit data registers plus 11 additional registers. It operates with a set of 45 instructions, has interrupt capability, can perform as many as seven nested subroutines and operates synchronously or asynchronously. All inputs and outputs are TTL compatible.

CIRCLE NO. 270

Cartridge recorder takes 1/4-in. tape



Kennedy Co., 540 W. Woodbury Rd., Altadena, Calif. 91001. (213) 798-0953. \$750.

Model 330 is designed for reliable data recording on the 1/4-in. 3M tape cartridge. Read/write speed is 25 in/s in both directions. Forward/reverse search or rewind is done at a speed of 90 in/s. Data are recorded separately on four tracks of a 300-ft tape using a density of 1600 bits/in. Model 330 meets the proposed ANSI standard. One and two track versions of the unit are also available. Cartridges recorded on these other versions can be used with the four-track unit.

CIRCLE NO. 271

Versatile interface collects lab data

Bell Engineering, 1425 N. Ridgeway Dr., Tucson, Ariz. 85712. (602) 296-9005. \$2500.

This compact rack or bench-mount interface, for IBM-1800 series computers, transfers control signals and 16-bit data words from IC or relay data sources. Designated as Model 275, the unit features optical coupling for ground loop isolation, logic level conversion with adjustable noise immunity and adjustable time delays for generating process interrupts. Data transfer from a source device can be initiated via an interrupt generated from the source or under program control. Available options include: built-in status indicators, a diagnostic test panel and modified logic levels for interface with other computers.

CIRCLE NO. 272

Interface controls data acquisition



Moxon Inc., SRC Div., 2222 Michelson Dr., Irvine, Calif. 92664. (714) 833-2000. \$1095; 3 wks.

Model-3900 analog-data-acquisition unit from the above manufacturer can be modified to send data serially via ASCII code (RS 232). Three circuit cards, costing \$770, format the characters, insert stop bits, control the number of words per printed line, and provide other functions. Baud rates of 110, 115 or 300 can be selected. There are two additional cards with optional applications. The fourth card permits remote control converter operation and the fifth card inserts time codes using any external BCD source. These cost \$175 and \$150, respectively.

CIRCLE NO. 273

Software package works with digitized data

Visicon Inc., Box 1008, State College, Pa. 16801. (814) 237-6521. See text.

Written in ASA Basic Fortran, this software package converts raster information from digitizing equipment such as flying-spot scanners to formats compatible with such devices as interactive drafting systems and digital incremental plotters. Requirements for use include a machine with Fortran capability and a memory of 16 to 20 k words depending on the I/O structures. An IBM 360/65, for example, can, per processing second, convert up to 16 inches of line information from the raster. The package is available on a leasing arrangement, with a cost of \$5000 for the first year and \$1000 per year thereafter. Maintenance and updating of the software is included in the lease.

CIRCLE NO. 274

DIGITEC'S NEW DATA LOGGERS



HAVE ALL THIS VERSATILITY

- Models to measure Voltage, Current, Resistance, Temperature & other transduced parameters.
- 20 selectable scan points standard, expandable to 200.
- Real-time digital clock with program interval for unattended operation, standard.
- Digital printout arranged for quick, easy reading.
- BCD and system interlocks brought out to interface peripherals such as: comparators, tape punch, and mini-computer.
- Loss of power indication.
- All LED long-life displays.

WITH PRICES UNDER \$1900

To see the DigiTec 1200 or 1500 series Data Loggers, simply contact your DigiTec representative. Or, you can call or write; **United Systems Corporation**, 918 Woodley Rd., Dayton, Ohio 45403 Phone (513) 254-6251.

All DigiTec instruments are available for rental or lease through Rental Electronics, Inc.

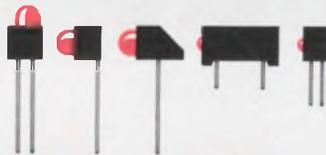
DIGITEC
UNITED SYSTEMS CORPORATION
subsidiary of **Monsanto**

Dialight sees a need:

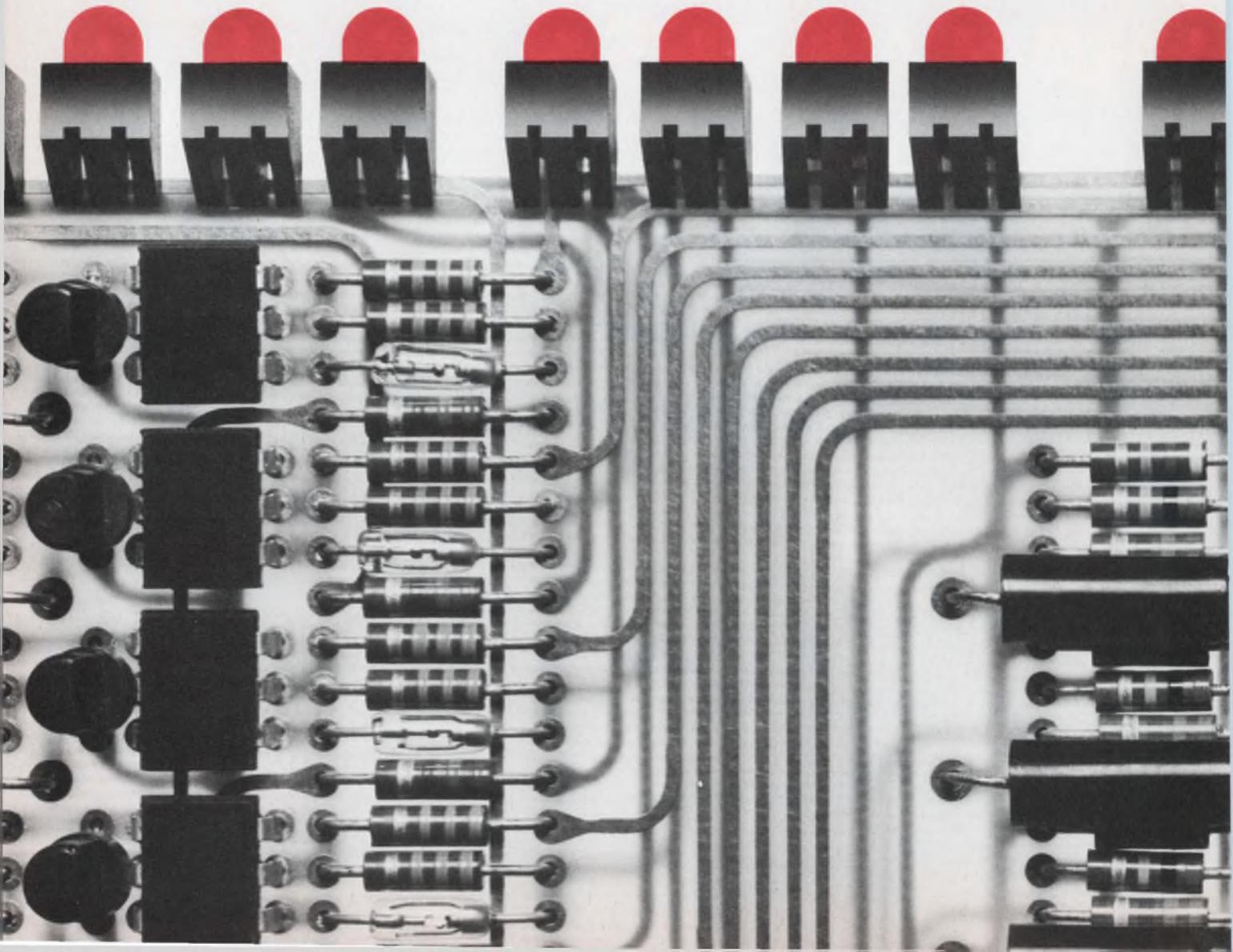
(**Need:** Find a very small fault in a very large system.)

See Dialight.

All printed-circuit boards need a fault indicator; that's why Dialight has developed such a broad family. These tiny LED devices signal where and when a fault occurs in a complex electronic circuit — and this can reduce downtime to a minimum. With some Dialight fault indicators, you can get as many as 10 units in just 1" of space. These devices, which come in a variety of sizes, are designed to operate from 1.6 to 14 volts and are available with both axial and right angle leads. They



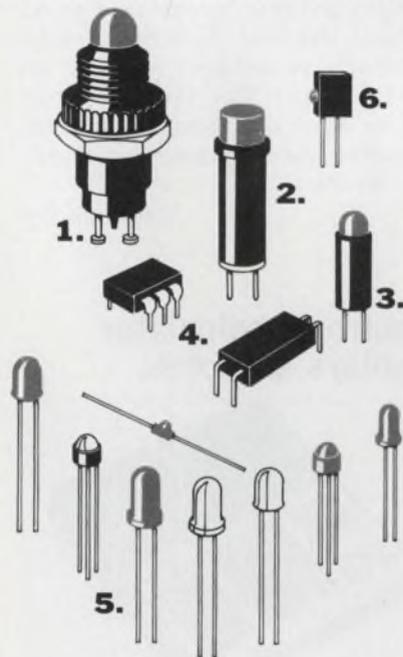
can be driven directly from DTL or TTL logic and can also serve as logic-state indicators, binary data displays, or just as indicators, as in this p-c board furnished by Struthers-Dunn, Inc.* But Dialight's fault finders are only a small part of their fast growing family of light-emitting diodes. Additional opto-electronic devices are extensively used in cartridges, lighted push-button switches, optoisolators, and readouts, all supplied by Dialight. A wide variety of discrete LEDs further adds to the broad family.



Dialight is a company that looks for needs . . . and develops solutions. That's why we developed the industry's broadest line of switches, indicator lights and readouts using LEDs. No other company offers you one-stop shopping in all these product areas. And no one has more experience in the visual display field. Dialight can help you do more with them. Talk to the specialists at Dialight first. You won't have to talk to anyone else. We can help you do more with LEDs than anyone else because we've done more with them.

Here are a few products in this family: **1.** Ultra-miniature indicator lights **2.** Datalamp cartridges **3.** Bi-pin LED lamp **4.** Opto-isolators **5.** LED solid state lamps **6.** Logic state fault indicators

*Used in their VIP Programmable Controller



Please send data on your LED products.

NAME _____

TITLE _____

COMPANY _____

ADDRESS _____

CITY _____ STATE _____

DIALIGHT

Dialight Corporation, A North American Philips Company
60 Stewart Avenue, Brooklyn, N.Y. 11237 (212) 497-7600

DATA PROCESSING

Disc drive uses head-per-track access

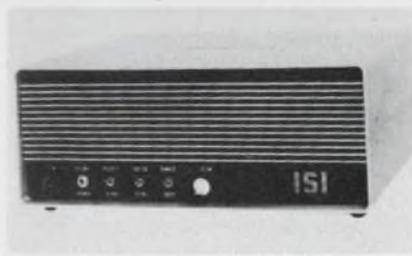


Dataflux, 1195 E. Arques Ave., Sunnyvale, Calif. 94086. (408) 732-7070. \$1200 to \$2500; 30 days.

Model 914 series disc-cartridge drives use a fixed head-per-track to access data. Storage capacities range from 0.5 to 8 Mbits using modules of 16 tracks. Rotation speeds of 1800, 2400 and 3600 rev/min result in average access times of 17, 12.5 and 8.5, ms, respectively. The number of sectors per track is variable from 0 to 2400. The data cartridges are removable. Prices range from \$1200 to \$2500 depending on storage requirements.

CIRCLE NO. 275

Voice response system has proper enunciation



Instrument Systems, Inc., 540 Easy St., Garland, Tex. 75042. (214) 272-8556. \$1295; 90 days.

Devices having parallel BCD with positive true logic can have their readings announced by this digital-to-voice converter. Designated the DIGIVOX, this low-cost unit communicates in proper cadence with a voice drop at the end of each phrase. Applications for the unit include laboratory instrumentation, medical reporting, business information systems and transportation announcement systems.

CIRCLE NO. 276

Plug-compatible line printer fits most minis



Digital Associates Corp., 1031 Post Rd., Darien, Conn. 06820. (203) 655-2222. Lease—\$279/mo.

Without hardware or software modification to the minicomputer, Model V-132-C can print at 600 lines/min with a width of 132 columns. It can be equipped for use with PDP-8, PDP-11, PDP-12, Data General Nova, Varian 620 and most other minicomputers. Installation and complete maintenance are available through Digital Associates nationwide and in Canada. The unit can also be purchased instead of leased.

CIRCLE NO. 277

Improved performance disc drive announced

Ampex Corp., 13031 W. Jefferson Blvd., Marina del Rey, Calif. 90291. (213) 821-8933. \$25,000; 90 days.

Model DM-330 disc drive is said to decrease access time by an average of 2 ms over that of the IBM Model 3330 which it is designed to replace. Other claims for this model include 15% lower price and 1/3 less volume as compared with the Model 3330. Up to 16 Ampex drives, storing 100-million bytes of data each, can be linked with controllers on IBM-370 computers without hardware or software modifications. All units, including those packaged for OEMs, have regulated power supplies and TTL circuitry.

CIRCLE NO. 278

X-Y plotter operates without software



Valtec Corp., 17751 Sky Park Circle, Suite G, Irvine, Calif. 92707. (714) 540-9591. \$3600; stock.

The use of internal logic is said to eliminate the need for supporting software at the computer source. Operation is therefore independent of the service or language used. Model 2024/121 is plug compatible with all TTY/RS232 devices, operates at 10, 15 or 30 characters/s., can use ASCII or EBCDIC data and may be operated on or off-line. Optional features include automatic paper feed and use of fan-fold paper. The fan-fold paper can be advanced from an internal magazine under program or operator control.

CIRCLE NO. 279

Electronic calculator displays subtotals



Casio, Inc., 1 World Trade Ctr., New York, N.Y. 10048. (212) 432-9230. See text.

Model 101-S is a 10-digit electronic calculator which can give accumulations at the same time as individual results of multiplication. This is done simply by pressing the appropriate memory key. The unit is intended to retail at a price of \$225.

CIRCLE NO. 280

Decision: Assume you need an alterable, non-volatile memory in your system, what choices do you have *right now*? And at what *true* and *complete* cost-per-bit?

Cores and plated wire—patchboards—diode arrays? Fine. Providing you need lots of memory—and you're not concerned about size, bulk and speed. Or power consumption. Or compatibility with existing and future logic forms. Or the additional cost of power-fail detection circuitry, or retrieval software and reload hardware—and the like.

Let's talk

Cost-per-Bit

Semiconductor memories? If you go with RAMs your bit cost per se may be lower. But you'll have to consider the extra cost of providing an uninterruptible power source. Or power-fail detection circuitry and battery back-up. Or retrieval software and reload hardware. Just to compensate for their inherent volatility.

If you consider ROMs—either the fixed or one-shot programmable variety—your cost-per-bit for memory alone could be even lower. Until you start adding up all the extra peripheral costs involved in trying to overcome their inherent unalterability. Simulation systems. Special masks and programmers. Surplus capacity for unused future options. Not to mention multiple spare parts inventories, field retrofits, obsolete stock, and spoilage due to errors.

So where do you go from there? Take a good look at RMMs!

AMORPHOUS RMM

ALTERABLE / NON-VOLATILE SEMICONDUCTOR MEMORIES

They're the only *inherently* non-volatile, *fully* electrically alterable semiconductor memories in production—*now!* You can use them just like any other hard-wired memory elements—but without having to buy and build a bunch of superfluous circuitry into your system just to protect stored data or correct program errors.

In fact, you can take Ovonic RMMs completely out of your system—for days, weeks, years at a time—without loss of data. And you can also change, up-date and re-alter stored information at will. Quickly, selectively and *repeatedly*—by simple electrical means.

Easy to apply, too. Standard packages. TTL/DTL compatible. Compatible with each other. Which means you can mix or intermix them any way you like to create flexible, expandable memory systems to meet present and future needs—*exactly!*

Cost-per-bit? Still a bit more than RAMs or ROMs on a straight device comparison basis.

But considering the fact that bit cost is the *only* cost with RMMs, you'll find they're worth it! Important, too: RMM costs have dropped dramatically in the past 18 months and haven't reached bottom yet. So if you start using them now, your true bit costs will be a lot less by the time you hit volume production.

Call or write for complete information today!

Energy Conversion Devices, Inc.

1675 WEST MAPLE ROAD • TROY, MICHIGAN 48064
TELEPHONE 313/549-7300



PUT THE BUGS BACK IN YOUR CIRCUITS...



...WITH A FREE LADY BUG FROM ADC!

If you've been thinking that most commercial transformers are pretty much alike, these new ADC Lady Bugs will change your mind.

We've engineered Lady Bugs to provide the kind of reliability you've come to associate only with transformers meeting military specifications. More than that, we've made sure these ADC Transformers offer something you haven't seen in a while: economy. So, beginning now, you can have the transformer performance you've always wanted, and still keep costs in line.

ADC Lady Bugs come in 46 different electrical configurations with power ratings from 50 mw to 2 watts. There are four different case sizes, with the smallest being approximately one-third cubic inch.

We don't want to bug you, but if you have a real need for miniature transformers, we will send you an evaluation sample free — no strings attached. Just tell us what your requirements are on the coupon and send it back to us. Or, if you just want more information, please circle the number on the Reader Service card.

ADC PRODUCTS

4900 West 78th Street
Minneapolis, Minnesota 55435

Yes, I would like an evaluation sample of the new Lady Bug transformer. Here's my application: _____

We anticipate using _____ units/year.
My needs are for _____ 30 days
_____ 60-120 days _____ Future

Division of Magnetic Controls Company
4900 West 78th Street
Minneapolis, Minnesota 55435
TEL: (612) 835-6800 TWX: 910-576-2832 TELEX: 29-0321

NAME _____

COMPANY _____

ADDRESS _____

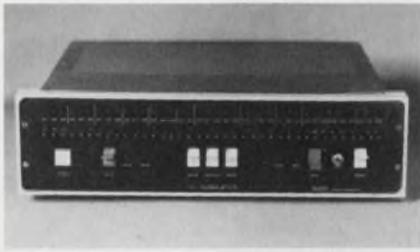
CITY _____ STATE _____ ZIP _____

TELEPHONE _____



DATA PROCESSING

Simulator helps debug peripheral hardware

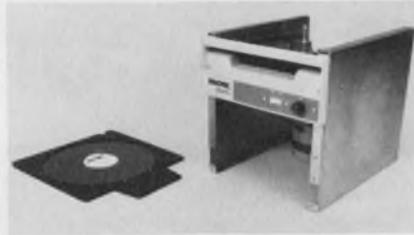


Teletron Co., 40 Elliott St., Melrose, Mass. 02176. (617) 665-5837.

The electrical and timing interface of the Model 11 simulator is identical to that of the PDP-11's Unibus. Any external device may be addressed, interrogated or written into under manual control thereby saving the time and labor of writing equivalent test programs. Proper operation of external interrupt and direct memory access (DMA) logic can be verified. The unit can apply stimuli to external devices along with suitable signals for synchronizing oscilloscope traces with the measured events.

CIRCLE NO. 281

Floppy disc has rectangular shape

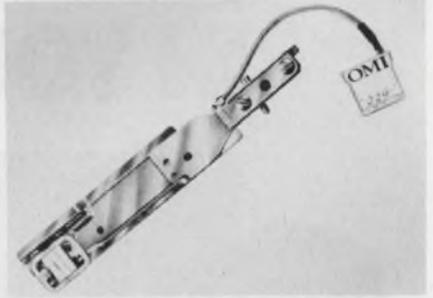


Innovex Corp., 4 Alfred Circle, Bedford, Mass. 01730. (617) 275-2110. \$990; mid-January.

Designated a "Diskette," this "floppy-disc" memory system boasts a 5- ms track-to-track access time and a bit transfer rate of 105 kbits/s.—all for the price of \$990. In operation, the disc remains stationary while the read/write head spins at 400 revs/min. The tape cartridge is a sheet of computer grade magnetic tape stretched on a 9 by 11 by 0.025 in. plastic frame. One-million bits of information are stored on 64 circular tracks. There is a 25 ms head settling time in addition to the 5 ms access time. The cartridges sell for \$7 each in large quantities.

CIRCLE NO. 300

Disc-drive flying head allows 500 tracks/in.



OMI Memories, Inc., 5621 W. Imperial Hwy., Los Angeles, Calif. 90045. (213) 641-7100. 2 weeks.

Over 500 tracks/in. with densities greater than 4000 bits/in. can be recorded by the model IX-150 flying head. The heads have track widths of 0.0015 ± 0.0001 in., and are designed to operate at 3600 rev./min. Recording densities to 2×10^6 bits/in. can be achieved. The heads are designed to fly approximately 45 microinches above the disc surface. Mounting configuration is compatible with standard 3330-type heads. Evaluation samples are available for delivery in two weeks.

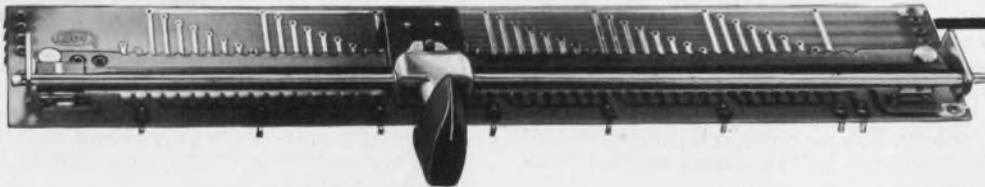
CIRCLE NO. 301



Beautiful
New Babies

BOTH TRULY REMARKABLE

CDI's New Baby: Series SL, Linear Slide Switch (Pat. Pending)



REMARKABLE BECAUSE:

- 1 Up to 100 or more positions (unique).
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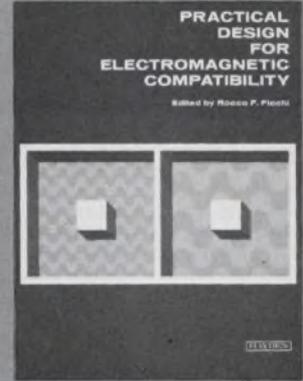
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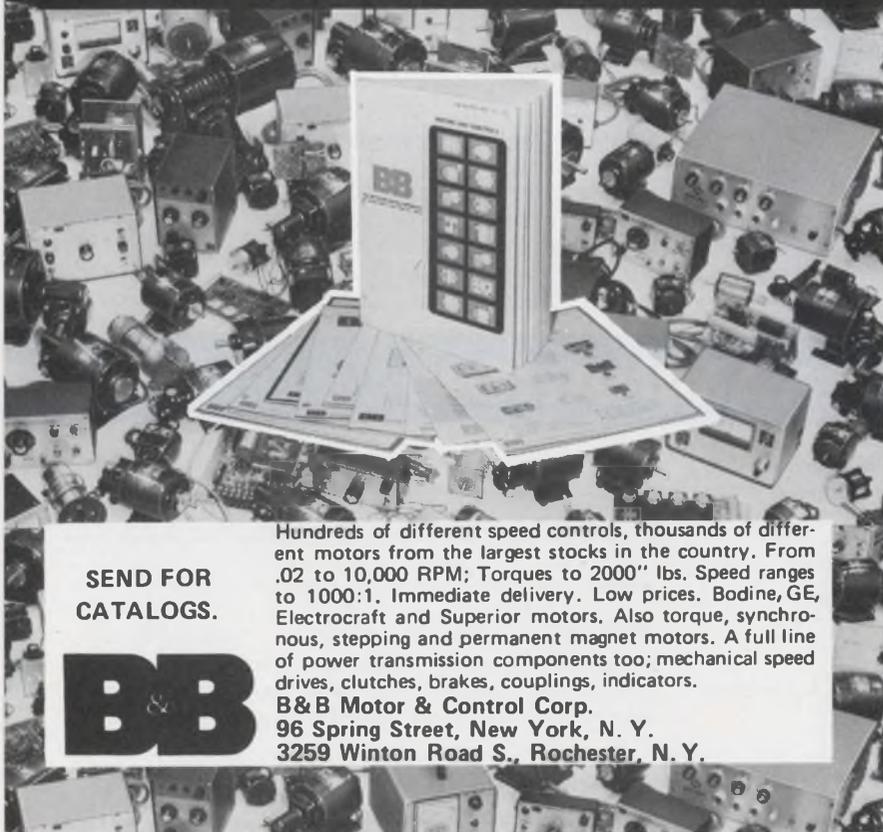
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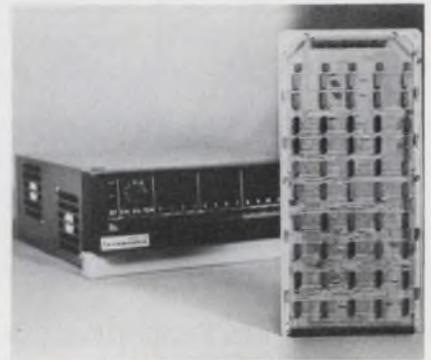
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DATA PROCESSING

Unit acts as watchdog for program errors



Interdata, 2 Crescent Pl., Oceanport, N.J. 07757. (201) 229-4040. \$600; April, 1973.

The entire unit consisting of controller, watchdog timer and from one to 16 nonvolatile 128-byte storage modules is contained on one 7 by 15 in. PC board. It is designed as an optional accessory for all of the company's "New Series" minicomputers. In operation the unit must be excited periodically by a software-generated output prior to a preset strappable timeout. If a program malfunction results in a failure to signal the unit before the set timeout (16 to 256 ms) then an automatic program reload will be performed from the 128-byte storage modules.

CIRCLE NO. 302

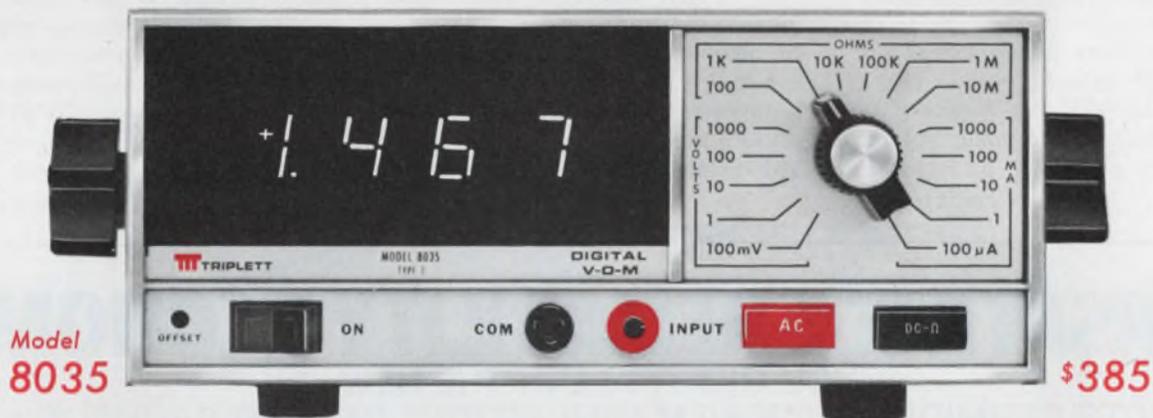
Fault analysis added to CAD software

Softech, Inc., 391 Totten Pond Rd., Waltham, Mass. 02154. (617) 890-6900.

Performance degradation of electronic circuits in the presence of short circuits or open circuits can now be analyzed with Softech's propriety CAD program, AEDCAP. Users implement the fault analysis capability by incorporating test points in the circuit description. Such points will have two values; one representing a component failure and the other effectively removing the test point from the circuit. An arbitrary number of faults may be analyzed either one at a time or in any desired combination.

CIRCLE NO. 303

If you need
 a high quality **3½-digit**
 V-O-M at your price . . .
 buy **Triplett's** new **8035**



1. **EASY OPERATION** — Single polarized plug for test leads eliminates switching leads when changing functions.
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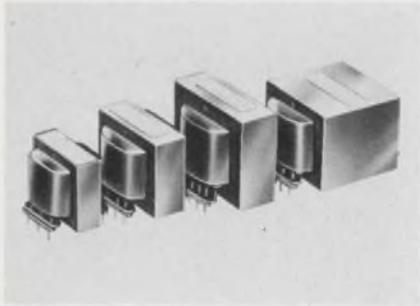
With 26 ranges, the Model 8035 boasts accuracies from $\pm 0.1\%$ to $\pm 0.7\%$ of reading ± 1 digit . . . ranking it among the best on the market. Its green, polarized window and its single-plane, seven-bar, fluorescent display combine to insure bright, reflection-free readability from virtually any viewing angle.

Hardware for rack mounting is available. See the **Model 8035**, priced at **\$385**, at your local distributor. For more information, or for a free demonstration of the convenience and accuracy of the 8035, call him or your Triplett representative. Triplett Corporation, Bluffton, Ohio 45817.

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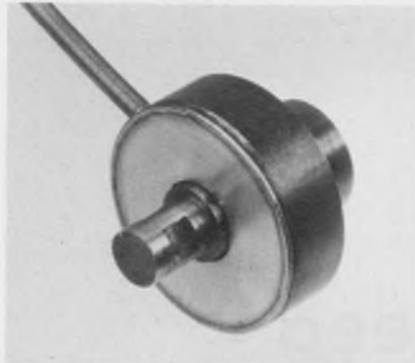


Signal Transformer Co., Inc., 1 Junius St., Brooklyn, N.Y. 11212. (212) 498-5111. Stock.

Signal's complete line of miniature plug-in power transformers run in sizes from 1 to 24 VA. They are made specifically for PC applications and are available in open-frame or epoxy-molded versions. These miniature transformers are offered with either a single 115 V or dual 115 V/230 V primary. A wide selection of secondary voltage ratings are available.

CIRCLE NO. 304

Small torque sensor has no slip rings



Sensotec Inc., 1400 Holly Ave., Columbus, Ohio 43212. (614) 294-5436.

The "Q" Series torque sensors do not have slip rings. They are connected directly in-line with the source of torque to be measured. And they are claimed to have a very high response rate (not given). Capacities range from 100 to 50,000 oz.-in. and sizes from 3/8 to 1-1/2 in. diameter. An impedance of 350 Ω makes these sensors compatible with all standard bridge type instrumentation.

CIRCLE NO. 305

Piezo accelerometer is self-amplifying



Columbia Research Laboratories, McDade Blvd. & Bullens La., Woodlyn, Pa. 19094. (215) 532-9464. \$300 to \$375; stock to 3 wks.

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CIRCLE NO. 306

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Analog Devices, Inc., Norwood, Mass. 02062.

*All prices are the 100-piece price.

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for everything you need to know about 5 volt DC powered DPM's.

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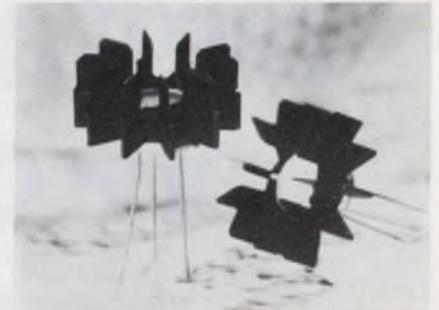
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INFORMATION RETRIEVAL NUMBER 72

COMPONENTS

Infrared sensor can respond to microwaves



The Harshaw Chemical Co., Div. of Kewanee Oil Co., 1945 E. 97th St., Cleveland, Ohio 44106. (216) 721-8300. \$95.

Harshaw's PY5 and PY6 Pyroelectric SBN infrared sensors provide a flat response from 1 to 11 μm for incident radiation intensities to 100 W/cm². The sensors are protected by a T-12 infrared window to keep them clean and eliminate output fluctuations caused by air convection currents. For spectral responses into the far infrared, different window materials can be used. Without a window, the spectral response extends to the microwave region. Rise times of approximately 2 ns can be obtained.

CIRCLE NO. 307

Slide switch provides 100 or more positions



Chicago Dynamic Industries, Inc., 1725 Diversey Blvd., Chicago, Ill. 60614. (312) 943-4600. 4 wks.

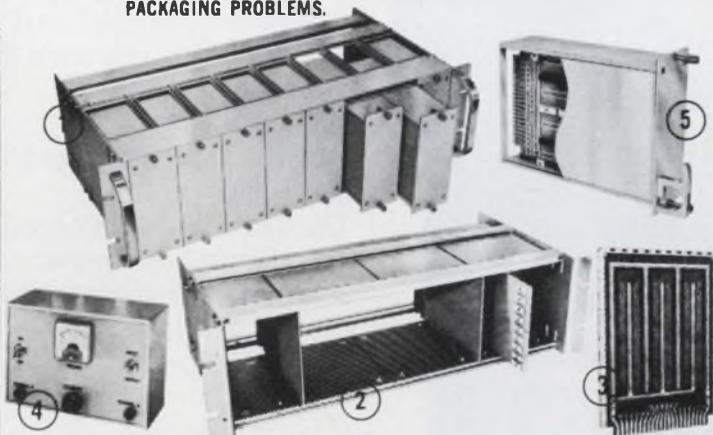
Up to 100 or more positions can be incorporated into the new Series SL single or multiple-pole slide switch. It can be positioned vertically or horizontally. Electrical characteristics include 200 M Ω min. insulation resistance, 1000 V min. dielectric strength and 2 A at 115 V ac current carrying and 125 mA at 115 V ac current breaking capability. Switch life is over 1-million detents. The unit is constructed on a glass-laminate PC board and precious-metal plating and contacts are used.

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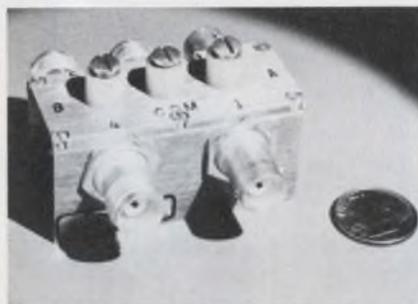


J-Tec Associates, Inc., 317 7th Ave., S.E., Cedar Rapids, Iowa 52401. (319) 366-1843. \$990; stock.

Using an ultrasonic technique, the Model CM 1106-B measures true fluid speed without moving parts. The sensor counts the frequency of the vortex stream formed behind a strut in the fluid flow, and is unaffected by changes in temperature, density, or depth. The frequency at which vortices are shed is directly proportional to the fluid speed. The user has a choice of either a pulse frequency or an analog voltage output.

CIRCLE NO. 309

Coax switch handles 50 W of rf power

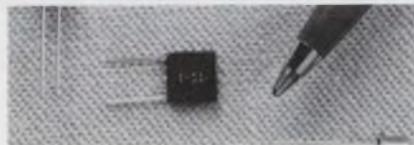


Dow-Key Div., Kilovac Corp., P. O. Box 4422, Santa Barbara, Calif. 93103. (805) 684-4560.

The multifunction coaxial switch, Part Number 209-101B, features two SPDT relays with a common connector in one small package with a basic size of $2 \times 1 \times 7/8$ in. The switch is particularly designed for use in aircraft. It has a nominal characteristic impedance of 50Ω , VSWR of 1.5:1 max at 400 MHz and an insertion loss of 0.5 dB max with 35 dB min isolation. The switch is actuated by a 26 V dc coil and the relay contacts will handle up to 50 W of rf power.

CIRCLE NO. 310

Thermal protection unit uses solid-state sensor

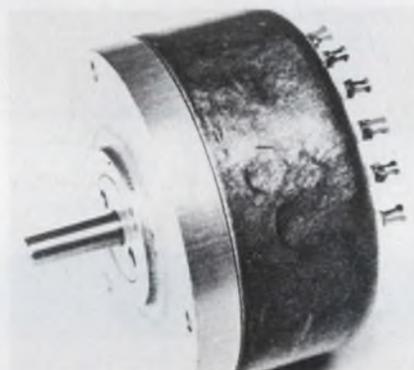


Multi-State Devices, Ltd., 1330 Trans-Canada Hwy., Dorval 740, Quebec, Canada. (514) 683-6331. Under \$1 (OEM qty.).

Multi-State's thermal switches for protecting circuits against overheating, cutoff at 85 C. These units use a solid-state polyconductor sensor and they have no moving contacts. They are said to be a new development for operation at this elevated temperature. Though designed primarily for electronic circuits, these switches can also be used in motor controls and automatically-controlled machines. Two styles are offered, the TS1-80 for surface mounting and the TS3-80 for feed-through mounting.

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Rotary encoder weighs only 2 oz. and is 1-3/8 D



Teledyne Gurley, 514 Fulton St., Troy, N. Y. 12181. (518) 272-6300.

Designated the 8602-69, Teledyne's rotary encoder was designed for the electrical measurement of length, angle, speed, or position in radars, computers and measuring devices. The encoder has an accuracy of three minutes of arc. Its small weight—less than 2 oz.—and its small diameter—1.375 in.—make it suitable for any application where weight and space are critical. It is resistant to shock and vibration. Standard units provide pulse counts over a range from 1 to 1024 counts per revolution.

CIRCLE NO. 452

Switch kit lets you try before you buy

Switchcraft, Inc., 5555 N. Elston Ave., Chicago, Ill. 60630. (312) 792-2700. \$12.50.

A designers' kit for designing dozens of pushbutton (Dual-Visual-Recognition) switches features continuous recognition of in and out switching positions without lamps or indicators. A black color band around the plunger indicates the out position; a brightly colored recognition cap shows when the switch is set to the in position. Kit No. K-133 includes two and four-pole DVR-2000 switch parts, high-current modules (11 A) and a selection of terminals.

CIRCLE NO. 453

Wire-wound resistors available in DIP

Arcidy Associates, 370 Commercial St., Manchester, N.H. 03101. (603) 668-2111. \$3-\$5 (100 up); 3-4 wks.

Series DP-WW resistors are DIP units with up to eight precision wire-wound resistors. They are available with four to 16 pins in a variety of circuit configurations. Values range from 0.1Ω to $200 \text{ k} \Omega$ with tolerances to 0.02%, tolerance matching to 0.01%, temperature coefficients to 5 ppm/°C and temperature coefficients matching to within 2 ppm/°C. They are available in a variety of interconnection patterns or as independent resistors.

CIRCLE NO. 454

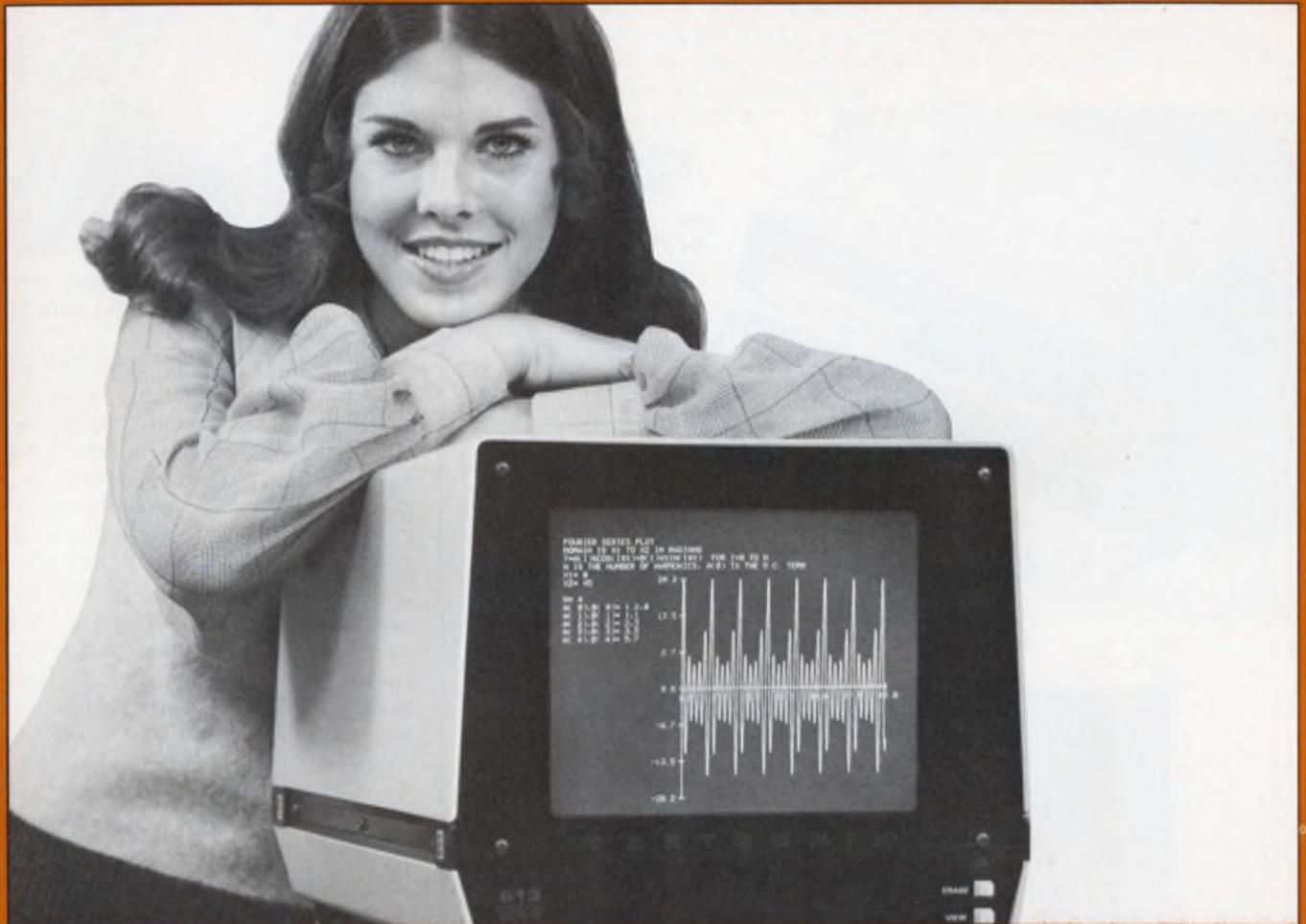
Delay lines to 1000 ns packaged in 16-pin DIP

Data Delay Devices, 253 Crooks Ave., Clifton, N. J. 07011. (201) 772-6820. \$3.50 (OEM qty.) 4 days.

Series 1504, DIP delay lines provide a delay range from 10 to 1000 ns, impedances from 100 to 500Ω with a T_d/T_r ratio of 5/1 in a standard 16-pin case. They can withstand 50 V dc, have a temperature coefficient of 100 ppm/°C and meet or exceed MIL-D-23859C standards.

CIRCLE NO. 455

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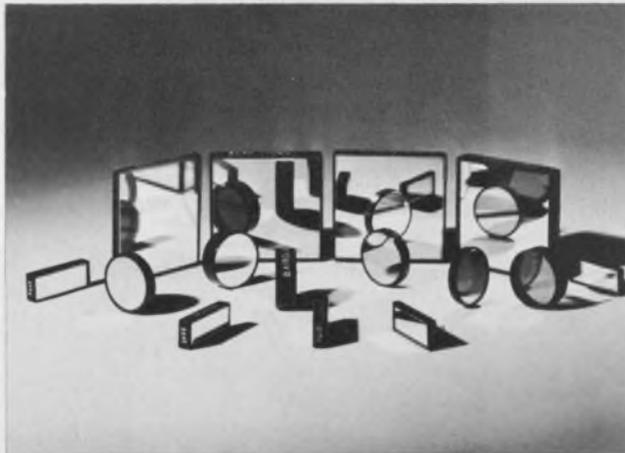


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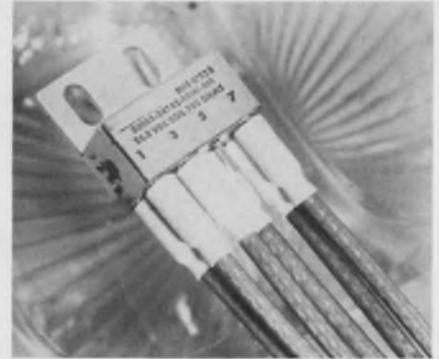
System Components Division

125 Middlesex Turnpike, Bedford, MA 01730
(617) 276-6420 Telex: 92-3491

INFORMATION RETRIEVAL NUMBER 77

COMPONENTS

Rf relay comes with coax leads attached



General Electric, 777 14th St.
N.W., Washington, D. C. 20005.
(202) 393-3600.

Half-size rf relays, Type 3SAV, feature 50-Ω, RG 316U coaxial-cable leads permanently attached for extra-low insertion loss and ease of installation. The relay is designed for transmission lines with 25 to 70-Ω impedance and frequencies under 500 MHz. The main contacts are rated at 100,000 operations to 75 W carrying capacity and 10 W interrupting capacity. Contact resistance is less than 0.050 Ω, operating time is less than 4 ms and coil sensitivities are 260 mW maximum for form D models.

CIRCLE NO. 456

Small magnetic sensor provides high output

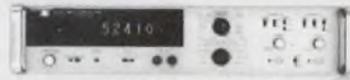
Electro Corp., 1845 57th St., Sarasota, Fla. 33580. (813) 355-8411.

Very compact, Electro's new magnetic sensor has a stainless-steel shell that measures just one inch in over-all length, and it mounts with a 1/4-40 thread. The unit, Model Number 3050, was developed expressly for computer peripheral use in timing and synchronization applications. It supplies a minimum of 12 V peak-to-peak at 1000 in./s with a 20-pitch, 30-tooth gear at 0.005-in. clearance and with a load of 100 kΩ. The sensor's output is stable over a temperature range from -100 to +225 F.

CIRCLE NO. 457

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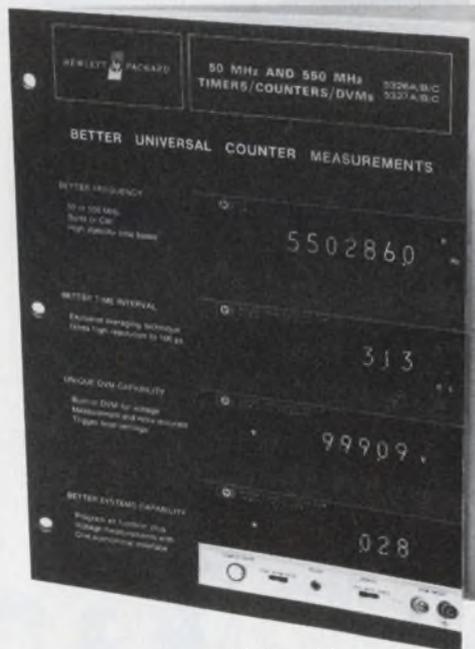
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LED drivers eliminate external resistors

Precision Dynamics Corp. Electronics Div., 3031 Thornton Ave., Burbank, Calif. 91504. (213) 845-7606. \$2.75 to \$3.55 (100-999).

The NOVA 5000 Series current-limiting LED drivers eliminate external resistors in driving seven-segment LED or filament displays. Constant current is delivered by the 20 mA devices as long as output voltage is maintained above 1.25-V dc. This allows single or double diode displays to be driven directly. A built-in quad latch allows displayed information to be held, while data input is either removed or changed. Ripple-blanking logic provides for suppressing of excess zeros. Six separate models come in standard 16-pin DIP.

CIRCLE NO. 458

Compact keyboards offer current-sinking outputs

Micro Switch Div. Honeywell, Inc., 11 W. Spring St., Freeport, Ill. 61032. (815) 232-1122. Stock.

The solid-state 12-key (12SW) and 16-key (16SW) keyboards have current-sinking outputs for compatibility with TTL and DTL. The keyboards permit greater fan out, since each key switch offers two isolated outputs rated at 3.2 mA (outputs may be wired in parallel to sink 6.4 mA). Both keyboards are available with either level or pulsed outputs. The small Hall-effect keyboards have been designed for end-to-end mounting, and have standard 3/4-in. key spacing.

CIRCLE NO. 459

Miniature amplifier inserts into microstrip



Optimax, Inc., P.O. Box 105, Colmar, Pa. 18915. (215) 822-1311. \$75; stock.

The AH-52 is a miniaturized modular amplifier designed for direct insertion into microstrip circuitry. The unit operates from 10 to 500 MHz and has a nominal gain of 14 dB at 16-V dc. A major feature is the high reliability—MTBF of 1.44×10^6 hrs per MIL-HDBK-217A. Other specs include a noise figure of 5 dB and an output power, at 1-dB gain compression of +10 dBm.

CIRCLE NO. 460

Power supplies slip into card cage

Mohawk Industries, Inc., 73 N. Second St., Easton, Pa. 18042. (215) 252-0968. \$86; stock.

Designated as Series 3127, these power supplies slip into a card cage alongside the circuit boards, thus eliminating all of the problems associated with cable routing, installation and noise. Eleven models are available from stock. Specs include: input voltage of 105 to 130 V ac, 50 to 60 Hz; output voltage adjustable and floating from 4.4 to 28.6 V dc; line and load regulation of 0.05%; ripple and noise less than 1.5 mV rms; and tc of 0.01%/°C.

CIRCLE NO. 461

A/d converter features 300-ps aperture time

Inter-Computer Electronics, Inc., Subsidiary of American Electronic Laboratories, Inc., P.O. Box 507, Lansdale, Pa. 19446. (215) 822-2929.

The Model IAD-2208 a/d converter system is designed for wide bandwidth data processing and data acquisition systems. The unit features 300-ps aperture time, eight-bit resolution at conversion rates up to 5 MHz, and an accuracy of $\pm 0.2\%$ of full scale $\pm 1/2$ LSB. The Model IAD-2208 includes sample-and-hold, a/d encoder system timing and decoding, and power supplies. It operates either asynchronously from an internal clock, or synchronously from an external signal source.

CIRCLE NO. 462

4-digit decade counter costs just \$79

Display Electronics, P.O. Box 1044, Littleton, Colo. 80120. (303) 781-7922. \$79; stock to 30 days.

The CM Series modules include a decade counter, latch, decoder-driver, and readout for each digit. Standard modules are available with from two to six digits. All ICs are 7400 series TTL. Minimum counting rate is typically 18 MHz. The modules operate over a temperature range of 0 to 70 C. Lamp test and zero blanking functions are provided. A single 5 V dc power supply is required. The readout tube is a seven-segment, incandescent type with a character nearly 1/2-inch high. A polarizing filter is furnished with each module.

CIRCLE NO. 463

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Crystal oscillator is miniaturized

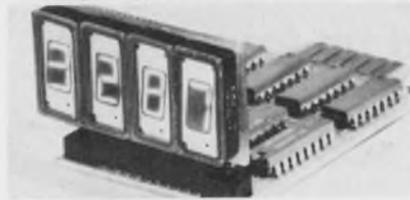


Scientific Research Corp., Sub. of Trak Microwave Corp., 4722 Eisenhower Blvd., Tampa, Fla. 33614. (813) 884-1411. \$350; 6-8 weeks.

The 5044-1006 is a complete crystal-controlled oscillator in a 1.33 x 1.33 x 0.35-inch package. It is said to be the smallest self-contained 920 to 1200-MHz crystal-controlled oscillator on the market today. The unit has a center frequency accuracy of ±0.0005%. Stability is ±0.002% from -40 to +70 C. Nonharmonically related spurs are 45-dB down, with harmonics 30-dB down. Power output is +7 dBm ±1.5 dB into a 50 Ω load. The 5044-1006 mounts on a PC board and requires +15 V at 60 mA.

CIRCLE NO. 464

Counter displays are complete decades



Instrument Displays, Inc., 225 Crescent St., Waltham, Mass. 02154. (617) 894-1577. \$80 ea. (25 four decade units); 2 wks. ARO.

Instrument Displays announces its new series of Counter Displays: a compact assembly of two to six decades in a single unit, with a readout character height of 3/8 inch. The readout uses 8 mA per segment, and has a brightness level of 700 FL at 5 V dc. The unit is available completely packaged, with bezel, filter and housing, or as a separate component. The readouts are mounted on a plug-in card and the entire package for a four-digit unit takes less than 2 in. of panel width, and is 1-3/8-in. high. Input is in TTL form at up to 10 MHz. Reset to 0, and 5 V dc inputs are on a single rear connector.

CIRCLE NO. 465

7-segment LED display offers cost savings



Fairchild Semiconductor Components Group, 464 Ellis St., Mountain View, Calif. 94040. (415) 962-3816. \$3.95 (100s).

The FND-70 1/4-inch-high digits are said to be approximately half the price of other quarter-inch LED displays. The unit uses only one LED per display segment. A molded plastic light pipe converts the spot of light into a uniform bar segment. A "fly's eye" lens (consisting of multiple convex lenses) on the display surface diffuses the light to provide bright displays over a viewing angle of 140°. The 10-lead DIP measures only 0.550 x 0.335-inch. Thus, four digits require no more panel space than three conventional 1/4-inch displays. The FND-70 uses a common cathode and operates at 10 to 25 mA per segment.

CIRCLE NO. 466

Introducing the expensive dual-trace scope that doesn't cost a lot.

The B&K Precision Model 1470.

The compact 5-inch solid-state 1470 is specially designed to meet 80% of all your scope applications.

It has DC to 10 MHz bandwidth with 10 mV/cm sensitivity. Sixteen triggered-sweep speeds range from 1 μsec/cm to 0.2 sec/cm. Triggers on input signals as low as 5mV.

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For more information, contact ADOLF MELLER CO., P.O. Box 6001, Providence, R.I. 02904. Tel: 401-331-3717.



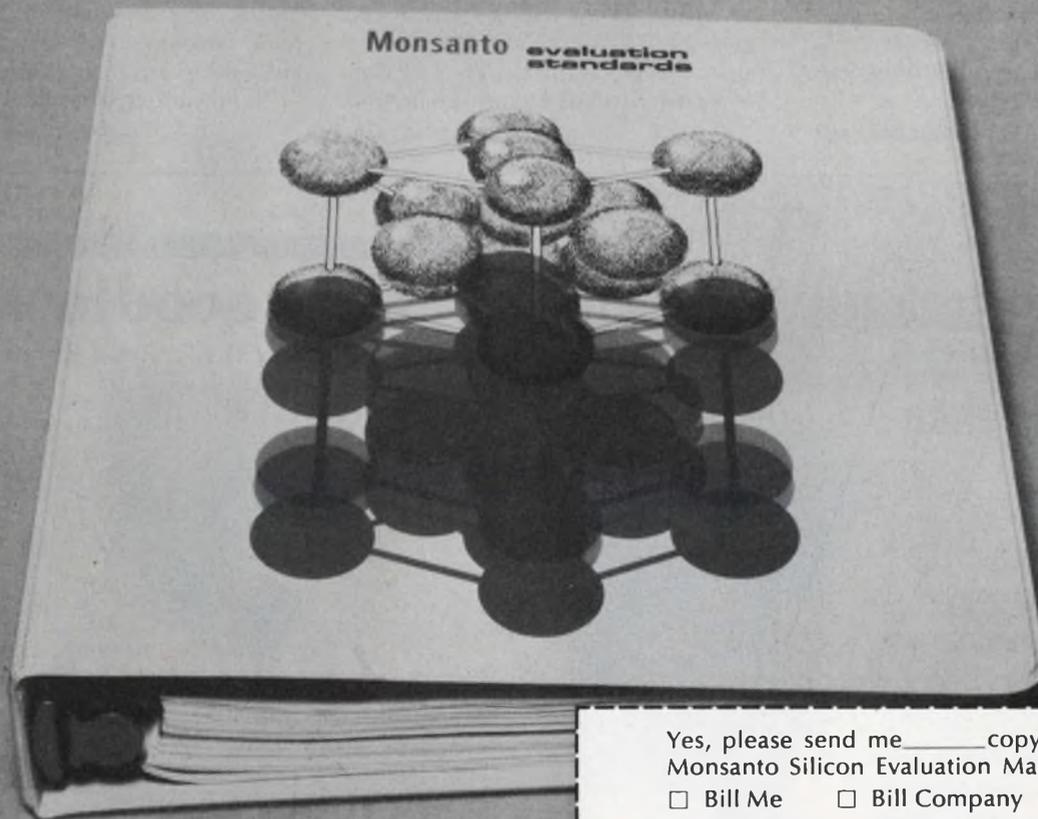
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Module converts synchro to linear output

Transmagnetics, Inc., 210 Adams Blvd., Farmingdale, N. Y. 11735. (516) 293-3100. \$595; stock to 5 wks.

Transmagnetics, Inc., announces the availability of their Series B678 synchro to linear dc converters which are compact solid-state units that convert all standard synchro or resolver inputs to a linear dc voltage proportional to the input shaft angle. Accuracies to ± 6 minutes at 25 C and ± 10 minutes over -55 to $+85$ C are now available. This series offers infinite resolution, does not require adjustment of any kind, is short-circuit proof, is available either for PC-board mounting or connector termination, and all units are fully transformer isolated. All models are hermetically sealed and can be supplied to meet or exceed MIL-E-16400. The units are said to be low profile and lightweight.

CIRCLE NO. 467

Small pulse generator tests CMOS circuits

American Laser Systems, Inc., 3888 State St., Santa Barbara, Calif. 93105. (805) 687-1212. \$125.00; stock.

The Model 727 CMOS-compatible pulse generator offers frequencies from 1 Hz to 1 MHz, and pulse-widths from 1 μ s to 100 ms. Additionally, a level detector, a noncapacitive differentiator, a NOR gate, a D flip-flop, and a pushbutton are provided. Q and \bar{Q} outputs and complementary inputs allow the synthesis of a wide range of digital functions. When powered by the circuit under test compatible test waveforms are assured, eliminating the possibility of damage to CMOS inputs. This makes it ideal for troubleshooting or for use in built-in test equipment. When powered from its own supply (3-15 V), up to 50 mA is available for powering external circuitry. Thus it can be used in design and at the bench.

CIRCLE NO. 468

Seven-segment display interfaces with MOS

Sperry Information Displays, P.O. Box 3579, Scottsdale, Ariz. 85257. (602) 947-8371.

Eight new seven-segment planar gas discharge displays have been added to the company's line. The SP-330 Series (1/3-in.) and SP-350 (1/2-in.) units are for interfacing with MOS/LSI and for use in dc or multiplexed applications, with or without suppressed (blanked) zeros. The units offer improvements over previous displays. A keep-alive cathode provides an internal ion source that reduces reionization time to less than 30 μ s, allows zero suppression and improves operation in dark environments and at low temperatures. The units in both of the series come in 1-1/2, 2, 3, and 2-1/2 digits. The one-half digit in each case consists of plus/minus symbols with an over-range numeral "1" and an extra decimal point.

CIRCLE NO. 469

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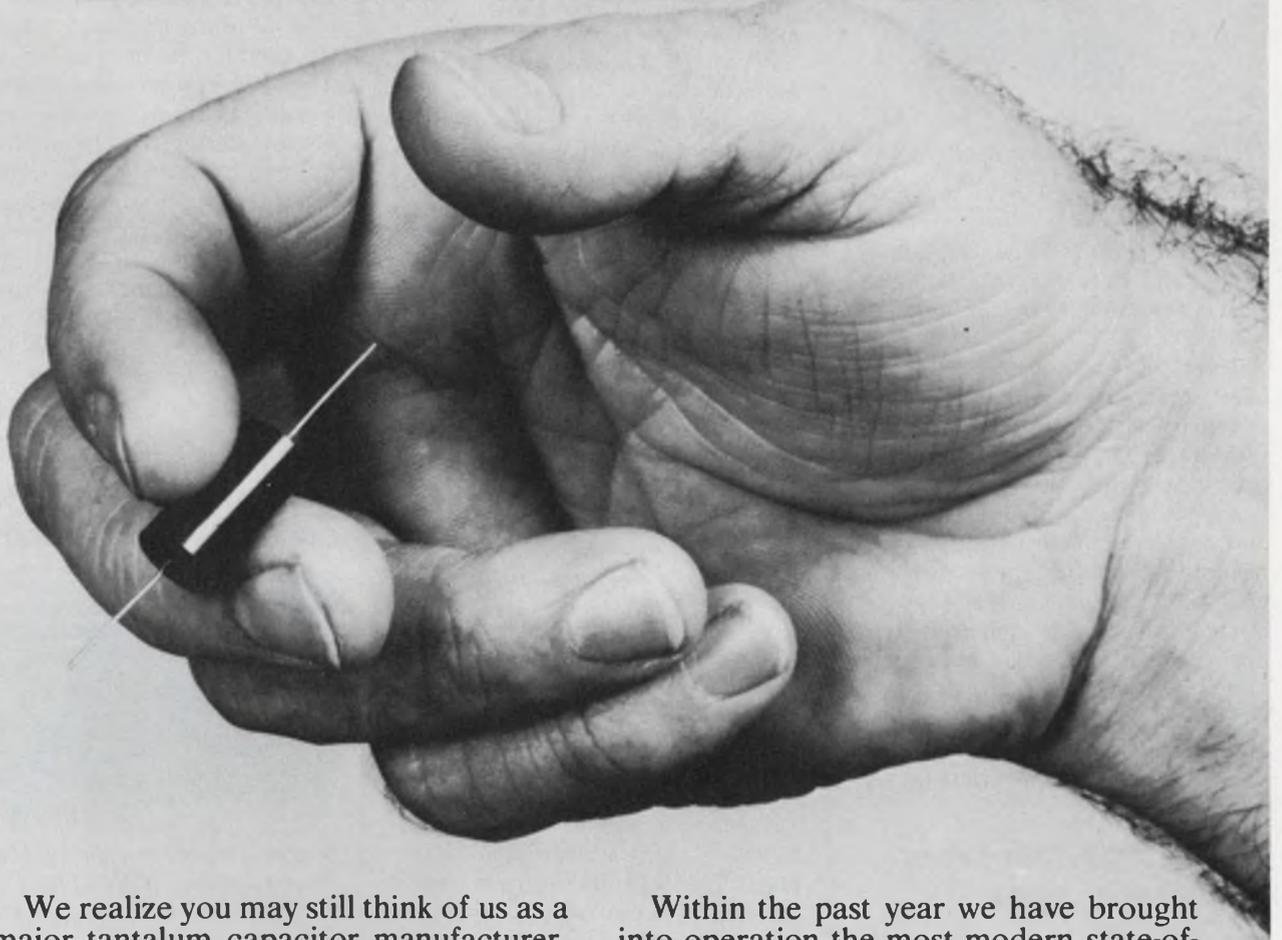
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INFORMATION RETRIEVAL NUMBER 86

ELECTRONIC DESIGN 1, January 4, 1973

INFORMATION RETRIEVAL NUMBER 85

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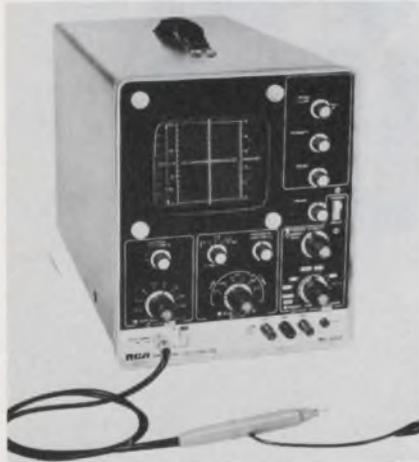
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COMPONENTS DEPARTMENT

Scope gives triggered or recurrent sweep



RCA Distributor Products, 415 S. Fifth St., Harrison, N. J. 07029. (201) 485-3900. \$329 (optional resale price).

This solid-state dual-mode scope offers both triggered or recurrent sweep operation at the touch of a button. In addition to dual-mode operation, the WO-535A has a usable bandwidth of dc to 10 MHz and comes complete with probes at no extra cost. Designed with special features for general purpose, electronic servicing and industrial applications, the scope requires a signal of only 5.9 mV pk-pk for 1-cm of deflection on the high-sensitivity range.

CIRCLE NO. 470

50-MHz counter-timer displays 6 digits

United Systems Corp., Subsidiary of Monsanto, 918 Woodley Rd., Dayton, Ohio 45403. (513) 254-6251. \$695.

A 50-MHz full-function counter-timer, Model 101C, has been released by Monsanto. This new counter features a standard six-digit display, time base stability to one part in 10^6 per day, BCD outputs for system compatibility and a sensitivity of 50 mV rms. Additional features include an adjustable display time with storage, two amplifiers with individual trigger controls and parallel inputs front and rear, and FCC type approval No. 3-174 for frequency monitoring.

CIRCLE NO. 471

Digital panel clock is system oriented



Newport Laboratories, Inc., 630 E. Young St., Santa Ana, Calif. 92705. (714) 549-4914. \$275; 3 wks.

Newport Laboratories has announced a new digital clock especially designed for data acquisition systems. Called the Series 6700, these panel instruments display time-of-day in four models ranging in full scale from 12 hours to 99 days. System BCD outputs are gated and buffered. Time base is derived from 50 or 60-Hz power lines. Two crystal oscillator time base options permit operation in areas where the line frequency is not sufficiently accurate. In the event of power failure, an indicator lights when power returns while the clock display resets to all zeros.

CIRCLE NO. 472

Backplane test system programs itself

Teradyne, Inc., 183 Essex St., Boston, Mass. 02111. (617) 482-2700. \$25,000 up; 12 wks. ARO.

This computer-operated Backplane Test System requires only a two-cable interconnection to the backplane under test. The N151 is self-programming and will record all shorts and opens, in the user's nomenclature, on either a CRT display or a printer. Magnetic-tape cartridges are used for program storage. Operation involves five keyboard commands—to analyze, test, print out a master connection list, store programs in memory, and edit programs. In normal use, a prototype or backplane known to be good is first connected to the system, which automatically "learns" the network. When production backplanes are tested, the system records all wiring errors instantly on the CRT display. Hard copy may also be obtained.

CIRCLE NO. 473

Automatic test system isolates IC faults

Texas Instruments Inc., Digital Systems Div., P.O. Box 1444, Houston, Tex. 77001. (713) 494-5115. \$50,000 and up.

The ATS-960 is a computer-controlled system for testing of ICs and PC boards. The system is intended for those who test a diversity of production modules: It tests digital, analog and hybrid circuits, and provides automatic fault isolation to pinpoint faulty components in complex electronic assemblies. The new system uses English language programs. Production tests on new designs can be implemented by merely writing a new program. Operating in a timesharing mode, the system can perform production testing of up to four different kinds of assemblies at the same time. The test system instructs the operator each step of the way via its display screen.

CIRCLE NO. 474

DPM features 0.05% accuracy, 3-1/2 digits



Gralex Industries, 155 Marine St., Farmingdale, N.Y. 11735. (516) 694-3607. From \$95; stock to 2 wks.

The Gralex Model 36 bipolar 3-1/2-digit DPM features 0.05% accuracy with negligible warmup time, 50 ppm/°C stability over a 0 to +50 C operating range, and a full one-year warranty. Offered in two autopolar ranges (± 1.999 V or ± 199.9 mV, F.S.), the Model 36 has a floating differential input which provides $> 1000\text{-M}\Omega$ input impedance and $> 70\text{-dB}$ CMR. The Model 36 features a choice of seven-segment planar or Nixie display, with 1/2-in. numerals. Autopolarity, automatic blanking, and programmable decimal points are included at no extra cost. BCD outputs are standard.

CIRCLE NO. 475

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INFORMATION RETRIEVAL NUMBER 89

Data generators zip along at 300 MB/s



Tau-Tron, Inc., 685 Lawrence St., Lowell, Mass. 01852. (617) 458-6871. From \$4365. 2-4 weeks.

The two members of the DG-525 series are said to be the world's fastest programmable data generators: They operate from one bit/s to over 300 MB/s. They produce serial bit streams of 16 and 32 bits per word, and you can increase that word size to 64 bits with DG-525 options. Serial data stream is NRZ or RZ format. Output signals feature 1-V amplitude (or ECL), and up to ± 1 -V dc offset. Rise and fall times are 0.8 ns. The units are operated with an external clock signal, either sine wave or pulse.

CIRCLE NO. 476

Spectrum analyzer spans vhf band, is portable



Systron Donner Microwave Div., 14844 Oxnard St., Van Nuys, Calif. 91409. (213) 786-1760. \$4250; 60 days ARO.

The Model 750 is a portable spectrum analyzer specifically for vhf use. It covers the frequency range up to 480 MHz in a single band. The entire band can be scanned in one sweep for panoramic evaluation of all signals in the vhf range. Low frequency operation extends down to 1 MHz. A 500-MHz low-pass filter is included at the input. The Model 750 is fully portable, capable of operating up to eight hours from an optional internal rechargeable battery pack. Also available is an option to operate from an external 14 to 20 volt unregulated dc power source.

CIRCLE NO. 477

4-1/2-digit DMM sells for \$495



Data Technology Corp., 2700 S. Fairview St., Santa Ana, Calif. 92704. (714) 546-7160. \$495.

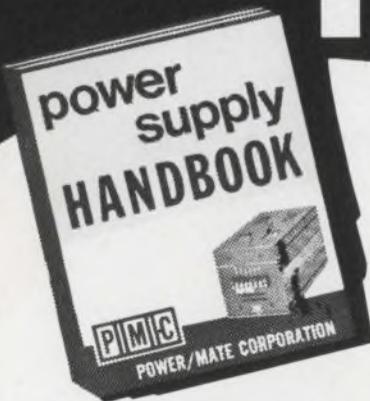
The Model 40 4-1/2-digit multi-meter provides fourteen ac, dc and ohms ranges with 0.02% and 0.03% accuracy. The instrument's dc measuring speed is 0.2 s and ac and ohm speed is 2 s and 500 ms, respectively. The fully-guarded DMM has 50 to 60-dB NMR and 90 to 100-dB CMR. Resolution is 10 μ V. A 1200-V overload, ac or dc, on any range prevents damage under all but the most severe conditions. Input impedance for ac is 1 M Ω , shunted by 50 pF. Dc input resistance is 10⁸ Ω .

CIRCLE NO. 478

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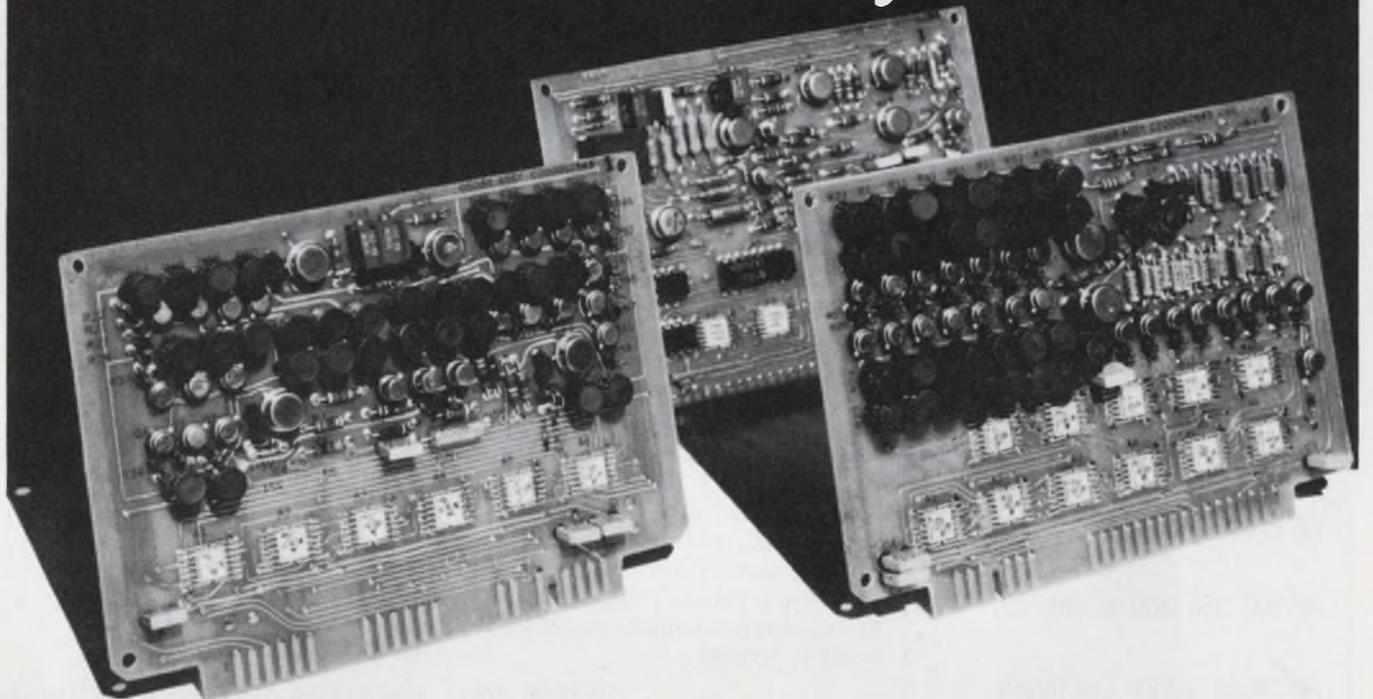
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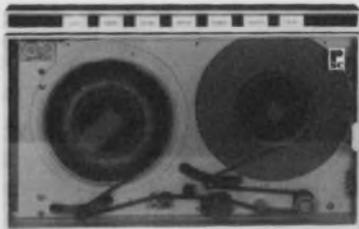
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INSTRUMENTATION

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Electronic Development Corp., 11 Hamlin St., Boston, Mass. 02127. (617) 268-9696. \$820; stock.

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CIRCLE NO. 479

2-1/2-digit DMM kit costs just \$79.95

Heath Company, Benton Harbor, Mich. 49022. (616) 983-3961. \$79.95 (mail order).

The IM-1202 is a 2-1/2-digit Multimeter kit. A cold-cathode readout ends parallax and interpolation errors. Accuracy is within 1% on dc volts, 1-1/2% on ac volts and ac/dc current, 2% on ohms. The 29 selectable ranges measure voltages from 10 mV to 1000 V on dc, either polarity; 10 mV to 700 V rms on ac; 10 μA to 2 A on ac or dc current, and 1 Ω to 2 M Ω on resistance. In addition, there are lighted indicators for overrange, positive and negative dc voltages and current, and a handy front-panel polarity switch.

CIRCLE NO. 480

2-channel recorder has plug-in-preamps



Recorder Systems Div., Gulton Industries, Inc., Gulton Industrial Park, E. Greenwich, R. I. 02818. (401) 884-6800.

The Techni-Rite TR-222 portable two-channel recorder accepts interchangeable plug-in preamps, weighs less than 30 lbs. and has electrically-selectable chart speeds of 0.5, 1, 2.5, 5, 10, 20, 50 and 100 mm/sec. Frequency response is dc to 30 Hz at 50 chart divisions and dc to 100 Hz (-3 dB) at eight divisions. Each channel is 50-mm wide. Preamps with gains of 10 mV/div. to 20 $\mu\text{V}/\text{div.}$ are offered as well as preamps that convert transducer signals. Time to change any preamp is approximately 10 seconds.

CIRCLE NO. 481

Spectrum analyzer is portable

Quan Tech, Div. of KMS Industries, Inc., 43 S. Jefferson Rd., Whippany, N.J. 07981. (201) 887-5508. \$3875.

Model 306 TDL is a tracking wave and spectrum analyzer with a frequency range of 10 Hz to 50 kHz and bandwidths of 10, 30, 100, 300 and 1000 Hz. The instrument is equipped for instant conversion to a 12-V dc source. Automatic tracking enables the unit to lock onto and track a signal whose frequency varies over narrow or wide limits. No external pilot or reference frequency is required. A 5-digit readout enables the operator to determine the frequency of the tracked signal or, in manual operation, the frequency to which the analyzer is tuned. The instrument has a dynamic amplitude range of up to 90 dB in the logarithmic mode and $> 70 \text{ dB}$ in linear operation.

CIRCLE NO. 482



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Data Precision's new, laboratory-quality Model 245 4½-digit multimeter puts .005% resolution right in the palm of your hand. The one and a quarter pound, pocket-size Model 245 measures DC volts, AC volts, DC current, AC current and resistance with 100% overranging. It operates on its own rechargeable 6-hour NiCd battery pack and on AC line. Supplied with battery pack, carrying case, charger and probes, its complete price is \$295. An outstanding example of what Data Precision considers good engineering — years ahead.

The 2500 Series 5½-digit DMMs provide a basic accuracy for 6 months of $\pm 0.001\%$ f.s. $\pm 0.007\%$ reading ± 1 l.s.d. Priced from \$995. The 2400 Series 4½-digit DMMs have a basic accuracy, 6 months, $\pm 0.007\%$ reading ± 1 l.s.d. Priced from \$580. Functions include DC volts, AC volts, resistance and DC ratio. Standard features include autoranging and 20% overrange; remote triggering and ranging; true differential floating circuit input; isolated BCD outputs and automatic zero stability.

All multimeters are documented by full test data and Certificate of Conformance. For complete information, specifications and copies of technical papers outlining the design features, write or call Data Precision Corporation, Audubon Road, Wakefield, Massachusetts 01880. Phone: (617) 246-1600.

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Fiber optic scanner detects 1-mil targets

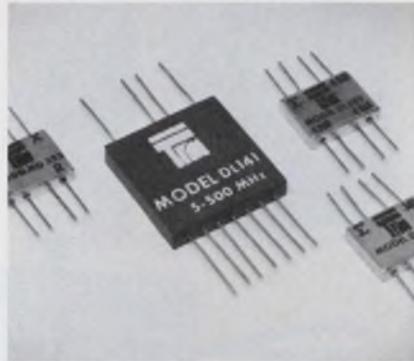


Skan-a-Matic Corp., P.O. Box S, Elbridge, N.Y. 13060. (315) 689-3986.

The S3010-3B Mini-Skanner, a fiber optic scanner, can detect a target as small as 1 mil in diameter. The tubular device has a minimum field of view of 10 mils in diameter, which enables it to differentiate between 10-mil wide lines spaced 10 mils apart. Repeatability of object positions of ± 0.1 mil is possible.

CIRCLE NO. 483

Flat-packs good for microstrips and plug-ins



Technical Research and Manufacturing, Inc., Grenier Field, RFD #3, Manchester, N.H. 03103. (603) 668-0120, \$18 (1-4); stock to 4 wks.

Two-way, 3-way and 4-way power dividers and DBM mixers are available in miniature case sizes as small as $1/2 \times 3/8 \times 1/8$ inches with frequency coverage from 0.2 to 500 MHz. Other features include characteristic impedance of 50 Ω , VSWR of 1.3:1, loss of 0.5 dB (max) and isolation of 30 dB (typ).

CIRCLE NO. 484

Thin film, wideband amps come in DIPs



Avantek, Inc., 2981 Copper Rd., Santa Clara, Calif. 95051. (408) 739-6170. From \$550 (small qty).

Two series of thin film, wideband, low noise amplifiers, designated the UDP-2032 and UDP-4000 Series, feature dual-in-line packaging. The devices cover the frequency ranges of 1 to 2 GHz and 2 to 4 GHz, respectively. The devices provide a minimum of 24 dB gain at 1 to 2 GHz (UDP-2032) and over 10 mW (+11 dBm) linear output power from UDP-4003. Units within a series can be cascaded to boost gain without affecting bandpass characteristics.

CIRCLE NO. 485

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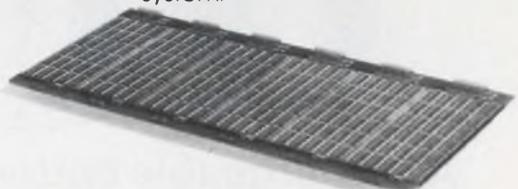
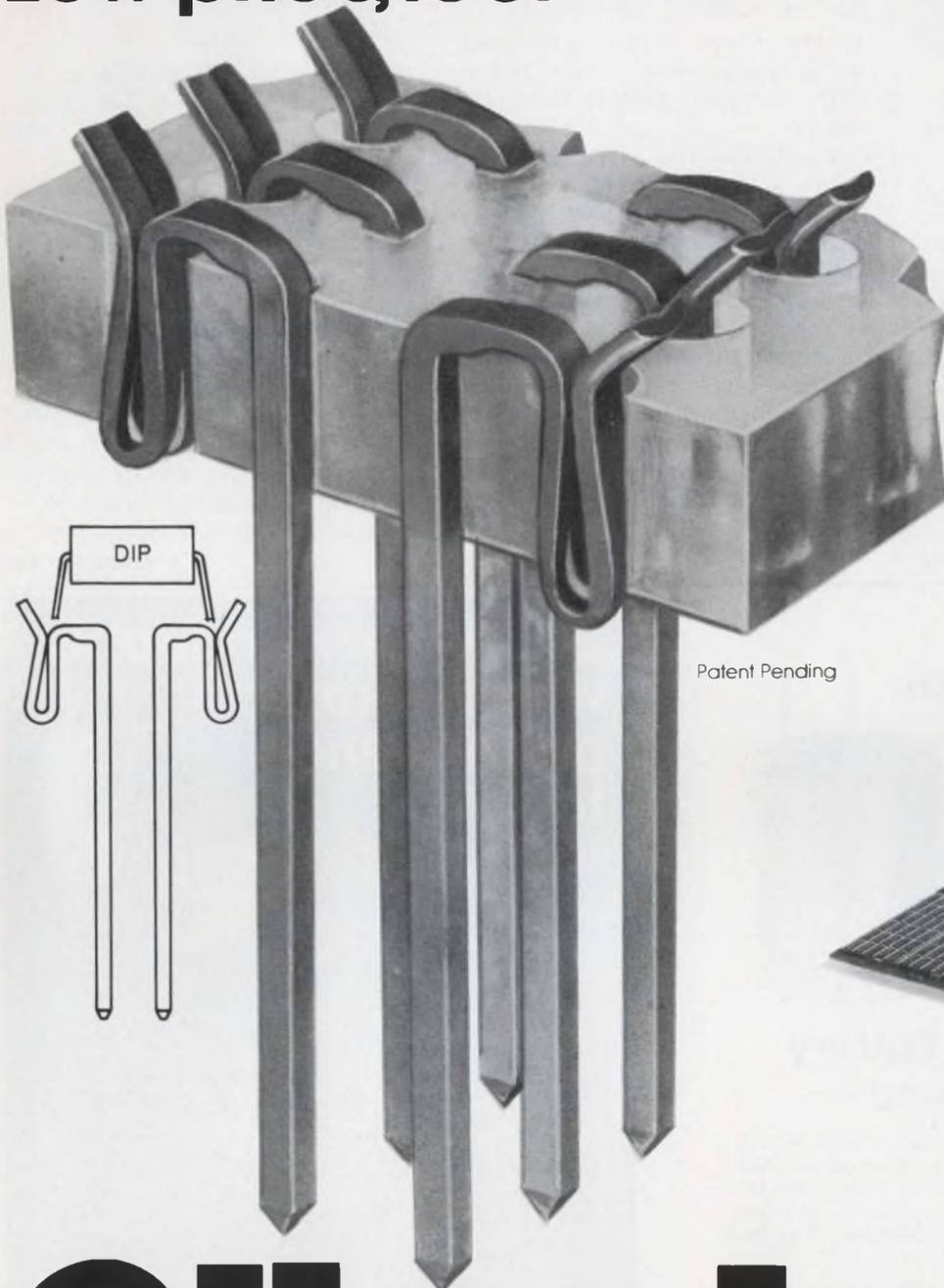
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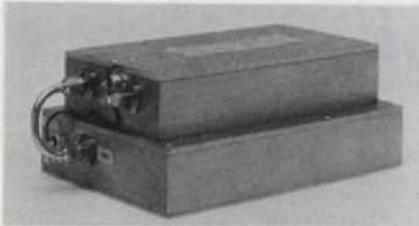
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INFORMATION RETRIEVAL NUMBER 97

Linear Class A amp covers 1-2 GHz range

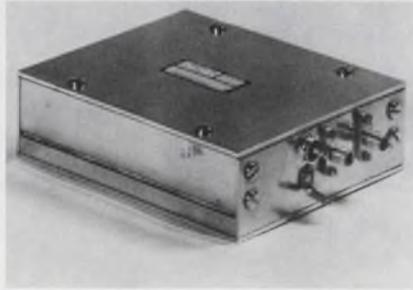


Microwave Power Devices, Inc., Adams Ct., Plainview, N.Y. 11803. (516) 433-1400. \$1950; 30 days.

The Model LWA1020, a solid state linear Class A amplifier, covers the complete frequency range of 1-2 GHz. The amplifier delivers 1 W at 1 dB compression, with a signal gain of 30 dB. The LWA1020 features complete field repairability due to the modular construction used throughout the amplifier. And 50 Ω spare modules that are factory prealigned can be replaced in the field by semi-skilled personnel.

CIRCLE NO. 486

Octave-tuned oscillators offer 1% linearity



Texscan Corp., 2446 N. Shadeland Ave., Indianapolis, Ind. 46219. (317) 357-8781. \$390 to \$475; 4-6 wks.

The LTO series of electronically tuned oscillators exhibit tuning linearity of ±1% without external circuitry. Tuning accuracy is also ±1%. Five standard units in octave bandwidths cover the frequency range of 32 MHz to 1 GHz with power output of 20 mW. The LTO oscillators are fully isolated for stable operation into a 10.0:1 VSWR; tuning voltage is less than 12 V and the tuning input may be frequency modulated at a 1-MHz rate.

CIRCLE NO. 487

Nd:YAG laser comes easy to use, compact

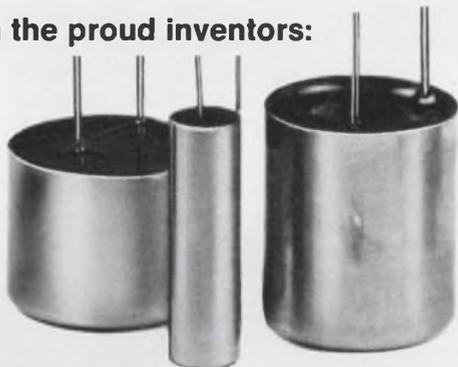


GTE Sylvania, Electro-Optics Organization, P.O. Box 188, Mountain View, Calif. 94040. (415) 966-9111. \$7000; 90 days.

A neodymium laser features quick-change pump lamps, safety interlock, and single-package design for ease of use and compactness. Designated Model 606, the Nd:YAG laser has a continuous output power of 3/4 W single transverse mode and 5 W multimode and operates at 1.06 mm. The 15-pound device is 4-1/4 × 4-1/4 × 15 inches. No special start-up procedures or alignments are necessary, according to the company.

CIRCLE NO. 488

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 Recovery: 25 Microseconds

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 Current Limiting:
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 Overvoltage (OV): Optional
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MODEL	VOLTS	AMPS	MODEL	VOLTS	AMPS
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200-12	11.5 to 12.5	10.0	200-1212	11.5 to 12.5	5.0
200-15	14.5 to 15.5	9.0	200-1515	14.5 to 15.5	4.5
200-24	23.5 to 24.5	7.5	200-2424	23.5 to 24.5	3.5
200-28	27.5 to 28.5	7.0	200-2828	27.5 to 28.5	3.5
200-48	47.5 to 48.5	4.0	(Any voltage 3 to 30 available)		
(Any voltage 3 to 50 available)			For OV models add -0 to model No.		

QUANTITY	SINGLE	WITH OV	DUAL	WITH OV
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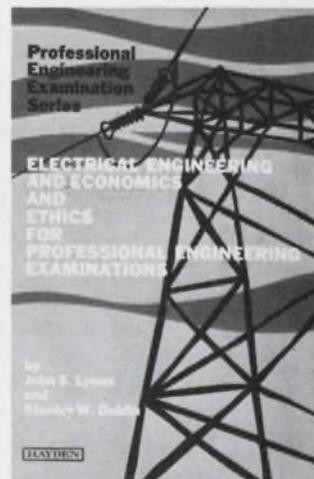
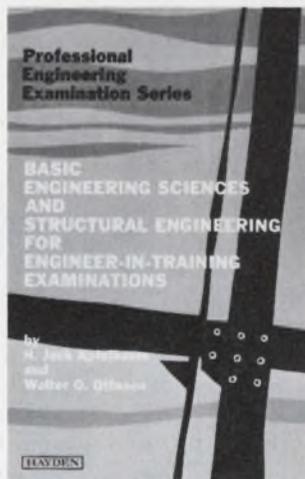
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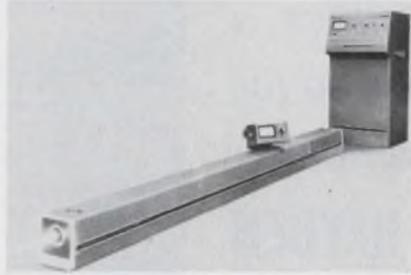
K-band generators boost power ratings

Polarad Electronic Instruments, 5 Delaware Dr., Lake Success, N.Y. 11040. (516) 328-1100. Stock to 30 days.

A series of calibrated microwave signal generators provide at least 0 dBm from 10.0 to 15.5 GHz and from 15.0 to 21.0 GHz. The new signal generators are Models 1709A, 1710A, 1809A and 1810A. Each reportedly provides a power output that's double that previously available. Other features include extended range FM, pulse and square wave modulation, (from 10 Hz to 10 kHz), $\pm 0.5\%$ digital frequency readout, greater maintenance-free reliability (MTBF) and low cost (compared to the tube units). Prices are \$3760 for Models 1709A and 1710A, and \$4000 for Models 1809A and 1810A.

CIRCLE NO. 489

Argon laser has 15 W cw output



Spectra Physics, 1250 W. Middlefield Rd., Mountain View, Calif. 94040. (415) 961-2550. 170-00: \$17,450; 170-03: \$22,750; 120 days.

Two argon lasers with output powers of 10 and 15 W, designated the Model 170-00 and Model 170-03, respectively, feature beryllium oxide (BeO) plasma tubes and Stab-lite resonators. The standard lasers come complete with snap-in mirror and prism mounts. With the broadband mirror, the 170-03 operates on all lines. With the prism, single wavelengths can be selected; over 6 W are available at 514.5 nm and over 700 mW in the UV range.

CIRCLE NO. 490

Scribing system claims chip-yield doubled

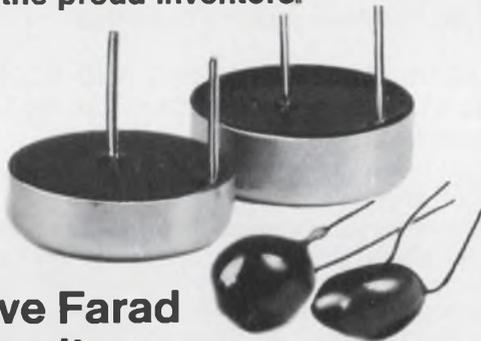


Electro Scientific Industries, 13900 N.W. Science Park Dr., Portland, Ore. 97229. (503) 646-4141.

The company's new scribing laser system boasts a throughput, or chip yield, that's more than twice that of previously achieved production levels, according to the company. Termed the SP3672, the system allows continuous scribing for a given substrate scribing pattern. Scribing speeds reach 6 ips.

CIRCLE NO. 491

from the proud inventors:



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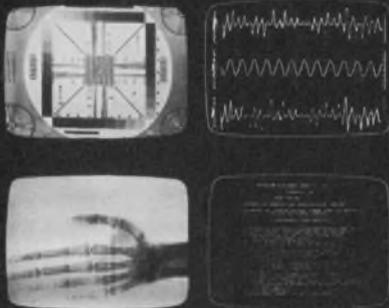
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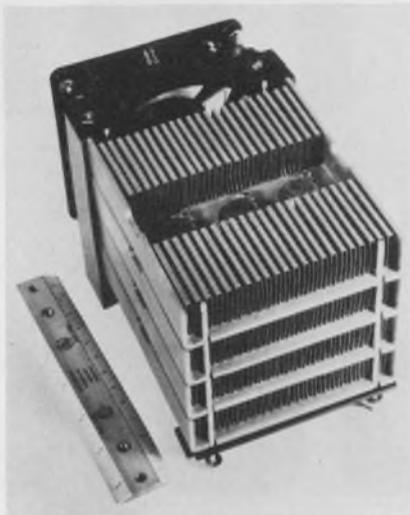


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INFORMATION RETRIEVAL NUMBER 104

PACKAGING & MATERIALS

Modular heat sink dissipates 720 W



W. F. Chew Enterprises, 441 E. 4th St., Long Beach, Calif. 90812. (213) 432-2704. \$49; stock.

Coldpak IV, a modular forced-convection heat sink dissipates 720 W (12 TO-3 transistors) with less than 35 C plate temperature rise above ambient. The heat sink is sized in an envelope of 5.25-in. H × 5-in. W × 6.5-in. L. Coldpak IV with two-lead egress holes of 203-mils diameter and mounting holes of 156-mils spaced for TO-3 cases. The unit accepts any standard 4 11/16-in. square fan providing a minimum air flow of 60 cfm.

CIRCLE NO. 492

Neutral flux for silver soldering boasts safety

Superior Flux & Mfg. Co., 1536 St. Clair Ave., Cleveland, Ohio 44114. (216) 781-9373.

Safety for users is a feature of silver solder flux No. 6 since it is neutral—not acid—and will not burn the operator's hands or skin. Flux fumes are claimed not to be harmful to eyes, lungs or nasal passages since they contain no free fluorides and cannot generate hydrofluoric acid or dangerous acid fumes. Superior No. 6 flux is used for brazing, hard soldering and silver soldering both ferrous and nonferrous metals and alloys such as mild steel, high carbon steel, stainless, monel, nickel, inconel, copper, brass, bronze and precious metals.

CIRCLE NO. 493

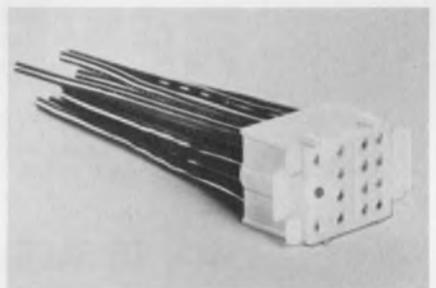
Beryllium oxide raises substrate conductivity

Ceradyne, Inc., 8948 Fullbright Ave., Chatsworth, Calif. 91311. (213) 882-8777.

Polished hot-pressed beryllium oxide (CERALLOY 418) substrates have a thermal conductivity seven times greater than sapphire. The substrates are diamond sliced, ground, and lapped from large, uniform billets. Surface finishes can be finer than three micro-inches, in sizes up to 5 × 5 inches. The fine surface finish is obtainable because the hot pressed ceramics are theoretically dense (zero porosity), free from glassy binders (no unequal lapping), and fine grained (no pull-outs). All properties are isotropic in contrast to the anisotropic properties of sapphire. This isotropy is achieved due to the randomly oriented, polycrystalline nature of the hot pressed ceramics.

CIRCLE NO. 494

Nylon relay socket handles 120 V, 5 A



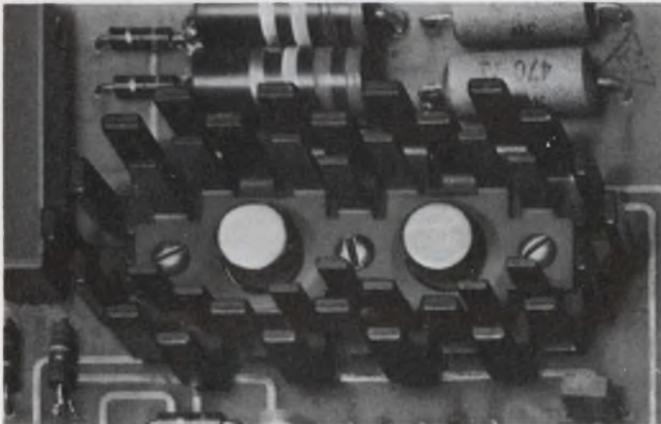
Waldom Electronics, Inc., 4625 W. 53rd St., Chicago, Ill. 60632. (312) 585-1212. \$19.20/100 (1000 up); stock.

The Series 1852-R nylon relay socket works for up to 14-contact, 4PDT relays, with a rating of 120 V, 5 A per circuit. The socket houses Waldom/Molex miniature, tin-plated brass terminals, which accept 18 to 24 gauge wire. The new socket snaps into standard chassis holes quickly and easily, without clips or screws. One side of the socket has a slide-in slot, while the opposite side has a mounting ear. The new socket is recommended for use with relays made by Comar, C.P. Clare, Guardian, P&B, Parelco, Sigma, etc.

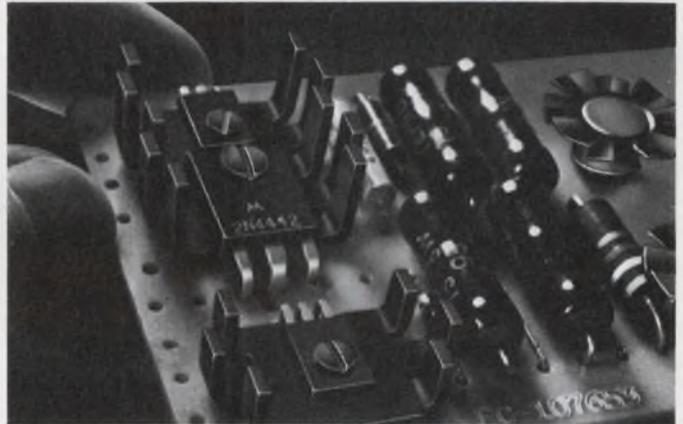
CIRCLE NO. 495

Tips on cooling off hot semiconductors

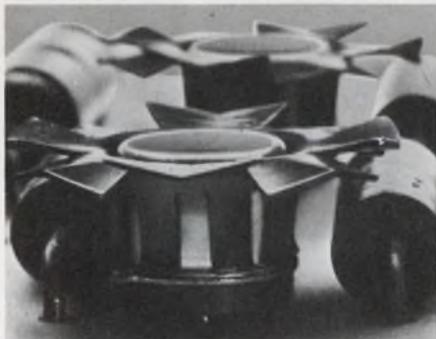
As power levels go up and up and package size shrinks, circuit designers are keeping semiconductors cool with IERC Heat Sinks/Dissipators. Reducing junction temperature gives many benefits: faster rise and fall times, faster switching speed and beta, fewer circuit loading effects and longer transistor life and circuit reliability.



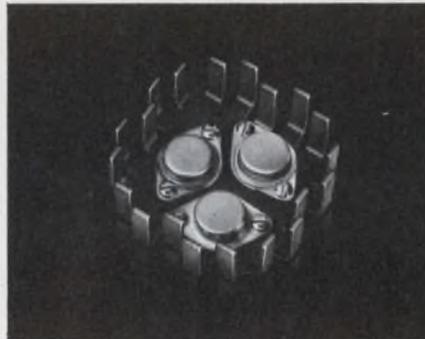
Thermal mating of matched transistors, such as these TO5's shown on a dual LP, maintains matched operating characteristics. The LP's unique multiple staggered-finger design (both single and dual models) maximizes radiation and convection cooling, results in a high efficiency-to-weight and -volume ratio.



Power levels of plastic power devices such as X58's, MS9's, and M386's can be increased up to 80% in natural convection and 500% in forced air when used with PA and PB Dissipators. PA's need only .65 sq. in. to mount; PB's 1.17 sq. in. Staggered finger design gives these light-weight dissipators their high efficiency.



TO5's and TO18's in high density packages can be cooled off with efficient push-on Fan Tops that cost only pennies. T-shaped, need no board room, let other components snug close. Spring fingers accommodate wide case diameter variations. Models for RO97's, RO97A and D-style plastic devices also.



High power TO3's, TO66's, TO6's, TO15's, etc. can be operated with much more power when used with HP's. These compact, light-weight staggered finger devices accommodate from one to four TO3's. Provide the same heat dissipation as an extrusion that's three times heavier and one-third larger.

Heat problems? IERC engineers welcome the opportunity to help solve your heat dissipation problems. As the world's largest manufacturer of heat sinks/dissipators for lead and case mounted semiconductors, they can come up with a practical, low cost solution.

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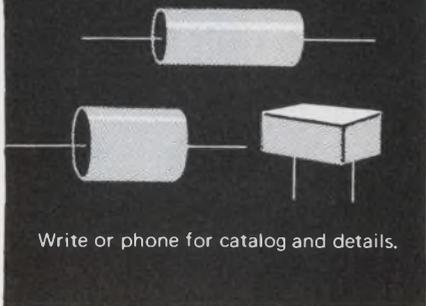
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INFORMATION RETRIEVAL NUMBER 106

PACKAGING & MATERIALS

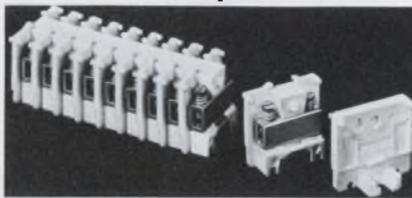
Copper-clad epoxy glass laminate boasts low cost

Cincinnati Milacron, 4701 Marburg Ave., Cincinnati, Ohio 45209. (513) 841-8444.

A PC board material for computer, communications and hostile-environment applications combines many of the best features of polyester-based laminates with those of general purpose and flame retardant glass-cloth reinforced epoxy laminates. The CIMCLAD EG material is a copper-clad laminate based on an epoxy-resin reinforced by a fiberglass mat. Its properties include lower dielectric constant (affects resistivity), lower dissipation factor (affects ability to hold charge), and greater arc resistance (reduces damage to circuit by shorting). The laminate is reported to be more economical than conventional epoxy, yet has better properties. CIMCLAD EG laminate is available in thicknesses of 47 mils to 125 mils and in four subtypes: EGA—one-ounce copper, one side; EGB—one-ounce copper, two sides; EGC—two-ounce copper, one side; and EGD—two-ounce copper, two sides.

CIRCLE NO. 496

Terminal blocks feature tubular clamp contacts

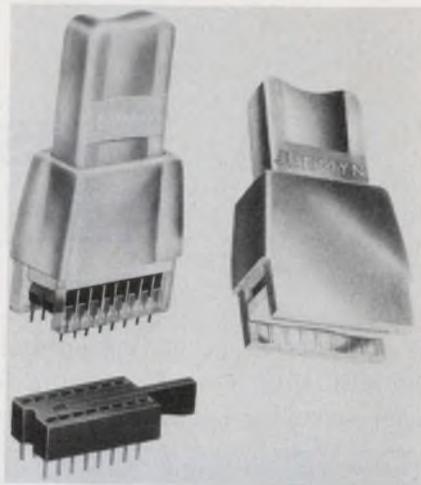


Buchanan Electrical Products Corp., 1065 Floral Ave., Union, N.J. 07083. (201) 289-8200.

Miniature 300-V sectional terminal blocks come with tubular screw and tubular clamp contacts for easy wire insertion and the elimination of lugging. The miniature blocks, handling a wire range through No. 12 AWG, are rated at 300 V NEMA general industrial control devices and 600 V NEMA limited power circuits. They are available in nylon or polypropylene, and other thermoplastic compounds.

CIRCLE NO. 497

DIP insertion tool aligns lead pitch



Jermyn, 712 Montgomery St., San Francisco, Calif. 94111. (415) 362-7431. \$2.50; stock.

A DIP insertion tool provides a safe means of inserting 14 and 16-pin DIPs into sockets and PC boards. The A23-2050 tool closes the IC leads to the correct 300-mil pitch before locating over the socket or PC board. The tool has a transparent base, facilitating visual alignment of the IC leads with the socket or PC board. Since no metal parts are incorporated into the tool, ICs can be inserted into live sockets without danger of short circuits.

CIRCLE NO. 498

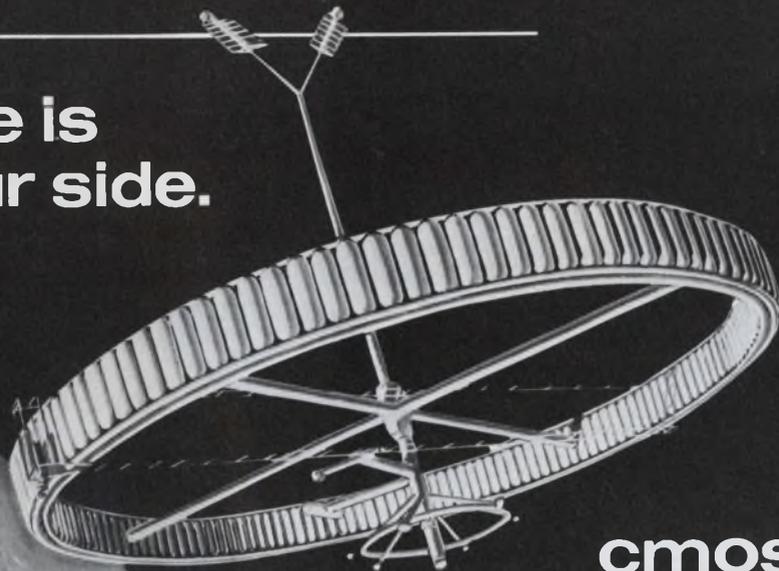
Zip-on insulation features high flexibility

The Zippertubing Co., 13000 S. Broadway, Los Angeles, Calif. 90061. (213) 321-3901.

A zip-on protective material, Type ZVF, features flexibility for applications such as bundling and covering welding lines and others where flexibility is a must. The zip-on ZVF insulation is a fiberglass material which has a lamination of vinyl on both sides. It features the Z-trac which zips on or off easily and which holds strongly during its lifetime of application. If required, the trac may be permanently sealed. A special inside overlap of fiberglass is part of the ZVF construction and gives added protection at the zipper trac location.

CIRCLE NO. 499

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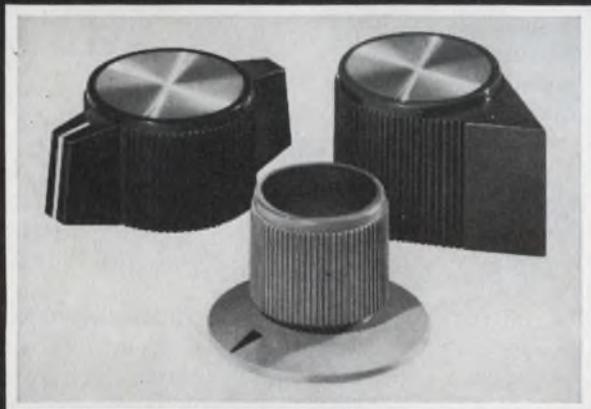
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ELECTRONIC DESIGN 1, January 4, 1973

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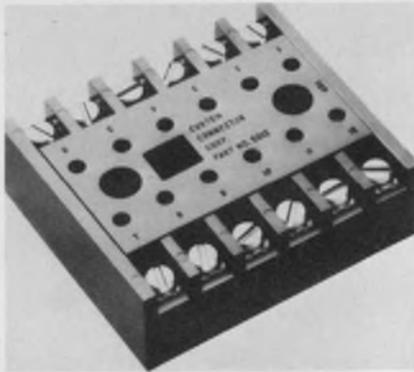
DATA DISPLAY PRODUCTS

8036 Westlawn Ave. Los Angeles, Ca. 90045
(213) 641 1232

INFORMATION RETRIEVAL NUMBER 110

PACKAGING & MATERIALS

Relay socket accepts proximity switches



Custom Connector Corp., 1738 E. 30th St., Cleveland, Ohio 44114. (216) 241-1679.

Relay socket for 12 and 14-pin, 219 frame, plug-in relays can also be used with most 12-pin, plug-in, proximity switches. The relay socket is molded of rugged Noryl Thermo plastic resin. It has closed back construction eliminating the need for insulation.

CIRCLE NO. 500

Casting resins feature low dielectric constants

Emerson & Cuming, Inc., 59 Walpole St., Canton, Mass. 02021. (617) 828-3300. \$3 to \$10/lb; stock.

A line of casting resins, Stycast 35, for the microwave and electronic industries features low loss tangents below 0.001 from 60 Hz to 10 GHz and low dielectric constants. The Stycast 35 series presently contains six members: Stycast 35: a clear low-viscosity liquid which becomes pure polystyrene upon cure; Stycast 35D: upon cure it becomes cross-linked polystyrene; Stycast 35PE: a mixture of cross-linked polystyrene and polyethylene, resulting in a somewhat lower dielectric constant than Stycast 35; Stycast 35DS: filled with low-loss silica microballoons resulting in the lowest dielectric constant in the series, 1.9; Stycast 35DT: a mixture of polystyrene and polutetrafluoroethylene, it has the highest temperature capability of the series: 350 F; Stycast 35DA: mineral filled, raising the dielectric constant to 5.0 without raising the loss tangent.

CIRCLE NO. 501

Thick-film resistor offers high stability

E. I. Du Pont de Nemours & Co., 1007 Market St., Wilmington, Del. 19898. (302) 774-2358.

The Birox 1400 series of thick-film resistor compositions offers excellent stability after abrasive or laser trimming, with trimmed resistors drifting 0.5% or less over the entire 10 to 100-k ohms-per-square range of sheet resistivities. Trimmed resistors withstand power loadings as high as 200 W per square inch and voltage stresses as high as 3000 V per inch. The temperature coefficient of resistance for the new series is less than ± 100 ppm/ $^{\circ}$ C over the range of -55 to 125 C.

CIRCLE NO. 502

Wiring duct prevents cutting wires to length

Marathon Special Products, P.O. Box 258, Bowling Green, Ohio 43402. (419) 352-1781.

A line of extruded PVC panel wiring duct and cover can be used to channel large or small amounts of wire within control panels and other places where multiple conductors are required, without the time consuming process of tying, wrapping or cutting to exact length. Duct-Dowel is used to hold up wires (by draping them over) at the time of panel assembly, and can be left in the wiring duct for later use on maintenance and changes.

CIRCLE NO. 503

Disconnects span wire sizes 10 to 22 AWG

Panduit Corp., 17301 Ridgeland Ave., Tinley Park, Ill. 60477. (312) 532-1800.

A line of Pan-Term disconnects provides quick, snap-in interconnections for wire sizes from 10 to 22 AWG. They are made from electro-tin plated brass to provide long, corrosion-resistant operating life. Serrated barrels are used on both male and female disconnects to assure high tensile strength and maximum wire contact after crimping.

CIRCLE NO. 504

Now-Gordos switches in Gordos relays.

Now we don't stop with making the heart of a relay; we make the relay, too. So you can buy Gordos quality inside and out . . . and automatically get the same switches used in high-quality relays for years.

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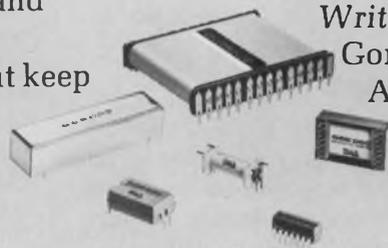


Order off-the-shelf from our first five families of Microminiature DIP,

Miniature Molded, Miniature Open, Compact and Large reed relays. Or, throw us your special problems and see how our design and production savvy can help you meet out-of-the-ordinary needs for speed and relay performance.

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INFORMATION RETRIEVAL NUMBER 111

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Accuracy: Within $\pm 10\%$ full scale.
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Speed Range: 3kHz ± 1 kHz
Readout Display: 4-digit counter type; unit, Hz, gate time, one second.
 - **FREQUENCY MEASUREMENT**
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Input Level: 100mV-30V
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* Please see our catalog for details.



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A compact, solid-state multimeter with digital readout — at a fantastic kit-form price. The new Heathkit IM-1202 has four overlapping ranges to measure voltages from 10 mV to 1000 V on DC (either polarity), 10 mV to 700 V rms on AC, 10 μ A to 2.5A on AC or DC current. Five resistance ranges measure from 1 ohm to 2.5 megohms. Front panel polarity switch reverses inputs without changing leads. 6 lbs.

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The Heathkit IB-1100 gives 1 Hz to over 30 MHz counting on a full 5-digit readout with 8-digit capability. The lighted overrange indicator makes misreading virtually impossible. Stable time-base circuitry assures accuracy better than ± 3 ppm from 22° to 37° C. Diode protected J-FET gives improved triggering over 100 mV to 150 V input range. Solid-state circuitry mounts on one large board for easy assembly. 6 lbs.

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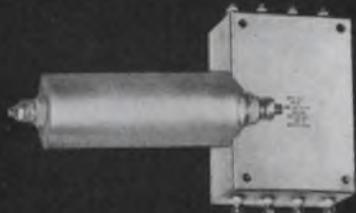
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160

evaluation samples

Reed relays

A commercial reed relay (manufactured in accordance with MIL-Q-9858A) features 1 A or 20 W switching up to 250 V. Coil voltages are available for 1, 3, 5, 6, 10, 12, 15 and 24 V. The relay measures 0.275-in. diameter by 0.950-in. long and can be PC board mounted on 1-in. centers with 0.100 or 0.150-in. spacing. The relay features magnetic shielding and hermetic sealed coil for all environmental conditions. Electronic Applications Co.

CIRCLE NO. 505

Pin headers

A range of pin headers has been extended by the availability of tall covers. The snap-on precision-made covers completely enclose the circuitry except for a small hole through which potting compound can be ejected. The 14 and 16-pin versions will house components up to 0.3 in. high; the 24-pin type will accommodate components up to 0.5 in. high. The contacts are gold plated phosphor bronze, and the body glass filled nylon Type A190. Jermyn.

CIRCLE NO. 506

Terminals

A quick-connect wire terminal, which requires no insulation, has its point of contact covered with protective nylon. The terminal comes in two sizes. One fits 0.250 male tabs; the other 0.187 male tabs. Both can be used with Nos. 14, 16 or 18 gauge wire. Great Valley Industries.

CIRCLE NO. 507

Antistatic cleaner

GTC-59 is a mildly alkaline preparation that cleans, degreases and imparts a hard, lustrous, water-repellent, antistatic finish to all nonporous surfaces, including glass, plastics and metals. Beaver Laboratories.

CIRCLE NO. 508

Temperature recorders

Model 442A, a four-position temperature recorder reported to be the world's smallest, features an accuracy of $\pm 1\%$. It indicates temperature in ranges from 110 F to 450 F (or 43 C to 232 C). When exposed to the rated critical temperature, the indicator window turns from pastel to black for a direct readout which is permanent and irreversible. The recorder is self-adhesive. William Wahl Corp., Temp-Plate Div.

CIRCLE NO. 509

Epoxy casting system

TRA-CAST 3109 is a two-part, solvent-free formulation designed for production potting, casting and coating applications. Color coded for easy mixing, this epoxy system cures in just a few hours at room temperature, with very low shrinkage and exotherm, making it suitable for larger mass castings (up to one gallon) and other large pour applications. Tra-Con, Inc.

CIRCLE NO. 510

Bridging clip

A bridging clip electrically interconnects adjacent terminals in the same row of 66 Type connecting blocks. The clip, stamped of stainless steel, slips over the terminals with just finger pressure, eliminating laborious interconnecting by wire. Removal is just as quick and easy. Fastex, Div. Illinois Tool Works Inc.

CIRCLE NO. 511

Slotted fastener

SwissLok is a fastener for joining sheet metal plates at right angles. Looking like the cross-section of a split rivet, the split has the configuration of a keyslot. The fastener is inserted through the opening of one sheet metal plate and the split portion straddles the edge of a second plate which is perpendicular to the first plate. A single blow with a hammer or air tool on the head of the fastener locks the two plates together. Waldman Corp.

CIRCLE NO. 512

design aids

Power transistors

A wall chart describes a complete range of high-current, high-voltage silicon power transistors. Major specifications of each type are included for device selection. Each chart includes a postage-paid reply card enabling you to receive a complete catalog with detailed specifications and price lists. Powertech, Inc.

CIRCLE NO. 513

Tantalum capacitor chart

A 16-page Established Reliability Tantalum Capacitor Conversion Chart compares the electrical, acceptance inspection test and marking requirements between MIL-C-39003C and MIL-C-39003A. The chart cross-references military part number designations and dash numbers for CSR13 capacitors from the original MIL-C-39003 specification through to the present C revision. Also included are capacitor outline drawings and dash number listings for CSR09, CSR13, CSR23 and CSR91 capacitors with a cross-reference to equivalent KEMET capacitor part numbers. Union Carbide Corp.

CIRCLE NO. 514

Multilayer board guides

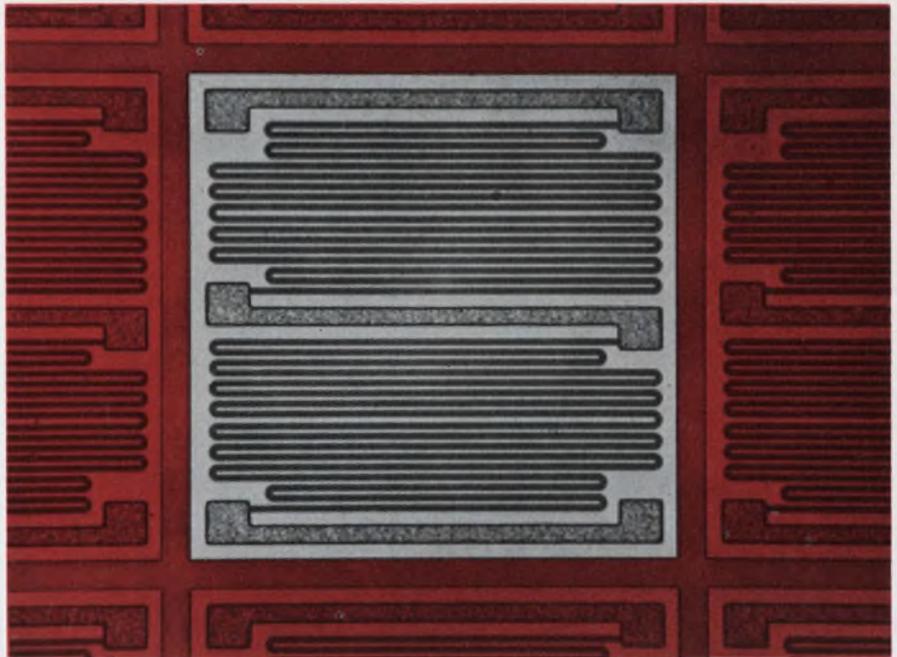
A wall-chart provides design information on multilayer boards. Graphs and tables describe various conductors, conductor plating, layout tolerances and dimensions, laminates, voltage between conductors and general specifications. A table outlines required specifications. Lockheed Electronics, Data Products Div.

CIRCLE NO. 515

Data conversion chart

All you want to know about data conversion is on a handy wall chart. The design reference guide includes calculations, terminology, theory, tables, codes and other reference information. Analogic.

CIRCLE NO. 516



New passivated thin-film resistor chips and wafers

from HYBEX a new division of Burr-Brown

Here's a new series of glass passivated thin-film resistors from a new, dependable source — Hybex. The unique "S" configuration, originated by Hybex personnel, greatly simplifies hybrid assembly.

Since these center-tap resistors contain three pairs of large surface aluminum bond pads, the operator can accomplish straight line wire bonding without reorientation of the 30 mil chip. Gold silicon backing also allows the use of all conventional die bonding techniques including eutectic and epoxy.

HYBEX "S" SERIES RESISTORS

- Temperature Coefficients: ● Standard Resistance Value Range:
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 - tracking to $\pm 5\text{ppm}/^\circ\text{C}$ 10% tolerance, 10 ohms to 470 kohms
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application notes

CMOS expandable gates

A technical bulletin outlines functions and circuitry of CMOS expandable gates. The bulletin describes the company's method of employing added buffer stages and is complete with diagrams on the configurations possible. Tables on dynamic and output-drive characteristics as well as circuit capabilities and over-all performance characteristics are included. Solid State Scientific, Inc., Montgomeryville, Pa.

CIRCLE NO. 517

Microprogrammed control

"Economic Advantages of Microprogramming" contains a descriptive breakdown of the costs incurred in putting an integrated circuit into a system. These expenses are then compared with the cost of microprogrammed control, which is presented as an alternative to random logic. The brochure reviews the types of control memory elements currently being used, such as read-only memories, random-access memories and fusible read-only memories which are programmed by the user. Signetics Memory Systems, Sunnyvale, Calif.

CIRCLE NO. 518

Dielectric products

"Dielectric Products and Their Applications" provides useful technical descriptions and applications of many resin and dielectric products. In some cases chemical formulations are given. The lines which are discussed include casting resins, adhesive systems, impregnating resins, molding compounds, ceramic encapsulants, glass, ceramic and plastic microballoons, silicone resins, plastic and ceramic foams, dielectric sheet and rod stock and syntactic foams for underwater buoyancy. Emerson & Cuming, Inc., Dielectric Materials Div., Canton, Mass.

CIRCLE NO. 519

Broadband receiver design

"Design of a Communications Security Test Receiver for Maximum Broadband Dynamic Range" describes the problems associated with detection of broadband signals, offers insight into the solution of those problems and presents the required receiver design techniques to maximize broadband sensitivity and linear, instantaneous dynamic range. Points stressed are 1) application of successive filtering of the receiver channel and 2) maximizing signal handling capability. The related considerations concerning local oscillator rejection for maximization of tuning range and equipment shielding are also presented. American Electronic Laboratories, Inc., Lansdale, Pa.

CIRCLE NO. 520

SCR protection

A bulletin on a high-power semiconductor series explains and illustrates the major causes of voltage transients in typical thyristor converter circuits and the basic approaches to transient protection to prevent malfunction or device failure. Nine fundamental suppression schemes are explained and compared for relative size, cost and complexity. A reference listing directs the designer to information for specific applications. Most of the seven-page publication is devoted to circuit illustrations. Westinghouse Electric Corp., Youngwood, Pa.

CIRCLE NO. 521

Capacitor diodes

More than 300 JEDEC registered types of voltage-variable capacitors are described in a four-page catalog. Specifications presented are nominal capacitance and tolerances, tuning ratio, voltage ranges over which tuning ratio is valid, temperature coefficient of capacitance, Q, leakage, etc. Also included is design information such as Q as a function of voltage and frequency and capacitance vs temperature. Codi Semiconductor, div. of Computer Diode Corp., Fair Lawn, N.J.

CIRCLE NO. 522

Consumer ICs

"New Developments In Consumer Integrated Circuits" reviews present state-of-the-art technology, including the continuing development of ion implementation. Technology improvements are illustrated by means of available products in TV-FM and automotive fields which utilize ion implementation. Sprague Electric Co., N. Adams, Mass.

CIRCLE NO. 523

Neon lamps

"Miniature Neon Lamps: Elements of Electronic Versatility," a 127-page book, gives detailed information on aspects of construction and application as indicators, in voltage regulation and reference and as electronic circuitry components. A handy reference to the characteristics of most available neon lamps is included. Glowlite Corp., a subsidiary of El-Tronics, Inc., Pauls Valley, Okla.

CIRCLE NO. 524

Troubleshooting motors

Common fractional horsepower motor troubles and their causes are examined in the company's Motorgram (Vol. 52, No. 5). Bodine Electric Co., Chicago, Ill.

CIRCLE NO. 525

Optimizing microstrip lines

Two papers discuss the construction and performance of microcircuit components built on a substrate of pure fused silica. "Hybrid Microwave Integrated Circuits for Millimeter Wavelengths," by members of The General Electric Co., Wembley, England, describes microstrip transmission lines 500 μm wide on 250 μm thick fused silica with 50- Ω characteristic impedance. "Low-Loss Microstrip Filters Developed by Frequency Scaling" published in the Bell System Technical Journal, reports building of low-pass and bandpass microstrip filters up to 30 GHz on fused silica substrates by photolithic reduction of optimized low-frequency models. Dynasil Corp. of America, Berlin, N.J.

CIRCLE NO. 526

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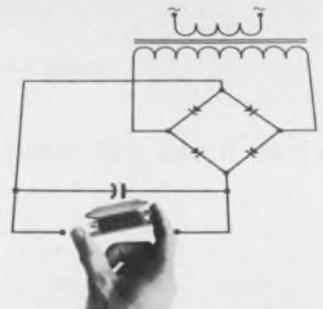
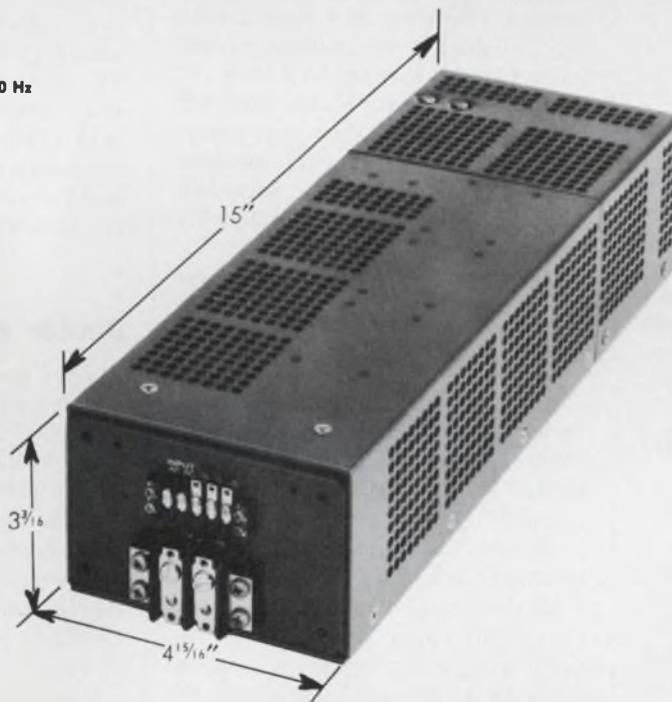
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INFORMATION RETRIEVAL NUMBER 116

new literature



Linear & data conversion

A 16-page guide describes a line of linear products, data conversion modules, multichannel a/d conversion systems and power supply modules. Forty-eight modular power supplies are listed, including miniature DIP compatible supplies offering ac to dc and dc to dc conversion, and single, dual and triple outputs. Electrical and mechanical specifications as well as photos, general descriptions, graphs and circuit diagrams are included. Price and ordering information are available. Zeltex, Inc., Concord, Calif.

CIRCLE NO. 527

Electron tubes and semis

A 100-page buyers guide of electron tubes and semiconductors includes over 1400 rectifiers, diodes, zeners, transistors, SCRs, FETs and unijunctions. A complete listing of foreign tube types is included. Prices are given. United-Page, Inc., Paterson, N.J.

CIRCLE NO. 528

Disc storage

A two-color, single-sheet Data Bulletin describes Fastrack 010 Series Disc Storage Systems. Pacific Micronetics, Inc., San Diego, Calif.

CIRCLE NO. 529

Dc-dc power converters

A two-page data sheet describes a line of ultraminiature dc-dc converters designed specifically to power linear ICs and a/d-d/a converters. It gives both electrical and mechanical specifications plus performance features. Included is a selection guide which categorizes dc-dc converters according to input/output (volts and current), line/load regulation data, price information plus complete operating specifications. Datel Systems, Inc., Canton, Mass.

CIRCLE NO. 530

Dc power supplies

The UM Series of miniature, solid-state, high-voltage dc power supplies are described in Bulletin UM792. The two-page data sheet contains features and applications for UM models with output ranges from 0-1000 through 0-24,000 V. Detailed specifications are included along with outline drawings showing case sizes. Complete installation instructions are included. Spellman High Voltage Electronics Corp., Bronx, N.Y.

CIRCLE NO. 531

MECL book

"MECL Data Book" contains basic performance specifications for each IC device in the MECL II, MECL III and MECL 10,000 logic families. Complete dc, ac and performance data are given in the 410-page book. Convenient abbreviated guides offer a quick selector for MECL logic blocks. The 36-page general information section contains a synoptic discussion of topics of value to the designer planning a MECL system. In addition, dimensioned drawings of MECL packages are shown. References to the MECL software support available are included by way of application note abstracts, as well as references to a sampling of MECL articles in the trade press. The book is available at \$2 per copy. Motorola, Inc., P.O. Box 20924, Phoenix, Ariz. 85036.

Technical services

A booklet describes the company's analysis and characterization services for the electronics industry. Typical of the services available is trace analysis or solid or liquid raw materials such as graphite, silicon, germanium, III-V and II-VI compounds and alloys, ferrous, nonferrous oxides, garnet and ceramics and other related materials such as glass and plastics. Techniques employed include emission spectroscopy, spark source mass spectroscopy, infrared absorption spectroscopy and electronic microprobe analysis. The company also is offering structure characterization through X-ray diffraction, electron scanning microscopy and electron microprobe analysis. Monsanto Commercial Products Co., St. Louis, Mo.

CIRCLE NO. 532

Negative hv power supplies

Negative high-voltage power supplies are described in a two-page brochure. Features detailed include variable high voltage to 2 kV at 10 mA, low ripple, voltage and current monitoring, separate ± 15 V supply for op-amp drive, low temperature coefficient and easy dial-in voltage. Pacific Photometric Instruments, Emeryville, Calif.

CIRCLE NO. 533

Double exposure holography

The uses and applications of double exposure holography are described in a four-page brochure. The brochure discusses how a double-pulse hologram is made as well as the specifications and design features of the Model 22HD double-pulse holographic laser. Apollo Lasers, Inc., Los Angeles, Calif.

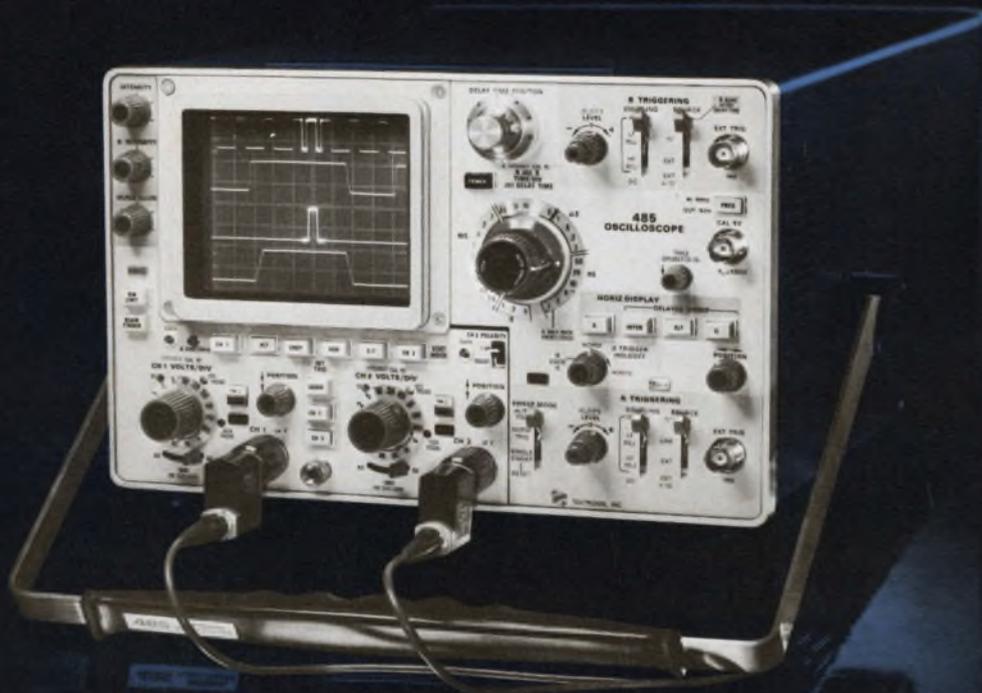
CIRCLE NO. 534

One-chip calculator-memory

The CT5005, claimed to be the industry's first MOS four-function 12-digit chip with a register for memory or constant operation, is described in an eight-page brochure. The k feature is operated by recalling the k number from memory. Cal-Tex Semiconductor, Inc., Santa Clara, Calif.

CIRCLE NO. 535

350 MHz



in a *portable* laboratory oscilloscope
that weighs only 23 pounds.

The dual-trace, 350-MHz TEKTRONIX 485 Oscilloscope is the newest addition to the world's most widely used portable family. Many features of earlier TEKTRONIX portables are retained, many others are expanded and a lot of new ones are added. The result is a new product which significantly expands the performance spectrum of portable scopes. Following are some of the features of the 485, an oscilloscope which measures with laboratory precision and carries with small-package ease.

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INFORMATION RETRIEVAL NUMBER 118

NEW LITERATURE



Heathkit catalog

Included in the Heathkit Catalog are color TVs, audio equipment, marine gear, amateur radio equipment, an electronic calculator, security systems and intercoms. More than a dozen pages are devoted to test and service instruments, plus educational kits. Heath Co., Benton Harbor, Mich.

CIRCLE NO. 574

Transistor test system

A 28-page brochure describes both the hardware and the software of the company's T347 computer-operated transistor test system. Sections are included on test techniques, end-of-life programs, automatic distribution analysis, as well as a basic system description and a section on applications. Tera-dyne, Inc., Boston, Mass.

CIRCLE NO. 537

COS/MOS IC products

"COS/MOS ICs," an eight-page catalog, contains logic diagrams with terminal designations and quick selection data charts for 52 ICs including gates, flip-flops, latches, multivibrators, shift registers, counters, display/counter/decoders/drivers, multiplexers, arithmetic circuits, memories and phase-locked loop. Information on COS/MOS high-reliability types conforming to MIL-STD-883 and MIL-M-38510, COS/MOS chips and COS/MOS technical publications are given. RCA Solid State Div., Somerville, N.J.

CIRCLE NO. 538

Designing computer logic

Techniques and procedures used in designing, building and assembling computer logic systems and interfaces for PDP-series computers are described in the 225-page Logic System Design Handbook. The illustrated handbook is designed as a complement to the annual Logic Handbook and is keyed principally to the utilization of the company's logic modules and supporting hardware and accessories. It can also be used as a reference work in designing other types of logic circuits. Step-by-step procedures for assembling and wiring are included. Digital Equipment Corp., Maynard, Mass.

CIRCLE NO. 539

Green glow lamps

Catalog GG-72 illustrates and describes green glow lamps and indicators. The catalog provides specification data on lamps, cartridge lamps, indicator lights and holders. Inter-Market, Inc., Glenview, Ill.

CIRCLE NO. 540

Active filter nomograms

A brochure on active filters compares the performance of Butterworth, Chebyshev, Cauer, and other standard filter types and provides easy-to-use nomographs for estimating filter complexity. A data sheet is included which lists various parameters which should be part of most active filter specifications. A standard product selection matrix enables active filter designers and users to select the Universal Active Filter most suited to their needs. Kinetic Technology, Inc., Santa Clara, Calif.

CIRCLE NO. 541

EDP directory

The 1972 EDP Industry Directory covers computers, peripherals, terminals, special-purpose systems, communications equipment, auxiliary equipment, supplies and accessories, software and services. Single copy price is \$25. Order direct from Technical Publishing Co., EDP Industry Directory, 1301 S. Grove Ave., Barrington, Ill. 60016.

Miniature lamps

A 40-page catalog covers descriptions and specifications for over 470 different miniature and sub-miniature incandescent and solid-state lamps. Complete operating parameters on each lamp are provided plus outline drawings with all necessary dimensions shown. An index is also included to show equivalent LAMPS model numbers and American National Standards Institute numbers to simplify selection. LAMPS, Inc., Torrance, Calif.

CIRCLE NO. 542

Cermet trimmer

A low-profile, cermet trimming potentiometer, measuring only 0.15-in. high, is the subject of a catalog sheet. Beckman Instruments, Inc., Fullerton, Calif.

CIRCLE NO. 543

Time sharing recorder

A thermistor probe and strip chart, which extends the range of the Model LT8200 recorder making it suitable for monitoring air conditioning and heating equipment, is described in a catalog sheet. Two other recorders described are a current recorder and a recording volt/ammeter. Amprobe Instrument, Div. of SOS Consolidated, Inc., Lynbrook, N.Y.

CIRCLE NO. 544

ROMs

High-speed read-only-memories are described in data sheets. Aztec Data Systems, Irvine, Calif.

CIRCLE NO. 545

Printer/plotter

A six-page illustrated brochure describes the CPE-57 Complot printer/plotter. The brochure outlines the functions of the printer/plotter in producing charts, graphs, alphanumeric, maps, drawings and other graphics using the electrostatic principle of operation. Applications ranging from weather maps to phototype setting are listed. Also included is a description of computer graphics plotting, non-impact line printing and software, as well as pricing and ordering information. Houston Instrument, Bellaire, Tex.

CIRCLE NO. 546

OUR CODES ARE NO SECRET



We discovered recently that we have more standard output codes available for our Thumbwheel switches than anyone else in the business. Actually, it has become difficult to catalog all the choices we offer.



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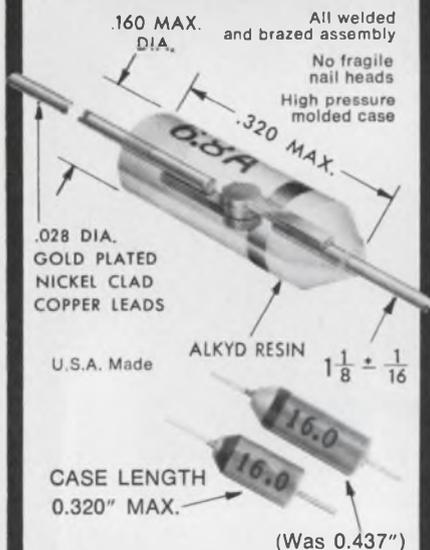
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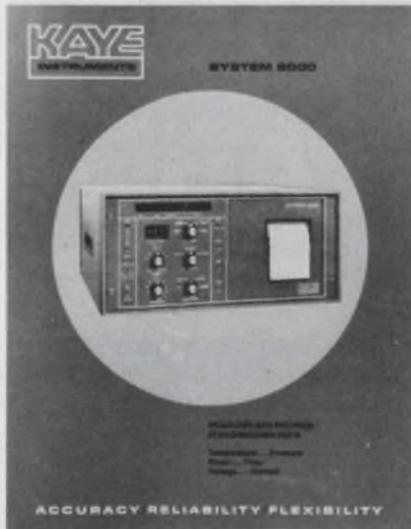
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NEW LITERATURE



Data system

An automatic data system for measuring and recording in engineering units temperature, pressure, strain, flow, voltage and current is described in a 12-page catalog. Kaye Instruments, Inc., Cambridge, Mass.

CIRCLE NO. 547

Analog multipliers

The GPS MU4100 series multipliers are described in a four-page bulletin. The miniature components need no external operational amplifiers. GPS Corp., Framingham, Mass.

CIRCLE NO. 548

Stepping switches

Catalog No. 601 provides detailed information on open or enclosed, spring-driven or direct drive, bracket-mounted or quick-mount stepping switches. The 56-page publication includes a thorough introduction to the design and construction of stepping switches, its uses, its physical and electrical characteristics, its circuitry, optional features and when to specify the switches, switch accessories and maintenance tools, plus a guide to selecting the proper switch. For each individual switch, the catalog offers complete physical and electrical specification data plus dimensional illustrations, mounting detail and full performance information. C.P. Clare & Co., Chicago, Ill.

CIRCLE NO. 549

Rectilinear potentiometers

The Model 910 series of plastic rectilinear potentiometers are specified in a bulletin. Available in a variety of sizes and in linear and nonlinear functions with center taps, the high resolution pots operate efficiently when exposed to hostile environments, such as, jet fuel or hydraulic fluid. Outlined in the bulletin are the electrical characteristics of the rectilinear potentiometers. Amphenol Connector Div., Controls Operations, Broadview, Ill.

CIRCLE NO. 550

Neon-tube applications

A convenient index of over 400 articles and letters which have appeared in the company's Application News lists each item by title, volume and number of the issue in which it appeared, as well as by the consecutive page number. Topics covered are neon glow lamps that are used as active components in electronics and as indicators in electrical equipment and high-energy devices which include spark gaps, transient surge protectors, noise sources and high-energy switches. Signalite, Neptune, N.J.

CIRCLE NO. 551

Capacitor matrices

Fourteen-pin DIP multi-layer ceramic capacitor matrices are described in two bulletins. The NPO Series 6900 accommodates up to 12 capacitors in a single unit and range from 50 to 500 pF at 50 V dc. The BX Series 6910C provide for installation of up to seven capacitors and range from 500 pF to 0.1 μ F at 50 and 100 V dc. Both units are manufactured in accordance with MIL-C-39014. The Potter Co., a div. of Pemcor, Inc., San Diego, Calif.

CIRCLE NO. 552

Flat-cable edge connectors

Data Sheet 208 describes flex-strip flat-cable edge-connector assemblies. The assemblies combine Series 608 connectors (which use the flat-cable conductors as contacts) and standard 0.100-pitch flat cable. Complete data and specifications are included. Ansley Electronics Corp., Doylestown, Pa.

CIRCLE NO. 553

Data conversion

A short form catalog describes data conversion and display products. The 12-page brochure offers specifications, applications and pricing. Analogic, Wakefield, Mass.

CIRCLE NO. 554

Connectors

Leaflets cover screwed GP connectors, BNC high-voltage connectors, connector-to-cable assemblies and a 70-MHz passive probe kit. Greenpar Engineering Ltd., Essex, England.

CIRCLE NO. 555

Motor information kit

An information kit contains eight separate catalogs containing full information on transistorized, SCR, ac, and autotransformer motor speed controls; and synchronous, instrument and torque motors. B & B Motors and Control, New York, N.Y.

CIRCLE NO. 556

Microwave tunnel diodes

Major electrical specifications of the company's diodes are detailed in a four-page brochure. Devices listed are microwave tunnel diodes, microwave oscillator diodes, germanium video detector and back diodes, gallium arsenide varactor and avalanche diodes and picosecond switching tunnel diodes. Micro State Products, Raytheon Co., Waltham, Mass.

CIRCLE NO. 557

EMR 6140 manual

The 6140 Mission-Matched computer system is described in a 20-page manual. The manual details ways in which the system performs concurrent real-time and background batch processing. It also describes the unit's unique architecture and flexible software usually found only on larger, more costly machines. The manual details hardware and software features, real-time applications, systems capabilities, a full range of available peripherals, and the systems instruction set. It is illustrated with photographs and diagrams. EMR Computer, Minneapolis, Minn.

CIRCLE NO. 558

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NEW LITERATURE

Power supplies

A 16-page, four-color catalog describes electronic instruments, power supplies and industrial controls. Products featured are laboratory bench power supplies, sub-unit power supplies, signal sources, telecommunications test equipment, digital and analog measuring instruments plus a digital logic instructional kit. Farnell Instruments Ltd., Yorkshire, U.K.

CIRCLE NO. 559

Microwave instruments

A microwave instrument catalog summarizes specifications for modular signal generators and signal sources, receivers, field intensity meters, antennas and spectrum analyzers. Polarad Electronic Instruments, Lake Success, N.Y.

CIRCLE NO. 560

Thermal cutoffs

The Microtemp thermal cutoffs are outlined in the six-page brochure MD-149. Micro Devices Corp., Dayton, Ohio.

CIRCLE NO. 561

General-purpose computer

The Model DC 6024/5, a 24-bit general-purpose computer, is featured in a two-color, 12-page brochure. Specifications, configurations and software are covered. Datacraft, Fort Lauderdale, Fla.

CIRCLE NO. 562

Control devices

All-solid-state control devices—timers, photoelectrics, resistance sensing relays and multiple relays—are described in a condensed catalog sheet. Regent Controls, Inc., Stamford, Conn.

CIRCLE NO. 563

Bisync analyzer

A specification sheet describes the Model 810 bisync line control analyzer. Paradyne Corp., Clearwater, Fla.

CIRCLE NO. 564

vendors report

Annual and interim reports can provide much more than financial-position information. They often include the first public disclosure of new products, new techniques and new directions of our vendors and customers. Further, they often contain superb analyses of segments of industry that a company serves.

Selected companies with recent reports are listed here with their main electronic products or services. For a copy, circle the indicated number.

Mohawk Data Sciences Corp. Data processing systems and peripherals, source data collection systems, keyboard switch assemblies and tape drives.

CIRCLE NO. 565

Tandy Corp. Consumer electronics, components, TV antennas, magnetic tapes and hobby kits.

CIRCLE NO. 566

Parker-Hannifin Corp. Aerospace and components.

CIRCLE NO. 567

General Automation, Inc. Mini-computers.

CIRCLE NO. 568

Avnet, Inc. Electronic components, entertainment and high-fidelity products and computers.

CIRCLE NO. 569

Western Digital Corp. MOS/LSI.

CIRCLE NO. 570

Systems Engineering Laboratories. Computers.

CIRCLE NO. 571

Beckman Instruments, Inc. Medical electronics, analytical and pollution control instruments, industrial instrumentation and components.

CIRCLE NO. 572

Lundy Electronics & Systems, Inc. Computers, military electronics and environmental systems.

CIRCLE NO. 573

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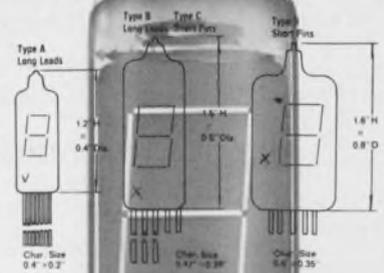
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DA-1200*	B	5	10	1,500	0.280"
DA-1300*	B	5	20	6,000	0.280"
DA-1600	B	12	30	85,000	0.280"
DA-2200*	C	5	10	1,500	0.230"
DA-2300	C	5	20	6,000	0.230"
DA-2600*	C	12	30	85,000	0.230"
DA-2900	D	5	20	5,000	0.468"

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• U.S. Agent: **DAIMETRICS CORPORATION**
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INFORMATION RETRIEVAL NUMBER 125

Plagued by Thyristor Noise?

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And with enough reason. Take insertion loss: they outperform ordinary noise-absorbing cores and coils by

20dB
(300 kHz—5MHz)

A unique advantage from Tokin design originality. And talking about design, size has been reduced—installation simplified. Is it any wonder, then, that Tokin SN Coils captured

95%

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Now you can afford to add instant graphic hard copy output to your data terminals, storage tubes, computer outputs, SSTV, scanning sensors.

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INFORMATION RETRIEVAL NUMBER 127

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INFORMATION RETRIEVAL NUMBER 128

ELECTRONIC DESIGN 1, January 4, 1973

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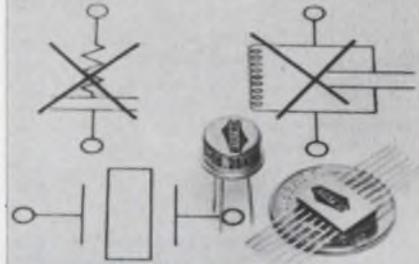
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Next, they're inexpensive. In production quantities, the cost may be lower than the less accurate, conventional LC/RC circuits you've been using. And high volume delivery is fast.

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Specifications

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Accuracy:

0 to 70°C 0.06%
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Better specifications available on request.

In addition, Statek offers low frequency standard or custom hybrid oscillators and filters.



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Phone: (714) 639-7810

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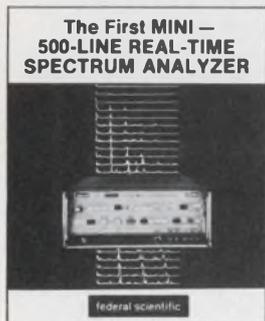
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Advertisements of booklets, brochures, catalogs and data sheets. To order use Reader-Service Card. (Advertisement)

500-line Real-Time Spectrum Analyzer Acts Like 650-Lines

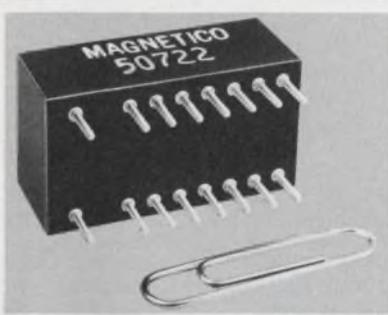


Second generation Mini-Ubiq™ Model UA-15A low frequency real-time spectrum analyzer — smaller, lighter, easier to use and less expensive than Federal's famous Ubiquitous® 500-line analyzer — is better for on-the-spot frequency analysis, machine noise diagnosis, computer automatic systems. Incorporates a sharper, computer-designed filter for increased selectivity — can separate closely spaced components as if it had 650 frequency lines. Widest choice of range — 12 ranges from 10Hz to 50kHz; highest frequency and amplitude accuracy; computer control of input amplitude range, analysis range, and presampling filter; operation with weighting function on or off; sweep termination adjustable for high sweep rates; earphone monitor of filtered input.

Federal Scientific Corp.

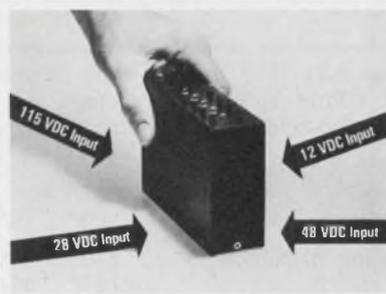
615 West 131st Street, New York, N. Y. 10027
(212) 286-4400

CIRCLE NO. 171



Scott-T-Transformers — Miniature size 13/16 x 1-1/2 x 5/8, input 90 or 11.8 volts, line to line, 400 Hz, output sine and cosine, 60 secs. accuracy, cost \$19. in quantity. Write for standard literature. Synchro to resolver & resolver to synchro. Magnético, Inc., East Northport, N.Y. 11731. (516)-261-4502.

INFORMATION RETRIEVAL NUMBER 181



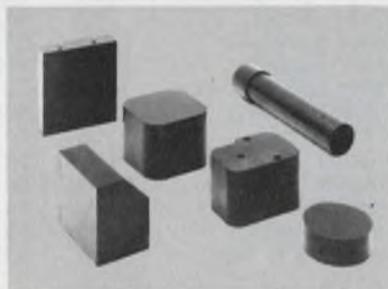
DC-DC Regulated Power Converters — loaded with power (6 watts/in³) and packed into pretested, encapsulated miniature packages. Modular design allows you to specify your own custom system without engineering charges. Inputs of 12, 28, 48, & 115 VDC with up to 6 outputs. Arnold Magnetics, Culver City, Ca. 90230. (213) 870-7014.

INFORMATION RETRIEVAL NUMBER 182



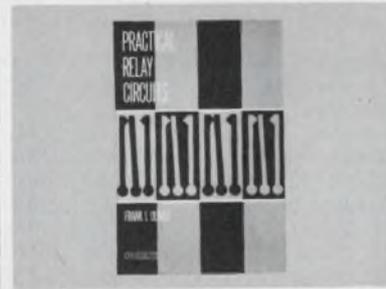
Thin-Trim® variable capacitors are designed to replace fixed tuning techniques. Applications include crystal oscillators, CATV amplifiers, communication and test equipment. Series 9410 has high Q's with five capacitance ranges from 1.0 - 4.5 pf to 10.0 - 50.0 pf. Johanson Manufacturing Corporation, Boonton, N. J. (201) 334-2676

INFORMATION RETRIEVAL NUMBER 183



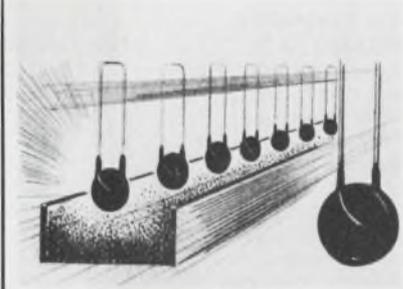
Glass laminated epoxy 155°C cases for component and circuit packaging are available in thousands of sizes. Thin wall tubes and headers offer optimum protection in all applications. Literature and samples available. Stevens Tubing Corp., 128 North Park Street, East Orange, New Jersey 07019. Telephone 201-672-2140.

INFORMATION RETRIEVAL NUMBER 184



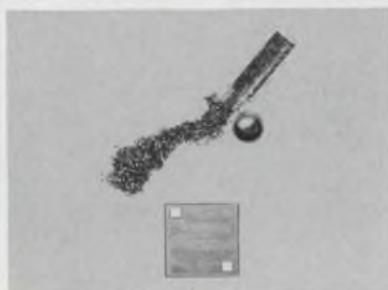
Practical Relay Circuits, by Frank J. Oliver. Time-saving guide classifies relays by function, presenting a rapid overview of the circuits that can solve the problem at hand. 384 pp., illus., cloth, \$14.95. Circle below for 15-day examination copies. Hayden Book Co., New York, N.Y. 10011.

INFORMATION RETRIEVAL NUMBER 185



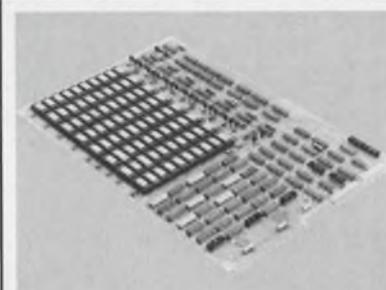
New Amicon Epoxy Powder. 30 second gel . . . 1 minute cure. Novaloy® Powders are outstanding for packaging delicate heat sensitive parts. Cures as low as 120°C. Fast cures with controlled flow, high gloss finish. Avail. in dip and electrostatic spray grades. Lit avail. from Amicon Corp., Polymer Prod. Div., Lexington, Ma. 02173. (617) 861-9600.

INFORMATION RETRIEVAL NUMBER 186



30 Mil Thin Film Chip Resistors up to 10 megohms are now available from Semi-Films Technology. Resistive material is improved tantalum nitride with greatly increased sheet resistivity. This new technology retains the stable properties inherent in the tantalum nitride process. Semi-Films Tech. Corp., Box 188, West Hurley, N.Y. 12491. 914-338-7714.

INFORMATION RETRIEVAL NUMBER 187



Low cost semiconductor memory system monostore IV/Planar 4K x 20 on a single card 9-3/4" x 14". Cycle 650 ns. Includes timing control, refresh, address register, decoding, sense and memory array. TTL compatible. 0.5" card spacing. 4Kx16 \$900 from stock. Monolithic Systems Corp., Englewood, Co. 80110 (303) 761-2275.

INFORMATION RETRIEVAL NUMBER 188



COS/MOS Pulse Generator—Features Squarewaves 1Hz-1MHz/Pulse-widths 1μs - 1 sec./"D" FF with S & R/Non-Capacitive Differentiator/Level Detector/"De-bounced" Push button. Q & Q outputs and complementary inputs available all functions. 3 - 15V circuit supply. Ideal as bench and built-in test equip. \$125. American Laser Systems. (805) 687-1212

INFORMATION RETRIEVAL NUMBER 189

product index

Information Retrieval Service. New Products, Evaluation Samples (ES), Design Aids (DA), Application Notes (AN), and New Literature (NL) in this issue are listed here with page and Information Retrieval numbers. Reader requests will be promptly processed by computer and mailed to the manufacturer within three days.

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There's plenty more where these

came from.

Literally, thousands more.

Actually, the odds are in your favor that we have the unlighted pushbuttons you need, right-off-the-shelf.

Our secret is interchangeable parts. Pushbutton modules. Switch modules (including hermetically sealed units and high/low temperature versions). Facenuts.

Even a selection of colored buttons.

We also give you a choice of momentary or alternate action. Or a combination of both. And finally, a pick of one, two, three or four pole circuitry.

Which gives you the opportunity to customize your panel — front and back. To make it the way you want it. And to do it economically.

For more information, call your MICRO SWITCH Branch Office or Authorized Distributor (Yellow Pages under "Switches, Electric").

Or write for Catalog 51.



MICRO SWITCH

FREEPORT, ILLINOIS 61032

A DIVISION OF HONEYWELL

MICRO SWITCH products are available worldwide through Honeywell International.

INFORMATION RETRIEVAL NUMBER 131



1973 SUPER TOP TEN CONTEST RULES

Reader Contest

PICK THE TOP TEN ADVERTISEMENTS IN THIS ISSUE . . . WIN A WINDJAMMER CRUISE FOR TWO . . . \$1,000 CASH . . . FREE JET FLIGHT . . . FREE RERUNS OF YOUR COMPANY'S AD . . . 100 PRIZES IN ALL.

Examine this issue of *Electronic Design* with extra care. Pick the ten advertisements that you think will be best remembered by your fellow engineer-subscribers. List these ten advertisements on the special entry form bound in at right. (Be sure to check the box marked "Reader Contest.")

Your selections will be measured against the ten ads ranking highest in the "Recall Seen" category of Reader Recall — *Electronic Design's* method of measuring readership. In making your choices do not include "house" advertisements placed by *Electronic Design* or Hayden Publishing Company, Inc. (such as this ad describing the contest). Don't miss your chance to be a Top Ten Winner! All entries must be postmarked no later than midnight, February 15, 1973. Winners will be notified in March 1973.

READER CONTEST RULES

1. Enter your *Top Ten* selections on the entry blank provided, or on any reasonable facsimile. Be sure to indicate the name of the advertiser and *Information Retrieval Number* for each of your choices. Do not use page number. (Ads placed by Hayden Publishing Company in *Electronic Design* should not be considered in this contest.)

2. No more than one entry may be submitted by any one individual. Entry blank must be filled in completely, or it will not be considered. The box on the entry blank marked "Reader Contest" must be checked. *Electronic Design* will pay postage for official entry blanks only.

3. To enter, readers must be engaged in electronic design engineering work, either by carrying out or supervising design engineering or by setting standards for design components and materials.

4. No cash payments, or other substitutes, will be made in lieu of any prize, (except the \$1,000 prize).

5. Contest void where prohibited or taxed by law. Liability for any taxes on prizes is the sole responsibility of the winners.

6. Entries will be compared with the "Recall Seen" category of Reader Recall (*Electronic Design's* method of measuring readership). That entry which in the opinion of the judges most closely matches the "Recall Seen" rank, will be declared the winner.

7. In case of a tie, the earliest postmark will determine the winner. Decisions of *Top Ten* contest judges will be final.

8. Free reruns of any advertisement will be made only from existing plates or negatives. If the advertisement qualifying for a free rerun is an insert, the winner's company may run a two-page spread from existing plates or negatives in up to 4-colors.

9. Hayden Publishing Company, Inc. reserves the right to schedule reruns at its discretion.

**FOR A COMPLETE DESCRIPTION OF PRIZES
FOR BOTH READER AND ADVERTISER CONTESTS
SEE PAGES 74 AND 75**

USE SPECIAL ENTRY BLANK BOUND IN AT RIGHT

(Additional entry blanks are bound inside the front cover)

Advertiser Contest

PICK THE TOP TEN ADVERTISEMENTS IN THIS ISSUE . . . WIN A WINDJAMMER CRUISE FOR TWO . . . \$1,000 CASH . . . FREE JET FLIGHT . . . COLOR TV . . . BULOVA TIMEPIECE.

There's a separate contest open to all marketing and advertising personnel in companies, and to advertising agencies.

Examine this issue of *Electronic Design* with extra care. Pick the ten advertisements that you think will be best remembered by *Electronic Design's* readers. List these ten advertisements on the special entry blank bound in the front or back of this issue. (Be sure to check the box marked "Advertiser Contest".)

In addition to valuable prizes, all ads that place in the *Top Ten* will be given free reruns. If you are a winner in the advertiser contest, and if you ran an ad in the January 4 issue that did not place in the *Top Ten*, that advertisement, or a like ad of your choice, will be given a free rerun. See rules if the winning ad is an insert.

ADVERTISER CONTEST RULES

1. All rules for the Reader Contest will similarly apply for this contest, with two exceptions: readers engaged in electronic design engineering work, as defined in the reader contest rules, are not eligible to participate in this special contest. The box on the entry blank marked "Advertiser Contest" must be checked.

2. Entrants in this contest may use the official reader contest entry blanks or any reasonable facsimile.

3. This special contest is open to marketing and advertising personnel only at all manufacturing companies and advertising agencies whether or not their companies or agencies have an advertisement in the January 4, 1973 issue. However, only those companies (or divisions thereof) advertising in the Jan. 4 issue, and the advertising agencies placing such advertisements are eligible for a free rerun of their advertisement should a member of their organization win.

4. Free reruns of any advertisement will be made only from existing plates or negatives. If the advertisement qualifying for a free rerun is an insert, the winner may run a two-page spread from existing plates or negatives in up to 4-colors.

5. Hayden Publishing Company, Inc., reserves the right to schedule reruns at its discretion.

**FOR A COMPLETE DESCRIPTION OF PRIZES
FOR BOTH READER AND ADVERTISER CONTESTS
SEE PAGES 74 AND 75**

USE SPECIAL ENTRY BLANK BOUND IN AT RIGHT

(Additional entry blanks are bound inside the front cover)

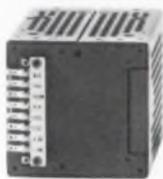
Do you face a make or buy decision on power supplies?

BUY LAMBDA LX SERIES

Choose from 7 packages, 39 models
All 1-day delivery. All guaranteed 5 years

"3" PACKAGE

DUAL OUTPUT . . . \$85
±15 TO ±12 VOLTS 0.4 AMPS



"A" PACKAGE

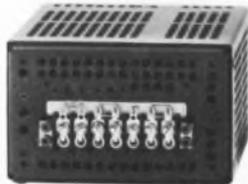
SINGLE OUTPUT . . . \$85
5 VOLTS 4 AMPS (with O.V.)



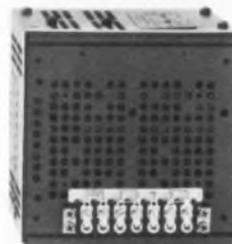
DUAL OUTPUT . . . \$125
±15 TO ±12 VOLTS 1 AMP

"B" PACKAGE

SINGLE OUTPUT . . . \$125
5 VOLTS 5.8 AMPS (with O.V.)



DUAL OUTPUT . . . \$150
±15 TO ±12 VOLTS 1.6 AMPS

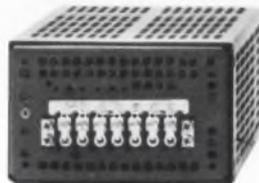


"4" PACKAGE

SINGLE OUTPUT . . . \$135
5 VOLTS 7.4 AMPS (with O.V.)

"C" PACKAGE

SINGLE OUTPUT . . . \$150
5 VOLTS 9 AMPS (with O.V.)



DUAL OUTPUT . . . \$160
±15 TO ±12 VOLTS 2.5 AMPS



"CC" PACKAGE

SINGLE OUTPUT . . . \$200
5 VOLTS 16 AMPS (with O.V.)

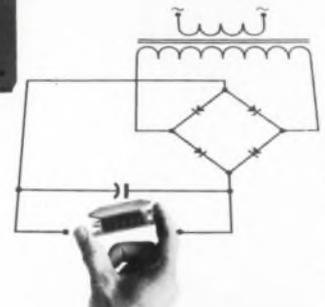
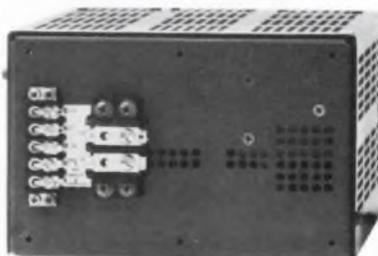
DUAL OUTPUT . . . \$235
±15 TO ±12 VOLTS 4.0 AMPS

"D" PACKAGE

SINGLE OUTPUT . . . \$235.
5 VOLTS 27.5 AMPS (with O.V.)

DUAL OUTPUT . . . \$280
±15 TO ±12 VOLTS 6.2 AMPS

TRIPLE OUTPUT . . . \$375
±15 TO ±12 VOLTS 3.1 AMPS
5 ± 5% VOLTS 12 AMPS
(with O.V.)



**WHETHER
YOU MAKE
OR BUY...**

LAMBDA
ELECTRONICS CORP.

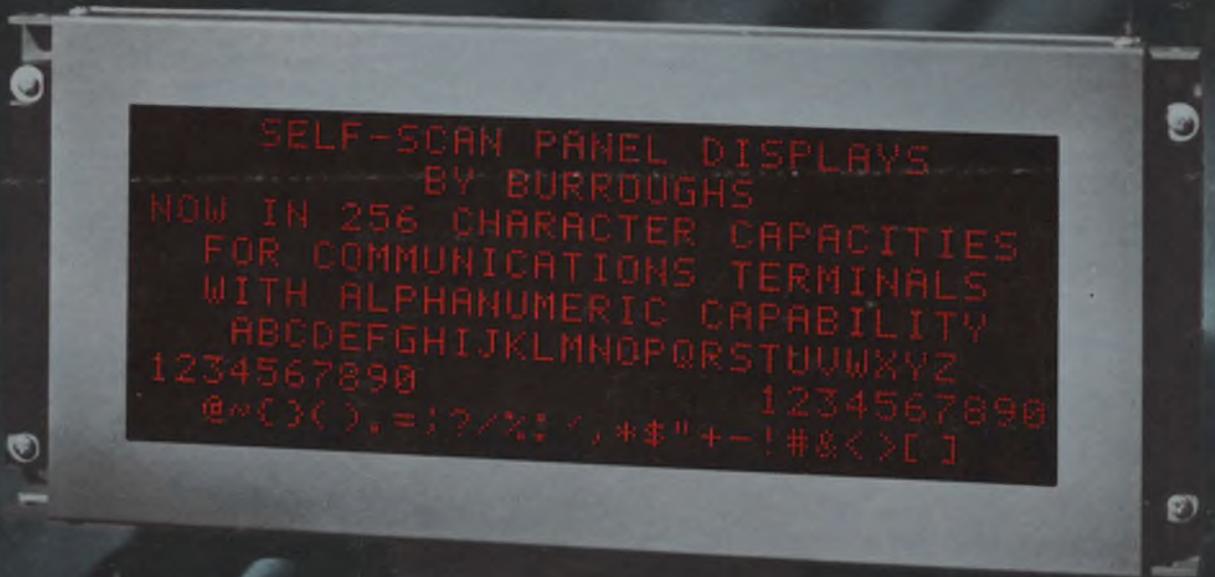
A Veeco Company

Line regulation 0.1% Load regulation 0.1%
Ripple and noise 1.5 mV RMS, 5 mV P-P with either positive or negative terminal grounded
AC input 105-132 VAC; 47-440 Hz
All 5-volt models include built-in overvoltage protection.
For information on other models up to 28 VDC, send for catalog.

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INFORMATION RETRIEVAL NUMBER 243

SELLS ON SIGHT



superior readability that competitors can't match

One look at an operating SELF-SCAN[®] panel display and you will know why you should be featuring one in your system. SELF-SCAN displays are a new solution to the operator machine interface that provides advantages to the system builder, to the system user, and to the system operator.

You can offer your customer the advantage of a custom-stylized unit that his operators can use efficiently. SELF-SCAN panels are measurably superior to CRT for operator accuracy while significantly reducing fatigue level in day in-day out high volume production applications.

The 0.2" high characters are in the popular 5x7 dot matrix format and are made up of dots on .040" centers. The unit is ASCII compatible and displays a modified 64-character ASCII character set.

256-character display subsystems are available from stock for immediate delivery. Call or write Burroughs Corporation, Electronic Components Division, Box 1226, Plainfield, New Jersey 07061, Phone: (201) 757-3400. Ask to have a Burroughs sales engineer stop by your office and show you his 256-character SELF-SCAN panel, keyboard, and power supplies packaged in a standard Samsonite[®] briefcase.

Burroughs 