

Photon-coupled devices emerge as major elements in computer, control and instrumentation data links. In these circuits, optical couplers suppress common-mode

interference, permit mixed logic interfacing and give high-voltage isolation. A host of nonstandard devices makes selection tough. Watch the tradeoffs. See p. 26.





FILM RESISTOR DALE SUPERMARKET

Everything you've always wanted to know about film resistors...but didn't know who to ask

You can do a lot more with Dale Film Resistors—and we're ready to send you a chart that proves it. Adding the Welwyn Group to our film resistor lines lets you rely on Dale for practically every resistance function in the book—and opens up new possibilities for saving time and cash.

Dale's expanded film resistor line now includes everything from the most exotic, to the least expensive. For example:

HIGHER VALUES—glass enclosed metal oxide film resistors to 1 billion ohms at 1% tolerance.

LOWER VALUES—down to .27 ohms at 1% tolerance.

HIGHER VOLTAGES—to 50KV pulse, 14KV continuous, with values to 150KM.

LOW-COST POWER—3 through 10 watt styles, 2%, 5% with flameproof coating.

CARBON COMP. COMPETITION—Beyschlag (W. Germany) carbon film resistors. Up to 2 watts in 2%, 5% tolerance.

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FILM RESISTOR GUIDE

*The Industry's
Broadest Range
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Faster from...*

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DALE**

DALE ELECTRONICS, INC.

1300 28th Avenue, Columbus, Nebraska 68601

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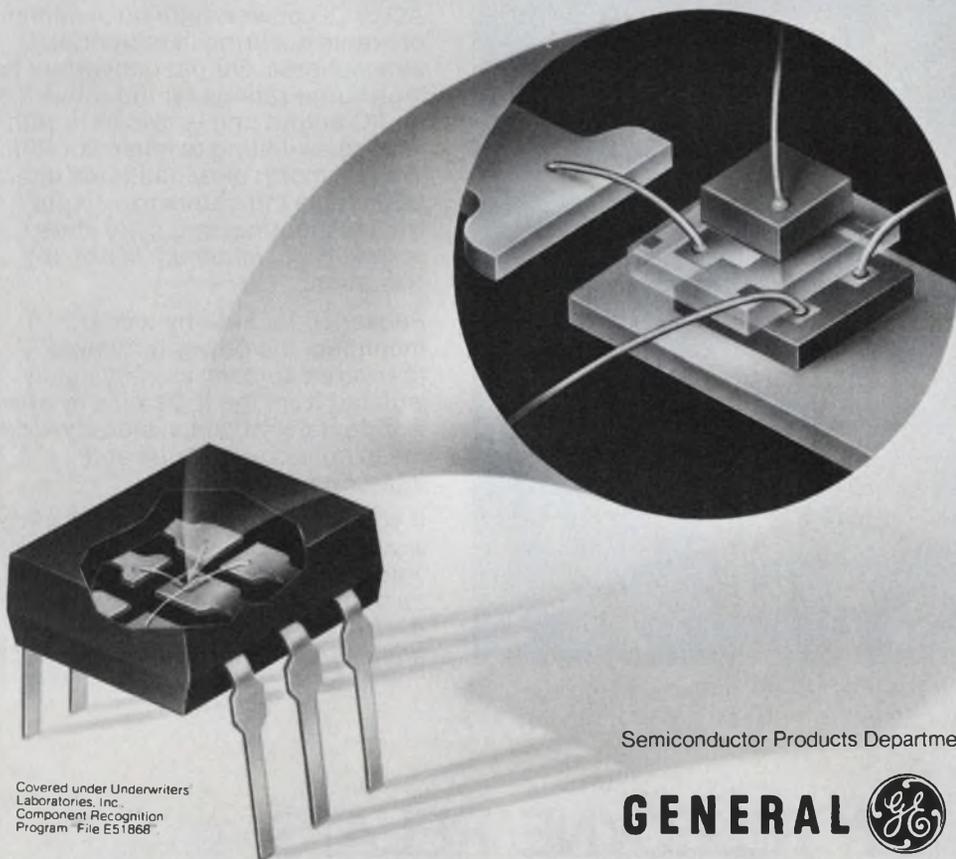
3,500 VOLT ISOLATION 100% CURRENT TRANSFER OPTO COUPLER

HOW GENERAL ELECTRIC DOES IT

General Electric's unique glass isolation produces precise alignment and controlled spacing between the LED and the silicon detector thus optimizing photon coupling...minimizing the effect of the inverse relationship of isolation voltage and current transfer ratio...and yielding optoelectronic couplers with BOTH high isolation voltage and high current transfer ratios.

3 new models 4N35, 36, 37 are characterized for high isolation voltage and high current transfer ratios. 4N35 offers 3,500 volts (peak) and 100% transfer ratio for \$1.85 each in 1,000 lot quantities.

Available now from any authorized GE Semiconductor distributor or GE Electronic Components Sales Office.



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Semiconductor Products Department, Syracuse, New York.

GENERAL  **ELECTRIC**

Teledyne in solid control

AC and DC I/O converters for programmable controllers



The boundary of the minicomputer mainframe or CPU world — of sensitive IC logic families — and the process control or machine tool world of motors, solenoids, lamps, and electro-mechanical switches is a tough place, demanding devices for fast quiet switching and load sensing — reliably.

Teledyne, the world's leader in solid state relays, offers the 671 series AC or DC input and output converter modules — state of the art in circuitry and packaging.

ALL SOLID STATE, the 671's are optically isolated between logic and AC or DC power; high noise immunity prevents misfiring in industrial atmospheres. Output converters have high surge ratings for inductive loads; an AC output unit is available with zero voltage switching to minimize RFI. There's more: easy multiplex operation, LED status indicators for simple troubleshooting, and solid state reliability . . . *minimum* life of 10^8 operations.

Packaged for side-by-side panel mounting, the power terminals (barriered screws) are physically isolated from the logic pins to prevent accidental intrusions; side-by-side units mean no terminal strips and interconnect wiring.

If you're in the mainframe business and want to offer process control, or if you're in the processing world and want computer control, write or call about the 671 series; our application engineers will put you in solid control.

 **TELEDYNE RELAYS**

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INFORMATION RETRIEVAL NUMBER 2

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Cover: Photo taken by Art Director, Bill Kelly.

- **Independent control of pulse high and low levels**
- **Pulse amplitude to 5 volts**
- **Output window +5 V to -5 V**
- **Less than 1 ns risetime**
- **250 MHz rep rate**

The Tektronix PG 502 Pulse Generator is a high performance instrument ideal for designing, testing, or maintaining the logic circuitry in high-speed digital computers, and similar applications. It is a general purpose signal source with rise and fall times less than 1 ns. Both the pulse duration and period of the PG 502 output can be controlled and independent control of the pulse high and low levels is offered. The trigger circuit includes external trigger input, manual triggers, and pre-trigger output.

Tektronix offers a range of signal sources in addition to the PG 502.

- FG 501 Function generator; 0.001 Hz to 1 MHz, five waveforms \$ 325
- FG 502 Function generator; 0.1 Hz to 11 MHz, 25 ns rise and fall, five waveforms \$ 425
- PG 501 Pulse generator; 5 Hz to 50 MHz, 3.5 ns rise and fall \$ 295
- PG 502 Pulse generator; 250 MHz, 1 ns rise and fall, independently controllable logic 1 and 0 levels \$ 995
- PG 505 Pulse generator; 100 kHz, 80 V floating output, independently variable rise and fall times \$ 265
- RG 501 Ramp generator; 10- μ s-to-10-s ramp, with four scope type trigger controls . . \$ 175

Signal Sources: Another way to think of Tektronix

SG 502 RC oscillator; 5 Hz to 500 kHz, sine and square-waves, 0.1% distortion \$ 295

SG 503 Sine-wave oscillator; regulated, constant-amplitude variable from 250 kHz to 250 MHz \$ 600

TG 501 Time-mark generator; 1-ns-to-5-s markers, measures timing errors with resolution within 0.1% over timing-error range of 7.5% \$ 650

Signal sources are just one category of instruments in the Tektronix TM 500 Series. Presently, 24 general purpose modular test and measurement instruments are available including digital counters, digital multimeters, power supplies, signal processors, and CRT

monitors. These interchangeable instruments plug into power units with single (\$115) or triple (\$150) compartments. In the triple compartment power unit, the modules can be interconnected via a common interface board and optional rear panel connectors. This results in increased intermodule capabilities and can actually produce a synergistic effect. The modularity feature also saves bench space. The TM 500 Series is based on the latest technology and proven principles developed in building oscilloscopes.

Send for a free brochure and spec sheets on signal sources, and Tektronix other TM 500 test and measurement instruments. They're all new ways to think of Tektronix!

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P. O. Box 500
Beaverton, Oregon 97005
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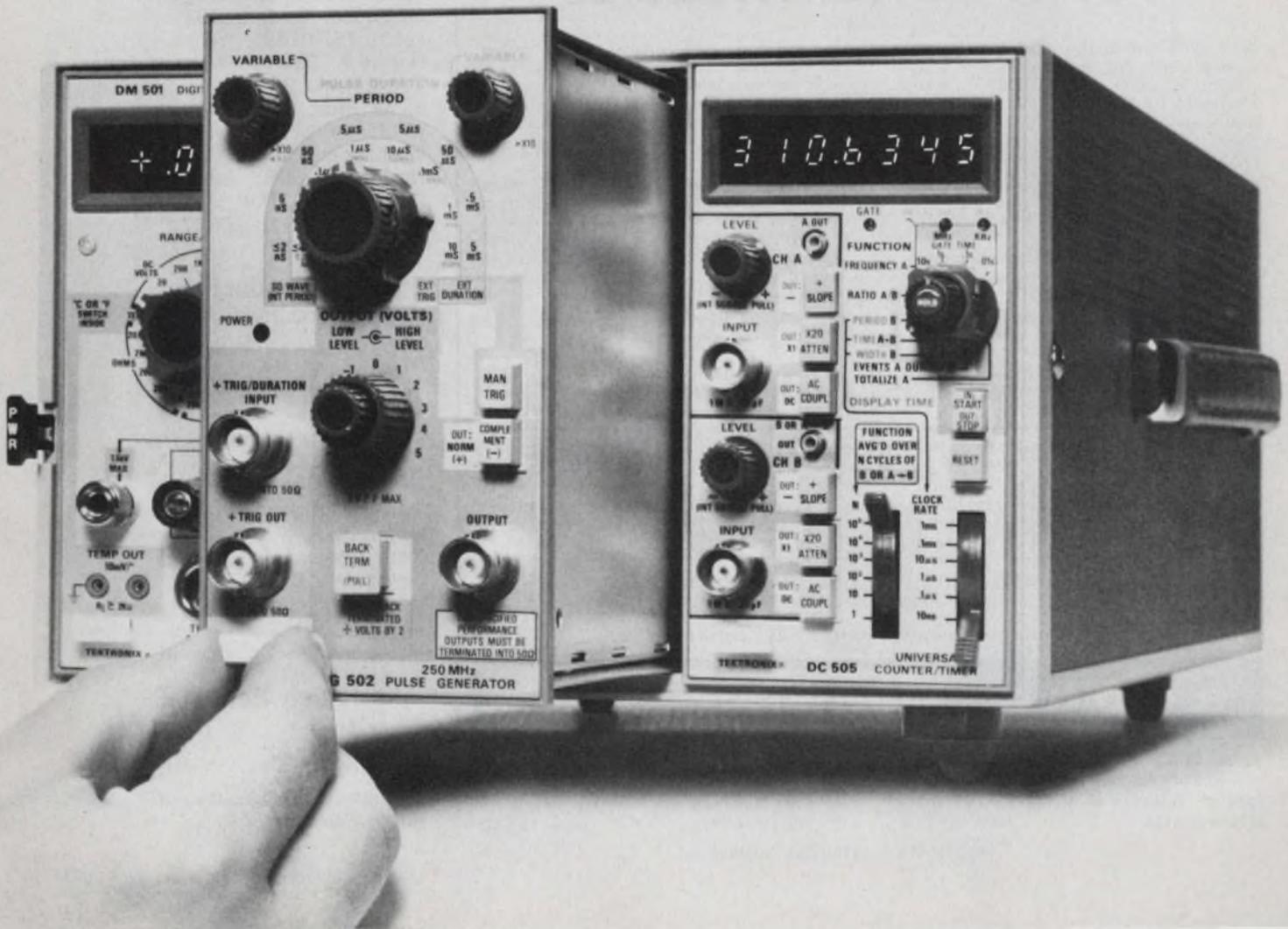


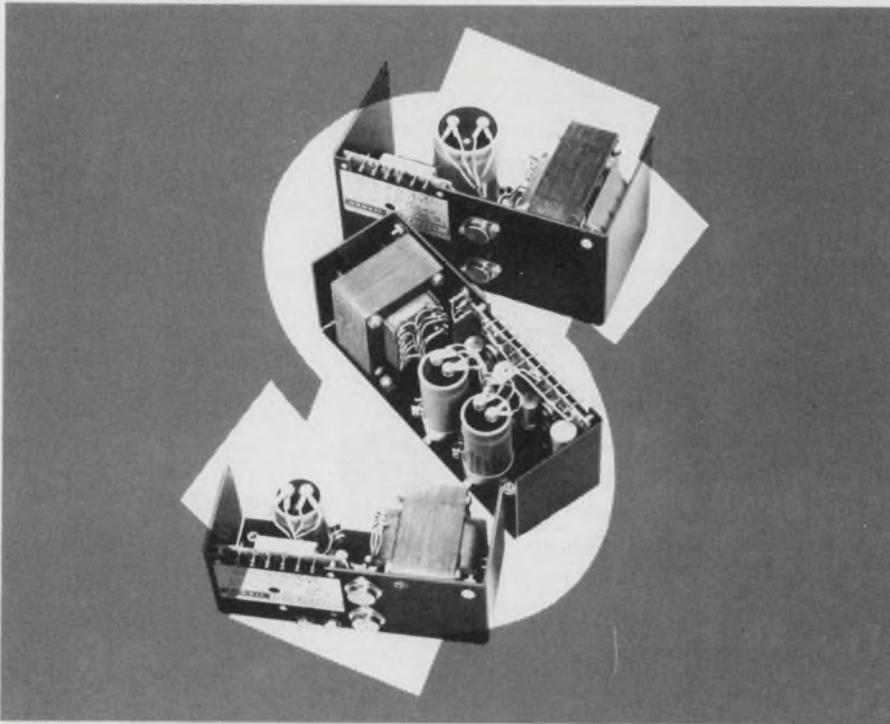
INFORMATION RETRIEVAL NUMBER 4
FOR DEMONSTRATION, CIRCLE 151

Digital Multimeter
Price, \$395

Pulse Generator
Price, \$995

Counter
Price, \$1,195





Start Getting Your Money\$worth Out of Power Modules

Now, you can really start getting your moneysworth out of power modules with Abbott's new LOW COST series. Designed to give you 100,000 hours of trouble-free operation (that's 11½ years), these reliable units meet the needs of OEM engineers. Their purchase price is about \$7 per year of service. The model LC series feature:

- 47-420 Hz Input Frequency
- 0.1% Regulation
- +50°C. Ambient Operation
- Single and Dual Outputs
- 1 Day Stock Delivery

These units provide more quality per dollar compared to similar items on the market. See table below for prices on some of our LC models. Many other LC models are listed in our catalog.

If analyzing the many similar power supplies on the market is confusing; if you are concerned about the long-term reliability of those units, then decide on an Abbott power supply for your system. Your best buy in OEM power modules is ABBOTT.

Abbott also manufactures 3,000 other models of power supplies with output voltages from 5 to 740 VDC and with output currents from 2 milliamps to 20 amps. They are all listed with prices in the new Abbott Catalog with various inputs:

- 60 to DC
- 400 to DC
- 28 VDC to DC
- 28 VDC to 400
- 12-24 VDC to 60

5V @ 6 Amps	5V @ 10 Amps	12V @ 10 Amps	15V @ 4 Amps	28V @ 1 Amp	±12V @ 1.2 Amps	±15V @ 4 Amps
LC5T6	LC5T10	LC12T10	LC15T4	LC28T1	LLC12T1.2	LLC15T4
\$72	\$81	\$99	\$81	\$72	\$99	\$135

Please see pages 581-593 of your 1973-74 EEM (ELECTRONIC ENGINEERS MASTER Catalog) for complete information on Abbott Modules.

Send for our new 56 page FREE catalog.

abbott transistor

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INFORMATION RETRIEVAL NUMBER 5

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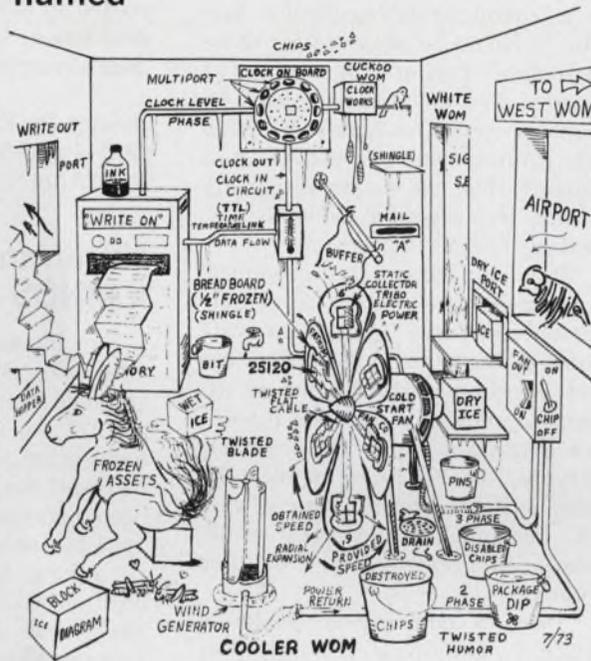
White WOMman named

The man destined to become famous immediately has become famous—if not immediately, at least after a short while. In its highly educational advertisement headlined "Become Famous Immediately" (ED No. 13, June 21, 1973, pp. 67-74), Signetics promised not mere fame, but immortality, to the person who figured out the best use for its 25120 WOM. That fortunate person would have a WOM named after him.

Since this Write-Only Memory has an endless variety of applications, the challenge was no small one—but it was finally mastered by Robert A. White of Albuquerque, N.M. He pointed out, understandably, that the schematic and wiring diagrams of the multiport WHITE WOM (Cooler WOM) were business secrets that could not be disclosed. But he furnished the application diagram, shown here for the first time in history. Well-versed readers will immediately recognize that summer snow (job) production is one of its many functions.

Though White walked off with the honors of immortality, in that a WOM now bears his name, others provided notable contributions. Here are some excerpts. Accompanying illustrations, schematics and truth tables have been entered in a WOM.

"After all, it, like any other sci-



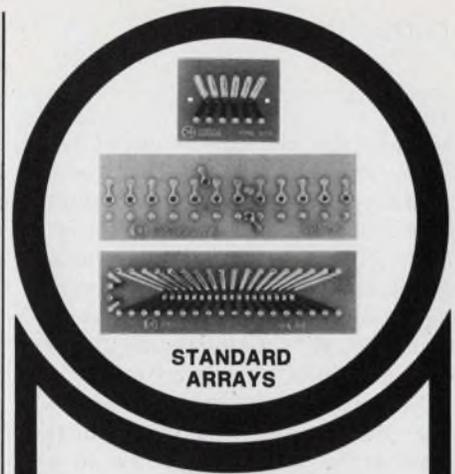
entific break-in, can be misused. Even the atomic bomb has been used in ways which endangered the health of some people."—C. A. Irvine, *The National Cash Register Co.*

"An ideal use would be allowing a few data sheets and a sample or two to leak to a Soviet agent. If it causes as much misspent time over there as it has around here, you will have indeed done an inestimable service to your government, to say nothing of possibly helping provide victory against them dirty, rotten Commie aggressors."—William Nurnberger, *Dept. of the Navy.*

"In the rare event that stored data need be retrieved, hypnosis of the original author, or even of the WOM, may not be attempted. Sodium pentathol (truth serum) may be injected up the drain (pardon

(continued on page 8)

Electronic Design welcomes the opinions of its readers on the issues raised in the magazine's editorial columns. Address letters to Managing Editor, Electronic Design, 50 Essex St. Rochelle Park, N.J. 07662. Try to keep letters under 200 words. Letters must be signed. Names will be withheld on request.



OPTRON OPTOELECTRONIC ARRAYS

IMMEDIATE DELIVERY
COMPETITIVE PRICING
CUSTOM CAPABILITIES

OPTRON sensor and emitter arrays are ideal for information input for such applications as tape readers, card readers, shaft encoders, level indicators, optical character recognition, etc.

They consist of discrete LED's and phototransistors in microminiature, hermetically sealed packages with collimating glass lenses and are mounted in printed circuit boards. This design enables pre-screening and tight matching of LED's and sensors, as well as accurate location to mounting holes.

Standard OPTRON arrays are available from stock with six and nine channels on 0.100" centers for tape readers, and with 12 channels on 0.250" centers and 18 channels on 0.087" centers for card readers. With a spacing of 0.100" between emitter and sensor arrays and an input of 30 mA, a typical output of 4 mA assures TTL compatibility.



In addition to standard arrays, OPTRON specializes in custom designed arrays (photo, above) to the most exacting specifications. All arrays, either single or in matched sensor-emitter pairs, are delivered tested and ready for installation.

Detailed technical data on standard arrays as well as other OPTRON products... chips, discrete components and assemblies... is available from your OPTRON sales representative or the factory direct.



OPTRON, INC.

1201 Tappan Circle
Carrollton, Texas 75006
214/242-6571

(continued from page 7)

the expression) if required."—*James Rieger, Dept. of the Navy.*

"Many programmable calculators have the ability to use subroutines. This is a dangerous waste of valuable memory space. Never-used subroutines could be stored in the WOM."—*Gary Davis, Davis Photographics and Electronics.*

"Scientists and engineers have long been taught that they must never erase incorrect entries in a notebook, but rather, cross them out. The Signetics WOM makes it possible to store incorrect entries—to the vast relief of science teachers and patent attorneys."—*Paul Wiener, Burroughs Corp.*

"Error-detecting codes and programs shall be employed such that a reasonable percentage of error bits shall be detected. These bits shall then be written into the WOM. As these bits are detected and stored in the WOM, they cannot be used again. Since the errors are taken out of circulation, the system will gradually improve and show a decreasing error rate."—*Peter Lefferts, Electro Audio Research.*

"You can use the WOM as an ecologically sound solution to the ear pollution from many standard broadcast stations. The program line is broken at the input to the transmitter. The offending signal is digitized and the digital signal fed to the WOM."—*W. J. J. Hoge, Nashville Audio Group.*

"You said that neatness counts, so I showered and shaved before writing this letter."—*Summer Weisman, Electrodyne.*

"Package the WOM with a tube of rubber cement and sell the package to automobile service stations as wheel-balancing kits. The stations could then advertise wheel balancing by computer technology."—*Larry LaCourse, Computer and Communications Service.*

"When I first heard about the Signetics fully encoded 9046 × n random access, write-only memory, I thought it was a gigantic hoax. But then I recalled that I thought waveguides were a hoax when they were first introduced (I still do). So I checked them out with an ohmmeter and I must admit that they passed the same test that the

original waveguide did, so they must be real."—*John A. Piper, Sanders Associates.*

"The WOM can be used to supplement the conventional memory in a computer-dating-service system. It would be reserved for those customers listing themselves as virgins. The advantage is twofold. First, there is no reason to recall this information, and second, it is unlikely that the memory capacity would be exceeded."—*Barry E. Becker, Circuit Technology.*

"It finally allows the economical implementation of the IF (Intermittent Failure) gate. This gate fails to function arbitrarily but recovers immediately prior to attempted repair. Due to its innocuous appearance and unfathomable purpose, the 25120 is an ideal IF gate, suitable for all state-of-the-art, designed-obsolescence products."—*Liebermann & Co., Los Angeles.*

"Two WOMs Never Make a Write."—*Andy Kyle, Houston, Tex.*

Gray spots noted in 'load of wash'

"Name Withheld's" letter headlined "Laundry Editorial Brings a Load of Wash" (ED No. 21, Oct. 11, 1973, p. 11) raises several questions. The example involving Fairchild's faster diode arrays and HP curve tracers might seem to imply some special knowledge, but what it indicates to me is a special ignorance (or perhaps a specially unfortunate random choice of examples). Fairchild does not sell diode arrays—fast, slow or in between—to HP. Individual diodes, yes; LED arrays, sometimes.

Further HP does not build and has not built curve tracers; if we had ever sold any to Fairchild, it would have had to be secondhand ones. Fairchild used to build its own, of course; we did buy a few of those. But that may not be really pertinent.

The writer speaks about the "last-look"/auction mode of procurement. The letter claims that "every major purchase" is involved with this practice, one for which

we all agree there are very few justifiable moral arguments. It does happen that HP's approach to corporate procurement contracts, has, for over 10 years, succeeded in avoiding the very pitfalls mentioned. It can be and is being done successfully.

Lawrence W. Johnson

Hewlett-Packard
1501 Page Mill Rd.
Palo Alto, Calif. 94304

Nitron marketing a MNOS memory

For the article "MNOS Memory Upstaging MOS and Fixed Heads in Some Areas" (ED No. 18, Sept. 1, 1973) to represent fully what is happening in the industry, it should be mentioned that Nitron Corp. has been marketing two versions of a 1024-bit nonvolatile MNOS memory during 1973. In contrast with most MNOS memory work, which has been Government-sponsored, these products were developed with in-house funding and made available to the commercial market.

*A. C. Tickle
Manager*

*Advanced Product Development
Nitron Corp.
10420 Bubb Rd.
Cupertino, Calif. 95014*

Ed. Note: Nitron did not announce the availability of its 1024-bit MNOS memories until Sept. 20, and thus it was not included in ELECTRONIC DESIGN's Sept. 1 article.

A slip spotted in subroutine

This letter is in reference to the article "How to Build a Microcomputer" (ED No. 19, Sept. 13, 1973, pp. 60-65). The subroutine—DECHL, for decrementing the combined H and L register memory address—shown in Table 2, p. 62, requires that the accumulator (A register) contain the contents of the L register before the CPI 377B instruction is executed. The LAL instruction must be inserted between the DCL instruction and the CPI 377B instruction for this

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MEASUREMENT COMPUTATION

innovations from Hewlett-Packard

NEWS

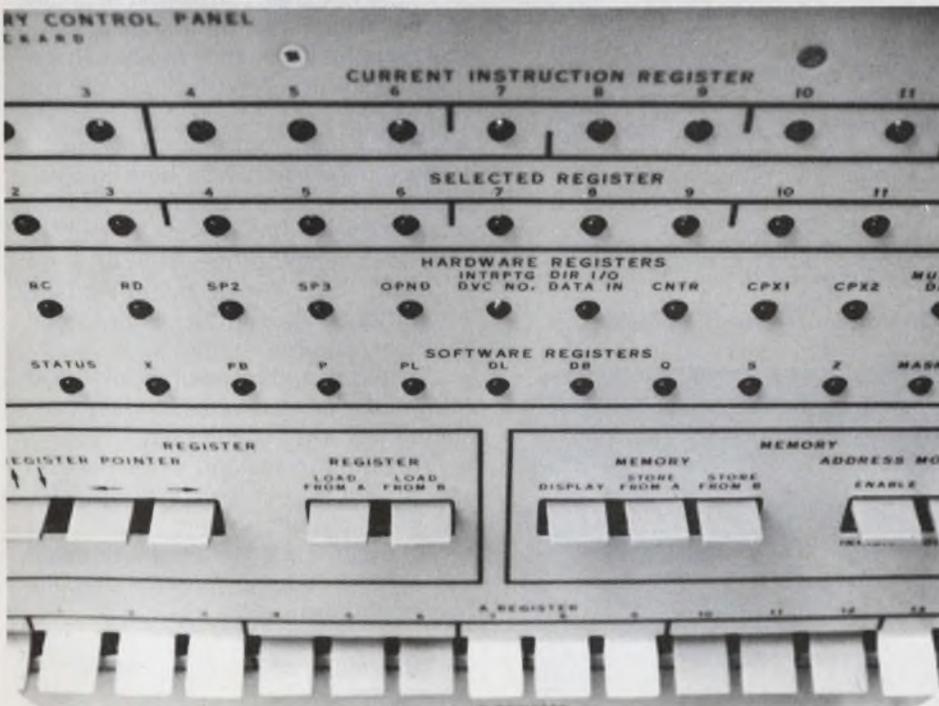
FEBRUARY, 1974

in this issue

Learn about logic

New solution to
component test problems

Two new oscilloscopes



New, large computer concept at a small system price

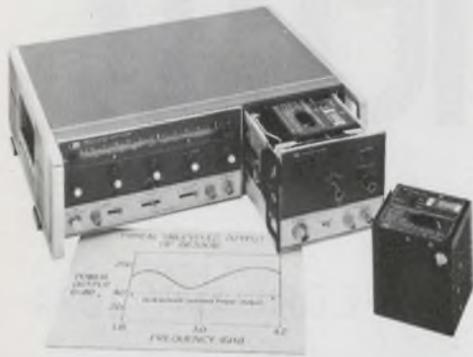
The HP 3000 multiprogramming, multilingual computer system gives you flexible, advanced computing capability at a price no other system can match.

Built around a unique operating system, the new HP 3000 multiprogramming system provides powerful computational capabilities to multiple users concurrently, whether they use interactive terminals or traditional batch devices for access. (This makes it easier for people and computers to work together.) You can program in high-level COBOL, FORTRAN, BASIC and SPL (System Programming Language) in any access mode. The HP 3000 combination of immediate access and powerful multiple capability is available at a cost no other computer system can match.

Convenient terminal access enables full-range program development, pro-

(continued on page 3)

Solid-state sweepers offer BWO-type power output



New solid-state RF power module for HP 8620 series sweepers delivers BWO-equivalent power, 1.8 to 4.2 GHz.

Swept frequency testing of high-loss S-band devices is now simpler and more practical. HP offers the first solid-state sweep oscillators whose power output above 2 GHz is comparable to that delivered by BWO-type sweepers.

The HP 86330B RF module for the HP 8620 series sweepers produces a guaranteed minimum of 40 mW leveled power from 1.8 to 4.2 GHz. Typically, power levels of 100 mW and above can be obtained. A wider band version, model 86331B, covers 1.7 to 4.3 GHz with some reduction in power at the band edges.

Altogether, solid-state RF units for the 8620 series sweepers span 3 MHz to 18 GHz to provide maximum flexibility for your swept measurement needs.

For full details, check N on the HP Reply Card.

Low profile recorder with options for varied applications

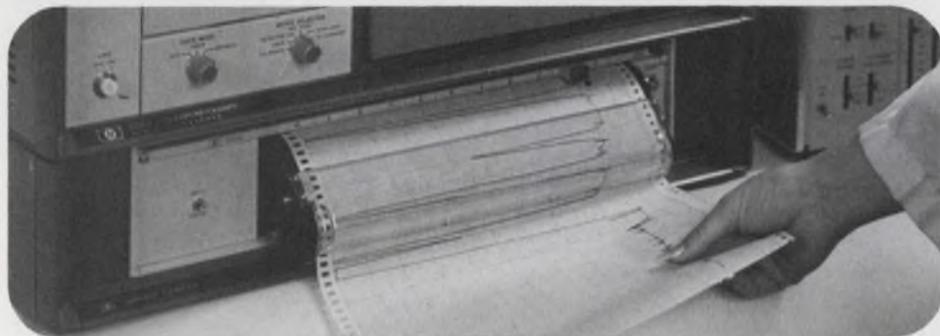
HP's 7123A strip-chart recorder is an ideal choice for applications where space is limited. Fast response time, high reliability and wide range flexibility are combined in a package only 3.5 in. (8.9 cm) high. The recorder fits easily into OEM equipment and saves valuable rack space, yet still provides an easy-to-read 10 in. (25 cm) chart.

Over 50 options for span sensitivity, chart speed and other performance features guarantee flexibility to meet any need at minimum cost. Three special options satisfy analytical needs, such as gas chromatography applications.

Solid performance and low-silhouette design—the 7123A recorder is an ideal running mate for the HP 5700A gas chromatograph.

Reliability—the keynote of analytical recording—is achieved by a unique linear servo motor system with only one moving part: the slider/pen assembly. There are no ink spills or priming problems; you use convenient quick-change disposable pens, available in several colors. The chart drive is slanted so that you can make notes during operation. The entire magazine swings out for easy paper loading.

For more information, check K on the HP Reply Card.



A new way to teach or learn digital logic



The logic lab's solderless, plug-in connection technique lets you breadboard circuits quickly and easily.

For a complete, concise course in practical digital electronics, try HP's new educational package. The 5035T logic lab contains all equipment and instructional material necessary to learn digital logic.

Designed for use in industrial training programs, high schools, technical institutes and universities, the 5035T is also handy for breadboarding logic circuits in engineering labs. This practical aid teaches digital logic in a realistic way that prepares the student to work in modern electronics. With the logic lab, you receive:

- 5035T mainframe—a complete, portable lab station with built-in 5V power supply, 2 clock sources, 4 LEDs, and removable breadboard assembly.
- 10525T logic probe, 10528A logic clip, and 10526T logic pulser—quality troubleshooting instruments for circuit stimulus-response testing.
- Textbook and lab workbook—both in modular format so the student can start at any level of difficulty.
- All components and wires necessary for the experiments including 30 integrated circuits.

Since learning is largely self-directed, the logic lab requires minimal preparation by the instructor.

To learn more, check G on the HP Reply Card.

New low-cost pulse generator for MOS circuits

HP's new 8011A pulse generator is an economical instrument ideal for testing newer MOS circuitry as well as linear circuits. It can drive all saturated logic families, low threshold MOS, CMOS and analog devices.

Amplitude ranges from 250 mV to 16V; rep rate, from 0.1 Hz to 20 MHz; and pulse width, from 25 ns to 100 ms with square wave selectable. Transition times are fixed at <10 ns. Source impedance on the lower ranges is 50Ω while in the 4V-16V range, impedance can be 50Ω or higher.

Choose positive, negative or symmetrical pulse polarity to change rapidly from positive to negative logic, or to enable duty cycles up to 100%.

To help overcome the problems of logic circuit design and troubleshooting, a counted pulse burst option is available. With this option, you simply pre-select the number of pulses you need, from 1 to 9999. You can clock circuits at

their operational clock rate, then analyze them under static conditions.

The 8011A is probably the lowest priced pulse generator of its kind...only \$435. Add \$300 for the pulse burst option.

For more information, check M on the HP Reply Card.



The 8011A with HP's unique counted burst option offers a new concept in logic test and troubleshooting.

(continued from page 1)

vides dedicated terminals for specific applications, and eliminates keypunching. Batch access to advanced computing power or batch execution gets batch production jobs done, while terminal users are also accessing the system. Full system capability is available to every user independent of access method, so people can use the method best suited for their problems.

A state-of-the-art multiprogrammed operating system (MPE/3000) assures maximum use of central processing resources through overlapping I/O and computation. MPE automatically schedules users for maximum operating efficiency.

The basis of the HP 3000 contribution is a unique architecture that provides advanced computer system concepts,

including separation of code and data, data stack, virtual memory through code separation, and a microprogrammed instruction set. Core memory options of 64, 96, and 128 kilobytes are available, along with a wide range of peripherals and terminals.

HP 3000 users are supported by comprehensive system training, documentation, regional and local service offices, and a flexible financial program ranging from lease arrangements to direct purchase.

The HP 3000 is currently in use in the U.S., Canada and Europe. For availability in other countries, contact your HP sales office. System prices start at \$175,000.

For more information, check D on the HP Reply Card.

New mainframe and plug-ins for HP 183 scopes

Two new plug-in modules and a new high speed scope mainframe enhance HP's proven 183 series oscilloscopes.

The new plug-ins add 200 MHz two-channel (model 1835A) or four-channel (1834A) general purpose measurements for both digital and analog applications. You can also couple these wide bandwidths with an HP time base module for accurate timing measurements in ECL and TTL logic circuits. Additional capability for high frequency timing applications is provided with the 4-channel chop rate of 500 kHz and the 2-channel chop rate of 1 MHz.

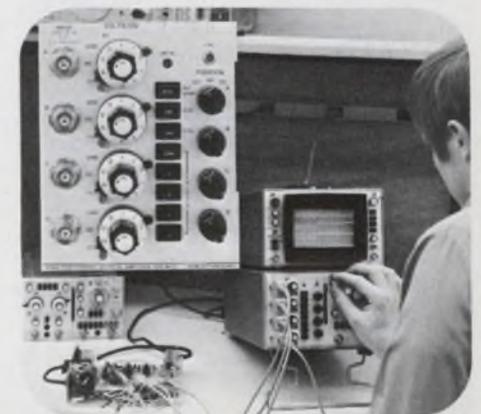
Both plug-ins have 10 mV/div deflection factors to 200 MHz. Selectable trigger source lets you reference any one channel while retaining time relationships with other channels. Composite triggering allows each channel to trigger independently with an alternate or added display.

Model 183B, option 005, is a new mainframe with high writing speed. The option 005 provides up to 24 cm/ns transient recording capability for the most demanding high-energy physics or laser detection applications. A direct-access plug-in allows real time, large signal transient analysis to greater than 600 MHz, as well as 10 mV/div capability to 250 MHz.

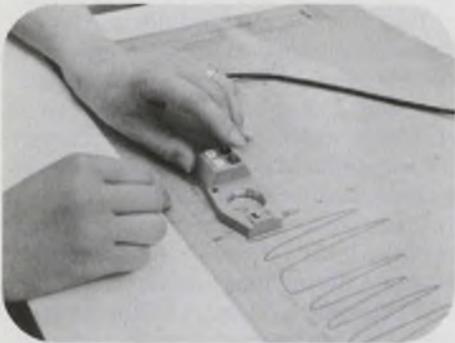
The 183B opt 005 costs \$2975. The 1835A dual channel amplifier, \$1400; the 1834A four-channel plug-in, \$1900.

For specifications, check C on the HP Reply Card.

Four-trace capability simplifies digital circuit testing.



Digitizer inputs graphic data for HP calculators



Here, the lab technician is digitizing a blood-analyzer strip-chart for medical data analysis and quality control.

The HP 9864A digitizer lets you enter analog data directly into an HP 9800 series programmable calculator for analysis without tedious manual measurements, conversion, and entry of

data. Simply move the cursor over the map, chart, or source material. The HP calculator then analyzes the digitized data according to your program. Resolution is .01 in. (.25 mm) and accuracy, 0.15 in. (.38 mm).

Applications for the digitizer are almost infinite. Use it to analyze contour maps, profile plots of terrain, mathematical curve fitting, nuclear data, cardiac plots, photographs, etc. Analog data can be in virtually any graphic form.

The standard platen will handle material up to 17 in. by 17 in. (43 cm by 43 cm). Options extend the platen maximum up to 42 in. by 60 in. (105 cm by 152 cm).

For more information, check P on the HP Reply Card.

Universal card reader inputs 300 cards per minute

HP's 300 cards-per-minute optical mark reader is flexible as well as fast: model 7260A accepts all types of punched or marked cards, even specially-designed forms. With appropriate clock marks, single cards may be both punched and marked—in any number of columns from 1 to 80. This desktop reader is quiet enough for your office; fast enough to keep up with your computer.

The 7260A can be used with terminals, computers or remote data systems via a modem or direct connection. Data rates are switchable from 110 baud to 2400 baud. Data is stored in buffers so that you can optimize the card feed rate for high transmission efficiency. The 7260A transmits data in 7-level ASCII code; other decoding options are available.

OEM and quantity discounts are also available.

For more information, check L on the HP Reply Card.



Students can mark cards at their desks or at home, then handle other tasks while their programs are read and processed.

New application notes on spectrum analysis



Three new spectrum analysis application notes are now available from HP. One is a general discussion of noise measurements; another treats CRT photography and x-y recording techniques; and the third is a "how-to-use" text about a versatile new HP analyzer.

AN 150A, *Using the 8558B Spectrum Analyzer*, introduces you to the operation, use and measurement capability of this 100 kHz to 1500 MHz instrument. A plug-in module that fits into any HP 180 series oscilloscope, the 8558B combines high performance with simple operation.

AN 150-4 shows how useful the spectrum analyzer can be for noise measurements. After distinguishing between random noise and impulse noise, the note deals with carrier-to-noise ratio, white noise loading, amplifier noise figure, and spectral purity characterization of several oscillator types.

Many spectrum analysis applications require photographs and plots for permanent records. AN 150-5 gives practical tips for making cathode ray tube photographs and x-y recordings of spectrum displays. Two types of CRTs and four types of recorders are covered.

Let us know which application note(s) you want; check T, U, or V on the HP Reply Card.

New A/D converter for HP computer systems

Now there's a new low-cost analog measurement capability for research labs or production test stations that measure a few analog channels along with their digital work. The 91000A is a 16-channel, 12-bit analog-to-digital interface subsystem for HP 9600 series measurement and control systems or HP 2100 series computers. It's easy to install—simply slip the A/D card into an I/O channel in the computer.

The 91000A card includes all necessary interface and control logic, 250-ns sample-and-hold amplifier, A/D converter, and an input multiplexer with capacity for 16 single-ended or 8 differential inputs. You can input, sample and digitize analog data at rates up to 20 kHz. The card accepts TTL-level external pacing signals.

Multiple A/D interface cards can be used together in a single 2100 series computer. And if your needs grow, your system can grow with them, to over 1000 analog channels, without changing your existing programs. Simply step up to the larger HP 2313B A/D interface system.

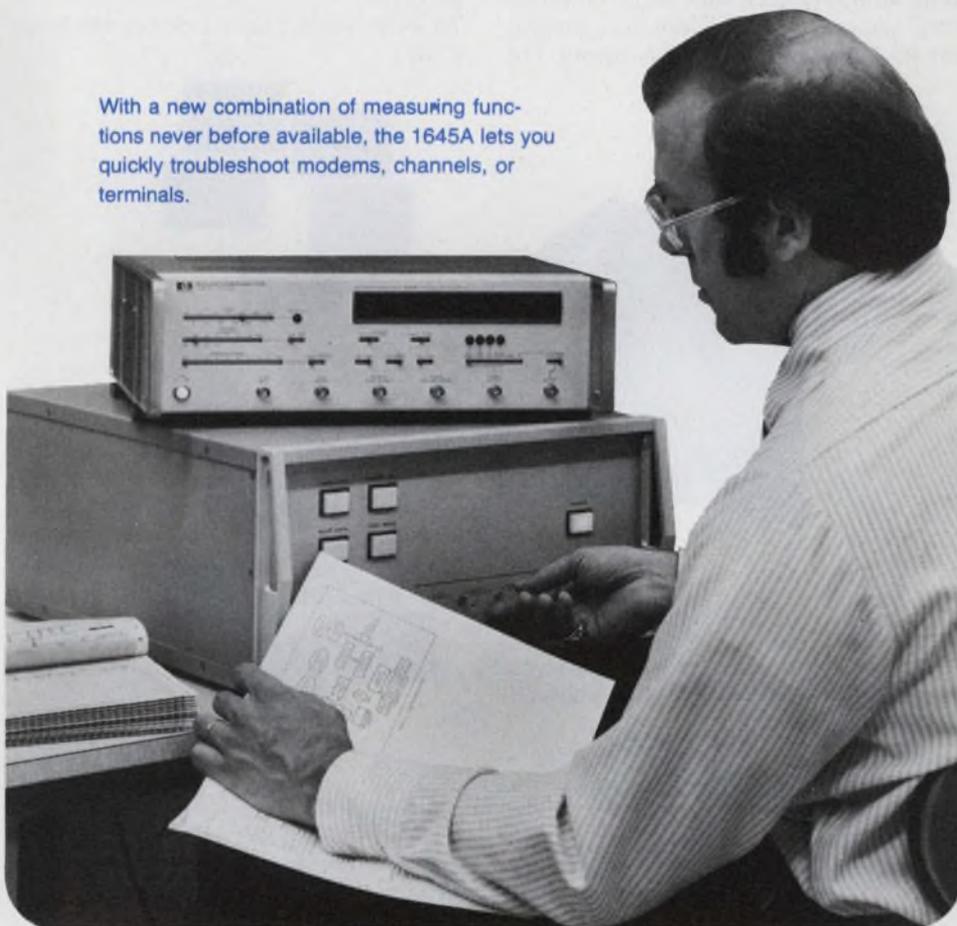
There's more. Just check O on the HP Reply Card.

The 91000A is a complete package with BCS or RTE driver software (interfaced to FORTRAN, ALGOL or real-time BASIC programs) and an operation and service manual.



New data link communications tester pinpoints system problems

With a new combination of measuring functions never before available, the 1645A lets you quickly troubleshoot modems, channels, or terminals.



HP's new 1645A data error analyzer quickly isolates data communications link problems with six simultaneous measurements. You can use it to test modems, data channels, whole data communications systems, or low-speed memories. Yet it's easy enough to operate with little or no technical knowledge.

The 1645A measures bit error and block error rates directly—requiring no recalculation or interpretation—and maintains synchronization throughout a test, even in the presence of dropouts. Information appears on a digital LED display.

The analyzer also measures data error skew; counts the number of times carrier loss occurs; measures jitter or total peak distortion (the sum effect of jitter and bias); and counts the number of clock slips. With all these measurements taken simultaneously, you can locate the faulty system components in your communications link. And the storage feature leaves you free to work on other projects while the 1645A makes long unattended transmission analyses.

To learn about easier troubleshooting, check B on the HP Reply Card.

Great way to make waves and save money

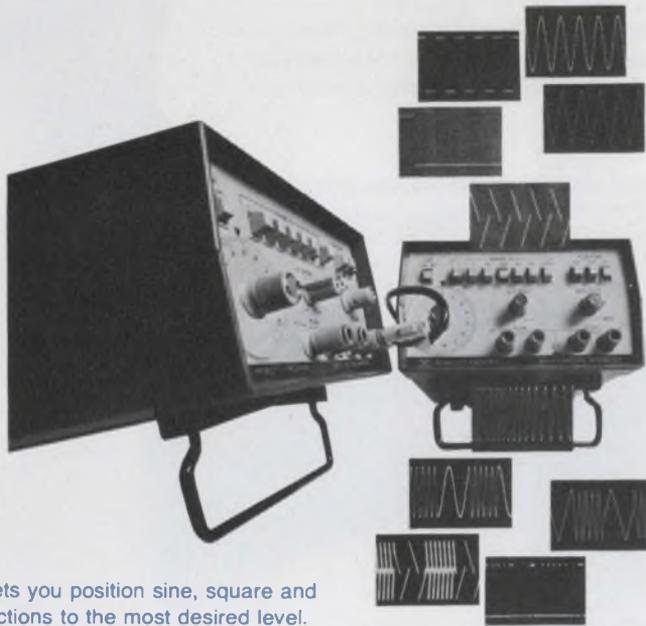
Sine waves, square waves, triangular waves—our low-cost function generator can produce them all, on 7 decades of range from 0.1 Hz to 1 MHz. The 3311A signal source also has dc offset and external sweep capabilities.

For convenience, there's pushbutton range and function selection. For versatility, you can put two function generators together and sweep the output. For

added value, the 3311A contains several features usually not found in this price range, such as 10:1 voltage control and separate pulse output for driving up to 20 TTL logic circuits. It also has a 15% duty cycle and 25 ns rise time.

All for an amazingly low price: just \$249.

To learn more, check E on the HP Reply Card.



DC offset lets you position sine, square and triangle functions to the most desired level.

New guide to HP electronic counters

Ever had to wade through mountains of specs to select a counter? Now, the HP counter brochure is here, making it easy to select from the most complete counter line available today. You'll find all types of counters here: simple low-cost units, battery-operated portables, universal counters/timers/DVMs, and models with versatile front-panel plug-ins. With HP counters, you buy just what you need, without paying for features you won't use.

Check R on the HP Reply Card and you can count on us to send your free copy.

Design tips on microwave transistor bias

To help the microwave circuit designer, HP offers a new application note, *Microwave Transistor Bias Considerations* (AN 944-1).

In microwave transistor circuit design, the dc bias network significantly influences such RF parameters as gain and noise figure. Inattention to bias conditions can sacrifice RF performance. AN 944-1 is a practical guide that relates dc stability factors to RF performance.

For your free copy, check S on the HP Reply Card.

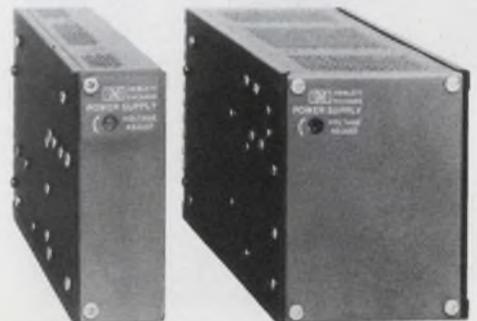
New power supplies have dual output

Now, dual output capability has been added to HP's growing line of modular power supplies. Four models are offered: $\pm 12V$ at 1.40A and 3.30A, and $\pm 15V$ at 1.25A and 3.00A. A single front panel control provides $\pm 5\%$ adjustment of both outputs. These series-regulated supplies deliver full-rated output from 0 to 40°C with derated operation up to 71°C. All models are specified at 0.01% line or load regulation, 1 mV rms and 5 mV p-p ripple and noise, and $\pm 1\%$ tracking accuracy.

Standard features include cut-back current limiting, overtemperature and reverse voltage protection, and remote sensing. Overvoltage protection is available as an option. These dual output power supplies are packaged in $\frac{1}{8}$ and $\frac{1}{4}$ -rack width cases.

For all the specifications, check I on the HP Reply Card.

These new power supplies are designed for powering operational amplifiers, core drivers, D/A and A/D converters, MOS devices, and voltage comparators.



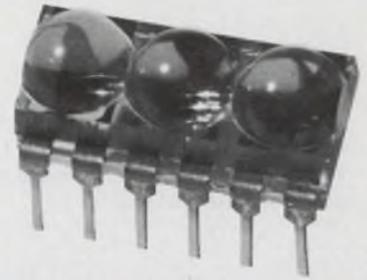
New two and three digit low-power displays

Low power and MOS compatibility characterize HP's new series of solid-state numeric displays. They require only 300 μ A per segment, thereby eliminating the need for segment drivers when you interface them with MOS circuits.

These monolithic displays have a character height of 0.11 in. (.28 cm) and a standard lower right-hand decimal point. They are end stackable; digits

are on 200 mil centers. Built-in magnification increases luminous intensity.

The new indicators are available in two-digit clusters (5082-7432) and three-digit clusters (5082-7433).



The new 5082-7430 series are ideally suited for use in handheld calculators and portable instruments.

For specifications, check H on the HP Reply Card.

Send for a new diode and transistor catalog

Hewlett-Packard offers a wide range of diodes and transistors to meet your power, frequency, design and reliability requirements. The latest HP Diode and Transistor Catalog contains key specifications for the following products:

- Small signal microwave transistors.
- Schottky diodes—for mixing and detecting, microwave Schottky diode quads for double balanced mixers, beam lead and other Schottky and PIN diodes for hybrid ICs.
- RF, general purpose and switching Schottky diodes for high volume applications.
- PIN diodes for VHF, UHF and microwave applications.
- IMPATT diodes.
- Step recovery diodes.
- High reliability products.

The catalog includes packaging specs and drawings to aid the circuit designer.

For your copy, check Q on the HP Reply Card.



Test components fast with new LCR meter



Typical uses for the 4271A LCR meter are: testing discrete components and varicap diodes, checking semiconductors, and L or C examinations of delay lines.

If you're testing diodes and capacitors or trimming IC capacitors and resistors, you need fast precise inductance, capacitance, resistance and loss measurements. Plug the new HP 4271A digital LCR meter into your system and you get 10,000 measurements or more per hour.

Using a four-pair measurement technique that reduces stray capacitance and residual inductance, this 1 MHz digital meter measures capacitance from 0.001 pF to 19,000 nF with an accuracy of 0.1%, and inductance from 0.1 nH to 1900.0 μ H. Capacitance loss components are measured as parallel conductance or as dissipation factor (as low as 0.0001). Inductance loss components are measured as series resistance (10 Ω to 10 K Ω) or dissipation factor (as low as 0.0001). And you can vary dc bias from 0 V to 39.9V in 0.1 V increments.

The LCR meter has a four-digit LED display with 90% overrange, and it interfaces easily with HP computers, calculators, and digital recorders.

To learn how to improve component testing, check F on the HP Reply Card.

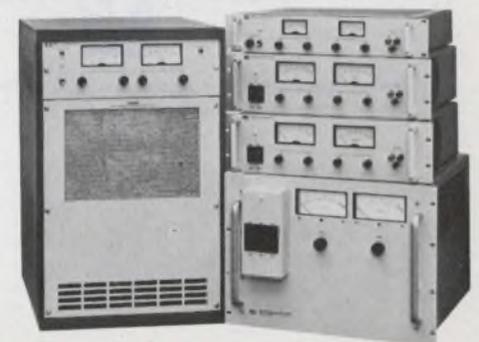
New efficient dc supplies save watts and dollars

Low cost, high efficiency, compact size, outstanding reliability—you get them all with HP's 6427B-6483C family of high-power dc supplies. Using an advanced SCR-regulator design with up to 75% efficiency, these constant-voltage/current supplies are well suited to applications requiring high power with moderate regulation and ripple. You can use them for testing component aging, battery charging and discharging, station batteries, precision welding, and dc motor control.

Standard features include remote sensing, remote V and R programming, and auto-series, auto-parallel and auto-tracking operation. Nineteen different models provide outputs from 0-8 V to 0-600 V at currents up to 1000A.

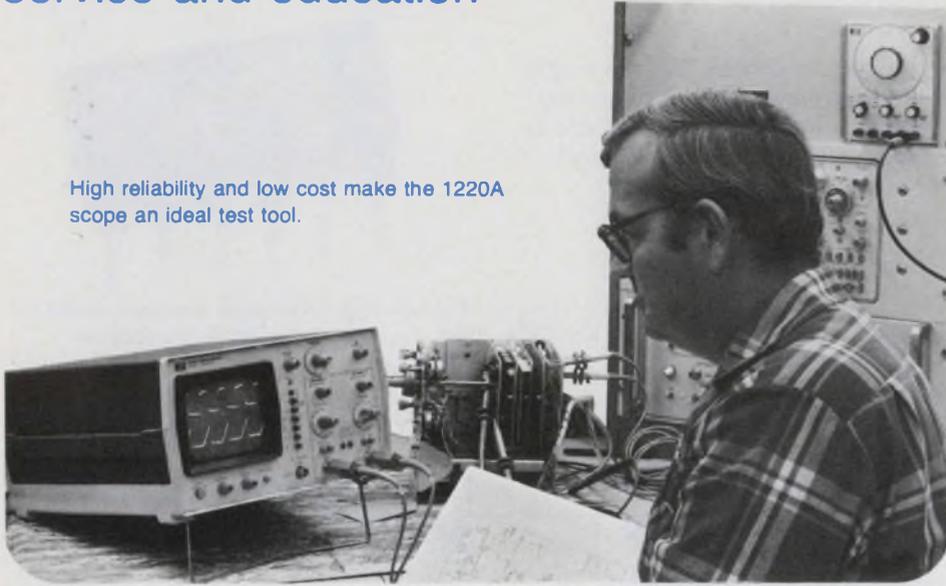
To learn more, check J on the HP Reply Card.

High-efficiency dc supplies come in 300W, 1000W, 3500W and 11,000W power ratings.



New high value oscilloscopes for manufacturing, service and education

High reliability and low cost make the 1220A scope an ideal test tool.



Two new 15 MHz oscilloscopes offer quality performance at minimum prices. Choose either the new 1220A dual channel scope, or the 1221A single channel model. Both have deflection factors from 2 mV/cm to 10 mV/cm for basic analysis of audio, video, logic circuits, FM, or direct output of mag pickups and heads. Built-in TV sync separation circuits make television servicing easy. And rugged construction makes these scopes useful in applications such as production and service of numerically-controlled machinery, process control equipment, automotive, aircraft, and marine electronics.

The large 8 by 10 cm graticule is internal, which eliminates parallax error.

Vertical accuracy of 3% and time base accuracy of 4% increase the validity of your measurements. Dc coupling is available for directly measuring absolute voltage levels, even on mixed ac and dc signals. A times-ten sweep expander makes it easy to examine signal details. The front panel controls are grouped functionally for easy understanding, and the pushbuttons are color-coded for easy use.

There's more: the automatic trigger sweep (just one control knob) assures stable displays. A bright base line is provided for fast setup in the absence of an input signal.

Built-in TV sync separation offers stable, automatic triggering on frame or

line for convenient TV troubleshooting. And, with the instrument's times-ten magnifier, vertical interval test signals can be "pulled out" for examination. The calibrated sweep helps identify timing problems in vertical or horizontal TV circuits.

An x-y mode makes reliable phase measurements with a phase shift of less than 3° at 100 kHz. The horizontal input also accepts horizontal drive signals from swept frequency oscillators for checking out tuners.

The 1220A displays two signals either in alternate for high sweep rates or, for lower rates, by chopping each sweep into short segments with blanking. The scope automatically selects the mode that will give you the best display. With dual channels, you can also compare input vs. output directly.

Solid-state design with its low power consumption and conservative component ratings makes for long, trouble-free life.

Check A on the HP Reply Card for more information.

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Yoyogi, Shibuya-ku, Tokyo, 151.

ACROSS THE DESK

(continued from page 8)

subroutine to work correctly. The subroutine uses the A register, and the main program must be written so that a change in the accumulator data, when this subroutine is called, will not produce erroneous results.

A subroutine to accomplish the same results without affecting any CPU scratch-pad register or the accumulator is as follows:

DECHL	DCL	decrement L
	INL	increment L
	JFZ	A jump if L ≠ 0
	DCH	decrement H
A	DCL	decrement L
	RET	return

The purpose of the INL instruction that follows the DCL instruction is to set the zero flag bit, if the L register was all zero when the subroutine was called. The rest of the subroutine is self-explanatory.

John M. Schulein
Engineer

Philco-Ford Corp.
Western Development
Laboratories Div.
3939 Fabian Way
Palo Alto, Calif. 94303

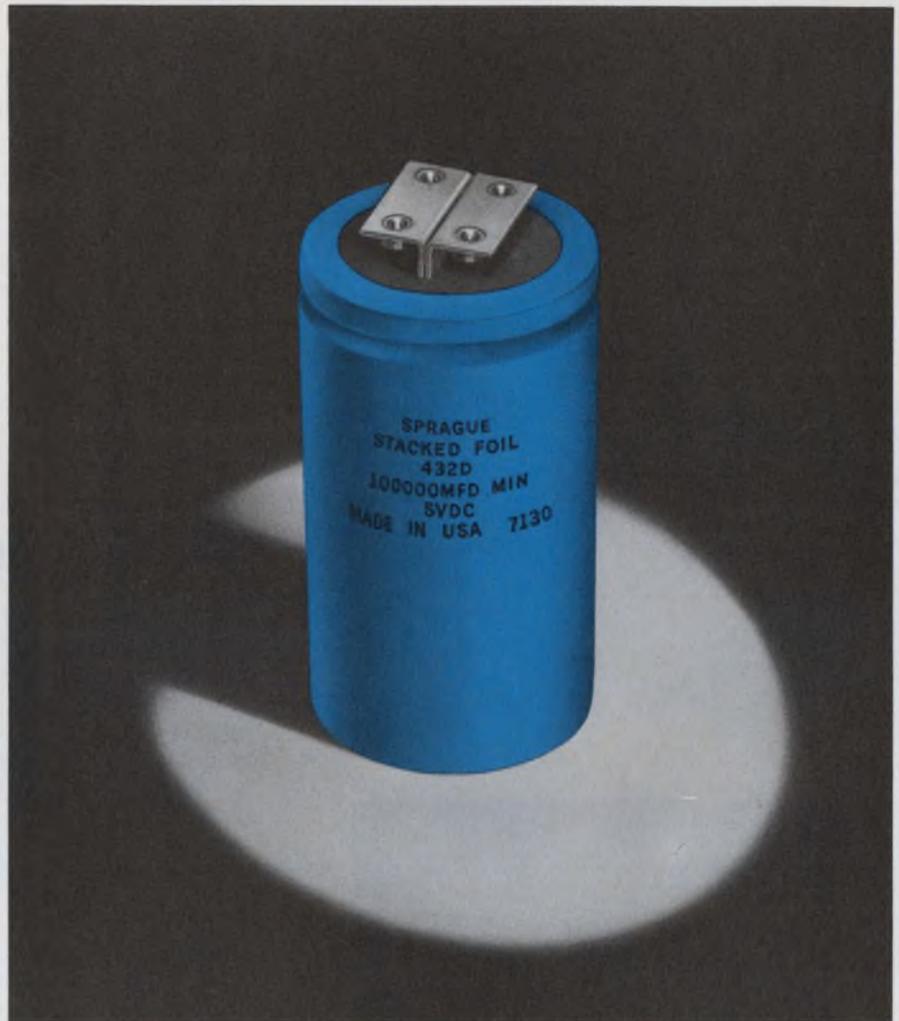
The author replies

Mr. Schulein is correct in his criticism of the subroutine DECHL. The subroutine, as shown, will not work without the missing instruction LAL between DCL and CPI 377. His subroutine is also correct.

It is true that the A register is used in the execution of the subroutine, and thus data cannot be retained in the A register. This must be considered when writing a program that uses the subroutine. The subroutine—as well as the one that Mr. Schulein has introduced—changes the contents of the zero flip-flop. Thus this status flag cannot be retained while the subroutine is executed. When a small microprocessor is used, this is a fact that one has to live with.

Donald R. Lewis
W. Ralph Siena

Lewis Associates
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New York, N.Y. 11415



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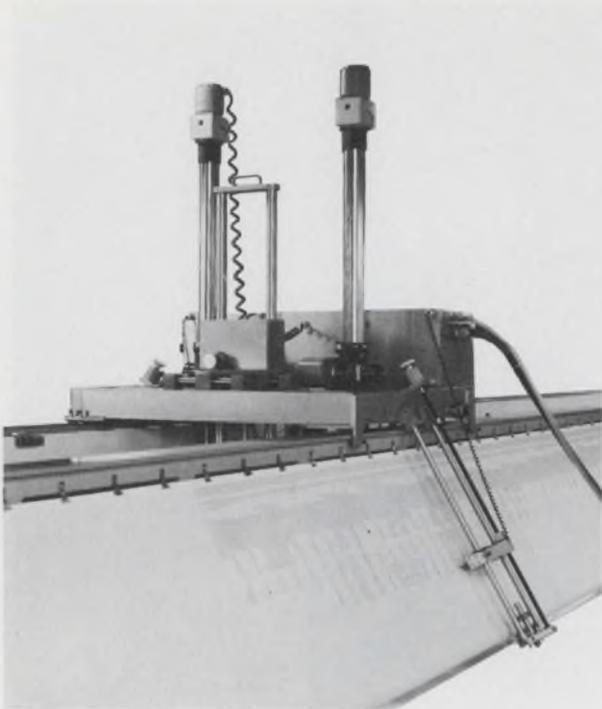
For complete technical data, write for Engineering Bulletin 3443 to: Technical Literature Service, Sprague Electric Co., 347 Marshall St., North Adams, Mass. 01247.

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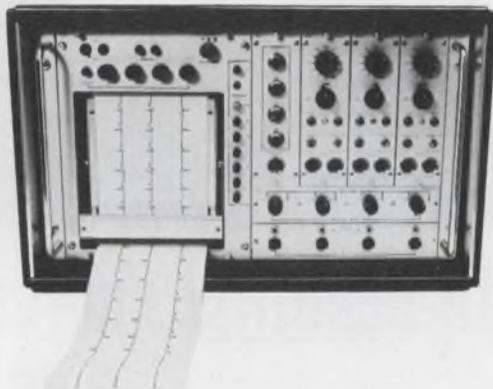
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A Recorder...

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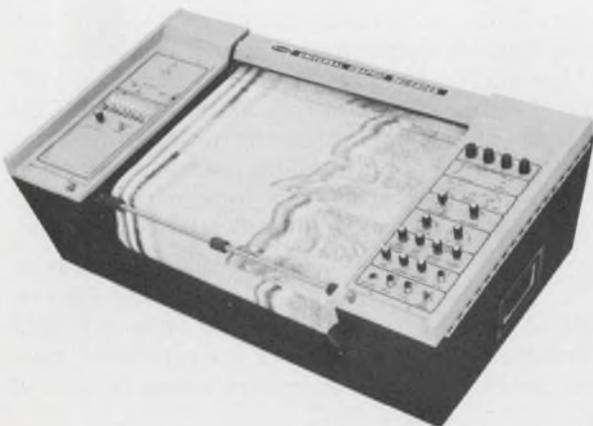
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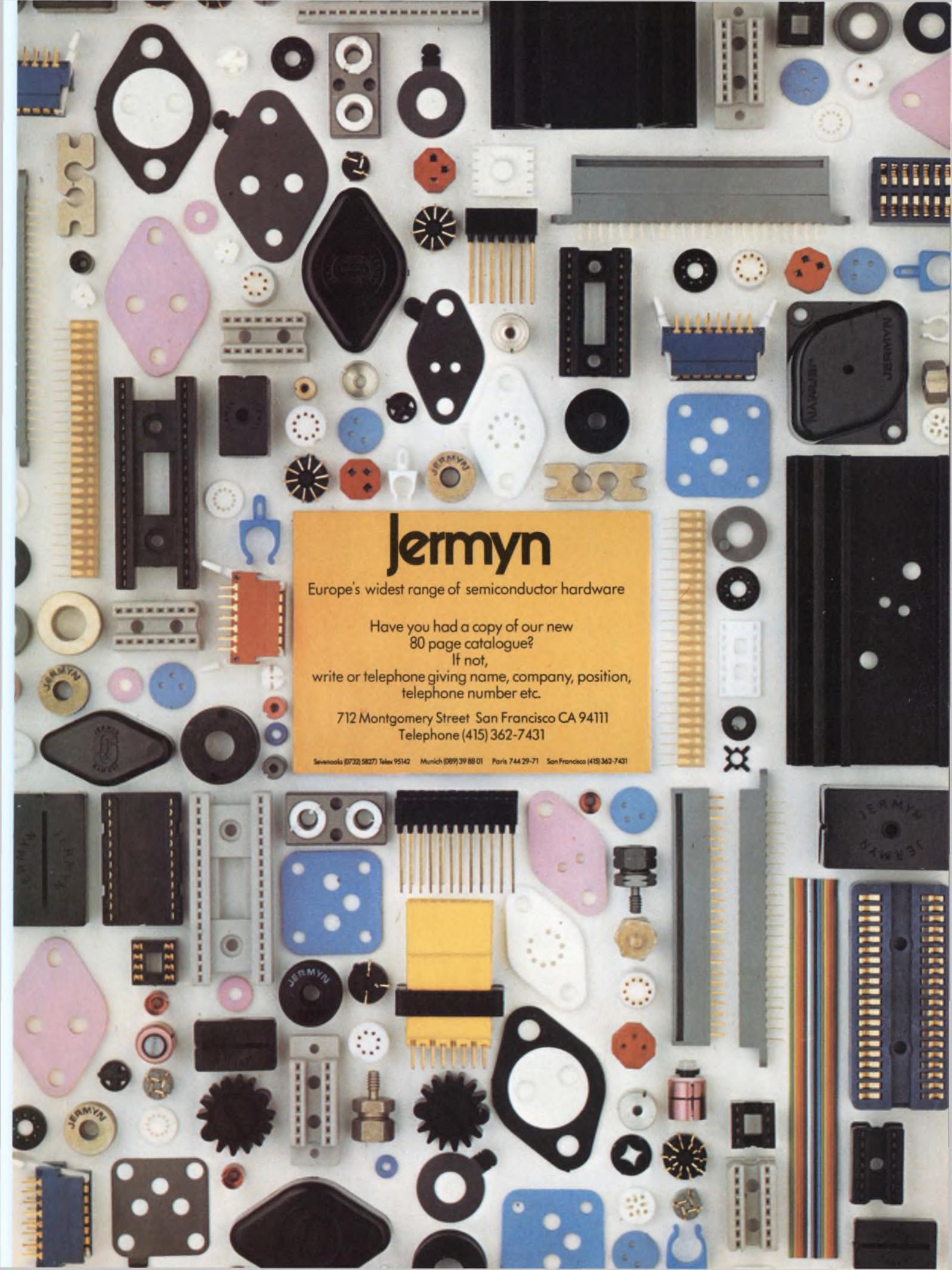
If you build specialized recording equipment, why not allow us to advise you on the selection of electro-sensitive, heat writing, pressure writing or other recording media. As a start, we would like to send you a free copy of our technical brochure "The dry electro-sensitive process". It's yours for the asking.



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With a \$3.1-billion budget, NASA sees year of growth

Funds available to NASA in 1974 are expected to remain stable around \$3.1-billion, having found a level of apparent acceptability to Congress and to the public.

The largest expenditures again will be on those programs that are already well into engineering development: the Apollo-Soyuz project, which will be launched in 1975, and the space shuttle.

Work is under way and will continue on two Viking unmanned orbiter lander spacecraft, scheduled for launching to Mars in 1975, and on the Mariner spacecraft for the Jupiter/Saturn fly-by mission, scheduled for launching in 1977.

Advanced space technology projects will get adequate funding at Jet Propulsion Laboratory, according to Frank J. Sullivan, director of NASA's Guidance Control and Information Systems Div. in the Office of Aeronautics and Space Technology.

Robotics, or machine intelligence, is one area to be developed, with a planetary rover for Mars as the initial hardware. Because of the distances that result in a communications lag between the earth and Mars of perhaps 30 minutes to 1-1/2 hours, the robot must be able to initiate action without instructions from the earth. Based on what it encounters—obstacles in its way or the elements in the atmosphere or soil that it finds—the robot will take the appropriate next step.

NASA plans to have a laboratory demonstration of the robot this year and hopes to test an autonomous rover in a desert area by 1978.

In laser communications the space agency hopes to work with the Air Force to flight-test a laser in a synchronous satellite by 1977, Sullivan says. The object would be

to determine the influence of the atmosphere on signal propagation and capacity. This would, in turn, determine how much bandwidth would be required.

NASA is leaning toward a CO₂ laser, although it is also studying the neodymium YAG. The YAG is not as well developed as the CO₂, but it does promise more capacity.

NASA will also develop ways to use the laser to detect and identify pollutants. The size of the wavelength of the tunable laser would identify the size of the particular pollutant being encountered, thereby identifying it and measuring the particle density.

Tuned rhodium dye lasers that can penetrate water up to 20 feet will be investigated for determining the health of the ocean by detection of chlorophyll, plankton and other matter.

Lasers will be tested as radar systems for mapping the shallow areas of the ocean, where it might be difficult for ships to operate. NASA's Langley Research Center, near Norfolk, Va., is working on this project with the Navy.

The space agency is intensely interested in extending the life of attitude-control systems for planetary probes. The problem lies in achieving efficient computer control of sensors, star trackers and thrusters. The computer system must be designed to discover any failure in a sensor or thruster system and then switch to alternate arrangements so the mission can be successfully continued.

NASA will investigate a low-cost attitude-control system for earth orbital missions that carry a large number of experiments, each requiring a different stabilization accuracy. The aim is to eliminate the need for separate gimballed platforms for each experiment.

Control moment gyroscope tech-

nology for earth orbital and planetary missions is being examined to see if energy can be drawn off the spinning gyroscope and stored in a flywheel. The energy could then be converted to electrical power, Sullivan notes.

An optical computer is to be developed with the hope that the high speed of the device will permit photographic data to be processed aboard satellites. The speed would have to equal that of parallel processing systems.

NASA is working on a solid-state bubble-memory recorder to replace the present magnetic-tape recorders, which store data and periodically "dump" the information to earth stations. The magnetic recorders, with their moving parts, have had a high failure rate, Sullivan says, and the bubble memories promise more reliability. NASA presently is trying to design a bubble-memory system with a capacity of 10⁸ bits.

U.S. gets its first domestic satcom net

The nation's first domestic communications satellite system went into full operation last month, using Canada's Anik II spacecraft and four U.S. earth stations. Operated by RCA Global Communications and RCA Alaska Communications, the network provides channels between the East and West Coasts of the U.S. and Alaska.

The four earth stations, which cost \$10-million are near New York City, San Francisco and Anchorage and Juneau in Alaska. Soon additional earth stations will be built in Alaska, and eventually, when the second phase of the program gets under way, RCA will put up its own satellites and build more stations in the U.S.

At present RCA uses two rf channels in the Canadian satellite—one full-time and a second part-time. The satellite channels operate in the 4-to-6-GHz band and have a nominal bandwidth of 36 MHz. The up link operates between 5925 and 6425 MHz, and the down link from 3700 to 4200 MHz.

The full-time transponder is capable of operation in any of the following modes:

- Up to 1000 one-way FDM/FM

voice channels on a single FM carrier.

■ 600 one-way voice channels with use of the single-channel-per-carrier technique.

A television channel to Alaska will cost about \$1200 an hour, as opposed to the \$2000 now charged voice channels on a single FM carrier.

RCA's Phase II system will consist of three 24-channel satellites in stationary orbits and a network of major earth stations. The first of the spacecraft is scheduled for delivery by October, 1975.

Two developments will make possible the 24-channel service without exceeding the weight and volume capacity of the launch vehicle: First, lightweight, graphite-fiber, epoxy-composite material is to be used as the basic material for each of 24 input and output multiplex filters, as well as for waveguide sections and antenna feeds. This material will replace the invar used in conventional designs. Second, three-axis attitude control will allow extra weight and power margins, compared with those available with current dual-spin satellites.

The main body of the spacecraft is to be approximately 5.3 by 4.1 by 4.1 feet and its orbiting weight approximately 1000 pounds. The orbiting satellites will be powered by solar energy derived from two arrays.

Each of the RCA Phase II satellites is designed to carry single-carrier analog transmissions, such as FDM/FM voice or FM/color TV, or single-carrier digital transmissions. Channels will also be capable of operating in the multiple-access mode for transmission of multiple-carrier analog or digital signals.

Optical design slashes encoded altimeter price

A new generation of encoding altimeters for private planes, designed as substitutes for expensive brush and magnetic-encoded devices, has been announced by Kollsman Instrument Co., Syosett, N.Y.

The new device uses an optical shaft encoder to convert the position of the altimeter needle to an electrical signal. Encoded altimeters are not new, a company

spokesman notes; commercial airliners have been using them for years. But until now they have cost \$5000 to \$6000. New rules by the Federal Aviation Administration, however, require private planes flying in high traffic areas to have encoded devices; a cheaper alternative to the magnetic and brush devices was considered essential.

By attaching an optically encoded wheel to the altimeter shaft and using light-emitting diodes to illuminate it, Kollsman has cut the price of the encoded altimeter to about \$1300. In addition the size and weight of the device have been considerably reduced.

New approach radar proves highly accurate

A new solid-state approach-control radar, with improved rejection of weather and ground clutter, has demonstrated marked superiority over older, comparable systems.

Developed by the Air Force Electronic Systems Div., Bedford, Mass., the new system—the AN/TPN-19—demonstrated 100% success in recent tests in tracking aircraft landing in rainfall as heavy as five inches an hour. In contrast, a nearby AN/FPN-16—a standard Air Force approach-control radar—was able to track only 6% of the same aircraft.

The tests were conducted at Eglin Air Force Base in Florida.

The new TPN-19 is a dual radar system that provides approach surveillance up to 60 miles and precision landing surveillance up to 20 miles. According to Wayne Wootton, deputy director of the TPN-19 program, the system has several other advantages over present radars. These include:

■ A phased-array precision approach radar with 15-by-20-degree constant coverage; current equipment is limited to a very narrow areas swept by a moving antenna.

■ Simultaneous landing control of up to six aircraft, separated by three minutes each; present radars handle one aircraft at a time.

■ An adjustable glide path from 2 to 13 degrees in increments of 0.1 of a degree; current equipment uses one fixed glide path, so that a helicopter is required to use the

same flat approach as a large aircraft.

■ Changeable antenna-beam direction via an automatic five-minute operational sequence. Present systems require turning the antenna manually.

Nine of the AN/TPN-19 radar systems will be produced by the Raytheon Co.'s Equipment Div. in Wayland and Waltham, Mass., under an \$18.32-million contract.

Modular packaging of the TPN-19 permits partial system use. The surveillance radar can be set up as far as 10 miles away from the precision-approach van. This permits matching the system to the terrain, rather than placing both antennas alongside the runway.

EIA components show geared to designers

A "new kind" of electronics show to bring component designers and the manufacturers' application engineers together will be held by the Electronic Industries Association from May 13 to 15 in Washington, D.C.

The show will run at the same time as the joint EIA-IEEE Electronic Components Conference, at which technical papers are presented. Both events will be held in the Statler-Hilton Hotel.

According to Bruce Vinkenulder, chairman of the organizing committee for the new show: "This is a new kind of a show, in that it is planned to be a one-to-one conference between the engineers of the parts manufacturers and the users' engineers."

Exhibitors are being urged to have high-level members of their engineering departments man the exhibit booths, so they can sit down with the user and discuss application problems on the spot.

TI challenge to HP-35

Texas Instruments has just introduced a new electronic slide rule that will compete with Hewlett-Packard's HP-35. Dubbed the SR-50, the new calculator does everything the HP unit does. In addition, it has hyperbolic, factorial, X^2 and sum of products functions. It costs \$169.95 compared to \$295 for the HP-35.

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TEKTRONIX

INFORMATION RETRIEVAL NUMBER 11



After 13 years, standardization of opto-isolators is beginning

A move toward standardization of optical isolators is under way 13 years after the introduction of the devices.

The trend has been made possible by the advent of light-emitting devices together with the use of silicon photosensor technology. These solid-state elements can be put in standard IC plastic packages.

For the designer, standardization means that, for the first time, second-sourcing of optical isolators will be available. Standardization will also give him a group of generic devices around which to design for mass production. And prices are dropping, too.

Jim McDermott
Eastern Editor

Optical isolators are photon-coupled devices in which an electrical signal is converted into light that is projected through an insulating interface and reconverted to an electrical signal. For years, there has been a broad variety of light-emitter/photosensor combinations in nonstandard packages. Standardization is beginning with dual-in-line plastic packages. A few JEDEC-registered devices have begun to appear, offered by Texas Instruments, Motorola and General Electric.

DIP package is popular

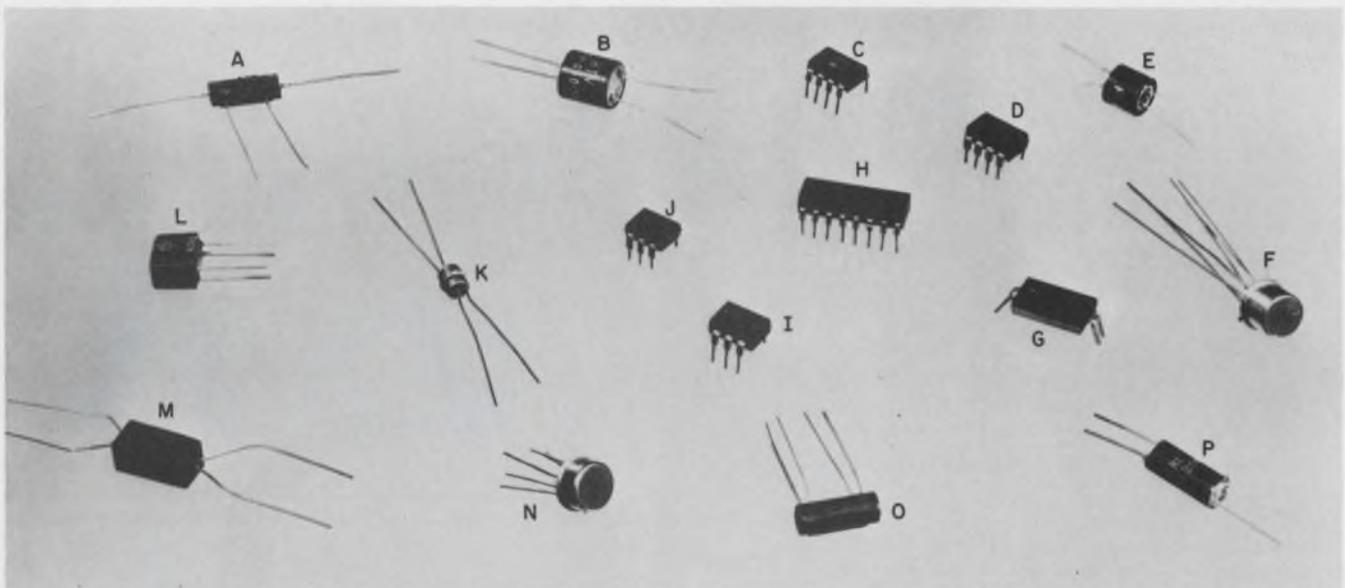
Other manufacturers using the DIP packages include Clairex, Dialight, Fairchild, Litronix, Monsanto and Vactec. Micro-sized opto-

isolators for incorporation in hybrid circuits are being produced by Spectronics (see photo).

Despite the industry efforts at standardization, however, many nonstandard devices are available, and they appear destined for use for some time to come. The variety of both devices and specifications makes it difficult to compare data; there is little consistency in the specs.

"Optical couplers are tough to specify," says William Sennhouser, district optoelectronic marketing manager for Texas Instruments, "because you have three sets of parameters. What does the input stage do? What does the output stage do? And what do they do together?"

Sennhouser notes: "One of the



Opto-isolators using combinations of LEDs and silicon photosensors come in a wide variety of packages and voltage ratings. LED/phototransistors by Spectronics (A, O), National Semiconductor Ltd. (E), Centralab (P), Dialight (G), Texas Instruments (K, M) have no base connection. Similar devices by Centralab (F), Fairchild (I),

General Electric (L) and T.I. (N) have base pins. Motorola unit (J) has a photo-Darlington output. Device by Monsanto (C) houses a photo-SCR, while that by Hewlett Packard (D) is a high-speed logic gate. The 16-pin DIP by Litronix (H) is a quad phototransistor device, while the device by Hamamatsu (B) is a LED/photodiode combination.

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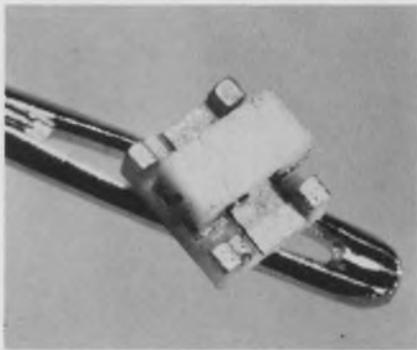
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INFORMATION RETRIEVAL NUMBER 12



This tiny opto-isolator is a miniature version designed for hybrid applications. The device, by Spectronics, Inc., comes with a LED and photodiode, a phototransistor or in a photo-Darlington isolator version.

critical parameters of solid-state opto-isolators is the current-transfer ratio." This is the ratio of the input, or forward, current I_F to the LED and the isolator output current. It is almost invariably expressed in percent.

Another major parameter, Sennhouser says, is the device's ability to withstand high voltages between input and output.

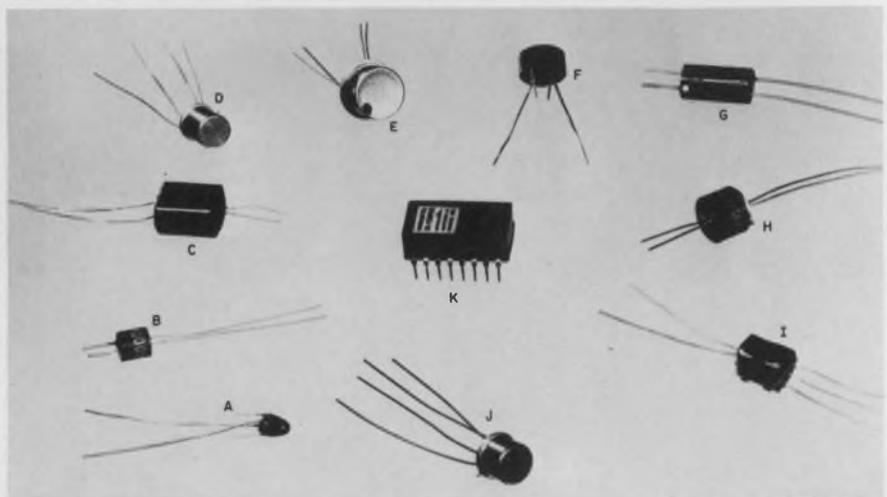
From the design point of view, these parameters are tradeoffs, Sennhouser explains. "To maximize the current-transfer ratio, the gap between the LED and the photodetector must be decreased," he points out. "But if you decrease the input-output gap, you lower the device's ability to isolate a higher voltage."

As an example, Sennhouser points to the TIXL 109, which is rated at 5 kV—about three times the usual device rating. To obtain this isolation, the LED and phototransistor have been separated enough to reduce the current-transfer ratio to a very low value of about 0.5%. Also, Sennhouser notes, the phototransistor output is down in the microampere region, whereas all the other TI devices are characterized in the low milliampere region.

The breakdown voltage of the usual device is specified at 1.5 or 2 kV. In special designs, like those by Sigma Instruments, it can run as high as 25 kV (see photo).

The manner in which the breakdown voltage is specified is frequently not the same from manufacturer to manufacturer or from device to device of the same supplier.

"These breakdown-voltage rat-



Isolation voltages of from 300 V to 10 kV are found in these isolators using LEDs to drive photoresistive cells. The OFF resistances range from a few hundred kilohms to megohms, while the ON resistances may be as low as a few hundred ohms. Single photo-isolator units include those by Quantrol Electronics (A,E,F); Clairex (B,H); Hamamatsu (C); National Semiconductor Ltd. (D,G)—the G device has the 10 kV rating; and Vactec (J,I)—the I unit has a single LED and twin photoresistors. A multiple isolator by Hamamatsu (K) has four photo-isolator devices in the 16-pin package. Isolation voltage for the quad devices is 1 kV, and up to 100 V can be placed across the photoresistor cells. The LED operating currents are 25 mA.

ings are one of the pitfalls in isolator specifications," says Henry Wearsch, advanced engineer at Reliance Electric, Cleveland. Responsible for the use of these devices as control-computer interface elements, he points out:

"If breakdown voltage listed happens to be dc and you apply an ac-rms voltage of that value, you'll exceed the rating. More than likely the unit will be destroyed."

Wearsch's advice is to make your own tests to be sure of what the device will actually handle. He has found a definite spread in the high-voltage tolerances between various devices and their specs.

Low capacitance gives isolation

The capacitive isolation obtained with optical coupling is typically 0.5 to 2 pF. The capacitance is measured with both leads of the input LED tied together and all leads of the output phototransistor shorted together.

David Barton, senior member of the technical staff at Litronix, points out that most of this capacitance is between the lead frames of the LED and transistor.

"Perhaps only 10 or 15% is directly to the transistor die, and perhaps half again is to the transistor base," he notes. "So we're

talking about 0.02 pF between the input and the base."

These low values of capacitance provide the isolation against electrical noise and common-mode signals on the input side of the coupler.

Transfer ratios have spread

Manufacturers' guaranteed minimum current transfer ratios generally have a wide spread for phototransistor opto-isolators. The guaranteed minimum ranges from 20 to 100%, depending upon the device and operating temperature, says William Sahm, application engineering consultant at General Electric, Auburn, N.Y. The outside limits of opto-isolator operation are normally specified at -55 to 100 C, with the high mark generally established by the reduced quantum efficiency of the LED at that temperature.

The current-transfer ratio is of major interest to the user over a range of LED input current. Yet most specification sheets simply give it at some nominal value of current and temperature. Curves may, but frequently don't, accompany the data from which the designer can interpolate his own spread.

Use of the values on the spec



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Actual Size

INFORMATION RETRIEVAL NUMBER 13



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sheets can lead to design trouble, cautions Virgil Merkel, senior development engineer at Potter & Brumfield, Princeton, Ind. "The transfer ratio for different input currents can vary widely from supplier to supplier," he notes, "and also from isolator to isolator within a given group."

Merkel points out that the current-transfer ratios of LED/photo-transistor devices that he has tested range from about 6 to 200%. For higher transfer ratios, he has found that LED/photo-Darlington configurations range from 100 to 600%.

Output can vary widely

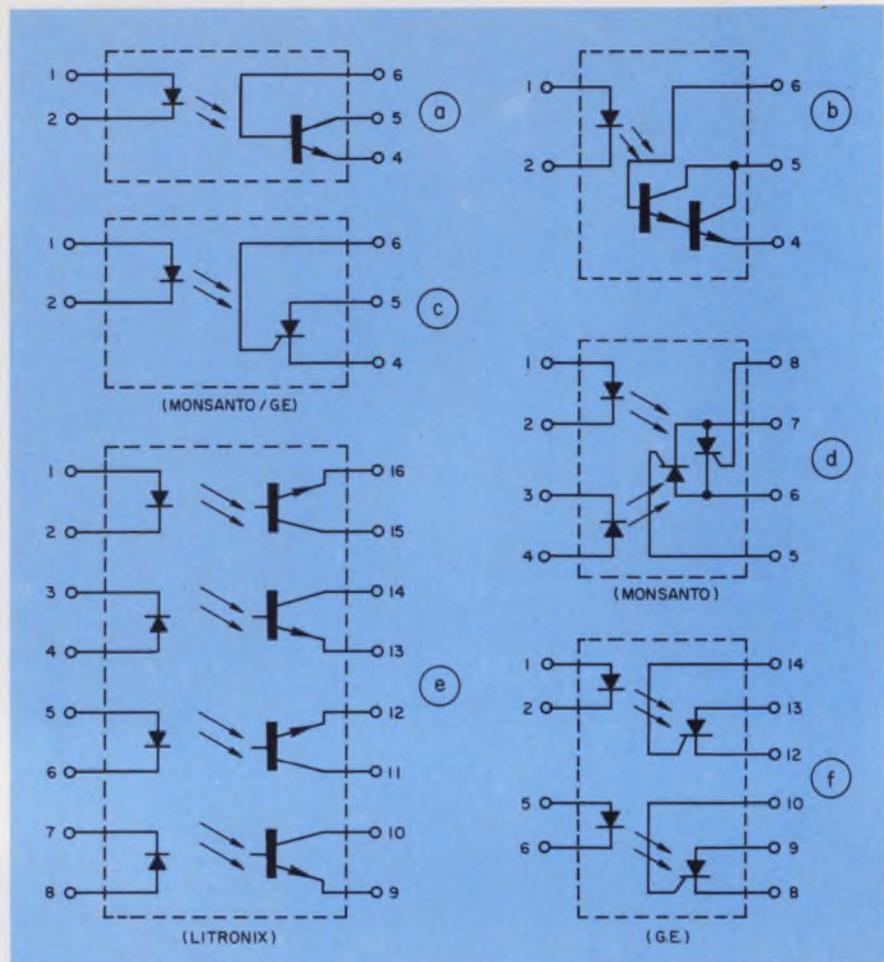
GE's Sahn points out that one of the biggest problems in applying LED opto-isolators is in determining just how much output current can be reliably expected for a given operating ambient temperature. The reason? The output is not only a function of temperature but also of the device's forward current transfer ratio, and the latter is subject to wide variation.

For example, in a 30-C ambient, 40 or 50 mA can generally be applied to opto-isolator LEDs. For a device with a 100% current-transfer ratio, 40 or 50 mA may be expected from the phototransistor. However, few applications can be designed on this low temperature margin. For a safe operating temperature, 60 C is more realistic. Use of this temperature reduces the allowable input to about 20 mA.

If the device has 100% current transfer, this would mean an output of 20 mA, but with a 20% device, only 4 mA could be obtained. It is therefore necessary to make sure that the guaranteed minimum current transfer ratio is high enough to provide sufficient current.

If, for example, 20-mA output were needed in a 60-C application, one answer would be to use an isolator with a photo-Darlington amplifier. The guaranteed minimums with these devices range from 100 to 600%.

"Photo-Darlington are used for the higher ambients or for heavier loads," says Sahn. "As the temperature rises, the Darlington beta goes up much more than that for



1. These photo-isolators with LEDs and silicon photosensors are available in DIP packages. The phototransistor (a) and photo-Darlington (b) are multi-sourced. The photo-SCR (c), bidirectional SCR (d), dual SCR (f) and the quad phototransistor unit (e) are made by the manufacturers indicated.

a transistor, giving a higher current transfer ratio. As a result, you can operate at a higher temperature for a given output current with the photo-Darlington than with a regular phototransistor."

The penalty paid is the reduced operating speed of the Darlington, which is typically around one-tenth that of the phototransistor. But for some applications, Sahn notes, this may be an advantage. For example, if noise spikes are present on the LED input, the slower response of the photo-Darlington can prevent the spikes from appearing at the output of the device.

Isolator speed is variable

Typical low-cost phototransistors generally specify turn-on and turn-off speeds of 3 μ s, says Sahn.

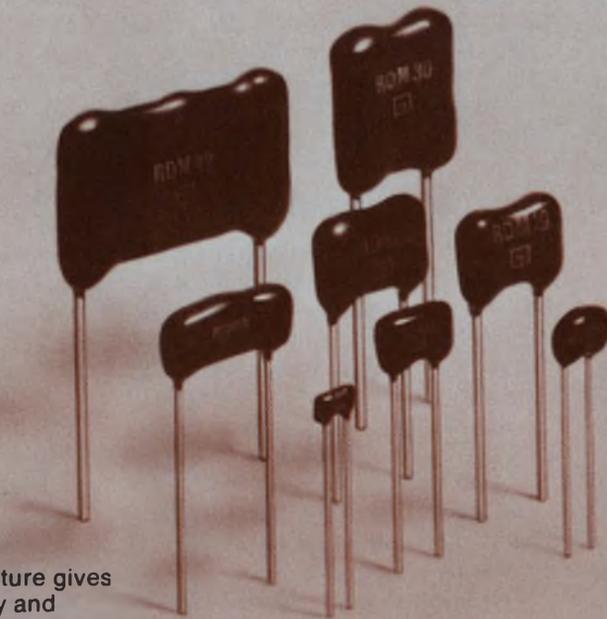
"But speed can be varied by orders of magnitude by biasing

the coupler," he notes, "so make sure you have the proper bias for the desired switching speed."

Most of the six-pin DIP packages with the LED/phototransistor combination have the base connected to one of the pins. However, for highest sensitivity, the base is usually left open. But sensitivity can be traded for higher speed by loading the base.

Sahn points out that using phototransistor isolators gives reasonably good linearity of response from ranges of LED input current of 1 or 2 mA up to 20 or 40 mA. And the response over a range of temperature is fairly linear because of a fortunate circumstance: The output of the LED has a negative temperature coefficient—that is, as temperature increases, the quantum efficiency of the LED decreases, producing less light. But this is offset to some degree by the positive temperature coefficient of the transistor.

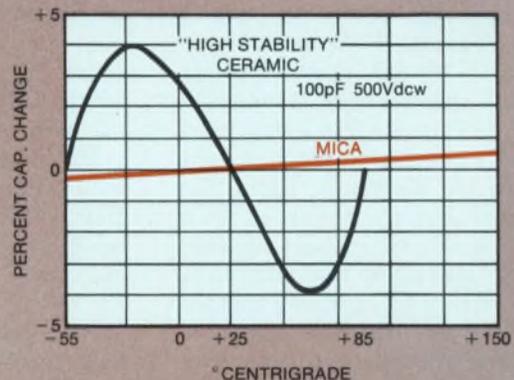
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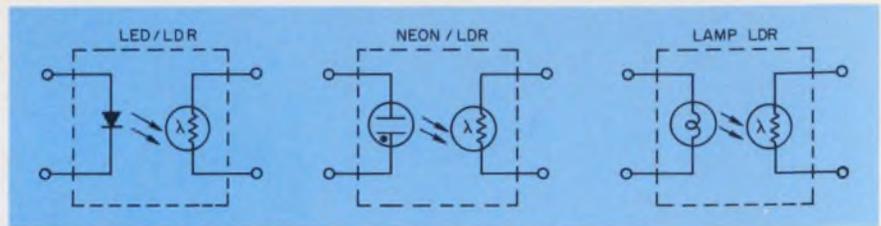
Special isolators are designed for high voltages. These units, by Sigma Instruments, are rated at 15 kV rms (left) and 1 kV (right). The 15 kV unit is a tungsten lamp/photoresistor device. The other has a LED.

By far the fastest opto-isolators are those using photodiodes. But since the diodes are operated in the back-biased condition, the output is usually small. Some diodes are designed for relatively high outputs. For example, in Monsanto's MCD2 isolator, the current output ranges from 40 to 100 μ A. For six-pin DIP devices, with a phototransistor, the base-collector diode can be used, with the emitter open.

In any event, the diode output must be amplified, either by an external transistor amplifier or by an amplifier stage on the same chip, as Hewlett-Packard does in its 4351 high-speed, optically coupled unit. Packaged in an eight-pin DIP, this device is useful up to 10 MHz. Current transfer ratios of 10 to 20% are realized, with outputs on the order of 1 to 10 mA. The HP device has the fastest isolator speed currently available. Its output can be directly coupled to TTL loads at TTL speeds.

A trend toward more circuitry in an isolator package is exemplified by HP in its 4360 device—a DTL/TTL-compatible isolated logic gate in an eight-pin DIP. The photodiode output is applied to a monolithic IC chip, which contains a linear amplifier that drives a Schottky-clamped output transistor. A 5-mA input to the 4360 sinks an eight-gate (13 mA) fan-out at the output. The device can operate at a 20-megabit rate.

Monsanto has an eight-pin DIP—the MCL 610—with a gallium-arsenide LED and a fast photodiode. The diode output is amplified with a differential amplifier/



2. Photo-isolators with photoresistor (LDR) outputs use light sources of visible LEDs, neon lamps and tungsten lamps. The bidirectionality of the LDR units makes them useful in applications using ac voltages.

comparator that drives a Schmitt trigger. The output of the Schmitt drives a standard TTL totem-pole circuit that has both sourcing and sinking capability. The operating speed is 1 MHz.

Litronix has gone in another direction with the "more-in-one" package by incorporating in a 16-pin DIP four separate LED/photo-transistor isolators. The device—the ILQ-74—specifies a 35% typical transfer ratio for the quad units.

SCR isolators switch power

Light-activated SCRs are packaged with gallium-arsenide diodes to provide isolation between low-power circuitry and ac line voltages carrying switching or relay functions. Monsanto's LED/SCR combination is packaged in a six-pin DIP, with 1500-V dc isolation and an anode rating of 200 V for the MCS2 and 400 V for the MCS-2400. The maximum anode current for both is 150 mA.

General Electric has equivalent units—the MC11C1 and the HC-11C2, with surge voltage isolation of 2500 and 1500, respectively. The maximum forward current is 300 mA, and the minimum peak reverse voltage is 300. GE also has a single LED/SCR unit in a TO-77 can with slightly higher ratings.

Monsanto packages a dual LED/SCR combination in an eight-pin DIP, with the SCRs connected anode to cathode internally or bidirectional switching. GE has two LED/SCR isolators in a 12-lead, 14-pin DIP. Connections to the SCRs are independent.

The majority of applications of optical isolators are digital, says David Barton, senior member of the technical staff at Litronix. Many methods of incorporating these devices into logic systems have been published, he says. But

his cardinal rule is: "To keep out of trouble, keep it simple." If you're going to drive the LED with a standard TTL, drive it in the current-sinking mode—never the current-sourcing mode.

To drive TTL logic with the phototransistor output, Barton continues, use the phototransistor collector as the output feeding into the gate input.

"Put a resistor of 15 K from the phototransistor collector-gate junction to V_{CC} and ground the emitter—that's all there is."

A generic class of opto-isolators uses photoresistive materials—cadmium sulfide, cadmium selenide, and cadmium sulfo-selenide—for the photosensor.

The latest isolators of this type are using visible gallium-arsenide-phosphide LEDs, because the photoresistive materials have peak sensitivity in the visible region.

For the LED-driven photoconductor isolators, the response speed is limited solely by that of the photosensor—normally on the order of a few milliseconds. This is also the case with neon units. With tungsten light sources, the thermal hysteresis of the filament can be the governing factor.

Tungsten-lamp devices have played important roles in telephone equipment, with life expectancies of 10 years or more obtained when the lamp is derated. But LEDs are replacing the tungsten lamps.

Norman Wolff, chief engineer at Vactec, points out that the big application for LED/photoresistor units is in audio circuits and similar applications, where the bilateral characteristic of the photoconductor is needed. A second big use, he says, is in high-voltage circuits, such as those that turn on triacs.

With a neon/photoresistor coupler, he points out, it is possible to apply line voltage to both sides of the device. For monitoring ac



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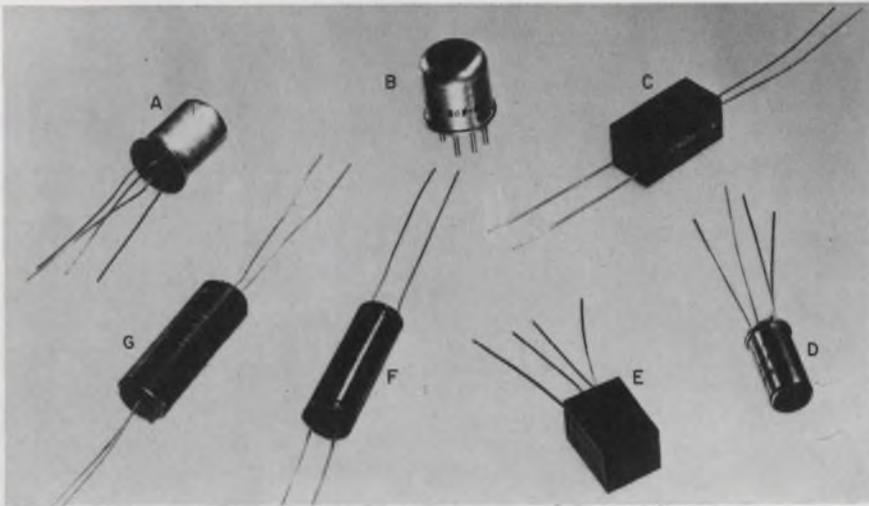
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Relatively high input voltages are applied to neon-lamp/photoresistor isolators because they require from 80 to 125 V dc to fire the lamp. They are used in on-off applications such as firing SCRs and triacs or for monitoring line voltages. Resistors are used in series with the neon bulb to limit current to a safe value. Some units incorporate this resistor as an integral part of the isolator package. Representative types shown are by Quantron Electronics A,C); Vactec (B,D,F) and Clairex (E,G). Most units are packaged in plastic, but others, like A and B are hermetically sealed.

line voltage and voltages with transient spikes, the slow speed of the photosensor filters out the 120-Hz ripple and other line pulses.

Tungsten lamps for the isolators are usually rated from 6 to 24 V. Sigma Instruments provides isolators with 150-V, 2 mA lamps.

A prime limitation of the photoresistive cell is its temperature sensitivity. Above 75 C, according to Wolff, permanent changes in the

characteristics can occur.

Another photon-coupled device being applied widely is the optical switch. Simple in form, it may be of the interrupter type, in which the output of a LED in one arm of the device falls upon a photosensor in the opposite arm (see photo). Or it may be of the reflective type, in which the radiation from a LED is reflected by some active surface back into the

The basic opto-couplers

There are five basic optical couplers that use LEDs—either gallium arsenide or gallium-arsenide-phosphide—as the source of radiation. They are LED/phototransistors, LED/photo-Darlington, LED/photodiodes, LED/SCRs and LED/photoresistive cells. Except for the LED/photoresistive cell, all are now appearing in DIP packages as well as nonstandard.

Two other types of opto-isolators have preceded the LED devices. One is a neon lamp with a photoresistor; the second is the tungsten lamp and photoresistor combination.

The neon-photoresistor and tungsten-photoresistor combinations are relatively slow, compared with solid-state devices, and specifications are fairly simple. The main specification problems arise with the solid-state devices that use LEDs as the light source.

phototransistor. These devices are fabricated with a single or a double LED/photosensor pair.

For the interrupter module, typical applications include optical shaft encoders, proximity detectors and choppers. The opto-reflectors are used for end-of-tape or beginning-of-tape sensing as well as mark sensing and in optical automobile ignition systems. ■■

Need more information?

The companies and products cited in this report have been selected for illustrative qualities. The photon-coupled devices of these and other companies are identified below. The code to these products indicates the available combination of optical emitter and photosensor; LD—LED/photodiode; LT—LED/phototransistor or photo-Darlington; LS—LED/silicon-controlled rectifier; LR—LED/photoresistor; NR—neon/photoresistor; TR—tungsten lamp/photoresistor; PS—photoswitch.

Centralab Semiconductor Products, 4501 N. Arden Dr., El Monte, Calif. 91734. (213) 686-0567. (L. Merrill Palmer) LD, LT, PS Circle No. 420
 Clairex Electronics, 650 S. 3rd Ave., Mount Vernon, N.Y. 10550. (914) 664-6602. (Gerald F. Smith) LT, LR, NR, TR Circle No. 421
 Dialight Corp., 60 Stewart Ave., Brooklyn, N.Y. 11237. (212) 497-7600. (Chester Dombroski) LT Circle No. 422

Fairchild Optoelectronics Div., 4001 Miranda Ave., Palo Alto, Calif. 94303. (415) 493-3100. LT, PS (Ralph Miller) Circle No. 423

General Electric Co., W. Genesee St., Auburn, N.Y. 13021. (315) 253-7321. (William Sahm) LT, LS, LR, PS Circle No. 424

General Electric, Hendersonville, N.C. 28739. (704) 692-1431. (David Stephenson) LR, TR Circle No. 425

Hamamatsu Corp., 120 Wood Ave., Middlesex, N.J. 08846. (201) 469-6640. (Ralph Eno) LD, LR, NR, TR Circle No. 428

HEI, Inc., Jonathan Industrial Center, Chaska, Minn. 55318. (612) 448-3510. (Peter Spaulding) PS Circle No. 429

Hewlett Packard, 640 Page Mill Rd., Palo Alto, Calif. 94304. (415) 493-1212. (Gary Spear) Amplified LD, Logic Gate Circle No. 426

Litronix, Inc., 19000 Homestead Rd., Cupertino, Calif. 95014. (408) 257-7900. (Robert Santos) LT Circle No. 427

Monsanto Electronic Special Products, 3400 Hillview Ave., Palo Alto, Calif. 94304. (415) 493-3300. (Daniel Balfe) LD, LT, LS, PS, Logic Gate Circle No. 430

Motorola Semiconductor Products, Inc., Optoelectronics Dept., POB 20912, Phoenix, Ariz. 85306. (602) 244-6900. (Ron Schilling) LT Circle No. 431

National Semiconductors, Ltd., 331 Cornelia St., Plattsburgh, N.Y. 12901. (518) 561-3160. (Duncan Clifton) LD, LR, NR, TR Circle No. 432

National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, Calif. 95051. (408) 732-5000. (Henry Carbajal) LT Inquire Direct Circle No. 435

Optron, Inc., 1201 Tappan Circle, Carrollton, Tex. 75006. (214) 242-6571. (Charles Bates) LD, LT, PS Circle No. 433

Quantron Electronics, Inc., 1820 Mills Ave., El Paso, Tex. 79901. (915) 532-4651. (Rhodes Chamberlain) LR, NR, TR Circle No. 435

Sensor Technology, Inc., 21012 Lassen St., Chatsworth, Calif. 91311. (213) 882-4100. (Irwin Ruben) PS Circle No. 436

Sharp, Shigoto Industries Ltd., 350 Fifth Ave., N.Y. 10001. (212) 695-0200. (Norman Axelrod) LT, PS Circle No. 437

Sigma Instruments, Inc., Braintree, Mass. 02148. (617) 843-5000. (William Cook) LR, NR, TR Circle No. 438

Solar Systems, Inc., 8124 N. Central Park, Skokie, Ill. 60076. (312) 676-2040. (William Megberg) LR, NR, TR, PS Circle No. 439

Spectronics, Inc., 830 E. Arapaho, Richardson, Tex. 75080. (214) 234-4271. (R. M. Stringer) LD, LT, PS Circle No. 440

Texas Instruments, P.O. Box 5012, Mail Sta. 12, Dallas, Tex. 75222. (214) 238-3821. (William Senhauser) Amplified LD, LT, PS Circle No. 441

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When you measure with The Danameter, you interpret nothing. All you are shown is a number that is precisely the information you require.

It's accurate to a degree that you never imagined possible in an instrument at this price.

Once you have selected the proper function position, The Danameter instantly interprets, selects, and converts your information. It shows in a large liquid crystal display that adjusts to all light conditions. Even direct sunlight.



Automatic Polarity.

In measuring voltage, you're accustomed to swapping leads to get a reading.

The Danameter instantly determines polarity, and then displays it as either positive or negative. All in a fraction of a second, with no help from you.

Almost indestructible.

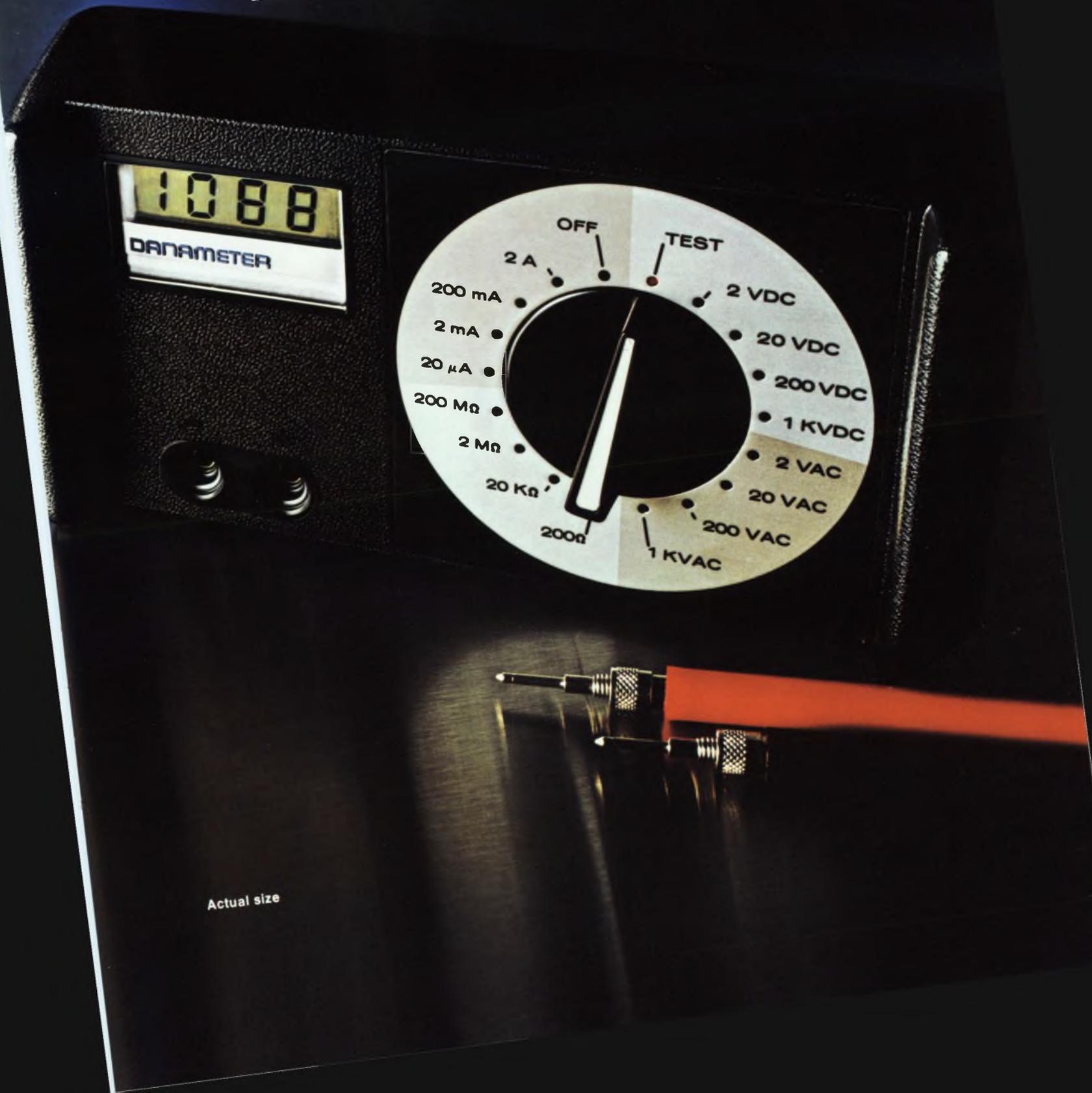
The Danameter has only one function selector. It's recessed behind the molded edges of its cyclac case. You can drop it on concrete. You can kick it down the hall.

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1974.



Actual size

Model 2000 Danameter Specifications

Warranty: 1 year.

Measurement Functions: (4) DC volts, DC current, AC volts and ohms.

Typical Specifications:	
DC Volts	
Ranges	2V, 20V, 200V, and 1KV
Resolution	1mV
Overload protection	1000V DC or peak AC, any range
Accuracy	±(1.5% Rdg. + .05% Range)
Polarity	Automatic
Input Resistance	10 Megohms
Normal mode rejection	50 dB min. at or near 60 Hz

AC Volts	
Ranges	2V, 20V, 200V, and 1KV
Resolution	1mV
Overload protection	1000V peak AC, 250V DC, any range
Accuracy	±(1.5% Rdg. + .15% Range) to 5 KHz
Input Resistance	2 Megohms

DC Current	
Ranges	20 μ a, 2 mA, 200 mA and 2A
Resolution	.01 μ a
Accuracy	±(1.5% Rdg. + .1% Range)
Overload protection	250V DC or RMS

OHMS	
Ranges	200 Ω , 20K Ω , 2M Ω and 200M Ω
Resolution	.1 ohm
Accuracy	±(2% Rdg. + .15% Range)
Maximum current through unknown	1 mA
Overload	250V DC or RMS

General	
Battery	One 9V dry battery
Est. battery life	1 year at normal usage
Test leads	Included
Size	4"H x 7 $\frac{1}{4}$ "W x 2 $\frac{1}{4}$ "D
Weight	1 lb.
Overload	Fully protected on all ranges

Price	
Model 2000 Danameter	\$195.00

Accessories	
Part No.	
2040	R.F. Probe (to 200MHz)
2030	H.V. Probe (to 30Kv)
2020	Carrying Case
2060	Extra Test Leads

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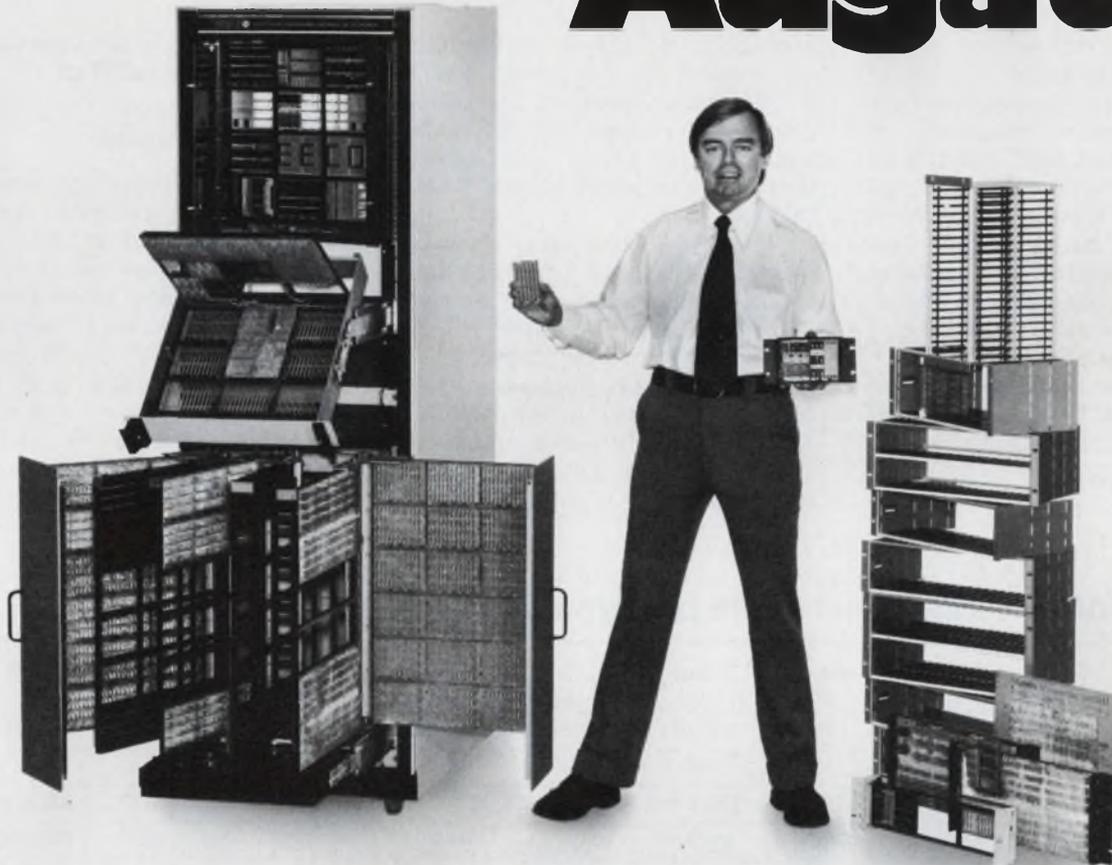
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4096-bit RAMs making the scene as an alternative to core—finally

After many delays and a few false starts, 4096-bit dynamic RAMs are finally getting into the hands of memory designers. It now appears that they will live up to their promise of being a cheaper and higher speed alternative to core. The 4-k RAMs are also reducing the number of packages and power dissipation in solid-state memories. All are n-channel types except for one company's.

Some of the manufacturers of 4096-bit RAMs have been in pilot

production for a few months; others are not too far behind. Frank L. Rittiman, product marketing manager for American Microsystems, Santa Clara, Calif., says there will be plenty of 4-k RAMs this year.

"In 1974," he says, "several manufacturers will be getting into actual production. As the memory boards are designed, there will be enough RAMs to fill them."

One industry spokesman predicts: "I bet that in the last half of 1974 we will see a couple of small to medium solid-state memories in production using the 4-k's.

The mainframe applications should start appearing in '75."

They're quite similar

With a few notable exceptions, the RAMs are similar in performance and packaging. All, except one, are provided in the 22-pin DIP. Access times range from 180 to 390 ns, cycle times from 340 to 575 ns and active power dissipations from about 250 to 400 mW. The units also vary in clocks required, refresh cycles and pin-outs.

The first 4096-bit RAM offered

Northe K. Osbrink
Western Editor

Specifications of the latest 4096-bit dynamic RAMs

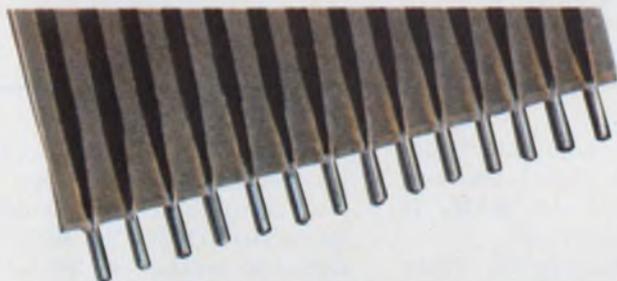
	TI	Motorola AMI	Intel (B)	EA (B)	Mostek (C)	MIL	SMC	AMS
Model No.	TMS 4030	6605	2107A	1504	MK 4096P	MF 7112 (E)	N4412 (G)	6004
Transistors in cell	1	3	3	1	1	3	3	3
Chip size in mils	160 × 180	168 × 195	137 × 167	—	157 × 185	149 × 166	159 × 170	200 × 209
Type (gate)	NMOS(Si)	NMOS(Si)	NMOS(Si)	NMOS(Si)	NMOS(Si)	NMOS(Si)	NMOS(Metal)	PMOS(Metal)
Access time (ns)	300 Max	230 Max	Approx 300	Approx 300	300 (D)	390	180	350
Cycle time (Read-write) (ns)	470-470 Max	470-430	Approx 500	Approx 500	450 (D)	510-455	340-340	575
Power dissipation Active (mW)	400	70 μ W/bit	—	400	<100 μ W/bit	<100 μ W/bit	300 TYP	60 μ W/bit max
Power Dissipation STBY (nonrefreshed) mW	2	5 μ W/bit	—	—	—	—	—	—
Power dissipation STBY (refreshed) mW	—	0.5 μ W/bit	—	50	<2.5 μ W/bit	<10 μ W/bit	2 TYP	50 μ W/bit max
Power								
V _{BB}	-3	-5	-5	-5	-12	-2	-2	+8
V _{CC}	+5	+5	+5	+5	+5			
V _{OD}	+12	+12	+12	+12	+12	+12	+15	-15
V _{SS}					0	0	0	+5
Inputs (compatible)	MOS/TTL	MOS/TTL	MOS/TTL	TTL	TTL	NMOS(H)	TTL	MOS/TTL
Outputs (compatible)	TTL	TTL(A)	TTL	TTL	TTL	Current(F)	Current(F)	Current(F)
Refresh rate (ms)	2	2	—	—	4	2	1	2
Refresh cycles	64	32	—	—	64	16	64	64
Clocks required	1-12 V(CE)	1-12 V(CE)	1-12 V(CE)	—	2-TTL	3-12 V	1-12 V	3-15 V
(A) Also available with ECL output for faster access time—as type 6606		(C) Uses 16-pin DIP, all others 22-pin			(E) E-Mask version		(G) Equivalent to four 1103-1 1-k RAMs	
(B) Approx values—data sheet not yet available		(D) Becomes 200, 300 ns in page mode			(F) External driver required for TTL compatibility		(H) Must be driven with a bi- polar to NMOS driver such as the MIL-MD6154	

Strength where it's needed!

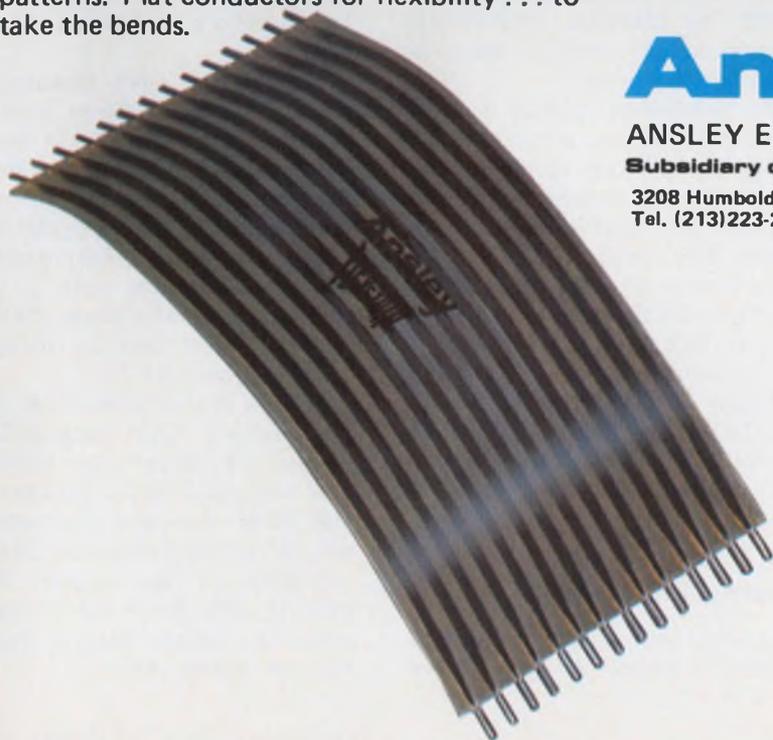


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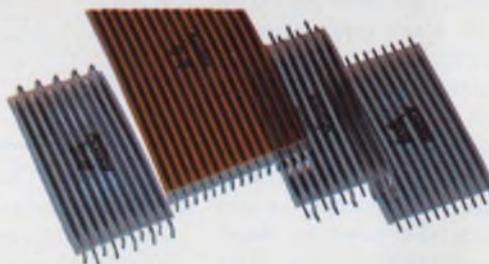


The secret is round pins and flat conductors. Round pins to fit p.c. board hole patterns. Flat conductors for flexibility . . . to take the bends.



Four insulating materials are available to cover a wide range of temperature (and cost requirements). Nomex*, Mylar*, Teflon*, Kapton* are available. Standard lengths are 1", 2" and 3". Conductor pin spacing can be .050, .100, .125, .150 or .200.

* Dupont Trademark



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commercially was the MF 7112 by Microsystems International Ltd., Ottawa, Canada. The original version—Model A, introduced in late 1972—was a large chip, 168 by 172 mils. Gradually Microsystems has been increasing the performance and decreasing the chip size. The current memory, Model E, is 149 by 166 mils, one of the smallest.

The Microsystems unit may be more difficult to design into a system than most of the other 4-k's, since it requires three high-level clocks and an external circuit to make the input TTL-compatible. John Roberts, senior applications engineer for the company, points out:

"The mainframe computer manufacturer who uses large numbers of memory packages usually feels that the peripheral circuitry is of relatively little importance. What he needs are parts that are producible, inexpensive and dependable."

Microsystems has been shipping the 7112 to at least one customer since early 1973.

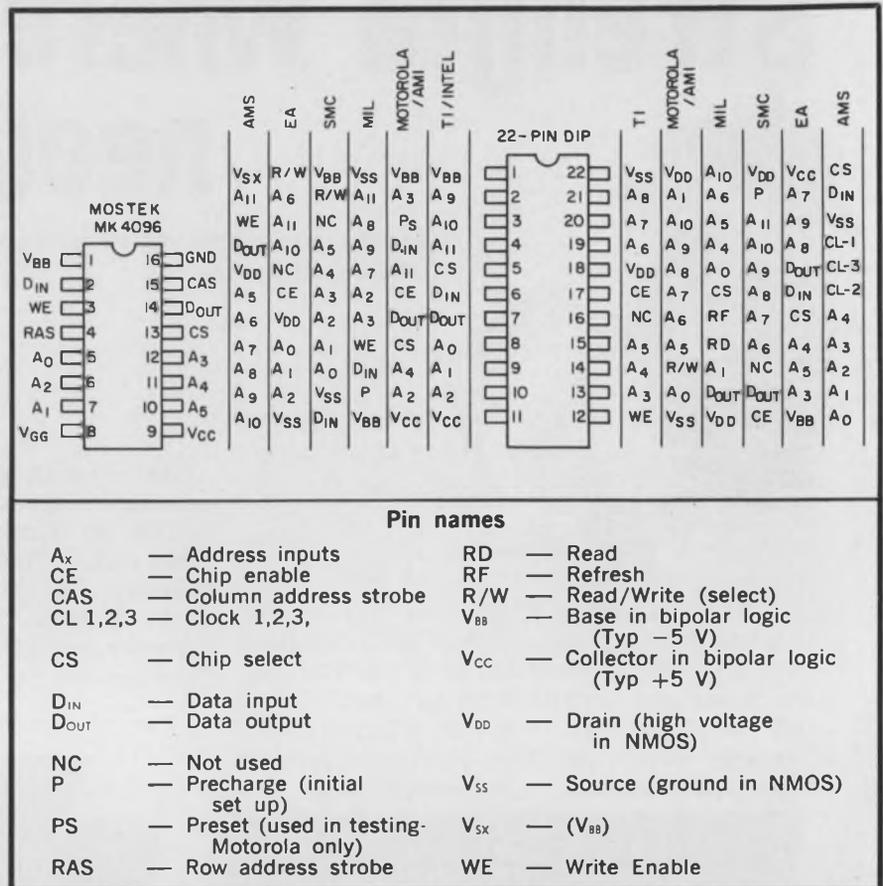
Texas Instruments in Dallas, which stayed out of the scramble to produce 1-k RAMs, has developed the TMS 4030—a one-transistor cell design, as opposed to the three-transistor cell used by most of the other manufacturers. The TI pinout arrangement has established itself as an early leader in the race to become the industry standard. A number of manufacturers are adopting it, even at the expense of redesigning parts well into the development stage.

Initially Intel in Santa Clara introduced its 2107 4-k RAM with its own pinout. But Mike Markkula, marketing manager for Intel, explains:

"TI liked our pinout and was going to use it, but somewhere in development there was a slip and their connections were different. There is no question that TI is the standard, so on our 2107 A we changed some connections, rotated the chip, and now we'll be using their pinout."

At least six other manufacturers are said to have adopted the TI pinout. Intersil in Cupertino, Calif., will be introducing in early spring a 4-k RAM that uses the TI pinout and will have basically the same electrical characteristics, although it uses a three-transistor

Pinout arrangement of 4-k dynamic RAMs



cell. Signetics in Sunnyvale, Calif., is working on a circuit that may second-source TI's 4-k RAM. It uses a one-transistor cell.

Motorola Semiconductor, Phoenix, and American Microsystems have jointly developed the masks for their RAMs. The 6605-6606 series from either manufacturer should be identical, though the manufacturing process may be somewhat different.

The 6605-6606 pinout has all power pins on the corners of the package, providing maximum isolation between power supplies in case of board or component failure. The circuit is fast and has a low power dissipation. It is the only 4-k RAM with a choice of TTL or ECL output.

A newcomer in the RAM field, Standard Microsystems of Sunnyvale, Calif., has based its memory on the 1103-1, a high-speed version of the widely used 1103 1-k RAM.

P-channel isn't dead

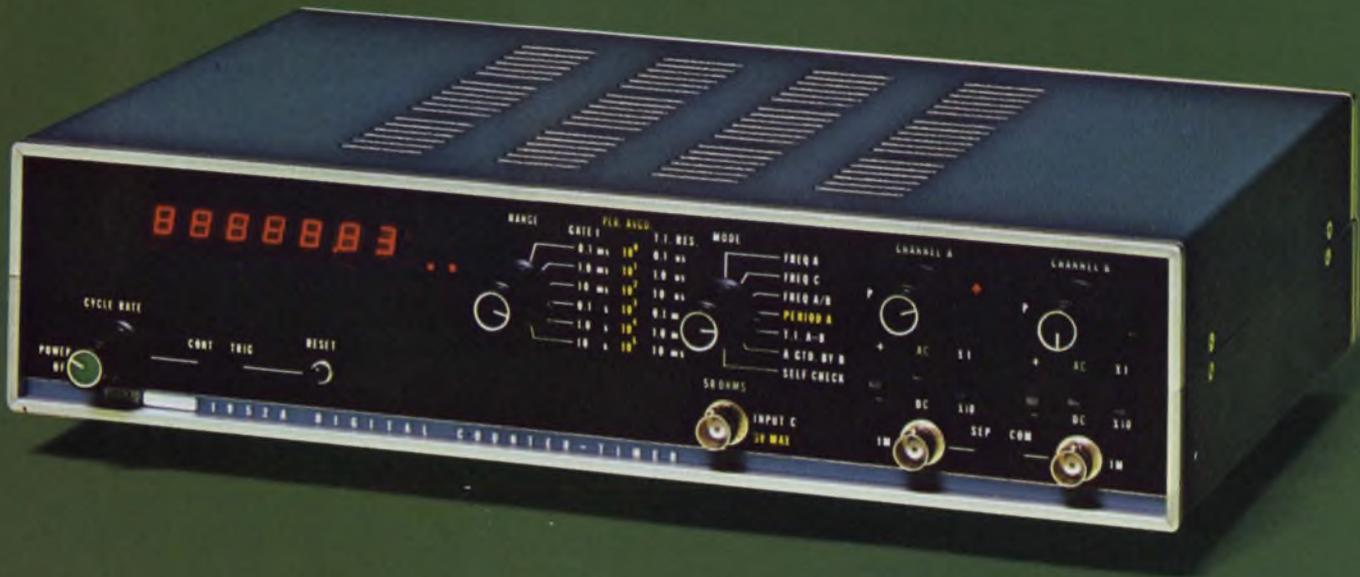
Proving that p-channel technology is still around, Advanced Mem-

ory Systems of Sunnyvale, Calif., is producing a p-channel 4-k RAM. Just as the SMC 4412 is designed to replace 1103s, the 6004 is designed to replace the 2-k-bit 6003. One user of the circuit will definitely be Advanced Memory Systems itself, since it uses a good percentage of its own production in memory modules that it sells.

The PMOS 6004 features 350-ns access and a 575-ns cycle. Because of the use of the familiar technology, one Advanced Memory Systems official says: "We should be ahead of the competition in making a profit. Remember, the only real problem with a larger chip is a generally lower yield. We make up for that by using the p-channel process."

Mostek of Carrollton, Tex., makes the only 4-k RAM packaged in a 16-pin DIP, rather than the otherwise universal 22-pin package. The MK 4096P uses a single transistor cell. A multiplexing and latching operation on the address inputs permits data to be stored and recalled by pages rather than by random access. ■■

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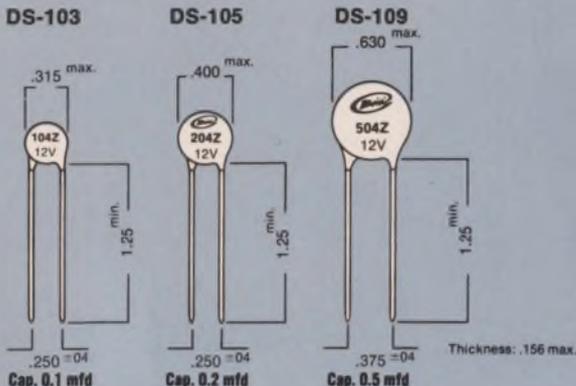
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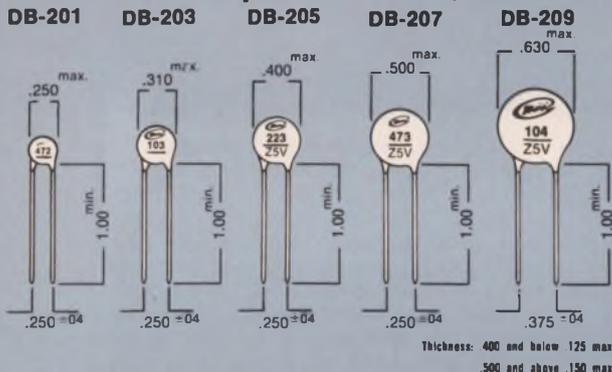
12V.DC Disc Capacitors—Y5S



SPECIFICATIONS

Temperature Characteristics: Y5S
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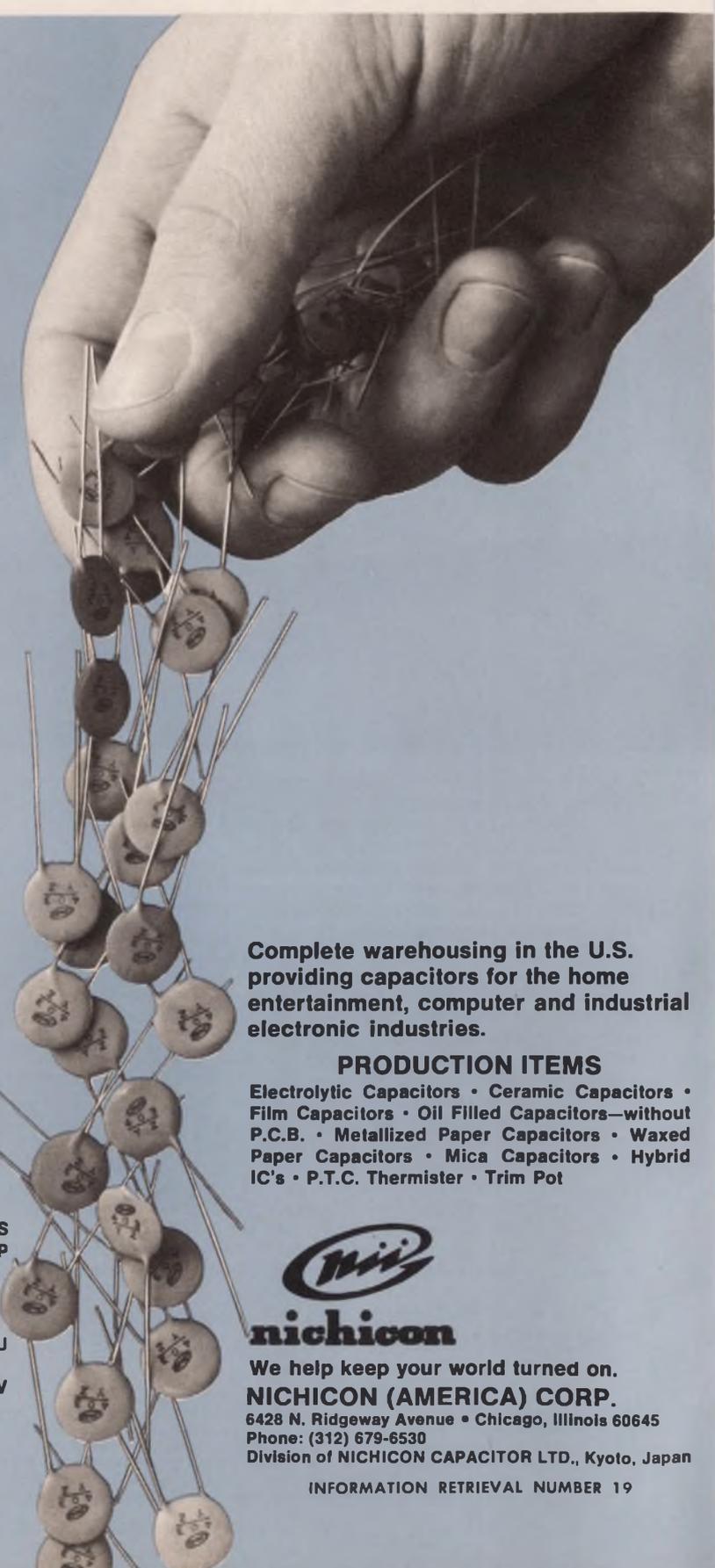
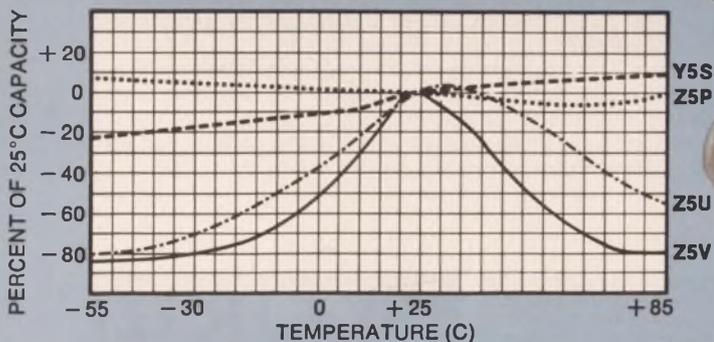
50V.DC Disc Capacitors—Z5P, Z5U and Z5V



SPECIFICATIONS

	Capacitance Range	Capacitance Tolerance
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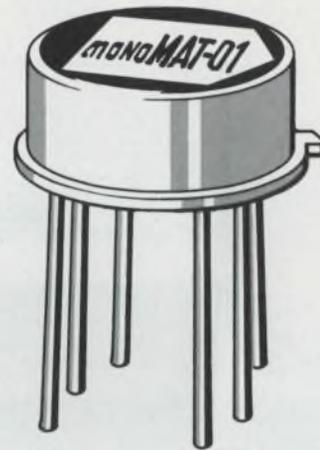
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$TCV_{OS} (-55^{\circ} \text{ to } +125^{\circ}C)$	0.5	0.5	1.8	1.8	$\mu V/^{\circ}C$
$h_{FE} @ I_c = 10\mu A$	500	330	250	250	•
$I_{OS} @ I_c = 10\mu A$	0.6	0.8	3.2	3.2	nA
$TCI_{OS} (-55^{\circ} \text{ to } +125^{\circ}C)$	90	110	150	150	$pA/^{\circ}C$
$I_B @ I_c = 10\mu A$	20	30	40	40	nA
BV_{CEO}	45	60	60	45	V
Price @ 100 pcs.	\$6.00	\$5.00	\$3.75	\$2.50	•

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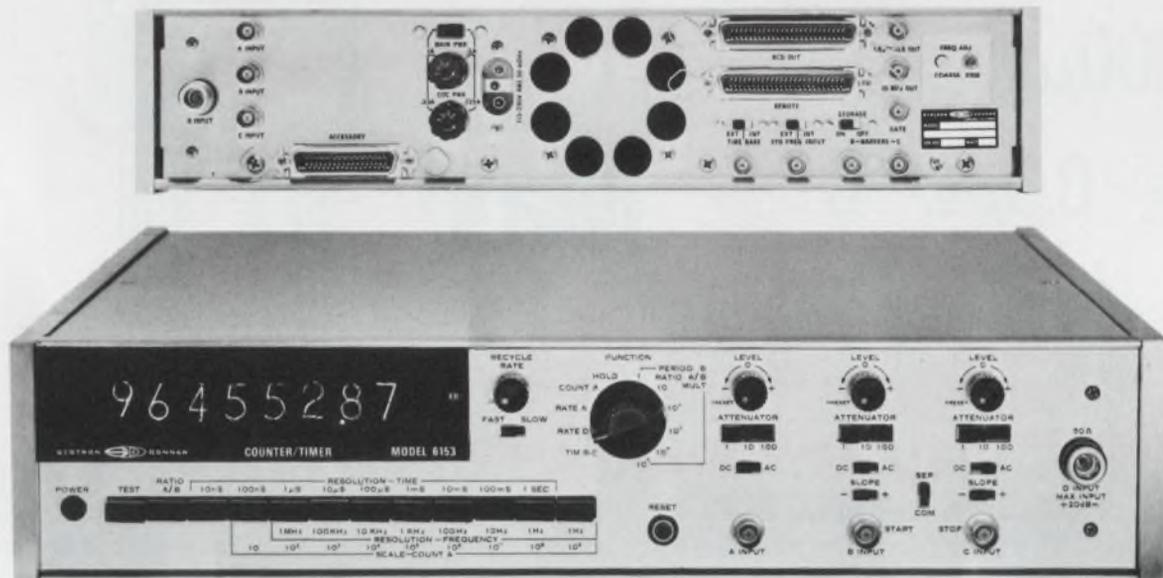
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INFORMATION RETRIEVAL NUMBER 21

washington report



Heather M. David
Washington Bureau

Pentagon sees threat in technology exports

Defense Dept. R & D officials are expressing fear that the Russians may learn vital techniques of microminiaturization of electronic components through proliferating sales of U.S. technology to the Soviet Union. The fears were expressed after Representative Ben Blackburn (R-Ga.) charged that the sale of a scientific computer by a British subsidiary of Control Data Corp. "enabled the Soviet Union to shorten by about two years the time required to create and perfect their first MIRV (Multiple Independent Re-entry Vehicle)."

The Pentagon sources said there was less concern about the sale of computational ability itself than the fact that the Soviet could learn techniques of microminiaturization by studying the equipment. As one official put it: "The Soviets can do the computer work, but it may take them a computer the size of a barn to do what we can do on an aircraft." Rep. Blackburn is collecting other data on U.S. technology sales to the Russians for hearings that may be held this month by the House Banking and Currency Subcommittee on International Trade. Blackburn will introduce a bill embargoing exports to any country that conducts a "policy intended to harm the economy or endanger the security of the United States."

The National Security Council meanwhile is urging a more lenient line than the Administration was considering last fall in permitting U.S. companies to sell computers and related technology to Communist-bloc countries. The Administration is now expected to okay a proposed American bid on a Soviet air-traffic-control system. The bid proposal is headed by IBM and would include IBM 9020 computers, smaller Univac computers and alphanumeric displays by Raytheon and Texas Instruments.

Government to spend \$15-billion for electronics in '75

The Federal Government should spend about \$15-billion for electronics during FY 1975, unless there are serious market disruptions because of the energy crisis. This is the average prediction of member companies of the Electronic Industries Association. The EIA predicts that military electronics spending estimated at \$12-billion for FY 1975, will go to \$14.9-billion by FY 1980.

In the area of defense, EIA sees the most important growth areas for the electronics industry over the decade to be strategic weapons, intelligence and communications projects, shipboard electronics and R&D. And as weapons become more sophisticated electronics will take an increasingly larger percentage share of the program dollars. For the fiscal year beginning July 1, EIA says the Defense Dept. should spend about \$7.9-billion for aircraft, with 27.9% for electronics; \$5.3-billion for missiles, 45.1% for electronics; \$586-million for military space, 46.6% electronics;

\$4.3-billion for ships, 23.1% electronics; \$1.1-billion for electronics and communications systems, 88% electronics; and \$21.8-billion for operations and maintenance weapons including spare parts, 11.3% of which would go for electronic equipment and parts.

EIA members surveyed said that NASA should spend about 37.7% of its approximately \$3.1-billion budget for electronics. This would include \$1.2-billion for manned spaceflight, 37.1% electronics; \$70.7-million for space sciences and applications, 46.8% electronics; \$68.8-million for space research and technology, 34.8% electronics; and \$176.6-million for aerospace technology and research, 26.8% electronics. The Federal Aviation Administration, EIA says, should spend about \$229.7-million in FY 1975 for electronics, a figure that should go to more than \$300-million a year by 1980.

The agency with the biggest potential growth in electronics, the industry association survey indicated, will be the Environmental Protection Agency, which will increase spending on pollution monitoring instrumentation over the next few years. EPA's FY 1975 electronics spending should reach \$158-million, a figure that could go to \$512-million in FY 1980, EIA said.

Other estimates made for FY 1975 electronics spending are: Coast Guard, \$82.6-million; Federal Highway Administration, \$131-million; Federal Railroad Administration, \$11-million; Urban Mass Transportation Administration, \$36-million; National Highway Traffic Administration, \$22-million; Housing and Urban Development, \$67-million; Health, Education and Welfare, \$996-million; Commerce, \$50-million; Law Enforcement Assistance Administration, \$86-million; and Postal Service, \$50-million in Government funding. The complete forecast is available from the Government Products Division, EIA, 2001 Eye Street, Wash., D.C. 20006.

Televised conferences by satellite and microwave

Comsat General and Microband Corp. of America, both of Washington, D.C., are discussing the feasibility of coupling Comsat's digital television transmission and Microband's microwave multipoint distribution system to provide the means for holding televised industrial conferences. Comsat says that business conferences or TV programs could be distributed to customers within a 20 to 25-mile radius of an omnidirectional antenna transmitting at 2150 to 2160 MHz to individual two-foot microwave dishes at each customer's location. The system would be able to receive and decode the digitized data for viewing on an unused channel of a standard TV set or a large screen display.

Capital Capsules: Garrett Corp.'s AiResearch Mfg. Co., Torrance, Calif., won an \$8-million contract for development of an advanced-technology rail vehicle. Garrett's design for the two-car train calls for a new flywheel propulsion system that stores energy aboard the train rather than dissipating it in wasted heat. . . . The Dept. of Transportation has issued a report called "Technology Sharing" for use by organizations and individuals interested in using federally developed technology and information. The report is available from the department at 400 Seventh St., S.W., Washington, D.C. 20590. . . . The Defense Dept.'s top telecommunications post may be downgraded from the Assistant Secretary of Defense slot to a lower post, following a recommendation by Edward Goldstein, vice president of AT&T, who made a 30-day management study. Some Capitol Hill sources disagree, saying that any office trying to get the three military services to cooperate and centralize their communications systems needs all the high-level clout it can get.



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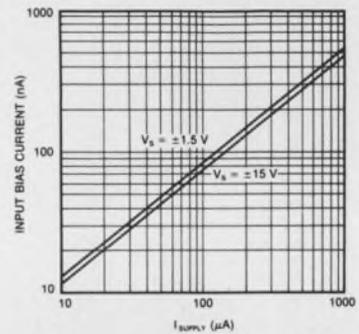
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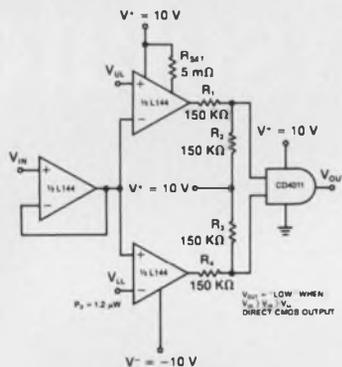
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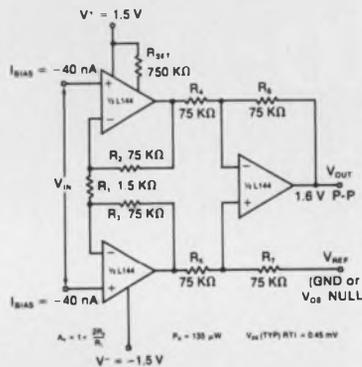
⁽¹⁾L144CJ 100-piece price



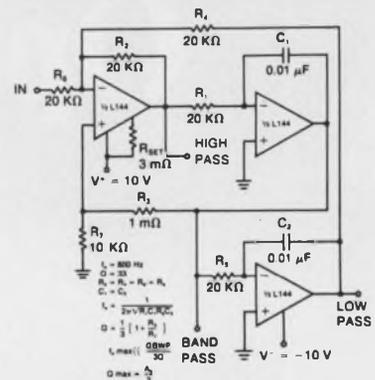
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INFORMATION RETRIEVAL NUMBER 23

ELECTRONIC DESIGN 3, February 1, 1974

The bureaucracy

In "The 900 Days," Harrison Salisbury tries to paint an unemotional picture of the siege of Leningrad by the German armies during World War II. He describes the despair of people trying to survive on sawdust, library paste and other such "nutrients" in a city whose streets were littered with corpses that the survivors weren't strong enough to bury.

What makes this saga terrifying, though, is more than the human suffering and the loss of a million lives—almost all through starvation. It's the behavior of the top Soviet bureaucrats. Until the Germans actually dropped bombs on Leningrad on June 22, 1941, Stalin refused to accept the copious evidence that the Germans were planning to violate his 1939 pact with Hitler. He issued orders that overflying German planes were not be fired at, lest Hitler be provoked. He punished or even executed "panic-mongers" who dared to prepare for a German invasion of the Soviet Union. When he finally began to fight back, he appointed generals and fired them on the basis of their loyalty to his administration—not on the basis of their military experience or acumen. He defended every decision, however disastrous, with the banner of "national security." He tolerated no criticism, for criticism could come only from "enemies of the State."

As we look back over the 30 years that have elapsed since January, 1944, when the Russians broke the siege of Leningrad, can we feel secure in knowing that we, here, are safe from bureaucratic bungling? How many of our designs come about because our boss wanted it that way? And how many times is the boss right because he's boss? And how easy is it for a boss to justify every decision "in the interests of the company" and to blast every critic as a "disruptive troublemaker"?

Certainly, one man (or woman) must make a final decision and be accountable for it. We can't accomplish anything if everybody pulls in a different direction. And disagreements are inevitable—especially on complex design or management decisions.

But disagreements should be aired—and welcomed. In more than a few companies—fortunately not the majority—disagreements and controversy are stifled—subtly, if not overtly. People know that a boss likes to have his own way, so, when they think he's wrong, they shut up. Or, worse, fearing retribution at salary review or promotion time, they pretend agreement.

When I was in the Army, we had a name for such people, and we could all feel superior to them. Sadly, weak managers (and the "I'm always right" managers are weak) force their people to be weak, too—and hurt their companies while they're at it.



A handwritten signature in dark ink that reads "George Rostky". The signature is written in a cursive, flowing style.

GEORGE ROSTKY
Editor-in-Chief

The hows and whys of log amps: Semiconductors used as feedback elements form the log response. And you can avoid drift and instability with carefully designed circuits.

How do logarithmic conversion circuits work, and how do the circuit techniques affect performance?

In brief, log amplifiers use the nonlinear properties of transistors, diodes and other devices to perform signal compression or expansion. But, like most active circuits, they are vulnerable to errors caused by temperature changes and drift, and they may have closed-loop stability problems.

The engineer, of course, has a choice of buying or building the unit he needs. He can create the design from the ground up by use of the most appropriate technique—linear approximation, diodes, matched-dual transistors or other components characterized by logarithmic transfer curves. Or he can buy a low-cost module that contains the necessary logging transistors, reference-current source, frequency-compensating networks and op amps. Table 1 shows several forms in which the more popular circuits are commercially available, with some pros and cons for each.

The basic log element: How it works

For a log amplifier to function properly, its nonlinear element—a diode or transistor—must have a logarithmic transfer function.

The current that flows through an ideal semiconductor diode is governed by this relationship:

$$I = I_0 \left(e^{\frac{qV}{kT}} - 1 \right).$$

In this equation I_0 is the theoretical reverse-saturation current, q is the value of a unit charge; k is Boltzmann's constant, and T is the absolute temperature. By dividing both sides by I_0 and taking logs to the base 10, we can rewrite the equation as:

$$V = \frac{kT}{q} (2.3) \log (I/I_0), \text{ provided } I/I_0 \gg 1.$$

When T is 302.4 K (29.25 C) ΔV is 60 mV

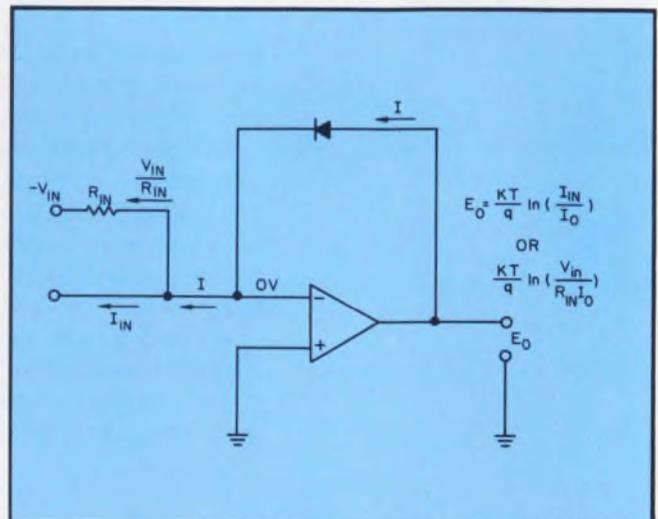
for a 10:1 change of I . If ideal (decade) elements were available the simple circuit of Fig. 1 would yield the desired response. Here the diode is connected in the feedback path of an op amp.

The direction of the diode determines the operating polarity of the circuit. Also, diodes can be stacked in series to increase voltage range, and can operate without grounding.

However, in practice, diodes have a limited logarithmic range. At the high end, ohmic and bulk resistances produce an additional voltage drop, IR_B , and at the low end, the slope of the characteristic undergoes one or more changes due to diffusion-current flow in extended regions—such as surface-inversion layers or channels—and to generation-recombination mechanisms in space-charge regions. The changes in slope can be represented by a multiplying factor, m ($1 \leq m \leq 4$). Thus the combined voltage for a real diode equation would be:

$$V = m \frac{kT}{q} (2.3) \log (I/I_0) + IR_B.$$

Since both the magnitude of m and the value of voltage at which the slope changes are functions of the individual diode (within a family), general purpose diodes provide a one or two-decade dynamic range at best. A better alterna-



1. The ideal diode log circuit delivers an output voltage proportional to the log of the input current divided by a reference current.

Dan Sheingold, Technical Information Manager, and **Fred Pouliot**, Product Manager, Analog Modules, Analog Devices, Route 1 Industrial Park, Norwood, Mass. 02062.

tive is to use dual matched transistors, connected as diodes.

Using the transdiode connection

If a transistor is connected to feed back around an op amp (Fig. 2) the collector current is determined by the input current or voltage. Ideally the op amp will maintain the collector voltage equal to the input current and will hold the collector voltage at zero. Since the base is grounded, the collector and base are at the same potential, even though the base current flows independently. The amplifier output voltage—which is also the emitter-to-base voltage—must meet the collector restraints, while furnishing any needed emitter current.

To investigate the relationship that controls the circuit of Fig. 2, use the modified Ebers and Moll equations¹ for emitter and collector currents of a grounded-base bipolar transistor:

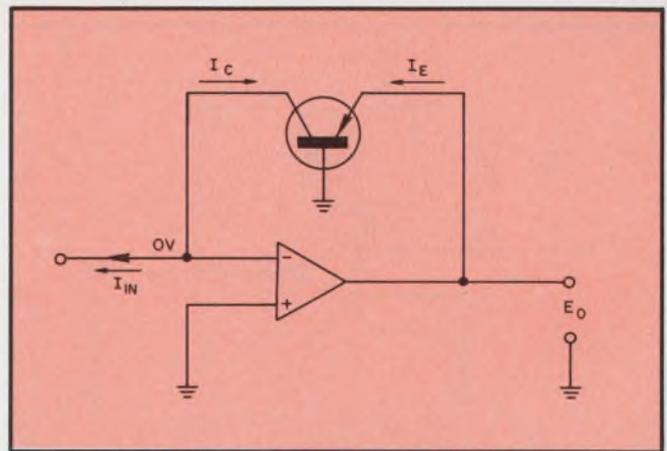
$$I_E = I_{ES} \left(e^{\frac{qV_E}{kT}} - 1 \right) - \alpha_i I_{CS} \left(e^{\frac{qV_C}{kT}} - 1 \right) + \sum I_{ES_j} \left(e^{\frac{qV_E}{m_j kT}} - 1 \right)$$

$$I_C = -\alpha_N I_{ES} \left(e^{\frac{qV_E}{kT}} - 1 \right) + I_{CS} \left(e^{\frac{qV_C}{kT}} - 1 \right) + \sum I_{CS_j} \left(e^{\frac{qV_C}{m_j kT}} - 1 \right)$$

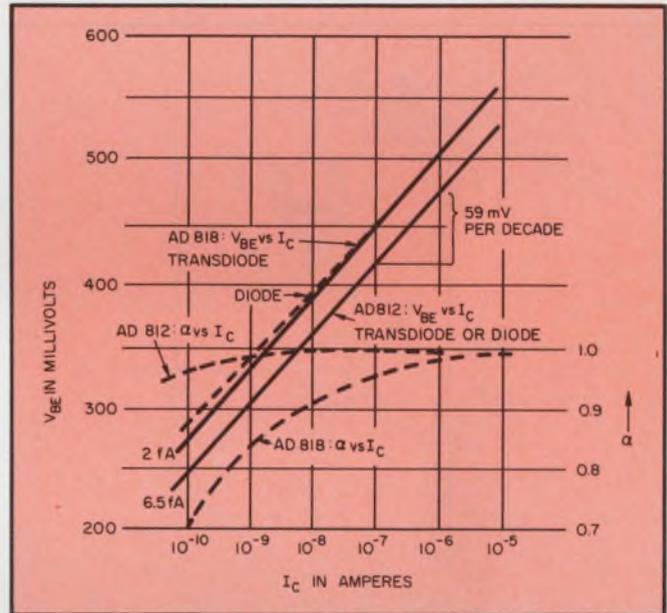
Here V_E and V_C are the emitter-base and collector-base voltages; I_{ES} and I_{CS} are the emitter and collector saturation currents; α_N and α_i are the current-transfer ratios in the normal and reverse directions, and $m_i > 1$ and $m_j > 1$ are "un-collected" current components that flow through the base circuit. Since V_C is held at zero for Fig. 2 the relationship between I_C and V_E becomes

$$I_C = \alpha_N I_{ES} \left(e^{qV_E/kT} - 1 \right).$$

But the op amp holds I_C equal and opposite to the



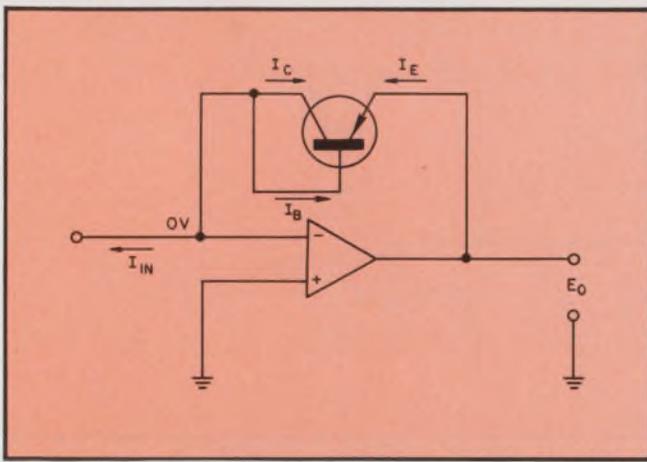
2. The transdiode connection grounds the base of the feedback transistor (pnp shown here).



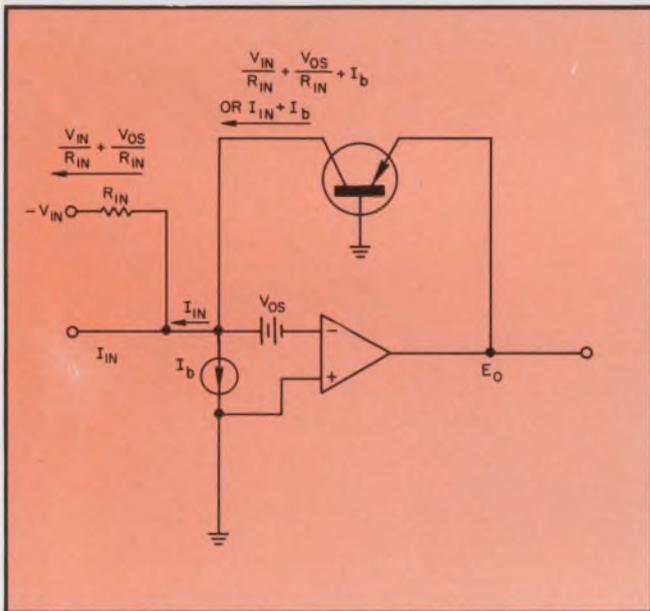
3. Some matched transistor pairs used as transdiodes and diodes are compared for α vs I_C and V_{be} vs I_C .

Table 1. Comparison of several log module types

Log module	Description of contents and applications	Advantages	Disadvantages
Basic log element	Two matched log transistors scaling and temperature compensating resistors For special-purpose log designs	Lowest cost, greatest flexibility	Most complex to apply, requires at least two external op amps plus dynamic stabilization in conventional log application
Log transconductor	Basic log element, has reference-current source to optimize operation at low levels	Best performance obtainable through op amp choice	Requires external op amp, gain trim, I_{REF} trim
Log amplifier	Log transconductor FET-input op amp The initial choice of all fixed-reference log applications	Easiest to apply, meets specs with no trimming or external components Best performance over a wide range	Op amp is optimized for most (but not all) applications



4. The 2-terminal diode-connected transistor can handle either polarity of input current.



5. When the circuit of Fig. 4 is modified to show the op amp error sources, its performance becomes more complex.

input current, so V_E must be

$$V_E = \frac{kT}{q} (2.3) \left[\log \frac{I_{IN}}{I_{ES}} - \log \alpha_N \right] \text{ for } \frac{I_{IN}}{I_{ES}} \gg 1.$$

For silicon-planar transistors, I_{ES} is typically 10^{-13} A or less. Therefore the V_E relationship in the previous equation is valid over a wide current range. The current transfer ratio α_N is nearly unity; thus $\log \alpha_N$ becomes negligible. (If $\alpha_N = 0.99$, its error contribution would be about 0.25 mV of constant offset.) Fig. 3 shows plots of V_{BE} and the grounded-base current gain, $\alpha(I_C/I_E)$, for two matched-transistor types designed for logarithmic circuits.

If the transistor's base and collector are physically shorted together (Fig. 4), the result is a two-terminal diode that conforms to the first of the two Ebers and Moll equations. In this equa-

Table 2. Values of error, as a function of h_{FE} , increase as h_{FE} decreases

h_{FE} ($\alpha_N \approx 1$)	α/α_N	$\frac{-kT}{q} \ln(\alpha/\alpha_N)$ mV at 25 C
∞	1	0
1000	0.999	0.03
200	0.995	0.13
100	0.99	0.26
50	0.98	0.51
19	0.95	1.32
11.5	0.92	2.14
9	0.9	2.7
4	0.8	5.7
3	0.75	7.4
1	0.5	17.8

tion the first term almost equals the collector current; the second term is zero, and the sum of the $m_i > 1$ terms thus equals the base current. Since the relationship, $I_{IN} = -(I_C + I_B)$, holds for any transistor, I_B can be replaced by I_C/h_{FE} and I_{IN} then becomes

$$I_C = -I_{IN} \left(1 + \frac{1}{h_{FE}} \right) = \alpha_N I_{ES} (e^{qV_E/kT} - 1) \left(1 + \frac{1}{h_{FE}} \right).$$

When this equation is solved for V_E (using natural logs) we get:

$$V_E = \frac{kT}{q} \ln(I_{IN}/I_{ES}) - \frac{kT}{q} \ln \left[\alpha_N \left(1 + \frac{1}{h_{FE}} \right) \right].$$

The term $1/h_{FE}$ can also be equated to $(1 - \alpha)/\alpha$, and if this form is substituted into the error term, the net result makes V_E equal to

$$V_E = \frac{kT}{q} \ln(I_{IN}/I_{ES}) + \frac{kT}{q} \ln \frac{\alpha}{\alpha_N}.$$

This result is shown in Table 2.

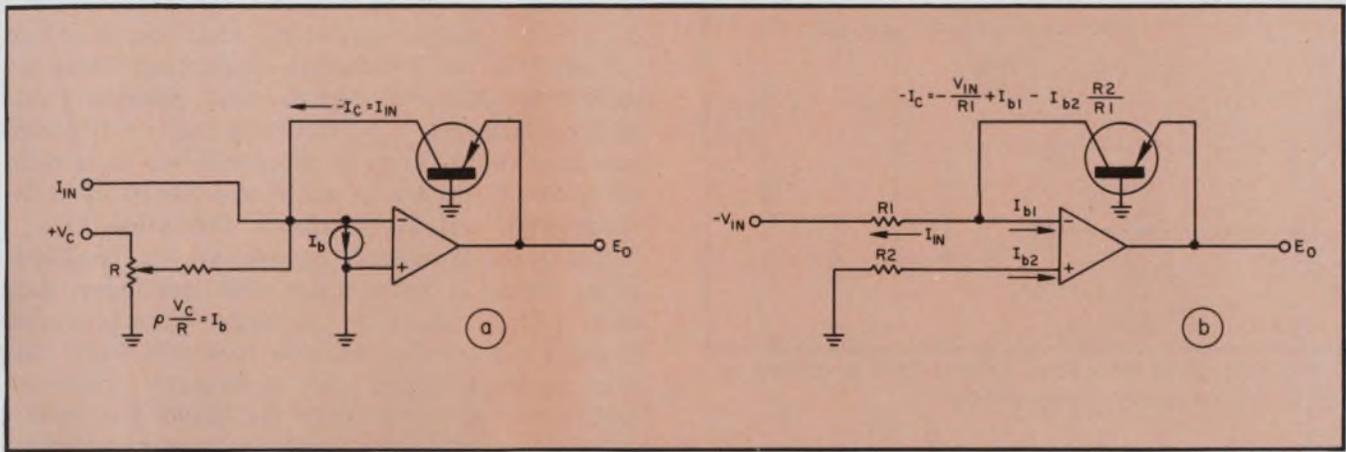
From Table 2 it should be clear that any transistor used as a two-terminal log diode requires that the h_{FE} be high and that it be maintained over a wide range of input current.

Other error sources compound the problem

If $V_{CB} \neq 0$, the terms in the second of the Ebers and Moll equations will contribute error currents that can significantly affect V_E , especially for low values of input current. In the forward conduction region

$$V_E = \frac{kT}{q} \ln \left[\frac{I_{IN}}{\alpha_N I_{ES}} + \frac{I_{CS}}{\alpha_N I_{ES}} (e^{qV_{CB}/kT} - 1) + \Sigma \dots \right].$$

For grounded-base circuits, the amplifier offset voltage, V_{OS} , will bias the collector, as any common-mode input voltage will do. And when the base is driven, the designer must ensure that the expected swing of V_{CB} is compatible with the



6. To compensate for the error current I_b , (a) a compensating current, $I_c = PV_C/R = I_b$ is added. Symmetry can

also be used (b) to null out the effects of I_b , both initially and with temperature.

desired low-current range.

Amplifier bias current, I_b , causes linearity errors that appear at the output as log-conformity errors. Offset voltage, V_{OS} , also causes an error current in the feedback path that is a function of the input resistance V_{OS}/R_{IN} . This current has the same effect as bias-current error (Fig. 5). There are several ways to reduce errors caused by bias current. Aside from the most obvious and expensive route (use of an amplifier with the necessary performance), Fig. 6 shows ways to null the effects of I_b by modifying the circuitry. In Fig. 6b a compensating resistor, in series with the positive input, provides bias-current compensation. If the amplifier input currents track one another

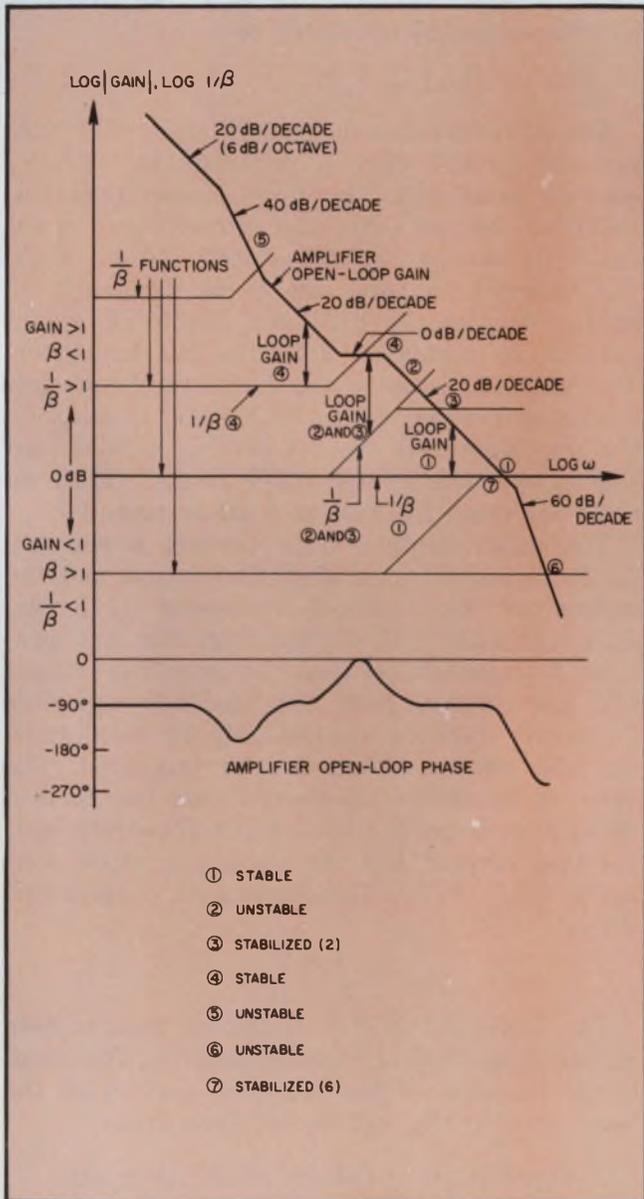
$$-I_c = I_{IN} - I_{b1} + I_{b2}(R_2/R_1).$$

And, for example, with $I_{b1} = I_{b2}$ and $R_1 = R_2$, then $-I_c = I_{IN}$. Thus $R_2 I_{b2}$ should be small enough to avoid significant errors due to V_C .

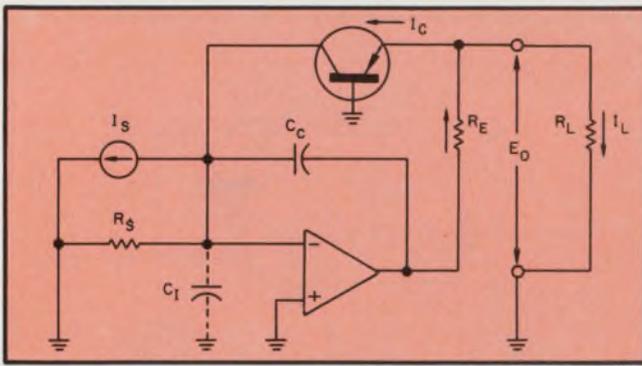
When the amplifier is zeroed at one temperature, current errors due to V_{OS} are temporarily reduced. Since I_{ES} could be 10^{-14} A or less, it is important to select the op amp with care and to minimize summing-point leakage current from all sources. Besides amplifier problems, there are also device problems. The temperature dependence of I_{ES} (doubling for every 10-C increase) and of the ratio kT/q (0.33%/°C at 27 C) total about 2 mV/°C—an intolerable change for accurate log circuits. As we shall see this problem can be circumvented by adding additional components.

Log amps also have stability problems

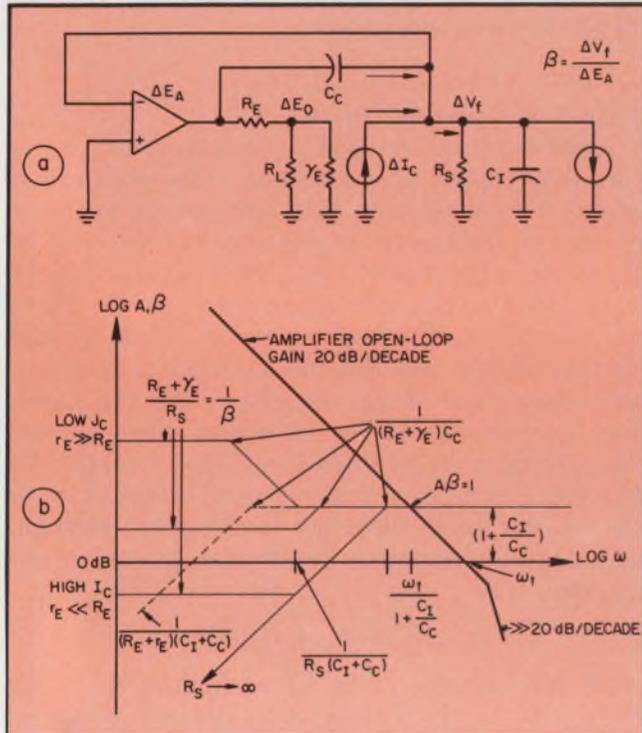
A necessary condition for stability of op-amp circuits is that the phase shift around the feedback loop be less than 180° at the frequency where the loop gain, $A\beta$, drops through unity. The hypothetical Bode plot of Fig. 7 corresponds



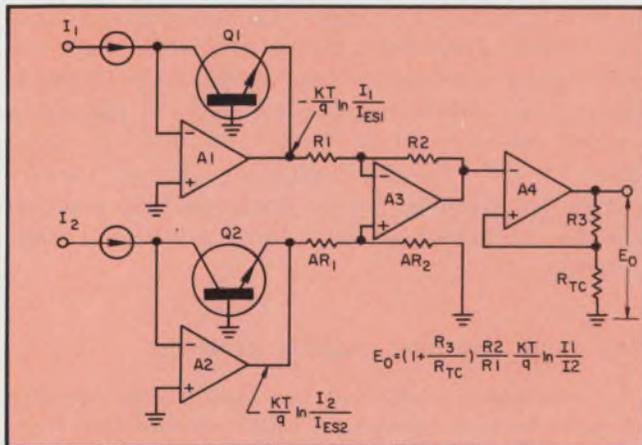
7. The Bode plot for stability analysis shows stable and unstable loop gain ($A\beta$) situations.



8. The transdiode circuit can be stabilized by adding R_E and C_C for frequency compensation.



9. The stability model for the circuit of Fig. 8 (a) can be used along with the Bode plot (b) to do a stability analysis of the transdiode circuit.



10. Amplifier A3, used as a subtractor of logarithms to perform a log-ratio calculation, has compensation for both I_{ES} and KT/q variations.

to a circuit with minimum-phase (RC) networks—for which A and β have slopes that should differ by less than 40 dB/decade when they cross at unity-loop gain. In circuits with passive feedback components, $1/\beta$ (feedback factor) is never less than unity. Thus if the amplifier gain rolls off at 20 dB/decade to unity, the circuit must be stable with resistive feedback (situation 1).

But in the transdiode connection, the feedback path, which is both active and nonlinear, can have voltage gain at the upper input-current levels. Even purely resistive feedback won't ensure stability. Thus the unity-gain crossover could occur at a frequency for which the amplifier gain is well under unity and accompanied by a large phase shift (situation 6). Also, since the gain is a function of signal level, a choice must sometimes be made between stability at high levels and bandwidth at low levels.

For small changes in the emitter current of the feedback transistor, the effective feedback admittance can be calculated by

$$\frac{dI_C}{dV_E} = \frac{q}{kT} I_C = \frac{I_C}{0.026} = \frac{1}{r_E}$$

But r_E covers a wide range: at $I_C = 1$ mA, $r_E = 26 \Omega$; and when I_C decreases to 1 nA, r_E goes up to 26 M Ω . Therefore conventional stabilization methods—like the connection of a capacitor across the feedback element—won't work. For example, to force the break frequency to be 1.6 MHz at the high end, 0.039 μ F would have to be paralleled with the log transistor. This large capacitance also forces the break frequency at the low end to be 1.6 Hz. In addition the amp may have trouble driving a 26- Ω load—even over the limited 0.6-V range. (Most op amps are rated for load of 1 k Ω or more.)

The usual solution is to connect a resistor, R_E , in series with the amplifier output and the emitter of the feedback transistor (Fig. 8). This connection unloads the amplifier and provides attenuation between the amplifier output and the emitter. Now the feedback capacitor C_C can be reduced considerably in magnitude, and the response time can be improved. The value of R_E can be calculated, since the current through it is equal to the emitter current plus the load current and the maximum diode voltage is about 0.7 V. Then, for a 10 V amplifier, we get

$$R_E = \frac{9.3 \text{ V}}{I_C + I_L}$$

The Bode plot of Fig. 9 can be used to help calculate the feedback capacitance, C_C . The small signal response of the feedback portion of the loop, $\beta = \Delta V_F / \Delta E_A$, can be obtained from

$$\frac{\Delta V_F}{R_S} (1 + R_S C_{IP}) = (\Delta E_A - \Delta V_F) C_{CP} + \Delta I_C,$$

$$\text{where } \Delta I_C = \frac{\Delta E_0}{r_E} = \frac{\Delta E_A}{R_E + r_E}$$

If this equation is solved for β ,

$$\beta = \frac{\Delta V_F}{\Delta E_A} = \frac{R_S}{R_E + r_E} \left[\frac{1 + (R_E + r_E) C_c p}{1 + R_S (C_I + C_C) p} \right]$$

Now approximations can be made. If the input is a current source ($R_S \rightarrow \infty$) and the frequencies are high ($p \rightarrow j\omega \gg 2\pi f_t$), β becomes $C_c / (C_I + C_C)$. At low frequencies and a voltage-source input, β becomes $R_S / (R_E + r_E)$. Since r_E is inversely proportional to I_C , the time constants that contain r_E will be proportional to r_E for low values of I_C and constant ($\approx R_E$) for high values of I_C .

To achieve small-signal stability, the numerator break frequency, $\omega_c = 1 / (R_E + r_E) C_c$, should be at least one octave less than the frequency at which $1/\beta = 1 + C_I/C_C$ crosses the amplifier's open-loop gain plot at the highest value of I_C .

For example, if $R_E = 2.2 \text{ k}\Omega$, $\omega_t = 10^7 \text{ rad}$, $C_I = 10 \text{ pF}$ and r_E at $1 \text{ mA} = 26 \Omega$, then

$$\frac{1}{2200 C_c} = \frac{1}{2} \cdot \frac{\omega_t}{1 + C_I/C_C}$$

When this equation is solved for C_c , we get $C_c = 88 \text{ pF}$; therefore a 100 pF standard value would be reasonable.

Making the circuits work

The temperature sensitivity of the circuits mentioned earlier gives them very limited practical value. In addition the output depends upon the value of αI_{ES} (reference current), which differs from device to device.

If two similar transistors are matched for V_{BE} at constant collector current and temperature, the ratio of the αI_{ES} terms would be almost constant over a wide temperature range. Compensation by use of matched pairs results in the following mathematical simplification: If $\frac{\alpha I_{ES2}}{\alpha I_{ES1}}$

is approximately unity, then

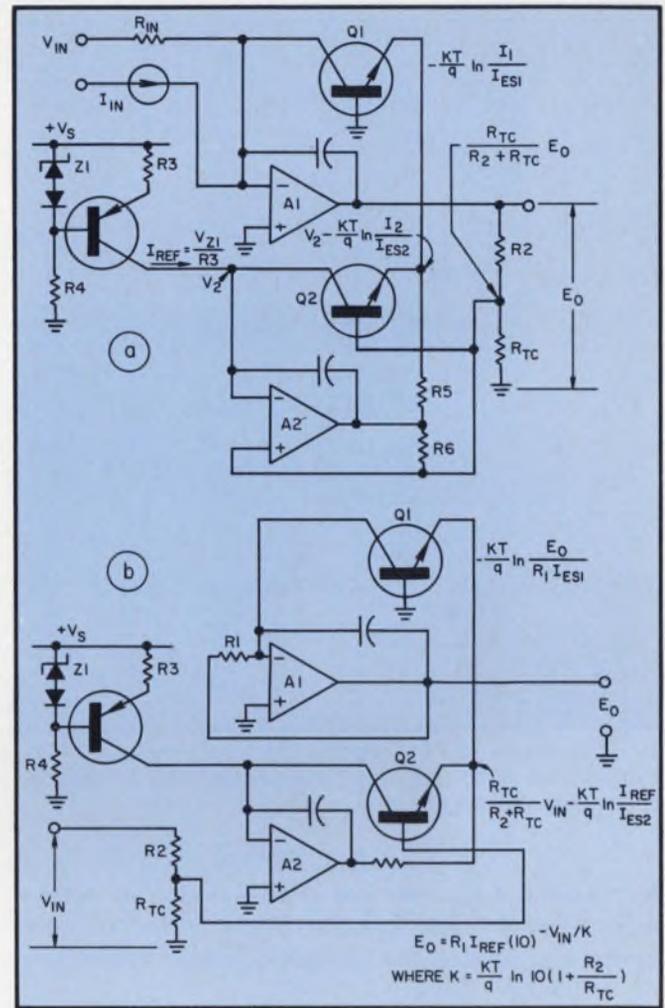
$$E_{IN} = \frac{kT}{q} \left[\ln \left(\frac{I_1}{I_{ES1}} \right) - \ln \left(\frac{I_2}{I_{ES2}} \right) \right] \quad (1)$$

$$= \frac{kT}{q} \ln \frac{I_1}{I_2} \quad (2)$$

If the subtraction operation of Eq. 1 is carried out with use of circuit of Fig. 10, the reference current is I_2 (zero output voltage when $I_1 = I_2$), and the output voltage becomes proportional to the resistance ratios that determine the gain of amplifiers A_3 and A_1 , allowing arbitrary scale factors (e.g., 1 V/decade).

Another possible subtraction method is shown in Fig. 11a. Fig. 11b shows the antilog connection for the two log circuits and the current source.

Performance of these circuits is practically independent of I_{ES} and temperature. For a single input, I_1 , the reference current, I_2 , can be set to normalize I_1 . And since kT/q is not usually con-



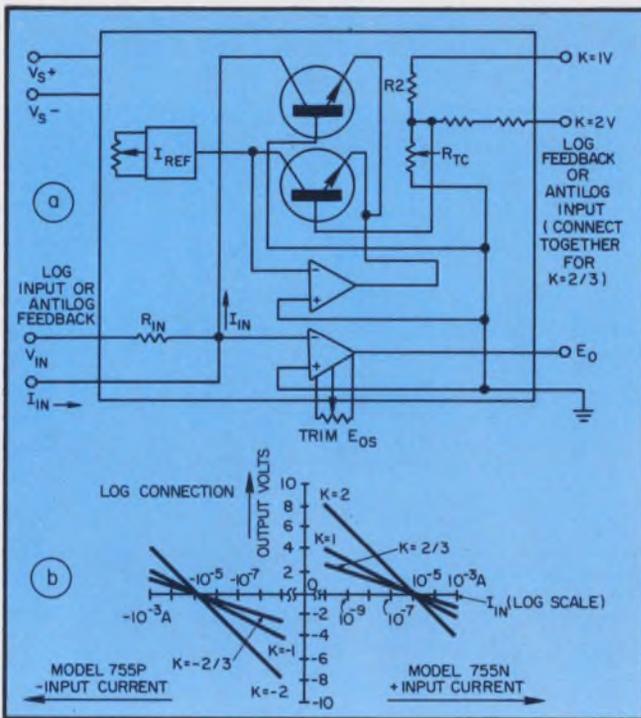
11. By using a controlled current reference, the temperature-compensated log circuit performs ratio calculations referred to I_{REF} (a). When some of the leads are reconnected as shown here the log circuit produces an antilog output (b).

sidered a convenient value of voltage with which to work, R_2/R_1 can be scaled to provide an appropriate value of gain.

For example, if a scale factor of 1 V per decade is desired, $E_0 = K \log_{10} (I_1/I_2)$, and K must equal 1 . For $K = 1$, R_2/R_1 must equal $q / (k \cdot T \cdot \ln 10)$, or 16.9 at 300 K . If the temperature sensitivity of this circuit is too great ($0.33\% / ^\circ\text{C}$) for the desired stability and range of temperature variation, a gain stage can be added with an equal but opposite temperature coefficient.

The circuit of Fig. 10 uses resistor R_{TC} for compensation. The resistor is chosen so that the gain equation of A_1 becomes $G = 1 + R_3/R_{TC}$ and has a $-0.33\% / ^\circ\text{C}$ sensitivity. Fig. 11a incorporates a fixed-current reference whose current is set by V_{Z1}/R_3 . Resistor R_6 allows the high end of the dynamic range to be extended through 1 mA —its negative-resistance effect tends to cancel the voltage drop of the bulk resistance of Q_1 .

In the antilog circuit, the output voltage, E_0 , has an exponential relationship:



12. The Model 755 log module (a) from Analog Devices can perform either log or antilog calculations. Voltage vs current curves appear in b.

$$E_o = -E_{REF} 10^{-V_{IN}/K}$$

If transistor Q_2 operates with a value of reference current large enough to ensure logarithmic operation, unaffected by base-collector variations of ± 600 mV, then

$$\frac{-kT}{q} \ln \left(\frac{E_o}{R_1 \alpha I_{ES1}} \right) = \frac{R_{TC}}{R_2 + R_{TC}} V_{IN} - \frac{kT}{q} \ln \frac{I_{REF}}{\alpha I_{ES2}}$$

and, when terms are rearranged,

$$\frac{q}{kT} \left(\frac{R_{TC}}{R_2 + R_{TC}} \right) V_{IN} = -\ln \left(\frac{E_o}{R_1 I_{REF}} \cdot \frac{\alpha I_{ES2}}{\alpha I_{ES1}} \right) \quad (3)$$

If the previous assumption is used, $\alpha I_{ES2} \approx \alpha I_{ES1}$, and Eq. 3 is changed back to exponential form,

$$E_o = R_1 I_{REF} \left[\text{Exp} \left(\frac{-q}{kT} \cdot \frac{R_{TC}}{R_2 + R_{TC}} \cdot V_{IN} \right) \right] \quad (4)$$

In the antilog connection, the same error sources are present; but some of them now appear in the exponent and others that were in the exponent have been repositioned as constant multipliers.

Dynamic errors, such as speed and frequency response, depend upon scaling, signal level and direction of change. Above currents of around $1 \mu\text{A}$, the response is dominated by the integrator time constant, changing little with signal level. Below about $1 \mu\text{A}$, $r_e C_c$ dominates the response; thus speed is reduced in proportion to the input current. A typical log amp might have

the following response times:

I_{IN} (increasing)	time
1 to 10 nA	1 ms
10 to 100 nA	100 μs
100 nA to 1 μA	7 μs
1 μA to 1 mA	4 μs
I_{IN} (decreasing)	time
10 to 1 nA	4.5 ms
100 to 10 nA	400 μs
1 μA to 100 nA	30 μs
1 mA to 1 μA	7 μs

The frequency response of log amps is measured at low-signal levels (3% to 10% of the average input level) to reduce distortion caused by log compression. Typical response figures might read as follows:

I_{IN}	-3 dB frequency
1 nA	80 Hz
1 μA	10 kHz
10 μA	40 kHz
1 mA	100 kHz

Designing with log amps

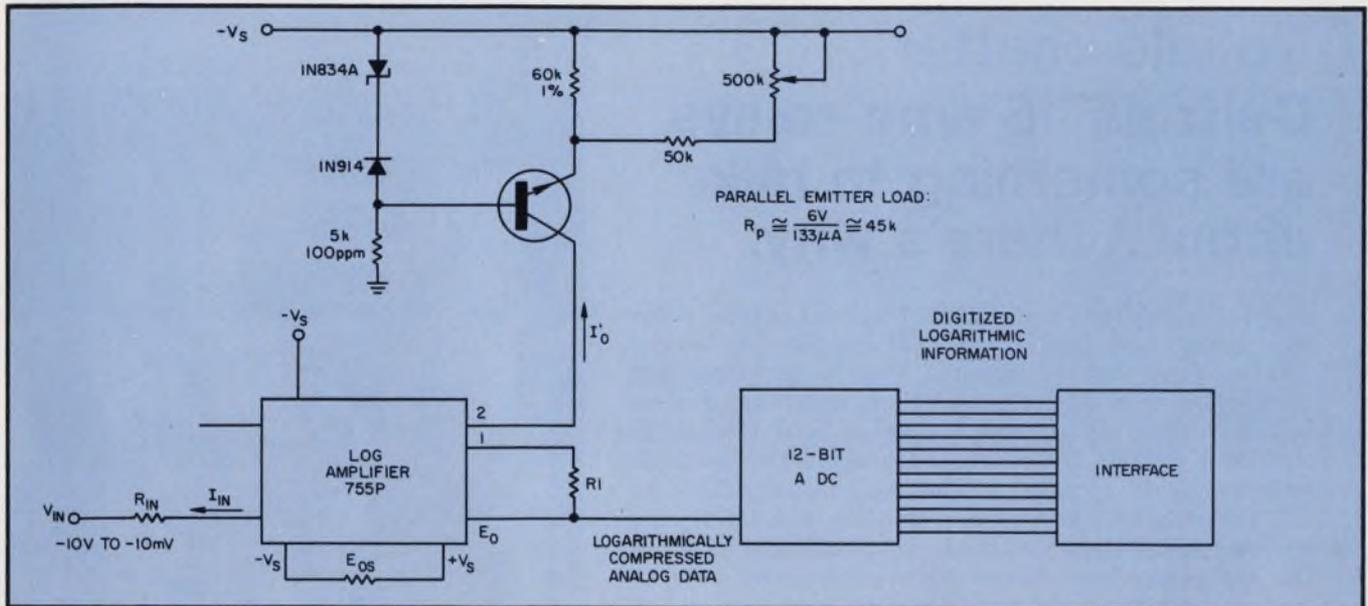
Log circuits can be applied easily to data collection and compression. For example, if a signal is introduced into a computer system or data link and it is desired to keep signal accuracy to within 1% throughout its entire range a circuit that responds to the log of the input can be used.

The standard linear approach would be to select an analog-to-digital converter with sufficient resolution to meet the accuracy requirement. If the input range is -1 to -10 V, the dynamic range would be from -0.01 V (i.e. 1% of 1 V) to -10 V, or about 1000:1. To obtain this resolution, a 10-bit converter could be used ($2^{10} = 1024$), and one least-significant bit would then represent 1% of the smallest signal. If the range is increased to -10 mV to -10 V, the converter would require a resolution of 0.1 mV to -10 V, or 1:100,000. In this case a 16-bit converter would barely be sufficient ($2^{16} = 65,536$).

An alternative approach uses a log-conversion circuit for signal compression over a three-decade range and a 12-bit a/d converter. The log circuit for this application is shown in Fig. 13a. To convert the log output to a unipolar signal, a current source can be used to shift the reference point to one end of the range. Resistor R_1 , added in series with the $K = 1$ output, adjusts the scale-factor setting. To provide a realistic design example, the Analog Devices 755 series of log amplifiers is used (Fig. 12).

The first step in the design is to select the proper polarity amplifier. If we assume the input ranges from -10 V to -10 mV, the "P" version of the 755 (for negative inputs) is required.

After selection of the log amp, the region of



13. A data compression system can be built with log amps. These amplifiers can reduce a wide ranging ana-

log signal to a more restricted range with no loss in dynamic range or increase in distortion.

best log conformity should be chosen for operation. For the 755P, the best log conformity is 0.5%—over 10 nA to 100 μ A. Resistor R_{IN} , used at the current input, determines the highest current needed at the highest input voltage magnitude:

$$R_{IN} = 10 \text{ V} / 100 \mu\text{A} = 100 \text{ k}\Omega$$

To find K , the input requirements of the following stage must be examined. If the a/d converter input covers a range from 0 to +5 V, K can be calculated as follows: The total output voltage is 5 V, and the input spans three decades. Thus $K = 5 \text{ V} / 3 = 1.67 \text{ V}$. From the data sheet for the log amplifier selected, a value of 15 k Ω is given for the input resistance of the 1 V per decade terminal. The total resistance then required is

$$R_t = (5/3) (15 \text{ k}\Omega) = 25 \text{ k}\Omega.$$

Thus a 10-k Ω resistor in series with the $K = -1$ terminal will provide a nominally correct scale factor. To allow for tolerances of the internal resistor, use a 10-k Ω , 10-turn, pot in series with a 5-k Ω resistor as R_1 .

To produce a zero output from the amplifier at one end of the range, I_{REF} should be adjusted to match I_{IN} . The curves for the 755P (Fig. 12b) indicate that a -2 V output would result if 100 nA is the input (with $K = -1 \text{ V}$). Since this is the current at which zero output is desired, the current I_o injected into the unused scale factor terminal must shift the output in the positive direction. To do this, the current input must be derived from a negative voltage reference. Calculate the input current from the total resistance connected to the scale-factor terminal, the output and the amount of voltage the output is to be shifted for $K = 1 \text{ V}$:

$$I = 2K/R_T = (2) (5/3) / 25 \text{ k}\Omega = 133 \mu\text{A}$$

A resistor to the negative supply (15 V/133 μ A = 30 k Ω) can be used to obtain this current. But shifts in the offset voltage at the dummy summing junction caused by the 60 mV/decade response to the input can cause noticeable errors. For example, if I_{REF} is adjusted as indicated, a shift of 180 mV would occur as the input signal increases to 100 μ A (3 decades at 60 mV/decade), resulting in a shift of offset current of

$$(180 \text{ mV}) / 15 \text{ V} \times 100 = 1.2\%.$$

To avoid this problem, a fairly simple current source is used, as shown in Fig. 13.

The trimming procedure for the log circuit is as follows: First E_{OS} should be adjusted for zero output; this can be done by grounding the input voltage. The trim pots for I_{REF} and scale factor should be left in mid-range to reduce interaction. The E_{OS} trim would then be adjusted for

$$E_o = -K \log (10 \mu\text{V} / E_{REF}) = -5 \text{ V}.$$

Adjusting for any voltage between -5 V and -6 V will ensure that E_{OS} has been adjusted to within 10 μ V. This adjustment should be performed carefully, since the gain is quite high at the 2.5 to 10 μ V level (about 100,000), and the reading will be noisy.

Next, to adjust I_{REF} , set $V_{IN} = 10 \text{ mV}$ and trim I_{REF} to force the zero output. K is then easily adjusted by increasing the input signal to its full value of -10 V, and adjusting R_1 for 5 V output.

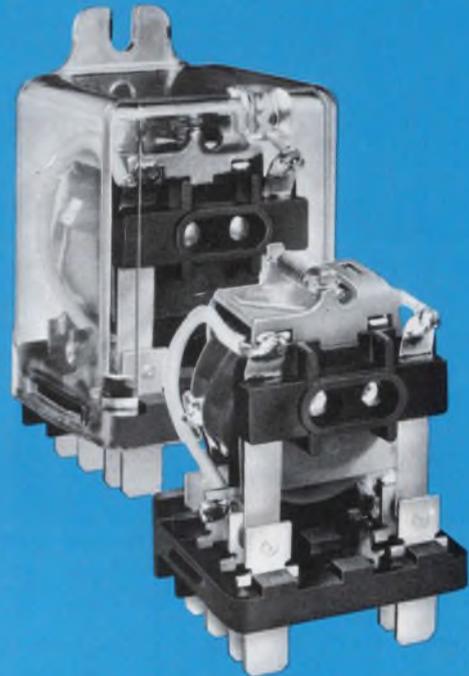
Some interaction between adjustments cannot be avoided, all trims should be repeated at least once in the same order as initially performed. ■■

Reference

1. Paterson, W. L., "Multiplication and Logarithmic Conversion by Operational-Amplifier-Transistor Circuits," *The Review of Scientific Instruments*, 34-12, December, 1963.

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	KB-6402	Digit	4	Invert	
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	KH-6288	Segment	8	Invert	
	KH-6800	Digit	6	Invert	
	KH-6811	Digit	9	Invert	
	KH-6813	Digit	6	Convert	
FLUORESCENT TUBE DRIVER	KM-6608	Segment & Digit	4	Convert	: Direct connection possible to LSI. : High performance, high reliability. : High withstanding voltage-low power consumption.
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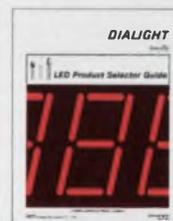
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Which IC timer to buy?

To choose from among single and dual types, and now counter-timers, know the tradeoffs and spec limitations.

IC timers, though versatile, tend to be relatively simple circuits. But you may not find it so easy to pick the right one for your application.

For one thing, the choice is expanding rapidly, with alternate-sourcing of several models. For another, the total cost to the user isn't always obvious. IC timers generate precise timing pulses or time delays with just a few external components. But the cost of the components sometimes greatly exceeds that of the timer itself.

Other key considerations, as you check the specs and analyze the tradeoffs, include these:

- Timers list an impressive range of possible delays—from microseconds to hours—but not all timers can provide those delays and still maintain accuracy and stability.

- Newer counter timers can be cascaded to provide accurate delays of up to a year or more. However, acceptable stability may not be achievable without an external reference oscillator connected to the timer.

IC timers: A wide selection

As a start in making your choice, consider the types of timers that are available (Fig. 1). The first class to gain acceptance was the single-cycle, or "one-shot," circuit. This type provides time

Alan B. Grebene, Vice President of Engineering, Exar Integrated Systems, Inc., 750 Palomar Ave., Sunnyvale, Calif. 94086.

delays in the range of microseconds to minutes. Available "dual" versions of these timers contain two identical timer sections in the same IC package.

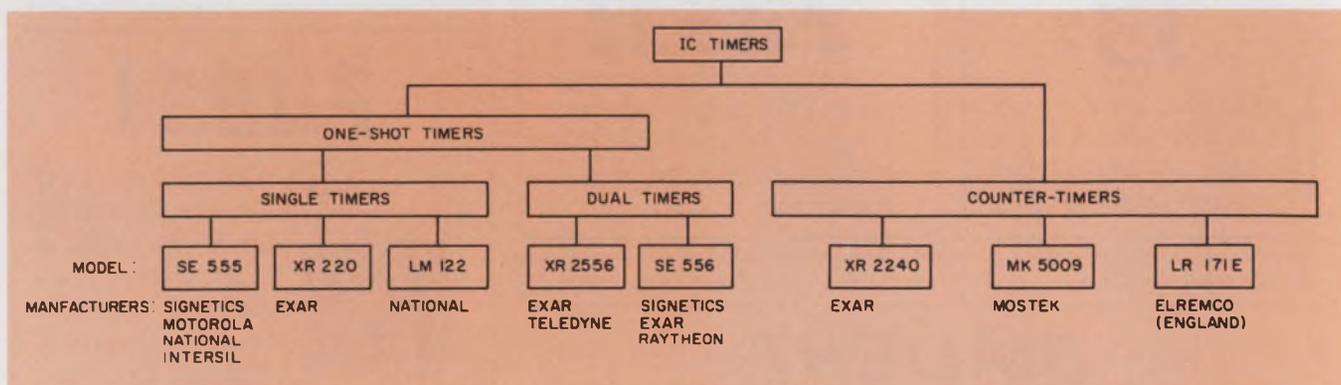
The basic one-shot IC timers have evolved into more complex counter-type timer ICs. These circuits contain a binary counter, in addition to a time-base oscillator, on a single chip.

The timing interval consists of a number of cycles of the internal time-base oscillator. And the over-all time delay results from a simple count down of the oscillator frequency. Hence time delays up to months or years are provided without the need for external large-value timing resistors or capacitors.

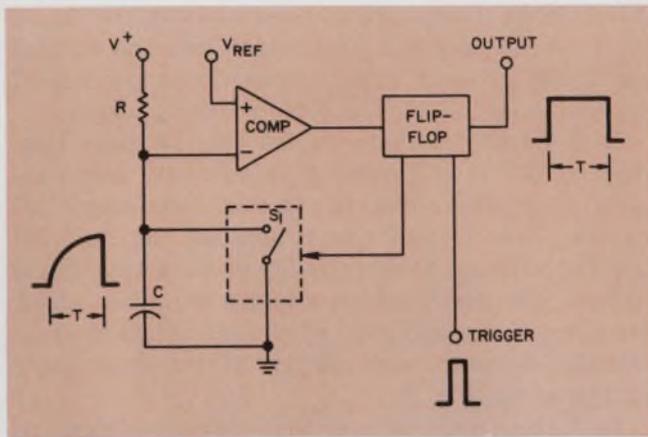
Timers contain simple circuitry

The single-cycle timers operate by charging an external capacitor through a resistor or a current source to generate a timing interval, T. This interval is proportional to the value of the external timing capacitor. Fig. 2 gives a simplified block diagram of such a timing circuit. Normally the internal switch S_1 is closed and the voltage across C is clamped to ground.

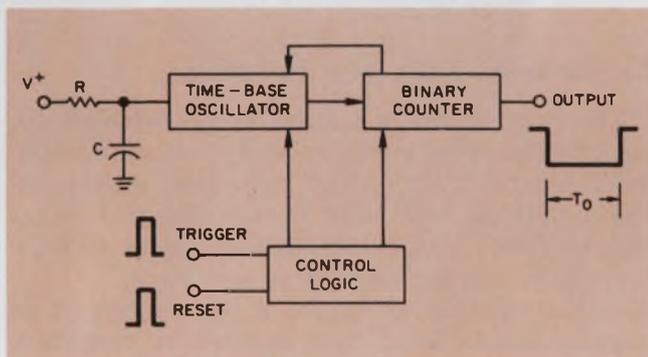
The timing cycle begins with the application of a trigger pulse to set the flip-flop and to open the switch S_1 across C. The voltage across C then increases exponentially with a time constant, RC. When this voltage reaches a threshold, V_{ref} , the voltage comparator changes state. This



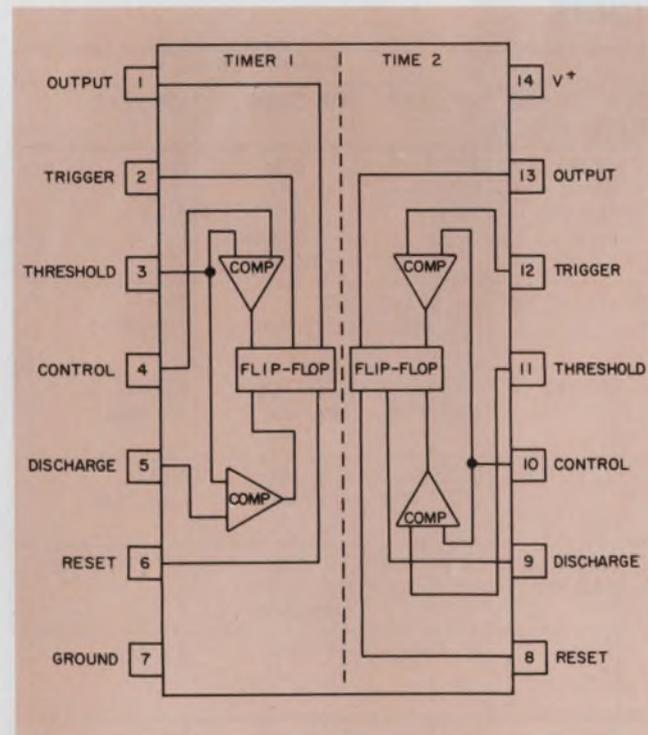
1. IC timers presently include several one-shots and counter-timers. More are expected to follow.



2. A basic single-cycle—or one-shot—IC timer generates a logic pulse whose duration is proportional to the external RC.



3. A counter-timer has a total timing interval that consists of multiple cycles of the time-base-oscillator period.



4. The XR-2556 dual-555 timer—in a 14-pin DIP—has a pinout with a symmetrical distribution of output and control terminals.

change resets the flip-flop, closes S₁, and ends the timing cycle. The output of the timer is a logic pulse of duration T, which is proportional to the external RC.

Counter-timers operate on a somewhat different principle. As shown in Fig. 3, they consist of three sections: (1) a stable time-base oscillator; (2) a binary counter, and (3) a control flip-flop. When the circuit is at rest, the time-base oscillator is off and the binary counter is reset to zero. An applied trigger pulse sets the control flip-flop and keys on the time-base oscillator to initiate the timing cycle.

The time-base oscillator generates precise timing pulses whose period, T, is proportional to the external RC time constant. The generated pulses are counted by the binary-counter section. When a preprogrammed count is reached, the circuit completes the timing cycle and resets itself.

The total timing duration, T₀, of the circuit equals NT, where T is the time-based period and N is an integer equal to the divide ratio of the binary counter. The total timing interval consists of multiple cycles of the time-base oscillator—hence the common reference to this kind of circuit as a “multiple-cycle” timer.

Three basic single-cycle versions

Three different ICs plus alternate-source versions fall into the category of single-cycle timers. These are the SE-555, introduced by Signetics, the XR-220, available from Exar, and the LM-122, from National Semiconductor. All of these circuits are extremely easy to use, requiring only an external RC network to set the timing interval.

Both the SE-555 and the LM-122 use the exponential-ramp principle already described and provide time delays of 1.1 RC and 1.0 RC, respectively. The XR-220 uses a constant-current source to charge the timing capacitor. The resulting time delay is 2.0 RC.

All three timer ICs can be used in a self-triggering mode as oscillators or clock generators. Typical applications include precision and sequential timing, pulse and clock generation, and pulse-width and pulse-position modulation.

For short-duration timing applications—up to several minutes—the three circuits have similar accuracy and stability characteristics. And they require similar values of external resistors and capacitors. A comparative listing of their electrical characteristics is given in the table.

Since each IC manufacturer specifies somewhat different test conditions for his circuit, the data in the table are intended only as a relative guideline for comparison of circuit performance. Here are some of the salient features and limitations

of the three IC timers:

- The SE-555 comes in an easy-to-use 8-pin package, has a high-current capability of 200 mA and offers an adjustable duty cycle. However, triggering and output levels are of single polarity.

- The XR-220 has multiple-polarity triggering and outputs, and it produces a linear ramp output. But it does not have a duty-cycle control.

- The LM-122 can operate up to 40 V, and has a multiple-polarity output that is also protected against short circuits. Hence it is more versatile than the SE-555. But the versatility may also make the 122 harder to use. And drive capabilities are limited to only 50 mA.

Dual timers simplify some uses

Monolithic dual-timer ICs contain two independent timing circuits in the same IC package. These ICs are particularly useful for those timing applications—such as sequential or delayed timing—that inherently require two or more timer circuits.

Presently two dual-timer ICs are available. These are the XR-2556 from Exar and Teledyne Semiconductor, and the SE-556 from Signetics, Exar and Raytheon Semiconductor. As shown in the table, both circuits have virtually identical electrical characteristics but different package pinouts. Both are designed as direct replacements for a pair of independent 555-type timers, and both designs have TTL-compatible outputs. The

XR-2556 dual-timer pinouts are shown in Fig. 4 for a 14-pin package. The output and the control terminals of each timer section are positioned symmetrically along the sides of the package.

In applications that require two or more timing circuits, dual timers offer cost and performance advantages over the use of two single IC timers. Lower costs result because the dual IC is often priced significantly lower than two single timers. The performance advantages come about from the close matching of the electrical characteristics between each section of the dual timer on the same chip.

In timing applications that require delays of several minutes, the conventional one-shot-type timers often require excessively large values of timing capacitance. And timing accuracy deteriorates due to the leakage currents associated with circuit components.

Counter-timers avoid large capacitors

The counter-timers eliminate this problem by use of a time-base oscillator and a binary counter on the same IC chip. The total timing cycle of the circuit depends only on the internal time-base oscillator, and it can be extended up to days or months without sacrifice of accuracy.

Another unique advantage of the counter-timer circuits results when two timers are cascaded. The total time delay associated with the system increases in geometric progression. For example,

Table. Comparison of available IC timers

	Single-cycle timers					Counter-timers		
	SE-555	XR-220	LM-122	XR-2556 (Dual 555)	SE-556 (Dual 555)	XR-2240	MK-5009	LR-171E
Supply voltage range	4.5 to 18 V	4.5 to 20 V	4.5 to 40 V	4.5 to 18 V	4.50 to 18 V	4 to 15 V	4.5 to 5.5 V, -9.6 to -14.4 V	6 to 45 V
Timing accuracy for given R,C (prime unit)	0.5% typ 2% max	0.5% typ 2% max	2% max	0.5% typ 2% max	1.5% typ	0.5% typ 2% max	Not specified	Not specified
Temperature stability ppm/°C (prime unit)	30 typ 100 max	100 typ 300 max	30 typ	30 typ 100 max	90 typ	30 typ 150 max	2000 typ No max	1500 typ No max
Power supply stability %/V (prime unit)	0.005 typ 0.02 max	0.07 typ 0.2 max	Internally regulated	0.005 typ 0.1 max	0.15 typ	0.07 typ 0.2 max	0.3 typ No max	Not specified
Maximum timing range. R = 10MΩ; C = 100 μF	1100 sec (18 min)	1000 sec (17 min)	1000 sec (17 min)	1100 sec (18 min)	1100 sec (18 min)	(256) (10 ³) sec 3 days	10 ⁵ sec R,C not specified	(5) (10 ⁶) sec
Programming capability for fixed R,C	None	None	None	None	None	256 steps	16 steps	8 steps
Package type	8-Pin DIP	14-Pin DIP	14-Pin DIP, or 10-Pin TO-5	14-pin DIP	14-pin DIP	16-pin DIP	16-Pin DIP	14-Pin DIP

if a counter-timer circuit produces time delays equal to, say, 2^8 cycles of the time-base oscillator, then a cascade of two such circuits would produce delays of $(2^8)^2$ or 2^{16} cycles of the time base.

In this manner, time delays of several months or years can be obtained readily from a single external RC network, without degrading the timing accuracy. But even in timing applications requiring delays of just a few minutes, counter-timers may be more economical to use than the one-shot types since the counter type requires a smaller and less expensive timing capacitor.

Another unique feature common to most counter-timers is their programming capability. A preset count in the binary divider determines the total timing cycle. As a result, the counter section can be programmed to generate various time delays from a single external RC setting.

The combination of a stable time base and a programmable binary counter on the same IC chip opens up a wide range of applications that reaches far beyond conventional timing functions. Some of these applications cover such diverse fields as a/d conversion, frequency synthesis and digital sample/hold.

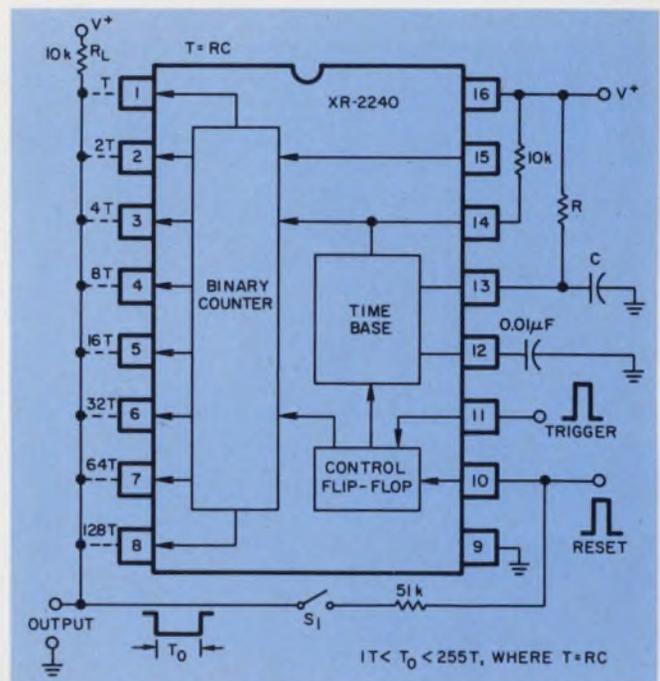
At present several counter-timer circuits are available, with more promised. The accompanying table provides a comparative listing of the electrical characteristics of available circuits.

The Exar XR-2240 contains a 555-style timer and an 8-bit programmable binary counter in a 16-pin, monolithic IC package. Each of the binary counter sections has a buffered open-collector output. The total time delay can be programmed from 1 RC to 255 RC if you simply connect the desired combination of counter outputs to a common-load resistor, as shown in Fig. 5. In addition to conventional timing applications with delays from microseconds up to five days, the circuit can be used with an external resistor ladder as a digital sample-hold or 8-bit a/d converter, as shown in Fig. 6.

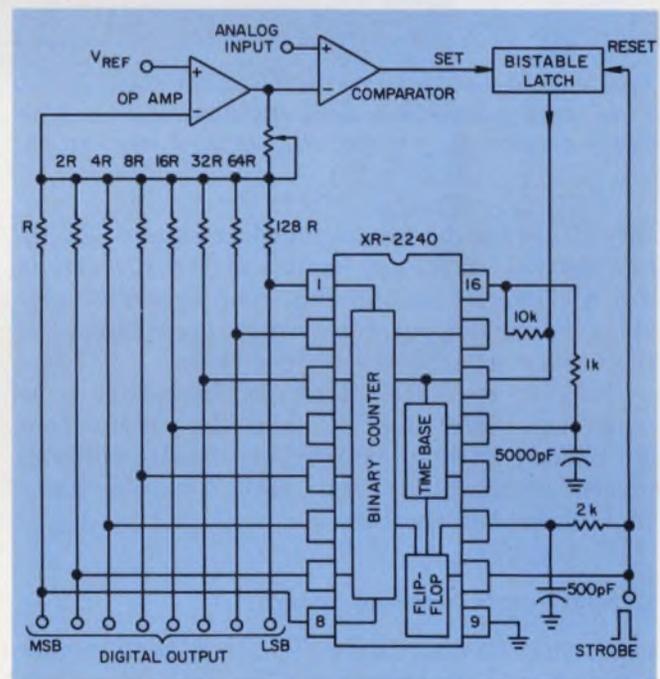
The major advantages of the XR-2240 include TTL-compatible outputs, a high accuracy of 0.5%, 256-step programming capability and a temperature stability of 50 ppm/°C. But the IC does not operate with an external crystal, and it has a relatively short divider chain—only up to a divide-by-256.

The Mostek MK-5009P, an MOS chip, contains an oscillator and frequency divider. A functional block diagram of the circuit appears in Fig. 7. The divider chain can be programmed in 16 discrete steps by the four address pins. The circuit can count down the local oscillator frequency by 36×10^8 and generate up to one hour of time delay from a 1-MHz crystal frequency reference.

Compared with other counter-timer circuits, the advantages of the MK-5009 include operation with an external crystal, 16-step programming



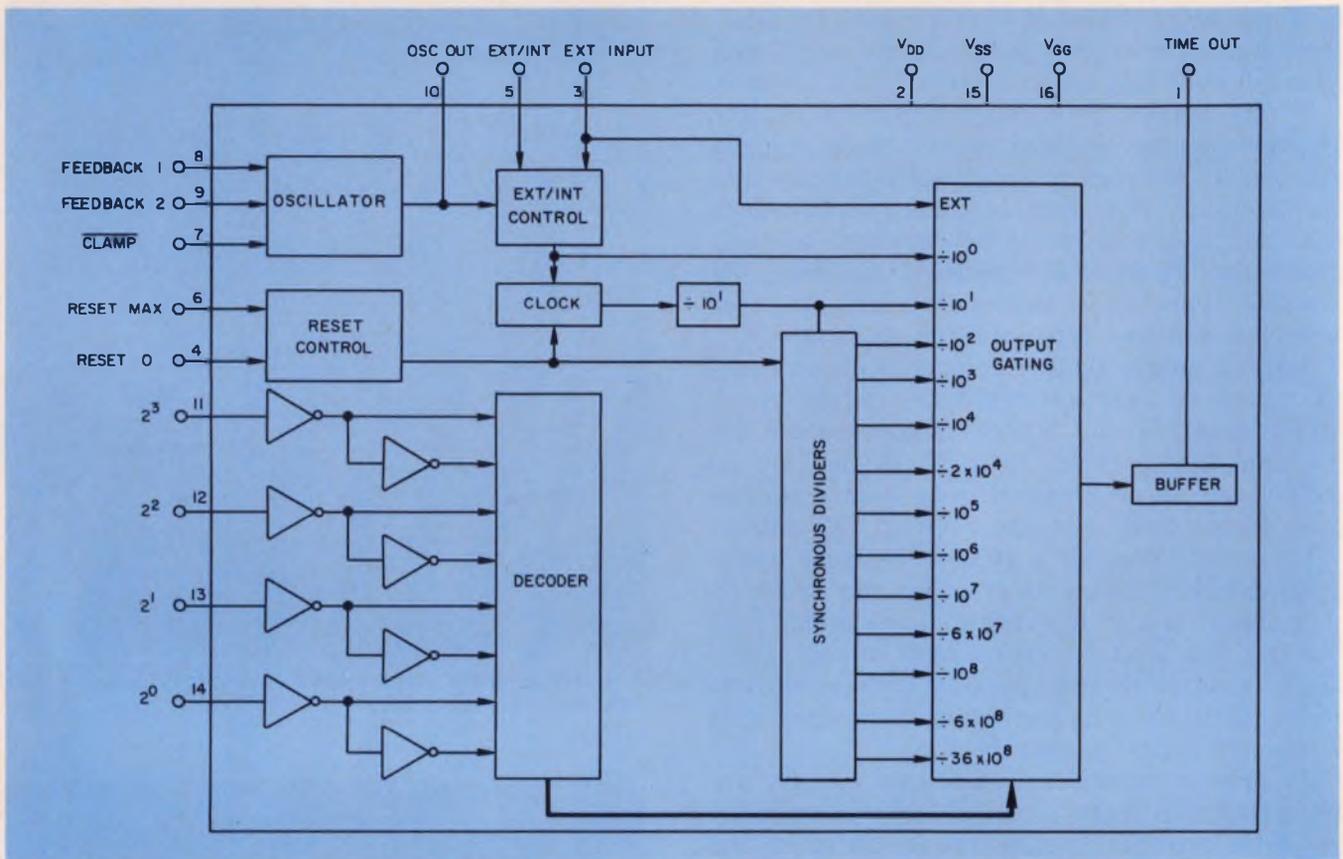
5. Counter-timers can be used as digitally programmed time-delay generators.



6. Even analog-to-digital converters can be built with counter-timer ICs.

capability and a long divider chain. And the timer gives seconds, minutes and hours of delay from a 1-MHz crystal. But the circuit requires split power supplies, and exhibits poor stability—up to 2000 ppm/°C—when an external RC network is used to set frequency.

The LR171E is manufactured by the Electronics Remote Control Company of England. This counter-timer contains a 12-bit binary counter and an RC oscillator in a 14-pin package. Total



7. An MOS counter-timer—the MK5009—can generate delays of seconds, minutes and hours. It uses an ex-

ternal 1-MHz crystal and has a 16-step programming capability. The IC can count down by 36×10^8 .

time delay can be programmed in eight steps up to 7500 RC. A unique feature of the LR171E is a d/a converter on the chip. The converter provides an analog-current output proportional to the binary count in the divider chain.

However the LR171E temperature drift is as much as $-1500 \text{ ppm}/^\circ\text{C}$, and the circuit does not operate with an external crystal. In addition, present availability of the LR171E counter-timer IC is limited in the U.S.

Consider costs and total delays

In applications with well-defined performance requirements, cost represents the main consideration when you choose an IC timer. But, remember, cost also includes the price of external components—the timing Rs and Cs to operate the circuit. In some applications—like those requiring fairly long time delays of a minute or so from one-shots—the cost of the external Rs and Cs easily exceeds the cost of the IC.

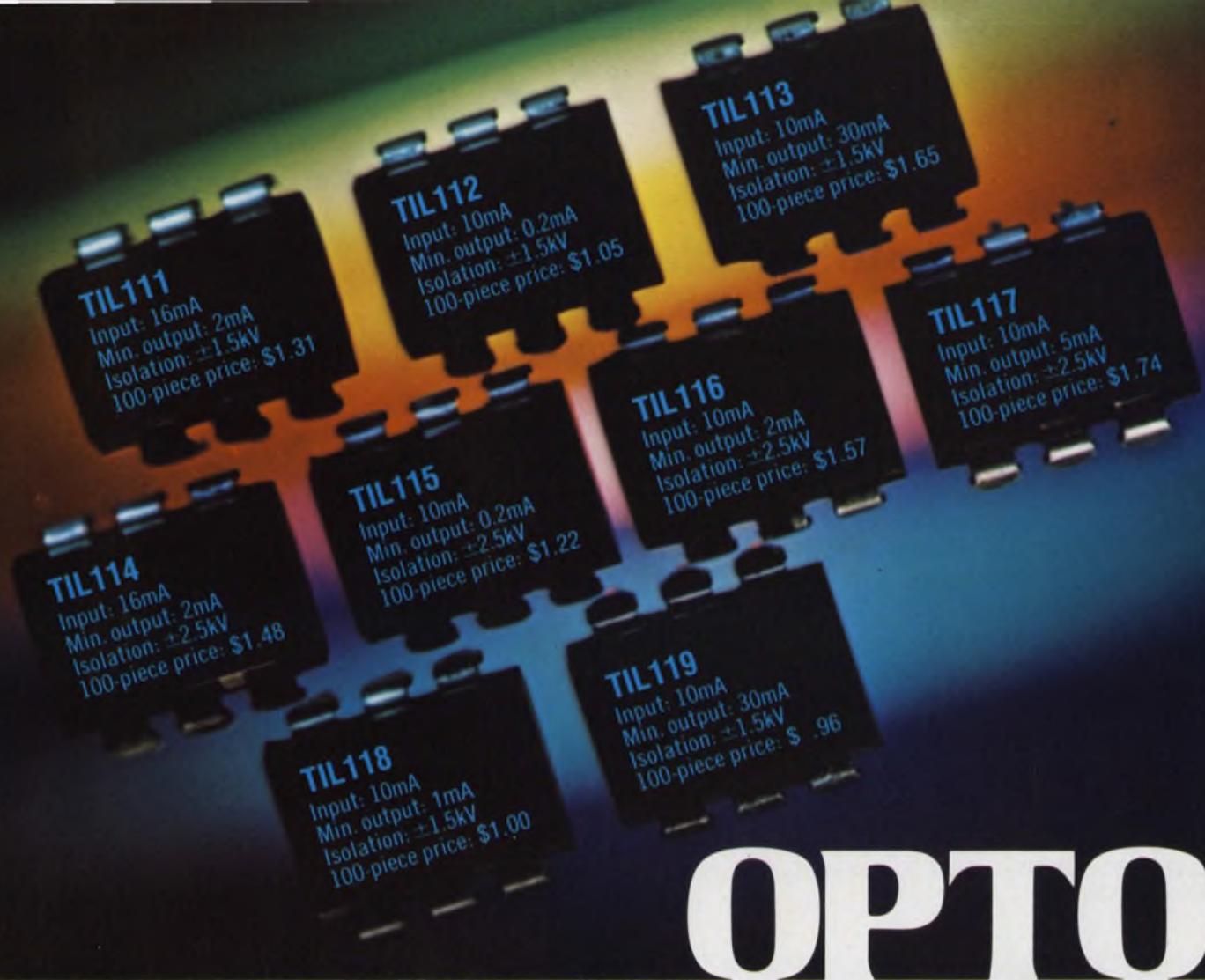
After cost, total time delay is the most important factor governing choice of the IC timer. In simple timing applications that require delays ranging from microseconds to seconds, the one-shot timers, such as the XR-220 or the SE-555, offer the most economical solution. For accurate

delays in the minutes or hours range, the counter-timers are by far the better choice.

The counter-timers are somewhat more complex, and are consequently more expensive than the one-shots. At present the commercial-grade one-shot timers are priced at 75 cents to \$1 in 100-up quantities, while the counter-timers are in the \$3 range. However, for timing applications of more than several minutes, this price differential is more than offset by savings in the external component cost.

For example, a time delay of approximately two minutes, with an error of less than $\pm 3\%$ over the 0-to-70-C temperature range, can be obtained with a one-shot timer. But the timer would require a $12\text{-}\mu\text{F}$ polycarbonate capacitor that costs about \$8. With a counter-timer, such as the XR-2240, the same delay can be achieved with a $0.05\text{-}\mu\text{F}$ capacitor, which costs about 50 cents.

Among counter-timers, the choice can be made on the basis of the required delay. For extremely long delays—of greater than a year—or for operation with an external crystal, a circuit such as the MK-5009, with a long divider chain, is best suited. However, the XR-2240 would be better for applications in the seconds-to-days range that do not require an external reference. ■■



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TEXAS INSTRUMENTS
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Use pulse width modulation to control dc motors. With this approach, both speed and direction can be controlled by a single potentiometer.

Here's a way to use multiple-device ICs—such as hex inverters and quad transistor pairs—to control both the speed and direction of a dc motor with a single potentiometer. The method uses pulse-width modulation instead of the more common, SCR-phase-angle approach, and eliminates the need for a reversing switch.

With just one pot, two ICs and a few discrete components, you can control small, instrument-type dc motors rated at up to 15 V at 100 mA. For larger motors, power capability is increased

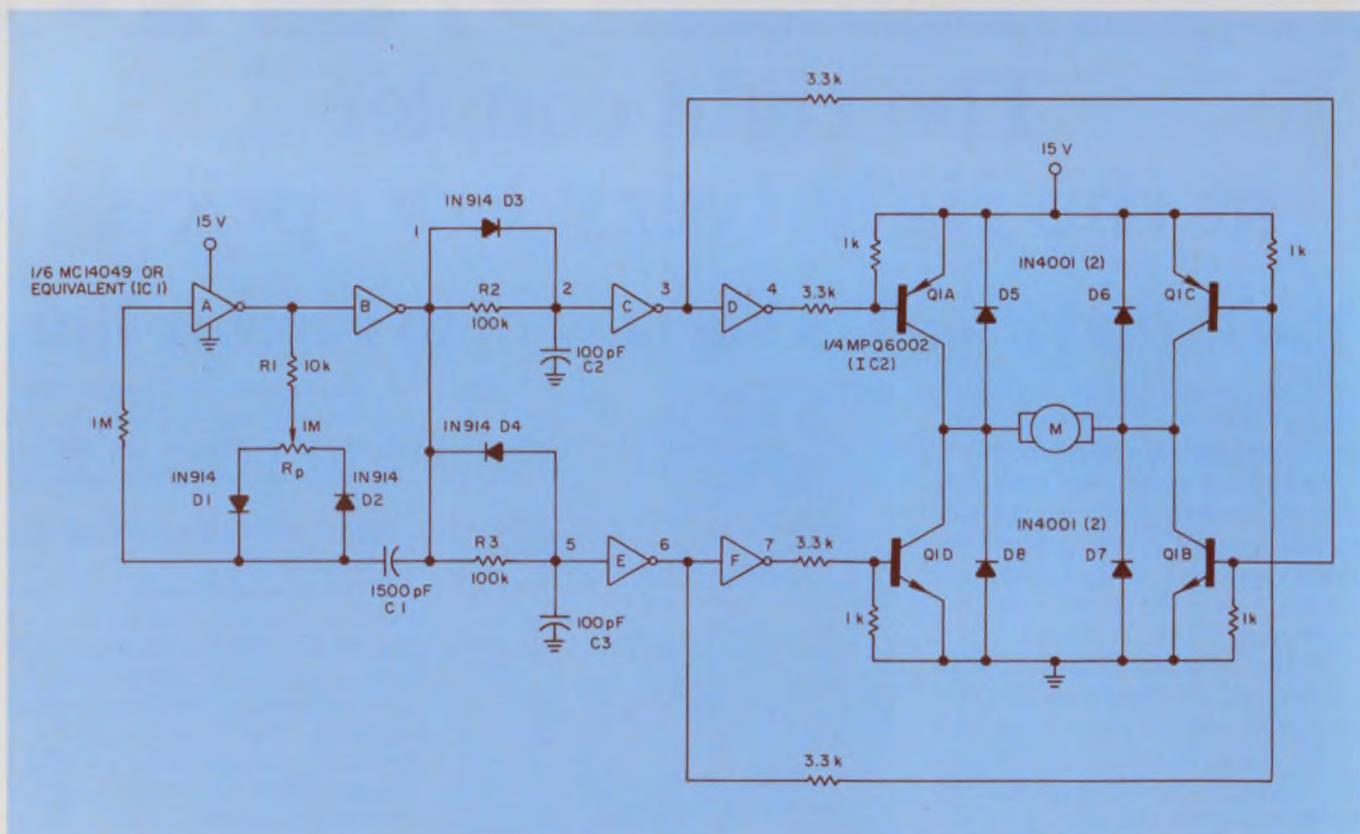
by addition of power transistors, which operate at higher voltages and currents.

Only two ICs are needed

The circuit consists of three basic blocks: a pulse-width modulated oscillator, a time-delay circuit and a bridge that acts as the motor driver (Fig. 1). A CMOS hex inverting buffer forms the oscillator and time-delay circuit, while the driver is composed of quad complementary transistor pairs. For larger motors, an npn transistor quad drives a complementary Darlington bridge circuit (Fig. 2).

The common-emitter bridge is driven in complementary fashion by two pulse-width-modu-

Al Pshaenich, Applications Engineer, Motorola Semiconductor Products Div., 5005 E. McDowell Rd., Phoenix, Ariz. 85008.



1. Both speed and direction of a small dc motor are controlled by a single pot in this pulse-width modula-

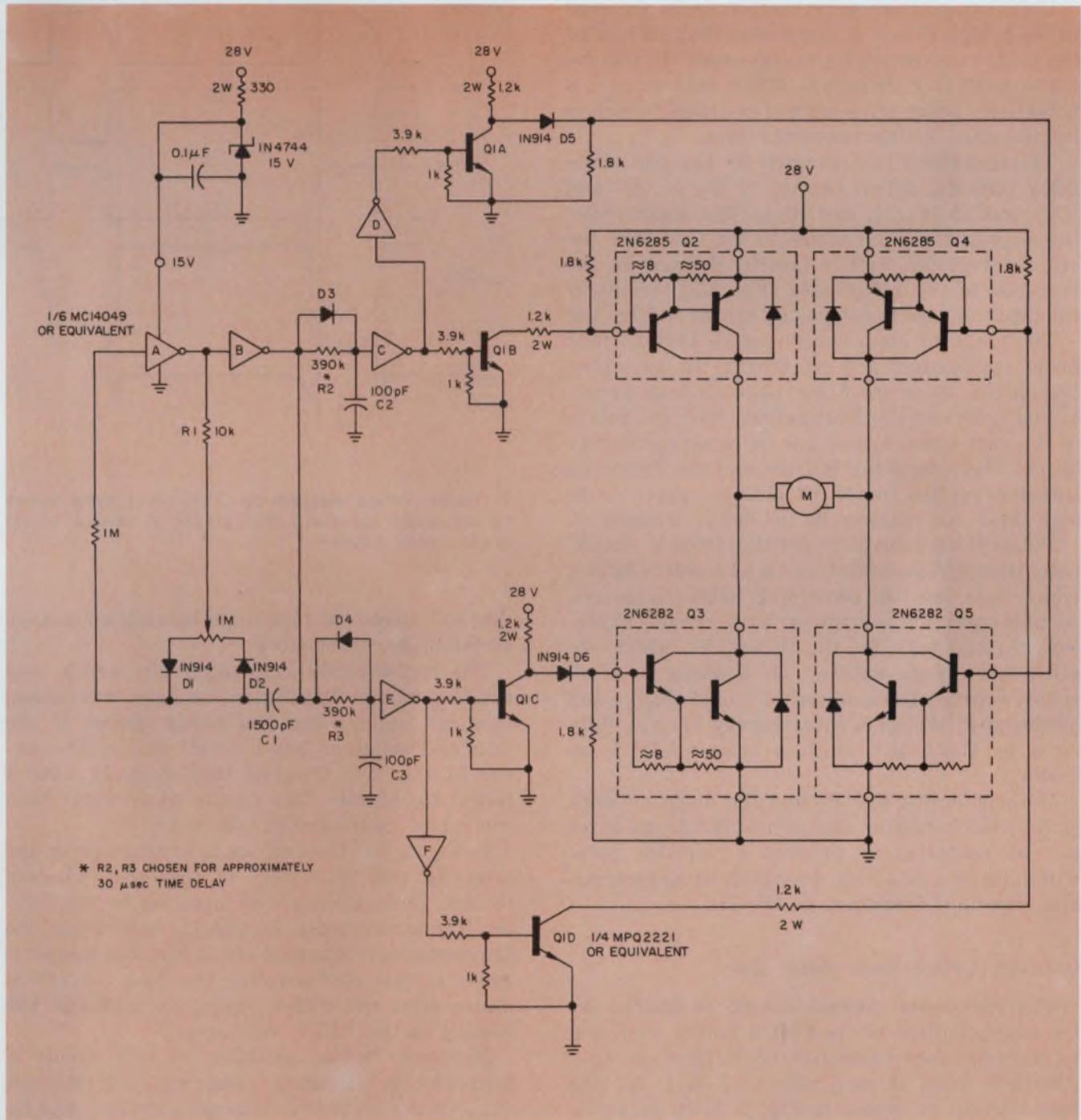
tion circuit. The oscillator and time-delay portion of the circuit use a CMOS hex inverting buffer.

lated signals derived from time-delay circuits. Thus opposite legs of the bridge are turned on alternately. The resultant algebraic current through the motor is a function of the pulse-width signal.

For example, if one pair of transistors, such as Q_1 and Q_4 in Fig. 1, are turned on by a waveform with a 75% duty cycle, then the complementary transistors, Q_2 and Q_3 , will be driven by one with a 25% duty cycle. The net, or integrated, motor

current is the difference between the two bridge currents, and determines both the speed and direction of the motor.

When the bridge is driven with a 50% duty cycle, the average current through the motor is zero and the motor is de-energized. At the maximum duty cycle of 95% (potentiometer R_p at one extreme), the motor rotates at maximum speed, either cw or ccw. As the potentiometer is turned toward the other extreme, the motor



2. Larger motors, which draw up to 5 A, can be controlled by use of power-Darlingtons in the bridge driver

and by use of a heftier supply. The input base current, about 20 mA, is drawn from the 28-V supply.

slows down, stops at the 50% setting, and then increases speed to the maximum in the opposite direction. Thus motor speed and direction are controlled by a single potentiometer.

Note that because of the absence of motor counter emf, the circuit draws maximum current when the motor is de-energized. However, this zero-speed current can be readily eliminated by ganging a switch to turn off oscillator power when the pot is at its center position.

Time delays prevent problems

Unless special preventative techniques are used in the bridge driver, it is possible that all legs of the bridge will conduct simultaneously during the finite switching duration. When this occurs, a potentially destructive current is drawn, which is limited only by the transistor beta.

This condition is prevented by the two time-delay circuits, which consist of R_2 , C_2 , D_3 and $IC_{1(C)}$ and R_3 , C_3 , D_4 and $IC_{1(E)}$. The negative-going edge of the input signal to the first time delay is integrated, and is thereby delayed by the threshold of the buffer gate (Fig. 3-2). Similarly the positive edge is delayed as shown in Fig. 3-5.

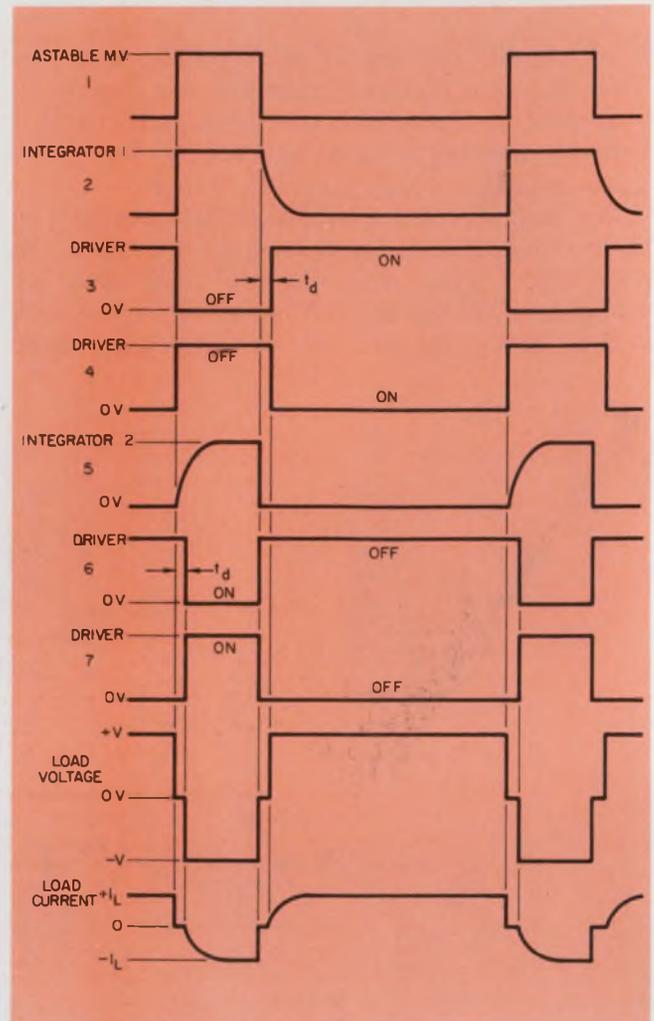
The resulting time delays ensure that all four bridge transistors are off during the switching transitions. Because of the relatively long propagation delays of the Darlingtons, the time delays of the high-power circuit are set to approximately 30 μ s. The time-delay buffers and the following inverter buffers should be able to source or to sink the 4 mA required by the driver transistors.

Pulse-width control is derived from a simple, potentiometer-controlled a s t a b l e multivibrator which uses the two remaining buffer inverters. Astable operation is achieved with just one capacitor, C_1 , and with R_1 , R_p , D_1 and D_2 , which—in effect—act as one resistor. (If a single, fixed resistor were used, the capacitor would charge and discharge at the same rate, thereby limiting duty cycle to about 50% with a typical CMOS inverter.)

With potentiometer R_p and the diode network shown, the capacitor charge and discharge rates can be regulated to produce a variable pulse width, hence a 5-to-95% duty cycle at an approximate constant frequency of 600 Hz.

Quad dissipation limits motor size

The low-power control circuit is limited by the supply voltage of the CMOS family used, and by the maximum dissipation of the quad device—1200 mW total at an ambient of 25 C for the four transistors shown in Fig. 2. With inductive loads, the bridge requires clamp diodes, D_5 through D_8 in Fig. 1, to prevent inductive spikes



3. Typical timing diagram for 75% duty cycle shows the important waveforms that prevail at various points in the control circuit.

that can exceed the maximum breakdown voltage of the bridge transistors.

The higher-power control circuit, which uses complementary Darlington bridge transistors, does not require external clamp diodes if the selected Darlington has internal diodes. The circuit of Fig. 2 is designed for 5-A loads, with a forced h_{FE} of 250. This results in an input base current of approximately 20 mA.

In Fig. 2, pnp Darlingtons are turned on by the saturated npn transistors of the quad, whereas the npn Darlingtons are clamped off by the drivers. The series diodes, D_5 and D_6 , ensure that the Darlingtons are clamped off at elevated temperatures. In this configuration the base current is drawn from the +28-V supply to minimize the loading on the +15-V logic supply.

Maximum power capability of this circuit is limited by the maximum voltage rating of the quad ($V_{CE0(max)} = 40$ V for the quad shown) and by the maximum collector current of the Darlington (in this example, $I_C(max) = 20$ A). ■■

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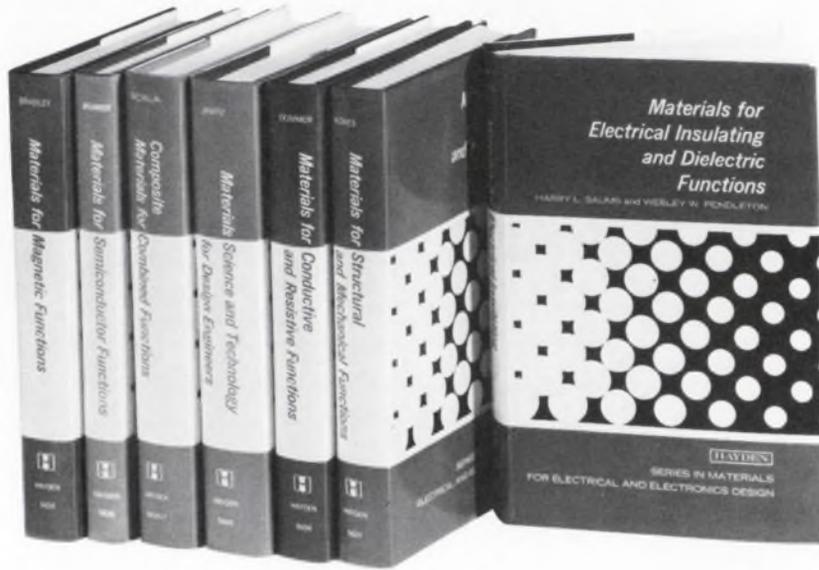


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INFORMATION RETRIEVAL NUMBER 28

Switch high inductive loads fast

with a push-pull current source that also cuts power consumption and boosts performance.

With a push-pull current-source driver to power an inductive load, you can improve switching times by over 30% and cut average power consumption by 50%—even for loads that draw pk-pk current of more than 7 A.

The driver uses essentially two circuits: One puts out high voltage to get the fast-flowing current into the inductive load; the other takes over during the steady state.

The design of push-pull current sources with outputs proportional to the input voltage is relatively simple for resistive loads. However, when it comes to driving an inductive load, the designer has a new set of problems, particularly when fast response is needed. The problems include these:

- Increased driver and power-supply complexity.
- Decrease in reliability because of high component stress.
- A need for some means for circuit cooling.
- Wasted power because of the use of high-voltage power supplies to get the fast response.

Carefully designed push-pull current sources can provide a solution to such inductive-load problems.

Start with resistive-load driver

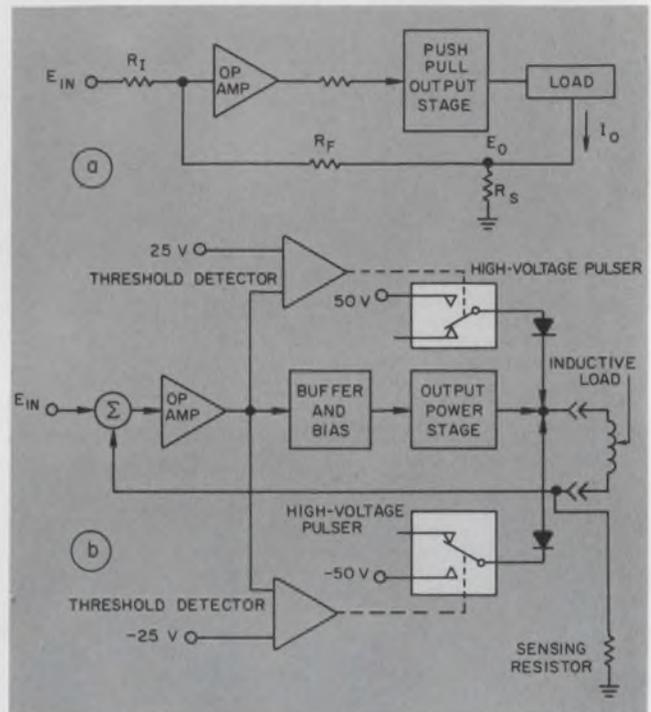
Fig. 1a shows a basic circuit for a current source, with the output current proportional to the input voltage. Voltage across the sensing resistor, R_s , depends on the magnitude of the input voltage, E_{in} , and the closed-loop gain of the circuit. When the load is placed in series with the R_s , the standard voltage amplifier turns into a current amplifier. The current in the load is directly proportional to the voltage developed across the R_s , and is given by

$$I_o = E_{in} (A/R_s), \quad (1)$$

where

- E_{in} = input voltage,
- A = closed-loop gain,
- R_s = sensing-resistor value in ohms.

John Logis and Ronald C. Scheerer, Design Engineers, Westinghouse Electric Corp., Friendship Airport, Baltimore, Md. 21203.

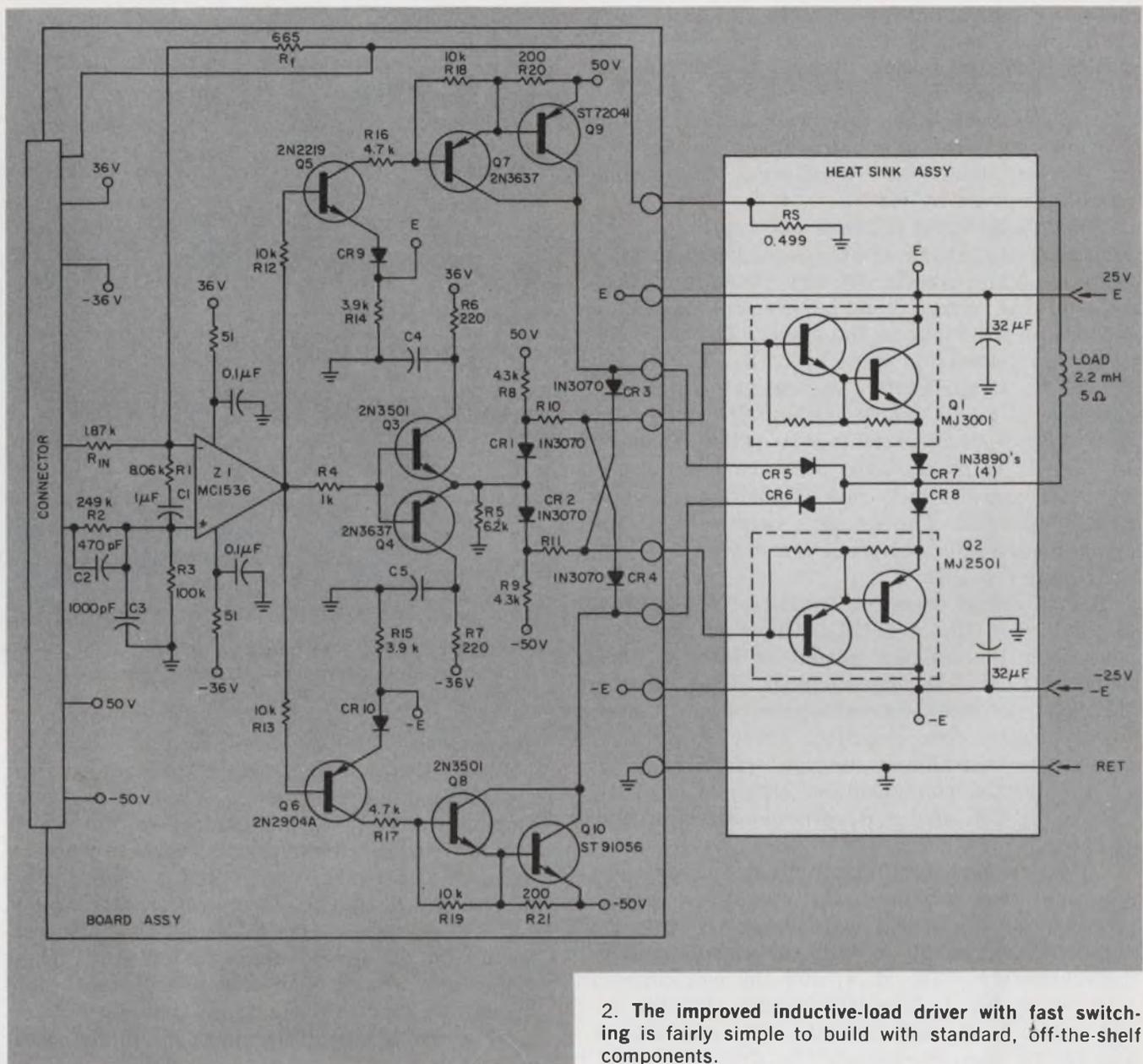


1. Relatively slow switching time and excessive power consumption of a standard feedback current amplifier (a) can be greatly improved by the addition of high-voltage pulsers that cause faster current build up in an inductive load (b).

The circuit of Fig. 1a works quite well with purely resistive loads. In the case of inductive loads, however, one question that immediately rises is: How fast can the current through the load be changed? In general, current through an inductive load is limited by the Ldi/dt of the coil, or, more specifically, by the voltage applied to the coil.

While the response speed can be increased by the use of higher-voltage supplies, the steady-state power dissipation would also increase, as would the stress on the components involved in switching the higher currents.

For this reason, the circuit in Fig. 1b was developed. Basically it has two signal-flow paths: one for steady-state operation, the other for fast switching. Note that the steady-state portion of the circuit is very similar to that of Fig. 1a. The load current is proportional to the voltage de-



2. The improved inductive-load driver with fast switching is fairly simple to build with standard, off-the-shelf components.

veloped across the sensing resistor. The only added circuitry is the buffer-and-bias networks to accommodate the fast switching feature.

The second signal path bypasses the buffer and bias circuits and the output stage. To understand its operation, let's look at what happens when a step voltage is applied to the circuit input.

As the input changes at a fast rate from one level to another, the output cannot follow it because of the Ldi/dt of the coil, and the op amp goes into saturation. Normally the op amp would stay saturated until the coil current reached the desired value, and then the circuit would begin to operate in a closed-loop configuration. From Fig. 1b, however, it is obvious that when the feedback path is opened and the op amp saturates (either at positive or negative level), one of the threshold-detector circuits is triggered. This, in turn, switches in the high-voltage supply

and causes coil current to build up at a higher rate.

Once the current reaches some desired level, the closed-loop configuration takes over, threshold detectors switch off, and the high-voltage supply is disconnected from the coil. Thus the approach in Fig. 1b yields two benefits:

1. Switching-time reduction, due to the presence of higher-than-normal voltage.
2. Power-consumption reduction, because a lower steady-state voltage can now be used.

Here is the actual circuit and its operation

Fig. 2 shows a practical circuit based on the approach, described in Fig. 1b. The basic feedback configuration is made up of resistors R_{in} , R_f , R , and R_s , op amp Z_1 , and transistors Q_1 and Q_2 . The buffer stage (an emitter follower) con-

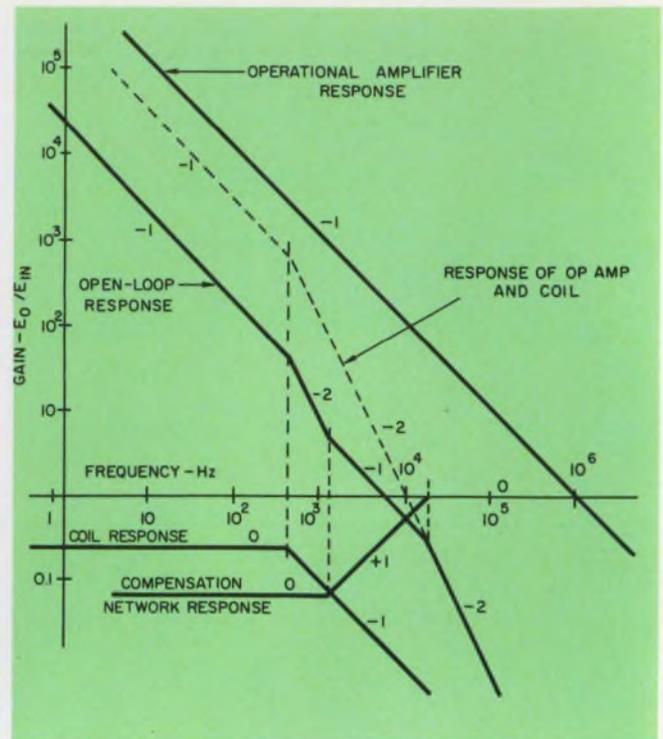
sists of R_5 , R_6 and R_7 , capacitors C_4 and C_5 , and Q_3 and Q_4 . The bias network, needed because of the high-voltage pulser circuits, is made up of R_8 , R_9 , R_{10} and R_{11} , and diodes CR_1 and CR_2 . The diodes reduce the crossover distortion and are blocking when the high-voltage pulsers are on. Under steady-state conditions, the output current is given by Eq. 1.

The op-amp input network plays an important role. Note that it is a double-ended compensation network. This cancels out any potential difference in the signal return between the input origin and the input to the driver. The RC compensation network is made up of R_{1n} , R_1 , R_2 , R_3 , C_1 , C_2 , C_3 . It shapes the over-all gain-frequency response to give a stable system with maximum bandwidth for fast switching. Its action is shown in Fig. 3. It makes sure that the over-all response crosses the unity gain axis with a -1 slope rather than -2 . The circuit's bandwidth is increased with this compensation network to approximately 5 kHz.

The threshold detectors consist of Q_5 , Q_6 , R_{12} , R_{13} , R_{14} , R_{15} , CR_9 , and CR_{10} . Under steady-state conditions the op-amp output is low, so that neither Q_5 nor Q_6 can conduct. Each of the threshold detectors drives a high-voltage pulser—one positive, one negative. These pulser networks are basically Darlington stages working in an inverted configuration. Diodes CR_3 , CR_4 , CR_5 , CR_6 , CR_7 and CR_8 provide steering and blocking.

To understand how the circuit works, let's go, step by step, through its operation. Under steady-state conditions, with a slowly varying signal applied to the op amp, the voltage gain is approximately $-(R_7/R_{1n})$, and the coil current is given by Eq. 1. Now let's assume that the input signal is at some positive level and that a fast-falling step commands the driver to reset the coil current to some new positive level. Because of the inherent coil lag, the output of the driver cannot slew as fast as the input. Thus the feedback loop is opened and the op amp saturates at a positive level. This causes Q_5 to conduct, triggering the Darlington pair, Q_7 and Q_9 , thus apply approximately +50 V dc to the junction of steering diodes CR_3 and CR_5 . Diode CR_5 permits the +50 V dc to appear across the coil, speeding up the coil current change.

While this process is taking place, certain protection measures are being enforced to guard other components from overstress. Thus CR_7 is forward-biased during steady state and allows positive current to flow to the coil from Q_1 . When the high voltage is applied directly to the coil by the pulser, this diode prevents the base-emitter junction of Q_1 from reverse-biasing beyond its maximum rating. Note that Q_2 does not conduct at this time, because its base and emitter



3. Amplifier stability is improved by the action of the op amp input compensation network (see Fig. 2) that introduces a positive unity slope.

are essentially at the same potential.

Diodes CR_1 and CR_2 , within the bias network, also perform an important function. With the op amp saturated, the voltage at the emitters of Q_3 and Q_4 is approximately equal to that provided by the bias network. The voltage at the junction of resistors R_9 and R_{11} is approximately +50 V, and CR_2 is reverse-biased. Thus this diode protects both Q_3 and Q_4 and the op amp. These diodes also ensure that only one of the output transistors conducts at a given time, by reverse-biasing the base-emitter junction of the other transistor.

After the current in the coil reaches the new desired level, the closed-loop operation takes over, the high-voltage pulser is de-energized, and the driver functions as a feedback amp.

A prototype model of the circuit of Fig. 2 was built and tested with an inductive load. The characteristic impedance of the coil was 2.2 mH and 5 Ω . The maximum differential switched current was 7.2 A. The circuit was compared with the standard feedback current amplifier, with the following results:

The switching time for the maximum differential current was reduced from 650 μ s to 450 μ s—a gain of more than 30%. The average power dissipation, based on the same switching time, was cut in half. The actual closed-loop bandwidth was 4.5 kHz. All theoretical assumptions used in the initial design were confirmed during test, and the circuit worked as anticipated. ■■

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Multiplexed operation of MOS registers more than doubles the data rate

With multiplexing, static MOS registers can compete in speed with dynamic registers. The scheme gives more than double the data rate of a static register, yet retains the convenience of static registers—no low-frequency limitation and use of a single-phase TTL-level clock.

The control circuitry generates two clock waveforms, ϕ_A and ϕ_B , from the system clock. These alternate the incoming data bits between the two pairs of 2533 registers. The quarter section of the 8233 demultiplexes the output data of the 2533s. The resultant register has a 4096-bit capacity.

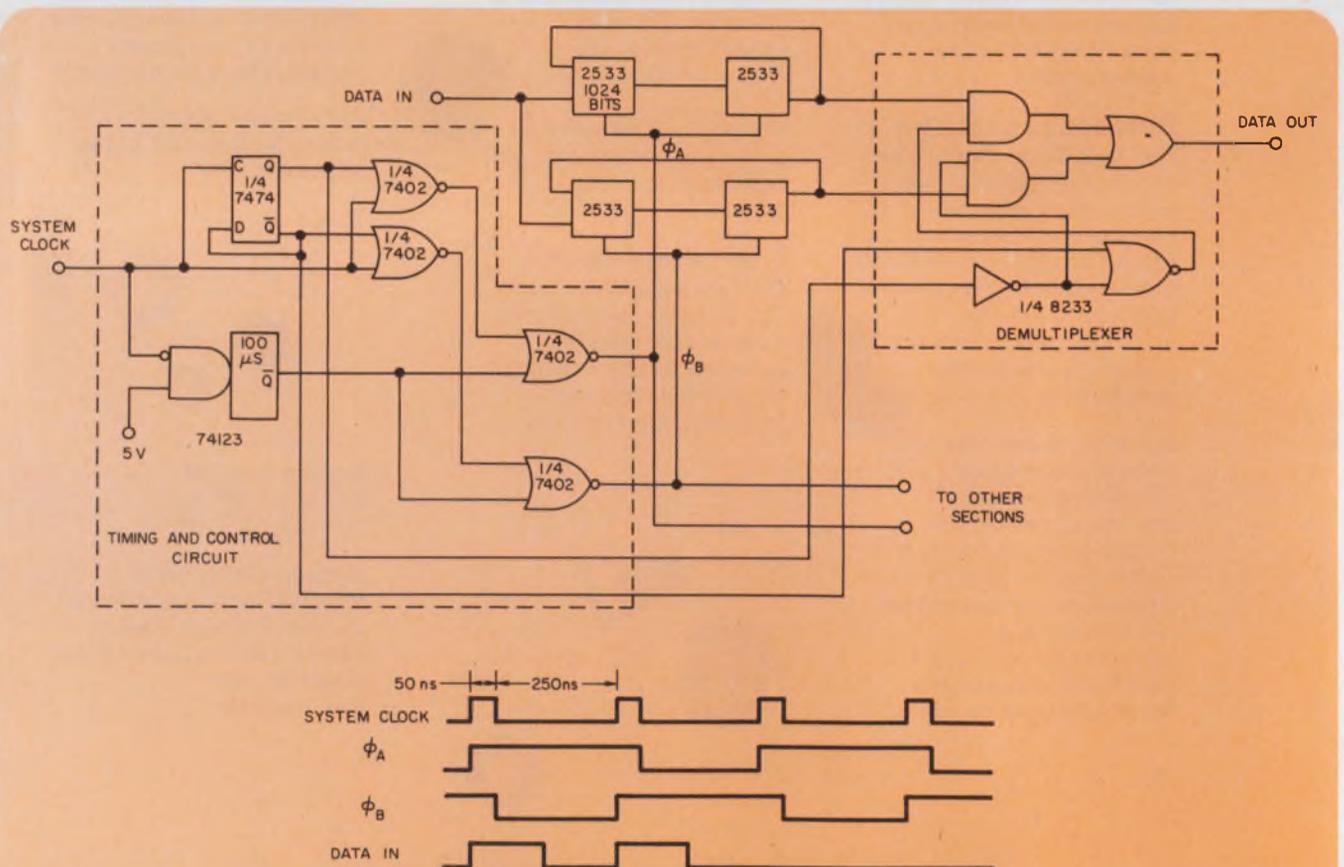
The system clock waveform shown permits

operation at data rates of 3.33 MHz. The one-shot returns ϕ_A and ϕ_B to ZERO after 100 μ s. This is a requirement for the static operation of the 2533 IC. The waveforms provided by the control circuit allow each chip to operate at a 1.666-MHz rate.

The scheme is readily extendable to shift register arrays. A single timing and control circuit operates up to eight 4-k channels. Two 8233s handle the eight output lines.

Bruce Threewitt, Applications Engineer, Signetics, 811 E. Arques Ave., Sunnyvale, Calif. 94086.

CHECK No. 311



Multiplexed static MOS registers allow more than double the speed of a single register—in this case

3.33 MHz rather than 2×1.5 MHz. The control circuit handles up to eight 4096-bit channels.

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OUTPUT VOLTAGE	OUTPUT CURRENT AMPS.	REGULATION LOAD $\pm\%$	REGULATION LINE $\pm\%$	RIPPLE MV RMS	PRICE	MODEL	SIZE INCHES
5	.250	.05	.05	0.5	\$39.00	5E25	2.3 x 1.8 x 1.00
5	.500	.1	.05	1	49.00	5E50A	3.5 x 2.5 x 1.00
5	1.0	.2	.05	1	69.00	5E100	3.5 x 2.5 x 1.25
5	1.5	.3	.1	1	98.00	5E150	3.5 x 2.5 x 1.25
5	2.0	.15	.05	1	110.00	5E200	3.5 x 2.5 x 2.00
5	2.5	.15	.05	1	125.00	5E250	3.5 x 2.5 x 2.00

...and the model you choose will be shipped 3 days after Acopian receives your order. With a 105-125 VAC input, use it at full rated load to 71° C. Short circuits won't damage it. These mini-modules can be mounted on a printed circuit

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Corp., Easton, Pa. 18042. Telephone: (215) 258-5441.

INFORMATION RETRIEVAL NUMBER 30

EXCLUSIVE-OR circuit handles wide range of input levels without power supply

Binary bits from a variety of sources can be compared with an EXCLUSIVE-OR circuit. The circuit shown (Fig. 1) requires no power supply and handles a wide range of input-signal level and load requirements.

The circuit obeys the standard EXCLUSIVE-OR truth table. When A is ZERO and B is a ONE, CR₁ and CR₂ are reverse-biased; therefore Q₁ will not conduct. The output is a ONE. Load current is conducted by R₃ and CR₃. When A is ONE and B is a ZERO, CR₃ is reverse-biased, the current through R₁ is shunted to ground and Q₁ is off. The output is again ONE, with load current conducted by R₂ and CR₂. If both A and B are ONE, CR₁ is reverse-biased and Q₁ conducts. And Y is a logic ZERO.

Choose R₂ and V_{OUT} according to the application, subject to limitations imposed by the input voltage.

Compute

$$I_L = \frac{V_{OUT}}{R_L} \quad (1)$$

Then calculate R₂ and R₃ (assumed to be equal here). Now

$$R_2 = R_3 = \frac{V_{IN} - V_D - V_{OUT}}{I_L} \quad (2)$$

With both inputs a logic ONE, the parallel combination of R₂ and R₃ determines

$$I_{C(Q1)} = \frac{V_{IN} - V_D - V_{CE(SAT)}}{R_2 \parallel R_3} \quad (3)$$

Then set

$$R + R_1 = \frac{V_{IN}}{I_{C(Q1)}/h_{FE}} \quad (4)$$

Choose R₁ to be much greater than the forward resistance of CR₁; then find R from Eq. 4. The circuit outputs with a variety of operating voltages, and the components are given in Fig. 2.

P. R. K. Chetty, Indian Space Research Organization, A 3-6, Peenya Industrial Estate, Bangalore, India 560022.

CHECK NO. 312

TRUTH TABLE		
A	B	Y
0	0	0
0	1	1
1	0	1
1	1	0

1. An EXCLUSIVE-OR circuit that needs no power supply. Transistor Q₁ is reverse-biased, except when A and B are both ONE, at which point the output is pulled to ground.

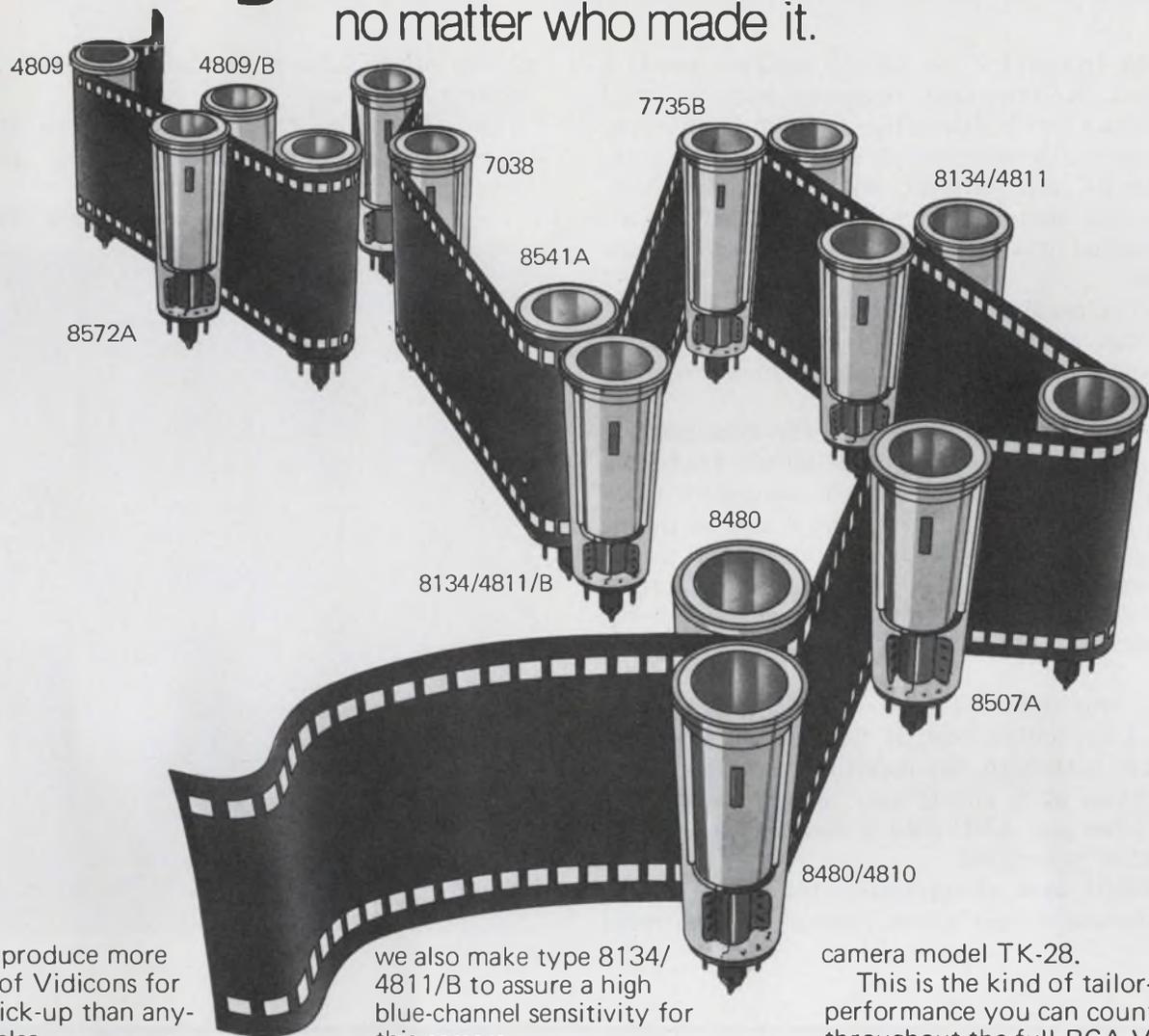
2. EXCLUSIVE-OR outputs for a variety of input signal levels and load resistances demonstrate the versatility of the circuit. The first circuit is designed to give a 3.5-V output.

INPUT VOLTS			OUTPUT VOLTS		
A	B	Y	A	B	Y
0	0	0	0	0	0
5	0	3.2	9	0	6.3
0	5	3.6	0	9	7.0
5	5	0.7	9	9	1.6

INPUT VOLTS			OUTPUT VOLTS		
A	B	Y	A	B	Y
0	0	0	0	0	0
18	0	1.4	30	0	2.3
0	18	1.5	0	30	2.6
18	18	2	30	30	8

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INFORMATION RETRIEVAL NUMBER 31

Edge-triggered R-S flip-flop built without capacitors

Quite frequently the digital designer needs a set-reset flip-flop that responds only to input transitions and is insensitive to input logic levels. One solution is to construct a flip-flop with gates and an RC input circuit, but this requires non-DIP components and results in a brief refractory period while the capacitors charge or discharge.

An inexpensive circuit that avoids these problems can be built with an AND-OR-INVERT gate and a J-K flip-flop—both of which are available in dual IC versions.

Feeding the outputs of the flip-flop back to the inputs allows only a single output transition direction upon receipt of each successive clock pulse. Compared with tying the J and K inputs for complementary operation, this method makes the circuit operation independent of the initial state of the flip-flop. The outputs also select the earliest valid input signal for clocking the flip-flop.

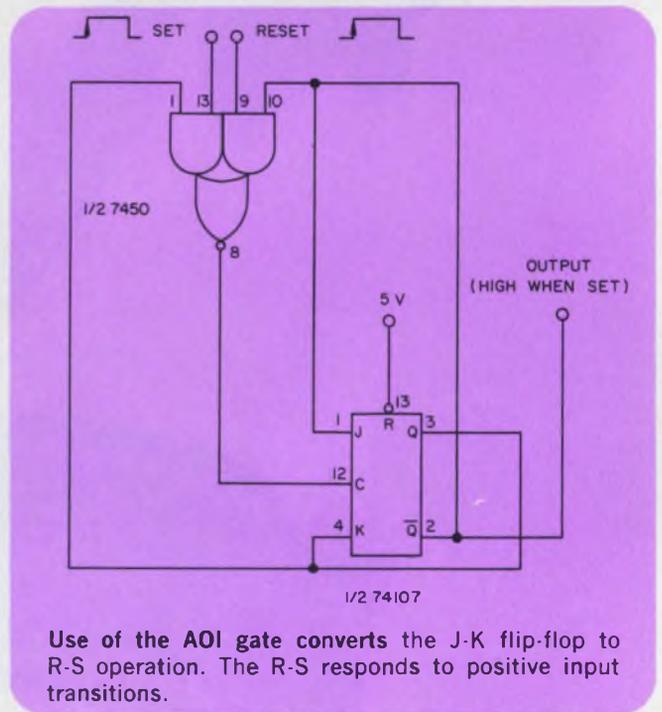
It is important not to slow the output with too great a capacitive load. If the Set and Reset inputs are both high, the resulting nonsymmetrical transitions of Q and \bar{Q} may cause a brief clock pulse after one AND gate is disabled and before the other is enabled.

A useful area of application for this circuit is in interface design where signals from external

devices often occur at random times and are of arbitrary duration.

Rudy Engholm, Phonetics Laboratory, University of Michigan, 1079 Frieze Building, Ann Arbor, Mich. 48104.

CHECK No. 313



IFD Winner of September 27, 1973

R. Dale Hefner, Electronics Director, The University of Tucson, College of Liberal Arts, Dept. of Chemistry, Tucson, Ariz. 85721. His idea "Variable-speed, synchronous-motor control operates from 12-V battery or 120-V-ac line" has been voted the Most Valuable of Issue Award.

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Formerly Electro Development Corporation

INFORMATION RETRIEVAL NUMBER 32

Display linked to computer lets operator intervene

By combining a graphical display terminal with a computer-controlled process, Siemens of West Germany has made it possible for an operator to have both a visual presentation of complex information and the capability to intervene in the process by way of a keyboard.

The terminal, called 3976, allows displays of up to 2048 characters or symbols. A total of 64 characters and 122 symbols can be used to compile different texts or figures in seven colors. The transmission rate is 9600 bits/sec.

The screen is divided into 32 lines, each with 64 positions—a total of 2048 positions—and an al-

phanumeric character or a symbol can be inserted at each position. Graphical representations are obtained when the symbols are joined in rows. Characters have a resolution of 5×7 dots, and symbols one of 7×9 dots.

The display terminal allows intervention in a complex process. Characters and symbols are fed in via keyboard and a stick that controls a light spot on the screen. Points are located with the control stick, and the selected position automatically fed to the computer. Additional information can also be inserted with special keys.

Any number of terminals can be connected in parallel.

CIRCLE NO. 319

Silicon IMPATT diodes show reduced noise

Improved, large-signal noise performance from silicon IMPATT diodes that use a new junction structure has been obtained by researchers at Thomson-CSF in Orsay, France. The diodes differ from the abrupt-junction kind in that a high-resistive, p-type layer forms a large part of the avalanche region. Modification of the avalanche region reduces noise that arises mainly from the avalanche-multiplication process.

The significant mechanisms in the effect are: a widening of the avalanche region, lowering of the electric field at breakdown, flattening of the electric field profile and more pronounced space-charge effects. Typical FM noise is 9 Hz/kHz^{1/2}, with a Q factor of 500.

CIRCLE NO. 317

Low-cost glasses made for optic communication

High-purity, low-cost glasses for fiber-optical communication systems have been produced by researchers at Sheffield University, England. In conjunction with the Standard Telecommunication Laboratories and the British Post Office, the researchers prepared soda-lime/silicate glasses by coupling rf power to glass that is held in a cold silica crucible.

This technique reduces contamination caused by the crucible and furnace refractories. The method has resulted in fiber-optics glasses that show losses approaching target specification for communication systems of 20 dB/km. The high-purity conventional glass can be fabricated as single or multimode optical waveguides.

CIRCLE NO. 318

Y circuit uses logs to derive products

A technique of adding logarithms in an npn bipolar circuit to derive the algebraic product of two variables has been developed by Plessey of Towcester, England. The Y circuit—ideal for integrated-circuit implementation—uses a simple method of distortion cancellation that is independent of the device's current gain and base spreading resistance. Accuracy is within 0.1% with current gains of about 150.

Memory cell built with CDI process

A memory cell that uses the collector-diffusion-isolation (CDI) process has been developed at Manchester University in England. The design draws an average power of 1 mW/bit in the unselected quiescent state. Power dissipation of the selected cell is about 15 mW/bit, and the sense current is more than 1 mA.

Because of the high ratio of selected to unselected power, many cells with a short cycle time can be provided on a single chip. A memory of 256 bits with a total power dissipation of 500 mW has been constructed.

Higher frequency devices built with ion implants

The implanting of ions on the quartz substrate of a surface-wave device increases the velocity of the surface waves. Higher frequency devices can then be built. Produced by researchers at Thomson-CSF in Orsay, France, the 100-keV ions modify the quartz surface from crystalline to amorphous.

Various ions have been used, with an ion-bombardment flux of about 10^{16} ions/cm². The greatest velocity increase—about 1.1% at 180 MHz—was obtained with positive lithium and helium ions. The insertion losses of surface-acoustic-wave delay lines are not significantly changed by ion implantation.

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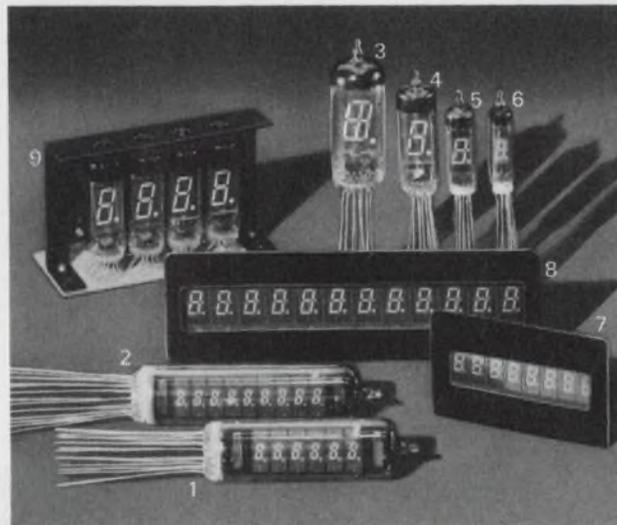
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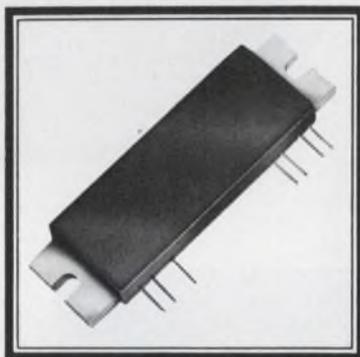
INFORMATION RETRIEVAL NUMBER 33

Available! RCA UHF Power Amplifier Modules... in production quantities.

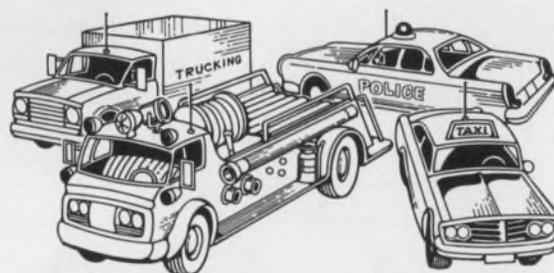
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Frequency Range (MHz)	395-440	395-440	395-440	440-470	440-470	440-470	470-512	470-512
Power Output, Min. (W)	10	13	15	10	13	15	10	12
Supply Voltage, Nom.	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5
Power Gain, Min. (dB)	20	20	20	20	20	20	20	20
Overall Efficiency, Min. (%)	35	35	35	35	35	35	35	35

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Data loggers catalog events by group size



Edmac Associates Inc., 333 W. Commercial St., East Rochester, N.Y. 14445. (716) 385-1440.

A line of event recorders and companion playback-printout unit can present time-event data in histogram form. The recorders—model 2042, a single channel unit or model 2043, a two-channel unit—record yes-no events at rates up to two a second on ordinary C-60 cassettes. The information is accumulated by group size in the memory of the playback unit, model 2150. The 2150 furnishes total event count per channel and total number of events in each group size. The counts are printed out on an adding machine tape. Thirty-one group classes are provided. An adjustable delay determines the grouping of multiple events.

CIRCLE NO. 250

Versatile CRT terminal also handles peripherals

Computer Communications, 5933 W. Slauson Ave., Culver City, Calif. 90230. (213) 391-0328. Under \$3000.

The CC-40 CRT terminal consists of a TV monitor, keyboard and a controller. The terminal has a storage capacity of 1920 characters and can display the dot-matrix characters in a single 24 × 80 page or two 12 × 80 pages. Transmission rates up to 50,000 bit/s can be used. Multiple terminals can be attached to a single line and polled. Available options include printers, tape cassettes and a light pen.

CIRCLE NO. 251

Flexible disc file accepts 3740 media

Memorex Corp., San Tomas at Central Expressway, Santa Clara, Calif. 95052. (408) 987-2200. From \$595.

Designed for manufacturers of IBM-compatible equipment, the 652 is a flexible-disc drive that reads and writes data on 3740 media. The unit can write and read at a transfer rate of 250-k bit/s. Data can be formatted in sector or index mode at the users option. The maximum capacity of the 652 is 77 tracks at 41-k bits each or a total of 3.1-M bits. Access time to data includes 10 ms settling time, 10 ms positioning time and 83 ms average latency. The model 651—without 3740 compatibility—affords higher data rates and storage capacity.

CIRCLE NO. 252

Controller adds eight data channels to mini



Digital Computer Controls, Inc., 12 Industrial Rd., Fairfield, N.J. 07006. (201) 227-4861. \$2000; 45 days.

A communications controller designated the 116431 handles eight asynchronous channels. The units, mounted on a 15 by 15-in. board, plug into a slot of the company's D-116 minicomputer. Each channel has its own independent send/receive speed with rates from 110 to 19,200 baud. The user can also specify parity, number of data bits (5, 6, 7 or 8), number of stop bits and auto answer (if desired). EIA RS-232 or 20 mA current loop operation is available on any channel.

CIRCLE NO. 253

Small POS terminal has 10-digit display



Mega Products Corp., P.O. Box 534, 622 Lancaster Ave., Berwyn, Pa. 19312. (215) 647-6422. Under \$300; 60-90 days.

A visual display and inquiry terminal that costs less than \$300 in quantity, the model 10-9, has a 10-digit display area, nine backlit panels, a 16-character keyboard and a "transmit" indicator light. The 10-digit display shifts from right to left as each character is entered. The panels have pre-printed legends that illuminate when the computer responds. Up to four panels can be lit at one time. The terminal provides buffering for up to 48 received or transmitted characters. Data communication is bit-serial at speeds of 150, 300, 600 and 1200 baud. Additional flexibility is provided by the terminal's micro-computer architecture. Options include check-digit verification, addition of arithmetic functions and provision for external input from point-of-sale reading devices.

CIRCLE NO. 254

Floating-point firmware for microprocessors

Recognition Systems, 15531 Cabrillo Rd., Van Nuys, Calif. 91406. (213) 785-2179. \$495; 2 wks.

A four-PROM floating point package for Intel's 8008 and 8008-1 Microprocessors provides the basic four arithmetic operations as well as square root and floating point-to-positional BCD output for display purposes. Floating point numbers are represented by three 8008 words; a two word mantissa (16 bit accuracy) and a third word which carries the mantissa sign and the characteristic. Included in the above are a number of double-word subroutines such as left-shift, right-shift, add, subtract, compare, transfer, and a fixed-to-floating point converter.

CIRCLE NO. 255

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SE-5455

Recessed chip mount for improved performance.
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Phototransistors



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Replaces TIL-613-616



SD-1440

Ideal for single-sided PC boards. Replaces L15E



SD-2440

Standard pill package
Replaces TIL, MRD & OP 601-604; LS 600



SD-5443

Replaces TIL-81, CLT 2130 thru 2160; L14F Type; MRD 300 and 3000 Series

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INCORPORATED

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Richardson, Texas 75080

DATA PROCESSING

PDP-11 family gains two midrange minis

Digital Equipment Corp., 146 Main St., Maynard, Mass. 01754. (617) 897-5111. See text.

Two new computers, an expanded PDP-11/05 and the PDP-11/35, have been added to the PDP-11 line. The expanded 11/05 has a larger chassis than the standard 11/05, comes with a minimum of 8 k core—instead of 4 k—and has increased power supply capacity. The price \$6495 is \$1700 more than its predecessor. The PDP-11/35 is available in two packaging configurations. The 10.5-in. high PDP-11/35 comes with 8 k words expandable in 8 k increments to 128 k and is priced from \$9495. The 21-in. high version begins with 32 k, but expands to 128 k in 32 k increments. The price: \$20,495.

CIRCLE NO. 256

Modular CRT systems have desk-top cabinets

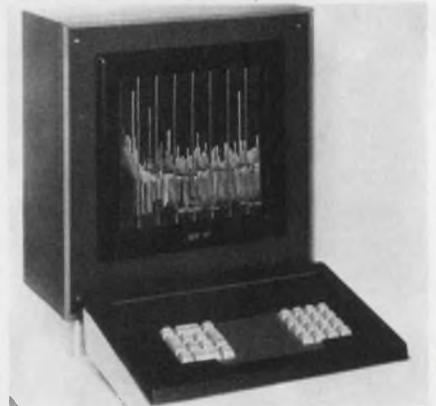


Ann Arbor Terminals, 6107 Jackson Rd., Ann Arbor, Mich. 48103. (313) 769-0926. From \$900; 15 days.

The Design III series of CRT terminals are complete desk-top terminals. But, their modular circuit cards are directly interchangeable with the company's Series 200 controllers and keyboards. All units have a 14-in. monitor and provide 9600 baud asynchronous communications. The series—available in 16 models—provides display formats to 40 lines \times 80 characters and can drive up to 10 video monitors. Optional configurations include graphics, printer add-ons and multidrop systems.

CIRCLE NO. 257

Display system creates patterns with numbers



Digicom, Inc., Paramount Building, North Chelmsford, Mass. 01863. (617) 251-8595.

Designed to permit visual interpretation of raw digital data the plasma-graph display system uses specially designed figures to represent binary digits from 0 to 15. These characters are optically weighted in proportion to their numerical value. The resulting patterns provide an analog representation of data content or meaning, yet retain the absolute value of each individual data point. The display system can operate on-line or off-line. An entire display of 10,800 characters takes less than 10 seconds to complete.

CIRCLE NO. 258

Data system transmits 16-bit parallel words

Kantronics Co., 1202 E. 23rd St., Lawrence, Kan. 66044. (913) 842-7745. \$880; 90 to 120 days.

Two model LLI-16 interfaces give bidirectional 16-bit parallel data transmission over distances up to 1000 feet. Each interface contains a receiver and transmitter that operate independently of one another. The transmitter takes data, adds a parity bit and sends 17 bits over the interconnecting cable. The receiver recomputes parity then presents 16 data lines to the local computer as well as a "parity correct" or a "parity error" flag. The maximum transmission rate is 65-k words/s in either direction.

CIRCLE NO. 259

MOSTEK's 1024-bit static RAM, the MK 4102P, gives you 450 ns access time. Another big move forward in MOS RAMs!

MOSTEK's MK4102P-1 features two industry firsts: it's the fastest 1024-bit static RAM (450 ns access time) and the first to combine N-channel silicon-gate and ion-implantation technologies, industry's most advanced processing technique. Plus, it's a pin-for-pin replacement for the 2102-1.

All inputs are directly compatible with TTL circuitry. The high impedance "off state" coupled with "chip select" input

permits large memory array construction with a minimum of additional circuitry.

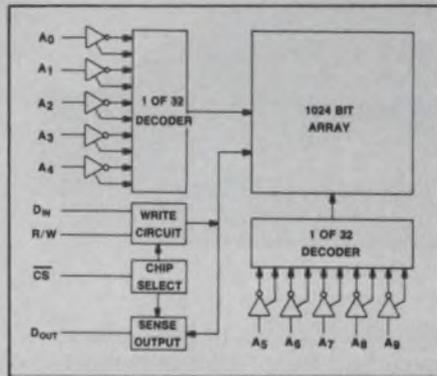
Volume production capacity backs-up the 4102. MOS RAM production at MOSTEK, bolstered through increasing use of 3-inch wafers, is currently exceeding 250 million bits per month with total deliveries to date of more than two billion bits. With this record, MOSTEK is now one of the world's largest producers of MOS RAMs. So you can be assured that your biggest orders will be handled promptly.

MOSTEK's memory heritage includes other popular RAM

circuits. The MK4006P dynamic RAM was the first TTL compatible 1024-bit RAM. The MK4007P 256-bit dynamic RAM was first to combine low power, high performance and wide voltage range. MOSTEK RAMs are available in volume now from distributor stocks.

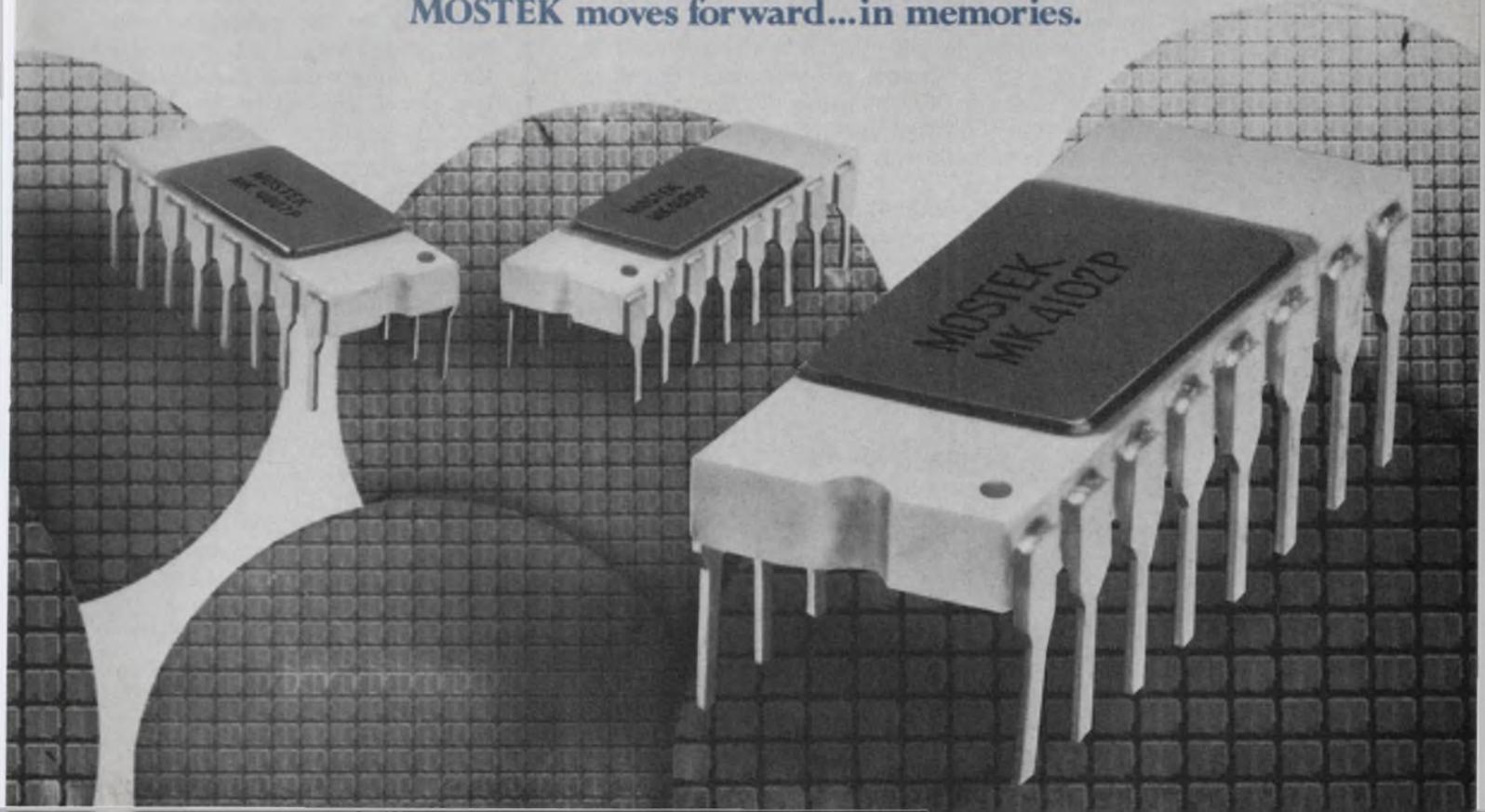
Performance and volume production capacity — good reasons to call MOSTEK for random access memories. *And watch for the next big development in RAMs — coming soon from MOSTEK.*

For a data sheet on the MK4102P-1 contact: MOSTEK, 1215 West Crosby Road, Carrollton, Texas 75006, (214) 242-0444. Or call the MOSTEK representative nearest you.



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MOSTEK moves forward...in memories.



Super Cop



Super protection with the unique adjustable Crowbar Overvoltage Protector. Makes the Sorensen SRL a great supply for lab/system uses. Fast front panel adjustment of overvoltage level without removing the load . . . instant front panel meter monitoring of set point, plus these additional SRL features: resistance and signal programmability; fast response time — 70 to 150 μ sec. — through full load range; low — 3½" to 7" — rack panel height; high power-density . . . in 14 models with outputs from 250 to 2000 watts. SRL — the super choice for maximum reliability, stability and value in medium power, low voltage applications. For complete data, contact the Marketing Manager at Sorensen Company, a unit of Raytheon Company, Manchester, N.H. (603) 668-4500.

Representative Specifications — SRL

- | | |
|---|---|
| <ul style="list-style-type: none"> • Voltage Mode <ul style="list-style-type: none"> Regulation (combined line & load) 0.1% Ripple (PARD) rms: 350 μv. p-p: 20 mv. Temperature Coefficient Δ/°C .01% + 200 μv. | <ul style="list-style-type: none"> • Current Mode <ul style="list-style-type: none"> Regulation (combined line & load) .02% + 4 ma. Ripple (PARD) rms: 0.5 to 30 ma. Temperature Coefficient Δ/°C .01% + 1 ma. |
| <ul style="list-style-type: none"> • Voltage Ranges <ul style="list-style-type: none"> 0-10 volts to 0-60 volts (14 models) | <ul style="list-style-type: none"> • Price Range <ul style="list-style-type: none"> \$500-1025 |

Sorensen
POWER SUPPLIES

INFORMATION RETRIEVAL NUMBER 37

Matched transistor arrays offer low-noise

Plessey Semiconductors, 1674 McGaw Ave., Santa Ana, Calif. 92705. (714) 540-9979.

A series of matched arrays, featuring low noise figures and f_T values greater than 2.5 GHz, consist of the following models: The SL360C, a matched pair, lists an h_{FE} of 65, noise figure of 4 dB and a minimum BV_{C10} of 30 V. The SL362C matched pair has an h_{FE} of 70, noise figure of 2 dB and minimum BV_{C10} of 20 V. The SL3145, a differential pair with a triplet array, has an h_{FE} of 80, noise figure of 3 dB and minimum BV_{C10} of 20 V. All arrays operate over the —55-to-125-C temperature range.

CIRCLE NO. 260

MSI register and arith units use less power

Fairchild, 464 Ellis St., Mountain View, Calif. 94042. (415) 962-3816. 93L38: \$5.90; 93L41: \$7.77 (100-999).

Low-power versions of the company's 9338 multiport register and 9341 arithmetic logic unit are now available. The 93L38 8-bit register dissipates only about one-fourth as much power while operating at half the speed of the standard circuit, according to the company. Similarly, the 93L41 4-bit arithmetic logic permits reduced costs through less power dissipation.

CIRCLE NO. 261

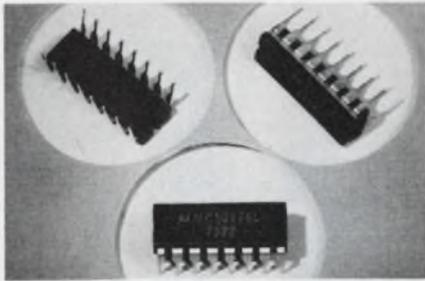
256-bit ECL pROM accesses in 15 ns

Signetics, 811 E. Arques Ave., Sunnyvale, Calif. 94086. (408) 739-7700. \$20.80 (100); 5 wk.

The 10139, a 256-bit ECL programmable ROM, features a typical access time of only 15 ns. The new pROM also offers full compatibility with ECL 10,000 and uses nichrome fuses as the memory elements. The 256-bit capacity of the 10139 is organized into 32 words of eight bits each. The words are selected through five binary address lines. Typical power dissipation is 580 mW.

INQUIRE DIRECT

Three ICs added to MECL 10,000 Line

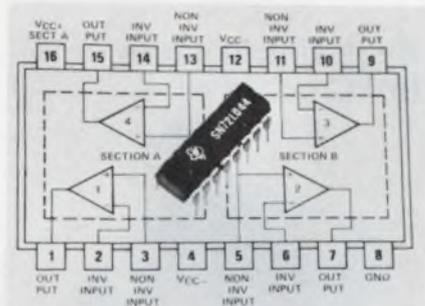


Motorola, P.O. Box 20924, Phoenix, Ariz. 85036. (602) 244-3466. MC-10123L: \$2.09; MC10172L: \$5.42; MC10176L: \$7.97 (100-999); stock.

Three ECL 10,000 ICs can be used to reduce system component count, and thus, cut costs. The MC10176L hex master-slave D flip-flop has a 125-MHz guaranteed toggle rate. The six flip-flops in a package reduce costs per function. The MC10172L dual binary-to-1-4 decoder can be used as a 2-line-to-4-line demultiplexer. The MC-10123L triple 4-3-3 input-bus driver provides twice the driving capability of other drivers.

CIRCLE NO. 262

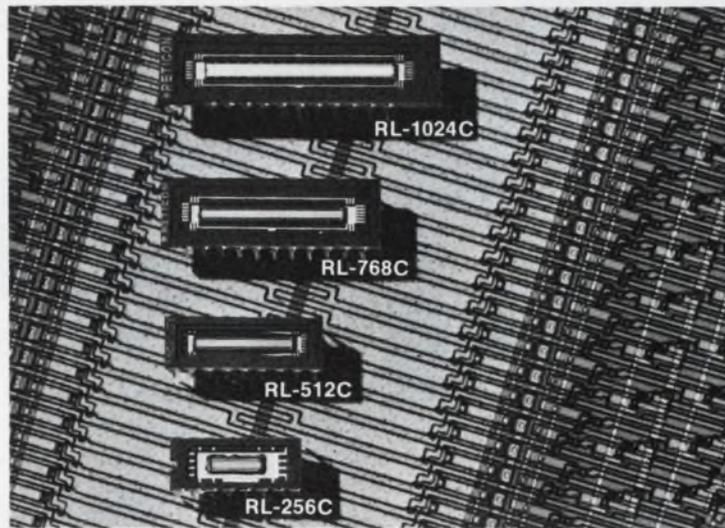
Quad op amp uses only 340 μ W



Texas Instruments, P.O. Box 5012, M/S 308, Dallas, Tex. 75222. (214) 238-3741. \$4.15 (100); 12 wk.

A quad low-power monolithic op amp, believed to be the first of its type, uses only 340 μ W at ± 2 V. Called the SN72L044, the new IC also has a low supply current of 0.25 mA at ± 15 V for all four amplifiers and a low equivalent input noise voltage of 50 nV/ $\sqrt{\text{Hz}}$. Power can be applied to one section, consisting of two amplifiers while the other section with the other two amplifiers remains unpowered. Other important features include internal frequency compensation, absence of latch-up and short-circuit output protection.

CIRCLE NO. 263



Solid State Image Sensing

Reticon offers the most complete line of solid state image sensors for OCR, facsimile, page/document reader, film scanning, real time spectroscopy, non contact measurement and inspection applications.

High resolution of up to 1024 elements on 1 mil centers is available on a single monolithic chip with serial video readout. Charge storage mode operation provides high sensitivity with scan rates up to 10 MHz. Low power dissipation of less than 10 mwatts and the highest quality silicon gate process assures minimum dark currents and maximum dynamic range.

Circuit cards (RC series) containing complete drive and video amplifier circuits are also available from inventory for any Reticon image sensor.

Our RL256C through RL1024C devices are much improved pin compatible replacements for previous designs.

Write or call for detailed data sheets and external circuit information.

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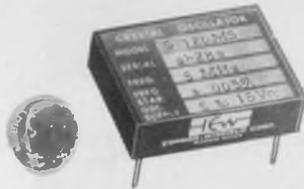
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(415) 964-6800 TWX 910-379-6552
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This SPECIAL OFFER is to introduce our "C" devices, which will be shipped complete with the RC series circuit cards providing all external drive and video amplifier circuits. Specify RL256C/RC, RL512C/RC, RL768C/RC and RL1024C/RC. Order must be received within 30 days from publication date and must be entered directly with the factory. Only one per customer. Offer is for U.S.A. domestic sale only.

\$100/bit
plus \$250 (for inclusion of complete drive & video circuitry)
as low as 25¢/bit in large OEM quantities

INFORMATION RETRIEVAL NUMBER 38

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CONNOR-WINFIELD'S SMOS Oscillator

Frequency:

Available at any fixed frequency, 50 kHz to 30 MHz.

Frequency Tolerance:

(accuracy + stability)
16 different combinations of tolerance and temperature range ranging from $\pm 0.001\%$, $+20^{\circ}\text{C}$ to $+40^{\circ}\text{C}$, to $\pm 0.05\%$, -55°C to $+125^{\circ}\text{C}$.

Supply Voltage:

Any supply voltage from 4 Vdc to 15 Vdc, with supply current from .2 ma to 13 ma, depending on supply voltage.

Output Waveform:

Square wave.
Rise time 50 ns nominal.

Output Amplitude:

from 2.6 Vpp to 12 Vpp into a 2 K Ω load, or
from 3.6 Vpp to 18 Vpp into a 10 K Ω load, depending on supply voltage.

Termination:

.03" diameter gold plated pins.

Dimensions:

1.6" L x 1.2" W x 0.4" H.

Delivery:

Stock to 4 weeks.

CONNOR-WINFIELD CORP.



West Chicago,
Illinois 60185
Phone: (312) 231-5270

INFORMATION RETRIEVAL NUMBER 39

PACKAGING & MATERIALS

Mounting package handles any DIP LED



Industrial Electronic Engineers, Inc., 7720-40 Lemona Ave., Van Nuys, Calif. 91405. (213) 787-0311.

Universal LED mounting hardware accepts any dual-inline LED display with 0.3 in. row spacing, regardless of manufacturer. The package consists of a one-piece nylon bezel, a circular polarizing window and a one-piece, behind-the-panel socket assembly, which eliminates all individual DIP sockets. Dual-inline displays with 14 or 16 pins can accommodate from two to eight units. The socket assembly has wrap terminations.

CIRCLE NO. 264

Paint your circuit with this conductive coating

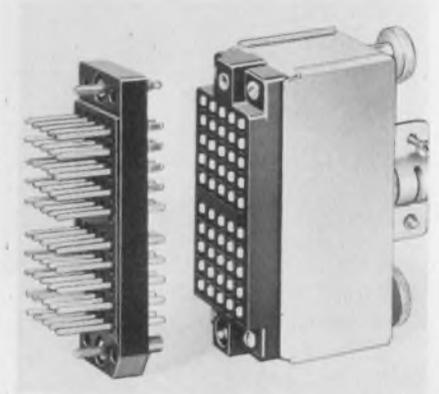


Acheson Colloids Co., Box 288, Port Huron, Mich. 48060. (313) 984-5581. \$35; experimenter's kit.

Care to make a microphone wire out of a ball of twine? Or paint your own electric circuit? Acheson's new series of +500 Electrodag high-temperature, nonsilicone coatings can be used for printed or painted circuitry, for heating elements and high temperature static-bleed applications. Important features include: ambient working temperatures of over 260 C; remains flexible over temperature range of -40 to over 260 C; and cures at room temperature.

CIRCLE NO. 265

Connectors use wrapped terminations

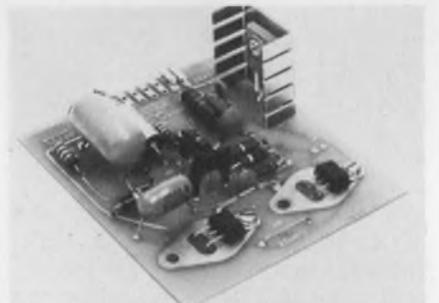


Underwriters Safety Device Co., 7300 W. Wilson Ave., Chicago, Ill. 60656. (312) 867-4600.

Originally developed for the telephone industry, these wire-wrappable connectors come in two sizes—50 or 72 connections. Contacts are gold-plated and rated at 3 A. The plug cover contains a cable strain-relief clamp and jack screws with a thumbwheel for mating and securing to the receptacle half of the connector. The plug and receptacle can have female or male contacts.

CIRCLE NO. 309

Heat sink solders to PC board



International Electronic Research Corp., 135 W. Magnolia Blvd., Burbank, Calif. 91502. (213) 849-2481.

PB1-36ND is a heat sink for TO-126 and other plastic power transistors. It solders directly and at right angle to a PC board. It measures only 1 W x 1/2 D x 1-3/16 H in. A 2N4442 transistor can dissipate 4 W with a temperature rise of about 70 C above ambient, when it is mounted on the heat sink. Only half as much power would cause the same temperature rise without the sink.

CIRCLE NO. 310

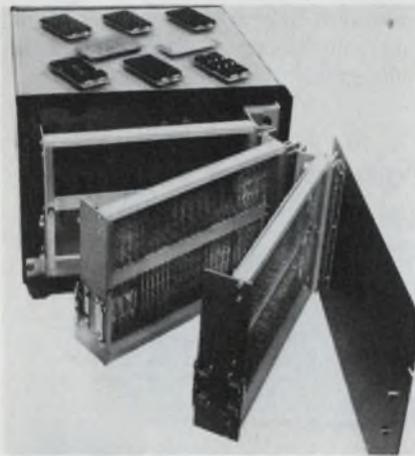
Plastic buttons replace screws and rivets

Richlok Corp., 5835 N. Tripp Ave., Chicago, Ill. 60646. (312) 539-4061.

A new line of Series MB rigid, natural-nylon, mounting buttons in 18 sizes for snap-in fastening applications can replace screws, nails or rivets. The buttons are offered in 0.37 and 0.48-in. holding widths that fit 0.156 and 0.187-in. dia holes. Each width is available in nine heights for thicknesses from 1/32 to 17/32 in. and in 1/16-in. increments.

CIRCLE NO. 266

DIPs packaged densely on page-hinged panels



Standard Logic Inc., 2215 S. Standard Ave., Santa Ana, Calif. 92707. (714) 979-4770.

The C-A-S-H page packaging system is compatible with standard 19-in. racks and cabinets and it features up to four mounting panels. The system is slide mounted and all the panels hinge like the pages of a book for convenient access to both the component and wiring sides of all panels. A single system with four pages can mount 160 C-A-S-H cards that can hold up to 4960 ICs. Input-output connectors are located adjacent to the panel hinges to permit minimum cable lengths. Other salient features of the packaging system include: over 100 cards with various combinations of DIP/IC sockets, I/O connectors and discrete component mounting provisions; large power capability with heavy-duty bus bars; and noise reduction features because of a laminated power-distribution plane that has high distributed capacitance.

CIRCLE NO. 267

Marking kit labels special panels

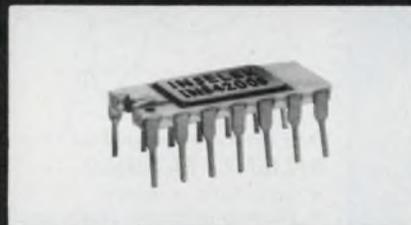


P. K. Neuses, Inc., Box 100, Arlington Heights, Ill. 60006. (312) 253-6555.

The Neuses' N-2315 numbering and lettering kit contains everything needed for the permanent marking of panels, junction boxes, subassemblies and chassis. The kit is intended for marking those few-of-a-kind assemblies; it is not intended for production marking. It comes in a steel carrying case and replacement supplies are available.

CIRCLE NO. 268

LOWEST POWER, HIGHEST SPEED 256 BIT SOS/ CMOS RAM IN THE INDUSTRY. IT'S HARD TO BE MODEST.



Our 256x 1 bit RAM is fully compatible with other CMOS & TTL devices. Its 26mW operating power dissipation & 140nS write, 180nS read cycle offer you the most optimum combination of speed and power available in the industry. This makes our INS42C0S ideally suited for use in scratch pad, buffer and main memory applications where high speed and low power are required.

Other features include: 5-15 volt supply range, full address decoding and bipolar compatible Pin-Cuts in 16 pin DIP.

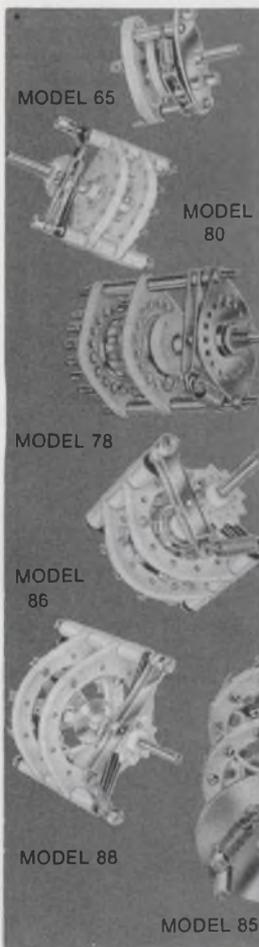
Available immediately in sample quantities, the INS4200S is priced at \$26 in quantities of 100-999.

For some immodest information call or write: Inselek, Inc., 743 Alexander Road, Princeton, N.J., 08540 (609) 452-2222.

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For RF and POWER APPLICATIONS

RSC switches are available in a variety of switching models. RSC high precision, quality built units are designed for applications requiring long life maintenance-free service. Types include shorting and non-shorting, single and multi-deck, up to 18 pole positions. Features include, 10 to 100 amp current carrying capacity, 20° to 90° detents, 2000 to 24000 volts flashover and corrosion-proof construction.



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and complete information.
RADIO SWITCH CORPORATION
Rt. 79, Marlboro, N. J. 07746

INFORMATION RETRIEVAL NUMBER 42

COMPONENTS

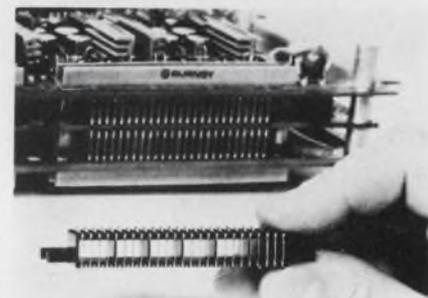
Rotary transducer has absolute output

Astrosystems, Inc., 6 Nevada Dr., Lake Success, N.Y. 11040. (516) 328-1600.

Up to 4000 BCD counts (0.1 degree) or 12 binary bits per revolution can be absolutely encoded with Model ST-11E transducer, which measures 1.062 D by 2 L in. and weighs only 4 oz. Every position of the transducer has a unique output that is instantly recoverable, should the system lose power. The transducer is a single-turn device, needs no adjustment or maintenance and operates over a temperature range of -20 to 85 C. Starting torque is 0.07 oz-in., maximum operating speed is 1200 rpm and maximum slew-speed is 3000 rpm.

CIRCLE NO. 269

Point contact replaces gold in board connector



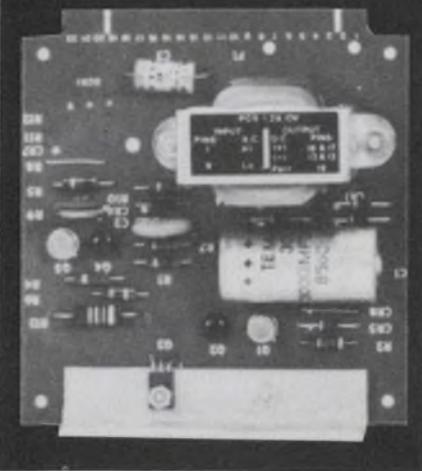
Burndy Corp., Richards Ave., Norwalk, Conn. 06856. (203) 838-4444.

Many connector makers have tried to substitute nonprecious metals for gold, but the replacements have often proved unreliable. The secret of Burndy's success with its GTH (gas-tight high-pressure) design is in its geometry. Concentration of the contact's spring force on a sharply pointed tip, causes the contact material to flow or extrude. This breaks down tarnish and corrosion films to establish fresh metal-to-metal junctions. Contact resistance with GTH is commonly as low as with gold—sometimes lower, according to Burndy. One GTH connector design connects a small circuit board to its master board with an easy push instead of with the use of a conventional gold-plated edge connector.

CIRCLE NO. 270

The tough little competitor can deliver. Fast.

Call us on your OEM power supply requirements.



Typical Specifications — PC Series
\$22.00 (10-99 unit quantity)

Input:	105-125VAC, 60 to 400 Hz
Line Regulation:	±25MV. Max.
Load Regulation:	±25MV. Max.
Ripple & Noise:	10MV. RMS Max.
Stability:	±5MV. After warm up.
Temperature Coefficient:	±2.5MV/°C
Operating Temperature:	-20°C to +71°C.
Storage Temperature:	-20°C to 85°C



Mighty Mouse © Viacom International

SALIENT FEATURES

- exceptional reliability
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- packaged for computer peripheral equipment
- meets U.L. and C.S.A. requirements

All standard supplies available in both discrete and I.C. versions. Liberal mix or match discounts available. All AMPSCO products are backed by unconditional 10-year guarantee.

Power Supplies by



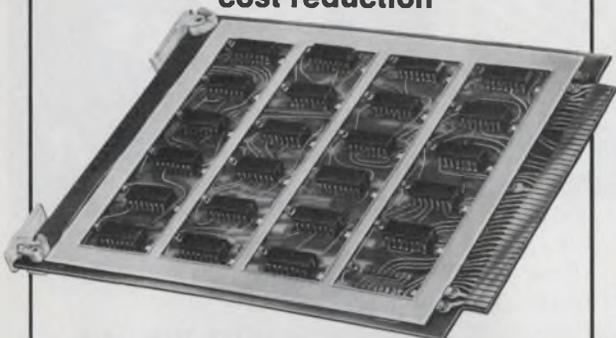
A Tough Little Competitor

American Power Systems Corp. • 51 Jackson St. • Worcester, Massachusetts 01608 • (617) 753-8103

INFORMATION RETRIEVAL NUMBER 43

Mini Bus[®] by Rogers

For noise and
cost reduction

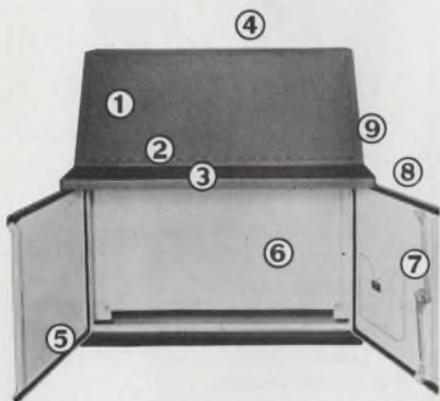


A small, voltage-distributing busbar for PC card application, each Mini/Bus gives you built-in capacitance . . . noise-cutting capacitance that means more reliable, compact circuit packaging at a fraction of multilayer prices. Write for data.



Rogers Corporation / Rogers, Conn. 06263

INFORMATION RETRIEVAL NUMBER 44



1. 24", 36", 48", or 60" width. 2. Hinged sloping control panel. 3. Optional writing desk. 4. Instrument panel top available. 5. Neoprene gaskets for complete oil tightness. 6. Accessory subpanel. 7. Three-point latches and key-locking handles. 8. Doors on both front and back. 9. All seams continuously welded. 10. NEMA-12 construction. 11. Many modifications available. Write for Bulletin C-14.

ENCLOSURES

Hoffman[®]

HOFFMAN ENGINEERING COMPANY
Division of Federal Cartridge Corporation
Anoka, Minnesota, Dept. ED52

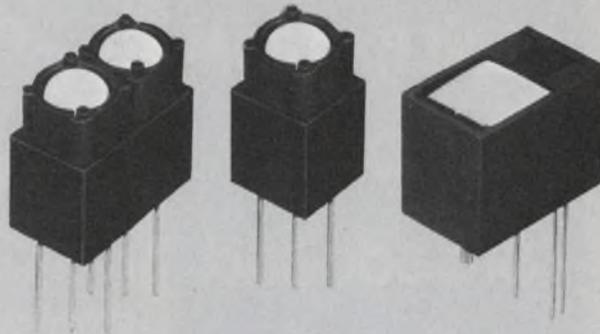
**ELECTRICAL
ENCLOSURES**

INFORMATION RETRIEVAL NUMBER 45

ELECTRONIC DESIGN 3, February 1, 1974



Light-Reflecting Electromagnetic Display Components



SERIES 32
0.3 inch (7.62 mm)
dual

SERIES 30
0.3 inch (7.62 mm)
single

SERIES 50
0.5 inch (12.7 mm)
single

STATUS INDICATORS

MEMORY — inherent remanent magnetism maintains the display state.

LOW POWER — one milli-watt second set/reset energy. Zero power to retain state. Drive voltages from 3-48 volts.

VISIBILITY — rotating fluorescent discs and flags provide excellent visibility over a wide range of ambient light conditions and wide viewing angles.

RELIABILITY — only one moving part rated for over 20 million operations. No lights or mechanical linkages to wear out. Virtually maintenance free.

FERRANTI-PACKARD STATUS INDICATORS

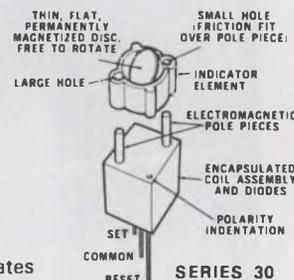
Ideal for

- Transient Recorders
- Industrial Process Displays
- Contact Status Indicators
- High Density Matrix Displays
- Portable Field Equipment.

Fluorescent discs and flags available in a range of colors.

The electromagnetic operation requires zero energy to maintain status.

Unique memory retention eliminates the need for memory circuits and reduces power supply and circuitry costs. Indicators are fully operational over a wide range of environmental conditions.



Ferranti-Packard's status indicators are light weight (Series 30, 0.17 oz (5 grams)) and are ideal for mounting on printed circuit boards and high density matrices.

For full information and specifications, contact the Display Components Department.

FERRANTI-PACKARD LIMITED

ELECTRONICS DIVISION
121 Industry Street,
Toronto, Ontario, M6M 4M3, Canada.
Telephone: (416) 762-3661.
Telex: 06-22007.

7304

INFORMATION RETRIEVAL NUMBER 46



THE NEXT GENERATION OF Broadband Power Amplifiers Starts with The **jsi** M403



.01-250MHz
100W min.
50db gain

**SMALLER
LIGHTER
QUIETER**

**DESIGNED FOR RELIABILITY
AND
EASE OF MAINTENANCE**

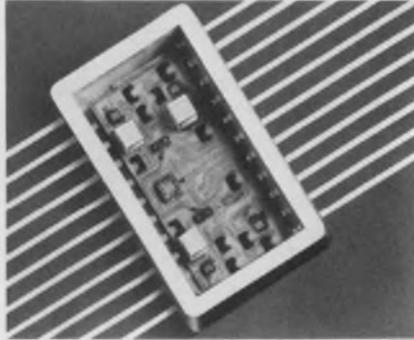
Solid State protection and control circuitry with complete remote control capability. *Write or Call.*

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INFORMATION RETRIEVAL NUMBER 47

COMPONENTS

Capacitors to 3.7 μ F
fit hybrid packages

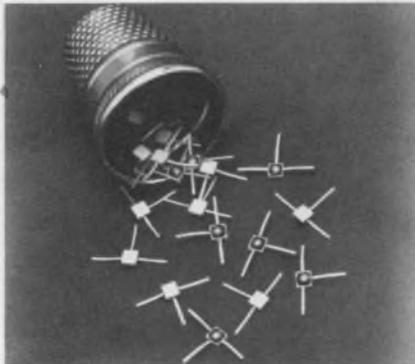


Johanson, Monolithic Dielectrics Div., Box 6456, Burbank, Calif. 91505. (213) 848-4465. 10 wk.

New extended-range ceramic chip capacitors feature capacitances of 1 pF to 3.7 μ F in seven standard sizes. The smallest size is 0.040 L \times 0.030 W \times 0.015 T in.

CIRCLE NO. 271

Small tantalum-film
resistor handles 1/4 W



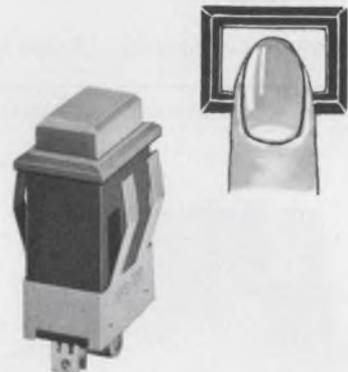
TRW/IRC Resistors, P.O. Box 887, Burlington, Iowa 52601. (319) 754-8491. \$0.58 (10,000 up); 4 to 8 wks.

These Tanfilm 1/4-W dual-resistor networks provide high component density. They consist of two tantalum-film resistors on a 0.075 \times 0.075-in. ceramic chip. The resistors' three-leads provide values of 1/2R, R or 2R. The resistance range is 20 Ω to 20 k Ω for the series combination with a tolerance of \pm 5%. Power is rated 0.25 W at 70 C and the temperature coefficient is -100 ± 25 ppm/ $^{\circ}$ C. Tantalum-nitride film is deposited on a 25-mil thick chip and protected by an epoxy coating. Gold-plated-copper leads are bonded to termination pads on the chip. Leads are planar configured and can be formed for PC-board insertion.

CIRCLE NO. 272

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finger?

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**LIGHTED PUSH-
BUTTON SWITCH**
SERIES LPS-100



(Actual size)

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- Snap-lock mounting.
- Matrix mounting is available.
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- Clean Color Button—Transparent cap with white diffusion filter. —Permit insertion of film with any LOGO or picture.
- Front lamp replacement.

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TOKYO, JAPAN

INFORMATION RETRIEVAL NUMBER 48
ELECTRONIC DESIGN 3, February 1, 1974

Keyboard assembly provides switching feel

Chromerics, 77 Dragon Court, Woburn, Mass. 01801. (617) 935-4850.

The ER family of keyboards features slightly convex key surfaces that deflect 0.035 in. under 4 to 6 oz of pressure. These keyboards provide the operator with a distinct feel of switch closure. They are available with 12 or 16 keys on 0.75 or 0.5-in. centers and a variety of formats and coded outputs. The ER switches have a life in excess of 10 million operations, a contact rating of 40 mA at 30 V, a contact resistance of 0.1 Ω and an operating temperature range of -40 to 180 F.

CIRCLE NO. 273

Switches made with a one-piece nylon toggle



Carlingswitch, Inc., Suite 800, 1428 Brickell Ave., Miami, Fla. 33131. (305) 358-5400.

One-piece nylon toggle G-Series switches eliminate the problem of the toggle separating from its pivot base. The pivot ball is reinforced with metal that adds strength to the fulcrum point and minimizes wear by providing metal-to-metal contact in the bushing. The nylon paddle toggle is available in a range of colors. The series has single and double-pole switches with both maintained and momentary contacts. Neoprene sealed bushings for marine and automotive applications are available.

CIRCLE NO. 274

NEWS
FROM
AIRPAX

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Airpax manufactures "passive" analog and "active" digital transducers (pick-ups) to provide the most effective and accurate means of converting mechanical motion into usable voltage control signals...without mechanical linkage. These magnetic pick-ups operate by accurately detecting moving ferrous discontinuities. Want to know more about pick-ups?... How is the selection made? How does the gear or discontinuity affect the pick-up output?

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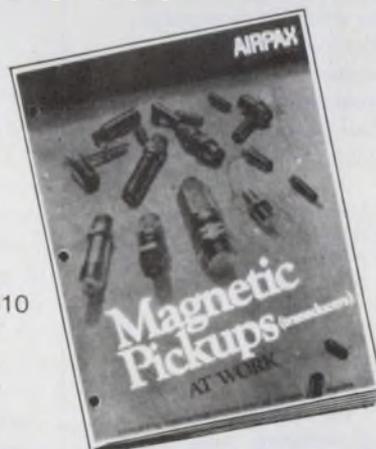
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INFORMATION RETRIEVAL NUMBER 49

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New from General Electric — an axial leaded, all welded tubular capacitor meeting the high CV small case size requirements of today's transistorized electronic equipment. Excellent for industrial and entertainment applications requiring maximum capacitance with limited space. Quality constructed for long life and high reliability, the 84F capacitor offers these features:

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- High ripple current capacity
- 1,000 hour life rating at 85 C
- Wide range of case sizes and voltages

For more information on these, or any of General Electric's wide range of capacitors, call your nearest GE sales office today, or write Section 430-54, Schenectady, N. Y. 12345.

MAKE SOMETHING OUT OF IT!

GENERAL  ELECTRIC

INFORMATION RETRIEVAL NUMBER 50

INSTRUMENTATION

Tiny DMM uses throwaway battery



Dana Laboratories, 2401 Campus Dr., Irvine, Calif. 92664. (714) 833-1234. \$195.

The Danameter is a miniature, portable DMM with a 3-1/2-digit liquid-crystal display and automatic polarity. The 1-lb. unit draws only 1 mW so that the internal battery can be thrown away after about a year. Ranges include ac and dc V, ohms and dc current.

CIRCLE NO. 275

Communications counter meets FCC specs



Systron-Donner, 10 Systron Dr., Concord, Calif. 94518. (415) 682-6161. \$1095; 60 days.

This new 512-MHz Frequency Counter, Model 6252, is designed for monitoring and measuring frequency carriers in the mobile communications bands. Input sensitivity of the unit is 25 mV rms to 50 MHz and 50 mV rms for inputs above 50 MHz. The measurement is displayed on a solid-state 8-digit readout with leading-zero suppression. Included in the field-portable counter, designed to FCC requirements, are a level meter coupled to the input for indication of signal level, an overload relay circuit to prevent damage to the input when overloads occur, and a frequency multiplier with a phase-locked local oscillator.

CIRCLE NO. 276

Pocket logic tester diagnoses ICs



Fluke Trender, 500 Clyde Ave., Mountain View, Calif. 94040. (415) 965-0350. \$395; stock.

A new hand-held instrument for testing ICs in-circuit is called the Model 200 IC TESTCLIP. The unit combines a logic probe, a logic clip and a logic comparator. The TESTCLIP automatically powers itself from the board it is checking. Truth-table or state behavior that differs from a reference IC, plugged into the case, is detected and displayed as a node failure at the failing pin number of the IC. A 16-position switch on the TESTCLIP's body enables the instrument to act as a logic probe.

CIRCLE NO. 277

Digital thermometer offers two ranges

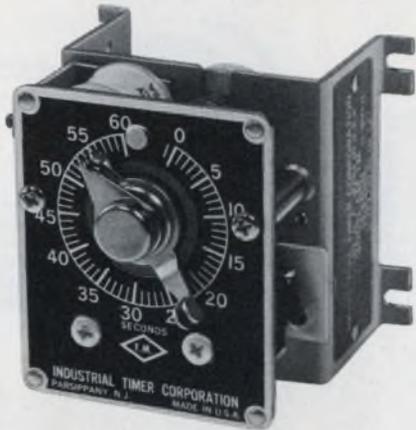


Hewlett-Packard, 1501 Page Mill Rd., Palo Alto, Calif. 94304. (415) 493-1501. \$700 (w/o probe); stock.

Model 2802A platinum resistance digital thermometer has two ranges: from -200 to +600 C, with a resolution of 0.1 C, and from -100 C to +200 C with a resolution of 0.01 C. Accuracy over both ranges is $\pm 0.5 C \pm 0.25 \%$ of reading. A linear analog output is standard. The unit operates within its rated accuracies over ambient conditions from 0 to 55 C and relative humidity to 95% at 40 C.

CIRCLE NO. 278

FOR THE UTMOST IN RELIABILITY



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It is one of industry's most versatile compact delay timers, offering dial adjustability, automatic reset, external clutching and 10 amp. SPDT snap action load contacts. Repeat accuracy is 1 1/2%. Resets in 1/2 second at maximum settings. Voltages: 120, 240/50-60 hertz. All of our timers are made to give you service far beyond what you'd reasonably expect. Our line consists of 17 basic types, each available in various mountings, voltages, cy-

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INFORMATION RETRIEVAL NUMBER 51

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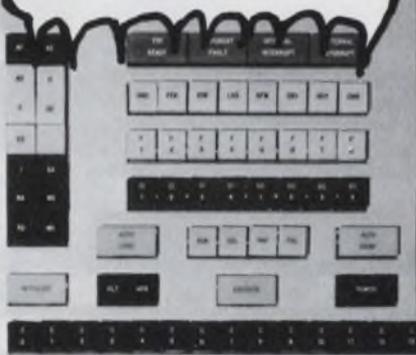
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INSTRUMENTATION

Level meter covers 17-MHz range

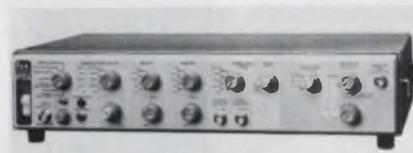


Siemens, 186 Wood Ave. S., Iselin, N.J. 08830. (201) 494-1000. D 2006: \$6550; W 2006: \$5450; stock.

The D 2006 L5 selective level meter has two calibrated film scales for accurate frequency tuning. The entire 17 MHz are continuously tuned without range switching and can be phase locked in 100-kHz increments. Within this range, the other scale fine tunes within 100 kHz. Frequency accuracy is 2×10^{-5} with level accuracy at ± 0.1 dB over-all. Sensitivity is -120 dBm.

CIRCLE NO. 279

50-MHz pulser sells for \$875

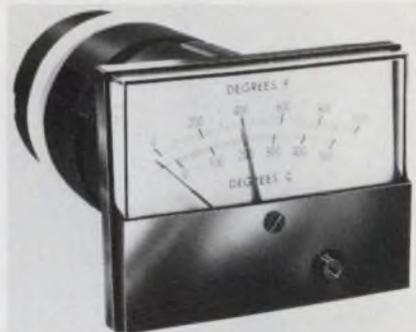


Interstate Electronics, 707 E. Vermont Ave., Anaheim, Calif. 92803. (714) 772-2811. \$875; 30 days.

P24 pulser is the newest addition to the company's SERIES 20 line. The unit offers all the specs and modes of the 50-MHz P23 and P25 but differs in output. The other SERIES 20 pulse generators provide positive/negative dual outputs with full offset to generate direct and complementary pulses. P24, basically a single-output version of the P25, at a 20% price reduction, offers single-channel selectable positive/negative pulses, full offset, and adjustable rise/fall to 5 ns, with independent rise and fall controls variable as much as 100:1.

CIRCLE NO. 280

Meter relays use battery power

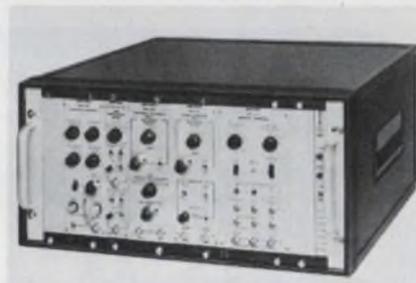


General Electric, 727 Lynnway, Lynn, Mass. 01910. (617) 594-5547. \$115 (100); approx. 10 wk.

This new line of ultra-precise Type 195 and 196 meter relays and pyrometers are now available in dc-powered versions. Covering five power ranges, from 12 to 125 V dc, the new models offer all of the features of their ac-powered counterparts, and may be used with either batteries or generated dc power.

CIRCLE NO. 281

Signal averager displays real-time amplitude

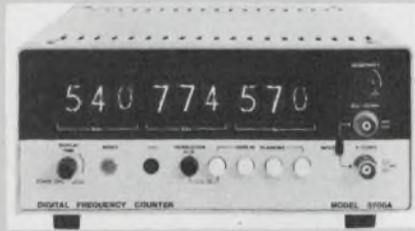


Ortec Inc., 203 Midland Rd., Oak Ridge, Tenn. 37830. (615) 482-4411. \$2915.

The 4623/4620 signal-averaging system displays a true average at every sweep, so that you need not count and then divide by the number of sweeps. The noise level can actually be watched receding on each successive sweep. The true signal amplitude can be read on a calibrated scope screen at any given time. As soon as the signal emerges clearly above the noise, averaging can stop and a permanent recorder or photographic record can be made. Heart of the signal-averaging system is the 4620 memory control, a 256-data-point MOS memory with 128 addresses and circuitry for control and readout.

CIRCLE NO. 282

The Ballantine 512 MHz DIGITAL COUNTER



The 5700A Frequency Counter. Range 10 Hz to more than 512 MHz. Nine digit display. Carrier measurements to 1 Hz resolution in 2 seconds of keyed transmitter time. Selective signal tone checks to 0.1 Hz resolution. Sensitivity 10 mV rms with AGC. Stability $3/10^7$ /month. $3/10^9$ /day optional.

- HIGHEST SENSITIVITY
- BEST RESOLUTION
- FASTEST COUNT RATE
- LOWEST PRICE **\$895**

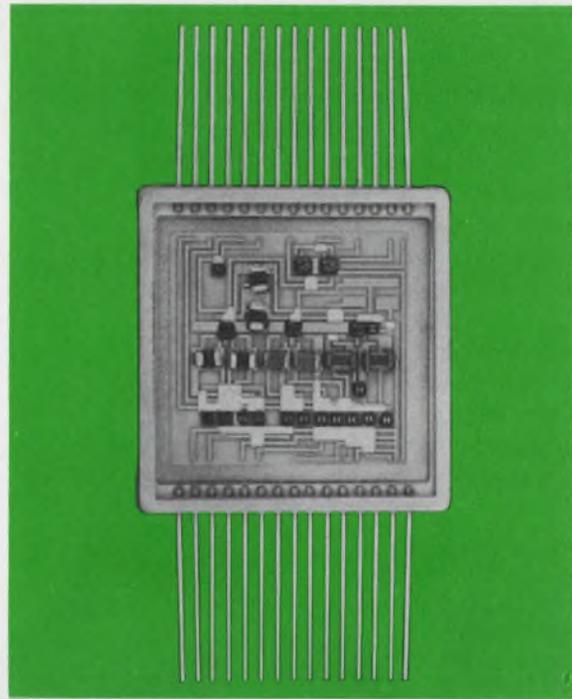
\$895

Meets FCC Requirements



Ballantine Laboratories, Inc.
P.O. Box 97, Boonton, New Jersey 07005
201-335-0900, TWX 710-987-8380

INFORMATION RETRIEVAL NUMBER 55



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ELECTRONIC DESIGN 3, February 1, 1974

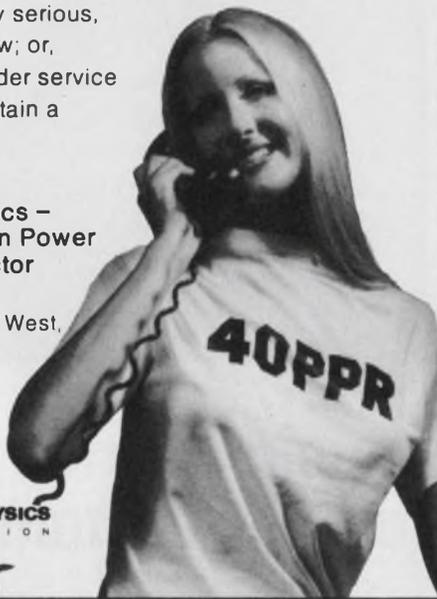
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If you're really serious, call Kathy now; or, circle the reader service number to obtain a data sheet.

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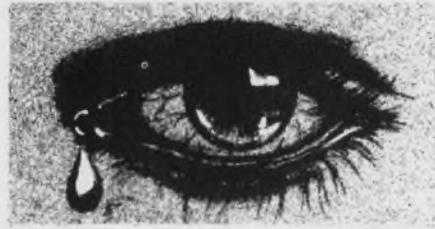
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RS-51

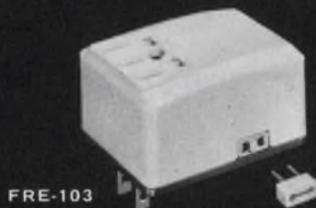
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INFORMATION RETRIEVAL NUMBER 60

ALCOSWITCH

REMOTE CONTROL RELAY

SPDT Relay plugs directly into AC outlet. Side receptacle accepts remote switch. Available N.O. or N.C. No additional wiring necessary. Operates on 117 VAC.



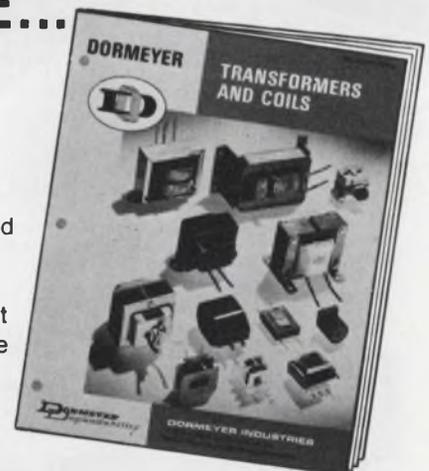
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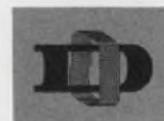
INFORMATION RETRIEVAL NUMBER 61

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INFORMATION RETRIEVAL NUMBER 62

ELECTRONIC DESIGN 3, February 1, 1974

Log amplifiers cover 80 dB dynamic range

Varian, Solid State East, Salem Rd., Beverly, Mass. 01915. (617) 922-6000. \$525.

The ITL-7 detection and video i-f amplifiers provide an input dynamic range of -80 to 0 dBm and log accuracy of ± 1 dB with operating frequencies of 30, 60, 70 or 160 MHz. They also have rise times as low as $0.03 \mu s$. The amplifiers are designed primarily for pulse or AM signals, but most can be supplied with dc coupled input to process cw information. Eight standard versions of the ITL-7 are available, as are special models having linear and limited i-f output. They can also be supplied as matched pairs with the log-video amplitude matched to input within 1 dB.

CIRCLE NO. 283

Adjustable-speed drives handle 1/4 to 3 hp

Cleveland Machine Controls, 7550 Hub Pkwy., Cleveland, Ohio 44125. (216) 524-8800.

The Series 50 adjustable-speed dc drives operate on 115/230 V, single-phase, 50/60 Hz. They include zero-overshoot current limiting, made possible by cascaded speed and current amplifier stages. Backup safety provisions include fast-acting line fuses or line circuit breakers, a control relay which prevents automatic restart after ac power interruption, plus suppressors for transient voltage and high-frequency electrical noise. Series 50 adjustable-speed drives are available in three basic models: Type O, an open chassis design that saves panel space for OEMs. Type P, that mounts directly on rear of equipment panel with speed pot, start and stop pushbuttons on front side and Type E, a nonventilated, totally enclosed unit offering protection against dust and oil—all models are available in 1/4 to 3 hp ratings, featuring nonreversing and coast-to-stop capability. Several off-the-shelf options are also available, such as tachometer feedback for 1% speed regulation and 100:1 range.

CIRCLE NO. 284

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BRUCE MYERS,
Senior
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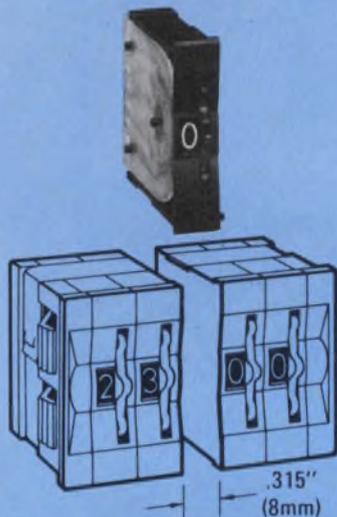
ECI is on Florida's West Coast in sunny, cosmopolitan St. Petersburg. If you're interested in a career opportunity on long-term programs in a stimulating environment, write in confidence today to William A. Peterson, Personnel Manager, Electronic Communications, Inc., Box 12248, St. Petersburg, Fla. 33733.

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INFORMATION RETRIEVAL NUMBER 63

MODULES & SUBASSEMBLIES

Audio amp accepts up to eight inputs



General Aviation Electronics, 4141 Kingman Dr., Indianapolis, Ind. 46226. (317) 546-1111. \$99.95.

The TAU/88 high power audio amplifier delivers 10 W of audio output power. The unit operates from 14 or 28 V dc and can handle eight audio inputs. It has built-in muting circuitry for fast, economical operation and good aircraft-generated noise rejection. The amplifier input impedance is 680 Ω , low level and 4 Ω , high level. Sensitivity for low levels is 1 V rms and the high level sensitivity is 5 W into 4 Ω . Power output for the 3.25 \times 2 \times 4.625 in module is 10 W at a supply voltage of 14 V dc and 16 W at 28 V dc. Output impedance stays between 3 and 6 Ω while input isolation is -50 dB.

CIRCLE NO. 285

V/f converter delivers 0.008% linearity

Intech, 1220 Coleman Ave., Santa Clara, Calif. 95050. (408) 244-0500. \$55 (1 to 9); stock.

The A-847 voltage-to-frequency converter has 0.008% linearity and an adjustable output frequency. It has input range of 0 to 10 V and output of 0 to 10 kHz. Guaranteed operating temperature range is -25 to +85 C. Package size is 1.125 \times 1.125 \times 1.4 in. The output is an uncommitted collector permitting interface with DTL and TTL logic families. Resolution achieved is equivalent to that of a 13-bit a/d converter. Serial output format allows for two-wire data transmission to magnetic tape or strip-chart recorders. Custom designs for other input voltages or output frequencies are also available.

CIRCLE NO. 286

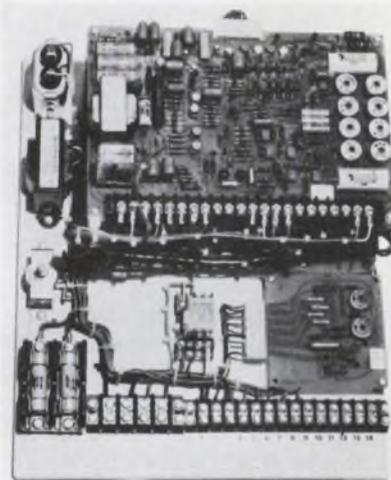
Wideband op amp needs only 55 mW

Optical Electronics, P.O. Box 11140, Tucson, Ariz. 85706. (602) 624-8358. \$41 (10 to 29).

The 9827 wideband low-power operational amplifier has differential inputs and a typical power consumption on ± 15 V supplies of 55 mW. It can operate from batteries with reduced voltage at less than 8 mW and maintain a 30 MHz gain bandwidth product. The 9827 is packaged in a 1.125 in. square by 0.44 in. high module and features: a ± 10 V/ μ s minimum slew rate, ± 10 V at ± 20 mA minimum output swing, ± 4 to ± 20 V power supply voltage range and -55 to +100 C operating temperature range.

CIRCLE NO. 287

Regenerative drive uses back-to-back SCRs



Cleveland Machine Control Inc., 7550 Hub Pkwy., Cleveland, Ohio 44125. (216) 524-8800.

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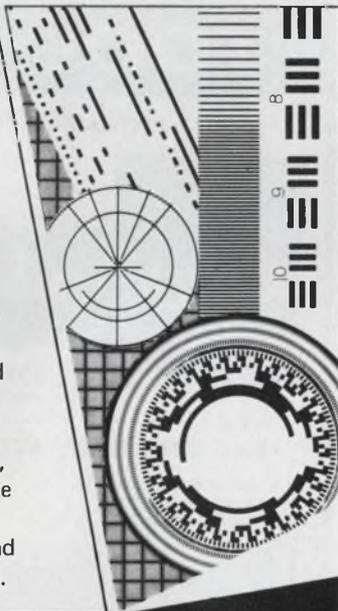
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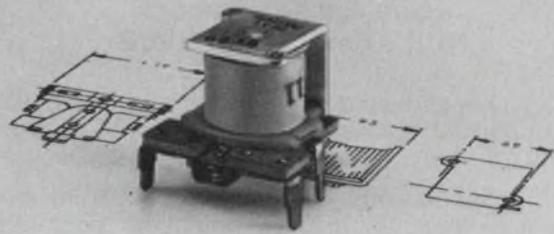
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INFORMATION RETRIEVAL NUMBER 65

ELECTRONIC DESIGN 3, February 1, 1974

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INFORMATION RETRIEVAL NUMBER 69

ELECTRONIC DESIGN 3, February 1, 1974

new literature



Data conversion products

A 40-page short-form catalog contains 17 new data conversion products along with electrical and mechanical specifications and over six pages of application information. Datel Systems, Canton, Mass.

CIRCLE NO. 289

Single-phase bridges

A series of bulletins describes single-phase bridges, doublers, center-tap and three-phase bridges. General Instrument, Hicksville, N.Y.

CIRCLE NO. 290

PM synchronous motor

A two-page data sheet highlights the Model 105 high-torque permanent magnetic synchronous motor with both mechanical and electrical control. Cramer Div., Conrac, Old Saybrook, Conn.

CIRCLE NO. 291

Test equipment

A four-page short-form catalog of electrical test equipment includes specifications and operating characteristics for insulation and dielectric breakdown testers, megohmmeters, electrostatic voltmeters, precision kV dividers and high-voltage power supplies. Also included are high-voltage connectors and switches, Wheatstone bridges and resistance decade boxes. Beckman Instruments, Cedar Grove, N.J.

CIRCLE NO. 292

Microwave power transistors

"Microwave Power Transistors," a 16-page brochure, contains basic design and application information on power transistors for microwave frequencies. RCA, Somerville, N.J.

CIRCLE NO. 293

Control knobs and switches

Panel knobs and miniature switches are featured in two catalogs. Raytheon, Waltham, Mass.

CIRCLE NO. 294

Sockets and heat sinks

An 84-page catalog describes and illustrates many types of sockets, heat sinks, washers, mounting pads and heat pipes. Prices are given. Jermyn, San Francisco, Calif.

CIRCLE NO. 295

Mixers and rf transformers

A 52-page catalog provides data on double-balanced mixers, power splitter/combiners and rf wide-band transformers. The catalog includes definition of terms, reliability considerations, applications, specifications and 365 performance curves. Mini-Circuits Laboratory, Brooklyn, N.Y.

CIRCLE NO. 296

Microcircuit equipment

A 24-page catalog includes data and pricing for such microcircuit equipment as screen printers, substrate cutoff equipment, substrate drills, diamond scribes, diamond wheels, vacuum encapsulators and furnaces. Aremco Products, Ossining, N.Y.

CIRCLE NO. 297

Consoles and cabinets

Standard cabinets, monitoring consoles, small instrument cabinets, poly-dimensional instrument/control cabinets are some of the styles illustrated in a 22-page catalog. AMCO Engineering, Chicago, Ill.

CIRCLE NO. 298

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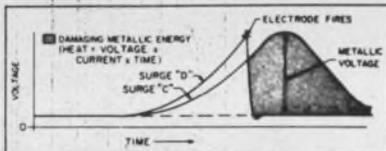
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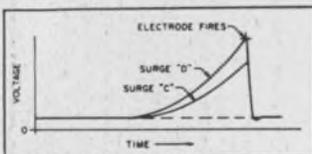


Model 16 (left) is used in all TII Surge Protectors such as Model 316 shown.



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"Visual Communications" describes state-of-the-art features that make CCTV equipment ideal for a variety of applications. The 12-page color brochure covers equipment needed for an effective CCTV installation from low-light-level and high-resolution cameras to video monitors, camera control consoles and other video accessories. Motorola, Schaumburg, Ill.

CIRCLE NO. 299

Cable ties

Cable ties, clamps, marker ties, push-mount ties and lashing ties are described in an eight-page brochure. Panduit Corp., Tinley Park, Ill.

CIRCLE NO. 300

Tracking adaptor

Model SAI-502 tracking adaptor, for use with the company's real-time spectrum analyzer/digital integrator, is featured in a two-page bulletin. Features are listed along with a description of controls and indicators, operational specifications and a block diagram. Honeywell, TID, Signal Analysis Operation, Hauppauge, N.Y.

CIRCLE NO. 301

Integrated packaging

An integrated socket packaging brochure provides the basis for a new concept of electronic packaging. The brochure describes the integrated socket and its supportive hardware, plus outlines on how to work with this concept in a design project. Cambridge Thermionic, Cambridge, Mass.

CIRCLE NO. 302

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INFORMATION RETRIEVAL NUMBER 74

ELECTRONIC DESIGN 3, February 1, 1974

bulletin board

An a/d and d/a converter applications contest has been announced by Micro Networks. The company will reward the most original, complete, and useful application submitted using these devices with a \$1000 U.S. savings bond. Several electronic calculators will be given as runner-up prizes. The contest ends Feb. 15, 1974.

CIRCLE NO. 303

Plessey Semiconductors has introduced a series of vhf frequency dividers, operating at input frequencies to 350 MHz and consuming half the power of comparable devices.

CIRCLE NO. 304

Improvements in execution time by factors of 2 to 28 can be demonstrated for FORTRAN with Hewlett-Packard's 2100 minicomputers. Twelve of the most-often used FORTRAN subroutines are implemented in a 196 ns microcode with the 1290A Fast FORTRAN Processor (FFP). This plug-in package is priced at \$1250.

CIRCLE NO. 305

Electronics interfacing CDC 1700 computers and the company's 6600 television display system have been introduced by Data Disc.

CIRCLE NO. 306

The models Am 8820/20A and Am 8830, high-speed differential line drivers and receivers—pin replacements for similar devices from Texas Instruments and National Semiconductor—are available from Advanced Micro Devices.

CIRCLE NO. 307

Teledyne Semiconductor has announced that 25 popular JFET types are available in the TO-92 package in volume quantities. TO-92 part types include the 2N5457-59, 2N5484-86, 2N5555, 2N5638-40, 2N5653 and 54 and 2N5668-70. Other types are the MPF102 and MPF111 series.

CIRCLE NO. 308

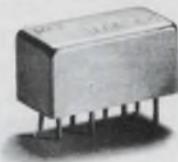
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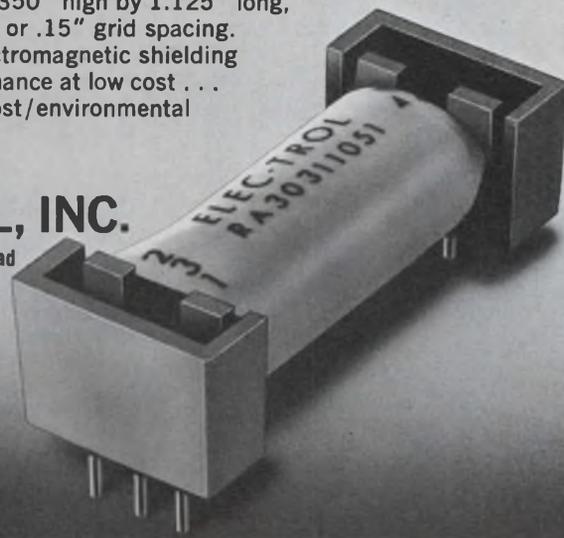
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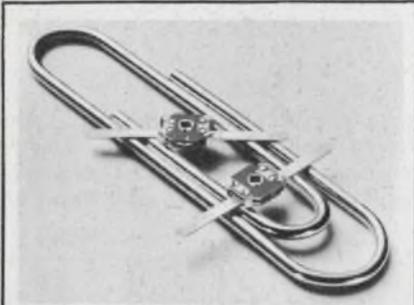
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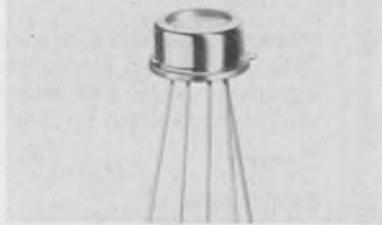
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Thin-Trim variable capacitors provide a reliable means of adjusting capacitance without abrasive trimming or interchange of fixed capacitors. Series 9401 has high Q's and a range of capacitance values from 0.2-0.6 pf to 3.0-12.0 pf and 250 WVDC working voltage. Johanson Manufacturing Corporation, Boonton, New Jersey (201) 334-2676.

INFORMATION RETRIEVAL NUMBER 181

UDT PHOTOPS 600



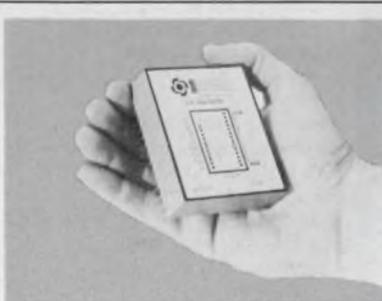
UDT PHOTOPS 600 high speed detector/amplifier combination has response to 10 megahertz with sensitivity to 5×10^{-12} watts. All PHOTOPS utilize latest FET circuitry and are available to 1cm^2 active area. PHOTOPS may be used as replacements for photomultipliers. United Detector Technology, Inc., 1732 21st Street, Santa Monica, CA

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400 Ideas for Design, Vol. 2, Edited by Frank Egan. Ready to borrow, modify, or adapt, the top recent contributions to Electronic Design's popular "Ideas for Design" column range from amplifiers to switching circuits. 288 pp., illus., cloth, \$11.95. Circle below for 15-day examination copies. Hayden Book Co., New York, N.Y. 10011

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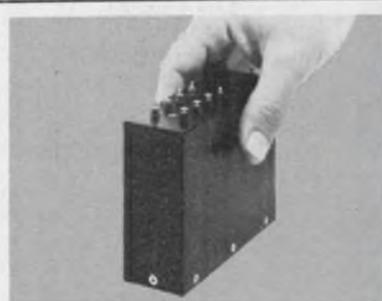
"Synchro to digital converters - 10, 12, or 14 bit output, errorless tracking up to 4 r.p.s., accuracy ± 4 min. of arc $\pm .9\text{LSB}$, resolution - 1.3 minutes, 60 or 400 Hz input, Module 2.6 x 3.1 x .82" H, Price From \$350 in qty. Computer Conversions Corp., East Northport, N.Y. 11731 (516) 261-3300."

INFORMATION RETRIEVAL NUMBER 184



Electric contact lubrication and oil creep control with special aerosols. NYETACT 505 reduces wear and noise on sliding contacts, incl noble metals. NYETACT 510 prevents tarnish, reduces wear on stationary separable contacts. NYE-BAR-F prevents oil creep onto contacts. Wm. F. Nye, Inc., Box G-927, New Bedford, Mass. 02742. (617) 996-6721.

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Big power supply for little spaces. 115 VAC, 50-500 Hz input. 1 to 6 isolated & regulated DC outputs. 120 W per output. 3.9 W delivered per cu. in. Modular construction lets you "Design-As-You-Order". Over 1200 configurations using off-the-shelf modules. Immediate deliveries! Arnold Magnetics Corp., Culver City Ca. (213) 870-7014.

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product index

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There's still time to enter *Electronic Design's* 1974 Top Ten Contest. You can win a free Windjammer Cruise in the Caribbean . . . \$1,000 in cash . . . free jet transportation . . . color TV . . . Bulova electronic timepieces . . . free ad reruns. There are 100 prizes in all!

Complete information and rules appeared in the Jan. 4 issue. Dig out your Jan. 4 copy and enter the contest now. (If the entry cards are all torn out, you can use the form that is printed below.) Entries must be postmarked before midnight, February 15.

DO NOT SELECT ADS FROM THIS ISSUE — USE ELECTRONIC DESIGN ISSUE NO. 1 — THE TOP TEN CONTEST ISSUE — PUBLISHED JANUARY 4, 1974



1974 SUPER TOP TEN CONTEST

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I have read all of the rules and estimate that the "Top Ten" advertisements receiving the highest Reader Recall "Percent Seen" scores in the January 4, 1974 issue will be:

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Clip and mail to: Top Ten Contest, c/o Electronic Design,
50 Essex Street, Rochelle Park, New Jersey 07662.

Cinch Dura-Con 0.050" centers Small. Dependable. Available.



Now you have an effective source for your micro-miniature connector needs. Cinch can produce and deliver these rugged reliable connectors on a timely basis, with size 24 contacts on 0.050" centers.

These connectors utilize the proven pin-socket contact system, where the pin, made from a precision spring cable, is the spring member. The seven cable strands are fused in a hemispherical weld, resulting in a strong flexible shock and vibration resistant contact with assured alignment and no discontinuities.

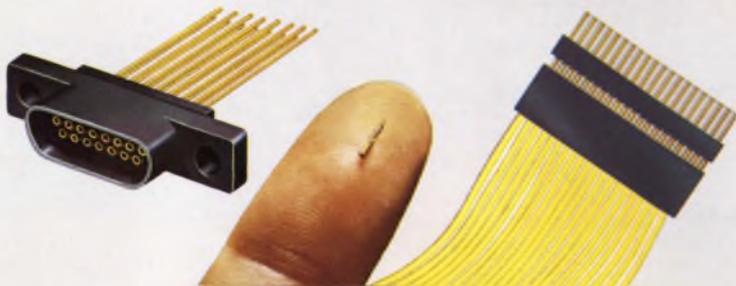
The Dura-Con pin is available in five sizes of Dura-

Con D-configurations as well as single row strip configurations. It can also be supplied in custom insulators.

The size 24 contacts with 0.050" centers are supplied factory terminated, with pigtail or wire leads. Size 22 contacts, on 0.075" and 0.100" centers, are crimp removable.

Cinch Dura-Con Micro-Miniature Connectors are described in Bulletin PBC-174, available from Cinch Connectors, an Electronic Components Division of TRW Inc., 1501 Morse Avenue, Elk Grove Village, Illinois 60007, (312) 439-8800

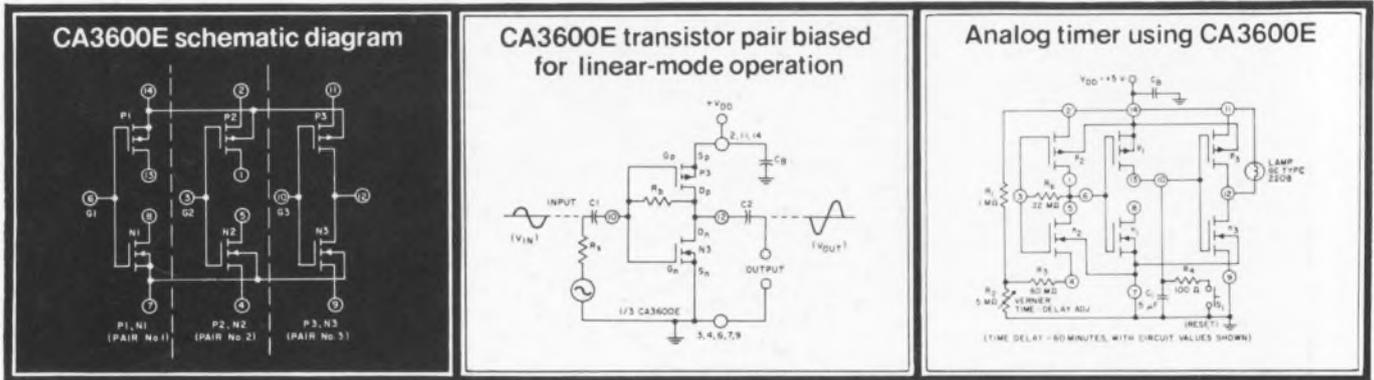
CM-7305



TRW CINCH CONNECTORS

INFORMATION RETRIEVAL NUMBER 245

Linear COS/MOS... RCA's CA3600E premieres



Meet the linear IC with the advantages of COS/MOS. The new RCA CA3600E Transistor Array... three pairs of complementary enhancement-type MOS (p-channel/n-channel) transistors on a single chip.

The CA3600E is designed for a great variety of applications requiring virtually infinite input impedance, wide bandwidth, matched characteristics, lower power consumption and general purpose circuitry.

And that's not all. With the new CA3600E you get performance advantages that include square-law characteristics, superior cross-modulation performance, and a greater dynamic range than bipolar transistors.

Whether you're working in timing, sensing and measuring or any other applications, or if you're tired of fighting beta variation in your bipolar circuit, let your "linear" imagination run wild. The features offered in the new CA3600E COS/MOS Linear IC

are too good to pass up.

- Virtually infinite input resistance/ 100 gigohms
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- Low gate-terminal current/ 10 picoamps
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- Matched p-channel pair/gate-voltage differential ($I_b = -100\mu A$) ... $\pm 20mV$ (max)
- Stable transfer characteristics over a temperature range of $-55^\circ C$ to $+125^\circ C$
- High voltage gain/up to 53dB per COS/MOS pair.

Supplied in the 14-lead dual-in-line plastic package, the CA3600E is available in production quantities from your local distributor or direct from RCA.

For complete data sheet/application note write: RCA Solid State, Section 57B-1, Box 3200, Somerville, N.J. 08876. Or phone: (201) 722-3200.

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