

Transducers get an uplift with new materials and circuitry. Their accuracy has improved and cost has dropped. Sensors measuring temperature, pressure, fluid flow

or other physical quantities use new active components. Solid-state circuits are now displacing simple passive transducers. For a look at what's new, see p.30.

94086CALC05B10N96 24/74 ED  
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SUNNYVALE CA 94086



# Can your resistors handle emergencies?

## Here's how to make sure:

When a resistor is confronted by a high energy pulse current, it should do one of two things: "Open"...in order to protect valuable circuit components or shrug off the pulse to assure that the circuit remains functional.

In a simple "open or shut" case like this, it's not hard to decide which choice is best for your product. But the going gets tougher when you try to match your "worst case" requirements with a resistor that's functional in performance, size and price. At this basic selection level, you often find you need to know a lot more about a resistor's emergency capabilities than most companies can tell you.

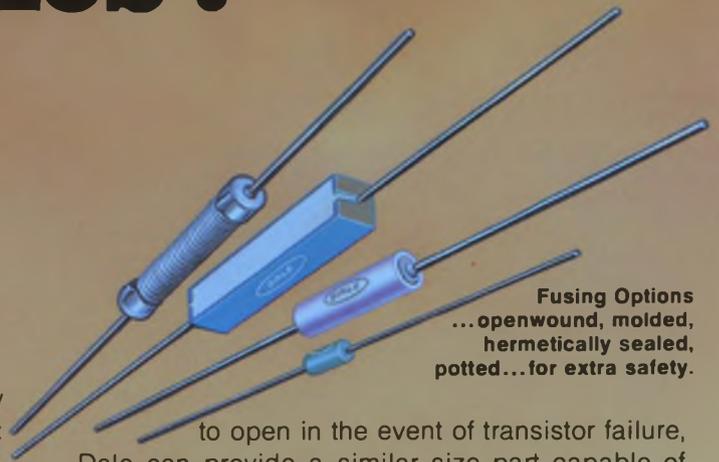
Which is why we get a lot of phone calls at Dale... and also why we've prepared some helpful new information on resistive pulse handling and fusing.

Let's say, for example, that you're planning to use one of Dale's 5-watt RS wirewounds in a transistor emitter circuit. These

new tables and formulas will show that it can

withstand millisecond pulses up to 24,000 watts! However, if you want the same circuit

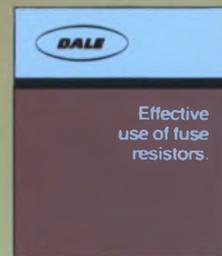
**24,000 Watts**  
...learn how to figure the pulse handling capability of your resistors.



**Fusing Options**  
... openwound, molded, hermetically sealed, potted... for extra safety.

to open in the event of transistor failure, Dale can provide a similar size part capable of opening in milliseconds at a pulse time/size level you specify.

This kind of "open or shut" option lets you be certain you're designing in the kind of extra protection that can make your products more valuable...and it's available throughout Dale's broad resistor line. Drop us a line or give us a call. In this sophisticated world, you'll be glad to find that someone is working at making the basics better.



*Write for these new publications.*

**DALE ELECTRONICS, INC.**  
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INFORMATION RETRIEVAL NUMBER 246



# SURPRISE!



**2½ times  
brighter green.**



**6 times  
brighter yellow.**



**6 times  
brighter red.**

HP brings you three new LED's that are many times brighter than our standard T-1 red lamps. All offer a 180° viewing angle, plus high axial luminous intensity and a good on-off contrast ratio. Ideal for front panel applications.

Our new green lamp (5082-4984) uses high-efficiency gallium phosphide to generate a typical luminous intensity of 2 mcd at 20 mA.

Our new yellow LED's are really yellow.

The 5082-4584 lamp offers 2.5 mcd typical at 10 mA.

And red has been dramatically brightened six times in output using non-saturating gallium arsenide phosphide. With a luminous intensity of 2.5 mcd at 10 mA our 5082-4684 high-efficiency red is unbeatable.

Just \$0.80\* in 100 quantities.

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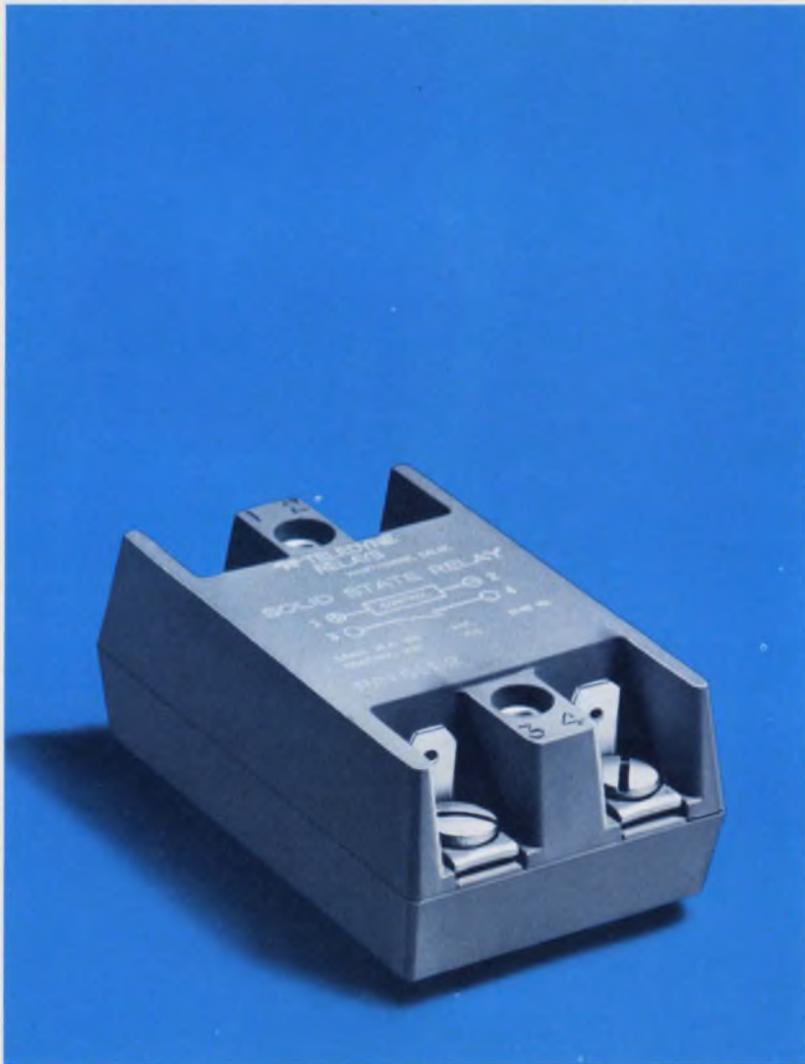
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INFORMATION RETRIEVAL NUMBER 2

# Solid state power

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Using sensitive low level IC logic to control brute force loads like motors, solenoids and actuators demands a whole new class of devices.

Teledyne, the world leader in solid state relays, introduces the 611. All the toughness of electromechanicals — 25 AMPS, 250 VAC rms; a THOUSAND PERCENT OVERLOAD surge rating on "contacts" for lamps and motor starting. All the sensitivity and quiet of good solid state design — compatible with TTL and most logic families (3-32VDC) the 611 will turn on with as little as 3VDC. TOTAL (optical) ISOLATION control to load; High Output Transient Immunity — 200V/ $\mu$ sec; zero voltage switching for RFI quiet; no arc or spark in explosive or hazardous environments.

All in a compact, functional and attractive package too — barriered quick disconnect and screw terminals and rugged case.

If you use or design for process or machine tool control, computer peripherals, business machines, or maybe traffic control systems — the Teledyne 611 can open up entirely new performance specs.

Ask your nearest Teledyne relay rep or call us direct for applications engineering help and immediate delivery.

 **TELEDYNE RELAYS**

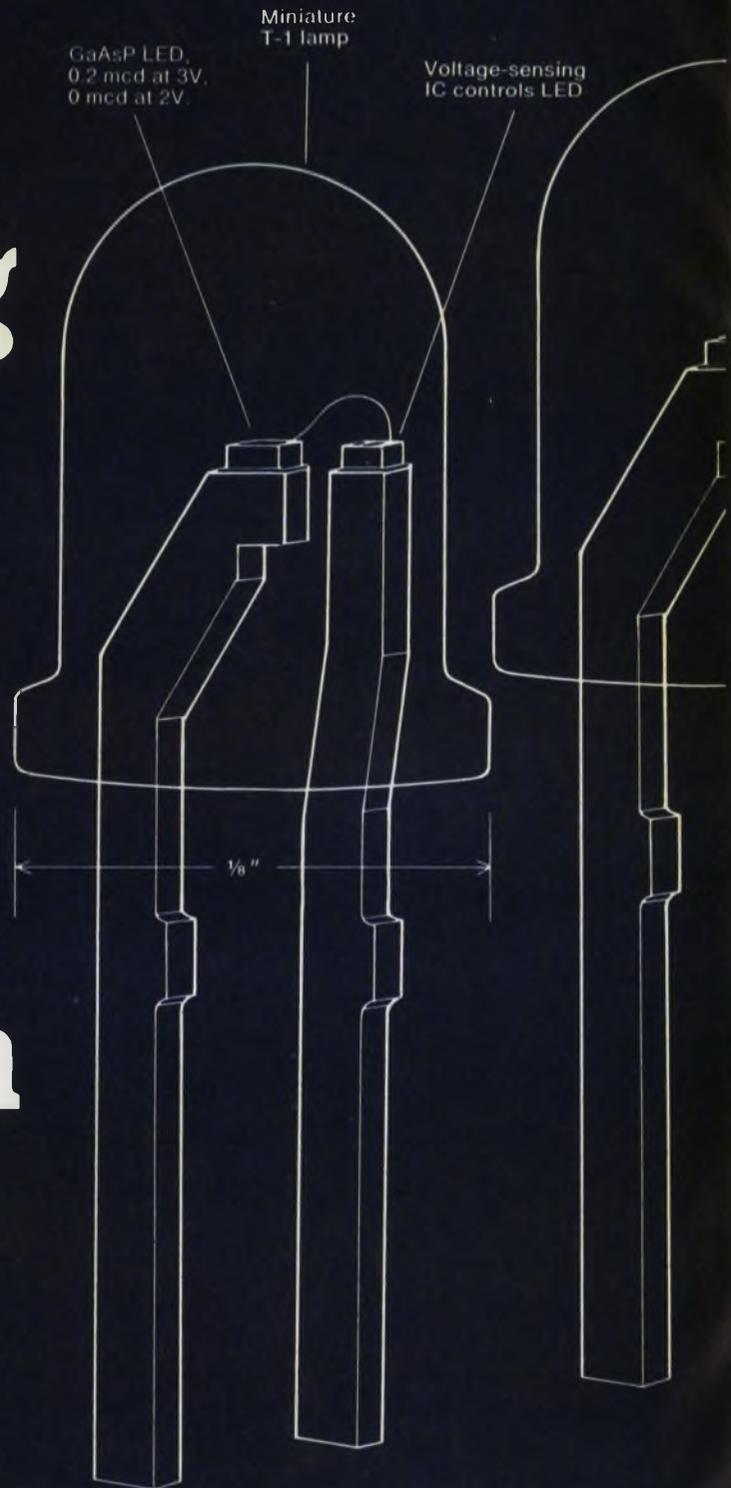
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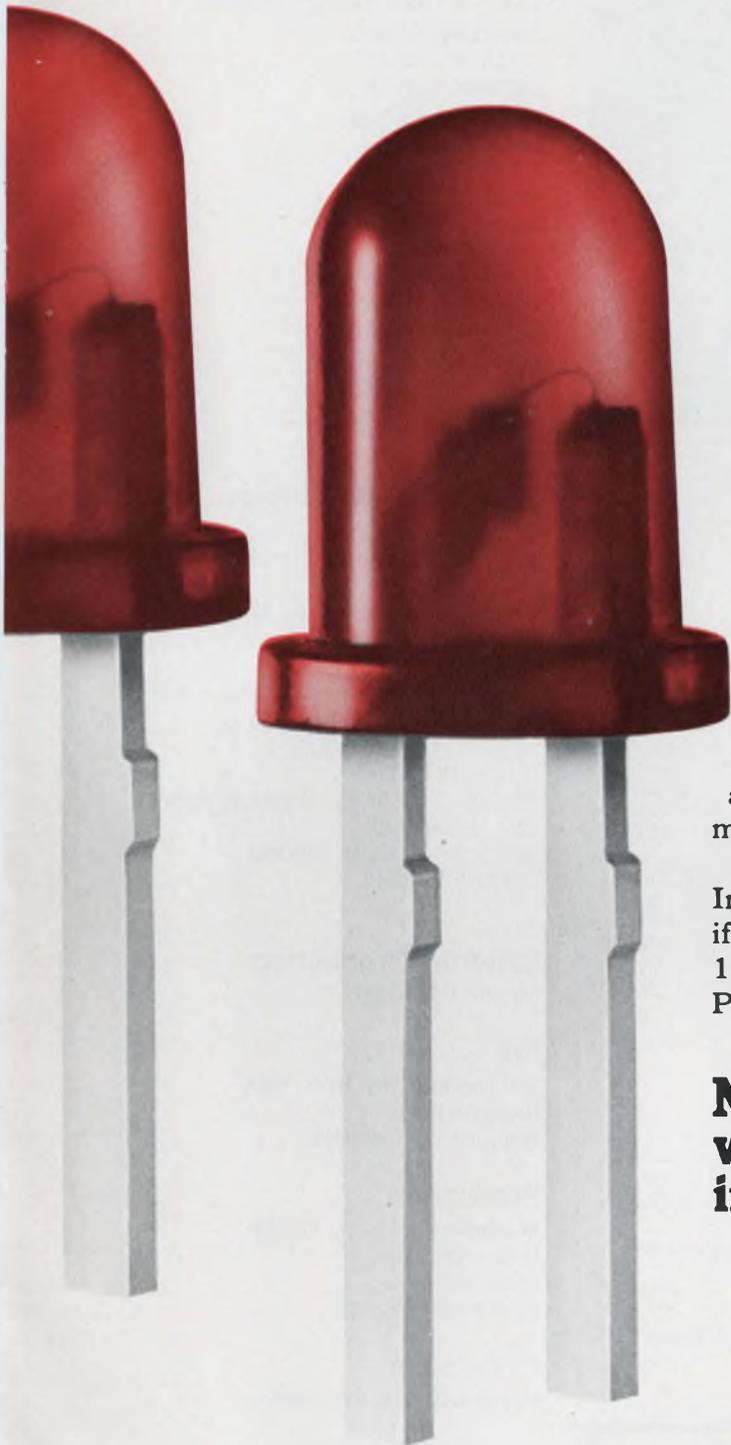
INFORMATION RETRIEVAL NUMBER 3

ELECTRONIC DESIGN 15, July 19, 1974



# Announcing the Battery Status Indicator— a new LED/IC combination





Dead batteries! Everyone hates 'em. And most battery powered equipment—cameras, tape recorders, calculators—don't warn you until it's too late.

Now Litronix—the world's largest manufacturer of LEDs—introduces the RLC-400 Battery Status Indicator. It's a red GaAsP warning light and voltage-sensing IC combined in one little T-1 lamp package. The light is on at 3V, off at 2V.

One of the nation's most prominent camera manufacturers uses it. Any battery-powered device that uses it may acquire an important competitive advantage at low cost.

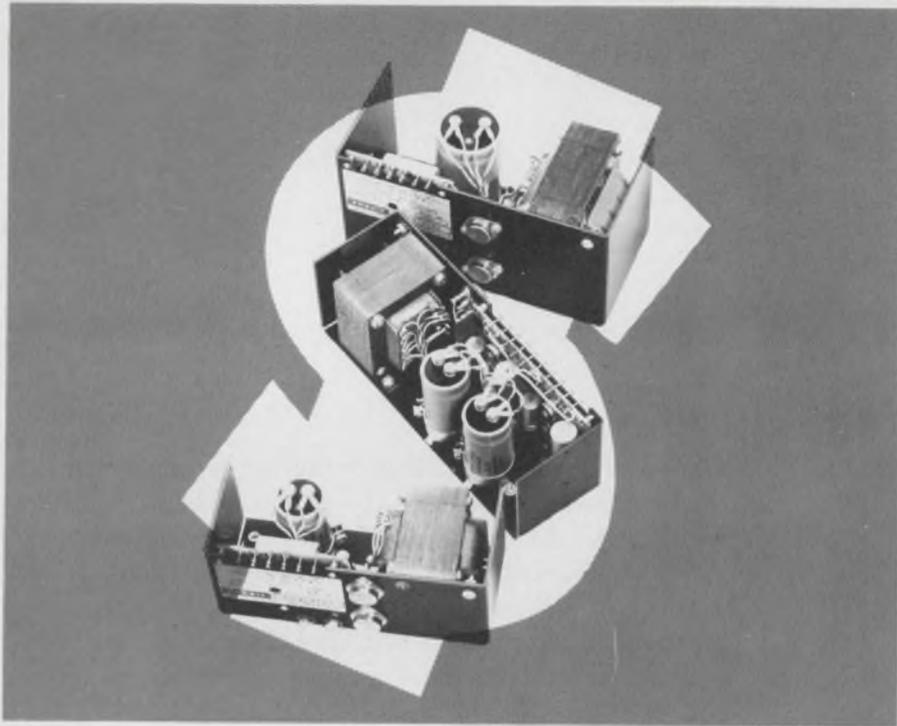
The Litronix Battery Status Indicator will cost you only 60¢ in quantities of 1000. And you keep production costs down because you don't have to test, assemble and inventory several components.

If you need a warning light that goes on and off at different voltages, get in touch with us. We may be able to help you.

You can get a free sample of the Battery Status Indicator by writing us on your company letterhead. Or if you want more information quick, contact Litronix, 19000 Homestead Road, Cupertino, California 95014. Phone 408-257-7910. TWX 910-338-0022.

**No wonder  
we're No.1  
in LEDs**

**litronix**



# Start Getting Your Money\$worth Out of Power Modules

Now, you can really start getting your moneysworth out of power modules with Abbott's new LOW COST series. Designed to give you 100,000 hours of trouble-free operation (that's 11½ years), these reliable units meet the needs of OEM engineers. Their purchase price is about \$7 per year of service. The model LC series feature:

- 47-420 Hz Input Frequency
- 0.1% Regulation
- +50°C. Ambient Operation
- Single and Dual Outputs
- 1 Day Stock Delivery

These units provide more quality per dollar compared to similar items on the market. See table below for prices on some of our LC models. Many other LC models are listed in our catalog.

If analyzing the many similar power supplies on the market is confusing; if you are concerned about the long-term reliability of those units, then decide on an Abbott power supply for your system. Your best buy in OEM power modules is ABBOTT.

Abbott also manufactures 3,000 other models of power supplies with output voltages from 5 to 740 VDC and with output currents from 2 milliamps to 20 amps. They are all listed with prices in the new Abbott Catalog with various inputs:

60  to DC  
 400  to DC  
 28 VDC to DC  
 28 VDC to 400   
 12-24 VDC to 60 

5V @ 6 Amps	5V @ 10 Amps	12V @ 10 Amps	15V @ 4 Amps	28V @ 1 Amp	±12V @ 1.2 Amps	±15V @ 4 Amps
LC5T6	LC5T10	LC12T10	LC15T4	LC28T1	LLC12T1.2	LLC15T4
\$72	\$81	\$99	\$81	\$72	\$99	\$135

Please see pages 581-593 of your 1973-74 EEM (ELECTRONIC ENGINEERS MASTER Catalog) for complete information on Abbott Modules.

Send for our new 56 page FREE catalog.

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INFORMATION RETRIEVAL NUMBER 5

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## across the desk

### No shortage of solutions to the paper shortage

Your "Good News Bad News" editorial about the paper shortage (ED No. 10, May 10, p. 47) is duly noted. God makes trees and He forgets nuthin! Some people keep forgetting to recycle our newsprint, magazines, forms, letters, etc., into paper so the limited tree supply can be turned into high-class coated and uncoated stock.

As many other smaller and more ecologically motivated mags than ED have already switched, you will find sympathy scarce until you clean up your own nest. Like the man said, "You ain't seen nuthin yet!"

*Jon Ramer  
Staff Engineer*

Martin-Marietta  
Orlando, Fla. 32805

Your May 10 editorial amused me. You, the main culprit, complaining about a paper shortage? How many tons of paper does your magazine consume each month? An impressive number of trees must become victims of your unsatiable appetite. Your magazine is putting on weight like a middle-aged engineer—obviously a sign of prosperity.

I know you like to eat, too. We engineers must be updated by magazines like yours—which, by the way, is the best of its class. And I intend to cash in on another series of articles. But let us review the present method of disseminating information with respect to efficient use of paper.

Think of what happens to your portly magazine when it reaches its destination. Let me tell you what I do with it, which may be

quite typical. I page through the issue and tear out all the articles, news items and ads of interest—10 to 15 pages at most. The rest—more than 90%—ends up in the basket. What a waste of resources! What a waste of energy! What a waste of money! Of course, it's all for a good cause.

There must be a better, more efficient and more economical way.

As a starter, here is my idea. In place of sending the complete issue, send your subscribers only the magazine cover with the contents and news items. More specifically, make the whole cover a reusable envelope. The inside pages can accommodate the contents, laid out like a shopping list. The back cover should have both your address and mine. Upon receipt, I would mark off the items of interest and promptly return it to you. First manually, later by machine, you would fill the envelope with material requested and mail it again.

Obviously all technical material must still be profusely padded with voluptuous blondes to display their wares. However, only subject-related advertisements are needed, since the clientele's interest is considerably narrowed.

It is all so simple. The engineer still receives his info. The advertiser still contacts his clientele. You and your staff can still feed your families; only your shipping clerks may need a little retraining.

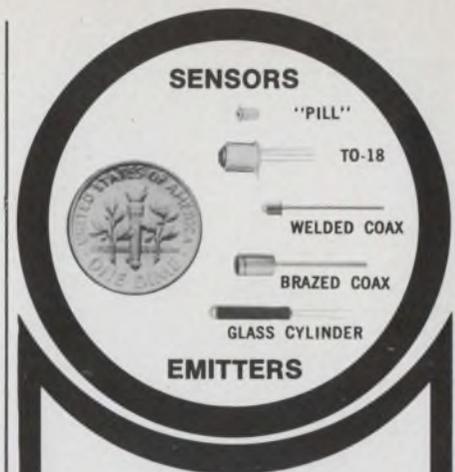
*Hermann Schmid*

General Electric  
Box 5000  
Binghamton, N.Y. 13902

Regarding your May 10 editorial, the solution is simple. Bring out a microfiche ELECTRONIC DESIGN.

*(continued on page 14)*

Electronic Design welcomes the opinions of its readers on the issues raised in the magazine's editorial columns. Address letters to Managing Editor, Electronic Design, 50 Essex St. Rochelle Park, N.J. 07662. Try to keep letters under 200 words. Letters must be signed. Names will be withheld on request.



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Detailed technical information on discrete components and other OPTRON optoelectronic products . . . chips, assemblies and PC board arrays . . . is available from your nearest OPTRON sales representative or the factory direct.



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# McMOS is the MSI supply...with

Logic functions with three-state outputs have achieved popularity because they permit multiplexing schemes which use a single element to drive a common bus line, while disabling all other drivers on that line.

Because the need is there, Motorola's MC14500 Series MSI offers more CMOS three-state logic functions, covering a wider range of system requirements, than you can find anywhere else.

From the beginning, Motorola's commitment has been to build the most useful CMOS logic family in the industry, based on the needs of the systems being designed for the marketplace. And, as the opportunity for new standard three-state functions arises, we will add them to the line. Several are in planning or under consideration at this time.

The broad McMOS\* line does offer more, and not only in three-state. MSI functions serve logic system needs with shift registers, timers, counters, decoders, latches, buffers, data routers, arithmetic functions,

and analog multiplexers. There are ROMs and RAMs, and specialized functions such as the dual schmitt trigger, priority encoder, and parity tree. Since the world still needs simple gates and flip flops, the McMOS line includes them, too.

were reduced significantly in May, with the biggest savings showing up on the MC14500 MSI Series. Naturally, the three-state logic types featured here are included. Don't take our word for it, though. Ask someone who's tried us recently.

## McMOS Three-State Logic Functions

MC14502	Strobed Hex Inverter/Buffer
MC14506	Dual Expandable AND-OR-INVERT Gate
MC14508	Dual 4-Bit Latch
MC14512	8-Channel Data Selector
MC14534	Real Time 5-Decade Counter
MC14580	4 X 4 Multiport Register
MC14583	Dual Schmitt Trigger
MC14034	8-Bit Universal Bus Register

## McMOS RAMs With Three-State Outputs

MCM14505	64-Bit Random Access Read-Write Memory
MCM14537	256-Bit Static Random Access Memory

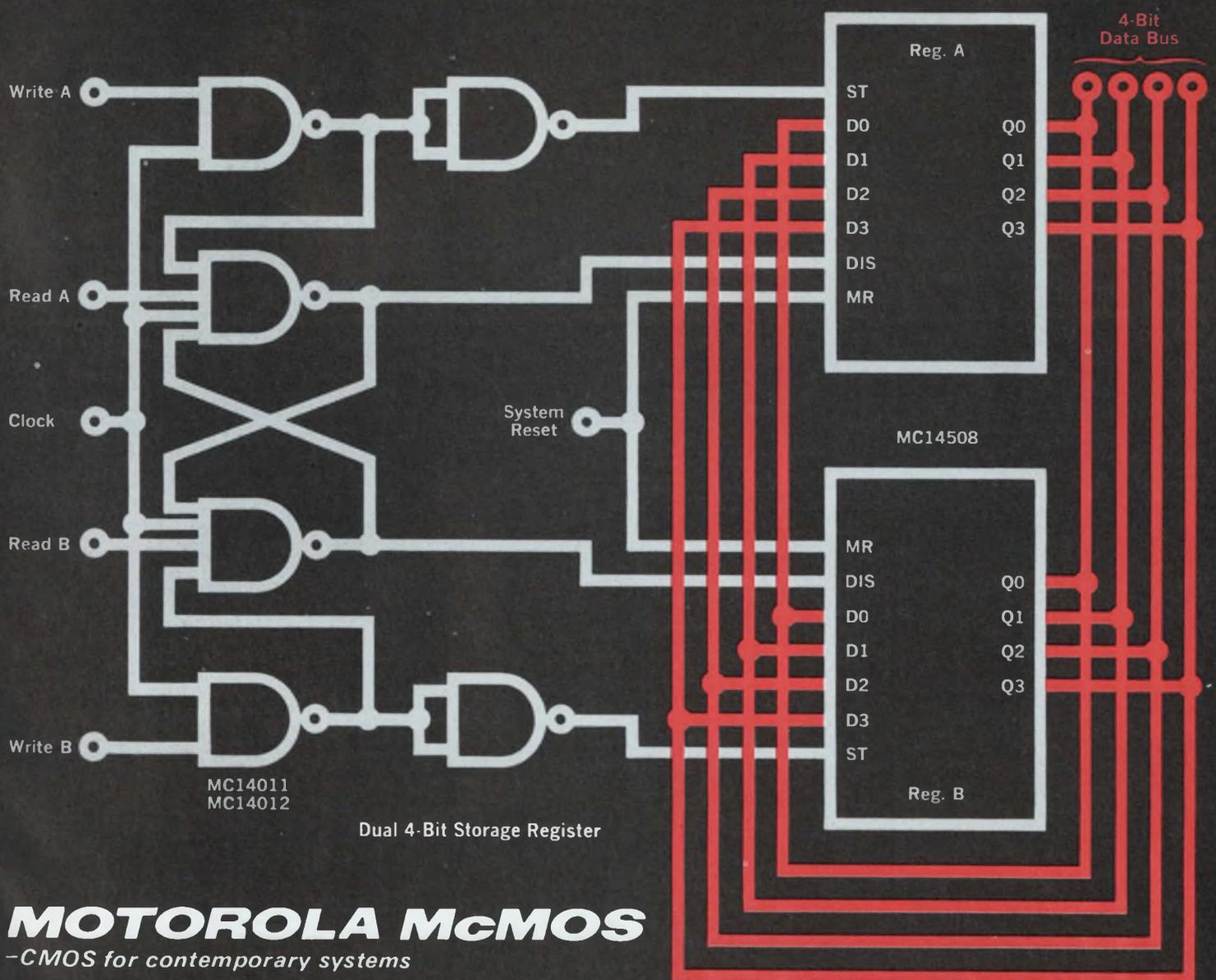
## Excellent availability... and the lowest prices ever

Availability is now excellent across the entire line, including the broad range of MC14500 Series MSI functions. Many types are available off-the-shelf, and we are quoting short 6 week delivery on most others. That's CMOS availability! And don't forget, McMOS prices

For applications information on three-state CMOS, respond to Motorola Semiconductor Products Inc., P. O. Box 20912, Phoenix, AZ 85036, or circle the reader service number. We'll send you AN715, "Introduction to CMOS Integrated Circuits With Three-State Out-puts," and a McMOS selector guide for reference.

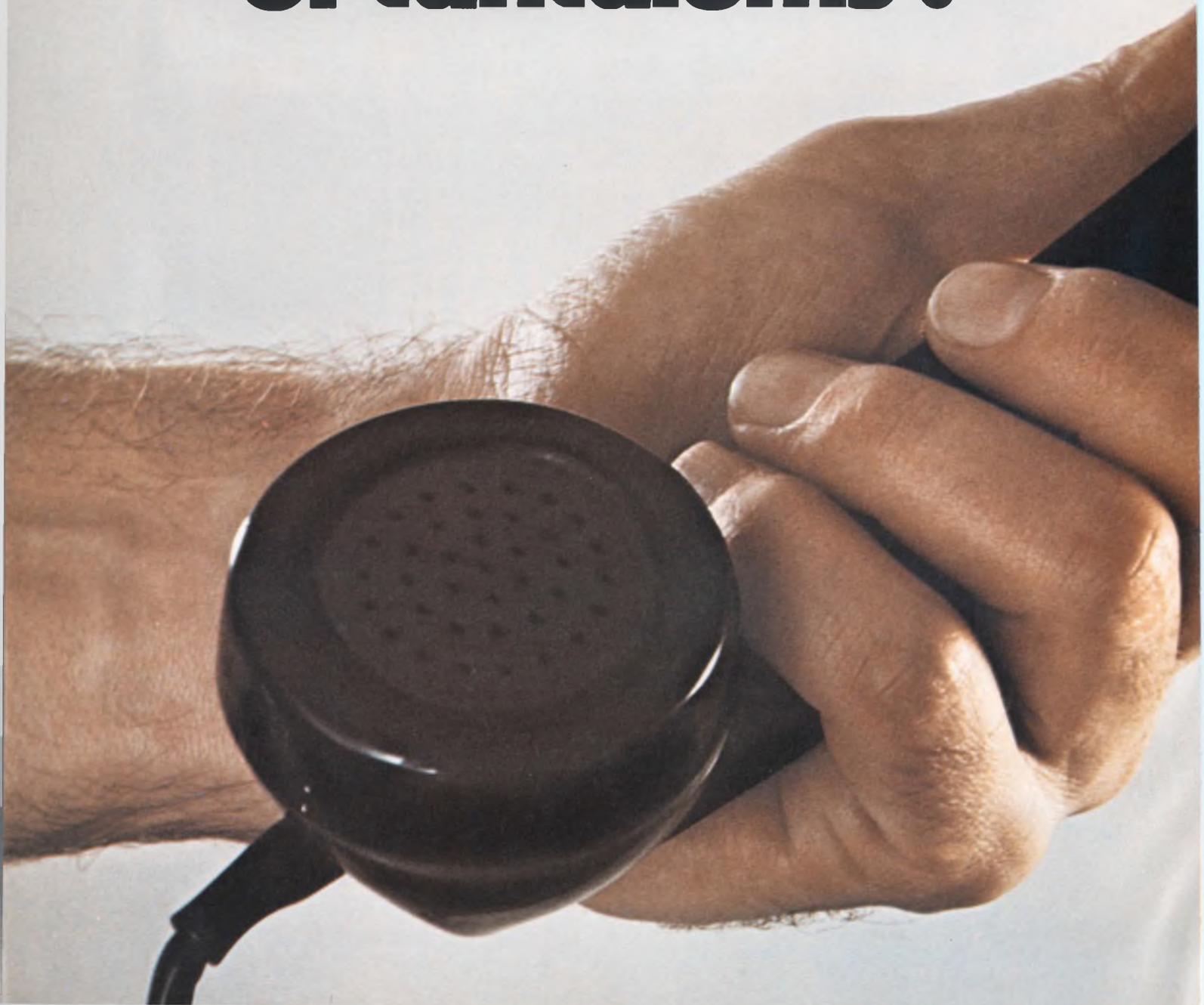


# more three-state CMOS.



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Our MINITAN<sup>®</sup> microminiature solid tantalum capacitors are epoxy-sealed in a polyester sleeve. They're available in both cylindrical cordwood and rectangular modular form, with a choice of axial or radial leads. Capacitance values are 0.001 to 220MFD, working voltages are 2 to 50VDC, and tolerances are  $\pm 10\%$  and  $\pm 20\%$ .

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INFORMATION RETRIEVAL NUMBER 9

## ACROSS THE DESK

(continued from page 7)

Mail costs go down. Printing costs go down. Storage space goes down. You can thumb your nose at the paper problem. All you need is a mailing envelope with the cover on the front and the index on the back, a bingo card and the microfiche inside. Why not?

Scott Campbell

Scott Campbell Engineering  
343 W. Patrick Circle  
Melbourne, Fla. 32901

## And here's another portable circuit tester

Your report on portable circuit testers (see "For Fast Digital Troubleshooting, Low-Cost Detectors Can't Be Beat," ED No. 5, March 1, 1974, p. 26) was brought to our attention by a user of our Dy-Nos-Stick Digital Test Probe. We agree with your basic theme. However, we feel that you made a serious mistake in not mentioning one of the more versatile products—namely, Dy-Nos-Stick.

Since the inception of our patented Dy-Nos-Stick Digital Test Probe, we have sold thousands in the domestic and foreign markets. Our product is used and re-ordered throughout the electronics industry by such customers as Univac, Bell Telephone, the major automobile manufacturers and the numeric-controlled tool industry.

H. F. Vandermark  
President

Nu-Concept Computer Systems  
Inc.

306 W. Logan St.  
Norristown, Pa. 19401

## A word about Eq. 2 in air-cooling guide

In reference to "A Guide to Good Air Cooling" (ED No. 4, Feb. 15, 1974, p. 76), the author is to be commended for his useful hints to the designer. But let me comment briefly on Eq. 2:

$$CFM = 1.76Q/\Delta T \text{ (ft}^3\text{/min)}$$

The equation holds only for air at a base temperature of approx-

imately 25 C at sea level. If the equation is rewritten as

$$CFM = kQ/\Delta T \text{ (ft}^3\text{/min)}$$

some values for k at sea level can be selected from the following table:

Medium	Temp °C	k (ft <sup>3</sup> C) W min
Air	24-3/4	1.76
Air	35	1.989
Air	40	2.1
SF <sub>6</sub>	15	0.506
Oil	30	0.00141

Casjen F. Hardens

D852 Erlanger  
Sieglitzhof  
Lange Zeile 115  
West Germany

## You're wrong; that wrong was a right

I found a mistake on the front cover of ED No. 10, May 10, 1974. In the first square in second row the digits number is 3, and the fingers show four.

Merla Rumold

Hewlett Packard  
Bldg. 170  
1601 California Ave.  
Palo Alto, Calif. 94304

Are you illustrating errors in digital equipment or did your Art Dept. let you down?

John Davidson Fogarty  
Professional Engineer

5130 Rondel Pl.  
Columbia, Md. 21043

(continued on page 25)

### Electronic Design 10

Can you count on your digits? With counters, that's what you'd like to know. But the last few digits in that long display may be meaningless. Crystal aging, temperature drift and trigger errors can clobber accuracy. And inputs that fall under 100 Hz or zip past 0.5 GHz bring new trouble in its wake. Check out counters on p. 30.





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# Super speed in plastic: Finally, ECL 10k you can afford.

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For super-speed logic you can't beat ECL 10k. But until now, cost has been the problem. Just the kind of problem we like to sink our teeth into.

Plastic's the ticket. It makes ECL 10k a standard in your budget. Because we've put so many low-cost plastic devices into low-cost volume production, our super-speed prices are competitive with other high-speed alternatives at last.

Now, in designing high performance systems for today's and tomorrow's market, you've got a choice. Before you might have designed with standard high-speed TTL logic costing 50¢/gate (100-up). Now you're suddenly able to design with super-speed ECL 10k logic in plastic costing 55¢/gate.

Variety? You bet. Early on we recognized the diversity you'd need—to cover design requirements of terminals, minicomputers, add-on memories... you name it. Signetics offers you a complete standard logic family of ECL 10k in plastic. And there's more to come, including the higher power MSI counters, shift registers and adders.

Here's the clincher: availability. Everything listed is in production. Everything in production—on our distributors' shelves. NOW. Should a local run clean a device out of stock, it's only temporary.



We can expand availability on short notice—meaning days or a few weeks, not months.

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<b>GATES</b>	10111	10116	10135
10101	10112	10124	
10102	10113	10125	<b>ENCODERS &amp; DECODERS</b>
10103	10117	10190	
10104	10118	10216	10132
10105	10119		10134
10106	10121	<b>LATCHES &amp; FLIP FLOPS</b>	10158
10107			10159
10108	<b>INTERFACE</b>	10130	10171
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# Synchronous and Asynchronous

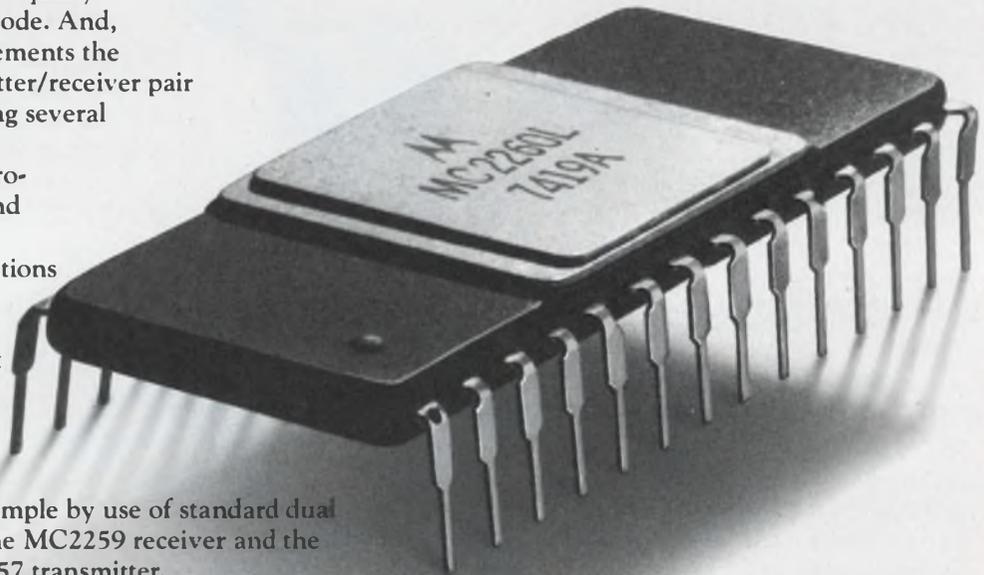
10000010 11001010 10011010 01110010



It makes no difference to the MC2260L terminal transmitter. This newest Motorola MOS subsystem for digital data communications operates equally well in either mode. And, the MC2260L perfectly complements the popular MC2257/59L transmitter/receiver pair it joins in the line, while offering several output functions not provided by the MC2257, such as synchronous transfer, internal clock, and word complete.

Typically, data communications devices of this complexity must be encapsulated in large, non-standard packages, but not with Motorola's approach to these functions. Because the receiver and transmitters are separate units, handling and insertion procedures are kept simple by use of standard dual in-line packages — 28-pin for the MC2259 receiver and the MC2260, 24-pin for the MC2257 transmitter.

Consistent yields from dedicated production facilities allow excellent availability of these types. The same factors help keep prices down. In 100-999 quantities, the MC2257 is \$9.00, the MC2259 is \$10.75, and so is the MC2260. For technical information, including an applications note on the operational aspects of these transmitter/receiver types, circle the bingo number or write to Motorola Semiconductor Products Inc., P.O. Box 20912, Phoenix, AZ 85036. For products, contact any franchised Motorola distributor or your Motorola sales office.



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From us. The Components Group of Digital Equipment Corporation. A new group, formed to supply proven, reliable computer components to the volume buyer at the lowest possible prices.

The products, described in detail on the following pages, are all used by Digital as components and peripherals in the PDP-8 and PDP-11 minicomputer systems, the most popular minis in the world. Our components—like our computers—are designed to deliver maximum price/performance.

Our peripherals can be interfaced readily with all commonly-used minicomputers. Additional products will be available in the near future; product families are planned to provide a range of capabilities.

Until now, if you wanted Digital components, you had to buy an entire system.

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Now, if you order fifty pieces or more, you can buy any of these components completely unbundled. Volume buying will get you price breaks you won't believe—just check out the prices on the next couple of pages.

And you can have our components off the shelf. When we've established our nation-wide network of warehouse/depots (due this fall), volume deliveries will be made as fast as we can process your order.

Behind our commitment to deliver stands the entire Digital manufacturing capability—over



two million square feet of manufacturing space in the United States, Puerto Rico, Canada and other countries overseas. These are the same facilities that have produced more minicomputers than anyone else, the facilities that manufacture and test the peripherals that support these computers. To meet your demands in the next year alone, we're planning several new plants in the United States and Canada and retooling present production lines to Components Group specifications.

To deliver these components quickly and to maintain our high standard of reliability, the Components Group is planning a network of warehouses. At these depots, products meeting our rigid specifications will be stocked for off-the-shelf delivery.

Our warranty is simple: all hardware is fully warranted for a specified time. If, during this period, any product should prove defective, you simply return it to the nearest depot for fast repair or exchange.

Over the next few years, we expect the cost of computer hardware—especially the cost of the computer itself—to keep going down. Entirely new applications will open up. Volume production of proven components and peripherals enables us to sell at greatly reduced prices. Our low-cost, high-quality products will provide our customers with an opportunity for enhanced profits and a competitive edge in an increasingly price-conscious market.



# Terminals and peripherals.

## **Our cassette mag tape system. Under \$1600 in quantities of 100.**

Priced below even paper tape, the TU60 is a truly reliable dual cassette system. We designed it to stand up to repeated use — with cassettes spec'd at a minimum of 1000 passes, and an error rate that's a full order of magnitude lower than most other systems.

Our proprietary cassette design reduces the possibility of hard error. The extra-thick 1 mil mylar tape is specially coated to resist extreme temperature and humidity.

The TU60's reel-to-reel drive increases tape life even more — there are no capstans, pulleys, pinch rollers, or brakes. DC servo-controlled motors reduce stretching and provide precise start/stop characteristics.

To reduce noise interference and ensure that even very low data levels will be read accurately, the TU60 employs an independent high-threshold data block detector and low-threshold data peak detector.

And the TU60 can't accumulate error from tape-speed fluctuation due to power variation or mechanical difficulties: the read electronics adapt themselves to the tape speed by means of a phase lock loop. Other error-reducing features include redundant dual-track recording, automatic leader detection, and CRC-type error control.

Because the TU60 places the burden of recording-reliability on its electronics, not its mechanics, less maintenance is required to keep the system in good working condition. And when maintenance is necessary, it's no problem. The top flips open, everything is accessible, and the two main modules can be replaced in minutes.

## **Our new DECscope video terminal. Under \$950 in quantities of 100.**

The VT50 is the most inexpensive CRT display terminal in the world. It'll give you fast, quiet alphanumeric video capability for the cost of a slow, noisy teletypewriter. Hardcopy output is available too, with our optional low-cost copier.

For a groundlevel budget price, you get 12-line, 80-column good-quality display — 64 ASCII-

standard upperface characters, each on a 5x7-dot matrix. After displaying 12 lines, the page scrolls upward from the bottom; its speed can be adjusted by the user.

The keyboard is an easy-to-use, audible, typewriter-style board, with 3-key rollover to permit fast typing. Our optional copier fits right into the desktop display cabinet.

The VT50 is fast — a full range of baud rates are switch-selectable up to 9600. Interfacing is with a standard 20mA current loop, with inexpensive EIA option.

Installation is easy, just plug it in. The VT50 has few moving parts, so maintenance is simple. Its keyboard is the same field-proven model we use on the LA36 teletypewriter. And its low heat output means no fans, less noise, and low power consumption.

At such an incredibly low price, the VT50 will go far. And fast.

## **Our remote terminals. Starting at less than \$600.**

The RT01 and RT02 terminals provide easy, low-cost interactive data entry and retrieval.

Uncomplicated keyboards make it easy for untrained personnel to enter or retrieve data. There's no need for confusing, numerically-coded instructions. The RT02 will even prompt the inexperienced operator by spelling out on the display what information is needed next.

The RT01 displays up to 12 digits of data in a Nixie™ numeric readout. For non-numeric response, it has programmable status indicators. The 16-key pad will input 30 ASCII characters.

The RT02 costs more and gives you more. A 64-character gas-discharge alphanumeric readout that displays up to 32 characters at once. 16-key or 58-key input. Interactive display prompting.

Both terminals are ASCII-compatible, so you can interface them to any computer with a Teletype™ port. EIA modem interface is also available.

Both have simple displays and few moving parts, for built-in reliability and ease of maintenance.

# Logic modules and interfacing.

Digital is the world's largest seller of solid-state modules. We give you the widest choice you can get — over 400 pretested modules, most of which we use ourselves, in our computers and controllers. We also carry a full line of compatible hardware, power supplies, plug-in boards, cabinets, racks and related equipment.

If you do your own interfacing, our Logic Products Handbook and Logic Systems Design Handbook will provide general support and solutions to specific standard problems. The Components Group will also supply, in volume, custom interfaces, custom modules, and custom variations of our standard terminals. Complete descriptive literature on any of these topics is available.

## **M Series modules.**

These high-speed logic modules for computer interfacing use monolithic TTL circuitry to give you high speed, high fanout, large capacitive drive capability and excellent noise margins, in frequencies up to 6MHz. Some of our newer M Series modules also employ current MOS technology.

## **K Series modules.**

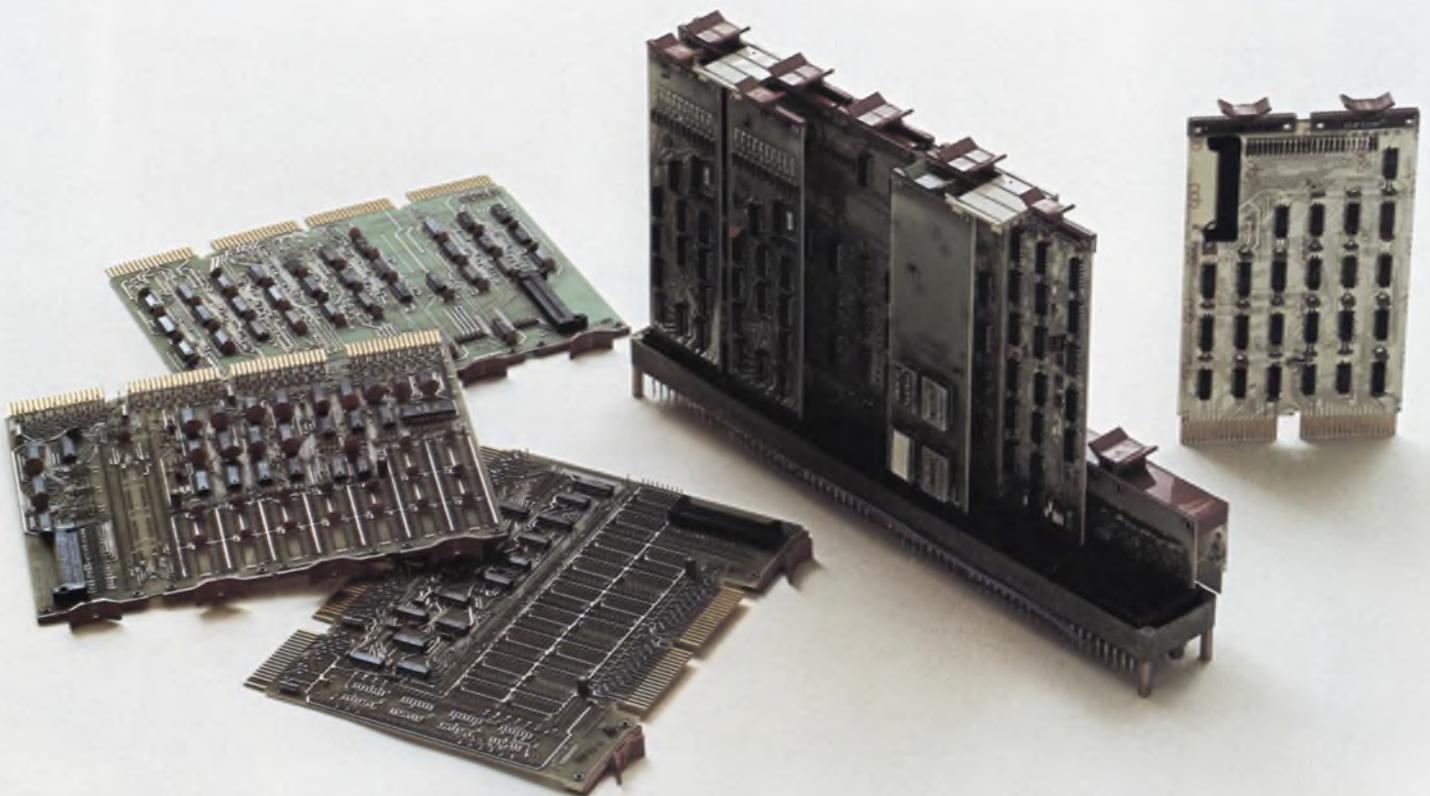
These noise-resistant modules are principally used for industrial control applications where noise-resistance is more important than speed. Frequencies from DC to 100KHz are typical, 5KHz frequencies can be obtained. K Series modules are designed for easy system checkout and troubleshooting and will fit both standard NEMA enclosures and computer mounting racks.

## **A Series modules.**

For communications between the computer and the outside world, these analog modules give 10-bit and 12-bit performance in a family of mutually compatible functions — multiplexers, operational amplifiers, sample-and-hold circuits, A/D and D/A converters, reference voltage sources, and multiplying A/D converters.

## **DECKit interfaces.**

Our DECKits provide pre-tested, fully-documented interfaces for a number of common interfacing situations. Basically just a few modules and a prewired systems unit, they eliminate design time, breadboarding, and wirewrapping in a number of areas. Complete descriptions of the specific interfaces are available.



# The start of a new family of component computers.

## The PDP-8/A. \$572 in quantities of 100 (CPU & 1K RAM).

For minicomputer applications, the PDP-8/A computer-on-a-board gives you speed and performance at an extremely low price.

The newest, smallest member of the PDP-8 family of minicomputers, the 12-bit PDP-8/A uses only proven, readily available, multi-source MSI semiconductor technology. We know it's reliable, and we can deliver in quantity, starting in late 1974.

To reduce the size and enable low-cost, user-tailored memory capacity, we've added expandable semiconductor memories: ROM, RAM, PROM, and ROM/RAM combinations, expandable from 1K to 32K words. Cycle time is 1.5 $\mu$ sec.

The PDP-8/A uses the same powerful instruction set as the PDP-8/E and is fully compatible with other PDP-8 family hardware, operating systems, and high level languages (such as BASIC, FORTRAN IV, FOCAL).

The PDP-8 Omnibus™ backplane facilitates direct interface with more than 60 PDP-8 options and peripherals. Seven commonly-used options are available on two option boards: serial-line interface, 12-bit parallel I/O, front-panel control, and real-time clock on one board; powerfail/auto-restart, memory extension, and bootstrap loader on the other.

The PDP-8A gives the user the flexibility, reliability, and expansion capability of a minicomputer at an extremely low price.

## The MPS microprocessor series. \$476 in quantities of 100. (CPU & 1K RAM).

The MPS microprocessor series of modules gives you a simple, versatile 8-bit controller that's inexpensive and easy to use. It will replace hard-wired logic in control applications and perform processing tasks in many new applications.

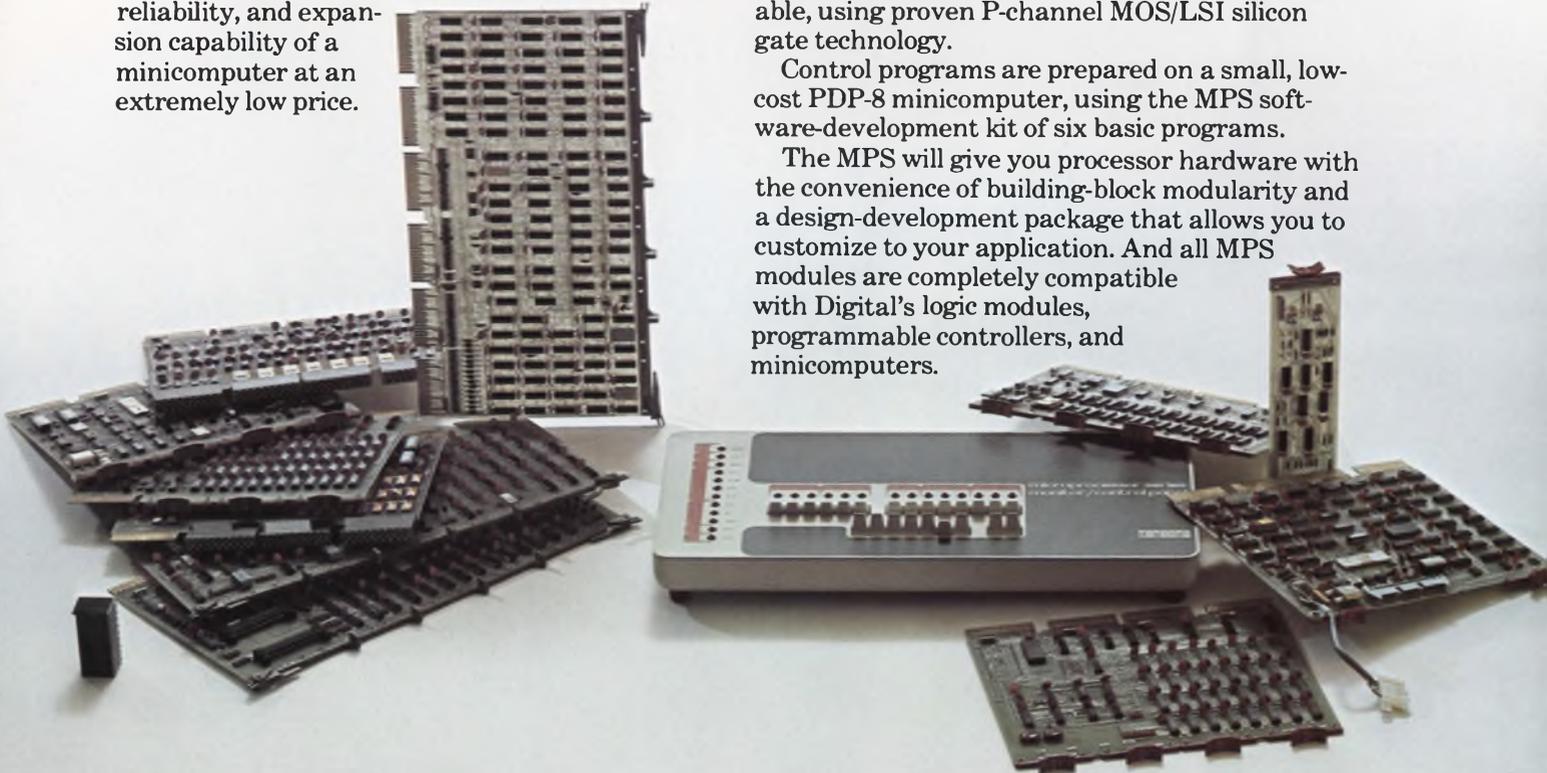
The MPS consists of four building-block modules and an optional control panel. A basic fully operational processor can be assembled from as few as two modules: the CPU and a memory module.

The CPU module with 8-bit parallel processor, 48 data-oriented instructions, and 12.5  $\mu$ sec cycle time, can directly address up to 16K words of memory. There are two memory modules: the Read-write Memory module consists of a fully-self-contained random access memory (1K, 2K or 4K words) and all address decoding logic; the Programmable Read-only Memory module contains up to 4K words of UV-eraseable, completely reprogrammable semiconductor memory. The External Event-Detection module provides power-failure detection and automatic start, with 6 interrupt request inputs. The Monitor/Control Panel, which can be cable-interfaced to the CPU, will perform such typical functions as monitoring data paths, memory, and addresses, handling general system operational and diagnostic checks, and entering programs.

We designed the MPS to be immediately available, using proven P-channel MOS/LSI silicon gate technology.

Control programs are prepared on a small, low-cost PDP-8 minicomputer, using the MPS software-development kit of six basic programs.

The MPS will give you processor hardware with the convenience of building-block modularity and a design-development package that allows you to customize to your application. And all MPS modules are completely compatible with Digital's logic modules, programmable controllers, and minicomputers.



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# Fast and easy... MOSTEK's MK4102-6 static 1K RAM.

## 275 ns!

MOSTEK's MK4102P-6 is fast — 275 ns access time! But speed is only one of its features. Just as important, it's easy to use, requiring only one +5 V power supply. All inputs are TTL compatible. And the processing technology is strictly state-of-the-art utilizing a combination of N-channel silicon gate plus ion implantation.

Also, you can accomplish large memory array construction with a minimum of additional circuitry because of the high impedance "off state" coupled with "chip select" input.

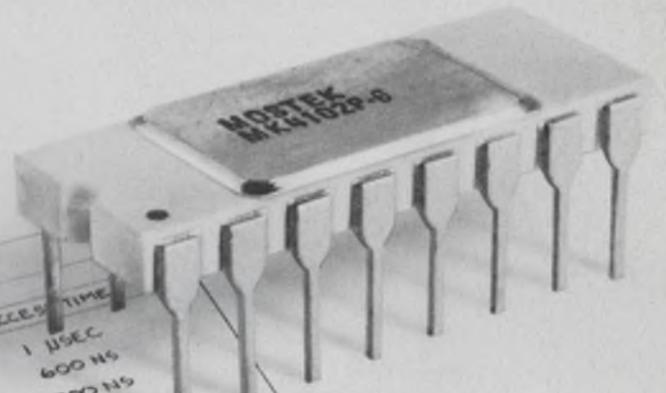
What else? Well, the MK4102P-6 is a pin - for - pin alternate for the 2102. But there's no comparison in access time. Check for yourself.

MOSTEK's line of 1K RAMs gives you plenty to select from, static or dynamic. They range from the MK4008-9 (at 800 ns) through two other versions of the MK-4102 (450 ns or 1  $\mu$  sec) up to the popular MK4006 (at 400 ns). Check the table below for the part number you need.

When your design requires an MOS memory, remember MOSTEK. Call your nearest MOSTEK distributor or representative or contact MOSTEK, 1215 W. Crosby Road, Carrollton, Texas 75006, (214) 242-0444. In Europe contact MOSTEK GmbH, TALSTR. 172, 7024 Bernhausen, West Germany, Tel. 798038.

**MOSTEK**®

MOSTEK moves forward...in memories.



MOSTEK MEMORIES		MAX. ACCESS TIME
ROMS		1 $\mu$ SEC
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2240-BIT CHARACTER GENERATOR		700 NS
2560-BIT ROM		700 NS
4096-BIT ROM (REPLACES MM 5232)		900 NS
4096-BIT ROM (REPLACES F5C 351A)		
16K-BIT ROM (REPLACES EA 4800)		
RAMS		400 NS
1024-BIT DYNAMIC RAM		900 NS
256-BIT STATIC RAM		500 NS
1024-BIT DYNAMIC RAM		800 NS
1024-BIT STATIC RAM		1 $\mu$ SEC
1024-BIT STATIC RAM		450 NS
1024-BIT STATIC RAM		275 NS
4096-BIT DYNAMIC RAM		350 NS
CIRCUIT		
MK 2300P		
MK 2400P		
MK 2500P		
MK 2600P		
MK 28000		
MK 4006P		
MK 4007P		
MK 4008P		
MK 4008P-9		
MK 4102P		
MK 4102P-1		
MK 4102P-6		
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R&D has also enabled Siemens to pioneer metallized polyester-film (MYLAR\*) capacitors, tuning-diodes, gas-filled SVP's® and cradle relays. And there are more innovations on the way.

If you depend on electronic components, you can depend on Siemens. Batch after batch, the quality never varies.

\*DuPont registered trademark.

For details, get in touch with your local Siemens specialist, or fill in the coupon below.

Please indicate your specific area of interest and mail to:  
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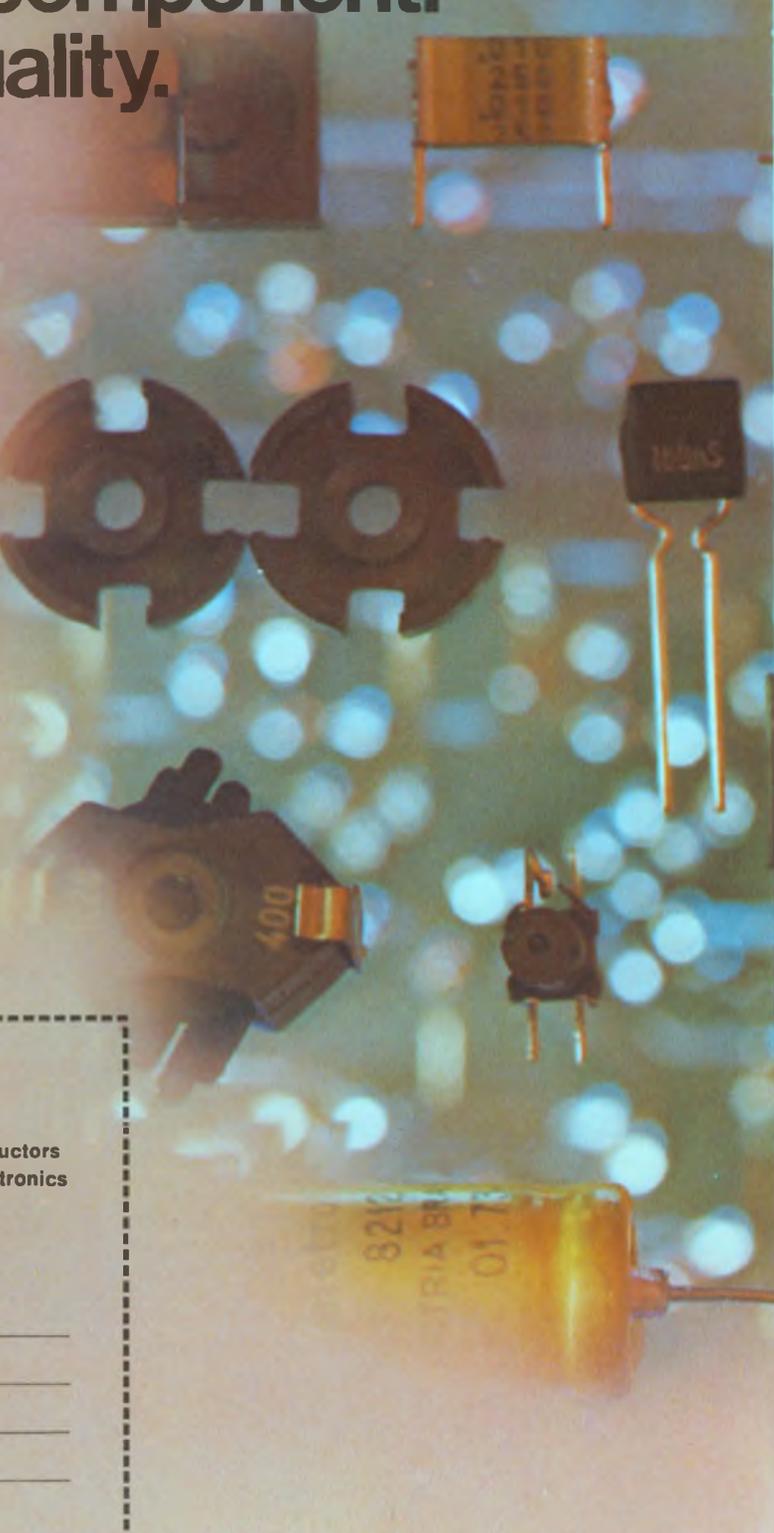
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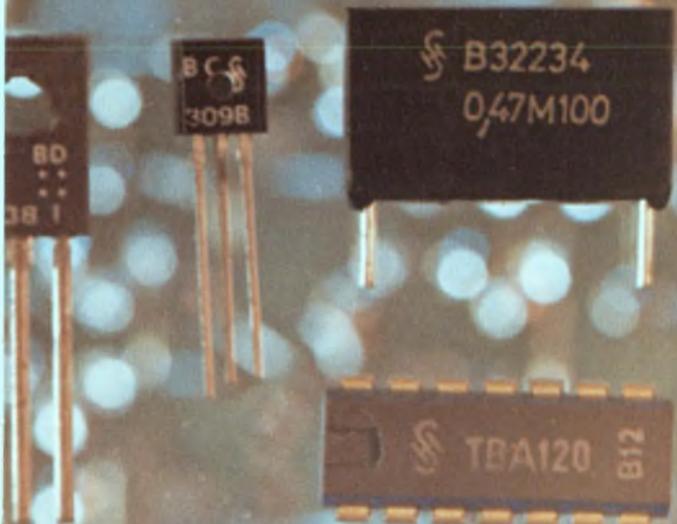
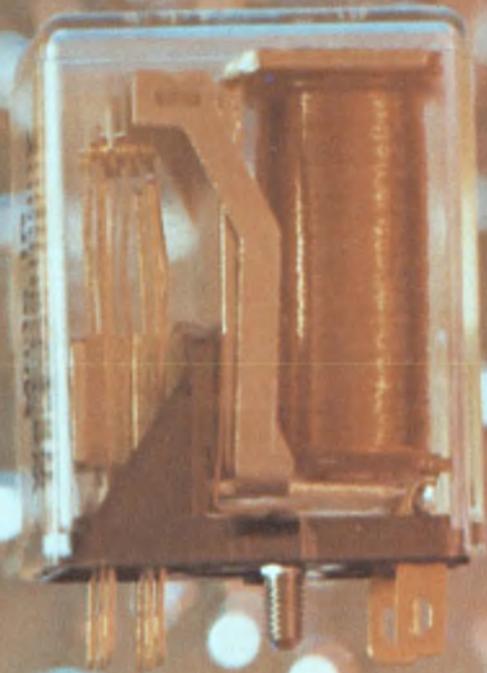
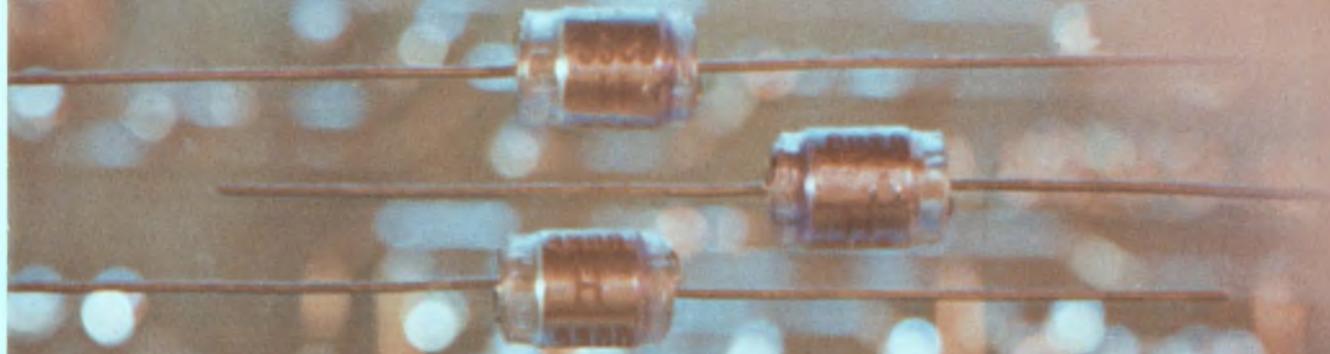
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Actual Size

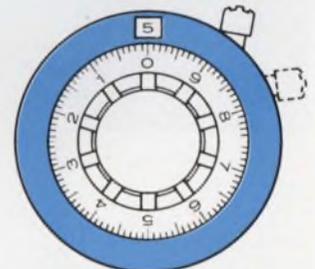
## KNOBPOT® CLOCKFACE POTENTIOMETERS

For those who prefer a clockface readout, our Models 3600 and 3640 KNOBPOT® potentiometers come in two sizes —  $\frac{3}{4}$ " and  $1\frac{1}{4}$ " — and extend only  $\frac{3}{8}$ " to  $\frac{1}{2}$ " behind your panel.



## TURNS COUNTING DIALS

Good looking 10-turn dials . . . simplified mounting — no special panel holes required; mounts directly to potentiometer shaft. For  $\frac{3}{32}$ ",  $\frac{1}{8}$ " and  $\frac{1}{4}$ " diameter shafts . . . with or without brake. Models H-490, H-510.



Actual Size

## DIGITAL COUNTING DIALS

Contemporary digital-style readout in our new H-357 KNOBPOT® Digital Dial. Ten-turn range, 100 counts per turn. Connects to any standard  $\frac{1}{4}$ " shaft potentiometer or similar rotating device. Only \$5.00 in production quantities.



## DIALS COUNT BETTER ON BOURNS PRECISION POTENTIOMETERS

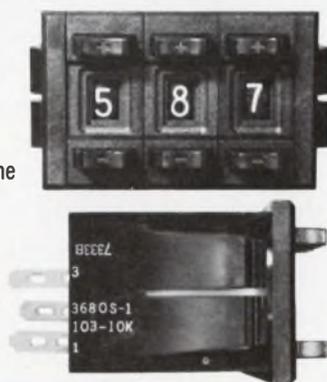
We back-up our turns counting dials with a broad line of superlative precision potentiometers. Choose from over 20 standard models . . . from our low cost Model 3540 wirewound family, to our super-smooth, superlonglife INFINITRON® conductive plastic models. If you have custom requirements, Bourns has a separate, full-time engineering and manufacturing operation devoted exclusively to custom work.



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### KNOBPOT® DIGITAL PUSHBUTTON POTENTIOMETER

Great new innovation from Bourns! A precision decade potentiometer **inside** a handsome pushbutton digital selector/display. The Model 3680 is extremely accurate, and a "snap" to install. Everything is **INSIDE** . . . no resistors or mini-PC boards are required.



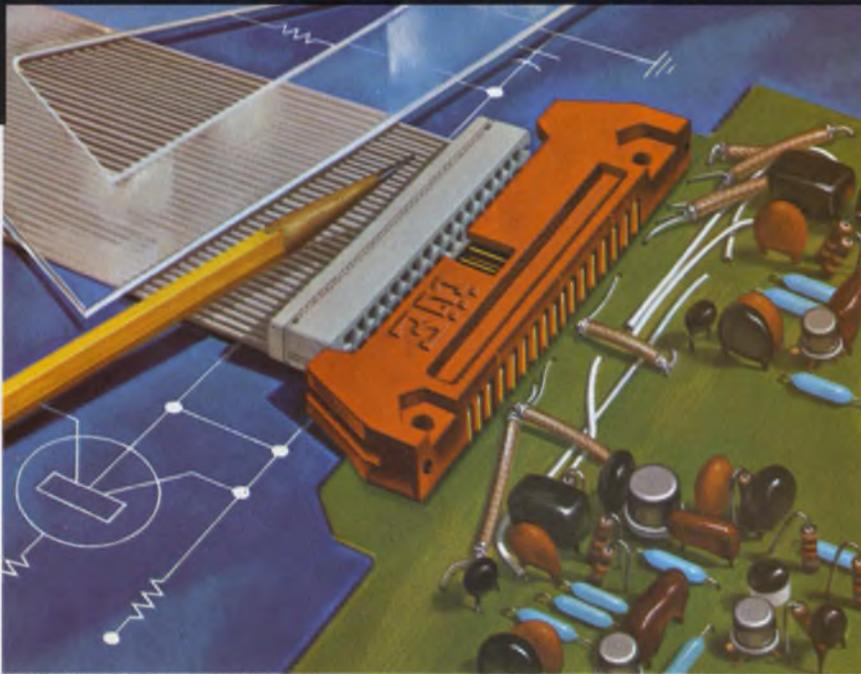
For a close-up look at Bourns PANEL POWER, dial EEM 800-645-9200 (toll-free) and ask for the name and number of your nearest Bourns sales representative.



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There's built-in reliability for your circuit inter-connects. Our flat, flexible PVC Cable has up to 50 precisely spaced conductors. The gold plated U-contacts are set into a plastic body to provide positive alignment. They strip through the insulation, capture the conductor, and provide a gas-tight pressure connection.

Assembly cost reductions are built-in, too. "Scotchflex" Connectors make up to 50 simultaneous connections without stripping or soldering. No special training or

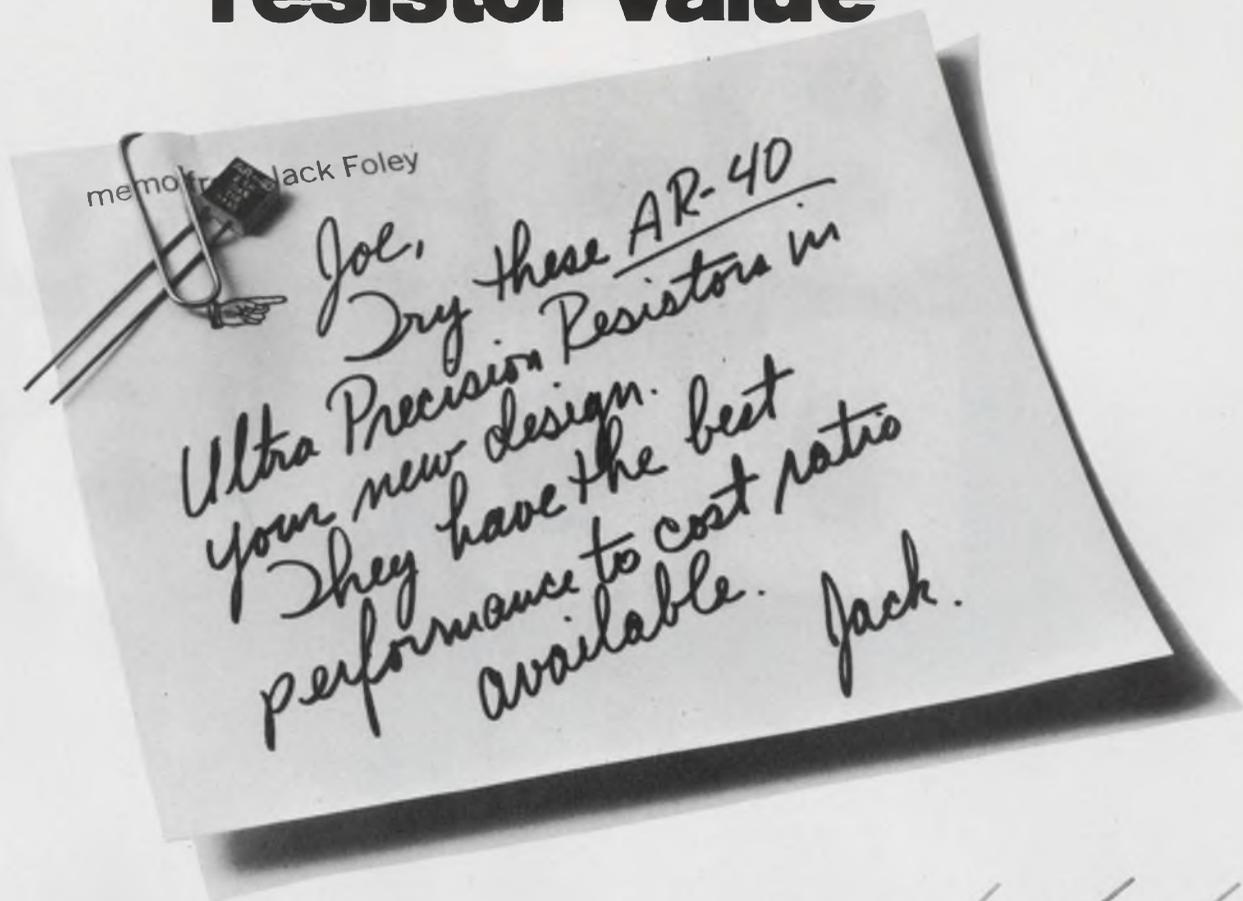
costly assembly equipment is needed.

Off-the-shelf stock offers you flat cable in a choice of lengths and number of conductors from 14 to 50. Connector models interface with standard DIP sockets, wrap posts on .100 x .100 in. grid, or printed circuit boards. Headers are available to provide a de-pluggable inter-connection between cable jumpers and printed circuit boards (as shown). Custom assemblies are also available on request.

For full information on the "Scotchflex" systems approach to circuitry, write to Dept. EAH-1, 3M Center, St. Paul, Minn. 55101.



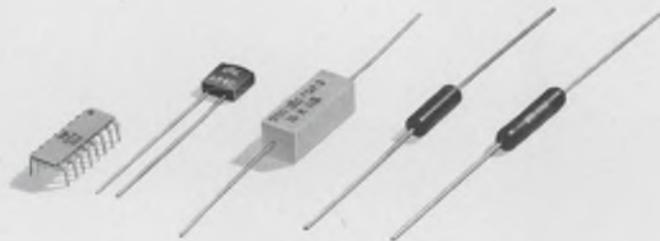
# The best ultra-precision resistor value



Hung up on resistor performance vs cost? Then check the AR40 metal film resistor—sophisticated, ultra-precision resistors from TRW's precision resistor technology.

With the AR40, you get ultra-precision, exceptional stability, and documented reliability. Temperature coefficient to  $\pm 2$  PPM/ $^{\circ}$ C and tolerances to .01% are standard. High frequency characteristics are outstanding and noise levels are not even measurable on commercially available equipment.

Additional value is provided by the AR40's rugged construction which withstands normal production handling. The AR40 is available now to solve your ultra-precision resistor problems at a cost you can afford.



*Complete resistor choice.* TRW offers you a total resistor capability—carbon comp., thin-film, Metal Glaze™, wirewound, networks. For specs and application data on the AR40, contact your local TRW sales representative. Or write TRW/IRC Resistors, an Electronic Components Division of TRW, Inc., 2850 Mt. Pleasant St., Burlington, Iowa 52601. (319) 754-8491.

## Performance and dimensions

TCR CLASS	STANDARD TEMP. COEFF. ( $^{\circ}$ C)	RESISTANCE RANGE* (Ohms)	STANDARD TOLERANCE RANGE ( $\pm$ %)	WATTAGE $85^{\circ}$ C	DIMENSIONS IN INCHES
T-18	2 ppm 0 to $60^{\circ}$ C 5 ppm $-55$ to $125^{\circ}$ C	20 to 100K	.01 to 1.00	.3 watts	Height .320 $\pm$ .020
T-16	5 ppm 0 to $60^{\circ}$ C 10 ppm $-55$ to $125^{\circ}$ C				Length .295 $\pm$ .010
					Width .100 $\pm$ .010
					Lead spacing .150 $\pm$ .010
					Lead gage #22 .0253**

\*Wider ranges available, contact factory. \*\*Lead length 1.00 minimum.

## TRW<sup>®</sup> IRC RESISTORS

INFORMATION RETRIEVAL NUMBER 16

# 85 amp DO-5



The ratings are back and even we're a little amazed at the fantastic results. We knew our upgraded DO-5 was a honey, but an 85 amp rating is (to say the least) a major breakthrough in power semiconductors.

Here's how it tested:

- Dimensions as per JEDEC DO-5 outline.
- Maximum Recurrent Peak Reverse Voltage . . . 100-1600 volts.
- Maximum Average Forward Current, Single Phase Half Wave Rating at 115°C. Case Temperature . . . . . 85 amps.
- Maximum Surge Current (One Cycle) . . . . . 1500 amps.
- (H) JC . . . . . 0.6

For detailed information, contact:  
FMC Corporation  
Semiconductor Products Operation  
Homer City, Penna. 15748  
(412) 479-8011

**FMC** Special  
Products

# THE NATIONAL ANTHEM



A review of New Products and Literature from National

## RUMORS TRUE!

### Thermostatted Pressure Transducers Are Here!

To all of you out there who have heard the rumors, and to all of you who have been waiting anxiously for the word, your wondering and waiting are over. Yes, transducer lovers, there really are thermostatted IC pressure transducers, and National makes them.

We call our new, high-performance (1%) transducers the LX3700 series. These transducers incorporate a temperature sensor and diffused heater resistors. The sensor thermostatically

controls the heating elements, which means that the entire transducer is temperature controlled. The scheme regulates transducer temperature to 170°F, the upper limit of control; the lower limit is -10°F - a 180°F range of temperature control.

The LX3700's temperature performance is spectacular: over the 180°F control range, the transducer's temperature coefficient is only 0.278 mV/°F (0.5 mV/°C) out of a 10-V full-scale output; and the temperature range over which we guarantee a tight spec is twice that of our LX1700 series. Further, you can extend the low end of thermostatic control by wrapping the transducer in a thermal insulating material (e.g., styrofoam).

Performance of the LX3700 over time is just as exciting: 30 seconds after power is applied the output voltage

(continued on page A3)



### Count 'em. Bunky! Now there's 21 JAN & JAN TX JFETs from National!

Starting in June, National Semiconductor will have available - off the shelf and in sizeable quantities - a complete series of JAN and JAN TX JFETs qualified to MIL-STD-19500. JAN TX processing goes one step beyond JAN processing and adds 100 percent reliability preconditioning.

We'll be offering 21 different types, all but two of which will qualify to both JAN and JAN TX specifications, and here they are:

- p-channel amplifiers—  
JAN2N2608-09
- p-channel switches and choppers—  
JAN/JANTX2N5114-16
- n-channel general purpose amps—  
JAN/JANTX2N3821-22
- n-channel vhf/uhf amplifiers—  
JAN/JANTX2N3823  
JAN/JANTX2N4416A
- n-channel choppers and switches—  
JAN/JANTX2N4091-93  
JAN/JANTX2N4856-61
- n-channel dual JFETs—  
JAN/JANTX2N5545-47

Circle No. 302 on Bingo Card

## "PICK A CARD...



## ANY CARD."

### The IMP-8C/200: a Programmable, De- bugged Microprocessor

There are games that start with someone telling you, "Pick a card. . . any card." And in these games the dealer always wins; he knows what card you're going to pick because the deck is rigged - you don't have a chance.

In the microprocessor card game, however, the deck can't be rigged. But the only way you can win is to pick the one card that you can use the way you want to use it.

And this is why we strongly suggest that you take a close look at our IMP-8C/200 integrated microprocessor card. A flexible, self-contained, low cost, eight-bit processor, the IMP-8C/200 is designed for computer oriented equipment such as data terminals, test systems, communications equipment, machine tool controllers, process control systems and peripheral device controllers.

(continued on page A3)

# NATIONAL STANDS ALONE

## MIL TTL? NSC is OPL.

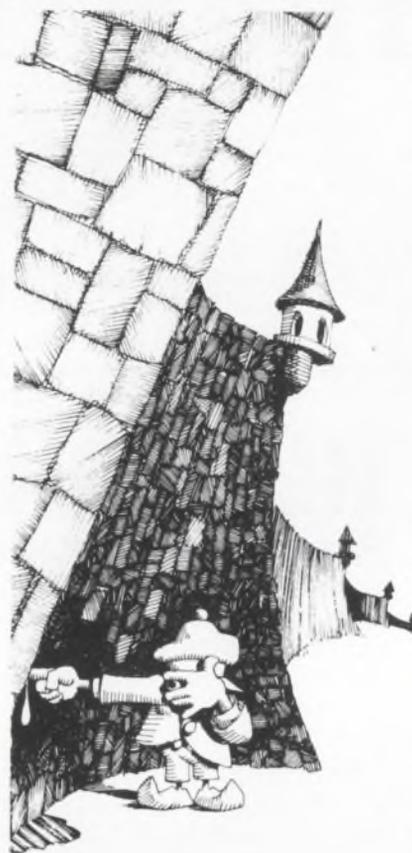
In a bind for MIL-spec, low power TTL parts? Then hear this: National Semiconductor can help you. We can supply the parts you need. And what's more, we're the *only* vendor who can do so.

That's right. National Semiconductor is the only vendor qualified to MIL-M-38510 for low power TTL parts. For example, we are currently qualified under DESC OPL 38510-13, Part 1, for 11 different parts, and are in process of qualifying for another eight types — all low power, series 54L TTL. For TTL in general, we currently are fully qualified under DESC 38510-13, Part 1, for 28 different parts and we are in process of qualifying for another 44 types. Further, our MIL TTL is available to you in either dual-inline packages or flatpacks — from us, both styles qualify.



NSC also meets the Level B and Level C requirements of MIL-M-38510. So when you need MIL TTL — especially low-power types — come to us. We have what you need.

Circle No. 303 on Bingo Card



## ULTRA-LOW LEAKAGE! A Process-84 Dual FETs Feature!

National Semiconductor rounds out its complete line of FETs with the introduction of the 2N5902 series. Fabricated by National's Process 84, a 2N5902-series device is a glassivated, monolithic, n-channel dual JFET with a diode-isolated substrate.

In other words, the new FETs have subpicoamp leakage over wide input swings, low capacitance, high CMRR and are tightly matched over a wide current range. They are thus eminently suitable for the most critical op amp input stages and electrometer single-ended preamps. They are, in fact, ideal wherever *sub-picoamp* inputs are important.

The 2N5902-09 have gate currents of 0.1 pA (typ.) even at  $V_{DG} = 25V$  (the curve is flat). Tracking is also excellent — units can be selected that show less than  $5 \mu V/^{\circ}C$  even at drain currents of only a few microamps.  $V_{GS}$ ,  $g_{fs}$  and  $g_{oss}$  are also matched, and the CMRR exceeds 110 dB. The FETs are housed in a seven-pin TO-78 package.

Circle No. 305 on Bingo Card



## Some Old Friends Still at Your Beek & Call

Every now and then we like to take some Anthem space to remind you about some not-so-brand-new products that still find wide use in a variety of applications.

Take our MM5202A and MM5203, for example: these silicon-gate MOS PROMs have been around for a little while now. They're non-volatile, bipolar compatible, 2048-bit static memories organized as 256 eight-bit words. (The MM5203 also can be organized as 512 four-bit words.)

You'll find that these memories have many uses in such applications as code conversion, random logic synthesis, table look-up, character generation and microprogramming. They're easily programmed in the field, and the quartz-

lid versions are erasable with ultraviolet light (at 253.7 nm).

The MM5202A and MM5203 feature 1- $\mu s$  (max.) access times for high-speed operation, common data busing with Tri-State® outputs and a chip-select control. (An additional feature of the MM5202A is that in the read-only memory mode, it is pin-compatible with Intel's 1602A and 1702A.)

Housed in 24-lead DIL packages, the MM5202AD (metal lid) and MM5202-AQ (quartz lid, silicon seal) are for  $0^{\circ}$  to  $70^{\circ}C$  operation. The corresponding D and Q versions of the MM5203 are also for the commercial temperature range. And for  $-55^{\circ}$  to  $85^{\circ}C$  ambients, try the MM4203D (metal lid) or MM4203Q (quartz lid, hermetic) variants.

Circle No. 304 on Bingo Card

## Apply your LED Lamp!

National Semiconductor's solid state, GaAsP lamp series — NSL000/100, NSL5020 and NSL5050 — are characterized by red light emission at 670 nm (typ.). Because the lamps function with as little as one to three milliamperes of forward current, they are ideal for use in low power, low voltage circuits.

The advantages of our solid state lamps are many, and include, among others, sub-microsecond rise/fall times; low impedance for compatibility with most semiconductor circuitry; low heat generation; life in excess of 100,000 hours; and low, low cost.

From simple on/off status indicators to complex-array displays, there are a multitude of applications for our solid-state lamps, including uses in anemometers, annunciators, appliances, cameras, computers, contactless pots, go/no-go gauges, ignition systems, medical instrumentation, numerical control equipment, remote control toys, space vehicles, telephones, test instruments, toll booths, TVs, vending machines, etc., etc. and so on; the list is virtually endless.

So we're pretty sure that somewhere, in something you're doing, a solid-state lamp can help you. And National makes solid-state lamps.

*Circle No. 311 on Bingo Card*

## NATIONAL SEMICONDUCTOR hits the road.

In the seven-week interval between April 25 and June 12, National Semiconductor will be showing lots of wares at a number of shows both at home and abroad.

The Hanover Trade Fair, for example, runs from April 25 to May 3. And at this fair — the industrial show of shows — we will announce our entry into the European consumer market with a booth display of our consumer calculator products.

A few days later, from May 6 to May 9, the National Computer Conference

## LITERACY TEST. 54C/74C Line Adds Read/Write RAM

National Semiconductor's expanding family of CMOS digital products has grown again, this time by the addition of a 16-word by four-bit random access memory. Called the MM74C89, the new RAM features a fast, 130-ns (typ.) access time at  $V_{CC} = 10V$ . The supply voltage can range from 3V to 15V, and dissipation at TTL supply-voltage levels is only 100 nW (typ.) per package.

Inputs to the memory consist of four address lines, four data lines, a write enable line and a memory enable line. An internal address register shifts the address data into the RAM only on the positive-to-negative transition of the memory enable input. This input, together with the four Tri-State® output lines, provides easy memory expansion.

The RAM has a fan-out of two low-power TTL (74L) loads. Noise margin is guaranteed to be at least one volt, and noise immunity is 45 percent (typically) of  $V_{CC}$ .

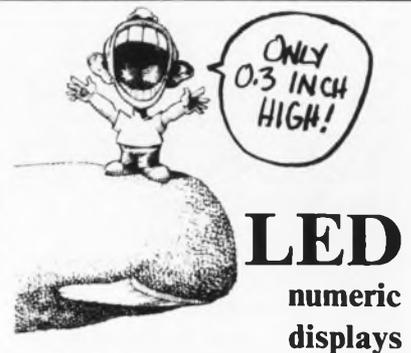
Both the MM74C89 (0° to 70°C) and the MM54C89 (-55° to 125°C) are packaged in 16-lead DIPs.

*Circle No. 313 on Bingo Card*

will have Chicago's McCormick Place humming. And National Semiconductor will be busy too, with a prominent display island (Booth 753) to show and demonstrate our wide line of microprocessors and microcomputers; and we'll be showing our memory systems, too.

Finally, there's a double-feature running in Chicago between June 9 and June 12. Between these two dates, McCormick Place will play the Chicago Consumer Electronics Show, as brought to you by the Consumer Electronics Group of the EIA. We'll be there too, with a grand booth to display our pocket calculators.

The second feature of the double bill is sandwiched in on June 10 and June 11,



## LED numeric displays

### use reflective techniques.

Optical reflective techniques give National's NSN71 and NSN74 numeric displays uniformly intense segments. The same techniques also contribute to the displays' low cost relative to their height.

Features of the new GaAsP displays include common-anode (NSN71) and common-cathode (NSN74) construction, fast switching/multiplexing and a 150° viewing angle.

Low cost and large size mean that the displays will find wide usage in new designs for desk-top calculators, digital clocks, point-of-sale equipment, DPMs, TV channel indicators, elevator floor displays and in any redesigns that previously had no display or used mechanical or gas-tube display devices.

National's NSN71, in right- and left-hand decimal versions, directly replaces the DL-1, -10, -410 and -707; the HP5082-7730; the MAN-1, -4, -10, -71 and -72; and the TIL-302 and -303.

Similarly, the NSN74 directly replaces the DL-4 and -704; the MAN-74; and the FND70. Though this last device is sole sourced and mechanically different from the NSN74, a redesign to use the National product gives you not only a larger digit but a multi-sourced product as well.

*Circle No. 314 on Bingo Card*

over at the Marriott Motor Hotel. This one is the Chicago Spring Conference on Broadcast and Television Receivers. We're looking forward to our booths (nos. 7 and 8) being busy with people interested in our wide range of products for the BC/TV RX industry.

We at National highly recommend that you pick the show (or shows) of your choice and do your thing; you can bet that we'll do ours.

*Circle No. 312 on Bingo Card*

# NATIONAL SIMPLIFIES YOUR LIFE!

## Our New Cross-Reference Guide to JFETs.

Can a simple chart be a cost-saving device? Yes, when it's National's deceptively simple, new, cross-reference guide to JFETs. The guide leads you to readily-available parts from a major supplier (us), and helps you to reduce the variety of JFET type numbers you need for any project. In addition, the new guide works beautifully with our earlier JFET Selection Guide, which we published last year (see *The National Anthem*, No. 13, Nov. 1973.)

The new guide — a handy, looseleaf-punched foldout — has two sections. One section lists 31 cost-effective, preferred JFET types. These will satisfy 95 percent of new design requirements. The JFETs in this section are categorized by application. Key parameters of each device are listed and, wherever possible, equivalent metal can and epoxy types are shown.

The second section of the new guide lists nearly 1300 JFETs, and shows the status of each type (stock or special-order item, special mark and/or electrical selection, JAN or JAN TX, etc.). All of these devices are available from National, and are listed by their NSC-available type number (the original designation, according to the original manufacturer), and cross-referenced to an alternate National stock type (which may or may not be the same as the original number). The 2N JFET types are listed regardless of current industry acceptance.

In short, our new cross-reference guide steers you to the more popular, stock, lower-cost, standard JFETs from the literally thousands of types available from a variety of manufacturers.

For types missing from the list, the probability is quite high that we can meet your needs. So if you're having delivery, price, quality or performance problems, or simply desire a major source, take a peek at the JFET cross-reference guide from National — the JFET people.

Circle No. 308 on Bingo Card



## More Reasons To Go National 54C/74C

By now you know that National's CMOS digital products form a nearly ideal logic family: low power dissipation (10 mW/gate at 1 MHz with a 50-pF load); short propagation delays (25 to 50 ns); controlled, ramp-like rise and fall times (20 to 40 percent longer than the gate delays); high noise immunity (45 percent of  $V_{CC}$ ); and a guaranteed noise margin (1.0V) two-and-a-half times that of TTL.

And by now you also know that our 54C/74C product line is alive and well, growing all the time, and gives you pin and functional CMOS equivalents of all the most popular 5400/7400 TTL parts.

Okay. But what you may not know is that our 54C/74C products are not only second sourced, but doubly second sourced. Teledyne Semiconductor has been supplying 54C/74C since last November. And now, Harris Semiconductor too is supplying 54C/74C.

So if you insist on buying only second-sourced products, that's fine with us. Because you can get all the features of 54C/74C parts from three sources. Or, to put it another way, now you have two more reasons to go to National for your CMOS logic needs.

Circle No. 309 on Bingo Card

# HERE COME DEBOUNCER!

Just as fish have to swim and birds have to fly, mechanical switch contacts have to bounce. Contact bounce has been and probably always will be a fact of life. In digital systems, particularly, contact bounce can be very nasty and give rise to temporarily-indeterminate inputs.

To eliminate bounce, you've probably had to resort to special networks — like, say, a couple of TTL gates and eight resistors for every four switches.

Now there's a better way: National's new DM8544 replaces those ten components, and does their job better and more cheaply.

The DM8544 quad switch debouncer is a contact-bounce eliminator par excellence: it's a single package that debounces four switches and needs no external components; is Tri-State® connectable to buses; has a strobe input for greater control; interfaces to all TTL; and is available in both commercial (8544) and military (7544) temperature versions. In addition, you have your choice of three package styles: molded DIL; *Ceramil* DIL; and flat-pack.

There's nothing else on the market quite like the DM8544. So try it; you'll like it.



Circle No. 310 on Bingo Card

## Thermostatted Pressure Transducers (Cont'd)

is within  $\pm 150$  mV of the spec'd nominal value; and in the interval from 120 seconds after power-up to shut-down, the output voltage remains within  $\pm 25$  mV of its value at the 120-second point — even after temperature cycling ( $-10^{\circ}$  to  $170^{\circ}$ F), pressure cycling and so forth.

The LX3700's long-term lack of drift is just as astounding: after a 120-second warmup, the output voltage will be within  $\pm 50$  mV of the output voltage of the previous powered period regardless of time, temperature and

pressure exposure between the powered periods.

You can reap the rewards of LX3700 operation anywhere that you operate a transducer over a wide range of temperature ambients. You now can add altitude reporting capability to a transponder, for example, that will meet the necessary requirements at altitudes to at least 30,000 feet. Altimetry and barometry are only two of many applications areas for thermostatted transducers.

The LX3700's sensitivity in the differential mode, for example, lends itself well to use in vehicular fuel control systems. There's a good, solid output signal available even at tenths of psid,

because the LX3700's full-scale output can be reached at a differential of only 1–1.5 psi.

The LX3700's interchangeability, nominal end-points, linearity, hysteresis and so forth are the same as those of our LX1700 series, and you have your choice of differential, absolute, or gage units. The LX3700's outer housing is nylon. Please contact us for detailed specifications.

As for the price. . . well, let's just say that you'd be hard pressed to find a transducer competitively specified for less than \$600. For that much money, you can walk away with a fist full of LX3700s.

Circle No. 306 on Bingo Card

## IMP-8C/200: (Cont'd)

The major functional units of the IMP-8C/200 consist of:

- a CPU;
- a clock generator;
- an input multiplexer;
- a data buffer;
- control flags;
- a conditional jump multiplexer;
- on-card memory;
- address latches;
- a page counter; and,
- a data multiplexer.

The IMP-8C/200's CPU supports a basic set of 38 instructions. There are provisions for plugging in a second

CROM, which will double the size of the basic instruction set.

And memory isn't limited. The IMP-8C/200 card itself contains 256 bytes of read/write memory, which you can expand to 2304 bytes by adding up to 2048 bytes of read-only memory. You can expand the total system memory to 65,536 bytes maximum. (The IMP-8C/200 interfaces to our 8192-by-eight-bit dynamic memory modules.)

Buffered data are available over an eight-bit, buffered-data-out bus for peripheral devices, control panel and add-on memory. Addresses are taken from a separate, 16-bit bus. A system

clock is provided for distribution outside of the IMP-8C/200 for synchronization of peripheral units.

In summary, the IMP-8C/200 offers you, on one 8-1/2-by-11-inch printed-circuit card, a proven, totally debugged processor that you can customize to your immediate application by programming, rather than by hard wiring. The technique is flexible and saves you considerable cost in terms of both money and development time. Remember, we want you to win. So ask us about the IMP-8C/200. Or ask the man who owns one.

Circle No. 307 on Bingo Card



### WITH TYPICAL MODESTY NATIONAL ANNOUNCES A NEW METHOD OF MEASURING TEMPERATURE THAT MAKES EVERY OTHER WAY LOOK SICK.

You're looking at it. The world's first 1-C, 5-tem pressure transducer. On a single monolithic integrated circuit chip, we've included a linear sensor amplifier for adjusting span and offsetting voltage reference so the transducer can be a real temperature controller. It reads out via our Ohms or microvolts. And comes calibrated to  $\pm 4^{\circ}$  C over a  $-55^{\circ}$  C to  $125^{\circ}$  C range.

Stack that up against the other ways to measure and control temperature: Thermocouples that have the problem of low output, non linearity, and require a cold junction reference. Resistive sensors and Thermistors that need a stable excitation, and are non-linear.

And all three of those other ways need an electronic box to translate the sensor output into temperature, which increases the size and cost of the units. Pretty sick.

For all you people doing in your distribution, the numbers to order are LX5600AH, LX5600H (the 4-lead TO-5 lead TO-8 package), LX5700AH, LX5700H (4-lead TO-8 package).

OK for those not convinced yet, you can get details by calling out nearest branch (and below or write National Semiconductor Corporation, 2900 Semiconductor Drive, Santa Clara, California 95051).

With new, better products like this, cranking off the production line all the time, it's sort of hard to remain humble.

**NATIONAL**



### HOW TO TRANSMIT THERMOCOUPLE, STRAIN GAGE AND PRESSURE GAGE SIGNALS WITHOUT A LOT OF SWEAT, HOURS, DOLLARS, INCHES AND OUNCES.

Introducing National's new 2-Wire Transmitter. It converts the voltage from a sense to current, and sends it through a receiver, utilizing the same simple twisted pair as the supply voltage.

**No sweat.** You buy it off the shelf, instead of having to purchase your own transmitters.

So naturally you save a lot of size, weight, effort, time, and space time in money — money.

**Goodbye noise.** But the 2-Wire Transmitter eliminates more than parasitic hums. It also eliminates line drops and voltage noise.

Line drops and voltage noise can only happen when your signal is being transmitted in the voltage mode. But we transmit in current mode — which is impervious to either resistance in the wire or voltage noise spikes. So you get fewer headaches all the way around.

Available in 8-lead TO-3 and 12-lead TO-8 package.

For the full story call our nearest office or write National Semiconductor Corporation, 2900 Semiconductor Drive, Santa Clara, California 95051.

**National**

## Use FUBES NOT TUBES



National's new Fube is the lowest price FET vacuum-tube replacement on the market. When you replace a tube with a Fube your equipment shows:

- Inherently higher (JFET) stability—your gear stays calibrated and you save maintenance and repair costs;
- Higher performance—reduction in error-zone means greater accuracy and repeatability than possible with tubes;
- Lower noise, fewer and smaller distortion products — JFETs are quiet, true square-law devices;
- Reduced power demand — save 2-2.5W for each tube replaced with a Fube (do your bit for the energy crisis);
- Tremendously increased life — all components run cooler when you get rid of the tubes.

While not a universal replacement, only a few Fube types replace a great variety of tube types. Fubes will be available to replace most of the popular

pentodes such as the 6AG5, 6AK5, 6AM6, 6AU6, 6BH6, 12AU6, 5654 6028, 403B, 408A and 415A, among others. Twin-triode replacements cover the 6BC8, 12AT7, 12AU7, 12AV7, 12AX7, 12AZ7, 6680, 60201, 396A, 407A, 407B and so on.

Laboratory test instruments (HP400-series VTVMs, Tektronix CA-type plug-ins, etc.) and telephone equipment, for example, benefit greatly from the use of Fubes. Because some changes require minor device selections, we are making available conversion kits, which include full instructions.

Until our Fube came along, there was only one source of FET tube replacements on the market. Now you've got a choice. But consider this: National's Fube is a cost-effective device; we combine unsurpassed processing capability with volume production and pass the savings on to you. So maybe you really don't have a choice after all.

Circle No. 315 on Bingo Card

## Tick Tock.



### Two-Phase Oscillator Clock Driver

National Semiconductor's brand new MH8803 is a totally self-contained clock and clock line driver. You needn't add a thing — neither crystal nor any other external timing component.

While not designed for systems that require a highly accurate frequency source with a tightly spec'd tolerance, the new oscillator/clock driver is well qualified for a number of applications, such as calculators and even mini-computers.

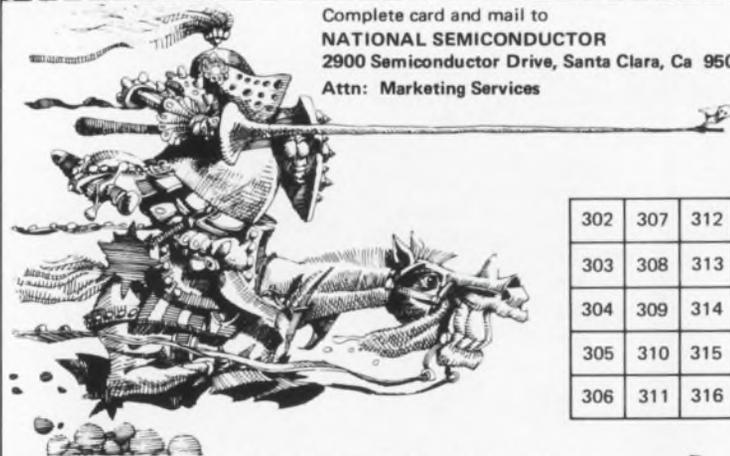
The MH8803 generates one of three primary frequencies and pulse widths. Both output frequency and pulse width are voltage controlled, so you can easily set your requirements by programming the input control voltages. You also can precisely tweak the frequency and pulse width with a potentiometer.

Outputs are non-overlapping, and adjustable in frequency from 100 to 500 kHz and in pulse width from 260 ns to 1.4  $\mu$ s. There are damped and undamped MOS outputs, and a TTL monitor output as well. The MOS outputs can drive 500-pF loads and still maintain rise and fall times within 150 ns. In addition, the outputs are current limited to protect against momentary shorts to the supplies.

The 14-lead, commercial temperature range MH8803 is available in both cavity and molded DIPs. For full military temperature range operation, we have the MH7803 in a cavity DIP.

Circle No. 316 on Bingo Card

Complete card and mail to  
**NATIONAL SEMICONDUCTOR**  
 2900 Semiconductor Drive, Santa Clara, Ca 95051  
 Attn: Marketing Services



302	307	312
303	308	313
304	309	314
305	310	315
306	311	316

BINGO

For FREE technical data, circle the numbers that correspond to the Bingo numbers at the bottom of the articles.

Please print clearly. This will be used as a mailing list.

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 COMPANY \_\_\_\_\_  
 ADDRESS \_\_\_\_\_  
 CITY \_\_\_\_\_ STATE \_\_\_\_\_ ZIP \_\_\_\_\_

ACROSS THE DESK  
(continued from page 14)

Really now! New math? Useful for WOM's? EOM's?

George K. Gastler

6609 Foxhall Lane  
Huntsville, Ala. 35806

*Ed. Note: Wrong count? Yes it was. Our "error" on the May 10 cover was deliberate. Many readers caught it and asked if the second picture in the first column was caused by a goof in our Art Dept. or by a deliberate miscount. We merely were trying to reinforce the first line in the cover text: "Can you count on your digits?" So we buried a miscount in the photographs while making a pun on "digits."*

*Incidentally, readers who caught the "goof" weren't alone. When we asked Systron-Donner to take the picture for us, their people thought we had made a mistake. Then our engraver called to inform us that there was a mistake in one picture. And later the printer called to notify us of the error. Finally many of our editors who weren't involved in the story came screaming about the error when they saw proofs of the cover.*

## Ohm's law upstaged by Murphy's law

I would like to know how  $100 \Omega$  in parallel with  $200 \Omega$  is equal to  $6 \Omega$ . Please note third paragraph of article entitled "Subnanosecond Transients Detected With ECL Logic," printed in the June 7 issue, p. 156.

G. Robert Bosworth  
Design Engineer

Eudaemonic Electronics  
Los Angeles, Calif. 90066

*Ed. Note: Simple. All it takes is a typographical error. The correct value is, of course, 66. Thanks for the eagle eyes.*

## Streakers defined

A streaker, we learned recently, is a fellow wearing a striped shirt and running through a parking lot at IBM.

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## A CCD memory emerging, an alternate for DEC

For several years now, semiconductor experts have been saying that charge-coupled devices could be used to replace disc and drum memories. Bell Northern Research in Ottawa, Canada, has decided that actions speak louder than words in constructing a CCD memory system that can replace the Digital Equipment Corp. RS64 disc, a peripheral to the PDP 11 minicomputer.

The CCD system is designed to have an average latency—the time required to reach the desired memory address—of 128  $\mu$ s. This is about two orders of magnitude better than the disc performance.

According to Chris Robinson, manager of device applications at Bell Northern, the new memory will be completed by the end of this month and will prove that CCDs can perform satisfactorily in a systems environment. Like the RS 64, the all-solid-state CCD memory will have storage capacity of 1 megabit—64,000 16-bit words—and a maximum data rate of 1 MHz.

In describing the new memory, Robinson notes that it is constructed with 8-k CCD chips, arranged on printed-circuit boards in sets of 16, so that each board stores 64,000 words. Each word is 2 bits long. A total of 8.5 boards are needed to form the memory. The extra half board provides error-correcting bits.

In explaining how the CCD memory works, Robinson points out that initially the memory is in an idle mode, where data are constantly being refreshed at a frequency of between 10 and 100 kHz. Once a transfer request comes along from the controller, the system goes into a race mode. The system then races at 1 MHz until its memory address coincides with the required address.

At this time, Robinson continues,

the system will go into a wait mode and then transfer the data asynchronously. If the cpu is too busy to transfer the data right away, the memory will automatically refresh the data until the cpu is ready.

Since fixed-head rotating memories generally store data in blocks of 256 words, the CCD memory was arranged this way, too, Robinson says. The organization of the CCD memory is such that an address pointer can be used to select the particular block of interest. To transfer integral blocks of data, the system then races until it reaches the zero address.

What appears to be the most interesting aspect of the CCD memory is what Robinson calls a "wrap-around" feature. What this means, he says, is that it is not necessary to start the transfer of data at the beginning of a block. Instead, it is possible to start at any memory location—22 for example—transfer information stored in locations 22 to 255 and then from 0 to 21. The wrap-around feature is interesting, Robinson says, because it means that the latency is reduced to the time it takes to transfer one bit. It is not the latency of the complete block of data. If this advantage is not used—and today's systems aren't geared for it—then the average latency is 128  $\mu$ s, he notes.

Robinson reports that in its current configuration, the memory is not a salable item, because parameters were not optimized.

### Kodak video player televises 8-mm film

A video film player that plays standard 8-mm film, with or without a magnetic sound track, on standard television sets has been announced by Eastman Kodak,

Rochester, N.Y.

Described as a miniature TV station by Arthur Sweeney, director of sales, the system use a flying-spot scanner that converts 8-mm film movies into standard signals. The signals are televised over Channel 3 of a TV set.

One model of the video player has its own internal synch signals. A second model has provision for external synch signals, so it may be operated as a studio unit in community-cable or regular TV stations. In the latter case, Sweeney sees the player being used to televise 8-mm film of extraordinary news events photographed by amateurs.

Developed for training and entertainment use by commercial, medical and government markets, the kodak system can reproduce both color and black and white film. It provides video pictures at either 18 or 24 frames a second.

At present, Sweeney points out, there is little equipment available to enable a station to play 8-mm film. Costly 16-mm camera setups are now common.

Deliveries of the Kodak player, which carries a suggested list price of \$1095, are to begin the end of this month.

### Sound sensor detects hard-to-find heart ills

A new technique that quickly pinpoints heart defects that may escape detection during routine electrocardiographic examinations has been developed by the General Electric Research and Development Center, Schenectady, N.Y.

Using a minicomputer and a super-sensitive "ear," the device can also evaluate the severity of the irregularities without resorting to complicated catheterization procedures that require the injection of chemicals through tubes inserted into the heart.

The key to the new technique is a small electronic sound sensor about the size of a silver dollar; it is placed on the patient's chest. The sensor detects sounds in the frequency range of 1 to 1500 cycles per second, compared with the 30 to 500 heard with an ordinary stethoscope.

The sounds detected by GE's sensor are converted to digital sig-

nals, fed into a computer and analyzed, and the results are printed out immediately. The physician then interprets the data and makes the diagnosis.

The system will help eliminate many variables that can produce inconclusive, stethoscope findings, GE says. For example, the pressure with which a stethoscope is placed against the patient's chest can affect the heart sound. By contrast, the GE transducer rests on the patient at a constant pressure.

In tests made at four teaching hospitals, the GE method has been reported instrumental in detecting restricted blood flow, abnormal muscle contraction, arterial blockage and the very early states of weakening heart valves.

The system is not intended to replace electrocardiograms but to supplement them. ECG's measure the electrical functions of the heart while the phonocardiogram tests, by contrast measure mechanical functions such as valve openings and closings and blood flows.

GE says the technique should be clinically qualified and ready for wide-scale application in two to five years.

## First 'Mill Run' ICs come off the line

The first ICs produced under the Government's Mill Run program are emerging from Signetics' plant in Orem, Utah.

The program provides for continual assembly-line monitoring by a Government Quality Assurance Representative to ensure that manufacturers are meeting the specs for JAN (military-qualified) semiconductors.

Before Mill Run there sometimes were delays of several months in deliveries while manufacturers waited for the Defense Supply Agency to send an inspector to check the finished ICs. With Mill Run, there is continuous production of inspected ICs, which can then be stockpiled for immediate delivery.

The program applied originally only to the aluminum industry but has now been extended to semiconductor manufacturers. Signetics, which negotiated with the Government for more than a year to put

Mill Run in operation, is making JAN 5400 and 54H ICs in Utah.

Mill Run ICs are specially marketed by the Quality Assurance Representative to indicate that they meet all source inspection requirements and no further verification is necessary.

Frank Jelenko, JAN product manager of Signetics notes: "Mill Run negotiations are still rather complex. They require a new facilities survey and other Government paper work. The results are certainly worth it, though. With the program, JAN customers can see, by a mark on the IC packages, that the products have been source-inspected at no additional cost to them. It should create a higher confidence level for all JAN customers buying the parts—and save them both time and money."

## Custom IC technology 'for sale' to users

Design assistance and the manufacturing technology to produce custom MOS/LSI circuits are being offered to all comers by a prototype semiconductor house. Until now, circuit manufacturers requiring custom ICs were dependent on semiconductor companies for their supplies.

The rules for laying out LSI circuits, the manufacturing technology and a technical assistance program are available from Mosfet Micro Labs, Inc., Quakertown, Pa. C/MOS, silicon and metal-gate PMOS and even CCD technologies are provided. The service costs about \$300,000. Production machinery and expendables add another \$100,000.

William Witmer, president of the company, says: "Now any firm can get into production with its own IC for about \$400,000—about a third of what it would cost to develop it in house."

The circuit-layout package is offered by the company to develop the art work for custom circuit masks, and contains background information on electrical parameters and topology. The production technology program explains how to produce IC wafers with a minimum of equipment and investment.

Mosfet Micro Labs has been in the business since 1969, assisting in the design of custom ICs and

doing prototype production. Witmer explains the company's decision to sell its technology this way.

"It has become very difficult for a small company to find a manufacturer for its custom IC. The big IC houses are producing so many stock parts that they are not interested in any short-run work. It used to be that they were happy to do a 50,000-part run for a customer; now even \$2-million contract doesn't generate much interest."

## X-ray imaging method improves crystal growth

An X-ray imaging technique that promises improved monitoring and control over crystal growth has been announced by two Western Electric scientists.

Developed by Harold D. Pruett and Swei Yuen Lien of Western Electric's Engineering Research Center in Princeton, N.J., the method was described at a recent International Conference on crystal growth in Tokyo.

The technique will be used at the company's Reading, Pa., plant to monitor and control the growth of gallium-phosphide crystals for the manufacture of light-emitting diodes. The method could also be used for other crystalline materials as well.

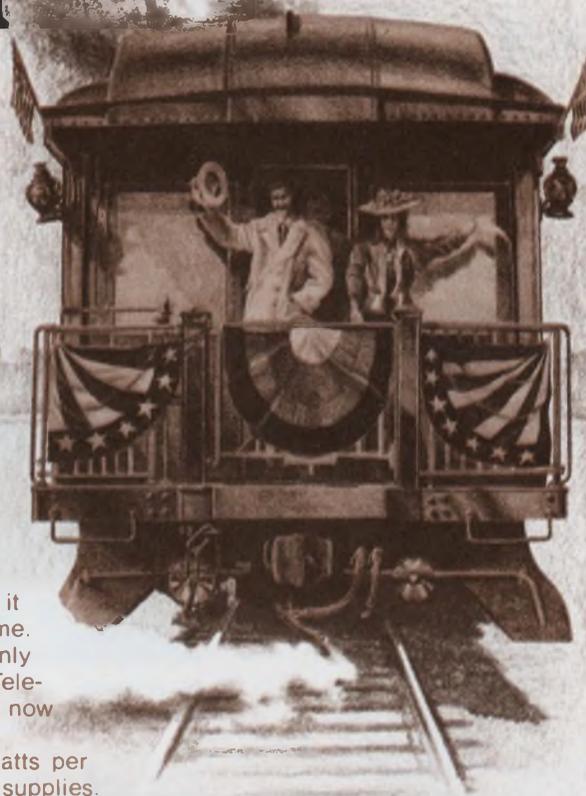
"The key advantage of the X-ray imaging system over the alternate optical viewing method is that the X-ray system allows the crystal to be observed from a side view throughout the growth cycle," Pruett said.

"An operator can see and even anticipate changes in crystal diameter and make adjustments to minimize them," he noted.

An X-ray source on one side of the growing chamber emits X-rays that pass through the crystal-growing apparatus to form a silhouette image on a fluorescent screen on the opposite side. A highly sensitive TV camera transmits the image to a monitor for remote viewing.

The system also offers better control of the growth process because it provides an accurate means to estimate the critical melt temperature, co-developer Lien said.

# The last time someone announced 74C, it was a national campaign.



When we saw 74C coming down the tracks, we knew it would be the hottest and most logical CMOS line in a long time. Flags waved, bands played, and thousands of engineers suddenly found CMOS easier to design in. The only thing missing was Teledyne's big production volume and competitive pricing, and now you've got that too.

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MM74C42	BCD-to-Decimal Decoder	MM74C192	Synchronous Up/Down Decade Counter
MM74C74	Dual D Flip-Flop	MM74C195	4-Bit Parallel-Access Shift Register

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INFORMATION RETRIEVAL NUMBER 20

# Sensors in 5 areas are getting tinier, cheaper and more precise

Sensing transducers, which are turning up on production lines, are smaller, more accurate and lower in cost than ever before.

Some are almost invisible to the human eye. Errors of less than 1% are common. And prices have plunged from the hundreds of dollars to the tens.

At the same time R&D is producing changes in design and new applications are being found. Some of the more outstanding advances are reported in these areas:

- **Temperature:** Monolithic ICs are becoming the actual sensing element. The chip contains all of the sensor's conditioning circuitry.

- **Pressure:** Hybrid ICs are now combined into a tiny sensor, with all the electronics.

- **Strain:** Semiconductor strain elements are replacing the foil gauges in some areas.

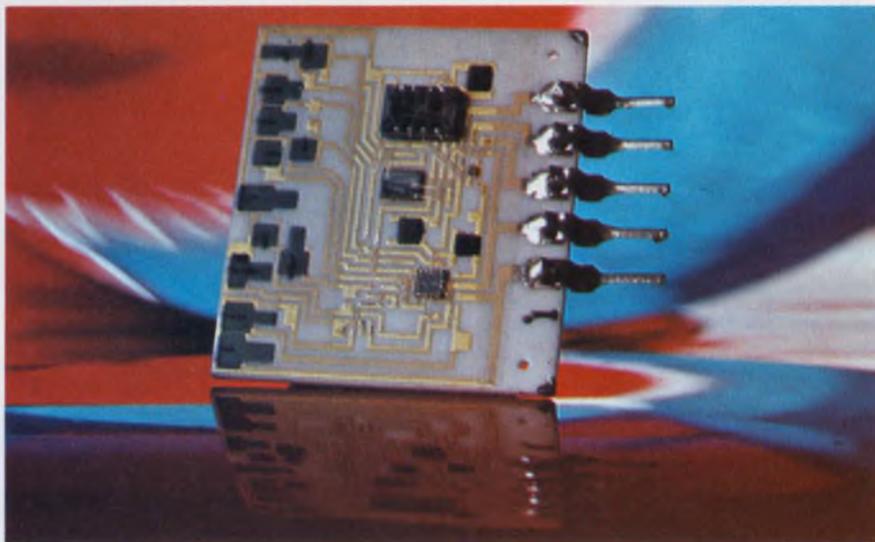
- **Acceleration:** New materials are giving the sensors higher outputs and new applications are generating more interest.

- **Displacement:** The linear-displacement variable transformer is still the most widely used, but magnetic flux, optical, rf and ultrasonic schemes are appearing.

One of the largest measurement areas—temperature—has seen the most significant change.

National Semiconductor has developed a complete temperature transducer on a single chip less than 100 mil<sup>2</sup>. This sensor, Model LX5600/5700 measures temperatures from -55 to +125 C with a calibration accuracy of  $\pm 4$  C.

On a single chip, the National LX5600 transducers have the temperature sensor, a voltage regulator, an output amplifier and a



IC pressure transducer made by National Semiconductor uses three different circuit chips and an array of thick-film resistors on a ceramic substrate.



Mark V flowmeter probes by Ramapo Instruments are retractable and can thus be moved from line to line for sampling and spot-checking flows in various size pipes.

driver transistor.

The internal op amp can modify the sensor output to almost any form, but ideally it delivers a linear 10 mV/ $^{\circ}$ K voltage change. The IC sensor costs \$13.35 (100-up).

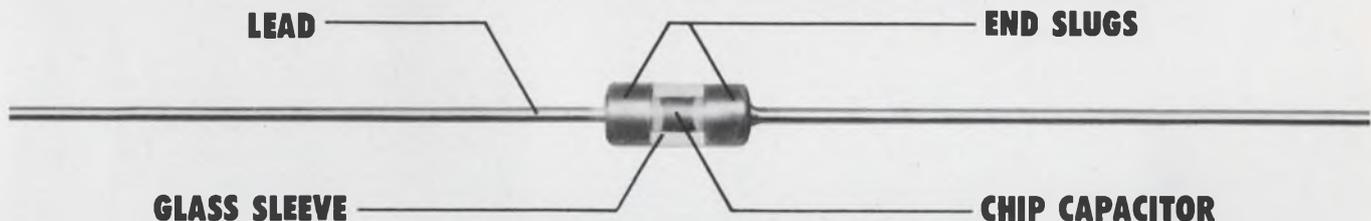
Thermocouples are not without their own unique advantages: They require no power source, cover a much wider temperature range and are just as small. They do, however, require special wiring methods, reference-temperature junctions and additional signal conditioning. Thermocouples cover a very wide range. For instance Chromel/Constantan spans 32 to 1800 F while 95% tungsten, 5% Rhenium/74% tungsten, 26% Rhenium covers 32 to 5000 F:

"Even though thermocouples have been around for many years, engineers still make some mistakes when connecting them," says Earl McKinley, director of engineering for Omega Corp. "For instance, the thermocouple should feed into a

(continued on page 34)

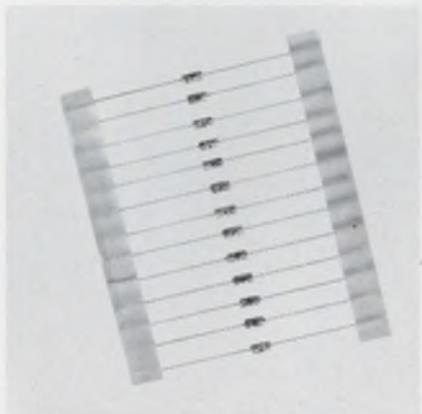
Dave Bursky  
Associate Editor

# MONO-GLASS... A JEWEL OF A CAPACITOR



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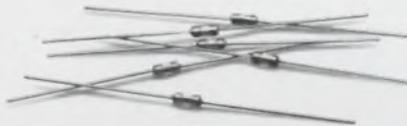


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If you use it, you know the substantial savings in time and cost. MONO-GLASS is designed for automatic insertion with the same equipment used for diodes and resistors. Reel packed and ready for your machines.

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USCC's production capability for chip capacitors is second to none. MONO-GLASS is produced by a simple assembly technique. Combine these two and you get the best possible delivery for high quantity requirements, at a budget price.

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Four case sizes are available . . . .200 x .100; .250 x .100; .300 x .150 and .400 x .150. The 50 and 100 WVDC units offer up to .01 mfd in COG dielectric, to .18 in X7R and up to 1.0 mfd in the Y5V dielectric.

## RELIABILITY:

USCC is the proven leader in state-of-the-art, demonstrated on N.A.S.A. life support and guidance systems. Commercial as well as military aerospace applications benefit from the high reliability features of our products—the best available.

MONO-GLASS is our lowest priced ceramic axial lead capacitor, offering a new quality capability for communications, navigation and guidance, computer business machines or anywhere that high volume, low price is required.

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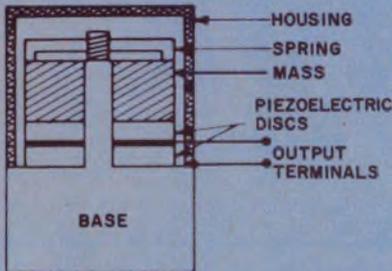
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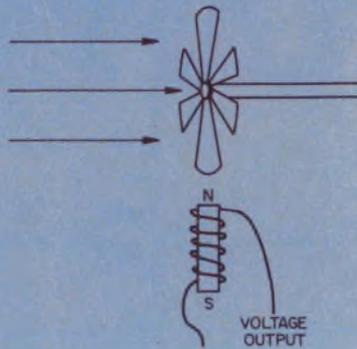


# Transducers: You name it, they make it

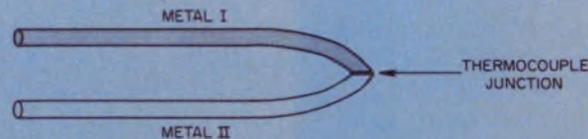
There are so many different types of transducers that it would take several books to explain how all work. Here are just a few of the different parameters that are measured and how:



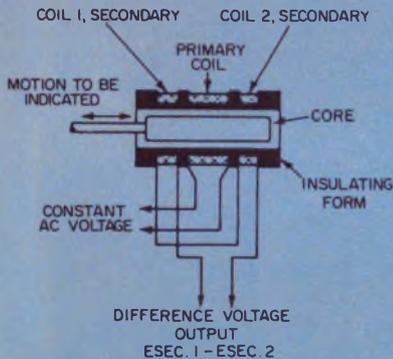
**Acceleration:** Devices that measure acceleration provide an electrical output when subjected to vibration. The electrical output is linearly proportional to the vibration over a limited frequency range. Accelerometers use techniques that are similar to those employed by pressure transducers—a crystal to generate the signal. Acceleration is usually measured in g's.



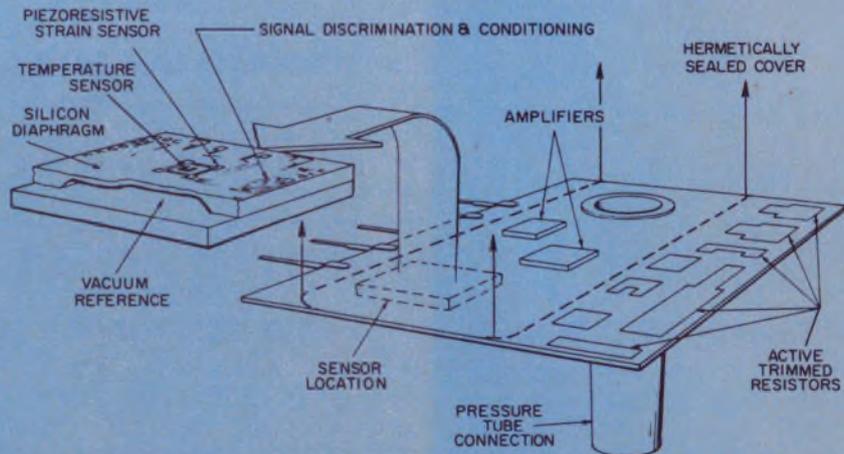
**Flow:** There are many different flow-measuring methods. Some of the more common use differential pressure transducers, tiny turbine rotors and magnetic pickups. The magnetic sensors are sometimes used in conjunction with the rotor. When the rotor turns, it produces a magnetic flux change that is converted into a pulse output that can drive other measuring or recording instruments. Flow is usually measured in gallons per minute.



**Temperature:** The most common device used is the thermocouple. Two dissimilar metals that are connected generate a voltage that is temperature-dependent. The voltage is usually several millivolts and needs special conditioning amplifiers and temperature reference points. Temperature is measured in degrees centigrade, Fahrenheit or Kelvin.



**Displacement:** The most common device to measure displacement is the linear variable differential transformer (LVDT). It produces an electrical output proportional to the internal displacement of a moveable core. LVDTs are also used to measure pressure. Other devices used for displacement measurement are the various forms of potentiometric circuits. These devices change resistance linearly as a slide is moved or a shaft rotated. Some change resistance when compressed and are used as load-measuring devices. Both LVDTs and the potentiometric devices require excitation voltages. Displacement is measured in inches, microinches or arc-seconds.



**Pressure:** Two basic types of devices measure pressure. Piezoelectric devices use a piece of crystal—usually lead-titanate-zirconate—that generates a voltage when compressed. But this voltage needs special charge amplifiers and other signal conditioning to be useful. Piezoresistive materials are also used in some pressure transducers. These materials change resistance when compressed. To be used, they are usually connected into a balanced-current bridge circuit. If the bridge unbalances, an amplifier can convert the unbalance into a voltage output. Pressure is usually measured in pounds per-square inch.

# Still fighting snap, crackle and pop?



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(continued from page 30)

high-impedance input or you can lose the signal, since the output is typically a few millivolts."

Some engineers, though, feed the thermocouple output into an analog panel meter after they run 30 to 50 ft. of wire. This will damp out and load down the thermocouple output to the point where the signal is wiped out.

Noncontacting temperature sensors are also gaining popularity. These devices use infrared sensitive semiconductor materials to generate linear output voltages. Spectran Instruments, for example, manufactures a noncontacting sensor that can measure temperatures of several thousand degrees, has a 1-s response time and is completely self-generating. Full-scale outputs of this device, depending upon the model, range from 2 to 10 mV. Prices for the units start at about \$350. All units have provision for water cooling.

### New uses for pressure transducers

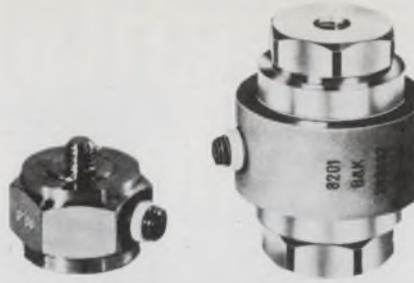
Pressure transducers also are undergoing substantial change.

One of the more outstanding developments, though over a year old, comes from National Semiconductor. The company has succeeded in reducing the strain element in the transducer and all of the required circuitry to three IC chips—a piezoresistive strain chip, complete with vacuum reference and two op-amp chips. These chips are mounted on a ceramic substrate that contains thick-film resistors. The substrate can then be placed in any desired package style.

Just released from National is an improved pressure transducer, the LX3700. The units in this series offer a sevenfold reduction in temperature coefficient—down to 0.5 mV/°C—and a doubling of the operating temperature range over which a tight spec is maintained to cover -25 to +75 C.

LX3700 units use a heating element to keep the internal temperature almost constant and to minimize drift. With the drift kept low, errors can be held to 1%. But these thermostated units draw more power—about 400 mA total, compared with 15 mA for the older LX1700 units.

Pressure transducers are finding



**Force transducers**—Models 8200 and 8201, made by B&K Instruments—can handle forces of -1000 to +5000 N or -4000 to +20,000 N, respectively.



**The TJE series of pressure transducers** feature a 0.1% static error band. These units, made by Sensotec, cover pressures as low as 20 in. of water to over 30,000 psi.

new applications in the automotive industry, where "engineers are taking good, reliable designs and reducing the cost tremendously through high-volume production," says John Hayer, director of marketing for Gulton Industries, Servionic/Instrumentation Div. Cast-metal housings are used instead of the finely machined cases required in military applications. Inside, though, the circuits are almost identical—and just as reliable.

In automotive applications pressure transducers will be used to measure manifold pressure—a part of electronic fuel-injection systems now being tested.

An example of where this change is occurring is in the GS-100 series of pressure transducers made by Gulton Industries. The GS series units are LVDT (linear velocity displacement transformer) pressure transducers. Some units include not only the signal conditioning electronics, but a voltage-regulator circuit. High-volume prices for these units are projected in the \$30-to-\$50 range.

Pressure transducers are constructed in many different ways. Some use piezoelectric crystals, piezoresistive materials or bonded strain elements. BLH Electronics and Genisco Technology use the bonded type. The full line of models offers full-scale ranges typically from 50 to 100,000 psi.

Schaevitz Engineering, on the other hand, uses the LVDT as a pressure transducer. Columbia Research Labs uses piezoelectric and piezoresistive materials to obtain pressure information.

All these older transducers require signal conditioning. Manufacturers such as Statham, Columbia, BLH, Schaevitz are including the signal conditioning circuitry inside the metal cases.

### Two types of strain gauges

Strain gauges have excellent dynamic response, long life, low hysteresis and good repeatability. Both foil or semiconductor types are used extensively, and each has its own advantages.

The life of metal-foil gauges depends upon the operating strain level; typically it is  $2 \times 10^6$  cycles when they are stressed by 1000 microinches/in. Piezoresistive semiconductor gauges have comparable lifetimes if large strains are avoided.

Although both have the same expected lifetime, the foil gauges are still preferred at high temperatures.

Semiconductor strain elements, although limited by their usable operating temperature range, are employed by such companies as Ramapo, Entran and Sensotec in various transducers that range from flow to acceleration.

Piezoresistive gauges have a resistance variation that is more than a hundred times greater than that of the foil type. Thus if the piezoresistive elements form the arms of a Wheatstone-bridge circuit, large output-voltage changes can be produced. However, these large swings also result in very nonlinear output variations.

Integrated strain elements have improved the resolution of strain gauges. The strain elements usually are mounted on a diaphragm that distorts under pressure. But there are problems with this scheme: It's hard to bond the foil elements onto the diaphragm; the bonding com-

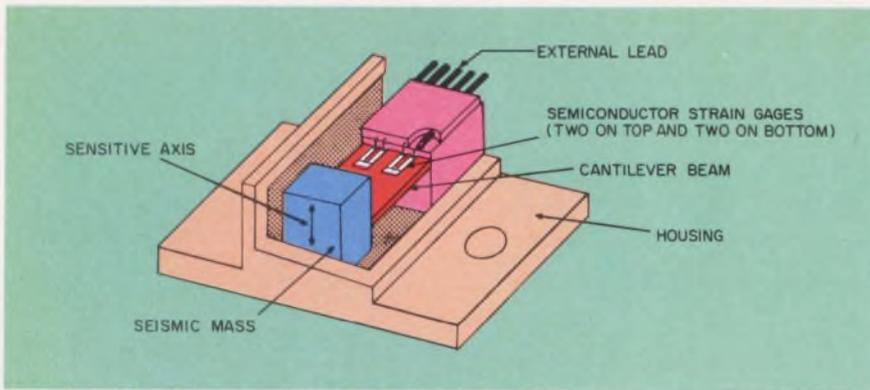
# ERIE RESPONDS. that's why WE'RE NO. 1 WORLDWIDE in Ceramic Capacitors



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The ECG-240 accelerometer from Entran uses semiconductor strain elements within a cantilevered beam and has a piezoresistive output.

pound loosens at high temperatures; strain elements may change position on the diaphragm's surface and the discrete strain elements are limited in frequency range.

To avoid some of these problems, strain elements are now diffused right into a silicon chip, which is then mounted on the diaphragm or, in some cases, becomes the diaphragm itself. Hayer of Gulston predicts that in "four years or so, strain-gauge diaphragms will have the conditioning circuits diffused into them along with the strain elements." These strain transducers should cost about \$5 each in million-piece orders, he says.

### Accelerometer applications grow

Sensors for measuring acceleration are also finding new applications. For instance, nuclear-powered generating plants are using them to detect shaft vibration in generating equipment and thus to help prevent massive generator failures. Several new piezoceramic materials can operate at high temperatures and radiation levels.

Accelerometers, such as those made by B&K Instruments, use piezoelectric materials to measure shock, vibration and, of course, acceleration. Most accelerometers require special signal-conditioning equipment, but this extra equipment is slowly disappearing as more manufacturers include the circuitry inside the sensor case.

Three materials, developed by B&K Instruments, cover a very wide range of applications: MT-8, lead-titanate-zirconate compound, has a high sensitivity (about 300 picocoulombs per newton) and can be used up to 260 C; MT-40, a

ceramic, is useful up to 400 C and has a very flat response curve; and MT-100, a quartz crystal, has the best long-term stability available and is used where low temperature coefficients are needed.

Piezoelectric accelerometers, still the most widely used, have a lot going for them:

- Different models can measure g forces from 0.001 to 100,000.
- Frequency responses can vary from 2 Hz to over 50 kHz.
- Accuracies range to within 3 to 5% of reading.
- Operating temperature ranges cover  $-425$  to  $+1400$  F.
- Prices range from about \$125 to over \$500.

Solid-state strain-gauge accelerometers, in comparison, cover forces from 5 to 1000 g's, frequencies from dc to 10 kHz and work with temperatures from  $-65$  to 250 F. Prices for these devices typically range from \$225 to \$400.

### LVDTs: Old reliables

One of the oldest and still most widely used transducers is the linear velocity displacement transformer (LVDT). There have been many developments that have kept them in the forefront of the field:

- Conversion circuitry to permit operation from dc or ac.
- A tertiary winding that improves resolution.
- Special impregnation compounds for critical environments.
- Better core alloys and better annealing processes to give very smooth magnetic characteristics.
- Internal electronics that does away with all supporting circuitry except the power supply.
- Spun magnetic shields to

eliminate interference from external fields.

The LVDTs provide frictionless measurement—there is no contact between the movable core and the coil structure.

Since there is no mechanical contact, the mechanical life is almost infinite. In addition, because of the physical separation of coil and core, a nonmagnetic material can be interposed. And, since LVDTs operate on an induction principle, they can respond to the most minute motion of the core and produce an output. The symmetry of the LVDT's coils also has another plus—null repeatability.

LVDTs are available for almost any application and at just about any price. Typical specs might read as follows: Input voltage, 6 V rms; frequency range, 50 Hz to 10 kHz; temperature range,  $-65$  to  $+300$  F; null voltage, less than 0.5% full scale output; linear range (depending upon model)  $\pm 0.05$  to  $\pm 25$  in.; sensitivity, typically 0.1 mV/0.001 in./V input and carrier phase shift, at 400 Hz, anywhere from  $+11$  to  $+45^\circ$ . Prices for units vary from \$15 to \$550.

Other types of displacement sensors include magnetic-flux sensing devices such as those manufactured by Electro Corp. The units can sense a change in the magnetic flux surrounding a permanent magnet and coil. When the flux changes, the coil delivers an electrical signal. Airpax and others also make these units.

Some of these flux sensors also include special circuitry that shapes the coil output into transistor-transistor logic-compatible pulses. This circuitry appears either as an IC chip, a hybrid or a discrete component array.

As light-emitting diodes are approaching the cost of incandescent lamps, more circuits that use the spectrally pure characteristics of the LED are being used to measure distance or displacement. A number of companies, including Scientific Technology and Controlcraft, make LED displacement sensors.

Other techniques such as rf or ultrasonic doppler circuits are being developed by Controlcraft to detect motion or displacement. New components are also helping to reduce the size of the complex circuits needed for these methods.

One of the hardest measurements

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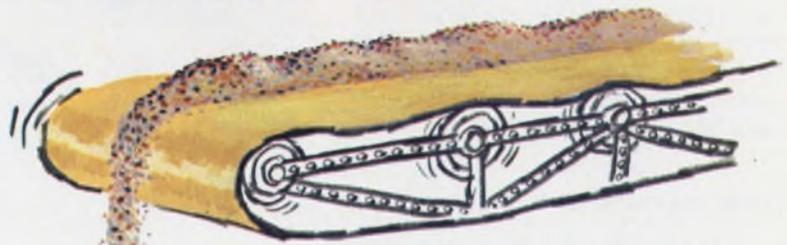
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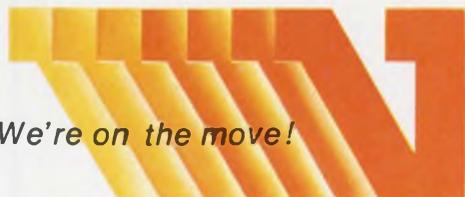
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to make without affecting what you are measuring is flow. There are many methods, including orifice plates, turbine generation, variable area, magnetic fluids, vortex precession, target area and strain gauge. Many different measuring methods are available from companies like Foxboro, Ramapo and Fluidyne.

### Flow measurements made easy

Ramapo, for example, uses foil strain gauges attached to a target within the flow stream. Typical flowmeters for a 1-in. diameter



**Noncontacting foil strain gauge transducers** from S. Himmelstein & Co. have a 200% overload capacity and a linearity of 0.1% of full scale.

tube and that cover a measurement range of 4 to 15 ft./s (equivalent water flow) cost about \$500. They are also usable over temperatures that span -65 to +300 F. Options for the flowmeters permit operation down to -320 F and add anywhere from \$75 to \$300.

Advances in optical design have led to the development of flowmeters that use LEDs and photosensors to determine flow. For instance, SpaceKom has developed an optical flowmeter that can convert fluid flow into equivalent units, in say, miles per gallon or any other scalable unit. ■■

## Need more information?

The companies and products cited in this report have been selected for illustrative qualities. The transducers of these and other companies are identified below. The code to these products indicates what functional area they cover: (A)—acceleration, (D)—displacement, (F)—flow, (L)—load, (P)—pressure, (S)—strain and (T)—temperature.

Acurex Corp., 485 Clyde Ave., Mountain View, Calif. 94042. (415) 964-3200. (T. Tilton). (D) **Circle No. 400**

Airpax Electronics, Inc., Controls Div., 6801 W. Sunrise Blvd., Fort Lauderdale, Fla. 33313. (305) 587-1100. (P Webster). (D) **Circle No. 401**

Astrosystems, Inc., 6 Nevada Dr., Lake Success, N.Y. 11040. (516) 328-1600. (G. Steinberg). (D) **Circle No. 402**

B & K Instruments, Inc., 5111 W. 164th St., Cleveland, Ohio 44142. (216) 267-4800. (B. Rhodes). (A) **Circle No. 403**

BLH Electronics Inc., 42 Fourth Ave., Waltham, Mass. 02154. (617) 890-6700. (H. Owens). (D,L,P,S,T) **Circle No. 404**

Bell & Howell, 360 Sierra Madre Villa Ave., Pasadena, Calif. 91109. (213) 796-9381. (R. Batiste). (A,P) **Circle No. 448**

C. J. Enterprises, P.O. Box 4134, Panorama City, Calif. 91412. (213) 764-2529. (M. Cantor). (P,S) **Circle No. 405**

Climatronics Corp., 1324 Motor Pkwy., Hauppauge, N.Y. 11787. (516) 234-2772. (T. Schreiber). (D,T) **Circle No. 406**

Columbia Research Labs., MacDade Blvd. & Bullens La., Woodlyn, Pa. 19094. (215) 532-9464 (J. Sarty). (A,L,P,S) **Circle No. 407**

Computer Conversions Corp., 6 Dunton Ct., East Northport, N.Y. 11731. (516) 261-3300. (S. Renard). (D) **Circle No. 408**

Controlcraft Corp., 213 Main St., West Chicago, Ill. 60185. (312) 231-7511. (R. Warner). (D) **Circle No. 409**

Crystal Technology Inc., 2510 Old Middlefield Way, Mountain View, Calif. 94043. (415) 961-9311. (L. Castelli). (A, P) **Circle No. 410**

Davco Manufacturing Co., 169 Ridgedale Ave., Morristown, N.J. 07960. (201) 267-4990. (J. Pappas). (D) **Circle No. 411**

Electro Corp., 1845 57th St., Sarasota, Fla. 33580. (813) 355-8411. (G. Gee). (D) **Circle No. 412**

Endevco, Rancho Viejo Rd., San Juan, Capistrano, Calif. 92675. (714) 493-8181. (R. Quackenbush). (A) **Circle No. 413**

Entran Devices, Inc., 145 Paterson Ave., Little Falls, N.J. 07424. (201) 785-4060. (W. Caplan). (A,L,P,S) **Circle No. 414**

Figaro Engineering, 3-15-6 Higashiyonaka, Toyonaka City, Osaka, 560, Japan. (K. Tsukada). (Gas) **Circle No. 415**

Fluidyne Instrumentation, 1631 San Pablo, Oakland, Calif. 94612. (415) 444-2376. (R. Jennings). (F) **Circle No. 416**

Foxboro, Foxboro, Mass. 02035. (617) 543-8750. (E. Seifert). (F,L,P,S,T) **Circle No. 417**

General Eastern Corp., 36 Maple St., Watertown, Mass. 02172. (617) 923-2386. (T. Richardson). (T) **Circle No. 418**

Genisco Technology Corp., 18435 Susana Rd., Compton, Calif. 90221. (213) 537-4750. (J. Muhleman). (A,P) **Circle No. 419**

Gilmore Industries, Inc., 3355 Richmond Rd., Cleveland, Ohio 44122. (216) 464-1200. (W. Heisler). (S) **Circle No. 420**

Gulton Industries, Inc., Metuchen, N.J. 08840. (201) 548-2800. (A. Orlicchio). (A,D,P,S) **Circle No. 421**

Gulton Industries, Inc., P.O. Box 4300, Fullerton, Calif. 92634. (714) 871-2150. (C. Edmiston). (A,D,P,S) **Circle No. 422**

HH Controls Co., Inc., 16 Frost St., Arlington, Mass. 02174. (617) 646-2626. (W. Edins). (D) **Circle No. 423**

Hy-Cal Engineering, 12105 Los Nietos Rd., Santa Fe Springs, Calif. 90670. (213) 698-7785. (A. Bowman). (T) **Circle No. 424**

ITT Barton, 580 Monterey Pass Rd., Monterey Park, Calif. 91754. (213) 283-6501. (G. Mechelin). (F) **Circle No. 449**

Keystone Carbon Co., St. Marys, Pa. 15857. (814) 781-1591. (T. Krellner). (T) **Circle No. 425**

Massa Corp., 280 Lincoln St., Hingham, Mass. 02042. (617) 749-4800. (M. Howard). (D) **Circle No. 426**

Metritape, Inc., 77 Commonwealth Ave., W. Concord, Mass. 01742. (617) 369-7500. (D.F.) **Circle No. 427**

Micro-Radian Instruments, 116 Main St., Seal Beach, Calif. 90740. (213) 598-2722. (T. Thurston). (D) **Circle No. 428**

National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, Calif. 95051. (408) 732-5000. (B. Hess). (P,T) **Inquire Direct**

Non-Linear Systems, Inc., 533 Stevens Ave., Solana Beach, Calif. 92075. (714) 755-1134. (P) **Circle No. 429**

Omega Engineering, Box 4047, Springdale Station, Stamford, Conn. 06907.

(203) 359-1660. (C. Gessner). (T) **Circle No. 430**

Ormond, Inc., 11969 East Rivera Rd., Santa Fe Springs, Calif. 90670. (213) 698-0641. (J. Wilbur). (L) **Circle No. 431**

PCB Piezotronics, Inc., P.O. Box 33, Buffalo, N.Y. 14225. (716) 684-0001. (J. Lally). (A) **Circle No. 432**

Ramapo Instrument Co., Bloomingdale, N.J. 07403. (201) 838-2300. (G. Anderson). (F) **Circle No. 433**

Relco Products, Inc., 2133 S. Bellaire St., Denver, Colo. 80222. (303) 756-1143. (R. Ruehle). (T) **Circle No. 434**

S. Himmelstein & Co., 2500 Estes Ave., Elk Grove Village, Ill. 60007. (312) 439-8181. (J. Hall). (S) **Circle No. 435**

Schaevitz Engineering, U.S. Rte. 130 & Union Ave., Pennsauken, N.J. 08101. (609) 662-8000. (H. Schaevitz). (A,D,P) **Circle No. 436**

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Sensors, Inc., 3908 Varsity Dr., Ann Arbor, Mich. 48104. (313) 973-1400. (D. Giles). (T) **Circle No. 438**

Sensotec Inc., 1400 Holly Ave., Columbus, Ohio. 43212. (614) 294-5436. (C. Easton). (L,P) **Circle No. 439**

Singer, 1150 McBride Ave., Little Falls, N.J. 07424. (201) 256-4000. (D. Katz). (A,D) **Circle No. 440**

SpaceKom, Inc., P.O. Box 10, Goleta, Calif. (805) 967-7114. (G. Spacek). (F) **Circle No. 441**

Spectran Instruments, P.O. Box 891, La Habra, Calif. 90631. (213) 694-3995. (T) **Circle No. 452**

Statham Instruments, 2230 Statham Blvd., Oxnard, Calif. 93030. (805) 487-8511. (G. Bourke). (P) **Circle No. 442**

Tempo Instruments Inc., E. Bethpage Rd., Plainview, N.Y. 11803. (516) 694-4402. (H. Pinto). (D) **Circle No. 452**

Tensitron, Inc., Harvard Depot Rd., Harvard, Mass. 01451. (617) 456-3511. (E. Saxl). (D,L,P) **Circle No. 443**

Thermo Electron Corp., 101 First Ave., Waltham, Mass. 01451. (617) 890-8700. (J. Beville). (P) **Circle No. 444**

Transducers Inc., 12140 East Rivera Rd., Whittier, Calif. 90606. (213) 945-3741. (H. Nielsen). (L,P) **Circle No. 445**

Trans-Tek Inc., Rte. 83, Ellington, Conn. 06029. (203) 872-8351. (S. Scyocurka). (D) **Circle No. 446**

Tyco Instrument Div., 4 Hartwell Pl., Lexington, Mass. 02173. (617) 861-7450. (R. Cerchione). (L,P) **Circle No. 447**

Vibra-Metrics, Inc., 150 Bradley St., East Haven, Conn. 06512. (203) 467-6335. (J. Judd). (A) **Circle No. 450**

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# Inflation, energy, semiconductors to dominate tomorrow's electronics

Almost every industry and government leader who spoke at a recent London conference emphasized three key factors that will dominate the electronics industry in the coming decade. In one way or another, they said, the industry will be affected dramatically by inflation, energy consumption and all-pervasive semiconductors.

The first speaker at the conference "Tomorrow in World Electronics," sponsored by ELECTRONIC DESIGN, the Financial Times, Electronics Weekly and British Airways, set the stage. Sebastian de Ferranti, chairman and managing director of Ferranti Ltd. pointed out that the recent fuel crisis drew attention to the fact that the era of very cheap fuel is finished. A more energy-conscious economy, he said, will develop energy by more capital-intensive means that will be initially more expensive, but will produce over-all economy.

While such schemes develop, Ferranti continued, applied electronics will grow rapidly, unaffected

by temporary or longer term alarms about energy economy. This is because most electronic devices use little energy so they provide good value for fuel. Further, a move towards real economy in energy consumption would stimulate electronic expansion.

## Energy quality vs. quantity

Taking a different tack, Dr. Edward David, Jr., executive vice president of Gould Inc., and former science advisor to President Nixon, made two basic assertions. First, he said, our post-Industrial society is moving from an energy-intensive society to an information and data-intensive one. And second, we will see greater emphasis on energy quality rather than quantity.

This progression comes about because, as a country develops, it tends to spend more on services—education, medical care, travel—and less on material goods. The evolution, David continued, is from machinery for manufacturing, mining and other production of goods, toward measurement, control and communications.

Actually, he went on, there is no

shortage of energy. The shortage is of energy available where and when it is required, in the form needed, and convertible to useful work efficiently. There are, in fact, vast amounts of energy available from unconventional fossil sources, the sun and the oceans. But the quality of these resources makes the energy available only with difficulty and at high cost because of expensive extraction techniques, low energy density, inconvenient location and form.

As an example of what remains to be done, David showed (Fig. 1) that the volume and weight of a battery in an electronic watch exceed that of the other components. There is great progress, though, in developing higher-energy-density battery systems. Two very promising examples lie in the zinc air battery, which uses air as one reactant, and the lithium battery, which uses highly reactive and light lithium as an anode.

More advanced battery systems (Figs. 2 and 3) may furnish even greater advantages in specific applications.

## The driving force: inflation

As the electronics industry expands, and all speakers at the conference agreed that it would, its biggest cause for anxiety will be the general problem facing industry in all advanced countries. That problem, according to David Price, Member of Parliament, chairman of the Parliamentary and Scientific Committee, and a founder of the Committee on Science and Technology, will be how to live with and adapt to mounting inflation and the inevitable oscillations of governments in their counter-inflationary policies.

Most industries, Price pointed

George Rostky  
Editor-in-Chief

Component	Minimum	
	Dimen., cm	Volume, cm <sup>3</sup>
Battery	0.42	0.88
Quartz Crystal	0.28	0.13
Electronics	0.13	0.016
Display	0.09	0.21

1. Space required by the battery is out of proportion to that needed by other components in an electronic watch. This is an area that needs improvement.

Even when it was only \$35 an ounce, gold was expensive. That's why we started long ago to reduce the amount of gold in our contacts to a minimum.

In 1958 we developed a really reliable gold dot contact. And no matter what anyone else says, only silver and copper are better electrical conductors than gold

(but gold doesn't oxidize or corrode).

Over the years we've been able to reduce the cost because we reduced the gold.

And we've been reducing the amount over the years without reducing the mechanical or electrical quality of our connectors.

Now, after all these years, we

find out that we not only reduced cost but we've been making our own small contribution to solving our country's gold problem.

And all because we wanted to design a more economical, more reliable gold-contact connector.

**GTE SYLVANIA**

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## Our small contribution to solving the gold problem.



Battery	Wh/Lb	W/Lb	\$/kWh	Life Cycle	Projected Availability
<b>Group I</b>					
Lead-Acid	16-18	25	20-50	300-2000	Now
Nickel-Iron	20-30	60	20-30	300-400	1976
Nickel-Zinc	30-40	75	20-25	250-350	1977
<b>Group II</b>					
Zinc-Chlorine (Hydrate)	60	60	10-20	500*	1978-79
Lithium-Sulfur	60-80	100	15-20	1000*	1980-85
Sodium-Sulfur	80-100	100	15-20	1000*	1980-85

\*Nominal life based on current experimental models.

**2. Characteristics of today's lead acid battery and other energy sources that are likely to be available in the future.**

out, have learned to adapt to some inflation without too many tears. But the rates of inflation currently being experienced are of a new and punishing order. All, he said, were much higher than have been experienced in previous years. He cited figures based on cost-of-living indices for the past 12 months and for the preceding year.

A few years ago, Price reminisced, we worried about a 3% continuing inflation. But today, he said, "I know of no government which knows how to keep inflation down to an annual rate of 3%—and get itself elected. For the electronics industry," he continued, "my message is very simple: Fasten your seat belts; you're expecting turbulence ahead."

**Role of government profound**

Government is important—not only in its role as inflation fighter. The electronics industry, Price pointed out, depends largely on government purchasing and on government specifications and standards. This point was emphasized by Dr. Ieuan Maddock, chief scientist of the British Department of Trade and Industry. "In nearly every country in the world," he pointed out, "you'll find government, in one form or another, provides a considerable amount of research and development funding of the electronics industry." And government is a very large customer of the industry—in defense, in those matters that concern safety, like

air-traffic control, and in telecommunications and broadcasting.

The deep involvement, said Maddock, creates a special problem, as it may have overemphasized R&D. We tend to look at the future of our industry in terms that outdate the product we are producing now. We persuade our customer that the thing he must buy now is out of date by 1980. We have an enormous technological push constantly to outdate the present. So every product has a limited lifetime.

**Electronics bucks inflation**

The electronics industry has certainly contributed to the "constant outdating" problem. But it has added little to inflation. In fact, many components and equipments have successfully resisted or, at times, overcome, the inflationary tide—directly and indirectly.

Earl Wantland, president of Tektronix, Inc., pointed out that a dc-to-20 MHz oscilloscope sold, in 1950, for \$1650—roughly \$3350 in today's dollars. Today, for \$3350 you can buy a scope with 10 times the bandwidth and 50 times the sensitivity. And it could include new features like delaying sweep, CRT readout of measurement parameters and greater display brightness, along with other convenience features.

He gave a further example, based, largely, on the marriage of the computer with instruments. The average salary of an engineer runs to about \$15,000 to \$20,000. The

installed value of his complement of instruments is about \$15,000 to \$20,000. But his salary is an annual expense, while the cost of his equipment is a one-time expenditure. And instruments that allow an engineer to do his work faster pay off handsomely.

One of the key responsibilities of instrumentation companies, Wantland suggested, is to supply the measurement tools for developing advanced technologies—a never-ending requirement.

The art of waveform measurements has made substantial progress already, Wantland said. But we are now on the threshold of even greater advances. A waveform has a lot of information that is not apparent from viewing it alone. So we'll need further computer processing and, in turn, smaller digitized increments for a computer to process. Digitization is relatively easy for waveforms that change slowly. It is far more difficult with incredibly fast waveforms like those encountered in nuclear physics and laser physics.

Today we can capture an event that lasts only 5 ns and hold the waveform in digitized form so that we can divide it into 500 slices, each representing 10 ps. But in the area of fast transient phenomena, we can't stop. Each achievement calls for the next, as scientists and engineers demand to see and understand more.

Further, when we take a digitized pulse waveform, we can perform the mathematical conversion from time domain to frequency domain via the Fourier transform. This technique is particularly useful in transmission systems as it provides a "signature" of the system that can be used for later troubleshooting.

Such an application is characteristic of the instrumentation industry; instruments extend the human mind by an easy-to-use interface to electronic calculations.

**Instruments to become smarter**

John Fluke, chairman of John Fluke Mfg. Co., emphasized some of the points made by Wantland. Tomorrow's instruments, he said, will increasingly relieve the engineer of calculation burdens. In addition more of them will be capable of operation by remote control.

The instrument manufacturer will be called upon to provide better service, Fluke said, today's being inadequate. Because of the lower cost of instrument, he will have to learn to distribute them better; he still doesn't know how.

Instruments will show greater emphasis on low power, small size and portability. So the use of rechargeable batteries will give way to disposable batteries.

Because of increasingly stringent reliability requirements, instruments, like other manufactured products, will increasingly be checked by something sufficiently stupid not to ask questions—something like automatic test equipment. So the cost of an instrument's labor content will be reduced. LSI will help reduce the cost and it will help improve reliability.

As LSI technology settles, instrument manufacturers will have to develop their own LSI-design capabilities. Because the instrument represents a considerable amount of originality, reliability and usability, and because of the close coupling required between instrument and LSI designer, the instrument manufacturer won't be able to relegate LSI design to outsiders.

### Integrating up and down

While Fluke saw instrument manufacturers driven to downward integration, another speaker, Dr. Morris Chang, group vice president of Texas Instruments, saw semiconductor manufacturers integrating upward. Chang pointed out that momentum has increased for semiconductor manufacturers to expand into systems business, but he argued that the reverse motion is less likely.

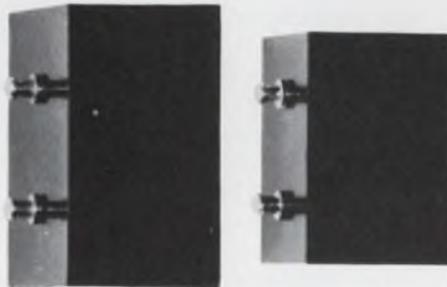
The first barrier to downward integration is that the systems manufacturer may not have semiconductor technology, and would require considerable time, investment and talent to develop it. The second barrier is that a systems manufacturer would have to develop a large production base in semiconductors and sufficient research and development to remain competitive.

On the other hand, said Chang, the drive to integrate upward is easier and it can be very fruitful.

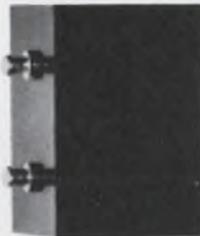
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## HEINEMANN

The most important motivation is higher growth resulting from increased value added for products where the principal function is already performed by semis.

As an example, consumer calculators have a semiconductor content of 30-35%. So if the manufacturer sells semiconductors to a calculator manufacturer he gets, say, \$15 of sales. But if he makes and sells the calculator himself, he gets \$45 of sales. Similar increases in value added exist, said Chang, in minicomputers with semiconductor memories. For data terminals, point-of-sale systems and electronic watches, the multiplying factor is even larger.

In other areas, however, the arithmetic is not so encouraging. Semiconductor manufacturers don't really know picture-tube technology, for example. So color TV is not an easy candidate for vertical integration by semiconductor manufacturers in the near term.

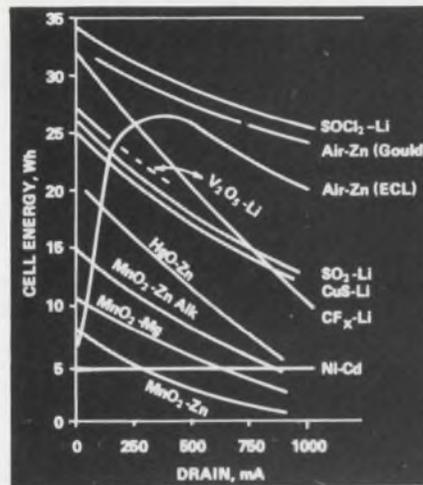
Similarly, the systems marketing, software and other technologies required in mainframe computers constitute great barriers to upward integration.

Another reason for upward integration is that the rapid advance of semiconductor technology has shrunk the product lifetime of end equipment, and this demands close coupling between the device manufacturer and the end market.

This rapid advance is best illustrated in the electronic calculator. In 1966 a four-function calculator sold for almost \$1500 and used more than 1000 transistors and diodes. In 1968, integrated circuits made calculators with transistors and diodes obsolete. In 1970 the MOS LSI calculator hit the market. And in 1971 a single MOS chip was sufficient for a four-function calculator. So the average life of a calculator has been no more than one or two years.

Similar changes can be seen in minicomputers and in electronic timepieces. So the rapid pace demands that the design of the semiconductor component, if it can still be called a component, proceed in parallel with the design of the end equipment.

While such parallel development can be done between a component vendor and a systems customer, trade secrets and proprietary inhibitions tend to make parallel de-



3. Cell energy as a function of current drain for several battery systems in D-cell size.

velopments between two companies less satisfactory than parallel developments within the same one.

Further, as semiconductor components become more complex, the investment required becomes more substantial. Rapid product obsolescence allows only a short time window in which to recover the investment. It thus becomes essential for the semiconductor manufacturer to use this window to the maximum by getting the end equipment to the market as early as possible.

Vertical integration doesn't benefit the semiconductor manufacturer alone. It provides a new element of competition in the end-equipment market, so it gives end customers a more competitive supply situation and gives them an advantage in cost and in wider choice of equipment.

The traditional systems manufacturer derives benefits, too—lower component cost and broader markets resulting from lowered semiconductor cost. As an example, it was estimated in 1971 that a portable calculator retailing for \$200 would open the large consumer market. It did. When the price was cut to the \$150 range, the market more than quadrupled. And it took another dramatic spurt when the price dropped to less than \$100.

### Semis to grow even faster

The growth of semiconductors suggested by Chang was made more explicit by Dr. C. Lester Hogan, president, Fairchild Cam-

era and Instrument Corp. Hogan argued that the greatest growth years of semiconductors lie ahead.

While the semiconductor market outside the United States is now larger than that within the U.S. and will continue to grow in comparison, the over-all market will continue to grow so rapidly that the U.S. total market will increase, despite the fact that its percentage of the total will decline.

The mix of semiconductor usage will change, too. By 1980 sales of discrete semiconductors will decrease from 51% to 39% of the total. But because total semiconductor usage will increase dramatically, discrete volume will actually increase—from \$2.7 billion to \$4.5 billion.

Percentagewise, bipolar digital ICs won't grow as fast as MOS, but each should enjoy an annual market of about \$2.5 billion in 1980. Today's projections don't include new technologies—like charge-coupled devices, which should reach some significant volume in 1980. The CCD is slower than MOS, but it can be a lot cheaper, perhaps 1/10 the cost.

### 100,000 bits per chip

The CCD may open up many new applications. It has already found a place in imaging devices. And it may find a place as a replacement for fixed-head disc memories—though it seems unable to compete with floppy discs, which appear much cheaper. But the whole architecture of computers might change as charge-coupled devices become available with complexities of, say, 100,000 bits on a chip, speeds that may be 10 to 20 times faster than today's fixed-head discs, and with 1/10 the cost.

So the semiconductor industry will expand, not only because of the normal expansion of its traditional customer base, but also by technological substitution—where solid state replaces electromechanical devices. Further, it will grow in applications not possible with other technologies—timepieces, calculators, appliances and what have you.

Dr. Robert Heikes, managing director of Motorola Europe, underscored Hogan's optimism. He pointed out that the world electronics industry is growing about 50% faster than the world economy.

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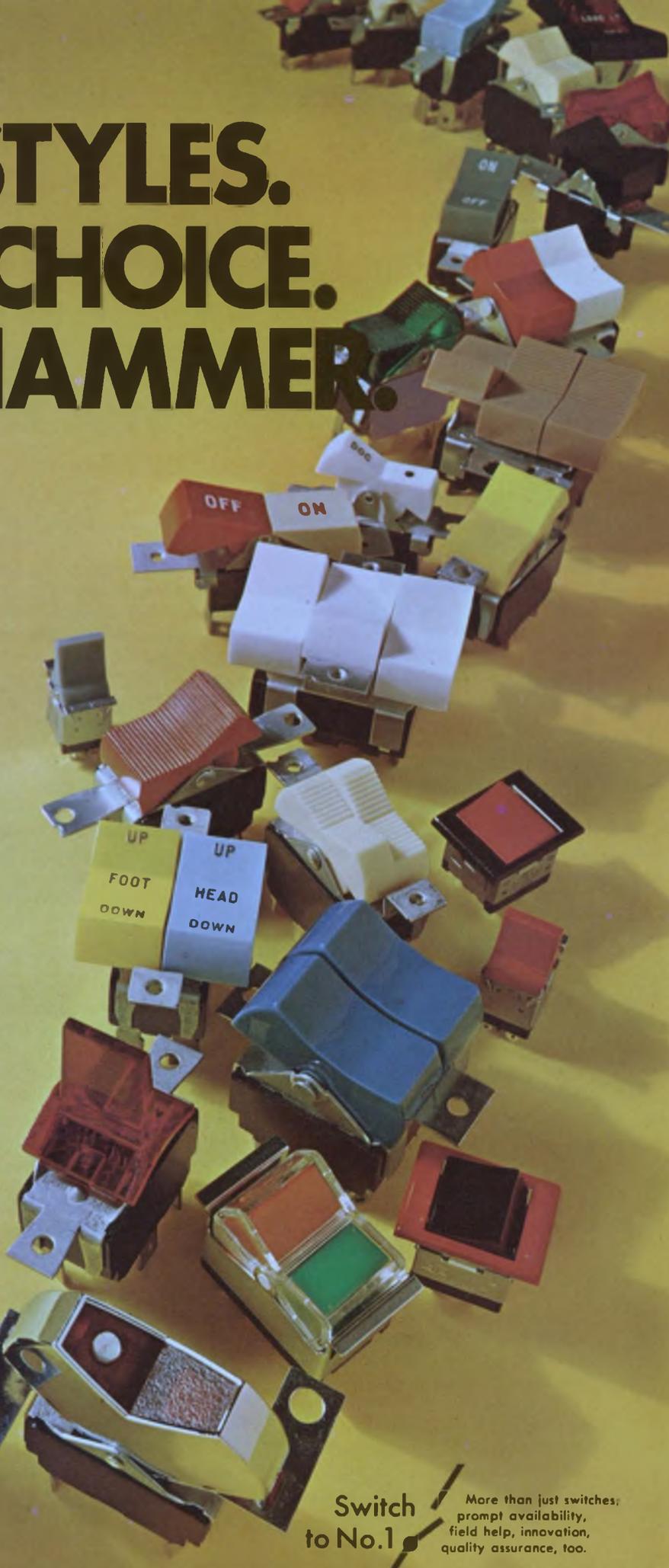
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More than just switches:  
prompt availability,  
field help, innovation,  
quality assurance, too.

Year	1950	1955—1955		1965—1965		1970
Device	Thermionic valves	Better Valves	Transistors	Better Transistors	Integrated circuits	Better Integrated circuits
Speed	1 $\mu$ s	100 ns	200 ns	10 ns	25 ns	2 ns
Signal size	$\approx$ 50 V	$\approx$ 50 V	<5 V	<5 V	<5 V	$\approx$ 1 V
Power dissipation	1 W	5 W	100 mW	100 mW	15 mW	30 mW
Gate packing density	< 50/ft <sup>3</sup>		$\approx$ 500/ft <sup>3</sup>		$\approx$ 5000/ft <sup>3</sup>	
Mean life	$\approx$ 10 <sup>1</sup> Hr		$\approx$ 10 <sup>7</sup> Hr		$\approx$ 10 <sup>8</sup> Hr/Circuit	

4. **Component progress has been startling** in a mere two decades. Speed, density and life have soared while power and signal level have plummeted.

And the semiconductor industry, in turn, is growing about 50% faster than that.

This almost explosive growth has been a result of a repeating cycle to increase volume and lower costs through applications leading, in turn, to increased volume and lower costs. The semiconductor industry, in fact, has been one of the few in which price per function has steadily decreased in spite of continuing inflation. It now appears though, Heikes conceded, that world leaders have finally designed an inflation rate that we may not be able to beat.

Because of the rapid pace of technological development, the semiconductor business is quite unforgiving to managerial errors. So the business has two main needs—speed of entry and access to the largest possible market. These create an impetus for semiconductor manufacturers to integrate upward.

#### Semis vs software

Equipment manufacturers can integrate downward into semiconductors, but Heikes felt this would have little likelihood of success. Or, he said, they could concentrate more on software, marketing and other aspects of the business while maintaining tight coupling with existing semiconductor manufacturers. Taking such a scenario a step further, Heikes concluded that any country lacking a competitive semiconductor business would be forced more and more into the software and marketing end of the electronics business.

The choices, then, boil down to encouraging the formation of indigenous competitive suppliers, encouraging the formation of foreign competitive suppliers and adjusting conditions so that local electronics manufacturers can get semiconductors at the same price as U.S. manufacturers so as to be competitive on a world market.

The multinational semiconductor companies, despite the emotionalism they may provoke, are the instruments for assuring the most rapid diffusion of semiconductor technology throughout the world. And semiconductors are basic to almost all technological progress.

#### Dramatic progress in computers

The contribution of semiconductors has been particularly dramatic in computers. Gordon Haley, manager of systems technology, ICL Computer Development Div., pointed to dramatic examples. From 1950 to 1970 (Fig. 4) semiconductors provided a 500:1 improvement in component speed while slashing component cost 20:1. And they provided other dramatic advances as well. Their contributions haven't stopped. We can expect further improvements (Fig. 5).

We can evaluate computer progress, said Haley, on the basis of user needs. These include more processing power, more throughput per unit cost, faster response time per transaction, reduced overhead in data-base management, higher reliability and systems resilience, distributed facilities with adequate intercommunications, growth and continuity, and better man-machine

communications.

The last depends on humanizing the input and output with visual-display output, pattern recognition on input, condensation and selection of output documents, voice input and output, privacy and improved languages.

The obstacles to technological progress, Haley pointed out, are cost, speed of light, thermal considerations, reliability, noise immunity, the lack of standards and complexity.

While superficially the hardware structure of computers has changed little in 20 years, the packaging has changed dramatically. Components are still mounted on packages that are plugged into backplanes, an assembly of which constitutes the complete functional unit. But the logic content of the units and subunits has changed. Packages in one generation become standard components in the next. A complete CPU of the early 1950s is now realizable on a single chip of silicon.

#### Consumer electronics, too

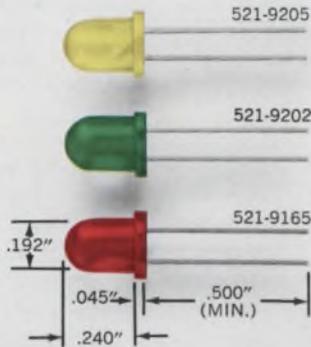
While the impact of semiconductors on computers has been most dramatic, semis had a profound effect, too, on consumer products like radio, tape products, audio products, video recorders and players. But only recently, said Dr. William Hittinger, executive vice president, RCA Corp., has there been a major shift away from vacuum-tube or hybrid sets to all solid state.

The consumer-electronics market, said Hittinger, breaks down into two categories—entertainment and non-entertainment—which are bound to become more fuzzy as we go along. While both areas will grow substantially in the years to come, each will be faced with problems of standardization. There are today, for example, various techniques for home video recording and for preparing pre-recorded video material from a disc or record. Both types of products should find a substantial market in a few short years, but their growth could meet considerable problems. This is especially true for video disc.

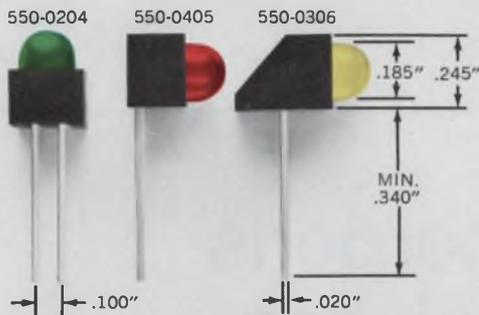
"I wish I could hold out hope," Hittinger said, "for early standardization of video disc, but it just is not so and is not likely to take place." The answer, he said, will

# Dialight sees a need:

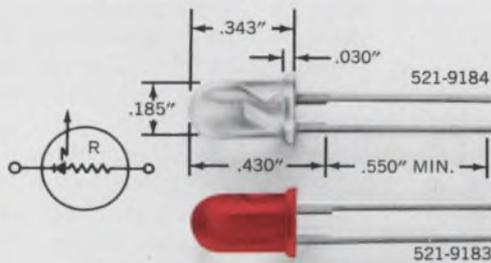
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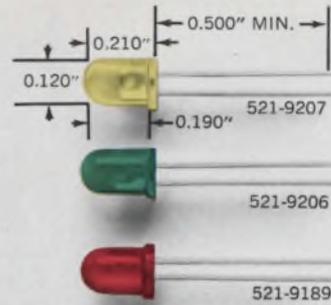
Now available in green, yellow and red. Mini-sized for maximum front panel density and easy panel mounting. High luminous intensity, low cost. Vibration/shock resistant. Solid state for long life. Wide viewing angles. Ideal for applications like panel lighting, film annotation and alpha-numeric displays.



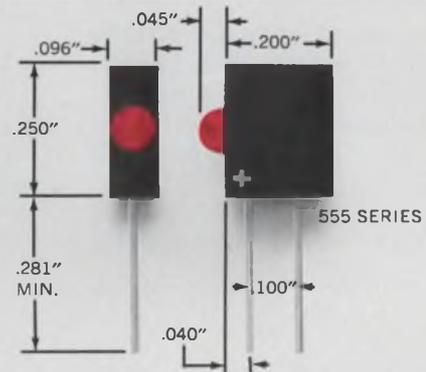
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Available in red or clear LED packages with or without a built-in current limiting resistor. Red LED is also made without resistor. Suitable for circuit status indication, alpha-numeric displays and visual indicators. Features long wire-wrappable leads. IC compatible with solid state reliability. High luminous intensity, low power consumption, low cost.



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come on the basis of who can bring a product to the market first and demonstrate that it works.

There are other products for which the technology exists today, but the limits are socio-economic and legal. Such products include the TV home-information center, computer terminals and facsimile sets in the home, home library and the home newspaper.

As an example of the type of problem one can anticipate, one can look at cable television. It has been with us for many years—first, for remote areas with poor off-the-air reception, then later, in large cities, where image reflection for color transmission has been a major problem. This industry has been slowed by complex matters like conflicts with the broadcasting industry and copyright of material being rebroadcast over cable systems. These issues are far from resolved.

According to another speaker, Dr. Ferdy Mayer, president of

	1950	Improvement factor	1970	Improvement factor	1990
Speed	1 $\mu$ s	500	2 ns	40	.05 ns
Signal size	50 V	50	1 V	5	0.2 V
Power dissipation	1 W	33	30 mW	30	1 mW
Gate packing density	50/ft <sup>2</sup>	100	5000	1000	5 $\times$ 10 <sup>6</sup>
Mean life	10 <sup>4</sup> Hr	10,000	10 <sup>8</sup>	1000	10 <sup>11</sup>
Cost	1	20	1/20	50	1/1000

**5. Our components are likely to improve dramatically.** Even where the progress in the next two decades is not as startling as it has been in the past the progress should have profound effects on tomorrow's computers.

Laboratoire d'Electronique et d'Automatique Dauphinois, electronics has just begun to penetrate the automobile. Mayer showed dozens of possible applications beyond the widely publicized ones like electronic ignition, seat-belt interlocks, pollution controls and anti-skid systems.

One of the most intriguing is a system that would store the profile of an ideal driver and provide a "standard driver's index." A com-

puter would prepare a "driver performance index" for the person driving the car and compare the driver performance index with the standard driver's index. The concept here is to reward the good driver, rather than punish the bad one.

The remaining papers at the conference dealt mainly with political and economic problems associated with electronics in Europe and the rest of the world. ■■

## Picosecond timing sharpens laser-rangefinder resolution

A novel method of picosecond timing is reported to give laser rangefinders such accuracy that measurements of continental drift and the wobble of the earth on its axis will be possible.

Resolution of 1 to 3 cm at distances up to 3000 km is listed by the designer, Aerospace Corp., of El Segundo, Calif., and the current program objective is to achieve resolution of  $\pm 0.7$  cm.

"The best laser rangefinders to date have only about 15-cm resolution at satellite-to-earth distances," says Kurt Golden, staff scientist at Aerospace.

Golden reports that NASA will experiment with the new timing in four laser rangefinders on the ground and one on a satellite. Those on the ground will be placed at different locations and used to position the satellite by triangula-

tion. The rangefinder on the satellite will measure the distance to any point on the earth. By measuring the distance to several points on the ground over a period of time, the relative motion of those points relative to each other can be determined. Golden notes that continental drift is on the order of 5 cm a year.

### Picosecond timing essential

Timing accuracy of  $\pm 40$ -50 ps is necessary to get range resolution of  $\pm 0.7$  cm. Conventional time-interval measurement techniques can't even come close to that. Typical timing accuracies with conventional techniques are on the order of  $\pm 1$  ns.

The timing technique used by Golden makes use of an image converter tube with rapidly driven de-

flection plates. Timing is related to the deflected position of the return laser pulse relative to the position of the transmitted pulse.

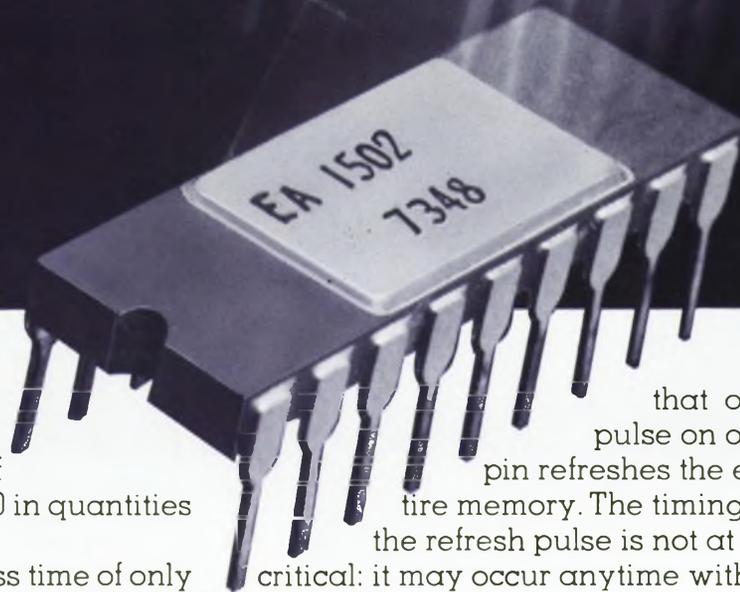
A Q-switched, mode-locked ruby laser at 6943 Å is fired to initiate the ranging operation. A trigger pulse is then delivered to the master timing control circuitry for a reference. The ranging pulse travels to the target and returns to the receiving optics.

Samples of the transmitted and received optical pulses are diverted by beam splitters to fast photomultiplier detectors, whose electrical outputs are used to start and stop a commercial time-interval meter (Golden is using a Model 536 meter from NanoFast, Chicago). The time-interval meter indicates pulse transmission time or range.

Start and stop enable gates are

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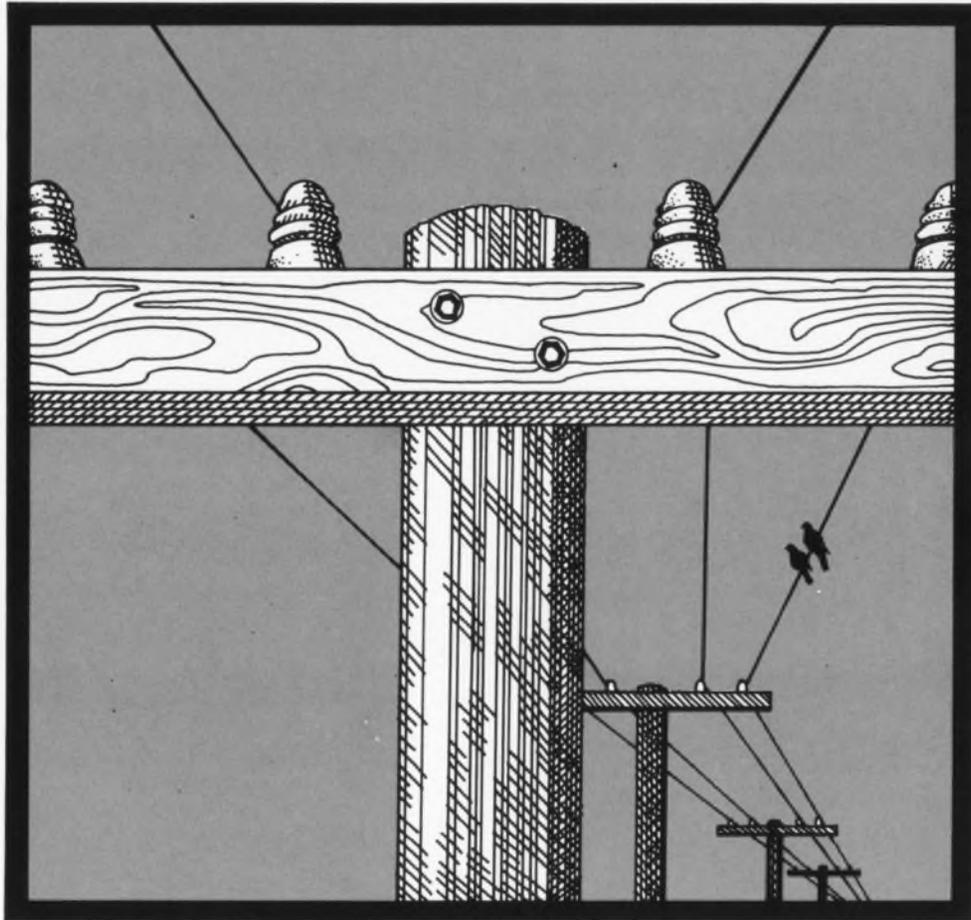
The pin-out of this 18-lead DIP is identical to the 1103. Although signal levels and shapes are different, you can replace 1103s with this speedier RAM without a total rework of your PC board.

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For critical resistance measurements the instrument provides completely isolated four terminal ohms with less than 4 volts open circuit from 200 ohms through 20 megohms.

So there are the specs.

Impressive? We think so. But remember—specs are one thing. That name on the panel, however... It's what makes a Cadillac a Cadillac.

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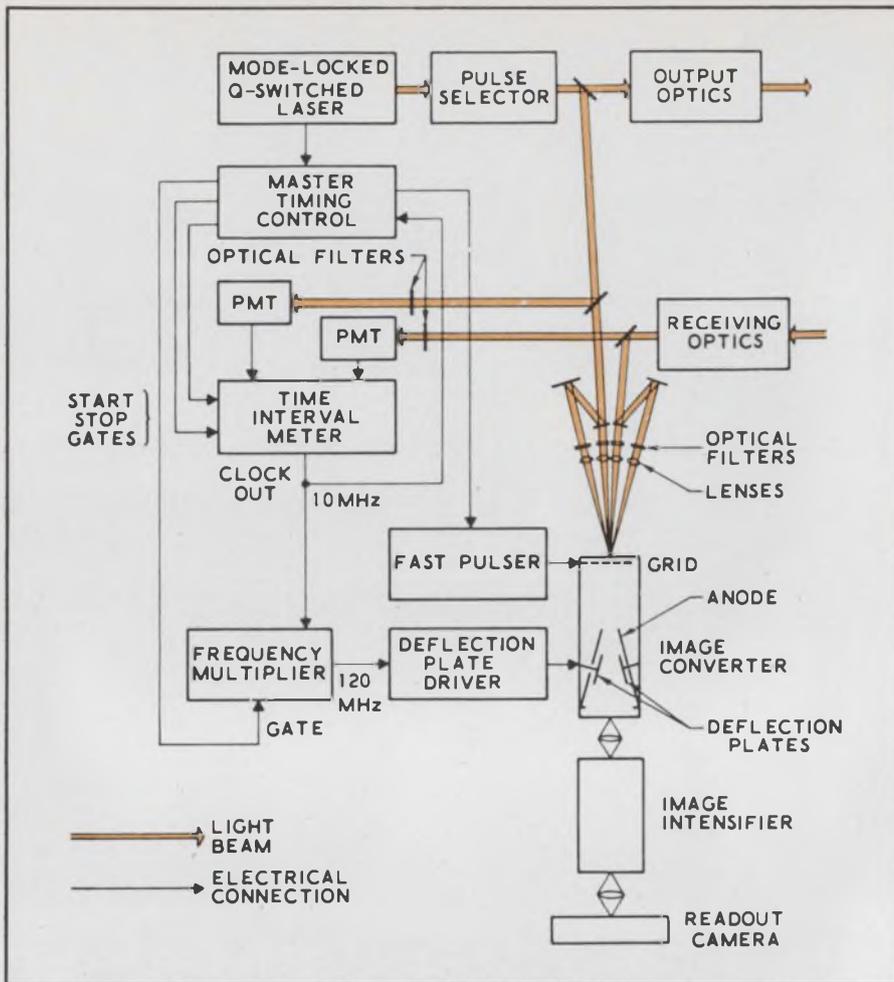
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Laser-range finder resolution of 1 to 3 cm at distances of 3000 km is reported with the picosecond timing scheme shown here. Coarse ranging is done with a timer-interval meter, and fine ranging by measurement of the relative positions of spots of light created by an image converter.

provided to the time-interval meter by the master timing control to minimize any effect of spurious pulses. These gates are provided at approximately the expected times of arrival of the start and stop pulses and are long enough to compensate for uncertainties in the expected arrival times. In a satellite-to-earth system, says Golden, atmospheric range uncertainties go from 1 cm when the satellite is at its zenith to about 6 cm when it is 15 degrees above the horizon.

With the time-interval meter, coarse range measurements of  $\pm 15$ -cm resolution are possible. To get finer resolution, a vernier system is used. Samples of the transmitted and received light pulses are focused on the photocathode of an image-converter tube equipped with a pair of deflection plates.

Each of these pulses is split fur-

ther by an optical beam splitter, and half the energy of each pulse is optically delayed before being focused on the image-converter photocathode. These four different light beams are arranged to produce four small spots of light, one above the other, on the photocathode. The line of spots is perpendicular to the direction in which the image-converter deflection plates deflect photoelectrons.

#### Timing by deflection position

Each of the four pulses of light hitting the photocathode gives rise to a bundle of photoelectrons. These bundles are first accelerated by a potential of about 2000 V, applied to a grid in front of the photocathode, and later by a potential of about 15,000 V on the anode. The accelerated photoelectrons pass between the deflector

plates and are deflected by a 120-MHz sinusoidal voltage derived by frequency multiplication, from the stable 10-MHz master oscillator of the time-interval meter. At the other end of the tube, the electrons strike a phosphor screen, and much of their energy is converted to optical photons.

If a spot on the photocathode were illuminated steadily, the sinusoidal deflection voltage would cause the resulting beam of electrons to move back and forth across the phosphor and to trace out a straight line. A short pulse of light at a point on the photocathode produces a short segment of the full-deflection straight line. The segment's position is determined by the time of arrival of the originating light pulse, and its length by the duration of the light pulse.

Thus, the arrival of the four incident pulses of light at the image-converter photocathode, at four different times, results in the appearance of four differently positioned line segments on the output phosphor.

The time interval between transmitted and reflected pulses is some large multiple of the period of the 120-MHz deflection sinusoid plus an additional fraction of a period.

"From the relative positions of the line segments produced by the transmitted laser pulse and those produced by the reflected pulse," Golden notes, "one can make a very precise determination of the magnitude of this additional fraction of a period."

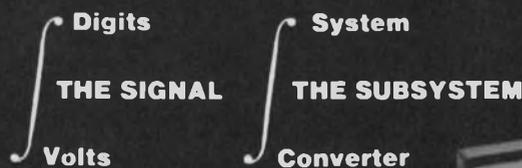
#### Systems to use CCDs

In the current experimental system, the output of the image intensifier is read by a camera. In future systems, the image intensifier will be replaced with a charge-coupled-device array on the output of the image converter. The position of the light spots will then be automatically determined by a controller based on the output of the CCD array.

Golden is also trying to eliminate the requirement for four spots by going to a circular or polar deflection. Then only the position of two spots on a circle will determine the required fraction of a period without ambiguity. ■■

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... The Digitizers

INFORMATION RETRIEVAL NUMBER 33

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Our **54C/74C series**, designed to reduce system costs, is pin-for-pin and function-for-function equivalent to T<sup>2</sup>L 7400 devices. Among their cost-saving features are low power supply requirements, less power supply regulation, fewer bypass capacitors, simpler design, and simplified power

distribution. The units also offer high noise immunity—typically 45% of supply voltage, and they have a guaranteed 1V noise margin. This means that 1V of noise at the input will not cause the output to rise beyond T<sup>2</sup>L levels. As a result, logic errors are less likely.

Applications are easy, too, with industry standardized input and output characteristics. Experience acquired with the 7400 series can also be applied directly to use of the 54C/74C's. For details, see your Harris distributor or representative.

	100-999 UNITS	
	-55°C to +125°C	0°C to +70°C
HD-54C00/74C00 Quad 2 NAND Gate _____	2.98	.69
HD-54C02/74C02 Quad 2 NOR Gate _____	2.98	.69
HD-54C04/74C04 Hex Inverter _____	3.30	1.04
HD-54C10/74C10 Triple 3 NAND Gate _____	2.98	.69
HD-54C20/74C20 Dual 4 NAND Gate _____	2.98	.69
HD-54C42/74C42 BCD to Decimal Decoder _____	7.15	3.30
HD-54C73/74C73 Dual J-K Flip Flop with Clear _____	4.75	2.26
HD-54C74/74C74 Dual D Flip Flop _____	4.20	1.45
HD-54C76/74C76 Dual J-K Flip Flop with Clear and Preset _____	4.75	2.26
HD-54C107/74C107 Dual J-K Flip Flop with Clear _____	4.75	2.26
HD-54C151/74C151 8 Channel Digital Multiplexer _____	6.40	3.95
HD-54C154/74C154 4-Line to 16-Line Decoder/Demultiplexer _____	16.20	5.40
HD-54C157/74C157 Quad 2 Multiplexer _____	5.10	2.88
HD-54C160/74C160 Decade Counter with Asynchronous Clear _____	10.40	5.70
HD-54C161/74C161 Binary Counter with Asynchronous Clear _____	10.40	5.70
HD-54C162/74C162 Decade Counter with Synchronous Clear _____	10.40	5.70
HD-54C163/74C163 Binary Counter with Synchronous Clear _____	10.40	5.70
HD-54C164/74C164 8-Bit Parallel Out Serial Shift Register _____	11.00	4.35
HD-54C173/74C173 Three State Quad/D Flip Flop _____	9.15	3.80
HD-54C192/74C192 Synchronous 4-Bit Up/Down Decade Counter _____	10.30	5.65
HD-54C193/74C193 Synchronous 4-Bit Up/Down Binary Counter _____	10.30	5.65
HD-54C195/74C195 4-Bit Register _____	5.70	3.75

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	100-999 UNITS			
	-40°C to +85°C		-55°C to +125°C	
	A	S	A	S
HD-4000 Dual 3 NOR Gate plus Inverter, 14 pin DIP	.78	1.86	1.17	3.10
HD-4001 Quad 2 NOR Gate, 14 pin DIP	.78	1.98	1.17	3.30
HD-4002 Dual 4 NOR Gate, 14 pin DIP	.78	2.04	1.17	3.40
HD-4007 Dual Complementary Pair plus Inverter, 14 pin DIP	.78	1.59	1.17	2.65
HD-4009 Hex Inverter/Buffer, 16 pin DIP	1.69	3.15	2.54	5.25
HD-4010 Hex Buffer, 16 pin DIP	1.69	3.15	2.54	5.25
HD-4011 Quad 2 NAND Gate, 14 pin DIP	.78	1.98	1.17	3.30
HD-4012 Dual 4 NAND Gate, 14 pin DIP	.78	2.07	1.17	3.45
HD-4013 Dual D Flip Flop, 14 pin DIP	1.62	2.85	2.43	4.75
HD-4019 Quad AND/OR Select Gate, 14 pin DIP	1.91	3.03	2.87	5.05
HD-4023 Triple 3 NAND Gate, 14 pin DIP	.78	2.06	1.17	3.44
HD-4025 Triple 3 NOR Gate, 14 pin DIP	.78	2.06	1.17	3.44
HD-4030 Quad Exclusive OR Gate, 14 pin DIP	1.63	2.27	2.45	3.79
HD-4804 Three State Hex Buffer with Level Translator, 16 pin DIP	-	6.15	-	7.67
HD-4805 Three State Hex Buffer Inverter with Level Translator, 16 pin DIP	-	6.15	-	7.67
HD-4806 Three State Triple True/Complement Buffer with Disable, Independent Level Translator, 16 pin DIP	-	6.15	-	7.67
HD-4807 Hex Buffer with Disable, 16 pin DIP	-	6.15	-	7.67
HD-4808 Three State Hex Buffer with Disable, 16 pin DIP	-	6.15	-	7.67
HD-4809 Triple True/Complement Buffer, 16 pin DIP	1.69	3.15	2.54	5.25
HD-4810 Three State Triple True/Complement Buffer with Disable, Common Level Translator, 14 pin DIP	-	6.15	-	7.67
HD-4811 Quad Exclusive NOR Gate, 16 pin DIP	1.63	2.27	2.45	3.79
HD-4814 Hex Inverter, 16 pin DIP	.97	2.27	1.45	3.80

# Harris

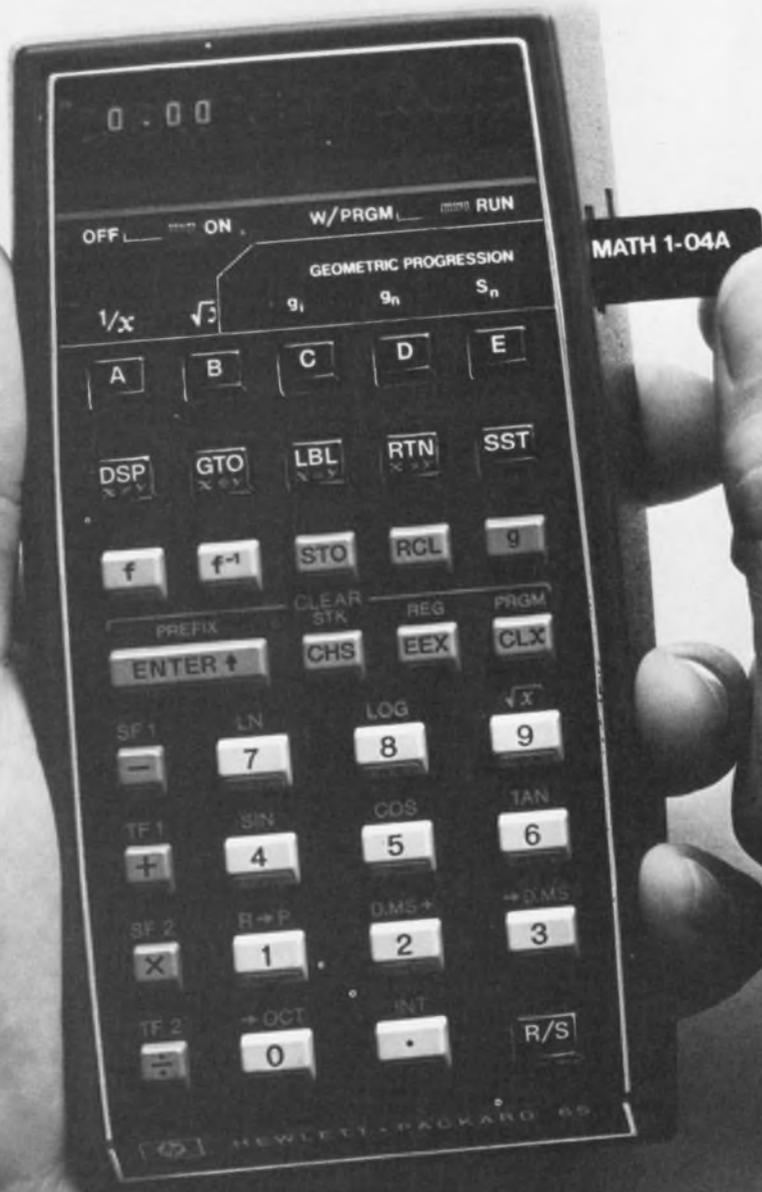


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The HP-65's 100-step program memory, in combination with its 51 pre-programmed arithmetic, logarithmic, trigonometric and exponential functions, its operational stack and its nine addressable memory registers, permits you to write exceedingly complex programs.

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HP offers a series of pre-recorded program packages called Application Pacs at \$45\* each. Each Pac contains as many as 40 programs dedicated to a specific discipline (currently Electrical Engineering, Mathematics, Statistics, Medicine and Surveying, with more to come).

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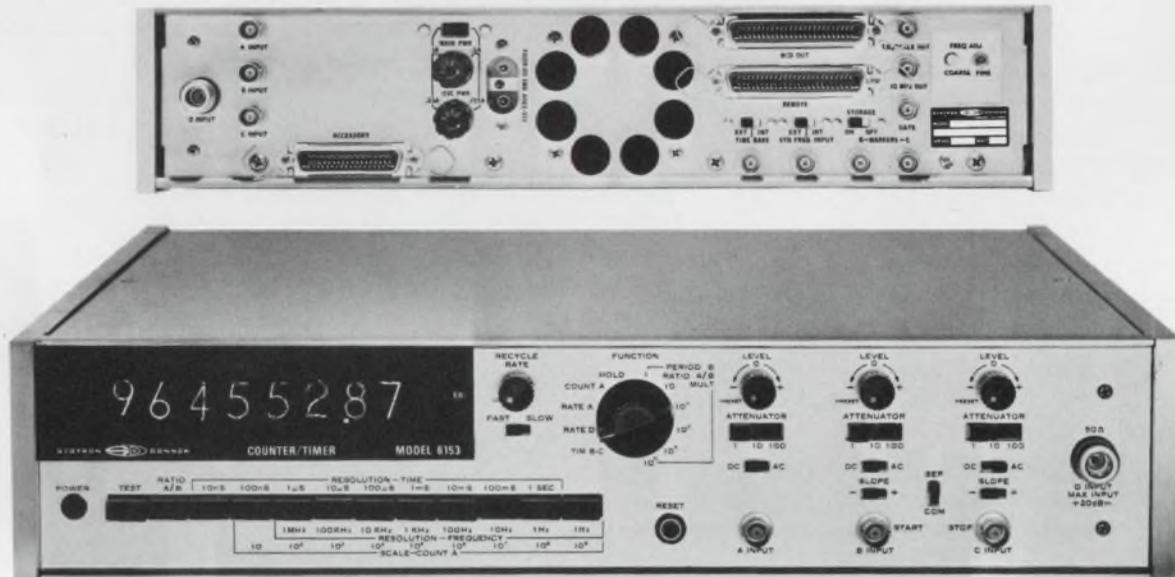
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# washington report

## **Senate bill aims to adjust contracts for inflation**

Prodded by the growing number of small businesses that are being driven to bankruptcy by inflation and materials shortages, Sen. William D. Hathaway (D-Me), chairman of the Senate Small Business Procurement Subcommittee, has introduced a relief bill. Joined by three other Senators—Alan Bible (D-Nev.), Jacob Javits (R-N.Y.) and William Scott (R-Va.)—Hathaway says the bill would require greater use of contract price-adjustment clauses to protect both the Government and the small-business contractor. The measure would permit contract prices to be amended in accordance with price rises that the contractor encountered. It would also recognize the energy and material shortages as excuses for delay rather than causes for default on a contract. "The Government should not be adding to the difficulties of the contractor by declaring him in default of his contract for a cause which was clearly beyond his control," Senator Hathaway says.

## **Satellite TV capacity doubled in Canadian test**

Digital TV transmission, as opposed to conventional FM, has doubled the Canadian ANIK-1 satellite's TV capacity through a single transponder. Tests of the new digital system were carried out jointly by Telesat Canada and Comsat Laboratories of the Communications Satellite Corp. (U.S.). The tests also demonstrated that the antenna-gain to system-noise temperature (G/T) at the receiving station could be lowered several decibels without loss in high-quality transmission. The system uses a transmission rate of 67.2 megabits per sec—the equivalent of sending more than 100 newspaper pages a minute. Transmission was from a 98-ft antenna in British Columbia through the ANIK-1 communications satellite to a 33-ft receiving antenna in Quebec. According to Comsat, the successful experiment points to increased TV capacity in the proposed U.S. satellite program.

## **More powerful lasers for nuclear fusion on the way**

Lasers with power 100 to 1000 times that of present units, and with power-generating efficiency still in the 25-50% range, are now feasible, according to physicists at the National Bureau of Standards. The bureau's researchers moved the quest for laser-fusion energy sources from the infrared and visible bands of the spectrum down into the far ultraviolet to attain successful excitation of krypton and xenon gas atoms. The Optical Physics Div. team, headed by Dr. Chris Kuyatta, concentrated on this ultra-low end of the energy spectrum after deciding that low-energy electron scattering had a high probability of exciting xenon gas. The gas

exhibits a strong resonance near its excitation threshold.

The work was undertaken for the Atomic Energy Commission's Los Alamos Laboratory, which is exploring ways to produce thermonuclear power from the laser-induced fusion of deuterium-tritium. The AEC has announced that it can undertake no further contracts to supply nuclear fuel because of diminishing sources of uranium and saturation of its processing capacity. But the sea is full of deuterium, and the tapping of this vast energy source appears on the horizon.

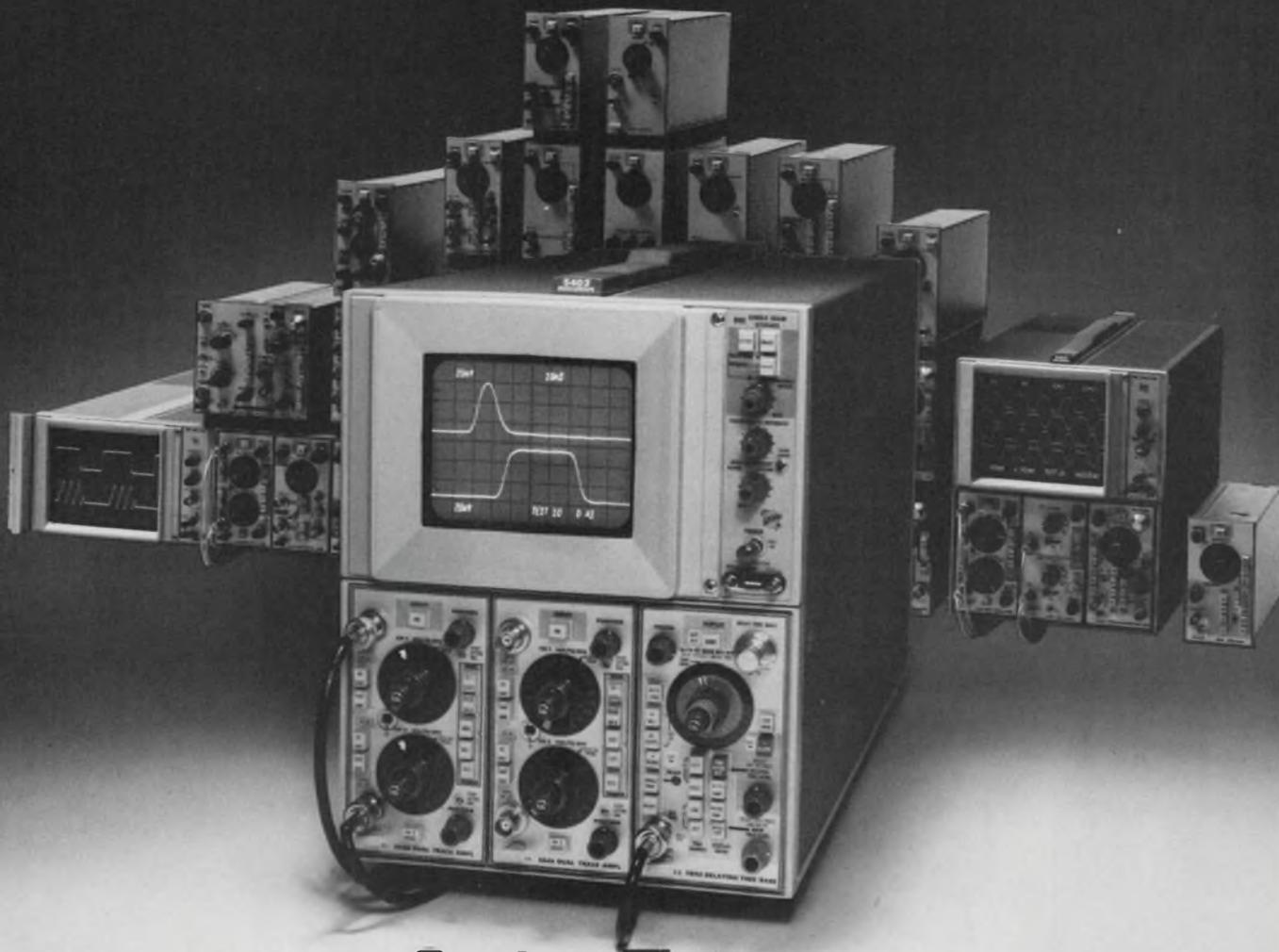
## Billions in electronic exports could be endangered

Up to \$5-billion a year in foreign sales of aircraft and electronic equipment could go down the drain if Senate Bill S 1541, now in a Senate-House Conference, should be passed.

Initiated by Sen. William Proxmire (D-Wisc.), the bill would require the Export-Import Bank to pay into the Treasury its income from loans, and loan disbursements would be treated as expenditures that required annual Congressional authorizations and appropriations. This year-to-year cycle (contracted with export financing, which runs for five to 10 years), together with vulnerability to budget cutbacks and constraints, would virtually eliminate the bank as a major source of long-term export financing. Such financing is important in selling jet aircraft and associated electronic equipment.

At present the Export-Import Bank is not only self-supporting but returns an annual profit of \$50-million to the Treasury through sale of its debentures and the purchase of discounted notes. The bank has financed the overseas sale of more than 1000 commercial jet aircraft, containing an estimated \$3-billion in electronic equipment, plus another \$3-billion in private jets, helicopters, navigational and landing aids and flight simulators.

**Capital Capsules:** FAA Administrator Alexander P. Butterfield wants to stick with Loran A as the basic transocean navigation system at least through July, 1979. U.S. Coast Guard, which must fund and man the stations, is anxious to get on with Loran C. . . . NASA has selected Odetics Corp., Anaheim, Calif., to design, develop and produce new tape recorders for future spacecraft. The \$4-million contract is for 30 units with  $10^9$  data-bit storage. . . . The Government Renegotiation Board, perennially slated for termination, has gotten a further lease on life, at least to 31 Dec 1975, by the House Ways and Means Committee. Critics argue that the Board costs government and industry far more than it collects but it is confounding its critics by collecting an estimated \$70-million the current fiscal year, well over double last year's forfeits. . . . After reviewing a wide variety of proposals for monster "flying trucks" from airframe manufacturers, foreign firms and just plain "inventors", NASA has decided simply to buy a used Boeing 747-100 from American Airlines for \$16-million. The jumbo jet will have fittings installed so it can carry piggyback the giant Space Orbiter and related hardware weighing up to 775,000 lb. . . . The Air Force has awarded a \$14.3-million contract to Magnavox Co., Ft. Wayne, Ind., for production of 16,000 ARC-164 aircraft communications sets—one of the largest and most hotly contested procurements for airborne radio since World War II. The solid-state units are uhf with 10 W of power output and 7000 channels with 25-kHz spacing, yet each weighs only 10 lb. The new sets will replace ARC-27 and ARC-34 sets. . . . The Senate Judiciary Subcommittee on Antitrust has resumed hearings on alleged infringements by the communications industry. The subcommittee will look at alleged anticompetitive practices by AT&T, particularly its prohibition against the use of non-Bell interconnect with Bell installations.



## Capture Those Hard to View Signals at Low Cost

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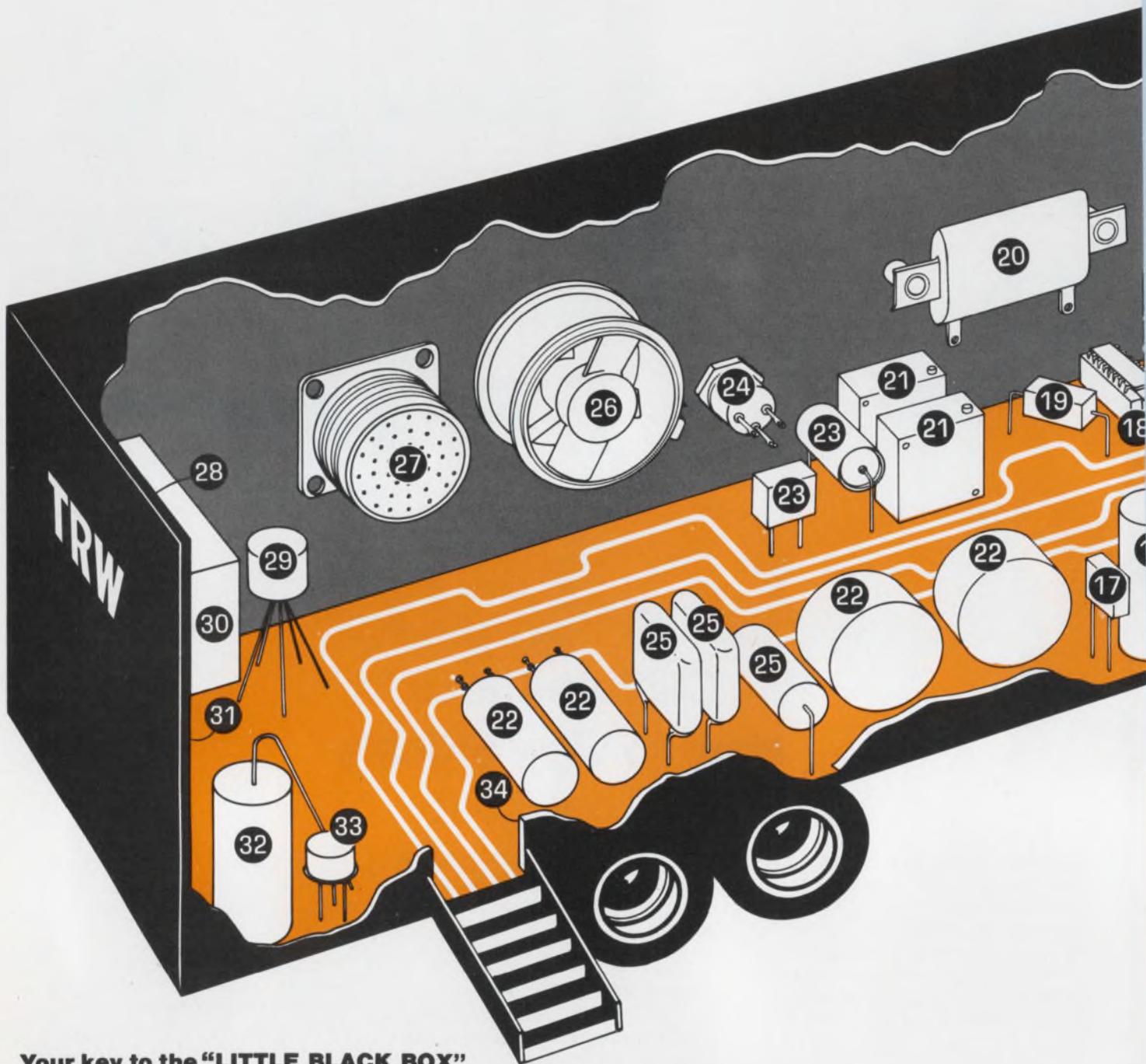
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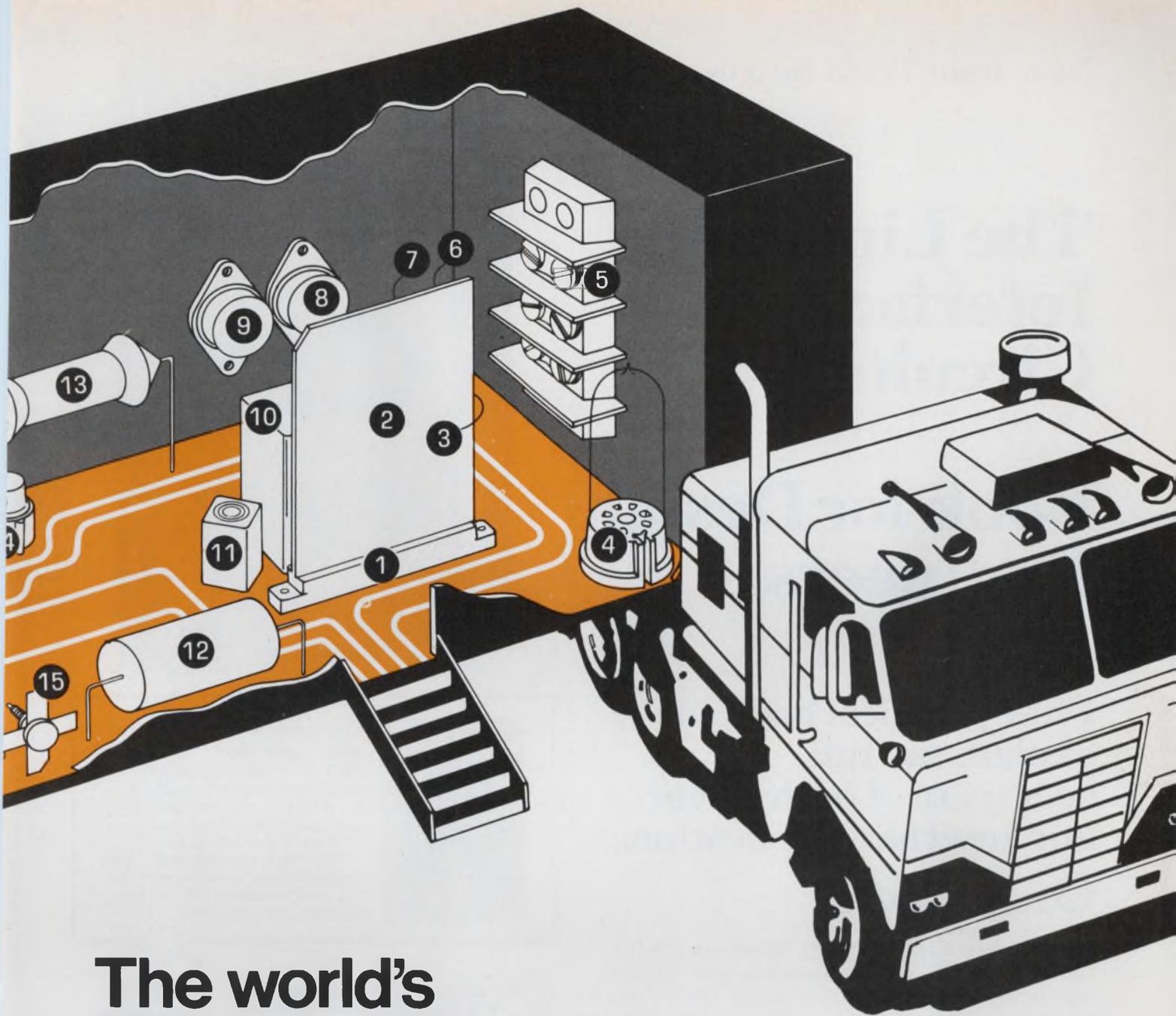
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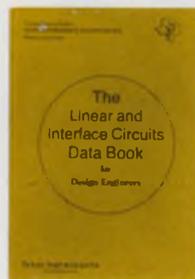
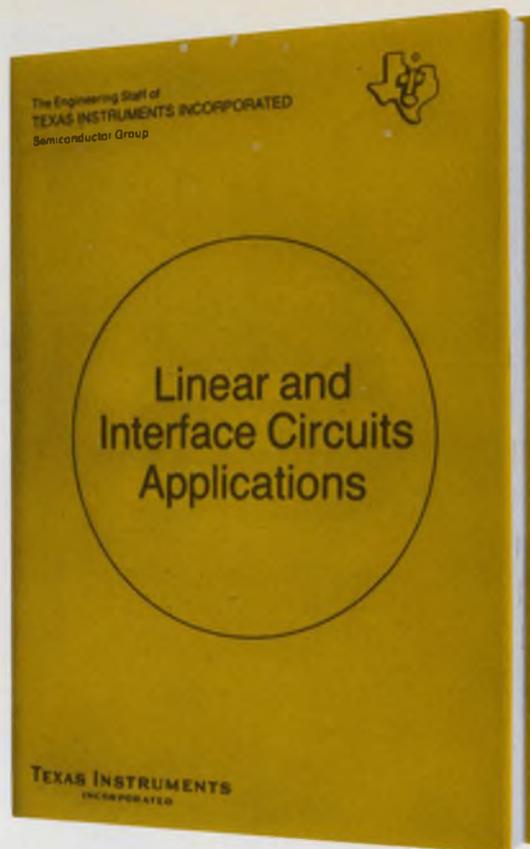
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## Too many foreigners

I envy these fellows who can feel at home anywhere in the world. For me, foreign travel is traumatic. Most of Europe is bad enough, as I get lost almost immediately in French, German, Dutch or Italian. But Japan is terrifying, as I can't read the signs (except those that say "Drink Coca Cola"), let alone understand them.

I don't mind England so much because I can pretty much cope with the language. But even there, the left-side drive scares the life out of me when I look the wrong way while crossing a street. I feel a stranger, even there, when I ask somebody for directions and learn that she's a foreign tourist.

I was particularly distressed at London's Heathrow airport. While waiting for another plane to Amsterdam after my original flight was canceled, and while waiting for the excitement over a nearby bomb explosion to subside, I was struck by a remarkable example of fine design. I guess it was my engineering background and journalistic eye for detail that made me admire and smile at this young lady, whose surface geometry left nothing to be criticized.

We didn't exchange a word, but fortune led us aboard the same plane and, purely by chance, of course, I found a seat beside her. Being shy, I didn't speak until she offered me a cigarette. When I tried to strike up a conversation, she smiled beautifully, then, in tones of velvet, exhausted her supply of English: "I speak only German."

And so it was throughout Europe. I was continually frustrated except when I was with those, in many countries, who spoke a common language—engineering. For engineering, like art and music, knows no language barriers. The components, circuits and equipment designed by engineers in one country can be understood and used by engineers in all countries. Resistors and capacitors in France are like resistors and capacitors in Germany, Italy or England. So are ICs and DVMs.

While politicians throughout the world, however well schooled in language arts, seem unable to communicate, engineers can understand each other with little difficulty. In the engineering community there are no foreigners.

Perhaps we should subject our politicians to the disciplines of engineering. And perhaps our engineers should devote themselves more to politics. Politics certainly wouldn't suffer. And engineering . . . well, a small setback might not hurt too much.



GEORGE ROSTKY  
Editor-in-Chief

# Taming noise in IC op amps: Signal-source impedance and operating-frequency band are the keys to selection of the right bipolar or FET-input op amp.

The selection of IC op amps for very-low-signal applications depends primarily on two parameters: the impedance of the signal source used and the operating-frequency band. Careful attention to these parameters can help overcome the noise limitations of the otherwise extremely versatile monolithic op amp.

Op amps generally employ bipolar transistors at the input, although a growing number of newer amplifiers have FET inputs. Both types are prone to the same sources of noise as discrete amplifiers that use such devices.

For a differential-input configuration, op amps use at least two, and sometimes four, input transistors that increase noise levels over those for a single-transistor input stage. Generally noise levels increase with the square root of the number of transistors.

Moreover IC op amps are usually internally biased, so designers cannot alter bias currents to reduce noise. However, newer programmable amplifiers return this option to the designer. (Programmable here means the ability to change internal operating currents by selection of an external resistor.)

## Rules help reduce noise

The problems caused by noise can be reduced by following these major design rules:

- Use bipolar-input op amps when source impedances are low and operating currents are high. Applications with very high impedances generally favor use of FET or super-beta transistor inputs operating at low current levels.

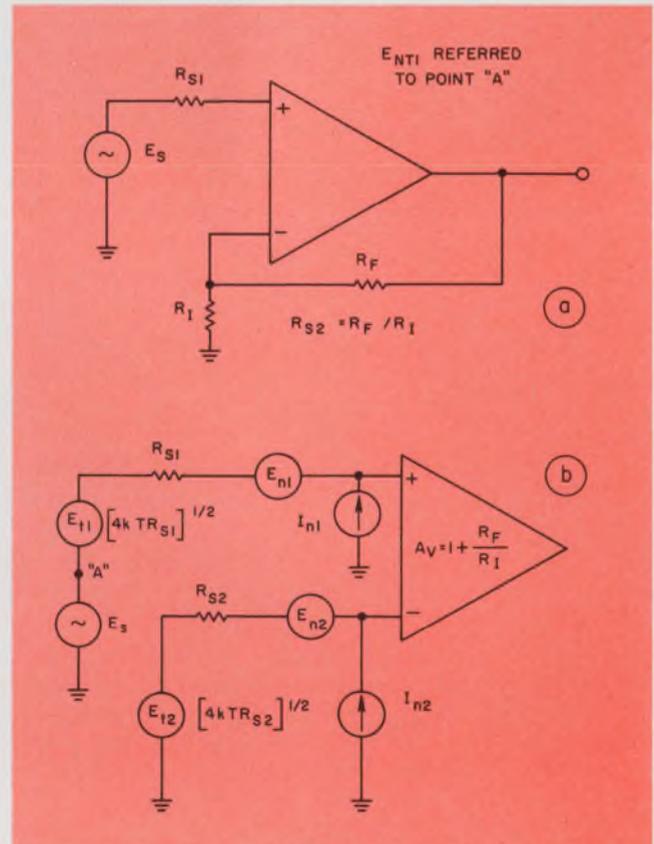
- Select bipolar-input op amps for moderate to low-impedance sources, particularly if the operating frequency band lies below 100 Hz.

- Expect burst, or "popcorn," noise when bipolar op amps operate at high input-bias currents. This type of noise is also more likely to occur when source impedances are high than when they are low.

- Limit circuit bandwidth to that necessary to process the desired signals. Unnecessary bandwidth increases noise voltages at the output.

## Bipolar model pinpoints noise sources

A typical op-amp circuit containing equivalent noise sources appears in Fig. 1. The sources are referred to the input and specified by their 1-Hz-bandwidth values. The term  $\sqrt{4kTR_s}$  represents the thermal noise voltage of source resistor  $R_s$ , while  $E_n$  is the noise voltage caused by the amplifier when  $R_s$  is zero. Current  $I_n$  represents noise contributed by the amplifier in addition to



1. A typical op-amp circuit (a) is terminated at its input by source resistors  $R_{s1}$  and  $R_{s2}$ . The equivalent circuit (b) exhibits the major sources of noise.

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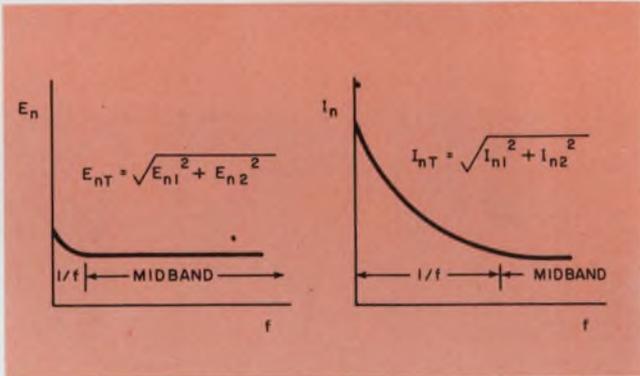
$E_n$  when  $R_s$  doesn't equal zero.

Since these sources are at random phase with one another, they must be added in rms fashion to obtain the total input-referred noise voltage. The total voltage per  $\sqrt{\text{Hz}}$  of bandwidth can be expressed as follows:

$$E_{nti} = \sqrt{4kTR_{S1} + 4kTR_{S2} + E_{n1}^2 + E_{n2}^2 + I_{n1}^2 R_{S1}^2 + I_{n2}^2 R_{S2}^2}^{1/2}$$

If  $R_{S1} = R_{S2}$  and the  $E_n$  and  $I_n$  generators are combined, the equation simplifies to

$$E_{nti} = [8kTR_s + E_{nT}^2 + I_{nT}^2 R_s^2]^{1/2}, \quad (1)$$



2. Typical  $E_n$  and  $I_n$  spectral density curves in bipolar op amps show greater  $1/f$  sensitivity for  $I_n$ .

where  $E_{nT} = (E_{n1}^2 + E_{n2}^2)^{1/2}$  and  $I_{nT} = (I_{n1}^2 + I_{n2}^2)^{1/2}$ .

Op-amp data sheets usually provide information on  $E_n$  and  $I_n$  in terms of  $E_{nT}$  and  $I_{nT}/\sqrt{2}$ , the approximate noise current at each input terminal.

Total noise voltage  $E_{nti}$  over a band of frequencies can be found by a plot of the noise spectral density,  $\overline{E_{nti}^2}$ , vs frequency and integration over the required frequencies. If the noise spectral density is fairly constant with frequency, as it is for "shot" noise, wideband  $E_{nti}$  can be found simply by multiplication of the narrowband, 1-Hz, value in Eq. 1 by the square root of the bandwidth.

### Three noise sources in bipolar op amps

A bipolar transistor contributes to  $E_n$  and  $I_n$  from three major sources:

1. Thermal noise from the base-spreading resistance  $r'_{bb}$ :

$$E_t = \sqrt{4kTr'_{bb}} \text{ in units of } V_{rms}/\sqrt{\text{Hz}},$$

where  $k$  is Boltzmann's constant,  $1.38 \times 10^{-23} \text{ W/}^\circ\text{K}$ , and  $T$  is temperature in degrees Kelvin.

2. Shot noise from dc-current flow in the emitter and base. This noise source can be modeled by two shot-noise current generators:

$$I_{se} = \sqrt{2qI_E} \text{ in } A/\sqrt{\text{Hz}}$$

and  $I_{sb} = \sqrt{2qI_B} \text{ in } A_{rms}/\sqrt{\text{Hz}}$ ,

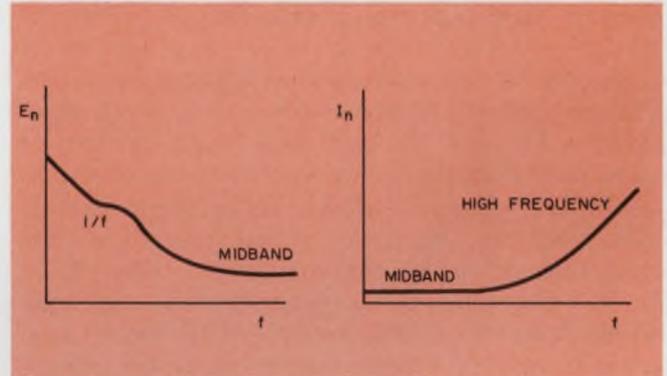
where  $q$  is the electronic charge  $1.59 \times 10^{-19}$

coulombs.

3. Flicker or  $1/f$  noise from the flow of base current through the emitter-base depletion region. This noise source can be modeled by a noise-current generator:

$$I_f = \frac{\sqrt{2qI_B f_L}}{f} \text{ in } A_{rms}/\sqrt{\text{Hz}}.$$

In Fig. 1b, voltage  $E_n$  represents the combined effects of the three noise generators when  $R_s = 0$ . With  $R_s$  still zero,  $r'_{bb}$  contributes its full thermal noise,  $E_t$ . Emitter shot-noise current  $I_{se}$  flows



3. Corresponding curves for a FET-input op amp reveal differences in magnitude and spectral responses.

through the emitter dynamic resistance  $r_e$  and so generates an equivalent input-noise-voltage term:

$$E_s = I_{se} r_e = \frac{kT}{qI_E} \sqrt{2qI_E} = \sqrt{\frac{K_E}{I_E}} = \frac{14.2 \times 10^{-12}}{\sqrt{I_E}}$$

in  $V_{rms}/\sqrt{\text{Hz}}$ .

Base shot-noise current  $I_{sb}$  flows through  $r'_{bb}$  and generates a noise voltage  $I_{sb} r'_{bb} = \sqrt{2qI_B} r'_{bb}$ , which is usually insignificant compared with  $E_t$  and  $E_s$ . Flicker-noise current generator  $I_f$  also flows through  $r'_{bb}$ , generating a  $1/f$  noise-voltage component of  $E_n$ . This component of  $E_n$  is only appreciable at frequencies below about 100 Hz, unless the operating current level is relatively high.

Hence the total value of  $E_n$  can be expressed as follows:

$$E_n = E_t^2 + E_s^2 + I_{sb}^2 r'_{bb}{}^2 + I_f^2 r'_{bb}{}^2 \text{ in } V_{rms}/\sqrt{\text{Hz}}.$$

At frequencies above 100 Hz, the equation has a uniform spectral value that allows the following approximation:

$$E_n = (E_t^2 + E_s^2)^{1/2} = (K_t r'_{bb}{}^2 + K_E/I_E)^{1/2} \text{ in } V_{rms}/\sqrt{\text{Hz}}. \quad (2)$$

Noise contributed by this source can be minimized if the amplifier is designed with transistors that have low  $r'_{bb}$  and the transistors are operated at relatively high emitter-current levels.

Remember that each input transistor of the differential amplifier contributes an  $E_n$  term. For

a two-transistor differential amplifier, the total  $E_n$  would be  $\sqrt{2}$  times the  $E_n$  of each transistor, if equal voltage for each is assumed.

The  $I_n$  term of Eq. 1 is simply the rms sum of  $I_{sb}$  and  $I_f$ :

$$I_n = \sqrt{I_{sb}^2 + I_f^2} = \sqrt{2qI_B[1 + f_i/f]} \\ = \sqrt{K_1 I_E (1 + f_i/f)} \text{ in A}/\sqrt{\text{Hz}} \quad (3)$$

Of course,  $I_n$  can be minimized through a reduction in base-bias current. The reduction can be achieved by use of input-stage transistors that have high dc betas at microampere collector currents.

Typical noise spectral-density curves for an op amp with bipolar input show greater frequency variations for  $I_n$  than for  $E_n$  (Fig. 2). Both  $E_n$  and  $I_n$  midband values are determined primarily by the operating current ( $E_n$  also varies with the number of input junctions). However, noise levels in the  $1/f$  region, dependent on manufacturing processes, may vary considerably.

For a fixed value of  $R_s$ , an optimum current minimizes  $E_{nti}$ . Eq. 1 can be manipulated to show that this optimum current occurs when  $E_n/I_n = R_s$ . Consequently a programmable op amp, which permits external control of the input-stage current, offers a simple way to minimize noise.

### Noise sources in FET op amps

The noise model for bipolar-input op amps applies also to amplifiers with FET inputs. Only the magnitudes and spectral responses are different. Typical FET spectral responses appear in Fig. 3.

The three sources of noise in a FET are as follows:

1. Thermal noise from channel conductivity.
2. Shot noise from gate-leakage current.
3. Flicker or  $1/f$  noise.

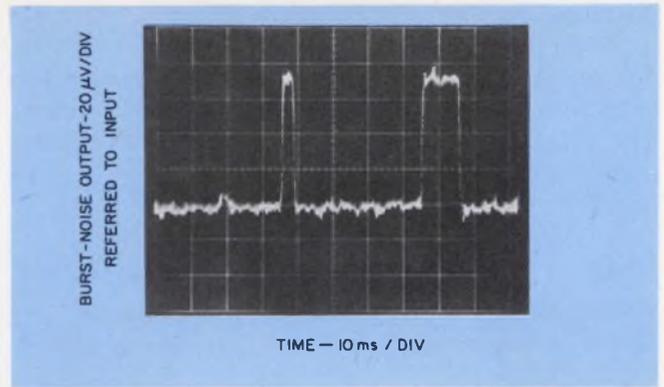
Here again,  $E_n$  represents the amplifier-contributed noise when  $R_s = 0$ , and  $I_n$  represents additional noise when the source impedance isn't zero.

Because of the exceedingly small gate-leakage current of FETs, particularly MOS types, the midband  $I_n$  term usually is small enough, relative to  $E_n$ , to be neglected. This approximation is especially valid in the  $1/f$  region at frequencies below 100 kHz. In this low and mid-frequency area,  $I_n$  results mainly from the shot noise generated by the reverse-diode gate-leakage current,  $I_{GL}$ , and it has the form  $I_n = \sqrt{2qI_{GL}}$ . Noise voltage  $E_n$  in the midband region results from the thermal noise of the channel resistance, and it has a noise resistance  $R_n$  of

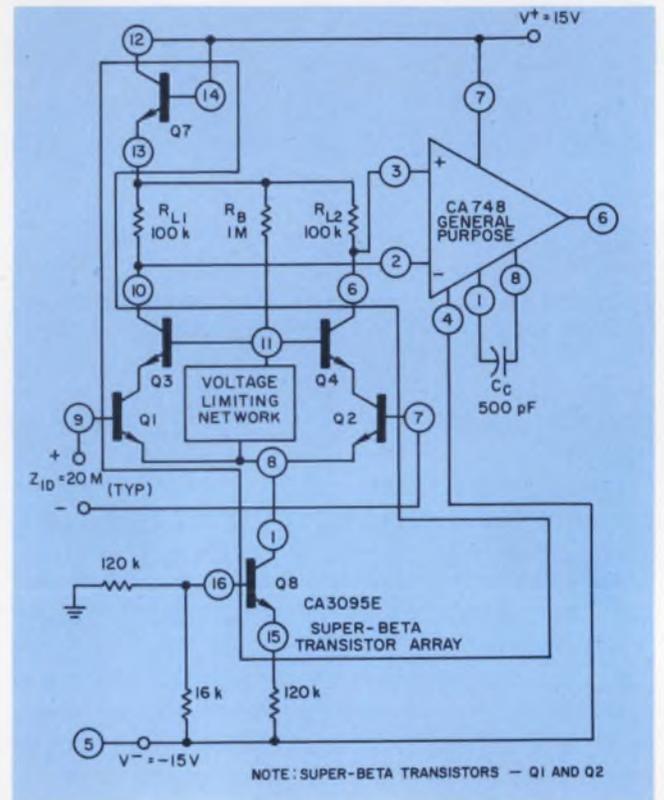
$$R_n = \frac{2}{3} \frac{1}{g_m},$$

so that

$$E_{n(\text{midband})} = \sqrt{4kTR_n} = \sqrt{\frac{8}{3} \frac{kT}{g_m}} \quad (4)$$



4. The characteristics of burst noise include random, abrupt changes in output level that can last from about 0.5 ms up to several seconds.



5. Op-amp circuit employs super-beta transistor array. The array serves the function of a programmable preamp to achieve low-noise characteristics.

The equation<sup>1</sup> suggests that midband-noise voltage falls off at high drain currents because of the inverse relation to  $g_m$ . However,  $g_m$  depends on  $\sqrt{I_D}$ , while  $E_n$  is related to  $\sqrt{1/g_m}$ . Hence  $E_n$  approximately decreases as the fourth-root of an increasing  $I_D$ , so that  $E_n$  is relatively insensitive to  $I_D$  variations.

The increase in  $I_n$  at higher frequencies results from a capacitive coupling of channel thermal noise into the gate circuit through the feedback capacitance,  $C_{fd}$ . Essentially  $C_{fd}$  reflects a parallel resistance,  $R_i$ , into the gate circuit. The resistance increases with frequency and contributes

the following thermal noise current at the input:

$$I_n = \sqrt{\frac{4kT}{R_i}} \text{ in } A/\sqrt{\text{Hz}} \quad (5)$$

This noise component can be obtained from a measurement of the real part of the input admittance at high frequencies.<sup>2</sup>

Unlike the situation with bipolar-input op amps, the  $E_n$  of FET-input amplifiers has a significant  $1/f$  characteristic; the  $1/f$  noise of a bipolar op amp occurs primarily in its  $I_n$  characteristic. The midband  $I_n$  of a FET op-amp is generally negligible, while the midband  $I_n$  for an op-amp with a bipolar input may be significant, depending on the source impedance used.

### 'Popcorn' noise a problem, too

In low-signal-level applications, burst noise, or popcorn noise, should be considered (Fig. 4). The characteristics include abrupt changes in output level that persist from about 0.5 ms to several seconds. And they occur at random rates from less than one per minute to several hundred per second.<sup>3</sup> This type of noise becomes most objectionable in very-low-frequency narrowband applications, because pk-pk noise levels are very low and burst-noise peaks may dominate the total noise output.

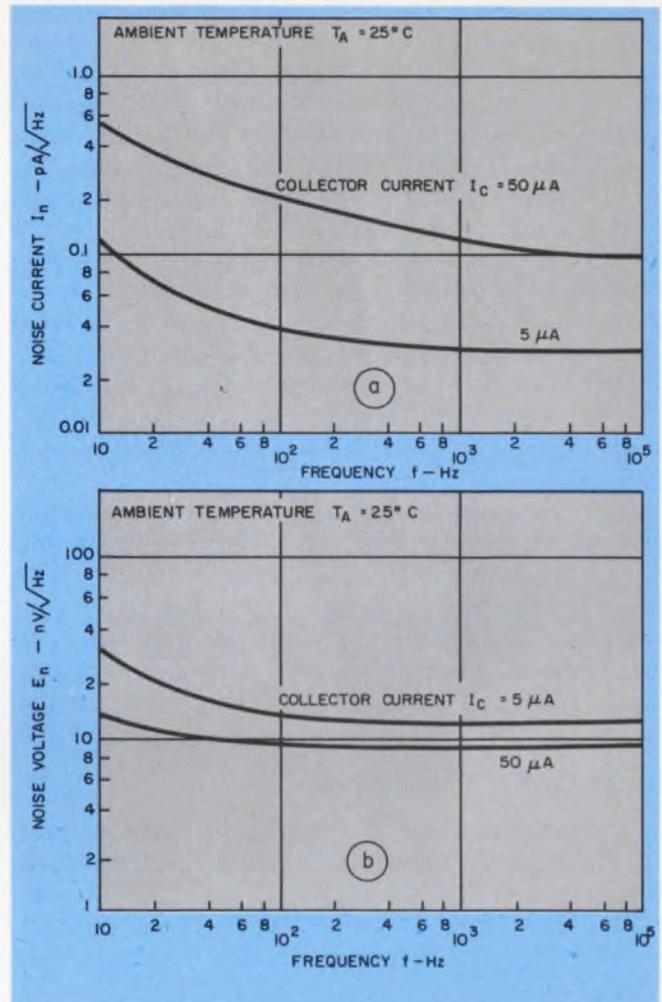
In the popcorn-noise model, the current generator has a magnitude that is proportional to the square root of the input-bias current. Hence the generator's effect can be reduced by use of op-amps with FET inputs or amplifiers with bipolar inputs in which the bias current is very low—such as those operating at very low collector currents with high dc beta. And since burst noise is an input-current noise, the amplitude of the bursts varies proportionally to the magnitude of the terminating source impedance,  $Z_s$ . Therefore to minimize burst noise, maintain  $Z_s$  as low as possible. Several available ICs are fully tested for popcorn noise at various source impedances.<sup>3,4</sup>

### Noise isn't everything

Of course, parameters other than noise enter into the selection of an op amp. They include offset voltage, offset-voltage drift, input-offset current and bandwidth.

Consider an application that calls for a low-level dc amplifier operating from a low-impedance sensor, such as a thermocouple. The best choice is probably an amplifier with a bipolar transistor input. This type of op amp has a lower offset drift than one with FET inputs, and at low source impedance,  $E_n$  is the dominant noise source.

For ac-coupled applications, where dc drift is not critical, the choice between bipolar and FET input depends largely on the source impedance



6. Noise-frequency characteristics for the super-beta op-amp circuit of Fig. 5 are shown for noise current  $I_n$  (a) and noise voltage  $E_n$  (b). The super-beta input transistors operate at collector currents of  $5 \mu\text{A}$  in Fig. 5.

of the sensor. At very high source impedances—greater than  $1 \text{ M}\Omega$ —op amps with FET inputs are probably the best choice; their exceptionally low  $I_n$  currents result in a lower  $I_n R_s$  product.

Low-source-impedance applications favor the use of op amps with bipolar inputs that operate in the 50-to-200- $\mu\text{A}$  collector-current range (to minimize  $E_n$ ). Higher-source-impedance applications favor the use of op amps with FET inputs or with bipolar inputs that can operate at low collector currents—less than  $10 \mu\text{A}$ —and that can still retain high dc beta. This mode of operation indirectly minimizes  $I_n$ .

Op amps that allow the current to be programmed are especially useful for applications with high source impedances. Input-transistor collector currents for these amplifiers can be altered externally to provide the best  $E_n$  vs  $I_n$  tradeoff for  $Z_s$ . (This point occurs when  $E_n/I_n = Z_s$ .)

Moreover the use of super-beta input transistors provides an  $E_n$  with low  $1/f$  characteristics (for bipolar transistors) along with  $I_n$  levels that

are much lower than those of conventional bipolar transistors. For example, the circuit in Fig. 5 shows a super-beta transistor array<sup>5,6</sup> coupled as a programmable preamp to a general-purpose op amp to provide very low noise characteristics. Typical noise parameters for the circuit appear in Fig. 6. (The 5- $\mu$ A curves of Fig. 6 apply to the circuit of Fig. 5.)

Low-frequency noise, such as 1/f or burst noise, depends on the IC process used. It varies substantially from manufacturer to manufacturer, and even from lot to lot of a given manufacturer. When this type of noise becomes critical, one solution is to use fully tested units. Another solution is to examine several vendors' op amps and test them yourself.

Midband noise doesn't depend heavily on the IC process. Rather it primarily reflects bias-current levels and device geometries; essentially it is contingent upon device design. As a result, only a relatively small sample of units generally need be examined to select an op amp with low midband noise.

### Designing for minimum noise

The general steps for minimum noise design, or maximum signal-to-noise ratio, are derived from an examination of Eq. 1. When the device is shot-noise limited—when the  $E_s$  term primarily determines the value of  $E_n$ —Eq. 1 has the following form:

$$E_{nti} = \sqrt{8kTR_s + 2 \frac{K_E}{I_E} + 2K_I I_E R_s^2}, \quad (6)$$

where  $I_E$  is the emitter dc current of the input transistors. Noise voltage  $E_{nti}$  has a minimum value at an  $I_E$  for which

$$\frac{K_E}{I_E} K_I I_E R_s^2 = E_{nT}^2 = I_{nT}^2 R_s^2. \quad (7)$$

Hence for a given value of  $R_s$ ,  $E_{nti}$  is minimum when  $E_n/I_n = R_s$ .

The circuit noise factor, defined by the ratio

$$NF = \frac{E_{nti}^2}{8kTR_s} = 1 + \frac{E_{nT}^2}{8kTR_s} + \frac{I_{nT}^2 R_s^2}{8kTR_s}, \quad (8)$$

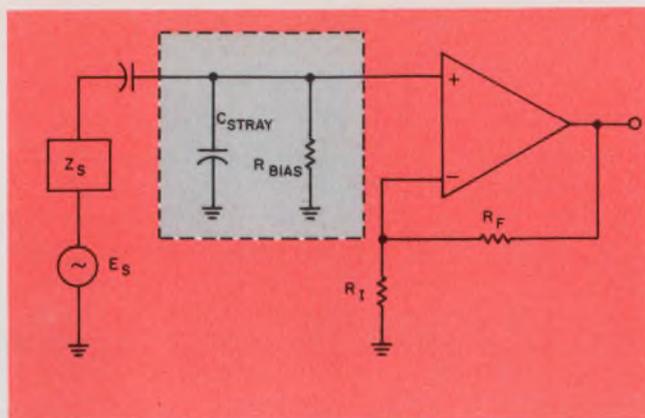
is also minimized when  $E_n/I_n = R_s = R_{OPT}$ . For this condition, the optimum noise figure,  $F_{OPT}$ , becomes

$$F_{OPT} = 1 + \frac{E_{nT} I_{nT}}{4kT}. \quad (9)$$

The minimum value of  $F_{OPT}$  is independent of operating current, so long as the current is low enough to make  $E_n$  shot-noise limited. This current level depends on the magnitude of  $r'_{bb}$  but generally operating-current levels below about 200  $\mu$ A yield minimum  $F_{OPT}$ .

The procedure then for the design of a minimum-noise system consists of the following six steps:

*Step 1.* With the sensor source impedance fixed



7. Stray capacitance and bias resistance degrade signal-to-noise ratios.

at  $Z_s$ , select an op amp that has  $E_n/I_n$  approximately equal to  $Z_s$  at the frequency for which noise is most critical. Alternatively, a programmable op amp adjusted to a current level for which  $E_n/I_n = Z_s$  can be used.

For very low source impedances—less than 100  $\Omega$ —the adjustment may not be possible without operation at very high current levels. There the base-resistance factor of thermal noise dominates  $E_n$ .

In this case  $F_{OPT}$ , corresponding to  $E_n/I_n \approx Z_s$ , is high because the  $I_{nT} R_s$  product matches the base-resistance factor of the thermal noise,  $\sqrt{4kTr'_{bb}}$ , rather than  $E_s$ , the shot-noise component of  $E_n$ . Noise-figure minimization results when the  $I_n (R_s + r'_{bb})$  product equals the shot-noise component of  $E_n$ , or when

$$I_{nT} (R_s + r'_{bb}) = \frac{(14.2 \times 10^{-12})}{I_E}. \quad (10)$$

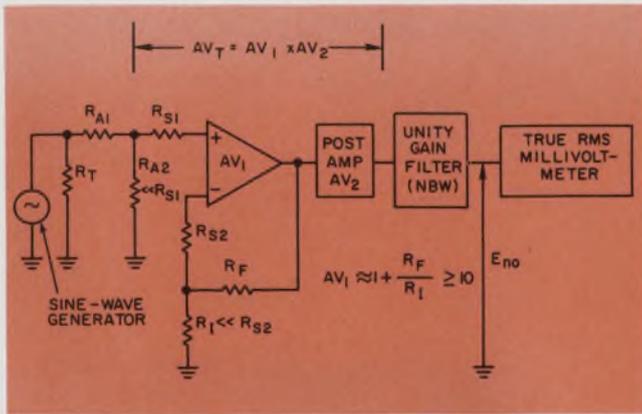
One of two designs may be used. First, a transformer can be employed at the input to raise the source impedance. If this is not practical, adjust the operating current of the input stage to satisfy Eq. 10. Generally, this occurs at collector currents in the range of 0.1 to 1.0 mA.

*Step 2.* If the first-stage op amp forms a low-gain stage, such as a follower, use a low  $E_n$  second stage as well. The  $I_n$  of the second stage is not as important normally, because the output impedance of the first stage is very low. Second-stage  $E_{nt2}$  affects the total input referred noise,  $E_{nti}$ , as follows:

$$E_{nti}^2 = E_{nt1}^2 + \frac{E_{nt2}^2}{A_{v1}^2}, \quad (11)$$

where  $A_{v1}$  is the voltage gain of the first stage.

*Step 3.* Resistors connected to the input terminals and which have dc voltage across them should be of a low-noise type, such as metal-film resistors. The requirement also applies to bias and feedback resistors connected to the op-amp input terminals. Most resistors generate noise in excess of the thermal noise,  $4kTR$ , when dc volt-



8. Measurement of  $E_{nT}$  and  $I_{nT}$  with this test system allows a variety of source impedances to be used.

ages are impressed upon them. The excess noise increases with voltage and has a  $1/f$  characteristic. The resistor figure of merit for this characteristic is called its noise index: the excess noise voltage it generates in microvolts per volt-dec per decade of bandwidth. A noise index of zero dB is poor, while a 20-to-30-dB index is good.

**Step 4.** The input-bias resistance ( $R_{BIAS}$  in Fig. 7) should be as large as possible, compared with the magnitude of  $Z_s$ . Because the resistor shunts the input,  $R_{BIAS}$  adds noise as a current source that is inversely proportional to the square root of its resistance value. Also, any attenuation of signal voltage  $E_s$ , resulting from the voltage division between  $Z_s$  and  $R_{BIAS}$ , degrades the signal-to-noise ratio. Voltage  $E_n$  is not similarly attenuated.

**Step 5.** The shunt capacitance ( $C_s$  in Fig. 7) should be kept as low as possible, to minimize its attenuation of  $E_s$ .

**Step 6.** Keep system bandwidth as narrow as possible, consistent with signal requirements, to minimize the total noise at the load. All the noise expressions given are based on a per-unit-bandwidth (1 Hz). However, the total noise power delivered to the load is proportional to the square root of the system's noise-power bandwidth.

### Measuring op-amp noise

Several methods can be used to measure the noise characteristics of different op amps. One measures total input noise voltage, with the input terminated by source impedances that are typical for the application. The measurement should use a filter to limit frequencies to those for which the op amp is intended. When several op amps are tested, the filter also ensures a consistent noise bandwidth. Otherwise comparative noise voltages read at the output may be as much a measure of differences in amplifier bandwidth as they are of amplifier noise.

A more general method measures  $E_{nT}$  and  $I_{nT}$

separately. This permits the calculation of noise performance for a variety of source impedances. Fig. 8 shows the test system.

The input sine-wave oscillator,  $R_{A1}$ - $R_{A2}$  attenuator and millivoltmeter measure the over-all test-system voltage gain,  $AV_T = AV_1 AV_2$ . They also measure the response characteristic of the system, including the filter. The filter has unity gain in the passband, and it has a noise-power bandwidth (NBW) that is not the same as the filter's 3-dB bandwidth. Rather, NBW represents the width of a rectangle on a frequency plot of voltage gain squared. The rectangle has the same area as that under the actual response curve and a height equal to the peak height of the actual response (Fig. 9). For example, a single-pole low-pass filter with a 3-dB frequency of  $f_p$  has a noise bandwidth of about  $1.57 f_p$ .

The post-amplifier in Fig. 8 ensures a total output-noise signal that is large enough for measurement with a true rms millivoltmeter. The voltage gain ( $AV_1$ ) of the op amp under test should be at least 20 dB, so that post-amplifier noise can be neglected. Also, meter bandwidth should be substantially wider than the filter NBW, so the filter remains the only factor in limiting bandwidth. If the meter used is an average detecting type, calibrated to read the value of a sine wave, multiply the output noise-voltage readings by 1.13 to obtain true rms noise voltage.

When noise must be measured at very low frequencies—less than 10 Hz—accurate rms readings on a meter are difficult to obtain. The best approach in this case is to view the noise at the filter output with an oscilloscope, so that pk-pk rather than rms noise can be measured. A storage oscilloscope with a sensitive plug-in is well suited for this measurement; it's also a good instrument for detection of burst noise, because it stores the burst.

For the total input-referred noise over the full filter bandwidth, disconnect the signal generator and measure the total output rms noise-voltage,  $E_{no}$ . Then calculate  $E_{nti}$  as follows:

$$E_{nti} = \frac{E_{no}}{AV_T} \text{ in } V_{RMS}$$

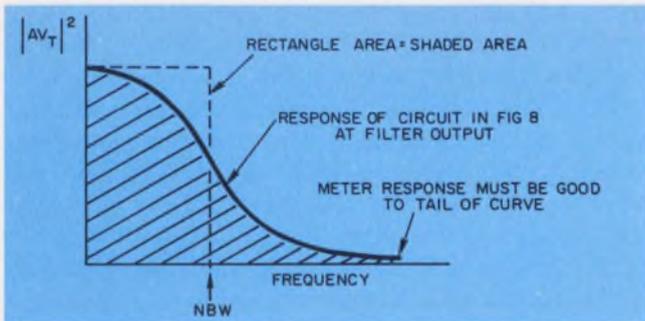
The average noise spectral density per  $\sqrt{\text{Hz}}$  is

$$\frac{E_{nti}}{\sqrt{\text{Hz}}} = \frac{E_{no}}{AV_T \sqrt{\text{NBW}}} \text{ in } V_{RMS}/\sqrt{\text{Hz}}$$

To measure the  $E_n$  component of op-amp noise, short out resistors  $R_{s1}$  and  $R_{s2}$ . Then calculate  $E_{nt}$  as follows:

$$E_{nt} = (E_{n1}^2 + E_{n2}^2)^{1/2} = \frac{E_{no}}{AV_T \sqrt{\text{NBW}}} \text{ in } V_{RMS}/\sqrt{\text{Hz}}$$

In this measurement, resistance  $R_{A2}$  and resistance ratio  $R_F/R_I$  must be sufficiently low so their thermal noise voltages are much lower than  $E_n$ .



9. The filter noise-power bandwidth (NBW) isn't the same as its 3-dB bandwidth.

To measure the total input noise current of the op amp,  $I_{nT} = (I_{n1}^2 + I_{n2}^2)^{1/2}$ , let  $R_{s1}$  and  $R_{s2}$  be equal and sufficiently high in value so  $I_n R_s$  is at least four times larger than  $E_n$  plus  $4kTR_s$ . An estimate of  $I_{nT}$  can be made by calculation of the theoretical value of  $I_n$  at midband from the relation

$$I_{nT} \approx 1.4 \sqrt{2qI_{IB}} \approx 1.4 I_{n1},$$

where 1.4 accounts for the fact that there are two noise-current generators, one at each input.  $I_{IB}$  is the input bias current. With the measured value of  $E_{nti}$ , calculate  $I_n$  as follows:

$$I_n \approx \frac{E_{nti}}{R_s} = \frac{E_{no}}{AV_T \sqrt{NBW} R_s} \text{ in } A/\sqrt{Hz}.$$

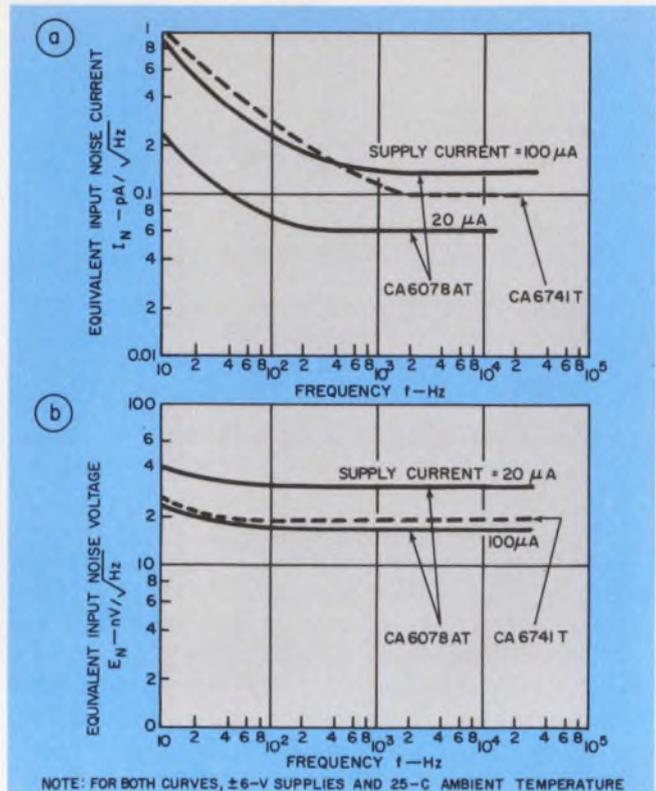
If  $E_n$  and  $4kTR_s$  are not negligibly small compared with  $I_n R_s$ , then  $I_n$  can be calculated from the measurement of  $E_{nti}$  as follows:

$$I_{nT} = \frac{\sqrt{E_{nti}^2 - E_{nT}^2 - 8kTR_s}}{R_s} \text{ in } A/\sqrt{Hz}.$$

Measurements of  $I_n$  when the values of  $R_s$  are very high must be performed carefully. Any shunt capacitance across  $R_s$ , including its own stray capacitance, can reduce the impedance of  $R_s$ , thereby reducing thermal noise and the  $I_n R_s$  product. The reduction results in an erroneous measurement of  $I_n$ . In addition instabilities might result from stray capacitance from the inverting terminal to ground or from the stray feedback capacitance to the noninverting input. Finally measurements of  $E_{nti}$  should be carried out in a well-shielded enclosure, because inputs terminated with high impedance are susceptible to hum pickup.

These problems are most severe when attempts are made to measure the very low midband noise currents of op amps with FET inputs or of op amps with bipolar transistor inputs and exceptionally low input-bias currents. Midband noise results primarily from shot noise, caused by input bias current flow ( $I_{IB}$ ) in the bipolar op amp or by gate-leakage current ( $I_{GL}$ ) in the FET op amp. Hence a simpler method to determine midband  $I_n$  is to measure  $I_{IB}$  and  $I_{GL}$  and then calculate  $I_n$ .

For op amps with bipolar-transistor inputs,



10. Compare noise characteristics of a programmable op amp, the CA6078T with a more conventional bipolar type, the CA6741T. Note the tradeoff between  $I_n$  (a) and  $E_n$  (b) for the same supply current.

use these formulas:

$$I_{n1} = \sqrt{2qI_{IB1}},$$

$$I_{n2} = \sqrt{2qI_{IB2}},$$

$$I_{nT} = \sqrt{I_{n1}^2 + I_{n2}^2} \text{ in } A/\sqrt{Hz}.$$

For FET inputs, these are the corresponding formulas:

$$I_{n1} = \sqrt{2qI_{GL1}},$$

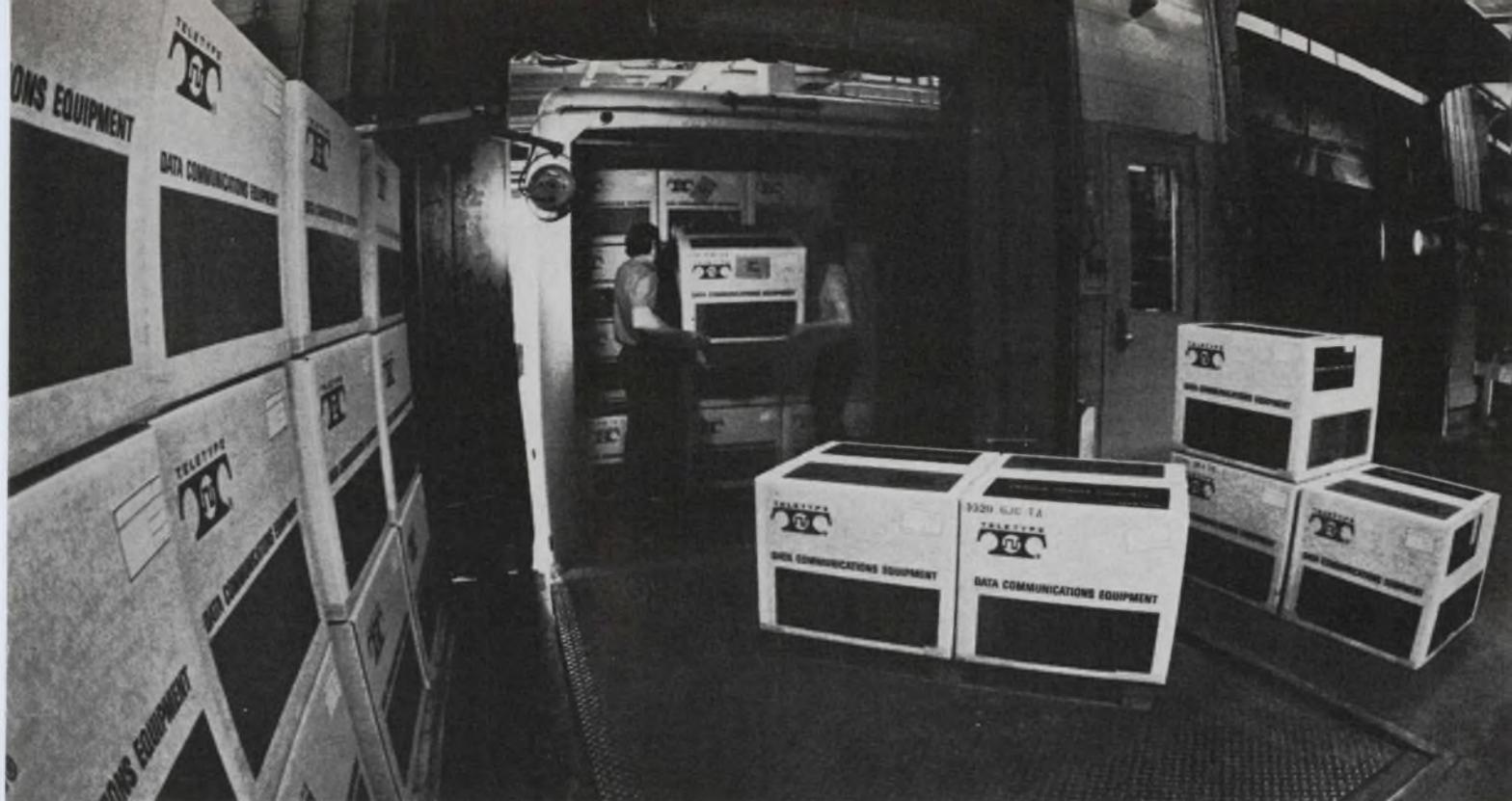
$$I_{n2} = \sqrt{2qI_{GL2}},$$

$$I_{nT} = \sqrt{I_{n1}^2 + I_{n2}^2} \text{ in } A/\sqrt{Hz}.$$

Fig. 10 shows the noise-current and noise voltage spectral-density curves for two bipolar-input op amps. Curves for the programmable amplifier exhibit the tradeoff between  $E_n$  and  $I_n$  as a function of operating current. ■■

#### References

1. Van Der Ziel, A., "Thermal Noise in Field Effect Transistors," *Proc. IEEE*, August, 1962.
2. Motchembacker and Fitchem, "Low Noise Electronics Design," John Wiley & Sons, New York, 1973, pp. 103-106.
3. Robe, T. J., "Measurement of Burst (Popcorn) Noise in Linear Integrated Circuits," *RCA Application Note ICAN-6732*, or *RCA Solid State DATABOOK Series SSD-202B*.
4. *RCA Data Bulletins CA6741T and CA6078T*, File No. 592, or *RCA Solid State DATABOOK Series SSD-201B*.
5. *RCA Data Bulletin CA3095E*, File No. 591, or *RCA Solid State DATABOOK Series SSD-201B*.
6. Robe, T. J., "Designing with an IC Transistor Array Containing Matched Super-Beta Transistors," *RCA Application Note ICAN-6222*.



## **Hundreds of thousands of model 33s have got to tell you something.**

What it tells you is that the model 33 is very popular in both message and data communications.

And the reasons behind this popularity are important to the hearts of most businessmen. Economy. Reliability. And versatility.

These are the three product qualities we started with when the model 33 was first introduced. And over the years we haven't forgotten them. That's why we've always had a team of engineers assigned to the model 33. Their job: make the model 33 even more economical, more reliable and more versatile.

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How much longer will we continue selling the model 33?

For as long as there's a market for economy, reliability and versatility. And the way things look today, that's going to be for a long, long time.

It takes more than manufacturing facilities to build the terminals Teletype<sup>®</sup> Corporation offers. It also takes commitment. From people who think service is as important as sales. In terminals for computers and point-to-point communications.

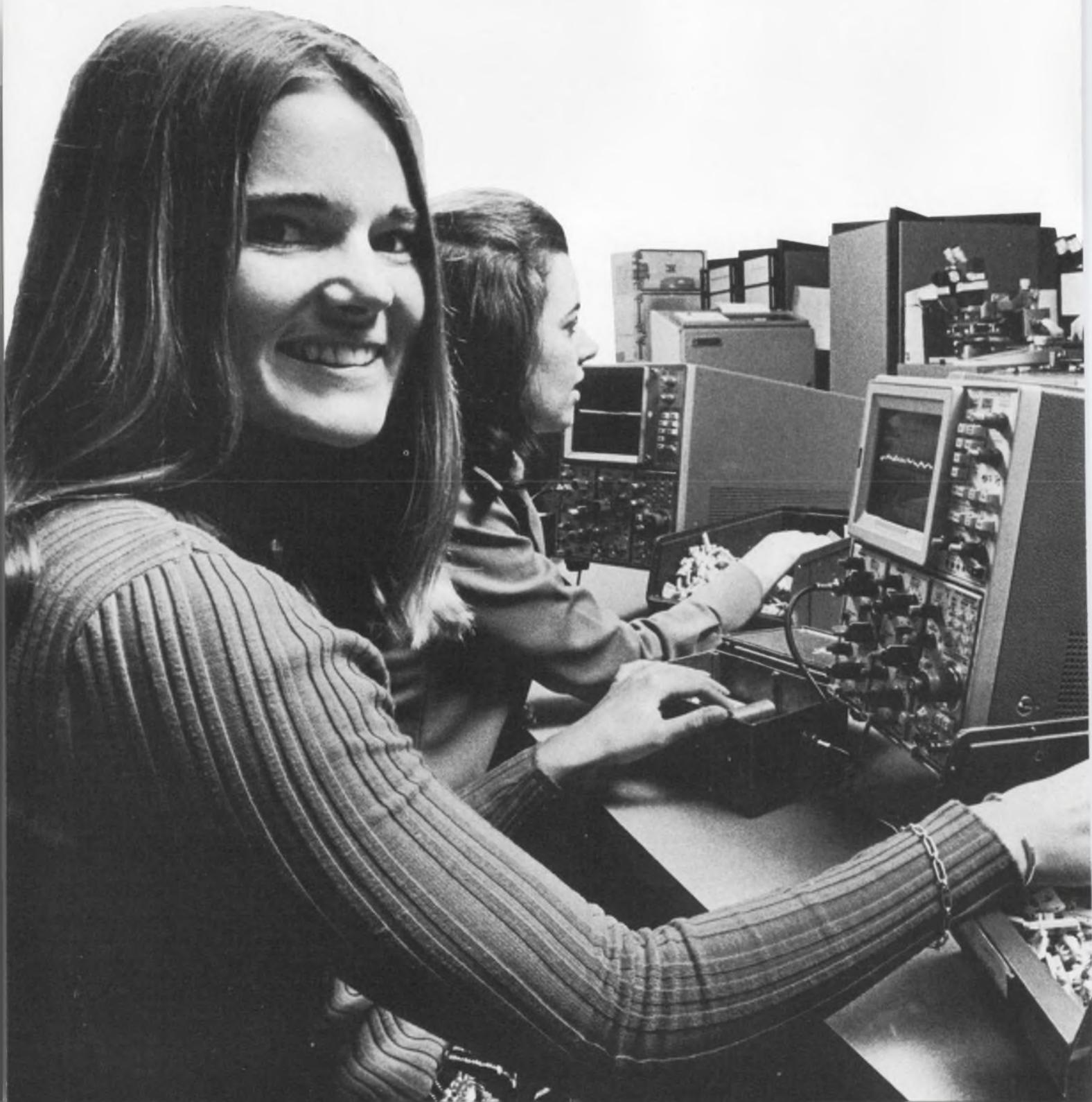


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# **FINALLY. A LOW NOISE GUARANTEE COMES TO IC FET OP AMPS.**

**The Analog Devices AD514 and how it came about.**



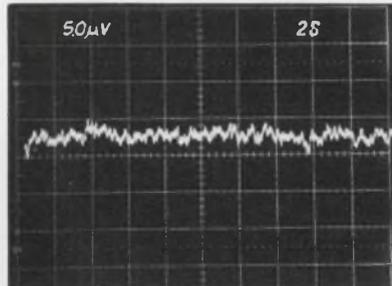
While everyone else was neglecting FET op amp noise performance, we were paying attention.

First we talked to people who worked with EKG amplifiers, pH electrode amplifiers, long term integrators— wherever noise was a problem.

Then we went to work.

The result is the AD514. An IC FET-input op amp carefully designed and processed for low noise. So you get a noise voltage level below  $5\mu\text{V}$ (p-p) max. And that's guaranteed. Because every AD514 is tested for noise parameters.

You also get a low bias current of  $10\text{pA}$  max, and a low  $V_{os}$  drift of  $25\mu\text{V}/^\circ\text{C}$ . And you'll find versions of the AD514 priced from \$5.90 to \$9.90 in hundreds.



AD514 noise performance.

**But this isn't our first FET op amp.**

It all began back with our original, general purpose, low bias current IC FET op amp. It was the first IC FET op amp ever introduced anywhere by anyone.

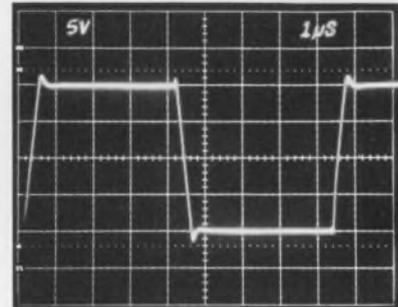
That became the prototype for the AD523. An IC J-FET op amp with a  $0.25\text{pA}$  max bias current and a cost of \$18.75 in hundreds. Which was one-third to one-half the cost of conventional low bias current op amps.

You liked the idea. So you asked for another one. This time with low drift.

That's when we gave you the AD506L. It offers you  $10\mu\text{V}/^\circ\text{C}$  max drift.

Along with  $1\text{mV}$  max offset voltage to maintain that low drift— even after nulling. All for only \$16 in hundreds.

High speed came next in the AD528. With a unity gain slew rate of  $70\text{V}/\mu\text{sec}$ . that needs no external compensation. Plus a bandwidth of  $10\text{MHz}$  and a price of \$12 in hundreds.



AD528 transient response.

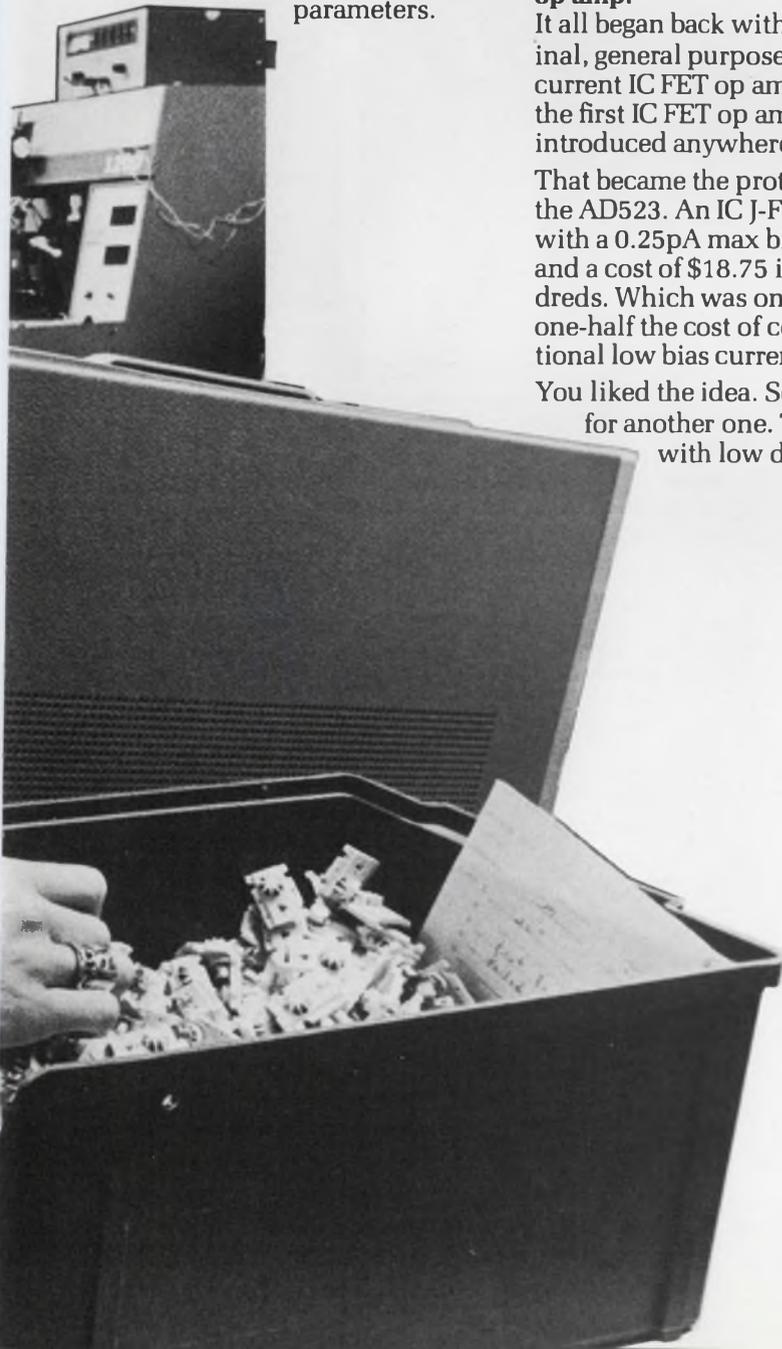
Sometimes though, your budget is low and you're willing to trade off some speed to find a lower price. That's when the AD540, with a slew rate of  $6\text{V}/\mu\text{sec}$ . and a price of only \$4.45 in hundreds goes to work.

As you can see, we're prepared to give you the IC FET op amp performance you need in the quantities you want.

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INFORMATION RETRIEVAL NUMBER 39



# Multiplex signals the analog way, and save on both parts count and cost. High-speed analog multiplexers provide the same accuracy as the converter-per-sensor scheme.

To reduce system complexity and cost, use analog signal multiplexing instead of digital. For many high-speed data-acquisition applications, the new analog signal-multiplexers are a low-cost alternative to schemes that use digital multiplexing and many analog-to-digital (a/d) converters.

Digital multiplexing circuits do, of course, have the highest speed, and their accuracy is almost assured—the signals are converted right at the source. However, today's analog signal multiplexers are just as accurate and almost as fast as the older multiconverter systems.

As an example, assume you must digitize 10 data channels, each of 250 kHz, to 8 bits a piece. A digital multiplexed system would require 10 converters, each capable of 0.5-MHz operation and each with a matching sample-and-hold (s/h) circuit. On top of this, add the costs of a high speed digital multiplexer and the control logic, and you get a system cost well over \$10,000.

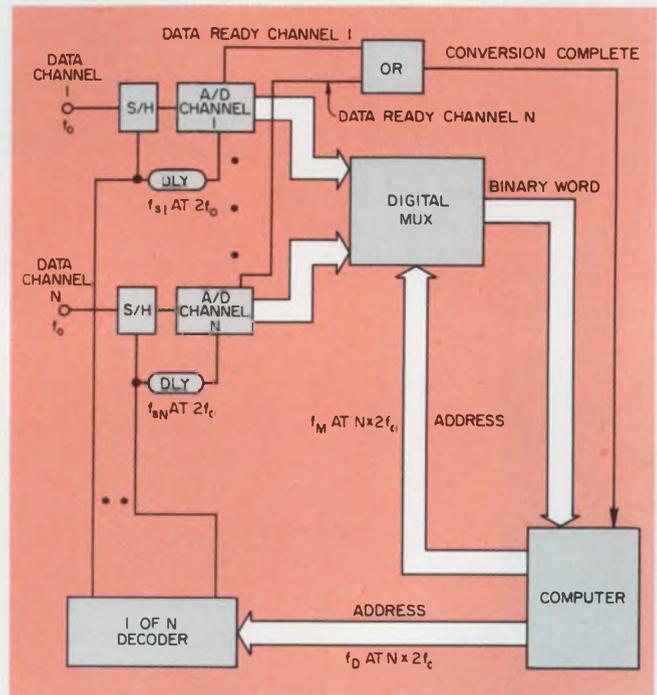
If you use an analog system, all you need is one a/d converter capable of operation at 5 MHz and a matching sample-and-hold. In front of this combination, you put the high-speed analog multiplexer. The cost for a system like this is less than half that of the digital multiplexing system.

In operation, the analog multiplexing system is similar to the digital, but it has fewer sub-systems. Let's compare the two.

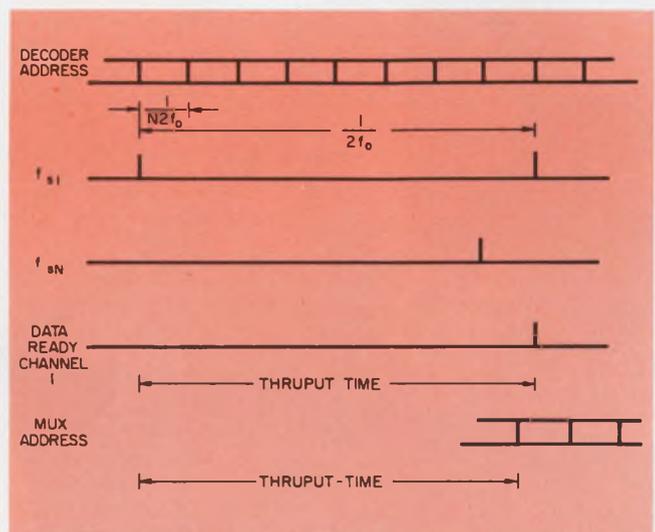
## A glimpse at digital multiplexing

The multichannel data-acquisition system in Fig. 1 can handle  $N$  channels of data. If we assume that each of the channels has a maximum frequency content of  $f_o$ , then each must be sampled at  $2f_o$ , as a minimum (which satisfies the Nyquist criterion for undistorted recovery of sampled data).

The computer must generate a binary address at a rate of  $N \times 2f_o$ . Then, under control of a decoding network, the respective channel will be sampled and the conversion process initiated.

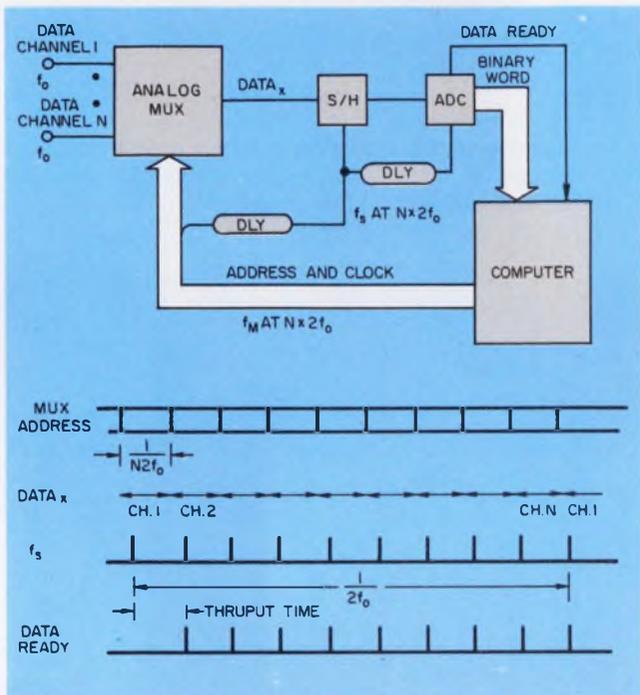


1. Block diagram of a digitally multiplexed data-acquisition system shows duplication of components for each of the data channels.



2. The timing sequence of the digital system has many delays associated with the addressing and decoding of the converters by the computer.

Lou Ruggeri, Senior Engineer, Inter-Computer Electronics, Subsidiary of American Electronic Laboratories, P.O. Box 507, Lansdale, Pa. 19446.



3. An analog multiplexer system is much less complex than its digital counterpart. Even the timing waveforms are much simpler for the analog system.

Typically the throughput time of the digitizing process is fixed; it depends directly upon the s/h circuit and the a/d converter selected.

Based upon this value, the computer issues another set of address commands. These instructions follow the same sequence as those presented to the decoder, but shifted in time (Fig. 2). The second address, when presented to the digital multiplexer, selects the channel that will next complete its conversion cycle.

A data-ready pulse, generated by the a/d converter, signals conversion completion and tells the computer that the data on the signal lines are valid. The same pulse can also be used to clock the data word into the computer.

You can build a simpler, equivalent system that does analog signal multiplexing (Fig. 3). In this case, a control unit must also generate address words and a synchronous clock signal. Each of these signals will cause a particular data line to

be connected onto the input line of the s/h circuit. After sufficient time has elapsed to allow for settling of the multiplexer output, the data can be sampled. Once the signal is sampled, it is encoded by the a/d converter and is delivered to the computer for analysis or storage.

For the analog system to handle the data as fast as the digital system does, all of its components must be capable of operation at the higher  $N \times 2f_0$  rate. You have only to choose the analog multiplexer with the range you need.

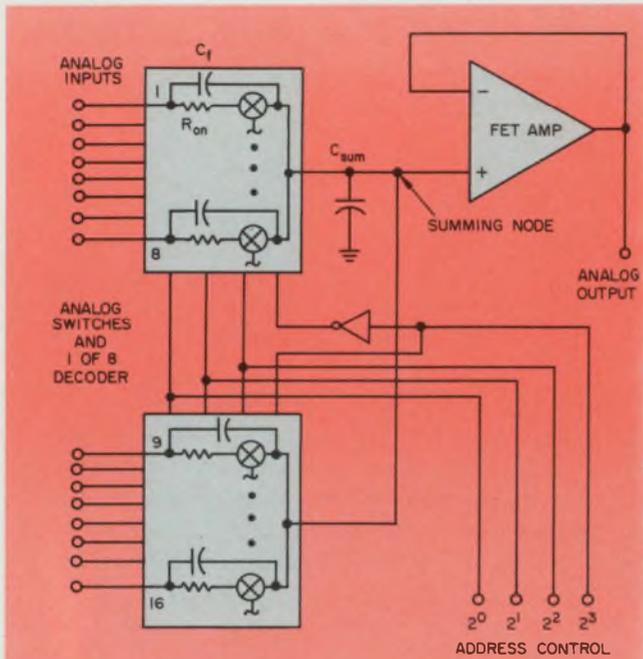
#### Analog multiplexer error sources

Obviously when you place an analog multiplexer in series with the signal flow, additional error sources can creep in (Fig. 4). When a multiplexer channel is selected, the analog signal sees the ON resistance of the switch and any load impedance in series with it. This impedance network forms a voltage divider that causes an error in the transfer accuracy. The ohmic value, especially in MOS switches, is often a function of the input signal level, but it can be minimized with some extra buffering. If a FET amplifier is used as a buffer/driver, it affects the over-all impedance transformation through the multiplexer.

In the switch, you also have a feedthrough capacitance,  $C_f$ , that allows a portion of the signal to be coupled through the OFF switch. This occurs in spite of a typical OFF impedance of 1 GΩ or so. The capacitance forms another voltage divider, combining with  $C_{sum}$  and  $R_{on}$  of the addressed channel, and causes crosstalk.

The capacitance of the multiplexer output,  $C_{sum}$ , becomes the total capacitive load to ground.  $C_{sum}$  is the amplifier input capacitance plus the sum of each component contributed by the OFF channel. The total channel OFF capacitance in this case is  $N-1$  times the output capacitance of one channel. This capacitive reactive component forms a time-constant with the ON resistance, and along with the amplifier's slew rate, it can be the limiting factor in the multiplexer's ability to settle quickly.

Even with these different error sources, you have analog devices available that can provide 16-



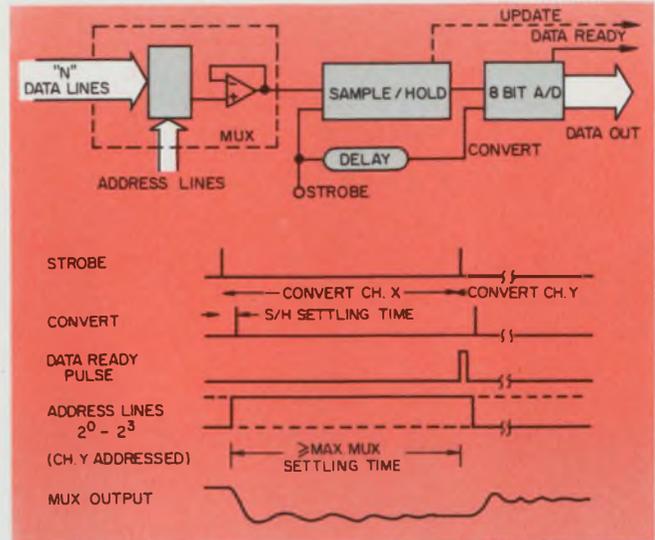
TRUTH TABLE				
2 <sup>0</sup>	2 <sup>1</sup>	2 <sup>2</sup>	2 <sup>3</sup>	CHANNEL SELECTED
0	0	0	0	1
1	0	0	0	2
0	1	0	0	3
1	1	0	0	4
0	0	1	0	5
1	0	1	0	6
0	1	1	0	7
1	1	1	0	8
0	0	0	1	9
1	0	0	1	10
0	1	0	1	11
1	1	0	1	12
0	0	1	1	13
1	0	1	1	14
0	1	1	1	15
1	1	1	1	16

4. The internal circuitry of an analog signal multiplexer has many possible error sources. Internal resistance and capacitance creates many leakage paths.

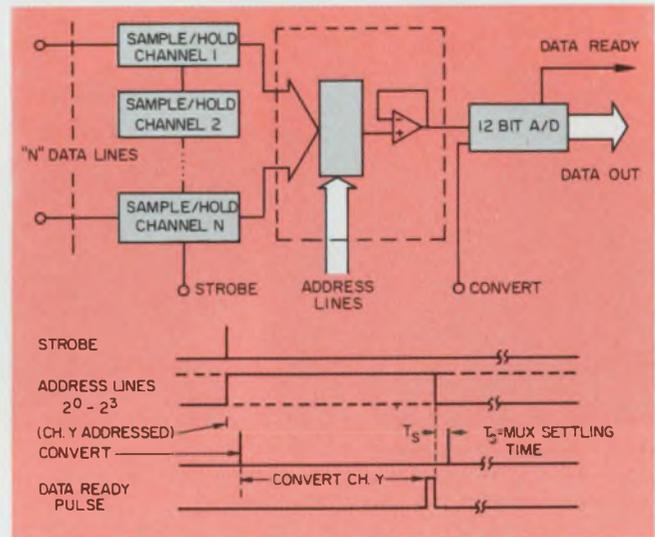
channel operation with 10-to-12-bit precision. Some of these units have settling times of 300 ns to  $\pm 0.01\%$  of full scale. When multiplexers like these are used with an addressing scheme called "preaddressing," you can convert your system to analog multiplexing with no loss in accuracy or conversion rate.

**Preaddressing: A faster way to get data**

Analog multiplexers can interface with the input of any sample-and-hold system or with the output of a bank of low-droop, high-accuracy sample-and-holds. Each method provides an N-level-to-1 translation and enables many channels of data to be processed by a single a/d converter.



5. Preaddressing the multiplexer helps to maintain the high conversion rate of the combined sample-and-hold amplifier and analog-to-digital converter.



6. For multichannel sample-and-hold applications, add the multiplexer settling time to the converter throughput time to find the maximum conversion rate.

The circuit in Fig. 5 shows a method of preaddressing the multiplexer in which the address gets updated shortly after the previously selected channel is sampled. This updating can be done either by programming control of the timing sequence or by the sample-and-hold update signal. While conversion of the previously selected channel's data is being performed, the multiplexer is allowed to settle to whatever desired accuracy you need prior to the next strobing.

As long as the reciprocal of the combined conversion rate of the s/h circuit and the a/d converter is greater than the maximum settling time of the multiplexer, the over-all system throughput isn't degraded.

Fig. 6 shows another method of data multiplex-



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## SPECIFICATIONS FOR LX SERIES

### DC Output

#### Regulated Voltage

regulation, line . . . . . 0.1%  
regulation load . . . . . 0.1%  
ripple and noise . . . . . 1.5 mV RMS, 5 mV pk-pk with either  
positive or negative terminal grounded  
temperature  
coefficient . . . . . 0.03%/°C

### AC Input

line . . . . . 105-132 VAC; 47-440 Hz. For 187-242 VAC, add  
suffix "V" to model numbers and add 12% or  
\$30.00 to the price, whichever is greater. For  
operation of LX-D, LXS-E, LX-EE, LXS-7, and  
LXS-8 units at 50 Hz or at 400 Hz, consult factory.  
Ratings apply to 57-63 Hz. For all other models  
delete 40°C rating for 50 Hz operation.

### Ambient operating temperature range

continuous duty from 0° to + 71°C with corresponding load  
current ratings for all modes of operation.

### Storage temperature range

-55°C to +85°C

### Overload protection

#### Thermal

thermostat, automatic reset when over-temp. condition is re-  
moved. (Not applicable to LX-D-3); circuit breaker must be reset  
on LX-8 models.

#### Electrical

external overload protection, automatic electronic current limit-  
ing circuit limits the output current to the present value,  
thereby providing protection for load as well as power supply.

### Overshoot

no overshoot on turn-on, turn-off or power failure.

### Input and output connections

through terminal block on chassis; output terminals on LX-7,  
LX-8 models are two heavy duty studs.

### Power hybrid voltage regulator or integrated circuit regulation

some models have Power Hybrid Voltage Regulator providing  
complete regulation system while others have an integrated  
circuit providing regulation system except for input and output  
capacitors, rectifiers and series regulation transistors.

### Controls

#### DC Output Control

simple screwdriver voltage adjustment over entire range.

#### Remote sensing

provision is made for remote sensing to eliminate effect of  
power output lead resistance on DC regulation.

### Transformer

MIL-T-27C, Grade 6

### Tracking accuracy (dual models)

2% absolute voltage difference; 0.2% change for all conditions  
of line, load and temperature.

### Fungus proofing

All fungi nutrient components are rendered fungi inert with  
MIL-V-173 varnish—Standard on all LX models and is included  
in price.

## 5 VOLTS ±5% SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-A-5-OV-R*	4.0	3.4	2.7	2.0	\$ 95.
LXS-B-5-OV-R*	5.8	5.0	4.0	3.0	130.
LXS-4-5-OV-R*	7.4	6.5	5.4	3.9	145.
LXS-C-5-OV-R*	9.0	8.0	6.8	5.3	160.
LXS-CC-5-OV-R*	16.0	14.5	12.7	10.5	220.
LXS-D-5-OV-R*	27.5	24.2	20.5	16.5	260.
LXS-E-5-OV-R*	35.0	30.0	24.0	17.5	320.
LXS-EE-5-OV-R*	45.0	39.0	32.0	25.0	445.
LXS-7-5-OV-R**	65.0	56.0	46.0	35.0	535.
LXS-8-5-OV-R**	85.0	77.0	68.0	56.0	580.

\*Includes fixed overvoltage protection at 6.8V ±10%

## 6 VOLTS ±5% SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-A-6-R	3.7	3.1	2.5	1.9	\$ 95.
LXS-B-6-R	5.5	4.7	3.8	2.9	130.
LXS-4-6-R	6.6	5.8	4.8	3.5	145.
LXS-C-6-R	8.8	7.8	6.7	5.2	160.
LXS-CC-6-R	15.2	13.8	12.1	10.0	210.
LXS-D-6-R	26.5	23.4	19.8	16.0	260.
LXS-E-6-R	34.0	29.0	23.0	16.5	320.
LXS-EE-6-OV-R†	42.0	36.0	30.0	22.0	445.
LXS-7-6-OV-R**	59.0	50.0	41.0	32.0	535.
LXS-8-6-OV-R**	70.0	70.0	68.0	56.0	580.

†Includes fixed overvoltage protection at 7.4V ±10%

## 12 VOLTS ±5% SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-A-12-R	2.7	2.2	1.8	1.5	\$ 95.
LXS-B-12-R	3.8	3.6	3.0	2.2	130.
LXS-4-12-R	4.4	3.8	3.1	2.5	145.
LXS-C-12-R	6.5	6.1	5.5	4.6	160.
LXS-CC-12-R	10.5	9.4	8.2	5.0	210.
LXS-D-12-R	16.0	14.0	11.9	8.0	260.
LXS-E-12-R	21.0	18.0	15.0	12.5	320.
LXS-EE-12-R	32.0	27.0	22.0	16.0	420.
LXS-7-12-OV-R**	40.0	36.0	30.0	23.0	535.
LXS-8-12-OV-R**	50.0	45.0	40.0	34.0	580.

## 15 VOLTS ±5% SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-A-15-R	2.4	2.0	1.6	1.3	\$ 95.
LXS-B-15-R	3.2	2.8	2.5	1.5	130.
LXS-4-15-R	4.0	3.5	2.8	2.3	145.
LXS-C-15-R	6.0	5.6	5.1	4.5	160.
LXS-CC-15-R	9.5	8.6	7.4	4.8	210.
LXS-D-15-R	14.0	12.3	10.4	7.5	260.
LXS-E-15-R	19.0	17.0	14.0	12.0	320.
LXS-EE-15-R	28.0	24.0	19.5	14.0	420.
LXS-7-15-OV-R**	36.0	32.0	26.0	20.0	535.
LXS-8-15-OV-R**	45.0	41.0	36.0	30.0	580.

\*\*Built-in continuously adjustable overvoltage protection crowbars output  
when trip level is exceeded. Included on all LXS-7, LXS-8 models.

# GUARANTEED LX SERIES. DELIVERY.

## 20 VOLTS $\pm 5\%$ SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-CC-20-R	7.7	7.2	6.5	4.4	\$210.
LXS-D-20-R	11.5	10.2	8.6	6.8	260.
LXS-E-20-R	15.0	13.0	10.5	7.0	320.
LXS-EE-20-R	22.0	18.5	14.5	10.0	420.
LXS-7-20-OV-R**	28.0	25.0	20.5	15.5	535.
LXS-8-20-OV-R**	32.0	29.0	25.0	17.0	580.

## 24 VOLTS $\pm 5\%$ SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-CC-24-R	6.8	6.4	5.7	4.4	\$210.
LXS-D-24-R	10.0	8.8	7.5	6.0	260.
LXS-E-24-R	13.0	11.0	9.5	6.0	320.
LXS-EE-24-R	19.0	16.5	13.0	9.5	420.
LXS-7-24-OV-R**	25.0	22.0	18.0	14.0	535.
LXS-8-24-OV-R**	30.0	27.0	23.5	17.0	580.

## 28 VOLTS $\pm 5\%$ SINGLE OUTPUT

MODEL	MAX. AMPS AT AMBIENT OF:				PRICE
	40°C	50°C	60°C	71°C	
LXS-CC-28-R	6.0	5.6	5.0	4.3	\$210.
LXS-D-28-R	9.0	8.0	6.8	5.5	260.
LXS-E-28-R	11.0	10.0	8.5	5.5	320.
LXS-EE-28-R	17.0	15.0	12.0	9.0	420.
LXS-7-28-OV-R**	22.0	19.5	16.0	12.5	535.
LXS-8-28-OV-R**	28.0	25.5	22.5	17.0	580.

## $\pm 15$ TO $\pm 12$ VOLTS DUAL OUTPUT <sup>(1)</sup>

MODEL	ADJ. VOLT. RANGE VDC	MAX. AMPS AT AMBIENT OF:				PRICE
		40°C	50°C	60°C	71°C	
LXD-3-152-R	$\pm 15$	0.400	0.370	0.340	0.300	\$ 90.
	to $\pm 12$	0.400	0.370	0.340	0.300	
LXD-A-152-R	$\pm 15$	1.0	1.0	0.9	0.7	130.
	to $\pm 12$	0.8	0.8	0.7	0.6	
LXD-B-152-R	$\pm 15$	1.6	1.4	1.2	0.7	160.
	to $\pm 12$	1.4	1.3	1.1	0.6	
LXD-C-152-R	$\pm 15$	2.5	2.3	1.9	1.5	170.
	to $\pm 12$	2.0	1.8	1.5	1.2	
LXD-CC-152-R	$\pm 15$	4.0	3.7	3.2	2.4	255.
	to $\pm 12$	3.0	2.7	2.3	1.8	
LXD-D-152-R	$\pm 15$	6.2	5.6	4.9	4.0	300.
	to $\pm 12$	4.5	4.1	3.7	3.0	
LXD-EE-152-R	$\pm 15$	12.5	11.0	9.0	7.0	455.
	to $\pm 12$	10.0	9.0	7.8	6.0	

Overvoltage protector accessory available for all models without built-in overvoltage protection.

(1)  $\pm 15$  to  $\pm 12$  and  $\pm 6$  to  $\pm 3$  volts are each dual tracking outputs; dual outputs can be connected in series for 30-24 volts and 12-6 volts, respectively.

## $\pm 6$ TO $\pm 3$ VOLTS DUAL OUTPUT <sup>(1)</sup>

MODEL	ADJ. VOLT. RANGE VDC	MAX. AMPS AT AMBIENT OF:				PRICE
		40°C	50°C	60°C	71°C	
LXD-B-062-R	$\pm 6$	2.7	2.4	1.9	1.4	\$170.
	to $\pm 3$	2.1	2.0	1.6	1.2	
LXD-C-062-R	$\pm 6$	3.5	3.3	2.7	1.7	180.
	to $\pm 3$	2.6	2.4	1.9	1.3	

## 5 VOLTS $\pm 5\%$ , $\pm 15$ TO $\pm 12$ VOLTS TRIPLE OUTPUT

MODEL	ADJ. VOLT. RANGE VDC	MAX. AMPS AT AMBIENT OF:				PRICE
		40°C	50°C	60°C	71°C	
LXT-D-5152-R	5 $\pm 5\%$ *	12.0	11.5	11.0	9.5	\$395.
	to $\pm 15$	3.1	2.7	2.2	1.7	
	to $\pm 12$	2.3	2.0	1.7	1.3	

\*5 volt output has fixed overvoltage protection at 6.8V  $\pm 10\%$ .  $\pm 15$  to  $\pm 12$  output is dual tracking output.

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INFORMATION RETRIEVAL NUMBER 40

# Why complicate frequency synthesis?

A direct digital method not only controls frequency, but also phase and wave shape—difficult with analog circuits.

Complicated mixers, discriminators and oscillators can be eliminated from frequency synthesizers if you use digital, rather than analog, techniques.

Unlike an analog frequency synthesizer, the digital, when supplied with a clock frequency and a binary frequency-control number, computes digital samples of the output frequency directly and continually. These samples are then converted into a continuous analog signal by a digital-to-analog (DAC) converter and a low-pass filter (Fig. 1).

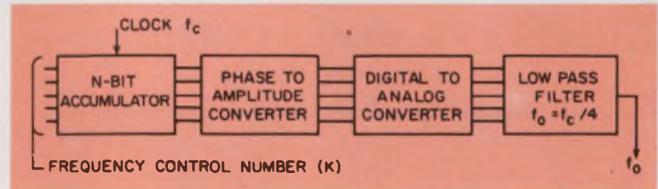
Once the basic principle of operation is understood, the designer can easily modify the circuit to select his own frequency range, frequency step size and maximum distortion. The frequency stability of the output signal is the same as that of the clock.

The synthesizer's first part, called the phase accumulator, determines the frequency range and resolution. The second part, called the phase-to-amplitude converter, converts the phase representation of the sine wave into an amplitude representation.

## Digital samples are accumulated

As shown in a simplified 4-bit example (Fig. 2a), the wave shape to be synthesized—say, a sine wave—is broken down into a number of equally spaced phase points, and each point is represented by a binary number. The 16 phase points of the sine wave need a minimum four-bit binary word to represent them (Fig. 2b).

The phase accumulator is simply an N-bit binary accumulator. The output of the accumulator at any time corresponds to a phase of the wave shape between 0 and 360 degrees. The frequency control number, K, represents a small phase-angle step that is added to the accumulator by each clock pulse every  $1/f_c$  seconds. Periodically the accumulator overflows. This occurs between 359 and 0 degrees. The rate of



1. A direct digital frequency synthesizer needs inputs of a clock frequency and a binary control number to generate a controlled output frequency.

overflow is equal to the output frequency,  $f_o$ . When N is the accumulator length,

$$f_o = Kf_c/2^N.$$

Since K can occur only in integer values, the frequency steps are in increments of  $f_c/2^N$ . Thus with a 20-bit accumulator and when  $f_c = 1.048$  MHz,  $f_o$  is in 1-Hz steps.

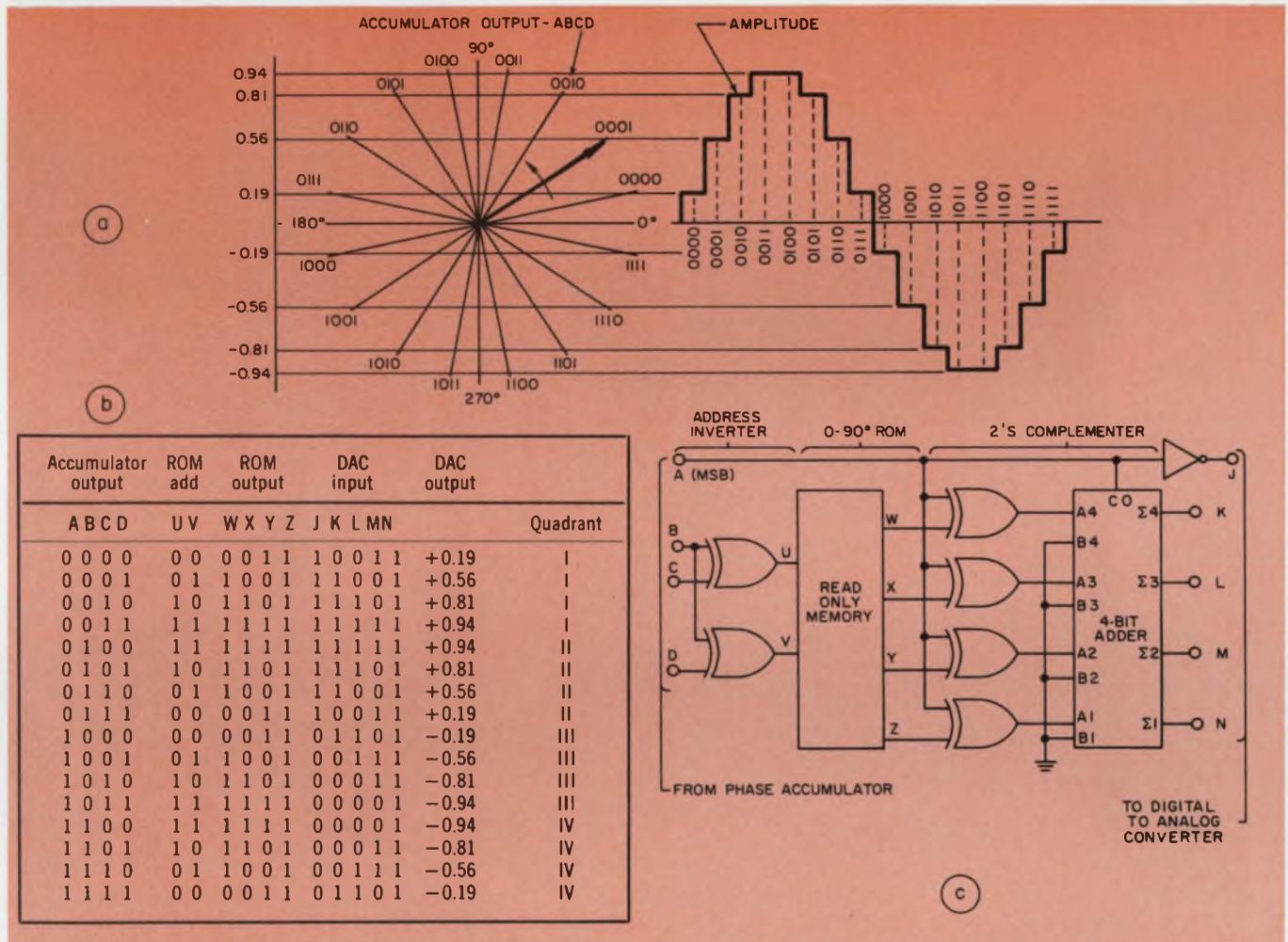
The phase-to-amplitude converter is basically a read-only-memory (ROM) that is programmed to contain amplitude values for the desired wave. To address the ROM by M bits is equivalent to dividing the 0-to-360-degree phase circle into  $2^M$  parts. It doesn't matter what angles are selected to be stored in the ROM; they need only be uniformly spaced. But if the wave shape has symmetry with the 180 and 0-degree axis and also the 90 and 270-degree axis (Fig. 2a), then, with some additional logic, a 0-to-90-degree ROM can be used to give values throughout the 0-to-360-degree range. The symmetry decreases the size of the ROM by a factor of four.

In this technique the two most-significant-bit outputs from the phase accumulator determine the quadrant of the signal, and the remaining bits address the 0-to-90-degree ROM (Fig. 2c). Note that the address of the ROM is inverted by bit "B" when the signal is in quadrant II or IV and the output of the ROM is TWOs-complemented by bit A when the signal is in quadrant III and IV. Also, the A signal is inverted to become the sign bit to the DAC.

## A 20-bit design example

A practical example of this synthesizer technique uses a clock frequency of 1.048 MHz and

Hamil W. Cooper, PE, Consultant, P.O. Box 9691, Austin, Tex. 78766.



2. A simplified synthesizer for sine waves takes advantage of symmetry of the wave shape so that values for

only 0 to 90 degrees need be stored. A d/a converter and filter (not shown) provide the final output.

a 20-bit accumulator (Fig. 3). The frequency resolution is therefore 1 Hz, and the maximum practical frequency is  $1.048 \times 10^6/4$ , or 262 kHz. Although TTL is used in this circuit, CMOS or DTL would work equally well. The accumulator consists of five 4-bit adders (SN7483) and 10 dual-D flip-flops (SN7474). The ROM is an AMI S8771 sine/cosine lookup table—a commercially available device. This particular ROM, however, divides the 0-to-90-degree quadrant into only  $2^7 - 1$  segments instead of  $2^7$  segments—

which would be preferred—but the error is insignificant.

The digital-to-analog converter is a 10-bit Datal DAC-I-10B, which has a settling time of 150 ns. The ONES-complement of the output of the ROM is used directly, instead of the TWOS-complement, as in Fig. 2, because this greatly simplifies the circuit and introduces very little error. The five dual-D flip-flops that precede the DAC are used to hold the DAC input during accumulator transitions to reduce output glitches.



The flip-flops can be eliminated with DACs that have internal storage.

Even though the synthesizer can generate frequencies to 262 kHz, a filter ( $f_c = 100$  kHz, four-pole Krohn-Hite Model 3202) ensures that the alias frequencies are at least 70 dB down from the fundamental. Also, output noise then is mainly from quantization and not from alias distortion.

The signal-to-noise ratio table shows measured and calculated distortion values for the 20-bit circuit over the frequency range of 10 to 60 kHz.

#### Digital synthesis has advantages

The primary advantage of this digital synthesizer over most analog versions is its positive control over the output. There is no question that the output frequency is specific for a given frequency control number and clock frequency. A linear FM sweep can be fashioned simply by the use of a binary counter to generate the control number. The start and stop count and the rate at which the counter is clocked will determine the sweep's characteristics.

For a random sequence, a custom programmed ROM can be addressed by the counter, and this ROM's output will supply frequency-control numbers. A very linear voltage-controlled oscillator can be made by the use of an a/d converter to generate the control numbers.

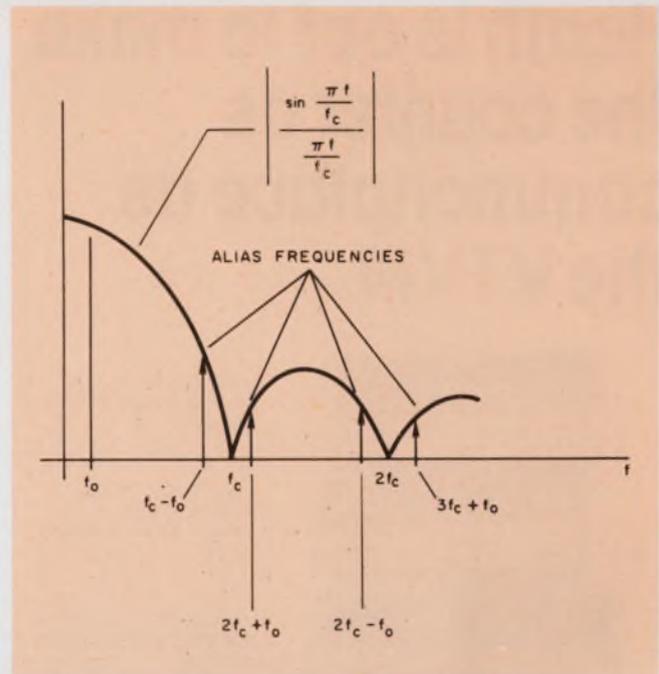
But no matter what the source of instruction is for the frequency changes, no phase discontinuities occur in the direct digital synthesizer.

Very accurate phase control is also possible. At any time the phase of the signal may be set to any desired value; the appropriate binary number is fed into the accumulator flip-flop clear and preset inputs. And the phase could be shifted by insertion of another adder between the output of the phase accumulator and the phase-to-amplitude converter. The size of the phase shift would depend on the number added to the accumulator output.

The output level of the synthesizer may be controlled by the use of a multiplying DAC or by an attenuator in the output.

The direct digital synthesizer also could synthesize signals other than sine waves. If the output of the accumulator is directly applied to the DAC, a saw-tooth wave results. If the most-significant bit of the accumulator is then used to complement the subsequent outputs of the accumulator, the result, when applied to the DAC, would be a triangular wave.

A square wave is obtained by use of only the most-significant bit of the accumulator as the output. And any arbitrary waveform can be produced if the entire phase-to-amplitude converter section is replaced with an appropriately pro-



4. Frequency-aliasing of a synthesizer limits the upper output frequency to about  $f_c/4$ .

grammed ROM that contains equally spaced values of the signal from 0 to 360 degrees.

#### Quantization is a problem

But digital synthesizers have their problems, too. The designer must contend with phase and amplitude-quantization noise, noise generated by the digital-to-analog converter and alias frequencies that pass through the nonideal low-pass filter. In general, phase and amplitude-quantization noise is constant and independent of the output frequency, while noise from the digital-to-analog converter increases with frequency.

For the sine-wave circuit in Fig. 3, the signal-to-noise ratio (SNR) that results from amplitude quantization can be expressed as<sup>1</sup>

$$\text{SNR} = 1.5 (2^A - 1)^2, \quad (1)$$

where A is the number of bits of amplitude quantization.

When expressed in decibels, the SNR becomes

$$\text{SNR}_{\text{dB}} \approx 6A + 1.75. \quad (2)$$

Experimental data taken on the synthesizer in Fig. 3 show that phase-quantization noise can be expressed approximately as

$$S/N \approx 6.8(2^{2B}),$$

where B is the number of bits of phase quantization. When expressed in decibels, the SNR becomes

$$\text{SNR}_{\text{dB}} \approx 6B - 8.3 \quad (3)$$

When Eqs. 1 and 2 are combined vectorially, the approximate relationship between the number of bits of phase and amplitude quantization and the output SNR is obtained (see table):

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## Measured and calculated signal-to-noise ratios

Measured S/N dB		Bits of phase quantization (B)				
		7	8	9	10	11
Bits of amplitude quantization (A)	6	33.2	36.8	38.0	38.2	38.2
	7	33.4	37.0	37.7	37.7	37.7
	8	33.6	39.2	42.6	44.0	44.4
	9	33.7	39.4	43.0	43.7	43.7
	10	33.8	39.7	45.2	48.8	50.3
11	33.7	39.7	45.4	49.0	49.7	
	33.5	38.8	46.0	52.5	55.2	
12	33.7	39.7	45.7	51.4	54.0	
	33.6	39.2	46.0	52.2	58.0	
13	33.7	39.7	45.7	51.7	57.0	
	33.7	39.7	45.7	51.7	57.0	

$$S/N \text{ dB} = -10 \log \sqrt{\frac{0.44}{2^{1A}} + \frac{46.0}{2^{1B}}}$$

$$SNR_{dB} \approx -10 \log \sqrt{\frac{0.44}{2^{1A}} + \frac{46.0}{2^{1B}}} \quad (4)$$

DACs add noise to the signal whenever a switching transient occurs. Therefore fast-setting DACs that have shorter transients introduce less noise. Further noise reduction results when the DAC is followed by a sample-and-hold circuit, where sampling occurs after the transients have subsided. And, finally, a large amount of this noise is also eliminated by the low-pass filter.

If the signal-to-noise ratio of the circuit is limited by quantization, greater spectral purity can be obtained only by use of more bits of quantization. Noise purity of 70 dB requires about 12 bits of amplitude quantization and 13 bits of phase quantization. However, the circuit requires a 2048 12-bit ROM.

A better alternative perhaps would be to use a ROM with only 64 12-bit words, and use linear interpolation to determine the amplitudes for intermediate values of phase. In Fig. 3 the eight most-significant bits of the accumulator would select the coarse phase points and the ninth through 13th bits would be interpolated.

Since this synthesizer provides an output sample every  $1/f_c$  seconds, the DAC output spectrum contains alias frequencies at  $f_c \pm f_o$ ,  $2f_c \pm f_o$ , ... etc., with amplitudes as shown in Fig. 4. A low-pass output filter must pass the output frequency,  $f_o$ , and reject the alias frequencies. Such a filter becomes quite complex when  $f_o$  approaches  $f_c/2$ . Therefore  $f_o$  should be less than  $f_c/4$ . ■■

### Reference

1. Stein and Jones, "Modern Communications Principles," McGraw-Hill, 1967, p. 208.

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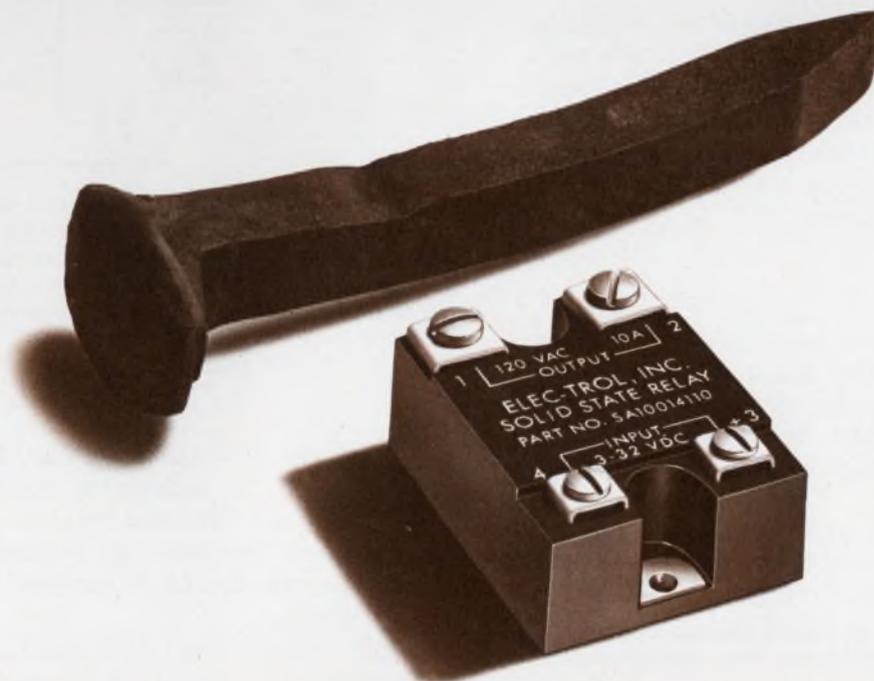
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INFORMATION RETRIEVAL NUMBER 42

# Design with lockout logic and get control of data lines. The circuits use as little as one contact per subscriber to prevent multiple use of a line.

When data must be transmitted over a party telephone line, the designer who understands lockout circuitry can prevent multiple use of the line. This also prevents eavesdropping, of course.

The simplest circuits can be built with relays (Fig. 1). To understand the circuit operation, assume that all relays are initially de-energized. If  $S_2$  is now depressed, an electrical circuit is completed between bus 1 and ground. The path is via the normally closed contacts of  $K_2$ , the coil of  $K_2$ , the button, the common wire and finally  $CR_1$  and  $CR_2$ . Because of the control relay,  $K_C$ , the 24-V-dc source is connected to bus 1 through the normally closed contact. Current therefore flows through  $CR_1$  and  $CR_2$ . The resulting voltage drop allows  $Q_1$  to turn on and thereby energize  $K_C$ .

Once  $K_C$  closes, the dc source is transferred from bus 1 to bus 2. And since the capacitors delay operation of relays  $K_1$  to  $K_N$ ,  $K_2$  will remain shut.

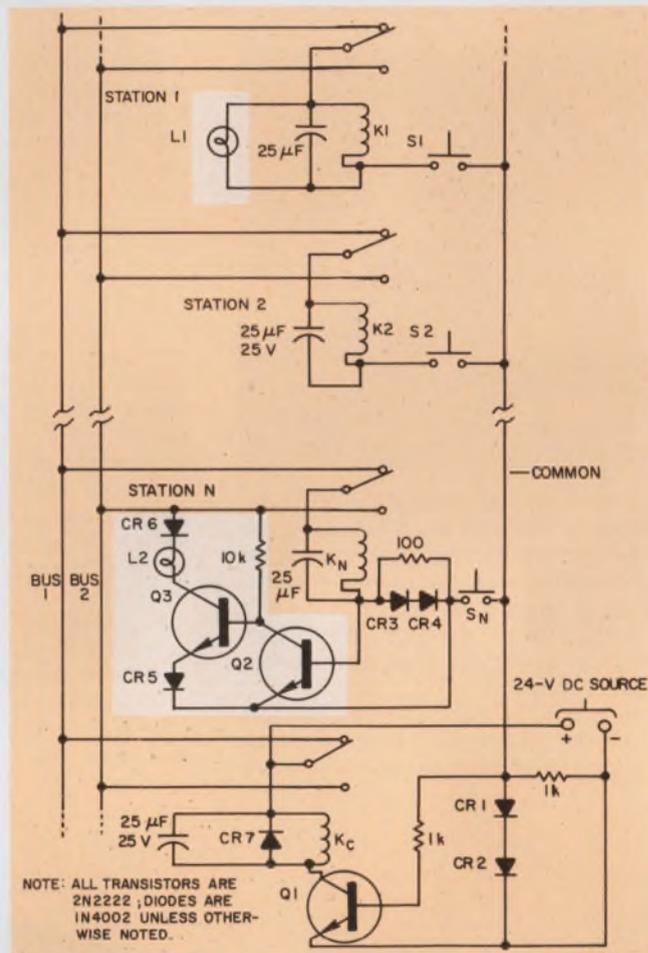
The necessary lockout has occurred. None of the other relays can operate until  $S_2$  is released. Only then will the control relay release and restore power to bus 1.

The circuit scheme allows use of an indefinite number of control relays,  $K_1$  to  $K_N$ . A single pole, double-throw contact is necessary for lockout. The remainder of the relay contacts perform the required switching operations. Delay capacitors needn't be used if the single control contacts are the make-before-break type.

## Lamps show line status

You can give the user a status signal in one of two ways: (1) A "line available" lamp, such as  $L_1$  is lighted when the relay closes. (2) A "busy" lamp lights when the user depresses a button and someone else on a different circuit has the line.

The transistor circuit use for the second method requires a voltage to exist on bus 2. This indi-

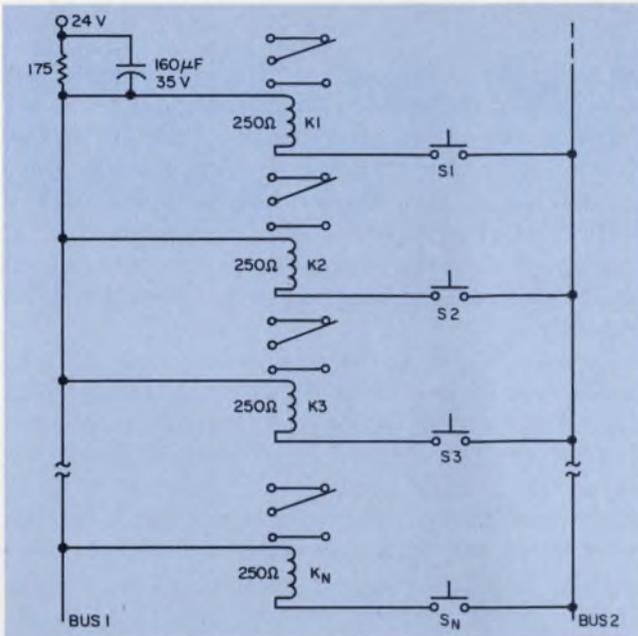


1. **Simple lockout circuits** can be built with relays. Only one station at a time can gain access when its corresponding relay operates. As long as the station is active, the other stations are locked out, because the control relay,  $K_C$ , has transferred power from bus 1 to bus 2. Lamps  $L_1$  or  $L_2$  and associated circuitry provide busy indications for the user.

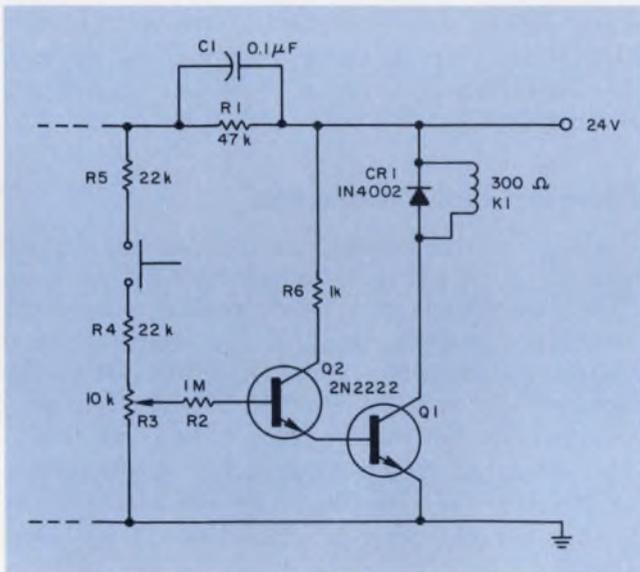
cates that the bus-transfer relay,  $K_C$ , has operated. When  $S_n$  is depressed, no current flows through  $CR_n$  and  $CR_1$ , and transistor  $Q_2$  is biased off. Therefore transistor  $Q_3$  conducts and lights  $L_2$ ; bias current for  $Q_3$  is supplied by the 10-k $\Omega$  base resistor.

But if current flows through  $K_n$ , the voltage drop across  $CR_3$  and  $CR_1$  biases on  $Q_2$  which

Dr. Walton N. Hershfield, Communications Consultant, Bentley Engineers, 149 New Montgomery, San Francisco, Calif. 94105.



2. No extra contacts are required in a lockout circuit, if you select relays for their pull-in and hold voltages. The initial current surge from  $C_1$  closes a relay when the station button is depressed. Once the capacitor charges, the voltage between bus 1 and bus 2 is less than that required for the other relays to operate.



3. Relay driver built with a Darlington amplifier helps reduce control current and gives adjustable relay differentials between the operate and hold conditions. The hold voltage is set with  $R_3$ .

in turn keeps  $Q_1$  off. And the busy lamp will not operate.

### Capacitor scheme eliminates contacts

Another type of lockout circuit that does not require relay contacts takes advantage of the difference in pull-in (closing) and release (open)

voltage of the relay (Fig. 2). With 24-V relays of certain mechanical design you should be able to select some that operate at 18 V and release at 5 V. This would be for a 250- $\Omega$  coil.

If  $R_1$  is selected as 175  $\Omega$ , then with a 24-V well-regulated power supply, the voltage drop across the relay would be 14.12 V. Obviously this is not large enough to pull the relay closed. That's where capacitor  $C_1$  comes into play. If its value is large—160  $\mu\text{F}$  at 35 V dc—and it has discharged to zero volts through the 175  $\Omega$  resistor, the closing of pushbutton switch (for example  $S_1$ ) will start a current charge surge through  $C_1$ . The surge will exceed the 18-V pull-in voltage of the relay and allow the relay to close. However, as  $PB_1$  is held shut, the dc condition of the relay stabilizes, and the voltage across  $C_1$  settles to approximately 10 V, thereby ensuring that the relay stays closed.

If while  $S_1$  is closed, another pushbutton—say,  $S_3$ —is also closed, the associated relay will not close. Why? Because the voltage between bus 1 and bus 2 is below the nominal 18-V pull-in voltage of the relay. Hence the other relays are locked out.

There is, however, one defect to this circuit. If too many pushbuttons are depressed, the closed relay may drop out. In the case of the circuit shown in Fig. 2, an excess of four relays across the line—the control and three others—would cause the control relay to fall open. But in circuits that are subject to random use of a single line—say, from five or 10 points—such multiplicities of simultaneous use seldom occur.

A more sensitive lockout circuit results if you use the current gain of a two-transistor Darlington circuit (Fig. 3). The parameters of  $K_1$  are selected as follows: 300- $\Omega$  coil resistance, pull-in at 18.0 V, release at 6.0 V. Each transistor has a nominal current gain of 250; the circuit provides a total current gain of 62,500.

For purposes of calculation, use an average current gain of 60,000. To have the relay pull in, the circuit must develop 18 V across a 300- $\Omega$  load, which means a 60-mA relay current. With a nominal current gain of 60,000, the control current to the base of  $Q_2$  equals 1  $\mu\text{A}$ .

A little arithmetic will show that with the contact potential of a silicon transistor, the total voltage drop at the base of  $Q_2$  is approximately 1.2 V dc. To limit the current flow to 1  $\mu\text{A}$ , the 24-V supply source would require a 22.8-M $\Omega$  series resistor. Since this value is quite large, a series resistance of 1 M $\Omega$  should be selected instead and the potentiometer in Fig. 3 should be used.

If 15 V were the hold voltage for the relay, you could adjust potentiometer  $R_3$  so the relay would pull in and then back off to get 15 V across the coil. In this case  $Q_1$  is not saturated

and will dissipate 9 V at 60 mA, or 720 mW. So pick  $Q_1$  to dissipate the power.

Notice that there is the same capacitor as in Fig. 2, but because the currents are lower, a 0.1- $\mu$ F capacitor is more than adequate. The discharge time (RC constant) is only one-half second for  $R_1$  and  $C_1$ .

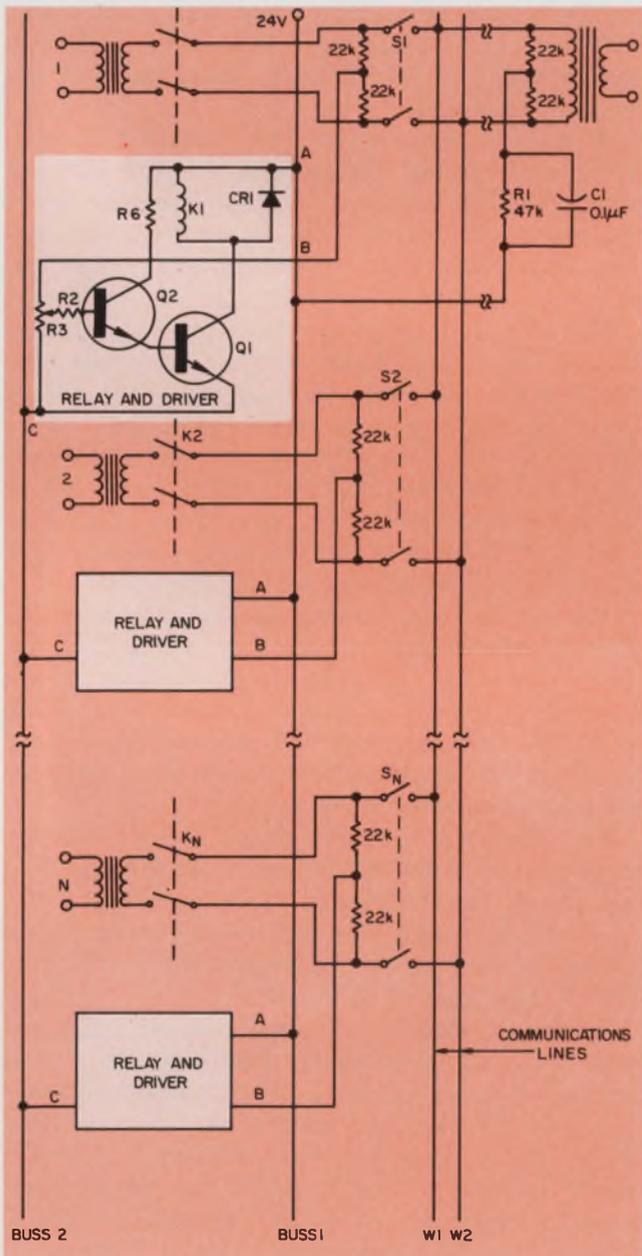
Operation of the pushbutton will cause a current surge through capacitor  $C_1$ . The surge into  $Q_2$  will be adequate for pull-in. When  $C_1$  is

charged, the circuit will settle and supply the 15 V needed to hold the relay closed.

Fig. 4 shows one practical application of the circuit. A common balanced transmission line,  $L_1$  and  $L_2$ , is used. It could be a typical 600- $\Omega$  0-dBm telephone line, a 45- $\Omega$  intercom line, a slow-speed data-transmission system or a 25 or 70.7-V audio-transmission system. Operation is as follows:

Assume that  $S_1$  is closed and that lines  $L_1$  and  $L_2$  are not in use. A voltage surge through  $R_1$ ,  $C_1$  and the 22-k $\Omega$  bridge resistors will trigger  $K_1$  to close. The driver circuit then settles to 15 V for the holding condition. If circuits 2 to  $N$  try to use the line, the voltage developed across their relays will be too low for them to operate.

This circuit is really a version of the one in Fig. 2, except that the current amplification allows use of 22-k $\Omega$  resistors. These are quite large compared with the 600- $\Omega$  line impedance; hence the line (equivalent to 22 k $\Omega$ ) is quite small. In addition the control current is limited to approximately 300  $\mu$ A, a value that normally will not damage small transformers. The circuit of Fig. 4 requires three wires and a ground. This is sometimes cumbersome, particularly if a twisted pair is the only line available. There might also be some objection to use of a positive 24-V-dc line. (If a negative ground is desired, the circuit can be designed with pnp transistors and reversed battery polarity.)



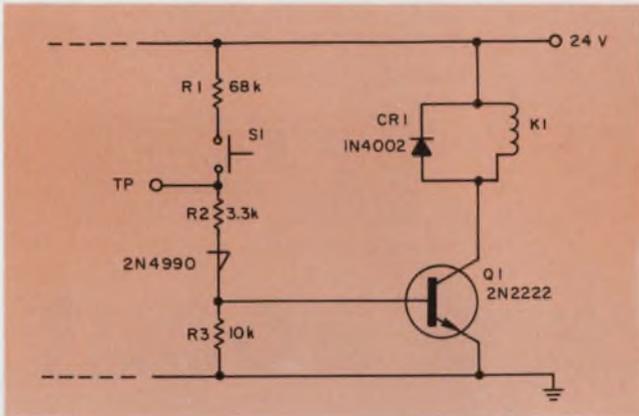
4. Stations 1 to  $N$  are connected to a data or phone line. The Darlington drivers, in conjunction with  $R_1$  and  $C_1$ , allow operation of only one station at a time. The 22-k bridge resistors provide sufficient control current, approximately 300  $\mu$ A, yet present a negligible load to the communications line.

#### Silicon-controlled-switch lockout

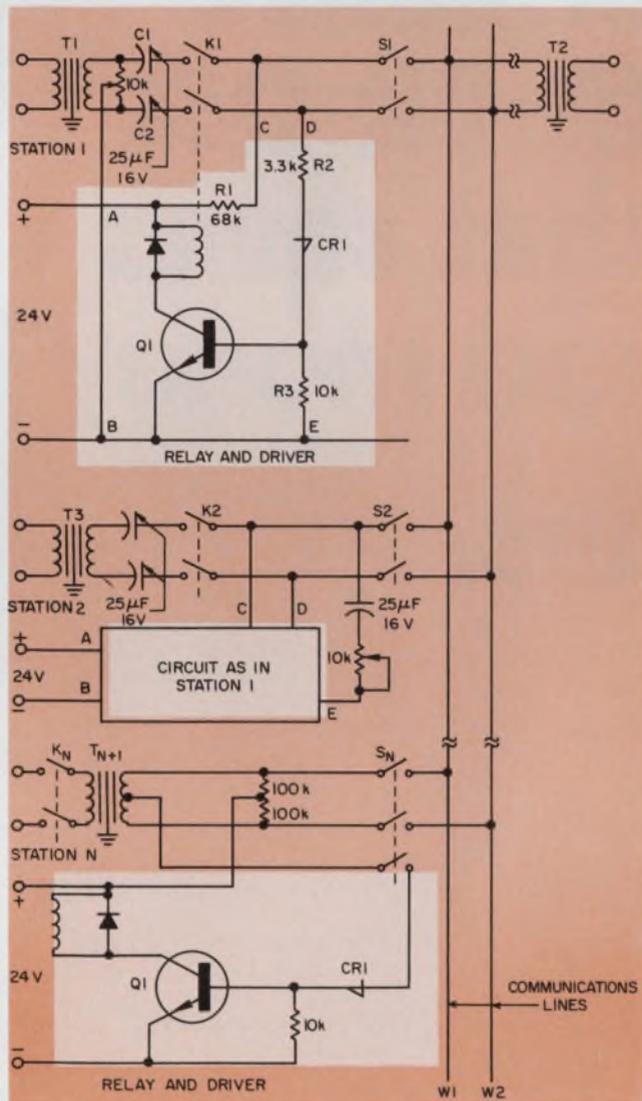
An interesting circuit, which does not depend upon the charge surge of a capacitor or the open-close differential of a relay, makes use of the breakdown characteristics of a silicon unilateral switch, the 2N4990 (Fig. 5). When OFF, the voltage differential across the 2N4990 is 7 to 9 V; when ON, the voltage drops to less than 1.0 V. Once fired, the switch requires 200  $\mu$ A to remain on. The unit can handle up to 175 mA, yet the leakage current prior to breakdown is less than 0.2  $\mu$ A.

To provide the 200- $\mu$ A sustaining current with a 24-V supply, the total circuit resistance cannot exceed 120 k $\Omega$ . For safety, the sustaining current of 325  $\mu$ A is selected. The total resistance used, 70.3 k $\Omega$ , takes account of voltage drops across  $CR_1$  and  $Q_1$ .

For correct operation in a lockout circuit, the voltage at test-point TP must drop to less than 7 V after  $CR_1$  turns on, so any circuits in parallel with TP will not turn on their respective relays. The voltage drops across  $CR_1$  and  $Q_1$  add up to 1.2 V in the ON condition. The drop across  $R_2$  is set for 1.07 V with a 325- $\mu$ A maintenance cur-



5. Lockout relay driver built with a silicon switch diode does not depend on relay characteristics or use an RC discharge. The switch provides the necessary differential between pull-in and hold voltages.



6. Use of the silicon switch circuit allows lockout operation with the twisted-pair alone. Circuits to balance the line are recommended. The first two use a 10-k potentiometer (stations one and two) and the third scheme requires a three-pole switch.

rent. If the pushbutton is closed with CR<sub>1</sub>, ON, R<sub>1</sub> has 22 V across it. Its value, 68 kΩ, gives the 325-μA maintenance current. The value of 3.3 kΩ for R<sub>2</sub>, assures low voltage at the test point. Under ideal conditions 1.07 V is dropped across R<sub>2</sub> and 1.2 V across CR<sub>1</sub> and Q<sub>1</sub> to make the total voltage at TP 2.27 V.

Conductors W<sub>1</sub> and W<sub>2</sub> represent an ordinary twisted-pair transmission line; transformer T<sub>1</sub> is the common circuit (Fig. 6). If switch S<sub>1</sub> is closed, the 24-V supply is applied to R<sub>1</sub>. Diode CR<sub>1</sub> conducts, and Q<sub>1</sub> is biased on. Relay K<sub>1</sub> closes to complete the balanced-line circuit between T<sub>1</sub> and T<sub>2</sub>. If the dc primary resistance of T<sub>1</sub> is small compared with the 68-kΩ and 3.3-kΩ resistors, the voltage on the line, L<sub>2</sub>, will be less than the turn-on voltage of CR<sub>1</sub> in circuits 1 to N. L<sub>2</sub> feeds the other selector switches, S<sub>2</sub> to S<sub>N</sub>. Therefore the closure of any switch S<sub>2</sub> to S<sub>N</sub> will not make the corresponding relay operate.

The dc load current caused by operation of any switch is approximately 0.2 μA, or the equivalent of 70 MΩ. Such current levels are certainly not enough to turn Q<sub>1</sub> on. Hence this circuit does not require additional conductors.

### Keep the lines balanced

Without additional corrective circuitry, the 68-kΩ and 3.3-kΩ resistors—one on each line—could unbalance the line and degrade the common-mode rejection. A typical value for such lines is 40 dB—which represents a ratio of 100:1 between the in-phase, common-mode voltages, applied to both sides of T<sub>2</sub>, and the out-of-phase voltage across the transformer. With balanced IC inputs, the ratio increases to 60 or 70 dB—more than 1000:1.

There are at least three different ways to correct this condition. A 10-kΩ balance potentiometer can be added, as shown, for T<sub>2</sub>. Potentiometer R<sub>1</sub>, in conjunction with C<sub>3</sub> can be used, or a three-pole switch and a pair of 100-kΩ resistors will do the job.

These circuits will prevent incompatible use of the line—such as between data exchange, TTY, remote tone controls and analog data transmission. In coded fire-alarm systems such circuits prevent simultaneous transmission of signals.

In addition the circuits can be expanded to furnish dc remote control of various functions at the same time that superimposed ac signals transmit other data. And there are a variety of forms. For example, time-division multiplexers have lockout properties if you have exclusive access to a line. A voltage applied to a clamp circuit in an IC will stop transmission until the line is free. ■■

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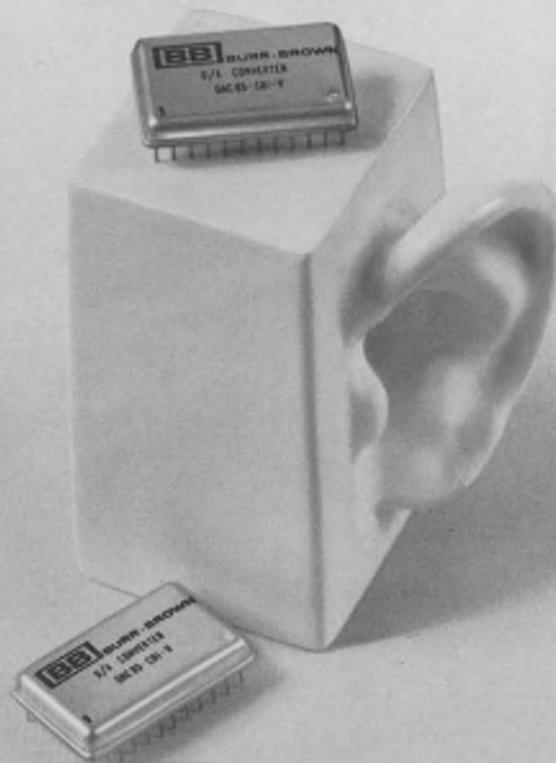
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INFORMATION RETRIEVAL NUMBER 44

# Interpolate sampled data rapidly.

Discrete Fourier transforms provide a mathematical short cut due to a quirk in classical sampling theory.

You can interpolate sampled data rapidly—to find values between the sampled points—by using Discrete Fourier Transforms (DFTs). With these transforms, data sampling allows what amounts to a mathematical short cut—one that automatically generates results as precise as conventional, and lengthy, interpolation techniques. But there are a few restrictions.

The short cut can be applied only when the sampled function is band-limited. Fortunately most practical interpolation tasks—such as those for synthesized speech data or geophysical phenomena—involve band-limited signals.

## The flip side of Nyquist

The interpolation technique is based on an unstated corollary of the Nyquist sampling theorem. The theorem states that the sampling frequency must be at least twice the highest frequency component of the signal if one is to faithfully represent the signal. This implies that nothing is gained by sampling at a frequency above the Nyquist rate. But though no new information is developed, rapid sampling does allow interpolation of the existing data.

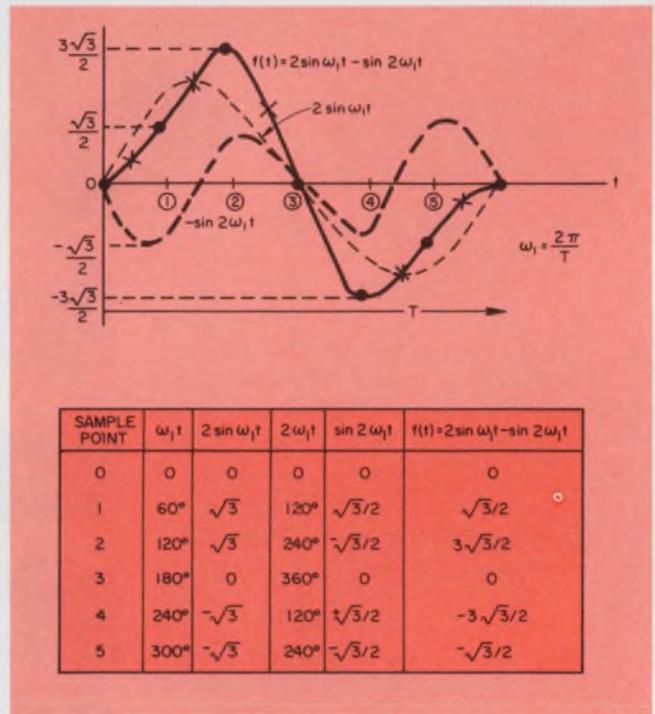
To sample at a higher-than-necessary rate, you must artificially add zeros (zero-amplitude frequencies) outside the spectrum under study. Then you can recover data in the amplitude domain. These data points are interstitially positioned and therefore not present in the original sampled data.

If the sampling rate satisfies the Nyquist criterion, the sampled function may be entirely reconstructed by use of DFTs. The process consists of three steps:

1. Calculation of the function's DFT.
2. Addition of a number of zero-amplitude frequencies to the resulting spectrum.
3. Calculation of the Inverse Discrete Fourier Transform (IDFT) of the combined spectrum.

The last step yields interpolated data points

**Richard D. Angelari**, Electronic Engineer, and **Joseph A. Calabria**, Electronic Engineer, Naval Navigation Laboratory, Naval Air Development Center, Warminster, Pa. 18974.



1. In this simplified analysis of the rapid interpolation technique, a function  $f(t)$ , consisting of two sine waves, is bandwidth-limited. The table shows how the curves are derived at the sampling points, 1 thru 5. The dots on the resultant curve represent the actual sampling points for the data, while the X's indicate the locations of interpolated points.

between the sampled data points. Any desired interpolation resolution can be achieved.

## Restrictions of rapid data sampling

There are two restrictions when interpolation is used:

1. The signal must be bandwidth-limited.
2. The sampling frequency must be at least twice the highest-frequency component,  $\omega_0$ , of the signal.

A function is bandwidth-limited if the Fourier transform

$$F(\omega) = (1/2\pi) \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt; \quad (1)$$

is zero outside the interval  $(-\omega_0, \omega_0)$ . In other

words, the Fourier transform,  $F(\omega)$ , is zero for  $\omega \geq \omega_0$ .

The second restriction is dictated by the Nyquist criterion. In the frequency domain, this requires that  $N$  (number of samples per unit time)  $\geq \omega_0/\pi$ .

What happens if you disregard the Nyquist restriction? An error, called aliasing distortion, results. This is an amplitude distortion that is most apparent in the frequency domain.<sup>1</sup> To ensure that aliasing does not occur, increase the number of data samples—or, in effect, increase the sampling rate. Another approach is to diminish the effects of aliasing by low-pass filtering the data to attenuate all harmonics above the sampling frequency.

### Algorithm for discrete Fourier transforms

The algorithm for the discrete Fourier transform is as follows:

$$F(n) = 1/N \sum_{i=0}^{N-1} f(i) e^{-j i n 2\pi/N} \quad (2)$$

and its inverse is given by

$$f(i) = \sum_{n=0}^{N-1} F(n) e^{j i n 2\pi/N}, \quad (3)$$

where  $F(n)$  is the frequency-domain function,  $f(i)$  is the time-domain function,  $j = \sqrt{-1}$ ,  $N$  is the number of sampled points and  $i$  is the sampled number. In general,  $F(n)$  and  $f(i)$  are complex numbers. Eqs. 2 and 3 are based on the standard Fourier integrals:

$$F(\omega) = 1/2\pi \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt; \quad (4)$$

$$f(t) = \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega. \quad (5)$$

The derivations of Eqs. 2 and 3 from Eqs. 4 and 5 have been demonstrated by Bice.<sup>2</sup>

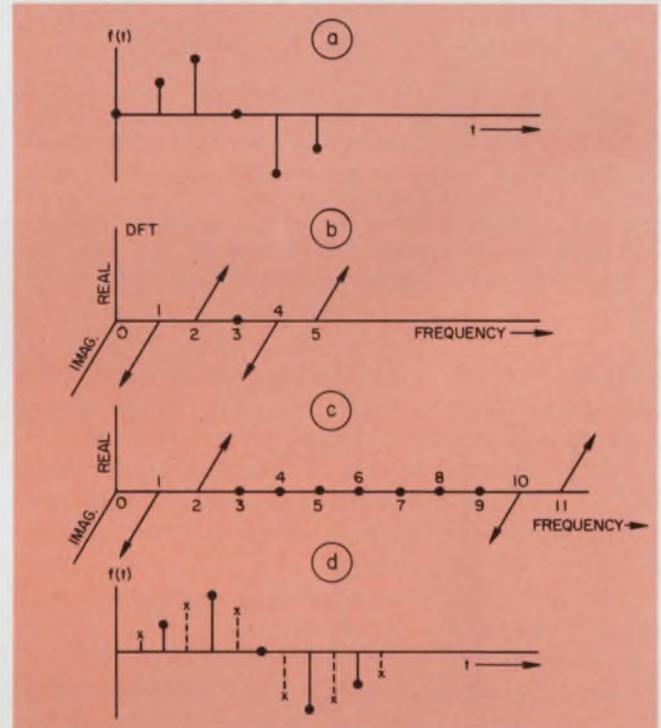
For a simplified illustration of the interpolation technique, let's sample a known bandwidth-limited function. All the functions will be assumed to be periodic. The basic transforms used are programmed in Fortran IV and are useful for relatively low values of  $N$ . For larger values, a Fast-Fourier-Transform (FFT) subroutine is appropriate.

Consider the function  $f(t) = 2\sin \omega t - \sin 2\omega t$ . This is bandwidth-limited, since it consists of only two sine waves, the second having half the amplitude and double the frequency of the first. Fig. 1 shows the function and its frequency components. The table shows the sample points (the dots on the curve) together with the associated sample data. The X's in Fig. 1 indicate the location of the interpolated points, whose values are to be determined.

The problem, of course, is to find the amplitude of the function  $f(t)$  at points between the sampled data points. The procedure to find the interpolated points is as follows:

1. Calculate the DFT of the function from Eq. 2. Fig. 2a represents the sampled function and Fig. 2b its DFT.

2. Determine the number of zero-amplitude frequencies to be added. Then insert  $(r-1)N$  zeros<sup>3,4</sup> in the middle of the frequency sequence, where  $r$  is the number by which we must multiply  $N$  to get the desired number of interpolated data



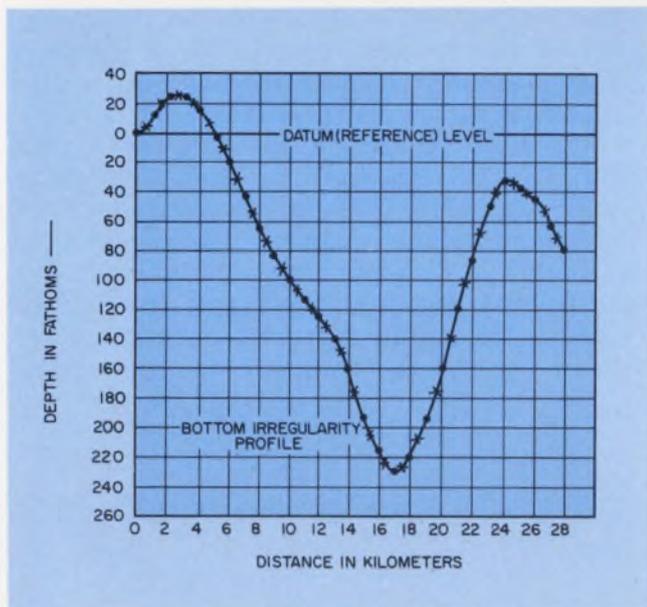
2. The sampled function (a) yields discrete Fourier transforms (b). When extra zeros are added (c) the DFT has the same four values but more points. Then the inverse transformation yields the original curve plus the interpolated points (d).

points. In Fig. 2c,  $N = 6$  and  $r = 2$ . (This says that we started with six data points and desire 12.)

3. The inverse DFT, shown in Fig. 2d, indicates a total of 12 points. If more resolution is required, increase  $r$  accordingly. Note that the original data points are preserved with this technique.

### Important applications in oceanography

Both the commercial and scientific communities show interest in ocean-bottom bathymetry—the measurement of irregularities in shape of the ocean floor. To minimize surveying data-acquisition costs, the number of samples taken should be no more than is needed to achieve the required



3. Rapid data interpolation is often used to expand limited samples of geophysical data. This curve shows the irregularities in a section of the sea bed. The dots represent measured data points, and the X's are interpolated points. For the plot shown,  $N=31$  and  $r=2$ .

definition of the irregularities (after data interpolation). The inexpensive DFT interpolation technique thus offers important cost savings.

In the example of Fig. 3, the mid-point values of 31 digitally recorded data values represent depth below and above a certain datum. Therefore  $N = 31$  and  $r = 2$ .

The interpolated points are compared with those obtained by use of a finite Fourier series, least-square-difference technique. Fig. 3 is a plot of depths vs distance across a seabed irregularity. The solid dots represent measured data points and X's are interpolated points. A mean error of 0.1 fathoms with a standard deviation of 0.43 fathoms was achieved for the interpolated values. The difference is due to the restriction placed on the finite Fourier series program, used to terminate the calculation when a predetermined minimum-squares difference was realized. Theoretically identical results would have been achieved had the program been permitted to continue. In both methods the original data were recovered. ■■

#### Acknowledgment

The authors wish to thank Richard Kaufman of the Naval Navigation Laboratory for the computer program and the resulting plot shown in Fig. 3.

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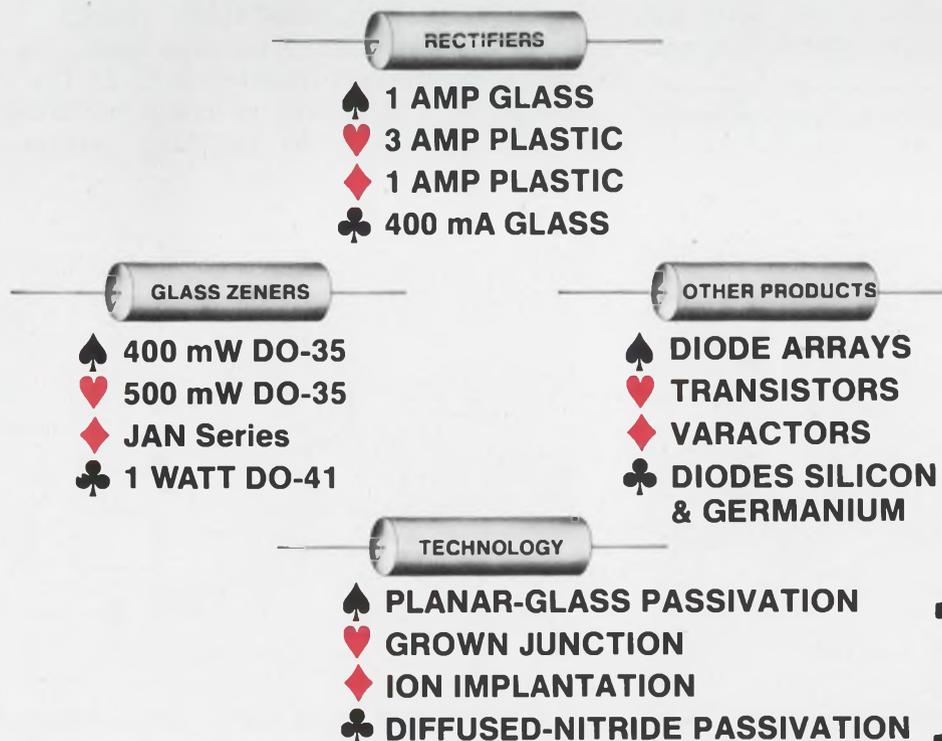
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To achieve high data rates at low cost, use ECL gates instead of discrete component drivers for the LEDs.

Replace discrete-component LED drivers with high-speed ECL gates, and you can transmit data at rates up to 100 MHz through fiber-optic cables. The method makes it feasible to use these cables, instead of wire, for the transmission of digital data, with savings in weight and improvements bandwidth.

The maximum data rate for a LED depends on the drive circuit's ability to supply charging current to the LED's capacitance. With presently available diodes, carrier lifetime  $f = 1/(2\tau_c)$ , theoretically allows operation at more than 200 MHz. But the data rates for practical circuits, so far have been only about 100 MHz maximum.<sup>1</sup>

The capacitance of high-frequency LEDs may vary, typically from 200 to 1000 pF during the switching time. Currents of 100 to 200 mA are required to charge this capacitance at 100 MHz (1000 pF is about 1.6  $\Omega$  reactive at 100 MHz), although the capacitance is shunted by an equally small dynamic resistance ( $r_d$ ).

LEDs can, of course, be modulated directly by step-recovery diodes, Gunn-effect diodes or Trapatt diodes at frequencies of 100 MHz and higher. But a forward-biased LED has a non-

linear low impedance. One way to achieve maximum speed is to drive the LEDs directly from a low-impedance source. However, such a brute-force method is not ideal for solid-state circuits—the efficiency is necessarily low.

If you want to prevent the LED rise time from limiting the system bandwidth, use the following rule of thumb:

$$t_r(\text{LED}) = 0.35 / (2.2 BW_{\text{rcvr}}).$$

Usually the bandwidth restriction should be assigned to the photoreceiver to maximize signal-to-noise ratio and sensitivity.

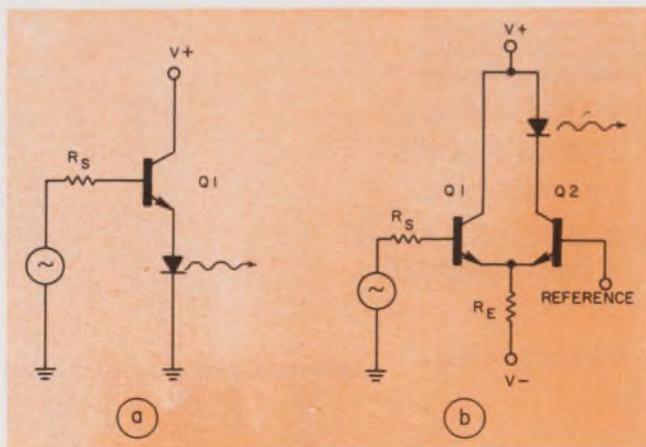
Two LED-driver approaches are possible: constant-current and nonconstant-current operation. Constant-current operation avoids the large  $dI/dt$  currents otherwise encountered in ground planes and bias lines.

## The approaches: You have a choice

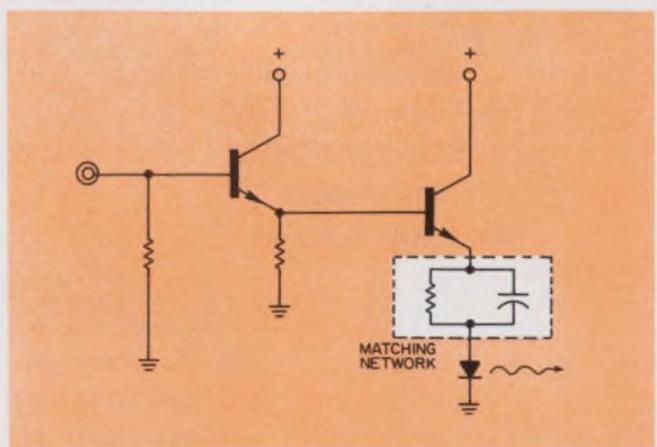
The two best circuits for high-speed LED driving are the emitter-follower and the emitter-coupled video stage. These draw nonconstant and constant currents, respectively (Fig. 1).

In Fig. 1a, if  $R_s > R_1$ , as is usual, the bandwidth can be approximated as  $f_1/\beta$ . The circuit design in Fig. 2 was proposed by White and Burrus<sup>2</sup> to solve the matching problem. The

**Bob Jarrett**, Senior Engineer, Naval Weapons Laboratory, Dahlgren, Va. 22448.



1. Two of the simplest LED-driver configurations include the emitter-follower (a) and the current-switch (b).



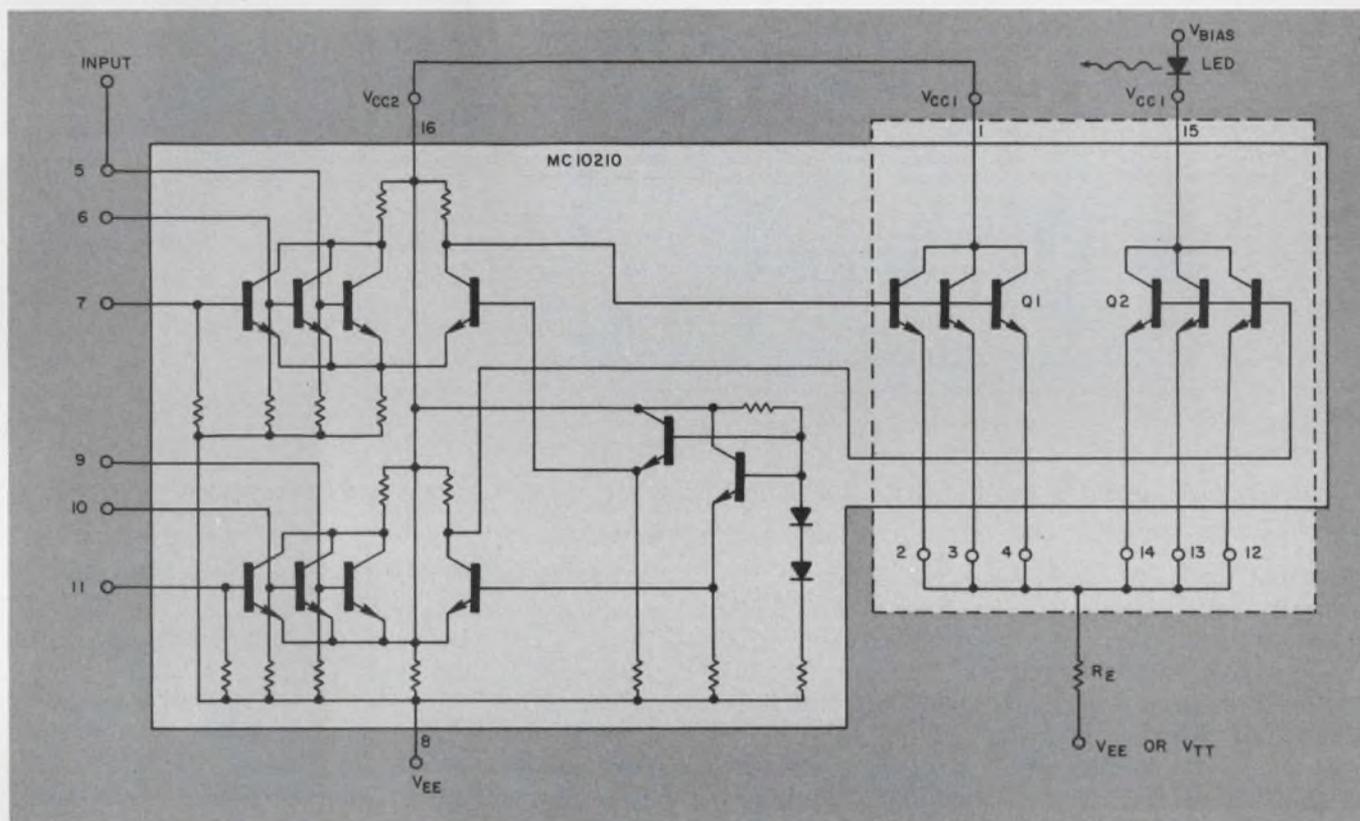
2. The White and Burrus circuit<sup>2</sup> uses an emitter-follower but adds a matching network in series with the LED.

emitter-follower input stage decreases the effective value of source impedance, and the addition of the parallel RC combination ahead of the diode increases the load impedance. The capacitor provides a compensating zero for the additional pole introduced by the series resistance.

It would seem that emitter-coupled logic (ECL) with its emitter-follower outputs would be ideal for the emitter-follower configuration. However, the 0.8-V pk-pk output swing of standard ECL gates is not optimum. But resourceful

supplies current to the output drivers, while  $V_{CC2}$  is connected to the circuit's logic transistors. The 10210 device, designed for clock driving, has three emitter-follower outputs for each of its two OR gates. Each output group of three drivers has its own  $V_{CC1}$  pin. Thus you have free access to the collectors of the output transistors for connection of the LED in a current-switch configuration.

By wire-ORing the output emitters, you can obtain the full current drive capability of the



3. The 10210 OR gate can be connected as a current switch to drive a LED. All you need is a single external

resistor for emitter bias. This configuration also preserves the normal logic function.

design allows use of a standard ECL circuit as a LED driver.

There are several ways to drive a LED at high speed with a \$2 circuit such as the MC10210—dual three-input/three-output OR gate.<sup>3</sup> This gate has a typical propagation delay of 1.5 ns.

The basic video stage of Fig. 1b is well known for its properties as a current switch. When using the discrete version of the video stage (or the circuit of Fig. 1a), you might normally select a relatively expensive device to obtain high speed in the 50-to-200-mA range. Or you would parallel two or more devices to obtain a composite  $Q_2$  stage, in which the current load would be shared.

Fortunately, most ECL circuits have two  $V_{CC}$  leads. These reduce cross-coupling and  $V_{BB}$  spiking when the ICs drive heavy loads. The  $V_{CC1}$  pin

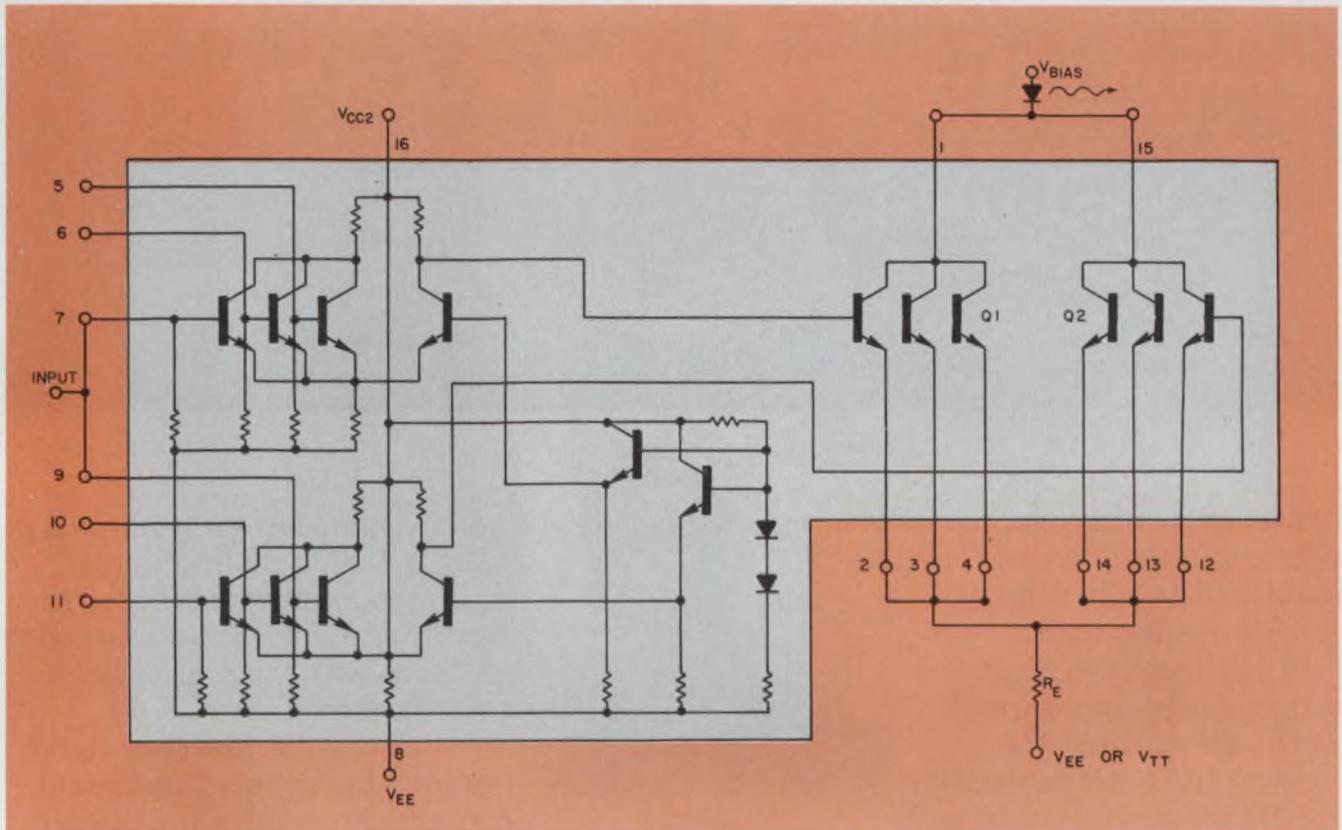
multiple OR-gate output structure.

Fig. 3 shows one LED-driver configuration in which the normal logic function is preserved. This allows the gate inputs on the LED-driving half of the IC to be left open (logic ZERO), while the logic signal can be applied to the other gate. Thus the output transistors function as a composite emitter-follower,  $Q_1$ , which drives a composite common-base amplifier  $Q_2$ .

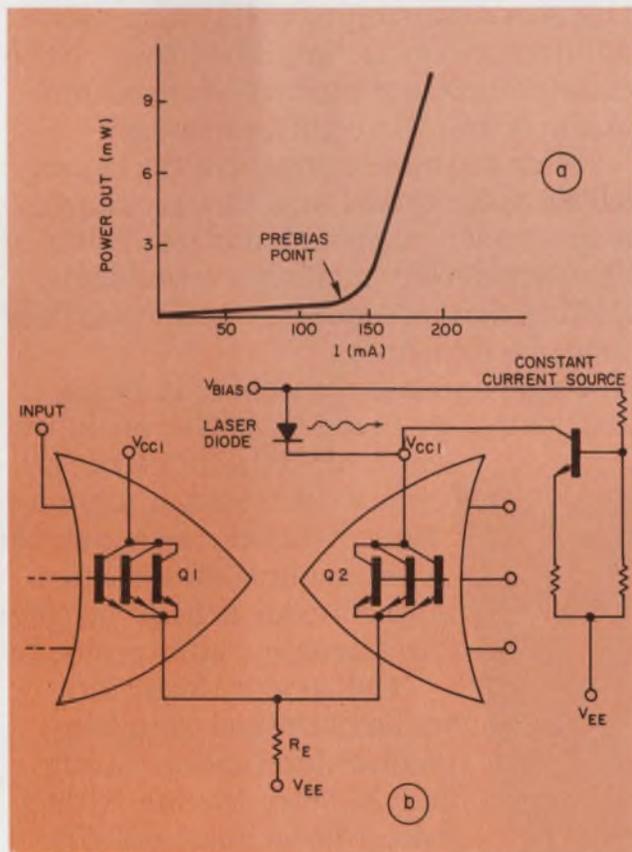
#### The basic drive circuits

The circuit can also be driven differentially by complementary operation of the two gates. The circuit of Fig. 3 would be expected to have slightly better frequency performance than the differential-drive circuit. This stems from the





5. A tandem hookup of the ECL OR gate doubles the drive current you can supply to the LED.



6. The typical power output characteristics of a double-heterostructure injection laser diode (a) makes it necessary to prebias the diode to a point just below the threshold level.

tions can also drive double-heterostructure, Al-GaAs, diode injection lasers. Such laser diodes have a power output that typically has a threshold level, but they can reach bit rates of 1 GHz (Fig. 6a). The diode should be prebiased to just below threshold to avoid the time delay associated with population inversion buildup when the current is switched on.

You can use the circuit of Fig. 3, with the addition of a discrete component current source as shown in Fig. 6b. The current through the laser diode is increased by  $(V_{OL} - V_{EE})/2R_E$  when the input goes low. The idling current is established by the current source but can also be produced by an inductively coupled bleed.

The 10210 is rated at 40 mA maximum for each output driver and should be capable of providing 150 mA total for all six drivers. If even more power is needed the tandem connection or a discrete component emitter-coupled current switch can be used. The recently introduced 10123 type device can supply a full 40 mA per output emitter-follower and might be more useful in some applications. ■■

#### References

1. Taylor, H.F., "Transfer of Information on Naval Vessels Via Fiber Optics Transmission Lines," NELC Technical Report No. 4763, 1971.
2. Burrus, C.A. and White, G. *International Journal of Electronics*, Vol. 35, No. 6, 1973, pp. 751-754.
3. "MECL Integrated Circuits Data Book," Motorola Semiconductor, 1972, pp. 389.

# "We subjected the Augat plug-in socket panel to an accelerated-life test in order to induce contact failure."

## "We failed."

Dave Fillio  
Principal Engineer, Component & Materials Engineering  
Honeywell Information Systems

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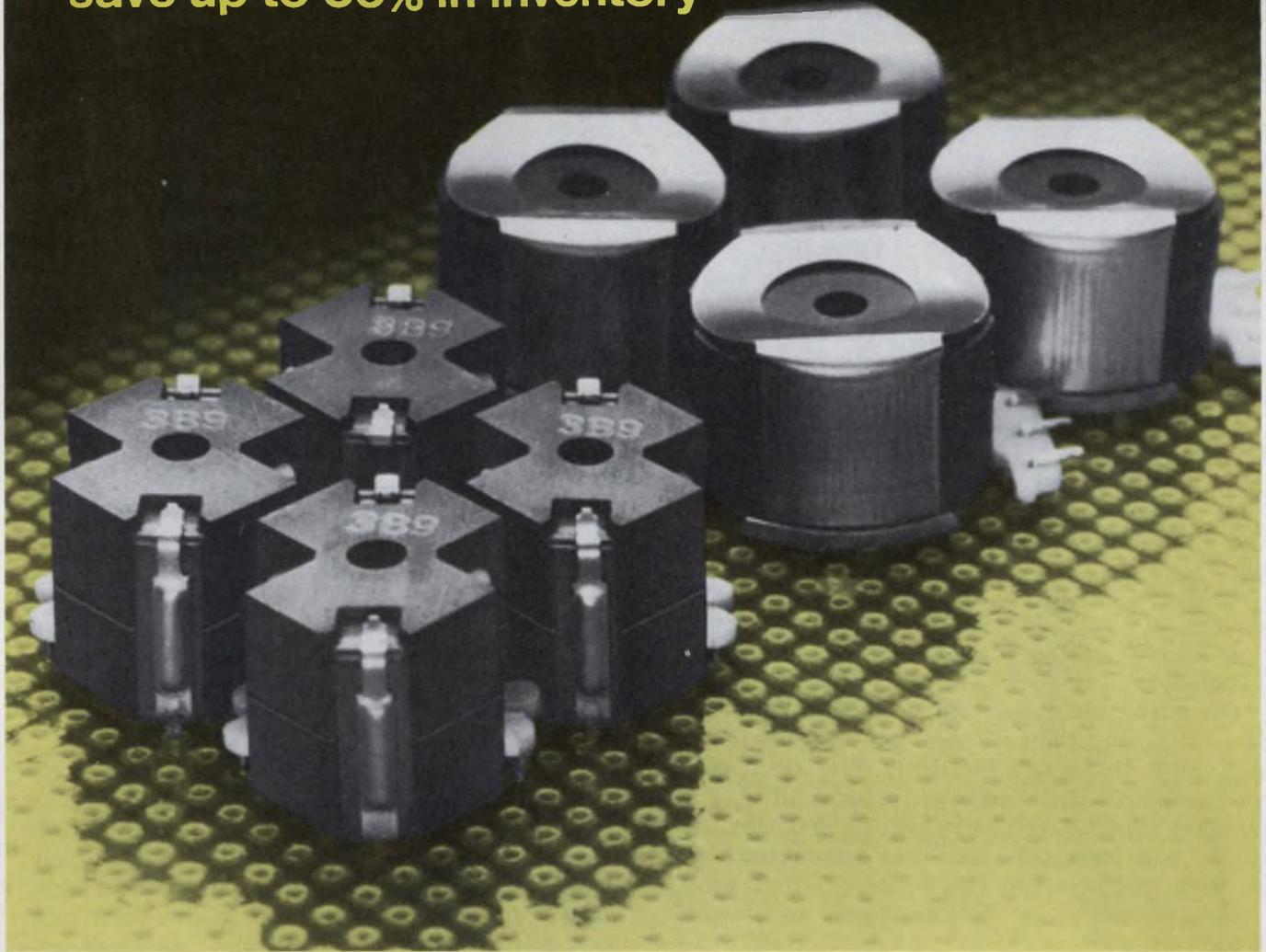
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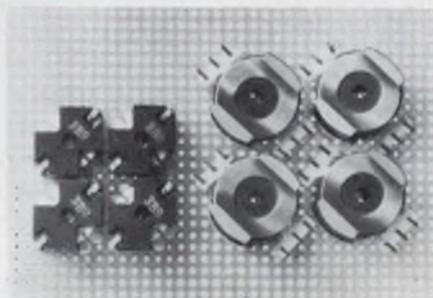
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INFORMATION RETRIEVAL NUMBER 48

## The case for unstructured management: job titles, organizational charts and other managerial trappings may hinder engineering in a new company.

I help to operate a company that, aside from top management, has few job titles, few middle managers, and no organizational charts or personnel department. We're small but growing rapidly. We use just enough management structure to avoid chaos. Why?

Because we don't want to bog down our engineers and programmers with duties that really are subsidiary to their main role in the company—to design products.

Unstructured management does the following for us:

- Gives engineers freedom to work on a variety of jobs.
- Keeps barriers from being built among disciplines.
- Makes it easier to match problems with talent.
- Allows engineering leadership to emerge naturally.

Of course, it's easier to operate a startup company this way than a large one, because in the beginning there are relatively few employees, and design is their primary responsibility. The business aspects, such as marketing, finances, and office administration aren't as important then as they will be when the company's first products come rolling off the line, ready to be marketed.

Clearly it gets more and more difficult to maintain a structureless management as the company gets bigger and bigger. Now we're small—120 people—and last year we earned just under \$2-million dollars. Before we become a \$50-million company, we'll undoubtedly have to install a certain amount of formal organization. But we intend to maintain a low-structure profile as long as we can, because, for one thing, it helps to make the engineer's work fun and interesting.

### Engineers enjoy being unencumbered

When a company grows, the relationships between engineering and the other departments become more exacting. To hold people accountable

---

**Joseph F. Cashen**, Director of Engineering, Prime Computer, Inc., Natick, Mass. 01760.

for such things as documentation, members of management start building a structured organization. They draw up organization charts that tell each man what his job is; the implication is that there are bounds around each job. Some engineers will give themselves bounds when they're given a job title.

In an unstructured atmosphere you can maximize the responsibility you give to people. When we started our computer company, we hired people to work on logic design, circuit design, system design and software problems. But no one did just one thing—we couldn't afford that luxury. Big companies can afford to have specialized groups that worry, for example, only about reliability.

In a small company like ours it's natural and easy, and almost unavoidable, in the beginning for everybody to do a little bit of everything in engineering. This is highly motivational. Our people like to work on a variety of jobs; they feel unencumbered, and they get a lot done.

Not everyone will be happy working in an unstructured company. Those who want to know exactly what they're supposed to do and who they're supposed to report to won't be happy. Those who lose interest in a problem once they've figured it out, who don't want to document what they did to help those who follow, won't fit into an unstructured atmosphere either.

So we looked for certain traits in the people we hired. For instance, we didn't hire a vertical specialist, because we found that he's either not interested in, or capable of, working on a job outside his own discipline. We looked for a mature, capable generalist, who we feel is, by talent and by personality, suited to jumping from one task to another. The best way to weed out the people who won't fit in is to interview them several times, lay your cards on the table and listen very carefully to how they think and how they approach problems.

You also have to be careful what discipline you hire. You may hire a specialist in a field that may not be as important a field tomorrow. Circuit design is one example. Developments in semiconductors and integrated circuits have some-

## Joseph F. Cashen and Prime Computer, Inc.

Before Joe Cashen helped to start Prime Computer in early 1972, he had spent five years with each of three employers. After earning a BSEE from Drexel Institute of Technology, and after completing course work for an MSEE at the University of Pennsylvania, he was hired as a development engineer by RCA. He quickly established himself as a superior engineer when he received the "David Sarnoff Outstanding Award" for his help in designing the RCA 110 computer.

By 1962, Joe moved on to the Digital Systems Div. of The Foxboro Company, first as a senior development engineer, and then as Manager of Hardware Development three years later. In 1967 he went to Honeywell and worked his way up to Chief Engineer of Data Acquisition and Control Systems. He is currently Director of Engineering at Prime where he's responsible for hardware design activities and interfacing with other organizations.

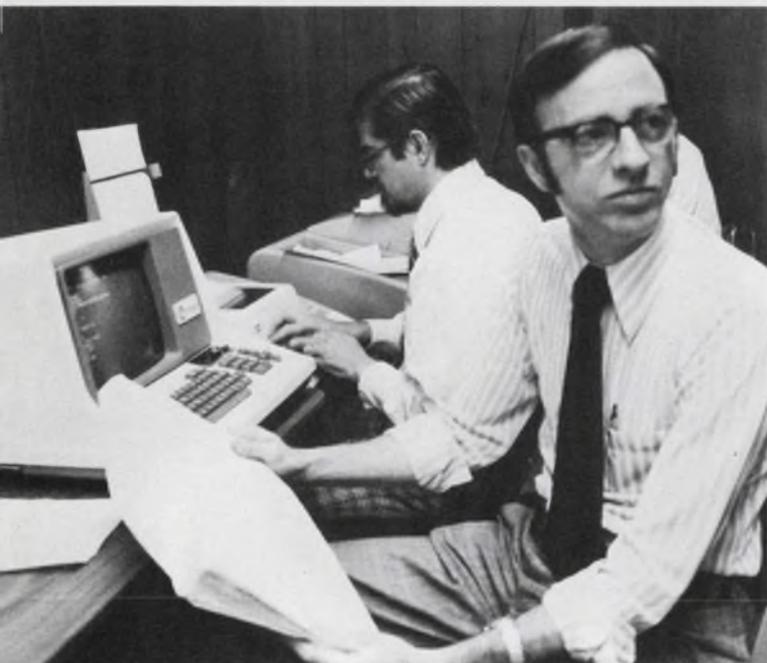
Within the first nine months of its operation, Prime shipped its initial computer—the Model 500. Before the year was out two more computers, the Prime 200 and 300 were announced along with a full range of data communication and data acquisition products, and several new peripheral devices. By following a software-first design philosophy, Prime has been able to offer a completely compatible line of computers, plus a level of software flexibility that's reportedly unduplicated on any competitively priced systems.



what diluted the importance of circuit design as a technology. The people who are capable only in the world of circuit design have quite a problem, because the need for that kind of talent is not nearly as high as it was, say, five to 10 years ago. The ability to change and to shift is an important quality we look for in people.

### **Making molehills out of mountains**

Many engineering companies that have a structured management build barriers within their engineering department and between the engineering department and all other departments or disciplines in the company.



Cashen checks out a computer's interactive terminal.

In computers, people have typically classified themselves as either hardware or software designers. Few are able to work or talk both sides of the fence. This has led to a lot of problems, because in designing any product in computers, you have to make computer hardware/software tradeoffs. If your hardware people don't understand much about software, and vice versa, you can have trouble getting the right tradeoffs.

We think that if the hardware man learns more about software, he's going to be more valuable to the company, and he'll be more valuable as a professional. In an unstructured organization he can learn both sides of the fence. For every piece of hardware we design, there are certain pieces of software that we design with it. We create diagnostic software, and we write drivers for the appropriate operating systems. The man who designs that particular piece of hardware

has a goal to write the driver and the diagnostic software. If he needs some support, we'll give it to him. But if you're working in a structured company and you tell the software manager that you're going to let the hardware guy write a piece of software, he'd get annoyed.

When barriers are built between functional disciplines, people tend to develop procedures for interfunctional dealings. It seems that more important to department managers than cooperating to get the product finished is protecting their departmental interests. When engineering gives something to manufacturing, suddenly there are a score of things that must be done before manufacturing will accept it. That kind of red tape tends to mushroom among all the departments, and it slows product development.

### **Structureless management aids in matchmaking**

Another advantage that an unstructured company can give is the ability to match problems with the people most capable of solving them.

If you work in a structured organization, the man who's responsible for, say, central processor design is going to handle any problems you may have with central processors. But it's conceivable that someone else in the company might be much better suited to work on your particular problem.

Let's say that you want to do a detailed cost analysis of several processors, and you have some technical ideas that you want evaluated from cost and marketing viewpoints. There may be someone else in the company who isn't as technically competent as the processor manager, but because of his interest and knowledge of business, he's much better suited to handle your problems.

In an unstructured company you can make that kind of assignment—match the talents of the people to the particular jobs—and not make people feel slighted. If you alter the flow of responsibilities in a structured management, you imply that someone isn't capable of doing his job. You can lose a lot of flexibility when you're forced to do things strictly via organizational charts.

### **Leaders aren't born—they emerge**

When a company starts in business, certain people are assigned to certain jobs. What happens is that those with leadership ability eventually emerge. We'll put two or three guys together on the same problem and watch one of them take over. Often it's the strongest personality that emerges, instead of the one with more experience. What'll happen is they'll hit a snag, and the leader will assert himself and say, "I think we ought to do this."

That's a much better way to get leaders than putting titles on business cards, because when a man becomes a leader naturally, he's recognized by his co-workers. When he gets a reputation within the company for being able to handle a certain kind of problem, the people naturally go to him when they need help. If we had told this man that he was a manager, he might have automatically set up the bounds of his job, which would limit his effectiveness.

Our people don't want to feel that they're going to worry about only one kind of problem. They recognize that vertical specialization has a lot of shortcomings, and if they are only good in one particular area, they've limited their value. By letting leadership emerge, we control some of the problems of engineering obsolescence.

### Troubles along the way

I certainly don't mean to imply that there are no problems in operating a company with an unstructured management.

Communication, for example, can be a real problem. In an unstructured environment the word may not get to everybody. Once you're structured, the top manager will hold a staff meeting and tell everyone what's happening. Achieving the same result in the unstructured environment is sometimes a bit more difficult, mainly because of people's more flexible responsibilities. When a man is working on one class of problems today and another class tomorrow, making sure that he is always aware of what he needs to know can be difficult.

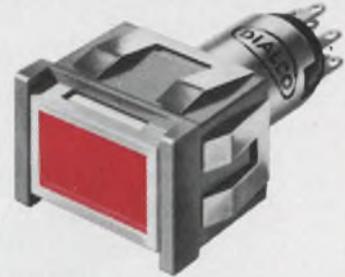
I think it's important for everyone to know a little bit more than they need to know to do their job; that gives them the feeling that somebody up there is concerned about them. It's very important to keep everyone aware of what the company is doing, trying to do, what its problems are and what the solutions are.

Another problem is that people feel a little less comfortable in an unstructured company than a structured one because there's a little less security. They miss not having a niche. Some people don't like not having a fixed boss to report to. If they want to change their vacation time, for example, whom do they ask? The answer for us has been for management to make itself available all the time. If anyone has a problem, he can walk into the office at any time and discuss it.

That's the answer to the challenge—to keep engineers happy and to maintain the atmosphere of a startup even after the company begins to grow. If the engineers and programmers believe that our company climate is pretty much the same at three years as it was at three months, that'll be quite an achievement. ■■

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## Coupling circuit ensures drive current from op amp to emitter-follower booster

A nonconventional coupling circuit overcomes a common problem in obtaining sufficient drive current when boosting the output of an op amp. The easiest way to increase the current is to add a complementary emitter-follower. However, a chief drawback of the conventional diode-biasing scheme, circuit (a), is a lack of base drive at the maximum swings of large signals, just when the output current must be maximum. The circuit (b), with the use of a third diode in a different configuration, ensures adequate base drive. And the output of a 741 can be boosted to 300 mA.

In circuit (a), the base drive for  $Q_1$  and  $Q_2$  is supplied by resistors  $R_1$  and  $R_2$ , respectively. The op amp cannot source any appreciable current to the bases. At either extreme of the output signal swing, the amount of base drive, which is

$$(15 - V_{be} - V_o) / R_1,$$

is minimum, because  $V_o$  is maximum.

But in circuit (b), the op amp drives  $Q_2$  directly for negative outputs. On only small positive swings,  $R_1$  supplies base drive to  $Q_1$ . Above the offset voltage for  $D_3$ , the op-amp output is high enough to begin to source current through  $D_3$ . Diode  $D_3$ , a germanium diode chosen for its small forward drop, allows the op amp to source its maximum output of 5 or 10 mA for  $Q_1$ . Diodes  $D_1$  and  $D_2$  are silicon, so they can provide the

necessary offset to eliminate almost all the crossover distortion.

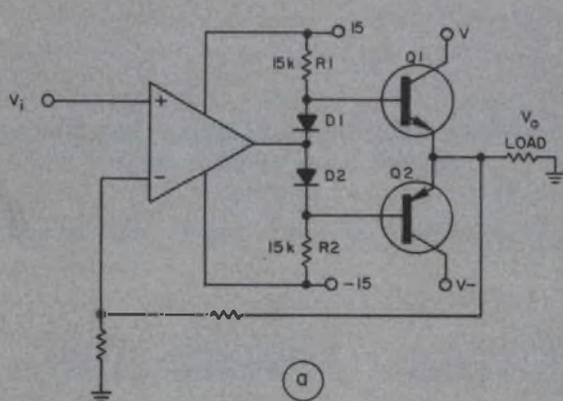
The price for improved performance is a second crossover point at the level at which  $D_3$  begins to supply  $Q_1$  base drive. At frequencies of less than 1 kHz (for a 741), this crossover distortion is unnoticeable, especially with small closed-loop gains. But at higher frequencies, the corrective response of the op amp begins to lag. Capacitor  $C_1$  (about  $0.1 \mu\text{F}$ ) helps diminish crossover distortion at higher frequencies. The 709 op amp might be a better choice when frequencies to 30 kHz are needed.

The small  $Q_1$ - $Q_2$  crossover distortion may be completely eliminated by insertion of a few hundred ohms in series with  $D_1$  and  $D_2$ . If made adjustable, this resistance can be increased from zero until the  $Q_1$ - $Q_2$  crossover distortion disappears from the waveform.

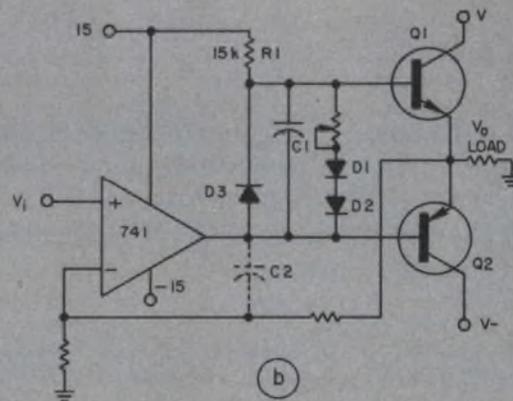
For stability, it is customary to place  $D_1$  in thermal contact with  $Q_1$  and  $D_2$  with  $Q_2$ .

This circuit can be handy if a high speed circuit is not required. The addition of  $C_2$  can slow the response without compensation problems. Other power drivers are not so easily "de-slewed."

*Neil Dvorak, Chief Electronics Engineer, Technical Equipment Corp., 917 Acoma St., Denver, Colo. 80204.* CIRCLE NO. 317



Conventional coupling circuit (a) fails to provide adequate drive current into the bases of  $Q_1$  and  $Q_2$ .



The circuit in (b), with one added diode, provides adequate current drive.

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5	.500	.1	.05	1	49.00	5E50A	3.5 x 2.5 x 1.00
5	1.0	.2	.05	1	69.00	5E100	3.5 x 2.5 x 1.25
5	1.5	.3	.1	1	98.00	5E150	3.5 x 2.5 x 1.25
5	2.0	.15	.05	1	110.00	5E200	3.5 x 2.5 x 2.00
5	2.5	.15	.05	1	125.00	5E250	3.5 x 2.5 x 2.00

... and the model you choose will be shipped 3 days after Acopian receives your order. With a 105-125 VAC input, use it at full rated load to 71° C. Short circuits won't damage it. These mini-modules can be mounted on a printed circuit

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INFORMATION RETRIEVAL NUMBER 51

# Single part minimizes differences in monostable and astable periods of 555

A single inexpensive component—a diode or a resistor—can minimize the difference between monostable (one-shot) and astable (free-running oscillator) periods of a 555 timer. When the 555 timer is used as an oscillator, the timing capacitor normally charges from  $1/3 V_{cc}$  to  $2/3 V_{cc}$  to provide an output period of  $0.69 RC$ . However, when used as a one-shot, or when strobed via the reset input, the capacitor must normally charge from zero volts to  $2/3 V_{cc}$ , and a longer period of  $1.1 RC$  is produced.

In the figure, the solid lines show the conventional circuit arrangement for the timer. The switch  $S$  selects either the astable or the monostable configuration. Either a resistor  $R_3$  or diode  $CR$ , shown dotted, may be added to equalize the timing periods.

A 1N662 diode, placed between pins 3 and 5, pulls down the pin-5 reference voltage to about  $0.9 V$  each time the output goes LOW. Thus the timing capacitor  $C$  must now drop to approximately  $0.45 V$  before the level at pin 2 can trigger another output pulse. The capacitor therefore starts to charge from near ground level in both the astable and monostable modes, and the periods agree within 5%.

The advantage of the diode method is that no computations or high-accuracy components are required to provide close matching of pulse widths. Also single potentiometer control of pulse widths is still possible. However, the lower threshold, and therefore the pulse width, depends on the diode's offset and drift characteristics.

In a second method, resistor  $R_3$  forces the monostable period to approach that of the astable when it prevents the timing capacitor from discharging completely. Careful adjustment of the voltage divider formed by  $R_1$  and  $R_3$  permits the timing-capacitor voltage to drop only far enough to trigger a new pulse. The timing capacitor starts to charge from about  $2/3$  of the supply voltage in both the monostable and astable modes.

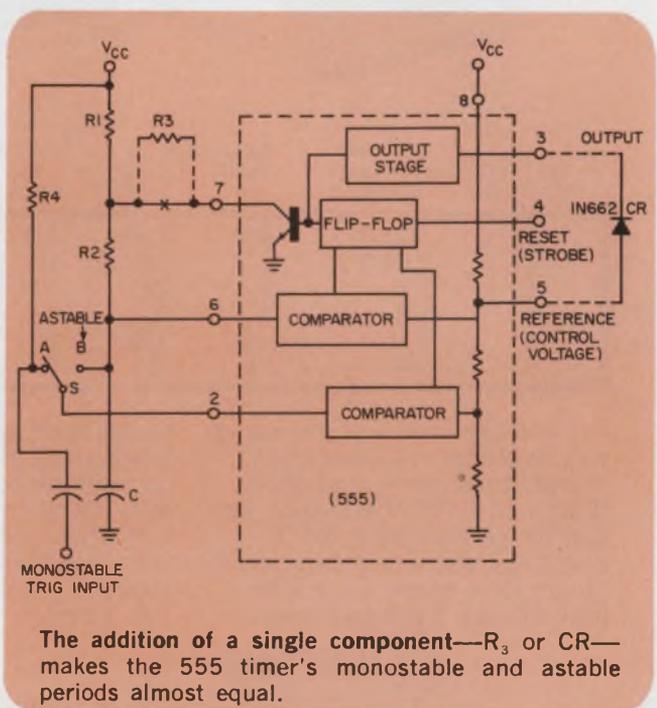
The advantage of the resistor method is that the periods of the two modes are governed by the adjustment of  $R_1$  and  $R_3$ . Thus the periods can

set very close to each other, and a bypass capacitor to ground can be placed on pin 5—as is done normally. Also the resistor method does not introduce the temperature drift of a diode, and the match of pulse widths tends to remain constant with supply-voltage variations.

One disadvantage is that the value of  $R_1$  cannot be varied to control pulse period without adjustments to  $R_3$  also. In addition, careful consideration of the tolerances of both internal and external voltage-divider resistances is required to attain close pulse-period matching. A cursory analysis shows that 5% resistors of  $4.7\text{-k}\Omega$  and  $1.5\text{-k}\Omega$  for  $R_1$  and  $R_3$  yield pulse periods matched to about 20%.

One-percent resistors would allow considerably closer matching. The resistor method is best when high stability is required, or when it is desirable to bypass or to modulate pin 5, and when it is not necessary to have a continuously adjustable pulse width.

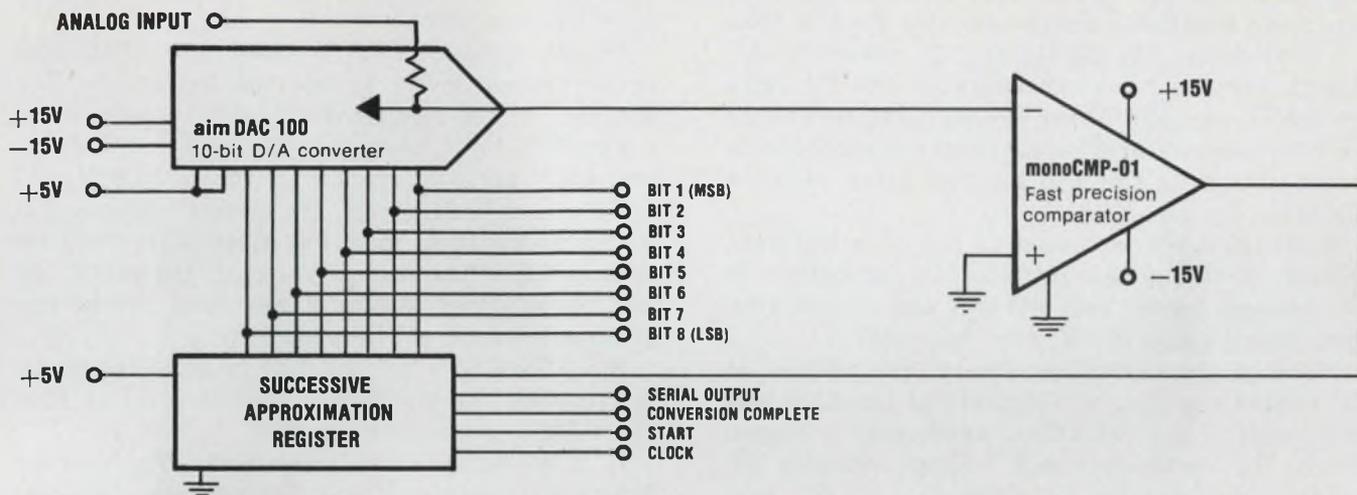
Arthur R. Klinger, 3245 Stuff Dr., Orlando, Fla. 32809. CIRCLE NO. 318



The addition of a single component— $R_3$  or  $CR$ —makes the 555 timer's monostable and astable periods almost equal.

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INFORMATION RETRIEVAL NUMBER 52

# Voltage probe uses five LEDs to indicate highest level reached

A versatile logic probe can be built with an inexpensive transistor array—such as the CA 3083—a transistor, five LEDs and 11 resistors. Although the five npn transistors on the CA 3083 are usually used in linear or switching transistor applications, the array's common p-material substrate allows its use also for four-layer pnpn or thyristor devices.

Each thyristor is biased to fire at a different voltage, so the probe provides an indication of five voltage levels. The voltages are adjusted by the resistor ratios  $R_a/R_b$  (see diagram).

None of the thyristors fires if the voltage at the common anode, or substrate at pin 5, is less than each of the individual anode-gate voltages. When the common anode voltage exceeds an anode-gate potential by about 0.7 V, the corresponding thyristor fires. The connected LED

lights and stays on until the probe tip is removed from the test point.

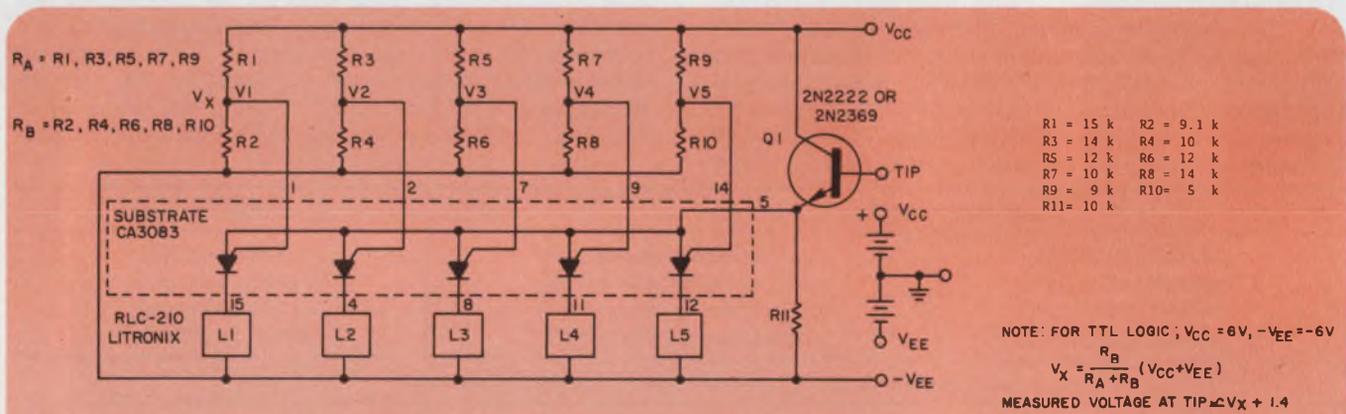
Supply voltage  $-V_{ee}$  is chosen to allow low probe voltage levels to fire the thyristors. The accuracy of the measured voltages is  $\pm 0.1$  V.

For TTL logic, voltage levels of 0, 0.4, 1.4, 2.4 and 4.9 V are good choices, with  $V_{cc} = 6$  V and  $-V_{ee} = -6$  V. However, the circuit voltages can be set about 15 V max for other logic families or linear ICs. The voltage range of the probe can also be increased to almost any level by the use of an attenuator at the probe tip.

Since the LEDs fire and stay on until the probe is removed, the maximum voltage level is provided for a given measurement.

*H. S. Kothari, Central Electronics Engineering Research Institute, Pilani (Rajasthan) 333 031, India.*

CIRCLE NO. 319



A LED lights when the voltage applied to the probe's tip passes a preset voltage level. All activated LEDs stay lighted, and the highest-valued

one indicates the maximum voltage. The LEDs extinguish when the probe is removed from the voltage source.

### IFD Winner of March 15, 1974

**Richard P. Rufer, Electronic Engineer, University of California, Lawrence Livermore Laboratory, Livermore, Calif. 94550.** His idea "Circuit Built with Quad Op Amp Measures Temperature Digitally" has been voted the Most Valuable of Issue Award.

**Vote for the Best Idea in this issue** by circling the number for your selection on the Information Retrieval Card at the back of this issue.

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# TECHNITROL Takes The Tough PT'S.

When it comes to pulse transformers (PT'S), Technitrol's experience leads the field. Technitrol was first with DIP transformer packaging and the H case. But, Technitrol is first where it really counts: getting the job—no matter how tough—done right. Here are two examples:

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## 2/Tough Packaging

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**8 resistors**

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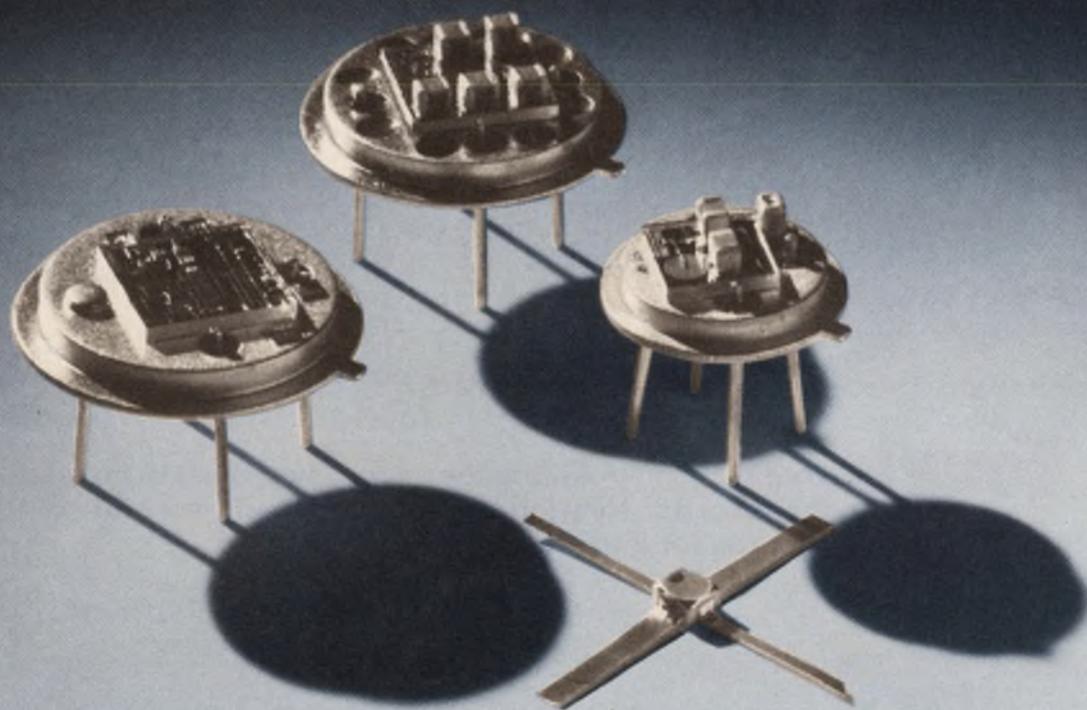
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INFORMATION RETRIEVAL NUMBER 53

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**Mini Magic Marriage.** Combine the fantastic low-noise capability of Avantek transistors with thin film technology—and you've got a real mini magic marriage. Avantek miniature microwave amplifiers and oscillators offer the designer a new level of versatility, with **NO** compromises in performance.

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the manufacturing processes and screening procedures for standard and "R" version UTO's. Data sheets also available for the asking. **INFORMATION RETRIEVAL NUMBER 55**

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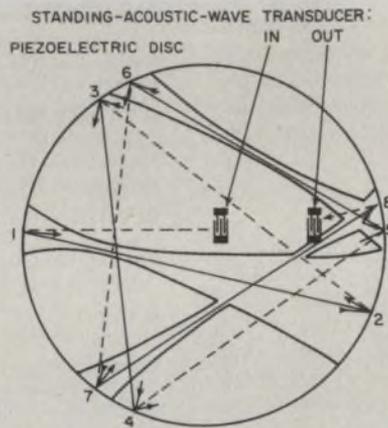
## Acoustic beam achieves millisecond delays

A surface-acoustic wave delay-line design with delays of the order of milliseconds has been developed at University College in London.

The delays are achieved when the acoustic beam is folded back and forth along the chords of a circular piezoelectric disc. At the disc periphery, the beam trajectory passes over the rounded edge, proceeds along a chord on the other side of the disc and emerges back over the edge onto another chord on the first face.

An infinite number of beam trajectories is possible. And when the beam is folded into a tightly woven pattern, full use is made of the available surface area.

Beam intersections do not lead to significant distortion unless they are particularly numerous, according to the researchers. In one design, a 22-mm-diameter disc of Y-cut quartz has two transducers on the upper face tuned to 41 MHz and isolated from each other by thin absorbing strips painted across the short direct



path. The acoustic beam takes a long path that involves several transits over the slightly rounded edges of the disc. The largest spurious response is 27 dB below the output at 96  $\mu$ s delay.

The experiment demonstrates that longer delay lines can be folded onto discs, with millisecond delays that call for a disc diameter of 50 mm. The illustration shows a delay line with eight beam trajectories.

## Microwave circulators replaced by TF versions

The familiar microwave circulator will be replaced by thin-film counterparts in the next few years, according to researchers at the Technical University of Gdansk in Poland.

The scientists forecast thin-film, lumped-element circulators that have broad bandwidth and allow easy adjustment of their operating frequencies because

they vary the level of the internal magnetic field of the thin films.

A bidirectional thin-film circulator—one that has two center frequencies—can be constructed by use of thin-film techniques, the researchers say. One of the two critical microwave-circulator parameters—common capacitance—would be in the same order of magnitude as the parasitic capac-

itance resulting from the thin-film fabrication method.

The other critical parameter—microstrip inductance—calls for a thin-film disc diameter of 1 mm. This appears to be realizable, the researchers point out, because thin-film junctions have already been deposited on discs as small as 2 mm.

## Waveguide to carry 500,000 calls at once

A 45-km waveguide between Darmstadt and Heidelberg is being installed and tested by West German postal authorities. Millimeter waves in this waveguide will carry up to 500,000 telephone channels simultaneously.

After gaining practical experience with this line, telecommunications planners expect to extend it to Frankfurt.

## Bandpass filters use acoustic elements

Prototypes of a new generation of bandpass filters built with acoustic-wave technology are mass-producible and stable, according to Mullard Research Laboratories in England. The acoustic elements are also suitable for integration into hybrid circuitry.

The researchers say that although the filters are but 1/500th the volume of conventional counterparts, the tiny devices give a comparable performance.

A filter that Mullard proposes for TV receiver circuits consists of a piezoelectric substrate—0.5-mm thick  $\times$  0.5-cm wide and 1-cm long—overlaid with two interdigital electrode patterns, one at each end. An electrical input signal applied to one pattern generates an acoustic wave that travels to the other end, where it is converted at the second set of electrodes back into an electrical output. The bandpass characteristics are produced by the acoustic interactions with the electrode patterns.

Mullard is using a computer to design photomasks that will produce bandpass filters with center frequencies ranging between 10 MHz and 1 GHz, and with passbands between 100 kHz and 300 MHz.

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INFORMATION RETRIEVAL NUMBER 58

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INFORMATION RETRIEVAL NUMBER 59

ELECTRONIC DESIGN 15, July 19, 1974

# Solder Clads for Electronics

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## Advantages:

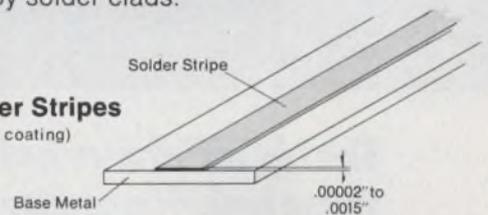
1. Reduced labor cost.
2. Increased flexibility in design.
3. Elimination of multiple handling and inspection of stamped parts.
4. Improved and consistent quality of the end-product.
5. Permanent solderability, providing increased shelf life.

## Applications:

Among the major users of solder clads are the semiconductor and electronic industries. More recently, manufacturers of communication equipment, connectors for data processing equipment, jewelry, automotive, and computer parts have recognized the advantages offered by solder clads.

## Availability:

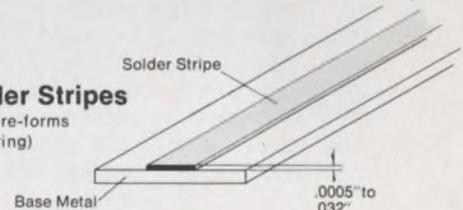
### Thin Solder Stripes (for protective coating)



- To insure a solderable surface when subsequently soldering or brazing.
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INFORMATION RETRIEVAL NUMBER 60

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The little differences are on the front panel (a start/stop mode of operation and a tape drive readout). Some people think they add up to \$320. For them, we built the 2001.

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In addition, its frequency, bandwidth, and output level are programmable, making it ideal for production test and systems use as well as in the design laboratory. If you're still not sure which sweeper we built for you, send for more information. Just circle the reader service number or give us a call.

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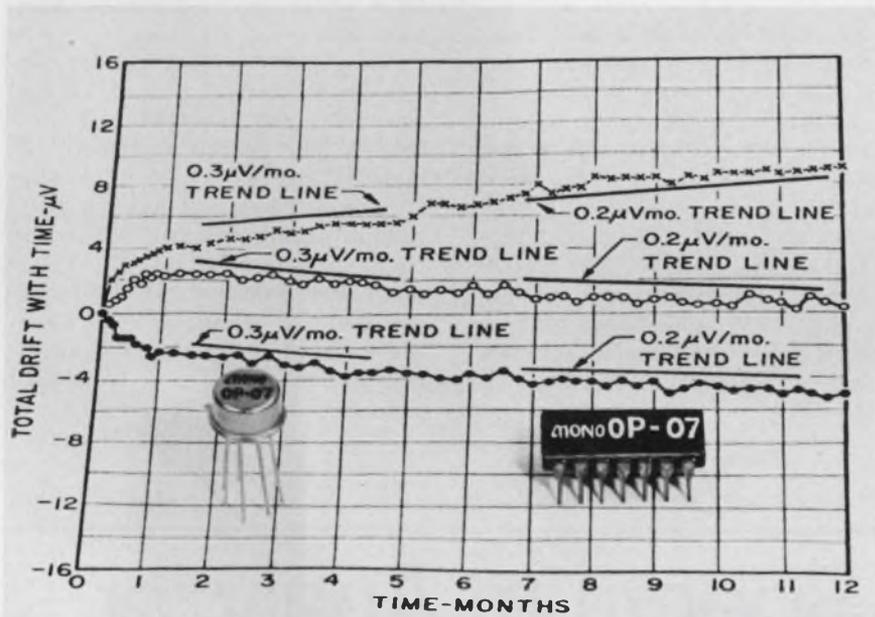
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Model 2000  
 \$1375



Model 2001  
 \$1695

## Bipolar op amp matches specs of chopper-stabilized units



Precision Monolithics, 1500 Space Park Dr., Santa Clara, Calif. 95050. (408) 246-9225. P&A: See text.

If you need a low-drift amplifier, your first inclination may be to use a chopper stabilized unit. A better buy, however, may be the monoOP-07, a monolithic bipolar op amp made by Precision Monolithics. It has an offset drift vs temperature of only  $0.2 \mu\text{V}/^\circ\text{C}$ , and costs less than a third that of equivalent chopper-stabilized units.

The OP-07 has input offset voltages of  $10 \mu\text{V}$  or less, and long-term offset drift averages  $0.2 \mu\text{V}$  a month. The op amp doesn't require the large compensating or holding capacitors, resistors or potentiometers usually found in monolithic chopper-stabilized devices or modular units.

Microvolt offsets are of dubious value if noise obscures the input signal, but the OP-07 has the advantage of a low  $0.6\text{-}\mu\text{V}$  pk-pk maximum input noise—less than one-hundredth that of monolithic chop-

pers made by two other companies (Model 2905 from Harris Semiconductor, P.O. Box 883, Melbourne, Fla. 32901, and Model SN72088 from Texas Instruments, P.O. Box 5012, M/S 308, Dallas, Tex. 75222). Also, the OP-07 input bias current remains below  $2 \text{ nA}$  over the entire operating temperature range (MIL:  $-55$  to  $+125^\circ\text{C}$ ; Commercial  $0$  to  $70^\circ\text{C}$ ). Since its output is free from chopper spikes, the amplifier can be used in high-impedance circuits.

The amplifier's bipolar front end provides a full differential input that can handle common-mode voltages of  $\pm 14 \text{ V}$ . The amplifier also has a common-mode rejection ratio of  $126 \text{ dB}$  at low frequencies. At unity gain, the amplifier has a bandwidth of  $1.2 \text{ MHz}$ .

Open-loop gain of the OP-07 is typically  $500,000$  and is guaranteed at  $300,000$  minimum for the MIL version. Input impedance in the differential mode is a high  $80 \text{ M}\Omega$ , while the common-mode input  $Z$  is

$200 \text{ G}\Omega$ . The output impedance, a low  $60 \Omega$ , can drive many load variations. Although normally requiring  $\pm 15 \text{ V}$  supplies, the OP-07 can operate with supply voltages as low as  $\pm 3 \text{ V}$ —a feat chopper-types are hard-pressed to match.

The amplifier's microvolt offset voltages are achieved when each input device is trimmed during wafer testing. A string of trimming resistors is diffused in series with the input stage's collector resistor. Each trim resistor also has a reverse-biased zener placed in parallel across it.

In normal operation the zener doesn't conduct, since the voltage across it is less than its breakdown rating. Automatic equipment that measures the amplifier offset determines the needed resistance change. A large current pulse is then routed via probes through one or more selected zeners, causing permanent short circuits and reducing the over-all value of the resistor string.

The monoOP-07 can directly replace the 725, 108 and monoOP-05 amplifiers without circuit changes. It can also replace 741 op amps, if the 741's nulling potentiometer is removed.

Four versions of the OP-07 are available: AJ, J, EJ and CJ, with max  $V_{\text{OS}}$  of  $25, 75, 75$  and  $125 \mu\text{V}$ , respectively. The AJ and J models are specified over the MIL temp range, while the EJ and CJ are specified for the commercial. Prices in 100-piece lots are  $\$60, \$25, \$15$  and  $\$9.95$ , respectively.

The amplifiers are housed in TO-99 or DIP cases and are available from stock.

Precision Monolithics **CIRCLE NO. 252**  
Harris Semiconductor

Texas Instruments **CIRCLE NO. 254**

**CIRCLE NO. 253**

**CIRCLE NO. 254**

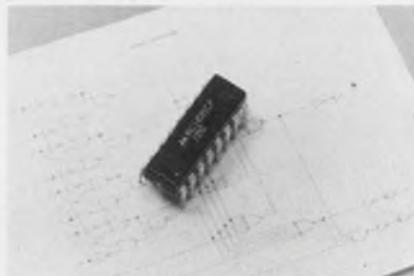
### FM audio system handles 2 W

ITT Semiconductors, 3301 Electronics Way, West Palm Beach, Fla. 33407. (305) 842-2411. \$2.20 (100-999).

A complete 2-W FM sound system in a single 14-pin DIP can be used to minimize the number of components needed in receiver applications. Called the ITT3701, the new circuit includes an i-f limiter, a quadrature type FM detector, a dc-operated volume control—which doesn't require the usual shielded cable—and an internally compensated 2-W audio amplifier. Full limiting occurs with less than 100  $\mu$ V input, and the circuit contains output short-circuit protection. The device can be operated at 4.5 and 10.7 MHz. Other intermediate frequencies are obtained with the connection of proper external components.

CIRCLE NO. 260

### 4-bit CMOS IC compares magnitudes

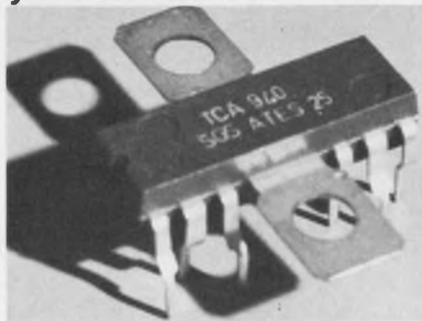


Motorola Semiconductor Products, Inc., Box 20924, Phoenix, Ariz. 85036. (602) 244-3466. \$3.90 up (100-999); stock.

The MC14585 CMOS 4-bit magnitude comparator takes two 4-bit words and determines whether one is less than, equal to or greater than the other. The IC can be cascaded to handle longer word lengths. It can be used with both binary and BCD codes and it provides a fanout of 50. The CMOS IC has a quiescent power dissipation of 25 nW, and it features pin-compatibility (but not direct electrical equivalence) with the TTL 7485 IC.

CIRCLE NO. 261

### Protected audio amp yields 7 W



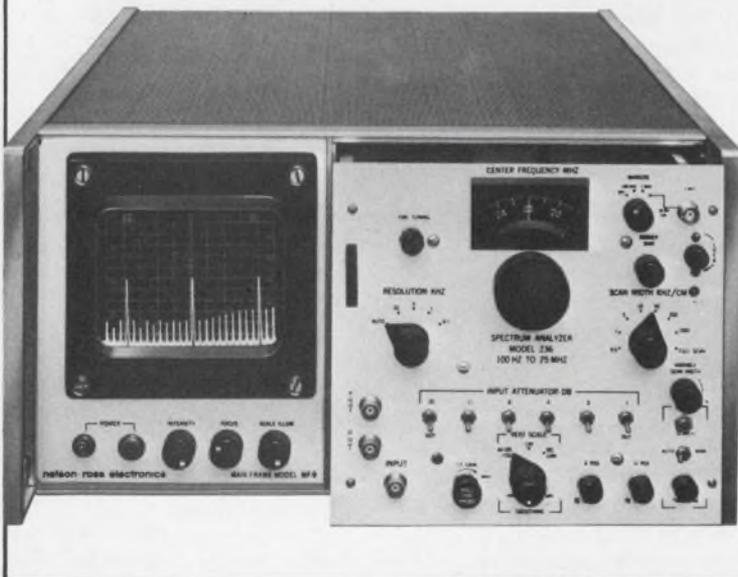
SGS-ATES Semiconductor Corp., 435 Newtonville Ave., Newtonville, Mass. 02160. (617) 969-1610. \$3.50 (100 up).

The TCA940 audio amplifier contains both thermal shut-down and power-limiting, short-circuit protection. The new IC outputs 7 W at 1% distortion (with 18 V supply and 4  $\Omega$  load). It has a supply-voltage range of 6 to 24 V and a ripple rejection of 45 dB. Other features include an open-loop voltage gain of 75 dB, a 3-dB bandwidth of 40 to 20-kHz and an efficiency of 65% at 5-W output power.

CIRCLE NO. 262

# Workhorse Spectrum Analyzer... **100Hz to 25MHz**

The new Nelson Ross Model 236 is a multi-purpose, easy to use, workhorse Spectrum Analyzer with outstanding performance features and an exceptionally low price of \$3275.



- Preset 0-25MHz quick-look scan and 0-10MHz adjustable scan widths
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## Voltage amp aims for telephone use

*Plessey Semiconductors, 1674 McGaw Ave., Santa Ana, Calif 92705. (714) 540-9979. \$5.07 (100-999); stock.*

The SL 1020, a class A or AB voltage amplifier, contains a remote dc gain-control capability. The new bipolar IC is primarily intended for use as a channel amplifier in telephone equipment. The SL 1020 features temperature-insensitive dc-gain control, noninteractive adjustment of gain and a 1:1 600- $\Omega$  transformer output that can be optimized for low inductance.

CIRCLE NO. 263

## 256-bit S-TTL RAMs switch to epoxy

*Signetics, 811 E. Arques Ave., Sunnyvale, Calif. 94086. (408) 739-7700. P&A: See below.*

Two high-speed Schottky-TTL RAMs, formerly offered in silicone packages, are now being manufactured in epoxy packages at a unit price of \$14 (100), or one-half the cost of the earlier versions. The two RAMs are 256-bit bipolar circuits with access times of less than 30 ns. The Model 82S16 has three-state outputs, and the 82S17 has open-collector outputs. Read time is also 30 ns, and write time is 20 ns. Power dissipation is 1.5 mW per bit.

INQUIRE DIRECT

## Calculator IC consumes 10 mW

*Cal-Tex Semiconductor, Inc., 3090 Alfred St., Santa Clara, Calif. 95050. (408) 247-7660. \$15; stock (up to 1000).*

The CT5031 calculator circuit represents the company's first in an expected series of ion-implanted calculator ICs that require less than 10 mW for operation. The CT5031 features the basic four functions (with powers and reciprocals), floating point and six or eight digits. The circuit comes in a 28-lead DIP, and it requires only digit drivers, LEDs, and segment resistors to complete the electronic component list for a calculator.

CIRCLE NO. 264

# GET ON BOARD... with TANTALEX<sup>®</sup> Low-Cost Solid Tantalum Capacitors

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*Call your nearest Sprague district office or sales representative, or write for the bulletins mentioned above to Sprague Electric Company, 347 Marshall Street, North Adams, Mass. 01247.*

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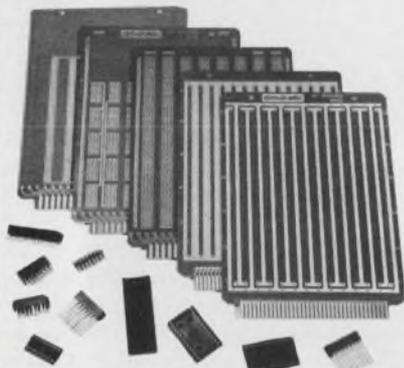
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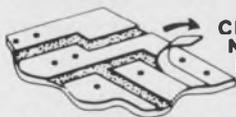
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INTEGRATED CIRCUITS

## Static 1-k RAM accesses in 80 ns and has chip select



*EMM SEMI, a division of Electronic Memories and Magnetics, 3883 N. 28th Ave., Phoenix, Ariz. 85017. (602) 263-0202. \$15 (100 to 999); September.*

The first fully static 1024-word  $\times$  1-bit n-channel MOS random-access memory (RAM) to come in under 100 ns is the 1218 from EMM SEMI. The memory accesses in 80 ns. Its cycle time, 180 ns, is the same as that of its closest competitor. The chip includes a select port for easy memory-system design.

The competing unit—the 7001 from Advanced Memory Systems (1276 Hammerwood Ave., Sunnyvale, Calif.)—has a 60-ns access and a 180-ns cycle time. But the 7001 costs \$20 (100 to 999), \$5 more than the 1218. Additionally, the 7001 is not fully static; it requires external charge-pump circuitry. And conventional refresh is not used.

Both the 1218 and 7001 have automatic "power-down" when chip select is disabled. The popular 2102 RAM available from Intel (3065 Bowers Ave., Santa Clara, Calif. 95051) and several other companies does not have this power-down capability and it is slower. It does, however, have TTL-compatible inputs and outputs and sense amplifiers on the chip. Neither the 1218 nor the 7001 has sense amps on the chip.

On the 1218 two complementary data-out signals are provided, and they may be used to drive a differential sense amp. The minimum data-out valid time is 20 ns; the typical, 25 ns.

When you consider standby power, AMS's 7001 consumes less, 60  $\mu$ W/bit vs 130  $\mu$ W/bit for EMM SEMI's 1218. In the operating mode it's the reverse; the 1218 consumes 543 mW vs 655 mW for the 7001.

The units operate over 0 to 70 C and come in ceramic 22-pin DIPs. And both are fully decoded on the chip.

The 1218 requires supply voltages of +15, +5 and -4.4 V. These are TTL voltages, except for the +15 V necessary for chip select.

Input capacitance is 6 pF and output capacitance is 5 pF. Chip select input capacitance is 80 pF.

EMM SEMI also sells two other chips that are pin-compatible with the 1218: the 1216 and 1217. Both have TTL-compatible inputs and outputs with sense amps on the chip. The 1216 accesses in 260 ns and sells for \$11 (100 to 999), the 1217 in 145 ns for \$13 (100 to 999).

For EMM SEMI      **CIRCLE NO. 255**

For Advanced

Memory Systems      **CIRCLE NO. 256**

For Intel

**CIRCLE NO. 257**

POWER SOURCES

**Portable unit delivers sine waves to 120 VA**



Nova Electric Manufacturing Co., 263 Hillside Ave., Nutley, N.J. 07110. (201) 661-3434. From \$498; 45 days.

Porta-Power makes portable ac power available in ranges of 30, 60 and 120 VA. Weighing from 18 to 40 lb., and using nonspillable gelled electrolyte batteries, Porta-Power units can provide 60 Hz, 115 V ac power in excess of one hour. The accessory battery charger will recharge a fully rundown battery in 8 h. Output sine wave has a maximum distortion of 6% with voltage regulation of  $\pm 1\%$ . The units are short-circuit proof and current limited.

CIRCLE NO. 265

**Switching supplies claim zero response time**

Advanced Power, 1621 S. Sinclair St., Anaheim, Calif. 92806. (714) 997-0034. 50A: \$395; 100A: \$495; 30 to 60 days.

CDS Series of 5-V-dc switching regulator power supplies claims zero response time for a line step change of 10%, or a load step change of 25% at 75% of full load. Overshoot and undershoot performance is typically 1% for a line step change of 10%, with 2% maximum for a load step change of 25%. Regulation is 0.1% for a 10% line change, and  $\pm 0.1\%$  from 10% to full load.

CIRCLE NO. 266

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262K Words Fixed Head Storage	RF 11-AA \$15,120	Model 3091 \$6,750
1.2M Words Cartridge Disk Drive	RK 11-DE \$11,000	Model 4091 \$8,250
20M Words Pack Disk Drive	RP 11-CE \$31,880	Model 4091 \$26,550

\*OEM Price List November, 1973

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INFORMATION RETRIEVAL NUMBER 66

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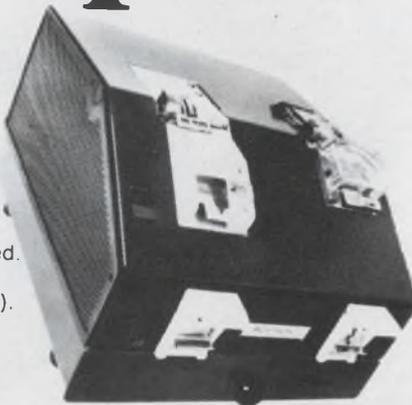
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**LITTON ABS**

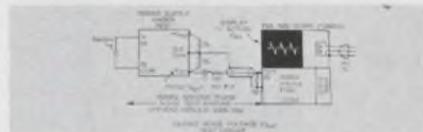
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INFORMATION RETRIEVAL NUMBER 67

## POWER SOURCES

### Dc/dc converter offers high isolation



Stevens-Arnold, 7 Elkins St., South Boston, Mass. 02127. (617) 653-0355.

Super Iso-Pak Model B12/D15/60/Y dc/dc converter is designed primarily for applications requiring low leakage and high breakdown levels. Effective C is 5 pF, effective R is  $1 \times 10^{11} \Omega$  and breakdown voltage is 8000 V dc. Input voltage is 12 V dc  $\pm 2.0$  V. Power efficiency is 55%. Output rating is  $\pm 15$  V dc,  $\pm 60$  mA (60 mA available from both sides simultaneously;  $P_o = 1.8$  W). Line and load regulation are typically  $\pm 0.01\%$ . Output noise is 1 mW true rms, measured over a system noise bandwidth of 20 MHz. Reflected input-ripple current is kept to 2% of the input current. No derating or external heat sink is required over  $-25$  to  $+71$  C.

CIRCLE NO. 267

### Six triple-output units share one case size



Faratron Corp., 280 Green St., South Hackensack, N.J. 07606. (201) 488-1440. \$152 to \$178; stock.

The triple-output MO series comes in six models, all in one case size. All units feature barrier-strip connections, with remote sensing leads available. Input is from 105 to 132 V ac, 47 to 420 Hz. Outputs are 5,  $\pm 15$  (or  $\pm 12$ ) V dc. Typical specs include line and load regulation of  $\pm 0.05\%$ , ripple of less than 1 mV rms, or 3.0 mV pk-pk, and stability of 0.05% or 20 mV. Tempco is 0.05%/°C + 1 mV.

CIRCLE NO. 268

## 30-W OEM series comes in four models

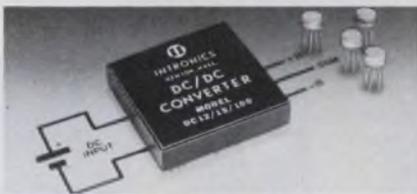


Sola Electric Co., 1717 Busse Rd., Elk Grove Village, Ill. 60007. (312) 439-2800. Approx. \$30; stock.

This line of 30-W, series-regulated dc supplies is for OEM use in minicomputers, point-of-sale terminals and other IC-logic circuitry. Four models are rated at 5 V/3 A, 12 V/1.8 A, 15 V/1.6 A and 24 V/1.2 A. Input voltage ranges from 108 to 132 V, or 216 to 264 V, with output regulation of  $\pm 1\%$ . Input frequency range is 50 to 400 Hz, with load derated to 75% for 400-Hz operation. Automatic short-circuit and overcurrent limiting is built in. Size is  $4 \times 4\text{-}3/4 \times 2\text{-}1/2$  in. and weight is 2-1/2 lb.

CIRCLE NO. 269

## Dc/dc converters offer high isolation



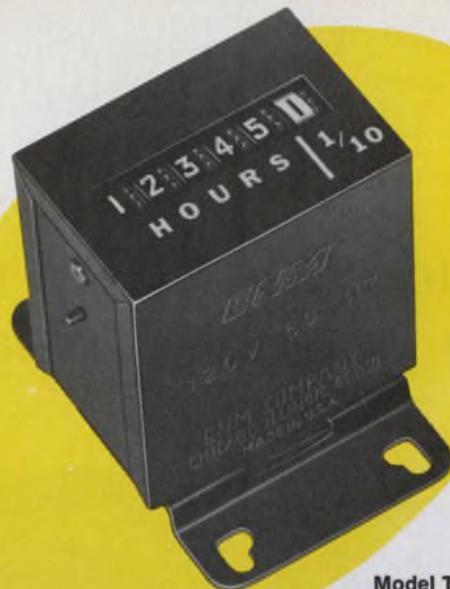
Intronics, 57 Chapel St., Newton, Mass. 02158. (617) 332-7350. 25 mA Series: \$45; 100 mA Series: \$69; 4 wks.

These dc/dc converters feature floating, tracking outputs with 0.02% regulation, a tempco of 0.02%/°C, output ripple and noise of 1 mV rms max and current limiting to 150% of full-load current. The internal oscillator frequency is 12 kHz. Two basic models provide either dual 25 mA or 100 mA outputs,  $\pm 12$  V or  $\pm 15$  V dc, with single unregulated voltage inputs from 5 to 28 V dc. Input/output isolation is  $10^9 \Omega/10$  pF.

CIRCLE NO. 270

# ENM COMPAC®

## time counts and we count time



Model T12  
Elapsed Time Indicator  
6 Digit, Base Mount

ENM's Compac® Model T12 elapsed time indicator counts/records up to 100,000 hours with tenths of hours in relief.

So what? So think of a better way to schedule maintenance, time processes or establish rental fees. And what about the way you warrant your product? Hours of use are a lot more meaningful and protective than mere length of ownership. One user's month may be another owner's year. A calendar warranty can't fairly cover both.

Thanks to its space saving epicyclic step-down gearing, the American made compact Model T12 will fit on almost anything—and with its five mounting styles—anyway you'd like.



Back of Panel



Flange Mount



NEMA Bezel Panel Mount



Round Panel Mount

**Model T12** 6-digit time scale to 99,999.9 hours. Figures .140" high, hours white on black, tenths black on white. Universal base mount and other mountings illustrated above. Synchronous motor requires no lubrication. 115 V. AC. Case width 1.72". Priced from \$7.42 in 1000 lot quantities.

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Write for it today, so you won't be wrong tomorrow.

# ENM COMPANY

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## Solid-state panel meter fills the gap between analogs and digitals



Simpson Electric, 5200 W. Kinzie St., Chicago, Ill. 60644. (312) 379-1121. Under \$100 (quan.).

In a push towards the ultimate panel meter, Simpson Electric has brought forth the ANA/LED, a solid-state indicator that claims some of the best attributes of both the APM and DPM.

Instead of a moving pointer, the ANA/LED displays signals with a linear array of discrete LEDs on a calibrated scale, 5-in. long. When an input is applied, all LEDs below the signal level light up in thermometer-like fashion.

A total of 53 LEDs are used: 50 to match the scale graduations, two to indicate reverse polarity and overrange, and one for zero—which remains on as long as the power does.

Is the ANA/LED the panel meter of panel meters? Not quite; nor was it intended to be. But the ANA/LED has a lot going for it. Among its virtues are these:

- has no moving parts.
- shows trends.
- responds fast: 15 ms, maximum, for dc.
- tolerates large overloads: 5-V spikes on a 50-mV signal have no affect.
- provides an amplified output signal of 0 to 5 V.

And the limitations? Unlike the APM—but like the DPM—the ANA/LED needs power: about 2.4 W worth from a dual 6-V supply. And like the DPM, signal isolation may be a problem if grounding precautions aren't taken or if bat-

teries aren't used to supply the power.

Since the ANA/LED responds to ac, as well as dc, signals, an active input filter is needed to prevent ripple from affecting the reading. The built-in filter attenuates a 120-Hz ripple by 10:1 but slows the meter down somewhat. However, the maximum delay for a zero-to-full-scale step is only 15 ms—and there's no overshoot.

The  $7.87 \times 1.97$ -in. dimensions of the ANA/LED hardly make it diminutive. But the surface-mount version projects just 3/4-in. in front of the panel, and even less behind.

Key specs of the Simpson ANA/

LED include an accuracy of  $\pm 2.0\%$  of full scale, a linearity of  $\pm 0.1\%$  of full scale and a tempco of  $\pm 0.03\%$  of full scale per degree C. Operating temperature range is 0 to 60 C.

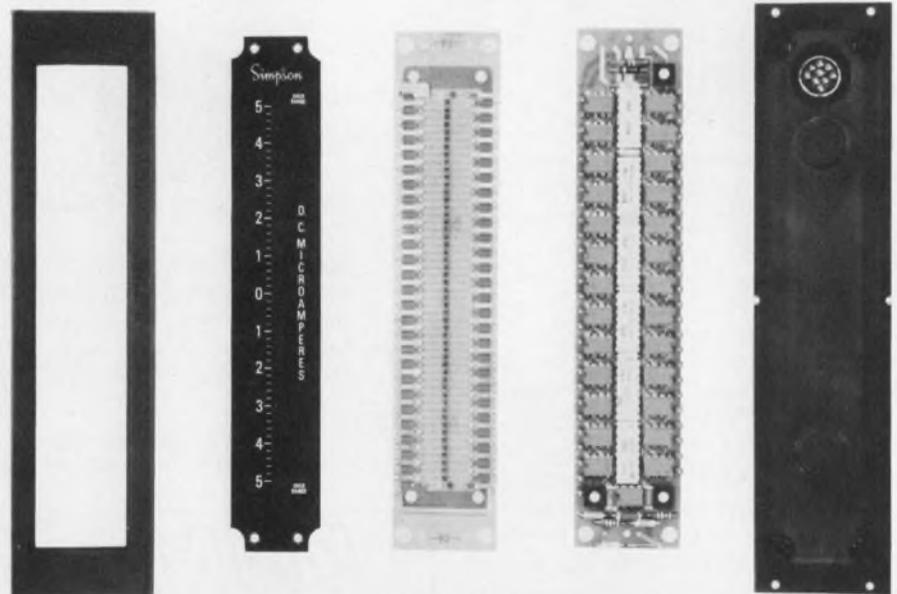
Maximum dc sensitivity of the solid-state unit is high compared with conventional APMs: Just 1  $\mu$ A will light up all the LEDs—that is, give a full-scale reading. For ac, full-scale can go as low as 10 mV pk-pk.

Of course, the linear "bar-graph" concept isn't new. The old Time-Systems' line of DPMs (now Faratron) included one with an auxiliary linear analog scale, composed of lamps that lit or turned off in order.

And Burroughs recently unwrapped its Self-Scan bar graph—a 4-in.-long analog display with 200 digitally controlled neon elements, for a resolution of 0.5%.

For Simpson **CIRCLE NO. 250**

For Burroughs **CIRCLE NO. 251**

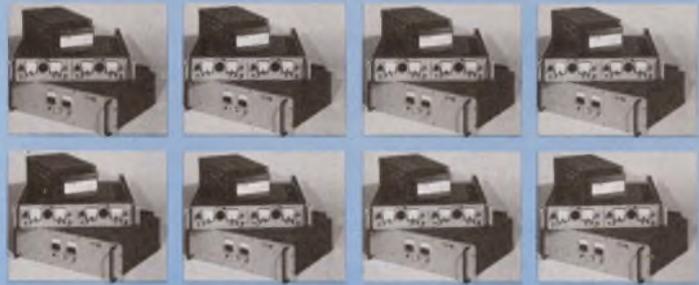


Five assemblies make up the ANA/LED: the cover, scale, LED board, electronics board (includes comparators and range network) and back plate.

Whether you buy  
one's, two's...



or multitudes—



## North delivers power reliability!

MODEL	11000	12000	13000	14000	15000	16000	17000	18000
VDC	AMPERES							
5.0	3.9	5.3	11.3	13.0	20.0	32.5	49.0	82.0
12.0	2.8	4.2	8.0	10.5	15.0	23.0	36.0	58.0
15.0	2.4	3.7	7.5	9.5	14.0	20.5	27.0	47.0
18.0	2.1	3.3	6.0	8.0	13.0	18.0	26.0	40.0
24.0	1.5	2.8	4.2	7.0	11.0	15.0	21.0	33.0
28.0	1.4	2.4	4.0	6.3	9.0	14.0	20.0	29.0
36.0	1.2	2.2	3.1	5.6	8.0	11.0	14.0	23.0
48.0	.95	1.8	2.6	4.2	6.0	8.0	10.0	18.0

MODEL	10000
VDC	AMPS
0-7.5	2.10
0-16	1.25
0-25	0.85
0-33	0.68

DUAL OUTPUT SUPPLIES	
MODEL	N63052
VDC	AMPS
±15 12	400MA
MODEL	N60052
VDC	AMPS
±15 12	1.0A

Listed here are the more popular models—many other voltages are available.

**NORTH**   
ELECTRIC COMPANY

North Electric Company / Galion, Ohio 44833 / A United Telecom Co.

Many O.E.M.'s agree that it just doesn't make sense to risk the reputation of a major piece of equipment over a minor component—especially, when the cost difference is so little.

If you're one of them, we'd like to quote your next power supply order. Whether you need one unit—or one hundred, North has the product selection and the production capacity to deliver more standard power reliability for your dollar.

To back it up, we offer the industry's finest technical specialists and over 40 years experience as the leader in custom power supplies.

Send for a catalog today, or call 419/468-8874.

SP-16

INFORMATION RETRIEVAL NUMBER 69

## Magnetic Reed BURGLAR ALARM

### Door and Window Switches for Concealed Installation

- No installation screws, nails or glue required
- No magnet loss in hollow doors
- Will operate through a big 1/2" gap
- Six types: SPST-NO, SPST-NC, SPDT. Each available with supervisory loop
- Guaranteed for 2 years or 10 million cycles
- Lowest price



Also available for steel doors.

Ask for free sample of SPST-NO on your letterhead or call 308-235-4645.



**GEORGE RISK  
INDUSTRIES, INC.**

802 South Elm, Kimball, Nebraska 69145  
Phone: 308-235-4645 TWX: 910-620-9040

INFORMATION RETRIEVAL NUMBER 70

ELECTRONIC DESIGN 15, July 19, 1974

**ALCOKNB**

Don't just take our beautiful **KNURLED KNOBS** for granted! They're different because they are completely machined, including the **KNURL** and then anodized. This takes a little more time and effort, but we think it's worth it. You'll agree, too, when you see these knobs.



KN  
SERIES

Call us today at  
(617) 685-4371  
for samples  
and prices.

**ALCO ELECTRONIC PRODUCTS, INC.**  
1551 Osgood St., No. Andover, Mass. 01845

INFORMATION RETRIEVAL NUMBER 71

**ALCOKNB**

**ALCOKNB**

We call this our "**GROOVY**" knob series because of its unusual "**MOD**" appearance. Fully machined in aluminum and anodized. First time ever, we're offering mated pilots, pushbutton switches, etc. You've got to see this new line to believe your eyes.

Call (617) 685-4371 now for a sample and literature describing this exciting line.



KG Series

**ALCO ELECTRONIC PRODUCTS, INC.**  
1551 Osgood St., No. Andover, Mass. 01845

INFORMATION RETRIEVAL NUMBER 72

**ALCOKNB**

**WANT BIG PERFORMANCE  
IN A SMALL  
MEMORY?**

**TRY THIS  
ON FOR  
SIZE**

If you need high speed, small capacity non-volatile storage — and cost is important — the MICROMEMORY 9000, is tailor-made for you. It is a complete memory system on a single 9" by 13.4" printed circuit card. No external circuitry other than power supply is required.

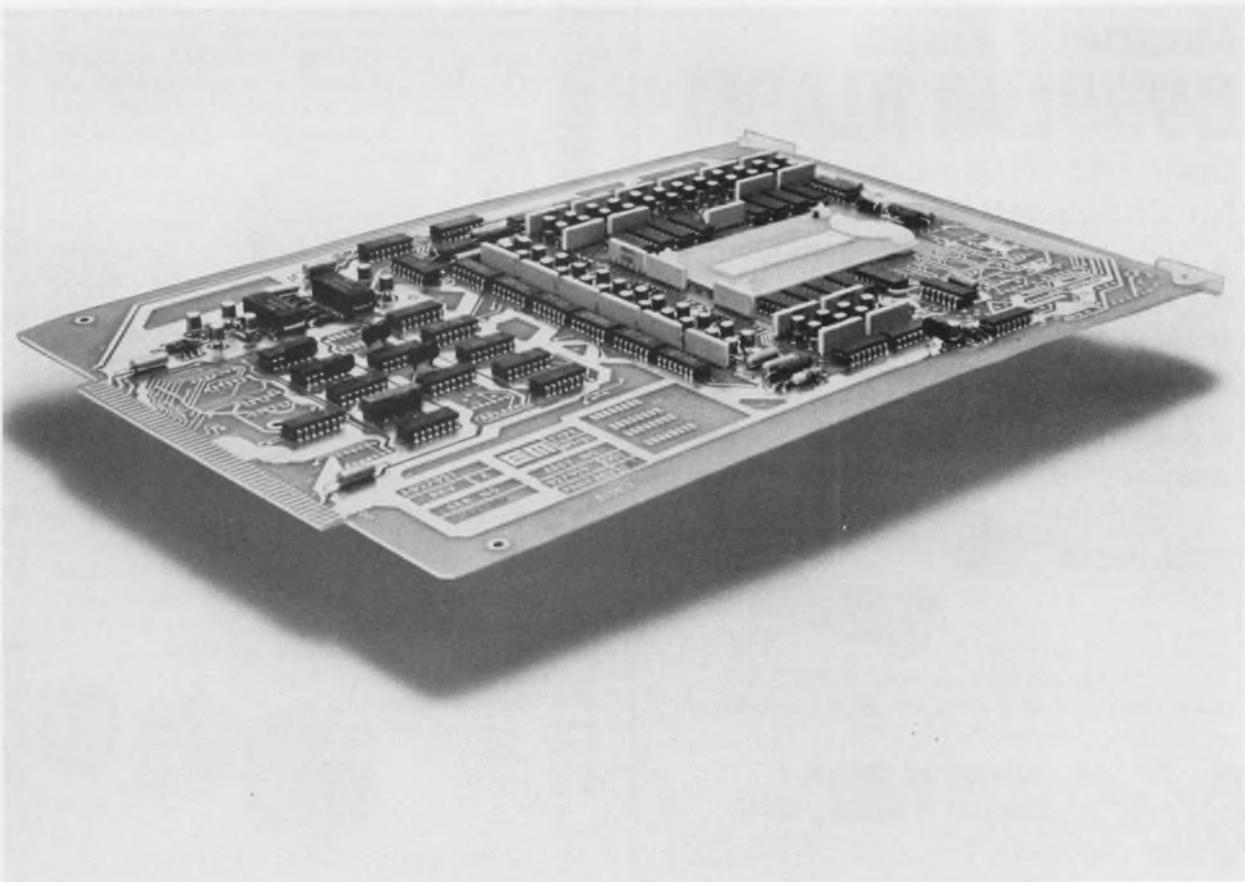
The MICROMEMORY 9000 cycles at 1.2 microseconds per bit, and accesses at 500 nanoseconds. Standard configurations are 8K by 1 bit and 4K by 1 bit. The system may be reconfigured (internally in the module) to binary multiples of the basic configuration. (e.g. the basic 8K x 1 module may be reconfigured to 4K x 2 or 2K x 4 or 1K x 8.)

The MICROMEMORY 9000 is an ideal solution for such applications as point of sale terminals, CRT displays, numerical controls, and any instrumentation application where data retention under power loss is essential.

Get full details on the MICROMEMORY 9000 from your local EMM office, or call Commercial Memory Products Marketing Department at (213) 644-9881.

**EMM** ELECTRONIC  
MEMORIES  
**COMMERCIAL MEMORY PRODUCTS**

A Division of Electronic Memories & Magnetics Corporation  
12621 Chadron Ave., Hawthorne, Calif. 90250



**Portable scopes come with built-in DMMs**



Tektronix, P.O. Box 500, Beaverton, Ore. 97005. (503) 644-0161. DM43, \$475; DM40, \$390 (add price of scope). August.

Models 465 and 475 portable scopes now come with optional, built-in digital multimeters. The 3-1/2-digit meter, called the DM43, offers five voltage ranges from 200 mV to 1200 V, 6 ohms ranges from 200 Ω to 20 MΩ, temperature probing capability from -55 to +150 C, and differential time-delay measurements between any two points on a CRT waveform display. A second version, the DM40, offers all of the above except temperature probing.

CIRCLE NO. 271

**Bench synthesizer covers vhf range**



Syntest Corp., 169 Millham St., Marlboro, Mass. 01752. (617) 481-7827. \$2295.

Model SI-200 vhf synthesizer provides outputs from 1 Hz to 200 MHz with 6-1/2-digit resolution in eight ranges, and with the stability and accuracy of its internal 1-ppm crystal clock. Range and frequency are selectable with front-panel thumbwheel switches. Output level is also adjustable by front-panel controls.

CIRCLE NO. 272

**Light-beam oscillograph refrigerates paper**



Hathaway Industries, 11611 51 St., Tulsa, Okla. 74145. (918) 663-0110. \$3350; 120 days.

Model 440, a new 12-in. direct-write oscillograph, is said to be the first light-beam unit with an optional solid-state refrigeration paper compartment. This compartment maintains the paper temperature below 100 F. With adaptors, paper width can be 8 or 10 in. The instrument has a 70-channel capacity, with chart speeds adjusted by seven pushbutton selectors. Speeds range from 0.1 to 80 ips.

CIRCLE NO. 273

**510-MHz amplifier gives 3 W into any load**



Electronic Navigation Industries, 3000 Winton Road S., Rochester, N.Y. 14623. (715) 473-6900. \$995.

Model 503L is a general-purpose, broadband amplifier capable of more than 3 W of linear power output when driven by any laboratory signal or sweep generator from 2 to 510 MHz. A linear Class A design, the 503L will boost the output of any signal source by a flat 40 dB ±1.5 dB and provide full forward output power into any load impedance from an open to a short. Although specified only over the 2-to-510 MHz frequency range, full power output is typically available from 1.6 to 540 MHz.

CIRCLE NO. 274

**There's an EMM office near you.**

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*Regional Office*

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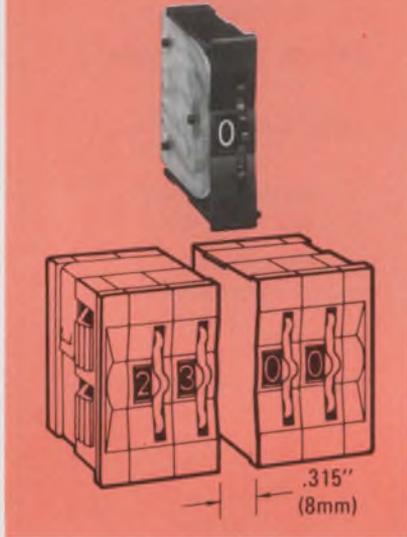
*Far East Headquarters*

**JAPAN**  
(03) 404-8520

**EMM** ELECTRONIC MEMORIES & MAGNETICS CORPORATION.

12621 Chadron Avenue  
Hawthorne, Calif. 90250  
(213) 644-9881

# It pays to be narrow minded



It pays in many ways to use our new Series 23000 narrow SNAP-IN SLIMSWITCHES. They cost less to buy, less to assemble, less to install. They conserve panel space too.

#### "LESS TO BUY"

Prices start at only \$2.50 per switch module... that's only 25¢ per switch function for a 10 position switch.

#### "LESS TO ASSEMBLE"

Using our unique assembly strap, you can stock parts and put switch assemblies together yourself without using tools. We will also build them for you at no extra cost.

#### "LESS TO INSTALL"

Snap-in mounting eliminates installation hardware and tools. The molded-on bezels cover irregular panel cut outs, chipped paint and panel abrasions.

#### "CONSERVES PANEL SPACE"

Width is only .315" (8mm) so you can put more switches into a given space with better readability.

So think "narrow"...think SLIMSWITCH...it really pays.

Send for more information today.

There is a Digitran distributor and sales engineering group near you.

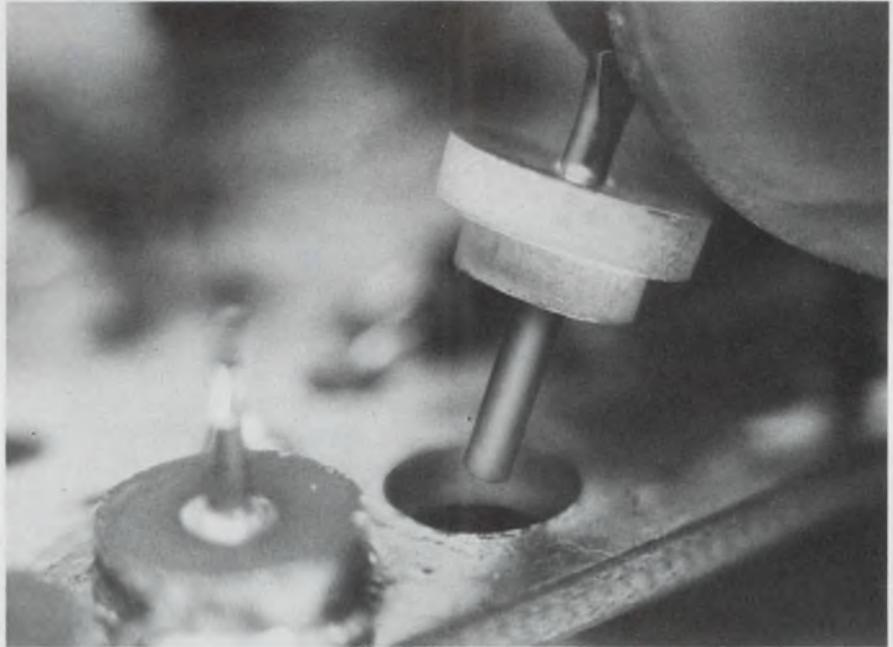
**SNAP-IN  
SLIMSWITCH**  
SERIES 23000 • ANOTHER SWITCH FROM THE  
**DIGITRAN**  
COMPANY

Division of Becton, Dickinson and Company [B.D.]  
855 South Arroyo Parkway / Pasadena, Ca. 91105  
Telephone: (213) 449-3110 / TWX 910-588-3794

INFORMATION RETRIEVAL NUMBER 75

## COMPONENTS

# Uncased ceramic disc filters boost available capacitance



U.S. Capacitor Corp., Centralab Electronics Div., Globe-Union, Inc., 2151 N. Lincoln St., Burbank, Calif. 91504. (213) 843-4222. \$0.45 to \$0.85 (25,000-up) stock to 2 wk (prototype quantities).

Eliminate the case from a ceramic disc feedthrough capacitor and you increase the capacitance/unit volume by up to 10 times. That's what USCC/Centralab is offering in its "U" family of uncased, ceramic stack filters.

In addition, the company says, costs drop to about a third that for the cased version. Also elimination of the case and end seals, the epoxy, internal solder joints and flux is said to yield a more rugged and reliable product.

Voltage ranges in the U-series filters span 50 to 1000 V dc. Capacitance values cover 50 pF to 0.75  $\mu$ F. While current ratings up to 25 A are available.

Dielectric breakdown voltage is a minimum of 2 kV. The operating temperature range is -55 to +125 C. Insulation resistance is 100 M $\Omega$  minimum at the rated dc voltage. Maximum leak rate is 10<sup>-8</sup> cc/s.

The filter is a small monolithic ceramic disc made of barium titanate with a wire through the center and plated on the outside. The disc diameter ranges from 0.135 to 0.35 in.

When the filter is used as a feedthrough capacitor, dc power can pass while rf energy is shunted to the surface to which the filter is soldered. The filter functions to 10 GHz, with better than 70 dB of insertion loss. USCC/Centralab plans future models with "L" section filters incorporating a ferrite inductor for additional attenuation at rf frequencies.

The only other uncased ceramic disc filter on the market is made by Spectrum Control (152 E. Main St., Fairview, Pa.). Its units are single-layer, lower-capacitance filters with values ranging from 6.8 to 1000 pF. Prices start at 12.5¢ in 25,000 pc lots and they are available in standard, 0.25 in. diameters. Spectrum Control plans to introduce monolithic stack uncased filters by the end of this year.

USCC/Centralab CIRCLE NO. 258  
Spectrum Control CIRCLE NO. 259

# MEET THE LUCKY WINNERS

## OF Electronic Design's TOP TEN CONTEST



"We enjoyed every minute we were there," writes Paul R. Saunders, winner of last year's Top Ten Contest. "The islands, the people of those islands and the cruise are wonderful . . . the hardest part of the whole trip was returning to reality." Paul and his wife are shown, left, at the end of their trip at English Harbour, Antigua. Paul also won \$1,000 cash and round-trip air tickets for two to the Windjammer Cruise home port. At the time of the contest Paul was associated with Varisystems Corporation, Long Island, N.Y.

### 1974 CONTEST—READER WINNERS

**1st  
PRIZE**

#### C. R. GOWAN

Development Engineer  
Hewlett-Packard  
Cupertino Division (Cal.)

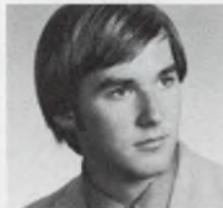
Mr. Gowan picked the ten best-read ads in *Electronic Design's* Jan. 4 Top Ten Contest issue, walked away with \$1,000 cash, air transportation and a Windjammer Cruise for two in the Caribbean.



**2nd PRIZE:** William H. Nott, Development Engineer, IC Development Section, Entertainment Products Division, GTE Sylvania. Mr. Nott's prize is a portable color TV.



KRAMISH



DISOSWAY



BIERMAN

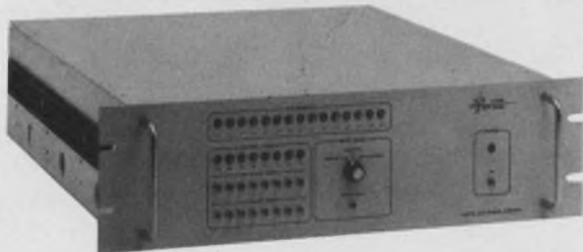
**3rd, 4th and 5th PRIZES:** This year a tie means 4 Bulova electronic timepieces have been awarded. Here are the winners: ARNOLD KRAMISH, Science Advisor, American Embassy (OECD), Paris, France; MARK DISOSWAY III, Advanced Engineering Dept., Delco-Remy, Anderson, Indiana; MARVIN BIEMAN, Director of Quality Control, Vernitron Corp., Deer Park, N.Y.; and (not pictured) HARVEY KAYLIE, Engineer, Mini-Circuits Lab, Brooklyn, N.Y.

95 OTHER TOP TEN CONTEST WINNERS HAVE BEEN NOTIFIED BY MAIL.

**NEXT YEAR TRY YOUR LUCK — You may be a winner. Watch for future announcements.**

# ANALOG - TO - DIGITAL CONVERTER

## 13 BINARY BITS - .5 MICROSECOND



- MODEL 2013 - 13 Binary Bits in 0.5 microsecond.
- 1.0 microsecond total throughput time with Sample and Hold Amplifier.
  - Sample & Hold Aperture time is 1.0 nanosecond.
- SERIES 2000 - From 8 Bits in 100 nanoseconds to 15 Bits in 1.0 microsecond.



**TUSTIN ELECTRONICS CO.**  
1656 South Minnie Street  
Santa Ana, Calif. 92707  
(714) 835-0677

INFORMATION RETRIEVAL NUMBER 77

## AT NCR/WICHITA YOU GET INVOLVED...

from conception through application of design... through manufacturing a reliable product profitably. In other words, you're an integral part of the whole.

That's because our management team is young and aggressive... educated and trained in the computer industry. We're working on many new projects, and the interaction you'll have with other products and divisions will give you a broader experience... and the opportunity to advance according to your ability.

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ACCOUNTING COMPUTER DIVISION

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INFORMATION RETRIEVAL NUMBER 901

## COMPONENTS

### Pressure transducer made of stainless steel



Daytronic Corp., 2875 Culver Ave., Dayton, Ohio 45429. (513) 298-7542. \$315 to \$345.

Measurement of low-level gauge or differential pressure is achieved by the new Series 501 pressure transducers. Based on the bonded-strain-gauge principle, these units are available in five ranges from 0-to-5 to 0-to-150 in. of water and provide 3-mV/V output with 0.2% accuracy in typical industrial use. Stainless-steel construction is used in all housings, diaphragms and pressure cavities. O-rings seal all electrical elements. The sensors are temperature compensated from -65 to 250 F and withstand shock acceleration of 200 G without damage.

CIRCLE NO. 275

### Nonpolar electrolytics operate to 160 WV

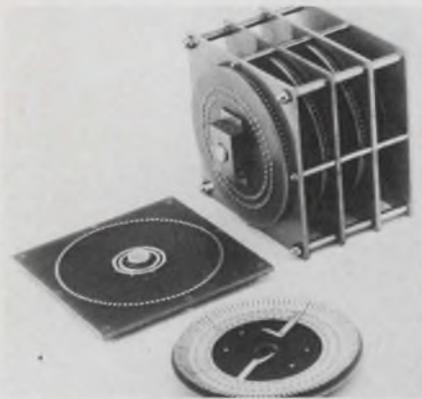


International Importers Inc., 2242 S. Western Ave., Chicago, Ill. 60608. (312) 329-9292. Typical: \$89.70 per thousand: NT(10,000 up); stock.

Rubycon aluminum electrolytic nonpolar capacitors are designed for use in crossover-network circuits or other low ac circuits. They are available with single-end leads (Type NW) or axial leads (Type NT). Operating temperatures for these units range from -10 to 70 C. Capacitance tolerance is  $\pm 20\%$ . Values for Type NW and NT capacitors range from 0.47 to 100  $\mu\text{F}$ , and they are available in seven different voltage ratings—from 10 to 160 WV.

CIRCLE NO. 276

## Special switch shorts all except one contact



Langevin Precision Switches, 2030 Placentia Ave., Costa Mesa, Calif. 92627. (714) 642-8083.

In its paralleling form, all switch positions are shorted together except one. This selected position becomes isolated from the rest on the same deck. The paralleling switch can be used in multiple-circuit cable testing for both continuity and voltage breakdown. The switch can also be modified for notch or tab homing, binary coding and position selection for remote control. The switch is also available in a progressive-shortening form that connects a new contact to all preceding contacts, each time the switch is advanced. The progressively shorting decks can be used for paralleling capacitors in decade units and to vary capacitance values in multiple, fixed-frequency generators, receivers and transmitters.

CIRCLE NO. 277

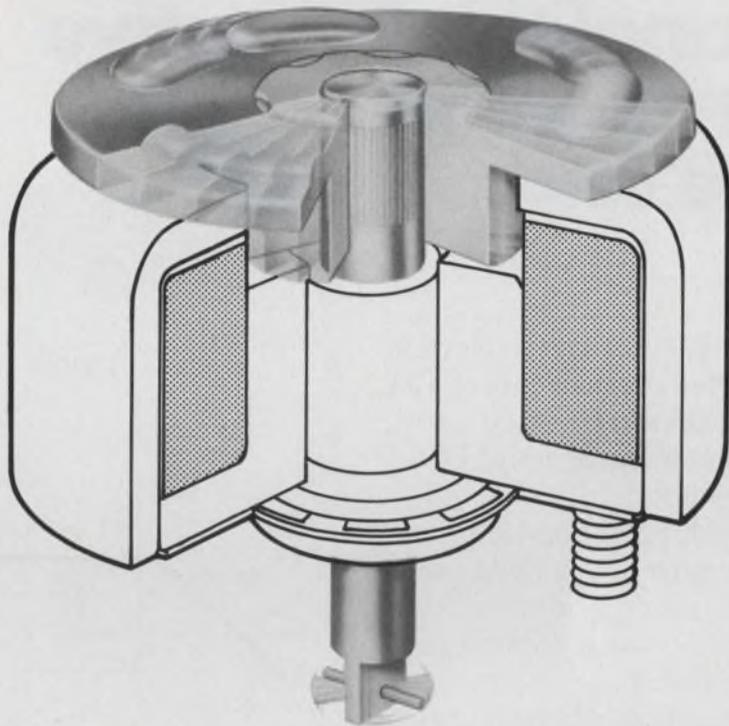
## Keyboard switch provides form D contact

Cherry Electrical Products Corp., P.O. Box 718, Waukegan, Ill. 60085. (910) 235-1572. \$0.99 (2000 up).

A new keyboard switch has two sets of contacts, one SPST-NO and the other SPST-NC. When used exactly as supplied, the M62-0900 momentary-action keyboard switch is a form A plus a form B. When the switch button is depressed, it first causes the NO to close. When the button is pressed further, the NC opens. This is a make-before-break action. A Form D, or SPDT make-before-break, is obtained by the simple process of wiring the poles together.

CIRCLE NO. 278

## Power in the turns makes all the difference



## in Ledex® Rotary Solenoids

You get all the power available when you apply a Ledex rotary solenoid to your turning application. The compact rugged design gives maximum power output with minimum weight and size.

You'll probably want high torque initially, or at the starting point of your turn. With Ledex it is available. Your design requirements can be matched to an existing broad range of solenoids, or specifically tailored for power where you want it.

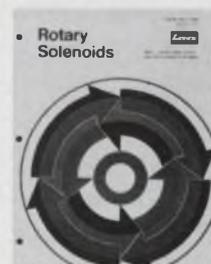
Quality, to you, means longer life. Ledex solenoids provide dependable service, and a life of over 100,000,000 cycles is available for those who need it. When you are making professional decisions, specifying Ledex rotary solenoids, tubular solenoids, stepping switches, rotary switches and push button switches can make a dramatic difference.

Send now for our free catalog of specifications, types and sizes of rotary solenoids. It contains complete details on solenoid construction, torque and stroke, duty cycles and other specifications.

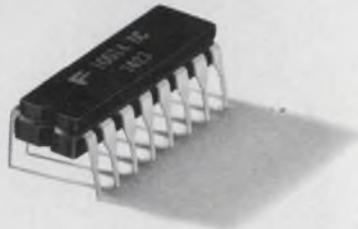
Toll free number for name of your nearest representative: 800-645-9200



**LEDEX INC.**  
123 Webster St.  
Dayton, Ohio 45401  
(513) 224-9891



# Announcing new low-cost monolithic ECL active terminators. The end.



Now, ECL interconnection can be just about as easy as TTL.

Thanks to Fairchild's new F10014 monolithic active ECL terminators.

Each F10014 device provides a handy monolithic package containing 14 terminators—all useable over a wide range of impedance.

Of course, wherever carefully controlled impedances are maintained, matched passive resistor termination remains technically preferable.

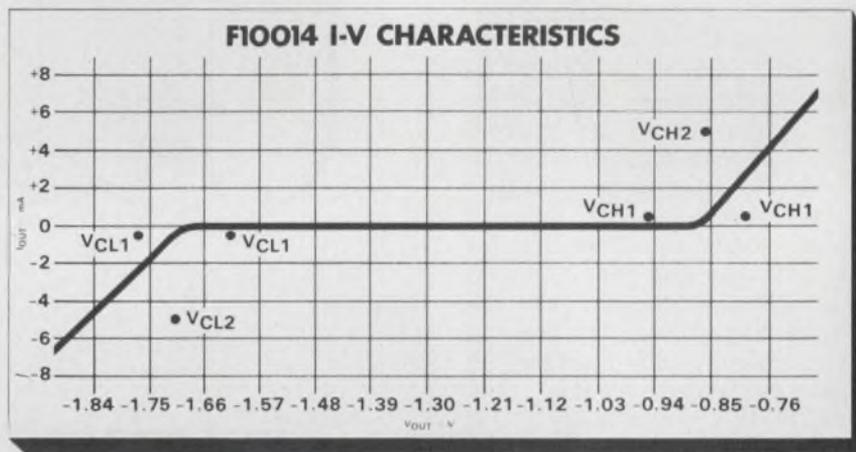
But where they aren't, our inexpensive (7¢ per termination at the 100 quantity) F10014 active terminators can really come in handy.

## How Fairchild's remarkable new F10014 ECL active terminator works.

Looking at our F10014 characteristic curve you can see that the F10014 device exhibits a high impedance when the input signal is within normal ECL operating levels. But as soon as ringing or overshoot appear, the impedance drops.

And the voltages are clipped.

You can use the F10014 as the only termination. Or, in conjunction with passive termination as well.



## Six key advantages.

Compared with diode clamps or conventional passive termination packages available, the new F10014 active terminator affords at least five or six worthwhile advantages.

1. The F10014 costs less per termination than other packages or diode clamps

(see cost comparison table).

2. It has self-contained reference voltages. No external components or -2V supply required.

3. The F10014 can reduce your total system cost. And it can help you save money in other ways. Like allowing you to use more wire-wrap interconnects.

4. It uses low power—about 7.0 mW per termination.

5. The F10014 reduces design time. It successfully terminates the varying impedances to be expected on wire-wrap boards used in prototyping or with design modifications.

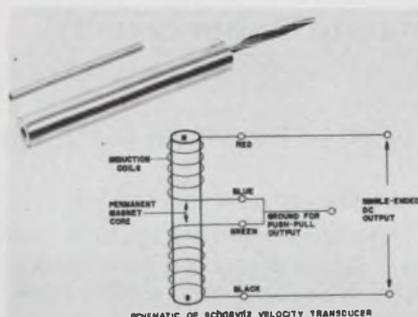
6. The F10014 is compatible with all ECL families. It avoids heavy drain on ECL families not rated for driving resistive terminations.

## Comparative ECL Termination Costs.

Type	No. of Terminations	Price 100-999	Cost of Termination
Packaged Resistor Networks	10-12	0.74-2.25	.074-0.19
Clamping Diodes	1	1.00-2.00	1.00-2.00
F10014	14	.98	.07

## COMPONENTS

### Velocity transducer uses a PM core



Schaevitz Engineering, U.S. Route 130 & Union Ave., Pennsauken, N.J. 08110. (609) 662-8000. \$78.50 to \$435.50; stock.

Schaevitz' new VT-Z Series of velocity transducers is electrical-ly and physically interchangeable with Hewlett Packard's LV Series. The units are of a permanent-magnet, self-generating type and require no excitation voltage or field calibration. The output voltage is linear to within 1.0% of full scale and directly proportional to the velocity of the movable core. The velocity transducers can be used for the measurement of acceleration by processing the velocity signal through a differentiator circuit.

CIRCLE NO. 279

### Chip and pellet caps suitable for microwaves

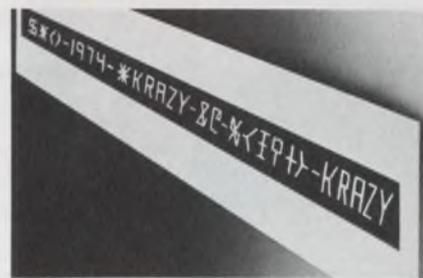


JFD Electronics Components Corp., 15th Ave. at 62nd St., Brooklyn, N.Y. 11219. (212) 331-1000.

Microwave, porcelain, ceramic, multilayer capacitors, called Micro-ceram have high Qs; high stability with temperature, voltage and frequency; have no aging or piezo-electric effects; are capable of withstanding severe environmental ambients; and they possess high-power and low-noise characteristics. The capacitors are suited for use in hybrid circuits. They are available in chip form 0.110 × 0.110 × 0.100-in. and pellet form 0.130 × 0.110 × 0.100 in., and in a variety of leaded configurations.

CIRCLE NO. 280

### Displays 32 characters from ASCII code



American Electronic Laboratories, P.O. Box 552, Lansdale, Pa. 19446. (215) 822-2929.

Alphanumeric LED display system, Model HMC 3093-32, is an ASCII compatible 32-character LED display with decimal points preceding each character. Complete display drive electronics and display data storage are included. The user need only provide parallel 6-bit ASCII data, data-load control, clock line and 5 and -12-V supply inputs. Three display modes are available. In the burst-display mode up to 32 characters are accepted in parallel code at speeds to 20,000 char/s and then displayed instantly following receipt of end-of-message signal. Internal refresh allows continuous display until new information is supplied. Start of a new message clears the old message in its entirety. The typewriter-display mode displays characters one by one as they are received, from left to right. Internal refresh is also provided. The walking-display mode displays characters one by one from right to left. As the 33rd character is entered the first entry is pushed out of the left end of the display.

CIRCLE NO. 281

### Thin-film trimmer pot in a TO-5 housing

Current Industries Inc., 3359 Ocean Ave., Oceanside, N.Y. 11572. (516) 678-3895.

A line of subminiature thin-film trimmer potentiometers in a TO-5 housing features a special glass-to-metal header whose polished surface serves as the substrate of a vacuum deposited film. The resistance of the film can be as high as 68 kΩ. A spring-loaded wiper arm ensures high stability and resolution. The power rating is 500 mW at 40 C.

CIRCLE NO. 282

### Where's the best place to use it?

Fairchild's intriguing new terminator is ideal for many applications. For example:

1. Economical PC board-to-board interconnect.
2. Fast, convenient intraboard design changes.
3. Breadboarding.
4. Extra "insurance." (At just pennies per termination, the F10014 makes excellent sense as a low-cost backup to conventional passive termination.)

### Where to get it.

The F10014 active terminator is now available in full production quantities.

The F10014 is just one of more than 40 Fairchild F10K ECL circuits available.

For complete design information, talk with your friendly Fairchild Distributor or Representative. Or write for your copy of our new ECL Designers Handbook today.

**MADE IN  
FAIRCHILD**

Semiconductor Components Group, Fairchild Camera & Instruments Corp., 464 Ellis St., Mountain View, CA 94040. Telephone (415) 962-5011. TWX: 910-379-6435.

# Sophisticated systems need sophisticated converters



**Perkin-Elmer will custom design Varidac® ac D/A converters to fit your circuitry.**

- Custom converters up to 15 bits of accuracy and 18 bits of resolution.
- Transformer based — highest reliability and stability.
- Designed in the system perspective.
- Off-the-shelf modules available up to 13 bits of accuracy and 12 bits of resolution: Varidac-1 mini-converters, Varidac-2 dual channel converters for D/S systems, Varidac-4 computing resolvers, and complementary transformers.

Send for data sheets, and for a free laminated Binary/Angular Conversion Card. Perkin-Elmer Corporation, Electronic Products Dept., Main Avenue, Norwalk, CT 06856. (203) 762-4786.

**PERKIN-ELMER**

INFORMATION RETRIEVAL NUMBER 81

## MICROWAVES & LASERS

### Signal sources span 1 to 12 GHz

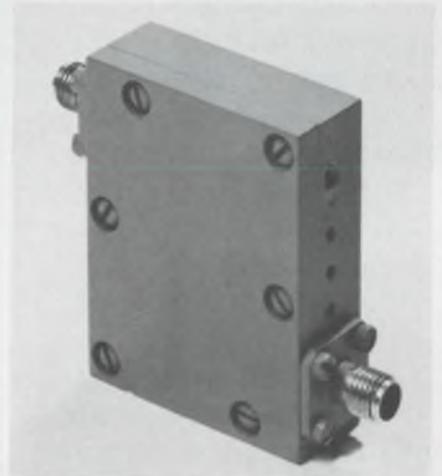


*Micromega, 12575 Beatrice St., Los Angeles, Calif. 90066. (213) 391-7137.*

A family of low-noise microwave signal sources, covering frequencies from 1 to 12.6 GHz, comes in both free-running and crystal-controlled models. Called the 28450 Series, the low-noise units feature a 22-cubic-inch package and stabilities of  $\pm .05\%$  (free-running oscillators) to  $\pm .0005\%$  (phase-locked sources with oven). Standard power levels are 10, 50 and 250 mW.

CIRCLE NO. 283

### Bandpass filters cover 1 to 16 GHz



*Microphase Corp., Box 1166, Greenwich, Conn. 06830. (203) 661-6200.*

A line of octave-band, inter-digital bandpass filters, called the HI series, covers the 1-to-16-GHz frequency range. The largest model, the HI-312JJ for the 1-to-2-GHz band, has a passband insertion loss of 0.5 dB and a maximum VSWR of 1.4. The unit provides 60-dB minimum rejection at 0.75 and 2.30 GHz. It measures 0.5 × 2.23 × 2.46 in. and weighs 5 oz. Power rating for the series is 100 W average.

CIRCLE NO. 284

## new SWITCHING VOLTAGE REGULATORS



### HIGH PERFORMANCE

High Efficiency . . . to 90%  
MTBF > 100,000 hrs  
Low Case Temperature Rise . . .  
< 10°C above ambient  
Load Regulation . . . 0.1%

### SMALL SIZE

2" x 2" x 7/8" Encapsulated Module

LOW COST **From \$30<sup>95</sup>** (1-9)

### FOR USE IN

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High Efficiency Power Supply  
Designs  
Battery Powered Applications

**1 or 2 Amp Models from 5 to 28 Vdc**

*Also Available: High Efficiency Power Supplies and Power Supply Kits*

Our NEW 32 page catalog describes our full line of component module, PC card, open-frame, cased, and laboratory power supplies, DC/DC converters, DC/AC Inverters, DC/DC Isolators, switching regulators, and power kits.



**SEMICONDUCTOR CIRCUITS, INC.**

306 RIVER STREET ■ HAVERHILL, MASSACHUSETTS 01830  
(617) 373-9104

INFORMATION RETRIEVAL NUMBER 82

## 2-to-8-GHz oscillators output up to 10 W

*Ailtech, 19535 W. Walnut Dr., City of Industry, Calif. 91748. (203) 965-4911.*

Expanding its line of high-frequency power sources, the company now offers its 448 Series. The new units cover the 2-to-8-GHz frequency range, with output powers that reach 10 W. Units are fixed tuned to customer-selected frequencies.

CIRCLE NO. 285

## Combiner/divider line meets stringent tests



*Waveline Inc., P.O. Box 718, West Caldwell, N.J. 07006 (201) 226-9100.*

Designed for rugged satellite ground-terminal applications, the company's series of combiners/dividers consist of the following: the Model 91216, a 2:1 signal combiner; the 91197, a 4:1 combiner; and the 91150, a 16:1 combiner. The first two units operate from 5.9 to 6.5 GHz; the last operates from 3.7 to 4.2 GHz. All units feature a minimum isolation of 40 dB, while insertion loss varies from 3.5 to 13 dB.

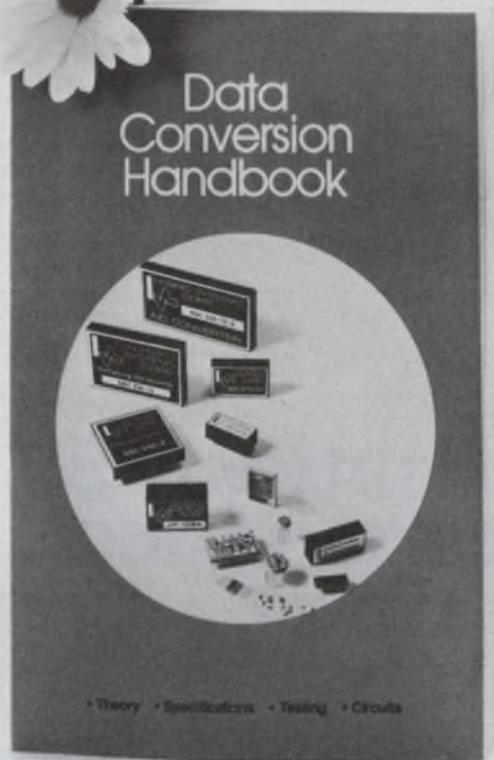
CIRCLE NO. 286

## Isolators, circulators aim for land-mobile use

*Western Microwave Lab., Inc., 1260 Birchwood Dr., Sunnyvale, Calif. 94086. (408) 734-1631. \$225 to \$240; stock.*

Isolators (Model 2J-470-512) and circulators (Model 3J-470-512) are offered for the uhf land-mobile communications band of 470 to 512 MHz. The devices feature a minimum isolation of 21 dB, maximum insertion loss of 0.5 dB and maximum VSWR of 1.25. Input power rating is 350 W cw, and load rating for the isolator is 20 W cw.

CIRCLE NO. 287



# The Book... From Hybrid Systems, Naturally.

This 176-page handbook is offered as a guide to design engineers and others who specify and/or buy electronics... and who are tired of groping their way through the muddle and mystique of data conversion.

It's readable... because it was written by practitioners rather than theoreticians, not to amaze but to inform. It defines the qualities, specifications and techniques that combine to give D/A and A/D converters their special character. It relates those considerations to specific areas of application.

Chapters include: DIGITAL-TO-ANALOG CONVERTERS • ANALOG-TO-DIGITAL CONVERTERS • SAMPLE/HOLDS • ANALOG MULTIPLEXERS • CODES.

Mail \$1.50 (for postage and handling) to:

87 Second Avenue, Burlington, Massachusetts 01803

**Hybrid Systems**  
CORPORATION

## Industrial klystron produces 50 kW cw



Thomson-CSF, Electron Tube Group, 8 rue Chasseloup-Laubat, 75737 Paris Cedex 15, France.

The Model TH 2054, 2450-MHz klystron generates up to 50 kW of cw power with an efficiency exceeding 60%. The klystron lists a gain of 49 dB, drive power of 700 mW and a beam rating of 25 kV and 3.2 A. A major use of the new klystron is expected to be in industrial materials-processing applications.

CIRCLE NO. 288

# Automatic 0.25% impedance measurement:



Our new Model 251 Digital Impedance Meter provides the most accurate measurements of inductance (L), resistance (R), capacitance (C), and conductance (G) available in any instrument up to five times the cost—plus it's fast and reliable.

Big, fat claims, right? But consider this: Accuracy of 0.25% + 1 digit, measurement speeds of a fraction of a second, high-intensity 3½-digit readout has overload blanking to prevent false readings, solid-state construction packed into a rugged 10-pound frame. And simple to operate.

You might consider this. Our reputation. We've led the building of precision impedance measur-

ing instruments for laboratory and quality control applications for 25 years.

Check us out, then call or write for the complete story. Ask about our discrete IC testers, too.

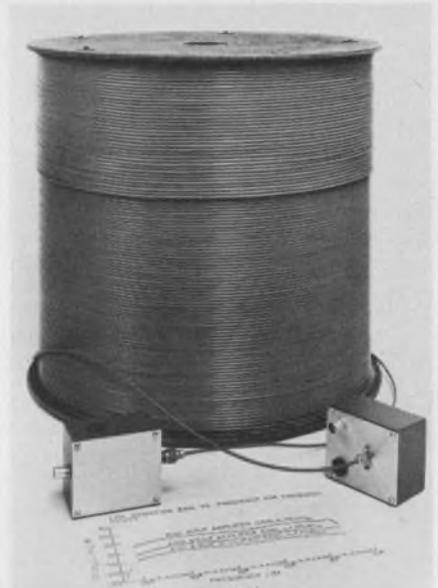
Electro Scientific Industries  
13900 N.W. Science Park Drive  
Portland, Oregon 97229  
Phone: (503) 646-4141

Openings: Product Manager, Application Engineers.

**\$990.**  
(U.S.A.)

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ELECTRO  
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## Optical waveguide limits loss to 30 dB/km



Corning Glass Works, Telecommunication Products Dept., Corning, N.Y. 14830. (607) 974-9000. P&A: See below.

Low-loss multimode optical waveguide bundles—Product #0790-B-19—and optical waveguide links—Product #0790-L-01—are available for prototype systems and related development work. The bundles have 30 dB/km maximum signal attenuation at a wavelength of 820 nm, and consist of 19 multimode step-index optical waveguides jacketed in polyvinylchloride.

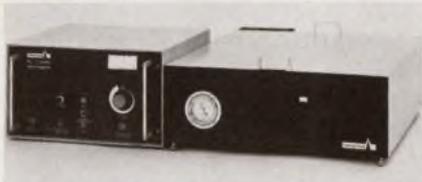
The optical waveguide link consists of a 19-fiber bundle with an electrical-to-optical signal converter at one end and a reconversion unit at the other. Links are available in lengths up to a maximum of 500 meters.

Attenuation characteristics of the bundles are best at wavelengths between 800 and 900 nm, which correspond to available GaAlAs diodes, and at 1060 nm, which correspond to Nd:YAG lasers. With a typical numerical aperture of 0.14, the waveguide bundles accept incident light rays striking the waveguide fiber cores at angles of 8° or less.

Cost of bundle, also available in lengths up to 500 m, is \$57 per meter for orders under 5 km and \$28.50 per meter for orders of five or more kilometers; the minimum order is \$1000. The link costs \$1000 for the transmitter and receiver modules.

CIRCLE NO. 289

### UV laser soars to 1 MW peak



Lambda Physik GmbH & Co. KG, D-34 Goettingen, Am Schelhdorn 7, Germany.

The Model M100 UV pulsed gas laser offers a peak output of 1 MW at 337.1 nm. The nitrogen laser has a pulse halfwidth of 2.5 ns, beam dimensions of 7 × 15 mm and repetition rates of 1 to 100 Hz. A dye-laser accessory, called the Model FL100, extends the laser's application range. With the accessory, a user can obtain a narrow linewidth nanosecond light source that can be tuned continuously from 235 to 800 nm.

CIRCLE NO. 290

### X-ray generator tests assembly lines



Analytical Development Associates Corp., 10300 Bubb Rd., Cupertino, Calif. 95014. (408) 255-6353.

The ADAC 100-kV constant-potential X-ray generator features solid-state electronics and computer-control interface for automatic operation. The generator produces both X-ray fluorescence and X-ray imagery to achieve nondestructive assembly-line testing of a variety of products. Other features include safety interlock and operating protection. The unit weighs less than 200 lbs.

CIRCLE NO. 291

### Components aid mm-wave designs



Electron Dynamics Div., 3100 W. Lomita Blvd., Torrance, Calif. 90501. (213) 534-2121. \$50 to \$175; 10 days.

Three series of waveguide components for the 26.5-to-110-GHz frequency range consists of E and H-plane bends, tapered transistions, and 45 and 90-degree twists. The E and H-plane bends are offered in 30, 45, 60, and 90-degree bend angles and in six standard waveguide sizes. Both the 45 and 90-degree twists are also available in six waveguide sizes.

CIRCLE NO. 292

GLENAIR

## SAV-CON CONNECTORS

Most electrical systems need connectors. But connectors can be a problem. Solution: Don't plug and unplug connectors, at least during the test and check out phase. Plug in a SAV-CON instead. SAV-CON interfaces between your test cable and unit connectors. Saves contact wear and tear on both. Do your connectors a favor. Plug in a SAV-CON.

GLENAIR Inc., 1211 Air Way, Glendale, California 91201. (213) 247-6000. TWX 910-497-2066. TELEX 67-3485.

Test cable connector

SAV-CON

Unit connector

One piece pin/socket contact design for maximum reliability.

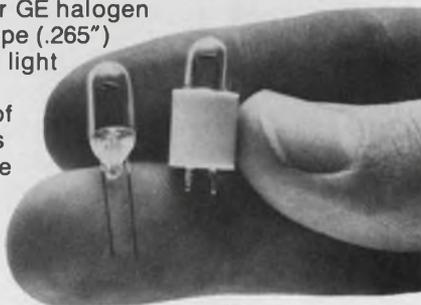
# New and improved General Electric lamps provide for increased design flexibility.

## Two new sub-miniature halogen cycle lamps ideal for miniaturization.

These new T-2, 6.3V, 2.1 amps, 75 hour GE halogen cycle lamps are the smallest of their type (.265") and set industry standards for size and light output (16-20 candlepower). They are the perfect lamps for miniaturization of equipment such as reflectors, housings and optical systems, and they also save on overall cost of your equipment.

In addition, they are less than half the cost of the #1973 quartz lamp they replace. Two terminal configurations are available: #3026 (20 candlepower) has wire terminals; #3027 (16 candlepower) has a new two pin, ceramic base that plugs in to make installation and removal a snap.

These lamps have an iodine additive that creates a regenerative cycle that practically eliminates normal bulb blackening. They will produce approximately 95% light output at 75% of rated life.



## An expanded line of Wedge Base Lamps for simple, low-cost circuitry.



Now you can have greater design freedom than ever before with wedge base lamps. GE now offers six large lamps in its line of T-1 $\frac{3}{4}$  (.230" max.) all-glass, sub-miniature wedge base lamps. In addition to our three 14V lamps (#37, #73 and #74), we now also offer two 6.3V lamps (#84 and #86) and a 28V lamp (#85).

These lamps are ideal for applications where space is at a premium. Their wedge-based construction allows you to design for low-cost sockets and virtually ends corrosion problems because they won't freeze in the sockets. And the filament, which is always positioned in the same relation to the base, offers more uniform brightness.

## Green Glow Lamp has been improved over previous lamp.



Actual Size

Now our G2B Green Glow Lamp, the only domestic green lamp on the market today, gives a more uniform, purer green light than our previous model. It's bright enough for your circuit component applications. With appropriate current limiting resistors, it can be used for 120/240 volt green indicator service. Or used together with our high-brightness C2A red/orange/yellow glow lamps to emphasize multiple functions with color.

All GE glow lamps give the benefits of small size, rugged construction and low cost — 12¢ each for the G2B, 44¢ each for the C2A in 100,000 quantities.

## Send today for newest literature.

For the most up-to-date technical information on any or all of these lamps, write: General Electric, Miniature Lamp Products Department, #0747-L, Nela Park, Cleveland, Ohio 44112.

**GENERAL**  **ELECTRIC**

INFORMATION RETRIEVAL NUMBER 86

## MODULES & SUBASSEMBLIES

### Optical data transmitter and receiver fit TO-5

*Meret, 1815 24 St., Santa Monica, Calif. 90404. (213) 828-7496.*

Hybrid optoelectronic transmitters and receivers, Models MLT and MDA 425/325, work with off-the-shelf glass fiber cable. They provide data links capable of operation from dc to 70 Mbit/s at lengths greater than 20 meters. Both the transmitter and receiver sections consist of three-pin TO-5 header terminations. The transmitter (MLT300 series) combines a high speed, high efficiency IR-LED, designated as ML-35 and a TTL-compatible driver capable of producing high current pulses to 1 A with rise times less than 50 ns. The transmitter requires +5.5 V with a current drain at 50% duty cycle of 200 mA at maximum power output. Trigger signals are applied at the third pin. The MLT300 package is designed to allow direct detachable coupling to a ferrule terminated fiber cable from 1 to 3 mm in diameter with minimum loss of the radiated 850-to-900-nm signal. The receiver (MDA320) has power supply requirements of +5.5 to +15 V at a current drain of less than 6 mA. The single power supply provides bias for the p-i-n photodiode and the operating voltage for the transimpedance amplifier.

CIRCLE NO. 293

### Precision a/d converter delivers 12-bits fast

*Intech, 1220 Coleman Ave., Santa Clara, Calif. 95050. (408) 244-0500. \$5.50 (1 to 9); stock to 4 wk.*

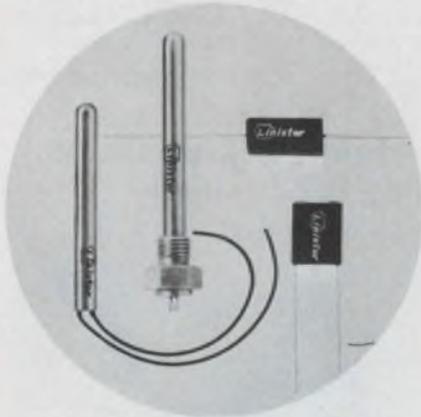
The A-851 12-bit a/d converter has a total conversion time of less than 2.5  $\mu$ s. It uses successive-approximation and has a precision voltage reference which the company claims virtually eliminates errors due to power supply line and load variations. Gain and offset temperature coefficients are guaranteed to less than 20 ppm/°C. Linearity is specified to better than 1.2 LSB,  $\pm$ 120 ppm. The converter is housed in a 2  $\times$  4  $\times$  0.4 in. plug-in module.

CIRCLE NO. 294

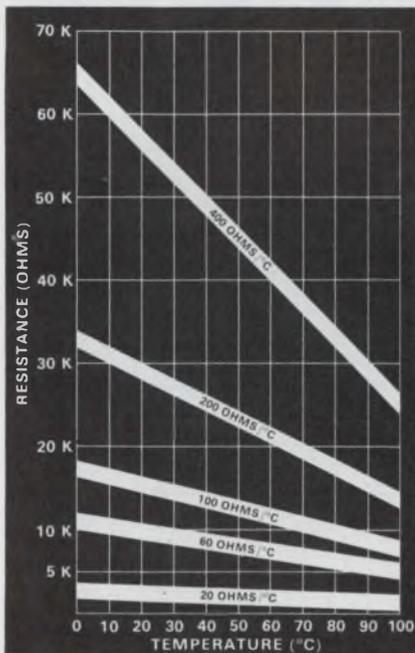
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sensitive linear  
negative temperature  
coefficient thermistor  
assemblies



Linistor assemblies will provide you with an accurate straight line resistance/temperature plot from 0°C to 100°C.



Linistors are ideal for temperature sensing and temperature compensating devices. They are now available in four standard encasements to satisfy most design applications. Write for Data Bulletin L-601.



Thermistor Division  
St. Marys, Pa. 15857  
Phone 814/781-1591

INFORMATION RETRIEVAL NUMBER 87  
ELECTRONIC DESIGN 15, July 19, 1974

## Digital comparator can monitor data lines

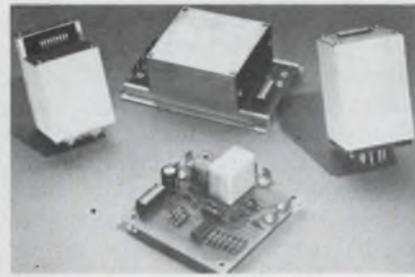


Nationwide Electronic Systems,  
1536 Brandy Pkwy., Streamwood,  
Ill. 60103. (312) 289-8820. From  
\$122; 3 to 4 wk.

The Slimline digital comparator/controller automatically monitors BCD data from a digital instrument (voltmeter, counter, clock, thermometer, etc.). It provides a signal when the data exceed the limit preset on the comparator's switches. The small package (9/16 in. thick) is easy to mount on fixed panels or in portable equipment. Up to 100 comparator/controllers can be cascaded together for multiple preset operation. Both single and dual-limit models are available.

CIRCLE NO. 295

## Modular time delay units are accurate to 0.0016%



Essex International, 1601 Wall St.,  
Fort Wayne, Ind. 46804. (219)  
743-0311.

The 295 series of time delays is accurate to  $\pm 0.0016\%$ . They can be programmed from 1 to 511 s in 1-s intervals. The units use an integrated circuit to perform all the timing functions and a relay as an output device. The time delay modules handle input voltages from 12 to 240 V ac, 60 Hz. The output can have up to a 3pdt set of relay contacts with output-contact ratings of up to 10 A, 120 V ac, 1/3 hp. Three different packages are available—printed-circuit board, plug-in or panel mount.

CIRCLE NO. 296

## Terminate connection problems with Curtis terminal blocks



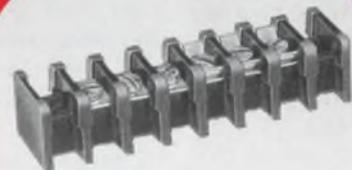
### G Series

Our popular 7/16" center barrier-type blocks are ideal for jobs demanding a variety of terminations at low cost. Tab, screw, clamp, PC pin, solder or taper pin terminals are available. Surface-connect and full feed-thru insulation models are also offered. Available in one thru 26 terminals. G Series feature precision-machined brass inserts, molded in place, for a full mechanical thread system. Rated 20 amps/300 volts.



### E Series

Designed primarily for electronic control and low power circuit application, these 3/8" center inexpensive barrier-type blocks are available in one thru 22 terminals. Your choice of screw, clamp, two, four or six tab quick-connect, PC pin or solder terminals. Surface-connect and feed-thru models are offered. Rated up to 15 amps/300 volts.



### SE Series

Several terminal variations coupled with miniature size make these 1/4" center blocks ideal for use in tight spaces where versatility must not be sacrificed. These barrier-type blocks are available in screw, clamp, two, four or six tab terminals. Surface-connect and full feed-thru insulation models are also offered. Available in one thru 26 terminals. Rated 5 amps/300 volts.

Send for free engineering catalog  
No. 1273.



**CURTIS**  
INDUSTRIES, INC.  
formerly Curtis Development & Mfg. Co.

3266 North 33rd Street, Milwaukee, Wisconsin 53216. Call (414)  
445-1817 for the name of a representative or distributor near you.  
In Canada: A.C. Simmonds & Sons, Ltd., Willowdale, Ontario.

1680

INFORMATION RETRIEVAL NUMBER 88

141

### Dedicated analog divider has accuracy to 0.1%

Function Modules, 2441 Campus Dr., Irvine, Calif. 92664. (714) 833-8314. For 1 to 9 pcs: \$69 (J), \$89 (K), \$139 (L); stock to 2 wk.

The 540 Series of dedicated dividers uses an improved variable transconductance technique to achieve accuracies of  $\pm 0.5\%$  (Model 540J),  $\pm 0.25\%$  (Model 540K) and  $\pm 0.1\%$  (Model 540L) over a 100 to 1 divisor range. Unlike most analog dividers, which use multipliers connected in a feedback configuration, these generate a two-quadrant division function directly. The dividers are housed in  $1.5 \times 1.5 \times 0.4$  in. packages.

CIRCLE NO. 297

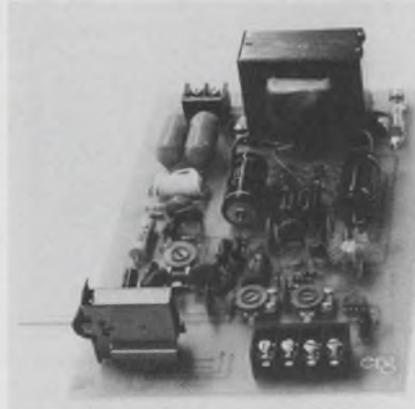
### Multiplexer subsystem includes a/d converter

Custer Research, P.O. Box 305, Fleetwood, Pa. 19522. (215) 376-2842. \$5630; 90 day.

The S5530 basic a/d multiplexer subsystem provides four single-ended analog channels. Each channel can handle a  $\pm 10$ -V signal. The internal converter delivers a 14-bit plus sign output, has a  $10 \mu\text{s}$  conversion time and 100 kHz throughput rate. The system is compatible with most Hewlett-Packard 2100 series operating systems. The S5530 also comes with a software package. Additional (up to 128) channels, differential sample-and-hold amplifiers and other special functions are optionally available.

CIRCLE NO. 298

### Two-way data sets hook up to ac power line



Electronics Research Group, 22 Mill St., Arlington, Mass. 02174. (617) 646-9760. \$109/pair; stock to 4 wk.

The ER-125 modular data transceivers wire directly to ac power lines. They transmit and receive digital (TTL) or analog data. An onboard switch determines the mode (transmission or reception) and LEDs monitor squelch presence. All transmission is FM on any of six carrier channels. Three inputs are available in the transmit mode: TTL, analog ( $\pm 1$  V max) and  $45 \Omega$  speaker. The receive mode allows three outputs: TTL, analog ( $\pm 5$  V range) and squelch. The analog output is buffered for a 200 mA load so that the same  $45 \Omega$  speaker can be used with the transmit/receive switch. Features of these modules include: audio frequency response to 7 kHz, signal limiting to prevent loss of phase locking and dc linearity better than 0.5% for the analog mode. Up to six carrier channels can operate two-way simultaneously in a large building.

CIRCLE NO. 299

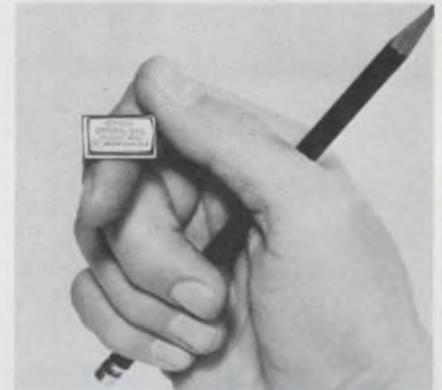
### TO-8 housed rf amp delivers 14-dB gain

Optimax, P.O. Box 105, Advance Lane, Colmar, Pa. 18915. (215) 822-1311. \$85; stock.

A single stage, thick film, rf amplifier provides a gain of 14 dB at +15 V dc. It operates over a bandwidth of 10 to 500 MHz. The amplifier, designated AH-521, has a noise figure of 4.5 dB and its power output at 1-dB gain compression is +5 dBm. The AH-521 amplifier is housed in a TO-8 package.

CIRCLE NO. 300

### Hybrid clock oscillator only 0.2 in. high



Motorola, Component Products, 2553 N. Edgington St., Franklin Park, Ill. 60131. (312) 451-1000.

Model K-1100A, hybrid clock oscillator, uses a crystal oscillator and thick-film hybrid processing. Factory adjusted frequencies from 250 kHz to 20 MHz are available. The oscillator has a frequency stability of  $\pm 0.01\%$  over 0-to-70-C temperature range. The oscillator package has a volume of only  $0.083 \text{ in.}^3$  and is 0.2 in. high.

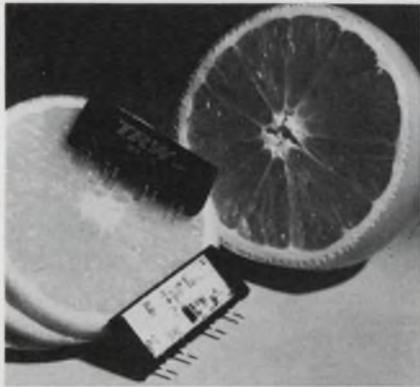
CIRCLE NO. 301



ANALOGY  
ACE OUT THE COMPETITION WITH THE A-860 12-BIT DAC YOUR SYSTEM WON'T NEED RIGGS FOR 100 NS CONVERSION SPEED AT 0.0125% LINEARITY. SETTLES TO THE BOTTOM LINE IN LESS TIME THAN HOWARD CAN SAY "WOMAN'S LIB."

**intech** INCORPORATED  
(408) 244-0500  
1220 COLEMAN, SANTA CLARA CA 95050

## Rf power module delivers 1.5 W at 20 dB gain



TRW, 14520 Aviation Blvd., Lawndale, Calif. 90260. \$41.75 (1 to 99); 6 to 8 wk.

The MX1.5 rf power modules are designed to operate from a 7.5 V battery supply. They provide 1.5 W at 20-dB gain with 50% efficiency. The units have full protection against overdrive and load VSWR. Harmonic outputs are more than 30 dB down. The modules are designed for operation in the 400-to-512-MHz range and have 50-Ω input and output impedances.

CIRCLE NO. 320

## CRT display generator makes 1, 2 or 3-D image

Optical Electronics, P.O. Box 11140, Tucson, Ariz. 85734. (602) 624-8358. From \$125 to \$3208; stock.

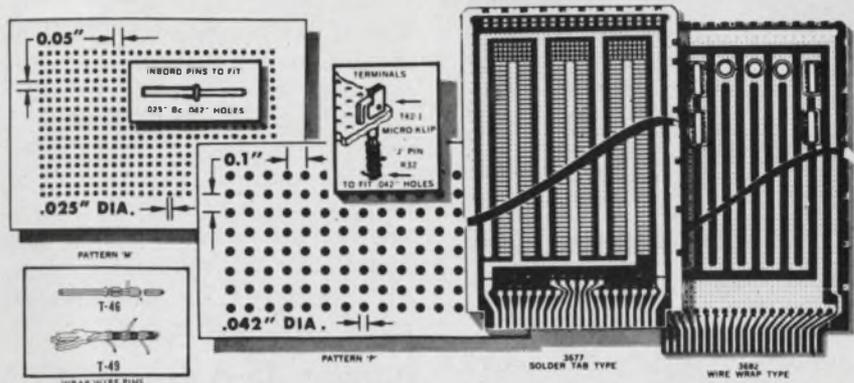
Model 6240 graphic display generator can produce static one, two and three-dimensional patterns and/or fixed graphic images. The 6240 uses one, two or three analog voltage inputs to address the various memory cells. Each cell consists of an external resistance element which is used to program the analog contents. The resistance may be a fixed resistor, potentiometer or FET. The user can change the memory contents as necessary although the intended application is for a nonchanging fixed background display. Some of the display generator's specs include  $\pm 10$  V analog video output voltage range, 1  $\mu$ s memory cell address time, 5  $\mu$ s minimum total memory scan time, -3 to +3 analog address voltage input,  $\pm 15$  V power supplies, minimum memory size of four cells and a maximum size of 262,144 cells.

CIRCLE NO. 321

*New*

## MICRO-VECTORBOARD AND D.I.P. PLUGBOARDS ARE HERE!

Save time — Save work — Save money



### WIDE SELECTION OF SIZES AND MATERIALS

**MICRO-VECTORBOARD "P"** .042" holes match D.I.P. leads. Epoxy glass or paper, cop. cl. also 1/64" to 1/16" thk.

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**NEW SOLDER-PAD D.I.P. PLUGBOARDS** — 3677 Series Epoxy glass, "P" pat. 1/16" thick with 44 etched plug contacts (2 side total) power, ground

busses, pads for up to 24 D.I.P.'s (14's) Also 21 units 16-leads D.I.P.'s, T.O's and discretes

**NEW WRAP WIRE D.I.P. PLUGBOARDS** — 3682 Series Similar to above but closely spaced bus lines for higher density. Up to 48 D.I.P. 14 lead wrap wire sockets mountable or T.O's and discretes

**TERMINALS** — Micro-Klips, Mini-Wire-Wraps, Rd. Pins, Patch Cords, etc., available.

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Phone (213) 365-9661 • TWX (910) 496-1539



INFORMATION RETRIEVAL NUMBER 90

## Fight Brownouts with TOPAZ LINE REGULATORS

- No Distortion • Most Efficient
- Lowest Cost • Smallest Size



500 VA to 24 kVA

Priced from \$290.

### SPECIFICATIONS:

**Input:** 85 to 125V sine wave

**Output:** 117 V sine wave

**Operating Frequency:** 47 to 63 Hz

**Response:** Less than 1 cycle

**Efficiency:** 98%

**Audible Noise:** Typically 2 dB

**TOPAZ**  
ELECTRONICS

SOLUTIONS TO  
POWER PROBLEMS

3855 Ruffin Road, San Diego, CA 92123 Phone (714) 279-0831 TWX (910) 335-1526

INFORMATION RETRIEVAL NUMBER 91

### Schottky detector diodes operate up to 18 GHz



Aertech Industries, 825 Stewart Dr., Sunnyvale, Calif. 94086. (408) 732-0880.

The A2S200 series units are zero bias, silicon Schottky detector diodes. They are designed for use as microwave detector diodes from 100 MHz to 18 GHz. This diode type performs well as compared with point contact, backward and standard biased type Schottky diodes and is optimized for tangential sensitivity and video resistance. Features include: No bias needed, typical  $T_{es}$  of  $-59$  dBm and low  $I/f$  noise.

CIRCLE NO. 322

### Opto-isolators available in low cost packages

Monsanto, 3400 Hillview Ave., Palo Alto, Calif. 94304. (415) 493-3300. \$1.50 (1000-up); stock.

The MCT66 is a low-cost version of the company's MCT6 dual-channel phototransistor opto-isolator. Two 8-pin MCT66 packages fit into one standard 16-pin DIP socket. The two channels offer complete external isolation, and between channels of typically 2.5 kV. The current transfer ratio is 15% typical and 6% minimum.

CIRCLE NO. 323

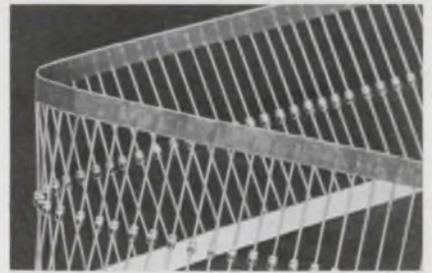
### Fast turn-off SCRs handle 35-A currents

RCA, Box 3200, Somerville, N.J. 08876. (201) 722-3200. From \$4 (1000-up); stock.

Six 35 A, fast turn-off silicon controlled rectifiers (S7432 series) have 50, 100, 200, 300, 400 and 600-V repetitive peak reverse voltage ratings. Types 2N3654, 2N3655, 2N3656, 2N3657, 2N3658 and S7432M have a maximum turn-off time of 10  $\mu$ s.

CIRCLE NO. 324

### Stabistor diodes come in over 50 models



American Power Devices, 7 Andover St., Andover, Mass. 01810. (617) 475-4705. G129: From \$0.10 (25,000-up); 4 to 6 wk.

Fifty stabistor diode types are available in subminiature glass packages. These stabistors are diffused silicon diodes with controlled forward voltage characteristics. They have reference voltages from 0.56 to 3.7 V and are housed in DO-35 glass packages. Voltage tolerances are typically  $\pm 5\%$ . Stabistor families include 1N4156-7, 1N5179, 1N3896-98, 1N4829-30, 1N816, BZ102 series, BZX75C series, G129 series, ST22 series, STB series and APD200 series (replaces GE MPD series).

CIRCLE NO. 325

## An autoranging DMM for only \$299?

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1-year accuracy guarantee, too!

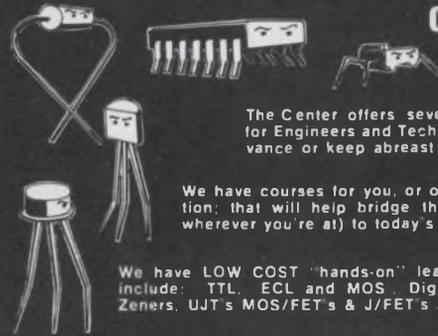


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ELECTRONIC DESIGN 15, July 19, 1974

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ELECTRONIC DESIGN 15, July 19, 1974

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Now! A highly reliable long life capacitor designed for applications requiring large amounts of ripple current at operating temperatures of 85 C and above. Ideal for power supplies, particularly the new switching mode types, energy storage and discharge, input filters for SCR power supplies . . . anywhere large amounts of ripple current are needed. Features include:

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● Standard units available in 21 case sizes — over two hundred ratings

For more information on these, or any of General Electric's wide range of capacitors, call your nearest GE sales office today, or write Section 430-53, Schenectady, N. Y. 12345.

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INFORMATION RETRIEVAL NUMBER 99

## new literature

The Industrial Buyer's Guide to Optical and Electronic Measuring Equipment



### Optical equipment

A 20-page illustrated buyers' guide features industrial microscopes such as measurescopes, polarizing microscopes, inspection and surface finish microscopes and dark field illuminators. Ehrenreich Photo-Optical Industries, Garden City, N.Y.

CIRCLE NO. 326

### Rf and i-f components

A 32-page catalog, "Rf and i-f Components, Circuits and Subsystems," includes sections on microwave mixers and modulators, mixer-preamplifiers, rf amplifiers, i-f amplifiers, rf sources, microwave cavities and subsystems. Varian, Beverly Div., Beverly, Mass.

CIRCLE NO. 327

### Cable-carrier system

A 32-page product bulletin covers the 82B cable-carrier system. The bulletin includes sections covering equipment identification, ordering information, installation procedures and maintenance. GTE Lenkurt, San Carlos, Calif.

CIRCLE NO. 328

### Torque fasteners

Prevailing-torque lock fasteners for general-purpose engineering assemblies are described in a six-page brochure. Elco Industries, Rockford, Ill.

CIRCLE NO. 329

### Power supplies

Descriptive material on standard off-the-shelf products, including military specification power modules, dc-to-ac inverters, OEM supplies, solid-state ac regulators, computer-application power units and related products, is contained in a four-page catalog. ERA Transpac, Moonachie, N.J.

CIRCLE NO. 330

### Hermetic connectors

Complete with dimensioned drawings, insert diagrams and lists of shell sizes and contact arrangements, a 14-page brochure describes a new family of ultra-high performance hermetic connectors. Gulton Industries, Buena Park, Calif.

CIRCLE NO. 331

### Copper

SSC-155, a new copper based metal, is detailed in a six-page bulletin. The bulletin presents data on strength, thermal and electrical conductivity, ductility and strength characteristics. Hussey Metals Div., Leetsdale, Pa.

CIRCLE NO. 332

### Pushbutton switches

The Series 90 switch light or indicator light units are described in a 16-page catalog. Master Specialties, Costa Mesa, Calif.

CIRCLE NO. 333

### Plastics guide

A desk-top leaflet, when opened, shows all of the major plastics families in terms of type, trade name, manufacturers, general characteristics and the standard shapes and sizes. Commercial Plastics & Supply, Cornwells Heights, Pa.

CIRCLE NO. 334

### Data-acquisition modules

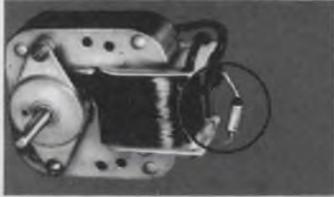
A six-page brochure highlights DATAx, a line of data-acquisition system modules. Data Translation, Framingham, Mass.

CIRCLE NO. 335

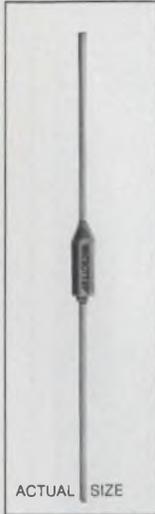
# 1/32 of an ounce of prevention for your electronic circuits.

## MICROTEMP SAFETY THERMAL CUTOFFS\*

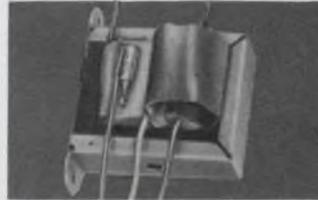
With a MICROTEMP installed on the winding of your motor or transformer, you'll get positive fail-safe protection without adding



any appreciable weight or size. Facilitating transformer and motor compliance with many UL specifications, especially UL506, UL544, and UL547, MICROTEMP will sense excessive temperature and interrupt the power circuit

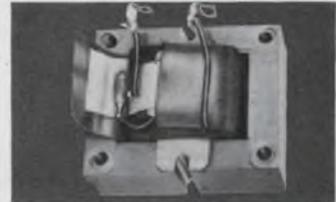


should a fault condition develop. An alternate means of protecting the transformer can be provided by a MICROTEMP which has a small heating element fitted to



its case. This heating element is connected in series with the secondary coil winding and its load, transferring heat to the MICROTEMP with the flow of current. Should the current flowing through the element exceed normal operating levels, the resulting heat will cause the

MICROTEMP to open, thus also opening the primary or secondary coil winding to which it is connected. Reliable, inexpensive and accurate to  $\pm 3^\circ\text{F}$ , MICROTEMPS are available in ratings to fit your application. Add our little prevention to your product now!



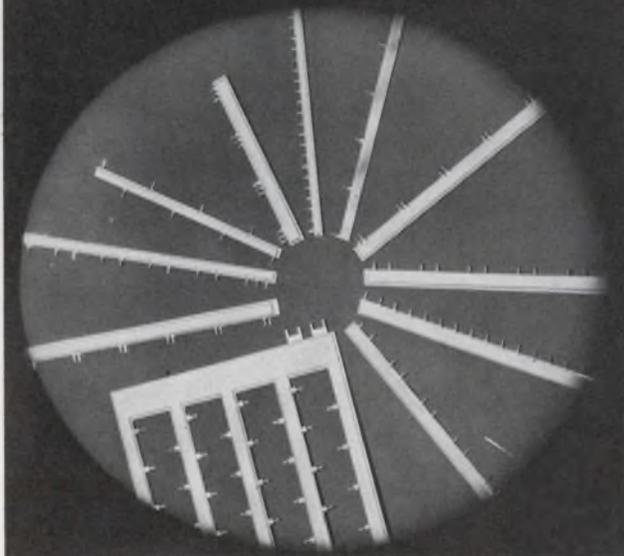
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ELECTRONIC DESIGN 15, July 19, 1974



\$395



\$445

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## OmniScribe™ Strip Chart Recorders

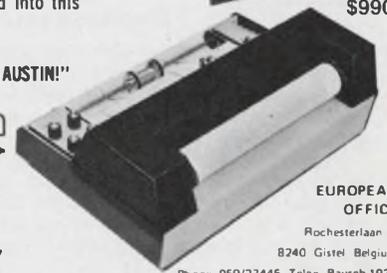
Here are five versions of the **OmniScribe™** 10 inch strip chart recorder. They're just a sample of the more than a score of possible combinations of speeds, spans, accessories and other goodies designed into this beautiful little unit.

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INFORMATION RETRIEVAL NUMBER 102

147

**2-wire data modem**

An eight-page brochure describes the VA-3400—a modem which provides full duplex data transmission at 1200 bits per second on dial-up or two-wire leased lines. The Vadec Corp., Mountain View, Calif.

CIRCLE NO. 336

**Optical communications**

"Optical Communications: Their Present and Their Promise" is a brief, nontechnical overview of the technology of communicating on beams of light using glass optical waveguides. Corning Glass Works, Corning, N.Y.

CIRCLE NO. 337

**RFI/EMC products**

Instruments, components and accessories for the RFI/EMC engineer are described in a 38-page catalog. The catalog includes not only performance specs, but application notes with test setup diagrams and an EMI prediction graph for rectangular and trapezoidal pulse interference. Solar Electronics, Hollywood, Calif.

CIRCLE NO. 338

**CATV amplifiers**

CATV hybrid amplifiers and discrete transistors are described in an eight-page catalog. Photographs and dimensional drawings are presented. TRW Semiconductor, Lawndale, Calif.

CIRCLE NO. 339

**Gallium phosphide**

Photographs of single and polycrystalline gallium phosphide as well as the equipment used to produce it are shown in a six-page foldout. Image Analysing Computers, Monsey, N.Y.

CIRCLE NO. 340

**IC logic boards**

A 16-page catalog on standard and custom integrated circuit logic boards describes six standard series of 1/8-in. thick epoxy glass boards with wire-wrappable socket terminals. TRW/Cinch Connectors, Elk Grove Village, Ill.

CIRCLE NO. 341

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INFORMATION RETRIEVAL NUMBER 104

# bulletin board

A nationwide, direct dial "hot line" for information on liquid inert test media is now in operation, sponsored by 3M's Commercial Chemical division. Called ALERT (Assistance for Liquid Electronic Reliability Testing), the service functions as a clearinghouse for data on Fluorinert electronic liquids. The number is (612) 733-6282.

CIRCLE NO. 342

A phase-loss and phase-sequence sensor for use with auxiliary power generating systems, either portable or permanent—operating from 110 to 480 V—has been introduced by Logitek.

CIRCLE NO. 343

Engineering Index has introduced a computer-readable data base, COMPENDEX, through on-line access. COMPENDEX provides abstracts/bibliographic citations, covering worldwide developments in all fields of engineering.

CIRCLE NO. 344

Current capabilities of 300 mA per driver and output voltages of up to 40 V are provided by the series SG55450B/75450B and SG-55460/75460 high-speed dual-peripheral-driver ICs available from Silicon General.

CIRCLE NO. 345

Interactive time-sharing software is available at Remote Computing Corp. for generating plots on either the CalComp 910-1136 drum plotter at the company's data center or any Zeta terminal-connected plotter at a user's location.

CIRCLE NO. 346

HP-developed software now enables users to convert and run existing IBM 1130 Fortran programs directly on the multiterminal Hewlett-Packard 3000 series computers. Conversion of an 1130 Fortran program can be completed in a matter of minutes, according to HP. The software is also useful in converting IBM 1800 Fortran programs.

CIRCLE NO. 347

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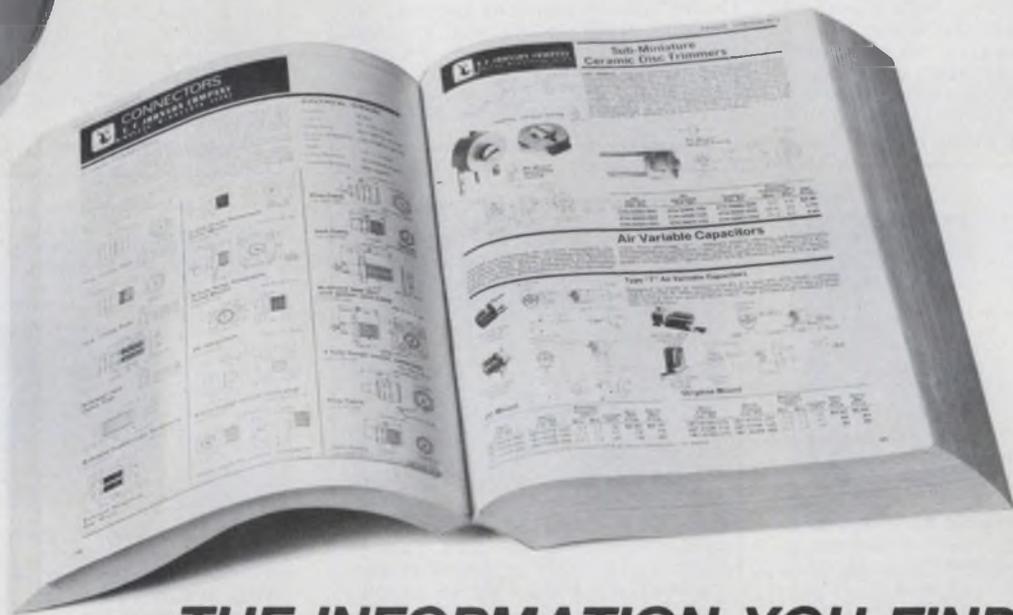
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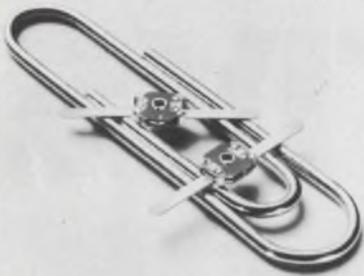
And the Directories — they're the most complete and comprehensive, the most thorough and useful reference sources ever compiled. Almost 7,500 manufacturers are listed with *complete* address, zip and phone. In most cases (where applicable) you also get 800 (toll-free) numbers, Telex, TWX, cable address, facsimile equipment with make and number, plus QPL and FSC designations, financial data and names of key officers.

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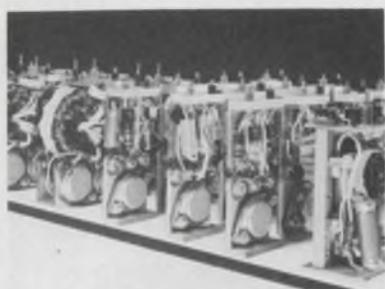
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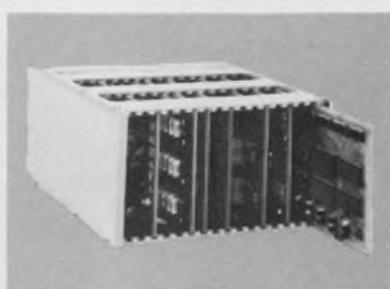
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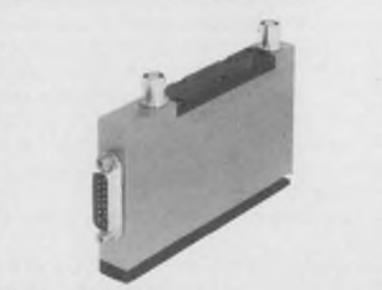
**Solid-State Voice Systems** for audio readout of numbers and words. Whole-words are stored in ROMs with natural sounding voice reproduction. Standard models offer 10 numeric words (0 - 9). Master Specialties, 1640 Monrovia, Costa Mesa, Calif. 92627. (714) 642-2427.

INFORMATION RETRIEVAL NUMBER 186



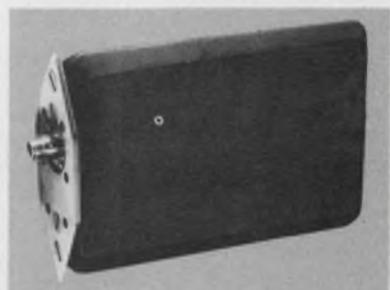
**AMP Capatron offers a complete line of quality data entry products.** From card reader/scanners to matrix badge readers. From tab and credit to magnetic and embossed card readers. All that makes it virtually certain we have what you need. AMP Incorporated, Capatron Division, Elizabethtown, Pa. 17022. (717) 367-1105.

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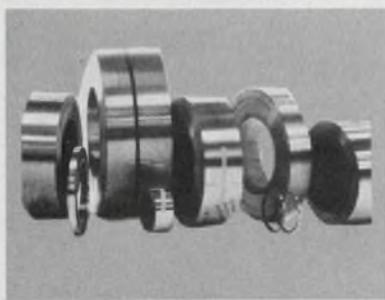
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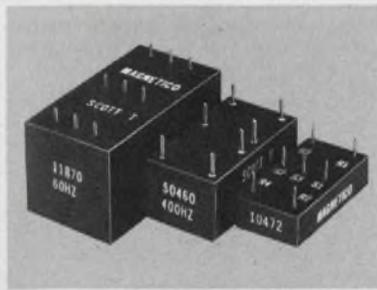
**"VLF to HF ACTIVE AIRBORNE ANTENNA** provides highly efficient reception for Omega, Loran C and Communication applications. Operating frequency is 10 KHz to 30 MHz with a 50 ohm constant output impedance." BAYSHORE SYSTEMS, Springfield, Va.

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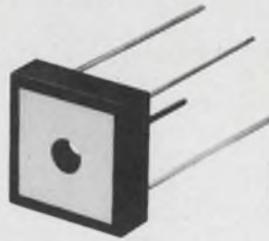
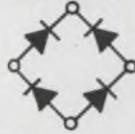
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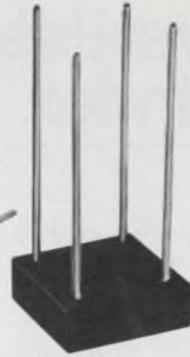


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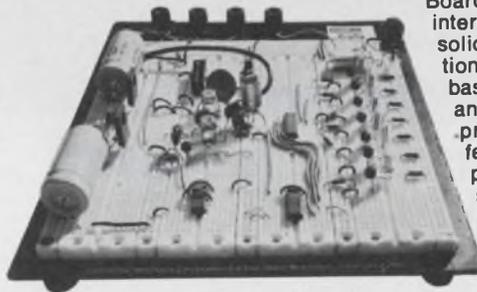
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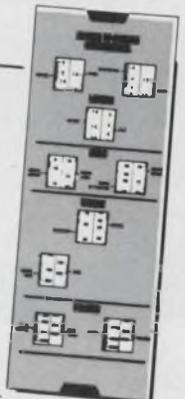


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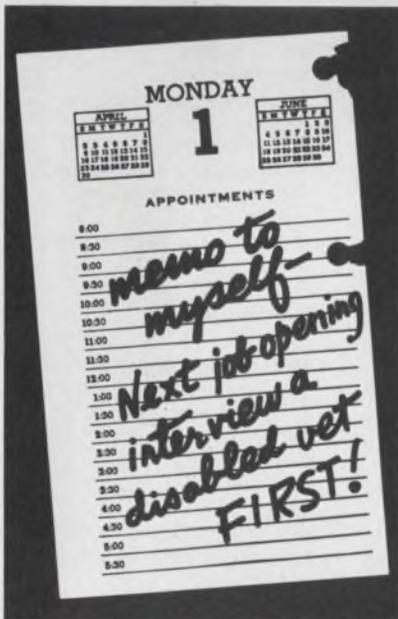
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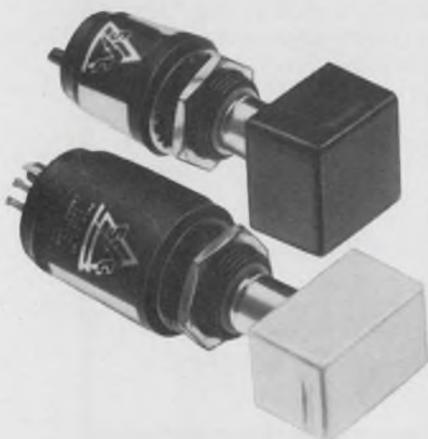
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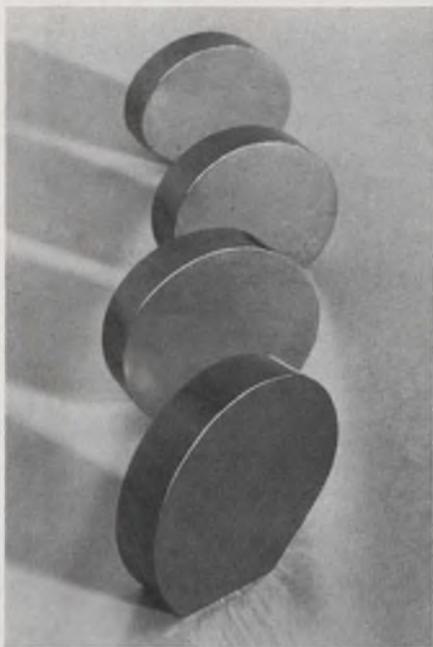
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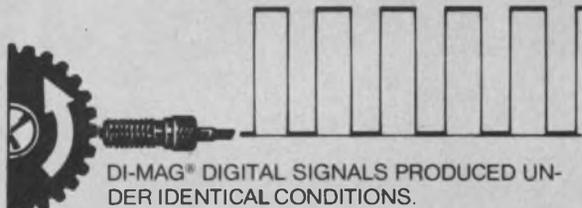
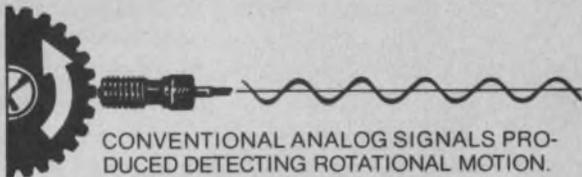
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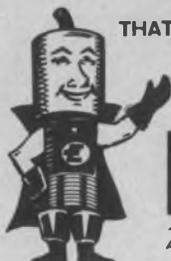


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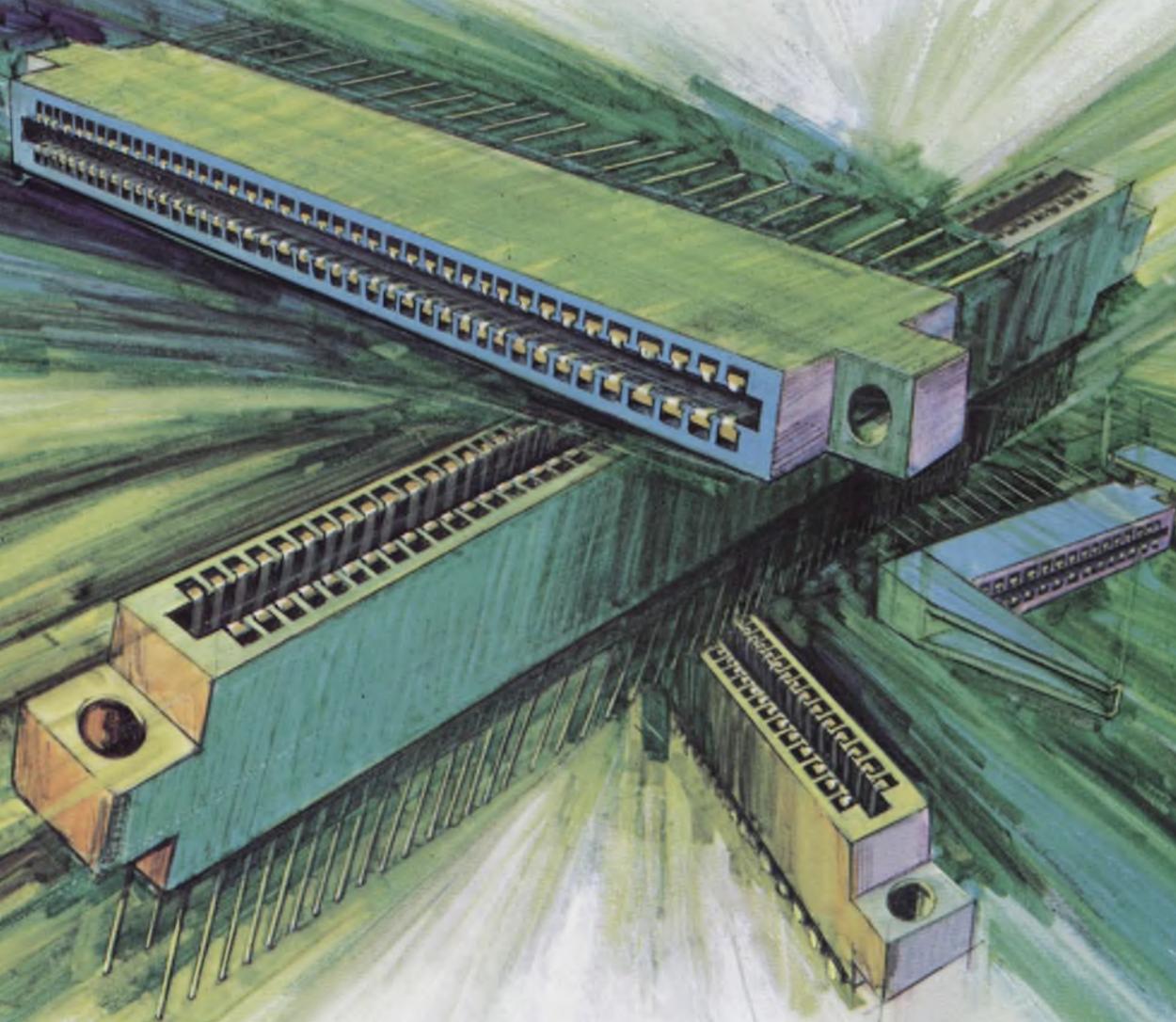
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ELECTRONIC DESIGN 15, July 19, 1974

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