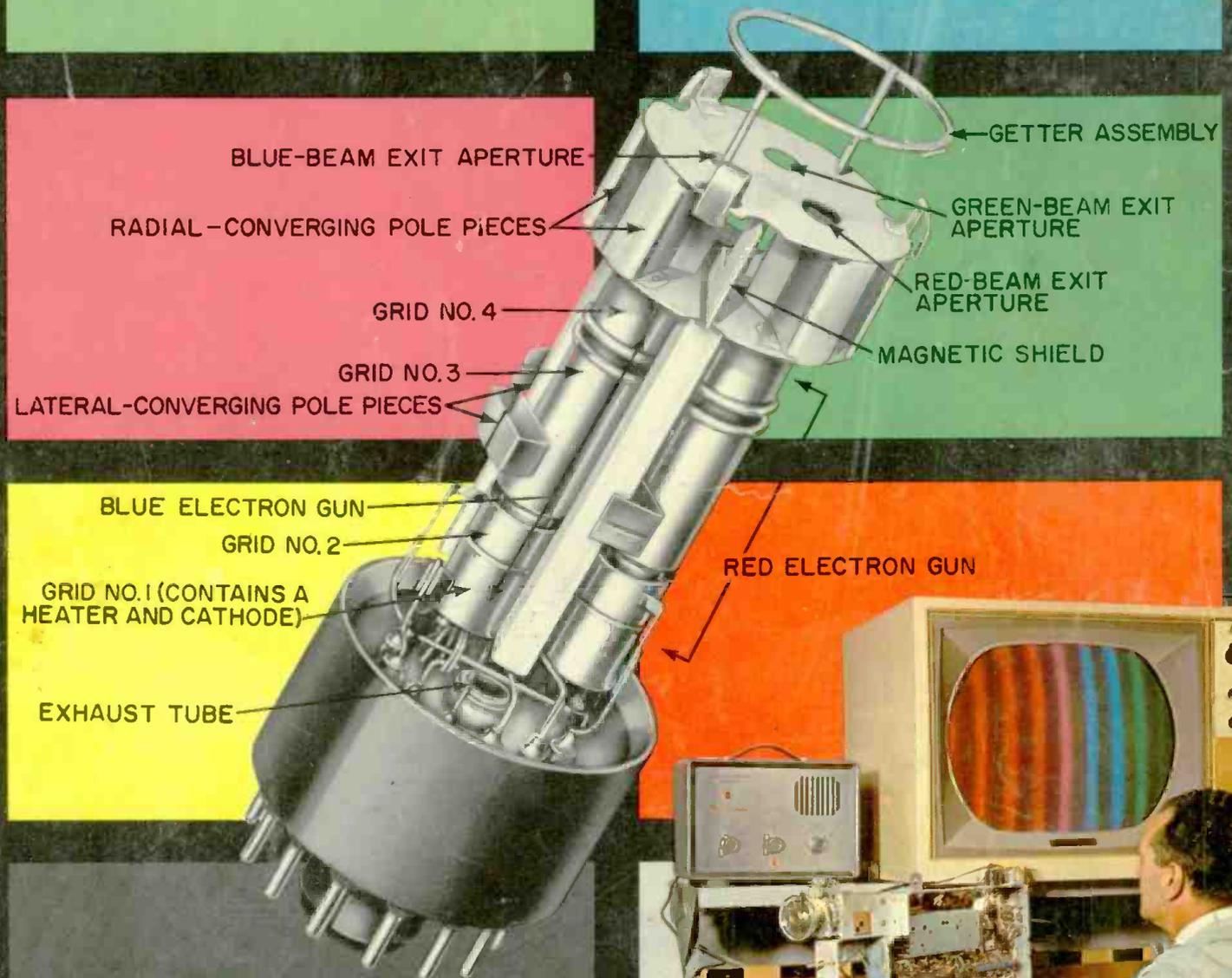


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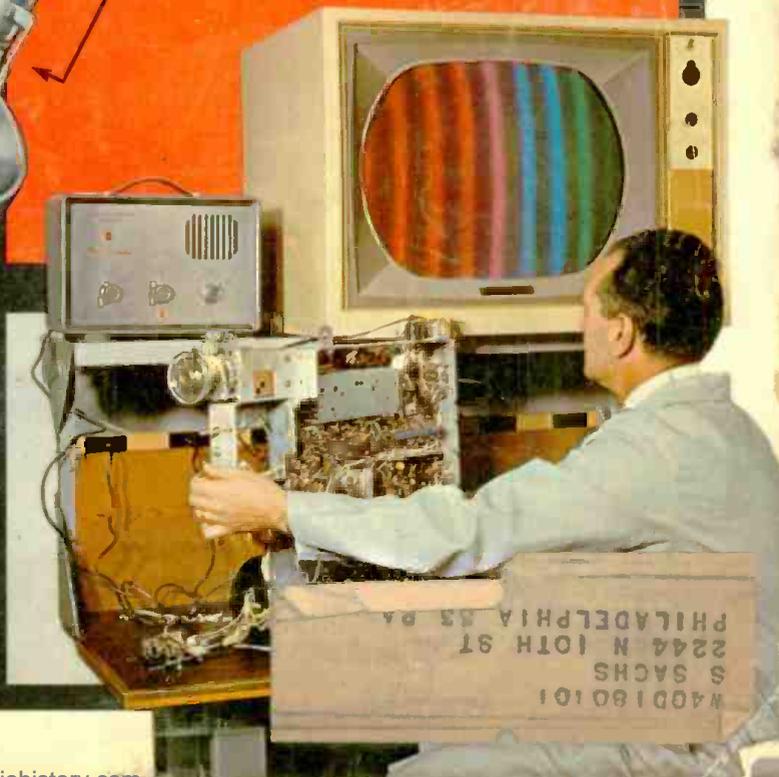
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## COVER STORY

(See Page 43)



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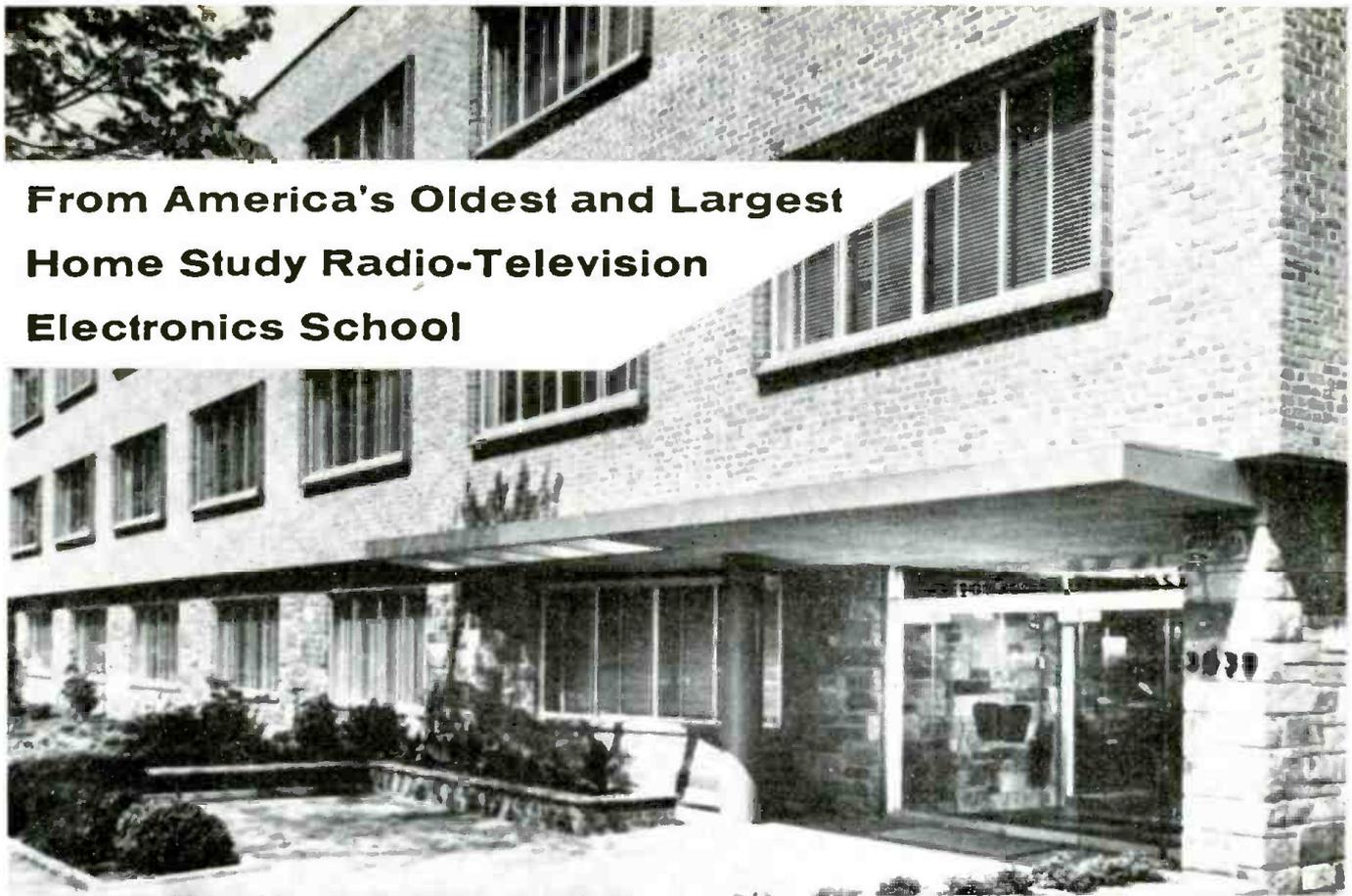
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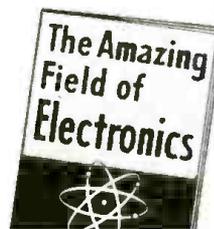
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## CONTENTS

### INDUSTRIAL AND GENERAL ELECTRONICS

Electronics for the Jet Age (Editorial)	W. A. Stocklin	6
Third-Quarter Component Output Declines		8
Spot News	Washington Correspondent	24
Tape Recording in Industrial Instrumentation	Ray A. Shiver & William Stillwell	61
Recent Developments in Electronics		76
Calendar of Events		86
Electronic Crosswords	Bruce Balk	117

### HIGH FIDELITY AND AUDIO

High-Quality T.R.F. AM Tuner	John Potter Shields	36
A Dimension Control for Stereo	Ralph Glasgal	56
Four-Track Tape System (Part 2—Playback Preamps)	Kenneth F. Buegel	58
Hi-Fi—Audio Product Review		66
Sound on Tape	Bert Whyte	82
Product Test Report (Harman-Kardon "Citation IV"; Channel Master CM-10 Speaker System; Pickering Model 381A Stereo Cartridge) EW Lab Tested		92
Hum Elimination	Charles E. Diehl	106

### SERVICING — TV, RADIO, ETC.

Color TV Service Today	Charles Tepfer	29
Home-Call TV Diagnosis	Walter H. Buchsbaum	33
Interference Tough Dogs	George P. Oberlo	40
Making Colors Electronically (Cover Story)		43
Tube Inventory for Service Shops	Robert A. Larsen	46
Diodes are Different	J. H. Hazlehurst	50
Understanding the Balance Sheet	John E. Flippin	52
New Products for the Radio and TV Service Technician		54
Mac's Service Shop	John T. Frye	60
Service Industry News		88
Voltage Regulator Diode-Tube Combinations	Dave Stone	104
Service Notes		122

### TEST EQUIPMENT

Simple Electronic Engine Analyzer	R. A. Lebowitz & R. M. Sonkin	38
Simple Crystal Mixer	Jennings David	85

### COMMUNICATIONS AND AMATEUR

Speech Clipper For CB Transceiver	Irving Krause & Gerald Wilner	32
Adjusting Communications Transmitters (Part 2)	Edward M. Noll	44
Changes in WWV Standard Broadcasts		51
Product Test Report (Eico Model 723 Amateur Transmitter Kit) EW Lab Tested		96
New Products for CB-Amateur and Communications		124

### ELECTRONIC CONSTRUCTION

TV Commercial Silencer	Robert J. Mack	48
------------------------	----------------	----

(For information on Next Month's Features, see page 8)

### DEPARTMENTS

Letters from Our Readers	12	Technical Books	102
Within the Industry	20	Manufacturers' Literature	108

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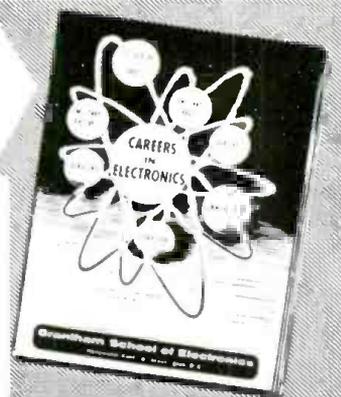
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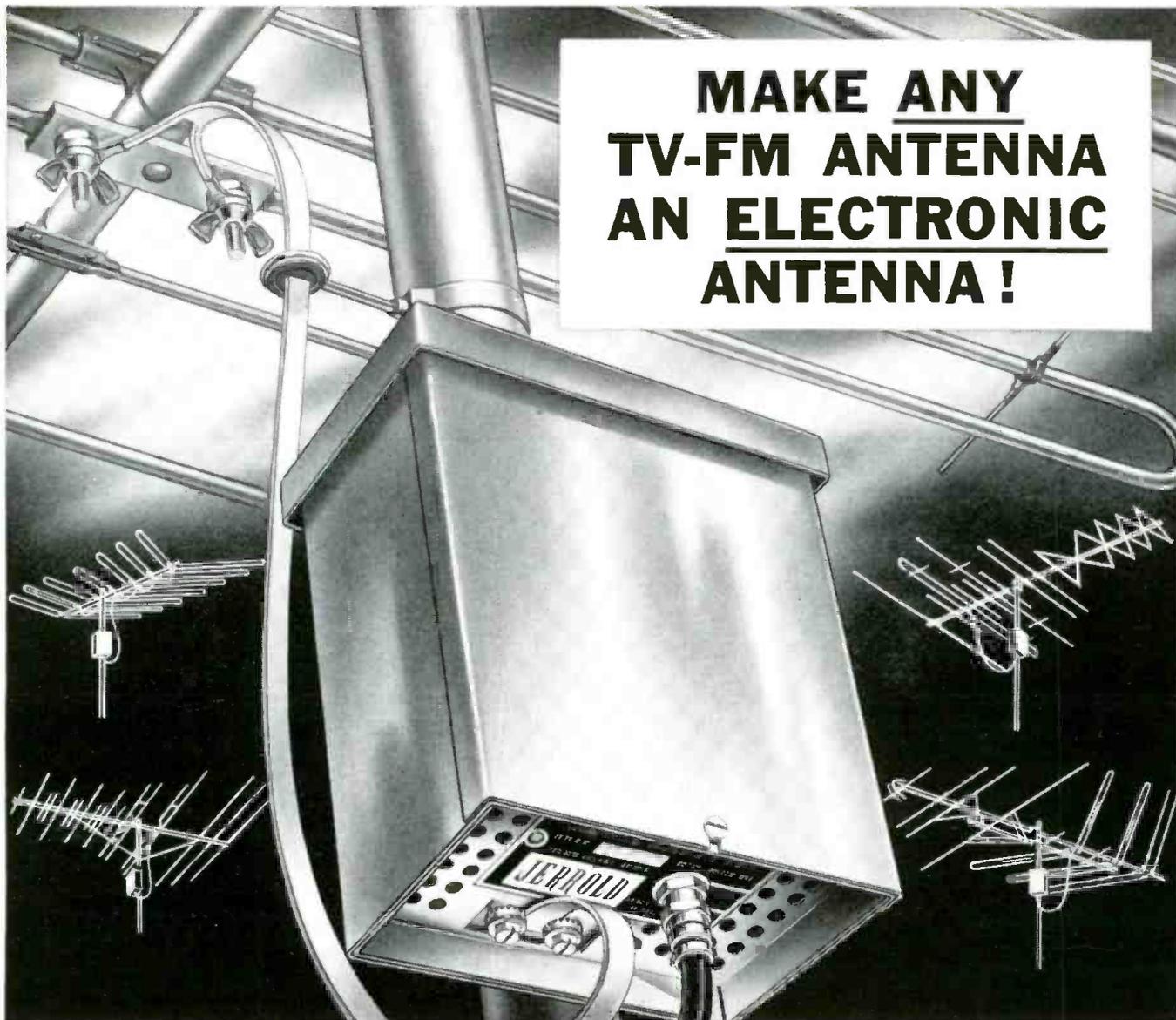
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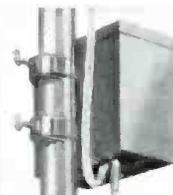


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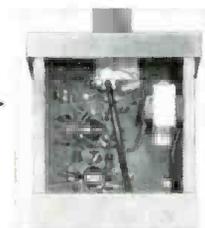


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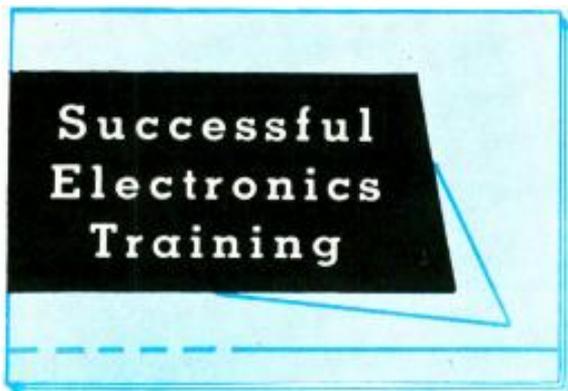
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## ...for the Record

By **W. A. STOCKLIN**  
Editor

### Electronics for the Jet Age

**A**LTHOUGH the precise cause of the mid-air collision over New York City last December has not yet been determined, and may never be, it is the first air tragedy in which an electronic device proved to be the mute witness. Today Federal regulations require that all aircraft capable of flying at altitudes above 25,000 feet carry a flight recorder.

In size, the flight recorder is comparatively small in relation to other electronic equipment aboard an aircraft. Its outside dimensions are approximately 20" x 8" x 6". Basically, it is an airborne oscillographic-type scribe (manufactured by *Waste King Corporation*) which provides a record of four in-flight parameters: altitude, air speed, heading, and vertical acceleration. This information is etched by a diamond stylus on a nickel-alloy tape. The unit is designed to survive heat of 2000 degrees F, a shock more than 100 times the force of gravity, and immersion in sea water for more than 36 hours.

Only one of the two planes involved in the New York City collision carried such a recorder—the jet which landed in a Brooklyn street. Despite the impact of the crash and the tremendous temperatures of the burning aircraft, the recorder was obviously recovered intact since investigators were able to study the flight path and the last minutes of the staggering, twirling aircraft as it hurtled from the sky. The recorded information is expected to play a vital role in determining just why the two aircraft collided while under the control and direction of the FAA air-traffic controllers.

Of importance not only in the case of collision, the flight recorders are being used by airlines to determine operation of aircraft at given altitudes and the response of their instruments to the ground navigational systems.

The flight recorder is, without question, a significant electronic contribution to aviation safety and all of us in the electronics industry have a right to be proud not only of this new development but of communications and landing systems that have been developed by our industry for the aviation field.

Obviously our industry cannot rest on its laurels since there is a dire need, in view of the coming jet age, for much improved electronic equipment—to reduce to an absolute minimum the possibility of human error.

We don't pretend, in this brief discussion, to offer a "solution" to our complex air-traffic-control problem—that we leave to the air-traffic-control experts.

But we would like to raise a few

questions. Air-traffic controllers at the New York Air Traffic Control Center work an eight-hour tour of duty, without a specified time for lunch. Aviation experts observing this unusual personnel practice concede that the controllers are doing an excellent job but question whether the average annual salary of \$6000 is commensurate with their responsibilities. They point out that higher salaries would attract men with a stronger electronic background which is certainly requisite in the jet age.

This recommendation appears to be in line with the philosophy of the new FAA administrator, Najeeb Halaby, who said "we should have more electronic controls so that everyone can fly safer." Mr. Halaby, a pilot-lawyer, is credited with making the first non-stop continental flight by jet in 1945 while serving as a Navy test pilot.

All of which puts the problem right back in our "electronic lap." Mr. Halaby, it appears, has pointed up our sins of omission.

The FAA's air-traffic-control system is using the same electronic equipment today as they used twenty years ago to guide and direct two-engined propeller craft whose top speed was not in excess of 200 mph. At this writing that same system, with slight modifications, is guiding and directing high-speed jet aircraft at more than 500 mph! It is almost like trying to meld horse-drawn vehicles into the traffic pattern of a high-speed turnpike.

In short, the present control system is incompatible with jet speed and inadequate for the supersonic aircraft which is expected by 1970.

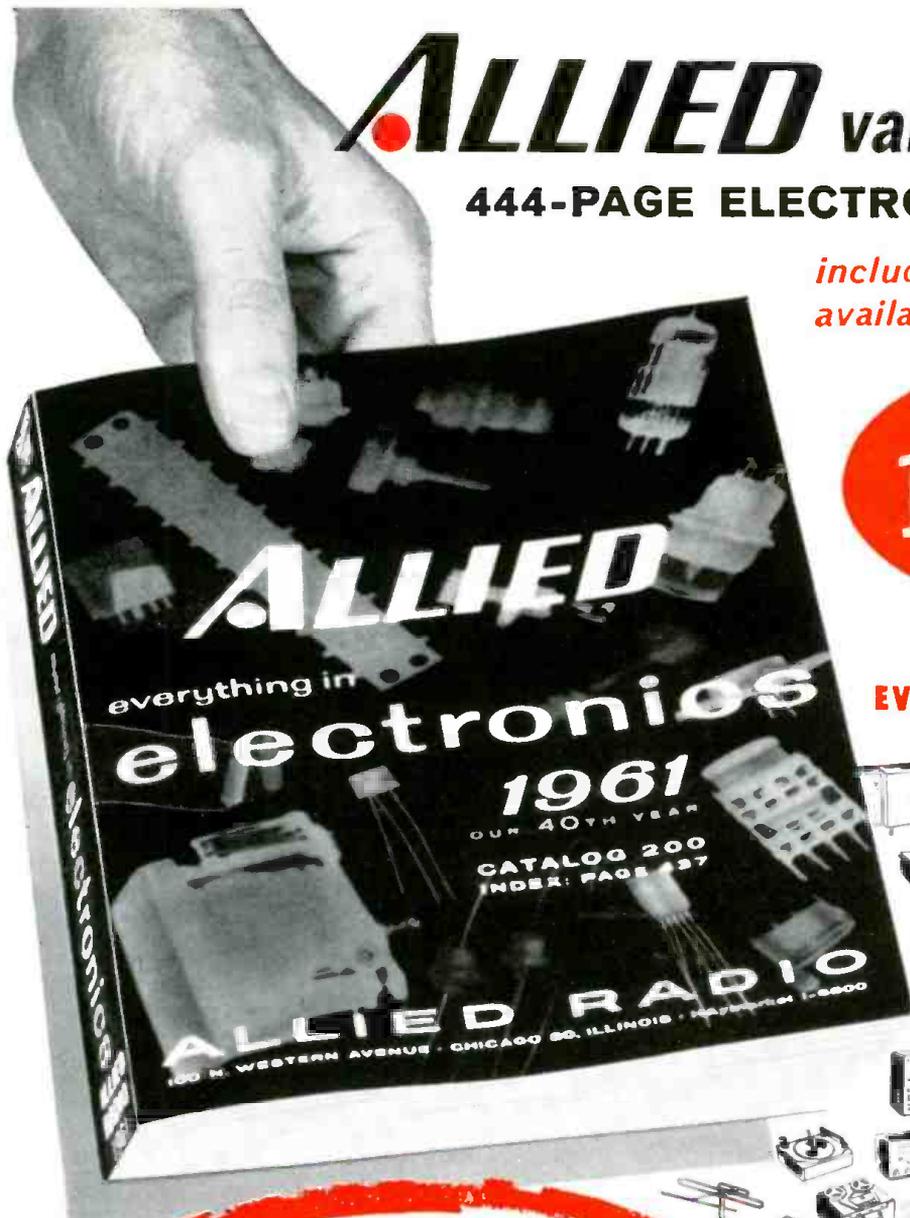
While no one can fail to be impressed by the achievements of the electronics industry in the field of missiles and space, its failure to provide the tools for the vital and immediate needs of air-traffic control cannot be overlooked. Such equipment is as important to the air traveller as the block-signal system is to the railroad passenger. We are told that three-dimensional radar is vital in high-density traffic areas such as New York, Chicago, and Los Angeles. Despite this urgency, such 3D radar is still in the "development" stage and the various types of computers to assist the air-traffic controller in handling the traffic load are "under test and experimentation."

The computers are scheduled for trial installation in the Boston Air Route Traffic Control Center later this year. Three-dimensional radar now undergoing test, even if proved successful, could not become operational before 1964 at the earliest.

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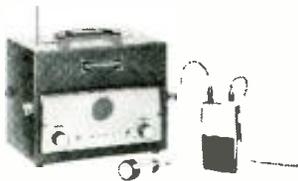
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tools for air-traffic control? Have we in the electronics industry failed to live up to our potential in this area or has the government failed to provide the necessary guidance and incentive? —30—

## THIRD-QUARTER COMPONENT OUTPUT DECLINES

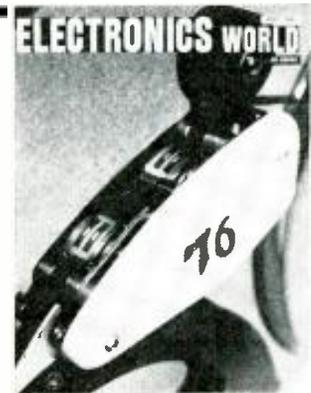
According to the U.S. Department of Commerce, shipments of electronic components declined approximately 5% during the third quarter of 1960. Most of the decline can be charged to components shipped for military

end-use although the report pointed out that non-military component output failed to show the normal upward movement during the latter half of the year. Following are details on unit and dollar value production. —30—

COMPONENT	UNITS	VALUE
Power and Special Purpose Tubes	2,661,000	\$ 58,728,000
Receiving Tubes	103,221,000	\$ 87,244,000
Semiconductor Devices	81,925,000	\$126,583,000
Capacitors	338,408,000	\$ 61,368,000
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### 4-TRACK STEREO ADDS DEPTH TO TAPES

Two-dimensional stereo can be achieved with 4-channel, 4-track tapes. Here is how such a system can be set up, including details on the requisite transistorized playback and record amplifiers.

### 1961 AUTO RADIOS: GM CARS

Practical and often hard-to-get information for the service technician on sets used in 1961 Chevrolets, Pontiacs, and Oldsmobiles.

### RUMBLE FILTERS FOR STEREO

Improve the quality of record reproduction by designing and building a rumble filter for stereo setups. All the necessary information, as well as practical examples, is included.

### SPEED-CHECKING I.F. SYSTEMS

Although i.f. systems are seldom the culprit, when they need to be checked, use this system to save trouble and time.

### SALVAGING "DO-IT-YOURSELF" JBBS

Nothing can be more time-consuming than a service job which the owner has "started"—often producing misleading

symptoms. Here's a practical system for coping with these "home-butchered" receivers.

### COMPUTER ARITHMETIC CIRCUITS

A basic discussion of the various types of adders used in binary systems.

### WIDE-RANGE INDUCTANCE METER

A simple, single-tube tester which will measure inductance values from 2.5  $\mu$ h. to 6300 h. It is designed to be used in conjunction with external generator and output meter to keep cost down.

### LIGHTNING PROTECTION FOR HAM STATIONS

Since lightning annually takes a larger toll of lives than either hurricanes or tornadoes, lightning protection for the ham station is a "must." The author provides practical tips and procedures.

All these and many more interesting and informative articles will be yours in the May issue of *ELECTRONICS WORLD* . . . on sale

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# IT COULD HAPPEN TO YOU...



Somewhere it said: "Build this kit in an amazing 10 hours!" Looks like you're running into overtime because you spent the first 7½ hours sorting out the jumbled mess of small parts and hardware. Well, it's good training for looking for needles in haystacks.



If drug manufacturers made the mistakes in labeling you find in some kits, the world would be a quieter, lonelier place. You know a selenium rectifier when you see one, and if this is a selenium rectifier, you're Thomas Alva Edison.

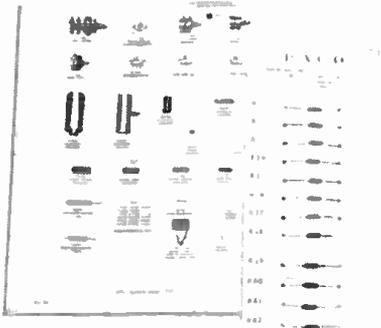


Let's see. On Page 5 it says; "See diagram Page 12." On Page 12 it says; "See instructions Page 5." Well, if you hold Page 5 open with your tongue, and Page 12 open with your left ear, that still leaves you three fingers on your left hand free for soldering and also...



Don't look now, but while Heifetz fiddles, your amplifier burns. When the smoke clears, you'll probably find that the 100 microfarad electrolytic was shorted because it had not been pre-tested. All work and no play, makes Jack a very mad boy!

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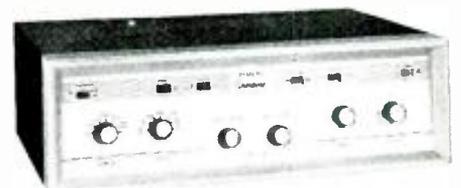
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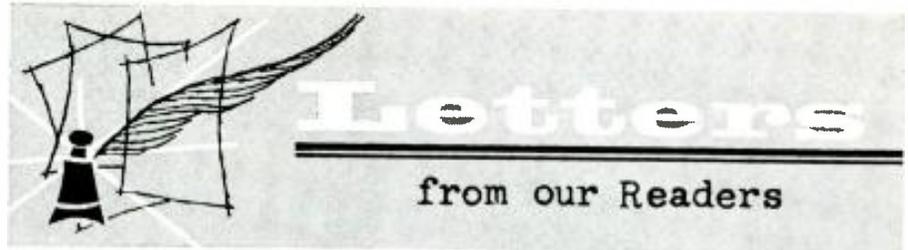
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**AUDIO-ULTRASONIC PICKUP**

To the Editors:

In the October, 1960 issue of *ELECTRONICS WORLD* is published an article titled "Audio-Ultrasonic Pickup Circuit" by Mr. Harold Reed.

This article covers construction of a transistorized voice-operated relay. The printed material and the wiring diagram shown in the article call for a 22.5-volt battery.

We are in process of building this unit. Having secured the specified G-E 2N107 transistors we note that the manufacturer specified a *maximum* voltage of -10 volts. Your article calls for -22.5 volts input.

Will you please check these contradictory specifications and give us the correct answer?

PHILIP A. BOERNER  
Tydings Electronics, Inc.  
Pittsburgh, Penna.

*Here are Author Reed's comments on the above question.—Editors.*

Dear Mr. Boerner:

You are right about the d.c. voltage being above the rating for the 2N107. Two circuits were set up here, one with CK722 transistors using a 22½-volt battery and the other with the 2N107 using a 9-volt battery. The 2N107 circuit was given in the article since it seemed to be more stable. The battery used with the CK722 was erroneously listed on the 2N107 diagram.

After receiving your letter I was naturally concerned about other constructors who may not notice this as you did so I made tests on the circuit as given in the article, using the 22½-volt battery. The maximum collector-base voltage listed by G-E for the 2N107 is 12 volts. In this circuit it measured 20 volts. Several transistors were tried for prolonged periods with no ill effects. This agrees with past experience in that I never lost a transistor due to exceeding, within reason, the maximum collector rating (usually accidentally) as long as the dissipation rating was not exceeded.

The constructor who uses the circuit as is, will probably experience no difficulty. Since you are in the process of building the unit, use a 22½-volt battery with transistors like the CK722 and a 9-volt battery with the 2N107.

HAROLD REED  
Hyattsville, Maryland

**THE TRANSISTOR "ALPHA BOX"**

To the Editors:

In Fig. 1 of my article "The Transistor 'Alpha Box'" which appeared in the November issue, transistor V<sub>1</sub> (2N293)

should be drawn as an *n-p-n* type rather than a *p-n-p*, as shown.

DON STONER  
Alta Loma, California

*We are sorry we couldn't catch this correction before we went to press. The circuit still operates just as indicated by the article, however.—Editors.*

\* \* \*

**HI-FI RECORD CHANGERS**

To the Editors:

In your article "Hi-Fi Record Changers" (*ELECTRONICS WORLD*, December 1960) relative to intermixing records, it is stated, "Of course, in all instances, the stack must be made up of records of the same speed."

I believe you will find that on *Webcor* models incorporating the "Magic Mind" (Models 141A, 1631A, 1641A, and others) seven-inch 45-rpm records and ten- or twelve-inch 33½-rpm records can be intermixed, and the changer will shift to the appropriate speed as each record is dropped.

JOHN E. HANNAN  
Plumb Electronics  
Houston, Texas

*In addition to the Webcor models indicated above, Glaser-Steers and Heath also have changers available with this same speed-changing function.—Editors.*

\* \* \*

**SENSITIVE ELECTRONIC RELAY**

To the Editors:

I have just finished building the electronic relay described in the January edition of *ELECTRONICS WORLD* and find it extremely sensitive. Sensitivity may be adjusted to maximum by adding a 3000-ohm, 4-watt potentiometer in series with R<sub>1</sub> and ground.

Your readers may be interested to know the relay makes an excellent "wet-the-bed" alarm for very young children.

L. PARKER  
Pickering, Ontario

To the Editors:

The electronic relay described on page 62 of your January, 1961 issue could easily be a lethal gadget since not only the chassis but also one of the control elements is connected directly to one side of the a.c. line. In one position of the a.c. plug this would mean that anyone touching one of the control elements and a ground such as a radiator, water pipe, furnace register, etc. would be subjected to full line voltage. The same device can be built at practically the same cost complete with a transformer supply, fuses, switch, enclosed cabinet, and a sensitivity control

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which would make it relatively safe, even for children. Most of your articles cover well-designed equipment which is reasonably safe to operate, but occasionally one is shown which is definitely unsafe. Too many people do not realize the danger present in those nice little bare wires and terminals under the chassis and poke around with soldering irons and screwdrivers among a maze of 200, 300, or more d.c. volts little realizing that 200 volts d.c. can be more deadly than a rattlesnake. Perhaps an article on electrical safety in some future issue would be in order.

I hope you will forgive the somber tone of this letter. In general, ELECTRONICS WORLD is a high-quality publication and has added to my education and enjoyment for many years. but, as an industrial engineer, I sometimes become concerned with the pictures and descriptions of seemingly innocent, but potentially deadly, a.c.-d.c. circuits, open chassis, etc.

K. C. McCARTT  
Senior Research Engineer  
Universal-Rundle Corporation  
Mahoningtown, Pa.

*We had hoped that by this time our readers should be pretty well aware of the dangers of working with electricity and in working with devices that do not use isolating transformers. We have run so many articles on the subject of safety, power-line hazards, the use of isolating transformers, and the use of polarized plugs, that we have lost count of them.*

*We do agree with you, however, that we should always be aware of the novice in the field who reads our articles, and that we should keep a strong emphasis on these warnings in any articles where they apply.*

*We would like to point out, however, that the article in question indicates at the very beginning of the circuit description that a polarized line plug should be used to reduce or eliminate danger of shock or short circuits. Perhaps we should have emphasized this very important matter even more.—Editors.*

\* \* \*  
**LINE-VOLTAGE ISOLATOR**

To the Editors:

With reference to your article "A Variable Line-Voltage Isolator" in your January issue, the output-outlet hookup isn't going to help the transformer as it is shown. In addition to this, there will be no output voltage as you have drawn the circuit.

W. GREEN  
Long Island City, New York

*Thanks to Reader Green for pointing out our oversight in the circuit. We were so concerned that the switch was hooked in right, that all of us who proofread the article neglected the very obvious short circuit across the outlet. If this lead is deleted, the circuit should then work properly as shown.—Editors.*

\* \* \*  
**FIVE-MINUTE CB TIMER**

To the Editors:

While I did not attempt to construct the "Five-Minute CB Timer" by Leo Morgan in your January issue, I did read the article with interest. That there is a five-minute time limit is news to me even though I am supposed to receive transmittal sheets from the FCC to keep me up to date.

I believe that you would do your readers a great service by printing an interpretation of the rules as they stand at this time.

FRANK W. KNOTTINGHAM  
Port Orford, Oregon

*The so-called five-minute rule on the Citizens Band has been covered by us in a brief one-column story that ran quite a few months ago. Briefly, the rule is that no contact should exceed five consecutive minutes and that this should be followed by a two-minute silent period. However, this rule does not apply to contacts between units of the same station, nor does it apply to emergency communications.*

*We refer you to paragraph 19.61 of the "FCC Rules and Regulations on Citizens Band" as amended March 15, 1960.—Editors.*



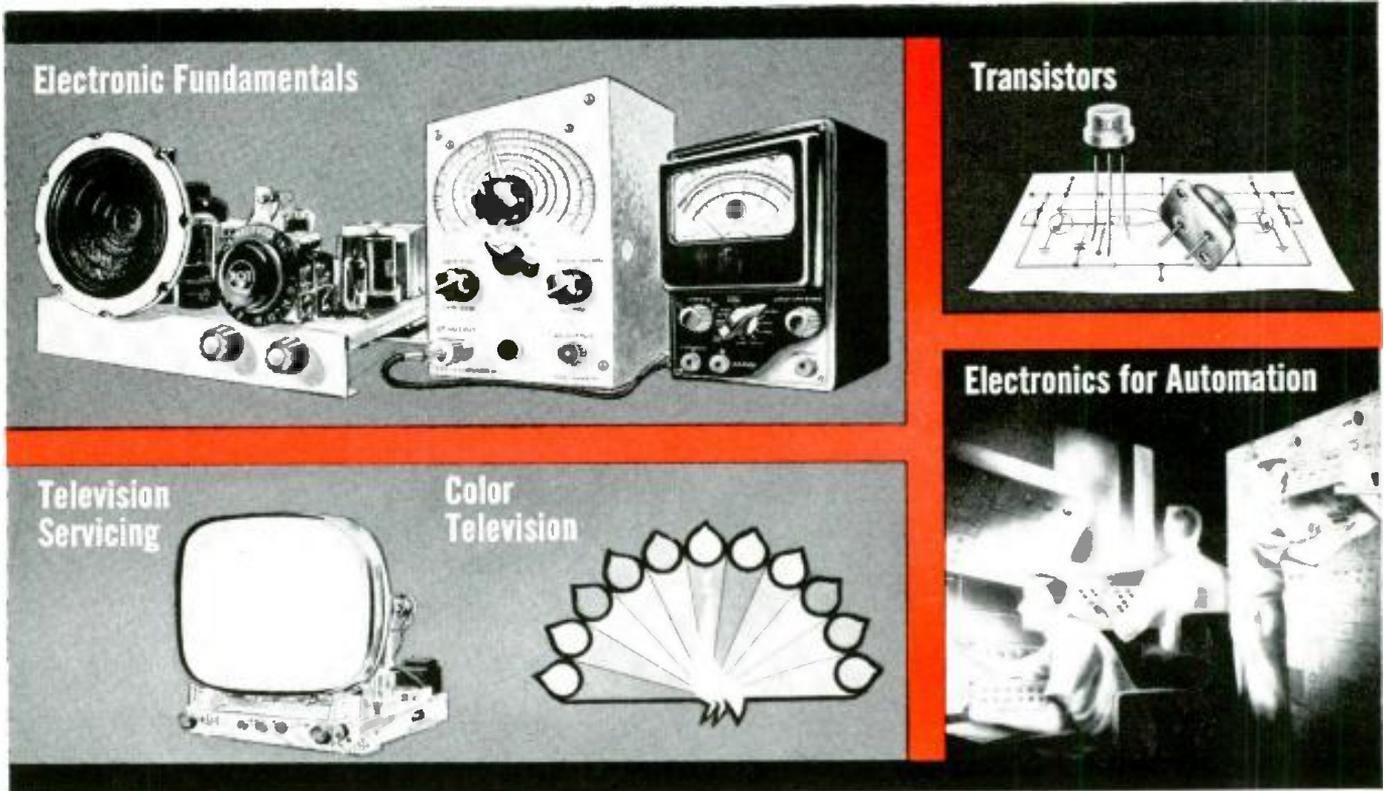
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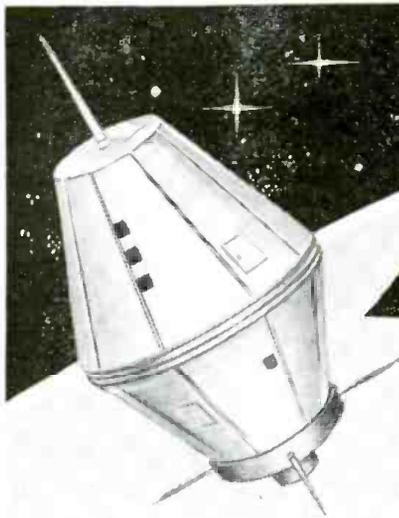
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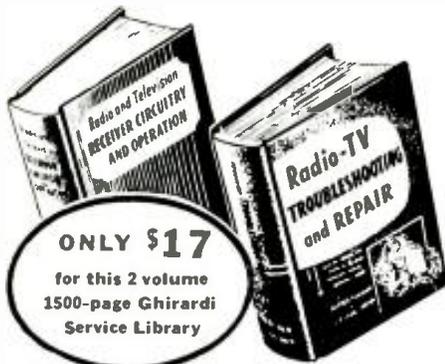


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# Within the Industry

WILL RAYMENT, president of *Sargent Rayment Co.*, has resigned his post to join the *Fisher Berkeley Corporation* as executive vice-president.



He joined *Sargent Rayment* in 1947 and served as chief engineer and general sales manager from 1950.

In his new job with the Emeryville, California manufacturer of intercoms and commercial sound systems, Mr. Rayment will concentrate on sales and the development of new products for industrial and commercial sound applications.

WESCON, the Western Electronic Show and Convention which will convene at the Cow Palace in San Francisco on August 22, 23, 24, 25, 1961, has named its principal executives for the 1961 show.

Albert J. Morris, of *Radiation at Stanford*, is chairman of the board while O. H. Brown, of *Eitel-McCullough*, will serve as chairman of the executive committee. Convention director is Dr. John V. N. Granger of *Granger Associates* and Calvin K. Townsend, of *Jennings Radio Corporation*, has been appointed show director.

Board members who will participate in the general policy of WESCON 1961 are Bruce S. Angwin of *General Electric*; Donald C. Duncan of *Duncan Electronics*; S. H. Bellue of *Osborne Electronic Corporation*; and Edward C. Bertolet of *Behlman Engineering*.

BERNARD REICH is now president of *Molecular Electronics Inc.*, a wholly owned subsidiary of *Precision Circuits, Inc.* . . . ROBERT E. MILLER has been elected to the new position of vice-president for advanced development by the board of directors of *Melpar, Inc.* . . . DR. GEORGE CARYOTAKIS is manager of the newly

formed high-power laboratory of *Eitel-McCullough*. . . CHARLES K. TITUS has joined the staff of the Communication and Data Processing Division of the *Collins Radio Company* as manager of the scientific analysis and programming department. . . PHILLIPS N. BUFORD has joined *Page Communications Engineers, Inc.*, a subsidiary of the *Northrop Corporation*, as senior staff engineer in the research and development directorate. . . JAMES K. DRAPER is now manager of engineering at *International Electric Industries, Inc.*, Nashville, Tenn. . . *Hollywood Radio and Electronics, Inc.* announces the election of DONALD AARONS as vice-president and member of the board. . . J. A. BRUSTMAN has been appointed manager, electronic system engineering of the Advanced Systems Development Engineering Activity, *RCA's Electronic Data Processing Division*. . . DR. WILLIAM O. BAKER, vice-president-research of *Bell Telephone Laboratories*, has been elected to the Board of Trustees of the Rockefeller Institute. . . *Essex Wire Corporation* announces three major executive appointments within its *Chicago Standard Transformer Division*: WILLIAM E. WILSON will be vice-president and general manager; JACK D. HALL will assume the duties of vice-president, sales and marketing; and KARL F. CREASE will be vice-president in charge of manufacturing. . . DR. TREVOR LAW, a former member of the technical staff at *Bell Labs*, has been named senior engineer of the materials department at *Motorola Semiconductor Products Division*. . . FRANK M. HICKEY is the new manager of industrial products sales for *CBS Electronics*. He was formerly merchandising manager of industrial products.

AUSTIN C. LESCARBOURA, who for the past 35 years has headed his own advertising agency, was recently tendered a dinner on the occasion of his 50th anniversary in the radio-electronic industry.

One of the wireless pioneers, he began his career as a ham in 1907. He served as assistant engineer for *Telefunken Wireless Telegraph Co.* and participated in some of the early wireless telephone demonstrations. He worked for *Electro Importing Co.*, a firm specializing in supplying the needs of the radio amateur. He was the editor of "Modern Electrics" and "The World's Advance" (now "Popular Science Monthly"), as well as managing editor of "Scientific American" from 1915-24.

He is the author of six books and innumerable articles in magazines, newspapers, and trade journals. He is a fellow of the Radio Club of America, a Senior Member of the IRE, as well as the recipient of an impressive number of honors.

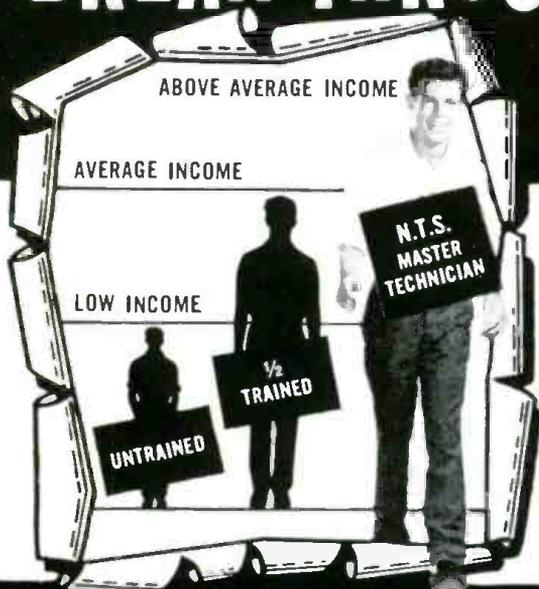
His many friends in the industry and ham fraternity join in wishing "A.C." a long and happy "retirement."

MOTOROLA INC. will move its corporate headquarters to its new administration building in Franklin Park, Illinois. The new \$7.5-million structure, at 9401 West Grand Ave., encompasses a total area

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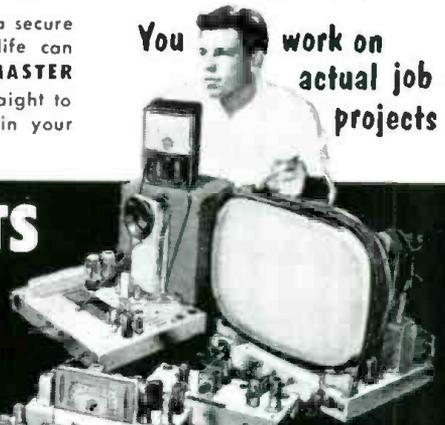
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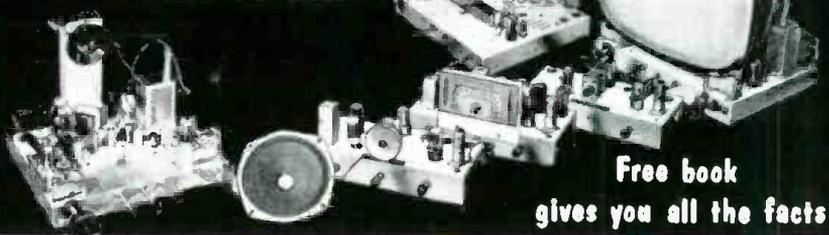
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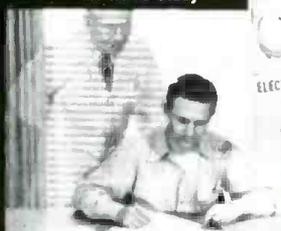
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of 327,148 square feet and has provision for the addition of a lightweight sixth floor to increase the usable area by as much as 52,000 square feet . . . **ROBERTS ELECTRONICS, INC.** of Los Angeles is erecting a new \$1-million, 50,000-square-foot plant at 5918 Bowercraft Ave. The building will house the company's administrative offices as well as engineering and warehousing facilities . . . **PEERLESS RADIO DISTRIBUTORS** has acquired a new building in Lynbrook, Long Island to house its industrial electronic sales division. The new building contains 25,000 square feet of office and warehouse space. . . **GENERAL INSTRUMENT CORPORATION** has opened its new \$3-million, 50,000-square-foot plant, devoted exclusively to the development and mass production of semiconductors, at Hicksville, N.Y. . . . **GENERAL ELECTRIC COMPANY** plans to spend more than \$1-million this year to enlarge its present communications products department headquarters at Lynchburg, Va. . . . **REMINGTON RAND's Univac** military department has selected Roseville, Minn. as the site of its new 130,000-square-foot building. Occupancy is slated for late this Spring . . . **HARMAN-KARDON, INC.** has moved from Westbury, Long Island to its new 52,000-square-foot high-fidelity equipment plant at Plainview, Long Island.

**ALBERT J. MORRIS** has been elected president of *Radiation at Stanford* which is a newly formed subsidiary of *Radiation Incorporated*. Previously, he was senior vice-president-engineering for the *Levinthal Electronic Products Corporation*.



Mr. Morris was named a director of WESCON in 1958 and became convention chairman the following year. This year he is chairman of the board for the 1961 WESCON show and convention. He is a past chairman of the San Francisco section of the IRE, and is currently a director and member of the IRE's Executive and Operating committees.

Prior to joining *Levinthal*, he was Research Associate (Electronics) for the U. S. Navy Office of Scientific Research in San Francisco.

**UTAH RADIO's** stock has been acquired by **SERRICK CORPORATION** of Defiance, Ohio. The purchase will facilitate the expansion of the company's facilities and products in both the industrial and distributor electronic markets. The corporate structure of the company will remain unchanged. . . . The name of the **MARION INSTRUMENT DIVISION** has been changed to **PRECISION METER DIVISION**. The name change was made to more clearly identify the division's product line . . . **LIONEL CORPORATION** has acquired **TELERAD MANUFACTURING COMPANY** of New York by purchasing the firm's authorized, but unissued, common stock. The new subsidiary will be (Continued on page 74)

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Latest Information

on the Electronic Industry

**Spot News**

By ELECTRONICS WORLD'S  
WASHINGTON CORRESPONDENT

**BRIGHT OUTLOOK SEEN FOR '61 INSTRUMENT SALES**—Sales of scientific and industrial instruments are expected to increase substantially in 1961, Washington reported recently. The sales surge is projected because of government outlays and spending by industry. About \$500-million has been budgeted for Federal research and facilities, with many of these dollars allocated for the purchase of meteorological, geophysical, and similar instruments for these laboratories. Industry is expected to up their purchases to about \$800-million, an increase of \$120-million over 1960.

**NAVY TO INSTALL 560,000-WATT SPACE SURVEILLANCE TRANSMITTER**—The gap in the Navy's silent satellite detection system, stretching across the southern part of the country, will be plugged by one of the world's most powerful transmitters—a 560,000-watt installation 35 miles southwest of Wichita Falls, Texas, near Archer City. Five times as effective as the largest television transmitter, signals will be fed into a nine-section antenna, each section measuring 576 feet long and 24 feet wide, so arranged that one can be operative without affecting the other.

**SATELLITE COMMUNICATIONS SHIP TO BE BUILT BY NAVY**—The Bureau of Ships is now designing and developing equipment for a shipboard satellite communications terminal capable of communicating with two Army shore stations through the "Advent" satellite. Aimed at creating a military capability for high-capacity, secure, world-wide instantaneous communications using high-altitude hovering satellites, "Advent" will receive and amplify signals received from the earth and re-transmit them to other earth-bound stations. Orbiting at an altitude of 22,000 statute miles over the equator, "Advent's" period will be 24 hours, just sufficient to keep it hovering over a fixed point on the earth. At this height, the single satellite will be in direct line-of-sight of all points on earth enclosed in a circle 11,300 miles in diameter, centered just beneath the satellite. Thus there will be no reason to store messages received on tape for later repetition as is done by the satellite "Courier." Messages received by "Advent" will be transmitted immediately and with extensive channel capacity.

**AIR FORCE TO ESTABLISH NEW COMMUNICATIONS SERVICE**—The Air Force will set up a new command on July 1st to be known as the Air Force Communications Service. Headquartered at Scott Air Force Base, Illinois, the new command will be responsible for the operation and maintenance of all Air Force telecommunications point-to-point and air-to-ground on a global basis, including operation of Air Force terminal and en-route navigation aids.

**FCC ISSUES EXPERIMENTAL GRANT TO BOUNCE SIGNALS OFF MOON**—The Commission recently authorized ITT to build an experimental station to bounce signals off the moon and passive (non-radio-equipped) earth satellites for basic research and study of space communications theory. The grant, for but one year, specifies operation on 2120 mc. or 2299.5 mc. until July 1, after which only 2299.5 mc. may be used. The station, which will be in Nutley, N.J., will use input power of 10 kw. to a 40-foot steerable antenna for directing narrow-band transmission space-ward. The reflected signals will be received by the same station. See page 77 for photo.

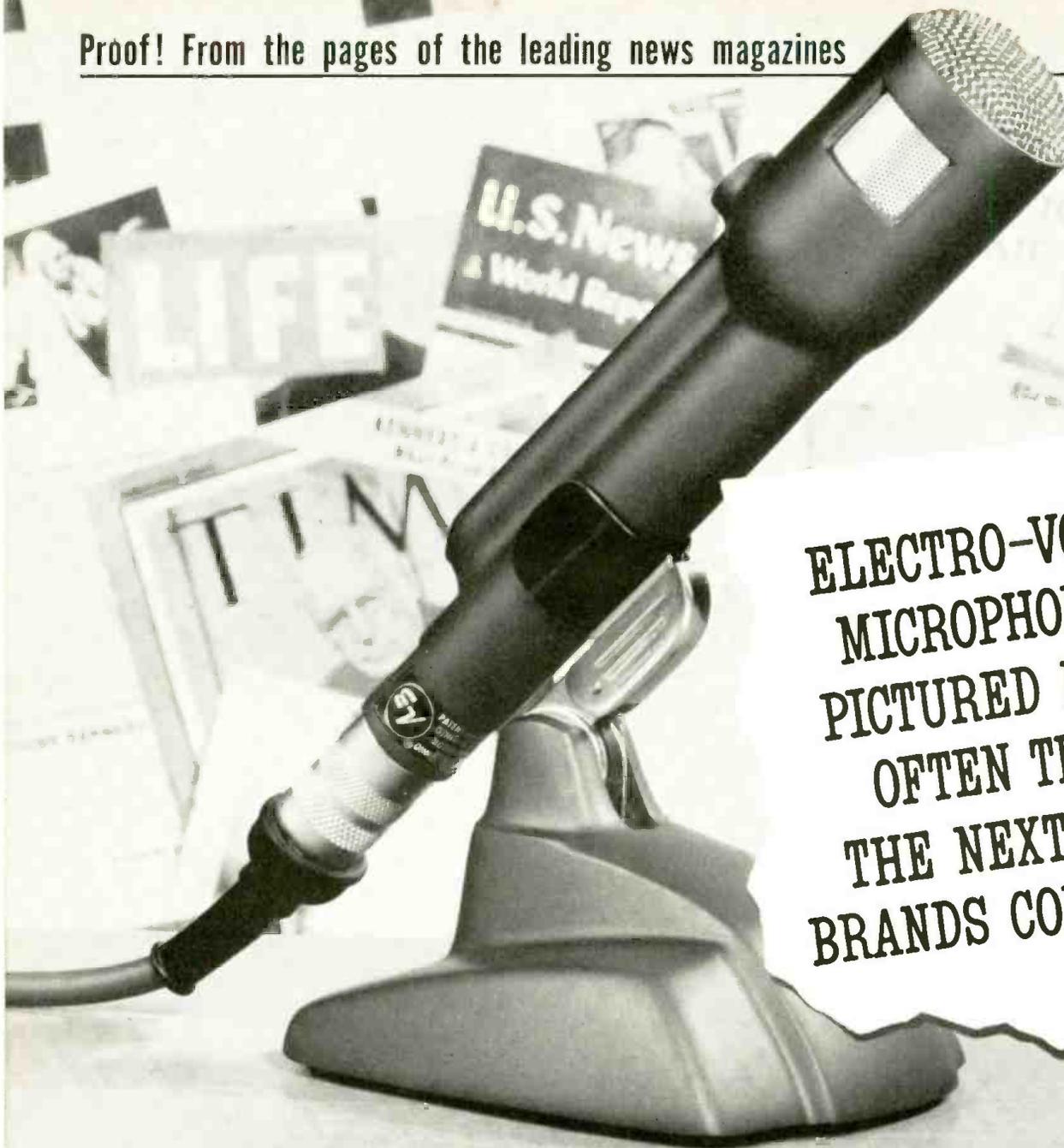
**ARMY MOBILE DIGITAL COMPUTER NOW IN EUROPE**—The Army's first operational mobile digital computer (MOBIDIC), a large-scale unit designed for field combat use, has been moved in three 30-foot trailers from the Brooklyn Army Terminal to the Seventh Army in Europe. After arrival at the French port of St. Nazaire, the vans were driven across France to NATO quarters at Zweibrucken, West Germany, the Army's stock-control center. Here, the computer will serve to control thousands of supply requisitions for urgently needed items such as replacement parts for rockets, guided missiles, electronic warfare, air defense, combat surveillance, and atomic artillery.

**\$38-MILLION TO BE SPENT FOR VOICE-OF-AMERICA RELAYS**—Two major "Voice-of-America" relays, costing almost \$38-million, will be installed in Greenville, North Carolina and Monrovia, Liberia. The U.S. station, which will cost over \$25-million, will have a total available power output in excess of 4.8-million watts.

-30-

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of 1960...



  
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PICTURED MORE  
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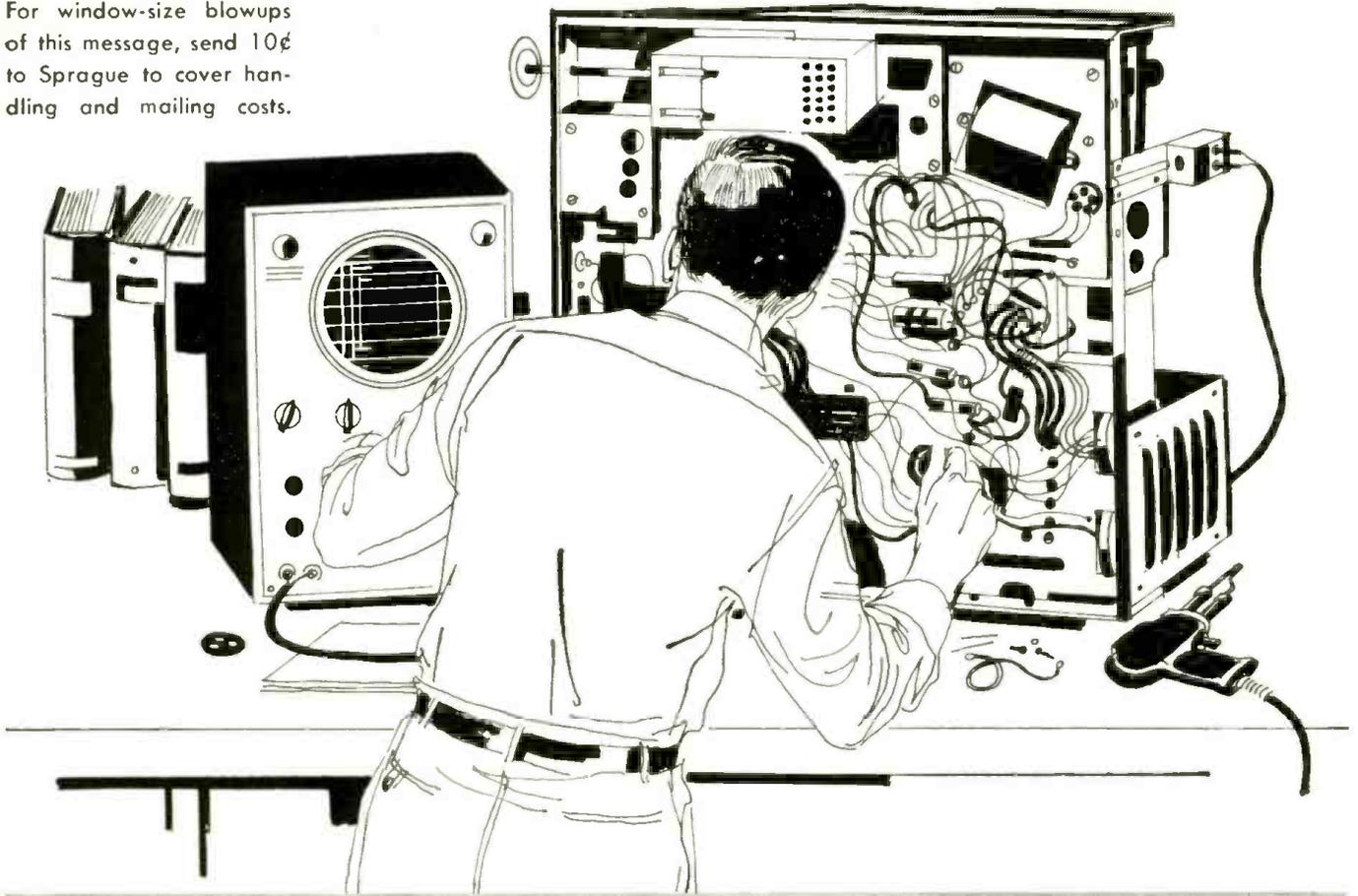
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manuals. He spends countless hours keeping up-to-date on new developments, new circuits, new trouble-shooting techniques.

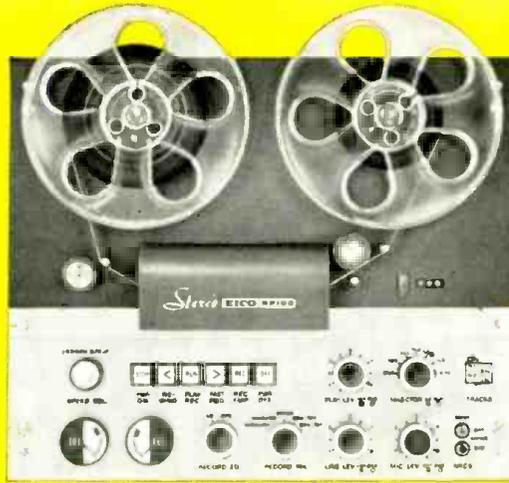
His training and experience qualify him as a modern, professional expert. As such, he asks a fair, professional price for his services. Since he will not use cut-rate methods or cut-rate parts in your TV set, he cannot offer cut-rate prices. *Remember, you get only your money's worth in TV-Radio service. When you are taken in by a "bargain-type" offer, you can expect to get "bargain-type" service. BEWARE THE SERVICE BARGAIN!*

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**MODEL RP-100W**

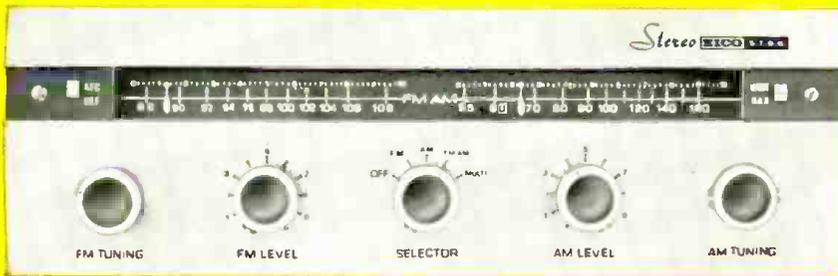
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Kit \$94.95 Includes Metal Cover Wired \$144.95

**40-WATT INTEGRATED STEREO AMPLIFIER ST40**

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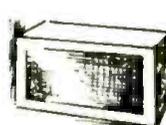
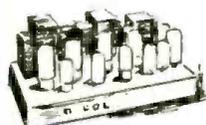
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# COLOR

## TV SERVICE TODAY

By CHARLES TEPFER

**Are there enough color sets to bother about? Can independents get the work? Can they handle it?**

**M**ANY YEARS have passed since the independent service technician was first told that he had to get ready to handle color receivers, and that he couldn't waste much time about it either. Many things were implicit in this statement, which he heard from the manufacturers, from the magazines he read, and in lectures at service-association meetings. It meant that there would soon be many color sets in use all over the country. It also meant that the independent was the man who would be called on to install, adjust, and repair this equipment.

What actually happened was something very different from this. The public was slow to buy. Today, in fact, only about one TV-viewing household in a hundred owns a color receiver. The overwhelming number of these sets were made by *RCA*, and most of these were sold with service contracts to be fulfilled by the *RCA Service Co.* Some independents, who in their eagerness to get an early jump, actively read up on the subject and even picked up color-bar generators and other accessories, have since had occasion to look ruefully at the layer of dust gathering on such paraphernalia. And writers stopped pushing the "get-ready-for-color-now" theme.

How has the situation changed, if at all? Does it even pay to read further in this article? Let's look at the signs.

The leading manufacturer, *RCA*, reports that the percentage increase in

color sales is spiraling upward. An optimistic statement, by itself, may be nothing more than whistling in the dark. However, it is a fact that this manufacturer is expanding its facilities significantly for producing both the three-gun picture tubes and the sets.

At the beginning of the color "boom" that never took place, at least half a dozen other set makers came out with color models. No significant quantity of these sets was sold. As a result, most manufacturers eventually withdrew, many of them saying that they would not get back into color until they could do so profitably. Today they are definitely coming back. *Admiral*, *Packard-Bell*, and *Magnavox* are some of those now selling color sets. *Emerson* has announced its definite intention of doing so. Others are being heard from as this is being written. These people are entering the field with the intention of staying and making a profit.

This still does not make a boom, but it does suggest a marked upward trend, and it is supported by other signs. The earliest color sets went to well-to-do buyers or to owners of such public places as bars and restaurants. Ownership of color TV was a mark of status, much as is ownership of a *Cadillac*. Today's statistics show that a very large percentage of such receivers are being bought on the installment plan. Members of the so-called lower-middle class are prominently represented in this group. Check a suburban area like that



Fig. 1. A degaussing coil is being used to demagnetize a color picture tube.

in Levittown, N. Y. and you get a surprise when you talk to service dealers. You say, "Not doing much on color, are you?" and they answer, "Well, you'd be surprised..." They then go on to tell you how many of their customers own or are now buying color TV.

Well, then, color really is on the way in. But does the independent shop get a chance to work on the sets? To answer this, let's start out with a familiar, full-page ad frequently run by RCA. "21-inch living color with only 8 more tubes than a black and white set," reads one. A large photo shows the top of a color-TV chassis. It is neat and looks relatively uncomplicated. "Servicing is so easy," the ad continues, "that most adjustments can be made without removing the back of the set. Components

give him a try? What can you lose?

Very well, you can get the work—but can you handle it? You probably can, and without much trouble. It is true that the latest color sets are simpler to adjust and service and less critical in operation. This is the result of continuing refinement in recent years, rather than radical change. It is true that most defects are identical with or similar to the ones you will run into on black-and-white sets. It is true that the faults peculiar to color circuits only still involve basic circuits that are familiar and should yield to conventional troubleshooting.

We will not attempt to prove the point with an exhaustive treatment of the theory and practice of color servicing. This has been done many times, al-

pens with black-and-white sets. Also, in many cases, it is not even necessary to demagnetize the color picture tube.

You remember that the picture tube and associated components often would pick up a residual magnetism in shipment because the tube, in the packing case, was moved through various magnetic fields (the earth's and others) during shipment. This would affect color purity and the tube had to be demagnetized with a large degaussing coil (Fig. 1) when the set was installed. Not only that, but this step was often necessary even when the set was moved within the same room in a home. Well, in many cases this is out. The picture tubes have closer tolerance in manufacture. Even more important, they are now all glass and do not have the mag-

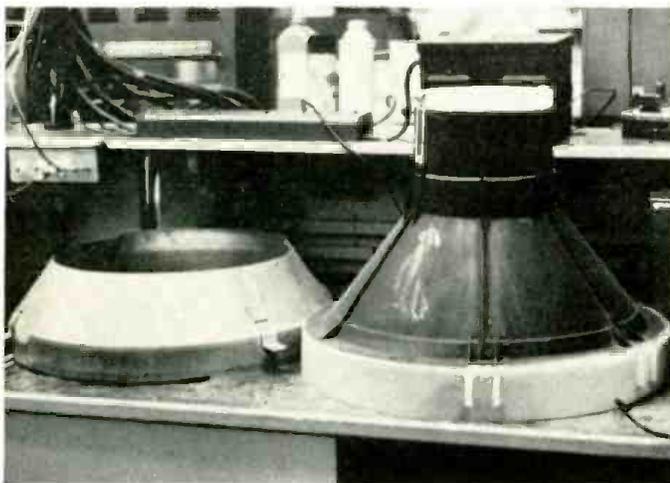


Fig. 2. Compare new CRT shield (left) with old shield (right).

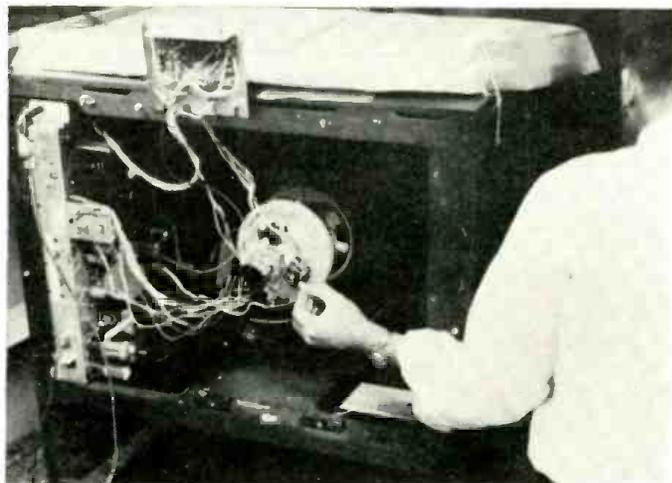


Fig. 3. Adjusting the convergence magnets in the yoke assembly.

used in color receivers provide superior performance and dependability as proved by actual life and performance tests."

How much truth there is in this claim involves another question, which we will get to later. The important thing is that, true or not, the public appears to be accepting it. Buyers know that the charge for installation and a 1-year service contract, which cost \$100 in 1959, is down to \$70 today. They also know that, whereas they started with service contracts on their monochrome sets many years ago, they soon found it cheaper to drop them and rely on individual service calls. In addition, the new buyers—who must watch dollars more carefully—can make a considerable saving at the time they decide to buy color by eliminating the contract. Add to this the fact that earlier buyers have actually found that they get little opportunity to use the service contracts they have paid for. Many of them do not renew.

Initially these color-TV owners without contracts doubtless feel that they can call the service company on a single-call basis when trouble occurs. However, when the defect develops, they tend to do the same thing they did with their black-and-white sets: The local independent is faster and probably less expensive. If he has proved dependable on monochrome TV and lets it be known that he can handle color too, why not

be it not recently. However, it will be useful to compare some of the "special" techniques still required today with these same procedures as they were performed just a few years ago.

#### The Improvements

Among the greatest headaches in color purity and convergence adjustments are the back-and-forth controls. You know the kind—first you adjust one control and then you go to another and then back to the first to touch it up, and then to the second again, and so on. This is not entirely eliminated in the new sets, but it is dramatically reduced. Adjustments are more positive and fool-proof.

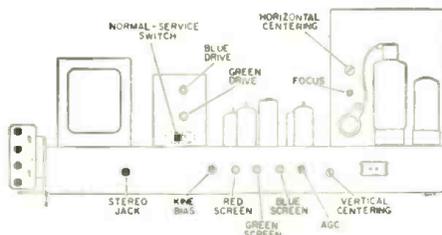
Second, during initial installation, it is no longer necessary to go through an elaborate set-up procedure. The sets work as soon as they are plugged in. Sure, some will not, but this also hap-

netically sensitive metallic shells.

Third, the author actually timed a complete "kine" replacement. From start to finish it took 13 minutes! This included all necessary color purity and convergence adjustments and a general touch-up of the set. Admittedly this was done by an expert, but he did not depart in any radical way from the step-by-step instructions contained in the service manual for the set. One of the reasons this is possible in the new sets is that it is no longer required to take the complete chassis out of the cabinet to change the CRT. Now, the cabinet is so arranged that the kine is in a harness right up at the safety glass and is simply locked into place. There is adequate clearance for the tube to be removed without jabbing into the high-voltage cage or other part of the chassis. Also, the CRT no longer wears the cumbersome corset shield of metal and plastic it once did. Now, it is protected by a much smaller shield which slips on as easily as a two-way stretch on a slender girl. The old and new shields are shown in Fig. 2.

Forget all about rim magnets for equalizing the magnetic field, forget about retaining rings and yoke shields. forget about turning the set down on its face on the floor. Replacing the kine in the new color sets is just about the same as for black-and-white tubes, mechanically that is. Now we come to the

Fig. 4. Most electrical adjustments for the CRT are located at rear of chassis.



kicker: what about the color adjustments?

### Color Adjustments

We said that the new color sets are more stable than their predecessors. What do we mean by stability? When you can set all rear-apron and interior chassis controls so that the set will operate satisfactorily with only minor and infrequent adjustment of the viewer controls, you have stability. The viewer controls on new color sets are: "on-off," volume, channel selector, fine tuning, color, tint, brightness, contrast, horizontal-hold, vertical-hold, and sometimes, sound tone. All other controls are interior ones, and not meant for the viewer to adjust. If the color set has been operating satisfactorily up until

First, turn the set on and adjust it for a good black-and-white picture. This of course involves the focus, linearity, hold, picture-size, and contrast adjustments. Next, connect a dot generator to the receiver, either at the antenna-input terminals (if the generator has a modulated r.f. output) or to some other points in the receiver according to the instructions for your instrument. Now adjust the red, green, and blue magnets in the deflection-yoke assembly (Fig. 3) to produce white dots in the center of the screen. The yoke assembly now contains these small plastic encased bar magnets. The convergence magnets are no longer on a separate ring as was the case in former sets.

The next step, demagnetizing the CRT, may or may not be necessary.

Now you are ready for the heart of the operation, the purity and convergence adjustments. Hold on to your hats, we'll race through them.

To obtain purity, we want a field of one color only—red. So we temporarily cut off output from the blue and green guns by manipulating the two appropriate controls available at the rear of the set (Fig. 4). Slide the entire yoke assembly back on the tube's neck and rotate the purity magnet (on the neck behind the yoke). At the same time, adjust the tabs on the magnet until you get a uniform red at the center of the CRT face. Now move the yoke forward against the bell of the tube, and adjust to obtain a completely uniform red screen.

At the rear of the set (Fig. 4), there



Fig. 5. Guns are balanced with vertical deflection killed.

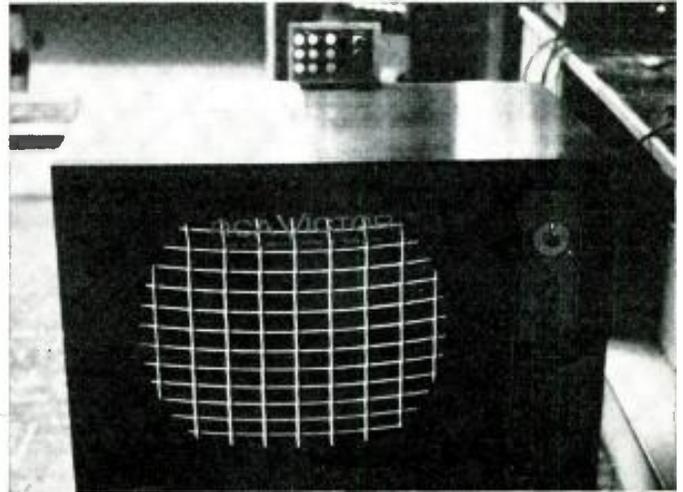


Fig. 6. Rear-mounted convergence-control board is swung up.

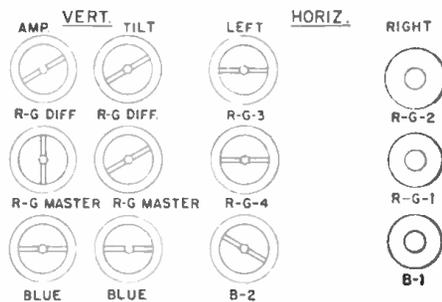


Fig. 7. Detail shows twelve adjustments mounted on the convergence-control board.

the time when the kine has to be replaced, because of age or some other reason confined to the picture tube, then chances are that the amount of color-control adjustment necessary will be minor. What happens though if this isn't the case, if the color set does need the complete "soup to nuts" color-adjustment job?

It is not our intention to go through a complete procedure. If you are faced with the necessity of doing this, better use the service-data manual for the specific set as a guide, although you will probably not need to after you have done it two or three times. However, a quick run-down on the new technique will allow you to compare it with the previous time-consuming, back-and-forth fiddling of the many controls.

However, it is a good precautionary measure in order to assure maximum color purity. To do this, use a degaussing coil 12 inches in diameter and made of 425 turns of number 20 enamel-covered copper wire (Fig. 1). Tape up the coil and connect the ends to a conventional line cord and plug so that it may be plugged into the a.c. line. Plug in the degaussing coil and slowly move it around in front of the kine face; then slowly withdraw to a distance of at least five feet before you remove the plug.

is a two-position "Normal-Service" switch. Flip it into the "Service" position, in which video and vertical-deflection circuits are cut out. The result, on the tube's face, is a horizontal trace (Fig. 5). Advance each of the color screen controls on the chassis so that the horizontal lines produced by each color are of equal brightness. You may have to touch up the bias control on the rear apron to bring up the brightness if you have trouble seeing a particular

(Continued on page 118)

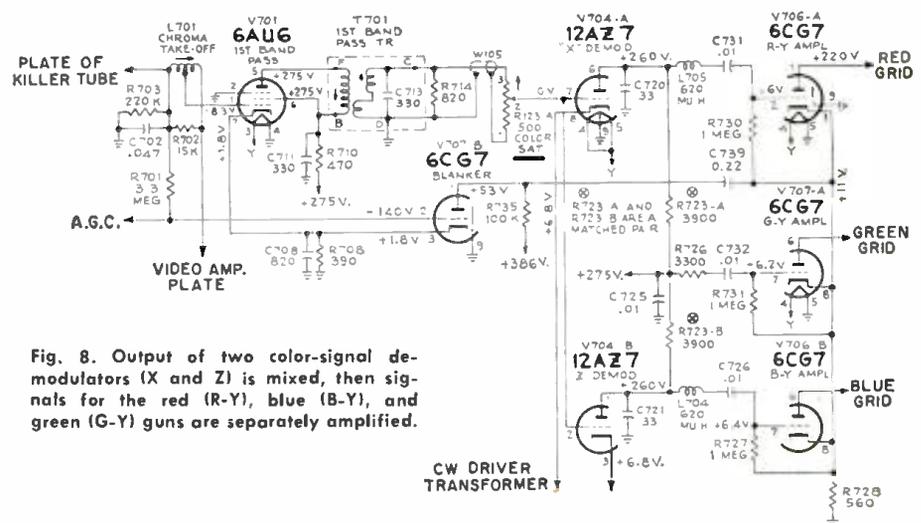


Fig. 8. Output of two color-signal demodulators (X and Z) is mixed, then signals for the red (R-Y), blue (B-Y), and green (G-Y) guns are separately amplified.

# Speech Clipper For CB Transceiver

By IRVING KRAUSE & GERALD WILNER

Increase the talk-power of your CB rig by building this simple transistorized speech-clipper circuit.

IF YOU HAVE constructed your own CB transceiver (see March 1959 issue of *ELECTRONICS WORLD*), then you know what a job it is to try and squeeze the last bit of power out of your transmitter and still stay within the legal FCC power input limit. Here's a suggestion for increasing the apparent output power of your transmitter without touching the transceiver itself. The method is well-known to hams and is commonly known as "speech clipping."

An analysis of ordinary speech will show a number of sharp peaks, as indicated in Fig. 1. This shows that the peaks, being so much larger in amplitude, tend to bring the average level, or

it would give rise to "splatter," creating unwanted additional sidebands. This, of course, would invite a citation from the FCC. In order to avoid this situation, a low-pass filter with a cut-off of about 3200 cycles is inserted after the clipper, which attenuates any higher order harmonics that may have been generated by clipping.

Speech clipping as high as 20 db may be accomplished before it affects intelligibility. It will be observed, however, that the "naturalness" of the voice decreases but the normal amount of clipping will actually increase intelligibility at a distant receiver because of the increase in sideband power.

Construction of the unit is neither difficult nor critical. The speech clipper was built in a small chassis box measuring 1 3/4" x 2" x 4". This particular unit was designed for a carbon microphone (Fig. 2) but if you are using a crystal, dynamic, or ceramic unit use the circuit suggested in Fig. 3. In this case, an additional mike preamp (V<sub>3</sub>) is used and the circuit of V<sub>1</sub> is modified. *Note:* In order to use a carbon microphone in conjunction with the original circuit, the grid of the 12AX7 was grounded and the microphone connected to its cathode. Thus the 12AX7 is supplied operating bias.

The microphone is fed into the emitter of V<sub>1</sub>, which supplies the operating bias for the carbon microphone. A greatly amplified signal appears across the clipping level pot, R<sub>2</sub>, which is then clipped by the zener diode, CR<sub>1</sub>, because the capacitor C<sub>2</sub> is large, the leakage increases the efficiency of the diode and the zener diode can be connected either way.

The resultant signal is fed through the low-pass filter consisting of C<sub>4</sub>, C<sub>5</sub>, and RFC<sub>1</sub>, whose cut-off is about 3200 cycles. An emitter-follower, V<sub>2</sub>, drives the succeeding circuitry (cathode of tube for carbon microphone and grid for crystal mike). Capacitor C<sub>7</sub> must be inserted if the speech clipper is to be used ahead of a crystal microphone input.

Just a word of warning. It is entirely possible that overmodulation of the transmitter could occur with this unit. Therefore, it is mandatory that the unit be adjusted by a person holding a commercial radiotelephone license. He will adjust the audio gain control and lock it so that overmodulation cannot occur. The clip level control may then be operated by the owner at his own discretion.

This clipping unit will operate with any type CB transceiver as long as it has an accessible mike jack. -30-

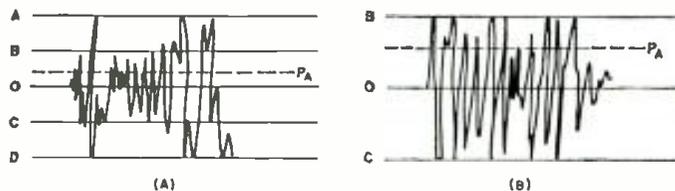
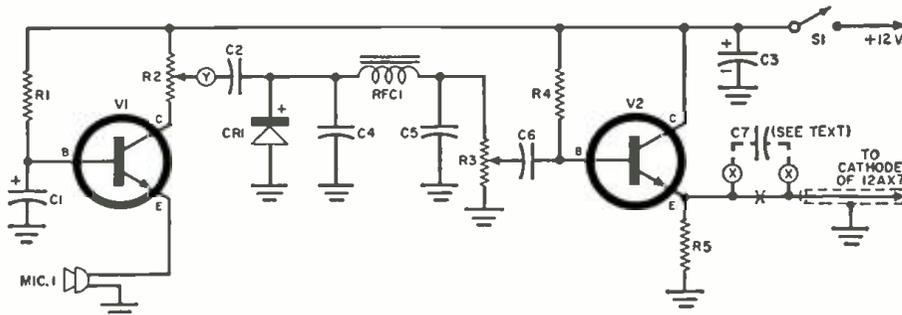


Fig. 1. Ordinary speech waveforms are shown at (A) before clipping. Note the low average power. After clipping (B), power is higher.



- |   |   |
|---|---|
| R <sub>1</sub> —82,000 ohm, 1/2 w. res.                   | C <sub>1</sub> , C <sub>2</sub> —.05 μf., 150 v. capacitor                              |
| R <sub>2</sub> —1000 ohm pot ("Clipping Level")           | RFC <sub>1</sub> —75 mhy. r.f. choke  |
| R <sub>3</sub> —5000 ohm pot (locking type, "Gain")       | Mic.—Carbon microphone (see text)   |
| R <sub>4</sub> —100,000 ohm, 1/2 w. res.                  | S <sub>1</sub> —S.p.s.t. switch   |
| R <sub>5</sub> —620 ohm, 1/2 w. res.                      | CR <sub>1</sub> —4.7-volt zener diode (Texas Instruments 1N750)                         |
| C <sub>3</sub> —50 μf., 12 v. elec. capacitor             | V <sub>1</sub> , V <sub>2</sub> —"n-p-n" transistor (Texas Instruments 2N364 or equiv.) |
| C <sub>4</sub> , C <sub>5</sub> —.1 μf., 150 v. capacitor |   |
| C <sub>7</sub> —50 μf., 150 v. elec. capacitor            |   |

Fig. 2. Diagram of the speech clipper designed for use with a carbon microphone.

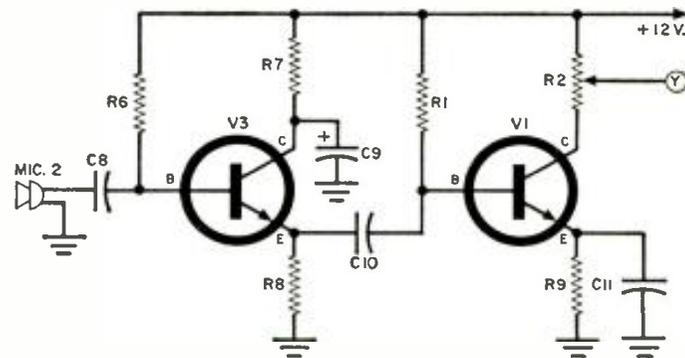
average power contained therein, down to a level indicated as P<sub>1</sub>. In fact, even if a transmitter were capable of 100% modulation (which many are not), the speech power would still be a small part.

Speech clipping consists of cutting off the peaks, leaving that portion between "B" and "C". The resultant wave will no longer contain many sharp peaks.

Due to this clipping, the remaining waveform will have a distinctly higher ratio of average power to peak amplitude (compare P<sub>1</sub> in Fig. 1A as against P<sub>1</sub> in Fig. 1B). Consequently, more sideband power will result when the clipped portion is used to modulate a transmitter at maximum level.

However, mere clipping does not give us any real advantage by itself because

Fig. 3. Preamp to be used with a crystal, ceramic, or dynamic microphone. Note that V<sub>1</sub> is the same stage as in Fig. 2, except for emitter-bias network that is employed.



- |  |   |
|--|---|
| R <sub>1</sub> , R <sub>2</sub> —82,000 ohm, 1/2 w. res. | C <sub>9</sub> , C <sub>10</sub> , C <sub>11</sub> —.1 μf., 150 v. capacitor            |
| R <sub>3</sub> —1000 ohm pot                             | C <sub>7</sub> —50 μf., 12 v. elec. capacitor   |
| R <sub>4</sub> —470 ohm, 1/2 w. res.                     | Mic.—Crystal microphone (see text)  |
| R <sub>5</sub> —2200 ohm, 1/2 w. res.                    | V <sub>1</sub> , V <sub>3</sub> —"n-p-n" transistor (Texas Instruments 2N364 or equiv.) |
| R <sub>6</sub> —200 ohm, 1/2 w. res.                     |   |

# HOME- CALL TV DIAGNOSIS

TV REPAIR

Can the set be fixed on the spot? Must it be pulled? What will it cost? Owners want quick answers.

By **WALTER H. BUCHSBAUM**  
Industrial Consultant

**L**IKE ANY professional man, the TV technician will find that his major assets are his knowledge and his time. Time is literally worth money to him because the more sets he can repair in a working day, the more profit he will make. Customers often think that the TV technician likes to build up a service job so as to be able to charge more; but the truth is that there is much more profit in many, quick repair jobs than in fewer, drawn-out ones. Many, quick jobs mean a faster turnover of the tube and parts inventory and a greater number of active customers, not to mention a reputation of being both honest and very capable.

Next to being able to repair every set at once, it would be nice if we could at least diagnose the trouble immediately so that we can tell the customer what the bill will be and how long the job will take. Many technicians have adopted the policy of taking a good guess whenever they are not sure what the trouble really is. Sometimes they are right, but often an optimistic guess leads to disappointment of both the customer and the technician. For this reason, many are reluctant to give estimates even though this makes the customer unhappy.

We know that perfection is not possible, but improvements can always be made, and the method which we offer in this article should help our readers to diagnose TV trouble more quickly. It is not the only possible approach, but it will be useful to those who do not have a better system or who have none at all. Although it is not fool-proof, it should work more than 75 per cent of the time. It requires a basic understanding of how a TV receiver works and what functions the different sections fulfill.

The main purpose of this method is to troubleshoot relatively simple defects rapidly and determine if a job will require considerable bench work. Before describing our method, certain ground rules concerning the home call have to

be established. These rules should be followed religiously, no matter how strong the temptation to "go just a little bit further":

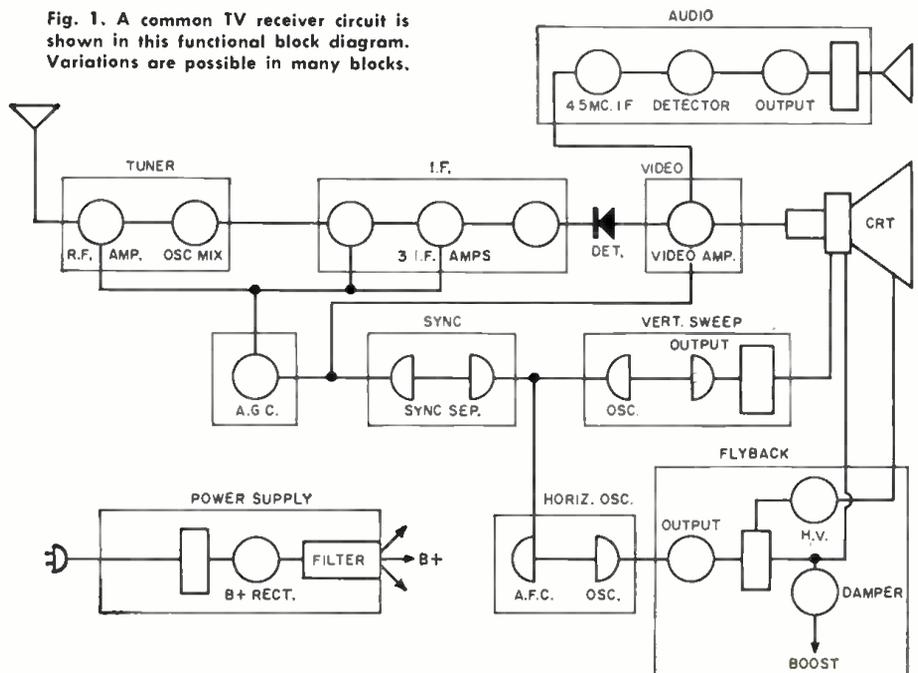
1. Explain to the set owner that you are going to attempt quick diagnosis, but if you cannot find the trouble it means the defect is more complex and the set will have to go to the shop for a more thorough investigation.
2. Total time spent on every set is to be no more than 30 minutes. (Don't count time to get at the tubes and inner controls.)
3. Use nothing more sophisticated than a v.o.m. or v.t.v.m.
4. A schematic diagram is desirable, but a tube layout is the minimum from which we can work.
5. Exclude all home-built sets or those where repairs or alterations have already been attempted by an amateur.

Such sets usually are "tough dogs" and the owner should be cautioned that costs will therefore be higher.

6. Go through the four following steps without skipping a point. (Once we allow the customer or some other influence to disturb our procedure, the whole value of using a methodical approach is lost and we might as well use the shotgun technique of the screw-driver mechanic.) And now to work:

A. *Symptoms.* Before we can repair a set, we must know what is wrong. The symptoms are established by first questioning the set owner and then verifying the complaint. Once the symptoms are verified, we will try to relate them to a likely area in the set. We can then replace tubes in that area and proceed with some basic tests. If the nature of the defect is now essentially known, we can estimate the repair or else estimate

Fig. 1. A common TV receiver circuit is shown in this functional block diagram. Variations are possible in many blocks.



Symptom	Probable Defect Location	What to Check	Remarks
1. No raster, no sound	Filaments, "B+" or a.c. line	Filaments on? Ohmmeter on a.c. line; voltage on "B+" line.	Is plug in outlet? Are series filaments used? Fuses or circuit breaker checked?
2. Sound, but no raster	High voltage, flyback, "B+", or video and brightness control, CRT	Filament of CRT on? Measure H.V. on CRT, measure d.c. on CRT.	Wait for slow-heating CRT or H.V. rectifier.
3. Raster, but no sound or picture (no "snow")	Antenna, lead-in, tuner, i.f. and detector sections	Filaments on in these sections? Measure "B+" on tuner, i.f. and measure a.g.c. bias on all stages.	+135 volts sometimes goes through audio output tube.
4. Raster and sound, but no picture	If separate audio i.f. is used, check video i.f., video amp., contrast control, a.g.c.	Measure bias on video amp., detector output, a.g.c. bus; measure "B+" on video and sync stages.	Check CRT socket and contrast control.
5. Weak, snowy picture; sound may be OK	Antenna, lead-in, tuner, i.f., detector, video and a.g.c. section	Check connections at antenna, lead-in, tuner contacts, and tube sockets. Measure a.g.c. bias.	Use portable antenna as test substitution.
6. Picture OK, sound weak or distorted	4.5-mc. sound i.f., or 21.25-mc. in separate (split) sound i.f. systems; FM detector, audio-output stages	Check limiter bias, FM det. d.c. output as fine tuning is varied. Check "B+" on plate and screen grid of output tube.	Defective parts replacement and alignment make this a bench job.
7. Picture fuzzy, raster lines don't show	Focusing circuit, brightness control or focus "B+"	Location and setting of FM focus ring or ion trap. "B+" on electrostatic CRT.	Dirty faceplate often aggravates this type of trouble.
8. Top or bottom of picture compressed or stretched	Vertical-sweep section; "B+" boost circuit	Adjust height and linearity. Measure d.c. voltages on vertical-output stage.	Defective resistors in vertical sweep often due to other trouble.
9. "Glittering" vert. lines, vert. streaks	Flyback section, damper, or deflection yoke	Tap horizontal output tube and damper. Check connections to yoke damping capacitor.	Barkhausen oscillation can be fixed by taping small magnet to output tube.
10. Bent or twisted pictures; edge tearing	Horiz. asc. or output, sync separator or video amp.	Try horiz. drive and width. Adjust a.g.c. control, check for intermittents.	Locating defective part may require scope signal tracing.
11. Picture rolls up or down	Vert. asc. or sync separator; video amp.	Adjust vert. hold and other vert. controls and a.g.c. Open or shorted vert. integrator network.	Loss of vert. sync usually requires scope signal tracing.
12. Picture appears "sliced" or weaves back and forth	Horiz. asc., sync separator, or a.g.c. (if keyed)	Try all horiz. adjustments. Look for overheated resistors.	Aging components can be compensated by slight adjustments.
13. Dark horiz. bar in picture on all channels (60 cps in video)	Tuner, i.f. or "B+"	Ohmmeter check "B+" filters; check for cathode-filament shorts.	Jump electrolytic across various "B+" points as check.
14. Picture OK but 60-cps audio hum on all channels	Video amp., detector, or 4.5-mc. traps	Try slight touch-up of each trap and FM detector. Check a.g.c. action.	Grid clipping on video amp. can also cause this.
15. All black lines smeared to right	Tuner, video i.f., video amp.	Check low-freq. compensating capacitor in video amp.	Loss of low frequencies usually means alignment.
16. Picture fades rapidly on all channels	Antenna, lead-in, tuner, a.g.c.	Ohmmeter on antenna and lead-in; check all wiring up to tuner input.	Intermittent a.g.c. filter is a possibility.
17. Intermittent picture and sound when set is hit or vibrated	Tuner, i.f., or video amp.	Check contacts on tuner, tube sockets and grounds. Tap tubes.	Tuner contact cleaner may clear up trouble at once.
18. Picture too narrow	Horiz. output, horiz. asc.; damper circuit	Adjust width and horiz. drive. Check grid bias of output tube, check "B+" on screen, "B+" boost.	When this occurs during warm-up, defective part will need scope signal tracing.
19. Picture too short top and bottom	Vert. asc., output, or "B+" boost-voltage section	Adjust height and linearity; measure tube voltages and "B+" boost.	Intermittent or warm-up type defect needs scope signal tracing.
20. Picture changes size when contrast or brightness is changed	Flyback and H.V. section; picture tube gassy	Measure H.V. under all conditions, including low power-line voltage.	Gassy CRT is least likely.

Table 1. Reference chart of common symptoms with causes, checkpoints, and cures.

the cost of further troubleshooting. But first the symptoms must be determined.

In this connection, a customer may simply say that the set "doesn't work right" and expect the technician to guess that the trouble only occurs on Wednesdays at 6 p.m. and only on one channel. It would then take a long time to determine that the "intermittent" is simply interference from a local source. Even when the set is completely dead, and nothing lights up inside, it helps to know if this happened after hours of playing, accompanied by smoke and arcing, or if the set has been dead ever since it was transported back from the summer vacation home. For this reason we should always question the set owner on the following points:

"What is wrong? Since when? How did it happen? On all channels? At all times or only occasionally? Has anyone tried to fix it? Who and how?"

Verifying the Complaint: Remember that the set owner, as a rule, is technically ignorant and will confuse such troubles as horizontal and vertical sync defects, brightness and contrast, audio distortion and mistuning, to cite just a few examples.

Each complaint must therefore be verified before troubleshooting can start. Defects due to heat, unauthorized tampering, certain intermittents and, of course, antenna troubles (if the set is brought to the shop) will usually take longer than 30 minutes and will require more elaborate test equipment. In such instances, the customer should be told the facts and our rapid TV troubleshooting technique can be abandoned. These few instances are likely to be involved, difficult, and expensive service jobs.

*B. Logical Analysis.* The amateur's approach to a defective TV set will be to first check and/or replace all tubes and, if this does not help, to look for broken wires and burnt resistors. In the average 16-tube set, the first step alone will usually take up the entire 30-minute period and yet may yield no results. What also happens occasionally is that a tube replacement works for a few hours, and then the trouble occurs again. This is due to a part failure which, in turn, burns out tubes. A professional technician cannot afford such a waste of time and must therefore proceed logically, using his knowledge of TV receiver circuitry to associate the symptoms with the defect.

To facilitate a rapid preliminary diagnosis, we include the troubleshooting check list of Table 1. A total of 20 frequent symptoms is listed here, together with probable locations of the defect and suggestions on how to check it quickly. Under the column "Probable Defect Location" are suggestions as to which tube replacements should be attempted.

As a reminder of the functions of the various tubes of a TV receiver, we also offer the block diagram of Fig. 1, which is based on a roughly typical receiver. Remember that many variations are possible. Older sets still use a separate sound i.f. section (21.25 mc.). In many

sets, more tubes are used for the vertical sweep, horizontal sync, sync separator, video amplifier, and other circuits. A tube layout diagram of the receiver should be available to save time in locating suspected tubes.

Once the symptoms have been verified, relate them to the particular receiver section and, if possible, to a particular stage. For example, if the picture is too short (Item 19 in the check list), we know that the defect is most likely in the vertical-sweep section. It could also be the vertical oscillator, output stage, or even the "B+" boost voltage. If the oscillator and output stage are housed in a single tube envelope, replacement of that tube will be the first step. Under "What to Check," we find a suggestion to adjust height and linearity controls. This will be part of the trouble verification and, if tube replacement does not remedy the defect, measurement of the voltages in the output section will be next. Voltage checks at the tube socket will show such defects as open controls or resistors. If voltages seem correct, it is apparent that more sophisticated troubleshooting will be required.

C. *Troubleshooting.* Once we have de-

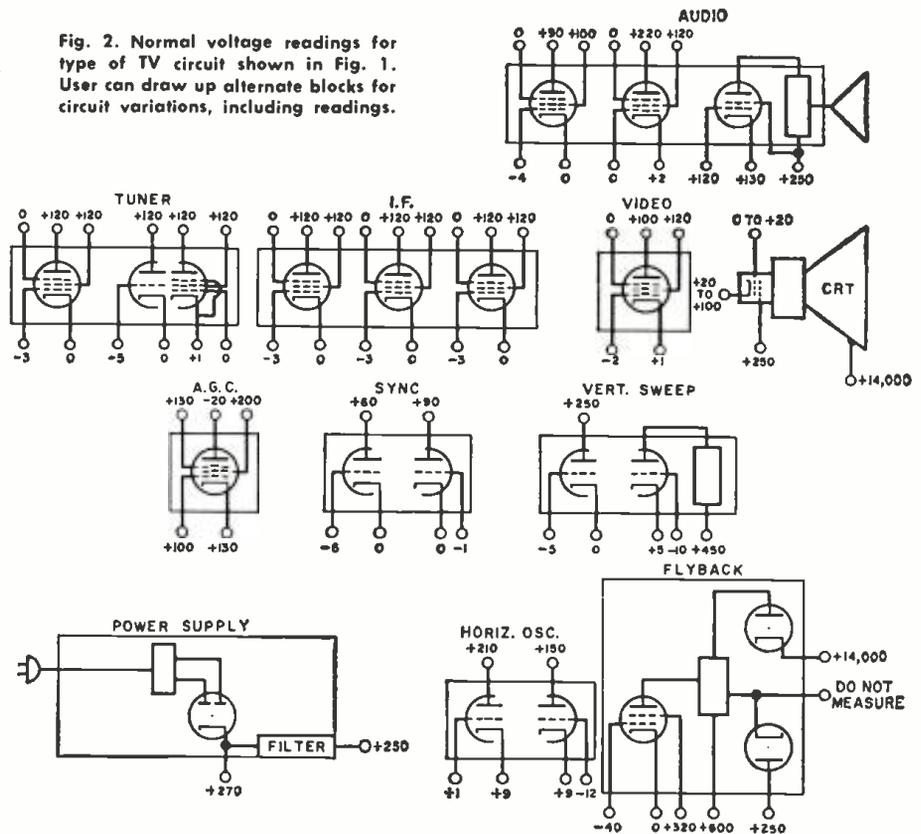
- |  |
|--|
| 1 Set Hand Tools (diagonal pliers, needle-nose pliers, socket wrenches, screwdrivers, gas pliers, soldering gun, solder, etc.) |
| 1 Octal Tube Socket Adapter  |
| 9-Pin Tube Socket Adapter  |
| 7-Pin Tube Socket Adapter  |
| 1 Set Alignment Tools  |
| 1 Interlock A.C. Cord (cheater)  |
| 1 Flashlight   |
| 1 Set of Clip Leads  |
| 1 V.O.M. or V.T.V.M.   |
| 1 High-Voltage Probe for V.O.M. or V.T.V.M.  |
| 1 Adjustable Indoor Antenna  |
| Tube Assortment  |
| 1 Isolating Transformer  |
| 1 80- $\mu$ f., 450-volt Electrolytic Capacitor  |
| Assorted Fuses   |
| Contact Cleaner (for tuners and potentiometers)  |
| Anti-Corona Dope   |

Table 2. Listed equipment will facilitate recommended house-call techniques.

vided where the defect is likely to be found and how we will attack it, we are ready to swing into action—but not before. Instead of blindly changing tubes, we can now proceed methodically. Where a clear-cut symptom points directly to a particular tube, we will replace it; but after the new tube is plugged in, the d.c. voltages should be checked. The diagram of Fig. 2 gives approximate voltages for each tube in a typical set. This serves to check that the defective tube was not damaged by wrong voltages due to some other defect. On some of the recent models which use printed wiring, the tube socket connections are readily accessible. On most older sets, a tube-socket adapter comes in very handy for checking voltages. (We have included a set of adapters in our list of tools, Table 2.) Watch for transformerless "hot" sets and use an isolating transformer or other precautions in such cases.

Also remember that, with the many

Fig. 2. Normal voltage readings for type of TV circuit shown in Fig. 1. User can draw up alternate blocks for circuit variations, including readings.



possible variations in individual circuits, corresponding variations would occur in the voltage readings. For example, normal voltages for a tuner using a pentode r.f. amplifier are shown. If a cascode r.f. amplifier is used, high "B+" voltage (about 250 volts) would appear at the plate of one triode but approximately half that value at the plate of the other triode. If a stacked "B+" supply is *not* used, plate voltage of the audio-output tube may or may not be lower than that shown, but grid and cathode voltages will be much closer to ground than those shown. Some sets will not use keyed a.g.c. Fig. 2 should therefore be considered to be not a definitive guide, but a skeleton aid to which common variations may be added.

Where the symptoms do not point clearly to a particular tube or where replacement does not help, certain additional checking is reasonable. Rapid visual and mechanical inspections are in order, plus some electrical tests.

In the visual inspection, clear away dirt and dust and apply some light to the specific chassis area in which the suspected section is located. Watch for such signs as leakage from capacitors, charred wires, resistors with the color coding burned off, and the like. Observe tubes for such internal clues as plates that get cherry red or the purplish glow around elements that indicates gas.

During the mechanical inspection, use an insulated alignment tool or small, rubber-tipped hammer for gently tapping tubes, connections, wires, and components in the suspected area. This often flushes out breaks or defective parts that escape visual observation. Rock each suspected tube gently in its socket to make sure that trouble is not

due to something like bad contacts.

As for electrical tests, our limited time permits only such major checks as voltage and resistance measurements. When nothing lights up, resistance checks of the primary power and the filament string are the first approach. When tubes light but neither sound nor video appears, we will check the various "B+" voltages and, if there is no "B+," resistance checks across the "B+" will determine the presence of a short circuit. The electrolytic capacitors in the "B+" filter will, of course, at first indicate a short on the ohmmeter, but the resistance will increase as the capacitors are charged up.

Voltage measurements should be made at the plate, screen, cathode, and grid of each tube in the suspected trouble area and the values should be noted down to permit the technician a few moments of orderly analysis of these test results.

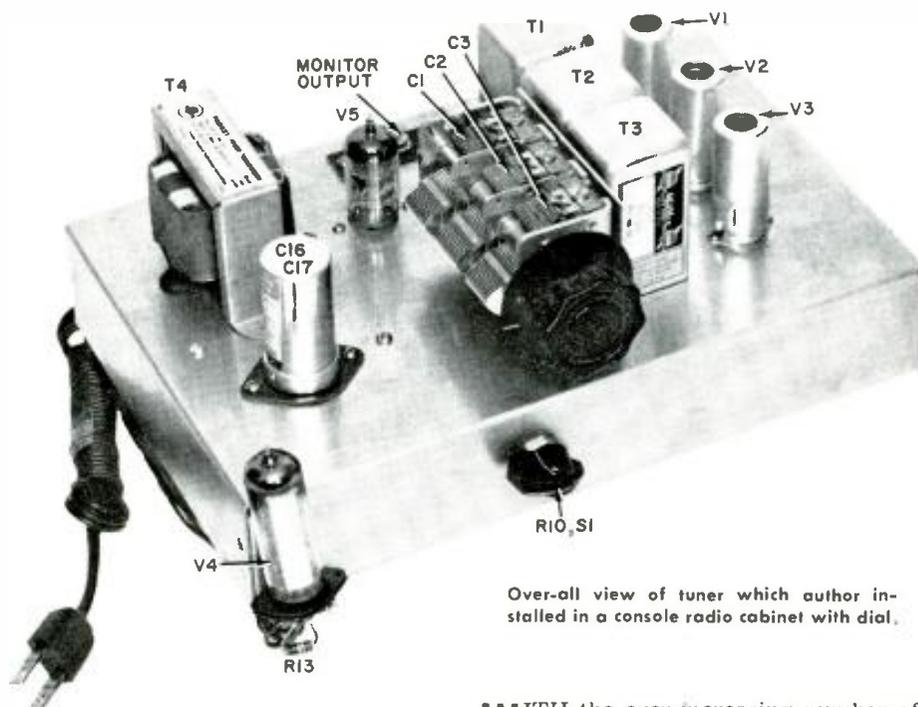
While it is not possible to make a thorough voltage or resistance analysis in the allotted 30 minutes, certain defects can be determined quickly. By measuring the voltage at the plate of a tube and comparing it with the "B+," we can see at once how much current passes through the load resistor and the tube. If the load resistance is correct and if "B+" and plate voltage are practically the same, very little current flows. This means that the tube is cut off and this, in turn, may be due to an open circuit in the cathode or some defect in the grid circuit. The audio limiter, sync clipper, and the a.g.c. amplifier are intended to work at or near cut-off.

Grid bias should not be measured

(Continued on page 87)

Here are complete construction details on a broadcast-band tuner that features very low distortion, that may be added to your present high fidelity sound setup.

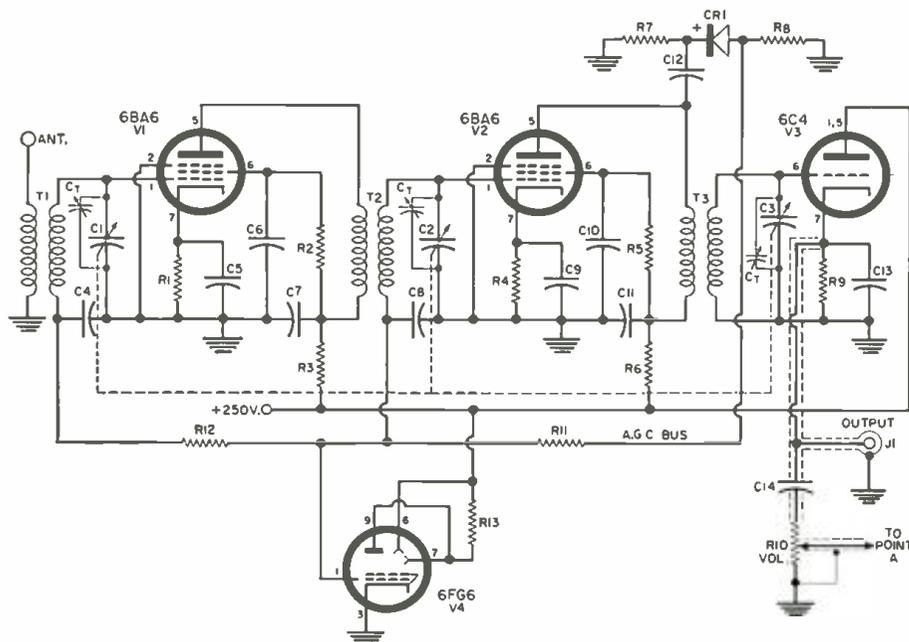
By JOHN POTTER SHIELDS



Over-all view of tuner which author installed in a console radio cabinet with dial.

# HIGH-QUALITY T.R.F. AM TUNER

Fig. 1. Circuit diagram shows use of 2 r.f. stages, infinite-impedance detector, along with an optional tuning indicator. If power requirements can be obtained from another piece of gear, no rectifier or filter are required for the tuner.



$R_1, R_2$ —68 ohm,  $\frac{1}{2}$  w. res.  
 $R_3, R_5$ —22,000 ohm,  $\frac{1}{2}$  w. res.  
 $R_4, R_6$ —10,000 ohm,  $\frac{1}{2}$  w. res.  
 $R_7, R_8, R_{11}, R_{12}$ —2.2 meg.,  $\frac{1}{2}$  w. res.  
 $R_9$ —100,000 ohm,  $\frac{1}{2}$  w. res.  
 $R_{10}$ —500,000 ohm audio taper pot  
 $R_{13}$ —470,000 ohm,  $\frac{1}{2}$  w. res.  
 $C_1, C_2, C_3$ —3-section variable cap., 365  $\mu\text{f.}$ /sect. with trimmers  
 $C_4$  to  $C_{11}$ —.01  $\mu\text{f.}$ , 600 v. disc cap.  
 $C_{12}$ —.05  $\mu\text{f.}$ , 600 v. disc cap.

$C_{13}$ —.0005  $\mu\text{f.}$ , 600 v. disc cap.  
 $C_{14}$ —.1  $\mu\text{f.}$ , 600 v. paper cap.  
 $T_1$ —Shielded antenna coil (Miller 44-A, or equiv.)  
 $T_2, T_3$ —Shielded r.f. coil (Miller 44-RF, or equiv.)  
 $CR_1$ —1N34-A, or equiv. germanium diode  
 $J_1$ —Phono or mic. jack  
 $V_1, V_2$ —6B.16 tube  
 $V_3$ —6C4 tube  
 $V_4$ —6FG6 E.M.84 tube

WITH the ever-increasing number of AM-FM stereo programs available and the generally improved quality of AM transmission, a good-quality AM tuner is almost a must for the serious audiophile. Such a tuner should have adequate r.f. bandpass characteristics so as to avoid carrier sideband attenuation, sufficient sensitivity, a low-distortion output at all carrier levels, and sufficient flexibility to tie in readily with existing audio gear. The tuner to be described was developed by the author with the above requirements in mind and is capable of excellent performance coupled with ease of construction and alignment.

Figures 1 and 2 show schematics of the complete tuner. It was decided to use a two-stage t.r.f. amplifier driving a low-distortion detector rather than the more conventional superhet arrangement, in order to easily obtain the wide bandpass characteristics. While it is quite possible to design a broadband superhet, it is not quite so simple for the experimenter to obtain and adjust i.f. transformers with the necessary broadband characteristics. Although "swamping resistors" may be shunted across the i.f. transformer windings to reduce their effective "Q", the stage gain is then reduced. This often requires an additional stage of amplification. Also, the t.r.f. circuitry is more economical of parts; requiring no converter stage, and the alignment is extremely simple.

## Circuit Description

Signals arriving at the antenna terminal are coupled by the antenna transformer,  $T_1$ , to the control grid of the first r.f. amplifier,  $V_1$ . The first section of the tuning capacitor,  $C_1$ , in conjunction with the secondary of  $T_1$ , select the desired frequency. The signal is amplified by  $V_1$  and applied across the primary of the r.f. transformer  $T_2$ . The secondary of  $T_2$  is tuned to the operating frequency by the second section of

the tuning capacitor,  $C_5$ , and the signal is applied to the control grid of the second r.f. amplifier stage,  $V_2$ . The signal is further amplified by  $V_2$  and applied to the primary of the next r.f. transformer,  $T_2$ . The r.f. signal developed across the secondary of this transformer, tuned by the third section of the tuning capacitor,  $C_5$ , is applied to the detector stage.

Considerable thought was given as to the proper type of detector to use with this tuner and it was finally decided to use the infinite-impedance detector for several reasons. First, unlike the diode detector which requires eight to ten

This gives a much better indication than the older indicator types, such as the 6E5, 6U5, etc.

The tuner is provided with two outputs: one directly from the infinite-impedance detector and a "monitor" output, which provides sufficient signal to drive a speaker at modest volume. This "monitor" output is supplied by a two-stage RC-coupled amplifier consisting of both sections of  $V_3$ , which receives its signal from the output of the detector *via* the volume control,  $R_{10}$ . The volume control is so connected that it does not affect the detector output. No output transformer was provided due to chassis space limitations, but any inexpensive universal output transformer with a primary impedance of around 6000 ohms can be used. Note that the leads from the tuner to the monitor speaker's transformer are "hot," so be careful.

The power supply is conventional, consisting of the isolation/power transformer,  $T_1$ , feeding a voltage-doubler rectifier setup using a pair of selenium rectifiers,  $SR_1$  and  $SR_2$ . A  $\pi$ -section RC filter smooths the output from the rectifiers.

If the constructor has another power supply available, or can get the voltages needed from other equipment, then it will not be necessary to build the rectifier circuit shown in Fig. 2. Just be sure the external supply can deliver at least 1½ amps. at 6.3 volts for the heaters and about 50 ma. at 250 volts for the plates. Also, if a monitor speaker is not needed, then the circuit with  $V_3$  will not be necessary. The output at  $J_1$  is then fed directly to the hi-fi preamp or amplifier. Output may also be taken at point A if control of volume is needed.

### Construction

The author built the tuner on a standard 7" x 9" x 2" aluminum chassis. No front panel or calibrated dial is shown in the photos as the tuner was installed in an old console cabinet which had an existing dial. The 6FG6 tuning

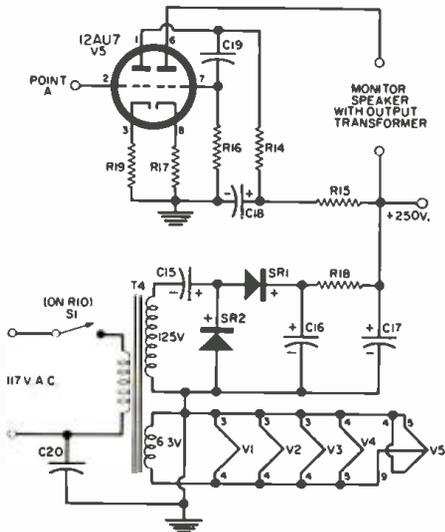
indicator socket was mounted on a small aluminum angle bracket which was screwed to the inside of the cabinet's front panel. Standard shaft extensions were used on the tuning capacitor and volume control shafts to lengthen them sufficiently to fit through the rather thick panel. (The two knobs shown in the photos were used only to "doll up" the tuner when its picture was being taken.)

### Alignment

As mentioned earlier, this tuner is a breeze to align. If you wish, you can align the tuner by means of a standard broadcast station signal although of course the use of a signal generator is to be preferred. If alignment by means of a broadcast station signal is to be used, select a station around 1400 to 1600 kc. and peak all three tuning capacitor trimmers for maximum signal output by ear or as indicated on the tuning indicator or a v.t.v.m. connected between the a.g.c. bus and ground. It is best to rock the tuning capacitor slightly as the trimmers are being peaked for maximum output. Now, select a station around 500 to 600 kc. and repeat this process. You may find that the trimmer settings are slightly different at the low frequency end of the band and it is therefore best to average out the high- and low-frequency trimmer settings.

If a signal generator is used in alignment, the low, middle, and high frequency settings of the band should be checked and the trimmers adjusted for nearly constant output over the entire band.

Well, that's the story on the little tuner. I'm sure you will be more than pleased with its performance. By the way, I think you will be more than a little surprised at how clean those few tenths of a watt from the monitor output will sound when fed into a decent transformer and speaker, or how fine the unit sounds when played through your hi-fi system.



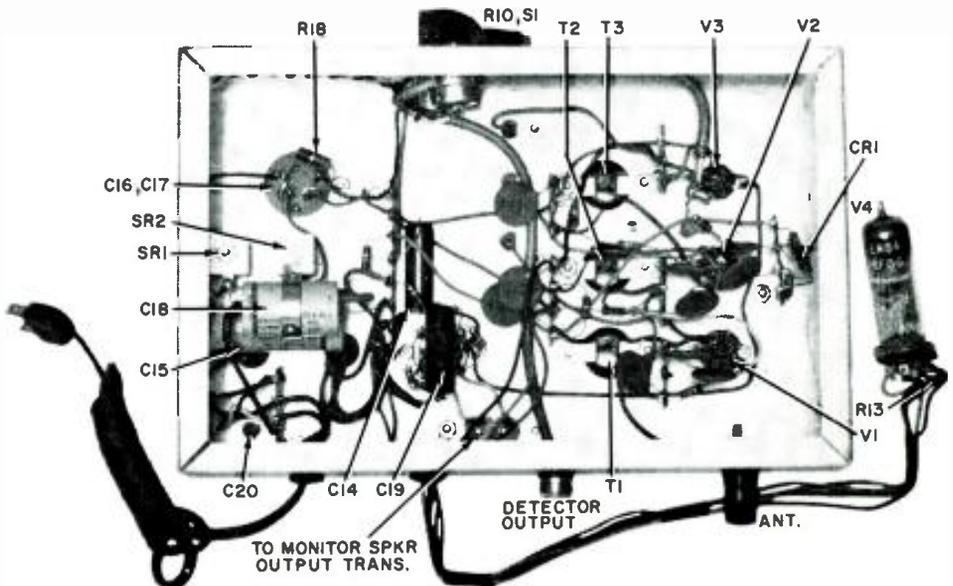
- $R_{11}$ —220,000 ohm, ½ w. res.
- $R_{12}$ —22,000 ohm, ½ w. res.
- $R_{13}$ —470,000 ohm, ½ w. res.
- $R_{14}$ —470 ohm, 1 w. res.
- $R_{15}$ —680 ohm, 2 w. res.
- $R_{16}$ —2200 ohm, ½ w. res.
- $C_{11}$ ,  $C_{12}$ —20  $\mu$ f., 150 v. elec. cap.
- $C_{13}$ ,  $C_{14}$ —40  $\mu$ f./40  $\mu$ f., 250 v. elec. cap.
- $C_{15}$ —1  $\mu$ f., 600 v. paper cap.
- $C_{16}$ —0.01  $\mu$ f., 600 v. disc cap.
- $T_1$ —Power/Isolation transformer, 125 v. @ 50 ma., 6.3 v. @ 2 amp. (Stancor P.1-8421, or equiv.)
- $S_1$ —S.p.s.t. switch on  $R_{10}$
- $SR_1$ ,  $SR_2$ —65 ma. selenium rectifier
- $V_3$ —12AU7 tube

Fig. 2. Optional power supply and output stage required to drive monitor speaker.

volts of r.f. input for an output of reasonably low distortion, the infinite-impedance detector provides an extremely low-distortion output for any given r.f. input voltage. This is due to the large amount of negative feedback provided by its large cathode resistor. Second, the effective output impedance of the infinite-impedance detector is considerably lower than that of a conventional diode detector. This allows a reasonable length of shielded cable to be run from the detector output to the amplifier input without appreciable attenuation of the higher frequencies.

The infinite-impedance detector has one distinct disadvantage however: it does not provide a convenient d.c. output voltage proportional to the carrier level which can be used for a.g.c. control purposes. To solve this problem, a separate diode a.g.c. rectifier is used, consisting of  $CR_1$ , plus its associated filter network,  $R_8$ ,  $R_{11}$ ,  $R_{12}$ ,  $C_1$ , and  $C_2$ . A 6FG6 tuning indicator is tied into the a.g.c. bus to indicate proper station tuning.

Under side of the chassis. Wiring need not be crowded as there is adequate space.



# Simple Electronic Engine Analyzer



By R. A. LEBOWITZ and R. M. SONKIN

Construction of a one-transistor instrument that will measure engine speed, point dwell, and battery voltage.

**T**HIS article describes a simple, one-transistor instrument that is capable of measuring engine speed, distributor contact-point dwell, and battery voltage. It needs no external power source and will operate on either 6- or 12-volt systems. It can be included in a permanent dashboard installation or used as a portable service instrument.

This small device can provide the user valuable information on the condition of the automobile electrical system. It can, for example, detect: 1. malfunctioning or worn spark plugs; 2. worn or incorrectly set distributor points; 3. maladjustment of the voltage regulator; 4. defective generator; and 5. shorted, weak, or overcharged battery.

The three functions (rpm, dwell, battery voltage) are individually selected by a rotary switch. The tachometer or rpm function needs little description. It measures engine speed in revolutions per minute (rpm). The maximum rpm reading can be adjusted by means of a calibrating control. This maximum value can be set for 5000 rpm for installation in American cars and for 8000 rpm for use in foreign cars or for service work.

The dwell function measures the time that the points are closed relative to the entire ignition cycle. Fig. 1 will be used to illustrate the dwell angle in further detail. Fig. 1A is the schematic of the ignition system of an automobile while Fig. 1B is the waveform appearing at the points. The ratio  $T_1/T_2$ , expressed as a percentage, is indicated directly on the dwell meter. To express this percentage

in terms of angle, the following constants of proportionality apply: 4-cylinder engine—% dwell  $\times 90 =$  degrees dwell; 6-cylinder engine—% dwell  $\times 60 =$  degrees dwell; and 8-cylinder engine—% dwell  $\times 45 =$  degrees dwell.

As shown in Fig. 2, there are two scales for percentage dwell. The top

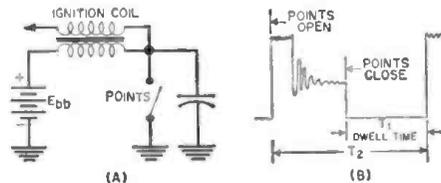


Fig. 1. The basic ignition system of a car, and the waveform at the car's points.

Fig. 2. The new meter scales used by the authors. The top scale indicates engine speed, the next two scales indicate dwell per-cent for cars with either a negative or a positive ground system, and the bottom scale indicates the voltage of the battery.



scale is for an automobile with its negative battery terminal grounded; the bottom for a positive terminal ground. The importance of proper dwell setting cannot be overemphasized; factory service manuals specify dwell to within  $\pm 2$  degrees.

The final function is that of a battery voltmeter. This serves to indicate the condition of the battery and of its charging apparatus.

## Principles of Operation

Fig. 3 will help to illustrate the operation of the tachometer circuit. When the points are open, transistor  $V_1$  will be conducting on an automobile with a positive ground (negative voltage applied to the transistor base) and cut off on one with a negative ground (positive voltage applied to the transistor base). When the points are in the condition to produce conduction in  $V_1$ , the applied battery voltage causes sufficient base current to flow to make  $V_1$  fully conducting. The rise and fall of current between conducting and cut-off states is almost instantaneous, hence  $V_1$  acts as if it were a switch that turns the current in  $R_1$  and  $R_2$  on and off. This produces a square wave of voltage across both portions of the potentiometer.

When the transistor is cut off, capacitor  $C$  charges through  $R_1$ ,  $CR_1$ , and the indicating meter,  $M_1$ . The time constant of this charging circuit is small so that only a sharp pulse of current flows. The diode,  $CR_2$ , is connected in the circuit in such a manner as to prevent the current from flowing in it when  $C$  is charging.

When the transistor conducts, the voltage at the junction of  $R_1$  and  $R_2$  drops (becomes less negative) and  $C$  discharges through  $V_1$ ,  $R_3$ ,  $R_6$ , and  $CR_2$ . The diodes in the input base circuit of the transistor ( $CR_1$  and  $CR_2$  in Fig. 5) pass a negative-voltage pulse to the base but block a positive-voltage pulse. The diodes are used to protect the transistor from high-voltage input spikes. If a higher-back-voltage diode is available, it can be installed in place of the 1N34 for  $CR_2$ . Under these conditions,  $CR_1$  would not be needed.

The number of pulses flowing through the meter per unit of time is proportional to the speed of the engine. The panel meter reading is proportional to the average direct current flowing through it which is, in turn, proportional to the number of pulses flowing in it per unit of time and thus to engine speed.

Fig. 4 will help to illustrate the operation of the dwell-angle circuit. The base-to-emitter voltage tends to remain constant when a transistor is conducting. It is approximately 0.3 volt for germanium. Thus the current through the meter in Fig. 4 remains constant when the transistor conducts and is zero when it is cut off. The meter reads the average current flowing over both states.

On an ignition system with a positive ground, the current flows when the points are open and thus the average meter current is inversely proportional to dwell angle. The longer the points are open, the greater proportion of the time that the current flows and thus the higher the meter reading. Under these conditions, the dwell time (during which the points are closed) is low.

On a negatively grounded system the current flows when the points are closed and the current is directly proportional to the dwell angle.

The battery voltmeter consists of a resistance in series with the milliammeter connected across the battery terminals.

### Construction

The layout and construction of the unit are not critical. Fig. 5 is the complete schematic of the unit. Transistor  $V_1$  can be practically any audio or general-purpose  $p-n-p$  germanium transistor. A *Motorola* 2N653 and a *Texas Instruments* 2N367 were used in the units constructed by the authors. The components may be laid out on a phenolic

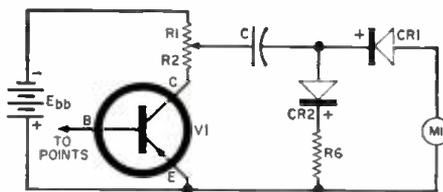


Fig. 3. Partial schematic of the analyzer, whose complete circuit is shown in Fig. 5, illustrating the engine-speed function.

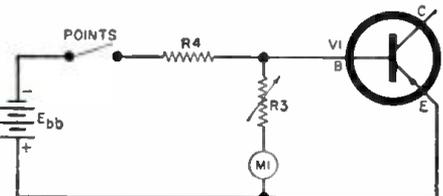


Fig. 4. This partial schematic shows the operation of the dwell-angle function.

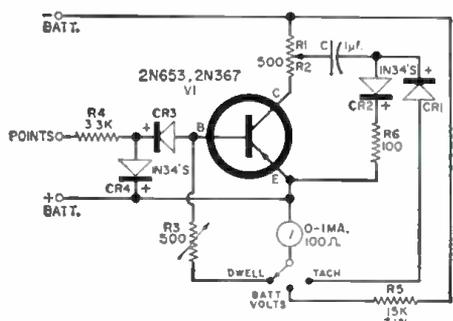


Fig. 5. Complete circuit diagram and parts values for the engine analyzer.

board and then mounted onto the meter case, as shown in the photographs. Another idea would be to buy a four-pole, triple-throw rotary switch and mount all components, except the potentiometers, on the unused terminals. Three wires are brought out to the rear of the unit. These wires are connected to the plus and minus battery terminals and to the primary terminal of the distributor. The 1-ma. meter should be of the low-resistance type, approximately 100 ohms.

To make the instrument useful with engines of various numbers of cylinders, the meter is calibrated in per-cent dwell instead of angle of dwell. Per-cent dwell can be corrected to angle by use of the formulas given earlier. If the unit is made for dashboard use, it can be calibrated directly in dwell angle for the specific engine.

The rpm circuit is the only one that requires auxiliary equipment for calibration. Obtain one of the following pieces of test equipment and connect it as required: 1. a calibrated mechanical or electrical tachometer, connected as specified in the instruction manual; 2. an oscilloscope with a calibrated sweep speed, connected between the distributor primary terminal and ground (obtain the sync signal from the same point); or 3. a Strobotac with its beam flashed upon the fan-belt pulley of the engine.

Connect the proper wires from the engine analyzer to the plus and minus battery terminals and to the distributor primary terminal. Rev up the engine to full speed, measure the speed by means of the auxiliary speed indicator (tach, scope, or strobe) and adjust potentiometer  $R_1$ - $R_2$  until the engine analyzer reads correctly.

The Strobotac and auxiliary tachometer are direct-reading in rpm, but the oscilloscope reads period or time directly rather than rpm and its dial indication must be converted to rpm. Adjust the oscilloscope dials to obtain one or two full ignition cycles on the scope screen and measure the cycle period. The following equation gives the relation between period and rpm for various engines:

$$rpm = \frac{120}{\text{period (in sec.)} \times \text{no. of cylinders}}$$

If no auxiliary tachometer or oscilloscope is available, it is possible to calculate the rpm portion of the engine analyzer if a manual shift automobile is used. The engine speed can be calculated back from the automobile speed through the various gear ratios between the rear wheels and the engine crankshaft.

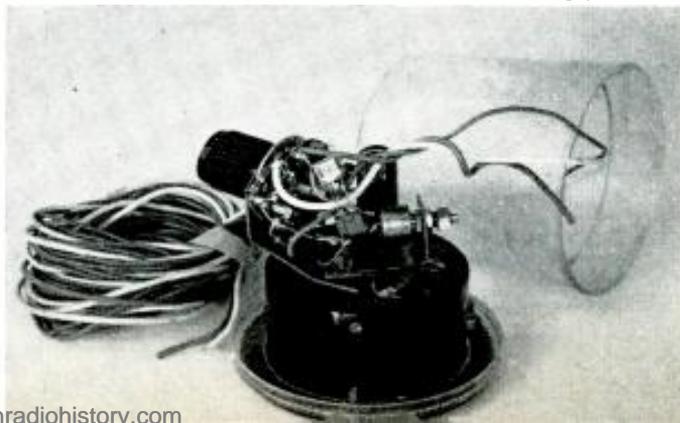
The voltmeter circuit requires no calibration since a 1 per-cent resistor is used for  $R_5$ .

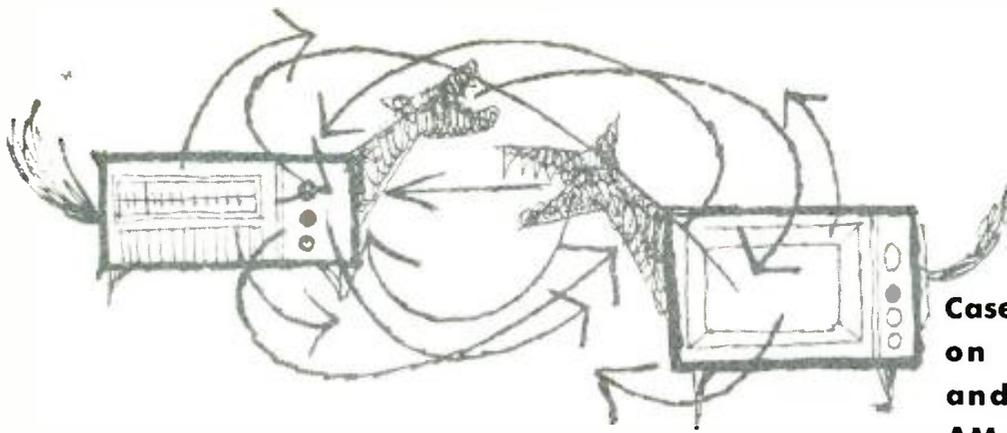
The dwell-circuit calibration is quite simple. The switch is thrown to "dwell" position and the engine is cranked in short bursts until the meter reads up-scale with the engine stopped.  $R_2$  is then adjusted for full-scale reading on the meter.

A pair of these units have been in use in the authors' automobiles for over 10,000 miles and have operated perfectly during this period. During a cross-country trip improperly operating points were discovered and replaced before a breakdown occurred.

The entire circuit is built within a housing that fits the meter. New scales have been drawn for the face of the meter.

In this model, all the components have been mounted on small metal brackets that are secured to the meter's binding posts.





Case histories shed light on the strange causes and cures involved with AM, FM, and TV reception.

# Interference Tough Dogs By GEORGE P. OBERTO

**W**ITH THE increasing number and variety of AM broadcast, short-wave, FM, TV, and other services in simultaneous operation today, difficulties due to interference have correspondingly increased. Although these many signals are carefully separated from each other so that they will not interact during transmission, there are numerous outside factors and conditions that will bring them into conflict, and these factors are seldom obvious. As a result, cases of interference tend to be tough dogs—the bane of the technician's existence.

No matter how difficult it may seem to meet these troubles, a cure is usually found if logic, past experience, theory, and careful observation are used to full effectiveness. However, there is such great diversity in causes and the ways of tracking them down that it is difficult to formulate a single troubleshooting technique. Perhaps more can be learned from evaluating individual case histories and noting how they were resolved.

## AM Broadcast

Some of the most commonly encountered interference problems involve broadcast radios. One that at first appears somewhat puzzling has been observed more than once on all types of radios, whether they use power transformers or are of the a.c.-d.c. type: automobile-ignition noise occurs on home AM reception. This can happen every time traffic passes through the street on which the receiver is located. Although ignition interference occurs over a broad range of frequencies, it is generally heavy enough to give trouble in the v.h.f. range—FM and TV—but not to broadcast receivers that are at a reasonable distance from the interference source.

When it does appear with AM signals, the likelihood is that spurious, high-frequency signals are being developed in the receiver's oscillator-converter stage. Parasitic oscillation generated here may be in the v.h.f. range, and ignition interference may react with this oscillation. This spurious signal then beats with the other signals present in the converter, and the interference is thus transferred to the desired signal.

The solution involves suppression of the parasitics. Low-ohmage resistors in

the grids of the converter stage will do the job. As shown in Fig. 1, a 47-ohm carbon resistor in series with the signal grid and another in series with the oscillator grid will do the job. Make connections close to the tube socket using short leads.

An unusual problem was encountered on an old (1939 vintage) set, which was otherwise operating well. A loud hum was riding through on all stations, but it was tunable. The hum disappeared whenever the radio was not set to receive a transmission. This radio did not have a built-in antenna, relying on an outside installation. A similar trouble could develop on any set, regardless of age, that uses an outdoor antenna. That the latter was involved became evident when the radio was checked in the shop; it had to be returned to its original location and original antenna for the symptom to appear.

An inspection revealed that the antenna system was in poor shape, with most connections badly corroded, including those to the ground rod. The lightning arrestor was almost shorted out. The arrestor was replaced and all connections were cleaned up. This eliminated the symptom.

What was happening was that the external ground, to which the chassis was connected, was making poor contact. The small 60-cycle current passing through the bypass capacitors across the a.c. line (Fig. 2) was therefore going to external ground through another path; the antenna system and the faulty

lightning arrestor. The latter, acting like a rectifier, mixed the 60-cycle signal with the incoming broadcast signal, resulting in hum. The hum path is shown in heavy lines.

It is not unusual to get an interfering short-wave transmission on local broadcast-band reception. A common headache of this kind occurs when a specific out-of-band station booms in on a specific, regular AM station. Reception on the latter becomes impossible whenever the interfering transmission is active.

Tracing signal in a set afflicted with this difficulty may show that the condition exists as far back as the converter stage. The strong, local, interfering signal will force its way in through the signal grid, although the latter is tuned only to the desired station. Since the oscillator, in addition to its fundamental frequency, is generating many higher harmonics, the interfering signal evidently beats with one of these harmonics to produce a beat at or near the intermediate frequency. This signal is then passed on through the i.f. section along with the desired one.

The cure is to block the interfering signal before it can get far enough to do the damage. A high-C, parallel trap is installed, as shown in heavy lines in Fig. 3, in series with the signal grid. This trap is tuned to the frequency of the interfering signal.

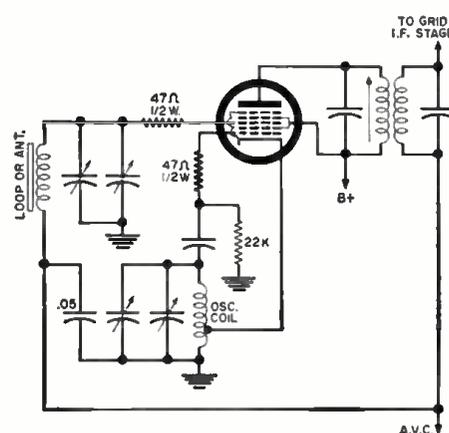
To find the proper frequency, a separate short-wave receiver can be used to identify the interfering signal. Most problems of this sort involve signals in the range from 1.8 to 6 mc., with the 75-meter voice and 80-meter code bands possible troublemakers.

A fixed mica capacitor, 140  $\mu\text{f.}$ , is used in conjunction with an adjustable inductance. The latter can be made up from a small, slug-tuned coil form, like the *National XR-50*. About 50 or 60 turns of #22 enamel wire will permit the coil to be tuned to trap out frequencies in the range from 3.5 to 4 mc. Peel off turns for higher frequencies and add turns for lower frequencies.

## Entry through Audio Stages

When sets suffer from interference that is evident no matter where the tuning dial is set, the unwanted signal may be entering through the i.f. system but is most likely getting into one of the audio stages directly. The interfer-

Fig. 1. Suppressor resistors (47 ohms) stop symptoms due to local parasitics.



ing signal may be of any frequency. The r.f. signal is usually picked up in the grid circuit of an audio stage, detected by some non-linearity in that stage, and amplified. This symptom obviously is not confined to receiving equipment; it could occur in a hi-fi amplifier or any other device that uses audio amplification.

The cure is to bypass or filter out the interfering signal at the point of entry. It is possible to use signal-tracing techniques to determine this point, but it is usually safe to apply the remedy to the first stage of audio amplification. If interference is reduced but still persists, other low-level, high-gain audio stages may be given the same treatment. Several ways of doing this are shown in Fig. 4.

For simple broadcast radios, the filter shown in heavy lines in Fig. 4A should be satisfactory. This will provide some roll-off of the higher audio frequencies, but not enough to make a difference on AM. In hi-fi systems, an r.f. choke in series with the tube's grid (2.5 millihenrys, Fig. 4B) should do the job without deteriorating the higher audio frequencies. Sometimes there is not sufficient room to accommodate the installation of this addition. In that case, a 47,000-ohm resistor (Fig. 4C), which is smaller, may do the trick.

### Short-Wave Reception

Interference to reception on short-wave sets, most often from lower-frequency signals like AM broadcasts, is not at all unusual. What's more, this may occur on anything from a simple set of the type used by a layman to an expensive communications receiver. Often it is not the receiver itself that is at fault.

In one case, a high-priced communications receiver suffered from heavy, broadcast-band interference in the range from 1.8 to 6 mc. It was first thought that the AM broadcaster was at fault; however, no interference showed up at all on the troubled set when it was checked in the shop, located just a few blocks up the street from the customer's home. The owner's antenna system was checked for deterioration or evidence of other defects, but none were found. A substitute antenna was tried anyhow, but without success. Next wave traps were tried, but again to no avail.

Finally a portable short-wave receiver was used as an interference probe. It was tuned to the points in the range from 1.8 to 6 mc. where the unwanted signals were noted to be coming in and moved about throughout the vicinity of the customer's home. A spot was finally found where the interference seemed to be worst. This also happened to be the point at which telephone lines led into the house.

The telephone service box, mounted on the outside of the house, was checked.

All connections looked dirty, with fraying evident on the wires. When the lightning-arrestor section was disconnected, by removing the two carbon elements, the interference disappeared

altogether. Actually, handling this property is outside the province of the service technician, so the results of the check were passed along to the local telephone company. A telephone repairman promptly went over the whole installation, putting things back in good shape. This resulted in a permanent cure.

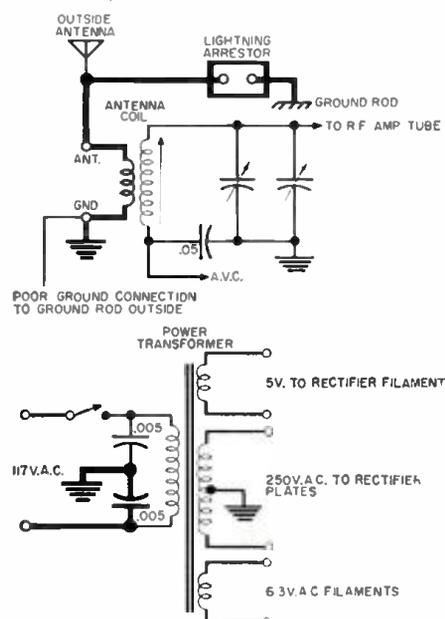
Evidently the lightning arrestor, particularly the two carbon blocks, was acting as a rectifier or non-linear device. Incoming, strong signals from nearby broadcast stations that were reaching this device were converted to spurious secondary signals, probably higher harmonics that fell in the short-wave band. These signals were being radiated well enough to be effective for a radius of a hundred feet or more.

The telephone problem calls to mind another unusual one involving a customer who was an enthusiastic experimenter. He brought a small, all-wave receiver into the shop with the complaint that there were severe whistles on the broadcast band as well as interference by AM broadcasts on short-wave reception.

After a complete check, which did not locate the fault, the set was returned to its owner. At this time, quite by coincidence, it was learned that he was working on a new crystal receiver with a transistorized audio amplifier. When the outside antenna that was being used with this experimental unit was disconnected, the trouble cleared up completely. The customer was simply instructed to switch out the crystal set's antenna when listening to his all-wave receiver. He was also strongly advised to check with his close neighbors to make certain that he wasn't bothering any of them.

When lower-frequency signals interfere with short-wave reception, it is not always because some outside agency is altering the frequency of the original,

Fig. 2. Sneak earth-ground path (heavy lines), set up by corrosion of outside antenna, caused tunable hum modulation.



interfering signal. Often the original signal enters through the antenna and causes havoc in some other way. Traps for various conditions and circuit configurations are shown in Fig. 5.

In some cases, the interfering signal is the same as the i.f. of the short-wave receiver. Many sets of the latter type use more than one i.f., and the higher one may fall in the broadcast band. In such cases, a series wave trap connected as shown by heavy lines in Fig. 5A and tuned to the intermediate frequency should be a satisfactory cure.

Often the strong, local AM broadcast signal enters through the antenna, but overloads the front end so that spurious signals of other frequencies are generated. The cure may still be obtained by trapping out directly the fundamental of the interfering signal. It may be necessary to use a combination of series and parallel wave traps for effective rejection, as shown in Fig. 5B. The combination to the left is used in conjunction with single-wire or unbalanced antenna-input systems. The configuration to the right, in which the elements of each trap are split up, is used with balanced antenna inputs.

Since all elements in each trap are adjustable, values for capacitance and

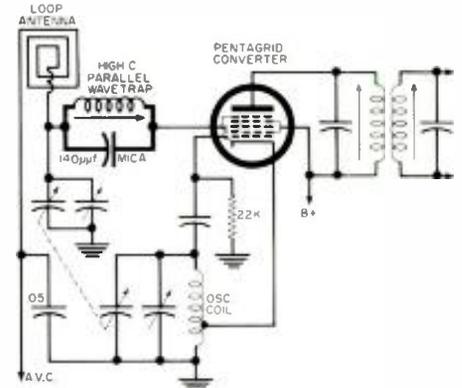


Fig. 3. A trap tuned to the undesired signal in the first-stage grid blocks interference entering through the antenna.

inductance can be quite broad. Trimmers that will tune from about 100 to 580  $\mu$ f. may be used for capacitors  $C_1$ ,  $C_2$ ,  $C_{11}$ ,  $C_{12}$ ,  $C_{21}$ , and  $C_{22}$ . Ferrite loop antennas, like Miller 2002, may be used as the inductors.

All traps are tuned to the frequency of the interfering signal. The configurations of Fig. 5B are also useful in a slightly more complicated type of situation. Sometimes more than one broadcast signal is giving trouble. Where two are involved, it is often possible to tune the series trap to one and the parallel trap to the other to achieve adequate rejection of both.

### FM Reception

A common source for interfering signals that intrude on FM reception is a TV transmission, usually on the lower v.h.f. band, or a TV receiver tuned to such a signal. One interesting case involved an expensive combination that included AM, FM, TV, and a phono-

graph. Reception on several of the local FM stations was being ruined by the same interference source, which was evident as a buzzing sound accompanied by a distinguishable voice signal. It was not too difficult to identify the ultimate origin of the unwanted sound; it was recognized as audio from the local TV station on channel 6, only two miles away.

After considerable checking, it was noted that the r.f. stage of the FM section was broadly tuned, so much so that it did not adequately reject the strong TV sound transmission, just below the FM band (87.75 mc.), which was overloading the front end. Further investigation showed that the same antenna was being used for both TV and FM reception—a single-bay conical pointed right at channel 6—and it was doing the dirty work. The cure proved easier than finding the trouble. A little careful re-orientation of the antenna cleared up the interference. Although it was rotated so that it no longer faced the TV transmitter squarely, there was no deterioration of reception on this nearby channel.

Another case involved teletypewriter interference on a v.h.f. police-alarm set, which occurred throughout the received band. Since the set used a conventional 10.7-mc. i.f. and teletypewriter gear operates close to this frequency, the cause was easy to localize: entrance was by radiation directly into the i.f. system. The interesting point is that the cure was also easy. Such measures as trapping and shielding might prove effective—but why use an elaborate technique when a simple one will serve? A slight re-alignment of the receiver to shift the intermediate frequency a little way from the interfering signal tuned out the latter with no impairment in reception. There is no sense in turning a difficulty like this into a tough dog—and some tough dogs are made, not born.

A portable AM-FM transistorized radio was brought into the shop with the complaint of a heavy hum or buzzing sound interfering with reception of the favorite FM station. As happens frequently, the symptom did not occur at all in the shop. Further checking in the customer's apartment was needed, but this was hampered by the fact that the interference occurred only intermittently. After several repeat visits to the apartment, the service technician arrived when the set was acting up.

Since the receiver was a portable, it was used directly as the interference probe. It was noticed that the symptom was at its worst when the east wall of the customer's apartment was approached. An investigation of the neighbor's adjoining apartment revealed a 21-inch TV set was located right against the wall, on the other side, and interference occurred only when the TV was turned on.

The TV receiver's horizontal-output amplifier was the culprit. This is a familiar situation with respect to interference on AM reception, but here is evidence that it can occur on FM too.

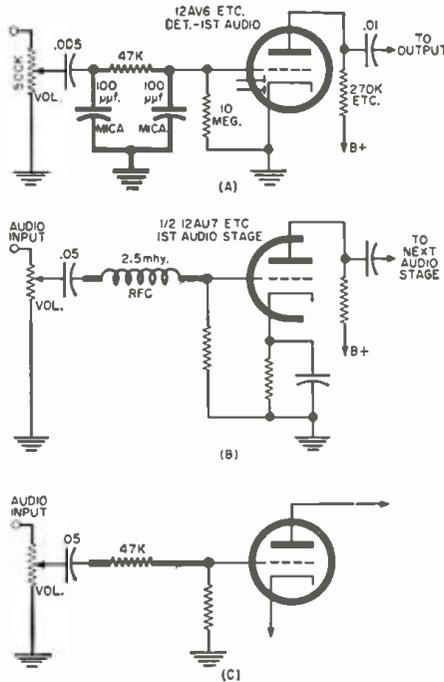


Fig. 4. Low-pass filters block audio-stage grid detection. One type (A) may be used in AM sets; others (B, C) preserve upper audio frequencies for hi-fi.

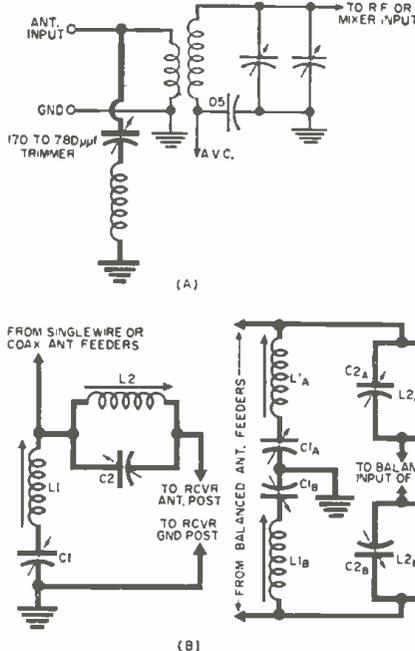


Fig. 5. Wave traps for short-wave sets: a single (A) series trap and combination series-parallel traps (B) for unbalanced (left) and balanced (right) antenna feed.

The most important step in effecting a cure was obtaining the cooperation of the neighbor. With his consent, a magnet was installed on the horizontal-output tube to eliminate Barkhausen oscillations, horizontal controls were re-adjusted, and the 300-ohm line inside the cabinet was re-dressed away from the horizontal circuit on the chassis.

#### A TVI Problem

An unusual and puzzling problem in interference on a TV set was encountered during a house call last spring.

The unit, a 21-inch console, exhibited severe cross-hatch interference at times on transmissions from the local channel 6. Since the problem was confined to the customer's home, it was thought that perhaps something inside the set itself was oscillating or that re-alignment might be needed. However, later on, the owner's 17-year-old son remarked that there was a ham operator living next door and wondered whether the latter could have anything to do with the problem.

The ham, a young fellow, was very cooperative. He permitted a portable TV set to be brought into his place as a probe and switched his transmitter to all ham bands during the process. Not a trace of interference could be induced on either the probing portable or the console next door. This possibility was abandoned and we returned to the home of the TV owner.

Almost at once, the interference returned. Acting strictly on a hunch, we made a return visit to the ham. His transmitter was turned off, but his communications receiver was on and tuned to a rock-and-roll broadcast on a local station operating on 1480 kc. When the portable TV probe was turned on in his home, the interference was clearly evident on this set, and the interference disappeared as soon as the communications receiver was turned off.

The amateur was using his 75-meter dipole as a receiving antenna for the communications receiver. When he tuned to any station other than the one on 1480 kc., the interference disappeared. When he was tuned to 1480 kc. but disconnected the dipole, the symptom also vanished. The cure was achieved when the ham agreed to switch in a shorter antenna for listening to the offending station. This also cleared up the problem.

What in blue blazes was happening? Why? How? With a mutually satisfactory solution already achieved on a practical basis, it was not possible to investigate further at the inconvenience of the people involved. However, one may speculate on possibilities. The dipole was obviously radiating some signal that wound up causing the interference, in one way or another. Was it being overloaded and re-radiating some high harmonic of the received 1480-ke. signal? It would take at least the 55th harmonic of this transmission to fall into the bandwidth of channel 6 directly. However, the dipole was pointed right at the troublesome AM station, which was only half a mile away. Perhaps the antenna, in conjunction with components in the input circuit of the receiver, set up a tuned circuit that was being forced into oscillation at some other frequency. Perhaps the local oscillator was in some way involved.

The many possibilities serve to illustrate the complex nature of interference problems, particularly where television is involved. This is a matter that cannot be covered briefly, as one part of a broad article. It merits a separate treatment, and perhaps it can be covered in a later article.

# MAKING COLORS ELECTRONICALLY

Three carefully adjusted electron beams excite three primary phosphors to reproduce all colors.

**A**LTHOUGH all color combinations and tones recognizable to the eye can be produced with remarkable fidelity on a color-TV receiver, this is achieved with no more than three primary color sources. These are obtained by precisely aiming the beams from three electron guns in the neck of the color CRT so that each can excite only one of the three color phosphors deposited on the face of the tube. The three-gun assembly appears diagonally across this month's cover.

To obtain the high degree of color fidelity that is possible, the receiver must be adjusted carefully, as is being done by the technician in the lower, right-hand corner of the cover. Fortunately, he does not have to check all possible color combinations, which are infinite. He is assured that the set will do its job faithfully if he knows that the three primaries are balanced out in a given way. He can determine whether this balance exists, or adjust for it, simply with reference to a few colors that may be easily recognized and identified. The reference colors will generally be among those in the cover's background.

However, as produced by such conventional color generators as the RCA WR-64A being used by this technician, the comparison colors appear as separate stripes rather than blocks.

Fig. 1. The basic colors, including black and white, with the electron guns that must be emitting to produce them.

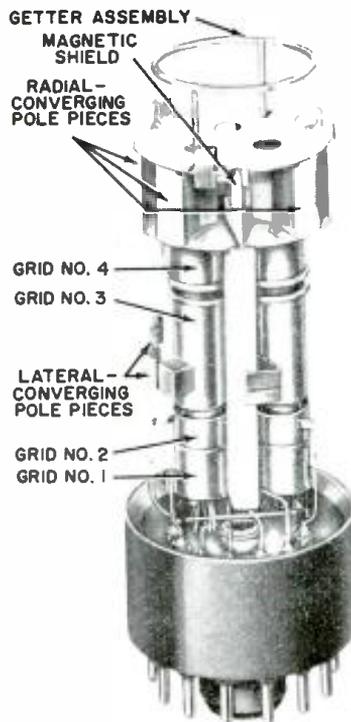
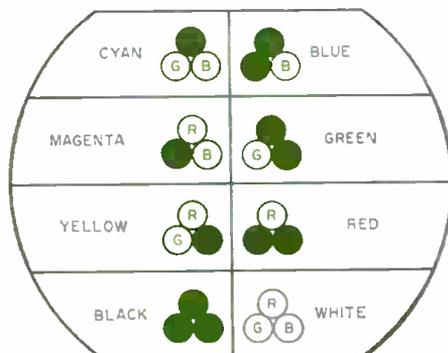


Fig. 2. The triple-gun assembly used in the neck of modern color picture tubes.

The electron gun on the cover is an assembly of three electrostatic-focus guns spaced 120 degrees apart when viewed head-on through the circular getter ring. The latter is identified at the top of Fig. 2. Although these guns appear to be parallel, each is tilted slightly inward toward the top, so that lines drawn from them would eventually converge at a single point. This point is actually slightly before the phosphor-coated faceplate of the tube. As a result, the three beams strike the faceplate at three separate but closely spaced points that form a tiny triangle. A shadow mask, covered with many minute, accurately placed holes, is located between the faceplate and the gun assembly, but closer to the faceplate to assure that each beam pro-

duces the appropriate primary color.

In a black-and-white picture tube, a single phosphor is used, and it is coated on the inside of the faceplate in a uniform film. A color CRT uses three phosphors, each of which will glow in a different primary color when excited. These are deposited, not as three separate films, but in a regular pattern of tiny dots covering the entire faceplate. The pattern consists of a series of triangles, each made up of three phosphor dots closely spaced to match the points at which the beams from the three guns will strike.

The radial-converging pole pieces of Fig. 2, one on each gun, are "aiming" devices. They are used to provide individual convergence control of each electron beam radially. Supplemental, horizontal control of the three beams is provided by the lateral-converging pole pieces. For the rest, design of each gun is quite similar to that of the single guns used in many monochrome picture tubes. The red, green, and blue guns are identified on the cover. The individual electron beams they produce speed screen-ward through the corresponding exit apertures.

All shades of white, gray, and black, as well as all colors, are obtained by controlling the relative intensities of the red, blue, and green beams, which

(Continued on page 121)

Fig. 3. RCA WR-64A generator produces color-bar, dot, or crosshatch patterns.



COVER STORY



Fig. 1. Motorola's "Private Line" vehicular 2-way radio, one of the Motrac series.

# ADJUSTING COMMUNICATIONS TRANSMITTERS

## PART 2

By EDWARD M. NOLL

**How r.f. tuning is done on a specific unit, and how audio level is set to avoid overmodulation.**

IN ORDER to properly service two-way radio equipment it is necessary that the electronic technician be capable of tuning transmitters. This knowledge is required in order to pass the radiotelephone license examination. Only a holder of a second-class radiotelephone license or better is permitted by the FCC to measure transmitter power, frequency, and modulation levels. In our previous article (March issue) we considered, in a general way, the steps involved in tuning the r.f. section of a transmitter. Let us now be more specific and follow the procedure recommended for commercial transmitters.

A *Motorola* mobile FM two-way radio unit is shown in Fig. 1. The schematic of the r.f. and modulator sections of the transmitter is shown in Fig. 2. The transmitter consists of a crystal oscillator, two doublers, a tripler, and a final power amplifier. Crystal frequencies fall into the range between 2.083 and 4.16 mc., and are multiplied by a factor of 12. The output frequency of the doubler-driver is somewhere in the 25

to 50 mc. band as a function of the crystal oscillator frequency. The power amplifier increases the FM-modulated signal to 30 or 50 watts as a function of the particular assignment. The output of the transmitter is coupled to the antenna system through a harmonic filter,  $Z_{in}$ . An antenna change-over relay switches the antenna from receiver to transmitter.

The output of the crystal oscillator is phase modulated by the voice-frequency components. The grid of the modulator is supplied with audio signal from a transistor audio amplifier and a clipper whose function is to limit modulation

peaks. By doing so a high average deviation can be obtained without exceeding 100% modulation on peaks. The level of the modulating audio is set by the IDC control.

Two crystal oscillators are employed to permit two-channel operation of the transmitter. A frequency control, capacitor  $C_{100}$  or  $C_{110}$ , is associated with each crystal. One of the first steps in tuning a transmitter is usually to set the oscillator to its precise frequency. A heterodyne frequency meter may be coupled to the oscillator and used to adjust capacitors  $C_{100}$  and  $C_{110}$  to secure the desired low frequency.

In most tune-up procedures it is customary to set the crystal oscillator as close as possible to the desired frequency. The final frequency check is made later by coupling the frequency meter to the transmitting antenna after the entire transmitter has been tuned. The frequency meter is then used to measure the actual center frequency of the radiated FM wave. If it is not in accordance with the assignment made, it is necessary to re-adjust  $C_{100}$  and  $C_{110}$ .

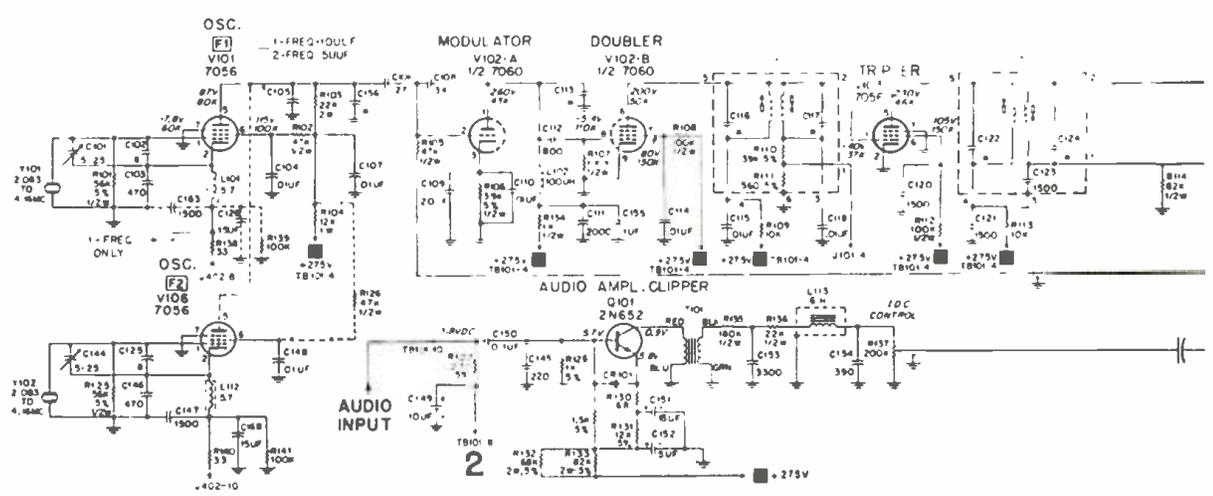


Fig. 2. Transmitter portion of the equipment shown in Fig. 1, including the r.f., speech, modulator, and output circuitry.

to place the transmitter precisely on its assigned frequencies.

A pentode crystal oscillator with an untuned output is employed. It supplies signal directly to the modulator and a following frequency doubler. No tuning adjustments are associated with the transmitter between the oscillator output and the input of the doubler.

The first tunable transformer is  $T_1$ , located between the doubler and the following tripler stage. A test jack,  $J_{101-1}$ , is available for measuring the tripler grid current. The test meter evaluates the grid current by measuring the voltage drop across resistor  $R_{111}$ . The primary and then the secondary tuning slugs are adjusted for maximum current reading. Maximum grid current flows when there is maximum excitation to the grid of the tripler. The resonant circuits have some interaction on each other, and therefore the two slugs should be re-peaked carefully.

The meter is now inserted into jack  $J_{101-2}$  to measure the grid current of the doubler-driver stage. The primary and secondary tuning slugs of  $T_2$  are adjusted for maximum grid current reading.

Next, the power amplifier grid current is measured by means of jack  $J_{101-3}$ . Inductor  $L_{103}$  is tuned for maximum grid current and then inductor  $L_{101}$  is adjusted for maximum grid current. As before, the two controls must be re-peaked several times because of interaction.

Next, the test meter is connected to test jack terminals  $J_{101-7}$  and  $J_{101-8}$  which connect the meter across a resistor ( $R_{121}$ ) in the plate circuit of the power amplifier. The final stage is set for low power operation by using a reduced value of screen voltage. To do this, switch  $S_{101}$  is opened. Three adjustments are associated with the plate circuit of the power amplifier. These are the plate tank capacitor,  $C_{106}$ ; the antenna trimmer,  $C_{108}$ ; and the coupling between the plate tank coil,  $L_{106}$ , and the antenna coil,  $L_{107}$ .

In the initial adjustment, loose coup-

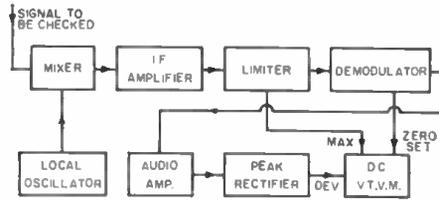


Fig. 3. An FM deviation meter, shown in block diagram, is a calibrated receiver.

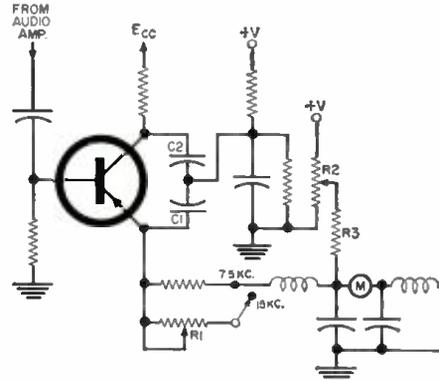


Fig. 4. Transistorized, peak-reading voltmeter used in instrument of Fig. 5.

ling is used between the two coils. (Although the schematic does not indicate it, the two coils can be moved apart.) The antenna trimmer is adjusted for minimum plate current reading. Next, the plate capacitor is adjusted for minimum plate current reading. The transmitter is switched to its high power output position. (Maximum screen voltage is applied to the power amplifier.) The plate voltage is set to the value that provides the desired power output. Note, if an output of 50 watts is to be obtained a plate voltage of 700 volts is needed. For 30 watts, 430 plate volts are needed. The plate tank capacitor and the antenna trimmer capacitor are again retuned for minimum plate current.

### Final-Stage Tuning

The next step in tuning the transmitter is to peak the final stage with power

being delivered to the antenna. The antenna coupling is now increased by moving the coils closer together. The tank capacitor is retuned for minimum current. The antenna trimmer is now tuned for maximum plate current. The increase of plate current as the antenna is tuned indicates that power is being absorbed by the antenna as the trimmer brings it into resonance. Watch the plate current meter as this is being done. In the case of the *Motorola* transmitter, maximum current is 140 milliamperes for 30 watts output and 130 milliamperes for 50 watts output. To increase or decrease the amount of current drawn, increase or decrease the coupling and then retune the antenna trimmer for maximum and the plate tank for minimum.

In summary, the adjustment procedure for the final power amplifier involves the transfer of energy into the antenna system with the power amplifier drawing the rated plate current or less, and the plate tank capacitor tuned to exact resonance. Remember that plate power input is now the product of the plate current reading and the plate voltage supplied to the stage.

### R.F. Output Indicator

Some form of r.f. indicator, such as a wattmeter or field-strength meter, is also helpful in tuning the final power amplifier and antenna system of a transmitter. The preferable wattmeter type is one that can be inserted in the transmission line between the transmitter and the antenna. This type of meter can be used for a reading without disturbing the match between the antenna and the transmitter, and permits the transmitter to operate in its normal manner. A field-strength meter also permits normal operation while measurements are being made. The output indication on the field-strength meter, however, is a relative measurement while the wattmeter actually measures the r.f. output of the transmitter in watts.

The tuning of a transmitter with the  
(Continued on page 120)

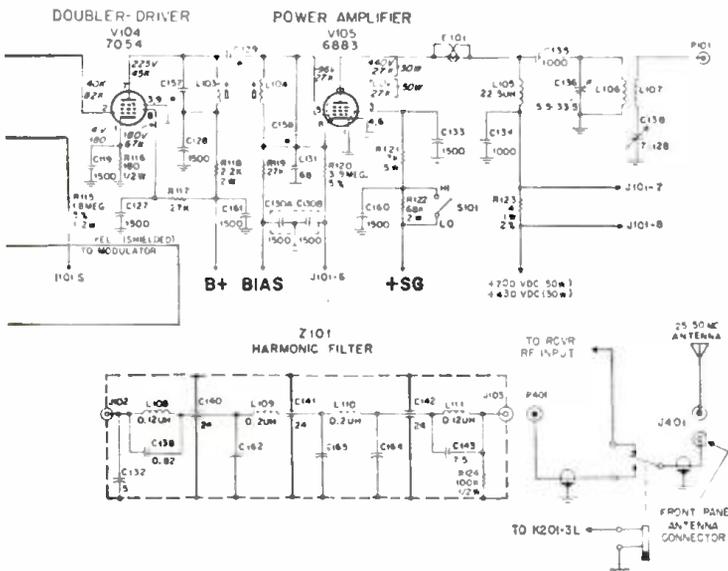


Fig. 5. The Gertsch Peak Modulation Deviation Meter, Model DM-3, is typical of deviation monitors used to set audio clip-pers. This setting keeps modulation within permissible limits.



# Tube Inventory for Service Shops

By **ROBERT A. LARSEN**  
Windsor Television, Inc.

**Make sure you have all needed types in the shop  
and in the caddy without tying up too much cash.**

**T**HE LARGEST, single capital investment for a television service shop is likely to be its stock of tubes. Due to a sharp decrease in over-the-counter sales in recent years, doubtless related to the growth in popularity of do-it-yourself tube checkers, tube movement or turnover for the average shop is not as good as it used to be. Wise shop owners therefore have all the more reason for keeping a careful watch over their inventory to avoid over-stocking of slow movers, in addition to the regular, also serious problem of not running out of stock on good movers.

The tube inventory listings shown here have been prepared from the actual records of a television service shop in a suburban, metropolitan v.h.f. area, and were carefully compared with such other statistics as stock-movement figures available to distributors. These listings have been devised to act as a guide not only for stocking and re-ordering for the shop itself, but also for the tube caddy.

There are two "quantity" figures following each tube type. The first indicates the number of tubes of the particular type moved in each thousand of tubes turned over. Actually this figure is based on a greater number of tubes moved than one thousand. The figure was averaged for a full year's activity. For instance, the first number following the listing for the 6BQ7 is 45. This indicates that 45 out of every

1000 tube sales were 6BQ7's. The amount the average shop turns over is probably something between 1500 and 2000 tubes per year. If this is true, the dealer could expect to sell about 68 to 90 6BQ7's during the year.

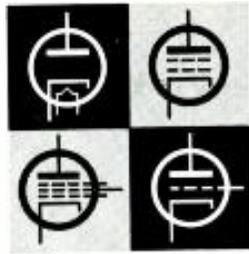
Some tubes have been deleted from the list as it appeared in earlier years because of obsolescence. Others are still carried because there is some movement although it is very low. For example, where the rate of turnover is only one in a few thousand, the tube type is still listed but the figure given in the first "quantity" column is a zero.

The second "quantity" figure gives the number of tubes of each type to be used in stocking the tube caddy. Since the average caddy holds only about 150 tubes, the second figure was drawn up with this capacity in mind. However, some alert dealers carry two tube caddies. One, for faster moving types, is brought into the customer's home on every outside call. The other, the slower movers, stays in the service truck so that, if a tube in it should be needed, there is no need for an extra trip to the shop. Optional types that may be put in the second caddy are designated by an asterisk (\*).

Proper inventory control is one of those business details which, if adhered to, will help the shop owner realize greater return from a smaller investment. To make it easy on yourself, get into the habit of checking your inventory period-

Type	Quantity	Type	Quantity	Type	Quantity	Type	Quantity	Type	Quantity
0Z4	10	3CF6	1	5AV8	1	6AQ5	14	6BD6	0
1AX2	1	3CS6	2	5BK7	1	6AQ6	0	6BE6	5
1G3/1B3	15	3CY5	0	5BQ7	1	6AR5	0	6BF6	0
1R5	5	3DT6	1	5BR8	1	6AS5	2	6BG6	8
1S4	1	3Q4	0	5CG8	1	6AS7	0	6BH6	0
1S5	2	3Q5	0	5CL8	3	6AS8	4	6BH8	1
1T4	1	3S4	1	5CQ8	1	6AT6	2	6BJ6	1
1U4	3	3V4	1	5J6	1	6AT8	2	6BK5	1
1U5	3	4AU6	1	5T8	1	6AU4	15	6BK7	8
1V2	2	4BC5	0	5U4	100	6AU5	1	6BL7	6
1X2	15	4BC8	1	5U8	5	6AU6	30	6BN4	1
2BN4	1	4BN6	0	5V3	1	6AU8	3	6BN6	1
2CY5	4	4BQ7	3	5V4	2	6AV5	1	6BN8	0
3AL5	1	4BS8	1	5X8	1	6AV6	8	6BQ6	35
3AU6	1	4BU8	1	5Y3	5	6AW8	6	6BQ7	45
3AV6	0	4BZ6	2	6AB4	2	6AX4	28	6BR8	1
3BC5	1	4BZ7	1	6AC7	15	6AX5	1	6BS8	3
3BE6	0	4CB6	1	6AG5	8	6AX8	1	6BU8	1
3BN4	1	4CS6	1	6AH4	1	6AZ8	1	6BX7	1
3BN6	2	5AM8	1	6AH6	1	6BA6	7	6BY5	1
3BU8	1	5AN8	2	6AK5	1	6BA8	1	6BY6	0
3BY6	0	5AQ5	2	6AL5	16	6BC5	8	6BZ6	6
3BZ6	3	5AS4	1	6AM8	1	6BC7	1	6BZ7	10
3CB6	3	5AT8	1	6AN8	3	6BC8	3	6BZ8	1

# 1961



# 1961

ically, if you are not doing so now. Small shops will find it best to keep a master list of tubes to be stocked, based on the one shown here, and to re-order on a regular basis, filling in those used to meet their own minimum requirements.

**EDITOR'S NOTE:** Readers who have been following this annual feature regularly will note that it breaks with the approach followed in past years in more ways than one: The compiler of this reference is not the one who has traditionally done the job. The consistent trend toward an increase in the number of listings has, for the first time, been reversed. Two different sets of quantity ratings have been included. The order of magnitude of the ratings themselves has been changed drastically. What does all this mean?

As to the first point, Murray Barlowe, who has been the faithful keeper of this list since its inception, has moved on to a new career in the highly diversified world of electronics that has nothing to do with service. Taking his place is the capable Robert Larsen, owner of one of the most successful shops in his area and the respected holder of more than one office, past and present, in his local and state service associations. Bob has decided to handle the problem in a different way. The result is something that is certainly no less useful.

As to the reduced listing, Bob has already cited one good reason: the decrease in over-the-counter sales makes it more important than ever that the service dealer avoid tying up cash in over-stocking. This alone does not account for the fact that, after the *addition* of newer types, this year's total comes to 235 whereas last year's went to 268, not including a separate listing for hi-fi. Of course, there have been some drop-outs of obsolescent types, as in the past. But additions have always been greater.

The axe has been applied mercilessly to all "special" types, like those used primarily or exclusively in auto radios or in industrial, color, u.h.f., and hi-fi equipment. Does this reduce the guide's value? We think not. The deletion can be justified simply by recalling the reason for running the inventory to begin with. It was made necessary by the bewildering profusion of tube types that came into regular use. When only a few basic types existed, there was no need for guidance.

Altogether there have been about 60 deletions in the five categories mentioned, an average of about a dozen types in each group. No dealer should have trouble determining his own requirements, if any, in each category. In fact, an "average" listing would be meaningless. For example, one particular shop may do no industrial or u.h.f. work at all.

As noted, the first quantity figure in each case is based on turnover rate. Thus it is bound to be out of step with earlier listings, which were minimum-quantity figures. For example, the highest figure for any type last year was 10. This year the 5U4 comes in with a whopping rating of 100!

This does not mean you should carry 100 5U4's. No list is better than the judgment with which it is used. The total number of tubes you turn over in a year, weighted against the frequency with which you re-order, can give you a correction factor for adjusting the rating.

Dealers who liked the way the old method worked and are reluctant to give it up don't have to. A close approximation of the old ratings can be obtained easily in this way: Divide new ratings by 3, but allow no figure higher than 10. Raise any fraction to the next highest whole number.

A final word: stock only latest versions of each type, since it will replace its predecessors. For example, the 5U4GB will meet all electrical requirements for any 5U4 type and, physically, will create no space problem.

-30-

Type	Quantity		Type	Quantity		Type	Quantity		Type	Quantity		Type	Quantity	
6C4	3	1	6DT6	1	*	6X4	2	1	12AZ7	1	1	17AX4	5	*
6CB6	35	3	6EA8	2	1	6X8	7	1	12B4	2	1	17D4	1	
6CD6	10	2	6EB8	1	1	6Y6	0		12BA6	5		17DQ6	2	*
6CF6	2	1	6EM5	1		7AU7	2	1	12BD6	1		19AU4	1	*
6CG7	33	3	6EW6	1		8AW8	1	*	12BE6	5		19BG6	0	
6CG8	1	1	6J5	4	1	8CG7	1	*	12BF6	0		19T8	0	
6CL6	1	1	6J6	12	1	8CM7	0	*	12BH7	15	1	25AX4	1	*
6CL8	1		6K6	1	1	8CX7	0		12BK5	0		25BK5	0	
6CM6	0		6L6	1		9AU7	0	*	12BQ6	5		25BQ6	3	*
6CM7	7	2	6S4	10	2	9BR7	0		12BY7	5	1	25CD6	1	1
6CN7	0		6SA7	1		10DE7	2	1	12BZ7	1	1	25CV6	1	
6CQ8	5	1	6SJ7	1	*	12AD6	1		12CA5	1	*	25DN6	1	
6CR6	0		6SK7	1	*	12AF6	1		12CU5	1		25L6	5	*
6CS6	1	1	6SL7	1	*	12AL5	0		12D4	1		25W4	1	*
6CS7	0	1	6SN7	47	3	12AQ5	0		12DQ6	7	1	35B5	1	
6CU5	1		6SQ7	2	*	12AT6	2	1	12L6	1	1	35C5	2	
6CY5	2		6SR7	1		12AT7	6	1	12SA7	1		35L6	2	
6CZ5	0	1	6T8	13	2	12AU6	3		12SK7	2		35W4	10	
6DA4	1		6U8	40	4	12AU7	30	2	12SN7	1	1	35Z5	10	
6DE6	3	1	6V3	1		12AV6	5		12SQ7	1		50B5	1	
6DG6	0	*	6V6	10	1	12AV7	7	1	12V6	1	*	50C5	17	
6DQ6	23	2	6W4	15	2	12AX4	18	1	12W6	1	*	50L6	7	
6DS5	0		6W6	14	1	12AX7	2	1	12Y4	1		5642	1	

# TV Commercial Silencer



By **ROBERT J. MACK**

**Build this simple circuit that will kill TV sound for one minute when a remote button is depressed.**

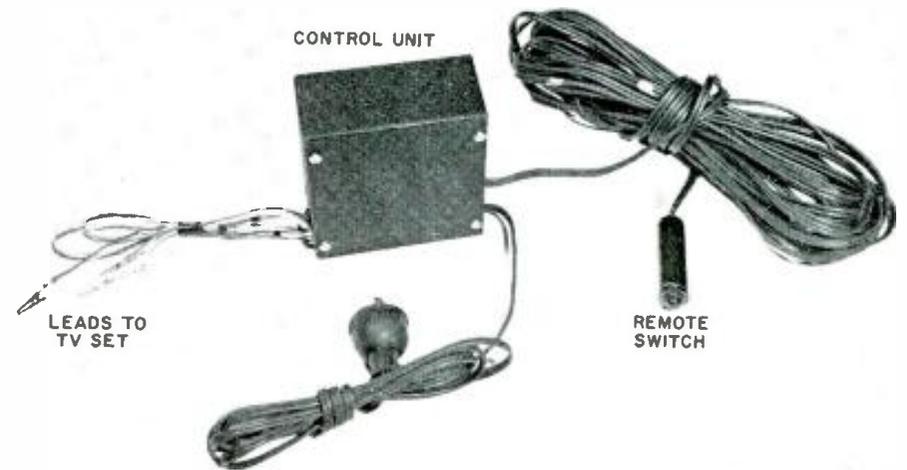
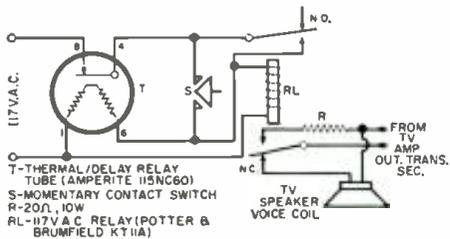
IT IS no longer necessary to "suffer" through television commercials. An inexpensive electronic device can silence the sound portion of the commercial and then automatically restore the sound when the "sponsor's message" is ended.

The device is simple to make and install and provides virtually "free" service as it consumes a negligible 3 to 6 watts. When listening to program material, the device is totally inoperative. It operates only when activated during commercials.

### Operation

Operation of this device is based upon the use of a relay and a thermal-delay tube. When the unit is activated by a switch, the relay opens the TV sound circuit, cutting off the commercial. At the same time, the thermal-delay tube is activated. This is a heat-operated switch which becomes operative in

Circuit of the commercial killer shows the use of a thermal-delay relay tube which operates a relay that disconnects the loudspeaker from the TV set's output transformer. A dummy load is then switched into the circuit, taking the place of the normally used loudspeaker.



The control unit is housed in a small 4" x 4" x 2" metal cabinet with a built-in chassis. Three leads from the control unit connect it to the TV set. A.c. line cord is employed to connect the remotely located insulated push-button switch.

about one minute. After the minute is over, the heat switch opens, de-energizing the relay and restoring the television sound.

In normal operation of the TV set, the TV speaker voice-coil circuit is completed by the normally closed contacts (N.C.) of relay *RL*. The relay and the delay tube (*T*) are inoperative since switch *S* and the normally open (N.O.) relay contacts energizing them are open.

When a commercial comes on, switch *S* is closed momentarily. This activates *RL* which (1) closes the normally open contacts, maintaining *RL* in an energized condition and energizing the heat-

ing element of the thermal-delay tube *T*; (2) opens the normally closed contacts, opening the TV speaker circuit; and (3) closes the other set of contacts of the normally closed relay contacts, placing a resistive load across the TV amplifier output.

After about one minute, the delay-tube contacts open, breaking the relay coil circuit and the delay-tube heating element circuit. All conditions now reverse: the relay contacts in the speaker voice-coil circuit close, restoring the TV sound; the other relay contacts return to their normally open position. When the delay-tube heating element cools

sufficiently (usually in 10 to 20 seconds) the delay tube contacts return to their normally closed position. Conditions are now the same as they were initially. It should be noted that because of the presence of a heating element in the circuit, the device requires a cooling period before it will again provide the full one-minute delay time. This is not usually a problem, however, as commercials are normally adequately spaced. If the device is activated before it has cooled completely, the delay time will be less than one minute.

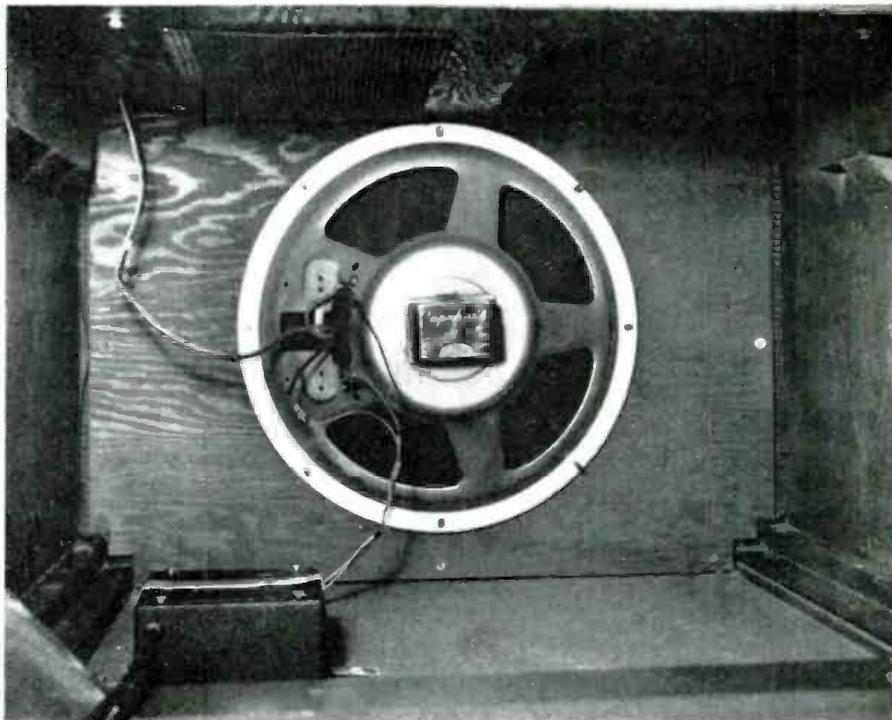
#### Construction

Construction of this silencer device is simple as there are few parts. These can be conveniently housed in one of the small (4" x 4" x 2") commercial-type metal cabinets. The type with a built-in chassis allows the parts to be easily mounted on a firm support.

Layout and wiring are not critical. The parts and cabinet specified allow adequate clearance for mounting and wiring. Before proceeding, it is well to observe two precautions: (1) Neither the metal chassis nor the metal case are part of the electronic circuit. No connection of any kind is to be made to these metal parts. (2) The number of the pins on the miniature 9-pin socket is given for the *bottom* view.

The first step is to locate and mount the relay and the thermal-delay-tube socket. Keep the relay bracket as far to one end of the chassis as possible to allow maximum clearance between the relay terminal strip and the delay tube when it is inserted in the socket. Next, move the delay tube socket as far toward the other end of the chassis as it can go and still have firm support.

After the relay and delay-tube socket are mounted, three 1/4" holes are drilled in the case. One is for the 117-volt a.c. line; the second is for the line to the switch, which is placed at the viewing position; and the third is for the speaker voice-coil leads. The power line and the switch line carry 117 volts a.c., so their holes are drilled in one end of the case. The voice-coil leads carry little current and this hole is drilled in the opposite end of the case. Each hole is grommeted



The control unit used by the author is shown here mounted inside and on the bottom of the TV cabinet. An aluminum strap holds the unit down. One lead is disconnected from the set's speaker and connections are made to the voice-coil circuit as described.

for safety. The parts are now ready to be wired.

#### Testing & Installation

The completed device can be tested as follows: Connect the two voice-coil leads from the normally closed relay contacts to a flashlight battery and bulb in series. The bulb should light. Now connect the a.c. power and press S. The relay should close and the bulb go out. After about one minute, the relay should open and the bulb light again. If this sequence occurs, the device is wired correctly and is ready for installation. If any part of the sequence fails to occur, the wiring should be rechecked.

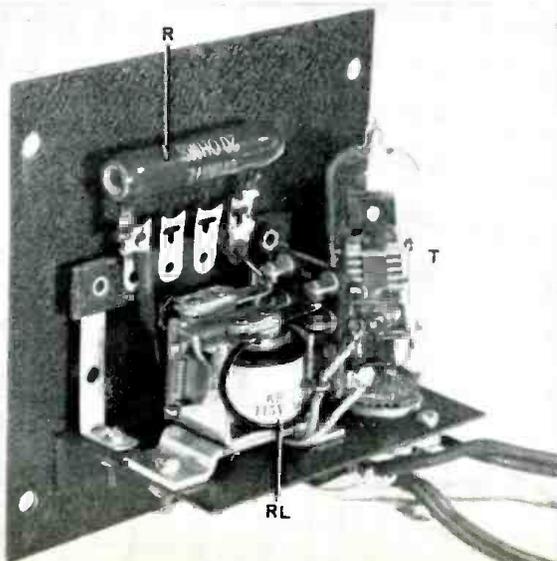
Installation is easy. The box will usually fit inside the TV speaker compartment. If it does not, it may be placed anywhere in the TV cabinet except near components which generate excessive

heat. Observe the usual precaution of first disconnecting the TV set. If desired, the box may be mounted external to the TV cabinet.

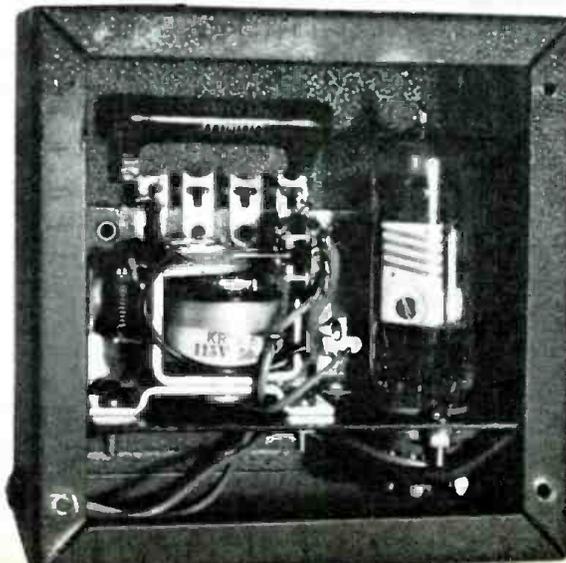
To connect the voice-coil circuit, unsolder (or cut if necessary) one of the leads from the secondary of the TV set's output transformer to the speaker voice-coil lug. Connect this lead to the armature of the relay. Connect the lead from the voice coil to the normally closed relay contact. The lead from the load resistor is connected to the other side of the voice coil (which is still connected to the output transformer). To install the switch, merely run the switch line under the rug or along the baseboard to the viewing position. When the a.c. plug is connected, the device is ready for use. You are now ready to enjoy television without commercials—at the press of a button!

-30-

The thermal-delay tube, relay, and resistor are first mounted on the small chassis bracket that is affixed to cabinet panel.



The control unit is shown here with the cabinet cover removed. Note that only three components are utilized in the unit shown.





# DIODES ARE DIFFERENT

By J. H. HAZLEHURST / **Some good advice for the experimenter or audiophile who wants to substitute silicon diodes for rectifier tubes.**

**T**HE USE of silicon diodes in power rectification has grown greatly in the last few years. This, of course, is due to the obvious advantages of compactness, reduced heat, relatively high current ratings, and competitive cost. In bridge circuits there is the additional benefit of saving the cost of separate filament transformers.

These diodes, however, have some peculiarities which are not widely known, specifically with respect to back resistance. As a result, some people have had what appears to be bad luck with them, particularly when they are used in series strings. A knowledge of these problems is necessary for the proper application of these devices.

## A Practical Example

Let's illustrate this with a practical example. Figure 1A shows a power supply that is typical in many hi-fi amplifiers. Now, if the rectifier tube gets old and tired, probably the cheapest and easiest thing to do is replace it. However, this is the point at which many do-it-yourself enthusiasts decide that the time is at hand to try semiconductor diodes and perhaps reduce the cabinet heat about 25 per-cent.

Now the first thing is to decide how many rectifiers to buy. Most of the low-cost diodes are rated to supply 200 or

500 milliamperes, and have a peak inverse voltage rating of 400 volts. In this case the decision is to use the 200-ma. units. Then our experimenter knows that in a full-wave supply such as this, the peak inverse voltage that the diode must withstand is 2.8 times the supply voltage, so he multiplies 2.8 by 375 and gets 1050 volts. Certainly three diodes each with a 400 p.i.v. rating ought to do this nicely with plenty of safety factor. So he makes up the supply shown in Fig. 1B. Now, as a matter of fact, this supply may work just fine, but sometimes not, because there are three serious mistakes made here. Two of these should be easy to spot, but the third is likely to be missed by all but those who are very familiar with the characteristics of silicon diodes.

In the first place, silicon or selenium diodes should work into a choke-input filter for best results. In this case, taking out the first filter capacitor might drop the output voltage of the filter too far for proper operation of the circuits. To meet this difficulty, a protective resistor should be installed between the diodes and the first filter capacitor. This resistor should be about 30 ohms per diode on one side of the supply. With three diodes 100 ohms would be a good value. This will cause a voltage drop, but this is about offset by the fact that

the voltage drop across the diodes is less than across the tube which is being replaced. Without this protection, the initial current surge into the first filter capacitor which, momentarily, looks like a short circuit, may exceed the rating of the diode. It is amazing, though, to see how diodes sometimes stand up under this beating when the capacity into which they feed is not unusually high.

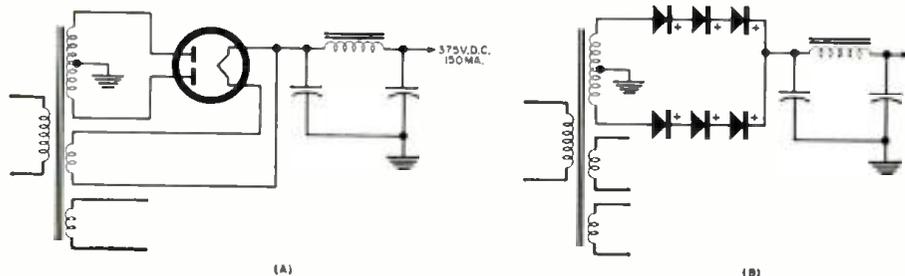
The second mistake our friend made was in computing the peak inverse voltage. This is *not* based on the output voltage of the filter, but on the a.c. voltage across the diodes. In this particular case, it would probably be in the neighborhood of 425 or 430 volts. When we multiply this by 2.8, we are right at 1200 volts which should be maximum for three diodes each with 400 p.i.v. rating. So there goes our safety factor that we might have thought actually existed.

When designing a supply of this sort with a transformer that we might have on hand, a good rough rule-of-thumb is to measure the open circuit voltage across half the transformer secondary, multiply this by .95 and then by 2.8 in order to compute the peak inverse voltage applied to the diodes.

Now we have our protective resistor, and while our diodes are operating at their limit, this limit is not being materially exceeded, so won't this supply work all right? Well, it may, and then again it may perk along for a while and then fail. When we check it out, we may find all three diodes on one side are short-circuited. When this happens, we may decide that maybe we shouldn't have worked so close to the p.i.v. limit and should use four diodes on a side. This runs up the expense and we begin to wonder if we should have stayed with

(Continued on page 98)

Fig. 1. Typical power supply using (A) a rectifier tube and (B) substitute diodes.



# Changes In WWV Standard Broadcasts

**Bureau of Standards transmissions now include a special time code for use in world-wide scientific observations.**

AT THE BEGINNING of this year, the National Bureau of Standards retarded the time signals broadcast from radio stations WWV and WWVH by 5 milliseconds, and at the same time started broadcasting on a permanent basis from WWV a special timing code which gives the day, hour, minute, and second (Universal Time) coded in binary form. The 5-msec. retardation brought the time signals into closer agreement with other standardized frequency broadcasting stations throughout the world.

The United Kingdom and the United States began coordinating their time and frequency transmission early in 1960. Coordination was begun to help provide a more uniform system of time and frequency transmissions throughout the world, needed in the solution of many scientific and technical problems in such fields as radio communications, geodesy, and the tracking of artificial satellites. The transmitting stations which are included in the coordination

plan are GBR and MSF at Rugby, England; NBA, Canal Zone; WWV, Beltsville, Maryland; and WWVH, Hawaii. In 1961 it is planned to maintain the frequency stable to 1 part in  $10^{10}$  and at the same offset value as before, i.e.,  $-150$  parts in  $10^{10}$  with reference to the U. S. Frequency Standard.

## Timing Code

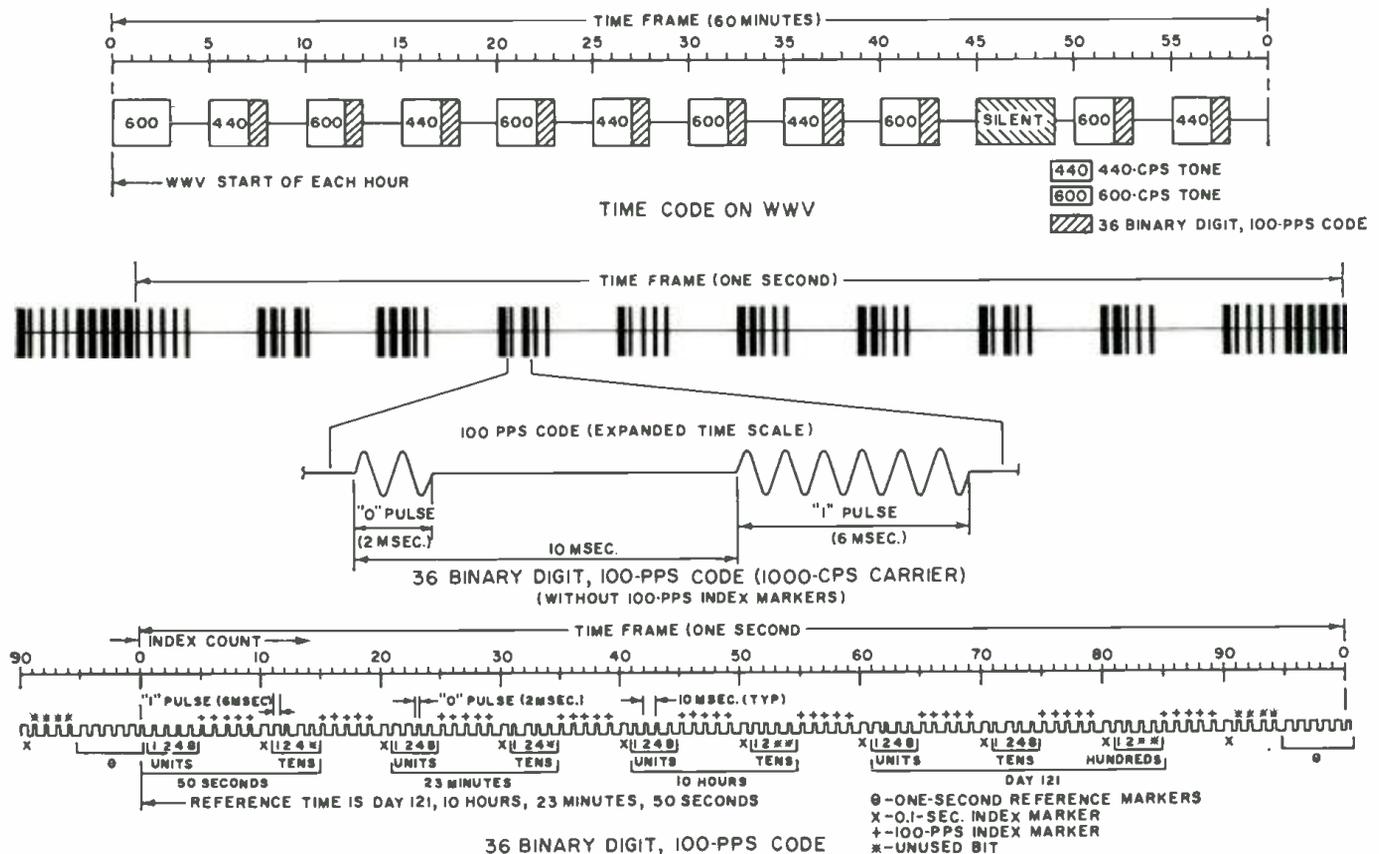
The timing code provides a standardized timing basis for use when scientific observations are made simultaneously at widely separated locations. It can be used, for example, where signals telemetered from a satellite are recorded along with these pulse-coded time signals; subsequent analysis of the data is then aided by having unambiguous time markers accurate to a thousandth of a second. Astronomical observations may also benefit by the increased timing potential provided by the pulse-coded signals.

These signals are in the form of a 36-bit, 100 pulse-per-second time code, car-

ried on 1000-cps modulation, all on WWV's carrier frequencies of 2.5, 5, 10, 15, 20, and 25 mc. The code is broadcast for 1-minute intervals, 10 times each hour as shown on the diagram below. Time-of-year information (Universal Time), given in seconds, minutes, hours, and day of year, which is locked in phase with the frequency and time signals, is given. The code is binary-coded decimal consisting of 9 binary groups each second in the following order: 2 groups for seconds, 2 groups for minutes, 2 groups for hours, and 3 groups for day of year. Code-digit weighting is 1, 2, 4, and 8 for each group, multiplied by 1, 10, or 100.

The code is a spaced code format; that is, a binary group follows each of the 10-per-second index markers. The last index marker is followed by a presently unused 4-bit group of "0" pulses just preceding the 1-second reference marker. The "0" pulses are 2 milliseconds wide (that is, 2 cycles at 1000 cps) and the "1" pulses are 6 milliseconds wide (6 cycles at 1000 cps). —30—

Details of the time-code transmissions from radio station WWV. For this particular example, the signals indicate the 50th second of the 23rd minute, of the 10th hour, of the 121st day of the current year. One second later, the first of the "units" pulses in the group designating "seconds" will change from "0" (a 2-millisecond pulse) to "1" (a 6-millisecond pulse), indicating the 51st second.



**H**A VE YOU, as a service dealer, ever asked yourself such questions as, "How much am I actually earning? How much am I really worth?" Or perhaps you have found it necessary to make such information available to someone else for business purposes and have, as a result, been surprised at your inability to come up with the facts in concrete form. In "Determine Your True Income" (December, 1960), we provide a means—the Income Statement—for answering the first question. Much of the information turned up then will be useful in answering the second question here.

The Income Statement, as was pointed out in the preceding article, is a prime accounting document. Another of equal importance is the *Balance Sheet*, which is a means for determining your net worth. If you have followed the preparation of the Income Statement, you will find that the Balance Sheet is even easier—yet, without the latter, you have little means for showing just how well your business is doing or what your ability to secure and pay back a loan is.

A finished example is shown in Table 1. We will explain the entries and their significance as we go along. The first three terms of importance are **Assets, Liabilities, and Capital.**

**Assets**, which may be considered the things used in the normal course of your business, fall into two subdivisions: **Current Assets** and **Fixed Assets**. **Current Assets** are those which are constantly being exhausted as a result of sales and service. **Fixed Assets** are those which are, more or less, a permanent part of the business.

**Liabilities:** A portion of your assets may not be wholly your own. For example, you may owe money on some of them. On the Balance Sheet, they will be regarded as Liabilities.

**Capital:** That portion of the assets that is entirely yours. (This Capital is also called *Net Worth*.) With just these three terms, the Balance Sheet can develop important information, and can express what it has to say in more than one way. The basic relationship among these three can be stated in a formula:

$$\text{Assets} = \text{Liabilities} + \text{Capital} \dots (1)$$

Now that we have an equation, we also have considerable flexibility. The formula may be manipulated, for ex-

ample, so that any one of its elements can be expressed in terms of the other two. In other words, we need know only two of them; the third can be computed.

Those who have read the preceding article will recall that we created an imaginary service dealer, Joe Smith, who went through the motions of accumulating data for his first Income Statement. It is only fitting that we allow him this privilege for the Balance Sheet as well. In fact, practically all the information he will now need has already been obtained with the earlier document.

#### Assets

Joe must first consider **Current Assets**. What is it that is constantly being exhausted as a result of his doing business? He decides there are three: money, merchandise, and shop supplies. The first is easy; he has a check-book balance of \$300 and \$100 in the cash drawer. The second is also easy, since he has drawn up an Income Statement for which he has had to take an inventory. Final inventory for June 30, 1960—the same period after which the Balance Sheet is being made up—was \$1700. The third item is not so easy. Joe Smith must evaluate all of his shop supplies (light bulbs, stationery, solder, and the like) that are now on hand. If he has drawn up his Income Statement properly, however, he has most of the needed information on hand. He finds that these supplies come to \$100 not in-

cluded as merchandise already listed in the inventory. As shown in Table 1, the sum of all these **Current Assets** comes to \$2200.

He finds there are only two groups of permanent (fixed) assets: his truck and his shop equipment. The latter includes all test equipment, tools, and accessories. As his Income Statement showed, the truck and all shop equipment each were valued at \$600 for a Total Equipment figure of \$1200, which is now entered on the Balance Sheet (Table 1). But there is a complication: What about depreciation? The Income Statement showed that both his truck and his total shop equipment depreciated \$60.00 each for a six-month period. Since he has had each of these for one year (purchased July 1, 1959), the accumulated depreciation for each is now \$120, or \$240 for both. So we have another formula:

$$\text{Total Fixed Assets} = \text{Total Equipment} - \text{Accumulated Depreciation} \dots (2)$$

Deducting the depreciation figure from the value of the equipment, we accordingly come up with Total Fixed Assets of \$960. For the final determination of Total Assets, we add the figure just obtained to that for Total Current Assets (\$2200) and come up with \$3160. This last calculation can also be put into a convenient formula:

$$\text{Total Assets} = \text{Total Current Assets} + \text{Total Fixed Assets} \dots (3)$$

#### Liabilities

In Joe's particular case, his Liabilities consist only of the money he still owes on two items, his truck and his shop equipment. Since a short-term loan is involved in each case, these are called **Current Liabilities**, and are so entered on the Balance Sheet of Table 1. If he happened to owe money on his shop supplies or merchandise, these would be additional entries under **Current Liabilities**. If he owned his own shop building and owed money (a mortgage) on that, the entry would be somewhat different. The building would be another Fixed Asset, but the money owed, which is a long-term debt, would be a **Non-Current Liability**. However, Joe is renting.

Joe's Total Liabilities then consist of nothing more than the \$100 he still owes on his truck and the \$60 he owes on equipment, or \$160 altogether. Another complication: this figure should not in-

# Understanding the Balance Sheet

By JOHN E. FLIPPIN

## Aside from the income it provides you with, do you really know how much your business is worth? Here is how you can find out.

### SMITH TELEVISION BALANCE SHEET

ASSETS		
<b>Current Assets:</b>		
Cash (In the Bank)	\$ 300.00	
Cash (On Hand)	100.00	
Inventory (June 30, 1960)	1700.00	
Shop Supplies	<u>100.00</u>	
<b>Total Current Assets</b>		<b>\$2200.00</b>
<b>Fixed Assets</b>		
Truck	\$ 600.00	
Shop Equipment	<u>600.00</u>	
<b>Total Equipment</b>	1200.00	
Less Depreciation	<u>— 240.00</u>	
<b>Total Fixed Assets</b>		<b>960.00</b>
<b>Total Assets</b>		<b><u>\$3160.00</u></b>
<b>LIABILITIES</b>		
<b>Current Liabilities</b>		
Truck	100.00	
Shop Equipment	<u>60.00</u>	
<b>Total Liabilities</b>		<b>— 160.00</b>
<b>CAPITAL</b>		
Capital		3000.00
<b>Total Liabilities Plus Capital</b>		<b><u>\$3160.00</u></b>

Table 1. A Balance Sheet, not hard to draw up, gives you a picture of Net Worth.

clude interest on the loan or loans. The Balance Sheet is only concerned with principal. Joe has accordingly made certain that this is the figure he enters here. But it would be unrealistic for him to ignore interest altogether in assessing an over-all financial picture, and he has not overlooked this expense. It belongs on the Income Statement as Interest Expense. In Joe's case, since only a small amount was involved, he was not so formal: he included it under the category of Miscellaneous Expense.

Reviewing what has been done, we see that Joe has arrived at figures for Assets and Liabilities. How can he determine his Capital? Simply by transposing formula (1) as follows: *Assets - Liabilities = Capital*. In other words, \$3160 - \$160 = \$3000. The job is done. Joe has a Balance Sheet showing his Net Worth.

#### Statement of Capital

When you make up your first Balance Sheet, a Statement of Capital will not be necessary. However, you will want to make one up for each succeeding period, to help you see how things are going. Joe Smith had made up his first Balance Sheet after the period ending January 1, 1960, at which time his Capital came out to \$2900. So he makes out a Statement of Capital for the period ending June 30, 1960 (Table 2) and the first item is the amount for Capital he determined on the earlier Balance Sheet, for the beginning of the year.

At that time, his Capital came to \$2900. He wants to find out his net Increase in Capital since then. To do this, he subtracts his Withdrawals (which will be explained later) during the intervening period from his Net Income (Income Statement, June 30, 1960). Since the former was \$1100 and the latter \$1200, his Income exceeded his

Withdrawals by \$100. This amount is the net Increase in Capital for the six-month period. Had his Withdrawals exceeded his Income, he would have had a net Decrease in Capital. However, this has not been the case, and he may add the increase to his Capital on January 1, 1960 to show that his Net Worth or Capital on June 30, 1960 is \$3000.

The only new term found here was Withdrawals. A Withdrawal is the amount of money that Joe takes out of his business for personal needs. We see, in the Statement of Capital, that Joe allowed \$100 of his income to remain in the business. Perhaps he used this to increase his supply of cash for use in the business or to pay on his truck or equipment. Whichever of these he did, he either increased Assets (the first case) or decreased Liabilities (the second).

The last paragraph should point out Joe's need for separating his personal business from that of the shop. If he allows them to mix willy-nilly, the Statement of Capital will not work out; but there is a way of keeping such matters under control—maintain two, separate checking accounts, one for his shop and one for personal use. This may sound as though it would make things more complicated rather than less so, since there will be some interaction between the two accounts, but an example shows that this is not so.

Let's start with the two accounts. The business account will be Smith Television and the personal one Joseph Smith. If Joe takes money out of the business for his own use or to pay his own salary, he draws a check on Smith Television and makes it out to Joseph Smith. For the Statement of Capital, this will be a Withdrawal. Should he decide to buy something for the business or pay on a loan from his personal account (add to Assets or subtract from

Liabilities), he makes out a check from Joseph Smith to Smith Television, then uses the money as intended. Since this amount will show up on the next Balance Sheet as either an increase in Assets or decrease in Liabilities, it must also be reflected as an Increase in Capital. Won't this maneuver, then, throw his records out of kilter? Not if he *subtracts* this amount he has put back into the business from Withdrawals on the Statement of Capital. This too will be an increase in Capital, and his record will balance out.

Thus we can see two important functions of the Statement of Capital: It shows Joe the amount he puts back into his business and it acts as proof to show that the Income Statement is in agreement with the Balance Sheet. Obviously if Joe had done a careless job of computing his Income Statement, to begin with, the amount for Capital shown

#### Statement of Capital For Period Ending June 30, 1960

Capital (Jan. 1, 1960)	\$2900.00
Net Income for the Period	\$1200.00
Less Withdrawals	<u>—1100.00</u>
<b>Increase in Capital</b>	<b>100.00</b>
<b>Capital (June 30, 1960)</b>	<b><u>\$3000.00</u></b>

Table 2. A Statement of Capital will check accuracy of your Balance Sheet.

on the Statement of Capital on June 30, 1960 would not agree with the separately computed entry under Capital on the Balance Sheet of the same date. If this were to happen, he would immediately be aware that something had gone wrong. He would have to go back and compare his check stubs to his invoices and other records to find errors.

For every dollar spent or received, there must be a corresponding change in Income, Expenses, Assets, or Liabilities. If these records have been kept properly they will coincide, and the Statement of Capital will have to agree with the Balance Sheet.

If you have never drawn up business records of the kind described here, you are now ready for your first Income Statement and Balance Sheet. You have surely concluded by this time that keeping track of inventories and accumulating data can be a tough job. This can be made a great deal easier using the classic "journal" and "ledger" of the double-entry bookkeeping system. But what you have learned from trying to make your first statements will help you absorb this with little effort.

What we have done is to start at the end of the accounting procedure, with the Income Statement and Balance Sheet, and suggest working back to the beginning. Why? Because, as you work back, you have the opportunity to see how each business transaction will affect the two important statements that are the end products of all accounting procedures.

# New Products for the Radio and TV Service Technician

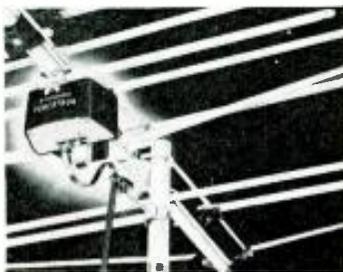
- 1 Test Equipment
- 2 Tools
- 3 Components



**1** Chicago Standard Transformer has announced three new exact-replacement transformers for Admiral TV sets. A total of 108 models and chassis is covered by these newly released flyback transformers.

**2** Heath Co. has available a new isolation transformer, Model IP-10, which features several improvements, including higher power rating, improved meter accuracy, and new styling.

Designed for the service technician, the new unit provides complete isolation from the a.c. power line and allows exact control of line voltage to the equipment under test. Output voltage is variable from 90 to 130 volts in .75-volt steps by means of two 8-position switches. Power rating is 300 watts continuous.

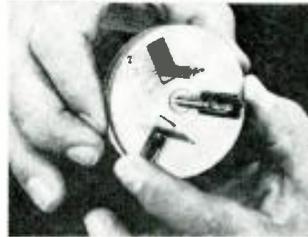


**3** Winegard Co. has just introduced what it claims is the world's first electronic TV receiving antenna, the "Powertron." The new unit, an all-channel yagi design, incorporates a built-in electronic r.f. amplifier.

The antenna is being offered in three models: a 14-element unit; a 21-element version; and a 30-element design. A compact isolation transformer unit plugs into the 117-volt power line, lowers the voltage to 24 volts for safe operation.

**4** Radio Shack Corp. has introduced a dual-trace scope in kit form for the service fraternity. Response is flat from 10 cps to 5 mc., useful to 9 mc. The circuit features push-pull vertical and horizontal amplifiers, cathode-follower inputs, and 5" screen.

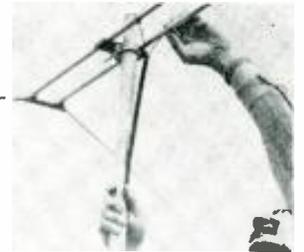
Over-all size of the scope is 13 1/4" x 8 3/4" x 18 1/2". The kit comes complete with detailed assembly and operating instructions.



**5** Zoron, Inc. is marketing a new "Z-Saw" hole cutter which is adjustable for cutting holes of any diameter from 1 1/8" to 2 1/4" in wood, plastic, or aluminum. An extra set of blades for cutting metal is supplied. It is designed for use with power hand drills.

**6** CBS Electronics has added a new tool to its service tool line, the "Kwik-Klip" for quick and easy TV antenna lead replacement.

The tool eliminates unnecessary danger for technicians when working on roof tops. Simple, one-hand, clip-on operation eliminates the bother of removing rusted or corroded nuts and bolts to replace the antenna lead-in. According to the company, the "Kwik-Klip" can improve reception and restore original strength in many older antenna installations. These new tools are being offered through CBS tube distributors.



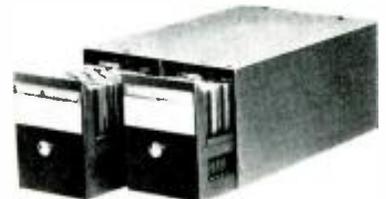
**7** RCA's Electron Tube Division has introduced a new "do-it-yourself" kit for its "Senior VoltOhmyst," featuring a pre-assembled and pre-soldered etched-circuit board. Designated WV-98B (K), the major sections of the kit are factory assembled, cutting construction time in half.

All of the components that go on the extra-thick, etched-circuit board are factory mounted and soldered to the board. In addition, a completely assembled input cable and probe, with built-in a.c./d.c.-ohms switch, is provided with each kit.

The unit features a 6 1/2" wide, easy-to-read meter; separate color-coded scales; 200- $\mu$ a. meter movement; precision  $\pm 1\%$  multiplier resistors; and rugged die-cast aluminum case with leather carrying handle.



**8** Sprague Products Co. has assembled a specially selected assortment of its "Difilm Orange Drop" radial-lead dipped tubular capacitors for the service technician. Two "file-drawer" groups are available.





9 *Aerovor Corp.* has announced a new electrolytic capacitor kit, AK-510, for transistor radio servicing applications.

Packaged in a handy, reusable plastic box, the kit contains 18 miniature Type PTT-PWE electrolytics covering over 90% of the replacement requirements for personal transistor radios and personal portable TV sets.

10 *Sencore-Service Instruments Co.*, Addison, Ill. is now offering a new substitution unit, the "Big 20". The unit has 20 power resistors for fast substitution of all power resistors; for service work or experimenting.

Each power resistor can be substituted in circuits that dissipate up to 20 watts and for all values between 2.5 and 15,000 ohms. It can also be used as a substitute for fuse resistors in TV repairs.



11 *National Radio Institute* is now marketing its "Professional Model 2 Battery Eliminator" designed for transistorized equipment.

The unit supplies clean, filtered d.c. fully variable from 0-15 volts. Output is sufficient for receivers up to 22½ volts. The unit cannot be damaged by short-circuits.

The instrument is shipped complete with plug-in jacks for external voltmeter, and 40" leads.



12 *The Beryllium Corp.* has added a group of miniature safety pliers to its line of non-sparking safety tools.

The line includes curved needle-nose, duck-bill, long-nose, and diagonal cutting types.

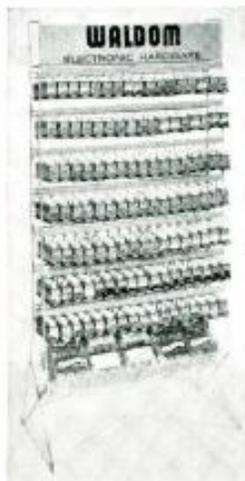


13 *Waldom Electronics, Inc.* has released a "point-of-purchase" display rack featuring a wide assortment of small electronic hardware items.

In order to attract buyers, the company has packaged its hardware in a new series of boxes, all of similar front dimensions and design. All boxes come with a window for product visibility.

The boxes are light blue and maroon for the "Blue-Line" (100 pack) Series and light green and maroon in the "Green-Line (small-pack) Series.

The packages are provided with a sturdy tab for hanging on the 118 hooks in the 30" x 65" x 18" wire hardware rack.



14 *Mercury Electronics'* new Model 700 transistor tester is "obsolete-proof," according to the manufacturer of this unit.

Designed for the service industry, the new instrument will check all r.f., i.f., audio, power output, and industrial transistors as well as diodes for forward-reverse ratio.

The unit is battery powered and has a special protective circuit arrangement to prevent transistor damage and excessive battery drain.

15 *Union Carbide* has come out with a new "Battery Displayer" to handle its line of "Eveready" hobby batteries in compact form.

The blonde wood and metal counter fixture displays a pre-tested assortment of 52 batteries in a little more than a square foot of counter space. It is free with a suggested order of the firm's hobby batteries.



16 *Electric Storage Battery Co.* is offering the "Aetivertter" which provides 110-volt a.e. power any place where a 12-volt battery is available or can be taken.

The unit can be used to operate a variety of electric equipment and is offered in four models with from 150 to 500 watts output.

The unit can also be used as a fast or slow charger for 6- or 12-volt batteries.



17 *Cornell-Dubilier* is offering a free "Pik-A-Pak" display rack, which holds 5000 capacitors, to distributors and jobbers who purchase a selection of C-D's most popular capacitors.

Occupying less than 3 sq. feet of floor space, the decorative and colorful display is designed to stimulate the sale of capacitors in quantity to service technicians.



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# A DIMENSION CONTROL

## FOR STEREO

By **RALPH GLASGAL**  
Consulting Audio Engineer

A new circuit and control that adjusts stereo separation ratio.

This technique enhances the stereo effect, cancels crosstalk, and compensates for poor loudspeaker placement.

**W**HY ANOTHER CONTROL? Isn't stereo complicated enough as it is?

For the more casual music listener, perhaps it is, but for the perfectionist and the experimentally minded much can be accomplished through the use of this special control circuit to enhance the stereophonic effect, to increase separation, to cancel crosstalk in cartridge or amplifiers, and to compensate for disadvantageous speaker placement. With this control, an audiophile can be his own recording engineer without being present at a recording session.

Ever since the inception of mass-produced stereo home sound systems, a flood of books, technical essays, magazine articles, and even cartoons have stressed the importance of placement of reproducers and listeners to achieve any semblance of stereophonic effect. The resultant well-publicized need for logistics in the living room has made weightlifters out of countless devoted audiophiles.

Stereo is the creation of the electronics engineer, and its problems should be solved by electronics, and not by the heavy moving industry. It is pleasant to report that some audio engineers have met this challenge and that the critical listener can now permit his wife to arrange the furniture to suit her aesthetic taste and still not interfere with his ability to obtain as much, or as little, stereo separation as he desires, with

only the effort involved in turning a knob.

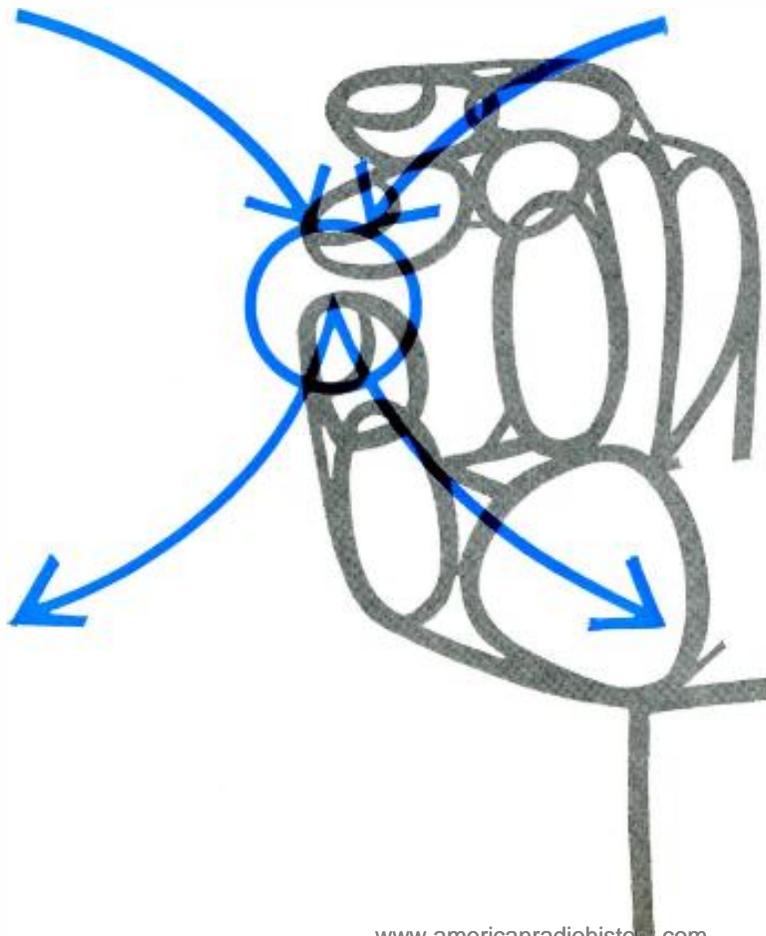
The stereo separation ratio control, sometimes called a "dimension control," is not a gadget or a toy for special effects or stunts. It is a logical and much needed extension of the recording studio equipment into the home, enabling the listener to add his own taste and experience to the judgment of the recording engineer. How this is accomplished will be made apparent as we examine the applicable electronic and acoustic principles.

### Recording in Stereo

To properly understand the purpose and function of the circuits described in this article, the layman must first rid himself of a widespread misconception. A stereo record is *not* an arbitrary division into right and left channels corresponding to the right and left sides of a stage or platform. It is, rather, a complex combination and division of sound compounded electronically at a console by a human musician-engineer and is offered as his best artistic expression of stereo music as he hears it, subject to the acoustic conditions peculiar to his own monitoring systems. To alter his interpretation during playback in the home is not sacrilege, nor does it constitute tampering with a fixed mathematical ratio. It is merely the addition of one more artistic judgment to a whole series of such judgments.

That it is quite possible to season the stereophonic effect to taste can be seen if we examine a typical stereo recording setup. Consider the MS (middle-side) recording method widely used in Europe (see Fig. 1). Two microphones are mounted coaxially at a center location in front of the orchestra. One microphone is capable of picking up sound equally from all parts of the orchestra. Let us represent its signal output as left+right+center or  $(L+R+C)$ . The other microphone, usually a ribbon type, has some rather unusual directional properties. A signal reaching the microphone from the extreme right produces a signal of opposite polarity from that of a sound source at the extreme left. Sounds which come from neither the right nor left produce no output at all. Therefore, we may represent the output from this microphone as left-right or  $(L-R)$ .

It is now the recording engineer's job to reduce these two microphone outputs to simple left- and right-channel outputs, which can then be recorded onto the master tape and used to cut two-channel stereophonic discs. This is accomplished by a process known as matrixing. The two outputs are added,  $(L+R+C) + (L-R) = 2L+C$ , to produce a signal containing left information with a reduced center signal com-



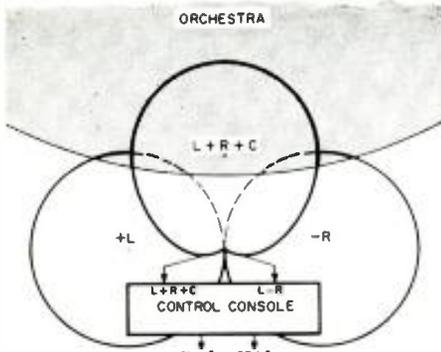


Fig. 1. The MS method of stereo recording.

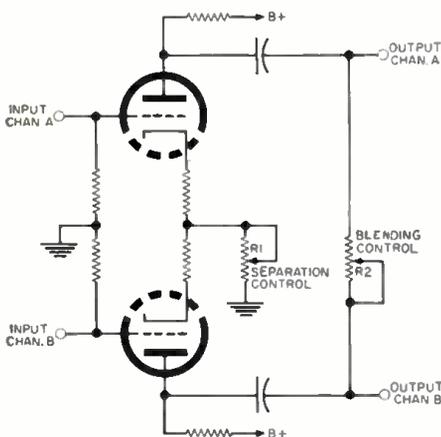


Fig. 2. Dimension control circuit that has been employed by Nippon Columbia Co.

ponent. The right-channel signal is obtained by subtracting the two microphone outputs to produce  $(L+R+C) - (L-R) = 2R+C$ . Hence, the required left and right signals have been separated out and there is some center information in both outputs. In actual practice, the addition and subtraction is accomplished by the recording engineer at the recording console on the basis of his experience and what he hears over a monitoring system.

The difference signal,  $(L-R)$ , represents the separation or stereo portion of the signal. By boosting this signal at the expense of the sum signal, increased separation is obtained. If the difference signal is attenuated by the recording engineer, soloists or center instruments become emphasized and the stereo dimension is reduced.

The engineer carefully adjusts the mixing and matrixing levels, blends in other solo or reverberation microphones until he obtains what he and a committee of professional musicians and recording executives consider to be optimum. Generally speaking, the combined judgment of these gentlemen can be relied upon, but they are only human and cannot be expected to compensate the recordings in advance so that they will sound realistic over all the myriad speaker systems and placements found in homes. Their judgment is of necessity based on what they hear through a limited number of monitoring systems, and represents a compromise to achieve results that will sound best over the greatest number of home systems, to

the greatest number of listening ears.

The apparent amounts of sum and difference signals are also affected by speaker placement, room acoustics, and listening position. Thus, if loudspeakers are placed very close together, the ear will hear mainly a sum signal and the stereo effect will be minimized. Also, a listener a great distance from the loudspeakers will hear only a monophonic signal. At the other extreme, the listener with stereophonic earphones or excessive speaker separation will hear more difference signal than the committee of experts intended him to. The effect will be pronounced separation.

### Purpose of the Control

What is needed then is a control which the listener can adjust in his own home to achieve exactly the ratio of sum to difference signal required to match his particular listening environment or artistic predilections.

In the MS system of recording, we have seen how the sum and difference signals are produced directly by the recording microphones. In other stereo recording systems, the sum and difference signals never actually exist as such, though their ratio is carefully controlled by a proper multiple microphone placement and judicious choice of mixing

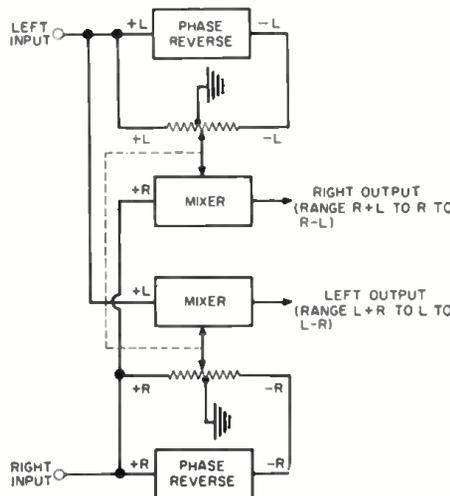


Fig. 3. Block diagram of the new stereo separation ratio control circuit described.

levels. Most of the better stereo recordings show a separation ratio of difference to sum signal of about 9 to 10; thus a good stereo recording is just slightly more monophonic than binaural.

A stereo dimension control is not a new idea. Such a control is included in most of the new multiplex adapters for use in the Crosby system of FM stereo broadcasting. Here, the sum and difference signals are actually being broadcast and it is therefore necessary to dematrix the signal to get a left and right signal. If one starts with a left and right signal as from tape or disc, and then desires to alter the separation ratio, it is possible to make sum and difference signals electronically, alter their ratio by means of controls, and then subtract and add them again to recover the new left and right signals. This is however a

cumbersome and rather parts-consuming method of altering the separation ratio.

A little simple arithmetic will show that it is not necessary to actually make sum and difference signals to alter the separation ratio. Suppose we desire to double the separation ratio of difference to sum signals in order to compensate for close-together speakers. We start with

$$\frac{\text{Diff.}}{\text{Sum}} = \frac{L-R}{L+R} = 1, \text{ and we then in-}$$

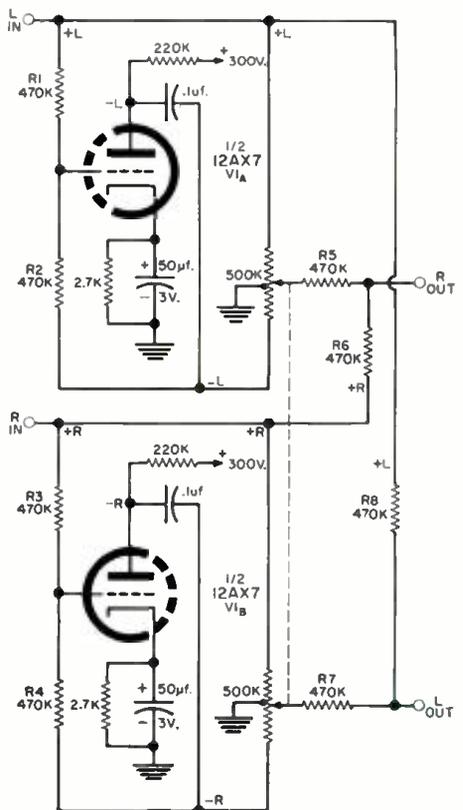
crease the ratio,  $\frac{2(L-R)}{L+R} = 2$ . By in-

creasing the difference signal to two times its former value, we achieve the desired ratio. Now let us reclaim the left and right signals and see how they have been altered. The right signal is the  $\text{Sum} - \text{Diff.} = L+R - 2(L-R) = 3R - L$ . The left signal is the  $\text{Sum} + \text{Diff.} = L+R + 2(L-R) = 3L - R$ .

This result shows that to alter the separation ratio it is only necessary to add to each channel an out-of-phase signal from the other. In this case, to double the separation ratio, an out-of-phase signal of  $\frac{1}{2}$  the amplitude must be combined with the signal of the opposite channel.

Figure 2 shows a portion of a circuit first proposed in print by Toshio Hirota of Nippon Columbia Co., Ltd. By increasing the value of the common cathode resistor  $R_1$ , the difference signal is amplified, and by decreasing the value of  $R_2$ , blending is achieved. This circuit is extremely simple and easy to install  
(Continued on page 116)

Fig. 4. Complete schematic of the control circuit that can be inserted into the pre-amp or just ahead of the power amplifier.



# PLAYBACK Four-Track Tape System PREAMPS

## PART 2-

By **KENNETH F. BUEGEL**

*Complete construction info on the electronics portion of stereo record playback system. Final adjustments as well as complete operation of the home-built system are covered in this final part.*

IN PART 1, we covered the construction of the recording preamplifiers and the power supply for the four-track tape system. Now we will take up the matter of the playback preamp and adjustment of the system.

### Playback Preamps

If the playback preamps are built on a separate chassis from that of the recording amplifiers another  $\frac{1}{4}$ " bonding strap must be added from the jack panel ground to the chassis. The playback-head signal grounds are carried through an insulated jack and connected to the chassis only at the ground point for  $R_{20}$  and  $R_{21}$ .

Proper ground techniques are an *absolute must*. The output signal from the playback head is only 2 millivolts and

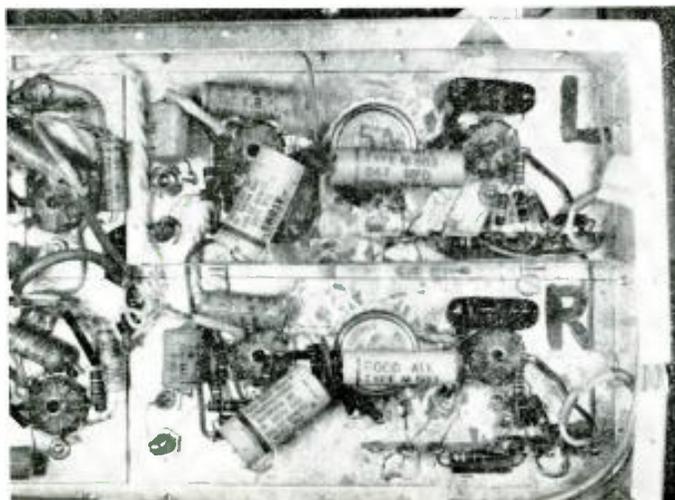
common grounds will certainly create a hum problem. For this same reason, a premium-type 7025 tube is used in the first two stages although if a number of 12AX7 tubes are available, it would be possible to hand pick one for minimum hum. See Fig. 4.

The signal appearing at  $J_1$  is amplified twice in  $V_{11}$  and  $V_{12}$  before it is applied to the "Playback Gain" control,  $R_{23}$ .  $V_{11}$  again amplifies the signal which is applied to  $V_{12}$ , a low-impedance cathode-follower. The output signal at  $J_1$  may be adjusted over a range of 0-3 volts. Most stereo control centers work well with about .5 to 1 volt signals into the "auxiliary" inputs.

The combination of  $R_{23}$  and  $C_{20}$  feeds back more of the high frequencies from the plate of  $V_{12}$  to the cathode of  $V_{11}$  to equalize the playback response. This preamplifier was originally used with two-track heads but the increased high-frequency response of the laminated four-track heads necessitated the addition of  $C_{20}$  between the plates of  $V_{11}$  and  $V_{12}$  to maintain flat response over the 50 to 10,000-cycle range. This capacitor may be omitted if the older two-track heads are used.

Most stereo control centers follow the general outline shown in Fig. 5A. The addition of a d.p.d.t. switch, as shown in Fig. 5B, will allow listening to the signal being recorded on the tape. When recording from a disc, a piece of lint caught under the stylus and producing distortion is immediately apparent. There is no need to rewind and playback the tape to determine the quality of the recording.

The input impedance of the recording



Under-chassis view of the playback preamp portion of the tape system. Two identical circuits are employed, one for the left channel and the other for the right channel. Shielding is used between the two sections in order to minimize the possibility of some crosstalk.

preamps is high and should not affect the cartridge preamp output. The playback preamp output impedance is low and may be applied directly to a level control, if one is ahead of the first amplifier following the selector switch. Almost all stereo control centers have the recorder output jacks connected prior to any tone-control circuitry. Connection of the output of the playback preamps to jacks designed to accommodate a tape-head input is not recommended since these inputs are usually equalized and will operate only on very low signals.

### Adjustments

Alignment of the completed system is easily accomplished with a standard alignment tape, a v.t.v.m., and a signal source—preferably an audio oscillator. Physical alignment of the heads is mandatory before any other adjustments are attempted. First, remove the oxide coating from a section of Mylar tape for about six inches. Then thread this tape from one reel to the other with the clear section over the heads. For better visibility, the pressure pad may be removed. Mylar tape will have less "curl" after removal of the oxide with lacquer thinner or nail polish remover than will acetate tape. In tape decks with the reels beneath the heads, such as the *Viking*, the left track is closest to the front panel.

Demagnetize all tools used in adjusting the head positions. As shown in Fig. 6, the tape heads should meet the tape squarely and the lower edge of the tape should just be even with the outside edges of the pole pieces nearest the tape-deck panel. Thoroughly demagnetize the heads before proceeding! Place the alignment tape on the deck and advance  $R_{25}$  on both channels to about mid-position. Set the v.t.v.m. to a low a.c. range and connect it between  $J_2$  and ground of either channel. While playing the section of tape with the high-frequency head alignment tone, set the azimuth adjusting screw on the playback head for maximum output, as indicated by the v.t.v.m. Now, connect the recording head windings to the playback inputs and set its azimuth adjustment in the same manner.

Return the head connections to normal and play the 1000-cycle level-set tone while adjusting  $R_{25}$  in each playback channel for the desired output level. Remember that this tone, as recorded on the test tape, will probably be about 15 db below saturation. In any event, the setting of  $R_{25}$  should be such that when the stereo selector switch is in the tape position, the level is about the same as that of the other inputs.

To set up the recording amplifiers, first measure the average output appearing at the recorder output jacks on the stereo control center. Then connect  $J_1$  on both channels to an audio oscillator, set for this output, at a frequency of 1000 cycles. Set  $R_{15}$ , the "Record Level" control, to mid position and adjust  $R_{16}$  on each channel until the a.c. voltage read by the v.t.v.m. at  $J_2$  is 1.8 volts. For this adjustment  $S_1$  must be in

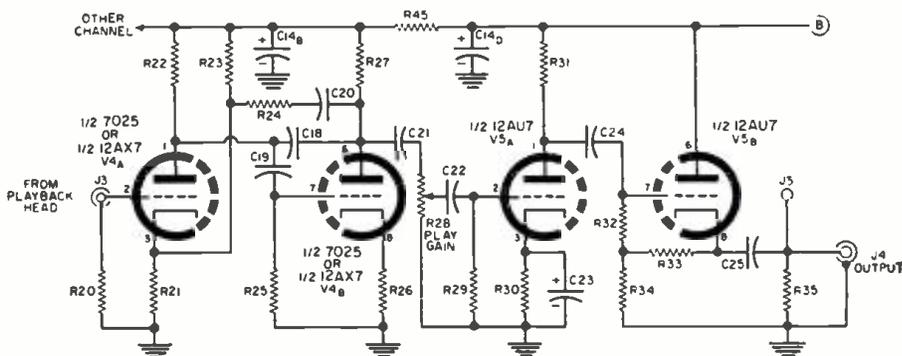
the "Record" position but do not depress the "Push-to-Record" button or the bias voltage on  $J_2$  will cover the audio voltage-age reading.

After setting  $R_{16}$  adjust  $R_{14}$  on each channel until each meter reads 70% of full scale. With the levels set to these values, your recordings will be about 3 db under tape saturation when the meter reading is at full scale. Recording at levels this close to saturation will not adversely affect performance. One definition of tape saturation is "that level at which a pure 400-cycle tone applied to the tape is reproduced with 1% distortion." While it is not the author's desire to enter into any of the arguments about the theory of tape recording and reproduction, just one comparison between a tape made with this system and any pre-recorded four-track tape will serve as testimony to the effectiveness of recording at this level. A word of caution, however. In use, set the

"Record Level" until most peaks just hit the 70% point, with an occasional peak of 100%.

To correctly set the "Noise Balance" control,  $R_{19}$ , thread a new tape on the deck and connect the v.t.v.m. to  $J_2$  of either channel. Set the "Record Level" to minimum and adjust  $R_{19}$  for a minimum reading with the system recording. This bias oscillator will completely erase a saturated tape in one pass when used with the recommended double-gap erase head.

When using the system for recording from a stereo broadcast source, output levels of the tuners may be conveniently balanced by reference to the meters. The meters are operating any time the "Record Level" control is advanced. If used to determine the relative signal per channel on playback only, be sure  $S_1$  is not in the "Record" position or an unpleasant reverberation will be added to the tape.



$R_{20}, R_{23}, R_{24}, R_{25}, R_{26}, R_{27}, R_{28}, R_{29}, R_{30}, R_{31}, R_{32}, R_{33}, R_{34}, R_{35}$ — $1\text{ megohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{21}$ — $1000\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{22}$ — $330,000\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{23}, R_{24}$ — $220,000\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{25}$ — $100,000\text{ ohm}, \frac{1}{2}\text{ w. res.} \pm 5\%$   
 $R_{26}$ — $3.3\text{ megohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{27}$ — $1200\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{28}$ — $500,000\text{ ohm audio taper pot}$   
 $R_{29}, R_{30}$ — $10,000\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{31}$ — $68,000\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{32}$ — $5600\text{ ohm}, \frac{1}{2}\text{ w. res.}$   
 $R_{33}^*$ — $5200\text{ ohm}, 1\text{ w. res.}$   
 $C_{19}^*$ —See record preamp parts list, Fig. 1, Part I  
 $C_{21}^*$ — $220\text{ }\mu\text{f. disc ceramic capacitor} \pm 10\%$

$C_{19}$ — $.03\text{ }\mu\text{f. } 400\text{ v. paper capacitor}$   
 $C_{20}$ — $820\text{ }\mu\text{f. } 600\text{ v. mica capacitor} \pm 5\%$   
 $C_{21}$ — $.047\text{ }\mu\text{f. } 400\text{ v. paper capacitor}$   
 $C_{22}$ — $.01\text{ }\mu\text{f. } 200\text{ v. paper capacitor}$   
 $C_{23}$ — $50\text{ }\mu\text{f. } 10\text{ v. elec. capacitor}$   
 $C_{24}$ — $.02\text{ }\mu\text{f. } 400\text{ v. paper capacitor}$   
 $C_{25}$ — $.1\text{ }\mu\text{f. } 200\text{ v. paper capacitor}$   
 $J_1, J_2$ —Phono jack  
 $J_3$ —Pin jack  
 $V_4$ —7025 or 12AX7 tube (see text)  
 $V_5$ —12AU7 tube  
 \*Parts so marked are used once in the circuit. All other parts must be duplicated for the second channel of the stereo setup.

Fig. 4. Two identical playback preamps like this one must be constructed.

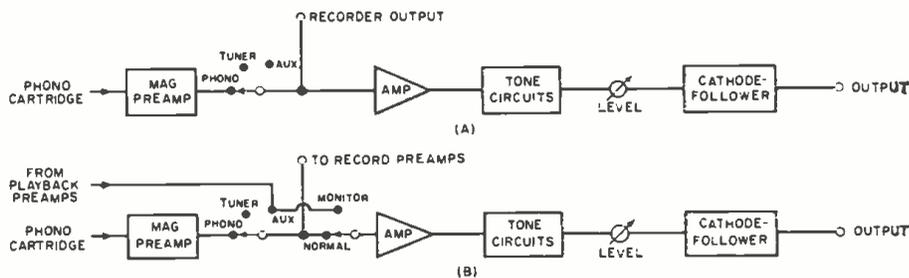
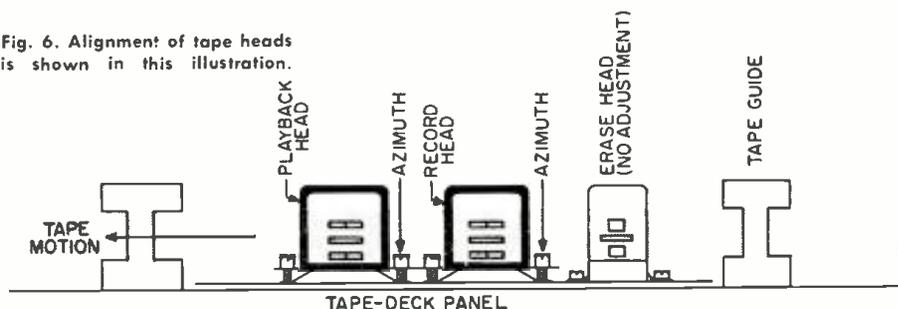


Fig. 5. Block diagram illustrating the modification of the stereo control center.

Fig. 6. Alignment of tape heads is shown in this illustration.





## Problems!

It was a perfect spring day. A warm breeze from the south gently nudged fleecy white clouds across an azure sky. Robins braced themselves on the green sod polka-dotted with yellow dandelions and yanked inch after reluctant inch of elastic worms from the warm earth. Tulips, jonquils, and redbud delighted the eye; the ears rang with the exciting lifting chorus of the birds; and the sweet fragrance of hyacinths made simply breathing a heady pleasure.

Inside Mac's Service Shop, Barney hummed happily to himself as he worked at the bench beside his employer.

"I don't need to stick my head outside to tell it's spring," the older man said with a grin. "You're certainly in tune with the season. I can almost see your fancy lightly turning to thoughts of you-know-what."

"Huh?" Barney said as he looked up with a puzzled frown. "Oh! I dig you, but you're out of phase. I'm just happy because I finally have all my transmitting beam antenna problems licked."

"Didn't know you had any problems."

"That's because I'm the strong silent type and seldom complain," Barney said with an impish look. "It all started when the ten-meter band began to fold up early this year. As you know, the sunspot cycle is rapidly going down hill. That means conditions on the higher frequencies will get progressively worse for the next few years; and good old ten meters, my favorite band, will be just about *Kaput* as far as consistent DX is concerned. For long distance work, a fellow is going to have to retreat first to fifteen meters and then, when that goes out, to twenty. The wise boys say even twenty will likely be pretty poor during the worst part of the eleven-year cycle.

"I decided the smart thing would be to take down my faithful old ten-meter beam and put up a tri-bander that would still let me work ten when it was open but would also let me operate fifteen and twenty when ten was blacked out. So I got myself a good four-element tri-

bander and made my first mistake: I put it up on the same heavy-duty TV rotator that had carried the old antenna. After all, that rotator had never failed to hold or turn the ten-meter job, even with a half-inch of ice frozen on the elements; so maybe it would handle the much-larger tri-bander.

"I should have known better. Instructions accompanying the beam said a heavy-duty TV rotator would hold the antenna only in winds up to twenty-five miles per hour. The jokers who wrote that must have actually checked it out, for the very first time we had gusts up to 25 mph, the wind turned the beam up against the stop and kept banging it there. Considering it has a sixteen-foot boom and a longest element of thirty-one feet and weighs nearly forty pounds without a mast, I had no reason to be disappointed.

"Anyway, the motor couldn't take much of that, and neither could I. I found myself cringing every time a breeze sprang up. Finally I did what I should have done in the first place: I replaced the TV rotator with a heavy-duty rotator especially designed for turning and holding heavy beams and arrays. This one has an arrangement that locks the two major parts of the rotator solidly together when the beam is at rest. When power is applied to the rotating motor, this brake is disengaged by a solenoid. That took care of my turning and holding problems."

"You had others?"

"Yep! But let me tell you how my 'antenna farm' is laid out. The rotator is mounted on the end of a six-foot length of 1½" galvanized pipe bolted to the top of a forty-foot telephone pole. The motor sits two or three feet above the top of the pole, and a five-foot 1¼" pipe mast holds the beam. One end of my all-band trap antenna is fastened to the 1½" pipe right at the top of the pole. The end insulator of this wire antenna is only about four feet from the pole and six or seven feet below the beam elements. I know this isn't the best arrangement in the world; but

Mom says flatly one mast is all we're going to have on the front of our lot, and that's that.

"The length of the control cable is very close to sixty feet—which is about a quarter-wavelength long on 75 meters. My old rotator control used lamps arranged around a compass pattern to indicate the beam direction, and when I first put up the ten-meter beam I discovered that when I was on 75 meters all the indicating lamps lighted up simultaneously. Parallel wires in the control cable were acting as resonant quarter-wave lines, and the r.f. across the bottom ends was sufficient to light the bulbs. I could have cured this by bypassing each bulb with a small ceramic capacitor, but I accidentally found that if I pulled the control unit a.c. plug from the socket when I was on 75 meters, the situation was no longer present. Doing this shifted the standing waves on the control wires enough so that the current loop moved away from the bulbs.

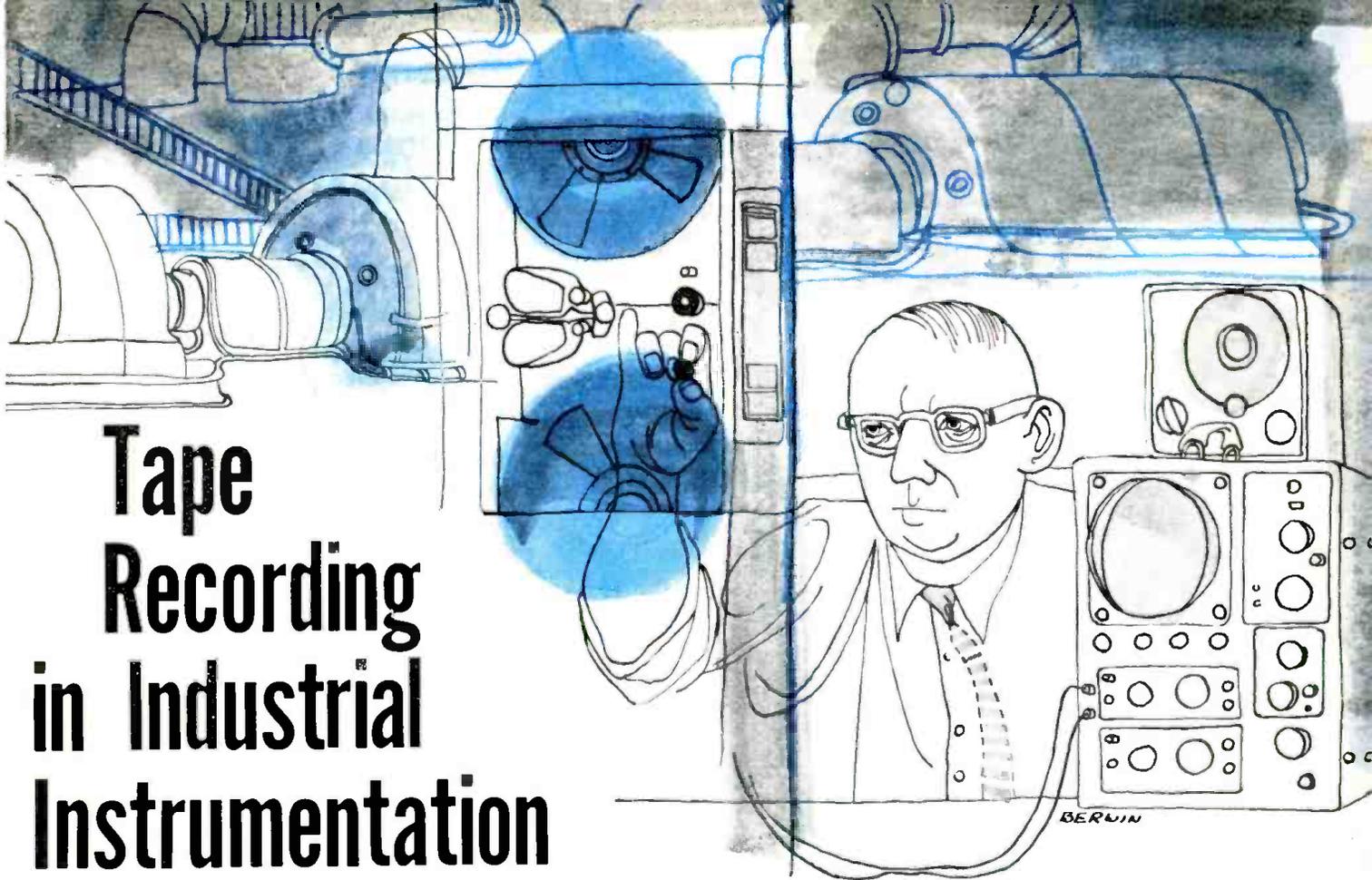
"The heavy-duty rotator uses a current meter in the control unit that works in conjunction with a potentiometer in the motor section to indicate direction. Two wires carry direct current up to the potentiometer, and one of these wires is fused with a 1/16-amp fuse in the control unit so that if a short-circuit accidentally occurs in the cable the precision potentiometer will not be damaged. Well, after I had the beam up and had checked everything out on the higher frequencies, I decided to tune up on 75 and report into our state traffic net. After I had tuned up, I reached over to rotate my pride and joy one more time and got a nasty shock. The beam turned all right, but the direction-indicating pointer never moved off the left-hand 'South.'

"I suspected the little fuse had blown, and it had. I also suspected, thanks to my experience with the other rotator, that r.f. had blown the fuse; so I put a pilot lamp in place of it and quickly found that when my transmitter was putting out 100 watts on 75 meters better than 125 ma. of current was going through the fuse rated to blow at around 85 ma. A .05- $\mu$ f. ceramic capacitor connected across the two wires carrying the d.c. voltage up to the potentiometer cured the difficulty completely by bypassing the r.f. right at the terminals before it ever got inside the control box.

"While a certain set of circumstances had to exist in my antenna system for this to happen, my set-up really is not too unusual. Lots of fellows use the same mast to support a beam and carry one end of a low-frequency antenna, and lots of them use a length of control cable that can become a resonant line at a low operating frequency. Under such circumstances, the mysterious blowing of that fuse could present a puzzling problem, especially if the r.f. current was marginal so that the fuse only blew now and then."

"Yeah, I can see the puzzled ham running up and down his tower like a

(Continued on page 112)



# Tape Recording in Industrial Instrumentation

By **RAY A. SHIVER**  
 & **WILLIAM STILLWELL**  
 Instrumentation Laboratory  
 AiResearch Mfg. Co. of Arizona

**A large variety of useful information can be gathered, recorded, stored, and then reproduced by this method.**

**W**HILE magnetic tape recording is well known in computer technology, automatic programming, and missile telemetry systems, its application to industrial instrumentation is a comparatively new field. With the introduction of high-speed turbo machinery and supersonic flight, design engineers became necessarily interested in frequencies above the audio range. To meet this need, instrumentation magnetic tape recorders were developed with a direct record frequency response to 100 kc. This has proved to be a valuable tool to the development engineer in the design of high-speed turbine wheels, bearings, and related components in the industrial field.

## Recorders for Instrumentation

Fig. 1 shows one of the first types of recorders used in instrumentation. This proved valuable but was limited by its narrow (for instrumentation applications) frequency response and the availability of only two channels. Fig. 2 illustrates one of the types of recorders in general use today. Note that both types are designed to be "mobile" since the job seldom is able to come to the recorder. The recorder shown is an *Ampex FR-*

100-A, providing facilities for recording and reproducing seven channels of data. Six tape speeds are available from 60 ips to 1 7/8 ips. The frequency response is a direct ratio of tape speed from 100 kc. direct-record and 10 kc. FM at 60 ips to 6250 cps direct-record and 312 cps FM at 1 7/8 ips. The top half of the console shown in the photograph of Fig. 2 contains meters, preamplifiers, and input-output attenuators for maximum flexibility. Included in the lower section of the control panel is a v.t.v.m., a pulse generator for supplying timing markers, two bridge-balance circuits for strain gage calibration, and a variable d.c. supply and meter for calibrating d.c. channels. Outboard equipment includes a dual-beam oscilloscope, a high-frequency oscillator, and a frequency counter. An indispensable item is a microphone for recording a running commentary during a test and for providing reference points to be used in data reduction.

## Recording Systems and Their Uses

The *Ampex FR-100-A* is equipped to record by any combination of four different methods: Direct-record, FM, PWM, and NRZ digital recording. Since our application concerns the recording of high-frequency and d.c. data, we shall concern ourselves with the direct-record and FM systems only. The direct-record method is similar to that used in home tape recorders in that the signal to be recorded is amplified, mixed with a bias oscillator signal, and applied directly to the record head. Of course, the instrumentation recorder has a much greater frequency response; more rigid tolerances for skew, wow, and flutter; and a

more elaborate system for playback equalization. Since this type of recording is most useful in recording high-frequency amplitude information, the problem becomes one of obtaining as flat a curve as possible from the reproduce amplifiers. The I.R.I.G. standard is  $\pm 3$  db, but with careful attention to equalization, much greater accuracy can be obtained. The section on a typical recording problem also indicates how this can be compensated for in the calibration process. If greater accuracies are required, a standard tape is reproduced for each direct-record channel and a frequency response curve drawn by an X-Y plotter. This allows any point on the curve, once the frequency has been established, to be corrected. Frequency reproduction accuracy on this particular recorder is better than 1%, being limited only by the stability of the tape transport system.

Fig. 3 shows some of the types of transducers that are applicable to direct recording. At left center is a speed pickup which is used in conjunction with a multi-tooth gear to provide an indication of unit rpm. As the gear revolves, each tooth in passing the pole piece of the pickup generates a pulse which is recorded on the tape as a function of rpm. At lower left is an accelerometer which, when properly attached to a member under test, will produce an a.c. output voltage proportional to vibration amplitude. Also pictured in Fig. 3, at the extreme right, is a strain gage shown bonded to a metal member. A strain gage consists of a special high-resistance wire or foil which when stretched or compressed produces a proportionate change in resistance and therefore out-

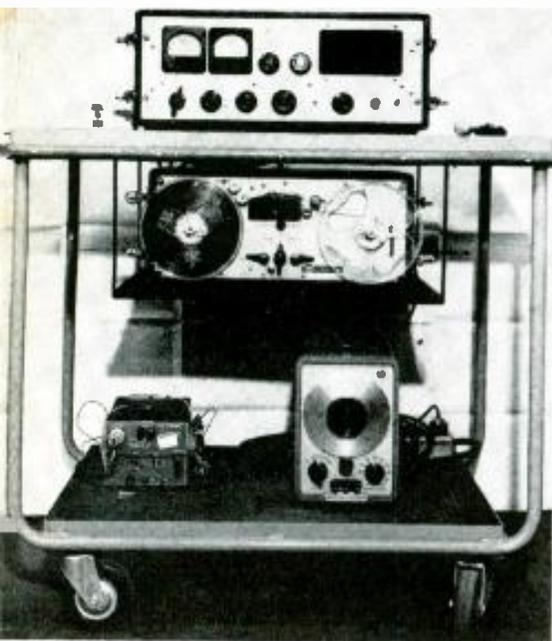


Fig. 1. In the early days of this technique, the audio tape recorder was pressed into service for some industrial instrumentation.

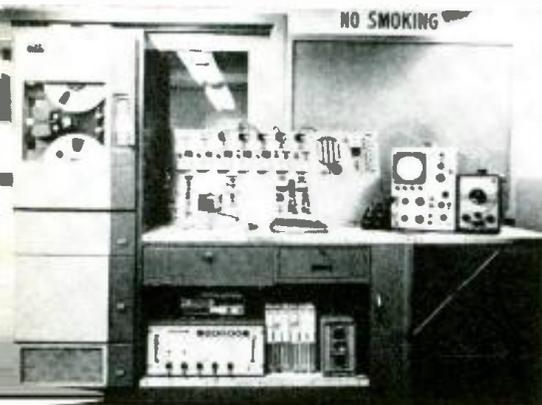


Fig. 2. Later, specialized recorders were developed specifically for this purpose. This setup handles seven channels of data.

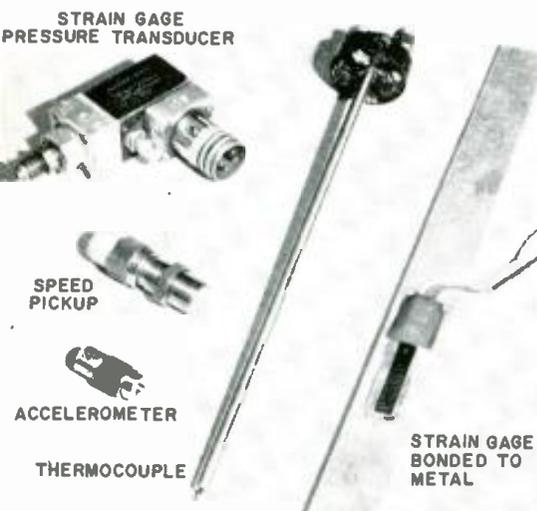


Fig. 3. Here are some of the special-purpose transducers that convert various characteristics into usable electrical signals.

put voltage. When the gage undergoes a resonant strain condition a sinusoidal voltage is produced which is amplified and recorded as a peak-to-peak strain signal.

The FM system is useful for recording low and medium frequencies (d.c. to 10 kc.) with extreme accuracy. This type of recording is not limited by equalization considerations and is dependent upon frequency accuracy—not amplitude only. The signal to be recorded is used to frequency modulate a center carrier frequency in the record amplifier and this, in turn, is recorded on tape. Since the level of the signal applied to the tape is designed for tape saturation, no bias signal is needed in FM recording. The function of the FM reproduce amplifier is to take the frequency-modulated carrier signal from the tape and convert it to conform to the original signal. This is done with conventional limiter and discriminator circuitry. At top left in Fig. 3 is a strain gage pressure transducer that would be applicable to FM recording. The "in-nards" of the transducer consist of a temperature-compensated strain-gage bridge circuit coupled to a movable diaphragm. With suitable excitation voltage applied to the transducer, a pressure applied to the diaphragm will produce an output signal proportional to the amount of pressure applied. This is applied through a suitable balance and control circuit directly to the FM-record amplifier. At the center in Fig. 3 is shown a thermocouple for measuring temperature. A thermocouple produces a feeble d.c. voltage that varies directly with a change in temperature. The temperature range to be recorded determines which type of thermocouple will be used, since a particular type will work well only over a limited temperature range. The most common types used in instrumentation work are cop-

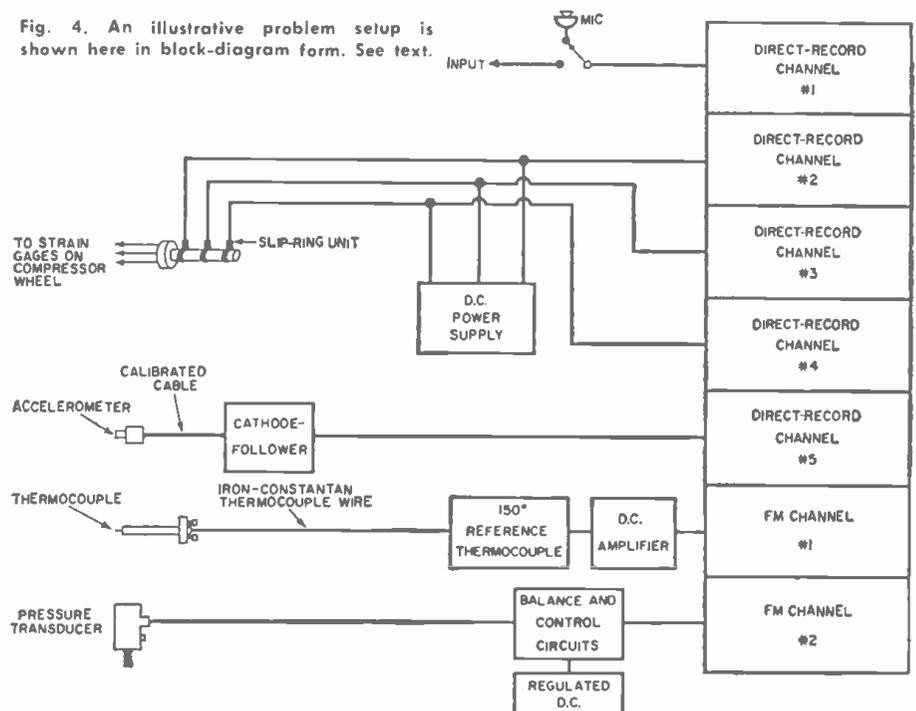
per-constantan for extremely low ranges ( $-300^{\circ}\text{F}$  to  $+200^{\circ}\text{F}$ ), iron-constantan for medium ranges ( $0^{\circ}\text{F}$  to  $+1000^{\circ}\text{F}$ ), and chromel-alumel for the higher ranges ( $+600^{\circ}\text{F}$  to  $2000^{\circ}\text{F}$ ). After the thermocouple signal is applied to a suitable reference junction, it is amplified by a d.c. amplifier to a level suitable for recording.

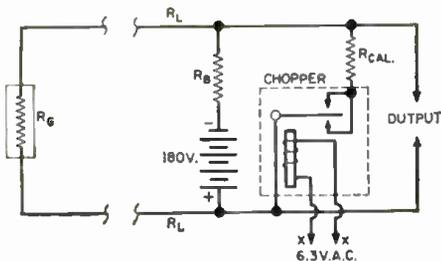
While at the present time the frequency response of the FM-record system is limited to 10 kc., there will be available shortly in the industry FM recording systems that are flat to 20 kc. and beyond. This will allow recording of amplitude information with very good accuracy and simplicity. In general, tape recording as applied to industrial instrumentation, is concerned only with the recording of medium- and high-frequency information. Therefore, d.c. and slow time-response information, except for purposes of correlation, is best left to other types of recording. For example, pressure transducers, thermocouples, and static strain gages, would be more suitable to high-sensitivity galvanometer recorders where many channels of such information can be recorded simultaneously with a minimum of electronic circuitry.

#### A Typical Recording Problem

A typical recording problem is illustrated in the block diagram of Fig. 4. In this case it was desired to measure the stresses present on a gas turbine compressor wheel along with bearing oil temperature, compressor discharge pressure, unit vibration, and compressor-wheel rpm. Three dynamic strain gages suitable for the temperatures to be encountered were bonded to the compressor wheel at the desired locations and brought out to a slip-ring unit. The wheel was then balanced and installed in the gas turbine. Direct-record channels 2, 3, and 4 were used for this appli-

Fig. 4. An illustrative problem setup is shown here in block-diagram form. See text.





$R_g$  = STRAIN-GAGE RESISTANCE 120 $\Omega$ , GAGE FACTOR 2.0  
 $R_L$  = LINE RESISTANCE 5 $\Omega$   
 $R_{CAL}$  = CALIBRATE RESISTOR REQUIRED FOR  $\epsilon$   
 $R_B$  = CURRENT-LIMITING RESISTOR FOR STRAIN GAGE 10K, 10W.  
 $\epsilon$  = CALIBRATION VALUE IN MICROINCHES/INCH

Fig. 5. Dynamic strain gage channel circuit.

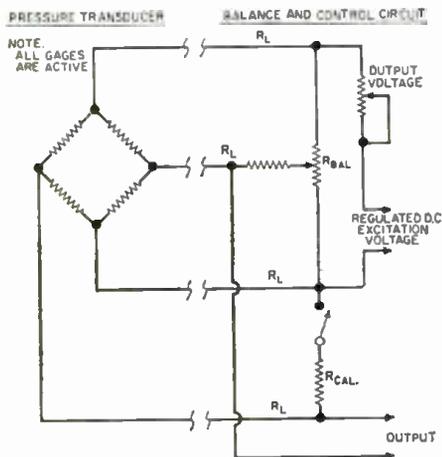


Fig. 6. Control and calibration circuitry.

calibration along with the associated circuitry shown in the block diagram. Direct-record channel 5 was used for the accelerometer signal and channel 1 for the voice commentary. Note that the microphone may be switched out of this channel so that it can be used for data recording as well. Bearing oil temperature was assigned to FM channel 1 and compressor discharge pressure to FM channel 2.

Once proper circuitry has been established, the next important step before recording data is to establish calibration points for each channel of information. This is to be used later in data reduction. Fig. 5 shows the complete circuit of a dynamic strain gage channel. We shall assume the values shown as a basis for calculating the calibrate resistor,  $R_{cal}$ . The gage, or "sensitivity," factor of a strain gage is the ratio of output signal to supply voltage when the gage is stressed within its operating range. This is supplied by the strain gage manufacturer and varies for different types of gages. Another important consideration is the line resistance in the lead wires since this will affect the gage factor. Calculating the new gage factor to allow for line resistance is done as follows:

$$\frac{G.F.}{G.F. (new)} = \frac{R_g + R_L}{R_g}$$

$$\frac{2.0}{G.F. (new)} = \frac{120 + 5}{120}$$

$$G.F. (new) = \frac{240}{125} = 1.92$$

Substituting the new gage factor in the general strain calibration formula and solving, we arrive at a calibration re-

sistance value to produce a simulated strain of 1000 microinches/inch on the gage.

$$R_{cal} = \frac{R_g}{G.F. (new) \times \epsilon} - R_g$$

$$= \frac{125}{1.92 \times 1000 \times 10^{-6}} - 125$$

$$= \frac{1.25 \times 10^2}{1.92 \times 10^{-3}} - 125 = 64,975$$

where:  $\epsilon$  denotes strain in microinches/inch.

However, simply shunting the strain gage with this calibrate resistor will produce nothing as far as the direct-record channels are concerned since they will record only a.c. voltage. Therefore, we must convert the signal into a "dynamic" form in order to record it on tape. This is accomplished by rapidly switching or chopping the calibration resistance in and out of the circuit to produce a square wave, as shown in Fig. 5. However, this is still not quite good enough since the direct-record channel will distort the square wave somewhat and make it difficult to measure. Therefore, we simply apply the square-wave calibration signal to an oscilloscope, match its amplitude with a sine wave from an oscillator, and record the sine wave on the direct-record channel. We now have a reliable calibration signal on the tape for each strain gage. This is done for several different frequencies within the range of interest in order to

ity of circuitry makes accelerometer signals easy to record, but they are difficult to analyze as we shall see in the section on data reduction.

Strain gage pressure transducers require the control and calibration circuitry of Fig. 6 for proper utilization. The transducer is first balanced for zero output voltage by  $R_{bal}$ . The calibrate resistor is then switched into the circuit which simulates a known pressure. Since the d.c. unbalance voltage is applied to an FM channel in this case, it is not necessary that the calibrate resistor be chopped as before. As a double check, a known static pressure may be applied to the pressure transducer and checked against the calibrate resistor. This is often done when critical tolerances are required. Values of calibrate resistors for pressure transducers are arrived at very conveniently with the aid of a pressure-indicating meter and an accurate variable air supply by direct reading of the amount of unbalance voltage produced by the calibrate resistor. No calculations are necessary in this case. Pressure transducers are available in the ranges from a fraction of a p.s.i. to special types that will read thousands of pounds of pressure.

To arrive at a calibration for temperature it is only necessary to refer to a set of tables for the particular type of thermocouple and reference temperature being used (in this case the reference thermocouple temperature is 150

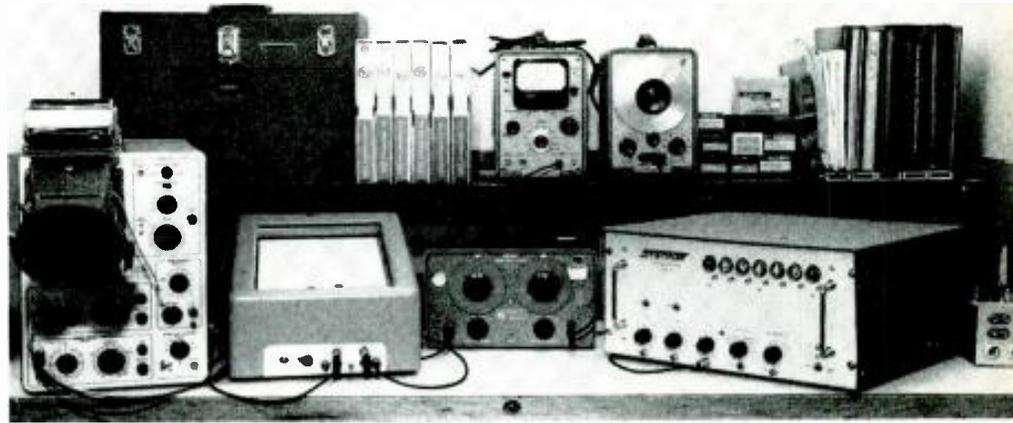


Fig. 7. A typical data-reduction setup for one particular industrial test procedure.

insure maximum possible accuracy.

Fig. 4 is a line diagram for recording vibration. The accelerometer and connecting cable come from the manufacturer complete with a calibration chart. The chart indicates how many millivolts r.m.s. or p.p. that will be generated for each  $G$  of acceleration. To record a calibrate signal of 100  $G$ 's on the tape, we insert a sine-wave signal from an oscillator at some frequency within the accelerometer range (usually 1000 cps) into the cathode-follower input and set the level for the calibration point by reading the oscillator signal on a v.t.v.m. For example, if the chart indicated that the accelerometer produces five millivolts r.m.s. for each  $G$  of acceleration, the calibration voltage for 100  $G$ 's would be 100 x .005 volt, or .5 volt. The simplic-

degrees). For example, if we wish to use an iron-constantan type thermocouple and place a calibrate signal of 500 degrees Fahrenheit on the tape, we refer to the appropriate table and find that an iron-constantan thermocouple with a 150-degree reference temperature will produce an output of 10.71 millivolts d.c. at 500 degrees. An accurate millivolt source is then used to apply this value to the d.c. amplifier and the gain set to provide a suitable level for recording on the FM channel. This completes the calibration for temperature and the thermocouple may now be connected.

The calibration of unit rpm is probably the simplest of all since it is only necessary to know the number of gear teeth coupled to the speed pickup. Knowing this, the formula for the cali-

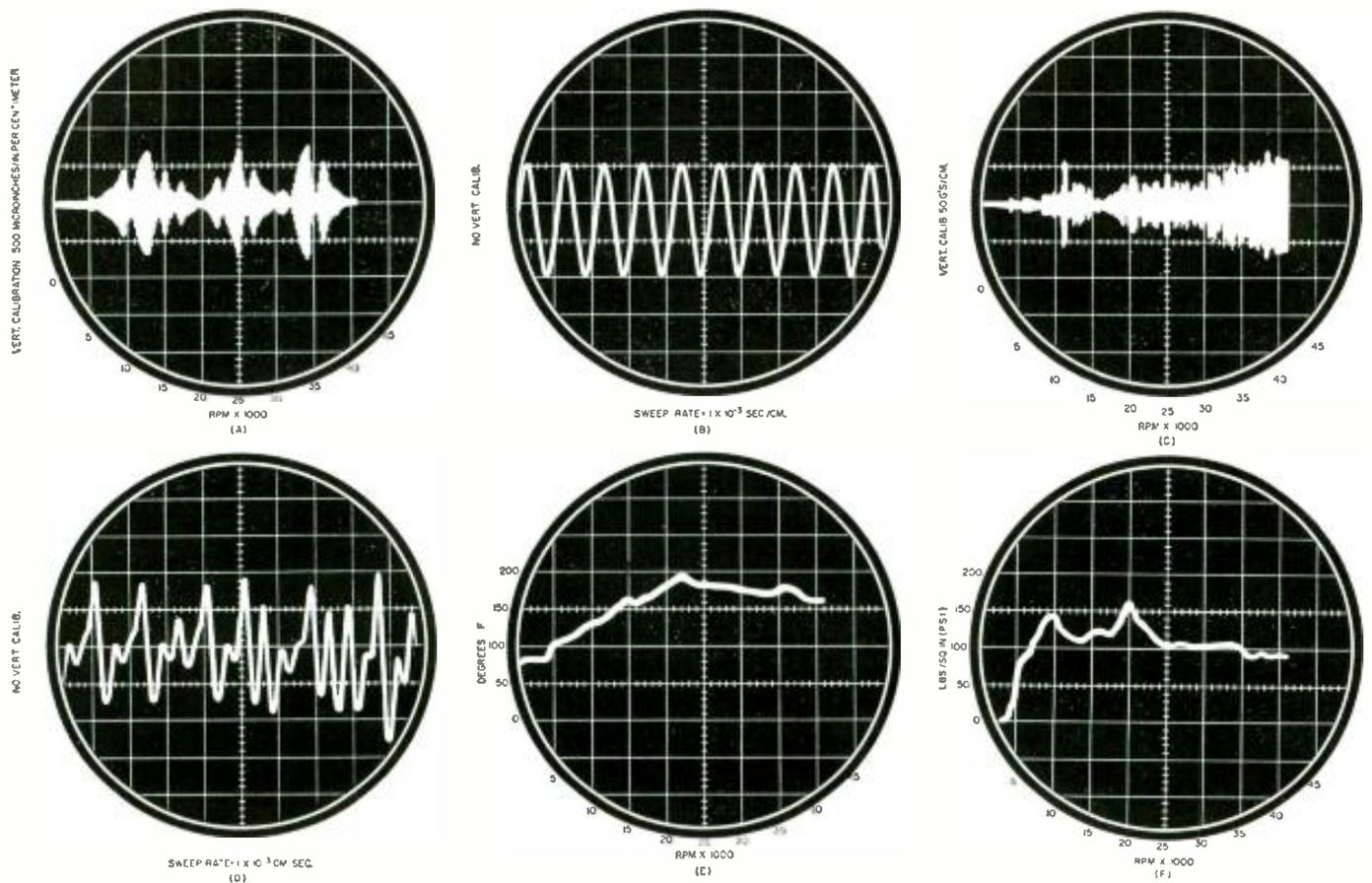


Fig. 8. This is what the information looks like as it appears on the scope. Note that each division equals 1 cm. (A) Dynamic strain amplitude (peak-to-peak) vs rpm. (B) Single sweep of strain point of part A. (C) Unit vibration (peak-to-peak) vs rpm. (D) Single sweep of vibration point of part C. (E) Bearing oil temperature vs rpm. (F) Compressor discharge pressure vs rpm.

brate frequency becomes the following:

$$\text{Calibration Frequency} = \frac{N \times S}{60} = \text{cps}$$

Where:  $N$  = number of teeth on the gear and  $S$  = speed calibration point (rpm).

An oscillator coupled to a digital frequency counter is used to apply the calibrate signal to the direct-record channel. No special precautions are necessary in the use of speed pickups except to monitor the input level of the signal to the tape recorder during the test to see that it does not become high enough to distort the waveshape. During the actual test run it is very important to keep an accurate record of each event to refer back to during the data reduction process. Information is worthless no matter how accurate, if a log is not maintained as to the conditions, time, sequence, and tape check points during the run. It is also necessary during the test run to watch the input meters carefully for any sign of abnormal readings that may indicate trouble in connecting cables or transducers.

#### Methods of Data Reduction

Although it sometimes requires only a few minutes of actual recording time for a test, it may require many hours of intense study and work to reduce the data to a usable form. We shall investigate a few of the methods employed

for reducing the information on the tape. Any type of information can be read out in the form of an X-Y plot. In this particular test rpm or time would be used for the X axis and the amplitude of the signal to be measured would be the Y variable. Since we need a very high response type of plotter for the strain gage and accelerometer information, we shall plot these two channels on the oscilloscope while photographing the complete test run. Polaroid projection-type film is used in the camera in order that standard 8 1/2" x 11" prints can be made. Fig. 7 shows a typical data reduction set up. On the left can be seen a dual-beam oscilloscope with the camera attached. To the right of the oscilloscope is an X-Y plotter which, in this case, is used to plot the temperature and pressure traces. Located in the center of the table is a variable band-pass filter which allows a bandpass of any width through the range of 0-200 kc. Immediately above the filter is a frequency meter which provides a d.c. analogue output voltage for frequency input. On the far right is a digital frequency counter which reads both cps and period measurement. Located above the counter is a sine-wave oscillator which is flat up to 600 kc. This represents only a partial listing of the equipment that may be used for data reduction depending on the requirements of the particular test.

Fig. 8 shows what the information

will look like once it is reduced to a usable form. Fig. 8A shows one of the strain gage signals on the compressor wheel with all the stress points from light-off of the unit to maximum speed. Note that there are three large stress points. These points would be of great interest to the design engineer since they represent critical points where damage to the wheel might occur. Therefore, we must be able to determine their exact magnitude and frequency. The magnitude can be read directly from the photograph as well as the speeds where they occur. However, to determine the exact frequency of each point, we must use another method. We first set the scope sweep to a convenient range to acquire an approximation of the frequency. Fig. 8B shows one sweep and it is observed to be near 20 kc. We then place an oscillator signal on the second channel of the oscilloscope and adjust the frequency for 20 kc. As we re-run the point on the tape we shift the frequency slightly each time until we have a stationary Lissajous pattern indicating the frequencies are at zero beat. Since the oscillator dial reading will not be accurate enough for our purposes, we now apply the oscillator signal to the digital frequency counter and read it out to within one cps. This process is repeated for each of the three stress points. We now have arrived at frequency and magnitude for one of the

(Continued on page 111)



# New G-E Tool Toter puts tools and parts at your fingertips

No more digging for the right tool—not with this handy new G-E Service Aid. The Tool Toter. Measures just 11" x 14", 12" high. It's especially designed to go along wherever tools are needed: on the bench, on the counter, on the job or for general maintenance. Pegboard with tool holders keeps screw drivers, pliers, nut drivers, etc., clearly visible and easily removed or replaced. High-impact plastic trays hold screws, nuts, lockwashers, fuses, and other small tools or parts that are needed on-the-spot. Order your Tool Toter today—helps make service calls more profitable. Saves your time and your temper. ETR-2338 Tool Toter.

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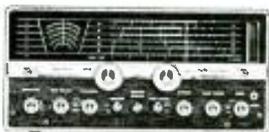
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## Hi-Fi-Audio

## Product Review

### TUNER AND STEREO AMPLIFIER

Sargent-Rayment Co., 4926 E. 12 St., Oakland 1, Calif. has brought out an FM tuner and stereo amplifier combination which features a pre-switched input



channel that accommodates other units for all types of stereo broadcasts, such as AM/FM, FM/FM, or FM/multiplex, depending on what other unit (tuner or multiplex adapter) is fed into that channel.

Designated as Model SR-1040, the new set includes a stereo amplifier with controls, rated at 10 watts per channel. Among its features are stereo inputs for phono and tape, a "center channel" output jack, and a "stereo separation" control.

### NEW AUDIO KITS

Radio Shack Corp., 730 Commonwealth Ave., Boston 17, Mass. has announced two new audio kits. Shown here is the "Realistic" FM tuner, Model 200, a kit version of the company's Model FM-3 tuner. The tuner uses a three-gang tuning capacitor, separate tuned



r.f. stage; cascade front end, and a.f.c. Response is given as 20 to 20,000 cycles.

Another new kit is the "Realistic" stereo integrated amplifier, featuring built-in preamp and controls as well as rated power of 20 watts per channel.

### NEW CERAMIC CARTRIDGE

Sonotone Corp., Elmsford, N.Y. has introduced its "Velocitone," an assembly that consists of the company's new "9T" stereo ceramic cartridge and two matched equalizers. The equalizers plug into the velocity or magnetic inputs of an amplifier to convert the output of the "9T" to a flat velocity response tailored for RIAA equalization.

Response of the new cartridge is said

to be flat,  $\pm 1/2$  db, from 20 to 6000 cycles, and 1 db to 17,000 cycles with "deliberate roll-off" to 20,000 cycles. Output voltage is 11 millivolts. Compliance is stated at  $3.5 \times 10^{-6}$  cm. dyne; tracking pressure given is 2 grams for professional tone arms and 3 grams for changers.

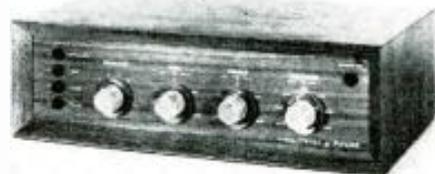
### NEW TURNTABLE KIT

Fairchild Recording Equipment Corp., 10-40 45th Ave., Long Island City 1, N.Y. has entered the kit field with the release of its new Model 440-2K turntable in do-it-yourself form.

The unit is similar to the Model 440 two-speed turntable introduced by the company last year. The kit is furnished with all parts, instructions, and a pre-cut mounting board.

### TRANSISTOR STEREO AMPLIFIER

Polar Electronics, Ltd., 1514 Oak St., So. Pasadena, Calif. has brought out an



all-transistor stereo preamplifier-amplifier, offering control facilities and a rated power output of 15 watts per channel. A unique feature of the unit is its complete circuit encapsulation which protects it from rough usage, dust, and moisture. Said to have no problems of heat, hum, or microphonics, the unit is fully guaranteed for 30 months.

First in a new line of transistorized stereo components being manufactured by the firm, the new amplifier can be operated on a.c. or d.c. power. Response is given as 20 to 20,000 cycles with less than 1 per-cent distortion. The unit measures 3 inches high by 12 inches wide by 7 inches deep and comes in a furniture-finished wood cabinet.

### COMPACT SPEAKER SYSTEM

Erconu Corp., 16 W. 46 St., New York, N.Y. is distributing a new Swedish speaker system of compact proportions. Known as the "Nordic I," the system includes woofer, tweeter, and crossover network pre-assembled in a furniture-finished enclosure.

A unique feature of the drivers is the use of a multi-layered free-floating cone, described as a "sandwich" and said to reduce harmonic distortion. Each layer of the speaker cone, from the edge sus-

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- "This is the best checker I have ever used."  
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- "I already own one. This is my second Mighty Mite."  
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- "Mighty Mite has paid for itself the first month."  
W. C., UNIONTOWN, PA., TV REPAIR
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L. K. E., W9PWQ, CHICAGO, HAM

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**MAGAZINE TEST LABS SAY...**

*PF Reporter, Nov., 1960, page 65...*  
"When putting the Model TC109 to work in the lab, I tried to 'trip up' the tester by throwing a few curves at it. Using my prized collection of rejected tubes that have mostly 'tough dog' defects, I proceeded with the tests given in the Sencore instructions. The results: The Mighty Mite found every trouble, even the toughest."

*Les Deane*

*Electronics World, Jan., 1961, page 103...*  
"We checked two dozen tubes known to be defective. Many had been passed as 'good' by other testers. Each failed at least one of the three tests provided by the TC109. On the other hand, every new tube previously known to be in good condition checked good on the Mighty Mite."

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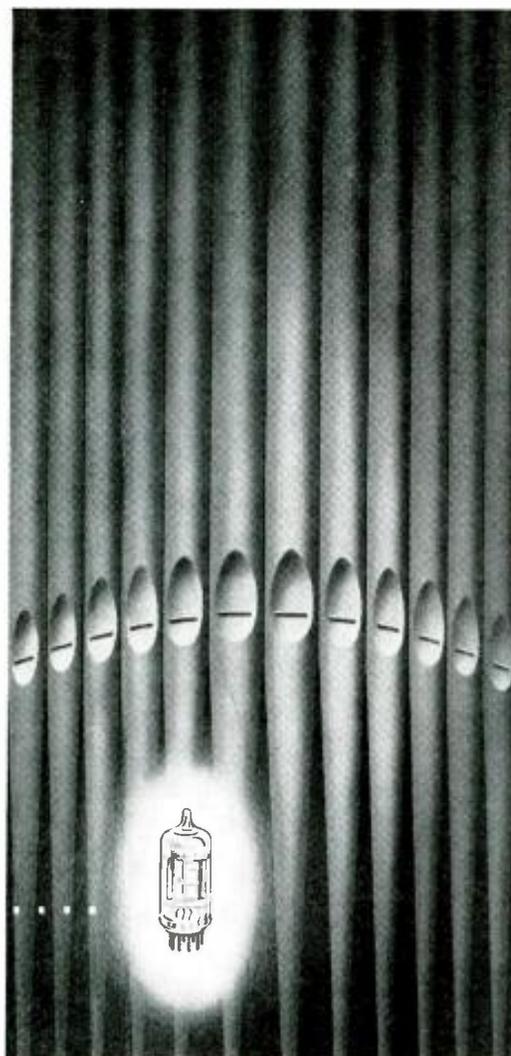


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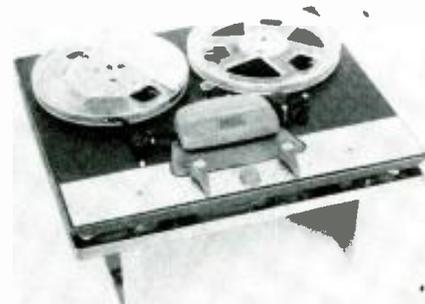
pension, through the damping layer, and then to the sound generating layer, is made of a different fibre. Claimed response is 45 to 18,000 cycles. The tweeter cuts in at 5000 cycles with crossover occurring at 7500 cycles.

**STEREO TAPE DECKS**

*Ampex Audio Co.*, 1020 Kifer Rd., Sunnyvale, Calif. has announced two tape players that contain the basic mechanism used in the company's Model 960 equipment.

Model 934 is supplied without playback preamplifiers, the signal being taken directly from the heads and fed to suitable inputs on an external pre-amplifier. Model 936 includes self-contained playback preamplifiers, equalized for connection to power amplifiers and/or an audio control unit.

Both tape decks are two-speed (3¾



and 7½ ips) units, and will play quarter-track stereo, half-track stereo, full-track, and monophonic.

**STEREO AMPLIFIER KIT**

*Allied Radio Corp.*, 100 N. Western Ave., Chicago 80, Ill. has introduced a 70-watt integrated stereo amplifier in kit form. Designated by stock number 83-YU-934, the unit delivers 35 watts power per channel, with an IHFM music-power rating of 96 watts. Featured is a blend control to regulate channel separation, as well as a "center channel" output.

Response is stated as +1 db, 20 to



35,000 cycles at 35 watts output on each channel. At this level, harmonic distortion is given as under 0.5% and IM distortion as under 1%. Hum and noise are better than 75 db below rated output.

Printed circuit switches, printed circuit boards, and special plug-in assemblies of resistors and capacitors are offered as time-saving and error-reducing features for the kit builder.

**AUDIO INPUT TRANSFORMERS**

*Chicago Standard Transformer Corp.*, 3501 W. Addison St., Chicago 18, Ill. has introduced three new audio input transformers which are claimed to have a wide variety of applications in both original equipment and as replacements.

All three transformers have a primary impedance of 600/500 ohms center-

tapped. *Stancor* unit A-4778 is a line-to-grid transformer. Model A-4779 is for line-to-single or push-pull grid applications. Model A-4780 is for line-to-push-pull applications. Additional information can be obtained by writing to the manufacturer, requesting *Stancor* Bulletin 575.

#### TRANSISTORIZED COMPONENTS

*Johnson Electronics, Inc.*, P.O. Box 1675, Casselberry, Fla. is offering tran-



sistorized components designed specifically for the background music industry.

Shown here is Model JE 25 MA, a 25-watt amplifier, with response from 30 to 7500 cycles,  $\pm 3$  db. The multiplex tuner features sensitivity of 2 mv. for 20 db of quieting. Audio response is between 50 and 9000 cycles. The tuner is crystal controlled. For more details, write to the manufacturer.

#### STEREO SERVICE KIT

*Motorola Inc.*, 4545 W. Augusta Blvd., Chicago 51, Ill. has introduced a "stereophono service kit" for service dealers and technicians. The kit includes three different ceramic cartridges, a *Motorola* idler wheel replacement, a strobe disc, a stylus pressure gauge, and a manual covering the latest record-changer servicing techniques.

The three phono cartridges are exact replacements for units employed in 1961 *Motorola* stereo sets, but reportedly can be used in most changers requiring ceramic pickups. All employ a diamond/sapphire stylus.

#### "STEREO ONLY" CARTRIDGE

*Benjamin Electronic Sound Corp.*, 97-03 43rd St Ave., Corona 68, N. Y. announces a new magnetic phono cartridge designed for use with stereo records only. According to the New York importer and distributor of *ELAC* products, the new cartridge "is the standard playback cartridge used by broadcast studios throughout Europe."

Called the "Studio" and designated as Model ST-310D, the new cartridge comes with a 0.52-mil diamond stylus. Stated specifications include: frequency range of 20 to 20,000 cycles; crosstalk damping of 24 db; tracking force, 3-5 grams.

#### "TRI-HELIX" SPEAKER

*Lafayette Radio Corp.*, 165-08 Liberty Ave., Jamaica 33, N.Y. has brought out a 10-inch three-way speaker designed expressly for "bookshelf" enclosures. Designated as the "Tri-helix," stock No. SK-180, the new speaker utilizes three mechanically and electronically independent speakers mounted within a single 10-inch frame. The two-inch tweeter and the five-inch mid-range speaker are fed by a built-in

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LK-72 72-Watt stereo complete amplifier kit (left), \$149.95. LT-10 Wide-Band FM Tuner kit \$89.95.\*

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" . . . I would run out of superlatives if I tried to adequately state how I feel about this tuner . . ." — Samuel R. Harover, Jacksonville, Ark.

" . . . without a doubt the easiest kit I have ever built (out of 11) . . ." — B. P. Loman, Jr., Rochester, N. Y.

" . . . finest kit I have ever built. And one of the finest tuners I have heard, kit or otherwise." — A. J. Zilker, Houston, Texas.

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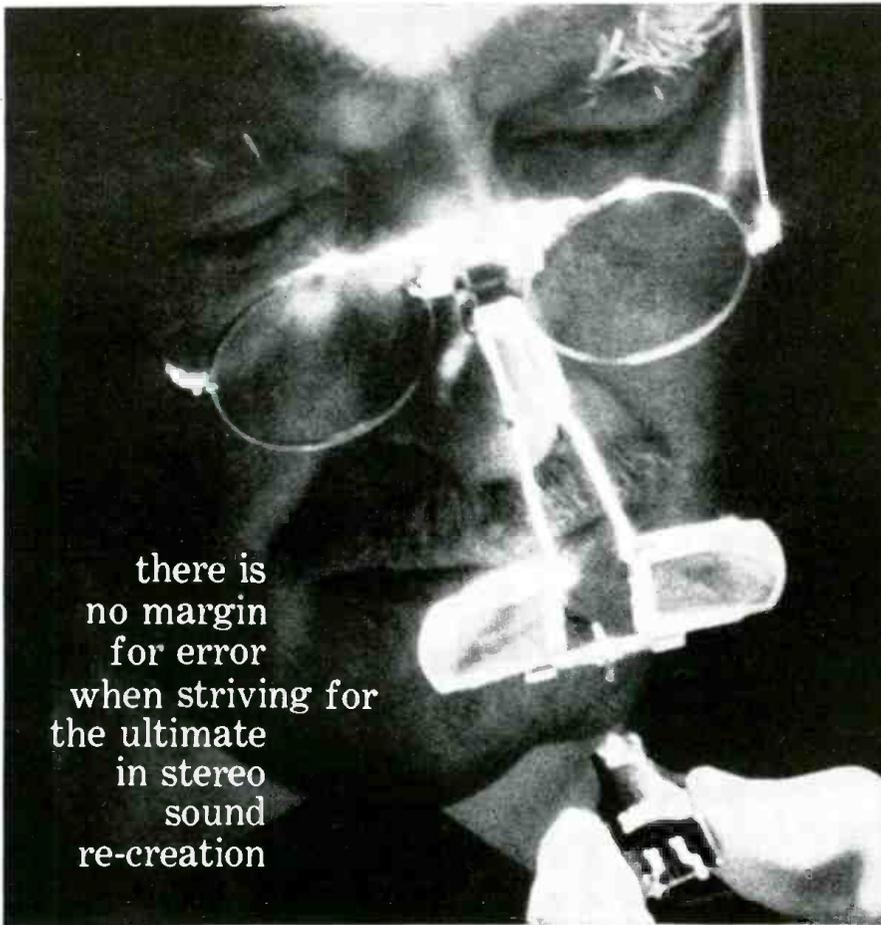
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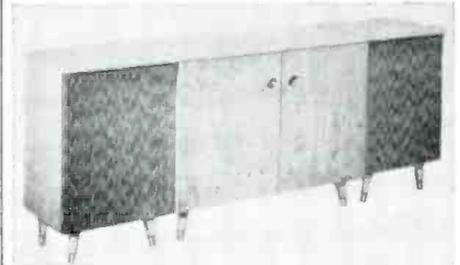
125-TD E. 88 St.

New York 28, N. Y.

electrical network with crossover frequencies at 1500 and 5,000 cps. To minimize interaction among the three cones, the mid-range and tweeter units are mounted eccentrically or off-center with relation to the woofer. Additionally, they are completely enclosed in their own baffles.

**MATCHED CABINETS**

Homewood Industries, 26 Court St., Brooklyn, N.Y. has introduced matched equipment and speaker cabinets for



housing various combinations of stereo components. The cabinets are fully assembled and ready to finish by the purchaser. The speaker enclosure unit has an adjustable bass-reflex port that can accommodate either 12-inch or 8-inch speakers.

The equipment cabinet is well-vented. Both units are of lowboy design and are fitted with 5-inch brass-ferruled legs.

**STEREO TUNER**

Electronic Instrument Co., Inc., 33-00 Northern Blvd., Long Island City 1, N.Y. has introduced a new Eico FM/AM stereo tuner, available in factory-wired or kit form. Two completely independent sets of controls allow the tuner, Model ST96, to be used for separate FM and AM reception, or for AM/FM stereo, or—with the addition of an adapter—for FM-multiplex.

Both the AM and FM sections have pre-wired, pre-aligned r.f. and i.f. stages to facilitate building the unit from the



kit. The FM section uses switched a.f.c., as well as a.g.c., stabilized low limiting threshold for weaker signals, and broadband ratio detector for "improved capture ratio and easier tuning." FM frequency response is given as 20 to 15,000 cycles.

The AM section features switched "wide" (to 14 kc.) and "narrow" (to 7 kc.) bandpass. AM frequency response is stated as 20-9000 cycles (wide) or 20-4500 cycles (narrow).

**QUARTER-TRACK STEREO HEAD**

Robins Industries Corp., Flushing 54, N.Y. has announced a new M/M quarter-track stereo record/playback tape head, designed as an exact replacement for a number of popular tape recorders. Known as Model 5Q17-105, the new

head serves as replacement on the following models: Bell T-200, T-201, T-203, BT205-1B, T-206, T-207S, T-211, BT205-0B; *Ektatape* 250, 360, 362; and VM 714 and 750A.

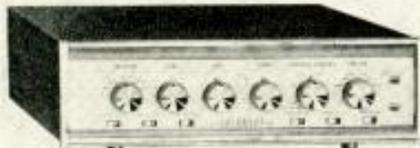
#### COMMUNICATIONS-RADIO SYSTEMS

Webster Productomatic Corp., 795 Monroe Ave., Rochester 7, N.Y. has announced a line of "communications-radio" systems for a number of uses in the home, such as answering the door, minding the baby, playing music throughout the house, communicating from room to room, and clock radio applications.

A variety of basic units and accessories is available in this new "Guardian" line. For full particulars, write to the manufacturer.

#### STEREO CONTROL AMPLIFIER

Sherwood Electronic Laboratories, Inc., 4300 N. California Ave., Chicago 18, Ill. has announced a new stereo amplifier-preamplifier rated at 80 watts, music-power rating. Designated as Model S-5000 II, the new instrument is said to be an improved model of the



firm's S-5000 amplifier. Power output of the new version is 36 watts per channel.

Included on the new amplifier are new 12 db-per-octave scratch and rumble filters, ten two-channel controls, stereo normal/reverse switch, phase inversion switch, and dual amplifier monophonic operation with either set of inputs. Hum and noise are listed as 60 db below rated output. Phono sensitivity is 1.8 mv. The amplifier provides for a "third channel" output.

#### STEREO REMOTE CONTROL

Sun Radio Service, 320 Chestnut St., Kearny, N.J. has announced a remote control unit for use in stereo systems that employ a separate preamp and power amp.

Controls include balance, channel, and volume. A special low-capacitance cable minimizes high-frequency loss. The unit may be used up to 30 feet away from the rest of the system. It is available in a metal enclosure or in a walnut or mahogany cabinet.

#### "CITATION" FM TUNER

Harman-Kardon, Inc., Plainview, Long Island, N.Y. has announced the



"Citation III" FM tuner, available as a kit or factory-assembled. Reportedly,

# 2 for the money

circuit by

**EICO**

tubes by

**Amperex**



EICO described the Amperex tubes used in their new HF89 100-Watt Stereo Power Amplifier with the word, "unsurpassed." And with good reason. The HF89 delivers 100 RMS watts undistorted from 20 to 20,000 cps. 1M distortion at normal listening levels (even with low-efficiency speakers)... less than 0.1%!

To achieve these standards, EICO chose 4 Amperex 6CA7/EL34's for the HF89's output stage and 1 Amperex 12AX7/ECC83 for its voltage amplifier stage. The results: full-rated power output, inaudible distortion, low hum and noise, and the absence of microphonics.

These and many other Amperex 'preferred' tube types have proven their reliability and unique design advantages in virtually all of the world's finest audio components.

Write today for the *Audio Designers Handbook*, new 33-page booklet featuring 14 pages of complete schematics of mono and stereo preamplifiers and amplifiers. Price, \$1.50. Amperex Electronic Corp., Special Purpose Tube Division, 230 Duffy Ave., Hicksville, Long Island, N. Y.



about hi-fi tubes  
for hi-fi circuitry

#### AMPEREX TUBES FOR QUALITY HIGH-FIDELITY AUDIO APPLICATIONS

##### POWER AMPLIFIERS

6CA7/EL34: 60 w. distributed load  
7189: 20 w., push-pull  
6BQ5/EL84: 17 w., push-pull  
6CWS/EL86: 25 w., high current, low voltage  
6BM6/ECL82: Triode-pentode, 8 w., push-pull

##### VOLTAGE AMPLIFIERS

6267/EF86: Pentode for pre-amps.  
12AU7/ECC81: Twin triodes, low hum, noise and  
12AX7/ECC83: J microphonics  
6BL6/ECF80: High gain, triode-pentode, low hum, noise and microphonics

##### RF AMPLIFIERS

6ES8: Frame grid twin triode  
6ER5: Frame grid shielded triode  
6EH7/EF183: Frame grid pentode for IF, remote cut-off  
6EJ7/EF184: Frame grid pentode for IF, sharp cut-off  
6AR5/ECC85: Dual triode for FM tuners  
6DCA/EBF89: Duo-diode pentode

##### RECTIFIERS

6V4/EZ80: Indirectly heated, 90 mA  
6CA4/EZ81: Indirectly heated, 150 mA  
5AR4/GZ34: Indirectly heated, 250 mA

##### INDICATORS

6FG6/EM84: Bar pattern  
1M3/DM70: Subminiature "exclamation" pattern

##### SEMICONDUCTORS

2N1517: RF transistor, 70 mc  
2N1516: RF transistor, 70 mc  
2N1515: RF transistor, 70 mc

1N542: Matched pair discriminator diodes

1N67A: AM detector diode, subminiature

#### Lag-55 Audio Generator Sine Square

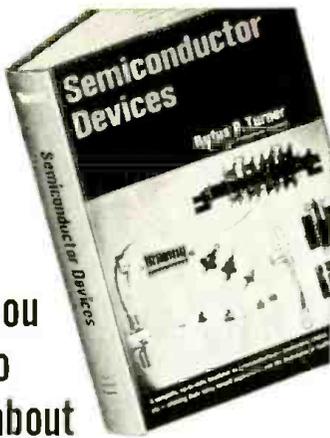
new "LEADER" test instrument

A multi-purpose generator for measurements on audio equipment-amplifiers, speakers, networks. Three waveforms: sine, square and complex for all types of measurements including response, distortion, transient and I-M distortion checks. Full range is from 20 to 200,000 cps, output 5 volts with minimum amplitude variation throughout whole range.



#### OHMATSU ELECTRIC CO. LTD.

850 Tsunashima-Cho, Kohoku-Ku  
Yokohama, Japan.



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what you  
need to  
know about

# SEMI- CONDUCTORS!

- DIODES • TRANSISTORS
- THERMISTORS • VARISTORS
- Power and controlled RECTIFIERS
- ZENER DIODES • PHOTO CELLS
- PARAMETRIC and MAGNETIC DEVICES, etc.

plus  
using, testing and  
measuring  
semiconductors

Here at last is a down-to-earth 278-page book that gives you a practical working knowledge of semiconductors—from transistors to diodes, power and controlled rectifiers, ZENER diodes, varistors, thermistors, photo cells, parametric and magnetic devices and all the rest! It answers your questions about these remarkable little devices—equips you with the complete know how of their types, construction, circuit applications, testing and use.

No other field of electronics in recent years has experienced such remarkable growth. SEMICONDUCTOR DEVICES by Rufus Turner gives you a clear understanding of the entire subject—and does it without a lot of complicated mathematics. It has been specifically written for electronic technicians, servicemen, experimenters who are finding it increasingly important to have more than just a casual knowledge of these little devices which are literally revolutionizing electronic circuitry and design.

Standard and special-purpose types and their uses are fully explained. Over 250 illustrations demonstrating semiconductor circuitry and operational and construction features greatly simplify your understanding of the subject. Of particular importance, methods of testing and measuring semiconductor devices are spelled out in detail. Price \$6.95 on 10-day money-back guarantee basis.

## 10-DAY FREE EXAMINATION

Dept. RN-41, Technical Division,  
HOLT, RINEHART and WINSTON, Inc.,  
383 Madison Ave., New York 17, N. Y.

Send Turner's big, 278-page SEMICONDUCTOR DEVICES Manual for 10-day free examination. If I decide to keep book, I will then promptly send you \$6.95 in full payment. If not, I will return book postpaid and owe nothing.

(SAVE! Send \$6.95 with order and we pay Postage. Same 10-day return privilege with money promptly refunded.)

Name \_\_\_\_\_  
Address \_\_\_\_\_  
City, Zone, State \_\_\_\_\_

OUTSIDE U.S.A.—\$7.45, cash only. 10-day return privilege with money refunded.

the new tuner has no measurable distortion or station drift, "breaks the noise barrier" of 5 db by using a 4 db RCA nuvistor tube for the front-end circuit (which is also claimed to increase sensitivity), and has an audio range stated as three octaves above and below human hearing.

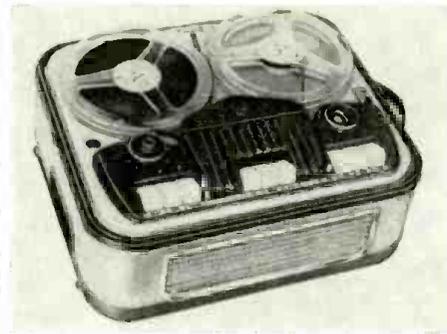
As in other "Citation" units, the tuner uses terminal-board construction. To facilitate the work of the kit-builder, most of the critical tuner elements are pre-wired and aligned in a newly developed "FM cartridge" which includes the third r.f. stage, mixer, oscillator, i.f. sections, and a.f.c. With this cartridge as a "standard," the hobbyist can use the two tuning meters provided to maintain alignment of other sections of the tuner.

The tuner embodies many other advanced circuit and design features; for full details, write to the manufacturer.

### 4-TRACK STEREO RECORDER

North American Philips Co., Inc., High Fidelity Products Div., 230 Duffy Ave., Hicksville, Long Island, N.Y. has announced the *Novelco* "Continental 300" (Model EL3542), a 4-track stereo playback and monophonic record/playback tape recorder.

Completely self-contained, the "Continental 300" includes a tape drive mechanism, recording/playback pream-



plifier, power amplifier, and a wide-range speaker. Also furnished is one of the firm's dynamic microphones.

The unit plays standard 4-track stereo tapes through an external preamplifier/amplifier, the signal being taken direct from the head. The machine will also record and play 4-track mono tapes through its own facilities or through an external sound system.

### NEEDLE ASSORTMENT

*Astatic Corp.*, Conneaut, Ohio, which recently announced the "Asta-Stock" system for distributors of its needle line, is now supplying dealers with a complete stocking and merchandising center for its needles.

The "center" consists of an attractive cabinet that contains 50 needles of 43 different types, as well as replacements for all new phonographs including 1960 stereo sets plus all popular mono replacements. Complete cross-reference information is provided.

### "LANGUAGE LAB" RECORDER

*Telectro Industries Corp.*, 35-16 37th St., Long Island City 1, N.Y. has announced its Model TR-922-C, designed

primarily for "language laboratory" applications. Its purpose is to assist an instructor teaching students a foreign language in group or individual instruction.

Special features of the TR-922-C include: a "record-practice" switch which permits the student to listen and record simultaneously; individual controls for instructor and student; dual headphone jacks; tape indexer; dual-track operation; and three speeds—1½, 3¼, and 7½ ips.

### ELECTROSTATIC SPEAKER KIT

*Neshaminy Electronic Corp.*, Neshaminy, Pa. has announced a wide-range speaker system "kit," consisting of an electrostatic mid- and high-range speaker, and a matching dynamic woofer pre-mounted on a rigid 19½" x 16" panel designed for installation in existing furniture, walls, or into custom-built units.



Known as the "JanKit 41," it employs a *JansZen* electrostatic speaker with two push-pull radiators responding from 700 to beyond 30,000 cycles. The woofer is a *Neshaminy* Model 350 speaker, a high-compliance, 11-inch cone woofer with response reported down to 30 cycles.

The system is supplied with instructions for mounting, or for building a shelf-type enclosure to house the system.

### NOVEL SPEAKER SYSTEM

*Polycooustic Co.*, 958 Arguello Drive, San Leandro, Calif. has introduced a speaker system that employs a total of 28 speakers, specially treated and installed in an enclosure described as a "vented infinite baffle." Six of the speakers are hard-cone tweeters.

The system is said to provide exceptionally wide sound dispersion, has a claimed response of 30 to 15,000 cycles ± 2 db, an efficiency of 20 per-cent, impedance of 8 ohms, and distortion of 1 per-cent at 100 db output.

The speaker is being offered in kit form or fully assembled.

### AUDIO CATALOGUES

#### BOGEN PORTABLES

*Bogen-Presto Div.*, Box 500, Paramus, N.J. is offering a six-page brochure and engineering specification sheets on the new *Bogen* VP-20 and VP-40 portable transcription players. The brochure (Catalogue No. 702) and the spec sheets (ES-VP-20 and ES-VP-40) are available on request to the manufacturer.

#### ROCKFORD CABINETS

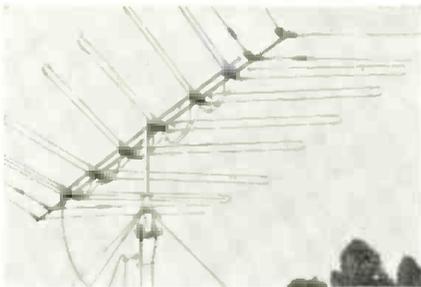
*Rockford Special Furniture Co.*, 1803 W. Belle Plaine, Chicago 13, Ill. has issued Bulletin R-19, describing new cabinets for housing stereo or mono high-fidelity components. Write to the company for a free copy.

# CHANNEL MASTER harps on one theme: PERFORMANCE!



To make the most, feature the best — sky-high quality products by Channel Master. Channel Master moves the goods because it delivers the goods. It's the brand that gives you those heaven-sent little "extras". Top quality and top performance for your customers — maximum volume and profits—you get the best of both. Just follow your "growth line" — Channel Master.

### CHANNEL MASTER SUPER 10 T-W ANTENNA



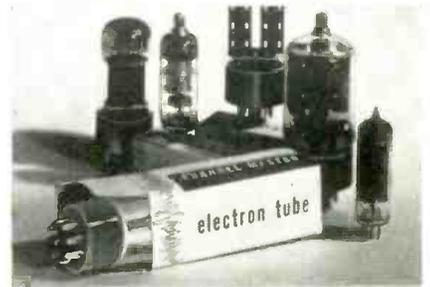
The most powerful super-fringe antenna yet developed. Based on Channel Master's unique Traveling Wave principle, it has 10 elements and offers up to **78% more power** for picture-poor homes.

### CHANNEL MASTER TENN-A-LINER ROTATORS



The only automatic rotator that can be aimed within **one degree** of the required direction. Unsurpassed accuracy, plus great repeatability and easier, quieter operation.

### CHANNEL MASTER PREMIUM QUALITY TUBES



America's fastest growing line! Longer-lasting, uniformly dependable, with minimum call-backs. No other tube make offers greater opportunity for profits than these fully proved performers.



**CHANNEL MASTER** works wonders in sight and sound  
ELLENVILLE, N. Y.

# COYNE'S New Complete Pin-Point TROUBLE SHOOTING Series

See All 4  
Books On 7-Day  
FREE TRIAL!

Takes Headaches Out Of  
All Servicing Problems!



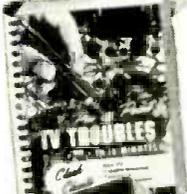
**Pin-Point**  
**TRANSISTOR TROUBLES**  
IN 12 MINUTES!

Trouble-shoot every type of circuit in ALL transistorized equipment! 525 pages; hundreds of illustrations; 120 check charts! \$5.95



**Pin-Point**  
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TROUBLES IN 5 MINUTES!

Locate mechanical and electronics troubles fast. Covers all makes. 320 pages; 450 photos; 58 check charts! \$3.95



**Pin-Point**  
**TV TROUBLES**  
IN 10 MINUTES!

Find the exact sound or picture trouble in any TV set from 700 possibilities! 300 pages; 300 diagrams, check charts! \$4.95



**Pin-Point**  
**COLOR TV TROUBLES**  
IN 15 MINUTES!

Covers every type of color TV and picture tube! 530 pages; 362 check charts, diagrams, picture patterns! \$5.95

## Simple Check Chart System Saves Time

These amazing practical handbooks with an ENTIRELY NEW METHOD, show you how to find the trouble in ANY tv, record changer or transistor circuit FAST! Index tells you where to look; famous Check-Charts help you pin-point the exact trouble in minutes! These on-the-job books quickly pay for themselves in profitable new business and valuable time saved!

### SEND NO MONEY!

Just mail coupon for 7 DAY FREE TRIAL. If you keep all 4 books, pay only \$3.00 per month until \$21.35 plus postage is paid. Cash price for Set only \$18.95. Or return books and pay nothing. Either way, FREE BOOK IS YOURS.

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- Rush 4-Book PIN-POINT Series for 7-day FREE TRIAL per offer. For individual books, check below.
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## Within the Industry

(Continued from page 22)

operated as a division of the parent firm under the direction of its present president, Charles George... **THOMSON RAMO WOOLRIDGE INC.** has moved to acquire **RADIO CONDENSER COMPANY** of Camden, N.J. by exercising its option to buy more than 90 per-cent of the New Jersey firm's outstanding stock.

**WILLIAM J. SLAWSON** has joined the sales staff of the *Weston Instruments Division, Daystrom, Incorporated*, as product sales manager of "Vamistors."



Mr. Slawson brings to his new job some twenty-one years of experience in electronic and industrial sales. Before coming to *Weston* he was general sales manager for the industrial division of *Telectro Industries*, and prior to that he held positions with *PRD Electronics*, *Pyramid Electric*, and *ITT Federal Division*.

Mr. Lawson attended New York University and is a member of the Institute of Radio Engineers.

**BELL TELEPHONE LABORATORIES** has received the annual "Industrial Science Achievement Award" given by the American Association for the Advancement of Science. (AAAS)

The award was made, in part, for *Bell Labs'* work with signals reflected from the passive satellite, Echo I; their work with an optical maser; their work with the first electronic telephone switching system; and other research and development projects.

**CHARLES A. VOLZ, JR.**, has been elected president of *Olympic Products*. He succeeds **JOSEPH B. SCHAEFER** who becomes chairman of the board of directors.

**RICHARD J. STONE** has been named supervisor of the Delay Line section of the *Corning Glass Works* research department.... **GEORGE E. SPAULDING, JR.**, has been elected to the newly created post of vice-president in charge of engineering operations, Photo Products Division of *Bell and Howell Company*.

*Hoffman Electronics Corporation* has named **DR. GEORGE WERTWIJN** as engineering head of its Evanston plant.

**ROBERT D. SCHMIDT** has been promoted to director of engineering by *Telemeter Magnetics Inc.*... **EVERETT TIBBETS** has been named general manager of *Exact Engineering and Manufacturing Inc.*... **JOHN P. HASTINGS** has joined the staff of *Cunoga Electronics Corporation* as manager, special projects.... **DR. JOHN C. R. KELLY, JR.** has been named director of the newly created centralized technical services of *Westinghouse* central laboratories.

**PALMER M. CRAIG** has been appointed director of operations of *Philco Corporation's* Western Development Labora-

tories.... *Texas Instruments* reports that **ROBERT C. DUNLAP, JR.** has been elected vice-president succeeding **FRED J. AGNICH** who has resigned.

**EMIDIO A. DeLOLLIS** has been appointed engineering manager of *Raytheon Com-*



*pany's* Receiving Tube Operations. Mr. DeLollis joined *Raytheon* as a design and development engineer in 1946, and has been assistant head of the receiving tube design department since 1957. He

will now direct design and specifications, product development, production engineering, and engineering services for the Operation.

During World War II, he was a major in the U. S. Marine Corps. He graduated from Clark University, received his M.A. from Boston University, and is a member of the American Physical Society.

Mr. DeLollis replaces Niles P. Gowell, who has been promoted to division engineering manager for *Raytheon's* Industrial Components Division.

**JOHN F. MORTEN** has been appointed to the new post of manager of marketing services for the *Weston Instruments Division* of *Daystrom*. He was formerly director of product planning for the division... *Motorola Semiconductor Products Inc.* has appointed **EDWARD C. MEHM** to the newly created post of distributor merchandising manager, eastern area. He will make his headquarters in Clifton, N.J.... **THOMAS P. CLEMENTS** has been promoted to the post of sales manager for the distributor division of *The Hickok Electrical Instrument Com-*

*pany*. He was formerly national service manager for the *Admiral Corporation* before joining the instrument firm in 1958... The Electronics Division of *Elgin National Watch Company* has named **E. C. SPEVAK** engineering manager and **DUANE C. MANNING** marketing manager. Both men will headquarter at the division's plant in Burbank, California.

**WALTER H. CHUDLEIGH, Jr.**, staff engineer for *General Atronics Corporation*, has been appointed a vice-president of the firm's subsidiary, *Atronic Products Inc.*



Prior to joining the firm in 1957, he taught at Rice, spent two years as a radar maintenance officer in the Navy, a year at guided missile research for the Naval Air Material Center at Johnsville, seven years at research for the *Philco Corporation*, and two years as a section manager with *Westinghouse*.

At *Philco* he did pioneer work in color television and traveling-wave tubes. He is co-inventor of a probability ratio-sequential detector for search radar and holds several other patents in addition.

**FROM GULFPORT  
MISSISSIPPI:**

"Color reception is amazing. For the first time we will really be able to sell color television."

**FROM GREAT BEND  
KANSAS:**

"I've tested and used about every fringe antenna. Your Powertron gives the sharpest reception I have ever seen here."

**FROM FARGO  
NORTH DAKOTA:**

"It's fantastic! We're getting several stations with Powertron we've never seen before."

# FIRST DEALER REPORTS ON THE WINEGARD POWERTRON

## World's First Electronic TV Antenna

The Powertron antenna has caused more letters to flow into Winegard's offices than any thing we have ever made. TV service-technicians who have tried one are amazed at the tremendous reception and advantages of this new antenna.

The Powertron is an all channel yagi antenna with a built-in high gain RF amplifier in one integral unit. It comes equipped with a power supply that lowers 117 V. AC to a safe 24 volts which is fed up the lead-in to the antenna. It is 5 to 9 times more powerful than any other antenna made.

With the Powertron, you can get your customers many channels they couldn't even see before. For example, in Burlington, Iowa, we easily pull in 9 channels where we used to pull in only 5 with a Color'Ceptor—our finest antenna before we developed the Powertron.

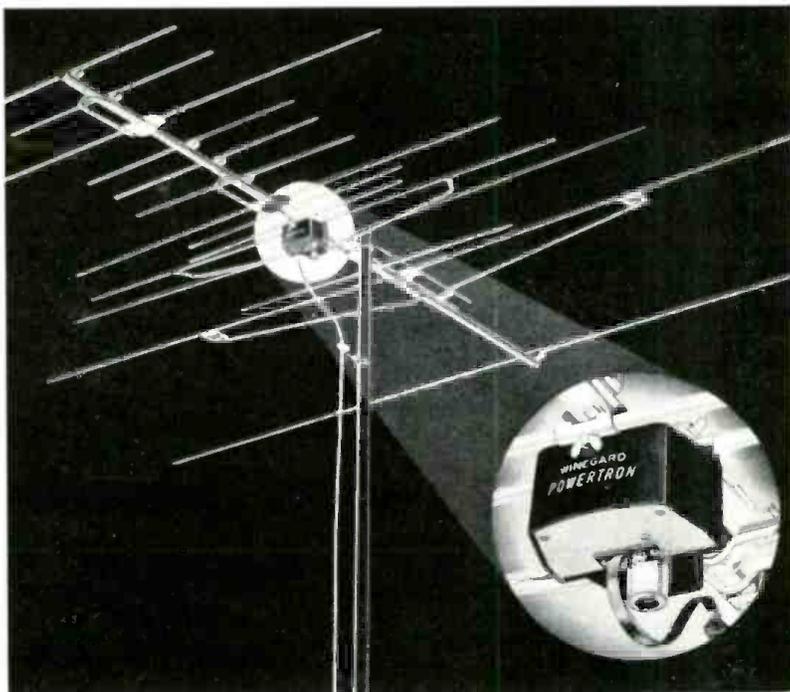
You can run 10 TV sets with a Powertron and all of them will have a better picture than you now get on one set with your present antenna.

You can make your installations 30 to 40% lower in height with a Powertron without affecting reception, in most cases.

You can remote the Powertron antenna 1/4 mile away from the TV set and get a better picture than with an ordinary antenna mounted next to the set.

You can deliver the clearest, sharpest, truest, color TV you've ever seen because the Powertron's extremely linear response makes it the *only* antenna that should be installed with a color receiver.

In short, this antenna is amazing. But don't take our word for it—test one and see for yourself. Ask your distributor or write today for *free* technical bulletin.



**Model P-44 Powertron** — \$74.95 list, 14 elements. 5 times more voltage gain than Color'Ceptor.



**Model P-44X Powertron with Pack** — \$91.90 list, 21 elements. Up to 54% more gain, higher front to back ratio than Model P-44.

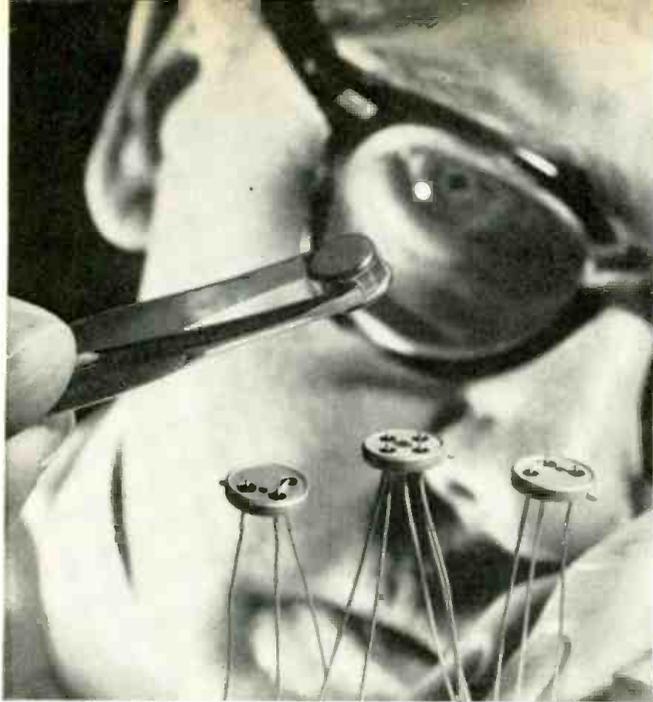


**Model SP-44X Super Powertron** — \$104.95 list, 30 elements. Twice the gain of Model P-44.



# Winegard

3003-4 Scotten Boulevard • Burlington, Iowa



### “Siamese-Twin” Transistor

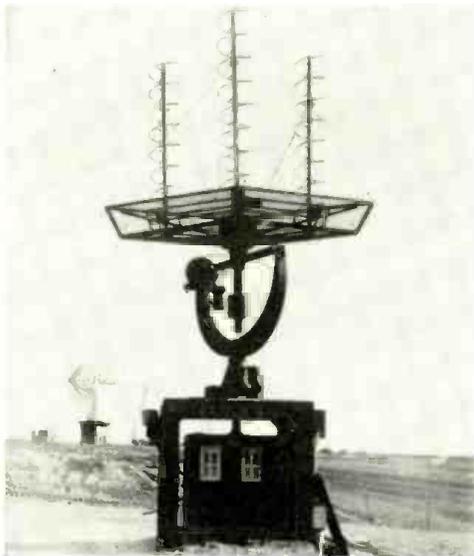
A valuable addition to *RCA's* line of transistors is a novel device dubbed the “Siamese-twin.” The design incorporates two identical transistors within a single housing. The transistors are two silicon types sharing a common collector. Initially, the unit will be offered as a d.c. chopper amplifier, a device that converts d.c. to a.c., so that it can be easily amplified or rectified to produce higher-voltage d.c. The selling price will be under \$25 per unit in lots of a thousand or more.

### Televised X-ray Pictures

X-ray studies are televised and recorded for repeated viewings with this new “Televex” x-ray system developed by the *Westinghouse Electric Corp.* Demonstrating the new system for the first time is Dr. Bertram R. Girdany, chief radiologist at Children’s Hospital of Pittsburgh, who proposed the system. At the right is the TV monitor where the x-ray image appears on the screen. Advantages of the system include improved visualization for the doctor, and reduced radiation exposure for the patient.



## Recent Developments in Electronics



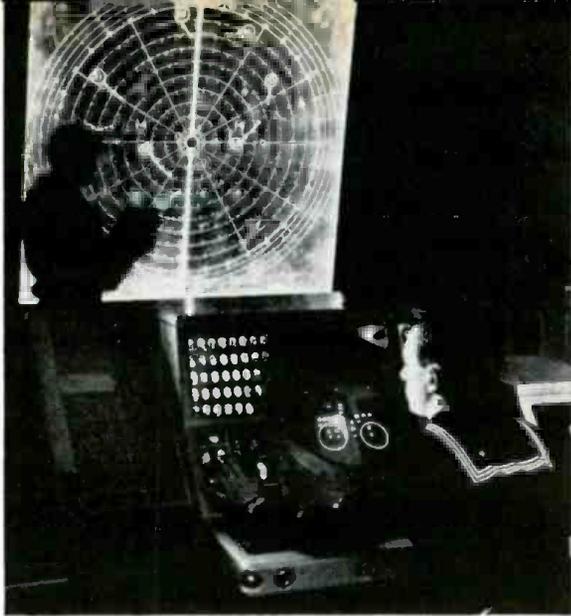
### “Discoverer” Tracking Antenna

This *Philco*-built tri-helix antenna array is used in the communications and control system of the “Discoverer” satellite program. The antenna receives v.h.f. doppler and telemetry information and permits simultaneous telemetry reception and doppler read-out to provide tracking data for the satellite.

### Computer-Designed Computer

*Bell Telephone Laboratories'* engineer is shown here checking out design information for the first computer built from complete information furnished by another computer. A subassembly of the computer is on the table. The computer will be used with the target-track radar for the Army’s “Nike-Zeus” anti-missile defense system.





### Data Displays for Missile Ships

Old, slow grease-pencil method of plotting aircraft seen in the upper portion of the photograph contrasts very sharply with the new U. S. Navy display console in the foreground. Developed by the *Hughes Aircraft Co.*, the console displays graphically all aspects of aerial, sea-surface, and submarine warfare for combatant ships within a fleet task force. Soon to be installed in Navy ships, the display system will eliminate human error and delays which often plagued the old system and will provide lightning-fast battle intelligence at a central point aboard each ship where prompt counter-action may be initiated.

### Jeep-mounted SSB Radio

The first production units of a highly mobile jeep-mounted single-sideband communication system, designed and manufactured by *Collins Radio Co.*, rolled into Camp Pendleton, Calif., ready for Marine Corps field use. The unit includes a 1-kw. transceiver, mounted in a water-tight encasement, with over 28,000 automatically tuned voice, c.w., and teletype-writer channels.



### Private Outer-Space Listening Post

Space communication scientists at *ITT Federal Laboratories* will use this 40-foot antenna to beam signals at outer space and to receive satellite signals. The company has received the first "earth-space" radio license granted by the FCC to a private concern, permitting experimental work in satellite and related space communications. One of the research goals is to collect data that will aid in development of a future world-wide satellite telephone-TV system.

### Quartz Crystals Grown Commercially

The world's first factory built to mass produce, synthetically, quartz crystals for communications purposes went into production on a commercial basis recently at the Merrimack Valley Works of the *Western Electric Co.* The step signified the emergence of the U. S. from dependence upon a foreign supply of quartz. A strategic material, quartz was in critically short supply during World War II. The entire crystal-growing process, which is done in closed vessels at a temperature of 700° F. and a pressure of 25,000 lbs./sq. in., is completely automatic. The operation requires 3-weeks' time, after which the crystals are withdrawn as shown in the photograph.



**50-WATT STEREO AMPLIFIER AND CONTROL CENTER**

Get the most from your stereo system with this superb unit; power-packed 50 watts (25 w. per channel); complete tone, balance and stereo /mono function controls; five dual-stereo inputs plus separate monophonic mag. phono; mixed-channel center speaker output; luggage-tan vinyl clad steel cover. 31 lbs.

Kit Model AA-100 ..... **\$84.95**  
 Assembled Model AAW-100..... **144.95**



**GET BIG STEREO SOUND AT LOWEST COST WITH THIS COMPLETE STEREO-PHONO CONSOLE . . . NOW IN ASSEMBLED OR KIT FORM FROM \$129.95 UP**

Modest only in size and price, this new Heathkit Stereo-Phono Console amazes every listener with its room-filling, true-to-life stereo sounds. Proportioned to fit any room, it's less than three feet long and only end-table height, yet it houses a complete stereo-phono system with features usually found only in much larger consoles. There's *six* speakers . . . two 12" woofers for smooth "lows," two 8" speakers and two 5" cone-type tweeters for "mid-range" and "highs". The 4-speed automatic stereo /mono record changer is equipped with an "anti-skate" device and a turn-over diamond and sapphire styli cartridge. On the front panel are separate, dual bass and treble controls plus a concentric volume control. The handsome cabinet with solid genuine walnut frame, walnut veneer front panel, and matching "wood-grained" sliding top measures just 31 3/4" L x 17 5/8" D x 26 3/4" H. Whether you buy the ready-to-play or kit form, the cabinet is factory assembled and finished. 70 lbs.

Kit Model GD-31 ..... **\$129.95**  
 Assembled Model GDW-31 ..... **149.95**

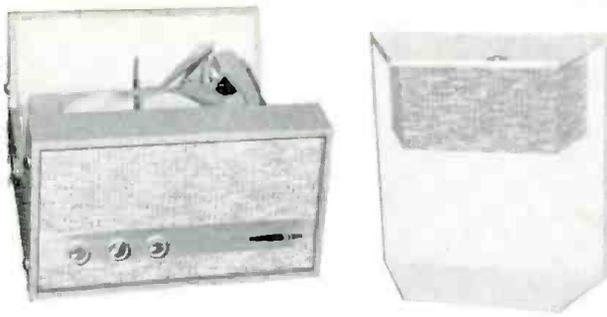
**COMPLETE 28-WATT AND 50-WATT STEREO CONSOLES**

Enjoy incomparable Heathkit stereo with factory wired components in beautiful preassembled, prefinished cabinets . . . ready to use! The consoles are available in both 28 and 50 watt models, with money-saving optional kit plans. The 28-watt model (HFS-26) contains the Heathkit AJ-10 stereo AM/FM tuner, SA-2 stereo amplifier, AD-50A stereo record changer and two US-3 12" coaxial hi-fi speakers. The 50-watt model (HFS-28) contains the Heathkit AJ-30 deluxe stereo AM/FM tuner; AA-100 deluxe stereo amplifier; AD-60B deluxe stereo record changer; and two Jensen H-223F coaxial 2-way 12" hi-fi speakers. Specify walnut or mahogany.

Assembled Model HFS-26 . . . 215 lbs. .... **\$475.00**  
 Kit Model HFS-27 . . . 215 lbs. .... **370.00**  
 Assembled Model HFS-28 . . . 264 lbs. .... **675.00**  
 Kit Model HFS-29 . . . 264 lbs. .... **550.00**

(Cabinets available separately, write for information)





**STEREO/MONO PORTABLE PHONOGRAPH**

Now you can thrill to magnificent stereo wherever you are, wherever you go! The smartly-styled cabinet with two-tone aqua and white durable vinyl covering comes completely preassembled. In closed carrying position the speaker wing and main cabinet blend into a single handsome unit in dazzling aqua and white vinyl. In use, the detachable speaker-wing top may be spaced at any distance for maximum stereo effect. The completely preassembled automatic changer plays your favorite stereo and mono records at speeds of 16, 33 $\frac{1}{3}$ , 45 and 78 rpm, while controls on the amplifier section give you complete command of volume, stereo-balance and tonal quality. 28 lbs.

Kit Model GD-10..... **\$69.95**

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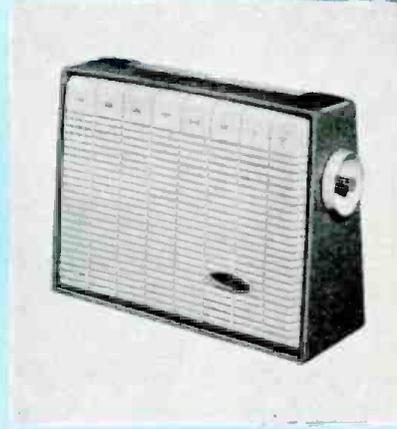
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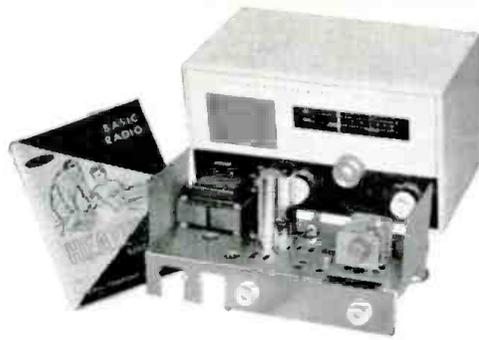
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# Sound on Tape

By BERT WHYTE

EDITOR'S NOTE: Our reviewer has been intimately connected with the recording industry for many years. Therefore, the opinions expressed below are mainly from the viewpoint of the quality record producer who has the critical listener and hi-fi purist in mind. From that point of view, we cannot argue with the following statements. On the other hand, reverberation units may fill a definite need for experimenters, for those doing home recording, for owners of old 78-rpm records, or for audiophiles interested in showmanship and dramatic (although perhaps artificially so) effects. For a statement of our position on this subject, see the editorial "Reverberation or Not" in our November, 1960 issue.

The world of audio can be a maddening and frustrating place to inhabit. In recent years, it has seemed to be compounded of one crisis after another. A new development supersedes the "revolutionary" one of the previous week. Fortunately, today's audiophile is somewhat more sophisticated than his predecessor and thus a reasonable degree of stability has been attained.

Nowadays, most new items are subjected to thorough scrutiny and a healthy skepticism is the prevailing attitude until a product has been thoroughly proven in the field. One can only hope that such mature evaluation will be accorded the latest "gimmick" that has been foisted on the audiophile. . . . I refer, of course, to the various instruments that manipulate reverberation. They have all been given catchy trade-names but no matter what they are called, speaking from the standpoint of one who has made hundreds of stereo recordings, they are the sort of thing that makes my hair turn gray!

Most conscientious recordists spend a great deal of time looking for halls and auditoriums which have an optimum reverberation period for various types of music. Thus, if the music of Tchaikovsky or one of the other Romantics is to be recorded, one seeks a hall with the capacity for fairly lush acoustics and longer reverb periods. On the other hand, the sharper "dry" orchestration of a Stravinsky or other Modernist calls for a hall with either shorter reverb periods or one in which the reverb can be controlled to produce a "tighter" and more detailed recording. Obviously, such halls are not easy to find and thus compromises must be made in the reverb content, usually by altering the orchestral positioning or the microphone placement, or by a combination of the two. In any case, this kindling of reverb is a very painstaking and difficult job in which a recordist must utilize all the knowledge and experience he possesses.

The top engineers are also aware of

the many variables that can affect their auditory perception of the degree of reverb content. Chief among these is the acoustics of the room in which the recording is monitored. More often than not, these rooms are haphazard affairs—either much too small or too large, with atrocious acoustics which must be corrected with either damping or reflective material—as the case may be. Needless to say, the type of speaker used in monitoring has a bearing on the character of the recorded sound. I might add here that there are very few recordists who have extensive stereo recording experience (two to three years of stereo hardly equals 15 to 20 years of mono recording) but most are rapidly learning to cope with the specialized requirements of stereo and to treat with respect the tricky handling of reverb.

So what happens? The manufacturers of stereo "packages" and consoles, looking for some gimmick to apply to sales and merchandising, have really outdone themselves by putting at the disposal of Joe Doakes a new control with which Joe can change the reverb characteristics of the stereo discs in his library. It is also claimed to alter the acoustics of the room in which Joe is listening!

Here we spend thousands of dollars making recordings, utilizing the best engineering talent that knows how to handle reverb and now we have what may be a totally untrained listener twiddling his new control and turning his stereo recording into a caricature of the original!

Several component manufacturers have produced reverb units for integration into a components system. There is more engineering caution in evidence with these units and undoubtedly the audio experimentalists are having a ball with them. That is where these units, for the most part, should remain . . . with the experimenters. About the only really valid excuse for using these units is when a person owns a number of old 78-rpm records which have the utterly dry, non-resonant characteristics (such as the Toscanini-Studio 8H discs) quite barren of any reverb. Used intelligently and with discretion, these old recordings can be made to exhibit some improvement. It is extremely doubtful, however, that there are many people who own stereo systems and who also have many of these old 78-rpm records.

Thus to an already confused public, just beginning to acquire a faint understanding of stereo, a new toy is given.

Needless to say, this new confusion can hardly be expected to have a salutary effect on record sales.

For the amateur tape recordist and those who buy recorded tapes, the reverb units will have the least effect. Tape users are, as a rule, more sophisticated than their record-playing brethren and tape playback units are usually found only in the higher-priced, lower-volume stereo consoles. Few of these units are likely to be equipped with reverb controls. The amateur recordist can make the only other valid use of the component-type reverb unit. He is often restricted to a given recording location and must accept the acoustics as they exist. With proper use of a reverb unit, he can overcome the usual compressed, "dry" sound and add considerable "liveness and presence" to his recordings.

To summarize, one can only hope that, like most gimmicks, the "reverbs" are just a passing fad and that their passing shall be swift and unmourned.

**GERSHWIN**  
**RHAPSODY IN BLUE**  
**CUBAN OVERTURE**

Eugene List, pianist, with Eastman Rochester Orchestra conducted by Howard Hanson. Mercury 4-track Stereo STA90138. Price \$5.95.

It was nice to receive this tape from Mercury, who for some reason has been very slow in releasing its vast backlog of stereo recordings in the 4-track format. At least, this is true of the classical recordings. If you will recall, back in the old two-channel days, Mercury was one of the most prolific suppliers of stereo tape, and it is to be hoped that the tempo of releases will increase in this new medium.

Of the many "Rhapsodies" now available on tape, this is to me the most satisfactory. The sound is very clear and crisp, recorded with great forward projection and possessing all the stereo virtues. Directionality is easily perceived and the ghost image piano stays put in the middle. The dynamic range is unrestricted and allows for great climaxes which are never distorted.

Add to this the fine performance of List. His tempi are faster than most, to be sure, but he gives the work an electric excitement that lifts it above the efforts of most of his contemporaries. His technique is not faultless, but this can be accepted for the rich expressiveness of his playing.

Dr. Hanson is a conductor well grounded in the American jazz idiom and his accompaniment is exemplary on all counts. The tape is filled out with the gay and spritely "Cuban Overture," a sonic memento of happier times and happier relations with Cuba.

**HAYDN**  
**CLOCK SYMPHONY, No. 101**  
**SURPRISE SYMPHONY, No. 94**  
 Vienna Symphony Orchestra conducted by Pierre Monteux. Victor FTC2030. Price \$8.95.

While Papa Monteux is more generally associated with Ravel and Berlioz



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and Stravinsky and the Ballet, it should come as no surprise to find that he is equally at home in the classic tracteries of Papa Haydn. After all, in 86 years, you can learn to conduct almost any kind of music!

There is nothing really sensational in the music and Monteux conducts the works in equally straightforward manner, hewing to the score and imposing no "interpretation" on the music.

As to sound, here is a case where I am positive we are dealing with a two-channel master. This, even though I don't think this tape is so old, but is two-channeled merely because there just didn't happen to be a three-channel machine available in Vienna at the time of the recording. Otherwise the sound is good with an exceptional pick-up on the first and second strings. Stereo is necessarily "left and right" but isn't objectionable. The wind pick-up was not the best and the strings often smother them. The tympani sound is also a bit muddy as a result of slightly too much reverb. But I am splitting hairs and the tape really sounds acceptable and has the virtue of having very little crosstalk.

### KHACHATURIAN MASQUERADE SUITE KABALEVSKY THE COMEDIANS

RCA Victor Symphony Orchestra conducted by Kiril Kondrashin. Victor FTC2028. Price \$8.95.

Mr. Kondrashin gained fame in this country as the conductor who accompanied Van Cliburn in his time of victory. While he was here for a repeat of the Van Cliburn Moscow concert, *Victor* hied him to a studio to record this tape.

There is nothing world shaking here, but the works are obviously in his milieu and his performances of them outstanding. Oddly enough, although this was a spur-of-the-moment type of recording, we are treated to one of the finest recordings *Victor* has done. The stereo effects are all one could want in the way of directionality and perception of depth, the ghost central image is rock-steady. Dynamic and frequency range is very wide and the over-all sound is crisp clean and bright.

This had the lowest tape hiss I've heard in ages and crosstalk was, for all practical purposes, absent. Perfection would have been achieved had there been a little better projection of brass and woodwind, but as it stands, one of the best tapes in the 4-track format.

### OFFENBACH GAITE PARISIENNE KHACHATURIAN GAYNE BALLETS SUITE

Boston Pops Orchestra conducted by Arthur Fiedler. Victor FTC2045. Price \$8.95.

After abandoning its ill-starred tape cartridge, *Victor* went to the 4-track reel-to-reel medium and although, at first, the releases were very slow, now they are beginning to flow in something like the abundance that made *Victor* the leader in the two-channel days.

One word of caution is in order how-

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Model GP-1  
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ever. Some of the more successful two-channel tapes are being reprocessed and made available on 4-track. Nothing wrong with this, except that certain of the old tapes were made quite a way back . . . before *Victor* started using 3-channel/half-inch masters. Thus you have a two-channel tape with no ghost central image, so don't go crazy trying to create that which isn't there!

This "Gaité Parisienne" is a good recording and while I believe it is a three-channel original, the ghost central image is down in level and rather hard to perceive and keep focussed. This is generally clean and the score being what it is, is full of sonic fireworks. Plenty of

cymbal clashes and heavy bass drum shots, along with bright boisterous brass and sizzling strings. The "Gayne" ballet is much in the same character.

Performances by the redoubtable Fiedler are among the best, and his tempestuous, headlong pace, kindles lots of sonic sparks. My quibble with this recording is an odd one . . . I feel as though a compressor may have been used in some of the climaxes and there is the feeling that too great a volume of sound is being contained in too small a space. There is a lot of reverb but there is so much sound it seems to fill up and spill, thus unfortunately blunting the climaxes. -30-

## SIMPLE CRYSTAL MIXER

By JENNINGS DAVID

**Build this circuit for use in making measurements and adjustments on r.f. circuits. Can also be employed to check the activity and frequency of quartz transmitting crystals.**

**T**HIS MIXER has proven handy when making measurements and adjustments on high-frequency circuits. It is useful, in conjunction with an external signal generator, in determining the frequency of an oscillator or transmitter or the frequency and activity of quartz crystals. It has been used over a frequency range from less than 100 kc. to above 200 mc.

Fig. 1 is the diagram of the simple mixer that can be built from parts to be found in almost every "junk box." The crystal used by the author was a 1N64, however any one of the popular types, such as the 1N34, may be used with equal success. The 5- $\mu$ f. coupling capacitors may be three or four turns of insulated hookup wire tightly wound around the connection to the hot end of the r.f. choke. The layout of the components is not critical.

To use the mixer in conjunction with a signal generator for determining the frequency of an oscillator or transmitter, couple the signal generator to the mixer at point "A" and the oscillator at point "B". The ground lead of the signal generator and oscillator should be connected to point "G". With a pair of earphones inserted in the phone jack, tune the signal generator until a beat note is heard. Adjust the signal generator until zero-beat is obtained; this frequency will, of course, be the frequency of the oscillator or transmitter provided the approximate frequency of the oscillator is known. If the approximate frequency is not known, proceed as follows:

1. Record the frequency of the signal generator at which the first beat note is obtained. This frequency will be  $F_1$ .

2. Carefully increase the frequency of the signal generator until the next beat note is heard. Be sure not to miss the next higher frequency beat note. Record this frequency as  $F_2$ .

3. The frequency of the oscillator or

transmitter can be determined from the following formula:  $F_x = F_1 \times F_2 / F_1 - F_2$ .

When measuring the frequency of a transmitter it will probably only be necessary to couple the transmitter to point "B" by means of a short antenna. If excessive power is coupled into the crystal circuit, the crystal will probably be burned out.

To determine the activity or frequency of quartz crystals or to use crystals to spot-check the accuracy of signal generators, connect the crystal in series with the signal generator and point "A" and connect a 50- $\mu$ a. meter in place of the phones (Fig. 2). As the signal generator is tuned through the crystal frequency there will be a very sharp rise in the current through the meter.

Many other uses for this inexpensive instrument will undoubtedly occur to the experimenter as he becomes familiar with the circuit. -30-

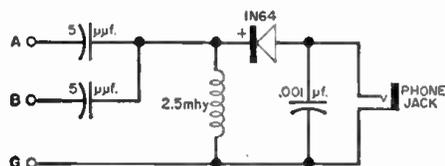
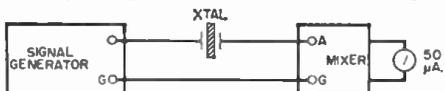


Fig. 1. Circuit diagram of the crystal mixer. Any of the popular general-purpose crystals, such as the 1N34, may be used in place of the crystal shown. The 5- $\mu$ f. capacitors are actually three or four turns of insulated hookup wire tightly wound around the connection to the r.f. choke.

Fig. 2. Circuit arrangement used to check activity or frequency of quartz crystals. As the signal generator is tuned through the crystal frequency, there will be a very sharp rise in the meter reading.



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						12
						19
						26

**CALENDAR of EVENTS**

**MARCH 20-23**

1961 IRE International Convention. Waldorf-Astoria Hotel and New York Coliseum. Details from IRE Headquarters, 1 E. 79th St., New York 21.

**MARCH 27-31**

1961 Symposium on Temperature. Sponsored by American Institute of Physics, Instrument Society of America, and National Bureau of Standards. Columbus, Ohio. Program information available from V. W. Sikorn, ISA, 313 Sixth Ave., Pittsburgh 22, Pa.

**APRIL 4-6**

Symposium on Electromagnetics and Fluid Dynamics of Gaseous Plasma. Sponsored by Polytechnic Institute of Brooklyn, IRE, Institute of Aeronautical Sciences, and U.S. Defense Agencies. Engineering Societies Bldg., 33 W. 39th Street, New York City. Details from PIB, 55 Johnson St., Brooklyn, N.Y.

**APRIL 4-7**

Spring Convention and Exhibit. Sponsored by the Audio Engineering Society. Ambassador Hotel, Los Angeles. Details from AES, P.O. Box 12, Old Chelsea Station, New York 11, N.Y.

**APRIL 4-9**

1961 Los Angeles High Fidelity Music Show. Sponsored by the Institute of High Fidelity Manufacturers. Ambassador Hotel, Los Angeles. Details from IHFM, 125 E. 23rd St., New York 10.

**APRIL 5-7**

Symposium on Materials and Electron Device Processing. Sponsored by American Society for Testing Materials. Benjamin Franklin Hotel, Philadelphia, Pa. Information from ASTM, 1916 Race St., Philadelphia 3, Pa.

**APRIL 12-13**

Third Symposium on Information and Decision Processes. Sponsored by IRE-PGIT and Purdue University. Purdue campus, Lafayette, Ind. Dr. Robert E. Machol, School of Electrical Engineering, Purdue University, Lafayette, Ind. for complete details.

15th Annual Spring Technical Conference. Sponsored by Cincinnati Section of IRE and Southern Ohio Section of American Rocket Society. Hotel Alms, Cincinnati. Technical papers and exhibits. Information from R. P. Schlemmer, c/o Engineering Specialties, 8115 Camargo Road, Madeira, Cincinnati 43.

**APRIL 19-21**

SWIRECO. Sponsored by the S.W. (Region 6) Section of IRE. Dallas Memorial Auditorium and Baker Hotel, Dallas, Texas. Program information available from Dr. L. D. Strom, Texas Instruments, 6000 Lemmon Ave., Dallas, Texas.

**APRIL 26-28**

Seventh Region Technical Conference and Trade Show. Sponsored by Region 7 of the IRE. Westward Ho Hotel, Phoenix, Ariz. Program information from H. W. Welch, Jr., Motorola Inc., P.O. Box 1417, Scottsdale, Arizona.

**APRIL 29**

Tenth Annual Dayton Hamvention. Sponsored by Dayton Amateur Radio Association, Inc. Dayton Biltmore Hotel, Dayton, Ohio. Varied program of events has been scheduled. Contact Harry E. Covault, K8GCS, 4820 Archmore Drive, Kettering 40, Ohio for details.

**MAY 2-4**

Electronic Components Conference. Sponsored by PGCP, AIEE, EIA, WEMA. Jack Tar Hotel, San Francisco, Calif. Details from Daniel Breeding, Fairchild Semiconductors Inc., Palo Alto, Calif.

**MAY 4-5**

Second National Symposium on Human Factors in Electronics. Sponsored by PGHFE of IRE. Marriott Twin Bridges Motor Hotel, Arlington, Va. Details from R. R. Riesz, Bell Telephone Labs, 2D-452, Box 262, Murray Hill, New Jersey.

**MAY 6**

Workshop in Graph Theory. Sponsored by PGCT of IRE. University of Illinois, Urbana, Illinois. Prof. M. E. Van Valkenburg, Department of Electrical Engineering, University of Illinois, Urbana, Ill. for program information.

**MAY 8-9**

Fifth Midwest Symposium on Circuit Theory. Sponsored by PGCT of IRE. Allerton Park & Urbana Campus, University of Illinois. Prof. M. E. Van Valkenburg, Department of Electrical Engineering, University of Illinois, Urbana, Ill. for program information.

**MAY 8-10**

Thirteenth Annual National Aerospace Electronics Conference. Sponsored by the IRE. Biltmore & Miami Hotels, Dayton, Ohio. Program details from Ronald G. Stimmel, 809 Larriwood Ave., Dayton 29, Ohio.

**MAY 9-11**

Western Joint Computer Conference. Sponsored by PGEC, AIEE, and ACM. Ambassador Hotel, Los Angeles, Calif. Prof. Cornelius Leondes, Department of Electrical Engineering, UCLA, 405 Hilgard Ave., Los Angeles 24 for program details.

**MAY 15-17**

1961 National Symposium on Microwave Theory & Techniques. Sponsored by PGMTT of IRE. Sheraton Park Hotel, Washington, D.C. Information on program from Gustave Shapiro, NBS, Washington, D.C.

**MAY 22-24**

1961 Electronic Parts Distributor Show. Conrad Hilton Hotel, Chicago. Closed Show. Hours 9 a.m.-6 p.m. Details from Electronic Industry Show Corporation, Suite 1501, 11 S. LaSalle St., Chicago 3, Illinois.

National Symposium on Global Communications. Sponsored by the AIEE and IRE. Sherman Hotel, Chicago. Details from Donald G. Campbell, ITT Kellogg, 5959 S. Harlem Ave., Chicago, Ill.

National Telemetering Conference. Sponsored by PGSET, AIEE, IAS, ARS, ISA. Sheraton Towers Hotel, Chicago. Jack Becker, AC Spark Plug Div., General Motors, Milwaukee, Wisc. for program information.

## Home-Call TV Diagnosis

(Continued from page 35)

with a low-impedance device. To avoid loading, a 100,000-ohm isolating resistor should be connected to the test probe of the voltmeter, but in a typical v.o.m. this will reduce the measured voltage. In many stages of the TV receiver, grid bias confirms the presence of a signal from the preceding stage. If a grid bias of  $-40$  volts appears at the horizontal-output tube, we know that the horizontal oscillator is working. Similarly, if a.g.c. bias is measured at about  $-3$  volts, this is a good indication that a signal is amplified and passed at least to the a.g.c. section.

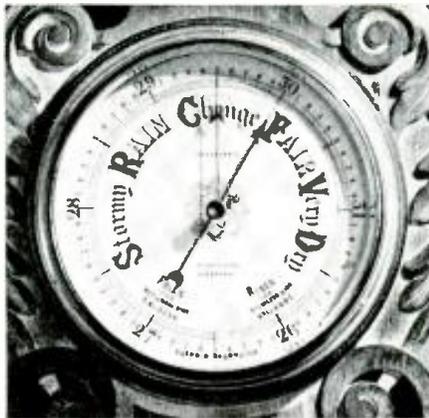
**D. Estimating Repairs.** The three logical steps for determining the symptoms, analyzing what can cause them, and troubleshooting further will usually result in the accurate location of the defective part. Often the technician will realize somewhere along the way that the service job is more complex than can be handled within the half-hour time limit well before that limit is reached. Only rarely will the entire half hour be consumed without producing at least a very strong indication of what the defect is.

If it is decided that the repair can be made at once or if a defect has been cleared up in the course of the 30 minutes allotted, there will be no problem in determining price. Most technicians will compute the bill by using their regular labor charge plus the list price of the defective part.

When the repair involves replacement of a component which the technician does not have at hand or when the exact defect is not known after the 30 minute troubleshooting period it becomes more difficult to determine the price. Many technicians will give an estimate at this point which includes the fee for a house call, one half-hour of troubleshooting time, one half-hour of alignment and adjustment time, and the list price of the most expensive component in the suspected trouble area. The picture tube is usually excluded from this type of estimate because it is almost always possible to determine quickly if it is defective. Experience shows that, after the recommended 30-minute procedure, very few cases will be real "tough dogs," so that by following this pricing policy the technician is bound to average a legitimate profit and the majority of his customers will have no reason to complain of overcharges.

The method outlined eliminates a lot of the uncertainty and guesswork which plague the TV technician making house calls. While some assumptions and simplifications made here do not always hold true, a technician following this method is bound to be more efficient than if a haphazard approach is taken. Experienced operators will be able to add many refinements to the method and will know how to modify it to suit local conditions and particular circumstances.

-36-



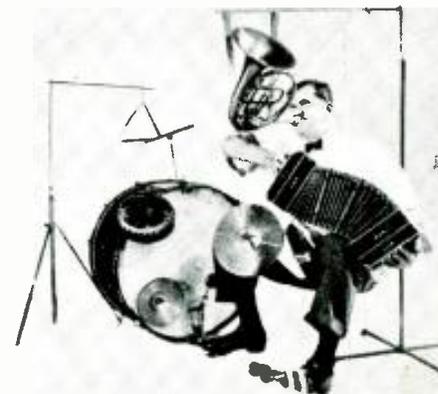
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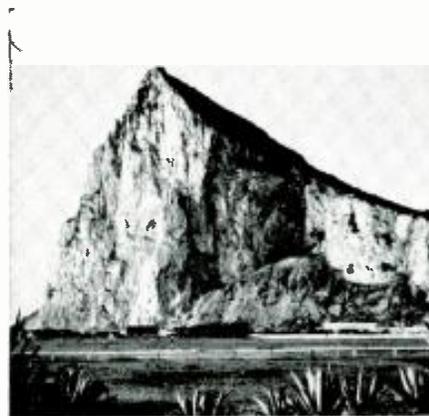
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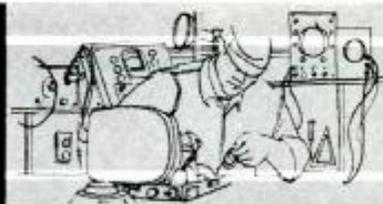
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# SERVICE INDUSTRY



# NEWS

THOSE OF US who look for meaningful patterns in the industry sometimes become a shade too eager to build large conclusions on small clues. Let us hope that is the case with an item from that respected service group, the Radio TV Guild of Long Island, N.Y.

A front-page story in our latest copy of "Guild News," captioned "Help Wanted," pleads for members to fill key executive positions so that the association may continue its record of accomplishment. They are needed, not to undertake new tasks, but to fill the gaps left by the loss of effective executives over the past couple of years. The Guild has lost at least five good men. Why? These people have gone on to greener fields.

Most of them are still in some aspect of electronics. One, for example, is a design engineer with a leading hi-fi manufacturer. We know of other cases where former shop owners have gone into manufacturing plants, or taken jobs with distributors. In still another case, a shop owner who has had the same business for 14 years is giving up although he does not have a definite, alternate job.

As compared to their fellows, each of these would be reckoned a successful dealer. Then why the defections? Some of these people did not take the initiative themselves: they were offered opportunities for improvement that they simply could not refuse. The fact is that these men had reached an end point as service dealers, even successful ones, at which full use of their capabilities was not being made and beyond which they could not go to better themselves. They now have better financial reward and more prestige.

Government statistics shed additional light on this situation. The average factory worker in the electronics industry gets about twice as much per hour as a man in a service shop. This does not mean that the individual who does wiring and routine assembly work on a TV chassis always gets paid more than the skilled analyst who later chases the tough dogs out of the equipment, but there is an obvious inequity here.

Good men are needed to render good service. They must be paid accordingly. If the industry cannot do something to improve its own condition, the entire field may eventually be yielded to the screwdriver mechanics by default. Recognition of the fact that cheap service cannot be good service must come, if this is to be prevented. Manufacturers and users of home electronic equip-

ment have as much at stake here as the service industry.

But perhaps things are not that bad. We know another officer of the same Guild that has been hit by a loss of leadership who was recently offered another position. He turned it down. He may just be a mule, he says, but he refuses to surrender the hope that his chosen field can be brought to the stature it deserves.

## What Service Thinks

The "Raster," official publication of the Electronic Service Council of the Ozarks, is going right to the source to find out what service people think. On the matter of the effect of electronic equipment imported from Japan, for example, this monthly draws interesting comment from two technicians. E. D. Muhleman, the first, says, "I have been puzzled to figure out what replacement parts I can get. Delay in the delivery of the repair job to the customer results, or I turn down the job with, 'Sorry sir, I just can't help you out on it now.'

"What to do about it? Well, what can we do about it? In time some of our American producers will make replacement parts available to us or else the importers will. Another possibility—by the time the customer has gone to several shops for service and gets the same answer, he will swear never to buy another Japanese-made item. My answer to the problem? Fix the ones that come in that we can fix and let time work out the answer."

Another respondent, W. A. Pryor, does not believe that importation will be permitted to continue to the point where it would seriously hurt domestic economy. He points out that such imports are under a Japanese export control program, and concludes with: "I would say that this is not a problem of the service technician. We have our own problems—let the manufacturer take care of his."

The "Raster" also queried readers on what they thought of printed circuits and whether their opinions had changed for the better since the printed boards were first encountered. James Rathbun realistically supposes that "we are going to have to live with printed-circuit boards inasmuch as most manufacturers are using them. My opinion of them has not changed much." He acknowledges improvements in the later boards (increased strength, better marking, easier parts location) and concedes that his continuing prejudice may partly be

due to the fact that most of his service experience is with older sets, therefore older boards. However, he feels that certain inherent problems in parts mounting and parts replacement continue—"like having to replace tube sockets after a tube had been pulled out two or three times and not being able to replace a part until I had removed a section of the printed board."

#### TV Promotion of TV Service

Broadcasters are becoming increasingly cooperative in advancing the cause of service. William Finnerty, president of the San Francisco Television Service Association, was interviewed by Ira Blue, Bay Area sportscaster, just before the Army-Navy football game this fall on KGO-TV, channel 7. In response to questions, Finnerty explained the correct adjustment of customer controls on the TV set for optimum viewing.

"We programmed this public-service interview," said the general manager of KGO-TV. "in the hope that those who have been dissatisfied with their TV picture will avail themselves of this opportunity to correctly adjust their sets. We have found that most complaints about 'transmitter trouble' stem, instead, from inaccurately adjusted receiving sets." The program ended with a full-screen display of the association's emblem.

Providing less instantaneous impact but more long-term effectiveness is the campaign in Indianapolis. Recognizing that good service is essential to maintain the largest possible viewing audience, WFBM-TV (channel 6) of that city is running daily spots showing the emblem of the Indiana Electronic Service Association, according to the organization's "Hoosier Test Probe," and explaining what IESA stands for. In return for this boost, members pass out literature supplied by the station on service calls, display bumper stickers, make sure that channel-6 reception is optimized on every job, and promptly report any reception problems to the broadcaster.

#### Advanced Radio Service

"More than 10 million radios were purchased by the American public in 1960," says George C. Isham, manager of marketing services for Sylvania's Electronic Tube Division, "and in 1961, the total should be just as high." The obvious conclusion, for service dealers, is that they are missing good business opportunities if they are neglecting the expanding number of such receivers in current use.

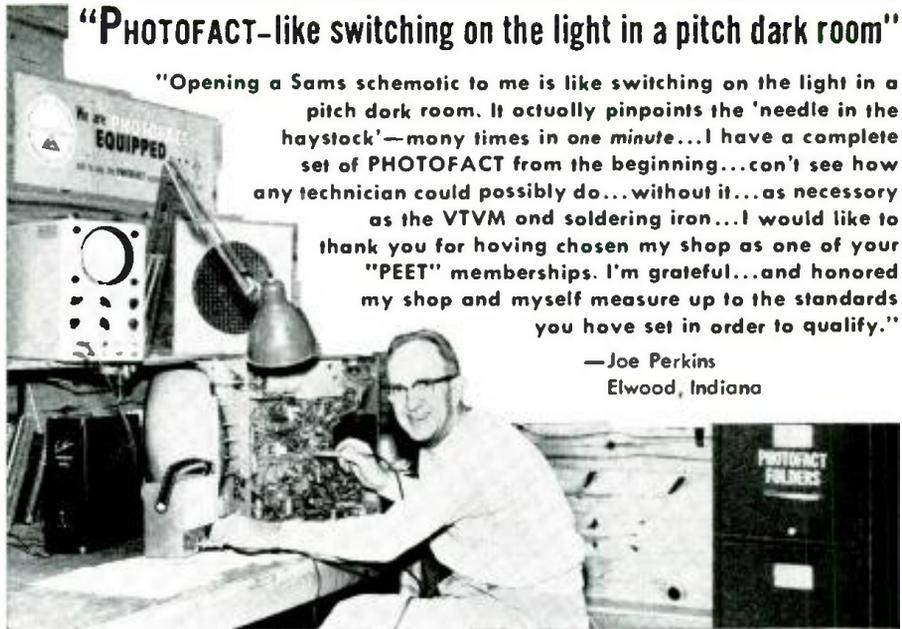
With this in mind, Sylvania offers "Advanced Techniques of Radio Servicing," a 12-lesson correspondence course, through authorized distributors. Does this course sound superfluous? Not if you consider what "radio" means today. Coverage includes AM-FM, transistorized, short-wave, auto, and foreign-made receivers, marine-radio gear, and other types. There's much here never dreamed of in the simple, table radio.

-30-

## "PHOTOFACT-like switching on the light in a pitch dark room"

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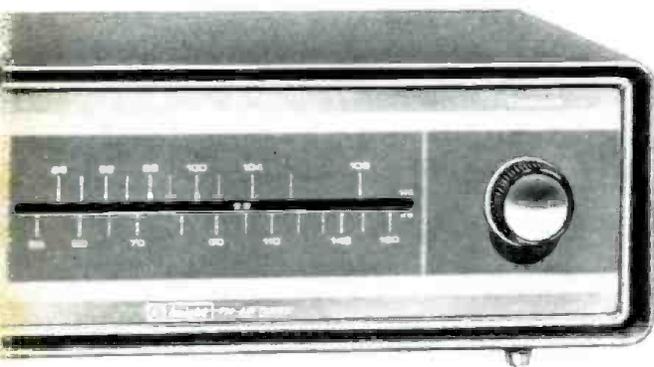
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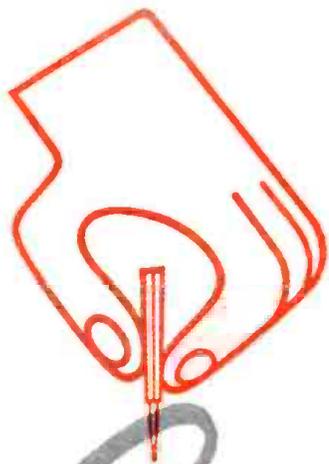
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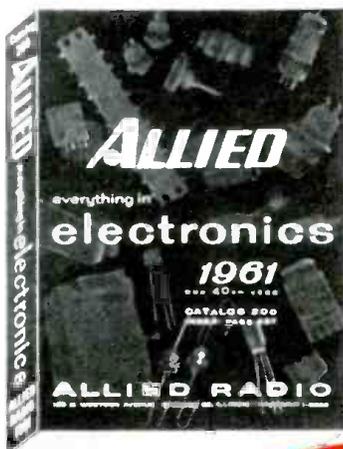
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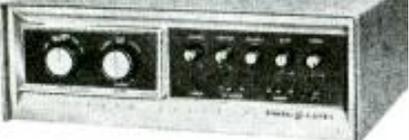
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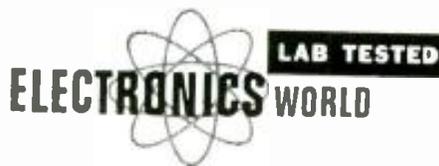
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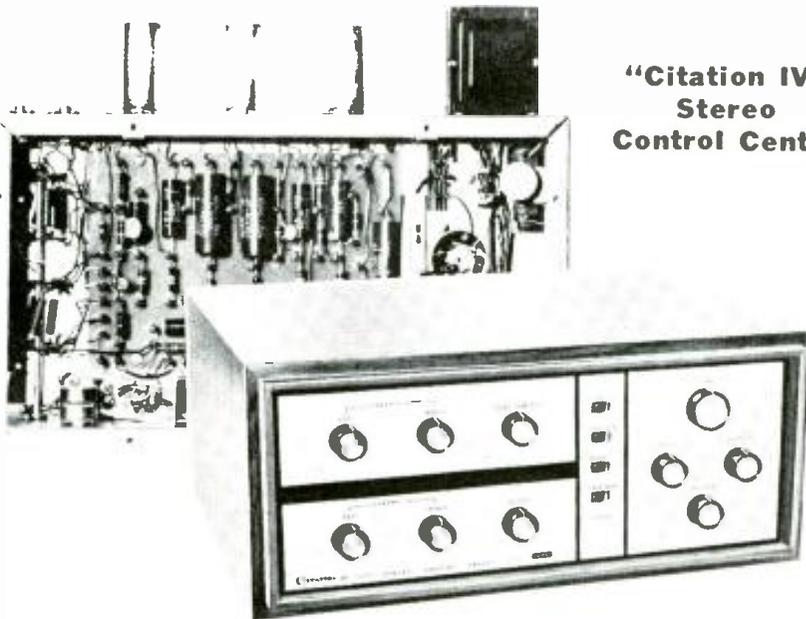
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# Product Test Report



**"Citation IV" Stereo Control Center Channel Master CM-10 Speaker System Pickering Model 381A Stereo Cartridge Eico Model 723 Amateur Transmitter Kit**



**"Citation IV" Stereo Control Center**

WE HAVE just completed assembling and testing *Harman-Kardon's* "Citation IV" stereo preamplifier and control center. Although the controls and input and output facilities are not unusual or different from many other preamplifiers on the market today, the performance of this unit comes pretty close to the ideal. There are only a few competitive designs that can match its low distortion and certainly none that we know of that can surpass it in this regard. Its mechanical and electrical design leaves no doubt in our mind that many, many hours of continuous operation should be obtained without maintenance problems. This is the first time that this reviewer has built a kit that employs military-type terminal boards. Such construction is much more rigid and professional appearing than is the case with many of the printed-circuit assemblies now in use. In addition, one has greater assurance that the soldering connections will be properly made.

The "Citation IV" is a stereo preamplifier employing six 12AX7/ECC83 tubes plus two selenium-rectifier assemblies. The front panel controls are quite conventional and include volume, balance, blend, and bass and treble controls for each channel. Slide switches are included for high- and low-frequency filters along with separate switches for contour (loudness) and tape monitor. A mode switch is incorporated to permit selection of straight stereo or reverse stereo, both A and B channels through

both speakers, mono channel A through both speakers, and mono B through both speakers. The function switch provides selection of six different inputs: auxiliary, tape, tuner, phono RIAA, phono LP, and tape head. A somewhat unusual, yet convenient, switch is incorporated that disconnects both bass and treble tone-control circuits completely in order to eliminate any distortion that these circuits might generate. This switch must be "on" when using either the scratch or rumble filters. A continuously variable "blend" control is also provided to obtain center "fill" as required. The control can be switched out of the circuit completely when not needed.

To those particularly interested in tape, this preamplifier's design is such that stereo tape can be played back using its equalizing circuits for the tape head. Any program material can be switched to the tape recorder to record a stereo tape. Also a tape-monitor switch permits monitoring of tape while recording.

With regard to the actual performance of this preamplifier, we found the frequency response to be within  $\pm .1$  db from 20 to 20,000 cps. The contour, bass, and treble controls were found to be extremely effective.

A very sharp cut-off rumble filter is incorporated. Our tests showed that at 100 cps, the response was only down .2 db, while at 20 cps it was -17.8 db. The scratch filter proved to have a more

gradual cut-off. Starting at 400 cps, the roll-off action was gradual, and it extended to -29 db at 20,000 cps. The RIAA magnetic phono equalizing circuit was found to be within  $\pm 1.3$  db from the standard. This represents so slight a deviation as to be not discernible when listening.

The sensitivity is much better than is required, being .186 v. for 1-v. output for all high-level inputs. For magnetic phono input, the sensitivity was 3.15 mv., for tape head 2.68 mv., and for ceramic phono input .1 v.; all for 1-v. output.

Our harmonic-distortion measurements were taken under two different conditions; first, at 1-v. output with a 1-v. input signal, and then at 2-v. output with a .5-v. input signal. This measurement was taken through a high-level input. We believe that any preamplifier should be capable of producing at least 2 volts output without excessive distortion. Our harmonic-distortion figures proved to be so low that one can almost claim distortion-free performance from this preamplifier. The actual figures, with 1-v. output, were .05% at 20 cps, .07% at 1000 cps, and .01% at 20,000 cps. There was no marked change in these figures at an output of 2 volts. Incidentally, we have subtracted the residual distortion of our test equipment in order to arrive at these figures. This may or may not be valid depending on the nature of the residual distortion.

The intermodulation distortion, taken at 60 and 6000 cps through the high-level circuit, proved to be only .009% (after having deducted the residual distortion in our test equipment) with the volume control adjusted to produce 2 volts output with a signal input of .5 volt.

In order to obtain some comparison between various preamplifiers when testing for noise and hum, we adjust the volume control to produce 1 volt output with an input signal of .006 volt into the magnetic input jack. At this volume-control setting, we found that for all high-level inputs, the hum and noise were down 71 db from a 1-v. output level. The magnetic tape head circuit showed hum and noise of -48 db, and the magnetic phono input circuit showed hum and noise of -60 db under the same conditions.

The channel separation, at 1000 cps, proved to be 49.5 db and, being curious, we checked channel separation at 15,000 cps. At this frequency, channel separation was 31 db, which is far beyond that required of any top-quality preamplifier.

It is disconcerting that even though amplifiers may test alike in the laboratory, they may not sound alike. This occurs because there are many not-too-well-known and not-too-easily-measured characteristics in an amplifier that affect quality of reproduction. Therefore, a listening test is required. This preamplifier provides no audible coloration in sound reproduction. One has the feeling of listening to a live musical performance instead of through a hi-fi system.

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**FILTERS & ATTENUATORS**, Edited by Alexander Schure, Ph.D. (No. 36 in the Electronic Technology Series.) This book will make filters, attenuators—their functions, the wide variety of types, circuitry and applications understandable. Both narrative and mathematical presentations are used. The characteristics of the capacitor-input type filter in power supplies is analyzed with problems and solutions. Numerous other filter types used in power supplies also are discussed in similar manner. Audio and video filters, wave filters and specialized types, are covered thoroughly—a chapter being devoted to each.

The text devoted to attenuators and equalizers is illuminated by means of numerical examples and solutions. The calculations include the determina-

tion of their component parts. Variable attenuators are also covered, as well as phase equalizers. This is an outstanding technical text for those interested in the configuration and analysis of filter and attenuator circuitry. Review questions appear at the end of each chapter. #166-36, \$2.25.

**TRANSFORMERS**, Edited by Alexander Schure, Ph.D. (No. 37 in the Electronic Technology Series) The transformer as it is used in electronic equipment is examined in a highly analytical manner with numerous mathematical examples. The examples give the reader a theoretical as well as a practical view of the transformer. Starting with a discussion of the magnetic principles underlying the operation of the transformer, it progresses to transformer design and construction, discussing efficiency and coil currents, flux density, core losses, leakage inductance, distributed capacitance and current as well as voltage waveforms. Power transformers are studied in full depth from the simple color coding of the leads to the relation of power transformers to rectifier-filter systems. Audio transformers are covered with emphasis on such important topics as impedance ratios, broad-band audio transformers and transistor transformers. In the area of high frequency transformers, the text treats the tuned and untuned primary and secondary windings in different combinations. It discusses in detail such special transformer items as saturable reactors, voltage regulating transformers, video transformers, pulse transformers and balancing transformers (baluns). Review questions appear at the end of each chapter. #166-37, \$2.00.

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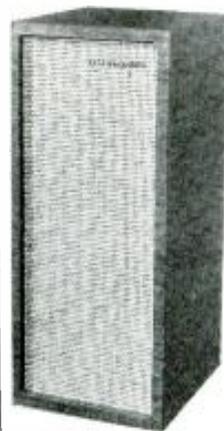
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This is not only one of the best units on the market but, as mentioned previously, we enjoyed immensely putting the kit together because of its military-type construction. It took us 17½ hours

to build the kit. The preamp is available at \$119.95 in kit form, and \$189 factory-wired. Neither of these prices include the walnut wood outer cabinet, which is available separately at \$29.95. —30—

### Channel Master CM-10 Speaker System

**T**HIS is a compact bookshelf-type loud-speaker system consisting of an 8-inch woofer and 2-inch coaxially mounted cone tweeter, in a ducted-port reflex enclosure. The crossover is at 3000 cps and the tweeter's level is non-adjustable. The system is rated at 10 watts power-handling capacity (continuous or program not specified) and 8 ohms impedance. The enclosure measures 10 inches



wide by 23½ inches high by 11 inches deep.

Sweeping a test tone through the audible range (with the speaker located in a corner, for maximum bass radiation), the CM-10 was found to have subjectively smooth, linear response from 100 to 15,000 cps, with a drop in the range between 1 kc. and 2 kc., and a broad, shallow dip between 200 and 600 cps. Above 2 kc. there was not a trace of audible deviation until 7 kc., at which point there was a slight dip, followed by a rise back to normal at 8 kc. Then there was another mild dip at 10 kc., and smooth, flat response from there out to 14 kc. Above that, a slow roll-off set in, but a significant contribution was observed to beyond 16 kc.,

at which point this reviewer's ears fail him. No distortion was audible at any frequency, even at fairly high listening levels.

On program material, the CM-10 was sharply brilliant. Over-all definition was excellent; details were very well reproduced, and there was some tendency toward spotlighting of brass instruments and soprano voices. String tone was reproduced cleanly and smoothly, although with a subtly cold, brittle quality. It was immediately obvious that the CM-10's treble performance was superior to its bass response which, although clean and well defined, was somewhat lacking in foundation. This effect is not altogether unusual, and it is not quite fair to expect the same fullness in the bass that would be produced by a somewhat larger woofer in a larger and more expensive enclosure.

Despite its modest power rating, the CM-10 proved able to handle considerable bass boost without audible strain, and a moderate amount of boosting was all that was needed to bring the system's sound into a good semblance of natural musical balance.

The addition of a second CM-10, for stereo pairing, might well augment the low range enough to provide good bass balance without external boosting, and the tweeter's broad high-frequency distribution (estimated at about 80 degrees) should enable the system to yield excellent stereo spread and fill in most listening rooms.

The CM-10 is priced at \$44.95. —30—

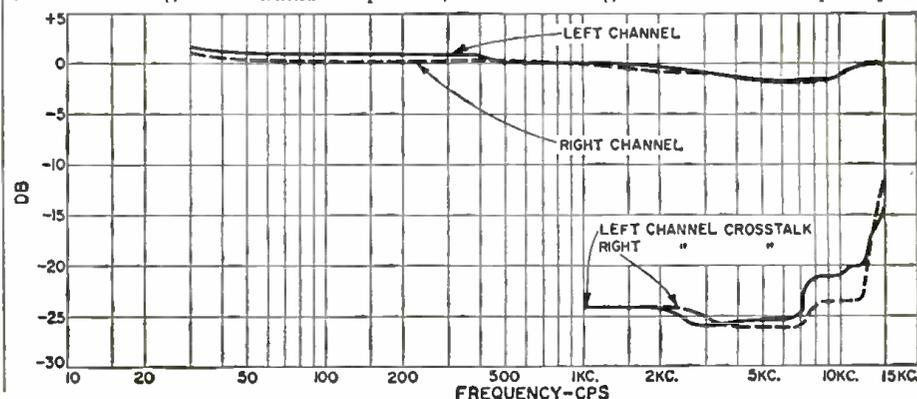
### Pickering Model 381A Stereo Cartridge

**A**LTHOUGH the new *Pickering* 381A stereo cartridge looks identical to the manufacturer's Model 380A, its performance is different. The 381A is much more expensive and has less output voltage, but its over-all reproduction quality makes it one of the very best stereo cartridges we have tested to date.

The 381A was specifically designed for use by recording engineers, not only for calibrating their audio amplifiers,

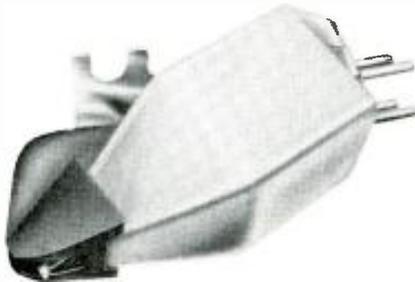
but for playback equipment to determine the quality of recordings. All cartridges are individually calibrated at the plant and the results are tabulated and shipped with each unit. It is *Pickering's* hope that this cartridge will be recognized as a standard for the recording industry and they have had some degree of success along these lines to date.

All this does not preclude the use of the cartridge in the home if quality is



most desired and price is no object. The frequency response and channel separation characteristics are shown in the accompanying graph. It is interesting to note the smoothness of the response, being  $\pm 1.8$  db from 30 to 15,000 cps, the limits of our test record.

This response is good in that it betters all other stereo cartridges we have checked recently by about a db or so. What is unusual and we feel extremely important is the channel separation. Both channels show a crosstalk down 24 db at 1000 cps. (We cannot measure much below this using the *Westrex* 1A test record.) The manufacturer claims 35-db channel separation, and it is quite possible that this is actually achieved. As pointed out in our report on the



Model 380A cartridge, *Pickering* has a specially designed test record which has a much greater signal-to-noise ratio than ours. Unfortunately, this record is not available to us for testing.

Greater separation than 20 db is not necessary for home listening, but, for best results, separation should not drop much below this figure out to 10 or 15 kc. Some recent studies conducted by *Bell Telephone Laboratories* indicate that full separation is required for home listening only out to about 8 kc. This conclusion was reached with the use of presently available stereo tapes and discs. In spite of this, it is still nice to know that we have some equipment available whose performance exceeds the needs for present-day in-home use. We can also foresee the possibility that future tapes and discs will have even more strict requirements for reproduction.

Many of the early cartridges had an opposite channel output voltage at 10,000 to 15,000 cps that was greater than the voltage from the proper channel. It is interesting to note that this new cartridge not only keeps the channels where they belong without interchanging them but, in addition, has good separation out to 15,000 cycles.

The output voltage measured was 4.55 mv. for the left channel, and 4.9 mv. for the right channel for 5 centimeters per second recording at 1000 cycles. The recommended load is from 47,000 to 100,000 ohms, and stylus pressure should be maintained between 2 and 3 grams. A .7 mil easily replaceable diamond stylus is used. A stylus is also available for 78-rpm records.

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		828	1.00	965	1.00	5Y35	.40
		829	1.00	966	1.00	5Y36	.40
		830	1.00	967	1.00	5Y37	.40
		831	1.00	968	1.00	5Y38	.40
		832	1.00	969	1.00	5Y39	.40
		833	1.00	970	1.00	5Y40	.40
		834	1.00	971	1.00	5Y41	.40
		835	1.00	972	1.00	5Y42	.40
		836	1.00	973	1.00	5Y43	.40
		837	1.00	974	1.00	5Y44	.40
		838	1.00	975	1.00	5Y45	.40
		839	1.00	976	1.00	5Y46	.40
		840	1.00	977	1.00	5Y47	.40
		841	1.00	978	1.00	5Y48	.40
		842	1.00	979	1.00	5Y49	.40
		843	1.00	980	1.00	5Y50	.40
		844	1.00	981	1.00	5Y51	.40
		845	1.00	982	1.00	5Y52	.40
		846	1.00	983	1.00	5Y53	.40
		847	1.00	984	1.00	5Y54	.40
		848	1.00	985	1.00	5Y55	.40
		849	1.00	986	1.00	5Y56	.40
		850	1.00	987	1.00	5Y57	.40
		851	1.00	988	1.00	5Y58	.40
		852	1.00	989	1.00	5Y59	.40
		853	1.00	990	1.00	5Y60	.40
		854	1.00	991	1.00	5Y61	.40
		855	1.00	992	1.00	5Y62	.40
		856	1.00	993	1.00	5Y63	.40
		857	1.00	994	1.00	5Y64	.40
		858	1.00	995	1.00	5Y65	.40
		859	1.00	996	1.00	5Y66	.40
		860	1.00	997	1.00	5Y67	.40
		861	1.00	998	1.00	5Y68	.40
		862	1.00	999	1.00	5Y69	.40
		863	1.00	1000	1.00	5Y70	.40

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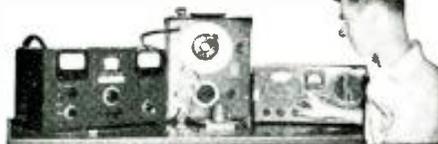
Type	Price	Type	Price	Type	Price	Type	Price
6Z4	.42	6AR	.60	7A4 JXN1	1.00	6X4	.44
1A7GT	.45	6AR1	.60	7A5	.44	12BH6	.44
1B6GT	.52	6AR2	.65	7A6	.44	12BH7	.44
1B7	.50	6AF1	.70	7A7	.44	12BH8	.44
1H5GT	.45	6AG1	.40	7A8	.44	12BH9	.44
114	.45	6AG2	.44	7A9	.44	12BH10	.44
116	.42	6AG3GT	.44	7B1	.44	12BH11	.44
1N56GT	.52	6AH1	.55	7B2	.44	12BH12	.44
1N56T	.52	6AK	.55	7B3	.44	12BH13	.44
1Q3GT	.51	6AL	.55	7B4	.44	12BH14	.44
1R3	.41	6AM8	.40	7B5	.44	12BH15	.44
1R5	.40	6AN	.44	7B6	.44	12BH16	.44
1T1	.41	6AQ1	.42	7B7	.44	12BH17	.44
1U4	.41	6AQ2GT	.44	7B8	.44	12BH18	.44
1U5	.42	6AQ3GT	.44	7B9	.44	12BH19	.44
1V2	.40	6AR5	.48	7C1	.44	12BH20	.44
1V3	.40	6AR6	.48	7C2	.44	12BH21	.44
1V4	.40	6AR7	.48	7C3	.44	12BH22	.44
2A3	.40	6A7	.44	7C4	.44	12BH23	.44
2A4	.40	6A8	.44	7C5	.44	12BH24	.44
2A5	.40	6A9	.44	7C6	.44	12BH25	.44
2A6	.40	6A10	.44	7C7	.44	12BH26	.44
2A7	.40	6A11	.44	7C8	.44	12BH27	.44
2A8	.40	6A12	.44	7C9	.44	12BH28	.44
2A9	.40	6A13	.44	7D1	.44	12BH29	.44
2A10	.40	6A14	.44	7D2	.44	12BH30	.44
2A11	.40	6A15	.44	7D3	.44	12BH31	.44
2A12	.40	6A16	.44	7D4	.44	12BH32	.44
2A13	.40	6A17	.44	7D5	.44	12BH33	.44
2A14	.40	6A18	.44	7D6	.44	12BH34	.44
2A15	.40	6A19	.44	7D7	.44	12BH35	.44
2A16	.40	6A20	.44	7D8	.44	12BH36	.44
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2A18	.40	6A22	.44	7E1	.44	12BH38	.44
2A19	.40	6A23	.44	7E2	.44	12BH39	.44
2A20	.40	6A24	.44	7E3	.44	12BH40	.44
2A21	.40	6A25	.44	7E4	.44	12BH41	.44
2A22	.40	6A26	.44	7E5	.44	12BH42	.44
2A23	.40	6A27	.44	7E6	.44	12BH43	.44
2A24	.40	6A28	.44	7E7	.44	12BH44	.44
2A25	.40	6A29	.44	7E8	.44	12BH45	.44
2A26	.40	6A30	.44	7E9	.44	12BH46	.44
2A27	.40	6A31	.44	7F1	.44	12BH47	.44
2A28	.40	6A32	.44	7F2	.44	12BH48	.44
2A29	.40	6A33	.44	7F3	.44	12BH49	.44
2A30	.40	6A34	.44	7F4	.44	12BH50	.44
2A31	.40	6A35	.44	7F5	.44	12BH51	.44
2A32	.40	6A36	.44	7F6	.44	12BH52	.44
2A33	.40	6A37	.44	7F7	.44	12BH53	.44
2A34	.40	6A38	.44	7F8	.44	12BH54	.44
2A35	.40	6A39	.44	7F9	.44	12BH55	.44
2A36	.40	6A40	.44	7G1	.44	12BH56	.44
2A37	.40	6A41	.44	7G2	.44	12BH57	.44
2A38	.40	6A42	.44	7G3	.44	12BH58	.44
2A39	.40	6A43	.44	7G4	.44	12BH59	.44
2A40	.40	6A44	.44	7G5	.44	12BH60	.44
2A41	.40	6A45	.44	7G6	.44	12BH61	.44
2A42	.40	6A46	.44	7G7	.44	12BH62	.44
2A43	.40	6A47	.44	7G8	.44	12BH63	.44
2A44	.40	6A48	.44	7G9	.44	12BH64	.44
2A45	.40	6A49	.44	7H1	.44	12BH65	.44
2A46	.40	6A50	.44	7H2	.44	12BH66	.44
2A47	.40	6A51	.44	7H3	.44	12BH67	.44
2A48	.40	6A52	.44	7H4	.44	12BH68	.44
2A49	.40	6A53	.44	7H5	.44	12BH69	.44
2A50	.40	6A54	.44	7H6	.44	12BH70	.44
2A51	.40	6A55	.44	7H7	.44	12BH71	.44
2A52	.40	6A56	.44	7H8	.44	12BH72	.44
2A53	.40	6A57	.44	7H9	.44	12BH73	.44
2A54	.40	6A58	.44	7H10	.44	12BH74	.44
2A55	.40	6A59	.44	7H11	.44	12BH75	.44
2A56	.40	6A60	.44	7H12	.44	12BH76	.44
2A57	.40	6A61	.44	7H13	.44	12BH77	.44
2A58	.40	6A62	.44	7H14	.44	12BH78	.44
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2A60	.40	6A64	.44	7H16	.44	12BH80	.44
2A61	.40	6A65	.44	7H17	.44	12BH81	.44
2A62	.40	6A66	.44	7H18	.44	12BH82	.44
2A63	.40	6A67	.44	7H19	.44	12BH83	.44
2A64	.40	6A68	.44	7H20	.44	12BH84	.44
2A65	.40	6A69	.44	7H21	.44	12BH85	.44
2A66	.40	6A70	.44	7H22	.44	12BH86	.44
2A67	.40	6A71	.44	7H23	.44	12BH87	.44
2A68	.40	6A72	.44	7H24	.44	12BH88	.44
2A69	.40	6A73	.44	7H25	.44	12BH89	.44
2A70	.40	6A74	.44	7H26	.44	12BH90	.44
2A71	.40	6A75	.44	7H27	.44	12BH91	.44
2A72	.40	6A76	.44	7H28	.44	12BH92	.44
2A73	.40	6A77	.44	7H29	.44	12BH93	.44
2A74	.40	6A78	.44	7H30	.44	12BH94	.44
2A75	.40	6A79	.44	7H31	.44	12BH95	.44
2A76	.40	6A80	.44	7H32	.44	12BH96	.44
2A77	.40	6A81	.44	7H33	.44	12BH97	.44
2A78	.40	6A82	.44	7H34	.44	12BH98	.44
2A79	.40	6A83	.44	7H35	.44	12BH99	.44
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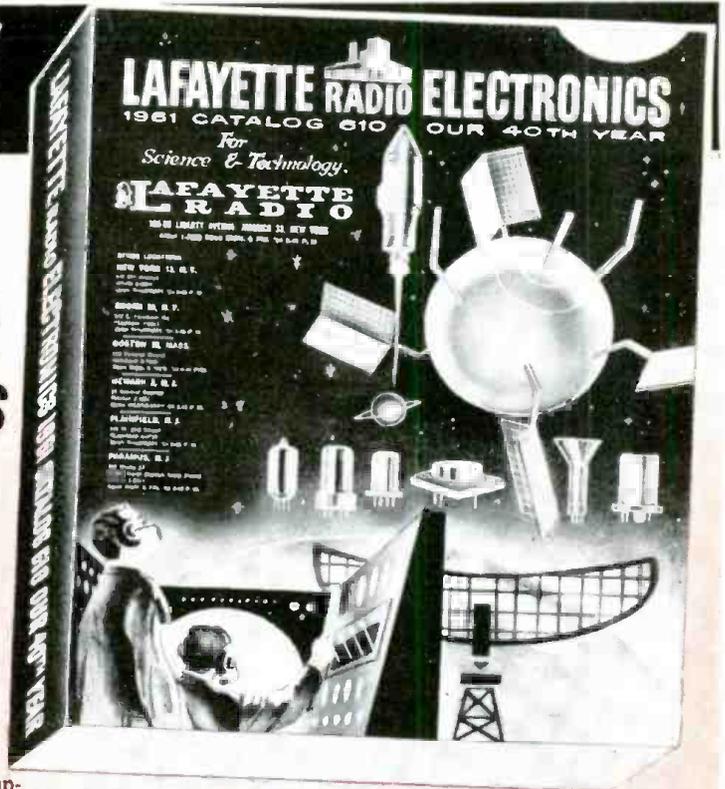
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## Diodes Are Different

(Continued from page 50)

the tube in the first place. But by now we are hooked, so we buy five new diodes and put four on a side. The chances are that this supply will stand up. But once in a while, if luck is against us, it goes too, and we find four shorted diodes.

### Back Resistance

The villain here is back resistance. The back resistance of diodes varies enormously. Anyone who has several silicon diodes on hand can get his eyes opened and increase his education by performing a very simple experiment. This consists of setting up the circuit shown in Fig. 2A. Any handy voltage

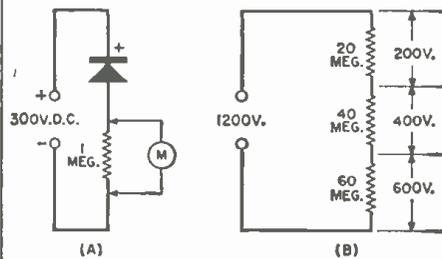


Fig. 2. (A) Simple setup to check back resistance of diodes. (B) The way that back voltage is distributed across diodes that have different back resistance values.

under the rated p.i.v. of the diode will do. The voltmeter shown reads the voltage drop across the 1-meg. resistor. This will be the back current through the diode in microamperes. In other words, one volt across the resistor means one microampere of back current.

The writer has made this test on 27 diodes, all with 400 p.i.v. rating. About half had 150- or 200-ma. ratings and the other half a 500-ma. rating. They represented five different styles of diodes from three different manufacturers.

Among the 27, the back current varied from 2 to 80 microamperes. This is a total range of back resistance of approximately 4 to 150 megohms. The range within one style was not so great, but in many cases covered a 3 to 1 range.

Now this has a serious effect when diodes are used in strings. Let's go back to the case of our hi-fi friend and his power supply. Suppose, as might very easily be the case, he had three diodes in one string with back resistances of 20, 40, and 60 megohms. When the 1200-volt peak is placed across these diodes, we have the situation illustrated in Fig. 2B. The voltage drop across the 20-meg. diode is 200 volts; across the 40-meg. diode, 400 volts; and across the 60-meg. diode it is 600 volts, or about 50 per-cent over rating. If this diode is operating near full current capacity, this high stress coupled with the heat generated at the junction on the forward-current pulse will set up a destruction cycle, and this diode will short out. Then the 1200 volts divides across the remaining diodes in the ratio of their resistances and the second diode shorts. Almost immediately the third one will go.

If four diodes are used, the chance of this sort of thing is greatly lessened, but again, if a high-resistance diode gets in the string with a couple of low-resistance diodes, even in this case there may be a failure. Now when single diodes are used across fixed low impedance sources that are less than rated p.i.v., this will not happen because the low resistance diode merely passes more back current. It is the series operation that causes the trouble.

### The Solution

The solution to this problem is a simple one and is quite familiar to those who use electrolytic capacitors in series. You equalize the voltages with shunting resistors. Values of 100,000 to 200,000 ohms will swamp out the variations among the diode back resistances.

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supply for the hi-fi addict who has spent so much money buying diodes. This is shown in Fig. 3. There are two things

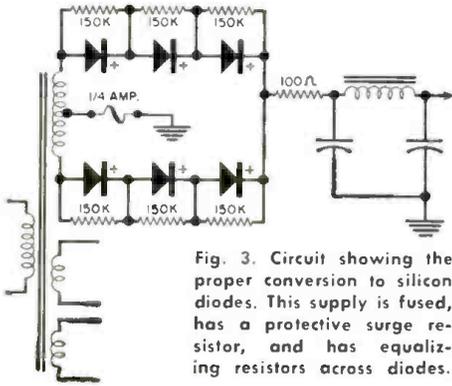


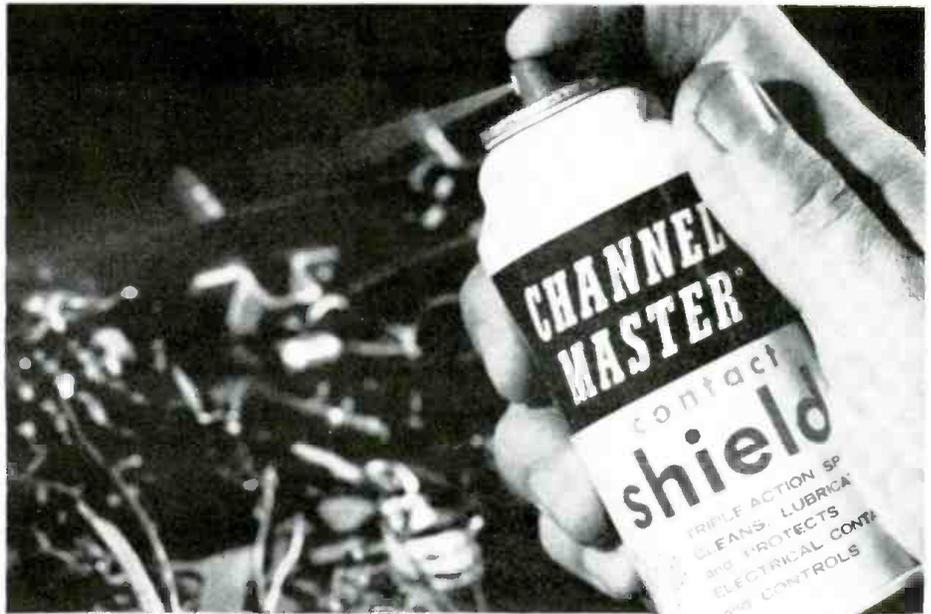
Fig. 3. Circuit showing the proper conversion to silicon diodes. This supply is fused, has a protective surge resistor, and has equalizing resistors across diodes.

that might be mentioned. First off, these resistors will pass some raw a.c. around the rectifiers. Will this affect hum? The answer is no; it won't be detected by the ear, although it can be noticed on the oscilloscope if it is cranked up. The second point is that the resistors generate heat—perhaps a couple of watts of it.

As a result of this we can make up a few simple rules by way of a summary:

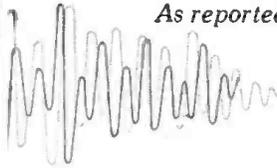
1. Don't forget that protective resistor with diodes. Better yet, use a choke input and improve regulation at the same time.
2. Fuse the power supply. This is always good advice, but especially with diodes because they are more prone than tubes to short out rather than open up.
3. Always use equalizing resistors when you put two or more diodes in series.
4. Provide ventilation. Diodes don't run cold, remember. Between equalizing resistors and junction heat, air circulation is needed.

Follow these simple rules and enjoy the very real benefits to be derived from the use of diodes in that ham transmitter or hi-fi amplifier.



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SUPERIOR'S NEW MODEL 770-A

## VOLT-OHM MILLIAMMETER



### FEATURES:

- Compact—measures 3 1/8" x 5 7/8" x 2 1/4".
- Uses "Full View" 20,000 accurate 850 Microampere D'Arsonval type meter
- Housed in round-cornered, molded case.

### SPECIFICATIONS:

- 6 **A.C. VOLTAGE RANGES:** 0-15/30/150/300/1500/3000 Volts.
- 6 **D.C. VOLTAGE RANGES:** 0-7.5/15/75/150/750/1500 Volts.
- 2 **RESISTANCE RANGES:** 0-10,000 Ohms, 0-1 Megohm.
- 3 **D.C. CURRENT RANGES:** 0-15/150 Ma., 0-1.5 Amps.
- 3 **DECIBEL RANGES:** -6 db to + 18 db, + 14 db to + 38 db, + 34 db to + 58 db.

The Model 770-A comes complete with test leads and operating instructions. Price is \$15.85. Terms: \$3.85 after 10 day trial then \$4.00 monthly for 3 months.

SUPERIOR'S NEW MODEL 79

## SUPER-METER



### WITH NEW 6" FULL VIEW METER

- SPECIFICATIONS:**
- D.C. VOLTS:** 0 to 7.5/15/75/150/750/1,500.
  - A.C. VOLTS:** 0 to 15/30/150/300/1,500/3,000.
  - D.C. CURRENT:** 0 to 1.5/15/150 Ma. 0 to 1.5/15 Amperes.
  - RESISTANCE:** 0 to 1,000/100,000 Ohms. 0 to 10 Megohms.
  - CAPACITY:** .001 to 1 Mfd. 1 to 50 Mfd.
  - REACTANCE:** 50 to 2,500 Ohms. 2,500 Ohms to 2.5 Megohms.
  - INDUCTANCE:** .15 to 7 Henries. 7 to 7,000 Henries.
  - DECIBELS:** -6 to + 18, + 14 to + 38, + 34 to + 58.

The following components are all tested for **QUALITY** at appropriate test potentials. Two separate **BAD-GOOD** scales on the meter are used for direct readings.

All Electrolytic Condensers from 1 MFD to 1000 MFD.  
All Selenium Rectifiers. All Germanium Diodes.  
All Silicon Rectifiers. All Silicon Diodes.

Model 79 comes complete with operating instructions, test leads and carrying case. Price is \$38.50. Terms: \$8.50 after 10 day trial then \$6.00 monthly for 3 months.

SUPERIOR'S NEW MODEL 77

## VACUUM TUBE VOLTMETER

### WITH NEW 6" FULL VIEW METER

Compare it to any peak-to-peak V.T.V.M. made by any other manufacturer at any price!



### SPECIFICATIONS:

- **DC VOLTS**—0 to 3/15/75/150/300/750/1500 volts at 11 megohms input resistance.
- **AC VOLTS (RMS)**—0 to 3/15/75/150/300/750/1500 volts.
- **AC VOLTS (Peak to Peak)**—0 to 8/40/200/400/800/2000 volts.
- **ELECTRONIC OHMMETER**—0 to 1000 ohms/10,000 ohms/100,000 ohms/1 megohm/10 megohms/100 megohms/1,000 megohms.
- **DECIBELS**—10 db to + 18 db, + 10 db to + 38 db, + 30 db to + 58 db. All based on 0 db = .006 watts (6 mw) into a 500 ohm line (1.73v).
- **ZERO CENTER METER**—For discriminator alignment with full scale range of 0 to 1.5/7.5/37.5/75/150/375/750 volts at 11 megohms input resistance.

Model 77 comes complete with operating instructions, probe and test leads and carrying case. Price is \$42.50. Terms: \$12.50 after 10 day trial then \$6.00 monthly for 3 months.

SUPERIOR'S NEW MODEL 80

## 20,000 OHMS PER VOLT ALLMETER



6 INCH FULL-VIEW METER provides large easy-to-read calibrations. No squinting or guessing when you use Model 80.

MIRRORED SCALE permits fine accurate measurements where fractional readings are important.

### SPECIFICATIONS:

- 3 **D.C. VOLTAGE RANGES:** (At a sensitivity of 20,000 Ohms per Volt) 0 to 15/75/150/300/750/1500/7500 Volts.
- 6 **A.C. VOLTAGE RANGES:** (At a sensitivity of 5,000 Ohms per Volt) 0 to 15/75/150/300/750/1500 Volts.
- 3 **RESISTANCE RANGES:** 0 to 2,000/200,000 Ohms. 0-20 Megohms.
- 2 **CAPACITY RANGES:** .00025 Mfd. to 3 Mfd. .05 Mfd. to 30 Mfd.
- 5 **D.C. CURRENT RANGES:** 0-75 Microamperes, 0 to 7.5/75/750 Milliampers, 0 to 15 Amperes.
- 3 **DECIBEL RANGES:** -6 db to +18 db, +14 db to +38 db, +34 db to +58 db.

NOTE: The line cord is used only for capacity measurements. Resistance ranges operate on self-contained batteries.

Model 80 Allmeter comes complete with operating instructions, test leads and portable carrying case. Price is \$42.50. Terms: \$12.50 after 10 day trial then \$6.00 monthly for 3 months.

SUPERIOR'S NEW MODEL 70 UTILITY TESTER

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As an electrical trouble shooter the Model 70:

- Will test Toasters, Irons, Broilers, Heating Pads, Clocks, Fans, Vacuum Cleaners, Refrigerators, Lamps, Fluorescents, Switches, Thermostats, etc.
- Measures A.C. and D.C. Voltages, A.C. and D.C. Current, Resistances, Leakage, etc.
- Incorporates a sensitive direct-reading resistance range which will measure all resistances commonly used in electrical appliances, motors, etc.
- Leakage detecting circuit will indicate continuity from zero ohms to 5 megohms (5,000,000 ohms).

As an Automotive Tester the Model 70 will test:

- Both 6 Volt and 12 Volt Storage Batteries • Generators • Starters • Distributors • Ignition Coils
- Regulators • Relays • Circuit Breakers • Cigarette Lighters • Stop Lights • Condensers • Directional Signal Systems • All Lamps and Bulbs • Fuses • Heating Systems • Horns • Also will locate poor grounds, breaks in wiring, poor connections, etc.

Model 70 comes complete with 64 page book and test leads. Price is \$15.85. Terms: \$3.85 after 10 day trial then \$4.00 monthly for 3 months.

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SUPERIOR'S NEW MODEL 82A  
**MULTI-SOCKET TYPE**

## TUBE TESTER



- SPECIFICATIONS:**
- Tests over 1000 tube types.
  - Tests OZ4 and other gas-filled tubes.
  - Employs new 4" meter with sealed air-damping chamber resulting in accurate vibrationless readings.
  - Use of 22 sockets permits testing all popular tube types and prevents possible obsolescence.
  - Dual Scale meter permits testing of low current tubes.
  - 7 and 9 pin straighteners mounted on panel.
  - All sections of multi-element tubes tested simultaneously.
  - Ultra-sensitive leakage test circuit will indicate leakage up to 5 mesohms.

Model 82A comes housed in handsome, portable, saddle-stitched Texon case. Price is \$36.50. Terms: \$6.50 after 10 day trial then \$6.00 monthly for 5 months.

SUPERIOR'S NEW MODEL TW-11  
**STANDARD PROFESSIONAL**

## TUBE TESTER



- Uses the new self-cleaning Lever Action Switches for individual element testing. Because all elements are numbered according to pin-number in the RMA base numbering system, the user can instantly identify which element is under test.
- Free-moving built-in roll chart provides complete data for all tubes. All tube listings printed in large-easy-to-read type.
- **NOISE TEST:** Phono-jack on front panel for plugging in either diodes or external amplifier will detect microphonic tubes or noise due to faulty elements and loose internal connections.
- **SEPARATE SCALE FOR LOW-CURRENT TUBES**—Previously, on emission type tube testers, it has been standard practice to use one scale for all tubes. As a result, the calibration for low-current types has been restricted to a small portion of the scale. The extra scale used here greatly simplifies testing of low-current types.

The Model TW-11 comes housed in a handsome, portable, saddle-stitched Texon case. Price is \$47.50. Terms: \$11.50 after 10 day trial then \$6.00 monthly for 6 months.

SUPERIOR'S NEW MODEL 83A

## C.R.T. TESTER

**Tests and Rejuvenates  
ALL PICTURE TUBES**



- ALL BLACK AND WHITE TUBES**  
From 50 degree to 110 degree types—  
from 8" to 30" types.
- ALL COLOR TUBES**  
Test ALL picture tubes—in the carton  
—out of the carton—in the set!

Model 83A provides separate filament operating voltages for the older 6.3 types and the newer 8.4 types.

Model 83A properly tests the red, green and blue sections of color tubes individually—for each section of a color tube contains its own filament, plate, grid and cathode.

Model 83A will detect tubes which are apparently good but require rejuvenation. Such tubes will provide a picture seemingly good but lacking in proper definition, contrast and focus.

Rejuvenation of picture tubes is not simply a matter of applying a high voltage to the filament. Such voltages improperly applied can strip the cathode of the oxide coating essential for proper emission. The Model 83A applies a selective low voltage uniformly to assure increased life with no danger of cathode damage.

Model 83-A comes housed in handsome portable saddle-stitched Texon case—complete with socket for all black and white tubes and all color tubes. Price is \$38.50. Terms: \$8.50 after 10 day trial then \$6.00 monthly for 5 months.

SUPERIOR'S NEW MODEL 85  
**TRANS-CONDUCTANCE TYPE**

## TUBE TESTER



- Employs latest improved **TRANS-CONDUCTANCE** circuit. Test tubes under "dynamic" (simulated) operating conditions. An in-phase signal is impressed on the input section of a tube and the resultant plate current change is measured as a function of tube quality. This provides the most suitable method of simulating the manner in which tubes actually operate in radio, TV receivers, amplifiers and other circuits. Amplification factor, plate resistance and cathode emission are all correlated in one meter reading.
- **SYMBOL REFERENCES:** Model 85 employs time-saving symbols (\*, •, ▲, ■) in place of difficult-to-remember letters previously used. Repeated time-studies proved to us that use of these scientifically selected symbols speeded up the element switching step. As the tube manufacturers increase the release of new tube types, this time-saving feature becomes necessary and advantageous.

• **"FREE-POINT" LEVER TYPE ELEMENT SWITCH ASSEMBLY** marked according to RETMA basing, permits application of test voltages to any of the elements of a tube.

• **FREE FIVE (5) YEAR CHART DATA SERVICE.** Revised up-to-date subsequent charts will be mailed to all Model 85 purchasers at no charge for a period of five years after date of purchase.

Model 85 comes complete, housed in a handsome portable cabinet with slip-on cover. Price is \$52.50. Terms: \$12.50 after 10 day trial then \$8.00 monthly for 5 months.

SUPERIOR'S NEW MODEL TV-50A

## GENOMETER 7 Signal Generators in One!



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A versatile all-inclusive **GENERATOR** which provides **ALL** the outputs for servicing:

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- Black and White TV • Color TV

The Model TV-50A comes absolutely complete with shielded leads and operating instructions. Price is \$47.50. Terms: \$11.50 after 10 day trial then \$6.00 monthly for 6 months.

SUPERIOR'S NEW MODEL 88

## TESTS ALL TRANSISTORS AND TRANSISTOR RADIOS



**AS A TRANSISTOR RADIO TESTER**

An R.F. Signal source, modulated by an audio tone is injected into the transistor receiver from the antenna through the R.F. stage, past the mixer into the I.F. Amplifier and detector stages and on to the audio amplifier. This injected signal is then followed and traced through the receiver by means of a built-in High Gain Transistorized Signal Tracer until the cause of trouble is located and pinpointed.

**AS A TRANSISTOR TESTER**

The Model 88 will test all transistors including NPN and PNP, silicon, germanium and the new gallium arsenide types, without referring to characteristic data sheets. The time-saving advantage of this technique is self-evident. A further benefit of this service is that it will enable you to test new transistors as they are released!

Model 88 comes housed in a handsome portable case. Complete with a set of Clip-on Cables for Transistor Testing; an R.F. Diode Probe for R.F. & I.F. Tracing; an Audio Probe for Amplifier Tracing and a Signal Injector Cable. Complete—nothing else to buy! Price is \$38.50. Terms: \$8.50 after 10 day trial then \$6.00 monthly for 5 months.

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### Technical BOOKS

"WORLD RADIO TV HANDBOOK" Edited and published by O. Lund Johansen. Copenhagen, Denmark. Distributed in the U.S. by *Gilfer Associates*, P.O. Box 239, Grand Central Station, New York 17, N.Y. 218 pages. Price \$2.70 postpaid. Soft cover.

This is the 15th edition of a work that has become virtually a standard reference guide to international radio and television. It supplies detailed and authoritative information on broadcasting in every country in the world, listing call letters, frequencies, hours, as well as relevant information such as location and administration for stations listed.

In addition to regular broadcasts, the book lists special, religious, and short-wave frequencies over the globe, and provides up-to-the-minute information on several related subjects, such as world time in all countries, survey of world television, likely s.w. conditions for the coming year. The book is recommended by a number of official and trade organizations throughout the world.

"BASICS OF ANALOG COMPUTERS" by Thos. D. Truitt & A. E. Rogers. Published by *John F. Rider Publisher, Inc.*, New York. 400 pages. Price \$12.50.

This is an unusually good treatment of a difficult subject. Presented as a one-volume training course, it explains in simple, clear detail the concepts, devices, and applications of the analog computer. The text is liberally enhanced with clever drawings that combine the familiar with the unfamiliar, to help guide the reader through the material. The reader with no previous knowledge of this subject should have little or no difficulty in learning a good deal from this book. The reader with some knowledge will find it a concise, easy-to-read review which should consolidate, and perhaps extend, his grasp of the field. Maintenance technicians and computer programmers should find it particularly interesting. Review questions and a glossary are provided.

"SERVICING TRANSISTOR RADIOS" by the Sams Engineering Staff. Published by *Howard W. Sams & Co., Inc.*, Indianapolis. 160 pages. Price \$2.95. Soft cover.

Vol. 7 in this series covers 48 transistor radios produced in 1959 and 1960. Like the preceding volumes, it features "Photofact" schematics, dial-cord stringing arrangements, cabinet and chassis photos, alignment instructions, parts lists, and replacement data.

"SCIENCE PROJECTS HANDBOOK" edited by Shirley Moore. Published by *Science Service, Inc.*, Washington, D.C. and *Ballantine Books*. 254 pages. Price 50 cents. Soft cover.

Numerous projects, used in the teaching of science, are summarized. Subjects

covered include botany, chemistry, electronics, entomology, geology, mathematics, medical sciences, physics, space sciences, and zoology. Discussion ideas and a lengthy bibliography are also included.

\* \* \*  
**"ELECTRICITY AND ELECTRONICS—BASIC"** by William B. Steinberg & Walter B. Ford. Published by *American Technical Society*, Chicago. 262 pages. Price \$4.50.

This is the second, revised edition of a basic text that has been used in industrial arts, vocational, and technical training programs. The explanations of basic theory and simple applications are straightforward and clear and the many photographs and drawings are carefully chosen and executed. Review questions are included.

The main sections of the book consist of "this electrical and electronic age," magnetism, basic circuits, "electricity for everyday living," communications, basic formulas, standard symbols, soldering hints, and supplementary projects for the trainee to work on.

\* \* \*  
**"RAPID AUTO RADIO REPAIR"** by G. Warren Heath. Published by *Howard W. Sams & Co., Inc.*, Indianapolis. 158 pages. Price \$2.95. Soft cover.

The vast number of auto radios in use, as well as the changes in the receivers themselves add up to the need for a book such as this. Written primarily for the service technician, it is a practical servicing guide, containing hundreds of trouble symptom cures. What's more, it

contains a good deal of basic auto radio theory and circuit explanations. Chapters 1 through 3 cover types of receivers, circuits, and components. Chapters 4 through 6 cover servicing problems from A to Z—or at least from A to W, specifically, starting with alignment and ending with "weak reception."

\* \* \*  
**"BUILDING UP YOUR HAM SHACK"** by Howard S. Pyle. Published by *Howard W. Sams & Co., Inc.*, Indianapolis. 128 pages. Price \$2.50. Soft cover.

Of interest to the veteran ham as well as the Novice, this book discusses the equipment to use in an amateur station, as well as how to arrange it. A wide range of subjects is covered, including receivers, transmitters, antennas, miscellaneous gear, planning the station, testing and measuring equipment, the Novice workshop, supplies, clubs and other organizations, preparing for advancement, ham bands, the amateur's code, Conelrad information, and data on the "C" and "E" frequencies. Numerous photos and drawings supplement the text.

\* \* \*  
**"SATISFYING CUSTOMERS FOR PROFIT"** An Electronic Industries Association Project. Published by *Howard W. Sams & Co., Inc.*, Indianapolis. 96 pages. Price \$1.25. Soft cover.

Herein are presented 25 case-histories, said to be typical of those confronting the radio-television service dealer. The situations are told in story form, and points highlighted to empha-

size the techniques used to fulfill the technician's goal, as suggested by the book's title. The book thus answers many questions of a business relations nature, often as important in this field as the technical problems themselves.

### INVITATION TO AUTHORS

Just as a reminder, the Editors of *ELECTRONICS WORLD* are always interested in obtaining outstanding manuscripts, for publication in this magazine, covering the fields of audio and high-fidelity and radio-TV-industrial servicing. Articles in manuscript form may be submitted for immediate decision or projected articles can be outlined in a letter in which case the writer will be advised promptly as to the suitability of the topic. We can also use short "filler" items outlining worthwhile shortcuts that have made your servicing chores easier. This magazine pays for articles on acceptance. Send all manuscripts or your letters of suggestion to the Editor, *ELECTRONICS WORLD*, One Park Avenue, New York City 16, New York.

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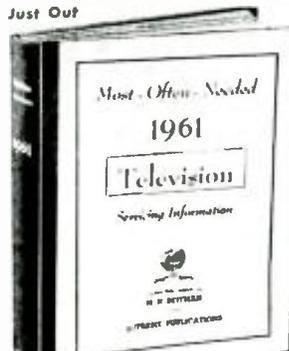
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## Voltage Regulator Diode-Tube Combinations

By DAVE STONE

Zener diodes with VR tubes prevent surges and permit various outputs.

ZENER voltage-regulating diodes and VR tubes can be used in efficient combinations for power-supply regulation applications. The lower-priced, low-voltage zener diodes can be connected in series with a VR tube when the power supply output may not be high enough to "fire" a VR tube alone.

For example, a VR-90 which requires 125 volts for firing can be replaced by an OA3 VR tube and a 15-volt, 1-watt diode. This combination will fire at 105 volts and regulate at the desired 90 volts. For 150-volt regulation, an OA2 VR tube which requires a firing voltage of 185 volts can be replaced with an OB2 and a 45-volt, 2-watt diode in series across the power supply. This pair will fire at 133 volts and regulate at 150 volts.

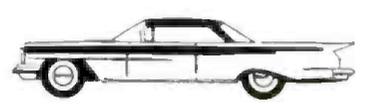
A diode-tube combination can be used to supply regulated voltages at levels which cannot be obtained with standard VR tubes. If a regulated 125 volts is needed, for instance, an OB2 and an 18-volt, 1-watt diode can be used. This combination will fire at 133 volts and regulate at 125 volts. A 200-volt regulated output can be obtained with an OA2 and a 50-volt, 2-watt zener which produces a pair that fires at 185 volts and regulates at 200 volts. The zener diode has no voltage drop until the VR tube conducts.

In general, the diode-VR tube pair is desirable because it never permits the output voltage to exceed the regulated level, which occurs when a VR tube alone is initially fired.

The table below lists several combinations of easily obtained components for the regulating applications described. Although the diode's cost is normally three to six times the cost of the VR tube, its long and almost indestructible life will insure little or no replacement problems in standard power supplies.

REGULATED VOLTAGE	FIRING VOLTAGE	VR TUBE TYPE	ZENER DIODE TYPE
90	105	OA3	15 v., 1 w. Motorola 1.5M15Z Hoffman 1N1775 Int. Rect. 1N1514
125	133	OB2 OC3	18 v., 1 w. Hoffman 1N1777 Int. Rect. 1N1526
150	133	OB2 OC3	45 v., 2 w. Motorola 10M45Z Hoffman 1N1366
200	185	OA2 OD3	50 v., 2 w. Motorola 10M50Z Hoffman 1N1368

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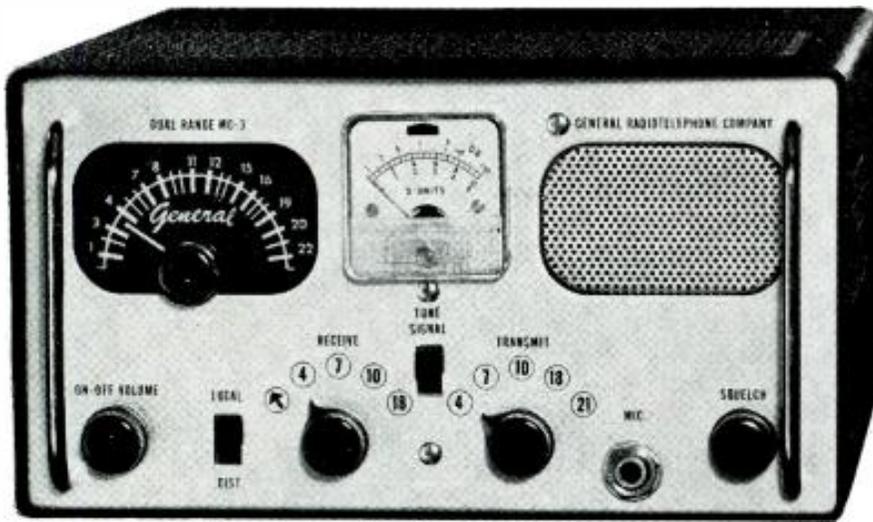
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# Hum Elimination

By CHARLES E. DIEHL

A simple, external control.



## DUAL RANGE — DUAL POWER — COMMERCIAL RADIOTELEPHONE MODEL MC-3

**RECEIVER:** Selectivity 5 kilocycles. Sensitivity better than  $\frac{1}{2}$  uv. Edge lighted dial face with luminous phosphor numerals. Cascade Dual Triode R-F Amplifier. Two gong tuning condenser tracks oscillator and mixer circuits. Exclusive tubeless Crystal Mixer circuit lowers noise level and eliminates current drain of tube. Two High-'Q' I.F. amplifier stages. Dual noise clippers. Sensitive squelch circuit with Auto-Time delay to minimize noise bursts breaking in. Self-contained 'S' meter. Four channel receive crystal selector plus 22-channel tuneable. External speaker plug. Each unit individually inspected and precision aligned for accurate calibration to assure low adjacent channel interference.

**TRANSMITTER:** Five channel Transmitter. Built-in Field Strength meter indicates loading and function. All coils wound of Moisture Proof wire. Built-in protection against obsolescence by use of oversize Power Transformer, Modulation Transformer, and Hi-Power tubes. Designed to operate at up to 15 watts input with no strain. Power Amplifier and Modulation tubes use high efficiency EL84 tubes for long life and stable output under the most rugged operating conditions. Tone signal generator for ringing remote units. G R C Plated Crystals for permanent frequency accuracy and output. Two-stage High-level Modulator. Antenna matches all low impedance antennas. Loading adjustment accessible externally.

**FREQUENCY RANGE:** 26.965-27.225 mc. **TUBES:** 6AN8, 6BQ5, 6BK7, 12AU7, 6BH6. 3 Germanium diodes, 5 Silicon diodes and 1 Dual Selenium diode. **POWER:** 40W/115V; 3.5A/12V; 7A/6V. Nominal. Complete Self-contained Power Supply for 6, 12 and 115 volts. **RELAY:** Hermetically Sealed for life. **SIZE:** 4.25"H x 8"W x 10.5"D. **WEIGHT:** 14 lbs. **FINISH:** Black wrinkle military finish over marine prime. Panel is Gold Anodized heavy aluminum. Chassis is triple plated with Cadmium, Copper, and Iridite gold finish. Moisture Fungus lacquer on underside of chassis. Brass and lacquer finished cabinet handles. Each set comes complete with 115 volt cord, crystal for one transmitting channel, Microphone (Ceramic, Chromed case, Push-to-talk switch), Instruction Guide, Form 505 for license, also Service Data is included for conversion to 15 watts. Parts and service Warrantied for 90 days. Model MC-3 Net Price \$199.95; 6v or 12v cord \$4.95; Mounting Rails \$1.95; Crystals, transmit or receive \$2.95 ea; FOB Burbank. Specifications subject to change without notice. Your Dealer or write:

GENERAL RADIOTELEPHONE COMPANY  
2806 West Burbank Boulevard  
Burbank, California, U.S.A.

\*Under present rules Part 19.32 the FCC does not provide for more than five (5) watt input in the Citizens Radio Service (26.965—27.225 mc band).

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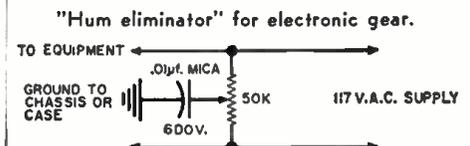
THE circuit shown in the accompanying diagram has produced very good results when it comes to eliminating hum from a variety of electronic gear. A similar circuit, in which the filament leads are bridged with a low-resistance potentiometer with its center-tap grounded, can also be used with varying degrees of success. By using a pot across the 117-volt supply, two things are accomplished: first, a much higher bucking voltage for phasing out the hum is obtained and complete isolation from the equipment circuit is achieved; second, it can be applied externally and tested for effectiveness. This circuit is also useful in emergency situations where the test setup has so much interference, from the ever-present a.c. potential, that measurements or other results are jeopardized.

It is often difficult to locate the exact point at which 60 cycles or a harmonic of 60 cycles is entering an amplifier circuit. This method facilitates locating the pickup point and applying the necessary correction.

Good results have been achieved in about 90 per-cent of the cases where it has been tried. The technique was used successfully on an audio generator which was unstable near 60 cycles or multiples of 60-cycle outputs. It enabled a frequency of 60.1 cycles to be produced without any of the previous jockeying to 60 cycles. It also cancelled the off-scale reading of an a.c. v.t.v.m. on the .01-volt full-scale position, when the meter was not connected to any circuit. This circuit is effective on some high-fidelity preamps but not effective on others. In recording on tape, it has helped most setups.

Different values of resistance from that shown in the diagram can be tried along with different capacities. It is desirable to use mica capacitors exclusively in this application because of their better leakage factor. Paper 600-volt capacitors will work, however, if they must be used. One thing to note is that a potentiometer across the 117-volt supply must have a high enough wattage rating to stand the load drawn. With the one-half-watt volume-control-type pot, about 50,000 ohms is the lowest feasible value. Anything up to 250,000 ohms will usually work in this circuit.

The values shown in the diagram have been found to be suitable in most cases. In use, of course, the technique involves variation of the potentiometer setting until the point of least hum pickup is found.



# “ THE CITATION SOUND ”

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“Over and above the details of design and performance, we felt that the Citation group bore eloquent witness to the one vital aspect of audio that for so many of us has elevated high fidelity from a casual hobby to a lifelong interest: the earnest attempt to reach an ideal—not for the sake of technical showmanship—but for the sake of music and our demanding love of it.”

Herbert Reid, Hi Fi Stereo Review

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Mr. Reid's eloquent tribute to Citation is one of many extraordinary reviews of these magnificent instruments. We are proud to present a brief collection of excerpts from Citation reviews written by outstanding audio critics.

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shading stood out clearly and distinctly for the first time . . . The kit is a joy to construct.”

C. G. McProud, Editor, Audio Magazine

“The unit which we checked after having built the kit, is the best of all power amplifiers that we have tested over the past years.”

William Stocklin, Editor, Electronics World

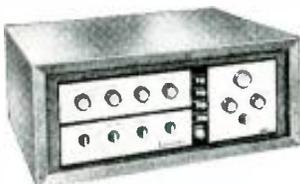
“Its listening quality is superb, and not easily described in terms of laboratory measurements. Listening is the ultimate test and a required one for full appreciation of Citation . . . Anyone who will settle for nothing less than the finest will be well advised to look into the Citation II.”

Hirsch-Houck Labs, High Fidelity Magazine

“At this writing, the most impressive of amplifier kits is without doubt the new Citation line of Harman-Kardon . . . their design, circuitry, acoustic results and even the manner of their packaging set a new high in amplifier construction and performance, kit or no.”

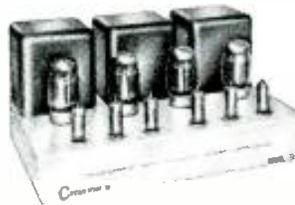
Norman Eisenberg, Saturday Review

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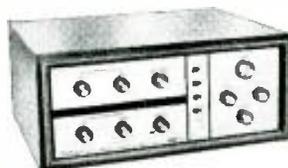
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**The CITATION III,  
Professional FM Tuner**

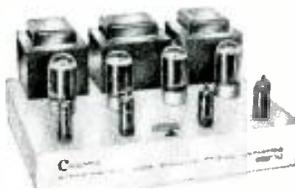
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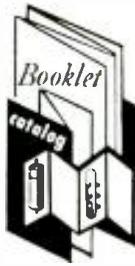
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For a free copy of any of these publications, write to the respective company.

**NEW RCA PUBLICATIONS**

*Radio Corporation of America*, Commercial Engineering, Semiconductor and Materials Division, Somerville, N.J. has issued two application booklets on transistors, and two for new tube types.

Application Guide No. 1CE-215 describes the special features and use of 16 RCA medium-power, intermediate-power, and high-power silicon transistors. Copies of this booklet may be obtained from the company's distributors or by sending 50 cents to the manufacturer.

Application Guide No. 1CE-228 describes the unique capabilities of RCA silicon v.h.f. transistors. These units—types 2N1491, 2N1492, and 2N1493—are intended for use in critical industrial and military applications at frequencies up to 300 mc. Copies may be obtained from distributors or by sending 50 cents to the manufacturer.

Application Note AN-189 describes two complements of newly developed tubes specially designed for series-string applications in either 4-tube or 5-tube home radio receivers. In addition, the Note describes and evaluates an experimental 4-tube economy receiver using a new 100-ma. complement consisting of tube types 18FX6, 20EQ7, 50FK5, and 36AM3-A.

Application Note AN-190 describes the performance of three recently developed power-output tubes. These tubes—types 34GD5, 50FK5, and 60FX5—are high-power-sensitivity miniature types especially designed for use in series-heater-string circuits operating at a total heater voltage of 120 volts and heater current of 100 ma. This Note also describes and evaluates the performance of three series-string stereo amplifiers utilizing the new tubes. These amplifiers provide maximum power outputs ranging from 1.0 to 1.25 watts per channel.

Copies of the Application Notes may be obtained from the manufacturer.

**LEE CATALOGUE**

*Lee Electric, Inc.*, 566 52nd St., West New York, N.J. has issued a new catalogue, available to the trade, covering signaling devices, transformers, push-buttons, and other devices.

**WIRE BOOKLET**

*Anaconda Wire & Cable Co.*, Dept. EFL, 25 Broadway, New York 4, N.Y. has published a 12-page booklet containing condensed data on the complete line of electronic hook-up wire manufactured by *Sequoia Wire & Cable Co.*, a new subsidiary.

For a copy of the booklet (DM-S-6014), write direct to the manufacturer.

**OPTICAL MASERS**

*Bell Telephone Laboratories, Inc.*, Murray Hill, N.J. has announced a booklet describing the theory and design of the solid-state optical maser. Copies may be obtained by writing to H. W. Mattson at the laboratories.

**MULLARD PUBLICATION**

*Mullard International Electronics Corp.*, 81 Spring St., New York 12, N.Y. has announced that copies of issue No. 45 of its publication "Mullard Technical Communications" are available on request.

The articles in this issue describe new developments in transistor-resistor logical circuits; a new approach to the design of ferrocube cores for wide-band h.f. transformers; a three-watt tape amplifier circuit; and transistor circuits for magnetic matrix stores.

**SEMICONDUCTOR PACKAGES**

*Frenchtown Porcelain Co.*, Frenchtown, Pa. is offering its Bulletin 1060 free on request to its sales department. This bulletin contains information on tunnel diode enclosures and insulated stud-type diode mounts.

Included is data on two bodies: Amadox R 4462, and Body 787.

**ERA BOOKLET**

The Electronic Representatives Association, 600 So. Michigan Ave., Chicago 5, Ill. has published a brochure entitled "The Right Return," which describes some 15 current services and activities as well as future projects of the ERA.

The booklet is intended to aid ERA Chairman Joseph Marsey, and the various membership chairmen of ERA's 21 local chapters, in reaching their 1961

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goal of 825 members. The organization now has 752 member firms, which represents a growth from 1959's total of 624.

#### SERVICING DATA

*Supreme Publications*, 1760 Balsam Road, Highland Park, Ill. announces it is now maintaining a complete library and file of other publishers' material and factory data covering radio and TV sets of all makes.

Charges for the material range from 40 cents to \$1.00, depending on the number of pages involved. For additional information as to which schematics are available, write to the company. Give complete details on the make, model number, and year of the set in question.

#### TUBE DIRECTORY

*Metropolitan Supply Co.*, 1133 Broadway, New York 10, N.Y. is offering a complete directory of electron tubes, listed by tube number and followed by the firm's price. For a free copy, write to the company on your own letterhead.

#### THYRATRON BULLETINS

*CBS Electronics*, Information Services, 100 Endicott St., Danvers, Mass. has published two new bulletins in its "Tech Tip" series. Bulletin PA-223 is entitled "Thyratrons Are Different" and Bulletin PA-503, "The Care and Control of Thyratrons."

Both bulletins are available through the firm's distributors or from the manufacturer direct.

#### RELAYS CATALOGUE

*Potter & Brunfield*, Princeton, Indiana, announces a 16-page, 2-color catalogue showing its complete line of electro-magnetic relays. Forty-two different series of relays are described. They are divided into four major groups: telephone, military, power, and general purpose types.

Copies of the catalogue are available free from company sales representatives or from the manufacturer's Technical Information Center.

#### LOUDSPEAKER STANDARD

The American Standards Association, Dept. PR 198, 10 E. 40 St., New York 16, N.Y. is offering, at \$1.20 per copy, its new "IEC Publication 124: Recommendations for the Rated Impedances and Dimensions of Loudspeakers." This publication applies to single moving-coil (dynamic) loudspeakers of the direct-radiator type.

#### P-C RESISTORS

*Reon Resistor Corp.*, 155 Saw Mill River Rd., Yonkers, N.Y. is offering free a two-page bulletin describing a complete line of encapsulated printed-circuit type resistors. Write to the manufacturer, requesting Bulletin P-3-7/60.

#### SEMICONDUCTOR DIRECTORY

*Newark Electronic Corp.*, 223 W. Madison St., Chicago 6, Ill. has issued a 24-page industrial electronic parts directory, geared specifically to the

April, 1961

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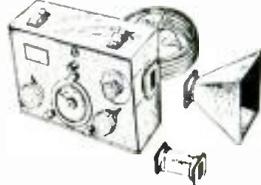


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Called "Semiconductor Directory No. 3," the publication lists the company's entire semiconductor stock.

### NBS MEASUREMENTS HANDBOOK

Boulder Laboratories, National Bureau of Standards, Boulder, Colorado has announced publication of a handbook on precision measurement. It consists of three volumes, totalling almost 3000 pages and includes information on the measurement of such quantities as electricity, heat, optics, and radiation. Material for a large section on electronics was furnished by the NBS Radio Standards Laboratory in Boulder.

Advance orders for these volumes may be placed now with the Chief, Special Service Section, United States Government Printing Office, P. O. Box 1533, Washington 13, D.C. The cost of each book is: Vol. I, "Electricity and Electronics," \$6.00; Vol. II, "Heat and Mechanics," \$6.75; Vol. III, "Optics, Metrology, and Radiation," \$7.00.

### AMP BULLETIN

AMP Incorporated, Harrisburg, Pa., has published a two-page product information bulletin (Series 701) to describe its line of high-voltage power supplies with output voltages of from 40 to 40,000 volts.

Specifications for a representative group of six of these power units are given. The data includes input, output,

ripple, regulation, temperature, size, weight, and special features.

### INSTRUMENT TUBES

CBS Electronics, 100 Endicott Street, Danvers, Mass. has announced the availability of an 8-page booklet which describes the uses and characteristics of a new line of special instrument tubes.

In addition to these ruggedized tubes, the brochure describes frame-grid tubes and a new secondary-emission tube.

For a free copy of this publication, write the manufacturer on your business letterhead and ask for Bulletin PA-391.

### NBS' SERVICES DATA

National Bureau of Standards has recently published a 5-page booklet entitled "Standard Frequencies and Time Signals from NBS Stations WWV and WWVH."

Publication 236 is available for 10 cents from Superintendent of Documents, U.S. Govt. Printing Office, Washington.

### WALSCO CATALOGUE

Walsco Electronics Mfg. Co., Rockford, Illinois has just published a 68-page guide to its service products for the electronic industry.

The catalogue contains complete descriptions of phono drives, exact replacement transformers, tools, chemicals, and electronic hardware. For a copy, write the company and ask for Catalogue FR-61-W.

There is always an avid audience on hand for each TV program scheduled for transmission in Nigeria. Here a group of friends and neighbors have gathered in anticipation of an evening's entertainment. Although there are only about 6000 TV sets in use, the actual viewing audience in the region may be on the order of 100,000 or more. It is not uncommon for crowds up to 100 to assemble before sets on display and family gatherings of 20 are commonplace in homes where TV is on. There are also "TV Shops" where the owner of the set makes a small charge for viewing. The government has arranged for its employees to obtain loans for the purchase of sets and many commercial firms in the area have similar arrangements. Some distributors also have easy-payment schemes. TV programs are transmitted for about five hours daily. This includes two hours of public-service material, of which one hour is devoted to special educational material. Programming is to be increased.



**Tape Recording in Industry**  
(Continued from page 64)

gages. The other two would simply be a repeat of the methods used for the first strain-gage channel. Often, because of brush noise or bounce in the slip-ring unit, the signal may be of such inferior quality that filtering and other methods may be needed to obtain any usable information. However, valuable information can usually be obtained except in cases of complete failure of the gages themselves.

Fig. 8C is an example of a photographic X-Y plot of the vibration channel. This is made in exactly the same manner as the strain-gage plots. Determining the frequency of the vibration points presents a much more complicated problem since vibration signals are usually a combination of many frequencies. It usually suffices to locate the frequency band in which most of the signal lies. This is accomplished with a variable bandpass filter by boxing in the point while a series of playbacks are made. In the majority of cases the energy will lie in a band of a few hundred cps. Occasionally, a predominant fundamental frequency will occur in a test which makes the job much easier since conventional means can be used to determine frequency.

Temperature and pressure signals are simple to reduce since they are taken directly from the FM channels and connected to the X-Y plotter. Once the input levels on the plotter are adjusted to the calibrate signals, it will trace out the information in one play of the tape. Figs. 8E and 8F illustrate what this information would look like. Note that compressor wheel rpm is used for the X axis in both cases.

At times it is useful to know the acceleration time for any point during the test run. The time-pulse generator would be used for this purpose by applying timing markers to the tape during the run. The timing mark would be placed on one channel of the dual-beam oscilloscope during the photographic plot for a ready timing reference.

Another feature of the tape recorder that is important in data reduction is the ability to slow down the tape speed in order to better examine fast time response information. In this case, frequency will be an even multiple of tape speed while the calibrate signal for amplitude will serve the same function as it would for the original recording speed. This technique is very useful in oscilloscope photography.

Thus we can see the large variety of information that can be gathered and reproduced by the instrumentation tape recorder. This data, once recorded, can be stored indefinitely and is a ready reference that can be called upon at any time to reproduce the original test conditions. Judging from recent improvements made in tape recorders, the surface would hardly seem to be scratched in producing new uses for this versatile machine.

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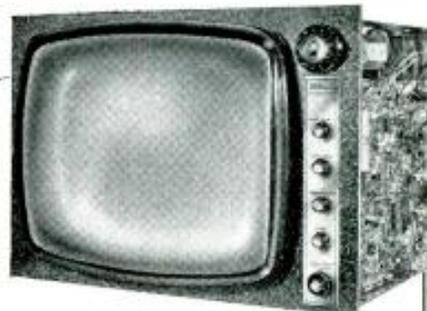
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## Mac's Service Shop (Continued from page 60)

monkey on a stick trying to locate the non-existent short circuit in his control cable," Mac agreed. "Probably he would finally decide it *had* to be inside the rotator and take it down. I should think changing rotators on a beam that size is a little different than changing rotators on a TV antenna."

"And you're so right! I knew better than try to do it myself or even with other ham help. Two antenna specialists used a sixteen-foot gin pole clamped to the telephone pole and carrying a block and tackle at the top. One guy worked on top of the pole, and the other stood on the ground and did the lifting and lowering of the beam with a long rope. Even so, I chewed my fingernails down to the first joint just watching them." "Well, the important thing is you finally whipped all your problems," Mac said with a sigh. "I wish I could say the same about my problems with printed circuits."

"What's wrong now? I thought you were getting pretty hot on the Tin-foil Terrors."

"Oh I'm getting better," Mac said defensively; "but lately I've run into a rash of printed circuit a.c.-d.c. sets with a most annoying form of intermittent. They develop noise along with changes in volume when they're in the cabinet;

but take that board out of the cabinet and the set may play all day without a bobble. Inside the cabinet, expansion produced by heat or mechanical stresses induced in the board by the supports cause the edges of a microscopic fracture of a printed lead to pull apart just enough to inject varying resistance, causing erratic performance.

"Not once have I been able to spot one of these tiny breaks with light shining through the board, with the illuminated magnifier, with the freon gas spray, with the heat lamp, or with any of the other dodges that are usually successful in pinpointing more clean-cut fractures. Tapping on the board or flexing it just *anywhere* will usually make a change in the noise level, but of course that is no help in isolating the break."

"So what system have you worked out to lick 'em?" Barney asked.

"Let's be accurate and say to *help* lick 'em," Mac answered with a wry smile. "First I know that printed leads are most likely to break around the edges of the board, in the vicinity of the tuning capacitor or the volume control, near any large heavy object mounted on the board, or close to support points. I concentrate on leads in these areas with a pair of sharp-pointed prods connected together with a test lead. While the noise is going or the volume is down, I span a considerable length of a suspected conductor with the prods. If this stops the noise or restores the volume, I move the leads closer together. The

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process is continued until I eventually have the poor connection bracketed between the test prods resting quite close together. Then I simply run solder along the lead between these final test prod positions. I don't even bother to try to see the tiny crack I know is there."

"I'd think it would be a little tricky being sure you didn't get those shorting prods across two separate conductors," Barney suggested.

"True, but then a good technician is always careful about where he touches his test prods. Experience has taught me a very high percentage of these troubles are caused by a break in the ground lead that runs around the edge of the board with conducting fingers going in to sockets and other ground potential points. Checking this lead out first, in the last three cases I've managed to run down the trouble and correct it in just over twenty minutes per set—which is about par for printed circuit intermittents in my book. The best part of this method is that when you can make the trouble go and come by bridging a section of a conductor with your probes, you're *sure* you've located the trouble—and that means a lot in time saved and peace of mind when working with intermittents."

"You can say that again!" Barney heartily agreed. "Working with intermittents is like spelling 'banana': the trick is to know when you're through. Bananananana—"

"Enough!" Mac interrupted. "I get the idea. And now that we've given our personal problems a good airing, let's get back to work. I'd like to take off a little early this evening and drive past a certain mushroom spot I know. If you think you can keep that big flannel Irish mouth of yours shut, you can go along."

Barney pressed his lips tightly together and made a sign of agreement as he grabbed up his solder gun. —30—

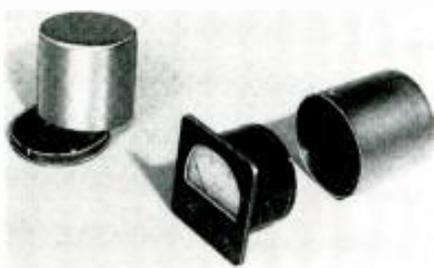
### METER SHIELDS FROM OLD SETS

By KENT A. MITCHELL, W3WTO

**DON'T** be in too great a hurry to turn down any offers of old radio sets made by your non-electronic-minded friends. Many old radios of the 1930's contain parts which are usable in unique applications.

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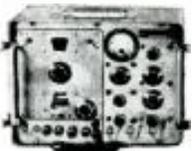
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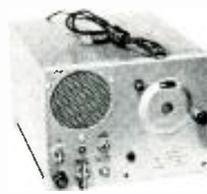
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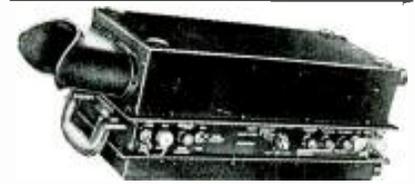
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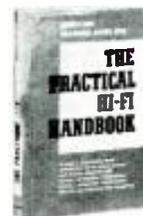
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**Stereo Dimension Control**

(Continued from page 57)

in many existing preamps and amplifiers. However, it suffers from two disadvantages. The bias voltages on the triodes change as  $R_1$  is varied, introducing possible distortion at some settings of the control. Also, the amount of increase in the difference signal is rather limited, being on the order of 1½ times. This may not be enough difference signal though it is sufficient for many applications.

**The Improved Circuit**

Figures 3 and 4 show a new circuit that can also accomplish this signal transfer.  $V_1$  and  $V_2$  are unity-gain phase inverters, sometimes called plate-followers.  $R_1$  and  $R_2$ ,  $R_3$  and  $R_4$  are adjusted so that the signal voltages at the plates are the same as at the respective input jacks. Both sections of the ganged pot have their center taps returned to ground. As the sliders move from ground, they pick up increasing amounts of either in-phase or out-of-phase signals, which are then combined through isolating resistors  $R_5$ ,  $R_6$ ,  $R_7$ , and  $R_8$  with the in-phase signal of the opposite channel. With the pots all the way to one side, complete blending is achieved and only the sum signals are available at both outputs. With the control all the way over to the other side, only the difference signals are available at both outputs. This produces a highly exaggerated separation effect as no center or sum signals are present. With the pots at their mid-positions, the outputs are strictly left and right signals at their respective outputs with neither blending nor more separation.

**Additional Benefits**

The modern stereo preamplifier is an extremely versatile instrument, capable of many more functions than are indicated by the necessarily limited nomenclature on its panel. Likewise, the separation ratio control in the hands of the knowledgeable audiophile will perform the following additional services: (1) cancellation of crosstalk in cartridge and/or amplifier; (2) electronic balance of preamps, amplifiers, and/or cartridges; and (3) an aid in setting up microphones for a stereo recording session.

Although the control can be very useful if used with discretion and understanding, it is not a cure-all. Just as you cannot make a grand piano out of a spinet, so a monophonic record must remain single-channeled. For monophonic program material the difference signal is zero, so that as you advance the separation control toward maximum separation the volume simply decreases to zero.

The control may be used to counteract crosstalk that occurs in other parts of the system, including preamps, power amplifiers, tape recorders, stereo cartridges, and even stereo cutting heads, for crosstalk simply means that a little

signal from one channel has leaked into the other. Crosstalk can therefore be cancelled by the introduction of a suitable amount of out-of-phase crosstalk which is, of course, exactly what this control does. It should be understood, however, that cartridge and amplifier crosstalk are not usually constant with frequency, so that it is difficult to get complete separation over the entire audio frequency range, though improvements of over 10 db in average crosstalk are quite possible. If further improvement is desired, capacitors can be added to the circuit so that the separation ratio becomes a function of frequency.

To adjust the control for minimum system crosstalk, readily available test records may be used in which only one channel of the cartridge is activated at a time. The control is then adjusted for minimum output in the opposite channel.

To electronically balance preamps and cartridges with the help of this control, simply rotate the control to the extreme separation position, play a monophonic record, and adjust the balance or channel-level controls until minimum sound is heard in the loudspeakers.

Stereo recording enthusiasts may wish to note that by rotating this control between its extremes, the sum and difference signals may be monitored and microphone levels and spacing adjusted to produce the optimum stereo separation ratio.

**Installation**

The stereo separation control, while primarily intended for inclusion in new equipment, may be readily installed and used in existing stereo systems. The circuit shown is useful at signal levels from .1 volt to 10 volts and so can handle most any signal level to be found in a stereo control system.

Those with tape-monitoring facilities in their preamps or control amplifiers, can easily install a stereo separation control by connecting their recorder output jacks to the separation control inputs and the control outputs to their monitoring input jacks. The tape-monitoring switch in this case serves as an on-off switch for the separation control. The circuit may also be easily inserted between a control preamplifier and its power amplifiers, but in either case, since the output impedance of the circuit is fairly high, the output lead lengths should be limited to a few feet.

If there is extra space on the preamp or control amplifier chassis, the stereo separation ratio control can be built right into such equipment. The lead going to the top of the volume control is removed and connected to one of the inputs of the control circuit. The output is then connected to the now empty volume control terminal.

While all the uses indicated previously add to the versatility of this type of control, its primary purpose is to make every home listener the final arbiter of stereo realism, and to substitute the muscles of thumb and forefinger for those of the back and arms when speakers must be moved about.

# ELECTRONIC CROSSWORDS

By BRUCE BALK

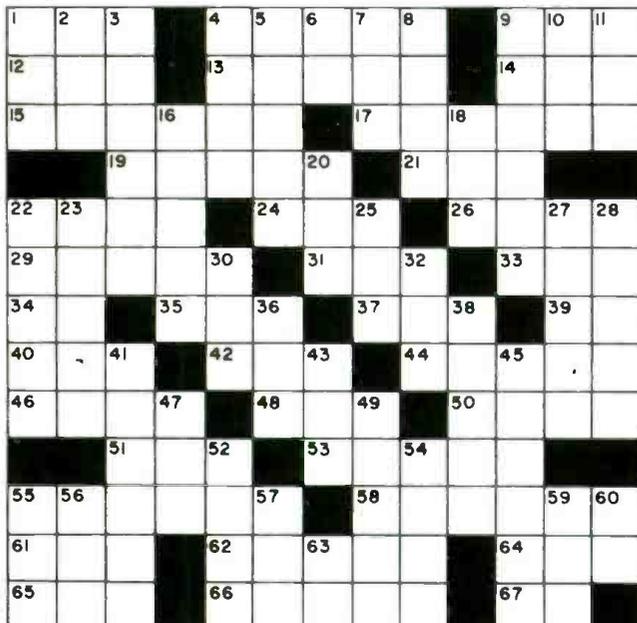
(Answer on page 127)

## ACROSS

1. Time standard (abbr.).
4. Phillips, Allen, for example.
9. Born (Fr.).
12. Describing coils without iron cores.
13. Small amount of coupling between two coils.
14. Voltage-resistance-current (abbr.).
15. Type of movable contact.
17. Crystal.
19. Authoritative instruction.
21. Youngster (slang).
22. Prevailing custom.
24. Radio receiver (colloq.).
26. It comes in "male" versions.
29. Large body of water.
31. Type of generator.
33. Greek letter.
34. Opposite of left (abbr.).
35. Plate current at resonance.
37. Animal foot.
39. You (Fr.).
40. Undermine.
42. Shelter.
44. Coaxial cables (colloq.).
46. Impetuous ardor.
48. Early transmitter.
50. Iranian (former abbr.).
51. Part of Morse Code.
53. 3000-30,000 mc. h.f. band.
55. Adjustable attenuator network.
58. Angle at which arc length is equal to radius.
61. Engineering society (abbr.).
62. Unit of equivalent absorption.
64. Resistance unit.
65. At the rate of.
66. Numerical value of orange in the color code.
67. "Legal Eagle" (abbr.).

## DOWN

1. Form of matter used in tubes.
2. One-thousandth of an inch.
3. A type of vacuum tube.
4. Snow vehicle.
5. Centers of coils.
6. An artificial language.
7. D.c. screen-grid voltage (symbol).
8. Frail.
9. Stylus.
10. Sea eagle.
11. It used to be RETMA.
16. Fear.
18. Type of mike worn on face.
20. Color code for two.
22. Inventor of the telegraph.
23. Tube base.
25. Peak.
27. Speak.
28. Flux density is measured in this unit.
30. Nothing.
32. Connection point made in body of resistor or coil.
36. Small, low-voltage incandescent lamp.
38. Rubbed lightly with a cloth.
41. Small capacitor in series with main capacitor.
43. Bitter vetch.
45. Time of cycle of an oscillating quantity.
47. Doze off.
49. Unit of radioactivity.
52. Examination.
54. Window glass.
55. Facial feature.
56. Exists.
57. Cheer.
59. Exclamation of surprise.
60. Southwestern state (abbr.).
63. Pertaining to Great Britain (abbr.).



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## Color TV Service Today

(Continued from page 31)

line. When this is done, slide the switch back to its "Normal" position.

The next step is vertical convergence, and for this a cross-hatch pattern is preferred. Since most dot generators also produce a cross-hatch, a flick of the instrument's switch is all that is necessary. Now the convergence-control board on the set is used. Normally, this is suspended at the back of the cabinet. Swing it up to the top of the cabinet, facing front (Fig. 6), so that you can make adjustments while watching the screen. The layout of controls on this board is shown in Fig. 7.

Adjust controls in accordance with the specific instructions in the service manual—but don't do any more than you have to. In effect, what you do is touch up, in tiny increments, only as many controls as necessary to get all the lines in the pattern sharp, untitled, and white, from top to bottom and from left to right. If you can do this by turning only two or three controls just a snip—as will often be the case—stop right there. You do not have to go through the business of turning every single control an appreciable amount just because the full procedure, in case it is needed, appears in the service manual. Furthermore, you will have to do less adjusting of whichever controls are involved. Nowadays there is less interaction between circuits (and controls) than there used to be. Back-and-forth time is reduced or eliminated.

This simplification in adjustment procedure over what was required a few years ago is not due to the increased use of multi-function tubes, but to an honest saving in circuitry. Compared to a 525-watt dissipating 1955 RCA color chassis draws only 330 watts. The 1955 set had red, blue, and green adder circuits (and tubes); the new sets do not. Instead they use X and Z demodulation directly into a R-Y, G-Y, and B-Y amplifier matrix (Fig. 8) such as has been used in recent years. No d.c. restorers either, with this matrix system. However this simplification in circuitry, like the reduction from five picture i.f. amplifiers to three and from two audio amplifiers to one is not that new; it has been in effect for the past four years. What is new is the constant improvement in circuit parameters to make the individual circuits more stable—less critical. This is what makes the service technician's job simpler and more predictable.

Another interesting touch that makes the service technician's life a little easier on the new sets is a circuit breaker whose re-set button is accessible at the rear of the chassis. This replaces the fuse in the "B+" power supply which formerly blew with momentary overloads and, in addition, protects the high-voltage circuits. It is now anticipated that the service technician will not be called as often for nuisance

fuse replacements as was formerly the case.

How about receiver service? The major trouble will continue to be faulty tubes, as is the case in black-and-white sets. This is especially true in color sets because all manufacturers use high-grade, industrial type components in all critical areas in the color set. Printed-wiring boards and transformer power supplies are used in all chassis. The new RCA chassis use a nuvistor r.f. amplifier in the tuner. Limited use of this new type vacuum tube has indicated that long life can be expected of it. This is true because of its rugged construction and also because of the lower operating voltages fed to the nuvistor. It also serves the purpose of increasing the sensitivity of the tuner, making the antenna less of a problem. In most cases now, the antenna already in use for the black-and-white set in the home will be good enough for color.

To anyone who has used a scope and sweep generator for monochrome TV alignment, the instructions for color-circuit alignment will be very familiar. The only additional circuitry to be considered includes the chroma bandpass, phasing, and demodulator circuits. All that can be said here is follow the instructions in the service manual and be certain that your scope and generators are accurately calibrated. As a practical note, however, you can be sure that you will be called upon to align these circuits about as often as you do a complete alignment of the typical mono-

chrome receiver. Try not to get rusty and, as a mental exercise, read over the instructions in the manuals for the new color receivers.

It has not been our intention here to close our eyes to the facts or sell a bill of goods: We do not say that color sets are so easy to service that any fool can handle the job. The technician who has had no practical experience at all in this direction will not look like a great authority on his first two or three jobs—although he might, depending on what has gone wrong. He may be able to replace a faulty tube with as much flair as he does on any other set. However, there is much less to worry over in the newer color sets than in the earlier models. The color-channel circuitry has reached much the same level of stability and reliability as the old-fashioned video and sound channels. Most important, the increasing number of sets reaching homes and the already developing service-seeking patterns of the owners make it likely that, at long last, the independent technician is in the picture.

Another factor, not yet mentioned, is the imminent entry of Japanese electronic fabricators into the U.S. color TV market. Sets shown so far are similar to those already made in this country. If the merchandising and pricing methods that have made Japanese transistor radios such a great success here carry over into color TV, the market will swell still more. And there will be few people to service these imported sets aside from independent dealers.

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1A7CT	3CB6	5Y8	6AV5CT	6BS8	6DE6	6SH7	7B6	12AQ5	12F5	25Z6GT
1B3CT	3Q4	5Y3	6AV6	6D6GT	6D6GT	6S7	7B7	12AT6	12H6	27
1H5CT	354	6A6	6AW8	6BZ6	6DF6	6SK7	7B8	12AT7	12K5	35A5
1L4	3V4	6AB4	6AX4CT	6BZ7	6E5	6SL7	7C4	12A06	12K7	35B5
1L6	4BQ7A	6AF4	6AX5CT	6C4	6F6	6S7	7C5	12A07	35C5	35C5
1N5CT	4B5B	6AG5	6B8	6C8A	6F5	6SR7	7C6	12AV6	12Q7	35W4
1R5	4BZ7	6AH4CT	6B8	6CB6	6H6	6T4	7C7	12AV7	12R5	35Z5
1S5	4CB6	6AM6	6B8	6CB6	6J4	6T8	7C8	12AX4CT	12S7	36
1T4	5AMB	6AK5	6B8	6CC7	6J5	6U5	7E6	12AX7	12S7	38
1U4	5ANB	6AL5	6B8	6CC8	6J7	6U8	7E7	12A27	12S7	39/44
1U5	5AT8	6AM8	6B8	6CC8	6J7	6V6CT	7F7	12A7	12S7GCT	41
1V2	5AV8	6AN8	6B8	6CM8	6K6CT	6WG6T	7F8	12BA6	12S7	42
1X2	5AZ4	6AQ5	6B8	6CL6	6K7	6X4	7F8	12BA7	12V6CT	43
2A4	5BR8	6AQ6	6B8	6CM6	6N7	6X5CT	7H7	12B6	12W6CT	50B5
2B4	5CC8	6AQ7	6B8	6CM7	6O7	6X7	7H7	12B6	12X4	50A5
2C75	5J6	6AR5	6B8	6CN7	6Q7	6Y6	7Q7	12RF6	14A7/12B7	50C5
3A5	5R4	6AS5	6B8	6CQ8	6R5	6Z4	7A4/XXL	12B7	14B5	50L6
3AL5	5Y8	6AT6	6B8	6CQ8	6S7	6Z4	7A6	12B7	14B5	56
3AU6	5U4	6AU6	6B8	6CS7	6SD7CT	7A7	7Y4	12B7	19A04CT	80
3BC5	5B8	6AU6CT	6B8	6CUS	6SF5	7A8	7Z4	12B7	19R6CT	84/624
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## Adjusting Transmitters

(Continued from page 45)

aid of an r.f. output indicator is quite similar to that described previously. The coupling is increased to a point at which an output indication can be obtained. The antenna trimmer is adjusted for maximum reading on the r.f. indicator. The plate tank is then tuned for a plate current dip (minimum). Coupling is increased until maximum r.f. output is indicated. It should be noted that maximum r.f. output does not necessarily follow maximum coupling but may occur at some point below maximum coupling. The coils are over-coupled when the antenna trimmer cannot be peaked (assuming that the antenna can be peaked at reduced coupling). It should also be noted that in some transmitters maximum power output occurs at some value less than maximum rated plate current. Under no circumstances should the transmitter be operated with higher than maximum rated-power amplifier plate current. According to FCC regulations, the power input should not exceed the rated value for a particular transmitter by more than 10%.

A final frequency check is now advisable. In the case of the 25 to 50 mc. transmitter just described, the frequency tolerance is 0.002%. Make certain that the frequency meter that you use has an accuracy substantially better than this figure. Use the crystal oscillator trimmer capacitor to set the transmitter on its exact assigned frequency.

## Modulation

In the previous paragraphs we discussed the proper tuning of the r.f. section of the transmitter, the special care required to provide the proper power input, and the correct operating wavelengths. The third factor with which the FCC is greatly concerned is the modulation level. The modulation level of the Motorola transmitter is a function of the operation of the transmitter's limiter circuit and the setting of the IDC control. This control regulates the amplitude of the modulating signal supplied to the grid of the phase modulator.

The function of the clipper stage is to "clip" off the sharp audio peaks that rise above the general level of the audio frequencies. The clipper, however, must not clip too sharply or distortion of the voice frequencies will result and spurious frequency components may be radiated by the transmitter. If the IDC control is set too high too much audio will be fed to the modulator, consequently there will be too severe clipping of the voice signals and possibly distortion. If the IDC control is set too low there will be insufficient audio power for proper modulation.

In summary, the over-all objectives of the adjustment of transmitter modulation is to keep the transmission within the frequency deviation limits required by the FCC, to obtain efficient peak clipping to prevent overmodulation, and at the same time to maintain a reason-

ably high average modulation percentage.

## Checking Frequency Deviation

An oscilloscope is most useful in the adjustment of modulation because it permits visual observation of peak clipping and the audio signal before clipping.

To check actual signal frequency deviation of the transmitter under broadcasting conditions an FM deviation meter can be used. An FM deviation meter is an FM receiver that is accurately tuned to the transmitting frequency, and contains a calibrated meter that reads peak detector-voltage output. As will be recalled, a fixed frequency, i.e., an unmodulated FM carrier signal produces no output voltage at an FM detector. Detector output voltage is developed only when the FM signal deviates from its base frequency. By proper design, it is possible to calibrate the forementioned output meter so that it reads directly in kc. deviation. Fig. 3 is a functional block diagram of this type of deviation meter while Fig. 4 is the circuit diagram of the transistorized peak-reading voltmeter used in the Gertsch deviation meter.

The Gertsch Peak Modulation Deviation Meter, Model DM-3, illustrated in Fig. 5, is typical of deviation meters of this type. This is the way it may be used.

The meter (antenna connected) is turned on and set to transmitter frequency. The switch to the left of the meter is turned to the position marked "Limiter Current." The transmitter is turned on and keyed, that is to say, the press-to-talk button is depressed, but no sound is applied to the mike. The transmitter now produces a fixed signal. The meter needle should now be exactly on 5—"Limiter Current" position. If not, move the deviation meter closer or farther away from the transmitting antenna.

The left-hand switch is now turned to "Frequency Set." The meter needle should remain exactly at the same point. If the needle is above or below 5 on the meter, the frequency control on the local oscillator (not the transmitter) should be adjusted until the needle is on 5. The left-hand switch is now moved to "Zero." The zero-set control to the right of the meter is used to set the needle to zero. The "Deviation Range" toggle switch is set to the desired range.

With the transmitter still keyed, the microphone is excited with audio of good amplitude. (A healthy, sustained "Ahhh" will do it.) Now, while "ahh-ing," the IDC control is adjusted until the desired deviation is secured. This figure will be indicated on the meter scale directly in kilocycles.

It should be noted that the FCC has ruled that all new mobile equipment be limited to "narrow-band" transmission, which is  $\pm 5$  kc. of the assigned frequency. Existing equipment may be operated at the bandwidth that was originally granted. However, should a new frequency be desired, or should a new license be required, the new narrow-band rule must be obeyed. —50—

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## Making Electronic Colors

(Continued from page 43)

determine the relative intensities with which the correspondingly struck "dots" of phosphor will glow. White light is produced by a correctly proportioned mixture of red, blue, and green light. As shown in Fig. 1 (lower, right-hand corner), this means that all three guns are "on" for white.

Fig. 1 will serve to identify the color blocks that make up the cover background. It also gives some idea as to which primaries are used to obtain basic color combinations. In each color block, the guns that must be "on" to obtain that color are indicated by white circles. However, there is no indication of the relative beam intensity required from the "on" guns. The importance of intensity can be demonstrated in the following way: To represent a neutral shade of gray, the relative intensity of each gun with respect to the others would be the same as it is for white, with all three guns on. However, the absolute intensity of all guns would be reduced, in the same proportion. Finally, if all guns are cut off, we have the absence of light. This is black, as shown in the lower, left-hand corner of Fig. 1. The guns that must be "on" or "off" for other colors shown on the cover are also indicated here.

Unless the naked eye is extremely

close to the viewing screen of the picture tube, it cannot see the individual color dots; the latter tend rather to blend together to produce the effects desired. A notion of their size can be obtained by noting that there are approximately 1 million individual phosphor dots serving as colored-light sources on the face of the current color CRT, the 21CYP22A—about 333,000 dots for each primary.

The generator being used by the technician on the cover, shown more clearly in Fig. 3, has already been identified as the RCA WR-64A. It is a crystal-controlled source that combines the functions of a color-bar generator with those of a dot-and-cross-hatch generator. Dot and cross-hatch outputs provide monochrome patterns that are important in making critical convergence adjustments on color sets (see "Color TV Service Today," page 29), but are also useful for linearity adjustment on all types of TV receivers.

The color-signal output consists of ten separately identified and accurately controlled color bars, ranging from yellow-orange on the extreme left and proceeding through orange, red, magenta, reddish-blue, blue, greenish-blue, cyan, bluish-green, and green at the extreme right. The man on the cover is getting correct color balance, but the receiver is adjusted for somewhat excessive width. As a result, he is pushing color bars at either extreme of the display off the sides of the CRT screen. —30—

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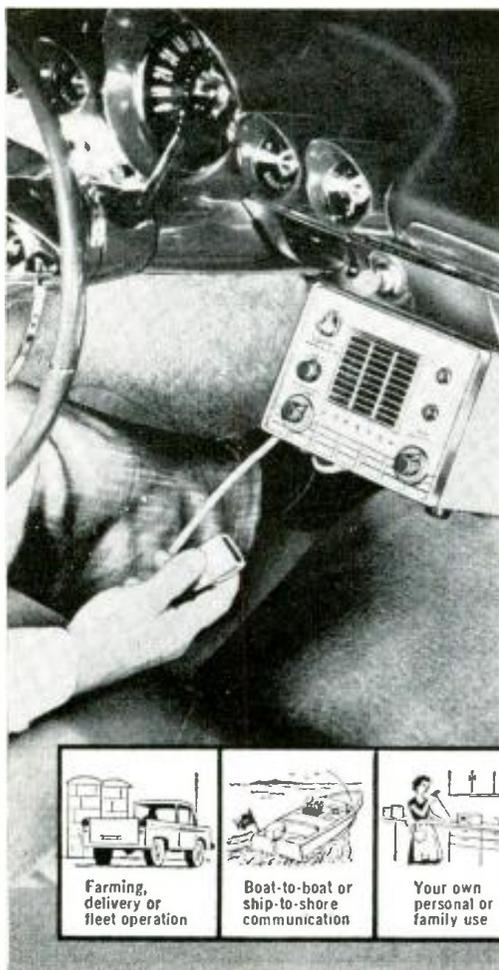
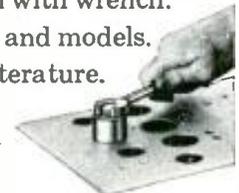
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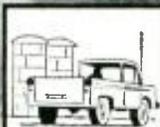
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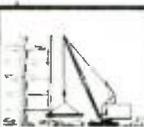
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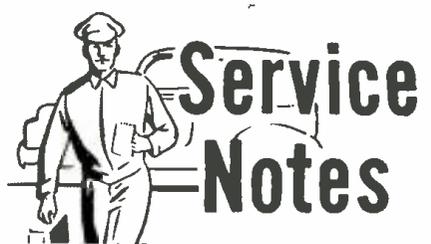
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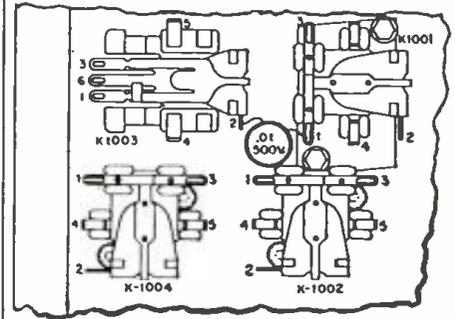


# Service Notes

## RCA TV: REMOTE PROBLEMS

RCA sends these tips along. CTP7A remote receiver; motor reverse relay chatters when actuated. Try connecting a .01- $\mu$ f., 500-volt capacitor between terminal 1 of the motor reverse relay (K1001) and terminal 2 of the channel relay (K1003). See Figs. 1A and 1B.

CTP7A and CTP9A are remote-control receivers used in black-and-white and color-TV sets. When the TV receiver changes stations in response to a remote-control signal calling for a



(A)

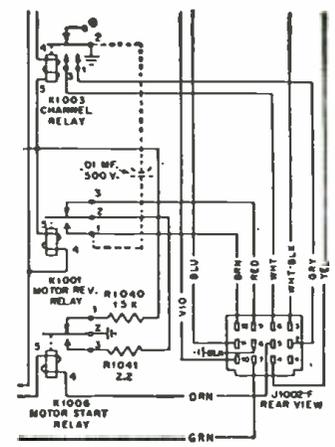


Fig. 1 (B)

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change in volume, or responds in some other erratic and incorrect way, the cause of the trouble may be that the relay contacts are faulty. Actual relay contact is made by small points that are welded to the leaves of the relays. When these points loosen or separate from the leaf of the switch, erratic signal response results.

CTP7, 8, and 9; the remote control will actuate the receiver only when brought close to the TV receiver. This may be due to a loose tube shield on the 12AX7 (V1001) used in the remote-control receiver. When this shield is improperly grounded, it picks up random signals and noise causing a high bias

level which, of course, reduces the remote-control receiver sensitivity.

When the channel selector on a remotely controlled receiver is jammed, do not try to force the selector free or damage may result. Jamming may have been caused by the station selector having moved of its own accord into the engaged position. This may have happened during shipment or storage when the receiver was placed on its side. To clear, use the remote control to actuate the motor and disengage the shaft from the gear box.

**G-E: NO REMOTE CONTROL**

No change in volume level in response to control signal. Check possibility of

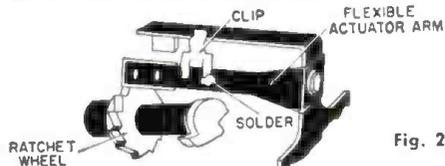


Fig. 2

the stepping relay in the remote receiver being stuck. To do this it is necessary to open the remote receiver chassis and inspect the relay and its ratchet wheel. If the flexible arm (Fig. 2) is jammed, move it gently back to its normal position. To prevent this trouble from repeating, solder a small clip on the arm as indicated in Fig. 2. Later runs of these sets have this modification incorporated.

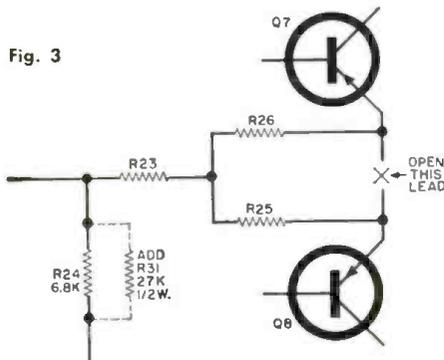
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Fig. 3



soldered, and then reconnected to their individual transistors. See Fig. 3. -30-

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Hallicrafters Co., 4401 W. Fifth Ave., Chicago 24, Ill. has announced its Model



S-120, a new short-wave receiver featuring three antennas, an adjustable b.f.o. on the front panel, and compact, slim-line styling. The set includes a built-in ferrite loop antenna for the standard broadcast band, and a collapsible whip antenna for s.w., as well as the normal connections for an external wire antenna. Its three s.w. bands cover the range from 1600 kc. to 30 mc.

Controls include: band selector, main tuning, bandspread tuning, standby/receive, b.f.o./selectivity, a.c. on/off and volume. According to the company, the S-120 is a "step-up version" of the manufacturer's Model S-38E, still in production.

### MOBILE RECEIVER

Autovox Corp. of America, 250 W. 57 St., New York 19, N.Y. has introduced the "Transmobil," an 8-transistor receiver for standard broadcasts and international short-wave bands.

The set can be used in cars, boats, in the home, or as a portable. It may be operated from an engine battery—6 or 12 volts—or on four regular or mercury penlite cells. Engineered in Europe, the set is claimed to be a "truly universal radio."

### MINIATURE TRANSCEIVERS

Seiscor Div., Seismograph Service Corp., Box 1590, Tulsa, Oklahoma has introduced two transistorized transceivers for use on CB frequencies. One is the "Telepath" Model PM-A, which uses a combination speaker/microphone, telescoping antenna, and weighs only 12½ ounces with standard 9-volt battery. Its range is given as ½ mile or better, depending on the surrounding area. Standard units operate on a frequency of 27.085 mc. Other frequencies between 27 mc. and 27.255 mc. are also available.

The second of the new units is the "Telepath" Model SC-A, a portable miniature base-station transceiver, said to make a perfect mate for the pocket-

model PM-A as well as for other "Telepath" industrial two-way models. The SC-A has a range of one mile or better. Choice of power supply is optional including a variety of batteries, line voltage, or low d.c. supplies. The transmitter has a full 100 mw. input to the r.f. amplifier.

The unit is available for operation on any single channel between 20-55 mc., with no license required for 27-mc. operation when the attached telescoping antenna is used. The receiver is a crystal-controlled type with a built-in PM speaker. For more information, contact the manufacturer.

### NEW CB UNITS

Lafayette Radio, 165-08 Liberty Ave., Jamaica 33, N.Y. has announced two new Citizens Band transceivers. Shown here is Model HE-20, described as a "no compromise" unit. Featured are a 5-watt-input crystal-controlled transmitter and a superheterodyne receiver. The transmitter may be operated on any four of 23 channels; the receiver has four crystal-controlled channels and is tunable over all 23 channels, with a



sensitivity of 1 μv. The unit has a built-in squelch and series-gate noise limiter. An "S" meter, switched, measures incoming signal strength and final amplifier wattage. Push-to-talk operation is used.

A more economical model is the HE-29, a portable set with a range from 1.5 to 7 miles, depending on terrain and conditions. This pocket-size instrument uses two controls, a telescoping antenna, and a built-in speaker that doubles as a microphone when transmitting.

### HAM POWER SUPPLY

Heath Co., Benton Harbor, Mich. has introduced its new Model HP-20 power supply which furnishes filament, plate, and bias voltages for converting Heath-kit "Comanche" and "Cheyenne" or other mobile amateur gear to fixed station operation. The HP-20 delivers 6.3 volts a.c. at 8 amps. or 12.6 volts a.c. at 4 amps for filaments; and 120 watt ICAS d.c. plate power of 500 volts d.c. at

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6AW8	.89	6SQ7	.73	12CU6	1.06
6AX4	.65	6T4	.99	12CX6	.54
6AX7	.64	6U8	.78	12D85	.69
6BA6	.49	6V6GT	.54	12DE8	.75
6BC5	.54	6W4	.54	12DL8	.85
6BC7	.94	6W6	.69	12DM7	.67
6BC8	.97	6X4	.39	12DQ6	1.04
6BD6	.51	6X5GT	.53	12DS7	.79
6BE6	.55	6X8	.77	12DZ6	.56
6BF6	.44	7AU7	.61	12EL6	.50
6BG6	1.66	7A8	.68	12EG6	.54
6BH6	.65	7B6	.69	12EZ6	.53

6BH8	.87	7Y4	.69	12F8	.66
6BJ6	.62	8AU8	.83	12FM6	.45
6BK7	.85	8AW8	.93	12K5	.65
6BL7	1.00	8BQ5	.60	12SA7M	.86
6BN4	.57	8CG7	.62	12SK7GT	.74
6BN6	.74	8CM7	.68	12SN7	.67
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6BQ6GT	1.05	8CX8	.93	12U7	.62
6BQ7	.95	8EB8	.94	12V6GT	.53
6BR8	.78	11CY7	.75	12W6	.69
6BU8	.70	12A4	.60	12X4	.38
6BY6	.54	12AB5	.55	17AX4	.67
6BZ6	.54	12AC6	.49	17BQ6	1.09
6BZ7	.97	12AD6	.57	17C5	.58
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5CG8	.76

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6AT8	.79
6AU4	.82
6AU6	.50

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6DG6	.59
6DQ6	1.10
6DT5	.76
6DT6	.53
6EU8	.79
6EA8	.79
6H6GT	.58
6J5GT	.51
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6K6	.63
6S4	.48
6SA7GT	.76

Qty. Type	Price
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12AX7	.63
12AZ7	.86
12B4	.63
12BA6	.50
12BD6	.50
12BE6	.53
12BF6	.44
12BH7	.73
12BL6	.56
12BQ6	1.06
12BY7	.74
12BZ7	.75
12C5	.56

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25L6	.57
25W4	.68
25Z6	.66
35C5	.51
35L6	.57
35W4	.52
35Z5GT	.60
50B5	.60
50C5	.53
50DC4	.37
50EH5	.55
50L6	.61
117Z3	.61



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200 ma., or 600 volts d.c. at 150 ma. and 300 volts d.c. at 100 ma. A separate bias supply furnishes 130 volts d.c. at 30 ma.

Designed to be built in one evening, the HP-20 kit can power SSB and c.w. transmitters requiring fixed bias for linear stages or grid-lock keying. The a.c. ripple is said to be less than 1 percent.

## TWO-WAY BUSINESS RADIO

Hammarlund Manufacturing Co., Inc., 460 W. 34 St., New York 1, N.Y. has announced what it calls the first, full-powered, business two-way radio system in a low-cost, versatile unit. Com-



pletely self-contained, the "Outercom" is a transceiver for use on 6- or 12-volts d.c. or 117-volts a.c.

The same basic unit may be switched around, from vehicle-to-vehicle or vehicle-to-office by minor re-connections made by the user. Complete details are available from the manufacturer.

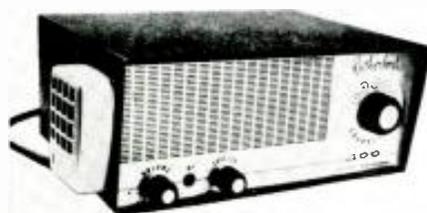
## CB TOWER ANTENNA

Mark Mobile, Inc., 6441 W. Fargo Ave., Skokie, Ill. has introduced its Model C.S.M.-11 antenna, designed exclusively for 27-mc. class D Citizens Band commercial system applications. It is said to enable the licensee to gain substantially greater and more reliable coverage while complying fully with FCC regulations.

The new antenna is designed for convenient side-mounting on existing or proposed TV, broadcast, or communications towers. It may be used in a single-bay or in stacked versions. Full information is available from the manufacturer.

## CB RADIOPHONE

Rutherford Electronics, 8930 Lindblade St., Culver City, Calif. announces its new Model R-400 Citizens Band radiophone. The receiver features three



stages of amplification, automatic noise limiting, and adjustable squelch. The transmitter and receiver use six crystal-controlled channels, with an illuminated dial indicating which channel is in use.

A removable microphone with press-to-talk switch operates the transmitter.

The set may be operated from 6- or 12-volts d.c. or 117-volts a.c.

## METER FOR CB USE

Crown Electric Products Co., P.O. Box 171, Orange, N.J. has announced a new "power output and modulation indicator" for use with Citizens Band transmitters.

Two models are available. One, the Model LS, gives the user a continuous indication of his set's power output and modulation. The other, Model TS, is similar except that it is used to check the set without its being on the air. The Model TS comes with a 50-ohm built-in dummy antenna. An accessory test cable, for connecting the set to the test meter, is also available.

## FM MOBILE FILTERS

Collins Radio Co., Western Div., 2700 W. Olive Ave., Burbank, Calif. has announced two new mechanical filters designed for FM mobile radio equipment. One, the Model F455YA-120, has a 45.5 kc. center frequency and a passband of 12 kc. With it, FM mobile receivers can be designed to match systems using the  $\pm 5$  kc. transmitter deviation specified under the FCC split-channel ruling.

The other filter, Model F455YA-320, has a 32-ke. bandpass and is suited for wideband mobile equipment applications.

## AIRCRAFT COMMUNICATOR

Gonset Div., Young Spring & Wire Corp., Burbank, Calif. has announced a new communications unit designed for use by airport ground vehicles, flying



schools, fixed-base operators, and in Unicom applications. It offers relatively high power output for two-way communications in the 108- to 136-mc. aircraft band in a completely self-contained package.

Designated Model G-150, it is available in 6-, 12-, or 28-volt d.c. or 117-volt a.c. versions. Transmit and receive frequencies are crystal-controlled. No external tuning is required. Complete technical data is available from the manufacturer.

## COMPACT CB TRANSCEIVER

Sonar Radio Corp., 3050 W. 21 St., Brooklyn 24, N.Y. has introduced a compact, battery-operated CB transceiver that may be held in the hand.

Named the "Sonarcom," the two-way set uses a crystal-controlled transmitter and receiver and has been designed to suit the industrial market where two-way communication can facilitate the

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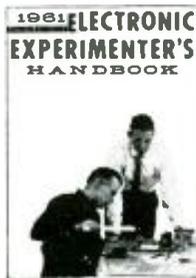
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### "ON CALL" SYSTEM

General Electric Company's Communication Products Dept., Lynchburg, Va. reports that a base-station transceiver, linked by a network of personal portable receivers, has helped personnel at Ormond Beach Hospital, Florida to make better use of their "on-call" time and still maintain instant contact with the hospital.

Personnel carry the lightweight voice communications receivers which receive messages from the transceiver at the hospital. To return the call, the staff member then telephones in, although staff physicians have standard two-way sets installed in their cars. The same hospital base-station transmitter is used for the vehicular network. —30—

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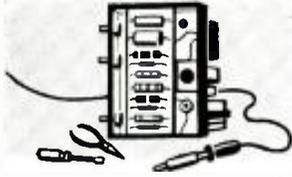


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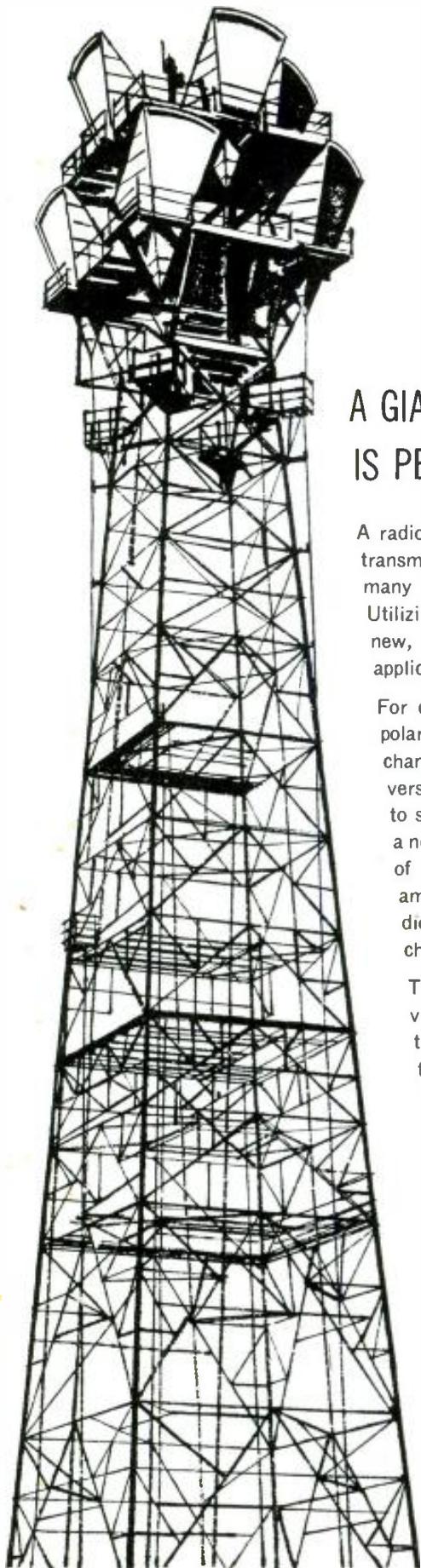
## INDEX OF

# Advertisers

APRIL  
1961

ADVERTISER	PAGE NO.	ADVERTISER	PAGE NO.
Airex Radio Corporation	122	Key Electronics Company	111
Allied Radio	7, 90, 91	Kuhn Electronics, Inc.	66
Almo Radio Co.	130	Lafayette Radio	97
Amperex Electronic Corp.	71	Lampkin Laboratories, Inc.	104
Ashe Radio Co., Walter	112	Lektron	108
Audio Unlimited	122	McGee Radio Co.	92
Audion	118	Mark Mobile, Inc.	98
B & K Manufacturing Co.	13	Milwaukee School of Engineering	95
Baltimore Technical Institute	118	Moog Co., R. A.	126
Barry Electronics Corp.	116	Moss Electronic, Inc.	100, 101
Bell Telephone Laboratories	Third Cover	National Radio Institute	1
Bogen-Presto	98, 99	National Technical Schools	21
British Industries Corp.	120	Nortronic Company, Inc., The	85
Browning	118	Oelrich Publications	99
Burstein-Applebee Company	123	Ohmatsu Electric Co. Ltd.	71
C & H Sales Co.	110	Olson Electronics	113
Cagan Sales, R. C.	111	Pacific International College of Arts & Sciences	116
Capitol Radio Engineering Institute, The	23	Paco Electronics Co., Inc.	10, 11
Candee Co., J. J.	126	Peak Electronics Company	82
Carston	70	Philco Technological Center	93
Center Industrial Electronics, Inc.	70	Picture Tube Outlet	120
Channel Master Corp.	73, 99	Quietrol Company	119
Chemical Electronic Engineering, Inc.	95	RCA Electron Tube Division	109
Cleveland Institute of Electronics	5	RCA Institutes, Inc.	14, 15
Columbia Electronics	124	R W Electronics	122
Commissioned Electronics Co.	93	Rad-Tel Tube Co.	125
Coyne Electrical School	74, 86	Radio Corporation of America	Fourth Cover
DeVry Technical Institute	16, 17, 18, 19	Radio-Television Training School	9
Dressner	118	Raytheon Company	105
Editors & Engineers, Ltd.	118	Reeves Soundcraft Corp.	84
EICO	27, 28, 117	Rek-O-Kut Company, Inc.	12
Electro-Voice, Inc.	25	Rider Publisher, Inc., John F.	93
Electronic Chemical Corp.	102	Sams & Co., Inc., Howard W.	88, 89
Electronic Book Service	114, 115	Schober Organ Corp., The	68
Fair Radio Sales	122	Scott Inc., H. H.	69
Fisher Radio Corp.	6	Sencore	67
G & G Radio Supply Co.	128	Shure Brothers, Inc.	70
General Electric Company	65	Sonar Electronic Tube Co.	96
General Radio & Telephone Company	106	Sonotone Corp.	83
Globe Electronics	102	Sprague Products Co.	26
Goodheart Co., R. E.	113	Superscope, Inc.	8
Grantham School of Electronics	3	Supreme Publications	103
Greenlee Tool Co.	121	Sylvania Electric Products, Inc.	Second Cover
Grylock Electronics	116	TAB	102
Hallicrafters	66	Texas Crystals	124
Harman-Kardon, Inc.	107	Transvision	111
Heath Company	78, 79, 80, 81	Tri-State College	70
Henshaw Radio Supply	99	Tube-a-Rama	119
Holt, Rinehart and Winston, Inc.	20, 72	U.S. Crystals, Inc.	92
Hy-Gain Antenna Products	84	U.S. #1 Electronics	112
Indiana Home Study Institute, The	94	University Loudspeakers, Inc.	87
Indiana Technical College	111	Valparaiso Technical Institute	96
International Radio & Electronics Corp.	86	Warren Dist. Co.	120
Jerrold Electronics Corporation	4	Webster Productomatic Corporation	104
Johnson Co., E. F.	121	Weller Electric Corp.	22
		Winegard	75, 127

Printed in U.S.A.



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For example, they arranged for the waves in adjacent channels to be polarized 90 degrees apart, thus cutting down interference between channels and permitting the transmission of many more telephone conversations in the same frequency space. They developed ferrite isolators to suppress interfering wave reflections in the waveguide circuits; and a new traveling wave tube that has ten times the power handling capacity of previous amplifiers and provides uniform and almost distortionless amplification of FM signals. They devised and applied a new high-speed diode switching system which instantly switches service to a protection channel when trouble threatens.

To transmit and receive the waves, the engineers applied their invention, the horn-reflector antenna. Elsewhere, this versatile antenna type is brilliantly aiding space communication research in the reception of radio signals from satellites. For radio relay, a single horn-reflector antenna can efficiently handle both polarizations of the 6000 megacycle waves of the new system; at the same time it can handle 4000 and 11,000 megacycle waves used for existing radio relay systems. Thus it enables all three systems to share economically the same radio towers and routes.

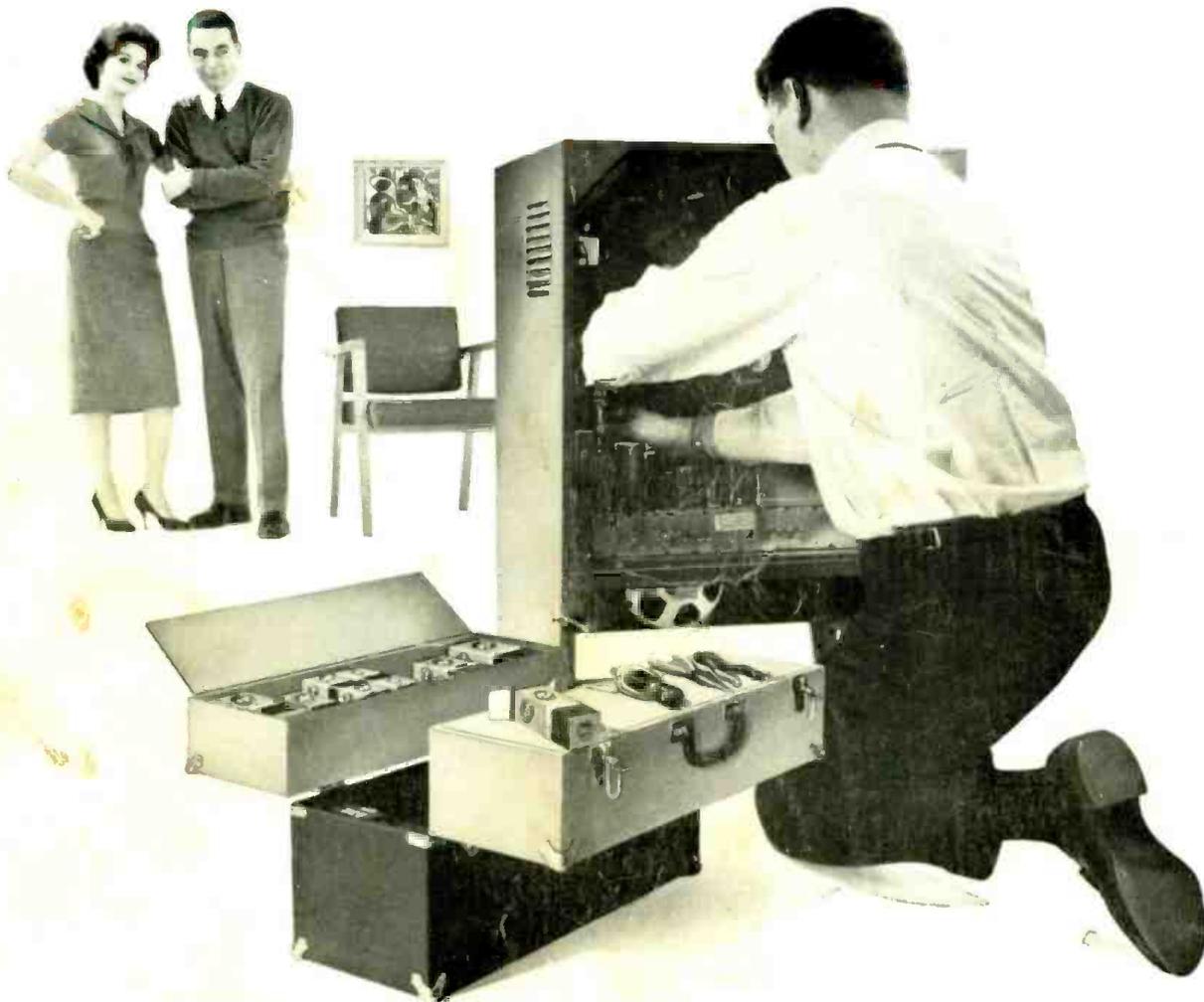
Produced by the Bell System's manufacturing unit, Western Electric, the new system is now in operation between Denver and Salt Lake City, and will gradually be extended from coast to coast. This new advance in radio technology is another example of how Bell Telephone Laboratories works to improve your Bell communication services.



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