

# Electronics World

APRIL, 1970  
60 CENTS

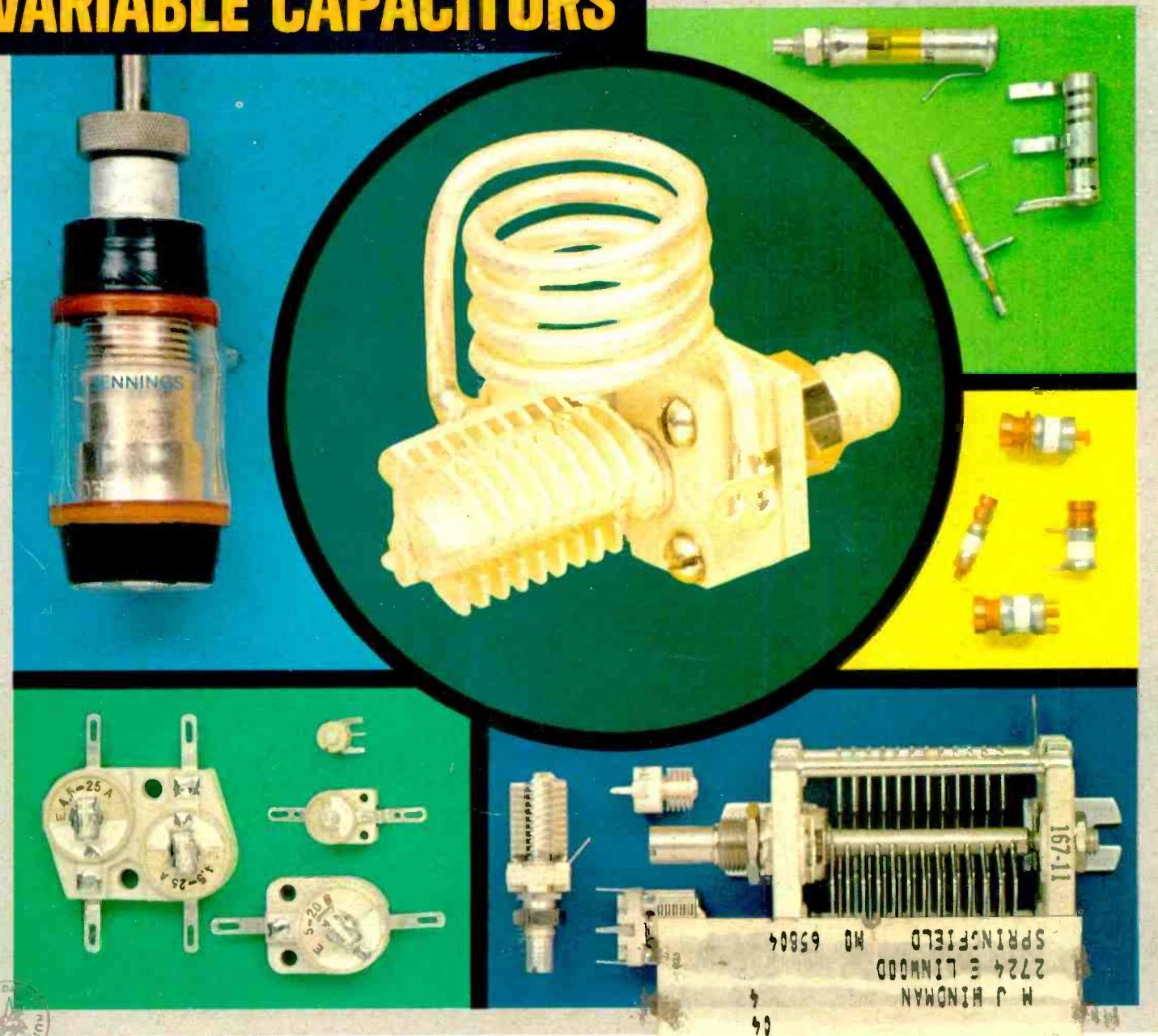
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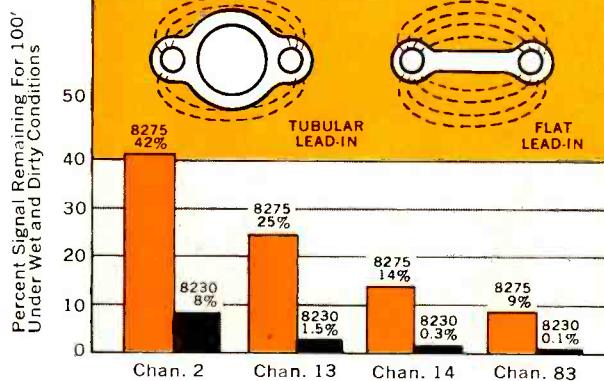
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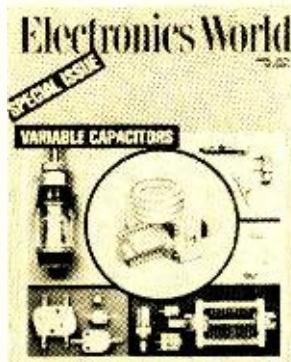
CIRCLE NO. 131 ON READER SERVICE CARD

# Electronics World

APRIL 1970

VOL. 83 NO. 4

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THIS MONTH'S COVER shows variable capacitors used for tuning and trimming. The enlarged tuned circuit in the circle, from E. F. Johnson Co., consists of a milled-plate air-dielectric variable capacitor shunted by a coil. At top left is an ITT Jennings high-voltage (10,000-V) vacuum capacitor. Below this is a group of ceramic disc trimmers from Erie Technological Corp. At the top right are a couple of glass piston trimmers along with a tuned circuit—all from JFD. Below these is a group of miniature air-tubular trimmers from Johanson. At the bottom right are air-plate trimmers from E. F. Johnson. Photo by Dirone-Denner.



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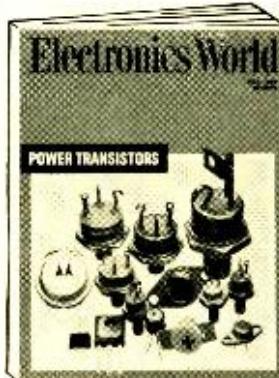
CIRCLE NO. 142 ON READER SERVICE CARD

# Coming Next Month

## Special Feature Article

### POWER TRANSISTORS

-a Status Report



#### PREDETERMINING DECIMAL COUNTERS

What's available now? What can we expect in the future? Paul Franson of Motorola explains how improvements in production techniques, in die design, and in packaging have resulted in better products and lower costs. Don't miss this comprehensive, up-to-the minute report.

#### ULTRA-LOW-FREQUENCY WOOFER ENCLOSURE

Here are details on a simple \$8.50/decade circuit that can be cascaded to divide or scale by any number from 1-9, 1-99, or 1-999. It can be used for counters, photo timers, lab scalers, frequency synthesizers, computers, and in calculators. Three IC's make construction easy.

#### DO YOU WANT TO BE CHIEF ENGINEER OF A RADIO STATION?

A unique speaker system, which has been designed for frequencies below 64 Hz, makes use of vibrating side panels and slot loading to achieve effect.

#### RCA'S SOLID-STATE COLOR CHASSIS—CTC 40

A Vocational Profile which explains what the job involves, along with its requirements. Because duties are so varied, most small stations make good training grounds for step to big-time broadcasting and telecasting. Learn how it's done.

#### PANIC BUTTON

Even with an advanced horizontal sweep section using SCR's, servicing problems on this color-TV receiver chassis are not unduly complicated.

Do you want to have some fun? Here are two sirens you can build—one manual, the other automatic—that are guaranteed to panic your friends.

All these and many more interesting and informative articles will be yours in the May issue of ELECTRONICS WORLD . . . on sale April 16th.

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ELECTRONICS WORLD

# Radio & Television news

By FOREST H. BELT /Contributing Editor

## Consumer Electronics Show Expands

Nearly 200 exhibitors will show their 1971 lines of home entertainment electronics at the annual Consumer Electronics Show. This year, the show runs from June 28 through July 1. As usual, it is at the New York Hilton and Americana hotels in Manhattan, and EIA Consumer Products Division's Jack Wayman will, as usual, be programming the seminar sessions. Some would-be exhibitors haven't yet been accommodated, but show officials are looking for more room. This show gets bigger every year, despite a few big-name manufacturers who don't participate. However, most of them can be found set up in nearby hotels the same week, taking advantage of the crowds of dealers and distributors attracted by the Show.

## U/V Tuners to Tune Alike

The issue of tuner "parity" has kicked around a long time. The FCC finally decided. The u.h.f. and v.h.f. tuners in all TV sets with 9-inch screens or larger, made or sold after May 1, 1971, must tune "with comparable ease." That could mean detented or switch-type u.h.f. as well as v.h.f. This could hasten development of all-electronic, diode-switched front-ends. Some RCA's already have them. Forthcoming tuners may include both bands on a single knob, such as Zenith and Sarkes Tarzian units, which provide six detented u.h.f. positions. Latest word, however, is that set makers intend to petition FCC for 1-year delay. So, users may have to struggle with their u.h.f. tuning for some time yet.

## Inflation is Rampant, Except . . .

There are signs of slight checking in the wild inflation that besets today's prices. But there's not enough slowdown to keep rises from overtaking repair parts for home entertainment. Receiving and picture tubes felt the inflationary needle recently. Price hikes ranged around 5 percent, and some twice that. Yet, there's no extra profit at the retail level.

Food and housing costs are still going up, so workers demand more wages. With the serious lack of really competent technicians, the best ones are wising up and insisting on pay that matches their training and skill. Shop owners with business sense are pushing repair charges upward to cover the cost of better technicians. And that makes service costs to the consumer seem right up there on the inflation ladder.

There's one consolation. But shop owners and technicians have to tell the customer about it or he never knows. TV service is still a bargain. The cost of owning a TV, even with maintenance figured in, makes it the cheapest entertainment an American family can buy. Count the hours the set is on each week, multiply by how many viewers watch it, multiply that by 50, and then divide these viewer-hours-per-year into half the cost of the TV set plus the year's repair charges. More than 20 cents an hour means you figured wrong or you don't watch enough TV to bother owning one. And this formula pretends the set is worn out in 2 years, which it isn't. Every way you calculate, TV and repairs are real bargains.

## Unfair-Laws Department

There's a strange legislative bill pending in California. It could keep a technician from being paid for a service call. If the customer decides not to have the set fixed after the technician has made a diagnosis in the home, the would-be law says it isn't a true service call. The same idea applies if the set needs shop repairs and the customer won't let it go. In neither case would the customer have to pay for the service call. Such a law, if applied this way to other professions, could make a lawyer's fee illegal unless he took the case. The absurdity of this kind of regulation seems obvious. The technician who comes into the home and uses his knowledge to make a diagnosis of trouble performs a useful service. This is no different from paying a doctor to diagnose a medical problem or paying a diagnostic car clinic to check your car.

## Horizontal FM is Okay

Many FM stations, when car-radio FM got so popular, added vertical polarization. This was at some expense, because it required a change in the transmitting antenna. But it helped reception distance in

automobiles. It made a great improvement for car-bound listeners to stereo FM. But vertical polarization can soon end. What should have been done long ago has been done this year. Auto antennas are at last horizontally polarized. New *General Motors* cars have a tiny wire dipole embedded in the windshield glass. The dipole matches the receiver's FM input better than any whip antenna of the past. It does an okay job for AM—although a few owners report they can't hear AM stations quite as far away. Insurance companies approve this denial of one more temptation to walk-by vandals; there's nothing about this new antenna they can break off.

## Hunting Old Recorder Parts?

Anyone having trouble finding parts for old or imported record changers or tape machines should ask his electronic parts distributor about *Game Industries'* catalogue 70D. You can get centerposts, drive wheels and belts, pulleys, idlers, even battery-operated motors for inexpensive import recorders. This Freeport, N.Y. company has an exhaustive stock to fit almost every changer or recorder ever built. If your distributor doesn't have the part you need, he can order it.

However, mechanical parts—such as trip pawls, change-cycle slides, cycling cams, etc.—still seem to be a problem to every technician. The only source is the manufacturer. And we hear continuing service reports that even they don't seem to have what's needed when it's needed. We keep hoping to hear of improvements in these parts situations, in place of mere buck-passing. If something effective isn't done soon, the problem will filter down to the consumer level. After that, the consumer-protection elements in government will have one more victim to feed to their lions.

## It Could (Does) Happen To You

The other day I was leaving a hearing of the National Product Safety Committee. It had been about fire and smoke in color-TV sets (see "Another Political Fire to Quench," January, 1970, page 15). As I walked down one long corridor, the words "color TV" sifted out from behind a closed door. From the keyhole, I saw a man in a hard chair facing several others at a table.

A guy at the table was pointing his finger.

"You have a responsibility. You sell those monstrosities, and just pocket your profits with no concern. We can't let you get away with that."

The man in the chair looked worried. He said, "But Congressman, how could we know people would try to lift their color sets? The dealers put them down wherever the customer says."

"That's immaterial. These hernias have got to be stopped. That's the purpose of this committee hearing. Even a single hernia caused by a heavy color TV is too many, and our survey has turned up seventeen. Not one—not ten—mind you—but *seventeen*. What do you say to that Mr. Setmaker?" His voice rose a notch with every sentence.

"Well—I—well, yes—but I understand three of those were in Texas. And . . ."

"Come on, now, sir, you're not going to try coping out on those three just because the sets were bigger, are you? It won't help your case, you know."

"But, Congressman, there are 25 million color sets. We have statistics . . . ."

"We? WE? You don't mean to imply you and other manufacturers are in collusion on this thing? In flagrant and defiant violation of the antitrust laws?"

"No. It's just that our association uncovered some facts that . . . ."

"Look," shouted the Congressman, "we're not in this hearing room for your facts. We have all the facts we want." He was pounding the table.

Another committee member jumped up. "It's clear that you'll have to put a label saying every color set can be injurious to humans."

The first man was talking again, waving his fist in the air. "Furthermore, we're going to require that no color set manufactured after next week can weigh over eleven pounds. And they all must have no less than five wheels, each one no smaller than six-and-a-half inches outside diameter and made of material that can withstand continual pounding by a toddler or chewing by a half-grown puppy. Each cabinet must have at least three handles. Floor models must have a built-in hydraulic jack. And safety belts." His voice became eloquent. "My constituents, the American people, deserve no less than complete safety from these diabolic cripplers."

I began backing down the hall.

The last thing I could hear was the lame voice of Mr. Setmaker. "Well. . . . my company has made arrangements for each set-owner, at no cost of course, to receive a complete . . . ."

I went outside. It all sounded too much like the "smoke and fires" story. I had to move quick to miss being run over by reporters hurrying out to file this latest "news." ▲

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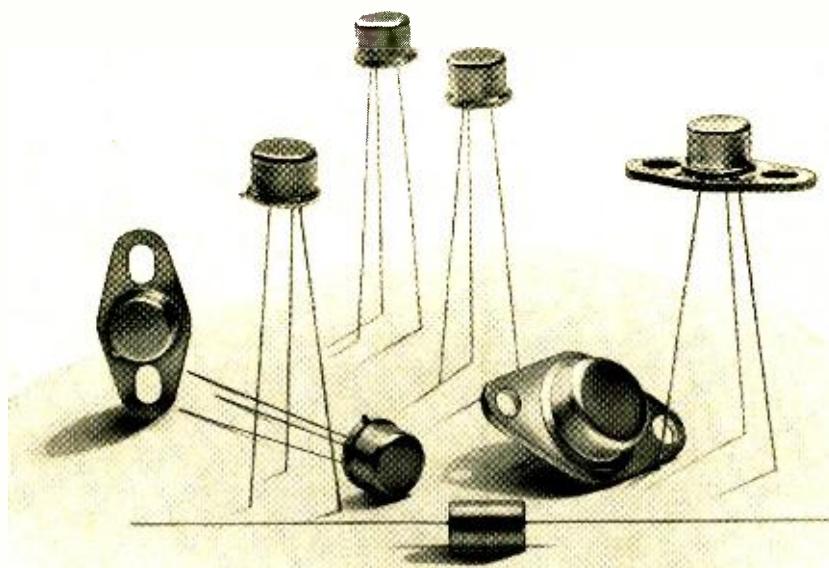
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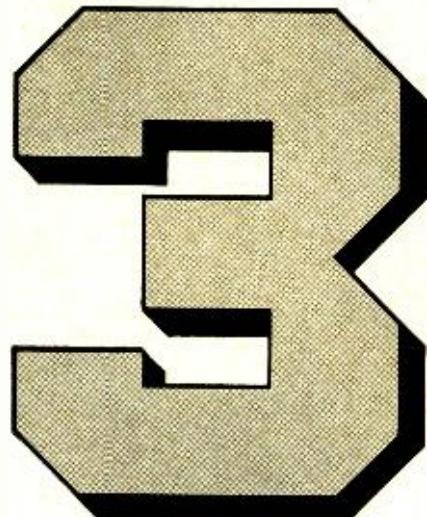


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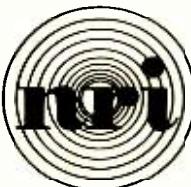
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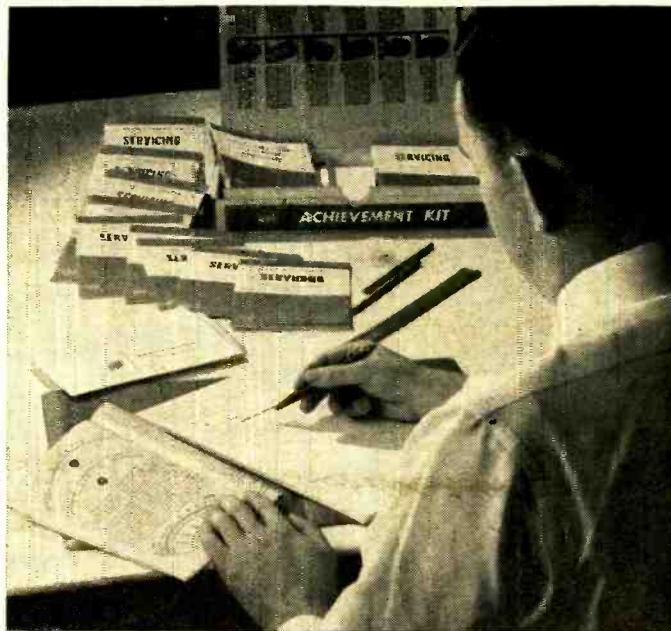


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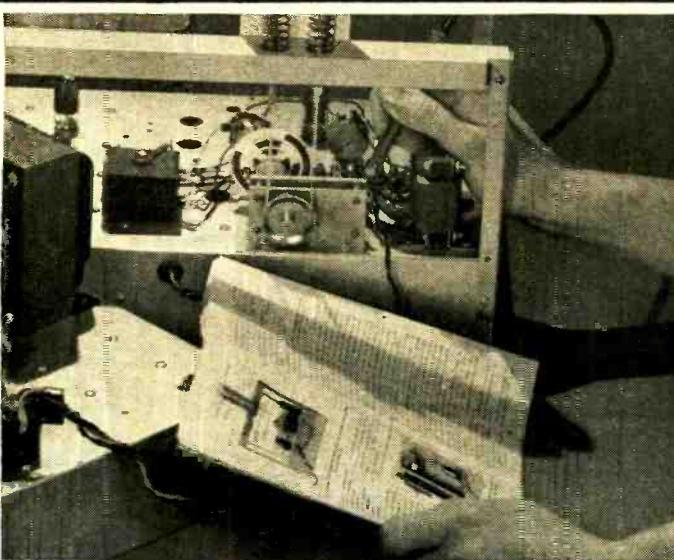
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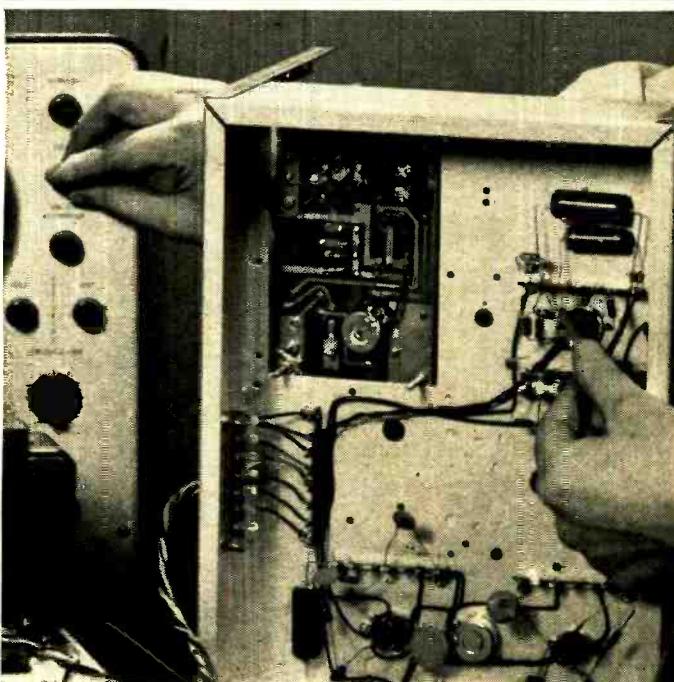
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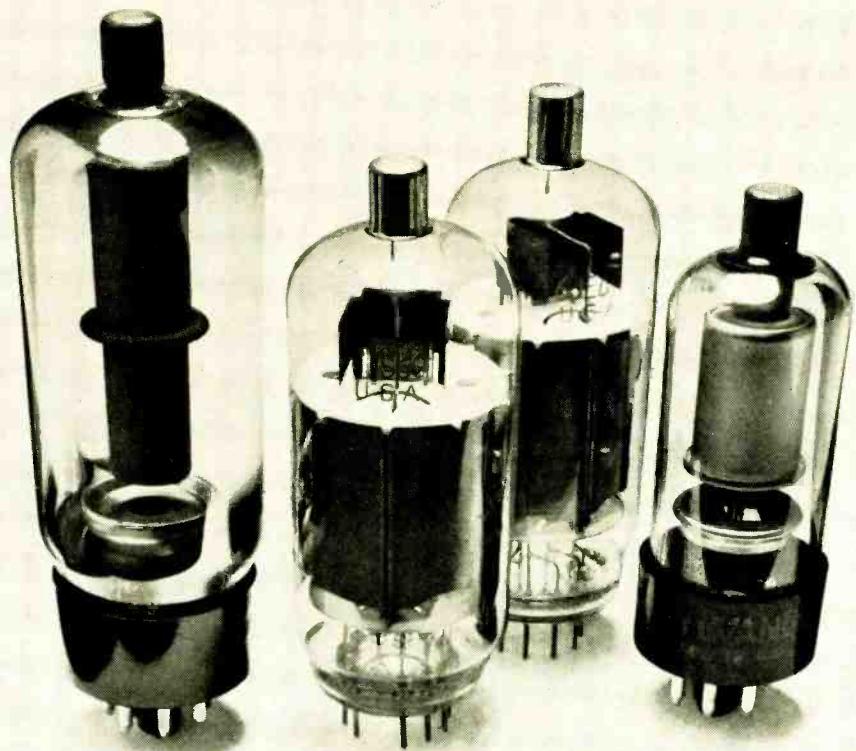
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# HI-FI PRODUCT REPORT

## NEW LAB TESTED

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McIntosh MC-3500 Power Amplifier  
Tandberg Model 11 Tape Recorder

### McIntosh MC-3500 Power Amplifier

For copy of manufacturer's brochure, circle No. 1 on Reader Service Card.



WHEN it comes to the *McIntosh* MC-3500 power amplifier, nothing less than superlatives will do. The MC-3500 is a basic mono power amplifier. It is the largest, heaviest, most powerful, and most expensive amplifier sold for home use. Its performance is of such a high caliber that we would have been unable to measure it before we acquired our *Radford* ultra-low-distortion oscillator and distortion analyzer.

The unit is a vacuum-tube amplifier—one of the last of that vanishing breed on the high-fidelity market. Transistors that can deliver 350 watts, while they have been made, are not yet economically practical for home audio equipment. Yes, we said 350 watts—the nominal and very conservative continuous power rating of this huge amplifier.

The amplifier weighs 125 pounds and measures 19 inches wide by 10½ inches high by 17 inches deep. Behind its imposing satin-finished panel (which is drilled for rack mounting) is a seven-

stage amplifier—push-pull throughout, except for the cathode-follower input stage—that culminates in eight husky output tubes of a type (6LQ6) normally used for deflection-amplifier service in TV receivers. A unity-coupled pentafilar (five-winding) output transformer, exclusive with *McIntosh*, couples the output tubes to load impedances switchable from 1 to 64 ohms. The five windings of the output transformer connect to the cathode, plate, grid, and screen circuits of the output tubes, plus a negative-feedback winding supplying 32 dB of over-all feedback and an additional 6 dB in a local loop.

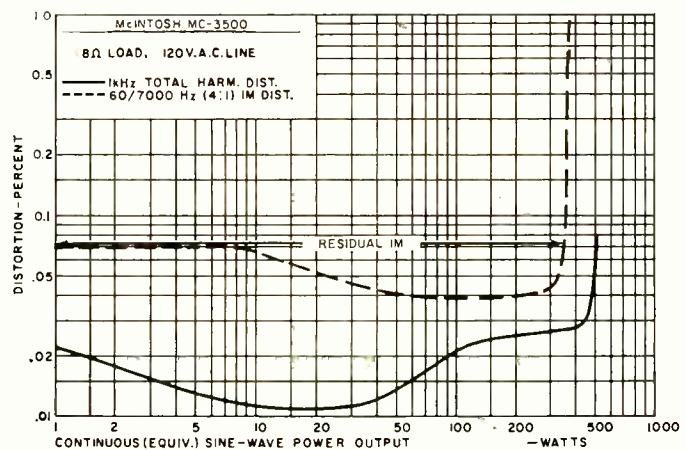
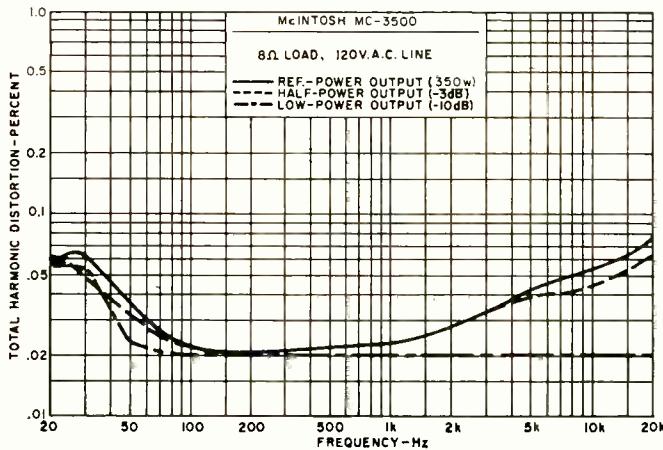
A large meter on the front panel serves several functions. In eight of the twelve positions of its selector switch, it reads the cathode currents of the output tubes for setting their grid biases. Two positions are for monitoring the output power in decibels, relative to the rated 350-watt output. One of them is 10 dB more sensitive than the other, so

that normal power levels down to a fraction of a watt may be read. Another position reads the output voltage—up to 150 volts—for laboratory applications, where the MC-3500 can be used (in conjunction with an oscillator) as an ultra-low-distortion, variable-frequency a.c. power generator. There is a gain control on the panel—a necessity since only 1.1 volts will drive the amplifier to 350 watts! A massive combination switch/circuit breaker turns the amplifier off and on. Parallel inputs with phono and lab-type BNC connectors are provided on both front and rear panels. The binding-post outputs on the front are also duplicated by screw terminals in the rear, where there is also a switch that rolls off the response at 6 dB per octave below 5 Hz.

The specifications of the MC-3500 are impressive. The output is 350 watts from 20 to 20,000 Hz, with less than 0.15 percent harmonic or IM distortion. Frequency response is within +0, -3 dB from 1 to 70,000 Hz at 1 watt. Hum and noise are 95 dB below 350 watts.

We had to parallel all our oil-cooled load resistors to handle the power of the MC-3500. At rated power and at half power, the harmonic distortion was less than 0.08 percent from 20 to 20,000 Hz, and under 0.03 percent over most of that range. At one-tenth power (a respectable 35 watts) the distortion was down to 0.02 percent from 70 to 20,000 Hz.

When the unit was operated at 1000 Hz into an 8-ohm load, the harmonic distortion was between 0.01 and 0.02 percent from 1.5 to 90 watts, increasing to 0.03 percent at 450 watts, and reaching only 0.08 percent at 500 watts. The IM distortion test merely indicated the



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residual distortion of our test instruments—less than 0.07 percent from 1 watt to 350 watts. The frequency response was  $\pm 0.1$  dB from 20 to 20,000 Hz at 10 watts, and was down 3 dB at 70,000 Hz. Only 0.16 volt was needed for 10-watts output (our standard reference power level), and hum and noise were 73 dB below 10 watts, which is completely inaudible.

The amplifier was cool in operation, and quiet, even with its built-in cooling fan. Our loads, however, heated their oil baths to a new high. The MC-3500 clipped cleanly when overdriven and showed no tendency to blow tubes or fuses.

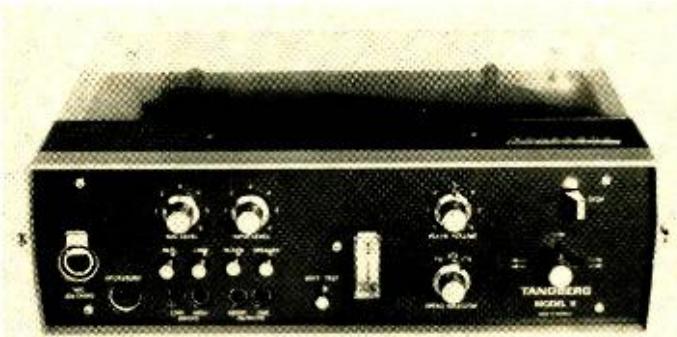
All of this naturally raises the question of why anyone would want an amplifier capable of delivering 500 watts in his home music system. We are not really sure, but properly fused, very

rugged low-efficiency speakers such as the AR-3a and *Bose* 901 could be used safely—and would perform beautifully—with the MC-3500. But under no circumstances would we advise using this particular amplifier without a suitably rated fuse in order to protect the loudspeaker.

The *McIntosh* MC-3500 is clearly the ultimate in high power and low distortion among amplifiers offered for home use. (*No doubt many recording engineers and industrial users will also be interested in this amplifier.—Editor*) It sells for \$1099, which is certainly not inexpensive for a single channel. But if money is no object, it is safe to say that when a pair of MC-3500's are installed, the amplifier can once and for all be eliminated as a potential limiting factor in any type of music-reproduction system. ▲

#### Tandberg Model 11 Tape Recorder

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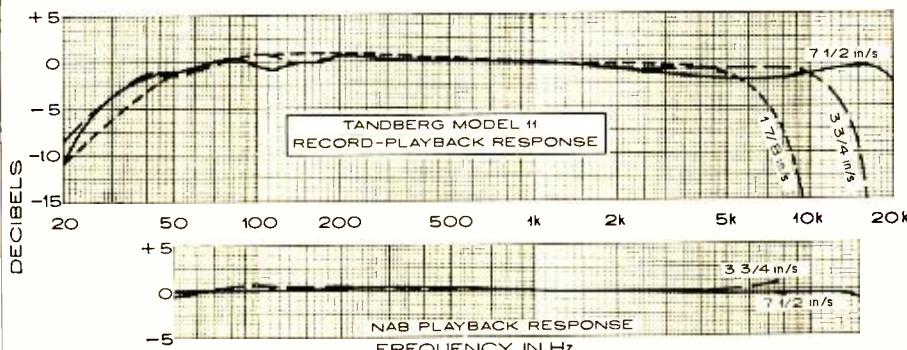


VIRTUALLY all new components coming to us for testing have been stereo models. In the case of tape recorders, mono models are still very much on the scene, but they are almost never meant for serious listening or professional use. An impressive exception to this rule is the *Tandberg* Model 11, a professional-quality portable mono reel-to-reel recorder.

The Model 11 is fully transistorized, and can be operated from a self-contained battery pack from which it draws 2 to 3 watts. If ordinary dry cells are used (ten 1.5-volt "D" cells are required), the battery life is about 5 to 6 hours in continuous operation, or about 20 hours if the machine is used half an

hour per day. Rechargeable nickel-cadmium cells can also be used for long-term economy. For a.c.-line operation, *Tandberg* provides an optional battery eliminator that physically replaces the internal battery pack. It can also be used externally to recharge nickel-cadmium batteries in the recorder, through an accessory connector. We tested the Model 11 with the a.c. power supply installed.

This is a half-track machine that takes 7-inch reels. It has three heads and separate recording and playback electronics for off-the-tape monitoring while recording. The microphone input, for a 200-ohm balanced dynamic microphone, uses a locking professional-type



connector. Two line inputs are provided, for high- and low-level signals. Separate recording-level controls for the microphone and line inputs make it possible to mix signal sources.

There are two playback outputs using miniature phone jacks. One is a monitoring output for 200-ohm unbalanced headphones; the other is a 600-ohm balanced output. Both are controlled by a single playback-level control. A small built-in speaker can be switched on to monitor either incoming or outgoing signals, but the line outputs are disconnected when the speaker is on. A meter indicates recording level, and when the "Play" button is depressed, it indicates the level at the line output. A battery-test button switches the meter to check the condition of the batteries.

The tape-transport control is a single lever that provides fast-forward and reverse when pushed right or left; normal speed is obtained by pushing it up. A separate recording-interlock button must be pressed simultaneously to record. The "Stop" lever starts and stops the tape instantly without causing the machine to switch out of the record mode.

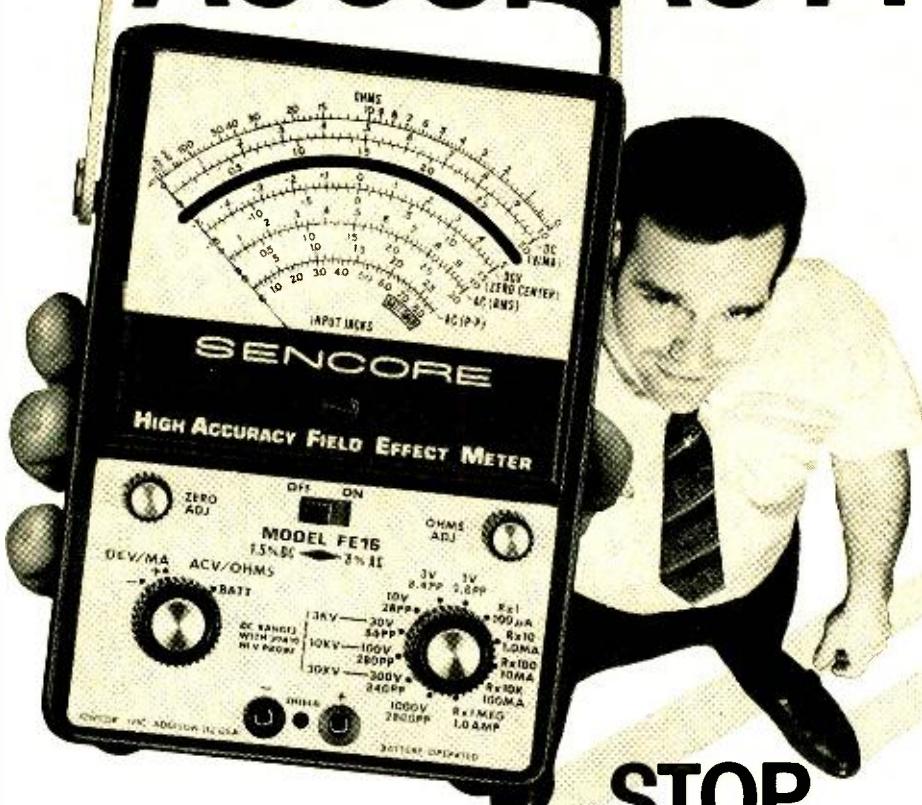
The three operating speeds of 1 $\frac{1}{8}$ , 3 $\frac{3}{4}$ , and 7 $\frac{1}{2}$  in./s are selected by a rotary switch that sets the unique electronic speed-control circuits of the Model 11. Precise and consistent speed is a necessity for professional applications and when operating on batteries there is no a.c. power line to establish the motor speed. A very effective electronic substitute was developed by Tandberg engineers.

A tachometer wheel on the capstan drive shaft generates an a.c. voltage in a special pickup head. This voltage is amplified, clipped, and then detected in a ratio detector whose d.c. output is proportional to the frequency or to the motor speed. The output of a separate 20-kHz square-wave generator is integrated to produce a triangular waveshape which is summed with the d.c. output of the ratio detector. The summed voltage controls a Schmitt-trigger circuit, the output of which is a series of 20-kHz pulses whose width is a function of the motor speed. The average value of these pulses, after filtering, is a d.c. voltage whose value is a function of motor speed. After amplification, it drives the d.c.-operated capstan-drive motor.

This system maintains an extremely accurate motor speed, since any tendency for the speed to change produces a corresponding compensating change in the d.c. voltage that operates the motor. For speed change, the tuning of the ratio-detector is changed, and the motor speed then changes accordingly to maintain a balanced condition.

We tested the Tandberg Model 11 with 3M type 150 tape, for which it had

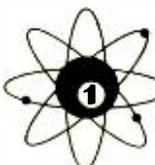
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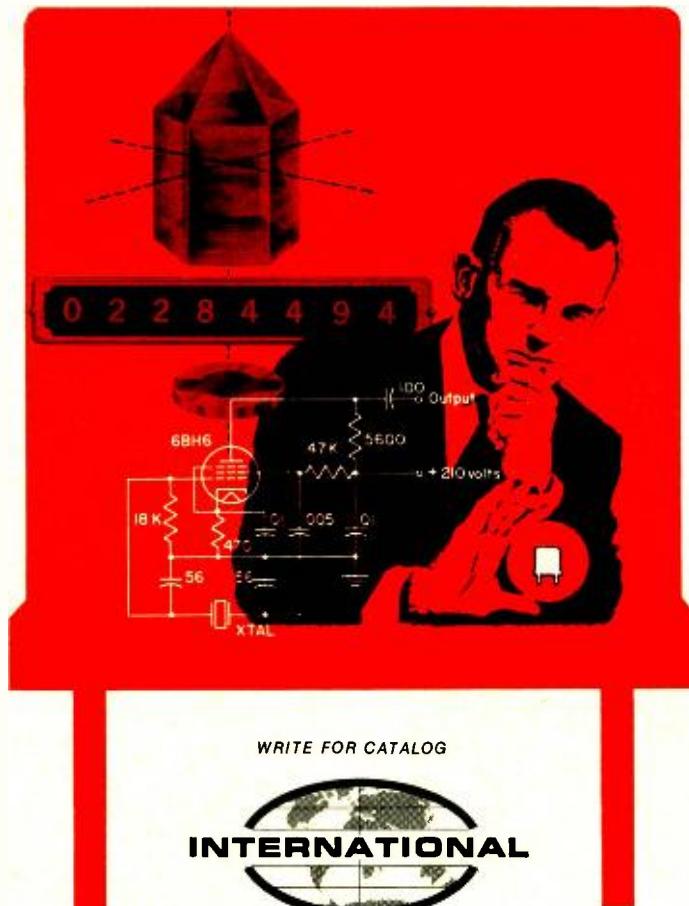
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been adjusted. Its performance was well within specifications, and was of a fully professional caliber. At 7½ in/s, the over-all record-playback frequency response was  $\pm 1.5$  dB from 35 to 20,000 Hz, and the NAB playback frequency response was  $\pm 0.5$  dB from 50 to 15,000 Hz. The unweighted signal-to-noise ratio was 60 dB. Wow and flutter were 0.03 and 0.09 percent, respectively.

At 3¾ in/s, the record-playback response was  $\pm 2.5$  dB from 30 to 12,500 Hz, and the NAB playback response was +0.4 dB from 50 to 7500 Hz. The signal-to-noise ratio was 59 dB, and wow and flutter were 0.5 and 0.1 percent, respectively. The 1⅓ in/s speed produced very listenable quality, although with a somewhat restricted frequency response of  $\pm 2$  dB from 40 to 6500 Hz. The signal-to-noise ratio was about the same as it was for 3¾ in/s.

The "High" line input required 0.12 volt and the "Low" required 3.4 millivolts for a 0-dB recording level. At 0 dB, the over-all distortion was 2.4 percent, dropping to less than 1 percent at -10 dB. The maximum line output before clipping was 3.3 volts. In wind and rewind, about 2 minutes were required to handle 1200 feet of tape. The normal operating speeds were exact, as determined by a tape stroboscope.

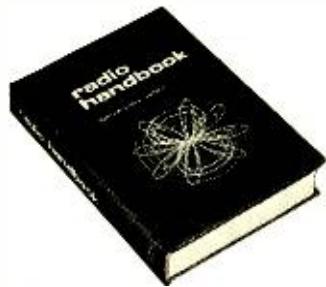
The Model 11 is not for the casual hobbyist, but should be an excellent choice for recording interviews for broadcast (the built-in switchable automatic level control will be useful) or other field operations where the weight and bulk of conventional professional recorders would be prohibitive. Its performance, both mechanical and electrical, leaves nothing to be desired for such applications. The unit measures 4 × 10 × 13 inches and weighs 12.1 pounds with batteries.

The Tandberg Model 11 sells for \$449.50. A full-track unit and a pilot-tone version for motion-picture sound synchronizers are also available. The optional a.c. power supply is \$44.95, and a leather carrying case with shoulder strap is \$29.95. ▲



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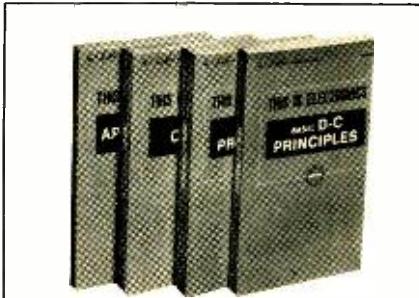
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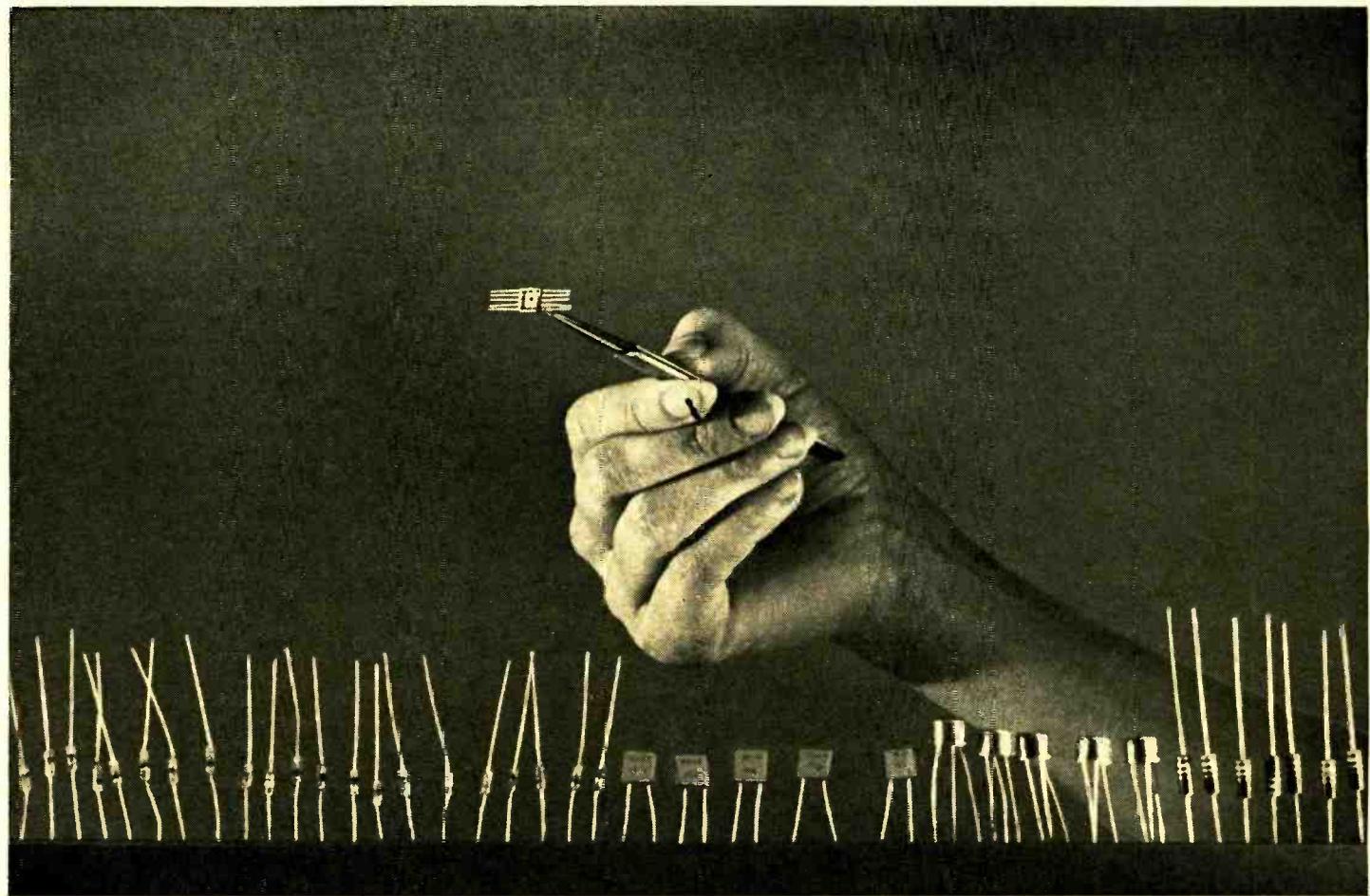
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Already, as a result, a two-way radio can now be fitted inside a signet ring. A complete hearing aid can be worn entirely inside the ear. There is a new desk-top computer, no bigger than a typewriter yet capable of 166,000 operations per second. And it is almost possible to put the entire circuitry of a color television set inside a man's wristwatch case.

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Soon kitchen computers may keep the housewife's refrigerator stocked, her menus planned, and her calories counted.

Money may become obsolete. Instead you will simply carry an electronic charge account card. Your employer will credit your account after each week's work and merchants will charge each of your purchases against it.

When your telephone rings and nobody's home, your call will automatically be switched to the phone where you can be reached.

Doctors will be able to examine you internally by watching a TV screen while a pill-size camera passes through your digestive tract.

### New Opportunities for Trained Men

What does all this mean to someone working in Electronics who never went beyond high school? It means the opportunity of a lifetime—if you take advantage of it.

It's true that the "chip" may make a lot of manual skills no longer necessary.

But at the same time the booming sales of articles and equipment using integrated circuitry has created a tremendous demand for trained electronics personnel to help design, manufacture, test, operate, and service all these marvels.

There simply aren't enough college-trained engineers to go around. So men with a high school education who have mastered the fundamentals of electronics theory are being begged to accept really interesting, high-pay jobs as engineering aides, junior engineers, and field engineers.

### How To Get the Training You Need

You can get the up-to-date training in electronics fundamentals that you need through a carefully chosen home study course. In fact, some authorities feel that a home study course is the best way. "By its very nature," stated one electronics publication recently, "home study develops your ability to analyze and extract information as well as to strengthen your sense of responsibility and initiative." These are qualities every employer is always looking for.

If you do decide to advance your career through spare-time study at home, it makes sense to pick an electronics school that specializes in the home study method. Electronics is complicated enough without trying to learn it from lessons designed for the classroom instead of correspondence training.

The Cleveland Institute of Electronics has everything you're looking for. We teach only Electronics—no other subjects. And our courses are designed especially for home study. We have spent over 30 years perfecting techniques that make learning Electronics at home easy, even for those who previously had trouble studying.

Your instructor gives your assignments his undivided personal attention. He not only grades your work, he analyzes it. And he mails back his corrections and comments the same day he gets your lessons, so you read his notations while everything is still fresh in your mind.

### Always Up-to-Date

Because of rapid developments in Electronics, CIE courses are constantly being revised. Students receive the most recent revised material as they progress through their courses. This year, for example, CIE students are receiving exclusive up-to-the-minute lessons in Microminiaturization, Logical Troubleshooting, Laser Theory and Application, Single Sideband Techniques, Pulse Theory and Application, and Boolean Algebra. For this reason CIE courses are invaluable not only to newcomers in Electronics but also for "old timers" who need a refresher course in current developments.

### ENROLL UNDER NEW G.I. BILL

All CIE courses are available under the new G.I. Bill. If you served on active duty since January 31, 1955, or are in service now, check box on reply card for G.I. Bill information.

Tiny TV camera for space and military use is one of the miracles of integrated circuitry. This one weighs 27 ounces, uses a one-inch vidicon camera tube, and requires only four watts of power.



### Get FCC License or Money Back

No matter what kind of job you want in Electronics, you ought to have your Government FCC License. It's accepted everywhere as proof of your education in Electronics. And no wonder—the Government licensing exam is tough. So tough, in fact, that without CIE training, two out of every three men who take the exam fail.

But better than 9 out of every 10 CIE graduates who take the exam pass it.

This has made it possible to back our FCC License courses with this famous Warranty: you *must* pass your FCC exam upon completion of the course or your tuition is refunded in full.

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## FOUR-CHANNEL STEREO

To the Editors:

On June 2, 1964 I filed a patent application entitled "Monoaxial Quadrangular Recording System," and received patent number 3,375,329 dated March 26, 1968. An abstract of the disclosure follows: "A method for recording and reproducing sound for creating a true environmental transposition of a given audio situation in which a quadrangular arrangement of microphones defining a plane is positioned in an overlying and surrounding relationship with respect to the audio sound stage from which a source of sound originates . . ."

My patent describes a method of reproducing the precise acoustical geometry of the sound stage by sampling the outputs of microphones surrounding the action, feeding the sampled output into a single-channel amplifier, and recording or transmitting the information received. Recovery embraces the inverse progression whereby the quadrangular placement of loudspeakers complements the microphone placement, and the output of microphone #1 is received only by loudspeaker #1, etc.

The rewarding virtue of such a single-channel system is that the phase-amplitude relationship throughout the transposition cannot be altered by any means. An increase or decrease in amplitude affects all relationships equally. A further advantage is that no FCC regulations are required. Picked up by an ordinary radio or TV receiver, straight monophonic reproduction is heard.

ROBERT PROUTY  
Olney, Md.

*There are a good many patents extant for various systems providing multi-channel stereo. It will be interesting to see which one, if any, of them will be used in the finally accepted 4-channel system. No doubt, compatibility with 2-channel stereo and with mono will be an important prerequisite for any 4-channel method.—Editors*

\* \* \*

## ELECTRONICS AND PLANTS

To the Editors:

I was happy to see the article "Electronics and the Living Plant" in the October issue. Enough work has been done in this field by groups and individual experimenters, from the University of Alberta to the Presidency College of Cal-

cutta, to assure us there is an important and practically untapped field of knowledge here.

One of the reasons for the lack of progress in this field is the fantastic difficulty of the subject. Not only are there 350,000 species of plants, but they can be subjected to an almost unlimited number of combinations of signal strengths and frequencies, from the fringe of the perceptible to the lethal, and from d.c. to light. Their response—as we have learned from the poinsettia—may be to narrow frequency bands and voltage ranges. Even audio—music—has been reported to have an effect on the growth of grain.

Another reason is the lack of communication. Many experimenters have been quite unaware of what others were doing, or indeed that any others were working in the field. This article should stimulate intercommunication, and the references may open new doors to some.

I did regret that no mention was made of possibly the first serious worker in this field, Sir Jagadis Chandra Bose. After distinguishing himself in wireless research in the '90's, he devoted the rest of his life to the study of plants. His results were so far in advance of his time that good orthodox scientists shunned him as a "mystic" and even suspected his mental competence.

Is it possible that the ostracism he suffered at that time has caused him to be forgotten entirely? If so, researchers would do well to look up his "Response in the Living and Non-Living" and "Plant Response." Some of his less-known (and later) books might be even more important, and the ingenious instruments that gained him envious praise from persons who could not accept his conclusions might still be useful.

Now that the times have caught up with him, modern researchers may not find him so "far out." Indeed, they may have surpassed him. Though Dr. Bose suggested that plants might be sentient beings, he never went so far as to claim extra-sensory perception for them!

FRED SHUNAMAN  
Plainfield, N. J.

\* \* \*

## PRINTED-CIRCUIT REPAIR KITS

To the Editors:

In the October issue of ELECTRONICS WORLD Mr. Sal DiNuzzo, in his article entitled "Printed Circuit Tech-

nology," wrote on page 41: "Repair kits are available which not only contain unique tools but also such items as copper foil, epoxy cement, conductive cement, conductive epoxies, eyelets, solvents, swabs, and other special items."

I would appreciate your sending the addresses of manufacturers of such kits.

JOEL T. WHITE, JR.  
Monticello, Miss.

*The repair kits referred to were made by Hazeltine especially for their own use and are not commercially available. There are some military repair kits available but here again these are strictly for military applications. We're sorry we do not know of any commercially available repair kits, although as our article "Printed Circuit Kits For Short Runs" indicated, there are quite a few printed circuit kits currently on the market.—Editors*

#### IC 12- TO 6-V CONVERTER

To the Editors:

With reference to my article in the January, 1970 issue on the converter for 12 to 6 V (p. 68), several of your readers have pointed out that we did not show values of resistors  $R_1$  and  $R_2$  either in Fig. 2 or in the text. The proper values are as follows:  $R_1$  is 330 ohms and  $R_2$  is 220 ohms.

E. A. SACK, V. P./Gen. Mgr.  
Integrated Circuits Div.  
General Instrument Corp.  
Hicksville, N. Y.

\* \* \*

#### ELECTROMAGNETIC SPECTRUM CHART

To the Editors:

I enjoyed your Electromagnetic Spectrum Chart in the January, 1970 issue (p. 37) of ELECTRONICS WORLD very much. It is a beautiful chart. However, there was a small typographical error; namely, "hard" and "soft" should be interchanged as follows: Soft—X-rays—Hard, since hard x-rays are the more penetrating ones.

If you have some of these charts available for distribution, I would appreciate having some for showing to my students.

YSPRAND HAVEN, Prof. of Physics  
Wake Forest Univ.  
Winston-Salem, N. C.

*Thanks to Prof. Haven and to all the other readers who found this chart useful in spite of the transposition of the words "hard" and "soft." We are sorry that we do not have for distribution extra copies of the Spectrum Chart or the Sound Chart on reverse side.—Editors.*

\* \* \*

#### DUAL 1219 PRICE CHANGE

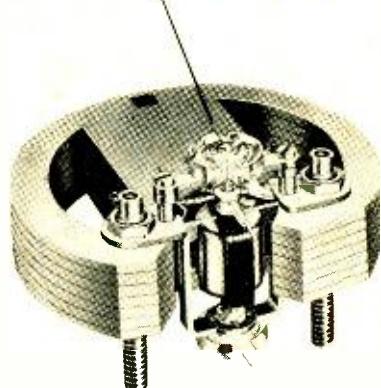
The price that was given in our February lab-tested report on the Dual 1219 automatic turntable is no longer correct (page 69). The present price of the unit is \$175 plus the base. ▲



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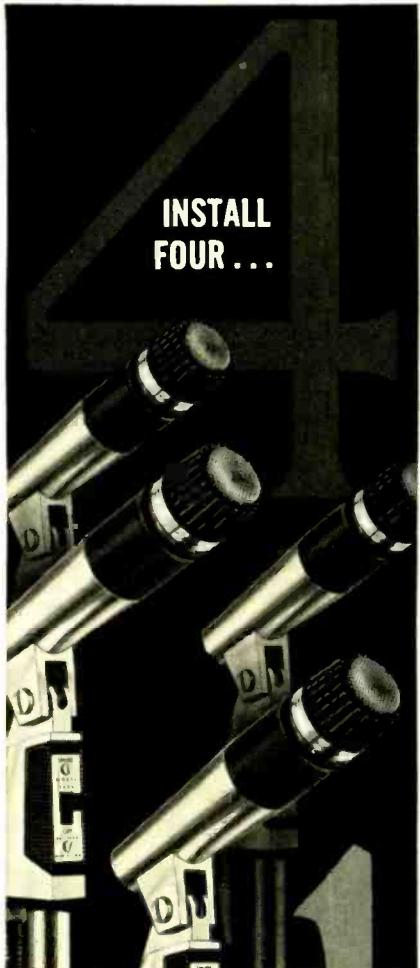


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ELECTRONICS WORLD



# NEWS HIGHLIGHTS

## Radar-Controlled Brakes

Bentley Associates of Chelmsford, Mass. has developed a radar-controlled braking system for automobiles that may put tailgaters out of business. Working on principle of Doppler radar, the system (depending on closure rate between car and object in front) operates vacuum-powered brake controls and throttle linkage; accordingly, higher closure rates cause longer braking durations than slower closure rates. System reaction time, measured in milliseconds, will keep vehicle at least one car length behind car in front and stop vehicle 8 to 10 feet from stationary objects. An audio beeper that warns driver of braking action and an overriding feature that cuts out all but beeper, allowing driver to pass slower objects, is included. Unit can be operated in either a high-speed ("country") or slow-speed ("city") mode. Transportation Secretary John A. Volpe has said that "... I think that it could potentially save a great many lives in this country." Device now costs \$800 but can be reduced to \$200 through mass production.

## Navigators Obsolescent?

When first 747 superjet took off for London from N.Y. in January it was guided across Atlantic by an inertial navigation system similar to the one that took our astronauts to moon and back last year. Applying space-age technology to commercial applications, General Motors' AC Electronics Div. created the Carousel IV inertial navigation system that can automatically steer aircraft, from starting point to destination, without radio, radar, magnetic aids, or the sun and stars. System supplies a multitude of information such as: instant position, distance and time to destination, wind speed and direction, etc. Extreme accuracy of system (five times better than standard form of transoceanic navigation) aids in shortening flight time and saving fuel. It also offers the possibility of narrowing the air corridors over oceans from the present 120-mile spacing to 60 miles—with safety.

## Computer Time Sharing

Despite the slowing trends forecast for the computer hardware industry, computer-time-sharing sales, which grew from \$80 million in 1968 to about \$150 million in 1969, will probably double in 1970. Long-time projections indicate that by 1972 sales should reach \$1 billion and exceed \$2 billion by 1975.

## Electronic Roll Call

An automatic vehicle monitoring system that can electronically identify and locate the position of over 1000 transponder-equipped vehicles in a matter of seconds has been developed by Hazeltine Corp. of Little Neck, N.Y. According to James W. Evans, vice-president of the firm's Industrial Products Div., this system will help alleviate congestion on city-agency and transportation-system radio voice channels in large urban areas. Upon receipt of a synchronizing signal from a central transmitter, each vehicle responds sequentially by transmitting a digitally coded pulse train at a frequency of 1000 MHz (L-band) to fixed receiving stations. Part of the pulse train is used by two pairs of these receiving stations to mathematically determine vehicle's position. This is then fed back to the central control station, together with the rest of the pulse train containing such digitally coded information as operational status, output of a passenger counter, or need for emergency assistance, to be processed by computer and

displayed. In a previous experiment conducted in a densely packed 1-square-mile high-rise area in midtown New York City, involving 274 individual tests, the error was less than 300 feet in 95% of the cases and less than 175 feet in 77% of the cases. Recently we witnessed a similar demonstration here in New York and were impressed with the results. System lends itself to such applications as: freight cars and passenger trains, police cars, ambulances, taxi fleets, cabs, delivery trucks, etc.

## Monitoring the Monitor

Tedium experienced by guards with constant vigilance of security system monitors can now be eliminated. GBC Closed Circuit TV Corp., N.Y. has come up with a motion detector, called the VS-101 Video Sensor, which lights a lamp or rings an alarm or siren to alert a guard to watch TV monitor when any unauthorized or unusual movement of light occurs on TV screen. Sensor uses two tiny sensing units which stick to front of monitor and can be positioned to monitor entire screen, or to concentrate on a particular area or item such as safe or file cabinet.

## Ersatz Moondust

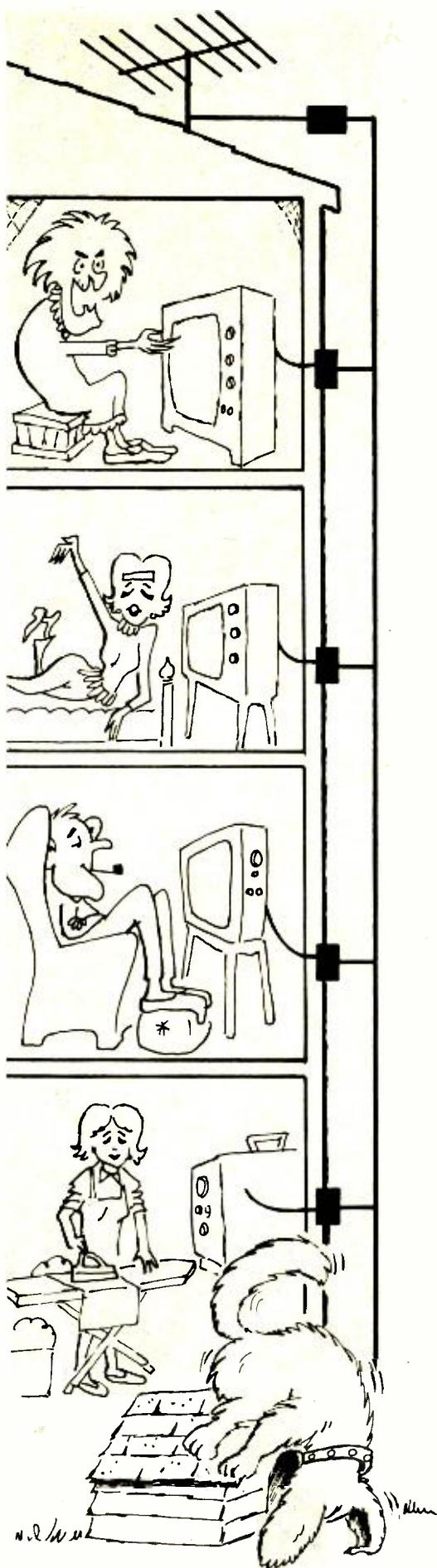
You don't have to go to the moon to have your own moondust. Edmund Scientific of Barrington, N.J. has come up with a product called "Moondust" that is so much like the real lunar soil that leading experts, using an 80-power microscope, can not tell them apart. Although chemically different, the physically similar properties suggest a myriad of uses for checking effects of lunar soil and dust on equipment destined to be used on moon's surface. For example, "Moondust" could be used to determine whether such instruments as sensitive gages, computers, and computer parts are "moondust-proof." And then again, wouldn't having your own moondust be a tremendous conversation piece? "Moondust" is available direct from Edmund.

## Search for Blind "Readers"

Unknown to many, one of the programs of Library of Congress is to look after "reading" needs of the blind. Program includes Braille books and "Talking Book" long-playing records and machines on which to play them. Recently, the Division for the Blind and Physically Handicapped, administrators of the program, purchased 10,000 GE portable cassette recorders to give handicapped persons opportunity to enjoy benefits of talking books while traveling or away-from-home situations. Although 1000 new "readers" are added each month, only 20% of those eligible are reached. Goal of Division's public information program is to reach remaining 80%.

## Electronics a'Sea

Chris-Craft Corp. recently introduced its new integrated marine electronics system, which consists of standardized navigation and communications equipment designed specifically for the boat and vice versa. An impressive array of equipment, including depth sounder, automatic pilot, automatic direction finder, 150-watt AM radiotelephone, and v.h.f.-FM radiotelephone, are set up like the flight deck of a jetliner rather than with the usual back-of-the-store workbench appearance which is characteristic in the boating industry today. The ice is broken and hopefully the rest of the boating industry will follow suit, providing added safety and increasing the range and enjoyment of cruising. ▲



# Set 'em up... anywhere!

These days when tiny TV's and FM radios are the rage and everybody wants one, you've probably had people asking you about master antenna systems to plug them into.

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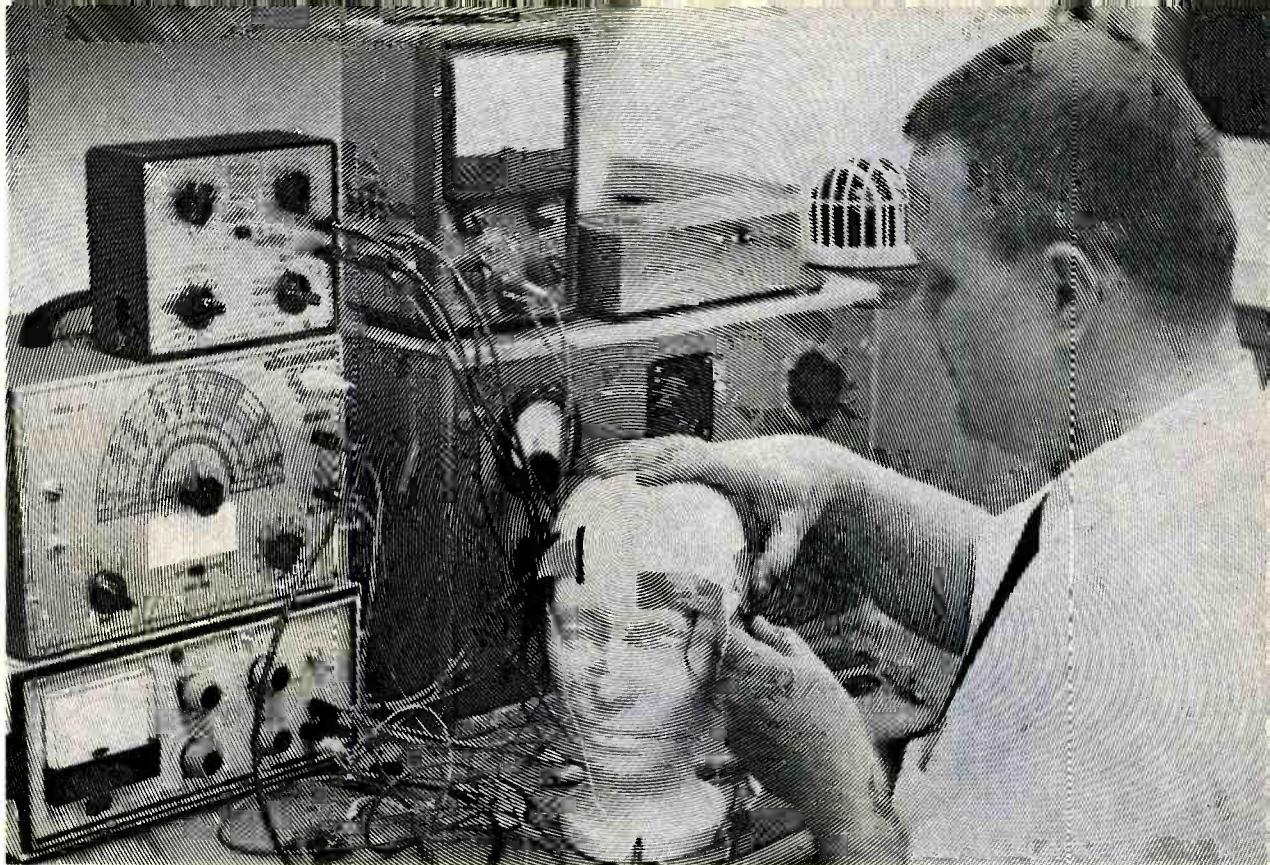
And, all it takes to do it is the tools in any tool kit. So go ahead and set 'em up anywhere ... and start enjoying TV!



## **CHANNEL MASTER**

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Conductive mannequin head used in electronic dream experiments to simulate electrical surface properties of cranium. Technician is shown taking skin and related measurements.



# Electronics and Parapsychology

By L. GEORGE LAWRENCE

*Does man possess latent psi-sensitivities that have been stifled by modern communications systems? Parapsychology, an aspiring science using modern electronic methods, has been working to unleash this "natural" ability in man.*

PARAPSYCHOLOGY, or psychic research, deals with the world of "psi." Extrasensory perception (ESP), psychokinesis (PK), and other mind-based phenomena are its way stations. Long suspect because of an occult background, the field continues to fight for a secure place among the accepted sciences; but some progress has been made. Today, the application of electronic instruments to this unique area has permitted dramatic experiments and brought forth a few stunning discoveries of excellent promise, which has prompted those most active in this field to predict that, in time, parapsychological methods might well rival the orthodox communications arts and sciences currently in use. Of course, due caution is suggested.

## Its Beginning

Critical experiments in parapsychology started in the second half of the 19th century. The "Society for Psychic Research," founded in 1882 in London, first used scientific methods for its studies, dissociating psychic phenomena

from superstition, spiritualism, and the various "mediumships" so fashionable at that time. Later, in 1906, Dr. Duncan MacDougall of Massachusetts General Hospital detected a small loss of weight at the instant of human death. Around 1930, Dr. William McDougall established a research group at Duke University, which attained considerable prominence under Dr. J. B. Rhine. To date, only a handful of university-connected ESP labs exist throughout the world; the oldest is at the State University of Utrecht in Holland, the newest at Andhra University in India. The bulk of research is carried on by interested individuals, private groups, and *ad hoc* societies.

## Concepts

The need for machine systems, capable of testing for ESP and PK in an unbiased, impartial manner, was recognized at an early date. It was the Italian scientist F. Cazzamali who developed, around 1923, a u.h.f.-type of apparatus for testing human telepathy.

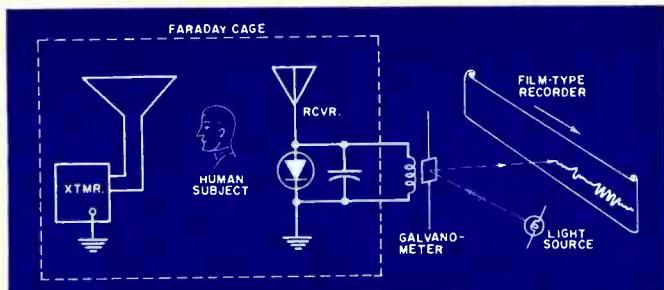


Fig. 1. Setup used by Italian scientist, Prof. Cazzamalli to do human telepathy research. An r.f.-beat signal was produced at receiver when transmitter and emotionally stimulated human brain radiate at near-identical electromagnetic wavelengths.

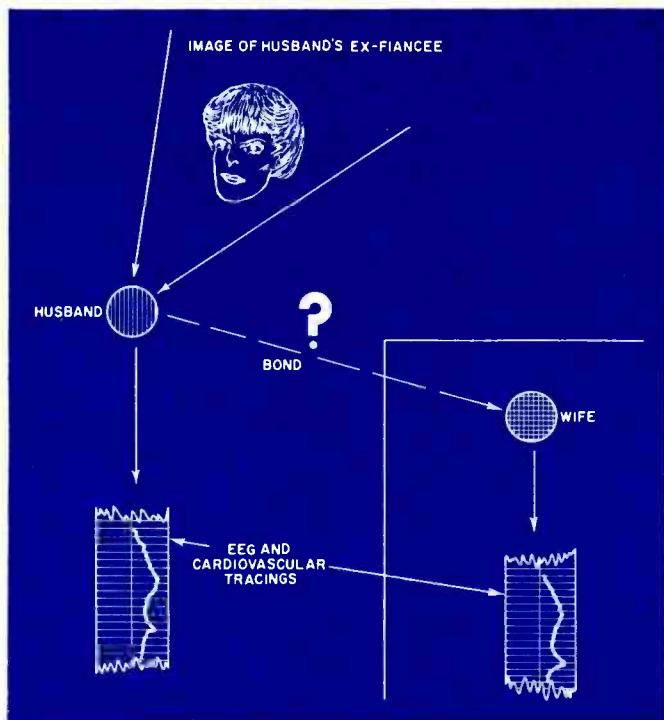
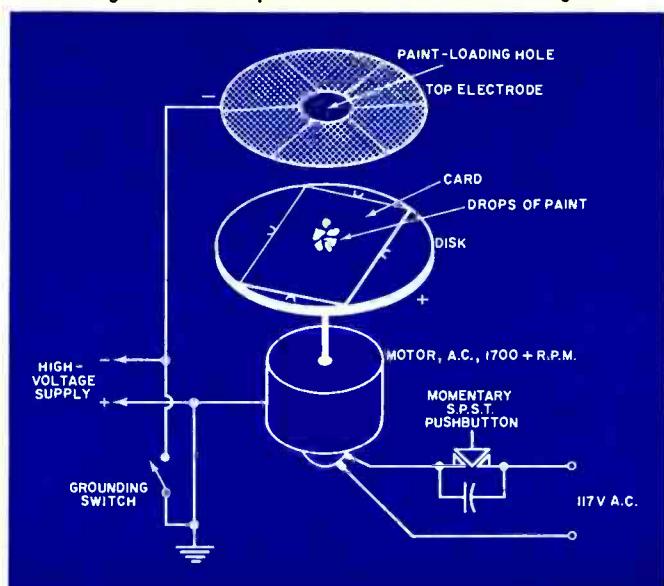


Fig. 2. Experiment performed to show evidence of "psi" bond between emotionally knit human subjects. EEG and cardiovascular tracings are identical for both husband and wife although image of husband's ex-fiancée is shown only to the husband.

Fig. 3. Color centrifuge equipment used to confirm existence of psi fields. With experimenter concentrating on an image on a separate card, while directing his thoughts on the card containing drops of paint, an identical or quasi-identical image of the original should be produced when the motor is energized.



As shown in Fig. 1, Cazzamalli placed his human subjects inside a Faraday cage and claimed that some of these individuals could produce r.f.-beat pulses when undergoing emotional stimulation of the brain. Since v.h.f./u.h.f. techniques were rather crude, it is open to conjecture whether this purported "brain radiation" was heterodyning with fundamental frequencies between 60 and 400 MHz of the local oscillator or interacting with more or less high harmonics. Unfortunately, Cazzamalli's experiments have never been repeated in depth. It is believed that his last paper appeared in 1941, at which time Benito Mussolini (Italian premier and dictator from 1922 to 1945) declared the work secret.

But, of course, progress never stops. A somewhat strange offspring of Cazzamalli's ideas and machinery is the "Integatron" designed by UFO-man G. W. Van Tassel. The apparatus, located at Yucca Valley, California, promises such wonders as rejuvenation of older people's body cells, anti-gravity, and the epitome of psychic ecstasies—time travel.

These two basic examples might have shown, perhaps, that parapsychology's instrumentation phase has two faces: hardcore science at one side, science-fiction type concepts at the other. But the psi-phenomena do persist and can be verified.

### Recent Experiments

At the research center of Rockland State Hospital, N.Y., scientists used instruments linked to a computer to record EEG, changes in blood volume in a finger, and heart rate. The human subjects (in this instance, husband and wife) were placed in separate rooms and subjected to emotional stimuli. When, for example, the husband was shown a projected picture of his ex-fiancée (Fig. 2), the record of his emotional response was matched on the wife's tracings, even though her projection screen was blank. As Dr. Esser, the principal investigator points out, only a very few people have this bond. He also reports that *alpha* waves (brain waves) in identical twins are synchronized. This ties in with the odd observation that twins frequently have an almost identical psychic life.

Owing to the uniqueness of such and related happenings, researchers are hard pressed to come forth with some kind of working theory. This leads to a consideration of the hypotheses evolved by both Drs. Roll and Wassermann, among others.

Here, W. G. Roll's concept of "psi-fields" is analogous to electromagnetic or gravitational fields, supposing that all objects, whether organic or inorganic (*i.e.*, nonliving), possess such fields. Psi-fields are seen as interacting with known physical fields and with each other, giving rise to phenomena at both animate and inanimate matter systems.

G. D. Wassermann, on the other hand, relates his postulates to quantum mechanics. Psi-fields, which enable individuals to have paranormal experiences, are regarded as having "very narrowly spaced energy levels" and "occupy wide regions of space." Thus, according to Wassermann, psi-fields emit and receive "extremely small quanta of energy"—typically smaller than quanta which can be absorbed by matter fields of classical physics.

Various efforts have been made to prove these hypotheses. An instrument for this purpose is the color centrifuge shown in Fig. 3. The device consists of an electric motor activated for a fraction of a second by pushbutton and a high-voltage field exciter. A paper card, upon which there are deposited a few drops of paint of different colors, is spun by the motor's disk. The entire assembly is housed in a transparent vacuum vessel.

To use this equipment as a psi-confirming aid, the experimenter concentrates on the image on a separate card and directs his thoughts upon the card in a centrifuge. With the paint in place and the motor energized, the machinery should now produce an identical or quasi-identical image of the original. This appears to work with some people and may be classified as telepathic/psychokinetic, since thought triggered a mechanistic replica.

Psi-type work of this kind ties in with experiments in the

"dream" area. At the Maimonides Medical Center in Brooklyn, for example, it appears that its dream laboratory was able to induce mental images telepathically in sleeping persons by an "agent" located in another room, about 100 feet away. The transmitting person, the agent, concentrates on a picture chosen from a group of famous paintings and tries to direct this thought-image at a sleeper. The lab was established in 1962 and, according to Drs. M. Ullman and S. Krippner, results have been good.

Dream-type work apparently has much promise for electronics, since sleep itself can be induced by electronic pulse generators. No standards can be fixed at this time, since different people have much different susceptibility to artificial pulse trains.

Attempts at inducing dreams by purely electronic methods are stifled by the fact that there are no "bulk"-picture transmitters available. TV-type video signals are unpleasant to induce and sensations are restricted to a "feel" of the low-frequency vertical blanking pulses.

But even if the transmission mode could be solved, a number of parallel problems require major attention as well. Exterior and interior conduction properties of the human cranium apparently are much more complex than suspected. Sweat, for example, is a highly conductive agent which causes odd current paths and spread patterns. Skin and related measurements, as shown in the lead photo of this article, can be made by simulating the cranium's exterior with conductive mannequin heads. Although respective data can be valuable, questions attached to the explicit propagation of dream-provoking electronic signals towards given receptor and processing areas *within* the human brain remain unanswered.

### Paranormal Matrix

Dr. Gardner Murphy, recognized as a psychologist of distinction, is a prolific contributor to parapsychology. He suggested the idea that man's failure to use interpersonal psi communications frequently may be due to our "psychological insulation" from one another. To that end, others see electronics-based communications as an awkward crutch and primitive substitute for latent, natural abilities. However, the lack of performance at psi-type levels can also be understood as Nature's safeguard against devastating telepathic impact. Otherwise, the world of man would function like an untuned radio receiver—too many messages would trigger chaos, intelligent action become impossible.

These considerations, taken together, have invited a search for discriminating devices and specific mind-intercoupling agents.

One of the most intriguing things to emerge in that area is the now-famous *Backster Effect* (ELECTRONICS WORLD, October, 1969). Here, since living plants seem to react bioelectrically to thought-images directed at their over-all well-being, New Jersey cytologist Dr. H. Miller thinks that the phenomenon is based upon a type of "cellular consciousness."

These and related considerations lead to the idea that psi is but a part of a so-called "paranormal matrix"—a unique communications grid that binds all life together. Its phenomena apparently work on a multi-input basis which operates beyond the known physical laws.

Some of these constituents can be seen in highly refined experiments of the Backster type. For example, a variety of electronic systems is employed to furnish pure audio tones, music, red light (as a growth stimulant), and excitation currents to the plants (Fig. 4). This provides the specimen with an emphatic "work psychology" or environment which can be disturbed for data-gathering purposes *after* lengthy conditioning.

To that end, psi-sensitivity can reach such a highly cultivated level whereby a plant (in our example) reacts to its owner's state of mind emotionally—even while he is far away. The data is expressed, of course, in the form of an electronically derived and processed biogram which is supplied with



Fig. 4. Experimental setup using Backster Effect for checking psi phenomena in living plants by subjecting them to artificial excitations (currents, red light, etc.), and monitoring responses. Note the red-light growth stimulator on Faraday cage.

time markers for identification purposes, as shown in Fig. 5.

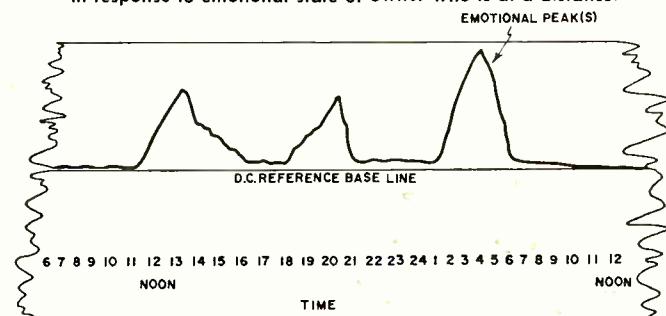
### Conclusion

Only a small family of experimental systems and approaches could be described. The field is complex, quite strange in many ways, but wide open for improvement. Indeed, as it appears from here, there is enough promise to warrant intensified research efforts. From an educational point of view, it's also necessary for investigators to look beyond their specialties and acquire more background knowledge in order to do meaningful work in a field such as this. ▲

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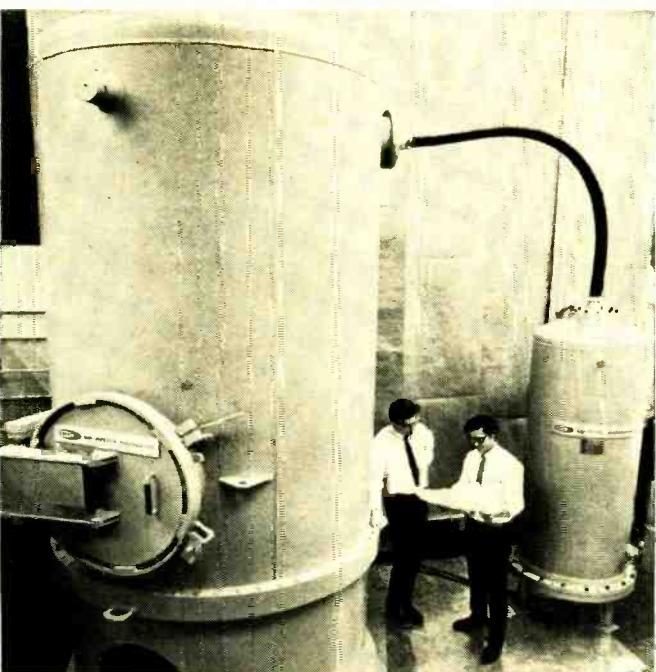
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Fig. 5. Biogram demonstrating psi-sensitivity level of plants in response to emotional state of owner who is at a distance.





# RECENT DEVELOPMENTS IN ELECTRONICS

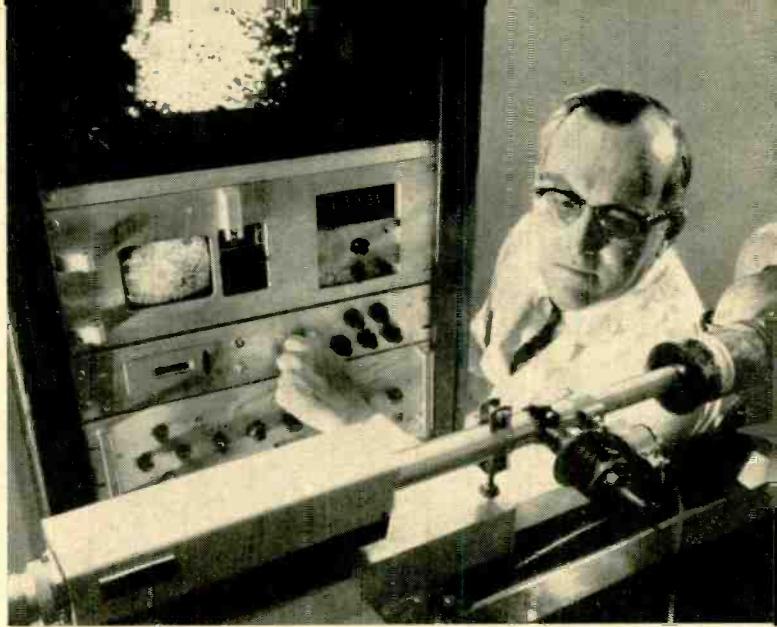


**TV Eyes for Delaware Bridge.** (Top left) From this vantage point 220 feet above the road surface of the twin-span Delaware Memorial Bridge, a TV camera will keep constant watch over traffic flow and road conditions. A second TV camera will be installed on the span's other tower, and two more cameras will be located atop the other span's two towers. Located in special housing in which they will be free to pivot and tilt in all directions, the cameras will be monitored on four 23-in TV monitors in the communications room below. Special windshield wipers are used to keep camera housings clear and clean. The cameras are specially adapted Sarkes Tarzian transistorized units, equipped with 1 1/4-in Plumbicon pickup tubes and zoom lenses. In designing the packages for the TV cameras, they had to be made small enough to fit through the small doors of the bridge-tower elevators. The TV system will be linked to the extensive communications and signaling network already in use by the Delaware River and Bay Authority. The CCTV system is being installed by U.S. Underseas Cable Corporation.

**Million-Volt Radar Modulator.** (Center) The two huge components in the photo are the radar modulator for an experimental Air Force radar. This radar is being developed to demonstrate the feasibility of a very high peak power, nanosecond radar system. By using higher powers, radar range should be increased so that targets will be detected at greater distances. By using shorter pulses, range resolution, or the ability to pick up separate targets that are closer together in range, should be improved. The modulator operates in the megavolt range, and it can produce extremely short pulses that are measured in nanoseconds (billions of a second) rather than microseconds (millions of a second). The equipment is produced by Ion Physics Corporation for Varian Associates.

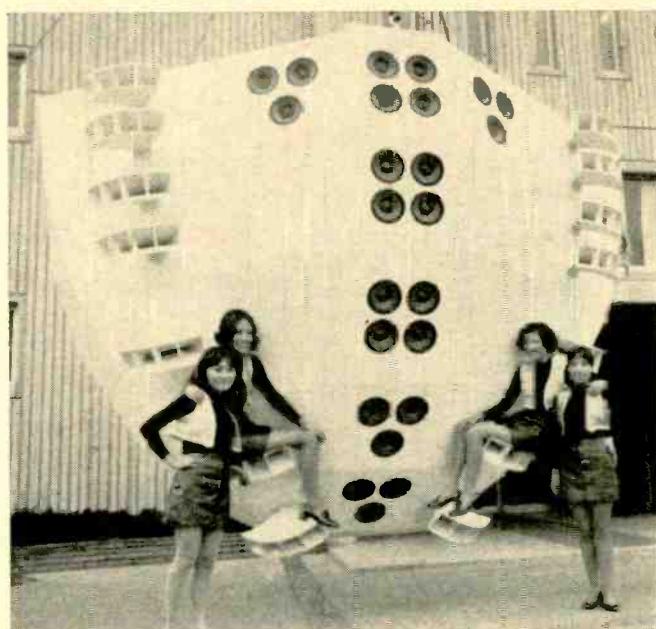
**Underwater Public-Address System.** (Below left) An advanced high-fidelity public-address system is being used in a unique film-making venture—to search for the great white shark which inhabits the waters of the Indian Ocean. The underwater system provides communications between crew members while engaged in their beneath-the-surface activities. Heart of the system is a tiny audio projector operated by a 200-watt amplifier that can illuminate a large underwater work area with acoustic signals. This enables cameramen working in deep waters to hear communications signals at a level equivalent to normal conversational speech at a distance of more than 100 feet from the projector, without special receiving apparatus. Speech signals are not only originated at the shipboard control center but also any member of the crew working below can broadcast over the system to every other member of the crew. This is made possible by a wireless sonar link to a receiving hydrophone suspended in the water. Each cameraman-diver has a microphone in his mask connected to a belt-mounted transmitter. The signal is picked up by the receiving hydrophone, demodulated, and rebroadcast over entire work area via the projector. System was developed by CBS Labs.

**Electronic Particle Counter for Metal Research.** (Top right) This high-speed counter, working in conjunction with its 300-power microscope, can count the thousands of tiny silicon particles in a polished surface area of an aluminum-silicon alloy in less than a second. To do the same job manually requires several hours. A CCTV camera scans the surface and flashes a picture onto a monitor. Electrical pulses from the particles in the study area are fed into the instrument's logic network, triggering the counters whose output is recorded for later evaluation. The instrument, designed by Reynolds Metals, is used in the company's research laboratories to measure particle size and distribution which affect the characteristics of aluminum.

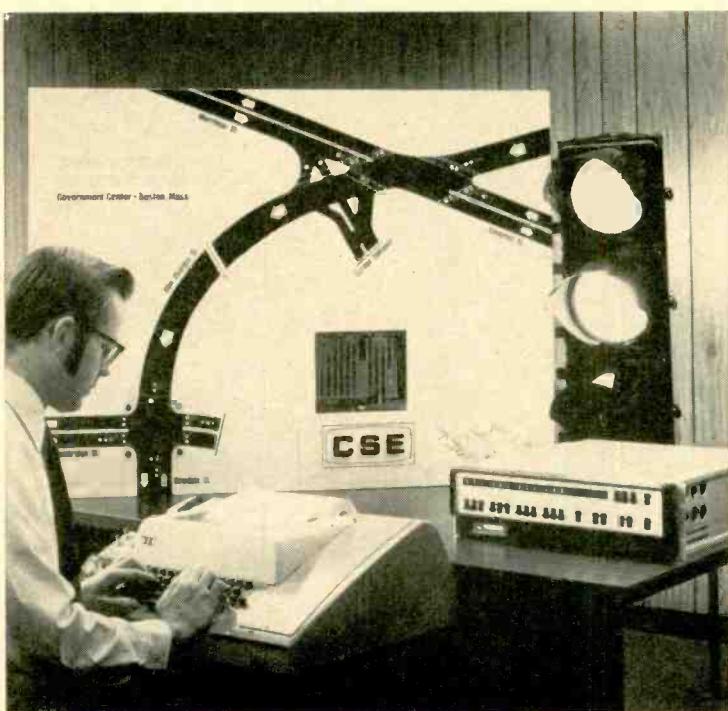
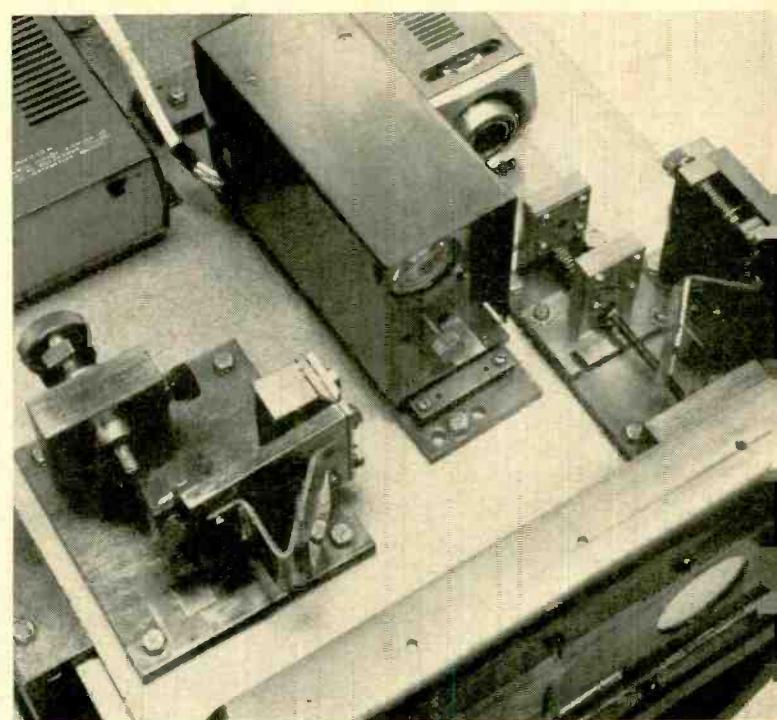


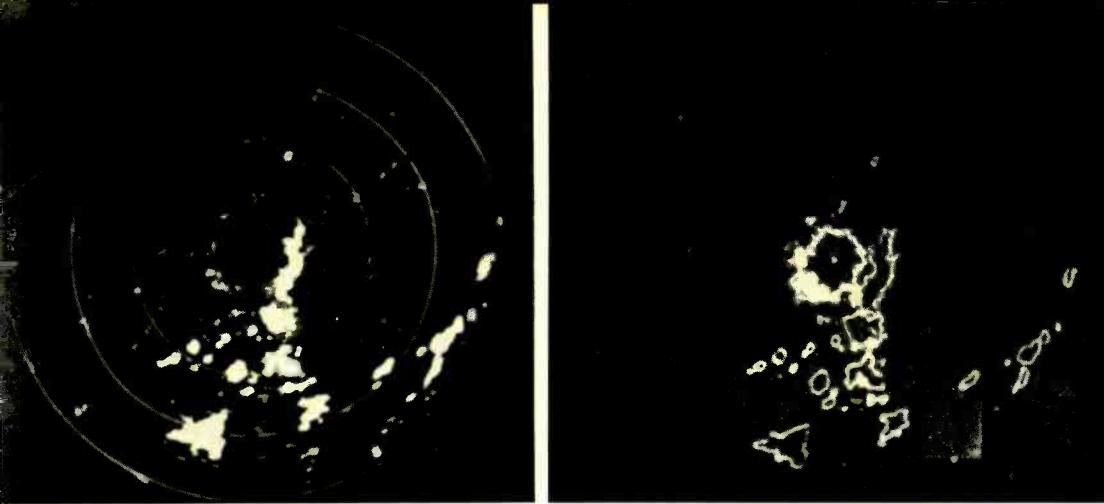
**Two-Ton Speaker for Expo '70.** (Center) Two gigantic loudspeaker systems, each weighing two tons, have been installed at the Festival Plaza of Expo '70 at Osaka, Japan. Each system has four 20-in woofers, 24 8-in mid-range speakers, and 14 multi-cellular tweeter horns, for a total of 42 speakers. The curved enclosures are suspended from the ceiling of the covered site, and are fed with 400 watts of power each. The loudspeaker systems will be used for public-address purposes. Systems were manufactured and installed by Pioneer Electronic Corp.

**Computer Traffic Control for Boston.** (Below left) Anyone who has done any driving in downtown Boston knows that the traffic and traffic-control leave much to be desired. Perhaps this computerized electronic traffic control system will improve things in the area it covers. The computer changes the traffic-light signals to meet the around-the-clock, constantly changing traffic needs. The traffic board in the photo shows the 32 light signals plus 24 walk/don't walk boxes, and four lighted pedestrian push-buttons in the Government Center area handled by the new system. System was developed for Boston's Traffic Department by Computer Systems Engineering.



**Laser Velocimeter.** (Below right) The components of a new laser velocimeter capable of measuring moving strip steel at better than 0.25-percent accuracy is shown. The device, located up to 15 feet from the moving strip, operates on Doppler-effect principle. The gas-laser beam is split to strike the metal from two angles. The difference in wavelength of the reflected light indicates speed of moving material. Readouts of material length and surface area can be in the form of digital display, printed cards, logs, or other printed records. Cost of equipment, made by GE, is in \$25,000 to \$30,000 range.





Radar scopes showing comparison between (left) conventional display of weather and (right) display using weather outline generator that only shows the outer contours of storms.

# Air Controller's Radar Sees Through Weather

By HOWARD L. McFANN / Project Manager, National Aviation Facilities Experimental Center, FAA

*Worried about flying in "bad" weather? Here's a new FAA weather-device that makes it possible for air traffic controllers to guide aircraft safely around all types of hazardous weather conditions.*

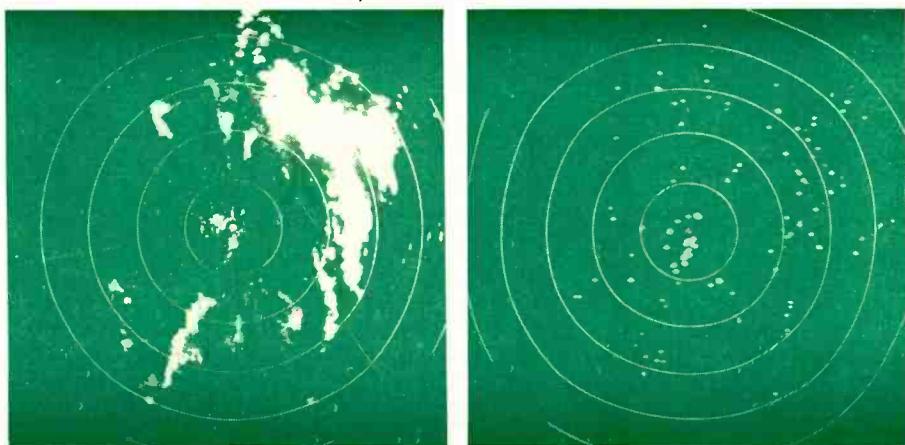
In an attempt to cut through the weather clutter that obscures vital target data on the air traffic controller's radar displays, engineers inadvertently created another potentially serious operational problem. As a result, a device, described in this article, was developed that solved this problem and opened new vistas for examining a storm's awesome proportions.

## Weather Clutter Obscures Aircraft

How would you like to control aircraft with your radar scope cluttered by heavy weather as shown in Fig. 1 (left)? The appearance of such clutter on radar scopes has long been considered unavoidable and it is obvious why it is necessary to clear up the display so aircraft target data can be followed more efficiently.

Persistent engineering effort resulted in design improvements, called "fixes," which enable the air traffic controller to cut through some of the interference. Most field radars are now equipped with several of these fixes; circular polarized antennas that discriminate against the signals returned by spherical particulate matter, such as raindrops, and

Fig. 1. Typical air traffic controller's radar PPI scopes showing (left) weather clutter interfering with identification of aircraft target data and (right) after removal of weather clutter by use of "automatic clutter eliminator."



logarithmic receivers with fast time constants to break up long clutter blocks.

A breakthrough in the problem of reducing weather returns appeared to have been made with the adoption of digital processing and narrow-band transmission of the radar video. The need to maintain low data rates on the telephone lines used to carry target information required stringent control of the false alarm rate, i.e., transmission of noise pulses as aircraft targets. The digitizer circuit that does this job is aptly referred to as an "automatic clutter eliminator."

The effectiveness of the clutter eliminator can best be judged by comparing the radar-scope photos shown in Fig. 1. Note that the radar signals on the time-correlated photograph of the digital display shown on the right are well defined symbols and that most of the dense clutter has been eliminated.

## The Problem

It soon became evident that complete removal of weather clutter by the digitizer gave rise to an equally serious operational problem. The air traffic controller was no longer able to provide pilots with essential weather advisories based on his personal observation of the radar clutter, and it became exceedingly difficult to maneuver aircraft around potentially hazardous weather such as convective storms containing damaging hail.

Clearly there was a need to satisfy both requirements: provide a see-through-clutter capability at low data rates *without* a loss of information about the storm's location, general size, and movement.

## The Solution

In attempting to answer this need, the Federal Aviation Administration worked with private industry to develop the weather-outline generator, a device that generates isoecho contours around the weather returns at any of

several preselected intensity levels. When coupled to the radar digitizer, the outlines are transmitted over the telephone lines along with aircraft identification and position data on a non-interfering basis.

With this additional input to his display, the controller can now see the storms picked up by his radar as sets of distinctive symbols outlining the precipitation areas.

### System Description

Fig. 2 is a simplified block diagram of the weather-outline generator. The device computes a continuous voltage estimate of the mean reflected power returned from small incremental areas of the storm scanned by the radar beam and is derived by integrating the clutter signals over an area 1.0 nmi in range by eight radar triggers (approximately 0.8 degree) in azimuth. The estimate is computed in this manner to reduce the likelihood of targets or strobotype interference being contoured as weather.

In range, the voltage is obtained by simply dividing the summed output of a tapped delay line by the number of taps. This produces a current sweep estimate of the mean clutter power received during the delay-line interval. Seventy-five percent of this voltage is then combined in another adder with 25 percent of the estimate computed for the previous sweep over the same range interval. The antenna has, of course, moved slightly during this period so that the resulting voltage represents the average clutter power received by the radar over the area bounded by both delay parameters; that is, the delay in range and azimuth. The weather outline points are generated from this voltage in threshold comparators, or slicers. Two slicers are presently used and they can be set to trigger at any level within the range of the system.

For best operation, the video input to the outline generator should be logarithmic with at least a 60-dB dynamic range to cover the intensity levels encountered in the strongest storms, and the radar fixes, used to reduce clutter, should be either turned off or bypassed.

Several refinements are incorporated to improve the integrity of the weather intensity estimate. Examples are the feedback loop that compensates for drift in the radar receiver's ambient noise level, and the swept-gain circuit, called the Sensitivity in Range Control (SRC), that corrects for the decrease in received signal power as a function of range. The SRC is needed because the echo power from precipitation varies as the inverse square of the range. If this correction were not applied, a close-in storm of low intensity would appear as strong as more severe weather farther away.

### Performance

The prototype outline generator was tested at the FAA's National Aviation Facilities Experimental Center near Atlantic City, New Jersey and far surpassed the original performance requirements. Not only did the system effectively outline the periphery of storms (photo on right of lead figure), it probed deeply into the clutter to define the stronger, more dangerous cells. This now provides a capability the controller did not have with his conventional display because of its narrow dynamic range.

Fig. 3 demonstrates the ability of the system to look into the heart of a storm. The weather activity portrayed consisted of widespread rain showers containing a small, yet dangerous tornado. The picture on the right is what the controller would normally see on his display scope. Note that it is impossible to discern the tornado from the relatively harmless rain that surrounds it. A picture of the outline generator output after transmission over the telephone lines is on the left. The outer edges of the storm were outlined by the series of dots, while the heavier, more dangerous cells were indicated by the "x" symbols. The location of the tornado was clearly displayed to the controller.

A production contract has been issued for procurement of equipment incorporating improvements in the original design. For example, the long time delay used to store the clutter power estimates from sweep-to-sweep was accomplished in a range-ordered core memory, which will now be done by less expensive shift registers. All of the mathematical operations in the prototype were performed by analog circuits; the new system is a hybrid that uses both analog and digital processing to best advantage.

Constructed with integrated circuits, the production unit will be housed within a 21" x 25" x 30" cabinet. As the equipment comes off the line, it will be included in the FAA's semi-automated air traffic control systems now being installed at high-density Air Route Traffic Control Centers around the country.

The development of the weather-outline generator is a good example of how the FAA continuously improves the electronic systems used by the air traffic controller to keep aircraft moving safely along the busy airways. ▲

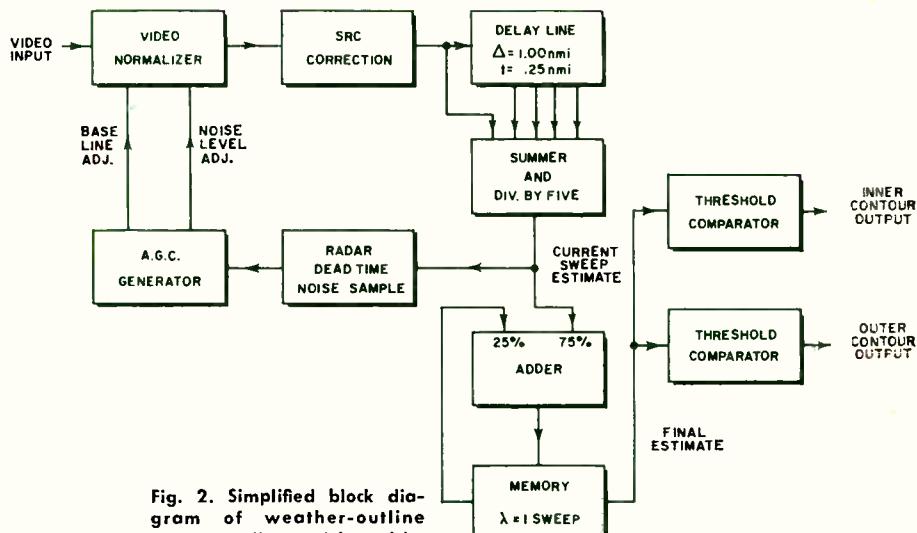
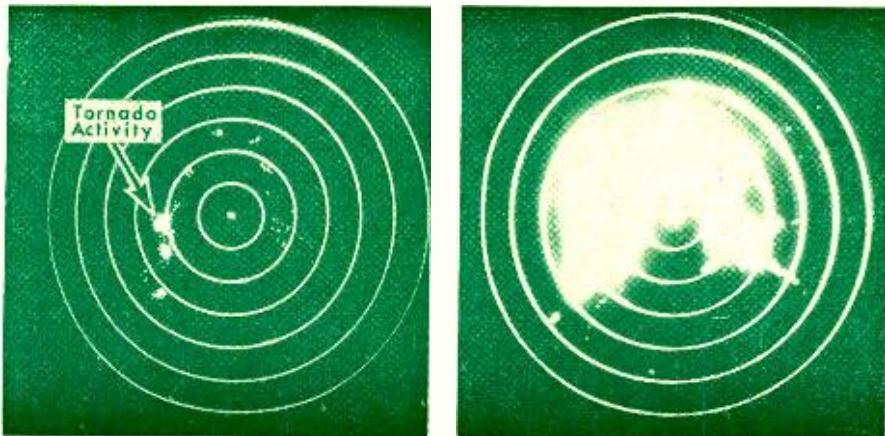


Fig. 2. Simplified block diagram of weather-outline generator discussed in article.

Fig. 3. Comparison of (left) digitized and (right) conventional wide-band radar display responses to tornado activity.



# INTEGRATED CIRCUIT MEMORIES

## Growth and Future (Part 2)

By DALE MRAZEK  
National Semiconductor Corp.

*New assembly methods and anticipated technological advances paint a bright picture for the IC memory market—and especially for bipolar devices.*

LAST month, Part 1 of this article described the read-write and read-only (ROM) memory IC's being developed for the computer memory field and the bipolar and MOS technologies used in producing them. This month we will describe the use of IC memories in such applications as scratchpad memories and shift registers and how, through circuit innovations, larger and faster storage memory arrays can be arranged. In addition, considering present design trends, the future of IC memories will be examined.

### Bipolar Scratchpads

The high cost of bipolar memory IC's limits their applications at present. One notable exception is found in bipolar scratchpads, which began replacing small, magnetic-film memories in computer main frames more than three years ago. Some scratchpad IC's are also used as registers and *vice versa*.

State-of-the-art in bipolar scratchpads is a capacity of 16 bits and a cycle time of 100 ns. Bipolar registers, designed as storage building blocks, typically attain a data rate of 25 MHz, while dissipating about 35 mW per bit. However, many designers still prefer to use standard TTL quad latches in these applications.

The bipolar scratchpad IC's generally contain set/reset flip-flops as the storage cells. One popular cell design, shown in Fig. 1, top, looks simple, but took a few years to produce

reliably. Until recently, IC developers called it the "forgetter" because of its tendency to change state randomly. Although the example of the storage cell shown in Fig. 1, bottom, appears more complex than the "forgetter," it is still being produced four years after its inception and is located on one of the few bipolar scratchpad IC's that contains an integral decoding network.

This type of scratchpad design was originally made for *Scientific Data Systems' Sigma 7* computers, and has been used to build registers and scratchpads containing up to 4096 bits. These storage cells have four applications in the Sigma 7 computer: (1) general registers that speed up the central processing unit's response to interrupt requests, (2) main-memory mapping, (3) key and lock storage for memory protection, and (4) input-output channel buffers. With external comparator logic to identify stored data by a key-word matching technique, the chip can also be used as a content-addressable (CAM) building block.

A representative 16-bit scratchpad array that is used to form larger arrays is shown in Fig. 2. Some manufacturers are assembling the multi-array planes as hybrid IC's; for

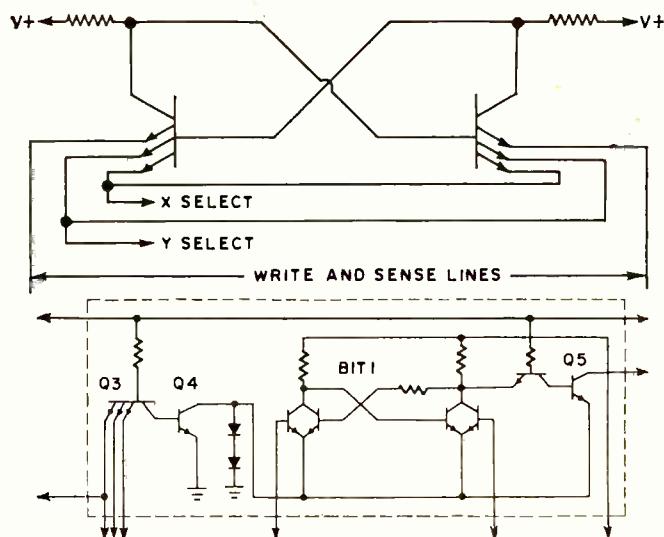
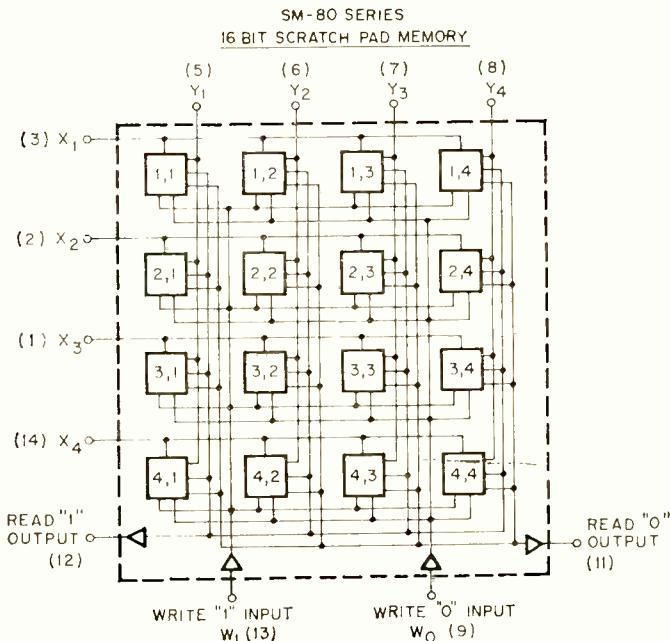


Fig. 1. (Top) Typical bipolar read-write, random-access set/reset flip-flop storage cell used in high-speed scratchpad IC's and (bottom) storage cell used on one of the few bipolar scratchpad/register IC's also containing decoder network.

Fig. 2. Sylvania's 16-bit bipolar scratchpad memory array.



example, eight 16-bit chips would be used to make a 128-bit hybrid IC. A typical hybrid IC is about an inch square and can cycle somewhat faster than 100 ns due to shorter lead lengths. The hybrids are an interim step between the 16-bit blocks and the large bipolar arrays of 32 and 64 bits that are being developed with LSI techniques.

In contrast, MOS monolithic scratchpads storing 64 bits do not utilize the present capabilities of MOS technology economically. Monolithic 256-bit MOS scratchpads will soon be in production and will feature random-access read-write, nondestructive readout, multiple-package decoding on the chip, operating rates of 4 MHz, and input-output compatibility with bipolar logic.

Fig. 3 outlines the configuration of such a scratchpad designed to go into a 16-pin package that will be faster than ferrite-core scratchpads, cost less to build, and be more efficient volumetrically. Alternate configurations include storage of 256 1-bit words with the pin arrangements shown, 128 2-bit words, and 64 4-bit words.

### MOS Shift Registers

MOS shift registers are the semiconductor equivalent of delay lines and can also be used as drum-type memories. These applications generally demand high capacity (several thousand bits of serial storage per chip) but not necessarily high speed. MOS registers with up to 512 storage stages are now being produced, compared with the bipolar maximum of 16 bits.

The main advantage that shift registers have over conventional delay lines in storage applications is clock control. Other advantages include elimination of transducers, amplifiers, and electromechanical drives, thereby reducing system "overhead" costs, and relatively low power dissipation. At present, the capacity at which it is cheaper to use MOS registers is several thousand bits in delay-line applications and about 200,000 bits in drum-memory applications.

Since shift rates are clock-controlled, storage or delay time is electrically variable. This feature may be used to synchronize parallel delay lines or drum-memory channels, to read in at low speed and read out at high speed in buffering applications, to reduce clock rates and conserve power between accumulator read-in and read-out operations, and to independently vary the times in delay-line segments. At minimum clock rates, average power dissipation in the range of a microwatt per bit can be achieved with MOS dynamic registers.

Words stored in a shift register or accumulator may be selected by applying a time address to the output control or by the CAM key-match technique.

Words can be read out sequentially from a channel in a drum-type system (Fig. 4A) or a few channels can be organized to present word bits in parallel. The TTL/MOS multiplexing technique shown in Fig. 4B multiplies the apparent speed of the MOS registers and achieves very high data rates. The speed record for this type of system appears to be 50 MHz, which American Astrionics reportedly achieved in a hybrid MOS/TTL IC, using specially designed shift registers.

A recirculation, or data-feedback, loop is generally used to obtain long-term storage. Several examples of register recirculation controls are: external TTL control gates (Fig. 5A), a 4-MHz accumulator with internal MOS controls (Fig. 5B), and a 3-register chip with internal controls (Fig. 5C). The taps at the 60th-bit positions (Fig. 5C) enable external bipolar logic IC's to make logi-

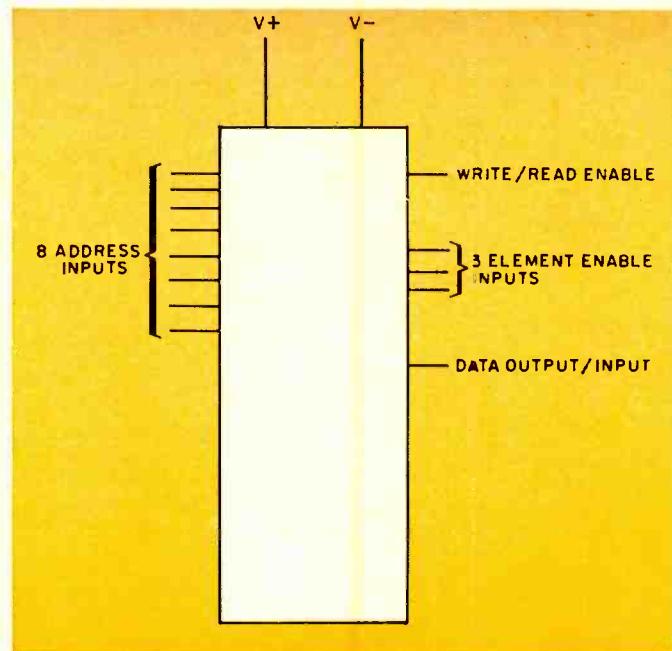


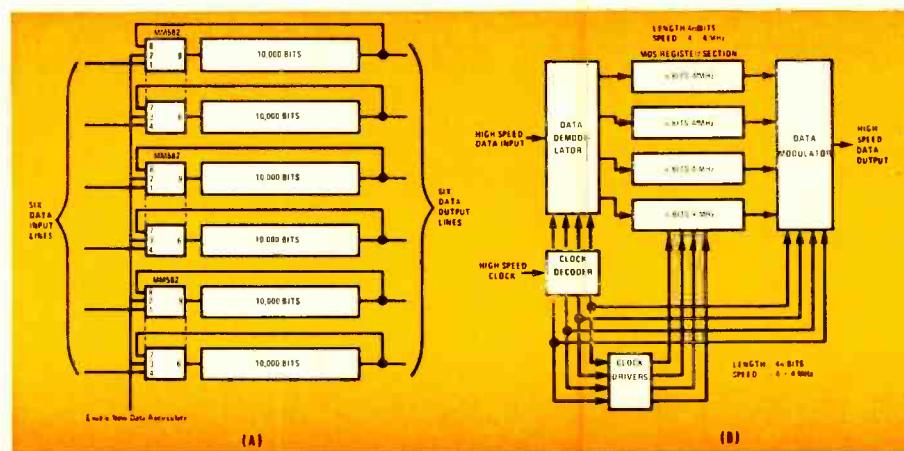
Fig. 3. Configuration of 256-bit, 16-pin package MOS scratchpad that is faster and less expensive than core scratchpads.

cal corrections to the data in four clock periods without retarding the recirculation flow.

The two generic types of MOS registers are static and dynamic. The storage cells of static types are latching circuits that will retain data while the clock is stopped, while dynamic registers must be clocked at some minimum frequency. The dynamic registers depend upon charge storage for data retention. If the clock is stopped, the charge will dissipate as leakage current, in a time that varies with temperature. Low-leakage types can be clocked as slowly as 100 Hz at room temperature. Standard dynamic registers are clocked with a two-phase signal, as in Fig. 1 (Part 1), and standard static registers take a single-phase clock and generate complementary clocks internally.

The main thrust of bipolar LSI development is aimed at the enormous computer memory market that is still dominated by cores, chiefly computer main memories. LSI is expected to increase bipolar IC capacity to 64 bits in the near future and to as much as 256 bits in the mid-1970's. Bipolar ROM's with capacities of 512 bits and content-addressable building blocks with capacities of 8 bits are also in development.

Fig. 4. (A) Drum-type register, built with shift registers, permits words to be read out sequentially from the selected channel. MOS switches at left of register control data read-in and recirculation. (B) Multiplexing data into parallel MOS storage registers multiplies the effective shift rate. With four channels, four times the normal MOS rate can be had if bipolar elements are used for control logic.



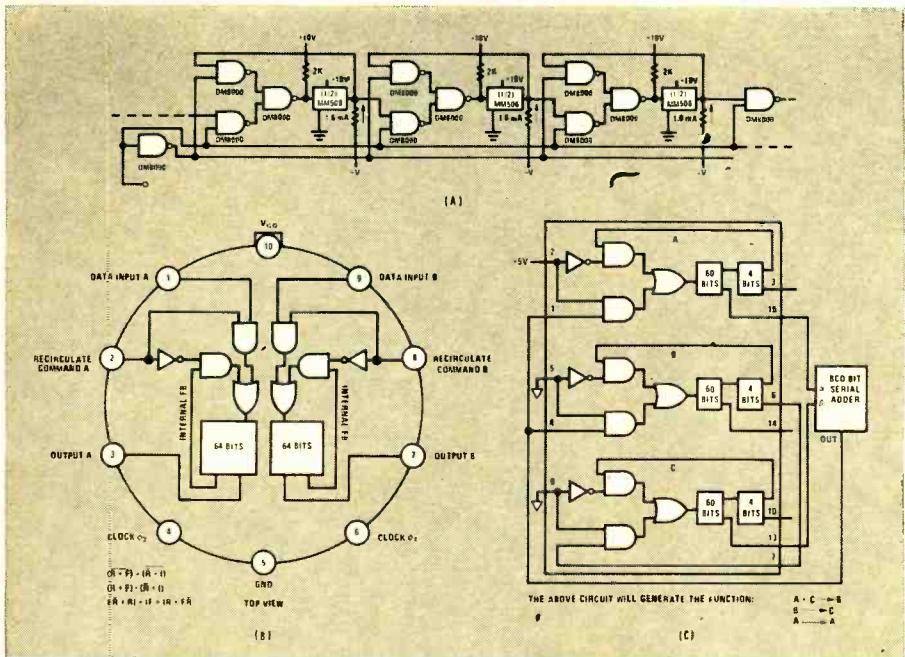


Fig. 5. Examples of recirculation loops. (A) TTL controlled high-speed segmented delay line, (B) dual accumulator with internal MOS controls, and (C) triple-shift register with internal controls for electronic calculators. Data can be corrected by external bipolar logic during the 61-64th bit intervals and re-inserted in loop without changing shift rate.

Considerably higher capacities and lower costs can be expected from the *p*-channel or *p*-MOS process in ROM's, registers, and medium-speed, read-write RAM's. A process known as C-MOS, using complementary *n*-channel and *p*-channel storage devices (Fig. 6A), looks promising for high-speed, low-power scratchpads. RCA, which has been developing this process under an Air Force contract, reports cycle times of 100 ns with standby power dissipation in the nanowatt range. However, C-MOS densities are low compared with *p*-MOS (see table in Fig. 6), and the larger number of packages required limits speed to about 250 ns

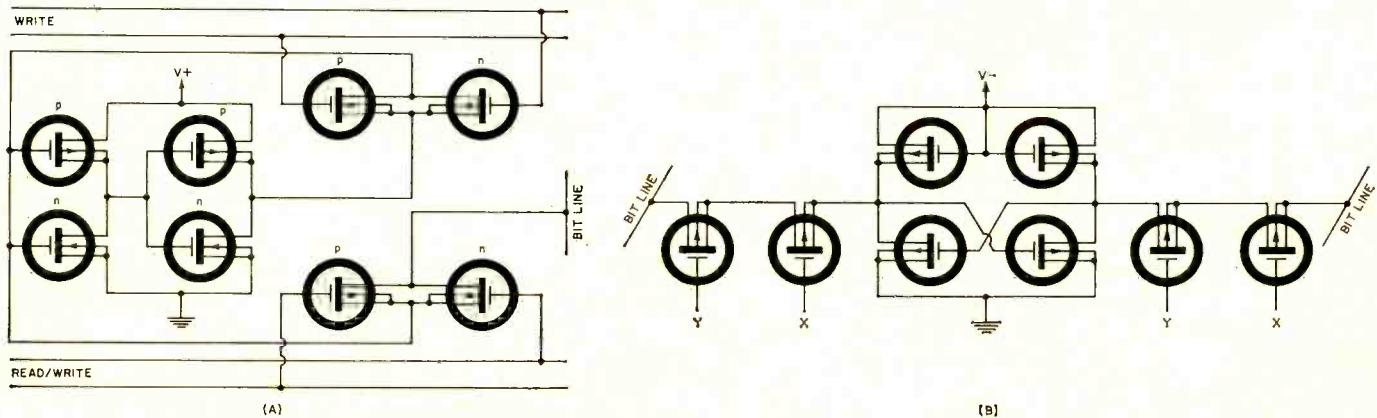


Fig. 6. Anticipated future LSI memory characteristics and schematics of the (A) C-MOS, (B) p-MOS, and (C) bipolar storage cells used in laboratories today to develop IC memories that will be competitive with ferrite core and other memory devices as far as performance and cost are concerned.

TECHNOLOGY	CELL AREA (sq. mils)	SPEED (ns)	POWER (Cell only, mW)	TYPICAL CELL
C-MOS	80	200	$10^{-6}$	Fig. 6A
P-MOS	15	250	0.01	Fig. 6B
Bipolar	10	100	0.5	Fig. 6C

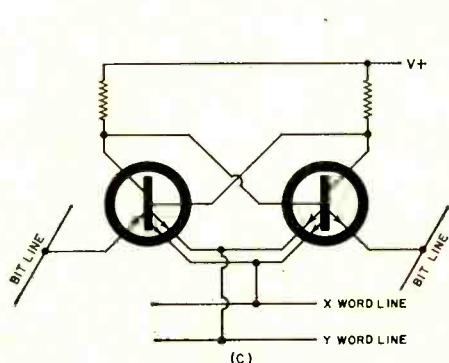
in most applications. Rates two to three times faster than standard MOS have also been achieved by overlapping the operation of *p*-MOS cells (Fig. 6B), but this requires expensive, complex, polyphase clocking networks.

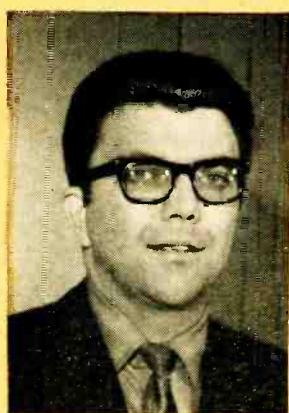
An interesting example of next-generation LSI bipolar registers is Raytheon's 4-bit register/counter cell, which contains 80 *nand* gates. It is claimed that arrays can be assembled as scratchpads, command memories, and logic-function memories. The memories control data flow and set up the registers to perform any of 16 functions, as required by each processing task.

The table in Fig. 6 summarizes one prediction of things to come in the early 1970's. Bipolar cell size (Fig. 6C) in random-access, read-write memories is expected to drop drastically as the number of minimum-geometry, minimum-power internal cells rises, and the number of buffers per cell drops. The bipolar devices are expected to cost less than 2¢ per bit if 256-bit chips are used in 4096-bit hybrid IC's.

Although this would make bipolar IC's competitive in cost and more than competitive in speed with core memory, core proponents hope to cut their costs in half in the 1970's. If that happens, it may be a very slow phaseout. However, cores are not the only competition on the horizon, since developers of thin-film, sonic-film, cryoelectric and optoelectronic memories are also competing with core memories as far as performance and cost are concerned.

No significantly new semiconductor process has been developed for several years. LSI, whether MOS or bipolar, is an extension of earlier techniques, made possible by improvements in masking optics and other processing methods and equipment. Increases in producible (Continued on page 63)





The author joined E.F. Johnson Co. in 1966 and in his present position is responsible for all development engineering pertaining to the entire component line. From 1962 to 1966, he was associated with General Electric Co.'s General Purpose Control Dept. He received his BSME degree from the University of Nebraska in 1962 and an MSME from Bradley University in 1965. He will complete requirements for an MBA degree at Mankato State College this June. He holds patents in capacitor, connector, and switch devices. He is a registered professional engineer in Minnesota and Illinois.

## Air-Dielectric Trimmers

By JACK L. BOWEN / Manager, Component Development, E.F. Johnson Co.

*Relatively small size, top performance, and low cost are main features of the air-dielectric, plate-type trimmer described. Here is what must be known in order to specify such trimmers.*

AIR trimmer capacitors are among the most popular trimmers due to the very favorable trade-off between cost and performance compared to solid-dielectric trimmers. Air trimmers are used in countless circuit applications. A few basic, specific examples are: tank circuits, filters, stable oscillators, helical resonators, and attenuators. These circuits are frequently used by manufacturers of communications equipment, such as business and personal two-way radio and aircraft transceivers. Manufacturers of such test equipment as oscilloscopes and counters, as well as medical electronics gear, also utilize these trimmers.

Some confusion exists between the terms "air trimmer" and "air tuner." Most manufacturers agree that tuner capacitors exhibit a rotational life in excess of 1000 tuning cycles while air trimmers most frequently exhibit rotational lives between 250 and 1000 tuning cycles. A tuning cycle is defined as 180 degrees rotor rotation in one direction and a corresponding 180-degree rotation back to its original position. Air trimmers are typically used inside equipment to peak or null a circuit and generally are not readjusted except for equipment calibration or repair. Tuner capacitors are typically used where frequent capacitance variation is required. Tuner capacitors are usually supplied to a straight-line-frequency or straight-line-wavelength tuning curve, while trimmers are commonly straight-line-capacitance devices (see Fig. 1).

Air trimmers can be categorized by construction, performance, mounting, and size. They range in price from one of the very lowest priced trimmers to one of the very highest priced trimmers. All have two features in common: (1) all use air as the primary dielectric, and (2) all require supporting members to position the rotor and stator. Because of these two features, we are faced with certain limitations.

The basic equation for the capacitance between two flat plates with air as the dielectric is:  $C = 0.0085KA/t$  where  $C$  = capacitance in pF,  $K$  = dielectric constant (for air,  $K = 1$ ),  $A$  = facing area in  $\text{cm}^2$ , and  $t$  = distance between plates, in cm.

As you can see, capacitance of an air trimmer can be increased only by using more plate area or by decreasing

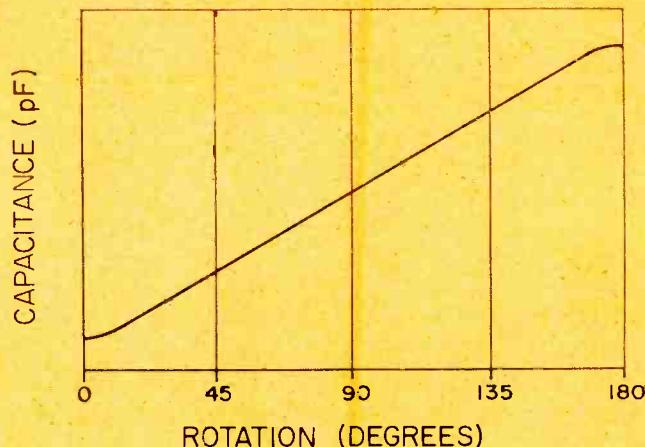
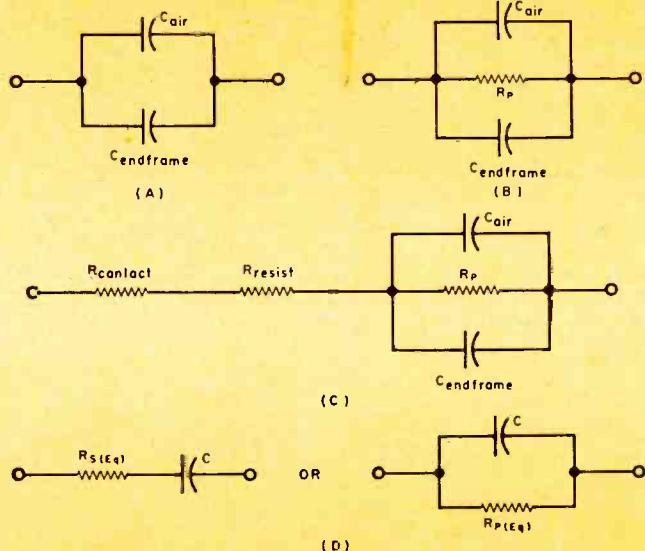


Fig. 1. Normal air trimmer tuning curve shows a capacitance variation that is linear with degrees rotation.

Fig. 2. Equivalent circuits of air trimmer capacitors.



DIELECTRIC MATERIAL	DISSIPATION FACTOR (at 1 MHz, 25°C)
Air	0.0000
Teflon	0.0002
Quartz	0.0002
High Alumina (95%)	0.0003
Stearite Grade L-5	0.0020

Table 1. Dissipation factors of some common dielectrics.

the plate spacing. Of course, as the spacing is decreased, the breakdown voltage decreases proportionally. Obviously, as the trimmer size decreases, capacitance values and/or voltage breakdown values must decrease. Certain capacitor configurations make more efficient use of the volume required. These configurations will be discussed later.

All air trimmers are, in reality, a composite of two capacitors; the air capacitor plus a solid-dielectric capacitor whose characteristics reflect the properties of the capacitor supporting member(s) or endframe. The endframe characteristics are important because the equivalent capacitor appears as shown in Fig. 2A.

If the capacitance through the endframe represents a significant percentage of the total capacitance, the resulting capacitor may be appreciably degraded in operating characteristics from the anticipated air-dielectric capacitor.

As an example, let's consider capacitor "Q," temperature coefficient (TC), and humidity performance. The "Q" of a capacitor is defined as the cotangent of the loss angle and is generally considered to be better as its value approaches infinity. The "Q" value, also known as the "quality factor" may also be defined as follows:  $Q = 1/DF = R_p/X_C = X_C/R_s$  where:  $DF$  = dissipation factor of the capacitor dielectric,  $R_p$  = equivalent parallel resistance,  $R_s$  = equivalent series resistance, and  $X_C$  = capacitive reactance.

Thus, we see that a low dissipation factor dielectric will yield a high- $Q$  capacitor. Table 1 lists dissipation factors of common capacitor dielectrics and endframe materials. As can be seen from this table, any endframe material will degrade the "Q" of an air trimmer and it must be considered when selecting a high- $Q$  air trimmer. Additionally, most dielectrics exhibit different dielectric constants ( $K$ ) at various temperatures. If the endframe  $K$  varies with temperature, then its TC will also vary.

Stearite and alumina ceramics are porous materials which will take on moisture unless they are treated. "Q" and voltage breakdown may be appreciably degraded upon exposure to moisture if the endframes are not treated. The most common ceramic treatment is a fired silicon process which performs adequately in most situations. Some manufacturers glaze the ceramic to achieve the same goal.

An equivalent circuit of an air trimmer which reflects endframe losses can now be represented as in Fig. 2B.

We have shown that an air trimmer necessarily falls a

Table 2. Various types of air trimmer capacitors along with applications and their maximum performance characteristics.

Air Trimmer Capacitor	MIL-Spec Number	Typical Application	Relative Cost Range	Typ. Max. Cap. (pF)	Typ. Max. Volt. Rat. (V d.c.)	Relative Size	Current-Carrying Cap.	Typ. Nom. TC (ppm/°C)
Soldered plate	MIL-C-92A, Styles CT04, CT06, CT12, CT13, CT14, CT15	Used in low to medium-power transmitter tuning, loading, and matching networks. Can be used in oscillators, resonators, attenuators, and filters.	Medium	5-200	4500	Medium	Low-medium	0-100
Staked plate	MIL-C-92A, Styles CT06, CT12, CT13, CT14, CT15	Used in high-power transmitter tuning, loading, and matching networks.	Medium	5-200	4500	Medium	High	0-100
Bolted plate	none applicable	Used in very high power r.f. generating equipment and in transmitter tuning, loading, and matching networks. Good at high temp.	Medium-high	25-1000	13,000	Large	Very high	100
Milled plate	MIL-C-92A, Style CT16	Used in low-power circuitry where low cost, high "Q," small size, and stability are most important. Examples include oscillators, resonators, attenuators, and filters.	Low	5-60	1000	Small	Low-medium	34-45
Concentric ring	none applicable	Used due to low inductance, low TC and high "Q." Applications in microwave receivers and v.h.f.-u.h.f. communications equipment.	Medium-high	5-60	1000	Very small	Low	0

NOTES: Ratings represent maximum available for a given design type and may not apply to all designs.  
 \*Mountings: 1 = PC board; 2 = Panel mounting; 3 = Chassis mounting

little bit short of a perfect capacitor due to losses in the supporting endframe. Let's now look at the balance of the device. Since the trimmer is a variable capacitor, it must also have a sliding contact between the rotor and the rotor connection. This contact necessarily has some finite resistance and therefore appears as a series resistance to the total capacitor, thus further reducing "Q." Another resistance, that being inherent in the resistivity of the conductors themselves, adds still another series resistance. The air trimmer total equivalent circuit thus appears as in Fig. 2C. The equivalent circuit may be shown as in Fig. 2D, where:  $R_{S(EQ)}$  = total equivalent series resistance and  $R_{P(EQ)}$  = total equivalent parallel resistance.

Through the use of a nearly lossless primary dielectric, an air trimmer which is functionally designed will naturally exhibit better and more stable "Q" and TC characteristics than solid-dielectric trimmers.

Many circuits require the use of air trimmers at u.h.f. and higher frequencies where the inductance of the capacitor leads may become critical. Both the resonant frequency of the capacitor and the "Q" at high frequencies are very important. The length of the conductors, plating materials, and endframe materials are all important in determining high-frequency trimmer characteristics. Units particularly well suited for high frequencies include the concentric-ring (Fig. 3) and the milled-plate designs (Fig. 4) which utilize low-loss endframes and short terminals.

"Q" measurements are very difficult to obtain at frequencies beyond 250 MHz. No standard "Q"-meter is

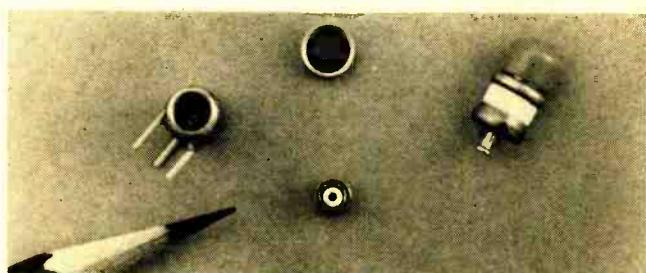


Fig. 3. Concentric-ring air trimmer capacitor is shown disassembled. Glazed ceramic and multiple rotor contacts are used in this device in order to keep losses very low.

available for measurement at these frequencies but many users obtain an indication of "Q" by looking at the relative bandwidth of a resonator or by looking at the insertion loss of a unit. Network analyzers are also used to obtain "Q" comparisons at high frequencies.

Capacitor manufacturers publish data based upon readings taken on either the *Boonton Radio 190A "Q"-meter* or a *Boonton Electronics 75-series capacitance bridge*. The "Q"-meter has a variable frequency feature which allows "Q" measurements up to 250 MHz with appropriate working coils. The capacitance bridge is a highly accurate device but its frequency is fixed at 1 MHz.

A need exists for equipment to accurately measure capacitor "Q" up to and beyond 1 GHz. Today, performance data beyond 250 MHz must be extrapolated from lower frequency data. The circuit designer has one bench mark in the fact that all trimmers exhibit lower "Q" with increasing frequency as is shown in Fig. 5. If "Q" is critical at high frequencies, a trimmer must be selected which exhibits high "Q" at lower frequencies.

#### Outstanding Features

The outstanding features of the air trimmer are high "Q," great stability, and low cost. Other features include their consistency of capacitance, "Q," and TC from lot to lot and from year to year. The typical temperature-coefficient curve (Fig. 6) shows excellent retrace and a nearly constant value for TC throughout the temperature range. Fig. 7 shows a common TC characteristic exhibited by solid-dielectric capacitors. However, TC is not readily modified in air trimmers and a negative TC is nearly impossible to obtain due to the growth of the meshing plates with increasing temperature. Typical air trimmer TC's range from zero  $\pm 10$  ppm/ $^{\circ}$ C for units manufactured with Invar plates or tubes to about  $+100 \pm 20$  ppm/ $^{\circ}$ C. Negative temperature coefficients can be obtained only through the use of special endframe materials or by the use of one or more bimetal plates.

An obvious limitation to air trimmers is the direct dependence of voltage breakdown upon physical size. Air trimmers are susceptible to reduced voltage breakdown in reduced pressure or in extremely "dirty" environments. Sealed versions, of course, do not have these shortcomings.

#### Regular and Special Types

Air trimmers are typically constructed by one of the following methods: soldered plate, staked plate, bolted plate, milled plate, or concentric ring (press fit or soldered tubes, impact extrusions or castings).

Table 2 lists the characteristics and applications of each type trimmer. Each type is best suited for a particular application. Table 2 should serve as a guide in the selection of an air trimmer. The milled-plate units are one of the newer configurations and are one of the best low-cost, high-performance small air trimmers available.

The milled-plate devices eliminate loose plates and offer sturdy, one-piece, current-carrying elements which are suitable at high frequencies. The concentric-ring devices

Typ. "Q" at 1 MHz	Typical Plating	Mounting Avail. <sup>s</sup>	Tuning Resolution
10,000	Nickel	1,2,3	Medium
7000	Nickel	1,2,3	Medium
4000	Unplated aluminum plates	2,3	Coarse
20,000	Silver	1,2,3	Fine
20,000	Gold	1,2,3	Extra fine

<sup>s</sup>agree with a particular manufacturer's standard devices.

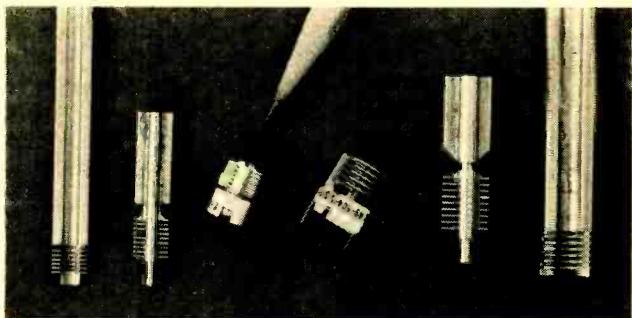


Fig. 4. Milled-plate air trimmer capacitors are shown with their respective brass rotor and stator extrusions. These units are especially suited for high frequencies.

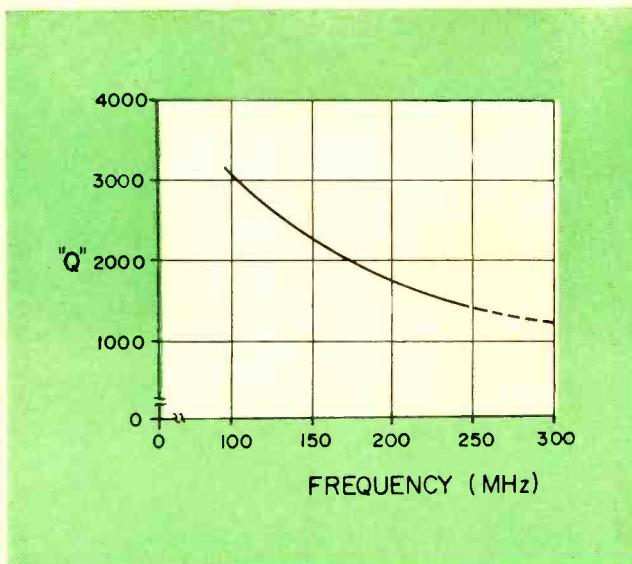


Fig. 5. Typical air-trimmer "Q" versus frequency. Above 250 MHz data must be extrapolated from lower frequencies.

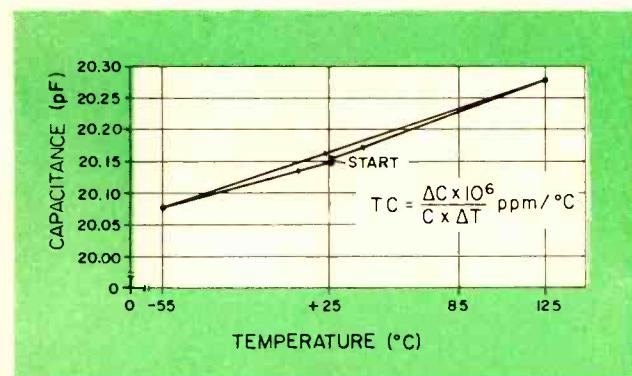


Fig. 6. Capacitance vs temperature of milled-plate trimmer. The temperature coefficient is approximately +50 ppm/°C.

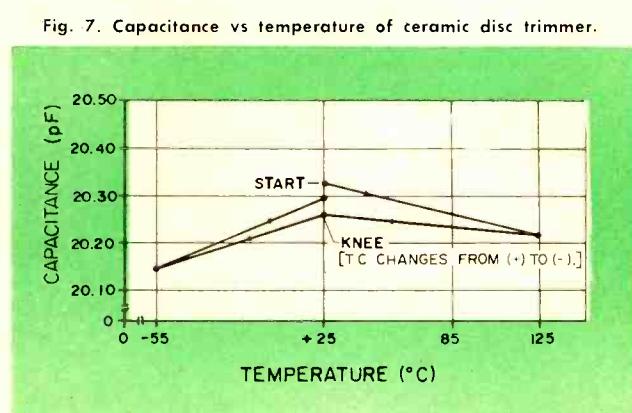


Fig. 7. Capacitance vs temperature of ceramic disc trimmer.

offer the shortest lead length and are most suitable at very high frequencies where cost is secondary to performance.

As can be seen from Table 2, each trimmer style has its outstanding characteristics. The user must first decide what capacitance is required, what "Q" is needed, and then decide which type trimmer he should use. The five types of units available have overlapping capacitance ranges and often share both desirable and undesirable features.

Variable capacitor manufacturers are conditioned to the needs of the user and consequently make available numerous special configurations upon request. For example, Fig. 8 shows a miniature low-cost tank circuit that can be supplied. Special terminations, plating, torque, voltage ratings, and capacitance ranges are frequently supplied to volume users of air trimmers. Low-torque trimmers utilizing ball bearings are frequently used to lengthen the rotational life and reduce tuning torque. Special plate shapes may be supplied to produce special tuning curves. Special terminal temper is often supplied to allow a user to stake-over the printed-circuit type terminals prior to wave soldering. This staking permits the PC board to be turned over without allowing the trimmer to fall off the board.

### Selection and Specification

Selection and specification of a standard catalogue air trimmer will save the user both time and money. Selection should begin with a list of *required* performance specifications. A wise applications engineer will insist on guaranteed ranges but will not select ranges beyond those specified by the circuit designer. Also, the use of a fixed padlock in series or parallel with the trimmer should be considered if it can result in the utilization of a lower cost or a more standard trimmer. Let's now assume that we need to specify a trimmer. What do we need to know? A list of characteristics must be prepared defining:

1. Cost
2. Capacitance range (maximum minimum and minimum maximum)
3. "Q" required (minimum value at 1 MHz)
4. Voltage rating required (use safety factors to de-rate for contamination, moisture, or altitude)
5. Rotational life (torque)
6. Resolution of tuning
7. Space available
8. Temperature coefficient and drift characteristics
9. Environmental conditions

In order to limit our problem, let's assume that we have decided to use an air trimmer because of its stability, "Q," cost, or other reasons. However, certain characteristics do not complement each other. For instance, a high capacitance and high voltage breakdown cannot both be offered in a small space. In other words, in a given space, additional capacitance in a given style trimmer can be obtained only at the cost of decreased voltage rating. Some style trimmers, however, offer a more efficient use of space (see Fig. 3) but will cost appreciably more than a unit such as the capacitor shown in Fig. 4.

Capacitor "Q" is largely dependent upon endframe and plating materials. When used at frequencies above 100 MHz, look for multiple rotor contacts, silver or gold plating, and low-loss high alumina endframes. Measurement of capacitance and "Q" in a shielded enclosure on a *Boonton Electronics* capacitance bridge is recommended for establishing and correlating vendor-user capacitance and "Q" readings.

Rotational life of air trimmers is usually 250 to 1000 cycles. A longer life can be offered at a premium price by using ball bearings in standard trimmers. The torque of trimmer capacitors usually ranges from 1 to 10 ounce-inches to enhance the mechanical stability of the capacitance setting. Most manufacturers test their air trimmers

for vibration and for shock according to MIL-Std-202C.

Resolution of tuning is important to some users. A higher degree of resolution indicates more degrees of rotation are required for a given change in capacitance. The concentric-ring construction offers a high degree of resolution.

Space availability often determines which type trimmer should be used. Small size does not necessarily mean high cost as can be seen in Table 2. The applications engineer must carefully weigh all criteria before selecting a capacitor.

Temperature coefficients of air trimmers can be selected with a high degree of confidence. A zero TC ( $0 \pm 15$  ppm/ $^{\circ}$ C) trimmer can be obtained by use of Invar tubes in the concentric-ring design. Small positive TC values such as  $35 \pm 15$  ppm/ $^{\circ}$ C are available in milled-plate devices. This TC merely reflects the coefficient of linear expansion of the brass rotors and stators used in their construction. Larger air trimmers offer a TC of up to  $+100 \pm 20$  ppm/ $^{\circ}$ C but, as can be seen by tight tolerance, these trimmers are extremely consistent. Air trimmers, as a family, offer excellent retrace of capacitance and exhibit very little drift upon temperature and/or humidity cycling. The use of poor endframe materials will, however, induce unwanted variations.

Environmental conditions place one of the most important limitations upon the use of air trimmers. Let's look at the three most important environmental factors: 1. temperature, 2. pressure (altitude), and 3. humidity.

Air trimmers are most commonly constructed by soldering the stator to the endframe with a standard 60-40 solder. The typical maximum temperature rating of such devices is 125 $^{\circ}$ C to 140 $^{\circ}$ C. This is not an ambient rating but a total temperature rating of the capacitor itself. Most manufacturers will supply identical devices with high temperature solder (H-T) which will boost the operating temperature allowed to as high as 200 $^{\circ}$ C. These temperatures must not be exceeded and extreme thermal shock should be avoided.

Air trimmers which are not sealed must be de-rated for use at high altitudes. As an example, the atmospheric pressure at 50,000 feet is 3.4 inches of mercury and a typical milled-plate trimmer will break down at 50% of its sea-level d.c. breakdown voltage.

Humidity will affect air trimmers if condensation develops on the endframe or on the capacitor plates. The effect of a severe humidity condition will be to lower "Q" and voltage breakdown and raise capacitance of the trimmer. Typical air trimmers exhibit less than 1% change in capacitance and not more than 20% reduction in "Q" and



Fig. 8. Miniature low-cost tank circuits can be supplied.

voltage breakdown after 24 hours at 60 $^{\circ}$ C and 95% RH (relative humidity). In general, this performance is far superior to that of solid-dielectric devices.

The applications engineer must use judgment in specifying an air trimmer. He must specify measurable quantities and the specified characteristics must allow for required manufacturing tolerances. An air trimmer specification should spell out at least the following characteristics:

1. Guaranteed minimum capacitance
2. Guaranteed maximum capacitance
3. Voltage breakdown (d.c.) at sea level
4. Minimum and maximum torque
5. Maximum physical dimensions
6. Mounting and/or terminal dimensions
7. "Q" minimum at 1 MHz
8. Type plating on all metal parts
9. Endframe material and treatment (if required)
10. Maximum and minimum TC
11. Solder type or maximum temperature of application
12. Acceptable supplier

Selection of the particular trimmer to be used must depend upon the relative importance of the various characteristics. Each application must be completely analyzed and the optimum trade-off of features must be established prior to the selection of the air trimmer. The ultimate trimmer selection must represent the best compromise of characteristics and cost for each individual application.

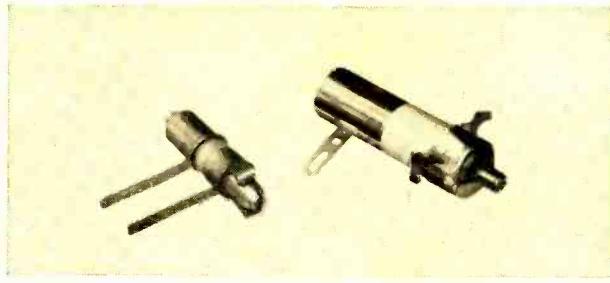
Many manufacturers offer sample kits and display boards to aid the applications engineer in his ultimate trimmer decision. ▲

## POLYSTYRENE TRIMMER CAPACITORS

BECAUSE of its excellent dielectric properties, polystyrene has been used in a variety of capacitor applications. One of these is in trimmer capacitors.

Polystyrene trimmers are available in both disc and tubular forms

Two styles of polystyrene trimmer capacitors.

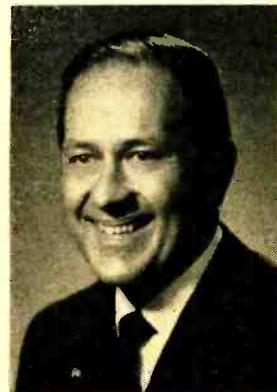


and are generally rated at 75 $^{\circ}$ C (167 $^{\circ}$ F) maximum temperature. Above this temperature the plastic softens enough to cause physical movement of any parts under stress. This thermal creep can cause a change in capacitance as well as possible mechanical failure.

With the low dielectric constant of 2.1, the capacitance ranges of polystyrene trimmers are low. Maximum capacitance of 8 pF is typical. The trimmers do exhibit excellent "Q," 1000 minimum, and good temperature coefficient. Polystyrene trimmers are economical capacitors intended for high-frequency applications. Typical price range for these trimmers is 10¢ to 15¢ each.

Soldering and cleaning operations are critical when using polystyrene trimmers. Because of the low temperature rating, these parts should be soldered using a very hot soldering iron. The heat can be transferred to the joint quickly and then removed before the trimmer itself reaches a temperature hot enough to cause damage. Also, since some solvents may dissolve the polystyrene, tests should be made on samples to determine their solvent resistance. ▲

The author received his B.S.E.E. and B.S.Ch.E. from Purdue University and from 1959 to 1966 served Erie Technological Products in various engineering capacities. Prior to that he was sales manager for Irvin Aaron Associates, and from 1949 to 1957 he served as assistant sales manager of the Centralab Division of Globe-Union. He is a member of IEEE and is the Chairman of the Ceramic Glass & Vitreous Capacitor Section, Parts Division, of the Electronic Industries Association.



# Ceramic Tubular Trimmer Capacitors

By WILLIAM G. TUSCANY / Manager, Applications Engineering, Centralab Electronics Div., Globe-Union Inc.

*Where reliable, low-cost capacitance trimming is required, the ceramic tubular meets the need. Information is included on ceramic dielectrics for both fixed and variable capacitors.*

**I**N the early 1930's a salesman from one of the ceramic supply houses had the foresight to realize the potential that could be developed for a new barium titanate ceramic material which he had heard about from component activity in Germany. This material could provide what in those days was high capacitance for a given size and at very reasonable cost. Soon two manufacturers in the United States started to use this material in fixed disc and tubular capacitors. From these meager beginnings, the ceramic capacitor industry has grown by leaps and bounds.

At the time the first material was used, little was known of its electrical characteristics. After application experi-

MOUNTING DETAIL	THREAD	A	B
	#6-32	.152"	.225"
#4-36	126"	190"	

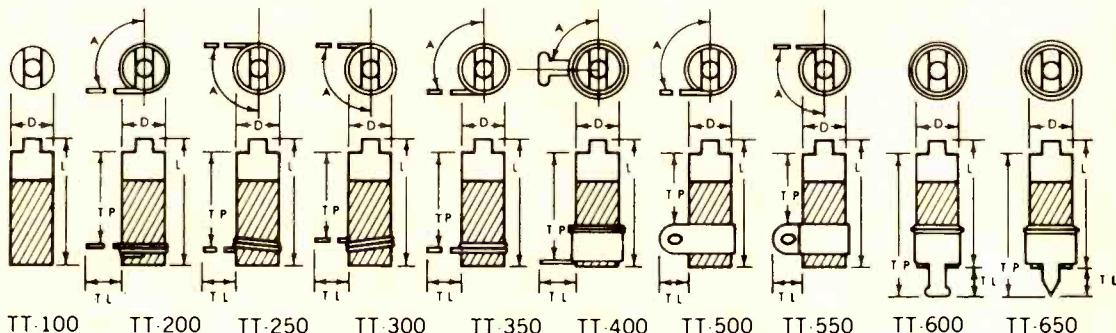
Tolerances  $\pm .005"$  Unless Otherwise Specified

A Mounting Hole Diameter

Fig. 1. Mounting-hole dimensions for tubular trimmers.

ence, it was found that it had definite and predictable temperature characteristics. This material evolved into what is now known as the N750 body, one of the temperature-compensating ceramic materials. It was found that this characteristic would be ideally suited to compensate for the positive temperature characteristic of coils

Fig. 2. Terminal configuration and dimensions for various types of ceramic tubular trimmer capacitors.



DIAMETER (D)	#6.32	.215	.215	.215	.215	.215	.215	N.A.	N.A.	.215	.215
	#4.36	.180	.180	.180	.180	.180	N.A.	.180	.180	N.A.	N.A.
TERMINAL (TL) LENGTH $\approx .032$	N.A.	1-1/2 Min.	1-1/2 Min.	1-1/2 Min.	1-1/2 Min.	.210	.160	.160	Variable	Variable	
TERMINAL (TP) POSITION						VARIABLE					
ANGLE (A)	—					ANGULAR RELATIONSHIP BETWEEN MOUNTING LUGS AND WIRE LEAD OR TERMINAL LUG IS VARIABLE					
LENGTH (L)						SEE CAPACITANCE-RANGE CHART (TABLE 1)					

(N.A.=NOT AVAILABLE. ALL DIMENSIONS IN INCHES)

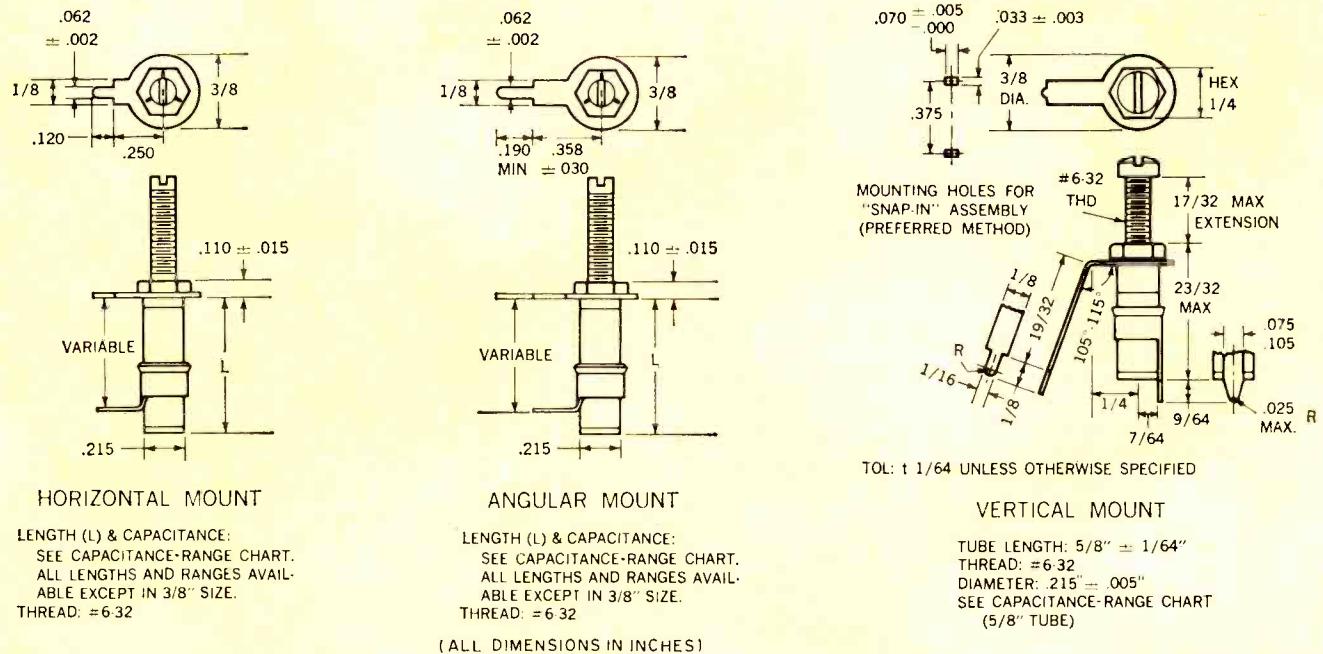


Fig. 3. Ceramic tubular trimmers with stamped terminals designed for horizontal, angular, or vertical chassis mounting.

and chokes and would help provide uniform non-temperature-dependent performance of tuned circuits.

Eventually two groups of ceramic formulations were developed—the temperature-compensating bodies, such as described above, and the Hi-K (high-dielectric-constant) dielectric materials. The temperature-compensating bodies are now available in characteristics of from P100 (positive 100 ppm/°C) to N5250 (negative 5250 ppm/°C). Since a variety of temperature-coefficient (TC) characteristics are available in this class of materials, the particular TC can be selected to provide the proper compensation required.

In this family is the NPO (negative-positive zero) body which, as its name implies, has little or no change, negative or positive, over a given temperature range. The NPO body is deservedly popular since it is very stable (usually varies no more than ±30 ppm/°C from -55° C to 125° C), and has excellent dissipation factor, high insulation resistance, high "Q", plus good frequency characteristics. This NPO dielectric, in fact, is more stable than many glass dielectrics.

The Hi-K ceramic materials are designed to give the most capacitance in the smallest size. They usually have their highest capacitance value at 20° C (68° F) and drop in value as the body is cooled below or heated above room temperature. There are a variety of Hi-K bodies available, but the user should realize the higher the K, the greater the changes in capacitance values as the capacitor is heated or cooled. A K value only as high as necessary to obtain the value in the required size should be used. In this way the minimum capacitance variation with temperature change will be obtained.

#### Ceramic in Trimmers

Fixed ceramic capacitors available on the market include tubular, disc, feed-through, and some of the newer types, such as the monolithics and capacitor chips. However, in this Special Section, we are concerned with variable capacitors and trimmers.

In the ceramic trimmer capacitors, only the temperature-compensating dielectrics are used, and for good reasons. These dielectrics offer the highest "Q", the highest insulation resistance, and the most predictable change in capacitance with temperature. Most trimmers are used in frequency-determining circuits, and the improved characteristics and greater stability of the temperature-compensat-

ing dielectrics are essential for these particular applications.

It is important to understand that the use of temperature-compensating dielectrics in trimmers does not mean that the dielectrics will perform exactly the same as when these materials are used in fixed disc or fixed tubular capacitors. In any ceramic trimmer capacitor, the capacitance obtained is not simply dependent upon the characteristics of the dielectric itself. In series with the dielectric in any ceramic trimmer is an air gap or a volume filled with a grease or lubricant with a higher dielectric constant than air alone. Therefore, the temperature characteristics of a ceramic trimmer capacitor are generally broader than the fixed capacitor made of the same material. Also, ceramics with larger TC's usually have higher dielectric constants, so that higher capacitance values may be obtained.

The ceramic disc trimmer is discussed in another article in this Special Section. Here, we want to focus on the ceramic tubular capacitor.

#### The Tubular Configuration

This type of trimmer capacitor is used in electronic circuitry because it has excellent reliability coupled with low cost. A variety of capacitance ranges can be supplied or tailored to a particular requirement. These values range from 0.5 pF up to 25 pF.

The most popular tubular configuration has one end that is notched to fit into a key-hole mounting (Fig. 1). A screw threaded into the ceramic body of the trimmer serves several functions. In addition to holding the capacitor upright from the chassis, the screw also serves as the adjusting element (rotor) to vary the capacitance. The stator electrode is a metal band painted on the ceramic body. There is a wide variety of terminal configurations available from several manufacturers. (See Fig. 2.)

There are two basic diameters of the tubular trimmers, one designed for use with a #6-32 screw has an outside diameter of 0.215", while the other is designed for use with a #4-36 screw in an outside diameter of 0.180". These trimmers are available in five different lengths: 3/8", 1/2", 5/8", 3/4", and 1" long. These are available in up to ten terminal combinations, including various types of wire break-outs, solder terminals, tabs, etc. to more readily facilitate their attachment and wiring into the circuit where they will be used. Another version of this trimmer is supplied with stamped terminals for both rotor and stator electrodes. These trimmer capacitors are designed for horizontal, an-

gular, or vertical mounting to the chassis. (See Fig. 3.)

The ceramic materials that are used for these trimmers fall into the temperature-compensating class. Materials used have TC's of N220, N400, and N750. In addition, steatite ceramic (a type of electronic porcelain) is employed in these trimmers. Steatite is quite dense, is very stable, and functions admirably as an inert dielectric. Steatite is used for the minimum capacitance ranges.

Capacitance values are determined by the selection of the dielectric materials as well as by use of the different diameters and lengths. The higher TC body together with the larger diameter and greatest length affords the highest capacitance (up to 25 pF) while the smallest diameter and shortest length with the steatite body offers the minimum value (0.5 pF to 2.0 pF). A listing of the most popular values is given in Table 1.

Some 20 percent increases in minimum and maximum capacitance limits can be obtained if the space between the screw thread and the inside thread of the ceramic body is filled by the manufacturer with a silicone grease. This option, available at a nominal price increase, provides a higher dielectric constant in series with the ceramic dielectric and increases the total capacitance accordingly.

The capacitance *versus* rotation curve for the tubular trimmer is a modified sawtooth curve since the contact between the screw thread and the internal ceramic thread varies as the adjustment screw is rotated. However use of the silicone grease tends to level out the variations in this capacitance change with rotation. ▲

Length	Steatite (P120)	N220	N400
$\frac{3}{8}$ "	.5-2.0	.9-3.0	1.5-6.0
	8-2.5	1.0-4.0	2.0-7.0
	1.0-3.0	2.0-5.0	2.5-9.0
	1.0-3.5**	2.5-5.5**	3.5-10.0**
$\frac{1}{2}$ "	.3-2.5	.5-4.0	1.0-7.0
	.5-3.5	1.0-6.0	1.5-9.0
	1.0-4.0	2.0-7.0	2.5-12.5
	1.0-5.0**	2.5-8.0**	3.5-13.0**
$\frac{5}{8}$ "	.2-3.0	.5-6.0	.8-8.0
	.5-4.5	1.0-8.0	1.5-12.0
	1.0-6.0	2.0-9.0	2.0-15.0
	1.0-6.5**	2.5-10.0**	2.5-16.0**
$\frac{3}{4}$ "	.2-4.0	.5-8.0	.8-11.0
	.4-6.0	1.0-10.0	1.0-14.0
	1.0-7.5	2.0-11.0	3.0-18.0
	1.0-8.0**	2.5-12.0**	3.5-20.0**
1"	.4-6.0	1.0-10.0	1.0-14.0
	1.0-7.5	2.0-11.0	3.0-18.0
	1.0-8.0	2.5-12.0	3.5-20.0
	1.0-10.0**	2.5-15.0**	3.5-25.0**

\*Note: The addition of silicone grease will increase both the minimum and maximum capacitance limits approximately 20%.

\*\*Available only on tubular trimmers without mounting lugs.

Table 1. Capacitance-range chart for the five standard trimmer lengths. All values are given in picofarads (pF).\*

## MICA COMPRESSION TRIMMERS

MICA compression trimmer capacitors consist of a low-dielectric-loss ceramic base and a number of metal plates separated from each other by a mica dielectric. The movable top plate is made of a spring material so that uniform torque can be applied to the lower mica dielectric and plates when the adjusting screw is tightened or loosened.

Depending on circuit application, two types of variable mica compression capacitors are available from such companies as Electro Motive Mfg. Co. (Elmenco): the physically larger padder type containing from 2-15 plates with nominal maximum capacitance ranges of 130 to 3055 pF for 250 WV d.c. and 120 to 2525 pF for 500 WV d.c.; and the smaller trimmer type containing from  $1\frac{1}{8}$  to 15 plates with nominal maximum capacitance range of 7 to 1400 pF for 175 WV d.c.

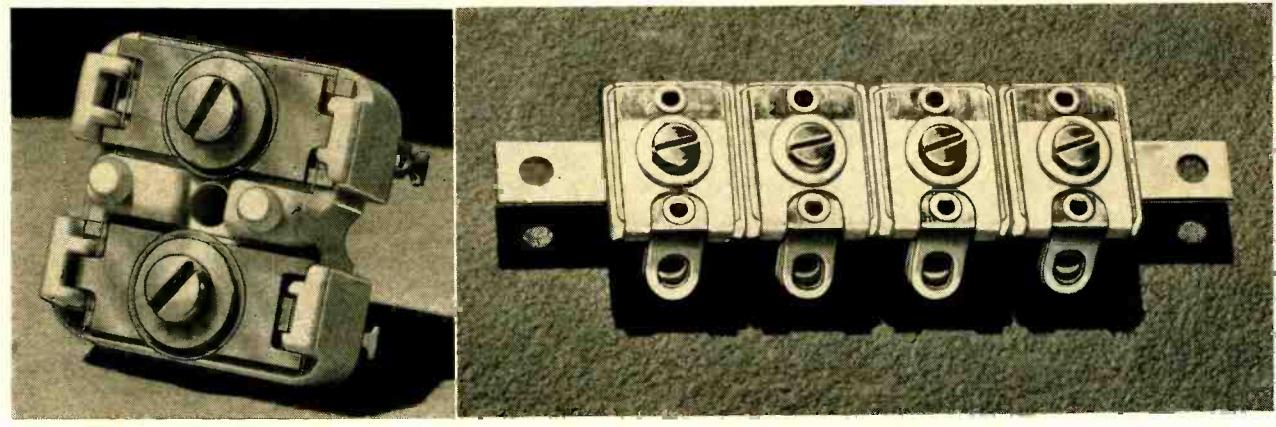
The padder types come in three sizes: a  $\frac{7}{8}'' \times 1\frac{9}{16}''$  single padder, a  $1'' \times 1\frac{15}{32}''$  single padder with a nominal maximum capacitance range of 80 to 240 pF for 175 WV d.c., and a  $1\frac{1}{16}''$  square dual padder (shown at the left photo) with nominal capacitance range of 80 to 240 pF for 175 WV d.c. The trimmer types also come in three sizes: standard ( $\frac{3}{4}'' \times \frac{5}{8}''$ ), miniature ( $\frac{3}{8}'' \times \frac{9}{16}''$ ), and midget ( $\frac{3}{8}'' \times \frac{3}{4}''$ ), with both chassis-mounting and printed-circuit mounting types available. For printed-circuit use, solid terminal lugs are provided to permit ease of mounting and to facilitate positioning and support of the capacitor. ▲

These capacitors are normally supplied with the capacitance adjusted to near nominal values, which occur between  $\frac{1}{4}$  and  $\frac{1}{2}$  turn from tight, where "tight" is defined as the maximum clockwise rotation of the adjusting screw. Minimum rated capacitance occurs at 3 turns from tight.

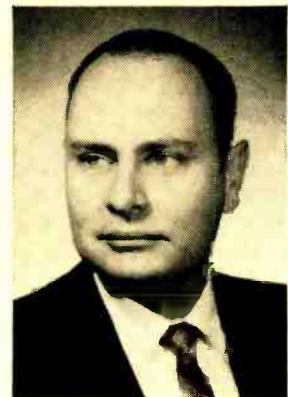
Capacitance of mica compression trimmers does not vary linearly with adjustment. For example, a mica capacitor with six plates will reduce to half the nominal maximum value within one opening turn while those with a greater number of plates require further screw disengagement for a similar percentage reduction in capacitance value. On the other hand, a capacitor with two plates will reach one-half the nominal maximum capacitance in less than one-half turn.

The "Q" factor for mica compression trimmers and single padders at nominal capacitance values of 400 and 1000 pF is 700 and at nominal capacitance values of 1 to 40 pF varies from 100 to 700. When the capacitors are subjected to a 100-hour humidity test at a temperature of 40°C and a relative humidity of 90-95%, and then allowed to remain at room temperature for one hour in circulating air, the "Q" factor will be reduced 50% for all capacitance values.

Both padder and trimmer capacitors can be obtained with special adjusting screws for ease of tuning. Special mounting brackets (shown in the right photo) are available for mounting one, two, three, or more trimmer capacitors simultaneously. ▲



The author is responsible for all components engineering, including piston trimmers, fixed and variable ceramic capacitors, and tuners. A graduate of the University of Southern California, he has been active as a design engineer and executive in the electronics industry since 1949. Prior to joining JFD, he was Director of the Applied Research Department of Bourns, Inc. and Executive Vice-President and General Manager of Monolithic Dielectrics Inc. He holds a dozen U.S. patents for electronic components and related items, including several patents in the ceramic and thick-film areas.



# Glass Piston Trimmer Capacitors

By KENNETH F. MILLER / Chief Engineer  
JFD Electronics Corp., Components Div. (subsidiary of Riker-Maxson Corp.)

*Providing high capacitance for their size, wide adjustment range, high "Q", precision adjustment, and ability to withstand unfavorable environments, these trimmers are widely employed in aerospace and military equipment.*

PISTON trimmers are very useful for circuits where stable and finely adjustable capacitances are required and where space is at a premium. For example, they are often used to tune filters for i.f. amplifiers.

A wide variety of piston trimmer types is available. A single manufacturer may offer as many as 2500 different standard and custom designs, to meet all types of requirements.

There are many different ways to classify piston trimmers: by dielectric, by size, sealed and non-sealed, precision and non-precision, by capacitance range, rotating or non-rotating piston, by type of mount, by temperature coefficient, and by number of operating cycles.

## Piston Trimmer Construction

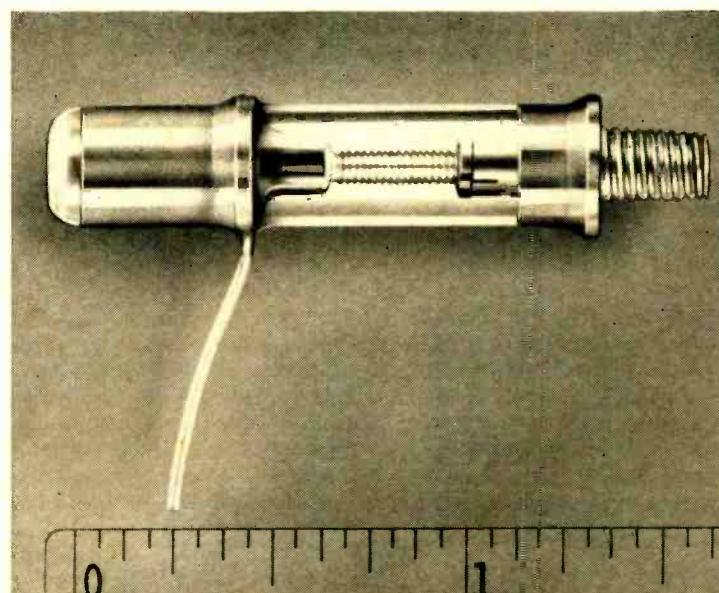
Fig. 1A shows the construction of a typical panel-mount piston trimmer. The piston is one capacitor electrode (rotor) and a metalized coating on the glass tube is the stator. Current flows through the panel-mount terminal, the bushing, the adjustment screw, to the piston electrode. The stator is connected to the other capacitor terminal. When the adjustment screw is turned, it pushes the piston into the stator or pulls it out, increasing or decreasing capacitance.

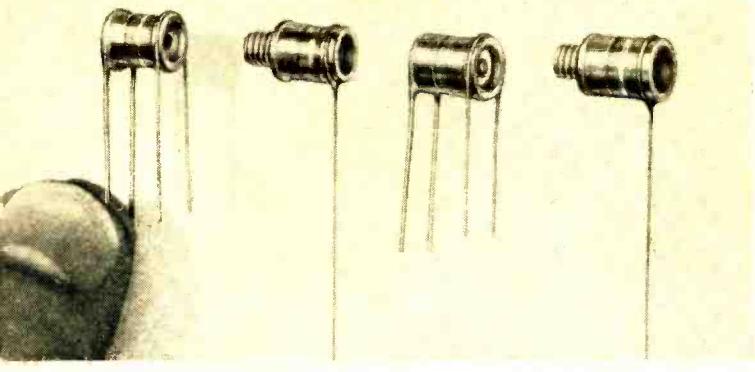
The first step in manufacturing a glass piston trimmer is to draw the glass dielectric tube to a size slightly larger than the specified final diameter. The glass used is carefully compounded to produce the desired dielectric properties of high  $K$  and high "Q." Then silver bands are printed around the glass. It is important that the silver bands be solid and homogeneous with a high-strength bond to the glass tube. The bond is achieved by fusing the bands at

1400° F. During fusion the diameter of the glass tube is reduced to the precise diameter required in the final product. The bands are then plated to reduce resistance and improve the solderability. Finally, the glass is cut to the necessary lengths, fitted with bushings and terminals, and an adjustment mechanism.

Fig. 1B shows the construction of a sealed miniature telescopic mechanism. The diameter is about the same as that of a standard piston trimmer, but the unit is much shorter.

A typical sealed panel-mount glass piston trimmer capacitor.





Some examples of typical unsealed glass piston trimmer capacitors, including printed-circuit and panel-mounted types.

The threads of the screw engage mating threads on a slotted flange extension of the inner bushing. Torque is supplied by the tension ring, which fits in a slot on the flange. The O-ring seal increases moisture resistance, insulation resistance, and dielectric strength.

A long-life sealed telescopic piston trimmer is shown in Fig. 1C. This type of mechanism is designed to permit a very large number of adjustments (500 or more cycles). Tension is applied to the adjustment screw by two axially spring-loaded tensioning nuts. These tensioning nuts fit into 90-degree opposing channels of the mounting bushing and provide torque to prevent accidental rotation of the lead-screw as well as eliminate backlash.

Some piston trimmers use a non-rotating, or direct traverse mechanism. At the end of the piston are two shaped slots. The arms of the bushing fit into these slots, keeping the pistons from rotating. As the tuning screw is turned, the piston moves from thread to thread, producing in and out movement. The tuning screw rotates, but does not move in and out with the piston.

The mechanism shown in Fig. 1D is a very long-life (10,000 cycle) non-rotating type. Backlash is eliminated by two tension nuts, one of which is an integral part of the inner piston assembly. The other tension nut rides in 180-degree opposed slots in an extension of the mounting base. A simple spring is mounted between the two tension nuts. This prevents backlash with the tuning screw, which remains stationary in the adjustment well. Torque can be preset to any value between 1 and 10 inch-ounces ( $\pm 0.5$  inch-ounce). Torque is controlled by an axial biasing spring between the bushing and the adjustment screw. This

trimmer uses an embedded stator to increase capacitance.

The MIL-Spec for piston trimmers is MIL-C-14409C. This spec covers 15 different types of piston trimmers, plus concentric-shell air-dielectric trimmers.

### When to Use Piston Trimmers

The prime advantage of a piston trimmer capacitor over other types is that it provides higher capacitance for a given size. Equally important, the capacitance-adjustment range of a piston trimmer is greater than that of almost any other trimmer type. Also, piston trimmers provide good temperature compensation, high "Q," and the ability to withstand unfavorable environments.

Piston trimmers have been widely used in missiles, satellites, space vehicles, as well as in other military and industrial applications. Piston trimmers, for example, have been used in the Apollo 11 and 12 lunar modules, Gemini and Minuteman "birds," as well as in more down-to-earth equipment.

On the other hand, piston trimmers are not recommended for extremely high capacitance or microwave applications. They are not the best choice for frequencies above 1.0 GHz because the "Q" is reduced rapidly at higher frequencies and stray inductance causes self-resonance at about this frequency.

The maximum capacitance that currently available piston trimmers can provide is about 300 pF. They can also be made for capacitances as low as 0.5 to 2 pF.

### How to Select Piston Trimmers

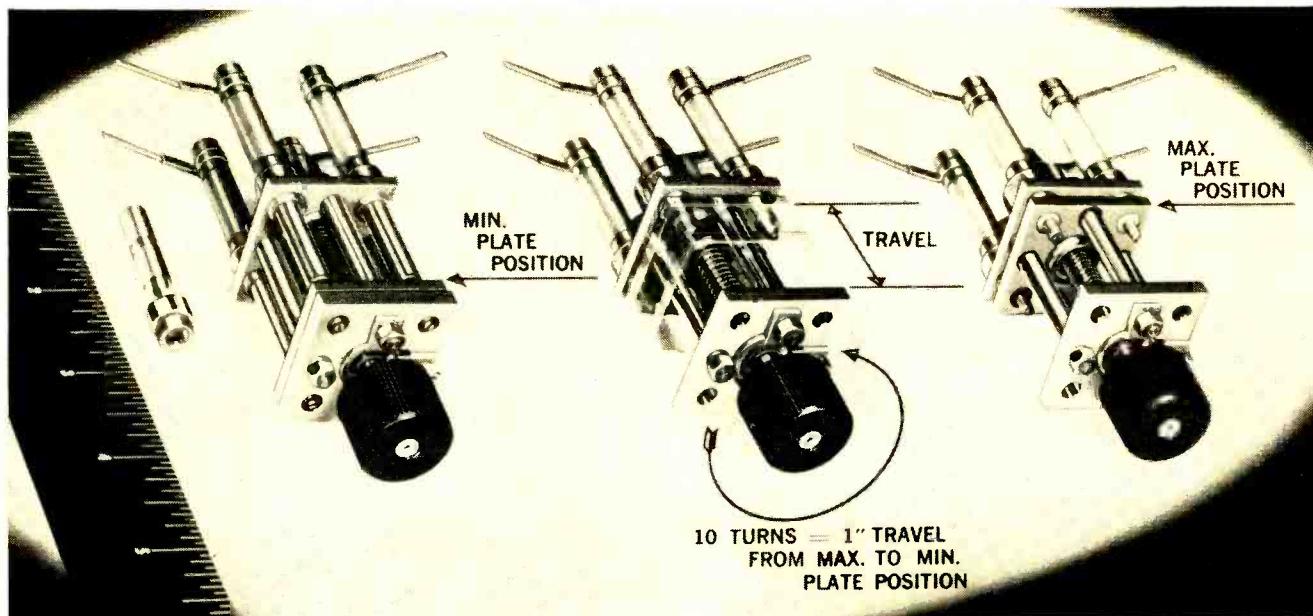
Because such a wide range of piston trimmers is available, it's not always easy to select the best one for each specific application. The following guidelines should be helpful.

#### 1. Precision or Non-Precision

Most piston trimmer capacitors used today are precision types. The air gap between piston and the dielectric wall is held to about 0.0004 inch. This requires that the inner diameter of the tube and the outer diameter of the piston be very precise. Further, dielectric tubing is made virtually stress- and scratch-free and inner walls are polished to a smooth, mirror-like finish, reducing friction. That users can buy piston trimmers this precise for less than \$1.00 is a tribute to modern manufacturing techniques.

Non-precision piston trimmers are also available, but they are not as widely used. They cost less, of course, and are therefore suitable for consumer applications, such as TV sets and other home-entertainment equipment.

Precision 4-gang tuning capacitor made from glass piston capacitors, showing movement of tuning mechanism.



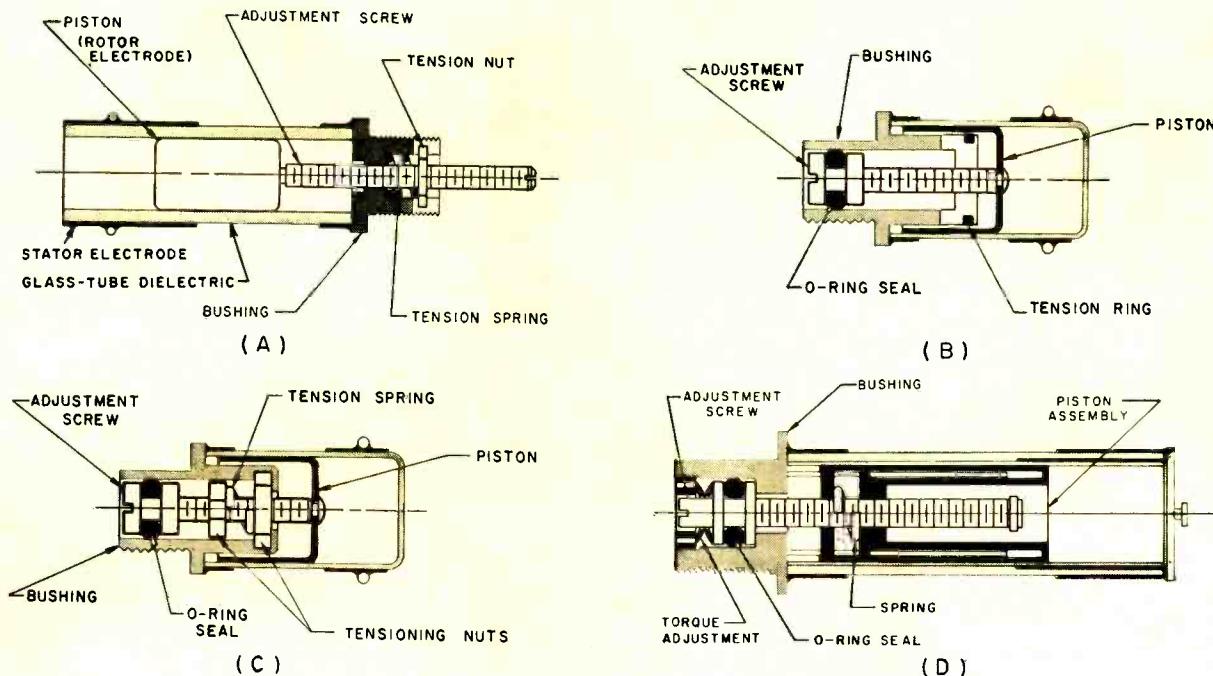


Fig. 1. (A) Cross-section of a typical panel-mount piston trimmer. (B) Telescopic adjustment mechanism used in miniature sealed trimmer. (C) Long-life (500 cycles) mechanism used in miniature sealed trimmer. (D) Very long-life (10,000 cycles) sliding travel adjustment mechanism, along with embedded electrodes and sealed construction.

## 2. Type of Dielectric

Piston trimmers use four kinds of dielectrics: standard glass, green glass, quartz, and ceramic. You choose the dielectric on the basis of the capacitance, size, voltage, and "Q" required in your circuit.

If size is not a problem, you will probably select an ordinary glass dielectric with a dielectric constant ( $K$ ) of about 6.7 and a dissipation factor of approximately 0.0012 at 1 MHz. If you need more capacitance in a given size, you will probably choose green glass as a dielectric. Green glass has a dielectric constant of 8.3 and a dissipation factor of 0.0007. Thus, it can increase both capacitance and "Q." Green-glass trimmers typically have capacitances about 30 percent greater and "Q" about 25 percent higher than ordinary glass types.

If very high "Q" is required, quartz may be the solution. Quartz is expensive but its dissipation factor is extremely low. However, the dielectric constant is only about 3 so that the available capacitance is lower or the size must be increased. Quartz units can also provide better temperature compensation.

Ceramic dielectric with a dielectric constant of 88 is called for when a low-cost high-capacitance trimmer is desired. The operating temperature range of ceramic piston trimmer capacitors is also higher, being  $-55$  to  $+150^{\circ}\text{C}$  compared with  $-55$  to  $+125^{\circ}\text{C}$  for glass. These advantages are offset by considerably higher temperature coefficient than for quartz or glass.

For maximum capacitance in a given size, embedded bands may be employed. Obviously, reducing the distance between the plates increases capacitance. In a piston trimmer, we do this by embedding the stator metalization between two layers of glass tubing (see Fig. 1D). The first layer is very thin (0.004 to 0.006 in compared with 0.020 in used on ordinary piston trimmers). It is coated with a metalized band and is then bonded to a thicker outer glass layer for strength. Contact electrodes are coated on the outside of this thicker layer of tubing. Thus, the stator is only as far away from the piston as the thickness of the thin inner glass layer of

tubing. Embedded piston trimmers provide a 300 to 600 percent increase in capacitance.

## 3. Sealed or Non-Sealed

As indicated in Fig. 1, some piston trimmers use an O-ring seal at the tuning-screw end. These trimmers also use a glass or metal seal at the other end of the piston trimmer. Such units are known as "sealed" piston trimmers and they provide environmental protection against dust and moisture. Sealed glass piston trimmers can also handle higher voltages, since glass has greater dielectric strength than air. If you anticipate a hostile environment, use a sealed unit. Otherwise a non-sealed piston trimmer is a better choice, since it costs less.

## 4. Type of TC

Temperature coefficient is usually specified in ppm/ $^{\circ}\text{C}$  (parts per million per degree centigrade) over the operating range of the piston trimmer. Some glass units go as high as  $\pm 450$  ppm/ $^{\circ}\text{C}$ , but most are in the range of  $\pm 50$  ppm/ $^{\circ}\text{C}$  to  $\pm 100$  ppm/ $^{\circ}\text{C}$ . The TC of quartz is better, generally about  $\pm 25$  ppm/ $^{\circ}\text{C}$ .

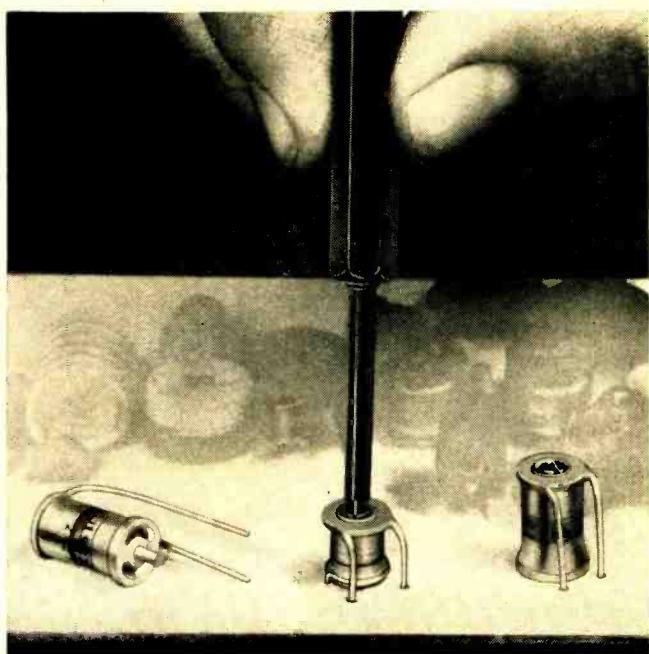
## 5. Type of Leads

Once you have chosen the desired electrical characteristics, you will have to consider the problem of mounting. Piston trimmers are available with a wide variety of lead types, but four styles are basic: panel-mount, 4-wire printed-circuit mount, 2-wire printed-circuit mount, and lug and lead printed-circuit mount. If the trimmer is to be welded, rather than soldered, a dumet lead (a gold-plated nickel alloy) is preferred.

Normally, panel-mounted piston trimmers are grounded. However, most panel-mount units can be ordered with nylon bushings to insulate them from ground. Top-end tuning may be desirable on a printed-circuit-mounted unit. This can easily be accomplished by using special miniature PC-mount trimmers.

## 6. Type of Tuning Mechanism

As discussed previously, you can choose between two basic types of tuning mechanisms: rotating or non-rotating. There has been a controversy within the industry as to



Mounting and top-end tuning of trimmers on PC board.

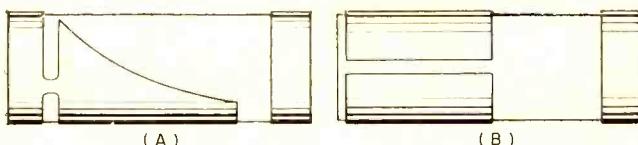


Fig. 2. (A) Straight-line frequency stator metalization is available, and (B) split-stator metalization.

which is better. Proponents of direct traverse mechanisms claim that rotating mechanisms cause reversals. They say that because the piston moves closer and farther away from the stator, capacitance sometimes changes in the wrong direction. This, of course, could be very disconcerting to the engineer or technician tuning the circuit. In truth, however, reversals are virtually unknown in precision piston trimmers of any type. Rotating piston trimmers are subject to flats (places where capacitance does not change when the tuning screw is adjusted), but this is seldom detectable in practical use.

Non-rotating mechanisms provide better linearity, but rotating mechanisms have advantages too. Dollar for dollar, they are more stable and last longer. One way of putting the controversy into perspective is to consider sales figures. At present, rotating types outsell non-rotating types by a ratio of at least 10 to 1.

Another important factor in choosing a tuning mechanism is the number of cycles of adjustment that will be required during the life of the piston trimmer. Most piston trimmers are specified to 500 cycles or more. Where long life is required, spring-loaded mechanisms are used (Fig. 1C) rather than the simpler split-collet (Fig. 1A) types. The mechanism shown in Fig. 1D is better still, providing an adjustment life of 10,000 cycles.

The unit with the longest adjustment life is not always the best choice, however, since long-life mechanisms cost more than ordinary mechanisms. Since trimming is basically a touch-up adjustment, it is rare that a piston trimmer is tuned more than 500 times during its lifetime.

#### Special Piston Capacitor Types

A number of unusual piston capacitors can be made to meet specific requirements. For example, most piston trimmers provide straight-line capacitance adjustment, but exponential capacitance for straight-line frequency adjustment units are also available.

To make an exponential trimmer, the glass tube is metallized in a pattern that is an exponential function of distance, as shown in Fig. 2A. Exponential metalizing is available as a "special" on almost any type of piston trimmer. It is very useful for applications where the top end of a frequency band is crowded, requiring very precise adjustment. Special spiral metalizing is also available to form inductors, LC tuners, and transformers.

Fig. 2B shows the stator assembly of another specialized piston trimmer, the split-stator type. Because of split-stator metalizing, this is actually two capacitors in one. Each separate stator electrode has capacitance to the common piston. Thus, tracking is virtually error-free. Split-stator units are ideal for push-pull applications. Another application is to reduce piston inductance by connecting to the two stator electrodes and insulating the moving piston.

Another special configuration is obtained by *differential* metalizing. In this case two separate complete (not split) stator bands are used and the piston moves between the two stator bands. As capacitance between the piston and one stator is increased, capacitance between the piston and the other stator is decreased. The crossover point is where the piston is equidistant from the two stators. Tuning is quite linear and sensitive. What's more, the sum of the two capacitances is nearly constant.

Some special piston trimmers are available to vary temperature compensation, rather than capacitance. When you tune a variable-TC piston trimmer, TC changes from maximum positive to maximum negative while the capacitance remains constant. This is accomplished by use of a special type of split-stator design in which the materials used and the construction of the piston are such as to change the TC depending on the position of the piston. The TC range of variations may be as high as  $\pm 800 \text{ ppm}/^\circ\text{C}$ . These units are especially useful to trim the temperature coefficients of crystal-controlled oscillator and filter circuits.

#### Piston Tuners

Most piston capacitors are used as trimmers, but the design is also excellent for tuning capacitors and tuned circuits. The coil for the tuned circuit is a silver metallized inductor fired onto the glass tubular element at the same time as the capacitor electrodes are formed.

Piston tuners are remarkably small, stable, and versatile. They can be used to provide precise tuning with high linearity for both straight-line capacitance and straight-line frequency applications.

The main difference between a piston tuner and a piston trimmer is the tuning mechanism. Piston tuners have linearities as good as one percent and are capable of 30,000 to 50,000 life cycles.

A 4-ganged piston tuner is shown in one of the photos. Units of this type utilizing modular construction can be provided with up to eight sections. Thus, a very wide range of types is available on a custom basis. Tuners may be strictly a number of piston capacitors ganged together or the capacitors may have metallized coils on the glass dielectric, resulting in ganged tuned circuits.

#### The Future of Piston Capacitors

Over the next 5 to 10 years, piston trimmers will probably retain their edge over other trimmers as the use of integrated circuits increases, except where extremely small size is the prime consideration. However, it is unlikely that piston trimmers will find a place in thick-film circuits. They will probably be replaced by some as yet undeveloped type of trimmer.

Sales of piston trimmers are likely to continue strong during the early 1970's, but they will probably begin to fall off during the last half of the decade. Piston tuners, on the other hand, will probably become much more popular in the near future, as new applications are found.

The author graduated in Mechanical Engineering in 1963 from Gannon College, Erie, Pa. He has worked in various capacities in engineering ceramic, glass, air, and plastic-dielectric trimmers.



# Ceramic Disc Trimmer Capacitors

By JOHN F. MOULTHROP / Supervising Engineer  
Trimmer Products, Erie Technological Products

*This popular trimmer type has undergone an evolution in size and voltage rating to keep pace with needs of industry.*

CERAMIC disc trimmer capacitors have been manufactured in the United States for about 30 years and have become the most popular type used. During this time they have undergone an evolution in size and voltage rating to keep pace with the requirements of the electronics industry. They have found wide acceptance because of their good volumetric efficiency, high "Q," ease of tuning, numerous terminal configurations, and unique construction.

A ceramic disc trimmer has three main parts: the stator, rotor, and dielectric. The stator electrode is a metallized pattern deposited on a lapped low-loss ceramic base. The rotor electrode is a metallized pattern deposited on the rotor. The dielectric is a temperature-compensating ceramic disc lapped to a given thickness. Turning the rotor varies the overlapped area between the rotor and stator electrodes, thus varying the capacitance. Trimmers are available in capacitance ranges from 1-3 pF to 11-110 pF depending on the rotor size and the dielectric material used. The typical "Q" of a ceramic disc trimmer is in excess of 1000 at 1 MHz.

The full capacitance range in most disc-style trimmer capacitors is covered in 180-degree rotation of the rotor. The best designs allow the greatest possible rotation in the linear portion of the tuning curve (Fig. 1).

To obtain the various capacitance ranges, dielectrics with dielectric constants ( $K$ ) of 7 to 190 are used. These correspond to temperature characteristics of P120 and N1500. Because of the construction of disc-style ceramic trimmers, the completed trimmer does not exactly reflect the temperature coefficient (TC) of the dielectric material used. For this reason these trimmers should *not* be relied upon as temperature compensating capacitors. This wide range of TC is reflected in the requirements of MIL-C-81, which is the military specification covering five styles of ceramic trimmers. These broad limits are shown in Table 1.

The five styles covered in MIL-C-81 have two separate diameters and voltage ratings. CV11, CV14, and CV21 have 0.656-in diameter rotors and are rated at 500 V d.c. CV31 and CV34 are 0.375-in diameter and 350 V d.c. rated. The specification temperature range is  $-55^{\circ}\text{C}$  to  $+85^{\circ}\text{C}$  but the trimmers are capable of  $125^{\circ}\text{C}$  operation.

Ceramic trimmers are available in two general temperature ranges:  $-55^{\circ}\text{C}$  to  $+85^{\circ}\text{C}$  and  $-55^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ . The  $85^{\circ}\text{C}$ -rated styles use certain materials in their construction which limit the upper working temperature. For equipment designs which will not exceed  $85^{\circ}\text{C}$ , these trimmers are available at generally lower prices than the  $125^{\circ}\text{C}$

C-rated units. Only ceramic and metal parts are used in the design of  $125^{\circ}\text{C}$ -rated trimmers.

## Specifying a Disc Trimmer

When a user needs to specify a trimmer capacitor, he must first consider what capacitance range he will require to tune his circuit by taking into account various tolerances of other components. In any disc-style trimmer the slope of the tuning curve varies with the capacitance range since the full range is covered in a maximum of 180 degrees. The larger the capacitance range the greater the change of capacitance per degree rotation of the rotor.

Voltage requirements are another factor for the designer to consider. Ceramic trimmers are designed so that they will withstand life testing at twice their rated voltage at the

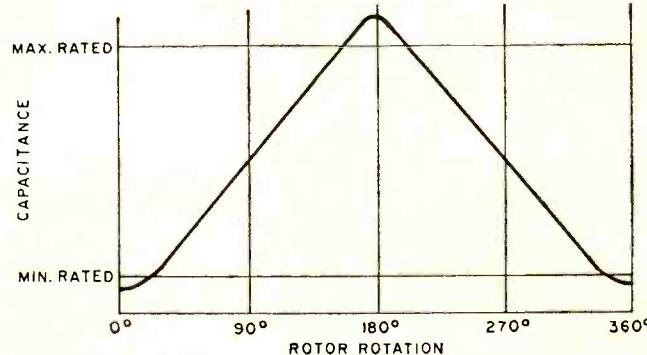
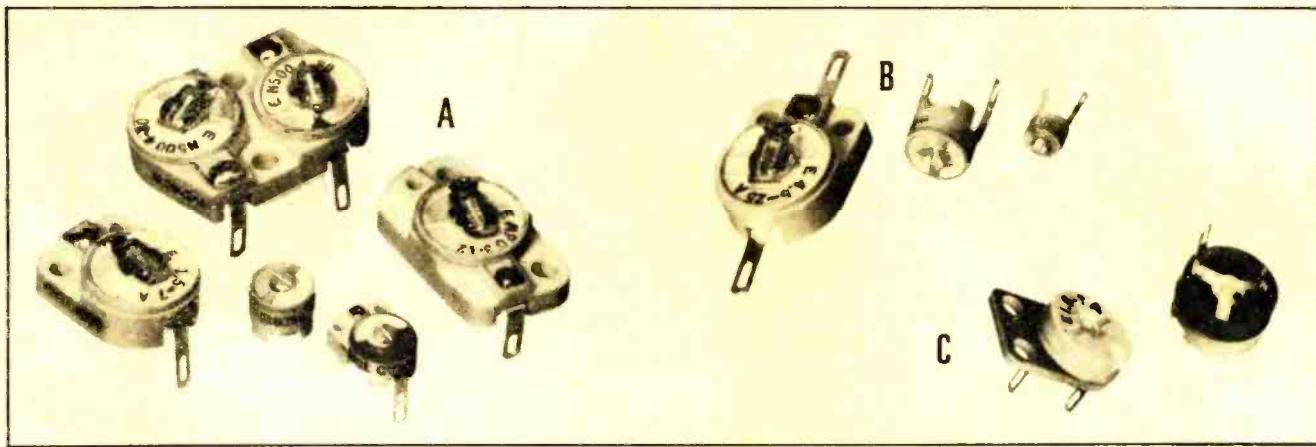


Fig. 1. Capacitance vs. rotation for ceramic disc trimmer.

Table 1. Capacitance change limits versus temperature.

DIELECTRIC		PERCENT CAPACITANCE CHANGE FROM VALUE @ 25°C					
Nominal Constant	Type Code	$-55^{\circ}\text{C}$		$+85^{\circ}\text{C}$		$+125^{\circ}\text{C}$	
		Min.	Max.	Min.	Max.	Min.	Max.
30	A	-4.5	+2.0	-2.5	+2.0	-4.2	+3.4
45	B	-1.0	+3.5	-2.5	-0.5	-4.2	-0.8
50	C	-1.0	+6.5	-4.0	-1.0	-6.7	-1.7
57	D	+1.5	+7.0	-5.0	-1.5	-8.5	-2.5
90	E	+1.75	+8.0	-5.75	-1.75	-9.5	-2.8
180	F	+6.0	+16.0	-11.0	-6.0	-15.0	-9.0



(A) These are the five styles of trimmer capacitors covered in MIL-C-81B. (B) Ceramic disc trimmers shown actual size illustrate the evolution in size over a period of 30 years. (C) Examples of 85° C-rated trimmer capacitors.

maximum operating temperature for 1000 hours without serious degradation. Some ceramic dielectrics have voltage characteristics which make it necessary to de-rate the voltage rating above 85° C. The early designs used dielectrics about 0.020-in thick and were rated at 500 V d.c. As the units became smaller the dielectric thicknesses had to be reduced to furnish useful capacitance ranges. Today, through the use of monolithic construction, dielectrics less than 0.005 in are common. Trimmers using this range of thickness are rated at 100 V d.c. or less.

With the use of smaller and more tightly spaced components, size becomes an important consideration in trimmer requirements. Because of the higher  $K$ 's available in ceramic dielectrics, ceramic trimmers are smaller than other types. Also with a wide choice of  $K$ 's many capacitance ranges are possible.

Another important point is that ceramic trimmers do not change size with capacitance range as do most tubular or plate-type air trimmers.

However, there are two reasons for limiting the use of dielectrics with  $K$ 's exceeding 200. The first is that these dielectrics are characteristically too thermally unstable for use in a trimmer. It would be very difficult to tune a circuit using such a trimmer because of the vague capacitance drift associated with the trimmer. The second reason is that a ceramic disc trimmer is actually two capacitors in series. One capacitance is due to the dielectric and the other due to the air gap between the dielectric and the stator. The total capacitance is affected by the dielectric constant multiplied by the air-gap thickness. As the  $K$  becomes larger, the trimmer capacitance does not increase in direct proportion. When  $K$  is increased above 200, the increase in total capacitance is slight and does not justify the use of such materials.

The "Q" or dissipation factor of the trimmer usually does not affect "Q" of the circuit since other components have much higher losses than the capacitor. Most ceramic trimmers have a minimum "Q" in excess of 500 at 1 MHz. Typically, "Q" exceeds 1000 in nearly all cases.

### Geometric Shapes and Mounting

The geometric shape of the trimmer and its mounting configuration have as much effect on its frequency characteristics as the dielectric. In the case of ceramic disc styles, the resonant frequency is in the 400-600 MHz range. This does not mean that the dielectrics used are limited to these frequencies but only that the particular combination of components shows these characteristics.

Tubular-style trimmers show much higher resonant frequencies than disc ceramic styles. Glass trimmers are good to approximately 1 GHz. Coaxial air trimmers exhibit resonant frequencies well above 1 GHz. These figures depend on capacitance setting, configuration, and fixturing.

When the type of trimmer and capacitance range are de-

cided upon, the mounting style must be investigated. There are a great many terminal configurations and mounting types available in all styles of trimmers. Ceramic trimmers offer a large number of printed-circuit, point-to-point, horizontal, vertical, and hardware mountings. The type of mountings available to fit an individual application is best determined from manufacturers' catalogues or by contacting the manufacturer directly. Most suppliers welcome a chance to help a user by providing special configurations.

Some hints on installing printed-circuit-style trimmers may be useful. When terminals are inserted through the board and crimped, care should be taken that undue force is not applied to the terminals when they are crimped. This may physically damage connections or even break the part. When the board is passed over a solder wave, the temperature of the solder and the duration of high temperature exposure must be noted. Too much time or too high a temperature can damage solder joints in the trimmer. With trimmers which utilize organic materials, temperatures must be reduced to avoid damage.

Flux during both the soldering and cleaning operations can cause problems. Flux residues can form around the rotor shaft and between the lapped surfaces. This can cause frozen rotors, poor "Q," and rough adjustment torque. A minimum amount of flux is recommended for soldering. The Freon or chlorethene solvents must be kept clean to

Table 2. Comparison of several styles of trimmer capacitors.

TRIMMER TYPE & APPROX. COST	ADVANTAGES	DISADVANTAGES
Ceramic disc \$.30-.40 each	Small size, rugged, fast accurate tuning, stable	Limited in operating frequency
Glass tubular \$.60-.90 each	Fine tuning, good TC, good high-frequency performance	Fragile, relatively large in size
Air disc \$.25-.30 each	Fast accurate tuning, high "Q," stable, good at r.f. frequencies	Large in size, susceptible to voltage breakdown and dirt contamination
Air coaxial \$1.75 each	High "Q," good at r.f. frequencies, fine tuning, excellent TC	Expensive, relatively large in size, susceptible to voltage breakdown
Mica compression \$.10-.15 each	Large capacitance ranges, low cost	Non-linear tuning, poor stability
Ceramic threaded tubular \$.04-.05 each	Low cost	Poor stability
Plastic \$.15-.20 each	High "Q," good stability	Limited in temperature range and in capacitance range

prevent dissolved flux from hardening on all surfaces. The time in cleaning solvents must be kept to a minimum to avoid washing away the lubricants from between the rotor and base. Certain solvents will attack the organic parts of some styles of trimmers. The user should experiment with his particular soldering and cleaning procedures in order

to determine the best processing methods to be applied.

Ceramic trimmers are available from domestic and foreign sources. Presently there are four U.S. suppliers as well as European and Japanese manufacturers. Table 2 has been included for easy comparison of the various style trimmer capacitors currently available. ▲

## TEFLON TRIMMER CAPACITORS

By LARRY G. FISCHER / Components Development Engineer, E.F. Johnson Co.

**T**HE Teflon trimmer capacitor has been made possible by the development of Teflon (*duPont* registered trademark) tetrafluoroethylene resins. These resins are members of the fluorocarbon family and possess unique electrical and mechanical properties which are highly desirable in trimmer capacitors.

Teflon is often used for its outstanding chemical inertness and low coefficient of friction. Other desirable physical properties include a low moisture adsorption rate of less than 0.01% which contributes to its high surface resistivity (greater than  $10^{11}$  ohms at 100% relative humidity). The material has exceptionally good thermal stability between  $-400^{\circ}\text{F}$  and  $+500^{\circ}\text{F}$ . The tetrafluoroethylene resins are excellent insulators and have high arc resistance. When exposed to an arc, the material vaporizes and leaves no carbonized path. The short-term dielectric strength of Teflon is quite high, varying around 500 volts per mil, depending on the thickness. The dielectric constant is low (approximately 2.02) and is unchanged from 60 Hz to 3000 MHz.

Because the dissipation factor of Teflon is small—less than 0.0003 from 60 Hz to 3000 MHz, "Q" is relatively high. "Q" will also be quite constant over a wide frequency range because the dissipation factor is quite constant. Data obtained from a batch of Teflon trimmer capacitors is shown in Fig. 1.

When tetrafluoroethylene resin is properly used as a dielectric, one can obtain a capacitor which is electrically stable over a wide range of conditions. The Teflon trimmer capacitor, constructed as shown in Fig. 2, is such a device. By designing the parts so that the Teflon displaces all possible air from between the rotor and the stator, the chance of variations in capacitance due to entrapped air is held to a minimum. The Teflon must be compressed when it is forced into the stator shell. The rotor screw then fits tightly into the Teflon. This method of construction also keeps all foreign particles, such as dust, moisture, and solder flux, from contaminating the dielectric and degrading the performance of the capacitor.

The capacitance is adjusted by turning the rotor screw in or out of the Teflon dielectric. The fine threads on this screw give a high degree of resolution to the adjustment so minute changes in capacitance can be made easily. This construction also reduces the number of parts needed in the capacitor, resulting in lower cost and greater reliability.

Capacitors using Teflon as a dielectric may also be constructed by two other methods: (1) substituting Teflon for air in a multi-plate capacitor, and (2) sliding a Teflon coated rotor in or out of a shell. Neither method utilizes Teflon to its fullest advantage because air is not completely eliminated. Contaminates may therefore come between the Teflon dielectric and rotor or stator to affect the set capacitance.

The high-voltage resistance of Teflon enables the trimmer to be used where other dielectrics would suffer from breakdown. The trimmer is especially useful in filter networks that require careful adjustment and long-term stability. Test-equipment manufacturers have found it ideal for use in equipment subject to extreme environmental conditions

where moisture, dust, or shock could disrupt other types of capacitors. Circuits used over very wide frequency ranges, especially in the v.h.f. and u.h.f. regions, will benefit from the exceptionally stable "Q." A limitation of this capacitor, however, is the maximum capacitance that can be easily obtained. Values above 5 pF are not common in this type of trimmer capacitor.

The unique mounting features of this trimmer provide two distinct advantages: (1) It can be readily used in circuits where minimum lead length is of vital importance. (2) The printed-circuit mounting features of the device enable it to be placed directly on the PC board by modern assembly equipment. Panel-mounted versions are also available. Typical prices are from 40¢ to 60¢ in small lots. ▲

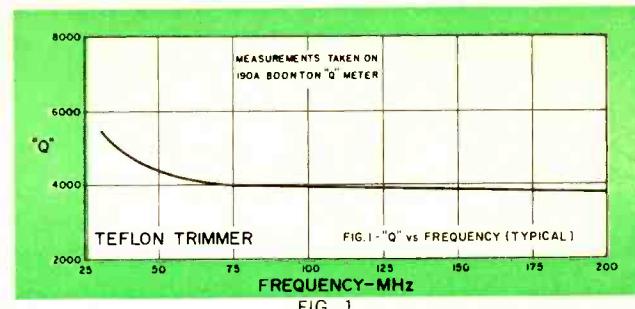
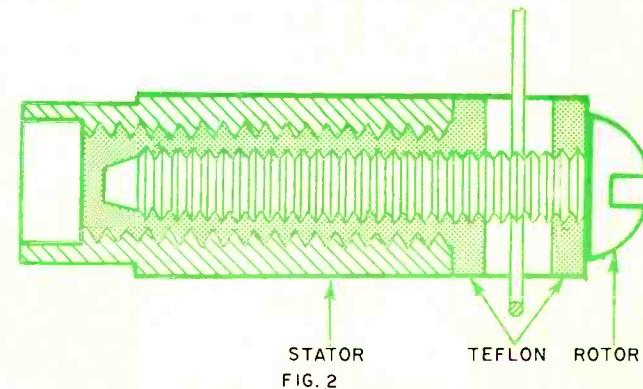
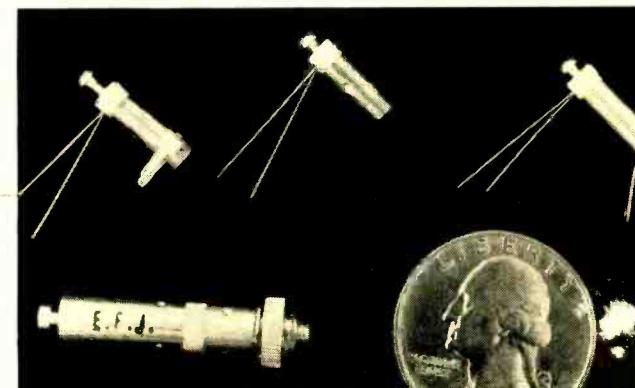


FIG. 1



Four common versions of Teflon dielectric trimmer capacitors showing the various mounting configurations used.





The author joined JMC in 1951. For the past ten years he has been actively engaged in the development of new products. At the present time, he is working on improving capacitor production methods.

# Air Tubular Trimmer Capacitors

By ROBERT HOWERING / Manager of Engineering  
Johanson Manufacturing Corp.

*This precision trimmer features small size, good stability, high resolution, and a maximum "Q," particularly at the higher operating frequencies.*

A VARIABLE capacitor must perform in a predictable and consistent manner. It must be accurate, stable, and may have to be small enough to be used with micro-circuits. It cannot have dips or reversals which will give false peaks or null points. It should provide high resolution through fine tuning, which is especially important in making critical adjustments at the higher frequencies. Once adjusted, it should be able to hold that adjustment under a wide range of stresses, both physical and electrical.

The air tubular trimmer meets all these requirements. Its tubular construction has the physical strength of a column, where stress is equally distributed. Indeed, air tubular trimmers have landed on the Moon—have been dropped from planes—and have even been shot from cannons. Because of its axial construction, it also has both lower inductance and higher "Q" values. And it has no detrimental mechanical resonant frequency points which might induce microphonics or physical fatigue. Lastly, a tubular air trimmer employs the stable, consistently predictable, and least expensive dielectric there is—air.

However, there are factors that may dictate the use of other dielectrics. One of these is dielectric strength or breakdown. Because size is often important, the dielectric thickness must be kept small. This results in lower breakdown voltages, around 1000 V d.c. or less. Other dielectrics will afford higher voltage ratings, but equally important characteristics, such as "Q," stability and mechanical strength, may have to be compromised. Another factor may be the need for higher capacitance in a given size. This requires the use of a dielectric with a dielectric constant that is greater than air.

Still another factor is cost. The use of air in a miniature trimmer requires the electrodes to be held in precise position relative to each other over the entire capacitance

range, and to tolerances of tens of thousandths of an inch. This must be accomplished without the use of any guides or supports in between the electrodes to degrade the properties of air. This means relatively expensive production. But today the tubular air capacitor can be produced more economically than ever before due to careful design; the use of high-speed precision equipment, and accurate, skillful assembly by experienced people. So cost is becoming less of a consideration in selection. (Present prices range from about \$3.50 to \$6.00 each in quantities up to 1000.)

The stability and dependability of the tubular air capacitor have led to considerable acceptance of it for applications in critical and even hostile environments, such as the satellite and space programs. There are 74 in Syncom II alone, and others are destined to land on Mars. It is not insignificant that the air tubular, which works at frequencies from v.l.f. up to u.h.f. is the only capacitor that will work into the microwave ranges. Some smaller models, which work in the C- and X-band regions, are self-resonant above 10 GHz. One interesting miniature type for such applications is supplied for mounting the same way that a fixed chip capacitor is mounted. The vertical mounting style has become very popular because it facilitates mounting the trimmer in approximately half the usual space, anywhere in the circuit.

## Types and Characteristics

Specifications permitting, the tubular air trimmer can be used in any application currently using other trimmers. And it is usable where higher orders of "Q" and optimum stability are required. A listing of typical specifications is given in Table 1.

While at least four designs of rotors and associated torque-maintaining devices are available, the basic structure in all cases is similar. Capacitance is established and varied

by means of coaxial tubes moved laterally, with the air dielectric between the tubes. These tubes are housed in a ceramic insulator, with the assembly joined by solder.

Units of  $\frac{3}{32}$ -in diameter, in the 0.8 to 10-pF range and with standard connections are the most in demand, thus are produced in the largest quantity and represent the lowest cost. This demand does, however, appear to be stabilizing, while demand for the smaller sizes (0.220-in diameter, 0.4 to 10 pF, and 0.145-in diameter, 0.35 to 5 pF) is rapidly increasing.

### MIL-Specification

In mid-1969, MIL-C-14409 was revised, and the tubular air trimmer was for the first time included in a MIL-Spec. Styles PC 25 and PC 26 are listed under /12 and /13 of MIL-C-14409C. This Spec offers only a limited choice, two configurations of the  $\frac{3}{32}$ -in diameter, 0.8 to 10 pF, being listed. The MIL requirements are substantially less than the capability of these units; stock trimmers offer greater stability and stress-handling capability than the Spec calls for.

Certain designs present problems in connection with the phenomenon termed "dynamic noise." This condition is the result of varying contact resistance between the rotor and its mount, and is apparent only under certain conditions of higher frequency and of circuit configuration. "Noise-free" designs are available, and the user is strongly advised to make his parts choice carefully where noise may be a consideration.

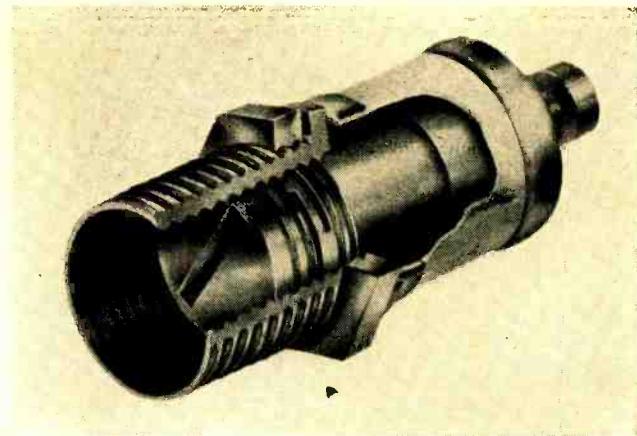
### Future Outlook

As frequencies go higher, the obvious direction for the capacitor is toward still smaller sizes. We look to narrower air gaps in the coaxial structure. This will be accomplished by refining manufacturing techniques to allow less air gap without affecting linearity or other parameters. This will result in higher capacitance in the same package, or equal capacitance in a smaller package.

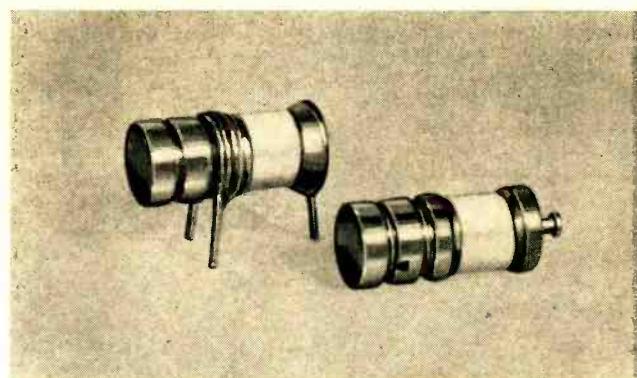
We look forward to development, by the instrument makers, of an accurate "Q"-measurement device at the higher frequencies—the higher the better. We would also hope for more accurate capacitance bridges at the lower values of capacitance.

The concern with "noise" will no doubt increase. This will probably lead to the development of comprehensive noise specifications.

As user knowledge and acceptance increase, we expect



**Cutaway view of a typical air tubular trimmer capacitor.**  
The stator and rotor electrodes are coaxial metal tubes, separated by air as the dielectric, which intermesh as the adjustment screw is rotated to provide the variation in capacitance. A threaded-on cap with a silicone rubber washer is normally used to cover the screw and seal the trimmer. Units are available in gold, silver, chrome finish. The materials used in the trimmer are Invar and brass, while the supporting ceramic insulation is glazed alumina. High-temperature solder is used in the assembly.



**The air tubular at left is designed for PC-board mounting; unit at right is for panel mounting, with turret terminal.**

that a MIL-Spec will develop for this type—satisfying the demand for stress capabilities in excess of MIL-C-14409. In the process, we believe the demand for the air tubular trimmer will continue to rise. ▲

**Table 1. Specifications for a line of air tubulars. The various types are available in a variety of mounting configurations, including panel-mount, PC-board mount, and strip-line mount. Lug, lead, or turret terminals are available.**

SERIES	5200	5400	5500	5600	5700	5800
Capacitance (pF)	0.8-10	1-14	1-20	1-30	0.6-6	0.4-3.5
Dielectric Strength (V d.c.)	500	500	500	500	500	500
"Q"	>5000	>3000	>1500	>1000	>10,000	>10,000
Insul. Res. ( $M\Omega$ )	$>10^6$	$>10^6$	$>10^6$	$>10^6$	$>10^6$	$>10^6$
TC (ppm / °C)	0 ± 15	0 ± 25	0 ± 30	0 ± 30	0 ± 15	0 ± 15
Torque (in-oz)	1.5	1.5	1.5	1.5	0.4-4	0.3-3

**Notes:** Capacitance measured at 1 MHz; "Q" measured at 100 MHz at max. C: Temp. Range - 65 to + 125° C.



The author, Assoc. Professor of Electrical Engineering at Pratt Institute, received his B.E.E. cum laude from CCNY in 1951 and attended Columbia and Hofstra Universities (M.A. in Physics, 1958). His areas of interest are solid-state electronics and computer logic. He is the co-author of "Semiconductor Fundamentals: Devices and Circuits" and is currently at work on a new book, "Electronic Circuit Analysis" which will be published very soon.

# Designing LC Tuned Circuits

By A. H. SEIDMAN / Contributing Editor

*How to choose the proper capacitance value for a given tuning range and how to properly temperature compensate resonant circuits. Also included are many practical examples illustrating circuit design.*

THE other articles in this Special Section described several types of variable capacitors that represent the present state-of-the-art. Information gained from these articles should enable the engineer and technician to select the right variable capacitor for a particular application. There are some questions, however, that remain unanswered. For example: What range of  $C$  is required to cover a band of frequencies? What is the significance of the  $L/C$  ratio? What should the voltage rating of a capacitor be? If a variable capacitor having a negative temperature coefficient is needed, how should it be specified?

The object of this article is to supply the reader with

design procedures, illustrated by practical examples, to permit him to arrive at answers to these and other questions pertaining to  $LC$  tuned circuits.

## Series RLC Circuits

In communications circuits, like those found in receivers, one desired frequency must be selected from many while all other frequencies are rejected. Two methods generally employed for accomplishing this depend on the properties of series and parallel  $RLC$  resonant circuits.

Consider the series  $RLC$  tuned circuit of Fig. 1A. Its impedance  $Z_s$  is:

$$Z_s = R + j(\omega L - 1/\omega C)$$

where  $\omega (= 2\pi f)$  is the angular frequency in radians per second. Resistance  $R$  is the total series resistance of the circuit including the winding resistance of the coil. The variations in reactances  $X_L = \omega L$  and  $X_C = -1/\omega C$  with frequency are shown in Fig. 1B. Note that at one, and only one frequency,  $f_r$ ,  $X_L = X_C$ . Frequency  $f_r$  is the *resonant frequency* and at this frequency the circuit is said to be in resonance. At the resonant frequency of a series tuned circuit,  $Z = R$  and is therefore real, and current  $I$  is maximum and in phase with the impressed sinusoidal voltage  $E$  (power factor is therefore unity). The resonant frequency  $f_r$  may be determined by equating  $X_C$  to  $X_L$  and solving for  $f_r$ ; the result obtained is:

$$f_r = \frac{1}{2\pi\sqrt{LC}} = \frac{0.159}{\sqrt{LC}} \text{ Hz} \dots \dots \dots (1)$$

where  $L$  is in henrys and  $C$  is in farads.

Plots of  $Z$  and  $I$  as a function of frequency are given in Fig. 2A. To obtain further insight into the series  $RLC$  circuit it is useful to plot the magnitude of the ratio of the admittance  $Y$  ( $Y = 1/Z$ ) to its value at resonance (which is equal to  $1/R = G$ ) as a function of frequency. This *normalized* plot is shown in Fig. 2B. The expression for  $|Y|/G$  is given by:

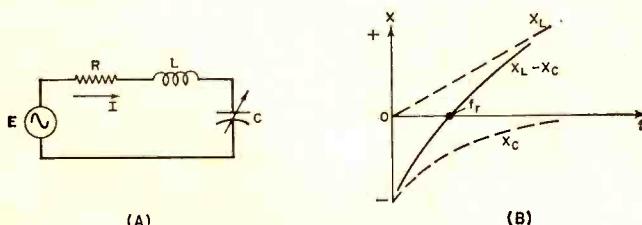
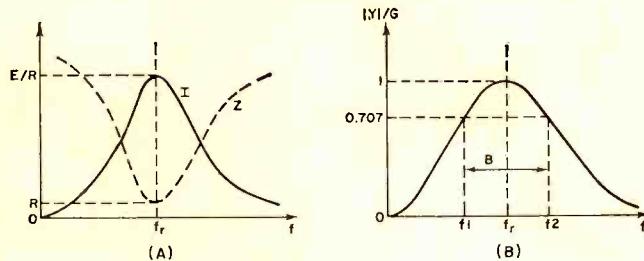


Fig. 1. The series RLC circuit along with its characteristics.

Fig. 2. Current, impedance, and admittance of series RLC circuit is shown here along with the bandwidth.



$$\frac{|Y|}{G} = \sqrt{1 + \frac{1}{R^2} \left( \omega L - \frac{1}{\omega C} \right)^2} \quad \dots \dots \dots (2)$$

We can now define the  $Q$  of such a series circuit as:

$$Q_s = \omega_r L / R \quad \dots \dots \dots (3a)$$

Since  $\omega_r = 1/\sqrt{LC}$ , we can also express  $Q_s$  by:

$$Q_s = \frac{1}{R} \sqrt{\frac{L}{C}} \quad \dots \dots \dots (3b)$$

In terms of  $Q$ , equation (2) may be expressed by:

$$\frac{|Y|}{G} = \frac{1}{\sqrt{1 + Q_s^2 \left( \frac{f}{f_r} - \frac{f_r}{f} \right)^2}} \quad \dots \dots \dots (4)$$

From Fig. 2B, it can be seen that the bandwidth,  $B$ , of the series  $RLC$  circuit is equal to the range of frequencies  $f_2 - f_1$  where the magnitude of  $|Y|/G = 0.707$  its value at the resonant frequency; the frequencies at which the magnitude is equal to the 0.707 value are also referred to as the half-power or  $-3$  dB points. Using equation (4) we obtain:

$$B = 2\pi f_r / Q_s \text{ or } 2\pi R f_r / \sqrt{L/C} \quad \dots \dots \dots (5)$$

Based on equation (5) we can then state that for a given value of  $R$ , the bandwidth varies *inversely* with  $Q_s$  or  $\sqrt{L/C}$ . Therefore, a high  $Q$  or a high  $L/C$  ratio yields a narrow bandwidth whereas a low  $Q$  or a low  $L/C$  ratio results in a wide bandwidth.

From a practical standpoint the  $Q$  of the circuit ( $Q_s$ ) is approximately equal to  $Q$  of the coil itself ( $Q_L$ ) that is:

$$Q_s \approx Q_L = 2\pi f_r L / R_L$$

where  $R_L$  is the effective series resistance of the coil winding. Resistance  $R_L$  is not constant but increases with frequency owing primarily to skin effect. Some typical curves showing the variation of  $Q_L$  as a function of frequency for single-layer coils with different coil length-to-diameter ratios and different wire size are shown in Fig. 3. Generally, a  $Q \geq 100$  is obtainable and for some coils the  $Q$  is nearly constant with frequency. If, in Fig. 1A, resistance  $R$  includes, for example, the input resistance of a junction transistor, the  $Q$  of the circuit will be much less than the coil  $Q$ .

The  $Q$  of a good quality variable capacitor can be greater than 1000 at frequencies of 100 MHz and higher. For this reason, the  $Q$  of the coil is usually the dominant factor in determining the bandwidth of a tuned circuit.

At resonance in a series  $RLC$  circuit, the magnitude of voltage  $|E_L|$  across the coil is  $|E_L| = |E| X_L / R = Q_s |E|$ . But at resonance the voltage across the coil is equal to the voltage across the capacitor  $|E_C|$ ; therefore, the magnitude of the voltage across the capacitor at resonance is  $|E_C| = Q_s |E|$ . This must be considered in specifying the capacitor, as well as the coil.

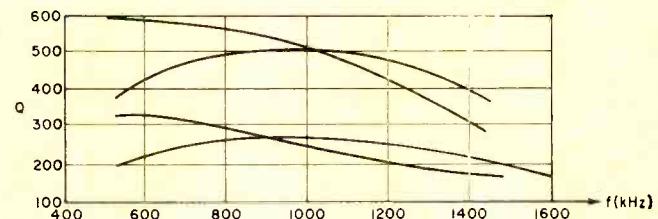


Fig. 3. Some typical  $Q$  values for single-layer coils.

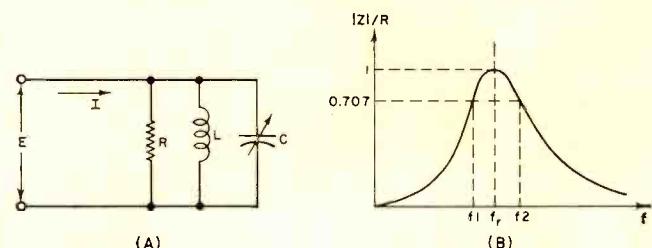


Fig. 4. Parallel RLC circuit along with its characteristics.

### Parallel RLC Circuits

Let us now examine the parallel  $RLC$  circuit of Fig. 4A. The impedance  $Z_p$  of the circuit is:

where  $Q_p$  is the  $Q$  of the parallel resonant circuit and is de-

$$Z_p = \frac{R}{1 + jR \left( \omega C - \frac{1}{\omega L} \right)} = \frac{R}{1 + jQ_p \left( \frac{f}{f_r} - \frac{f_r}{f} \right)} \quad \dots \dots \dots (6)$$

fined by:

$$Q_p = \frac{R}{\omega_r L} = R \sqrt{\frac{C}{L}} \quad \dots \dots \dots (7)$$

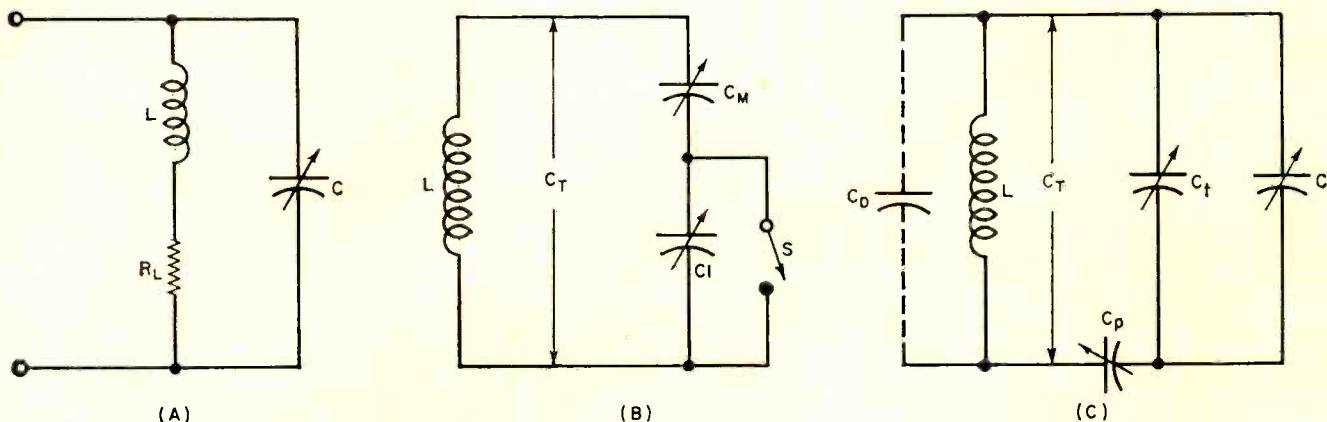
At resonance  $\omega_r C = 1/(\omega_r L)$  and the resonant frequency of the parallel circuit is identical to that of the series circuit and is expressed by the same equation (1). Impedance  $Z_p$  is maximum and current  $I$  is minimum at resonance, opposite to that for the series case. Fig. 4B shows a normalized plot of  $|Z|/R$  as a function of frequency. The bandwidth of the parallel circuit can be expressed as:

$$B = 2\pi f_r / Q_p \text{ or } \frac{2\pi f_r}{R \sqrt{\frac{C}{L}}} \quad \dots \dots \dots (8)$$

Unlike the series circuit, from equation (8) it is seen that for a given value of  $R$  the bandwidth of the parallel resonant circuit varies inversely with a high  $C/L$  or with a low  $L/C$  ratio.

A more typical parallel tuned circuit is that of Fig. 5A where the coil resistance  $R_L$  is shown in series with  $L$ . It can

Fig. 5. (A) Parallel tuned circuit with resistance shown in series with coil. (B) Use of the series capacitor to expand tuning range. (C) Use of trimmer and padder capacitors in circuit.



be shown that the impedance  $Z$  of the network is:

$$Z = \frac{R_L Q_s^2 \left( 1 + j \frac{f_r}{Q_s f} \right)}{1 + j Q_s \left( \frac{f}{f_r} - \frac{f_r}{f} \right)} \quad (9)$$

For  $Q_s \geq 10$  the imaginary term in the numerator may be neglected in the vicinity of the resonant frequency and expression (9) becomes identical to (6) where  $R = Q_s^2 R_L$  and  $Q_s \approx Q_p$ .

Returning to (9) when  $f = f_r$ , impedance  $Z$  is not real because the numerator is still complex. Analysis shows that two resonant frequencies can be defined: (1) for unity power factor  $f_{rm} = f_r \sqrt{1 - 1/Q_s^2}$  and (2) for maximum magnitude of  $Z$ ,  $f_{rm} = f_r \sqrt{1 - 1/Q_s^4}$ . For  $Q_s \geq 5$ , these expressions are, for all practical purposes, equal to  $f_r$ .

For parallel resonance the current flowing in  $C$  and  $L$  is equal to  $Q_s I$ . The voltage across  $L$  and  $C$  is equal to the impressed circuit voltage.

### Practical Examples

At this point we shall apply the results of the previous section to solve some practical problems dealing with tuned  $LC$  circuits. Each application will be illustrated with an example. For many calculations a computer terminal will reduce the arithmetic drudgery often encountered in solving tuned-circuit problems. If a computer is not available, the next best bet is a reactance slide rule or a reactance chart like that shown in Fig. 6. To find reactance on the chart, enter the frequency and proceed vertically until the chosen value of  $C$  or  $L$  is intersected. At the point of intersection a horizontal line projected to the left vertical axis determines the reactance. For example, at 10 kHz and  $L = 100 \mu\text{H}$ ,  $X_L \approx 6.3 \text{ ohms}$ .

To find the resonant frequency, determine the intersection of the  $L$  and  $C$  lines corresponding to the values in your design. A line projected vertically down from the point of intersection determines the resonant frequency. For example, if  $L = 20 \mu\text{H}$  and  $C = 100 \text{ pF}$ , the resonant frequency  $f_r \approx 3600 \text{ kHz}$ . If  $L$  (or  $C$ ) and  $f_r$  are shown, the value of the other component  $C$  (or  $L$ ) can be determined by entering  $f_r$  and projecting a line vertically until the value of  $L$  (or  $C$ ) is intersected. For example, if  $f_r = 100 \text{ kHz}$  and  $L = 0.001 \text{ H}$ ,  $C \approx 0.0025 \mu\text{F}$ .

The analytical methods developed for the design of tuned circuits will enable the engineer to arrive at component values that will, in general, be excellent approximations of expected performance. For practical reasons, however, the final choice of components may be dictated by other factors, such as cost and availability. If, for example, a  $Q_p = 50$  is required for a parallel tuned circuit, it may be more economical to use a coil with a  $Q_p = 100$  and shunt a resistance across the circuit to bring the  $Q$  down to 50.

If the tuned circuit were connected across the input of an active device whose input capacitance varied with operation, the minimum value of capacitance used in the tuned circuit would have to be much greater than the input capacitance to "swamp" its effect on the resonant frequency. These practical situations must always be recognized in the design of tuned circuits.

#### Example 1:

Design a parallel tuned  $LC$  circuit to cover the AM broadcast band from 550 kHz to 1600 kHz. It is assumed that a practical bandwidth for the circuit is a minimum of 20 kHz at the lower frequency of 550 kHz. Select the values of  $L$ ,  $Q_s$ , and  $C$ . Assume that the distributed capacitance of the coil and the wiring capacitance are on the order of 20 pF. The minimum capacitance of this variable tuning capacitor is 25 pF.

**Solution.** Value of  $L$  is selected for minimum capacitance in the circuit ( $20 \text{ pF} + 25 \text{ pF} = 45 \text{ pF}$ ) at 1600 kHz. Using

the reactance chart of Fig. 6 or equation (1),  $L \approx 220 \mu\text{H}$ .

The maximum value of  $C$  is determined at the lower frequency, 550 kHz, using this value for  $L$ . From the reactance chart  $C \approx 380 \text{ pF}$ . But there is 20 pF of distributed capacitance; therefore the maximum capacitance required is  $380 - 20 = 360 \text{ pF}$ . A variable capacitor with a range of 25 pF to 360 pF is selected.

From equation (5)  $Q_s = 2\pi f_r / B = (6.28 \times 550 \times 10^3) / (20 \times 10^3) = 173$ .

#### Example 2:

The frequency range of a tuned circuit may be extended by inserting a capacitor  $C_1$  in series with the main tuning capacitor  $C_M$  as shown in Fig. 5B. The value of two capacitors in series ( $C_T$ ) is:

$$C_T = C_1 C_M / (C_1 + C_M) \quad (10)$$

The value of  $C_1$  is determined from equation (10):

$$C_1 = C_T C_M / (C_M - C_T) \quad (11)$$

Because  $L$  is the same whether  $C_M$  or  $C_T$  in series with  $C_1$  is present, then for two frequencies  $f_1$  and  $f_2$ , from (1) we can write:

$$\frac{(0.159)^2}{f_1^2 C_M} = \frac{(0.159)^2}{f_2^2 C_T} \text{ or } C_T = f_1^2 C_M / f_2^2 \quad (12)$$

Suppose the maximum capacitance of  $C_M = 100 \text{ pF}$  and  $C_1$  is shorted, that is, switch  $S$  closed. The circuit tunes from  $f_1 = 1 \text{ MHz}$  to  $f_2 = 2 \text{ MHz}$ . (a) What values of  $C_{M(\min)}$ ,  $C_1$ , and  $L$  are required so that the minimum frequency with  $S$  open is 2 MHz? (b) What is the maximum frequency the circuit can tune to with  $S$  open?

**Solution.** (a) Equation (12) may be used for finding  $C_{M(\min)}$  with  $S$  open. From equation (12),  $C_T = C_{M(\min)} = (1)^2 100 \text{ pF} / (2)^2 = 25 \text{ pF}$ . This represents the minimum capacitance of the main tuning capacitor. Using equation (11),  $C_1 = (25 \times 100) / (100 - 25) = 33.3 \text{ pF}$ .

Inductance  $L$  will be chosen so that it will resonate with  $C_M = 100 \text{ pF}$  at 1 MHz when  $S$  is closed. Using the reactance chart of Fig. 6,  $L \approx 250 \mu\text{H}$ .

(b)  $C_{T(\min)} = (25 \times 33.3) / (25 + 33.3) = 14.3 \text{ pF}$ . From the reactance chart  $f_{max} \approx 2.5 \text{ MHz}$ .

#### Example 3:

An oscillator circuit which may be used in a superheterodyne receiver is shown in Fig. 5C. Capacitor  $C$  is the main tuning capacitor,  $C_t$  is the trimmer, and  $C_p$  the padder capacitor. The distributed capacitance across  $L$  is represented by  $C_D$ . The net capacitance across  $L$ , defined by  $C_T$ , is:

$$C_T = \frac{(C + C_t) C_p}{C + C_t + C_p} + C_D \quad (13)$$

Solving (13) for  $C_p$  we obtain:

$$C_p = \frac{(C + C_t) (C_T - C_D)}{C + C_t + C_D - C_T} \quad (14)$$

To keep the numbers simple, assume that a receiver tunes from 550 kHz to 1550 kHz and the intermediate frequency is 450 kHz. The oscillator, therefore, must tune from  $(550 + 450) \text{ kHz} = 1 \text{ MHz}$  to  $(1550 + 450) \text{ kHz} = 2 \text{ MHz}$ . Let inductance  $L = 200 \mu\text{H}$ ,  $C$  tunes from 10 pF to 240 pF,  $C_t$  is set to 10 pF, and  $C_D = 10 \text{ pF}$ . Select  $C_p$  and check to see if for the chosen value of  $C_p$  the oscillator tunes to 2 MHz at the high end.

**Solution.** The value of  $C_p$  is determined at the lowest frequency of the oscillator, that is, at 1 MHz in this example. Using the reactance chart it is found that for  $f = 1 \text{ MHz}$  and  $L = 200 \mu\text{H}$ ,  $C_T \approx 130 \text{ pF}$ . From equation (14),  $C_p = (240 + 10) (130 - 10) / (240 + 10 + 10 - 130) = 230 \text{ pF}$ .

For the value of  $C_p = 230 \text{ pF}$ , the minimum capacitance in the circuit is:  $C_{T(\min)} = [230 (10 + 10) / (230 + 10 + 10)] + 10 \approx 28.4 \text{ pF}$ . From the reactance chart, the maximum frequency of oscillation is approximately 2.1 MHz, which is slightly greater than the required 2 MHz. The trimmer capacitor  $C_t$  may be adjusted to obtain the exact value of 2 MHz. Varying the trimmer will have negligible effect on the low frequency limit of the oscillator.

# REACTANCE CHART

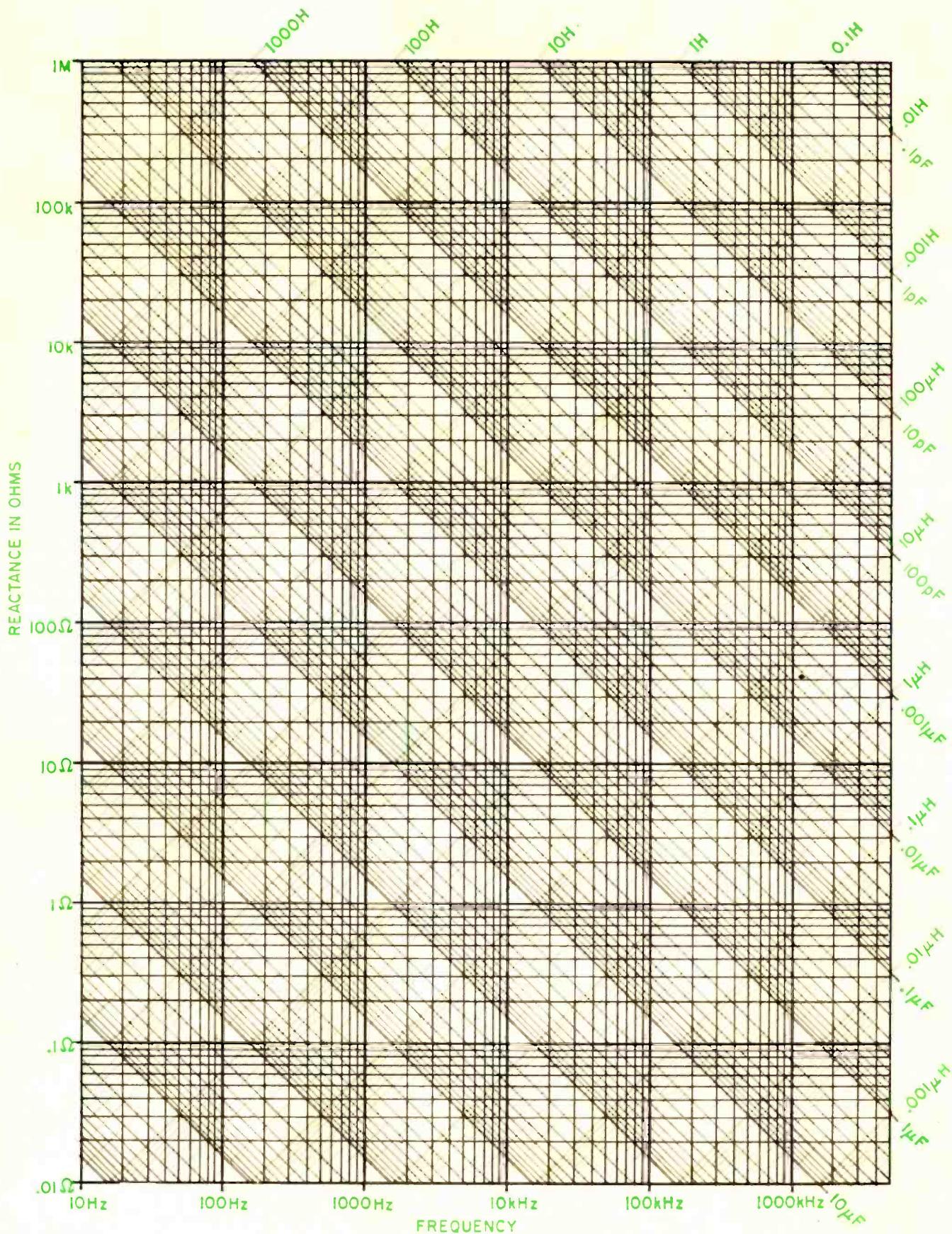


Fig. 6. Inductive and capacitive reactance over a wide range of operating frequencies.

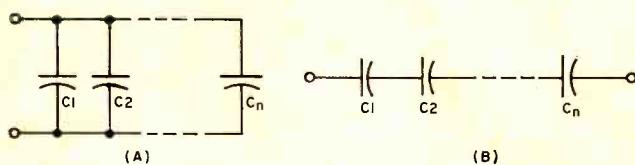


Fig. 7. Capacitors in parallel and in series have differing equivalent temperature coefficients as described.

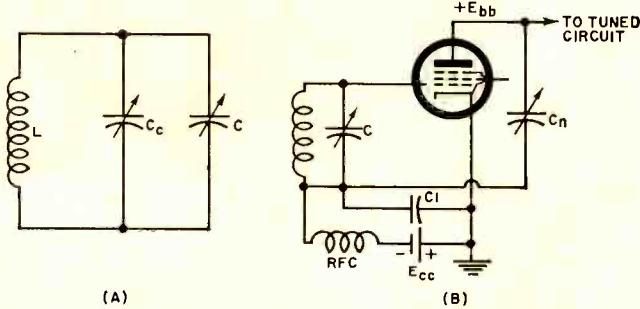


Fig. 8. (A) Circuit showing use of temperature-compensating trimmer across main tuning capacitor. (B) Circuit diagram illustrating the use of neutralizing trimmer.

Temperature drift may be a serious problem for tuned circuits such as those used in an oscillator. Because coils exhibit a positive temperature coefficient, it is possible to introduce an appropriate capacitor in the circuit, such as a ceramic type, which has a negative temperature coefficient to cancel the positive coefficient of the coil. Temperature coefficient,  $TC$ , of a capacitor is defined as:

$$TC = \frac{(C_2 - C_1) \cdot 10^6}{C_1(T_2 - T_1)}$$

where  $TC$  = temperature coefficient in parts per million per  $^{\circ}\text{C}$  ( $\text{ppm}/^{\circ}\text{C}$ );  $T_1$  = reference temperature, normally taken at  $25^{\circ}\text{C}$ ;  $T_2$  = maximum test temperature, typically  $85^{\circ}\text{C}$  or  $125^{\circ}\text{C}$ ;  $C_1$  = value of capacitor at  $T_1$ ; and  $C_2$  = value of capacitor at  $T_2$ .

If  $TC$  is positive the letter "P" precedes the values of the coefficient; if negative, the letter "N" precedes the coefficient. For a zero temperature coefficient, the designation "NPO" is used.

For a number of capacitors in parallel (Fig. 7A) it can be shown that the equivalent temperature coefficient  $TC_p$  for the combination is:

$$TC_p = \frac{C_1(TC_1) + C_2(TC_2) + \dots + C_n(TC_n)}{C_1 + C_2 + \dots + C_n} \quad .(15)$$

where  $TC_1$  is the temperature coefficient of  $C_1$ , etc.

In the case of capacitors in series (Fig. 7B), the equivalent temperature coefficient  $TC_s$  is:

$$TC_s = C_T (TC_1/C_1 + TC_2/C_2 + \dots + TC_n/C_n) \quad .(16)$$

where  $C_T = 1/(1/C_1 + 1/C_2 + \dots + 1/C_n)$ .

#### Example 4.

Assume that two capacitors in parallel have the following nominal values:  $C_1 = 30 \text{ pF}$  and  $TC_1 = +200$ ,  $C_2 = 20 \text{ pF}$  and  $TC_2 = -500$ . Determine the equivalent temperature coefficient of the combination.

*Solution.* From equation (15),  $TC_p = [30(200) + 20(-500)] / (30 + 20) = -80 \text{ ppm} = N80$ . Total capacitance is, of course,  $50 \text{ pF}$ .

Consider the parallel tuned circuit of Fig. 8A where  $C_e$ , a temperature-compensating capacitor, is shunted across main-tuning capacitor  $C$ . Let  $C_T = C_e + C$ . Accounting for the effects of the temperature coefficient, equation (1) may be expressed as:

$$f_r = \frac{0.159}{\sqrt{LC_T(1 + TC_L)(1 + TC_p)}}$$

where  $TC_L$  is the temperature coefficient of the coil (a typical value is  $+30 \text{ ppm}$ ) and  $TC_p$  is the temperature coefficient of  $C_T$ . Expanding terms under the radical we obtain:

$$LC_T(1 + TC_L + TC_p + TC_L \cdot TC_p)$$

Because  $TC_p$  and  $TC_L$  are in ppm, the product  $TC_L \cdot TC_p$  is much less than either  $TC_L$  or  $TC_p$  and may be neglected; therefore, the preceding expression reduces to:

$$LC_T(1 + TC_L + TC_p)$$

If  $TC_L = -TC_p$ , then the expression is equal to  $LC_T$  and the frequency becomes independent of temperature.

#### Example 5:

For the parallel-tuned circuit of Fig. 8A,  $C = 200 \text{ pF}$  and  $TC = +50 \text{ ppm}$ ;  $C = 20 \text{ pF}$ . Determine the temperature coefficient of the temperature compensating capacitor  $C_e$  to compensate for the positive temperature coefficient ( $+30 \text{ ppm}$ ) of the coil.

*Solution.* From equation (15)  $TC_p = -30 = [20(TC_e) + 200(50)] / (20 + 200)$ . Solving for  $TC_e$ , a value of  $TC_e = -830 \text{ ppm}$  is obtained. A capacitor with a negative temperature coefficient close to this value would be used.

Practical capacitors have tolerances on their values of temperature coefficient and capacitance. Although, for simplicity, these were neglected in our examples, they most likely will have to be considered in the design. Furthermore, the temperature coefficients of capacitors are not constant with temperature. For this reason it is necessary to make temperature runs or calculations to determine the tracking of frequency with temperature.

Although ceramic trimmers have been used for temperature compensation, their  $TC$  is variable and their use is therefore not recommended when high precision is required. Special types of stable ceramic or glass piston trimmers are available, but at a premium price. Generally, a standard *fixed* ceramic capacitor having the required  $TC$  is used in the temperature compensation of tuned circuits.

Tuned circuits are often temperature-compensated experimentally. For example, suppose an oscillator, having a tuned circuit like that of Fig. 5C is set to frequency  $f_o$  at temperature  $T_1$ . At an elevated temperature  $T_2$  the change in  $f_o$  is measured to be  $f_1$ . The circuit is cooled to its initial temperature  $T_1$  and a negative-temperature-coefficient capacitor  $C_1$  having a coefficient of  $N500$  or  $N750$  is shunted across the main-tuning capacitor. The pad is adjusted to provide the same initial frequency  $f_o$ . The modified oscillator is again elevated to temperature  $T_2$  and the new frequency drift  $f_2$  measured. The actual value of  $C_e$  required is:

$$C_e = \frac{C_1 f_1}{f_2 \pm f_1}$$

The plus sign is used if  $f_2 > f_1$  and the minus sign is used if  $f_2 < f_1$ .

Although it is usually avoided if possible, there are occasions when it is necessary to neutralize an r.f. power amplifier to keep it from breaking into oscillation. A number of schemes exist and one example using a neutralizing capacitor  $C_n$  is illustrated in Fig. 8B. The voltage rating of the neutralizing capacitor is equal to the plate voltage  $E_{bb}$  for c.w. and SSB operation and  $2E_{bb}$  for AM. A typical value for  $C_1$  is  $1000 \text{ pF}$  and its voltage rating is equal to  $E_{bb}$ .

For neutralization,  $C_n C_i = C_1 C_{gp}$ , or

$$C_n = C_1 C_{gp} / C_i$$

where  $C_{gp}$  is the grid-plate capacitance of the tube and  $C_i$  includes the grid-cathode capacitance ( $C_{gk}$ ), stray capacitance, and the endframe capacitance of  $C$ . At very high voltages the neutralizing capacitor used is a vacuum type.

An attempt has been made to pick out from a multitude of  $LC$  tuned-circuits those designs that are fundamental in illustrating the selection and specification of variable capacitors. The literature is rich in other examples, charts, and nomograms for various tuned circuits and filters. Some books worth exploring include "Fundamentals of Circuit Theory" by Balabanian, "Essentials of Radio" by Shurzberg and Osterheld, ARRL's "The Radio Amateur's Handbook," and Terman's "Radio Engineers' Handbook."

The author wishes to thank William F. Geist, Design Supervisor at Hazeltine Corporation, for his comments on  $LC$  tuned-circuit design.

# Vacuum Variable Capacitors

By MURRAY SUNTAG / Associate Editor

*Widely used in broadcast transmitters and in other high-power equipment requiring high-voltage and high-frequency operation.*

**V**ACUUM capacitors are distinguished from other capacitors by their use of a vacuum instead of a "mass" (gas, liquid, or solid) dielectric. Variable capacitors use vacuum or gas (which includes air) dielectrics, of which the vacuum types offer the highest maximum-to-minimum capacitance-change ratio. Actually, about 70% of all vacuum capacitors produced are variables.

If electrical performance, rather than size and cost, were the only consideration in selecting a capacitor, then the vacuum type would be almost the only choice. In addition, since most capacitors are used in low-energy applications, the high efficiencies associated with vacuum types are generally not required. Consequently, over 95% of the capacitors manufactured use mass dielectrics.

Vacuum capacitors, both fixed and variable, are manufactured using either an evacuated glass or ceramic envelope with copper anodes at both ends. The enclosed heavy copper capacitor plates, shaped like tubular cans of different diameters telescopically arranged, are separated from each other by the vacuum dielectric. Each of the plate assemblies is provided with a heavy copper connection to fully utilize the high current-carrying capability of the copper plates. The capacitance of the vacuum variable capacitor is changed by turning the capacitance-adjustment screw causing one set of plates to move in or out with respect to the other set, varying the overlapping capacitor plate area (capacitance is directly proportional to plate area). As shown in the diagram, movement of the plates is effected in the vacuum by the use of bellows.

## Characteristics

Vacuum capacitors are characterized mainly by their ability to handle high current at high frequencies (up to 1000 MHz) and high voltages. As frequency and power are increased, this type becomes the smallest and most economic capacitor to use. In fact, for a given capacitance rating, the vacuum capacitor, due to its enormous dielectric strength can tolerate the highest possible voltage of any capacitor. The nominal maximum capacitance ranges in which both ceramic and/or glass vacuum variable capacitors are available, and their voltage ratings, are listed in the table.

Although a vacuum capacitor will withstand internal arcing over that would ordinarily destroy solid-dielectric capacitors, continuously applied voltages should never exceed 60% of its rated test (peak) voltage to obtain maximum capacitor efficiency and life, except as noted below. For d.c. plus r.f. applications, the sum of the d.c. plus the peak r.f. voltage should never exceed 60% of the peak test voltage.

Since vacuum capacitors are rated for a maximum peak test voltage and a maximum operating current, limited by temperature rise, it may be impossible to apply rated voltage without exceeding rated current at low capacitive-reactance values; hence, the capacitor will be current-limited. Likewise, at high capacitive-reactance values it may be impossible to apply rated current without exceeding rated voltage; hence, the capacitor will be voltage-limited.

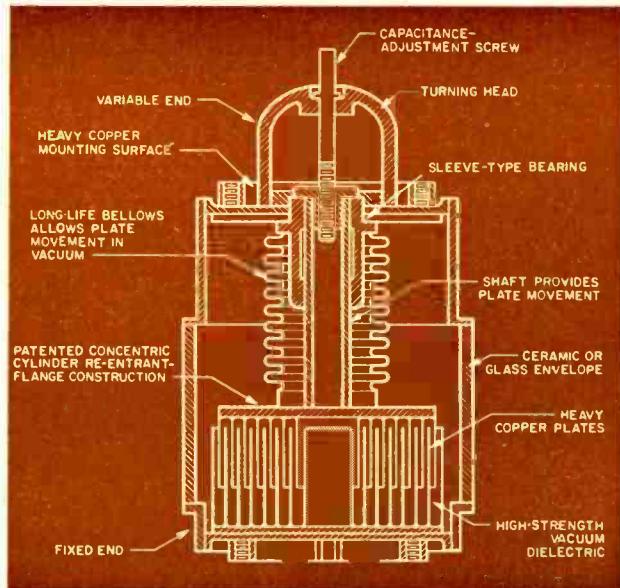
With normal convection cooling in a room ambient of 22°-26° C, ceramic vacuum capacitors are rated for an operating temperature of 120° C and glass vacuum capacitors for 87° C. However, by cooling the anodes of the capacitor externally with heat sinks (large straps, forced air, or water cooling) the current rating can be increased by a maximum of 50%. In addition, special vacuum capacitors can be constructed with forced-air-cooled bellows that will operate safely at 200% of the convection-cooled rating, or

with water-cooled bellows that will be limited only by voltage and be able to pass any current that can be impressed on them, through 32 MHz. Under no conditions should the current rating exceed 150% of the convection-current rating.

Because of its vacuum dielectric and low-loss glass or ceramic envelope, extremely low losses occur in vacuum capacitors. Consequently, the vacuum capacitor is a very efficient capacitor since the slight loss that does occur is only due to the r.f. resistance (few milliohms) of its copper construction. Typically, the ratio of stored energy to dissipated energy or "Q" factor is on the order to 1000 to 5000, or higher.

## Applications

Vacuum capacitors are mainly used in the tuning and neutralizing circuits of high-power r.f. generating devices, such as broadcast transmitters, induction and dielectric heating equipment, and r.f. sputtering equipment. In fact, the use of vacuum capacitors is almost mandatory for plate-tank circuits of high-power transmitters. They are also widely employed in high-voltage communications equipment where space and weight are critical and/or where they are exposed to severe environments (e.g., aircraft or marine vehicle transmitters and antenna couplers). ▲



Typical construction and electrical characteristics for ceramic and glass vacuum variable capacitors made by Jennings ITT.

NOMINAL MAXIMUM CAPACITANCE RANGE (pF)		VOLTAGE RATING (kV)
CERAMIC	GLASS	
200-3000	250-5000	2-5
---	8-5000	7.5-15
30-2300	---	7.5-20
---	25-500	20
250-2000	---	25-65
---	35-1000	25-60

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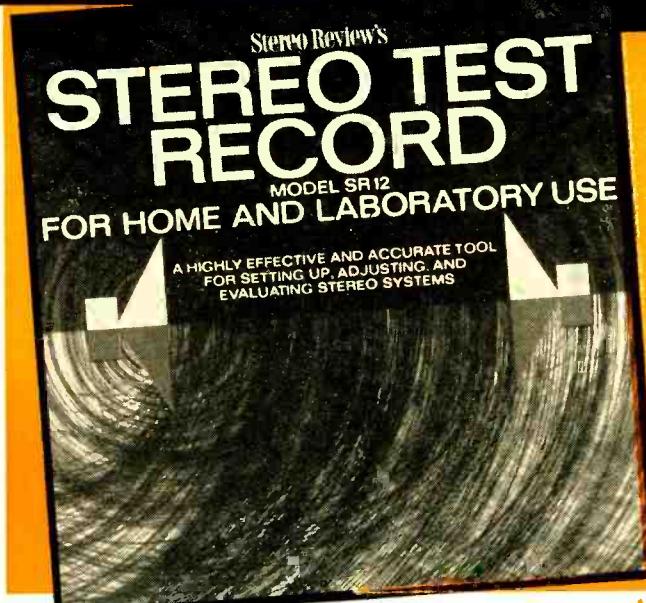
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- Sine-wave tone-bursts to test transient response of pickup.
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- Intermodulation sweep to show distortion caused by excessive resonances in tone arm and cartridge.
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# COMPUTERIZING YOUR GROCERY LIST

*By the end of the decade, computers promise to become indispensable in managing chain stores.*

By **John Frye**

MATILDA, the office girl at Mac's Service Shop, returned from her lunch hour grocery shopping in an obviously irritated frame of mind. "Sorry I'm late, Boss," she said to Mac, "but that supermarket was impossible today. I stood in that checkout lane a full half hour to get this ten-inch grocery slip. Now I wonder if I got everything I intended to get. You can't tell much by looking at this slip unless you're a genius at connecting prices marked only 'Mt' or 'Gr' with the items on your shopping list. Right now I feel more like 'Gr-r-r-r-r-r!'"

"Cheer up, Matilda; help is on the way," Mac solaced her. "My wife's younger brother, who works for a large computer company, stopped in last night on his way across the country; and this morning at breakfast he was regaling us with an enthusiastic account of how computers are just starting to move into supermarket management. I think you might like to hear about it—especially right now."

"I want to hear about it too," Barney said, sticking his head out of the door of the service department.

"You'd listen to me read tube price lists to get out of work," Mac retorted; "but come on. Suppose we start by picturing how a trip to the supermarket will be seven or eight years from now:

"First, Matilda, you will notice that the gondola or shelf carrying each item will carry a unit price, but the individual cans, jars, or boxes will not be price-marked. Instead each unit will carry a distinctive number made up of several digits. You will collect the various items in your cart just as you have always done and take them to the checkout counter. There the girl will place each item so that an Optical Character Recognition (OCR) scanner can read the identifying number and flash it to a computer that may be miles away. It will recognize the number, identify and price the item, and send back this information to be displayed for your benefit. Meat and other items sold by the pound will be placed on a scales there at the counter so that its number may be read as it is weighed, and it, too, will be identified and priced by the distant computer.

"Each item will be identified almost instantly and then placed on a conveyor belt that will take it to an automatic boxing device that will arrange all the items of your order neatly in a container ready to be carried out. When all the items in your cart have been identified, the girl will push a button and the computer will give you a grocery slip on which each item is identified by code number, description, and price. For example one line may read: '3489475 Orange Juice .49.' The bill will be totalled; taxes will be added; tendered coupons will be subtracted; trading stamps will be issued. If you prefer to use your credit card, you will place it in a slot and your hand in a little compartment. The computer will compare the outline of your hand with the outline on file assigned to the person to whom the card was issued. If the topography is the same, it will query the bank about your credit. If all is OK on both counts, this will be indicated and the amount of the grocery bill will be transferred from your account to that of the store. All this will take

place in a split second, and at the same time the items you bought will be automatically subtracted from the store's inventory and, if necessary, replacement stock will be ordered."

"Hey, I like the sound of that!" Matilda exclaimed. "I especially like that business of having items on the grocery slip identified, and it sounds as though it will take much less time to get checked out."

"Sounds pretty far-fetched to me," Barney said skeptically.

"I'm not talking crystal-ball stuff," Mac answered. "Supermarkets and computer manufacturers are already experimenting with systems similar to what I have described. When I tell you that *IBM*, *National Cash Register*, *Inventory Management Systems*, *General Electric*, *RCA*, the *Frieden Division of Singer*, the *Sweida-Kimball Division of Litton Business Systems*, the *American Totalisator Co.*, *Alpex Computer Corporation*, and the *ADS Anker Corporation* of West Germany are all deeply interested in computerizing the supermarkets, you will know I am not talking science-fiction.

"On the West Coast last fall *Inventory Management Systems, Inc.* arranged a pilot installation of its 'Marketron' system in a *Food Fair* store in Baldwin Hills, California. Nine combination cash register-inventory controller terminals were installed at checkout stations and hooked to a remote *Honeywell* computer on a real-time basis. In this instance the check-out operator key-punched the department, the quantity, and the code number of each item into the terminal. It flashed this information to the computer which recorded the price and displayed it for the customer to see on a readout at the terminal. At the same time the item or items were subtracted from inventory. At the end of the transaction the computer issued a totalled grocery slip such as I have described. In the *IMS* installation, however, the customer's bill identified each item by code number, department, and price but not by name; nor were there any provisions for credit card verification or automatic boxing.

"Inputs from different 'Marketron' terminals were fed to a modern/multiplexer and then over leased wires to a communications computer controller which separates inputs from different stores. From the information supplied, the computer gave instructions to the individual checkout counters. The operation was obviously a success because it is being expanded to several more *Food Fair* stores in Los Angeles this spring as well as in *Ralph's Grocery Store* chain units. Next month it is planned to start installing the 'Marketron' system in several of the *Daitch-Shopwell* stores in New York and Connecticut."

"Seems to me the store benefits more than the customer," Barney said.

"And you're right," Mac agreed. "Joseph Davis, *IMS* vice-president, says the real advantage of the 'Marketron' system is in inventory control. The store manager can interrogate the computer at any time as to what has been sold, he can find how much cash is in each 'Marketron,' he can instantly change the price of any item, and—most important of all—the computer can be made to perform automatic ordering and restocking functions. Finally, the system practically elimi-

nates checkout operator under-rings, which is estimated to represent an average loss of .7% of sales."

"How about the over-rings?" Matilda asked. "I'd think they would cancel out the under-rings. Why is there a net loss of .7%?"

"Ned Harwell, author of *Checkstore Management*, gives cogent reasons based on actual studies. Seems the checkout girl encountering a smudged price is much more likely to give the customer the benefit of the doubt and under-ring the item rather than over-ring it. In the 'Marketron' system, the computer detects most punching errors and warns the operator by a flashing red light and an audible signal.

"IMS is not a manufacturer of computer equipment; so it does not make its own hardware or software. IBM, on the other hand, also conducted a test for four weeks in a *Safeway* store to gather some specific information they needed, and of course they used *IBM* equipment. They installed terminals at two checkout stands and code numbered a little less than 3000 items. However, since not all stands could receive unpriced items, it was necessary to have the price as well as the code number on each item. This made it impossible to observe the answer to an intriguing question: what will be the customer's reaction to items without prices on them? The *IBM* slips given the customer

had the name of the item as well as the code number and the price. At the present time they are evaluating the results of these tests."

"Sounds to me as though *IMS* has stolen the ball and run with it while the computer giants are hesitating," Barney observed. "Since there are so many advantages for store managers and since it is potentially such a huge and lucrative market for computer manufacturers, why the hanging back?"

"There are good reasons according to my brother-in-law," Mac replied. "First, such an installation represents a lot of money. No store chain wants to put huge sums into a system that may soon become obsolete. Secondly, for the system to work, there should be a universal system of code numbering. Ideally the code would be put on the label by the manufacturer; but he doesn't want to go to the expense of changing his labeling equipment, his present computer setup, his billing, his warehousing, etc., until he is sure there will be equipment to utilize it.

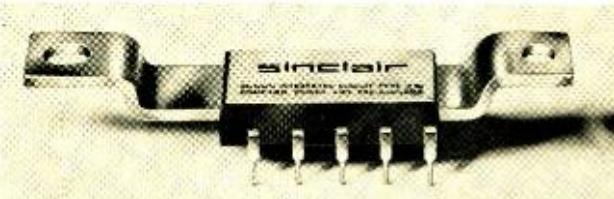
"Probably the code is the biggest bottleneck at this time. When using a punch code, the most commonly sold items are given the lowest, or two-digit numbers; the next-most-popular items are given three-digit numbers, etc. But if we go to an OCR system of number scanning, which seems inevitable in the long run, this will not be necessary. The National

Association of Food Chains, with help from others, has been working on such a code for several years but still has not decided on a code structure. When it comes, probably in the next year or two, it will likely be a seven- or eight-digit number, too long to key. Then it will likely take three to five more years for the manufacturers to produce the necessary equipment to use the code. *RCA* and *Kroeger* have been working together to produce a suitable OCR device, and it is said that *National Cash Register* and *IBM* are working hard on this same project.

"*GE* has a 'Tradar' (Transaction Data Recorder) system which is a complete package of terminals, coding and communication devices, special software programs, computers, and peripheral equipment that reads magnetically encoded merchandise tickets and verifies credit cards. The *J. C. Penney* retail chain has signed a \$10,000,000 contract with *GE* for 'Tradar' and plans to have the system in all fifty of the *Penney* outlets in Los Angeles by the end of the year.

"But progress will probably be made a little gingerly because we are dealing with that mysterious quantity, a woman shopper," Mac continued, grinning mischievously at Matilda. "No one is quite certain whether she really *wants* to be speeded through her recess from home and sometimes the kids." ▲

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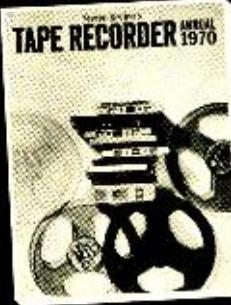
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EW-4-70

## IC Memories

(Continued from page 36)

chip sizes and decreases in cell sizes account for much of the present and predicted rises in chip capacity.

### Experimental Processes

*Bell Telephone Laboratories* is currently experimenting with a semiconductor production process that may help bipolar LSI capture the large-memory market. This process, which involves the formation of a very thin *p*-type layer on the semiconductor wafer, allows transistor bases and collectors and resistors to be diffused in one cycle, thereby obviating the need for big bathtub isolations now required around transistors. The process is reported to shrink element size approximately 60 percent and to be almost as simple as that used for MOS. The cells must operate at both low voltage and low power levels, which can be an advantage in memories, and switching speed is in the present bipolar range.

Several R&D groups are attempting to develop electrically alterable ROM's with a new version of MOS. The MOSFET gate insulation is made with layers of silicon oxide and silicon nitride.

High-potential electrons injected through the gate get trapped in the nitride, altering the switching voltage threshold for more than a year. The effect is somewhat like the oxide-programming technique now used, but the trapped charge can be erased and the transistors reprogrammed if the situation warrants it.

A more immediate use of silicon nitride in MOS IC's will probably be as a passivation coating. The nitride appears impervious to moisture and contaminants, and may permit MOS IC's to be packaged in plastic at much lower cost than hermetic packaging. The technique seems to work well for bipolar IC's, but long-term reliability tests must be completed before it can be determined that this is an acceptable substitute for sealed MOS packages. ▲

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—: "Hughes Sets New Kind of Trap to Wed MOS to Silicon Nitride," *Electronics*, April 28, 1969, pg. 39.

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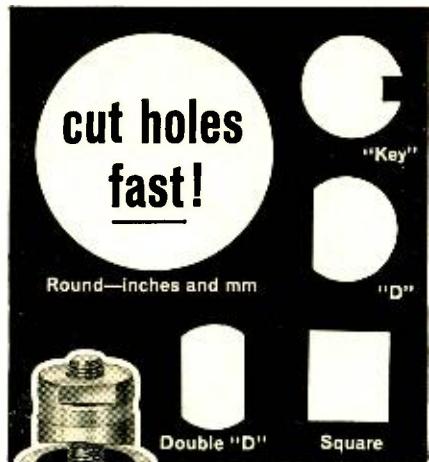
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The image shows the front cover of a catalog titled "HARD-TO-FIND TOOLS". The title is at the top in a bold, sans-serif font. Below it is a large, stylized graphic of various tools like wrenches, hammers, and saws. The catalog is bound in a dark cover with visible stitching along the right edge.

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# **Single-Signal S.W. Receiver**

By LARRY LISLE, K9KZT

**N**EED an extra short-wave receiver? —one you can leave tuned to WVV, a favorite short-wave broadcast station, or to an often-used amateur frequency? For less than five dollars you can convert an old a.c.-d.c. table radio into a crystal-controlled s.w. receiver for one frequency between 5 and 20 MHz.

The necessary modifications are extremely simple. The converter stage of a typical broadcast receiver is shown in Fig. 1A, while the same stage after conversion is shown in Fig. 1B. The set's loop antenna has been replaced by a s.w. coil,  $L_1$  (15 t. #20 plastic-covered solid hookup wire, closewound on  $\frac{3}{4}$ " insulated form), the cold end of which is connected to ground instead of to the a.v.c. line to keep the stage from being blocked by the local oscillator. A crystal, either above or below the signal frequency by the amount of the intermediate frequency (usually 455 kHz) has been substituted for the oscillator coil. (Crystals are available from *International Crystal*, 10 N. Lee, Oklahoma City, Okla. 73102. Specify "EX" type. Price \$3.95 postpaid.) The tun-

type. Price \$3.50 postpaid.) The tuning capacitor of the oscillator section is not used. A 150-pF capacitor couples the antenna to the receiver and a small choke, *RFC1*, in the screen circuit keeps the r.f. where it belongs. If reception of c.w. signals is desired, the i.f. stage may be made to oscillate by connecting a very small capacitor (1 or 2 pF) between the grid and plate of the i.f. tube.

One other modification should be made in the interest of safety. *Ground the chassis to a good earth ground, and connect only the ungrounded side of the line cord to the wall outlet.* Unless this step is taken, if the antenna-

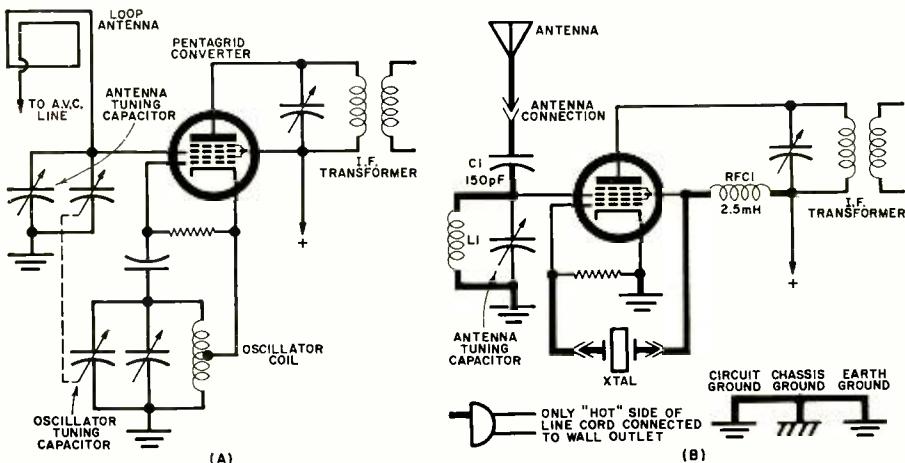
coupling capacitor should fail, the full line voltage may appear between the antenna and ground. Aside from this danger, grounding the chassis is always a good idea when modifying an a.c.-d.c. set, since it is extremely easy to bypass a safety feature installed by the manufacturer without being aware of it. This is especially important when using the set in the vicinity of other electronic equipment, whose chassis are grounded (or should be).

Construction is not critical, and parts may be placed in any available space. In the receiver modified by the author, a single-section 365-pF variable capacitor replaced the original tuning capacitor which was badly rusted. The crystal was placed on the front chassis lip, but may be placed elsewhere if desired. Instead of a conventional crystal socket, a nine-pin miniature tube socket was used, as this fit an existing hole.

After wiring has been completed and double checked, attach the chassis ground wire to a water pipe, ground stake, etc. Connect the antenna, and plug the "hot" side of the power cord into a wall socket. If the tubes fail to light, reverse the plug. When the set warms up, rotate the tuning capacitor to the point of best reception.

The i.f. transformers may be adjusted by ear for maximum output. Begin with the primary of the first transformer, and work towards the detector. Then repeat each step, proceeding from the detector back to the mixer. Once placed in operation, the receiver will require no adjustment: Sensitivity and selectivity will be roughly equivalent to that which may be expected of one of the smaller short-wave sets. ▲

Fig. 1. (A) Converter stage of a typical a.c.-d.c. broadcast-band table radio. (B) The same, except for modifications (in heavy line), for short-wave conversion.



# ELECTRONIC CROSSWORDS

By JOHN D. RICHARD

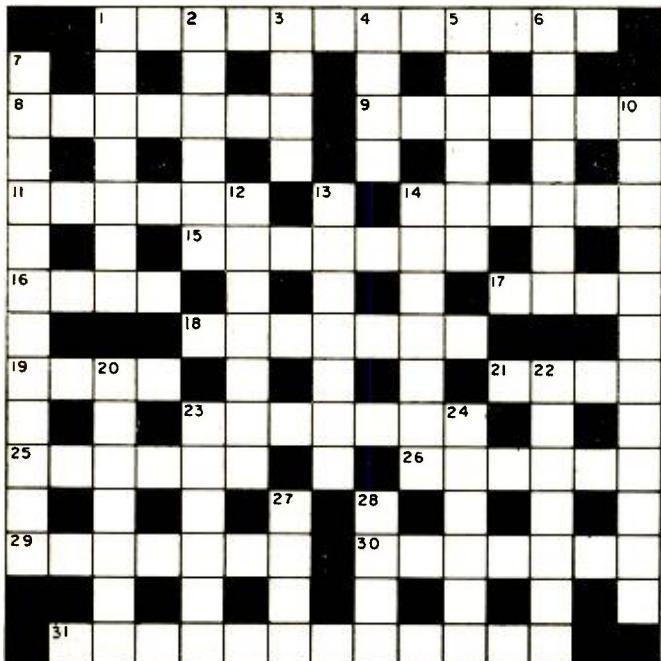
(Answer on page 92)

## ACROSS

- Useful sort of scatter for v.h.f. DX.
- Tube filaments.
- 90° from quadrature.
- Heat units.
- So nice, this base over hypotenuse arrangement!
- If the solution is acid, this reads less than 7.
- A gripping affair in the workshop.
- What you hear when reading c.w.
- This character just will not agree with computer logic.
- Colloquially, to produce coherent light.
- One is one bit, this is the other bit.
- The capacitor could be micro-this!
- Can offer piles of power.
- Similar to 4 down, yet finds a home in a thermojunction.
- An effect which provides an apt cure for similar-channel FM interference.
- Add a neutron or two to produce this.
- The frequency between first and second detectors.

## DOWN

- Signal these for radio troubleshooting.
- If coulomb = C, this is 1 C/s.
- Expel what's hidden.
- The conductors of a transmission circuit.
- Caveat this when shopping for components.
- What you must do to visualize j.
- The effect when light produces an e.m.t.
- Like the saxophone, this instrument can incorporate a vibrating reed.
- Old insulating varnish.
- Precedes electric and motors.
- Funny how the capacitor dielectric is also employed for pots!
- Could describe a languorous lateral camera scan.
- Those early wet electrolytes would occasionally do this.
- One of several that the digital voltmeter displays.
- Can result from high voltage spikes.
- Non-kinky tetrode.
- Tie.



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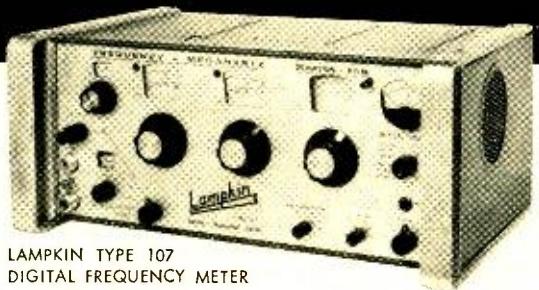
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## FEEDBACK MODULE for MOTOR CONTROL

By R. F. SCHWABENLENDER / Manager  
Information Services, Cutler-Hammer, Inc.

*Using an SCR sensing and power circuit, device monitors motor speed, changing power with load.*

DESIGNED to do for small motor appliances what the automatic transmission did for the automobile, a new electronic speed-control module performs the electrical equivalent of shifting gears. When the module detects increased strain, it automatically boosts power to the motor; if it detects lessened strain, it cuts power.

Developed by the Specialty Products Division of Cutler-Hammer, Inc., the module uses an SCR sensing and power circuit to monitor motor speed and automatically increase or decrease power proportionate to the load. This module, shown in the diagram, constitutes the smallest SCR power drive, with feedback, that is available for commercial use.

Combined with a variable resistor and an "on-off" switch, the module provides stepless motor speed control. The effectiveness of the feedback circuit is made obvious by an almost constant-speed characteristic under varying load.

The variable-speed package has applications on fractional horsepower universal motors with normal loads less than 4 amperes, which would benefit from high torque capability, such as sewing machines, food blenders, hand-held mixers, floor scrubbing and polishing equipment, etc.

Power tool manufacturers have also incorporated a trigger-switch version of the variable-speed package on electric hand drills and jig saws. Hand tools equipped with the switch have particular appeal to craftsmen needing precise speed control. The feedback package allows precise drilling at slow speeds through such objects as concrete and hard-wood.

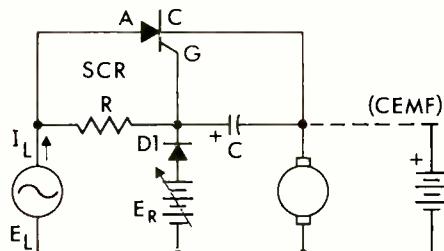
A decrease in speed due to loading of the motor results in an advanced SCR firing angle which provides more power to the motor and compensates for the increased load. A consistent firing angle (speed) at any setting or load eliminates cogging, loping, or other noise-produced speed variations.

The variable-speed module requires three leads: two power leads of 18-gauge wire and a control lead of 22-gauge wire.

The module is available for under \$3 in quantities of 10,000 or more, with package variations such as the trigger-switch version running slightly more.

The feedback module, which is an integral part of the control circuit, must be engineered to the specific characteristics of each motor's application. Delivery time is thus dependent on motor characteristics of each application and the resultant engineering requirements.

For several years Cutler-Hammer has offered a full-wave quadrac circuit without feedback. The full-wave module without feedback provides stepless, variable control in light dimmers, table lamps, slide projectors, and heating units, in addition to variable-speed control of small universal motors such as those incorporated on a centrifuge. ▲



Schematic of electronic speed-control module that monitors the motor speed and, depending on the load, automatically increases or decreases power input.

# C.E.T. Test, Section #3

## Components

By DICK GLASS\*

### What is your electronics servicing I.Q.? You must get 75% on entire exam to pass.

This is the third in a series of 12 test sections to be published monthly. While these test exam sections are not part of the actual NEA C.E.T. examinations presently being administered, they are similar in nature. Should you find you are able to correctly answer 75% or better, you might be a candidate to become a registered CET. You can take the exam in your area but you must show 4 years of experience to qualify.

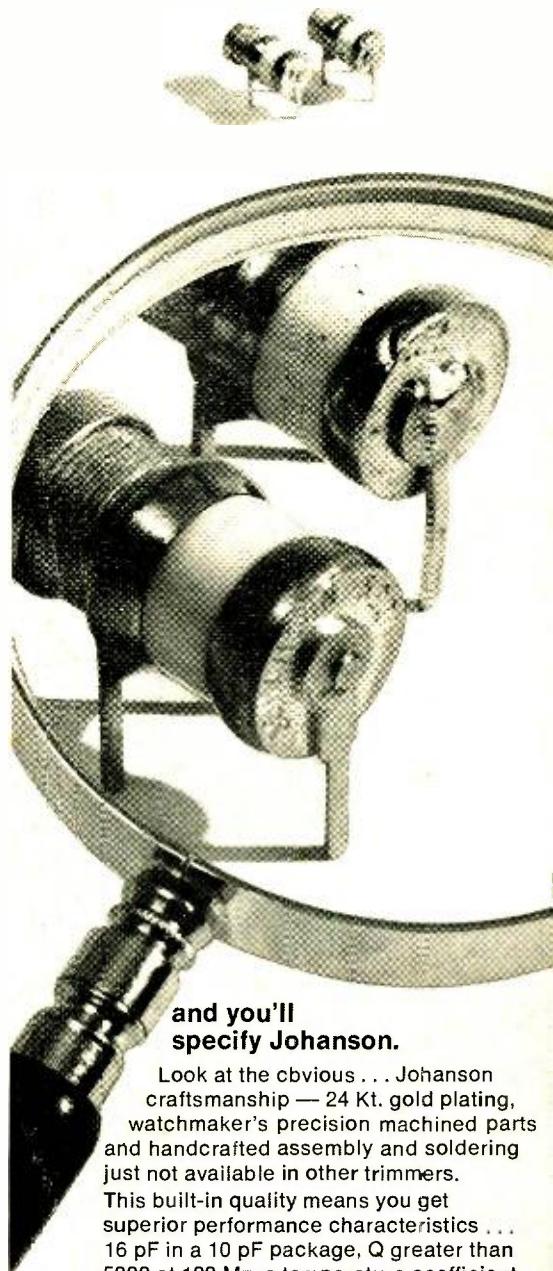
(Answers will appear next month.)

Answers to last month's quiz appear on page 92

1. A capacitor marked "P1500" will react to temperature increases by:  
(a) increasing in capacitance  
(b) decreasing in capacitance  
(c) remaining constant within a specific range of temperature  
(d) marking has nothing to do with its capacitance characteristics
2. The fourth color code band on a carbon resistor means:  
(a) 10% tolerance when gold colored  
(b) number of zeroes following significant digits  
(c) 20% tolerance when missing  
(d) 2-watt resistor when red
3. X-radiation is least likely to be produced in a color picture tube:  
(a) at the face of the tube and the shadow mask  
(b) when a neck shadow is produced by yoke placement  
(c) in the electron gun assembly  
(d) at the front and sides of the funnel assembly
4. To compensate for yoke resistance as the temperature increases, a ..... is used in series with the yoke windings  
(a) thermistor  
(b) surgistor  
(c) voltage dependent resistor (VDR)  
(d) NPO capacitor
5. Capacitor specifications are least important:  
(a) in vertical oscillator grid circuits  
(b) as screen bypasses in color bandpass amplifiers  
(c) as coupling capacitors in horizontal oscillator circuits  
(d) as oscillator trimmers in auto radios
6. To reduce hum pick-up in long audio-cable runs, you might:  
(a) change from a magnetic pick-up to a crystal  
(b) use a ceramic microphone  
(c) use a low-impedance microphone  
(d) use high-impedance audio cable
7. Integrators have time constants which allow:  
(a) high-frequency pulses to be changed to sharp spikes  
(b) low-frequency pulses to be passed through  
(c) low-frequency pulses to be filtered out of the desired signal  
(d) high-frequency pulses to be filtered out of the desired signal
8. Line transformers generally are used in multi-speaker paging systems to:  
(a) increase voice-coil losses  
(b) match impedance and increase line losses  
(c) decrease power from output transformer  
(d) simplify the installation of various speakers
9. Normally, a filter capacitor may not be replaced by another with:  
(a) less than 90% of the rated capacitance value  
(b) less than 80% of the rated capacitance value  
(c) more than 60% over the rated capacitance value  
(d) more than 50% over the rated capacitance value
10. Capacitors often used because of their thermal stability are:  
(a) silver mica capacitors  
(b) ceramic disc capacitors  
(c) tubular  
(d) hi K

\*Executive V.P., NEA, 12 South New Jersey St., Indianapolis, Ind. 46204,  
assisted by Lew Edwards, chairman of Test Make-up Subcomm.

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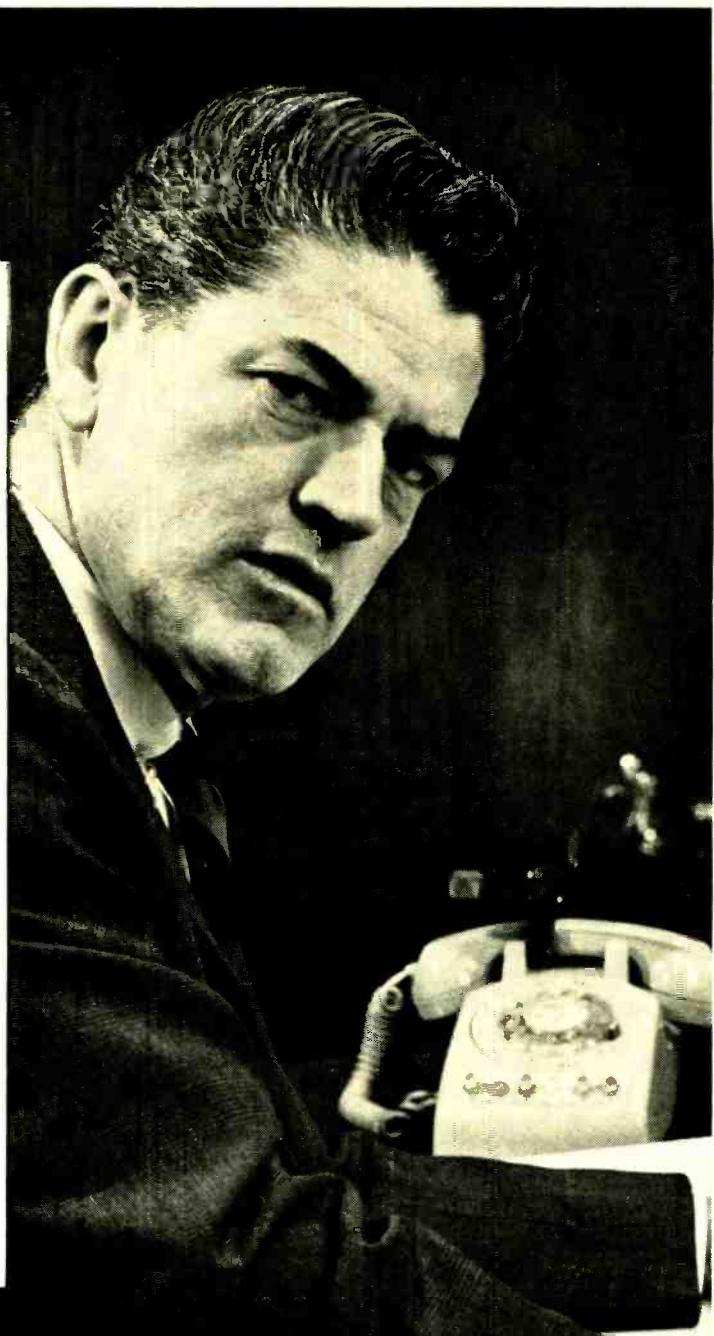
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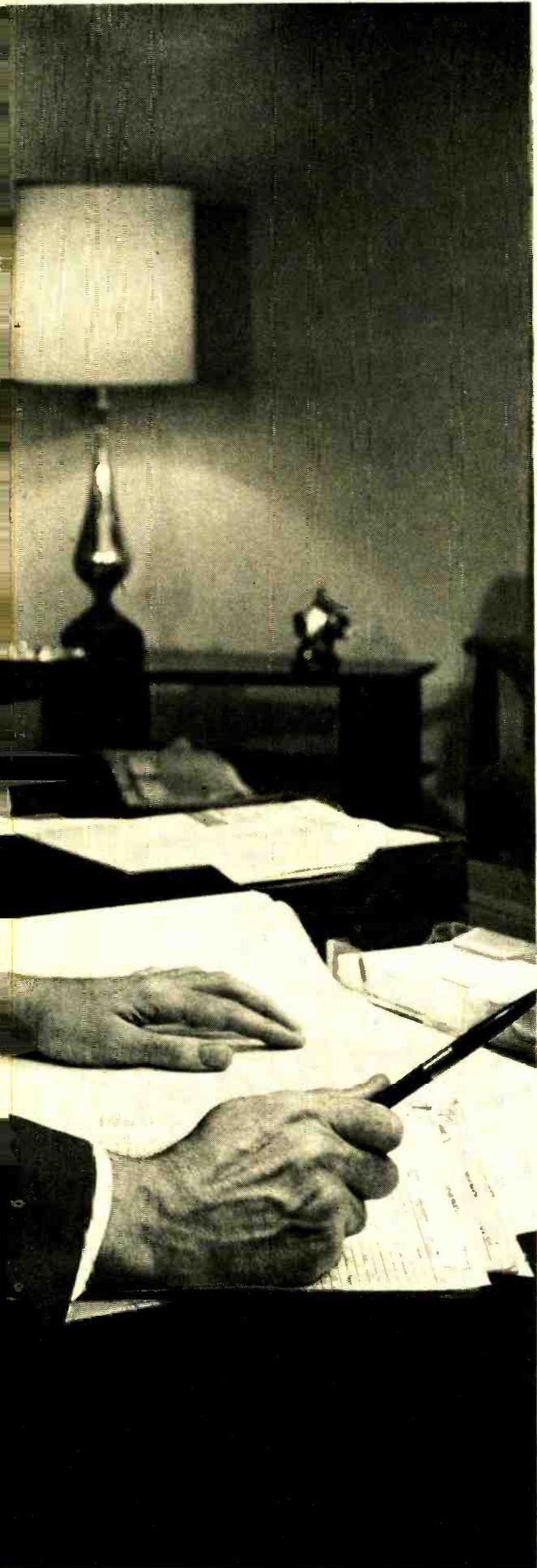
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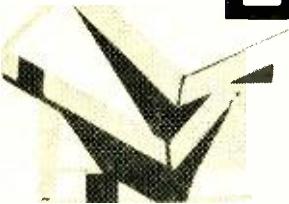
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# BOOKS



"WRITING FOR TECHNICAL AND BUSINESS MAGAZINES" by Robert H. Dodds. Published by John Wiley & Sons, Inc., New York. 188 pages. Price \$7.95.

This book is for that army of engineers and the technically knowledgeable who want to share their expertise with their fellow engineers and/or enlightened laymen.

The author presents a number of cogent arguments for the engineering writer: because it is part of his work, because he "owes" his profession information on new developments, because it brings recognition to the author, and because recognition is essential to professional success.

A number of information-packed chapters are devoted to the bread-and-butter techniques of writing and marketing articles for the technical press. The appendices include a style guide, copyreading symbols, and a listing of technical and business publications that accept contributed articles, along with their addresses.

\* \* \*

"1-2-3-4 SERVICING AUTOMOBILE STEREO" by Forest H. Belt & Associates. Published by Howard W. Sams & Co., Inc., Indianapolis. 189 pages. Price \$3.95. Soft cover.

The booming market for in-car stereo equipment has opened up a new field for service technicians and provided plenty of headaches for those who don't know how to handle such servicing. By the very nature of the "beast" auto stereo equipment usually requires more frequent and better servicing than in-home systems. Vibration, dust, dirt, and moisture all take their toll and the author suggests a program of preventive maintenance to keep all such equipment in top-notch condition.

The first chapter explains the author's plan of "1-2-3-4 Servicing" which is applicable to all electronic equipment once mastered. This technique consists of diagnosing, locating the faulty stage, isolating the trouble to a small portion of the instrument, and pinpointing the fault to a specific part. The second chapter shows how this same procedure can be applied to mechanical equipment such as record changers. The next five chapters cover the specific auto stereo equipment while the final four chapters explain how the "1-2-3-4" system is applied to this specific problem.

The text is concise, well-illustrated, and written in an informal but no-nonsense format.

\* \* \*

"ELECTRONIC CIRCUITS FOR THE BEHAVIORAL AND BIOMEDICAL SCIENCES" by Mitchell H. Zucker. Published by W. H. Freeman and Company, 660 Market St., San Francisco, Calif. 94104. 235 pages. Price \$9.75.

Although this is a book for a rather specialized audience of researchers who must work with or devise electronic equipment for use in their studies, many of the circuits covered are adaptable to non-research applications.

Since the author is an electronics technician at the University of California's Department of Psychology, he is familiar with the problems faced by researchers and is well aware of their deficiencies when it comes to working with and understanding electronic equipment. The circuits he describes have all been tested and are foolproof. He further assists his colleagues by providing complete parts lists with sources.

The book opens with three basic chapters dealing with semiconductor operation, understanding circuit diagrams,

and construction techniques. The balance of the book is concerned with troubleshooting, power-supply circuits, sensing and control circuits, programming and time-delay circuits, and audio circuits.

\* \* \*

**"INSTALLING & SERVICING HOME AUDIO SYSTEMS"** by Jack Hobbs. Published by *Tab Books*, Blue Ridge Summit, Pa. 17214. 250 pages. Price \$7.95 hard cover, \$4.95 paperbound.

This book is for practicing or potential service technicians who are interested in getting a slice of the burgeoning audio market. The author is convinced that there is "gold in them thar decibels" and technicians are making a mistake in not mining this lode.

After the persuasive chapter on why the technician should take up audio service work and the equipment he will need to do a professional job, the author deals with AM receiver maintenance, FM tuners, servicing stereo-FM equipment, preamps and amps, combination units, solid-state power supplies, tape recorders and players, mobile radios and tape players, automatic record changers, how to sell and install audio systems, commercial audio work, and home and business intercom installations.

Since the book's audience is assumed to be professional, the author does not deal in basics but in how to work effectively with his present technical skills and in improving his work habits. To this end, the book is filled with professional hints and shortcuts, schematics, photographs of servicing procedures, typical equipment of various types, and waveforms.

\* \* \*

**"101 QUESTIONS & ANSWERS ABOUT HI-FI & STEREO"** by Leo G. Sands and Fred Shunaman. Published by *Howard W. Sams & Co., Inc.*, Indianapolis, Ind. 124 pages. Price \$3.50 soft cover.

This book is designed for anyone interested in hi-fi sound reproduction—beginner or advanced audiophile as well as audio service technician. The format is one of questions and answers but the material has been divided into six parts so that the reader doesn't need to go through all 101 Q&A's to find the material he needs.

The first section deals with hi-fi systems, next comes the part on amplifiers, then tuners, record and tape players, speakers, and finally troubleshooting and maintenance. Each part has an index listing the questions and answers covered in that section.

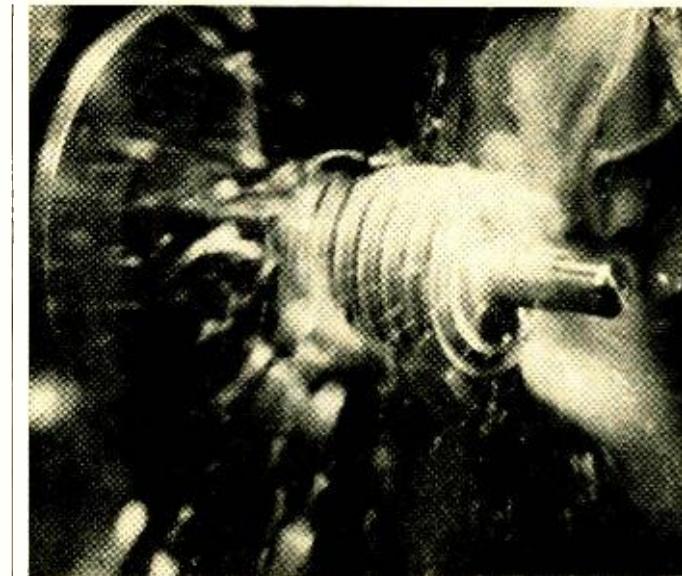
The text is lavishly illustrated and easy to read. The only reservation is that, as so often happens when experts discuss their specialty, the material swings wildly from over-simplification to discussions of circuits and standards without any explanation (*viz.*, no explanation of Hz, references to phase inverters, push-pull output tubes, modified class-A, decoupled stages, feedback-type controls, etc.). Thus, if you are not quite the "beginner" that the authors envision, you should have no trouble understanding the material.

\* \* \*

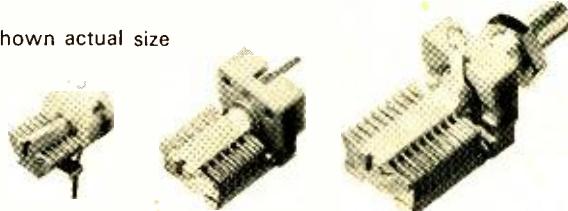
**"ELECTRONIC CIRCUITS"** by J. Richard Johnson. Published by *Holt, Rinehart and Winston, Inc.*, New York. Two volumes, \$9.95 each hardbound, \$6.50 each paperbound.

These two volumes, designed for technical institute and junior college courses, cover direct current (Vol. 1) and alternating current (Vol. 2).

The author, who is with *Bell Telephone Laboratories*, offers a carefully developed presentation for those embarking on a career in electronic technology. The student should have a working knowledge of algebra and trigonometry but other than that requirement, these volumes are complete and the student can develop his skills as he goes along. The inclusion of a number of worked out problems as well as hundreds of exercises for the student enables the instructor to check on the student's comprehension before going on to the next topic.



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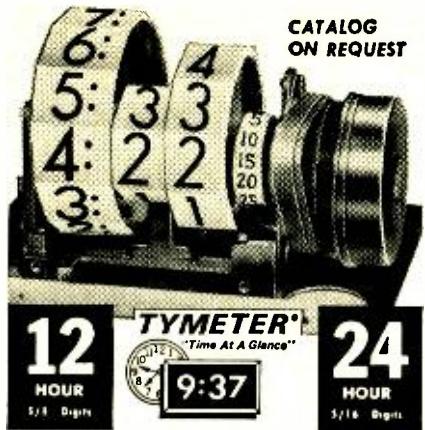
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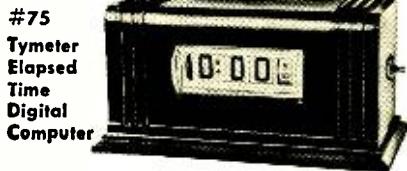


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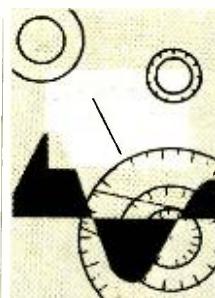
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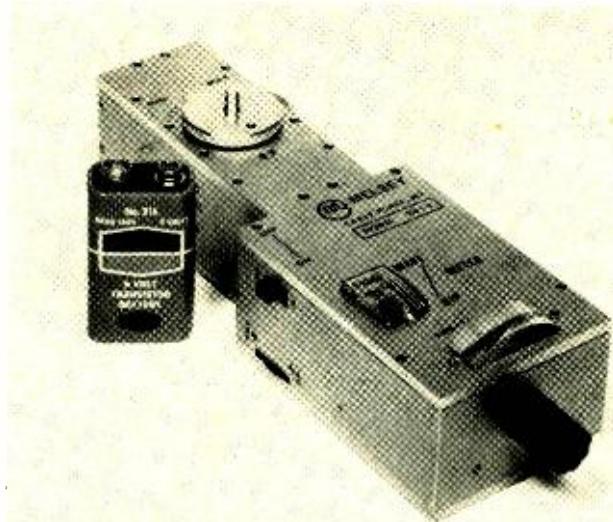


# TEST EQUIPMENT

## Product Report

### Melsey SN-2 Wave/Dip Meter

For copy of manufacturer's brochure, circle No. 3 on Reader Service Card.



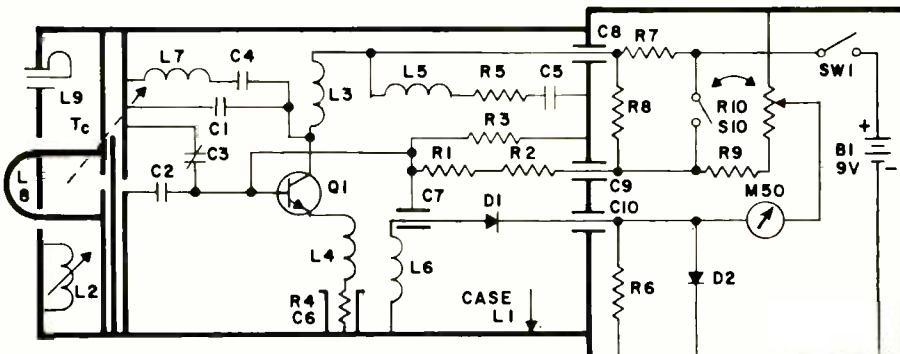
If you talk to just about any knowledgeable ham about a grid-dip meter, he should be able to give you at least a half dozen uses for this versatile, compact piece of test equipment. These include finding the resonant frequency of tuned circuits, acting as a signal generator or field-strength meter, measuring  $L$ ,  $C$ , and  $Q$ . The Melsey SN-2 is a transistor version of the grid-dipper but operating at the u.h.f. frequency range of 400 to 1150 MHz. This 6-in, 10½-oz unit provides continuous tuning and is directly calibrated to better than 1 percent by use of a 30-in steel tape on which the frequency is marked.

Power for the instrument is obtained from a single 9-V transistor-radio battery. Current drain is only 1 mA when the unit is used as a wavemeter, and 2.5 mA when used as an oscillator.

The oscillator circuit (see diagram)

is a modified Colpitts in a cavity configuration. Tuning is by means of a patented variable capacitor ( $T_C$ ), consisting of a precision glass tube with silver-plated brass bands around the outside. A copper-plated Invar slug traveling within the tube forms a glass-piston variable tuning capacitor with the outer bands. There are no wiping contacts and the piston moves smoothly through the tube without rotating. A second glass capacitor assembly ( $C_1$  and  $C_2$ ), fitted over the variable tuning capacitor, forms the transistor base and collector coupling capacitors.

The entire capacitor assembly is mounted within the forward section of a double compartment case and contact with the front and rear walls of the section completes the cavity structure ( $L_1$ ). The rear compartment shields



the retractable tuning slug and accommodates the isolation feedthrough capacitors (C8, C9, and C10).

The oscillator output is inductively coupled by means of L4 and L6 through a pair of crystal diodes to the indicating meter. With the oscillator operating and with external coil L8 brought close to a resonant circuit, the current will dip sharply as the wave/dip meter is tuned through the same frequency as the resonant circuit. The exact frequency can then be read directly from the calibrated dial of the instrument. With the oscillator turned off, the unit is used as a wavemeter or

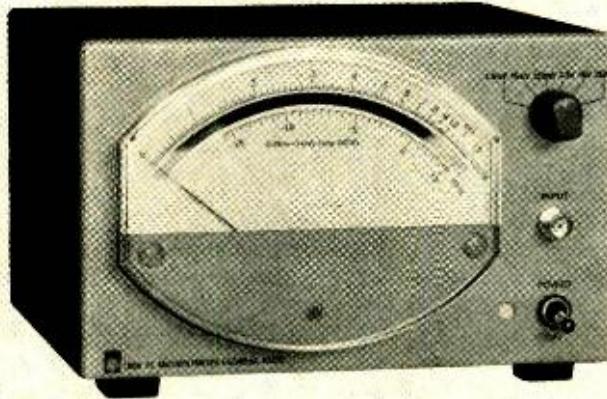
field-strength meter. Now the meter peaks to a maximum value when the instrument is tuned to the same frequency as the external circuit. Note that when used as a dipper, power need not be applied to the circuit under test, but when the instrument is used as a wavemeter, the external circuit must be powered.

A miniature coax receptacle is also provided for direct connection to a 50-ohm cable. The connector assembly can be rotated to provide at least 30 dB variable attenuation.

Price of the *Melscy Model SN-2* wave/dip meter is \$185. ▲

### General Radio Type 1808 A.C. Voltmeter

For copy of manufacturer's brochure, circle No. 4 on Reader Service Card.



**A**n a.c. voltmeter is a general-purpose instrument that is sensitive enough to measure a.c. signals in the millivolt range. Such an instrument is widely used to take audio measurements or measurements in the ultrasonic and low r.f. ranges. It is also used for attenuator testing and for calibrating various types of transducers.

The new *General Radio Type 1808* is a laboratory or production-line instrument of this type. It is a sensitive, average-reading voltmeter calibrated to read r.m.s. values of a sine wave. The most sensitive of the meter's six ranges reads up to 1.5 mV full-scale, while the highest range is 150 volts. A separate attenuator probe is available to extend this to 1500 volts. The dynamic range is high, 20 dB per range, permitting a single scale to be used for all readings. The usual dB scale is also provided on the meter. Frequencies can be measured over the extremely wide range of from 10 Hz up to 10 MHz and the meter accuracy is  $\pm 1$  percent of reading over most of this range.

An FET input buffer provides the high 10-megohm input impedance and frequency-compensated resistive dividers add to the uniform frequency response. The diodes that are used to convert a.c. signals to d.c. values that can be read on the meter are inside the feedback loop of the amplifier used. This prevents any diode nonlinearity from affecting meter reading. The amplifier provides high open-loop gain even at the top frequency of 10 MHz.

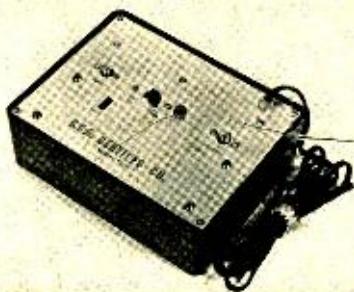
Compared to a service-type a.c. voltmeter, this instrument is expensive. The Type 1808 sells for \$295 while a service-type meter might cost around \$90. However, the less expensive instrument is not as accurate (it may be 2 to 3 percent of full-scale rather than 1 percent of the actual reading); not as sensitive (the lowest range might be 10 mV rather than 1.5 mV); not as wide in frequency coverage (it may go up to 1 or 1.5 MHz rather than 10 MHz); and it may not be as stable. Hence, when the need exists for this better performance, a higher price must be paid. ▲

### Eico Model 465 Oscilloscope

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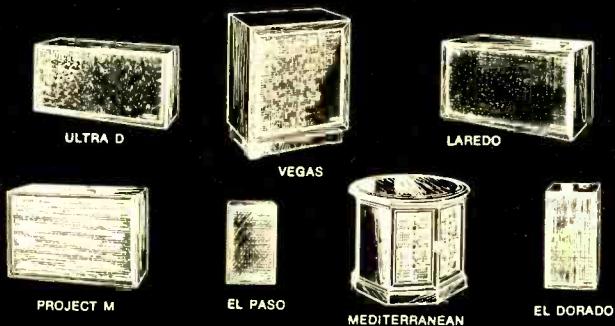


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el 427 is a more sensitive 5-incher with a response from d.c. to 500 kHz, priced at \$99.95 as a kit or \$139.95 factory-wired. The Model 460 is a 5-incher that is only slightly less sensitive but with a wider frequency band (d.c. to 4.5 MHz), priced at \$99.95 in kit form or \$149.95 factory-wired. The top of the *Eico* scope line and the subject of our report this month is the Model 465, which the company refers to as its professional oscilloscope. More expensive than the other scopes in the line (\$179.95 as a kit, \$249.95 factory-wired), this model offers more features and better performance.

The new Model 465 has a vertical-amplifier response from d.c. to 8 MHz, which is more than adequate for color-TV service. The horizontal-amplifier response is from d.c. to 1 MHz. Both amplifiers are push-pull and direct-coupled throughout, permitting true voltage measurements and observations of just about any waveform. The scope can also be used as a vectorscope for color-TV work. A pair of zener-controlled voltage reference sources provide an accurate source of calibration voltages for both the vertical and horizontal channels. Vertical sensitivity is 12 mV (r.m.s.)/cm; horizontal sensitivity is nearly as great at 17 mV (r.m.s.)/cm. Four-step calibrated and frequency-compensated input attenuators are provided for both channels.

The scope has automatic sync with a sync limiter and amplifier to provide rock-steady waveforms over the entire sweep range. A flat-face CRT is used with a Mumetal neck shield to minimize the effects of external magnetic fields.

One problem that comes up in the design of any high-gain scope such as this one is the presence of residual hum, especially in the low-level vertical-input stage. If this stage uses a tube with only a very slight amount of heater-cathode leakage, the hum voltage will be amplified along with the signal to be observed. As a result, the horizontal portions of the waveforms will be thicker

than they should be, making accurate study of the waveform difficult. To prevent this, the low-level tubes must be carefully selected or hum-balancing circuitry must be used.

We used one of the early Eico 465's, and we discovered this very problem. By merely substituting another pair of 6AUS input tubes, the residual hum was cut way down and the waveforms seen on the screen were extremely sharp. The company has been selecting these tubes carefully so that this problem should not occur in subsequent models of the scope.

The two removable side panels, each held with only four screws, make it simple to perform internal adjustments or do any servicing that may be required. One side panel exposes all the tubes and adjustments while the other side panel exposes all the below-chassis point-to-point wiring.

After using the new Eico Model 465 for a while, we can say that it is certainly a worthy addition to the company's line of scopes.

#### "SWITCHLESS" DUAL-RANGE VU METER

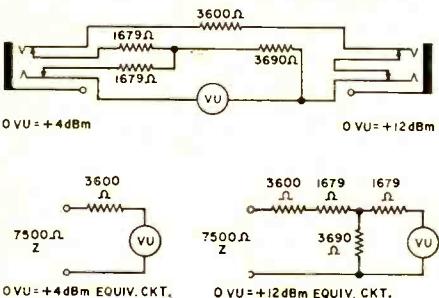
By WINSTON THARP

**A**Ssume that you have to provide an option of a vu meter or a vu meter through an 8-dB pad for monitoring 600-ohm balanced audio lines in a patch panel.

How do you handle it? The existing patch panel used shorting type "stereo headphone" jacks rather than the more common (and expensive) double phone jacks. The vu meter was to be used with a series 3600-ohm resistor so that 0 vu was indicated for a line level of +4 dBm. This meant that the 8-dB pad had to be switched in and out on the meter side of the 3600-ohm resistor and had to exhibit 3900 ohms impedance in and out in order to maintain a constant load on the 600-ohm lines to be monitored. Switching the pad in and out would be simple if it were on the other side of the 3600-ohm resistor, but this would upset the bridging impedance of the vu meter circuit.

The secret is to take advantage of the non-polarized nature of the vu meter. To see how it is done, refer to the diagram below.

Method of hooking up the non-polarized vu meter so that it indicates two ranges depending on where the plug is inserted.



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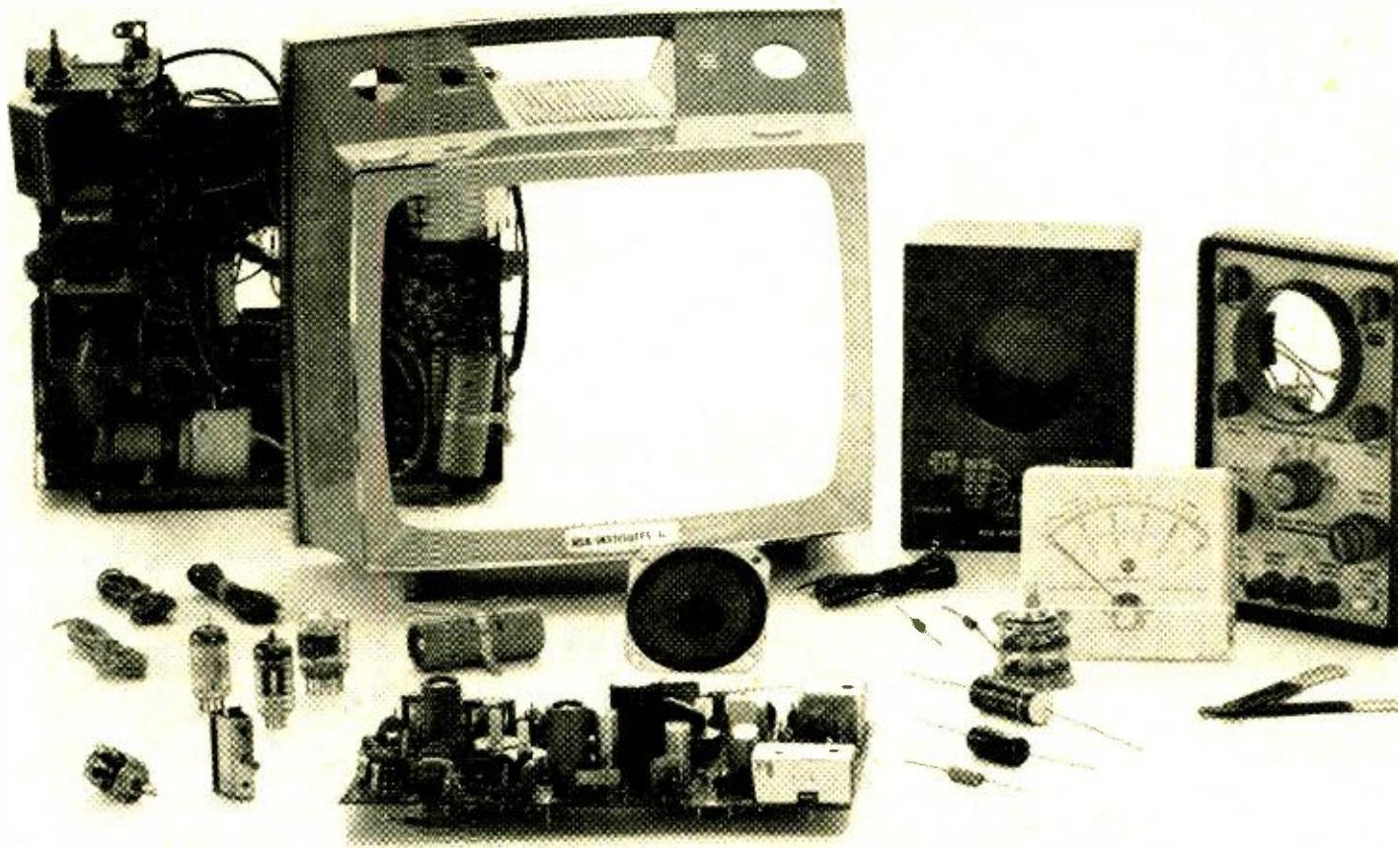
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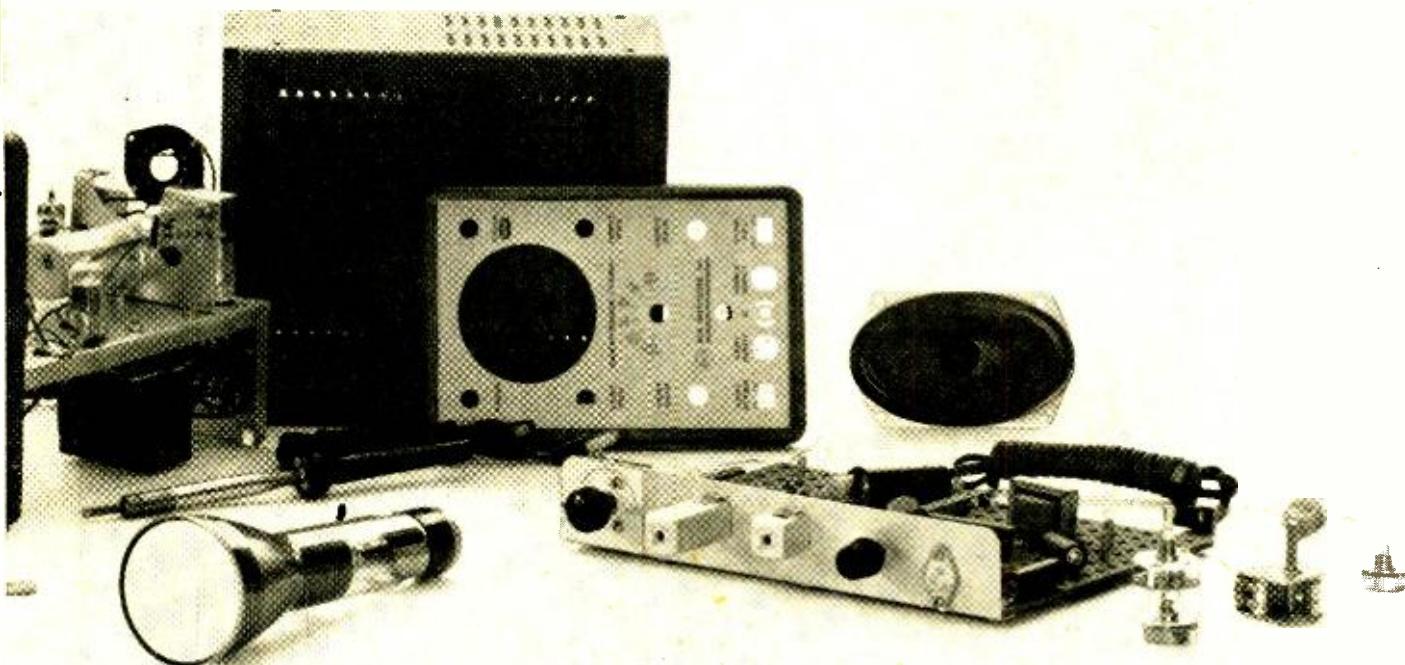
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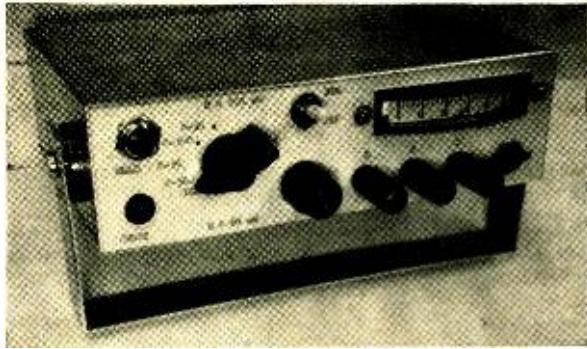


Fig. 1. Low-cost, multirange transistor checker.

# Multirange Transistor Checker

By J. E. ORME

*Inexpensive, portable tester measures beta on two ranges at two different collector power levels. Also checks for opens, shorts, and leakage of transistors and diodes.*

SOME commercially available transistor checkers are found to be somewhat inaccurate and limited in versatility; usually they give only an indication of quality, i.e., a "yes-no" answer as to whether the transistor is operative or not. Thus, these models are unsuitable for matching transistors or for precise measurements of *beta* under varying conditions of base current or collector power. Furthermore, many commercial units are a.c.-line operated which leads to problems when servicing units in the field. One would think that battery-operated devices should be checked with testers which are also battery operated, thus leading to a greater degree of portability. Last, but not least, commercial units are expensive, starting at about \$100 while the unit described here is capable of measuring more variables than the average tester and can be built for about \$20 or less, depending on what spare parts the technician may have available.

## Description

The multirange transistor checker (Fig. 1) can measure *beta* on two ranges, 0-50 and 0-500, at two different collector power levels, making a total of four *beta* ranges in all. It also tests diodes, measures transistor leakage currents, and indicates short- and open-circuit conditions. The schematic diagram of the unit is shown in Fig. 2.

The circuit is essentially a constant-current base drive to a common-emitter transistor circuit. The collector current is measured by a 0-50 microammeter (*M1*) that is calibrated directly in terms of *beta* (0-50) and microamperes (0-50). The higher *beta* range (0-500) is obtained by shifting the decimal point in the 0-50 range reading. A 2-pole, 5-position wafer switch (*S1*) selects the proper base current and meter shunt resistors simultaneously. A 4-pole, double-throw toggle switch (*S2*) selects the correct transistor polarity "NPN/PNP" by reversing both battery and meter connections. A push-to-make "Read" switch (*S3*) is the test switch. Some of the component values, such as shunt resistors *R4* and *R5*, may have to be changed to match the resistance of the meter used. A 1600-ohm meter (.50  $\mu$ A) was used in this case.

Because the transistor checker is used intermittently in most testing applications, only four 1½-volt "C" or "D" cells are required to power the unit. The midpoint between the four cells is used for the base drive circuit. No "on-off" switch is required since the "Read" switch (*S3*) is spring loaded and is in series with the battery supply. No current can be drawn unless a transistor or diode is connected to the test terminals or plugged into socket *SO1*. When the

transistor is in place, base current will be drawn continuously, while collector current will flow only when the "Read" button is pressed. Transistors can be left connected when the switch is in the " $I_{CEO}$ " position, as no base current can be drawn under this condition.

## Measuring Beta

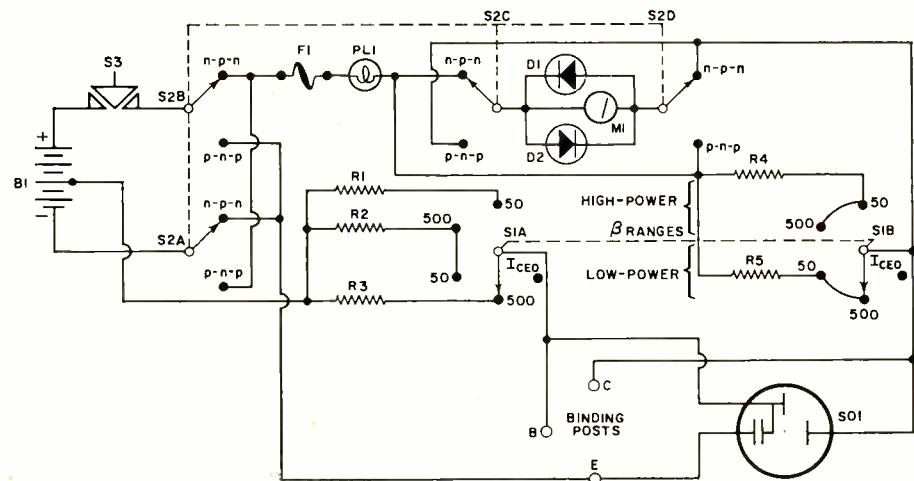
The parameter *beta* ( $\beta$ ) is, of course, the current gain or amplification, considered with the base terminal as the input and the collector as the output. This configuration, the common-emitter circuit, is the most commonly used one in present-day circuits. This transistor checker measures d.c. *beta*, i.e., the ratio of d.c.-output to d.c.-input current, whereas some instruments measure the a.c. or dynamic *beta*, using an alternating-current signal for this purpose.

Strictly speaking, *beta* is defined as  $\left| \frac{I_C}{I_B} \right|$  where  $I_C$  = collector current and  $I_B$  = base current.

When using the multirange transistor checker to measure  $\beta$ , the results change very little if the collector voltage, depending on the transistor, is allowed to vary from test to test. This is because transistor characteristics, analogous to those of a pentode, are independent of collector voltage as long as the operating point is maintained in the "plateau" region. What is considered more critical is the constancy of the base drive current which is obtained in this circuit by a "constant-current generator" approach with  $I_B = (V_{BB} - V_{BE})/R_B$  where  $V_{BB}$  = base supply battery voltage,  $V_{BE}$  = base-emitter junction voltage drop,  $R_B$  = base current-limiting resistor, and  $I_B$  = base current.

Fig. 2. Schematic and parts list of transistor checker discussed in article.

R1—1300 ohm tes.	S3—S.p.s.t. normally open push-button switch
R2—13,000 ohm res.	PL1—2.2 V lamp with holder
R3—130,000 ohm res.	F1—1/4-A pigtail fuse
R4—0.8 ohm res.	M1—0-50 microamp meter
R5—8.0 ohm res.	SO1—Transistor socket
S1—D.p. 5-pos. rotary wafer switch	B1—Four 1½ V "C" cells in series
S2—4-pole, d.r. toggle switch	D1, D2—Low-power silicon diode (1N4001)



Thus  $I_B$  is constant (0.02 mA to 2.0 mA in four ranges), as long as  $V_{BB}$  and  $V_{BE}$  are constant. Depending on the transistor being checked, small variations of  $V_{BE}$  ( $\pm 0.1$  V) might result in a 5 percent error in beta. With a constant-current base drive, it is only necessary to calibrate the microammeter on the collector output directly in terms of beta. Different values of  $R_B$  are selected by switch S1 to change the  $\beta$  range, which also causes the meter shunt resistors to change (Fig. 2).

To obtain a measurement that indicates how beta varies with base drive, it is only necessary to switch between the high- and low-beta ranges (within the same power level setting). The beta will be read for two base currents, 0.02 and 0.2 milliamperes. The constancy of the base current is assured by driving the base from a high-impedance source (constant-current drive), as previously mentioned. However, the voltage source for the base drive circuit is kept at 3 volts to ensure that the  $BV_{BE}$  (emitter-base reverse breakdown voltage) is not exceeded in case of accidental reverse connection. In many common transistors, the  $BV_{BE}$  is surprisingly low; approximately 6 volts.

To measure beta variation with temperature, it is only necessary to place the transistor, with extension leads, in an oven with a thermometer. The foregoing tests can then be carried out at different temperatures, and an accurate plot of the transistor behavior with changing temperature obtained. In addition, with this transistor checker, the collector current-voltage characteristic can be plotted by altering the collector battery voltage. For this purpose, an external variable voltage series supply can be inserted at the binding posts.

As mentioned previously, beta can be measured at two power levels. The low-power range is 60 milliwatts maximum, proportional to meter reading and the maximum power level on the high setting is 600 milliwatts. Small-signal transistors can be measured at the 60-milliwatt level while the

600-milliwatt level corresponds roughly to the dissipation of power transistors without a heatsink attached. These two power levels are obtained by driving the base at different currents to get 10 milliamperes collector current for the low power beta ranges, and 100 milliamperes maximum for the high power range. With a 6-volt battery, the 60-milliwatt and 600-milliwatt levels are obtained, as:  $Collector\ Power\ Dissipation = V_C \times I_C$ .

Diodes can be tested by connecting them between the emitter-to-collector terminals of the tester; the meter will then read 0-100 milliamperes maximum in the forward-bias direction. The polarity across the diode can be reversed by operating the "NPN/PNP" switch (S2), allowing the reverse leakage to be checked on the 0-50 microampere " $I_{CEO}$ " range of the tester.

Short circuits are indicated when "Short" lamp (PL1) glows and extreme meter overload is prevented by the inclusion of diode, lamp, and fuse protection in the meter circuit.

A test of  $I_{CEO}$  (collector leakage with base open) is provided on the 0-50 microampere meter range.

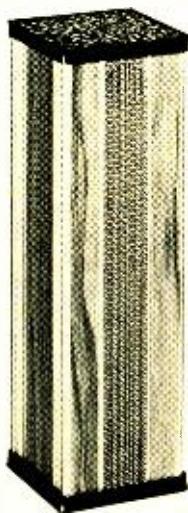
### Operating Procedures

When operating the multirange transistor checker follow these procedures:

1. Plug in transistor and choose the correct polarity by placing the "NPN/PNP" switch in the appropriate position, as given by the maximum beta reading.
2. Check transistor for shorts on the low-power, high-beta range. Shorts show as infinite beta or the "Short" lamp (PL1) glowing. Open circuits show beta equal to zero.
3. Measure beta on the four beta ranges as required; use the low-power range first.
4. Check  $I_{CEO}$  only if no shorts are evident. Read  $I_{CEO}$  (leakage current) on the 0-50 microampere scale.
5. Disconnect transistor after testing.



## TWO NEW BELL RINGERS FROM DELTA

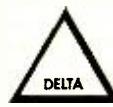


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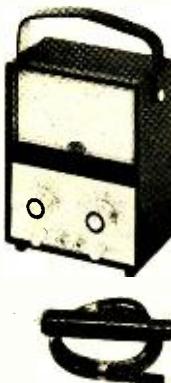
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# NEW PRODUCTS & LITERATURE

COMPONENTS • TOOLS • TEST EQUIPMENT • HI-FI • AUDIO • CB • COMMUNICATIONS

## MODULAR STEREO SYSTEMS

A new line of audio components which provides capability to custom-tailor two-, three-, or four-channel stereo systems has been introduced in both kit and factory-wired versions.

The first units in the new line are the HL-100 preamplifier and control unit and the HL-210



power amplifier and speaker-switching panel. The units feature solid-state circuitry throughout, IC's and transistors combined for optimum performance. These modules can be combined into a complete four-channel system using the HL-110 (two preamps) and HL-120 (two control units) connected to a four-channel volume level indicator (HL-330 or HL-340) for on-line monitored input. Four-channel power amplifiers may be used alone, in combination with speaker selectors, remote location controls, or with bi-amplification provided by the variable crossover dividing networks. Hegeman Labs

**Circle No. 6 on Reader Service Card**

## H. V. METER KIT FOR COLOR TV

The safe, accurate, and continuous monitoring of picture-tube anode voltage of all color-TV chassis under test is now possible with the new 10J110 meter kit.

Designed to enable service technicians to adjust precisely the high-voltage output to manufacturers' specifications, the new unit helps avoid excessive voltage and possible abnormal x-radiation.

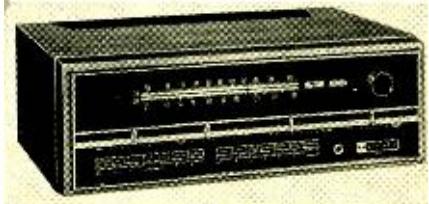
The kit has been designed for quick and easy installation into any of the company's color test jigs—10J102, 103, 104, 105, and the 11A1015A. It can also be adapted for universal mounting in any other test jig. The kit consists of a 3½-inch rectangular 50-μA meter with a dial scale calibrated for a range of 0 to 35 kV d.c. with 70 scale divisions, a meter multiplier and cable assembly, a meter ground lead, and meter mounting hardware and instructions for installation in color test jigs. RCA Parts and Accessories

**Circle No. 7 on Reader Service Card**

## AM/STEREO-FM RECEIVER KIT

A deluxe medium-power AM/stereo-FM receiver has been put on the market as the AR-19. The kit incorporates new circuitry ideas and a power output considered to be ideal for most home stereo systems.

The receiver incorporates five IC's with a total of 57 transistors and 35 diodes. Frequency response is 6-35,000 Hz with less than 0.25% har-



monic and IM distortion at any power level, according to the company.

Eight circuit boards which snap in and out in seconds make the AR-19 easier to build. It also has built-in test circuitry (probes and meters) to enable the builder to check each circuit part without the need for external test equipment.

The factory assembled and aligned FM tuner has a 2-μV sensitivity. For AM the set has a built-in antenna that swivels in two planes for better signal reception.

Further information on this new receiver will be supplied on request. Heath

**Circle No. 8 on Reader Service Card**

## TREASURE/METAL LOCATOR

The Model KG-366 treasure/metal-locator kit can be assembled even by beginners.

The unit is sensitive enough to detect an object as small as a half-dollar six inches under ground. When the search coil approaches metallic objects, a clear audible indication is heard through the unit's built-in speaker. This eliminates the need to watch a meter and makes easy nighttime use possible. It is also possible to distinguish between ferrous and non-ferrous metals by the pitch of the signal.

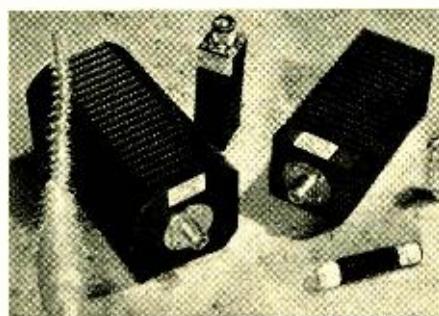
The locator has a dynamically balanced, telescoping 36" tubular aluminum handle and a waterproof 6½"-diameter hermetically sealed search coil. The unit operates from a single 9-volt battery. Allied Radio

**Circle No. 9 on Reader Service Card**

## R.F. LOAD RESISTORS

The new Models 8166 and 8164 "Termaline" r.f. load resistors are the latest additions to a family of dry air-cooled line terminations designed for use in any position.

With the announcement of the new 150 and



100-watt units, Bird Electronic Corporation now has two 10-watt units with integral male or female N connectors, and basic 25, 100, and 150-watt units with a choice of 17 common coaxial connectors each. This QC "Quick-Change" connector feature provides unique flexibility at the time of order or in the field and eliminates performance-degrading adapters.

For complete specifications on the new units as well as the other models in the line, write to H. H. Heller, Senior Staff Engineer, at 330303 Aurora Road, Cleveland (Solon), Ohio 44139.

## REPLACEMENT RECTIFIERS

Universal 2.5- and 3.5-amp silicon rectifiers, capable of replacing all diodes having voltage characteristics up to 100 volts, are now available. These new units permit the service technician to carry two rectifiers instead of stocking hundreds of replacement types. The 2.5-amp subminiature rectifier (R250F) has a 50-amp maximum surge

while the 3.5-amp unit (R350F) has a 70-amp maximum surge.

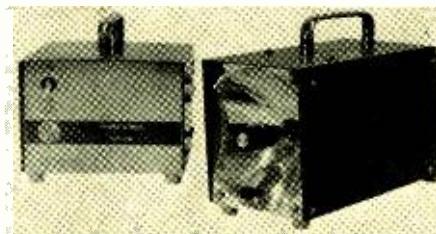
The 2.5-amp rectifier is suitable for TV, radio, and communications applications and replaces HEP157 through HEP170, GE504A, GE509, IN2069/A, IN2070/A, and IN2071/A, among others. The 3.5-amp unit is suitable for higher power circuits in original and replacement applications as well as for industrial circuits requiring ratings up to 1000 volts p.i.v. International Rectifier

**Circle No. 10 on Reader Service Card**

## ULTRA-HIGH-SPEED STROBE

For high-speed motion analysis and optical experimentation, a new full-capability stroboscope with a continuous repetition rate of 600,000 flashes per minute has been introduced.

The instrument features vernier frequency



control, ultra-short-duration light pulses, and ultra-high stability for precise synchronization and examination of subjects without spread, blur, or confusion of the image for motion analysis, according to the company.

The virtual point-light source, 0.20-microsecond light-pulse duration, and high repetition rate allow adaptation to many optical applications, including ranging and visual communications. U.S. Scientific Instruments

**Circle No. 11 on Reader Service Card**

## FIRE AND INTRUDER ALARM

The "Alert DC-6" is a low-cost fire and burglar alarm system for home or office use. The system consists of a special hair-thin wire, contact switches for doors and windows, and mounting pins.

The system is key-locked so only the key holder can turn off the alarm. An electronic delay timer permits the owner to leave the protected property and close the door before the alarm system is activated. The latched circuit allows the alarm to operate even if the protected door or window is closed after entry. MRL, Inc.

**Circle No. 12 on Reader Service Card**

## MARINE RADIOTELEPHONE

The Model MWW-18 radiophone is all solid-state except for the last three transmitter stages. The unit has been type-accepted by the FCC and meets all requirements of the recent FCC ruling on marine radiotelephones: 0.001% frequency tolerance; ± 5 kHz frequency deviation; 25 watts maximum allowable power output; 1-watt output "low power" capability for in-harbor use; and a post-limiter audio roll-off filter. This means that the MWW-18 will require no modification during the new rule implementation period from March 1, 1969 to January 1, 1974 or thereafter.

The unit features full coverage of both marine v.h.f.-FM bands, with six transmit/receive channels which may be distributed within the two bands as the user requires. It is designed around a plug-in control head measuring only 4½" w. x

**3 1/4" h. x 3 1/4" d.** An accessory extension cable is also available to permit the control head to be placed in one location and the chassis elsewhere.

Full specs on this new marine radiotelephone will be forwarded on request. Heath  
Circle No. 13 on Reader Service Card

#### FM TUNER CHANNEL SELECTOR

The Model 804 FM tuner features digital read-out tuning to replace the conventional FM dial. Instead of the familiar tuning band and dial for an FM tuner, the face of the 804 contains a black rectangular window which flashes the number of the channel which has been set. Tuning is positive to the exact center of the channel.

According to the company, all drift, misalignment, and mistuning have been eliminated. The new technique pinpoints the frequency since it is tunable only to the one-hundred discrete channels designated by the FCC for FM broadcasting. Selection of the desired channel is made by activating the dual-function channel selector switch, manually or automatically. The tuner can also be programmed for 24 hours of selected listening by means of an accessory clock programmer. C/M Laboratories

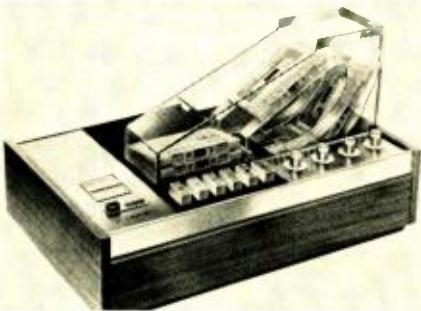
Circle No. 14 on Reader Service Card

#### CONTINUOUS CASSETTE PLAYBACK

A new cassette "circulator"—a snap-on device that gives continuous playback capacity to automatic cassette changers—has been introduced as the Model CC6.

The circulator, which has no moving parts, makes possible 12 hours of non-stop, no-repeat playback and then starts the cycle over again. It functions with four to six cassettes, automatically flips each for second-side play, and restacks the cassettes for playing again.

Functionally styled in tinted plastic and stand-



ing 5 inches high, the CC6 is simply snapped on for instant use. It is compatible with Norelco cassette changer models 2401, 2401A, and 2502 as well as Bell & Howell models 332 and 337 and Ampex Micro 90 and 95 units. Norelco

Circle No. 15 on Reader Service Card

#### INTEGRATED MUSIC SYSTEM

The "Landmark 100" is a complete music system which incorporates an AM/stereo-FM tuner and record changer and comes with "Acoust Array" speaker systems. Each system incorporates three full-range loudspeakers and a tweeter in a relatively small truncated cube enclosure. One speaker faces forward but the others are placed at asymmetrical angles at the back of the cabinet, radiating sound so that it is reflected into the listening area. The cabinets are walnut finished and have dark brown grille cloths. Each measures 10" x 10" x 10".

The tuner features all-silicon transistor circuitry with an FET front-end. Four IC's perform



the functions of AM and FM i.f. and multiplex. The unit has automatic mono/stereo switching with a stereo indicator light. A zero-center tuning meter aids accurate tuning.

A Garrard automatic turntable is included and features the new "Stereo-V" magnetic cartridge. Electro-Voice

Circle No. 16 on Reader Service Card

#### WORLD TIME DIAL FOR SWL'S

A new, easy-to-use, pocket-size world time dial combined with radio frequency charts that lets the SWL, DX'er, ham, or electronics hobbyist quickly convert the time differences between local standard times to that of other cities through-



out the world, as well as GMT, is now available for \$1.00 a copy.

The compact, two-color selector measures 4" x 5" and can be used with the turn of a big, easy-to-read dial. The frequency charts include the international SW broadcast bands, radio and TV broadcast bands, communications and navigation frequencies, ham bands, standard time and frequency signals.

Send your order, with payment, direct to Dept. PR, The Hallicrafters Co., 600 Hicks Road, Rolling Meadows, Ill. 60008.

#### STEREO RECEIVER WITH IC'S

The Model 5000A 180-watt AM/stereo-FM receiver features all solid-state design with IC's in the four i.f. amplifiers and an all-new 4-gang capacitor and FET in the 1st r.f. stage, plus two FET's in the 2nd r.f. and mixer stage. The unit also features linear tuning in the FM section for pinpoint station location.

Specifications include 180 watts of IHF music power providing 75 watts per channel of continuous power at 4 ohms. FM tuner sensitivity is 1.8  $\mu$ V (IHF), selectivity is better than 50 dB at 98 MHz, and stereo separation is better than 35 dB. The amplifier section provides a flat frequency response from 10 to 50,000 Hz.

Complete specifications on this new receiver will be forwarded on request. Sansui

Circle No. 17 on Reader Service Card

#### 5-MHz QUARTZ FILTERS

The Piezoelectric Division of Gould Inc., 232 Forbes Road, Bedford, Ohio 44146 has announced the availability of a new Clevite 6-pole coupled-mode quartz filter with a center frequency of 5 MHz.

The filters are designed for matching solid-state circuitry in communications receivers operating in the v.h.f. and u.h.f. frequency ranges, as well as in telemetry, radar, and aerospace voice radio systems.

These filters have a 3-dB bandwidth of 14 kHz and a 60-dB bandwidth of 70 kHz. They are supplied in a flat-pack coldweld case.

Complete specifications on these filters are available upon letterhead request to the Marketing Services department of the company.

#### STEPPING MOTORS

The Kearfott Division of Singer-General Precision, Inc., Little Falls, New Jersey is supplying specially designed Size 11 stepper motors and power/logic supplies for use in the U.S. Geological Survey's stereo-image alternator system—an

image-separation arrangement for viewing either black-and-white or color stereoscopic models in projection-type stereoplotters without need for filters.

Consisting of rotating cylindrical shutters in both projection and viewing fields, and synchronized so that each eye sees only the image emanating from a corresponding left or right projector, the system is an improvement over earlier anaglyphic viewing instruments.

Stepping rates for projector and viewer motors are controlled by switches on the C70 4919 002 power/logic modules, while the CR 0191 010 stepper motor provides 1.8 in-oz holding torque, 90°/step stepping angle, 220 steps/s stepping rate, and 450-ohm winding resistance.

#### MULTI-FREQUENCY OSCILLATORS

A new series of multi-frequency fork oscillators for use in inverters, data communications test sets, peripheral computer equipment, and other related applications has been introduced by American Time Products of Bulova Watch Company's Electronics Div.

The series consists of FS-300, which provides frequency outputs of 60, 120, 240, and 480 Hz, and the FS-400 with frequency outputs of 50, 100, 200, and 400 Hz. Input is +5 V d.c. at 100 mA; output is square-wave compatible with logic circuitry such as TTL. Standard accuracies are as great as  $\pm 0.002$  percent.

All units are hermetically sealed, weigh approximately 2 1/2 ounces, and measure 1 1/2" square by 1 3/16" high.

For additional information, address your letterhead request to the attention of the Product Sales Manager at 61-20 Woodside Ave., Woodside, N.Y. 11370.

#### INTRUSION ALARM

The Model ACA-140 ultrasonic intrusion alarm system is completely self-contained with the sensitive detection device and 8" alarm bell housed in a walnut wood cabinet measuring 7 5/8" x 8 1/8" x 11 3/8".

Identical in appearance to a bookshelf speaker



cabinet, the "Space Probe" projects an ultrasonic beam which blankets a given area. Any intruder interrupting this beam activates the unit, turning on a light and, in about 15 seconds, the alarm bell. The unit cannot be bypassed or defeated. No installation is necessary—the unit is merely plugged into an 117-volt a.c. outlet, turned on, and adjusted for the required range sensitivity. Bourns Euphonics

Circle No. 18 on Reader Service Card

#### AUDIO CONTROL CENTERS

Designed for home and professional sound installations, the new CC series of audio control centers allows up to four or six stereo speaker systems to be selected for simultaneous operation. The centers will provide full stereo sound in every room throughout the house with simple push-button operation.

The unique "push-on and push-to-release" switches are housed in a black metal case which looks like leather. A contrasting brushed aluminum escutcheon plate houses ivory white push-buttons and identification plate.

No external power is required for operation and the center may be used in low or high im-

Where  
do you  
put  
your  
speakers  
in a  
room  
shaped  
like  
this?

No matter what shape your room is in, Scott's new Quadrant Q-100 speakers solve your placement problems. Scott Quadrants, with two woofers and four midrange / tweeters placed around the enclosure's four sides, project full-frequency sound in a complete circle. The sound is both projected directly at you and reflected off your walls, to

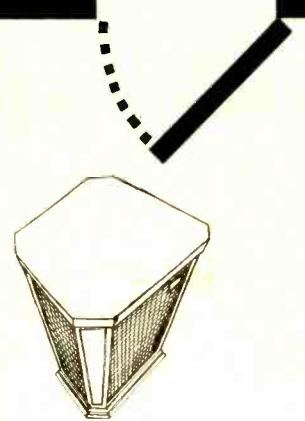
heighten the live stereo effect. No matter where you place the Quadrant speakers, your entire listening area becomes a giant stereo sound chamber. Go anywhere in the room... even sit on a speaker... you're surrounded by rich, full-range stereo sound!

Unbelievable? Hear the Quadrant's wall-to-wall stereo, at your Scott dealer's. You'll become a believer. \$149.95.

For more details, write:

**SCOTT**

H.H. Scott, Inc., Dept. 160-01, Maynard, Mass. 01754



CIRCLE NO. 121 ON READER SERVICE CARD

pedance circuits. Currently six models are available in the series. Full details on features and price are available on request. Alco  
Circle No. 19 on Reader Service Card

#### NOISE-LOADING TEST SET

Electronic Communications, Inc., Box 12248, St. Petersburg, Fla. 33733 has developed a noise-loading test set for measuring intermodulation distortion of h.f./SSB equipment and components in accordance with MIL-Std.-1311 and 188.

Designated the Model 975, the unit has an output power which is continuously variable from 10 mW to 100 watts. Minimum notch depth is 50 dB, accommodating signal-to-intermodulation distortion measurements up to that figure. Eliminating the interpretation of spectrum analyzer displays inherent in two-tone testing, the unit provides direct meter indication of distortion level.

The basic model provides a 12-kHz bandwidth notched noise test signal centered at any given frequency in the 2 to 30 MHz h.f. range (4 MHz typical). An option provides a baseband notched noise signal in accordance with MIL-Std.-188C.

Inquiries and requests for additional information should be sent to the Director of Customer Requirements at the above address.

#### 2000-WATT LINEAR AMP

The SB-220 linear amplifier uses a pair of Eimac 3-500Z's in the grounded-grid final to provide up to 2000 watts p.e.p. input on SSB and 1000 watts on CW and RTTY, yet requires only 100 watts drive for full output. A pretuned broadband pi input delivers maximum efficiency and low distortion throughout the 80-10 meter ham bands, according to the company.

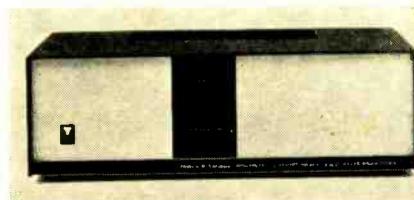
Features include a built-in solid-state power supply that can be wired for either 120 or 240 volts a.c. and circuit-breaker protection. A zener diode regulates operating bias and reduces zero signal plate current for cooler operation and longer tube life.

The company estimates that the kit can be assembled in 20 hours. Heath

Circle No. 20 on Reader Service Card

#### HIGH-POWER ENERGIZER

The new SE460 solid-state energizer incorporates all of the features of the company's SE400S

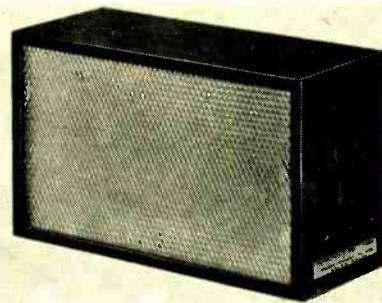


plus 120 watts of continuous r.m.s. output. Among the features of the new model are custom equalizer boards that tailor the signal for the specific speaker system connected to it, all solid-state circuitry, and low distortion. JBL  
Circle No. 21 on Reader Service Card

#### COLOR-ORGAN KIT

An easily assembled color-organ kit which can be connected to the speaker terminals of any receiver, amplifier, or console has been introduced as the Model KG-338.

The all-solid-state three-channel circuitry separates the high, middle, and low frequencies into



blue, green, and red colored lights that provide a three-dimensional display through the prismatic screen.

The organ is supplied complete with a vinyl-clad wood case which is finished in simulated walnut veneer. It measures 8 1/4" x 14 1/4" x 5 3/4". Allied Radio

Circle No. 22 on Reader Service Card

#### CONTACTLESS SOLID-STATE SWITCH

A contactless digital-output switch element that can cycle up to one million times a minute has been introduced by Micro Switch, 11 W. Spring St., Freeport, Ill. 61032.

The ISS1 solid-state switch combines a Hall element, an amplifier, and unique switching circuitry in a miniature package to control discrete and/or integrated logic circuits. Since the switching element is magnetically actuated, the life of the ISS1 is virtually unlimited, according to the company.

The switch package is constructed around an IC chip only 0.040-inch square, bonded to a metal grid. The entire switch measures 1/2" x 1/2" x 1/8" and is housed in a plastic case and wrap-around aluminum shield.

Complete technical specifications on the ISS1 are available upon letterhead request.

#### PORTABLE P.A. SYSTEM

The Model 280 portable p.a. system features all solid-state circuitry, extended voice projection, a dynamic microphone, and weighs less than four pounds with its six standard "D" cells.

The unit is suitable for use by tour guides, in schools, by civic groups, or other organizations where voice amplification is necessary when addressing a crowd. The VP Company

Circle No. 23 on Reader Service Card

#### DUAL-PURPOSE NEON DEVICE

Signalite Inc., 1933 Heck Avenue, Neptune, N.J. 07753 has introduced a new neon device which acts as a suppressor for light-powered transients and as an audio pass device on telecommunications lines.

As a transient suppressor, the Type A280 will arrest all transient peaks which exceed 205 volts, the firing voltage rating of the device. After re-

removal of the transient, the device will extinguish at 45 volts. Operation does not interfere with normal line voltage.

As an audio pass device it is turned on with the application of d.c. pulses on the telephone line. A bias voltage is supplied to keep the device in the maintaining mode after the turn-on pulse has been removed. An audio signal can be superimposed on the bias and passed by the tube to the instrument.

The A280 is housed in a glass tube 1" long x 0.244" diameter. It has one-inch tinned leads.

#### NEON READOUT

Alco-Display Division, P.O. Box 1348, Lawrence, Mass. 01842 is now marketing the "Elfin" MG-19, a 9-segmented cold-cathode indicator that forms numerals 0 through 9, +, -, decimal point, and some alpha characters and the MC-17, which is similar except it has 7 segments to form 0 through 9, -, two decimal points at upper left and lower right, and alphabet indications.

Both units have a combination spacer and mount that simplifies PC wiring and changes leads from round to straight lines.

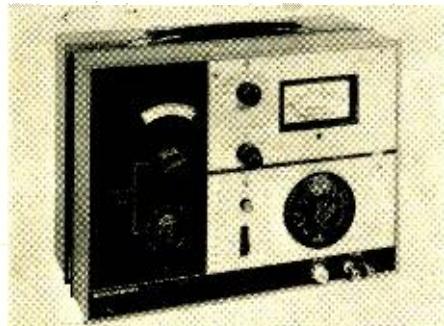
For technical assistance in application planning and additional information, address your letterhead request to Philip Mignanelli, the product sales manager of the firm.

#### FM SIGNAL GENERATOR

A new FM signal generator designed specifically for laboratory use and in production-line testing of sensitive and distortion-free hi-fi FM receivers has been introduced as the Model 188.

According to the company, two-speed tuning control and electronic incremental tuning provide exceptionally fast and accurate receiver alignment. Internal or external modulation may be measured in three convenient ranges without need for an external voltmeter. The unit may also be used with existing multiplex modulators.

An all-solid-state power supply provides regu-



lated plate, heater, and low-distortion audio voltages. The unit features double shielding, 50-ohm source impedance at a low v.s.w.r., and wide deviation with low distortion.

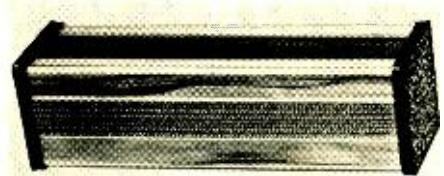
A technical data sheet on this instrument is available on request. Measurements

Circle No. 24 on Reader Service Card

#### MOTION-DETECTION SYSTEM

The new ultrasonic motion detection system, called "DeltAlert", is designed to detect any motion or intrusion and can be used both as an anti-burglary device and as a convenience item. The convenience aspects of the system include activation of night lights in carports, garages, offices, warehouses, or homes.

Operating on a frequency of 35 kHz, the unit



will monitor an area of 15-30 feet, depending on environmental conditions such as shape of the area. The receiving and transmitting elements are coupled both electrically and acoustically and the unit has been designed to yield a relatively broadband characteristic, forcing oscillation to occur at a point of maximum acoustical sensitivity.

The unit is designed to plug into any wall outlet. The lights, alarms, or bells to be activated are simply plugged into a receptacle on the back of the unit. No rewiring is necessary. Delta Products

Circle No. 25 on Reader Service Card

#### TIME-LAPSE VIDEO RECORDER

A video tape recorder that has been specifically designed for time-lapse recording is now available as the Model EV-330TLV "Videocorder."



The unit can continuously record more than 60 hours of picture on a single reel of 1-inch video tape. One image is recorded in approximately one second. The tape can be played back at the recorded speed or up to 60 times faster to locate a particular scene on the tape. Tapes recorded on this unit are interchangeable with any other EV series Videocorder.

The time-lapse recording can be used in research and science, time and motion studies, and for surveillance. As a regular video tape recorder the unit is suitable for any industrial, educational, medical, or other CCTV application. Sony Corp.

Circle No. 26 on Reader Service Card

#### FULL-RANGE SPEAKER SYSTEM

The "Quadrant Q-100" is a full-range speaker system which produces a 3-dimensional stereo effect throughout the room, according to its maker.

The new system is especially suited to the requirements of the recently introduced 4-channel stereo, either with two Quadrants used as the front pair or four systems all around.

Each system uses two 8" woofers and four 3" tweeters. Frequency range is 38-20,000 Hz and impedance is 6-8 ohms. The system will handle 80 watts of integrated program material in its air-suspension enclosure. Amplifier power requirements are 10 watts minimum.

The cabinet, which measures 14 1/4" w. x 14 1/4" d. x 22" h., is of contemporary walnut design with a brown cane-pattern grille cloth. H. H. Scott

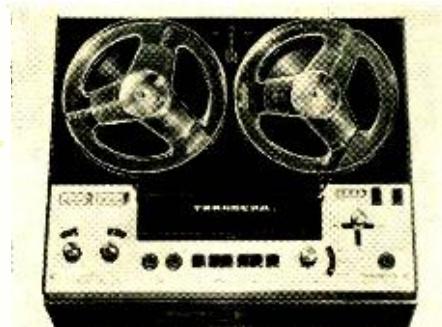
Circle No. 27 on Reader Service Card

#### SOLID-STATE TAPE RECORDER

The first in a new series of tape recorders to be introduced in the 1970's has made its appearance as the three-speed, solid-state 6000X stereo deck—a 57-transistor instrument.

The compact new deck offers four precision-gapped, Mumetal screened heads with the unique crossfield design. It is available in quarter-track and half-track models; may be used with low-noise, high-output tape; operates in vertical or horizontal position; and is housed in a walnut cabinet.

Important features include peak-reading vu meters for record and playback levels; automatic overload protection; independent mike/line rec-



ord-level controls for each channel; push-button control for electrical functions and channel selection; and a single-level tape transport control.

Frequency response is 40-22,000 Hz at 7 1/2 in/s ± 2 1/2 dB. Tandberg

Circle No. 28 on Reader Service Card

#### CASSETTE TAPE

A new blank tape cassette which features "Super Dynamic SD" tape is capable of extending the high-frequency response of most cassette recorders. The cassette offers virtually flat response from 50 to 10,000 Hz, with good frequency response above and below these figures.

A new ferric oxide formulation uses a needle-like particle shape which permits eight times greater density of magnetic particles, improving resolution and reducing sound distortion, according to the company. The new binder system reduces cross-modulation and static charge and there is no shedding of magnetic coating, thus dropouts are eliminated. TDK Electronics

Circle No. 29 on Reader Service Card

## MANUFACTURERS' LITERATURE

#### PRESSURE-SENSITIVE TRANSISTORS

Stow Laboratories, Inc., 159 Kane Industrial Drive, Hudson, Mass. 01749 has just issued an 8-page brochure describing the physical sensing and transistor characteristics of its "Pitran" pressure-sensitive transistors.

The latest technical and applications data is included, along with typical circuits.

#### AUDIO EQUALIZERS

A new 6-page catalogue describing a complete line of audio equalizers is available from Melcor Electronics Corp., 1750 New Highway, Farmingdale, New York 11735.

The equalizer line includes amplifier models, graphic module units, shelf module, and active program equalizers. These equalizers are used in the broadcasting, recording, and sound systems industry.

The publication includes detailed electrical and mechanical specifications for all units. Photos, wiring diagrams, performance curves, and general descriptive information are also provided.

Address your letterhead request for a copy of the catalogue to N. Sakellaros, vice-president of the company at the above address.

#### CENTRIFUGE FOR TESTING

A new 44-page engineering data file on its "Centrisafe" centrifuge for acceleration testing of semiconductors, integrated circuits, hybrid circuits, and other solid-state devices has been announced by Trio-Tech Inc. of California, 2435 N. Naomi Street, Burbank, California 91504.

Complete descriptions, specifications, and safety features are included for variable-speed and fixed-speed models. Also included is data on centrifuge accessories consisting of rotors, G-converters, acceleration multipliers, and spindle adapters.

#### THERMOCOUPLE DATA

Omega Engineering, Inc., Box 4047, Stamford, Conn. 06907 has announced the availability of its free 36-page thermocouple catalogue. It contains both technical and price information on thermocouples, thermocouple probes, bare and insulated

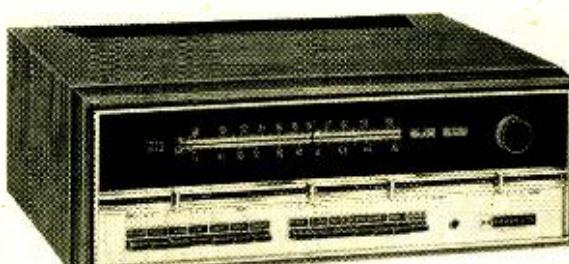
(Continued on page 92)

# Exciting New Kit Ideas from Heath

## New Heathkit 100-Watt AM/FM/FM-Stereo Receiver

World's finest medium power stereo receiver . . . designed in the tradition of the famous Heathkit AR-15. All Solid-State . . . 65 transistors, 42 diodes plus 4 integrated circuits containing another 56 transistors and 24 diodes. 100 watts music power output at 8 ohms — 7 to 60,000 Hz response. Less than 0.25% distortion at full output. Direct coupled outputs protected by dissipation-limiting circuitry. Massive power supply. Four individually heat sunked output transistors. Linear motion bass, treble, balances and volume controls. Push-button selected inputs. Outputs for 2 separate stereo speaker systems. Center speaker capability. Stereo headphone jack. Assembled, aligned FET FM tuner has 1.8 uV sensitivity. Two tuning meters. Computer designed 9-pole L-C filter plus 3 IC's in IF gives ideally shaped bandpass with greater than 70 dB selectivity and eliminates alignment. IC multiplex section. Three FET's in AM tuner. AM rod antenna swivels for best pickup. Kit Exclusive: Modular Plug-In Circuit Boards . . . easy to build & service. Kit Exclusive: Built-In Test Circuitry lets you assemble, test and service your AR-29 without external test equipment. The AR-29 will please even the most discriminating stereo listener.

**Kit AR-29, (less cabinet), 33 lbs.....\$285.00\***  
**Assembled AE-19, Assembled oiled pecan cabinet, 10 lbs.....\$19.95\***



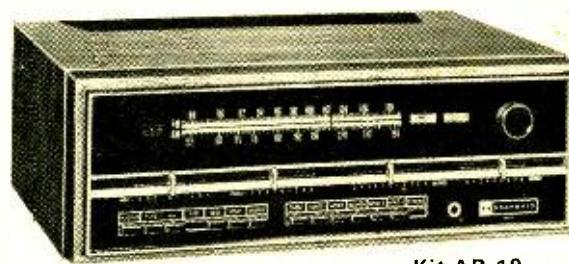
**Kit AR-29  
\$285<sup>00</sup>\***

## New Heathkit 60-Watt AM/FM/FM Stereo Receiver

The AR-19 circuitry reflects many of the advanced concepts of the AR-29. It uses 108 transistors and 45 diodes including those in 5 integrated circuits. It delivers 60 watts music power at 8 ohms. At any power level, Harmonic and IM Distortion is less than 0.25%. Frequency response ranges from 6 to 35,000 Hz. Direct coupled outputs are protected by dissipation-limiting circuitry. A massive power supply includes a section of electronically regulated power. The assembled, aligned FET FM tuner has 2.0 uV sensitivity.

A preassembled and factory aligned FM IF circuit board gives 35 dB selectivity. The multiplex IC circuit provides inherent SCA rejection. It features two switched noise muting circuits; linear motion controls for bass, treble, volume and balance; input level controls; outputs for 2 separate stereo speaker systems; center speaker capability; two tuning meters; stereo indicator light; front panel stereo headphone jack. The Modular Plug-in Circuit Board design speeds assembly. Built-in Test Circuitry aids assembly, simplifies servicing. "Black Magic" panel lighting, black lower panel, chrome accents. Compare it with any model in its price range . . . the AR-19 will prove itself the better buy.

**Kit AR-19, (less cabinet), 29 lbs.....\$225.00\***  
**Assembled AE-19, cabinet, 10 lbs.....\$19.95\***



**Kit AR-19  
\$225<sup>00</sup>\***

## New Heathkit Deluxe 18-Watt Solid-State Stereo Phono

Looks and sounds like it should cost much more. Here's why: 16-transistor, 8-diode circuit delivers 9 watts music power per channel to each 4½" high-compliance speaker. Speaker cabinets swing out or lift off . . . can be placed up to 10' apart for better stereo. Has Maestro's best automatic, 4-speed changer — 16, 33-1/3, 45 & 78 rpm. It plays 6 records, shuts off automatically. Ceramic stereo cartridge with diamond/sapphire stylus. Has volume, balance & tone controls. Changer, cabinet & speaker enclosures come factory built . . . you build just one circuit board . . . one evening project. Wood cabinet has yellow-gold & brown durable plastic coated covering. This is a portable stereo you can take pride in.

**Kit GD-109, 38 lbs.....\$74.95\***



**Kit GD-109  
\$74.95\***

## New Heathkit 80-10 Meter 2 KW Linear Amplifier

Incomparable performance and value. The new SB-220 has 2000 watts PEP input on SSB & 1000 watts on CW and RTTY. Uses a pair of Eimac 3-500Z's. Pretuned broad band pi input coils. Requires only 100 watts PEP drive. Solid-state power supply operates from 120 or 240 VAC. Circuit breaker protected. Safety interlocked cover. Zener diode regulated operating bias. Double shielded for max. TVI protection. Quiet fan — fast, high volume air flow. Also includes ALC to prevent over-driving. Two meters: one monitors plate current; the other is switched for relative power, plate voltage and grid current. Styled to match Heath SB series. Assembles in about 15 hours.

**Kit SB-220, 55 lbs.....\$349.95\***



**Kit SB-220  
\$349.95\***

## New Heathkit Portable Fish-Spotter

Costs half as much as comparable performers. Probes to 200 ft. Spots individual fish and schools . . . can also be used as depth sounder. Manual explains typical dial readings. Transducer mounts anywhere on suction cup bracket. Adjustable Sensitivity Control. Exclusive Heath Noise-Reject Control stops motor ignition noise. Runs for 80 hrs. on two 6 VDC lantern batteries (not included). Stop guessing — fish electronically.

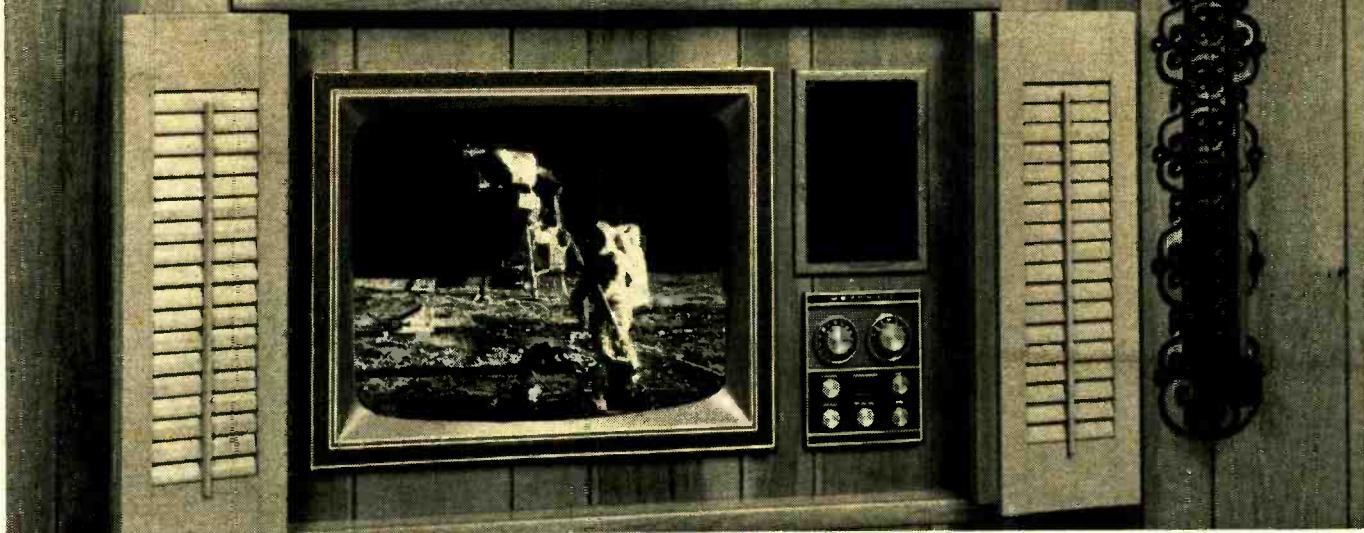
**Kit MI-29, 9 lbs.....\$84.95\***



**Kit MI-29  
\$84.95\***

# NEW IMPROVED 1970 HEATHKIT® COLOR TV

## New Lower-Than-Ever Prices



### Here's How The Color TV That Thousands Call Best Became Even Better and Lower In Price

Since the very first model was introduced, thousands of owners, electronic experts, and testing labs have praised the superior color picture quality and extra features of Heathkit ColorTV. Now Heath has made improvements that make the 1970 models even better.



**Sharper, More Detailed Pictures.** Latest design improvement in the circuitry of Heathkit Color TV video amplifiers has increased their bandpass capabilities. The result is an increase in the number of lines of resolution . . . greater than in any other brand of color TV we have tested. This improvement means you get sharper, more detailed pictures as shown by test pattern measurements. You not only get the superior *color* pictures Heathkit Color TV has always been noted for, but you also get sharper pictures.

**New Brighter Tube.** Now all Heathkit Color TV models include the new brighter picture tube you've read so much about. These new tubes produce noticeably brighter pictures with more life-like, natural colors and better contrast. (We also offer the RCA Hi-Lite Matrix tube as an extra-cost option for the Heath GR-681 and GR-295 kits.)

**New Safety Features.** As an added safety precaution, AC interlocks have been added to all Heathkit Color TV cabinets.

**Now The Best Costs Less.** How can Heath make improvements in its Color TV Models and still reduce the prices? We have passed on to you the savings which have accrued due to reduced picture tube prices. The result is your 1970 Heathkit Color TV will cost you \$20 to \$55 less depending upon which model you choose . . . proof that Heathkit Color TV is a better buy than ever.

#### All Heathkit Color TV's Have These Superior Features

- New brighter American brand rectangular color tube with bonded-face, etched anti-glare safety glass • Exclusive built-in self-servicing aids so you can adjust and maintain the set for best performance always • Automatic degaussing plus mobile degaussing coil • New broader video bandwidth for better resolution • 3-stage video IF • Improved retrace blanking • Gated automatic gain control for steady pictures • Automatic color control • Exclusive Magna-Shield surrounds picture tube for better color purity • Deluxe VHF tuner with "memory" fine tuning and precious metal contacts (models with automatic fine tuning also are available in all 3 picture tube sizes) • 2-speed UHF solid-state tuner • Completely shielded hi-voltage supply • Extra B+ boost for better definition • 2 hi-fi sound outputs for built-in speaker or your hi-fi system • 300 ohm & 75 ohm antenna inputs • Circuit breaker protection • Optional wireless remote control can be added anytime • Factory assembled and adjusted tuners, IF section, and hi-voltage supply • Exclusive 3-way installation capability — in a wall, custom cabinet or Heath cabinets

**Choose Your Heathkit Color TV Now . . .**

**It's Better Than Ever in Performance . . . and A Better Buy Than Ever**



**NEW**

#### FREE 1970 CATALOG!

Now with more kits, more color. Fully describes these along with over 300 kits for stereo/hi-fi, color TV, electronic organs, guitar amplifiers, amateur radio, marine, educational, CB, home & hobby. Mail coupon or write Heath Company, Benton Harbor, Michigan 49022.

HEATH COMPANY, Dept. 15-4  
Benton Harbor, Michigan 49022

Enclosed is \$ \_\_\_\_\_

Please send model(s).  Please send FREE Heathkit Catalog.  Please send Credit Application.

Name \_\_\_\_\_

Address \_\_\_\_\_

City \_\_\_\_\_

**HEATHKIT**  
a Schlumberger company

plus shipping.

CIRCLE NO. 137 ON READER SERVICE CARD

#### New Lower-Than-Ever Prices On All Models

Heathkit GR-681  
(295"-AFT)  
save \$30

Now only \$ 469.95\*



Heathkit GR-681MX  
(with Matrix tube)  
save \$55

Now only \$ 479.95\*



Heathkit GR-295  
(295")  
save \$30

Now only \$ 419.95\*



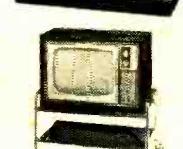
Heathkit GR-295MX  
(with Matrix tube)  
save \$55

Now only \$ 429.95\*

cabinets from \$65 \*

Heathkit GR-581  
(227"-AFT)  
save \$20

Now only \$ 399.95\*



Heathkit GR-227  
(227")  
save \$20

Now only \$ 359.95\*

cabinets from \$39.95 \*

Heathkit GR-481  
(180"-AFT)  
save \$30

Now only \$ 329.95\*



Heathkit GR-180  
(180")  
save \$30

Now only \$ 299.50\*

cabinets from \$27.50 \*



CL-377

thermocouple wire, ultra-miniature thermocouples, connectors, panel boards, ceramic insulators, cold-junction compensators, ice-point reference chambers, portable pyrometers, and many thermocouple-related items.

#### SWITCH CATALOGUE

An 8-page catalogue covering a line of snap-action, rocker-actuated, paddle, toggle, and push-button switches has been issued by McGill Manufacturing Company, Inc., Valparaiso, Indiana 46385.

Bulletin MC-90 contains data on several new switch series, including lighted miniature rocker switches, three-pole and four-pole toggle and rocker switches, and a sealed splash-proof switch.

The line includes miniature standard size snap-action, rocker, and paddle switches. Most types are available in a variety of ratings, circuitry, actuator styles, colors, and mounting arrangements.

#### STOCK PLASTIC BOXES

The 1970-71 Bradley Industries catalogue of stock plastic boxes, listing more than 300 standard sizes in 16 different styles, is now available for distribution.

The 36-page illustrated brochure provides complete information on stock rigid polystyrene boxes in square and rectangular hinged and non-hinged boxes, the "Heritage Line," round (non-hinged), compartmented, slide top, pegboard, specialty, and stock drawers and trays—also stock vials and stock semi-rigid containers. Style is illustrated for each, with individual dimensions and prices per thousand.

For a copy of the brochure, write on your letterhead to Dept. SB of the company at 353 Main Avenue, Norwalk, Conn. 06852.

#### SOLID-STATE A.C. RELAYS

A new brochure summarizing the specifications of TO-5 and solid-state a.c. relays is now available from Teledyne Relays, 3155 W. El Segundo Blvd., Hawthorne, Calif. 90250.

The six-page publication presents specifications and drawings for each line of relays produced by the company, including basic and hybrid military TO-5's, industrial TO-5's, and industrial solid-state relays. One page in the brochure describes five lines of military hybrid TO-5's, which may be ordered with transistor drives and/or operational amplifiers inside the TO-5 case.

#### H. V. RECTIFIER COLUMNS

A 24-page illustrated engineering bulletin (B-107) describing a line of high-voltage rectifier columns has been issued by the Semiconductor Division of International Rectifier, 233 Kansas Street, El Segundo, California 90245.

The columns are designed to meet the demand for high-voltage and high-power rectifiers used in power supplies and for other blocking and steering diode applications. They are available in 14 basic series with peak-reverse voltages up to 500,000 volts. Continuous current ratings range from 1 to over 220 amps.

#### FLUIDIC CONTROL MODULES

The Fluidic Products Department of Corning Glass Works, Corning, N.Y. 14830 has just published a 28-page illustrated booklet (EDP-FBR-2) describing its complete family of fluidic industrial control modules (FICM) and associated mounting manifolds.

A two-page introduction to fluidics and a two-page explanation of basic fluidic technology is followed by five pages of FICM component descriptions. A fold-out chart gives symbols and truth tables for the various elements and their corresponding symbols in other technologies.

#### PLASTIC BONDING ADHESIVES

A new 4-page, 2-color illustrated catalogue (Z-PB) describing a new line of six "Scotch-Grip" plastic bonding adhesives that offer a wide variety of properties to meet many plastic bonding applications is now available from the Adhesives, Coatings and Sealers Division, 3M Company, St. Paul, Minn. 55101.

A guide lists the six plastic bonding adhesives and 17 types of plastics, and designates the proper adhesive for each plastic bonding application. A physical properties and applications data chart describes the outstanding features, application methods, solvent, color solids content, consistency, coverage, and bonding range for each adhesive.

#### CONVERTER TABLES

Commercial Plastics & Supply Corp., 2001 W. Clearfield St., Philadelphia, Pa. 19132 is now offering its "Square Foot Converter Tables" in combination with a "Dial-a-Decimal" circular two-way table with readout of decimal and metric equivalents of fractions, or vice versa. Both can fit into a shirt pocket.

The converter applies to plastic sheets up to 96 in by 120 in as well as to aluminum, copper, steel, or other metallic sheets. This pocket-sized combination kit further aids precise cutting or shearing and quickly determines measurements.

#### RESISTOR HANDBOOK

RCL Electronics, Inc., 700 South 21st St., Irvington, New Jersey 07111 now has available its new 1970 "Handbook on Precision and Power Wire Wound Resistors."

Included are new developments in the resistor field as well as updated technical information on over 35 series of wirewound resistors.

#### LIGHTED PUSH-BUTTONS

The Specialty Switch Division of Arrow-Hart, Inc., 103 Hawthorne Street, Hartford, Conn. 06106 has published a 12-page catalogue section describing its new line of lighted push-button switches.

Called "Adapt-a-Switch," the new line was designed with a building-block concept to enable the user to build more than 25,000 switching variations from 31 stock components.

The catalogue section contains rating and circuit data on the new switches along with detailed information on components, applications, operating characteristics, optional features, and ordering information.

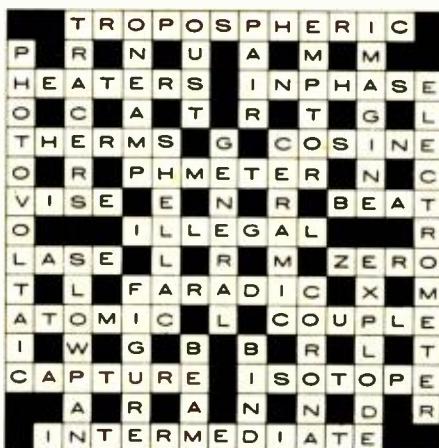
#### ARTWORK FOR PC BOARDS

The 1970 edition of the combined technical manual and catalogue 104A has been released by Bishop Graphics, Inc., 7300 Radford Ave., North Hollywood, Calif. 91605.

Describing more than 15,000 pressure-sensitive electronic-component drafting aids, techniques, and systems, the 68-page manual illustrates new ways to save time and money in preparing master artwork for printed wiring boards.

New products include the preparation of negatives for prototype boards without photography by using the "B neg" negative drafting system developed by the company. ▲

#### Answer to ELECTRONIC CROSSWORDS Appearing on page 65



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## Answers to C.E.T. Test, Section #2

Published in Last Month's Issue:

- (a) Blanking is considered black; sync is considered "blacker-than-black" as the picture tube is cut off by sync more than by the darkest portion of video.
- (d) The sound normally comes from a separate transmitter. Amplitude is fixed and not related to the video waveform. Frequency of the audio varies with modulation.
- (c) The "hammerhead" is used to cause the integrator to charge in the same manner on both even and odd fields.
- (d) Sync tips are the moments of maximum transmitter power or maximum modulation. White areas are periods of least modulation or power.
- (a) Significant i. f. frequencies are 41.25 MHz (sound carrier); 42.17 MHz (color subcarrier); 45.75 MHz (picture carrier); 47.25 MHz (adjacent sound carrier); and 39.75 MHz (adjacent picture carrier).
- (c) The 4.5-MHz sound i. f. frequency is derived by beating the sound carrier against the video carrier in the video-detector circuit. Ahead of this point, the sound is at 41.25 MHz.
- (c) The 8 cycles of burst are located on the "back porch."
- (a) The vertical scanning frequency is 60 Hz while the horizontal scanning frequency is 262½ times this, or 15,750 Hz.
- (d) Modern FM receivers use 10.7-MHz i. f. carriers.
- (b) The equalizing pulses during vertical blanking control the precise timing of the vertical oscillator, and interlace.

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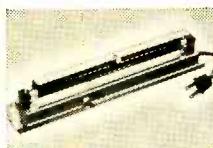
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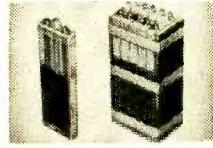
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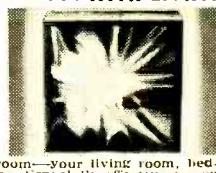
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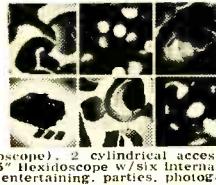
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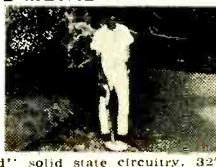
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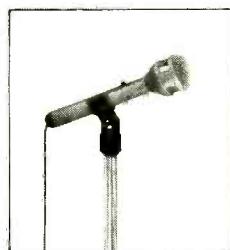


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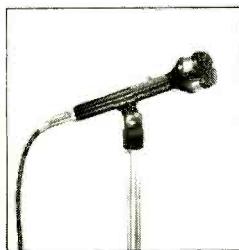


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