98 Monolithic op amps with field-effect-transistor input
106 Thin-film memory competes with disks and drums
115 Precision amplifier processes analog signals for computer
8,000 bit ROM'S performing at 2.5 MHz

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THE NEW "202X" SERIES

<table>
<thead>
<tr>
<th>No. Outputs</th>
<th>No. Address Bits</th>
<th>Configuration</th>
<th>Part No.</th>
</tr>
</thead>
<tbody>
<tr>
<td>7</td>
<td>11</td>
<td>7 x 9 x 128</td>
<td>MCS 2022</td>
</tr>
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<td>8</td>
<td>10</td>
<td>8 x 1024</td>
<td>MCS 2023</td>
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<td>9</td>
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<td>9 x 7 x 128</td>
<td>MCS 2024</td>
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<tr>
<td>10</td>
<td>10</td>
<td>10 x 768</td>
<td>MCS 2025</td>
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<td>(10 x 12 x 64)</td>
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31 Electronics Review

SOLID STATE: Hybrid vidicon imager emerges, 31
SOLID STATE: Laser opens way to single diffusion, 31
AUTOMOTIVE ELECTRONICS: Radar "crash center" may be answer, 32
AUTOMOTIVE ELECTRONICS: Mini runs electrical tests, 32
AUTOMOTIVE ELECTRONICS: Ampex technique finds defect, 33
SPACE ELECTRONICS: Rest of world watches Anik shot, 33
COMPUTERS: Next wave: a network of networks, 34
COMPUTERS: How to update tapes without recopying, 36
COMPUTERS: Computer, gages tell rain story, 36
OPTOELECTRONICS: Laser cleans, helps preserve statues, 38
INTEGRATED ELECTRONICS: C-MOS used for majority logic chip, 39
INDEX OF ACTIVITY: 40
MEMORIES: Hybrid technique yields mass memory, 41
COMMERCIAL ELECTRONICS: LED shortage to extend into 1973, 44
COMMERICAL ELECTRONICS: Point-of-sale point of view, 44
MEETINGS: WEMA Monterey session gains popularity, 45
PACKAGING: Epoxy bonding makes gains, 46

55 Electronics International

JAPAN: Color TV player uses audio cassette, 55
WEST GERMANY: Compact transceiver ends "helium speech," 55

68 Probing the News

GOVERNMENT ELECTRONICS: Adding zip to the mail, 67
COMPANIES: Firm wins calculator gamble, 70
MEDICAL ELECTRONICS: Medical engineering: prognosis fair 76
MANAGEMENT: WEMA unites on electronics trade, 82

91 Technical Articles

OPTOELECTRONICS: Shedding needed light on optical measurement, 91
SOLID STATE: Understanding FET operation yields J-FET op amp, 98
DESIGNER'S CASEBOOK: MOSFET acts as multiplexing switch, 102
Stepper drive circuit boosts motor torque, 103
Voltage-tuned filter varies center frequency linearly, 104
MEMORIES: Film a few atoms thick promises huge mass memories, 106
INSTRUMENTATION: Precision amplifier conditions computer inputs, 115
ENGINEER'S NOTEBOOK: Suppression networks for SCR converter, 120
Testing power supplies quickly and cheaply, 121
Comparing coaxial cable shielding effectiveness, 121

133 New Products

IN THE SPOTLIGHT: Calculator has full Basic capability, 133
INSTRUMENTS: Servo upgrades audio recorders, 136
PACKAGING & PRODUCTION: Memory tester is programmable, 140
DATA HANDLING: Terminal offers four data rates, 144
SEMICONDUCTORS: C-MOS rate multiplier draws only 250 nW, 146
MATERIALS: 152

Highlights

Post Office becomes big electronics buyer, 67
Over the next six years the U.S. Postal Service plans to spend $2.4 million on electronic gear that will automate handling of perhaps 75% of the mail. Volume mailers are expected to add to this market by investing in complementary equipment.

Luminance, illuminance, illumination, 91
Do these terms have the same meaning, or two or three different meanings? The terminology of light measurement is confusing and often arbitrary, and the techniques are sometimes unfamiliar to EEs who now need to be able to make intelligent use of optoelectronic devices. This article explains the language and some procedures.

The thinner the film, the larger the memory, 106
A fast mass memory, which outperforms disks and drums and costs less, too, is being developed around a permalloy film only 100 angstroms thick. Its bit-density is 100 times that of conventional thin-film memory arrays.

A calculator as clever as a computer, 133
When a calculator can talk Basic like a minicomputer and can perform much like a minicomputer, the distinction between them blurs. From the user's viewpoint, however, the new calculator is still much the easier to operate.

And in the next issue . . .

Report from Japan on the Japanese electronics industries . . . electronic organ building made simple with C-MOS.

The cover
Tektronix J16 digital photometer-radiometer takes the measure of a light beam.
Hand-held calculators are coming of age as a consumer product. But the day is still to come when they will be considered as indispensable a feature in the American household as, say, a radio or a cassette recorder. Nonetheless, the compact electronic calculator, now entering the steepest part of its growth curve, is having a significant effect on the electronics industries.

Take the example of Bowman/All, a company that has hitched its wagon to the calculator growth curve. As Gail Farrell of our Boston bureau reports in the article on page 70, it was only a year ago that the company made the decision to go with consumer calculators. Now, turning out 2,000 units a day, the company can call itself the world's largest producer. And its appetite for components, especially light-emitting diodes and circuits, has been one of the main reasons for the nationwide shortage in those items.

Gail, who has been helping us cover electronics around Boston for the last four years, says that Charles Krakauer, president of the Acton, Mass., company, is as surprised as anyone about the suddenness of the public's acceptance of pocket-sized calculators.

A year ago, he found a lot of resistance to the machines when he took home some developmental models and tried to loan them to his neighbors for a field trial. Many people said that they just could not think of anything significant to do with them, but he urged them to try anyway. A few weeks later, he had as hard a time getting the prototypes back, as many of the neighbors wanted to keep them, asking how much he would sell them for.

Since then, the company has undertaken a number of marketing studies and has found that business use accounts for a major share of sales. Yet letters from satisfied consumers keep coming. One of the best is from a family that uses a company calculator to keep track of the complicated statistics of its big leisure-time activity—sket- shooting.

The leading edge of technology, even in these times of relative austerity, is broad. On page 106 you'll find an article about a development at the leading edge of ultra-high-density-memory work. What's more, development of the so-called "oligometric" memory is sure to have repercussions up and down the frontiers of memory and computer technology. In fact, last year, when our computer editor, Wally Riley, was working on the "Computers in the '70s" special report, he was told by J. Presper Eckert, co-inventor of the pioneering Eniac computer, that oligometric memory work was one of the important areas to watch. We have been not only watching, but working with the technique's developers to bring you yet another in-depth report on leading-edge technology.
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**Readers comment**

**Matsushita widens ZNR activity**

To the Editor: The box, “Turning the tables” [p.94] in the article entitled “Metal-oxide varistor: a new way to suppress transients” [Electronics, Oct. 9, p.91], states, “Matsushita is producing zinc-oxide ceramic devices (ZNRs) only for installation in its own consumer electronic equipment,” and then it goes on to say that, “although Matsushita would like to sell its devices in the American market, the company has no plans to do so at this time.”

These statements differ from the present status of Matsushita’s activities in ZNRs. These devices have been installed in both consumer and industrial electronic equipment that is being produced, not only by Matsushita, but also by other Japanese companies. Moreover, Matsushita has prepared to sell the ZNRs in the world market—including the United States.

Yoshio Iida
Assistant director
Wireless Research Laboratory
· Matsushita Electric Industrial Co.
Osaka, Japan

**SCM calculators made in U. S.**

To the Editor: We were very interested in your article, “U. S. homes in on calculators.” [Electronics, Sept. 25, p.69]. However, the statement that reads, “Hitachi makes units for Unicom and Singer, Brother for Singer, Casio for SCM, and Canon for Monroe,” is not accurate with respect to SCM.

SCM is presently procuring all of its calculators from production within the United States; further we have never purchased any units from Casio.

Our entire marketing effort is directed toward utilization of American technology, American labor, and American designs. SCM Marchant is procuring all of its calculators on a “made-in-U.S.A.” basis.

Matthew E. Meek
Vice president and general manager
Marchant Group
Business Equipment division
SCM Corp.
New York, N. Y.

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**40 years ago**

From the pages of Electronics, November 1932

Radio manufacturers go into a final 1932 spurt offering more technical tricks than were considered possible two years ago, and at prices which cannot be compared with those of the same period. It is true that some of these new circuits are not necessary, but neither are six-cylinder engines, four-wheel brakes or balloon tires.

It is conceivable that some ultra-conservatives exist who prefer to tune a 1929 or 1930 set without benefit of acv, or, better still, quiet acv, or acoustically compensated volume control, or the still-to-be announced automatic tone control—but they must be compared with those who still prefer a one-horse shay.

The first fishing schooner to be fitted with an electronic fathometer is the Boston vessel "Joffre" which returned there recently with 100,000 lb. of halibut.

By using the electronic depth-finding apparatus, the "Joffre" was able to take soundings in rapid succession, accurately and while the vessel was under way.

Component parts manufacturers have complained bitterly in recent months of excessive chiseling indulged in by purchasing agents of the larger set manufacturers.

No one who has a broad view of any industry can consider super-chiseling as anything but practices destructive to manufacturing pride and profit, as deterrents to research and experiment, and in the final analysis as adversely affecting quality.

But there is another practice which large-quantity buyers lay at the doors of the components people. Quoting a low price on thousand lots, the parts maker actually makes a few hundred more than the thousand, sells these few hundred to small buyers at the same price given the large buyer. The large buyer, getting no advantage by his heavy buying, demands a still further reduction in price on his next purchase, thereby forcing the price to lower level. Thus the circle is completed.
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<table>
<thead>
<tr>
<th>Mfr.</th>
<th>Commercial or Trade Names</th>
<th>Device Nomenclature</th>
</tr>
</thead>
<tbody>
<tr>
<td>IR</td>
<td>Klip-Sel</td>
<td>KSA • • • • •</td>
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<tr>
<td>(W)</td>
<td>Volt-Trap</td>
<td>SO1, 2AA • • •</td>
</tr>
<tr>
<td>Syntron</td>
<td>Surge Stop</td>
<td>SD1544 • • • •</td>
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<tr>
<td>Sarkes Tarzian</td>
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This subsystem is the closest thing to a universal op amp yet devised. Already an industry standard, it's a high quality device that, with the addition of a simple external resistor, can be tailored for optimum performance over an enormous span of applications. The wide range of programmable characteristics make it one of the most versatile and useful op amps to appear in years. Applications range from a nanowatt amplifier to a high-accuracy sample and hold amplifier. 100-piece price: $3.00.

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**9616 EIA line driver ( & 9617 receiver)**
Our 9616 triple line driver subsystem has both internal inhibit and slew rate control. And it's all on one chip. Our 9617 EIA triple line receiver completes the set. They meet all EIA RS-232-C specs. And more. Together, they provide the simplest low-cost solution to problems at the interface in data terminal equipment and data communications. 100-piece price is $4.50 for the 9616; and $3.50 for the 9617.

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People

Sharif finding spot for Collins MOS work

Louay Sharif hopes to find the right niche for the MOS operation he's heading at Collins Radio Co., but it's likely to be quite different from that of MOS maker Mostek Corp., which he helped found, or of Texas Instruments, where he earlier ran an MOS operation.

Sharif, 40, was born in Iraq, but his more than 20 years in Texas (even his Ph.D. in physical chemistry is from the University of Texas) have given him the manner and accent of a Texan. So his move to Newport Beach, Calif., to head Collins' component operations from a staff job in Dallas, is apparently being made with the regret of a Texan leaving Texas. Sharif will certainly notice differences in the Collins MOS approach at Newport Beach where, unlike at TI and Mostek, MOS is a sideline.

Many large corporations have MOS operations, but few of them seem completely successful. Those that serve the corporations have often remained as expensive laboratories, while those with charters to make money have generally had to do more than serve sister parts of their companies. Collins' MOS operation has felt this tension.

Originally set up because outside suppliers have shown little interest in low-volume, high-reliability work, the Collins group has also tried to work with other companies. One way was to offer standard parts, including some acquired from Philco-Ford when it gave up its MOS operation. Another approach was to offer extensive computer-aided-design capability, including training courses, but this also attracted little industry attention.

The latest, and perhaps most surprising, activity has been processing low-cost, high-volume chips for such calculator companies as Commodore and Eldorado. Sharif says: "This is a good business for us now. We can be competitive because we have very high yields—our customers say ours are the highest of their suppliers. But I don't expect it to be a long-term business. The industry is greatly increasing its MOS capacity, and prices will be dropping again on these popular parts." A case in point is Cal-Tex, a Collins customer, which is now establishing its own plant in Houston.

Instead, Sharif is expecting to emphasize two major areas, both clearly tied into other activities at Collins. One is custom business. To service this market, he says, "Collins has developed automated techniques to reduce design costs, and even though parts designed this way use more silicon area than average, this is not a problem in low-volume applications, where design costs are more significant."

His other interest is communications, and here the group hopes to draw on the expertise of other parts of Collins for guidance. Sharif says that the MOS group is designing a family of standard parts that he hopes will satisfy most requirements and greatly reduce design costs.

Willey has big plans for credit-checking system

Even though Credit Systems Inc. of Colmar, Pa., has been a successful small company among giants, new president James T. Willey is aiming to add to the company's stature. Credit Systems, a maker of credit-authorization terminals, is a sup-
There's a lot of noise these days about RAMs and new super, bipolar processes. Well, we'd like to challenge all those bipolar claims. In fact, you can too. All one needs to do is pick up the data sheets and compare.

You may have heard or read that MOS is slower than bipolar. The fact is that the EA1500 N-channel silicon gate 1K RAM has an access time of 85nsec—worst case, including voltage variation, over the 0° to 70°C temperature range. Our “fair” competition also specs their 1K bipolar RAM at 85nsec—but at a nominal voltage and a junction temperature of 25°C!

OK, let’s just assume it’s a standoff in speed. In power dissipation, the EA1500 with a maximum, worst case, guaranteed .220mW/bit wins right out. The 93415 draws .684mW/bit at 75°C case temperature. That would take a whole bunch of air conditioning if you're going to use more than one.

Then, of course, there’s price. The EA1500 sells for about one-third less than the 93415. That’s 2.4¢/bit vs. 6.8¢ per bit in 100 up quantities. Just add up your bits and add up your savings. Finally, when you come to EA, you can get it. Because we don’t tout it until we got it.

THE GREAT RAM CHALLENGE:
N-CHANNEL VS. BIPOLAR.

Electronics/November 6, 1972

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Fact is, we’ve got the broadest line of synchro converters on the market. Single and “building-block” modules with errorless tracking . . . single and multi-speed converters of high resolution . . . multiplexed converters going D/S or S/D . . . synchro to linear converters . . . DC angle or invariant sin/cos. Chances are, the very device you need is sitting right here on the shelf.

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People

plier to major retail outlets such as Macy’s, Abraham and Strauss, and J.C. Penney.

“A major concern for us now,” says Willey, “is point-of-sale. Although POS is not a direct competitor, it’s a market we would like to be in. Unfortunately, we are a small company and don’t have the finances.” Willey, who was promoted to president from marketing vice president, figures there are two ways to get a share of the POS market. The first is to go in on a limited basis. “We can do this for about a million dollars,” he calculates. “We would have a limited system geared to the small store owner, such as a hardware store.” Willey also says that several larger companies have said they’re interested in merging with Credit Systems. A third alternative, he says, is to go public.

Another innovation instituted by the 38-year-old Willey was to expand the company’s sphere of interest from retail markets to banking. The company recently introduced an authorization system that stores checking account information. A teller, instead of phoning for the information, can use the calculator-sized system to authorize checking. It is tied into Credit Systems’ central processor in New York City. Willey says the system could be linked to a bank’s main computer, but “it is less complicated to tie it into our own central processor.”

Willey is also aiming to penetrate more markets with the check system. “There are 15,000 banks in the United States,” he says, “and if we got 10% that would be a large market. But we think there are other markets too, because actually banks do less check cashing than other outlets. For example, there is the insurance business, and this credit system would be ideal for actuarial work.”

Another Willey concept is a small-scale credit authorization system for small companies. The system is an in-house unit in which the retailer has credit terminals tied into an in-store minicomputer. “This,” adds Willey, “could enable several little companies to share the same minicomputer.”
Fluke problem solvers

The new multimeter
with advanced L.S.I.
for more function power:
26 ranges, 5 functions.

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Fluke's new 8000A,
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Now you can put the unmatched quality of Fluke instrumentation to work for you at the price of an ordinary multimeter.
Here's the DMM with more function power. It's got 26 ranges, including five ranges of AC and DC volts, five ranges of AC and DC current, and six ranges of resistance. Push button control gives you the simplest most reliable error-free operation possible.

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For a few dollars more, you can add a rechargeable battery pack to give you completely portable operation for over eight hours. And when you’re back on the line, the batteries will recharge automatically. Other options include digital printer output, deluxe test leads, high voltage probe, rf probe, 200-amp ac probe, carrying case and rack mount kits.

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But with or without options, the Fluke 8000A comes complete with test leads and spare fuses. It all adds up to an instrument you can count on day after day, year after year. Isn’t this what you want in a digital multimeter at any price? Fluke thinks so.
"Scotchflex" Flat Cable Connector System makes 50 connections at a time.

Build assembly cost savings into your electronics package with "Scotchflex" flat cable and connectors. These fast, simple systems make simultaneous multiple connections in seconds without stripping or soldering. Equipment investment is minimal; there's no need for special training. The inexpensive assembly press, shown above, crimps connections tightly, operates easily and assures error free wiring.

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Passive components are alive and well and living in Morristown, San Diego and Mineral Wells...
In the component OEM jungle, just staying alive is all some companies ask for. At MEPCO/ELECTRA we've got a different story to tell. In the last five years, while a lot of the competition has marked time and worried about the economy, we've tripled our volume.

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Which of these General Electric lamps can help you most?

New Green Glow Lamp!

Finally, a broad spectrum bright green glow lamp from General Electric, that gives you greater design flexibility than ever before. It emits green and blue light with suitable color filters. It is called G2B.

What’s more, the G2B is directly interchangeable electrically and physically with our high-brightness C2A red/orange/yellow glow lamp. So you can use the G2B alone for 120 volt green indicator service. Or together with the C2A to emphasize multiple functions with color. For example: for safe/unsafe functions, dual state indications and to show multiple operations in up to 5 colors. And remember. Both the G2B and C2A save you money because of their low cost, small size and rugged construction.

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If space for indicator lights is your problem, this new GE T-1 1/4 size all-glass wedge-base lamp is your solution. It measures less than 1/2" in diameter.

The filament is always positioned in the same relation to the base. It won’t freeze in the socket, which virtually ends corrosion problems. And like its big brother — the T-3 1/4 wedge base lamp — it features a simplified socket design.

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Get more than twice the useful output of other GE solid state lamps with GE SSL-54, SSL-55B and SSL-55C.

The increased energy concentrated in a narrow 20° cone allows you to use less sensitive detectors. Or to operate the lamps at lower current. Or to space lamps and detectors farther apart.

All are excellent matches for GE photodetectors and can be used in many photoelectric applications. They’re also particularly useful in applications demanding an infrared source capable of withstanding severe shock and vibration.

To get free technical information on any or all of these lamps, just write: General Electric Company, Miniature Lamp Products Department, Inquiry Bureau, Nela Park, Cleveland, Ohio 44112.

GENERAL ELECTRIC

Meetings

Electronica 72: Munich Fair Grounds, Munich, West Germany, Nov. 23-29.


National Telecommunications Conference: IEEE, Astroworld, Houston, Dec. 4-6.


Annual Fall Conference: IEEE, Sheraton-O’Hare, Chicago, Dec. 4-5.

Fall Joint Computer Conference: AFIPS, Convention Center, Anaheim, Calif., Dec. 5-7.

Nuclear Science Symposium: IEEE, Deauville Hotel, Miami Beach, Fla., Dec. 6-8.


Southwestern IEEE Conference and Exhibition (SWIEECO): IEEE, Houston, Texas, April 4-6.


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SUPR DIP can cut your board reworking by a factor of 10. And can improve your standard AQL six times. We guarantee it:

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What's our secret? We utilize the best provisions of several user specs; plus add a few of our own.

What do you get? Top-notch standards:

- 100% production electrical testing.
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In addition, outgoing lot quality acceptance testing includes a .15% AQL for functionality; and a 1.0% to .15% AQL for mechanical and other electrical criteria.

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Another customer concerned with board reworking bought 70,000 parts, specially identified them and inserted them into boards. After final shipment records of all systems built with SUPR DIP were collected, he ded up the results. There were only .001% defects out of 70,000 parts! And, finally, the customer who took 4,000 SUPR DIP parts and tested them over temperature. He ran the test from zero to 100°C and back to zero again. And found that many failures—zero.

Just check the number of devices per board you assemble on the chart below; then read off the percentage of board reworks at the standard AQL (point A) and at 100% pretesting (point C). Then compare it to the dramatic savings you’ll get with SUPR DIP (points B, D).

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The 97 Series is basically the same connector as our original “Old Vet” AN (MIL-C-5015). In commercial applications such as computers, traffic controls, dynamometers and welding controls, 97 Series connectors are lowering costs.

On-the-shelf inventory at your Amphenol distributor’s means fast delivery, less for you to stock. Of all the orders we ship, 90% are straight from stock. Another good reason to specify Amphenol “97 Series” right on your drawings.

Get the “straight” story from our salesman or your Amphenol Industrial Distributor (AID). Amphenol Connector Division, 2801 South 25th Avenue, Broadview, Illinois 60153.
AMI developing one-chip auto distributor CPU

American Micro-systems Inc., Santa Clara, Calif. is developing a one-chip MOS central processor unit that will replace the automobile engine's distributor. Present distributors with mechanical and vacuum spark-advance systems make generalized guesses as to the best time to ignite the sparkplug. But the CPU would calculate exactly the proper moment for each cylinder by taking into account fuel mixture, engine torque requirements, and piston position. The result would be increased performance with decreased emissions, since no fuel would be wasted by badly timed ignition. AMI says it is working with "a major automotive supply company."

Display shortage expected to lengthen

Not only is there a shortage of light-emitting-diode displays for the personal-calculator market [see p. 42], but the industry can look forward to another pinch—this one in gas-discharge and vacuum fluorescent panel displays for desk calculators.

That's the forecast of Texas Instruments' Ian McCrae, optoelectronics marketing manager for the Semiconductor group in Dallas, who expects the shortage to extend through the first half of 1973. As a result, "TI has developed cost-competitive hybrid LED displays," he says. "They're bigger than 0.2 inch and, to conserve material, they're composed of either solid bar segments or dots that are optically enlarged by the package surface."

And there's an advantage in staying solid-state, he says. "The manufacturer can take the guts of the personal calculator and drive the larger displays in desk machines; the only differences are in the keyboards and case." TI has customers committed to this approach, adds McCrae, that plan to introduce the new calculators early in 1973.

National puts clock, driver in one package

One-chip calculators and one-chip CPUs make system design easier, but they still require many external components—such as the clock generator and driver. But a new IC from National Semiconductor puts this function in a single package. The new circuit combines an oscillator, pulse-shaping network, high-current driver, and a current-limiting circuit in a single dual in-line package. It supplies a two-phase clock drive and operates at MOS or TTL voltage levels.

The circuit requires no external components at all—the frequency is programmed by a single pin connection. If the pin is left unconnected, the frequency is 200 kilohertz. If it is connected to the high rail (+12 volts in an MOS system, for example), output frequency is 500 kHz; and if it is connected to the low rail (-5 V in an MOS system), the frequency is 50 kHz. A second version, with a frequency range of from 200 kHz to 2 MHz is also expected to be available.

LED lamps give 2-color display

A new series of light-emitting-diode lamps, developed by Monsanto, may lead to increased use in commercial and military applications. The lamps offer two advantages not available before—two colors, and ac operation. Basically, the lamps consists of two LED chips in a single diffused epoxy header. Different color combinations of red, green, and yellow chips can be ordered.
AT&T files for DUV network

AT&T wants to compete in the digital data business with such special-service common carriers as Datran and the MCI companies by setting up a 96-city net by 1976 using DUV—its data-under-voice technique. AT&T has asked the FCC to approve the first five-city microwave link (Boston, New York, Chicago, Philadelphia, and Washington, D.C.) for 1974. It would use data rates of 2.4, 4.8, 9.6, and 56 kbits/s.

Hybrid scan matrix eyed for ESS

Bell Laboratories is looking into a hybrid scan matrix for its electronic switching systems as a replacement for the scan circuits now using ferrite cores coupled to sense amplifiers. A scan matrix provides the interface between the high-noise input and the central processor.

Bell figures it can save money and increase reliability with the new hybrids, which are better equipped to handle the 500-volt input and heavy noise characteristics of real-time ESS applications. The hybrid scan circuit consists of eight thin-film resistor-capacitor networks interconnected to an eight-scan-point IC. The IC consists of 26 transistors, 33 diodes, and 34 resistors. Beam leads are used for interconnection on the substrate. Each package can withstand maximum power dissipation of 500 milliwatts, and can operate in a 0° to 70° environment.

Adhesive LSI seal promises plastic prices for ceramic

DuPont has developed an adhesive seal for LSI packages that it says could help bring the price of ceramic packages down to 25 to 45 cents in quantity. This would make them competitive with the 30-cent price usually quoted for premolded plastic packages. With the new seal, said to be a hundred times better than old adhesive methods, duPont says it can get leak rates as low as 10⁻⁸ centimeters per second, which meets the hard-to-attain Military Standard 883.

DuPont says that the new adhesives seal packages, with epoxy die bonding, could bring prices down into the range of premolded plastics.

Dietzgen to sell $695 electronic slide rule

A well-known maker of traditional slide rules, the Dietzgen Corp. of Chicago, is going electronic. It is now market testing in Chicago a Japanese-made desktop machine that will begin retailing later this month for $695. William T. Laube, sales vice president for Dietzgen, says the machine will offer more than Hewlett-Packard’s $395 H-P 35—hyperbolic functions, cube roots, degree-radian conversion, and automatic conversion to decimals from degrees, minutes, and seconds.

Addenda

Hewlett-Packard has turned up an algorithm error in one of the functions of its H-P 35 electronic slide rule. A company spokesman says the error rate is less than 1%, and it occurs when the machine is performing the exponential function. H-P has told purchasers it will fix things free.

NRMEC’s planned $100 one-chip slide rule [Electronics, April 10, p. 36] is back on the drawing board because the chip got too big for economical production. New target date: February or March.

A process for making hot-pressed ferrite recording head cores promises to be a boon for computer peripherals makers. National Micronetics Inc. has acquired the proprietary process, and president Ned Buymaster says the technique will cut the price of hot-pressed ferrites for these applications from about $100 per cubic inch to between $5 and $10."
Let's face facts. Debugging the hardware, writing the system software, checking the whole system out... in a nutshell, what it costs to get the computer to perform... has been the biggest problem facing system users.

The fact is, labor dependent system software and engineering development costs often add up to many times the system hardware costs.

The new GRI-99 series addresses itself directly to the systems integration dilemma; minimizing post-purchase problems and maximizing the inherent advantages of the minicomputer.

Today's real-time applications call for more efficient ways to put information into a computer and get it out again.

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Electronics/November 6, 1972

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from our MK 5009 P time base circuit (all versions)
- Alarm tone generated on-chip; no external oscillator required (all versions)

Interfacing with your display is easy. If you're using anode tubes, our 5017 will drive your display directly (no driver transistors necessary). Or, you can interface with LED, incandescent, gas discharge tube or light emitting film displays with minimal additional circuitry. And if you’re using some other type, check our latest applications literature to shed some light on your problem.

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Electronics review
Significant developments in technology and business

Old technique spawns hybrid vidicon imager

Westinghouse gets TV quality with 200,000 phototransistors and hybrid scanning, control panel in unit built for NASA

For years, engineers have been attacking the stubborn problem of how to get the bulky high-voltage electron-beam scanning system out of the otherwise solid-state-target video camera. One solution applies the new technology of charge-coupled-device imaging, which uses simple MOS clock-scanning techniques. But now an older technology—the culmination of an effort under way for more than a decade—has entered the picture.

Built by the Westinghouse Defense and Electric Systems Center for NASA, the latest all-solid-state imager achieves TV quality with an imaging surface of 200,000 phototransistors and a hybrid scanning and control panel. Together they form a novel array camera—completely self-contained and needing only 110 volts. And the camera's output fits into conventional TV studio-type display monitors.

The phototransistors are organized in an X-Y matrix of 400 rows by 500 columns. The sensors are made by standard silicon processing on a 2.5-inch slice, with individual devices on 2-by-2.5-mil centers, adding up to a resolution of 200 line pairs in the vertical direction and 250 in the horizontal.

The scan circuit, built by hybrid bare-chip techniques, takes the raw serial video image and, with separate blank and synchronization pulses, converts it to a 1-V EIA composite video signal. Scan synchronization is from a digital generator, while master clocking is from either a 9.45-megahertz crystal-controlled source or an externally variable source that allows the system scan rate to be tailored to the application.

Camera power and weight are still high—12 watts and 5 pounds—but newer models are expected to be reduced to 1 w and 1 lb.

Laser opens way to single diffusion

Monolithic power Darlington transistors have been available for about two years. But until now, no single-diffused Darltons, with their much higher safe area than epitaxial-base and triple-diffused versions, have been made. Motorola Semiconductor and Soliton Devices have just announced the first such parts, opening the possibility for even lower power-transistor costs.

The first Motorola parts have output devices similar to the popular 2N3771. Paradoxically, however, the Darlington version, which incorporates two transistors in a series configuration, uses significantly less silicon than the lower-gain single part—220 by 180 mils instead of 240 mils square. According to Leo Lehner, Motorola power operations manager, this opens the door to large cost savings when the process gets into high gear. Not only will the supplier's costs be less, but there'll be a savings of one complete package and mounting.

The reason for the smaller size is that conventional single-diffused
parts are gain-limited rather than current-limited. The newer parts, however, maintain their gains to 20 rather than only 10 amperes. "We cram base current like crazy into the second transistor," says Lehner.

Two new developments were necessary to make the parts practical, says Lehner. One was laser-scribing. "You can't scribe and break these parts because you would have to go over a bump in the surface, and that doesn't work." The only alternatives to the laser would be sawing or deep etching, both time-consuming methods that would require up to 15 mils waste between the parts instead of the few mils required by the 1-mil laser kerf.

Lehner says that a new method of making an internal or monolithic contact for the input base resistor was necessary. It actually goes under the emitter, using the diffused contact for the input base resistor. The circuit also includes an unusual output diode, a notch in the diffusion that provides a local short from the output collector to the emitter. This protects against reverse-emitter spiking with a positive-going signal.

The price of the parts is still higher than the two equivalent parts it replaces ($3.30 for the 2N6355, its type number, vs. $3.10 for a 2N3771 and 2N3054, all 100-up prices), but that figure should come down with volume, says Lehner. Coming up soon will be a Darlington version of the popular 2N3055 and high-voltage triple-diffused Darlington.

### Industrial electronics

**Mini runs electrical tests**

What fails most often in a new car? The electrical system, one of the big three American auto makers discovered, which has to be repaired at the manufacturer's cost, and owner's inconvenience, under the car's warranty. To reduce the failure rate, the auto maker is borrowing a technique familiar to the electronics industries—automated, minicomputer-directed testing of the finished product.

The test system, called VETS (Vehicle Electrical Test System), was developed by a minicomputer manufacturer, General Automation Inc. This firm's Automotive Industries Division in Southfield, Mich., has been concentrating on applying its machines to chores in the auto factories.

VETS is essentially a programmed go/no-go tester and information store. It presents written test instructions on a 10-by-24-inch display panel that hangs in front of the windshield of the car as it moves down the assembly line. Peering through the windshield from inside the car, a worker reads the instruc-

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**Radar ‘crash center’ may be a better answer to car safety than radar braking, says DOT**

Braking radar just may not be practical for the automobile of the next decade or so, according to a study conducted at the Department of Transportation's Transportation Systems Center, Cambridge, Mass.

Researcher J.B. Hopkins, in reviewing the results of the study, notes wryly that collision-avoidance radar systems will be "challenging developments" if they are possible at all. Instead, Hopkins suggests the adoption of radar crash centers to trigger passive restraint systems like air bags—a job they would do more effectively than the electromechanical systems now being studied.

The problem with braking radar is simple: the environment is too complex for it. It would have to be too powerful; its signals would require too much processing, and in the end it could be quite costly. In addition, drivers might well disable it because of false alarms and consequent sudden deceleration.

On the other hand, crash centers could become part of automotive equipment lists before 1980, estimates Hopkins. Today in most experimental systems an accelerometer is used to trigger inflation of air bag restraints. The accelerometer begins working at the instant of impact, and operation of the whole restraining system takes about 50 milliseconds.

The advantage of a radar-like crash center would be in its advance warning. Accelerometer-equipped cars are "safe" only up to about 30 miles per hour now, but the radar center's one or two meters of warning would be enough to increase the safe speed of a restraint-equipped car to about 60 miles per hour.

The center has worked out a parts list for such a system—a bplanar array antenna, Lsi signal processor, Gunn diodes, and mixer—and has priced it at $10 to $20 in volume. But that is only parts cost, and installation, test, handling, and margin for profit could easily raise the initial cost to $75 or more. Adding in customer-paid inspection and maintenance would raise the ante to about $150; in what is becoming a typical 10-million-car sales year, the center systems market would total about $1.5 billion dollars, of which 10% would be a market for electronics firms.

As envisioned by the center, such a sensor would probably be a continuous-wave doppler radar with a range of a couple of meters. It would not be much of a radiation hazard as radiated power at the antenna would be only about a quarter of a milliwatt per square centimeter and 0.002 milliwatt a meter away. Nor would the crash center be prone to false alarms as the more powerful braking radars: it just wouldn't have the range to mistake a tree trunk for a trailer truck.
tions and puts the car manually through its electrical paces. Instructions are generated on the basis of punched-card data describing the electrical options in each car. Whether each part of the electrical system—such as the headlights, or the air conditioner's blower motor, or the motors driving the windshield wipers or windows—performs satisfactorily is determined by sensing the current supplies from the car's storage battery and comparing it with data on permissible limits stored in the computer's core memory. If the current is within limits, VETS goes on to the next test. But if the current falls out of limits, a no-go indication is given, and the fault is identified and printed out on a teletypewriter. At the end of each day, management has a complete report on faults found in all cars coming off the line.

In addition to a clamp probe that hooks up to the car, the General Automation system includes an analog-to-digital converter; the company's SPC-16 minicomputer with 8,192 words of core memory; the display panel which projects as many as 64 test and go/no-go instructions printed on slides; and a hand switch with which the operator signals the test results so that the system may proceed to the next test. An out-of-bounds current calls for a retest before a fail message is stored in the computer.

So far, General Automation has delivered several of the VETS system to be tried on assembly lines both in this country and at a plant in West Germany.

**Ampex technique finds auto defect**

A new twist on an old theme is undergoing tests at Ampex Corp. in Redwood City, Calif. For the past several years Ampex has been experimenting with optical data-processing techniques for processing essentially acoustical information [Electronics, Nov. 8, 1971, p. 75]. Previous Ampex work with the Office of Naval Research and with NASA's Langley Research Center has been aimed at finding mechanical failures in jet engines and airframes. But now, according to Ampex, the auto industry is interested.

One of the Big Three in Detroit has contracted with Ampex to develop a system for determining if certain parts are missing from auto engines as they come off the assembly line. Tests to date have been with bearing inserts, and David Rodel, one of the engineers on the project, says, "We've been very successful."

Basically, the Ampex technique compares the frequency spectrum from the engine under test with one that is known to be complete. The audio signal from the engine under test is picked up by a microphone and is fed to an electron-beam recorder that "writes" the signal in a raster pattern across photographic film. The laser beam is then passed through the film and onto another piece of film, and through a lens. The second image is actually the Fourier transform of the original signal, and thus it is a plot of the full frequency spectrum that was present in the original signal but not visible on the time vs frequency plot.

Since each dot and blip on the transformed photo represent something in the engine under test, and since the parts are alike in all engines of the same type, a comparison of the photos can easily indicate a missing part.

To make the system truly useful, each part in the engine must be identified as a blip on the photo. The next stage at Ampex is to try out the equipment's success at spotting a missing piston ring.

**Space electronics**

**Rest of world watches Anik shot**

When the West's first domestic satellite goes up this week—launch is scheduled for Nov. 9—it will do more than supply Canada with television, voice, and data communi-
Looking up. Canadian domsat Anik 1 takes its name from the Eskimo word for brother.

cations. It will also provide a test-bed for ideas that could revolutionize communications and even society in underdeveloped nations.

According to Harold A. Rosen, manager of commercial satellite operations at Hughes Aircraft Co. in El Segundo, Calif., many countries are apparently waiting to see whether Anik 1, built for Telesat Canada, fulfills its promise of providing practical communication to the remote regions of northern Canada. They should know soon, for operation is expected to start in January. In the U.S., Hughes has already found a buyer in Western Union for its proposed domestic system, and Rosen also expects to sell to at least one other domsat company.

Two Aniks are scheduled to go into synchronous orbit (one as backup) to provide coverage of Canada, with a third held on the ground in reserve. They will connect a ground network incorporating two conventional heavy-route stations with 30-meter antennas in Toronto and Vancouver, a tracking and command station, two northern telecommunications stations with TV receive and two-way message capability, six network TV stations for TV relay, and 24 remote TV receiving stations.

Added to this will be about 20 thin-route stations providing two-way message channels for native villages and other installations in the far north, where conventional microwave or line communications would be prohibitively expensive. This varied capability offers much promise to other countries without the complete telecommunications networks of the U.S., Japan and Western Europe.

The Hughes birds, which incorporate substantial subassemblies made by Canadian firms Northern Electric Co. and Spar Aerospace Products [Electronics, Aug. 1, 1970, p. 152], offer much of the capability of the much larger Intelsat IVs built for Comsat by Hughes. But Anik incorporates a number of innovations that keep the size, weight, and systems cost down—the total cost to Canada is about $60 million for satellites, earth stations, and boosters.

Among these are a unique dual-mode antenna system designed to cover Canada, and orbit control to ±0.1° to permit use of low-cost non-tracking antennas on earth. The 12 36-megahertz channels do not have redundant traveling-wave tubes, but two channels are considered spares in the design, and the receivers are fully redundant. The spacecraft antenna uses a new gold-plated aluminum honeycomb with graphite exterior. The thin reflective mesh is transparent to solar pressure, but not to the 4- and 6-gigahertz operating frequencies. Total height is 11.6 feet, diameter 75 inches, and weight 1,200 lb at liftoff, compared to the 17.5 ft, 93.5 in. and 3,100 lb of the Intelsat IV with its similar 12 channels.

For future domestic satellites, Rosen anticipates interest in adding capability for the newly authorized 2.5-gigahertz band for community broadcasting. Though not suitable for direct transmission to an unmodified home receiver, this range could be used with a 10-ft dish and simple transistor converter for a $1,000 station—a long way from the $100,000 versions that will be used with Anik. For this use, Hughes has developed a special high-efficiency TWT that can put out 50 watts at over 50% efficiency. Further off in the concept stage could be direct broadcast at 12 GHz, where unlimited power is allowed, and a 1-meter dish and small mixer for TV reception. In both cases, Rosen sees direct broadcast of less interest in the U.S. than overseas.

Computers

Demonstration heralds next wave: connecting a network of networks

Now that plain computer time-sharing has been replaced by networks of computers as the newest important trend in extending computer power, it’s inevitable that somebody would take the next step—hooking up a network of networks. And that’s what was done as part of last month’s International Conference on Computer Communications in Washington.

One of the highlights of the conference was a demonstration of the Advanced Research Projects Agency’s Arpanet [Electronics, Dec. 20, 1971, p. 64]. This is a coast-to-coast network of about 20 large computers at various Government, university, and private research centers, interconnected by wideband telephone lines at 50,000 bits per second. Each computer’s connection to the network is through an Interface Message Processor, a small Honeywell computer modified by Bolt, Beranek, and Newman Inc. In addition, a few centers have terminal IMPS, or TIPs, which provide access to the network but do not furnish computational capability to it.

For the demonstration, a TIP was set up in the hotel and 29 terminals, of almost that many different kinds, were connected through the TIP to Arpanet. Using any of these terminals, conference attendees had ac-
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Another TIP in Arpanet is at NASA-Ames Research Center in Mountain View, Calif. Ames is also a customer of Tymshare Inc., a commercial time-sharing concern whose headquarters are in Cupertino, Calif. Tymshare operates its own commercial computer network under the name Tymnet. Tymnet's lines are an order of magnitude slower than Arpanet's and the system works under a different set of rules, but in many other ways the two are quite similar. Corresponding to Arpanet's IMPS, for example, are Tymnet's Tymsat's, satellite computers that provide an interface between the computers and the communication lines.

With an interconnection between Ames' TIP and Ames' Tymsat, Tymnet users had access to Arpanet facilities, and Arpanet was able to use a Tymnet computer facility in Paris, via transatlantic cable—the first time Arpanet has gone beyond the continental U.S.

The hookup was intended to show feasibility only, and under regulations of the Federal Communications Commission was to be dismantled after the conference. But since the experiment succeeded, and since ARPA wants to spin off the network as a self-sustaining operation, probably under private ownership, the link can easily be restored at some future time, and other links can be established between other computer networks.

Meanwhile, with the great interest in computer networks indicated by the many sessions on this topic at the conference and the crowds in the Arpanet demonstration room, networks clearly are the wave of the future, just as time-sharing was the wave of the future only six or seven years ago.

"In the next few years you'll see a proliferation of private computer networks, just like the time-sharing companies that sprang up in the late 1960s," says Frank E. Heart, director of the Computer System division at Bolt, Beranek and Newman. In fact, Heart reports many inquiries from companies thinking of buying IMP-like machines for terminals, and BB&N itself is looking into the possibility of establishing a private network. And of course the company, as builder of the IMPS and TIPS, is actively soliciting business from other interested parties.

"We've had lots of bites," says Heart, "but we don't have any fish in the frying pan yet." But a couple of dozen groups from foreign countries en route to or from the conference have been touring his laboratory in the weeks preceding and following the meeting.

How to update tapes without recopying

One of the difficulties with using magnetic tape as a storage medium lies in the mechanical characteristics of tape and of tape drives—they don't permit a new record to be written directly on the tape between two previously written records. To add new data, the whole reel must be read, the appropriate records processed, and everything rewritten on a different reel.

This rewriting is no longer necessary, claim engineers at the Boeing Co.'s data systems group in Seattle, Wash., who have found a way to update records directly. There's a price, of course—inefficient use of the "real estate" on the tape, and thus of the time required to read records—but this can be less inefficient than copying a reel.

In standard usage, a 0.6-inch gap separates tape records. When the tapes stops, the read/write head is somewhere near the middle of this gap, which provides room for deceleration and acceleration without losing data. Often all the records on a reel are divided into groups or files, each of which is terminated by a special one-character record called a file mark plus a special 3-in. gap.

The new technique worked out at Boeing assigns a number to each record. The record and its number become two separate records that together form a file, followed by the standard file mark and 3-in. gap. Thus, to update a numbered record known to be somewhere on a reel of tape, the reel is searched for that number. The revised record is written directly over the old one, immediately after the number, a new file mark is added, and a new 3-in. gap created behind it. As all records are the same length, this stops the tape just in front of the identifying number for the next data record.

The cost in terms of tape inefficiency is easy to calculate. Suppose each data record consists of the equivalent of 10 ordinary punched cards, or 800 characters. These occupy an inch of tape, and in conventional recording would be followed by the 0.6-in. inter-record gap. The total length of tape occupied by a single record is thus 1.6 in., of which 1.0 in. actually stores data, making the efficiency 62.5%. Double the record length gives 77%.

But with the Boeing technique, the inch of tape storing data would be accompanied by a short record of a few characters labeling the data, a one-character file mark, two standard inter-record gaps, and a 3-in. file gap—a total length of 5.2 in. and an efficiency of 19.2%. In this case, doubling the record length increases the efficiency only to 32.2%.

A similar approach has been used by Digital Equipment Corp. for many years with its DECtape units. However, DECtapes come only in reels of a few hundred feet, compared to the standard 7-in. 2,400-foot reels. They have no inter-record gaps, and the drives have to be used with a controller, which compensates for the lack of gaps, recognizes the record numbers, and searches along the tape either forward or backward for a particular record. Corresponding functions are by software in the Boeing method.

Computer, gages tell rain story

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Electronic review

about the havoc too much weather can create.

In San Francisco, plagued by winter rainfall problems for many years, the problem is complicated by the city's famous hills, which tend to concentrate the runoff from a rainstorm—sometimes in unexpected places. But the department of sanitary engineering is using a computer in conjunction with an array of rain gages and sewage gages to establish just where in the city rain falls most heavily, what kind of load the rainfall places on storm sewers, and how and where new sewerage facilities should be built to prevent overflows.

With the results, the computer can print an outline map of the city, showing where the rain fell most heavily at any particular time during a storm; a series of maps showing the rainfall pattern at intervals a few minutes apart shows the storm working its way across the city, with occasionally heavy downpours occurring at isolated spots.

Like most other cities, the local government relied for many years on a single rain gage at a central point. After every storm, or at intervals during an extended storm, somebody from the weather bureau would look at the gage and note the amount of rainfall in inches. Then the department of sanitary engineering would try to relate this number to the difficulties encountered with flooded streets and inconvenience to the citizens—usually without much success.

Thirty gages. When it was decided that this system was inadequate, 30 rain gages were installed at strategic points throughout the city along with 120 sewage gages—following a good deal of preliminary experimentation and some political diplomacy. Each rain gage consists of a pair of small vials during an extended storm, whose locations are interpreted by the computer.

A California oceanographer has developed a laser technique to clean and protect priceless works of art, make perfect images for posterity, and detect faults.

It started when the W. H. Munks—he is a professor at the University of California’s Scripps Institution of Oceanography in La Jolla and she is a sculptress—visited Venice, a city where polluted air is

Laser cleans, helps preserve statues

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slowly deteriorating priceless sculptures. After his wife interested him in the problem, Munk, with J. F. Asmus of Science Applications Inc. and R. F. Wuerker of TRW Systems, took holographic apparatus to Venice last spring.

Wuerker says most restorers feel that their most important single result was in the statuary cleaning, and the Italians have bought a laser for this use. But the team also hopes that eventually holograms could be placed on display so that actual pieces wouldn't be subjected to attacks like the one on the Pieta, and holograms could provide templates for restoration. The low-budget project was partly funded by a $7,000 grant from ENI, the Italian Petroleum Institute, which operates some of the refineries that cause the pollution.

Laser bursts seem ideal for cleaning marble pieces, which are typically almost black with a corrosive mixture of carbon, soot, chalk, calcium carbonate, iron oxides, and silicates as much as a centimeter thick. Present methods of cleaning are either very slow or unselective in removing parts of the statue as well as the crust. According to Wuerker, however, the ruby laser used removes the dark deposit, but has little effect on the light-colored marble beneath.

Unexpectedly, the dark color of the subjects interfered with attempts to provide enough light to make holograms of the complete pieces. Wuerker estimates that a laser more powerful than the 1-joule ruby model used could do the job.

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**Integrated electronics**

**C-MOS used for majority-logic chip**

The C-MOS boom is accelerating as designers make the technology more attractive. First, the performance of standard C-MOS product lines was boosted by dielectric and polysilicon isolation fabrication techniques [Electronics, Oct. 9, p. 127], and now
flexibility will be added by a different kind of logic, called majority logic. Motorola plans to introduce the industry's first C-MOS majority-logic chip in December—a five-input device that could replace 25 standard transistor-logic gates.

The chip is undoubtedly flexible. It can be used for all the common logic functions, like \( \text{AND, NAND, OR, and NOR} \), as well as the basic combination and comparison functions and their inverses. More significantly, it can be used in arrays to perform correlation functions—such as comparing multiple samples with a test bit—or sequential functions in which the output is determined by the character of the inputs. For example, there's the two-input flip-flop that will change state only when the inputs agree, or a unique three-input condition.

Lane S. Garrett of Motorola, one of the key developers of the chip, feels that this type of logic has not been used throughout the industry because its usefulness is not generally understood. Also, it makes a fairly complex MSI chip, containing a total of 88 devices (44 n-channel, 44 p-channel) on a die 59 by 67 mils. Garrett sees the device finding its way into many standard military
and industrial applications, and points to character recognition as a prime example.

Hybrid technique yields mass memory

The prospect of semiconductor mass memories—several million bits—based on hybrid techniques is growing brighter with the success of a CMOS memory and logic subsystem built by the Westinghouse Electric Corp. for the Naval Air Development Center. This type of hybrid subsystem, which has 192 words by 32 bits, could serve as a building block for a 3.6-million-bit memory.

The CMOS unit, which meets military specs, contains CMOS random-access memories built by Westinghouse and standard off-the-shelf decode and logic CMOS chips. What's innovative is that they're all put down as bare chips on one substrate, so that each package is a self-contained unit that includes memory, address, and decode. By comparison, conventional semiconductor memories are built up with dual in-line RAMS and peripheral circuitry in separate packages.

In a mass memory, each Westinghouse substrate would actually house 256 words of 18 bits each and be wire-bussed to others to form one package—in this case a 4,096-word by 18-bit section. Finally, these packages may be wire-bussed to build up memory modules of 32,768 words by 18 bits.

Now that this approach to mass memory has been operating successfully at the NADC labs since June 1971, Westinghouse plans to replace the CMOS RAMS, which occupy a great deal of chip and have n-channel leakage difficulties, by nitride MNOS RAMS. These would have the advantage of being nonvolatile, but would require more power. Interestingly, the same CMOS logic—with some level shifting—could be used with the MNOS units.

While the early work was done

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<th>CRYSTAL RANGE</th>
<th>OVERALL ACCURACY</th>
<th>25°C TOLERANCE</th>
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<td>6000KHz to 60MHz</td>
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<td>+ .0005%</td>
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Electronics review

under a $25,000 Navy contract, the MNOS effort will be performed under an 18-month contract of $570,000 from the Army Electronic Systems Command, Ft. Monmouth, calling for demonstration and development of reliability data.

Commercial electronics

LED shortage to extend into 1973

The personal-calculator industry is beset by a shortage of light-emitting diodes—and suppliers and users expect the deficit to continue into 1973.

Monsanto's Hank Carbajal, product marketing manager for displays in Cupertino, Calif., says two factors led to the situation. First, "Many calculator makers were counting on liquid-crystal displays: when liquid crystal didn't come about, the makers switched to LEDs." Second, there's a material shortage.

The shortage could affect prices. "The eventual price of consumer calculators is to a large extent dictated by the availability of displays," says Ian S. McCrae, optoelectronics marketing manager at Texas Instruments. "Basically, it's a materials problem—the price and availability of the gallium-arsenide-phosphide chip. And people buying gallium-arsenide wafers and doing their own epitaxial work are finding a basic shortage of GaAs." TI's solution is to convert customers from the 100-mil digit to a 70-mil size.

In Santa Clara, Calif., National Semiconductor's LED display production is heavily committed to the NSN-33 three-digit cluster. National's experience with that product is typical of what's happening with LEDs today. Paul Pagnini, LED product marketing manager at National, says the NSN-33 never has been announced as a product. National simply sampled a few customers, and the orders came faster than they could be handled. "We had a massive backlog even before we started production."

Charles Krakauer, president of Bowmar/ALI Inc. of Acton, Mass., says, "One interesting guessing game is when capacity will reach demand. We keep pushing the date ahead. It could be well into '73 before supply catches up with demand." Bowmar itself was short of LEDs for a while, and had to go outside. Production has risen, however, so that Bowmar has once again become a supplier as well as a user. And the GaAs shortage is getting less acute, Krakauer says.

Monsanto's Carbajal agrees. He says material shortages should be eased somewhat by construction of additional manufacturing facilities at Monsanto, TI, and Litronix. In fact, a Litronix marketing manager says, "We're in pretty good shape—we're meeting our commitments—because we significantly increased our capacity over the past six months." But, says Dan Davis, manager of Litronix' Consumer division, "We can't build for stock—we have no cushion."

Some optimism is being emitted by Bell & Howell in Pasadena, Calif. There, Robert D. Burr, prod-

Number of numbers

What's the light-emitting diode market for calculators? James Lovette, LED marketing manager at Fairchild's Microwave and Optoelectronics division, puts it at $20 million to $26 million for 1972. At an average price of $2 a digit, that comes to 10 million to 13 million digits. Lovette, who says Fairchild is doing more LED-display business by dollar volume than anyone else, places the total shipping rate for all suppliers at about 25 million digits a month. From talks with several industry sources, the shipping rate in digits per month looks like this:

- TI 500,000
- Litronix 500,000
- Fairchild 450,000
- Bowmar 350,000
- H-P 300,000
- Monsanto 250,000
- Others 300,000
- TOTAL 2,650,000

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Electronics review

uct manager for the Electronic Materials division, doesn’t see the materials shortage as a long-term proposition. “It shouldn’t last more than three or four months.”

Point-of-sale is a point of view

No doubt about it, the point-of-sale market has begun to bloom; what appeals to retailers is the basic premise of POS: it saves them money. But D.C. Leonard of the TRW Systems Application Center, asserts that it isn’t that clear-cut. Like everything else in electronics and engineering, there are tradeoffs.

According to his figures, there already are 30,000 credit-checking POS terminals in operation, and growth is projected at 250,000 by 1976. In addition, there are 3 million to 4 million cash registers in the United States, and many are potential candidates for replacement by POS terminals. However, questions arise—are users asking too much, and can makers supply POS systems that are both cost-effective and profitable?

In Leonard’s study, POS systems break down into three families; verification systems separate good account numbers from bad; authorization systems separate good account numbers from bad; authorization systems separate good account numbers from bad; authorization systems separate good account numbers from bad; authority systems enable transactions in amounts above so-called local

News briefs

H-P cuts mini prices
Hewlett-Packard has cut prices of end-user and OEM minicomputer prices by up to 35%. The reduction, says William Nilsson, marketing manager for the Data Systems division, is due mostly to reduced core costs. Another factor, he says, is volume discounts. The price cuts may be expected to shift H-P’s traditional end-user emphasis somewhat more toward the OEM.

At Data General and Digital Equipment Corp., spokesmen profess to be unimpressed. A DEC official says H-P systems will still be more expensive than DEC’s; Data General believes that if H-P is attempting to use the new prices as an entree to the OEM market, it may not have much luck.

Asbestos-free phenolic
As of the first of the year, all phenolic supplied by GE for molding will be asbestos-free. The material, a thermosetting plastic, has been used for 40 years in terminal blocks, tube sockets, and connectors. The asbestos enhances heat resistance of the molded product. About 40 million pounds a year are used by the electronics industries. Now, the Occupational Health and Safety Administration has targeted asbestos for regulation due to its toxicity.

Lawrence finds a builder
The ultrafast printer capable of spewing out 30,000 lines a minute, which Lawrence Livermore Laboratory was looking for last year [Electronics, July 19, 1971, p. 32], is to be built by Honeywell Information Systems in its plant at Oklahoma City. Honeywell won’t talk about how it plans to do the job—the old machine, built by Radiation Inc., formed the characters with tiny black spots burned into special paper by arcs from a row of electric styluses—but figures on being ready to deliver to the laboratory by the third quarter of 1973.

Teradyne to buy printer
Printer Technology Inc.’s PT-100, which at 100 characters a second is billed as three times faster than any other serial, full-character impact printer, has won its first significant contract—$200,000 from Teradyne Inc., the test-system maker.

Printer Technology of Woburn, Mass., expects the $2,200 PT-100 to fill the gap between the 30 character-per-second serial full-character models and the much faster, but more expensive, line printers.
floor-release limits; and transactional systems enable entry and display of any data needed to make and record transactions. The verification systems are the least complex, and generally cost the least, while the transactional systems, the most costly and complex, are the focus of POS development.

On-line POS system communications problems are like those of telephone systems because the capacity to handle peak load periods during the business day ensures under-utilization of the communications network during off hours. Leonard figures that peak traffic levels can be as much as five times as high as average levels.

Speed needed. Also, a good POS system must offer fast response. While this isn’t much of a problem with simple terminals, transactional systems can take almost half a minute to respond during peak traffic periods, while clerk and customers trade glares. Human factor studies, Leonard says, show that terminal operators get “upset” when response time exceeds about 15 seconds. This places more stress on the speed of communications and, in turn, translates not only into a need for a more capable network—and further under-utilization—but also into electronic switching, rather than less costly rotary switches and dials.

Thus, both the POS terminals and the communications nets that link them to their central computers bid fair to cost a great deal.

---

**Meetings**

**WEMA’s Monterey attendance rises**

To the young and growing electronics company, proper exposure to the financial community, while essential, is generally hard to come by. If the company goes to the financial press or analysts, it is accused of pumping; but if the small company has to wait to be “discovered,” Wall Street may never hear of it.

This is especially a major problem

---

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Electronics review

about their epoxy bonding processes.

In the words of Daniel D. Zimmerman of the Applied Physics Lab at Johns Hopkins University, “the rumors in support of epoxy have been enthusiastic, but the hard facts just haven’t been available.” For last week’s conference in Washington of the International Society for Hybrid Microelectronics, Zimmerman prepared a paper dealing with compatibility of various epoxies used in hybrid assemblies. He also discussed their electrical and mechanical characteristics when used with nonpassivated chips in thick and thin film.

It’s estimated that 100 of the 500 makers of hybrids in the U.S. have been using epoxies for the past year. At Motorola Semiconductor, the reason is that in eutectic bonding the die has to be mounted in a collet for scrubbing. This often chips or scratches the die. Says Michael Clayton, manager of process engineering at Motorola’s Mesa, Ariz., plant, “Epoxy bonding requires no scrubbing and so yields have increased dramatically.”

National Semiconductor Corp., Santa Clara, Calif., is using epoxy die attach for light-emitting-diode display products. The reason: most LED displays consist of slivers attached to a substrate—a single digit has seven slivers (or segments) and a dot for the decimal point. Thus, eight die-attach operations must be performed; on three-digit clusters, such as those used in calculators, there are 24 die-attach operations.

Pierre Lamond, vice president, engineering, says: “You can’t employ eutectic die attach because the substrate would have to be heated up for too long a time to make all of the bonds, and with eutectic die attach, the slivers tend to float out of position—and in a display, position is critical. But with epoxy, no heating is involved—except maybe for a few minutes at 200° for curing, but this isn’t like the 400° to 800° needed for eutectic—and the die stays put.” An added feature is that the epoxy can be screened onto the substrate assuring precise chip placement.
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<table>
<thead>
<tr>
<th>Frequency Range</th>
<th>50 MHz</th>
<th>200 MHz</th>
<th>512 MHz</th>
<th>3 GHz</th>
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<td><strong>Counters Price:</strong></td>
<td>$1195</td>
<td>$1495</td>
<td>$2150</td>
<td>$2995</td>
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Circle 50 on reader service card
When a nuclear missile warhead reenters the earth’s atmosphere, the electromagnetic radiation from its explosion may be “contained within a hemisphere” of laser beams created by multiple prismatic deflection of the pulsed output of extremely high-power systems operating in the 10.6-micrometer region. This is the encouraging conclusion drawn by U.S. military researchers from experiments at the Army’s White Sands Missile Range near Albuquerque, N.M. If increased funding of the program proves out the concept, it will eliminate the long-standing threat of the EMP effect—the blackout of antimissile radars by the expanding cloud of electromagnetically pulsed radiation that is generated by an exploding warhead and permits later ICBMs to reenter the atmosphere undetected. The program’s potential was reportedly an important consideration in the U.S. agreement with the USSR to limit ABM missiles to 200 per nation.

U.S. military and civil service leaders are upset by National Security Council approval of a plan to begin sharp reductions next year in the number of military and civilian jobs throughout the defense establishment. The aim is to cut back in the number of U.S. bases, to relocate some Washington-area organizations like the Army Security Agency to lower-cost labor markets, and to replace many uniformed employees by civilians.

Goal of the program, which is unrelated to a Vietnam settlement, is to hold down soaring defense personnel costs in order to maintain adequate funding for technology R&D and hardware procurement in an inflated economy. Reportedly scheduled for disclosure in the period after the election but before the convening of the new Congress, the job cuts could reduce defense-related military employment by as much as 20% over a period of a year in the Washington area alone. Defense Secretary Laird, recently conceding that the fiscal 1974 budget now in preparation will exceed the $76.5 billion passed this year, says most of next year’s cost increases will come from pay increases and increased retirement benefits for uniformed military personnel.

A plan to reorganize the White House Office of Science and Technology and the whole science advisory structure is ready for post-election unveiling. Completed some time ago at President Nixon’s request by a task force headed by Patrick Haggerty, Texas Instruments chairman and close Nixon associate, the plan gives equal prominence to industrial use of technology and the academic interests of pure science.

The reorganization will replace the single science adviser to the President, a post now held by Bell Laboratories alumnus Edward David, with a council headed by a troika representing the interests of industrial technology, science, and engineering. Candidates for the new top jobs include Bell Labs president William C. Baker, now chairman of a science and engineering council of the Committee for the Re-election of the President, and William Magruder, a special consultant to the President who got mixed reviews in earlier assignments as director of the New Technological Opportunities Program and as overseer of the defunct supersonic transport effort.
Washington commentary

The problem of peace

Whether your first reaction to Henry Kissinger's White House briefing on a Vietnam settlement was a positive "Peace, at last!" or a querulous "Peace, at last?"—and there were more of the latter in his Oct. 26 audience—the inseparable political and economic possibilities demand examination. To restrict that look to no more than technology in general and its electronics community in particular would be ludicrous—as absurd as attempting to examine the future of America without looking at the rest of the world.

It is an absurdity born of electronics technology. Who can dispute, for example, that communications satellites, which daily brought the horrors of war into America's living rooms in living color, made a major contribution to the evolution of Vietnam as a major political issue? Unable to escape it, citizens were obliged to think about it. That technology was not available when the United States first began its Vietnam adventure more than 16 years ago.

No short-term threats

Current Washington estimates are that a Vietnam settlement will be as protracted as that of the Korean War, despite the different circumstances. Yet most of the spending cuts associated with military electronics for Asia have already come. Over-all defense costs for the war will run to $7.1 billion in fiscal 1973, the Pentagon points out, about one-quarter of the fiscal 1969 peak. Some significant cuts are still to come in some areas—ordnance, for example, and its microelectronic fuzes and laser guidance systems—yet industry expects offsetting outlays to replenish inventories in antisubmarine warfare, tactical and strategic communications, and strategic weapons in general.

Management members of the Electronic Industries Association concluded at their annual Government market outlook on Oct. 31 that there will be a steady but conservative period of growth in the military market through 1980 that will maintain pace with inflation but not much more. Drawing heavily on Pentagon estimates of the economic crunch [Electronics, Aug. 28, p. 25], as well as inputs from EIA's top military members, Sylvania Electronic Systems group marketing chief Clifford Bean concludes that Government contracts' electronic dollar growth will match forecast inflation, maintaining the Federal position as the largest market for technology, even though it is no longer viewed as an expanding one.

For industry that must therefore look to public non-Government markets for growth, there are some problems. Such business is more fragmented and less uniform in both its industrial and consumer segments. It is a business that presidential science adviser Edward David defines as one where "the human aspects of technology become much more important." And its base is a "worldwide public in many cases."

The American image

However, the expansion of that base by U.S. electronics industries that can now see beyond national boundaries faces problems more severe than market fragmentation requiring increased venture capital. Those problems are the long-term consequences of the rootless pragmatism of unilateral international actions by the White House. They are actions ranging from the melodrama of a presidential trip to China to the international monetary negotiations of a year ago that were pulled without warning like rabbits from a hat—actions that left much of the world believing that U.S. policy is erratic and egocentric and that its principles are no more than self-serving.

They are actions that have left Japan, labeled "our most important ally" by President Nixon in February 1971, with the feeling it had been betrayed when it learned a few months later that Henry Kissinger had been negotiating secretly with China's Chou En-lai preparatory to a visit to Peking by President Nixon.

Similarly, the President's decision later last summer to unpeg the dollar from gold and slap a 10% surcharge on imports was a unilateral move, taken without prior consultation with allies who believed it a violation of existing trade agreements. And that action, designed to improve the American trade and payments balances that had been turned into deficits by the drain of Vietnam, left allies such as Canada and with a larger U.S. trade deficit of its own as it moved toward its own national elections. Canadian officials, who contend they have yet to recover, are now more inclined to view the United States with mistrust, rather than as the mainstay of world stability.

These are the serious intangibles that electronics and other technologies seeking to diversify their world base will have to face in the months and years ahead. They are admittedly less easily dealt with by engineers and their managers than are the problems of manufacturing and marketing and their capital requirements. Yet they are part of the package that will come with peace.

—Ray Connolly
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HiNIL offers MSI. Included in the Series 300 are such complex functions as BCD to decade decoders and drivers, Nixie® drivers, decade and hexadecimal counters, a quad latch and a 4-bit comparator.

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Color-TV player shows single frames and uses audio cassette

The best markets for video tape recorders today are in education and sales applications. And Matsushita Electrical Industrial Co. is betting it can expand this market many times with a new type of color television cassette player that gives one still picture every 3.6 seconds. Developed by engineers at the Wireless Research Laboratory, the player uses a standard Philips audio cassette, but with two video tracks running in the center of the tape between the usual audio tracks.

For applications where continuous motion is not really necessary, this system can provide up to 1,000 separate pictures on a standard 1-hour cassette, which operates 30 minutes in each direction. Although Matsushita now can only guess at the program costs, it estimates they will run between 5% and 10% of standard video tapes. It says that in Japan, unrecorded video tape costs about $30 an hour, while blank audio cassettes sell for between $1.67 and $3. Matsushita also says it will try to sell the color cassette player at 50% to 66% the price of a color video tape recorder.

**Tracks.** The tape in the standard audio cassette is 3.8 millimeters wide. If stereo, it has two 600-micrometer-wide tracks in either direction for stereo, but if monaural, it may have only one double-width track in either direction. A guard band 600–700 micrometers wide separates the directional tracks, and it’s in this space that Matsushita puts the two video tracks, each 200 micrometers wide. These tracks are played back by heads whose speed with respect to the tape is somewhat more than 10 meters per second, about the same relative speed as in usual video tape recorders. The video signal frequency format is similar to that used in helical-scan video tape recorders.

**Slide show.** Using a standard Philips cassette, Matsushita single-frame color player sends both audio and video signals to a TV set.

The drum carries three video heads spaced equally around its periphery. It is designed to allow an air film to form between tape and drum, reducing the drag on the narrow tape. The drum rotates 20 times a second. Switching circuits permit playback in succession from the three heads giving an output at the standard rate of 60 fields per second. Since all heads reproduce the same track, though, the fields are not interlaced, and the vertical resolution is lower than for standard video tape recorders.

**Transceiver ends “helium speech”**

The “helium speech” distortion that plagues divers breathing a no-nitrogen helium-oxygen mixture is due to an upward shift of the vocal tract’s resonance frequency. The speech’s resulting Donald Duck quality often confuses underwater communications.

The various attempts to solve this problem with voice unscrambling techniques or channel vocoder principles unfortunately calls for fairly bulky and expensive equipment—and even then the human voice cannot be faithfully reproduced. But now, under a project sponsored by West Germany’s Ministry for Science and Education, researchers at AEG-Telefunken’s laboratories in Ulm have come up with a small inexpensive unit that can restore helium speech to the naturalness of telephone speech.

The new equipment uses delta pulse-code modulation, where only the difference values between two subsequent signals are processed, obviating the need to handle individual signal content as a whole. The difference values are quantized and coded before transmission.

The Ulm researchers have implemented their approach in a prototype two-way intercom system that is made up of a pair of identical transceivers, each no larger than a pocket radio. By using integrated-circuit and multilayer-design techniques, the company says, it can reduce the transceiver’s dimensions to cigarette-pack size.

---

**Electronics**/November 6, 1972
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It's called the Strippable CIP. The new CIP/2002 is the minimum hardware framework from which you can build your own minicomputer. You get only the basic components you need to build your own dedicated system. The CIP/2002 can save OEM users considerable cost because all but the most essential hardware has been stripped away. Only the control board, two data boards, and the frame remain. This allows the system builder to use the power of the minicomputer creatively. Incorporating and adapting the unit to your needs is vastly simplified. Best of all, the variety of options lets you pick just those you need. You don't pay for "frills" you don't need. And the price is very low as a result.

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Philips proposes cassette changes for high-energy tapes

Philips Gloeilampenfabrieken has launched a bid to standardize compact consumer cassettes loaded with chromium dioxide and similar high-resolution tapes. The Dutch company, through the Netherlands delegation to the International Electrotechnical Commission, proposed at a late summer subcommittee meeting that time constants for high-energy tape be standardized at 70 microseconds and 3.180 microseconds. These constants—times at which recording correction networks switch in or out—compare to 120 and 1.590 microseconds for regular tapes.

Philips has paired with the time-constant proposal a second one covering the cassettes themselves. It calls for sensing holes in the rear edge of the cassette, alongside the knockout lugs already there to prevent inadvertent recording over a previously recorded tape. For cassettes loaded with high-energy tapes, the added holes would make possible automatic switch-over from standard correction characteristics to high-energy characteristics. Philips and the West German tapemaker BASF already use the added holes, and Philips thinks it's a sure thing that IEC will adopt both proposals.

Sweden moves to back native computer maker

The Swedish government is negotiating with Saab-Scania AB on formation of a joint development company in the computer field. This move is part of a surprise decision that gives Saab-Scania a contract for two military computers, despite strong recommendations by the defense department that the order go to IBM [Electronics, Oct. 9, p.65]. Details on the development company plans were not given, but it has been known that the government is interested in working out deals with private companies to give support in fields where large investments are needed to keep Swedish industry internationally competitive.

Toko, AMS to trade memory know-how

Toko Inc. and Advanced Memory Systems Inc. have received Japanese government approval for an exchange of semiconductor- and plated-wire-memory know-how. Toko has been in plated-wire memories for over 10 years, and is the leading independent manufacturer in the field, supplying memory stacks and systems to various computer manufacturers all over the world. AMS has been a leader in semiconductor memories in the U. S. and is now selling devices and systems worldwide.

Toko plans to produce memory chips under license from AMS at Kyodo Electronic Laboratories Inc., a subsidiary. Toko will package the devices and build the packages into memory systems at its own memory division. AMS intends to explore expansion of its product line with the addition of Toko's plated-wire memories.

British develop film sensitive only to electron beam

Researchers at the Runcorn, Cheshire, laboratories of Imperial Chemical Industries Ltd. have developed a film sensitive to an electron beam but not to light. It produces an instant image with no wet processing and with resolution similar to high-quality silver halide film—about 1,000 lines per millimeter at 30% contrast transfer function. Thus, the technique should make possible real-time recording on film of electronic-
ally generated data without the usual optical stage. Initially the film is yellow; the exposed areas turn blue. The main snag to development now is that beam power required is relatively high: about $2 \times 10^{14}$ electrons per square inch. But ICI is actively investigating marketing possibilities.

Sony Corp. is stepping up production of the company's video cartridge player, the U-Matic. The corporation is opening a new plant in Japan to produce 100,000 players in 1973. Production for 1972 was scheduled at 40,000 units. The increase is credited to the success of the U-Matic during a test-bed year. In June, the only other commercially available video player, Cartridge TV Inc.'s Cartrivision, was introduced to the consumer market.

If final tests work out all right, an entirely digital transatlantic television standards converter built by Britain’s Independent Broadcasting Authority will get its first operational use this week. Several European broadcasting organizations in the European Broadcasting Union hope to use it to convert their coverage of the U.S. presidential elections. The tests include the ability of the converter to produce a Secam-compatible output as well as PAL signals, which are already proved.

The system uses eight-bit quantization and a 10.7-megahertz sampling frequency. To convert the U.S. 60 fields per second to the European 50 fields per second, the digitized equivalents of the five consecutive field pairings in six consecutive U.S. fields are used to construct by interpolation five fields that together last the same time. Similarly, an extra line is added to the 525-line picture approximately every five lines by interpolating from the digital equivalents of the three surrounding lines in each interlacing field. IBA engineers maintain that compared to the two other existing conversion techniques—electronic analog developed by the British Broadcasting Corp. and optical by Fernseh of West Germany—their digital system has less noise, better resolution, and fewer scintillation effects on sloping edges. It should also cost less and need no setting up. IBA will follow the present one-way converter with a two-way machine and license manufacturers to make them for sale.

The automotive electronics market is getting a boost of sorts, now that a West German car accessory maker has started large-scale production of quartz clocks for dashboard installation. The new clocks, from VDO Adolf Schindling GmbH, a leading European dashboard equipment producer, are for all Mercedes-Benz cars now being made, but can also be fitted in certain BMW models. VDO says other car manufacturers are considering using its quartz clock in the near future.

The VDO clocks contain an integrated circuit that incorporates an oscillator, several divider stages for frequency reduction, and an output stage for the synchronous motor. All active components in the power supply are also integrated. Under normal ambient temperatures the clocks have a time deviation of less than 1 second per day. The company says the new clock sells for about $21 if exchanged for a conventional car clock.
goes where hands can’t

ties in less than a second

adjusts automatically to bundle diameter

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We’ve eliminated hands from the wire tying and harnessing operation—the tool does it all. Now the operator simply applies the tool to a wire bundle, squeezes the trigger and a nylon TY-RAP® Tie feeds itself around the bundle, tightens to a preset tension, locks securely and the excess nylon is neatly snipped off flush to the tie’s head . . . in 8/10 of a second. There is no tool adjustment needed regardless of bundle diameter from 1/32” to 5/8”. The tool is cartridge loaded with 50 standard ties.

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Features: 1,500 V Isolation
200% Transfer Ratio

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Variable Speed Control for Induction Motors
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  - 55°C to +125°C
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- Temperature range: 
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  - 55°C to +125°C
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Pin for pin compatible with CD 4012A.

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- Low power: 1nW
- Temperature range: 
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  - 55°C to +125°C
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TERADYNE
Electronics will add zip to mail

Multibillion market is seen for processing gear; manufacturers build automation equipment for mass-mailing firms and post offices

by William F. Arnold, Aerospace Editor

After years of planning and testing electronic mail-handling equipment, the U.S. Postal Service (USPS) is on the verge of spending an estimated $2.4 billion during the next six years for electronic and electronic-related equipment. This equipment, being sought to speed up service and cut costs, includes computers, mini-computers, optical character readers, code and address readers, sorters, and cancelers.printers.

The electronics gear is part of a $6 billion modernization program that the USPS board of governors is expected to approve, possibly by December, says Harold F. Faught, senior assistant postmaster general, Mail Processing group. Contracts are expected to go out for the first equipment within a year, adds Kent H. Comegys, manager of the Code-letter Mail Systems division.

But the market doesn’t end with the Post Office. Automation of the postal system will create a revolution in the mail rooms of large-volume mailers, such as telephone, insurance, and credit-card companies. By using electronic equipment to address, encode, sort, and further process their bills, these mailers can cut down the time it takes for their customers to receive and pay their bills, explains E. E. Lang, advanced postal systems manager of the Garland, Texas, divisions of E-Systems Inc., a postal equipment maker [Electronics, Sept. 11, p. 30].

What’s more, postal officials are considering preferential treatment for volume mailers who encode and sort their mail before sending to the post offices. Because 75% of all letter mail is “major-mailer-generated,” Comegys says that USPS is urging mass mailers to cooperate by adding a binary bar code in the address area of all envelopes. Precoded originating mail processors (POMP) at the postal centers will read and transfer this bar code to the lower right-hand portion of the envelopes for standard processing.

Toward that end, Cincinnati Bell Telephone Co., Ohio Casualty, Blue Cross, and United Shield are cooperating in an experiment for the Cincinnati Postal Service test bed. Participants are developing computer programs so that the bar code can be formulated for each piece of mail, and they are modifying high-speed printers to handle the additional bar code. USPS is asking companies to add the bar code to return envelopes, which make up 10% of the total mail stream.

The bar-code reading technique is to be added to the sorting system already under test. The entire program is built around two systems—one for bulk mail and the other for preferential—or letter, mail. Most of the electronic equipment will be used in the $4 billion preferential-mail network that will include 180 to 200 regional mail centers, Faught explains.

First preference. The basis for the preferential-mail centers is the letter-mail code-sort system (LMCSS) now in operational development at Cincinnati. The LMCSS is set up as a three-tier system for processing mail. The first tier consists of reading and processing bar-coded letters; the second is reading the address, extracting, and printing the code; and “the court of last resort,” says Comegys, is manual intervention, whereby an operator sitting at a code desk encodes pieces that are rejected by readers.

LMCSS can use any of several systems. One built by the Rohr-Plessey Co., Clark, N.J., is being tested at the Cincinnati post office. The integrated mail-prep system, which routes mail into the three tiers described earlier, is controlled by a Digital Equipment Corp. PDP-14 minicomputer. The $200,000 prototype system has an air culler, direct-feed system, single output facer-canceler, code detector/reader, and a transport system to funnel mail at a fast clip. Andrew Morrison, program manager, predicts that the entire market for postal automation equipment will be in the billions during the next five years.

Already the number of companies producing equipment for postal services and large mailer markets is sizable. In addition to Rohr-Plessey and E-Systems, they include A. B. Dick, Chicago; Burroughs Corp., Paoli, Pa.; Data Card Corp., Minneapolis; Business Machines division of Kenco Corp., Cherry Hill, N.J.; IBM Federal Systems Center, Gaithersburg, Md.; NCR Postal Systems division, West Columbia, S.C.; Pitney-Bowes Inc., Stamford, Conn.; Philco-Ford, Willow Grove, Pa.; US Envelope Mail Systems divi-
Probing the news

sion, Homestead, Fla.; Fairchild Industries, Pasadena, Calif.; Postal & Data Systems Corp., Fairfield, N. J.; Xerox Corp., Rochester, N. Y., ITT Corp., New York City, and FMC Corp., Santa Clara, Calif. And just this month Emerson Electric’s electronics and space division, St. Louis, Mo., was awarded a $4 million contract by the USPS to design, manufacture, and install two computerized printing systems for routing mail to post offices.

Optical precision. These companies produce a wide range of mail-handling equipment. But one of the toughest technological problems they face is developing the optical character readers to read addresses and sort letters. The OCRs have to read 240 different type fonts, and check misspellings. Advanced OCRs by Recognition Equipment and IBM’s Federal Systems Center are being tested by postal officials in New York City. Philco-Ford also has its OCR-2 under test in Boston.

The advanced OCR is designed to read and sort up to 86,000 envelopes an hour by mail carrier, building, firm, or post office box number. In addition, it can sort outgoing mail by city and region without using zip-code information. The equipment searches a 2.9-in. band on the face of an envelope to see if there is a machine-printed address block, explains J. L. Poitevent, vice president for postal marketing at Recognition Equipment. At the read station, two types of logic are combined: template matching (which compares the unknown character with prestored patterns) and feature analysis (which compares combinations of features, such as stops, intersections, and curves to a matrix). “We use both techniques and send the results through a voting algorithm,” says Poitevent.

The Postal and Scanning Systems Operations group of Philco-Ford has supplied 21 of the 23 OCR units now used by the Postal Service. In addition, Philco has an $84,500 contract to modify two of its OCR-1 mail-sorting devices being used by the New York City post office to read bar codes as well. And, it is possible, says Frank A. Teklits, manager of Philco postal systems engineering, that all 20 of the company’s machines will be modified to read bar-code addresses.

Also being developed by the company—this time with Philco’s own funds—are a dedicated bar-code reader and a solid-state scanner to replace the flying-spot scanner tube used in the OCR-1 and OCR-2 machines. The bar-code reader has been breadboarded in the laboratory and should be brought to market in early 1973, says market planner Charles Bradley.

A new step in automation is the computer-driven carrier sequencer. One such unit, built by Burroughs, is now being tested by the Postal Service, but the USPS will go out on competitive bid when it is ready to buy production models, Comegys says. The carrier sequencer receives already encoded and sorted mail and then re-sorts the mail in accordance with the way a letter carrier walks his route.

Code readers, a hot item. Code readers will be installed throughout the system to cull out precoded mail from the mail-prep system, verify already encoded information in the code-sort OCRs and the POMPs, and process mail in the carrier sequencer. Fairchild Industries, FMC Corp. and Postal & Data Systems already have provided the USPS with prototype systems, Comegys says.

Postal and Data Systems, a 2½-year-old subsidiary of Intelcom Industries, has three readers differing in such parameters as fields of view, error rates, and the ability to distinguish bars printed with various inks and paper. The price of the readers ranges between $3,000 and $10,000, depending on quantity and the versatility desired, says Geoffrey Haigh, director of electro-optics.

All of the readers are solid-state, using as a reading element a monolithic array of silicon diodes. Letters move past the array at 200 inches per second, equivalent to about 15 mail pieces per second.

Six in a second. FMC Corp. derives about 30% of its business from postal service contracts, according to David G. Curphey, manager, Controls group. The most successful product, says Curphey, is the bar-half-bar code reader, which can read six letters per second, six times faster than a human. Curphey says that the new technology involved in the code reader is called “interpreting”—the reader uses code-tracking logic that allows the reader to determine what mail is readable and what is not. The machine decides where each pile of mail is to go, depending on how it was addressed.

FMC has four code readers undergoing field tests in Cincinnati, and one in New York City’s main post office. FMC hopes to sell about $4 or $5 million in mail sorters, says Curphey. This year, though, the company hopes to reach the $500,000 level, he says. Curphey calls the code mail-sorting system the “hottest thing going” and the best funded because of its widespread acceptance by postal officials.
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**Sprague Catalog Number Resolution Settling Time to ±1/2 LSB (μs) External Reference Voltage Full Scale Output Temp Coef. (°C/ppm) Unit Price (1-24)**

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<th>Full Scale Output</th>
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**4-QUADRANT MULTIPLYING(2)(3)(4)**

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<td>3</td>
<td>57.59</td>
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Electronics / November 6, 1972

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World Radio History
Firm wins calculator gamble

Bowmar Instrument, unable to sell its LEDs, put them in its own calculators and got a jump on that market; sales have doubled since '71

by Gail Farrell, Boston bureau

Two thousand pocket-size calculators a day come off the assembly line at Bowmar/ALI, Acton, Mass., reportedly the world's largest producer. Yet it was only a year ago that Bowmar decided to enter the consumer calculator market.

"We never dreamed in our wildest dreams it would be as big as it is," says Charles Krakauer, Bowmar/ALI president. The calculator is the first consumer product turned out by Bowmar Instrument Corp. of Fort Wayne, Ind., which was founded in 1951 by Edward A. White when he was 23.

The company's original product line was tiny, high-precision gear trains and counters for the aerospace industry. By 1962, following the purchase of a potentiometer manufacturer, sales were at $13 million. A year later, the industry fell on hard times, and White was forced to close some plants and take "some wicked losses."

In 1961, however, Bowmar had already started placing outside research and development contracts for solid-state displays. By the mid 1960s, these orders led to the establishment of an optoelectronics facility, Bowmar Canada Ltd., Ottawa, Ontario. And this company became Bowmar's springboard into calculators, the product that is largely responsible for Bowmar's fiscal '72 sales of about $26 million.

During the early 1960s, Bowmar also acquired Acton Laboratories Inc., makers of telephone instrumentation equipment and data-transmission testers; this became Bowmar/ALI. Last year, when it came to making a decision about calculators, Krakauer says that White "was willing to gamble; it was like 'bet your company.'" That gamble has paid off, and Bowmar now finds itself in the enviable routine of being able to sell as many units as it can make—the only immediate limit to its growth appears to be availability of parts.

Light on LEDs. Ironically, Bowmar is a major cause of the shortages of light-emitting diodes and MOS LSI circuits that now plague the calculator industry. Bowmar, however, isn't suffering from shortages because Bowmar Canada supplies most of the LED displays. Bowmar/ALI also depends on LEDs from Monsanto and Hewlett-Packard.

And long before LSI chips had become a supply problem, Bowmar had contracted with TI to supply a chip containing a 3,520-bit read-only memory, a 182-bit random-access memory, a decimal arithmetic logic unit, and control, timing, and output decoders.

This chip, made to Bowmar's specifications, is at the heart of the Bowmar 901B calculator, but the LEDs are the reason for its existence. In 1970, Bowmar Canada was ready to make production quantities of LEDs, but Bowmar chief Ed White couldn't find anyone to buy them. White tried to push the idea of using LEDs in such hand-held devices as calculators and meters, but "U.S. and Japanese calculator makers could buy a vacuum-tube display for 54 cents, while ours cost $2."

So he and Krakauer decided to make calculators themselves in the Acton plant. "We built a few by hand, estimated the cost, and concluded, here's something people can use," recalls Krakauer. "The big companies said it would never sell, and when I heard that I was tickled to death."

By May 1971, Bowmar had some samples ready to show New York retailers who received them favorably. Production went full speed ahead, and the first units were sold last October.

In August, Bowmar/ALI started producing the 905 calculator to be sold under the Sears logo for $99.95. The $119.95 price on the earlier 901B model has been reduced $20 by using fewer components and reducing the amount of wiring.

Even though Bowmar was early into the market with the personal calculator, company officials realize that the Japanese would be strong competition before long. However, Krakauer doesn't regard

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**Probing the news**

Electronics/November 6, 1972

the $60 calculators made by Japan's Casio and Busicom as direct competition. "These have only six digits, no decimal point, and they are larger than pocket size," he says.

In contrast, the Bowmar calculator is a four-function machine that performs chain or mixed multiplication and division. It has eight digits for entry and readout, full floating decimal point, plus or minus sign capability, and indicators that denote power on, low battery, overflow, error, and negative result. It measures about 5x3x1 in.

Bowmar does not intend to respond to Japanese units by cutting its prices. When and how far down the price goes, Krakauer says, is a function of what the components makers do. Bowmar/ALI marketing manager James White says that his firm has offset the low labor rates of the Japanese by designing the calculator with a minimum number of parts for maximum production automation. Bowmar keeps unit production time to about an hour.

**Meanwhile, in the U.S. . . .**

There's also the matter of American competition. North American Rockwell Microelectronics Co. is supplying Sears, Bowmar's star customer, with a desk-top machine having a liquid-crystal display for $99.95. But because the machine is a desk unit, Bowmar officials don't consider NRMEC a competitor even though the price is the same as the hand-held Bowmar 905 calculator Sears is selling.

But other competitors have stung Bowmar's stock, if not their sales. TI has come out with a hand-held unit and Solitron Devices Inc., San Diego, Calif., expects to market a pocket-sized calculator by the end of the year.

According to Research Institute Investors Service, New York, Bowmar's stock rose from a low of 11 1/4 in February 1972 to a peak of 46 3/4 in August. Then, the stock fell back 50% "as concern over the effects of competition mounted."

As for TI competition, Krakauer says, "We were smart enough to see the market in the first place. We feel smart enough to handle TI."

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Probing the news

Kraakauer. But starting in January, the 905, now being made only for Sears, will be marketed through all Bowmar distributors. Recalling early days, Jim White points out, "When we got to the place where we knew we had a good product, we realized we didn't have the knowhow to sell it." So rights to distribute to electronics outlets were granted to the Craig Corp., Los Angeles, which markets the calculator under its name. Star Case Inc., of New York also markets Bowmar units to quality consumer stores, as well as special models that were made for Commodore Business Machines.

Calculator sales are having a salutary effect on Bowmar's employment record and its earnings. The number of people employed at Bowmar/ALI has quadrupled in the past year and a half. Sales for fiscal 1971 were $13,353,000, with net earnings of $333,000. In the first nine months of fiscal 1972, which started in October 1971, when the calculator was introduced, sales were $20,093,890, and earnings were $801,655. White says sales for 1972 are "over twice the sales of last year."

Future. No one at Bowmar is willing to estimate how large the potential market is. Kraakauer says. Some equate the sale of personal calculators with the sale of portable typewriters, which is 2.5 million a year. A figure of 4 million units is predicted by Jay Rodney Reese, vice president of TI's Solid State division. He says the average price will be $100 each.

Bowmar's Jim White agrees with TI's Reese and Tadashi Sasaki, executive director of Japan's Sharp Industrial Instruments division, that the consumer calculator market is nowhere near saturation. And Bowmar/ALI will soon introduce a 10-digit machine and a desk-size model.

"Given our 'druthers,'" says Kraakauer, "we want to provide machines to consumers and expand our production line to business purposes, single-memory calculators, and hard print-out. We're trying to bring high technology to the consumer marketplace."
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Fairchild Systems

Electronics/November 6, 1972

Circle 75 on reader service card
Medical engineering: prognosis fair

Because of their financial structure, few hospitals can now afford bioengineers; new health care laws should open jobs there and in industry

by Paul Franson, Los Angeles bureau manager, and John N. Kessler, Associate Editor

Medical engineering, once prescribed as a cure for aerospace unemployment, needs nursing by the Government before it achieves real vitality. And even then it faces career problems.

While nearly four million people are employed in health care, only 4,000 of these are engineers, reports a recent U.S. Department of Labor study conducted by the National Society of Professional Engineers, Washington, D.C. Nor will many more than 1,000 of the 65,000 unemployed engineer-scientists from aerospace find jobs as medical engineers over the next three years, the society adds.

The key to the rapid growth of medical engineering as well as health care delivery services lies with Congress, says Charles W. Garrett, executive secretary of the committee on the interplay of engineering on biology and medicine, National Academy of Engineering, Washington, D.C. “One of these days,” he says, “Congress is going to pass a bill creating and funding national health care delivery service.” Such legislation Garrett believes will provide the influx of dollars that will, in turn, create a market for medical engineers.

Obstacles. The major problem at the moment is the way in which payment for hospital services is structured. As Clifford D. Ferris, acting director of the bioengineering program at the University of Wyoming in Laramie, points out, “a smaller hospital cannot afford to hire a medical engineer.” Garrett explains an engineer’s costs come out of a hospital’s overhead—and the hospital administrator is concerned with cash flow from third-party insurers, which does not affect overhead but would absorb any cost savings effected by the engineer. But this will change radically when legislation for national health care delivery services is passed by Congress.

The second factor that will expand medical engineering, Garrett believes, is medical device safety legislation. Right now, the Food and Drug Administration is embarking on a program for developing standards for medical device safety. When these recommendations are incorporated into a law, hospitals will be required to employ medical engineers if they use electronic equipment.

The third factor, says Garrett, includes the whole range of health care maintenance organizations which are just beginning to be established. These, typified by the Kaiser Foundation Health Plan in California, will increase as the Federal Government, community groups and unions push for the amalgamation of medical services.

The time frame for significant growth, in Garrett’s opinion, is about five years. Today, there are about 160 academic institutions which offer programs in biomedical engineering, according to the Institute of Electrical and Electronics Engineers’ group on biomedical engineering. And the total opportunities this year for employment in this field are only 395. But by 1973-75, thanks...
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probing the news

largely to growth in instrumentation and appliance manufacture, employment opportunities will grow to 2,955, to quote estimates from the National Society of Professional Engineers report.

Consequently, the Federal Government’s retraining programs will have an insignificant impact on medical engineering—not only because of the few people opting for retraining, but because of the inherent limits on employing medical engineers today. And beyond the fact of numbers, is the scope of education required for biomedical engineers. As Ferris at the University of Wyoming puts it, “The problem with retraining aerospace engineers is that their training has been in a very narrow field. Bioengineering is very broad, requiring knowledge in physics, basic engineering, and biological sciences.” Ferris feels that younger engineers can be successfully retrained, but that it is more difficult with older engineers who “have forgotten a lot of the basics.”

Two programs. Two retraining programs in biomedical engineering specifically for unemployed aerospace engineers have recently been conducted under the sponsorship of the U.S. Department of Labor. One, taught at Los Angeles Valley College in California and directed by Bruce S. Angwin, has found jobs for most of the 15 engineers enrolled. Participants were virtually assured of jobs by lining up employers before the course, and were provided with subsistence living costs, transportation, and other costs. The nine-week program has been completed so recently that conclusions are hard to draw, but Angwin regards the course as a prototype that he hopes will lead to retraining on a larger scale in the future.

The other program started this fall at two colleges in Florida. Marvin Olsen, a TRW executive, is coordinating it as the on-loan executive director of the regional Environmental Training and Research Organization Inc., Cocoa, Fla. “We are banking on a broad engineering background that can be utilized, plus courses to fill in those areas needed for specific jobs in medical engineering,” says Olsen. He emphasizes that students spend 40 hours on campus, and that the training is rigorous.

At Florida Institute of Technology in Melbourne, 19 students are enrolled in a program of medical systems engineering, aimed at developing managers who can evaluate the computer needs of hospitals and recommend and implement EDP systems.

Nineteen students are also enrolled in the medical data-processing supervisor program at Brevard Community College, in Cocoa, Fla., which is training technicians to evaluate hardware and integrate a system of minicomputers and computer terminals with a central computer. Also at Brevard is a program aimed at former aerospace technicians; the 15 students look forward to careers as biomedical equipment-repair technicians—who can maintain and repair electronic equipment, such as electrocardiographs and blood cell counters.

Each program is to run for 34 weeks, and Olsen says there will be much more emphasis on the placement of engineers than is the case with most engineering colleges. Studies have been made of the needs of various local hospitals, he explains, adding that better than 95% of engineers in similar retraining programs in environmental control have found jobs.

On the job. Once an EE gets a job in bioengineering, his biggest need, says Bruce S. Angwin, medical-engineer-program director, technology utilization project, National Society of Professional Engineers, is to learn the language of physicians. Also needed is a certain amount of anatomy and physiology, and an understanding of the way the health field is organized.

A basic problem is that biological systems seem foreign to the typical physical engineer. “Not only are biological systems very complex,” says Bruce A. Barkalow, bioengineer at Sutter Community Hospital in Sacramento, “but their basic nature is little known. Much research and practice in medicine involves trying to analyze simultaneously varying data while attempting to find patterns and causes, unlike physical phenomena, where

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Principles are generally understood.

Experiences of engineers who work at hospitals differ considerably. Barkalow, a 30-year old Ph.D., finds his work interesting and satisfying. Among his experiences, he mentions, “We can modify existing equipment to meet current legal and medical standards. Before, the hospital had to throw it out and get new equipment, an expensive proposition. Alternatively, we can pick industrial equipment that is cheaper and often more suitable.” He says that relations with the MDs are good, particularly since Sutter is a community hospital where the atmosphere is not academic. “It hasn’t been a real problem. We have to work with them and show them how we can solve their problems. The demand from physicians sold the administration, in fact.” Having a Ph.D. helps, he admits, but he feels that interest in the work is the most important trait a bioengineer can have.

Less enthusiastic is Donald L. Behrendt, who describes himself as a “typical refugee from 20 years in aerospace,” and who is working—on his own time and money—for a master’s degree. Behrendt contends that professional engineers don’t fit into hospitals. For example, he finds it hard to convince the administration and researchers of concepts that are widely accepted in the electronics industry, like periodic calibration of instruments, or the need for continuing education or conference attendance.

Why not try a minicomputer?

Behrendt also mentions a researcher collecting vast quantities of analog data on instrumentation recorders, then laboriously analyzing it by hand, when a system based on a minicomputer would be much cheaper and more efficient. Yet in spite of recommendations, the man recently bought a $13,000 recorder rather than giving serious consideration to the digital equipment. He finds that, although medical people spend a great time in school, “in spite of what they sometimes think, they don’t learn everything about everything.”

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In addition to speeding resistor throughput, Dale plans to use the System/7 for order tracking and monitoring and control of testing and production machinery.

Full information on the System/7 is available through your IBM representative or local office. Or write IBM Data Processing Division, Department 807-E, 1133 Westchester Avenue, White Plains, N.Y. 10604.
Management

Unity is key to WEMA success

No longer limited to West Coast membership, the 683-member organization boasts a growing list of activities and a growing impact on legislation

by Stephen Wm. Fields, San Francisco bureau manager

While the Electronic Industries Association recently lost one prominent member because of an inability to take a unified industry position on matters like international trade [Electronics, Sept. 11, p. 25], WEMA, the Palo Alto, Calif.-based trade association, has quietly gone ahead expanding its membership and influence. And the key to WEMA’s success has been its members’ common viewpoint, particularly on international trade.

Although chartered as the West Coast Electronics Manufacturing Association in 1943, WEMA has dropped geographical requirements for membership. Now the letters of its name do not even denote specific words, but stand for 683 members and associates allied by a major interest in the future of electronics and its effect on international trade.

This commonality of viewpoint, says E.E. Ferrey, WEMA’s executive vice president, is what has made the organization especially successful in Washington. But there are other reasons for its success:

- WEMA has liberalized its membership requirements and now permits companies in businesses related to electronics—such as banks, venture capital companies, and electronic-components distributors—to join as associate members. And companies producing computer software are allowed full membership.
- Membership in WEMA runs from just a few hundred dollars to a maximum of $1,500—less than what some private consulting firms charge for a salary survey.
- WEMA puts emphasis on what is pertinent to running a business in the form of studies, surveys, and seminars.

WEMA’s impact on Federal legislation is exemplified by the effect of testimony by Earl Wantland, president of Tektronix Inc., Beaverton, Ore., during Congressional “oversight” hearings on the Export Administration Act of 1969. Wantland, sent to testify by WEMA, charged that Government policies were handicapping many U.S. firms in competing effectively in the East European and the new Chinese markets. As a result of this and other industry statements, proposals by Sen. Robert Taft (R., Ohio) to ease the control of electronic exports were added as amendments to the act.

Not limited to Government affairs, WEMA has made available to its members what is considered a benchmark wage and salary survey. It has produced an operations-ratio report, which allows a company to compare itself with others of similar size and product interest, or even by the percentage of sales that are commercial vs Governmental. And an upcoming study will be devoted to executive compensation. Such reports are particularly useful to young companies, which may have difficulty in affording the cost of these studies from private consultants.

Pertinent. How does WEMA determine what is “pertinent” to its membership? The ideas come from committees made up of industry people, not WEMA staff members—although staff people help get things going. For example, a seminar on East-West trade slated for Dec. 12 got started because small-company members don’t know how to do business with the East. In the planning stages is a seminar on the nuts and bolts of international trade—to be explained by executives with first-hand experience who will “tell how to do it,” says Ferrey.

Generally, he says, “the seminars and reports are the result of a melding of ideas. The staff tries to assess suggestions from members and also at board meetings we try to determine what our member companies need.” Ferrey points out that a “financial-affairs committee was set up because of concern about such matters by our members.” Results of this committee were the mergers and acquisition seminar, an upcoming session on the strategy in corporate finance, an annual Monterey conference bringing together small-company executives and securities analysts (see p. 45), and the operations-ratio survey.

Activity. Alan J. Grant, executive vice president at Aerojet-General Corp., El Monte, Calif., and a WEMA vice president, says, “WEMA is a service association to the electronics industries. It provides a forum for key executives to get together and discuss things of common importance.” The WEMA group in Los Angeles, at a recent dinner meeting attended by 400 corporate executives, hosted Soviet embassy officials, who spoke about what the Russians wanted to buy from the U.S., and how to go about it.

R.S. “Sam” Carlson, president of North American Rockwell Microelectronics Co. in Anaheim, Calif., found the meeting “very revealing.” He also finds WEMA’s services useful: NRMEC uses the local compensation studies, operations-ratio surveys, financial studies, and seminars on market strategy, for example.
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Shedding some needed light on optical measurements

To take maximum advantage of recent developments in optoelectronics, it is more important than ever for electronics engineers to master the techniques and terminology of photometry and radiometry.

by Michael A. Zaha, Tektronix Inc., Beaverton, Ore.

Light-emitting diodes, lasers, self-scanned photodiodes, and other optoelectronic devices offer attractive new solutions to many electronic design problems. But they will not be used to their best advantage until engineers have become familiar with the terminology and techniques of light measurement.

Unfortunately, there is more misunderstanding about radiometry and photometry than about measuring any other portion of the electromagnetic spectrum. The difficulty lies not in the basic concepts, which are fairly straightforward, but in deficiencies in terminology—especially in photometry.

To make sense of the situation, therefore, it is best to grasp the underlying theory before attempting to assimilate the sometimes arbitrary systems of measurement. Finally, it also desirable to have some idea of the practical problems that will be encountered in the actual taking of measurements.

Radiometry vs photometry

Radiometry is concerned with the measurement of radiation for all wavelengths within the so-called optical spectrum—that is, ultraviolet radiation, visible light, and infrared radiation. An ideal radiometric detector has a flat spectral response. The basic unit of power in radiometry is the watt.

Photometry, on the other hand, deals only with the measurement of visible light, which falls between the wavelengths of 380 and 750 nanometers. An ideal photometric detector has a spectral response that approximates the response of the average human eye. The basic unit of power in photometry is the lumen.

An occasional complication in photometry is the existence of two average human-eye responses. At normal levels of illumination, the eye's response is determined by the cone-shaped cells in the retina, and the eye is said to exhibit a photopic response. At very low light levels, the retina's rod-shaped cells take over and cause a shift in the response curve (Fig. 1) to what is referred to as scotopic vision. Rod cells are insensitive to color, so that color vision is lost at very low light levels.

Unless otherwise specified, photometric measurements are based upon the photopic eye response, which peaks at 555 nm. At this wavelength, and at this wavelength only, 1 watt of radiant power is defined as the equivalent of 680 lumens of luminous power. (For those people who like to work in the dark, the scotopic lumen has been invented. One watt of radiant power is equivalent to 1,746 scotopic lumens at the peak of scotopic vision—507 nm.)

Converting measurements

To convert a radiometric power measurement into photometric units, the spectral-response characteristics of the human eye and the spectral output of the light source being measured must be taken into account. Then the conversion can be accomplished by multiplying the energy radiated at each wavelength by the relative luminosity factor at that wavelength and summing the results.

Mathematically, total luminous power ($\Phi_v$) is equal to the maximum luminous efficacy factor ($K_m = 680$ lumens/watt) times the integral of the product of the relative luminosity function—$V(\lambda)$—and the radiant-power function—$\Phi(\lambda)$—over the wavelength interval from 380 to 750 nm. That is,

$$\Phi_v = K_m \int_{380}^{750} V(\lambda) \Phi(\lambda) \, d\lambda$$

Notice that this basic equation can be modified for
use with detectors other than the human eye, such as
vidicons and photographic film, by replacing $V(\lambda)$ by
the appropriate relative luminosity function.

Since analytic expressions for relative luminosity
functions are not easy to come by, the basic equation is
usually evaluated by numerical methods, often using a
computer. Graphical methods are occasionally em-
ployed as in the following calculation of the luminous
efficiency of a 48-inch, standard cool white (T-12) fluo-
rescent lamp. (Fig. 2). The spectral output, rated power
consumption, and luminous output (3,200 lumens) for
the lamp can be found in the Illuminating Engineering

The area under the lamp spectral output curve in Fig.
2 is proportional to the quantity of radiant power a ra-
diometric detector would measure. This curve, multi-
plied by the relative luminosity curve of Fig. 1, yields
the curve showing the photometric spectral output of
the lamp. The colored area under this last curve rep-
sents the relative amount of power a photometric detec-
tor would see—that is, the luminous output of 3,200 lu-
mens. The colored area is about 50% of the lamp
spectral output area, indicating that only about one-half
of the lamp's total radiant output is detectable by the
human eye. The total radiant power output is thus:

$$\Phi_r = \Phi_e / K_m \text{ or}$$

$$\Phi_e = 3,200 \text{ lumens} / (50\% \times 680 \text{ lumens/w}) = 9.4 \text{ w, approx.}$$

The lamp thus consumes 40 w of electrical power to
produce 9.4 w of radiant power, half of which the eye
responds to as 3,200 lumens of luminous power (or 4.7
so-called "lightwatts"). The luminous efficiency of the
lamp is thus 47/40, or about 12%. The luminous effi-
ciency figure is only a percentage. If it is necessary to re-
late the lamp's input to its output in lumens, the desired
quantity is the lamp's luminous efficacy. In this case, the
lamp's efficacy works out at 3,200 lumens/40 watts, or
80 lumens/watt.

Sometimes the efficacy referred to is not relative to
the electrical input power, but to the radiant output
power. In the preceding example, this radiation efficacy
would be 3,200 lumens/9.4 w or 340 lumens/w. Obvi-
ously, if all of the power is radiated at 555 nm, the lu-
minous efficiency is 100% and the radiation efficacy is
680 lumens/watt (the equivalent of $K_m$ in the basic
equation).

### Terms and definitions

Since it is almost impossible to collect and measure
the total power output of a source, many terms have
been developed for more limited measurements of
propagating radiant energy. The concepts underlying
these terms are almost identical for radiometry and
photometry; the terminology differs only in that the ad-
djective radiant is used for radiometric terms and lu-
mious for photometric terms.

#### TABLE I: RADIOMETRIC AND PHOTOMETRIC EQUATIONS AND UNITS

<table>
<thead>
<tr>
<th>Definition</th>
<th>Equation</th>
<th>Radiometric</th>
<th>Photometric</th>
</tr>
</thead>
<tbody>
<tr>
<td>Energy</td>
<td>$E = \frac{\text{d}Q}{\text{d}t}$</td>
<td>radiant energy</td>
<td>lumen-sec</td>
</tr>
<tr>
<td>Energy per unit time = power = flux</td>
<td>$P = \frac{\text{d}W}{\text{d}t}$</td>
<td>radiant flux</td>
<td>watt</td>
</tr>
<tr>
<td>Power input per unit area</td>
<td>$E = \frac{\text{d}W}{\text{d}A}$</td>
<td>irradiance</td>
<td>lm/m²</td>
</tr>
<tr>
<td>Power output per unit solid angle</td>
<td>$I = \frac{\text{d}W}{\text{d}\Omega}$</td>
<td>radiant intensity</td>
<td>W/steradian</td>
</tr>
<tr>
<td>Power per unit solid angle per unit projected</td>
<td>$L = \frac{\text{d}W}{\text{d}A \cos (\theta)}$</td>
<td>radiance</td>
<td>W/steradian</td>
</tr>
</tbody>
</table>

*International System of Metric Units

---

1. Shift. The dark-adapted (scotopic) eye has a peak response
about 50 nm below that of the light-adapted (photopic) eye. There is
no color perception under scotopic conditions.
The radiometry terminology that follows is more logical and coherent, and it is illustrated in Fig. 3.

**Radiant energy** \( (Q_e) \) is energy traveling in the form of electromagnetic waves and is measured in joules.

**Radiant power** \( (\Phi_e) \), also called radiant flux, is the time rate of flow of radiant energy. It is expressed in joules/second or watts.

**Irradiance** \( (E_e) \) is the density of radiant power incident on a surface. It is generally measured in watts/square meter.

**Radiant exitance** \( (M_e) \) is the density of radiant power emitted from, transmitted through, or reflected from a surface. It was formerly known as radiant emittance, and is measured in watts/square meter.

**Radiant intensity** \( (I_e) \) is the radiant power per unit solid angle, traveling in a given direction. It is measured in watts/steradian. (By definition, one steradian of solid angle originating from the center of a sphere of 1-meter radius will subtend an area of 1 square meter on the surface of that sphere, as shown in Fig. 4.)

**Radiance** \( (L_e) \) is the radiant intensity per unit area leaving, passing through, or arriving at a surface in a given direction, where the surface area is the projected area as seen from the specified direction. It is measured in watts/steradian-square meter (Fig. 5).

The photometric terminology is exactly parallel (see Fig. 6).

**Luminous energy** \( (Q_r) \) is simply light energy. It is measured in lumen-seconds, where 1 lumen-second equals 1 talbot.

**Luminous power** \( (\Phi_r) \) is light-energy flow per unit time. It is also called luminous flux and is expressed in the basic unit of photometry: the lumen.

**Luminance** \( (E_r) \) also called illumination, is the density of luminous power incident upon a surface. One lumen per square meter equals 1 lux, which is also known as 1 meter-candle. (See Fig. 7 for a comparison of the metric units described thus far and their English equivalents.)

**Luminous exitance** \( (M_r) \) is the luminous power leaving a unit area of surface. It is measured in lumens/square meter. It was formerly called luminous emittance.

**Luminous intensity** \( (I_r) \) is the luminous power per unit solid angle, traveling in a given direction. One lumen of power per steradian is called one candela of intensity.

**Luminance** \( (L_r) \) is the luminous intensity per unit area leaving, passing through, or arriving at a surface in a given direction. The surface area is the projected area, as viewed from the specified direction. Luminance is measured in lumens/steradian-square meter or candela/square meter. Luminance is sometimes called photometric brightness and is a widely used quantity. Five of its main units are:

- 1 stilb = 1 candela/square centimeter
- 1 lambert = 1/\( \pi \) candela/square centimeter
- 1 nit = 1 candela/square meter
- 1 apostilb = 1/\( \pi \) candela/square meter
- 1 footlambert = 1/7\( \pi \) candela/square foot

The footlambert is still commonly used in engineering applications in the U.S.

For a perfectly diffusing surface, luminance can be
5. Radiance. The key to understanding radiance is to realize that its definition refers to the radiant intensity per unit area over a projected surface area as viewed from a specified direction.

6. Photometry. It’s not just the output of a light source that counts. The reader of this page is more interested in the luminance of this paper than in its illuminance or in the power consumption of the bulbs (if any) that provide the light.

Table 2: Illumination Conversion Factors

<table>
<thead>
<tr>
<th>Footcandles</th>
<th>Lux</th>
<th>Phot</th>
<th>Milliphot</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>10.76</td>
<td>0.0929</td>
<td>929</td>
</tr>
<tr>
<td>Lux*</td>
<td>1.00</td>
<td>1.00</td>
<td>1.00</td>
</tr>
</tbody>
</table>

*Recommended SI units.

Table 3: Luminance Conversion Factors

<table>
<thead>
<tr>
<th>Footlamberts</th>
<th>Candela/m²</th>
<th>Millilambert</th>
<th>Candela/in.²</th>
<th>Candela/ft²</th>
<th>Stilb</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.2919</td>
<td>0.929</td>
<td>452</td>
<td>3.142</td>
<td>2919</td>
</tr>
<tr>
<td>Candela/m²</td>
<td>3.426</td>
<td>1.319</td>
<td>1.550</td>
<td>10.76</td>
<td>10,000</td>
</tr>
<tr>
<td>Millilambert</td>
<td>1.076</td>
<td>0.3142</td>
<td>487</td>
<td>3.382</td>
<td>3,142</td>
</tr>
<tr>
<td>Candela/in.²</td>
<td>0.00221</td>
<td>0.000645</td>
<td>0.00205</td>
<td>1</td>
<td>0.0094</td>
</tr>
<tr>
<td>Candela/ft²</td>
<td>0.3183</td>
<td>0.0929</td>
<td>0.2957</td>
<td>1</td>
<td>0.929</td>
</tr>
<tr>
<td>Stilb</td>
<td>0.00034</td>
<td>0.0001</td>
<td>0.0032</td>
<td>0.155</td>
<td>0.00108</td>
</tr>
</tbody>
</table>

*Recommended SI units.

Mission on Illumination (CIE) to standardize the preceding mass of redundant units. Table 1 summarizes the definitions and the International System of Metric Units (SI), which are recommended for use in optical measurements.

Since many other units are currently used in engineering practice, Tables 2 and 3 are provided for convenient reference. Also, to provide an intuitive feeling for photometric units, Tables 4 and 5 present the illumination and luminance of some natural scenes and various light sources.

Practical considerations

Those accustomed to measuring voltages to within 0.01% or better, and who routinely make nine- or 10-place frequency measurements, may be surprised to learn that optical measurements with errors of less than 1% are very rarely made. To get an accuracy within 5% is difficult; a knowledgeable practitioner with good equipment can probably keep his errors between 10% and 20% on a routine basis, but a small error in technique can easily introduce errors in excess of 50%.

Typically, large errors are caused by using detectors (and matching filters) with the wrong spectral response related to luminous exitance, since such a surface will disperse light per solid angle in a uniform and predictable way. It can be shown that 1 lumen/ft² of exitance will yield 1/π candela/ft² (or 1 footlambert) of luminance from such a theoretical surface. Of course, no perfect diffusers exist, but they are the rationale for the luminance terminology.

Attempts are being made by the International Commission on Illumination (CIE) to standardize the preceding mass of redundant units. Table 1 summarizes the definitions and the International System of Metric Units (SI), which are recommended for use in optical measurements.
Confusion. Footcandles—that is, lumens per square foot—replace lux when English units are used. The point that ties it all together is the 4Π factor relating candelas and lumens: a uniform point source with an intensity of one candela will radiate one lumen onto a one-square-foot surface placed one foot from the source.

for the radiation source. It is essential to know the detector's spectral response within the wavelength range of the measurement to be made. A “good” detector may be specified as being “within 1% of perfect (CIE) photopic response which generally means that the area under the detector’s response curve approximates the area under an idealized response curve within 1%. However, this can be misleading, because mismatches at specific wavelengths may deviate considerably more and can cause large errors.

Fig. 8 shows the responses of two detectors to a red LED’s output. The photometric device responds approximately 25% too high, the radiometric detector about 3% high; therefore, errors of +25% and +3% result here from spectral mismatches alone. Moreover, since most photometric detectors are not as accurate at 650 nm as the one shown, even greater errors are likely, unless great care is taken to determine their actual responses. (While photopic detectors exhibiting better red response are available, their over-all response is usually less accurate for general-purpose photometric measurements.)

Additional sources of error come from detector aging and filter deterioration (drifts of 2% per year are not uncommon), nonlinear detector responses, nontemperature-compensated circuitry, and stray light. Periodic calibration is absolutely essential if high accuracy (within 1% to 5%) is needed.

Some direct measurements

The illuminance (or irradiance) of a surface can be measured directly by placing a calibrated detector in the position of that surface. To avoid errors, it is essential that the complete area of the calibrated detector be illuminated, because illuminance is a measure of flux

8. Errors. Even though the photometric detector provides a rather close match to the ideal (CIE) photopic response, it introduces an error of +25% when it’s used to measure the output of a red LED. The radiometric detector shown is only 3% high at the red LED wavelength.
density per defined area. If at all possible, the detector should be oriented normal to the incident flux to avoid modification to the detector’s projected area and to minimize reflections from the filters in front of the detector. If it is not possible to have most of incident flux strike the detector perpendicularly, then an angular sensitivity plot for the detector system must be used to avoid large errors.

Attempting to measure the illumination on a surface by measuring the exitance from it is not recommended because exitance is a function of the surface’s spectral reflectivity. Also it is impractical to collect all of the light without interfering with the incident illumination.

A typical luminance (or radiance) probe works by measuring the incoming light intensity per unit area arriving at a detector surface. The acceptance angle of the detector is restricted as shown in Fig. 9. However, the simple measurement assumes that the external source has sufficient area to fill the probe’s acceptance angle. If it doesn’t, there are two possibilities: either the measurement can be corrected by taking the actual viewing angle of the probe into account, or the source can be treated as a point source and an intensity measurement made, by using an illuminance probe and applying the inverse-square law to calculate intensity.

The second option is never as accurate as the first. Experience shows, however, that when dealing with LEDs and other miniature radiators, much confusion can be avoided by treating them as point sources.

**Some indirect measurements**

Some of the most common optical measurements are not made directly, however. Intensity, for example, is determined indirectly by measuring the illuminance (or irradiance) produced on a test surface. (Remember, the luminance discussed above is measured in lumens per square meter, while illuminance or illumination is measured in lumens per steradian-square meter.) Now, illumination of a surface by a point source of light varies directly with the intensity of the source (I) and inversely as the square of the distance, d, between the source and the surface—that is, \( E = I/d^2 \) or \( I = Ed^2 \). Therefore, if a calibrated illumination detector measures 10 footcandles of illumination at a distance of two feet from a point source, then the intensity of the source is

\[
I = Ed^2 = 10 \text{ footcandles} \times 2 \text{ ft}^2 = 40 \text{ candelas.}
\]

The point source assumed in inverse-square law calculations is seldom encountered in practice. However, an error of only approximately 1% will result if the source diameter is restricted to less than 10% of the distance between the source and the illuminated surface.

This selection of procedures, though simplified, illustrates the ideas basic to optical measurements. The bibliography suggests further reading: the book by Prof. Meyer-Arendt is particularly recommended.

<table>
<thead>
<tr>
<th><strong>TABLE 4:</strong> APPROXIMATE LEVELS OF NATURAL SCENE ILLUMINATION</th>
</tr>
</thead>
<tbody>
<tr>
<td>(Footcandles)</td>
</tr>
<tr>
<td>Direct sunlight</td>
</tr>
<tr>
<td>Full daylight</td>
</tr>
<tr>
<td>Overcast day</td>
</tr>
<tr>
<td>Very dark day</td>
</tr>
<tr>
<td>Twilight</td>
</tr>
<tr>
<td>Deep twilight</td>
</tr>
<tr>
<td>Full moon</td>
</tr>
<tr>
<td>Quarter moon</td>
</tr>
<tr>
<td>Starlight</td>
</tr>
<tr>
<td>Overcast starlight</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th><strong>TABLE 5:</strong> APPROXIMATE VALUES OF LUMINANCE FOR VARIOUS SOURCES</th>
</tr>
</thead>
<tbody>
<tr>
<td>(Footlamberts)</td>
</tr>
<tr>
<td>Atomic fission bomb (0.1 ms after firing, 90-ft-diameter ball)</td>
</tr>
<tr>
<td>Lighting flash</td>
</tr>
<tr>
<td>Carbon arc (positive crater)</td>
</tr>
<tr>
<td>Tungsten filament lamp (gas-filled, 16-lumen/watt)</td>
</tr>
<tr>
<td>Sun (as observed from the earth’s surface at meridian)</td>
</tr>
<tr>
<td>Clear blue sky</td>
</tr>
<tr>
<td>Fluorescent lamp (T-12 bulb, cool white, 430 ma medium loading)</td>
</tr>
<tr>
<td>Moon (as observed from earth’s surface)</td>
</tr>
</tbody>
</table>

**BIBLIOGRAPHY**

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Circle 97 on reader service card
Better understanding of FET operation yields viable monolithic J-FET op amp

Input current in the nanoampere range, together with low offset voltage, enables a monolithic op amp to do jobs that were once delegated to hybrid devices; the result is to bring higher accuracy within the range of less expensive systems

by David Fullagar, Intersil Inc., Cupertino, Calif.

Although monolithic operational amplifiers have been around for almost a decade, the analog designer invariably turns to an expensive hybrid device when he builds a system intended for accurate data acquisition.

Usually it's a two-chip design with junction field-effect transistors to provide low input currents. In contrast, the monolithic J-FET approach has always run into problems of excessive input currents, excessive drift, and faulty biasing techniques.

An improved J-FET circuit design, however, results in a monolithic device that combines the input and stability features of the hybrids at about half the hybrid's price. At last the monolithic J-FET-input op amp can take its place alongside such familiar, all-bipolar products as the 741 and the 101A. It should all but replace modules in op amp applications such as log and antilog amplifiers, photocell amplifiers, peak detectors, sample-and-hold circuits, high impedance buffers, and active filters.

Why J-FETs?

The J-FET input can operate with extremely small input currents, plus fairly low offset voltages, which can be nulled to zero. Such conditions allow small signals to be detected with practically no distortion. In two-chip hybrids one chip is used for the input and a second for the rest of the amplifier. This approach separates the touchy input structure from the gain stages of the device, and makes the design of the front end much easier.

For a successful monolithic equivalent the trick is to integrate both the J-FET input stage and the bipolar gain

Small draw. Monolithic op amps with field-effect transistors at their input can now compete with hybrid modules in precision amplifier applications. The J-FET inputs, which allow an op amp to operate at extremely low bias currents, are shown in the center on the extreme left of this photomicrograph. A third J-FET (upper left) is used for biasing. The chip, 83 by 54 mils, incorporates designs that minimize input current at high gain, while maintaining stability. Sample-and-hold, log, and photocell circuits will benefit.

1. Basic J-FET. Junction FET, built with standard p-channel processing, has n-type emitter diffusion and epi collector material which becomes top and bottom gates of the two-gate structure. For high gains and low leakage the back gate must be tied to the source, thus removing the leakage path between back gate and substrate.
2. Getting protection. Schematic of the 8007 shows method of protecting the input stage. Transistors Q3 and Q4 protect the input J-FETs from voltages in excess of 6.3 volts. Notice that offset nulling is done in the second pnp stage, minimizing voltage drift in J-FET-input stages onto the same chip without degrading the performance of either.

Unfortunately, integrating J-FETs is no easy job, although many attempts have been made and versions of such a device have been available for about three years. The fundamental problem has been circuit design, resulting from the failure of designers to fully comprehend the nature of the J-FET structure and its relationship to the rest of linear bipolar processing.

Indeed, early monolithic op amps with J-FET inputs suffered from three major problems. Input currents were often too large for many applications, especially charge-storage circuits such as sample-and-hold circuits, peak detectors, and so on. The offset drifted with temperature, especially after initial null setting. And poorly designed bias networks in the front end often resulted in acute manufacturing yield problems.

Integrating J-FETs

In general, the excess input current in any J-FET structure is a function of both the particular FET geometry chosen and the inherent leakage of the process. The most convenient method of making a junction FET, with only minor changes to a standard bipolar process, is to build the p-channel device shown in Fig. 1. Here the base diffusion forms the channel, while the n-type emitter diffusion and the epitaxial collector material become the top and bottom gates respectively.

Unfortunately, a J-FET so formed has several limitations. First, its transconductance—typically 300 microhm—is inherently lower than that in equivalent discrete devices, but when the device is used as a source follower, the low $g_{m}$ is no problem. Also, its drain-gate breakdown voltage is only 6.3 volts and to some degree complicates the front-end biasing circuits. Worst of all is the excess gate current that occurs if the two gates are tied together.

At first sight, it is tempting to do this in order to maximize the transconductance, $g_{m}$. But the effect is to create a disastrously large gate current. This is because in monolithic form the back-gate-to-substrate junction has a very large surface area, giving rise to excessive leakage currents between it and the negative supply. This leakage current adds to the J-FET-input bias current, which becomes large in its turn and renders the J-FET input ineffective for sensitive measurements.

A better way of achieving low leakage while max-

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Typical value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input bias current</td>
<td>0.3 pA</td>
</tr>
<tr>
<td>Input offset voltage</td>
<td>15 mV</td>
</tr>
<tr>
<td>Input resistance</td>
<td>$10^{12}$ Ω</td>
</tr>
<tr>
<td>Offset voltage drift</td>
<td>20 μV/°C</td>
</tr>
<tr>
<td>Common-mode rejection</td>
<td>90 dB</td>
</tr>
<tr>
<td>Input voltage range</td>
<td>± 12 V</td>
</tr>
<tr>
<td>Slew rate</td>
<td>6 V/μs</td>
</tr>
<tr>
<td>Output swing</td>
<td>± 12 V</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Type</th>
<th>$e_{n}$ (at 10 Hz)</th>
<th>$i_{n}$ (at 10 Hz)</th>
</tr>
</thead>
<tbody>
<tr>
<td>8007</td>
<td>300 nV/√Hz</td>
<td>0.01 pA/√Hz</td>
</tr>
<tr>
<td>741</td>
<td>25 nV/√Hz</td>
<td>0.7 pA/√Hz</td>
</tr>
</tbody>
</table>
3. Setting limits. The 8007's input stage is protected against high currents should the input transistors break down under fast transient conditions. In other monolithic J-FET op amps, a high-speed '0-V pulse could cause transistors Q3 and Q4 to return directly to the negative supply, forcing high current to ground. Shown in (b) is the 8007 answer to this problem—to limit this current with Q11.

imizing transconductance and gain is to tie the back gate to the source, thus removing the back-gate leakage path from the input current. In this case, since the back gate is more lightly doped than the channel, most of the depletion region goes the wrong way, that is, into the gate. The result: a small reduction in $g_{m}$ (by about only 10%), and most significantly a great reduction in leakage.

Getting the drift down

Once high gains at low input currents are achieved, it's necessary to go after low drifts. Unfortunately, the J-FET has inherently worse drift performance than its bipolar counterpart. However, just as there are design techniques for minimizing the drift of bipolar transistor pairs, so there are equivalent techniques for minimizing the drift of J-FET pairs.

But merely following the bipolar example leads to trouble. In the case of the bipolar transistor pairs, the first-order drift terms can be minimized by mismatching the collector current $I_{c}$ until the base-to-emitter voltage differential, $\Delta V_{BE}$, equals zero. In the equivalent J-FET case, however, mismatching the drain current $I_{D}$ until the differential in gate-to-source voltage, $\Delta V_{GS}$, equals zero will result in overwhelmingly large voltage drifts. The key to achieving minimum drift with J-FET pairs is rather to match the drain currents as closely as possible, and to perform the offset nulling in such a manner as not to disturb this match. This means that offset nulling must be implemented in the second stage.

A third design challenge involves biasing the J-FET input stage so as to maximize manufacturing yield without degrading electrical performance. Over a period of months, run-to-run variations in the manufacturing process will produce J-FETs with a range of drain-to-source current ($I_{DSS}$) from one third the typical value to triple this value, a 9:1 spread.

Now, if an attempt is made to bias the J-FET stage with a fixed current, as was done in some old designs, a value less than $I_{DSS}$ must be selected. If not, some of the devices will be forward-biased. But when this same current is used to bias those J-FETs that are toward the high end of the $I_{DSS}$ range, $V_{GS}$ will be high and the input common-mode range will suffer proportionally. And matters get worse when a wide temperature range is involved.

The solution is to bias the J-FET differential stage from another J-FET. The input stage J-FETs are then operated at about $0.8 I_{DSS}$. $V_{GS}$ is always low, thus ensuring an exceptional common-mode range for a J-FET amplifier. There is no danger of forward-biasing the J-FET, and the scheme assures these conditions hold good over wide temperature ranges.

The outcome

These design features have been incorporated into the Intersil monolithic 8007 op amp, shown in Fig. 2. The sensitive input J-FETs, Q1 and Q2, are protected from voltages in excess of 2.5 volts (well below breakdown) by the bootstrap loop comprising Q3, Q4, Q5, and Q6. This loop maintains a fixed drain-to-source voltage across the J-FETs regardless of the input voltage, and also contributes toward the exceptional common-mode rejection of the circuit. Notice that the offset nulling in the pnp gain stage has no effect on the drain current match of the first-stage J-FETs.

A key feature of the circuit is the operation of transistors Q14 and Q15, which serve to generate the bias current for the input stage. Q14 is a p-channel J-FET connected so as to generate a suitable drain-to-source current. This current is scaled down by about 20% by the resistors in the emitters of Q2 through Q6, in this way insuring that transistors Q1 and Q2 will not be forward-biased.

Another input feature of the 8007 is the current source Q11, which limits the input current should either $Q_{1}$ or $Q_{2}$ break down under fast transient conditions. Consider, for example, the effect of a high-speed positive pulse on one input, as shown in Fig. 3a. If the pulse were of sufficient amplitude, and if $Q_{3}$ and $Q_{4}$ were returned directly to the negative supply, excessive currents could flow through the path indicated in the figure. At best, there is a danger of latch-up—an input J-FET would remain in a breakdown state. The current source shown in Fig. 3b, on the other hand, eliminates
5. Logging it in. In typical log amplifier (a) and antilog amplifier (b), the low bias current of the J-FET op amp increases the sensitivity of the log range. Typically nine decades can be accommodated when a low-leakage IT120 transistor is used with the op amp.

the problem. Here the output stage is of conventional design, being very similar to the stage which is used in the 741.

Performance tells the story

The circuit performance of the 8007 is summarized in Table I. Note particularly that the typical input current is substantially less than 1 picoampere at 25°C, well within the design specifications of even the best J-FET-input modules. Equally important is the 8007’s ability to perform with low noise. The total mean-square noise of an operational amplifier for a bandwidth \( \Delta f = f_2 - f_1 \) is given by

\[
e_{\text{tot}}^2 = \int_{f_1}^{f_2} e_n^2 \, df + R_s^2 \int_{f_1}^{f_2} i_n^2 \, df + 4KTR_s \Delta f
\]

where the critical terms are: the source resistance, \( R_s \); the input noise voltage generator, \( e_n \); and the input noise current generator, \( i_n \).

Typical values of the 8007 for \( e_n \) and \( i_n \) are compared in Table 2 with figures for the general-purpose 741 op amp. It is clear that for general-purpose applications, where high source resistance (\( R_s \) greater than 1 megohm) and low input noise are requirements, the J-FET input is superior to the standard bipolar design. The details of the total input noise of the 8007 as a function of source resistance are shown in Fig. 4.

One of the 8007’s uses

An application which illustrates the advantages of the low input current of the 8007 is the log circuit of Fig. 5a and its antilog counterpart, Fig. 5b. In this setup, a low-leakage discrete transistor, such as the IT120, is connected across the op amp. This transistor has accurate logarithmic relationship between \( V_{BE} \) and \( I_c \) over a remarkably wide range of collector currents—10 decades (0.1 pA to 1 mA) are possible. At the low end of the current range, the accuracy of the circuit is primarily dependent on the ability of the amplifier to function. The 8007 with its picoamp bias currents becomes an ideal choice in this situation.

The photocell amplifier circuit of Fig. 6 can also profit from the 8007’s input parameters. In this circuit, a light meter directly displays the log of the light intensity as an exposure value. (An Exposure Value is a photographic term, each unit change in which corresponds to a factor-of-two change in light intensity.) To minimize leakage errors, the silicon cell is operated at zero voltage. Any current drawn by the op amp will directly subtract from the photocell output and show up as an error. This is especially true at low light levels, where the cell current may be only a few tens of picoamps. Thus the picoampere range of the 8007 again makes it a natural choice of photocell circuits.

Another use

An application that relies on the high slew rate of the 8007 is the Wien bridge oscillator, which can be used to generate large signal oscillations over a wide band of frequencies. When general-purpose amplifiers, such as the 741, are used to obtain signals with amplitudes greater than about 100 millivolts, the slew rate (the maximum rate at which the output voltage can change) is the parameter that determines the upper operating frequency. If the amplifier slew rate is less than a critical threshold, distortion will occur. For example, for a sine wave above about 10 kilohertz, an amplifier with 0.6 V/s slew rate (the 741, for example) will not handle a 20-V peak-to-peak signal.

Typically the 8007 has a slew rate of 6V/\( \mu s \), and thus offers an operating-frequency range that is 10 times the 741’s. Indeed, using the 8007 in a typical Wien Bridge oscillator provides a 20-V peak-to-peak output at 40 kHz. In this circuit, the amplitude may simply be controlled by \( R_4 \). For smaller output swings, correspondingly higher frequencies can be obtained.

BIBLIOGRAPHY

Gated MOSFET acts as multiplexing switch

by Glen Coers
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A four-terminal MOSFET makes a handy series analog gate for time-multiplexing either ac or dc signals. An array of these MOSFETs can, for instance, be used to gate a number of voltages that are being monitored periodically by a chart recorder or a voltmeter, as shown in the figure. Here, the BCD-to-decimal decoder switches one MOSFET analog gate at a time for a given interval before switching another.

The decoder outputs are high except for the output number being decoded. An operational amplifier, connected as a comparator, is used to switch each MOSFET on and off. Each comparator's inverting input is set to a dc reference voltage of approximately 1.6 volts.

When a logic 0 appears at the selected decoder output, the associated comparator's output goes to -14 V. The MOSFET that is tied to the comparator output then conducts, gating the analog input voltage to the voltmeter or chart recorder. When the decoder output returns to logic 1, the comparator output switches to 14 V, turning off the MOSFET.

Since MOSFETS are bilateral devices, they can handle both positive and negative voltages. For this circuit, the maximum input voltage swing is ±10 V, but can be extended by raising the level of the positive and negative supply voltages that bias the MOSFET's gate terminal. The multiplexer circuit has good isolation and leakage properties.

MOSFET gate. Analog signals can be gated selectively by using a BCD-to-decimal decoder to switch array of MOSFETs. All decoder outputs are high, except for the one selected to be the output number. When selected decoder output goes low, output of associated comparator also goes low, turning on MOSFET and permitting analog input to pass to circuit's output. Both positive and negative inputs can be gated.
The output power of a stepping motor can be boosted when it’s stepping, while the dissipated power during its dwell (holding) intervals is minimized, by effectively doubling the supply voltage of the motor-drive circuit with capacitor charge. The boosted drive circuit shown is intended for four-phase 28-volt motors.

During the dwell intervals, the drive circuit supplies the pair of motor coils that were energized during the previous clockwise step. Transistor \( Q_1 \) is on, but conducts only leakage current because transistors \( Q_2 \) and \( Q_3 \) are off. This permits capacitor \( C_1 \) to charge to the supply voltage of 24 V. (Transistors \( Q_1 \) and \( Q_2 \) form a complementary Darlington transistor pair.)

The motor’s advance sequence is dictated by a pulse stream that increments the motor’s winding-sequence counter and also triggers the monostable multivibrator at the input of the drive circuit. When the \( \bar{Q} \) output of this one-shot goes low, its \( Q \) output goes high, turning off transistor \( Q_1 \) and turning on transistors \( Q_2 \) and \( Q_3 \).

Since diode \( D_1 \) is reverse-biased, the potential at \( Q_2 \)’s collector rises to about 24 V, and the capacitor is restricted to a discharge path through the motor windings. Therefore, the voltage available for the coil common lead is nearly twice the supply voltage—or approximately 48 V. With this boosted voltage, motor-winding current rises rapidly to enhance available torque.

Once the current buildup time is over, the one-shot completes its timing cycle, turning off transistors \( Q_2 \) and \( Q_3 \), while turning on transistor \( Q_1 \), which is current-limited by resistor \( R_1 \). Capacitor \( C_1 \) recharges to the supply-voltage level. This cycle repeats for every stepping pulse.

The timing of the one-shot is not critical. A reasonable timing period would be half of the shortest period between advance pulses.

Stepping up torque. Drive circuit for stepping motor boosts available stepping power without increasing supply voltage. During motor dwell time, capacitor \( C_1 \) charges to 24-volt supply level. When advance pulse triggers one-shot, transistor \( Q_1 \) turns off while transistors \( Q_2 \) and \( Q_3 \) turn on. Coil common voltage then builds to twice the supply level because \( Q_2 \)’s collector voltage rises by 24 V.

The timing of the one-shot is not critical. A reasonable timing period would be half of the shortest period between advance pulses.
Voltage-tuned filter varies center frequency linearly

by Vassilios J. Georgiou
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Although a voltage-tunable multiple-feedback active filter generally offers constant gain and constant bandwidth throughout its tuning range, its tuning curve for center frequency versus control voltage is usually highly nonlinear for extended frequencies. This is due to the nonlinearity of the field-effect transistor, which is used as a variable resistor, and because the center frequency varies inversely with the square root of the FET's drain-source resistance. Employing feedback, therefore, to linearize the FET's behavior is not a solution.

Instead, a modified version of the diode function generator can be used to drive the FET's gate terminal. For the voltage-tunable bandpass filter shown, center frequency remains nearly linear for changing control voltage over a center-frequency range of 4.5:1.

Resistor R1 and supply voltage VGG bias the FET at -3 volts, thereby setting the filter's first breakpoint for Vc = 0 at 1,460 hertz. For negative values of control voltage, only diode D1 conducts, and the gain of the amplifier is determined by resistors R2 and R3.

For positive control voltages, diode D2 conducts, and amplifier gain is about half the value it is for negative control voltages. As a result, the lower portion (right-hand side) of the filter's tuning curve tilts upward and aligns with the upper portion (left-hand side) to form a linear characteristic.

Diodes D3 and D4 define the second filter breakpoint—at Vc = 2.4 v—by further reducing amplifier gain and extending linear operation to 570 Hz. Preferably, the germanium diodes, D1 and D2, should be gold-doped so that they have a low forward-voltage drop.

**BIBLIOGRAPHY**


Designer's casebook is a regular feature in Electronics. We invite readers to submit original and unpublished circuit ideas and solutions to design problems. Explain briefly but thoroughly the circuit's operating principle and purpose. We'll pay $50 for each item published.

**Straight-line tuning.** Modified diode function generator (in color) drives FET variable resistor for voltage-tunable bandpass filter, causing center frequency to vary linearly with control voltage over 4.5:1 frequency range. Gain of function-generator amplifier is reduced for positive control voltages to raise lower section of (uncompensated) tuning curve. Compensated filter remains nearly linear.
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**Write for Data**

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Film only a few atoms thick promises very large mass memories

Permalloy film less than 50 atomic diameters thick achieves data storage at 100 times the density of other films, has random access at microsecond speeds; yet it costs no more per bit than a head-per-track drum does by E. J. Torok, Univac Defense Systems Division, St. Paul, Minn.

A new type of thin-film memory has so much larger a bit capacity than conventional thin-film memories that it qualifies for use as a mass memory. It is faster than many present mass memories, but is very small and light, and dissipates little power. In addition, it could easily replace fast head-per-track disks and drums, being not only competitive in price but vastly superior in performance.

A feasibility model of the new memory, called an oligatomic film memory, has been tested by the National Aeronautics and Space Administration at its Marshall Space Flight Center, Huntsville, Ala., and further development is under way at Univac Defense Systems division. Although its first use is likely to be in aerospace applications, where its ruggedness, non-volatility and compactness make it especially desirable, calculations of cost versus performance show that it can also be valuable in commercial equipment.

Present thin-film arrays are used primarily as main memories in computers. The oligatomic film memory, however, can serve as a much larger main memory in a high-speed computer system that uses a cache memory. The parameter values that make this possible are listed in the table on p. 108.

A few atoms thick

An oligatomic film has a thickness of only a few atomic diameters—less than 50. The prefix, "olig-," is from the Greek for few, and the whole word was coined by the German scientist Ulrich Gradmann, who studied the magnetization and surface anisotropy of layers between 2 and 200 angstroms in thickness. (In permalloy, the atomic diameter is 3.5 angstroms, and most magnetic films are several hundred to a thousand or so angstroms thick.)

A typical magnetic oligatomic film consists of a 100-
2. Thin film storage element. Colored arrows show normal magnetization along film's easy axis storing binary Os. The one reversed arrow designates an area that has been switched, and therefore stores a 1. Word current rotates magnetization perpendicular to easy axis.

angstrom layer of permalloy, which is deposited on a 2-by-3-inch copper substrate in a vacuum in the presence of a magnetic field. This field imposes an easy axis upon the film. When magnetized, later, the film is in its lowest energy state when the magnetization vector is either parallel or anti-parallel to this easy axis. If an external magnetic field is applied perpendicular to the easy axis, but parallel to the plane of the film, the magnetization vector of the film will rotate to follow it, but returns to its original orientation when the external field is removed. Simultaneously applying a magnetic field in both hard-axis and properly oriented easy-axis directions causes the film magnetization vector to switch—that is, to reverse its direction.

These external fields are applied by passing current through one of two sets of copper overlays (Fig. 1), made by etching a copper-polyimide laminate. One of the two overlays forms a set of parallel word lines, the other a set of parallel sense/digit lines at right angles to the first set; each intersection defines a bit location.

If the whole film is initially magnetized in a given direction, and if direct current pulses of the appropriate polarity are then applied to one word line and one sense/digit line, there appears under the intersection a boat-shaped magnetic domain magnetized in the opposite direction to the rest of the film (Fig. 2). This domain is about as wide as the word line and rather longer than the sense/digit line is wide.2 A current in the word line alone twists the magnetization in the domain to one side, and the resulting flux change generates a signal in the sense/digit line.

However, because the oligomagnetic field is so thin, the total flux linking the sense/digit line is very small. Therefore, to get a usable signal in the sense/digit line, an alternating current is used in the word lines. (The reasons for using an ac signal are discussed more fully later.) The alternating word current, which has a frequency of 10 megahertz, causes the magnetization in the domain to rock back and forth with a similar frequency, so that the flux in the hard-axis direction fluctuates at this frequency. However, as the hard-axis flux increases, the easy-axis flux decreases, and vice versa; in the absence of an applied easy-axis field, the easy-axis flux always returns to its original orientation regardless of the direction of the hard-axis flux.

The result is an easy-axis component of the total flux oscillating between a peak value and zero at twice the frequency of the word current. When the easy-axis flux is at its minimum—essentially zero—the hard-axis flux is at a positive or negative maximum. But the easy-axis flux links the sense/digit wire and the hard-axis flux does not. Therefore the sense signal generated by the changing flux is also generated at 20 MHz, twice the frequency of the word signal.

Furthermore, the phase of the 20-MHz signal depends on the orientation of the magnetization vector. Labeled a binary 0, the vector parallel to the film's original easy axis produces an output 180° out of phase from the antiparallel magnetization vector, called a binary 1.

Signal alternation

This alternating sense signal is of the greatest importance, because it permits the use of tuned sense amplifiers that respond only to a narrow band of frequencies. With a 10-MHz drive, the 20-MHz amplifier rejects noise coupled from the word line at 10 MHz, as well as most of the thermal noise generated by the film itself. In conventional thin-film memories, the word noise is sometimes larger in amplitude than the data signal.

The general arrangement of the electronic circuitry
used with an oligatomic film memory is shown in Fig. 3. The array is approximately square. Along one edge a word selection matrix directs the output of a 10-MHz oscillator into one of approximately 10,000 word lines. A sense/digit selection matrix lies along an adjacent edge, and performs two functions: it directs digit currents into some of the approximately 10,000 sense/digit lines when writing, or it picks up sense signals from the lines, compares them with reference signals, and routes them to a set of 288 tuned sense amplifiers.

The reference signal originates in a reference line (Fig. 4) that serves eight sense/digit lines. The thin film under the reference line is always in the 0 state: its 20-MHz output is essentially identical to the output from the sense/digit line when a data 0 is read. When these two signals drive a differential amplifier, its output is nearly zero. But the reference signal is 180° out of phase for a binary 1, and the differential amplifier's output in this case is nearly doubled the amplitude of the two inputs.

The spikes that often occur between successive read signals originate at the gates in the sense/digit selection matrix. They occur in conventional film memories too, where they come along with the data signal and have to be lived with. But in the oligatomic film memory with its ac signals, the data keeps coming and detection can wait until the selection noise dies out.

Although a sense amplifier with several stages of tuned circuits was used in the module built for NASA, a better and less expensive sense amplifier has been built since then. It is a phase angle voltmeter using a balanced demodulator, and has an easily adjustable bandwidth and better noise rejection. Having no tuned circuits or inductors, it can be built as a hybrid circuit for less than a tenth the cost of the former amplifier. This makes it economically possible to provide enough sense amplifiers in the memory system to read out several hundred bits in parallel—a desirable capability when the oligatomic film memory is used with a cache.

**Whys and wherefores**

The extreme thinness of the film and the ac signals represent departures from conventional film memory design. They were dictated by the purpose of the oligatomic film memory: to provide a large random-access storage capacity at the lowest possible cost in a small volume. The desired capacity—about 100 million bits—is two orders of magnitude larger than the capacity of a conventional film module, such as Univac's mated-film memory, as used in the Navy's developmental antisubmarine warfare aircraft, the S-3A. Therefore the memory needed a bit density two orders of magnitude greater if the same volume was to be retained.

Getting this high density presents a serious problem—a field, created by magnetic poles at the edges of mag-
and four is followed by Os (sweep time is about 20 microseconds).

5. Sense line outputs. Scope traces show a sequence of one, two, single dc pulse in the word line rotates the film magnetization can be continually rocked back and forth many times without becoming demagnetized by creep.

The only alternative way of reducing the demagnetizing field requires the pole strength to be correspondingly reduced. Since the magnitude of the poles is proportional to the film thickness, the latter had to be reduced by a factor of ten.

Making the film so much thinner brings mixed blessings. Ordinarily, two thresholds are associated with thin magnetic films: a rotational switching threshold and a creep threshold. To switch the film requires an external magnetic field of greater strength than the rotational switching threshold, while to guarantee that the film remains unaffected, the field must remain below the creep threshold. But repeated applications of a field in the no-man's-land between the two thresholds cause the magnetic state of the film to fade away gradually. However, in an oligatomic film, the creep threshold is nearly equal to the rotational switching threshold, for magnetostatic reasons. Because of this, the magnetization can be continually rocked back and forth many times without becoming demagnetized by creep.

On the other hand, the reduced film thickness provides a very low signal output. The signal is proportional to the flux change, and the flux is proportional to both the film thickness and the width of the domain; both of these have been reduced by a factor of 10.

To get around the small-signal problem, the tuned amplifier was used in place of the conventional wideband pulse amplifier. In conventional memories, a single dc pulse in the word line rotates the film magnetization into the hard direction, and this induces a single pulse in the sense/digit line. The wideband amplifier amplifies this pulse—plus the accompanying thermal noise and capacitively coupled word noise. But the tuned amplifier can be designed to reject all but the signal frequency and to use a microvolt rather than millivolt signal. In fact, oligatomic films 100 angstroms thick with word lines 3 mils wide can develop 50 µV at 20 MHz—a very comfortable signal for a tuned amplifier.

New gates

Of course, the change to a tuned sense amplifier required a corresponding change in the design of the gates driving the word lines and the sense/digit lines. Conventional word gates work with unipolar dc pulses only. But bipolar radio frequencies are involved in the oligatomic film memory, so that low-distortion rf techniques were necessary in the gate design (Fig. 6). Showing that these new designs work was one of the most important things accomplished by the NASA tests.

The high bit density in the film requires very narrow word lines. But the magnetic field at the surface of a conductor is proportional to the current density in that conductor. Thus, to produce a field of a given strength around a conductor of a given thickness, a stripline 3 mils wide requires only one-tenth the current that a 30-mil line would require. Furthermore, such narrow conductors are more easily made if they are also thinner.

Consequently, while conventional wire and film memories require about 500 milliamperes for the word current, the oligatomic film memory requires only 28 mA. Such small currents bring the whole device potentially well within the current-supplying capabilities of large-scale integrated circuits.

Calculating the cost per bit of different memory tech-

**5. Sense line outputs.** Scope traces show a sequence of one, two, and four 1s followed by 0s (sweep time is about 20 microseconds).

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**Pricing problems**

Although the cost per bit of a memory technology is one of its most important parameters, few numbers are less reliable than the cents-per-bit predictions made by advocates of a particular technology—regardless of what that technology may be. In the past, such predictions have been off by as much as two or even three orders of magnitude. Moreover, different organizations define their costs differently. Some commercial firms find that their selling prices have to be three times their "cost" in order not to lose money, while, by law, military suppliers must sell at a price only slightly above "cost."

A nonpartisan manufacturing department can usually estimate the cost of a memory technology fairly accurately, provided it is given the detailed design information. But another way to arrive at comparative figures for various technologies is to calculate the costs of those parts that are used in large numbers in a single memory—selection gates, overlays, and sense amplifiers, for example. Furthermore, even though these repeated parts may differ in detail from one technology to another, their costs remain so nearly constant that correct cost ratios of various technologies can easily be obtained.
Hybrid packages. Word gates are in hybrid IC containing 18 large square patches (resistors); package is 125 mils across. Other package (both square and oblong resistor patches) contains 12 sense/digit gates, measures 160 mils across. In both ICs the small black spots are field-effect transistors—18 in one, 12 in the other.

Technologies, for purposes of comparison, is at best tricky; but with some educated guesses and an assumption or two, as outlined on page 109, the relative costs can be predicted. Four such calculations yield the comparison shown in Fig. 7, which shows the cost of the oligatomic film memory to be very much lower than that of mass plated-wire, mass ferrite-core, or large metal-oxide-semiconductor arrays.

Cost analysis

The designs evaluated for this comparison are derived from present-day technology, since that of several years in the future would involve too much speculation. For that reason, the module capacities chosen for mass wire and mass core are 65,536 words—today's state of the art. Future designs for plated wire will probably use simpler support structures, thinner films, and higher bit densities; their module sizes will therefore be larger and their cost per bit lower.

Semiconductor memories, on the other hand, do not benefit from economies of scale as do magnetic memories. As a result, they are most useful in small sizes, such as buffers and caches, while magnetic memories are better for main-frame and mass memories. This distinction is reflected in the choice of the 32,768-word semiconductor module for the comparison in the diagram.

The cost per bit of the oligatomic film memory is determined by the costs of film deposition, of photoetched overlays, of selection gates, of interconnections, and of sense amplifiers. Film deposition and photoetching costs are determined by area, not by the number of bits or conductors. Thus by increasing the density by a factor of 100, the cost per bit of these factors is decreased by the same factor. Of course, above a certain density the yield plummets, and the cost increases again; but at the present time the oligatomic film is well below this critical point.

In a square memory organization, where the numbers of word lines and sense/digit lines are equal, the costs of selection gates and of interconnections are each inversely proportional to the square root of the memory's capacity. Gates and interconnections are both arranged along the periphery of the memory array. The photoetched overlays for the lines can be made in long strips and connected only at the edges of the array. This low interconnection cost, incidentally, just cannot be achieved with semiconductor memories.

Finally, the number of sense amplifiers equals the number of bits read out of the memory at any one time, that is, the memory's word length, and remains the same whether the memory stores 100 such words or 100,000. As a result, the total cost of sense amplifiers depends on the word length, but is independent of module capacity. Since the total cost is a constant as capacity varies, the cost per bit of the memory system contributed by the sense amplifiers is inversely proportional to module capacity.

In the same way, the cost per bit can be calculated for non-random-access memories, such as drums, disks, bubble memories, domain tip propagation devices, and ferroacoustic memories. In all of these memories access time is traded for fabrication cost—they are very inexpensive per bit, but they are also very slow. But ignoring access time for the moment, the cost per bit of oligatomic films is slightly less than that of commercial head-per-track drums, about the same as magnetic bubbles, and much more than movable-head drums—at today's state of the art for all these technologies.

Proponents of bubble technology expect (probably justifiably) drastic reductions in the costs of substrates, depositions, and sense amplifiers. However, the costs of overlays and selection matrixes for oligatomic film memories are also sure to drop, especially with LSI. As a result, oligatomic films and bubbles will probably cost much the same as each other over the long run, and will approach movable-head disks and drums. The difference is in the performance, because the film is random-access and the bubble memory is serial.

Two revolutions in recent computer history are profoundly affecting memory design: the use of a cache memory, and multiprogramming. The cache revolution has replaced the concept of a large, fast main memory with the idea of a small, slow memory that acts as a read cache. This change has had a profound effect on the design of high-speed memories, because it has made it possible to use a smaller, cheaper memory for the same purpose. The multiprogramming revolution has had a similar effect, because it has made it possible to use a smaller, cheaper memory for the same purpose. The latter effect is particularly important, because it has made it possible to use a smaller, cheaper memory for the same purpose.
with a combination of a small, fast buffer and a large, relatively slow and inexpensive backing store.\textsuperscript{3,4} The multiprogramming revolution is eliminating the input-output-boundedness of most older computers by storing several programs at once in the main memory, thus enabling the processor to work continuously on several programs in turn, instead of being halted whenever the program demands information stored on a drum.

The place for oligatomic films

When a cache memory is used, its size is likely to be between 2,000 and 8,000 words, and its speed is fast enough not to limit the processor's operation—typically 15 to 200 nanoseconds. Meanwhile the backing store used in conjunction with a cache is likely to have a capacity of 32,000 to 500,000 words and an access time of 0.5 to 40 microseconds. When the processor needs data from memory, it looks first in the cache. Since the word is usually there, the average access time over the long run is only slightly greater than the actual access time of the cache. Meanwhile the capacity of the system is that of the less costly backing store.

Calculations made with the aid of readily available formulas\textsuperscript{3,4} show that the performance of a computer system containing both a cache memory and an oligatomic film backing store is much better than any remotely competitive present-day technology. Figures of merit, shown in the table below, are based on the number of accesses per second per dollar of memory cost. The other revolution, that of multiprograming, is related to the cache revolution. Basically, multiprograming is a technique in which many different programs are stored in the main memory. At any particular time, only one of them is running. But when that program requires the use of a piece of input-output equipment—for example, the program requires a page of information from a disk—the I/O operation proceeds independently while the computer, instead of standing idly by, switches to another program. Several programs may be stacked up and run a little at a time, either in rotation or according to a priority arrangement.\textsuperscript{11,12,13}

But the several programs and their data bases may require as much as 10$^6$ or even 10$^{10}$ bits—far more than any physical main memory can hold today. The overflow is stored on drums and disks, which, being rotating devices, have a latency of 3 to 100 milliseconds. (Low latency is characteristic of the most expensive head-per-track machines; the higher values are found in some moving-head units.)

An example shows the effect of latency on processor performance. Suppose a processor is running a mix of programs that requires access to a disk on the average of once every 8,000 instructions. In monoprogramed mode, executing one instruction each microsecond, the disk access request would occur once every 8 ms. But if the disk has a 40-ms latency, the machine spends 83% of its time idling, waiting for the disk.

If the processor, still monoprogramed, were multiplied in speed by a factor of 5—by adding a cache or by other means—throughput would be improved by only 14% and the 40-ms idle time would be increased to 97%.

This takes into account only the delay in transferring data to or from the disk. If the program uses other input/output equipment as well, latency effects are combined with the mechanical delays of other equipment.

But the throughput can be increased by using a larger main memory that stores many programs at once—that is, by multiprograming. Then while one program waits for the disk, the processor can execute another program. The higher the multiprograming level, the better the performance improvement, because the probability is lower that all programs are waiting for the disk.

In an attempt to keep the memory size down, a system designer might try using fast drums for part of his

7. Cost comparison. These relative costs per bit of four memory technologies are calculated by rules discussed in panel, p. 109. They are figured on the basis of defense and space project costs, not commercial; and they reflect present, not future, prices.
input-output requirements. This works pretty well up to a certain point. But when an improved processor comes along, perhaps as a multiprocessor system in which two separate machines share the work load of several programs stored in a single memory, the problem returns. To keep both machines busy all the time, with a substantial level of I/O, requires a very high level of multiprogramming and an extremely large memory.

Even this isn’t adequate if the multiprocessor is to be used in a real-time transaction application. An example of this is an airline reservation system, which has many remote terminals and an I/O demand rate five to 10 times that of an ordinary business application.11

But with its extremely low cost per bit, used in conjunction with a cache memory, the oligatomic film memory can serve the needs of even the largest multiprogrammed multiprocessor system at a reasonable cost. Its performance/cost characteristics are shown in the bar chart (Fig. 8) in comparison with various other technologies and combinations. The chart contains several assumptions: a total capacity of 200 million bits; a cost of $20,000 for a processor capable of executing a million instructions per second and $50,000 for one five times as fast; an average program size of 38,000 words and an executive of 65,000 words; I/O access every 8,000 instructions; and costs per bit of 4c for mainframe core, 2c for 300-ns MOS, 1c for 1-µs mass core, 0.1c for 3-µs mass oligatomic film, 0.1c for a 4-µs head-per-track drum, and 0.01c for a 40-ns movable-head drum.

In every case the systems that use cache memories are better than systems of similar size without a cache. The faster drum, even at an order-of-magnitude higher cost per bit, is better than the slower one. And even though the oligatomic film mass memory costs the same as the head-per-track drum, its performance is so much better that the difference in cost-effectiveness is enormous.

In the bar chart, the bottom bar represents a three-level hierarchy—one level more than is ordinarily used today. At the bottom level, the bipolar memory is a cache for the conventional main memory, which can be core in a commercial machine or mated-film in an aerospace application; the main memory, in turn, is a cache for the oligatomic film mass memory. The cost-performance of this three-level hierarchy is nearly two and a half times as good as the best conventional two-level hierarchy, shown by the third bar from the bottom.

8. Cost/performance comparison. All examples represent 200 million bits of storage, executing a program mix of 70% business applications and 30% scientific applications. Individual costs per bit and access times are discussed in the text.
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<table>
<thead>
<tr>
<th>MMI Part No.</th>
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<th>No. of Characters</th>
<th>SCAN</th>
<th>ACCESS ns</th>
<th>Pkg. Pins</th>
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Instrumentation amplifier conditions computer inputs

Two-stage amplifier detects more than 100 multiplexed signals at computer-speed scanning rates with minimum noise over wide frequency range; signal levels can range from microvolts to volts

by Thomas C. Lyerly, IBM General Systems Division, Boca Raton, Fla.

□ Since the job of data gathering has become so complex that computers are needed to process measurement information, increasingly stringent performance requirements are being placed on the instrumentation amplifier. A single instrumentation amplifier must frequently accept more than 100 multiplexed signals with levels ranging from a few microvolts to several volts. The amplifier must also reject unwanted noise signals from dc to hundreds of megahertz, as well as provide a noise-free, properly scaled, single-ended output signal that can be sampled quickly for processing.

Precision low-level signal conditioning can be achieved with a two-stage amplifier that employs cascode transistor pairs, degenerative feedback, and balanced frequency compensation to provide exceptional gain-bandwidth performance without gain-adjustment potentiometers. Even in noisy environments, this amplifier can detect microvolt signals at high scanning rates. It can also be adapted for programable gain selection.

The environment for the precision amplifier is the computer analog input subsystem, such as the typical one shown in Fig. 1 for the IBM System/7 computer. As many as 128 analog input signals may be connected through single-pole low-pass filters to the multiplexer, which is made up of p-channel MOSFET switches. The multiplexer can handle up to eight parallel groups of signals, with each group consisting of up to 16 parallel channels.

The differential output of the multiplexer is connected to an instrumentation amplifier through a balun transformer that serves as a high-frequency noise filter for the amplifier. Multiplexed analog input signals must be accurately processed by the amplifier at scanning rates as fast as 20 kilohertz without any adverse effects from noise sources that are both external and internal to the analog input subsystem.

External noise may be separated into two types—common-mode, and normal- or differential-mode signals. Differential-mode noise is the easier to reject. It can be filtered by passive low-pass networks located at

1. The environment. Analog input computer subsystem challenges the instrumentation amplifier. Data is filtered before being multiplexed to eliminate normal- or differential-mode noise. Balun transformer acts as high-frequency common-mode noise filter for the amplifier.
the multiplexer inputs, as shown in Fig. 1, since a given channel is generally sampled at a rate that is much slower than the speed at which the amplifier scans the channels.

Common-mode noise is more difficult to reject because low-frequency common-mode filtering reduces the multiplexer's ac common-mode rejection ratio, while increasing its common-mode settling time. For the analog input subsystem to operate at fast multiplexer-scanning rates, the instrumentation amplifier must be able to reject common-mode noise over a large bandwidth. Therefore, a balun transformer is placed at the amplifier input as a high-frequency common-mode filter to reject the common-mode noise beyond the bandwidth of a practical amplifier.

(This noise is filtered to prevent the amplifier from rectifying rf noise on the input lines and effectively producing dc offset errors. The balun transformer of Fig. 1 is a low-pass common-mode filter with a bandwidth of approximately 5 megahertz.)

Noise within the analog input subsystem, which takes the form of capacitively coupled noise signals and switching transients, is primarily caused by the multiplexer because of the device capacitance of the MOSFET switches. This internal noise source appears to the amplifier to be primarily common-mode noise as a result of the balanced design of the multiplexer and the low-pass input filter.

Configuration outline

An instrumentation amplifier that provides excellent rejection of unwanted common-mode noise is sketched in Fig. 2. The circuit also offers good gain-bandwidth characteristics and can be adapted for programable gain selection.

Amplifiers A1 and A2 provide the desired input characteristics and signal ranging. A third amplifier, A3, acts as an inverting unity-gain device for differential inputs and operates as a precision broad-bandwidth subtractor for unwanted common-mode signals. To reject common-mode signals over a large bandwidth, A1 and A2 must perform as broadband unity-gain amplifiers, generating balanced common-mode signals for subtractor amplifier A3.

The common-mode rejection ratio of the over-all amplifier can be expressed as:

$$CMRR = \frac{(R_i/R_f)(1 + 2R_m/R_i) + (CMRR_1 + CMRR_2)}{(1 + 2R_m/R_i)(R_f/R_i) + (CMRR_1 + CMRR_2)}$$

where CMRR1, CMRR2, and CMRR3 are the individual common-mode rejection ratios of amplifiers A1, A2, and A3, respectively.

Other common-mode input errors, not included in this equation, are caused by the voltage-divider effect between the source impedance of each analog input line and the common-mode input impedance of its amplifier. To prevent common-mode signals from being converted into differential signals from source imbalance at the input of the over-all amplifier, amplifiers A1 and A2 must maintain a high common-mode input impedance over a large bandwidth.

The high impedance of these two amplifiers also helps the over-all amplifier to reject the transients generated when the multiplexer channels are switched. These transients are caused by common-mode voltages, sometimes as high as 10 volts, that are switched into the instrumentation amplifier inputs at rates that can approach several hundred volts per microsecond.

The first stage

A first-stage design that satisfies the tough input performance requirements is illustrated in Fig. 3. Basically, the circuit attempts to eliminate amplifier input errors caused by offset voltage, bias current, offset-voltage drift, offset-current drift, and input impedance.

Input offset voltage can be reduced to less than 2 microvolts with the nonlinear potentiometer network of resistors R1, R2, and R3, and the voltage divider set up by resistors R4 and R5. The input-offset voltage drift with temperature is also low because the difference between the base-emitter voltage drops of matched input transistors Q1 and Q2 is nearly zero.

Additionally, input bias current can be adjusted to less than 1 nanoampere by parallel potentiometers R6 and R7, which are driven by the high-impedance constant-current source, consisting of cascode transistors Q3 and Q4 and resistor R8. The potentiometers are also driven by the common-mode input voltage through a feedback network in the emitter circuit of the Q1-Q2 input transistor pair. The network, made up of transistors Q5, Q6, and Q7 and resistor R9, supplies a constant voltage for biasing resistors R10 and R11 that is independent of the common-mode input voltage.

The input-impedance component of the amplifier from the feedback bias network is several thousand
megohms. Therefore, this feedback circuit provides a stable bias current without reducing the input impedance of the amplifier. A heated-substrate matched-input transistor pair can further improve the bias current, the offset-current drift, and the offset-voltage drift of the amplifier.

To increase the amplifier's common-mode input impedance, FETs Q8 and Q9 are connected in a cascode configuration to feed the common-mode emitter voltage of transistors Q1 and Q2 back to their collectors. The feedback reduces the effective input capacitance, but increases the effective input resistance between the base and collector of both input transistors. The impedance in the emitter loop of the Q1-Q2 input pair is also increased by a cascode pair, Q10 and Q11, along with resistor R42, in the emitter-current source.

The first-stage design can provide a common-mode input resistance of more than 2,000 megohms and an input capacitance of no more than a few tenths of a picofarad. It also offers a good common-mode rejection ratio, as well as power-supply rejection ratio because of the high drain output impedance of the FET cascode circuits. (Voltages V1 and V2 are zener-stabilized levels.)

**The second stage**

Performance requirements for the second stage are determined primarily by the programable signal ranging and gain-bandwidth requirements of the over-all instrumentation amplifier. An ideal amplifier has an infinite open-loop gain so that its closed-loop voltage gain is determined only by external resistive networks. However, a practical amplifier's gain accuracy decreases for increasing values of closed-loop gain because it has a finite open-loop gain. The closed-loop gain for the practical amplifier of Fig. 2 can be written as:

$$\text{CLG} = \frac{1 + 2R_m}{R_n}(R_m/R_1)[1/(1 + 1/A)
+ (1 + 2R_m/R_n))][1/(1 + (R_1 + R_2)/A_1)]$$

where A represents open-loop gain:

$$A = A_1 = A_2 = A_3$$

Instrumentation amplifiers with large closed-loop gains usually require gain-adjustment potentiometers if a high degree of gain accuracy must be maintained. However, a second-stage design with sufficient gain can eliminate the need for potentiometers without degrading gain accuracy. A schematic of a high-gain second stage is shown in Fig. 4.

The dc gain of the stage is directly proportional to the impedance at the drain terminal of FET Q1. A high-impedance node is developed at point A because the Q1-Q2 cascode pair drives the Q2-Q3 cascode pair and FET Q3 is connected as a source-follower. The dc resistance from node A to ground may be as high as 500 megohms, depending on the quiescent current of the cascode pairs and the resistance in the emitter circuits of transistors Q2 and Q4.

**Cascading the stages**

The circuit permits voltage gains in excess of several million to be achieved with a single stage. To make the gain of the stage less sensitive to changes in transistor parameters, emitter degeneration is provided by the resistors labeled R8 so that the voltage gain is approximately equal to the ratio of the resistance of high-impedance node A and the value of resistor R8.

When the first- and second-stage designs are cascaded, they form a differential amplifier with a stable and well-defined open-loop dc voltage gain that can exceed 140 decibels. Since the open-loop gain is very large, the errors in the closed-loop gain caused by a finite open-loop gain are reduced to a negligible level. Therefore, gain-adjustment potentiometers are not required, and the closed-loop gain of the instrumentation amplifier can be established by resistive networks alone.

To satisfy the fast sampling-rate requirements of the analog-input subsystem, the settling time of the amplifier must be minimized. Settling time is determined by both bandwidth and slew rate, which is a measure of the rate at which the amplifier output can change.

**Slew-rate limiting**

Slew rate is limited in feedback amplifiers when the maximum output rate of change that is fed back to the inverting input is less than the rate of change at the noninverting input. Under these conditions, a large differential error is produced across the amplifier inputs. The differential input impedance drops while the amplifier is slew-rate limiting and may be further reduced if the input step voltage exceeds the amplifier differential breakdown voltage.

The low input impedance that occurs during slew rate limiting can produce large errors if low-pass filters with long recovery time constants are associated with the multiplexer, because charge is transferred from the filter capacitors to the amplifier inputs. To minimize this error, the amplifier must have a fast slew rate, as well as...
4. Second stage. Since this stage can attain voltage gains of several million without losing gain accuracy, gain-adjustment potentiometers are not needed. Circuit gain approximately equals the resistance ratio of high-impedance node A and resistor $R_e$.

A relatively high open-loop input impedance.

In a practical amplifier, one that must operate over a wide range of closed-loop gains, the fastest possible response time is achieved for large closed-loop gains by extending the natural break frequencies of the open-loop amplifier to obtain the largest possible gain-bandwidth product. Amplifier capacitance, which determines bandwidth, can then be kept small, and the slew rate, which is also fixed by amplifier capacitance, can be held at a large value.

A high open-loop gain presents a difficult frequency-compensation problem when a fast unity-gain closed-loop response is needed. For example, suppose the same bandwidth must be available from a single-pole 6-dB/octave amplifier for unity-gain operation and for a closed-loop gain of 512. To do this, the amplifier's open-loop gain must be reduced by a factor of 512 at the desired bandwidth by increasing the internal compensation capacitance by a factor of 512. The increase in capacitance decreases the slew rate by a factor of 512 and degrades the unity-gain time response. One solution to the problem is to select the appropriate frequency-compensation components digitally so that the settling time for each gain setting is optimized.

The simplified Bode plots of Fig. 5 show the individual frequency responses of the over-all amplifier, along with the closed-loop responses for unity gain and a gain of 512. The bandwidth for a closed-loop gain of 512 is determined primarily for first-stage capacitors $C_1$ and $C_2$ and second-stage capacitor $C_1$, all of which assume small values. The 125-kilohertz upper frequency limit is determined by the RC networks of Fig. 2.

The capacitive component and the resistive component of high-impedance node A of the second stage establish the first break point of the amplifier. Since the resistive component is very large, the first break point occurs at a relatively low frequency with only a small value of capacitance, thereby permitting slew rates of several hundred volts per microsecond to be realized.

The second break frequency, at around 4 kHz, is determined by time constants $R_{13}C_1$ and $R_{14}C_2$ in the first stage. The resulting two-pole response reduces the open-loop gain at a rate of 12 dB/octave, which increases slew rate and the high-frequency loop gain more than the 6-dB/octave rate.

The unity-gain bandwidth can be determined by a lag-lead network that is digitally selected at the high impedance node of the second stage, as shown in Fig. 4. This type of unity-gain compensation has the advantage of a 12-db/octave rolloff. Unlike the compensation for a gain of 512, the unity-gain compensation increases bandwidth while decreasing slew rate so that the settling times for the two gain settings are approximately the same. Similarly, opposing compensation networks can be traded off for gain values between unity and 512.

Two additional lead-compensation networks in the first stage (time constants $R_{15}C_1$ and $R_{16}C_2$) and one in the second stage (time constant $2R_eC_2$) complete the over-all amplifier's internal frequency compensation. These three lead networks cancel poles in those cascode transistor pairs that have two natural poles.

The gain degeneration employed throughout the amplifier design stabilizes the lag and lead compensation networks, and provides an over-all gain-bandwidth performance that is determined by passive components, instead of sensitive semiconductor parameters.
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Electronics / November 6, 1972
Choosing the best suppression network for your SCR converter

by L.R. Rice
Westinghouse Power Semiconductor Division, Youngwood, Pa.

Although a wide variety of schemes exists for suppressing the energy transients in semiconductor converters, unfortunately there is no single circuit that fits all needs. Instead, the design engineer must select that network that best suits his particular requirement.

Transients in most power systems arise from rapid electrical-circuit changes, such as energizing and de-energizing of a reactive circuit. Conventional RC suppression circuits will limit the magnitude or rate of rise of transient waveforms, but thyristor circuits generally require controlling the slope of transients. Diodes use shaping to reduce recovery losses.

Inductance is a convenient point to start looking for transient generation. In any practical circuit, a finite inductance exists. This may be caused by the wiring bus, transformer leakage reactance, or an inductance purposely designed into the circuit, such as the transformer windings or a filter choke used in the power supply.

Voltage transients can be caused by interruption of the power-transformer magnetizing current (either opening or closing the on-off switch in the primary winding) by a switching rectifier with an inductive load across the input, or by load switching. Also a dv/dt switch transient can be caused by closing of primary switch or when operating with a fuse, but without a filter network. Load-generated transients, such as over-voltage due to switching of motor load and resulting regeneration, however, pose less of a problem, since they can be easily suppressed by clamping diodes or a dissipative network.

In thyristor circuits, an inductor may cause false anode firing via dv/dt transients. For many circuits, simple RC filters may not sufficiently suppress the transient. This is especially true for converters operating from high-kVA transformerless connections. In these instances, the high device impedance and low bus inductance do not provide enough of a voltage drop, and dv/dt transients as high as 1,000 volts/microsecond can occur.

BIBLIOGRAPHY
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<table>
<thead>
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<th>Circuit</th>
<th>Use</th>
<th>Circuit Limitations</th>
<th>Size</th>
<th>Cost</th>
<th>Complexity</th>
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<td>Clamps voltage across SCR to less than its rated forward blocking voltage, ( V_{FHM} )</td>
<td>Does not control ( dv/dt )</td>
<td>6</td>
<td>5</td>
<td>6</td>
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<td><img src="Image" alt="Circuit Diagram" /></td>
<td>Varistor to increase dissipation with high voltage</td>
<td>Does not control ( dv/dt )</td>
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<td>6</td>
<td>7</td>
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<td><img src="Image" alt="Circuit Diagram" /></td>
<td>Current transient voltage to charging current and lower transient magnitude</td>
<td>Causes high ( dv/dt ) and peak current, needs some line impedance to slow down ( dv/dt )</td>
<td>9</td>
<td>7</td>
<td>9</td>
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<tr>
<td><img src="Image" alt="Circuit Diagram" /></td>
<td>Same as capacitors, but controls ( dv/dt ) shaping with lower ( dv/dt )</td>
<td>Requires a compromise between allowable amounts of ( dv/dt ) and ( dv/dt )</td>
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<td><img src="Image" alt="Circuit Diagram" /></td>
<td>Same as RC types, but an ( h kVA ) source, the inductance provides regulation to allow the RC to work and lower surge current</td>
<td>Usually requires large ( R ) or a high ( L ) to minimize initial current surge. This can be expensive and bulky</td>
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<td>1</td>
<td>4</td>
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<td>Similar to linear inductor but sat reactor lowers size and cost</td>
<td>Diode recovery time must be less than ( 1 \mu s ) or a high ( dv/dt ) is required</td>
<td>4</td>
<td>3</td>
<td>5</td>
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<td><img src="Image" alt="Circuit Diagram" /></td>
<td>Same as RC types, but allows high charging current and low ( dv/dt )</td>
<td>Diodes in the bridge must have recovery times less than ( 1 \mu s ) to minimize ( dv/dt )</td>
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<td>Same as capacitor type for series connection where ( R_1 ) &gt;&gt; ( R ), and ( C_2 &gt;&gt; C_1 )</td>
<td>Same as RC circuit, but with overvoltage protection that causes SCR to turn on before ( V_{FHM} ) is reached</td>
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1. Ranked in descending order
2. 100-A rms device

World Radio History

Electronics/November 6, 1972
Testing power supplies quickly and cheaply

by L. Tatapudi
Washington State University, Pullman, Wash.

In only a few minutes, the line and load regulation of a precision regulated power supply can be measured with an inexpensive test circuit. Usually, expensive test equipment is needed to detect a change of a few millivolts in the supply's output of a few tens of volts. The test circuit shown, (parts less than $30), permits accurate measurements to be made with a dc voltmeter by amplifying the change in power-supply voltage.

The output voltage of the operational amplifier is nulled to zero by adjusting potentiometer $R_P$.

$$V_o = V_2(1 + G) - V_1G$$

where $V_1$ represents the output of the supply under test, $V_2$ the null reference voltage, and $G$ the closed-loop gain of the op amp. If the supply's load and/or line voltage changes, the op-amp's output becomes:

$$V_o = V_2(1 + G) - (V_1 - \Delta V_1)G = \Delta V_1G$$

which is simply the change in supply voltage, $\Delta V_1$, amplified by op-amp gain $G$.

To measure load regulation, adjust potentiometer $R_P$ until a null is obtained at the circuit's output with switch $S_1$ open. Then close the switch, read the voltmeter, and divide this reading by op-amp gain $G$ to find the change in supply voltage. Similarly, line regulation is measured by leaving switch $S_1$ open, changing the supply's ac line voltage from one value to another, and then dividing the resulting voltmeter reading by $G$ to determine the supply's output change.

Op-amp gain, of course, is simply the ratio of feedback resistance to input resistance:

$$G = (R_{1} + R_{TP})/R_{1}$$

For the component values noted, a gain of 100 can be obtained. The circuit equations are accurate within 0.01%, even for a gain of 1,000, provided that the op-amp's open-loop gain is about 100 decibels.

The reference supply voltage, $V_{REF}$, should be at least equal to the output voltage of the supply under test. To measure supply stability, a standard cell can be substituted for $V_{REF}$ and the test run in a reasonably constant ambient environment. Also, components that have low temperature drift should be chosen.

Measuring the supply's temperature coefficient is similar to the regulation measurement. The test circuit should be removed from the test power supply and kept at a reasonably constant ambient temperature.

If an op amp with a drift of 2 microvolts/°C is used, and if temperature varies by 50°C, then the circuit's offset voltage drifts by 10 µV. This change is considerably less than the output-voltage shift of most precision supplies over an eight-hour period or over a temperature range of 0°C to 70°C. The error introduced by the circuit, therefore, becomes practically negligible.

Regulation check. Power-supply line and load regulation can be accurately determined by amplifying supply's output voltage change.

Comparing coaxial cable shielding effectiveness

Radiation from coaxial cables has always been a concern of design engineers. That concern has been intensified by the most recent FCC document on cable TV system radiation, which all CATV systems must now meet. And although these requirements apply to the CATV system as a whole (the cable, connectors, splitters, amplifiers, and other components), the allowable radiation levels for coaxial cables must be kept to a minimum for good shielding effectiveness.

Whether you're looking for a low-cost coaxial cable for short runs that will meet the FCC specification, or merely comparing effectiveness of the different shielding configurations, the following curves should prove helpful. The curves supplied by Belden Corp.'s Electronic division, Chicago, show the results of shielding
effectiveness tests on RG/59/U-type CATV drop cable (for short runs from main cable to a subscriber’s house) from 5 megahertz to 270 MHz.

The top curve illustrates the relative effectiveness of a shielding configuration consisting of Belden Duofoil film-sandwiched aluminum foil, plus a 61% shield coverage of tinned copper braid. The other two curves detail the isolation performance of 59/U-type CATV drop cables without foil and with different amounts of tinned-copper-braid shield.

The middle curve details isolation versus frequency for a cable with 94.5% coverage braid (this kind is usually specified by the military services). The lower curve illustrates the shielding effectiveness of the same grade and style of cable, but with a relatively open 55% coverage braid.

All the curves dip in their values of isolation at about 70 MHz and 200 MHz. These dips result from quarter-wave resonance inherent in the 3-foot cable sample. Changing the sample length does not eliminate these resonance dips—it only alters the frequencies at which they occur.
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Grayhill is in termination hardware because our customers wanted something different.
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NEW Heathkit 2½ Digit DMM only 79.95*
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NEW Heathkit 30 MHz Counter only 169.95*
The Heathkit IB-1100 gives 1 Hz to over 30 MHz counting on a full 5-digit readout with 8-digit capability. The lighted overrange indicator makes misreading virtually impossible. Stable time-base circuitry assures accuracy better than ±3 ppm from 22° to 37° C. Diode protected J-FET gives improved triggering over 100 mV to 150 V input range. Solid-state circuitry mounts on one large board for easy assembly. 6 lbs.

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124 Circle 124 on reader service card

World Radio History

Circle 169 on reader service card
Computerized data bank offered for power transistors

If you need a power transistor, Motorola Semiconductor has a new computerized information bank available to anyone with a time-sharing computer terminal and telephone coupler. There are actually two services—if you have some specs and need to find a type number, you feed in typical parameters—such as $I_e$, $V_{CEO}$, and $h_{FE}$—and the computer lists a number of devices, along with other relevant parameters. Conversely, if you key in a type number, including house numbers from other companies, the computer supplies suitable substitutions with specs—including transistors with relaxed parameters, but consequent lower cost.

The access number is 602-949-7000 (10 characters per second) or 602-949-4221 (30 characters per second), and the computer gives the instructions after you push the originate button on your terminal. There's no charge, other than for the telephone call.

Guide available to control systems

Designers of electromechanical control systems should be interested in a new 12-page guide to electric and electrohydraulic automation that is being offered without charge by Honeywell's Apparatus Controls division, 2727 South Fourth Ave., Minneapolis, Minn. 55408. Entitled "Factory Machinery Controls," the illustrated guide consists mainly of schematic diagrams of systems for controlling such factors as speed, position, force, power, torque, and pressure.

Each diagram is accompanied by a brief description of system operation and key design considerations. Two pages of the guide are devoted to applications formulas and conversion data. Another two pages contain Honeywell catalog information.

Glass-free gold pastes aid bonding

A new family of glass-free gold conductor pastes for application directly on alumina and beryllia ceramics is available from the Electronic Materials division of Owens-Illinois in Toledo, Ohio. The line is called Au 99+.

Glass-free pastes have many advantages. Since there's no glass to interfere with bonding at the upper surface, silicon die bonding and thermo-compression wire bonding are easier. The elimination of glass also does away with the major contributor to resistor and dielectric incompatibility. What's more, the absence of glass at the gold-ceramic interface avoids the significant thermal barrier usually found in thick-film pastes. This, says Owens-Illinois, permits up to 30% greater dissipation of heat.

Seminar scheduled on sampled-data techniques

Attention, all cost-conscious computer users: a seminar called "Recent Developments in Modern Numerical Methods" can help computing costs by teaching you how to use sampled-data techniques to simulate either continuous or discrete processes. The three-day seminar, which will be held in Los Angeles from Dec. 11 to 13, will cover digital and hybrid simulation, digital and hybrid control systems, problem solving on minicomputers, and applied numerical analysis. Software Research Corp., P.O. Box 24564, St. Louis, Mo., is sponsoring the course. The fee is $235.
Think Twice:

What's one of the biggest measurement problems in the computer industry today?

Low Duty-Cycle Measurements—Making timing-pulse adjustments, and finding noise pulses in, or locating missing bits from low duty-cycle digital signals. Countless lost hours and eyes-strain have resulted from this problem—trying to view low rep-rate signals like those found in disc, tape, or drum peripheral units. But with your refresh cycle occurring at such long intervals, coupled with short phosphor persistence, it’s no wonder that you’ve spent an inordinate amount of time making such measurements. And it’s no wonder that you often came out from under your scope hood rubbing your eyes. Well, no more!

Storage CRT With Unmatched 400 cm/s Writing Speed. Hewlett-Packard just made it possible for you to throw away your scope hood by developing a new bright, burn-resistant, high-speed, variable-persistence CRT—available in either 100 cm/μs or 400 cm/μs writing speeds. Placing these new CRTs into an all new mainframe that’s optimized for high-writing-speed storage measurements, HP now gives you a new dimension in storage scopes—the HP 184A. This unique combination offers the variable-persistence mesh storage effect brings your waveforms to life. And for simplicity of operation, we think you’re in for a pleasant surprise when you compare the 184A against the competitive unit.

Variable-Persistence Storage and Standard in One Scope. Further, you’ll find that your 184A is a true general purpose scope that offers you the capability to choose, by way of plug-ins, all the functional features of the HP 180 Series of oscilloscopes, including such items as selectable-input impedance, and sampling to 18 GHz. And for simplicity of operation, we think you’re in for a pleasant surprise when you compare the 184A against the competitive unit.

Superior Technology. HP believes the most important part of a scope system is the CRT—the interface between you and your measurement. As the pioneer in practical applications of dome-mesh magnification, HP was first to expand the size of high-frequency CRT’s to 6 x 10 cm; first to 8 x 10 cm; and first to 10.4 x 13 cm—all in high-frequency mainframes. HP was also the first to use dome-mesh technology to substantially lower power requirements for CRT deflection (making possible the only line of 35 and 75 MHz portable scopes—scopes that really are portable).

Display True Replicas of Your Waveforms. You’ll appreciate being able to adjust persistence down to 0.2 seconds; that’s 75 times lower than a major competitive unit. For those measurements that require faster sweep times, you’ll know you are displaying true replicas of your waveforms when you’re using an HP 184A. Capture low duty-cycle pulse trains, through repetitive sweeps, simply by adjusting the persistence to “maximum,” to build up the intensity of dim traces. This feature in the new 184A oscilloscope lets you do many jobs you previously allocated to expensive, single-shot scope/camera systems.

Burn-Resistant CRT’s. HP placed variable-persistence in many of its scopes including the 181A, 1702A, and 1703A storage units. And now HP has developed, for its current line of storage instruments, carefree CRT’s so highly burn resistant they require little more care than conventional CRT’s. The new 184A high-writing-speed scope also has unprecedented inherent resistance to burns.

Yes, Scopes Are Changing. How many times have you wished for a scope that could display a low rep-rate digital signal brightly and clearly, and one that could also be used for a variety of general purpose measurements. That scope is here now in HP’s 184A storage mainframe, $2200 (for only $500 more, you can boost your 184A’s writing speed to 400 cm/μs), with plug-in capability to 100 MHz real time, or 18 GHz sampling. Think twice; put away your scope viewing hood and call your local HP field engineer for a demo today. Or write for our “No Nonsense Guide to Oscilloscope Selection.” It covers the other members of HP’s variable-persistence storage scopes. Hewlett-Packard, Palo Alto, California 94304. In Europe: P.O. Box 85, CH-1217 Meyrin 2, Geneva, Switzerland. In Japan: YHP, 1-59-1, Yoyogi, Shibuya-Ku, Tokyo, 151.

Scopes Are Changing; Think Twice.

HEWLETT PACKARD

OSCILLOSCOPE SYSTEMS

Circle 127 on reader service card 127
New from Amphenol's Spectrum

MOS/LSI Planar Plug-In connectors (above) for leadless, flat mount ceramic substrates. Permits fast, easy replacement of IC package, no screws, has snap-down lid. Free-standing terminal (below) terminates IC's to PC boards for lowest total systems cost.

Box contact connectors (above) intermate with .025" square or round contacts. Low insertion force. Terminations for crimp, wire wrapping or wave solder. Zero insertion force connectors (below) improve PC board and connector life by eliminating strain and wear.

Above are seven new ideas from Amphenol Industrial Division's Spectrum of interconnection capability. Amphenol's SPECTRUM offers you all four levels of interconnections from our unmatched breadth of product line:

**Level 1 . . . DEVICE TO BOARD OR CHASSIS.** We offer interconnections for components such as tubes, relays, transistors, IC packages, trimmers, resistors or capacitors to a PC board or chassis.

**Level 2 . . . BOARD TO MOTHERBOARD OR BACK PLANE.** We offer interconnections for PC boards or other sub-circuit modules to a motherboard or to a back plane.

**Level 3 . . . MOTHERBOARD OR BACK PLANE WIRING.** We offer interconnections for levels to each other and to other sub-circuits with multi-layer circuit boards, wire wrapping, clip terminations, jumper techniques and dip-soldering.

**Level 4 . . . INPUT/OUTPUT CONNECTIONS.** We offer interconnections for power and signals to and from a system. This interface may be between sub-assemblies within the same enclosure or between individual units.
of interconnections.

Low cost strip connectors (above) are used as jumpers in back plane wiring. Intermates with .025" square or round posts. Circuit Concentration Bay (below) consists of wire wrapable panels that are five times as compact as the telephone distribution frames they replace.

Modular Integral Connector concept lets you make your own pin & socket connector to fit your needs. Five contact sizes, thousands of combinations. Sufficient components for six connectors in handy MIC-KIT. Design and assemble your own prototypes.

From the simple tube socket—to a myriad of electrical/electronic connectors—to complete and complex termination systems . . . SPECTRUM.

But SPECTRUM is far more than products. It is a depth of capability in engineering, manufacturing and quality control. Amphenol's SPECTRUM is a new height of service, availability and distribution backed by seven Amphenol interconnection-oriented divisions.

Amphenol can fulfill your total interconnection requirements because we are not limited to specifics such as one or two product lines, one or two levels.

Therefore we approach your interconnection needs with complete open-mindedness.

For more new ideas and specific information, write for your copy of “SPECTRUM.” Amphenol Industrial Division, Bunker Ramo Corp., 1830 South 54th Ave., Chicago, Illinois 60650.
If you do, you are fortunate.
If you do not, you are unfortunate. Because whether you own one or not, you are most assuredly helping to pay for one.

Somebody has to. A featherbed is an unnecessary job that pays somebody for doing nothing. And for every somebody who is paid for not working, there has to be a somebody who does work, to foot the bill.

There are all kinds of featherbeds in this rich and benignly negligent country.
The most visible, and the most publicized, carry a union label. They are the result of quite open and perfectly legal agreements to pay some specially favored people for doing nothing—or as next-to-nothing as human ingenuity can devise.

But there are others. Some of the plusthest of all featherbeds are to be found, cleverly camouflaged, in executive suites. Some of the snuggest are built into the very structure of federal, state and local bureaucracies. Some of the coziest are discreetly tucked away in the private recesses of the various professional establishments. And some of the most sumptuous are those precious family heirlooms that are generously handed down from generation to generation.

No one knows how many featherbeds there are in the U.S. No one knows how much the total bill for featherbedding actually comes to. But there are some things we do know, and others we can surmise.

In the construction industry, for example, we know that featherbedding is open, unabashed and rampant. According to a survey by Engineering News-Record, anywhere from 15% to 40% of the construction payroll dollar goes to pay for work not done. For time wasted in adherence to restrictive work rules, or for time spent in meaningless, unproductive activities.

The cost of this sanctioned, legalized waste in the construction industry is an estimated $16-billion a year. Which is $16-billion added, unnecessarily, to the cost of everything built in this country—homes, apartments, stores, factories, roads, highways, bridges, schools, churches and hospitals.

Executive and white-collar featherbedding is less visible and hopefully, less prevalent. But it is painfully apparent that, judging by the results, somebody, somewhere, has too often been paid too much for doing too little. At a cost reckoned in inefficient and ailing companies, lagging and troubled industries, and spectacular failures and bankruptcies.

With regard to the ancient and apparently ordained institution of bureaucratic featherbedding, we know that the combined federal, state and local government payroll has increased 88% in the last ten years, to a total of $110-billion. Today there are more government employees (14.4-million of them), making more money (average salaries up 64%). But if there has been a corresponding increase in bureaucratic efficiency, or the quality of government services, it has escaped the attention of most taxpayers.

Featherbedding in the professions is, in the nature of things, a moot question. Mere laymen can only guess at what goes on behind the impenetrable screen of fraternal solidarity and lofty mystique. But even mere laymen, when they pay their bills, are painfully aware that, of all the costs of living in a fantastically expensive world, the cost of professional services has increased the most, with the most devastating impact.

Finally, we know that the American economy as a whole has become markedly less productive, at a cost in terms of lost output of about $60-billion in the last two years. Part of the decline in productivity, and part of the
featherbed?

$60-billion loss, surely must be charged against the featherbed account.

Any attempt to define the nature and suggest the extent of featherbedding in our society runs the risk of misinterpretation. In spite of the very obvious fact that the overwhelming majority of union members, of business men and white-collar workers, of government employees, and of doctors, lawyers, engineers and educators, belong to and make up the working majority.

Any attempt to quantify the total cost of featherbedding in the U.S. runs an even greater risk. It is almost certain to be wrong. But at whatever risk, it must be said. The real extent of featherbedding, and the real cost, can be summed up in two words—too much!

Because featherbedding, whatever else it is, is clearly waste. Deliberate, purposeless, wanton waste of time, money, energy, effort, talent and spirit.

And no economic system, whatever its strengths and capacities, can tolerate endless and unlimited waste. At some point, the system becomes not just markedly less productive, but fatally less productive. Costs mount, prices and taxes rise—and keep on rising, ever faster, until the system breaks down.

The American economic system is not at, or near, the breakdown point. But it is at the point where most of us are finding that, in every area of our lives, we are paying progressively more and more for less and less.

Part of what we are paying is the cost of deliberate, needless waste, with its cancerous effect on productivity. So that the real problem with featherbedding becomes clear.

The problem is not that some people, by hook or by crook, are getting something for nothing. It is that a lot of people—most Americans—are increasingly getting nothing for something.

The problem is not that featherbedding is a cynical con game, played by a favored few at the expense of the tolerant and permissive many. The problem is that it is a losing game, played or permitted at the common and disastrous expense of us all.

So that the question for the working majority is not, how much featherbedding will we accept? But, quite simply, how much featherbedding can we afford?

And the issue for the working majority—and for featherbedders and would-be featherbedders as well—is, even more plainly and directly, how much farther can we go with a losing game?

The answer in both cases is clear and compelling.

No more! And no farther!

We at McGraw-Hill believe in the interdependence of American society. We believe that, particularly among the major groups—business, professions, labor and government—there is too little recognition of our mutual dependence, and of our respective contributions. And we believe that it is the responsibility of the media to improve this recognition.

This is the fifth of a series of editorial messages on a variety of significant subjects that we hope will contribute to a broader understanding.

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John R. Emery, President
New gallium phosphide LEDs from Microsystems International—in red and green.

That's right, a line of red and green LEDs offering low, low operating current levels of 5mA-10mA, I.C. compatibility and bright (the brightest you've ever seen) with wide viewing angles of 90° each side of normal. All this made possible by Microsystems' gallium phosphide technology and unique optical designs.

At the top of the line, our panel-mount MA2300 series (the one in the foreground of the photo), with its built-in lens/reflect system produces a sparkling 2.0mcd luminous intensity at I = 5mA. On its left is the MA2200 series, the same lamp, but with axial leads.

Just behind the MA2300, is the MA2400 series in the industry accepted panel-mount package. It produces a glowing 1.5mcd at 10mA—compare this with other standard lamps. At the far right is the MA2500 series in a standard TO-18 header, and putting out 0.4mcd at 10mA.

For the colour conscious designer there are optional: clear, clear diffused, tinted clear, or tinted diffused epoxy packages. Just about any colour and package combination for your signal and indicator lamp applications—and they're available now at competitive prices.

Gallium phosphide LEDs from the performance leader Microsystems International

For further information—call or write your nearest Microsystems sales office or distributor.
New products

Calculator has full Basic capability

H-P’s top-of-the-line 9830 can access time-shared computers directly; 40-kilobyte desktop unit comes with built-in cassette memory

by Stephen Wm. Fields, San Francisco bureau manager

Calculators have been rapidly approaching the capability of small computers. One recent development [Electronics, Sept. 25, p. 129] is a calculator that has special keys that perform program functions in Basic, a high-level language. And now Hewlett-Packard Co. has developed a calculator that is completely Basic-compatible—in fact, the machine performs more like a computer with a keyboard and display than a calculator; yet, it is as simple to use as a calculator.

The new model 7830, which bridges the gap between traditional calculators and minicomputers, employs H-P Basic (the same as GE Basic), has an alphanumeric keyboard and display, and comes complete with a built-in cassette memory. An optional high-speed, page-width printer is also available.

As the top of the H-P 9800 calculator line, the 40-kilobyte system is described as the world’s most powerful desktop calculator. It has a 15-kilobyte operating system built in and ready to run as soon as the calculator is turned on. This feature, implemented in read-only memory, means that the user can immediately use the system—the calculator need not be loaded prior to use. The model 30 is equivalent to a 10- or 12-kilobyte minicomputer that must store its compiler in read/write memory.

LED display. Instructions and programs in the Basic language are typed in through the standard typewriter keyboard and displayed on the 32-character, light-emitting-diode alphanumeric display. A built-in memory, with a capacity of 80 kilobytes in each cassette, stores data and programs in a file structure that the calculator user specifies.

The cassette also has read/write ability so that the user can read a file, modify it if desired, and return it to the same location. The cassette, with bidirectional search, has interrupt capability, which permits simultaneous calculator operation and cassette file search.

The built-in cassette is for program, data, or special-function key storage. In addition to the internal cassette, up to nine peripheral cassettes (H-P model 9865A) can be operated with the calculator.

Quiet. The new 9866A page-width printer, designed specifically for the model 30, is a quiet thermal printer capable of printing 80 alphanumeric characters per line at 250 lines per minute, or more than 330 characters per second. Characters are generated from a 5-by-7 dot matrix. The printer, which mounts on top of the calculator, may be added at any time. It also may be replaced by a 9861A typewriter with no change in software.

Calculator memory is expandable both by adding the user’s read/write memory, and by plug-in ROM blocks pioneered by H-P in previous desktop calculators. A wide range of peripherals is also available. The model 30 calculates results to 12 significant digits. All trigonometric functions are built in—a special plug-in ROM block is not required.

Numbers may be entered from the typewriter keyboard or, for easier and faster numerical entry, through a duplicate set of keys in the standard adding-machine format to the right of the keyboard. A set of 10 special function keys completes the keyboard.

The machine has several program-editing features. With editing keys, the user can delete, modify, or correct program lines or individual characters within a line—there is no need to retype an entire line to change one character.

Errors are detected immediately, with an error note appearing on the display. Any part or all of a program may be listed in the printer for error analysis, and any line may be recalled to the display by the “fetch” key. If an error note appears as a line is entered into the calculator, the “recall” key brings it back into the display for analysis and correction.

A 32-character LED display indicates keyboard entries, program steps, instructions, and results of calculations. It consists of 9/16-inch-high characters made up of a 5-by-7 matrix, and not bar segments. Thus, numbers, letters, and symbols are more easily read.

End of line. When more than 32 characters are entered, the display automatically shifts to the left as ad-

Power. The H-P 7830 calculator performs like a computer with a keyboard and display.
Now available to help you:

Secrets of SUCCESSFUL JOB HUNTING

Looking for a better job?
Out of a job?
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Compiled from the pages of CHEMICAL ENGINEERING, Secrets of Successful Job Hunting, brings you the combined wisdom of 11 job-hunting specialists. In its pages you'll learn how to find and generate job offers... how to launch a job-hunting campaign, either in person or by mail... how to negotiate your salary... how to prepare for and handle your interviewer... how to evaluate the job offers you get. But most of all you'll learn the real secret of successful job hunting: How to sell yourself.

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Your Job-Hunting EQ*

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<td>5. Always state your exact salary requirements</td>
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<td>6. A quick thank-you note makes you seem overanxious</td>
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<td>9. Ask for a 10-20% salary increase in a new job</td>
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<td>10. Type as many carbons as possible of your resume</td>
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*Effectiveness Quotient. Answers will be found in Secrets of Successful Job Hunting.

Attention: Miss Janice Ruvere
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New York, N. Y. 10020

☐ Yes, I want to know the secrets of successful job hunting. Enclosed is my check (money order) for $ for copies of Secrets of Successful Job Hunting. I understand that if I am not completely satisfied with the book, I can return it within 10 days and my money will be refunded.

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Circle 134 on reader service card
New products

Additional characters are keyed in. To go back to the beginning of a line, a right-hand arrow key is pressed; a left-hand arrow key moves the display in the opposite direction.

Ten special-function keys (in the upper left of the keyboard) can each have two special functions assigned for a maximum of 20 special functions. These keys may be defined in three ways. Each may be defined as a string of commonly used characters, such as print, go to next, and SQR. Pressing a key causes the mnemonic to be typed on the display, which saves typing each mnemonic into the calculator letter by letter.

Each key may also represent single or multiline functions. Different parameters can be passed to the function from the main program, or between functions. Each key may also store an entire program. Programming and editing rules are the same as those for normal programming. A template, with blanks in which the user can write his key definitions, is provided. All special functions can be stored on the cassette. Thus, the model 30 has all of the advantages of a "keyboard Basic" machine, but it also has a full alphanumeric keyboard.

Add-on. The memory of the model 30 can be expanded in two ways. The user read/write memory can be expanded from 4 kilobytes to 8 kilobytes. ROMs can be added in 4-kilobyte increments to a total of 16.

The model 30 offers the user flexibility that has never been available before. Probably most important is that, since the model 30 is completely Basic-compatible, it can be interfaced with other Basic systems, such as time-shared computers, to take advantage of their large memories.

The machine’s capability can also be increased through the plug-in ROMS. Eight of these can be used with the model 30—five plug into a compartment in the side of the calculator, and three go inside the machine. Plug-ins are available either in the cigarette-package size for the five outside slots, or as printed-circuit cards for more permanent installation inside. The ROMS are also easy to use—there are no keys specifically assigned to plug-in blocks; in other words, the use of the ROM blocks is not keyboard-limited. The user simply calls for the function from the alpha keyboard as if it were hard-wired into the machine.

ROMS are available for matrix operation, string-variable operation, X-Y plotter control, and an extended I/O ROM that permits instruments and other peripherals to be connected. Thus the calculator can be the heart of a complete test system, including voltmeters, counters, and plotters. A fifth ROM, one that will allow the model 30 to be connected to other computer systems via a modem, will be available early in 1973.

The basic model 30, complete with 4 kilobytes of read/write memory, cassette drive, keyboard, and display, sells for $5,975; the optional full-width page printer sells for $2,975; optional read/write memory is $1,475 for another 4 kilobytes, and the add-on ROMS sell for $485 each. Delivery is scheduled for early 1973.

Inquiries Manager, Hewlett-Packard Co., 1501 Page Mill Rd., Palo Alto, Calif. 94304 [338]
New products

Instruments

**Servo upgrades audio recorder**

Kit transforms unit for instrumentation-quality recording up to 20 kHz

There are many high-quality instrumentation tape recorders on the market, but many applications don’t require an $8,000 machine. For example, people working on acoustic testing, vibration analysis, or transient-performance testing can use a high-quality audio tape recorder for their work if the timing accuracy is good and if the tape flutter is low. However, most audio tape recorders don’t meet those requirements.

But by taking one of the industry’s leading audio tape recorders—the Ampex AG 440—and adding a capstan servo kit to it, Ampex engineers have come up with an economical solution to recording instrumentation quality signals in the 30-Hz to 20-kHz range. The servo is available either as an option on new machines or as a kit for field installation on existing recorders.

Basically, the servo consists of a dc capstan motor, which is driven by a high-frequency oscillator. Thus, fluctuation associated with line variations is eliminated. To further reduce speed errors, a single shaft is used to mount the dc motor, tachometer, and tape-drive capstan—there is no belt slippage because there are no belts. Mark Sanders, designer of the servo, claims that this combination of isolation from ac line voltage variations, plus direct drive, provides tape speed accuracy to within ±0.08%. Unweighted flutter at 7.5 inches per second is typically 0.03%.

Besides operating from an internal reference, the servo can be connected to an external 9,600-Hz source. Sanders points out that servos have been used with audio transports before, “but these have been velocity servos,” he says. “The velocity servo is not as accurate as the comparator servo that is used in the 440, because with the velocity servo there is some error signal.”

The servo is available on new machines for $325, in addition to the $2,250 to $3,500 for the 1/4-in.-tape versions of the AG 440. The retrofit kit sells for $650. Delivery time is 90 days.

Ampex Corp, Professional Audio Products Division, 401 Broadway, Redwood City, Calif. 94063 [351]

Oscilloscope plug-in offers delay by time and by events

Delay by time and delay by number of events are features offered by a 7000 series oscilloscope plug-in, the 7D11 digital delay unit. These delays enhance scope waveform viewing and are available as output signals for other applications. In delay time, following a trigger and after a preselected time, the unit will give a delayed trigger output. The delay time is indicated on the scope CRT readout and is displayed along with the measured signal. In delay by events, following a selectable number of events after a master sync or index pulse, the unit provides delay outputs. Accuracy is to within 0.5 part per million ±2 nanoseconds. Jitter is less than 2.2 ns, delay time

is 100 ns to 1 s, and resolution is 1 ns. Price is $1,475.

Tektronix Inc., P.O. Box 500, Beaverton, Ore. 97005 [353]

Voltage calibrator/reference offers standard-cell accuracy

The model MV115/B calibrator-transfer standard provides full-scale voltage ranges of from 1.111110 vdc to 1.111110 vdc to accuracies within ±0.005%—within unsaturated standard-cell error tolerances. Features include a circuit condition indicator to warn the operator of short circuit or malfunction. A polarity switch permits reversal of output polarity between floating terminals for zero voltage reference check, and provides a method for checking ambient temperature references in dc thermocouple applications. Price is $820. A rack-mounted version is $835.

Electronic Development Corp., 11 Hamlin St., Boston, Mass. 02127 [354]

Recorder provides eight extra-wide channels

A portable, direct-writing, eight-channel recorder is designated the Super 8 and is a complete unit, including high-speed galvanometer,
Q.1 Who's got a primerless, non-corrosive adhesive/sealant?
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Q.3 How can I cut prototype mold costs by 25%?
Q.4 What's a practical way to protect delicate parts from shock?

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A2 Definitely. With GE Silicone Rubber. It improves TV set performance because its electrical properties are far superior to those of other elastomers. And because it takes less material to do the job with silicone rubber, you save space and weight. Fire resistance? GE Silicone Rubber meets all the latest TV industry safety requirements. It's perfect for wire insulation, corona rings and anode caps. Circle Reader Service No. 92.

A3 Use GE RTV-700, the strong, two-part silicone mold-making compound that needs no postbake, cures in 24 hours and has the high tear strength and elongation to reproduce precision parts quickly and accurately. Circle Reader Service No. 93.

A4 With GE RTV-619 Silicone Gel. It cures at room temperature into a clear, resilient, dielectric gel cushion for circuitry and for protecting electronic assemblies. RTV-619 cures without exotherm and can withstand temperatures from —65°C to +150°C. Circle Reader Service No. 94.

For all the details, write: Section N 11374 Silicone Products Dept., General Electric Co., Waterford, N.Y. 12188.

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Portable ohmmeter checks low resistance values

The circuitry of a precision micro-ohmmeter sends through its pulse probes a 50-ampere, 10-millisecond pulse to the test device or component once every second. The unit is designed for nondestructive resistance measurements, and employs a four-terminal measuring technique. Due to the current-pulsing technique used, the unit simulates an actual circuit condition for determining the quality of electromechanical properties of component heat-sink modules and for detecting high-resistance joints caused by poor contacts or corrosion.


Wattmeter measures pulsed rf systems, is portable

Operation from ac lines or batteries is offered by the model 4314 portable peak- or average-reading directional wattmeter. In addition to continuous-wave, average-power measurement, the unit is designed to measure pulsed-rf systems such as radar, telemetry, air navigational aids, television, command and control, and single-sideband peak envelope power. To read the peak of power pulses, the peak read button is depressed and locked, an action that inserts a peak reading servo amplifier between the demodulated pulse delivered by the plug-in sensing element and the meter. Price is $625 and the plug-in elements range from $32 to $75.

Bird Electronic Corp., 30303 Aurora Rd., Cleveland, Ohio 44139 [356]

Generator offers ramp times from 1,000 s to 1 µs

The model 180 is a pulser containing two independent ramp generators with ramp times from 1,000 seconds to 1 microsecond. The generators may be operated independently or synchronized for 1:1, 2:1, and 4:1 interface. Two independent power amplifiers offer ±10 V of variable dc offset, 80-decibel step attenuation in 10-db steps and 20 db continuously variable between steps. Trigger and gate modes are provided allowing independent single-shot and burst operation by...
application of an external trigger or gate, or by depressing a front-panel pushbutton. Price is $845.

Exact Electronics Inc., 455 S.E. Second Ave., Hillsboro, Ore. 97123 [358]

Digital voltmeter operates up to 800 megahertz

A digital voltmeter called the model PM2422 offers three-digit resolution and an overrange digit in any of five ranges of ac or dc current and voltage, and six ranges of resistance. Accessories extend the unit's measuring capabilities to 800 MHz for rf potentials as high as 16 V rms, to 30 kV dc and 100 amperes at 400 Hz. Maximum ac measurement error is ±(0.2%+2 digits) over most of the instrument's bandwidth of 30 Hz to 30 kHz with a maximum error of 1.0% at 30 kHz. Price is $395. Accessories range from $20 to $40.

Test & Measuring Instruments Inc., 224 Duffy Ave., Hicksville, N.Y. 11802 [359]

Spectrum analyzer extends range of time compression

A series of real-time spectrum analyzer/digital integrators features extended time-compression range, increased dynamic range, and digital exponential averaging in the integrator. The models 51B-54B provide time-compression analysis up to 50 kHz in addition to a 1-MHz scale and increased dynamic range through the use of a 10-bit analog-to-digital converter. Also included in the integrator are linear and peak hold modes.

Signal Analysis Industries Corp., 595 Old Willets Path, Hauppauge, N.Y. 11787 [360]

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We make them for both stripline and PC mounting. And we make them miniature—just 0.250" diameter. With Q typically 2500 at 1MHz and temperature characteristics like these:

<table>
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<tr>
<th>Temperature</th>
<th>Capacity Change (%)</th>
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<tr>
<td>-55°C</td>
<td>±3.0 Max., ±0.5 Min.</td>
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<td>+85°C</td>
<td>±1.0 Max., ±3.0 Min.</td>
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<tr>
<td>+125°C</td>
<td>0 Max., -5.0 Min.</td>
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Worth looking into? All it costs is a stamp.

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Packaging & Production

**Tester is Programmable**

Designed for semiconductor memory users, it exercises whole array or any section

A user of semiconductor memories needs test equipment that takes care of three requirements—engineering evaluation, quality assurance, and production testing. All three needs can be filled by a programmable exerciser, called the model 4604, introduced by Technitrol Inc. The unit, designed primarily to test semiconductor memories, will test anything that can be plugged into it.

The exerciser is a special-purpose computer, programmed by a series of instructions that specify the test pattern—a pattern of any necessary degree of complexity that may cover the entire memory array or any part of it. Complex patterns are programmed and executed by a relatively simple program that contains one or more iterative loops, by which the program works its way step by step across the array.

The first time a program is loaded into the 4604, it must be set up manually by the switches on the console. The program can then be stored on a tape cassette.

Each test consists of a sequence of binary word pairs; the first word is the instruction, and the second contains the address on which that instruction is performed. Each word contains 40 bits. Each instruction-word bit corresponds to a separate instruction, and 20 bits in the address word refer to a maximum of 1,048,576 locations. These 20 bits, however, are divided into four different fields that can refer, for example, to address segments, such as the row and column on a chip, or to specific cards in a system. The other 20 bits are unused. No instruction coding is necessary.

Tests are executed at any speed from 50 kilohertz to 10 megahertz, as determined by a switch setting on the console. When stored in the cassette, this setting is represented as part of a program. If the dynamic memory being tested must be refreshed from time to time, the refresh cycle can be programmed to occur with priority over other testing cycles. These refresh intervals are specified by another switch setting, which can be either manual or become part of the program. This enables the memory to be tested to ensure that it operates properly at the minimum refresh rate specified by the manufacturer.

The basic machine has a capacity of 16 words or eight instruction-address word pairs, expandable up to 128 words or 64 pairs. Price range is $29,000 to $39,000, depending on the program memory size.


**Positive artwork used to make prototype boards**

Making prototype circuit boards can be a frustrating and time-consuming operation, but Vector Electronics has developed a method that can eliminate much of the bother—the need for making a negative of the artwork. The technique, which can be used for multiple copies, provides high resolution with minimum undercutting.

The Vector method requires artwork to be prepared directly on a clear Mylar sheet for exposing the board. This artwork can be changed easily. The key to the process is Vector's direct-positive resist coating for the boards. Vector supplies boards precoated with this type of resist at a price similar to that for conventional photoresists. The boards are supplied, either punched or unpunched, in both phenolic and epoxy-glass materials, and in numerous shapes and sizes.

The boards can be exposed by sunlight or by conventional photolamp bulbs, then developed with a special developer supplied by Vector. Each step can take as little as a few minutes, depending on the ultraviolet content of the light. Etching procedure is conventional; the kits include plastic bags of etchant to be mixed with hot water for use in this application.

The artwork can be prepared in a number of ways on the Mylar: the Vector kits include opaque film, pre-printed patterns, tape for conductors, and transfer resist that can also be used on the boards themselves. Two kits are available, a sampler (32X) at $8.95 and a larger one (32XA) at $24.95. The larger kit includes five phenolic boards, etchant, developer, glass plate, clear Mylar film, artwork materials, touchup resist, and grid paper. The materials are also available in bulk.

Vector Electronics Co., 12460 Gladstone Ave., Sylmar, Calif. 91342 [392]

**Mounting trays provide predrilled, tapped rails**

To accommodate high-density packaging of integrated circuits, mounting trays provide predrilled and tapped rails for direct socket mounting in side-buttting positions. Socket density of a 20-inch tray is 117 devices maximum, while maximum IC density is 585 units. Seventeen-inch trays are also available, and both sizes come with or without straight or tilted sides.

Cambridge Thermionic Corp., 445 Concord Ave., Cambridge, Mass. 02138 [394]

**Parts collection system is for use with hand test fixtures**

A parts collection system, designated the Auto Collector model 008, is designed for use with hand test...
Our filter connectors are designed to eliminate interference from your circuits. See those attenuation curves? They are just a part of our selection. We can mix and match filters to solve your low pass filtering requirements. Small wonder Bendix filter connectors are first choice in the fight against electronic noise pollution.

Bendix filters come packaged in connectors intermateable with MIL-C-26482, MIL-C-83723, MIL-C-38999, and MIL-C-5015 connectors. In addition, filter contacts can be packaged to mate with other popular connector types including rectangular in military, industrial and commercial applications. There’s sure to be one to meet your attenuation and frequency requirements.

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You get ceramic substrates quickly from Coors, regardless of order size. That’s because we’re one of the largest producers of ceramic substrates. And have one of the most modern production facilities. And lots of experience in the business.

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New products

fixtures or can be integrated into automatic handling systems by the user. The unit is available with a choice of standard categories up to 13. It is self-powered or can be directly programed by the tester via switch closures. The 008 is a positive binning system and can provide 13-category sort rates to 10,000 per hour with test times of about 100 ms.

Engineered Automation, Division of A-B Tool and Mfg. Inc., High Bridge, N.J. 08829 [395]

Microscope designed for device production line

Optical inspection of semiconductors on the production line is possible with the model KK08 semiconductor microscope. The optics attached to the microscope provide bright-field, dark-field, and interference contrast, and the unit uses a high-intensity halogen source for the vertical illuminator. Defects such as pinholes, stacking faults, alignment errors, mechanical damage, bonding defects, and etching problems are detectable in three dimensions or in color.

Carl Zeiss Inc., 444 Fifth Ave., New York, N.Y. 10018 [396]

Connectors use individual pressure-sensitive seals

Connectors, designated series C-21, are designed to provide moisture-sealing capability by means of individual pressure-sensitive seals that are attached to each contact. Two other seals are included—one at the rear where the wire is attached to the contact, and the other at the link between the pin and the socket. Both seals are designed so that a pressure differential between the inside and the outside of the connector, which is normally a cause of sealing failure, will, instead, improve the seal. The units are designed for use in airborne equipment, shipboard and undersea applications, and in deep space and electronic equipment requiring highly reliable moisture-sealing in harsh environments.

Hughes Connecting Devices, 500 Superior Ave., Newport Beach, Calif. 92663 [393]

Laser scribe operates with continuous stream of pulses

The model 900 mini Laserscribe is a semiconductor wafer-scribing system that employs a continuous stream of focused, high-intensity and overlapping laser pulses. This rapidly heats the surfaces of the semiconductor materials above their vaporization point. The unit can scribe all types of semiconductor wafers including silicon, germanium, gallium arsenide, and gallium
phosphide. It can also scribe passivated or coated wafers such as oxides, nitrides, and metal film and glass overcoats. Price is $22,500, or $19,900 if the purchaser can supply a Tempress model 1713C laser system for modification and integration with the new one.

Quantronix Corp., 225 Engineers Rd., Smithtown, N.Y. 11787 [397]

Computer hook-up wire uses new insulation

A computer hook-up wire is extruded from Tefzel, a material that has characteristics similar to those of Teflon. Tefzel provides a high-temperature thin-wall wire, suitable for wire-wrapping applications. The wire has high cut-through, abrasion resistance and long flex life. The dielectric constant is 2.6, and temperature range is from −100 to +150°C continuous.

Apha Wire Corp., 711 Lidgerwood Ave., Elizabeth, N.J. 07207 [398]

Wire-wrapped connectors are for dense packaging

In a series designed specifically for dense-packaging applications, wrapped-wire connectors have a 0.025-inch-square cross-section. The 30/60 pin types offer replaceable contacts with bifurcated mating surfaces for low contact resistance and high reliability. The contacts are on 0.125-inch centers, and over-all length is 4.555 inches. Removable polarizing keys may be placed between the contacts as required. Price is as low as $1.41 each.

Methode Electronics Inc., 7447 West Wilson Ave., Chicago, Ill. 60656 [399]

Silicon Rectifiers

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<td>All series available with fast recovery characteristics.</td>
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<td>High reliability at economical cost</td>
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<td>$1.49 ea (VG20, 20KV PRV, 1000 qty)</td>
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Electronics/November 6, 1972 Circle 170 on reader service card

Circle 143 on reader service card
Terminal offers four data rates

Automatic send-receive unit with non-impact printer includes twin cassettes

Extending its Silent 700 series of electronic data terminals, Texas Instruments has added a low-priced keyboard send-receive model plus a twin-cassette automatic send-receive type. Both include thermal printers. At the same time, TI announced reductions in prices for existing models in the Silent 700 series.

The new 733 KSR model, selling for $1,500 in single quantities, can be upgraded to the second new model, the 733 ASR, with the addition of an upper cassette module. The ASR version, at $2,750, features switch-selectable data transmission rates of 10, 15, 30 and, optionally, 120 characters per second. In addition, the twin-cassette model offers simultaneous transmit and receive and on-line transmission, and off-line data preparation.

The 733 KSR sells for $1,500 and leases for $75 a month.

Texas Instruments, Digital Systems Div., P.O. Box 1444, Houston, Texas 77001 [361]

Assembly of modules generates display vectors

Most makers of precision graphics systems build their own vector generators. But manufacturers now can buy a vector generator subassembly—a 7- by 8-inch printed-circuit board with 12 interconnected function modules already on the board—and plug it into a standard 44-pin edge connector. This VG110 unit, developed by Intrinsics Inc., will sell for about $750.

The VG110 unit, developed by Intrinsics Inc., will sell for about $750.

Card reader is aimed at data-terminal applications

Designed for data-terminal applications and matched to minicomputer performance, the model

New products
8020 card reader offers reading speed geared to the data-transfer rates commonly used for data communications. Reading only full-size 80-column cards at 200 cards per minute, the unit is priced at $980 in OEM quantities. Another model, the 8045, which reads pencil-marked or punched 80-column cards, sells for $2,265; and a third, the model 8803, for IBM Systems/3 users, handles 80-column cards and stubs, 96-column cards and 96-column stubs. It is priced at $6,800.

Two options are available for the 8020: a mark/hole reading capability and an RS232C communications interface.

Bridge Data Products Inc., 738 South 42nd St., Philadelphia, Pa. 19104 [363]

Data terminals built for remote job entry, batching

The DT1000 series of data terminals is designed for applications in remote job entry and batch processing. The units, which are IBM-compatible, can also be used as data-entry keystations and for media conversion, in addition to applications in optical character readers, magnetic-link character readers, point-of-sale, and factory data-collection systems. The basic DT1000 consists of a data-entry keyboard, a control panel to select operating modes, a display panel, communications electronics, and a magnetic-tape drive. Input/output peripherals include a card reader, paper-tape reader, line printer, and serial-character printer. Price for the basic configuration ranges from $4,000 to $6,000.

Pertec, 10880 Wilshire Blvd., Los Angeles, Calif. 90024 [364]

Card reader transmits pertinent data only

Remote entry of card data to time-shared computers is provided by the model 100 card reader. The unit transmits only leading spaces and data, suppressing trailing spaces so that only pertinent data is transmitted. Data conversion from Hollerith code to eight-bit ASCII is standard, and interfacing is EIA RS-232C compatible, with a choice of even, odd, or no parity. Transmission rates are from 110 baud to 1,200 baud in either half- or full-duplex. Fully programmable automatic codes accompany transmissions to provide control characters to the computer. Price of the card reader is $2,875.

Omega Data Processing, 180 Valley Rd., Wayne, N.J. 07470 [366]

Magnetic heads permit drive speeds to 300 in./s

A line of digital heads for tape drives provides increased access time and higher transfer rates, in addition to greater storage capacity per tape reel and self-threading capability. The units operate at speeds to 300 inches per second with a density of 3,200 bits per inch, phase-encoded, at a bit transfer rate of 960 kilohertz. A head profile maintains head-to-tape contact over the entire speed and tension range to provide minimum spacing loss and good forward/reverse signal ratio.

Nortronics Co. Inc., 8101 10th Avenue North, Minneapolis, Minn. 55427 [368]
Semiconductors

Rate multiplier draws 250 nW

Low-power C-MOS device performs arithmetic and algebraic functions.

Taking advantage of the low power characteristic of complementary-metal-oxide semiconductors, Motorola has developed a binary-coded-decimal rate multiplier that performs arithmetic and algebraic functions, and draws only 250 nano-watts quiescent at 5 volts dc and 25°C.

Designated the MC14527, the multiplier has two inputs, one for a pulse frequency, and the other for a BCD number. The output is proportional to the product of the two; for example, six pulses emerge for every 10 input pulses if the BCD number is six. This property can be used to add, subtract, divide, raise to a power, and to solve algebraic and differential equations. It can also be used to generate trigonometric functions and natural logarithms.

The MC14527 can also be used in digital filtering, motor speed control, and frequency synthesis applications.

In addition to its low power drain, the new multiplier has high noise immunity, typically 45% of the drain voltage, and a supply voltage that can be as low as 3 V, or as high as 16 or 18 V.

The part is internally synchronized for high-speed operation (up to 5 megahertz typically). A strobe input permits the output to be inhibited or enabled, and the device output count occurs on the convenient, positive-going clock input. Complementary outputs are provided, and the device can operate in either fixed- or variable-rate mode. Two or more of the parts can be operated in cascade, and a special “9” output is available for this use.

Maximum zero-output level at 25°C and 10-v drain supply is 0.01 V, and minimum one-output level is 9.99 V. Output drive current is typically –0.9 mA at 9.5-V output (p-channel) and 1.6 mA (n-channel).

Two versions of the MC14527 are supplied, both in 16-pin ceramic dual in-line packages, one with an AL suffix, for –55°C to +125°C, and one with a CL suffix, for –40° to +85°C. The 100-quantity prices are $11.85 and $6.60.

Motorola Semiconductor Products Inc., Technical Information Center, P.O. Box 20924, Phoenix, Ariz. 85036 [411]

Chip drivers designed for gas-discharge readouts

The increasing popularity of Panoplex-type gas-discharge displays in calculators and digital clocks has created a demand for a new type of integrated-circuit driver—one that can generate the high voltages that are characteristic of discrete transistors, rather than ICs. To meet that need, the mono DRV-01 has been built by Precision Monolithics Inc., Santa Clara, Calif. The device is an array of five high-breakdown cathode-segment drivers constructed on a single monolithic chip. Each driver consists of a high-voltage—145 volts minimum guaranteed breakdown—transistor, along with two resistors and a diode that provides dc restoration when the device is employed in ac-coupled multiplex configurations. The input of the -01 is compatible with MOS logic levels.

Garth Wilson, engineering vice president, explains that standard IC processes cannot provide transistors with 150-volt breakdown ratings. And while a dielectric-isolation process could be employed, this would add to the cost and mean that the wafers could not be run through the company's standard linear processing line. But the DRV-01 can be built on that standard line. The new rules call for deeper and wider diffusions, as well as thicker epitaxial layers that are lightly doped. As a result, while some density is sacrificed, the higher breakdown voltage is easily achieved.

The mono DRV-01, available from stock, sells for $2.95 each in quantities of 100.

Precision Monolithics Inc., 1500 Space Park Dr., Santa Clara, Calif. 95050 [412]

Dual-voltage translator links TTL, DTL with MOSFET

A dual-voltage translator is a second-source integrated circuit to the DM7800/DM8800 now on the market. The new device, called the SN55/75180, is for use in temperatures from –55 to 1251°C, and is a plug-in replacement for the 7800. An industrial model, the SN75, is a replacement for the 8800. The translator is designed for linking TTL and DTL, voltage levels to those levels associated with high-impedance jun-

SCRs, diodes incorporate 2½-inch silicon slice

A family of high-power SCRs and diodes each incorporates a 2½-inch-diameter silicon slice. The family, designated type D1200, is offered in a capsule package or in a flat-base package for single-sided cooling.
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CITCO AIRCRAFT CONTROL CABLE: 12 triples shielded jacketed, stranded copper conductors, PVC insulated, individual shield jacket color coded, cabled overall PVC jacket.

CITCO ELEVATOR CONTROL CABLE: 35 conductors, stranded copper, PVC insulated, conductors color coded by colors and printed numbers, cabled with open binder; individual conductors U/L listed.

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CITCO STATION CONTROL CABLE: 37 conductors, stranded polyethylene and PVC insulated, color coded, cabled, overall tough PVC jacket; per NEMA/IPCEA Specifications.

CITCO MUNICIPAL COMMUNICATION CABLE: 50 pairs, polyethylene insulated, cabled, continuous layer of copper shielding tape, PVC jacket; per spec. IMSA-19-2, 600 volts.

CITCO SHIPBOARD CABLE: Stranded conductors, nylon-jacketed PVC insulation, pairs shielded and jacketed, cabled, PVC jacket, and aluminum braid armor overall; per spec. MIL-C-915.

CITCO COAXIAL CABLE: Type RG-218/U, solid copper conductor, polyethylene insulated, copper braid shield, PVC jacket; per spec. MIL-C-17/79.

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CITCO COMPUTER CONTROL CABLE: 55 conductors, stranded copper conductors, PVC insulated, formed into 7 groups of 7 conductors, cabled, PVC jacket; U/L listed.

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New products

The SCRs, which have current ratings of up to 1,500 amperes, can handle transient voltages to 3.5 kilovolts and surges up to 16,000 A. The diodes have current ratings up to 1,500 A, transient voltage ratings to 3 kv and surge current ratings up to 33,000 A.

Westcode Semiconductors, 282 Belfield Rd., Rexdale 605, Ont., Canada [414]

Beam-lead diodes supply large-volume applications

Applications for which large volumes of high-frequency diodes are required may be supplied by the model 5082-2837 beam-lead diode. The unit has epitaxial, planar-passivated construction, its leads are coplanar gold-plated, and it measures 4 mils wide by 1/2 mil thick. Breakdown voltage is 70 volts, and reverse leakage current is 200 nanoamperes. Capacitance is 2 pico farads, and effective minority-carrier lifetime is 100 picoseconds maximum. Price is 99 cents in quantities of 1 to 99.


Tracking regulators power operational amplifiers

Constructed to supply the voltage required by operational amplifiers and analog multipliers in control and instrumentation circuitry, the model MC1568 voltage regulator is preset for ±15 volts, accurate within ±200 millivolts. It may be programmed to outputs of ±14.5 v through ±20 v by adding two suitable external resistors. At ±15 v, the absolute value of output voltages agrees within a maximum of 1%. Output current of up to ±100 milliamperes may be obtained without external current-boosting transistors, while maximum unregulated input voltage is ±30 v. Price in 100-piece quantities ranges from $2.80 to $7 depending on temperature range and package styles.

Motorola Inc., Semiconductor Products Division, P.O. Box 20912, Phoenix, Ariz. 85036 [417]

Schottky diodes operate in uhf to Ku bands

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TEC Inc., 9800 N. Oracle Rd., Tucson, Ariz. 85704 [420]
New products/materials

A glass-epoxy copper-clad laminate permits faster, more reliable inspection of through-hole plating of printed-circuit boards. The laminate, designated Quick-Spec, fluoresces upon exposure to ultraviolet light, and after a copper-clad panel has been drilled, sensitized, and copper-plated, it is examined under ultraviolet light. Voids in copper show up as luminescent spots.

Norplex Division, Universal Oil Products Co., 1300 Norplex Drive, LaCrosse, Wis. 54601

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Technical Wire Products Inc., 129 Dermody St., Cranford, N.J. 07016

A neutral flux contains no acids or free fluorides. The flux fumes are not harmful to eyes, lungs, or nasal passages. No. 6 flux can be used for brazing, hard-soldering, and silver-soldering both ferrous and non-ferrous metals and alloys. Hot water will remove excess flux or residues. Another flux, No. 30, is specifically for radio, telephone and electronic parts work, particularly printed-circuit boards.

Superior Flux & Mfg. Co., 1536 St. Clair Ave., Cleveland, Ohio 44114

New literature

Semiconductors. A multiple semiconductor catalog is available from Texas Instruments Incorporated, P.O. Box 5012, Dallas, Texas 75222. The 96-page publication highlights devices with more than one chip in a package and describes the packaging of diodes and transistors in integrated-circuit-compatible packages. Circle 421 on reader service card.

Peripherals. Datum Inc., 170 East Liberty Ave., Anaheim, Calif. 92801. A 12-page catalog contains a brief description of the company, specifications for typical magnetic tape input/output systems, digital cassette drives and mass-memory devices, all with software and interfacing to a range of minicomputers.

Communications. The use of microwaves to provide extended control for retail business is outlined in a brochure published by Motorola Inc., Communications Division, 1301 Algonquin Rd., Schaumburg, Ill. 60127. The 10-page brochure describes how retail-management problems are being solved through voice, visual, and alarm control, as well as data-communications systems linking cities.

Converters. An application note on digital-to-analog conversion using the company's CD4007 C-MOS integrated circuit, a dual complementary pair plus inverter, is available from RCA, Solid State Division, Route 202, Somerville, N.J. 08876.

Control devices. A line of solid-state control devices, including timers, photoelectronics, resistance-sensing relays, and multipole relays, is described in a condensed catalog sheet.
being offered by Regent Controls Inc., Harvard Ave., Stamford, Conn. 06902 [425]

**Disk drive.** Mohawk Data Sciences Corp., Palisade St., Herkimer, N.Y. 13350, has available literature for the models 2900/2800/2500 disk drive system and for the 8420 tape transport, 8803 controller, and 2007 drive. [426]

**Video delay line.** A product bulletin issued by the Corning Glass Works, Memory Products Dept., Raleigh, N.C. 27602, describes how a video delay line is used to store analog signals for television vertical enhancement and other analog image-processing functions. [427]

**Magnetic test system.** A 36-page brochure from Computest Corp., 3 Computer Dr., Cherry Hill, N.J. 08002, details the Delta 400 stored-program magnetic test system. The brochure includes sections on cost advantages, operating data, data acquisition, and software, in addition to application notes. [428]

**Instrumentation recorders.** Test & Measuring Instruments Inc., 224 Duffy Ave., Hicksville, N.Y. 11802. A 36-page brochure discusses the Ana-Log 7 and Ana-Log 14 portable cartridge instrumentation recorders for fundamental and applied research. Technical descriptions, accessories and background information are included. [429]

**Connectors.** A catalog describing cylindrical, subminiature rectangular, crimp-removable cylindrical, and filtered contact connectors is available from General Connector Corp., 80 Bridge St., Newton, Mass. 02158. [430]

**Proximity switch.** Product sheet 10lt., published by Micro Switch, a division of Honeywell Inc., 11 West Spring St., Freeport, Ill. 61032, describes a solid-state proximity switch, listing dimensions, applications, and specifications. [431]

**Microelectronics.** A four-page brochure from Tegal Corp., 815 S. 10th St., Richmond Calif. 94804, discusses chemistry applications in microelectronic and optics. Photore sist striping, substrate cleaning and etching, and optical-surface preparation are described. [432]

**Sockets.** Augat Inc., 33 Ferry Ave., Attleboro, Mass. 02703. A 16-page technical catalog on sockets for testing and packaging integrated circuits and components includes specifications, schematics, dimensions, and photographs. [433]

**Pulse generator.** The model 10433 pulse generator is detailed in a specification sheet available from MCL Inc., 10 North Beach Ave., La Grange, Ill. [434]

**Variable resistors.** A short-form catalog describes the specifications and dimensional data for resistors with 1/2-inch diameter conductive plastic and 1%-inch diameter carbon elements. The catalog is available from Reon Resistor Corp., 420 Lincoln Highway, Frazer, Pa. [435]

**Thermistors.** A revised and expanded 12-page catalog from Yellow Springs Instrument Co. Inc., Box 279, Yellow Springs, Ohio 45387, describes precision interchangeable thermistors. [436]

**Connector assemblies.** Ansley Electronics Corp., Old Eastern Rd., Doylestown, Pa. 18901, has issued data sheet 208 on flex-strip flat-edge cable connector assemblies. [437]

**Rf components.** Werlatone Inc., East Branch Ave., Brewster, N.Y. 10509. Radio-frequency and intermediate-frequency components are discussed in a four-page data sheet. The products include power dividers, hybrid junctions, directional couplers, phase shifters and mixers. [438]

**Digital printer.** A two-page technical bulletin from Veeder-Root, 70 Sargeant St., Hartford, Conn. 06102, provides information on the series 7703 digital printer. Applications, specifications, options, and dimensions are given for this solid-state impact-type device. [439]
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