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Signal theft has been around ever since signal scrambling was introduced. Today, the cable industry estimates that it loses more than $4 billion to signal pirates each year. More serious than an individual pirating a cable signal are the commercial establishments who redistribute programming to others for a fee, and cable company employees who do their part to make a quick buck. As the cable and satellite-TV industries prepare for new, interactive technologies, they have become increasingly aggressive in trying to thwart the pirates.

— Paul Paradise

CHIP TESTER
This inexpensive IC tester is easy to build, and yet quite versatile.
— Mark Hanslip

PROGRAMMABLE SINEWAVE GENERATOR
Generate sinewaves on the fly with this circuit and a PC or single-board computer.
— Ronald J. Portugal

ISOLATION TRANSFORMER
Isolate yourself from the AC line when you service electronic equipment.
— Doyle Whisenant

POWER CONTROLLER
Use a 68705 microcontroller to control eight channels of 120-volt AC power.
— Richard L. Roane
Phantom of the Ether
The new energy-saving fluorescent bulbs save money on electric bills, but they can cause problems with remote controls. — Tom Heald

Operational Amplifiers
Learn how to design op-amp circuits. — Ray Marston

Video News
What's new in this fast-changing field. — David Lachenbruch

Equipment Report
Allison Technology O-Scope I PC Oscilloscope Module.

Computer Connections
What is user-interface design? — Jeff Holtzman

Hardware Hacker
Halogen cycle mysteries, programmable interconnects, and more. — Don Lancaster

Audio Update
Service with a smile. — Larry Klein

Drawing Board
Converting sparks per second to engine RPM. — Robert Grossblatt

What's News
1994 Annual Index
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January 1995, Electronics Now
AMD to offer Pentium Processors

Advanced Micro Devices Inc. (AMD) intends to go head-to-head with Intel Corporation again over a new generation of microprocessors. It recently announced that it expects to begin volume production of Pentium-like MPU chips by the middle of the year. AMD, which already makes functional equivalents of Intel's 486 MPU, said its new K5 device was twice as fast as Intel's Pentium and would be compatible with Windows software from Microsoft Corporation.

1994 National Medal of Technology winners

Four persons and two companies received the 1994 National Medal of Technology in recognition of their contributions to America's technical innovation and economic competitiveness. The Presidential Awards were granted by Commerce Secretary Ronald H. Brown to Amgen (Thousand Oaks, CA), Corning, Inc. (Corning, NY), Joel S. Engel (America Tech Corp.), Richard H. Frenkiel (AT&T Consumer Products), H. Joseph Gerber (Gerber Scientific), and Irwin M. Jacobs (Qualcomm).

Amgen, the world's largest biotech firm, was granted a medal for its development of innovative medications for critically ill patients based on cellular and molecular biology. Amgen scientists discovered and introduced genetically engineered human erythropoietin, or Epo- gen, a protein essential to the maturation of oxygen-carrying red blood cells.

Epo-ogen, for treating anemia in kidney dialysis patients, has virtually eliminated the patient's need for blood transfusions. Another Amgen-developed product is Neu- pogen, a recombinant protein that stimulates the production of infection-fighting white blood cells. Neupogen decreases possible infection associated with chemotherapy.

Corning, well known for its glass products, was honored for its technical innovations over the past 125 years. A Corning glass envelope enclosed Edison's first incandescent light bulb and fiber optic cables from the company are now replacing copper wires in telephony and communication. Corning has also participated in such scientific activities as providing the windows for America's space shuttle, mirrors for giant telescopes, and ceramic filters for pollution control.

Joel Engel and Richard Frenkiel were jointly honored for their fundamental contributions to the theory, design, and distribution of cellular mobile communications systems. Their work led to important advances in local area networks as well as worldwide communications based on satellites.

Joseph Gerber's medal was for past and on-going invention, development, and commercialization of efficient, cost-effective automated manufacturing systems. He holds 600 patents, and his inventions have had a significant impact on electronics, cartography, ships building, and the apparel, aircraft, automotive, and optical industries.

Irwin Jacobs was honored for his contributions to the field of digital wireless communications and for his development of code-division multiple access (CDMA), a U.S. standard for cellular digital communications. He and his colleagues developed a television signal scrambling system, as well as innovations that will improve the next generation of cellular telephones and personal computers. Mr. Jacobs also developed a data-transmission and vehicle location system based on satellites for the trucking and shipping industries.

Commerce Secretary Brown declared, "Their achievements have contributed to U.S. economic prosperity and job creation while benefiting millions of people at home and around the globe. The dedication, energy, and unique creativity of each honoree should serve to inspire and motivate all Americans. Each medalist deserves special recognition as models for the new American economy.”

More advanced semiconductor IC plants

The Fujitsu-Advanced Micro Devices (AMD) joint venture (FASL) has opened a factory for the production of flash memories in Japan. The memory devices will be fabricated with 0.5-micron design rules.

FASL expects that the $750-million plant, at full production, will produce more than 5000 eight-inch silicon wafers weekly. The 280,000-square-foot plant is expected to employ somewhere around 400 people when it is fully operational.

In a related announcement, Micron Technology said that it would spend $1.3 billion to build a new 200-acre manufacturing plant, probably in Boise, Idaho, where the company is now based. The largest expansion ever, the plant would double the company's manufacturing capacity. Construction of the new plant is expected to begin in the first quarter of 1995 and it is expected to employ 3500 people when it is complete.

Wavetek to Acquire a Schlumberger Division

Wavetek Corp. has agreed to acquire the worldwide assets of the Schlumberger Communications Test Division (CTD). These include both the Radio Communications Test Equipment Business located in Germany and the Telecommunications Test Equipment business located in France.

CTD developed the first modular test set capable of testing all kinds of radio communications systems. It now builds test equipment for video transmission, data communication, and fiber optic networks. Schlumberger will retain a minority interest in the business. (Continued on page 16)
TekMeter™ can show you the answer before you even know the question.

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• **Network indexer.** ABC will make it easier to index your videotapes, according to current plans. The network has agreed to broadcast “Index Plus” information during the vertical blanking interval (VBI) of its broadcasts. The data that its affiliated stations will send out will trigger specially equipped VCRs to record its programs and make a record of the programs recorded, which can be displayed on-screen. For subsequent viewing, the VCR owner can select any program from an on-screen directory and push a remote-control button. Presto—the VCR advances to the proper point and begins playback. The system also makes it possible to display a list of programs with a guide showing the volume number of the cassette on which each is recorded.

The information transmitted by ABC will be on the “extended data service” (EDS) portion of the VBI—which actually is filed number 2 of the closed-caption line, number 21. The system also will provide continuous program information—the name of the program, a brief description, and time remaining—as an aid to channel surfers. Whether or not to transmit that information is up to ABC’s affiliated stations. Index Plus was invented by Gemstar Development Corporation, the company responsible for the highly successful VCR Plus+ recording system. The only known previous use of the EDS line is its employment by PBS affiliates to set the clocks on three current-model Sony VCRs (Electronics Now, August 1994).

• **Hollywood likes DVD.** Seven major movie studios have formed an “ad hoc advisory group” on the digital video disc (DVD), the upcoming medium designed to record 135 minutes of high-resolution video on a single five-inch disc. Columbia Pictures, Disney, MCA/Universal, MGM, Viacom, Paramount, and Warner Brothers said that their goal in forming the group was “to encourage public and industry discussion” of the new medium.

The group listed six major goals for DVD: (1) It must accommodate a full-length movie on a single disc. (2) Picture quality should be “ideally superior” to that of “current high-end consumer video playback systems,” presumably a reference to laserdisc. (3) Audio should be compatible with surround sound and other high-quality systems. (4) It should be able to accommodate three to five different languages on the same disc. (5) Some form of “copy protection” is a must. (6) A parental-lockout system should be built in, or, alternatively, the disc should be able to accommodate two versions of the same program.

At our press time, two major systems appeared to be vying for industry standardization. Sony and Philips are collaborating on one system, whose disc physically appears identical to a standard audio CD and actually has one-way compatibility with audio CD in that DVD players will be able to play audio CDs. The other system is being promoted by an alliance of Toshiba and Time Warner. That system, according to some reports, is the same size as an audio CD but has two sections laminated together (although it’s a single-sided disc).

Both the hardware and the software industries are anxious to field a single standard system to avoid a duplication of the Beta–VHS confusion. The advantages of the DVD system presumably include substantial core savings in replication and shipping because of low material use and light weight, higher picture quality—presumably including the ability to display widescreen movies in full width and resolution—and better audio than existing systems.

• **Recordable digital discs.** While the electronics world awaits definitive word on the specifications for digital video discs, TDK an-
How to get surround sound without buying the theater...

Chase Technologies brings you an amazing new patent pending surround sound decoder that turns your stereo into a five-channel home theater.

By Charles Anton

As much as I love renting videos, it’s just not the same as seeing a movie in a theater. I remember the first time I saw Jurassic Park—I nearly jumped out of my seat when the dinosaurs roared. One of the reasons movies seem so real is because surround sound makes it seem like you’re actually there when events are happening. Now there’s an incredible new way to get that same surround sound in your home.

It takes more than five speakers to get surround sound; there needs to be a way of separating the signals. The new Chase Technologies HTS-1 decoder does just that, and in a revolutionary way that rivals the best Dolby Pro-Logic and THX systems.

WINS over critics. In the September ’94 issue of “High Performance Review,” noted audio critic Daniel Kumin said “the HTS-1 can do quite a job of recreating a 3D theatrical experience...surround effects emanated with satisfying fullness...sound was clean at any level...with quite involving and natural sound ambience.” Plus, John Sunier, the leading authority on surround sound and producer of Audiophile Audition, a nationally syndicated radio program for audio enthusiasts, says, “...the new Chase HTS-1, when used to decode the hidden ambience in all musical recordings, definitely outperforms all the Dolby and THX processors (which could cost you up to $5,000)...I am impressed!”

The secret of surround sound

Surround sound has become the rage of the 90’s because it adds depth and realism to stereo sound, giving you the home theater experience. It makes you feel like you’re actually at a concert or theater. To “fill a room” with surround sound, you need more than two channels. The HTS-1 provides five channels of sound from any two-channel stereo source.

Free center channel. By connecting your VCR or laserdisc player to your TV, you get sound from your TV speaker; this acts as the fifth or “center channel.”

Upgradeable. The new HTS-1 gives you the ability to upgrade by adding the “Dialog” powered center channel speaker (instead of using your TV speaker). The decoder can also feed an extra amp for the rear speakers if you want the ultimate in discrete five channel performance.

Submerge yourself in rich surround sound.

Easy installation. Hooking up the HTS-1 is easy—just connect the speaker outputs of your receiver or amp to the HTS-1, then connect speaker wire to the front and rear speakers. The rear channel speakers don’t have to be big. We suggest the Chase ELF-1 in either black or white finish to match your decor.

Center Channel. The “Dialog” powered center channel speaker is the perfect add-on for home theater. It keeps voices and sound effects centered on screen for stunning localization and clarity.

Risk-free home trial. The best way to evaluate surround sound is in your home, not in a showroom. That’s why we’re offering this risk-free home trial. We’re so sure that you’ll be delighted with the quality of these products and the surround sound experience that we are giving you 30 days to try them for yourself. If they’re not everything we say, return them for a complete “No Questions Asked” refund.

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HOWLER SUBSTITUTE

I install a lot of office telephone systems, which often requires that I string a lot of cable. It takes a long time to make sure that I have the right wire going to the right frame positions. I was using a "howler" to trace lines, but mine stopped working and it turns out to be an expensive item to replace. Do you have some simple alternative that will do the same job and, if possible, provide several tones to allow me to test more than one wire pair at a time? That last requirement isn't absolutely necessary, but it would save me hours of running up and down the stairs.—A. Spiwak, San Francisco, CA.

Telephone line howlers are, for my money, too big, too expensive, too noisy, and eat batteries at an unacceptable high rate. For companies that are supposed to be on the cutting edge of technology, some of the equipment seems to be only one step away from steam-powered equipment.

Creating something that will help you trace cable is not only easy, but is also cheap, and the power requirements are so low that the batteries should last almost as long as their rated shelf life—maybe that's a bit of an exaggeration. The circuit shown in Fig. 1 is exactly what you need.

The LM3909 is a cheap, versatile IC. The circuit will produce a 1-kilo-hertz square wave with a peak-to-peak voltage equal to about 80% of the battery voltage. It will also work off a single 1.5-volt battery. Just about the only restriction here is that the circuit output should always see at least a 10K load. If that's a problem, you can do it with a single resistor.

The trimmer in the circuit adjusts the duty cycle of the square wave output. Shifting the duty cycle will change the sound of the tone. This will let two additional circuits produce uniquely different sounds and that will let you trace more than one pair of wires at a time.

This circuit is right from National Semiconductor's data book. It is so simple that you can put several of them in a single enclosure and have each produce a different frequency. While you could power all of them from a single battery, you might want to have a separate battery for each circuit. There's always a chance of having some signal leakage and crosstalk through the power supply and, even though critical audio isn't a concern with your job, it's so easy to avoid that you might as well do it anyway. Having separate batteries also means that they will last longer. It isn't often that a cheap alternative will work just as well as an expensive gadget. But when one does, it pays to take advantage.

FIG. 1—THIS CABLE TRACER is inexpensive and the batteries last a long time.

ROBOT CONTROLLER

I recently bought an 8085 microprocessor trainer to build a controller for a robot. I don't understand the instruction set and haven't been able to program the microprocessor. I could build the controller with discreet logic but it wouldn't be as versatile. Do you have any ideas as to what I should do?—D. Vitez, Clinton, PA.

The old saying, "If you can't do the time, don't do the crime" pretty much sums up the problem you have at the moment. There's no point in playing with microprocessor hardware unless you also make a commitment to the Great Software God as well—one is pretty much useless without the other.

The 8085 instruction set isn't all that complex, and it's fairly representative of microprocessor instruction sets in general. If you're having a hard time with this one, chances are you'll have a hard time with any of them. You might be having a hard time because the trainer programming environment isn't user friendly. It's a lot easier to develop software on a real computer than on a trainer.

Some microprocessors (such as the old 8052) have a BASIC interpreter built-in so software can be written in a dialect of BASIC. This makes it easier to write software because computer languages don't come much simpler than BASIC. 8052 BASIC (and newer versions) contains the usual BASIC commands plus special features for control applications.

Single board computers are also available that provide a programming environment similar to the one on a desktop. Software can be developed on a desktop computer and either downloaded into the single board RAM or burnt into an EPROM for testing. The secret to writing software is having some way to debug it—and 640K of RAM in a desktop PC is a good place to do that.

If you're locked into the idea of using a microprocessor to control your robot—which is the best way to go—there's no way to get around the software. Contact some microprocessor manufacturers (such as Intel and Motorola) and find out what chips are best suited for your application. A microprocessor designed specifically for control applications is going to be easier to use than one that's not.

Continued on page 12
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The MECP will be administering tests at various locations across the country in the first three months of 1995. In January they will be given in Indianapolis (January 5), Las Vegas (during the Winter Consumer Electronics Show, January 8), Denver (January 12), San Diego (January 19), and New Orleans (January 26).

The tests will be held in Dallas/Fort Worth on February 2, Fresno on February 9, St. Louis on February 16, and Pittsburgh on February 23. In March, tests will be administered in Omaha (March 2), White Plains, NY (March 9), Minneapolis (March 16), and Madison, WI (March 23).

Registration deadlines are two weeks before the test dates. For more information on test locations, study guides, and cost, contact: MOBILE ELECTRONICS CERTIFICATION PROGRAM 2512 Artesia Boulevard Redondo Beach, CA 90278 Phone: 310-376-8458 Fax: 310-798-4598

TRANSFORMER TEST

I just received the November, 1994 issue of Electronics Now. As usual, I found most of the material quite interesting, especially "The TextGrabber," "The Frequency Doubler," the Tesla coil article, and "All About Phase-Locked Loops." However, I have five comments on "Simple Test for Transformers."

First, the value of the transformer secondary voltage was given as 6.8 volts—twice in the text and once on the circuit diagram. The standard voltage for transformers is 6.3 volts and multiples of that value (e.g., 12.6 and 25.2). The 6.8 value is a standard for resistor ohms.

Second, 6.3-volt transformers might be hard to find (Mouser Electronics lists several). Any transformer voltage near 6 volts can be used (I found a 5.6-volt unit that worked). By contrast, 12.6-volt center-tapped transformers are available widely; connect one wire to the center tap and the second wire to the end terminal.

Third, a shorted transformer, connected as shown, will overload the transformer in the tester. I think a resistor should be connected between the top terminal of the 6.3-volt secondary and the top terminal of the AC voltmeter. That would also give a larger voltage drop if there were a shorted turn on the transformer under test. However, there would be a very small drop across the resistor if the transformer is good.

I would choose the resistor that would limit the current to the transformer's current rating. For a 6.3-volt, 1-ampere transformer, it would be 6.2- or 6.8-ohm, 10-watt resistor; for a 6.3-volt, 0.2-ampere transformer, it would be a 33-ohm, 2-watt resistor.

Fourth, there is a possible safety hazard in the project. If another 6.3-volt transformer is being tested, and the secondary winding is connected to the test circuit, nearly 120 volts would appear on the unconnected primary leads of the transformer under tested, if it is a good unit. To avoid this hazard, first measure the resistance of the windings of the suspect transformer with an ohmmeter, and then connect only the winding with the highest resistance to the test circuit.

Fifth, many of the items pictured in the photograph accompanying the article cannot be tested with this circuit. In the last paragraph of the article, the word "chokes" should have been "iron-core chokes and larger ferrite-core chokes and coils." At 60 Hz, the reactance of a 100-MHz coil is about 36 ohms, and many of the coils in the photo look much smaller than those suitable for 100-MHz operation. If the test frequency were higher, smaller coils could be tested.

As a result of reading this article, I now have some ideas for a simple circuit operating at 2000 to 3000 Hz with an audible as well as a metered output. I plan to get to work on this project soon.

BILL STILES, CET Hillsboro, MO

MORE ON TRANSFORMERS

I have been reading Radio Electronics and Electronics Now since the 1970’s, and I have enjoyed learning and gaining ideas from your magazine—especially from authors like Don Lancaster. The magazine seems to have a good balance between simple and complex articles and projects. I believe that many newcomers to electronics can learn from the simpler articles—if the technical information in them is accurate and complete.

That is not the case with “A Simple Test for Transformers” (Electronics Now, November 1994). The article did not point out some shortcomings and hazards that are involved in the test method presented.

The inductive reactance of a coil winding depends on the number of turns and the core material. For example, an air-core winding would not have sufficient reactance at 60 Hz for the test to be valid. A good coil would appear as a short circuit, and its windings, which would only represent a low resistance, could burn out if high current were applied. The test method in the article is suitable only for low-frequency, iron-core transformers.

I measured the short-circuit output current of a 6.3-volt, 600-milliampere transformer. I obtained a reading in excess of 2.5 amperes.
If a 10-kilohm, 2-watt, flameproof resistor is wired in series with the primary winding of the 6.3-volt transformer, the secondary short-circuit current is reduced to a safe value of less than 200 milliamperes.

It is important to point out that when testing a step-down transformer's secondary winding, an unexpected high voltage—which would constitute a shock hazard—can appear on the primary winding.

ROBERT J. JOHANSEN
Staten Island, NY

QUESTIONING CSICOP
The Committee for the Scientific Investigation of Claims of the Paranormal, or CSICOP (recently praised by Don Lancaster and Larry Klein), does precious little scientific investigation and a lot of debunking and smearing of claims of the paranormal. The committee has three main operating principles:

1. Condemnation before investigation. The committee will not seek to verify claims of UFO experiences, success with dowsing, out-of-body experiences, or sightings of spirits. It denounces claims presented to them. Judging from its written opinions, the committee is adamantly opposed to anything that cannot be explained by existing physical science.

2. The committee picks on the weak, absurd, and vulnerable reports of the paranormal, and exposes and ridicules them (as they should). But it implies that there are no reports worth investigating (which is untrue).

3. Evidence must be physical. Thousands of people have testified to the reality of myriad paranormal phenomena—it has generally been non-conflicting testimony that would be accepted in a court of law. Yet the CSICOP calls such testimony anecdotal, not repeatable, hallucination or, worse yet, fraud.

It is just such narrow-minded people that now make up CSIOP (professors, intellectuals, and scientists) who have cried “impossible” and tried to prevent the introduction of any fundamentally new ideas in the fields of politics, religion, medicine, and science.

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Probably not! However, through constant playing and using of degrading dry or wet cleaners, the output of your video tapes has slowly diminished to an unacceptable level and the VCR plays as if it has a head cold! The culprit is most likely clogged and dirty video and/or audio heads.

The 3M Black Watch™ Head Cleaner Videocassette uses a patented magnetic tape-based cleaning formation to remove head clogging debris. No foreign substances such as cloth, plastics or messy liquids and no harsh abrasive materials are present. The cleaner's usable life is 400 cleanings or more!

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Once your VCR's head cold is cured, and the unit plays like new, consider using the finest videocassette you can buy—the 3M Black Watch™ T120 Hi Pro VHS 4410 Videocassette. The 4410 is the highest performing videocassette available today for use with all standard format VHS recording hardware!

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**Q&A**

continued from page 8

**LONG CABLE RUNS**

My office has a small network installed and we recently took some more space on the floor below us. I want to put the computers in the new office on the network but the Novell manuals specify a maximum of 250 feet of cable on either side of the file server. Is there some simple way to get beyond this limit? I have to go almost twice this distance to reach the new office.—G. Nightingale, Bamford, NY.

The best around this problem depends on who gives the advice. Network people will start talking about a WAN (wide area network), hardware people will start talking about transceivers or short-haul modems, and everybody will talk about spending a lot of money.

It's true that networks work best when cable length limitations are observed and transceivers are installed when you must exceed standard distances. However, the maximum possible cable length without any degradation in network performance is also a function of the cable and connectors.

Network cable comes in different grades, and the cable quality will drastically affect the maximum safe lengths you can have. Better quality cable costs a bit more per foot but it's less expensive and much less of a hassle than adding additional hardware to the network.

Use double shielded cable to get beyond the standard Novell length limitation. This type of cable has a standard braided shield under the outer insulation and it also has the center conductor's insulation wrapped in foil. This extra shielding really cuts down on noise and signal loss on the network. I've run this cable over 700 feet from a file server without any loss in performance.

Double shielded cable is a pain in the neck to use because it's difficult to remove the foil when installing connectors, but it's an easy solution to your problem. Make sure to use good quality connectors, or you'll defeat the purpose of buying expensive cable.
A n oscilloscope is probably the most useful test instrument that an electronics technician can have. When the capabilities of a digital multimeter (DMM) are exhausted, an oscilloscope takes over. A DMM can indicate the presence of an AC or DC voltage, but it doesn’t allow the user to visualize the signal. An oscilloscope is necessary for determining such things as the presence of an audio signal or whether the signal is being amplified. Troubleshooting digital circuitry also requires an oscilloscope to determine if digital data is present where it should be and if it is correct.

Although oscilloscope prices have declined dramatically over the last decade, cost still restricts many oscilloscope purchases. A new basic oscilloscope will cost about $300, although at that price, it will lack many desirable features. The most inexpensive full-featured oscilloscope will cost upwards of $500, and high-performance instruments with digital storage are priced over $1000.

Every electronics enthusiast should really have an oscilloscope on his test bench, but the price of a versatile high-performance instrument is often too high for the average hobbyist—even many professional service centers need ultra-low-cost instrumentation for some of their repair stations.

An alternative

It’s a safe bet that more Electronics Now readers own personal computers than personal oscilloscopes. A PC contains a CRT in its monitor, and its sophisticated circuitry can be programmed to do countless tasks under software control. What happens if a test signal is presented to an input port on a PC? With the right software, the computer can display the signal just like an oscilloscope!

That’s just what the Allison Technology O-Scope I does—it’s a low-cost, single-channel, digital storage oscilloscope module for an IBM PC-AT (or better) compatible computer. (XT compatibles are too slow to be used successfully with the scope module.) The module connects to a PC’s printer port and converts the computer into a single-channel digital storage oscilloscope. (Allison Technology Corp., 8343 Carvel, Houston, TX 77036, 713-777-0401.)

The O-Scope I can display input signals from DC to 22 kilohertz, and freeze the display at any time. The plot can then be printed or saved to disk for later use or for inclusion in other programs. Vertical resolution ranges from 10 volts per division down to 50 millivolts per division. Sweep rates from 100 seconds per division to 500 microseconds per division can be selected. Digital signal processing allows the sweep to be expanded from \(x \times 2\) to \(x \times 16\).

The O-Scope I also numerically displays voltage, frequency and period measurements in an on-screen table. The voltages include peak-to-peak, average, peak, minimum, and RMS. In addition, a 128-point Fourier spectrum analyzer mode permits the display of frequency-spectrum information from DC to one half of the set sampling rate.

A single-channel, 22-kilohertz oscilloscope is not the most versatile of instruments, but for the amateur electronics enthusiast, O-Scope I’s bang for the buck can’t be beat. The unit sells for $169.95 fully assembled in a shielded plastic case, and for $119.95 as a kit without the case, which is available separately. The unit has enough practical uses that many hobbyists—and many professionals who need an extra oscilloscope—might want to take advantage of the deal.

Operation

O-Scope I is connected to the PC’s printer port with the supplied ribbon-cable. The default port is LPT1, but other port addresses can be specified when the program is started. A test program is included for users who are unsure of the address of their computer’s printer port. An AC adapter that plugs into the scope module and provides the necessary 12-volts DC oscilloscope operation is supplied.

A standard \(x \times 1\) or \(x \times 10\) oscilloscope probe (not included) connects to a BNC connector on the module. A probe is not included with either the assembled O-Scope I or the kit. The program runs in DOS only, and is started by typing “OS-
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COPE" at the DOS prompt, followed by a port address if other than LPT1 is used.

The cursor keys control most of the oscilloscope functions. The up and down cursors move a function indicator to different menu selections, and a selection is changed with the left and right cursors. Other commands are activated by keystrokes. The A key selects AC coupling; C toggles connecting lines between samples; D selects DC coupling; F toggles between sweep and spectrum; X toggles between ×1, ×2, and ×5 sweep expansion; the Space bar freezes the display until the next keystroke; P cycles through special DSP processing to expand the sweep by ×2, ×4, ×8, and ×16; L toggles the log-to-disk option; and Escape terminates the program and returns to DOS.

To use O-Scope I, both it and the PC must be powered up before the two are connected together. O-Scope I should also be powered and connected to a PC before the probe is connected to an external circuit.

O-Scope I has an input impedance of one megohm, and a maximum input voltage of ±60-volts DC or 40-volts AC. It is accurate to within 3 to 4%. Although the scope's input is fuse-protected, excessive voltages can damage both the module and the computer, so it might be better to use an older computer with the scope module and reserve your new 486- or Pentium-based machine for more conventional applications. The performance of O-Scope I will not be enhanced by a powerful computer.

All in all, the O-Scope I should be especially easy for anyone familiar with both PCs and oscilloscopes, and easy to learn for anyone unfamiliar with either or both.

Even though the $169.95 fully assembled O-Scope I is a practical investment for an electronics hobbyist, avid kit builders might want to take advantage of the extra savings ($50) offered by purchasing the kit version. Building the kit is not complex; there is enough work to keep a builder busy for about an evening. A DMM is the only instrument needed for checking voltages and continuity. Calibration calls for adjusting only a single potentiometer that roughly centers the 0-volt DC level on the display.

Anyone who wants to do professional-level testing will probably need more than the O-Scope I offers. But for hobbyists and others who are still learning electronics—and might be saving their money for a high-performance scope—O-Scope I offers a lot.

WHAT'S NEWS

continued from page 4

Electronics Industry Hall of Fame inductees

Three technicians/service dealers were inducted into the Electronics Technicians Division of the Electronics Industry Hall of Fame on August 13, 1994. George Bluze CET/CSM of Largo, FL, Robert Villont CET/CSM of Tacoma, WA, and Don Winchel CET of Smartville, CA, were inducted at the National Professional Electronics Convention held in Portland, OR.

Bluze served as president of the National Electronics Service Dealers Association (NESDA) and president of NESDA-Florida. He has been a test administrator for the International Society of Certified Electronics Technicians (IS CET) since 1979. Bluze has also been NESDA Man of the Year, Officer of the Year, and Outstanding State President. and he was IS CET Technician of the Year in 1982.

Villont was NESDA president during the association's move from Indianapolis to Fort Worth and was the NESDA Region 10 director for several years. He was NESDA's representative to the IS CET Board of Governors for 13 years from 1980 to 1993 and he has also been NESDA's Man of the Year Award.

Winchel was a board member for both NESD and IS CET for more than 11 years. He served two terms each as chairman of IS CET and was president of the California State Electronics Association. An IS CET test administrator for many years, he made the IS CET Serviceability program prominent nationally.

Official nomination forms for the Hall of Fame are available from the Electronics Industry Hall of Fame, Inc., 500-B Bi-County Blvd., Farmingdale, NY 11735.
Meet the new TEST BENCH DMMs, with more of what made the original a best seller. B+K PRECISION's original TEST BENCH testers became overnight best sellers because they fused the power of many instruments in one compact meter. These new models also out-feature ordinary DMMs, and outperform them as well. All are ruggedized, offer long-battery life and carry a three-year warranty.

With True RMS, 4½ digit, 20,000 counts and 0.05% DCV accuracy, the Model 391 is a BEST BUY. Now you can have very high accuracy, extra resolution and True RMS reading at a very affordable price. The Model 391 Test Bench DMM also has frequency, logic, duty cycle and data hold. It's even water-resistant.

There's a TEST BENCH DMM to fit every application and budget. Choose from three, 3½ digit TEST BENCH DMMs, starting with the Model 388A. All measure AC/DC voltage or current, ohms, frequency, logic levels and test components and continuity. The Models 389 and 390 add 4½ segment bar graphs for smooth peak, null or level adjustments; Min/Max, memory and relative modes. The 390 also has a temperature probe.

So why carry an ordinary DMM, when you can grab a TEST BENCH! See your local distributor for immediate delivery.
Electronics Paperback Books

- **BP109—Everyday Electronics Data Book...$10.00.** An invaluable source of electronics information—the text contains many sections that deal with the underlying theory of electronic circuits and a wide range of practical electronic applications.

- **BP245—Digital Audio Projects...$5.95.** Practical details of how to construct a number of practical projects. All should be of interest to most audio and electronic music enthusiasts. Some of the projects are: oscilloscope storage and triggering circuit, A/D converter, negative supply, input amplifier, low-noise microphone preamp, compressor and expander circuits, input mixer, echo effect circuit, and others.

- **BP322—Modern OpAmp Projects...$5.75.** Various projects that make use of operational amplifiers available to hobbyists. Text includes low-noise, low-distortion, ultra-high input impedance, low-slew-rate and high current types.

- **BP277—High-Power Audio Amplifier Construction...$6.25.** Practical construction details of how to build a number of useful audio power amplifiers ranging from about 50 to 400 watts rms. Text includes MOS-FET and bipolar transistor designs.

- **BP330—Electronic Board Games...$6.00.** Complete plans for 20 novel electronic board games that you can build with ease. Some projects are: Motion sensing, search for buried treasure or gold at Ft. Knox, wheel of fortune, a musical quiz—plus others.

**COMPUTER TOPIC BUY-OUTS**

- **BP109—The Art of Programming the 1K ZX81—$3.95.**
- **BP114—The Art of Programming the 16K ZX81...$4.95.**
- **BP119—The Art of Programming the ZX Spectrum...$4.95.**
- **BP129—An Introduction to Programming the ORIC-1...$2.50.**
- **BP128—20 Programs for the ZX Spectrum and 16K ZX81...$4.75.**
- **BP143—An Introduction to Programming the Atari 600/800 XL...$4.95.**
- **BP154—An Introduction to MSX (Universal Japanese) BASIC...$4.95.**
- **BP156—An Introduction to QL Machine Code...$3.95.**
- **BP157—How to Write ZX & Spectrum+ Games Programs...$3.95.**
- **BP158—An Introduction to Programming the Commodore 16 & PLUS4...$4.95.**
- **BP161—Tinto the QL Archive (database program)...$2.95.**
- **BP187—A Practical Reference Guide to Word Processing on the Amstrad PCW 8256 & PCW 8512...$9.95.**

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VIDEO COMPUTER DISC CHIP SET. Texas Instruments has introduced the industry's first video CD chipset that is expected to simplify the design of Moving Picture Experts Group-1 (MPEG-1) video and audio decompression subsystems. The chip set decodes, synchronizes, and decompresses audio/video data that has been encoded to the MPEG international compression standard.

Capable of introducing a full-motion video (FMV) subsystem to home-entertainment products such as CD-based movie players, video games, and karaoke systems, the set consists of the TMS320AV220 MPEG-1 video decoder, the TMS320AV120 MPEG audio decoder, and the TMS320AV420 National Television Standards Committee (NTSC) encoder.

Those three devices, installed with a 4-megabit DRAM and a digital-to-analog converter for converting the audio output, will turn a CD player into a video CD player. The set produces a video signal encoded in the NTSC format for broadcast TV and an audio signal that can be played back either over TV or through a stereo system for CD-quality digital sound.

The audio encoder is packaged in either a 44-pin plastic leaded-chip carrier (PLCC) or an 80-pin quad flatpack (QFP). The video decoder is packaged in a 160-pin QFP, and the NTSC encoder is packaged in an 80-pin QFP.

The high-volume pricing for the complete set is under $40.

Texas Instruments Incorporated

CIRCLE 20 ON FREE INFORMATION CARD

PORTABLE SCOPE-PLUS-METER. Fluke Corporation has introduced the latest of its ScopeMeter test instruments, the Series II. It combines a dual-channel, 50-MHz digital storage oscilloscope and a 3½ true-RMS multimeter in one battery-powered, handheld unit.

The new models have additional measurement functions including a "measure menu" that automatically configures the instrument for any of 30 measurement tasks and a "continuous autoset," function that eliminates the need for manual front-panel adjustments when the probe is moved from one test point to another. The instrument can be switched back to conventional operation at any time.

Series II ScopeMeters offer a "windowing" menu structure that gives quick access to any function with a few keystrokes. Moreover, a Series II in meter mode continuously displays waveforms simultaneously with measurement values. It is not necessary to switch to oscilloscope mode to see a signal waveform view of a signal unless

SMT/THRU-HOLE REPAIR CENTER. The SMD-250 surface-mount and leaded component repair and rework station from A.P.E. is a set of tools for removing and replacing surface-mount and leaded components by hot-air or thermal methods. It can perform conventional thru-hole desoldering and both reflow and conventional soldering. It also includes vacuum parts handling and solder paste dispensing capability.

CIRCLE 21 ON FREE INFORMATION CARD

The repair system has two programmable digital controllers under closed-loop temperature control. The tool tip can be set at any temperature from 350 to 875°F without changing either the tip or the heater element. Temperatures are displayed on a three-digit LED readout.

The SMD-250 includes a fast-response, rotary-vane vacuum pump that provides a vacuum at 23 inches of mercury in 150 milliseconds which can withdraw molten solder in 30 milliseconds. A variable-pressure output control adjusts hot-air flow for surface-mount component solder reflow. Zero-voltage thyristor switching protects voltage- and current-sensitive devices against transient voltage spikes.

Both the 120- and 240-volt SMD-250 models are priced at $1995.

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greater waveform detail is needed.

Two "min/max" functions have been included: A min/max TrendPlot function simultaneously graphs the minimum, maximum, and average readings of a signal between two minutes and 30 days; A min/max envelope function gives a record of all changes to the displayed oscilloscope waveform, displaying all the minimum and maximum values on the screen simultaneously.

Four Series II models are available: dual-channel 99, 96, and 92, and the single-channel 91. An RS-232 interface permits the printout of data from the 96 and 99 (shown here). Optional FlukeView software for DOS- or Windows-based PCs is available for the Model 99.

Model 99 includes a signal generator for producing sinusoid, squarewave, and component test signals. It also performs waveform calculations. The Model 99 can store 10 screens, 20 waveforms, and 40 instrument setups. The Model 96 can store five screens, 10 waveforms, and 20 front-panel setups.

The price of the Model 99 is $2195, the 96 is $1895, the 92 is $1595, and the 91 is $1295.

**Fluke Corporation**
P. O. Box 9090
Everett, WA 98206
Phone: 800-44-FLUKE
Fax: 206-356-5116

**DATA DEBUGGING TOOLSET.**
Data Debugging Toolset (DDT) software from CST Images will assist in debugging complex data-manipulation software. It is said to fill the gap between standard source-code debuggers and generic graphic toolsets.

DDT provides non-graphic, logic-based debugging controls to be embedded in a user program under development. The DDT routines generate remote X11 graphic displays that permit viewing program data results on a SPARC Unix workstation, control debugging flow, and analyze massive data arrays into a clear graphic format.

The program was developed as a quick analysis tool for general data processing, signal processing, data acquisition, and other scientific and engineering data processing. DDT allows the developer to insert debug routine calls into C and FORTRAN code at key points where the data can be viewed or checked for complete algorithm verification.

One program call generates one graph. The controls allow the program results to be stepped or viewed after a number of computations without intervention. DDT is available for SPARC/Solaris computers, Motorola 167 processors, and various CSPI Supercards.

DDT has a price of $499 per library.

**CST Images**
5055 Viewridge Ave. B
San Diego, CA 92123
Phone: 619-277-7833
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**RED-LIGHT VISIBLE LASER DIODE.** The TOLD9521 red-light-emitting visible laser diode (VLD) from Toshiba America, draws 75 milliamperes while emitting at a wavelength of 635 nanometers. It produces 3 milliwatts of output power when operated in the rated ambient temperature range of \(-10^\circ\text{C}\) to \(50^\circ\text{C}\).

The TOLD9521 is seven times brighter than Toshiba's 670-nanometer VLD. Its brighter beam can be seen more easily by the human eye at safe power levels. The TOLD9521 is intended as a light source in instruments for leveling and aligning ceilings, barcode scanners, laser printers, and communications systems.

Visible red-light emitting diodes are smaller, have lower power requirements, and higher efficiency than helium neon (HeNe) gas lasers that emit in the same visible region. They also have a higher response to input currents. Toshiba's visible laser diodes are made from crystals containing indium, gallium, aluminum, and phosphorous (InGaAlP).

TOLD9521 red-light-emitting VLDs are priced at $100 each.

**Toshiba America Electronic Components, Inc.**
9775 Toledo Way
Irvine, CA 92718
Phone: 714-455-2000

**MINIATURE SURFACE-MOUNT TRANSFORMER.**
The miniature TC4-1W RF transformer from Mini-Circuits has a bandwidth of 3 to 800 MHz and features DC isolation between its primary to secondary windings. Recommended for impedance matching and land-mobile radio, it measures only 0.16 x 0.16 x 0.16 inch.

The surface-mountable transformer was designed for circuit-board placement with pick-and-place machines. The transformers are available taped on reels for placement with those machines.

The TC4-1W transformer is priced at $4.95 each.

**Mini-Circuits**
P. O. Box 350166
Brooklyn, NY 11235-0003
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Filtech software complete with a manual containing sample designs and a tutorial on filters is priced at $275.

Number One Systems
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Pleated-Foil-Covered I/O Cable Assemblies. 3M Electronic Products Division; 6801 River Place Blvd., Austin, TX 78726-9000; Phone: 800-225-5373; free.

This four-page, color brochure describes 3M's new, pleated foil-covered input/output cable for computer data transmission, communications, and instrumentation data transfer. The cable assembly includes the 3M miniature delta ribbon (MDR) connector and pleated-foil cable (PFC). Its durable construction is said to offer high signal density, excellent electrical performance, and EMI shielding.

The brochure includes a cross-section illustration of the MDR/PFC assembly, a chart outlining the cable assembly's electrical properties, color illustrations, and complete cable ordering information.

I Need a Cellular Phone ... But Where Do I Start? Motorola Cellular Information Center; Phone: 800-331-6456, extension 2504; free.

A cellular phone is a valuable time-saving convenience for anyone who must travel extensively and yet stay in touch with a home office or operations base, customers, clients, or prospects. But buying a phone, subscribing to a cellular telephone company, and selecting a service plan can be daunting even for sophisticated people.

Motorola’s brochure lists tips to keep in mind when buying a cellular phone. It explains the different categories of cellular phones. Mobile phones, which are permanently installed in a vehicle, consume three watts of power and are ideal for those people who must spend a lot of time in their cars.

Transportable phones have self-contained batteries so they can be moved from one vehicle to another. They are a better choice for those who are likely to drive several different cars each day or must spend a lot of time away from their cars.

Portable, lightweight, handheld phones, can be carried in a purse or briefcase. They are recommended for those who are continually on the move, who switch from private to public transportation, or who must walk around a lot during the day.

The brochure outlines the six key points to investigate when buying a cellular telephone: talk time, sound quality, range, comfort, special features, and price. A glossary of cellular phone terms is also included.

Security Systems for Your Home and Automobile; by Gordon McComb. Prompt Publications, 2647 Waterfront Parkway, East Drive, Indianapolis, IN 46214-2012; Phone: 800-428-7267 or 317-298-5710; Fax: 317-298-5604; $16.95.

This book explains how to save money by installing your own security system. Modern security systems can deter property theft, vandalism, property boundary violations, and unwanted home intrusion. They even warn of fire and smoke danger.

Looking Good with CorelDRAW! Third Edition; by Sheldon Nemoy and C.J. Aiken. Ventana Press, P.O. Box 2468, Chapel Hill, NC 27515; Phone: 919-942-0220; Fax: 919-942-1140; $27.95.

This book explains how to get the most out of version 5 of CorelDRAW! This updated third edition contains hundreds of illustrations and step-by-step instructions for creating attractive graphics with CorelDRAW! 4 or 5.

A section of the book covers fundamental elements and program calls. It gives instructions for and examples of advanced techniques for constructing those elements. Icons on the screen indicate instructions that are specific to versions 4 or 5.

Nemoy and Aiken offer a wealth of practical advice for producing graphics including posters, book jack-
The authors also explain how to save time with the program’s tabbed dialogs, accent art work, and perform color, shading or texture fills. You’ll also learn how to make 3D extrusions with up to three light sources.

Op Amps Selection Guide. Analog Devices, Inc., 181 Ballardvale Street, Wilmington, MA 01887; Phone: 617-937-14228; Fax: 617-821-4273; free.

This six-page selection guide to Analog Devices’ single-supply operational amplifiers includes key specifications and technical information on more than 30 products. The brochure simplifies the selection of dual, single and triple op-amps such as the low-power, precision, instrumentation, and low-noise models that operate from single 1- to 36-volt supplies.

Eaton’s Literature Review identifies more than 55 catalogs that are available from Eaton’s many divisions that manufacture products ranging from relays, sensors, switches, and transducers to other parts like actuators and circuit breakers.

The four-color brochure details catalogs from divisions that include Arrow-Hart, Consolidated Controls, Control Displays, Cutler-Hammer, Heinemann, and MSC Products to simplify selecting the right one for the specific products you need.


This book explains how to turn your personal computer into your principal production tool for a personal-computer based business venture—It could be writing, accounting, consulting, desktop graphics preparation, or any of a number of other interesting possibilities.

The author discusses the requirements for success in any new venture, and explains how to evaluate your skills, goals and readiness to start your own business. You’ll learn how to select the right business to match your expectations and skills, how to make a business plan, sell your services, and run your home-based business.

It also explains how to choose the necessary computer software, hardware, and peripherals for your new business. The book discusses finances, including the need for startup money and where to get the money.

Davis describes in detail many business possibilities and the requirements for entry into them. He balances his discussion by listing potential roadblocks, but he explains how to avoid them. A separate appendix lists and describes 75 more home-based business ventures that depend on the personal computer.


This book explains how to assemble a complete home theater from standard, off-the-shelf, audio and video components.

Wolenik describes the many options available for building a home theater including stereo, broadcast and cable television, VCR, laser disc player, satellite receiving antenna, surround-sound speakers, and camcorders.

The author goes into technical detail in explaining the differences between the many products in each of the entertainment product categories. For example, you’ll learn what some of the important differences are between rear-projection, front-projection, and direct-view television receivers.

He also explains the importance of color, clarity, and resolution for pleasurable viewing, and the difference between Dolby Surround and Dolby Pro Logic. You’ll even learn how to place your speakers for the optimum surround-sound effect with encoded programming.

In addition to discussing the manufactured products, Wolenik includes guidance on the selection of the optimum room in your house or apartment for the installation of a home theater system.

He tells you how to install acoustic insulation in that room to minimize or eliminate unwanted noise to improve viewing and listening pleasure.

A 16-page, full color insert in the book illustrates actual home-theater installations, and pricing information is included for many of the components shown.
Last month I started a discussion of computer-industry unmentionables, beginning with the “D” word, documentation. Second on my list is the user-interface design. What is user-interface design?

Some think of it as sizing, shaping, and coloring screen widgets to achieve a visually pleasing result. That viewpoint is so outrageously incorrect as to be unworthy of comment. It comes from a prejudice based on an underlying “how” view of the world, versus a philosophic, theosophic, or even aesthetic “why” point of view.

Look at your computer (or at Fig. 1). It’s got a serial interface, a parallel interface, a hard-disk interface, a network interface, and a user interface. From one point of view (POV1), the user interface is just another thing that links the computer to some peripheral device, be it a printer, a modem, a network, or in this case, a user. That view might sound ridiculous, but that’s how many computer and software designers view the situation.

It would be easy to adopt a contrary point of view (POV2) that says the user is primary, and the computer secondary. The computer is just another member of the class of things that we human beings use to extend our capabilities, much like the car, the telephone, the microscope, and the telescope. This is a tack frequently taken by social scientists, anthropologists, and cultural analysts.

A third point of view (POV3) avoids the reductionist simplifications offered by the first two. It doesn’t seek understanding by reducing a complex situation to a set of interactions among simple elements. Rather, it views the situation as a whole, along with the interactions among the elements, as primary. User interface design thus becomes user interaction design.

Context

If you view the user interface as a conduit between the user and the computer, as do both POV1 and POV2, then you tend to focus on the characteristics of the conduit, the objects attached to either end of it, or the couplings between the conduit and the objects. From this mechanistic point of view, increasing bandwidth is seen as the primary means of increasing efficiency. In reality, this results in an ever-escalating desire for faster computers and higher resolution video screens—as well as smarter users. But suppose we had computers of infinite speed, and output devices of infinite resolution. Would computers be any easier to operate? In the absence of other changes, the answer is a resounding No!

POV3, or user interaction design, does not discount the need for greater computing power and resolution. But rather than putting the objects first, it views their interaction, their environment, and their Gestalt as primary.

Gestalt is a German word im-

USER INTERFACE DESIGN: Is the user just another peripheral with her own special interface? Is the computer an extension of human capabilities? Or is there something more to it?
ported into English by turn-of-the-century psychologists who sought to surpass the mechanistic (Newtonian) notions prevalent in the dominant theory of the time, associationism. Associationism holds that perception is the summation of numerous acts of sensation. The problem was that the associationists failed to show how electrical impulses in nerves translated into concepts such as life, love, or God.

Borrowing from then-emerging concepts of field theory, Gestalt theory posited, in contrast, that apprehension of the whole cannot be reduced to the mere sum of the parts. Quite the opposite in fact: The parts are only comprehensible within the context of the whole. Context is what poor interface designers usually fail to grasp. Context is what good interaction designers grasp implicitly. In real estate, it's location, location, location. Where the user interface is concerned, it's context, context, context.

**Context is dynamic**

Explanations of Gestalt theory frequently depend on static metaphors. An oft-cited example is that of identifying a structure presented in a skyline. The associationists would have us believe that the skyline is the sum of the perceptions of the individual structures. By contrast, Gestalt holds that the individual structures are identifiable only insofar as they are elements of that skyline.

Likewise, technologists tend to view the world as a collection of function boxes: input, process, output. The user clicks a mouse button, the computer does some processing, then presents some new output. Input, process, output. User, computer, screen. By contrast, a Gestalt view would see one thing—the interaction process—as a dynamic context in which inputs, processing, and outputs occur.

There are thus two primary yet diametrically opposed points of view concerning human-computer interaction: functional and process-oriented. The functional view has prevailed throughout the entire history of computing; it is only in the last few years, with the rise of the field called usability engineering, that the process-oriented point of view has started to attract serious attention. In the commercial world, the shift is beginning to manifest itself with a shift away from the functional paradigm toward something else, for which there is, as yet, no fully developed example.

The DOS version of the number one selling word processor, WordPerfect, is a prime example of the functional point of view. WordPerfect has scores and scores of functions, which despite their individual utility, lack an overarching unifying principle, or Gestalt. With Gestalt, all those features and functions would come to have meaning, to stand out as clearly as the Empire State Building does in the New York City skyline.

I have no example of a software product of any complexity that exhibits a fully developed Gestalt of the type I have discussed. But here is how you might recognize one.

First is the obviousness of its use, given a basic understanding of the overall Gestalt. Second is the elegance of its design, which in practical terms means discernible pattern in the way functions are grouped and presented. Third is scope consistency, or consistency at various levels of design (low, middle, and high). The opposite of scope consistency is a huge catchall of features.

Command-line oriented operating system shells are interesting to discuss from this perspective. The Unix C shell and the DOS COMMAND.COM are two prime examples. The Unix shell has an almost astounding collection of tools, which is great. What is bad is the total lack of consistency among them. Even among people who aren't afraid of command-line interfaces, Unix commands provide a severe test. It's not hard to stump even experienced Unix users on some arcane feature or another.

The MS-DOS shell can be viewed as a very limited subset of the Unix shell, but it is, nonetheless, full of inconsistencies. For example, modern versions of the dir command allow you to select and sort directory listings in various ways. In a better system, the same select and sort options would apply to commands across the board. For example, the command DIR /AD /S /B lists all directories beneath the current directory. If the COPY command had the same options, I could duplicate the disk structure, without copying all the associated files, by typing COPY FROMDISK TODISK /AD /S /B.

In the graphical user interface (GUI) world, it is instructive to compare OS/2 to Windows 3.1 and to the upcoming version of Windows, code-named Chicago, but now officially known as Windows 95. There is nothing to be said that hasn't already been said about the problems with the Program Manager/File Manager dichotomy in Win31.

On the other hand, not enough has been said about the elegant, consistent design exhibited by OS/2 2.x and later versions. The reason is probably the large difference in usage between it and the most popular mainstream system.

The June '94 beta version of Windows 95 shows a typical Microsoft response to the migration problem. The W95 shell takes a step toward OS/2-like consistency and elegance, but fails to go all the way. Of course, because it is a beta, the shell can (and almost certainly will) change, but given Microsoft's history, I doubt that it will go as far as OS/2 has. This is a smart marketing move by Microsoft, and a risky one by IBM. But if history repeats itself, Microsoft's "not as good as it could be, but at least it's a step forward" approach will win, rather than IBM's "here's the solution to all your problems, just drop all current ways of doing things" approach. Don't get me wrong—I'd like to see IBM's approach win. But I think Microsoft's will win.

**Tools, environments, and agents**

Let's get back to the subject. The purpose of traditional user interface design is to build a link between two static objects, a computer and a user. The purpose of user interaction design is to build (1) tools and (2) an environment to ease and enhance the interaction among (3) two or more actors or agents. Let's now look at each component in more detail, in reverse order.

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person or a computer process.

2. A given environment might include one or more persons or processes. Processes might operate on one or more computers.

1. A tool is what I referred to easier as a function or a collection of functions. A tool is designed and integrated within a conceptually unified architecture; it is not just a random collection of capabilities (the WordPerfect model).

More generally, the environment consists of everything perceivable—presently sight, touch, and sound, but eventually including taste and smell. It won't be long before so-called virtual reality technology gives rise to the VUI.

GUI-building tools such as Visual Basic and App Studio must evolve from being only drawing tools for creation of static screen objects, to become "interface" simulators that allow self-modifying actors to interact. In this scenario, user-interface design becomes less like a drawing activity, and more like specifying the rules of an expert system.

Objects

Object-oriented technology holds some promise for improving user-interface design. The reason has nothing to do with encapsulation, inheritance, or polymorphism. It is rather the real-world modeling that frequently accompanies object-oriented technology projects. The problem here is model proliferation. The human body is a good analogy. In it, multiple subsystems (circulatory, respiratory, nervous, skeletal, muscular) coexist and interact simultaneously. As software continues to increase in complexity, a similar concept is necessary so that user-interface design and implementation can proceed essentially independently of functional design and implementation.

The question then becomes how computer system design generally can evolve to support multiple simultaneously functioning and interacting subsystems explicitly. But that's a topic for another time.

Meanwhile, don't let anyone fool you. There is much more to user interaction design than is obvious. As always, comments are welcome: email jkh@acm.org.

continued from page 6

nounced that it will develop a recordable version next year. The TDK system will be a write-once type and is claimed to be much cheaper than proposed multi-recordable systems, which can erase and record many times. TDK says that its write-once system also will be much cheaper than rewritable types that use phase-change technology.

● "Multimedia" camcorder.

Building on the success of its Viewcam—which combines an LCD monitor screen with a camcorder—Sharp has introduced a new version that doubles as a communications device. Sharp is calling it the first multimedia camcorder. The new top-of-the-line Viewcam contains a four-inch LCD color monitor with excellent resolution. It has connectors built into its base so that it can be placed on a stand (included with the camcorder) that connects it to a TV for playback. But that's not the only use for the connectors in the bottom of the machine. The camcorder also docks easily onto an extra-cost "Viewcam teleport" that has a built-in telephone jack. Also in the teleport is a solid-state memory device capable of storing 10 still color pictures, which can be selected from the tape in the camcorder, photographed live, or adapted form any other video source.

The teleport-equipped camcorder can send pictures via a standard phone connection to any other similarly equipped Viewcam. At the receiving end, the teleport can store up to 10 pictures in its solid-state memory for later viewing—either on the Viewcam's LCD screen or on a TV set. The digital transmissions provide three grades of picture, depending on transmission time—8, 11, or 20 seconds per picture. At a recent demonstration, the 20-second version was undistinguishable from the original.

The teleport also includes an audio-visual telephone answering system. If the called party doesn't answer, a recorded voice says: "Please transmit a video picture or
The theft of video signals has cable-TV and satellite-TV programmers aggressively pursuing signal pirates.

**Signal Theft**

**PAUL PARADISE***

VIDEO SIGNAL THEFT IS NOT NEW. It's hardly sensational, and it's rarely prosecuted. However, the cable-TV industry, by its own estimates, loses billions of dollars each year because of it. As the cable and satellite-TV industries prepare for new interactive technologies, they have become increasingly aggressive in trying to thwart signal pirates.

Perhaps the most dramatic action by a signal pirate was the transmission of the following message that was seen by hundreds of thousands of cable subscribers in the East and Midwest during an HBO cablecast of the movie *The Falcon and the Snowman*: "Good Evening HBO from Captain Midnight. $12.95 a month? No way! (Showtime/The Movie Channel Beware.)"

The sender, who used a satellite uplink to superimpose his message on the HBO transmission, was eventually caught and prosecuted. But his sentiments regarding the rising cost for premium cable television and signal scrambling are shared by many.

In January 1986, HBO and Cinemax, both owned by Time, Inc. became the first two cable programmers to scramble their satellite signals, thereby preventing people who owned satellite-TV reception (or TVRO) systems from watching their programming without paying a monthly subscription fee.

*Excerpted from the forthcoming book: Designer Counterfetting.*
In May, 1986 little more than a week after Captain Midnight's pirate broadcast, Showtime and the Movie Channel followed suit and scrambled their signals. Today, virtually all of the major cable networks scramble their satellite feeds.

Despite signal scrambling and a significant enforcement effort by the cable industry and the Motion Picture Association of America (MPAA) to apprehend illegal users, signal theft remains rampant. According to the National Cable Television Association (NCTA), almost one-quarter of all cable viewers in this country do not pay for the service. In 1992, the NCTA estimated that signal theft amounted to a loss to the cable industry of $4.75 billion.

**Satellite scrambling history**

Signal theft grew in popularity with the growth of the home satellite TV market in the early 1980s. Home TVRO systems first became available in 1979 and were particularly attractive to TV-starved rural residents. At that time, a home satellite system cost $10,000.

In just a few years, the cost for satellite dishes dropped to $2,500, and demand for the dishes surged even in urban areas. Home TVRO systems became a growing concern to programmers. They worried that the availability of consumer satellite-TV systems would cause cable-TV subscriptions to plummet, thus reducing their revenues. The industry sought a way to prevent unauthorized viewers from watching their signals; the result was that programmers scrambled their satellite-delivered signals.

Signal scrambling upset consumers and dealt a major blow to the satellite-TV industry. Sales of satellite systems, which had reached 70,000 a month, fell to fewer than 15,000 a month. The early signal scrambling, however, spawned a new industry: illegal descrambling.

The scrambling method chosen by HBO that became the de facto standard for satellite-delivered television was VideoCipher II, developed by M/A-COM. VideoCipher II scrambles the video portion of the signal by replacing the horizontal- and vertical-sync signals with digital data. The digital data stream contains the audio portion of the signal, as well as the authorization codes or addresses of all legitimate descramblers. The digital data are encrypted with the data encryption standard or DES.

Although the DES itself was never "beaten" by signal pirates, VideoCipher scrambling proved to be easy to defeat through several "back doors." Descramblers, for example, were cloned so that a single legitimate subscription could turn on thousands of descramblers.

After pirates had compromised the security of VideoCipher II, General Instrument Corp., which bought the technology from M/A-COM, was forced to develop a new scrambling scheme called VideoCipher II Plus. The Plus system has yet to be successfully "hacked." The most recent version of the scrambling technology is VideoCipher Renewable-Security or VCRS.

The VCRS system has two features that make it resistant to piracy. First, developing a way to defeat the system would require a considerable investment in advanced technology. Second, the VCRS module has a provision to accept smart cards to update the encryption technology to counteract any "hacks" or security breaks. The smart cards can be produced quickly and cheaply, allowing any security breaks to be patched promptly.

**Other Satellite piracy**

Despite the development of the VCRS that has virtually eliminated signal theft by home satellite-TV viewers, satellite theft remains a serious problem, according to Dennis Powers, Chief of Signal Security, Legal Department of HBO. "The main focus of our signal theft efforts is the commercial misapplication of our satellite signal," said Powers. "We're not necessarily talking about boxes or modules that have been compromised or pirated, but multiple dwelling areas like trailer parks, apartment complexes, and recreational-vehicle parks that have set up their own cable..."
systems under the guise of being TVRO installations. The pirate is paying a user fee, but is bringing down our signal and then redistributing it throughout the complex and charging a fee to each subscriber.”

According to Powers, the illegal user is acting as an illegal distributor or illegal franchisee by selling the programming to other users who may, or may not, realize that he is doing so without authorization.

Other forms of satellite theft include sports bars that pick up sporting events not usually available on broadcast channels or cable networks.

Some sporting events that are distributed by satellite are not available in certain “black out” areas. For example, Major League Baseball has ruled that out-of-town games should not be made available anywhere where the home team is in action. That means that an avid fan of the San Francisco Giants who lives in New York would not be able to view his favorite team if either the Yankees or Mets were in action. The rules for NFL football prohibit a home game from being televised in the team’s region if the stadium isn’t sold out 72 hours prior to kickoff.

Such rules can be enforced by VideoCipher, which has the ability to black out programming according to ZIP codes. However, some TVRO system owners have been known to give incorrect address information when ordering program subscriptions so that they could watch programming that would otherwise have been blocked out to them.

Commercial establishments such as sports bars that masquerade as residences have been another problem. In this case, an establishment attempts to reduce its subscription fees by registering for a residential instead of commercial subscription.

Such satellite theft is difficult to trace. Leads for enforcement come in through many avenues, including rival sports bars that have legitimate program subscriptions. Agents who work for the major leagues or private investigators visit sports bars throughout the country to monitor what is being shown. Late last year, NFL Enterprises, Inc. filed civil suits against dozens of bars across the country for buying residential subscriptions to its NFL Sunday Ticket package. Residential subscriptions cost $139 for the football season, while commercial establishments pay from $600 to $2000, depending on their size.

To catch suspected signal pirates, NFL enterprises sent out teams of investigators to sports bars. During stops in play, the league caused all VideoCipher modules to display their identification numbers on the TV screen so that its investigators could note them and compare them against its subscription database.

Yet another form of satellite-signal theft occurs overseas. The Motion Picture Association of America (MPAA) has repeatedly cited the Caribbean area as a hotbed of piracy, both for pirated videocassettes and signal theft. However, the MPAA does not authorize cable programmers to distribute their services outside the U.S. If people in the Caribbean countries want cable services, they have no choice but to engage in signal theft.

“Technically, the footprint of the satellite signal is there,” said Matthew Sappern, manager of corporate affairs for HBO. “HBO doesn’t have the right to legally distribute and market its services outside the U.S. based on the covenants we have with the Hollywood studios.” Because cable programmers lack distribution rights in the Caribbean area, their anti-piracy efforts are hindered.

According to Powers, the Caribbean Cable Association is lobbying the MPAA in Hollywood to allow the programmers to distribute outside the U.S. The MPAA has thus far not granted distribution rights because of its release schedule for new movies. The release schedule is a marketing umbrella whereby new movies are released first to the U.S. theaters, then to the foreign theater market, before being released for videocassette distribution, cable television and network television. This prevents a movie from appearing in the theaters and on videocassette or cable television at the same time.

**Direct-broadcast satellites**

In October of last year, a new satellite service was rolled out nationally: the RCA Digital Satellite System which broadcasts digital video and audio signals from high-power direct-broadcast satellites (DBS). The three major players responsible for the launch are RCA/Thomson Consumer Electronics, DirecTV (a unit of General Motors Hughes Electronics), and
The encryption and conditional-access system chosen for DSS, a completely digital system, was developed by the News Datacom division of Rupert Murdoch’s News Corporation. The receiver accepts a smart card through a slot in its front panel, which allows the receiver to decode the programming that it is authorized for.

The rationale for choosing the system is that the smart card is difficult to reverse-engineer, yet is easy and inexpensive to upgrade and replace if a security break makes it necessary. In that way, it is similar to VCRS.

However, in Europe, a very similar system from News Datacom provides conditional access control for the Sky satellite service. The system has been repeatedly subjected to "hacks" by satellite pirates. Officials of the companies involved remain confident that any security breaks in the DSS encryption will be repaired quickly and inexpensively.

What the law says

Signal theft became a Federal crime under the Cable Communications Policy Act of 1984 [Title 47 USC, Section 605]. The Act states that "No person shall intercept or receive or assist in intercepting or receiving any communications service offered over a cable system, unless specifically authorized to do so by a cable operator or as may otherwise be specifically authorized by law." Satellite-delivered programming, because it is distributed primarily to cable companies, is also covered under the Cable Act.

The Act clearly mentions equipment used for signal theft. It states: "For the purpose of this section, the term assisting in intercepting or receiving shall include the manufacture or distribution of equipment intended by the manufacturer or distributor (as the case may be) for unauthorized reception of any communications service offered over a cable system."

For a first offense under the Cable Television Consumer Protection and Competition Act of 1992 [Title 47 USC, Section 553], a fine of $50,000 and imprisonment of up to two years, or both, may be handed down. A repeat offender can be fined up to $100,000 and imprisoned for more than five years.

Only a manufacturer or distributor of illegal decoders or other descrambling devices is likely to receive imprisonment under the Cable Acts. A homeowner with no criminal record is not likely to go to jail for illegally connecting to the cable system. In many instances, the homeowner will be offered amnesty by the cable company and asked to subscribe.

"Our department performs many functions," says Bob Astarita, vice-president of security for Cablevision, the fifth largest Multiple Systems Operator (MSO) in the country. "One of the most critical is what we call a tap-audit function. Security technicians literally walk the system and make a determination if anyone is connected improperly or illegally."

In the first instance, according to Astarita, the illegal tap is treated as an unauthorized connection—one in which an individual is receiving programming through no fault of his own. That could happen, for example, if someone moved into an apartment and hooked his equipment up before determining that the prior occupant forgot to contact the cable company to have the service discontinued.

After the programming is cut off and the connection removed, a salesman will call and ask if the party would like to subscribe. If a tap audit discloses that the party is hooked up illegally a second time, it is treated as an illegal theft. The illegal connection is photographed and removed as evidence.

"Now you are illegal," says Henry Hack, director of investigations for Cablevision. "You have committed a crime. Theft of services is a Class A misdemeanor in New York State. You will be sent a cease-and-desist letter, and the security department will monitor the situation." No legal action will be
taken unless the party hooks up for a second time. After the second offense, Cablevision will initiate either a civil action or a criminal action.

In a criminal action, a police officer will come to the house, determine that the party is hooked up illegally, and issue a desk appearance ticket. In New York State, theft of services is punishable by up to a $1000 fine or a year in jail. In most instances, if the homeowner has no criminal record, he will be able to plea bargain to a lesser offense. Most legal actions involve a civil suit. Damage awards start at about $1,500 in a civil suit.

"When I think of a pirate, I think of a seller or a distributor of illegal electronic products, not a homeowner," says Hack. "This is a business entity that advertises openly and is aware of the law." According to Hack, most illegal distributors do not sell in the states in which they are located to avoid prosecution under state law.

A typical brochure from a mail-order operation will display seemingly top-of-the-line equipment with brand names such as General Instrument, Panasonic, Toshiba and Scientific Atlanta. Usually, the channel converter, which can be legally acquired, will be offered for sale, along with the add-on or stand-alone descrambler—also called a starbase, a blackbox, a pancake, or a hotplate in the pirate trade.

In some instances, the equipment offered for sale is acquired from a cable operator who is about to upgrade the equipment in his franchise. In such cases, a distributor who buys the inventory that is to be upgraded diverts the equipment to a pirate operation.

"Piracy goes well beyond electronic hobbyists," Astarita said. "We encounter people who have Ph.D.s and others who have extensive backgrounds and degrees in many other academic disciplines."

Astarita, who is a former FBI agent, heads a staff of former law enforcement professionals. He and his staff conduct "buy-and-bust" operations and gather information to be used against pirate operations as part of their daily jobs.

Cable-signal theft can mean more than lost revenue to cable companies. One of the most serious problems caused by the proliferation of pirate electronic equipment is signal leakage. Hooking up an illegal decoder requires some technical expertise and the proper tools. A decoder that is not properly installed will cause signal leakage—radiation that poses a threat by interfering with commercial aircraft radio frequencies.

"We're supposed to be a closed system and there should be no leakage," said Hack. "The FCC does flyovers and measures the signal leakage, if the amount exceeds the cumulative leakage index (CLI), we will be fined heavily." Most cable operators have CLI teams who seek out potential signal leakage throughout the cable system.

Cable fights back

The technological battle between the cable companies and the pirates has led to some interesting anti-piracy devices, including the "electronic bullet." In April 1991, for example, American Cablevision of Queens, New York, filed suit against 317 cable customers who were pirating signals.

Jerrold Communications, a division of General Instrument Corp., learned that its converters were being compromised by an override chip. The black market chips were installed in a basic converter to obtain free premium programming. After obtaining several pirate devices, Jerrold engineers devised a strategy for outwitting the chip. The engineers invented a "bullet" that used the chip's own programs to neutralize it.

"The bullet is designed to blow out a box that has been tampered with," Hack explained. "Our computers talk directly to the decoders that we purchase from the manufacturer and tell it what to authorize. To use the bullet, we send a signal down the line that says: 'ignore the next message,' and the legitimate boxes will ignore the next message—the next
message being: "blow yourself up." There is no fusing or electrical charge or "bullet"—just a deauthorization. Incredibly, the bullet succeeded because irate homeowners with pirated boxes—unaware that a "bullet" had been fired—called the cable company to complain about the lack of reception.

Despite the penalties afforded under the Cable Acts of 1984 and 1992, the sale of illegal equipment is rampant. Illegal decoders are offered for sale in electronics stores, through mail-order companies, and are even advertised in national magazines. The sale and advertisement of illegal decoders can be found throughout the country.

Will Nix who joined the Motion Picture Association of America (MPAA) in 1976 and was promoted to the title of Chief Operating Officer of the MPAA's anti-piracy division, participated in organizing a nationwide effort to combat signal theft. Nix left the MPAA in 1991.

According to Nix, at one time during the 1980's about fifty percent of the satellite decoders sold by General Instrument were being compromised by a illegal computer chips. "General Instrument wanted to transfer its in-house anti-piracy effort into a larger, national effort," Nix said. "We helped organize the Office of Cable Signal Theft (OCST) as a joint effort by the Satellite Communications Broadcast Association (SCBA) and the MPAA."

OCST was formed in 1986 and today is part of the National Cable Television Association, in Washington, D.C., and funded by both the NCTA and the MPAA. OCST works closely with the Department of Justice, the F.B.I., U.S. Customs, state and local prosecutors, as well as law enforcement agencies throughout the country. OCST provides assistance to these enforcement agencies in prosecuting criminal violators. In the last three years, OCST has been involved in the seizure of 400,000 illegal decoders.

"Another organization that I assisted in forming is the Coalition Opposing Signal Theft (COST)," Nix said. "COST was set up as a joint venture between the NCTA and the MPAA, and was designed to address issues in the area of signal theft."

Many of the more than 10,000 cable operators are members in the OCST and COST, which is part of the OCST advisory committee. Mr. Astarita is the current vice-chairman of COST.

The inside problem
"When I first moved into Manhattan, the cable technician who hooked me up asked if I wanted to do this the legal way or the illegal way," said HBO's Matthew Sappern.

For some cash, the cable technician was offering to hook up the premium channels for Sappern, who would thereafter receive them for free. Sappern's experience is by no means an isolated one. Moreover, the largest source of illegal decoding devices on the black market today is cable operators themselves. It is estimated that as much as 90% of the market in illegal decoders can be traced back to the cable operators. It should be noted that in many instances, a cable operator who is upgrading his equipment will unknowingly sell his existing inventory to a distributor who, in turn, will divert the inventory to an illegal use.

"We at Cablevision are aware that a great deal of the illegal product comes from within," Astarita explained. "Cablevision monitors what happens to its old cable boxes, and in some instances we destroy the boxes if we cannot sell them to a reputable source."

Cablevision prides itself on being a leader in the field of addressing theft. It conducts due diligence inquiries on contractors and vendors with whom it does business. It will sell old cable products only to a distributor who can document the inventory's destination or to a licensed franchise cable operator.

Future problems?
Interactive television will dramatically change the content of cable programming and the problem of signal theft. In late 1994, Time Warner Cable Systems was scheduled to introducing interactive television to some 4000 homes in Orlando, Florida. The Orlando project will cost about $5000 per household. Digital Equipment Corp. and General Instrument Corp. are joining forces to produce the interactive equipment, which will combine DEC's microprocessor, distribution, and storage technologies with GI's encryption system that allows financial and other information to be sent confidentially.

The Orlando endeavor is the largest of many interactive television projects that will get underway this year. Interactive television will ultimately change the concept of the cable operator, who will be offering much more than simple television programming. EMInteractive television is the result of a merger of the technologies of many industries: computer, cable, television and telephone. Interactive television will allow the subscriber to 'interact' with the television. In the envisioned systems, the interactive cable subscriber will be able to talk face to face with his neighbor or his employer, shop and bank from his television, and view conventional television programming as well. Virtually all of the signals for interactive TV will be digital.

In June 1994, British television viewers got their first introduction to interactive television. Two commercial broadcasters, Carlton Television and London Weekend Television, joined forces with a cable operator to offer an experimental interactive London news channel. The cable operator's 65,000 subscribers can choose from four channels of programming to concentrate on weather, traffic, community and social action reports or the regular news program. In 1995, the cable operator hopes to introduce interactive programming that will allow the viewer to communicate with the studio. Viewers will be able to vote on programs or the performance of a politician.

Continued on page 90
This simple, passive integrated-circuit tester can be a valuable addition to your test equipment.

MARK HANSLIP

A TESTER FOR INTEGRATED CIRCUITS can be passive or active. An active tester determines how a device reacts to a set of input signals. It can determine if an IC is faulty, but only if the device is removed from its host circuit. The passive tester described here can test ICs in a circuit, and does not need to be reconfigured for each device to be tested. A passive tester can also function as a logic analyzer to monitor input and produce output signals.

This article describes how to design, build, and use a simple, inexpensive passive IC tester that can be a valuable addition to your suite of test equipment. But keep in mind that the tester is designed for testing TTL and CMOS devices powered by +5 volts, only.

The tester can test devices with any number of pins. The author designed his prototype to test ICs with up to 20 pins. Chips with 8 to 20 pins that are packaged in DIPs (dual in-line packages) usually have the same width and pin spacing. Thus if a zero-insertion-force (ZIF) socket is added to the integrated-circuit tester, it will be able to accept most 8-, 14-, 16-, 18-, and 20-pin ICs.

The IC tester puts one or more pins of a known good device in parallel with the corresponding pins of a suspect device. The tester then lights one LED lamp if differences are found in the signals between any matching pins, and other LEDs on the tester light up to show where those differences are.

Circuit design

A typical input circuit is shown at left in the Fig. 1 schematic; one is needed for each test pin. (Only one input circuit is shown. It can test only one suspect pin at a time, but the tester can be built with as many input circuits as you need. Connect additional input circuits to the latch circuit via the 1N4148 diodes as shown in the schematic.) The 74LS266 is an open-collector quad EXCLUSIVE NOR (XNOR) gate. One input to each 74LS266 gate is attached to one pin of the device under test (DUT), and the other input is attached to the same pin of the "good" chip. A single 74LS266 can accommodate up to four inputs, although only a single input is shown in the schematic.

When the two inputs to a 74LS266 gate are the same (e.g., pin 3 of the DUT and pin 3 of the reference device), the output is high; when the inputs differ, the output is low.

Multiple 74LS266 output signals are added together through a series of 1N4148 diodes which are connected to the latch circuit. Only a single latch circuit is needed for the entire tester. After power is applied to the tester, push reset button S1 to initialize the circuit. The reset
FIG. 1—THIS SIMPLE IC TESTER compares two logic signals and indicates whether the signals are the same or different.

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Rain forests occupy just 2% of the earth's surface. Yet, these rain forests are home to half of the planet's tree, plant and wildlife species. Tragically, 96,000 acres of rain forest are burned every day. You can help stop this senseless destruction. Right now you can join the National Arbor Day Foundation, the world's largest tree-planting environmental organization, and support Rain Forest Rescue to stop further burning.

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causes bi-color LED2 to light up green. After that, any low output from a 74LS266 will trigger the latch circuit which drives the bi-color LED to red. That color indicates that at least one pin of the DUT doesn't agree with the good chip. The faulty pin is flagged by the LED (LED1 in Fig. 1) attached to the corresponding gate's output. Press the reset pushbutton again to start a new test.

The 330-ohm resistor that parallels the comparator's inputs (R2) allows the signals to the DUT to flow to the reference IC as well. That resistor also prevents the output of the DUT from affecting the reference IC. The jumper that parallels the resistor can short circuit the ground and +5-volt pins of the DUT to the reference IC so the reference IC can be powered by the DUT circuit. Power for the remainder of the test circuit (LED, comparators, and latch) must come from an external power supply.

Remember that the tester is designed for testing 5-volt TTL and CMOS devices only. To prevent damage, do not exceed that voltage on any pin.

The tester can be converted to a logic analyzer by inserting a DIP header into the test socket. All of the DIP header pins except the power pin should be connected together and grounded. This will allow you to monitor the signals going to and coming from the DUT with the green LEDs.

Tester use

To use the tester, first connect the test input to the suspect pin of the DUT. Next, connect the reference input to the same pin of an identical reference chip that is known-to-be-good. Push the reset button to begin the test; the green section of the bi-color LED will be illuminated. Any signal on the test device that differs from the one on the reference device will then momentarily light the LED lamp that corresponds to that pin, and also latch on the red section of the bi-color LED. That indicates that the device under test is faulty. If the reference and DUT signals are the same, the DUT is OK, and the green LED will remain lit.
A programmable sinewave generator can be a lot more accurate than an analog-based generator. When teamed with a PC or single-board computer, a programmable generator becomes an application-specific instrument offering a limitless variety of software-based “front panels” without the need to modify the hardware. It’s a fun device to build and experiment with. Plus, you have to build it only once, but you can program it forever!

There are many tasks that can be performed with a programmable sinewave generator (PSG):

- Convert RS-232 signals to audio or RF frequency FSK (frequency shift keying) format for phone line or wireless modem transmitters
- Function as a signal source for bode plots
- Function as a linear, log, discrete, or programmed sweep generator
- Act as a local oscillator and carrier frequency generator for a transceiver
- Function as a general-purpose generator for industry, education, and experimenter labs
- Synthesize single-voice music compositions
- Generate telephone keypad tones
- Synthesize voice or sound
- Act as a general-purpose secondary frequency standard
- Generate frequency bursts
- Generate continuous-wave amplitude modulation
- Provide a stable, accurate voltage-controlled oscillator for amateur radios
- Generate automatic-test-equipment sweep signals

A computer’s parallel port is ideal for controlling a PSG because the parallel port is easy to use, and there is one in most personal computers made today—including most laptop models. Although the serial port could be used, the required
FIG. 1—PSG SCHEMATIC. The NCO chip is a serial input device that needs either 32 or 64 bits of data to generate sinewaves; 32 bits are required for single-frequency operation and 64 bits are required for dual-frequency (FSK) operation.

Once the sinewave has been synthesized, it is level-shifted to be symmetrical around zero volts and then filtered to remove the remaining components of the high-frequency NCO clock frequency (32 MHz). Finally, the sinewave is buffered and fed to the PSG's output.

How does it work?

Refer to the upper left-hand corner of the schematic, Fig. 1. The DATA, CLOCK, FLOAD, and ON/
### Table 1

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<th>7</th>
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<td>DATA</td>
<td>CLOCK</td>
<td></td>
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</tbody>
</table>

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### PSG COMPONENT SIDE.

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### PSG SOLDER SIDE.

OFF input lines couple the board to a PC's parallel port. Each of the four inputs is buffered by IC1 and then fed to the HSP45102 NCO chip. The NCO chip is a serial input device that needs either 32 or 64 bits of data to start generating sine-waves; 32 bits are required for single-frequency operation and 64 bits are required for dual frequency shift keying (FSK).

A shift-clock pulse is generated by the PC with each data bit fed to the DATA input, and it is fed to the CLOCK input of the NCO. When all 32 (or 64) data bits have been fed to the NCO, the FLOAD line is activated and the new frequency(s) become available at the output of the generator. The ON/OFF control line turns the output signal on or off under program control.

The TTL-compatible FSK modulation input selects one of the two programmed frequencies to be seen at the output of the instrument. For example, assume the two programmed frequencies are 1.0001 megahertz and 0.9999 megahertz. A high level (TTL logic 1) at the FSK input would cause the 1.001-megahertz signal to appear at the output, while a low level (TTL logic 0) would cause the 0.999 megahertz signal to show up at the output. The switching delay between signals is six clock pulses—in this case, 187.5 nanoseconds.

The FSK input is held high by 100K resistor R6 to ensure that the first 32 bits of input data activate the NCO. The FSK input is protected from negative voltages by D1 and voltages in excess of +5 volts by D2.

When the NCO has received valid data, it computes the location of the sinewave amplitudes (stored in ROM) needed to generate the output signal. For example, if a 1-megahertz sinewave has been requested, the NCO computes the location of the 32 amplitude values necessary to make up the 1-megahertz sinewave \( F_{CLK}/F_{OUT} = \text{number of amplitude values} \) and then sends the binary values in a 12-bit format to 12 output lines at a 32-megahertz rate (every 31.25 nanoseconds). A digital-to-analog converter (DAC) connected to the NCO's output lines converts the amplitudes to analog voltages. A 12-bit, 31.25-nanosecond-setting-time DAC is needlessly expensive, so an 8-bit DAC is substituted. The DAC's vertical
resolution, better than 0.4%, is adequate for this application.

The amplitude of the DAC output signal is controlled by R7 while the sinewave DC zero level is set by R9. The DAC output (0 to +5 volts unloaded) must be level-shifted to produce a sinewave symmetrical around zero volts. It also must be filtered to produce clean sinewaves.

Because the number of samples per sinewave cycle is equal to the ratio of the clock frequency and the desired output frequency, it can be seen that at 5 megahertz, the number of samples forming the sinewave will be 6.4 (32 MHz/5 MHz), which is a pretty "steppy" sinewave.

The two problems, filtering and level-shifting, are solved by the Maxim MAX436 wideband transconductance amplifier IC5. A transconductance amplifier is a true differential amplifier with high-impedance inputs. It provides accurate gain without negative feedback, eliminating closed-loop phase shift. This is the main cause of oscillation in voltage-output, high-speed amplifiers. The output of the transconductance amplifier is a current that is proportional to the differential input voltage, and the amplifier is virtually short-circuit proof. The gain of the circuit is set by the ratio of two external impedances and an internal current gain factor K:

\[ \text{Gain} = \frac{K(Z_{LOAD}/Z_T)}{K} \]

The device also has a bandwidth in the 275-megahertz range with an 800-volt-per-microsecond slew rate.

For level-shifting, R9 is connected between +5 volts and ground with its center tap fed to the negative input terminal of the MAX436. Simply adjust R9 so that the output signal is symmetrical about ground.

Three resistive-capacitive (RC) sections are distributed throughout the circuit. The first section consists of the output impedance of DAC IC3, R7, R8, and C3. The second is comprised of R13, the output impedance of the transconductance amplifier, the input impedance of the complementary

**PARTS LIST**

All resistors are 1/4-watt, 5%, unless noted.

- R1–R5: 10,000 ohms
- R6: 100,000 ohms
- R7: 500 ohms, \( \frac{\text{1/4}}{\text{inch}} \) round, single-turn cermet trimmer potentiometer
- R8: 120 ohms
- R9: 2000 ohms, \( \frac{\text{1/4}}{\text{inch}} \) round, single-turn cermet trimmer potentiometer
- R10: 390 ohms
- R11, R14–R16: 1000 ohms
- R12: 4700 ohms
- R13: 4700 ohms
- R17: 39 ohms
- C1, C2, C5–C7, C11, C12: 0.1 µF ceramic
- C3, C8: 47 pf, 5%, ceramic NPO
- C4: 22 pf, 5%, ceramic NPO
- C9–150 pf, 5%, ceramic NPO
- C10: 47 µF, 25 volts, electrolytic
- C13: 22 µF, 25 volts, electrolytic
- C14: 560 µF, 16 volts, electrolytic
- Semiconductors
  - IC1: 74HC245 octal non-inverting bus transceiver
  - IC2: HSP4512 12-bit numerically controlled oscillator (Harris)
  - IC3: CA3336A 8-bit DAC (Harris)
  - IC4: NEL HFS102 32-MHz clock oscillator module (Mouser No. 332-3320 or equivalent)
  - IC5: MAX436 wideband transconductance amplifier (Maxim)
  - IC6: 7805.5 volt regulator (TO-220 package, Motorola or equivalent)
  - IC7: LM2574-5 inverting switching
emitter-follower (Q1 and Q2), and C8. The final RC section consists of R10, R11, and C4. With the values shown in Fig. 1, the NCO generates a relatively constant 5-volt peak-to-peak signal into an open circuit from 0.1 hertz to 5 megahertz. At 10 megahertz the output amplitude is down to 3 volts peak-to-peak.

The impedance seen looking into the joined emitters of the two transistors (Q1 and Q2) that make up the simple complimentary emitter-follower output driver is about 11 ohms. The 39-ohm resistor (R17) in series with the output terminal sets the output impedance seen by the load to 50 ohms.

Two operating voltages are required for this circuit to work: +5 volts and −5 volts. Both voltages are derived from a 9-volt AC-to-DC adapter. The +5 volts is supplied by an LM7805 voltage regulator. A National Semiconductor LM2574 switching regulator generates the −5 volts. Diode D4 in series with the regulators protects the board against accidental power-supply reversals. The +5-volt supply must provide about 200 milliamperes, so the LM7805 should be fitted with a heat sink.

The 32-megahertz oscillator could have been built with discrete components for a few dollars less than the clock module IC4 that is specified. However, 32-megahertz oscillators can be cranky at times, and they tend to be noisy. By contrast, the module specified is small and quite reliable.

**Programming**

The PC must manipulate four control lines for the PSG to work. The clock line is a PC-simulated switch for moving data (on the data line) into the NCO buffer. The FLOAD line transfers data from the NCO's input buffer to its active registers, and the ON/OFF line turns the PSG output on and off. The four control lines correspond to the first four lines of the parallel port data register as shown in Table 1.

To program the PSG, first
specify some output frequency. Enter that frequency with an input statement (assuming a program written in QBASIC) and then convert the frequency to the format that the NCO wants to see by using the following equation:

\[ N = \text{Integer Portion} \left( f_{\text{OUT}} \times 2^{32}/f_{\text{CLK}} \right) \]

where: \( N \) = NCO code number, \( f_{\text{OUT}} \) = The output frequency, and \( f_{\text{CLK}} \) = 32 MHz.

The integer portion of the equation means that only the digits to the left of the decimal point are used for \( N \). Using Basic's long-integer suffix ensures that the NCO frequency code number \( N \) will be stored in a 32-bit format. An "&" following a variable declares it a long-integer which happens to be 32 bits long.

The program for the PSG shown in Listing 1 is written in QBASIC version 4.5. The program has a few nice features such as: parallel-port selection (LPT1, LPT2, or LPT3), a multi-color display, error messages, and user prompts. The program has been tested on both a 386-based IBM-compatible PC and an old monochrome 8088-based PC running at 4.77 megahertz, and it performs equally well on both machines.

This article will not include a line-by-line analysis of the program. However, consider the "sub load" subroutine. This is where the NCO data word is converted from parallel to serial format and sent to the NCO board. The easiest way to understand what's going on here is to study Fig. 2, a partial flowchart of the subroutine.

First the 32-bit NCO frequency code must be read into the board bit-by-bit. The board is set up for most-significant-bit first entry of the serial data (bit 32 goes to the NCO first and bit 0 is sent last). Next, long-integers in QBASIC are stored as groups of four successive bytes in the PC's memory, least-significant-byte first, most-significant-byte last. Once the memory location of \( N \) is known, \( N \) must be read in reverse order, fourth byte to first byte. The "Set byte count to 3" and "Decrement BY" lines keep track of which byte is being processed.

The byte now must be scanned from the top down; that is, the most-significant-bit to the least-significant-bit. This is where the "Set bit counter to 7," "Test bit BT," "Set DATA to 1 or 0," "Toggle Clock Decrement BT," and "TEST BT" blocks are used. The program looks at each bit of \( N \), MSB first, and then decides whether the bit is a one or a zero. It then sets the DATA line and toggles the CLOCK line, sending the DATA bit to the NCO.

After each pass through the inside loop (the bit test loop), the bit counter content (BT) is tested to see if all the bits have been scanned—if not, the loop is complete again. When a bit scan has been completed, the BY counter is adjusted and tested to see if the last byte has been processed. Again, the program loops until all bytes have been processed.

With the powerful instructions available in QBASIC, the whole procedure can be completed with just a few lines of code:

```qbasic
FOR J = 3 TO 0 STEP -1
FOR X = 7 TO 0 STEP -1
IF PEEK(VARPTR(N&)) + J THEN dt = 2 ELSE dt = 0
OUT dp, 0 + dt + 4 : OUT dp, 1 + dt + 4 NEXT J
NEXT X
```

The "IF PEEK..." line is fairly complex. The FOR NEXT J loop accounts for the bytes and the FOR NEXT X loop handles the bit tracking. Starting from the inside and working out, the VARPTR(N&) function returns the address of the variable N&.
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the PEEK function selects one of the four N& bytes.

The AND logical operator creates the logical results of ANDing two quantities, in this case the eight-bit word supplied by the VARPTR and the eight-bit equivalent of $2^X$. Since $2^X$ takes on binary values only (0, 1, 2, 4, 8, 16, 32, 64 and 128), only one bit of binary word equivalent to $2^X$ is high for each value of X. When two bits are ANDed, the result is a one when both bits are ones. If the N& byte being scanned has a one as its MSB, and it is ANDed with $2^7$, the result of the AND function will be a binary word equivalent to decimal 128. If the MSB is zero, the resulting word will be zero. This process is called “masking” and it should be familiar to anyone experienced with C or machine-language programming. As the value of X changes from 7 to 0, each bit of the current byte is tested by the AND function.

The final part of the program line, THEN, sets variable dt to either a 2 or a 0. Refer to Table 1. Data to be fed to the NCO appears as the second bit of the parallel-port data word, and it has a binary weight of 2.

The two OUT instructions send bytes to the parallel port data register (dp). The first OUT instruction sends the results of the bit analysis (0 or 2) plus 4 to the NCO. The “4” (refer to Table 1) controls the NCO’s FLOAD input that should be set high when data is being transferred to the chip. The second OUT instruction is identical to the first OUT instruction except for an additional “1.” That “1” turns on the NCO CLOCK input, producing a positive edge that shifts the value into the NCO.

You might have to read the preceding paragraphs several times so that you understand how the load subroutine works. Once you understood the procedure, you can program the NCO board to do anything its capable of doing. The rest of the program provides visual enhancements to the screen display, and generally forms a clean control panel for the PSG.

(Continued on page 66)
The new energy-saving fluorescent bulbs save money on electric bills, but they can interfere with infrared remote controls.

TOM HEALD

I was watching a movie on a cable channel one night when suddenly my TV set jumped channels. I grabbed my universal infrared remote control and tried to switch back to the channel I was watching but nothing happened. The remote was dead! So I went to my cable box and changed the channel back to the program I was watching. However, a few minutes later the channel switched again. What was going on? Nobody else had been near either my remote control or cable box.

I then pointed my remote control at my TV set, reset the channel, adjusted the volume and tested the mute. All three functions worked. Five minutes later the TV screen bloomed into a field of snow, and the hiss of static overcame the audio. The cable box had turned itself off.

The next day the remote control worked fine with the TV and VCR but not with the cable box. I called my local cable company and asked if it was experiencing technical difficulties. A spokesman for the cable company declared "No, it's those universal remotes. They're always causing problems with our boxes. If you rent one of our remotes, it'll work just fine."

Rather than follow this suggestion, I returned my cable box and swapped it for a new one, thinking that the problem would be solved. The replacement box worked just fine, but a few days later the remote control started acting up again.

Mystified, I called Universal Electronics, makers of my One For All remote control, and explained my problem. The customer service representative said he had not heard about my spontaneous switching problem before, but he suggested that the cause could be in the code for my cable box. I was given a special code to reset my remote control, and then I tried all the codes for my Scientific Atlanta cable box. Everything worked well for a couple of hours before the glitch finally returned.

I thought about probable causes and over the next few days I carried out a concerted attack on the mystery. First, I bought new batteries for my remote control, then I rented a dedicated remote control from the cable company. Finally, in desperation, I exchanged the cable box again and bought a brand new remote control.
Everything worked well during the day, but at night neither my new universal remote control nor cable-box remote would work. I then concluded that the cause might be noise on the cable—or perhaps some energy source interfering with my remote's signal. Although I felt foolish doing it, I turned off all the lights in my house and, with my remote, switched a number of channels. Had the problem been solved?

Then I turned the lights back on, one at a time, and eventually narrowed down the offending source to new energy-saving fluorescent tubes that I had installed months earlier. These bulbs were interfering with my remote control, but the standard fluorescent tubes in my kitchen lighting fixture had no effect on it.

I ruled out power consumption as a cause: the energy-saving fluorescent tubes were rated for 30 watts, but the kitchen fixture contained four 40-watt tubes. It seemed that the fluorescent bulbs were producing an infrared signal that jammed my cable box and, on occasion, simulated the remote control's signal.

I phoned several fluorescent lamp manufacturers to see if they could shed some light on this interference. "Yes, we have had some complaints," said Scott Mack, a spokesman for Philips Lighting. He advised me to make sure the energy-saving bulbs were at least 10 feet away from my TV set and cable box and that they were plugged into different household electrical circuits.

"But that's the cure for radio frequency interference," I protested, "what about infrared interference?" He agreed with me, but said that until Philips came up with a definitive solution this was the suggested response to any complaints. "In fact," he added, "if those suggestions don't work, try moving the energy-saving lamps to a different room."

**Ghost busting**

I connected the lamp with the fluorescent bulb to a different electrical circuit with an extension cord, and I moved it 16 feet away from the cable box—but that didn't help. To prove to myself that it was infrared energy emitted from the bulb and not RFI on the line, I put the lamp in a large cardboard box. With the lamp turned on inside the closed box, there was no interference. But as soon as the box lid was opened, the remote stopped working.

Next, I tried a magnetically ballasted fluorescent desk lamp with an circular eight-inch diameter tube. (The energy saving fluorescents lamps are electronically ballasted.) The remote was unaffected. Even when I held the desk lamp six inches from the cable box, the remote worked. First I assumed that the desk lamp's tube produced a more natural "daylight" spectrum, and perhaps that was why it differed from the fluorescent bulbs.

**HOW DOES YOUR REMOTE CONTROL WORK?**

Modern remote controls apply many different techniques to communicate with TVs, VCRs, and other consumer electronic products. Their coded signals might vary, but all remote control circuits are basically the same. Most transmit pulses of infrared energy at a specific frequency (e.g., 36 kilohertz). Each time a key is pressed, a group of coded pulses is generated.

A typical code contains 24 bits of binary information. The first four bits determine which one of 16 possible products is to be controlled. For example, 0 is for the TV receiver, 1 is for the first VCR, 2 is for the second VCR, and 3 for a compact disk player. The next eight bits in the sequence identify the key that has been pressed. Those eight bits permit a total of 256 possible key codes. The last 12 bits are check bits which are compared with the first 12 bits to detect errors.

When the receiver within the host product detects an infrared signal, it compares it with a clock pulse operating at the same frequency. If the signal is high, a binary one is generated; otherwise, a zero is generated. After the message is decoded the host equipment is commanded to respond.
Visible light occupies only a small part of the electromagnetic spectrum. It is generally considered to span the range of wavelengths from 380 nanometers (violet light) to over 700 nanometers (red light). These limits are also be expressed as 0.38 to 0.70 micrometers.

Infrared remote controls based on readily available infrared-emitting LEDs (IREDs) emit at wavelengths of about 1000 nanometers (1 micrometer) in the near infrared region.

The light emission spectrum from a fluorescent tube depends on the phosphor coating inside the tube. About 90 % of its energy is converted to light with the remaining 10 % dissipated as heat (infrared) radiation. The light spectrum illustrated is for one of the most common "white" fluorescent lamps that emit a more natural light than earlier tubes. The fluorescent spectral distribution curve closely brackets the visible light spectrum.

An incandescent bulb, by contrast, is only about 10 % efficient. Most of the remaining 90 % of the energy is dissipated as heat in the near infrared region. Its spectral distribution extends beyond 2800 nanometers.

It’s not the intensity of infrared radiation that interferes with remote controls. It’s the frequency of the modulating signal applied to the neon tube. Electronically ballasted fluorescent lamps can overwhelm a remote control by producing a stronger signal "tuned" to the infrared receiver circuit's frequency.

This assumption turned out to be faulty: I then guessed that the interference had something to do with the way the electronically ballasted lamp worked.

"Compact fluorescent tubes operate at high-frequencies," explained Arnold Buddenberg, a researcher at the Lighting Research Center of Rensselaer Polytechnic Institute in Troy, NY. He said those high frequencies modulate the tube's infrared output and cause interference for remote controls based on infrared emission.

The heavy magnetic ballast associated with standard fluorescent tubes limits the flow of 60-hertz current through the tube. That ballast produces a flicker that can be annoying in rooms lit by the older fluorescent lights. Their flicker rate is 120 hertz, twice that of line power.

The operating frequency of electronically ballasted fluorescent lights is between 25 and 50 kilohertz. They produce a 50- to 100-kilohertz flicker, which is too fast for human eyes to sense. However, it is this non-visible flicker in the form of a switched infrared signal that interferes with infrared remote controls. The remote controls for switching cable boxes, TV sets, VCRs, and stereo also switch in the 50- to 100-kilohertz range to transmit binary data to receiving circuits built into those products.

"We woke up one morning and our sets didn't work," reports Don Lowry, Matsushita Electronics' director of engineering. "Each case is a little bit different, but our countermeasures have been effective in managing all of them."

The latest infrared receiver circuits in consumer electronic products include automatic gain control (AGC) and a clocking circuit that isolates the remote-control signal from spurious infrared radiation. Some circuits look at the signals center frequency and pulse width and reject all infrared transients that are shorter than valid code signals.

In addition, the latest products have better infrared shielding that limits the view from the infrared receiver to a narrow cone of energy incident at the front of the host equipment.

"We're trying to find an infrared interference prevention scheme that will be acceptable to all manufacturers," reported Tom Mock, speaking for the Electronics Industries Association (EIA) in Washington, DC. Its Consumer Electronics Group includes representatives of lighting and consumer electronics manufacturers.
TABLE 1

<table>
<thead>
<tr>
<th>Lights Tested</th>
<th>Watts: Rating / Replaces</th>
<th>Model Number</th>
<th>Replacement Tube</th>
<th>Price</th>
<th>Type</th>
<th>CABLE</th>
<th>VCR</th>
<th>STEREO</th>
</tr>
</thead>
<tbody>
<tr>
<td>Lights of America eight inch circular tube.</td>
<td>30 / 115</td>
<td>C2030TP-L</td>
<td>FCL30EX-L</td>
<td>14.99</td>
<td>EB</td>
<td>S</td>
<td>I</td>
<td></td>
</tr>
<tr>
<td>Panasonic Twin Light Capsule</td>
<td>27 / 100</td>
<td>EFD27LE</td>
<td>Integrated</td>
<td>19.99</td>
<td>EB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Lights of American eight inch circular tube. (Reduced THD)</td>
<td>22 / 100</td>
<td>2022TP</td>
<td>FC8TEX-L/RS</td>
<td>12.99</td>
<td>EB</td>
<td>S</td>
<td>I</td>
<td></td>
</tr>
<tr>
<td>GE Energy Choice</td>
<td>26 / 90</td>
<td>22857</td>
<td>Integrated</td>
<td>9.99</td>
<td>EB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>OSRAM DULUX EL</td>
<td>20 / 75</td>
<td>DULUX EL</td>
<td>Integrated</td>
<td>16.99</td>
<td>EB</td>
<td>I</td>
<td></td>
<td></td>
</tr>
<tr>
<td>GE Soft White (Reduced THD)</td>
<td>20 / 75</td>
<td>11302</td>
<td>Integrated</td>
<td>9.99</td>
<td>EB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Philips Earth Light</td>
<td>18 / 75</td>
<td>SL*18</td>
<td>Integrated</td>
<td>16.99</td>
<td>EB</td>
<td>S</td>
<td>I</td>
<td></td>
</tr>
<tr>
<td>Abco Table Lamp Conversion Set Electric Saver</td>
<td>16 / 60</td>
<td>7430</td>
<td>13W/27K u6</td>
<td>19.99</td>
<td>MB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Panasonic Light Capsule</td>
<td>15 / 60</td>
<td>BFG15LE</td>
<td>/ A-C</td>
<td>14.99</td>
<td>MB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Light of America Lifelight U-tube</td>
<td>12 / 60</td>
<td>6000-1</td>
<td>FUL12T60W 9308</td>
<td>9.99</td>
<td>MB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>FEIT Electronic U-tube.</td>
<td>9 / 60</td>
<td>BPMPL9</td>
<td>9W/2700K</td>
<td>12.99</td>
<td>MB</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Dana swing arm magnifier desk lamp with a circular tube.</td>
<td>22 / 75</td>
<td>370WHT</td>
<td>FCL-22D</td>
<td>47.99</td>
<td>MB</td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Legend:
- "Watts" shows the actual wattage rating of the fluorescent unit and the manufacturer's approximation of the incandescent bulb it replaces.
- "Price" is the actual price paid at the Orchard Supply Hardware store in Gilroy, CA.
- EB = Electronically Ballast, MB = Magnetic Ballast.
- S = Solid failure, I = Intermittent failures, and a blank indicates no failures.

Personal computer manufacturers have developed a standard for interconnecting computers and peripherals in networks with infrared signals. It would, for example, permit a printer, to be located anywhere in the room. It would also permit a personal digital assistant (PDA) to download data to a personal computer without a cable connection.

The Consumer Electronics Bus (CEBus) is a multimedia standard for home control. It covers signaling over powerlines, radio frequency and infrared transmission, and coaxial and twisted-pair cabling. The infrared emission frequency is about 100 kilohertz in the near infrared region. Mr. Mock said that so far no problems have been encountered with the energy-saving fluorescent tubes "but we still have to make sure the tubes don't emit in that frequency range."

**What's the payback?**

If you consider all of the interfering signals that these energy-saving fluorescent lights transmit, why should you consider buying them? The answer is to save money on electric bills. All fluorescent lighting saves money over equivalent incandescent lighting because it produces light more efficiently.

A fluorescent tube costs 60 to 75% less to operate than an equivalent incandescent bulb, and it has a life that is about ten times longer. Also, with higher efficiency lighting, less heat is dissipated in the room—especially important in air-conditioned rooms.

A typical 100-watt incandescent bulb costs about 90 cents and lasts 750 hours. By contrast, a 22-watt compact fluorescent tube will last 10,000 hours while giving an equivalent amount of light. For starters, you can buy a compact fluorescent tube for less than $12—the cost of 12 replacement incandescent bulbs.

If your average lighting usage is three hours a day, and you pay a typical rate of 8.5 cents per kilowatt-hour, you will save $7.26 per year on each light tube. At the very high New York City utility rate of 20 cents per kilowatt-hour, you'll save $17.08. At that rate, each fluorescent light will save you $154 over its nine-year life.

**Testing the lamps**

To see how pervasive interference is, I tested a number of consumer electronics products in the presence of 12 fluorescent lights made by eight different manufacturers. With the exception of a swing-arm desk lamp/magnifier, all the compact fluorescent lamps had threaded bases that screw into standard incandescent lamp sockets.

Electronic ballasts are light in
weight and start the associated fluorescent lamp instantly, but, as has been pointed out, they can interfere with infrared remote controls. However, if you consider the many different fluorescent-lamp operating frequencies and the differences between the brands of infrared receiver circuits in the host entertainment products, you quickly realize that there is no way to predict which combination will cause interference problems.

Bulky magnetic fluorescent tube ballasts might weigh more than ten ounces, so they can make a table lamp top-heavy. Moreover, these lights flicker for a few moments when turned on, and some might hum. But they don't interfere with your infrared remote control, and they also save on your electric bill.

I made my tests on popular consumer electronics products: a Scientific Atlanta 8500321 cable converter, Mitsubishi CS-2655R and Toshiba CE2058 TV receivers, and an RCA VR680HF VCR. I tested all three products with their original equipment remote controls as well as the universal URC-2085 from Universal Electronics.

I went on to test three Technics products: an SA-R277 stereo receiver, a CL-PC10 CD player, and a SR-TR155 dual-cassette tape deck. One original equipment remote control operates all of those components.

I encountered six instances of infrared interference, as shown in the last five columns of Table 1. As expected, only the electronically ballasted fluorescent tubes caused interference. I believe continuous interference is caused only when the ballast frequency is half that of the infrared remote control's modulation frequency.

My test results suggest that intermittent interference is more likely to be caused by harmonic frequencies in the infrared region. This is supported by my test of the two eight-inch circular fluorescent lamps. The reduced total harmonic distortion version did not interfere with the stereo; however, both lamps interrupted the cable box.

I prefer electronically ballasted lamps because they offer instant starting and lighter weight. However, most of the tubes I tested were heavier and took up more space than the incandescent bulbs they replaced. The one exception is Abco's table lamp conversion set. A table lamp with this tube is not top-heavy because the ballast is located in a small box that plugs into a power line wall outlet. It has a socket for the lamp's line cord.

This arrangement permits a circular, compact fluorescent light to fit easily around the lamp's shade-supporting "harp" which is too small to accommodate most of the other energy-saving fluorescent tubes with screw-type bases.

If you decide to buy an electronically ballasted lamp, look for one that has a label stating that it has reduced total harmonic distortion. It will produce far fewer annoying frequencies. My favorites are a 22-watt tube from Lights of America and a 20-watt tube from General Electric.
OPERATIONAL AMPLIFIERS

Learn how to design with operational amplifiers and put them to work in various analog and audio circuits

RAY MARSTON

THE OPERATIONAL AMPLIFIER (OP-amp) is a high-gain, DC-coupled amplifier with a differential input (two input leads) and a single-ended output (one output lead). It is one of the most versatile circuits ever invented because it closely approximates the ideal amplifier.

The versatility of the op-amp has made it a key functional building block in linear or analog circuitry because it eliminates the need for bulky transformers in many low-frequency and audio circuits. This article will focus on the role of the op-amp in performing audio signal processing.

The op-amp was developed more than 40 years ago to perform mathematical operations such as addition, subtraction, integration, and differentiation in analog computers. Originally a vacuum-tube, DC-amplifier circuit, it evolved into a discrete transistor circuit before being made as a monolithic integrated circuit.

The availability of mass-produced, low-cost, monolithic op-amps has had a significant impact on all linear circuitry. Op-amps are included in both discrete and monolithic circuits for signal conditioning, power regulation, active filtering, function generation, digital-to-analog conversion, and many other applications.

Ideal amplifier

An op-amp has many of the characteristics of an ideal amplifier. It will be instructive to review the characteristics of an ideal amplifier and then compare them with the performance characteristics of existing monolithic IC op-amps. The characteristics of the ideal amplifier are:

Gain. An ideal amplifier would have infinite gain. However, this is not desirable in a practical amplifier because the smallest input signal would cause maximum output. Thus, high but controllable gain is acceptable.

Input impedance. An ideal amplifier would have infinite input impedance or resistance so its input source would not be incorrectly loaded.

Output impedance. An ideal amplifier would have zero output impedance or resistance so that it could be connected to a load with any resistance value without affecting its output voltage.

Bandwidth. An ideal amplifier would have infinite bandwidth so that it could amplify any frequency from zero hertz (DC) to the upper limits of the radio-frequency spectrum.

Common-mode rejection ratio. An ideal amplifier would have an infinite common-mode rejection ratio or CMMR. This means that if the amplifier has two input terminals (one positive and the other negative), there will be no output if both inputs (common mode) receive the same signal simultaneously. The output of an amplifier that exhibits high CMMR is essentially a zero output if the same signal is applied simultaneously to both of its inputs.

Supply voltage. An ideal amplifier would be unaffected by reasonable variations in power supply voltage.

Practical monolithic op-amps

The 741 is a mature, popular, general-purpose monolithic IC operational amplifier. A bipolar device, it was developed more than 25 years ago by Fairchild Semiconductor Corp. (acquired by National Semiconductor Corp.) as the µA741, an improved version of its µA709. It has retained its popularity and become an industry standard. The µA741 had internal frequency compensation and full overload protection on both its inputs and output.

Many different manufacturers make their own brands of the µA741 and some have improved the performance of the original. Nevertheless, all have similar electrical characteristics. Among the alternate-sourced 741s are four versions from Analog Devices, four from...
Far from being a leading-edge device, the 741 is, nevertheless, well suited for experiments and prototyping because of its low price and ready availability.

A "commodity" 741 can be purchased from electronic distributors for less than 50 cents, and that unit price falls significantly in large purchases of hundreds.

Some of the typical electrical characteristics of the 741 are given in the first column of Table 1. Many op-amps now in production have characteristics that surpass those of the 741, but they generally cost more. The performance of the two other op-amps included in the table will be discussed later in this article.

Figure 1 is the schematic for the 741 illustrating its complexity. (This contains 19 transistors, but in other versions diodes have replaced two transistors.) Figure 2 is the pinout diagram for the commodity 741 in an eight-pin plastic DIP case. Figure 3 is the standard schematic symbol for all op-amps, but power supply connections are not always shown.

Many op-amps are powered from split power supplies as shown in Fig. 3. The +V, −V and ground (zero volt) rails permit the op-amp’s output to swing on either side of zero volts and be set at zero volts when the differential input voltage is zero. However, some op-amps can be powered from single-ended supplies.

Figure 4 is the frequency response curve or Bode plot of a 741 op-amp. The 741 offers low-frequency (below 10 Hz) voltage gain that is greater than 100 dB. However, that gain rolls off at 6 dB per octave (20 dB per decade) at frequencies above 10 Hz. It eventually falls to unity gain (0 dB) at its \( f_T \) unity gain transition or cutoff frequency of 1 MHz.

The Bode plot of Fig. 4 can also represent the latest op-amps, but those devices will typically have different values of low-frequency gain and cutoff frequency.

**Closed-loop amplifiers**

The op-amp usually serves as the active device in a feedback circuit. Gain is precisely determined by the negative feedback applied from output to input through the components in the external feedback loop. The values of those components set the gain value. However, the feedback loop effectively cancels the op-amp’s open-loop electrical characteristics.

Figure 5 shows an op-amp configured as a fixed-gain inverting amplifier. The output is fed back to the input, and voltage
FIG. 4—BODE PLOT for the 741 op-amp showing values of gain under open- and closed-loop conditions.

TABLE 1
TYPICAL ELECTRICAL CHARACTERISTICS OF THREE OP-AMPS

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>SYMBOL</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input offset voltage</td>
<td>$V_o$</td>
<td>2</td>
</tr>
<tr>
<td>Input offset current</td>
<td>$I_o$</td>
<td>20 (1)</td>
</tr>
<tr>
<td>Input bias current</td>
<td>$I_b$</td>
<td>80 (1)</td>
</tr>
<tr>
<td>Input resistance</td>
<td>$R_{in}$</td>
<td>$2 \times 10^6$</td>
</tr>
<tr>
<td>Large-signal voltage gain</td>
<td>$A_{OL}$</td>
<td>200</td>
</tr>
<tr>
<td>Output voltage swing</td>
<td>$V_o$</td>
<td>±14</td>
</tr>
<tr>
<td>Common-mode rejection ratio</td>
<td>CMRR</td>
<td>90</td>
</tr>
<tr>
<td>Supply current</td>
<td>$I_s$</td>
<td>1.7</td>
</tr>
<tr>
<td>Slew rate</td>
<td>$SR$</td>
<td>0.5</td>
</tr>
<tr>
<td>Gain-bandwidth product</td>
<td>$GBW$</td>
<td>3.7</td>
</tr>
<tr>
<td>Supply voltage</td>
<td>±18</td>
<td>±15</td>
</tr>
<tr>
<td>Power dissipation</td>
<td>50</td>
<td>8</td>
</tr>
</tbody>
</table>

(1) nanoamperes (2) volts per volt

gain A is determined by the ratio of R1 to R2, and equals $-R1/R2$. This ratio also equals the output voltage divided by the input voltage. This circuit's input impedance equals the value of R1. The circuit can easily be modified to give any desired gain and input impedance values by changing component values.

Current induced at the junction of R2 and R1 is A times greater than that caused by the input signal alone. Therefore, the input acts as if it has an impedance of R2/A connected between the terminal and ground, so it acts like a low-impedance "virtual ground."

Figure 6 shows an op-amp configured as a fixed-gain noninverting AC amplifier. Here the closed-loop voltage gain equals $(R1 + R2)/R2$ or the output voltage divided by the input voltage. The input impedance approaches infinity.

An op-amp can be made to function as a differential input amplifier by combining the inverting and noninverting connections. If that differential amplifier is modified so that two or more input signals can be added algebraically, the op-amp becomes a summing amplifier.

The op-amp can also be configured to act as an integrator, differentiator, and logarithmic amplifier, useful functions for performing analog computer calculations.

Op-amp selection

There are many possible variations in op-amp design and manufacture because of the range of desired options. These include temperature range (commercial, industrial and military), manufacturing process (e.g., bipolar, BiMOS, BiFET, and JFET), and package styles (e.g., plastic and ceramic DIP, and metal cases). Therefore, it is easy to see why the list of op-amps available from so many manufacturers is long and bewildering—even for experienced professional circuit designers.

Where required in the application, the designer can choose from a wide selection of op-amps today. Some are proprietary designs and others are alternate-sourced-versions of standard products. Many op-amps are optimized to obtain
The Harris CA3140 is an example of a high-volume BiMOS op-amp that offers very high input impedance ($1.0 \times 10^{12}$ ohms) that can operate from either single or dual power supplies. The CA3140 combines the advantages of high-voltage PMOS transistors with high-voltage bipolar transistors on a single chip.

The CA3140 has a bipolar output stage, is internally compensated, and has the versatility of 741 op-amps. Column 2 of Table 1 lists some of its typical electrical characteristics.

National Semiconductor's LF411 is a low-cost, high-speed JFET input op-amp that is also made in volume. It offers low input offset voltage and low voltage drift. A large gain-bandwidth product and fast slew rate are maintained with low supply current. High-voltage input JFETs give the LF411 its low input bias and offset current. It is both pin-compatible and interchangeable with the 741. Column 3 of Table 1 lists some of its typical characteristics.

**Linear amplifiers**

There are many ways to configure op-amps as linear amplifier circuits. Although the 741 series op-amps is specified in the schematics discussed in the remainder of this article, all of the op-amps discussed here will work in these circuits.

Figure 7 shows an op-amp organized as an inverting AC amplifier with an overall voltage gain of 10. Noninverting input pin 3 is grounded through resistor R3. It has the same value as R2 to preserve the op-amp's DC balance. Input impedance $Z_{in}$ equals the value of resistor R1.

Figure 8 also shows the 741 configured as a noninverting AC amplifier with an overall voltage gain of 10. However, in this circuit modification, resistors R1 and R2 are isolated from ground by nonpolarized capacitor C2.

At normal operating frequencies, C2 has a low AC impedance, so voltage gain is still set by the ratios of R1 and R2. However, inverting input pin 2 receives all of the DC negative feedback through R1, giving the circuit excellent DC stability.

Again, for optimum biasing, resistor R3 should have the same value as R1. The op-amp's input impedance $Z_{in}$ at noninverting pin 3 is several hundred megohms, but it is shunted by resistor R3, which reduces the circuit's overall input impedance to approximately 100-kilohms value.

Figure 9 shows how the circuit in Fig. 8 has been modified to give the op-amp a 50-megohm input impedance ($Z_{in}$). The location of capacitor C2 has been changed, and the lower end of resistor R3 is connected to the junction of R2 and C2 rather than directly to ground.

The AC feedback signal that appears on the R2-C2 junction is nearly identical to the input signal at pin 3. As a result, nearly identical signal voltages appear on both ends of resistor.
R3. Thus it passes negligible signal current.

Theoretically, the apparent impedance of R3 is raised to thousands of megohms by this "bootstrap"-feedback action, but in practical circuits the input impedance is limited to about 50 megohms by external leakage paths in the op-amp's mounting socket and/or the circuit board.

For optimum biasing of the circuit in Fig. 9, the sum of the values of resistors R2 and R3 should equal R1. However, in practical circuits the value of R3 can differ from this ideal by as much as 30%. Thus, a 100-kilohm resistor will work for R3.

**Voltage followers**

An op-amp can function as a voltage follower if the inverting and noninverting connections are combined for unity voltage gain. Ideally the differential amplifier's output responds only to the difference in voltage between the two inputs and does not respond to a voltage common to the two inputs (common-mode voltage).

Figure 10 illustrates some of the design options for a voltage follower with all of its negative feedback applied from output to inverting input pin 2 through resistor R2.

Ideally, resistor R1 (which determines the circuit's input impedance) and R2 should have equal values. Again, in practical circuits, the value of R2 can be any value up to 100 kilohms without significantly affecting circuit accuracy. If the circuit's op-amp has a low-frequency cutoff value like that of the 741, R2 can usually have a value of zero. However, op-amps with high cutoff frequency values tend to be unstable when operated in the unity-gain mode.

Stability can be assured by installing an R2 of 100 kilohms, or by adding 1-kilohm plug-in resistor R3 in series. The 0.470μF capacitor C2 across R2 reduces the op-amp's AC impedance.

A very high input impedance can be obtained from an AC voltage follower by configuring the circuit as shown in Fig. 11. Resistor R1 is "bootstrapped" from the op-amp output through capacitor C2. Thus, the impedance of R1 is increased to the multimegohm range.

A 741 op-amp circuit will typically have an input impedance (Continued on page 66)
Build An Isolation Transformer

Build an isolation transformer to protect yourself—and your equipment—while you service electronics.

DOYLE WHISENANT

Everyone who regularly services television sets really should have an isolation transformer. One side of the chassis of most line-powered TV receivers and tube-type radios is connected directly to the AC line. Therefore, servicing this electronic equipment can be very dangerous because the chassis can be “hot.” An isolation transformer isolates the chassis of the equipment being serviced from the AC line. This article explains how to build an isolation transformer for a fraction of the price of a commercial product. It will even supply more current than most commercial units.

The heart of this project is the transformer. The author obtained the two transformers required from two discarded microwave ovens. Buying a new transformer for this project will not save you much money over buying a commercial isolation transformer because the transformer required can cost more than $150. For example, B&K Precision sells an isolation transformer for $189.00. Although electronics distributor Mouser Electronics sells one for $63.50, it will supply only 2.17 amperes, or about 250 watts. Even this modest price is almost three times what our complete project will cost!

Operation

Figure 1 is the schematic for the isolation transformer. Fuse-protected AC line power is first applied to power switch S1. When S1 is closed, neon power indicator NE1 lights up, and power is applied to a cooling fan and to standby switch S2. This arrangement allows transformer power to be turned off, while permitting the fan to continue cooling the transformer.

Neon standby indicator NE2 is wired across switch S2 so that it lights when S2 is open. When S2 is closed, power is applied to the primary side of 1:1 isolation transformer T1. The secondary side of T1 supplies isolated AC power to receptacle SO1. Neon indicator NE3 lights when power is applied to the receptacle SO1.

The isolation transformer will supply 1000 watts for short periods of time, and 500 watts or less continuously. However, it will run too hot if 500 watts is exceeded for more than about half an hour.

The transformer for this project was made from the windings of two microwave-oven transformers. Microwave ovens have heavy-duty transformers (see Fig. 2) that consist of three windings: a 120-volt AC input coil, a 2000- to 3000-volt AC output coil, and a 3- to 5-volt AC coil that serves as the filament winding for the oven’s magnetron. The magnetron is the vacuum tube that produces the microwave energy for the oven.

The filament winding is easily identified; it consists of three to five single turns of 12- or 13-gauge enamel-covered wire. This winding is usually wound directly over the 120-volt AC winding which is wound from

FIG. 1—ISOLATION TRANSFORMER SCHEMATIC. Switch S2 allows power to the transformer to be turned off while the fan continues to cool the transformer.
approximately the same size wire as the filament, but it has more turns. The high-voltage winding, which will be discarded for this project, consists of many turns of much smaller gauge wire.

The microwave oven's fan or blower that cools the magnetron is also needed for this project. The transformer will run warm under load, and the oven fan is an economical way to keep it cool. None of the other parts (see the Parts List), while commonly available, will be found in a microwave oven.

**Modifying the transformer**

Locate two surplus or discarded microwave ovens that are identical, or as similar as possible. As stated earlier, the transformers from two ovens are needed to build the isolation transformer. These transformers usually remain in good working condition. As an alternative, two surplus transformers might be easier for you to obtain than two scrap microwave ovens.

The pencil in Fig. 2 points to one of the welds that must be removed from the microwave-oven transformer. With a handheld grinder, very carefully grind away the welds on both sides of the transformer and separate the top core from the base. Figure 3 shows a transformer that has been disassembled. Remove the windings from the core, being careful not to disturb the insulation on the windings. Discard the high-voltage windings.

The 120-volt AC input coils from the two transformers will be used to make the isolation transformer. Place both 120-volt coils back on the core of one of the transformers to form a 1:1 isolation transformer. Do not disturb the insulation on the windings when reinstalling them on the core. Place the windings very close to one another to ensure satisfactory transformer coupling. Some transformers have spacers between the coils and the core (see Fig. 4) that must be replaced in the correct locations.

Once the windings are correctly positioned back on the core, reinstall the base of the transformer. To do this, weld the base back onto the transformer. If you have access to an electric welder and know how to use it, do this yourself. Otherwise, take the transformer to a welding shop and let a skilled welder do the job for you. Regardless of who does the welding, make sure that the transformer core does not get too hot and that sparks from the welder don't burn the insulation on the coils.

Check the completed transformer with an ohmmeter to make sure that there are no short circuits to the core and from coil to coil. Test the transformer by connecting a voltmeter to the leads of one coil designated as the output coil. Connect the leads from the other coil to an AC line cord through a 5-ampere fuse. Insulate all exposed connections.

Power up the transformer just long enough to get a reading on the voltmeter. Record the output reading, disconnect the AC power, and reverse the input and output coil connections. Repeat the procedure and check the output voltage again. Determine which output coil voltage measures closest to 120-volts AC; it will be the output side. The prototype transformer had a lower voltage reading in one direction than in the other.

**Construction**

This project requires a sturdy metal case that measures approximately 14- × 7- × 9-inches to hold both the fan and the transformer, and still have room for all connections.
This project consists of only a few parts, so point-to-point wiring can be used throughout. Figure 5 shows the inside of the prototype unit. Test fit the fan and the transformer before drilling any holes in the case. The fan should be mounted so that its air stream is directed at the transformer. Once the correct positions are determined for the fan and transformer, mark the locations and drill the mounting holes, but don’t mount anything yet.

If you purchase the case specified in the Parts List, you will find that many of the necessary holes are already punched out. Otherwise, prepare the enclosure by drilling a hole and mounting the line cord to the back of the enclosure. Prepare the front of the enclosure by drilling holes to mount the neon indicators, NE1, NE2, and NE3. Then drill holes for switches S1 and S2. The prototype unit has two large holes punched in each end to allow the fan to draw in cool air and exhaust hot air. Place a screen over those holes to prevent debris from being drawn inside the unit. Prepare an opening for the duplex receptacle on the front panel with a nibbling tool.

Once all the metal working on the enclosure is complete, it can be painted. Next label the enclosure; the labels can be protected with a coat of clear spray enamel.

When the enclosure is completely dry, the transformer and fan can be mounted. Start with the transformer, mounting it to the base of the enclosure with rubber washers to reduce vibration. Mount the fan in the direction so that the cooling air flow will be blowing over the transformer. Next install the fuse holder, the line cord, the three neon indicators, switches S1 and S2, and the duplex receptacle S01.

The isolation transformer can produce several amperes of current, so use 14- to 16-gauge wire for all connections to and from the transformer. However, smaller gauge wire can be used for connecting the fan and neon indicators.

Refer to the schematic dia-
agram (Fig. 1) and begin the wiring by connecting the hot side of the line cord (black wire) to one side of the fuse holder. Next solder a wire from the other side of the fuse holder to one terminal of the main power switch, S1.

Connect the other terminal of S1 to the other side of the fan and to one terminal of S2. Connect power indicator NE1 across the fan terminals so it will indicate when power is applied to the fan and to S2.

Standby switch S2 allows power to the transformer to be shut off while still allowing the fan to work. Wire indicator NE2 across S2 so that it illuminates when S2 is open, or when the unit is in the standby mode. Next, connect S2 to the other side of the transformer. Connect the neutral (white) wire from the line cord to one side of the fan and also connect it to one terminal on the input side of the transformer.

Connect both output leads of the transformer to the AC receptacle SO1. Next connect the output-power indicator NE3 across the receptacle. As a last important step, run a ground connection from the line cord (the green wire) to the base of the transformer and to the fan. If the transformer has not been grounded to the chassis, be sure to do so now with a separate wire.

**Testing**

Before closing up the case, plug an appliance such as a coffee maker, a lamp, or another appliance that draws about 500 watts into the isolation transformer outlet and turn on the power. Run the transformer with the load turned on for approximately 30 minutes while checking it every five minutes or so for excess heat.

The prototype was tested with an 800-watt coffee maker, and the transformer ran warm—but not hot—to the touch. Do not use the isolation transformer to power anything with that high a power rating for extended periods of time. Most modern TVs, even those with large screens, consume 350 watts or less.

**SINEWAVE GENERATOR**

*continued from page 52*

**Construction**

A circuit board with a ground plane is required for building this project because of the high frequencies involved. You can make your own board or buy one from the source given in the Parts List. Figure 3 is the parts-placement diagram. The NCO and DAC ICs are expensive and can be damaged if they must be removed, so it is recommended that you install them in low-profile, machined-contact sockets.

Do not mount the input/output connectors on the PCB board. BNC connectors are recommended for the FSK input and sinewave output. Attach a grounding lug to the BNC connectors, and then solder it to ground plane of the board to provide mechanical support for the connectors. Wire the power source directly to the board or wire a suitable power jack to the board.

Cut a four-foot length of five-conductor cable for the PCB cable. Solder one end of the cable leads to a male DB-25 connector, as shown in Fig. 3, and the other end directly to the PCB board. Figure 4 shows the complete board.

After carefully inspecting the board for incorrectly installed components and poorly soldered joints and making any necessary repairs, the generator is functional. Now you can generate any sinewave you need up to 10 megahertz on the fly.

**OP-AMPS**

*continued from page 62*

of about 50 megohms. As stated earlier, this limit is set by the leakage impedance caused by the mounting socket and/or circuit board. A conductive trace "guard ring" on the circuit board surrounding noninverting input pin 3 and tied to output pin 6 will improve input impedance. However, if significantly higher impedance is required, substitute an FET-input op-amp such as the LF411.

**Audio mixer circuit**

It was stated earlier that the voltage gain of the basic inverting amplifier circuit equals $\frac{R_1}{R_2}$. Consequently, signal currents flowing in $R_1$ and $R_2$ are always equal but opposite in phase, regardless of their individual values.

The inverting amplifier circuit shown in Fig. 5 can be modified as shown in Fig. 12 to become a *summing amplifier*. It has four identical resistor-capacitor input networks in parallel, all connected to inverting input pin 2.

The signal current flowing in feedback resistor R6 will equal the sum of the input signal currents flowing in resistors $R_1$ through $R_4$. The circuit's output signal voltage then becomes proportional to the sum of the signal voltages.

If the input and feedback resistors have equal values (100 kilohms in this circuit), the summing amplifier will provide unity voltage gain between each input pin and the output pin. The circuit's output is equal to the sum of the four input signal voltages.

This simple circuit can become a practical audio mixer by feeding each input signal to its input network channel with a 10-kilohm, volume-control potentiometer. If desired, the circuit can provide voltage gain greater than unity by increasing the value of feedback resistor R6. The number of input channels can also be increased by adding additional RC networks for each new channel desired.
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HAVE YOU EVER WANTED TO VARY the power delivered to a 120-volt AC load under software control? In this project a 68705 microcontroller will do just that. Specifically, it can control eight discrete power Triacs, each of which delivers power in 32 smoothly graduated steps ranging from 0 to 97% of full power. The value delivered to one channel is independent of the value delivered to any other channel. Loads can include light displays, universal motors, heaters, and other appliances.

In this circuit, the power level is set by software, not a potentiometer. The software includes a basic set of routines for processing interrupts and setting the power level. The software also includes five test and demonstration routines for putting the circuit through its paces. Moreover, there's plenty of room to add your own routines to the 68705's built-in EPROM. An easy-to-build single-sided circuit board makes assembly easy.

The basic circuit is simple, yet versatile enough to accept inputs from on-board DIP switches; alternatively, the inputs can be driven from a microcomputer bus or parallel port, or a stand-alone device with TTL-compatible outputs. There are 12 input bits to set modes and specify values.

Circuit design

The circuit, shown in Fig. 1, consists of a power supply, AC line synchronizer, Triac output control, input circuitry, and support devices.

The power supply is a conventional 5-volt circuit built around a 7805 regulator (IC3) and several other components (transformer T1, bridge BR1, and C1-C4). The AC line synchronizer consists of an optocoupler (IC2), a current-limiting resistor (R1), and a bias resistor (R2). The power controller generates variable power levels with phase-control techniques. When using a Triac to control a load, the power delivered can be varied by triggering the Triac after the start of an AC half-cycle.

For example, by triggering the Triac shortly after the start of a half-cycle, the load will receive almost full power. Triggering in the middle of a half-cycle will supply the load with half power and triggering close to the end of a half-cycle will result in the load receiving little power.

In this project the controller is synchronized to AC power-line zero crossings, which occur at a rate of 120 times per second. The microprocessor's internal timer then divides the interval between crossings into 32 steps, thus delivering gradually increasing amounts of power to the load.

The output of the optocoupler is a negative-going pulse that drives the microcontroller's interrupt input directly at a rate of 120 hertz. Each time IC1 receives an interrupt, it recalculates the time to generate Triac trigger pulses on Port B of IC1.

Each bit of Port B is connected to a Triac control circuit; since they're all identical, only Port 7 will be described in detail. Port B7 of IC1 drives transistor Q1 via resistor R4. (Q1 is required because the 68705 can't sink enough current to trigger Triac-driver IC4 directly.)

When it's time to turn on Triac TR1, the microcontroller delivers a 10-microsecond negative-going pulse to port PB7. This pulse briefly enables the transistor, which causes current flow through the LED inside IC4. Although a Motorola MCP3011 Triac driver was used in this design, any similar device could be used, as long as it doesn't have an internal zero-crossing detector. That type of driver allows only two modes of operation: full on and full off.

The Triac driver's LED then triggers the photocoupled Triac within the IC, which in turn
triggers TR1 and delivers power to the external load. Resistor R5 provides current limiting for IC4, and R6 and C7 form a snubber network to filter line transients that could cause the Triac to trigger falsely.

The hot side of the power line connects to the MT1 terminal of all the power Triacs (TR1–TR8). The specified Triacs are rated for 4 amperes at 200 volts. They are isolated-tab versions, and were selected because heatsinking is mandatory. With the specified Triacs, the maximum load is 100 watts per output. Larger loads can be handled by substituting Triacs with higher current ratings. Be sure to use proper heatsink and isolation techniques.

**Input circuit**

The input circuit consists of Ports A and C of the microcontroller, along with two banks of DIP switches (S1 and S2), SIP resistors (RN1 and RN2), four sets of 0.1 inch header jumpers (P1–P4) for mode selection, a 14-pin header (P5) connected to Port A, and a four-pin header (P6) for input selection.

The P1–P4 jumpers allow both the common resistor legs and the common switch poles to be tied to either ground or +5 volts DC, or to be disconnected from the circuit entirely. If programmed as inputs, the ports should not be left floating because this might cause erratic operation. Connector P6 allows an external device (e.g., a computer) to drive the controller’s inputs.

The 68705P3 requires a few support components. Crystal XTAL1 runs at a frequency of 3.58 megahertz, which should not be altered. Capacitor C5 loads the oscillator to keep it at the correct frequency, and capacitor C6 keeps the reset pin low for an instant, thereby giving the 68705 time to stabilize after power up. Momentary switch S3 provides for resetting the circuit. Although unused in the prototype, an external connection is provided to the microcontroller’s reset input, which could allow an external device to reset the circuit when desired.

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**FIG. 1—COMPLETE SCHEMATIC OF THE 68705-BASED POWER CONTROLLER.** The controller reads switch values from Ports A and C, and delivers software-controlled 120-volt AC power to Port B.
All resistors are ¼-watt, 5%, unless otherwise noted.
R1—12,000 ohms, 1 watt
R2—10,000 ohms
R3, R7, R11, R15, R19, R23, R27,
R31—220 ohms
R4, R6, R8, R10, R12, R14, R16,
R18, R20, R22, R24, R26, R28,
R30, R32, R34—1000 ohms
R5, R9, R13, R17, R21,
R25, R29, R33—180 ohms
RN1—4700 ohms x 9 resistor network, common terminal
RN2—4700 ohms x 5 resistor network, common terminal

Capacitors
C1—1000 µF, 16V, radial electrolytic
C2—68 mF, 16V, tantalum
C3—10 µF, 16V, radial electrolytic
C4, C15—0.1 µF, monolithic
C5—27 pF, ceramic
C6—1 µF, 16V, radial electrolytic
C7–C14—0.22 µF, 400V, poly film

Semiconductors
IC1—MC68705P3 microcontroller
IC2—H11AA1 AC optocoupler
IC3—MC7805CT 5-volt regulator
IC4—IC11—MCP3011 Triac driver
Q1—Q8—2N3906 NPN transistor
TR1—TR8—Q2004L3 Triac, 200V, 4A, isolated tab
BR1—Bridge rectifier, 50V, 1A, DIP

Other components
J1—3-terminal AC power connector
J2—9-terminal AC power connector
P1—P4—3-pin single-row 0.1 inch male header
P5—14-pin single-row 0.1 inch male header
P6—4-pin single-row 0.1 inch male header
S1—8-position DIP switch
S2—4-position DIP switch
S3—SPST momentary pushbutton switch
T1—Transformer, 120V primary, dual 6.3V secondaries (Digi-key T101-ND or equiv.)
XTAL1—3.579545 MHz crystal, HC-18

Miscellaneous
Shorting jumpers for P1—P4, heatsink for TR1—TR8, PC board, solder, wire, etc.

Note: The following items are available from Richard L. Roane, Route 601, Cologne, VA 23037:
- Source code listing and programmed MC68705P3—$24.95 paid
- VA residents must add appropriate sales tax.

FIG. 2—MOUNT ALL COMPONENTS AS SHOWN HERE. Note that four jumpers mount on the component side of the board.

POWER CONTROLLER FOIL PATTERN.

Software design
The complete listing of the software is available from the author, as detailed in the Parts List. It is also available on the Gernsback BBS (516-293-2283, v.32, v.42bis); look for file POWCON.ASM. An overview of the major routines follows:

The interrupt routine sets up
TABLE 1—POWER LEVELS

<table>
<thead>
<tr>
<th>Power Level</th>
<th>Voltage (VAC)</th>
<th>Percent On (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.2</td>
<td>1.0</td>
</tr>
<tr>
<td>1</td>
<td>1.9</td>
<td>1.6</td>
</tr>
<tr>
<td>2</td>
<td>2.6</td>
<td>2.2</td>
</tr>
<tr>
<td>3</td>
<td>6.6</td>
<td>5.5</td>
</tr>
<tr>
<td>4</td>
<td>9.2</td>
<td>7.7</td>
</tr>
<tr>
<td>5</td>
<td>12.2</td>
<td>10.2</td>
</tr>
<tr>
<td>6</td>
<td>15.6</td>
<td>13.0</td>
</tr>
<tr>
<td>7</td>
<td>19.5</td>
<td>16.3</td>
</tr>
<tr>
<td>8</td>
<td>23.6</td>
<td>19.7</td>
</tr>
<tr>
<td>9</td>
<td>27.9</td>
<td>23.3</td>
</tr>
<tr>
<td>10</td>
<td>32.8</td>
<td>27.3</td>
</tr>
<tr>
<td>11</td>
<td>37.7</td>
<td>31.4</td>
</tr>
<tr>
<td>12</td>
<td>42.9</td>
<td>35.8</td>
</tr>
<tr>
<td>13</td>
<td>48.2</td>
<td>40.2</td>
</tr>
<tr>
<td>14</td>
<td>53.6</td>
<td>44.7</td>
</tr>
<tr>
<td>15</td>
<td>59.0</td>
<td>49.2</td>
</tr>
<tr>
<td>16</td>
<td>64.4</td>
<td>53.7</td>
</tr>
<tr>
<td>17</td>
<td>70.8</td>
<td>59.0</td>
</tr>
<tr>
<td>18</td>
<td>75.2</td>
<td>62.7</td>
</tr>
<tr>
<td>19</td>
<td>80.2</td>
<td>66.8</td>
</tr>
<tr>
<td>20</td>
<td>85.2</td>
<td>71.0</td>
</tr>
<tr>
<td>21</td>
<td>90.0</td>
<td>75.0</td>
</tr>
<tr>
<td>22</td>
<td>94.5</td>
<td>78.8</td>
</tr>
<tr>
<td>23</td>
<td>97.8</td>
<td>81.5</td>
</tr>
<tr>
<td>24</td>
<td>101.6</td>
<td>84.7</td>
</tr>
<tr>
<td>25</td>
<td>105.3</td>
<td>87.8</td>
</tr>
<tr>
<td>26</td>
<td>107.3</td>
<td>89.4</td>
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<tr>
<td>27</td>
<td>110.2</td>
<td>91.8</td>
</tr>
<tr>
<td>28</td>
<td>112.7</td>
<td>93.9</td>
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<td>29</td>
<td>114.8</td>
<td>95.7</td>
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<tr>
<td>30</td>
<td>116.4</td>
<td>97.1</td>
</tr>
<tr>
<td>31</td>
<td>0.0</td>
<td>0.0</td>
</tr>
</tbody>
</table>

TABLE 2—APPLICATION AND JUMPER SELECTION

<table>
<thead>
<tr>
<th>Value</th>
<th>Application</th>
<th>JU1</th>
<th>JU2</th>
<th>JU3</th>
<th>JU4</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>Manual</td>
<td>GND</td>
<td>+5</td>
<td>+5</td>
<td>GND</td>
</tr>
<tr>
<td>1</td>
<td>External</td>
<td>-</td>
<td>-</td>
<td>+5</td>
<td>GND</td>
</tr>
<tr>
<td>2</td>
<td>Sequencer</td>
<td>-</td>
<td>-</td>
<td>+</td>
<td>GND</td>
</tr>
<tr>
<td>3</td>
<td>Run and Flash</td>
<td>-</td>
<td>-</td>
<td>+</td>
<td>GND</td>
</tr>
<tr>
<td>4</td>
<td>Test</td>
<td>-</td>
<td>-</td>
<td>+5</td>
<td>GND</td>
</tr>
<tr>
<td>5-15</td>
<td>Not used</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

TABLE 3—MANUAL MODE POWER LEVELS

<table>
<thead>
<tr>
<th>Port C Data</th>
<th>Power Level</th>
</tr>
</thead>
<tbody>
<tr>
<td>Decimal</td>
<td>Decimal</td>
</tr>
<tr>
<td>0</td>
<td>31</td>
</tr>
<tr>
<td>1</td>
<td>0</td>
</tr>
<tr>
<td>2</td>
<td>2</td>
</tr>
<tr>
<td>3</td>
<td>4</td>
</tr>
<tr>
<td>4</td>
<td>6</td>
</tr>
<tr>
<td>5</td>
<td>8</td>
</tr>
<tr>
<td>6</td>
<td>10</td>
</tr>
<tr>
<td>7</td>
<td>12</td>
</tr>
<tr>
<td>8</td>
<td>14</td>
</tr>
<tr>
<td>9</td>
<td>16</td>
</tr>
<tr>
<td>10</td>
<td>18</td>
</tr>
<tr>
<td>11</td>
<td>20</td>
</tr>
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<td>12</td>
<td>22</td>
</tr>
<tr>
<td>13</td>
<td>24</td>
</tr>
<tr>
<td>14</td>
<td>26</td>
</tr>
<tr>
<td>15</td>
<td>30</td>
</tr>
</tbody>
</table>

Suppose that an application calls for a power level of 16 at Output 3, and a level of 30 at Output 7. In that case simply store values of 16 and 30 in control bytes PWRC3 and PWRC7, respectively. The outputs will immediately and simultaneously reflect these levels. Note that although the desired voltages were specified in decimal form, you must store the corresponding hexadecimal value in the output-control byte.

ASSEMBLER VARIATIONS

In developing the software for this article, the intention was to provide a single source file that would assemble correctly under three assemblers: the TEC 6805 Assembler, Motorola's 6805 Assembler, and Motorola's Freeware Assembler. In the course of testing, a bug was discovered in the Freeware assembler. After encountering an instruction that uses direct addressing on page zero of memory, the assembler starts generating garbage. Both of the other assemblers force extended addressing, thus avoiding the problem. The only point in the code where this is a problem is in the jump table, where there is the instruction:

JMAN: JMP MAN

By changing that instruction as follows, the problem can be avoided:

JMAN: BRA MAN

Branching, rather than jumping, works because the target routine is within 128 bytes of the jump table.

Construction

Assembly is straightforward. Figure 2 shows the parts layout on the single-sided circuit board. Load the board by inserting lowest- to highest-profile (Continued on page 76)
Recoton develops wireless technology which transmits stereo sound through walls, ceilings and floors up to 150 feet.

Fif you had to name just one new product "the most innovative of the year," what would you choose? Well, at the recent International Consumer Electronics Show, critics gave Recoton's new wireless stereo speaker system the Design and Engineering Award for being the "most innovative and outstanding new product."

Recoton was able to introduce this whole new generation of powerful wireless speakers due to the advent of 900 MHz technology. This newly approved breakthrough enables Recoton's wireless speakers to rival the sound of expensive wired speakers.

Recently approved technology. In June of 1989, the Federal Communications Commission allocated a band of radio frequencies stretching from 902 to 928 MHz for wireless, in-home product applications. Recoton, one of the world's leading wireless speaker manufacturers, took advantage of the FCC ruling by creating and introducing a new speaker system that utilizes the recently approved frequency band to transmit clearer, stronger stereo signals throughout your home.

Crisp sound throughout your home. Just imagine being able to listen to your stereo, TV, VCR or CD player while you move freely between rooms, exercise or do other activities. Unlike infrared headphones, you don't have to be in a line-of-site with the transmitter, giving you a full 150 foot range.

The headphones and speakers have their own built-in receiver, so no wires are needed between you and your stereo. One transmitter operates an unlimited number of speakers and headphones.

150 foot range through walls! Recoton gives you the freedom to listen to music wherever you want. Your music is no longer limited to the room your stereo is in. With the wireless headphones you can listen to your TV, stereo or CD player while you move freely between rooms, exercise or do other activities. Unlike infrared headphones, you don't have to be in a line-of-site with the transmitter, giving you a full 150 foot range.

The headphones and speakers have their own built-in receiver, so no wires are needed between you and your stereo. One transmitter operates an unlimited number of speakers and headphones.

Full dynamic range. The speaker, mounted in a bookshelf-sized acoustically constructed cabinet, provides a two-way bass reflex design for individual bass boost control. Full dynamic range is achieved by the use of a 2" tweeter and 4" woofer. Plus, automatic digital lock-in tuning guarantees optimum reception and eliminates drift. The new technology provides static-free, interference-free sound in virtually any environment. These speakers are also self-amplified; they can't be blown out no matter what your stereo's wattage.

Stereo or hi-fi, you decide. These speakers have the option of either stereo or hi-fi sound. You can use two speakers, one set on right channel and the other on left, for full stereo separation. Or, if you just want an extra speaker in another room, set it on mono and listen to both channels on one speaker. Mono combines both left and right channels for hi-fi sound. This option lets you put a pair of speakers in the den and get full stereo separation or put one speaker in the kitchen and get complete hi-fi sound.

Factory direct savings. Our commitment to quality and factory direct pricing allows us to sell more wireless speakers than anyone! For this reason, you can get these speakers far below retail with our 30 day "Dare to Compare" money-back guarantee and full one year manufacturer's warranty. For a limited time, the Recoton transmitter is only $69. It will operate an unlimited number of wireless speakers priced at $89 and wireless headphones at $59 each. Your order will be processed in 72 hours and shipped UPS.

Recoton Transmitter (you must have a transmitter to operate speakers and headphones)......$69 $7 & H Wireless products compatible with the Recoton transmitter: Recoton Wireless Speaker.............$89 $9 & H Recoton Wireless Headphones.......$66 $6 & H Please mention promotional code 165-ET104.

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components. Make sure that you observe polarities of all semiconductors, SIP resistors, and electrolytic capacitors.

For the prototype, four Triacs were mounted each to two 90° aluminum heatsinks. The AC power input was brought to one heavy-duty, three-terminal connector, and the eight Triac outputs plus AC common were brought to a separate nine-terminal connector.

The circuit board has 120-volt AC signals on it, so check and double-check your work before plugging in and testing the project. Figure 3 is a photo of the author's prototype.

**Built-in applications**

On power up, a selection routine reads Port C and selects the corresponding application. Note that following power-up, Port C can be used for other purposes. Table 2 lists Port C values, along with the corresponding routines and PC-board jumper settings. In general, if no host is connected and Port A will input data from S1, set the jumpers as shown for application 0 (manual). Also note that in the design, once a routine has been selected, the only way to change to a new routine is to reset the system. Following is a description of each application:

**Manual**—The software scans Port A waiting for a bit to go low. When that occurs, the microcontroller loads power-level data from Port C and stores it in the power-control byte specified by the value in Port A. For example, placing 05 on Port C and bringing PA2 low will set output 2 to power level 8. Because Port C has only four input bits, it can only specify 16 power values ($2^4 = 16$). Thus a look-up table (shown in Table 3) spreads the 16 specifiable values across the entire 32-value range.

**Sequencer**—This routine demonstrates the controller's ability to power light displays. It turns on the first output, waits, etc.

(Continued on page 90)
I recently reviewed several books that I believe are worth reading. Who Owns Information? by Anne Branscomb (Basic Books, 1994) seems to cover everything from the Internet to the Dead Sea Scrolls. It focuses on the new intellectual properties that are challenging traditional copyright laws.

While the book is thorough, it essentially expresses the viewpoint of a conservative lawyer. This book would be far better balanced if it had more input from publications such as the Free Software Foundation or Wired Magazine.

For a totally different take on a related topic, read Winn Schwartau's Information Warfare: Chaos on the Electronic Superhighway (Thunder's Mouth Press, 1994).

I've long been a fan of Richard Feynman, the physicist and gadfly. He was one of my great heroes. No Ordinary Genius: The Illustrated Richard Feynman has been newly released by Richard Phillips (W.W. Norton, 1994). It's a "life and times" summary that adds to such titles as James Gleick's Life and Science of Richard Feynman (Pantheon, 1992). In addition, read Feynman's own Surely You're Joking Mr. Feynman (W.W. Norton, 1985) and What Do You Care What Other People Think? (1988).

My other heroes? Well, since you asked: Perry Ferrell, Buckminster "Bucky" Fuller, Ed Abbey, P.T. Barnum, and William M. Gaines. I think Gaines was the greatest philosopher of the twentieth century.

Science Versus Pseudoscience? is an important and easy to read Nathan Aaseng book (F. Watts Press, 1994). It clarifies several topics I have kicked around here quite a bit. My own definition of pseudoscience is pretty much one of "looks like a duck, quacks like a duck."

When you've been at the research game for a long while, the pseudoscience stuff becomes painfully and laughingly obvious: correspondence like those dreary chain letters that spend five pages telling you they are not chain letters.

Aaseng is much more specific because he lists ten crucial tests to tell the differences between pseudoscience and real science. I've reproduced the list here as Fig. 1. The only thing I'd personally add to his list is: "Science requires that extraordinary claims demand extraordinary proof."


Magnetic Measurements Handbook is a 95-page self-published book by J. M. Janicke and offered by Magnetic Research. Included in the book is hard-to-find information on magnetic fundamentals along with a lot of construction projects for fluxmeters, Helmholtz coils, and other similar stuff.

In addition to publishing, Magnetic Research also sells fluxgates and Hall-effect probes. However, the Hall-effect probes are totally unsuitable for most compass bearing and navigation applications. The same goes for its abysmal batch of magnetoresistors. Today, a fluxgate compass is the only way to go. A competing, low-cost source for fluxgate coils, useful for homebrew compass projects, is OrthoLogic. There is more on the subject of electronic compasses in my Hardware Hacker reprints.

**Vector-to-step conversions**

Suppose you want to mill a diagonal cut on a CAD/CAM machine that can step only north-south or east-west. How would you do it? Or suppose you want to show a slanted line on a raster scan display or perhaps on a laser printer's bitmap? Maybe you want to map a tumbling
three-dimensional object with animation software?

All of these tasks require vector-to-step conversions. These are some of the most basic and important requirements in computer graphics. A short review of the fundamentals is given in Fig. 2.

A vector is a number that expresses two or more values such as speed and direction. For example, the representation of walking east-northeast (ENE) for 10.2 miles is a vector quantity. Vectors can be resolved into their basic components. For instance, by walking 10.2 miles ENE you will arrive at the same place as walking 9.4 miles due east and then walking 3.9 miles due north.

Trigonometry can resolve vectors. As an example, ENE is at an angle of 22.5° counterclockwise from east. By multiplying 10.2 times the cosine of 22.5° you will obtain the 9.4-mile east component. Also, 10.2 times the sine of 22.5° gives the 3.9-mile north component.

Obviously, walking the 10.2 mile direct route is shorter and probably a lot easier. A CAD/CAM machine that cuts only east and then travels

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---

The goal of vector-to-step conversion is to change a diagonal tool path or a slantly line on a screen or printer bitmap into discrete unit steps that travel only in north-south or east-west directions...

First, you correct your input vector so it starts at your actual initial position. This prevents closure errors from piling up. If not already done, you then resolve your input vector into its x and y components. For a vector of length Z and an angle of θ...

\[ x = Z \cos(\theta) \quad \text{and} \quad y = Z \sin(\theta) \]

Next, calculate the slope y/x and save it for later use. Then round x and y off to the nearest integer values to get the actual steps needed. Compare the signs of x and y, and the absolute sizes of x and y to find an octant...

<table>
<thead>
<tr>
<th>Octant</th>
<th>0</th>
<th>45</th>
<th>90</th>
<th>135</th>
<th>180</th>
</tr>
</thead>
<tbody>
<tr>
<td>x+y</td>
<td>+</td>
<td>+</td>
<td>+</td>
<td>+</td>
<td>+</td>
</tr>
<tr>
<td>x-y</td>
<td>-</td>
<td>-</td>
<td>+</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>x+y</td>
<td>+</td>
<td>+</td>
<td>+</td>
<td>+</td>
<td>+</td>
</tr>
<tr>
<td>x-y</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
<td>-</td>
</tr>
</tbody>
</table>

If you are in octant #0, you always step by +x and sometimes step by +y. To determine whether a +y step is needed, multiply the total number of x steps so far by the slope. If the current y total is more than 0.5 steps under this value, also add a new y step.

Here are the rules for the other octants...

In octant #0, always step by +x and sometimes step by +y.
In octant #1, always step by +y and sometimes step by +x.
In octant #2, always step by +y and sometimes step by -x.
In octant #3, always step by -x and sometimes step by +y.
In octant #4, always step by -x and sometimes step by -y.
In octant #5, always step by -y and sometimes step by -x.
In octant #6, always step by -y and sometimes step by +x.
In octant #7, always step by +x and sometimes step by -y.

For the maximum possible speed, replace on-the-fly calculations by table lookups, compiling, special hardware, or similar techniques.

---

The maximum possible speed, replace on-the-fly calculations by table lookups, compiling, special hardware, or similar techniques.

A position in space is said to be absolute if it is measured from some 0.0 axis reference point. A position is relative if it is measured from the last determined or referred position in space.
A 10.2-mile straight-line hike is considered absolute if you start from home and end up 10.2 miles from home. Now, suppose that today’s hike, part of a week-long trek, lands you 10.2 miles from this morning’s start. That’s considered to be a relative position. Typically, absolute positioning is used for the first point in any path, while relative position is used for all points that follow.

The first step in a vector-to-step conversion is to correct the vector. Typically you want to go from “where you thought you were” to “where you want to be.” But you probably are not where you thought you were. Why? Because roundoff errors will change your actual position from your desired position. If you do nothing about these errors, they will accumulate on you. That’s one reason why you should take topographical maps with you on a hike.

Instead, you’ll correct the input vector so that it routes from “where you know you now are” to “where you want to be.” This calls for a measurement or else a transform from existing device space back into user space. The net result is that the input vector will change slightly in size and direction, thus “swallowing” previous position errors, and correcting on-the-fly.

There are eight possible vector-to-step cases; each can end up “alike but different somehow.” Let’s call east-west the x and north-south the y components. Now, x could be positive or negative, and y could be positive or negative. Moreover, the length of x can be greater or less than that of y.

The next step is to decide which of the eight cases you have. Then, pick the correct case and use it for the actual conversion. If your computer or microcontroller and the available processing time allows you the luxury of real trigonometry, you could find the arctan, or “angle whose tangent is,” and then divide by 45 to get a 0 to 7 case.

When speed is essential (or if your microcontroller isn’t very powerful), test the signs of x and y plus the absolute lengths of x compared to y to pick one of the eight cases. The selected case is then the one that is run.

Assume the math coordinate orientation, rather than the geographical one, with east at 0 degrees, north at 90, west at 180, and southeast at 315°. Then call any of the eight cases an octant. A vector of 10.2 miles ENE is in octant zero.

Now, in octant zero, x absolutely must be positive and absolutely must be larger than y. Moreover, y also must be positive. Otherwise, you would be in some other octant. So, in octant zero, simply apply the rule “always step by x and maybe step by y.”

Assume that the corrected vector has been resolved into x = 9.4 and y = 3.9 components. Since you are allowed only whole integer steps, you cannot take 9.4 unit steps. In this case, we will round down to nine steps. Thus, you want nine x steps and you want four y steps. The question is when to add the y steps to get closest to the original vector.

If rounding down gives an x value of zero, exit. The little missed piece will be picked up on the next vector. Exiting on a zero length also gets rid of the possible divide-by-zero in the next step.

Next, calculate the slope by dividing the little y number by the bigger x one, or in this case y/x. Save this value.

Then step along your x axis, always taking one x step. After each x step, compare the actual y against the desired y position. The desired y position is obtained by multiplying x times the slope. Whenever you end

FIG. 3—SOME CAD/CAM SYSTEMS can apply x and y stepper phase by interleaving techniques to improve their apparent resolution dramatically.
up more than half a step (or 0.5) low, add a y step. Continue this for each needed x step. That's all there is to this.

To review: For any vector-to-step conversion, first correct the vector so it travels from where you really are to where you want to be. Then pick one of eight octants, based on the size and sign of the x and y components. Then pick an octant-specific code that always steps along x but only sometimes steps along y, or vice versa.

**Getting fancy**

There are several refinements that can be added here. Testing for a 0.5 unit error becomes less accurate the steeper the vector gets. But 0.5 is more than satisfactory for most applications. For the best fit, use 0.5 times the cosine of the slant angle.

If you can't "afford" a real cosine, \( 1 - \frac{\text{angle in radians}^2}{2} \) could substitute for it pretty well. Cruder useful substitutions are \( 0.5 - \left(\frac{\text{angle in degrees}}{300}\right) \). Or you could even let 0.44 split the difference.

Some CAD/CAM applications will let you move your x and y steps simultaneously. This is called **stepper phase interleaving**. It means that you can travel east or northeast in octant zero. What you have done is combined an east step with a north step into a single northeast one, eliminating a sharp corner in the process. That dramatically improves the resolution, speed, and smoothness of the actual cuts. Figure 3 shows the improved results.

**A PostScript example**

There are all kinds of variations on these vector-to-step schemes. It all depends on how fast you want to be and whether your microprocessor is capable of performing trigonometry rapidly.

In some cases (such as computer animation), the rendering speed is everything, and you must use every machine language trick possible to make things happen quickly. Elsewhere (such as computeraided design), a more leisurely pace is acceptable, and a powerful and friendly higher-level language works just fine.

I have found the general purpose **PostScript** computing language to be ideal for medium-speed conversions, especially for real-time CAD/CAM. Figure 4 shows PostScript code that can do these conversions for you. This is a very simple tutorial example that can be (and has been) significantly improved.

With table-lookup code, speeds in the 13,000-steps-per-second range are easily reached. Results can be recorded and then sent out later at arbitrarily high speeds.

The key point here is that you can now easily apply PostScript to ultra-low-cost homebrew hacker applications; it is much better than any other way I know of. It is particularly good for such tricks as microsizing and compensating for tool paths and diameters.

**How can you use PostScript's graceful curves and fancy lettering?** Curves are simply broken down into a lot of individual straight-line vectors which are short enough to meet your accuracy goals. PostScript's **charpath** and **flattenpath** operators are used for curve-to-vector conversions.

More examples of vector-to-step conversions are given in my POSTVECT PS, FLUTWUMP PS and FLUTOOLS PS on Genie PSRT. I've also got some exciting new products in the works that are based on these concepts. Give me a call if you need advanced details or help with your own project.

**The halogen cycle**

I've received several helpline calls about early fusion lamp failures on
Despite the fancy name, a quartz halogen lamp is still fundamentally an incandescent bulb with a more or less ordinary tungsten filament. The only difference between them is that the halogen lamp is run much hotter for higher efficiency. The quartz bulb is more resistant to heat shock than ordinary glass. Some wondrously magic chemistry known as the halogen cycle presumably makes the filament last longer.

Tungsten readily forms compounds with halogen gases such as chlorine and fluorine: examples are tungsten hexachloride or tungsten hexafluoride. These gases are stable at lower temperatures, but dissociate at very high temperatures.

Now, one big shortcoming of high-temperature filament life is that the tungsten literally boils off. This both weakens the filament and blackens the glass, leading to early lamp failure.

Here is how the halogen cycle works: Near the hot filament, ejected tungsten mixes with the dissociated halogen. Away from the hot filament, the two substances merge to form a stable halide gas. When the lamp is turned off, much of the dissociated tungsten redeposits back on the filament. Normally, there is little opportunity for bulb darkening.

However, there are two important rules for quartz halide lamps: Never touch them! and Always cool them completely! Fingerprint can cause a high-temperature spot on the glass, leading to mechanical stress and a possible darkening. Moreover, a cooling-off period is mandatory for the halogen cycle to complete itself.

Consequently, there might be a quality control problem. Or maybe somebody who doesn’t know better is handling the lamps during assembly or service. But I have the following hunch: That “green” lower energy operation of new laser printers is dead wrong for the halogen cycle. The worst thing you can do to a quartz halogen lamp is to cycle it repeatedly.

Here are some possible solutions: Run the lamp continuously for an hour every now and then, outside of the printer (perhaps even at 120% of rated voltage). See if that

Canon EX laser engines, such as the 4M+ or Pro630. The symptom of the failure is a darkening of the bulb before it burns out. Well, I have some theories here...

A quartz halogen lamp located inside the bottom roller intermittently turns on and off. It heats the roller to a regulated 375°F temperature.
lightens it up any. Do this in a room where a kilowatt of heat can be safely dissipated. And, of course, keep fingerprints away!

Other solutions are to design a new lamp technology specifically for the new "green" energy cycles, or go to some type of PTC self-regulation.

**Programmable interconnects**

The next logical progression beyond programmable integrated circuits is fully programmable systems in which all of the conductors between ICs can be conveniently and quickly rearranged. Obvious uses that come to mind are for breadboarding, development, and field upgrades.

An ideal interconnect would be dense and cheap, allowing arbitrary connection of any function anywhere. Connections would permit analog or digital signals to move out in either direction without delays.

Both the "on" resistance and any crosstalk would be very low, and these devices should consume little or no power. They would have to "remember" all their connections between powerdowns and be fully reprogrammable at any time.

As you might imagine, the semiconductor houses are scrambling to offer new programmable interconnect devices. I have listed the key players in this month's resource sidebar.

Unfortunately, nearly all devices offered today miss on one or more objectives. Aptix seems to be at the top of the heap. Its devices are quite dense, extremely flexible, bi-directional analog/digital, and have low "on" resistance and crosstalk. But they are expensive and have to be reprogrammed each time power is applied to the system.

Pioneer and Quality offer very low cost and easy to use bi-directional bus switches, but their density is very low. Programming is external. Atesla has arrays of direct interconnects with blowable fuses. They are medium low-cost items that offer bi-directional analog/digital operation. But once blown, the results are permanent and programming cannot be changed.

Apparently, those programmable logic device manufacturers are re-labeling their existing PLA and PLD variations so that they can claim they are interconnects. While dense, reprogrammable, and low priced, the functions are often digital only and one-way only. There are also propagation delays to consider.

One brand new source is Lattice Semiconductor with its Generic Digital Switch, shown in Fig. 5. Densities up to 11 x 11 are offered. Any lead can be "taught" to be an input or a three-state digital output that can be its input, the complement of its input, a one, or a zero. The devices are reprogrammable. But an A-side input/output can only be routed to B-side pins. These devices are ideal as DIP-packaged switch replacements.

Meanwhile, i-Cube is offering FPID devices, short for Field Programmable Interconnect Devices. While essentially PLD-style devices, those also provide for high-impedance analog applications.

Crossbar architecture is available with densities as high as 320 x 320. Since this is static-RAM
based, it must be retaught every time power is turned off. Each pin can be taught to have eight different functions and each pin can be non-buffered for analog signal pass-through. Digital inputs can be buffered or latched. Outputs can be buffered, registered, or held either high or low.

Information on newer devices likely to overcome all of the obvious defects of this current crop of products should show up in the usual electronics publications such as E.E. Times, EDN, Electronic Design, Electronic Component News, and in Electronic Products.

Let's have your thoughts on new hacker applications for these exciting parts. The usual Incredible Secret Money Machine II book rewards for your contributions.

New tech lit

Motorola has a new Master Selection Guide. One unique new IC is the MC144143 TV closed-caption decoder.

Tektronix has a number of videos and application notes that you might be interested in. One video is on The VectorScope, a crucial instrument for color TV broadcasting and video production. There's also a pair of videos on cable measurement, plus others on such specialized top-
ics as cable TV sweep systems. Of their many offerings, you might also find their application note on spectrum analyzers to be handy.

Real live human neurons are now offered by Stratagene according to its inside cover ad in the September 2, 1994 issue of Science. If I understand this ad correctly, these neurons can be hot wired for direct electrical to biological neuron computing experiments.

Three good weather satellite resources are MultiFAX, Accu-Weather, and ZFX.

Harris Publishing has a new 1995 Electronic Industry Telephone Directory. If it is not already in my Synergetics Master List, the EITD is the reference I’ll always check first.

Access to Energy is a labor-of-love publishing venture that bills itself as a high-tech, free enterprise, monthly newsletter.

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3 NEW BOOKS for the Project Builder

Electronic Board Games

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Twenty novel electronic board games that you can build from the plans in this book. Whether you are interested in motor racing, searching for buried treasure on a desert island or for gold in Fort Knox, spinning the wheel of fortune, or doing a musical quiz—there is something for you to build and enjoy!

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Antennas for VHF and UHF

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<th>BP301—ANTENNAS FOR VHF AND UHF</th>
<th>$6.00</th>
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From installing a TV or FM antenna to setting up a multi-antenna array for shortwave listening or amateur radio, this book explains the basics of VHF and UHF antenna operation and installation. The text describes in easy-to-understand terms the essential information about how antennas work, the advantages of different antenna types, and how to get the best performance from an antenna.
A

s with many other boys, it all started for me when I was about 13 years old. Not sex electrons. Hours of immersion in The Boy Electrician, Everybody's Radio Manual, and Radiocraft ultimately led me to apply for an after-school apprenticeship at a local radio repair shop. I'm sure that I got the job as a result of the World War II home-front manpower shortage rather than any precocious electronic know-how. But in any case, 50-odd years later I still remember an incident from my first day of work.

I was told to check out a five-tube, table model radio. It seemed O.K. for the first few minutes after warm-up, but then the output began to distort. My boss, who was working on something else, glanced at the radio and said: "Change the leaky 0.01 condenser between the plate of the 12SQ7 and grid of the 50L6."

I was stunned! How did he know what needed changing—or even what tubes were in the set? I vowed that one day I too would be the proud possessor of such arcane knowledge. And, by the time I joined the Army in 1946, I was so proficient in the electronic mysteries that I was sent to White Sands Proving Grounds to be an electronics technician during the start-up of the U.S. space program—but that's another story.

Post-service servicing

My career as a service technician continued after the Army. After several jobs with local car and home-radio repair shops, I found myself repairing test and hi-fi equipment for the Electronic Instrument Company (EICO) during the day, attending college in the evenings, and freelancing hi-fi repairs over the weekends. This went for five years or so until I traded in my soldering iron for the proverbial blue pencil and became the technical editor of Popular Electronics. (One might say that I went from repairing electronic equipment to fixing electronics prose...but perhaps not.)

During the time I've been in publishing I've witnessed the advent of the transistor, the IC, and the slow demise of tube electronics. From a very personal point of view, the virtual takeover by solid-state electronics has somewhat saddened me. It's not that I found something romantic in the soft glow and warmth of tube equipment; it's just that when something went wrong I could fix the damned thing! (I suspect that I now enjoy repairing old tube radios from yard sales and thrift shops mainly to offset lurking feelings of electronic impotence.)

My slow transition from Mr. Fixit to a normally incompetent electronics consumer was painful, but inevitable. As we all know, electronic technology is in such a state of rapid change that, like the situation with Alice's Red Queen, "It takes all the running you can do to keep in the same place. If you want to get somewhere else, you must run at least twice as fast as that."

Although I've hung up my Nike Airs, I can usually follow complex descriptions of new technologies—but please don't ask me to troubleshoot the products!

Manufacturers' warranties

When I first became involved in
audio in the Fifties, there were some strange ground rules embedded in manufacturers' warranties. It seems that the stores that sold hi-fi products were not allowed to do in-warranty repairs on them. For that, there were "factory authorized" warranty stations (which usually had contracts with several major companies) and, of course, the factory itself. I wondered at the time how the warranty stations could stay in business, given the very meager fixed-labor rate paid for each repair. It was explained to me that out-of-warranty repairs, including referrals from the manufacturers, made the difference—particularly since warranties usually were in force no longer than 90 days.

When transistor equipment appeared, many, if not most, electronic manufacturers optimistically extended their warranties to a year. A bad mistake, as it turned out. The transistors blew up, broke down, and sometimes fell out of their sockets during shipment. Yes, small-signal semiconductors were plugged into sockets because (1) they didn't stand up well to soldering heat, (2) the manufacturer was unsure about their reliability, and (3) they sometimes needed to be changed during component assembly and final test.

I recently spoke to an old friend who ran a warranty station during this transition period. He asserted that transistor problems not only caused the demise of many warranty stations—including his own—but also drove several hi-fi companies into deep financial trouble.

Aside from the arguments pro and con about transistor sound quality in the hi-fi magazines, the main consumer concern was equipment reliability. Knowing this, at least one manufacturer, Dave Hafler of Dynaco, held off joining the rush to solid state for at least a year until his products were, in his view, virtually bulletproof. Guess what? His amplifiers ran into trouble anyway— including the two that blew up in my living room.

Several years went by before a combination of better circuit design and improved semiconductors finally resolved the reliability question. Although today's equipment still breaks down for one reason or another, anyone who grew up with vacuum tubes is very much aware of the enormously improved reliability of solid-state components.

**Today's complaints**

During the very early days of hi-fi when I was doing my after-hours service work, no one ever complained to me about the high cost of repairs. After all, I was the hi-fi doctor bringing my curative know-how to their sick, but cherished, components. However, once audio equipment became a mass-production commodity, the audio repairman suddenly had no more status than the TV repairman—and might even have been the same person.

I've written several times that the high cost of a repair compared to the original product price is an inevitable result of modern manufacturing technology. To put it simply: Products are built by efficient, computerized, automated assembly lines, but they are repaired by the equivalent of 19th-century hand labor. For that reason, a skilled technician could easily put in $25 or more worth of labor to repair a $50 radio.

I've always held that the manufacturer was the best source for making repairs, whether in warranty or not. But I've noticed that some major hi-fi manufacturers now refer you to outside service organizations for repairs on their products. I'm not sure whether this results from downsizing, a desire to avoid the onus of repair problems, or in some other way reflects the currently problem-beset audio market, but the existing fact of life is that many manufacturers don't seem to want to do in-house repairs.

**The Shack solution**

Radio Shack for years has had a well established in-house repair service to handle its own exceptionally wide range of electronic products. Seeing an opportunity to bring a nationally known and responsible company name to an enterprise that strikes many consumers as a stress-inducing caveat-emptor situation, Radio Shack has apparently committed itself wholeheartedly to the consumer-electronics repair business. The "Repair Shop" at most Radio Shacks will handle more than 40 brands of equipment with the usual cost of repair ranging from $50 to $75.

In truth, I don't fully understand the economics of the situation from Radio Shack's point of view, but the company president estimates that the new repair business could generate $500 million a year by 1999. Their prospects seem favorable. According to the U.S. Commerce Department, consumers spent a total of $3.8 billion last year getting their electronic goodies fixed. And I find it embarrassing that I contributed my pitance to that pot.
It's been a long time coming but we're down to the last leg in the design of the tachometer. At this point, some arithmetic must be done, and here's where the job can get tedious.

The output of the latest circuit (see November 1994) is the number of sparks produced by an engine every three seconds. The following formula converts that to revolutions per minute:

\[ \text{rev./min.} = \frac{\text{sparks/sec.} \times \text{rev./spark} \times \text{sec./min.}}{3} \]

The first part of the expression is related to the number available at the output of the circuit, the second part is related to the size of the engine, and the last part is just standard conversion. If you simplify the expression and use "N" as the number of sparks per revolution for a particular engine, you wind up with a description of the arithmetic that you have to do:

\[ \text{RPM} = \frac{\text{(circuit count)} \times 20}{\text{N}} \]

There are two arithmetic operations to perform. One is to multiply the count delivered at the multiplexed output bus of the 4508s by 20 (60 seconds/3 seconds of sparks), and the other is to divide the spark count by a factor dependent on the size of the engine. There are many ways to do this: a bit of forethought can help you find the easiest.

If you were to do the multiplication first, you would have to deal with some awkwardly large numbers. For example, a 12-cylinder engine running at 6000 rpm produces 1800 sparks per second. Multiplying that by 20 means you'll need a circuit that can handle 36,000 decimal—that's 1000 1100 1010 0000 binary. Sixteen data bits are difficult to deal with.

The numbers that you have to work with will be much more manageable if the division is done first.

The question is, where should the division be done? Doing it after the 4508s might seem logical, but it would require too much extra circuitry. An easy place to do the division is right on the clock line feeding the 4040 counters.

Since the largest value you'll have for N is 6 (for a 12-cylinder engine), you can do the division with a 4017 decade counter and a bunch of jumpers as shown in Fig. 1. When the PC board is laid out, jumpers can be added to configure the tachometer circuit for engines with different numbers of cylinders.

The most straightforward way to handle the multiplication operation is with a rate multiplier. The 4089 is a CMOS binary rate multiplier that is perfectly suited for the required multiplication. The pinout of the chip is shown in Fig. 2.

When a clock signal is fed to pin 9 of the 4089 with most of the control pins grounded, and a binary number is placed on the data inputs, the chip will have two different outputs. The first output is the BASE RATE and the second is the MULTIPLIED RATE. The relationship between the two outputs makes the chip perfect for the tachometer application. For each pulse that is output at the BASE RATE pin, a number of pulses equal to the binary number preloaded at the data inputs are produced at the MULTIPLIED RATE pin.

To multiply two numbers (X and Y) with a rate multiplier, present one of them to the data inputs before the clock is started. Then keep track of both the base rate and the multiplied rate to get your answer. The rate
multiplier does that by counting up to \( X \) repeatedly at the multiplied output, and it indicates how often it's doing it at the base rate output. The rate multiplier is really doing successive addition. When it is asked to multiply two numbers together, it repeatedly counts up to one of them, and outputs the number of times it does it.

The rate multiplier needs a clock signal to operate it, but surprisingly it doesn’t matter what the clock frequency is. Simple algebra shows why this is true. Assume that you want to multiply \( X \) times \( Y \):

\[
\text{The base rate} = \text{input clock}/16 \\
\text{The multiplied rate} = (\text{input clock}/16)X \\
\text{The multiplied rate} = (X \text{base rate})
\]

thus:

\[
X = \text{multiplied rate/base rate} \\
X = (\text{input clock}/16)X)/(\text{input clock}/16)
\]

or

\[
X = X
\]

The only number that affects how many of pulses appear at the multiplied rate output is the number that’s preloaded on the data inputs. Multiplying two numbers is done by loading one number at the data inputs and letting the rate multiplier do successive addition a number of times equal to the second number. The answer is obtained by counting the total number of pulses at the multiplied rate output. See Fig. 3.

Since you’re dealing with eight bits of data from the spark counter and the 4089 has only four bits worth of data inputs, you’ll have to cascade two rate multipliers (IC16 and IC17). The only other IC you need is a counter that will stop the rate multipliers after they’ve made 20 passes of successive addition. This part of the circuit is made up of the 4040 (IC18) and the 4081 quad AND gate (IC19).

The 4040 counts the number of 4089 base rate output pulses and when the count reaches 20, and gate IC19-a detects the count and puts a high on the 4089’s inhibit inputs to stop pulses from appearing at the multiplied rate output.

One control signal is still missing, however. The AND gate stops the rate multipliers from working after multiplying the spark count by 20, but you need some way to restart the multipliers when a new count appears at the outputs of the spark counter.

This problem is solved by the 4040’s reset pin (pin 11). Every time a new spark count is ready to be multiplied, the two-hertz clock outputs a pulse that controls the 4040’s reset pin. As you can see in Fig. 3, the two-hertz clock signal is delayed by a half monostable circuit made up of a 4081 and gate (IC19-b), and this delayed signal triggers the 4040’s reset pin. The RC values in the half monostable circuit ensure that the 4040 won’t be reset until the correct count is available at the output of the spark counter.
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leaves a message at the tone. Transmitted messages or pictures are automatically recorded on the Viewcam's HI8 cassette, which permits up to two hours of audio or video information.

The system uses JPEG (Joint Photographic Experts Group) standards, has compression ratios of 20:, 15:, and 8-to-1, depending on the transmission speed: has a screen resolution of 384 x 240 pixels; and transmits images at 9600, 7200, 4800, and 2400 baud. Sharp thinks it will find many uses in business, where it's necessary to transmit detailed color images, as well as for personal use (sending baby pictures to Grandma, etc.)

The system isn't exactly cheap—the camcorder lists at $2500, the teleprompt at $900. And, of course, it takes two to tango.

**POWER CONTROLLER**

continued from page 76

then turns it off. It then repeats that action for output 2, and so on. After output 7 toggles, the software then repeats the cycle.

**Run and flash**—This is a variation of the sequencer application. It sequences the outputs for five cycles, then flashes all eight three times and repeats the cycle.

**Test**—The test application tests the controller. The routine steps the outputs through all 32 power levels, pausing one second between each.

**External**—Here's where things get interesting. This routine allows an external source, such as an intelligent I/O module or a computer, to control power levels. To get into this mode, set switch S2 to a value of 2, install the correct jumpers, then reset the circuit. From then on, input Port C0 functions as a strobe that causes the microcontroller to read the value on Port A and perform the proper function.

When VCC goes low, the microcontroller reads Port A. It then splits the value into a 5-bit power specification (PA0–PA4), and a 3-bit output port (PA5–PA7). The 5-bit power specification allows 1 of 32 values; the 3-bit output port allows 1 of 8 ports.

For example, assume you place the value 57 on Port A and strobe VCC low. In binary, 57 = 0101 0111. Taking the upper three bits yields 010, or 2. Taking the lower 5 bits yields 10111, or 23. Thus the controller will set output 2 to level 23.

**Summing up**

As you can see, both hardware and software are simple and suitable for being customized. For example, you could connect the output of an A/D converter to Port A, then vary power levels based on some analog quantity.

When creating your own routines, be sure to include it in both the power-on Select routine and the Jump Table. That way the controller will know where to find it.

**SIGNAL THEFT**

continued from page 40

vian and enter competitions.

By 1996, it is estimated that the U.S. market for digital cable converters will reach 4.5 million units annually, as cable companies upgrade the 65 million converter boxes now in use. The new converters—in conjunction with digital compression and fiber optic cable—will expand the television's receiving capacity to perhaps as many as 500 channels.

Numerous joint ventures are underway to develop a new converter, and the result is that several types of converters will be on the market. Among the projects in progress: Hewlett-Packard is building a radio-based system. Intel, Microsoft, and General Instrument are creating a cable box based on Intel's microprocessors and G1's digital compression technology. Scientific Atlanta is building digital terminals for Time Warner's Full Service Network and U.S. West's video dialtone trial.

There is an industry-wide requirement for adequate signal security. A pirate who develops the technology to intercept a digitally compressed signal might be able to access a person's bank account, ATM number, and phone number, as well as other personal information.

The starting point for the scrambling that will be used for interactive television is the encryption already in use for digitally transmitted signals. Those transmitted signals are already in limited use by several programmers such as HBO.

Interactive television promises to be a revolution in television viewing. By any account it will be a boon to the cable industry and generally to the electronics industry. Reaping the full benefits of this technology will be no small feat. Signal theft will be one of the major obstacles. Not only will a foolproof encryption standard have to be developed, but intra-industry security must be carried out along with a uniform policy for marketing and distribution.
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- VCF, Symmetry
- Variable DC Offset Control

2MHz Sweep Function Gen. w/Freq. Counter
FG-150
Reg. $399. $229.00
- 4 Digit LED Display
- Sine, Square, Triangle, TTL
- Pulse, Ramp, Skewed Sine
- Linear/Logarithmic Sweep
- 10 MHz Freq. Counter

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- 4 Selectable Gate Times
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DC Power Supply
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- 0.1 - 3A
- Short & Overload Protection

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- 0.1 - 10A
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2 yr. Parts/Labor Warranty

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OS-3324
Reg. $599. $399.00
OS-3344
Reg. $899. $649.00

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- DC to 25 MHz, Dual Channel
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- Rise time 14ns Sec. or less.
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- Acceleration Potential 2kV
- 60MHz (X1 X10) Probe Kit: 2 sets
- Power: 115/230V AC

OS-3324
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3 Function
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2. Dual Component Tester/Comparator
3. Triple DC Power Supply
   5VDC, +12VDC, -12VDC

OS-3344
Reg. $899. $649.00
5 Function
1. OS-3304
2. OS-3324
3. OS-3344
4. Frequency Counter 100MHz, 7 Digit LED Display
5. Function Generator 0.02 Hz to 2.0 MHz

Oscilloscope Probe Kit
Switch Selectable X1/X10

Pen-Type
Reg. $79.

DM150
Reg. $59. $59.00
- 3 1/2 Digit
- Dual Display
- Auto & Manual
- DCV, ACV, ACA, DCA, U
- Logic
- CMOS/ TTL
- Data Hold
- Diode
- Continuity

DM2500
Reg. $59. $39.00
- 3 1/2 Digit
- 15" Big LCD
- 20A AC/DC
- 10A AC/DC
- Signal
- Inserter
- Diode
- Continuity
- Holster

Oscilloscope Probe Kit
Switch Selectable X1/X10

Multifunction DMM
Reg. $89. $59.00

DM150
Reg. $59. $59.00
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- Dual Display
- Auto & Manual
- DCV, ACV, ACA, DCA, U
- Logic
- CMOS/ TTL
- Data Hold
- Diode
- Continuity

DM2500
Reg. $59. $39.00
- 3 1/2 Digit
- 15" Big LCD
- 20A AC/DC
- 10A AC/DC
- Signal
- Inserter
- Diode
- Continuity
- Holster

DM3050
Reg. $59. $39.00
- 3 1/2 Digit
- 15" Big LCD
- 20A AC/DC
- 10A AC/DC
- Signal
- Inserter
- Diode
- Continuity
- Holster

DM5100
Reg. $59. $39.00
- 11 Function / 45 Range
- Basic DCV Accu.: ± 0.25%
- 3 1/2 Digit
- Auto Power Off
- Data Hold & Peak Hold
- Amp: Up to 20A AC/DC
- Ohm: Up to 200MΩ
- Freq.: Up to 20MHz
- Capacitance: 1pF - 20.000μF
- Logic: TTL
- TR-NF, Diode
- Continuity Beep
- Double Insulated Jack
- Alligator Clip Test Leads
- Deluxe Holster w/Strap

Wide Range Multimeter w/Logic
Reg. $49. $119.00

Capacitance Meter
Reg. $79. $49.00
CM210
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- 0.1pF-2000μF
- 9 Ranges
- 0.5% basic Accu.
- Zero Adj. Knob

Digital Clamp-On
Reg. $89. $54.00
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- 3 1/2 Digit
- Auto
- Data Hold
- Continuity
- Over Range
- Case Included

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- Multimeter
- Volt: AC/DC
- Amp: AC/DC 2A
- Ohm: Up to 2000MΩ
- Multi-Function Beep
- Capacitance Range
- 9 Ranges
- 0.1pF - 20.000μF
- Zero Adj. Knob
- Trig Lamp
- Double Insulated Jack
- Alligator Clip Test Leads
- Deluxe Holster w/Strap

Wide Range Multimeter w/Logic
Reg. $49. $119.00

Multifunction DMM
Reg. $89. $59.00

DM5100
Reg. $89. $59.00
- 11 Function / 45 Range
- Basic DCV Accu.: ± 0.25%
- 3 1/2 Digit
- Auto Power Off
- Data Hold & Peak Hold
- Amp: Up to 20A AC/DC
- Ohm: Up to 200MΩ
- Freq.: Up to 20MHz
- Capacitance: 1pF - 20.000μF
- Logic: TTL
- TR-NF, Diode
- Continuity Beep
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The Ultimate Meter
TRUE RMS - LCR - Hz - dBm

Popular Electronics (Reviewed - May 1993)
"Not only does the Kelvin 94 boast a lot of features ... the features go the extra distance."
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$199.95

Model 94 #990111

Comes complete with yellow Holster, Probes, Battery, Fuse, Stand

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GREEN $65
SA-3 $43
M-80 $65
SA-3DF $69

Please call for 20 and 50 piece prices

FACTORY EQUIPMENT

<table>
<thead>
<tr>
<th>Brand</th>
<th>Model</th>
<th>Price</th>
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<tr>
<td>Zenith</td>
<td>ST 1600</td>
<td>$239</td>
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<tr>
<td>Tocom</td>
<td>5503</td>
<td>$239</td>
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<tr>
<td>Pioneer</td>
<td>6300</td>
<td>$319</td>
</tr>
<tr>
<td>Pioneer</td>
<td>6150</td>
<td>$299</td>
</tr>
</tbody>
</table>

All prices are for 10 pieces, subject to change without notice. Some quantities may be limited. 30-Day Money Back Guarantee. One year parts and labor warranty.

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- Starcom 6 BB $17.50
- Starcom 6 Chip $10
- RZ/V5/CFT Kit $29.99

PIONEER
- 51XX-61XX NEW!!! Pio Kit $25
- Never Goes E-4 $29.99

TOCOM
- 5503 $14
- 5507 $14

ZENITH
- ST-1000-ST 16XX $11

SCIENTIFIC ATLANTA
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- Quick Boards CALL
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FIBRE OPTIC TUBES

These US made tubes are "pulls" from equipment, in excellent condition. Have 25/40mm diameter, fiber-optically coupled input and output windows. The 25mm tube has an overall diameter of 57mm and is 60mm long, the 40mm tube has an overall diameter of 80mm and is 92mm long. The gain of these is such that they would produce a good image in approximately 1/2 moon illumination, when used with a suitable "fast" lens, but they can also be IR assisted to see in total darkness. Our HIGH POWER LED IR ILLUMINATOR kit, and the IR filter are both suitable for use with these tubes. The superior resolution of these tubes would make them suitable for low light video preamplifiers, wildlife observation, and astronomical. Each of the tubes is supplied with an 18V EHT power supply kit. INCREASING PRICES:

$85 For the 25mm intensifier tube and supply kit.
$130 For the 40mm intensifier tube and supply kit.

We also have a good supply of the same tubes that may have a small blemish which is not in the center viewing area.

$50 For a blemished 25mm intensifier tube and supply kit.
$70 For a blemished 40mm intensifier tube and supply kit.

IR "TANK SET"

A set of components that can be used to make a very responsive Infra Red night viewer. The matching IR tube, lens and eyepiece sets were removed from working military quality tank viewers. We also supply a very small EHT power supply kit that enables the tube to be operated from a small 9V battery. The tube employed is probably the most sensitive IR responsive tube we ever supplied. The resultant viewer requires low level IR illumination. Basic instructions provided.

$105 For the tube, lens, eyepiece and the power supply kit.
When ordering specify preference for a wide angle, or a telescopic objective lens.

IMAGE INTENSIFIER TUBE AND SUPPLY

These are the key components needed for making a PASSIVE NIGHT VIEWER. The small pre-focused Russian image intensifier tube only requires a low current EHT power supply to make it operational, which we provide in kit form. Drawn 20mA from a small 9V battery. With a suitable low light objective lens (we provide) the resultant viewer will produce useful pictures in sub-moonlight illumination and it can also be IR assisted. ON SPECIAL.

$90 For the Russian image intensifier tube and an EHT power supply kit. All that is needed to make a complete passive night viewer is a lens, an eyepiece, a 9V battery, a case and a switch.

HIGH POWER LED IR ILLUMINATOR

This low cost FM transmitter Kit includes a PCB, all on-board components plus casing. Supplied module power supply plus 60 high intensity 880nm IR (Invisible) LEDs. Variable output power. Low cost, easy to use, for illuminating IR responsive CCD cameras, IR night viewers etc. Professional performance at a fraction of the price of the commercial product. COMPLETE KIT PRICE: $44

VIDEO TRANSMITTERS

Low power NTSC standard UHF TV transmitters. Have audio and video inputs with adjustable levels, a power switch, and a power input socket. 10-14V DC/ 10mA operation. Enclosed in a small metal box with an attached teleoscopic antenna. Range is up to 300ft. with the teleoscopic antenna supplied, but can be increased to approximately 1000ft. by the use of a small directional UHF antenna. INCREASING PRICING:

$18 For the tube, lens, eyepiece and the power supply kit.
When ordering specify preference for a wide angle, or a telescopic objective lens.

INFRA RED FILTER

A very high quality IR filter and a RUBBER lens cover that would fit over most torches including MAGNETES, and convert them to a good source of IR. The filter material withstands high temperatures and produces an output which would not be visible from a lens less than about 1000mm (40") from the filter, that enables an image intensifier tube. The viewer is a USSR military standard, and will produce useful images in very low ambient light. Has adjustable low light objective lens, adjustable eyepiece and is supplied with a carry case. ON SPECIAL.

$11 For the filter and the rubber lens cover.

FM TRANSMITTER KIT - MKII

This kit includes two PCB's, all on-board components plus casing. Supplied module power supply plus 60 high intensity 880nm IR (Invisible) LEDs. Variable output power. Low cost, easy to use, for illuminating IR responsive CCD cameras, IR night viewers etc. Professional performance at a fraction of the price of the commercial product. COMPLETE KIT PRICE: $44

SECOND GENERATION TUBES

We should have a regular supply of some new USSR made 8mm 2nd. Gen. Fiber optically coupled image intensifier tubes, approx. $500 and also some used US-European made tubes, approx. $320. Some of these may require an export permit.

PASSIVE NIGHT VIEWER

This is a complete commercial monocular hand held night viewer, that employs an image intensifier tube. The viewer is of a USSR military standard, and will produce useful images in very low ambient light. Has adjustable low light objective lens, adjustable eyepiece and is supplied with a carry case. ON SPECIAL.

$220 For the filter and the rubber lens cover.

CCD CAMERA

Monochrome CCD Camera which is totally assembled on a small PCB and includes an Auto Iris lens, 9-12V DC operation. It can work with illumination of as little as 0.1 Lux, and is IR responsive. Can be used in total darkness with Infra Red illumination. A suitable illuminator is our HIGH POWER LED IR ILLUMINATOR kit. Overall dimensions of camera are 24 x 66 x 70mm and it weighs less than 40 grams. Can be connected to any standard monitor or the video output on a video tape recorder. EA (US-NTSC) compatible.

$145

MINIATURE FM TRANSMITTER

Not a kit but a very small ready made complete FM transmitter enclosed in a small black plastic case, powered by a single small 1.5V silver oxide battery, and has an inbuilt microphone. SPECIFICATIONS: Tuning range: 88-108MHz, Antenna: Wire antenna - attached, Microphone: Electret condenser, Battery: One 1.5V silver oxide cell, Battery life: 60 hours, Weight: 15g, Dimensions: 1.2" x 0.9" x 0.4".

$25

MICROSECOND ITEMS COMPONENTS AND KITS

SINGLE CHANNEL UHF REMOTE CONTROL KIT. One transmitter and one receiver. $32 additional transmitter. $11 4 CHANNEL UHF REMOTE CONTROL KIT. Two transmitters and one receiver. $58 ELECTRIC THERM KIT with components $28 GARAGE/DOOR/GATE REMOTE CONTROL KIT. $1 13. $5 GLOVE LASER BEAM COMMUNICATOR KIT. TX & RX with IR LED, $39 PLASMA BALL KIT. PCB and components $28 BEAM COMMUNICATOR KIT with Linking IR LED. $18 HIGH POWER IR LED'S, 880nm/30mA/12deg, @ 100mA... $10 for $6

All our kits are provided with high quality fibreglass, silk screened and solder masked, printed circuit boards and instructions. 

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January 1995. Electronics Now

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**PERSONAL PROTECTOR ALARM**

**G5058**

**SALE**

$6.95

2/$12.00

**SALE WAS** $8.95

Very talk model Radiosonde made for tracking all types of weather data. These were to be sent aloft attached to a weather balloon (not included). Each is about 10 1/2” long x 3 1/2” thick x 8” wide. Inside of the removable cardboard sleeve is a styrofoam chamber housing a sophisticated 8 IC circuit board which has sensors attached to measure atmospheric pressure, temperature and humidity. As it gathers the information, it transmits the data at a rate of 1.577 Viggenber [Hz]. These are prime, brand new units that were not shipped from the manufacturer (Space Data Corporation) to the government when the contract ended. These are complete except for the 24V battery (we connected two 9V batteries in series and the unit worked perfectly fine). Sorry, no schematics available. These cost the government a bundle to have made but we are selling them at a giveaway price. Hurry, get your Radiosonde today!

**THE AMAZING RADIOSONDE**

**G6135**

$19.95

Electronic high-tech game features a large easy to read display and a convenient pocket size. Choose either Poker or Blackjack with the press of a button. Features automatic score keeping and operates from two AAA batteries (not included). Blackjack features split, surrender dealer stand on 17, double down on any points insurance when dealer has 11, variable 1 to 20 betting, etc. Poker features automatic 5 point bet per hand, player can hold or draw 5 cards, etc. Each game features music for winning/losing. Compact fun game for hours of fun. In retail blister pack.

**G6135**

**G5809**

$14.95

These are very interesting ultrasonic people detectors. They were designed for open doors at stores when a human approached. They have an adjustable range of 4” to 10” with a relay contact closure. Made by a company called Microwave Sensors but these are ultrasonic sensor technology. They are the complete circuit board assembly from their model 144 and feature 12VAC or 12VDC operation (use a transformer or our 9VDC adapter shown on pg. 71 of our catalog; a contact detection pattern, response time of 2 sec, hold time continuous (as long as you are in its field of view), reset time accommodates 1 to 15 seconds. Current draw 60 ma. They are designed for AC power and SPDT relay contacts. Size of board: 4” x 2 1/8”.

**ULTRASONIC PEOPLE DETECTOR**

**G5809**

**G5535**

$12.25

12/12.00 + 120/110.00

Make all kinds of IR remote activated projects with this transmitter and an IR infrared module. These were originally designed to activate a burglar alarm system (which we don’t have) by remote control. The transmitter features a red activation button, a dip switch inside to change output code, operates from 9V battery (not included), red LED transmitter indicator to show when IR energy is being transmitted and a compact 1/4” x 1/3” x 1/4” 3/4” black Styrofoam case. Brand new in blister pack with 2 peel and stick “permanent protected” stickers. We also supply an on sheet that shows how to convert this transmitter unit into a programmable IR receiver to pick up any of these transmitter units could be both transmit and receive functions.

**SUPER POWER MINIATURE IR TRANSMITTER UNIT**

**G6134**

$7.95

TL084 QUAD OP AMP (SMD)

Prime popular TL084 JFET input tiny SMD quad op amp. Power output is 250mW or more. G6250 79¢

**THERMAL FUSE**

**G5907**

3/$1.00 100/$25.00 • 1,000/$220.00

Same type found in copiers, fax machines, copiers and printers. These hand held devices are made of material, however, when their temperature rating is exceeded fifty “blow out” permanently for fail safe operation. This one is made by Micromax Brand new in blister pack.

**TRANSISTORS BY THE SCOOP**

**G5071**

Less than 1¢ each

1 scoop $5.00

10 scoops (about 5,000) $40.00

We just purchased close to 1 1/2 million BJT transistors made for an OEM. Each is House Numbered and has full weight heel. They are absolutely first quality – not rejects. We think there are Darlington and small signal NPN transistors. We do know that there is at least 4 different house numbers. Most are regular size TO222 cases however, there are also a few 1 watt TO222 cases. Tremendous value as we are selling them by the scoop. Each scoop holds at least 500 transistors. Sorry we can’t separate them, but at this price you can and you’ll save a bundle!

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Our best assortment ever. Contains 25 pieces of various size copper clad circuit board blanks. Each is double sided and you will receive thickness types from ultra thin to standard thickness. Minimum size 2” x 2” to a maximum of 6” square. A PC board makers delight.

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- 4 independent channels, 8 traces
- Time/ Voltage Cursor measurement
- ALT triggering function for 4 ch.
- Sweeps in 2msec, Delayed Sweep
- TV Sync. Ch. 1 output, Z-axis input
- 2 probes (x1, x10)

**OS-6100B**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>OS-6100B</td>
<td>Best value all purpose scope</td>
<td>$1,329.95</td>
</tr>
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</table>

### DC Linear Power Supplies
- Single Output

**FG-8016G**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
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<tbody>
<tr>
<td>FG-8016G</td>
<td>Digital Display Function Generator</td>
<td>$239.95</td>
</tr>
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### 50 MHz Triggering Oscilloscope
- Dual Channel
- Hold Off Function
- Delayed Sweep
- Build-in Delay Line
- TV Sync

**OS-653**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
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<tbody>
<tr>
<td>OS-653</td>
<td>50 MHz Triggering Oscilloscope</td>
<td>$699.95</td>
</tr>
</tbody>
</table>

### 20 MHz Oscilloscope
- Dual Channel
- ALT Triggering
- Delayed Sweep
- TV Sync
- 2 probes (x1, x10)

**OS-622B**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>OS-622B</td>
<td>20 MHz Oscilloscope</td>
<td>$344.95</td>
</tr>
</tbody>
</table>

### Programmable DC Power Supplies
- Dual trace, X-Y operation
- TV Synch. Z-axis input, Ch. 1 output
- High sensitivity 1 mV/div
- Trigger level 10 mV/div
- 2 probes (x1, x10)

**OS-6588**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
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<tbody>
<tr>
<td>OS-6588</td>
<td>Programmable DC Power Supplies</td>
<td>$899.95</td>
</tr>
</tbody>
</table>

## Digital Display Function Generator
- Frequency Range: 0.02Hz to 2MHz
- 3 Instrument mode in one: Function generator, Pulse generator & Frequency counter
- Frequency: 1Hz, Square, TTL Pulse and CMOS output
- Built-in 6 digit counter with INT/EXT function
- 1000:1 tuning range
- Variable DC offset control

**FG-8015**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
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<tr>
<td>FG-8015</td>
<td>Digital Display Function Generator</td>
<td>$239.95</td>
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### Digital Multimeter & C Meter
- Programmable features
- High performance
- Auto power off
- Auto range, relay mode, Max/Min
- Variable DC offset control

**DM-8034**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
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<tbody>
<tr>
<td>DM-8034</td>
<td>Digital Multimeter &amp; C Meter</td>
<td>$179.95</td>
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</tbody>
</table>

### Model DM-392
- 3½ digit DC multimeter
- Auto/Manual range (3 ranges)
- 42 Segment bargraph display
- Auto HOLD/Max/Min memory
- Relative mode
- Auto power off
- Overload protection
- Available continuity check (diode test)
- 4 continuity levels
- 10A DC current accuracy
- Auto True RMS (DM-394 only)

**DM-392**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
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<tbody>
<tr>
<td>DM-392</td>
<td>Programmable DC Power Supplies</td>
<td>$109.95</td>
</tr>
</tbody>
</table>

## Contact Information
- ALFA ELECTRONICS
  - 741 Alexander Rd., Princeton, NJ 08540
  - (800) 526-2522/(609) 520-2002
  - FAX:(609) 520-2007

- Visa, Master Card, American Express, COD, Purchase Order Welcome
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**Muscle Wires Project Book & Deluxe Kit**

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**Electric Piston Deluxe 5-Pack**

Incredible miniature cylinders lift 1 pound each! Just 10 cm long, they shorten by 23 mm with just 1 volt, 5 amps. Cycles up to 6 times per minute. Pack has 5 Electric Pistons, one high current battery and complete plans for four unique projects.

#3-137 $29.95

**Robot Builder's Bonanza, 99 Inexpensive Robotics Projects**

A huge collection of practical, ready-to-use circuits & devices. Sections on parts, tools, methods, remote control, vision, grippers, navigation & more! 596 pages, 280 illus. A great value for robot builders of all experience levels.

#3-114 $17.95

**Space Wings II - now variable speed**

Sleek silver wings flap silently - using only 5 cm of Muscle Wire. Perches on your PC, annoys cats! Flaps up to 36 times per minute. With circuit board, parts, detailed instructions. Requires soldering and 2 AA batteries. Makes an ideal introduction to electronics and Muscle Wires.

#3-001 $19.95

---

**BEFORE YOU PRESS HERE**

In an emergency, help isn't on the way unless someone calls. So before you press on their chest, breathe in their mouth or even check their pulse, call 9-1-1 or your local emergency number.

---

To learn more about life-saving techniques, call your Red Cross.
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Hours: Monday through Friday 8am to 7:30pm EST - Saturday 10am to 3pm.
51756 Van Dyke St. #330, Shelby Township, MI 48316

Free Calculator with order!

CONVERTER

<table>
<thead>
<tr>
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<th>10</th>
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<tr>
<td>PANASONIC TZ-PC 145362</td>
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<td>$64</td>
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<tr>
<td>WAVEMASTER</td>
<td>$65</td>
<td>$60</td>
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<tr>
<td>DRZ-3 A &amp; B DUAL INPUT</td>
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CONVERTER/DESCRAMBLERS

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<tr>
<td>8580</td>
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<td>DPV-7</td>
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ADD-ON DESCRAMBLERS

10 LOT SPECIAL

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<tr>
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<tr>
<td>PIONEER GREEN</td>
<td>$65</td>
<td>J-TVT-GOLD</td>
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<td>SA-M80</td>
<td>$65</td>
<td>J-MINI TVT</td>
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<td>J-TNT</td>
<td>$65</td>
<td>H-MLD 1200-3</td>
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<tr>
<td>J-PURPLE</td>
<td>$49</td>
<td></td>
</tr>
</tbody>
</table>

NOTE: MENTION AD FOR THESE PRICES!
NO MICHIGAN SALES

We are now offering a 6 month warranty. In order for warranty to be in effect, this form must be signed and returned. FOR VCR, SECOND, THIRD, ETC. HOOK-UPS.

☐ YES, I agree all units are to be used or resold in compliance with Federal and State laws.

Signature ___________________________ Date ___________________________

NAME ___________________________ ADDRESS ___________________________

CITY ___________________________ STATE __________ ZIP ______ PHONE __________

It is not the intent of B&S Sales to defraud any pay television operator and we will not assist any company or individual in doing the same.
In recent independent tests Cool-Amp is proven **better** than electroplating.

(For 50 years we've said Cool-Amp is "equal to" electroplating in performance. It is better.)

**Cool-Amp**

![Graph comparing Cool-Amp and Electro Plate connections over time.](image1)

**Conducto-Lube**

![Graph comparing Conducto-Lube with Factory and No Lubrication connections.](image2)

**From the report:**

"...compare the conducting properties of Cool-Amp silver plating compound with factory silver electro-plated bus and bare copper bus.

"The test results indicated that the contact resistance of the Cool-Amp plated bus connection was slightly lower than that of the electro-plated bus connection and much lower than that of the bare copper bus connection. The final temperature at temperature equilibrium of the bus connection employing Cool-Amp was slightly lower than that of the electro-plated bus connection and the bare copper bus connection...

**Cool-Amp How it works:**

- Applies on the job. Application is simple. Yet Cool-Amp adheres permanently. As tests show, it is better than electroplating.
- Minimizes overheating and power loss by silver plating high amperage connections.
- Saves time, reduces maintenance. Cool-Amp is so simple to apply on the job. It assures maximum conductivity for copper, brass, or bronze contacts and prevents losses due to oxidation.

**Conducto-Lube How it works:**

- This is the conductive lubricant; highly conductive because it contains pure silver.
- Originally developed to lubricate switches, to the point tension can be adjusted to factory specs allowing full rated capacity of the switch to be maintained at all times.
- Uses have continued to expand—from switches and breakers—to any application where a conductive lubricant is needed.

**Cool-Amp Conducto-Lube Company**

15834 Upper Boones Ferry Road
Lake Oswego, Oregon 97035
Order factory direct:
503/624-6426, Fax 503/624-6436

*Various tests were performed on both products in the Electra-Test, Inc. facilities in Portland, Oregon during January-March, 1994. Evaluation of plating thickness of Cool-Amp was performed by Surface Science Laboratories of Mountain View, Calif.*
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• easy-to-follow, detailed instructions
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• safety precaution checklists
• comprehensive replacement parts list
• directory of manufacturers

January 1995, Electronics Now
122
Price: $400.00 extra per set. Price: $1,200.00 ea. Checked.

Price: $195.00 Used Repairable
"Just arrived" R-390's. They look to be in pretty good shape (no meters). But still a great investment @ $165.00 Used Repairable

Price: $695.00 round emblem.

Price: $295.00 New in Orig Carton.

Price: $65.00 ea. & less filters.

Price: $695.00 Radio only-less filters.

Price: $350.00 Complete sets only.
STATIC FREQUENCY CONVERTER
Finally a simple way to power up all that 400 cycle stuff. This is a completely self contained solid state converter that just plugs in to any 115 vac 60 Hz power source and provides easy instant 400Hz single phase 115 vac output @ 500 watts. Price: $395.00 ea. New in Original Carton (Product size 2.2" x W 1/2" x H 1/2"  Weight: 900s)

NIDA ELECTRONIC TRAINER
For those of you with limited funds this system provides you with the most essential instruments in one system. It incorporates the following:
- 10MHz oscilloscope
- Autoranging DVM
- Function generator
- "3" variable dc power supply
- "11" variable ac power source
- Precision decade resistance
- Speaker and 2 analog meters
This unit comes complete with a number of electronic experiments assembled on easy to use plug-in cards. Price: $365.00

Just Arrived - $35.00
8-DAY AIRCRAFT CLOCK
1-7/8" dial
Great collectors item for the ham shack, fifteen vintage clock hands.

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SELECTED EXCELLENT COND......$849.00
VERY GOOD CONDITION..............$695.00

These instruments are fully checked out and calibrated. They are supplied with an original front panel cover and complete service manual. Original TEK Probes are $75.00 each with each purchase.

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Model 1982
FREQ range 80kHz-520Mhz with calibrated output levels from -127 dBm to +13dBm. Resolution 10Hz. It can be freq., phase or amplitude modulated from ext or int modulation sources. RF output resolution is 0.1dB, reverse power protection of up to 50W is possible without damage to the instrument. This instrument is microprocessor controlled and very easy to use, a must for any serious repair or development lab. Price: $1750.00 Checked

PDR-63 PORTABLE RADIAC METER
This portable radiac set is loaded with all kinds of extras featuring six ranges of sensitivity for both Gamma or Beta radiation measurements. The 1st scale 0-1 rad/hr up to 0-5000 rad/hr. The unit comes supplied with headset & bat/charger. Reg's only 4 AA Batteries. Price: $149.95

CIRCLE 335 ON FREE INFORMATION CARD

January 1965, Electronics Now
Liquid Crystal Displays

160 x 128 dot LCD with Built-in controller. (T6963C)

20 character x 16 line capability. $79.00 2 for $149.00

Mfr. Toshiba TLX-1013EO.
Unit is EL back-lit. Dim: 5" x 1/2 L x 4" 1/2 H.
The built-in controller allows you to do text and graphics without adding an additional controller card.

Alphanumeric-parallel interface

16 x 1 3 for $25.00 16 x 2 $8.00
20 x 2 $12.00 16 x 4 $25.00
20 x 4 $25.00 4 x 2 $12.00
32 x 2 $20.00 40 x 2 $2 for $25.00
40 x 4 $25.00 4 x 2 $5.00
5V power required. Built-in D-EC LCD driver & controller. Easy "Microprocessor" interface. 88 ASCII character generator. Certain modes are backlit, call for more info.

Graphic and alphanumeric-serial interface

Size Mfr. Price
640 x 480 Epson $50.00
640 x 400 (backlit) Panasonic $35.00
640 x 200 Toshiba $19.00
480 x 128 Hitachi $15.00
256 x 128 Epson $25.00
240 x 128 (backlit) Optrex $20.00
160 x 128 Optrex $15.00

LASER PRODUCTS

HeNe Laser Head (10mW max. output) TM600, 15.5" long MFG. INC. $149.50
Laser Power Supply (for HeNe tube) $100.00
LASER SCANNER ASSEMBLY $29.00
Assembly intended for a laser printer. Includes laser diode, polysil market (self) and auto. optics and lenses.
LASER DIODE (5mW) with collimator $20.00
LASER DIODE: Sharp part#: LT022MC
5mW at 780 nm, single transverse mode $10.00

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IRMA BOARD 8 bit $99.00
Links 3270 mainframe systems to IBM PC.
Proxnet ProNet-4 Model p1247 Token Ring Board $79.00
16 bit x 4 Mbps IEEE 802.2 and 802.5 compatible twisted pair interoperable with IBM Token Ring network.

POS & BAR CODE

MAGNETIC CARD READER $25.00
Includes: 20 character dot matrix display with full alphanumeric capability, keypad with full alphanumeric entry, separate 7.5 VDC/0.5 Amp power supply, standard telephone interface extension cord, lithium battery and flat-cone speaker.
HP bar code wand (HBSC 2300) $35.00

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73 WATT SWITCHING $15.00 or 2 @ $25.00, (2) 4 pin power connectors attached -115-230 Volt, Dim: 85/4" L x 4.5" W x 2" H. Output: 5V @ 2.9-7.5 A, +12V @ 0-1.5 A, +5V @ 0.0-4.4 A, +12V @ 0.5 A
68 WATT SWITCHING $12.00 or 2 for $20.00, 115/230 Volt, Dim: 5.5" L x 3.2" W x 1.7" H. Output: 5V @ 4 A, +12V @ 4 A

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ADAPTEC 4070A (RLL) OR 4000A (MFM) SCSI Controller, your choice $49.00
IBM 370 option XT and AT emulation boards $50.00

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Non-Enclosed TTL
Comes with prong 12V at 1.4 Amp input, horizontal frequency 15 KHz. Ability to do 40 and 80 columns.
5 inch Black & White $35.00
7 inch Amber $39.00
9 inch Amber $29.95
12" Green or B & W $19.95

Enclosed
9" Green BNC composite 115V/230V $69.00
12" White BNC composite 24V $79.00
Mfr. Electrohome. For very high quality medical and industrial applications.

5" COLOR MONITOR $69.00
Flat Face Plate 320 x 200 Dot Resolution 2 for $109.00
CGA & Hercules Compatible
12 VDC Operation 15.75 KHz Horiz. Freq.
60 Hz Vert. Sync. Freq. Open Frame
Construction Standard Interface Connector
Degaussing coil included. Mfr. Samtron

CHARGE COUPLED DEVICES

"The Spy In The Sky" $49.00
Sony CCD Imager - designed for black and white composite video cameras. Picture elements: 384 (H) x 491 (V)
Chip size 10.7 (H) x 9.3 (V) mm². Unit cell size 23.0 (H) x 13.4 (V) um².
Ceramic 24 pin DIP package. Mfr. Sony, Part# S16AE
4096 element CCD $29.00
2048 element CCD $15.00
1728 element CCD $15.00

HACKER CORNER

Proxim - Spread Spectrum RF Modem $199.00
The Proxlink is a small communication device that replaces the use cable hook up with wireless (Radio Frequency) technology. Each modem functions as an RS-232 compatible modem for any other RS-232 transmit/ receive operating in the 902-928 MHz band. Indoor range is approximately using standard 1/4 wave antenna. Units support data rates of kilobaud (full duplex) and uses multiple channels to avoid overlapping signal conflicts. Message format is 8 data bits, no parity, and unit requires 5 VDC supply at a maximum of 230 mA. This configuration can be accommodated with standard 9600 baud (9600) and 19,200 baud (19,200) signals. The Proxlink is a small, lightweight device that can be tucked into a side pocket or carried on an overhead strap.

Portable Micro Terminal
Flip up LCD display (9-16 VDC) Can communicate with any computer having RS-232 port. Can communicate with another Micro Terminal. Use by itself as electronic notebook. Onboard microprocessor, data RAM (256K) and Video RAM (64K). Complete built-in diagnostic and setup capabilities. Original intention for DOS applications. Display size 40x16 (256 x 128 pixels). Dimensions: 6.3" W, 7.7" H. (With LCD up height is 7.7"").

All in one 326 boards
Includes: 266-12Mhz CPU (1 wait state). Built-in IDE & floppy controller. 16Mb memory (16 Mb SIMMS). Comes with 90 day warranty. On board speech. Real time clock. Phoenix BIOS. Note: There is one long non-standard bus connector on board.

Minimum order: $20.00. Minimum shipping and handling charge $5.00. We accept credit cards, checks, M/C or VISA. No personal checks or COD's. CA residents add 8.5% sales tax. We are not responsible for typographical or clerical errors. All merchandise subject to prior sale. Prices are subject to change without notice. 20% restocking fee for returned orders.

CIRCLE 275 ON FREE INFORMATION CARD
They’re here! These new BASIC Stamp modules are the latest computers. These modules are perfect for numerous applications, trains to monitoring factory sensors. They have 8 or 16 I/O lines, which of digital and analog purposes. And like the original BASIC Stamp, these modules are programmed in BASIC.

Our special “PBASIC” language includes familiar instructions, such as GOTO, FOR...NEXT, and IF...THEN, as well as SBC instructions for serial I/O, pulse measurement, and button debounce. In the new BS2-IC, there are even instructions for interfacing to popular devices from other companies, such as the Dallas Semiconductor “Time-In-a-Can” real-time clock.

* Carrier board provides battery clips, prototype area, and PC connector.

The BASIC Stamp Programming Package contains everything you need to program Stamps using your PC. The package includes our editor software, programming cables, manuals, application notes, and free technical support. The package is available for $99; Stamps must be purchased separately.

**PIC®16/17Cxx DEVELOPMENT TOOLS**

New prices make PIC development more affordable

**ClearView In-Circuit Emulators**

20-MHz in-circuit debugging for PIC16C5x/64/71/84/...
Set breakpoints, step through code, and modify registers.
Friendly DOS and Windows software.
$499 each! (separate units for “5x” and “xx” PICs)

**PIC Programmer Hobbiest Pack**

Programmer for PIC16C5x/64/71/74/84/...
Documentation on disk.
User-supplied cables and power supply.
Just $99!
DC-2000 MHz

AMPLIFIERS

In plastic and ceramic packages, for low-cost solutions to dozens of application requirements, select Mini-Circuits' flatpack or surface-mount wideband monolithic amplifiers. For example, cascade three MAR-2 monolithic amplifiers and end up with a 25dB gain, 0.3 to 2000MHz amplifier for less than $4.50. Design values and circuit board layout available on request.

It's just as easy to create an amplifier that meets other specific needs, whether it be low noise, high gain, or medium power. Select from Mini-Circuits' wide assortment of models (see Chart), sketch a simple interconnect layout, and the design is done. Each model is characterized with S parameter data included in our 740-page RF/IF Designers' Handbook.

All Mini-Circuits' amplifiers feature tight unit-to-unit repeatability, high reliability, a one-year guarantee, tape and reel packaging, off-the-shelf availability, with prices starting at 99 cents. Mini-Circuits' monolithic amplifiers...for innovative do-it-yourself problem solvers.

<table>
<thead>
<tr>
<th>Model</th>
<th>Frequency Range</th>
<th>Gain</th>
<th>Output Power</th>
<th>NF</th>
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<tbody>
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<td>18.5</td>
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<td>1000-2000 MHz</td>
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<td>MAV-10</td>
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<td>17.5</td>
<td>6.5</td>
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Notes:
- Frequency range DC-1500MHz
- Gain: dB at 1000MHz
- Output Pwr: +dBm
- NF: dB

Typical Circuit Arrangement

Finding new ways...
Setting higher standards...