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The Professional Radio-TVman's Magazine

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Service Encyclopedia

This new, bigger, 2nd Edition of the already popular Mallory Television Encyclopedia contains all the TV listings from the 1st Edition...plus a complete list of TV sets produced since that time...plus an up-to-date supplement for the 6th Edition of the Mallory Radio Service Encyclopedia.

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The Service Technician's Standard Replacement Authority!
ASSURES YOU the most complete tests of all tubes including television.

ACTUALLY APPLIES 19 separate filament voltages—eliminates usual compromises.

TESTS OVER 700 tubes listed on roll chart—Many thousand tubes used to properly evaluate correct settings.

POSITIVE INDIVIDUAL test of each element.

SPECIAL CIRCUIT feature accurately compensates to provide correct voltages on each tube test.

IMPROVED LEVER switching originated by Triplett for complete control of each tube element.

EACH ELEMENT quickly and conclusively tested for shorts by a flip of the switch.

ILLUMINATED SPEED-ROLL chart with latest tube listings. Kept up-to-date.

LARGE 6" meter—RED-DOT Life-time Guaranteed.

FOR COUNTER or portable use.
PRE-SELLING

THE RADIART CORP.

TELE-ROTOR
PAT'S PEND

CORNELL-DUBILIER

CORNELL-DUBILIER SOUTH PLAINFIELD, N. J.

THE RADIART CORPORATION CLEVELAND 2, OHIO
with a Startling Consumer Campaign on Key TV Stations in The Major TV Markets!

Here are more and bigger profits for everybody in the TV field! Setting sensational sales records everywhere on merit alone... NOW — watch for even BIGGER sales starting with our NEW series of announcements on key TV stations in all the important markets. These film demonstrations will reach into millions of homes... ALL YOUR POTENTIAL CUSTOMERS... telling them of the advantages and superiority of the TELE-ROTOR! These will do a PRE-SELLING job for YOU... so get set NOW... for this big business ahead... by featuring the BEST... the TELE-ROTOR.

ONLY Rotator with ALL the Important Features

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www.americanradiohistory.com
SYNC PULSES

by San D'Arcy

Radiomakers Get Ultimatum. F.C.C. Chairman Wayne Coy informed members of RTMA that unless they become more cooperative they are heading for serious trouble. It seems that, as Mr. Coy puts it, "Interference is caused in some areas and under certain circumstances by TV and FM receivers having excessive oscillator radiation." The radiation interference not only is spoiling TV entertainment for TV set owners located near unshielded sets, but in addition the interference may be affecting with deadly results commercial airlines' communications systems. Mr. Coy also contended that set makers have failed to release much valuable technical information that their work has brought to light and this contributes toward keeping the 'freeze' in effect longer than might otherwise be necessary. So, unless the radio makers correct their short-comings they may be forced to furnish an FCC transmitter license with each TV or FM set they sell, if it is to be operated near an airline communications center, and they may never get the ultra high frequencies opened, which in effect would hold down the sale potential of TV sets.

Sounds, Too Personal. Police in a New Jersey city were quite patient with an Evangelist to whom a permit for the use of a sound system had been granted even when many citizens complained about "his pious ejaculations in an extremely loud manner." But matters got past the breaking point recently when the soul-saver started pointing his finger at passers-by, at the same time yelling, "Heaven or Hell?" This was construed as being "an invasion of privacy" and the PA user was told to stop at once "or else".

HoTelevision. A financial house recently offered to sell stock in an enterprise that would enable hotels to transmit TV programs from one master control to any number of its rooms. (A dozen of the largest hotels in key cities are already using the system, and the demand for additional installations by other hotels is impressive). The stock issue was sold quickly. Seems like investors have confidence in TV's future.

TV Still Killing Laymen. Another sad TV killing has occurred in Dayton, Ohio. A 31 year old laundry owner was installing his new TV antenna. He attached the antenna to a long metal pole, which when raised, touched a 6300 volt wire with deadly results. Falling, the pole touched a metal fence, charging it. The victim's 26 year old wife, running to his aid, touched the fence and she, too, died. Three children ranging from 7 months to 6 years survive. We professional servicemen MUST do something in the way of educational promotion with the aid of our local newspapers to teach the TV set buying public not to attempt to do its own TV installation and service work because it is a dangerous and treacherous past-time that can and will kill.

RADIO-TELEVISION SERVICE DEALER  ·  SEPTEMBER, 1950
**EDITORIAL**

by S. R. COWAN

**TV Antennas Violate Laws**

Fire department heads in areas having TV are now greatly disturbed by TV antenna installations which may soon be written onto the civic Law Statutes as being violations of fire or local building safety codes, and justly so. For example, a glance at the roof-edge of almost any large apartment house will show mast after mast, each set within few feet each other. Likewise you'll see a maze of antenna arms interweaving one another so that in effect a fireman attempting to get onto a roof from a ladder has to go through a picket fence of metal poles and bars.

Studying the situation from the roof itself one sees antenna arms poking out all over, and at varying heights, with transmission lines running helterskelter, hither and yon, blocking fire-escapes and hatches. All these constitute a risk to firemen and law enforcement authorities who have the right to demand elimination of hazards which make their normally dangerous work even more treacherous.

It would seem to us that we of the service profession should establish our own code of safety ethics and abide by them before strict laws are put on the books which will force us to do what we should have done in the first place. Here's our proposal: 1) Never set a TV mast closer than 8 feet from the nearest mast. 2) Never set a TV antenna up in a place whereby the lowest arms will be closer than 8 feet off the ground to insure plenty of head clearance, even for firemen wearing helmets. 3) Never string transmission lines across roofs or open spaces unless 8 feet of head clearance is afforded. 4) Never allow transmission lines to block fire escapes or roof hatches. Or, put another way—make your installations conform to the way you'd want them to be if you were a fireman who had to get up onto roofs to fight fires, or if you were a policeman who was called upon to scramble across roofs in pursuit of law-breakers. Help the law—don't hinder it! In doing so you will at least be able to sleep nights knowing that the job you did will not cause injury to someone else.

**Extended TV Lines**

The 208 mile underground coaxial cable for TV has been completed between Omaha and Kansas City. The link between Chicago and Omaha, running through Des Moines, is progressing on schedule, too. After a short period of testing the network will go into service. September 30th is the date scheduled, Hurrah! The vast area encompassed between St. Louis, Mo., Kansas City, Omaha and Chicago has anxiously awaited this network tie-in with New York which is far and away the capitol of TV programming. To all service dealers and servicemen in the mid-west areas which will soon get TV, we say “Welcome and Good Luck!”
HERE'S YOUR REPLACEMENT

No Other Control Gives You All These

59 IRC CONTROLS WITH AMAZING ADAPTABILITY MEET ALL YOUR NEEDS WITH LESS STOCK

Compare the amazing adaptability of your IRC Q Control with any other. You'll agree no other control so closely meets all your servicing needs... no other gives you so much for your money! Feel its cushioned turn, examine its lustrous finish, study its practical design—ask your Distributor for IRC Q Controls, and you know you’re buying the very best.

INTERCHANGEABLE FIXED SHAFTS
Easy replacement of standard shaft with any of 13 special fixed shafts is made possible by exclusive IRC Resilient Retainer Ring. This revolutionary feature provides widest replacement control coverage.

WIRE WOUND CONTROLS
Dependable 2 watt controls available with center tap for TV centering. Specific TV values now available with Knob Master Shaft to accommodate both knurled and flatted knobs.
NO. 1 CONTROL

Modern Servicing Features!

- Fits both flatted and knurled knobs
- Separate switches
- Modern small size
- Fixed shaft convenience with complete shaft interchangeability
- 23 tapped types
- Shorter bushing
- Sparkling appearance
- ½ watt rating

INTERNATIONAL RESISTANCE COMPANY
401 N. BROAD STREET, PHILADELPHIA 8, PA.

This original IRC feature provides a ready solution to your special control requirements. With this kit of parts you assemble practically any concentric dual control quickly and easily. In a matter of minutes you can prove the advantages of this practical IRC feature.

INTERCHANGEABLE BASE-ELEMENTS
Principally intended for use with Concentrikit, this IRC innovation gives you limitless opportunities for adapting controls to specific requirements. Each unit includes molded base, element, terminals and collector ring—no loose parts. Available in 33 resistance values and a variety of taps.

Multisections
For standard duals, IRC Multisections are added to Q Controls like switches. 17 values provide over 11,000,000 variations of dual, triple and quadruple controls; accommodate switches, too!

INTERNATIONAL RESISTANCE COMPANY
413 N. Broad St., Phila., Pa.

Please send me additional IRC Q Control information checked below:

- Free Catalog Bulletin DC1A
- Enclosed find 25¢ in stamps or coin for comprehensive Concentric Dual Replacement Manual

Name ____________________________
Company __________________________
Address ___________________________
TRADE FLASHES

A "press-time" digest of production, distribution & merchandising activities.

2nd Phila PRSMA Exhibit

The second annual Radio, Television and Electronics Exhibit sponsored by the Philadelphia Radio Service Men's Association will be held at Philadelphia's Broadwood Hotel from September 25-27, it was announced by David Krantz, Show Committee Chairman.

Purpose of the show is to acquaint service men, dealers and others in the servicing industry with the newest developments in electronics. For this purpose, many important educational seminars and lectures will be held during the daily sessions, which will begin at 7:00 p.m., September 25 and run from 10:00 a.m. to 10:00 p.m. on September 26 and 27.

"No Parts Shortage"

"There is no immediate threat of a serious shortage of replacement parts for servicing television and radio receivers," President Robert C. Sprague of the Radio-Television Manufacturers Association said recently following a spot check in New York City where complaints of such a shortage have been reported recently.

"Distributors contacted by RTMA in New York reported that they are generally well stocked with replacement parts for TV requirements although they have had to allocate certain components because of unusual demands from dealers since the Korean outbreak," Mr. Sprague said.

"Allocations were brought on by a small minority of dealers and servicemen who were trying to hoard some of the components in short supply, he explained. Receiving tubes, resistors, antennas, television tubes, and condensers are being allocated by parts distributors at present in the New York area.

"The distributors seem to be handling a difficult situation very well and are trying to be fair in their allocation of components most in demand from dealers and servicemen," Mr. Sprague said.

"Despite heavy demands from set manufacturers who are at a peak production pace and regardless of large anticipated military requirements for electronic components, the industry by reason of its expanded capacity can keep its distribution outlets adequately supplied for any normal requirements of set servicing, both in New York City and elsewhere.

"I am confident that most dealers and servicemen go along with the distributors, trying to treat the public favorably and avoid hoarding. However, a few unscrupulous dealers, if permitted to do so, could create shortages of components whose full production is required to meet normal requirements of manufacturers and distributors."

N.Y. Offers Decal-Banner and Sign for Service-Dealer Use

National Union Radio Corporation has announced the release of a three-piece dealer sales promotion package available through N.U. distributors. This eye-catching three-piece sales-promotion package is ideal to stimulate sales during the late summer when the radio business often slows down. It includes one Giant Weather-proof Banner, size 29" x 48"; one Metal Flange Sign, size 24" x 8 1/4" and one 7 1/4" x 8" Door Decal, complete with the dealer's street number.

Town Meetings Under Way

The Town Meetings of Television Dealers, financed and sponsored by 17 leading television manufacturers and the R-TMA, is being held in 60 cities throughout the country in August, September, and October. At the meetings dealers will be shown sound slide-films designed to help them re-examine their sales, merchandise, business-management, and service practices.

"These films," Ehle declared, "embrace the best principles of good business housekeeping we can gather from all segments of the television industry. They have been examined and approved by manufacturers, distributors, and dealers, to say nothing of professional managerial experts.

"They represent, we hope, a step..."
"We doubled our store space... increased our staff"

Sylvania Electric Products Inc.
Advertising Department
Emporium, Pa.

Gentlemen:

During January, February and March I sent 12,000 postal cards to each occupant of three suburban towns, Elmhurst, Villa Park, Lombard and Countryside. I had a local letter service handle addressing and mailing at a cost of only 17¢ per card.

Business began to pour in soon after the first mailing. In January it was up 37%, February 55% and March up 78% compared to service business in similar months in 1940. Yet, service business increased an average of 38% the first three months of this year, over last.

Due to the increased business we've had as a result of your campaign mailing, we have doubled our store space, increased our service staff from two to six bench positions, and added an outside staff for antenna installations.

Just thought you would like to know! Thanks for your help in the rapid growth of "Better Radio".

Cordially,

Howard J. Wittman
President
BETTER RADIO INC.

Now let this SYLVANIA DEALER CAMPAIGN boost your business!

The above letter is actual proof of how Sylvania's Service Dealer Campaigns step up sales.

Now the new fall campaign is ready for you. It's tied in with the advertising your customers will be seeing in the Saturday Evening Post, Life, Look, Collier's and Radio and Television Best. It's sure-fire, powerful and complete...from colorful window and counter displays to bright, business-pulling postal cards...even radio spot announcements and ad mats.

All yours ALL FREE...you pay only the postage (1¢ for each card). So don't delay, mail the coupon TODAY!
ESFETA Protests Jobbers Selling at Retail

A regular meeting of ESFETA, Inc., was held on Sunday June 25th, 1950 at Bayville, Long Island. Guests in attendance were representatives of several participating manufacturers of the 1949-1950 educational lecture series coordinated by ESFETA through the local technicians organization.

There was considerable discussion held relative to the practices prevalent within the industry especially those of retail customer and distributor. After much debate the following resolution was unanimously adopted.

"Resolved: The policy of Radio Jobbers and/or Distributors to sell to retail customers at wholesale prices is objectionable. This practice deprives Technicians of their contact with a potential customer and consequently a loss of their legitimate income.

The member organizations of ESFETA representing some 3000 Radio & Television Technicians of New York State, recommend to the members of NEDA that this practice be eliminated to the betterment of relations of all groups of the Radio & TV Industry."

Doyle Resigns as Alliance Proxy

Mr. R. F. (Buss) Doyle has been associated with Alliance Mfg. Co. since its inception 25 years ago, and President of the firm since 1946, has resigned. Mr. Doyle's future business plans have not been announced as
Uniform sharpness of trace to the very edges of the screen distinguishes the new Du Mont Bent-Gun.

A higher degree of pre-focusing passes a smaller-diameter beam through the deflection field. Spot distortion is reduced and a uniform overall focus results. Other design changes are: Improved bulb spacer insures proper anode contact and electron gun centering; rounded corners on pertinent gun parts eliminates stray emission at higher anode voltages; new grid-cathode assembly allows a longer G-2 (second grid) without increasing overall length.

This new Du Mont Bent-Gun is now being incorporated in ALL Du Mont Teletrons. Therefore, whether planning a new TV receiver or modifying an old one, be sure to include the Du Mont Teletron for the best in TV pictures. Simply specify DU MONT.
NEW LOW PRICE

WORKSHOP

Single . . . Double-Stacked

plus Matching Bars

Now thoroughly proven in over 40,000 installations, the double-stack DUBL-VEE's new low price and outstanding all-channel reception is a combination you cannot match at any price. In addition, newly designed truss-angled matching bars provide extra strength and even better performance.

Write for Bulletin E

Clearer Pictures—higher gain brings in stronger signal — especially on higher channels
Clearer Pictures — narrow beam cuts down multi-path ghosts
Clearer Pictures—better impedance match on all channels maintains high signal strength
Clearer Pictures — true horizontal polarization — no out-of-phase ghosts
Clearer Pictures—no parasitic elements — all dryen
Clearer Pictures—designed by the pioneers in the antenna industry

For the new low prices on
MODEL 2VV — Double Stack
MODEL VV — Single Bay
MODEL SK-2VV — Stacking Bars

call your distributor

THE WORKSHOP ASSOCIATES, INC.
135 CRESCENT ROAD, NEEDHAM 94, MASS.

yet. However, he is still a stockholder and director of Alliance Mfg. Co.

TV Installation Book Available

TV Installation Techniques, by Samuel L. Marshall the latest publication of John F. Rider Publisher, Inc., 480 Canal Street, New York 13, N. Y., is now available at Rider jobbers.

Every man who is actively engaged in the specialized field of operation of installing television antennas and receivers, or the man who contemplates entering it, needs this text to enable himself to successfully participate.

All phases of Television installation—construction, materials, methods, locations, installations, adjustments, municipal regulations, etc., are thoroughly discussed with the graphic assistance of 270 illustrations. Equal emphasis is devoted to metropolitan, suburban, and fringe area installations.

The book furnishes installation precautions concerning wind surfaces and ice loadings, the proper means of guyings, in fact, all the factors necessary for the elimination of return calls due to improper antenna erection. It stresses the means whereby antenna installation can be accomplished in minimum time. It's a practical time-saving and money-making book from cover to cover. The text contains 336 pages in a cloth binding. It is priced at $3.90.

$50,000,000 In TV Orders

Orders for the new line of 17 and 19-inch tube Telesets totaling $51,700,000 have been placed by Du Mont distributors for fall delivery according to Walter L. Stickel, national sales manager of Allen B. Du Mont Laboratories, Inc.

New Booklets

RCA Receiving Tubes for AM, FM, and TV Broadcast (revised)—Provides quick and easy reference to the characteristics and socket connections for more than 450 RCA receiving tubes and picture tubes, including more than 50 new tubes.

The new RCA Receiving Tubes Booklet (Form 1275-E) can be obtained from RCA Tube Distributors, or by sending 10 cents to Commercial Engineering, RCA Tube Department, Harrison, N. J.

You Don't Have to be a Recording Expert—How sound recording tape works; provides suggestions on care and use of sound tape; describes techniques of erasing and splicing tape. Minnesota Mining and Mfg. Co., 900 Fauquier St., St. Paul 6, Minn.
Here are some of the many reasons why there are more Simpson 260 high sensitivity volt-ohm-milliammeters in use today than all others combined. The Simpson 260 has earned world-wide acceptance because it was the first tester of its kind with all these "Firsts":

Simpson 260 SET TESTER
WORLD FAMOUS FOR ALL THESE "FIRSTS"

- First high sensitivity instrument to use a metal armature frame.
- First to use fully enclosed dust proof rotary switch with all contacts molded in place accurately and firmly.
- First to do away with harness wiring.
- First to provide separate molded recesses for resistors, batteries, etc.
- First to cover all resistors to prevent shorts and accidental damage and to protect against dust and dirt.
- First with a sturdy movement adapted to the rugged requirements of a wide range of service work or laboratory testing.
- First to provide easy means of replacing batteries.
- First to use all bakelite case and panels in volt-ohm-milliammeters.
- First volt-ohm-milliammeter at 20,000 ohms per volt with large 4½" meter supplied in compact case (size 5¼" x 7" x 3½").
- First and only one available with Simpson patented Roll Top Case.
- First to provide convenient compartment for test leads (Roll Top case).
- First to offer choice of colors.

The Model 260 also is available in the famous patented Roll Top safety case with built-in lead compartment. This sturdy, molded, bakelite case with Roll Top provides maximum protection for your 260 when used for servicing in the field or shop.

RANGES
20,000 Ohms per Volt DC, 1,000 Ohms per Volt AC
VOLTS: AC & DC—2.5, 10, 50, 250, 1,000, 5,000
OUTPUT: 2.5, 10, 50, 250, 1000
MILLIAMPERES, DC: 10, 100, 500
MICROAMPERES, DC: 100
AMPERES, DC: 10
DECIBELS: (5 ranges)—12 to +55 DB
OHMS: 0-2,000 (12 ohms center), 0-200,000 (1200 ohms center), 0-20 megohms (120,000 ohms center).

Prices: $38.95 dealers net; Roll Top $45.95 dealers net.

SIMPSON ELECTRIC COMPANY • 5200-18 W. Kinzie St., Chicago 44, Ill. • In Canada: Bach-Simpson, Ltd., London, Ont.
RADIO-TELEVISION SERVICE DEALER • SEPTEMBER, 1950
NOW! A FULLY AUTOMATIC ANTENNA ROTATOR BY ALLIANCE

The New HIR

with The Most Accurate Indicator On the Market!

JUST SET THE POINTER AND FORGET IT!

• AUTOMATIC — the new deluxe model HIR Alliance Tenna-Rotor is fully automatic! The antenna turns to any setting on the dial and stops.

• FASTER INSTALLATION — the only rotator where no orientation of antenna is required. Has special "Zip" feature—4-conductor cable.

• NEVER OUT-OF-DATE — station selector dial is eraseable. May be marked for present or new channels at any time by viewer.

• MOVING MYSTIC LIGHT — light moves along dial—shows position while antenna rotates. Pointer indicates antenna direction at all times!

Alliance Manufacturing Co.
Alliance, Ohio
Export Department: 401 Broadway, New York, N. Y., U. S. A.

And remember! Only ALLIANCE delivers a national TV campaign to five million viewers around 60 stations.

• Has more than 250,000 users
• Comes with special "Zip" feature 4-conductor cable.

The famous Model DIR also available with handy — North — South — East — West indicator. Approved by Underwriters' Laboratories — guaranteed for one year!
Mechanical Features of Tape Recorders

by C. A. TUTHILL

Good judgment will prompt private owners as well as operators of commercial tape recorders to become thoroughly familiar with the vital mechanical features of their machines. Since they are machines, and must be well built and maintained mechanically, details will be given here for the benefit of servicemen heretofore mainly versed in the circuit servicing of radios. In some cases discussion will pertain to a specific construction so as to effect a thorough coverage. Good design offers all components readily accessible. Quiet mechanical operation is essential. Certain basic requirements of all tape recording machines are:

1. Stability - A steady state of speed, free from vibration, is vital to all recording machines as regards flutter and pitch. Load variations due to the use of large and small tape reels, or temporary friction from bent or warped reels, require adequate drive motor and capstan action to counteract resultant drag. Heavy duty induction motors, designed for constancy of speed over a wide range of voltage variations, are frequently used. Filtering mechanisms are sometimes inserted between motor and capstan to minimize speed variations. Generous flywheels replace the heavy platters of disc machines.

2. Alignment - Constancy of alignment of the entire tape width across the recorder and reproducer poles is necessary as a function of response. When one edge of either the gap or the tape is displaced, even a few thousands of an inch, from its proper position, high frequency response will fall off.

3. Constancy of Takeup - A pressure roller and motor-driven capstan jointly serve to pull the tape toward the takeup reel at consistent and proper speed. A belt and pulley assembly or a dry-slipping clutch generally drives the takeup reel which actually is engaged by a friction-drive disc or washer to allow for slippage as the tape load circumference varies. Takeup tension should be great enough to wind the tape evenly upon the takeup reel yet not great enough to drag the tape past the capstan beyond the desired rolling speed.

Several commercial treatments of tape handling are described under the heading Tape Threading and Rewind. Takeup components are detailed under Mechanical Construction.

4. Shock-proof Mounts - Freedom from vibration is essential to any recording machine. Protection against building rumble or local vibration is gained through mounting plate shock-mounts such as the Twin Trax example illustrated in Fig. 1. Rubber grommet motor mounts (P 123) and rubber drive roller (A 181) of the Pentron recorder are shown in Fig. 2. This rubber drive roller is carefully designed to minimize any movement of the capstan, drive motor, or takeup reel which might result in tape slippage or rumble.
Fig. 2. Rubber grommet motor mounts and drive roller of pentron machine.

Fig. 3. Exploded view of Ampro Model 730 recorder.

adjusted for a firm contact with the main flywheel of the mechanism. Precision-ground rubber contacting surfaces are a must. Excessive pressure may prevent the motor from starting while insufficient pressure results in slippage and wows.

Mechanical Construction

Typical construction of a portable tape recorder, selling for less than $100. is detailed in the exploded view of the Ampro Model 730, Fig. 3. Major components are identified. For reasons of simplicity, some spindles, washers and screws have been deleted. It is at once obvious that, if caution be taken while dismantling for repair, much time and labor will be saved during re-assembly. Lay the parts out consecutively, as removed, upon a clean hard cloth.

The item number headings which follow correspond to the numbers given in Fig. 3.

Item #5 - Control Panel and Guard - This plastic control panel (3) is slotted for tape threading since it covers record and erase heads and their associated components. It is held in place by three Phillips head screws and is readily removed. An input jack in its center connects to microphone or other source. Four control knobs across the panel face control, (a) amplifier; (b) play-record-microphone switching; (c) volume control and (d) motor from left to right in that order. The larger holes above the threading slot house recording level and amplifier neon indicator lamps (#25 in amplifier ass'y).

Item #58 - Pressure Roller Bracket Ass'y - This bracket is adjusted to allow pressure roller (54) to turn freely. The pressure pads (48 and 49), for record head and erase head, are aligned to enter the slots in the heads. These pads are adjusted to bear firmly upon the proper surfaces of the heads in such manner as to obtain proper contact and alignment between the recording tape and the heads. This is accomplished by a cam-operated lever assembly which is brought into action the instant the drive motor is switched to "On". One single knob performs the double-function. At once it starts the motor and swings pressure pads (48 and 49) into normal operating position. This introduces a load upon the motor, thus, uneven or jerky tape transport and possible tape damage is avoided.

When worn down to a thickness of 1/16" these pads should be removed, using Petroleum Naptha (140-210°F) as a solvent. New pads are installed by using MMM cement (#EC-104) as a retainer which must be allowed to dry thoroughly before resumption of operations. The edge of the pads must be kept parallel to the edges of the pad brackets (47) and the ends of the pads must be flush with the ends of the brackets.

During disassembly or reassembly, care must be taken to avoid injury to the lightly constructed components. For example, - the pressure pads must introduce a proper degree of pres-
Sure against the recording head and such control has been pre-determined at the factory. When spring tension is altered, due to bent springs or some other fault, correction is necessary prior to satisfactory operation. This points out the need for care when heads and pads are cleaned with cloths.

Proper alignment during reassembly must be reestablished. This applies not only to parts associated with tape travel but also to all mechanical components throughout the mechanism. Detent and lever actions offer continual mechanical resistance to changes constantly made during normal operation. Therefore, the top panel knobs controlling such action must be tightly screwed to the flats of their shafts.

When the recorder is inactive, the motor control must never be left “On” or a dimple will develop in the pressure roller and cause "wows" during reproduction. The manufacturers of the above equipment call attention to the following:

Tape recorders will be turned over to servicemen for one of three reasons: (a) unsatisfactory performance due to operational errors; (b) periodic inspection and maintenance, or, (c) unsatisfactory performance due to wear or failure of components.

Dirt is the cause of many irregularities. Therefore all parts in the path of the tape should be cleaned with a hard cloth dampened with carbon tetrachloride before attempting inspection or test of the equipment.

 Owners have been instructed not to lubricate this machine but instead to refer to the service technician for this service which should occur only on an annual or 500 operating-hour basis. Only pure mineral instrument oil and light graphite grease should be used and then sparingly. Details are given in the Instruction Manuals where trouble shooting tables are included. It should be remembered that this is a dual track device. Considerations therefore apply which were given concerning the Twin-Trax machine in Radio Service Dealer issues of May and June 1949.

**Recorder Head Assembly**

In Fig. 4, we see details of relationship between the Pentron recording head (A-106) and erase head (A-107) as regards tape guide and pressure facilities. For clarity, the heads are shown lowered from their operating positions. By means of screws in slotted holes in the head bracket, both heads are adjusted to enter into the tape guide block (A-103) until the pressure pads within the block (A-108) are depressed slightly less than 1/32 inch. Again this adjustment is pre-set at the factory and will persist during normal operation.

Tape pressure pads (A-108), within the tape guide block (A-103) are pressed downward by phosphor bronze springs (A-104). These springs exert a pressure of 30 grams for each head when the recording tape is in operating contact. Too great a pressure at this point will create flutter. Correc-

of reels. A tape record library is liable to be stm by loosening the screws holding the head-mounting bracket so that the head may be lowered slightly. Care must be observed to disturb alignment of the recording head.

Final head adjustment is made by slowly turning the head until the air gap in its lamination or shoe is exactly at right angles to tape travel. This is best accomplished by playback of a constant level 3000 cycle tone record. The head is rotated for maximum response on an output meter and then locked into place by screws.

An open-circuited head must be replaced. Worn or damaged laminations (P-127 or P-128, Fig. 4) can be replaced. First, release the holding screws whereupon the two heads and bracket plates are released on one unit. Next, carefully pry out the laminations with a screwdriver. Then, new laminations can be pressed in with one's fingers until the laminations come up solidly against a bottom yoke. Care must be taken to have the steel portion of each lamination uppermost in the tape guide when the machine is in normal operating position.

**Takeup Mechanism**

The takeup pressure lever (A-113, Fig. 4) is normally set so that it is vertical when the control knob is in “Play-Record” position. Under this condition the arm adjusting plate (M-105) is set so that it clears pressure arm (M-104) by 1/64th inch. When the control knob is turned from “Off” to “Rewind”, this machine has a rewind ratio of 20 to 1 against its recording speed of 7½ inches per second.

Takeup mechanisms should provide for interchangeability of various types.

[Continued on page 33]
The Synchroguide system

The most widely used and most economical system of AFC is the synchroguide system, often called a pulse-width type of AFC. The synchroguide circuit does not operate on the same principle as the Synchrolock or the phase detector but the main elements of a frequency comparing feature, an error voltage and an oscillator which is controlled by it, are also found in the synchroguide.

In the circuit of Fig. 9, the 6SN7 shown at the right is both the oscillator and the control tube. The triode section containing T1, is a blocking oscillator circuit, generating a square and sine wave combination which is converted into a sawtooth through the R-C network R12, C14, C15 and C9. T1 is a tapped coil and in some older receivers the winding from C-D is lacking. This coil was inserted after it was found that the circuit had a tendency to be unstable and the main function of this inductance is to stabilize the circuit. The frequency of the oscillator depends mainly on the inductances in T1 and the grid bias across R7. It will be noted that the grid of the oscillator is returned to a tap on the cathode bias resistor of the control tube. At the same time a portion of the oscillator grid bias is applied to the grid of the control tube through R5. Since the oscillator grid bias is a relatively large negative voltage, this will tend to keep the control tube cut-off for anything except strong positive signals. A large cathode bias on the control tube helps further to keep this triode section cut-off.

The frequency comparing action of the control triode depends on three different voltage waves, similar in appearance to the wave shapes shown in Figs. 7 and 8. The sawtooth wave is coupled from point D on T1 through R11 to point (I). The synchronizing pulse comes from the synch clipper and amplifier through C3 and a small additional pulse is fed back from the plate of the damper tube through R16 and C12. The result of all three pulses is the wave shape shown in Fig. 10. The control tube is at such a high bias that only the small positive pip on top of the wave makes the tube conduct. If this pip is broad, current passes for a longer time than if the pip is a very sharp point. The current passing through the control tube determines the cathode bias developed across R6 and R8 and filtered by C6 and the combination C5-R4. As we mentioned above, one half of the control tube cathode bias is applied to the grid of the oscillator tube and this is in effect the error voltage. Even a slight variation in bias will influence the frequency of the oscillator. The horizontal hold control R14 is part of a B plus voltage divider and sets the plate voltage for the control triode. The plate voltage determines
the operating point of this tube as well as the amount of current and thereby controls the cathode bias, which in turn is the error voltage.

Consider the voltage wave at point (1) in Fig. 9, again. If the synchronizing pulse would occur just before the steep portion of the sawtooth, the pip on top would obviously be broader. If the synchronizing pulse would occur slightly later, only the narrow feedback pulse from the damper tube would be perched on top of the sawtooth and this would mean a shorter current passing interval at the control tube. The appearance of the pulse pip is controlled by C13, usually labeled "Lock-In Range" control. This trimmer is part of the capacitive voltage divider C1 and C12, and determines the pulse height and width. Once this adjustment is made it need not be touched unless major circuit changes are required. After the pulse width for normal operation is set through the adjustment of C13, the two separate windings in T1 must be adjusted to oscillate at the proper frequency. If, for some reason the frequency of the oscillator changes slightly, the width of the pip on top of the sawtooth wave appearing at point (1) will vary. A variation in pulse width at the grid of the control triode results in a variation of the cathode bias of this tube. This cathode bias is actually the error voltage which controls the speed of the oscillator through R7, the grid resistor of the oscillator triode.

**Synchroguide Operation**

As example for the operation of the synchroguide circuit consider the case when the oscillator seems at a lower frequency. The synchronizing pulse will occur slightly before the feedback pulse which will effectively broaden the pip. A wider pip results in longer conduction through the control tube and in a higher cathode bias. A higher cathode bias is equivalent to a more positive error voltage which means a reduction of the negative bias on the oscillator grid. Reducing the negative bias on the oscillator grid has the effect of increasing the oscillator frequency, bringing the oscillator back to the proper synchronizing pulse speed. Because of the pulse width feature, the synchroguide is effective only when the natural frequency of the oscillator is the same as that of the incoming pulses. The adjustment of C13, the Lock-In trimmer is also quite critical, since it sets the level of the controlling pulse and if the pulse is too small the error voltage developed will be insufficient to control the oscillator. If, on the other hand, the pulse is too strong, the error voltage will overcompensate, which also results in unsatisfactory performance.

The range of the hold control depends on the voltage across R14, and usually permits only a slight variation of the plate voltage of the control tube. In normal operation at mid-point setting the synchroguide will lock-in instantly when channels are switched. At either extreme setting the picture will not lose sync while the signal remains constant, but when stations are changed, synchroinism may be lost. The horizontal drive trimmer acts in a manner similar to that in the phase detector and also influences the frequency of the oscillator somewhat.

Two different methods of adjustment are in use and either may be followed successfully. One method requires an oscilloscope and this is the more thorough approach. Usually the oscilloscope method is used only when a major repair has been made and T1 must be completely re-adjusted. In using the oscilloscope a 10,000 ohm decoupling resistor should be connected in series with the "hot" side of the 'scope to avoid detuning the circuit with the 'scope input capacity. Below is a suggested procedure for aligning a synchroguide AFC system with an oscilloscope.

1. Set oscilloscope to approximately 15 kc and connect probe through 10,000 ohm resistor to last video amplifier. Adjust scope to give two cycles of synchronizing pulses.

2. Connect 'scope probe through the same resistor to point (1) in Fig. 9. Adjust the slug which tunes coil A-F until two sawtooth waves appear and stand still. Adjust C13 to give a curve like the one shown in Fig. 10. Readjust the slug if necessary.

3. Set the horizontal hold control to approximately center and adjust C14 for maximum width and brightness. Retune T1 to obtain a locked-in picture and a 'scope as in Fig. 10.

4. Short antenna terminals and connect 'scope lead to point C on T1. Adjust the slug of coil C-D for a pattern as in Fig. 11. Make sure a symmetrical sine wave appears between the sharp portions of the curve.

5. Remove the oscilloscope lead, connect antenna properly and check.

[Continued on page 39]
Recent engineering advances and production economies have enabled RCA Victor to actually improve performance while reducing prices in the development of its new "Million Proof" line of television receivers and TV-radio-phonographs.

Use of improved and simplified circuits with new types of tubes and components has made practical a chassis with almost 30 per cent fewer parts and 20 per cent fewer connections, and one that consumes almost 50 per cent less power than previous models. Yet the new receiver is more powerful, more sensitive, and has a better signal-to-noise ratio and more sound power output than similar previous models.

Because the kinescope is mounted in the new chassis before shipment, and because picture centering controls have been simplified and the focus control made more accessible, it has been possible to reduce installation set-up time as much as 25 per cent.

These television chassis have also been designed with the serviceman in mind. All of the parts and connections are easily accessible. Many service jobs may be performed without taking the chassis out of the cabinet. For instance, the horizontal oscillator adjustment is now in a more accessible location, right at the back of the chassis. The new focus control is within easy reach, so that the adjustment can be easily made. The new type of picture centering control sets a new standard for ease of operation. The self-centering kinescope mask has a new dust seal. This will prevent dust from collecting between the kinescope face and the safety glass and eliminate the need to remove the kinescope in order to clean the inside of the glass.
The high sensitivity of the new chassis is due partially to use of the new 6CB6 tube in the r-f and picture i-f stages. This tube, with its inherently higher gain, permits the reception of weaker signals than ever before. The picture i-f band width remains exceptionally wide, insuring excellent picture detail.

The receiver input circuits are very well balanced, which helps to prevent ghost signal pickup on the antenna transmission line from causing interference. The r-f unit is exceptionally well shielded. This, together with other design factors, insures an extremely low r-f oscillator radiation, reducing to a minimum the possibility of interference with other nearby sets which may be receiving weak signals.

A highly efficient "direct drive" horizontal sweep output deflection system provides greater deflection and more high voltage, with fewer circuit components and less power consumption than previous systems.

All receivers have built-in antennas, either in the cabinet itself or in a stand designed for use with some table models.

It will be noted that throughout the chassis, while circuits have been simplified, making the servicing job simpler and faster, at no point has any sacrifice in quality been made. Although some circuits have been eliminated, the new chassis is actually superior to excellent chassis of earlier design. The new receivers represent a combination of three vital ingredients: the endless research and study of RCA engineers, high manufacturing quality standards, and invaluable information from the field. They are literally "Million Proof," because they are backed by the experience gained with more than a million RCA Victor home television receivers.

Fig. 6. The provision of an extension on the vernier focus control enables the serviceman to make adjustments while simultaneously checking the raster on the television screen. The vernier control covers a wide range, even under extreme line-voltage variations.

Fig. 7. The new and simplified centering vernier adjustment of the "Million Proof" chassis is a simple two-way lever that can be adjusted and locked in less than half the time normally required with standard adjustments.

Fig. 8. Another feature of the "serviceman's dream chassis" is the new wide-range width control which permits definite adjustment for full picture width, even under wide variations of AC line voltage. It, too, is easily accessible for rapid adjustment.

Fig. 9. The "Million Proof" chassis also features a fool-proof switch for automatic gain control. The switch controls three degrees of AGC action and will enable the serviceman to set the AGC for peak performance for a specific location.

Fig. 10. Indicative of the "keep-the-serviceman-in-mind" theme which underlined the development of the "Million Proof" chassis is the simplification of RF oscillator adjustments, the majority of which can now be made at the front of the set, via the channel selector switch. The formula is simple. Remove the escutcheon from the selector switch and flip the channel selector to the channel to be adjusted. The masking guide will automatically guide the serviceman to the proper adjustment.

The "Million Proof" chassis is a simple two-way lever that can be adjusted and locked in less than half the time normally required with standard adjustments.
LOOKING FOR Trouble?

by Cyrus Glickstein

(American Radio Institute)

Presenting a unique type of trouble-shooting article which attempts to go through the actual steps of servicing a TV receiver. This technique is designed to maintain interest while demonstrating and explaining actual service problems and principles. A number of these are planned for the future.

HOW good are you at finding trouble when you go looking for it—in TV receivers, that is. Here's your chance for a quick check.

We're going to start with a trouble in the old standby—RCA 630—and go through the actual steps of servicing the set on the bench. You can follow along and contribute your opinion each step of the way.

Each question should be answered before going on to the next since some questions are given away in the following question. Answers and discussion follow the completion of these questions.

1. The first step in trouble-shooting teletsets is generally to turn the set on and check the information present on the screen and coming from the speaker. The next step is usually manipulating appropriate controls to check if there is actual trouble or just misadjustment of controls or switches.

With a blank screen and normal sound, the most important control to check first would be: (Check one of the following)

- Fine tuning
- Horizontal drive
- Contrast
- Brilliance

2. The brilliance (brightness) control was varied through its entire range, after the contrast control was set at maximum. Rotation of the brilliance control gave a very dim picture at one point only—about 34 of maximum. All other points gave a blank screen. At the setting where the picture was visible, it did not fill the mask horizontally. Right side of the picture had a bright line (fold-over) and ended 3 inches short of the right side of mask. Variation of horizontal drive control made picture disappear.

On the basis of screen and speaker information plus the data from manipulating controls such as mentioned above, the next step in trouble-shooting is to decide in what section or sections the trouble is most probably located, in order to make a further check there. In the basis of the above information, the fault most likely is in: (Check one of the following)

- Brilliance control and/or CRT circuit
- High voltage circuit
- Horizontal sweep circuit
- Low voltage system

3. All tubes in the horizontal circuit including the horizontal output tube, 6BG6, the damping tube, 5V4 and the high voltage rectifier, 1B3 were changed. No improvement.

The schematic of the set was referred to: Fig. 1

Since a scope was handy, the following waveform checks (Fig. 2) were made at the indicated points and compared to the correct wave shapes given in the manufacturer's service manual:

On the basis of comparing the observed with the normal waveforms, the trouble apparently is located between the following points: (Check one of the following)

Only 75¢! You cannot afford to be without this temper-time-and-money saver. Get your Hytron Tube Pullers from your Hytron jobber today.

**It's Easy! TO PULL:** Push Tube Puller onto top of 7-pin miniature. Just enough for firm grip, and without depressing release button at top. Pull straight up and out; no need to bend pins by violent rocking. Hold tube securely in one hand. With other, push release button quickly. Compressed air pops out tube. Or, holding down release button, remove Tube Puller by rocking it. To insert: Align arrow on skirt of Tube Puller with keyway of tube. Push tube into Tube Puller. Using arrow as guide, insert tube. Push button quickly to release. Maintain pulling action at peak. Wipe inside of Puller occasionally with clean cloth to remove dirt and grease.

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**PIN STRAIGHTENERS, 7-Pin and 9-Pin — 55¢ net ea.** You merely press tube gently into Hytron Straightener until button base seats squarely. Premo, pins are straight! Fast ... safe. Avoiding one broken tube pays for Straightener twice over. Precise, stainless-steel insertion die. Comfortable knurled aluminum holder. For hand, bench, or tube tester use.


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**TUBE TAPPER — 5¢ net.** Handy combination pencil, eraser and tube tapper. Discovers microphonism, shorts, and opens in tubes, etc. Compact, non-metallic, rugged. Doubles in brass for writing orders, etc.
a. Plate of the Horizontal Oscillator and Grid of Horizontal Discharge tube
b. Grid of Horizontal Discharge and Plate of Horizontal Discharge tube
c. Plate of Horizontal Discharge tube and grid of Horizontal Output tube
d. Grid of Horizontal Output tube and screen of Horizontal Output tube

4. Voltage readings were taken around the Horizontal Discharge tube circuit, V120-B, 6SN7GT, with a VTVM. The following readings were noted: (and compared to values on schematic—Fig. 1 (B+ = normal)

6BG6 Screen Grid -20 K
Control -500 K
Cathode -100
6SN7 Plate -20 K
(Hor. Dis.) Grid -250 K
Cathode -0

These readings can be checked against schematic—Fig. 1.

What's the Trouble? (Check one of the following)

a. Plate resistor R-204 shorted across or greatly reduced in value
b. Coupling condenser C-178 shorted
c. Sawtooth condenser C-179 shorted
d. Coupling condenser C-178 open

ANSWERS & DISCUSSION

Answer 1.—d:

Discussion

Brilliance control should be turned to maximum first to make raster visible, if present. Raster should be visible under normal operation even if contrast control is all the way down, if brightness control is at maximum. Turning up contrast control is for the purpose of bringing in picture information. Horizontal drive control has only a small effect in varying brightness. If sound is normal for a given channel, fine tuning adjustment can only detune sound and have little effect on unblinking screen.

Answer 2.—c: Discussion

Picture that is dim at one point and blanked out at other points of brilliance control rotation can be caused by a defect in any of the following circuits: CRT, high voltage, horizontal sweep. However, the additional fact of foldover along the right edge usually points to trouble originating in the horizontal sweep circuit. That is, a non-linear horizontal sawtooth of low amplitude could cause both low high voltage foldover.

In normal operation, when brilliance is turned all the way up, picture blooms (expands) as it brightens. This is due to more current through the CRT because of reduced bias; more current through the large filter resistor, (R-235, Fig. 1) 1 megohm, in the high voltage system reduces the high voltage; sweep currents through the deflection coils therefore have more effect on the slower moving beam; and since deflection sensitivity is increased, the picture is larger. In this case, increasing the brightness control beyond the one critical point produced more current through the CRT and evidently reduced the already low high voltage to the point where there was no visibility.

Answer 3.—b: Discussion

As usual in all methods of isolating trouble, the defective stage is between

[Continued on page 35]
In the last installment (July, 1950) we made mention of stagger tuning as one of the methods of obtaining wide band frequency response in Front Ends. We also illustrated how this was done by means of a block diagram and a hypothetical example. Figure 3-18 illustrates a simplified circuit diagram of the stagger-tuned r-f stages employed in the General Instrument Model 44 Electuner. Connections are shown for high band operation. In both high and low band operation the plate circuit of the 1st r-f amplifier provides the low frequency stagger component, and the plate circuit of the second r-f amplifier provides the high frequency stagger component. A sketch of a typical r-f pass band for this unit is shown in Fig. 3-19. If an r-f sweep input is applied to the antenna terminals and an oscilloscope connected to the point marked “scope” as shown in Fig. 3-18 the resultant overall response will appear as shown in Fig. 3-20.

Referring again to Fig. 3-18, L61 and L63 are the high frequency r-f transformers, $C_{44}$ and $C_{45}$ are conventional trimmers, $C_{41}$ and $C_{42}$ are the first and second sections of a 3-gang tuning condenser, $C_{25}$ and $C_{26}$ are fixed ceramic condensers which are connected in series with the tuning condensers during high band operation.

In practice, $C_{44}$ staggers the response characteristic toward the pix carrier, and $C_{45}$ staggers the response towards the sound carrier. This adjustment is made on Channel 13. Channel 7 tracking is accomplished by adjusting coils L61 and L63. Similarly, tracking of the low frequency channels is done by adjusting the additional coils switched into the circuit during operation on Channels 2 to 6. For purposes of simplifying the ex-
Conversion of TV Signal

The purpose of the converter (mixer) and oscillator in a TV receiver is similar to that in an AM or FM receiver, that is, it reduces the incoming r-f signal to a lower (intermediate) frequency called the i-f. This is accomplished by combining or mixing the incoming r-f signal with another signal of a higher frequency locally produced in a separate r-f oscillator stage. (See RSD June 1950, Page 19, Fig. 3-1)

The wide range of frequencies (6 me) contained in any one TV channel must also appear in the plate circuit of the converter as part of the i-f signal. It would be appropriate at this point, therefore, to examine the frequency distribution of the signal before and after conversion.

Referring to Fig. 3-21, we observe the waveform of a typical r-f signal (Channel 4) as it enters the converter. The oscillator frequency must be equal to the sum of the video r-f carrier frequency (67.25 mc) and the video i-f carrier. Thus, assuming a video i-f carrier frequency of 25.75 mc, the oscillator frequency would have to be: 25.75 + 67.25 = 93 mc

When this frequency beats against the sound r-f carrier (71.75 mc) the resulting sound i-f carrier frequency becomes:

93 - 71.75 = 21.25 mc

The waveform of the signal in the plate circuit of the mixer appears as shown in Fig. 3-22. Notice that in comparison with the waveform at the grid or input (Fig. 3-21) the sound carrier is now lower in frequency than the video carrier.

As the receiver is tuned from channel to channel the oscillator frequency changes in step with each new r-f band, producing the same i-f frequency. Thus, referring to the table in Fig. 3-23, we observe that no matter what channel is tuned in, the video and audio i-f carriers remain the same: 25.75 and 21.25 mc respectively.

Converter Requirements

A good converter must provide high conversion gain, low input and output values of tube capacitance, and a high signal to noise ratio. High conversion gain and low input and output values of tube capacitance are obtained with specially designed tubes such as the 6J6, 6AG6, 6CB6, 7FS, etc. The use of triodes of the 6J6 type or pentodes of the 6CB6 types depends on the particular preference of the designer. While triodes have better noise characteristics, pentodes do not require neutralization, have somewhat better gain, and are more stable in operation.

Better signal to noise ratios, whether sought in triodes or pentodes, may be realized by operating these tubes at relatively low plate currents, and by keeping the signal injected by the oscillator at a reasonable value. As an example, General Instrument Corp. specifies 2 volts at the “Looker Points” if its Electuner (Fig. 3-18) measured with a Voltohmmyst through a 10,000 ohm resistor.

Fig. 3-23: Frequency relationships of Pix and sound carriers in r-f and i-f stages.

Coupling between the converter and the oscillator may be capacitive or inductive. Capacitive coupling is usually effected by means of a small capacitor of 1 or 2 uuf, although sometimes a gimmick, or even the capacity between wiring and components, is used to wholly or partially effect the desired energy transfer between oscillator and converter. If inductive coupling is used the oscillator and r-f coils may be wound on the same form, or near enough to each other for magnetic coupling to take place. A link winding may also be used between the mixer and oscillator circuits for this purpose as employed in the RCA 650 TS.

Converter Output Circuit

The output circuit of the converter depends on whether the receiver is of the split-sound or intercarrier type. It must be recalled that in a split-sound receiver the sound and i-f signals are separated at the output of the converter; this separation, in an intercarrier receiver, takes place at the output of the video amplifier. For example, in the simplified circuit of the Standard Tuner Model
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TV-101 shown in Fig. 3-24, L2 and C15 constitute a combination sound trap and take-off coil - as used in split-sound receivers, and is tuned to 21.25 mc, the sound i-f carrier. This permits the sound signal to pass into the sound i-f section and at the same time keeps it out of the video i-f section. Coil L2, which is tuned to 21.8 mc is designed to accept the very high video modulating frequencies, which will be recalled from Figs. 3-21 and 3-22, extend toward the sound carrier. The manner in which the i-f section tunes in the full video range will be discussed in a later installment.

Some receivers do not take off the sound in the mixer plate circuit but do this in the plate circuit of the following i-f stage. Thus, the Westinghouse Model A 196, which is a split-sound receiver, employs an adjacent channel sound trap, L2-C15 in the plate circuit of the converter as shown in the partial schematic of Fig. 3-25, and takes off its sound signal in the plate circuit of the following video i-f stage.

Most commercial Front Ends can easily be used with split-sound or intercarrier receivers. Thus, referring to the Standard Tuner again, if we wish to use this Front End in conjunction with an intercarrier receiver we merely:

1) Disconnect the green lead from the trap on L12.

2) If a 21.25 mc trap is not required in the first i-f transformer, remove C15 (68 uuf condenser). If a 19.75 mc trap (adjacent channel video carrier) is required, replace C15 with an 80 uuf condenser.

3) The 6AG5 then becomes the 1st intercarrier i-f amplifier.

### A Popular TV Oscillator

Although a number of oscillator circuits are used in TV, the greater majority of modern receivers employs some form of modified Colpitts circuit utilizing a triode, so that our discussion will be principally confined to this type of oscillator. A basic Colpitts circuit is shown in Fig. 3-26, and operates briefly as follows: A properly phased feedback voltage is developed across C2 which excites the tuned circuit comprising Lr, C1, and C2. Energy from the tuned circuit is amplified by the tube, and the feedback cycle is repeated. Condenser C2 and resistor R4 provide the necessary "C" bias for the tube for proper operation as an oscillator.

Referring to Fig. 3-27 which is a simplified version of the oscillator circuit employed in many G.E. receivers, we find that Lr is the oscillator tuning inductance, Ls is a cathode choke which isolates the cathode from ground and maintains its r-f potential above ground. Without this choke, the feedback circuit represented by C4 would be short-circuited and no oscillations would take place.

Capacitor C5 is a by-pass condenser between plate and ground. C1 and C2 shown in the basic Colpitts circuit (Fig. 3-26) are replaced by C6 and C7, the equivalent grid to cathode and plate to cathode interelectrode capacitances within the tube.

### Temperature Compensating

Notice that an additional capacitor, C6, is connected across the oscillator tuned circuit. This is a temperature compensating capacitor with a negative temperature coefficient characteristic. The latter is made necessary by the slight increase in capacity taking place in the various oscillator components because of their temperature rise. If left uncompensated for, this increase in capacitance, though small, [Continued on page 36]
Western Auto D 2919—Instability and Distortion on F. M.

It is a good idea to first follow the service data given in Rider's manuals of replacing condenser C-29 with a larger unit and adjusting length of leads as described. This improves performance considerably especially in strong signal areas but where signal is weak there is still noticeable distortion caused by regeneration. We have found that by replacing condenser C-2 with about a 250 µf unit instead of the 10 µf used in the set has increased the gain and stability of the set remarkably. This condenser is used to couple the 300 ohm antenna to the Ant. coil. We arrived at the 250 µf value by playing the set on a weak station and using an outside antenna, we shunted the 10 µf condenser with different size mica units until we had the best reception. This value might not be the right value for all sets of the same model, but should be found experimentally using, if possible, the antenna and leadin to be used with the set. This set had been returned to the factory for adjustment and when it was returned was no better than before. We drew the sweat provoking job of making it play right.

Submitted by:
Wayne E. Lemons
Buffalo, Mo.

Westinghouse Model H-216—Picture Distortion Due to Magnetism

If a strong magnetic field is brought near the 16A4 cathode ray tube, the metal cone of the tube can be magnetized sufficiently to cause objectionable distortion of the picture. The primary indication of this type of distortion is a kink in the edge of the raster.

Close contact of the tube's metal cone with any strong magnetic field must be avoided. The most likely cause of cone magnetization is contact of the metal cone with the frame of a PM speaker. Magnetized sections near the middle and small end of the cone produce the most disturbance. The magnetism is usually localized and can be detected with a pocket compass.

A magnetized cone can be demagnetized by the use of the AC magnetic field produced by a simple coil.

Such curlers are about 3 inches in length and sold at the dime stores.

Submitted by:
H. Leeper
Canton, Ohio

Cleaning Volume Controls

In many instances a radio receiver has a special volume control which is difficult, if not impossible, to get, and the control is stiff, sounds harsh, makes static.

There's a way to stop this. Take the control completely apart if possible, removing the shaft by prying the "cw" washer out of the shaft slot with a small screwdriver and a pair of needle-nose pliers.

Now, put a piece of clean, thin cloth over the end of your little finger, apply a small amount of lubricate to the cloth, and run it back and forth along the carbon strip several times. This way you will remove all loose particles of carbon which are causing the noise in the control.

A reasonable amount of care must be exercised in cleaning the carbon strip. Too heavy a pressure will remove too much of the carbon surface, affecting the control's efficient operation and attenuation.

Before re-assembling the control clean the shaft, contacts and the contact ring, putting a touch of lubricate on the shaft and the contact ring. The control is now cleaned and lubricated and should give good service.

Never use carbon tet on a volume control. Not only does it put a coating on the strip, but it dissolves the carbon.

This cleaning method is not recommended for tone controls or other controls working on high voltage because of possibilities of arcing along the carbon strip.

Submitted by:
J. Frederick Shane
Spokane, Wash.

Noisy RF Tuners-Stromberg Carlson

There have been a few cases of noise in the RF tuner of the TV-12 television receivers. The noise appears as a growl as the tuning shaft is rotated, making it difficult to tune in the desired station. This is especially true of the high frequency channels.

When this happens the tuner is in need of cleaning and re-lubrication which is done as follows:
1. Remove the cover from the ganged coils in a clean, dust-free location.
2. With a soft small brush and some carbon tetrachloride, clean all the turns of the coils, the end rings and the coil tracks.
3. Re-lubricate with a small amount of Lubriplate 105, covering all the surfaces just cleaned.
4. Replace the dust cover.

The Lubriplate 105 can be obtained from any hardware store or from Fiske Brothers Refining Company, Newark: 5, New Jersey and Toledo, Ohio. Only Lubriplate 105 should be used.

Stromberg-Carlson
Service Dept.

Sentinel Models 412, 413, 414, 415

To Improve Horizontal Hold

Field reports indicate that with some types of tubes there was a tendency for the above models to require a different setting of the "Horizontal Hold Control" when the set was first turned on (cold) and after it was warmed up (hot).

To correct this, the following changes have been incorporated in chassis having "Series YY" ink stamped on the back of the chassis. They are not

[Continued on page 22]
Magnavox CT 214

One of the problems common to all makers of TV receivers is the protection of the audio output transformer during service operations. The speaker is generally mounted in the cabinet and does not come out with the chassis. It is common practice to use PM speakers with voice coil lead extending to the chassis where a detachable plug completed the circuit. The serviceman, understandably confused by the many shafts frequently, turns up the audio volume in error and does not have the speaker connected to load the output transformer. Voltages of several times normal build up across the transformer under such circumstances.

Magnavox CT 214 — Audio circuit

The Magnavox instrument under discussion, the schematic of which is shown, has solved this problem in a simple manner. It will be observed that the plate supply for the first audio stage, the grid section of a 6AT6, passes through a link on the speaker connecting plug. When this plug is withdrawn the plate voltage is removed from the tube and no amplification takes place in the audio channel. Thus, there will be no audio voltage appearing across the output transformer primary to cause it to breakdown.

General Electric Model 805 — Obtaining focus coil current

The Magnavox instrument under discussion, the schematic of which is shown, has solved this problem in a simple manner. It will be observed that the plate supply for the first audio stage, the grid section of a 6AT6, passes through a link on the speaker connecting plug. When this plug is withdrawn the plate voltage is removed from the tube and no amplification takes place in the audio channel. Thus, there will be no audio voltage appearing across the output transformer primary to cause it to breakdown.

General Electric Model 805

This ten inch TV receiver makes use of an unusual method of provid-
NEW PRODUCTS

HIGH-PASS FILTER

The Brach Manufacturing Corporation of 200 Central Avenue, Newark, New Jersey announces the development of a new 75 to 800 ohm matching transformer with high pass filter action.

The new transformer Brach No. 72-500 is designed to be a perfect termination at channels 2-13 but offers a serious mismatch to diathermy and short wave interference transmissions in the i-f band. A coaxial fitting is provided with the transformer to make a low loss connection to RG59/U. The transformer has negligible loss over the complete TV band and a voltage gain of 2:1.

BEAMAJUSTER

Perfection Electric Co., 520 South State St., Chicago 7, Ill., has recently introduced a control for centering television pictures that cuts out the time required for this operation to only 3 seconds.

The Beamajuster, consisting of a pair of rotating aluminum plates, one of which holds a permanent magnet, is installed by snapping it on the back cover of the TV tube yoke. It fits any standard yoke and is suitable for any size tube. The picture is centered by rotating the outer plate with the fingers, as shown outside the outer plate up or down or to either side, above. Fine adjustments are made by moving the yoke. Once set, the picture will not drift. Full details may be obtained from Perfection Electric Company.

WIDE BAND OSCILLOSCOPE

Jackson Electrical Inst., Co., Dayton, Ohio announces the Model CRO-2 Oscilloscope. Full five-inch SU/P1 CR tube. Wide band vertical amplitiier response uniform from 20 cycles to 1.5 megacycles. Height Sensitivity 0.18 RMS volts-per-inch with response uniform to 100 KC. Vertical Input Impedance 1.5 Megohms, shunted by 20 mmf. Direct to plate balanced 6 Megohms shunted by 11 mmf. Horizontal Input Impedance 1.1 megohms.

Voltage calibration permits peak to peak voltage measurement of all waveforms. Switching arrangement provides vertical pattern reversal. New electronic return trace blanking system. Sweep Oscillator provides saw-tooth wave, 20 cycles to 30 kilocycles in 6 steps. Sine wave sweep of 60 cycles also available. Direct connection, through capacitors to CR tube deflection plates. Intensity modulation, either external or internal 60 cycles. Removable calibration screen. Demodulation probe also available to use for signal tracing. All steel cabinet finished in gray Ham-R-Tex with leather carrying handle size 12 3/4" high X 16 1/2" wide 15 1/4" deep. Net weight 26 lb.

BOOSTERS-BLONDE OR BRUNETTE

The Regency Television Signal Booster Model DB 400 can adapt to individual decorating tastes. Dick Mitchell, Sales Manager for I.D.E.A. Incorporated of Indianapolis, makers of the Regency Booster, poses with two models, one in an ivory plastic case and the other in a deep-tone mahogany.

Both Boosters measure 4 1/2 inches in height, 5 1/4 inches in width and 3 3/4 inches in depth.

Installation of the Regency Booster is uncomplicated. The TV set plugs into the Booster and the Booster plugs into the wall outlet. The easy-to-read dial face and single knob tuning make child's play of the channel tuning. Clear reception of both audio and video on all 12 channels is assured with the wide bandwidth.

LOCKING SHAFT POTENTIOMETER

Ohmite 2-watt molded composition potentiometers with linear taper are now available from stock with a short screw driver shaft and locking nut. This new model is available in addition to the regular 2" long round shaft model, it was announced.

Known as the Type AB Locking Shaft Potentiometer, the new unit is particularly useful in industrial and military applications where resistance adjustments are infrequent, and where tampering with the adjustment is discouraged.

For complete information, write for Bulletin 111A to Ohmite Manufacturing Company, 4974 West Flournoy Street, Chicago 44, Illinois.

NEW ALL-CHANNEL BOOSTER

The TUNE-O-MATIC, a new high-gain, self-tuning television booster with all-channel band circuit and 4-stage amplification, is announced by Electro-Voice, Inc., Buchanan, Michigan.

This unique new Electro-Voice Booster completely simplifies installation and operation. Plugs in between the television receiver and electric outlet—and is turned ON or OFF automatically by the TV receiver switch.

Signal Generator Kit

In response to the consistent demand of great numbers of servicemen, engineers and "hams" Electronic Instrument Co., Inc., 214 Newport Street, Brooklyn 2, N.Y., has just released the widely accepted EICO Model 315 Deluxe RF Signal Generator in kit form. Called the Model 315-K, this modern professional laboratory-precision signal generator kit has all the accuracy and

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The .005 uf. condenser C-55 and the 470,000 Ohm resistor R-59 parallel filter in the output circuit of the 6AL5 Phase Detector have been removed from the circuit.

(b) The 100,000 Ohm resistors R-55 and R-59 in output circuit of the 6AL5 Phase Detector have been replaced by a series parallel resistor and condenser combination consisting of the following:

(1) The 100,000 Ohm resistors R-55 and 59 (see Fig. 2) have been changed to 470,000 Ohm ± 5% 1/2 Watt resistors, part No. 27E1009-55, list price $0.18.

(2) The .002 µf. 220 V. condensers C-85 and C-86 (see Fig. 2) have been added in parallel with R-55 and R-59, part No. 23E205, list price $0.18.

(3) The 33,000 Ohm ± 10% 1/2 Watt resistors R-116 and R-117 (see Fig. 2), have been added in series with R-59 and pin #5 and in series with R-55 and pin #7 on the 6AL5 Phase Detector tube socket, part No. 27E333-2, list price $0.06.

Sentinel Radio Corporation
Service Department

CIRCUIT COURT

[from page 30]

adding resistors in series with, or across, the coil. Fine control is made by a 100K pot which is part of a voltage divider across the coil network. The arm of this pot determines the point on the bias to which the grid of the tube is returned. Thus, it is possible to control the plate current, and consequently the cathode voltage, of the tube over a narrow range.

With the two adjustments it is possible to control the current through the focus coil over a wide range but retain desirable ease of adjustment.

Recordio Model 8J10

This compact, portable, a-c operated instrument contains provision for ra-
Threading through the double idlers, at the left of the sketch, assures stability of tape travel while the takeup pressure idlers are plainly visible at the right of the sketch. The arrangement in Fig. 4C offers double load facility with continuous recording a reality. Ordinarily these units are designed for rack mounting with the exception of single channel remote equipment.

Tape threading of the more expensive Ampex machine is shown in

---

**TAPE RECORDERS**

[from page 17]

To include several types of reels which today are not playable on all machines. To this end, the NAB is attempting to standardize hubs and flanges and set up accepted reel sizes to allow for variation in footage loads.

**Tape Threading & Rewind**

The Magneord system exhibits a flexibility of tape handling made possible when additional units are added to their PT6-K recording amplifier. In Fig. 5A, we see a basic studio or professional layout where in the method of tape threading is shown. In Fig. 5B, an auxiliary spooling mechanism is shown identically threaded to a basic unit. This arrangement records and plays programs of extended length and facilities are included which rewind a 1200 ft. reel in 40 seconds.

---

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by MILTON KAUFMAN

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Fig. 6. Here also at the left we find two feed idlers; one small idler at the end of an arm mounted beneath a larger idler. Speed constancy is immediately introduced by a flywheel type of idler (large weighted idler) at this early moment of tape travel. The capstan and takeup pressure idlers at the right are smoothened mechanically by an electro-mechanical flywheel drive. In addition, a safety device is included. Between the capstan and the takeup reel a power cutoff tension arm and idler protects the recording from damage. In the event of tape buckle or similar fault, whenever tape tension toward the takeup reel becomes unduly slack, the spring actuated tension arm will automatically cause a power cutoff until correction is made. Tape travel will not start unless the tape is properly threaded through this safety device.

During periods of rewind or fast forward roll to a cued section of the tape, the recording head/housing gate is opened to prevent unnecessary wear of tape surface. At such times the tape is merely slipped across pyrex guides at the ends of the housing. Less than 60 seconds are required for rewind of a full 10½ inch reel. With this equipment, 15,000 playbacks are claimed for one tape.

Fig. 7. Threading mechanism of Ampex recorder.

Normal threading derives benefit from the unique design of components in contact with the tape as shown in Fig. 7. The rounded and tapered skirtings of reel guards, idlers and capstans are so angled that the tape finds a natural threading around these...
points of contact. It is claimed that tape _snagging_ is next to impossible. One three-way manual switch controls the mode of tape transport. Its positions are: _play-back, fast forward, _and rewind. One final switch selects one of two tape speeds and simultaneously cuts in proper mechanical and electrical equalization for the speed selected. No change in gearing or in other linkages is necessary as the two speed motor is switched for the speed chosen.

**Commercial Examples**

Some typical examples of what may be expected from properly equalized commercial machines are tabulated according to the manufacturer’s literature.

<table>
<thead>
<tr>
<th>Name</th>
<th>Tape Speed</th>
<th>Special</th>
<th>Description</th>
</tr>
</thead>
</table>
| Algen         | 35 c.      | 1,000    | Tape recorder tape, incorporates a large increase in the radial time constant, as a result of large resistance, through a particular circuit. | 30
| Fairchild     | 35 c.      | 1,000    | Tape recorder tape, incorporates a large increase in the radial time constant, as a result of large resistance, through a particular circuit. | 30
| Ampex         | 35 c.      | 1,000    | Tape recorder tape, incorporates a large increase in the radial time constant, as a result of large resistance, through a particular circuit. | 30
| IP-204        | 3lerc     |           | Tape recorder tape, incorporates a large increase in the radial time constant, as a result of large resistance, through a particular circuit. | 30
| IP-204        | 3lerc     |           | Tape recorder tape, incorporates a large increase in the radial time constant, as a result of large resistance, through a particular circuit. | 30

*Chart of tape recorder characteristics of various types*

Naturally the above data is not derived from one set of readings under identical conditions. Some conform to the NAB sub-committee standards and some do not. They are merely representative of what may be expected from various tape machines ranging in price from below $100 to above $3,000.

**LOOKING FOR TROUBLE**

(from page 24)

the points where the signal is normal and where the signal is defective.

**Discussion**

A higher negative voltage on the plate indicates either more current through R-201 or a large increase of resistance, in both cases causing a larger voltage drop or difference of potential across it. However, an increase of resistance is not likely because while this would cause the sawtooth to be smaller because of the increased time constant, at the same time the wave would be linear. (The sloping portion of the wave would be straight rather than curved). The sawtooth condenser would be using less of its charging curve and would remain on the linear portion. Scope showed a definite non-linearity.

Now, while the increased current through R-201 might be coming from

---

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the tube, this also is not probable. First, the bias has not changed substantially, according to the voltage check. Second, the signal input was the same, according to the scope. Third, the tube was O.K. (had been changed). These factors point to another path for the increased current through R-204.

5.—c

Discussion

The two main possibilities for the increased current through R-204 are a shorted or leaky coupling condenser C-178 or sawtooth condenser C-179. Resistance reading showed C-179 shorted. (However, sometimes condensers break down only under voltage and check normal for resistance measurements with the power removed. In such cases, the suspected parts are removed and substitutions made.)

R-204 very much reduced in value could give 20 K ohms to B — but then there would be no such increase voltage drop across it as measured in preceding question. C-178 shorted would give a much higher reading than 20 K going from plate thru C-178 through grid resistor to B — together with the plate resistor in parallel.

FRONT ENDS

(from page 28)

would result in a frequency drift large enough to cause loss of sound in a split-sound receiver. In inter-carrier receivers no loss of sound is experienced as a result of frequency drift of this nature. With the use of this capacitor and careful circuit planning, modern tuners have been able to keep this drift to well below 100 kc, even under extreme conditions of temperature change.

Other means of maintaining frequency stability in Front Ends are the use of special materials in their construction, such as mycalex, micro-filled low-loss bakelite, and polyethylene as coil forms, and silver alloys as contact materials.

Referring again to Fig. 8-27, a vernier condenser, C5, provides for fine tuning of the oscillator circuit. Most Front Ends employ a small variable capacitor of this type connected across the oscillator circuit, this condenser being brought out concentrically with the main switching mechanism, and which allows for fine or
Fig. 3-28: Simplified A-F-C circuit used in r-f oscillator of Philco 49-receivers.

vernier tuning of the receiver after the initial switching operation. Exceptions to this occur in continuously tuned Front Ends, where the very nature of the tuning mechanism precludes the need for this fine tuner.

Automatic Frequency Control

Many receivers employ AFC (Automatic Frequency Control) in the r-f oscillator to stabilize frequency drift tendencies. Fig. 3-28 illustrates in partial form the circuit used by Philco in its 49-Model receivers.

The block diagram in Fig. 3-29 will assist the reader in analyzing how this circuit operates. First, a shift in oscillator frequency, for any reason, reduces or increases the resultant sound i-f frequency. This produces an unbalance in the discriminator output voltage which is reflected back into the Oscillator Control tube as a change in grid bias. The Oscillator Control tube acts effectively as a shunt capacitor across the complete r-f oscillator, the amount of this shunt capacitance being controlled by the "C" bias on the Oscillator Control tube. Thus, an initial change in r-f oscillator frequency reflects itself back into the Oscillator Control tube as a change in capacitance across the oscillator—thereby bringing it back to its original frequency. R-F oscillator...
frequency changes brought on by temperature variations, mechanical vibrations, and electrical transients are thus automatically compensated for by this circuit.

**Oscillator Radiation**

Oscillator radiation is rapidly becoming a foremost consideration in the design of Front Ends because of the tremendous amount of complaints that have arisen as a result of its interfering effects in other receivers. This radiation may take place in one or more of three ways: 1) directly at the receiver if unshielded, 2) through the r-f stage and back into the antenna via the downlead, 3) through the power lines.

Much is being done in modern circuit design to reduce this effect to a minimum. This includes the use of more effectively shielded components and circuits, reduced operating potentials, and increased filtering.

**Oscillator Troubles**

Troubles in oscillator circuits, aside from circuit failures tube breakdown, switching defects, frequency drift and radiation, may arise as the result of certain conditions associated with very high frequency operation. These are:

1) **Parasitics**—these are very high frequency oscillations often caused by stray capacitances setting up feedback paths between components and wiring. Parasitic oscillations may also be generated by the inductive effects of lead present in the plate and grid circuits. Correct parts placement, lead dress, short wiring, and the use of plate and grid series resistors (10 to 50 ohms) are effective in reducing these parasitics.

2) **Audio Flutter**—this is a condition where a strong audio signal frequency modulates the oscillator through a high impedance path in the "B" supply. Good "B" line filtering is generally the cure for this condition.

3) **Squegging**—this is an interuption of the continuous operation of the oscillator caused by excessive oscillator amplitude pulses. Correct operating potentials as well as proper values of grid leak and condenser will generally eliminate this condition.

4) **Microphonics**—these are set up by sound vibrations from the speaker causing frequency modulation of the oscillator tube and other vibrating components. Special non-microphonic tubes such as the 6BC6, the use of weighted caps fitted over the oscillator tube, shock mounting of the oscillator tube, and correct speaker placement have proven effective means of reducing this effect.

[To Be Continued]
the operation on a station. With the hold control in a midpoint position all stations should lock-in instantly. With the control set at one extreme, jitter may occur and when stations are switched the picture may be completely out of synchronism. At the other extreme setting the hold control may cause the picture to lose synchronism with no effective AFC action. If it appears that the correct setting for the horizontal hold control is not approximately at the midpoint, re-adjust the frequency controlling slug of T1, which is the slug tuning coil A-F. In some receivers a frequency control trimmer is used which is effectively across this coil. The adjustment of this trimmer is the same as the frequency slug.

If an oscilloscope is not available the following method is suggested:

1. Open all trimmer condensers and screw the slug which tunes coil C-D outward.
2. Set the horizontal hold control to approximate center and adjust the slug controlling the frequency of T1, coil A-F, until the picture appears to lock-in.
3. Adjust C14 until the overdrive bars disappear or until a linear and bright image is obtained.
4. Turn the horizontal hold control slowly and observe a jumping of the picture as it passes through the point of optimum lock-in action. Tighten trimmer C13 until this jumping disappears and the picture slides smoothly from left to right as the hold control is turned.
5. Screw the slug tuning coil C-D on T1 inwards until it throws the picture out of synchronism. Re-adjust the other slug on T1 or the frequency control trimmer if used, to bring the picture back into synchronism.

The operation of the synchroguide circuit as outlined in paragraph 5 for the oscilloscope method.

The operation of the synchroguide depends to a large extent on strong synchronizing pulses of constant amplitude. To obtain such pulses most receivers using the synchroguide have two or more stages of synchronizing oscillators, limiters and amplifiers, including in most cases a diode for maintaining constant amplitude. In the circuit shown in Fig. 9, the synchroguide circuit as outlined in paragraph 5 for the oscilloscope method.

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pulses are obtained from the cathode of the half of the 6SN7 at the left. The appearance of these pulses on the oscilloscope is shown in Fig. 12 and

![Fig. 12. Horizontal sync pulses on cathode of sync separator: 10 volt peak to peak.](image-url)

one good check on the operation of the synchroguide tubes and TI some of the critical parts are R12, R17, a 5% 1 watt resistor and R6 and R8. Most of the resistors used in the synchroguide circuit should be at least 10% types and all condensers 600 volt paper or molded types with the smaller values 1000 volt units. One particularly sensitive condenser is C8 which is often subject to capacity variations due to temperature. The most desirable condenser for this application is a 600 volt molded or an oil-filled type.

The most frequent defect in the synchroguide circuit will be found due to a defective 6SN7. A shorted or open TI or a defective trimmer condenser are the next likely offenders. If none of these items seem to be at fault an exact resistance check will usually reveal the defective component. In a few cases it may be necessary to make a point to point check with the oscilloscope.

The synchroguide circuit described here is the one most widely used but several variations of it are found in older television models. One variation does not use the stabilizing coil C-D on TI in Fig. 9 but features a frequency control trimmer and slightly different resistor values. Another variation omits the feedback network C12, R16, without any apparent difference in performance. Still other variations of the synchroguide system use different resistor and condenser values. All these systems, however, operate on the same principle and are serviced and adjusted in the same manner.
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