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LEWIS WINNER Editor



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Modified Sentinel Video Amp Grid-Control Which Prevents Crystal Detector Failures
NBS Constant-Amplifier Oscillator
Regency UHF Converter
Revised Video IF in Sentinel Chassis Which Halts Picture Tearing and Rolling
Selenium Rectifier Forward Test Circuit
Selenium Rectifier Output Voltage Tester
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Designed for fringe areas. Stacking kit available for extreme fringe areas.

> Admiral Duo-Vee VHF-UHF Antenna No. AN1 Designed for metropol-

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Extra profits for servicement NOW you can add UHF to the thousands of VHF Super Fans presently installed in your area, with Channel Master's exclusive new Ultra Dapter, Model No. 414. In 5 minutes you can convert any Super Fan into an all-channel VHF-UHF an-tenna. See your distributor for

details.



Now! Get all 82 channels

with the

New



Write for literature on Channel Master's new complete line of UHF antennas including such models as these:



Ultra Bow Model No. 401



Ultra Bow with screen reflector Model No. 403



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CHANNEL MASTER CORP. ELLENVILLE,



MEMBER

Single Bay

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HORIZONTAL POLAR PATTERNS



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BEST IN OVER-ALL POINT QUALITY!

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Lasted Longer than others tested!

Only Sylvania tubes showed NO FAILURES after 1400 hours ... at accelerated voltages

Exhaustive tests conducted under the supervision of an outside impartial laboratory, the United States Testing Company, showed Sylvania Picture Tubes lasted longer than any others tested.

"IT'S A TRUE

BLUE-RIBBON TUBE"

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RADIO TUBES; TELEVISION PICTURE TUBES; ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT; FLUORESCENT TUBES, FIXTURES, SIGN TUBING, WIRING DEVICES; LIGHT BULBS; PHOTOLAMPS; TELEVISION SETS

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BY U.S. TESTING

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Nearly seven million employees of industry are "providing for their personal security and at the same time helping in the building of our national defenses."

- they are the men and women who availed themselves of the opportunity referred to by Mr. Hahnthe opportunity to enroll in the Payroll Savings Plan for the systematic purchase of U.S. Defense Bonds.
- they represent a high percentage of their companies' employees—in plant after plant, the averages are climbing to 60%, 70%, 80%—even higher.
- their investment in Defense Bonds-and Americaadd up to \$140 million per month.
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Excellence in Electronics

 SERVICE, JANUARY, 1953 16

MAKESHIFT

REPLACEMENT

PICTURE

TUBE



The Guarantee Tussle

IN SERVICING, especially since the advent of TV, Service Men have been plagued by the ever-provocative issue of guarantees.

Now, the rash, oleaginous promises of too many in servicing, and even industry, have become so frequent that associations and better-business groups have decided to enter the scene and wage war.

Believing that there are an army of earnest and honest operators who are anxious to pitch in and serve in the cause, the BBBs have asked Service Men for their assistance. Questionnaires have been submitted asking for forthright answers to the knotty problem. It is heartening to report that many replies have been received and with enlightening information. In one review of the situation, a Service Man* declared that the confusing state of guarantees could be ironed out by engaging in a bold public-relations program, carrying messages to Service Men, the consumer, and even set manufacturers. The theme of the program, it was said, should be that no guarantee is stronger than the intent behind it, and based solely on the sincerity of those involved.

Commenting on the type of supporting statements that should appear to describe the insurance value of a valid guarantee, this operator noted that ads and bulletins should stress the fact that only well-trained, skilled Service Men are able to repair chassis, in a reasonable time, and are thus entitled to an equitable payment for material and their effort. The public should not demand free labor within 90 days or longer following a repair job, and will not, if they are convinced that such a request is completely unreasonable.

The report then referred to a very vital point, the complexity of the TV chassis, which contain more circuits, components, wires and controls, than any of the standard household appliances, such as vacuum cleaners, sewing machines, toasters, or even the midget radio; thus more knowledge and experience is absolutely essential.

Unfortunately, it was noted, too many sets have been sold on the premise that they are absolutely trouble free, and if manufactured correctly, will never break down. Recently some chassis makers have revised their philosophy and begun to follow the practice of automobile manufacturers, who bluntly advertise the fact that efficient repair facilities are available at convenient locations, acknowledging that their cars do require attention, with occasional replacement of worn parts. It was suggested that all TV manufacturers should subscribe to this type of thinking and indicate that if their equipment eventually requires attention, and possibly repair and part replacement, a capable Service Man should be called in.

Stressed, too, should be the fact that even though parts and tubes might carry a long-term guarantee and new parts are available at no charge, servicing is still required, for the defective parts or tubes must be removed and replaced by a trained man who is certainly entitled to compensation for his labor.

Set owners would not become so disturbed about repair expenses, if they adopted a budget plan, it was pointed out, setting up a fund as a reserve for repair and replacement; perhaps based on 25 per cent per annum of the cost of the receiver. Thus, the owner of a \$200 receiver would put aside \$1 a week and set up a base kitty of \$20. The owner of a \$250 console could bank \$25 in a TV budget envelope, and then set aside \$1.25 each succeeding week.

Newspapers could also be very helpful in this campaign, it was indicated. by careful advertising solicitation and presentation. The dailies should print only TV repair ads that contain bonafide addresses, and nonevasive and complete specifications of what services are offered in return for the advertised amount. As an example, if a service-call charge is noted as \$5.95, the advertiser should state that this covers a half-hour labor charge at home, and time over the first 30 minutes will be charged at a \$5.00-an-hour rate. It should also be clearly stated that part replacements involve an additional charge.

Congratulations to the BBBs and cooperating Service Men on this crusade, which it is hoped will rout the irresponsible and their brash claims, and bring a justifiable soundness to the term guarantee.

Phono Designers-Please Help**

WITH THE INTEREST in ultra-fidelity galloping along, more and more have become very conscious of all of the special elements that are required to provide this improved reproduction. Of particular concern has been the *needle*, that tiny item so vital to the successful operation of the hi-fi chain.

Unfortunately, in too many systems the installation of the needle has been a monumental job, instead of a simple task. At one time, pickup cartridges were designed around the needle. Since the advent of hi-fi, and with the intention of improving quality, the procedure has been reversed, with the cartridge being designed first and the needle assembly following. In many instances, this has resulted in the oddest assortment of needle shapes and methods of replacement, with a weird variety of positioning springs, secreted set screws and complex mounts holding assemblies in place. Service Men have found it impossible to insert new needles in most of these jig-saw assemblies.

It must be admitted that the technique of designing the cartridge first, with the needle assembly following along, has resulted in a definite improvement in response, as long as the needle remained in good condition. But, since no needle has a permanent life, it must be eventually replaced. Not even the stouthearted diamonds last forever. Eventually, even the most durable of all substances succumb to the attricious attack of the spinning groove.

While it may be impossible to return ever to a single uniform needle design, it should be possible to limit the variety of designs and standardize on methods of removal and replacement. Perhaps pickup and phono-system designers should form a committee to set standards for phono-needle shanks, and also evaluate the problems which may develop after the equipment has been installed. Immediately, phono manufacturers can help remedy the condition by supplying well-prepared instructions, detailing exactly how to replace the needle, and also advising honestly how long the needle in the cartridge will really last.

Service Men will be forever indebted to phono designers, if they will make it a pleasure, instead of a chore to replace those precious needles.—L. W.

*Arthur E. Rhine. **With apologies to E. J. Marcus of Tetrad.

Parallel-Wire Transmission

Circuitry Features of Continuous 70-Channel Unit Which Employs Input Filter to Reduce Image and Spurious Response, Curb Oscillator Radiation of Converter, and Serves to Provide Decoupling Isolation From Antenna Line at VHF Frequencies

IN DESIGNING CONVERTERS for *uhf* application, there are several approaches that can be followed. On several occasions, many of these have been discussed in SERVICE.*

In Fig. 1 appears the circuit of one type, recently developed, which features the use of two sets of parallelwire transmission lines as tuning elements. To gain compactness, as well as to simplify the slider and tuner drive mechanism, the lines are circularly shaped. Tuning is accomplished by using silver-plated sliders, and is continuous via a dial drive shaft covering 70 channels in 340° of rotation, permitting use of a direct dial scale. Included in the tuner are two stages of *if* amplification.

In the tuning mechanism, which provides tuning of both circuits simultaneously, anti-backlash drive and speed reduction are obtained by using a spring-loaded dial cord around a molded bakelite ring to which the preselector and oscillator sliders are attached.

The circuitry of this converter is quite simple. The overall *rf* circuit consists of a balanced high-pass input filter, preselector transmission line tuning section and a crystal mixer.

The input filter has been designed to reduce image response, reduce spurious responses, especially high powered *vhf*-TV or FM broadcast stations; and reduce oscillator radiation of the converter itself.

There is still another function of the filter which can be quite useful,

*Martin, Wyn, UHF Continuously-Tuned Oscillator; May, 1952. Martin, Wyn, UHF Selectors; Nov., 1952. Hesse, Henry R., UHF TV Converter; Sept. 1952. Percy, M. W., Ser-Cuits; May and June, 1952. and that is decoupling-isolation of the uhf converter from the antenna transmission line at vhf frequencies. This is particularly applicable when combination vhf-uhf antennas are being used.

It is perhaps interesting to compare the electrical and physical appearance of the filter since this points up strikingly the change from conventional circuitry wrought at *uhf*. The electrical diagram of the filter is shown in Fig. 2 and its actual physical appearance is illustrated in Fig. 3. The filter capacitances are represented by C and 2C, while L represents the inductance. The unique feature of the filter, in its physical form, is that no conventional capacitors are used nor are there any soldered joints.

Capacitance is obtained by the proximity effects of the wires; that is, by placing them close to one another. To form the smaller capacitance C (Fig. 2), leads from each inductance are brought together and held by small wire staples. For the larger 2C, one circuit lead and one inductance lead are similarly held by metal staples. The dielectric between the conductors,

 $^1\mathrm{An}$ application for a patent, which covers the mechanical configuration, has been filed.



UHF CONVERTER Line

b y

R. A. MORRIS, Chief Engineer, I.D.E.A., Inc.

for both capacitances, is provided by the wire insulation.1

The capacitance value, C, is on the order of 1 mmfd and the inductance value is .06 uh. The impedance of this double T, constant K, high-pass filter is 300 ohms and the cut-off frequency is 400 mc (approx.). The selection of this value of cutoff frequency, rather than one closer to 470 mc, the lower limit of the uhf band, was made to avoid excessive loss in the neighborhood of 470 mc. Signals passing through this filter suffer an average loss of about 3 db. Below 400 mc the attenuation rises rapidly reaching a value of 28 db at 250 mc. Losses in excess of 30 db are obtained in the vhf and FM bands. These attenuations are directly addable to the inherent attenuation in the non-passband of the tuner.

Following the filter is the preselector, which uses a half-wave transmission line with the input coupling loop positioned at one end and the crystal mixer at the other. A movable shorting bar determines the active electrical length of the line, and over the entire uhf 470 to 890-mc band, it covers a distance of 4".

The oscillator circuit is of the ultraaudion variety using a 6AF4. The tuning circuit here is a quarter-wave transmission line which is capacityloaded at its open end. Addition of this capacity tends to shorten the required length of the line.

Both the oscillator and preselector lines are made of 1/4" wide curved parallel strips of silver-plated brass. Tuning by means of a parallel line of adjustable electrical length has been found to provide a large frequency range, simplicity of tuning, and uniformity of tuning, which facilitates tracking and flexibility of design.

It will be noted that whereas the rf preselector circuit employs a half-wave length of line, the oscillator uses a quarter-wave length. This is so, because the local oscillator tunes from 275 to 710 mc, while the rf preselector covers the 470 to 890 mc range. It will also be noted that the local oscillator frequencies are not exactly half of the uhf frequencies; this unusual condition is taken care of by adding a capacitor across the open end of the quarter-wave line. This serves to shorten the line so that each shorting bar will travel over the same distance. Since the shorting bars of both lines

are ganged to the same tuning shaft,



Fig. 2. Electrical schematic of input filter.

adjustments must be provided to in-sure proper tracking. This is accomplished by using two trimmers on the preselector lines. One trimmer is used for adjustment at the hf end and another trimmer is for adjustment at the lf end. On the oscillator tuner line there is a small trimmer across the open end of the line; this establishes the frequency at the low end of the range.

High stability is available in the local oscillator. The warm-up drift of the local oscillator at the hf end of the band has been found to be approximately +200 kc and at the low end of the band it is approximately -200 kc. The frequency stabilizes after about five minutes of operation. The maximum deviation due to line voltage drift is approximately 70 kc throughout the range of 95 to 125 volts line change.

The output of the crystal mixer is fed to a two-stage intermediate amplifier. A 6BK7 double triode is used. The amplifier tuned circuits are adjusted to vhf channel 10. Actually, any of the vhf channels 8, 9, 10, 11, or 12 can be chosen, permitting a choice of the channel which is most free of undesirable interference.

The power gain of the intermediate amplifier at 200 mc measured as the

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ratio of power at the 300-ohm input to the power into the grid of the input stage has been found to be 21 db. The bandwidth of the intermediate amplifier has been found to be adequate to allow for mistuning and drift, and prevent appreciable amplitude distortion. The overall bandwith is approximately 7 mc and is reduced as much as possible to obtain maximum gain and provide maximum attenuation to spurious vhf signals.

Not only can this unit be used as a complete uhf device, but as a tuner installed on a vhf chassis proper with the tuner working into the high vhf channels. This is particularly true for receivers using a 25-mc if. In these instances spurious responses can be overcome by switching the vhf tuner to channels 8, 9, 10, 11, or 12, whichever is free of undesirable response, and adjusting the if output trimmer control on the rear of the tuner accordingly.

In another application of this unit, the uhf tuner would have a 40-mc if output frequency and would couple directly into a 40-mc if amplifier system. In this case, two preselector stages will be used in the uhf tuner. Finally, this uhf tuner can be combined with a compatible vhf tuner serving as a compact and complete tuning unit.



Comprehensive Analysis of Vital Audio Components Detailing Electronic and Physical Features of Crystal and Magnetic Pickup Compensators . . Preamps for Magnetic and Capacitive or FM Pickups . . . Treble Preemphasis and Methods Now Available to Suppress Surface Noise on Records

PICKUP COMPENSATORS

IN THE EARLY DAYS of acoustical recording the artists played or bellowed into large horns which led directly to the recording diaphragm, and the cutting head was expected to do as well as it could with the undoctored original sound. This procedure is, of course, no longer followed today; the signal that is fed to the magnetic recording head is electrical rather than acoustical, and has been changed according to a definite plan, so that the relative intensities of the original bass and treble frequencies are radically altered. If the disc were played back

through a *flat* (uniform frequency response) system the results would be thin in the bass and screechy in the treble. It is necessary, therefore, that the record playback system restore the original frequency distribution to the recorded signal.

This restoration is performed by the frequency discriminating characteristics of the pickup or of the circuit into which the pickup works. It is this circuit which is called the pickup or record compensator. Actually it compensates simultaneously for both the record and the pickup, and its design

Fig. 1a. How groove modulations (for the same signal amplitude) increase as the frequency is lowered; constant velocity recording. The effect of bass attenuation, producing constant amplitude recording below the turnover frequency, is shown in b. Bass attenuation (6 db per octave) required for b, as illustrated in c.



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depends upon the frequency characteristics of each.

Recording Characteristics

The groove *excursion* or displacement required for the recording of a signal of given amplitude is not constant at all times, but increases as the frequency of the signal is lowered. Bass notes will therefore be recorded by relatively wide groove modulations, while treble notes of the same power will be confined to a much narrower area of excursion.

If this natural effect is not checked the width of the groove modulations at very low frequencies will be extremely great. In such a case either the spacing of the grooves must be made very wide, so that the small number of grooves-per-inch is unsatisfactory from the point of view of playing time, or over-cutting from one groove to another will take place.

The modern solution¹ to this problem is illustrated in Fig. 1. Bass attenuation is introduced into the recording itself, below a given frequency called the turnover point, and is compensated for in playback. In this way a signal of given power will create groove modulations of the same width at all frequencies below turnover. The rate of attenuation required to accomplish this purpose is 6 db per octave. and this rate is standard in commercial records of all makes. Unfortunately, however, no standard turnover frequency has been adopted by the record industry, and values ranging from 250 to 750 cycles have been used. European recording companies have in general used the lower values.

It is clear that, no matter what turnover frequency is used, the reproduced

¹This was not a serious consideration in earlier recording, because the bass regions could only be recorded with greatly diminished amplitude anyway.



Fig. 2. Graph of the *af* spectrum as it is recorded. This curve is known as the *recording characteristic*.

and **PREAMPS**

sound will be very tinny unless the bass attenuation is equalized during playback.

by MARK VINO

Treble Preemphasis

Random irregularities in the record groove create well-known source of irritation, surface scratch. This noise has two adverse effects; it is an extremely annoying sound to listen to, and in addition the high-frequency signals (whose groove excursion is very small, sometimes comparable to the dimensions of the groove irregularities) may be masked so as to become inaudible, or lost in the mud.

Modern recording has adopted a technique to reduce surface noise, which is directly analogous to the treble preemphasis employed in FM broadcasting. The high frequencies are boosted in the recording, so that the ratio of treble signal-groove deviation to that of the random irregularities is increased. Playback equipment must therefore provide treble *deem-phasis*, as in an FM receiver. This makes the music sound natural again, and in addition cuts the surface noise appreciably.

As in the case of bass turnover, the record companies have not reached agreement on the best treble preemphasis curve to use. To illustrate, on Columbia 78 and $33\frac{1}{3}$ records, treble

Fig. 3. Preamplifier for magnetic pickup. (Courtesy G.E.)



preemphasis begins at 1,590 cps, and the rate of treble boost is 6 db per octave. RCA uses 1,000 cps as a treble preemphasis base for their 78s, while the rate of treble boost is $2\frac{1}{2}$ db per octave. In contrast, the FFRR Decca records (78 and $33\frac{1}{3}$) have a treble preemphasis base of 3,000 cps; rate of treble boost is 3 and 6 db per octave, respectively.

A graph of the complete frequency spectrum as it is recorded, including bass attenuation and treble preemphasis appears in Fig. 2. The particular curve used to doctor the recorded signal is called the *recording characteristic*.

Crystal Pickup Compensators

The frequency response or playback curve of a phono should be the mirror image of the recording characteristic, as illustrated by the dotted line of Fig. 2. The crystal phono pickup has a natural frequency response which resembles this required playback curve, and crystal pickups are therefore often used with a minimum of compensation. There is invariably some compensation, however, as the grid resistor

²For use in conjunction with a particular cartridge or series of cartridges.

Fig. 4. Typical circuit for crystal pickup compensator. Values for *R* usually range fom .25 to 2 megohms; for *C*, 50 to 200 mmfd.



across which the crystal is connected acts as a compensating circuit element. The lower the value of this resistor the less will be the bass response of the pickup. There is an optimum value normally recommended by the manufacturer which should always be used. This is usually between $\frac{1}{2}$ and 1 megohm.

More elaborate crystal pickup compensators may be purchased² or constructed with a few simple parts, and in most cases these greatly increase the fidelity of reproduction. A typical circuit design is shown in Fig. 4. Proper values for particular pickups are generally obtainable from the cartridge manufacturer. These values are usually chosen to effect a compromise between the various recording characteristics in use by record companies, and additional frequency adjustments may be introduced by use of the phono's tone controls.

Magnetic Pickup Compensators

The frequency response of modern magnetic pickups, unlike that of crystals, is uniform over the frequency band. Bass boost to balance the bass attenuation in recording, and treble droop to compensate for preemphasis, must therefore be introduced by the circuits following the pickup. Treble (Continued on page 48)

(Contractor out fuge to)

Fig. 5. How to connect a preamp for magnetic pickups.



SELENIUM Rectifier TESTER

by EARL STEIKER and OSCAR NELSON, Jr.

Gen. Manager, Rectifier Div. Senior Design Engineer Galvanic Products Corporation

HIGH-VOLTAGE miniature selenium rectifiers, introduced early in '46, have since found widespread use in all types of radio and TV sets, because of their many advantages. In addition, shortages of scarce materials, whose use they can eliminate, have now greatly increased the popularity of these rectifiers.

While proving quite satisfactory to chassis manufacturers, these disc rectifiers have been quite a problem to Service Men, due not only to the difficulty in testing them properly, but to the high cost of building homemade equipment necessary to provide an adequate test. In addition, there has been confusion as to what actually constitutes a good test for these rectifiers, and what limits should be used on this test.

General Methods of Test

Two methods have been generally used to test miniature selenium rectifiers; the ohmmeter test and the substitution test. Both of these have been found to be inadequate and a source of [See Front Cover]

serious confusion or damage. While the ohmmeter test does provide a fair indication of forward conductivity, it is not too practical when used to measure the reverse characteristics of the rectifier, because it does not apply the proper peak inverse voltage to the rectifier. Many rectifiers, which apparently are all right at the lower voltage, will pass excessive reverse leakage current or break down completely at the higher voltage. Excess reverse leakage can damage electrolytics or cause the stack to burn out in a very short time.

Substitution Method Problems

The substitution technique can lead to trouble because there is not always a positive indication that the rectifier being replaced is at fault rather than some other component, and because the replacement rectifier may be faulty. This can cause damage to a number of good rectifiers, series resistors, and



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electrolytics before the trouble is located.

Deforming Requirement

Both of these tests have also been found to be ineffective, because they do not account for the deforming characteristics of selenium rectifiers. Often, rectifiers that have been on the shelf will decrease in reverse resistance and draw excessive reverse leakage current when the voltage is first applied. This excessive reverse current can damage the electrolytic or the rectifier itself and can also cause low B voltage. However, if voltage of the proper peak value is applied to these rectifiers for a short time before they are installed, many of them will reform; that is, their reverse resistance will increase until they pass less than the maximum allowable leakage current. Incidentally, this reverse leakage current is peculiar to dry metallic rectifiers and does not exist in vacuum tubes. When the current is excessive, it can cause the rectifier to overheat, causing it to age rapidly or burn out. Excessive leakage current can also, as has been mentioned, cause low output voltage or damage the electrolytics.

Other Suggested Tests

Recently, two other tests have been suggested. One of these, the output voltage test, is shown in Fig. 1. This means of checking has been found to be inadequate, too. One important difficulty has appeared in the electrolytic setup; since these capacitors age with time, there will appear variations in output voltage, other than those for which the rectifier is responsible. Also, rather intricate protective equipment has been found to be necessary to protect all of the components should a dead short-circuited stack be placed on test. This protective equipment would be quite important if the tester was also to be used as an electroforming device.

The other recommended tests are illustrated in Figs. 2 and 3 (p. 56-57).

(Continued on page 56)



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Test adapter designed to bring all socket con-nections topside, and permit measurement of voltage, resistance, gain or trace signals and monitor intermittents. (Courtesy Hytron)



LLEN

To MEET THE DEMAND FOR more and more gain from TV chassis, it has been necessary to develop a host of new circuits and new tubes, too. One of the most popular of the circuits designed for high-gain service has been the cascode amplifier, discussed on several occasions in this journal.1 Recently, there appeared a tube designed especially for this unusual circuit, a 6BK7A* which is a heater-cathode type double triode of miniature construction, featuring an extremely high transconductance and a high ratio of transconductance to plate current. The problem of interstage coupling has been solved by locating an internal shield between the two sections of the tube.

In Fig. 1 appears a cascode amplifier circuit** in which this tube is used, with a series arrangement which provides a more remote-cutoff characteristic for agc action, requires fewer circuit components and is said to result in lower effective interstage capacitance. The series cascode also provides slight advantages in noise and gain performance. On the other hand, the series arrangement necessitates using the grounded-grid stage at an elevated heater-cathode voltage; and, for the same plate voltage on each triode, a higher plate-supply voltage is required.

The problem of biasing the groundedgrid stage can be solved either by operating this section with a grid-leak

¹Menarik, Bernard A., Cascode Tuner Conver-sion, and Percy, M. W., Capehart CX-36; SERVICE; September, 1952. *Raytheon. For use in vhf cascode circuits at trequencies below approximately 300 mc.

**Based on Raytheon tube application data.

Circuitry of Cascode Amplifiers Using Miniature Heater-Cathode Double Triodes With Internal Shields...Other TV Tube Developments: Miniature High-Perveance Double Triodes for Vertical **Deflection...Horizontal Frequency Damper Diodes** . . . Sharp Cutoff Video Pentodes . . . Miniature **Output Stage Power Pentodes**

resistor between grid and cathode, or by connecting the grid to a fixed voltage from a voltage divider connected between the plate-supply voltage and ground.

It should be noted that cathode bias is not used on the grounded-cathode section, because this stage is connected to the agc line, and the grid effectively

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sees a high impedance for dc. As a result of the contact-potential characteristics of the 6BK7A, a bias of .5 to 1.0 volt is developed across this source impedance. The contact-potential bias of the grounded-cathode section effectively determines the bias on the other section that is required for optimum dc voltage division between the two series



TV tuner using 6BK7A as rf amplifier in cascode circuit. (Courtesy Raytheon)

hen was the last time

you were knocked

on your



It won't happen again with the





Junction transistor now being produced in quantities for military and commercial applications. (Types CK721 and CK722; Raytheon.)

sections. Any increase in bias on the grounded-cathode section such as would result by adding a cathode-bias resistor, would necessitate increasing the bias on the grounded-grid stage to maintain voltage balance, and this action would result in reduced plate current and transconductance.

It is also important to keep the effect of the cathode lead inductance of the grounded-cathode stage to a minimum. The cathode, therefore, must be connected directly to ground with the shortest possible lead. Similarly, special care must be taken in grounding the grid of the grounded-grid stage. The shortest possible lead lengths and a low-inductance capacitance should be employed.

Optimum performance of a cascode amplifier requires that interstage capacitance shunting effects be kept to a minimum. Unavoidable capacitance shunting exists in the form of stray wiring capacitance and heater-cathode capacitance of the grounded-grid stage. This capacitance loading is very severe; particularly on the high channels. To compensate for this undesired shunting, an inductance, Ln, has been added between the sections and a capacitor, C_n , connected from the plate of the grounded-cathode section to the ground side of the input transformer. These two components effectively combine with the heater-cathode capacitance of the grounded-grid stage to form a tuned pi network. The values of inductance and capacitance must be selected so that the response of the network is peaked at the high TV channels.

The interstage impedance is limited by the input impedance of the grounded-grid stage and is approximately equal to the reciprocal of the transconductance of the grounded-grid



Transistor socket molded of Mycalex 410, a gluss-bonded mica insulation said to have low dielectric loss, immunity to high temperature and humidity exposure, combined with maximum mechanical strength.

stage. This low impedance shorts the interstage network and as a result the frequency response of the network is very broad. If the network is peaked at the center of the high channels, improved performance will result on all of the high channels. As a result of the interstage network, the difference in performance between the low and high channels is kept to a minimum. The low interstage impedance also contributes to the high stability characteristics of the cascode amplifier.

The capacitor, C_n , also serves as a feedback network to correct for interstage degeneration and increases the effective input impedance of the first stage. The value of this capacitor has a very marked effect on the gain of the cascode amplifier. For the circuit shown, a value of 4.7 mmfd is recommended for C_n as a compromise between degree of performance and uniformity of performance.

The frequency response of the input transformer is affected by the input impedance of the grounded-cathode section. Because the input impedance increases with decreasing frequency, the response of the input transformer becomes narrower on the lower channels. As a limit, the bandwidth of the input circuit must not become less than that of the *if* amplifier. If necessary, a resistor in the order of 15,000 ohms can be connected directly across the transformer secondary on the low channels to minimize the effects of variations in input impedance from

Tube tester designed for production testing of electrostatic picture tubes: Checking of breakdown, stray emission, astigmatism, spot or raster cutoff, spot examination, line width, deflection factor or sensitivity, leakages, angle between traces, deflection plate cutoff and base alignment, etc. (Type 2166; Du Mont.)





Complete experimental audio amplifier stage in which four junction transistors, mounted on a small plug-in base, perform the combined functions of two or more electron tubes, an ouput transformer and other components. Operating off a small low-voltage battery, this transformerless and tubeless audio amplifier developed at the David Sarnoff Research Center of RCA at Princeton, N. J., can provide sufficient amplification to operate a loudspeaker.

tube to tube, with only a slight sacrifice in performance.

Other TV Tube Developments

Also announced recently for TV applications is a miniature, high perveance, double triode, vertical deflection amplifier; 12BH7[±].

The unit consists of two completely independent medium-mu triodes in a T- $6\frac{1}{2}$ envelope. One section may be used as the sawtooth generator while the other section serves as the vertical deflection amplifier. Both sections are designed to withstand the high pulse voltages normally encountered in vertical amplifier service. For certain applications where the plate supply voltage must be kept low, parallel connection of the two sections may be used. The heater of the 12BH7 is designed to operate from either 6.3 or 12.6 volts.

Two new diodes[‡] for use in horizontal frequency damper circuits have also been produced; 6AX4GT and 12AX4GT. They are half-wave, indirectly heated diodes contained in T-9 envelopes, designed to withstand the extremely high voltage pulses of line irequency between cathode and both heater and plate elements, normally encountered in direct drive circuits.

The tubes are identical except for heater characteristics. The 6AX4GT requires 6.3 volts at 1.2 amperes, and the heater of the 12AX4GT requires 12.6 volts at 600 milliamperes.

A new television pentode, the 12BY7[‡], is now in production, too.

This is a high transconductance, sharp cutoff video pentode, featuring a

(Continued on page 57)

‡Sylvania.





Fig. 1. Method used in past to measure antenna characteristics; faults common in antenna test sites are illustrated here.

Measuring TV ANTENNA

ACCURATE, RELIABLE measuring techniques are an absolute necessity in the design of TV antennas. The demand for more and more gain for fringe areas, and the increased complexity of *uhf* receiving problems makes adequate test facilities even more important.

There are three indications of antenna merit. The first is the antenna's gain. It is the measure of an antenna's ability to gather signals arriving from a given direction and deliver them to the receiver. The second is the antenna's radiation pattern, which indicates the ability of the antenna to discriminate against unwanted signals arriving from other directions. Another characteristic of antennas is the voltage standing-wave-ratio, which measures an antenna's usefulness in delivering power to a load of given impedance level.

The theory of measuring both antenna gains and antenna patterns is simple and straightforward. To measure gain, one connects the antenna under test to its proper transmission line and measures the power available to a matched load at the transmission line terminals. One then substitutes for the antenna under test a standard antenna, (usually the standard is a matched half-wave dipole) and measures the power available at the transmission line terminals. The ratio of these two powers is the gain of the antenna. This ratio is usually expressed in decibels (db).

To measure the pattern of an antenna, the antenna is connected to a power measuring device and the power



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A Report on the Lab and Field Facilities Employed to Evaluate VHF and UHF Antenna Merit Involving Gain, Radiation Pattern and VSWR



Characteristics

received by the antenna is recorded as the antenna is turned past a distant transmitter. The plot of power received against angle of arrival of the signals is the pattern of the antenna.

In practice there are many complications to this straightforward theory.

High-frequency radio energy travels in straight lines and when it strikes an obstacle it bounces, again traveling in straight lines away from the obstacle. From a small obstacle the energy scatters in all directions. From an extended obstacle it usually travels only in those directions, so that the angle of incidence equals the angle of reflection. A site for measuring antenna characteristics must be entirely free of obstacles which can produce reflections. This is an exceedingly difficult requirement since the earth itself is such an obstacle.

A common method of measuring antenna characteristics is to place a transmitting antenna and the antenna under test on towers, as illustrated in Fig. 1. It will be noted that radiation can arrive at the antenna under test from many directions, and, consequently, the power measured at the antenna terminals may not be a reliable indication of the antenna's ability to receive only from the direction of the transmitting antenna.

It is possible, by using a highly directive transmitting antenna and by carefully choosing the height and loca-

(Continued on page 61)

*Based on field test procedure data prepared by the lab staff of Gabriel Laboratories, research center for Ward Products, with lab facilities in Needham, Mass., about 15 miles from Boston, and additional test site at Natick, Mass.

(Right)

Fig. 6. Loss in the gain of an antenna to a specified mismatch at the input.

by DONALD PHILLIPS



Fig. 5. Block diagram of complete system designed for pattern measurements.



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RALPH G. PETERS b y

THE INTRODUCTION of commercial uhf in Portland, Oregon, provided an unusual opportunity to evaluate on a broad scale, the problems and possibilities of the ultrahighs, and probe the types of antennas and accessories that are necessary to insure reliable performance.

Portland has five shadow areas where it has been found difficult to receive sufficient signal strength for suitable pictures. For the most, these areas are so hilly that the signals have been found to vary considerably with elevation. Because at these higher uhf frequencies there is less refraction to bend the wave, it is difficult to receive adequate signal strength in the depths of these hills unless it is due to a reflected condition. Should a signal be found on the ground floor of these hills, it might well come from any direction, even opposite to that direction of the transmitter.

However, hills alone are not the only gathering place for reflections or low signal strength. In relatively clear areas, trees can splatter the signal causing reflections as well as absorbing the signal strength. Any area, while it may represent flat terrain, if behind an obstacle and is located in the shadow cast by that obstacle can suffer from insufficient signal strength, too. But, with careful choice of antenna, and a thorough probe of both roof and height, it has been possible

On-the-Scene Survey[‡] of UHF Reception in Portland, With Analysis of Results Obtained With Assorted Antennas, Leadins and Accessories

to satisfy most installation requirements.

It is generally known that most antennas originally designed for vhf will receive uhf, too, after a fashion. They operate at uhf strictly on harmonics and as such have omnidirectional, multi-lobed patterns that intercept from all directions. This does not, of course, contribute to satisfactory uhf reception.

One type of 2-83 mc antenna found quite effective has been the V. While

A 75-300 ohm matching transformer. Precision impedance match at 75 and 300 ohm screw ter-minedance match at 75 and 300 ohm screw ter-minals said to provide a means of eliminating standing waves and line reflections in individual installations, as well as master TV systems. Providing a 2 times increase in signal voltage and signal-to-noise ratio, when transforming from 75 to 300 ohm level, this unit has been designed for installation at the terminals of many types of antennas that feed into 300 ohm, or open wire lines. This application is said to be necessary in the case of stacked arrays and multi-element yagis where the impedance of the antenna is often 75 ohms or less. (Model MT-1; Blonder-Tongue Labs.) Blonder-Tongue Labs.)



their gains are usually limited and their patterns wide at vhf, they have been considered sufficient for major area vhf installations. At uhf, their gains rise rapidly offering gains of 7 to 12 db at uhf frequencies. The forward lobe at the ultrahighs has been found to be extremely sharp and thus is decidedly useful for rejection of reflections.

One should carefully consider the use of a multi-channel vhf-uhf antenna and make certain that its characteristics are favorable to the channels assigned to his area, plus the fact that the signals from both vhf and uhf transmitters will be reflection free and adequate in strength where this antenna type is to be installed.

Another type available is the bow tie antenna, one of the simplest of broadbanded uhf antenas. It covers all channels, 14 through 83, with its wide, bidirectional, figure-eight reception pattern that intercepts as well off the back, as it does from the front. With moderate signal gain, up to 4 db, it has been found to be good for major signal area installations where reflections are at a minimum. When reflections are bothersome or additional signal strength is needed, the use of a reflector with the bow tie will elim-

[#]Based on a field report prepared by Lee Allen of Amphenol.



Universal Video Generator

Hickok, through 42 years of uninterrupted quality production has pioneered and developed numerous well-known electrical and electronic equipments now recognized as standards for the industry.

Elicice of the Experts

The newest Hickok contribution is the Model 650 Universal Video Generator. It accurately and rapidly localizes trouble in any stage of a TV receiver. It's use accomplishes in minutes tasks that normally take hours.

THE HICKOK ELECTRICAL INSTRUMENT COMPANY **Cleveland 8, Ohio**

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10514 Dupont Avenue



A multi-element beam uhf duplex yagi, which is said to have high gain and excellent directivity over the entire uhf band. (Model 300; Telrex.)

inate back pickup and provide approximately another 2 to 4 db gain. As in vhf, stacking antennas at uhf will further increase your signal gain. In Portland, practically all the bow ties use reflectors.

The corner reflector represents another uhf type that offers interesting possibilities. A high gain broadband antenna, it has but a single forward lobe with signal gains from approximately 6 db at the lower uhf channels to 12 db at the higher channels. Its unidirectional pattern rejects reflections approaching from the sides or back and its increased gain permits installation in fringe or shadow areas. It is one of the larger types and normally more costly.

The Rhombic

Still another type is the rhombic with signal gains of 2 to 8 db, and a narrow main lobe. Only 10° to 25° wide at half power point, it is like the beam of a searchlight pointing the way to reflection-free reception. When the problem is reflections, the *rhombic* might be the answer.

The familiar yagi, which won wide acclaim at uhf because of its tremendous gain over a narrow bandwidth, limited to one or two channels, at uhf has a bandwidth which extends from five channels at the low end to about ten channels at the high end. Its peak gain of about 10 db for a six-element array which drops only about 3 db over that bandwidth has been found to make it an ideal antenna for deep fringe applications, or wherever the narrow single forward lobe selectivity is necessary. These, physically, will most likely be available in the five to eight-element types.

In Portland, in some areas, it was found that the problem of signal strength was not as acute as reflections. While in others, such as shadow or hilly areas, it was found necessary to fight for every ounce of signal all the way. In these areas, movement of the antenna in any direction, up, down, or sideways could have considerable effect, good or bad, upon the sig-



UHF corner reflector with antenna mounted behind the mast. Reflecting screen is said to be held rigid by two separate U-bolt assemblies which are welded to the extreme ends of the screen. Antenna has free space terminals to prevent the accumulation of dirt and moisture at the feed points. (Model 405; Channel Master.)

nal. Tipping the antenna, upwards or downwards, didn't seem to have much effect. However, polarization was found to be very important. The moment an antenna is rotated from its horizontal position toward vertical, with every degree additional signal is lost until at vertical, all is lost.

When mismatching of impedances occur, with resultant standing waves, and the signal is inadequate, the standard vhf metal ringed type standoff insulators were found to be very critical of placement in transmission line support. If one is not careful under these conditions, the limited signal being received can be lost entirely by placing the standoffs along the transmission line at the wrong points. Of course, standing waves can also develop double images on a TV screen just like reflected signals. It is very important, therefore, at uhf that impedances be matched.

Vhf lighting arresters, likewise, were found to be contributors to signal

Jay Saphier, of Brach Manufacturing Corp. (right), Seymour Wiedenbaum (left) of National Radio Distributors, and Sol Verter (center) with recently developed *uhf* corner reflector with bow-tic elements. The open-mesh construction is said to present the least possible wind load. Both reflector sections and the antenna element are supported so that they cannot change posi-tions with vibretion. Antenna is claimed to tions with vibration. Antenna is claimed to have a high front-to-back ratio, with a gain of 8 to 12 db over the uhf band. (Radar-Tenna model 479.







Kit with all necessary parts to enable assembly of six complete *uhf* antennas. By experimenting of six complete *uhf* antennas. By experimenting with the six basic *uhf* designs, the user can de-termine by actual test, it is said, the antenna best suited to *uhf* reception in his area. (Miller Television Co., 2840 North Naomi Ave., Bur-bank, Calif.)

loss. In many installations it was observed that the lightning arrester was affixed to the house beneath the transmission line, but the line was not connected into its circuit because of its effect upon the picture. Lightning arresters and standoff insulators designed for uhf applications are now on their way from various manufacturers, and these necessary components will be welcome, particularly for these critical installations.

Unquestionably, the leader in popularity as far as transmission lines were concerned in Portland, was the tubular 300-ohm line. Portland has a rainy season and the ability of tubular at uhf frequencies to conserve three times the signal as that of the popular flat ribbon type in wet weather is indeed appreciated. Open wire line, while it doesn't enjoy the acceptance of tubular, is being used extensively, too. However, there is rebellion on the part of some Service Men to the mechanical and physical problems often involved in its handling and installation.

It has been indicated that the major signal range of Portland's uhf station is approximately 20 miles, with fringe or secondary reception possible up to 30 to 40 miles. Salem, Oregon, 43 airline miles south of Portland, was found to represent an ideal reception condition because it is flat between it and Portland. At this point it has been found possible to receive signals of 350 to 600 microvolt intensity at 20' heights above most roofs. The results were particularly impressive, because the station presently is only operating on one-fifth of its ultimate power.

While one should be conservative in uhf optimism, because we have really experienced only the low end of the band's performance, Channel 27, it is difficult to withhold one's elation. It is possible that the higher *uhf* channels will increase the problems, but as in the past Service Men will rise to the occasion and come through with practical solutions.

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34 • SERVICE, JANUARY, 1953


1953 VIEWED AS RECORD-SHATTERING YEAR BY EXPERTS--Unparalleled expansion will prevail not only in TV, but in radio and allied fields, during the new year, according to management and engineering heads, association chairmen, and trade specialists. Their optimism is based on many sound facts. For instance, with between 100 to 150 new TV stations expected to go on the air during the new year, approximately 5-million additional families will be brought within the TV service range. . . . Not only is it expected that new TV receivers will be installed in the new market areas, but that replacements and second sets will be required in communities where stations have been operating. . . . In addition, new stations opening in fringe areas should cause a strong upward swing in such vital markets as Detroit, Cleveland, Chicago, and other cities which have had TV since early postwar years. . . . Because of this huge anticipated receiver requirement, the picture-tube industry will be asked to produce more than 8-million tubes, of which 2 million will be for replacement. It is expected that the 21-inch rectangulars will be the most popular, and the 17 inchers will run second. Liberal quantities of receivers with 24-, 27- and 30-inch picture tubes will also be produced. . . . With 20-million viewers in American homes, the replacement-parts market will assume greater importance during the next 12 months. Servicing of these receivers will require more replacement components than ever before in the 6-year postwar history of the industry. . . . It is estimated that nearly 4½-million TV sets, now in use, have screens smaller than 16", and will probably require replacement or conversion this year. . . . Radio-set production will also continue firm in '53, with about 9-million sets coming off the line.... The servicing of communications equipment will also become an extremely dominant factor during the year, in view of the increased use of two-way equipment not only among police and fire departments, but pipelines, taxicabs, lumber-camps, trucking concerns, farmers and ranchers, strip mines, doctors, ambulances, newspapers, motion picture companies and others. . . . According to one industry association prexy, within another five years 50-million TV sets should be in operation, and the replacement markets alone thereafter, will require production almost as great as at present.

<u>OUTSTANDING VARIETY OF PARTS NOW BEING MADE</u> -- To meet the growing requirements of today's radio-TV servicing industry, and the initial equipment needs of labs, schools and others, manufacturers are now obliged to produce an unusually wide assortment of components. According to one supplier engaged in manufacturing capacitors, whereas a few years ago their line consisted of a few hundred different numbers, today, over 4,500 different types are being processed, with approximately over 900 different electrolytics, 300 tubulars, 1,200 oil-filled, 300 metallized-papers, 400 micas and 200 ceramic types coming off the line to take care of all needs. Thanks to robust factory stocks, permitting fast delivery cycles, distributors can draw on these inventories at any time for their customers. . . This expanding and still-expanding selection of components represents a dominant achievement in the parts industry, which will play a significant role in servicing during '53*.

<u>UHF TELECASTING SPREADS TO EAST AND MIDDLE WEST--At long last, ultrahigh broadcasting</u> has begun to spread its wings eastward. . . . Two cities roared a welcome to <u>uhf</u> shortly before New Year's Day--York, Pa., and Atlantic City, N. J. In the former instance, WSBA-TV went on the air on channel <u>43</u>, and in the latter case, WFPG-TV began telecasting on channel <u>46</u>. . . As this column was being written, WSBT-TV (channel <u>34</u>) in South Bend, Ind., began testing, and WBRE-TV (channel <u>28</u>), Wilkes Barre, Pa., pulled its on-the-airswitch, too. . . It is expected that WFMJ-TV (channel <u>73</u>) and WKBN-TV (channel <u>27</u>) in Youngstown, Ohio, will also be on the air as this issue comes off the press.

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*With apologies to Charles Golenpaul of Aerovox.



<u>TV BUILDING PERMITS STILL POURING OUT OF WASHINGTON--Over 165</u> have now received authorization to construct TV stations. Among those who have received grants recently are: Community Telecasting Service, Bangor, Maine (channel 5), which represents the first station in that state; WONN-TV, Lakeland, Fla. (16); Thames Broadcasting, New London, Conn. (26); Harrisburg Broadcasters, Harrisburg, Pa. (71), the second station authorized in that city, WHP-TV (55) receiving the first grant; Gable Broadcasting, Altoona, Pa. (10); KCNA-TV, Tucson, Ariz. (9); WIRK-TV, West Palm Beach, Fla. (21), and WEEX-TV, Easton, Pa. (57).

<u>16-CHANNEL VHF/UHF ROTARY TUNER INCLUDED IN ALL-CHANNEL CHASSIS</u> -- A rotary-type tuner receiver, providing selection of any combination of vhf and uhf stations up to a total of 16, will soon be available. As shipped, 12 of the 16 inserts for which the tuner has been designed will be pretuned for 12 vhf channels. Inserts pretuned at the factory for any specified uhf channels will be supplied by the manufacturer for insertion in the remaining four spaces. Should more than four ultrahigh channels be required in any area, inserts tuned for the additional channels can be substituted for an equal number of vhf inserts in the tuner. . . New tuner is based on operation of the fundamental of the oscillator frequency, rather than the harmonic. . . An analysis of the circuitry used in this receiver will appear soon in SERVICE.

<u>CBS URGES EARLY SETTLEMENT OF COLOR DISPUTE--</u>In a plea to bring color to the public at the earliest possible moment, <u>CBS</u> declared in a special statement that it . . . "genuinely hopes that the industry committees in groups now working on . . . a compatible system, will be successful in their efforts, and will press forward to obtain approval of its standards in 1953." According to Columbia . . . "The manufacturing industry, broadcasters, and the FCC, owe the public the obligation of promptly considering whether it still remains true, as CBS believes . . . that the present field-sequential system is the only practical, workable and inexpensive color system, or whether this approved system is to be replaced by a compatible system which must be equally practical, workable and inexpensive. All elements in the industry and in the government should strive promptly to resolve this question, so that all can go forward in vigorous efforts under whichever system prevails."

TRANSISTORS NOW ON PRODUCTION LINE--Substantial quantities of transistors are now being processed not only for the military, but the commercial world. As a result, many extremely active developmental projects are now underway. Some efforts have already been quite productive. In one instance, hearing aids, featuring pea-sized transistors in amplifier circuits, have been evolved. . . During the next few months many similar transistorized devices will probably appear, and at this writing, it seems as if the transistor may soon become a factor in complete amplifiers and radio sets. According to the headman of the TV division of one leading eastern manufacturer, transistors might even appear in production model TV chassis in about a year or so.

<u>MULTIPLE ANTENNA BUSINESS BOOMS ON PACIFIC COAST</u>--The installation of master-antenna systems in apartment developments has become a roaring project in California. One servicing organization in San Diego has received a contract for the installation of a 420' antenna tower to feed 552 apartments in 12 apartment buildings. In another assignment, an antenna is being installed to pipe signals to 1,200 apartments.

<u>SERVICE</u> <u>APPLAUSE</u> <u>CONTINUES</u>--Reports Johnny Sky of Portland, Oregon, in a letter to ye editor . . . "You certainly have a wonderful magazine!'' . . . A. W. Gotcher, also of Portland, notes that of the six radio and electronic publications he subscribes to, SERVICE is . . . "the only one devoted entirely to <u>service</u>. . . . I enjoy the audio articles, your coverage of recent <u>uhf</u> developments, and the Ser-Cuits department. I want to thank you for all the excellent articles, which are, in my opinion, getting better all the time." . . . It is gratifying to learn, gentlemen, that SERVICE serves you so well.--L. W.



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BALANCED TONE ARM provides feather-light needle ride and optimum tracking. Available equipped with crystal or G.E. Triple Play Cartridge —or for plug in of magnetic cartridges.

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EXTRA-HEAVY TURNTABLE --mounted on ball bearings. Extra weight and precise bolancing allow it to act as flywheel for motor. Makes for constant, accurate speeds.

TWO-TIER MAINPLATE made of 18-gauge steel. Will not warp or throw parts out of alignment. Spring mounted to absorb unwanted vibrations.

Model 126 HF



"wow" and "rumble" delivers accurate, constant speeds,

4 POLE-SHADED POLE MOTOR - for smooth

power. Eliminates "hum,"

STEP-DRIVE COUPLING —for accurate transfer of speeds from motor to turntable. Has fewer working parts.



C w/C-1952



Webcor's mechanical excellence and design superiority make it the ultimate in automatic record changing for custom, high-fidelity installations. The powerful 4 pole shaded pole motor is statically and dynamically balanced for positive, accurate speeds—and to eliminate "hum," "wow" and "rumble." The ball-bearing mounted, extra-heavy turntable changes speeds smoothly and accurately by means of the new "step-drive" coupling.

This Webcor precision means the utmost in convenient listening pleasure—up to four hours of uninterrupted music—then, automatic shut-off. It means your precious records will sound better and last longer on a Webcor "HF" Diskchanger.*

*Available mounted on beautiful base pan for plug into phono-jack of radio, television, or amplifier.

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Servicing Helps

EXCESSIVE SOUND BARS in a picture, that are not due to fine tuner misadjustment, normally indicate that the crystal is about to fail. Ultimately, complete failure will result in weak picture and loss of sync.

In Sentinel chassis,* this condition is caused by a momentary surge current in the control grid circuit of the 6AH6 video amplifier tube due to internal shorting of the screen grid to the control grid damaging the 1N60 crystal detector.

To remedy a 270-ohm 1/2-watt resistor (R_{ss}) should be added between the .1-mfd capacitor (C_{24}) and the control grid (pin 1) of the 6AH6 video amplifier, if this resistor is not already in the set. (This change has been incorporated in all but the early production chassis.)

Picture Tearing and Rolling on Strong Signals

Picture tearing and rolling on strong signals, when not caused by locality adjuster switch on Sentinel sets,* being in the wrong position, or on weak or medium position in a strong signal location, may be caused by overloading of the 6CB6 third if amplifier due to low plate voltage of



this tube, preventing it from properly handling strong signals.

Necessary Changes

In initial production, the screen and plate were tied together to the 150-volt line. If a chassis is encountered in which the plate is tied to the 150-volt line and the picture tears or rolls on strong signals, the following changes should be made to tie the plate of the third video if tube to the 265-volt line:

(1) Change the 6CB6 82-ohm cathode resistor, R25, to 220 ohms, 1/2 watt.

(2) Remove the jumper wire that runs from the screen, pin 6, of the 6CB6 to terminal 1 of the fourth video if transformer. This will leave the screen of the third video if tube connected to the 150-volt line through a 1,000-ohm resistor.

(3) Add a 1,000-ohm 1/2-watt resistor between terminal 1 of the fourth video if transformer and the 265-volt line.

(4) Add a .001-mfd 500-volt capacitor between terminal 1 of the fourth

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*Models 454, 455, 456 and 457.

Preventing Premature Crystal Detector Failure...Halting Picture Tearing and Rolling on Strong Signals...Cures for Horizontal Jitter and Unstable Sync in Fringe Areas, Picture Shift at Maximum Contrast and HV Breakdown and Corona . . . AGC Threshold Control Adjustment

> video if transformer and chassis ground.

Hoffman Field Service Notes

Horizontal Jitter in Fringe Areas. ... Chassis 200, 201, 202: When horizontal jitter in fringe areas is reported in these chassis, the value of the capacitor connected between pin 4 of the horizontal multivibrator and ground should be increased from .01 to .05 mfd. A 20-per cent 400-v capacitor may be used.

Unstable Sync in Fringe Areas.... Chassis 196, 196M, 196T: Some of these chassis have exhibited unstable sync in fringe areas. To remedy this situation, the 1/2-watt 1-megohm resistor that is wired across pins 1 and 6 of the agc keyer tube socket (front, left-hand socket when viewing chassis from the bottom rear position) should be clipped from the chassis. This change has been incorporated in production runs on all receivers produced after J243241.

Picture Shift at Maximum Contrast. ... Chassis 210, 210M, 211, 212, 212M and 213: This condition can be remedied by increasing the value of R_{304} , a 47-ohm 1/2-watt resistor to a 150-ohm, 1/2-watt resistor. A connection should

(Continued on page 62)



Fig. 1. Modifications in control-grid circuit of video amplifier tube in Sentinel chassis which serve to prevent premature crystal detector failure.

Fig. 2 (right). Revised circuit of third video if amplifier in Sentinel receivers which halts pic-ture tearing and rolling on strong signals.



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elements

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Line — television's *new* "Master of the Elements"—now meets the pressing demand for *better* electronic equipment. This complete line of *quality* TV Antennas, Mounting Accessories and Wire represents more built-in ruggedness than any now known—proves that *only the Lest meets the test of time!*

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by KENNETH STEWART

Highlights of Tuner, Amplifier, Speaker and Enclosure Specification Data Now Supplied to Aid Architects and Builders Including Audio Systems in New and Modernized Homes...Hoffman Chassis Audio Output with Crossover Network for Two Speakers . . . High-Gain IF Amplifier for FM Tuners

THE INSTALLATION OF COMPLETE audio systems, with matched amplifiers, changers, speakers, enclosures, and perhaps tuners, preamps and remote units, no longer has a limited appeal, but instead is of genuine interest to a growing audience of better music enthusiasts. The trend has been especially significant among new home owners anxious to have audio systems installed as a permanent feature, with built-in audio facilities. Others have specified arrangements which would permit such installation at a future date.

As a result, architects and builders have become quite audio conscious and often sought the advice of Service Men specializing in audio, to determine just what should be provided to insure better reproduction. In many instances, this information has been translated into a special audio spec section in the building plans. Some manufacturers of audio gear have also sought to help and now include such



Modified audio output circuit of Hoffman radio chassis 182, models 21M900, 21B901, 21P902. Two speakers are used. one a five-inch speaker (tweeter) for high frequency, the other a twelve-inch speaker (woofer) for low frequency. A cross-over system is employed; 1 and 50-mid capacitors shunt the high frequencies across the twelve-inch speaker and therefore, hf are reproduced only in the tweeter. The choke, L_{22} , offers high impedance to high frequencies across the tweeter and low impedance to the low frequencies; thus only the low frequencies are reproduced in the woofer.

spec information in their engineering data sheets.

In one such spec section,¹ there appears data on speakers, enclosures,

¹Stromberg-Carlson, ²Stromberg-Carlson SR-

tuners and hi-fi amplifiers, which it is felt will provide quality results. In an analysis of tuner² requirements, the specs note that the output impedance of the tuner should be 150, 600 or 10,000 ohms. Continuing, the specs declare that the required fidelity and sensitivity will be available if a maximum of 5 microvolts input signal obtains to provide a minimum of 30 db quieting in the FM band. In a description of the circuits used in their tuners, the manufacturer notes that the rf amp, antenna stage and oscillator circuits use metallized coils on glass forms and are tuned by means of powdered-iron cores. Two stages of if amplification are provided and the bandwidth is 200 kc.

To provide maximum fidelity and minimum noise, a rectilinear ratio-detector preceded by a limiter stage is employed. Over-all frequency response is within $\pm 1\frac{1}{2}$ db from 20 to 20,000 cps. The tuner includes an automatic (*Continued on page* 64)

High-gain 6-tube intermediate frequency amplifier designed to operate with an FM tuning unit and provide a frequency response of 20 to 20,000 cps. with distortion less than 1 per cent. It is tuned to 10.7 mc, and has a bandwidth better than 150 kc. Three *if* amplifiers are used, two cascade limiters and a discriminator type of detector. The *if* and discriminator transformer are *hi-Q*, slug-tuned units. Output of discriminator is ½ volt. A 6BA6 serves as the first *if* amplifier, two 6AU6s are used as second and third *if* amplifiers, and two more 6AU6s serve as limiters and a 6AL5 is the discriminator. (*IF-6; Collins Audio Products Co., Inc., P. O. Box 368, Westfield, N. J.*)



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In addition to a strong forward reception lobe, the Inline has uniform gain over the entire range of VHF channels—less variation than the 3 decibel change which causes "fuzziness." The Inline is also available in stacked array for those fringe or trouble areas which require additional signal strength.

The Amphenol Tubular Twin-Lead provides very low-loss and constant impedance. The tubular construction minimizes the effect of moisture and dirt deposits on the concentrated field of energy and ends weather interference. Because of these characteristics, Amphenol Tubular Twin-Lead has been recommended by leading TV manufacturers and authorities for any installation where UHF is, or will be available.



This illustration clearly shows that the concentrated field of energy between the two conductors, which are 7 strands of #28 copper weld wire, is contained by the tubular construction. This important field of energy is unaffected by any exterior conditions.

Your free copy of this book is available from your Authorized Amphenol Distributor. It contains complete factual and test data on the factors which determine Better TV Picture Quality.





consider the evidence.



The test patterns on *both* high and low bands reveal the Amphenol Inline Antenna's superior uni-directional reception lobe. This single forward lobe intercepts the TV signal at its maximum available strength. It also rejects unwanted reflected signals or side interference that cause "ghosts" and unsteady pictures.

No other broadbanded antenna can present as favorable a reception pattern on *all* the VHF channels as does the Amphenol Inline Antenna.

Reading Difficult TV Schematics

by CYRUS GLICKSTEIN

MOST SERVICE MEN realize that in deciphering a TV schematic, one cannot simply follow a connecting wire by eye alone. The complexity of most schematics makes this almost impossible. To determine where a connecting line goes, it is good practice—in fact, almost essential—to follow carefully with a pencil, pen or tool, each line to its destination, including the detours or side-roads through terminals and plugs. An example of the need for this procedure is illustrated in Fig. 1; the partial schematic of the Hallicrafter T-64 chassis.

Points which may help one travel through a plug and jack without getting lost are:

(a) When following a wire into a plug, the pin number on the plug should be noted; the correspondingly numbered pin should be found on the jack or socket and tracing of the wire continued to its destination.

(b) Some schematics often show a plug and a corresponding socket without numbers on the pins as indicated

Part II . . . Tracing Complex Connections Through Plugs . . . Deciphering Complicated Diagrams Through Use of Arrowheads to Indicate Current Flow

in plug 6, socket 4 in Fig. 1. Schematics are generally drawn so that the plug and jack (socket) terminals with the same relative position connect with each other. If in doubt, one can pencil in a keyway in the same position at the bottom of the plug and of the socket, and count around on the plug (or socket) until the pin is reached which connects to the wire being traced. In the next step, one should count around to the pin with the same number on the corresponding socket (or plug) to find the pin through which the connection is continuing.

(c) It is important to make certain that the connection is being traced through the correct male and female connections. In most schematics, the plug and corresponding socket are drawn close to each other. In some, however, they are separated. Usually, the plug and jack have the same numerical designation; viz., P501 goes to [501. In some cases, different numbers are used; P601 may go to J401. When there is any question as to which plug and jack go together, it is necessary to check the numerical designations of all plugs and jacks and note the number of terminals on the plug and jack under question as compared to those on the other plugs and jacks on the diagram. The plug and jack which go together obviously must have the same

(Continued on page 46)





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- Cascode circuit!
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Proof of the Turner Booster's popular appeal to TV set owners piles up every day from dealers all over the country. "They're asking for it!" say the dealers, "Double our order for the Model TV-2." Get your share of the profitable Turner Booster sales that are pyramiding from coast to coast. Order this finest of all TV boosters now!

THE TURNER COMPANY, EXPORT: Ad. Auriema, Inc. 89 Broad Street, New York 4, N. Y. Cedar Rapids, Iowa IN CANADA: Canadian Marconi Co., Toronto, Ont., and Branches.

How to Read Schematics

(Continued from page 45)

number of and the same physical arrangement of terminals.

Unfamiliar Circuits

In reading schematics, unfamiliar circuits often present a problem. To cut down the time lost due to this, Service Men must keep abreast of current developments and new circuits. Most have little trouble in following the path of the signals through the signal circuits, and through the front end, the video and audio strips. There is usually little trouble, too, in following sync signals through the sync stages until they are applied to the sweep generators. Circuits which may give even experienced Service Men some trouble include unusual arrangements of the low-voltage supply. In some models, stages are connected in series-parallel to form voltage dividers across the B + supply. These circuit variations were analyzed in a previous discussion.*

Confusing Diagrams

Probably the greatest cause of confusion, next to switches, are diagrams with many criss-crossing connections. When the number of connecting lines is multiplied, the schematic becomes harder to follow.

In deciphering such diagrams, arrows should be inserted on the lines to show the direction of current flow. Current flows from a lower to a higher potential to a maximum B point in

*Glickstein, Cyrus, TV Troubleshooting by Voltage Measurements, SERVICE; September and October, 1952.

(Below)

Fig 3. Types of symbols used in recent schematics released by DuMont. Large symbol with extra line around represents voltage source. Small symbols without surrounding line show circuit points connected to source.



(Above) Fig. 2. Assortment of arrowheads which can be used to indicate current flow in more than one bus.



the power supply. To make tracing even easier, the arrowheads can be numbered in sequence. Arrowheads can be added to the diagram to indicate the flow of current through a B+bus to the +250 v point in the low voltage supply. Where there is more than one key circuit to trace out, different arrowheads can be used. Some of the different types of arroweads which can be used are illustrated in Fig. 2.

Power supply connections can be quite involved. It may be necessary to trace the connections from the plate of a given stage all over the schematic before getting back to the B + supply point. Sometimes this results in following wires that lead to blind alleys. It is then necessary to return to the last junction and taking another turn, very much like in the maze puzzles children play with, until the correct path is found. However, it is usually simpler, both in maze puzzles and in this kind of diagram, to start at the end and work back. It is easier to start at the B+ output of the power supply and to follow the B+ distribution line back to the various stages.

In recent schematics, some have tried to eliminate some of the confusion caused by the maze of interconnecting lines. These lines have been omitted and keyed symbols used to show which circuit points are connected to which power supply points. Each power supply point of a given potential in the diagram has a symbol drawn next to it, but with an extra line surrounding the symbol. Other points in the diagram which are connected to the power supply point do not have conecting lines, but instead have a smaller symbol of the same kind, without the surrounding line. Two examples are shown in Fig. 3 Use of this method minimizes the number of connecting lines.

SMALL BATTERY CAMPAIGN AIDS



Window streamer and combination counter card and battery display stand, designed to promote alkaline dry-cell B (RCA VS216) and redesigned As (RCA VS236), which are said to provide up to ten times more playing hours than conventional battery combinations previously employed in most small personal type portable radios. Counter card, a two-color self-supporting type, measures 17" high and 14" wide.

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TEST SIGNALS UP TO 80 FT.

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Pickup Compensators

(Continued from page 21)

cut may not be included in the circuits immediately ahead of the pickup, since the main treble tone control can be used for this function. Bass boost, however, is always introduced in these early stages, so that any hum generated in low-level stages will not be boosted along with the signal bass frequencies. Simpler compensator circuits for magnetic pickups use a compromise bass turnover frequency of about 500 cps, while some record compensators provide a multi-position

48 • SERVICE, JANUARY, 1953

switch which brings into play the proper circuit for equalizing both the bass and the treble of various types of records.

The dc resistance into which the magnetic pickup works has the opposite effect from the resistive load of a crystal; it introduces treble losses instead of bass losses. This effect can be used for equalizing treble preemphasis. When separate magnetic cartridges are employed for standard and lp records, a measure of variable equalization may be introduced by decreasing the load resistance for the lp cartridge. A small resistor of about 5,000 ohms is wired directly across the lp

cartridge terminals. Since the treble preemphasis of 78 records is in general less than that of the microgrooves, the added resistor automatically corrects the equalization when cartridges are changed.

Preamplifiers for Magnetic Pickups

Although it is possible to buy variable record compensators (for magnetic pickups) by themselves, this compensation is usually incorporated in the circuit of an electronic preamp, most commonly a dual triode stage with the two sections connected in cascade. A preamp is required because the output of the magnetic pickup is inadequate to drive the ordinary audio amplifier. Crystal pickups have signal outputs ranging from about 1/2 to several volts, while magnetic pickups have much smaller outputs, in the range between 10 and 100 millivolts. This disadvantage of magnetic pickups is offset by their high quality.

Preamps are rated in much the same way as amplifiers, except that many of the standards to which the power output stage must conform do not apply. The preamp should have a low hum level (at least 60 db below output) low harmonic distortion (preferably less than 1%), and accurate frequency compensation.

Some preamps contain their own power supply, while others furnish leads for tapping power from an amplifier or tuner (Fig. 5, p. 21). The amount of power used is very small (.3 amp heater current, and 2 or 3 mils plate current), so that overload of the supply from which power is borrowed is not a danger. There is one extremely important consideration relative to this power supply, however; hum. A1though the preamp contains its own B+ filter sections no supply point which is not very well filtered should ever be used. Occasionally even the selection of a physical point at which to connect the ground lead may be a factor in keeping hum low. The heater supply should be carefully selected also, and heater circuits which merely ground one side, rather than grounding the center tap of the filament winding or of a bridging resistor, should be avoided. The best type of heater circuit to connect to is one in which the heater winding is grounded through the center tap of a hum balancing potentiometer.

In general, it will be found that power is best borrowed from audio stages, whether on the tuner or amplifier, because purely *rf* chassis' do not require as careful hum precautions in their design. Where the preamp has its own independent power supply the relative polarity of its line plug, and the extent of electrical bonding between the preamp and other chassis', may affect the hum level. The phono preamp is potentially the greatest single source of hum in the entire radio-phono assembly.

The preamp should be located physically near the pickup so that the pickup lead can be short, to avoid high frequency losses and opportunities for hum pickup by the lead.

Many modern audio amplifiers, and tuners with audio stages, include a preamp stage for magnetic pickups. Care must be taken to avoid connecting crystal pickups through such preamp stages, or excessive gain and boomy reproduction will result. Similarly, if the output of a preamp is accidentally connected through a crystal compensating network the treble frequencies will be unduly boosted.

Available also is the capacitive or FM pickup, designed to frequency modulate a supersonic carrier signal created by the circuit to which it is connected. It, therefore, requires a special type of preamp containing its own oscillator.

Some years ago scratch suppression was attempted by the use of resonant filters which attenuated a certain band of frequencies in the mid-high range. Today, it is recognized that surface noise covers the entire audio spectrum but becomes more apparent as the frequency goes up, and the above method has been abandoned. Present-day methods of combatting record surface noise (especially from older shellac records) include:

(1) General treble attenuation by the tone control.

(2) Sharp treble cut-off at selected predetermined frequencies. This method is made available in some record compensators, and is superior to turning down the treble control, as it leaves a maximum frequency range for the recorded signal, while eliminating the worst of the high frequency noise and distortion.

(3) Volume expansion (increasing amplifier gain for loud signals, relative to the gain for weak signals). Although this feature is introduced primarily to increase the dynamic range of the music, it also has an apparent scratch reducing effect, since it allows the music to be played at a lower average intensity level.

(4) Dynamic suppression of record noise. The *Scott* system of noise suppression, which is included in several makes of amplifiers and in the *Dynaural* preamp, automatically controls a variable treble cut-off according to the frequency content of the signal.



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by M. W. PERCY

Review of Circuits Used in Printed-Circuit AC-Clock and AC-DC Table Models ... UHF 3-Channel Translators ... Constant-Amplitude Oscillator System



Fig. 1. Hallicrafters foto-etch chassis circuit, featuring provision for a clock.

PRINTED CIRCUITRY, described on several occasions in Service,¹ has now been adopted as a production technique by several manufacturers for table models.

In Fig. 1 appears the circuit of one such set utilizing a foto-etch chassis for a clock radio.

In this method, the base of the chassis is formed by laminating a sheet of Formica and copper under high heat and pressure until a perfect bond is achieved.

The copper side of the sheet is then covered with an emulsion. A negative of the circuit is laid on the emulsion, an exposure made and the base is then developed like a photographic plate. Next, the sheet is given an acid dip, which washes away the unwanted copper, leaving only the lines of the circuit.

Small holes for the tube sockets and the leads of small component parts such as capacitors and resistors are then automatically punched in the base and the parts manually mounted

¹September and October, 1952.

Fig. 2. View of Hallicrafters pc clock-radio chassis.



in position. The sheet is then dipped into a non-corrosive cleaning solution which is followed by a single dip into a solder pot which solders all connections in one operation.

The clock radios have a standard broadcast receiving band, a *wake-up* switch connected to the radio, and built-in antenna.

As indicated earlier, in servicing these chassis one must avoid carelessness in making solder joint connections. If one is careless and splatters solder around over the bottom of the chassis plate, some short circuits will occur between the wiring that's photoetched on the chassis base. Some Service Men may become apprehensive about pc sets, fearing that they cannot replace components in this type of receiver in the manner that they're normally accustomed to when servicing wired chassis. There is no need to be so concerned, since conventional



Fig. 3. Circuit of G.E. 103 uhf translator which provides for three-channel pickup. In the first, second and third uhf switch positions, the output transformer *T*₁ is connected to receiver transformer, and the vhf antenna is disconnected. In the fourth position, or vhf contact, the output is disconnected, and *R*₁₁ (22,000 ohms) is switched in to drop *B*+; the vhf antenna is connected to the receiver antenna.

components such as tube sockets, *if* transformers, resistors and capacitors are used and readily removable and replaceable. The Hallicrafters' *pc* chassis only uses the photo-etch process to provide wiring connections between sockets and components.

According to Hallicrafters there are available a replacement supply of photo-etched chassis plates should any replacement ever be needed.

The model illustrated is an ac type. Available too, from another source¹ is an ac-dc model, using the same tube lineup, but without a clock in the circuit. In making voltage readings or resistance measurements, test leads with needle point prods should be used to avoid possibility of shorts between sections of the printed circuit wiring.

UHF Translators

To permit reception of three uhf channels on vhf receivers, there has been developed a detent switch-type unit (G. E. 103; Fig. 3), which can

¹Admiral 5C3 chassis.

be installed inside of the TV cabinet. As shipped from the factory, unit has its output stage tuned to channel 5, to which the TV receiver must be tuned. However, output stage can be

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realigned for channel 6 operation, should 5 be active.

The Service Man must individually adjust each of the three *uhf* positions (Continued on page 52)

Fig. 4. Circuit diagram of NBS constant-amplifier oscillator. The unit utilizes one-half of a 12AT7 twin triode as an oscillator and the other half as a clamper tube. A 6AL5-diode rectifier across the output of the oscillator supplies the input voltage to the clamper tube. The constant-amplitude oscillator is a source of *rf* voltage that has been found to remain reasonably constant irrespective of changes in tube parameters, supply or heater voltage, or load impedance.



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Ser-Cuits

(Continued from page 51)

for operation on the local active *uhf* channels. The tuning ranges of the three *uhf* positions are all identical and cover the entire *uhf* spectrum.

Constant-Amplitude Oscillator

In electronic equipment such as exciters, signal generators, and highquality communication receivers, the adjustable-frequency oscillators must be stabilized against changes arising from possible variations in circuit components. Automatic volume control systems have been modified to provide the stabilization, but it has been found that they have proved ineffective for class-C oscillators because of the self-biasing feature associated with this class of operation. Fixedlevel clipper circuits have also been utilized but the output waveform has normally contained strong, undesirable harmonic components.

To overcome these objections, a constant-amplitude oscillator has been developed. The circuit evolved at the Bureau of Standards[‡], and shown in Fig. 4 (p. 51), has been found to maintain the apparent grid-plate gain of the oscillator reasonably steady. The input and output capacitances have been held practically constant, and the clipping of the output waveform reduced to very low levels. The moderate amount of clipping that does occur is said to be due only to the diode detector across the oscillator output.

The oscillator was originally designed as a fixed-frequency local oscillator in a gain-stable receiver. It utilizes both sides of a 12AT7 twin-triode as the oscillator and clamper tube, respectively, and a 6AL5 diode detector. The grid tank circuit is composed of a fifth overtone crystal (30 mc), a frequency-shifting trimmer, and a crystal-peaking coil. A coil in the plate circuit of the oscillator section of the 12AT7 serves to resonate at the crystal frequency.

The clamper tube is initially biased in the region of plate cutoff. The oscillator output, after rectification by the diode, is applied as a positive voltage to the grid of the control tube, the other half of the 12AT7. When the oscillator output voltage reaches a sufficiently high level, the clamper begins to draw plate current and causes a reduction of plate voltage. Because the oscillator is connected to the same plate-dropping resistor, it too suffers a reduction of plate supply. Thus, the tendency of the clamper, as the oscillator output voltage increases, is to

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Fig. 5. Installing G.E. translator in TV chassis.

maintain the final output voltage at a relatively fixed level.

The bias for the clamper tube is usually obtained from a low impedance source of constant potential. In the test model of the constant-amplitude oscillator, bias voltage was obtained from batteries with internal resistances of about 5 ohms. Normally, the bias voltage is adjusted so that the control tube is always slightly conductive at the minimum level of oscillator voltage anticipated. Hence, positive control action is available at all times. Under these conditions, the best regulating characteristics are obtained with the largest plate-dropping resistor that still permits the desired plate voltages. A plate-dropping resistance of 40,000 ohms was found to give satisfactory operating conditions.

An experimental investigation of the effect of different plate-loading resistances on the oscillator output voltage revealed that a resistance of 10,000 ohms permitted a 12-volt variation for a change in plate supply from 200 to 350 volts. A plate-load resistance of 40,000 ohms, however, restricted the output variation to 1.5 volts with the same change in plate supply. In both of these instances the bias supply voltage was held at 18. It was noted that output voltage is determined largely by the bias voltage with the plate-loading resistor adjusted for satisfactory regulation.

Improved clamping may be obtained by employing a voltage-multiplier type of rectifier to drive the clamper tube. Thus, a greater ratio of dc control bias to rf output can be obtained, resulting in better regulation. Also, if a power amplifier replaced the clamper portion of the 12AT7, its greater plate-current capabilities will result in more positive control action. Further, if the clipper diode is fed from the final output of the oscillator-buffer circuits with more gain included between the oscillator and the rectifier-control circuit, the sensitivity to small changes in output will increase and improved stability will result.

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PartII..TheServiceMan's

Role in the Hi-Fi Market

UNLESS ONE is looking for an excuse to stay out of the hi fi picture, the Service Man's position in the distribution network is as strong and indispensable as ever. It is important to remember that the Service Man who is invited into the homes to service radios, TV, appliances, etc., represents the one group who know at first hand the individual's needs, tastes, and financial capabilities. In most cases you are Mr. Music to the buying public in your neighborhood and you have their confidence. This adds up to a highly encouraging position which should at least entice a fair share of prospects if you set the stage a little and do a reasonable amount of promotion.

It was noted that a Service Man's position was not only strong, but indispensable. That happens to be true, for the most part. While quite a good deal of hi fi sales are being made to the experimenter and hobbyist (similar to the interest and activity displayed in the radio amateur field), the great bulk of complete system sales, which incidentally account for the major share, go to the out and out music lover who is interested in the result and not the cause. No one package is going to satisfy these golden ears. Not only do these people require service but more often as not want the system installed in a special way or place. And that's just where you come in-service; that's you. You can survey a prospect's requirements, engineer the system which consultation with both the customer and your jobber indicates will be most suited to his needs, make the installation and provide him with future maintenance as may be required from time to time.

Despite recent competitive trends in marketing *hi-fi* equipment, Service Men will find that jobbers can be used to considerable advantage in establishing one's self. First, your plans should be discussed with the jobber in detail, and every effort made to con-



vince him that you are serious about it. You will find that he will begin to turn over to you for follow up, leads that have come his way, often from the manufacturers of hi-fi equipment who receive hundreds of letters from individuals who write directly. Certainly the last thing a jobber wants is the burden of surveying the customer's needs, nor has he any inclination to do an installation or follow up service calls. In fact, he barely has time to check on leads and welcomes the opportunity to turn them over to reliable and loval Service Shops.

Many jobbers today already have or are in the process of setting up audio demonstration rooms or salons. It has been found that most jobbers openly invite Service Men to bring their customers to such studios, use their facilities and the guidance of their sound specialists, and offer protection in consummating the sale. Access to such facilities is a worthy and valuable asset which you should attempt to exploit, and which can be easily accomplished by merely an understanding with your jobber. This has been accomplished in many places in the country to the extent where even the Ican get it wholesale customers find it possible to work equitably with the Service Men.

Working with a jobber makes it possible not only to start in the *hi-fi* business, but *remain in it profitably*. By having available to you the lines and stock of your jobber, your own investment in components and parts is reduced to a simple working and turnover level.

Having established the existence of three major markets and discussed the problems therein, let us examine the merchandising of audio from the point of view of application. Obviously, a *market* is simply descriptive of the *place* in which audio is to be used while the application describes the *function* of audio. An excellent chart listing *basic* uses for audio, showing the relation of place and function, appeared in the initial installment last month.

Though it is possible to evolve a chart in even greater detail (one need only to refer to a dictionary and list every conceivable application starting with A bbey and ending with Z oo), the chart offered is a practical, workable one in which ten functions transgress the specific applications to result in thousands of opportunities for the alert Audio Man. When one realizes that all this can be accomplished with virtually the same pieces of equipment, the great potential which exists in the audio business becomes apparent, and extremely stimulating.

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Selenium Rectifier Tester

(Continued from page 22)

Two operations are involved and, if used properly, a good indication of the quality of the rectifier will obtain. This test method, or some slight variation of it, is used as a production test by most of the manufacturers of selenium rectifiers. The forward test measures the non-linear conducting resistance of the rectifier at the operating voltage by the E-I method. This test is important, as excessive forward (conducting) resistance can cause low output voltage, ripple and resulting hum, and overheating of the rectifier, causing it to age (further increase in forward resistance) or burn out.

The reverse test measures reverse leakage current (current which flows through the rectifier in the blocking direction) at the rated PIV of the stack. Excess reverse leakage will definitely cause the stack to overheat and thus age quickly or burn out. It can also cause a low output voltage or, if the leakage is extremely high, cause damage to the electrolytic.

Although these two tests give an adequate check, they are not often used by Service Men, because the equipment is expensive and also offers various technical problems, such as the difficulty of building protection against shorted stacks into the circuit. Also, if the two circuits are combined into one, the forward test would read good upscale and the reverse test would read good downscale, necessitating a pair of opposing meter scales which could lead to confusion. (The reverse circuit could be used for electroforming.)

Practical Tester Requirements

From the foregoing, it is apparent that a practical and economical tester would have to provide a positive rapid indication of short-circuited and open rectifier stacks; a definite indication of excessive forward resistance and excessive reverse current; an electroforming circuit; scale readings in the same direction for both forward and

¹Galvanic Seletester.



Fig. 2. Forward test which measures non-linear conducting resistance of rectifier at operating voltage by E-I method.



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Fig. 3. Reverse test which measures reverse leakage current at rated PIV of stack.

reverse test; positive protection for the meter and other components when shorted stacks are tested; indication that a stack is electroforming, and protection for the meter when the reverse leakage current is high during electroforming; whenever possible, the ability to test the rectifier in the set without unsoldering any wires; and portability.

To meet these specifications, the tester¹ diagramed on the cover was developed.

In this instrument the problem of a single scale has been solved by a change in the forward circuit, which makes it possible to measure the forward resistance as a function of the voltage across the rectifier with the rated current flowing through it, rather than by measuring it as a function of the forward current with a fixed voltage across the stack.

Protection Circuit

Protection against short-circuited stacks has been provided by means of a special relay circuit, which connects the meter in the circuit only when the reverse current will read on scale. The meter is also protected against excessive forming currents by a rectifier plate acting as a parallel non-linear resistance. This causes considerable cramping at the high end of the scale so that no matter how high the reverse current is when a stack is forming, the needle will still be on scale. This provision allows the reverse circuit to be used as an electroforming circuit; and the user is always aware of the forming progress, since the drop in reverse current can be continuously observed.

When the tester is used to test all rectifiers in half-wave circuits, no connections need be broken; the stack can be tested as it is connected in the set by turning the switch to off and removing any one tube. In the case of doubler circuits, however, the units can be tested by unsoldering two of the three wires involved.

Tube News

(Continued from page 26)

miniature T-61/2 construction, and said to be capable of furnishing large



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★ Think of it ... hundreds and hundreds of Radelco U.H.F. Antenna installations in Portland ... and not a single, solitary complaint. The Portland Proving Graund was quick to prove that Radelco engineers know how to design and make antennas for Ultra High Frequencies. The Radelco Model US:102 antenna is a high gain job. Gain increases with increasing frequency... this means that the antenna compensates for the decreasing wave length at the high frequency end of the band. It is a tried, tested and proved antenna ... proved to outperform them all. Better get Radelco, because you can't get a better U.H.F. antenna!

7580 GARFIELD BLVD.

CLEVELAND 25, OHIO

output voltages across low values of load resistance and supply voltage. Has separate suppressor grid connection. The heater may be operated from either 6.3 or 12.6 volts.

UHF ANTENNA

MODEL US-102

DOUBLE STACK

Completely preassembled. Matches 300 ohm line. Durably

constructed of finest materials.

Shipped as shown above, less

For remote fringe areas. Model

US-104 Quad Stack with Jumper

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PRICE

A nine-pin miniature power pentode (6CL6) for use in the video output stage has been added to another tube line.²

Video Circuit, Voltage Gain

Using this tube it is said to be possible to obtain a voltage gain of from

2G. E.

40 to 45 in wide-band video circuits. The tube features high transconductance, low capacitances, and high output current capability.

Peak-to-Peak Output

The tube is claimed to provide a high plate current at low plate voltages and able to supply enough peak-topeak output voltage to drive large picture tubes with high efficiency and low amplitude distortion. It is capable of supplying 132 volts peak-to-peak output across a load resistor of 3,900 ohms.



So compact they fit anywhere. So many listings (over ten dozen) that you can meet any capacitance, voltage and combination requirement. Yes, singles, duals, triples and auads.

Multiple-section units have stranded wire leads and safety sleeves. Hi-purity aluminum construction minimizes corrosion. Vented for excessive gas pressures.

If ever there was a Jack-of-alltrades electrolytic, this is it— Aerovox Type PRS Dandee.

Ask your Aerovox distributor for Aerovox Dandees. Ask for latest catalog—or write us.



CATALOGS. BULLETINS

RCA Victor, Tube Department, Harrison, N. J., is now distributing the '53 edition of its pocket reference and calendar notebook. Pocket book contains technical information on picture tubes, receiving and transmitting tubes, electronic components, test equipment, batteries and miniature lamps. Includes 16-page color maps, 58-page diary, and TV troubleshooting data.

JFD Manufacturing Co., Inc., 6101 16th Ave., Brooklyn 4, N. Y., has published a 36-page catalog, TV Almanac, No. 450. describing in detail indoor and outdoor antennas, lightning arresters, boosters, couplers, wave traps, ballasts, mounts, screw eyes, tools, phono switches, and accessories. * * *

Jensen Industries, Inc., 329 S. Wood St., Chicago 12, Ill., has released a brochure, Your Favorite Phonograph Records' Best Friends, discussing advantages of diamond-pointed needles, and offering helpful hints and facts on records, cartridges, etc * * *

Blonder-Tongue Laboratories, Inc., 526 North Ave., Westfield, N. J., has issued an installation manual, The B-T Unit System for Better TV, providing tech-nical data on all types of master TV systems. Included are layout of a master system, type of transmission line to use, location and installation of various units, and methods available for the elimination of ghosts and other interference.

Ram Electronics Sales Co., Irvington-on-Hudson, N. Y., has published the '53 edition of TV Replacement Manual, with over 6,200 listings covering manufacturer's name, chassis and model numbers and corresponding Ram part numbers. Manual, with 32 pages, also features Manual, with 32 pages, also features schematics of typical circuit applications Priced at \$1.00.

Brach Manufacturing Corp., 200 Central Ave., Newark, N. J., has released a book-let, *How to Select UHF-TV Antennas*, that outlines the major differences between *vhf* and *uhf*, and solutions to prob-lems that may arise. Detailed also are uhf multiple installation systems.

John F. Rider Publisher, Inc., 480 Canal St., New York 13, N. Y., has released TV Manual Vol. 10 which features three separate sections: manufacturer's servicing information ; replacement parts listings; and production changes, trouble cures and servicing hints. Book contains equivalent of 2,350 pages, priced at \$24.00.

TEN YEARS AGO

TEN YEARS AGO Service Men were declared essential to the proport of the war effort, according to a bulletin subject of the war effort, according to a bulletin subject of the war effort, according to a bulletin even of the war effort, according to a bulletin subject of the war effort, according to a bulletin even of the war effort, according to a bulletin subject of the war effort, according to a bulletin even of the war effort, according to a bulletin with a reversible motor for the turnthe and work of the turnthe and work of the turnthe and the cover feature. A choop circuitry, 1,5-volt even feature. A merican Institute of below and the Meissner, Stromberg-Carlson a warded to Maior Edwin H. Armstrom, Meissner, Billis Travers was appointed for eyes of the first and public relations at Crosley. Meissner M. Bullet was named vise president of builts of the subject was and assistant sales intend W. Bullet was named assistant sales



Chicago 25, Illinois Manufacturers of Electronic Equipment Since 1928

enma-

Rep Talk

THE REPRESENTATIVES of Electronic Products Manufacturers, Inc., has become the official title of this national organization. A meeting of the group's board of gov-ernors was held recently at the Hotel Congress in Chicago. Members of the board now include: R. W. Farris (Mis-souri Valley), B. C. Landis (New York), David N. Marshank (Los Angeles), Wil-liam E. McFadden (Buckeye), M. K. Smith (Dixie), and W. S. Trinkle (Mid-Lantic).... Twenty-three more (thirteen seniors and ten associates) have been admitted to the Rep's membership; total membership is 574, with New York chap-ter's 81 members the largest single unit. Seniors elected to the New York Seniors elected to the New York chapter are: Al Gary, 1961 Broadway, New York 23; Carrol S. Banfield and Richard Gentry, RSA Co., 68 Hudson St., Hoboken, N. J.; Hy Bloom, 8 W. 18th St., New York 11; Jerry Greenberg, 1902 Avenue L, Brooklyn 30; Harry Miller, 1180 Raymond Blvd.. Newark 2, N. J.; Robert A. Stang, 79 Storer Ave., Pelham, N. Y.; and William W. Weiss, 509 Fifth Ave., New York 17.... Senior members elected to the Chicagoland chapter in-Ave., New York With the Chicagoland chapter in-clude: Harry Monson, 919 N. Michigan Ave., Chicago 11; William M. Linz, 7115 N. Mobile Ave., Chicago 31; and Dayton L. Warner, 15423 Honore Ave., Harvey, Ill. Associates include: William K. Faw-cett. Ridley Associates, 1551 N. Austin Blvd., Chicago 51; Roy J. Bouda, Wil-liam E. Burgoyne, 7001 N. Clark St., Chicago 26; A. A. Sroka, Roy J. Magnu-son associate, 4258 W. Irving Park, Chi-cago 41: and Robert Engstrom, Harry W. Gebhard associate, 5129 W. Devon Ave., Chicago 30. . . Seniors elected to Mid-Lantic chapter were: George A. Shelps, 9 Chelsea Lane, Allentown, Pa., and Paul Williamson, 720 Rittenhouse, Philadelphia 44, Pa. Associates elected were: William G. Bauer, Jr., and Charles W. Janton, Jr., associated with Wilmer Ill. Associates include: William K. Fawwere: William G. Bauer, Jr., and Charles W. Janton, Jr., associated with Wilmer S. Trinkle. 2 Roberts Block, Glenside, Pa.; Tom Cox, R.S. 1, Green Lane, Pa.; Horace C. Johnson, associated with An-drew A. Foley, 640 Federal St., Camden, N. J.; Arthur J. Stobbart, associated with L. D. Lowery, 50 E. Wynnewood Rd., Wynnewood, Pa.; and W. H. Watt, 225 S. 69th St., Upper Darby, Pa. ... Perci-val Ridley has been elected president of the Chicagoland chapter. Other officers the Chicagolaud chapter. Other officers elected included Roy J. Magnuson, vice president. Roger Clark, treasurer, and Karl Engle, secretary. ... Ralph T. Sul-livan has moved his offices to 1551 N. Austin Blvd., Chicago 51, Ill. Bruce Matson has joined the firm as an asso-ciate. . . . George S. Gordes, formerly connected with Fafnir Bearing Co., has connected with Fahnr Bearing Co., has become a member of the sales staff of Henry Lavin Associates, Box 196, Meri-den, Conn. . . Adolph L. Gross Asso-ciates, Inc., 45 W. 45th St., New York, N. Y., have been named reps for General Hi-Fi Speaker Co. in metropolitan New York. Robert Hertzberg has resigned as vice president of the company Lee YOR. Robert Herizberg has resigned as vice president of the company. . . . Lee Naylor has been named rep for Channel Master Corp., in the northwest territory. . . . Nat Louis, 1867 Kapiolain Blvd., Honolulu, T. H., is now a rep for Don Good, Inc., in the Hawaiian Islands. . . . William J. Doyle, vice president in charge of sales of The Astatic Corp., has re-

of sales of The Astatic Corp., has re-signed his position, and will become a rep in the Chicago area.



- 12 driven elements on high band!
- 8 driven elements on low band!
- High gain—low noise!
- One antenna—one transmission line!
- Total weight only 8 lbs.!



Here's the key to more and more installations in fringe areas-the new FINCO 20-in-1 Antenna that provides the best reception over 100 miles from stations. Your customers will say "you are a magician" when they compare FINCO reception with any other antenna. You can build yourself an outstanding reputation by recommending the FINCO 20-in-1 because every satisfied customer tells and sells another. Get your share of the profitable sales that are just waiting to be made in areas where good reception has never been available before by getting acquainted with the FINCO 20-in-1 today. See your Jobber.

...Preassembled for easy-fast-simple installation The Finney Company 4612 ST. CLAIR CLEVELAND 3, OHIO

On the dias at the recent annual stag dinner party of the Reps at the Woodstock Hotel, New York City, left to right: Joe Sprung, Jules Bressler, James Pickett, Wally Shulan. Standing, left to right: Sam Shaw, John Kopple, Dan Bittan, Leo Freed, Bob Breuer and Bill Gold.







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- (a) Long Life
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- (a) Various sizes and shapes
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60 • SERVICE, JANUARY, 1953

Associations

ARTSNY

THE ASSOCIATION OF RADIO and Television Servicemen of New York has altered its setup and established two chapters within the group, devoted to the business and technical aspects of the profession, with elected officers and board members for each chapter.

Under the new arrangement, Max Liebowitz will serve as prexy and executive director, while Sid T. Perlin will be treasurer. Business chapter officers include: Phil Goldfarb, vice president; Arthur Rhine, corresponding secretary; Jerry Macheronne, recording secretary; John Lacey, financial secretary; Jack Ornstein, business director; and Lew Gioia, sergeant-atarms. Members of the business board of directors include: Jack Katz, Arthur Kummel, Peter Cusimano, Edward Eisen and Kingsley Sherwood. Technical chapter officers are: O. Capitelli, vice president; Harold Levinson, corresponding secretary; Jacob Allen, recording secretary; Joe Guarnieri, financial secretary; Lou Benz, technical director; and Sid Cornfield, sergeant-at-arms. Members of the technical board of directors include: Harry Temler, Harry Oxer, John Wagonny, Ted Caumont and Henry Levine.

The technical chapter will hold meetings on the first and third Thursdays of the month, and the business chapter will hold meetings on the second and fourth Thursdays. All officers and members of the board of directors of both chapters will have their own executive meetings once a month.

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6 full, machined threads provide "bulldog" grip, anchor the screw-eye for good! No stripping of any screw-eye, no slipping of strap! Reinforced "arch-bridge" construction prevents bending or buckling of clamp no matter how much the stand-off is tightened. Ultra-low loss polyethylene insert and sturdy electro-galvanized steel strap for universal mounting on any mast up to $2\frac{1}{2}$ " od. Available for both single and dual lead-ins in $3\frac{1}{2}$ ", $5\frac{1}{2}$ ", $7\frac{1}{2}$ " and 12" sizes.

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Antenna Measurement

(Continued from page 29)

tion of the towers to eliminate all these effects. Without careful planning, however, a range of this type can become very cumbersome and inflexible. In Fig. 2 (p. 28) appears a range layout found to provide complete control of test. By placing the transmitting antenna on the ground and the receiving antenna on the roof of the lab, harmful reflections have been entirely eliminated. Reflections from the ground and from the building bounce up into the air away from the antenna under test. There are no objects directly behind the antenna to cause reflection. All radiation arriving at the antenna under test arrives from one direction only.

The transmitting antenna used in this instance is a corner reflector type with interchangeable dipoles. A photo of this antenna with the vhf dipole in place is shown in Fig. 3 (p. 28). The corner has considerable gain, which makes it possible to use a precision low-power laboratory signal generator, and also eliminates interference to TV sets operating in the vicinity of the lab.¹

Antenna gains can be measured on this system by substitution of a standard antenna. The accessibility of the test site makes this process very rapid.

Auxiliary equipment is available for recording automatically antenna patterns. This consists of a precision rotator which is electrically coupled to a polar recorder. As the antenna is rotated, a turntable turns in complete synchronism with it. After turning on the signal generator and tuning the receiver, a single control causes the antenna to rotate and the recorder to plot its radiation pattern.

With the automatic recorder a complete set of radiation patterns of an antenna at all frequencies of interest throughout the vhf and uhf bands can be taken quickly and accurately.

The Meaning of Voltage Standing-Wave-Ratio

As indicated earlier *vswr* is a particularly important factor in antenna design. If energy is introduced into a transmission line of a given characteristic impedance, it will flow to the end where a certain part enters the termination (antenna, receiver, or

¹A military type APR-4 receiver has been tested and found adaptable for use in the system. . . The input circuit of the receiver which is normally 50 ohms unbalanced must be modified so that it is very accurately 300 ohms balanced, and the output circuit must be modified to remove certain non linearities which were not important in the military applications. With these two modifications the receiver has been found to meet all the requirements for a detector in the system; viz., it presents a matched load, its output is linear, it rejects unwanted frequencies, it is sensitive, and it is easily and rapidly tuned. Announcing THE FERALOY Extra Long Life-Tip Same size as standard tip of the Wan Soldering Gun but specially coated to protect LASTS 20 against corrosion and silver platec to insure continuous TIMES AS good electrical contact and heat transfer. It stays tinned LONG indefinitely, never requires dressing, is more rigid, retains full tip con-act area. Where soldering is constant and tip life is Important, (as in factory production or bench work) this Feraloy Ip is terrific. One 50c plant reports standard lips had to be changed every half hour-Wen Feraloys every two weeks. MAKERS OF THE BETTER ELECTRIC SOLDERING GUN The 250 Watt electric soldering gun that's Underwriter's approved. Its excellent design and construction preven overheating, so MO DUTY CYCLE; can be used almost constantly. Operates on 120 Volt AC, 60 cycle. Mandles all soldering requirements 50 to 250 Watts. Retails \$12.95. Fully guaranteed. EXPORT AGENTS, SCHEEL INTERNATIONAL, INC. . CHICAGO 18, ILL. PRODU 5806 NORTHWEST HIGHWAY . CHICAGO 31, ILL.

other transmission line) and a certain part is reflected. The reflected wave combines with the original wave to produce a standing wave on the line. The ratio of the maximum voltage to the minimum voltage is the voltage standing-wave-ratio or *vswr*. Only if the impedance of the termination equals the characteristic impedance of (Continued on page 62)

Fig. 7. View of slotted line and balun used to measure vswr.







SELENIUM RECTIFIER TESTER

Tests all types 20 to 650 ma
 - 25 to 300 VAC.

• Gives positive indication - GOOD or BAD - on 3" meter. Shows voltage drop across rectifier under load.

• Novel system gives correct setting, even if rectifier rating is unknown. • Small, compact – 7" x 3¹/4" x 4¹/4". Has permanent, "lossproof" color-coded test leads.

• Operates on 110-125 VAC. "Line Adjust" for accurate testing.

• Model 710 Dealer Net Price only \$29.50. See it at your distributor's.



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Antenna Measurement

(Continued from page 61)

the line will there be no reflected energy. When an antenna intercepts energy it reradiates part of it and delivers the rest to the tranmission line. The *vswr* of the antenna when used as a transmitter is simply related to the loss of signal caused by reradiation when used as a receiver. Only when the antenna impedance is the same as the transmission line impedance is reradiation a minimum. The loss incurred by having an antenna with varying degrees of mismatch is illustrated in the graph of Fig. 6 p. 29).

The method of measuring gain described previously takes this loss into account. Nevertheless, for design purposes it is useful to know the *vswr* of an antenna.

A slotted line and balun for measuring vswr's is shown in Fig. 7 (p. 61). The combination of balun and antenna produces exactly the same mismatch in the 75-ohm coax line as the antenna alone produces in 300-ohm twinlead. This scheme is used because of the many difficulties in vsver measurements on open lines.

Servicing Helps

(Continued from page 39)

be run from the top, not ground, of this 150-ohm resistor to the fringe position of the maximum performing selector switch on the rear of the set, so that when in a fringe position maximum contrast can still be obtained.

High Voltage Breakdown and Corona. . . . Chassis 200, 201 : To reduce tendency to breakdown or corona, the 1B3 filament winding should be moved as far from the hv winding as possible. The lead that goes from the 1B3 filament to the picture tube anode connection should be attached to pin 2 instead of pin 7, and all sharp points of solder on the socket lugs should be removed. All 1B3 socket lugs should be bent toward the center of the socket. and the lug on the electrolytic capacitor located under the 1B3 bent down as far as possible. All sharp points-should be removed from the flyback transformer lugs. The 1B3 socket, transformer lugs, and top of the damper-tube socket, should be sprayed with a plastic spray.

Stopping Pix Smear in 24-Inch Models: In Hoffman sets (chassis 187 series), if the red deflection yoke lead is dressed too close tothe picture tube cathode lead, the yellow lead connected to the picture tube socket, horizontal voltage pulses will be coupled to the picture tube cathode, causing the picture tube to draw grid current on the negative portion of the voltage pulse. There is also the possibility of the horizontal pulse reaching the sync circuits via the picture tube cathode lead and rc circuit between this lead and the first sync separator. If the coupling is severe enough a Christmas tree condition is apt to occur. To remedy, the yellow cathode lead and red yoke should be dressed lead away from one another, taking care not to dress the red yoke too near the 6BL7GT.

6BK7/6BQ7 Interchangeability in Cascode Tuner: In Hoffman service manuals, it has been noted that either the 6BK7 or 6BQ7 can be used in the rf stage, but that the two types are not directly interchangeable. Substitution of the same tube type was recommended. However, should necessity require that one type be substituted for the other the tuner alignment should be checked and corrected if necessary, since the interelectrode capacities of the two types differ enough to affect the tuned circuits in the tuner.

RCA TV Service Hints

AGC Threshold Control Adjustment: The agc control on RCA chassis** is adjusted at the factory to provide maximum possible gain without clipping sync for all signals above the receiver threshold up to 25,000 microvolts. The adjustment of this control should not be touched in the field unless it is definitely known to be incorrect. If the control is misadjusted so as to increase the receiver gain, it may overload when a strong signal is received, or when a weak signal temporarily increases in strength due to unusual propagation conditions. On the other hand, if the receiver gain is lowered by the agc control, the sync noise immunity is reduced.

To reduce the prominence of snow on weak signals it is important that the picture control not be operated at its maximum clockwise position. Such an adjustment will provide a higher contrast picture but at the same time may produce an apparent poorer signal-to-noise ratio, due to the fact that an excessive amount of signal on the picture-tube grid causes the snow to bloom or defocus, thus causing the flake particle to become larger and more prominent than normal. At the

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same time it is equally important that the receiver be focused to obtain the appearance of the least amount of snow in the picture. To do this, the receiver should be focused by the method described in the service data. As a final adjustment, the focus control should be adjusted for the appearance of minimum snow in the picture.

Conditions for AGC Adjustment

Only under two conditions can it be considered permissible to adjust the *agc* control. In an area where the signal is so weak that the snow prac-

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tically obscures the picture after having taken all the foregoing precautions, then the *agc* control may be adjusted to give the best signal-to-noise ratio. It should be recognized, however, that trouble from loss of sync noise immunity might be experienced.

Adjustment for Strong Signal

The other condition which would justify adjustment of the *agc* control is where a signal of over 25,000 microvolts is received. Under this condition the *agc* control should be adjusted until the receiver no longer overloads.

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^{**}Models 17T150/1/3/4/5/160/162/163/172/ 172K/173/173K/174/174K and 21T159/165/176/ 177/178/179



Audio

(Continued from page 42)

frequency-control circuit designed to prevent drift on the FM band and correct for normal errors in tuning. A switch is provided to disconnect the *afc* circuit. Oscillator radiation does not exceed 50 microvolts per meter measured at 100' and meeting RTMA specification REC-129-C. The input circuit to the FM section of the tuner provides for a 72 to 300-ohm input for use with a dipole antenna.

AM Receiver Requirements

On the AM band, a signal of 5 microvolts provides not less than .25-volt output. The AM section of the tuner includes a tuned rf stage and a twostage if system. An efficient automatic gain-control circuit is incorporated to minimize the effects of fading and prevent overloading on strong signals. A 10-kc filter is also provided to prevent inter-station whistle; the frequency response of the AM section is within ± 3 db from 20 to 7,500 cps. Temperature-compensating capacitors and coils are used to minimize drift. High-impedance antenna terminals are available for short antennas and separate low-impedance terminals provide for a low-impedance loop or a flat-top antenna with coax leadin.

Hi-FI Amplifier Specst

Reviewing hi-fi amplifier requirements, the spec data note that the unit should be complete with a power supply on a single cold-rolled steel chassis. The specific amplifier^a referred to, in this instance, was described as having a frequency response flat within ± 1 db from 20 to 20,000 cps; power output 10 watts at less than 1 per cent harmonic content; hum level 70 db below rated output; intermodulation distortion less than 1.3 per cent at 6 watts as measured on the usual intermodulation output meter and a damping factor 10 to 1.

Direct Radiator Speakers

Reporting on loudspeaker characteristics, and covering direct radiator types consisting of separate high and low-frequency pm mechanisms, the specs note that these units should be mounted coaxially together. Referring to the type^{*} they produce, it is noted that the response is 30-14,000 cps,

*Stromberg-Carlson AR-410.

⁴Stromberg-Carlson RF-471.

Vino, Mark, Picking Out the Right Amplifier, SERVICE; December, 1952.

Containers for replacement cartridges which feature a floating suspension to prevent cartridge from touching the case at any point, thus insuring the cartridge reaching its destination in perfect condition. Container also has a hinged top with a purse-type clasp. Model number and list price of cartridge appear on each end of the package. (Webster Electric Co.)



power-handling capacity 32 watts, angle of coverage 100° throughout the entire range, and impedance of the speaker system approximately 8 ohms at 400 cps. The low-frequency cone in this instance is heavy-weight ribbed and moulded fibre 12" in diameter with a $1\frac{1}{2}$ " diameter voice coil, while the *hf* unit is $3\frac{1}{2}$ " equipped with a 2" cone and $\frac{3}{4}$ " voice coil. Describing mounting, it is said that the speaker should be mounted on a 14" square baffleboard 1" thick, drilled with 12 clearance holes for No. 8 flathead wood screws for fastening in a cabinet.

Exponential Acoustical Labyrinth

The architects' and engineers' specifications also describe the requirements of an exponential acoustical labyrinth to provide an acoustically correct speaker enclosure for 12" and 15" coax speakers. The finished size, it is said, should be 357%" high, 23¼" wide and 18" deep, and provide direct forward exposure of the front of the coax speaker and acoustical loading of the back of the low-frequency cone by means of a 5' exponential air column folded on itself.

While the data in these specs refer to items produced by this manufacturer, it will be found that many of the general details will hold for equipment made by others. Thus, this information can serve as an example of typical specs which Service Men either might have to read or prepare. Exceptions will usually prevail in the speaker and enclosure required; the requirements will usually vary with the range wanted, area available and built-in or external housing demands.

Basic 10-watt amplifier for average hi-fi home system. Distortion at 10 watts said to be 1% harmonic and 2% intermodulation; frequency response at 3 watts \pm .5 db, 20 to 50,000 cps; frequency response at 10 watts. \pm 1 db 30 to 20,000 cps. (Model 100BA; Precision Electronics, 9101 King Ave., Franklin Park, Ill.



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 Output transformers
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Tiniest and biggest: Marty Thurnblad, grandson of Thomas A. White, Jensen president and general manager, with tiny experimental 2" subminiature speaker. On the left is giant 18" model used for commercial sound.



Turn-over pickup which is said to have an output of 30 millivolts at 10 cm per second, and can be mounted in any type arm. 260; Pickering and Co.) (Model

KNOWS HIS



SERVICE, JANUARY, 1953 • 65



UNIVERSITY LOUDSPEAKERS · INC 80 SO. KENSICO AVE., WHITE PLAINS, NEW YORK

66 SERVICE, JANUARY, 1953 SID HARMAN NOW EXECUTIVE V-P OF HARMAN-KARDON

Sidney Harman has resigned as vice president and general manager of David Bogen, Inc., and acquired a half interest in Kardon Manufacturing Corp., 52 W. Houston St., N. Y., which will hereafter be known as Harman-Kardon, Inc. Harman will be executive vice president and Bernard Kardon, who established the predecessor company three years ago, has become president of the new firm.



Sid Harman

H. C. Stacey

WEBSTER ELECTRIC APPOINTS STACEY SALES MANAGER

Howard C. Stacey, formerly assistant sales manager, has become sales manager of the sound sales division of Webster Electric, 1900 Clark St., Racine, Wis.

*

* * BERNARD L. CAHN ELECTED INSULINE V-P

Bernard L. Cahn, formerly general sales manager, has been elected vice pres-ident of the Insuline Corporation of America, 3 City, N. Y. 3602 35th Ave., Long Island



O. E. Bishop

MALLORY PROMOTIONS

B. L. Cahn

O. E. Bishop has been promoted to manager of sales operations, distributor division, of the P. R. Mallory and Co., Inc., 3029 E. Washington St., Indian-apolis, Ind. In his new position, Bishop will assist J. E. Templeton in coordinating field sales activities.

Dan Mischler, formerly a distributor rep, will replace Bishop as sales service manager. * * *

VAN AUKEN JOINS MARK SIMPSON

John A. Van Auken has been appointed general manager of Mark Simpson Manufacturing Co., Inc., Long Island City, N. Y. * * *

FEIR AND FELTMAN JOIN DUMONT

Sol D. Feir has been named district sales manager for Manhattan by the New York factory distributor, Allen B. Du Mont Laboratories, Inc.

John Feltman has been named assistant manufacturing manager of the picture tube division.

AEROVOX ELECTS GOLENPAUL AND MARSHALL V-Ps

Charles Golenpaul, formerly distributor sales manager, has been elected vice president, distributor sales, of the Aerovox Corp., New Bedford, Mass. Frank Marshall, formerly director of sales, manufacturers division, has also been promoted to vice president, manufacturers sales.

MILLER EXPANDING An addition of 2,000 square feet at the rear of their plant, has been announced by Miller Television Co., 2840 N. Naomi Ave., Burbank, Calif.



WIKE APPOINTED UTAH SALE'S MANAGER

Gaius Wike has been named general sales manager of Utah Radio Products Inc., 1123 East Franklin Street, Co.. Huntington, Ind.

Wike succeeds Fred Tower, who has been promoted to division manager and vice president of the Caswell-Runyan division of Utah.

C-D ANTENNA ROTOR WINDOW STREAMERS AND ENVELOPE STUFFERS

Free window streamers and envelope stuffers promoting antenna rotors are now available through jobbers from the Cornell-Dubilier Electric Corp., South Plainfield, N. J

Streamer is 101/2" x 28", printed yellow, red and black. * *

KUNZ ELECTED SANGAMO V-P

H. Laurence Kuns, general manager of the capacitor division of the Sangamo Electric Co., Marion, Ill., has been elected vice president.

Kunz started his career with Sangamo appointed capacitor division s-m in '45. *William W. Taylor* has been appointed sales manager of Sangamo's capacitor division, succeeding John G. Twist, who

resigned.

Bruce E. Vinkemulder has been named sales promotion manager of the division. Vinkemulder, who was formerly distributor sales manager, is succeeded by A. E. McCluskey.



H L. Kunz



B. E. Vinkemulder





A. E. McCluskey



Opens

TESTS @ Shorts

pensive components.

•

NEW BUILDING FOR ALLIED RADIO

A building, said to cost \$2,000,000, is now under construction for Allied Radio Corp., Chicago.

Allied's new site, with a total floor area of 150.000 square feet, will be in almost the exact geographical center of the city

on Western Ave. and Washington Blvd. According to Allied, its \$2,500,000 inventory for 19,000 items, will be substantially increased within a few years, to cover perhaps up to 25,000 items.



A SELENIUM RECTIFIER ESTE

The ONLY instrument ever designed to provide The Four Essential Tests for Selenium Rectifiers used in radio and TV receivers:



JFD CONSTRUCTS NEW PLANT

A 140,000-square-foot plant, expanding factory space to a total of more than 200,-000 square feet, has been announced by JFD Manufacturing Co., Inc., 6101 16th Ave., Brooklyn 4, N. Y. The company has also purchased a

32,000-square-foot area which temporarily will be used as a stop-off point for incoming trucks and as a parking space for JFD employees.







the solution for all your high voltage TV filter replacement problems

This package contains six (6) Style 413 Erie Universal High Voltage TV Filter Ceramicons and an assortment of 14 adapter terminals.

Carry one of these handy package assortments with you on all your TV service calls. You are assured of having, at all times, the CORRECT RE- PLACEMENT UNIT for any receiver rated at 20 KV or lower.

assortment If your requirements are for all of one combination of terminals, the Style 413 may also be obtained in handy plastic kits of ten HV Ceramicon bodies. Adapter terminals are supplied in packets of five each of a type. Order through your jobber.



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SPRAGUE CAPACITOR MANUAL

Sprague Products Co., 61 Marshall St., North Adams, Mass., has issued a 44page edition, *TV Replacement Capacitor Manual*, that lists capacitor replacements for 2,460 receivers of 78 manufacturers.

Also included is a printed circuit guide which shows replacement recommendations for the units used by 46 TV manufacturers. On the back cover appears color code information on capacitors which appeared in former Sprague *Tell U How* wall chart. Copies are available free from Sprague distributors, or by sending 10c to cover handling and postage to Sprague.



CISIN TV CONSULTANT BOOK

A modernized expanded analysis of the Cisin rapid TV troubleshooting method has been published in a 70-page book, TV Consultant, by Harry G. Cisin, 200 Clinton St., Brooklyn 2, N. Y. Featured are 213 picture and 76 raster

Featured are 213 picture and 76 raster troubles and sound troubles, which are keyed or *classified* to a specific part of the TV set. Book contains four sections : rapid TV troubleshooting method; rapid TV alignment method; installation and servicing of *uhf* units; and rapid checks (over 100). TV alignment section is an entirely new section, with the methods developed in the shop under actual working conditions. Priced at \$2.00.

TV ANTENNA GUIDE



Pocket-size book on TV antenna installations with chapters on *uhi* antennas, indoor directronic TV antenna system, and Yagis. Other subjects in the book include antenna dimension guide, channel frequencies, and proper feed methods for stacked arrays. Book was prepared by Edward M. Noll, Matthew Mandl and Edgar Daily. Listing at \$1.00 a copy, copies may be obtained without charge by writing directly to Dick Morris, Snyder Manufacturing Company, Philadelphia 40, Pa.



SPRAGUE CAPACITOR-RESISTOR

ANALYZER

A capacitor-resistor analyzer, model TO-4 *Tel-Ohmike*, has been introduced by Sprague Products Co., 61 Marshall St., North Adams, Mass.

Instrument includes pushbutton range selection, capacitance ranges from 1 mmfd to 20,000 mfd, resistance measurement range of from $2\frac{1}{2}$ ohms to 25 megohms at line frequency, direct meter reading of insulation resistance up to 20,000 megohms for checking all types of electrostatic capacitors, direct leakage current readings of electrolytics at rated dc working voltage, and a three-range power factor measurement of electrolytics. All capacitors are automatically discharged for safety after test by simply releasing the range selector pushbuttons. A magic cye tube is used to simplify Wien bridge balance on capacitance and resistance measurements.



[Additional new part news on page 74 and 75]

Tools . . . Instruments Parts . . .

ASTRON CAPACITOR STORAGE KIT

A plastic-metal capacitor storage kit, Jiffy-Kit, that stores bypass and coupling capacitors in clear plastic drawers, with identification labels, all housed in steel, is now available from the Astron Corp., E. Newark, N. J.

Capacitor kit features type AM, a molded paper tubular unit said to be highly resistant to humidity and designed for continuous operation at 85°C. Kit contains 113 capacitors representing 26 different values claimed to be the most frequently replaced by Service Men.



JCT POWER SUPPLIES

Two power supplies, Mini-Pak, that employ a selenium rectifier for a source of instant power, and designed to plug into a standard ac female receptacle, has been developed by Jersey City Technical Lab, 880 Bergen Ave., Jersey City 6, N. J. Model R is said to provide 108 volts

Model R is said to provide 108 volts regulated low ripple dc with an OB2 voltage regulator tube, maintaining constant voltage output with load variations up to 15 ma, or lightly loaded with input variations from 100 to 130 volts ac. Model P, a voltage doubler, 10 watt power source, of low ripple dc, is claimed to provide no load voltage output of 330 volts; at 50 ma maximum constant duty current output is said to be 200 volts. For intermittent use, the current may up to 65 ma.



In The Field*



Fig. 1. A thick trace on the 'scope screen is less desirable to work with than a thin trace. A thin trace can be obtained by using sufficient accelerating voltage in the *crt* so that the intensity control does not have to be advanced to the defocusing point; furthermore, the relative *dc* voltages on the other electrodes of the *crt* must be correct in order to obtain good focusing.



Fig. 2. Peaking of the *rf* or *if* amplifier at the high picture-frequency end (near the sound end) results in excessive contrast of high-frequency picture elements as illustrated in this test pattern reproduction; the vertical wedges appear darker than the horizontal wedges.

Tracing Motorboating in TV IF Stages . . . Locating Points of Takeoff . . . Oscillation Problems and Cures ...Response-Curve Peaking and its Relation to Picture Distortion . . . Tin-Foil Slide Effects on Leadin . . . Overpeaked IF Amplifier Effects...Reactive Distortion in FM Detector Deemphasis Networks

WHAT IS MEANT by the statement that response-curve peaking causes picture distortion?

Probably everyone is familiar with the technique of peaking up the receiver signal circuits in the vicinity of the picture carrier to obtain more contrast and less snow, when a very weak signal is to be received. This is a form of picture distortion (often deemed desirable) which produces abnormal lf response and subnormal hfresponse. The opposite type of peaking produces abnormal hf response and subnormal lf response, as shown in Fig. 2. Such high-video peaking is deemed desirable by a sizable proportion of the viewing audience.

How CAN an open bypass capacitor in an *if* amp produce *lf* motorboating?

An open bypass capacitor (platescreen or grid bypass) in the if amplifier does not always cause hf oscillation in the receiver. In some cases, the resulting hf feedback is insufficient to cause if oscillation, but the if response curve becomes distorted and the picture quality usually suffers. In addition, a very low-frequency feedback circuit may be established through the power supply, causing the receiver to motorboat at a very slow rate; the picture remains satisfactory for 15 to 30 seconds, and then slowly fades from the screen, disappears for another 15 to 30 seconds, whereupon the cycle repeats itself continuously.

CAN INSUFFICIENT horizontal width be caused by parasitic oscillation in the horizontal-output tube?

Parasitic oscillation in the horizontal-output circuit, involving the heater line, can cause subnormal picture width. Bypassing of the heater line to chassis at the socket terminal of the horizontal tube should eliminate the parasitic oscillation.

WHEN RECEIVER take off occurs, could it be caused by open decoupling or open common bypass capacitors?

When a receiver takes off or oscillates within sync, sweep, or other circuits, the trouble is usually caused by open decoupling, or open common bypass capacitors. A 'scope can be applied across the suspected capacitors to determine whether they are hot or cold. However, in many receivers bypassing is incomplete under normal conditions. Hence, it may be necessary to check the capacitors by substitution. If a normally operating receiver of the same type is available, a comparison check can be made across corresponding capacitors in the two receivers by means of a 'scope.

[‡]Based on questions posed during meetings conducted by **R. G. Middleton**, senior engineer at Precision Apparatus Co., Inc., and author of TV Troubleshooting and Repair Guide Book, published by John F. Rider. WHEN TESTING an interlocking booster and horizontal-oscillator circuit, should an auxiliary power supply be used?

Since the horizontal oscillator plate is occasionally supplied with B+voltage from the booster circuit, it may be difficult to decide whether low plate voltage at the horizontal oscillator is due to sweep-circuit trouble, or to horizontal-oscillator circuit trouble. To test this type of system, an auxiliary power supply can be used to provide normal B+ voltage to the plate of the horizontal oscillator. A 'scope check of operating waveforms will then show whether the horizontal oscillator is at fault or whether the sweep circuit is defective.

IN SWEEP ALIGNMENT of the FM detector, is the deemphasis network a source of reactive distortion?

Reactive distortion in the S-curve display when sweep-aligning an FM detector causes the S curve on the forward trace to appear higher than the S curve on the return trace. This reactive distortion is often caused by connection of the 'scope at the output of the deemphasis network, instead of at the input of the deemphasis network. It is also preferable to connect the 'scope at the input of the network, because the markers are then stronger; the deemphasis network is a low-pass filter which reduces the size of a beat marker.

(Continued on page 72)




A NEW TOOL TO MAKE TV SERVICING Easier, Faster, More Accurate AND MORE PROFITABLE

No probes made anywhere do the job of SCALA oscillograph probes so efficiently, so easily. Use with your present scope . . . low cost will be paid ten times over in a month. Check your local distributor or write factory and specify model number:

BZ-1 SIGNAL TRACING PROBE . . . locates dead I.F. stages, marks ratio detector curve, calibrates marker generator, adjusts video amplifiers, checks output of sweep generator, views response of single I.F. stage, traces buzz pulse in sound I.F. strip. Can be used with V.T.V.M. Contains demodulator of low-capacitance, high-impedance design, useful to 225 MC.

BZ-2 LOW CAPACITY PROBE . . . makes it possible to trace video, sync or sweep waveforms through high-impedance circuits without causing waveform distortion due to circuit loading. Cuts the effective input capacitance of scope by a factor of 10 and gives an attenuation of 10 to 1.

BZ-3 100:1 VOLTAGE DIVIDER PROBE . . . is very useful in trouble-shooting horizontal sweep circuits. It may be applied directly to plate of horizontal output tube or at the plate of the damper tube to check the operation waveforms and to measure their peak to peak voltages without impairing the wave shape or incurring danger to the oscillograph.

SCALA RADIO CO., 2814 - 19th St., San Francisco 10, Cal.

WHY DOES SLIDING a piece of tinfoil along the leadin produce better picture contrast in fringe areas?

The tinfoil produces in-phase reflection of lf picture voltages (when properly located), as is obvious from Fig. 3. The in-phase reflection recovers video voltage which would normally be lost by mismatch to the rf tuner. DOES THE Zero-Volt reference provided by sweep generator permit measurement of wideband circuit bandwidth?

When a circuit, such as an rf transformer, is being sweep-aligned, often the sweep width of the sweep generator is insufficient to display completely the response curve on the 'scope screen. In this case, the location of the half-voltage points on the response curve can be quite difficult to locate, particularly if the circuit has a very wide-band response. The half-voltage points must be known to determine the bandwidth of the circuit. However, the half-voltage points can be very easily determined in this instance if the sweep generator is capable of providing a zero-volt reference line. Although the lower portion of the response-curve skirts are not present in the display, the half-voltage point is given by the level half way between the zero-volt reference line and the peak of the response curve.

In the Field

(Continued from page 70)

WILL SLIGHT fluctuations in picture brightness be caused by intermittent high-voltage filter capacitors?

Tests with a high-voltage capacitance-divider probe and 'scope will usually show that slight intermittent fluctuations in picture brightness are caused by a fluctuating voltage across the high-voltage filter capacitor. This is due to an intermittent condition in the capacitor, which must be replaced.

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CLEARBEAM BURBANK CALIFORNIA

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CAN AN open damping resistor across *if* coil cause receiver oscillation?

Carbon resistors occasionally become defective in use, either developing greatly increased resistance, or opening up completely. The condition may be intermittent. Such a resistor across *if* coils can be responsible for *take-off* in the *if* amplifier circuit. If a resistor is suspected, it should be checked by substitution, since the surge of current from an ohmmeter may temporarily heal an intermittent resistor and lead to false conclusions.

Fig. 3. Traces illustrating effect of sliding a piece of tinfoil along the leadin, with a weak signal present. To prepare these patterns, a small sweep-frequency voltage was mixed with the incoming TV signal at the antenna terminals of the receiver, to show the effect on both the picture signal and on the response curve when the tinfoil was moved along the line. The picture-carrier station marker appears at the top of the response curve. In reproduction at left the tinfoil was placed at a position for the weakest picture; the peak-to-peak voltage of the picture signal is comparatively small. View at right shows result when tinfoil was placed to provide the best contrast in the picture; the peak-to-peak voltage of the picture signal is comparatively large, reducing the gain of the if amplifier, which in turn reduces the height of the response curve. It will be noted that the shape of the response curve changed slightly, and the picture-carrier marker remained at the peak of the curve.





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NEW YORK 1, N. Y.

WOULD SECTIONAL ISOLATION be the best approach to localize a take-off circuit?

Yes. When a receiver *takes off*, the best troubleshooting procedure usually consists of providing separate B+voltages to the individual receiver sections, such as the sync horizontaloscillator, sweep circuit, etc., since in many cases the oscillation is caused by feedback through some branch of the common plate-power supply. Provision of separate B- voltages from B- batteries or from line-operated power supplies will serve to stop the oscillation in such cases, and indicate the receiver sections which are faulty. In some cases the feedback takes place from one section to another, as from the sweep section to the sync section. However, in other cases oscillation can arise within a section, as when the sync amplifier is not properly neutralized in certain receivers.

WILL YOU SHOW the effect on the picture of over-peaking the if amplifier in the receiver?

The visible effect of over-peaking varies considerably, depending upon the amount of misalignment which exists. However, the screen pattern shown in Fig. 4 is typical of what may be expected.

How DOES ONE go about locating an oscillating *if* stage?

An oscillating if stage can be located by connecting a clip-lead across the first if coil, and noting whether a change in reading is obtained on a dc vtvm connected across the picturedetector load resistor. If no change in indication is noted, the clip lead should be disconnected from across the first if coil, and connected across the second if coil, again noting whether a change in reading occurs on the vtvm. This test should be continued until a large drop is noted in the scale indication, which thereby localizes the oscillating stage.

Fig. 4. Complete picture break-up caused by excessive peaking of the if amplifier.



WHEN THE COILS in an if amplifier are peaked at 34.8 and 36.9 mc, for example, should the humps in the response curve appear at these frequencies also?

(PP)

Usually no. Often, only one hump may appear, as shown in Fig. 5, due to circuit tolerances. And, even if the tolerances are close, and a doublehumped curve is obtained, the peaks of the humps will appear wi hin the peaking frequencies of the individual circuits, as illustrated.

Fig. 5. Variations in shape of the if response curve, due primarily to variations in Gm ef the individual if tubes, and also to other circuit tolerances. The knee frequencies of the response curve are not the peaking frequencies of the if coupling coils. (Bandwidth measured between half-voltage points.)





FOR Better

B-T Antenna Accessories

Every Service-Technician knows that you can't just hook up a TV set to an antenna and expect that it will always work the way you would want it to. There are too many 'ifs', 'ands', and 'buts' that enter into the picture. That's why Blonder-Tongue Laboratories has devoted its facilities to the creation of accessories designed to assist the Serviceman in meeting these problems.



The B-T LINE SPLITTERS provide the lowest cost means for dividing a transmission line to feed branch lines, or to distribute signals to several TV sets or distribution units in multiple dwellings or community installations. Each Line Splitter supplies up to four impedance-coupled branch lines from one input, with flat response over all channels.

Other B-T ANTENNA ACCESSORIES include: Line Loss Equalizer, Attenuator, Remote Control, and Weather-Proof Housing for B-T Units. Sold at Leading Distributors

Complete literature available describing the B-T Unit System for Easy-toinstall Master Systems and Community Installations, B-T Boosters, ond B-T Antenna Accessories.

Write for Catalog FA8



BROWNING FM MODULATION MONITOR

A frequency modulation monitor, MD-33, designed to check the modulation swing of FM transmitters operating in the special service bands from 25 to 174 mc, has been announced by Browning Laboratories, Inc., 750 Main Street, Winchester, Mass. Continuous coverage is accomplished in two bands without the use of plug-in units.

Modulation swing is indicated directly on a 4" panel meter with a 20-kc fullscale linear calibration. A dual-range flasher circuit permits checking overmodulation by the shortest of voice peaks at either of two pre-set amounts of swing.



PILOT FM-AM TUNER

A 9-tube FM-AM radio tuner, Pilo-tuner AF-821, intended for use as the central control head of a hi-fi music system, has been announced by the Pilot Radio Corporation, Long Island City, N. Y. Incorporates a two-stage preamplifier with adjustable equalization for various makes of reluctance phonograph cartridges, separate input connections for phono and TV operation, extended range bass and treble controls, a temperature compensated oscillator for drift-free FM reception, and afc at the option of the user. Tuner can be left in the open on a shelf or table, or mounted in a single large rectangular opening in the front of a cabinet.

Overall dimensions are $14\frac{1}{4}$ " by $7\frac{1}{4}$ " by $8\frac{1}{2}$ ".

IRC FOUR-WATT RESISTORS

Power resistors, PW4, rated at four watts, have been introduced by International Resistance Co., 401 North Broad St., Philadelphia 8, Pa.

Insulated with an inorganic core material molded in a high temperature plastic, unit, it is claimed, will not support combustion. Wire element is wound on glass fibre core with axial leads $1\frac{1}{2}$ " long, .036" diameter. Body dimensions: $1\frac{3}{4}$ " long by 21/64" diameter. Available from 1 to 8200 ohms in $\pm 5\%$ and $\pm 10\%$ tolerance.

Resistors are recommended for TV circuits requiring 2 to 3 watts actual dissipation at high ambient temperature, resistance element of resistance-capacitance filter in auto receiving sets where operation is at high ambient temperature, and all other circuits where a stable resistor is required, with wattage dissipation of 4 watts and less.

* * *

HELLER CABLE FASTENING GUN

A hand-held automatic fastening gun for cables has been developed by the Heller Co., 2153 E. Superior Ave., Cleveland 14, O.

Gun drives extra-size band with leg lengths varying from $\frac{3}{16}$ " to $\frac{1}{2}$ ".



Multiple Installations in Fringe Areas Using the AutoCoupler and AutoBooster

The ITI AutoCoupler is an exceptionally well-made unit which permits driving more than one set with a single antenna. The Coupler has low losses, but even the ITI AutoCoupler does cause some attenuation. In fringe areas, special arrangements must be used involving the use of one or more AutoBoosters depending upon the signal strength. An IT-90AB Cascode AutoBooster

An IT-90AB Cascode AutoBooster can be inserted in the lead-in from the antenna, boosting the signal before it gets to the AutoCoupler. Splitting into two separate paths—as many as four paths are possible if an IT-118A AutoCoupler is used instead of an IT-117A Auto-Coupler—the signal proceeds toward the receivers. It can be further amplified by an economical IT-102A Super Auto-Booster located at the input of each receiver.

An unfortunate condition that sometimes exists is interaction. Interaction is occasionally caused by the local oscillator of an offending TV set acting as a transmitter and sending a signal back along the lead-in to the other set

a transmitter and sending a signal back along the lead-in to the other set The IT-102A Super AutoBooster, if put in the lead-in of the offending receiver, should cure this trouble by providing effective isolation. An Auto-Booster strongly amplifies a signal going in the design direction, but stops any signal attempting to go through it in the reverse direction.

in the reverse direction. Just as the AutoCoupler is a must for multi-set operation in the show room or home, the ITI Tenna-Clip is an absolute essential for the service and repair shop. The Tenna-Clip permits instantaneous attachment of wires to terminals. Clipping it on takes no more time than to snap one's fingers. The wise technician will put one of

The wise technician will put one of his Tenna-Clips on the receiver end of his antenna lead-in. With that lead-in suspended near his shop ceiling but dangling free to the service bench, he can quickly transfer his antenna input from one set to another on the bench.

For additional copies of this and earlier issues of Techni-Topics, catalog sheets on all ITI products and free sample Tenna-Clip, write. on your letterhead, to Industrial Television, Inc.

Industrial Television, Inc. 369 LEXINGTON AVENUE CLIFTON, N. J. GRegory 3-0900



TV Parts ... Accessories

TRANSVISION PICTURE TUBE TESTER-REACTIVATOR-SPARKER AND TV RECEIVER KITS

A picture-tube test and repair unit, *Tester-Reactivator-Sparker*, that is selfpowered, has been developed by Transvision, Inc., Dept. DG-3, New Rochelle, N. Y.

As a tester, instrument measures cathode emission, locates shorts between elements, high resistance shorts or leakage up to 3 megohuns, and indicates whether the tube has lost or is losing its vacuum. As a reactivator, unit is said to rejuvenate dim tubes; reactivation can be done in the customer's home without removing the picture tube from the TV set.

As a sparker, unit sparks out electrical leakage.

Six TV kits for home assembly, A-4 series, that feature afc, agc, choice of several tuners, optional remote control, retrace-elimination, ready addition of uhf channel strips without converters, optional power of 60, 50 and 25 cycles, have also been announced.

Kit, when completed, comprises 25 tubes with $6'' \times 9''$ pm speaker.



HAMMARLUND VHF-UHF CAPACITOR

A vhf-uhf variable capacitor, vu, designed for use in tuned circuits that operate at frequencies from 50 to 500 mc, has been introduced by the Hammarlund Manufacturing Co., 460 W. 34th St., New York 1, N. Y.

Capacitor design is said to place two capacitor sections in series and eliminate the need for contacts to the rotor. Rotor is isolated by the use of pyrex glass ball bearings.



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WALSCO TV CONSOLE ROLLER-COASTER

caster assembly for television sets, TV Rolabout, that is said to fit almost *IV Ralabout*, that is said to fit almost any console, has been announced by the Walter L. Schott Co., 3225 Exposition Place, Los Angeles 14, Calif. *Rolabout* has 4 ball bearing casters mounted on a heavy steel cross brace which is attached to the base of cabinet.



G-C HV TV TEST PROBE

A tester for checking hv TV circuits, 8836, has been introduced by General Ce-ment Manufacturing Co., 919 Taylor Ave., Rockford, Ill.

Measuring about 7" in length, servicing tool is said to provide margin of safety in testing by glowing when in contact with high voltage. Shows points of high voltage to eliminate dangerous shocks.

RADIO APPARATUS LINE VOLTAGE BOOSTER

A booster, V-15, that is claimed to provide full rated performance from any 110-volt electrical device requiring be-tween 500 and 1,500 watts, has been introduced by the Radio Apparatus Corp., 55 N. New Jersey St., Indianapolis 4. Meter reads actual line voltage and load voltage; switch increases 5 volts-perseten and is said to raise 95.

per-step, and is said to raise 85 volts to 120 volts with 1,250-watt load.

* * * EBCO CRT DYNAMIC ANALYZER

An instrument, Dynamic Analyzer. that can be attached to a vtvm to convert it into a picture-tube tester, has been introduced by Electronic Beam Corp., 923 Old Nepperhan Ave., Yonkers 3, N. Y.

Analyzer is claimed to check all socket voltages of a TV set while in operation, check emission of the picture tube, and opens and shorted elements, and leakage.





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Dual Speakers



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DEPENDABLE PROFITS: Completeness of line, excellence of product, dependable delivery, right prices—thor's the ATLAS combination that meons high, steady Industrial Sound profits for You!







UHF Crystal Diode Troubleshooting

by HENRY R. HESSE Senior Engineer, TV Receiver Division Allen B. DuMont Labs

Part II ... Checking Current of Crystals... Resistance Reading Interpretation ... How To Replace Crystals



Fig. 1. Circuit and plot illustrating operation of a harmonic crystal multiplier, as employed in some tuners to multiply frequency of vhj oscillator.

IN TROUBLESHOOTING CRYSTAL diodes in ultrahigh circuits, measurement of the *dc* crystal current is a particularly



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important, offering a check on the coupling and tuning, too.

A lack of any crystal current indication would disclose either a burnedout crystal or a defective oscillator tube. A check of the voltage developed across the oscillator grid leak would disclose whether the oscillator was functioning and its relative strength.

Ohmmeter Tests

Crystals can be tested with an ohmmeter. Two resistance readings should be taken; one will indicate the crystal's forward resistance which should read between 50 and 500 ohms, and the other of the back



CHEMICAL ELECTRONICS CORP. P.O. Box 127, Irvington, N. Y. Modern Chemistry for Better Electronics resistance obtained by reversing the crystal where the resistance should be above 10,000 ohms. One should not use an ohmmeter with a battery voltage greater than 1.5 volts, to prevent burnout of the crystal during measurements. A burned-out crystal will be indicated by either a low or high resistance in both directions.

Crystal Replacement

Replacement of crystals is quite simple since they can be either clipped or soldered into the circuit. Recognition of some soldered-in crystals is difficult because of their similarity in appearance to carbon resistors. Crystals can be identified by the printed crystal schematic symbol and the absence of the resistor color bands; also crystals are usually located close to the local oscillator tube. In soldering crystals, to prevent crystal damage due to the heat of the soldering iron, the crystal lead should be held in the jaws of a long-nosed pliers, holding the lead as close as possible to the body of the crystal. The long-nosed pliers should always be used to hold the crystal lead between the point of soldering and the body of the crystal to act as a heat dissipator, thus preventing overheating and possible damage to the crystal. The clip-in crystals have an advantage in that they may be checked as easily as tubes by the substitution method. In addition, the clip-in crystals cannot be damaged by the soldering operation.

RTMA Exhibit at AVA Convention



A. Coumont, RTMA service coordinator; Eugene D. Fink, Chief of Bureau of Vocational Curriculum, Development and Industrial Teacher Training, University of the State of New York and A. C. W. Saunders, director of Saunders Radio and Electronic Schools, Inc., Boston, Mass., in booth of RTMA service committee, at the annual convention of the American Vocational Association in Boston. The exhibit, under the direction of a subcommittee consisting of E. W. Merriam, Sylvania, F. B. Ostman, Capehart-Farnsworth, and J. A. Milling, Howard W. Sams, demonstrated a test bench for rapid TV chassis troubleshooting and displayed TV techniciams servicing and training aids including charts, pamphlets, manuals and a trainer chassis. The purpose of the exhibit was to announce RTMA's offer of supplementary teaching aids for the training of radio and television technicians. A brochure explaining details of this offer was distributed and discussed with administrators, supervisors, teacher trainers and teachers in vocational and industrial arts education.





JOTS AND FLASHES

THE HUGE QUANTITIES of parts required for TV chassis was strikingly revealed recently in a report from a midwestern set manufacturer, which disclosed that over \$400,000 worth of components are consumed each working day to meet their production schedule of receivers. Robert F. Halligan has been promoted to assistant operations manager of the Hallicrafters Co. . . . The second annual report by the self-employed, covering '52 earned net income for Social Security purposes, is due between January 1 and March 15, 1953. The amount of tax for '52 is still 21/4 per cent of net earnings from \$400 up to \$3,600 a year. Social Security report is made on the combined scheduled C and Ca which is filed with the Form 1040. Service Men are precautioned to make these returns in duplicate, retaining a copy for future reference. ... Edgar M. Villchur, a SERVICE contributor, will present a course, The Re-production of Sound, at New York University, Division of General Education, Washington Square. Course, which will cover the theory of sound, plus in-stallation procedures, will start Wednes-day, February 4, 7-9:45 P.M. . . . To insure service for Zenith's Hawaiian TV customers, a TV service school and clinic has been introduced by the manu-facturer's distributor. facturer's distributor. . . G. E., it is said, will double its production of germanium diodes next year. Each of the 6.5-mil-lion TV sets expected to be built by industry next year will incorporate as many as three of the tiny devices, it was noted. Ralph Aasen has been appointed chief engineer and G. Leonard Werner director of sales engineering of Mark Simpson Manufacturing Co., Inc. ... M. Robert Wilson has been appointed vice president in charge of sales for the Hallicrafters Co. . . The Audio Fair in Chicago will be combined with the '53 International be combined with the 53 International Sight and Sound Exposition to be held at the Palmer House, Sept. 1, 2 and 3... Prestoseal Manufacturing Corp. is now located at 37-27 33rd St., Long Island City, N. Y.... The David Bogen Co., Inc., has noved to new quarters at 29 Ninth Ave., New York 14, N. Y. ... Ralbh Glogeer, product manager of Len-Ralph Glover, product manager of Jensen Manufacturing Co., has become a member of the RTMA high-fidelity committee. . . . New address of the adminis-trative and home offices of National Union Radio Corp. is Jacksonville Rd., Hatboro, The American Phenolic Corp. and Pa. . . Cornish Wire Co. have signed a licensing agreement permitting Cornish to manu-facture, package and sell tubular twinfacture, package and sen tubular twin-lead under Amphenol's Krueger patent 2,543,696. . . . RCA, Harrison, N. J., Sarkes Tarzian, Inc., Bloomington, Ind., and J. W. Miller Company, Los Angeles, have become participants in the Photofact services of Howard W. Sams and Co., Inc.; RCA will participate in behalf of Inc.; RCA will participate in behalf of transformer components; Sarkes Tarzian for selenium rectifiers and Miller for coils. . . *Sidney Pariser*, president of Radio Merchandise Sales, was recently honored by his firm for his 25-year record of achievement in the radio and TV parts industry.

Sidney Pariser

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