## A RIDER PUBLICATION

## RECEIVING TUBE



## SUBSTITUTION

# G U I D E <br> B 



# RECEIVING TUBE SUBSTITUTION GUIDEBOOK 

 BYH. A. MIDDLETON

FIRST EDITION

JOHN F. RIDER PUBLISHER, INC. 480 CANAL STREET NEW YORK 13, N. Y.

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## FOREWORD

Reccizing Tube Substitution Guide Book is a greatly enlarged and revised edition of the book Wartime Radio Service published in 1944. This new book lists about 750 receiving tube types and their bases, including all of the following series:

4, 5, 6, 7, and 7L old-style base series
Octal base series
Loctal base series
7-pin miniature series
9 -pin•noval series
Subminiature series.
During the past eight years we have made many tube substitutions. Most of them were easy to make and all resulted in from excellent to reasonable performance. The majority of substitutions shown here have actually been tried. We are passing this information on to you in the belief that it will save you many hours and enable you to make necessary repairs to electronic equipment in spite of shortages. Also, when shortages no longer exist, you will again save time in restoring equipment to its original condition after substitutions have been made.

All substitutions listed here describe in detail the necessary data for changing or rewiring the sockets. It is recommended that in making the circuit changes listed you follow the sequence exactly as indicated in order to avoid any errors in rewiring.

You will note that a few types have no substitutes listed. We do not presume to be infallible. We may have omitted some tube substitutions. If you know of tube substitutions which have been omitted we would like to hear from you about them.

Besides a tube substitution listing we have included other important information that will make this book
even more useful as a substitution guide. In Section 3 we offer a compilation of television receiver filament circuit arrangements including various filament diagrams. These were compiled by John F. Rider Publisher, Inc., to whom we owe thanks for their contribution. The information was taken from the five presently existing Rider TV Manuals. It is hoped that this information will not only aid tube substitution operations, but will prove helpful in connection with TV servicing in the home. A group of servicing suggestions are also included to help in repairing the filaments of burned-out tubes, making adapters, and for the change over of battery-operated radios to electric operation.

Most significant is the last section of this book which covers different charts and tables. A complete listing of the characteristics of receiving tubes and bases and cathode-ray tubes and bases are included in this section. Thus this book, besides serving as a tube substitution guide, also functions as a tube handbook.

We wish to express our appreciation to the American Radio Relay League for their cooperation in permitting us to reprint their receiving tube characteristics charts from their ARRL handbook. In our estimation these are the most complete charts available at this time. To Tung-Sol Lamp Works, Inc., for supplying us with the data on tube classifications, ballast tube and resistor numbering codes, and RTMA resistor, capacitor, and transformer color codes our thanks; also to Sylvania Electric Products; Inc., for supplying us with the data on cathode-ray-tube characteristics; to Federal Telephone and Radio Corp. and Radio Receptor Corp. for their kind cooperation.

November, 1950
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## THE BACKGROUND OF TUBE SUBSTITUTIONS

Were it not for the fact that tube development is a never-ending activity, there would be no purpose in describing the background of tube substitution. The substitution lists contained herein would suffice, for they include practically every tube which is used for receiving purposes serving many different electronic applications. These applications consist of radio receivers of all varieties ( $a-m, f-m$, and TV), radar, facsimile (commercial and military), public address amplifiers, record changer amplifiers, test equipment, electronic computers - in fact every kind of equipment with the exception of transmitters, although even there, receiving tubes make their appearance in the speech amplifiers.

The basis of tube substitution is similarity or equivalence between the original and the substitute. The choice of these two words with different connotation is deliberate ; similarity may mean equivalence in some respects but not in all. Thus if two tubes are similar (or identical) in electrical characteristics, one is the equivalent of the other. The use of two tubes, however, to replace one single tube which affords certain facilities, creates a state of equivalence rather than a state of similarity.

This is not intended as a play on words but deals with a very important situation that is developing fast in television receivers. Unwelcome as it may be, it means constructional modifications and even more important, a careful analysis of what suits the purpose. Any attempt to list all the substitutes within the meaning of equivalent as we have described it, would be a monumental task and would more than likely, never see the light of day. We hope, therefore, that the general details of the background of tube substitution given in this section combined with the tube substitution lists and the knowledge possessed by the technician who makes the change (and selects the substitutes) will result in satisfactory substitutions.

An examination of the tube substitution lists will disclose that the substitution of one type for another is not too frequently accomplished by a simple replacement of tubes. Differences in tube characteristics may demand some modifications in the circuit within the apparatus. Sometimes, only a change of socket is needed because of differences in the basing of the substitute tube. In other instances, definite restrictions
are imposed relative to the heater circuits; some substitute tubes may be used only in parallel-wired heaters without any circuit changes, whereas in other instances, a tube substitution is applicable only to series-wired heaters. In some cases, a tube substitution may demand modifications in the cathode, control grid, plate, or screen circuits, or possibly in the power supply, so as to satisfy the needs of the substitute and accomplish the best possible performance. These circuit changes are not listed because they are peculiar to each system.

All of this means that although the lists in this Guide Book give the substitute or substitutes as the case may he, the final selection cannot be made without considering the conditions existing in the equipment which will receive the substitute. Where changes in heater or filament wiring are required, they are described. Changes necessary in the signal electrode circuits such as those of the control grid, screen grid, cathode, and plate so as to attain best possible performance become the function of the technician and are determined by the constants of the specific circuit in which the substitution is made.

As shown in the three series of Rider's Manuals (AM-FM, TV, and PA), many tens of thousands of models of receivers and amplifiers comprise the hundred odd million units which may require substitute tubes.

Fortunately, a certain amount of standardization does exist in receivers and other equipment designed to work with the tubes listed herein. This situation, together with the circuit and operating voltage details given in the above-mentioned manuals and manufacturers' literature affords the technician the opportunity of determining the operating conditions thereby enabling him to establish the correct voltages at the different signal electrodes. A familiarity with these techniques is not difficult to acquire, although we hasten to add that too many differences exist to permit circuit modifications based on guesswork or memory. Schematic wiring diagrams, operating voltage cables, and the tube characteristic charts demand attention if longest tube and component life are desired, and also, if best circuit performance is to be attained with the substitute tube.

Design engineers have their own ways of accomplishing performance with the standard run of tubes. Many substitutes are possible but all will not afford like performance. In listing the substitutions, only those sub-

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stitutions considered practical, that is, which do not demand redesigning of circuits, were included. Many substitutes possess sufficient similarity to the original as to require no changes in either heater wiring or sockets. These are listed with the note "No changes." This does not mean, however, that the signal electrode operating conditions are identical for the original and the substitute. This should be checked in the tube characteristics chart contained in this Guide Book. It only requires a few minutes of time to do this and its results can be very gratifying.

If upon examination, the differences in electrical characteristics between the recommended substitute and the original are more than moderate, changes in the signal electrode operating circuits may be required. Since the plate voltage requirements for tubes in similar categories do not differ greatly, changes are not too frequent in the plate circuits. It is only when battery type and a-c operated tubes are being compared that one finds radical differences in plate and screen voltages. More critical points are the control grid and cathode bias - especially the latter. Small numerical differences in bias voltages (which are related to the plate current) produce great performance differences. For example, a change in bias from -2 volts to -4 volts is only 2 volts, but it represents a change of 100 per cent, and can very materially influence performance. A situation of this kind would demand a change in the value of the bias resistance.

A bias tube may be listed as the substitute for a zero bias tube. Reference to the electrical characteristics will disclose that the grid resistor must be changed; sometimes from 10 megohms to as low as 0.25 megohm. In addition, a cathode resistor of such ohmic value as will develop the bias shown in the tube characteristic chart must be added. Thus, the statement "No changes," does not refer to signal electrode operating conditions, rather to the fact that neither heater wiring nor socket changes are required.

Each substitution is an individual case requiring individual consideration, unless it is definitely known that the original and the substitute are identical in all respects other than heater voltage. Even then, if the substitution is made in a system which involves a state of resonance, realignment will be required. Similar tubes, even identical ones, do not possess identical values of interelectrode capacitance. This difference affects the final value of tuning capacitance. It is very important to bear this in mind when substitutions are made in wideband amplifiers particularly, since here, the interelectrode capacitance (direct and reflected) plays a paramount role in the peaking action. Examples are the video amplifiers in television receivers and the amplifiers in oscilloscopes and the like. In making substitutions it is often necessary to consider the function of the tube and its circuit so as to insure best performance in the circuit. The various types of circuits and functions will now be discussed.

## Oscillator Systems

These may be heterodyning arrangements which involve tracking with other tuned circuits, such as in converter systems and separate oscillator and mixer circuits, or nontracking arrangements, such as beatfrequency oscillators. Also, there are the various kinds of multivibrator systems in television receivers. Each of these demands individual consideration.

Combination oscillators and mixers (converters) require substitutes which contain not only the identical number of electrodes as the original, but in addition, the functions of these electrodes must be the same. This immediately limits the number of possible substitutes. The list of tubes, classified by function found at the end of this section, is an aid in this respect. If the required substitutes can not be procured, it does not make sense to redesign the circuit so as to replace a single tube with two individual tubes. That is a design engineer's job. If the oscillator and mixer functions are performed by individual tubes in separate envelopes, then the latitude of substitution is greater, provided that the selection of the substitute tube is made carefully.

The higher the frequency of operation, the more critical is the choice. That is why new tubes are born as operating frequencies increase. Tubes designed for the broadcast band are frequently unsuited for use in the vhf band and most certainly not in the uhf band. Thus, in addition to recognizing the oscillator function, it is also imperative to pay heed to the frequency of operation. If a choice is available, the tube intended for a higher frequency is suitable for a lower frequency, but not vice versa with complete freedom.

Sometimes tubes specifically intended for use as oscillators will not perform properly in that position, it is difficult to account for this, but it is a fact nevertheless. This does not condemn the tube as a tube it can still perform other functions - nor does it mean that another tube of like brand and type will behave in similar fashion. There is no remedy for such failure to function properly - it is simply a statement of fact.

What should be examined when comparing tubes intended for oscillators? Neglecting heater or filament ratings for the moment, these being assumed to be suitable and assuming that the number of circuit electrodes of the substitute original are the same, such details as the grid bias, the plate (and screen) voltages, the plate (and screen) currents, and the transconductance are paramount factors. If the exact duplicate is not available, the substitute tube which requires lower plate and screen voltages (differing only moderately from the original) is preferable to the substitute tube which requires higher plate (and screen) voltages than the original. The tube with the higher transconductance is preferable to the tube with the lower transconductance, everything else being equal. These preferences are more apt to furnish heterodyning voltage

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over the entire band embraced by the receiver, especially if the bias resistor is modified to suit the specifications of the substitute.

## R-F and I-F Amplifiers

The general run of $r$ - $f$ and i-f amplifiers utilize tetrodes and pentodes. Since pentodes used as triodes (in a-f amplifiers) are substitutes for triodes, it is important when selecting a substitute to know the manner in which the tube is used in the r-f or i-f amplifier. A triode is a poor substitute for a pentode; if a pentode is used, the substitute should be a pentode. However, if a tetrode is used, the substitute may be either a tetrode or a pentode. Care should be exercised to note if a shield is a part of the tube. An unshielded tube may be substituted for a shielded tube provided that an external shield is used and is grounded properly. Single-ended tubes may be substituted for coubleended tubes, but the reverse may be troublesome. Care must be exercised relative to the control-grid lead dress so as to minimize regeneration.

Sharp cutoff tubes should be replaced by similar tubes; similarly with remote cutoff tubes. However, sharp cutoff tubes may be replaced by remote cutoff types without too much trouble. The avc may be affected somewhat, but this does not interfere with the effectiveness of the receiver. When sharp cutoff tubes replace remote cutoff types, however, some minor problems may arise. Their best location would be in places where the signal level is lowest, for example, in the first stage in either an r-f or i-f amplifier. If distortion is severe on loud signals (due to rectification in the sharp cutoff stage), a divider network may be required so as to reduce the avc bias being applied to the sharp cutoff tube. This is best accomplished at the source of the avc, and might call for a separate avc line to the sharp cutoff tube. It might even be satisfactory to operate the sharp cutoff tube (if it is located at the point of lowest signal level in the amplifier) without any avc, using a low fixed bias.

Where there is a high input signal, sharp cutoff tubes must be used in place of remote cutoff tubes, an auxiliary volume control (or divider) at the front end of the receiver (perhaps in the antenna circuit) may be required. This would be operated only on those channels which cause trouble. A panel switch would control the operation of this signal control element.

Transconductance is the important electrical characteristic to consider in r-f and i-f amplifier substitutions. The higher the mutual conductance is relative to an r-f or i-f transformer the better, assuming that the plate and screen voltage conditions are satisfied or approached. Inability to equal the original tube in transconductance means reduced gain in the stage, but this seldom is a problem in a-m or $\mathrm{f}-\mathrm{m}$ receivers because the average receiver has excess gain for the reception of chain or local broadcasts. The same can be
said about television receivers, provided that the receiver is located in a primary service area. When such a receiver is relatively close to a station, the problem is too much rather than insufficient signal, so that a reduction in r-f or i-f amplification (unless it is too severe) usually can be tolerated. In fringe areas, the situation is different, especially when the received signal levels already border on the inadequate. There it becomes necessary to approach the original, and if this cannot be attained, then it is preferable to select tubes with higher than the original transconductance and to adjust the operating voltages accordingly. General instructions of this kind are given elsewhere in this section.

Where r-f and i-f systems are subject to tube substitutions, realignment of the coupling transformers associated with the input and output circuits of the substitute stage are imperative. Sometimes it may appear that proper performance is being secured without realignment. This should not be accepted as fact without a test to establish if the circuits are peaked properly.

Whether the shift in frequency peaking is upward or downward depends upon the direction of the capacitance change. A reduction in distributed capacitance, which includes the plate-to-cathode (or control grid-to-cathode) capacitance tends to cause peaking at a higher frequency, whereas an increase in distributed capacitance tends to cause peaking at a lower frequency.

Many i-f transformers and some r-f transformers are permeability tuned, utilizing the related distributed capacitance including the tube capacitance to provide the $C$ for the tuned circuit. Because of this, changes in distributed capacitance, due to different tube electrode capacitances, can cause major variations in operating conditions. Whenever possible, substitute tubes should approximate the input-output capacitance of the original tube. This data is found in the tube specification charts of Section 5.

Exception to the need for realignment of r-f and i-f coupling systems is found in those equipments which employ $R-C$ coupling between tubes. While not a common practice, it is to be found in receivers. Sometimes the coupling element consists of a resistive plate load and a tuned grid load for the succeeding tube. The resistive plate load on a substitute tube requires no readjustment, but if the substitution is made in that stage which has a tuned grid load, realignment will be required. Examples of such arrangements are listed elsewhere in this section in connection with $r-f$ and $i-f$ transformer replacement.

## Audio Amplifiers

All types of tubes are found in audio amplifiers: triodes, tetrodes, pentodes, pentodes used as triodes, and various kinds of output-stage power amplifiers. Voltage amplifiers are, in the main, resistance-coupled
systems, whereas power amplifiers are transformercoupled. The difference between these two general categories is the plate circuit load, that is, load impedance, and the grid bias.

There are some differences between the signal electrode operating conditions in resistance-coupled amplifiers, their operating voltage or load resistance may differ, but many substitutions are possible without changes. A fair degree of similarity exists between the fundamental designs of these circuits so that it is possible to generalize concerning substitutions. Pentodes can be used in place of triodes and, in turn, triodes may replace pentodes or tetrodes. The load resistances are pretty much the same for all of these tubes since the limitation is set by the plate voltage supply, and this does not differ too greatly in like categories of equipment. Naturally, the ideal condition is when the substitute is used exactly as the original, or the substitute type is the same as the original type.

In the case of triode-type tubes used in audio amplifiers, with the exception of the output stage, the amplification constant of the tube is the pertinent factor. The higher the amplification constant, the higher the stage gain, provided that the internal plate resistance is not too high relative to the load resistance. The higher the internal plate resistance of the tube, relative to the load resistance, the less the amount of signal taken out of the tube will be. The portion of the available signal taken out of the tube is expressed as

$$
\frac{R_{1}}{R_{p}+R_{1}}
$$

where $R_{1}$ is the load resistance in ohms and $R_{p}$ is the internal plate resistance expressed in ohms.

Another matter of concern to keep in mind is that relating to grid bias. Quite a few tubes used in $R-C$ coupled amplifiers as well as in $L-C$ coupled systems are of the zero-bias type. When adequate substitutes are not available and a self-bias tube is used in place of a zero-bias one, provision for the bias must be made in the circuit. This can be in the form of a bypassed cathode resistor. In addition, the grid resistor (grid leak) of the substituted stage will require reduction to perhaps one-thirtieth or one-fortieth of its original value. Zero-bias tubes utilize grid resistors of from 5 to 10 megohms. Self-bias amplifier tubes utilize grid resistors of from 0.1 to perhaps 0.3 megohms. These bias- and grid-resistor references will be found to apply to pentodes and tetrodes as well as triodes. When a zero-bias tube is used in place of a self-bias tube, the above-required changes in circuits are reversed.

In the output stages, for that matter, also in driver stages in audio amplifiers, attention must be paid to the recommended load impedance represented by the output transformer. Not only does it determine output power, which may or may not be important, but it also determines the quality of reproduction. The latter is important.

To begin with, the recommended load impedance for substitute tubes should be the same or less than that for the original. By being less than the original a fair semblance of the original quality will be retained because the tules are working into a higher impedance, that represented by the output transformer already in the device. Power output will be reduced somewhat but quality of reproduction will be retained. If it is impossible to find substitutes which require the same, or a lower load impedance than the original, then a higher rating will have to be accepted, but it should be the closest approximation to the original.

A receiver installation can afford to sacrifice some power for quality. In public address systems, it is a question of how the system is used. If its full-rated power output is seldom used, then it can sacrifice some output for quality. If it is used for the reproduction of speech only, it can afford a greater mismatch than systems which reproduce music and speech. In the last analysis it is a compromise and each individual requirement determines the choice.

In view of the power-handling requirements of the output stage, only those substitutes, both triodes and pentodes, are usable which can handle power. These are interchangeable but only on that basis.

When two individual tubes are used in a push-pull output stage and a substitution is being contemplated for one tube, it should be carried out for both. If the characteristics of the original and the substitute differ markedly, parasitic suppressors may be required in grid and plate leads (if they are not already in the circuit). Fifty-ohm resistors capable of handling the currents involved are adequate. If two individual tubes replace two tubes in a single envelope, such resistors may prove very important because the changes in wiring and lengthening of the leads may cause oscillation.

Negative feedback is used in many audio systems between the output power stage and a preceding stage. Tube substitutions can upset the feedback conditions, especially if the electrical characteristics of the substitute are unlike the original. If audio quality or power over-all gain seems to have suffered too much, the feedback circuit should be checked.

When tube substitutions in a-f driver stages are contemplated, the range of substitutes is more limited than in the case of voltage amplifiers. While tubes designed for the driver stages of a-f amplifiers may be used in other capacities, tules designed for other functions very often are not usable in a driver stage. Because the tube grid in the driver stage is driven into the positive region during certain portions of the signal cycle, the tube which feeds the driver-stage input transformer must be of the correct type for operation with the driver-stage input transformer. In like manner, the driver stage is impedance-matched to the transformer which feeds the succeeding stage. This is another requirement that must be satisfied when the substitute tube is selected from a number of types which possess
the required over-all similarity in electrical characteristics.

## Phase-Inverter Stages

Phase-inverter stages present no serious problems in substitution except for the fact that differences between the original and the substitute may demand readjustment of the load resistor so as to arrange that the signals from the phase-inverter stage to the control grids of the succeeding push-pull stage are of like magnitude. If the phase-inverter stage serves just one function, inverting the signal to one of the succeeding push-pull stage tubes, and it is of the same type as its related amplifier tube which feeds the other succeeding push-pull tube, then it may be convenient to substitute like tubes for the phasc inverter and its related amplifier.

## Diode Rectifiers (Signal)

Too much need not be said about signal-rectifying diodes. One significant detail is that power rectifiers are not substitutes for signal rectifiers. (They are not shown as substitutes on the list, but the comment is still required.) There is very little to choose from between signal-rectifying diodes for virtually anyone will perform the functions of the others, except perhaps in connection with frequency of operation. The transit time (time taken for the electrons to advance from cathode to plate relative to the period of a cycle of the signal) limits the application of the tube in terns of frequency. Uhf diodes are stuitable for operation at lower frequencies. On the other hand, the low or conventional frequency diodes are not suitable for the rectification of uhf and sometimes even vhf signals, unless so specified.

It is interesting to note that the equivalent of conventional signal-rectifying diodes may be formed out of conventional triodes by tying the grid and plate together thus forming one element. or by tying the plate to the cathode and using the control grid as the second element. Such equivalence is not indicated in the list of substitutions, but it should be kept in mind.

Sometimes multipurpose tubes used in receivers do not employ all of the electrodes. Quite frequently a duo-diode may have its two plates tied together forming a single diode to be used for a single purpose. It is well to try to disconnect one of the plates and to see if the operation is impaired; if not, then the other diode plate may, in conjunction with the common cathode, be used as the substitution diode. Whether or not such is possible depends upon the manner in which the common cathode is being used.

New advances in the design of germanium crystal diodes facilitate.the use of these components as replacements for conventional diode tubes in signal-rectifying and detecting circuits. An important consideration in
this connection is the fact that they require no heater supply and have an average life of over 10,000 hours.

Germanium crystal diodes are usable in vhf and even uhf circuits since their maximum operating frequency is about 500 Mc . They are rated for voltages of from 25 to 200 volts, with peak anode currents up to 200 ma . These components are particularly suitable for detector circuits where their low shunt capacities (of the order of 1 mmf ) are advantageous.
The sulstitution of a crystal diode for a conven-tional-type tube is particularly simple because there is no need for a heater supply circuit. A typical use of a 1N34-type crystal diode is illustrated in Fig. 1-1.


Courtesy Sylvania Rlectric Products Inc.
Fig. 1-1. The use of a 1 N34 type germanium crystal diode in the video detector circuit of a television receiver. Notice that the value of the circuit parameters are similar to those found in most video detector stages.

Here the component is shown being used in a videodetector circuit of the type common in most television receivers. The performance of the circuit with the 1N34-type crystal diode depends upon the proper choice of circuit parameters. In most circuits, however, it will be found that there need be no component modifications for grood performance. Conventional-type tubes for which germanium crystal diodes are successful replacements are the $6 \mathrm{AL} 5,6 \mathrm{H} 6,6 \mathrm{~T}$, and 12AL5. In the replacement of duo-diodes not only must the detector function be taken care of, but the sync limiter or other use must also be replaced. This is possible by using a 1 N35-type matched duo-diode crystal component. See the table of geranium crystal diodes in Section 5.

For further information as to the use of germanium crystal diodes in video and f - m detector circuits as well as in other signal rectifiers, see 40 Uses for Germanium Diodes, a booklet obtainable from Sylvania Electric Products, Inc.

## Diode Rectifiers (Power)

Power rectifiers are of two types, high-vacuum and gaseous. Normally, high-vacuum rectifiers are interchangeable as are gaseous ones, within the limitations set by the current and voltage ratings of the device.

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Gaseous-type rectifiers frequently may replace vacuumtype rectifiers provided that the electrical characteristics are the same and the related circuit requirements are satisfied. Replacement of high-vacutum rectifiers by the gaseous kind is not recommended except when high currents are involved and when a constant voltage drop in the rectifier is required: the need for high voltage alone is not sufficient.

To take a typical case, the mercury-vapor rectifier requires choke input instead of capacitor input in the filter system. The high current surges which occur with capacitor input would destroy the gaseous tube. Also. gaseous tubes are suitable for the rectification of medium voltages and higher ( 500 volts output and up) and they are intended for systems wherein high current loads exist and where the variations in current load are large. In the case of a-c-d-c receivers, there are no gaseous equivalents for the high-vacuum types used. Gaseous rectifiers, moreover, are a source of r-f "hash" and, therefore, are not suitable for use in close proximity to circuits susceptible to such radiations.

High-vacuum tubes, on the other hand, are suitable replacements for mercury-vapor rectifiers if the rectifier system can stand the increased voltage drop which occurs in the high-vacuum tube and if the electrical requirements are satisfied. As a rule, the heater current for high-vacuum rectifiers is less than that required for gaseous rectifiers of comparable d-c voltage and current output. Other important electrical requirements to consider are the a-c input voltage, output current, and inverse peak voltage. The last-named term expresses the ability of the tube to withstand the peak voltage between the anode and the cathode during the nonconducting portion of the cycle.

Assuming the lack of recommended substitutes, high-vacuum tubes are suitable for substitution in systems which operate at lower d-c output voltages and currents than the high-vacuum tubes are rated for, provided that the heater requirements are satisfied. Such substitution should be made only in extreme cases when no other means are possible and a system must be restored to operation. For that matter, in such an event, the mercury-vapor kind also can be used provided that there is a choke input in the filter system. This is a MUST conclition.

The substitution of a filament-type rectifier for a cathode-type one introduces certain complications, especially when the remainder of the tubes in the system are of the cathode-heater variety. The difference in heating time would result in the very rapid build-up of the voltage output from the rectifier before the tubes receiving the plate and other voltages were in a conducting state. Thus, the rectifier would be operating for a period of time with practically no load. This results in a high output voltage - much higher than when the load is applied - and could very easily break down the filter capacitors and also some of the bypass capacitors in the equipment receiving its voltage from
the rectifier. Replacing a filament-type rectifier with a heater type causes no complications of this sort.

From a practical viewpoint it seems worthwhile to go to no end of trouble to find a suitable filament-type stibstitute for a filament-type original. This seems easier than changing the voltage rating of all of the filter capacitors and the bypass capacitors for high working voltage units. Of course, if examination of the capacitor voltage ratings and measurement of the rectifier output voltage shows that the momentary peak is within the operating voltage rating of the capacitors, the change can be made without endangering the filter and bypass units. If this is not the case and replacement of the filter and bypass capacitors is not feasible, then the only alternative is to use an increased bleeder load and thus reduce the over-all output voltage from the power supply.

For medium- and low-voltage requirements, selenium rectifiers are far more suitable substitutes for highvacuum rectifier tules than are gaseots tubes. Miniature selenium rectifiers are available in various sizes rated from 50 to 500 ma . The $50-, 65-$, 75 -, and $100-$ ma, sizes will, in most cases, best serve as replacements for half-wave rectifiers in a-c-d-c equipment.

Generally speaking, to replace the vacuum-tube rectifier in a phonograph oscillator, use the selenium rectifier rated for 50 ma , for three-tube amplifiers use the 65 -ma size, for five- or six-tube receivers without a push-pull output, use the $75-\mathrm{ma}$ rectifier, and for sixtube sets and up use the 100 -ma rated one. To replace the $25 Z 5,25 Z 6,35 W 4,35 Y 4,35 Z 3,35 Z 4,35 Z 5,45 Z 5$, 50 Y 6 , and $50 \mathrm{Z7}$, use a 403 D 2625 A type selenium rectifier with a rating of 100 ma .

When a rectifier tube is replaced by a selenium rectifier, a compensating resistor must be inserted into the filament circuit to make up for the resistance drop due to the elimination of the rectifier tulee if its filament was in series with other filaments. The value of this compensating resistor depends upon the rectifying tube that has been replaced. The following table lists the resistance to be used for the tubes mentioned above.

| TUBE | RESISTOR <br> (ohms) | WATTS |
| :--- | :---: | :---: |
| 25Z5 | 85 | 15 |
| $25 Z 6$ | 85 | 15 |
| $35 W 4$ | 230 | 10 |
| $35 Y 4$ | 230 | 10 |
| $35 Z 3$ | 230 | 10 |
| $35 Z 4$ | 230 | 10 |
| $35 Z 5$ | 230 | 10 |
| $45 Z 5$ | 300 | 10 |
| 50 Y 6 | 330 | 15 |
| $50 Z 7$ | 330 | 15 |
| $117 Z 3$ | none required |  |
| $117 Z 6$ | none required |  |

In some sets, the pilot light may be connected across a low-voltage tap on the rectifier tube filament. If this

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is so in the set in which the rectifier tube is being replaced, connect the pilot light across a tapped-down portion of the compensating resistor (about 10 to 25 ohms will do depending upon the current in the filament circuit). A No. 47 pilot light can be used in this case.

When replacing vacuum-tule rectifiers by selenium rectifiers in a-c-d-c portables using battery-type tubes that obtain filament voltages from $\mathbf{B}$ plus through a dropping resistor, reduce the value of the shunt resistor connected from the low end of the filament dropping resistor to the negative point. This will compensate for the increase in filament voltage.
In most cases, a protective resistor should be inserted in series with the selenium rectifier to protect the rectifier and filter capacitors from excessive current peaks cluring operation. The value of this resistor will vary from 5 to 50 ohms depending upon the current load of the rectifier; the higher the load, the smaller the protective resistor needed.

Manufactured adapters will probably be available for use with miniature selenium rectifiers in the future, in the meantime, they can be made fairly easily by using discarded tube bases. Following are instructions for making adapters for a few of the most popular rectifier tubes used in a-c-d-c equipment.

To make an adapter for the $35 Z 5$ used in series circuits:
a) connect a 230 -ohm, $10-\mathrm{w}$ resistor from No. 2 to No. 7 on an octal base
b) connect a 20 -ohm, $1 / 2-\mathrm{w}$ resistor from No. 2 to No. 3
c) connect 25 -ohm, $1 / 2$-w resistor from No. 8 to positive side of rectifier
d) connect No. 5 to negative side of rectifier.

To make an adapter for a $35 Z 5$ used by itself, follow the above steps but delete steps a) and b).

For the 25Z6, 25X6, 35Z6, 50AX6, 50Y6, and the 117 Z 6 when these tules are used by themselves as halfwave rectifiers, make an adapter as follows:
a) connect a 25 -ohm, $1 / 2$-w resistor from Nos. 4 and 8 on octal base to the positive side of the rectifier
b) connect Nos. 3 and 5 to negative side of the rectifier.
If the filaments of these tubes are in a series circuit, then naturally a compensating resistor must be added with the selenium rectifier. This resistor, whose value may be obtained from the table given previously, will le connected between pins No. 2 and No. 7. No resistor is needed when the 117 Z 6 is replaced.

## Wideband Amplifiers (Video and Others)

Although referred to earlier in this section, these systems are singled out for elaboration because of their seemingly peculiar conditions of operation. Ex-
amination will show that very low values of plate-load resistance are used and also that the applied plate voltage is very low. much lower than that shown in tule characteristic charts.

This is so because it is necessary to have wide frequency response. Gain in each stage is sacrificed for the attainment of low reflected capacitance and also the creation of suitable resonance. ${ }^{1}$ By means of shunt or series peaking, or both, a wide band of frequencies can be amplified. (This is explained in detail in the book referred to in the footnote.)

Tube substitutions in wideband amplifiers, therefore, require yery serious consideration. The substitute tube characteristics should approximate most closely the complete conditions existing in the original. Interelectrode capacitance is very important. Plate-current, grid-bias, and grid-circuit resistance ratings should be the same. Lead dress must le maintained as much as possible because changes in the position of leads will affect the frequency of resonance and thereby the overall loandwidth of the system. This is very important if socket changes are required.

If possible, all stages should be replaced by like substitutes even if only one stage requires replacement. This is expensive but advantageous. If the facility to check frequency bandwidth exists, then it is possible to confine the replacement to only one stage, the one in which the original tube is bad. Make the frequency run, and if the response is satisfactory after the replacement in that stage, the other stages need not be changed. Such tests can be made by means of a squarewave generator or a sine-wave generator. Usually the limits of response are expressed by the lowest and highest frequency signals which are down not more than 3 db from the top. In some instances, the amplifier design is more critical and the over-all response is expressed in terms of only 1 db down from the top.

## Utilization of Sections of Multifunction Tubes

A number of tubes found in television and other equipments comline three and four sets of electrodes in a single envelope, thus performing three or four different functions. Direct substitutions for these tubes may not be available. In that event it is necessary to utilize two individual tubes containing such electrodes as will furnish the facilities originally contained in the single tube which is being replaced. For example, a triple diode-triode such as the 6 T 8 may require replacement. If the original is not available, pairs of substitutes must be used, for example, a 6AL5 and a 12AV6 or a 6AL5 and 6AQ6. These are the recommended combinations, other combinations of a doublediode with a clouble-diode triode, or single diode-triode

[^0]will function satisfactorily. One of these tubes takes over the function of two diodles in the 6T8 and the other tube takes over the function of the remaining diode-triode.

Substitution of two tules for one is not easy; it means adding sockets and perhaps even changing sockets on crowded chassis where space is at a premium. This requires planning of the socket location and the location of shunt and series resistors, so as to keep connecting leads short. But it can be done, and it is a vivid example of how tubes with more electrodes (and capable of more functions) than the original may be used in replacements so long as only the necessary number of electrodes are utilized. Also it is an example of how it may be necessary to utilize several substitute tubes to perform the function of one original. Incidentally, pairs of tubes which can be used in place of other multifunction tubes are listed in an addendum to the tube substitution list. Which combination of substitute tubes fills the replacement of a single original is a matter of individual circuit design. Very many possible substitutions of this kind exist, especially in so far as signal diodes are concerned.

## Tube Substitution Techniques

Heater circuits are very significant in connection with tulbe substitutions because tube types are organized in terms of heater voltage. Therefore, it is quite in order to show the techniques involved in arranging tube heater circuits so as to accommodate substitute tubes. Before discussing the methods, however, in fact even before speaking about heater ratings, it might be well to emphasis one very important point, all heater ratings are interpretable in terms of resistance. The ohmic value of a heater is the same when it is operated on direct current or alternating current. Any reference to heater voltage considers the d-c value and rms or effective a-c value as the same. Thus a tube heater rating of 6.3 volts means 6.3 volts d.c. or 6.3 volts rms a.c. The same applies to any other numerical rating. Note: Many battery-operated tubes zeill not function properly on a.c.

Heater current is treated in like fashion. A reference to 0.15 ampere or 150 ma means d.c. or a.c., the latter being the rms value. The rms value is used because it is responsible for the heating effect in filaments and to get equivalent heating in d.c. and a.c., the d-c value must equal the rms a-c value.

While the above statement is true in all conditions associated with resistance, it should not be assumed to apply to all a-c systems regardless of circumstances. For example, the $\mathrm{d}-\mathrm{c}$ value of voltage is related to the peak value of an a-c voltage when insulation resistance is involved. This is important in the operation of capacitors and in connection with the insulation breakdown of rectifier tubes during the nonconducting portion of the cycle.

## Heater Ratings versus Heater Circuits

It is common practice among electronic equipment manufacturers to use certain kinds of tubes for certain kinds of equipment. For example, in most a-c-d-c equipment, the tube heaters are connected in series across the line. The same is true when such equipment is intended for battery-operated portable use (the threeway portalles). Other equipments are designed for operation from the a-c power lines only and the heaters are arranged in parallel chains. Still other equipments use a combination of series-parallel systems, as for example, a-c-d-c television receivers.
Sometimes the series chain is singular; sometimes there are a number of chains connected in seriesparallel between different points as shown in the schematics at the end of Section 3. In the parallel systems, several independent parallel chains are used. Usually the rectifiers are wired individually and, in the true sense, are series circuits. The remainder of the tubes are, however, in parallel, all being on one chain or divided among a number of chains fed from individual voltage sources. These too are illustrated in Section 3. Incidentally, the receivers inclucled in that section represent practically every one produced and sold in the years 1938 through October, 1950 as contained in Rider's TV Manuals Volumes 1 through 5.

## Parallel Circuits

Parallel chains will accommodate tubes which require equal heater voltage ; they will also accommodate tubes with heater voltage ratings with are lower than that being supplied to the remainder of the tubes. This is shown in Fig. 1-2. The cuirrent rating of the heater is a matter of secondary concern in parallel chains.


Fig. 1-2. Parallel connection of vacuum-tube heaters. The voltage drops across the heaters so connected are equal to the voltage across the secondary of the power transformer as shown.

If the supply voltage source (the heater transformer) is capable of supplying the required current at its rated output voltage, then any reasonable heater current requirement set by the substitute can be satisfied. The only limitation which exists relative to parallel connected heaters is that the output voltage rating of the heater transformer cannot be exceeded. The current through the parallel heater is determined by the resistance of the heater so that, if the voltage is correct, the current will be correct. If the current drain of the substitute heater added to the total current drain of the other tubes in the parallel chain exceeds the current output capabilities of the heater transformer, the

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voltage will fall on all the heaters. It is possible to operate all receiving tubes at perhaps ten per cent below the normal voltage and current ratings. In special cases this reduction can be exceeded but it is not recommended.

Tule sulbstitutes which bear heater voltage ratings lower than that of the original tube can be applied readily to parallel circuits. All that is needed is to drop the supply voltage to the level demanded by the substitute. The correction must be applied directly in the circuit which feeds the substitute tube. This is shown by the location of $R$ in Fig. 1-3. The amount of volt-

Fig. 1-3. When substituting a tube with lower voltage requirements than the original, a series resistor is added in the branch of the parallel feed in which the tube is placed. The resistor may be a single one as in (A), or two smaller ones as in (B).

age to be dropped is the difference between the supply voltage $E$ and the tube heater requirement $E_{1}$. Suppose we wish to substitute a 2 B 7 with a 2.5 -volt heater for a 6B7 whose 6.3 -volt heater drew its supply from a filament transformer with an output of 6.3 volts. The difference $E-E_{1}$ is 3.8 volts and this must be dropped at the heater current rating of the substitute tube, namely, 0.8 ampere. The value of the voltage-dropping resistor then is

$$
R=\frac{E-E_{1}}{I}=\frac{3.8}{0.8}
$$

or

$$
R=4.75 \text { ohms or roughly } 5 \text { ohms. }
$$

The power rating of $R$ is

$$
P=I^{1} R=0.8^{2} \times 4.75=3.204 \text { watts }
$$

In the examples cited, the substitute imposes a load that is somewhat greater than the original; the power consumption of the 6B7 heater is 1.89 watts whereas that of the 2B7 is 2.0 watts. To this must be added the power dissipated across the voltagedropping resistor $R$, for, after all, it is a part of the newly created load. Roughly, this amounts to 3 watts. So, the substitution of a 2 B 7 for a 6 B 7 means the imposition of a 5 -watt load in place of the original 1.89 watts, or an increase in load of 150 per cent.

Normally, the addition of such a load will cause no trouble, but in the event that several tubes require sub-
stitution, the load may be increased to the extent that the voltage drop in the transformer secondary becomes excessive, and the voltage across all of the heaters will be lowered.

Some television receivers utilize a heater voltage supply which is the equivalent of two 6.3 -volt windings in series, with the centertap grounded and acting as a common return path for two parallel chains of 6.3 -volt heaters. This is shown in Fig. 1-4. Each winding furnishes 6.3 volts for its respective chain, but by virtue of a common center connection, the difference of potential between the extremes of the two windings is twice that of each, or 12.6 volts. Consequently, a $12.6-$ volt heater can be used by connecting it across the extremes of the windings.

Fig. 1-4. Filament circuit of the type found in many television receivers. The center tap between the two windings is grounded to serve as a return for the filaments in parallel, each of which receives 6.3 volts from its part of the secondary.


If necessary, more than one tube substitution can be handled in this way. The voltage between the extremes of the two windings is a maximum which cannot be exceeded, therefore, even such an arrangement does not permit the use of a tube which requires more than 12.6 volts (or whatever the voltage happens to be between the two extremes of the windings).

The number of 12.6 -volt tubes which can be handled in the manner shown in Fig. 1-4 is not without limit. The power-handling capability of the two windings is the controlling factor. The substitution of a single 12.6 -volt tule in place of a 6.3 -volt tube is no problem especially when the power consumption is the same for both heaters; more than likely it will not cause any concern even if an increased load is created by the selection of some special type of 12.6 -volt tube.

## Series Circuits

The substitution of tules in series-wired heater arrangements hinges upon the following fundamentals of Ohm's law relating to series circuits:

1. In a series circuit there is only one path for the current.
2. The current in a series circuit is equal to the applied voltage divided by the total resistance.
3. The sum of the individual voltage drops in a series circuit equals the applied voltage.
Illustrated in Fig. 1-5(A) are four tube heaters connected in series across a voltage supply source $E$. Only one path exists for the flow of current $I$, therefore, the current must be the same in all parts of the circuit,

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that is, in each heater. This immediately establishes the requirement that all heaters connected in series must have similar current ratings. A variation of 10 per cent in heater rating is permissible so long as the heater has a higher rating than the current required by the other heaters in the circuit.

Fig. 1-5. Filaments connected in series (A) may be represented as individual resistances (B), each of which passes the same current determined by the applied voltage divided by the total resistance.


The numerical value of the current is dependent upon the applied voltage $E$ and the total resistance $R$ of all of the heaters, as stated in statement 2. above Since resistances connected in series are additive, the total heater resistance $R$, is equal to $R_{1}+R_{z}+R_{3}$ $+R_{\natural}$, as indicated in Fig. 1-5(B). If, for the moment, we assume that each heater is rated at 12.6 volts and 0.15 ampere ( 150 ma ), then the resistance of each is 12.6 divided by 0.15 or 84 ohms. The four heaters in series, therefore, represent a total resistance of 336 ohms. Knowing the total $R$ and the required current, the supply voltage necessary to limit the current to the required value is

$$
E=I R
$$

or

$$
E=0.15 \times 336=50.4 \text { volts }
$$

If the voltage drops across each heater (or the voltage required across each heater) are aggregated, it is seen that the sum of the voltage drops equals the applied voltage. Thus are illustrated statements $1 ., 2$., and 3.
In view of what follows it might be well to devote a little more time to the matter of voltage drops and applied voltage, or the possibilities of statement 3 . Current flowing through a resistance will cause a voltage drop across that resistance. If the current flow is the rated value, then the voltage drop numerically is the same as the voltage rating of the resistance. If the resistance is the heater (or filament) of a tube, and the current through it is the rated value, then the voltage drop is equal to the voltage rating of the heater.
We have simplified the problem by deliberately making the applied voltage (which we also can identify as the line voltage) equal to the total of the voltage drops in the load. As a rule, this is not found in practice; the line voltage always exceeds the total of the voltage drops across the tube heaters. This excess voltage is dropped by means of a line voltage-dropping resistor across which there is a voltage drop equal to the difference between the sum of the tube heater voltage drops and the line voltage. For example, if the line
voltage is 117 volts and the total of the tube heater voltage drops is 50.4 volts as in the above case, the line voltage-dropping resistor will drop 117 - 50.4 or 66.6 volts at the value of current which is flowing through the series chain.

Statement 3 still holds, except that now the series line voltage-dropping resistor has been added to the elements (heaters) which comprise the load. This action of the line voltage-dropping resistor may be considered from a different viewpoint. It is the means whereby the line voltage is dropped to that value which equals the sum of the voltage drops across the heater elements. This is not a play on words; it simply presents the relationship between the line voltage and the total heater drops from two angles relative to the purpose of the line voltage-dropping resistor. In one case, the line voltage-dropping resistor is considered a part of the load and, in the other, only the tube heaters are considered to comprise the load. Personally, we prefer the former and shall hold to it in these explanations.


Fig. 1-6. A series chain of four filaments or heaters with a line voltage-dropping resistor. The voltage drop across the line voltage-dropping resistor makes up for the differences between the line voltage and the voltage required by the four heaters.

An example of the above is shown in Fig. 1-6. Here the elements of the load are shown to the right of the vertical dotted line and the applied voltage source is shown to the left. The series system indicates a total heater voltage drop of 50.4 volts at 0.15 ampere and a line voltage of 117 volts. The difference in voltage is dropped across the resistor $R$. Since the line voltagedropping resistor is in series with the heater chain, the same current will flow through $R$ as through the heaters. The voltage drop across this resistor is, therefore, a function of the current through it and its resistance. Since this voltage drop represents a dissipation of energy, the line voltage-dropping resistor bears a wattage rating in addition to its resistance rating. The power dissipation is a very important factor and must be taken into account in the event of any changes; in fact, it determines the type of resistor element which suits this purpose. The power dissipation in watts is expressed by either $I E, I^{2} R$, or by $E^{2} / R$, where $I$ is the current in amperes, $R$ is the resistance in ohms, and $E$ is the voltage in volts, exactly the same units as are used for the other Ohm's law calculations.

The ohmic value of $R$ is

$$
\begin{aligned}
R & =\frac{117-50.4}{0.15} \\
& =\frac{66.6}{0.15} \\
& =444 \text { ohms }
\end{aligned}
$$

Its power dissipation is

$$
\begin{aligned}
P & =E \times I \\
& =66.6 \times 0.15 \\
& =9.99 \text { watts (approx. } 10 \text { watts) }
\end{aligned}
$$

or

$$
\begin{aligned}
P & =I^{2} R \\
& =0.0225 \times 444 \\
& =9.99 \text { watts (approx. } 10 \text { watts }) .
\end{aligned}
$$

To prove these figures, the total resistance of the four heaters is $4 \times 84$ or 336 ohms; adding this to the 444 ohms resistance of the line voltage-clropping resistor results in a total circuit resistance of 780 ohms. With a current of 0.15 ampere flowing in the system, the applied voltage is $E=0.15 \times(336+444)=117$ volts.

Let us now examine the possible variables in a simple series chain of the kind shown in Fig. 1-6. Statement 3. of Ohm's law relates to an equality between the line voltage (applied voltage) and the total of the voltage drops in the load. No restriction is evident concerning the number of elements (tube heaters) which may comprise the load and across which the total of the heater drops will occur. In the system shown in Fig. 1-6, four elements comprise the heater load. These could be any number provided that the total voltage drop did not exceed the line voltage ; if it equaled the line voltage, then the line voltage-dropping resistor ( $R$ in Fig. 1-6) would not be required in the circuit and the system would become the equivalent of Fig. 1-5(A), with more heaters than are shown there.

As a matter of fact, no matter what the total of the rated voltage drops across the heaters in the load is, this value can never exceed the applied (line) voltage, for statement 2 . establishes that the current will adjust itself automatically in accordance with the total resistance and the total applied voltage. For example, if fourteen 12.6 -volt, 0.15 -ampere tubes were used in series across a 117 -volt line, the total resistance would be 1,176 ohms. The current, therefore, would be

$$
\frac{117}{1.176}
$$

or 0.099 ampere, and the voltage clrop across each heater would be $0.099 \times 84$ or 8.3 volts. It is obvious that the voltage across these heaters would be insufficient for proper operation of the tubes. Correction of this state would demand a revision of the circuit or an increase in the line voltage; the latter is impractical, so the former is the only solution. It will be treated later.

On the other hand, the need may arise to substitute a lower voltage rated heater for a higher rated one,
such as a 6.3 -volt tube for a 12.6 -volt one. If the rated voltage drop across the series heaters is at least ten times the rated voltage drop across the substitute heater, the latter may be inserted into the string without requiring any correction. Thus, if the total rated voltage drop across the series heaters is 75 volts, and a 6.3 -volt tube is a replacement for a 12.6 -volt heater in the string, the replacement will be subject to a slightly higher voltage (and current) but it will do no harm.

For example, if the original series string consists of a 25 -volt, 0.15 -ampere tulse and four 12.6 -volt, 0.15 ampere tubes, the total resistance of these heaters is 502 ohms. Operation from a 117 -volt line demands a dropping resistor of 227 ohms, making a total load resistance of 779 ohms. Substituting a 6.3 -volt tube for the 12.6 -volt one reduces the heater resistance to 460 ohms, and the total load to 737 ohms. This results in a circuit current of 0.158 ampere, and as a result, the 12.6 -volt tubes are subjected to a voltage of 13.27 volts, the 6.3 -volt tube to 6.6 volts, and the 25 -volt tule to 26.4 volts. None of these voltages are so extreme as to endanger the tubes.

Battery tubes, however, should be treated with more care and every effort should be made to keep the voltage as close to the rated voltages as possible, especially when operation is intended on a-c lines.

Circuit conditions encountered in practice seldom are such that the total voltage drop across the heaters or filaments equals the applied or line voltage. The use of a line voltage-dropping resistor is very common, consequently, any change in the total voltage drop across the load caused by a substitution demands that the drop across the line voltage-dropping resistor be changed, and this means a change in its ohmic value. Whether the latter is done by shunting another resistor across it, by physically changing its length (as happens with line cords), or by substituting a new one of proper ohmic value for the original is determined by whichever is most convenient. If the total voltage drop across the heaters is increased, the drop across the line resistor must be decreased, and vice versa. A typical example follows.

Seven 6.3-volt heaters are in series with a 35 -volt heater. All are rated at 0.3 ampere. The total voltage drop across the heaters is 79.1 volts and the total resistance of the heater load is 264 ohms as shown in Fig. 1-7(A). With a supply of 117 volts, 37.9 volts must be dropped across the line dropping resistor $R$. At 0.3 -ampere current flow, the ohmic value of $R$ must be 126 ohms and its power dissipation, therefore, is 11.3 watts.

Two 12.6 -volt, 0.3 -ampere tubes must be substituted for two of the 6.3 -volt tubes. The modified circuit is shown in Fig. 1-7(B). Simple calculation of the total voltage drop across the heaters shows an increase of 12.6 volts, therefore, it is obvious that the value of $R$ will have to be decreased. Its value may be determined

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in a number of ways, but a simple procedure is the following

$$
\begin{aligned}
R_{\text {new }} & =\frac{\begin{array}{c}
\text { Original value of } E_{R}-\text { Increased voltage } \\
\text { drop across heaters }
\end{array}}{\text { Current through the system }} \\
& =\frac{37.9-12.6}{0.3} \\
& =84 \text { ohms. }
\end{aligned}
$$

The power dissipation in the new $R$ is

$$
\begin{aligned}
P & =I^{2} R \\
& =0.09 \times 84=7.5 \text { watts }
\end{aligned}
$$



Fig. 1-7. In (A), a series chain of seven 6.3 -volt heaters and one 35 -volt heater requires a line voltage-dropping resistor $R$ of 126 ohms to bring the applied voltage of 117 volts down to the value required by the heaters. When the total voltage drop across the heater is increased by 12.6 volts as in (B), the value of $R$ must be decreased to 84 ohms.

## Substituting Low-Current Rated Heaters for Higher-Current Heaters

Suppose that in the circuit of Fig. 1-7(A) two 12.6volt heaters rated at 0.15 ampere must replace two of the 6.3 -volt 0.3 -ampere heaters. Let us select $H_{3}$ and $H_{s}$ as the specific heaters. How would this be accomplished? Two methods are practical, one being simpler than the other. Suppose we treat the more difficult one first.

Since the circuit current is 0.3 ampere and each substitute heater draws only 0.15 ampere, it stands to reason that they just cannot be connected into the circuit as is, otherwise each would be subject to a 100 per cent current overload. However, two such heaters connected in parallel would require 0.3 ampere, and because of the division of currents in a parallel circuit in accordance with the resistance of each branch, connecting these two tubes in parallel would result in 0.15 ampere flowing through each heater. Moreover, the voltage drop across two elements in parallel is the same as that across a single element and, since the total drop across the two 6.3 -volt heaters which are being replaced equals 12.6 volts, the two 12.6 -volt heaters in parallel can replace the two individual 6.3 -volt heaters without changing the total voltage drop across the
string of heaters. This is shown in Fig. 1-8(A). Note that the total drop across the string of 6.3 -volt heaters originally [Fig. 1-7(A)] was 79.1 volts, and that the total drop across the heaters with the two parallel 12.6volt substitutes is 79.1 volts. This means that the line dropping resistor $R$ need not be changed since it is called upon to drop 37.9 volts at 0.3 ampere, the same as in the original circuit.

The other means of accomplishing the substitution is shown in Fig. 1-8(B). Instead of connecting the two


Fig. 1-8. Two methods of substituting 12.6 volt, 0.15 -ampere heaters for 6.3 -volt, 0.3 -ampere ones are shown. In (A), both substitutes are paralleled together, splitting the current and keeping the voltage drop of the system intact; in (B), each heater has its own shunt, thereby drawing its rated current but increasing the total voltage drop of the heaters.
substitute heaters in parallel, they are treated individually and separate current shunts are connected across each one. Since it is desired to split the current equally between the heater and its shunt, the ohmic values of the shunts must equal the resistances which they shunt. This means that $R_{s}=84$ ohms and $R_{s}=84$ ohms, and each dissipates 1.89 watts. [See Fig. 1-8(B)].

However, handling these substitutions in this manner means that the total voltage drop across the string of heaters has been increased by 12.6 volts, since two 12.6 -volt heaters in series total 25.2 volts, and two 6.3volt heaters in series total only 12.6 volts. The increased drop of 12.6 volts must be compensated for by reducing the drop across the line resistor $R$. Figs. 1-7(A) and 1-8(A) are comparable, as are Figs. 1-7(B) and 1-8(B). In Figs. 1-8(A) and (B), the total line current of 0.3 ampere flows into the junctions of the parallel systems (the parallel heaters in (A), and the heaters paralleled by the shunt resistors in (B), divides equally between the two paths, and then recombines again to equal the 0.3 -ampere line current. Thus, the 0.3 -ampere, 6.3 -volt heaters receive the proper current and so do the two 12.6 -volt, $0.15-\mathrm{am}$ pere heaters.

If four tubes required substitution and they were of like voltage ratings, two pairs of heaters could be paralleled as shown in Fig. 1-8(A). If there were an odd number of substitutions, two heaters could be located in parallel and the odd one would be operated with a shunt as shown in Fig. 1-8(B). As a matter of fact, it is the principle underlying these techniques rather than the actual number of tubes involved which is important. Once the principles are understood, it will be simple to apply them, and in general, the most convenient method should be used depending on the circuit and the components available. For example, the availability of resistors is a determining factor in deciding whether the line dropping resistor will be replaced or if two small resistors will be used for the current shunts. If the substitution demands new sockets, then paralleling of the heaters is no problem, but if the sockets do not require changing to accommodate the substitutes it is more convenient to use the current shunts.

## Substituting Higher-Current Heaters for Low-Current Heaters

Suppose the requirement is for the use of higher current heaters in place of lower current heaters in a series circuit. A single 0.3 -ampere heater is to replace one rated at 0.15 ampere in a series string of five 12.6 -volt, 0.15 -ampere heaters and one 25 -volt, 0.15 ampere heater. This substitution is to occur at $H_{\sigma}$ in Fig. 1-9(A). Several solutions are shown in Figs. 1-9(B) through (G). The choice is determined by which is most convenient and best fits the need. The one fundamental requirement created by such a substitution is that the total line current must be increased to 0.3 ampere so as to serve the increased current demand of the substitute tube. Whether this means that the line current will be limited to 0.3 ampere or increased above that value is determined by the organization of the heaters which form the load. One circuit system [Fig. 1-9(B) and (C)] needs 0.45 -ampere line current, whereas other arrangements can be served by 0.3 ampere; there is no way, however, of satisfying the requirements of the 0.3 -ampere tube with a line current of 0.15 ampere. For comparison, let us keep the constants of the original circuit [Fig. 1-9(A)] in mind. Here we have a total drop of 88 volts across the heaters, and 29 volts across the line dropping resistor at a current flow of 0.15 ampere.

One solution for the substitution is the use of two series paths, one for the 0.15 -ampere heaters and the other serving the 0.3 -ampere heater, as shown in Fig. 1-9(B). In order not to change the total voltage drop in the 0.15 -ampere chain, a resistance ( 84 ohms) corresponding to that of the heater $\left(H_{s}\right)$ which has been removed is inserted in its stead. This establishes the total voltage drop at the original value of 88 volts and


Fig. 1-9(A). A series chain of heaters each driwing 0.15 ampere in a circuit with a single voltage-dropping resistor.


Fig. 1-9(B). $H_{6}$ of Fig. 1-9(A) has been replaced by a 12.6 -volt, 0.3 -ampere one requiring a separate series circuit and an increase in the current drawn from the line source. Now there are two dropping resistors, one in each branch of the circuit.


Fig. 1-9(C). Same as Fig. 1-9(B) except that the dropping resistor in the longer branch now is a combination of the dropping resistor $R$ and the compensating resistor $R_{1}$ of the previous diagram.
the original line dropping resistor remains intact. Compare Figs. 1-9(A) and (B). Since the drop across the 0.3 -ampere heater is 12.6 volts and the line voltage is 117 volts, a line dropping resistor must be added to this circuit. $R_{g}$ serves this purpose; its ohmic value ( 348 ohms) is such that it will drop 104.4 volts at 0.3 ampere.

Examination of the two series circuits of Fig. $1-9$ (B) shows that they are actually in parallel since each goes from the 117 -volt line to ground. This is illustrated in the equivalent diagram in Fig. 1-9(B). The total resistance of each of the parallel branches is such that 0.15 ampere flows in one, whereas 0.3 ampere flows in the other.

The equivalent circuit in Fig. 1-9(B) is an important one to understand because it shows the application of two series circuits connected in parallel. Television receivers intended for use on a-c-d-c lines employ such circuit arrangements quite frequently, see Fig. 1-8 and the schematics at the end of Section 3.

A modification of Fig. 1-9(B) appears in (C). The substitution requirement remains the same, but this time the resistance equivalent of the heater which has been removed is not inserted. Instead, the line dropping resistor is changed in value so as to compensate for the reduced total voltage drop across the heaters. With one 12.6 -volt heater removed, it has fallen to 75.4 volts from the original 88 volts. This necessitates an increase in the line resistor $R$ from the original value of 193 ohms to 277 ohms. (This follows from the fact that the heater removed from the string had a resistance of 84 ohms, and in order to maintain the original amount of current in the circuit, this amount of resistance must be added to the line dropping resistor. The change is essentially the transposition of the resistor $R_{i}^{*}$ in Fig. 1-9(B) from its position at the grounded end of the string to the line dropping resistor.) Now the drop across the line dropping resistor is 41.6 volts, or the original 29.6 volts plus the 12.6 volts representing the displaced heater. The second series leg of the circuit is the same as shown in Fig. $1-9(B)$, because its demands have not been changed in any way by the modifications applied to the other series circuit.

Several other interesting details may be mentioned about the arrangements in Figs. 1-9(B) and (C). In the latter, the increase in the value of the line dropping resistor means an increase in power dissipation. The power dissipation in the resistor in (B) is 4.34 watts; the power dissipation in the resistor in (C) is 6.23 watts. However, it is necessary to add to the former the amount dissipated in the resistor $R_{1}$ which has replaced the heater. This power is 1.89 watts, which when added to the 4.34 watts, totals the same amount as is dissipated in the higher value of resistance used in Fig. 1-9(C). At first glance there may appear to be no difference between the two systems, yet there is a substantial difference. It is simply that two resistors, one of 4.34 watts and another of 1.89 watts rating (or whatever may be the wattage ratings selected to afford ample safety factor), are definitely more expensive than a single resistor of such wattage rating as will satisfy a power dissipation of 6.23 watts.

For purposes of comparison let us identify the power dissipation in the system shown in Fig. 1-9(C). The power dissipation in the $150-\mathrm{ma}$ leg is 11.34 watts in the heaters and 6.18 watts in the line dropping resistor $R$, a total of 17.49 watts. The power dissipated in the 300 -ma circuit is 3.78 watts in the heater and 31.32 watts in the line dropping resistor $R_{1}$, making a branch total of 35.10 watts. The dissipation in both circuits is the sum of the branch wattages or 52.59 watts.

A third possible arrangement for the substitution is shown in Fig. 1-9(D). In a way, this is a more practical way to connect a 12.6 -volt, 0.3 -ampere heater in place of a 0.15 -ampere heater of like voltage rating. Only one series string is arranged, although it contains two parallel circuits. This system operates in a similar manner to that shown in Fig. 1-8. Of course, the ability to assemble such a circuit depends upon the number of heater elements present. The four heaters $H_{2}$, $H_{J}, H_{4}$, and $H_{5}$ are of like constants, therefore, two series pairs connected in parallel result in a system requiring 25.2 volts and 0.3 ampere. In order that heater $H_{1}$ draw only 150 ma , it is shunted with a resistance equal to its own resistance. Thus, the original six tules now are arranged so that they can be assembled into a single series string and supplied with 0.3 ampere of current.

The rearrangement of the $150-\mathrm{ma}$ tubes reduces the total voltage drop across the heaters because the paralleled pair of series heaters draws only 25.2 volts compared to its former 50.4 volts. The result is that the total drop across the heaters is reduced to 62.8 volts. This requires a change in the line dropping resistor to that ohmic value ( 181 ohms) which will draw 54.2 volts and so drop 117 volts to the 62.8 volts at 0.3 ampere required by the heaters. Relative to the power consumption in such a system, the four series-parallel


Fig. 1-9(D), (E), and (F). Various methods are shown here for shunting the heaters of the circuit shown in Fig. 1-9(A), after the substitution of a 12.6 -volt 0.3 -ampere heater for $H_{8}$, so that the voltage and current requirements of each heater are satisfied.

Fig. 1-9 (G). Part of a television receiver filament circuit showing the isolating chokes used between the heaters in the scries chain. The shunts shown in dotted lines are unacceptable because they nullify the action of the chokes.

(G)
heaters dissipate 1.89 watts each for a total of 7.56 watts; the 25 -volt heater $H_{t}$ with its shunt consumes 7.5 watts ; the 12.6 -volt 300 -ma heater $H_{6}$ consumes 3.78 watts; and the line dropping resistor consumes 16.26 watts. The total power dissipation of the whole circuit is, therefore, 35.1 watts. A comparison between the total power consumption of the circuit in Fig. 1-9(D) and that in Fig. 1-9(C) illustrates the economy in power consumption possible by a choice of circuits.

A modification of the circuit in Fig. 1-9(D), designed to allow the replacement of a $150-\mathrm{ma}$ heater tube with a $300-\mathrm{ma}$ one, is shown in Fig. 1-9(E). Here, all the heaters are in a single chain with a current shunt across each 150 -ma tube ; the 300 -ma heater $H_{6}$ does not require a shunt. The ohmic value of these shunts is equal to the resistance of each of the shunted heaters. The power consumption of the entire system totals 36 watts made up as follows: each of the shunted $12.6-$ volt heaters with its shunt consumes 3.8 watts, the unshunted 0.3 -ampere tube requires approximately the same amount of power, the 25 -volt shunted heater with its shunt consumes 7.5 watts, and the line dropping resistor consumes 8.7 watts, a total of 35.2 watts. This is slightly more than the consumption of the circuit of Fig. 1-9(D), but it is much less than that required by circuit 1-9(C). As to the relative ease of installation of circuits 1-9(D) or (E), it is a matter of specific circumstances, there being little to choose in terms of power saving.

The reduction of the line voltage-dropping resistor $R$, in Fig. $1-9(\mathrm{E})$ is significant. It means a smaller unit and one with lower power dissipation rating, making it more convenient to install than larger units.

A simplification of the shunted heaters is shown in Fig. 1-9(F). Instead of individual current shunts, a single shunt $K_{i}$ of suitable value (equal to the combined resistance of the shunted heaters) is connected across the 150 -ma heaters, $H_{1}$ to $H_{5}$. As indicated in the diagram, this resistance amounts to 502 ohms, which is the aggregate of four heaters of 84 ohms each, and one heater of 166 ohms. The $300-\mathrm{ma}$ heater $H_{6}$ requires no shunt, therefore, it is not included by the common shunt $R_{t}$.

The use of a common shunt across several tube heaters is not generally applicable to television receivers without taking special precautions. The reason for this is that it is common practice in series-wired television
receivers to isolate one heater from the other by means of isolating chokes [see Fig. 1-9(G)]. These are part of the filament circuit, but their d-c resistance is extremely low. Any attempt to shunt current around these heaters must exclude the choke from the shunted circuit otherwise the effectiveness of the choke will be materially reduced, if not completely nullified. This means that the current shunts shown in dotted lines in Fig. 1-9(G) are undesirable, instead, each tube should be shunted separately and care must be exercised to see that the shunt is connected directly across the terminals of the related heater and does not include the associated choke.

## Series-Parallel Circuits

Having described the parallel and the series systems separately, the organization of the series-parallel system should pose no problem. It is doultful that the occasion will arise which requires the design of a complete new heater system, usually, the substitution involves one or two tubes at the most and these can be treated as illustrated in Figs. 1-9 (B) through (G). An example of a series-parallel combination somewhat more complex than the usual is illustrated in Fig. 1-10. To simplify the treatment of this circuit, we will divide the heaters into two strings, and examine each separately.

In string 1, heaters $H_{1}$ and $H_{s}$ require heater current equal to the total line current entering the string. Heaters $H_{2}$ through $H_{3}$, are alike in their requirements for they draw the same current and voltage, however, the total current drawn by these heaters is less than $I_{1}$ because of the presence of the current shunt $R_{1}$. Furthermore, we note a number of voltage drops in string 1 indicated by the letter $E$ with subscripts. Voltage drop $E_{1}$ appears across the extreme limits of the string and is equal to $E$, the line voltage. The presence of the line dropping resistor $R$ in series with the heaters in string 1 indicates that the total voltage drop in the system $E_{1 I}$ is less than the applied voltage. The latter is equal to the sum of $E_{11}$ and $E_{12}$. In turn $E_{11}$ is composed of the sum of the voltage drops $E_{a}, E_{b}$ and $E_{c}$.

Suppose, for the moment, that heater $H_{1}$ is rated at 25 volts and 0.8 ampere, heater $H_{8}$ is rated at 12.6 volts and 0.8 ampere, and heaters $H_{2}$ through $H_{z}$ are rated at 12.6 volts and 0.15 ampere. This idenitifies $E_{b}$
as being 37.8 volts, and $E_{11}$, therefore, amounts to $25+12.6+37.8$ or 75.4 volts. The line dropping resistor $R$, therefore, disposes of 41.6 volts at 0.8 ampere. The series-parallel arrangement of heaters $H_{2}$ through $H_{i}$, without the shunt $R_{1}$ requires only 0.3 ampere, however, the line current is 0.8 ampere. Therefore, shunt $R_{1}$ must bypass 0.5 ampere. Its value can be determined by $R=E / I$, where $E$ is the voltage across the shunt, in this case $E_{b}(37.8$ volts), and $I$ is the current to be shunted through the resistor ( 0.5 ampere). $R_{t}$, therefore, is equal to 75.6 ohms.


Fig. 1-10. In a series-parallel arrangement of tube heaters such as shown here, each string should be considered separately to find the requirements of each heater.

The distribution of voltages and currents in string 2 requires no special comment. What has been said so far will make the organization of this string easy to follow with the possible exception of the shunting of heater $H_{13}$ across the series pair $H_{11}$ and $H_{12}$. This is made possible by virtue of the relative voltage ratings of these three heaters; heaters $H_{11}$ and $H_{18}$ are rated at one-half of that of $H_{13}$, or the total drop across the series pair $H_{11}$ and $H_{12}$ equals the drop across $H_{13}$. The total current drawn by $H_{11}, H_{12}$, and $H_{13}$ must equal the current flowing in the line through $H_{s}$ and $H_{10}$. Further examples of such circuits will be found in Section 3.

## Dual-Heater Voltage and Current Tubes

Some tubes contain dual heaters which are connected in series and tapped at the midpoint, offering three points for connection. They bear one voltage rating when the two heaters are used in series and another voltage rating (half the previous value) when they are connected in parallel. Naturally, the parallel connection bears a current rating which is twice that
of the series rating. Circuitwise, the heaters appear as shown in Fig. 1-11, and are listed in a tube characteristic chart as follows:



Fig. 1-11. Dual heaters such as appear in dual-heater tubes have their midpoint tapped. This makes it possible to connect the heaters either in series or in parallel with each other.

The use of such tubes in a system affords a more convenient means of substitution than the use of single rated heaters for, by simply arranging the heaters in parallel, they can be made to serve in circuits which require the lower of the two voltages and the higher of the two current ratings. By using the tube with series-connected heaters, it will suit the needs of circuits which require the higher voltage rating and the lower current rating.


Fig. 1-12. A defective heater in a dual-heater tube may be replaced by an external resistor equal in resistance to the defective element.

Each of these dual heaters is a resistance and, when the heaters are used in parallel, the resultant resistance is half that of either. When they are used in series, the total resistance is equal to twice that of either. In the event of failure of either heater, the remaining heater is capable of causing sufficient electron emission from the cathode and the tube may be treated as if it had but one heater. If it is a matter of maintaining a certain voltage drop in a heater system, the defective heater may be replaced by an external resistance equal in value to that of the original heater. This is illustrated in Fig. 1-12. It must, of course, be understood that when this external resistance replaces the bad heater it will contribute nothing to the emission.

## Resistor Substitution

A number of factors control the substitution of resistors, these are :

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a. Type (wire or processed)
b. Ohmic value
c. Tolerance
d. Wattage rating.

Kelative to the type, wire-wound resistors should not be used in frequency-sensitive circuits unless so stated. The reason for this is the winding has inductance and distributed capacitance. If a resonant peaking circuit contains a carbon resistor in series with the peaking coil, replacing that resistor with a wire-wound unit will change the frequency of resonance, and so alter the operation of the device. Such conditions will be found in wideband amplifiers. In general, therefore, replacement resistors should be of the same type as those which were removed. Carbon resistors are preferable in all high-frequency circuits, unless otherwise indicated. In circuits which are not frequency sensitive, the replacement of a processed resistor by a wire-wound one is satisfactory, except when wire resistors appear in both grid and plate circuits of the same tube. This may result in feedback and oscillation in amplifier circuits which handle reasonable amounts of power. Resonance may be created by means of the related distributed capacitance and the inductance of the resistor.

Concerning the ohmic value, it is assumed that the correct substitution will be made with whatever tolerance is indicated in the reference information that describes the constants of the circuit where the replacement is being made. Data concerning tolerance identifications on processed resistors will be found in Section 5.

Sometimes, a single resistor must be replaced by two resistors or a shunt must be added so as to change the ohmic value of a portion of the circuit in order to satisfy the requirements of a tube substitution. The equivalence between a single resistor and other combinations which can produce the same value is shown in Fig. 1-13.

When resistances are in series, the total resistance is equal to the sum of the individual resistances, no matter how many there are [Fig. 1-13(A)]. The re-


Fig. 1-13. The use of a combination of resistors to produce the same total resistance as a single one is shown in (A), ( B ), and (C). The total resistance of each of the combinations may be found from the formula beneath it and is equal to the single resistance $R$ shown at the left.
sultant resistance of two resistances in parallel is equal to the product divided by the sum, see Fig. 1-13. The number of resistances which may be placed in parallel is limited by practical considerations. If more than two must be shunted in order to arrive at a certain resultant, the following equation should be used
$\frac{1}{R}=\frac{1}{R_{s}}+\frac{1}{R_{s}}+\frac{1}{R_{i}}+\ldots$ [see Fig. $\left.1-13(\mathrm{C})\right]$.
For the case of three parallel resistors, the resultant reduces to the fraction shown in Fig. 1-13(C).

Sometimes the situation demands that a certain resistance be shunted by another to produce a certain final value. The ohmic value of the shunt is determined as follows

$$
R_{\mathrm{shunt}}=\frac{\text { desired resistance } \times \text { original resistance }}{\text { original resistance }- \text { desired resistance. }}
$$

For example, a 100.000 -ohm load resistance must be reduced to 30,000 ohms in order to suit the new tube used. What shall be the ohmic value of the shunt required for this job? Using the equation given above

$$
\begin{aligned}
R_{\text {shunt }}= & \frac{30,000 \times 100,000}{100,000-30,000}=\frac{3,000,000,000}{70,000} \\
& =43,000 \text { ohms (approx.) }
\end{aligned}
$$

Tolerance ratings, expressed in percentage, are the amounts by which a rated resistance may differ from the actual resistance of the element. A plus tolerance means that the actual value may be higher than the rated value by some amount not exceeding the tolerance figure; a minus tolerance means that the actual value may be lower than the rated value by some amount not exceeding the tolerance. Thus, a 1-megohm resistor rated at +5 per cent means that it may be as high as $1,050,000$ ohms; if the tolerance was - 5 per cent, its value might be as low as 950,000 ohms. Combining a plus tolerance resistor with a minus one is a good way of arriving at a desired resultant when two of like value are not available. There are many resistors that have a plus and minus tolerance rating. Thus, a $1,000-\mathrm{ohm}$ resistor of $\pm 10$ per cent may be as high as 1,100 ohms, or as low as 900 ohms.

The power dissipation in a resistor carrying current may be expressed by any one of the following methods

$$
P=I^{2} R=\frac{E^{v}}{R}=E I
$$

where $I$ is the current flowing through the resistor; $R$ is its ohmic value, and $E$ is the voltage drop across the resistor. In most cases, the wattage rating of a resistor is an important factor. In certain grid circuits, however, where the current is so small as to be negligible, the resistor's power dissipation value is not important. A half-watt rating will be found suitable for all such circuits. However, in those instances when
grid current exists and is used to develop all or part of the grid lias, the wattage rating must be based upon the calculated power dissipation. In general, a maximum safety factor of 100 per cent should be allowed above the calculated value. This means that the wattage rating of the resistor chosen should be equal to twice the calculated power dissipation. Such a factor of safety is more than ample. For example, if the dissipation is 1.2 watts, use a 2 -watt resistor; if it is 3 watts, use a 5 -watt resistor ; if it is 6 watts, use a 10 -watt resistor ; and if it is 13 watts, use a 20 -watt resistor. Note that the required wattage is slightly less than double the calculated value in each case. Thus we see why a 100 -per cent factor of safety is considered a maximum.
A consideration of moment is the possible tube damage resulting when a resistor burns out. If damage can result due to an excessive rise in plate current or voltage, in the event that a resistor burns out, it is advisable to use a resistor which has a higher wattage rating than the one being replaced.
If the occasion arises to replace a resistor in one leg of a balanced circuit, for example, in the plate or grid circuit of a push-pull stage, it may be necessary to replace the resistor in the other leg also so as not to disturb the balanced condition of the circuit elements. When a replacement is made in such a case, both resistors should have not only similar ohmic values, but should be of similar construction and have similar tolerances and wattage ratings as well.

## Fixed Capacitor Substitution

The cardinal factors associated with fixed capacitors are the capacitance, $\mathrm{d}-\mathrm{c}$ working voltage, and leakage resistance. The requirements relative to capacitor values are so obvious as to require no discussion other than to mention the equivalence between several arrangements, as shown in Fig. 1-14. Two like-value capacitors in series produce a resultant which is equal to one-half the capacitance of either one. Two or more unlike capacitors in series are treated the same as resistors in parallel. Capacitors in parallel are additive.

The d-c working voltage corresponds to the peak a-c voltage which may be applied to the capacitor. Practically speaking, $\mathrm{d}-\mathrm{c}$ working voltage ratings are somewhat lower than can actually be applied to the capacitor


Fig. 14. Combinations of capacitors which give resultant capacitances equal to that of a single capacitor are shown here with the resultant capacitance of each combination listed below it.
because of the safety factor, but common sense dictates that operations should be carried on within the limits set by the rated working voltage. In view of this situation, care must be exercised against interpreting the d-c working voltage as being the equivalent of the rms or effective value of a-c voltage; if this is done, the probability exists that the peak a-c voltage in the circuit will puncture the capacitor. The correspondence between these different values of voltage is as follows

D-C Working Voltage $=$ Peak A-C Voltage $=$ $1.414 \times$ RMS Voltage.
If by error the rms voltage in a circuit equals the $d-c$ working voltage rating of the capacitors, the peak a-c voltage in those circuits (exclusive of surges) will be 1.414 times higher. If any question arises concerning the rms voltage and the d-c working voltage of a capacitor in a circuit, the rms voltage which is usable may be found from the following equation
RMS Voltage $=\mathrm{D}-\mathrm{C}$ Working Voltage $\times 0.707$.
This is an important consideration in rectifier systems and wherever both a-c and d-c voltages are involved. The input capacitors in capacitance input filter systems should have a d-c working voltage rating which is somewhat higher than the peak voltage available from the plate winding of the power transformer. This will take into account possible surges which may occur. It is well to bear in mind that repeated failure of capacitors at one point in a system is proof of an insufficient voltage safety factor in the selection of the voltage rating. This is especially true when a substituted rectifier is of the filament type, whereas tubes which receive their voltage from the rectifier are of the heater type. In such cases, high voltages will prevail in the rectifier during the time required for the load tubes to reach the conducting state.
If parallel or series capacitor combinations are used as replacement for a single capacitor, care must be taken that the d-c working voltage across each part of the combination is its rated one. For example, if two capacitors are in series the voltage across each should be inversely proportional to their capacitances and together should equal the total voltage across them. When the combination is a parallel one, the same $\mathrm{d}-\mathrm{c}$ working voltage will appear across each capacitor.
The d-c leakage in fixed capacitors is an important item in connection with substitution. For example, capacitors which are intended to isolate one point from another relative to d.c. should have low leakage, which means high insulation resistance. High leakage in coupling capacitors can very materially influence the bias on the grid of the tube connected to the resistor and adversely affect the performance of that tube. In this connection, electrolytic capacitors have the highest leakage, paper dielectric capacitors are lower, and mica or ceramic capacitors have the lowest leakage. Vacuum capacitors are, of course, ideal but their use is limited mostly to high-voltage points in transmitters and similar equipment.

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When working in high-frequency circuits, the substitution should, if at all possibie, be a duplicate of the capacitor being replaced, which in many cases will be a ceramic capacitor. If it is not available, then a mica is the next best choice.

As a means of conserving space, some ceramic capacitors are dual units, that is, the same housing includes a resistor (possibly more than one) which is associated with the operation of the device. Sometimes two such capacitors and a resistor, forming a complete load assembly, may be in one unit. These should be replaced as a unit, but in an emergency, a substitute may be used for only that part of the assembly which has failed. Note: an examination of a circuit may disclose more components than are present physically; some of these "missing" elements may be included in dual units.

## I-F Transformer Substitution .

The replacement of i-f transformers is determined by circuit location and circuit constants. The location determines whether it falls within the category of an "input," "interstage," or an "output" transformer. These identifications are found in service notes and parts catalogs. With the exception of receivers which contain only a single stage of i-f amplification, all superheterodynes make use of the aforementioned three general types of transformers. The input and interstage kinds may be interchangable but the output transformer, which feeds a diode demodulator, is of a special design. Therefore, when it is necessary to replace the i-f transformer which feeds the signal to the diode demodulator, every effort should be made to secure a replacement which has been designed to perform that function.

Substantial differences may be found in the numerous varieties of i-f transformers which are employed by receiver manufacturers. Replacement of identical units is possible only by procuring the part from facilities related to the original receiver manufacturer. However, general replacement i-f transformers are suitable substitutes if the proper precautions are exercised when the substitution is made. For example, some i-f transformers used in combination a-m-f-m receivers are of the dual-frequency variety, that is, two different transformers contained in the same can. In other cases, trimmers, or filter elements related to the stage are contained in the same can with the transformers. Examples of these two are shown in Figs. 1-15(A) and (B).

The replacement of such devices by substitutes involves consideration of all of the factors involved. Two individual i-f transformers, an a-m and a separate $\mathrm{f}-\mathrm{m}$ unit, may be connected externally to form the equivalent of the original shown in Fig. 1-15(A). However, if the original contains additional elements
such as resistors and filter capacitors, these must be added in the sulstitution. The same is true of the replacements for either a-m or $\mathrm{f}-\mathrm{m}$ transformers which contain special elements. We are referring particularly to units in which the trimmer capacitor is a combination element, part of it being used in the grid filter system of that stage. This may not become evident in a casual inspection of the device or the schematic, for the symbols representing the filter resistors and capacitors are not necessarily shown as a part of the trimmer. This calls for a careful examination of the transformer and the filter circuits. If the transformer is removed and with it all of the filter elements, then a substitution must consist of a corresponding number of units.


Fig. 1-15. (A) An i-f transformer of the dual-frequency variety found in $a-m-f-m$ receivers. The $a-m$ and $f-m$ windings of the i-f transformer are in series and are contained in the same can; in (B) is shown a unit which contains, besides the i-f transformer, the filter capacitors and trimmers used in the associated circuit.

Relative to the general requirements of i-f transformers, those designed for use with pentodes will serve with any pentode or tetrode. The specific electrical characteristics of all pentode or tetrode i-f amplifiers are not alike, but the differences in i-f transformer performance due to this variable will not be significant if all other requirements are satisfied.

The intermediate frequency is another controlling factor in the selection of a substitute i-f transformer. Several broad categories exist, those used in a-m receivers, those in f-m receivers, and those in television receivers. In each group, the bandwidth requirement is pertinent to the selection of the replacement as is the specific intermediate frequency. Reference to the service data on the receiver is essential; the intermediate frequency used in a receiver does not dis-
close the specific bandwidth conditions in the i-f transformers. In some cases, all transformers are relatively broadband, being closely coupled. In other instances, the over-all broadbanding is accomplished by staggering the i-f peaks in the individual stages.

Concerning the center frequency, i-f transformers intended for a-m receivers have been standardized to four center frequencies, $130 \mathrm{kc}, 175 \mathrm{kc}, 262 \mathrm{kc}$, and 455 kc . From this point on, different types produced by different manufacturers afford different over-all frequency coverage. These vary from a low of about 5 per cent to a high of 40 per cent of the center frequency. For example, one manufacturer may produce an i-f transformer with a center frequency of 455 kc and an over-all tuning range of 50 kc , which is the equivalent of 25 kc each side of the rated center frequency. Some other manufacturer may design his transformers so that the over-all tuning range may be 200 kc , equal to about 40 per cent of the center frequency.

As a rule, the higher the center frequency, the wider is the over-all tuning range, but all makes of i-f transformers of like center frequency do not afford like frequency coverage. In other words, the selection of a transformer demands recognition of the bandwith requirements of the stage wherein it is to be used. Attention must also be paid to the tuning range of a unit if the intermediate frequency in the receiver is not the same as the center frequency of the transformer.

Concerning dual i-f transformers (a-m and $\mathrm{f}-\mathrm{m}$ ), the generally standardized frequencies found in the i-f systems of such receivers preclude any problems other than the one we referred to earlier, that is, to be certain that all of the filter components which exist inside of the original receiver manufacturer's unit appear in the receiver after the replacement has been made.

Up to this point we have neglected the factor of space relative to $i$ - $f$ transformer substitution. It can well be a problem. If the substitution is a transformer for a transformer, that is, single band for single band, it is not too difficult even if the substitute is larger than the original (which seldom is the case). If a dual band (single can) transformer must be replaced by two individual transformers, however, we have a problem. It is possible to find i-f transformers which are smaller than the usual variety. It takes effort to select the ones needed because several factors must be taken into account, but it can be done.

## Power-Transformer Substitutions

The physical size and the electrical ratings are two dominant factors in such substitutions. The limitations caused by size are so obvious as to require no elaboration. Concerning electrical ratings, the first essential is that the transformer afford the same over-all capabili-
ties as the original, that is, its windings should be equal in number to that of the original so as to duplicate the functions of the original. This statement is subject to some slight qualifications which will appear when we discuss the filament windings, but in general, it can be said that the maximum convenience in substitution is attained if the substitute has at least as many different windings of like electrical rating as the original.

So far as physical characteristics are concerned, if the original transformer is shielded completely, the substitution unit should be likewise. If the original employs vertical shield mounting, so should the substitute; if the original has horizontal shield mounting, the replacement should duplicate it. Such attention to shielding will result in freedom from field troubles. Open-core transformers can cause trouble if located close to grid and plate wiring. If they must be used because the exact replacement is not available, the possibility of hum troubles must be recognized.

Each winding bears a voltage and a current rating with supplementary identification concerning the center tap. Although a center tap can be arranged by means of a center-tapped resistor connected across an untapped winding, it is preferable if the tap is a part of the winding. A suitable value for a resistor to be used for a center tap is 100 ohms.

Increasing Heater Voltage Rating. Although it is best if the filament windings on the transformer are the same in number and rating as the original, it is very possible that such replacements will not be available. In that event, the following information will be useful. Filament windings when connected in series furnishes a resultant voltage which is the sum of the voltage ratings of the individual windings. A 2.5 -volt winding in series with another of 5.0 volts will be the equivalent of a voltage source rated at 7.5 volts. Care must be exercised to see that the two windings are connected with the windings aiding each other. An a-c voltmeter connected across the combined windings will indicate if they are aiding or bucking. The current rating of a series winding of this kind is limited to the lower of the two ratings of the individual windings.

For example, if two 6.3 -volt windings, each rated at 1.2 amperes are connected in series aiding, the voltage rating of the two windings is 12.6 volts at 1.2 amperes. If one of these is rated at 0.9 ampere and the other at 1.5 amperes, the current output of the series winding would be limited to 0.9 ampere.

Increasing Heater Current Rating. Windings may be connected in parallel so as to increase the current output rating, provided that each of the windings connected in parallel is rated at the same value of voltage. The current ratings need not be the same; the total current output will be the sum of the two individual current ratings. Care must be exercised to see that the two windings are connected in proper phase, otherwise they will buck each other. An a-c voltmeter connected across one winding while the other is being connected

## RECEIVING TUBE SUBSTITUTION GUIDE

in parallel will show whether the phase is correct. If the voltage is reduced, they are bucking.

Relative to the center-tap connection, if two like voltage windings are connected in series, the junction between them can serve as the center tap; individual center taps on the two windings being disregarded. If two unlike voltage windings are connected in series, the midpoint of a 100 -ohm resistor, shunted across the combined windings, can be used as the center tap.

If two winclings are connected in parallel and each of them has a center tap, the two center taps may be connected together to serve as the combined center-tap connection. If only one of two windings in parallel has a center tap, it cannot be used as the center tap to serve both windings, a 100 -ohm center-tapped resistor should be connected across the untapped winding and its midpoint joined to the other center tap, at which point the common connection can be made.

Substitute Heater Windings. If the replacement transformer does not contain all the required heater windings, a supplementary filament transformer, capable of furnishing the required voltage and current, can be used apart from the regular power transformer. Its primary should be connected in parallel with the other transformer.

Half-wave rectifier heater windings do not require center taps. Either end of the winding will serve as the positive output lead with a filament-type tube. Full-wave rectifiers should employ center-tapped heater windings even if the rectifiers are of the cathode type.

## Heater-Winding Insulation

As a rule, the voltage breakdown requirements of most heater windings which are a part of the power transformer can be satisfied by a rating of about 2,000 volts since the highest voltage in the system is far less than this amount. In cathode-ray equipment and other systems, it is possible that the cathode may be as much as 4,000 volts above ground and, since it is connected to the center tap of the heater winding, the latter is also above ground by the corresponding amount. This demands that the heater voltage winding be so insulated as to withstand this difference of potential. Sometimes (although very seldom), this requirement may be stated in the specifications. If it is not, it becomes the province of the technician to decide the voltage breakdown requirements of the heater winding.

## Rectifier Plate Windings

The conditions surrounding the selection of a substitute power transformer relative to the plate winding are varied, so much so, that it becomes necessary to examine several approaches to the subject. To begin with, the constants of a power transformer utilized in a receiver (or some other kind of equipment) may not
be fully identified in service literature; a part number always is given, and sometimes, the current and voltage ratings of the heater windings are stated on the manufacturer's schematic. If this data is not given, the number required and the current rating of each become evident when reference is made to the schematic wiring diagram of the equipment in which the substitution is to be made. It discloses the number of heater or filament chains, and the voltage and current requirements of each. Summation of these indicates the minimum current ratings of the heater windings. The constants of the plate winding, however, are generally omitted. This means that some way must be found to ascertain the requirements of the plate winding so a proper substitute can be found in the event that an exact replacement from the original equipment manufacturer is not available.

The type of rectifiers and their ratings indicates the maximum voltage and current requirements of the plate winding. Seldom, if ever, are these tubes operated very close to their maximum ratings. Therefore, by noting the limits indicated in the tube characteristic chart, and the practical voltages being applied to the tubes in the system under consideration, it is possible to arrive at the voltage and current ratings of the plate winding. Whether it should be a full-wave winding, that is, center tapped, or a half-wave winding is indicated in the schematic of the equipment and by the organization of the rectifier system as a whole. But it is conceivable that there still may arise problems in establishing the voltage rating of the plate winding in view of the conditions experienced in choke- and capacitor-input filter systems, and because of the manner in which the parts catalogs describe the capabilities of the plate windings of power transformers. Generalizing, we can state that when the input of the power-supply filter system is capacitive, the voltage rating of each half of the power-supply plate winding in a full-wave system can be as much as 10 to 15 per cent lower than the d-c voltage output of the rectifier at the prescribed value of d-c load. This stems from the fact that the input filter capacitance can be charged to approximately the peak value of the a-c voltage applied to the rectifier tubes. Some parts catalogs state the voltage and current ratings based on full-wave operation of the rectifier with capacitance input, whereas many others show the a-c voltage across each half of the plate winding at certain d-c values in terms of choke input. This is a cause of confusion; in one case, the a-c voltage between the center tap and the extremes of the plate winding is less than the d-c voltage output from the rectifier by as much as 8 to 10 per cent, whereas in the other case, the a-c voltage rating of the plate winding may be as much as 10 to 15 per cent higher than the $d-c$ voltage output from the rectifier.

What can be used as a guide in determining the basic requirements of the plate winding? The original
schematic of the equipment should be the first source of information, especially when it is supplemented by a voltage chart which indicates the voltages being supplied by the power supply. If the plate-current requirements of the tubes are not shown in the voltage chart, a reasonable approximation of these current values can be developed from the tube characteristic charts contained herein. Then, allowing for a 10 per cent voltage drop in the filter system of the power supply and perhaps a loss of about 5 per cent of the total output current through the bleeder connected across the power supply, one can arrive at the total current load requirements of the system and the maximum a-c voltage required between the center tap and the extremes of the full-wave plate winding.

These data are naturally subject to variations, but the approach we have described is not too far off the path which must be followed. At least it suggests a way to gather the necessary information.

It may appear, because of the large number of commercial models, that receivers and amplifiers are distinctive in their general requirements. Such is not the case, for all fall into certain groupings and reflect certain general design considerations. It would be foolish to deny that such circuits as shown in Rider Manuals can serve as the guide for substitution requirements. So far as tube heater and signal electrode voltages and currents are concerned, there isn't much difference between the five- or six-tube table models produced by different manufacturers. Individuality appears in the number of tubes, the specific designs of the transformers, the combination of functions and the like, but these play very little part in establishing the requirements of a power supply.

## Cathode-Ray-Tube Substitutions

Cathode-ray-tube substitutions are more involved than ordinary receiving tube substitutions, if for no other reason than that the physical dimensions of the various cathode-ray tubes differ, and the replacement of one by another may require substantial physical changes in the cabinet. Nevertheless, substitutions are possible and the following are offered as suggestions. They are to be used in conjunction with the cathode-ray-tube specifications contained in this Guide Book.

1. All picture tube phosphors must be number 4. This is the last digit in the tube type number.
2. Wholly electrostatically operated picture tubes must be replaced with similar tubes. Since these are restricted in screen size, replacement for 7 - and 10 -inch electrostatically deflected and focused picture tubes are very limited.
3. Tubes which employ magnetic deflection and electrostatic focusing have no substitutes among either completely electrostatic or magnetic types. The reverse is, of course, also true, a combination magnetic-deflec-

FOCUS COIL CURRENT RATINGS FOR MAGNETIC
TYPE CATHODE-RAY TUBES

| $\mathbf{C - R}$ <br> Tube | Focus Coil Current (Ma) | C-R <br> Tube | Focus Coil Current (Ma) | $\mathbf{C - R}$ <br> Tube | Focus Coil Current (Ma) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10BP4 ${ }^{\text {d }}$ | 132 | 14CP4 | 115* | 16MP4 | 110 |
| 10BP4A |  | 14DP4 | 104 | 16MP4A |  |
| 10CP4 | --- | 14FP4 | 115* | 16QP4 | 125* |
| 10DP4 | --- | 15AP4 | 159 | 16RP4 | 100* |
| 10EP4 | 132 | 15CP4 | 133 | 16 SP 4 | 110 |
| 10FP4 | 115 | 15DP4 | 140 | $16 S P 4$ A |  |
| 10MP4 | ] --- | 16 AP4 | 89 | 16 TP 4 | 115* |
| $10 \mathrm{MP4}$ A |  | 16AP4A |  | 16 UP4 | 100* |
| $12 \mathrm{JP4}$ | 158 | 16 CP 4 | 110 | 16 VP 4 | 110* |
| $12 \mathrm{KP4}$ 4 | ) 140 | $16 \mathrm{DP4}$ | 115* | 16 WP 4 | 110* |
| 12 KP 4 A ) |  | 16DP4A |  | 16XP4 | 100* |
| 12LP4 | 114 | 16 EP 4 | 105 | 16 YP 4 | 100* |
| 12LP4A |  | $16 \mathrm{EP4A}$ |  | $17 \mathrm{AP4}$ | 115* |
| 12QP4 | 148 | 16 FP 4 | 140 | 19AP4 | 140 |
| 12QP4A |  | 16GP4 | 100* | 19AP4A |  |
| $12 \mathrm{RP4}$ | 148 | $16 \mathrm{HP4}$ | 110 | 19DP4 | ) 140 |
| 12 TP 4 | 114 | 16 HP 4 |  | 19DP4A |  |
| 12UP4 | ) 114 | 16 JP 4 | 120 | 19EP4 | 140* |
| 12 UP 4 A \} |  | 16 JP 4 A |  | 19FP4 | 97-126* |
| 12VP4 $\}$ | , | 16 KP 4 | 97* | 19GP4 | 107-126* |
| $12 \mathrm{VP4} 4$ |  | 16LP4 | 110 | 20BP4 | 122 |
| $14 \mathrm{BP4}$ | 115 | 16LP4A |  | 22AP4 | \} 108* |

* Types employ RTMA Focus Coil 109 , all others RTMA focus focus coil $\$ 106$.


## Courtesy DuMont Labs

tion and electrostatic-focusing type tube cannot be a replacement for either an electrostatically or magnetically deflected and focused picture tube. Since the $7 \mathrm{DP} 4,9 \mathrm{AP} 4,10 \mathrm{DP} 4$, and 12 AP 4 are tubes of this type, they have no replacements except each other.
4. Picture tubes differ in the focusing coil currents, consequently, in some instances the focusing coil for the substitute tube may require more current than for the original. This necessitates modification of the focusing current supply system. Conversely, some substitute tubes may require less current through the focusing coil than the original, in which case a resistor shunted across the coil will serve the purpose. This current shunt can be calculated using the $d-c$ resistance of the focusing coil and the value of the current, just as in the case of heater current shunts. A variable resistance, $2,500-15,000$ ohms, shunted across the coil can be used to determine the value for the fixed resistance shunt. The accompanying table lists the focusingcoil currents for the different magnetic-type cathoderay tubes.
5. Replacing outside coated tubes with metal-cone types (or the reverse) requires care concerning the connection to the coating or the metal cone. The coating usually is connected to ground, whereas the metal cone usually is connected to a high voltage. The original receiver manufacturer's service notes must be consulted.
6. When a large tube is replaced by a smaller one, the characteristics of the substitute should be determined by reference to the characteristic chart; if the

## RECEIVING TUBE SUBSTITUTION GUIDE

conditions in the receiver exceed the maximum voltage ratings of the tube, these must be reduced in order to employ the substitute. Usually, those operations are too complicated for the average technician; such substitutions are not recommended.
7. All picture tubes do not utilize like tube basing. See the cathode-ray-tube basing chart in Section 5.
8. Bear in mind that the ion-trap magnets in magnetically focussed picture tubes are not all alike, some call for a single magnet, others for dual magnets; check the cathode-ray-tube characteristics in Section 5.
9. If tube characteristics indicate that the original tube has an external coating furnishing a certain
amount of capacitance and the substitute tube does not, a corresponding value of capacitance should be added to the high-voltage power supply at the high-voltage output terminal. This capacitor must have the appropriate $\mathrm{d}-\mathrm{c}$ working voltage rating.
10. If the ion-trap magnet for the original tube is of the electromagnetic type (coil) and the substitute utilizes a permanent magnet, the coil unit may be left intact (placed in a recess of the cabinet), or it may be replaced ly an equivalent resistance of suitable wattage rating located as closely as possible to the power supply. It should not be disconnected without substituting the equivalent resistance into the current supply circuit.

FUNCTIONAL CLASSIFICATION OF TUBES

| APPLICATION |  | HEATER VOLTAGES |  |  |  |  |  |  |  |  | 150 MILLIAMPERE HEATER CURRENT |  | 300 MILLIAMPERE HEATER CURRENT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.4 | 2.0 | 2.5 | 6.3 |  |  |  | 12.6 |  |  |  |  |  |
|  | TRIODES | $\begin{aligned} & 26 \\ & 957^{*} \\ & 958^{*} \end{aligned}$ | $\begin{aligned} & 1 \mathrm{H} 4 \mathrm{G} \\ & 30 \end{aligned}$ | $\begin{aligned} & 27 \\ & 56 \\ & 485 \dagger \dagger \end{aligned}$ | $\begin{aligned} & \text { 6AD4 } \\ & \text { 6C4 } \\ & \text { 6J4 } \\ & \text { 6K4 } \\ & \text { 6N4 } \end{aligned}$ | 7A4 <br> 37 <br> 76 <br> 955 <br> 9002 | XXL |  | 14A4 |  | $\begin{aligned} & \text { 6AD4 } \\ & \text { 6C4 } \\ & 955 \\ & 9002 \end{aligned}$ |  | $\begin{aligned} & \hline 7 \mathrm{A4} \\ & 37 \\ & 76 \end{aligned}$ |  |
|  | DOUBLE TRIODES | 3B7/1291 |  | 3B7/12914 | $\begin{aligned} & \text { 6AH7GT } \\ & \text { 6J6 } \\ & \text { 7AF7 } \\ & \text { 7F7 } \end{aligned}$ | 7F8 |  |  | $\begin{aligned} & \text { 12AH7GT } \\ & \text { 12AT7 } \\ & \text { 14AF7/XXD } \\ & \text { 14F7 } \end{aligned}$ | $\text { 19J6 } 6$ | $\begin{aligned} & \text { 12AH7GT } \\ & \text { 12AT7 } \\ & \text { 14AF7/XXD } \\ & \text { 14F7 } \end{aligned}$ | $19 J 6$ | $\begin{aligned} & \text { 6AH7GT } \\ & \text { 7AF7 } \\ & \text { 7F7 } \\ & \text { 7F8 } \end{aligned}$ | 12AT7 |
| $\underset{8}{4}$ | TETRODES |  | 1A4T 1DSGT 1ESGT 32 | $\begin{aligned} & 24 \\ & 35 \end{aligned}$ | 36 |  |  |  |  |  |  |  | 36 |  |
|  | PENTODES | 1AB5** <br> AAD4 <br> 1AD5 <br> 1L4 <br> 2LC5 <br> 1LN5 <br> 1NSGT <br> 1P5G <br> 1P5GT <br> 1SA6GT <br> 1 T4 <br> 1 U4 <br> 1W5* <br> 3E6 <br> 959* | 1A4P 1B4P 1DSGP 1ESGP 15 34 | $\begin{aligned} & \hline \text { 3E6\% } \\ & 57 \\ & 58 \end{aligned}$ | 6AG5 <br> 6AH6 <br> 6AK5 <br> 6AU6 <br> 6BA5 <br> 6BA6 <br> 6BC5 <br> 6BD6 <br> 6BH6 <br> 6BJ6 <br> 6C6 <br> 6CB6 <br> 6D6 <br> 6E7 <br> 6J7 <br> 6J7G <br> 6J7GT | 6K7 <br> 6K7G <br> 6K7GT <br> $6 \mathbf{6} 7$ <br> 6S7G <br> 6SD7GT <br> 6SG7 <br> 6SG7GT <br> 6SH7 <br> 6SH7GT <br> 6SJ7 <br> 6SJ7GT <br> 6SK7 <br> 6SK7GT <br> 6SS7 <br> 6S57GT | 6U7G <br> 6W7G <br> 7A7 <br> 7AB7 <br> 7AD7 <br> 7AG7 <br> 7AJ7 <br> 7B7 <br> 7C7 <br> 7G7 <br> 7H7 <br> 7L7 <br> 7V7 <br> 39/44 <br> 77 <br> 78 | 954 956 9001 9003 | 12AU6 <br> 12AW6 <br> 12BA6 <br> 12BD6 <br> 12B7 <br> 12J7GT <br> 12K7GT <br> 12SG7 <br> 12SH7 <br> 12SH7GT <br> 12SJ7 <br> 12SJ7GT <br> 12SK7 <br> 12SK7GT <br> 14A7/12B7 <br> $14 \mathrm{C7}$ | 14H7 | 6BA5 <br> 6BH6 <br> 6BJ6 <br> 657 <br> 6S7G <br> 6SS7 <br> 6SS7GT <br> 6W7G <br> 7AB7 <br> 7B7 <br> 7C7 <br> 12AU6 <br> 12AW6 <br> $12 \mathrm{B7}$ <br> 12BA6 <br> 12BD6 <br> 12J7GT <br> 12K7GT | 12SG7 <br> 12 SH 7 <br> 12SH7GT <br> 12SJ7 <br> 12SJ7GT <br> 12SK7 <br> 12SK7GT <br> 14A7/12B7 <br> 14C7 <br> 14H7 <br> 954 <br> 956 <br> 9001 <br> 9003 | 6AU6 <br> 6BA6 <br> 6BD6 <br> 6C6 <br> 6D6 <br> 6E7 <br> 6 J 7 <br> 6J7G <br> 6J7GT <br> 6K7 <br> 6K7G <br> 6K7GT <br> 6SD7GT <br> 6SG7 <br> 6SG7GT <br> 6SH7 | 6SH7GT <br> 6SJ7 <br> 6SJ7GT <br> 6SK7 <br> 6SK7GT <br> 6U7G <br> 7A7 <br> 7AG7 <br> 7AJ7 <br> 7H7 <br> 7 L 7 <br> 39/44 <br> 77 <br> 78 |
| ? | TRIODES |  |  |  | 6AB4 |  |  |  |  |  | 6AB4 |  |  |  |
|  | DOUBLE TRIODES |  |  |  | 6 J 6 | 12AT7 |  |  | 12AT7 | 19J6\% | 12AT7 | 19 J 6 | 12AT7 |  |
| $\underset{i}{\text { min }}$ | PENTODES |  |  |  | 6AB7 6AC7 6AGS | 6AK5 6AU6 6BC5 | $\begin{aligned} & \text { 6BH6 } \\ & \text { 6CB6 } \end{aligned}$ |  | 12AU6 |  | $\begin{aligned} & \text { 6BH6 } \\ & \text { 12AU6 } \end{aligned}$ |  | 6AG5 <br> 6AU6 <br> 6BC5 <br> 6CB6 |  |
| $1.25 \mathrm{~V}$ |  |  | 1.2 V . | tt 3.0 V |  | - 2.8 V |  | ** 18.9 V |  |  |  |  |  |  |

FUNCTIONAL CLASSIFICATION OF TUBES

| APPLICATION |  | HEATER VOLTAGES |  |  |  |  |  |  |  | 150 MILLIAMPERE HEATER CURRENT | 300 MILLIAMPERE HEATER CURRENT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.4 | 2.0 | 2.5 | 5.0 | 6.3 |  |  | 12.6 |  |  |  |  |
|  | TRIODES | $\begin{array}{\|l} \hline \text { 1C3 } \\ \text { 1E4G } \\ \text { 1G4GT } \\ \text { ILE3 } \\ 26 \end{array}$ | $\begin{aligned} & \hline 1 \mathrm{H} 4 \mathrm{G} \\ & 30 \end{aligned}$ | $\begin{aligned} & 27 \\ & 56 \\ & 485 t \dagger \end{aligned}$ | 01 A | 6AESGT <br> 6AD5G <br> 6AFSG <br> 6C5 <br> 6C5GT <br> 6F5 <br> 6F5G <br> 6FSGT | 6 J 5 <br> 6J5GT <br> 6KSG <br> 6K5GT <br> 6LSG <br> 6P5GT <br> 6SF5 <br> 6SF5GT | $\begin{aligned} & \hline 7 \mathrm{A4} \\ & 7 \mathrm{B4} \\ & 37 \\ & 56 \\ & 75 S \\ & 76 \end{aligned}$ | $\begin{aligned} & \hline \text { 12ESGT } \\ & \text { 12F5GT } \\ & \text { 12JSGT } \\ & \text { 12SF5 } \\ & \text { 12SFSGT } \\ & \text { 14A4 } \end{aligned}$ | $\begin{aligned} & \text { 6LSG } \\ & \text { 12ESGT } \\ & \text { 12F5GT } \\ & \text { 12J5GT } \\ & \text { 12SF5 } \\ & \text { 12SF5GT } \\ & \text { 14A4 } \end{aligned}$ | 6AESGT <br> 6AF5G <br> 6ADSG <br> 6 CS <br> 6C3GT <br> 6F5 <br> 6F5G | 6FSGT <br> $6 J 5$ <br> 6J5GT <br> 6K5G <br> 6K5tT <br> 6PSGT <br> 6 SF5 | $\begin{aligned} & \hline \text { 6SF5GT } \\ & \text { 7A4 } \\ & \text { 7B4 } \\ & 37 \\ & \text { 56 } \\ & 75 S \\ & 76 \end{aligned}$ |
|  | DOUBLE TRIODES |  |  | 53 |  | 6A6 <br> 6AE7GT <br> 6C8G <br> 6F8G <br> 6N7 <br> 6N7G <br> 6SC7 <br> 6SC7GT | 6SL7GT 6SN7GT <br> 6Y7G <br> 6Z7G <br> 7AF7 <br> 7F7 <br> 12AU7 <br> 12AX7 <br> 12AY7 <br> 79 |  |   <br> 12AU7 14F7 <br> 12AX7  <br> 12AY7  <br> 12SC7  <br> 12SL7GT  <br> 12SN7GT  <br> 14AF7  <br>   | $\begin{aligned} & \text { 12AU7 } \\ & \text { 12AX7 } \\ & \text { 12AY7 } \\ & \text { 12SC7 } \\ & \text { 12SL7GT } \\ & \text { 14AF7 } \\ & \text { 14F7 } \end{aligned}$ | $\begin{aligned} & \hline \text { 6C8G } \\ & \text { 6SC7 } \\ & \text { 6SL7GT } \\ & 627 \mathrm{G} \\ & 7 \mathrm{Fy} \\ & 12 \mathrm{AU7} \\ & 12 \mathrm{AX7} \end{aligned}$ | $\begin{aligned} & \text { 12AY7 } \\ & \text { 12SN7GT } \end{aligned}$ |  |
|  | TETRODES |  | 32 | 24 |  | 36 |  |  |  |  | 36 |  |  |
|  | PENTODES | $\begin{aligned} & \text { 1L4 } \\ & \text { 1LG5 } \\ & \text { 1U4 } \\ & 959 \end{aligned}$ | $\begin{aligned} & \text { 1B4P } \\ & \text { 1ESGP } \end{aligned}$ $15$ | 57 |  | 6AU6 <br> 6BA5 <br> 6BH6 <br> 6C6 <br> $6 \mathrm{J7}$ <br> 6J7G <br> 6J7GT <br> 6R6G <br> 6SG7 <br> 6SG7GT | 6SH7 <br> 6SH7GT <br> 6SJ7 <br> 6SJ7GT <br> 6W6GT <br> 6W7G <br> 7AB7 <br> 7AG7 <br> 7AH7 <br> $7 C 7$ | 7E5 <br> 7G7 <br> $7 \mathrm{L7}$ <br> 7T7 <br> 7V7 <br> 7W7 <br> 77 <br> 717A <br> 954 <br> 956 <br> 9001 <br> 9003 | $\begin{aligned} & \text { 12AU6 } \\ & \text { 12J7GT } \\ & \text { 12SH7 } \\ & \text { 12SH7GT } \\ & \text { 12SJ7 } \\ & \text { 12SJ7GT } \\ & 14 \mathrm{C7} \\ & 14 \mathrm{V7} \end{aligned}$ |   <br> 6BH6 12SJ7GT <br> 6W7G $14 C 7$ <br> 7AG7 954 <br> 7AH7 956 <br> 7C7 9001 <br> 7ES 9003 <br> 12AU6  <br> 12J7GT  <br> 12SH7  <br> 12SH7GT  <br> 12SJ7  | 6AU6 <br> 6C6 <br> 6J7 <br> 6J7G <br> 6J7GT <br> 6R6G <br> 6SG7 <br> 6SG7GT <br> 6SH7 <br> 6SH7GT <br> 6517 <br> 6SJ7GT | $\begin{aligned} & \text { 7L7 } \\ & \text { 7T7 } \\ & 7 W 7 \\ & 77 \end{aligned}$ |  |
| 4 0 8 3 2 2 | TUNING INDICATORS |  |  | $\begin{aligned} & \text { 2ES } \\ & 2 G 5 \end{aligned}$ |  | 6AB5/6N5 <br> 6ADGG <br> 6AF6G <br> 6AL7GT <br> 6E5 <br> 6G5 <br> 6T5 <br> 6U5/6G5 |  |  |  | 6AL7GT | $\begin{aligned} & \text { 6ES } \\ & \text { 6G5 } \\ & \text { 6TS } \\ & \text { 6U5/6G5 } \end{aligned}$ |  |  |
|  | INDICATOR CONTROL |  |  |  |  | 6AE6G |  |  |  | 6AEGG |  |  |  |
| $\dagger \dagger 3.0 \mathrm{~V} . \quad \bullet 1.25 \mathrm{~V}$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

receiving tube substitution guide

FUNCTIONAL CLASSIFICATION OF TUBES

| APPLICATION |  |  | HEATER VOLTAGES |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 150 \text { MILLI- } \\ & \text { AMPPRE } \\ & \text { HEATER } \\ & \text { CCRRENT } \end{aligned}$ | $\begin{aligned} & \text { 300 MILLI- } \\ & \text { AMPERE } \\ & \text { HEATER } \\ & \text { CURENT } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1.4 | 2.0 | 2.5 | 5.0 | 6.3 | 12.6 | 18.9 | 25 | 35 | 50 |  |  |
|  |  | TRIODES |  | $\begin{array}{\|l\|l} \hline \begin{array}{l} 1 H 4 G \\ 30 \\ 31 \end{array} \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 2 \mathrm{AB} \\ \hline 45 \end{array}$ | $\begin{array}{\|c\|} \hline 01 \mathrm{~A} \\ 12 \mathrm{~A} \\ 71 \mathrm{~A} \\ 183 \\ \hline \end{array}$ | 6A3 $\quad 50 \dagger$ <br> $6 A 5 G$ <br> 6AC5GT <br> 6A4G <br> 6C4 |  |  | 25ACSGT |  |  |  | 25AC5GT |
|  |  | DOUBLE TRIODES | $\begin{array}{\|l\|} \hline 1 \mathrm{G} 6 \mathrm{GT} \\ 3 \mathrm{C} 6 / \mathrm{XXB} \end{array}$ | ${ }_{19}^{176 G}$ |  |  | 6A6 6Y7G <br> 6ASTG 627G <br> 6E6 79 <br> 6N7  <br> 6N7GT  |  |  |  |  |  |  | 627G |
|  |  | TETRODES |  | 49 | 46 |  | 6AL6G |  |  |  |  |  |  |  |
|  |  | PENTODES |  | $\begin{aligned} & 1 F 4 \\ & 1 F 5 \\ & 1 F 5 G \\ & 1 G 5 G \\ & 115 G \\ & 33 G \\ & 950 \end{aligned}$ | $\begin{aligned} & 2 \text { 2AS } \\ & 3 A 4 \# \\ & 3 C 5 G T * \\ & 3 L E 4 * \\ & 304 \\ & 3 S 4 \\ & 3 V 4 \\ & 47 \\ & 59 \end{aligned}$ | 257 | 6A4/LA 6RGG <br> 6AG7 $7 B 5$ <br> 6AK6 38 <br> 6ANS 41 <br> 6AR5 42 <br> $6 F 6$ 89 <br> $6 F 6 \mathrm{G}$ 89 <br> 6 FGGT  <br> 6 GKG  <br> 6KGT  | 12A5 |  | $\begin{aligned} & 25 A 6 \\ & 25 A 6 G T \\ & 25 B 6 G \\ & 43 \end{aligned}$ |  |  | $\begin{aligned} & \hline \text { 6AK6 } \\ & \text { 6G6G } \end{aligned}$ | $\begin{aligned} & 6 A 4 / \mathrm{LA} \\ & 12 \mathrm{AS} \\ & 25 A 6 \\ & 25 A 6 \mathrm{GT} \\ & 25 B 6 \mathrm{G} \\ & 38 \\ & 43 \end{aligned}$ |
|  |  | BEAM PENTODES | $\begin{array}{\|l\|l} \hline 105 G \\ 105 G T \\ 175 G T \\ 3 B 5 G T \\ 33 F 4 \\ 3 L 5 S G T \end{array}$ |  | $\begin{array}{\|l\|l\|} \hline \text { 3BGGT* } \\ \text { 3LF4F } \\ \text { 3QSGT } \end{array}$ |  |  | $12 A 6$ 12 AGT 14 AKT 14 CS 1625 |  | $\begin{array}{\|l} \hline 25 \mathrm{C} 6 \mathrm{G} \\ 25 \mathrm{~L} 6 \\ \text { 25L6GT } \end{array}$ | 35L6GT 35A5 3585 35 C 5 | 50AS 50 BS 50 C 50 COG 50 L 6 GT |  | $\begin{aligned} & \text { 25CGG } \\ & \text { 25L6 } \\ & 25 L 6 G T \end{aligned}$ |
|  |  | DOUBLE PENTODES |  | 1E7G |  |  |  | 12L8GT |  |  |  |  | 12L8GT |  |
|  |  | DIRECT COUPLED |  |  |  |  | $\begin{array}{\|l\|l\|} \hline \text { 6AB6G } & \text { 6BS } \\ \hline \end{array}$ |  |  | $\begin{array}{\|l\|} \hline \text { 25BS } \\ \text { 25N6GT } \end{array}$ |  |  |  | ${ }^{2585}$ |
|  |  | beam pentodes |  |  |  |  | 6AUSGT 6BGGGT 6AVSGT 6CD6G 6BG6G |  | 19BG6G | 25BQ6GT |  |  |  | 19BG6G 25BQ6GT |
|  |  | $\begin{aligned} & \text { TRIODES OR } \\ & \text { TRIDE CONECTED } \\ & \text { PENTODES } \end{aligned}$ |  |  |  |  | 6ARS 6K6GT $6 S 4$ GSNGT 6W6GT 12AUT | $\begin{array}{\|l\|} \hline 12 A U 77 \\ 12 S N 7 G T \\ \hline \end{array}$ |  |  |  |  | 12AU7 | $\begin{aligned} & 12 \mathrm{AUV} 7 \\ & 12 \mathrm{SN} / \mathrm{GT} \end{aligned}$ |
| - 1.25 V |  |  | \% $2.8 \mathrm{~V} . \quad \dagger 7.5 \mathrm{~V}$. |  |  |  |  |  |  |  |  |  |  |  |

Courtesy TUNG-SOL Lamp Works, Inc.

FUNCTIONAL CLASSIFICATION OF TUBES

| APPLICATION |  | HEATER VOLTAGES |  |  |  |  |  |  |  |  |  | 150 MILLIAMPERE HEATER CURRENT | 300 MILLIAMPERE HEATER CURRENT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.4 | 2.0 | 2.5 |  | 6.3 | 12.6 | 25 | 35 | 70 | 117 |  |  |
|  | GATED BEAM |  |  |  | 6BN6 |  | 12BN6 |  |  |  |  | 12BN6 | 6BN6 |
|  | DIODE TRIODES | 1H5G 1H5GT 1L.H4 |  |  | 6Q6G |  |  |  |  |  |  | 606G |  |
|  | DOUBLE-DIODE TRIODES |  | $\begin{aligned} & 1 \mathrm{~B} 5 / 25 S \\ & 1 \mathrm{H} 6 \mathrm{G} \end{aligned}$ | $\begin{aligned} & \text { 2A6 } \\ & 55 \end{aligned}$ | 6AQ6 6AO7GT $6 A 76$ $6 A V 6$ $6 A W 7 G T$ $6 B 6 G$ $6 B F 6$ $6 B K 6$ $6 B T 6$ $6 B U 6$ |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & \text { TRIPLE-DIODE } \\ & \text { TRIODES } \end{aligned}$ |  |  |  | $\begin{array}{\|l\|} \text { 6R8 } \\ \text { 6S8GT } \end{array}$ | 6T8 | 1258GT | 19T8\% |  |  |  | $\left\lvert\, \begin{aligned} & 12 \mathrm{SBGT} \\ & 19 \mathrm{~T} 8 \end{aligned}\right.$ | GS8GT |
|  | DIODE PENTODES | $\begin{aligned} & \hline 1 \mathrm{LD5} \\ & 106^{*} \\ & 155 \\ & \text { 1SB6GT } \\ & \text { 1T6 } 6^{*} \\ & 1 \mathrm{US} \end{aligned}$ |  |  | $\begin{aligned} & \text { 6SF7 } \\ & \text { 6SF7GT } \\ & \text { 6SV7 } \end{aligned}$ |  | 12SF7GT |  |  |  |  | 12SF7GT | $\begin{aligned} & \text { 6SF7 } \\ & \text { GSV7 } \end{aligned}$ |
|  | DIODE POWER PENTODES | 1N6G <br> 1N6GT |  |  |  |  |  |  |  |  |  |  |  |
|  | DOUBLE-DIODE PENTODES | 1F6 <br> 1F7G <br> 1F7GiI |  | 2B7 | $\begin{array}{\|l\|} \hline \text { 6B7 } \\ \text { 6B8 } \\ \text { 6B8G } \\ \hline \end{array}$ | $\begin{aligned} & \text { 6B8GT } \\ & \text { 7E77 } \\ & \text { 7R7 } \\ & \hline \end{aligned}$ | $\begin{aligned} & 12 C 8 \\ & 14 E 7 \\ & 14 \mathrm{R}^{2} \end{aligned}$ |  |  |  |  | $\begin{array}{\|l\|} \hline 12 \mathrm{C8} \\ 14 \mathrm{E} 7 \\ 14 \mathrm{R} 7 \\ \hline \end{array}$ | $\begin{array}{ll} \text { 6B7 } & \text { 6B8GT } \\ \text { 6B8 } & 7 E 7 \\ \text { 6B8G } & 7 R 7 \end{array}$ |
|  | TRIODE PENTODES |  |  |  | $\begin{aligned} & \text { 6AD7G } \\ & \text { 6F7 } \end{aligned}$ | $\begin{aligned} & \text { 6F7G } \\ & \text { 6P7G } \end{aligned}$ | 12B8GT | 25B8GT |  |  |  | 2588GT | 6 6F7 $^{6 F 7 G}$ 6P7G |
|  | DIODE TRIODE PENTODES | $\begin{aligned} & \text { 1B8GT } \\ & \text { 1D8GGT } \\ & \text { 3A8GT } \end{aligned}$ |  | 3A8GT; |  |  |  | 25D8GT |  |  |  | 25D8GT |  |
|  | HALF-WAVE RECTIFIERS POWER PENTODES |  |  |  |  |  | 12A7 | 25A7GT |  |  |  |  | $\begin{aligned} & \text { 25A77 } \\ & { }^{25 A} \end{aligned}$ |
|  | HALF-WAVE RECTIFIERS BEAM PENTODES |  |  |  |  |  |  |  | 32L7GT ${ }^{\circ}$ | $\begin{aligned} & \text { 70A7GT } \\ & \text { 70L7GT } \end{aligned}$ | $\begin{array}{\|l\|} \hline 117 \mathrm{~L} 7 / \\ \text { M7GT } \\ \text { 117N7GT } \\ \text { 117P7GT } \\ \hline \end{array}$ | $\begin{aligned} & \text { 70A7GT } \\ & \text { 70L7GT } \end{aligned}$ | 32L7GT |
| - 1.25 V |  |  | \% 2.8 V . |  | \# $18.9 \mathrm{~V} . \quad$ - 32.5 V . |  |  |  |  |  |  |  |  |

Courtesy TUNG-SOL Lamp Works, Inc.

FUNCTIONAL CLASSIFICATION OF TUBES


FUNCTIONAL CLASSIFICATION OF TUBES

| APPLICATION |  |  | HEATER VOLTAGES |  |  |  |  |  |  | 150 MILLIAMPERE HEATER CURRENT | 300 MILLIAMPERE <br> HEATER CURRENT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | COLD CATHODE | 1.4 | 2.5 | 5.0 | 6.3 | 12.6 | 25 |  |  |
|  |  | DIODES |  | $\begin{aligned} & \text { 183GT } \\ & \text { 1X2 } \\ & 1 \mathrm{V2} \\ & 1 \mathrm{Y2} \\ & 1 \mathrm{Z2} \end{aligned}$ | $\begin{aligned} & \text { 2V3G } \\ & \text { 2X2 } \\ & \text { 2X2/879 } \\ & \mathbf{8 7 9} \end{aligned}$ |  |  |  |  |  |  |
|  |  | DOUBLE DIODES |  |  |  |  | 6ALS | 12ALS |  | 12ALS | 6ALS |
|  |  | DIODES |  |  |  | 5V4G | 6U4GT 6W4GT |  | 25W4GT |  | 25W4GT |
|  |  | DIODE CONNECTED |  |  |  |  | 6AS7G |  |  | 6AS7G |  |
|  | ※枈 | DOUBLE DIODE |  |  |  |  | 6ALS | 12ALS |  | 12AL5 | 6.425 |
|  | 点学空 | DIODES | $\begin{aligned} & \text { 0Y4 } \\ & \text { 0Y4G } \end{aligned}$ |  |  |  |  |  |  |  |  |
|  |  | DOUBLE DIODE | $\begin{aligned} & \text { 0Z4 } \\ & 024 \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & \mathbf{8 2} \\ & \mathbf{8 3} \end{aligned}$ |  |  |  |  |  |  |
|  |  | GLOW DISCHARGE DIODE | 0 A 2 <br> 0A3／VR－75 <br> 0B2 <br> 0B3／VR－90 <br> 0C3／VR－105 <br> OD3／VR－150 |  |  |  |  |  |  |  |  |
|  |  | GAS TRIODE | 1 C 21 |  | $\begin{aligned} & \text { 2A4G } \\ & \text { 2B4 } \\ & \text { 2C4 } \\ & 885 \end{aligned}$ |  | $\begin{aligned} & \hline \text { 6D4 } \\ & 6 \mathrm{Q} 5 \mathrm{G} \\ & 884 \end{aligned}$ |  |  |  |  |
|  |  | GAS TETRODES |  |  |  |  | $\begin{aligned} & \text { 2D21 } \\ & 2050 \\ & 2051 \end{aligned}$ |  |  |  |  |
|  |  | RELAY TUBE | OAS |  |  |  |  |  |  |  |  |

## SECTION

## RECEIVING TUBE SUBSTITUTION GUIDE

This section includes the actual information on the tube substitutions. Four columns are included. The first column lists the tule type for which a substitute is desired. This listing is in numerical and alphabetical order. For example 6CB6 precedes 6CD6 and 6ZY5 precedes 7A4. We have not indicated any difference between metal and glass tubes of the octal type. The tube listed can thus be considered either as metal or a glass type. The letters $G, G T, G T / G, G A$, or $G P$ indicates that the tube has a glass envelope, the $G T$ and $G T / G$ are smaller and newer versions of the $G$ type. The glass tubes, in practically all cases, have the same characteristics as the metal types.

One of the primary differences between the glass and metal tules is that the metal type usually have an internal shield. A pin at the base of these tubes is connected to this shield. In most cases this pin is wired to the common ground or B minus of the set. In a few cases substituting a glass type for a metal type causes the circuit to become unbalanced or feedback occurs due to a lack of proper shielding. Most often this can be overcome by shielding the tule or realigning the set.

The second column lists the various possible substitutes. Quite often more than one substitute is listed for a single tube. In such cases the tulee in the first column is not repeated for each substitute but is listed only once.

The third column lists the performance of each tube. Three performance ratings are shown in this list. These are $E$ for EXCELLENT, $G$ for GOOD, and $P$ for POOR. They define the suitability of a substitute predicated upon its electrical characteristics as compared to those of the original and upon the relationship between the characteristics of the substitute to the constants of the circuit, which was designed to function best with the original. The comparison between the characteristics of the tubes excludes the filament or heater voltage and current ratings. It is assumed that whatever may be the performance characteristics of the substitute - the filament or heater voltages and current are correct, even if it requires certain minor circuit modifications to accomplish this condition.

Concerning the $E, G$, and $I^{\prime}$ ratings, it stands to reason that those tules which bear $E$ (excellent) ratings are either the exact equivalents differing perhaps in
basing and maybe in filament or heater voltage and current ratings - or so closely approximate the electrical characteristics of the original as to require no significant major modifications. All applicable tube substitutions which might bear an $E$ rating in performance are not shown in the main listing. Some appear on the addendum pages. These represent lastminute additions as the result of information received from television receiver manufacturers and appear at the end of this section.

Concerning the $G$ (good) rating, it reflects more than just moderate differences in tube characteristics between the substitute and the original that is being replaced. It still means a triode substitute for a triode original, or a pentode substitute for a pentode original, and sometimes the conversion of a pentode into a triode, but the plate (and screen) voltage demands of the substitute may be higher than that of the original - or the transconductance or amplification constant of the substitute may be less than the original - all of which means that the circuit demands incorporated in the equipment design are not being met by the substitute tube. Possibly the plate impedance of the substitute is higher or lower, reducing the originally intended over-all amplification; perhaps a slight amount of distortion is added to the signal by the substitute. Yet the sulbstitute may be used even if it is not as good in performance as the original, for again it is a matter of continuing the operation of a device.

Those substitutions which bear $P$ (poor) ratings are used only as a last resort. They represent the extremes in tube substitution when it is a matter of accomplishing a repair job of sorts, rather than none at all because more appropriate substitutes are not available. Of course, modifications can be made in the circuit design and circuit constants so as to accommodate the tule rated poor, in which case, considerable improvement may be accomplished. It must be remembered, of course, that the $P$ rating - or for that matter, the $G$ rating - is not a reflection upon the capalilities of the tube or the brand. It simply means that the tube, so designated in the list. was not intended for use in the type of system for which it is suggested as a sulbstitute. With proper circuit changes, it might, as we said before, become a better performing sulstitute. But whether or not such design changes are warranted is a matter of individual consideration. As
far as circuit modification is concerned, it can be a tedious task. Much depends upon comparative reference data and background knowledge of circuits. Finally such changes are possible only if the cost is acceptable to the owner of the equipment.

The fourth or last column lists the circuit changes that are necessary to make the substitute operate properly. In many cases no change whatsoever is required, the original tube is pulled out and the substitute plugged in. Where the reference "parallel circuits only" or "series circuits only" is found, it refers only to the type of filament circuit arrangement in which the substitute tube can be used.

## Original and Substitute Sockets

The tube substitution lists contain illustrations of the original and the substitute tube sockets when the tube interchange involves a change in sockets. These are offered as a convenience in wiring. The views are the bottoms of the sockets and these correspond to the pin locations on the bottom of the respective tube bases. The bottom socket view of the original tube will always be found to the left of the change writeup and will bear the designation "ORIG." The bottom socket view of the substitute tube will always be found to the right of the change writeup and will bear the designation "SUB."

The instructions given between the two illustrations state the respective socket terminals involved in the rewiring operation. In view of the necessity for removing one socket before mounting the other, it is suggested that as each wire is disconnected from the original socket, it be labeled with a tiny tag showing the appropriate socket connection number. These correspond to the pin numbers on the tube base. Then when being rewired to the new socket, all that is required is to solder the numbered lead to the terminal on the socket as stated in the instructions.

Care must be exercised to see that the socket connections are read in accordance with the location of the key as shown on the pages. In order to attain correspondence between the socket mounted on the chassis and the instructions, one or the other should be changed in physical position so that the keys or identifying terminals are in the same relative position. Another precautionary note relates to the grid caps. In many cases capped tubes are replaced by single ended tubes, and vice-versa. The leads must be properly connected. Finally in some substitutions the pin numbers on the original and the substitute are the same, that is, 1 to 1 , 2 to 2,3 to 3 and so on. This is not standard for all the tubes, nor is it standard for all the pins even if it is true for some of them in any one substitution. In other words, the instructions should be read completely. Nothing should be taken for granted.

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Appendix

## 336 pages

270 illustrations
$\$ 3.60$

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JOHN F. RIDER, PUBLLSHER, Inc., 480 Canal St., New York 13, N.Y.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 00A | 01 A | E | No changes. |
|  | 40 | G |  |
| 01 A | 00A | E | No changes. |
|  | O0AA | E |  |
|  | 01 B | E |  |
| 0 A 2 | $0 \mathrm{B2}$ | P | Where application is not too critical. |
| 0A3 | VR75 | E | No changes. |
| 0 A 4 | 1267 | E | No changes. |
| 0B2 | 0 C 3 | E | Where space permits. Change socke to octal and rewire as follows: |
|  |  |  | No. 1 on miniature <br> to No. 5 on octal <br> 2 <br> 5 <br> to 5 |
| $0 \mathrm{B3}$ | VR90 | E | No changes. |
| 0C3 | VR105 | E | No changes. |
|  | $0 \mathrm{B2}$ | E | Reverse 0B2 to 0C3 procedure. |
| 0D3 | VR150 | E | No changes. |
| OY4 | 0Y4G | E | No changes. |
| 0Y4G | 0 Y4 | E | Ground pin No. 1 |
| $0 \mathrm{Z4}$ | 0 Y4 | G | No changes. |
|  | $\text { 0Z4A/ } 1003$ | E |  |
|  | $1005 / \mathrm{CK} 1005$ | E |  |
|  | $6 \mathrm{X5}$ | E | Solder socket terminal No. 2 to chassis. Connect 6 V hot lead to No. 7. Motorolas and some other car radios have filament wired and the 6X5 may be used without making any changes. |
|  | 7 Y 4 | E | Change socket to loctal and rewire as follows: |
|  |  |  |  |
|  |  |  | Connect No. 8 on loctal to chassis and No. 1 on loctal to 6 V hot lead. |
|  | 84 | E | Reverse 84 to $6 \times 5$ procedure. |
| 0Z4A | $\begin{aligned} & \text { 0Y4 } \\ & 1005 / \mathrm{CK} 1005 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. |
| 1 A3 | 1B4/1294 | E | Where space permits. Change socket to loctal and rewire as follows: <br> No. 1 on miniature to No. 1 on loctal |
| $1 \mathrm{A4}$ | 1 B4 | E | No changes. |



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 1 A 7 | 1D7 | P | No changes, unless there is a resistor across 1 A7 filament, which must be removed. 1D7 is rated 2 V 60 mils and draws slightly less than 50 on i.4. |
|  | 1 L 6 | G | Same as 1A7 to 1U6. |
|  | 1 LA6 | E | Change socket to loctal and rewire as follows: |
|  | 1 LC 6 | E |  |
|  | 1 R 5 | G | Make adaptor as follows: Solder rather heavy wires three inches long to all lugs except No. 5 of miniature socket. Break the 1A7, clean out the base and save the cap. Push the wires from miniature socket thru the base pins as follows: |
|  |  |  | The octal socket could be replaced by a miniature using the above connections but it is usually hard to find a place to mount it. <br> If 1 R5 squeals, reduce value of oscillator grid resistor to 75000 ohms or less if necessary. This resistor is, connected between terminal No. 5 on the the $1 A 7$ socket and ground or filament. |
|  |  |  | An idea we have been using successfully is to dig a trough from pin No. 5 to pin No. 7 on the adaptor, filling this with the graphite preparation made for volume controls, measuring the resistance, and filling the trough until the desired resistance is acquired. |
|  | 1 U6 | G | Parallel circuits only. Change socket to miniature and rewire as follows: <br> No. 2 on octal to No. 1 on miniature <br> 3 <br> 4 <br> to 5 <br> to 4 <br> to 3 <br> $\begin{array}{ll}\text { to } & 7 \\ \text { to } & 6\end{array}$ |
| $1 \mathrm{AB5}$ | 1 AD 5 | G | Parallel circuits only. Change socket to subminiature and rewire as follows: |
| $1 \mathrm{AC5}$ | 1 V5 | E | No changes. |
| $1 \mathrm{AD4}$ | 1 AD5 | G | Parallel circuits only. |
|  | 1 AE 4 | G | Reverse 1AE4 to 1AD4 procedure. |
| 1 AD 5 | $1 \mathrm{AB5}$ | G | Parallel circuits only. Reverse 1AB5 to 1AD5 procedure. |



Pin numbers on 1 AD4 number from right to left from red mark on base, as shown.

1 AF4 1 AF5

|  | $1 \mathrm{L4}$ |
| :---: | :---: |
|  | 1 T4 |
|  | 1 U 4 |
| 1 AF 5 | 1 LD5 |


|  | 1 S 5 | G |
| :--- | :--- | :--- |
| 1 B 3 | 1 X 2 | E |
| $1 \mathrm{~B} 4{ }^{*}$ | 1 A 4 | E |
|  |  |  |
|  | 1 D 5 | E |
|  | 1 E 5 | E |
|  | 32 | E |
|  | 34 | E |
| 1 B 5 | 1 H 6 | E |

G
G
P
P

E

E

E

No. 5 to No. 1
2 to 5
3 to 4
Do not use terminal No. 3 for anchor
G No changes. Parallel circuits only.
Rewire as follows:

No chall

Parallel circuits only. Where space permits. Change socket to loctal and rewire as follows:

|  | No. 1 on miniature | to No. | 1 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 3 | to | 4 |  |
|  | 4 | to | 3 |  |
|  | 5 | to | 2 |  |
|  | 6 | to | 6 |  |
|  | 7 | to | 8 |  |

G Parallel circuits only. No changes.
E Reverse 1 X2 to 1 B3 procedure.
E No changes.
E Same as 1A4 to 1D5.

E No changes.

Change socket to octal and rewire as follows:

| No. 1 on six prong | to No. 2 on octal |  |
| :--- | :--- | :--- |
| 2 | to | 3 |
| 3 | to | 4 |
| 4 | to | 5 |
| 5 | to | 6 |
| 6 | to | 7 |


| $25 S$ | E | No changes. |
| :--- | :--- | :--- |
| 1 A7 | E | Parallel circuits only. No changes. |
| 1 L6 | G | Parallel circuits only. Same as 1A7 to 1 U6 |
| 1 LA6 | E | Parallel circuits only. Same as 1A7 to 1LA6. |
| 1 LC 6 | E |  |


| TUBE | sub. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| $1 \mathrm{B7}$ | 1 R5 | G | Parallel circuits only. Same as 1 A7 to 1 R5. |
|  | 1 U6 | G | Parallel circuits only. Same as 1A7 to 1 U 6. |
| $1 \mathrm{B8}$ | 1 D 8 | E | No changes. |
| 1 C 3 | $1 \mathrm{G4}$ | G | Where space permits. Change socket to octal and rewire as follows: <br> No. 1 on miniature to No. 2 on octal |
|  | 1 LE3 | G | Where space permits. Change socket to loctal and rewire as follows: <br> No. 1 on miniature to No. 1 on loctal |
| 1 C 5 | 1 A5 | G | Parallel circuits only. No changes. |
|  | 1D8 | P | Remove and tape up any wires connected to 6 and 8. No connection to top cap. |
|  | 1 LA 4 | G | Same as 1A5 to 1LA4. Parallel circuits only. |
|  | 1 LB4 | G |  |
|  | 1Q5 | G | No changes. Bias different but tone is reasonably good. |
|  | 1S4 | G | Same as 3Q5 to 3S4, but connect nothing to No. 5 on miniature. |
|  | 1 T 5 | G | Parallel circuits no changes. Series circuits shunt 35 ohm resistor across filament. |
|  | 3Q4 | P | Change socket to miniature and rewire as follows: |
|  | 3S4 | P |  |
|  | 3Q5 | P | Same as 1Q5 to 3Q5. |
| 1 C 6 | 1 A 6 | G | Parallel circuits only. No changes. |
|  | $1 \mathrm{C7}$ | G | Same as 1A6 to 1C7. Either series or parallel circuits. |
|  | 1D7 | G | Same as 1A6 to 1C7. Parallel circuits only. |
| $1 \mathrm{C7}$ | 1 A6 | G | Reverse 1A6 to 1 C 7 procedure. Parallel circuits only. |
|  | 1 C 6 | E | Reverse 1A6 to 1C7 procedure. |
|  | $1 \mathrm{D7}$ | E | Parallel circuits only. No changes. |
| 1 C 8 | 1 AE5 | G | Parallel circuits only. |
|  | 1 E 8 | E | No changes. |
| 1 C 21 |  |  | No practical substitute. |


$P \quad$ Change socket to four prong and rewire as follows:


1E5* 1D5
Change socket to four prong and rewire as follows:


1 E7
1 E8

1 F5
32
34
951

1 F5

1 F6

1 F4

1 F7

1 C 8

1A4

## 1 B4



G No changes.

P
$P$
P
$P$
P
No practical substitute.
E No changes.

E

No. 2 on octal
5
7

Change socket to octal and rewire as follows:


No. 1 on five prong
to No. 2 on octal
2
4
3
5

| to | 3 |
| :--- | :--- |
| to | 4 |
| to | 5 |
| to | 7 |



E Reverse 1 F4 to 1 F5 procedure.
E
Change socket to octal and rewire as follows:
No. 1 on six prong to No. 2 on octal

2
3
4
5
6
cap

| TUBE | SUB. | PERF. | CIRCUIT CHA.NGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 1 F 7 | 1F6 | E | Reverse 1F6 to 1F7 procedure. |
| $1 \mathrm{G4}$ | 1 C 3 | G | Reverse 1C3 to 1G4 procedure. |
|  | 1E4 | G | No changes. |
|  | 1 H 4 | P |  |
|  | 1 LE3 | G | Same as 1E4 to 1LE3. |
|  | 30 | P | Same as 1E4 to 30. |
| 1 G5 | 1 J 5 | G | No changes. |
| 1 G6 | 1 J 6 | P | Parallel circuits only. No changes. |
| 1 H 4 | 1E4 | P | No changes. |
|  | 1LE3 | P | Same as 1E4 to 1LE3. |
|  | 30 | P | Same as 1E4 to 30. |
| 1 H 5 | 1 H 6 | P | Connect grid cap to socket terminal No. 6. Connect Nos. 4 and 5 toge |
|  | 1 LD5 | G | Change socket to loctal and rewire as follows: |
|  | 1 LH 4 | E | Change socket to loctal and rowire as follows: |
|  | 155 | G | Change socket to miniature or make adaptor wiring as follows: |
| $1 \mathrm{H6}$ | $1 \mathrm{B5}$ | E | Change socket to six prong and rewire as follows: |
| 1 J 5 | 1 G5 | G | No changes. |
| $1 J 6$ | 19 | E | Reverse 19 to 1J6 procedure. |
| 1 L 4 | 1 AF 4 | G | Parallel circuits only. No changes. |
|  | 1SA6 | G | Same as 1T4 to 1SA6. |
|  | $\begin{aligned} & 1 \mathrm{~T} 4 \\ & 1 \mathrm{U} 4 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. |



1L6-ILA6

## RECEIVING TUBE SUBSTITUTION GUIDE

3Q4 3 S 4

3Q5
1 LA6

1 A7

1B7

1L6
1LB6

1 LC6
1 R5

In case this substitution squeals on the high frequency end of the dial, change the oscillator grid resistor to 100 M ohms or less if necessary.


1LC5-1LO5
TUBE SUB.
1 LC5

1 LC6

1LD5

1SA6

## RECEIVING TUBE SUBSTITUTION GUIDE

## PERF.

G
Change socket to octal and rewire as follows:
No. 1 on loctal to No. 2 on octal

2
3
4
6
8

| to | 8 |
| :--- | :--- |
| to | 6 |
| to | 3 |
| to | 4 |
| to | 7 |



G Same as 1 LG5 to 1 L4.
G Same as 1 LG5 to 1 L 4 .
G Change socket to octal and rewire as follows:
No. 1 on loctal

| to No. 2 on octal |  |
| :--- | :--- |
| to | 3 |
| to | 6 |
| to | 5 |
| to | 4 |
| to | 7 |
| to | cap |

G Reverse 1A7 to 1 LA6 procedure. Parallel circuits only.
G Same as 1 LA 6 to 1 U6.
E No changes.
P Same as 1LA6 to 1LB6.
G Same as 1LA6 to 1 R5.
G Same as 1LA6 to 1 U6. Parallel circuits only.
P Parallel circuits only. Reverse 1AF5 to 1LD5 procedure.
G Change socket to octal and rewire as follows:


G Change socket to miniature and rewire as follows:


G
G
Change socket to octal and rewire as follows:

| No. 1 on loctal | to No. 2 on octal |  |
| :--- | :--- | :--- |
| 2 | to | 3 |
| 3 | to | 4 |
| 4 | to | 5 |
| 6 | to | 8 |
| 8 | to | 7 |




G
Same as 1 LC5 to 1 S4. Parallel circuits only.




| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 1 T 4 | $1 \mathrm{U4}$ | G | No changes. |
| 1 T5 | 1 A5 | G | No changes. 1 T5 pulls 10 mils more but it works OK. |
|  | 1 C 5 | G | Parallel circuits only. No changes. |
|  | 1D8 | P | Remove and tape up wires if any anchored on No. 6 and 8. Parallel circuits only. |
|  | 1 G4 | P | No changes. Emergency works good in most cases. |
|  | 1 LA4 | P | Same as 1A5 to 1LA4 |
|  | $1 \mathrm{LB4}$ | P |  |
|  | 1Q5 | G | Parallel circuits only. No changes. |
|  | 1S4 | G | Same as 3 Q 4 to 3 S 4 parallel circuits only except omit connection No. 8 on octal to No. 5 on miniature. |
|  | 304 | P | Electric operation only. Same as 3Q5 to 3S4 but connect nothing to No.. 5 |
|  | $3 \mathrm{S4}$ | P | on miniature. |
| 1 T6 | 1Q6 | E | Rewire as follows: |
|  |  |  | No. 3 to No. 2 <br> 1 to |
|  | 1S6 | E | No changes. |
| 1 U4 | 1AF4 | G | Parallel circuits only. No changes. |
|  | 1 L 4 | G | No changes. |
|  | 1S5 | G | Rewire as follows: |
|  |  |  | $\begin{array}{rll} \text { No. } 5 & \text { to No. } & 1 \\ 2 & \text { to } & 5 \\ 3 & \text { to } & 4 \end{array}$ |
|  | 1SA6 | G | Where space permits. Same as 1T4 to 1SA6. |
|  | 1 T4 | G | No changes. |
| 1 U5 | 1S5 | E | Rewire as follows: |
|  |  |  | No. 2  <br> Reverse 3 and to No. 5 <br> 4  |
| 1 U6 | 1 L 6 | E | Parallel circuits only. No changes. |
| 1 V | 623 | E | No changes. |
|  | $12 \mathrm{Z3}$ | G | No changes necessary. Series circuits only. Six volts added to the filament string makes no difference. |
| 1 V 2 |  |  | No practical substitute. |
| 1 V 5 | $1 \mathrm{AC5}$ | E | No changes. |


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :--- | :---: | :---: | :---: |
| 1W4 | 1LA4 | G | Where space permits. Reverse 1LB4 to 1W4 procedure. |
|  | 1LB4 | G |  |
|  | $3 E 5$ | $G$ | Rewire as follows: |

Connect 1 and 7 together

P No changes.
G Where space permits. Change socket to octal and rewire as follows:


## Change socket to seven prong and rewire as follows:

No. 1 on six prong to No. 1 on seven prong

|  | 2 | to | 2 and 3 |  |
| :---: | :---: | :---: | :---: | :---: |
| $00^{0} 0^{6}$ | 3 | to | 4 | $\mathrm{O}_{3}{ }^{4}{ }_{5}^{\circ}$ |
| $\mathrm{O}_{2} 50$ | 4 | to | 5 | $\left(\begin{array}{ll} \\ \hline & 5 \\ \hline & 5\end{array}\right.$ |
| ${ }^{\circ} \mathrm{O}$ | 5 | to | 6 | 0 |
| onte. | 6 | to | 7 | Sub |
|  | cap | to | cap |  |


|  | 55 | $E$ | Parallel circuits only. No changes. |
| :--- | :--- | :--- | :--- |
| $2 A 7$ | $2 A 7 S$ | $E$ | No changes. |
| $2 B 7$ | $6 B 7$ | $E$ | Heater voltage - current ratings differ. |





3V4 G Parallel circuits only. No changes.

## No practical substitute.



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 3Q5 | 3V4 | G | Change socket to miniature and rewire as follows: |
| 3S4 | 3E5 | G | Parallel circuits only. Same as 3Q4 to 3E5. |
|  | 304 | G | No changes. |
|  | 3 V 4 | G | Same as 3Q4 to 3V4. |
| 3V4 | $3 \mathrm{A4}$ | P | Parallel circuits only. Reverse 3A4 to 3V4 procedure. |
|  | 3E5 | G | Parallel circuits only. No changes. |
|  | 3Q4 | G | Reverse 3Q4 to 3V4 procedure. |
| 4A6 |  |  | No practical substitute. |
| 5A6 |  |  | No practical substitute. |
| 5AX4 | 5 AZ4 | G | No changes. |
|  | 5U4 | G |  |
|  | 5 V 4 | G |  |
|  | 5W4 | G |  |
|  | 5 Y 3 | G |  |
|  | $5 \mathrm{Z4}$ | G |  |
| 5AZ4 | $5 \mathrm{AX4}$ | G | No changes. |
|  | $5 \mathrm{U4}$ | G |  |
|  | 5 V 4 | G |  |
|  | 5W4 | G |  |
|  | 5 Y3 | G |  |
|  | 5Z4 | G |  |
| 5R4GY | 5T4 | G | No changes. Use only where inverse peak voltage does not exceed 450 |
|  | 5 U4 | G | volts per plate. |
|  | 5 V 4 | P |  |
|  | 5 Y 3 | P |  |
|  | 5Z4 | P |  |
|  | 5X4 | G | Same as 5 T 4 to 5 Y 4 |
|  | 5 Y 4 | P |  |
|  | $5 \mathrm{Z3}$ |  |  |
|  | 80 | $\mathbf{P}$ | socket to four prong and rewire as follows: |
|  | 83 | G | (9) No. 2 on octal to No. 1 on four prong |
|  | 83 V | G | (2) |
| 5T4 | $5 \mathrm{AX4}$ | G | No changes. |
|  | 5AZ4 | G |  |
|  | $5 \mathrm{U4}$ | G |  |
|  | 5 V 4 | G |  |
|  | 5W4 | G |  |
|  | 5 Y3 | G |  |
|  | $5 \mathrm{Z4}$ | G |  |


| 5T4-5x4 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |  |
| :---: | :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES | ARY |
| 5 T 4 | 5 Y 4 | G | Make adaptor as follows: <br> No. 1 on base <br> 2 <br> 4 <br> 6 <br> 8 | to No. 1 on top  <br> to 8 <br> to 3 <br> to 5 <br> to 7 |
| 5U4 | 5AX4 <br> 5AZ4 <br> 5 T4 <br> 5V4 <br> 5W4 <br> 5 Y3 <br> 5Z4 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |  |
|  | $5 \mathrm{Y4}$ | G | Same as 5T4 to 5Y4. |  |
|  | $\begin{aligned} & 5 Z 3 \\ & 80 \\ & 83 \\ & 83 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathbf{E} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 5R4GY to 5Z3. |  |
| $5 \mathrm{V4}$ | 5AX4 <br> 5AZ4 <br> 5T4 <br> 5U4 <br> 5W4 <br> 5 Y3 <br> 5Z4 | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. |  |
|  | 5 Y 4 | G | Same as 5T4 to 5Y4. |  |
|  | $\begin{aligned} & 5 Z 3 \\ & 80 \\ & 83 \\ & 83 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 5R4GY to 5Z3. |  |
| 5W4 | 5AX4 <br> 5AZ4 <br> 5 T4 <br> 5U4 <br> 5 V4 <br> 5 Y3 <br> 5Z4 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |  |
|  | 5 Y 4 | G | Same as 5T4 to 5Y4. |  |
|  | $\begin{aligned} & 5 Z 3 \\ & 80 \\ & 83 \\ & 83 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 5R4GY to 5Z3. |  |
| 5X3 | 5Z3 <br> 80 <br> 83 <br> 83 V <br> 1275 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |  |
| 5X4 | 5 T4 <br> 5 U4 <br> 5V4 <br> 5 Y3 <br> 5Z4 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Rewire as follows: $\quad \begin{array}{r} \\ \\ \text { No. } \\ 7 \\ 3 \\ 5\end{array}$ | $\begin{array}{ll} \text { to No. } & 2 \\ \text { to } & 4 \\ \text { to } & 6 \end{array}$ |




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## 6AB4-6AC5G

TUBE SUB. 6AB4 6N4

9002
$6 \mathrm{AB} 5 / 6 \mathrm{~N} 5 \quad 6 \mathrm{E}$ 6U5/6G5

6AB6
6AC6
6B5
G

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## PERF.

P Parallel circuits only. Rewire as follows:

Reverse No. 6 and No. 7
Connect No. 1 to No. 5 Remove and tape any wires connected to unused pins.

P Rewire as follows:
Remove and tape up any wires anchored on pins No. 2 and No. 5

P Parallel circuits only. No changes.
P Parallel circuits only. No changes.
G Parallel circuits only. No changes.
G Change socket to six prong and rewire as follows:



7W7 G Change socket to loctal and rewire as follows:

$\begin{array}{llll}6 A C 5 G & \text { 6AC5GT } & \mathrm{E} & \text { No changes. } \\ & 6 \mathrm{AC} 5 \mathrm{GT} / \mathrm{G} & \mathrm{E} & \end{array}$


Remove wires from No. 3 and connect to No. 4. Connect grid lead to No. 5. This pin may be used for anchor. Extend to grid cap.

6K5 G Rewire as follows:
Connect terminal No. 5 to grid cap. This terminal may be used as an anchor.

7B4 G Change socket to loctal and rewire as follows:


6AD6 6AF6 G No changes.

6AD7-6AG6G

| TUBE | SUB. | PERF. |
| :---: | :---: | :---: |
| 6AD7 | $6 F 7$ | $G$ |

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## CIRCUIT CHANGES NECESSARY <br> Parallel circuits only. Change socket to seven prong and rewire as follows: <br> No. 1 on octal to No. 5 on seven prong <br> 2 to <br> (3)

6P7 G Parallel circuits only. Remove wires from No. 5 and extend to grid cap. Rewire as follows:

| No. 4 | to No. 5 |  |
| ---: | :--- | :--- |
| 3 | to | 4 |
| 7 | to | 3 |
| 1 | to | 7 |

No changes.
6AF5
6 C 5
6.55 6 P5

6AH7

6N7

| 6 AF5 | 6 AD5 | G | No changes. |
| :---: | :---: | :---: | :---: |
|  | 6AE5 | G |  |
|  | 6 C 5 | G |  |
|  | 6 J 5 | G |  |
|  | 6 P 5 | G |  |
| 6AF6 | 6AD6 | G | No changes. |
| 6 AF7 |  |  | No practical substitute. |
| 6AG5 | 6AJ5 | P | Parallel circuits only. No changes. |
|  | $6 \mathrm{AK5}$ | G | Parallel circuits only. No changes. |
|  | 6 AU6 | G | No changes. |
|  | 6BC5 | G | No changes. |
|  | 5590 | G | Parallel circuits only. No changes. |
|  | 5591 | G |  |
|  | 9001 | G |  |
|  | 9003 | G |  |

No practical substitute.

| TUBE | SUB. | PERF. | CIRCUTT C |
| :--- | :---: | :---: | :--- |
| 6AG7 | 6AK7 | E | No changes. |
| 6AH5 | $6 A L 6$ | $G$ | Rewire as follows: |

6L6

$6 \mathrm{AH} 6^{*} \quad$| 6 AJ 5 |
| :--- |
|  |
|  |

6AS6

6AU6
6BC5
6BD6

## EF50

6AE6
6C8

6SN7

7N7

6AJ5
6AG5
6AK5
6AU6

No. 4
1
6
to cap
to 4
to 5
G Rewire as follows:
No.

| to No. 3 |  |
| :--- | :--- |
| to | 4 |
| to | 5 |

P Parallel circuits only. No changes.
P
P
Parallel circuits only. Rewire as follows:
Reverse No. 2 and No. 7

|  | 6AU6 | P | Parallel circuits only. No changes. |
| :---: | :---: | :---: | :---: |
|  | 6BC5 | G | Parallel circuits only. No changes. |
|  | 6BD6 | P | Parallel circuits only. No changes. |
|  | EF50 | P | Parallel circuits only. Reverse EF50 to 6BA6 procedure. |
| $6 \mathrm{AH7}$ | 6AE6 | G | Parallel circuits only. Reverse 6AE6 to 6AH7 procedure. |
|  | 6C8 | G | Rewire as follows: |
|  |  |  | Connect wire from No. 1 to grid cap. Remove wires from No. 2 |
|  |  |  | No. 8 to No. 2 <br> 4 to 8 |
|  |  |  | Connect wires removed from No. 2 to No. 4. |
|  | 6SN7 | P | Parallel circuits only. Rewire as follows: |
|  |  |  | Reverse No. 2 and No. 3 |
|  |  |  | Remove wires from No. 4 |
|  |  |  | No. 5 to No. 4 |
|  |  |  | 6 to <br> Cennect wires removed from No. 4 to No. 6. |

Parallel circuits only. Change socket to loctal and rewire as follows:


No. 1 on octal 2 4 5 6 7 8

Parallel circuits only. No changes.
P No changes.
P Parallel circuits only. No changes.

6AJ7-6AM6
6AK7 6AG7 E No changes.

6AL5 6H6

6 AL7
6AM5
6AQ5

6AR5

6AM6
6AH6 6AK6

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6AJ7 | $\begin{aligned} & 6 \mathrm{AB} 7 / 1853 \\ & 6 \mathrm{AC} 7 / 1852 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
|  | 6SD7 | G | Parallel circuits only. No changes. |
|  | 6SE7 | G |  |
|  | 6SJ7 | G |  |
|  | 6SK7 | G |  |
|  | 6SS7 | G |  |
|  | 5693 | G |  |
| 6AK5 | 6AG5 | G | Parallel circuits only. No changes. |
|  | 6AH6 | G | Parallel circuits only. Connect No. 2 and No. 7 together. |
|  | 6AJ5 | P | No changes. |
|  | 6AU6 | P | Parallel circuits only. No changes. |
| 6AK6 | 6 AR5 | G | Parallel circuits only. Rewire as follows: |
|  |  |  | Connect No. 2 and No. 7 together |

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Connect No. 2 and No. 7 together

G Where space permits. Change socket to octal and rewire as follows: No. 1 on miniature to No. 8 on octal

G Reverse 6AH5 to 6AL6 procedure.
E Rewire as follows:
cap to No. 3

No practical substitute.
Parallel circuits only.
No. 7 to No. 6

P Parallel circuits only. Rewire as follows:
No. 7 to No. 6

G
G

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :--- | :---: | :---: | :---: |
| 6AM6 | 6AU6 | $G$ | Rewire as follows: |
|  | 6BA6 | $G$ | Remove wires from No. 2 |
|  | 6BD6 | $G$ | No. 6 |

No. 7 to No. 2

6AN6
6AN7
6AQ5

6AQ6 | 6BD7 | G |  |
| :--- | :--- | :--- |
|  |  |  |
|  | 6AT6 | G |
|  | 6AV6 | G |
|  | 6BF6 | G |
|  | 6BK6 | G |
|  | 6BT6 | G |
|  | 6BU6 | G |
| 6AQ7 | 6AW7 | G |

6AN5

6 AR5

6AS5
6BF5
6 V 6

6AW7
6AV6
G
G
G
G

No practical substitute.
No practical substitute.
P Parallel circuits only. Rewire as follows:
No. 7
to No. 1
to
7

No. 7
to No. 1

G Parallel circuits only. Reverse 6AS5 to 6AQ5 procedure.
P Parallel circuits only. No changes.
G Where space permits. Change socket to octal and rewire as follows:
No. 1 on miniature to No. 5 on octal

|  | 2 | to | 8 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 3 | to | 2 |  |
|  | 4 | to | 7 |  |
|  | 5 | to | 3 |  |
|  | 6 | to | 4 |  |
|  | 7 | to | 5 |  |

Parallel circuits only. Reverse 6BD7 to 6AQ6 procedure.
G Parallel circuits only. No changes.

G Rewire as follows:

Remove wires from No. 1
No. $2 \quad$ to No. 1
Connect wires removed from No. 1 to No. 4.
Remove wires from No. 3
No. 5 to No. 3
Connect wires removed from No. 3 to No. 6.

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TUBE
6AR5

6AR6

6AR7
6AS5

6AS6

6AS7G
6AT6

SUB.
6AK6

6 AM5

6AQ5

6 AS5
6F6
6G6
6 K 6
6L6
6U6
6 V 6
6W6
6 Y 6
5824
asta

6AN5

6AQ5

6AR5

6BH6
6BJ6 6CB6
6AH6

G
$\mathbf{G}$
G

No practical substitute.
G Parallel circuits only. Rewire as follows:
Reverse No. 1 and No. 2
5 to 1

7 to 5
G Parallel circuits only. Rewire as follows:
Reverse No. 1 and No. 2 5 and 7

G Parallel circuits only. Rewire as follows:
Reverse No. 1 and No. 2
to $\quad 1$
to 5

P Parallel circuits only. Rewire as follows:
Reverse No. 2 and No. 7

No practical substitute.
G Parallel circuits only. No changes.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6AT6 | 6AV6 | G | No changes. |
|  | 6BF6 | G |  |
|  | 6BK6 | G |  |
|  | 6BT6 | G |  |
|  | 6BU6 | G |  |
|  | 6 BD 7 | G | Parallel circuits only. Reverse 6BD7 to 6AQ6 procedure. |
| 6AU5 | $6 \mathrm{AV5}$ | G | Parallel circuits only. No changes. |
|  | 6BD5 | G |  |
| 6AU6 * | 6AG5 | P | No changes. |
|  | 6AJ5 | P | Parallel circuits only. No changes. |
|  | $6 \mathrm{AK5}$ | P |  |
|  | 6BA6 | G | No changes. |
|  | 6 BH 6 | G | Parallel circuits only. Rewire as follows: |
|  |  |  | Reverse No. 2 and No. 7 |


|  | EF50 | G | Reverse EF50 to 6BA6 procedure. |
| :---: | :---: | :---: | :---: |
| 6AV5 | 6AU5 | G | No changes. |
|  | 6BD5 | G |  |
|  | 6BQ6 | G | Parallel circuits only. Reverse 6BQ6 to 6BD5 procedure. |
| $6 \mathrm{AV6}$ | 6AQ6 | G | Parallel circuits only. No changes. |
|  | 6AT6 | G | No changes. |
| 6 AW 7 | 6AQ7 | G | Reverse 6AQ7 to 6AW7 procedure. |
| $6 \mathrm{AX5}$ | 6AX6 | E | Parallel circuits only. Tie Nos. 4 and 8 together. |
|  | 6BY5 | E | Parallel circuits only. Rewire as follows: |
|  |  |  | Connect Nos. 1 and 8 together; also Nos. 3 and 4. |
|  | 6W5 | G | Parallel circuits only. No changes. |
|  | 6X5 | G |  |
|  | 6ZY5 | G |  |
|  | 1274 | G |  |
| 6AX6 | 6 AX5 | G | Can be used only where No. 4 and No. 8 in 6AX6 are connected together |
|  | 6W5 | G | without change. |
|  | 6X5 | G |  |
|  | $6 \mathrm{ZY5}$ | G |  |
|  | 1274 | G |  |

EF50

6AU5 6BD5 6BQ6

6AQ6
6AT6
6AQ7
6AX6
6BY5

Reverse No. 2 and No. 7

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6 B6
6SQ7

7B6

7C6

75

2B7
6B7

P No changes.
E No changes.

E
Make adaptor as follows:

| No. 1 on base | to No. 1 on top |
| :---: | :--- |
| 2 | to |
| 3 | to |
| 4 | to |
| 4 | to |
| 5 | to |
| 7 | to |
| 8 | 7 |
| Extend No. 2 on top to grid connection. |  |

E Parallel circuits only. No changes.
G Change socket to loctal ard rewire as follows:
No. 2 on octal to No. 1 on loctal


3
4
5
7
8
cap

| to | 2 |
| :--- | :--- |
| to | 5 |
| to | 6 |
| to | 8 |
| to | 4 or |

E Same as 6B6 to 7B6. Parallel circuits only.

E
Change socket to six prong and rewire as follows:


E
eater voltage-current ratings differ.


| $68 C 7$ |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 6 BC 7 |  |  | No practical substitute. |
| 6BD5 | 6AU5 | P | Parallel circuits only. No changes. |
|  | $6 \mathrm{AV5}$ | P |  |
|  | 6BQ6 | G | Parallel circuits only. Reverse 6BQ6 to 6BD5 procedure. |
| 6BD6 | 6AH6 | P | Parallel circuits only. No changes. |
|  | EF50 | G | Reverse EF50 to 6BA6 procedure. |
| 6BD7 | 6AQ5 | G | Parallel circuits only. Change socket to miniature and rewire as follows: No. 1 on noval to No. 7 on miniature |
|  | 6AT6 | G |  |
|  | 6BF6 | G | 2 to 1 |
|  | 6 BT 6 | G | ®®® 3 to 2 |
|  | $6 \mathrm{BU6}$ | G |  |
|  |  |  | ORic. 5 to 4 |
|  |  |  | 6 to 6 |
|  |  |  | 8 to 6 |
| 6BE6 | 6 BA 7 | G | Change socket to nine pin noval and rewire as follows: <br> No. 1 on miniature to No. 2 on noval 2 to 3 |
|  |  |  |  |
|  |  |  |  |
|  |  |  | -(6) 3 to 4 |
|  |  |  |  |
|  |  |  | ORic. 5 to 9 Stict |
|  |  |  | 6 to 1 |
|  |  |  | 7 |
|  | 5915 | G | No changes. |
| 6BF5 | 6AQ5 | P | Parallel circuits only. No changes. |
|  | 6AR5 | P | Parallel circuits only. Short No. 7 to No. 1. |
| 6BF6 | 6BD7 | G | Parallel circuits only. Reverse 6BD7 to 6AQ6 procedure. |
|  | $6 \mathrm{BU6}$ | G | No changes. |
| 6BF7 | 6BG7 | E |  |
| 6BG6 | 6BQ6 | P | Parallel circuits only. Rewire as follows: |
|  |  |  | $\begin{array}{cl}\text { No. } 8 & \text { to No. } 4 \\ 3 & \text { to } \\ 8\end{array}$ |
|  |  |  |  |
|  | 6CD6 | P | Parallel circuits only. No changes. Sometimes it is necessary to increase wattage rating of screen resistor. |
| 6BG7 | 6BF7 | E | No changes. |
| 6BH6 | 6BJ6 | G | No changes. |
|  | 6AS6 | G | Parallel circuits only. No changes. |
|  | 6 BC 5 | P |  |
|  | 6C B6 | G |  |
| 6BJ6 | 6AS6 | G | Parallel circuits only. No changes. |
|  | 6 BC 5 | P |  |
|  | 6CB6 | G |  |

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| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6BJ6 | 6BH6 | G | No changes. |
| 6BK6 | 6AT6 | G | No changes. |
|  | 6 AV6 | G |  |
|  | 6BF6 | G |  |
|  | 6BT6 | G |  |
|  | 6BU6 | G |  |
| 6BN6 |  |  | No practical substitute. |
| 6BQ6 | 6AVJ | G | Parallel circuits only. Rewire as fullows: |
|  | 6 BD5 | G | No. 5 to No. 1 |
|  |  |  | 8 to 3 |
|  |  |  | cap to 5 |
|  |  |  | 4 to 8 |
|  | 6BG6 | P | Parallel circuits only. Rewire as follows: |
|  |  |  | No. $8 \quad$ to No. 3 |
|  |  |  | 4 to 8 |
|  | 6CD6 | P | Where extra filament current is available. Parallel circuits only. Rewire as follows: |
|  |  |  | No. 8 $\text { to No. } 3$ |
| 6BT6 | 6AQ6 | G | Parallel circuits oniy. No changes. |
|  | 6BD7 | G | Parallel circuits only. Reverse 6BD7 to 6AQ6 procedure. |
|  | 6BK6 | G | No changes. |
| 6BL6 | 6BD7 | G | Parallel circuits only. Reverse 6BD7 to 6AQ6 procedure. |
|  | 6BF6 | G | No changes. |
| € BY5 | 6AX5 | G | Parallel circuits only. Where No. 1 and Nc. 8 are connected rogether, change connections as follows: |
|  | 6W5 | G |  |
|  | 6 X 5 | G |  |
|  | $6 \mathrm{ZY5}$ | G | No. 4 to No. 3 |
|  | 1274 | G |  |
| 6 C 4 | 6AB4 | G | Rewire as follows: |

Connect No. 5 to No. 1

6J4 P Parallel circuits only. Rewire as follows:

| No. 7 | to No. 2 |
| :---: | :--- |
| 1 | to |
| 5 | to |







| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6G5 | $6 \mathrm{AB5}$ | G | Parallel circuits only. No changes. |
|  | 6E5 | G | No changes. |
|  | 6 T5 | G |  |
|  | 6 U 5 | G |  |
| 6G6 | 6A4/LA | G | Parallel circuits only. Reverse 6A4/LA to 6F6 procedure. |
|  | $6 \mathrm{F6}$ | G | Parallel circuits only. No changes. |
|  | 6 K 6 | G |  |
|  | 6V6 | G |  |
|  | 12A6 | P | Series circuits only. No changes. |
|  | 41 | G | Same as 6F6 to 42. Parallel circuits only. |
|  | 42 | G |  |
|  | 89 | G | Same as 6F6 to 89. Parallel circuits only. |
| 6H4 | 6H6 | G | Parallel circuits only. Rewire as follows: |

No. 4 to No. 3
Connect No. 3 and No. 5 together.
Connect No. 4 and No. 8 together.

| 6U5/6G5 | E |
| :--- | :--- |
| 6AL5 | G |
| 6W5 | P |
| 6X5 | P |
| 6ZY5 | P |
| 7A6 | E |
|  |  |
|  |  |
|  |  |
|  |  |
| $7 Y 4$ | $P$ |
| $7 Z 4$ | $P$ |

No practical substitute. Parallel circuits only. Rewire as follows:

| Nos. 1 and 5 | to | 6 |
| :---: | :---: | :---: |
| 7 | to | 1 |
| 2 | to | 7 |





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| 6C6 | G | Reverse 6C6 to 6J7 procedure. |
| :---: | :---: | :---: |
| 6D6 | E |  |
| 6D7 | G | Same as 6J7 to 6D7. |
| 6 E 7 | G |  |
| $6 \mathrm{J7}$ | G | No changes. |
| 6Q7 | P | Cut off pins No. 4 and No. 5. Emergency substitution. |
| 6S7 | G | Parallel circuits only. No changes. |
| 6SH7 | G | Same as 6J7 to 6SJ7. |
| 6SJ7 | G |  |
| 6SK7 | E |  |
| 6SS7 | G | Same as $12 \mathrm{K7}$ to 12SK7. Parallel circuits only. |
| 6U7 | G | No changes. |
| 6W7 | G | Parallel circuits only. No changes. |



|  |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :--- | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 6L6 | 6AL6 | G | Rewire as follows: |

Connect No. 3 to cap.





| 6S6-6SC7 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. P | PERF. | CIRCUIT CHANGES NECESSARY |
| 6S6 |  |  | No practical substitute. |
| 6SA7 | 7Q7 | G | Same as 12SA7 to 14Q7. |
|  | 6SB7Y | G | No changes. |
|  | 6SD7 | P | Same as 12SA7 to 12 SK 7. |
|  | 6SH7 | P |  |
|  | 6SK7 | P |  |
| 6S8GT |  |  | No practical substitute. |
| 6S7 | 6D6 | G | Parallel circuits only. Reverse 6C6 to 6J7 procedure. |
|  | 6D7 | G | Same as 6J7 to 6D7. Parallel circuits only. |
|  | 6E7 | G |  |
|  | $6 \mathrm{J7}$ | G | Parallel circuits only. No changes. |
|  | 6K7 | G |  |
|  | 6SJ7 | G | Parallel circuits only. Same as $12 \mathrm{K7}$ to 12SK7. |
|  | 6SK7 | G |  |
|  | 6SS7 | E | Same as 12 K 7 to 12 SK 7. |
|  | 6 U7 | G | Parallel circuits only. No changes. |
|  | 6W7 | G | No changes. |
|  | 7A7 | G | Parallel circuits only. Same as $12 \mathrm{K7}$ to 7B7. |
|  | $7 \mathrm{B7}$ | G | Same as 12 K 7 to 7B7. |
|  | 7C7 | G |  |
|  | 12 K 7 | P | Series circuits only. No changes. |
|  | 12 SK 7 | P | Series circuits only. Same as 12 K 7 to 12 SK 7. |
|  | 14A7/12B7 | P | Series circuits only. Same as 12 K 7 to $7 \mathrm{B7}$. |
|  | 39/44 | G | Parallel circuits only. Same as 6 K 7 to 39/44. |
|  | 77 | G | Parallel circuits only. Reverse 6C6 to 6 J 7 procedure. |
|  | 78 | G |  |
|  | 666 | G |  |
| 6SB7Y | 6BE6 | G | Change socket to miniature and rewire as follows: |
|  |  |  | No. 1 on octal to No. 2 on miniature <br> 2 to <br> 3  |
|  |  |  | (9) 3 (0) to 5 |
|  |  |  | (3) 4 (3) to 6 |
|  |  |  | (3) 5 (1) 5 to 1 |
|  |  |  | Onfic. 6 to 2 sue. |
|  |  |  | 7 to 4 |
|  |  |  | 8 to 7 |
| 6 SC 7 | 6C8 | G | Same as 6SC7 to 6F8. |




| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6SJ7 | 6D7 | G | Change socket to seven prong type and rewire as follows: |
|  | 6 E 7 | G | No. 2 on octal to No. 1 on seven prong |
|  |  |  | $3$ to $4$ |
|  |  |  |  |
|  |  |  |  |
|  |  |  | (10) 6 to 3 e |
|  |  |  | ORtG.O 7 to |
|  |  |  | 8 to 2 |
|  | 6J7 | E | Same as 12SK7 to $12 \mathrm{K7}$. |
|  | $6 \mathrm{K7}$ | G |  |
|  | 6U7 | G |  |
|  | 6S7 | G | Same as 12SK7 to $12 \mathrm{K7}$. Parallel circuits only. |
|  | 6W7 | G |  |
|  | 6SK7 | G | No changes. |
|  | 5693 | E |  |
|  | 6SS7 | G | Parallel circuits only. No changes. |
|  | 7A7 | G | Same as 12SJ7 to 7B7. |
|  | $7 \mathrm{B7}$ | G | Same as 12SJ7 to 7B7. Parallel circuits only. |
|  | 7C7 | G |  |
| 6SK7 | 6AB7 | G | Parallel circuits only. No changes. |
|  | 6AC7 | G |  |
|  | 6AH6 | G | Same as 6SK7 to 6AU6. Parallel circuits only. |
|  | 6AK6 | G |  |
|  | $6 \mathrm{AU6}$ | G | Change socket to miniature and rewire as follows: |
|  | 6BA6 | G | No. 2 on octal to No. 3 on miniature |
|  | 6BD6 | G | 3 to 2 |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  | 8 to 5 |
|  | 6 C 6 | G | Reverse 6C6 to 6SJ7 procedure. |
|  | 6D6 | E |  |
|  | 77 | G |  |
|  | 78 | E |  |
|  | 6D7 | G | Same as 6SJ7 to 6D7. |
|  | 6E7 | G |  |
|  | 6 J 7 | G |  |
|  | 6K7 | E | Same as 12 SK 7 to 12 K 7 . |
|  | $6 \mathrm{U7}$ | G |  |
|  | $6 \mathrm{S7}$ | G | Same as 12SK7 to 12K7. Parallel circuits only. |
|  | 6W7 | G |  |
|  | 6SG7 | G | No changes. |
|  | 6SH7 | G |  |
|  | 6SJ7 | G | No changes. |

6SK7-6SN7
TUBE
6SK7

6SL7

6SN7

| SUB. | PERF. |
| :--- | :---: |
| 6SS7 | G |
|  |  |
| 36 | G |
| $39 / 44$ | E |

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CIRCUIT CHANGES NECESSARY
Parallel circuits only. No changes.
Change socket to five prong and rewire as follows:
No. 2 on octal to No. 1 on five prong 3 and 5 to 4 4 6 7 8


7A7 E Same as 12SJ7 to 7B7.
7B7 E Same as 12SJ7 to 7B7. Parallel circuits only.
7 C 7
G
2C21 P
6C8 G
6F8
G Make adaptor as follows:

| No. 1 on base | to | cap on top |
| :--- | :--- | :--- |
| 2 | to | 3 |
| 3 | to | 4 |
| 4 | to | 5 |
| 5 | to | 6 |
| 6 | to | 8 |
| 7 | to | 7 |
| 8 | to | 2 |

6SC7 G If the 6SL7 employs the two cathodes separately this substitution may be
G If the 6SL7 employs the two cathodes separately
6SN 7 G Parallel circuits only. No changes.
6SU7
7F7

6F8
6SC7
6SL7
757
G No changes.
G Change socket to loctal and rewire as follows:

|  | No. 1 on octal | to No. | 4 on loctal |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 | to | 3 |  |
| (0) | 3 | to | 2 | (9) 3 |
| (3) ${ }^{(3)}$ | 4 | to | 5 | (3) ${ }^{3}$ |
| (3) | 5 | to | 6 | (2) 0 |
| onic. | 6 | to | 7 | sue. |
|  | 7 | to | 1 |  |
|  | 8 | to | 8 |  |

G Same as 6SL7 to 7F7. Parallel circuits only.
E No changes.
P
G Reverse 2C21 to 6SN7 procedure.
G Same as 6SL7 to 6F8. Parallel circuits only.
G Reverse 6SC7 to 6SL7 procedure. Parallel circuits only.
G Parallel circuits only. No changes.
G Same as 6SL7 to 7F7. Parallel circuits only.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6SN7 | 7F8 | G | Parallel circuits only. Change socket to loctal and rewire as follows: $\begin{array}{ll}\text { No. } 1 \text { on octal } & \text { to No. } 1 \text { on loctal } \\ 2 & \text { to } \\ 3\end{array}$ |  |  |
|  |  |  | (0) 3 | to 4 |  |
|  |  |  |  | to 8 |  |
|  |  |  | (3) 0 <br> 5 | to 6 |  |
|  |  |  |  | to 5 |  |
|  |  |  | 7 | to 7 |  |
|  |  |  | 8 | to 2 |  |
|  | 5691 | P | No changes. |  |  |
|  | 5692 | G |  |  |  |  |
| 6SQ7 | 6AQ6 | G | Same as 6SQ7 to 6AT6. Parallel circuits only. |  |  |
|  | 6AT6 | G | Change socket to miniature and rewire as follows: |  |  |
|  | 6AV6 | G | No. 2 on octal | to No. 1 on miniature |  |
|  | 6BF6 | G | 3 to | to 2 |  |
|  | 6BK6 | G | (0) (3) 4 | to 5 |  |
|  | 6BT6 | G | $5$ | to 6 |  |
|  | 6BU6 | G | 0 | to 7 |  |
|  |  |  | onic. 7 to | to 4 |  |
|  |  |  | 8 to | 3 |  |
|  | 6B6 | G | Make adaptor as follows: |  |  |
|  |  |  | No. 1 on base to | to No. 1 on top to cap |  |
|  |  |  | 2 to |  |  |  |
|  |  |  | 3 to | 8 |  |
|  |  |  | 4 to | 4 |  |
|  |  |  | 5 to | 5 |  |
|  |  |  | 7 to | 7 |  |
|  |  |  | 8 to | 2 |  |
|  | 6 C 7 | G | Change socket to seven prong and rewire as follows: |  |  |
|  |  |  | No. 2 on octal to | to cap on seve | prong |
|  |  |  | (9) 3 to | to 6 | $\left(\begin{array}{ccc} 0_{3} & 8^{6} \\ 0_{2} & 8 \\ 0 & 70 \\ 0 & 0 \end{array}\right)$ |
|  |  |  | (3) (3) 4 - ${ }^{\text {a }}$ | to 4 |  |
|  |  |  | (2) 5 5 to | to 5 |  |
|  |  |  | Onl6. 6 to | to 2 |  |
|  |  |  | 7 to | to 1 |  |
|  |  |  | 8 to | - 7 |  |
|  | 6Q7 | E | Same as 6SQ7 to 6B6. |  |  |
|  | 6R7 | G | Same as 6SQ7 to 6B6. |  |  |
|  | 6SR7 | G | No changes. |  |  |
|  | 6ST7 | G | Parallel circuits only. No changes. |  |  |
|  | 6 T 7 | G | Same as 6SQ7 to 6B6. Parallel circuits only. |  |  |
|  | 6 V 7 | G |  |  |  |  |  |  |
|  | 7B6 | E | Change socket to loctal and rewire as follows: |  |  |
|  | 7E6 | G | No. 2 on octal | to No. 3 on loctalto 4 or 7 | $\cdots$ |
|  |  |  |  |  |  |
|  |  |  |  | to 5 |  |
|  |  |  |  | to 6 |  |
|  |  |  |  | to 2 |  |
|  |  |  |  | to 1 |  |
|  |  |  |  | to 8 |  |



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| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6ST7 | 6SQ7 | G | Parallel circuits only. No changes. |
|  | 6SR7 | G |  |
|  | 6 T 7 | E | Same as 6SQ7 to 6B6. |
| 6 6U7 | 6SL7 | E | No changes. |
|  | 6SN7 | P |  |
| 6SV7 | 6SF7 | G | No changes. |
| 6SZ7 | 6SQ7 | G | Parallel circuits only. No changes. |
|  | 6SR7 | G |  |
|  | 6ST7 | G | No changes. |
| 6 T 5 | 2E5 | E | Heater voltage-current ratings differ. |
|  | 6AB5 | G | Parallel circuits only. No changes. |
|  | 6E5 | G | No changes. |
|  | 6G5 | G |  |
|  | 6 U5 | G |  |
| 6 T 6 |  |  | No practical substitute. |
| 6 T 7 | 6B6 | G | Parallel circuits only. No changes. |
|  | 6Q7 | G | Parallel circuits only. No changes. |
|  | 6R7 | G |  |
|  | 6SQ7 | G | Same as 12Q7 to 12SQ7. Parallel circuits only. |
|  | 6ST7 | E | Same as 12Q7 to 12SQ7. |
|  | $6 \mathrm{V7}$ | G | Parallel circuits only. No changes. |
|  | $7 \mathrm{B6}$ | G | Same as 6Q7 to 7B6. Parallel circuits only. |
|  | 7 C 6 | G | Same as 6Q7 to 7B6. |
|  | 12Q7 | P | Series circuits only. No changes. |
|  | 12SQ7 | P | Same as 12Q7 to 12SQ7. Series circuits only. |
|  | 75 | G | Same as 6Q7 to 75. Parallel circuits only. |
|  | 85 | G |  |
| 6T8* | 6R8 | G | No changes. |
| $6 \mathrm{U4}$ | 6W4 | E | No changes. |
| 6U5/6C5 | 6N5 | E | Parallel circuits only. No changes. |
| 6U5/6G5 | 2E5 | E | Heater voltage-current ratings differ. |
|  | 6E5 | E | No changes. |
| 6U6 | 6A4/LA | $P$ | Parallel circuits only. Reverse 6A4/LA to 6F6 procedure. |
|  | 6AR6 | P | Where additional filament current is available. Reverse 6AR6 to 6F6 procedure. |


| 6U6-6V6 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 6 U6 | $6 \mathrm{F6}$ | G | Parallel circuits. No changes. |
|  | 6G6 | P |  |
|  | 6 K 6 | G |  |
|  | 6L6 | P |  |
|  | 6V6 | G |  |
|  | 6W6 | P |  |
| 6 U7 | 6 AU6 | G | Same as 6K7 to 6AU6. |
|  | 6BA6 | G |  |
|  | 6BD6 | G |  |
|  | 6C6-77 | G | Reverse 6C6 to 6J7 procedure. |
|  | 6D6-78 | G |  |
|  | 6D7 | G | Same as 6J7 to 6D7. |
|  | 6E7 | G |  |
|  | 6K7 | G | No changes. |
|  | 6 67 | G | Same as 6J7 to 6SJ7. |
|  | 6SH7 | G |  |
|  | 6SJ7 | G |  |
|  | 6SK7 | G |  |
|  | 6SS7 | G |  |
|  | 6W7 | G |  |
|  | 7A7 | G | Same as 6K7 to 7A7. |
|  | 7B7 | G | Same as 6K7 to 7A7. Parallel circuits only. |
|  | 7C7 | G |  |
|  | 7G7 | G |  |
|  | 36 | G | Same as 6 K 7 to 39/44. |
|  | 39/44 | G |  |
| 6V4 | 6X4 | E | Reverse 6X4 to 6V4 procedure. |
|  | 6X5 | G | Where space permits, reverse 6X5 to 6V4 procedure. |
| 6 V 6 | 6A4/LA | P | Parallel circuits only. Reverse 6A4/LA to 6F6 procedure. |
|  | $6 \mathrm{AD7}$ | G | Parallel circuits only. Remove and tape up any wires anchored on pins Nos. 1 and 6. |
|  | 6AQ5 | G | Reverse 6AQ5 to 6V6 procedure. |
|  | 6AR6 | P | Where additional filament current is available. Reverse 6AR6 to 6F6 procedure. |
|  | 6F6 | G | Parallel circuits only. No changes. |
|  | 6G6 | P |  |
|  | 6K6 | G |  |
|  | 6 L 6 | G | Parallel circuits only. No changes. |
|  | 6 U6 | G |  |
|  | 6 Y 6 | G |  |
|  | 7A5 | G | Parallel circuits only. Remove and tape up any wires anchored on pins Nos. 1 and 6. |


|  |  |  | RECEIVING TUBE SUBSTITUTION GUIDE 6V6-6W7 |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUT CHANGES NECESSARY |
| 6V6 | 7B5 | G | Same as 6K6 to 7B5. |
|  | $7 \mathrm{C5}$ | G |  |
|  | 38 | G | Same as 6F6 to 38. Parallel circuits only. |
|  | 41 | G | Same as 6F6 to 41. Parallel circuits only. |
|  | 42 | G |  |
|  | 89 | G | Same as 6F6 to 89. Parallel circuits only. |
| 6V7 | 6C7 | G | Same as 6Q7 to 6C7. |
|  | 6R7 | G | No changes. |
|  | 6SQ7 | G | Same as 12 Q 7 to 12 SQ 7 . |
|  | 6SR7 | G |  |
|  | 6T7 | G | Parallel circuits only. No changes. |
|  | $7 \mathrm{B6}$ | G | Same as 6Q7 to 7B6. |
|  | 7C6 | G | Same as 6Q7 to 7B6. Parallel circuits only. |
|  | 7E6 | G | Same as 6Q7 to 7B6. |
|  | 75 | G | Same as 6Q7 to 75. |
|  | 85 | G |  |
| 6W4 | $6 \mathrm{U4}$ | E | No changes. |
| 6W5 | 024 | G | No changes. Do not use where AC plate voltage exceeds 250 volts per plate. |
|  | 6AX5 | G | Parallel circuits only. No changes. |
|  | 6AX6 | E | Parallel circuits only. Tie No. 4 and No. 8 together. |
|  | 6BY5 | G | Parallel circuits only. Rewire as follows: |
|  |  |  | Connect Nos. 1 and 8 together No. 3 to No. 4 |
|  | 6X5 | G | Parallel circuits only. No changes. |
|  | $6 \mathrm{EY5}$ | G |  |
|  | 626 | G | Parallel circuits only. Short Nos. 4 and 8. |
|  | $7 \mathrm{Y4}$ | G | Same as 6X5 to 7Y4. |
|  | 7 74 | G |  |
|  | 1274 | G | No changes. Parallel circuits only. |
| 6W6 | 6AR6 | G | Reverse 6AR6 to 6F6 procedure. |
|  | 6L6 | G | Parallel circuits only. No changes. |
| 6W7 | $\begin{aligned} & 6 \mathrm{C} 6-77 \\ & 6 \mathrm{D} 6-78 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Reverse 6C6 to 6J7 procedure. |
|  | $\begin{aligned} & \text { 6D7 } \\ & \text { 6E7 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 6J7 to 6D7. Parallel circuits only. |



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6 X 5 | 6W5 | G | Parallel circuits only. No changes. |
|  | 6X4 | G | Reverse 6X4 to 6X5 procedure. |
|  | $6 Y 5$ | E | Parallel circuits only. Change socket to six prong and rewire as follows: |
|  | 074 | E | No changes. Do not use where AC plate voltage exceeds 250 volts per plate. |
|  | 675 | G | Same as 6X5 to 6Y5. Parallel circuits only. |
|  | 6Z6 | G | Same as 6W5 to 6Z6. |
|  | 6ZY5 | G | Parallel circuits only. No changes. |
|  | 7 Y 4 | E | Parallel circuits only. Change socket to loctal and rewire as follows: |
|  | $7 \mathrm{Z4}$ | G | Same as 6X5 to 7Y4. |
|  | 84 | E | Change socket to five prong and rewire as follows: |
|  | 1274 | G | Parallel circuits only. No changes. |
| 6X6G |  |  | No practical substitute. |
| 6Y3G |  |  | No practical substitute. |
| $6 \mathrm{Y5}$ | $6 \times 5$ | G | Parallel circuits only. Reverse 6X5 to 6Y5 procedure. |
|  | 625 | G | Rewire as follows: |

Connect Nos. 2 and 6 together.

| 6AR6 | G | Reverse 6AR6 to 6F6 procedure. |
| :--- | :--- | :--- |
| 6G6 | P | Parallel circuits only. No changes. |
| 6K6 | $G$ |  |
| 6L6 | $G$ |  |
| 6U6 | $G$ |  |
| 6V6 | $G$ |  |
| 7A5 | $G$ | Same as 6K6 to 7B5. Parallel circuits only. |
| 7B5 | $G$ | Same as 6K6 to 7B5. Parallel circuits only. |
| 7C5 | $G$ |  |

6Y7-6ZY5

| TUBE | SUB. | PERF. |
| :---: | :---: | :---: |
| $6 \mathrm{YF}^{*}$ | 6 A 6 | G |

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## CIRCUIT CHANGES NECESSARY

Change socket to seven prong and rewire as follows:
No. 2 on octal to No. 1 on seven prong


3
4
5
6
7
8

G Parallel circuits only. No changes.
6N7

623
$6 Z 4$
路
$6 \mathrm{Z7}$

6 ZY 5

E No changes.
G Parallel circuits only. Change socket to six prong and rewire as follows:


No. 1 on five prong
2
3
4
5
to No. 1 on six prong to 3
to 5
to 4
to 6


E No changes for six volt operation.
G Same as 6Y7 to 6A6. Parallel circuits only.
G Parallel circuits only. No changes.

G
627
1 V
6 Y 5

6 Y5
6A6
6N7
6 Y7
$0 \mathrm{Z4}$
6AX5
6AX6
6BY5

6W5
6X5
6 Y5
6Z5
7 Y4
$7 Z 4$
84 G
1274
G

G

G
G

G

G

625

W5 G Parallel circuits only. No changes.
X5 G Parallel circuits only. No changes.
Y5 G Same as 6X5 to 6Y5. Parallel circuits only.

G Same as 6X5 to 7Y4. Parallel circuits only.
G Parallel circuits only. Tie Nos. 4 and 8 together.
G Parallel circuits only. Rewire as follows:
Connect Nos. 1 and 8 together
No. 3 to No. 4

Same as 6 X 5 to 84. Parallel circuits only.
Parallel circuits only. No changes.


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Connect wires removed from No. 8 to No. 7
Connect No. 4 and No. 7 together.

RECEIVING TUBE SUBSTITUTION GUIDE

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 7AB7 | 1204 | E | No changes. |
| 7AD7 | 7AG7 | P | Parallel circuits only. No changes. |
|  | 7AH7 | P |  |
|  | 7AJ7 | P |  |
|  | 7AK7 | P |  |
|  | 7B7 | P |  |
|  | 7C7 | P |  |
|  | 7G7 | P |  |
|  | 7H7 | P |  |
|  | 7L7 | P |  |
|  | 7T7 | P |  |
|  | 7V7 | P |  |
| 7AF7 | 7F7 | G | No changes. |
|  | 7N7 | G | Parallel circuits only. No changes. |
| 7AG7 | $7 \mathrm{AH7}$ | G | No changes. |
|  | 7B7 | P |  |
|  | 7C7 | P |  |
|  | 7AJ7 | P | Parallel circuits only. No changes. |
|  | $7 \mathrm{AK7}$ | P |  |
|  | 7G7 | G |  |
|  | 7H7 | G |  |
|  | 7 L 7 | G |  |
|  | $7 \mathrm{T7}$ | G |  |
|  | 7V7 | G |  |
| 7AH7 | 7AG7 | G | No changes. |
|  | 7B7 | P |  |
|  | 7C7 | P |  |
|  | 7AJ7 | G | Parallel circuits only. No changes. |
|  | $7 \mathrm{AK7}$ | P |  |
|  | 7G7 | P |  |
|  | 7H7 | P |  |
|  | 7L7 | P |  |
|  | 7 T 7 | P |  |
|  | 7V7 | P |  |
| 7AJ7 | $7 \mathrm{AH7}$ | G | Parallel circuits only. No changes. |
|  | 7AK7 | P |  |
|  | 7 B 7 | P |  |
|  | 7 C 7 | P |  |
|  | 7G7 | P |  |
|  | $7 \mathrm{V7}$ | P |  |
|  | 7H7 | P | No changes. |
|  | 7L7 | P |  |
|  | 7T7 | P |  |
| 7AK7 | 7AH7 | P | Parallel circuits only. No changes. |
|  | 7AJ7 | P |  |
|  | 7B7 | P |  |
|  | 7 C 7 | P |  |
|  | 7G7 | P |  |
|  | 7H7 | P |  |
|  | 7L7 | P |  |
|  | 7T7 | P |  |
|  | $7 \mathrm{V7}$ | P |  |


| 7B4-7B7 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| $7 \mathrm{B4}$ | 6AD5 | G | Reverse 6J5 to 7A4 procedure. |
|  | 6AE5 | G |  |
|  | 6 F 5 | G | Change socket to octal and rewire as follows. |
|  | 6 J 5 | G | Reverse 6J5 to 7A4 procedure. |
|  | $6 \mathrm{K5}$ | G | Reverse 6 K 5 to 7B4 procedure. |
|  | 6 P5 | G | Reverse 6J5 to 7A4 procedure. |
|  | 7A4 | G | No changes. |
|  | XXL | G |  |
| 7B5 | $6 \mathrm{AD7}$ | G | Parallel circuits only. Reverse 6K6 to 7B5 procedure. Remove and tape up any wires anchored on unused pins. |
|  | $6 \mathrm{F6}$ | G | Parallel circuits only. Reverse 6K6 to 7B5 procedure. |
|  | 6 K 6 | E | Reverse 6K6 to 7C5 procedure. |
|  | $6 \mathrm{L6}$ | G | Parallel circuits only. Reverse 6K6 to 7B5 procedure. |
|  | 6 66 | G |  |
|  | 6V6 | G |  |
|  | 6 Y 6 | G |  |
|  | $7 \mathrm{A5}$ | G | Parallel circuits only. No changes. |
|  | 7C5 | G |  |
|  | 41 | G | Change socket to six prong and rewire as follows: |
|  | 42 | E | No. 1 on loctal to No. 1 on six prong |
|  |  |  |  |
|  |  |  | 8 to 6 |
| $7 \mathrm{B6}$ | 6B6 | E | Reverse 6B6 to 7B6 procedure. |
|  | 6Q7 | E | Reverse 6Q7 to 7B6 procedure. |
|  | 6R7 | G |  |
|  | 6SQ7 | E | Reverse 6SQ7 to 7B6 procedure. |
|  | 6 T 7 | G | Parallel circuits only. Reverse 6Q7 to 7B6 procedure. |
|  | 7C6 | G | Parallel circuits only. No changes. |
|  | 7E6 | G | No changes. |
|  | 75 | E | Reverse 75 to 7E6 procedure. |
|  | 85 | G | Reverse 75 to 7E6 procedure. |
| 7B7 | 6C6 6D6 | G | Parallel circuits only. Reverse 6C6 to 7A7 procedure. |


|  |  |  | RECEIVING TUBE SUBSTITUTION GUIDE | 787-7c4 |
| :---: | :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |  |
| 7B7 | 6D7 | G | Same as 7A7 to 6D7. Parallel circuits only. |  |
|  | 6E7 | G |  |  |
|  | 6.57 | G | Parallel circuits only. Reverse 6J7 to 7L7 procedure. |  |
|  | 6K7 | G | Parallel circuits only. Reverse 6K7 to 7A7 procedure. |  |
|  | 6S7 | G | Reverse 6K7 to 7A7 procedure. |  |
|  | 6SH7 | G | Parallel circuits only. Reverse 12SJ7 to 7B7 procedure. |  |
|  | 6SJ7 | G |  |  |
|  | 6SK7 | G |  |  |
|  | 6SS7 | G | Reverse 12SJ7 to 7B7 procedure. |  |
|  | 6U7 | G | Parallel circuits only. Reverse 6K7 to 7A7 procedure. |  |
|  | 6W7 | G | Reverse 6K7 to 7A7 procedure. |  |
|  | 7 A 7 | G | Parallel circuits only. No changes. |  |
|  | $7 \mathrm{C7}$ | G | No changes. |  |
|  | $7 \mathrm{H7}$ | G | Parallel circuits only. No changes. |  |
|  | 12 J 7 | P | Series circuits only. Reverse 6 K 7 to 7A7 procedure. |  |
|  | $12 \mathrm{K7}$ | P |  |  |
|  | 12SG7 | P | Series circuits only. Reverse 12SJ7 to 7B7 procedure. |  |
|  | 12SH7 | P |  |  |
|  | 12SJ7 | P |  |  |
|  | 12SK7 | P |  |  |
|  | 14A7/12B7 | P | Series circuits only. No changes. |  |
|  | 39/44 | G | Same as 7A7 to 39/44. Parallel circuits only. |  |
|  | 77 | G | Parallel circuits only. Reverse 6C6 to 7A7 procedure. |  |
|  | 78 | G |  |  |
| $7 \mathrm{B8}$ | 6 A 7 | G | Reverse 6A7 to 7B8 procedure. |  |
|  | 6 A 8 | G | Reverse as 12A8 to 14B8 procedure. |  |
|  | 6D8 | G | Parallel circuits only. Reverse 12A8 to 14B8 procedure. |  |
|  | 6 J 8 | E | Reverse 12A8 to 14B8 procedure. |  |
|  | 6 K 8 | E |  |  |
|  | 7A8 | G | Parallel circuits only. No changes. |  |
|  | 737 | G | No changes. |  |
|  | 757 | G | No changes. |  |
| 7 C 4 | 1203A | E | No changes. |  |
|  | 9006 | G | Change socket to miniature and rewire as follows: |  |
|  |  |  | No. 1 on loctal <br> to No. 3 on miniatu |  |
|  |  |  | 101 |  |

705-7c7

TUBE
7 C 5 $7 C 6$

7C7

PERF.
RECEIVING TUBE SUBSTITUTION GUIDE
SUB. 6AD7 6F6 6G6 6 K 6 6L6 6U6 6V6 6Y6 7A5

## 7B5

41
42
6B6 6Q7 6R7 6SQ7 6ST7 6 T 7 7B6 12Q7 12SQ7 $12 S R 7$
14B6 P 14E6 75 85 6 C 6 6D6 77 78

G

G G G G G E G

G
G Parallel circuits only. No changes.
G G

G G G

G Parallel circuits only. Reverse 6SQ7 to 7B6 procedure.
G Reverse 6SQ7 to 7B6 procedure.
G
G Parallel circuits only. No changes.
P Series circuits only. Reverse 6Q7 to 7B6 procedure.
P Series circuits only. Reverse 6SQ7 to 7B6 procedure.
P
$\mathbf{P}$
P

G
G

G
G
G
G
G
G
G Reverse 6K7 to 7A7 procedure.
G Reverse 12SJ7 to 7B7 procedure.
G Reverse 6K7 to 7A7 procedure.
G Parallel circuits only. No changes.
G No changes.
G Parallel circuits only. No changes.

| TUBE | RECEIVING TUBE SUBSTITUTION GUIDE |  |  |
| :---: | :---: | :---: | :---: |
|  | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 7 C 7 | 12 J 7 | P | Series circuits only. Reverse 6K7 to 7A7 procedure. |
|  | 12 K 7 | P |  |
|  | 12SG7 | P | Series circuits only. Reverse 12SJ7 to 7B7 procedure. |
|  | 12SH7 | P |  |
|  | 12SJ7 | P |  |
|  | 12SK7 | P |  |
|  | 14A7/12B7 | P | Series circuits only. No changes. |
|  | 36 | G | Same as 7A7 to 39/44. Parallel circuits only. |
|  | 39/44 | G |  |
| 7D7 |  |  | No practical substitute. |
| 7E5 | 7 A 4 | P | Parallel circuits only. Rewire as follows: |
|  | 7B4 | P | Remove wires from No. 1 |
|  |  |  | No. 2 l $\begin{aligned} & \text { 2 and } 7\end{aligned}$ |
|  |  |  | 4 and $6 \quad$ to $\quad 7$ |
|  |  |  | 5 to 6 |
|  |  |  | Connect wires removed from No. 1 to No. 6 |
|  | 1201 | E | No changes. |
| 7E6 | 6B6 | G | Reverse 6Q7 to 7B6 procedure. |
|  | 6Q7 | G |  |
|  | 6R7 | G | Reverse 6Q7 to 7B6 procedure. |
|  | 6SQ7 | G | Reverse 6SQ7 to 7B6 procedure. |
|  | 6SR7 | G | Reverse 6SQ7 to 7B6 procedure. |
|  | 6 T7 | G | Parallel circuits only. Reverse 6Q7 to 7B6 procedure. |
|  | 75 | G | Reverse 75 to 7E6 procedure. |
|  | 85 | G | Reverse 75 to 7E6 procedure. |
|  | $7 \mathrm{B6}$ | G | No changes. |
|  | 7C6 | G | Parallel circuits only. No changes. |
| 7 E 7 | 6B8 | G | Reverse 6B8 to 7E7 procedure. |
|  | 7R7 | G | No changes. |
| 7F7 | 6 C 8 | G | Reverse 6C8 to 7F7 procedure. |
|  | $6 \mathrm{F8}$ | G | Parallel circuits only. Reverse 6C8 to 7F7 procedure. |
|  | 6SC7 | G | Reverse 6SC7 to 7F7 procedure. |
|  | 6SL7 | G | Reverse 6SL7 to 7F7 procedure. |
|  | 7AF7 | G | No changes. |
|  | 7F8 | G | Reverse 7F8 to 7F7 procedure. |
|  | 7N7 | G | Parallel circuits only. No changes. |



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 7K7 | $7 \mathrm{B6}$ | G | Rewire as follows: |
|  | 7E6 | G | No. 2 to No. 7 |
|  |  |  | 3 to 2 |
|  |  |  | 4 to 3 |
|  | 7X7 | G | Rewire as follows: |
|  |  |  | Remove wires from No. 2 |
|  |  |  | No. 3 to No. 2 <br> 4 to 3 |
|  |  |  | Connect wires removed from No. 2 to No. 4 |
| $7 \mathrm{L7}$ | $6 \mathrm{J7}$ | G | Reverse 6J7 to 7L7 procedure. |
|  | $6 \mathrm{K7}$ | G | Reverse 6K7 to 7A7 procedure. |
|  | 7A7 | G | No changes. |
|  | 7G7 | G | Parallel circuits only. No changes. |
|  | 7H7 | G | No changes. |
|  | 7T7 | G | No changes. |
|  | 7V7 | G | Parallel circuits only. No changes. |
| 7N7 | 6C8 | G | Parallel circuits only. Reverse 6C8 to 7F7 procedure. |
|  | 6F8 | G | Reverse 6C8 to 7F7 procedure. |
|  | 7AF7 | G | Parallel circuits only. No changes. |
|  | 7F7 | G | Parallel circuits only. No changes. |
| 7Q7 | 6SA7 | G | Reverse 12SA7 to 14Q7 procedure. |
| 7R7 | 7 E 7 | G | No changes. |
| 7S7 | 6 A 7 | G | Reverse 6A7 to 7B8 procedure. |
|  | 6A8 | G |  |
|  | 6 J 8 | G | Reverse 6J8 to 7J7 procedure. |
|  | 6 K 8 | G |  |
|  | 7B8 | G | No changes. |
|  | 7J7 | G |  |
| $7 \mathrm{T7}$ | 7A7 | G | No changes. |
|  | 7B7 | G | Parallel circuits only. No changes. |
|  | 7C7 | G | Parallel circuits only. No changes. |
|  | 7G7 | G | Parallel circuits only. No changes. |
|  | $7 \mathrm{H7}$ | G | No changes. |
|  | $7 \mathrm{L7}$ | G | No changes. |
|  | 7V7 | G | No changes. |
|  | 1231 | G | Parallel circuits only. No changes. |



## RECEIVING TUBE SUBSTITUTION GUIDE



| 12AT6-12AY7 |  | RECEIVING TUBE SUBSTITUTION GUIDE |  |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 12AT6 | $12 \mathrm{AV6}$ | G | No changes. |
|  | 12BF6 | P |  |
|  | 12BK6 | G |  |
|  | 12BT6 | P |  |
|  | $12 \mathrm{BU} 6$ | P |  |
|  | 12SQ7 | G | Where space permits. Reverse 12SQ7 to 12AT6 procedure. |
|  | 12 SR 7 | P |  |
|  | 12SW 7 | P |  |
| $12 \mathrm{AT7}$ * | 12 AH 7 | G | Where space permits. Reverse 12AH7 to 12AT7 procedure. |
|  | $12 \mathrm{AU7}$ | G | No changes. |
|  | 12AV7 | G | Parallel circuits only. No changes. |
|  | $12 \mathrm{AX7}$ | G | No changes. |
|  | 12AY7 | G |  |
|  | 12 BH 7 | G | Parallel circuits only. No changes. |
| 12AU6 | 12AW6 | G | Reverse Nos. 2 and 7. |
|  | 12 BA 6 | G | No changes. |
|  | 12BD6 | G |  |
| 12AU7* | 12AT7 | G | No changes. |
|  | 12AV7 | G | Parallel circuits only. No changes. |
|  | 12AX7 | G | No changes. |
|  | $12 \mathrm{AY7}$ | G |  |
| 12AV6 | 12 AT 6 | G | No changes. |
|  | 12BF6 | P |  |
|  | 12 BK 6 | G |  |
|  | 12BT6 | G |  |
|  | $12 \mathrm{BU6}$ | G |  |
| 12AV7 | 12AT7 | G | Parallel circuits only. No changes. |
|  | $12 \mathrm{AU7}$ | G |  |
|  | $12 \mathrm{AX7}$ | G |  |
|  | $12 \mathrm{AY7}$ | G |  |
|  | 12 BH 7 | G |  |
| 12AW6 | 12AU6 | G | Rewire as follows: |
|  | 12 BA 6 | G | Reverse No. 2 and No. 7 |
| 12AX7 | 12AT7 | G | No changes. |
|  | 12AU7 | G |  |
|  | 12AV7 | G | Parallel circuits only. No changes. |
|  | 12AY7 | G | No changes. |
|  | 12 BH 7 | G | Parallel circuits only. No changes. |
| 12AY7 | 12AT7 | G | No changes. |
|  | 12AU7 | G |  |
|  | $12 \mathrm{AV7}$ | G | Parallel circuits only. No changes. |



12BU6-12K7

| TUBE | SUB. | PERF. |
| :--- | :--- | :---: |
| 12BU6 | 12AT6 | $\mathbf{P}$ |
|  | 12AV6 | P |
|  | 12 BF 6 | $\mathbf{G}$ |
|  | 12 BK 6 | $\mathbf{P}$ |
|  | 12 BT 6 | $\mathbf{P}$ |
| 12C8 |  |  |
|  | 14 E 7 | G |
|  | $14 R 7$ | G |

$12 \mathrm{K7}$
14 A 7 E

1626

12 J 5
$12 S F 5$

12AL5

12 F 5
$12 S F 5$

14 A4

1626

6S7
6W 7

7 B7
7C7
12B7
$12 \mathrm{K7}$

12SG7
12SH7
12SJ7
12SK7

6S7

P P

P
E
G
G
G
E
$\mathbf{G}$

E
P

RECEIVING TUBE SUBSTITUTION GUIDE

## CIRCUIT CHANGES NECESSARY

No changes.

Change socket to loctal and rewire as follows: No. 2 on octal to No. 1 on loctal

| 3 | to | 2 |
| :--- | :--- | :--- |
| 4 | to | 3 |
| 5 | to | 4 |
| 6 | to | 5 |
| 7 | to | 8 |
| 8 | to | 7 |
| cap | to | 6 |

Parallel circuits only. No changes.
Rewire as follows:
No. 4 to No. 3. Connect grid wire to No. 5.
Same as 6F5 to 6SF5.
No practical substitute.
Change socket to miniature and rewire as follows:
No. 2 on octal to No. 3 on miniature


| 3 | to | 2 | 5 |
| :--- | :--- | :--- | :--- |
| 4 | to | 5 | es) |
| 5 | to | 7 | 0 |
| 7 | to | 4 |  |
| 8 | to | 1 |  |

G Rewire as follows:
No. 3
to No. 4
Connect wire from No. 5 to grid cap.
G Same as 12SF5 to 12J5.

G Same as 6J5 to 7A4.
Parallel circuits only. No changes.
Series circuits only. No changes.

Same as 12 K 7 to $7 \mathrm{B7}$ but in series circuits only.

Same as 12 K 7 to 787 but in series circuits only.
Series circuits only. No changes.

RECEIVING TUBE SUBSTITUTION GUIDE



## 12SA7-12SC7

## RECEIVING TUBE SUBSTITUTION GUIDE

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 12SF5 | 12 F 5 | G | Reverse 6F5 to 6SF5 procedure. |
|  | 12 J 5 | G | Rewire as follows: <br> Reverse No. 2 and No. 8 <br> Reverse No. 3 and No. 5 |
| 12SF7 | 12SK7 <br> and Germanium Diode | P | Rewire as follows: $\begin{aligned} & \text { Move wire from No. } 2 \text { to No. } 4 \\ & 6 \text { to } 8 \\ & 8 \text { to } \quad 2 \\ & 4 \text { to } 6 \\ & \text { Remove wires from No. } 5 \\ & \text { Connect No. } 3 \text { and No. } 5 \text { together } \\ & \text { Diode crystal from No. } 3 \text { or } 5 \text { to wires } \\ & \text { removed from No. } 3 \end{aligned}$ |
| 12SG7 | 12AU6 12BA6 12BD6 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Change socket to miniature and rewire as follows: |
|  | $\begin{aligned} & \text { 12SH7 } \\ & \text { 12SJ7 } \\ & \text { 12SK7 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
| 12SH7 | $\begin{aligned} & \text { 12AU6 } \\ & \text { 12BA6 } \\ & \text { 12BD6 } \end{aligned}$ | G | Same as 12SG7 to 12BA6. |
|  | $\begin{aligned} & \text { 12SG7 } \\ & \text { 12SJ7 } \\ & \text { 12SK7 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
| $12 \mathrm{SJ7}$ | $\begin{aligned} & \text { 6S7 } \\ & 6 \mathrm{~W} 7 \end{aligned}$ | $\begin{aligned} & \mathbf{P} \\ & \mathbf{P} \end{aligned}$ | Same as 12SK7 to 12K7. Series circuits only. |
|  | $\begin{aligned} & 12 \mathrm{~B} 7 \\ & 14 \mathrm{~A} 7 \\ & 14 \mathrm{C} 7 \end{aligned}$ | $\mathbf{G}$ | Change socket to loctal and rewire as follows: |
|  | $\begin{aligned} & 12 \mathrm{~J} 7 \\ & 12 \mathrm{~K} 7 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 12SK7 to 12K7. |
| 12SK7 | $\begin{aligned} & \text { 6S7 } \\ & 6 \mathrm{~W} 7 \end{aligned}$ | $\begin{aligned} & \mathbf{P} \\ & \mathbf{P} \end{aligned}$ | Same as 12SK7 to 12K7. Series circuits only. |
|  | 6SS7 | P | No changes. Series circuits only. |

12SK7-12SQ7



| 14A5-14E7 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 14A5 | 12A6 | E | Reverse 35L6 to 35A5 procedure. |
|  | 1284 | P | No changes. Connect No. 4 to No. 7 for best results. |
| 14A7/12B7 | 6 S 7 | P | Reverse $12 \mathrm{K7}$ to 7B7 procedure. Series circuits only. |
|  | 6W7 | P |  |
|  | 6SS7 | P | Reverse 12SJ7 to 7B7 procedure. Series circuits only. |
|  | $7 \mathrm{B7}$ | P | Series circuits only. No changes. |
|  | 7C7 | P |  |
|  | 12B7 | E | No changes. |
|  | $14 \mathrm{C7}$ | G |  |
|  | 14H7 | G |  |
|  | 1280 | G |  |
|  | 1284 | E |  |
|  | 12 J 7 | G | Reverse 12K7 to 7B7 procedure. |
|  | $12 \mathrm{K7}$ | E |  |
|  | 12 SH 7 | G | Reverse 12SJ7 to 7B7 procedure. |
|  | 12SJ7 | G |  |
|  | 12SK7 | E |  |
| 14AF7/XXD | 12AH7 | G | Reverse 12AH7 to 14AF7/XXD procedure. |
|  | 14F7 | G | No changes. |
|  | 14N7 | G | Parallel circuits only. No changes. |
| 14B6 | 7 C 6 | P | Series circuits only. No changes. |
|  | 12Q7 | E | Reverse 6Q7 to 7B6 procedure. |
|  | 14E6 | G | No changes. |
| 14B8 | 7 A 8 | P | Series circuits only. No changes. |
|  | 12A8 | G | Reverse 12A8 to 14B8 procedure. |
|  | 14J7 | G | No changes. |
|  | 14S7 | G |  |
| 14 C 5 | 14A5 | G | Parallel circuits only. No changes. |
| $14 \mathrm{C7}$ | 7B7 | P | Series circuits only. No changes. |
|  | 7C7 | P |  |
|  | 12B7 | E | No changes. |
|  | 14A7 | G |  |
|  | $14 \mathrm{H7}$ | G |  |
|  | 1280 | G |  |
|  | 1284 | E |  |
| 14E6 | 12Q7 | G | Reverse 6Q7 to 7B6 procedure. |
|  | 14B6 | G | No changes. |
| 14E7 | 12 C 8 | G | Reverse 12C8 to 14E7 procedure. |



15-25A6 TUBE 15 17
19C8

1E5

32 34 951

## SUB.

J6

57
58
19 TB
19C8

PERF.
G
For battery operation only. Parallel circuits. Change socket to octal and rewire as follows:

No. 1 on five prong to No. 2 on octal

| (3) $0^{6}$ | 2 | to | 3 | (3) ${ }^{6}$ |
| :---: | :---: | :---: | :---: | :---: |
| (2) 0 | 3 | to | 4 | (3) ${ }^{\circ}$ |
| (2) 0 | 4 | to | 7 |  |
| (1) ©anc. | 5 | to | 7 | ${ }_{\text {Sus }}$ |
|  | cap | to |  |  |

G Same as 15 to 1B4. Battery operation only. Parallel circuits.

No practical substitute.
No practical substitute.
E Change socket to octal and rewire as follows:


P Rewire as follows:
$\begin{aligned} \text { No. } 8 & \text { to No. } 4 \\ 3 & \text { to } 8\end{aligned}$


G No changes.
G No changes.
G Parallel circuits only. No changes.
No practical substitute.
No practical substitute.
No practical substitute.
G Use as IF or RF amplifier. Does not make good detector.

## CIRCUIT CHANGES NECESSARY

8

G
E
Change socket to six prong and rewire as follows:
No. 1 on five prong to No. 1 on six prong

## RECEIVING TUBE SUBSTITUTION GUIDE

| (3) $0^{6}$ | 2 | to | 2 | 0 O |
| :---: | :---: | :---: | :---: | :---: |
| (2) ${ }^{(2)}$ | 3 | to | 3 | ) |
| (1) (3) | 4 | to | 4 and 5 | $0 \cdot 0$ |
| Damis. | 5 | to | 6 | suo. |
|  | cap | to | cap |  |


| 25 B 6 | $G$ |
| :--- | :--- |
| 25 C 6 | G |
| 25 L 6 | G |

43
Change socket to six prong and rewire as follows:

No. 2 on octal to No. 1 on six prong



| 2508GT-2525 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 25D8GT |  |  | No practical substitute. |
| 25 L6 | 25A6 | G | No changes. |
|  | 25B5 | G | Reverse 25B5 to 25N6 procedure. |
|  | 25B6 | G | No changes. |
|  | 25C6 | G |  |
|  | 25N6 | G | No changes. |
|  | 43 | G | Reverse 43 to 25L6 procedure. |
|  | 5824 | E | No changes. |
| 25N6 | 25B5 | G | Reverse 25B5 to 25N6 procedure. |
| 25S | 1B5 | E | No changes. |
| 25W4 | $25 \mathrm{Z6}$ | E | Rewire as follows: |
|  |  |  | No. 8 to No. 2 <br> 3 to 4 |
|  |  |  | Connect No. 4 and No. 8 together |
|  |  |  | 3 and 5 together |
| 25X6 | $25 \mathrm{Z6}$ | G | Where 25X6 is used by itself only. Replace line cord with 310 ohms. No changes. |
|  | 50X6 | G | When 25X6 is used by itself, replace line cord or filament dropping resistor with 445 ohms. Change socket to loctal and rewire as follows: <br> No. 2 on octal <br> to No. 1 on loctal |
|  |  |  | (3) 3 to 3 |
|  |  |  | (1) $0_{0}^{0}$ 2 ${ }_{0}$ |
|  |  |  |  |
|  |  |  |  |
|  | 50 Y 6 | G | Where 25X6 is used by itself, replace line cord or filament dropping resistor with 445 ohms. |
|  | 50 Y 7 | G | When 25X6 is used by itself, replace line cord or filament dropping resistor |
|  | $50 \mathrm{Z7}$ | G | with 445 ohms. Do not use No. 6 for anchor. |
| 25 Y 4 |  |  | No practical substitute. |
| 25 Y 5 | $25 \mathrm{Z5}$ | E | No changes. |
|  | $25 \mathrm{Z6}$ | E | Same as $25 \mathrm{Z5}$ to 25Z6. |
| 2573 |  |  | No practical substitute. |
| 25Z4 | 25Z6 | E | No changes. Remove and tape up wires on unused terminals. |
| $25 Z 5$ | 6 J 5 | P | Connect 60 ohm 5 watt resistor in series with filament circuit, will not work in voltage doubler circuit. If one cathode is used by itself for field excitation connect 4 and 8 together. |
|  | $25 Y 5$ | E | No changes. |



2807-35A5
$1 F 4$ C
950
1 A4
1 B4
32
951
6G6

12A6

14A5


Use only in conventional circuits where rectifier is first in the string and A.C. is connected to No. 7.

## RECEIVING TUBE SUBSTITUTION GUIDE

## CIRCUIT CHANGES NECESSARY

changes.
No changes.
No practical substitute.

o. 1 on four prong


Parle circuits only. No changes.
Parallel circuits only. No changes.
No changes. 34 does not make good detector. the same. Use only where 32 L 7 does not have other tubes in series with it.
everse 6 and 8 . Cord is correct

Remove or short out the filament resistor and reverse connections 4 and 5 to socket.

Parallel circuits only. No changes.

No changes.
G
G
G
P Same as 35 A 5 to 35 L 6 but put a 250 ohm 10 watt resistor in series with the filament circuit.

P Same as above but put a 250 ohm 10 watt resistor in series with filament circuit.

P Put 125 ohm 10 W resistor in series with filament.


| 35L6-3 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 35L6 | 6G6 | P | Put 250 ohm 10 watt resistor in series with filament circuit. |
|  | 12A6 | P | Insert 150 ohms resistance in series with the filament circuit. |
|  | 12J5 | P | Insert 150 ohms resistance in series with the filament circuit. |
|  | 35A5 | E | Change socket to loctal and rewire as follows: |
|  | 50A5 | G | No. 2 on octal to No. 1 on loctal |
|  |  |  | (9) 5 5 to 2 , (8) |
|  |  |  | (1) 4 - to 3 |
|  |  |  | (2) 5 to 6 - 1 (0) |
|  |  |  | OR16. 8 to 7 to |
|  |  |  | 7 to 8 |
|  | $35 \mathrm{B5}$ | E | Change socket to miniature and rewire as follows: |
|  | 50B5 | G | No. 2 on octal to No. 3 on miniature |
|  |  |  | (9) 3 to 5 |
|  |  |  |  |
|  |  |  | (3) 5 (2) to 1 |
|  |  |  | Oftie. 7 to 4 to |
|  |  |  | 8 to 2 |
|  |  |  | Do not use No. 7 on miniature. |
|  | 35 C 5 | E | Change socket to miniature and rewire as follows: |
|  | 50C5 | G | No. 2 on octal to No. 3 on miniature |
|  |  |  | (8) 3 (3) to 7 |
|  |  |  | (9) $0^{\circ}$ 4 to 6 - |
|  |  |  | (1) 5 2 5 to 2 e |
|  |  |  | 7 to 4 sue. |
|  |  |  | 8 to 1 |
|  |  |  | Do not use terminal No. 5 on miniature. |
|  | 50C6 | G | No changes. |
|  | 50L6 | G |  |
| 35W4 | 35 Y 4 | E | Where space permits. Reverse 35 Y 4 to 35W4 procedure. |
|  | 35Z3 | E |  |
|  | 3525 | E |  |
|  | $117 \mathrm{Z3}$ | G | Where 35W4 is used by itself only. Remove line cord resistor or filament dropping resistor and replace with ordinary line cord. Rewire as follows: |
|  |  |  | Remove and tape up any wires on No. 6 <br> No. 7 to No. 6 |
|  |  |  | Pilot light will not burn. In order to light pilot light, connect 40 ohm 1 watt resistor in series with filament and connect pilot light across it. |
| 35 Y 4 | 35W4 | E | Change socket to miniature and rewire as follows: |
|  |  |  | No. 1 on loctal to No. 3 on miniature |
|  |  |  | (9) 2 to 5 |
|  |  |  | (0) 4 (0) to 4 |
|  |  |  |  |
|  |  |  | onic. 8 to 4 |
|  | $35 \mathrm{Z3}$ | E | No change is necessary but pilot light will not light. Pilot light can be lit by same method as used from $35 Z 5$ to $35 Z 4$. |



3525-40
6J7 G
$6 \mathrm{K7} \quad \mathrm{E}$
$6 S 7$ G

6SH7
6SJ7
6SK7 E
6SS7 G
$6 \mathrm{U7} \quad \mathrm{G}$
6W7 G
7A7 E

7H7
7L7 G
7B7 G

7 C 7

00 A
01A
12A

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| $35 \mathrm{Z5}$ | $35 \mathrm{Z4}$ | E | No change is necessary but pilot light will not light. In order to light the pilot light, put a 40 ohm resistor in series with the filaments and connect the pilot light across it. This resistor must have a 1 watt rating. |
|  | $45 Z 5$ | G | No changes. |
| 35Z6 | $25 \mathrm{Z6}$ | G | No change, unless $35 Z 6$ is used singly in which case put 35 ohm 10 watt resistor in filament string. |
|  | $50 \mathrm{Z6}$ | G | No changes. Where a full set of five or six tubes are used, little change in operation will be noted. If $35 Z 6$ is used by itself, this substitution may not be satisfactory. |
| 35/51 | 24A | G | No changes. |
| 36 | $\begin{aligned} & \text { 6C6 } \\ & \text { 6D6 } \end{aligned}$ | $\begin{aligned} & \mathbf{E} \\ & \mathbf{G} \end{aligned}$ | Same as 37/44 to 6D6. |
|  | 39/44 | G | No changes. |
|  | 77 | E | Same as 37/44 to 6D6. |
|  | 78 | G |  |
| 37 | 76 | E | No changes. |
| 38 | 41 | G | Parallel circuits only. Reverse 41 to 38 procedure. |
|  | 42 | G |  |
| 39/44 | 6 C 6 | G | Change socket to six prong and rewire as follows: |
|  | 6D6 | E | No. 1 on five prong to No. 1 on six prong |
|  | 77 | G | (3) $0^{6}$ 2 to 2 为 |
|  | 78 | E |  |
|  |  |  | (1) (5) 5 to 6 |
|  |  |  |  |

G

G
G
RECEIVING TUBE SUBSTITUTION GUIDE

No change is necessary but pilot light will not light. In order to light the pilot light, put a 40 ohm resistor in series with the filaments and connect the pilot light across it. This resistor must have a 1 watt rating.

No changes.
No change, unless $35 Z 6$ is used singly in which case put 35 ohm 10 watt resistor in filament string.

No changes. Where a full set of five or six tubes are used, litule change in peration will be noted. If $35 Z 6$ is used by itself, this substitution may not be satisfactory.

No changes.
Same as $37 / 44$ to 6D6.

No changes.
Same as $37 / 44$ to 6D6.

No changes.

Reverse 6 K 7 to $39 / 44$ procedure.
$\qquad$

G

G E

G

G r

Reverse 7A7 to 39/44 procedure.

Reverse 7A7 to 39/44 procedure. Parallel circuits only.

No changes.
G No changes.





| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 56 | 27 | G | No changes. |
|  | 485 | G | No changes. |
| 56AS | 37 | E | Parallel circuits only. No changes. |
|  | 76 | E |  |
| 56S | 27 | E | No changes. |
|  | 56 | E |  |
| 57 | 58 | G | No changes. |
| 57AS | 6C6 | E | Parallel circuits only. No changes. |
|  | 77 | E |  |
| 57S | 57 | E | No changes. |
|  | 58 | E |  |
| 58 | 57 | G | No changes. 58 is not a good second detector. |
| 58AS | 6D6 | E | Parallel circuits only. No changes. |
|  | 78 | E |  |
| 58 S | 57 | E | No changes. |
|  | 58 | E |  |
| 59 | 47 | G | Reverse 47 to 59 procedure. |
|  | 1619 | G | $\begin{aligned} & \text { Parallel circuits only. Make adaptor as follows: } \\ & \text { No. } 1 \text { on base } \\ & 2 \end{aligned}$ |
|  |  |  | 3 to 4 |
|  |  |  | 4 to 5 |
|  |  |  | 5 and 6 to 8 |
|  |  |  | 7 to 7 |
|  |  |  | There are or will be many used 1619 tubes available. |
| 70A7 | 32 L 7 | G | No changes. Where no other tubes in series with the 70 A 7 which has 150 mil filament instead of 0.3 amp . |
|  | 70L7 | E | Change connection as follows: |
|  |  |  | No. 8 to No. 6 <br> 6 to 8 |
|  |  |  | Connect Nos. 7 and 8 together. |
|  |  |  | Pilot light will not light but may be lit by same procedure as $50 \mathrm{Z7}$ to 50 Y 6 . |
|  | 117 L 7 | E | Remove the line cord resistor and replace with straight AC cord. Reverse |
|  | 117 M 7 | E | connections to 4 and 5. |
|  | 117 N 7 | E | Remove line resistor cord and replace with straight AC cord. |
|  | 117 P 7 | E | Remove wire from No. 8 |
|  |  |  | Move No. 1 to No. 8 |
|  |  |  | Reverse Nos. 4 and 5 |
|  |  |  | Move No. 6 to No. 7 |
|  |  |  | Place No. 8 on No. 6 |
| 70L7 | 32L7 | G | Cord is correct. If 32 L 7 is alone in circuit. Reverse Nos. 6 and 8. |
|  | 70A7 | E | Change connections as follows: |
|  |  |  | No. 6 to No. 8 |
|  |  |  | 8 to 6 |


| 70L7- |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 70L7 | 117 L 7 | E | Remove line resistor cord and replace with straight AC cord. |
|  | 117 M 7 | E | Reverse Nos. 4 and 5 <br> Reverse 6 and 8 |
|  | 117 N 7 | E | Remove line cord resistor and replace with straight AC cord. |
|  | 117 P 7 | E | Reverse Nos 4 and 5 |
|  |  |  | No. 8 on No. 7 |
|  |  |  | 1 on 8 |
| 71A | 482 | G | No changes. If push-pull circuit, both tubes must be changed to avoid hum. |
|  | 483 | G |  |
| 75 | 6AQ6 | G | Same as 75 to 6AT6. Parallel circuits only. |
|  | 6AT6 | G | Change socket to miniature and rewire as follows: |
|  | 6AV6 | G | No. 1 on six prong to No. 3 on miniature |
|  | 6BF6 | G | 2 2 to 7 |
|  | 6BK6 | G | $0^{\circ} \mathrm{O} \mathrm{O}^{6} 3$ to 3 |
|  | 6BT6 | G |  |
|  | 6BU6 | G | $\begin{array}{llll}0 & 5 & \text { to } \\ \text { onic. } & \\ & 6 & \text { to } & 4\end{array}$ |
|  |  |  | cap to 1 |
|  | 6B6 | E | Change socket to octal and rewire as follows: |
|  | 6Q7 | E | No. 1 on six prong to No. 2 on octal |
|  | 6R7 | G | $\bigcirc{ }^{\circ} 2$ |
|  |  |  | ${ }^{3}{ }^{3}{ }_{50}{ }^{3}$ - to ${ }^{\text {a }}$ |
|  |  |  |  |
|  |  |  | 6 6 to 6 to 7 eve. |
|  |  |  | cap to cap |
|  | 6C6 | P | Emergency substitution. No changes but considerable loss of volume. |
|  | 6SQ7 | E | Reverse 6SQ7 to 75 procedure. |
|  | 6SR7 | G |  |
|  | 6T7 | G | Same as 75 to 6Q7. Parallel circuits only. |
|  | 6V7 | G | Same as 75 to 6Q7. |
|  | $7 \mathrm{B6}$ | E | Change socket to loctal and rewire as follows: |
|  | 7E6 | G | No. 1 on six prong to No. 1 on loctal |
|  |  |  | $2$ $2$ |
|  |  |  |  |
|  |  |  | 20 40 to 4 (2) |
|  |  |  |  |
|  |  |  |  |
|  |  |  | cap to 3 |
|  | 7 C 6 | G | Same as above. Parallel circuits only. |
|  | 85 | G | No changes. Sometimes works excellent, other times not so well. |
| 76 | 6AE5 | G | Reverse 6C5 to 37 procedure. |
|  | 6C5 | E | Reverse 6C5 to 37 procedure. |
|  | 6 J 5 | G | Reverse 6C5 to 37 procedure. |





## 85-117N7

32 L 7

70A7

70L7

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 85 | 75 | G | No changes. |
| 85AS | 85 | E | No changes. |
| 89 | 6K6 | G | Same as 6F6 to 89. Parallel or series circuits. |
|  | 41 | G | Reverse 41 to 89 procedure. |
|  | 42 | G | Parallel circuits only. Reverse 41 to 89 procedure. |
| 99 V |  |  | No practical substitution. |
| X99 | 20 | G | Parallel circuits only. No changes. |
| 117L7 | 32 L 7 | G | Place 280 -ohm cord or 50 -w resistor in series with filaments. Reverse socket connections Nos. 4 and 5. |
|  | 70A7 | G | Place 300 -ohm cord or 10 -w resistor in series with filaments. Reverse socket connections Nos. 4 and 5. |
|  | 70L7 | G | Place 300 -ohm 10 -w resistor in series with filaments. Reverse socket connections Nos. 4 and 5, also 6 and 8. |
|  | 117M7 | E | No changes. |
| $\begin{gathered} 117 \mathrm{~L} 7 \\ \text { or } \end{gathered}$ | $\begin{gathered} 117 \mathrm{~N} 7 \\ \text { or } \end{gathered}$ | E | Make adaptor as follows: <br> No. 1 on base <br> to No. 8 on top |
| 117 M 7 | 117 P 7 | E | $2$ |
|  |  |  | 3 to 3 |
|  |  |  | $4$ to $4$ |
|  |  |  | $5$ <br> to 5 |
|  |  |  | 7 to 7 |
|  |  |  | 8 to 6 |
|  |  |  | AC line must connect to No. 7 |
| 117L7/M7 | 25A7 | G | Connect 300 -ohm line cord in place of AC cord and change connections as follows: |
|  |  |  | Reverse Nos. 4 and 5. |
| 117 M 7 | $32 \mathrm{L7}$ | G | Same as 117 L 7 to 32 L 7 . |
|  | 70A7 | G | Same as 117L7 to 70A7. |
|  | 70L7 | G | Same as 117L7 to 70L7. |
| 117N7 | 25A7 | G | Connect 300 -ohm line cord in place of AC cord and change connections as follows: | follows:

No. 6
to No. 7
8
to 6
1
to 8
Reverse Nos. 4 and 5.
RECEIVING TUBE SUBSTITUTION GUIDE

## CIRCUIT CHANGES NECESSARY

G No changes.
o changes. Same as 6F6 to 89. Parallel or series circuits. Parallel circuits only. Reverse 41 to 89 procedure.

No practical substitution.
Parallel circuits only. No changes.
Place 280 -ohm cord or 50 -w resistor in series with filaments. Reverse Place 300 -ohm cord or 10 -w resistor in series with filaments. Reverse socket connections Nos. 4 and 5.

Place 300 -ohm $10-$ w resistor in series with filaments. Reverse socket No changes.
follows:

Connect 300 -ohm line cord in place of AC cord and change connections as Reverse Nos. 4 and 5.

Reverse Nos. 4 and 5.
G Remove and tape up any wire anchored on No. 1. Place 280 -ohm cord or 50 -w resistor in series with filaments. Reverse socket connections Nos. 4 and 5. Move No. 8 to No. 1.

G Place 300 -ohm cord or $10-$ w resistor in series with filaments. Reverse socket connections Nos. 4 and 5. Move No. 8 to No. 1 and No. 6 to No. 8.

G Remove and tape up any wires connected to No. 1. Place 300 -ohm cord or 10-w resistor in series with filaments. Reverse Nos. 4 and 5, move No. 8 to No. 1 and short Nos. 7 and 8 together. For use in circuits where AC line is connected to No.7.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 117 N 7 | 117 P 7 | E | No changes. |
| $117 \mathrm{P7}$ | 25A7 | G | Same as 117N7 to 25A7. Cord or resistor must dissipate 90 w . |
| $117 \mathrm{Z3}$ | 35W4 | G | Replace line cord with 533-ohm resistor cord. Rewire as follows: $\begin{aligned} & \text { No. } 6 \text { to No. } 7 \\ & \text { Do not use No. } 6 \text { for anchor. } \end{aligned}$ |
|  | 45Z3 | G | Replace line cord with 960 -ohm resistor cord. Rewire as follows. <br> Do not use unused terminals for anchors. |
|  | $117 \mathrm{Z4}$ | G | Where space permits. Change socket to octal and rewire as follows: |
| $117 \mathrm{Z4}$ | 11723 | G | Reverse $117 \mathrm{Z3}$ to $117 \mathrm{Z4}$ procedure. |
|  | $117 \mathrm{Z6}$ | E | No change except to remove and tape up any wires which may be anchored to Nos. 3 and 4. |
| 117 Z 6 | 6X5 | P | Connect 200 -ohm 100 -w resistor in series with filament. Use only where Nos. 4 and 8 are tied together. |
|  | $25 \mathrm{Z6}$ | G | Connect $\mathbf{3 0 0 - o h m ~ l i n e ~ c o r d ~ o r ~ 5 0 - w ~ r e s i s t o r ~ i n ~ s e r i e s ~ w i t h ~ f i l a m e n t . ~}$ |
|  | 50Y6 | E | No change except that a $450-$ ohm 20 -w resistor or line cord must be used in series with the filament. |
|  | 50Z6 | E | Connect $\mathbf{2 2 0 - o h m ~ l i n e ~ c o r d ~ i n ~ p l a c e ~ o f ~ A C ~ c o r d . ~}$ |
|  | 5027 | E | Connect 440-ohm line cord in place of AC cord. |
| 182B/482B | $\begin{aligned} & 71 \mathrm{~A} \\ & 183 / 483 \end{aligned}$ | $\begin{aligned} & \mathbf{E} \\ & \mathbf{E} \end{aligned}$ | No changes. |
| 183/483 | $\begin{aligned} & 71 A \\ & \text { 182B/482B } \end{aligned}$ | $\begin{aligned} & \mathbf{E} \\ & \mathbf{E} \end{aligned}$ | No changes. |
| 210 T | $\begin{aligned} & \text { VT52 } \\ & 10 \\ & 50 \end{aligned}$ | $\begin{aligned} & \mathbf{P} \\ & \mathbf{E} \\ & \mathbf{G} \end{aligned}$ | No changes. |
| 485 | 27 | G | No changes in connections but put one inch piece of screen wire doubled in series with one side of filament winding. |
|  | 56 | G | Same as 485 to 27. |
| 864 |  |  | No practical substitute. |
| 950 | 1 F4 | G | No changes. |
|  | 33 | G | Parallel circuits only. No changes. |
| 954 | 956 | E | No changes. |


| 955-1274 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 955 | 5731 | P | No changes. |
| 956 | 954 | E | No changes. |
| 957 | 958 A | G | Parallel circuits only. No changes. |
| 958A | 957 | G | Parallel circuits only. No changes. |
| 959 |  |  | No practical substitute. |
| FM1000 |  |  | No practical substitute. |
| 1005/CK1 005 | 0 Y 4 <br> 0Z4A | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
| CK1013 | 5517 | E | No changes. |
| 1201 | 7E5 | E | No changes. |
| 1203 | $7 \mathrm{C4}$ | E | No changes. |
| 1204 | 7AB7 | E | No changes. |
| 1206 | 7G8 | E | No changes. |
| 1221 | $6 \mathrm{C} 6$ | E | No changes. |
|  | $77$ | E |  |
| 1223 | 657 | E | No changes. |
| 1229 | 1 A4 | E | No changes. |
|  | 1 B4 | E |  |
|  | 32 | E |  |
|  | 951 | E |  |
| 1230 | 30 | E | No changes. |
| 1231 | 7G7 | G | No changes. |
|  | 7V7 | G |  |
| 1232 | 7G7 | E | No changes. |
| 1247 |  |  | No practical substitute. |
| 1265 |  |  | No practical substitute. |
| 1266 |  |  | No practical substitute. |
| 1267 | 0A4 | G | No changes. |
| 1273 | 7A7 | G | No changes. |
|  | 7AJ7 | G |  |
|  | 7H7 | G |  |
|  | 7L7 | G |  |
|  | 7T7 | G |  |
| 1274 |  |  | Parallel circuits only. No changes. |
|  | 6W5 | G |  |
|  | 6ZY5 | G |  |
|  | 6AX6 | G | No change necessary but tie Nos. 4 and 8 together if convenient. |


| TUBE |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
|  | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 1274 | 6BY5 | G | Parallel circuits only. Rewire as follows: Connect Nos. 1 and 8 together No. 3 to No. 4 |
|  | 6 X 5 | E | No changes. |
|  | 7Y4 | E | Same as 6X5 to 7Y4. Parallel circuits only. |
|  | $7 \mathrm{Z4}$ | E |  |
| 1275 | 5X3 | G | No changes. |
|  | 5Z3 | E |  |
|  | 80 | G |  |
|  | 83 | G |  |
|  | 83 V | G |  |
| 1276 |  |  | No practical substitute. |
| 1280 | 12B7 | G | No changes. |
|  | 14A7 | G | No changes. |
|  | 14 C 7 | G |  |
|  | 14H7 | E |  |
|  | 1284 | G |  |
| 1284 | 12B7 | G | No changes. |
|  | 14 A 7 | G |  |
|  | 14 C 7 | G |  |
|  | 14 H 7 | G |  |
|  | 1280 | G |  |
| 1291 | 3B7 | E | No changes. |
| 1293 | 1 LE3 | G | Parallel circuits only. No changes. |
| 1294 | $1 \mathrm{R4}$ | E | No changes. |
| 1299 | 3D6 | E | No changes. |
| 1612 | 6L7 | E | No changes. |
| 1614 | 6L6 | E | No changes. |
| 1619 | 2 A 5 | G | Reverse 2A5 to 1619 procedure. |
| 1620 | $6 \mathrm{J7}$ | E | No changes. |
| 1626 | 12E5 | G | Parallel circuits only. No changes. |
|  | $12 \mathrm{J5}$ | G |  |
| 1629 |  |  | No practical substitute. |
| 1634 | 12SC7 | G | No changes. |
| 1644 | 12L8 | G | No changes. |
| 1654 |  |  | No practical substitute. |
| 2050 | 2051 | E | No changes. |
| 2051 | 2050 | E | No changes. |
| 5517 | CK1013 | E | No changes. |


| 5517/CK1013-5691 |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 5517/CK1013 |  |  | No practical substitute. |
| 5590 | 6AG5 | P | Parallel circuits only. No changes. |
|  | 6BC5 | G |  |
|  | 5591 | G | No changes. |
|  | 9001 | G |  |
|  | 9003 | G |  |
| 5591 | $6 \mathrm{BC5}$ | P | Parallel circuits only. No changes. |
|  | 6AG5 | G |  |
|  | 5590 | G | No changes. |
|  | 9001 | G |  |
|  | 9003 | G |  |
| 5608-A | 53 | E | No changes. |
| 5618 | 2 E 30 | G | Parallel circuits only. Rewire as follows: |
|  | 5812 | G | Remove wires from No. 4 |
|  |  |  | No. 1 to No. 4 |
|  |  |  | 6 to 1 |
|  |  |  | 3 to 6 |
|  |  |  | 7 to 3 |
|  |  |  | 5 to 7 |
|  |  |  | 2 to 5 |
|  |  |  | Connect wires removed from No. 4 to No. 2. |
| 5635 |  |  | No practical substitute. |
| 5636 |  |  | No practical substitute. |
| 5643 |  |  | No practical substitute. |
| 5646 |  |  | No practical substitute. |
| 5647 |  |  | No practical substitute. |
| 5654 | 6AJ5 | G | No changes. |
|  | 6AK5 | G |  |
| 5670 | $7 \mathrm{F8}$ | G | Where space permits. Same as 2C51 to 7F8. Parallel circuits only. |
| 5672 | 5678 | G | No changes. |
| 5676 | 5677 | P | Parallel circuits only. No changes. |
| 5677 | 5676 | G | Parallel circuits only. No changes. |
| 5678 | 5672 | G | No changes. |
| 5679 | 7A6 | E | Where No. 4 is not used on 5679. No changes. |
| 5686 |  |  | No practical substitute. |
| 5687 | 6J6 | G | Parallel circuits only. Reverse 6J6 to 5687 procedure. |
| 5691 | 6SL7 | E | Parallel circuits only. No changes. |
|  | 6SN7 | P | No changes. |
|  | 5692 | P |  |


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 5692 | 6SN7 | G | No changes. |
|  | 5691 | P |  |
| 5693 | 6SJ7 | E | No changes. |
|  | 6SK7 | P |  |
| 5694 |  |  | No practical substitute. |
| 5697 |  |  | No practical substitute. |
| 5702 | 5784 | G | No changes. |
| 5703 | 5744 | P | No changes. |
| 5704 |  |  | No practical substitute. |
| 5718 | 5719 | P | No changes. |
| 5719 | 5718 | P | No changes. |
| 5722 |  |  | No practical substitute. |
| 5725 | 6AJ5 | P | No changes. |
|  | 6AK5 | P |  |
| 5726 | 6X4 | G | Parallel circuits only. Rewire as follows: |
|  |  |  | 2 to 1 |
| 5731 | 955 | $\mathbf{P}$ | No changes. |
| 5744 | 5703 | P | No changes. |
| 5783 |  |  | No practical substitute. |
| 5784 | 5702 | G | No changes. |
| 5785 |  |  | No practical substitute. |
| 5787 |  |  | No practical substitute. |
| 5812 | 2E30 | G | No changes. |
| 5823 |  |  | No practical substitute. |
| 5824 | 25A6 | P | No changes. |
|  | 25 B6 | E |  |
|  | 25C6 | P |  |
|  | 25L6 | E |  |
| 5840 | 5899 | G | No changes. |
|  | 5900 | G |  |
|  | 5901 | G |  |
| 5847 |  |  | No practical substitute. |
| 5879 |  |  | No practical substitute. |
| 5896 |  |  | No practical substitute. |
| 5897 | 5898 | $\mathbf{P}$ | No changes. |


| 5898-XXL |  |  | RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 5898 | 5897 | P | No changes. |
| 5899 | 5840 | G | No changes. |
|  | 5900 | G |  |
|  | 5901 | G |  |
| 5900 | 5840 | G | No changes. |
|  | 5899 | G |  |
|  | 5901 | G |  |
| 5901 | 5840 | G | No changes. |
|  | 5899 | G |  |
|  | 5900 | G |  |
| 5910 |  |  | No practical substitute. |
| 5915 | 6BE6 | E | No changes. |
| 5931 |  |  | No practical substitute. |
| 5932 |  |  | No practical substitute. |
| 9001 | 5590 | P | No changes. |
|  | 5591 | G |  |
|  | 9003 | G |  |
| 9002 | $6 \mathrm{AB4}$ | P | Rewire as follows: |
|  |  |  | No. 2 to No. 7 <br> 5 to $\quad 1$ |
| 9003 | 5590 | G | No changes. |
|  | 9001 | G |  |
| 9004 |  |  | No practical substitute. |
| 9005 |  |  | No practical substitute. |
| 9006 |  |  | No practical substitute. |
| X6030 |  |  | No practical substitute. |
| XXFM | 7X7 | E | No changes. |
| XXL | 6C5 | E | Reverse 6 J 5 to XXL procedure. |
|  | 6J5 | E | Reverse 6J5 to XXL procedure. |
|  | 6K7 | E | Reverse 6K7 to XXL procedure. |
|  | 7 A 4 | E | No changes. |



## ADDENDUM <br> receiving tube substitution guide

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :--- | :--- | :--- | :--- |
| 6Y7G | 79 | G | Reverse 6 N 7 to 79 procedure. |
| 79 | 6 Y 7 G | G | Reverse 6 N 7 to 79 procedure. |
| 1603 | 6 C 6 | E | No changes. |
|  | 7700 | E |  |
| 1611 | 6 F 6 | E | No changes. |
| 7000 | $6 \mathrm{J7}$ | E | No changes. |
| 7700 | 6 C 6 | E | No changes. |
|  | 1603 | E |  |
|  |  |  |  |

IDENTICAL TUBES WITH UNLIKE HEATER VOLTAGE AND CURRENT RATINGS
Substitute high voltage tubes for low voltage tubes in series circuits only with suitable shunt resistor when required. Substitute low voltage tubes for high voltage tubes in parallel circuits with voltage dropping resistor in series with filament -- in series circuits with suitable shunt resistor. For all cases see instructions in Section 1. The performance for each substitution is excellent.

| TUBE | SUB. | TUBE | SUB. | TUBE | SUB. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 A 3 | 6 A 3 | $7 \mathrm{B6}$ | 14B6 | 14B8 | 7B8 |
| 2 A 5 | 42 | $7 \mathrm{B8}$ | 14B8 | 14E6 | 7 E 6 |
| 2 A 6 | 75 | 7E6 | 14E6 | 14E7 | 7 E 7 |
| 2 A 7 | 6 A 7 | 7E7 | 14 E 7 | 14 F 7 | $7 \mathrm{F7}$ |
| $2 \mathrm{B7}$ | 6B7 | 7F7 | 14F7 | 14 F 8 | 7F8 |
| 6A3 | 2 A 3 | 7F8 | 14F8 | 14 J 7 | 7 J 7 |
|  | 1276 | 7J7 | 14 J 7 | 14N7 | 7 N 7 |
| 6A6 | 53 | 7N7 | 14N7 | 14N7 | 7N7 |
| 6 A 7 | 2 A 7 | 7Q7 | 14Q7 | 14Q7 | 7Q7 |
| 6A8 | 12A8GT | 7R7 | 14R7 | 14R7 | $7 \mathrm{R7}$ |
| 6B7 | $2 \mathrm{B7}$ | 12A8GT | 6A8 | 25B8GT | 12B8G |
| 6B8 | 12 C 8 | 12B8G | 25B8GT | 25L6 | 1632 |
| 6 F 5 | 12F5GT | 12 C 8 | 6B8 | 30 | RK42 |
| 6H6 | 12H6 | 12F5GT | 6 F 5 | 42 | 2 A 5 |
| $6 \mathrm{J5}$ | 12 J 5 GT | 12H6 | 6H6 | 53 | 6A6 |
| 6.J7 | 12 J 7 GT | 12 J 5 GT | 6 J 5 | 55 | 85 |
| 6 K 7 | 12 K 7 GT | 12 J 7 GT | 6 J 7 | 56 | 56AS |
| 6 K 8 | 12 K 8 | 12 K 7 GT | $6 \mathrm{K7}$ |  | 76 |
| 6L6 | 1631 | 12 K 8 | 6 K 8 | 56AS | 56 |
| 6Q7 | 12Q7GT | 12Q7GT | 6Q7 |  | 76 |
| 6SA7 | 12SA7 | 12SA7 | 6SA7 | 57 | 57 AS |
| 6SC7 | 12SC7 | 12SC7 | 6SC7 | 57AS | 57 |
|  | 1634 | 12SF5 | 6SF5 | 58 | 58AS |
| 6SF5 | 12SF5 | 12SF7 | 6SF7 | 58AS | 58 |
| 6SF7 | 12SF7 | 12SG7 | 6SG7 | 75 | $2 \mathrm{A6}$ |
| 6SG7 | 12SG7 | 12 SH 7 | 6SH7 | 76 | 56 |
| 6SH7 | 12SH7 | 12SJ7 | 6S.J7 | 85 | 55 |
| 6SJ7 | 12S.J 7 | $12 \mathrm{SK7}$ | 6SK7 | 1276 | 2A3 |
| 6SK7 | 12SK'7 | 12SL7GT | 6SL7GT |  | 6 A3 |
| 6SL7GT | 12SL7GT | 12SN7GT | 6SN7GT | 1631 | 6L6 |
| 6SN7GT | 12SN7GT |  | 1633 | 1632 | 25L6 |
|  | 1633 | 12SQ7 | 6SQ7 | 1633 | 6SN7GT |
| 6SQ7 | 12SQ7 | $12 \mathrm{SR7}$ | 6SR7 |  | 12SN7GT |
| 6SR7 | 12SR7 | 14A4 | 7A4 | 1634 | 6SC7 |
| 7 A 4 | 14A4 | 14B6 | 7B6 | RK42 | 30 |

## TELEVISION RECEIVER FILAMENT CIRCUIT ARRANGEMENT

The filaments of the tubes in most television receivers are either arranged in parallel, series and parallel, or series-parallel circuits. It is necessary to know the filament arrangement of a particular television receiver before some of the tubes in the circuit may be substituted because in many cases, a substitution will involve the addition of a resistor (or other circuit component), or the rearrangement of some part of the filament circuit to make for proper tube operating conditions. For example, the substitution of a tube with a 6.3 volt filament for one with a 12.6 volt filament requires the addition of a series resistor or a shunting resistor depending upon whether the filament is in a parallel or a series circuit respectively. (see Section 1 ).

In the following section all of the information about filament circuits needed to effect successful substitutions is given for most television receivers. The receivers are listed by model number (or chassis number for those sets having no model number) under the name of the manufacturer. In the second column is found the first page number of the section in the Rider Television Manuals in which all of the servicing information as well as schematics for the

| Model | Rider Man. Page | туре Cir. | No. of Chains | Sch. |
| :---: | :---: | :---: | :---: | :---: |
| ADMIRAL CORP. |  |  |  |  |
| 4H15A, 4H15B, Ch. 20Al; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| 4H15S, 4H15SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H16A, 4H16B, Ch. 20Al; 4Jl, Radio Ch. | 4-1 | $\mathbf{P}$ | 2 | 1 |
| 4H16S, 4H16SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H17A, 4H17B, Ch. 20Al; 4J1, Radio Ch. | 4-1 | $\boldsymbol{P}$ | 2 | 1 |
| 4H18C, 4H18CN, Ch. 20B1; 4K1, Radio Ch | 4-1 | $\mathbf{P}$ | 2 | 1 |
| $\begin{aligned} & 4 \mathrm{H1} 8 \mathrm{~S}, 4 \mathrm{H} 18 \mathrm{SN}, \mathrm{Ch} .30 \mathrm{Al}, 30 \mathrm{B1}, 30 \mathrm{C} 1 \text {, } \\ & \text { 30D1; 4H1, Radio Ch. } \end{aligned}$ | 3-17 | $\mathbf{P}$ | 5 | 3 |
| 4H19C, 4H19CN, Ch. 20B1; 4K1, Radio Ch | 4-1 | P | 2 | 1 |
| $\begin{aligned} & \text { 4H19S, } 4 \text { H19SN, Ch. 30A1, 30B1, 30C1, } \\ & \text { 30D1; 4H1, Radio Ch. } \end{aligned}$ | 3-17 | $\mathbf{P}$ | 5 | 3 |
| $4 \mathrm{H} 115 \mathrm{~S}, 4 \mathrm{H} 115 \mathrm{SN}, 4 \mathrm{H} 116 \mathrm{~S}, 4 \mathrm{H} 116 \mathrm{SN}$, 4H117S, 4H117SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | $\mathbf{P}$ | 5 | 3 |
| 4H126A, 4H126B, Ch. 21A1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| ```4H126C, 4H126CN, Ch. 21A1; 4K1, Radio Ch.``` | 4-1 | P | 2 | 1 |
| 4H126S, 4H126SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H137A, 4H137B, Ch. 21A1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| ```4H137S, 4H137SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch.``` | 3-17 | P | 5 | 3 |
| 4H145A, 4H145B, Ch. 20B1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| 4H145C, 4H145CN, Ch. 20B1; 4K1, Radio Ch. | 4-1 | $\mathbf{P}$ | 2 | 1 |
| 4H145S, 4H145SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |

set are given. Under "Type Circuit", a "P" indicates that all of the filaments are in parallel chains across the secondaries of the power and/or filament transformers, an "S, P"indicates that some of the filaments are in parallel chains and some are in series circuits across the line or power transforme $r$, and " $S$ - $P$ ' indicates that the filaments are in a series-parallel circuit across the line. Where the filament arrangement is either "S,P" or "S-P", the filament circuit is reproduced at the end of this section, and appears with the number shown in the "Schematic" column. The schematics numbered 1-6 are typical of the majority of parallel filament circuits except for the addition of one or two chains similar to those shown. The schematics $7-35$ are reproductions of the " $S, P$ ", and 'S-P' circuits previously referred to.

The number of circuits or chains into which the filaments of any set are divided appears under the "Number of Chains" column. NOTE: The 1 B3 high voltage rectifier circuit has not been included in the number of chains since this rectifier in practically all cases comes off the secondary of the horizontal output transformer.

| Model | Rider <br> Man. <br> Page | Type Cir. | No. of Chains | Sch. |
| :---: | :---: | :---: | :---: | :---: |
| ADMIRAL CORP. (Cont'd) |  |  |  |  |
| 4H146A, 4H146B, Ch. 20B1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| 4H146C, Ch. 20R1; 4 Kl , Radio Ch. | 4-1 | P | 2 | 1 |
| 4H146S, 4H146SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H147A, 4 H147B, Ch. 20 Bl ; 4J1, Radio Ch | h. 4-1 | P | 2 | 1 |
| 4H147S, 4H147SN, 4H155S, 4H155SN, Ch. 30A1, 30B1, 30C1, 30D1, 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H156C, 4H156CN, Ch. 20B1; 4K1, Radio Ch. | 4-1 | P | 2 | 1 |
| 4H156S, 4H156SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 4H157A, 4H157B, Ch. 20E1; 4J1, Radio Ch. | 4-1 | $\mathbf{P}$ | 2 | 1 |
| 4H157S, 4H157SN, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | $\mathbf{P}$ | 5 | 3 |
| 4H165A, 4H165B, Ch. 20B1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |
| $\begin{aligned} & \text { 4H165S, 4H165SN, Ch, 30A1, 30B1, 30C1, } \\ & \text { 30D1; 4H1, Radio Ch. } \end{aligned}$ | 3-17 | P | 5 | 3 |
| 4H166A, 4H166B, Ch. 20B1; 4J1, Radio Ch. | 4-1 | $\mathbf{P}$ | 2 | 1 |
| 4H166C, 4H166CN, Ch. 20B1; 4K1, Radio Ch. | 4-1 | P | 2 | 1 |
| ```4H166S, 4H166SN. Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch.``` | 3-17 | P | 5 | 3 |
| $\begin{aligned} & \text { 4H167A, 4H167B, Ch. 20B1; } \\ & \text { 4J1, Radio Ch. } \end{aligned}$ | 4-1 | P | 2 | 1 |
| 4H167C, 4H167CN, Ch. 20B1; 4K1, Radio Ch. | 4-1 | $\mathbf{P}$ | 2 | 1 |

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Model
Rider
Man. Type No. of Page Cir. Chains Sch.

|  | Rider |
| :--- | :--- |
| Model | Man. Type No. of |
| Page Cir. Chains Sch. |  |

## ADMIRAL CORP. (Cont'd)

4H167S, 4H167SN, Ch. 30A1, 30B1, 30C1, 3-17 P 30D1; 4H1, Radio Ch.

| $8 \mathrm{C} 11, \mathrm{Ch} .30 \mathrm{Al}$; 8C1, Radio Ch. | $2-1$ | P | 5 | 3 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $8 \mathrm{C} 11,8 \mathrm{C} 11 \mathrm{~N}, 8 \mathrm{C} 11 \mathrm{~S}, 8 \mathrm{C} 11 \mathrm{SN}, 8 \mathrm{C} 11 \mathrm{~T}$, | $3-17$ | P | 5 | 3 | 8Cl1, 8C11N, 8C11S, 8Cl1SN, 8C11T,

8C11TN, 8C11UL, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch.

| $8 \mathrm{C} 12, \mathrm{Ch} .30 \mathrm{~A} 1 ; 8 \mathrm{C} 1$, Radio Ch. | $2-1$ | P | 5 | 3 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $8 \mathrm{C} 12,8 \mathrm{C} 12 \mathrm{~N}, 8 \mathrm{C} 12 \mathrm{~S}, 8 \mathrm{C} 12 \mathrm{SN}, 8 \mathrm{C} 12 \mathrm{~T}$, | $3-17$ | P | 5 | 3 | 8C12TN, 8C12UL, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch.

8C13, Ch. 30A1; 8C1, Radio Ch. $2-1 \quad P \quad 5 \quad 3$
$8 \mathrm{8C13}, 8 \mathrm{C} 13 \mathrm{~N}, 8 \mathrm{C} 13 \mathrm{~S}, 8 \mathrm{C} 13 \mathrm{SN}, 8 \mathrm{C} 13 \mathrm{~T}, \begin{array}{lllll}3-17 & \mathbf{P} & 5 & 3\end{array}$ $8 \mathrm{C} 13 \mathrm{TN}, 8 \mathrm{C} 13 \mathrm{UL}, \mathrm{Ch} .30 \mathrm{~A} 1,30 \mathrm{~B} 1,30 \mathrm{C} 1$, 30D1; 4H1, Radio Ch.

| 19A1IS, 19A11SN, 19A12S, 19A12SN, 19A15S, 19A15SN, Ch. 19A1 | 3-1 | P | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { 20X11, 20X12, } 20 \times 122, \text { Ch. } 20 \times 1 \text {; } \\ & \text { 4L1, Radio Ch. } \end{aligned}$ | 4-38 | P | 2 | 1 |
| 20X136, 20X145, 20X146, 20X147, Ch. 20 Y1; 4L1, Radio Ch. | 4-38 | P | 2 | 1 |
| 24A12, 24A125, Ch. 20A1 | 4-1 | P | 2 | 1 |
| 24A125AN, Ch. 20X1; 4L1, Radio Ch. | 4-38 | P | 2 | 1 |
| 24C15, 24C16, Ch. 20B1 | 4-1 | P | 2 | 1 |
| 24X15, 24X15S, 24X16, 24X16S, 24X17S, Ch. 20X1; 4Ll, Radio Ch. | 4-38 | P | 2 | 1 |
| 25Al5, 25Al6, 25Al7, Ch. 21Al | 4-1 | P | 2 | 1 |
| 26X35, 26X36, 26X37, Ch. 24D1; 29X16, 29X17, Ch. 24F1 | 4-1 | P | 3 | 2 |
| $30 \mathrm{Al2}, \mathrm{30A12N} 30 \mathrm{Al} 12 \mathrm{~S},, 30 \mathrm{Al2SN}$, | 3-17 | P | 5 | 3 | $30 \mathrm{~A} 12,30 \mathrm{~A} 12 \mathrm{~N}, 30 \mathrm{~A} 12 \mathrm{~S}, 30 \mathrm{~A} 12 \mathrm{SN}$, $30 \mathrm{~A} 12 \mathrm{~T}, 30 \mathrm{~A} 12 \mathrm{TN}, 30 \mathrm{~A} 12 \mathrm{UL}, 30 \mathrm{~A} 13$, $30 \mathrm{~A} 13 \mathrm{~N}, 30 \mathrm{~A} 13 \mathrm{~S}, 30 \mathrm{~A} 13 \mathrm{SN}, 30 \mathrm{~A} 13 \mathrm{~T}$, 30A13TN, 30A13UL, 30A14, 30A14N, $30 \mathrm{~A} 14 \mathrm{~S}, 30 \mathrm{~A} 14 \mathrm{SA}, 30 \mathrm{~A} 14 \mathrm{SN}, 30 \mathrm{~A} 14 \mathrm{~T}$, $30 \mathrm{~A} 14 \mathrm{TN}, 30 \mathrm{~A} 14 \mathrm{UL}$, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch.


| 30 A 15 | $1-1$ | $\mathbf{P}$ | 5 | 3 |
| :--- | :--- | :--- | :--- | :--- |
| 30A15, 30A15N, 30A15S, 30A15SA, <br> 30A15SN, 30A15T, 30A15TN, 30A15UL, | $3-17$ | $\mathbf{P}$ | 5 | 3 |
| Ch. 30A1, 30B1, 30C1, 30D1; 4H1, <br> Radio Ch. |  |  |  |  |

Radio Ch.

| 30 Al 6 | 1-1 | P | 5 | 3 |
| :---: | :---: | :---: | :---: | :---: |
| $30 \mathrm{~A} 16,30 \mathrm{~A} 16 \mathrm{~N}, 30 \mathrm{~A} 16 \mathrm{~S}, 30 \mathrm{~A} 16 \mathrm{SN}$, 30A16T, 30A16TN, 30A16UL, Ch. 30A1, 30B1, 30C1, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| $30 \mathrm{~B} 15 \mathrm{~S}, 30 \mathrm{~B} 15 \mathrm{SN}, 30 \mathrm{~B} 16 \mathrm{~S}, 30 \mathrm{~B} 16 \mathrm{SN}$, $30 \mathrm{~B} 17 \mathrm{~S}, 30 \mathrm{~B} 17 \mathrm{SN}, \mathrm{Ch} .30 \mathrm{~A} 1,30 \mathrm{~B} 1,30 \mathrm{C} 1$, 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| $30 \mathrm{C} 15 \mathrm{~S}, 30 \mathrm{C} 15 \mathrm{SN}, 30 \mathrm{C} 16 \mathrm{~S}, 30 \mathrm{C} 16 \mathrm{SN}$, 30C17S, 30C17SN, Ch. 30A1, 30B1, 30C1. 30D1; 4H1, Radio Ch. | 3-17 | P | 5 | 3 |
| 30F15, Ch. 20B1; 4J1, Radio Ch. | 4-1 | $\mathbf{P}$. | 2 | 1 |
| 30F15A, Ch. 20B1; 4K1, Radio Ch. | 4-1 | P | 2 | 1 |
| 30F16, Ch. 20B1; 4J1, Radio Ch. | 4-1 | P | 2 | 1 |

## ADMIRAL CORP. (Cont'd)

| 30F16A, Ch. 20B1; 4K1, Radio Ch. | $4-1$ | $P$ | 2 | 1 |
| :--- | :--- | :--- | :--- | :--- |
| 30F17, Ch. 20B1; 4J1, Radio Ch. | $4-1$ | $P$ | 2 | 1 |
| 30F17A, Ch. 20B1; 4K1, Radio Ch. | $4-1$ | $P$ | 2 | 1 |
| 36X36, 36X37, Ch. 24E1; 39X16, 39X17, | $4-1$ | P | 3 | 2 | Ch. 24 Gl

AFFILIATED RETAILERS, INC.

| AR-TV-10C, AR-TV-12X, AR-TV-12X | 3-1 | P | 3 | 4 |
| :---: | :---: | :---: | :---: | :---: |
| AR-23-TV-1 | 3-8 | P | 3 | 2 |
| 16CX, 816, 816CR | 5-1 | P | 3 | 4 |
| AIR KING PRODUCTS CO., INC. |  |  |  |  |
| A-1000 | 2-1 | P | 3 | 5 |
| A-1001-A, A-2000, A-2001, A-2002 | 3-1 | P | 2 | 1 |
| 12C1, 12T1, 12T2, Ch. 700 | 5-1 | $\mathbf{P}$ | 2 | 1 |
| 16C1, Ch. 700-1 | 5-3 | $\mathbf{P}$ | 3 | 2 |
| 16C2, Ch. 700-1 | 5-3 | P | 3 | 2 |
| $16 \mathrm{Kl}, \mathrm{Ch} .700-2 ; 507$, Radio Ch. | 5-3 | P | 3 | 2 |
| 16T1, Ch. 700-1 | 5-3 | P | 3 | 2 |
| 712, Ch. 700 | 5-1 | P | 2 | 1 |
| 718R, Ch. 700-1 | 5-3 | P | 3 | 2 |
| $\frac{\text { ALLIED PURCHASING CORP. }}{\text { DIV. OF ALLIED STORES }}$ |  |  |  |  |
| G-16, V16, 616, 816, Same as Tele-King 616 | 5-1 | P | 3 | 4 |
| 910, Same as Tele-King 510 | 4-1 | P | 3 | 4 |
| 912, Same as Tele-King 512 | 3-1 | P | 3 | 4 |
| 1012, Same as Tele-King 612 | 3-1 | P | 3 | 4 |

## ALTEC LANSING CORP.

| ALC201 | $3-1$ | $P$ | 4 | 6 |
| :--- | :--- | :--- | :--- | :--- |
| $202 A$ | $4-1$ | $P$ | 3 | 2 |
| 205 | $4-2$ | $P$ | 3 | 2 |

ANDREA RADIO CORP.

| BCO-VJ12-2, Ch. VJ12-2 | $2-3$ | P | 5 | 3 |
| :--- | :---: | :---: | :---: | :---: |
| BCO-VJ15, Ch. VJ15 | $2-3$ | P | 5 | 3 |
| BT-VK12, Ch. VK12 | $2-8$ | $P$ | 5 | 3 |
| C-VJ12, CO-VJ12, Ch. VJ12, CO-VJ12-2, <br> Ch. VJ12-2 | $2-3$ | $P$ | 5 | 3 |
| CO-VJ15, Ch. VJ15 | $2-3$ | $P$ | 5 | 3 |
| CO-VK15, Corinthian; CO-VK16, Caronia; $2-8$ <br> Ch. VK15-16 | P | 5 | 3 |  |
| CO-VK16 Late, Caronia, Ch. VK-19 | $2-8$ | $P$ | 5 | 3 |
| CO-VK16'C", Dynasty, Ch. VK15-16 | $2-8$ | $P$ | 5 | 3 |

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| ANDREA RADIO CORP. (Cont'd) |  |  |  |  |
| CO-VK124, Edgemont, Ch. VKl24 | 2-8 | P | 5 | 3 |
| CO-VK125, Ridgeway, Ch. VK12 | 2-8 | P | 5 | 3 |
| CVK19, Normandy, Ch. VK-19 | 2-8 | P | 5 | 3 |
| CVK-126, Gramercy, Ch. VK12 | 2-8 | P | 5 | 3 |
| T-VJ12, Ch. VJ12 | 1-1 | P | 5 | 3 |
| TVK12, Saratoga; TVK-127, Sharron; Ch. VK12 | 2-8 | P | 5 | 3 |


| 701 | 2-1 | P | 3 | 5 |
| :---: | :---: | :---: | :---: | :---: |
| 702, 113 AM-FM, Radio | 2-2 | P | 3 | 5 |
| 717, 718, 725, Ch. P-101 | 4-1 | P | 3 | 5 |

## ASSOCIATED MERCHANTS CORP.

| AM510, Same as Tele-King 510 | $4-1$ | $P$ | 3 | 4 |
| :--- | :---: | :--- | :--- | :--- |
| AM712, Same as Tele-King 712 | $4-1$ | $P$ | 3 | 4 |

THE ASTATIC CORP.

| AT-1, Booster | 4-1 | P | 1 |
| :---: | :---: | :---: | :---: |
|  | ATWATER TELEVISION CO. |  |  |
| 135, 513 | 5-1 | P | 3 |


| AR-TV-709 | 2-1 | S-P | 2 | 7 |
| :---: | :---: | :---: | :---: | :---: |
| TV-12-49, TV-12-50 | 4-1 | S-P | 3 | 8 |
| TV-16-49, TV-16-50, TV-16-51 | 3-1 | P | 3 | 2 |
| TV-1205 | 5-5 | S-P | 3 | 8 |
| TV-1205, Series B | 5-1 | P | 1 |  |
| TV-1294 | 5-5 | S-P | 3 | 8 |
| TV-1294, Series B | 5-1 | $\mathbf{P}$ | 1 |  |
| TV-1605, TV-1615 | 5-5 | S-P | 3 | 8 |
| TV-1649, TV-1650, TV-1651, Series B | 5-6 | P | 3 | 2 |
| TV-1694 | 5-5 | S-P | 3 | 8 |
| TV-5001 | 5-2 | P | 1 |  |
| TV-5006 | 5-2 | P | 1 |  |
| TV-5012 | 5-2 | P | 1 |  |
| TV-5061, TV-5077 | 5-2 | P | 1 |  |
| TV-5111 | 5-2 | P | 1 |  |

BACE TELEVISION CORP.

| $16 \mathrm{RCC}, 16 \mathrm{RCH}, 19 \mathrm{RCC}, 19 \mathrm{RCH}$ | $4-1$ | P | 5 | 3 |
| :--- | :--- | :--- | :--- | :--- |
| $150-\mathrm{D}$ | $2-1$ | P | 5 | 185 |
| 160 C | $2-1$ | P | 3 | 5 |
| $160-\mathrm{K}$ | $2-1$ | P | 3 | 5 |


| Model | Rider <br> Man. <br> Page | Type Cir. |  | Sch. |
| :---: | :---: | :---: | :---: | :---: |
| BACE TELEVISION CORP. (Cont'd) |  |  |  |  |
| 160 TM | 2-1 | P | 3 | 5 |
| 190-K, 190-KFD, 190 KHD | 2-1 | P | 3 | 5 |
| BAGDAD TELEVISION CO., INC. |  |  |  |  |
| 19 Tube Set | 2-1 | P | 2 | 1 |
| BELL TELEVISION, INC. |  |  |  |  |
| $\begin{aligned} & \text { 16DD, } 16 \mathrm{~T}, 16 \mathrm{TD}, 19 \mathrm{DD}, 19 \mathrm{~T}, 19 \mathrm{TD} \text {, } \\ & 1502,1503,2002,2003 \end{aligned}$ | 4-1 | P | 3 | 5 |
| $\frac{\text { BELMONT RADIO CORP. }}{\text { (RAYTHEON) }}$ |  |  |  |  |
| Coronet | 3-1 | S-P | 9 | 10 |
| Observer | 3-1 | S-P | 3 | 9 |
| A-7DX22-P, Series A | 4-1 | S-P | 3 | 9 |
| A-10DX22, Observer; A-10DX24, Ch. A, B, C, D; Radio Ch. | 3-1 | S-P | 6 | 10 |
| B-10DX22, Ch. A, B, C, D; Radio Ch. | 3-1 | S-P | 6 | 10 |
| C-1102, Ch. 12 AX 22 | 4-6 | P | 2 | 1 |
| C-1104B, Ch. $12 \mathrm{AX27}$ | 5-1 | P | 3 | 2 |
| C-1401, Ch. 14AX21 | 5-9 | P | 3 | 2 |
| C-1602, Ch. 16AX23, 16AX25, 16AX26 | 5-21 | P | 2 | 1 |
| 7DX21 | 2-6 | S-P | 3 | 9 |
| 7DX21, Series B | 2-6 | S-P | 3 | 9 |
| 10AXF43, Ch. A, B, C, D; Radio Ch. | 3-1 | S-P | 3 | 9 |
| 10DX21, Ch. A, B, C, D; Radio Ch. | 2-1 | S-P | 6 | 10 |
| $\begin{aligned} & \text { 10DX22, 10DX24, Coronet, Ch. A, B, C, } \\ & \text { D; Radio Ch. } \end{aligned}$ | 31-1 | S-P | 6 | 10 |
| 18DX21 | 2-6 | S-P | 3 | 9 |
| 18DX21A | 2-6 | S-P | 3 | 9 |
| 21 A21 | 1-1 | P | 2 | 1 |
| 22A21, 22AX21, 22AX22 | 1-25 | P | 2 | 1 |
| BENDIX RADIO DIV. |  |  |  |  |
| 235 B1 | 2-1 | P | 2 | 1 |
| 235 B1, Codes A, B, C, D, E, F, G, H, I, J, K, L, M, MA, MB, MC, MD | 3-1 | P | 2 | 1 |
| 23M1 | 2-1 | P | 2 | 1 |
| 325M8, Codes A, B, C, D, E, F, G, H, I, J, K, L, M, MA, MB, MC, MD | 3-1 | P | 2 | 1 |
| 2001, 2002, 2020, 2021; 2000 Series | 3-21 | P | 3 | 2 |
| 2025 | 4-1 | P | 3 | 2 |
| 2051 | 5-1 | P | 3 | 2 |
| 3001, 3002, 3030, 3031; 3000 Series | 3-21 | P | 3 | 2 |
| 3033 | 4-1 | P | 3 | 2 |

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| GAMBLE-SKOGMO, INC. |  |  |  |  | GAROD RADIO CORP. (Cont'd) |  |  |  |  |
| FA43-8965A, FA43-8965B | 3-1 | S-P | 3 | 9 | 2043 T | 4-10 | P | 3 | 4 |
| FA43-8966 | 4-1 | S-P | 6 | 10 | 2546 T | 4-10 | P | 3 | 4 |
| TV43-8908 | 4-15 | P | 3 | 2 | 2547 T | 4-10 | P | 3 | 4 |
| TV43-8960 | 3-10 | P | 3 | 2 | 2548 T | 4-10 | P | 3 | 4 |
| 94TV1-43-8940A | 4-21 | P | 2 | 1 | 2549 T | 4-10 | P | 3 | 4 |
| 94TV2-43-8970A, 94TV2-43-8971A | 3-17 | P | 4 | 6 | 3912TVFMP; 11 FMT, Radio | 1-1 | P | 4 | 6 |
| 94TV6-43-8953A | 5-9 | P | 3 | 2 | 3915 TVFMP; 9FMT, Radio | 2-12 | P | 4 | 6 |
| GAROD RADIO CORP. |  |  |  |  | GENERAL ELECTRIC CO. |  |  |  |  |
| 10 TZ 20 , Ambassador: 10 TZ 21, Malibu; 10TZ22, Monticello: 10 TZ 23 , Catalina | 4-5 | P | 4 | 6 | HM-171 | 1-1 | P | 3 | 2 |
|  |  |  |  |  | HM-185 | 1-3 | P | 3 | 2 |
| 12TZ20, Belvedere; 12TZ21, Claridge; 12TZ22, Caronet: 12TZ23, Carlton | 4-5 | P | 4 | 6 | HM-225, HM-225B | 1-14 | P | 2 | 1 |
| 15TZ24: 15TZ25, 15TZ26, $15 \mathrm{TZ27}$ | 4-5 | P | 4 | 6 | HM-226B, HM-226-7A | 1-14 | P | 2 | 1 |
| 19C6, | 5-18 | P | 3 | 4 | $10 \mathrm{C} 101,10 \mathrm{C} 102,10 \mathrm{TI}, 10 \mathrm{~T} 4,10 \mathrm{~T}, 10 \mathrm{~T} 6$ | 5-1 | S-P | 2 | 19 |
| 900 Serzes | 2-1 | P | 4 | 6 | 12C101, 12C102, 12C105 | 5-25 | S-P | 2 | 19 |
| 1000 | 2-1 | P | 4 | 5 | 12C107, 12C108, 12C109 | 5-35 | S-P | 2 | 20 |
| 1042G | 3-7 | P | 3 | 4 | 12C107, 12C108, 12C109, B Version | 5-35 | S-P | 2 | 20 |
| 1042 T | 4-10 | $P$ | 3 | 4 | 12 Kl | 5-12 | S-P | 2 | 19 |
| 1043G | 3-7 | P | 3 | 4 | 12 TI | 5-25 | S-P | 2 | 19 |
| 1043T | 4-10 | $P$ | 3 | 4 | 12T3, 12 T 4 | 5-35 | S-P | 2 | 20 |
| 1100 | 2-1 | P | 4 | 6 | 12T3, i2T4; B Version | 5-35 | S-P | 2 | 20 |
| 1142 | 4-1 | P | 3 | 4 | $800 \mathrm{~A}, 800 \mathrm{~B}, 800 \mathrm{C}, 800 \mathrm{D}$ | 4-1 | S-P | 2 | 18 |
| 1143 | 4-1 | P | 3 | 4 | 801, Early, Late | 1-28 | P | 3 | 2 |
| 1200 | 2-1 | P | 4 | 6 | 802 | 1-52 | $P$ | 4 | 6 |
| 1244 T | 4-12 | P | 3 | 4 | 803 | 2-1 | $P$ | 4 | 6 |
| 1245 T | 4-10 | P | 3 | 4 | 805, Early, S, T, U, W, Versions | 3-1 | S-P | 2 | 18 |
| 1344 | 4-1 | $p$ | 3 | 4 | 806, 807, Early, S, T, U, W, Versions | 3-1 | S-P | 2 | 18 |
| 1345 | 4-1 | P | 3 | 4 | 809, Early, S, T, U, W, Versions | 3-1 | S-P | 2 | 18 |
| 1346 T | 4-11 | P | 3 | 4 | 810 | 2-11 | P | 5 | 5 |
| 154*T | 4-10 | P | 3 | 4 | 811 | 2-11 | P | 5 | 5 |
| 1542 T | 4-10 | P | 3 | 4 | 814 | 2-22 | P | 5 | 5 |
| 1549 I | 4-10 | P | 3 | 4 | 817, S, T, U, W, Versions | 4-9 | S-P | 2 | 18 |
|  | 4-1 | P | 3 | 4 | 818 | 4-24 | S-P | 2 | 18 |
|  | 4-1 | P | 3 | 4 | 820 | 3-16 | $P$ | 5 | 5 |
|  | 4-1 | P | 3 | 4 | $821, \mathrm{~S}, \mathrm{~T}, \mathrm{U}, \mathrm{W}$, Versions | 4-9 | S-P | 2 | 18 |
|  | 4-1 | P | 3 | 4 | 830, Early, R, T, Versions | 3-31 | P | 5 | 5 |
|  | 5-15 | P | 3 | 4 | 835, Eariy, R, Versions | 3-45 | P | 4 | 5 |
|  | 5-18 | P | 3 | 4 | $840$ | 4-34 | P | 5 | 5 |
|  | 4-15 | $P$ | 3 | 4 | 901, Preliminary | 1-73 | P | 5 | 3 |

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| MOTOROLA INC |  |  |  |  | $\frac{\text { NORTH AMERICAN PHILLIPS CO., INC. }}{\text { (NORELCO) }}$ |  |  |  |  |
| $12 \mathrm{VF} 26 \mathrm{~B}, 12 \mathrm{VF} 26 \mathrm{~B}-\mathrm{C}, 12 \mathrm{VF} 26 \mathrm{~K}$, 12VF26R-C, Ch. TS-23A, TS-23B |  | $P$ | 3 | 4 | 160, Protelgram | 3-1 | P |  |  |
| $12 \mathrm{VK} 11,12 \mathrm{VK} 11 \mathrm{~B}, 12 \mathrm{VK} 11 \mathrm{R}$, Ch. TS-23, TS-23A, TS-23B | 4-19 | P | 3 | 4 | OL YMPIC RADIO \& TELEV. INC. |  |  |  |  |
| $12 \mathrm{VK} 15 \mathrm{~B}, 12 \mathrm{VK} 15 \mathrm{R}, \mathrm{Ch} . \mathrm{TS}-30, \mathrm{TS}-30 \mathrm{~A}$ | 5-8 | P | 3 | 4 | DX-214, DX-215, DX-216, Serial No. H-200,001 to H-205,000 | 4-1 | P |  |  |
| $12 \mathrm{VT} 13,12 \mathrm{VT} 13 \mathrm{~B}, 12 \mathrm{VT} 13 \mathrm{R}$, Ch. TS-23, TS-23A, TS-23B | 4-19 | $\mathbf{P}$ | 3 | 4 | $\begin{aligned} & \text { DX-619, DX-620, DX-621, DX-622, } \\ & \text { DX-931, DX-932, DX-950 } \end{aligned}$ | 5-1 | P |  |  |
| $16 \mathrm{~K} 2 \mathrm{~L}, 16 \mathrm{~K} 2 \mathrm{LB}$, Ch. TS-52 | 4-19 | P | 3 | 4 |  | 3-1 |  |  |  |
| 16VK1B, $16 \mathrm{VK1R}$, Ch. TS-52 | 4-19 | P | 3 | 4 | TV-104, Cruzair; TV-105, TV-106, Challenger; TV-107, Pacemaker; TV-108, DeLuxe Ten |  | P |  |  |
| $16 \mathrm{VK} 7 \mathrm{~B}, 16 \mathrm{VK} 7 \mathrm{R}, \mathrm{Ch}$. TS-16, TS-16A | 4-30 | P | 3 | 4 |  |  |  |  |  |
|  |  |  |  |  | TV-922 | 2-1 | P |  |  |
| 19F1, 19F1B, 19K1, Ch. TS-67, TS-67A | 5-22 | P | 3 | 4 | TV-922L, DeLuxe Ten | 3-1 | P | 3 | 2 |
| MULTIPLE TELEV. M | FG. CO |  |  |  | TV-928 | 2-1 | P | 4 | 6 |
| M-1500, M-2000 | 2-1 | P | 4 | 5 | TV-944, Beverly; TV-945, Plaza; TV-946, Champion | 3-1 | P | 3 |  |
| MR-1500, MR-2000 | 2-2 | $\mathbf{P}$ | 4 | 5 | TV-947, Baronet; TV-949, TV-950 | 3-11 | P | 3 | 2 |
|  |  |  |  |  |  |  |  |  |  |
| MT-1250 | 2-1 | P | 4 | 5 | XL-210, XL-211, XL-612, XL-613 | 5-8 | P | 3 | 4 |
| MUNTZ T-V, INC. |  |  |  |  | PACKARD-BELL CO. |  |  |  |  |
| M-12, Ch. M-158 | 3-1 | P | 3 | 4 | 1091, Ch. 3091; 1080, Radio Ch. |  | $P$ | 3 | 5 |
| M-20, M-21, M-22, Ch. M-159-A |  |  |  |  |  | 4-1 |  |  |  |
|  | 3-2 | P | 3 | 4 | 001-TV, 2002-TV |  | P | 3 | 4 |
| M30, Ch. TV16A1; M31, Ch. TV16A2; M31R, M32, Ch. TV16A3 | 5-1 | P | 3 | 4 | $2091 \text {-TV, 2092-TV }$ | 5-3 | P | 3 | 4 |
| M-159, Ch. | 4-1 | $\boldsymbol{P}$ | 3 | 4 | ```2291TV, 2292TV, 2293TV, 2294TV, 2295TV, 2296TV``` | 4-10 | P | 3 | 4 |
| M-159-B, Ch. | 3-3 | P | 3 | 4 | 2297-TV, DeLuxe, Standard; 2298-TV | 4-16 | P | 3 | 4 |
|  |  |  |  |  |  |  |  |  |  |
| M-169, Ch. | 3-4 | P | 3 | 4 | $2601-\mathrm{TV}, 2692-\mathrm{TV}$ | 5-9 | P | 3 | 5 |
| M-169, Ch., Revised | 4-2 | P | 3 | 4 |  | 4-5 | P | 3 |  |
|  |  |  |  |  | 2981, Ch. |  |  |  | 5 |
| NATIONAL CO. ${ }^{\text {INC. }}$ |  |  |  | 23 | 2991-TV | 4-20 | P | 3 | 5 |
| NC-TV-7, NC-TV-7M, NC-TV-7W; <br> 1st Revision <br> 2nd Revision | $\begin{aligned} & 2-1 \\ & 3-1 \\ & 3-3 \end{aligned}$ | S-P | 2 |  | $3191 \mathrm{TV}, 3192 \mathrm{TV}$ | 4-2i | P | 3 | 5 |
|  |  | S-P | 2 | $\begin{aligned} & 23 \\ & 6 \end{aligned}$ |  |  | P | 3 | 5 |
|  |  | P |  |  | 3193TV, 3194TV; 10520, R-F Tuner | 3-1 |  |  |  |
| NC-TV-10C | 4-1 | P | 4 | 6 | 3381 TV | 3-4 | P | 3 | 5 |
| NC-TV-10T | 4-1 | P | 4 | 6 | 4580 TV | 3-12 | $\mathbf{P}$ | 5 | 1 \& 5 |
| TV-1001, TV-1025 | 4-1 | P | 4 | 6 | 4691-TV | 4-23 | P | 5 | 1 \& 5 |
| TV-1201 | 5-3 | P | 4 | 6 | 10527, R-F Tuner | 3-23 | P | 1 |  |
| TV-1226, TV-1601, TV-1625 | 5-3 | P | 4 | 6 | PATHE TELEVISION CORP. |  |  |  |  |
| NEW ENGLAND TELE | v. CO. |  |  |  | 12-2, Ch. 700 | 5-4 | P | 2 | 1 |
| Custom Console THE NIELSEN TELE | 2-1 CORP | P | 4 | 6 | $16-21,16-22,16-23,16-24,16-25$ <br> Ch. 700-1 | 5-9 | P | 3 | 2 |
| 1018 | 2-1 | P | 3 | 5 | PHILCO CORP. |  |  |  |  |
| 1618 | 4-1 | $\mathbf{P}$ | . ${ }^{3}$ | 5 | $\begin{aligned} & \text { 48-700 } \\ & \text { 48-1000, 48-1000-5, Code 125; } \\ & \text { Code 122 } \\ & \text { Code } 121 \end{aligned}$ | 2-1 | P | 3 | 2 |
|  |  |  |  |  |  | 1-1 | P | 3 | 4 |
| NORELCO |  |  |  |  |  | 2-20 | P | 3 | 4 |
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| PHILCO CORP. (Cont'd) |  |  |  |  | PILOT RADIO CORP. (Cont'd) |  |  |  |  |
| 48-1001, Code 121 | 1-17 | P | 3 | 4 | TV-37U | 2-1 | S-P | 2 | 27 |
| 48-1001, Code 122 | 1-17 | P | 3 | 4 | TV-40, TV-42 | 2-8 | P | 5 | 5 |
| 48-2500, Code 122; 48-2500, 48-2500-5 | 1-23 | P | 3 | 4 | TV-44 Series, TV-46, TV-47 | 3-1 | P | 3 | 5 |
| 49-1002 | 2-70 | P | 3 | 2 | TV-120 Series, TV-121 | 3-10 | P | 3 | 2 |
| 49-1040, Code 121 | 3-1 | P | 3 | 2 | TV-125 | 5-1 | $\mathbf{P}$ | 3 | 2 |
| 49-1040, Code 123 | 4-3 | P | 3 | 2 | TV-161 | 5-1 | P | 4 | 6 |
| 49-1075 | 2-70 | S, P | 4 | 12 | TV-950, TV-952 | 2-8 | P | 5 | 5 |
| 49-1075, 49-1076, Code 122 | 4-25 | S, P | 4 | 12 | See INTERSTATE SLTORES BUYING CORP. |  |  |  |  |
| 49-1076, Code 123; 49-1077, Code 122 | 4-3 | S, P | 4 | 12 | RADIO CORP. OF AMERICA |  |  |  |  |
| 49-1150, Codes 121A, 121B, 122A, 122B | 3-4 | P | 3 | 2 | (RCA) |  |  |  |  |
| 49-1150, Codes 123A, 123B, 124A, 124B | 3-19 | $\mathbf{P}$ | 3 | 2 | S1000, Ch. KCS31-1; RC617B, Radio Ch. | 5-48 | P | 3 | 2 |
| 49-1175, Codes 121A, 121B, 122A, 122B | 3-4 | S, P | 4 | 12 | T100, Ch. KCS38 | 5-65 | P | 3 | 2 |
| 49-1175, Codes 123A, 123B, 124A, 124B | 3-19 | S, P | 4 | 12 | T120, Ch. KCS34C | 5-80 | P | 3 | 2 |
| 49-1240 | 2-70 | P | 3 | 2 | T121, Ch. KCs34C | 5-95 | P | 3 | 2 |
| 49-1240, Code 123 | 4-25 | $\mathbf{P}$ | 3 | 2 | TRK-5, Ch. KC-3A; RC-429, Radio Ch. | 1-1 | P | 4 | 5 |
| 49-1240, Code 124 | 4-3 | P | 3 | 2 | TRK-9, Ch. KC-4A, KC-4C; RC-427A, Radio Ch. | 1-14 | P | 5 | 5 |
| 49-1275 | 2-70 | S, P | 4 | 12 |  |  |  |  |  |
| 49-1278, Code 122 | 4-25 | S, P | 4 | 12 | TRK-12, Ch. KC-4, KC-4B; RC-427, Radio Ch. | 1-14 | $\mathbf{P}$ | 5 | 5 |
| $\begin{aligned} & \text { 49-1278, Code 123, 49-1279, Code 122; } \\ & \text { 49-1280, Code 121 } \end{aligned}$ | 4-3 | S, P | 4 | 12 | TRK-90, Ch. KC-4H; RC-427G, Radio Ch. | 1-14 | P | 5 | 5 |
| 49-1450, Codes 121A, 121B | 3-4 | P | 2 | 1 | $\begin{aligned} & \text { TRK-120, Ch. KC-4F, KC-4J; } \\ & \text { RC-427F, Radio Ch. } \end{aligned}$ | 1-14 | P | 5 | 5 |
| 49-1450, Codes 123A, 123B | 3-19 | P | 2 | 1 | TT-5, Ch. KC-3 | 1-1 | P | 4 | 5 |
| 49-1450, Codes 123TA, 123 TB | 3-23 | P | 2 | 1 | 8PCS41, 8PCS41-B, 8PCS41-C, <br> Ch. KCS-24B-1, KCS-24C-1 | 2-1 | P | 7 | $2 \% 6$ |
| 49-1475, Codes 121A, 121B | 3-4 | S, P | 4 | 12 |  |  |  |  |  |
|  |  |  |  |  | 8T241, 8T243, 8T244, Ch. KCS-28 | 3-1 | P | 3 | 2 |
| 49-1475, Codes 123A, 123B | 3-19 | S, P | 4 | 12 | 8T270, Ch. KCS-29; 8TC270, 8 TC271, | 3-15 | $\mathbf{P}$ | 3 | 2 |
| 49-1475, Codes 123TA, 123TB | 3-23 | S, P | 4 | 12 | Ch. KCS-29A |  |  |  |  |
| 49-1480, Codes 121A, 121B | 3-4 | S, P | 4 | 12 | 8TK29, Ch. KCS-32A, KCS-32C; RK-135, RK-135A, Radio Ch. | 3-29 | P | 4 | 3 |
| 49-1480, Codes 123A, 123B | 3-19 | S, P | 4 | 12 |  |  |  |  |  |
| 49-1480, Codes 123TA, 123 TB | 3-23 | S, P | 4 | 12 | 8TK320, Ch. KCS33A-1; RK135A-1, Radio Ch. | 4-1 | $\mathbf{P}$ | 4 | 3 |
| 50-T1104, Code 123 | 4-27 | P | 3 | 4 | 8TR29, Ch. KCS-32, KCS-32B; RK-135, RK-135A, Radio Ch. | 3-29 | P | 4 | 3 |
| 50-T1105, 50-T1106 | 5-1 | P | 3 | 4 |  |  |  |  |  |
|  |  |  |  |  | 8TS30, Ch. KCS-20J-1, KCS-20K-2 | 2-11 | P | 3 | 5 |
| 50-T1400, 50-T1402, 50-T1404 | 4-27 | P | 3 | 4 |  |  |  |  |  |
| 50-T1600, 50-T1632, 50-T1633, Code 121 | 5-17 | P | 3 | 4 | 8TV41, Ch. KCS-25D-1, KCS-25E-2; RK-117A, Radio Ch. | 2-26 | P | 3 | 5 |
| PHILHARMONIC RADIO TV-1049, TV-1249 | $\mathrm{CORP}_{2-1}$ | P | 4 | 6 | 8TV321, 8TV323, Ch. KCS-30-1; RC-616B, RC-616C, RC-616J, RC-616K, Radio Ch. | 3-43 | P | 3 | 2 |
| PHILMORE MFG. CO | , INC. |  |  |  | 9PC41, Ch. KCS24C-1, KCS24D * | 4-16 | $p$ | 7 | 2*6 |
| P30 | 2-1 | $\mathbf{P}$ | 3 | 5 | 9T240, Ch. KCS28; 9 T240K, Ch. KCS28A | 4-26 | P | 3 | 2 |
| PILOT RADIO CORP. |  |  |  |  | 9T246, Ch. KCS28C, KCS38 | 4-41 | P | 3 | 2 |
| TV-37 | 2-1 | S-P | 2 | 27 | 9T256, Ch. KCS38C | 5-1 | P | 3 | 2 |

## RECEIVING TUBE SUBSTITUTION GUIDE

| Model | Rider Man. Page | Type Cir. | No. of Chains | Sch. | Model | Rider <br> Man. <br> Page | Type Cir. | No. of Chains | Sch. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RADIO CORP. OF AMERICA (Cont'd) |  |  |  |  | $\frac{\text { REEVES-SOUNDCRAFT CORP. }}{\text { (VIDEON) }}$ |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| 9T270, Ch. KCS-29, KCS-29C | 3-61 | P | 3 | 2 |  |  |  |  |  |
|  |  |  |  |  | AR-100 | 3-1 | P | 10 | $4,5 \& 6$ |
| 9TC240, Ch. KCS28B | 4-26 | P | 3 | 2 |  |  |  |  |  |
|  |  |  |  |  | REGAL ELECTRONICS CORP. |  |  |  |  |
| 9TC245, Ch. KCS34B; 9TC247, 9TC249, Ch. KCS34, KCS34B | 4-58 | P | 3 | 2 | CD31, CD36 | 3-1 | P | 3 | 5 |
| 9TC272, 9TC275, Ch. KCS-29, KCS-29C | 3-61 | P | 3 | 2 | TV-1030 | 2-1 | P | 3 | 5 |
| 9TW309, Ch. KCS41-1; RK135C, Radio Ch | .5-16 | P | 4 | 6 | TV-1031 | 2-1 | P | 3 | 5 |
| 9TW333, Ch. KCS30-1; RC-616N, Radio Ch. | 4-73 | P | 3 | 2 | 16 T 31 | 3-1 | P | 3 | 5 |
|  |  |  |  |  | $16^{\prime}$ '36 | 3-2 | P | 3 | 5 |
| 9TW390, Ch. KCS31-1; RC617A, Radio Ch. | 5-32 | $\mathbf{P}$ | 3 | 2 | 1007, 1207, 1208 | 3-4 | P | 4 | 3 |
| 621 TS, Ch. KCS-21-1 | 1-44 | $\mathbf{P}$ | 4 | 6 | 1230 | 3-6 | P | 3 | 5 |
| 630TS, Ch. KCS-20A, KCS-20C-2 | 1-76 | $\mathbf{P}$ | 3 | 5 | 1607 | 3-7 | P | 4 | 3 |
| $641 \mathrm{TV}, \mathrm{Ch} . \mathrm{KCS}-25 \mathrm{~A}-1, \mathrm{KCS}-25 \mathrm{C}-2$; RK-117A, Radio Ch. | 1-117 | P | 3 | 5 | See REMINGTON RADIO CORP. |  |  |  |  |
| $\begin{aligned} & \text { 648PTK, Ch. KCS-24-1; RK-121A, } \\ & \text { Radio Ch. } \end{aligned}$ | 1-174 | P | 5 | 3 | $\frac{\text { REMINGTON RADIO CORP. }}{\text { (REMBRANDT) }}$ |  |  |  |  |
| 648PV, Ch. KCS-24A-1; RK-121A, Radio Ch. | 1-174 | P | 5 | 3 | Night Watch, Remington | 4-1 | $\mathbf{P}$ | 2 | 1 |
|  |  |  |  |  | 80, 130 | 1-1 | P | 5 | 3 |
| 721 TCS, Ch. KCS-26A-1, KCS-26A-2 | 1-232 | P | 3 | 2 |  |  |  |  |  |
|  |  |  |  |  | 721, 1606, 1606-15 | 4-1 | P | 2 | 1 |
| 721 TS, Ch. KCS-26-1, KCS-26-2 | 1-232 | P | 3 | 2 |  |  |  |  |  |
|  |  |  |  |  | 1950 | 2-1 | P | 2 | 1 |
| 730TV1, Ch. KCS-27-1; RC-610A, Radio Ch. | 1-255 | P | 4 | 6 | 1950, Revised | 4-1 | P | 2 | 1 |
| 730TV2, Ch. KCS-27-1; RC-610B, Radio Ch. | 1-255 | P | 4 | 6 | REPUBLIC TELEVISION INC. |  |  |  |  |
|  |  |  |  |  | TL-10 | 1-1 | P | 3 | 2 |
| 741 PCS, Ch. KCS-24B-1 | 2-47 | P | 7 | $2 \& 6$ |  |  |  |  |  |
|  |  |  |  |  | SARKES TARZIAN |  |  |  |  |
| RADIO CRAFTSMEN, INC. |  |  |  |  | TT2 | 4-1 | P | 1 |  |
| RC100 | 4-1 | $\mathbf{P}$ | 2 | 1 | TT3 | 4-3 | P | 1 |  |
| RADIO MERCHANDISE SALES, INC. |  |  |  |  | SCOTT RADIO LABS., INC. |  |  |  |  |
| SP-2, Antenna Booster | 3-1 | P | 1 |  | 6-T-11 | 2-1 | P | 4 | 6 |
| SP-4, Preamplifier | 4-1 | P | 1 |  | 13-A | 1-1 | P | 4 | 5 |
| $\frac{\text { RADIO \& TELEVISION INC. }}{\text { (BRUNSWICK) }}$ |  |  |  |  | SEARS, ROEBUCK \& CO. |  |  |  |  |
| C-8125, C-8165 | 4-1 | P | 3 | 4 | 101, Ch. 549.100 | 5-1 | P | 3 | 2 |
| 55B, $55 \mathrm{M}, 55 \mathrm{R}, 5 \mathrm{~W}, \mathrm{Ch} .66 \mathrm{Z}$, Canton | 2-1 | S, P | 4 | 28 | 112, Ch. 478.289 | 5-9 | $\mathbf{P}$ | 4 | 5 |
| 506-B, Ch. 66Z, Tibet; L-14, Radio | 2-1 | S, P | 4 | 28 | 125, Ch. 478.257 | 4-1 | P | 4 | 6 |
| 512, 513 | 4-1 | P | 3 | 4 | 8132, Ch. 101.854 | 3-12 | P | 3 | 2 |
| 702L; 711, Club; Ch. 66Z | 2-1 | S, P | 4 | 28 | 8133, Ch. 101.846; 101.829-1, Radio Ch. | 2-1 | P | 3 | 2 |
| 812, 816 | 4-1 | P | 3 | 4 | 9119, 9120, Ch. 101.865 | 3-23 | P | 3 | 2 |
| 911, 922B, 922M | 3-1 | P | 3 | 5 | 9120A, Ch. 101.865-1; |  |  |  |  |
| 5125, 6165 | 4-1 | P | 3 | 4 | 9120B, Ch. 101.865-2 | 4-37 | $\boldsymbol{P}$ | 2 | 1 |
|  |  |  |  |  | 9121, Ch. 101.867 | 4-10 | P | 2 | 1 |
| See BELMONT RADIO | CORP. |  |  |  | 9122, Ch. 101.864 | 3-12 | P | 3 | 2 |

## receiving tube substitution guide



## RECEIVING TUBE SUBSTITUTION GUIDE

| Model | Rider Man. <br> Page | Type Cir. | No. of Chains | Sch. | Model | Rider Man. Page | Type Cir. | No. of Chains | Sch. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STEWART-WARNER ELECTRIC |  |  |  |  | TECH-MASTER PRODUCTS CO. (Cont'd) |  |  |  |  |
| DIV. OFSTEWART-WARNER CORP. |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | AGC Kit | 4-1 | P | 1 |  |
| AVC1, Code 9054B; AVC2, Code 9054-C | 3-15 | S-P | 6 | 30 |  |  |  |  |  |
| AVC3, Code 9054-B; AVT1, Code 9054-A |  |  |  |  | BC 1223, Blue Ribbon | 4-2 | P | 3 | 2 |
|  |  |  |  |  | TVB, Booster Kit | 4-6 | P | 1. |  |
| T-711, Code 9031-A; T-711M, | 2-1 | $\mathbf{P}$ | 3 | 2 |  |  |  |  |  |
| Code 9031-AM; T-712, Code 9031-B; TRC-721, Code 9037-A |  |  |  |  | 16CK, Conversion Kit | 4-8 | P | 1 |  |
|  |  |  |  |  | 630 TK , Same as RCA 630 TS | 1-76 | P | 1 |  |
| $9100-\mathrm{A}, 9100-\mathrm{B}, 9100-\mathrm{C}, 9100-\mathrm{D}$, | 3-1 | S-P | 5 | 29 |  |  |  |  |  |
| $9100-\mathrm{E}, 9100-\mathrm{F}, 9100-\mathrm{G}, 9100-\mathrm{H}$ |  |  |  |  | 930, 1230 | 3-1 | P | 3 | 5 |
| 9103-B, 9103-C, 9103-E | 4-1 | P | 2 | 1 | 1530, 1630, 1631, 2031 | 3-2 | P | 3 | 5 |
| 9104-A, 9104-B, 9104-C | 4-22 | $\mathbf{P}$ | 2 | 1 | TELECOIN CORP. |  |  |  |  |
| 9106-A, 9106-B | 5-1 | $\mathbf{P}$ | 2 | 1 | (TELE-VID |  |  |  |  |
| 9108-A, 9108-B | 5-15 | P | 2 | 1 | AR-100, Same as Reeves-Soundcraft AR-100 | 3-1 | P | 10 | 4,5\&6 |

## STOLLE ENGINEERING \& MFG. CO.

| Magic Lantern | $3-1$ | $P$ | 3 | 4 |
| :--- | :--- | :--- | :--- | :--- |
| $4830-12$ | $3-2$ | $P$ | 3 | 5 |

STROMBERG-CARLSON CO.

| TC-10, Manhattan | $4-1$ | $P$ | 2 | 1 |
| :--- | :--- | :--- | :--- | :--- |
| TC-19, TC-19 Rev., TC-19-M5M | $5-1$ | $P$ | 4 | 5 |
| TC-125 | $4-5$ | $P$ | 2 | 1 |
| TS-15, TS-16, TS-125, Series | $3-1$ | $P$ | 4 | 5 |
| TV-10L, Ch. 112020, Series 10 | $1-1$ | $P$ | 7 | $4 \& 6$ |
| TV-10L, Ch. 112020, Series 11 | $1-1$ | $P$ | 7 | $4 \& 6$ |
| TV-10LW, Ch. 112020, Series 10 | $1-1$ | $P$ | 7 | $4 \& 6$ |
| TV-10LW, Ch. 112020, Series 11 | $1-1$ | $P$ | 7 | $4 \& 6$ |
| TV-10PM, Ch. 112025, Series 11; | $1-1$ | $P$ | 7 | $4 \& 6$ |
| 1220, Ch. 112022, Radio |  |  |  |  |
| TV-10PY, Ch. 112025, Series 11; | $1-1$ | $P$ | 7 | $4 \& 6$ |
| 1220, Ch. 112022, Radio |  |  |  |  |
| TV-12H1M, TV-12H2A, TV-12H2M, | $1-17$ | $P$ | 3 | 2 |

SYLVANIA ELECTRIC PRODUCTS INC.

| $1-075$, Ch. 1-139 | $4-1$ | $P$ | 2 | 1 |
| :--- | :--- | :--- | :--- | :--- |
| $1-076$, Ch. 1-108 | $5-1$ | $P$ | 2 | 1 |
| $1-090$, Ch. 1-168 | $4-16$ | $P$ | 2 | 1 |
| $1-113,1-114,1-124,1-125$, Ch. 1-139 | $4-1$ | $P$ | 2 | 1 |
| $1-128$, Ch. 1-108 | $5-1$ | $P$ | 2 | 1 |
| $1-177$, Ch. 1-186 | $4-14$ | $P$ | 2 | 1 |
| $1-210$, Ch. 1-139 | $4-1$ | $P$ | 2 | 1 |

TELECRAFT CORP.
15-Inch Set, See RCA 8TS30 $\quad 2-11 \quad P \quad 3 \quad 5$
TELE-KING CORP.

| 210,310 | $2-1$ | $P$ | 5 | 3 |
| :--- | :--- | :--- | :--- | :--- |
| 410 | $3-1$ | $P$ | 3 | 4 |
| 416 | $5-1$ | $P$ | 3 | 4 |
| 510 | $4-1$ | $P$ | 3 | 4 |
| 512 | $3-1$ | $P$ | 3 | 4 |
| 612 | $3-1$ | $P$ | 3 | 4 |
| 612, Revised | $4-1$ | $P$ | 3 | 4 |
| 616 | $5-1$ | $P$ | 3 | 4 |
| 710 | $3-1$ | $P$ | 3 | 4 |
| 712 | $4-1$ | $P$ | 3 | 4 |
| 716 | $5-1$ | $P$ | 3 | 4 |
| 816 | $5-1$ | $P$ | 3 | 4 |

See ELECTRO-TECHNICAL INDUSTRIES

TELE-TONE RADIO CORP.

| 7-Inch AC-DC | $2-1$ | $\mathrm{~S}-\mathrm{P}$ | 3 | 31 |
| :--- | :--- | :--- | :--- | :--- |
| TV-149 | $2-2$ | $\mathrm{~S}-\mathrm{P}$ | 3 | 32 |
| TV-208TR | $3-1$ | $\mathrm{~S}-\mathrm{P}$ | 3 | 17 |
| TV-249 | $2-7$ | P | 4 | 6 |
| TV-254TR, Ch. TK | $4-1$ | P | 2 | 1 |
| TV-255, TV-256, Ch. TS | $4-6$ | P | 3 | 2 |
| TV-284, Ch. TJ | $4-12$ | P | 4 | 5 |
| TV-284 up to Serial \#C12-127, Ch. TH, | $5-2$ | $P$ | 4 | 5 |
| TJ |  |  |  |  |
| TV-286, Ch. TJ | $4-12$ | $P$ | 4 | 5 |

## RECEIVING TUBE SUBSTITUTION GUIDE



## RECEIVING TUBE SUBSTITUTION GUIDE



## RECEIVING TUBE SUBSTITUTION GUIDE



## WILCOX-GAY CORP. (Cont'd)

| OL Series, Serial Nos.Below 26,000 | $5-22$ | P | 3 | 2 |
| :--- | :--- | :--- | :--- | :--- |
| 9V Series | $4-1$ | $P$ | 2 | 1 |
| 9W Series | $4-12$ | S,P | 2 | 34 |

ZENITH RADIO CORP.


FILAMENT SCHEMATICS



ALC FILAMENTS SHOWN ABOVE DERIVE THEIR INPUT FROM POWER TRANSFORMERS

RECEIVING TUBE SUBSTITUTION GUIDE


| No | TYPE | FUNCTION | NO | TYPE | FUNCTION | No | TYPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V1 | 6AU6 | RF AMP. | V12 | 6at6 | AUDIO AMP. | V1 | 6AG5 |
| V2 | 6ag5 | MIXER | V13 | 2516 | AUDIO OUTPUT | V2 | 6.96 |
| $v 3$ | 6.56 | RF OSC. | Vl 4 | 12SN7 | HORIZ. OSC. | $\nabla 3$ | 6au6 |
| v4 | 6ac6 | 1ST. IF AMP. | V15 | 12SN7 | HORIZ. OUTPIST | $V_{4}$ | 6AU6 |
| $v 5$ | 6av6 | 2ND. IF AMP. | $v 16$ | 12SN7 | VERT. OSC. | V5 | 6aUb |
| v6 | 6av6 | 3RD. IF AMP. | V17 | 12SN7 | VERT. OLTPIT | V6 | GADG |
| V7 | OAL5 | VIDEO 2ND. DETECTOR | V18 | 2520 | L.V.RECTIFIER | V7 | 6AL5 |
| v8 | GAU6 | VIDEO AMP. | V19 | $6 \times 5$ | L.V.RECTIFIER | V8 | 12 AU 7 |
| V9 | 6av6 | VIDEO OUTPLTT | V20 | 12SN7 | fi.v. OSC. | V9 | 6au6 |
| V10 | bavo | RATIC DETECTOR DRIVER | v22 | 7JP4 | PICTURE TUBE | V10 | 6AL5 |
| V11 | 6AL5 | RATIO DETECTOR |  |  |  |  |  |



## RECEIVING TUBE SUBSTITUTION GUIDE


(10)


RECEIVANG TUBE SUBSTITUTION GUIDE

receiving tube substitution guide


RECEIVING TUBE SUBSTITUTION GUIDE



## RECEIVING TUBE SUBSTITUTION GUIDE



|  | Iuge | Function |
| :---: | :---: | :---: |
| $v 1$ | 6AU6 | R.F. Mmplifier |
| $v z$ | 6agS | Mixer |
| $\checkmark 3$ | 6 CH | Local oscillator |
| va | 6 AU6 | First vioce I.f. maplifier |
| vs | 6 AU6 | Second video I.f. Anplipier |
| vos | 64.46 | Third video I.F. Amplifier |
| V7 | 6als | video detector-mutomatic Gain Control |
| vo | 6auc | videc amplifier |
| V14 | sau6 | Sync Clipper-D.C. Westorer |
| v9 | gave | 4.5 Mc. Retio Detector oriver |
| V10 | 6als | Ratio Detector |
| V18 | 6at6 | Audio mplifier |
| V19 | 25L6GT/G | audio Output |
| Vi3 | 12SM76T | vertical sweep Generator |
| V12 | 12Sm7GT | vertical swoep output |
| vis | 12SMTGT | Horizontal smeop cenerator |
| V14 | $125176 T$ | Horizontal smeep output |
| $v 20$ | $12 \mathrm{AU7}$ | R.F. High voltage oscillator |
| $v 21$ | 18361/8016 | High voltage mectifier |
| $\checkmark 16$ | 2526GT/G | Low voltage Doubler-D Minus voltage Rectifier |
| v17 | 6×56T/G | Voltage Multiplier |
| $\checkmark 22$ | TJP: | Picture Tube |



## RECEIVING TUBE SUBSTITUTION GUIDE



NOTE:
MODEL 506.0 (TIOET) PAOVO CAPSSIS FILANENTS APE IN APARALCLC APRANGEMFNT.

PICTURE TUPE
RATIO DET.
AUDIO AMP.
AUDIO OUT:
1ST. VIDEO
1ST. VIDEO IF
2ND
2ND. VIDEO IF
3RD. VIDEO
3RD. VIDEO
VIDEO DET.
VIDEO AMP.
VIDEO AMP. AND DC REST.
SYNC. SEP. AND DC REST.
SYNC. AMP. AND HOR. OSC
HOR. SYNC. DISCR.
HOR. OSC. AND DISCH.
HOR. OUT.
ERT. OSC.
VERT, AMP.
RF AMP.
CONVERTER
CONVERT
RF OSC.
$\mathrm{H} . \mathrm{V}$. osc.


## RECEIVING TUBE SUBSTITUTION GUIDE



## SECTION 4

## SERVICING SUGGESTIONS

## Suggestions For Making Adapters

When they are available, the manufacturer's bases and sockets are the thing to use in making adapters but, when this material is not to be had, we have found the following methods very practical.

There is a molded octal socket sold everywhere, which, with the tinned metal mounting removed, fits into the top of a bakelite octal tube base as if made for the purpose. No. 24 or 26 wires are soldered to the socket and pulled down through the tube base pins, soldered and cut off. Bits of spaghetti should be used to avoid shorts. In the case of 12 K 7 and other tubes with top caps,a hole is drilled in the side of the base opposite the grid pin. A flexible wire with grid clip is brought out through this hole to connect the top cap. In case of substituting a loctal for an octal such as the 1 LA6 for 1A7 the grid lead from tube socket is brought out through this hole to connect the top cap.

In case of substituting a loctal for an octal such as the 1LA6 for $1 A 7$, the grid lead from the tube socket is brought out through the side of the base and an old tube cap soldered on. Always select bakelite bases with eight pins. Most octal tubes have only 7 pins or less, but pin 6 is needed in most adapters.

Another, and we believe, better way to make adapters is to remove the 8 pin wafers from the bases of metal tubes. Use No. 18 tinned wire soldering them in the pins first, preferably by dipping, then bend each one so that it will meet the terminal lug on whatever kind of socket is necessary. All of the socket terminal lugs sit down on the bakelite ridge around the wafer and the wires hold them firmly in place.

If 1 R5 tubes are comparatively plentiful and 1A7's are impossible to secure, an adapter can be made easily and quickly as follows:

Select an 8 pin octal base with metal band. With the pliers remove the metal, leaving the bottom wafer and pins. Cut 5 pieces of No. 18 tinned wire $11 / 4$ inches long, dropping them down into pins $2,3,5,6$, and 7 , bending them over enough to avoid their falling through and then solder the ends. Put a piece of spaghetti $3 / 8$ inch long on the wire from pin 6 and bend it flat down on the wafer and across to the pin 3, then straight up. Push the wires through holes in miniature socket lugs as shown in substitution data, bend wires outward and down, then cut off close, clinch with pliers and solder. This makes a rugged adapter with very little danger of shorts. The same procedure is followed in making an adapter to use a 1 T 4 in place of a 1 N 5 . An 8 pin wafer from the base of a metal tube also makes a good adapter.

Adapters are best soldered by dipping. Melt enough solder in a very small pan or tin can lid over an electric or gas hot plate to just touch the ends of the pins on an octal
base when the guide pin is on the bottom. Use a quarterinch dowel pin or piece of shaft, pushing it down inside the guide pin so that it can be used as a handle. Dip the pins for 3 or 4 seconds then lift it out and dip the ends of the pins in water to cool them quickly. This is very much faster and better than doing it one pin at a time with a soldering iron.

To Repair the Filaments in 150 Ma Tubes
(For Emergency Use Only)
Many $150-$ ma heater tubes can be made to give additional service after they have been burned out, that is, after the filament is open. The necessary parts are: a power transformer with a $50-\mathrm{ma}$ secondary that will deliver 750 volts across the high-voltage winding, seven octal sockets, two loctal sockets, and a chassis pan with room enough to mount them. The connections are very simple, as illustrated in the diagram of Fig. 4-1, and require less than two hours to assemble.


NOTE
BOTTOM VIEW OF SOCKETS ARE SHOWN
FIG. 4-1. Illustrating the setup for filament repair.

We have found by experience that putting the push button in the primary side of the transformer, in addition to protecting the operator from shocks, causes a hotter starting arc to weld the broken filament. The six sockets connected in series are for testing the repaired tubes. Put enough tubes in series to make as close as possible to 115 volts and short the filament connections on the remaining sockets that are left empty. Number 3 octal socket is for a 12SQ7, $6 S Q 7$, and a few other types which have their heater connections on pins 7 and 8.

The operation is as follows. Insert the line plug, turn on the switch, and place the tube to be repaired in the proper socket. A low-wattage lamp drawing. current from the same electric circuit should be in front of the operator. Press the button quickly, making as shor t a contact as possible. If the lamp dims, you have welded the ends of the
heater together. If they are not welded, press the button several more times, while snapping at the tube with the fingers of the other hand. If this does not weld the filaments, allow three seconds to elapse when working with metal tubes and then push the button again. Repeat this, then wait ten seconds and press for the last time. The switch contact should be as short as possible each time.

For 6- and 12-volt glass tubes, the same procedure is employed except that you must observe the tube and continue to press the button at intervals until the filament shows light. For higher voltage tubes such as 50L6, 35L6, 35A5, etc. the button must be held down slightly longer. Success has been obtained in repairing about forty percent of burned out $150-$ ma heater tubes which include 12SA7, 12SK7, 12SQ7, $50 \mathrm{~L} 6,35 \mathrm{Z5}$, and almost all other $12-, 14-, 35-$, and 50 -volt heater tubes. The filaments of tubes having current ratings of less than 150 ma will be completely destroyed when burned in this apparatus, and tubes with high current ratings will overload the transformer severely, although in some cases a repair can be made. If the results are not satisfactory, try using a different transformer. Our experience shows, however, that a 750 -volt secondary is the most satisfactory.

We have had many inquiries about the low-wattage lamp mentioned above. This lamp should be not larger than 40 watts and does not have to be connected to the apparatus. It may be the light in the shop where you are working and serves only to show you when the current has welded the ends of the broken filament in a metal tube. When the high voltage passes through the filament, there is a surge of current lasting only a very small fraction of a second. The transformer draws a rather large amount of current from the electric light line, pulling the voltage down and causing the light to blink or flicker. It is not needed in the case of glass tubes since you are able to see when the filament lights.

The average life of repaired tubes is short. We describe this process for use only in case of emergency and in no case recommend the use of a repaired tube when a new one is available. Even when the tube is not available, a repaired tube should be burned for at least one hour before putting it in a customer's radio.

## 35Z5 Tubes

Possibly most service men know this, but it will bear repeating for the benefit of those who do not. The $35 \mathrm{Z5}$ filament is between pins 2 and 7 with a tap brought out to pin 3. This tap is about 5 volts, from pins 2 to 3 and provides current for the pilot light. Operating the radio with burned out pilot light causes this section to burn out and breaks the filament circuit. Pins 2 and 3 may be shorted together so as to use the remaining 30 -volt filament and the tube may still give long service. Check every burned out 35Z5, and if there is continuity between pins 3 and 7 , the tube is still usable.

If it is necessary to use the pilot light, connect a 25- to 30 -ohm resistor from pins 3 to 2, either on the tube base (be careful that it does not short to metal chassis) or on the socket terminals, and the pilot light will light as usual.

## Substitution of Complete Sets of Tubes

Most of the popular $12-, 35-$, and 50 -volt tubes now in use are nearing the end of their lives. Often a customer comes in and pays for a substitute tube and the necessary rewiring job, only to be back again within a week or ten days with another "impossible to get" tube burned out. He may again go to considerable expense to replace that one and have the same thing happen again.

Since most of the 6- and 25 -volt, 0.3 -ampere tubes are comparatively plentiful, a complete changeover job is more practical and satisfactory. Replace 12 SA 7 with 6SA7, $12 S K 7$ with $6 \mathrm{SK} 7,12 \mathrm{SQ} 7$ with $6 \mathrm{SQ} 7,50 \mathrm{~L} 6$ or 35 L 6 or any of the other 25 -volt, 0.3 -ampere output tubes, and 25 Z 5 with 25Z6. The only necessary changes are in connection with the rectifier tube and replacement of the a-c line cord with a line resistor cord of 130 ohms. Red goes to the switch and black to pins 3 and 5 of the $35 Z 5$ socket after removing the pilot light wire from pin 3. Any wire on pin 4 is removed and taped up, 4 is connected to 8 , the line cord resistor and a 25 -ohm resistor are connected to the wire from pin 3 and the other end of resistor to pin 2.
Changing Battery-Operated Radios For Electric Operation
This is not a job for the novice, but any experienced radio serviceman can make the change with very satisfactory results if there is room on the chassis for an additional tube.

First find a location for the rectifier tube, drill a hole and mount the socket. Remove all battery wires. Connect one side of the line cord to pins 2, 3, and 5 of a 117 Z 6 socket; connect the other side of the cord to the A battery switch, ground the other side of the switch and also pin 7 of the 117 Z 6 .

From pins 4 and 8, the cathodes of the rectifier, connect a $1-\mathrm{w}, 1,500$-ohm resistor, R 1 , to the screen grid of the 3Q5 tube or whatever output tube is used. This is the filter resistor and must have a $20-\mathrm{mf}, 150$-volt capacitor, C 1 , from each end of the resistor to ground for 60 -cycle operation, or 40 mf for 25 -cycle operation.

It is quite likely that you will find one end of each tube filament connected to ground. All of these grounds must be removed and the filaments connected in series as shown in Fig. 4-2. The tubes indicated are for a typical battery-operated receiver. The capacitors and resistors connected to pins 2 and 7 may be left where they are, at least for the present. (We are using pin numbers of octal tubes. If the loctal series is used, the filament pins are usually 1 and 8 instead of 2 and 7. The loctal 1LA6 or 1 LC 6 is the equivalent of the octal 1A7, the loctal 1LN5 or 1 LH4 for the octal 1 H 5 , and the loctal 1LA4 or 1LB4 for the octal 1A5 or 1T5.) If there are more tubes than are shown in the diagram, connect their filaments between the 1N5 and the 1H5.


FIG. 4-2. Typical circuit arrangement for changing battery-operated radio to electric operation using a 117 Z 6 GT rectifier tube.

Connect a 2,500 -ohm resistor between the rectifier cathodes and one side of the filament of the output tube. This is the filament dropping resistor and has a filter capacitor of from 40 to 200 mf connected between its low

## RECEIVING TUBE SUBSTITUTION GUIDE

end and ground. This capacitor should be rated at 25 volts because if a tube burns out the voitage rises and might break down a 6- or 12 -volt rated capacitor. The filament dropping resistor should be 10 watts if mounted above the chassis and at least 20 watts if mounted underneath where it cannot radiate the heat so readily. There is a 2,200 -ohm, 16-w flexible resistor, that seems to be quite plentiful, rather low priced, and is very easy to mount since it is insulated.

Wire in the resistors R4 and R5 permanently, and R3 temporarily as it may have to be changed. If a 1 A5 or 1 T5 is used instead of the 3Q5 or 3B5, resistor R4 is omitted. The purpose of R4 and R5 is to bypass the current passed from plate to filament in the output tube and to avoid overloading the other filaments.

Now check the grid resistors. The resistor from the grid of the output tube should go directly to ground and each of the others to its own negative filament, pin 7. The lower end of the volume control is connected either directly or through a resistor to ground, or to a filament (which has been disconnected from ground). Leave it where it is for trial; however, if there is distortion, try returning it to the filament circuit between the 1A7 and 1 H5 for 1.4 -volt bias, or between the 1 H 5 and 1 N 5 for 2.8 -volt bias, leaving it wherever the tone is best.

Now make up a resistor to take the place of a set of tubes. The resistance of each 1.4 -volt filament is approximately 28 ohms, and for the set shown in Fig. 4-2 should be a total of 140 ohms. If it had a 1 A5 or 1 T5 in the output, the resistance would be 28 ohms less, or 112 ohms. If there should be an additional 1.4 -volt tube, it would be 28 ohms more, or 168 ohms. Connect this resistor from pin 2 of the output tube to ground. Put in the rectifier tube, connect the line cord of the set and then turn it on. The voltage across the resistor should be slightly less than 7
volts. If over 7 volts, replace resistor R3 with a lower value. If under 6.2 volts, replace $R 3$ with a higher value. If you have difficulty in getting the correct filament voltage, remember that increasing the capacitance of C1 at the rectifier increases the voltage, and if this capacitor does not have sufficient capacitance you cannot get the correct voltage.

When the voltage has been adjusted, remove resistor R3 and then insert the tubes. The bypass capacitor C4 may already be in the set. If the capacitors are not in and there is a tendency to distort or oscillate, put them in, and make sure that all No. 1 pins of the tubes are grounded to chassis. If the radio does not have a series capacitor in the antenna, it is necessary to put in a 0.01 mf between the antenna and coil to avoid burning out the coil if the antenna should be grounded.

Many other types of rectifiers may be used instead of the 11726 which was chosen as the example because it does not require a resistor line cord. For 25Z6, use a line-cord resistor of 300 ohms , connecting red to switch, black to pins 3 and 5 , and resistor to pin 2; for 3525 and $35 Z 4$ tubes, use a 540 -ohm resistor cord, connecting black to pin 5 , red to switch, and resistor to pin 2; for a $25 \mathrm{Z5}$ tube, use a 300ohm cord, connecting red to switch, black to pins 2 and 5, resistor to pin 1, pin 6 to ground, and the filter resistor to pins 3 and 4. These are the most popular rectifiers, but several others may be used with the proper line-cord resistor.

The grounding system and physical factors of the receiver to be worked on should be examined before attempting the changeover. Some bugs may be expected on the first job so do not be discouraged if it does not work perfectly right at first; a little patience in trying to get rid of the bugs will be well rewarded. Remember that the filaments of tubes in most battery-operated radios are only d-c operated. Always check the filament conditions of the tubes with which you are working.

## SECTION

## CHARTS AND TABLES

In this section a number of charts and tables are shown that we believe will be very helpful to users of this book. Included in this grouping is a complete listing of receiving tube characteristics and bases and also a separate listing of cathode-ray-tube characteristics and bases. In addition such tabulated matter as RTMA capacitor, resistor, and transformer color codes, ballast tube and resistor number-
ing codes, pilot lamps, and a cross index of Army VT numbers and commercial vacuum-tube numbers are included. The last named chart will not only help ArmedForces personnel but will be of valuable aid to anyone who has surplus Army tubes and desires to identify the equivalent commercial number for possible use or substitution in commercial equipment.

## RTMA RECEIVING TUBE RATINGS

It shall be standard to interpret the ratings on receiving types of tubes according to the following conditions:

## 1. CATHODE

The heater or filament voltage is given as a normal value unless otherwise stated. This means that transformers or resistances in the heater or filament circuit should be designed to operate the heater or filament at rated value for full-load operating conditions under average supply-voltage conditions. A reasonable amount of leeway is incorporated in the cathode design so that moderate fluctuations of heater or filament voltage downward will not cause marked falling off in response; also, moderate voltage fluctuations upward will not reduce the life of the cathode to an unsatisfactory degree.

## A. 1.4-VOLT BATTERY TUBE TYPES

The filament power supply may be obtained from drycell batteries, from storage batteries, or from a power line. With dry-cell battery supply, the filament may be connected either directly across a battery rated at a terminal potential of 1.5 volts, or in series with the filaments of similar tubes across a power supply consisting of dry cells in series. In either case, the voltage across each 1.4 -volt section of filament should not exceed 1.6 volts. With power-line or storage-battery supply, the filament may be operated in series with the filaments of similar tubes.

For such operation, design adjustments should be made so that with tubes of rated characteristics, operating with all electrode voltages applied and on a normal line voltage of 117 volts or on a normal storage-battery
voltage of 2.0 volts per cell (without a charger) or 2.2 volts per cell (with a charger), the voltage drop across each 1.4 -volt section of filament will be maintained within a range of 1.25 to 1.4 volts with a nominal center of 1.3 volts. In order to meet the recommended conditions for operating filaments in series from dry-battery, storage-battery, or power-line sources it may be necessary to use shunting resistors across the individual 1.4 -volt sections of filament.

## B. 2.0-VOLT BATTERY TUBE TYPES

The 2.0 -volt line of tubes is designed to be operated with 2.0 volts across the filament. In all cases the operating voltage range should be maintained within the limits of 1.8 volts to 2.2 volts.

## 2. POSITIVE POTENTIAL ELECTRODES

The power sources for the operation of radio equipment are subject to variations in their terminal potential. Consequently, the maximum rating shown on the RTMA Vacuum Tube Data Sheets have been established for certain design center voltages which experience has shown to be representative. The design center voltages to be used for the various power supplies together with other rating considerations are as given below:

## A. A-C OR D-C POWER-LINE SERVICE IN U.S.A.

The design center voltage for this type of power supply is 117 volts. The maximum ratings of plate voltages, screen-supply voltages, dissipations, and rectifier output currents are design maximums and should not be exceeded in equipment operated at a line voltage of 117 volts.

## B. STORAGE-BATTERY SERVICE

When storage-battery equipment is operated withouta charger, it should be designed so that the published RTMA maximum values of plate voltages, screen-supply voltages, dissipations, and rectifier output currents are never exceeded for a terminal potential at the battery source of 2.0 volts per cell. When storage-battery equipment is operated with a charger, it should be designed so that $90 \%$ of the same RTMA values are never exceeded for a terminal potential at the battery source of 2.2 volts.

## C. "B"-BATTERY SERVICE

The design center voltage " $B$ " batteries is the normal voltage rating of the battery block, such as 45 volts, 90 volts, etc. Equipment should be designed so that under no condition of battery voltage will the plate voltages or dissipations ever exceed the recommended respected maximum values shown in the data for each tube type by more than $10 \%$.

## D. OTHER CONSIDERATIONS

1) Class A Amplifiers

The maximum plate dissipation occurs at the 'zerosignal" condition. The maximum screen dissipation usually occurs at the condition where the peak-input signal voltage is equal to the bias voltage.
2) Class $B$ Amplifiers

The maximum plate dissipation theoretically occurs
at approximately $63 \%$ of the "maximum-signal" condition, but may occur practically at any signal voltage value.
3) Converters

The maximum plate dissipation occurs at the "zerosignal" condition and the frequency at which the oscillator-developed bias is a minimum. The screen dissipation for any reasonable variation in signal voltage must never exceed the rated value by more than $10 \%$.
4) Screen Ratings

When the screen voltage is supplied through a series voltage-dropping resistor, the maximum screen voltage rating may be exceeded, provided the maximum screen dissipation rating is not exceeded at any signal condition, and the maximum screen voltage rating is not exceeded, at the maximum-signal condition. Provided these conditions are fulfilled, the screen-supply voltage may be as high as, but not above, the maximum plate voltage rating.

## 3. TYPICAL OPERATION

For many receiving tubes, the data show typical operating conditions in particular services. These typical operating values are given to show concisely some guiding information for the use of each type. They are not to be considered as ratings, because the tube can be used under any suitable conditions within its rating limitations.

## RECEIVING TUBE SUBSTITUTION GUIDE

## RECEIVING TUBE BASES

The diagrams on the following pages show standard socket connections corresponding to the base designations given in the column headed "Socket Connections" in the classified tube-data tables. Bottom views are shown throughout. Terminal designations are as follows:


Alphabetical subscripts D, P, T and HX indicate, respectively, diode unit, pentode unit, triode unit or hexode unit in multi unit types. Subscript M, T or CT indicates filament or heater tap.

Generally when the No. 1 pin of a metal-type tube in Table 1, with the except:on of all triodes, is shown connected to the shell, the No. 1 pin in the glass (G or GT) equivalent is connected to an internal shield.

## R.M.A. TUBE BASE DIAGRAMS

Bottom views are shown. Terminal designations on sockets are shown above.


2 D


3N


4AF


$4 B R$


4 F


$4 Y$


2 N

$3 T$


4AH


4 B



46
(3) (3)


$2 T$


4AA


4AJ


4BB



4 H



5A


22


4AB


4 AM


4BC



4J


(2):

5AA

[^1]

4AC


4AD


4AP
4AT

4BJ




4 K





5AB

## RECEIVING TUBE SUBSTITUTION GUIDE

R.m.a. TUBE BaSE DIagrans

Bottom views are shown.


## RECEIVING TUBE SUBSTITUTION GUIDE

R.M.A. TUBE BASE DIAGRAMS

# RECEIVING TUBE SUBSTITUTION GUIDE 

R.M.A. TUBE BASE DIAGRAMS

## Bottom views are shown.

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5AM |  |  |  | 5AS |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  | 5BT | $5 B U$ |  <br> 5C |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  | 6AX |

## RECEIVING TUBE SUBSTITUTION GUIDE

R.M.A. TUBE BASE DIAGRAMS

Bottom viens are shown.


RECEIVING TUBE SUBSTITUTION GUIDE
R.M.A. TUBE BASE DIAGRAMS

|  |  | Bottom | e shown. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
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|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  | 7R |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## RECEIVING TUBE CHARACTERISTICS

TABLE I-METAL RECEIVING TUBES
Characteristics given in this fable apply to all tubes having type numbers shown, including metal tubes, glass fubes with " $\mathbf{G}$ " suffix, and baniam fubes with " $G$ T" suffix.
Characieristics given "G" and "GT" tubes not listed (not having metal counterparts), see (ables II, VII, VIII and IX.

table i-metal receiving tubes - Continued

| $\mathbf{T}_{\text {ypo }}$ | Name | Socke Connections | Fil. or Heater |  | Capacitance $\mu_{\mu} \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Volts } \end{aligned}$ | Screen Current Mo. | Plate Current Ma. | $\begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}$ | Transconductance Micromhos | Amp. Factor | $\left\|\begin{array}{c} \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}\right\|$ | PowerOulputWatts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| $65 F 7$ | Diode Variable- $\mu$ Pentode | 7AZ | 6.3 | 0.3 | 5.5 | 6 | 0.004 | Class-A Amp. | 250 | - 1.0 | 100 | 3.3 | 12.4 | 700000 | 2050 | - |  |  | 65F7 |
| 6SG7 | Semivariable-u Pentode | 8BK | 6.3 | 0.3 | 8.5 | 7 | 0.003 | H.F. Amp. | 250 | - 2.5 | 150 | 3.4 | 9.2 | Ovar 1 mag. | 4000 |  |  |  | 6SG7, |
| 6SH7 | Sharp Cut-oft Peniode | 8BK | 6.3 | 0.3 | 8.5 | 7 | 0.003 | Class-A Amp. | 250 | - 1.0 | 150 | 4.1 | 10.8 | 900000 | 4900 |  |  |  | $65 \mathrm{H7}$ |
| 65574 | Sharp Cut-off Pentode | 8N | 6.3 | 0.3 | 6 | 7 | 0.005 | Cluss-A Amp. | 250 | - 3.0 | 100 | 0.8 | 3 | 1500000 | 1650 | 2500 |  |  | 6517 |
| $65 \mathrm{K7}$ | Variable- $\mu$ Pentode | 8 N | 6.3 | 0.3 | 6 | 7 | 0.003 | Class-A Amp. | 250 | - 3.0 | 100 | 2.4 | 9.2 | 800000 | 2000 | 1600 |  |  | $65 \mathrm{K7}$ |
| 6507 | Duplex-Diode Triode | 80 | 6.3 | 0.3 | 3.2 | 3.0 | 1.6 | Class-A Amp. | 250 | - 2.0 |  | - | 0.8 | 91000 | 1100 | 100 |  |  | 6507 |
| 6SN7 | Duplex-Diode Triode | 80 | 6.3 | 0.3 | 3.6 | 2.8 | 2.40 | Class-A Amp. | 250 | - 9.0 | - |  | 9.5 | 8500 | 1900 | 16 |  |  | 6SR7 |
| 6557 | Variable- $\mu$ Pentode | 0 N | 6.3 | 0.15 | 5.5 | 7.0 | 0.004 | Class-A Amp. | 250 | $-3.0$ | 100 | 2.0 | 9.0 | 1000000 | 1850 |  |  |  | 6587 |
| 6557 | Duplex-Diode Triode | 90 | 6.3 | 0.15 | 2.8 | 3 | 1.50 | Class-A Amp. | 250 | -9.0 |  |  | 9.5 | 8500 | 1900 | 16 |  |  | 6517 |
| 6SV7 | Diode R.F. Pentode | 7AZ | 6.3 | 0.3 | 6.5 | 6 | 0.004 | Class-A Amp. | 250 | $-1$ | 150 | 2.8 | 7.5 | 800000 | 3400 |  |  |  | 65V77 |
| 6527 | Duplex-Diode Triode | BO | 6.3 | 0.15 | 2.6 | 2.8 | 1.10 | Class-A Amp. | 250 | -3 |  |  | 1.0 | 58000 | 1200 | 70 |  | - | 6587 |
| 6T7 | Duplex-Diode Triode | 7 V | 6.3 | 0.15 | 1.8 | 3.1 | 1.70 | Class-A Amp. | 250 | - 3.0 | - | - | 1.2 | 62000 | 1050 | 65 |  | T | 6T7 |
| 6V6 | Beam Power Amplifier | 7AC | 6.3 | 0.45 | 2.0 | 7.5 | 0.7 | Class-A1 Amp. ${ }^{5}$ | 250 | - 12.5 | 250 | 4.5/7.0 | 45/47 | 52000 | 4100 | 218 | 5000 | 4.5 | 6V6 |
|  |  |  |  |  |  |  |  | Class-AB, Amp. ${ }^{6}$ | 250 | -15.0 | 250 | 5/13 | 70/79 | 60000 | 3750 |  | $10000{ }^{\text {8 }}$ | 10.0 |  |
|  |  |  |  |  |  |  |  |  | 285 | -19.0 | 285 | 4/13.5 | 70/92 | 65000 | 3600 |  | 8000: | 14.0 |  |
| 1611 | Penlode Power Amplifor | 75 | 6.3 | 0.7 |  |  |  | Audio Amp. | Characteristics same as 6F6 |  |  |  |  |  |  |  |  |  | 1611 |
| 1612 | Penlagrid Ampliner | 75 | 6.3 | 0.3 | 7.5 | 11 | 0.001 | Class-A Amp. | 250 | - 3.0 | 100 | 6.5 | 5.3 | 600000 | 1100 | 880 | - |  | 1612 |
| 1620 | Sharp Cut-oft Pentode | 7R | 6.3 | 0.3 |  |  |  | Class-A Amp. |  | Characteristics same as 6.17 |  |  |  |  |  |  |  |  | 1620 |
| 1621 | Power Amplifier Pentode | 75 | 6.3 | 0.7 |  |  |  | Class-AB3 ${ }^{\text {Amp }}{ }^{\text {6 }}$ | 300 | -30.0\| | 300 | 6.5/13 | 38/69 | - | - |  | $4000{ }^{8}$ | 5.0 | 1621 |
| 1621 | Power Amplifier Pentode | 75 | 6.3 |  |  |  |  | Class-A1 Amp. ${ }^{1}$ | 330 | $50{ }^{*}$ |  |  | 55/59 |  |  |  | $5000{ }^{\text {s }}$ | 2.0 |  |
| 1622 | Beam Power Amplifor | 7AC | 6.3 | 0.9 | - |  |  | Class-A1 Amp. | 300 | -20.0 | 250 | 4/10.5 | 86/125 |  |  |  | 4000 | 10.0 | 1622 |
| 1851 | Tolevision Amp. Pentode | 7R | 6.3 | 0.45 | 11.5 | 5.2 | 0.02 | Class-A Amp. | 300 | -2.0 | 150 | 2.5 | 10 | 750000 | 9000 | 6750 | - | - | 1851 |
| 5693 | Sharp Cut-off Pentode | 8 N | 6.3 | 0.3 | 5.3 | 6.2 | 0.005 | Class-A Amp. | 250 | $-3$ | 100 | 0.85 | 3.0 | 1000000 | 1650 |  |  |  | 5693 |
| * Cathode resistor-ahms. |  | ${ }^{1}$ Screen tied to plate. <br> 2 For 6SA7GT use base diagram BAD. |  |  |  |  | ${ }^{3}$ Grid bias-2 valts if seporate osciliator excitation is used. <br> "Also Type "6SJ7Y." |  |  |  |  |  | ${ }^{5}$ Values are for single tube. <br> - Values are for two tubes in push-pull. |  |  |  | 7 Max.-signal value. <br> ${ }^{3}$ Plate-to-plato value. <br> ${ }^{9}$ Ose. grid leak-Scrn res. |  |  |

TABLE II-6.3-VOLT GLASS TUBES WITH OCTAL BASES

| Type | Namo | Socket Connections | Fil. or Heater |  | Copacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volis | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Volis } \end{gathered}$ | Screen CurrenMa . | Plate Current Ma. | $\begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}$ | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c\|} \hline \text { Load } \\ \text { Resilstance } \\ \text { Ohms } \end{array}$ | Powen Oulput Waft: | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlaleGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 C 22 | Triodo | 4AM | 6.3 | 0.3 | 2.2 | 0.7 | 3.60 | Class-A Amp. | 300 | -10.5 |  |  | 11 | 6600 | 3000 | 20 | - |  | $2 \mathrm{C22}$. |
| 6A56 | Triode Power Ampliflor | $6 T$ | 6.3 | 1.0 | - |  |  | Class-A Amp. ${ }^{4}$ | 250 | -45.0 |  | $\cdots$ | 60 | 800 |  | 4.2 | 2500 | 3.75 |  |
|  |  |  |  |  |  |  |  | P.P. Class AB ${ }^{\text {s }}$ | 325 | -68.0 | - |  | 80 | - | 5250 |  | $3000{ }^{\text {6 }}$ | 15.0 | 6A5G |
|  |  |  |  |  |  |  |  | P.P. Class AB ${ }^{\text {b }}$ | 325 | 850* |  |  | 80 | - |  |  | 5000 \% | 10.0 |  |
| 6AB6G | Direct-Coupled Amplifer | 7AU | 6.3 | 0.5 |  |  | - | Class-A Amp. | 250 | 0 |  |  | 3.0 | 40000 | 1800 | 72 | 8000 | 3.5 | 6AB6G |
|  | High- $\mu$ Power-Amplifior Triode | 60 | 6.3 | 0.4 |  | - |  | Plass-A Amp. | 250 | 0 |  | tput | 34.0 |  |  |  |  |  | 6AC5G |
| 6AC5G |  |  |  |  |  |  |  | P.P. Class B | 250 | 0 | - | - | 5.0 | 36700 | 3400 | 125 | 100009 | 8.0 |  |
| 6AC6G | Direct-Coupled Amplifior | 7 AU | 6.3 | 1.1 |  |  | - | Class-A Amp. | 100 | 0 | Input |  | 7.0 | - | 3000 | 54 | 4000 | 3.8 | 6AC6G |
| 6ADSG | High- $\mu$ Triodo | 60 | 6.3 | 0.3 | 4.1 | 3.9 | 3.3 | Class-A Amp. | 250 | - 2.0 | - | - | 0.9 | - | 1500 | 100 | ma. | - | 6ADSG |
| 6AD6G ${ }^{10}$ | Electron-Ray Tube | 7AG | 6.3 | 0.15 |  |  |  | Indicator | 100 |  | 0 for $90^{\circ} ;-23$ for $135^{\circ} ; 45$ for $0^{\circ}$. Targol current 1.5 ma . |  |  |  |  |  |  |  | GADSG 6AD7G |
| 6AD7G | Triode-Pentode | 8AY | 6.3 | 0.85 |  |  |  | Triode Amp. | 250 | -25.0 | - | - | 4.0 | 19000 | 325 | 6.0 |  | - |  | - |
| 6407 G |  |  |  |  |  |  |  | Pentade Amp. | 250 | -16.5 | 250 | 6.5 | 34 | 80000 | 2500 |  | 7000 | 3.2 |  |
| 6AE5G ${ }^{10}$ | Trioda Amplifior | 60 | 6.3 | 0.3 |  |  |  | Class-A Amp. | 95 | -15.0 |  |  | 7.0 | 3300 | 1200 | 4.2 |  |  | 6AESG |
| 6AE6GT ${ }^{10}$ | Twin-Plate Triode whih |  | 6.3 | 0.15 | Remote cut-off |  |  | Class-A Ámp. | 250 | - 1.5 |  | - | 6.5 | 25000 | 1000 | 25 | - | - | 6AEGGT |
|  | Single Grid |  |  |  | Shorp cut-off |  |  | Class-A Amp. | 250 | $-1.5$ |  |  | 4.5 | 35000 | 950 | 33 |  |  |  |

TABLE II-6.3-VOLT GLASS TUBES WITH OCTAL BASES - Continued

| Type | Name | Socket Conneclions | Fil. or Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\left\lvert\, \begin{gathered} \text { Screen } \\ \text { Volts } \end{gathered}\right.$ | Screen Current Ma. | Plate Current Ma. | $\begin{array}{\|c\|} \text { Plale } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c\|} \hline \text { Load } \\ \text { Ressistance } \\ \text { Ohms } \end{array}$ | Power Output Watts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlareGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 6AE7GT ${ }^{\text {Co }}$ | Twin-Input Triode | 7AX | 6.3 | 0.5 | - |  |  | Driver Amplifior | 250 | -13.5 |  |  | 5.0 | 9300 | 1500 | 14 |  |  | 6AE7GT |
| 6AFSG | Triode | 60 | 6.3 | 0.3 |  |  |  | Class-A Amplifier | 180 | -18.0 |  |  | 7.0 | $\cdots$ | 1500 | 7.4 |  |  | 6AF5G |
| 6AF7G | Twin Electron Ray | 8AG | 6.3 | 0.3 | - |  |  | Indicator Tube |  |  |  |  |  |  |  |  |  |  | 6AF7G |
| GAGBG | Power-Amplifer Pentode | 75 | 6.3 | 1.25 |  |  |  | Class-A Amplifier | 250 | -6.0 | 250 | 6.0 | 32 |  | 10000 |  | 8500 | 3.75 | SAGGG |
| 6AH5G | Beam Power Amplifier | 6AP | 6.3 | 0.9 | - |  |  | Class-A Amplifier | 350 | -18 | 250 |  |  | 33000 | 5200 |  | 4200 | 10.8 | 6AH5G |
| 6AH7GT | Twin Triode | 8BE | 6.3 | 0.3 |  |  |  | Converter \& Amp. | 250 | -9.0 | - |  | 121 | 6600 | 2400 | 16 | - |  | 6AH7GT |
| 6AL6G | Baam Power Amplifler | 6AM | 6.3 | 0.9 | - | - |  | Class-A Amplifier | 250 | -14.0 | 250 | 5.0 | 72 | 22500 | 6000 |  | 2500 | 6.5 | 6AL6G |
| 6AL7GT | Electron-Ray Tube | 8CH | 6.3 | 0.15 | - |  | - | Indicator | Outer | edge of to its ele | any of 1 ctrode. | he three il Similar in | minated ard disp. | -5 | d $1 / 16 \mathrm{in}$. min . No patiern | n. outwa with $\qquad$ | ard with +5 6 volts grid. | volts | 6AL7GT |
| 6AQ7GT | Duplex Diode Triode | 8CK | 6.3 | 0.3 | 2.3 | 1.5 | 2.8 | Class-A Amplifier | 250 | - 2.0 | - |  | 2.3 | 44000 | 1600 | 70 | - |  | 6A07GT |
| GARG. | Beam Power Amp. | 6BO | 6.3 | 1.2 | 11 | 7 | 0.55 | Class-A Amplifier | 250 | -22.5 | 250 | 5 | 77 | 21000 | 5400 | 95 |  |  | 6ARG |
| 6AR7GT | Diode Triode | 8 CG | 6.3 | 0.3 | 1.4 | 1 | 2 | Class-A Amplifier | 250 | $-2$ |  |  | 1.3 | 66500 | 1050 | 70 |  | - | 6AR7GT |
| 6AS7G | Low-Mu Twin Triode | 8BD | 6.3 | 2.5 |  |  |  | D.C. Amplifier | 135 | 250* |  |  | 125 | 280 | 7500 | 2.1 |  |  |  |
| GAS7G | Low-Mu Twin Triode | 880 | 6.3 | 2.5 |  |  |  | Class-Al Amp. P.P. | 250 | 2500* |  |  | 100/106 | 280 | 2259 |  | $6000{ }^{6}$ | 13 | 6AS7G |
| 684G | Triode Power Amplifier | 55 | 6.3 | 1.0 |  |  | - | Power Amplifiler |  |  | aracleristi | tics same | as Type 6A | 3-Table IV |  |  |  |  | 684G |
| 686G | Duplex-Diode High - $\mu$ Triode | 7 V | 6.3 | 0.3 | 1.7 | 3.8 | 1.7 | Detec:or-Amplifer |  |  | haracteris | stics same | as Type 75 | -Table IV |  |  |  | - | 686G |
| 6BQ6GT | Beam Pentode | 6AM | 6.3 | 1.2 |  |  |  | Deflection Amp. | 250 | 47* | 150 | 2.1 | 45 |  | 5500 |  |  |  | 6B96GT |
| 68G6 | Beam Power Amplifier | 5Bt | 6.3 | 0.9 | 11 | 6.5 | 0.5 | Deflection Amp. | 400 | -50 | 350 | 6.0 | 70 | - | 6000 |  |  |  | 6BG6 |
| 6 CBG | Twin Triode | 8 G | 6.3 | 0.3 |  |  |  | Amp. 1 Section | 250 | -4.5 |  |  | 3.1 | 26000 | 1450 | 38 |  |  | 6C8G |
| 608 G | Pentagrid Converter | 8 A | 6.3 | 0.15 |  |  |  | Converter | 250 | - 3.0 | 100 | Catho | de current | 13.0Ma. | Anode 9 | grid (No. | 2) Volts $=2$ | $250{ }^{3}$ | 6D8G |
| 6F8G | Triode-Hexode Converter | 80 | 6.3 | 0.3 | - |  |  | Converter | 250 | $-2.0$ |  |  |  | Triode Plate | 150 volts |  |  |  | 6E8G |
| - 6 FEG | Twin Triode | 8G | 6.3 | 0.6 |  |  |  | Ampliner | 250 | -8.0 | - |  | 91 | 7700 | 2600 | 20 | $\cdots$ |  | 6 F\&G |
| 6G6G | Pentode Power Amplifier | 75 | 6.3 | 0.15 |  |  |  | Class-A Amplifier | 180 | -9.0 | 180 | 2.5 | 15 | 175000 | 2300 | 400 | 10000 | 1.1 |  |
| 6G6G | Penlode Power Amplifier | 75 | 0.3 | 0.15 |  |  |  | Class-A Amplifier | 180 | -12.0 |  |  |  | 4750 | 2000 | 9.5 | 12000 | 0.25 | 6G6G |
| 6 H 4 GT | Diode Rectifier | 5AF | 6.3 | 0.15 |  | - | - | Delector | 100 | - | - | - | 4.0 | $\square$ | - | - | - |  | 6H4GT |
| 6 H 8 G | Duo-Diodo High- Pentode | 8 E | 6.3 | 0.3 | - |  | - | Closs-A Amplifier | 250 | -2.0 | 100 |  | 8.5 | 650000 | 2400 | - |  |  | 6H8G |
| $618 \mathrm{G}^{10}$ | Triode Heptode | 8 H | 6.3 | 0.3 |  |  | - | Converter | 250 | $-3.0$ | 100 | 2.8 | 1.2 | Anode-g | grid (No. 2) | 250 volts | $\mathrm{s}_{\text {max. }}{ }^{3} \mathrm{~m}$ |  | 6J8G |
| $6 \mathrm{~K} 5 \mathrm{GT}{ }^{\text {IM }}$ | High $-\mu$ Triode | 50 | 6.3 | 0.3 | 2.4 | 3.6 | 2.0 | Class-A Amplifier | 250 | - 3.0 |  |  | 1.1 | 50000 | 1400 | 70 | , | . | 6K5GT |
| 6 KGGT | Pentode Power Amplifier | 75 | 6.3 | 0.4 |  |  |  | Class-A Amplifier |  |  |  | Charac | teristics sam | ne as Type 4 | 1-Tabla iV |  |  |  | 6K6GT |
| 615 G | Itiode Amplifier | 60 | 6.3 | 0.15 | 2.8 | 5.0 | 2.8 | Class-A Amplifier | 250 | - 9.0 | - |  | 8.0 | - | 1900 | 17 | - |  | 6L5G |
| 6 MGG | Power Amplifier Pentode | 75 | 6.3 | 1.2 |  |  |  | Class-A Amplifier | 250 | -6.0 | 250 | 4.0 | 36 |  | 9500 |  | 7000 | 4.4 | 6M6G |
| 6 MFG | Pentode Amplifier | 7 R | 6.3 | 0.3 |  |  | - | R.F. Amplifier | 250 | -2.5 | 125 | 2.8 | 10.5 | 900000 | 3400 |  | - |  | 6M7G |
| 6 MEGT | Diode Triode Pentode | 8 AU | 6.3 | 0.6 |  |  |  | Triode Amplifier | 100 |  |  |  | 0.5 | 91000 | 1100 |  |  |  | GM8GT |
|  |  |  |  |  |  |  |  | Pentode Amplifier | 100 | -3.0 | 100 | $\underline{\square}$ | 8.5 | 200000 | 1900 |  |  |  | SM8 |
| 6N6G ${ }^{\text {-1 }}$ | Diract-Coupled Amplifier | TAU | 6.3 | 0.8 |  |  |  | Power Amplifier |  |  | aracterist | tics same | as Type 6B | 5-Table IV |  |  |  |  | 6N6G |
| 6P5GT: | Triode Amplifier | 60 | 6.3 | 0.3 | 3.4 | 5.5 | 2.6 | Class-A Amplifer | 250 | -13.5 | - | - | 5.0 | 9500 | 1450 | 13.8 | - | - | 6P5GT |
| 6P7 G ${ }^{16}$ | Triode-Pentode | 70 | 6.3 | 0.3 |  |  |  | Class-A Amplifier |  |  |  | Char | acteristics s | ame as 6F7- | Table IV |  |  |  | 6P7G |
| 6P8G | Triode-Hexode Converter | sk | 6.3 | 0.8 | - |  |  | Converter | 250 | $-2.0]$ | 75 | 1.4 | 1.5 |  | riode Plate 1 | $00 \mathrm{v}$. | 2 ma . |  | 6PBG |
| 6069 | Diode-Triode | 6r | 6.3 | 0.15 |  |  |  | Class-A Amplifier | 250 | -3.0 | - | - | 1.2 | - | 1050 | 65 |  |  | 606 G |
| 6R6G | Pentode Amplifier | 6AW | 6.3 | 0.3 | 4.5 | 11 | 0.007 | Class-A Amplifier | 250 | -3.0 | 100 | 1.7 | 7.0 | - | 1450 | 1160 | - | - | 6R6G |
| 656GT | Remote Cut-off Pentode | 5AK | 6.3 | 0.45 |  |  | - | R.F. Amplifier | 250 | -2.0 | 100 | 3.0 | 13 | 350000 | 4000 |  |  |  | 656 GT |
| 658GT | Triplo Diode Triode | 8 CB | 6.3 | 0.3 | 1.2 | 5 | 2 | Class-A Amplifier | 250 | -2.0 |  |  | 0.9 | 91000 | 1100 | 100 |  |  | 658GT |
| 6SD7GT | Medium Cut-off Pentode | 8 M | 6.3 | 0.3 | 9 | 7.5 | . 0035 | R.F. Amplifier | 250 | -2.0 | 100 | 1.9 | 6.0 | 1000000 | 3600 |  | $\underline{-}$ |  | 6SD7GT |
| 6SE7GT | Sharp Cui-off Pentode | 8N | 6.3 | 0.3 | 8 | 7.5 | . 005 | R.F. Amplifier | 250 | - 1.5 | 100 | 1.5 | 4.5 | 1100000 | 3400 | 3750 | - | - | 6SE7GT |
| 6SH7L | Pentode R.F. Amp. | 8BK | 6.3 | 0.3 | - |  | - | Class-A Amplifier | 100 | -1.0 | 100 | 2.1 | 5.3 | 350000 | 4000 |  | - |  | 6SH7L |
| 6SL7GT | Twin Triode | 8BD |  |  |  |  |  |  | 250 | - 1.0 | 150 | 4.1 | 10.8 | 900000 | 4900 |  |  |  |  |
| 6SN7GT | Twin Triode |  | 6.3 | 0.3 |  |  | - | Closs-A Ampifiner | 250 | - 2.0 | - |  | 2.31 | 44000 | 1600 | 70 | - |  | 6SLTGT |
|  | Twin Triode | 88 D | 6.3 | 0.6 | - | - | - | Class-A Amplifer | 250 | - 8.0 | - | - | 9.01 | 7700 | 2600 | 20 | - | - 6 | GSNTGT |

TABLE II-G.3-VOLT GLASS TUBES WITH OCTAL BASES - Continued


TABLE III-7-VOLT LOCK-IN-BASE TUBES
For other lock-in-base types soe Tables VIII, IX, and X

| Type | Name | Socket Connections | Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Voits } \end{gathered}$ | Screen Current Ma. | Plate Current Mo. | $\begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}$ | Transconductance Micromhos | Amp. Factor | $\left\|\begin{array}{c} \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}\right\|$ | PowerOutputWalts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 744 | Triode Amplifier | 5AC | 7.0 | 0.32 | 3.4 | 3 | 4 | Class-A Amplifer | 250 | -8.0 |  |  | 9.0 | 7700 | 2600 | 20 |  |  | 7 A 4 |
| 7 AS | Beam Power Amplifior | 6AA | 7.0 | 0.75 | 13 | 7.2 | 0.44 | Class-A, Amplifer | 125 | - 9.0 | 125 | 3.2/8 | 37.5/40 | 17000 | 6100 |  | 2700 | 1.9 | 7A5 |
| 7A6 | Twin Diode | 7AJ | 7.0 | 0.16 |  |  |  | Rectifier |  |  | Max. | A.C. volts | per plate- | 150. Max. O | utput current- | 10 ma |  |  | 746 |
| 7 A 7 | Remota Cut-off Pentode | 8 V | 7.0 | 0.32 | 6 | 7 | . 005 | Class-A Amplifer | 250 | - 3.0 | 100 | 2.0 | 8.6 | 800000 | 2000 | 1600 | - |  | $7 \mathrm{7A}$ |
| 7As | Multigrid Converter | 80 | 7.0 | 0.16 | 7.5 | 9.0 | 0.15 | Converter | 250 | - 3.0 | 100 | 3.1 | 3.0 | 50000 | Anode | -grid 25 | 50 volts max | x. ${ }^{1}$ | 7A8 |
| 7AD7 | Pentode | 8 V | 6.3 | 0.6 | 17.5 | 7.5 | 0.03 | Class-A, Amp. | 300 | 68* | 150 | 7.0 | 28.0 | 300000 | 9500 | - |  |  | 7AD7 |
| 7 AF7 | Twin Triose | 8AC | 6.3 | 0.3 | 2.2 | 1.6 | 2.3 | Class-A Amp. | 250 | -10 | - |  | 9.0 | 7600 | 2100 | 16 |  |  | 7 AF7 |
| $7 \mathrm{AG7}$ | Sharp Cut-off Pentode | BV | 7.0 | 0.16 | 7.0 | 6.0 | 0.005 | Class-A, Amp. | 250 | $250 *$ | 250 | 2.0 | 6.0 | 750000 | 4200 |  |  |  | 7AG7 |
| 7 AH7 | Pentode Amplitier | 8 V | 6.3 | 0.15 | 7.0 | 6.5 | 0.005 | Class-A1 Amplifier | 250 | 250* | 250 | 1.9 | 6.8 | 1000000 | 3300 |  |  |  | 7AH7 |
| 784 | High- $\mu$ Triode | SAC | 7.0 | 0.32 | 3.6 | 3.4 | 1.6 | Class-A Amplifier | 250 | -2.0 |  |  | 0.9 | 66000 | 1500 | 100 | - |  | 784 |
| 785 | Pentode Power Amplifier | 6A:' | 7.0 | 0.43 | 3.2 | 3.2 | 1.6 | Class-A Amplifier | 250 | -18.0 | 250 | 5.5/10 | 32/33 | 68000 | 2300 | - | 7600 | 3.4 | 785 |
| 786 | Duo-Diode Triode | 8W | 7.0 | 0.32 | 3.0 | 2.4 | 1.6 | Class-A Amplifer | 250 | - 2.0 |  |  | 1.0 | 91000 | 1100 | 100 |  |  | 786 |
| 787 | Remote Cul-off Pentode | 8 V | 7.0 | 0.16 | 5 | 7 | . 005 | Class-A Amplifor | 250 | - 3.0 | 100 | 2.0 | 8.5 | 700000 | 1700 | 1200 | - |  | 787 |
| 788 | Pentagrid Converter | 8 X | 7.0 | 0.32 | 10.0 | 9.0 | 0.2 | Converter | 250 | - 3.0 | 100 | 2.7 | 3.5 | 360000 | Anode | -grid 25 | 0 volis max |  | $7 \mathrm{B8}$ |
| $7 \mathrm{C5}$ | Tefrode Power Amplifier | 6AA | 7.0 | 0.48 | 9.5 | 9.0 | 0.4 | Class-A1 Amplifier | 250 | -12.5 | 250 | 4.5/7 | 45/47 | 52000 | 4100 | - | 5000 | 4.5 | $7 \mathrm{C5}$ |
| 7 Cb | Duo-Diode Triade | 8W | 7.1 | 0.16 | 2.4 | 3 | 1.4 | Class-A Amplifior | 250 | - 1.0 |  |  | 1.3 | 100000 | 1000 | 100 |  |  | $7 \mathrm{C6}$ |
| $7 \mathrm{C7}$ | Pontode Amplifier | 8 V | 7.0 | 0.16 | 5.5 | 6.5 | . 007 | Class-A Amplifier | 250 | - 3.0 | 100 | 0.5 | 2.0 | 2 meg . | 1300 |  | - | - | 707 |
| $7 \mathrm{D7}$ | Triode-Hexode Converter | 8AR | 7.0 | 0.48 |  |  |  | Convertor | 250 | -3.0] |  |  | Triod | Plate (No. 3 | 150 v .3 .5 m | ma. |  |  | 707 |

TABLE III-T-VOLT LOCK-IN-BASE TUBES-Continued

| Type | Name | Sockel Connections | Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plafe Supply Volts | Grid Bias | Screen Volis | Screen Current Ma. | Plate Current Mo. | $\begin{array}{\|c\|} \hline \text { Plate } \\ \text { Resistance } \\ \text { Olims } \end{array}$ | Transconductance Micromhos | Amp. Factor | $\left.\begin{array}{\|c\|} \text { Load } \\ \text { Resisfance } \\ \text { Ohms } \end{array} \right\rvert\,$ | Power Output Wotts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 7E6 | Duo-Diode Triode | 8W | 7.0 | 0.32 |  |  |  | Class-A Amplifier | 250 | - 9.0 |  | $\square$ | 9.5 | 8500 | 1900 | 16 | - | - | 7E6 |
| $7 E 7$ | Duo-Diode Pentode | BAE | 7.0 | 0.32 | 4.6 | 4.6 | . 005 | Class-A Amplifier | 250 | - 3.0 | 100 | 1.6 | 7.5 | 700000 | 1300 |  |  |  | $7 E 7$ |
| 7F7 | Twin Triade | OAC | 7.0 | 0.32 |  | - |  | Class-A Amplifier ${ }^{\text {2 }}$ | 250 | $-2.0$ |  |  | 2.3 | 44000 | 1600 | 70 |  |  | 7F7 |
| 7 Fs | Twin Triade | 8BW | 6.3 | 0.30 | 2.8 | 1.4 | 1.2 | R.F. Amplifier | 250 | -2.5 | - | - | 10.0 | 10400 | 5000 |  |  |  | 7F8 |
|  |  |  |  |  |  |  |  |  | 180 | - 1.0 |  |  | 12.0 | 8500 | 7000 |  |  |  |  |
| $\begin{aligned} & 7 G 71 \\ & 1232 \end{aligned}$ | Sharp Cut-off Pentade | 8 V | 7.0 | 0.48 | 9 | 7 | . 007 | Class-A Amplifler | 250 | - 2.0 | 100 | 2.0 | 6.0 | 800000 | 4500 | - | - | $\cdots$ | $\begin{aligned} & 767 / \\ & 1232 \end{aligned}$ |
| $\begin{aligned} & 768 / \\ & 1206 \end{aligned}$ | Dual Tetrode | 8BV | 6.3 | 0.30 | 3.4 | 2.6 | 0.15 | R.F. Amplifier ? | 250 | - 2.5 | 100 | 0.8 | 4.5 | 225000 | 2100 | - | - | - | $\begin{aligned} & 768 / \\ & 1206 \end{aligned}$ |
| 7H7 | Semi-Variable- Pentode | 8 V | 7.0 | 0.32 | 8 | 7 | . 007 | R.f. Amplifier | 250 | -2.5 | 150 | 2.5 | 9.0 | 1000000 | 3500 | - | - | - | 7H7 |
| 757 | Triode-Heptode Converter | BAR | 7.0 | 0.32 |  |  |  | Converiter | 250 | -3.0 | 100 | 2.9 | 1.3 | Triode Plate 250 v. Max. ${ }^{1}$ |  |  |  |  | 737 |
| $7 \mathrm{K7}$ | Duo-Diode High- $\mu$ Triode | 8Bf | 7.0 | 0.32 |  |  |  | Class-A Amplifier | 250 | - 2.0 |  |  | 2.3 | 44000 | 1600 | 70 |  |  | $7 \mathrm{K7}$ |
| 717 | Sharp Cul-off Pentode | 8 V | 7.0 | 0.32 | 8 | 6.5 | . 01 | Class-A Amplifier | 250 | $-1.5$ | 100 | 1.5 | 4.5 | 100000 | 3100 | Cathode Resistor 250 ohms |  |  | 717 |
| 7N7 | Twin Triode | BAC | 7.0 | 0.6 | $\begin{aligned} & 3.4 \\ & 2.9 \end{aligned}$ | $\begin{aligned} & 2.05 \\ & 2.4 \end{aligned}$ | $\begin{array}{l\|} \hline 3.0{ }^{3} \\ 3.0 \cdot \end{array}$ | Class-A Amplifier ${ }^{2}$ | 250 | -8.0 |  | - | 9.0 | 7700 | 2600 | 20 |  | - | 7N7 |
| 707 | Pentagrid Converter | 8AL | 7.0 | 0.32 |  |  | - | Converter | 250 | 0 | 100 | 8.0 | 3.4 | 800000 | Grid No. 1 resistor 20000 ohms |  |  |  | 7197 |
| 7R7 | Duo-Diode Pentode | 8AE | 7.0 | 0.32 | 5.6 | 5.3 | . 034 | Class-A Amplifier | 250 | - 1.0 | 100 | 1.7 | 5.7 | 1000000 | 3200 | - | - 1 |  | 7R7 |
| 757 | Triode Hexode Converter | 8BL | 7.0 | 0.32 |  | 二- | - | Converrer | 250 | - 2.0 | 100 | 2.2 | 1.7 | 2000000 | Triode Plate 250 v. Max. ${ }^{\text {I }}$ |  |  |  | 757 |
| 777 | Pentode Amplifer | 8 V | 7.0 | 0.32 | 8 | 7 | . 005 | Class-A Amplifer | 250 | $-1.0$ | 150 | 4.1 | 10.8 | 900000 | 4900 | - | - | - | 757 |
| 7V7 | Sharp Cuf-off Pentode | 8 V | 7.0 | 0.48 | 9.5 | 6.5 | . 004 | Class-A Amplifier | 300 | 160* | 150 | 3.9 | 10 | 300000 | 5800 | - | - | - | 7V7 |
| 7W7 | Sharp Cut-off Pentode | 8BJ | 7.0 | 0.48 | 9.5 | 7.0 | . 0025 | Class-A Amplifer | 300 | - 2.2 | 150 | 3.9 | 10 | 300000 | 5800 |  |  | - | 767 |
| 7X7 | Duo-Diode Triode | BB2 | 6.3 | 0.3 |  |  | - | Class-A A mplifier | 250 | - 1.0 |  |  | 1.9 | 67000 | 1500 | 100 | - |  | 7×7 |
| 1231 | Pentode Amplifier | 8 V | 6.3 | 0.45 | 8.5 | 6.5 | . 015 | Class-A Amplifier | 300 | 200* | 150 | 2.5 | 10 | 700000 | 5500 | 3850 | - |  | 1231 |
| 1273 | Nonmicrophonic Pentode | 8 V | 7.0 | 0.32 | 6.0 | 6.5 | . 007 | Class. A ${ }_{1}$ Amplifier | 250 | $\begin{array}{r}10 \\ -3.0 \\ \hline-10\end{array}$ | 100 | 0.7 | 2.2 | 1000000 | 1575 | - | - - | - | 1273 |
| 5679 | Twin Diode | 7 CX | 6.3 | 0.15 |  |  | - | V.T.V.M. Rectifjer | 100 | - 1.0 | 100 | 1.8 | 5.7 | 400000 | 2275 |  |  |  | 5679 |
| XXL | Trinde Oscillator | SAC | 7.0 | 0.32 | - | - | -- | Oscillator | 250 | -8.0 | - | - | 8.0 | - | 2300 | 20 | - | $\square$ | XXI |

* Cathode resistor-ohms.

Applied through 20000-ohm dropping resistor.
Each section.
${ }_{3}$ Triod. No. 1.
1 Triode No. 2.
TABLE IV-6.3-VOLT GLASS RECEIVING TUBES

| Type | Name | Base | Socket Connections | Fil. or Healer |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Volts } \end{gathered}$ | Screen Current Ma. | $\begin{gathered} \text { Plate } \\ \text { Current } \\ \text { Ma. } \end{gathered}$ | $\begin{array}{\|c} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c} \text { Loed } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Power Oulput Watts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volis | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \hline 2 \mathrm{C21/f} \\ & 1642 \\ & \hline \end{aligned}$ | Iwin-Triode Amplifior | M. | 7BH | 6.3 | 0.6 | - | - | - | Class-A Amp. | 250 | -16.5 | - | - | 8.3 | 7600 | 1375 | 10.4 | - |  | $\begin{aligned} & \text { 2C21/ } \\ & 1642 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  | Cless-A Amp. | 250 | -45 |  |  | 60 | 800 | 5250 | 4.2 | 2500 | 3.5 |  |
| 6 A3 | Triode Power Amplifier | M. | 40 | 6.3 | 1.0 | 7.0 | 5.0 | 16.0 | Class $\mathrm{AB}_{1} \mathrm{Amp}^{\text {mad }}$ | $\begin{array}{r} 300 \\ 300 \\ \hline \end{array}$ | $\begin{array}{r} -62 \\ 850 \end{array}$ |  | dBias Bias | $\begin{aligned} & 80 \\ & 80 \\ & \hline \end{aligned}$ | -- | - | - | $\begin{aligned} & 3000111 \\ & 500011 \end{aligned}$ | $\begin{array}{r} 15 \\ 10 \\ \hline \end{array}$ | 6 A3 |
| 6 644 ${ }^{6}$ | Pentode Power Amplifier | M . | 5B | 6.3 | 0.3 |  |  |  | Class-A Amp. | 180 | -12.0 | 180 | 3.9 | 22 | 00000 | 2500 | 150 | 3000 | 1.5 | 6A4 |
| 6A6 | Twin Trione Amplifier | M. | 78 | 6.3 | 0.8 |  |  | - | Class-B Amp. P.P | $\begin{aligned} & 250 \\ & 330 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\square$ | $\square$ | powar | deutis for load, plate | $\begin{aligned} & \text { One fube at } \\ & \text {-to-plate } \end{aligned}$ | stated | $\begin{array}{r} 8000 \\ 10000 \end{array}$ | $\begin{array}{r} 8.0 \\ 10.0 \\ \hline \end{array}$ | 6A6 |
| - ${ }^{\text {A } 7}$ | Pentagrid Converter | S. | 7 C | 6.3 | 0.3 | 8.5 | 9.0 | 0.3 | Convomar | 250 | - 3.0 | 105 | 2.2 | 3.5 | 360000 | Anode gris | 1 (No. 2 | 2) 200 volis | max. | 647 |
| GABS/6NS | Elactron-Roy Tube | S. | 6R | 6.3 | 0.15 |  |  |  | Indicator Tube | 180 | Cut-off | Grid Bias | $=-12 \mathrm{v}$. | 0.5 |  | Target Curren | nt 2 ma . |  |  | 6AB5/6N5 |
| 6AF6G | Electron-Ray Tube Twin Indicator Type | s. | 7AG | 6.3 | 0.15 |  |  | - | Indicator Tube | $\begin{aligned} & 135 \\ & 100 \end{aligned}$ |  | $\begin{aligned} & \text { Ray Co } \\ & \text { Ray Co } \end{aligned}$ | trol Voltag trol Volta | $\begin{aligned} & e=81 \mathrm{for} \\ & e=60 \mathrm{for} \end{aligned}$ | $\begin{aligned} & 0^{\circ} \text { Shadow } \\ & 0^{\circ} \text { Shadow } \end{aligned}$ | Angla. Targe Angle. Targe |  | $\begin{aligned} & \text { nt } 1.5 \mathrm{ma} . \\ & \mathrm{n} \mid 0.9 \mathrm{ma} . \end{aligned}$ |  | 6AF6G |
| 685 | Direct-Coupled Power Amplifier | M. | 6AS | 6.3 | 0.8 | - |  |  | Class-A Amp. ${ }^{9}$ Push-Pull Amp. | $\begin{aligned} & 300 \\ & 400 \end{aligned}$ | $\begin{array}{\|c} 0 \\ -13.0 \end{array}$ | 二 | $\begin{aligned} & 61 \\ & 4.51 \end{aligned}$ | $\begin{aligned} & 45 \\ & 40 \end{aligned}$ | 241000 | $\underline{2400}$ | ${ }^{58}$ | $\begin{gathered} 7000 \\ 10000 \\ \hline 11 \end{gathered}$ | $\begin{aligned} & 4.0 \\ & 20 \end{aligned}$ | 683 |

TABLE IV-6.3-VOLT GLASS RECEIVING TUBES-Continued


TABLE V-2.5-VOLT RECEIVING TUBES

| Typo | Name | Base | Socket Connections | Fil. or Heater |  | Copacitance $\mu, \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Volts } \end{aligned}$ | Screen Current Ma. | Plate Current Ma. | $\|$Plate <br> Resistance <br> Ohms | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c\|} \hline \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Power Outpul Walts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| $25 / 45$ | Duodiode | M. | 50 | 2.5 | 1.35 |  |  | - | Detector | Al 50 d.c. Volts per plate, cathode ma. $=80$ |  |  |  |  |  |  |  |  |  | 25/45 |
| $2 A^{2}$ | Triode Power Amplifier | M. | 4D | 2.5 | 2.5 | 7.5 | 5.5 | 16.5 | Class-A Amp. | Characteristics same as Type 6A3, Table IV |  |  |  |  |  |  |  |  |  | 243 |
| $2 A 5$ | Pentode Power Amplifier | M. | 68 | 2.5 | 1.75 |  |  |  | Class-A Amp. | Characteristics same as Type 42, Table IV |  |  |  |  |  |  |  |  |  | 2A5 |
| 246 | Duplex-Diode Triode | 5. | 6 G | 2.5 | 0.8 | 1.7 | 3.8 | 1.7 | Class-A Amp. | Characteristics same as Type 75, Table IV |  |  |  |  |  |  |  |  |  | 2A6 |
| 247 | Pentagrid Converter | 5. | 7 C | 2.5 | 0.8 |  |  | - | Converter | Characteristics same as Type 6A7, Table IV |  |  |  |  |  |  |  |  |  | 2 A 7 |
| 286 | Direct-Coupled Amplifier | M. | 7 J | 2.5 | 2.25 |  |  |  | Amplifier | 250 | -24.0 | - |  | 40.0 | 5150 | 3500 | 18.0 | 5000 | 4.0 | 2B6 |
| 287 | Duplex-Diode Pentode | S. | 70 | 2.5 | 0.8 | 3.5 | 9.5 | . 007 . | Penlode Amp. | Characteristics same as rype 687-rable IV |  |  |  |  |  |  |  |  |  | $2 \mathrm{B7}$ |
| $2 \mathrm{E5}$ | Electron-Ray Tube | 5. | 6R | 2.5 | 0.8 |  |  | - | Indicator Tube | Characteristics same as Type 6E5-Table IV |  |  |  |  |  |  |  |  |  | 2 E 5 |
| $2 \mathrm{G5}$ | Electron-Ray Tube | 5. | 6R | 2.5 | 0.8 |  |  |  | Indicator Tube | Characteristics same as 6U5/6G5-Table IV |  |  |  |  |  |  |  |  |  | 2G5 |
| 24-A | Tetrode R.F. Amplifior | M. | 5 E | 2.5 | 1.75 | 5.3 | 10.5 | . 007 | Screen-Grid R.F. Amplifier | 250 | - 3.0 | 90 | 1.7 | 4.0 | 600000 | 1050 | 630 |  | - | 24-A |
|  |  |  |  |  |  |  |  |  | Bias Detector | 250 | - 5.0 | 20/45 | Plate current adjusted to 0.1 ma . with no signal |  |  |  |  |  |  |  |
| 27 | Triode Detector-Amplifier | M. | 5A | 2.5 | 1.75 | 3.1 | 2.3 | 3.3 | Class-A Amp. | 250 | -21.0 |  | - | 5.2 | 9250 | 975 | 9.0 | - | L | 27 |
| 27 | Triode Delector.Amplinar | M. |  |  |  |  |  |  | Bias Detector | 250 | -30.0 | $\underline{\square}$ | Plate current adjusted 100.2 ma . with no signal |  |  |  |  |  |  |  |
| 35/51 | Remote Cut-off Pentode | M. | 5E | 2.5 | 1.75 | 5.3 | 10.5 | $.007$ | Screen-Grid R.F. Amplifier | 250 | - 3.0 | 90 | 2.5 | 6.5 | 400000 | 1050 | 420 | - | - | 35/51 |
| 45 | Triode Power Amplifier | M. | 4D | 2.5 | 1.5 | 4 | 3 | 7 | Class-A Amo. | 275 | -56.0 |  |  | 36.0 | 1700 | 2050 | 3.5 | 4600 | 2.00 | 45 |
| 46 | Dual-Grid Power Amp. | M. | 5 C | 2.5 | 1.75 | - | - |  | Class-A Amp.' | 250 | -33.0 | - |  | 22.0 | 2380 | 2350 | 5.6 | 6400 | 1.25 | 46 |
| 46 | Dual-Grid Power Amp. |  |  |  |  |  |  |  | Class-B Amp. ${ }^{3}$ | 430 | 0 |  |  | 12 | Power output for 2 tubes |  |  | 5800 | 20.0 |  |
| 47 | Pentode Power Amplifier | M. | 5 B | 2.5 | 1.75 | 8.6 | 13 | 1.2 | Class-A Amp. | 250 | -16.5 | 250 | 6.0 |  | 60300 | 2500 | 150 | 7000 | 2.7 | 47 |
| 53 | Twin Triode Amplifier | M. | 7 B | 2.5 | 2.0 |  |  |  | Class-B Amp. | Characteristics same as Type 6A6, Table IV |  |  |  |  |  |  |  |  |  | 53 |
| 55 | Duplex-Diode Triode | 5. | 6G | 2.5 | 1.0 | 1.5 | 4.3 | 1.5 | Class-A Amp. | Characteristics same as Type 85, Table IV |  |  |  |  |  |  |  |  |  | 55 |
| 56 | Triode Amplifier, Detector | S. | 5A | 2.5 | 1.0 | 3.2 | 2.4 | 3.2 | Class-A Amp. | Characteristics same as Type 76, Table IV |  |  |  |  |  |  |  |  |  | 56 |
| 57 | Sharp Cut-off Pentode | 5. | 6 F | 2.5 | 1.0 |  |  |  | R.F. Amplifier | 250 | - 3.0 | 100 | $\begin{aligned} & 0.5 \\ & \hline 2.0 \end{aligned}$ | 2.0 | 1500000 | 1225 | 1500 | - | - | 57 |
| 58 | Remote Cut-off Pentode | s. | $6 F$ | 2.5 | 1.0 | 4.7 | 6.3 | . 007 | Screen-Grid R.F. Amplifier | 250 | - 3.0 | 100 |  | 8.2 | 800000 | 1600 | 1280 | - | - | 58 |
| 59 | Pentode Power Amplifier | M. | 74 | 2.5 | 2.0 |  |  |  | Class-A Triode ${ }^{\text {4 }}$ | 250 | -28.0 | $\overline{250}$ | $\underline{-1}$ | 26.0 | 2300 | 2600 | 6.0 | 5000 | 1.25 | 59 |
| 59 | Pentode Power Amplifier | M. | 74 |  |  |  |  |  | Class-A Pentode ${ }^{\text {a }}$ | 250 | -18.0 | 250 | 9.0 | 35.0 | 40000 | 2500 | 100 | 6000 | 3.0 |  |
| RK15 | Triode Power Amplifier | M. | $4{ }^{\text {d }}$ | 2.5 | 1.75 |  |  |  |  | Characteristics same as Type 46 with Class-B connections |  |  |  |  |  |  |  |  |  | RK15 |
| RK16 | Triode Power Amplifier | M. | 5A | 2.5 | 2.0 | - |  | - |  | Characteristics same as Type 59 with Class-A triode connections |  |  |  |  |  |  |  |  |  | RK16 |
| RK17 | Pentode Power Amplifier | M. | 57 | 2.5 | 2.0 |  |  |  |  | Characteristics same as Type 2A5 |  |  |  |  |  |  |  |  |  | RK17 |

${ }^{1}$ Grid connection to cap; no connection to No. 3 pin. ${ }^{2}$ Grid No. 2 tied to plate. ${ }^{3}$ Grids Nos. 1 and 2 tied together. $\quad$ Grids Nos. 2 and 3 connected to plate. ${ }^{5}$ Grid No. $\mathbf{2}$, screen; grid No. $\mathbf{3}$, suppressor.

TABLE VI-2.0-VOLT BATTERY RECEIVING TUBES

| Type | Name | Base | Socket Connec fions | Filament |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volis | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Volts } \end{gathered}$ | Screen Curren Ma. | Plate Current Ma. | $\left\lvert\, \begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}\right.$ | Transconductance Micromhos | $\left\lvert\, \begin{gathered} \text { Amp. } \\ \text { Factor } \end{gathered}\right.$ | $\begin{array}{\|c\|} \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | PowerOutputWatts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | $\begin{aligned} & \text { Plate- } \\ & \text { Grid } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| 1A4P | Voriable- $\mu$ Pontode | S. | 4M | 2.0 | 0.06 | 5 | 11 | . 007 | R.F. Amplifier | 180 | $-3.0$ | 67.5 | 0.8 | 2.3 | 1000000 | 750 | 750 | - | - | 1A4P |
| 1A4T | Voriable- $\mu$ Tetrode | 5. | 4K | 2.0 | 0.06 | 5 | 11 | . 007 | R.F. Amplifiar | 180 | $-3.0$ | 67.5 | 0.7 | 2.3 | 980000 | 750 | 720 | - | - | IA4T |
| 1 146 | Pentagrid Converter | S. | 6 L | 2.0 | 0.06 |  |  |  | Converter | 180 | $-3.0$ | 67.5 | 2.4 | 1.3 | 500000 | Anode grid | d (No. 2 | 2) 180 max. | volis | IA6 |
| 184P/951 | Pentode R.F. Amplifier | s. | 4M | 2.0 | 0.06 | 5 | 11 | . 007 | R.F. Amplifier | $\begin{array}{r} 180 \\ 90 \end{array}$ | $\begin{array}{r} -3.0 \\ -3.0 \end{array}$ | $\begin{aligned} & 67.5 \\ & 67.5 \end{aligned}$ | $\begin{aligned} & 0.6 \\ & 0.7 \end{aligned}$ | $\begin{aligned} & 1.7 \\ & 1.6 \end{aligned}$ | $\begin{aligned} & 1500000 \\ & 1000000 \end{aligned}$ | $\begin{aligned} & 650 \\ & 600 \end{aligned}$ | $\begin{array}{r} 1000 \\ 550 \end{array}$ | - | - | 1B4P/951 |
| 185/25S | Duplex-Dioda Triode | s. | 6M | 2.0 | 0.06 | 1.6 | 1.9 | 3.6 | Triode Class-A | 135 | $-3.0$ | - |  | 0.8 | 35000 | 575 | 20 | - |  | 185/25S |

table vi-2.0-volt battery receiving tubes-Continued

| Typo | Namo | Daso | Socket Connections | Filament |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plale Supply Volts | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Yolts } \end{gathered}$ | Screen Curren Ma. | PlateCurrent Ma. | $\left.\begin{array}{\|c\|} \hline \text { Plate } \\ \text { Ressistance } \\ \text { Ohms } \end{array} \right\rvert\,$ | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c} \text { Load } \\ \text { Resisfance } \\ \text { Ohms } \end{array}$ | $\left\|\begin{array}{l\|} \text { Power } \\ \text { Outpu1 } \\ \text { Watts } \end{array}\right\|$ | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 166 | Pentagrid Convorter | 5. | 66 | 2.0 | 0.12 | 10 | 10 |  | Converter | 180 | - 3.0 | 67.5 | 2.0 | 1.5 | 750000 | Anota grid (No. 2) 135 max. volts |  |  |  | 1 Cb |
| $1 F 4$ | Pentode Power Amplifer | M. | 5K | 2.0 | 0.12 |  |  |  | Class-A Amp. | 135 | -4.5 | 135 | 2.6 | 8.0 | 200000 | 1700 | 340 | 16000 | 0.34 | 1154 |
|  |  |  |  |  |  |  |  |  | R.F. Amplifer | 180 | - 1.5 | 67.5 | 0.6 | 2.0 | 1000000 | 650 | 650 |  |  | IF6 |
| 1F6 | Duplex-Diode Penlode | s. | 6W | 2.0 | 0.06 | 4 | 9 | . 007 | A.F. Amplifier | 135 | -1.0 | 135 | Plate, 0.25 megohm; screen, 1.0 megohm |  |  |  |  | Amp. $=48$ |  | 176 |
| 15: | Sharp Cut-off Pentode | 5. | 5 F | 2.0 | 0.22 | 2.3 | 7.8 | 0.01 | R.F. Amplifer | 135 | -1.5 | 67.5 | 0.3 | 1.85 | 800000 | 750 | 600 |  |  | 15 |
| 19 | Twin-Triode Amplifier | 5. | ${ }^{6} \mathrm{C}$ | 2.0 | 0.26 |  |  |  | Class-B Amp. | 135 | 0 |  | - | $\underline{\square}$ | Load olate-to-plata |  |  | 10000 | 2.1 | 19 |
| 30 | Triode Detector Amplifier | S. | 4D | 2.0 | 0.06 |  |  |  | Class-A Amp. | 180 | -13.5 | $\cdots$ |  | 3.1 | 10300 | 930 | 9.3 |  |  | 30 |
| 31 | Triode Power Amplifier | 5. | 40 | 2.0 | 0.13 | 3.5 | 2.7 | 5.7 | Class-A Amp. | 180 | -30.0 |  |  | 12.3 | 3600 | 1050 | 3.8 | 5700 | 0.375 | 31 |
| 32 | Sharp Cut-off Pentode | M. | 4K | 2.0 | 0.06 | 5.3 | 10.5 | . 015 | R.F. Amplifor | 180 | $-3.0$ | 67.5 | 0.4 | 1.7 | 1200000 | 650 | 780 | $\underline{-}$ |  | 32 |
| 33 | Pentode Power Amplifier | M | 5K | 2.0 | 0.26 | 8 | 12 | 1 | Class-A Amp. | 180 | -18.0 | 180 | 5.0 | 22.0 | 55000 | 1700 | 90 | 6000 | 1.4 | 33 |
| 34 | Variable- $\mu$ Pentode | M. | 4M | 2.0 | 0.06 | 6 | 11 | . 015 | R.F. Amplifior | 180 | - 3.0 | 67.5 | 1.0 | 2.8 | 1000000 | 620 | 620 |  |  | 34 |
|  |  |  |  |  |  |  |  |  | Class-A Amp. ${ }^{1}$ | 135 | -20.0 |  | - | 6.0 | 4175 | 1125 | 4.7 | 11000 | 0.17 |  |
| 49 | Dual-Grid Power Amp. | M. | sc | 2.0 | 0.12 |  |  |  | Class-B Amp. ${ }^{2}$ | 180 | 0 |  |  | Power output for 2 fubes |  |  |  | 12000 | 3.5 | 49 |
| 840 | Pentode | S. | 51 | 2.0 | 0.13 |  |  |  | Class-A Amp. | 180 | - 3.0 | 67.5 | 0.7 | 1.0 | 1000000 | 400 | 400 | - |  | 840 |
| 950 | Pentode Power Amplifier | M. | 5K | 2.0 | 0.12 |  |  | $\square$ | Closs-A Amp. | 135 | -16.5 | 135 | 2.0 | 7.0 | 100000 | 1000 | 125 | 13500 | 0.575 | 950 |
| RK24 | Triode | M. | 4 D | 2.0 | 0.12 |  |  |  | Class-A Amp. | 180 | -13.5 |  |  | 8.0 | 5000 | 1600 | 8.0 | 12000 | 0.25 | RK24 |
| 1229 | Tetrode | M. | 4K | 2.0 | 0.06 |  |  |  |  | Special Type 32 for low grid-current applications |  |  |  |  |  |  |  |  |  | 1229 |
| 1230 | Triode | M. | 40 | 2.0 | 0.06 | 3.0 | 2.1 | 6.0 |  | Special Type 30 for low grid-current applications |  |  |  |  |  |  |  |  |  | 1230 |

Discontinued.
${ }^{1}$ Grid No. 2 tied to plate.
${ }^{2}$ Grids Nos. 1 and 2 fied togethor.
TABLE VII-2.0-VOLT BATTERY TUBES WITH OCTAL BASES

| Typo | Nama | Socket Connections | Filament |  | Copacilance $\mu \mu \mathrm{fd}$. |  |  | Uso | Plate Supply Volts | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Volts } \end{gathered}$ | Screen Current Ma. | Plate Current Mo. | $\begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}$ | Transconductance Micromhos | Amp. Factor | $\begin{array}{\|c\|} \text { Load } \\ \text { Resisfance } \\ \text { Ohms } \end{array}$ | Powor Oufput Watts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 1C7G | Heptode | 72 | 2.0 | 0.06 | 10 | 14 | 0.26 | Converter | Characteristics same as Type IC6-Table VI |  |  |  |  |  |  |  |  |  | IC7G |
| 105GP | Variable- $\mu$ Pentodo | 5 Y | 2.0 | 0.06 | 5 | 11 | . 037 | R.F. Ampliffar | Characteristics same as Type 1A4P-Table VI |  |  |  |  |  |  |  |  |  | IDSGP |
| 1DSGT. | Variable- $\mu$ Tetrode | 5R | 2.0 | 0.06 |  |  |  | R.F. Amplifier | 180 | -3.0 | 67.5 | 0.7 | 2.2 | 600000 | 650 |  |  |  | 1DSGT |
| ID7G | Pentagrid Converter | 72 | 2.0 | 0.06 | 10.5 | 9.0 | 0.25 | Convertar | Characteristics same as Type 1A6-Table VI |  |  |  |  |  |  |  |  |  | 1D7G |
| IESGP | Pentode Amplifier | 5 r | 2.0 | 0.06 | 5 | 11 | . 007 | R.F. Amplifier | Characteristics same as Type 184-Table VI |  |  |  |  |  |  |  |  |  | 1ESGP |
| $1 E 7 G$ | Double Pentode Power Amp. | 8 C | 2.0 | 0.24 |  |  |  | Class-A Amplifor | 135 | -7.5 | 135 | $2.0{ }^{1}$ | 6.51 | 220000 | 1600 | 350 | 24000 | 0.65 | 1E7G |
| IFSG | Pentode Power Amplifier | $6 \times$ | 2.0 | 0.12 |  |  |  | Class-A Amplifier | Characteristics same as Type 1F4-Table VI |  |  |  |  |  |  |  |  |  | IFSG |
| $1 F 7 G^{2}$ | Duplex-Piode Pentode | 7 AD | 2.0 | 0.06 | 3.8 | 9.5 | 0.01 | Detestor-Amplifier | Charactaristics same as Type 1F6-Table VI |  |  |  |  |  |  |  |  |  | IF7G |
| 1G5G | Pentode Power Amplifier | $6 \times$ | 2.0 | 0.12 |  |  | - | Class-A Amplifier | 135 | -13.5 | 135 | 2.5 | 8.7 | 163000 | 1550 | 250 | 9000 | 0.55 | 1656 |
| 1H4G | Triode Amplifier | 55 | 2.0 | 0.06 |  |  |  | Detector-Ampliñer | Characteristics same as Type 30-Table VI |  |  |  |  |  |  |  |  |  | 1H4G |
| 1H6G | Duplex-Diode Triode | 7AA | 2.0 | 0.06 | 1.6 | 1.9 | 3.6 | Detector-Amplifier | Characteristics same as TYpe 185-Tade VI |  |  |  |  |  |  |  |  |  | 1H6G |
| 1156 * | Pentode Power Amplifior | $6 \times$ | 2.0 | 0.12 |  |  | - | Class-A Amplifier | 135 | -16.5 | 135 | 2.0 | 7.0 | - | 950 | 100 | 13500 | 0.45 | 1J5G |
| 116 G | I win Triode | 7 AB | 2.0 | 0.24 |  |  |  | Class-8 Amplifier | Characteristics sama as Type 19-Table VI |  |  |  |  |  |  |  |  |  | 1J6G |
| 4A6G | Twin Triode | 81 | 2.0 | 0.12 |  |  |  | Class-A, I sectior | 90 | $-1.5$ | - | - | 1.1 | 26600 | 750 | 20 |  |  |  |
| 4A6G |  | 82 | 4.0 | 0.06 |  |  |  | Class-B, 2 sections | 90 | -1.5 |  | - | $10.8{ }^{3}$ |  |  |  | 8000 | 1.0 | 4A6G |

* Discontinued.

${ }^{1}$ Total current for both sections; no signal.

[^2]Max. signal.
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TABLE VIII-1.5-VOLT FILAMENT BATTERY TUBES
See also Table $X$ for Special 1.4 -volf Tubes

| Type | Name | Base | Socket Connections | Filament |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plale Supply Volts | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Volts } \end{aligned}$ | Screen Current Ma. | Plate Current Ma. | $\begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}$ | Transconductance Micromhos | Amp. Facto | $\begin{array}{\|c} \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | $\left\|\begin{array}{c} \text { Power } \\ \text { Output } \\ \text { M-wotis } \end{array}\right\|$ | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 1A5GT | Pentode Power Amplifer | 0. | $6 \times$ | 1.4 | 0.05 |  |  |  | Class-A1 Amp. | 90 | -4.5 | 90 | 0.8 | 4.0 | 300000 | 850 | 240 | 25000 | 115 | IA5GT |
| IA7GT | Penlagrid Converter | 0. | 72 | 1.4 | 0.05 |  |  | - | Convertar | 90 | 0 | 45 | 0.6 | 0.55 | 600000 | Anode-grid volts 90 |  |  |  | IATGT |
| 1485 | Pentode R.F. Amplifier | t. | 5BF | 1.2 | 0.05 | 2.8 | 4.2 | 0.25 | R.F. Amplifier | $\begin{array}{r} 90 \\ 150 \end{array}$ | $\begin{gathered} 0 \\ -1.5 \end{gathered}$ | $\begin{array}{r} 90 \\ 150 \end{array}$ | $\begin{aligned} & 0.8 \\ & 2.0 \end{aligned}$ | $\begin{aligned} & 3.5 \\ & 6.8 \end{aligned}$ | $\begin{array}{r} 275000 \\ 125000 \\ \hline \end{array}$ | $\begin{aligned} & 1100 \\ & 1350 \end{aligned}$ | - | - | - 1 | $1 \mathrm{AB5}$ |
| 187GT + | Heptode | 0. | 72 | 1.4 | 0.1 | - | - |  | Converter | 90 | 0 | 45 | 1.3 | 1.5 | 350000 | Grid No. 1 resistor 200,000 ohms |  |  |  | 187GT |
| 1B8GT | Diode Triode Pentode | 0. | 8AW | 1.4 | 0.1 | - | - |  | Triode Amplifier Pentode Amp. | $\begin{aligned} & 90 \\ & 90 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0 \\ -6.0 \\ \hline \end{array}$ | 90 | 1.4 | $\begin{aligned} & 0.15 \\ & 6.3 \end{aligned}$ | $\underline{24000}$ | $\begin{array}{r} 275 \\ 1150 \\ \hline \end{array}$ | - | $\overline{14000}$ | 210 | 188GT |
| 1C5GT | Pentode Power Amplifier | 0. | 6X | 1.4 | 0.1 | - | - | - | Class-A Amp. | 90 | -7.5 | 90 | 1.6 | 7.5 | 115000 | 1550 | 165 | 8000 | 240 | ICSGT |
| 108GT | Diode Triode Pentode | 0. | 3AJ | 1.4 | 0.1 | - | - | - | Triode Amp. Pentode Amp. | $\begin{aligned} & 90 \\ & 90 \\ & \hline \end{aligned}$ | $\begin{array}{r} 0 \\ -9.0 \end{array}$ | 90 | 1.0 | $\begin{array}{r} 1.1 \\ 5.0 \end{array}$ | $\begin{array}{r} 43500 \\ 200000 \end{array}$ | $\begin{aligned} & 575 \\ & 925 \\ & \hline \end{aligned}$ | 25 | - |  | ID8GT |
| 1E4G | Triode Ampliflor | 0. | 55 | 1.4 | 0.05 | 2.4 | 6 | 2.40 | Class-A Amp. | $\begin{aligned} & 90 \\ & 90 \end{aligned}$ | $\begin{gathered} 0 \\ -3.0 \end{gathered}$ | - | - | $\begin{aligned} & 4.5 \\ & 1.5 \end{aligned}$ | $\begin{aligned} & 11000 \\ & 17000 \end{aligned}$ | $\begin{array}{r} 1325 \\ 825 \\ \hline \end{array}$ | $\begin{aligned} & 14.5 \\ & 14 \end{aligned}$ | - | - 1 | 1E4G |
| 1G4GT | Triode Amplifier | 0. | 55 | 1.4 | 0.05 | 2.2 | 3.4 | 2.80 | Class-A Amp. | 90 | -6.0 | - |  | 2.3 | 10700 | 825 | 8.8 | - |  | 1G4GT |
| IG6GT | Twin Triode | 0. | 7 AB | 1.4 | 0.1 |  | - | $\square$ | Class-A Amp. | 90 | 0 |  |  | 1.0 | 45000 | \| 675 | 30 |  |  | 1G6GT |
| 1H5GI | Diode High- Triode | 0. | 5 L | 1.4 | 0.1 | 1.1 | 6 | 1.00 | Class-B Amp. | 90 | 0 |  |  | 1/7 | 34 volts input per grid |  |  | 12000 | 675 | 1G6G |
| ILA4 | Pentode Power Amplifler | 1. | 5AD | 1.4 | 0.05 |  | - |  | Class-A Amp. | 90 | Characteristics same as 1A5GT |  |  |  |  |  |  |  |  | ILA4 |
| ILA6 | Pentagrid Converter | 1. | 7AK | 1.4 | 0.05 |  |  |  | Convertar | 90 | 0 | 45 | 0.6 | 0.55 | Anode Grid Volts 90 |  |  |  |  | ILA6 |
| 1184 | Pentode Power Amplifier | $\underline{L}$ | 5 SAD | 1.4 | 0.05 |  |  |  | Class-A Amp. | 90 | -9 | 90 | 1.0 | 5.0 | 200000 | 925 | - | 12030 | 200 | 1184 |
| 1L86 | Heptode Converter | 1. | ${ }^{\text {B }}$ AX | 1.4 | 0.05 |  |  |  | Converter | 90 | 0 | 67.5 | 2.2 | 0.4 | Grid No. 4-67.5 v., No. 5-0 v. |  |  |  |  | 1186 |
| ILC5 | Remote Cut-off Pentode | 1. | 7AO | 1.4 | 0.05 | 3.2 | 7 | . 007 | R.F. Amplifier | 90 | 0 | 45 | 0.2 | 1.15 | 1500000 | 775 | - |  | $=1$ | ILC5 |
| $12 \mathrm{C6}$ | Pentagrid Convertor | $t$. | 7AK | 1.4 | 0.05 | - |  |  | Converter | 90 | 0 | 35. | 0.7 | 0.75 |  | Anode Grid Volts 45 |  |  |  | 1166 |
| ILD5 | Diode Panlode | 1. | 6AX | 1.4 | 0.05 | 3.2 | 6 | 0.18 | Class-A Amp. | 90 | 0 | 45 | 0.1 | 0.6 | 950000 | 600 | - | $\cdots$ | - | ILDS |
| 12 E 3 | Triode Ar.rplifier | L. | 4AA | 1.4 | 0.05 | 1.7 | 3 | 1.70 | Closs-A Amp. | $\begin{aligned} & 90 \\ & 90 \end{aligned}$ | $\begin{array}{r} 0 \\ -3 \end{array}$ | - | - | $\begin{array}{r} 4.5 \\ 1.3 \\ \hline \end{array}$ | $\begin{aligned} & 11200 \\ & 19000 \end{aligned}$ | $\begin{array}{r} 1300 \\ 760 \\ \hline \end{array}$ | 14.5 | - | - | 1153 |
| 1LG5 | Pentode R.f. Amp. | L. | 7AO | 1.4 | 0.05 |  |  |  | Class-A Amo. | 90 | 0 | 45 | 0.4 | 1.7 | 1020000 | 800 |  |  |  | 11G5 |
| 11H4 | Diode High $\mu$ Triode | L. | SAG | 1.4 | 0.05 | 1.1 | 6 | 1.00 | Class-A Amp. | 90 | 0 |  |  | 0.15 | 240000 | 275 | 65 |  |  | 11 H 4 |
| ILNS | Remote Cut-off Pentode | L. | 7AO | 1.4 | 0.05 | 3.4 | 8 | . 007 | Class-A Amp. | 90 | 0 | 90 | 0.3 | 1.2 | 1500000 | 750 |  | - | $-1$ | ILN5 |
| INSGT | Remota Cut-off Pentode | 0. | 5 Y | 1.4 | 0.05 | 3 | 10 | . 007 | Class-A Amo. | 90 | 0 | 90 | 0.3 | 1.2 | 1500000 | 750 | 1160 |  | $\underline{-1}$ | INSGT |
| INGG ${ }^{\text {a }}$ | Diode-Power-Pentode | 0. | TAM | 1.4 | 0.05 |  |  |  | Class-A Amp. | 90 | -4.5 | 90 | 0.6 | 3.1 | 300000 | 800 |  | 25000 | 100 | INGG |
| IPSGT | Pentode | O. | 5 Y | 1.4 | 0.05 | 3 | 10 | . 007 | R.F. Amplifer | 90 | 0 | 90 | 0.7 | 2.3 | 800000 | 800 | 640 |  |  | IPSGI |
| 105GT | Tetrode Power Amplifier | 0. | 6AF | 1.4 | 0.1 | - | - | - | Class-A Amp. | $\begin{aligned} & 85 \\ & 90 \end{aligned}$ | $\begin{array}{\|l\|} \hline-5.0 \\ -4.5 \end{array}$ | $\begin{aligned} & 85 \\ & 90 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.2 \\ & 1.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.2 \\ & 9.5 \end{aligned}$ | $\begin{array}{r} 70000 \\ 75000 \\ \hline \end{array}$ | $\begin{aligned} & 1950 \\ & 2100 \\ & \hline \end{aligned}$ | - | $\begin{aligned} & 9000 \\ & 8000 \end{aligned}$ | $\begin{array}{r} 250 \\ 270 \\ \hline \end{array}$ | 1QSGT |
| IR4/1294 | U.h.I. Diode | 1. | 4A.H | 1.4 | 0.15 | -- |  | - | Rectifiter | Max. r.m.s. voltage per plate -30 |  |  |  |  | Max. d.c. oulout current $-340 \mu \mathrm{a}$. |  |  |  |  | 1R4/1294 |
| ISA6GT | Medium Cut-off Pentode | 0. | 6CA | 1.4 | 0.05 | 5.2 | 8.6 | 0.01 | R.F. Amplifiar | 90 | 0 | 67.5 | 0.68 | 2.45 | 820020 | 970 |  | , |  | ISA6GT |
| 1586GT | Diode Penlode | 0. | 6 CB | 1.4 | 0.05 | 3.2 | 3 | 0.25 | Class-A Amp. | 90 | 0 | 67.5 | 0.38 | 1.45 | 700000 | 665 |  |  |  | 15B6GT |
| ISEGT | Diode Peniode | 0. | 6 Ca | 1.4 | 0.05 |  | 3 |  | R.C. Amplifer | 90 | 0 | 90 | Screan resistor $5 \mathrm{meq} .$, qrid 10 meq. |  |  |  |  | 1 meg. | $110^{2}$ | ISB6GY |
| ITSGT | Beam Power Amplifiar | 0. | 6AF | 1.4 | 0.05 | 4.8 | 8 | 0.50 | Class-A Amp. | 90 | -6.0 | 90 | 1.4 | 6.5 | -- | 1150 | -- | 14000 | 170 | 1T5GT |
| 387/1291 | U.h.f. Twin Triode | 1. | 7BE | $2.8{ }^{\circ}$ | 0.11 | 1.4 | 2.6 | 2.6 | Class-A Amp. | 90 | 0 | - | - | 5.2 | 11350 | 1850 | 21 |  | - 3 | 387/1291 |
| 1293 | U.h.f. Triode | $t$. | 4AA | 1.4 | 0.11 | 1.7 | 3.0 | 1.7 | Class-A Amp. | 90 | 0 |  |  | 4.7 | 10750 | 1300 | 14 | - | - 1 | 1293 |
| 3D6/1299 | U.h.f. Tetrode | L. | 68B | $2.8{ }^{3}$ | 0.11 | 7.5 | 6.5 | 0.30 | Class-A Amn. | 135 | -6 | 90 | 0.7 | 5.7 | - | 2200 |  | 13000 | 500 | 306/1299 |
| 3E6 | R.F. Pentode | t. | 7 CJ | $\begin{array}{\|l\|} \hline 1.4 \\ 2.8 \end{array}$ | $\begin{aligned} & 0.10 \\ & 0.05 \end{aligned}$ | 5.5 | 7.5 | 0.007 | Class-A Amp. | 90 | 0 | 90 | 1.3 | 3.8 | 300000 | 2100 | - | - | - 3 | 3E6 |
| RK42 | Triode Amplifer | 5. | 40 | 1.5 | 0.6 |  | - |  | Class-A Amp. |  | Characteristics same as Type 30-Table VI |  |  |  |  |  |  |  |  | RK42 |
| RK43 | Twin Triode Amplifler | 5. | 6 C | 1.5 | 0.12 |  |  |  | Class-A Amp. | 135 | -3 | - | - | 4.5 | 14500 | 900 | 13 | - | - R | RK43 |

table ix－high－voltage heater tubes

| Type | Name | Base | Socket Connec－ tions | Heater |  | Capacitance $\mu \mu \mathrm{fd}$ ． |  |  | Use | $\left\|\begin{array}{c} \text { Plafe } \\ \text { Supply } \\ \text { Volts } \end{array}\right\|$ | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Yolts } \end{aligned}$ | Screen Current Ma． | PlateCurrent Ma． | $\begin{array}{\|c\|} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Transcon－ ductance Micromhos | $\begin{aligned} & \text { Amp. } \\ & \text { Factor } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Load } \\ \text { Resisfance } \\ \text { Ohms } \end{array}$ | Power Outpu Watts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp． | In | Out | Plate－ Grid |  |  |  |  |  |  |  |  |  |  |  |  |
| 12A5 ${ }^{\text {8 }}$ | Pentode Power Amplifier | M． | 7F | $\begin{array}{r} 12.6 \\ 6.3 \end{array}$ | $\begin{aligned} & 0.3 \\ & 0.6 \end{aligned}$ | 9.0 | 9.0 | 0.3 | Class－A Amp．${ }^{6}$ | $\begin{aligned} & 100 \\ & 180 \end{aligned}$ | $\begin{array}{\|l\|l\|} \hline-15 \\ -25 \end{array}$ | $\begin{aligned} & 100 \\ & 180 \end{aligned}$ | $\begin{aligned} & 3 / 6.5 \\ & 8 / 14 \\ & \hline \end{aligned}$ | $\begin{aligned} & 17 / 19 \\ & 45 / 48 \\ & \hline \end{aligned}$ | $\begin{aligned} & 50000 \\ & 35000 \end{aligned}$ | $\begin{aligned} & 1700 \\ & 2400 \\ & \hline \end{aligned}$ | 二 | $\begin{aligned} & 4500 \\ & 3300 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.8 \\ & 3.4 \end{aligned}$ | 12A5 |
| 12A6 | Beam Power Amplifier | 0. | 7AC | 12.6 | 0.15 |  |  |  | Class－A Amp． | 250 | －12．5 | 250 | 3.5 | 30 | 70000 | 3000 |  | 7500 | 3.4 | 12 A 6 |
| 12A7 | Rectifier－Amplifier | M． | 7K | 12.6 | 0.3 |  |  |  | Class－A Amp． | 135 | －13．5 | 135 | 2.5 | 9.0 | 102000 | 975 | 100 | 13500 | 0.55 | 12 A 7 |
| 12A8GT | Heptode | 0. | 8A | 12.6 | 0.15 | 9.5 | 12 | 0.26 | Converter | Characteristics same as 648－Table I |  |  |  |  |  |  |  |  |  | 12A8GT |
| 12AH7GT | Twin Triode | 0. | 8 BE | 12.6 | 0.15 | Each Triode Sect． |  |  | Class－A Amp． | 180 | －6．5 |  |  | 7.6 | 8400 | 1900 | 16 |  |  | 12AH7GT |
| 12 B 6 M | Diode Triode | 0. | 6 Y | 12.6 | 0.15 |  | － |  | Class－A Amp． | 250 | － 2.0 |  |  | 0.9 | 91000 | 1100 | 100 |  |  | 1286M |
| 1287 ML | Pentode Amplifier | 0. | 8 V | 12.6 | 0.15 |  |  |  | Class－A Amp． | 250 | $-3.0$ | 100 | 2.6 | 9.2 | 800000 | 2000 |  | $\cdots$ |  | $12 \mathrm{B7ML}$ |
| 12B8GT ${ }^{8}$ | Triode－Pentode | 0. | 8 T | 12.6 | 0.3 | Triode Section Pentode Section |  |  | Class－A Amp． | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{array}{\|l\|} \hline-1 \\ \hline \end{array}$ | 100 | 2 | $\begin{aligned} & 0.6 \\ & 8 \end{aligned}$ | $\begin{array}{r} 73000 \\ 170000 \end{array}$ | $\begin{array}{r} 1500 \\ 2100 \\ \hline \end{array}$ | $\begin{aligned} & 110 \\ & 360 \end{aligned}$ | 二 |  | 12B8GT |
| 12 Cs | Duplex－Diode Pentode | 0. | 8 E | 12.6 | 0.15 | 6 | 9 | ． 005 | Class－A Amp． | Characteristics same as 688－Table I |  |  |  |  |  |  |  |  |  | $12 \mathrm{C8}$ |
| 12ESGT | Triode Amplifior | 0. | 69 | 12.6 | 0.15 | 3.4 | 5.5 | 2.60 | Class－A Amp． | 250 | －13．5 |  |  | 50 | － 1 | 1450 | 13.8 | － | $\cdots$ | 12E5GT |
| 12F5GT | Triode Amplifier | 0. | 5M | 12.6 | 0.15 | 1.9 | 3.4 | 2.40 | Class－A Amp． | Characteristics same as 6SF5－Table 1 |  |  |  |  |  |  |  |  |  | 12F5GT |
| $12 \mathrm{G7G}$ | Duplex－Diode Triode | 0. | 7 V | 12.6 | 0.15 |  |  |  | Class－A Amp． | 250 | － 3.0 |  |  | － | 58000 | 1200 | 70 |  |  | 12G7G |
| $12 \mathrm{H6}$ | Twin Diodo | 0. | 70 | 12.6 | 0.15 |  |  | － | Rectifor | Characteristics same as 6 6 Ho －Table 1 |  |  |  |  |  |  |  |  |  | 12H6 |
| 12J5GT | Triode Amplifler | 0. | 60 | 12.6 | 0.15 | 3.4 | 3.6 | 3.40 | Class－A Amp． | Characteristics same as 615 －Table 1 |  |  |  |  |  |  |  |  |  | 12 J 5 GT |
| $12 \mathrm{J7GT}$ | Shapp Cut－off Pentode | 0. | 7 R | 12.6 | 0.15 | 4.2 | 5.0 | 3.8 | Class－A Amp． | Characteristics same as 6 J7－Table I |  |  |  |  |  |  |  |  |  | 12 J 7 GT |
| 12K7GT | Remote Cut－off Pentode | 0. | 7R | 12.6 | 0.15 | 4.6 | 12 | ． 005 | R．F．Amplifier | Characteristics same as 6K7－rable 1 |  |  |  |  |  |  |  |  |  | $12 \mathrm{K7Gr}$ |
| $12 \mathrm{K8}$ | Triode Hexode Converier | 0. | 8 K | 12.6 | 0.15 |  |  | － | Converter | Characteristics same as 6 K8－Table 1 |  |  |  |  |  |  |  |  |  | 12K8 |
| 12L8GT | Twin Pentode | 0. | 8BU | 12.6 | 0.15 | 5 | 6 | 0.70 | Class－A ${ }_{1}$ Amp． | 180 | － 9.0 | 180 | 2.8 | 13.0 | 160000 | 2150 |  | 10000 | 1.0 | 12L8GT |
| 1207 GT | Duplex－Diode Triode | 0. | 7 V | 12.6 | 0.15 | 2.2 | 5 | 1.60 | Class－A Amp． | Characteristics same as 607－Table 1 |  |  |  |  |  |  |  |  |  | 1297GT |
| 1258 GT | Triple－Diode Triode | 0. | BCB | 12.6 | 0.15 | 2.0 | 3.8 | 1.2 | Class－A Amp． | 250 | － 2.0 | － |  | 0.9 | 91000 | 1100 | 100 |  | － | 1258GT |
| 12547 | Heptode | 0. | 8R | 12.6 | 0.15 | 9.5 | 12 | 0.13 | Converter | Characteristics same as 65A7－Table I |  |  |  |  |  |  |  |  |  | 12SA7 |
| 125 C 7 | Twin Triode | 0. | 8 S | 12.6 | 0.15 | 2.2 | 3.0 | 2.0 | Class－A Amp． | Characteristics same as 6SC7－Table 1 |  |  |  |  |  |  |  |  |  | 125 C 7 |
| 12555 | High－$\mu$ Triode | 0. | 6AB | 12.6 | 0.15 | 4 | 3.6 | 2.40 | Class－A Amp． | Characteristics same as 6SF5－Table 1 |  |  |  |  |  |  |  |  |  | 125 F 5 |
| 12557 | Diode Variable－$\mu$ Pentode | 0. | 7AZ | 12.6 | 0.15 | 5.5 | 6.0 | ． 004 | Class－A Amp． | Characteristics same as 6SF7－Table 1 |  |  |  |  |  |  |  |  |  | 12557 |
| $125 \mathrm{G7}$ | Medium Cut－off Pentode | 0. | 8BK | 12.6 | 0.15 | 8.5 | 7.0 | ． 003 | Class－A Amp． | Characteristies same as 6SG7－Tabla ！ |  |  |  |  |  |  |  |  |  | 125G7 |
| 125 H 7 | Sharp Cut－off Pentode | 0. | 8BK | 12.6 | 0.15 | 8.5 | 7.0 | ． 003 | H－F Amplifier | Characteristics same as 65H7－Table 1 |  |  |  |  |  |  |  |  |  | 125H7 |
| 12517 | Sharp Cut－off Pentade | 0. | 8 N | 12.6 | 0.15 |  |  |  | Class－A Amp． | Charactaristics same as 65J7－Table 1 |  |  |  |  |  |  |  |  |  | 12517 |
| 12SK7 | Remote Cut－of Pentode | 0. | 8 N | 12.6 | 0.15 | 6.0 | 7.0 | ． 003 | R．F．Amplifer | Characteristics same as 6SK7－Table I |  |  |  |  |  |  |  |  |  | 125K7 |
| 12SL7GT | Twin Triode | 0. | 8BD | 12.6 | 0.15 |  | － |  | Class－A Amp． | Characteristics same as 65L7 GT－Table il |  |  |  |  |  |  |  |  |  | 125L7GT |
| 12SN7GT | Twin Triode | 0. | 8BD | 12.6 | 0.3 |  |  |  | Class－A Amp． | Characteristics same as 65N7GT－Table II |  |  |  |  |  |  |  |  |  | 12SN7GT |
| 12507 | Duplex－Diode Triode | 0. | 80 | 12.6 | 0.15 | 3.2 | 3.0 | 1.60 | Class－A Amp． | Characteristics same as 6507－Table 1 |  |  |  |  |  |  |  |  |  | 12507 |
| 12SR7 | Duplex－Diode Triode | 0. | 80 | 12.6 | 0.15 | 3.6 | 2.8 | 2.40 | Class－A Amp． | Characteristics same as 6R7－Table 1 |  |  |  |  |  |  |  |  |  | 12SR7 |
| 125 W 7 | Duplex－Diode Triode | 0. | 80 | 12.6 | 0.15 | 3.0 | 2.8 | 2.4 | Class－A Amp． | 250 | $-9$ |  | 三－ | 9.5 | 8500 | 1900 | 16 |  |  | 125 W 7 |
| $125 \times 7$ | Twin Triode | 0. | 8BD | 12.6 | 0.3 | 3.0 | 0.8 | 3.6 | Class－A Amp．${ }^{\text {i }}$ | 250 | －8 |  | － | 9 | 7700 | 2600 | 20 | － |  | 125x7 |
| $125 Y 7$ | Heptode Converter | 0. | 8R | 12.6 | 0.15 | Osc．－Grid leak 20000 ohms |  |  | Converter | 250 | － 2 | 100 | 8.5 | 3.5 | 1000000 | 450 |  | － |  | 125Y7 |
| 14A4 | Triode Amplifier | 1. | 5AC | 14 | 0.16 | 3.4 | 3.0 | 4.00 | Class－A Amp． | Characteristics same as 7A4－Table III |  |  |  |  |  |  |  |  |  | 14A4 |
| 14A5 | Beam Power Amplifior | 1. | 6AA | 14 | 0.16 |  |  |  | Class－A Amp． | 250 | －12．5 | 250 | 3．5／5．5 | 30／32 | 70000 | 3000 | － | 7500 | 2.8 | 14A5 |
| $\begin{aligned} & 14 A 7 / \\ & -12 B 7 \\ & \hline \end{aligned}$ | Remote Cut－off Pentode | L． | 8 V | 14 | 0.16 | 6.0 | 7.0 | ． 005 | Class－A Amp． | 250 | － 3.0 | 100 | 2.6 | 9.2 | 800000 | 2000 | － | － |  | $\begin{array}{\|l\|} \hline 14 A 7 / \\ 12 B 7 \\ \hline \end{array}$ |
| 14AF7 | Twin Triode | 1. | BAC | 14 | 0.16 | 2.2 | 1.6 | 2.30 | Class－A Amp． | 250 | $-10$ |  | － | 9 | 7600 | 2100 | 16 | － |  | 14AF7 |
| 14B6 | Duplex－Diode Triode | L． | 8W | 14 | 0.16 | － | － |  | Class－A Amp． | Characteristics same as 786－Table III |  |  |  |  |  |  |  |  |  | 1486 |
| 1488 | Pentogrid Converiter | L． | $8 \times$ | 14 | 0.16 | $\mathrm{lc} 2=4 \mathrm{Ma}$ ． |  |  | Convertar | Characteristics same as 7B8－Table III Characteristics same as 6V6－Table I |  |  |  |  |  |  |  |  |  | 1488 |
| 14C5 | Beam Power Amplifier | L． | 6AA | 14 | 0.24 |  | －1 | － | Class－A Amp． |  |  |  |  |  |  |  |  |  |  | 14 CS |

TABLE IX - HIGH-VOLTAGE HEATER TUBES—Continued


TABLE IX-HIGH-VOLTAGE HEATER TUBES-COntinued

tagle X-5pecial receiving tubes

| Type | Name | Base | Socket Connections | Fil. or Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Uso | Plate Supply Volts | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Volts } \end{aligned}$ | Screen Current Ma. | PlateCurrent Ma. | $\left\lvert\, \begin{gathered} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{gathered}\right.$ | Transconductance Micromhos | Amp. Factor | Load ResistanceOhms Ohm | Power <br> Output <br> Wafts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volls | Amp. | 1 n | Out | Plale. Grid |  |  |  |  |  |  |  |  |  |  |  |  |
| 00.A ${ }^{\text {? }}$ | Triode Deteclor | M. | 40 | 5.0 | 0.25 | 3.2 | 2.0 | 8.50 | Grid-Leak Det. | 45 |  |  |  | 1.5 | 30000 | 666 | 20 | $\cdots$ | $\square$ | OO-A |
| O1-A | Triode Detector Amplifler | M. | 4 D | 5.0 | 0.25 |  |  |  | Class-A Amo. | 135 | -9.0 |  |  | 3.0 | 10000 | 800 | 8.0 |  |  | 01-A |
| 3Aagt | Diode Triode Pentode | 0. | 8AS | 1.4 | 0.1 | 2.6 | 4.2 | 2.0 | Class A Triode | 90 | 0 |  |  | 0.15 | 240000 | 275 | 65 |  | - | 3ABGT |
|  |  |  |  | 2.8 | 0.05 | 3.0 | 10.0 | 0.012 | Class-A Pentode | 90 | 0 | 90 | 0.3 | 1.2 | 600000 | 750 |  |  |  |  |
| 385GT | Beom Power Amplifier | 0. | 7AP | $\left[\begin{array}{l} 1.4 \\ 2.8 \end{array}\right.$ | $\begin{aligned} & 0.1 \\ & 0.05 \end{aligned}$ |  |  |  | Class-A Amp. | 67.5 | - 7.0 | 67.5 | $\begin{aligned} & 0.6 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 6.7 \end{aligned}$ | 100000 | $\begin{aligned} & 1650 \\ & 1500 \end{aligned}$ | - | 5000 | $\begin{aligned} & 0.2 \\ & 0.18 \end{aligned}$ | 385GT |
| 3C5GT | Power Output Pentode | 0. | 740 | $\begin{array}{r} 1.4 \\ 2.8 \\ \hline \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.05 \end{aligned}$ |  |  | - | Class-A Amp. | 90 | - 9.0 | 90 | 1.4 | 6.0 | - | $\begin{aligned} & 1550 \\ & 1450 \end{aligned}$ | - | $\begin{array}{r} 8000 \\ 10000 \\ \hline \end{array}$ | $\begin{aligned} & 0.24 \\ & 0.26 \end{aligned}$ | 3C5GT |
| $3 \mathrm{C6}$ | Twin Triode | L. | 78w | $\begin{aligned} & 1.4 \\ & 2.8 \end{aligned}$ | $\begin{aligned} & 0.1 \\ & 0.05 \end{aligned}$ |  |  |  | Class-A Amp. | 90 | 0 | - | - | 4.5 | 11200 | 1300 | 14.5 | - | - | $3 \mathrm{C6}$ |
| 3154 | Power Amplifiar Pentode | $\underline{L}$ | 6BA | 2.8 | 0.05 |  |  |  | Class-A Amo. | 90 | - 9.0 | 90 | 1.8 | 9.0 | 110000 | 1600 |  | 6000 | 0.30 | 3LE4 |
| 3LF4 | Power Amplifier Tetrode | L. | 688 | $\begin{array}{\|l\|} \hline 1.4 \\ \hline 2.8 \\ \hline \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.05 \end{aligned}$ |  |  |  | Class-A Amp. | 90 | - 4.5 | 90 | $\begin{aligned} & 1.3 \\ & 1.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 8.0 \end{aligned}$ | $\begin{aligned} & 75000 \\ & 89000 \end{aligned}$ | $\begin{aligned} & 2200 \\ & 2000 \end{aligned}$ | - | $\begin{aligned} & 8000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 0.27 \\ & 0.23 \end{aligned}$ | 3LF4 |
| 305GT | Beam Power Amplifier | O. | TAQ | $\begin{array}{\|l\|} \hline 1.4 \\ \hline 2.8 \\ \hline \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.05 \end{aligned}$ | Parallel Filaments Series Filaments |  |  | Class-A Amp. | 90 | - 4.5 | 90 | $\begin{aligned} & 1.3 \\ & 1.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 7.5 \\ & \hline \end{aligned}$ | - | $\begin{aligned} & 2100 \\ & 1900 \\ & \hline \end{aligned}$ | - | 8000 | $\begin{aligned} & 0.27 \\ & 0.25 \end{aligned}$ | 3Q5GT |
| 4A6G | Twin Triode Amplifier | 0. | 81 | $\begin{aligned} & 4 \\ & 2 \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.12 \end{aligned}$ | Triodes Parallel |  |  | Class-A Amp. | 90 | - 1.5 | - |  | 2.2 | 13303 | 1500 | 20 | - | , | 4A6G |
|  |  |  |  |  |  | Both Sections |  |  | Class-B Amp. | 90 | 0 | - |  | 4.6 |  |  |  | 3000 | 1.0 |  |
| 6F4 | Acorn Triode | A. | 7BR | 6.3 | 0.225 | 2.0 | 0.6 | 1.90 | Class-A Amp. | 80 | 150* |  |  | 13.0 | 2900 | 5800 | 17 | - | - | 6 F4 |
| 614 | U.H.F. Triode | A. | 7BR | 6.3 | 0.225 | 1.3 | 0.5 | 1.6 | Class-A Amp. | B0 | 150* |  |  | 9.5 | 4400 | 6400 | 28 | - |  | 614 |
| 10 | Triode Power Amplifier | M. | 4D | 7.5 | 1.25 | 4.3 | 3.0 | 7.00 | Class-A Amp. | 425 | -37.0 |  |  | 18.0 | 5000 | 1600 | 8.0 | 10200 | 1.6 | 10 |
| 11/12 ${ }^{7}$ | Triode Dotactor Amplifier | M. | 4F/4D | 1.1 | 0.25 |  |  |  | Cliss-A Amp. | 135 | -10.5 |  |  | 3.0 | 15000 | 440 | 6.6 | 二 | - | 11/12 |
| $20^{7}$ | Triode Power Amblifier | 5. | 4 D | 3.3 | 0.132 | 2.3 | 2.3 | 4.10 | Clasi-A Amo. | 135 | -22.5 | $\square$ |  | 6.5 | 6300 | 525 | 3.3 | 6530 | 0.11 | 20 |
| $22^{7}$ | Tetrode R.F. Amplifer | M. | 4K | 3.3 | 0.132 | 3.5 | 10 | 0.02 | Class-A Amp. | 135 | - 1.5 | 67.5 | 1.3 | 3.7 | 325000 | 500 | 160 | - |  | 22 |
| 26 | Triade Amplifiar | M. | 40 | 1.5 | 1.05 | 2.8 | 2.5 | 8.10 | Class-A Amp. | 180 | -14.5 |  | - | 6.2 | 7300 | 1150 | 8.3 | - | + | 26 |
| $40^{7}$ | Triode Vollage Amplifer | M. | 4D | 5.0 | 0.25 | 2.8 | 2.2 | 2.00 | Class-A Amp. | 180 | $-3.0$ |  | - | 0.2 | 150000 | 200 | 30 | - |  | 40 |
| 50 | Triode Powar Amplifier | M. | 4D | 7.5 | 1.25 | 4.2 | 3.4 | 7.15 | Class-A Amp. | 450 | -84.0 |  | -- | 55.0 | 1830 | 2100 | 3.8 | 4350 | 4.6 | 50 |

table X-special receiving tubes-Continued

| Typo | Nome | ecse | Socke: Connactions | fii. or Hoator |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | $\begin{array}{\|l\|} \text { Plate } \\ \text { Supply } \\ \text { Volis } \end{array}$ | Grid Bias | $\begin{array}{\|c\|} \text { Screen } \\ \text { Volts } \end{array}$ | Screen Currenl Ma. | Plate Current Ma. | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{array} \\ \hline \end{array}$ | Transconductance Mieromhos | Amp. Factor |  | Power Watts$\square$ | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ¢ volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 71.A | Triode Power Amplifier | M. | 4D | 5.0 | 0.25 | 3.2 | 2.9 | 7.50 | Class-A Amp. | 180 | -43.0 | - | 二二 | 23.0 | 1750 | 1700 | 3.0 | 4800 | 0.79 | 71.4 |
| 996 | Triode Detector Amplifer | S. | 40 | 3.3 | 0.063 | 2.5 | 2.5 | 3.30 | Closs-A Amp. | 90 | - 4.5 | - | - | 2.5 | 15500 | 425 | 6.6 |  | -- | 99 |
| 112A ${ }^{\text {T }}$ | Triode Delector Amplifier | M. | 4D | 5.0 | 0.25 |  |  |  | Class-A Amp. | 180 | -13.5 | - | $\cdots$ | 7.7 | 4700 | 1800 | 0.5 |  | - | 112A |
| $\begin{aligned} & 18281 \\ & 4828 \\ & \hline \end{aligned}$ | Triode Amplifer | M. | 4D | 5.0 | 1.25 | - | - | - | Class-A Amp. | 250 | -35.0 | - | - | 18.0 | - | 1500 | 5.0 | - | - | $\begin{aligned} & 1828 / \\ & 4828 \end{aligned}$ |
| 183/483 ${ }^{\text {7 }}$ | Power Triode | m . | 4D | 5.0 | 1.25 | - | - | - | Class-A Amp. | 250 | -60.0 | - | - | 25.0 | 18000 | 1800 | 3.2 | 4500 | 2.0 | 183/483 |
| $485^{7}$ | Triode | S. | 5A | 3.0 | 1.3 |  | - | $=$ | Class-A Amp. | 180 | - 9.0 | - | $\cdots$ | 6.0 | 9300 | 1350 | 12.5 | $\square$ |  | 485 |
| 864 | Triode Amplifer | 5. | 40 | 1.1 | 0.25 |  |  |  | Class-A Amp. | 90 | -4.5 | - | - | 2.9 | 13500 | 610 | 8.2 |  |  | 864 |
|  |  |  |  |  |  |  |  |  | Class-A Amp. | 250 | -3.0 | 100 | 0.7 | 2.0 | 1.5 meg . | 1400 | 2000 |  | - |  |
| 954 | Amplifier | A. | 3bB | 6.3 | 0.15 | 3.4 | 3.0 | 0.007 | Bias Detector | 250 | -6.0 | 100 | $\square$ | Plate curre | entio be adju | justed to 0.1 | na. with | no signal |  | 954 |
| 955 | Triode Defector, | A. |  |  |  |  |  |  |  | 250 | - 7.0 | - | $\cdots$ | 6.3 | 11400 | 2200 | 25 | - |  |  |
| 955 | Amplifier, Oscillator | A. | 5BC | 6.3 | 0.15 | 1.0 | 0.6 | 1.40 | Class-A Amp. | 90 | - 2.5 |  | - | 2.5 | 14700 | 1700 | 25 |  |  | 955 |
| 956 | Voriable- $\mu$ Pentode | A. | 5BB | 6.3 | 0.15 | 3.4 | 3.0 | 0.007 | Closs-A Amp. | 250 | -2.0 <br> -10.0 | 100 | 2.7 | 6.7 | 700000 | 1800 | 1440 |  | - | 956 |
| Os | R.F. Amplifier |  | SBE | 6.3 | 0.15 | 3.4 | 3.0 |  | Mixer | 250 | $-10.0$ | 100 |  |  |  | Oscillator peor | ak volts | -7 min. |  | 956 |
| 957 | Triode Detector, Amplifier, Oscillator | A. | 5BD | 1.25 | 0.05 | 0.3 | 0.7 | 1.20 | Closs-A Amp. | 135 | $-5.0$ | - | - | 2.0 | 20800 | 650 | 13.5 | - | - | 957 |
| $\begin{aligned} & 958 \\ & 958-A \end{aligned}$ | Triode A.F. Amplifier, Oscillator | A. | 5BD | 1.25 | 0.1 | 0.6 | 0.8 | 2.60 | Class-A Amp. | 135 | - 7.5 | - | - | 3.0 | 10000 | 1200 | 12 | - | - | $\begin{aligned} & 958 \\ & 958-\mathrm{A} \end{aligned}$ |
| 959 | Penlode Detector, Amplifier | A. | 5BE | 1.25 | 0.05 | 1.8 | 2.5 | 0.015 | Class-A Amp. | 145 | - 3.0 | 67.5 | 0.4 | 1.7 | 800000 | 600 | 480 | - | - | 959 |
| 7E5/1201. | U.h.f. Triode | 1. | 8BN | 6.3 | 0.15 | 3.6 | 2.8 | 1.50 | Class-A Amp. | 180 | $-3$ |  | - | 5.5 | 12000 | - | 36 | - | - | 7E5/1201 |
| 7C4/1203 | U.h.f. Diode | 1. | 4AH | 6.3 | 0.15 |  |  |  | Rectifar |  |  | x. r.m.s. | voltage-1 |  | Max. | d.e. output e | current- | 8 ma . |  | 7C4/1203 |
| $\begin{aligned} & 7 \mathrm{AB71} \\ & 1204 \\ & \hline \end{aligned}$ | Sharp Cut-off Pentode | 1. | 8 BO | 6.3 | 0.15 | 3.5 | 4.0 | 0.06 | Class-A Amp. | 250 | - 2 | 100 | 0.6 | 1.75 | 800000 | 1200 | - | - | - | $\begin{aligned} & 7 \mathrm{AB7/} \\ & 1204 \\ & \hline \end{aligned}$ |
| 1276 | Triode Power Amplifier | M. 1 | 140 | 4.5 | 1.14 |  |  |  | Class-A Amp. |  |  |  |  | haracteristi | tics similar 90 | -6A3 |  |  |  | 1276 |
| 1609 | Pentode Amplifor | 5. | 5B | 1.1 | 0.25 | - |  |  | Class-A Amp. | 135 | - 1.5 | 67.5 | 0.65 | 2.5 | 400000 | 725 | 300 |  |  | 1609 |
| 9004 | U.h.t. Diode | A. | 48. | 6.3 | 0.15 | - | - | - | Delector |  |  | Max. | a.c. vollorg | -117. | Max. d.c. out | utput current- | -5 ma. |  |  | 9004 |
| 9005 | U.h.f. Diode | A. | 5BG | 3.6 | 0.165 | - |  |  | Datector |  |  | Max. | a.c. voltag | -117. | Max. dic. out | utput currant- | -1 ma. |  |  | 9005 |
| EF-50 | Sharp Cul-off Pentode | 1. | 9 C | 6.3 | 0.3 | 8 | 5 | 0.007 | I.F.-R.F. Amp. | 250 | 150* | 250 | 3.1 | 10 | 600000 | 6300 |  | - |  | EF-50 |
| $\begin{aligned} & \hline \text { GL-2C44 } \\ & \text { GL-464A } \\ & \hline \end{aligned}$ | U.h.f. Triode | O. | , Fig. 17 | 6.3 | 0.75 | - | - | - | Closs-A Amp. and Modulator | 250 | 100* | - | - | 25.0 | -- | 7000 | - | - | - | $\begin{aligned} & \text { GL-2C44 } \\ & \text { GL-464A } \end{aligned}$ |
| $\begin{aligned} & G L-446 \mathrm{~A} \\ & G L-446 \mathrm{~B} \\ & \hline \end{aligned}$ | U.h.f. Triode | 0. | Fig. 19 | 6.3 | 0.75 | - | - | - | Oscillator, Amp. or Converter | 250 | 200* | - | - | 15.0 | - | 4500 | 45 | - | - | $\begin{aligned} & \text { GL-446A } \\ & \text { GL-446B } \end{aligned}$ |
| $\begin{aligned} & 559 \\ & \text { GL-559 } \\ & \hline \end{aligned}$ | U.h.f. Diode | 0. | Fig. 18 | 6.3 | 0.75 | - | - | - | Detector or trans. line switch | 5.0 | - | - | - | 24.0 | - | - | - | - | - | $\begin{aligned} & 559 \\ & G L-559 \end{aligned}$ |
| NU-2C35 | Special Hi-Mu Triode | 0. | Fig. 38 | 6.3 | 0.3 | 5.2 | 2.3 | 0.62 | Shunt Voltage Regulator | 8000 | -200 | - | - | 5.0 | 525000 | 950 | 500 | - |  | NU-2C35 |
| VT52 | Triode | M. ${ }^{\text {i }}$ | - 4D | 7.0 | 1.18 | 5.0 | 3.0 | 7.7 | Class-A, Amp. | 220 | -43.5 |  | - | 29.0 | 1650 | 2300 | 3.8 | 3800 | 1.0 | VT52 |
| $\times 6030$ | Diode | 1. | Fig. 4 | 3.0 | 0.6 | - | -1 |  | Noise Diode | 90 | - |  | - | 4.0 | - | - | - | - - |  | $\times 6030$ |

TABLE X-SPECIAL RECEIVING TUBES-Continued

| Type | Nome | Bose | Socke 1 Connecfions | Fil. or Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Piate Supply Yolis | Grid Bias | $\begin{aligned} & \text { Screen } \\ & \text { Volts } \end{aligned}$ | Screen Current Ma. | $\begin{gathered} \text { Plate } \\ \text { Current } \\ \text { Ma. } \end{gathered}$ | PlateResistanceOhms | Transconductance Micromhos | Amp. Factor | Load Resistance Ohms | Power Outpul Walts | Typo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Voits | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| XX8 | Twin-Triode Frequency Converter | L. | Fig. 9 | 2.8/ | $\begin{aligned} & 0.05 / \\ & 0.10 \end{aligned}$ |  |  | - | Converter ${ }^{2}$ | $90^{1}$ | 0 | - | - | $\begin{aligned} & 4.5^{4} \\ & 4.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 11200^{4} \\ & 11200^{5} \end{aligned}$ | $\begin{array}{r} 13004 \\ 1300^{5} \\ \hline \end{array}$ | 14.51 | - | - | XXB |
|  |  |  |  | $\begin{gathered} 3.2^{3} / 4 \\ 1.6 \end{gathered}$ | $\underline{\square}$ |  |  |  |  |  | - 3 | - | - | $\begin{aligned} & 1.4^{4} \\ & 1.45 \\ & \hline \end{aligned}$ | $\begin{aligned} & 19004 \\ & 1900^{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & 760^{4} \\ & 760^{5} \\ & \hline \end{aligned}$ | 14.51 | - | - |  |
| XXFM | Twin-Diode Triode | L. | 8BZ | 6.3 | 0.3 | - |  |  | Class-A Amp. | 250 | -1 | $\square$ | - | 1.9 | 6700 | 1500 | 100 | - | $\square$ | XXFM |
| XXFm | Twin-Diode Triode | 4. | 8 Bz | 6.3 | 0.3 |  |  |  |  | 100 | 0 |  | - | 1.2 | 85000 | 1000 | 85 |  |  |  |
| * Cathode resistor-ohms. |  | 1 Both sections. <br> : Section No. 2 recommended for h.f.o. |  |  |  |  |  | ${ }^{3}$ Dry battery operation. <br> 4 Section No. 1. |  |  | ${ }^{5}$ Section No. 2. <br> - Same as X99. Type V99 is same, but socket connections are $4 E$. |  |  |  |  |  |  | ${ }^{7}$ Discontinued. |  |  |

TABLE XI-MINIATURE RECEIVING TUBES
Other miniature types in Tables XIII and XV

| Type | Name | Base | Sockel Connections | Fil. or Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{gathered} \text { Sereen } \\ \text { Volts } \end{gathered}$ | Screen Curren 1 Ma. | Plate Curren Ma. | $\begin{array}{\|c\|} \hline \text { Plate } \\ \text { Resistonce } \\ \text { Ohms } \end{array}$ | Transconductance Micromhos | Amp. <br> Factor | $\left\lvert\, \begin{gathered} \text { Load } \\ \text { Ressistance } \\ \text { Ohms } \end{gathered}\right.$ | Power Outpul Walts | Prototyp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | PlatoGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 143 | H. F. Diode | B. | 5AP | 1.4 | 0.15 | - | - | - | Detector F.M. Discrim. |  | Max. a.c. voltage per plato-117. |  |  |  | . Max. output current-0.5 ma. |  |  |  |  | - |
| 114 | Sharp Cut-off Pentode | B. | 6AR | 1.4 | 0.05 | 3.6 | 7.5 | . 008 | Class-A Amp. | 90 | 0 | 90 | 2.0 | 4.5 | 350000 | 1025 | - |  |  | INSGT |
| 1R5 | Pentagrid Converter | B. | 7AT | 1.4 | 0.05 | - |  | - | Convertor | 90 | 0 | 67.5 | 3.0 | 1.7 | 500000 | 300 | Grid No. 1100000 ohms |  |  | IATGT |
| 154 | Pentagrid Power Amp. | B. | 7 AV | 1.4 | 0.1 | - |  |  | Class-A Amp. | 90 | - 7.0 | 67.5 | 1.4 | 7.4 | 100000 | 1575 |  | 8000 | 0.270 | 195GT |
|  |  | B. |  | 1.4 | 0.05 |  |  |  | Class-A Amp. | 67.5 | 0 | 67.5 | 0.4 | 1.6 | 600000 | 625 |  |  |  |  |
| 155 | Diode Pentode | B. | 6AU | 1.4 | 0.05 |  |  |  | R-Coupled Amp. | 90 | 0 | 90 | Screen resistor 3 meg., grid 10 meg. |  |  |  |  | 1 mag . | 0.050 |  |
| 174 | Variable- $\mu$ Pentode | B. | 6AR | 1.4 | 0.05 | 3.6 | 7.5 | 0.01 | Class-A Amp. | 90 | 0 | 67.5 | 1.4 | 3.5 | 500000 | 900 |  |  |  | 1P5GT |
| 104 | Sharp Cut-off Pentode | B. | 6AR | 1.4 | 0.05 | 3.6 | 7.5 | 0.01 | Class-A Amp. | 90 | 0 | 90 | 0.5 | 1.6 | 1500000 | 900 | - | - | - | INSGT |
| 105 | Diode Penlode | B. | 6BW | 1.4 | 0.05 |  |  | - | Class-A Amp. | 67.5 | 0 | 67.5 | 0.4 | 1.6 | 600000 | 625 |  |  | - | - |
| 2 C 51 | Twin Triode | 8. | 8 CJ | 6.3 | 0.3 | 2.2 | 1.0 | 1.3 | Class-A1 Amp. | 150 | - 2 |  |  | 8.2 | - | 5500 | 35 |  | - | $7 \mathrm{F8}$ |
| 2E30 | Beam Power Pentode | B. | 7 CO | 6.0 | 0.7 | 10 | 4.5 | 0.5 | Class-A ${ }^{\text {a }}$ Single | 250 | 450* | 250 | $7.4^{2}$ | $44^{2}$ | 63000 | 3700 | $40^{5}$ | 4500 | 4.5 |  |
|  |  |  |  |  |  |  |  |  | Class-A1 Amp. ${ }^{3}$ | 250 | 225* | 250 | 14.8: | 88. |  |  | 80 - | $9000{ }^{\circ}$ | 9 | - |
|  |  |  |  |  |  |  |  |  | Clast-AB ${ }^{\text {a }}$ Amp. ${ }^{\text {a }}$ | 250 | -25 | 250 | $13.5{ }^{2}$ | $80^{2}$ | - | - | 486 | $8000{ }^{\circ}$ | 12.5 |  |
|  |  |  |  |  |  |  |  |  | Class-AB2 ${ }^{\text {Amp }}{ }^{3}{ }^{\text {a }}$ | 250 | -30 | 250 | $20{ }^{2}$ | 1202 | - | - | $40^{\circ}$ | $3800{ }^{\circ}$ | 17 |  |
| 3 A4 | Power Amplifer Pentode | B. | 7BB | $\begin{aligned} & 1.4 \\ & 2.8 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.2 \\ 0.1 \end{gathered}$ | 4.8 | 4.2 | 0.34 | Class-A Amp. | $\begin{aligned} & 135 \\ & 150 \end{aligned}$ | $\begin{array}{r} -7.5 \\ -8.4 \end{array}$ | $\begin{aligned} & 90 \\ & 90 \end{aligned}$ | $\begin{aligned} & 2.6 \\ & 2.2 \end{aligned}$ | $\begin{aligned} & 14.9^{2} \\ & 14.1^{2} \end{aligned}$ | $\begin{gathered} 90000 \\ 100000 \end{gathered}$ | 1900 | - | 8000 | $\begin{aligned} & 0.6 \\ & 0.7 \\ & \hline \end{aligned}$ | - |
| 3A5 | H.F. Twin Triode | B. | 7BC | $\begin{aligned} & 1.4 \\ & 2.8 \end{aligned}$ | $\begin{array}{\|l\|} \hline 0.22 \\ 0.11 \\ \hline \end{array}$ | 0.9 | 1.0 | 3.20 | Class-A Amp. | 90 | - 2.5 | - | - | 3.7 | 8300 | 1800 | 15 | - | - | - |
| 304 | Power Amplifer Pentode | B. | 7BA | $\begin{aligned} & 1.4 \\ & 2.8 \end{aligned}$ | $\begin{aligned} & 0.1 \\ & 0.05 \\ & \hline \end{aligned}$ | Parallel filaments Serias Filaments |  |  | Class-A Amp. | 90 | - 4.5 | 90 | $\begin{aligned} & 2.1 \\ & 1.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & 9.5 \\ & 7.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} 100000 \\ 120000 \\ \hline \end{array}$ | $\begin{array}{r} 2150 \\ 2000 \\ \hline \end{array}$ | - | 10000 | $\begin{aligned} & 0.27 \\ & 0.24 \\ & \hline \end{aligned}$ | 305GT |
| 354 | Power Amplifior Pentode | B. | 78A | $\begin{aligned} & 1.4 \\ & 2.8 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 0.1 \\ 0.05 \\ \hline \end{array}$ | Parallel Filaments <br> Sories Filaments |  |  | Class-A Amp. | 90 | - 7.0 | 67.5 | $\begin{aligned} & 1.4 \\ & 1.1 \\ & \hline \end{aligned}$ | $\begin{array}{r} 7.4 \\ 6.1 \\ \hline \end{array}$ | 100000 | $\begin{aligned} & 1575 \\ & 1425 \end{aligned}$ | - | 8000 | $\begin{aligned} & 0.27 \\ & 0.235 \end{aligned}$ | 3Q3GT |
| 3V4 | Power Amplifier Penlode | B. | 6BX | 1.4 | 0.1 | Parallel Filaments Serias Filaments |  |  | Class-A Amp. | 90 | - 4.5 | 90 | 2.1 | 9.5 | 100000 | 2150 |  | 10000 | 0.27 | 305GT |
|  |  |  |  | 2.8 | 0.05 |  |  |  | Class-A Amp. | 90 | -4.5 | 90 | 1.7 | 7.7 | 120000 | 2000 |  | 10000 | 0.24 |  |
| 6AB4 | Triode R.F. Amp. | B. | 5CE | 6.3 | 0.15 | 2.2 | 0.5 | 1.5 | Class-A Amp. | 250 | - 2 | - | - | 10 | - | 5500 | 55 | - | - | $\begin{array}{\|c\|} \hline \text { Single unit } \\ 12 \mathrm{AT} 7 \\ \hline \end{array}$ |
| 6AG5 | Sharp Cut-oft Pentode | B. | 7BD | 6.3 | 0.3 | - | - | - | Class-A Amp. | $\begin{aligned} & 250 \\ & 100 \\ & \hline \end{aligned}$ | $\begin{aligned} & 200^{*} \\ & 100^{*} \end{aligned}$ | $\begin{aligned} & 150 \\ & 100 \end{aligned}$ | $\begin{aligned} & 2.0 \\ & 1.6 \end{aligned}$ | $\begin{aligned} & 7.0 \\ & 5.5 \end{aligned}$ | $\begin{aligned} & 800000 \\ & 300000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5000 \\ & 4750 \\ & \hline \end{aligned}$ |  | - | - | 6SH7GT |
| 6AH6 | Sharp Cut-off Pentode | B. | 7CC | 6.3 | 0.45 | 10 | 2 | 0.03 | Pentode Amp. | 300 | $\frac{160^{*}}{160^{*}}$ | 150 | 2.5 | 10 | 500000 | 9000 | $=$ | $\cdots$ | - |  |
| SANG | Shap Curor Ponnodo |  |  |  |  | 10 | 2 | 0.03 | Triode Amp.: | 150 | 160* | - | - | 12.5 | 3600 | 11000 | 40 | - |  | 6AC7 |
| 6AJ5 | Sharp Cut-off Pentode | B. | 7PM | 6.3 | 0.175 | - | - | - | R.F. Amplifier | 28 | 200* | 28 | 1.2 | 3.0 | 90000 | 2750 | 250 | 280006 |  | - |
|  |  |  |  |  |  |  |  |  | Class-AB Amp. ${ }^{3}$ | 180 | - 7.5 | 75 | 2 | 7 | - | $\pm$ | - | $28000{ }^{5}$ | 1.0 |  |
|  | Sharp Cut-off Pentode | B. | 7BD |  |  |  |  |  |  | 180 | 200** | 120 | 2.4 | 7.7 | 690000 | 5100 | 3500 | - | - |  |
| 6 aks | Sharp Cul-off Pentode | B. |  | 6.3 | 0.175 | 4.3 | 2.1 | 0.03 | R.F. Amplifier | 150 | 330** | 140 | 2.2 | 7.0 7.5 | 420000 <br> 340000 | 4300 <br> 5000 | $\begin{array}{r}1800 \\ \hline 1700\end{array}$ | = | $\underline{\square}$ |  |

TABLE XI-MINIATURE RECEIVING TUBES-Continued

| Type | Name | Base | Socke ${ }^{+}$ Conneclions | Fil. or Heater |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Us* | Plate Supply Volts | Grid Bios | Screen | Screen Current Ma. | Plate Current Ma. | $\begin{array}{\|c\|} \text { Plate } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Transconductance Micromhas | Amp. Factor | $\begin{array}{\|c} \text { Load } \\ \text { Resistance } \\ \text { Ohms } \end{array}$ | Power Output Wafts | Prototype |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | PlateGrid |  |  |  |  |  |  |  |  |  |  |  |  |
| 6AK6 | Power Amplifier Pentode | 8. | 7BK | 6.3 | 0.15 | 3.6 | 4.2 | 0.12 | Class-A Amp. | 180 | - 9.0 | 180 | 2.5 | 15.0 | 200000 | 2300 |  | 10000 | 1.1 |  |
| 6ALS | U.h.f. Twin Diode | B. | 6 BT | 6.3 | 0.3 |  |  |  | Detector |  |  | Max. r.m.s. voltage-150. Max. d.e. output current-10 ma. ${ }^{1}$ |  |  |  |  |  |  |  | 6H6GT |
| GANS | Power Amp. Pentode | B. | 780 | 6.3 | 0.5 | 9.0 | 4.8 | 0.05 | Class-A1 Amp. | 120 | - 6 | 120 | 12 | 35 | 12500 | 8000 |  |  |  | 6AG7 |
| GANS | Twin Diode | B. | 7BJ | 6.3 | 0.2 |  | - |  | Detector | R.m.s. voltage per plate $=75$ volts; d.c. output $=\mathbf{3 . 5} \mathrm{ma}$. with $\mathbf{2 5 0 0 0}$ ohms and $8 \mu \mu \mathrm{fl}$. load; peak current per plate $=10$ ma.; peak inverse voltage $=210$. |  |  |  |  |  |  |  |  |  | - |
|  |  | B. | 782 | 6.3 | 0.45 | 7.6 | 6.0 | 0.35 | Class-A, Amp. | 180 | -8.5 | 180 | $4.0{ }^{2}$ | 30 : | 58000 | 3700 | 29 : | 5500 | 2.0 | 6V6GT |
| 6AO5 | Beom Power Yotrode | B. | 7 BZ | 6.3 | 0.45 | 7.6 | 6.0 | 0.35 |  | 250 | -12.5 | 250 | $7.0{ }^{2}$ | 47: | 52000 | 4100 | 45. | 5000 | 4.5 |  |
|  |  |  |  |  |  |  |  |  | Class-A Triode | 250 | - 3.0 |  |  | 1.0 | 58000 | 1200 | 70 |  |  | 6T7G |
| A06 | lode | ${ }^{\text {B. }}$ | 781 | 6.3 | 0.15 | 1.7 | 1.5 | 1.80 |  | 100 | - 1.0 | - |  | 0.8 | 61000 | 1150 | 70 |  |  |  |
| 6AR5 | Pentode Powor Amp. | B. | 6CC | 6.3 | 0.4 |  | - |  | Class-A Amp. | 250 | -18 | 250 | $5.5{ }^{2}$ | $33^{2}$ | 68800 | 2300 |  | 7800 | 3.4 | 6K6GT |
|  |  |  |  |  |  |  |  |  |  | 250 | -16.5 | 250 | 5.5 ? | 35 | 65000 | 2400 | - | 7000 | 3.2 |  |
| 6AS5 | Beam Pentode | B. | 7 CV | 6.3 | 0.8 | 12 | 6.2 | 0.6 | Class- $A_{1}$ Amp. | 150 | -8.5 | 110 | 2/8.5 | 35/36 |  | 5600 |  | 4500 | 2.2 | - |
| 6AS6 | Sharp Cut-off Pentode | B. | 7 CM | 6.3 | 0.175 | 4.0 | 3.0 | 0.02 | Class-A Amp. | 120 | 2 | 120 | 3.5 | 5.5 | - | 3500 | - |  |  |  |
| 6AT6 | Duplex Diode Triode | B. | 7B7 | 6.3 | 0.3 | 2.3 | 1.1 | 2.10 | Class-A Amp. Class-A Amp. | 250 | - 3 |  |  | 1.0 | 58000 | 1200 | 70 | - |  | 60761 |
| GAU6 | Sharp Cut-off Pentode | B. | 7BK | 6.3 | 0.3 | 5.5 | 5.0 | . 0035 |  | 250 | -1 | 150 | 4.3 | 10.8 | 2000000 | 5200 |  |  |  | 65H7GT |
| GAV6 | Duodiode Hi-mu Triode | B. | 78 T | 6.3 | 0.3 |  |  |  | Class-A A Amp. | 250 | 2 |  |  | 1.2 | 62500 | 1600 | 100 |  |  | 6SO7GT |
| 6896 | Remote Cut-off Pentode | B. | 7CC | 6.3 | 0.3 | 5.5 | 5.0 | . 0035 |  | 250 | 68* | 100 | 4.2 | 11 | 1500000 | 4400 |  |  |  | 6SG7GT |
| 68A7 | Pentogrid Converter | B. | ${ }^{\text {BCT }}$ | 6.3 | 0.3 | 9.5 | 8.3 |  | Convertior | 250 | - 1 | 100 | 10 | 3.8 | 1000000 | 3.5 |  | $\square$ |  | 65B7Y |
| 6806 | Remote Cut-off Pentode | B. | 7CC | 6.3 | 0.3 |  | - |  | Class-A Amp. | 100 | - 1 | 100 | 5 | 13 | 120000 | 2350 |  |  | $\square$ | 6SK7GT |
| 6806 | Remote Cut-oft Pentode |  |  |  |  |  |  |  |  | 250 | - 3 | 100 | 3.5 | 9 | 700000 | 2000 |  |  |  |  |
| GEE6 | Pentagrid Converter | B. | 7 CH | 6.3 | 0.3 | Ose. Grid $50000 \Omega$ |  |  | Converter | 250 | - 1.5 | 100 | 7.8 | 3.0 | 1000000 | 475 |  |  |  | 6SATGT |
| 68F6 | Duplex-Diode Triode | B. | 7BT | 6.3 | 0.3 | 1.8 | 1.1 | 2.0 | Class-A $\mathrm{A}_{1}$ Amp. | 250 | - 9 |  |  | 9.5 | 8500 | 1900 | 16 | 10000 | - | 6SR7GT |
| 68H6 | Sharp Cut-off Pentode | B. | 7 CM | 6.3 | 0.15 | 5.4 | 4.4 | 0.0035 | Class-A ${ }_{1}$ Amp. | 250 | - 1 | 150 | 2.9 | 7.4 | 1400000 | 4600 |  | - |  | 6S57GT |
| 6856 | Remote Cut-off Pentode | B. | 7CM | 6.3 | 0.15 | 4.5 | 5.0 | . 0035 | Class-A, Amp. | 250 | - 1 | 100 | 3.3 | 9.2 | 1300000 | 3800 |  | - |  |  |
| $6{ }_{6} 4$ | Triode Amplifier | B. | 6BG | 6.3 | 0.15 | 1.8 | 1.3 | 1.60 | Closs-A ${ }_{1}$ Amp. | 250 | - 8.5 |  |  | 10.5 | 7700 | 2200 | 17 |  |  | 6J5GT |
| 654 | U.h.f. Grounded-Grid R.F. Amplifier | B. | 7BQ | 6.3 | 0.4 | 5.5 | 0.24 | 4.0 | Grounded-Grid <br> Clast $A_{1}$ Amp. | 150 | 200* | - |  | $\begin{aligned} & \hline 15.0 \\ & \hline 10.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 4500 \\ & 5000 \end{aligned}$ | $\begin{array}{\|l\|} \hline 12000 \\ \hline 11000 \\ \hline \end{array}$ | 55 | - |  | — |
|  |  |  |  |  |  |  |  |  |  | 100 | 100* |  |  |  |  |  |  |  |  |  |
| 856 | Twin Triode | B. | 7BF | 6.3 | 0.45 | 2.2 | 0.4 | 1.6 | Closs-A Amp. Mixer, Oscillator | 100 |  | - | - | 8.5 | 7100 | 5300 | 38 | - |  | - |
| 6 N 4 | U.h.f. Triode Amplifior | 8. | 7CA | 6.3 | 0.2 | 3.0 | 1.6 | 1.10 | Class-A Amp. | 180 | - 3.5 |  |  | 12.0 |  | 6000 | 32 | - | - | - |
| $6 \mathrm{~T} /$ | Triple-Diode Triode | 8. | 9E | 6.3 | 0.45 | 1.5 | 1.1 | 2.4 | Class-A, Amp. | 250 | 3 | — | - | 1.0 | 5800 | 1200 | 70 |  |  | - |
| 678 | Triple-Diode Triode | B. | $9 E$ | 6.3 | 0.45 | 1.5 | 1.1 | 2.4 |  | 100 | - 1 | 二 |  | 0.8 | 5400 | 1300 | 70 | k mo. |  |  |
| 12AL5 | Twin Diode | B. | 68T | 12.6 | 0.15 | 2.5 | - | - | Detector |  | R.m.s. voltage per plaper plate-3.0 |  |  | $\begin{gathered} =117 ; d . \\ 54 ; \text { peak } \\ 1.0 \end{gathered}$ | $\begin{aligned} & \text { c. output =9 } \\ & k \text { inverse volt } \end{aligned}$ | $\begin{aligned} & 9 \mathrm{ma} \text {. per plo } \\ & \text { ltage }=330 . \\ & \hline \end{aligned}$ | ; peak |  |  | 12H6GT |
| 12AT6 | Duplax Diode Triode | B. | 7BT | 12.6 | 0.15 | 2.3 | 1.1 | 2.10 | Class-A Amp. | 250 |  |  |  | 58000 | $1200$ | 70 |  |  |  |  |
| 12AT7 | Double Triode | B. | 9A | 6.3 | 0.3 | 2.5 | 0.45 | 1.45 | Class-A ${ }^{2}$ Amp. Each Uníl | 250 | -2 |  | - |  | 10 | 10000 | 5500 | 55 |  |  | - |
|  |  |  |  | 12.6 | 0.15 | 2.5 * | $0.35{ }^{\text { }}$ | 1.458 |  | 180 | - 1 |  |  | 11 | 9400 | 6600 | 62 |  | - |  |  |
| 12AU6 | Sharp Cut-off Pentode | B. | 7 CC | 12.6 | 0.15 | 5.5 | 5.0 | . 0035 | Class-A Amp. | 250 | $-1.0$ | 150 | 4.3 | 10.8 | 1 meg. | 5200 |  |  |  | 125H7GT |  |
| 12AU7 | Twin-Triode Amplifier | B. | 9A | 6.3 | 0.3 | 1.6 | 0.5 | 1.5 | Class-A Amp. | 250 | $-8.5$ | - | - | 10.5 | 7700 | 2200 | 17 | $\cdots$ | - | 125N7GT |  |
|  |  |  |  | 12.6 | 0.15 | 1.6 \% | $0.35 \times$ | 1.58 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12AV6 | Duodiode Hi-mu Triode | B. | 7 BT | 12.6 | 0.15 |  |  |  | Class-A, Amp. | 250 | - 2 |  |  | 1.2 | 62500 | 1600 | 100 | - |  | - |  |
| 12AW6 | Sharp Cut-off Pentode | 8. | 7 CM | 12.6 | 0.15 | 6.5 | 1.5 | 0.025 | Pentode Amp. | 250 | 200* | 150 | 2.0 | 7.0 | 800000 | 5000 |  |  |  | - |  |
| I2AWb |  |  |  |  |  |  |  |  |  | 250 | 825* |  |  | 5.5 | 11000 | 3800 | 42 |  |  |  |  |
| 12AW7 | Sharp Cut-off Pentode | B. | 7 CM | 12.6 | 0.15 | 6.5 | 1.5 | 0.025 | Class-A, Amp. | 250 | 200* | 150 | 2.0 | 7.0 | 0.8 meg . | 5000 |  | - | - |  |  |
| 12AX7 | Doubla Triode | B. | 9 A | 12.6 | 0.15 | 1.6 | 0.46 | 1.7 | Class-A Amp. | 250 | - 2 | - | - | 1.21 | 62500 | 1600 | 100 |  |  |  |  |
|  |  |  |  | 6.3 | 0.3 | 1.6 | 0.34* | 1.78 |  | 100 | - | - | 二 | 0.5 | 8000 | 1250 | 100 | - |  |  |  |
| 12AY7 | Dual Triode | B. | 9A | $\begin{array}{r} 12.6 \\ 6.3 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 0.15 \\ 0.3 \\ \hline \end{array}$ | 1.3 | 0.6 | 1.3 | Class-A Amp. Lo-Level Amp. | 250 | 2700* | 100 | - | 3 | - | 1750 | 40 | - |  | 12SG7G |  |
|  |  |  |  |  |  |  |  |  |  | 150 |  |  | Plate resistor $=20000$ s!. Grid resistor $=0.1$ Meg. V. $6 .=12.5$ |  |  |  |  |  |  |  |  |
|  | Remote Cut-off Pentode | B. | 7 CC | 12.6 | 0.15 | 5.5 | 5.0 | . 0035 | Clast-A Amp. | 250 | ${ }^{8} 8$ * |  | 4.2 | 11.0 | 1500000 | 4400 |  |  | - |  |  |

TABLE XI - MINIATURE RECEIVING TUBES - Continued

table XII - SUB-miniature tubes - Continued

| Type | Name | Base | Socket Connec tion | Fil. or Heater |  | Copacitance $\mu \mu \mathrm{fd}$ d |  |  | Use | Plate Supply Volis | Gria Bias | Screen Volis | Screen Current Ma. | Plate <br> Current Ma. | PlateResistanceOhms | Transconductance Micromhos | Amp. Factor | LoadResistanseOhms | Power <br> Oulput Wafts | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Out | Prate- Grid |  |  |  |  |  |  |  |  |  |  |  |  |
| 2G21 | Triode Heptode | 1 | 2 | 1.25 | 0.05 |  |  |  | Converter | 22.5 |  | 22.5 | 0.2 | 0.3 |  | 75 | - | - |  | $2 \mathrm{G21}$ |
| 2622 | Convertar |  | : | 1.25 | 0.05 |  |  |  | Converier | 22.5 | 0 | 22.5 | 0.3 | 0.2 | 500000 | 60 |  |  |  | 2 G 22 |
| 6 K 4 | Triode |  | I | 6.3 | 0.15 | 2.4 | 0.8 | 2.4 | Class A Amp. | 200 | $680^{*}$ | - |  | 11.5 | 4650 | 3450 | 16 |  | - 6 | 6 K 4 |
| 1247 | Diode | 1 | 2 | 0.7 | 0.065 |  |  |  | R.F. Probe |  |  | Max. a.c. volis - $300 \mathrm{r.m.s}$. D.C. plate current- 0.4 Ma |  |  |  |  |  |  |  | 1247 |
| CK501 | Pentode Voltage Amplifier | - 1 | $\because$ | 1.25 | 0.033 |  |  |  | Class-A Amp. | 30 | 0 | 30 | 0.06 | 0.3 | To00000 |  | - |  | - | CK501 |
| CK502 | Peniode Output Amplifier | -1 | : | 1.25 | 0.033 |  |  |  |  | 45 | -1.25 | 45 | 0.055 | 0.28 | 1500000 | 300 |  |  |  |  |
| CK503 | Pentode Output Amplifier | - | \% | 1.25 | 0.033 |  |  |  | Class-A Amp. | 30 | 0 | 30 | 0.13 | 0.55 | 500000 | 400 |  | 60000 | 0.003 | CK502 |
| CK504 | Pentode Output Amplifier | - | : | 1.25 | 0.033 |  |  |  | Class-A Amp. | 30 | 0 | 30 | 0.33 | 1.5 | 150000 | 600 |  | 20000 | 0.006 | CK503 |
|  |  |  |  |  |  |  |  |  | Class-A Amp. | 30 | -1.25 | 30 | 0.09 | 0.4 | 500000 | 350 |  | 60000 | 0.003 | CK504 |
| CKS0s | Pentode Voirage Amplifier | - | : | 0.625 | 0.03 |  |  | - | Class-A Amp. | 45 | -125 | 30 | 0.07 | 0.17 | 1100000 | 140 | - | - |  | CK 505 |
| CK506 | Pentode Output Amplifier | - | : | 1.25 | 0.05 |  |  |  | Class-A: Amp. | 45 | -4.5 | 45 | 0.4 | 1.25 | 120000 | 500 | - | 30000 | 0.025 | CK506 |
| CK 507. | Penlode Output Amplifier | - | - | 1.25 | 0.05 |  |  |  | Closs-A, Amp. Class-A Āmp. | 45 | -2.5 | 45 | 0.21 | 0.6 | 360000 | 500 |  | 50000 | 0.010 | CK507 |
| CK509 | Triode Voltage Amplifier | -1 | " | 0.625 | 0.03 |  |  |  |  | 45 | 0 |  |  | 0.15 | 150000 | 160 | 16 | 1000000 |  | CK309 |
| CK510 | Dual Space-Charge Tatrode | - | " | 0.625 - | 0.05 |  |  |  | Closs-A Amp. | 45 | 0 | 0.2 | $200 \mu \mathrm{x}$ | $60 \mu x$ | 500000 | 65 | 32.5 | - |  | CK510 |
| CK512 | Low Microphonic Pentode | 1 | 2 | 0.625 | 0.02 |  |  |  | Voltage Amp. Class-A Amp. | 22.5 | 0 | 22.5 | 0.04 | 0.125 | - | 160 |  | - |  | CK412 |
| CK5158X | Triode Voltage Amplifier | - | : | 0.625 | 0.03 |  |  |  |  | 45 | 0 |  |  | 0.15 |  | 160 | 24 | 1000000 |  | CK5158X |
| CK520AX | Audio Pentode | 1 | : | 0.625 | 0.05 |  |  |  | Class-A A Amp. | 45 | -2.5 | 45 | 0.07 | 0.24 | - | 180 |  | - | 0.0045 | CK532AX |
| CK521AX | Audio Pentode | 1 | - | 1.25 | 0.05 |  |  |  | $\begin{array}{\|l\|} \hline \text { Closs-A Amp. } \\ \hline \text { Closs-A Amp. } \end{array}$ | 22.5 | -3 | 22.5 | 0.22 | 0.8 | $\underline{-}$ | 400 |  | - | 0.006 | CK521AX |
| CK522AX | Audio Pentode | 1 | : | 1.25 | 0.02 |  |  |  |  | 22.5 | 0 | 22.5 | 0.08 | 0.3 |  | 450 |  |  | 0.0012 | CK522AX |
| CK523AX | Pentode Output Amp. | $\stackrel{1}{1}$ | - | 1.25 | 0.03 |  |  |  | $\begin{array}{\|l\|} \hline \text { Class-A, Amp. } \\ \hline \text { Class-A Amp. } \\ \hline \end{array}$ | 22.5 | -1.2 | 22.5 | 0.075 | 0.3 |  | 360 |  |  | 0.0025 | CK523AX |
| CKS24AX | Pentode Output Amp. | 1 | - | 1.25 | 0.03 |  |  |  | Class-A Amp. | 15 | -1.75 | 15 | 0.125 | 0.45 |  | 300 |  | - | 0.0022 | CK514AX |
| CK525AX | Pantode Output Amp. | ${ }^{1}$ |  | 1.25 | 0.2 | - |  |  |  | 22.5 | -1.2 | 22.5 | 0.06 | 0.25 | - | 325 |  | - | 0.0022 | CKS23AX |
| CK526AX | Pentode Output Amp. | 1 |  | 1.25 | 0.2 |  |  | - | Class-A Amp. | 22.5 | -1.5 | 22.5 | 0.12 | 0.45 | - | 400 |  |  | 0.004 | CK526AX |
| CK527AX | Pentode Output Amp. | 1 |  | 1.25 | 0.015 |  |  |  | Class-A Amp. | 22.5 | 0 | 22.5 | 0.025 | 0.1 |  | 75 |  |  | 0.0007 | CK527AX |
| CK529AX | Shielded Output Pentode | 1 | - | 1.25 | 0.02 |  |  | - | Class-A Amp. Detector-Amp. | 15 | -1.5 | 15 | 0.05 | 0.2 | - | 275 |  |  | 0.0012 | CK529AX |
| CKS5IAXA | Diode Pentode | 1 | 2 | 1.25 | 0.03 |  |  |  |  | 22.5 | 0 | 22.5 | 0.04 | 0.17 | - | 235 |  |  |  | CKS5IAXA |
| CK533AXA | R.F. Pentode | 1 | \% | 1.25 | 0.05 |  |  |  | Detector-Amp. Class-A Amp. | 22.5 | 0 | 22.5 | 0.13 | 0.42 | - | 550 |  |  | - | CKS53AXA |
| CK556AX | U.h.f. Triode | 1 | 2 | 1.25 | 0.125 |  |  |  | R.F. Oscillator | 135 | -5 |  |  | 4.0 | $\square$ | 1600 |  |  |  | CK536AX |
| CK568AX | U.h.f. Triode | 1 | 2 | 1.25 | 0.07 |  |  | - | R.F. Oscillator | 135 | -6 | - |  | 1.9 |  | 650 |  |  |  | CK568AX |
| CK569AX | R.f. Pentode | 1 | 2 | 1.25 | 0.05 |  |  |  | Class-A, Amp. | 67.5 | 0 | 67.5 | 0.48 | 1.8 |  | 1100 |  |  |  | CK569aX |
| CK605CX | Sharp Cuf-off Pentode | 1 | $\cdots$ | 6.3 | 0.2 |  |  | - | Class-A Amp. | 120 | -2 | 120 | 2.5 | 7.5 | - | 5000 |  |  |  | CK60sCX |
| CK606BX | Single Diode | 1 | $?$ | 6.3 | 0.15 |  |  |  |  | 150 a.c. |  | - |  | 9.0 de. | - |  |  |  |  | CK606BX |
| CK608CX | U.h.f. Triode | 1 | $:$ | 6.3 | 0.2 |  |  | - | $\begin{array}{\|l\|} \hline \text { Detector } \\ \hline 500-\mathrm{Mc} . \text { Osc. } \\ \hline \end{array}$ | 120 | -2 |  |  | 9.0 | $\square$ | 5000 |  |  | 0.75 | CK608CX |
| CK619CX | Hi-Mu Triode | ' | : | 6.3 | 0.2 |  |  |  | Class-A, Amp. | 250 | -2 |  |  | 4.0 |  | 4000 |  |  |  | CK619CX |
| CK624CX | Sharp Cut-off Pentode | 1 | - | 6.3 | 0.2 |  |  |  | Class-A Amp. <br> Class-A Amp. | 120 | -2 | 120 | 3.5 | 5.2 |  | 3000 |  |  |  | CK624CX |
| CK650AX | Sharp Cut-off Pentode | 1 | 2 | 6.3 | 0.2 |  |  |  |  | 120 | -2 | 120 | 2.5 | 7.5 |  | 5000 |  |  |  | CK650AX |
| CK5672 | Pentode Output Amp. | 1 | - | 1.25 | 0.05 |  |  |  | $\begin{aligned} & \text { Class-A Amp. } \\ & \text { Class-A Amp. } \end{aligned}$ | 67.5 | -6.25 | 67.5 | 1.0 | 2.75 | 二 | 625 |  |  | 0.06 | CK5672 |
| $\begin{aligned} & \text { HY113 } \\ & \text { HY123 } \end{aligned}$ | Triode Amplifier | -1 | 5K | 1.4 | 0.07 | - | - | - | Class-A Amp. | 45 | -4.5 | - |  | 0.4 | 25000 | 250 | 6.3 | 40000 | 0.0065 | $\begin{aligned} & \text { HY113 } \\ & \text { HY123 } \\ & \hline \end{aligned}$ |
| HY115 HY145 <br> HY 125 | Pentode Voltage Amplifier | -1 | 5K | 1.4 | 0.07 | - | - |  | Class-A Amp. | $\begin{aligned} & 45 \\ & 90 \\ & \hline \end{aligned}$ | $\begin{array}{r} -1.5 \\ -1.5 \\ \hline \end{array}$ | $\begin{array}{r} 22.5 \\ \hline 45 \\ \hline \end{array}$ | $\begin{aligned} & 0.008 \\ & 0.1 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.48 \end{aligned}$ | $\begin{aligned} & 5200000 \\ & 1300000 \end{aligned}$ | $\begin{array}{r} 58 \\ 270 \\ \hline \end{array}$ | $\begin{aligned} & 300 \\ & 370 \\ & \hline \end{aligned}$ | - |  | $\begin{aligned} & \text { HY115 } \\ & \text { HY145 } \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { HY125 } \\ & \text { HYI5 } \end{aligned}$ | Pentode Power Amplifier | $\square$ | 5K | 1.4 | 0.07 |  |  |  | Class-A Amp. | $\begin{aligned} & 45 \\ & 90 \end{aligned}$ | $\begin{array}{r} -3.0 \\ -7.5 \\ \hline \end{array}$ | $\begin{array}{r} 45 \\ 90 \\ \hline \end{array}$ | $\begin{aligned} & 0.2 \\ & 0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.9 \\ & 2.6 \end{aligned}$ | $\begin{array}{\|} 823000 \\ 420000 \\ \hline \end{array}$ | $\begin{array}{r} 310 \\ 450 \\ \hline \end{array}$ | $\begin{aligned} & 255 \\ & 190 \\ & \hline \end{aligned}$ | $\begin{array}{r} 50000 \\ 28000 \\ \hline \end{array}$ | $\begin{aligned} & 0.0115 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { HY125 } \\ & \text { HY1S5 } \\ & \hline \end{aligned}$ |
| M 4.4 | $\frac{\text { Tetrode Power Amplifier }}{\text { Tehinde Voltage Amplifier }}$ | ${ }^{1}$ | : | 0.625 | 0.04 |  |  |  | Class-A Amp. | 30 | 0 | 30 | 0.06 | 0.5 | 130000 | 200 | 26 | 35000 | 0.005 | M54 |
| M74 | Tatrode Voltage Amplifier | 1 | 2 | 0.625 | 0.02 |  |  |  | Class-A Amp. | 30 | 0 | - |  | 0.03 | 200000 | 110 | 25 |  |  | M64 |
| RK61 | Gas Triode | 1 | 2 | 1.4 | 0.02 |  |  |  | Class-A Amp. Radio Cantrol | 30 | 0 | 7.0 | 0.01 | 0.02 | 500000 | 125 | 70 |  |  | M74 |
| 50917 A |  |  |  |  | 0.05 |  |  |  |  | 45 |  |  | - | 1.5 | - | - |  | - |  | RK61 |
| 5637 | Triode | 1 | : | 6.3 | 0.15 | 2.6 | 0.7 | 1.4 | Radio Control Class-A1 Amp. | 100 | $820 *$ | - | $\square$ | 1.4 | 26000 | 2700 | 70 | - | - | $\begin{aligned} & \text { SD917A } \\ & 5637 \end{aligned}$ |

TABLE XII - SUB-MINIATURE TUBES - Continued

| Type | Name | Base | Socket Connecfions | Fil. or Hoaler |  | Capacitance $\mu \mu \mathrm{fd}$. |  |  | Use | Plate Supply Volts | Grid Bias | $\begin{gathered} \text { Screen } \\ \text { Volis } \end{gathered}$ | Screen Current Ma. | Plate Current Ma. | Plate <br> Resistance <br> Ohms | Transconductance Mieromhos | Amp. Factor | Load <br> Resistanee <br> Ohms | $\text { ce } \begin{gathered} \text { Power } \\ \text { Oulput } \\ \text { Watts } \end{gathered}$ | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volts | Amp. | In | Oui | $\begin{array}{\|l\|} \hline \text { Platoo- } \\ \text { Grid } \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { SD828A } \\ & 5638 \\ & \hline \end{aligned}$ | Audio Pentode | 1 | 2 | 6.3 | 0.15 | 4.0 | 3.0 | 0.22 | Class-A1 Amp. | 100 | 270* | 100 | 1.25 | 4.8 | 150000 | 3300 | $\square$ | - | - | $\begin{aligned} & \text { SD828A } \\ & 5630 \end{aligned}$ |
| $\begin{aligned} & \text { SD828E } \\ & 5634 \\ & \hline \end{aligned}$ | Sharp Cut-off Pentode | , | - | 6.3 | 0.15 | 4.4 | 2.8 | 0.01 | Class-A1 Amp. | 100 | 150* | 100 | 2.5 | 6.5 | 240000 | 3500 |  | - | - | $\begin{aligned} & \text { SD828E } \\ & 5634 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \hline 5 N 944 \\ & 5633 \\ & \hline \end{aligned}$ | Remote Cut-off Pentode | + | - | 6.3 | 0.15 | 4.0 | 2.8 | 0.01 | Class-A1 Amp. | 100 | 150* | 100 | 2.8 | 7.0 | 200000 | 3400 |  | - | - | $\begin{aligned} & \mathrm{SNO44} \\ & 5633 \end{aligned}$ |
| SN946 | Diode | 1 | : | 6.3 | 0.15 | 1.8 |  | - | Rectifier | 150 |  | - |  | 9.0 | - | - |  | - |  | SN946 |
| $\begin{aligned} & \text { SN947D } \\ & 5640 \\ & \hline \end{aligned}$ | Audia Beam Pentode | 1 | 2 | 6.3 | 0.45 | - | - | - | Class-A1 Amp. | 100 | -9 | 100 | 2.2 | 31.0 | 15000 | 5000 | - | 3000 | 1.25 | $\begin{aligned} & \text { SN947C } \\ & \mathbf{5 6 4 0} \end{aligned}$ |
| SN948C | Voltage Regulator | 1 | - | - |  | $\square$ | - | 2 | Regulator |  |  |  | Perating | oltage $=9$ | 5; Max. cur | rent $=25 \mathrm{Ma}$ |  |  |  | SN948C |
| SN953D | Power Pentode | 1 |  | 6.3 | 0.15 | 9.5 | 3.8 | 0.2 | Clast-A Amp. | 150 | 100* | 100 | 4/7.5 | 21/20 | 50000 | 9000 |  | 9000 | 1.0 | SN933D |
| $\begin{aligned} & \text { SN954 } \\ & 5641 \\ & \hline \end{aligned}$ | Half-Wave Rectifier | 1 | 2 | 6.3 | 0.45 | - |  | - | Rectifier | 300 | - | - | - | 45.0 | - | - |  | - | - | $\begin{aligned} & \hline 5 N 954 \\ & \hline 5641 \\ & \hline \end{aligned}$ |
| SN9558 | Dual Triode | 1 | 2 | 6.3 | 0.45 | 2.8 | 1.0 | 1.3 | Class-A, Amp. ${ }^{\text {a }}$ | 100 | 100* | - | - | 5.5 | 8000 | 4250 | 34 |  |  | SN9538 |
| $\begin{aligned} & \text { SN956B } \\ & 5642 \\ & \hline \end{aligned}$ | H.V. Halt-Wave Rectifier | - | - | 1.25 | 0.14 |  |  | -- | H.V. Rectifier |  | Poak | k inverse | V. $=100$ | Max. A | Average lp = | 2 Ma. Peak | $\mathrm{Ip}=23 \mathrm{~A}$ |  |  | $\begin{aligned} & \hline \text { SN956B } \\ & 5642 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { SN957A } \\ & 5645 \\ & \hline \end{aligned}$ | Triode | ${ }^{2}$ | 2 | 6.3 | 0.15 | 2.0 | 1.0 | 1.8 | Class-A, Amp. | 100 | 560* | - | - | 5.0 | 7400 | 2700 | 20 | - | - | $\begin{aligned} & \hline \text { SN957A } \\ & 5645 \\ & \hline \end{aligned}$ |
| SN1006 | Triode | 1 | 2 | 6.3 | 0.15 |  |  |  | Class-A1 Amp. | 100 | $820^{*}$ |  | I | 1.4 | 29000 | 2400 | 70 | - | - | SN1006 |
| SN10078 | Mixer | , |  | 6.3 | 0.15 | 5.0 | 2.8 | 0.003 | Mixer | 100 | 150* | 100 | 5.0 | 4.0 | 230000 | 900 |  | - |  | SN1007B |


| TYpe | Name | Base | Sockel Connec. fions | Cathode | Fil. or Heater |  | Use | Peak Anede Volfage | Max. <br> Anade Ma. | Minimum Supply Voltage | Operating Voltage | Operating Ma. | $\begin{gathered} \text { Grid } \\ \text { Resisfor } \end{gathered}$ | Tube Voltage Drop | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Volts | Amp. |  |  |  |  |  |  |  |  |  |
| OA2 | Voltage Regulator | 7 -pin 8. | 580 | Cold |  |  | Voitage Regulator | - | - | 185 | 150 | 5-30 | - | - | OA2 |
| OAS | Gas Pentode | 7-pin B. | Fig. 33 | Cold | - |  | Relay or Trigger | Plate-750 V., Screen-90 V., Grid-3 V., Pulse-85 V. |  |  |  |  |  |  | OA5 |
| OB2 | Voltoge Regulator | 7 -pin 8 . | 580 | Cold | - |  | Voltage Regulator | - | - | 133 | 108 | 5-30 |  | - | OB2 |
| $\begin{aligned} & \text { OA4G } \\ & 1267 \end{aligned}$ | Gas Triode Starter-Anode Type | 6-pin 0. | $\begin{aligned} & 4 V \\ & 4 V \end{aligned}$ | Cold | - | - | Cold-Cathode Startor-Anoda Rolay Tube | With 105-120-volt a.c. anode supply, peak slarter-anode a.c. voltage is 70 , peak r.f. voltage 55. Peak d.e. $m a=100$. Average d.c. $m a=25$. |  |  |  |  |  |  | $\begin{array}{\|l\|} \hline \text { OA4G } \\ 1267 \\ \hline \end{array}$ |
| 1847 | Voltage Regulator | 7 -pin B. |  | - | - | - | Voltage Regulator | - | - | 225 | 82 | 1-2 |  | - | 1847 |
| $1 \mathrm{C21}$ | Gas Triode <br> Glow-Discharge Type | 6-pin 0. | 4V | Cold | - | - | Relay Tube | 125-145 | 25 | 660 | - |  |  | 73 | 1C21 |
| 2A4G | Gas Triode Grid Type | 7 -pin 0. | 55 | Fil. | 2.5 | 2.5 | Control Tube | 200 | 100 | - | - |  |  | 15 | 2A4G |
| 6056 | Gas Triode Grid Type | 8 -pin 0. | 60 | Hir. | 6.3 | 0.6 | Sweep Circuit Oscillator | 300 | 300 | - | - | 1.0 | 0.1-10: | 19 | 605 G |
| 284 |  | 5 -pin M. | 5A | Hir. | 2.5 | 1.4 |  |  |  |  |  |  |  |  | 284 |
| 2 C 4 | Gas Triode | 7 -pin B. | 5AS | Fil. | 2.5 | 0.65 | Control Tube | Plate volts $=350$; Grid valts $=-50 ;$ Avg. Ma, $=5 ;$ Peak Ma. $=20 ;$ Voltage drop $=16$. |  |  |  |  |  |  | $2 \mathrm{C4}$ |
| 2021 | Gas Tetrode | 7 -pin B. | 7BN | Hir. | 6.3 | 0.6 | Grid-Controlled Rectifier | 650 | 500 | - | 650 | 100 | 0.1-10 ${ }^{7}$ | 8 | 2D21 |
| 2021 |  |  |  |  |  |  | Relay Tube | 400 |  | - | - | - | 1.0 \% |  |  |
| 3 C 23 | Gas and Mercury Vapor Grid Type | 4-pin M. | 3G | Fil. | 2.5 | 7.0 | Grid-Controlled Rectifier | 1000 | 6000 |  | 500 | 1500 | -4.5.5 ${ }^{\text {\% }}$ | 15 | $3 \mathrm{C23}$ |
| 604 | Gos Triode | 7-pin B. | 5AY | Hitr. | 6.3 | 0.25 | Control Tube | Plate volts =350; Grid volts $=-50 ;$ Avg. Ma. $=25$; Peak Ma. $=100$; Vollage drop $=16$. |  |  |  |  |  |  | 6D4 |
| 17 | Mercury Vapor Triode | 4-pin M. | 3G | Fil. | 2.5 | 5.0 | Grid-Controlled Rectifior | $\frac{7500^{j}}{2500}$ | 2000 | $\overline{-53}$ | $\overline{1000}$ | 500 |  | 10-24 | 17 |
| 874 | Voltage Regulator | 4-pin M. | 45 |  |  |  | Voitage Regulator | - | - | 125 | 90 | 10-50 | - |  | 874 |
| 876 | Current Regulator | Mogul |  |  |  |  | Current Regulator | - | - |  | 40-60 | 1.7 | - |  | 876 |
| 884 | Gas Triode Grid Type | 6-pin 0. | 60 | His. | 6.3 | 0.6 | Swaep Circuit Oscillator | 300 | 300 |  | $\cdots$ | 2 | 25000 |  | 884 |
| 884 |  |  |  |  |  |  | Grid-Controlled Rectifier | 350 | 300 |  | - | 75 | 25000 |  |  |
| 885 | Gas Triode Grid Type | 5-pin S. | 5A | Hir. | 2.5 | 1.4 | Same as Type 884 | Characteristics same as Type 884 |  |  |  |  |  |  | 885 |

table xili－control and regulator tubes

| Type | Name | Base | Socket Connec－ tions | Cathode | Fil．or Heator |  | Use | Peak Anode Voltage | Max． <br> Anode Mo． | Minimum Supply Voltage | Operating Voltage | Operating Ma． | $\underset{\text { Resistor }}{\text { Grid }}$ | Tube Voltage Drop | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Volts | Amp． |  |  |  |  |  |  |  |  |  |
| 886 | Current Requlator | Mogul | － |  | 二 | $\square$ | Current Regulator | － |  | － | 40－60 | 2.05 | － | － | 886 |
| 967 | Mercury Vapor Triode | 4－pin M． | 3G | Fil． | 2.5 | 5.0 | Grid－Controlled Rectifior | 2500 | 500 | －5 ${ }^{\text {d }}$ |  |  |  | 10－24 | 967 |
| 991 | Voltage Regulator | Bayonet |  |  |  |  | Voltage Regulator | － | － | 87 | 55－60 | 2.0 | － |  | 991 |
| 1265 | Voltage Requlator | 6 －pin 0. | 4AJ | Cold | － | － | Vollaqe Requlator | － | － | 130 | 90 | 5－30 | － | － | 1265 |
| 1266 | Voltage Regulator | 6－pin 0. | 4AJ | Cold | － | － | Vollage Regulator | － | － | － | 70 | 5－40 | － | － | 1266 |
| 1267 | Gas Triode | 6 －pin 0. | 4 V | Cold | － | － | Relay Tube |  |  | Characte | ristics same | as OA4G |  |  | 1267 |
| 2050 | Gas Tetrode | 8 －pin 0. | 8BA | Hir． | 6.3 | 0.6 | Grid－Controllad Rectifier | 650 | 500 | － | $\cdots$ | 100 | 0．1－10 ${ }^{\text {P }}$ | 8 | 2050 |
| 2051 | Gas Tetrode | 8 －pin 0 | 8BA | Hit． | 6.3 | 0.6 | Crid－Controlled Rectifior | 350 | 375 | － | － | 75 | $0.1-10^{7}$ | 14 | 2051 |
| $\begin{aligned} & \text { 2523NT// } \\ & \text { 128AS } \end{aligned}$ | Gas Triode Grid Type | 5－pin M． | 5A | Hir． | 2.5 | 1.75 | Relay Tube | 400 | 300 | － | － | 1.0 | $300{ }^{7}$ | 13 | $\begin{aligned} & 2523 N 1 / \\ & 128 A 5 \end{aligned}$ |
| 5651 | Voltage Regulator | 7－pin B． | 5BO | Cold |  | － | Voltage Regulator | 115 | － | 115 | 87 | 1．5－3．5 | － | － | 5651 |
| KY2．1 | Gas Triode Grid Type | 4－pin M． | － | Fil． | 2.5 | 10.0 | Grid－Controlled Rectifer | － | － | －－ | 3000 | 500 | － | － | KY21 |
| RK61 | Thyratron |  | － | Fil． | 1.4 | 0.05 | Radio－Controlled Relay | 45 | 1.5 | 30 | － | 0．5－1．5 | 37 | 30 | RK61 |
| RK62 | Gas Triode Grid Type | 4 －pin S． | 4D | Fil． | 1.4 | 0.05 | Relay Yube | 45 | 1.5 | － | 30－45 | 0．1－1．5 | － | 15 | RK62 |
| RM208 | Permatron | 4－pin M． |  | Fil． | 2.5 | 5.0 | Controlled Rectifier ${ }^{\text {1 }}$ | $7500^{2}$ | 1000 | － | － | － | － | 15 | RM208 |
| RM209 | Permatron | 4－pin M． | $\bar{\square}$ | Fil． | 5.0 | 10.0 | Controlled Rectifier ${ }^{1}$ | 7500： | 5000 |  |  | － | － | 15 | RM209 |
| OA3／VR75 | Voltage Regulator | 6－pin 0. | 4AJ | Cold |  | － | Voliage Regulator | － | Som | 105 | 75 | 5－40 | － | $\underline{ }$ | OA3／VR75 |
| 083／VR90 | Voltage Regulator | 6 －pin 0. | 4AJ | Cold |  | － | Voltage Regulator | 二 | － | 125 | 90 | 5－40 | － | － | OB3／VR90 |
| OC3／VR105 | Votage Regulator | 6 －pin 0. | 4AJ | Cold | 二 | － | Voltage Regulatior | － | $\square$ | 135 | 105 | 5－40 | － | － | OC3／VR105 |
| OD3／VR150 | Volloge Regulator | 6 －pin 0. | 4AJ | Cold | 二 |  | Voltage Regulator | － |  | 185 | 150 | 5－40 | － | － | OD3／VR150 |
| KY866 | Mercury Vapor Triodr | 4－pin M． | Fig． 8 | Fil． | 2.5 | 5.0 | Grid－Controlled Rectifor | 10000 | 1000 | 0－150 | － | － | － | － | KY866 |
| ${ }^{1}$ For use as grid－controlled rectifier or with external magnetic control．RM－208 has characteristics of 866，RM－209 of 872. |  |  |  |  | ${ }^{2}$ When under control peak inverse rating is reduced to 2500. <br> d At 1000 anode volts． |  |  |  |  | Grid tied to plate． Peak inverse vollage． |  | ${ }^{6}$ Grid． <br> 7 Megohms． | ${ }^{8}$ Grid <br> ${ }^{9}$ No <br> Cour | oltage． <br> se．Tinne <br> sy ARR | wire leads． <br> Handbook |

## RECEIVING TUBE SUBSTITUTION GUIDE

TABLE XV—RECTIFIERS-RECEIVING AND TRANSMITTING
See also Table XIII-Control and Regulatur Tubes

| Type No. | Name | Base | Socket Connec tions | Cathodo | Fil. or Heater |  | Max. <br> A.C. <br> Voltage <br> Per Plate | D.C. Current Ma. | Max. Peak Voltage |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Volts | Amp. |  |  |  |  |  |
| BA | Full-Wave Rectifer | 4-pin M. | 4J | Cold |  | - | 350 | 350 | Tube drop | P 80 v . | G |
| BH | Full-Wave Rectitier | 4-pin M. | 4J | Cold |  | - | 350 | 125 | Tube dr | P90 v . | G |
| BR | Holf-Wave Rectifier | 4-pin M. | 4H | Cold |  |  | 300. | 50 | Tube dr | p 60 v . | $G$ |
| CE-220 | Holf-Wave Reclifier | 4-pin M. | 4P | Fil. | 25 | 3.0 |  | 20 | 20000 | 100 | HV |
| OY4 | Half-Wave Rectifer | 5 -pin 0. | 4BU | Cold | $\begin{aligned} & \text { Connect Pins } \\ & 7 \text { and } 8 \end{aligned}$ |  | 95 | 75 | 300 | 500 | G |
| OZ4 | Full-Wave Rectifier | 5-pin 0. | 4R | Cold |  |  | 350 | 30-75 | 1250 | 200 | G |
| 1 | Half-Wave Rectifier | 4-pin S. | 4 G | Hit. | 6.3 | 0.3 | 350 | 50 | 1000 | 400 | MV |
| 1.v | Half-Wave Rectifer | 4-pin S. | 4G | Ht. | 6.3 | 0.3 | 350 | 50 | $\cdots$ |  | HV |
| 183GT/8016 | Half-Wove Rectifier | 6-pin 0. | 3C | Fil. | 1.25 | 0.2 | $\underline{-}$ | 2.0 | 4000 | 17 | HV |
| 1848 | Half-Wave Rectifier | 7-pin B. |  | Cold |  |  | 800 | 6 | 2700 | 50 | G |
| $1 \times 2$ | Half-Wave Rectifier | 9-pin B. | Fig. 29 | Fil. | 1.25 | 0.2 |  | 1 | 15000 | 10 | HV |
| 122 | Half-Wave Rectifior | 7-pin B. | 7CB | Fil. | 1.5 | 0.3 | 7800 | 2 | 20000 | 10 | HV |
| 2825 | Half-Wave Rectifier | 7-pin B. | 3 T | Fil. | 1.4 | 0.11 | 1000 | 1.5 | - | 9 | HV |
| 2V3G | Half-Wave Rectifor | 6-pin 0. | $4 Y$ | Fil. | 2.5 | 5.0 |  | 2.0 | 16500 | 12 | HV |
| 2W3 | Half-Wave Rectifler | 5-pin 0. | 4X | Fil. | 2.5 | 1.5 | 350 | 55 | - | - | HV |
| $2 \times 2 / 87910$ | Half-Wave Rectifior | 4-pin 5. | 4AB | Hir. | 2.5 | 1.75 | 4500 | 7.5 |  |  | HV |
| 2×2-A | Half-Wave Rectifier | 4-pin S. | 4AB | Same as $2 \times 2 / 879$ but will withstand severe shock \& vibration |  |  |  |  |  |  | HV |
| $2 Y^{2}$ | Half-Wave Rectifier | 4-pin M. | 4AB | Fil. | 2.5 | 1.75 | 4400 | 5.0 | , | - | HV |
| 222/G84 | Half-Wave Rectifor | 4-pin M. | 4 B | Fil. | 2.5 | 1.5 | 350 | 50 | - |  | HV |
| 3824 | Ha,f-Wave Rectifler | 4-pin M. | T-4A | Fil. | $\begin{aligned} & 5.0 \\ & 2.5, \end{aligned}$ | $\begin{aligned} & 3.0 \\ & 3.0 \end{aligned}$ |  | $\begin{aligned} & 60 \\ & 30 \end{aligned}$ | $\begin{aligned} & 20000 \\ & 20000 \end{aligned}$ | $\begin{aligned} & 300 \\ & 150 \\ & \hline \end{aligned}$ | HV |
| 3825 | Half-Wave Rectifier | 4-pin M. | 4 P | Fil. | 2.5 | 5.0 | - | 500 | 4500 | 2000 | G |
| 3 B 26 | Half-Wave Rectifer | 8 -pin 0. | Fig. 31 | Hir. | 2.5 | 4.75 |  | 20 | 15000 | 8000 | HV |
| DR-3827 | Half-Wave Rectifer | 4-pin M. | 48 | Fil. | 2.5 | 5.0 | 3000 | 250 | 8500 | 1000 | HV |
| 5AZ4 | Full-Wave Rectifier | 5-pin 0. | $5 T$ | Fil. | 5.0 | 2.0 | Same as Type 80 |  |  |  | HV |
| 5R4GY | Full-Wove Rectifior | 5-pin 0. | $5 T$ | Fil. | 5.0 | 2.0 | $\begin{aligned} & 900^{7} \\ & 950^{7} \end{aligned}$ | $\begin{aligned} & 1504 \\ & 1757 \end{aligned}$ | 2800 | 650 | HV |
| 5 T 4 | Full-Wave Rectifer | 5 -pln 0. | 51 | Fil. | 5.0 | 3.0 | 450 | 250 | 1250 | 800 | HV |
| 5U4G | Full-Wave Rectifier | 8 -pin 0. | $5 \bar{T}$ | Fil. | 5.0 | 3.0 | Same as Type 5z3 |  |  |  | HV |
| 5V4G | Full-Wave Rectifier | 8 -pin 0. | 51 | Htr . | 5.0 | 2.0 | Same as Type 83 V |  |  |  | HV |
| 5W4 | Full-Wave Rectiffer | 5 -pin 0. | 57 | Fil. | 5.0 | 1.5 | 350 | 110 | 1000 | - | HV |
| $5 \times 3$ | Full-Wave Rectifier | 4-pin M. | 4 C | Fil. | 5.0 | 2.0 | 1275 | 30 | - | - | HV |
| 5 $\times 4 \mathrm{G}$ | Full-Wave Rectifior | 8 -pin 0. | 50 | FH. | 5.0 | 3.0 | Same as 523 |  |  |  | HV |
| 5 Y3G | Full-Wave Rectifor | 5-pin 0. | 51 | Fil. | 5.0 | 2.0 | Same as Type 80 |  |  |  | HV |
| 5Y4G | Full-Wave Rectifier | 8 -pin 0 | 50 | Fil. | 5.0 | 2.0 | Same as Type 80 |  |  |  | HV |
| 523 | Full-Wave Rectifior | 4-pin M. | 4 C | Fii. | 5.0 | 3.0 | 500 | 250 | +1400 |  | HV |
| 524 | Full-Wave Rectifor | 5-pin 0. | 51 | Hir. | 5.0 | 2.0 | 400 | 125 | 1100 | - | HV |
| 6W4GT | Damper Service | 6 -pin 0. | 4CG | Hrr. | 6.3 | 1.2 |  | 125 | 2000 | 600 | HV |
|  | Half-Wave Rectifier |  |  |  |  |  | 350 | 125 | 1250 | 600 |  |
| 6W5G | Full-Wave Rectifior | 6-pin 0. | 65 | Hir. | 6.3 | 0.9 | 350 | 100 | 1250 | 350 | HV |
| $6 \times 4$ | Full-Wavo Rectifier | 7-pin B . | 7CF | Htr. | 6.3 | 0.6 | 325 | 70 | 1250 | 210 | HV |
| $6 \times 5$ | Full-Wave Rectifor | 6-pin 0. | 65 | Htr. | 6.3 | 0.5 | 350 | 75 | $\underline{\square}$ | - | HV |
| 6Y3G | Half-Wave Rectifier | 5-pin O. | 4AC | Htr. | 6.3 | 0.7 | 5000 | 7.5 | - |  | HV |
| 6 Y 519 | Full-Wave Rectifer | 6-pin 5 . | $6 J$ | Hit. | 6.3 | 0.8 | 350 | 50 |  | - | HV |
| 623 | Half-Wava Roctifior | 4-pin M. | 4 G | Fil. | 6.3 | 0.3 | 350 | 50 | - |  | HV |
| 62510 | Full-Wave Rectifior | 6 -pin 5 . | 6K | Hir. | 6.3 | 0.6 | 230 | 60 | - | - | HV |
| 6ZY5G | Full-Wave Rectifior | 6-pin 0. | 6S | Htr. | 6.3 | 0.3 | 350 | 35 | 1000 | 150 | HV |
| $7 Y 4$ | Full-Wave Rectifier | $8-\mathrm{pin} \mathrm{L}$. | 5AB | Hr. | 6.3 | 0.5 | 350 | 60 |  |  | HV |
| 724 | Full-Wave Rectiflor | 8-pin L. | 5AB | Htr. | 6.3 | 0.9 | $\begin{aligned} & 4501 \\ & 325 \end{aligned}$ | 100 | 1250 | 300 | HV |
| 1247 | Rectifier-Pantode | 7 -pin S . | 7K | Htr. | 12.6 | 0.3 | 125 | 30 | - | - | HV |
| 1223 | Half-Wove Rectifier | 4-pin S. | 46 | Htr. | 12.6 | 0.3 | 250 | 60 |  | - | HV |
| $12 \mathrm{Z5}$ | Voltage Doubler | 7 -pin M. | 71 | Mri. | 12.6 | 0.3 | 225 | 60 |  | - | HV |
| 14 Y 4 | Full-Wave Reclifier | 8 -pin L. | 5AB | Htr. | 12.6 | 0.3 | $\begin{array}{r} 4501 \\ 3254 \\ \hline \end{array}$ | 70 | 1250 | 210 | HV |
| 1423 | Hall-Wave Rectifer | 4 -pin S. | 4G | Htr. | 12.6 | 0.3 | 250 | 60 | - | - | HV |
| 25A7G 10 | Rectifior-Pentode | $8-\mathrm{pin} 0$. | 8 F | Htr. | 25 | 0.3 | 125 | 75 | - |  | HV |
| 25 W 4 | Half-Wave Rectifier | 6-pin 0. | 4CG | Htr. | 25 | 0.3 | 350 | 125 | 1250 | 600 | HV |
| 25X6GT | Voltage Doubler | 7-pin 0. | 70 | Htr. | 25 | 0.15 | 125 | 60 | - | - | HV |
| 25Y4GT | Half-Wave Rectifer | 6-pin 0. | 5AA | Htr. | 25 | 0.15 | 125 | 75 | - | - | HV |
| $25 \times 5{ }^{\text {IU }}$ | Voltage Doubler | 6 -pin S. | 6E | Htr. | 25 | 0.3 | 250 | 85 | - | - - | HV |
| 2573 | Half-Wave Rectifer | 4-pin S. | 4G | Hr. | 25 | 0.3 | 250 | 50 | - | - | HV |
| 2574 | Half-Wave Rectifer | 6-pin 0. | 5AA | Hir. | 25 | 0.3 | 125 | 125 | - |  | HV |
| 2575 | Rectifior-Doubler | 6 -pin 5 . | 6 E | H\%. | 25 | 0.3 | 125 | 100 | - | 500 | HV |
| 2576 | Rectifior-Doubler | 7-pin 0. | 70 | Hfr. | 25 | 0.3 | 125 | 100 | - | 500 | HV |
| 2825 | Full-Wave Rectifler | 8 -pin L . | 5AB | Hr. | 28 | 0.24 | $\begin{aligned} & 4507 \\ & 325 \end{aligned}$ | 100 | - | 300 | HV |
| 3217G7 | Rectifier-Tefrade | 8 -pin 0. | 8 Z | Hitr. | 32.5 | 0.3 | 125 | 60 |  | $\underline{\square}$ | HV |
| $35 \mathrm{W4}$ | Half-Wave Rectifler | 7 -pin B. | 5BQ | Htr. | 352 | 0.15 | 125 | 100\% | 330 | 600 | HV |
| 35 Y 4 | Half-Wave Rectifior | 8 -pin 0. | 5AL | Htr. | 352 | 0.15 | 235 | $\begin{gathered} 60 \\ 100: \\ \hline \end{gathered}$ | 700 | 600 | HV |
| 3573 | Half-Wave Rectifier | 8 -pin L. | 4Z | Hit. | 35 | 0.15 | 250 | 100 | 700 | 600 | HV |
| 3574GT | Half-Wave Rectifier | 6-pin 0. | SAA | Hitr | 35 | 0.15 | 250 | 100 | 700 | 600 | HV |
| 35756 | Half-Wave Rectifior | 6 -pin 0. | 6AD | Ht. | 35 : | 0.15 | 125 | $\begin{gathered} 60 \\ 100^{8} \\ \hline \end{gathered}$ | - | - | HV |

RECEIVING TUBE SUBSTITUTION GUIDE
TABLE XV-RECTIFIERS-RECEIVING AND TRANSMITTING - Continued
See also Table XIII-Control and Regulator Tubes

| Type No. | Name | Ease | Socket Connections | Cathods | Fil. or Heater |  | Max. A.C. Volioge Per Plate | D.C. Outpul Current Ma. | Mox. Inverse Peak Voltage | Peak Plate Current Ma. | Typo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Volts | Amp. |  |  |  |  |  |
| 3526 G | Voltage Doubler | 6-pin 0. | 70 | Hir. | 35 | 0.3 | 125 | 110 |  | 500 | HV |
| 4025GT | Half-Wave Rectifier | 6-pin 0. | 6AD | Htr. | 40: | 0.15 | 125 | $\begin{gathered} 60 \\ 100 \\ \hline \end{gathered}$ | - | - | HV |
| 4523 | Halt-Wave Rectifer | 7-pin B. | SAM | Htr. | 45 | 0.075 | 117 | 65 | 350 | 390 | HV |
| 4525GT | Holl-Wove Rectifier | 6-pin 0. | 6AD | Htr. | 45: | 0.15 | 125 | $\begin{gathered} 60 \\ 100 \end{gathered}$ | - | - | HV |
| $50 \times 6$ | Voltage Doubler | 8 -pin 1. | 7AJ | Hir. | 50 | 0.13 | 117 | 75 | 700 | 450 | HV |
| 50Y6GT | Full-Wave Rectiliter | 7-pin 0. | 70 | Htr. | 50 | 0.15 | 125 | 85 |  |  | HV |
| 50Y7GT | Voltage Doubler | 8-pin L. | 8 AN | Hht. | 50 | 0.15 | 117 | 65 | 700 |  | HV |
| 5026G | Voltage Doubler | 7-pin 0. | 70 | Hro. | 50 | 0.3 | 125 | 150 | - | - | HV |
| $5027 \mathrm{Cl}^{10}$ | Voltage Doubler | 8 -pin 0. | BAN | Mr. | 50 | 0.15 | 117 | 65 |  | - | HV |
| 7047 GT | Rectifier-Tetrode | 8 -pin 0. | 8 AB | Hitr. | 70 | 0.15 | $125{ }^{3}$ | 60 |  |  | HV |
| 70L7GT | Rectifior-Tetrode | 8 -pin 0. | BAA | Htr. | 70 | 0.15 | 117 | 70 |  | 350 | HV |
| 72 | Half-Wave Rectifler | 4-Din M. | 4P | Fil. | 2.5 | 3.0 | - | 30 | 20000 | 150 | HV |
| 73 | Half-Wave Rectifier | - 4 - 0 . | 4 Y | Fil. | 2.5 | 4.5 | $\square$ | 20 | 13000 | 3000 | HV |
| 80 | Full-Wave Rectifier | 4-pin M. | 4 C | Fil. | 5.0 | 2.0 | $\begin{aligned} & 350^{4} \\ & 500^{2} \\ & \hline \end{aligned}$ | $\begin{aligned} & 125 \\ & 125 \\ & \hline \end{aligned}$ | 1400 | 375 | HV |
| 81 | Half-Wave Rectifler | 4.pin M. | 48 | FII. | 7.5 | 1.25 | 700 | 85 | - | - | HV |
| 82 | Full-Wave Rectifior | 4-pin M. | 4 C | Fil. | 2.5 | 3.0 | 500 | 125 | 1400 | 400 | MV |
| 83 | Full-Wave Rectifier | 4 -pin M. | 4 C | FI. | 5.0 | 3.0 | 500 | 250 | 1400 | 800 | MY |
| $83 . \mathrm{V}$ | Full-Wave Rectifior | 4-pin M. | 4AD | Hir. | 5.0 | 2.0 | 400 | 200 | 1100 |  | HV |
| $84 / 624$ | Full-Wave Rectifior | 5 -pin 5. | 50 | Hir. | 6.3 | 0.5 | 350 | 60 | 1000 | - | HV |
| $\begin{aligned} & 11747 \mathrm{GT} / \\ & 117 \mathrm{M} / \mathrm{GT} \end{aligned}$ | Rectifler-Tetrode | 0 -pin 0. | 8 AO | Htr. | 117 | 0.09 | 117 | 75 | - | - | HV |
| 117 NFGT | Rectifor-Tetrode | 8-pin 0. | BAV | Hir. | 117 | 0.09 | 117 | 75 | 350 | 450 | HV |
| 117P7GT | Rectifier-Tutrode | S-pin 0. | sav | Hir. | 117 | 0.09 | 117 | 75 | 350 | 450 | HV |
| 11723 | Half-Wave Rectifer | 7 -pin 8. | 4BR | Hir. | 117 | 0.04 | 117 | 90 | 330 | - | HV |
| 1172467 | Half-Wave Rectifer | 6-pin 0. | 5AA | Hr. | 117 | 0.04 | 117 | 90 | 350 |  | HV |
| 1172691 | Voltage Doubler | 7-pin 0. | 79 | Atr. | 117 | 0.075 | 235 | 60 | 700 | 360 | HV |
| 217-A ${ }^{111}$ | Half-Wave Rectiller | 4-pin J. | 4AT | Fil. | 10 | 3.25 |  |  | 3500 | 600 | HV |
| 217-6 | Half-Wave Rectifer | 4-pin J. | 4AT | Fil. | 10 | 3.25 |  |  | 7500 | 600 | HV |
| 7225 | Half-Wave Rectifier | 4-pin M. | 4P | Fil. | 2.3 | 5.0 | - | 250 | 10000 | 1000 | MY |
| 249-8 | Holf-Wave Rectifier | 4-pin M. | Fig. 53 | Fil. | 2.5 | 7.5 | 3180 | 375 | 10000 | 1500 | MV |
| HK253 | Half-Wave Rectifior | 4-pin J. | 4AT | Fil. | 5.0 | 10 |  | 330 | 10000 | 1500 | HV |
| $\begin{aligned} & \text { 705A } \\ & \text { RK-705A } \end{aligned}$ | Half-Wave Rectifler | 4-pin W. | T-3AA | FII. | $\begin{aligned} & 2.5^{9} \\ & 5.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} 5.0 \\ 5.0 \\ \hline \end{array}$ |  | $\begin{array}{r} 50 \\ 100 \\ \hline \end{array}$ | $\begin{aligned} & 35000 \\ & 35000 \end{aligned}$ | $\begin{aligned} & 375 \\ & 750 \end{aligned}$ | HV |
| 816 | Half-Wave Rectifler | 4-pin S. | 4 P | Fil. | 2.5 | 2.0 | 2200 | 125 | 7500 | 500 | MV |
| 836 | Half-Wave Rectifer | 4-pin M. | 4 P | Hir. | 2.5 | 5.0 |  |  | 5000 | 1000 | HV |
| 8601/866 | Holf-Wave Rectifior | 4-ptn M. | $4 P$ | Fit. | 2.5 | 5.0 | 3500 | 250 | 10000 | 1000 | MV |
| 8608 | Half-Wave Rectifer | 4-pin M. | 4 | Fil. | 5.0 | 5.0 | T | - | 8500 | 1000 | MV |
| 866 Jr . | Half-Wave Rectifler | 4-pin M. | 48 | Fil. | 2.5 | 2.5 | 1250 | 2503 |  |  | MV |
| HYas6 Jr. | Half-Wave Rectifier | 4-pin M. | 4P | Fil. | 2.5 | 2.5 | 1730 | $250{ }^{3}$ | 5000 |  | MV |
| RK866 | Holf-Wave Rectifor | 4-pin M. | 4 P | Fil. | 2.5 | 5.0 | 3500 | 250 | 10000 | 1000 | MV |
| $871{ }^{10}$ | Half-Wave Rectifior | 4-pin M. | 4P | Fil. | 2.5 | 2.0 | 1750 | 250 | 5000 | 500 | MV |
| 878 | Half-Wave Rectifier | 4-pin M. | 4P | Fil. | 2.5 | 5.0 | 7100 | 5 | 23000 | - | HV |
| 879 | Half-Wave Rectifier | 4-pin 5. | 4P | Fil. | 2.5 | 1.75 | 2650 | 7.5 | 7500 | 100 | HV |
| 872A/872 | Half-Wave Rectifior | 4-pin d. | 4AT | Fil. | 5.0 | 7.5 | $\underline{\square}$ | 1250 | 10000 | 5000 | MV |
| 9754 | Half-Wave Rectifier | 4-pin J. | 4AT | Fil. | 5.0 | 10.0 |  | 1500 | 15000 | 6000 | MY |
| $\begin{aligned} & \text { OZ4A/ } \\ & 1003 \end{aligned}$ | Full-Wave Rectifier | 5-pin 0. | 4R | Cold | $\underline{\square}$ |  | $\cdots$ | 110 | 880 | - | G |
| $\begin{aligned} & 1005 / \\ & \text { CK } 1005 \end{aligned}$ | Full-Wave Rectifier | 8 -pin 0. | 5AQ | Fil. | 6.3 | 0.1 | - | 70 | 450 | 210 | G |
| $\begin{aligned} & 1006 / \\ & \text { CK } 1006 \end{aligned}$ | Full-Wave Rectifier | 4-pin M. | 4 C | Fil. | 1.75 | 2.25 | - | 200 | 1600 | - | G |
| CK 1007 | Full-Wave Rectifier | 8 -pin 0. | T-9G | Fil. | 1.0 | 1.2 |  | 110 | 980 | $\underline{\square}$ | G |
| CK 1009/BA | Full-Wave Rectifier | 4-pin M. |  | Cold | $\cdots$ |  |  | 350 | 1000 |  | G |
| 1274 | Full-Wave Rectifier | 6-pin 0. | 65 | Hir. | 6.3 | 0.6 | Same as 7 Y 4 |  |  |  | HV |
| 1275 | Full-Wave Rectifler | 4-pin M. | 4 C | Fil. | 5.0 | 1.75 | Same as 52.3 |  |  |  | HV |
| 1616 | Half-Wave Rectifior | 4-pin M. | 4 P | Fil. | 2.5 | 5.0 | $=$ | 130 | 6000 | 800 | HV |
| $\begin{aligned} & 1641 / \\ & \text { RK60 } \end{aligned}$ | Full-Wave Rectifier | 4-pin M. | T-4AG | Fil. | 5.0 | 3.0 | — | $\begin{array}{r} 50 \\ 250 \\ \hline \end{array}$ | $\begin{aligned} & 4500 \\ & 2500 \end{aligned}$ | - | HV |
| 1654 | Half-Wave Rectifier | 7-pin B . | 27 | Fil. | 1.4 | 0.05 | 2500 | 1 | 7000 | 6 | HV |
| 5517 | Half-Wave Rectifier | 7-pin 8. | 5BU | Cold | - | $\underline{\square}$ | 1200 | 6 | - | 50 | G |
| 5825 | Half-Wave Rectifier | 4-pin M. | 4P | Fil. | 1.6 | 1.25 | - | 2 | 60000 | 40 | HV |
| 8008 | Malf-Wave Rectifler | 4-pin ${ }^{\text {c }}$ | Fig. 11 | Fil. | 5.0 | 7.5 | - | 1250 | 10000 | 5000 | MV |
| 8013 A | Half-Wave Rectifer | 4-pin M. | 4 P | $F 1$. | 2.5 | 5.0 | - | 20 | 40000 | 150 | HV |
| 8016 | Half-Wave Rectifier | 6-pin 0. | 4AC | Fil. | 1.25 | 0.2 | - | 2.0 | 10000 | 7.5 | HV |
| 8020 | Hall-Wove Rectifier | 4-pin M. | 4P | FII. | 5.0 | 5.5 | 10000 | 100 | 40000 | 750 | HV |
|  |  |  |  |  | 5.8 | 6.5 | 12500 | 100 | 40000 | 750 |  |
| RK19 | Full-Wave Rectifier | 4-pin M. | 4AT | Her. | 7.5 | 2.5 | 1250 | 2004 | 3500 | 600 | HV |
| RK21 | Half-Wave Rectifier | 4-pin M. | 4P | Htr. | 2.5 | 4.0 | 1250 | 2004 | 3500 | 600 | HV |
| RK22 | Full-Wave Rectifier | 4-pin M. | T-4AG | Hir. | 2.5 | 8.0 | 1250 | 2004 | 3500 | 600 | HV |

[^3][^4]
## CATHODE-RAY TUBE BASES



## RECEIVING TUBE SUBSTITUTION GUIDE

$11 E$

$11 F$








117






14 A

$14 B$







14L


CATHODE-RAY TUBE CHARACTERISTICS
electrostatic types-cathode ray tubes

| Type | Heater |  | Nominal Dimensions |  | Base |  | Screen |  | Maximum Design Center Ratinga |  |  |  | Typical Operating Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | Diameter Inches | Length Inches |  |  | Fluorescence | Peraistence | Anode \#1 Volts | Anode \#2 Volts | Anorle $\$ 3$ Volcs | Anode \#2 to <br> Deflection <br> Plate <br> Peak Volis$\|$ | $\left\|\begin{array}{c} \text { Anode \#2 } \\ \text { Volts } \end{array}\right\|$ | $\begin{gathered} \text { Anode \#1 } \\ \text { Avg. Vol ts** } \end{gathered}$ | Anode : 3 Volts | Grid Aenge Volts* | $\begin{gathered} \text { Deflection } \\ \text { Avp. Volte DC/Inch } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | D 1-2 | D 3-4 |
| $\begin{aligned} & 2 \mathrm{AP1}, \\ & \text { 2AP1A) } \end{aligned}$ | 6.3 | 0.6 | 2 | 7-7/16 | Small She 11 <br> Magnal 11 Pin | $\begin{aligned} & 1118 \\ & 11 \mathrm{~L} \end{aligned}$ | Green | Medium | 500 | 1000 | $\ldots$ | 600 | $\begin{array}{r} 500 \\ 1000 \\ \hline \end{array}$ | $\begin{aligned} & \hline 125 \\ & 250 \\ & \hline \end{aligned}$ | $\ldots$ | $\begin{aligned} & 15-45 \\ & 30-90 \end{aligned}$ | $\begin{aligned} & 115 \\ & 230 \end{aligned}$ | $\begin{array}{r} 98 \\ 196 \\ \hline \end{array}$ |
| $2 \mathrm{PP1}$ | 6.3 | 0.6 | 2-1/16 | 7-5/8 | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 12 \text { Pin } \end{aligned}$ | $\begin{aligned} & 12 \mathrm{~F} \\ & 12 \mathrm{~F} \end{aligned}$ | Green | Medium | 1000 | 2500 | .... | 500 | $\begin{aligned} & 1000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 150-280 \\ & 300-560 \end{aligned}$ | $\ldots$ | $\begin{aligned} & 0-67.5 \\ & 0-135 \end{aligned}$ | $\begin{aligned} & 115-155 \\ & 230-310 \end{aligned}$ | $\begin{array}{r} 74-100 \\ 148-200 \end{array}$ |
| $\begin{aligned} & 3 \mathrm{SPI}, \\ & 3 \mathrm{PPP} 1 A) \\ & 3 \mathrm{AP4}, \end{aligned}$ | 2.5 | 2.1 | 3 | 11-1/2 | Medium 7 Pin | $\begin{aligned} & \text { 7AN } \\ & \text { 7CF } \\ & 7 \mathrm{AN} \end{aligned}$ | Green Green White | Medium Medium Medium | 1000 | 1500 | $\cdots$ | 600 | 600 800 1000 1200 1500 | $\begin{aligned} & 170 \\ & 230 \\ & 285 \\ & 345 \\ & 475 \end{aligned}$ |  | $\begin{gathered} 14-40 \\ 14-40 \\ 17-50 \\ 20-60 \\ 22.5-67.5 \end{gathered}$ | $\begin{array}{r} 47 \\ 61 \\ 76 \\ 91 \\ 114 \\ \hline \end{array}$ | $\begin{array}{r} 45 \\ 58 \\ 73 \\ 87 \\ 109 \\ \hline \end{array}$ |
| $\begin{aligned} & \begin{array}{l} 3 \mathrm{RP} \mathrm{P}_{1} \\ 3 \mathrm{BP} 1 \mathrm{~A}) \end{array}, ~ \end{aligned}$ | 6.3 | 0.6 | 3 | 10 | Medium Shie ll Diheptal 12 Pin | $\begin{aligned} & 144 \\ & 144 \end{aligned}$ | Green Green | Medium Medium | 1000 | 2000 | $\ldots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{array}{r} 430 \\ 575 \end{array}$ | $\ldots$ | $\begin{gathered} 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{aligned} & 168 \\ & 221 \end{aligned}$ | $\begin{aligned} & 123 \\ & 164 \end{aligned}$ |
| ${ }^{3} \mathrm{P} \mathrm{P}_{1}$ | 6.3 | 0.6 | 3 | 10-3/8 | Medium <br> Mafnal 11 Pin, Sleeve | IIC | Green | Medium | 1000 | 2000 | $\ldots$ | 50 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 430 \\ & 575 \end{aligned}$ | $\ldots$ | $\begin{gathered} 22.5-67.5 \\ 30-90 \end{gathered}$ | ${ }_{124}^{165.5}$ | $\begin{aligned} & \hline 221 \\ & 165 \end{aligned}$ |
| $\begin{array}{\|l\|l\|} \hline 3 \mathrm{P} 11 \\ 3(P P 1 A) \end{array}$ | 6.3 | 0.6 | 3 | 10-7/16 | $\begin{aligned} & \text { Medium She ll } \\ & \text { Diheptal } 12 \text { Pin } \end{aligned}$ | $\begin{aligned} & 14 \mathrm{C} \\ & 14 \mathrm{H} \end{aligned}$ | Green | Medium | 1000 | 2000 | $\ldots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 430 \\ & 575 \end{aligned}$ | $\ldots$ | $\begin{gathered} 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{aligned} & 166 \\ & 221 \end{aligned}$ | $\begin{aligned} & 123 \\ & 164 \end{aligned}$ |
| ${ }^{36 P 1}$ | 6.3 | 0.6 | 3 | 9-15/15 | Large Mafer <br> Magnal 11 Pin, Sleeve | 11A | Green | Medium | 1000 | 2000 | $\ldots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{array}{r} 430 \\ 575 \end{array}$ | $\ldots$ | $\underset{\substack{\text { 22.5-67.5 } \\ 30-90}}{ }$ | $\begin{aligned} & 165.5 \\ & 221 \\ & \hline \end{aligned}$ | $\begin{aligned} & 124 \\ & 165 \end{aligned}$ |
| $\begin{aligned} & 3 F P 7 \\ & 3 P P 7 A \end{aligned}$ | 6.3 | 0.6 | 3 | 10 | Medium Shell Dilieptal 12 Pin | $\begin{aligned} & 14 B \\ & 140 \end{aligned}$ | Characteristica of Phosphor No. 7 |  | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 2000 \\ & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 575 \\ & 430 \\ & \mathbf{5 7 5} \end{aligned}$ | $\begin{aligned} & 2000 \\ & 3000 \\ & 4000 \end{aligned}$ | $\begin{gathered} 30-90 \\ 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{aligned} & 221 \\ & 221 \\ & 295 \end{aligned}$ | $\begin{aligned} & 164 \\ & 163 \\ & 217 \end{aligned}$ |
| $\begin{aligned} & 3{ }_{3} \mathrm{CP}_{1} \\ & 3 \mathrm{GPP} 4 \end{aligned}$ | 6.3 | 0.6 | 3 | 11-1/2 | $\begin{array}{\|l\|} \hline \text { Medium She } 11 \\ \text { Mapnal } 11 \text { Pin } \\ \hline \end{array}$ | $\begin{aligned} & 11 A \\ & 11 A \end{aligned}$ | Green White | Medium Medium | 1000 | 1500 | .... | 500 | $\begin{aligned} & 1000 \\ & 1500 \end{aligned}$ | $\begin{aligned} & 234 \\ & 350 \end{aligned}$ | $\ldots$ | $\underset{25-75}{16.5-49.5}$ | $\begin{array}{r} 80 \\ 120 \\ \hline \end{array}$ | $\begin{array}{r} 70 \\ 105 \end{array}$ |
| $\begin{aligned} & 3 G P 1 A \\ & 3 \in P 4 A \\ & \hline \end{aligned}$ | 6.3 | 0.6 | 3 | 11-1/2 | $\begin{aligned} & \text { Medium Sheil } \\ & \text { Magnal } 11 \text { Pin } \end{aligned}$ | $\begin{aligned} & 11 \mathrm{~N} \\ & 1 \mathrm{~N} \end{aligned}$ | Green White | Medium Medium | 1000 | 1500 | .... | 550 | $\begin{array}{r} 1000 \\ 500 \end{array}$ | $\begin{aligned} & 163-291 \\ & 245-437 \end{aligned}$ | $\ldots$ | $\begin{gathered} 16.5-49.5 \\ 25-75 \end{gathered}$ | $\begin{aligned} & 96-96 \\ & 96-144 \end{aligned}$ | $\begin{aligned} & \hline 56-84 \\ & 84-126 \end{aligned}$ |
| 3.JP1 | 6.3 | 0.6 | 3 | 10 | $\begin{aligned} & \text { Medium Shell } \\ & \text { Diheptal } 12 \text { Pin } \end{aligned}$ | $\begin{aligned} & 14 \sqrt{1} \\ & 143 \end{aligned}$ | Green | Medium | 1000 | 2000 | 4000 | 500 | $\begin{array}{r} 500 \\ 2000 \\ 500 \\ 2000 \end{array}$ | $\begin{aligned} & 430 \\ & 575 \\ & 430 \\ & 575 \end{aligned}$ | $\begin{aligned} & 1500 \\ & 2000 \\ & 3000 \\ & 4000 \\ & \hline \end{aligned}$ | $\begin{gathered} 22.5-67.5 \\ 320-90 \\ 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{aligned} & 120 \\ & 160 \\ & 150 \\ & 200 \end{aligned}$ | $\begin{array}{r} 89 \\ 119 \\ 111 \\ 148 \\ \hline \end{array}$ |
| $\begin{aligned} & 3 \mathrm{KP1} 1 \\ & 3 \mathrm{KP} 4 \\ & \hline \end{aligned}$ | 6.3 | 0.6 | 3 | 11-1/2 | Medium Shell Magnal 11 Pin | $\begin{aligned} & 11 \mathrm{M} \\ & 11 \mathrm{M} \end{aligned}$ | Green Wite | Medium Medium | 1000 | 2500 | $\ldots$ | 500 | $\begin{aligned} & 1000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 160-300 \\ & 320-600 \end{aligned}$ | $\cdots$ | $\begin{aligned} & 0-45 \\ & 0-90 \end{aligned}$ | $\begin{array}{\|c\|} \hline 50-68 \\ 100-136 \end{array}$ | $\begin{aligned} & 38-52 \\ & 76-104 \end{aligned}$ |
| 3481 | 6.3 | 0.6 | 3 | 8 | $\begin{array}{\|l\|} \hline \text { Sma II She I1 } \\ \text { Duodecal } 12 \text { Pin } \\ \hline \end{array}$ | 12 F | Green | Medium | 1000 | 2500 | $\ldots$ | 500 | $\begin{array}{r} 1000 \\ 2000 \\ \hline \end{array}$ | $\begin{array}{r} 200-350 \\ 400-700 \\ \hline \end{array}$ | $\ldots$ | $\begin{aligned} & 0-63 \\ & 0-126 \end{aligned}$ | $\begin{aligned} & 140-190 \\ & 280-380 \end{aligned}$ | $\begin{aligned} & 130-180 \\ & 260-360 \end{aligned}$ |
| 30P1 | 6.3 | 0.3 | 2-3/4 | 6-1/8 | Furopean 9 Pin | 9 D | Green | Medium | 700 | 1500 | .... | 550 | $\begin{array}{r} 800 \\ 1200 \end{array}$ | $\begin{array}{r} 200-320 \\ 240-480 \\ \hline \end{array}$ | $\ldots$ | $\begin{aligned} & 21-50 \\ & 31-74 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 143-193 \\ 214-290 \\ \hline \end{array}$ | $\begin{array}{\|} 89-121 \\ 133-181 \\ \hline \end{array}$ |
| $\begin{aligned} & 3 \text { 3PP1 } \\ & 3 R P 1 A \end{aligned}$ | 6.3 | 0.6 | 3 | 9-1/8 | $\begin{aligned} & \text { Small Shell Duodecal } \\ & 12 \text { Pin } \end{aligned}$ | 12F. | Green | Medium | 1000 | 2500 | $\cdots$ | 500 | $\begin{aligned} & 1000 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 165-310 \\ & 330-620 \\ & \hline \end{aligned}$ | $\ldots$ | $\begin{array}{r} 67.5 \\ 13.5 \\ \hline \end{array}$ | $\begin{aligned} & \hline 85 \\ & 61 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 172 \\ & 122 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 3 \text { SPP1 }^{3 S} \\ & 3 S P_{4} \end{aligned}$ | 6.3 | 0.6 | $3 \times 1$ 1-1/2 | 9-1/8 | $\begin{aligned} & \hline \text { Small Shell } \\ & \text { Duodecal } 12 \text { Pin } \\ & \hline \end{aligned}$ | 12 E | Green White | Medium Mediun | 1100 | 2750 | $\ldots$ | $\ldots$ | $\begin{aligned} & 1000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 165-310 \\ & 330-620 \end{aligned}$ | $\ldots$ | $\begin{gathered} 28.5-67.5 \\ 58-135 \end{gathered}$ | $\begin{gathered} 73-99 \\ 146-198 \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline 52-70 \\ 104-140 \\ \hline \end{array}$ |
| 5AP1 | 6.3 | 0.6 | 5-1/4 | 13 | Large Wafer <br> Mapnal 11 Pin, Sleeve | 11 A | Green | Medium | 1200 | 2000 | $\ldots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 430 \\ & 575 \end{aligned}$ | $\ldots$ | $\begin{aligned} & 31-57 \\ & 40-74 \\ & \hline \end{aligned}$ | 93 | 90 |
| $5 \mathrm{AP4}$ | 6.3 | 0.6 | 5-1/4 | 13 | Larpe Wafer <br> Mapnal 11 Pin, Sleeve | 114 | Wite | Medium | 1200 | 2000 | $\cdots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 430 \\ & 575 \end{aligned}$ | $\cdots$ | $\begin{aligned} & 17.6-57 \\ & 22.8-74 \end{aligned}$ | 93 | 90 |
| $\begin{array}{\|l\|} \hline 5 \mathrm{BP1} \\ 58 P_{4} \\ 58 \end{array}$ | 6.3 | 0.6 | 5.1/4 | 16-3/4 | Larpe Wafer Marnal 11 Pin | $\begin{aligned} & 11 \mathrm{~A} \\ & 11 \mathrm{~A} \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | $\cdots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 310 \\ & 425 \end{aligned}$ | $\ldots$ | 20-60 | $\begin{aligned} & 63 \\ & 84 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 57 \\ & 76 \\ & \hline \end{aligned}$ |
| 58P1A | 6.3 | 0.6 | $5-1 / 4$ | 16-3/4 | Nedium Shell Maparil 11 Pin | 11 N | Green | medium | 1000 | 2000 | $\cdots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | 337-450 | $\ldots$ | $\begin{aligned} & 15-45 \\ & 20-60 \\ & \hline \end{aligned}$ | $\begin{aligned} & 63 \\ & 84 \\ & \hline \end{aligned}$ | $\begin{aligned} & 57 \\ & 76 \\ & \hline \end{aligned}$ |
| 5RP7A | 6.3 | 0.6 | 5-1/4 | 16-3/4 | $\begin{array}{\|l\|} \hline \text { Medium She 11 } \\ \text { Magnal ll Pin } \end{array}$ | 1 N | Characteri P7 Scr | stics of reen | 1000 | 2000 | $\ldots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 235-420 \\ & 315-560 \end{aligned}$ | $\ldots$ | $\begin{aligned} & 15-45 \\ & 20-60 \end{aligned}$ | $\begin{aligned} & \hline 52-74 \\ & 70-98 \end{aligned}$ | $\begin{aligned} & 47-67 \\ & 63-89 \end{aligned}$ |

Cormanly used Phosphors off voltage. Supply should be adjustable from 0 to value shown.
Courtesy Syivania Electric Products Inc.
electrostatic types-cathode ray tubes

| Type | Heater |  | Nominal Dimensions |  | Pase | $\begin{gathered} \text { RalA } \\ \text { Basing } \end{gathered}$ | Screen |  | Maximum Design Center Ratings |  |  |  | Typical Operating Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | Diameter Inches | Length Inches |  |  | Fluorescence | Persistence | Anode \#1 Volts | Anode ${ }^{2} 2$ Volts | Anode \#3 Volts | Anode ${ }^{2}$ to toDeflectionPlatePeak Volts | $\left\|\begin{array}{c} \text { Anode \#2 } \\ \text { Volts } \end{array}\right\|$ | $\left\lvert\, \begin{gathered} \text { Anode } \neq 1 \\ \text { Avg. Volts"* } \end{gathered}\right.$ | $\left\|\begin{array}{c} \text { Anode }: 3 \\ \text { Volts } \end{array}\right\|$ | Grid Range | $\begin{gathered} \text { Deflection } \\ \text { Avg. Volts DC/Inch } \end{gathered}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | D 1-2 | D 3-4 |
| $\begin{aligned} & 5 \mathrm{SPP}_{1} \\ & 5 \mathrm{CP4} \end{aligned}$ | 6.3 | 0.6 | 5-1/4 | 16-3/4 | Yedium Shell <br> Tiheptal 12 Pin | $\begin{aligned} & 14 \mathrm{~B} \\ & 14 \mathrm{~B} \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 2000 \\ & 1500 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 575 \\ & 430 \\ & 575 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2000 \\ & 3000 \\ & 4000 \\ & \hline \end{aligned}$ | $\begin{gathered} 30-90 \\ 22.5-67.5 \\ 30-90 \\ \hline \end{gathered}$ | $\begin{aligned} & 73 \\ & 69 \\ & 92 \\ & \hline \end{aligned}$ | $\begin{aligned} & 64 \\ & 56 \\ & 74 \\ & \hline \end{aligned}$ |
| $5 C P 1 A$ | 6.3 | 0.6 | 5-1/4 | 16-3/4 | $\begin{array}{\|l\|} \hline \text { Medium Shell } \\ \text { Diheptal } 12 \text { Pin } \end{array}$ | $\begin{aligned} & 14 \mathrm{~J} \\ & 14 \mathrm{~J} \end{aligned}$ | Green | Medium | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 2000 \\ & 1500 \\ & 2000 \end{aligned}$ | $\begin{array}{r} 575 \\ 430 \\ 575 \\ \hline \end{array}$ | $\begin{aligned} & 2000 \\ & 3000 \\ & 4000 \\ & \hline \end{aligned}$ | $\begin{gathered} 30-90 \\ 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{array}{r} 73 \\ 69 \\ 92 \\ \hline \end{array}$ | $\begin{aligned} & 64 \\ & 56 \\ & 74 \end{aligned}$ |
| ${ }^{56 P 1}$ | 6.3 | 0.6 | 5-1/4 | 16-3/4 | Large Wafer Magnal 11 Pin, Sleeve | 11A | Green | Medium | 1000 | 2000 | .... | 500 | 2000 | 425 | $\ldots$ | 24-5¢ | 36 | 72 |
| $\begin{aligned} & 5 \mathrm{Pl} \\ & \hline 5 \mathrm{Pl} \\ & \hline \end{aligned}$ | 6.3 | 0.6 | 5-1/4 | 16-3/4 | $\begin{aligned} & \hline \text { Large Wafer } \\ & \text { Marnal } 11 \text { Pin, Sleeve } \end{aligned}$ | $\begin{aligned} & 11 A \\ & 11 A \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | .... | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{array}{r} 310 \\ 425 \\ \hline \end{array}$ | $\cdots$ | $15-4.5$ $20-60$ | $\begin{aligned} & 63.5 \\ & 84.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 57.8 \\ & 77.0 \end{aligned}$ |
| 5HP1A | 6.3 | 0.6 | 5-1/4 | 16-3/4 | Large Wafer Mapnal 11 Pin, Micanol | 11 N | Green | Medium | 1000 | 2000 | .... | 500 | $\begin{array}{r} 1500 \\ 2000 \\ \hline \end{array}$ | $\begin{array}{r} 337 \\ 450 \\ \hline \end{array}$ | $\cdots$ | $\begin{aligned} & 15-45 \\ & 20-40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 63 \\ & 84 \\ & \hline \end{aligned}$ | $\begin{array}{r} 57 \\ \hline 76 \\ \hline \end{array}$ |
| $\begin{array}{\|l\|} \hline 5 \cdot \mathrm{JPl} \\ 5 \mathrm{JP4} \end{array}$ | 6.3 | 0.6 | 5-5/16 | 16-3/4 | $\begin{aligned} & \hline \text { Medium } \\ & \text { Magnal Il Pin } \\ & \hline \end{aligned}$ | $\begin{aligned} & 11 \mathrm{E} \\ & 11 \mathrm{~F} \end{aligned}$ | Green White | Medium Medium | 100n | 2000 | 4000 | 500 | $\begin{aligned} & 1000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 260 \\ & 520 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2000 \\ & 4000 \\ & \hline \end{aligned}$ | $\begin{gathered} 22.2-51.8 \\ 45-105 \\ \hline \end{gathered}$ | 95 | 96 |
| $\begin{aligned} & \text { 5JP1A } \\ & \text { 5JP4A } \end{aligned}$ | 6.3 | 0.6 | 5-5/16 | 16.3/4 | Medium Nharnal 11 Pin | $\begin{aligned} & 115 \\ & 115 \\ & \hline \end{aligned}$ | Green Mite | Medium Medium | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 250-472 \\ & 333-630 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3000 \\ & 4000 \end{aligned}$ | $\begin{aligned} & \hline 34-79 \\ & 45-105 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 58-86 \\ & 77-115 \end{aligned}$ | $\begin{aligned} & \hline 58-86 \\ & 77-115 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 5 L P 1 \\ & 5 L P 4 \end{aligned}$ | 6.3 | 0.6 | 5-5/16 | 16-3/4 | Medium Mapnal 11 Pin, Sleeve | $\begin{aligned} & 11 \mathrm{~F} \\ & 11 \mathrm{~F} \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 1000 \\ & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 375 \\ & 500 \end{aligned}$ | $\begin{aligned} & 2000 \\ & 3000 \\ & 4000 \end{aligned}$ | $\begin{array}{c\|} 15-45 \\ 22.5-67.5 \\ 30-90 \\ \hline \end{array}$ | $\begin{array}{r} 52 \\ 77 \\ 103 \\ \hline \end{array}$ | $\begin{aligned} & \hline 45 \\ & 68 \\ & 90 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 5 L P 1 A \\ & 5 L P 4 A \end{aligned}$ | 6.3 | 0.6 | 5-5/16 | 16-3/4 | Medium Mmanal 11 Pin, Sleeve | $\begin{aligned} & 117 \\ & 117 \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | 4000 | 550 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 282-475 \\ & 376-633 \end{aligned}$ | $\begin{aligned} & 3000 \\ & 4000 \end{aligned}$ | 22.5-67.5 <br> 30-90 | $\begin{aligned} & \hline 62-93 \\ & 83-124 \end{aligned}$ | $\begin{array}{\|l\|} \hline 54-81 \\ 72-108 \\ \hline \end{array}$ |
| $\begin{aligned} & \hline \text { SNP1 } \\ & \text { SNP4 } \\ & \hline \end{aligned}$ | 2.5 | 2.1 | 5-5/16 | 15-7/8 | Large 7 Pin | $\begin{aligned} & \text { 7AN } \\ & \text { TAN } \end{aligned}$ | Green White | Medium Medium | 1000 | 1500 | .... | 600 | $\begin{aligned} & 1000 \\ & 1500 \end{aligned}$ | $\begin{aligned} & 250 \\ & 375 \end{aligned}$ | $\ldots$ | $\begin{gathered} 16.5-49.5 \\ 15-45 \end{gathered}$ | 65 | 50 |
| $\begin{aligned} & \text { 5NP1 } \\ & \text { 5NP4 } \end{aligned}$ | 6.3 | 0.6 | 5-5/16 | 16-3/4 | Larre Wafer Magnal 11 Pin, Sleeve | $\begin{aligned} & 11 \mathrm{~A} \\ & 11 \mathrm{~A} \end{aligned}$ | Green White | $\begin{aligned} & \text { Medium } \\ & \text { Modium } \end{aligned}$ | 1000 | 2000 |  | 500 | $\begin{array}{r} 1500 \\ 2000 \end{array}$ | $\begin{aligned} & 337 \\ & 450 \end{aligned}$ |  | $\begin{aligned} & 15-4.5 \\ & 20-60 \end{aligned}$ | 84 | 76 |
| $\begin{aligned} & \text { 5RP1 } \\ & 5 R P 4 \end{aligned}$ | 6.3 | 0.6 | 5-1/4 | 16-3/4 | $\begin{aligned} & \begin{array}{l} \text { Medium She } 11 \\ \text { Diheptal } 12 \text { Pin } \end{array} \end{aligned}$ | $\begin{aligned} & 14 \mathrm{~F} \\ & 14 \mathrm{~F} \end{aligned}$ | Green White | Medium Nedium | 15550 | 3500 | 25500 | 1200 | $\begin{array}{r} 2000 \\ 2000 \\ \hline \end{array}$ | $\begin{aligned} & \hline 518 \\ & 528 \end{aligned}$ | $\begin{aligned} & 10000 \\ & 20000 \end{aligned}$ | $\begin{aligned} & 30-90 \\ & 30-90 \\ & \hline \end{aligned}$ | $\begin{aligned} & 30-45 \\ & 36-54 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 30-45 \\ & 36-54 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & \text { 5RP1A } \\ & \text { 5RP4A } \end{aligned}$ | 6.3 | 0.6 | 5-2/4 | 16-3/4 | Ahedium She 11 Dilieptal 12 Pin | 14 F | Green White | Medium Nedium | 15550 | 3500 | 25500 | 1200 | $\begin{aligned} & 2000 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 518 \\ & 528 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10000 \\ & 20000 \end{aligned}$ | $\begin{aligned} & \hline 30-90 \\ & 30-90 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 30-45 \\ & 36-54 \\ & \hline \end{aligned}$ | $\begin{aligned} & 30-45 \\ & 36-54 \\ & \hline \end{aligned}$ |
| $\begin{array}{\|l\|} \hline 5 S P 1 \\ \text { 5SP4 } \end{array}$ | 6.3 | 0.6 | 5-1/4 | 18-1/2 | Medium Shell <br> Dilieptal 12 Pin | $\begin{aligned} & 14 K \\ & 14 K \end{aligned}$ | Green White | Medium Medium | 1000 | 2000 | 4000 | 500 | $\begin{aligned} & 1500 \\ & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & \begin{array}{l} 431 \\ 431 \\ 575 \end{array} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1500 \\ & 3000 \\ & 4000 \\ & \hline \end{aligned}$ | $\begin{gathered} 22.5-67.5 \\ 22.5-67.5 \\ 30-90 \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 55 \\ & 69 \\ & 92 \\ & \hline \end{aligned}$ | $\begin{array}{r} 48 \\ 59 \\ 79 \\ \hline \end{array}$ |
| SUP1 | 6.3 | 0.6 | 5-1/4 | 14-3/4 | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal } 12 \text { Pin } \\ \hline \end{array}$ | 12F, | Green | Hedium | 1000 | 2500 | $\cdots$ | 500 | $\begin{aligned} & 1000 \\ & 2000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 170-320 \\ & 340-640 \end{aligned}$ | $\ldots$ | $\begin{gathered} 22.5-67.5 \\ 30-90 \end{gathered}$ | $\begin{aligned} & 28-38.5 \\ & 56-77 \\ & \hline \end{aligned}$ | $\begin{aligned} & 28-31 \\ & 46-62 \end{aligned}$ |
| 5VP7 | 6.3 | 0.6 | 5-1/4 | 16-3/4 | $\begin{aligned} & \text { Medium Shell } \\ & \text { Magnal ll Pia } \end{aligned}$ | 11 N | Characteristics of Phosphor No. 7 |  | 1000 | 2500 | $\cdots$ | 500 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 236-422 \\ & 315-562 \end{aligned}$ |  | $\begin{aligned} & \hline 15-45 \\ & 20-40 \end{aligned}$ | $\begin{aligned} & 52-74 \\ & 70-98 \end{aligned}$ | $\begin{aligned} & 47-67 \\ & 63-89 \end{aligned}$ |
| 5XP1 | 6.3 | 0.6 | 5-1/4 | 17-5/8 | $\begin{aligned} & \text { Medium She } 11 \\ & \text { Diheptal } 12 \text { Pin } \end{aligned}$ | 14 F | Green | Medium | 1550 | 3500 | 25500 | 1200 | $\begin{aligned} & 2000 \\ & 2000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & \begin{array}{l} 362-695 \\ 362-695 \\ 362-695 \end{array} \end{aligned}$ | $\begin{array}{r} 4000 \\ 10000 \\ 20000 \end{array}$ | $\begin{aligned} & 30-90 \\ & 30-90 \\ & 30-90 \end{aligned}$ | $\begin{array}{r} 72-108 \\ 102-695 \\ 362.695 \\ \hline \end{array}$ | $\begin{aligned} & 24-36 \\ & 34-52 \\ & 46-68 \end{aligned}$ |
| $7 \mathrm{EP4}$ | 6.3 | 0.6 | 7 | 15-1/2 | Nedium Shell Magnal 11 Pin | 11N | White | Medium | 1500 | 3300 | $\ldots$ | 700 | 2500 | 650 | $\ldots$ | 36-84 | 110 | 95 |
| $7{ }^{7} \mathrm{PP}_{4}$ | 6.3 | 0.6 | 7 | 14-1/2 | Medium Shell Diheptal 12 Pin | 146 | White | Medium | 1500 | 4000 | $\cdots$ | 500 | 3000 | 810-1200 | $\ldots$ | 36-84 | 93-123 | 75-102 |
| $\begin{aligned} & \text { 7JP1 } \\ & \text { 7JP4 } \\ & \hline \end{aligned}$ | 6.3 | 0.6 | 7 | 14-1/2 | $\begin{array}{\|l} \hline \text { Medium Shell } \\ \text { Diheptal } 12 \text { Pin } \end{array}$ | 146 | Green White | $\begin{aligned} & \text { Medium } \\ & \text { Medium } \end{aligned}$ | 2800 | 6000 | $\cdots$ | 750 | 6000 | 1620-2400 | $\ldots$ | 72-168 | 186-246 | 150-204 |
| 8EP4 | 6.3 | 0.6 | 8-3/4 | 16-1/2 | Medium Shell Diheptal 12 Pin | 146 | White | Medium | 3100 | 6600 | $\ldots$ | 750 | 6000 | 2000 | $\cdots$ | 72-168 | 146-198 | 124-198 |
| 9 NPI | 2.5 | 2.1 | 9 | 21 | Medium 6 Pin | 6EN | Green | Medium | 1500 | 5500 | .... | 1500 | 5000 | 1150 | $\ldots$ | 45-135 | 190 | 175 |

- Cut-off voltage. Supply should be edjustable from 0 to value shown.
*- Borey value for focus. Voltage should be adjustable about value shown.
Courtesy Sylvania Electric Producta Inc.
electrostatic types-cathode ray tubes

| Type | Heater |  | Nominal Dimensions |  | Base | $\begin{gathered} \text { RMA } \\ \text { Basing } \end{gathered}$ | Screen |  | Maximum lesigu Center Ratings |  |  |  | Typical Operating Conditions |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | DiameterInches | Length Inchies |  |  | Fluorescence | Peraistence | Anode il Volts | Anode 2 <br> Volts | Anode $\# 3$ Volts | $\begin{aligned} & \text { Anode } \# 2 \text { to } \\ & \text { Deflectinn } \\ & \text { Flate. } \\ & \text { Peok Volis } \end{aligned}$ | Anode ${ }^{2} 2$ Volte | $\left\|\begin{array}{c} \text { Anode \#1 } \\ \text { Avz. .olta } \end{array}\right\|$ | Anode \#3 Volts | Grid Range | $\begin{array}{\|c\|} \hline \text { Deflection } \\ \text { Ave. Volts DC/Inch } \\ \hline \end{array}$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | D 1-2 | D 3.4 |
| 10GP4 | 6.3 | 0.6 | 10 | 18-1/2 | Medium Shell <br> Diheptal 12 Pin | 146 | White | Medium | 2000 | 5000 | . | 500 | $\begin{aligned} & 4500 \\ & 5000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1130-1660 \\ & 1250-1850 \\ & \hline \end{aligned}$ | $\ldots$ | $\begin{array}{r} 54-126 \\ 60-140 \\ \hline \end{array}$ | $\begin{array}{\|l\|l\|} 112-149 \\ 125-165 \\ \hline \end{array}$ | $\begin{array}{r} 90-127 \\ 100-135 \\ \hline \end{array}$ |
| 101 P 4 | 6.3 | 0.6 | 10 | 19-1/4 | Medium Sliell Mineptal $12 \mathrm{P}_{\mathrm{in}}$ | 145 | White | 4edium | 2 non | 5000 | $\cdots$ | 600 | $\begin{aligned} & 414001 \\ & 5000 \end{aligned}$ | $\begin{array}{r} 960-1440 \\ 1200-1800 \\ \hline \end{array}$ | $\begin{aligned} & \hline \ldots . \\ & \ldots \end{aligned}$ | $\begin{array}{r} 48-112 \\ 60-140 \\ \hline \end{array}$ | $\begin{array}{\|r\|} \hline 88-120 \\ 110-150 \\ \hline \end{array}$ | $\begin{aligned} & \hline 68-92 \\ & 85-115 \end{aligned}$ |
| 12PP7 | 6.3 | 0.6 | 12 | 24 | Aledjum Slie II Dilieptale 12 Pin | 14 F . | Characteristics of Hiosphor No. 7 |  | 2000 | 4000 | 8000 | 1000 | 2000  <br> 4000  <br> 3000  <br> 4000  | $\begin{array}{r} 625 \\ 1250 \\ 937 \\ 1250 \end{array}$ | $\begin{aligned} & 4000 \\ & 4000 \\ & 4000 \\ & 8000 \end{aligned}$ | $\begin{aligned} & 30-90 \\ & 30-90 \\ & 30-90 \\ & 30-90 \end{aligned}$ | $\begin{array}{r} 55 \\ 83 \\ 110 \\ \hline \end{array}$ | $\begin{array}{r} 63 \\ 94 \\ 125 \end{array}$ |
| 126P7 | 6.3 | 0.6 | 12 | 22 | Medium Shell Diheptal 12 Pin | 148 | Characteristics of Phosphor No. 7 |  | 2000 | 4000 | 600 n | 1000 | $\begin{aligned} & 3000 \\ & 3000 \\ & 4000 \\ & 4000 \end{aligned}$ | $\begin{array}{r} 857 \\ 857 \\ 1143 \\ 1143 \end{array}$ | $\begin{aligned} & 3000 \\ & \text { K000 } \\ & 4000 \\ & 6000 \end{aligned}$ | $\begin{aligned} & \text { 49-147 } \\ & \text { 49-147 } \\ & 65-195 \\ & 65-199 \end{aligned}$ | $\begin{array}{r} 73 \\ 89 \\ 97 \\ 108 \end{array}$ | $\begin{array}{r} 68 \\ 83 \\ 91 \\ 101 \end{array}$ |
| 124P1 | 6.3 | 0.6 | 12 | 23-1/2 | Medium Mapral 11 Pin, Sleeve | 11 J | Green | Medium | 1500 | 5510 | $\ldots$ | 10 m | 5000 | $\begin{gathered} 1150 \\ +25 \% \\ -30 \% \end{gathered}$ | .... | 45-135 | 19 | 25 |
| $\begin{aligned} & 144 \mathrm{Pl} \\ & 14 \mathrm{AP4} \\ & \hline \end{aligned}$ | 2.5 | 2.1 | 13-3.8 | 24-1/4 | $\begin{array}{\|l\|} \hline 12 \text { Pin } \\ \text { Peripheral Contact } \\ \hline \end{array}$ | $\begin{aligned} & \hline 12 \mathrm{~A} \\ & 12 \mathrm{~A} \\ & \hline \end{aligned}$ | Green Minte | Mledium Medium | 1800 | 400 | 8000 | .... | $\begin{aligned} & 2000 \\ & 40 \mathrm{~m} \\ & \hline \end{aligned}$ | $\begin{aligned} & 500 \\ & 1000 \end{aligned}$ | $\begin{aligned} & 4000 \\ & 8000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 20-60 \\ & 40-120 \end{aligned}$ | $\begin{array}{r} 65 \\ 130 \end{array}$ | $\begin{array}{r} 65 \\ 130 \\ \hline \end{array}$ |
| $\begin{aligned} & \hline 20 \mathrm{API} \\ & 20 \mathrm{AP} 4 \end{aligned}$ | $\begin{aligned} & 2.5 \\ & 2.5 \end{aligned}$ | $\begin{aligned} & 2.1 \\ & 2.1 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | $\begin{array}{\|l\|} \hline 27-7 / 8 \\ 27-7 / 8 \end{array}$ | $\begin{aligned} & 12 \text { Pin } \\ & \text { Periplieral Contact } \end{aligned}$ | $\begin{aligned} & \hline 12 \mathrm{~A} \\ & 12 \mathrm{~A} \end{aligned}$ | Green White | Medium Medium | $\begin{aligned} & 1800 \\ & 1800 \end{aligned}$ | $\begin{aligned} & 4000 \\ & 4000 \end{aligned}$ | $\begin{aligned} & 8000 \\ & 8000 \end{aligned}$ | $\cdots$ | 2000 <br> 4000 <br> 2000 <br> 4000 | $\begin{array}{r} 500 \\ 1000 \\ 500 \\ 1000 \\ \hline \end{array}$ | $\begin{aligned} & 4000 \\ & 8000 \\ & 4000 \\ & 8000 \end{aligned}$ | $\begin{aligned} & 200-60 \\ & 40-120 \\ & 20-60 \\ & 40-120 \end{aligned}$ | $\begin{array}{r} 5.5 \\ 110 \\ 65 \\ 130 \end{array}$ | $\begin{array}{r} 55 \\ 110 \\ 65 \\ 130 \end{array}$ |
| 902 | 6.3 | 0.6 | 2 | 7-1/2 | $\begin{aligned} & \text { Sedium Shell } \\ & \text { Octal B Pin } \end{aligned}$ | 8(1) | Greea | ${ }^{\text {Hed }}$ Iediur | 3 c | 600 | $\ldots$ | 347 | $\begin{aligned} & 400 \\ & 600 \end{aligned}$ | $\begin{aligned} & 100 \\ & 150 \end{aligned}$ | $\ldots$ | $\begin{aligned} & 20-60 \\ & 30-90 \\ & \hline \end{aligned}$ | $\begin{array}{r} 93 \\ 139 \end{array}$ | $\begin{array}{r} 78 \\ 117 \\ \hline \end{array}$ |
| 902-A | 6.3 | 0.6 | 2 | 7-7/16 | Medium She 11 Octal 8 Pin | 8 CD | Green | Medium | 300 | \%on | $\ldots$ | 347 | $\begin{gathered} 400 \\ 600 \end{gathered}$ | $\begin{aligned} & 1000 \\ & 150 \end{aligned}$ | $\cdots$ | $\begin{aligned} & \hline 20-60 \\ & 30-90 \\ & \hline \end{aligned}$ | $\begin{array}{r} 93 \\ 139 \end{array}$ | $\begin{array}{r} 78 \\ 117 \\ \hline \end{array}$ |
| $\begin{aligned} & 905 \\ & 907 \\ & 909 \end{aligned}$ | 2.5 | 2.1 | 5-1.4 | 16-1/2 | $\begin{aligned} & \hline \text { Lmp She II } \\ & \text { Medium } 5 \text { Pin Micenol } \end{aligned}$ | $\begin{aligned} & 5 R P^{\prime} \\ & 5 R P \\ & 5 R P \end{aligned}$ | Creen Blue Bluish-White | $\begin{array}{\|c\|} \hline \text { Nedium } \\ \text { Very Shott } \\ \text { Long } \end{array}$ | 600 | 2000 | .... | 10 m | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 338 \\ & 450 \end{aligned}$ | $\cdots$ | $\begin{gathered} 13-39 \\ 17.5-52.5 \end{gathered}$ | $\begin{array}{r} 86 \\ 115 \end{array}$ | $\begin{aligned} & 73 \\ & 97 \end{aligned}$ |
| 905-A | 2.5 | 2.1 | 5-1/4 | 16-1/2 | $\begin{array}{\|l} \hline \text { Long She Il } \\ \text { Medjum } 5 \text { Pin Aticanol } \\ \hline \end{array}$ | 58 B | Freen | Medium | 600 | 2000 | .... | 10007 | $\begin{aligned} & 1500 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 338 \\ & 450 \end{aligned}$ | $\ldots$ | $\begin{array}{r} 13-39 \\ 17.5-52.5 \\ \hline \end{array}$ | $\begin{array}{r} 86 \\ 115 \\ \hline \end{array}$ | $\begin{aligned} & 73 \\ & 97 \end{aligned}$ |
| $\begin{aligned} & 908 \\ & 910 \end{aligned}$ | 2.5 | 2.1 | 3 | 11-1/2 | Medium 7 Pin | $\begin{aligned} & \text { 7AN } \\ & \text { 7AN } \end{aligned}$ | $\begin{array}{c\|} \hline \text { Rluish } \\ \text { Bluish-White } \end{array}$ | Very Short Long | 1000 | 1500 | $\ldots$ | 60n | 600 <br> 800 <br> 100 <br> 1200 <br> 1500 <br> 10 | $\begin{aligned} & 170 \\ & 230 \\ & 285 \\ & 345 \\ & 475 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 13-46 \\ & 30-70 \end{aligned}$ | $\begin{gathered} 46.3 \\ 62 \\ 77 \\ 94 \\ 115.2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 44 \\ 57.8 \\ 72.5 \\ 88 \\ 110 \\ \hline \end{gathered}$ |
| 908-A | 2.5 | 2.1 | 3 | 11-1/2 | Medium 7 Pin | 7CE | Blue | Very Short | 1000 | 1500 | $\cdots$ | 500 | $\begin{aligned} & \hline 1000 \\ & 1500 \\ & \hline \end{aligned}$ | $\begin{array}{r} 287 \\ 430 \\ \hline \end{array}$ | $\ldots$ | $\begin{gathered} 16.5-49.5 \\ 25-75 \\ \hline \end{gathered}$ | $\begin{array}{r} 76 \\ 114 \\ \hline \end{array}$ | $\begin{array}{r} 73 \\ 109 \\ \hline \end{array}$ |
| 912 | 2.5 | 2.1 | 5-1.4 | 16-1/2 | $\begin{aligned} & \text { Medium } \\ & 5 \text { Pin Micanol } \end{aligned}$ | 912 | Green | Medium | 4500 | 1500 | $\cdots$ | 7000 | $\begin{array}{r} 5000 \\ 10,000 \\ 15,000 \\ \hline \end{array}$ | $\begin{aligned} & 1000 \\ & 2000 \\ & 3000 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 27-81 \\ & 31-93 \\ & 35-105 \end{aligned}$ | $\begin{aligned} & 306 \\ & 620 \\ & 910 \\ & \hline \end{aligned}$ | $\begin{aligned} & 248 \\ & 498 \\ & 745 \\ & \hline \end{aligned}$ |
| 913 | 6.3 | 0.6 | 1-5/8 | 4-3/4 | $\begin{aligned} & \text { Small Wafer Octal } \\ & \text { B Pin } \\ & \hline \end{aligned}$ | 913 | Green | Medium | 200 | 500 | $\ldots$ | 250 | $\begin{gathered} 25 n \\ 50 \end{gathered}$ | $\begin{gathered} 50 \\ 100 \\ \hline \end{gathered}$ | $\ldots$ | $\begin{aligned} & 10-30 \\ & 32-98 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 169 \\ & 363 \\ & \hline \end{aligned}$ | $\begin{aligned} & 121 \\ & 254 \\ & \hline \end{aligned}$ |
| 914 | 2.5 | 2.1 | 9-1/4 | 21-1/2 | Medium 6 Pin | ${ }^{6 B F}$ | Green | Hedium | 1900 | 2000 | $\cdots$ | 3 mon | $\begin{aligned} & 1500 \\ & 2500 \\ & 5000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{array}{r} 300 \\ 515 \\ 1030 \\ 1450 \end{array}$ |  | $\begin{aligned} & 25-75 \\ & 25-75 \\ & 25-75 \\ & 25-75 \end{aligned}$ | $\begin{aligned} & 75 \\ & 124.5 \\ & 248 \\ & 348 \\ & \hline \end{aligned}$ | $\begin{gathered} 58.7 \\ 97.8 \\ 195 \\ 274 \\ \hline \end{gathered}$ |
| 914A | 2.5 | 2.1 | 9-1/4 | 20-1/1K | Medium 6 Pin | 914A | Gireen | Nedium | 1900 | 7 non | $\ldots$ | 3000 | 1500 <br> 2500 <br> 5000 <br> 7000 | $\begin{array}{r} 320 \\ 550 \\ 1100 \\ 1550 \\ \hline \end{array}$ |  | $\begin{aligned} & 25-75 \\ & 25-75 \\ & 25-75 \\ & 25-75 \\ & \hline \end{aligned}$ | 69.5 <br> 115 <br> 231 <br> 323 | $54 . \mathrm{K}$ <br> 91 <br> 182 <br> 254 |
| $\begin{aligned} & \hline \mathrm{VCR} \\ & 139 \mathrm{~A} \end{aligned}$ | 4.0 | 1.1 | 2-3/4 | 7-7/8 | Furopean | $\begin{aligned} & \hline \mathrm{VCR} \\ & 139 \mathrm{n} \end{aligned}$ | Green | Medium | 1000 | 1000 | .... |  | $\mathrm{BnO}_{1}$ | 120-150 | $\cdots$ | 7-16 | 104 | 140 |


| Type | Heater |  | Pulb |  |  |  |  |  | $\left\|\begin{array}{c} \text { Ion } \\ \text { Trap } \\ \text { Requi i ed } \end{array}\right\|$ | Base | $\begin{aligned} & \text { RMA } \\ & \text { Basing } \end{aligned}$ | unf Filter Capacitance Provided by Bull Coating | $\begin{aligned} & \text { Deflection } \\ & \text { and } \\ & \text { Focusing } \\ & \text { Me thod } \end{aligned}$ | Maximum Design Center Ratings |  | Typical Operation |  |  | $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | Nominal Face Dimensions in Inches | $\begin{aligned} & \text { Lengetli } \\ & \text { in } \\ & \text { Haclies } \end{aligned}$ | $\begin{gathered} \text { Con- } \\ \text { struction } \end{gathered}$ | Terminal | $\begin{aligned} & \text { Face } \\ & \text { Plate } \\ & \text { Color } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Deflection } \\ \text { Anale } \\ \text { in Uepreses } \\ \text { (Noce 1) } \end{array}$ |  |  |  |  |  | $\left(\left.\begin{array}{l} \text { Anode } \\ \text { Volts } \end{array} \right\rvert\,\right.$ | Accelerator Grid Volts | $\begin{aligned} & \text { Anode } \\ & \text { Volts } \end{aligned}$ | $\begin{aligned} & \text { Acceler- } \\ & \text { ator } \\ & \text { Grid } \\ & \text { Volts } \end{aligned}$ |  |  |
| 3HP7 | 6.3 | 0.6 | 3 Diam. | 9-13/16 | Glass | Snap | Clear | 55 | None | Medium Shell $\text { Octal } 8 \mathrm{Pin}$ | 5AN | None | Mapnetic | 5000 | 200 | $\begin{aligned} & \hline 4000 \\ & 5000 \end{aligned}$ | $\begin{aligned} & \hline 150 \\ & 150 \end{aligned}$ | $\begin{aligned} & 15-45 \\ & 15-45 \end{aligned}$ | 3HP7 |
| $3{ }^{3} \mathrm{P} 4$ | 6.3 | 0.6 | 2-9/16 Diam. | 10 | Cilass | Recessed Small Ball | Clear | 42 | None | Special 5 Pin | 3 NP 4 | 275 Min, 375 Max. | Marnetic | 25000 | $\cdots$ | 24000 | $\ldots$ | 60 | 3NP4 |
| $5_{5 \times P 4}{ }^{4}$ | 6.3 | 0.6 | 5 Diam. | 11-1/8 | Glass | Hecessed Small Ball | Clear | 53 | None | $\begin{aligned} & \text { Medium Shell } \\ & \text { Octal \& Pin } \\ & \hline \end{aligned}$ | 8 BX | None | Magnetic | 8000 | 300 | 6000 | 250 | 45 | 5FP4A |
| 5FP7A | 6.3 | 0.6 | 5 Diam. | 11-1/2 | Glass | $\begin{aligned} & \text { Fecessed } \\ & \text { Small Ball } \end{aligned}$ | Clear | 53 | None | Medium Sliell Octal 8 Pin | 8BX | None | Mapnetic | B000 | 700 | $\begin{array}{r} 4000 \\ 7000 \\ \hline \end{array}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{array}{r} 25-70 \\ 25-70 \\ \hline \end{array}$ | 5FP7A |
| $5 \mathrm{FP7}$ | 6.3 | 0.6 | 5 Diam. | 11-1/8 | Glass | Snap | Clear | 55 | None | Small Wafer Octal 8 Pin with Sleeve | SAN | None | Magnetic | 7000 | 300 | $\begin{aligned} & 4000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{array}{r} 25-75 \\ 25-75 \\ \hline \end{array}$ | 5FP7 |
| 5FP14 | 6.3 | 0.6 | 5 Diam. | 11-1/8 | Glass | Snap | Clear | 55 | None | Small Wafer Octal 8 Pin with Sleeve | 5AN | None | Marnetic | 7000 | 700 | $\begin{array}{r} 4000 \\ 7000 \\ \hline \end{array}$ | $\begin{array}{r} 250 \\ 250 \\ \hline \end{array}$ | $\begin{aligned} & 25-75 \\ & 25-75 \\ & \hline \end{aligned}$ | $5 \mathrm{FP14}$ |
| $5 \mathrm{FP}_{4}$ | 6.3 | 0.6 | 5 Diam. | 11-3/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cayity } \end{aligned}$ | Clear | 50 | None | $\begin{aligned} & \text { Medium Shell } \\ & \text { Diheptal } 12 \mathrm{Pin} \end{aligned}$ | 12C1 | 100 Min, 500 Max. | Note 2 | 27000 | 350 | 27000 | 200 | 70 | $5 \mathrm{PP}_{4}$ |
| 5WP15 | 6.3 | 0.6 | 5 Diam. | 11-7/16 | Glass | $\begin{aligned} & \text { Mecessed } \\ & \text { Small Covity } \end{aligned}$ | Clear | 50 | None | $\begin{aligned} & \text { Small She 11 } \\ & \text { Duodecal } 7 \text { Pin } \\ & \hline \end{aligned}$ | 12 Cl | $100 \mathrm{Min}, 500 \mathrm{Max}$. | Note 2 | 27000 | 350 | 20000 | 200 | 70 | 5WP15 |
| $7 \mathrm{AP4} 4$ | 2.5 | 2.1 | 7-1/8 Diam. | 13-1/2 | Glass | None | Clear | 55 | None | Medium 5 Pin | 5AJ | None | Note 2 | 35000 | No Grid | 35000 | No Grid | 67.5 | $7 \mathrm{PP4}$ |
| ${ }^{7} \mathrm{FP} 1$ | 6.3 | 0.6 | 7 Diam. | 13-1/4 | Glass | Snap | Clear | 55 | None | $\begin{aligned} & \text { Octal } 8 \text { Pin } \\ & \text { with Sleeve } \\ & \hline \end{aligned}$ | 5AN | None | Mapnetic | 7000 | 675 | $\begin{aligned} & 4000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \\ & \hline \end{aligned}$ | 78P1 |
| 7BP7 | 6.3 | 0.6 | 7 Diam. | 13-1/4 | Gilass | Snap | C.lear | 55 | None | Octal 8 Pin with Sleeve | 5AN | None | Magnetic | 7000 | 300 | $\begin{aligned} & 4000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{array}{r} 50 \\ 50 \\ \hline \end{array}$ | $7 \mathrm{PP7}$ |
| $7 \mathrm{PP7} 7$ | 6.3 | 0.6 | 7 Diam. | 13-1/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Ball } \end{aligned}$ | Clear | 53 | None | Medium Shell $\text { Octal } 8 \text { Pin }$ | 8B入 | None | Magnetic | 8000 | 700 | $\begin{aligned} & 4000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{aligned} & 25-70 \\ & 25-70 \\ & \hline \end{aligned}$ | $78 P 7 \mathrm{~A}$ |
| $7{ }^{\text {CP1 }}$ | 6.3 | 0.6 | 7 niam. | 13-7/16 | Glass | Snap | Clear | 57 | None | Medium Shell Octal 8 Pin | 6 AZ | None | Note 2 | 8000 | 300 | $\begin{aligned} & 4000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{array}{r} 250 \\ 250 \\ \hline \end{array}$ | $\begin{array}{r} 45 \\ 45 \\ \hline \end{array}$ | 7 CP 1 |
| $7 \mathrm{CP4}$ | 6.3 | 0.6 | 7 Diam. | 13-7/16 | Ginss | $\begin{aligned} & \text { Recessed } \\ & \text { Small Ball } \\ & \hline \end{aligned}$ | Clear | 57 | None | $\begin{aligned} & \text { Medium Shell } \\ & \text { Octal } 8 \text { Pin } \end{aligned}$ | 6 AZ | None | Note 2 | 8000 | 300 | 6000 | 250 | 45 | ${ }_{7} \mathrm{CP}_{4}$ |
| 7 DP 4 | 6.3 | 0.6 | 7-3/16 Diam. | 14-1/16 | Glass | $\begin{array}{l\|} \hline \text { Recessed } \\ \text { Sinall Cavity } \\ \hline \end{array}$ | Clear | 50 | Double | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal ? Pin } \\ \hline \end{array}$ | 12:2 | $400 \mathrm{Min}, 1500$ Nax. | Note 2 | 8000 | 410 | 6000 | 250 | 45 | 7DP4 |
| $7 \mathrm{HP4}$ | 6.3 | 0.6 | 7-3/16 Jiam. | 13 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Ball } \\ & \hline \end{aligned}$ | Clear | 50 | None | Small Shell Duodecal 7 Pin | 1202 | 500 Max. | Magnetic | 8000 | 410 | 6000 | 250 | 33-77 | $7 \mathrm{HP4}$ |
| 8AP4 | 6.3 | 0.6 | 8-1/2 Diam. | 14-1/4 | Hecal | Cone Lip | Clear | 54 | Sinple | Small Shell Duodecal 7 Pin | 12H | None | Marnetic | 10000 | No Grid | 9000 | No Grid | 27-63 | $8 \mathrm{APP}_{4}$ |
| $8 \mathrm{AP4A}$ | 6.3 | 0.6 | ${ }^{8-1 / 2 ~ D i a m . ~}$ | 14-1/4 | Metal | Cone Lip | Gray | 54 | Single | Small Shell Duodecal 5 Pin | 12H | None | Magnetic | 9000 | No Grid | 7000 | No Girid | 27-63 | 8AP4A |
| $9 \mathrm{AP4}$ | 2.5 | 2.1 | 9-1/8 Пiam. | 21 | Glass | Cap | C.lear | 40 | None | Medium 6 Pin | 6 AL | None | Note 2 | 7000 | 250 | $\begin{aligned} & 6000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | $9 \mathrm{AP4}$ |
| ${ }_{9} \mathrm{CP} 4$ | 2.5 | 2.1 | 9 Diam. | 15-7/8 | Glass | Cap | Clear | $\cdots$ | Nosie | 6 Pin Base | 4 AF | None | Magnetic | 7000 | No Grid | $\begin{aligned} & 6000 \\ & 7000 \end{aligned}$ | No Grid | $\begin{array}{r} 90 \\ 100 \\ \hline \end{array}$ | $9^{\text {CP4 }}$ |
| $9{ }^{(1) 7}$ | 6.3 | n.f | 9 Diam. | 17 | Glass | Cap | Clear | 55 | None | $\begin{aligned} & \text { Octal 8 Pin } \\ & \text { with Sleeve } \end{aligned}$ | 5AN | None | Magnetic | 7000 | 300 | $\begin{aligned} & 4000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | 96P7 |
| 9.JP1 | 2.5 | 2.1 | 9 Diam. | 15-11/16 | Filass | Snap | Clear | 55 | None | Small Wafer Octal <br> 8 Pin witi Sleeve | 88月 | None | Note 3 | 5000 | No Grid | $\begin{aligned} & 2500 \\ & 5000 \\ & \hline \end{aligned}$ | No Grid | $\begin{array}{r} 45 \\ 90 \\ \hline \end{array}$ | 9.P1 |
| $91{ }^{9} 7$ | 6.3 | 0.6 | ${ }^{4}$ Diam. | 14-31/32 | Glass | Cap | Clear | 55 | None | Octal 8 Pin with Sleeve | 5 AN | None | Mapnetic | 7000 | 300 | 4000 4000 7000 7000 | $\begin{aligned} & 250 \\ & 125 \\ & 250 \\ & 125 \end{aligned}$ | $\begin{aligned} & 55-105 \\ & 30-50 \\ & 60-100 \\ & 30-50 \end{aligned}$ | 9LP7 |
| 9MP7 | 6.3 | 0.6 | 9 niam. | 17-1/2 | Glass | Cap | Clear | 55 | None | $\begin{aligned} & \text { Octal } 8 \text { Pin } \\ & \text { with Sleeve } \\ & \hline \end{aligned}$ | 5 AN | None | Magnetic | 7000 | 300 | $\begin{aligned} & 4000 \\ & 6000 \end{aligned}$ | 250 | 25-75 | 9\%P7 |
| 10 BP 4 | 6.3 | 0.6 | 10-1.2 Diam. | 17-5/8 | Glass | $\begin{aligned} & \hline \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Clear | 50 | Double | $\begin{aligned} & \text { Small She } 11 \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 1212 | $500 \mathrm{Min}, 2500 \mathrm{Mlax}$. | Magnetic | 10000 | 410 | 9000 | 250 | 20-60 | 10BP4 |
| 10BP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 10 BP 4 A |
| $10 \mathrm{CP4}$ | 6.3 | 0.6 | 10-1/2 Diam. | 16-5/8 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Ball } \end{aligned}$ | Clear | 50 | None | $\begin{aligned} & \text { Sinall Slie } 11 \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12 D 2 | 50 Max . | Mapnetic | 11000 | 410 | 8000 | 250 | 30-66 | ${ }_{10 \mathrm{CP}}$ |

magettic type cathode ray tubes

| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Heater |  | Rulb |  |  |  |  |  | $\left.\begin{array}{\|c\|} \text { Ion } \\ \text { Trap } \\ \text { Resui red } \end{array} \right\rvert\,$ | Base | $\begin{array}{c\|} \text { RMA } \\ \text { Basing } \end{array}$ | ниf Filter Capacitance Provided by Bulb Coatinp | $\begin{aligned} & \text { Deflection } \\ & \text { and } \\ & \text { Focusing } \\ & \text { Metliod } \end{aligned}$ | Maximum DesianCienter Hatings |  | Typical Operation |  |  | $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | Nominal Face Dimensions in laclies | $\begin{aligned} & \text { Lengeth } \\ & \text { inches } \\ & \text { nach } \end{aligned}$ | Construction | Termical | Face Plate Color | $\begin{gathered} \hline \text { De Clection } \\ \text { Ansle } \\ \text { in Deprees } \\ \text { (Note 1) } \\ \hline \end{gathered}$ |  |  |  |  |  | $\begin{array}{\|c\|} \text { Anode } \\ \text { Volts } \end{array}$ | Accelerator Grid Volts | $\begin{array}{\|l\|l\|} \hline \\ \text { Anode } \\ \text { Volts } \end{array}$ | $\square$ |  |  |
| 10DP4 | 6.3 | 0.6 | 10-1/2 Diam. | 17-5/8 | Glas: | Recessed Small Cavity | Clear | 50 | None | Small Shell <br> 「Modecal 7 Pin | 12 C 3 | None | Note 2 | 10000 | 410 | 9000 | 250 | 36-84 | 100P4 |
| 10EP4 | 6.3 | 0.6 | 10-1/2 lisam. | 17-5/8 | Glass | Snap | Clear | 50 | Double | Sma 11 She 11 Duodecal 7 Pin | 12 n | . $\cdot$. | Magnetic | 11000 | 330 | 8000 | 250 | 20-65 | $10 \mathrm{EP4}$ |
| 10 FP 4 | 6.3 | 0.6 | 10-1/2 Diam. | 17-5/8 | Glass | Hecessed Small Cavity | Clear | 50 | None | $\begin{aligned} & \text { Sma1d She 11 } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12 Cl | 500 Min, 2500 Max. | Mapnetic | 10000 | 410 | 9000 | 250 | 27-63 | 10FP4 |
| 10KP7 | 6.3 | 0.6 | 10-1/2 Diam. | 17-5/8 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Clear | 50 | None | Small Shel! Duodecal 7 Pin | 1201 | None | Magre Cic | 10000 | 200 | $\begin{aligned} & 7000 \\ & 9000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ | $\begin{aligned} & 27-63 \\ & 27-63 \end{aligned}$ | 10KP7 |
| $10 \mathrm{MP4}$ | 6.3 | 0.5 | 10-1/2 Diam. | 17 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Clear | 52 | Double | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal } 5 \text { Pin } \\ \hline \end{array}$ | 12 G | 500 Min, 2500 Max. | Mapnetic | 10000 | No Grid | 9000 | No Grid | 27-63 | 10WP4 |
| 10MP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 10MPM |
| 12AP4 | 2.5 | 2.1 | 12-1/16 Diam. | 25-3/8 | Glass | Cap | Clear | 40 | None | Medium 6 Pin | ${ }^{6} \mathrm{AL}$ | None | Note 2 | 7000 | 250 | $\begin{aligned} & 6000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{array}{r} 250 \\ 250 \\ \hline \end{array}$ | $\begin{aligned} & 75 \\ & 75 \\ & \hline \end{aligned}$ | 12NP4 |
| $12 \mathrm{CP4}$ | 2.5 | 2.1 | 12-1/16 Diam. | 18-5/8 | Glass | Cap | Clear | . ${ }^{\text {a }}$ | None | 6 Pin Base | 4 AF | None | Mamnetic | 7000 | No Grid | $\begin{aligned} & 6000 \\ & 7000 \end{aligned}$ | No Grid | $\begin{array}{r} 90 \\ 110 \\ \hline \end{array}$ | 12CP4 |
| 121)7 | 6.3 | 0.6 | 12 Diam. | 20-3/4 | Glass | Medium Cap | Clear | 55 | None | Small Wafer Octal 8 Pin with Sleeve | 5N0 | None | Mametic | 7000 | 300 | $\begin{aligned} & 4000 \\ & 7000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ | $\begin{aligned} & 25-75 \\ & 25-75 \end{aligned}$ | 120P7 |
| 120P7A | 6.3 | 0.6 | 12 Diam. | 19-5/8 | Glass | Medium Cap | Clear | 50 | None | $\begin{array}{\|l\|} \hline \begin{array}{l} \text { Medium Shell Octal } \\ \text { B Pin } \end{array} \\ \hline \end{array}$ | 8 Ba | None | Magnetic | 10000 | 700 | $\begin{aligned} & 4000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{array}{r} 250 \\ \\ \hline \end{array}$ | $\begin{aligned} & 25-70 \\ & 25-70 \\ & \hline \end{aligned}$ | 12DP7A |
| 12JP4 | 6.3 | 0.6 | 12 Diam. | 17-1/2 | Glasa | Snap | Clear | 50 | None | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal } ; \text { Pin } \\ \hline \end{array}$ | 12D1 | None | Magnetic | 12000 | 410 | 10000 | 250 | 27-63 | 12JP4 |
| $12 \mathrm{KP4}$ | 6.3 | 0.6 | 12-7/16 Diem. | 17-5/8 | Glase | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Clear | 54 | None | $\begin{aligned} & \text { Small She I1 } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 1212 | 500 Min, 2500 Max. | Magnetic | 12000 | 410 | 10000 | 250 | 27-63 | 12KP4 |
| 12KP4A | 6.3 | 0.6 | 12-7/16 Diam. | 17-5/8 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Gray | 54 | None | Small She 11 <br> Duodecsl 5 Pin | 1202 | $500 \mathrm{Min}, 2500 \mathrm{Max}$. | Magnetic | 12000 | 410 | 11000 | 250 | 27.63 | 12 KPMA |
| 12 P 4 | 6.3 | 0.6 | 12-7/16 Diam. | 18-3/4 | Glass | Receased Small Cavity | Clear | 54 | Double | $\begin{aligned} & \text { Simall She ll } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1212 | 750 Min, 3000 Max. | Magnetic | 12000 | 410 | 11000 | 250 | 27-63 | 12194 |
| 121P4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | $12 \mathrm{LP4}$ |
| $12 \mathrm{PP}_{4}$ | 6.3 | 0.6 | 12-7/16 Diam. | 17-1/2 | Glas: | Receased <br> Small Ball Cap | Clear | 55 | Sinple | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 1201 | None | Magnetic | 12000 | 410 | 10000 | 250 | 27-63 | 120P4 |
| 120P4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 120 P 4 A |
| 12RP4 | 6.3 | 0.6 | 12 Diam. | 17-1/2 | Giass | Recessed <br> Small Ball Cap | Clear | 56 | Sinple | $\begin{aligned} & \text { Small Shell } \\ & \text { 1) odecal } 7 \text { Pin } \end{aligned}$ | $12 \mathrm{D2}$ | $\cdots$ | Magnetic | 12000 | 410 | 10000 | 250 | 27-63 | 12RP4 |
| 12SP7 | 6.3 | 0.6 | 12-7/16 Diam. | 18-3/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Carity } \\ & \hline \end{aligned}$ | Clear | 55 | None | $\begin{array}{\|l\|} \hline \text { Small She } 11 \\ \text { Duodecal } 7 \text { Pin } \\ \hline \end{array}$ | 1201 | None | Magnetic | 10000 | 410 | 9000 | 250 | 27-63 | 12SP7 |
| 12TP4 | 6.3 | 0.6 | 12-7/16 Diam. | 18-3/4 | Glase | Recessed Small Carity | Clear | 54 | Double | $\begin{aligned} & \text { Smal1 Shell } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12D1 | None | Magnecic | 12000 | 410 | 11000 | 250 | 27-63 | 12TP4 |
| 12LP4 | 6.3 | 0.6 | 12-7/16 Diam. | 18-5/8 | Metal | Cone Lip | Clear | 54 | Double | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 1203 | None | Magnetic | 12000 | 410 | 11000 | 250 | 27-63 | 121P4 |
| 121P4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 12UP4 |
| 12UP4B |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 12LP48 |
| $12 \mathrm{VP4}$ | 6.3 | 0.6 | 12-3/8 Liam. | 18 | Gioss | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Clear | 55 | Double | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duoderal } 5 \text { Pin } \\ \hline \end{array}$ | 12G | $750 \mathrm{Min}, 3000$ Max. | Magnetic | 12000 | No Grid | 11000 | No Grid | 33-77 | 12VP4 |
| $12 \mathrm{VP4A}$ |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 12 VPM |
| 14BP4 | 6.3 | 0.6 | 12-1/2 $\times 9-11 / 16$ | 16-13/16 | Glats | Recessed Small Cavity | Gray | 65 | Double | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1202 | $500 \mathrm{Min}, 2000$ Max. | Magnetic | 12000 | 410 | 11000 | 250 | 27-63 | 14PP4 |
| $14{ }^{1} \mathrm{P}_{4}$ | 6.3 | 0.6 | 12-1/2 $\times 9$-11/16 | 16-3/4 | Glas: | Hecessed Small Cavity | Gray | 65 | Double | $\begin{array}{\|l\|} \hline \text { Small She } 11 \\ \text { Duodecal } 5 \text { Pin } \end{array}$ | 1202 | 1500 | Magnetic | 14000 | 410 | 12000 | 300 | 33-77 | $14 \mathrm{CP4}$ |
| 14DP4 | 6.3 | 0.6 | 12-1/2 $\times$ 9-11/16 | 16-3/4 | Gloss | Recessed Small Cavity | Gray | 65 | llouble | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal } 5 \mathrm{Pin} \\ \hline \end{array}$ | 12D1 | None | Magnetic | 14000 | 410 | 11000 | 250 | 27-63 | 140P4 |
| 15AP4 | 5.3 | 0.6 | 15-1/2 Hiam. | 20-1/2 | Glass | Recessed Small Ball | Clear | 52 | None | $\begin{array}{\|l\|} \hline \text { Small Shell } \\ \text { Duodecal } 7 \text { Pin } \\ \hline \end{array}$ | 12 G | None | Magnetic | 15000 | 410 | 12000 | 250 | 27-63 | 15194 |
| 15CP4 | 6.3 | 0.6 | 15-1/2 Diam. | 21-2,2 | Glass | Recessed Small Cavity | c.lent | 37 | Double | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12D1 | None | Mapnetic | 15000 | 410 | $\begin{array}{r} 9000 \\ 15000 \\ \hline \end{array}$ | $250+$ | 45 | 15CP4 |

magnetic type cathode ray tubes

| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Heater |  | Bult |  |  |  |  |  | $\left\|\begin{array}{c} \text { lon } \\ \text { Trap } \\ \text { Required } \end{array}\right\|$ | Base | $\operatorname{man}_{\text {Basing }}$ | $\mu \mu$ Filter Capacitance Provided by Bulb Coatinf | $\begin{gathered} \text { Deflection } \\ \text { and } \\ \text { Focusine } \\ \text { Merhod } \end{gathered}$ | Maximum Desien Center Ratings |  | Typical Operation |  |  | $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volts | Amperes | $\begin{gathered} \text { Nominal } \\ \text { Face } \\ \text { Dimensions } \\ \text { in Inches } \end{gathered}$ | $\begin{gathered} \text { Lenpth } \\ \text { in } \\ \text { Inches } \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Con- } \\ \text { struction } \end{gathered}\right.$ | Terminal | $\begin{aligned} & \text { Fuce } \\ & \text { Pluce } \\ & \text { Color } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { Heflection } \\ \text { Anple } \\ \text { in Werrees } \\ \text { (Note 1) } \\ \hline \end{gathered}$ |  |  |  |  |  | $\begin{array}{\|} \text { Anode } \\ \text { Yolct } \end{array}$ | Acceler- <br> ator <br> Grid <br> Volts | Anode Volta |  | Control <br> Grid <br> Negative <br> Volts |  |
| 15DP4 | 6.3 | 0.6 | 15-1/2 Diam. | 20-1/2 | Giass | Fiecessed <br> Small Ball Cap | Clear | 57 | Double | $\begin{aligned} & \text { Small Sliell } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1211 | Nane | Mapnetic | 15000 | 410 | 13000 | 250 | 27-63 | 150P4 |
| 16AP4 | 5.3 | 0.6 | 15-7/8 Diam. | 22-5/15 | Netal | Cone Lip | Clear | 53 | Doulle | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1203 | None | Mapnetic | 14000 | 410 | $\begin{array}{r} 9000 \\ 12000 \\ \hline \end{array}$ | $\begin{aligned} & 300 \\ & 300 \end{aligned}$ | $\begin{aligned} & \begin{array}{l} 33-77 \\ 33-77 \end{array} \end{aligned}$ | 16AP4 |
| 16AP4A |  |  |  |  |  |  | Gruy |  |  |  |  |  |  |  |  |  |  |  | 16AP4A |
| $16 \mathrm{CP}_{4}$ | 6.3 | 0.6 | 15-7/8 Diam. | 21-1/2 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \end{aligned}$ | Clear | 52 | Doulite | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 121 | None | Magnetic | 15000 | 410 | 12000 | 250 | 27-63 | 16CP4 |
| $16 \mathrm{DP4}$ | 6.3 | 0.6 | 15-7/8 Diam. | 20-3/4 | Glass | Hecessed Small Cavity | Clear | 60 | Double | Small Shell Muodecal 7 Pin | 1201 | Nane | Magnetic | 15000 | 410 | $\begin{array}{r} 9000 \\ 12000 \end{array}$ | 250 | 45 | 16DP4 |
| 16DP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 160P4A |
| 16FP4 | 6.3 | 0.6 | 15-7/8 Diam. | 19-5/8 | Metal | Cone Lip | Clear | 60 | Double | $\begin{aligned} & \text { Small She II } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1213 | None | Mapnetic | 14000 | 410 | 12000 | 300 | 33-77 | 16EP4 |
| 16FP44 |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 16EP4A |
| $16 \mathrm{FP}^{4} 4$ | 6.3 | 0.5 | 16-1/8 Diam. | 20-1/4 | Gless | $\begin{array}{\|l\|} \hline \text { Recersed } \\ \text { Small Ball Cap } \\ \hline \end{array}$ | Clear | 62 | Single | $\begin{aligned} & \text { Sma I1 She II } \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12DI | None | Magnetic | 16000 | 410 | 13000 | 250 | 27-63 | 16PP4 |
| 16GP4 | 6.3 | 0.th | 15-7/8 Diam. | 17-11/16 | Metal | Cone Lip | Clear | 70 | Single | Small Shell Duodecal 5 Pin | 1213 | None | Magnetic | 14000 | 410 | 12000 | 300 | 33-77 | 16GP4 |
| 161P4 | 6.3 | 0.6 | 15-7/8 Tiam. | 21-1/4 | Glass | Recessed Small Cavity | Clear | 60 | Doutle | $\begin{aligned} & \text { Small She 11 } \\ & \text { Duodecal } 5 \text { Pin } \\ & \hline \end{aligned}$ | 1202 | 1500 Min, 3500 Max. | Hegnetic | 14000 | 410 | 12000 | 300 | 33-77 | $16 \mathrm{HP4}$ |
| 1614P4 |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | $16 \mathrm{HP4A}$ |
| 16JP4 | 6.3 | 0.6 | 16-1/8 Diam. | 20-3/4 | Glass | $\begin{aligned} & \text { Pecessed } \\ & \text { Small Cavity } \end{aligned}$ | Clear | 60 | Doulle | $\begin{aligned} & \text { Small She Il } \\ & \text { Duodece } 15 \text { Pin } \end{aligned}$ | 1212 | $750 \mathrm{Min}, 2000 \mathrm{Max}$. | Magnetic | 14000 | 410 | 11000 | 250 | 27-63 | 16.5 P 4 |
| 16.JP4A |  |  |  |  |  |  | Grey |  |  |  |  |  |  |  |  |  |  |  | 16.514 |
| 16KP4 | 6.3 | 0.6 | 14-3/4 $\times 11-1 / 2$ | 18-3/4 | Glass | Recessed Small Cavity | Clear | 65 | Single | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 12 D 2 | 1500 | Mapnetic | 16000 | 410 | 14000 | 300 | 33-77 | 15 KP 4 |
| 16LP4 | 6.3 | 0.6 | 15-7/8 Diam. | 22-1/4 | Glass | Hecessed Small Cavicy | Clear | 52 | Double | $\begin{aligned} & \text { Smoll Shell } \\ & \text { Uuodecal S Pin } \\ & \hline \end{aligned}$ | 12ग2 | 1500 Min, 3500 Max. | Mapnetic | 14000 | 410 | 12000 | 300 | 33-77 | $16 \mathrm{LP4}$ |
| $16 \mathrm{LP4A}$ |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 161P4A |
| $16 \mathrm{TP4}$ | 6.3 | 0.6 | 16-1/8 Diam. | 21-3/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \end{aligned}$ | Clear | 60 | Donilile | $\begin{aligned} & \text { Small She II } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1202 | $1500 \mathrm{Min}, 3500 \mathrm{Max}$. | Magnetic | 14000 | 410 | 12000 | 300 | 33-77 | $16 \mathrm{MP4}$ |
| 16MP4 |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 16MP4A |
| 16094 | 6.3 | 0.6 | 14-3/4 $\times 11-17 / 32$ | 19.146 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \end{aligned}$ | Giray | 65 | Double | $\begin{aligned} & \text { Sma11 Sle } 11 \\ & \text { Duodecal } 7 \text { Pin } \end{aligned}$ | 12DI | None | Magnetic | 16000 | 410 | $\begin{array}{r} 8080 \\ 14000 \\ \hline \end{array}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline 250 \end{aligned}$ | 27-63 | 16984 |
| 16RP4 | 6.3 | 0.6 | 14-3/4 $\times 11-1 / 2$ | 18-3/4 | Glass | $\begin{aligned} & \text { Recesaed } \\ & \text { Small Cavity } \end{aligned}$ | Gray | 65 | Single | Simall She 11 Duodecal 5 Pin | 12D2 | 1500 | Magnetic | 16000 | 410 | 12000 | 300 | 33-79 | 16RP4 |
| 16SP4 | 6.3 | 0.6 | 15-7/8 Dram. | 17-5/16 | Gless | Recessed Small Cavity | Clear | 70 | Double | Small Shell Duodecal 5 Pin | 12L2 | 1500 Min, 3500 Max. | Mapnetic | 14000 | 410 | 12000 | 300 | 33-77 | 16SP4 |
| 16.P44A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 16 SP4A |
| $16 \mathrm{TP4}$ | 6.3 | 0.6 | 16-1/8 Diam. | 18-1/8 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \end{aligned}$ | Gray | 70 | Single | $\begin{aligned} & \text { Small Shell } \\ & \text { Thodecal } 5 \text { Pin } \end{aligned}$ | 12D2 | 1500 | Magnetic | 14000 | 410 | 12000 | 300 | 33.77 | $16 \mathrm{TP4}$ |
| 16ITP4 | 6.3 | 0.6 | 14-3/4 $\times 11-1 / 2$ | 18-1/8 | Glans | Recrssed Small Cavity | Gray | 65 | Sinfle | $\begin{aligned} & \text { Small Shell } \\ & \text { Duodecal } 5 \text { 'Pin } \end{aligned}$ | 1201 | Nune | Mafnetic | 15000 | 410 | 12000 | 300 | 27-63 | $161 \mathrm{P}_{4}$ |
| 16VP4 | 6.3 | 0.6 | 15-7/8 Diam. | 17-3/16 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Covity } \\ & \hline \end{aligned}$ | Gray | 70 | Sinfle | $\begin{aligned} & \text { Small Shell } \\ & \text { Moodecal } 5 \text { Pin } \end{aligned}$ | 12 n | None | Mapnetic | 15000 | 410 | 12000 | 250 | 27-63 | 16VP4 |
| $16 \mathrm{WP4} 4$ | 6.3 | 0.6 | 15-7/8 Diam. | 17-3/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Small Cavity } \\ & \hline \end{aligned}$ | Gray | 70 | Double | $\begin{aligned} & \text { Small Shel1 } \\ & \text { Duodecal } 5 \text { Pin } \end{aligned}$ | 1201 | None | Mapnetic | 15000 | 410 | 12000 | 250 | 27-63 | 16WP4 |
| 16xP4 | 6.3 | 0.6 | 14-3/4 $\times 11-17 / 32$ | 18-3/4 | Glass | $\begin{aligned} & \text { Recessed } \\ & \text { Smnll Cavity } \\ & \hline \end{aligned}$ | Gray | 65 | Double | $\begin{aligned} & \text { Small Shell } \\ & \text { Dundecal } 5 \mathrm{Pin} \end{aligned}$ | 1201 | None | thapnetic | 15000 | 410 | 12000 | 250 | 27-63 | 16xP4 |
| 16YP4 | 6.3 | 0.6 | 15-7/8 Diam. | 17-5/16 | Glass | Recessed Small Cavity | Gray | 70 | Single | $\begin{aligned} & \text { Small Shell } \\ & \text { Moodecal } 5 \text { Pin } \end{aligned}$ | 12m | $750 \mathrm{Min}, 2000 \mathrm{Max}$. | Mapnetic | 14000 | 410 | 12000 | 300 | 33-77 | 16YP4 |
| 19AP4 | 6.3 | 0.6 | 18-5/8 Diam. | 21-1/2 | Matal | Cone Lip | Clear | 66 | Single | Sma 11 She 11 Duodecal 7 Pin | 12 n 3 | None | Magnetic | 1900n | 410 | 13000 | 250 | 27-63 | 19AP4 |
| 19AP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 19AP4A |

magnetic type cathode ray tubes

|  | Heater |  | Bult |  |  |  |  |  | $\begin{array}{\|c\|} \hline \text { Ion } \\ \text { Trap } \\ \text { Required } \end{array}$ | Base | $\begin{gathered} \text { RMA } \\ \text { Basinf } \end{gathered}$ | $\mu \mathrm{f}$ Filter Capacitance Provided by Bulb Coatinf | $\begin{gathered} \text { Defiection } \\ \text { and } \\ \text { Focusing } \\ \text { Mechod } \\ \hline \end{gathered}$ | Maximum Desien Center Ratings |  | Typical Operation |  |  | $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Type } \\ \text { No. } \end{gathered}$ | Volts | Amperes | Nominal Face Dimenaions in Inches | $\begin{aligned} & \text { Lenpth } \\ & \text { in } \\ & \text { Inches } \end{aligned}$ | Construction | Terminal | face Plate Color | $\begin{array}{\|l\|} \begin{array}{c} \text { Deflection } \\ \text { Angle } \\ \text { in Dearees } \\ \text { (Note 1) } \end{array} \\ \hline \end{array}$ |  |  |  |  |  | $\begin{array}{\|l\|l} \text { Anode } \\ \text { Volts } \end{array}$ |  | $\begin{array}{\|l\|l} \text { Anode } \\ \text { Volty } \end{array}$ |  | Control <br> Grid <br> Negative <br> Volts |  |
| 190P4 | 6.3 | 0.6 | 18-7/8 Diam. | 21-1/2 | Glass | Recessed <br> Small Cavity | Clear | 65 | Double | $\begin{aligned} & \text { Small She } 11 \\ & \text { Duorecal } 5 \text { Pin } \\ & \hline \end{aligned}$ | 12 D 2 | $1000 \mathrm{Min}, 3000$ Max. | Mapnetic | 19000 | 410 | 13000 | 250 | 26-63 | 19DP4 |
| 19FP4 | 6.3 | 0.6 | 18-7/8 Diam. | 22 | Glass | Recessed Small Carity | Gray | 66 | Iouble | $\begin{array}{\|l} \hline \text { Small She ll } \\ \text { Duodecal } 5 \text { Pin } \\ \hline \end{array}$ | 12 D 1 | None | Mapnetic | 19000 | 410 | 13000 | 250 | 27-63 | 19PP4 |
| 19CP4 | 6.3 | 0.6 | 18-7/8 Diam. | 21-1/4 | Glass | Recessed Small Cavity | Gray | 66 | Sinfle | $\begin{array}{\|l} \hline \text { Small She ll } \\ \text { Duodecal 5 Fin } \\ \hline \end{array}$ | 12 n 1 | None | Mapnetic | 19000 | 410 | 13000 | 250 | 27-63 | 19CP4 |
| 20 PP 4 | 6.3 | 0.6 | 20 Diam . | 28-3/4 | Glass | Medium Cap | Clear | 54 | None | $\begin{array}{\|l\|} \hline \text { Small She ll } \\ \text { Duodecal } 7 \mathrm{Pin} \end{array}$ | $12 \mathrm{D1}$ | None | Mapnetic | 16500 | 750 | $\begin{aligned} & 10000 \\ & 15000 \end{aligned}$ | $\begin{aligned} & 250 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{array}{r} 25-70 \\ 25-70 \\ \hline \end{array}$ | ${ }^{208 P 4}$ |
| $22 \mathrm{AP4}$ | 6.3 | 0.6 | 21-11/16 Diam. | 22-7/8 | Metal | (Cone Lip) | Clear | 70 | Single | $\begin{array}{\|l\|} \hline \text { Small Sluell } \\ \text { Buodecal 5 } \mathrm{Pin}_{\text {in }} \\ \hline \end{array}$ | 1213 | None | Magnetic | 19000 | 410 | 14000 | 300 | 33-72 | $22 \mathrm{AP4}$ |
| 22AP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 22AP4A |
| 904 | 2.5 | 2.1 | 5-1/16 Diam. | 16-1/4 | Glass | Cap | Clear | $\cdots$ | None | Medium 6 Pin | ${ }^{6 A l}$. | None | Note 4 | 4600 | 250 | $\begin{aligned} & 1000 \\ & 3000 \\ & 4600 \\ & \hline \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \\ & 250 \\ & \hline \end{aligned}$ | $\begin{aligned} & 34 \\ & 35 \\ & 39 \\ & \hline \end{aligned}$ | 904 |
| 5WP11 | 6.3 | 0.6 | 5 Diem. | 11-7/16 | Glass | Recessed Small Cavity | Clear | 50 | None | $\begin{aligned} & \text { Small She 11 } \\ & \text { lhoodecal ? Pin } \\ & \hline \end{aligned}$ | 12.2 | 100 Min, 500 Max. | Note 2 | 27000 | 350 | 27000 | 200 | 42-98 | 5WP11 |
| 7MP7 | 6.3 | 0.6 | 7-3/16 Dism. | 12-1/2 | Glass | Hecessed Small Cavity | Clear | 50 | None | $\begin{aligned} & \text { Sma I Shell } \\ & \text { Thodecal } 5 \text { Pin } \end{aligned}$ | 12D1 | None | Magnetic | 8000 | 700 | $\begin{aligned} & 4000 \\ & 7000 \\ & \hline \end{aligned}$ | $\begin{array}{r} 250 \\ 250 \\ \hline \end{array}$ | $\begin{aligned} & 27-63 \\ & 27-63 \\ & \hline \end{aligned}$ | 7MP7 |
| 19EP4 | 6.3 | 0.6 | $17 \times 13-3 / 32$ | 21-1/8 | Glass | Recessed Small Cavity | Gray | 65 | Single | $\begin{aligned} & \text { Small She } 11 \\ & \text { Duodecal } 5 \text { Pin } \\ & \hline \end{aligned}$ | 1202 | 1000 Min, 2500 Max. | Maenetic | 19000 | 410 | 13000 | 250 | 26-63 | $19 \mathrm{EPP}_{4}$ |
| 16ZP4 | 6.3 | 0.6 | 15-7/8 Diam. | 22-1/4 | Glass | Recessed Small Cavity | Gray | 52 | Single | $\begin{aligned} & \text { Small She 11 } \\ & \text { Duodecal 5 Pin } \\ & \hline \end{aligned}$ | 1212 | 750 Min, 2000 Max. | Mametic | 16000 | 410 | 12000 | 300 | 33-77 | 16234 |
| 16.3P4A | f. 3 | 0.6 | 15-7/8 Diam. | 17-3/4 | Glass | Recessed Smail Cavity | Gray | 70 | Sinple | Small She 11 Duodecal 5 Pin | 12D2 | 750 Min, 2000 Max. | Magnetic | 16000 | 410 | 12000 | 250 | 27-63 | 16WP4A |
| 171944 | 6.3 | 0.6 | 15-3/8 $\times 12-1 / 4$ | 18-5/8 | Glass | Recessed Small Cavity | Gray | 65 | Single | $\begin{array}{\|l\|} \hline \text { Small She } 11 \\ \text { Duodecal } 5 \mathrm{Pin} \\ \hline \end{array}$ | 12 D 2 | $750 \mathrm{Min}, 2000 \mathrm{Max}$. | Magnetic | 15000 | 410 | 12000 | 300 | 33-77 | 17AP4 |
| ${ }^{17 \mathrm{PP} 4}$ | 6.3 | 0.6 | 15-25/64 $\times 12-9 / 64$ | 19-5/8 | Glass | Recessed Small Cavity | Clear | 65 | Sinple | Small Sle 11 Duodecal 5 Pin | 12122 | 750 Min, 2000 Max. | Magnetic | 16000 | 410 | 12000 | 300 | 33-77 | 178P4 |
| 17EP4A |  |  |  |  |  |  | Gray |  |  |  |  |  |  |  |  |  |  |  | 178P4A |
| 10FP4 41 | 6.3 | 0.6 | 10-1/2 Diam. | 17-5/8 | Glass | Recessed Small Cavity | Gray | 54 | None | Sma11 Sliell 11 Tuodecal 5 Pin | 12 D 2 | $500 \mathrm{Min}, 250 \mathrm{Max}$. | Mapnetic | 12000 | 410 | 11000 | 250 | 27-63 | 10FP4A |

Note 1: Horizontal Deflection Angles are given for Rectangular Tubes.
Courtesy SyIvania Electric Products Inc.
Note 2: Mapnetic Deflection, Flectrostatic Focusing.
Note 3: Fiectrostatic and Magnetic Deflection, Magnetic Focusing.
Note 4: Electrostatic and Mapnetic beflection, Electrostatic Focusing

## CROSS INDEX OF ARMY VT NUMBERS AND COMMERCIAL NUMBERS

| VT | COMMERCIAL |
| :---: | :---: |
| NUMBER | NUMBER |


| $\begin{aligned} & \text { VT-1. } \\ & \text { VT-2 } . \end{aligned}$ | . . . WE-203A (obsolete) |
| :---: | :---: |
| VT-3. | . . Obsolete. |
| VT-4A | . . Obsolete. |
| VT-4B | . . . Commercial 211. |
| VT-4C | . . . JAN 211. |
| VT-5 | . . WE-215A |
| VT-6. | . . 212A (obsolete) |
| VT-7. | . . WX-12 (obsolete) |
| VT-8. | . . UV-204 (obsolete) |
| VT-10 | . Obsolete. |
| VT-11 | . . . Obsolete. |
| VT-12 | . . Obsolete. |
| VT-13 | . . Obsolete. |
| VT-14 | . . Obsolete. |
| VT-16 | . . Obsolete. |
| VT-17 | . . 860. |
| VT-18 | . . Obsolete. |
| VT-19 | . . 861. |
| VT-20 | . . Obsolete. |
| VT-21 | . . Obsolete. |
| VT-22 | . . 204A. |
| VT-23 | . Obsolete. |
| VT-24 | . . 864. |
| VT-25 | . . 10. |
| VT-25A | . . . 10 Special. |
| VT-26 | . . 22. |
| VT-27 | . . 30. |
| VT-28 | . . 24, 24A. |
| VT-29 | . . 27. |
| VT-30 | . $01-\mathrm{A}$ |
| VT-31 | . 31. |
| VT-32 | . . Obsolete. |
| VT-33 | . . . 33. |
| VT-34 | . . 207. |
| VT-35 | .. $35 / 51$. |
| VT-36 | . . 36. |
| VT-37 | . 37. |
| VT-38 | . . 38. |
| VT-39 | . . 869. |
| VT-39A | . . 869A |
| VT-40. | . 40. |
| VT-41 | . . 851. |
| VT-42 | . . 872. |
| VT-42A | . . 872A (Special fil.). |
| VT-43 | . . 845. |
| VT-44 | . . 32. |
| VT-45 | . 45. |
| VT-46 | . . 866. |
| VT-46A | . 866A. |
| VT-47 | . 47. |
| VT-48 | . . 41. |
| VT-49 | . . 39/44. |
| VT-50 | . 50. |
| VT-51 | . 841. |
| VT-52 | . . . 45 Special. |


| VT <br> NUMBER | COMMERCIAL NUMBER | VT <br> NUMBER | COMMERCIAL <br> NUMBER |
| :---: | :---: | :---: | :---: |
| VT-53 | . Canceled (superseded by VT-42A). | $\begin{aligned} & \text { VT-99. } \\ & \text { VT-100 } \end{aligned}$ | $\begin{aligned} & \text { 6F8G. } \\ & 807 . \end{aligned}$ |
| VT-54 | . 34. | VT-100A. | 807 Modified. |
| VT-55 | . 865. | VT-101. | 837. |
| VT-56 | . 56. | VT-102. | Canceled. |
| VT-57 | . 57. | VT-103. | 6SQ7. |
| VT-58 | . 58. | VT-104. . | 12SQ7. |
| VT-60 | 850. | VT-105. | 6SC7. |
| VT-62 | . 801,801A. | VT-106. | 803. |
| VT-63 | . 46. | VT-107.. | 6V6. |
| VT-64 | . 800. | VT-107A. | 6V6GT. |
| VT-65 | . 6C5. | VT-107B. | 6V6G. |
| VT-65A | . 6 C 5 G . | VT-108. | 450 TH. |
| VT-66 | . 6F6. | VT-109. | 2051. |
| VT-66A | . 6F6G. | VT-111. | 5BP4/1802P4. |
| VT-67 | . 30 Special. | VT-112.. | 6AC7/1852. |
| VT-68 | . 6B7. | VT-114. . | 5 T 4. |
| VT-69 | . 6D6. | VT-115. | 6L6. |
| VT-70 | . 6F7. | VT-115A. | 6L6G. |
| VT-72 | . 842. | VT-116. | 6SJ7. |
| VT-73 | . 843. | VT-116A. | 6SJ7GT. |
| VT-74 | . 5Z4. | VT-116B. | 6SJ7Y. |
| VT-75 | . 75. | VT-117. | 6SK7. |
| VT-76 | . 76. | VT-117A. | 6SK7GT. |
| VT-77 | . 77. | VT-118. . | 832. |
| VT-78 | . 78. | VT-119. . | 2X2/879. |
| VT-80 | . 80. | VT-120. . | 954. |
| VT-83 | . 83. | VT-121. | 955. |
| VT-84 | . 84/6Z4. | VT-122. | 530. |
| VT-86 | . 6 K 7. | VT-123. . | RCA A-5586 (super- |
| VT-86A | . 6 K 7 G . |  | seded by VT-128). |
| VT-86B | . 6K7GT. | VT-124. . | 1 A 5 GT . |
| VT-87 | . 6L7. | VT-125. . | 1C5GT. |
| VT-87A | . 6L7G. | VT-126. | 6X5. |
| VT-88 | . 6R7. | VT-126A. | 6X5G. |
| VT-88A | . 6R7G. | VT-126B. | 6X5GT. |
| VT-88B | . 6 R7GT. | VT-127. . | Special tube. |
| VT-89 | . 89 | VT-127A. | Special tube. |
| VT-90 | . 6 H 6. | VT-128. . | 1630 (A-5588). |
| VT-90A | . 6 H 6 GT . | VT-129. . | 304 TL . |
| VT-91 | . 6J7. | VT-130. . | 250 TL . |
| VT-91A | . 6 J 7 GT . | VT-131. . | 12SK7. |
| VT-92. | . 6Q7. | VT-132. . | 12 K 8 Special. |
| VT-92A*. | . 6Q7G. | VT-133. | 12SR7 |
| VT-93 | . 6B8. | VT-134. . | 12 A 6. |
| VT-93A | . $6 \mathrm{B8} \mathrm{G}$. | VT-135. . | 12J5GT. |
| V'T-94 | . 6J5. | VT-135A. | 12 J 5. |
| VT-94A | . 6 J 5 G . | VT-136. . | 1625. |
| VT-94B | . 6J5 Special selec. | VT-137. . | 1626. |
| VT-94C | . 6J5G Special selec. | VT-138. . | 1629. |
| VT-94D | . 6J5GT. | VT-139. . | VR150-30. |
| VT-95 | . 2A3. | VT-140*.. | 1628. |
| VT-96. | . 6N7. | VT-141.. | 531. |
| VT-96B | $\therefore$ 6N7 Special selec. | VT-142. . | WE-39DY1. |
| VT-97 | . 5W4. | VT-143. . | 805. |
| VT-98. | . $6 \mathrm{U} / 6 \mathrm{G} 5$. | VT-144... | 813. |

[^5]| VT <br> NUMBER | COMMERCIAL <br> NUMBER | VT <br> NUMBER | COMMERCIAL NUMBER | VT <br> NUMBER | COMMERCIAL <br> NUMBER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VT-145. | . 5Z3. | VT-185. . | 3D6/1299. | VT-230. . | 350A. |
| VT-146. | . 1N5GT. | VT-186. | Special tube. | VT-231. | 6SN7GT. |
| VT-147. . | . 1A7GT. | VT-187. | 575A. | VT-232. | E-1148. |
| VT-148. | 1D8GT. | VT-188. | $7 \mathrm{E6}$. | VT-233. | 6SR7. |
| VT-149. | . 3A8GT. | VT-189. | 7 F7. | VT-234. | HY-114B. |
| VT-150. . | 6SA7. | VT-190. | 7H7. | VT-235. | HY-615 |
| VT-150A. | 6SA7GT. | VT-191. | 316A. | VT-236. | 836. |
| VT-151. | 6A8G. | VT-192. | 7 A 4. | VT-237. | 957. |
| VT-151B. | 6A8GT. | VT-193. | 7C7. | VT-238. | 956. |
| VT-152. | . 6 K 6 GT . | VT-194. | 7 J 7. | VT-239. | 1 LE 3. |
| VT-152A. | $6 \mathrm{K6G}$. | VT-195.. | 1005. | VT-240. | 710A. |
| VT-153. | . 12 C 8 Special. | VT-196.. | 6W5G. | VT-241. | 7E5/1201. |
| VT-154. | . 814. | VT-197A. | 5Y3GT/G. | VT-243. . | 7C4/1203A. |
| VT-155. | . Special tube. | VT-198A. | 6G6G. | VT-244. | 5 U G. |
| VT-156. | . Special tube. | VT-199. | 6SS7. | VT-245. | 2050. |
| VT-157. | . Special tube. | VT-200. | VR-105-30. | VT-246. | 918. |
| VT-158. | . Special tube. | VT-201. | 25 L 6. | VT-247. | 6AG7. |
| VT-159. | . Special tube. | VT-201C. | 25L6GT. | VT-248. | 1808P1. |
| VT-160. | . Special tube. | VT-202. . | 9002. | VT-249. | 1006. |
| VT-161. | . 12SA7. | VT-203. | 9003. | VT-250. | EF50. |
| VT-162. | . 12SJ7. | VT-204. | HK24G. | VT-251. | 441. |
| VT-163. | 6C8G. | VT-205. | 6ST7. | VT-252. | 923. |
| VT-164. | . 1619. | VT-206A. | 5 V 4 G . | VT-254. | 304 TH . |
| VT-165. | 1624. | VT-207. | 12AH7GT. | VT-255. | 705A. |
| VT-166. | 371 A. | VT-208. | $7 \mathrm{B8}$. | VT-256. | ZP486. |
| VT-167. | . 6 K 8. | VT-209. | 12SG7. | VT-257. | K-7. |
| VT-167A. | . 6 K 8 G . | VT-210. | 1 S 4. | VT-259. | 829. |
| VT-168A. | 6Y6G. | VT-211. | 6SG7. | VT-260. | VR75-30. |
| VT-169. | . 12C8. | VT-212. | 958. | VT-264. | 3Q4. |
| VT-170. | . 1E5-GP. | VT-213A. | 6L5G. | VT-266. | 1616. |
| VT-171. | . 1 R5. | VT-214. | 12 H 6. | VT-267. | 578. |
| VT-171A. | . Loctal Equiv. of | VT-215. | 6 E 5. | VT-268. | 12SC7. |
|  | 1 R5. | VT-216. . | 816. | VT-269. | 717A. |
| VT-172. | . 1S5. | VT-217. | 811. | VT-277. | 417. |
| VT-173. | . 1 T4. | VT-218. | 100 TH. | VT-279. | GY-2. |
| VT-174. | . 3S4. | VT-219.. | Canceled. | VT-280*. | C7063. |
| VT-175. | . 1613. | VT-220. | 250 TH . | VT-281** | HY-145ZT. |
| VT-176. . | . 6AB7/1853. | VT-221.. | 3Q5GT. | VT-282. | ZG489. |
| VT-177. | . 1 LH4. | VT-222. | 884. | VT-283* . | QF-206. |
| VT-178. | . 1 LC 6. | VT-223. | 1 H 5 GT . | VT-284* | QF-197. |
| VT-179. | . 1 LN 5. | VT-224. . | RK-34. | VT-285*. | QF-200C. |
| VT-180*. | . 3LF4. | VT-225. | 307A. | VT-286. | 832A. |
| VT-181. . | . 7Z4. | VT-226. . | 3EP1/1806P1. | VT-287. | 815. |
| VT-182. . | . 3 B7/1291. | VT-227. . | 7184. | VT-288. . | 12 SH 7. |
| VT-183. . | . 1R4/1294. | VT-228. . | 8012. | VT-289.. | 12SL7GT. |
| VT-184. . | . VR90-30. | VT-229. . | 6SL7GT. |  |  |

[^6]
## BALLAST TUBE AND RESISTOR NUMBERING CODES FOR AC-DC RECEIVERS USING 0.3 AMP. SERIES CONNECTED HEATERS

There are two numbering codes now in use for ballast and resistor tubes. Both codes use parts of the type designation to indicate the various divisions of the tube's service. For example, type numbers in the first system (A) might be BKX51DJ or L55B and, in the second system (B), might be 200R44 or 200R. These letter and number combinations are explained by the following examples.

## SYSTEM A



NOTE 1.
"Ballast" action indicates that the pilot lamp shunt resistor has low starting resistance when cold, protecting the lamp filament from the initial current surge, and has much higher resistance when hot, applying full operating voltage to the lamp.

NOTE 2.

| Tube Letter | Lamp No. | Volts | Amperes | Bead Color |
| :---: | :---: | :---: | :---: | :---: |
| K | 40 and 47 | 6.3 | 0.15 | Brown |
| L | 44 and 46 | 6.3 | 0.25 | Blue |
| $M$ | 50 and 51 | 7.5 | 0.2 | White |

NOTE 3.
$X$ denotes a 4 pin base and metal shell. $Y$ or $Z$ denote octal bases but with different pin connections. (See Figures $A$ to K.)

NOTE 4.
This number includes the drop in the series resistor plus the drop in the pilot lamp and its shunt. The number represents the difference between the sum of the heater voltages and the line voltage of 117.5 volts. Tubes are made with the following numbers: $98,92,86,80,73,67,61,55,49,42,36,30$, $23,17,11$. The number to be used is the one closest to the voltage difference mentioned above.


All tubes under System B have glass bulbs and 4 pin bases and their type designations start with a number.


EXAMPLE

The numbers 4, 8, or 44, in combination with the preceding letter, indicate the internal tube connections. (See below.)

The letters R, L, or $M$, when followed by a number, indicare the type of pilot lamp which must be used with this tube. See Note 2, using the letter $R$ in place of $K$. (The letter $R$, alone, indicates only a form of internal tube connection without pilot la,np.)
$\rightarrow$ This number indicates the equivalent resistance in ohms of 0.3 ampere. Thus, $200 \times 0.3=60$ volts drop.

A8 or L8 or m8


R44 or 144 or $M 44$


EXAMPLE: $2130 \mu \mu \mathrm{f} . \pm 7 \%, 600 \mathrm{~W} . \mathrm{V}$. (Values for color shown in the above parenthesis)

| FIRST DIGIT OF CAPACITANCE IN MICROMICROFARADS | THR | EE DOT CO SECOND DIG CAPACITAN MICROMICRO | CODE |  |
| :---: | :---: | :---: | :---: | :---: |
| color | DIGIT NUMERAL | DECIMAL MULTIPLIER | tolerance | working voltage |
| BLACK | 0 | 1 | 20\% | - |
| BROWN | 1 | 10 | $1 \%$ | 100 |
| RED | 2 | 100 | $2 \%$ | 200 |
| ORANGE | 3 | 1000 | 3\% | 300 |
| YELLOW | 4 | 10000 | $4 \%$ | 400 |
| GREEN | 5 | - | 5\% | 500 |
| BLUE | 6 | - | 6\% | 600 |
| VIOLET | 7 | - | $7 \%$ | 700 |
| Gray | 8 | - | $8 \%$ | 800 |
| WHITE | 9 | - | 9\% | 900 |
| GOLD | - | 0.1 | - | 1000 |
| SILVER | - | 0.01 | 10\% |  |

## POWER TRANSFORMER LEAD COLOR CODE

Power transformer leads in radio receivers may be identified by the following colors (or color patterns) on the lead coverings.


Courtesy tinG-SOL Lamb Works, Inc.


RESISTANCE VALUE: The nominal resistance value $\ln$ ohms is identified by a three digit symbol. The first two diglts are the first two figures of the resistance value in ohms. The third digit specifies the number of zeros which follow the first two figures.

## I-F TRANSFORMER LEAD COLOR CODE

I-F transformer leads in radio receivers may be identified by the following colors on the lead coverings.

| PLATE LEAD | BLUE | GRID (or diode lead) | GREEN |
| :--- | :--- | :--- | :--- |
| B+ LEAD | RED | GRID RETURN | BLACK |

FOR "FUIL-WAVE" TRANSFORMER SECOND DIODE LEAD WILL BE GREEN-BLACK.

## AUDIO TRANSFORMER LEAD COLOR CODE

Interstage and Output Audio Transformer leads in rodio receivers may be identified by the colors on the lead coverings as shown.


In coses where use is made of a single primary and/or a single secondary, the upper half of the diagram indicates the color coding. The brown and yellow leads indicate the start of the primary and secondary windings respectively and will be used in place of the blue and green (as shown) where polarity indications are required.

RECEIVING TUBE SUBSTITUTION GUIDE

| PILOT LAMP TABLE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lamp No. | Volts | Amperes | Bead Color | Miniature Base | Bulb Type |
| 40 | 6-8 | 0.15 | Brown | Screw | T-3 1/4 |
| 41 | 2.5 | 0.50 | White | Screw | T-3 1/4 |
| 42 | 3.2 | 0.35 | Green | Screw | T-3 1/4 |
| 43 | 2.5 | 0.50 | White | Bayonet | T-3 1/4 |
| 44 | 6-8 | 0.25 | Blue | Bayonet | T-3 $1 / 4$ |
| 45 | 3.2 | 0.35 | White | Bayonet | T-3 1/4 |
| 46 | 6-8 | 0.25 | Blue | Screw | T-3 $1 / 4$ |
| 47 | 6-8 | 0.15 | Brown | Bayonet | T-3 1/4 |
| 48 | 2.0 | 0.06 | Pink | Screw | T-3 1/4 |
| 49 | 2.0 | 0.06 | Pink | Bayonet | T-3 1/4 |
| 50 | 6-8 | 0.20 | White | Screw | G-3 1/2 |
| 51 | 6-8 | 0.20 | White | Bayonet | G-3 1/2 |
| 55 | 6-8 | 0.40 | White | Bayonet | G-4 1/2 |
| 292 | 2.9 | 0.17 | White | Screw | T-3 1/4 |
| 292A | 2.9 | 0.17 | White | Bayonet | T-3 1/4 |
| 1455 | 18.0 | 0.25 | Brown | Screw | G-5 |
| 1455A | 18.0 | 0.25 | Brown | Bayonet | G-5 |
| 1490 | 3.2 | 0.16 | - - | Bayonet | T-3 1/4 |


|  | GERMANIUM CRYSTAL DIODE CHARACTERISTICS |
| :--- | :---: | :---: | :---: | :---: | :---: |

NOTE: Crystals 1 N48, 1 N51, 1 N52, 1 N63, 1 N64, and 1 N65 are General Electric types, all others are Sylvania types unless otherwise indicated.

* Units are matched in the forward direction at +1 volt so that the current flowing through the higher resistance unit is within $10 \%$ of that in the lower resistance unit. Ratings shown are for each diode.
** Consists of 4 specially selected and matched germanium diodes whose resis tances are balanced within $\pm 2.5 \%$ in the forward direction at 1.5 volts. For additional balance, the forward resistance of each pair of varistor crystals are matched within 3 ohms. Ratings shown above are for each diode.
+ Units are tested in a circuit employing an input of 1.8 volts rms at $40 \mathrm{mc} .70 \%$ modulated at 400 cycles. Demodulated output across a 4700 ohm resistor shunted by a 5 mmf capacitor is a minimum of 1.1 volts peak to peak.
- JAN types
${ }^{+\dagger}$ Consists of four matched low impedance germanium diodes each of which, with a voltage of one volt impressed in the forward direction, will pass a current within one ma of the average current of the four. Ratings shown above are for each diode.


# FIRST SUPPLEMENT RECEIVING TUBE S UBSTITUTION GUIDEBOOK 

BY

H. A. MIDDLETON



JOHN F. RIDER PUBLISHER, INC. 480 CANAL STREET NEW YORK 13, N. Y.

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## FOREWORD

Continued development and improvement of radios, television receivers, and other electronic equipment is to a great extent dependent on new and better vacuum tubes. Because of constant circuit changes and improvements, keeping a current list of tube substitutions for radios and television receivers is almost a never-ending job. Therefore, as the number of new substitutions justify it, supplements such as this one will be published periodically in order to keep your information up-to-date.

There are about 750 new substitutions listed in this supplement. Among these are some of the older tube types that were left out of the original Receiving Tube Substitution Guide Book. Substitutions are also listed here for some of the types for which we then thought were no substitutes. Most of the substitutions listed are for television receivers. When substituting tubes in television receivers, refer to the information given in the article 'Tube Substitutions in Television Receivers" in this supplement.

It is not the object of these instructions to tell you how to improve radios, television sets, and other electronic equipment, but rather to help you in using the tubes you have to replace those that are not available.

It is important to understand that the information here calls for substitutes only. We do
not recommend the use of these tubes when the original type is available. However, when you do not have the original tube types needed to repair electronic equipment, the Receiving Tube Substitution Guide Book and this supplement will prove invaluable to you. They will save you many hours and expedite repairs. In spite of over eight years experience in making and compiling these substitutions, there are no doubt some substitutions not listed here. Although a sincere effort has been made to list all the practical substitutions, to do so is practically an impossibility. We noticed while compiling these substitutions that one substitute served as a thought starter that brought others to mind. It may work the same way for you. You may find a substitute that we do not have listed. If you do work out a good substitute, do not trust your memory, but write it up in a form similar to that used here and attach it to the proper page in your Substitution Guide Book.

In addition to assisting you during times of tube shortages, this substitution information will help you to use tubes you have had on hand for long periods of time. Also, when tubes are plentiful, the information can be used for reconverting in cases where the substitute is less efficient than the original.

November, 1951

## SECTION 1

## TUBE SUBSTITUTIONS IN TELEVISION RECEIVERS

Television sets of a few years ago, with their 7- to 10 -inch picture tubes, used ordinary receiving tubes throughout except for the highvoltage rectifier tubes and, of course, the cath-ode-ray tubes. Consumer demand called upon the ingenuity of the television receiver and tube manufacturers for larger and larger pictures. Along with larger size picture tubes, it was necessary to develop other specialized types of television tubes. Special circuits in television receivers require characteristics in receiving tubes which are different from those of most ordinary radio receiving types.

Consider the use of magnetically deflected picture tubes. The magnetic picture tube requires sweep amplifiers capable of high power output. Tube manufacturers developed special tube types for these circuits which are capable of high plate current without the use of extremely high plate voltages. It is entirely possible that efficient operation in this circuit could have been accomplished by the use of higher output tubes which were already available and by increasing the size and output of the low-voltage power supply. However, the cost of building and maintaining this larger power supply, its greater size and weight, and the added danger are only a few of the reasons why this was not done. By designing new and special tube types, improved performance was made possible, circuits were simplified, and troubleshooting was made easier and safer for the television technician.

Although there are some twenty to thirty stages commonly used in television receivers, there are only about thirteen different tube classifications denoted by manufacturers in common use. There are many variations within each of these thirteen classifications. A large portion of tubes in a given similar classification which are designed for the same circuit application are enough alike to operate in some fashion when substituted for each other without change of circuit components. Sometimes a type designed for one circuit gives
excellent results in another circuit، It is sometimes necessary to make mechanical changes in order to accomplish substitutions.

Because of the similarity of characteristics of many tubes, the more familiar the technician is with the circuit use of, the similarity between, and the satisfactory or unsatisfactory operation of one tube type compared to another, the more versatile and valuable his tube stock becomes. This is true especially in an emergency.

Listed on page 2 are thirteen classifications of tubes used in television receivers along with the commonly used types. Under each classification are listed the majority of individual circuits in which these tubes are used. A careful study of this chart will familiarize you with the tubes used in the most common television receiver circuits and will serve to expedite your service problems.

These listings will serve to indicate the most common usages of the tube types in each classification. Other types that are not listed may come to mind as you look over this list, or you may find additional listings in your Receiving Tube Substitution Guide Book. Differences in circuitry as used by various manufacturers may place some of the tubes into categories other than those shown here. As stated before, the object of the chart is to list the most common types in their most common circuits.

It has been found that substitutions in the front end or in the video strip can be more satisfactorily accomplished in television receivers located in strong signal areas than those located in fringe areas. A very small loss or gain that would go unnoticed when a substitution has been made in a receiver located in a strong signal area might be sufficient to seriously impair the picture quality in a fringe area.

In some areas, fringe conditions may exist on one channel while local conditions exist on another channel. Referring to the classifications

TELEVISION RECEIVER TUBES

| Classification | Common Types | Specific Circuits |
| :---: | :---: | :---: |
| 1. Low-voltage Rectifier | 5U4, 5V4, 5Y, , 6AX5, 6X5, 25Z6 | Low-voltage rectifier |
| 2. High-voltage Rectifier | 1B3, 1V2, 1X2, 1Y2, 1Z2, 5642 | High-voltage rectifier |
| 3. Pentode Power Amplifier and Beam Power Amplifier | $\begin{aligned} & \text { 6AQ5, 6F6, 6K6, 6L6, 6V6, } \\ & \text { 6Y6, 7B5, 7C5, 25L6, 35L6, } \\ & 50 \mathrm{~L} 6 \end{aligned}$ | Audio output <br> Vertical sweep output Horizontal sweep oscillator High-voltage r-f oscillator Video output |
| 4. Duo-diode Triode | $\begin{aligned} & \text { 6AT6, 6AV6, 6SQ6, 6BF6, } \\ & \text { 6BK6, 6BT6, 6BU6, 12AT6, } \\ & \text { 12SQ6 } \end{aligned}$ | First audio amplifier |
| 5. High-frequency Triode | 6AB4, 6C4 | Local oscillator in front end Vertical sweep oscillator |
| 6. R-f Pentode | $\begin{aligned} & \text { 6AG5, 6AJ5, 6AK5, 6AU6, } \\ & \text { 6BA6, 6BC5, 6BD6, 6BH, } \\ & \text { 6CB6, 12AU6, 12BA6 } \end{aligned}$ | Video i-f amplifier <br> Sound i-f amplifier <br> Radio-frequency amplifier <br> Video output |
| 7. Twin Triode | 6BL7, 6F6, 6F8, 6J6, 6SL7, 6SN7, 7F7, 7F8, 12AT7, 12AU7, 12AV7, 12AX7, 12AY7, 12AZ7, 12SN7 | Video amplifier <br> Sync separator <br> Mixer oscillator <br> Vertical sweep output |
| 8. High-power Beam Pentodes | $\begin{aligned} & \text { 6AU5, 6AV5, 6BD5, 6BG6, } \\ & \text { 6BQ6, 6CD6 } \end{aligned}$ | Horizontal sweep output |
| 9. Damper Rectifier | 6AX6, 6V4, 6W4, 12AX4, 25W4 | Damper |
| 10. Twin Diode | 6AL5, 6H6, 7A6, 12AL5, 12H6 | Video detector circuit Horizontal discriminator Sound ratio detector |
| 11. Triple-diode Triode | 6R8, 6S8, 6T8 | Ratio detector and first audio |
| 12. Gated Beam Pentode | 6BN6, 12BN6 | FM detector <br> Vertical sweep oscillator |
| 13. High-frequency Triode Pentode | 6U8, 6X8 | Oscillator mixer |

as specified in the performance column of your Substitution Guide, the substitution of a " $G$ " or " $P$ " classified type in the front end or video strip may impair the picture quality or even cause loss of the picture entirely in the case of the fringe area station while the local stations continue to be received satisfactorily. However, in times of tube shortages, when the original or a substitute with a classification of " $E$ " is unavailable, this would be better than no reception at all.

The lack of uniformity of design and the variability of materials used in the manufacture of the same tube types by different manufacturers may cause premature failure in a given circuit in one run of tubes while a different run will hold up well. A certain run of 6BG6 tubes installed in sets with a 17 -inch picture tube may fail after a week or two because of their lack of power-handling capabilities. Tubes from this same run may give good service in other sets where the power output requirements are less. The same may be found to be true of damper rectifier types where extremely high peak inverse voltages may cause flashover in an inferior run of 6 U 4 types. Low-voltage rectifiers in certain runs have been known to have inefficient filaments, and their output falls off rapidly when used in large-tube sets where output current requirements are high. When your service department finds such a run of tubes on hand, use them in the smaller-tube sets for most reliable service.

## Low-voltage Rectifiers

Requirements for rectifier tubes in the lowvoltage power supply of a television receiver are the same as for those used in ordinary radio receiving equipment, except that higher output current is usually required.

When choosing a substitute, it is only necessary to select a type which has sufficient cur-rent-carrying capacity and a peak inverse voltage rating equal to or greater than the original type. If the substitute type meets these requirements but also has higher filament current requirements that will reach the maximum rating of the available filament transformer winding, it is recommended as a substitute over another type that falls short of output current and does not have at least an equal peak inverse voltage. This is so even though this latter type has the same filament rating as the original tube.

Selenium rectifiers can be used as substitutes for tube-type rectifiers. When substituting with selenium rectifiers in the lowvoltage power supply, it is good practice to use a large safety factor. For example, if the tube rectifier has a rated output current capacity of 225 ma , use at least a $300-\mathrm{ma}$ selenium rectifier or a larger one if space permits. Rectifiers in the low-voltage power supply haye had a high record for failure. Thus, the practice of using at least the next size larger as a substitution will help to eliminate expensive callbacks. Refer to the Receiving Tube Substitution Guide Book for additional information on selenium rectifiers.

## High-voltage Rectifiers

There are only a limited number of types of high-voltage rectifiers being currently produced. When choosing a substitute, use the type that has an equal or higher peak inverse voltage rating than the type for which you are substituting. The output current requirement from these rectifiers is so small that little consideration need be given to this characteristic of the substitute type.

Since there are only a few of this type of tube available, mechanical alterations are frequently necessary when making a substitution. You must either extend the plate lead, install sockets, or do other rewiring. It is sometimes necessary to increase the size of the high voltage shield or modify it in some other way. Make sure that all high voltage leads are properly insulated and that the shield is fastened securely for safety's sake. One of the most difficult substitutions here is for the Sylvania type 5642 because of the small size of this subminiature tube. It is necessary to find space for mounting a tube socket and a shield can.

## Pentode Power Amplifiers

Pentode power amplifier tubes and the small beam power types are generally used in five different circuits in television receivers. They are the audio output stage, the vertical sweep output, the horizontal sweep oscillator, the high-voltage r-f oscillator, and video output stage.

When substituting in the vertical output or high-voltage r-f oscillator circuits, be sure to choose a type whose output is equal to or
greater than the original because of the amount of power involved in these stages. The use of a lower-powered tube than the original can sometimes be made to give from fair to good results by altering the values of the circuit components. The interelectrode capacitances are not generally considered to be a critical characteristic of the tube used in this circuit.

The audio output circuits of television receivers are not different from those used in ordinary radio receivers. Only in cases where high audio power is required from the receiver are substitutions in this stage critical. Component part changes may sometimes be necessary in order to secure optimum output from the substitute tubes.

The video output stage is a wide-band amplifier and is not critical with respect to power output. This is true because it is feeding into a relatively high impedance load. It is important to choose a substitute with similar interelectrode capacitance in order to insure uniform amplification throughout the entire video band. It is better to choose a tube with lower interelectrode capacitance than the reverse. If the substitute tube has lower interelectrode capacitance than the original, over-peaking may result. This can be compensated for by the installation of small carbon resistors across the peaking coils. Their value will vary with the substitution and can be determined by experimentation.

The horizontal sweep oscillator circuit is the least critical of all stages discussed in this section. Therefore, when a receiver utilizes a similar tube in any of the other four stages just mentioned, make the substitution in the horizontal oscillator stage. For example, assume that the vertical output tube is the same type as that used in the horizontal oscillator. If the vertical output tube is to be substituted for, it is usually desirable to transfer the horizontal oscillator tube to the vertical output stage and then substitute for the horizontal sweep oscillator.

## Duo-diode Triodes

Duo-diode triodes are generally used in only one stage of television receivers, namely, the first audio amplifier. This circuit is identical to those used in ordinary radio receivers. When choosing a substitute for this circuit, the main consideration is the amplification factor
of the triode section. Try to choose a substitute that has approximately the same amplification factor for best results. These types are often used only as triodes and no connection is made to the diode terminals. Under these conditions, they can be substituted for with a triode tube having characteristics similar to those of the triode section.

## High-frequency Triodes

These types are generally used in two television circuits, the local oscillator in the front end and the vertical sweep oscillator.

Local oscillator circuits used in television receivers are basically the same as those used in radio receivers. Television oscillators, however, operate at a much higher frequency than do oscillators in ordinary radio receivers. For this reason, they are very critical as to any substitution. Even a very small change in the inductance or capacitance of the circuit may cause the circuit to become inoperative or operate at an incorrect frequency. Leads should be kept as short as possible. This should be kept in mind when making substitutions that require wiring changes. All of the mechanical characteristics of the circuit should be made as similar as possible to the original. Some oscillator tubes have more than one of the pins connected to the same element in the tube. When a substitution is made, the same method of connection should be followed.

The interelectrode capacitance of the substitute tube has a large effect on the circuit operation. The type of oscillator and the physical construction of the circuit afford different tolerances according to the specific case. If the grid-to-plate capacitance is higher in the substitute tube, the oscillator frequency would be lower in proportion to the increase in capacitance. If the capacitance is lower, the oscillator frequency will be higher. If the oscillator slug adjustment will not resonate the circuit to the proper frequency and the interelectrode capacitance is not too far off, it is possible that adjustment of the coils in the circuit will effect satisfactory operation. This, however, is no job for the novice, and, if you are not very sure of exactly how to go about it, let the job go until a satisfactory substitute or the original type becomes available. The adding or removal of a shield in this circuit will sometimes change the effective
circuit capacitance enough to make the difference between satisfactory and unsatisfactory operation.

The vertical sweep oscillator operates at 60 cps so that high-frequency triodes are not actually required for this circuit. However, they are sometimes used for this service. Under these conditions, they are not considered critical as to substitution. The ordinary radio receiving type triode will make a good substitution in this stage. If the local ordinary oscillator in the front end fails and the same type is used in the vertical oscillator stage, place the tube from the vertical oscillator stage into the local oscillator socket and make the substitution in the less critical vertical sweep oscillator stage.

## R-f Pentodes

Radio-frequency pentodes are the most used classification of tubes in television receivers. Because of this, there have been many variations of this type produced. Many of these are of the miniature, seven-pin construction.

In addition to some miscellaneous applications, they are used in four different circuits of a television receiver. These are the radiofrequency amplifier in the front end, the video i-f amplifiers, the sound i-f amplifiers, and the video amplifiers.

The small size of the miniature version of this tube type makes possible higher efficiency circuits at the very high frequencies. Therefore, the substitution of a larger tube designed for operation at lower frequencies will usually not be satisfactory. For example, a 6SH7 could not be used as a substitute for a 6BC5 because of the higher interelectrode capacitance of the larger tube. This, in addition to the greater distributed capacitance in the circuit due to longer leads required when changing the tube socket, would make alignment of the circuit almost impossible.

The radio-frequency stage in the front end is used primarily as an isolation stage between the antenna and the mixer. This stage is required to have a wide pass band so that not too much amplification is possible. This tube is therefore considered to be reasonably noncritical as to substitutions. Even a large difference in the gain of the tube used has little effect on the overall operation of the receiver.

The video i-f strip utilizes three or more
stages of amplification. Of these, the first and the last usually contribute the least to the amplification of the signal. These are, therefore, the least critical as to substitutions. It is suggested that, when substitution is necessary in the $i-f$ strip and where several tubes of identical type are used, that you first attempt a substitution without changing either alignment or component parts. Refer to your Receiving Tube Substitution Guide Book for performance classifications as well as characteristics. Tubes with high transconductance are usually the most satisfactory in this circuit, where amplification requirements are high. Theoretically, when a substitution is made in any of the video i-f stages, complete realignment is mandatory. However, from a practical standpoint, this may not be necessary.

The sound i-f strip has a much narrower bandwidth than the video i-f strip, and the available amplification is ordinarily greater than is required. For this reason, a reasonable reduction in the gain of the sound i-f stage is considered unimportant, making the circuit less critical to substitutions than are the video i-f stages.

It may be found that one of the video i-f tubes in a given receiver is defective and that the tubes used in the sound i-f are of identical types. In this case, replace the defective video stage tube with one of the sound stage tubes and proceed with the substitution in the less critical sound stage.

In the circuits discussed above, it is very important that connecting leads be kept short. When changing a socket, be sure to reconnect the leads the same way as they were originally in order to avoid increasing the distributed capacitance of the circuit and to minimize the possibility of regeneration.

The video output stage is not very critical as to substitutions. If you have a variety of substitutes, it is recommended that you try them all and use the one that produces the best results. If over-peaking is evident in the picture after a substitution has been made, this can be eliminated by shunting the peaking coils with small carbon resistors, as mentioned previously.

## Twin Triodes

Twin triodes have many equivalents and many uses. Some of these are the following:
mixer-oscillator, sync separator, video amplifier, vertical oscillator, horizontal oscillator, and horizontal frequency control.

In its application as mixer-oscillator in the front end, substitution is very critical. It is important to choose a substitute type tube whose interelectrode capacitance is very similar and which was designed for the same circuit. If the interelectrode capacitance is not too different from that of the original, adjustment of the oscillator tuning slug will resonate the oscillator circuit at the proper frequency. For further information on the operation of the oscillator section, refer to the paragraph discussing high-frequency triodes used as local oscillators in the front end. When twin triodes are used (with one triode as the local oscillator and the other as the mixer), so long as the oscillator circuit operates properly with the substitute, the mixer circuit can usually be relied upon to operate equally well. The mixer alignment should be checked and adjusted if necessary.

Sync separators operate at low frequencies and at low power. They are considered noncritical as to substitutions. In making your choice of a substitute for this circuit you need give little consideration to the interelectrode capacitance and to the recommended operating frequency of the type used. Try to choose a type in which the plate current, amplification factor and grid bias are approximately the same as the original.

Video amplifiers are wide-band amplifiers, and, therefore, when choosing a substitute type, select one that has similar interelectrode capacitance in order to insure uniform amplification throughout the entire band.

The vertical oscillator and the vertical output stage functions in television receivers are ordinarily performed by the same tube when a triode is employed. It is important when choosing a substitute for these stages that the substitute type have equal or higher power rating characteristics. All other characteristics are relatively unimportant, and the circuit is generally considered non-critical as to substitutions.

The horizontal oscillator and frequency control circuit functions are sometimes performed by the same tube. The circuits are also considered fairly non-critical as to substitutions. When choosing a substitute for these circuits,
select one that has similar power rating characteristics. The interelectrode capacitance has little effect on the circuit.

## High-power Beam Pentodes

These types, as used intelevision receivers, were especially designed for use with magnetically deflected picture tubes. Effectively, they are redesigned versions of the high-power audio output pentode tubes as used in low power amplifiers. They are highly insulated in order to withstand the high peak voltages in the horizontal output circuit of a television receiver. The high output power needed requires these tubes to be so designed that they draw high plate current while using low operating voltages. When substituting in this circuit, it is important that the substitute be capable of equal or higher output as compared with the original type.

## Damper Rectifiers

Damper rectifiers with indirectly heated cathodes are especially designed for television service and are capable of withstanding high peak inverse voltages and of producing fairly high output currents. When choosing a substitute for the damper stage, be sure that it is capable of withstanding the high voltage without flashover and that it has at least an equal current rating as compared to the original. A high percentage of failure of this tube type is due to flashover between the heater and cathode. If no substitute tube is available that has an equal or higher peak inverse and output current rating, try an ordinary radio power rectifier that has the required output current rating. The filament must be heated by a separate transformer having a breakdown voltage rating of not less than 3,000 volts. When this substitution is made in a transformer-type television receiver, the original filament leads should be disconnected and securely taped. In transformerless receivers, where the damper tube filament is a part of a series circuit, the original filament leads must be disconnected from the socket and reconnected to a resistor of the correct value to properly complete the filament circuit. Data for computing the filament resistor necessary is contained in the Receiving Tube Substitution Guide Book.

## Twin Diodes

Twin diode tubes are generally used in three different television circuits. These are the video detector, the horizontal discriminator, and the sound detector. There is a very limited choice in this classification. It may sometimes be found necessary to use the corresponding diodes in some multi-purpose tube to accomplish substitution in these stages. When this is done, connect all unused elements in the substitute tube to ground. If a substitute tube is not available, any of these circuits can be made operative by the use of a pair of germanium crystal diodes whose current ratings are comparable to the original tube. When a substitution has been made in the sound detector, the last i-f sound stage should be checked for alignment. When a substitute has been made in the video detector, the alignment of the last video i-f stage should be checked and realignment performed if necessary.

## Triple-diode Triodes

Triple-diode triodes especially designed for television receivers are frequently used in the ratio detector and first audio circuits. There are a very limited number in this classification of tubes. The circuits are considered fairly non-critical as to substitutions, but the problem of finding a substitute with the necessary quantity of elements may be difficult. A good substitute, however, is a duo-diode triode having similar characteristics and the addition of a germanium crystal diode to take the place of the missing diode element. Where space is not a factor in the substitution, a combination of two tubes may be used to accomplish the same purpose. When making substitutions of this kind, select a tube with a triode section that has similar characteristics to the original type. Realignment of the last sound i-f stage is ordinarily necessary after this substitution has been made.

## Gated Beam Pentodes

Designed especially for television and f-m receivers, the gated beam pentode is used in the $\mathrm{f}-\mathrm{m}$ detector circuit and in the vertical oscillator circuit. No other tube type can be easily substituted in this circuit. The number
of types available in this classification are very few.

When this tube is not available, it will be necessary to substitute another circuit using conventional tubes. A ratio detector should be substituted for the $\mathrm{f}-\mathrm{m}$ sound detector. The reason for suggesting a ratio detector circuit is that a limiter stage is not usually required. Since the gated beam tube f-m detector does not require the limiter stage, the ratio detector circuit involves fewer circuit changes. This substitution could be accomplished with a triplediode triode tube such as the 6T8 or with a duo-diode triode such as the 6AT6 in conjunction with a germanium diode crystal. It is necessary to change the last sound i-f transformer to a ratio detector transformer and to change any other components necessary for this new circuit.

If the gated beam pentode is used as the vertical oscillator, it will again be necessary to change the circuit when the original type or a similarly classified type tube is not available. Any conventional triode having the required characteristics may be used as the vertical oscillator if the blocking oscillator circuit is employed. Any conventional twin triode with the required characteristics may be used if the multivibrator oscillator circuit is employed.

## High-frequency Triode Pentodes

These types are recent additions to special television types and are for use in the front end as the local oscillator and mixer. Like the high-frequency triode tube used as the local oscillator in the front end, they are very critical as to substitution. The type is composed of two separate sections: a high-frequency triode for use as the local oscillator and a pentode section for use as a mixer. The interelectrode capacitance of any substitution for these types must be very similar to the original. Shielding these types will change the circuit capacitance considerably. Since the variety of these types is very limited, it may be necessary to use two tubes as a substitute. The placement and the length of the connecting leads are a critical consideration when mechanical and wiring changes are required. The older type triode pentodes such as the 6F7, 6AD7, and 6P7 are not capable of operation on television frequencies and cannot be satisfactorily used as substitutes.

## EXAMPLES OF PRACTICAL TELEVISION TUBE SUBSTITUTIONS

RCA 630TS. The following substitutions were made in an RCA 630TS television chassis. This chassis is not only used in RCA television receivers but also in a great many other brand sets.

Before the substitutions were made, all tubes and component parts in the set were carefully checked and found to be in good condition. The chassis was also carefully and completely realigned for peak performance. Suitable test equipment was used to show the differences in the response curves with the original and substitute tubes.

The procedure was as follows: The response curve of the stage in which the substitution was to be made was observed on an oscilloscope and the gain and bandwidth were carefully noted. The substitute tube was then installed and the
difference in response and gain were tabulated. The set was then completely realigned for optimum output. The change in efficiency of operation was then noted. The original tube was then reinstalled and the set was again completely realigned and made ready for the next substitution.

Component parts were changed to adjust the bias and operating voltages of the substitute tube when required. In none of the following substitutions was there enough improvement to justify the use of the substitute rather than the original tube. A change in alignment was necessary in some cases in order to retain the correct response curve. In a few cases it was necessary to readjust the sound traps after making a substitution.

The results of making substitutions for the video i-f amplifiers follow. The original tube was a 6AG5.

RCA 630 TS Video I-f Amplifier Substitutions

| Substitute | Stage | Circuit Changes and Results |
| :---: | :---: | :---: |
| 6AU6 | 1st, 2nd, 3rd video i-f | No changes. Results equal to original after careful realignment. |
| 6AU6 | 4th video i-f | This substitution is not recommended. |
| $6 \mathrm{BC5}$ | 1st, 2nd, 3rd video i-f | No changes. Results equal to original without realignment. |
| $6 \mathrm{BC5}$ | 4th video i-f | No changes. Results equal to the original after careful realignment. |
| 6AK5 | All video i-f | No changes. Different heater current but, because of parallel connection, no rewiring required. |
| 6CB6 | All video i-f | The cathode and suppressor grids are connected internally in the 6AG5 but these elements are separate on the 6CB6. Connect pins 2 and 7 together on the socket. If pin 2 is used as a tie point on the 6AG5, remove leads from pin. Solder these together and tape. Results equal to original. |
| 9003 | All video i-f | No changes. About 5 percent loss in gain after careful realignment. |
| 6AH6 | 1st, 2nd, 3rd video i-f | Results equal to original after careful realignment. |
| 6 AH 6 | 4th video i-f | This substitution is not recommended. |

RCA 630 TS Video I-f Amplifier Substitutions (cont'd)

| Substitute | Stage | Circuit Changes and Results |
| :--- | :--- | :--- |
| 6BA6 | 1st, 2nd video i-f | No changes. Results equal to original without realign- <br> ment. |
| 6BA6 | 3rd video i-f | No changes. About 20 percent loss in gain after care- <br> ful realignment. |
| 6BA6 | 4th video i-f | No changes. About 30 percent loss in gain after care- <br> ful realignment. <br> Connect pins 2 and 7 together on socket. Results <br> equal to original after careful realignment. |
| 6BD6 | 1st, 2nd, 3rd video i-f | Connect pins 2 and 7 together on socket. Results <br> equal to original without realignment. |

The results of making substitutions for the 1st video amplifier follow. The original tube was a 6 AU6.

RCA 630 TS 1st Video Amplifier Substitutions

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 6CB6 | No changes. About 10 percent increase in gain. |
| 6AG5 | No changes. About 20 percent increase in gain after <br> careful realignment of 4th video i-f stage. |
| 6AK5 | No changes. Heater current differs, but, since par- <br> allel connection is used, no rewiring required. About <br> 30 percent increase in gain. |
| 6BA6 | No changes. Results equal to original without realign- <br> ment. |
| 6BH6 changes. The suppressor grid and cathode pin |  |
|  | connections are reversed but both are connected to <br> the same point. Results equal to original without <br> realignment. |

The results of making substitutions for the 2 nd video amplifier follow. The original tube was a 6K6.

RCA 630 TS 2nd Video Amplifier Substitutions

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 6 F 6 | No changes. Heater currents differ, but this is a <br> parallel circuit. Operates well without change or <br> adjustment. |

## SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

## RCA 630 TS 2nd Video Amplifier Substitutions (cont'd)

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 6L6 | No changes. Heater currents differ, but this is a <br> parallel circuit. About 20 percent increase in gain <br> without adjustment. |
| 6U6 | No changes. Heater currents differ, but this is a <br> parallel circuit. About 20 percent increase in gain <br> without adjustment. |

The results of making substitutions for the first two sound i-f amplifiers follow. The original tube used in the first two stages was a 6BA6.

RCA 630 TS Sound I-f Amplifier Substitutions

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 6AU6 | No changes. Equal results after realignment. |
| 6BD6 | No changes. About 50 percent loss in gain resulted. <br> This substitution is not recommended in other than <br> strong signal areas. |
| 9003 | No changes. Heater currents differ, but this is a <br> parallel circuit. About 20 percent loss in gain <br> resulted. |

Because of slight differences in tube characteristics and variations in television receiver circuits and operating voltages, results obtained in every case may not match exactly those results given above. However, diffierences in results should not be too great.

Belmont 18DX21A. A Number of tube substitutions were made in a Raytheon Belmont television set, model number 18DX21A. Exactly the same procedure was used as in the case of the RCA 630 TS. The results of making substitutions for the limiter stage follow. The original tube was a 12AU6.

Belmont 18DX21A Limiter Substitutions

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 12BA6 | No changes. Operation is equal to the original. Re- <br> alignment does not improve operation. |
| 12BD6 | No changes. About 30 percent loss in gain. Realign- <br> ment and changes in operating voltages were at- <br> tempted without satisfaction. If the set is located in <br> a strong signal area little change will be noticed. Do <br> not attempt this substitution for fringe area operation. |

Belmont 18DX21A Limiter Substitutions (cont'd)

| Substitute | Circuit Changes and Results |
| :---: | :--- |
| 12AW6 | The suppressor grid and cathode are connected to <br> opposite pins. In this set these elements are con- <br> nected together; therefore, no change is required. <br> Substitution gives a 30 percent increase in gain <br> without realignment and is recommended for fringe <br> area operation. |

The results of making substitutions for the i-f stages follow. The original tubes used were 6BA6's.

Belmont 18DX21A I-f Amplifier Substitutions

| Substitute | Stage | Circuit Changes and Results |
| :--- | :--- | :--- |
| 6AU6 | 1st i-f | No changes. Results equal to original after careful <br> realignment. |
| 6AU6 | 2nd i-f | No changes. About 30 percent increase in gain after <br> careful realignment. Recommended for fringe area <br> operation. |
| 6AU6 | 3rd i-f | No changes. Results equal to original. No realign- <br> ment required. |
| 6BD6 | 1st i-f | No changes. About 10 percent loss in gain after <br> careful realignment. |
| 6BD6 | And, 3rd i-f i-f | No changes. Results equal to original after careful <br> realignment. |
| 6CB6 | 1st i-f | No changes. Results equal to original after careful <br> realignment. |
| 6BC5 | 2nd, 3rd i-f | No changes. Results equal to original after careful <br> realignment. |

In addition to the above, a 19C8 was substituted for the 19 T 8 FM discriminator and first audio amplifier. No changes were required. The only apparent result was a slight loss in audio gain.

As pointed out previously, because of slight differences in tube characteristics and variations in circuits and voltages, the exact results given above may not always be obtained. However, great differences should not be found.

## SECTION 2

## RECEIVING TUBE SUBSTITUTION GUIDE

This section includes the actual information on the tube substitutions. The same format is followed as was used in the Receiving Tube Substitution Guide Book. Four columns are used. The first column gives the tube type for which a substitute is desired. The listing is in numer-ical-alphabetical order. No distinctions are indicated insofar as glass or metal tubes are concerned and the letters G, GT, GT/G, GA, or GP all have been omitted. In most cases, these letters simply indicate a glass type whose characteristics are practically the same as the metal type having the corresponding type number.

Column three lists the performance rating. Substitutions that we have found through practical experience will operate with equal or very nearly equal results compared to the original and those that have equal or nearly equal electrical characteristics are given a performance classification of $E$ for EXCELLENT. Substitutions that we have found to operate satisfactorily, although they do show a distinct loss, or those that have the same functional classification as the tube being substituted for but whose electrical characteristics are from 20 percent to 50 percent different, are classified G for GOOD. Others that are less efficient but which did operate in a fashion and those whose functional classification is different or whose critical characteristics are unlike the original by more than 20 percent are classified $P$ for POOR. These are recommended for emergency use only.

Column four gives the necessary circuit changes. It is impractical to include a listing of component part changes in order to alter the circuit with the substitute tube. The changes would vary widely with the type of circuit and the applied voltages; therefore, information correct for some sets would be grossly incorrect for others. Because of this, substitutions other than those classified $E$ are not completely worked out for you. However, those
substitutions classified G are satisfactory in most cases without component part changes, thus saving the equipment owner added parts and labor changes. A complete discussion covering the technique of computing substitute bias and load resistance is contained in the Receiving Tube Substitution Guide Book. When making changes in component parts, always make a complete record of the original values of the circuit altered, and securely attach it to the chassis of the equipment.

The necessary wiring changes, socket changes, and filament voltage adjustments are described in detail for each substitution listed. The instruction "No changes" indicates that the base wiring for the substitute is the same and that the filament voltage and current ratings are equal. The note "Parallel circuits only" indicates that the filament current ratings of the two tubes are unequal. This note is appended to some types that are not usually used in other than parallel circuits. This has been done to make the information more uniform and less confusing to the novice.

A few substitutions are followed by the note "Series circuits only." In these, the filament current of the substitute is equal to that of the original but the filament voltage is unequal. If the filament voltage of the substitute is higher than the original, then the voltage is reduced on all the other tubes in the circuit. If the substitute has a lower filament voltage rating, the voltage is increased on all the other tubes in the circuit. A series filament resistor is recommended where the increase in voltage amounts to more than five percent. When making substitutions requiring rewiring or socket changes, always make a note showing the original type used and the circuit in which the substitution is made. Then attach the note securely to the chassis.

Some substitutions listed, like the nineprong noval series, have a heater center-tap
connection which permits them to be operated at either 6.3 volts or 12.6 volts. These types are almost always numbered to indicate the higher heater voltage (12AT'7, 12AU7). These types are listed as substitutes for the 6 and 7 series tubes having 6.3 -volt heaters. When this is done the two halves of the noval tube heater are connected in parallel, thus cutting the necessary filament voltage in half and doubling the current required. Depending on the heater current of the type being substituted for, these types may be marked "Parallel circuits only" or they may be usable in either parallel or series circuits. These same tubes may be listed elsewhere as substitutes for 12.6 -volt heater types. Whether these types are used as substitutes for 6.3 -volt or 12.6 -volt tubes, they will be operating at the proper voltage.

Some miniature tubes with 12.6 -volt heaters do not have tapped heaters. These are usually used in series circuits that are connected
directly to the line. Occasionally, a 12.6 -volt winding is provided on the power transformer for the heaters in a parallel circuit.

When substituting for 12.6 -volt tubes in series circuits with 6.3 -volt types having equal current ratings, the increase in voltage spread over all the other tubes is small and need not be considered. However, it is good practice to shunt a small resistor of about 300 ohms across the heater of the 6.3 -volt tube in order to reduce the current flow through it during the time it takes for the tubes to heat. When a transformer winding is provided for the 12.6volt tube and it is desired to use a 6.3 -volt type, this can be done simply by moving one of the socket heater connections to the center-tap of the heater winding.

It should be pointed out that when "electric operation" is referred to in the substitutions which follow, the term is taken to mean nonbattery operation. In other words, the receiver is to operate from the power line.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 0A3 | 0B3 | P | No changes. |
| $0 \mathrm{Z4}$ | 6 AX5 | E | Rewire as follows: <br> Connect No. 2 to chassis <br> Connect No. 7 to 6 volt filament. |
|  | 6AX6 | E | Rewire as follows: <br> Connect No. 4 and No. 8 together Connect No. 2 to chassis Connect No. 7 to 6 volt filament. |
|  | 6BY5 | E | Rewire as follows: No. 3 No. 4 Connect No. 1 and No. 8 together Connect No. 2 to chassis Connect No. 7 to 6 volt filament. |

6V4 E Change socket to noval and rewire as follows:


6X4 E Change socket to miniature and rewire as follows:


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| OZ4 | 6 Y 5 | E | Change socket to six prong and rewire as follows: <br> No. 3 on octal to No. 3 on six prong <br> 5 <br> to <br> 5 <br> 8 to 4 <br> Connect pin No. 1 on six prong to chassis Connect pin No. 6 to 6 volt filament. |
|  | 6 Z5 | E | Change socket to six prong and rewire as follows: |
|  | 6ZY5 | E | Same as 024 to 6AX5. |
|  | 724 | E | Change socket to loctal and rewire as follows: 3 (9) |
|  | 1274 | E | $\text { No. } 3 \text { on octal }$5 to 6 <br> 8 to 7 <br> Connect No. 8 on loctal to chassis and No. 1 on loctal to 6 V hot lead. |
| $1 \mathrm{A4}$ | $\begin{aligned} & 1 \mathrm{~A} 4 P \\ & 1 \mathrm{~A} 4 \mathrm{~T} \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
| 1 A5 | 1 W 4 | G | Change socket to miniature and rewire as follows: |
|  |  |  | No. 2 on octal <br> $\begin{array}{ll}\text { to No. } & 7 \text { on miniature } \\ \text { to } & 2 \\ \text { to } & 3 \\ \text { to } & 6 \\ \text { to } & 1\end{array}$ |
|  | $\begin{aligned} & \text { 3LE4 } \\ & \text { 3LF4 } \end{aligned}$ | $\mathbf{P}$ | Electric operation only. Same as 6W6 to 7A5 except do not connect No. 8 on octal to No. 7 on loctal. |
| 1 A 5 | 3V4 | $\mathbf{P}$ | Electric operation only. Change socket to miniature and rewire as follows: |
|  |  |  | No. <br> to No. 1 on miniature <br> Do not use pin No. 5. |
| 1 A 7 | 1 LB6 | G | Change socket to loctal and rewire as follows: |
| $1 \mathrm{AE4}$ | 1 L4 <br> 1 T4 <br> 1 U4 | $\begin{aligned} & P \\ & P \\ & P \end{aligned}$ | Parallel circuits only. Not satisfactory for oscillator. No changes. |
| 1 AF5 | 1 U5 | G | Parallel circuits only. Change connections as follows: <br> Remove, connect and tape up any wires connected to No. 2 <br> Connect No. 5 to No. 2 <br> Reverse connections between Nos. 3 and 4 |

Change socket to four prong and rewire as follows:


No. 2 on octal to No. 1 cap

| to | 4 |
| :--- | :--- |
| to cap |  |



Required filament voltage for $\mathbf{1 Y 2}$ is $\mathbf{0 . 2 5}$ volt higher but operates satisfactorily in most cases.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 1B3 | $1 \mathrm{Z2}$ | G | Parallel circuits only. Same as 1B3 to 1X2A Filament voltage 0.25 volts higher. Do not use on large sets where inverse peak voltage exceeds 20,000 volts. |
| 1 C 5 | 1W4 | G | Parallel circuits only. Same as 1A5 to 1W4. |
|  | $\begin{aligned} & 3 \mathrm{LE} 4 \\ & \text { 3LF4 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Change socket to loctal and rewire as follows: |
|  | 3V4 | G | Change socket to miniature and rewire as follows: |
| 1 F4 | 1 J 5 | G | Change socket to octal and rewire as follows: |
|  | $\begin{aligned} & 33 \\ & 950 \end{aligned}$ | $\underset{\mathbf{G}}{\mathbf{G}}$ | Parallel circuits only. No changes. No changes. |
| 1 F 5 | $\begin{aligned} & 1 \mathrm{J5} \\ & 33 \\ & 950 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. <br> Reverse 1 F4 to 1 J 5 procedure, parallel circuits only. Reverse. 1F4 to 1 J 5 procedure. |
| 1G5 | 1 F4 | E | Reverse 1F4 to 1 J 5 procedure. |
|  | 1 F5 | E | No changes. |
|  | 33 | G | Reverse 1F4 to 1J5 procedure. Parallel circuits only. |
|  | 950 | G | Reverse 1F4 to 1J5 procedure. |
| $1 \mathrm{G6}$ | 19 | G | Parallel circuits only. Change socket to six prong and rewire as follows: |
| 1 H 4 | 1G4 | E | No changes. |
| $1 \mathrm{H5}$ | 1 N6 | G | Rewire as follows: <br> Remove, connect, and tape up any wires anchored on No. 4 and No. 6 Connect No. 3 and No. 4 together. <br> No. 5 to No. 6 <br> Grid lead to No. 5 |
|  | 1SB6 | E | Change connections as follows: <br> Remove, connect, and tape up any wires anchored on terminals No. 4 and No. 8. |

1 U5 G Change socket to miniature and rewire as follows:


| 1J5-1LE3 |  | SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE |  |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 1 J 5 | 1 F4 | G | Reverse 1F4 to 1 J 5 procedure. |
|  | 1 F5 | G | No changes. |
|  | 33 | G | Reverse 1F4 to 1J5 procedure. Parallel circuits only. |
|  | 950 | E | Reverse 1F4 to 1 J 5 procedure. |
| $1 J 6$ | 1G6 | G | Parallel circuits only. No changes. |
| $1 \mathrm{L4}$ | 1 S 5 | G | Same as 1 T4 to 1S5 |
|  | 1 U5 | G | Cut off pin No. 4 on 1 U 5. <br> Rewire as follows: <br> Connect No, 1 \& 5 together. |
| 1 L 6 | 1 R 5 | G | Reverse connections between No. 5 and No, 6. |
|  | 1 U6 | G | Connect a 56 ohm $\frac{1}{2}$ watt resistor from terminal No. 1 to No. 7 when used in series circuits. Resistor not required in parallel circuits. No other changes. |
| $1 \mathrm{LA4}$ | 3D6/1299 | G | Parallel circuits only. Same as 1LB4 to 3D6. |
|  | $\begin{aligned} & \text { 3LE4 } \\ & \text { 3LF4 } \end{aligned}$ | $\begin{aligned} & \mathbf{P} \\ & \mathbf{P} \end{aligned}$ | For electric operation only. Rewire as follows: Remove, connect, and tape up any wires connected to pin No. 7 of 1 LA 4. |
|  | $\begin{aligned} & \text { 3LE4 } \\ & \text { 3LF4 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Change connections as follows: Remove No. 8 lead and connect to No. 7 Connect No. 1 and No. 8 together. |
|  | 3V4 | P | Electric operation only. Change socket to miniature and rewire as follows: |
|  | 3V4 | G | Parallel circuits only. Change socket to miniature and rewire as follows: |
|  |  |  |  |
| 1LB4 | $\begin{aligned} & \text { 3LE4 } \\ & \text { 3LF4 } \\ & \text { 3D6/1299 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{P} \end{aligned}$ | Parallel circuits only. Change connections as follows: Remove No. 8 lead and connect to No. 7 Connect No. 1 and No. 8 together. |
|  | 3 V 4 | P | Same as 1 LA4 to 3V4 for electric operation only. |
|  | 3V4 | G | Same as 1LA4 to 3V4 for parallel circuits only. |
| 1 LE 3 | $1 \mathrm{L4}$ | G | Change socket to miniature and rewire as follows: |
|  | 1 T 4 $1 \mathrm{U4}$ | $\stackrel{\mathbf{G}}{\mathbf{G}}$ | No. 1 on loctal |
|  | $\begin{aligned} & 1 \text { LC5 } \\ & 1 \text { LG5 } \\ & 1 \text { LN5 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Rewire as follows: <br> Remove, connect, and tape up any wires anchored on No. 3. Do the same for No. 4. <br> Connect No. 2 and No. 3 together. <br> Connect No. 4 and No. 5 together. |



Parallel circuits only. Change socket to miniature and rewire as follows:


No.
1 on loctal
2
3
4
6
8


G
Change socket to octal and rewire as follows:


G
Change socket to miniature and rewire as follows:


| No. $\begin{aligned} & 1 \text { on loctal } \\ & 2 \\ & 3 \\ & 4 \\ & 4 \\ & 6 \\ & 8\end{aligned}$ |  |
| :---: | :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |



1 LD5

P
Parallel circuits only. Change socket to octal and rewire as follows


No. 1 on loctal

Connect No. 3 and No. 4 to No. 1
Cap connection not used.

1LH4-IS4
TUBE SUB.
1 LH 43 A 8
TUBE SUB. PERF.

Electric operation only. Change socket to octal and rewire as follows: No. 1 on loctal to No. 2 on octal

.
2
4
6
8

| to | 6 |
| :--- | :--- |
| to | 8 |
| to | 5 |
| to | 7 |

Connect No. 2 and No. 3 to No. 1 .

| 1LN5 | 1 L 4 | G |
| :--- | :--- | :--- |
|  | 1 T4 | G |
|  | 1 U 4 | E |
|  | 1 LG 5 | G |
|  |  |  |
| 1N5 | 1 U 5 | G |

Same as 1 LG5 to 5910.

No changes.
Change socket to miniature and rewire as follows:


G
Change socket to miniature and rewire as follows:


No. 2 on octal
3
4
5
7
to No. 1 on miniature

| to No. | 1 on miniature |
| :--- | :--- |
| to | 2 |
| to | 4 |
| to | 3 |
| to | 7 |

1 LC5
1 LG5
1 LN5

G Parallel circuits only. No changes.
G Parallel circuits only. Same as 1A5 to 1 W4.
P Same as 1C5 to 3LE4. Same as 1C5 to 3LE4.

Same as 1C5 to 3V4.
Parallel circuits only. Change connections as follows:
No.

| to | 3 |
| :--- | :--- |
| to | 1 |



|  | 1 U | G | Cut off pin No. 4 on 1 U 5 . Connect terminals No. 1 \& No. 5 together. |
| :---: | :---: | :---: | :---: |
| 1 T 5 | 3 LE 4 | G | Parallel circuits only. Same as 1C5 to 3LF4. |
|  | 3LF4 | G |  |
|  | 1W4 | G | Same as 1A5 to 1W4. |
|  | 3V4 | P | Electric operation only. Same as 1A5 to 3V4. |
| $1 \mathrm{U4}$ | 155 | G | Same as 1 T4 to 155. |
|  | 1 U5 | G | Cut off pin No. 4 on 1U5. Rewire as follows: Connect No. 1 and No. 5 together. |
| 1 V | 14Y4 | G | Series circuits only. Same as $12 \mathrm{Z3}$ to 14Y4. |
|  | 37 | G | Change socket to five prong and rewire as follows: |
|  | 76 | G |  |
| $1 W^{4}$ | 154 | G | Parallel circuits only. Rewire as follows: <br> $\begin{array}{lll}3 & \text { to No. } 4 \\ 6 & \text { to } & \\ 6\end{array}$ <br> Do not use pin No. 6 as anchor. |
| $1 \times 2$ | 1 Y 2 | E | Change socket to four prong and rewire as follows: <br> Nos. 1, 4, 6,\& 9 on noval to No. 1 on four prong. Nos. 2, 5, \& 8 on noval to No. 4 on four prong. Cap on Noval to cap on four prong. |
|  |  |  | 19 |

1×2-385
TUBE SUB.

PERF

Change socket to octal and rewire as follows:

$\begin{array}{ll}2,5,7 & \text { to } \\ \text { cap } & \text { to }\end{array}$

G Parallel circuits only. Reverse 1B3 to 1Y2 procedure. Filament voltage will be 0.25 volts high on 1B3 and will serve to shorten its life. A small piece of resistance wire placed in series with the filament will correct this.

E
Change socket to four prong and rewire as follows:


No. 1 on four prong
to No. 2 on noval
cap

Change socket to miniature and rewire as follows:


No. 1 on four prong
to No. 1
4 to
cap to
Connect No. 1, 3, 4, and 6 together.
Connect No. 2, 5, and 7 together.


Do not use where inverse peak voltage exceeds 20,000 volts.
Change socket to noval and rewire as follows:
Nos. $1,3,4, \& 6$ on miniature to Nos. $1,4,6, \& 9$ on noval.
Nos. 2,5, \& 7 on miniature to Nos. 2, 5, \& 8 on noval.
Cap on miniature to cap on noval.


Reverse 1Y2 to $1 \mathrm{Z2}$ procedure.


Nos. $1,3,4,6$ on miniature to No. 2 on octal
rmits. Change socket to octal and rewire as follows:
cap


No. 1 on four prong
4
cap
to 4

Parallel circuits only. Change socket to six prong and rewire as follows:


No. 1 on four prong


G Parallel circuits only. Change socket to five prong and rewire as follows:


No. 1 on four prong 2
3
4

Same as 1Q5 to 1 S 4 .
Change socket to miniature and rewire as follows:

| No. 2 on octal | to No. 1 on miniature |  |
| :--- | :--- | :--- |
| 3 | to | 2 |
| 4 | to | 3 |
| 5 | to | 6 |
| 7 | to | 7 |
| 8 | to | 5 |

SUB.
PERF.
CIRCUIT CHANGES NECESSARY

3LF4
3 LE4

3LF4

6 A6

6 A7

627

6AN7

6BA7

7A8

6AN7

E

G
G
$\mathbf{G}$

E
$\underset{\mathbf{G}}{\mathrm{E}}$
$\stackrel{E}{\mathrm{E}}$
$\underset{\mathbf{G}}{\mathbf{G}}$

Change socket to miniature and rewire as follows:

| No. 1 on loctal | to No. 1 on miniature |  |
| :--- | :--- | :--- |
| 2 | to | 2 |
| 3 | to | 4 |
| 6 | to | 3 |
| 7 | to | 5 |
| 8 | to | 7 |

Change socket to octal and rewire as follows:
No. 1 on loctal


No changes.
Same as 3LE4 to 3 Q4.

Same as 3LE4 to 3 Q5.

| 3Q4 | E |
| :---: | :---: |
| 3S4 | G |
| 3Q5 | E |
| 3B5 | E |
| 3C5 | G |
| 6 Y 7 | G |
| $6 \mathrm{Z7}$ | G |

G Parallel circuits only. Change socket to loctal and rewire as follows:

G Parallel circuits only. Change socket to noval and rewire as follows: No. 2 on octal


G Change socket to noval and rewire as follows:


No. 1 on seven prong

No. 1 on seven prong to No. 1 on loctal

2
3
4
5
6
7 to No. 4 on noval

3
4
5
cap
6
7
8

| to | 7 |
| :--- | :--- |
| to | 1 |
| to | 9 |
| to | 2 |
| to | 8 |
| to | 5 |
| to | 3 |



No. 1 on seven prong

2
3
4
grid cap
5
6
7

| to No. | 4 |
| :--- | :--- |
| to | 7 |
| to | 1 |
| to | 8 |
| to | 8 |
| to | 2 |
| to | 9 |
| to | 3 |
| to | 5 |



TUBE SUB.
6A8

6AD7
6 U8

PERF.
G


CIRCUIT CHANGES NECESSARY

Parallel circuits only. Change socket to noval and rewire as follows:



6CD6 G Parallel circuits only. Same as 6AR6 to 6BG6. Use only where additional current is available from the filament power supply.

G Parallel circuits only. Change socket to five prong and rewire as follows: No. 1 on octal to No. 4 on five prong.


## 6AU6-6C5



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6CB6 | 6 AG5 | G | No changes. |
|  | 6BC5 | G |  |
|  | 6 AJ5 | P | Parallel circuits only. No changes. |
|  | 6 AK5 | G |  |
|  | 5590 | G |  |
|  | 5591 | G |  |
|  | 5654 | G |  |
|  | 9001 | P |  |
|  | 9003 | P |  |


|  | 6AU6 6BA6 6BD6 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Change connections as follows: <br> Reverse connections between terminals 2 and 7. |
| :---: | :---: | :---: | :---: |
| 6CD6 | KT66 | G | Parallel circuits only. Reverse 6L6 to 6BG6 procedure. |
|  | 807 | P | Parallel circuits only. Reverse 807 to 6BG6 procedure. |
| 6CG6 | 6AG5 <br> 6AU6 <br> 6BA6 <br> 6BC5 <br> 6BD6 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. |
|  | 6AH6 6AJ5 6AK5 5590 5591 5654 9001 9003 | G $\mathbf{P}$ $\mathbf{G}$ $\mathbf{P}$ $\mathbf{G}$ $\mathbf{G}$ $\mathbf{G}$ $\mathbf{P}$ $\mathbf{P}$ | Parallel circuits only. No changes. |
| 6E6 | $\begin{aligned} & \text { 6N7 } \\ & 6 Z 7 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Same as 3LE4 to 3Q5. |
|  | $6 \mathrm{Y7}$ | G | Same as 3LE4 to 3Q5. |
| 6 F 6 | 6AQ5 | G | Parallel circuits only. Change socket to miniature and rewire as follows: |



|  | 6AN7 | G | Parallel circuits only. Same as 6A8 to 6AN7. |
| :---: | :---: | :---: | :---: |
|  | 6BA7 | G | Same as 6A8 to 6BA7. |
| $6 \mathrm{L5}$ | 6SJ7 | G | Parallel circuits only. Same as 6C5 to 6SJ7. |
| 6L6 | 6BG6 | E | Change connections as follows:   <br> No.   <br> 3 to cap  <br> 8 to 3 <br> 4 to 8 |
|  | 6CD6 | E | Parallel circuits only. Same as 6L6 to 6BG6. When making this substitution be sure the filament power supply is capable of supplying an additional 1.6 -ampere load. |

6J6-6L6

| TUBE | SUB. |
| :--- | :--- |
| $6 J 6$ | $6 S L 7$ |

$6 A 7$

G
6BA7
6SJ7
6BG6
$6 \mathrm{CD6}$
PERF.

SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE
CIRCUIT CHANGES NECESSARY
$P \quad$ Change socket to octal and rewire as follows:


E Parallel circuits only. Where space permits. Change socket to loctal and rewire as follows:


TUBE SUB.

| 6 L 6 | 41 |
| :--- | :--- |
|  | 42 |

KT66
E
E

5881
6SJ7
6 U 8
$6 \times 8$

| 6 P 7 |
| :--- |
|  |
|  |
|  |
|  |

$\mathbf{G}$
$\mathbf{G}$

PERF.
G
G

| 6Q7 | 6AT6 | $\mathbf{E}$ |
| :--- | :--- | :--- |
|  | 6AV6 | $\mathbf{G}$ |
|  | 6BK6 | $\mathbf{G}$ |
|  | 6BT6 | $\mathbf{E}$ |
|  | 6BU6 | $\mathbf{P}$ |


| 6R7 | 6AT6 | $\mathbf{P}$ |
| :---: | :---: | :---: |
|  | 6AV6 | P |
|  | 6BK6 | P |
|  | $6 \mathrm{BT6}$ | P |
|  | 6BU6 | E |
| 6R8 | 6 V 8 | P |
| $6 \mathrm{S4}$ | 12AT7 | G |
|  | 12AU7 | G |
|  | 12AV7 | G |
|  | $12 \mathrm{AX7}$ | G |
|  | 12AY7 | G |
|  | 12BH7 | G |

Change socket to five prong and rewire as follows:

| No. 2 on octal | to No. 1 on five prong |  |
| :--- | :--- | :--- |
| 3 | to | cap |
| 4 | to | 2 |
| $\mathbf{4}$ | to | 3 |
| 7 | (3) |  |
| $\mathbf{7}$ | to | 5 |
| 8 |  | 4 |



Parallel circuits only. No changes.
Same as 6C5 to 6SJ7.
Parallel circuits only. Change socket to noval and rewire as follows:


No. $\begin{aligned} & 2 \text { on } \\ & 3 \\ & 4 \\ & 5 \\ & \\ & \\ & \text { cap } \\ & 6 \\ & 7 \\ & \\ & 8\end{aligned}$


Change socket to miniature and rewire as follows:


Parallel circuits only. Change socket to six prong and rewire as follows:
No. 2 on octal


Parallel circuits only. No changes.
$\square$


No. 2 on octal

Same as 6Q7 to 6AT6.

Same as 6T8 to 6V8.
Parallel circuits only. Same as 6S4 to 12BH7.
12AU7
12AV7
$12 \mathrm{AY7}$

12BH7
Rewire as follows:

Remove wires from No. 5.
Connect No. 4 and No. 5 together.
$\begin{array}{lll}\text { No. } 6 & \text { to No. } 7 \\ 9 & \text { to } & 6\end{array}$
Connect wires removed from No. 5 to No. 9.
Reverse No. 2 and No. 3 connections.
Connect No. 3 and No. 8 together.
Connect No. 1 and No. 9 together.

6SA7-6SG7
TUBE SUB.
6SA7 6BA7

6BE6

7A8

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

## PERF. <br> CIRCUIT CHANGES NECESSARY

E

Change socket to noval and rewire as follows:


E
Change socket to miniature and rewire as follows:

|  | No. 1 on octal | to No. | 2 | miniature |
| :---: | :---: | :---: | :---: | :---: |
|  | 2 | to | 3 |  |
|  | 3 | to | 5 |  |
| (3) ${ }^{(3)}$ | 4 | to | 6 | (8) |
| (2) 0 | 5 | to | 1 | (3) |
| (1) ${ }^{(8)}$ | 6 | to | 2 | ( ) |
| onis. | 7 | to | 4 | sue. |
|  | 8 | to | 7 |  |

G Parallel circuits only. Change socket to loctal and rewire as follows: No. 1 on octal to shield connection on loctal socket to No. 1



The 7A8 heats faster than the other tubes and a 200 ohm $1 / 2$ watt resistor must be connected across the filament terminals 2 and 7 or its life will be very short.

| $6 S B 7 Y$ | 6BA7 | E |
| :--- | :--- | :--- |
|  | 6SA7 | G |
|  | $7 A 8$ | G |
|  |  | $7 B 8$ |
|  | $7 \mathrm{J7}$ | P |
|  | 7S7 | P |
|  | $7 \mathrm{Q7}$ | E |

E Change socket to loctal and rewire as follows:


| $6 S C 7$ | 12AT7 | $\mathbf{P}$ |
| :--- | :--- | :--- |
|  | 12AU7 | $\mathbf{P}$ |
|  | 12AY7 | $\mathbf{G}$ |
|  | 12AZ7 | $\mathbf{P}$ |
|  | 12AX7 | $\mathbf{E}$ |

Change socket to noval and rewire as follows:


|  | 12AV7 | $P$ |
| :---: | :--- | :--- |
|  | 12BH7 | $\mathbf{P}$ |
| 6SG7 |  | 6BA6 |
|  | 6AU6 | E |
|  | 6BD6 | $\mathbf{P}$ |

12BH7
6SG7

|  | 12AV7 | $\mathbf{P}$ |
| :---: | :--- | :--- |
|  | 12BH7 | $\mathbf{P}$ |
|  |  |  |
| 6SG7 | 6BA6 | $\mathbf{E}$ |
|  | 6AU6 | P |
|  | 6BD6 | $\mathbf{G}$ |

Same as 6SA7 to 6BA7.
No changes.
Parallel circuits only. Same as 6SA7 to 7A8.
Same as 6SA7 to 7A8. Series or parallel circuits.

Parallel circuits only. Same as 6SC7 to 12AT7.

Change socket to miniature and rewire as follows:


\begin{tabular}{|c|c|c|c|c|}
\hline TUBE \& SUB. \& PERF. \& CIRCUIT CHANGES NECESSARY \& \\
\hline 6SH7 \& \begin{tabular}{l}
6AU6 6BA6 \\
6BD6
\end{tabular} \& \[
\begin{aligned}
\& \mathbf{G} \\
\& \mathrm{P} \\
\& \mathbf{G}
\end{aligned}
\] \& Same as 6SG7 to 6BA6. \& \\
\hline 6SJ7 \& \[
\begin{aligned}
\& \text { 6AG5 } \\
\& \text { 6BC5 }
\end{aligned}
\] \& \[
\begin{aligned}
\& \mathbf{G} \\
\& \mathbf{P}
\end{aligned}
\] \& Change socket to miniature and rewire as follows: \&  \\
\hline \& \begin{tabular}{l}
6 AJ5 \\
6AK5 \\
5591 \\
9001 \\
9003
\end{tabular} \& \[
\begin{aligned}
\& P \\
\& P \\
\& P \\
\& P \\
\& P
\end{aligned}
\] \& Parallel circuits only. Same as 6SJ7 to 6AG5. \& \\
\hline 6SK 7 \& \begin{tabular}{l}
6AG5 \\
6BC5
\end{tabular} \& \[
\begin{aligned}
\& \mathbf{G} \\
\& \mathbf{G}
\end{aligned}
\] \& Same as 6SJ7 to 6AG5. \& \\
\hline \& \begin{tabular}{l}
6 AJ5 \\
6 AK5 \\
6AN5 \\
5591 \\
9001 \\
9003
\end{tabular} \& P
G
P
P
G
G \& Same as 6SJ7 to 6AJ5. \& \\
\hline \& \[
\begin{aligned}
\& \text { 6BH6 } \\
\& \text { 6BJ6 }
\end{aligned}
\] \& \[
\begin{aligned}
\& \mathbf{G} \\
\& \mathbf{G}
\end{aligned}
\] \& Parallel circuits only. Same as 6SK7 to 6CB6. \& \\
\hline \& 6CB6 \& G \& Change socket to miniature and rewire as follows:

No.

2 \& | 3 on miniature |
| :--- |
| 7 |
| 1 |
| 2 |
| 6 |
| 4 |
| 5 | <br>

\hline 6SL7 \& $7 \mathrm{F8}$ \& $\mathbf{P}$ \& Change socket to loctal and rewire as follows: \&  <br>

\hline \& $$
\begin{aligned}
& 12 \mathrm{AT} 7 \\
& 12 \mathrm{AU} 7 \\
& 12 \mathrm{AX} 7 \\
& 12 \mathrm{AY} 7
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathbf{G} \\
& \mathrm{P} \\
& \mathbf{G} \\
& \mathbf{G}
\end{aligned}
$$
\] \& Change socket to noval and rewire as follows: \&  <br>

\hline \& $$
\begin{aligned}
& 12 \mathrm{AV7} \\
& 12 \mathrm{BH} 7
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathbf{P} \\
& \mathbf{P}
\end{aligned}
$$
\] \& Parallel circuits only. Same as 6SL7 to 12AT7. \& <br>

\hline 6 SN7 \& $$
\begin{aligned}
& 12 \mathrm{AT7} \\
& 12 \mathrm{AU7} \\
& 12 \mathrm{AV7} \\
& 12 \mathrm{AX} 7 \\
& 12 \mathrm{AY} 7
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathbf{P} \\
& \mathbf{G} \\
& \mathbf{P} \\
& \mathbf{P} \\
& \mathbf{P}
\end{aligned}
$$
\] \& Parallel circuits only. Same as 6SL7 to \& <br>

\hline \& $$
\begin{aligned}
& 12 \mathrm{BH7} \\
& 12 \mathrm{SZ7}
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& \mathbf{G} \\
& \mathbf{G}
\end{aligned}
$$
\] \& Same as 6SL7 to 12AT7. \& <br>

\hline 6SQ7 \& 6SZ7 \& E \& Parallel circuits only. No changes. \& <br>
\hline
\end{tabular}

| 6U4 | $6 \mathrm{AX5}$ | G | No changes. |
| :--- | :--- | :--- | :--- |
| 6U5/6G5 | $6 \mathrm{AB5}$ <br> 6 N 5 | $\mathbf{G}$ | Parallel circuits only. No changes. |
|  | 6 G 5 | G | No changes. |
| 6U6 | 5881 | $G$ | Parallel circuits only. No changes. |

6SR7-6V8
TUBE SUB. PERF.
6SR7 7B6

7 E 6

7 C 6
85

6S8
6 T8

6V8

6U5/6G5

6U6

6V6

6BG6
6W6
6R8
6 T8

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE
CIRCUIT CHANGES NECESSARY
P Change socket to loctal and rewire as follows:

| No. 2 on octal | to No. 3 on loctal |  |
| :--- | :--- | :--- |
| 3 | to | 4 or 7 |
| 4 | to | 5 |
| 5 | to | 6 |
| 6 | to | 2 |
| 7 | to | 1 |
| 7 | to | 8 |

P Same as 6SR7 to 7B6.
G Change socket to six prong and rewire as follows:
No. 2 on octal


G Parallel circuits only. Where space permits, change socket to octal and rewire as follows:


G Change connections as follows:
Remove wires from No. 1.

| No. | 9 | to No. |
| ---: | :--- | :--- |
| 6 | to | 9 |
| 6 | to | 6 |
| 8 | to | 8 |
| 3 | to | 3 |
| 7 | to | 7 |

Connect wires removed from No. 1 to No. 2.

P Parallel circuits oniy. Change socket to octal and rewire as follows:
No. ${ }_{8}^{5}$ on octal


G Parallel circuits only. Same as 6L6 to 6BG6.

to No. 1 on miniature

G Parallel circuits only. No changes.
P Reverse 6T8 to 6V8 procedure.


7A7-7C5

| TUBE | SUB. |
| :--- | :--- |
| 7A7 | 6 BH 6 |
|  | 6 BJ 6 |
| 7A8 | $6 \mathrm{AN7}$ |

7AF7

7B4

7 B5

| B6 | 6AV6 |
| :---: | :---: |
|  | 6BF6 |
|  | 6BK6 |
|  | 6BT6 |
|  | 6BU6 |
| 7B7 | 6AU6 |
|  | 6BA6 |
|  | 6 BC 5 |
|  | 6BD6 |
|  | 6BH6 |
|  | 6BJ6 |

7 F8

7B6

7C6
6AQ5

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE
PERF.
P Parallel circuits only. Same as 7 B 7 to 6 BH 6 .
$P$
G

G
Rewire as follows:
Remove wires from No. 4
$\begin{array}{ll}\text { No. } 2 & \text { to No. } 4 \\ 1 & \text { to } \\ 2\end{array}$
Connect wires removed from No. 4 to No. 1. Remove wires from No. 5.
No. 7 to No. 5
Connect wires removed from No. 5 to No. 8.
Rewire as follows:
Remove and tape up any wires anchored on terminal No. 3.
Do the same for No. 4 and No. 5.
No. 6 to No. 3
Connect Nos. 4, 5, and 6 together.
E
G
Parallel circuits on

| No. 1 on loctal | to No. 3 on miniature |
| :--- | :--- |
| 2 | to |
| 3 | to |
| 6 | to |
| 7 | to |
| 7 | to |
| 8 |  |


| G |
| :--- |
| $\mathbf{G}$ |
| $\mathbf{P}$ |
| $\mathbf{G}$ |
| $\mathbf{G}$ |
| $\mathbf{P}$ |
|  |
| $\mathbf{G}$ |
| $\mathbf{E}$ |
| $\mathbf{G}$ |
| $\mathbf{G}$ |
| $\mathbf{G}$ |
| $\mathbf{G}$ |



Same as 7C6 to 6AQ6.

Parallel circuits only. Same as 7A7 to 6AU6.

Change socket to miniature and rewire as follows:


| 7AH7 | G | No changes. |
| :--- | :--- | :--- |
| 5590 | P | Same as 7A7 to 6AU6. |
| 5591 | P |  |
| 9001 | P |  |
| 9003 | G |  |
|  |  |  |
| $6 A N 7$ | G | Parallel circuits only. Same as 7A8 to 6AN7. |
| 6AQ5 | G | Same as 7B5 to 6AQ5. |


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 7 C 6 | 6AQ6 | G | Change socket to miniature and rewire as follows: |
|  | 6AT6 <br> 6AV6 <br> 6BF6 <br> 6BK6 <br> 6BT6 <br> 6 BU 6 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{P} \\ & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{P} \end{aligned}$ | Parallel circuits only. Same as 7C6 to 6AQ6. |
| $7 \mathrm{C7}$ | 6AU6 6BA6 6 BC5 6BU6 | $\begin{aligned} & \mathbf{E} \\ & \mathbf{G} \\ & \mathbf{E} \\ & \mathbf{E} \end{aligned}$ | Parallel circuits only. Same as 7A7 to 6AU6. |
|  | $\begin{aligned} & \text { 6BH6 } \\ & \text { 6BJ6 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Same as 7B7 to 6BH6. |
|  | 7AB7/1204 | P | Rewire as follows: <br> Remove wires from terminal No. 1 <br> $\begin{array}{ll}\text { No. } & 3 \\ 2 & \text { to No. } \\ 1\end{array}$ <br> Connect wires removed from No. 1 to No. 2 <br> Remove wires from No. 8 <br> No. 7 to No. 8 <br> Connect wires removed from No. 8 to No. 7 <br> No. 6 to No. 5 <br> Do not use terminals No. 4 or No. 6. |
|  | $\begin{aligned} & \text { 7AG7 } \\ & 7 \mathrm{AH} 7 \end{aligned}$ | $\begin{aligned} & P \\ & \mathbf{G} \end{aligned}$ | No changes. |
| 7 E 6 | 6AT6 6AV6 6BF6 6BK6 6BT6 6BU6 | $\begin{aligned} & P \\ & P \\ & \mathrm{P} \\ & \mathrm{P} \\ & \mathrm{P} \\ & \mathrm{E} \end{aligned}$ | Same as 7C6 to 6AQ6. |
| 7 F 8 | $7 \mathrm{F8}$ W | E | No changes. |
|  | $\begin{aligned} & 12 A T 7 \\ & 12 A U 7 \\ & 12 A X 7 \\ & 12 A Y 7 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{P} \\ & \mathbf{G} \end{aligned}$ | Same as 7F8 to 12AV7. |
|  | $\begin{aligned} & 12 \mathrm{AV7} \\ & 12 \mathrm{BH} 7 \end{aligned}$ | $\begin{aligned} & \mathbf{P} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Change socket to noval and rewire as follows: |
| 7G8 | 1206 | $\underline{5}$ | No changes. |
| $7 \mathrm{J7}$ | 6AN7 | G | Parallel circuits only. Same as 7A8 to 6AN7. |
| 7N7 | $\begin{aligned} & 12 A T 7 \\ & 12 A U 7 \\ & 12 A V 7 \\ & 12 A X 7 \\ & 12 A Y 7 \\ & 12 A Z 7 \end{aligned}$ | $\begin{aligned} & \mathbf{E} \\ & \mathbf{E} \\ & \mathbf{G} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Same as 7N7 to 12 BH 7. |

7N7-12A6

TUBE SUB.
7N7 12 BH 7

7Q7

7R7

7S7
7Y4

7 Z4

12A6

6SN7

PERF.

E


## CIRCUIT CHANGES NECESSARY

Change socket to octal and rewire as follows:

| No. 1 on loctal | to No. 8 on octal |  |
| :--- | :--- | :--- |
| 2 | to | 3 |
| 3 | to | 2 |
| 4 | to | 1 |
| 5 | to | 4 |
| 6 | to | 5 |
| 7 | to | 6 |
| 8 | to | 7 |

E Change socket to noval and rewire as follows:
No. 1 on loctal to Nos. 4 \& 5 on noval


G Parallel circuits only. Same as 14Q7 to 7A8.
G

Change socket to noval and rewire as follows:
No. 1 on loctal

| to No. 4 on noval |  |
| :--- | :--- |
| to | 6 |
| to | 7 |
| to | 8 |
| to | 1 |
| to | 2 |

G

E

E
$6 \times 4$
E

0 Z4

6 AX5

12A5

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

Same as $14 Q 7$ to 7A8. Series or parallel circuits.


Parallel circuits only. Same as 7A8 to 6AN7.
Same as 7 Y 4 to 6AX5. Filament leads need not be connected.
Parallel circuits only. Change loctal socket to octal and rewire as follows:


No. 1 on loctal
to No. 2 on octal
No. 1 on locta


Parallel circuits only. Change socket to miniature and rewire as follows:


Same as 7 Y 4 to $6 \mathrm{AX5}$. Filament leads need not be connected. If required output current exceeds 70 ma . this substitution is not recommended.

G Parallel circuits only. Same as 7Y4 to 6AX5. 6AX5 has lower output current rating. If required current exceeds 70 ma . this substitution is not recommended.

Parallel circuits only. Change octal socket to seven prong and rewire as follows:


TUBE
12A8

|  | $12 A Z 7$ | $P$ |
| :--- | :--- | :--- |
|  | $14 F 8$ | $G$ |
| $12 A V 7$ | $6 S N 7$ | $P$ |

PERF.
$P$ 7A8

## 12AU7

12AX7
12AY7 12AZ7

6AQ6 12AZ7 14F8

7 F8

6SN7

P
E
E
P

G
G
G
G

P

G
P

Series circuits only. No. 2 on octal


Change socket to noval and rewire as follows:


Do not use socket terminal No. 9 as tie point.
P Parallel circuits only. Same as 12AH7 to 12AU7.

12AZ7 E No changes.

12AW6 6BH6

For 12 volt operation on


Change socket to loctal and rewire as follows:

| No. 1 on noval | to No. 3 on loctal |  |
| :---: | :---: | :---: |
| 2 | to | 1 |
| 3 | to | 4 |
| 4 | to | 2 |
| 5 | to | 2 |
| 6 | to | 6 |
| 6 | (2) | 8 |
| 7 | (2) | 8 |
| 8 | to | 5 |
| 9 | to | 7 |

P Parallel circuits only. No changes.
For 12 volt operation only. Same as 12AT7 to 14 F8.
Parallel circuits only. Change socket to octal and rewire as follows:


Same as 12AW6 to 6BH6.
Parallel circuits only. No Changes.

For 12 volt operation in parallel circuits only. Same as 12 AT 7 to 14 F 8 .
No wiring changes necessary in series circuits. Install a $300 \mathrm{ohm}, \frac{1}{2}$ watt resistor from terminal No. 3 to terminal No. 4 on the socket.

In parallel circuits disconnect and tape up filament supply lead connected to terminal No. 3. Install new wire from terminal No. 3 to center tap of 12.6 volt filament winding.

## 12AX4-12SF5




14N7 E Same as 12SN7 to 14AF7. Series or parallel circuits.
Change socket to loctal and rewire as follows:


No. 2 on octal
3
4
5
6
7
8
to No. 3 on loctal


12SR7-14B6

| TUBE | SUB. |
| :--- | :--- |
| 12 SR 7 | $6 S T 7$ |

6 T7

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE
PERF.
P Series circuits only. No changes.
P Series circuits only. Make adaptor as follows:

| No. | to No. 1 on top |  |
| :---: | :---: | :--- |
| 2 | on base | to |
| 3 | cap |  |
| 4 | to | 8 |
| 5 | to | 4 |
| 5 | to | 5 |
| 6 | to | 3 |
| 7 | to | 7 |
| 8 | to | 2 |

7C6

14X7
12SW7

|  | 6 T 7 |
| :--- | :--- |
|  | 7 C 6 |
|  | 14 X 7 |
| 12 SY 7 | 12 BE 6 |

12Z3
14 Y 4

12AU6
12 BA 6
12BD6
12 AT 7
12 AU 7
$12 \mathrm{AX7}$
$12 \mathrm{AY7}$
$12 \mathrm{AZ7}$

| 12AV7 | P |
| :--- | :--- |
| 12BH7 | G |
|  |  |
| 12AT6 | G |
| 12AV6 | G |
| 12BF6 | P |
| 12BK6 | G |
| 12BT6 | G |
| 12BU6 | P |

CIRCUIT CHANGES NECESSARY

P
Series circuits only. Change socket to loctal and rewire as follows
No. 2 on octal

3
4
5
6
7
8


Same as 12 SQ 7 to 14 X 7 .
Series circuits only. Co changes.
Same as 12 SR 7 to 6 T7. Series circuits only.
Same as 12SR 7 to 7C6. Series circuits only.
Same as 12 SQ 7 to 14 X 7 .
Change socket to miniature and rewire as follows:


Change socket to loctal and rewire as follows:
No. 1 on four prong


2
3
4


Same as 7A7 to 6AU6.

Change socket to noval and rewire as follows:


Parallel circuits only. Same as 14AF7 to 12AT7.

Change socket to miniature and rewire as follows:



14N7-33

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 14 N 7 | 12 BH 7 | G | Same as 14AF7 to 12AT7. Series or parallel circuits. |
| 14 Q 7 | 7A8 | G | Series circuits only. Rewire as follows: <br> Remove wires from terminal No. 5 and tape up. No. 5 to No. 3 |
|  | $\begin{aligned} & \text { 12A8 } \\ & \text { 12K8 } \end{aligned}$ | $\begin{aligned} & \mathrm{P} \\ & \mathrm{G} \end{aligned}$ | Change socket to octal and rewire as follows: |
|  | 12BA7 | G | Change socket to noval and rewire as follows: |
|  | 12BE6 | G | Change socket to miniature and rewire as follows: |
|  | 1488 | G | Same as 14 Q 7 to 7A8. |
| 19C8 | 19V8 | G | Reverse 19 V 8 to 19 C 8 procedure. |
| 19 T 8 | 19V8 | G | Reverse 19 V 8 to 19 C 8 procedure. |
| 19V8 | $\begin{aligned} & 19 \mathrm{C} 8 \\ & 19 \mathrm{~T} 8 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | Rewire as follows: <br> Remove wires from No. 9 |
| 25N6 | 43 | P | Same as 6 L6 to 41. Series or parallel circuits. |
| 26Z5W | 25X6 <br> 25Z6 <br> 35Z6 | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \\ & \mathrm{P} \end{aligned}$ | Parallel circuits only. Change socket to octal and rewire as follows: |
| 33 | $\begin{aligned} & \text { 1F5 } \\ & \text { 1G5 } \\ & 1 \mathrm{J5} \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Parallel circuits only. Same as 1 F4 to 1J5. |


$50 \mathrm{Y7} \quad \mathrm{P}$

P
P

Rewire as follows:
Remove and tape up wires on No. 3. Do the same for Nos. 4 \& 6
Connect No. 3 and No. 5 together.
Connect No. 4 and No. 8 together.
Do not use terminal No. 6 .
Change socket to loctal and rewire as follows:
No. 2 on octal to No. 1 on loctal


Connect 40 ohm, 1 watt resistor from No. 1 to No. 3.

## 35Z5-50c6

| TUBE | SUB. | PERF. |
| :--- | :--- | :---: |
| $35 Z 5$ | $50 Y 6$ | P |
|  |  |  |
|  | 50 Y 7 | P |
|  | 50 Z 7 | P |
|  |  |  |
| $40 \mathrm{Z5}$ |  |  |
| 45 | 2 A 5 | G |
|  | 47 | G |
| $45 \mathrm{Z5}$ | 35 Y 4 | G |

50 C 6

## PERF.

P

G
P

14A5 G
35C5

35B5
35C5
50B5
35A5
E

E
E
E

## SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

Same as $35 Z 5$ to 50 Y 7 . Also connect a 40 ohm, 1 watt resistor from No. 2 to No. 6.

Rewire as follows:
Remove and tape up wires on No. 4. Do the same for No. 6 Connect No. 3 to No. 6 .
Connect No. 3 and No. 5 together.
Connect No. 4 and No. 8 together.
Refer to type $45 \mathrm{Z5}$ for substitute.
Parallel circuits only. Same as 2A3 to 2A5.
Parallel circuits only. Same as 2A3 to 47.
Change socket to miniature and rewire as follows:


Do not connect to unused terminals.
G Same as 35 Z 5 to 50 Y 6 .
G Same as $35 Z 5$ to 50 Z7.

35C5
Change socket to octal and rewire as follows:


Place a 250 ohm, 10 watt resistor in series with filament.
G Put a $250 \mathrm{ohm}, 10$ watt resistor in series with filament.
Rewire as follows:
Interchange No. 1 and No. 2 connections.
Interchange No. 5 and No. 7 connections.
Place $100 \mathrm{ohm}, 10$ watt resistor in series with filament.
Same as complete 50B5 to 35C5 procedure. Except that for 50B5 no filament resistor is required.

Change socket to loctal and rewire as follows:


Place $100 \mathrm{ohm}, 10$ watt resistor in series with filament.

35B5

E


No. $\begin{aligned} & 2 \text { on octal } \\ & 3 \\ & 4 \\ & 5 \\ & 7 \\ & 8\end{aligned}$


Do not use No. 7 on miniature. Place 100 ohm, 10 watt resistor in series with filament.

E
Change socket to miniature and rewire as follows:


Do not use terminal No. 5 on miniature. Place 100 ohm, 10 watt resistor in series with filament.

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 50C6 | 50B5 | E | Same as 50C6 to 35B5. |
| 50L6 | 14A5 | G | Same as 35 L 6 to 14 A 5 except place a 250 ohm , 10 watt resistor in series with filament. |
|  | 50A5 | E | Same as 35L6 to 14A5. Except do not add filament resistor. |
|  | 50 C 6 | E | No changes. |
| 50Y6 | 50X6 | E | Change socket to loctal and rewire as follows: |
| 57 | $\begin{aligned} & 35 / 51 \\ & 24 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | Parallel circuits only. Same as 34 to 1D5. |
| 58 | $\begin{aligned} & 24 \mathrm{~A} \\ & 35 / 51 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{G} \end{aligned}$ | Same as 57 to $35 / 51$ |
| KT66 | 6AL6 | G | Farallel circuits only. Same as 6L6 to 6AL6. |
|  | $\begin{aligned} & \text { 6BG6 } \\ & \text { 6CD6 } \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | Parallel circuits only. Same as 6L6 to 6BG6. |
|  | 6 L 6 | G | Parallel circuits only. No changes. |
| 71A | 12A | P | No changes. |
|  | $\begin{aligned} & 182 \mathrm{~B} / 482 \mathrm{~B} \\ & 183 / 483 \end{aligned}$ | $\underset{\mathrm{G}}{\mathbf{G}}$ | Parallel circuits only. No changes. If push-pull circuit, change both tubes. |
| 84/6Z4 | 0Z4 | E | Change socket to octal and rewire as follows: |
|  | 6 Y 5 | G | Parallel circuits only. Change socket to six prong and rewire as follows: |
|  | 6ZY5 | G | Same as $84 / 6 \mathrm{Z} 4$ to $0 \mathrm{Z4}$ procedure. Parallel circuits only. |
| 89 | 89 Y | E | No changes. |
| 117 N 7 | $\begin{aligned} & 117 \mathrm{~L} 7 \\ & 117 \mathrm{M} 7 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | Make adaptor as follows:  <br> No. 1 on base to No. 8 on top <br> 2 to <br> 3 to <br> 4 to <br> 4 4 <br> 5 to <br> 7 to <br> 8 to <br> 8 7 <br> AC line must connect to No. 7.  |
| 807 | 6AL6 | G | Reverse 6AL6 to 807 procedure. |
|  | 6AR6 | G | Parallel circuits only. Reverse 6AR6 to 807 procedure. |
|  | 6BG6 | E | Change socket to octal and rewire as follows: |


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 807 | 6CD6 | E | Parallel circuits only. Same as 807 to 6BG6. When making this substitution be sure the filament power supply is capable of an additional 1.6 ampere load. |
|  | 6 L 6 | G | Reverse 6 L 6 to 807 procedure. |
| 1614 | 6AL6 | G | Same as 5881 to 6AL6. |
|  | 6AR6 | G | Parallel circuits only. Rewire as follows:   <br> No.2 to No. 8  <br> 8 to 1 <br> 4 to 5 <br>  5 to <br>  7  <br> 7 to 6 |
|  | 6BG6 | E | Same as 6L6 to 6BG6. |
|  | 6CD6 | E | Parallel circuits only. Same as 6 L 6 to 6 BG 6 . Use only where addidional current is available from the filament power supply. |
|  | 5881 | E | No changes. |
| 5642 |  |  | Substitution can be accomplished by using 1 X 2 ; $1 \mathrm{X} 2 \mathrm{~A}, 1 \mathrm{~V} 2,1 \mathrm{Y} 2,1 \mathrm{Z} 2,1 \mathrm{~B} 3 \mathrm{GT}$ only if space is available for mounting sockets and shield can. Refer to section 1 of book. |
|  | 1B3 | E | Install octal socket and rewire as follows: <br> Remove wires connected to the pair of filament leads protruding from one end of the 5642 and reconnect to Nos. 2 and 7 respectively on the 1B3 socket. |
|  |  |  | Remove the wires connected to the plate lead protruding from the other end of the 5642 and reconnect to the cap of the 1B3. |
|  | 1 X 2 | E | Install noval socket and rewire as follows: <br> Remove wires connected to the pair of filament leads protruding from one end of the 5642 and reconnect to Nos. 1, 4, 6, \& 9 and $2,5, \& 8$ on the 1 X 2 socket respectively. |
|  |  |  | Remove the wires connected to the plate lead protruding from the other end of the 5642 and reconnect them to the cap of the 1 X 2 . |
|  | 1 Y2 | E | Install four prong socket and rewire as follows: Remove wires connected to the pair of filament leads protruding from one end of the 5642 and reconnect to Nos. 1 and 4 respectively. |
|  |  |  | Remove wires connected to the plate lead protruding from the other end of the 5642 and reconnect to the cap of the 1 Y 2 . |
|  | $1 \mathrm{Z2}$ | E | Install miniature socket and rewire as follows: <br> Remove wires connected to the pair of filament leads protruding from one end of the 5642 and reconnect to Nos. 1, 3, 4,\& 6 and $2,5, \& 7$ respectively on the $1 Z 2$ socket. |
|  |  |  | Remove wires connected to the plate lead protruding from the other end of the 5642 and reconnect to the cap on the $1 \mathrm{Z2}$. |
| 5881 | 6AD7 | P | Parallel circuits only. Remove and tape up any wires anchored on pins Nos. 1 and 6. The 5881 is an industrial type 6L6 with identical characteristics. |
|  | 6AL6 | P | Parallel circuits only. Rewire as follows: Connect No. 3 to cap. |
|  | 6AR6 | P | Parallel circuits only. Same as 1614 to 6AR6. |
|  | 6 F 6 | P | Parallel circuits only. No changes. |
|  | $6 \mathrm{K6}$ | P |  |
|  | $6 \mathrm{U6}$ | P |  |
|  | $6 \mathrm{V6}$ | P |  |
|  | $6 \mathrm{L6}$ | E | No changes. |
|  | 1614 | E | No changes. |
| XXD |  |  | Same as type 14AF7 substitutes. |

# SECOND SUPPLEMENT <br> RECEIVING TUBE SUBSTITUTION G U I D E B O O K 

 BYH. A. MIDDLETON


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## FOREWORD

This Second Supplement to the Receiving Tube Substitution Guidebook, in addition to the original volume and the First Supplement to it, is an accumulation of over twelve years of experience in substituting tubes in radios, television receivers and other electronic equipment. It is a never-ending process which we shall continue in an effort to keep your information as current as possible.

Most of these additional substitutions are for use in television receivers and therefore, because of their critical application in some cases, special consideration should be given your selection when you have a choice of substitutes. A stage-by-stage discussion of the most popular circuits used in television receivers is included in the First Supplement. If there is any question as to whether or not the stage being substituted is a critical one and which characteristics of the substitute should be given special consideration, take a moment to read the article covering the stage in question.

The information herein, in the large part, calls for substitutions only. It is not the object of these instructions to tell you how to improve radios, television receivers and other electronic equipment but rather to help you use the tubes you have, in order to replace those that are not available. Exceptions to the above statement are tubes especially designed as replacements of types where
improvement is needed generally or for specific use such as 5881 for 6L6, 5AW4 for 5U4G, 6CU6 for 6BQ6GT, and the same type numbers in ruggedized tubes designated by an additional ending letter, as 6SN7WGT. Types such as these are designed to improve the life of the tube, the efficiency of the circuit in which they are applied, or both. Characteristics are generally identical to the type they replace. Elements are heavier duty or especially treated in order to withstand greater overloads and construction is more rugged.

Also included in this supplement is a cumulative index indicating the volume and page where the tube you wish to substitute is located.

We have endeavored to list all the practical substitutions. Some, no doubt, have been omitted. When considering substitution, others not listed will likely come to mind. When this happens, write the tube number down immediately in the form used here and attach it in its proper place.

This supplement includes picture tube substitutions. It is recommended that before substitution of picture tube is attempted, a few moments be taken to read over the short article which precedes the picture tube section.

Phoenix, Arizona
January, 1954
H. A. Middleton

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| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1B3 | 1 AX 2 | E | Change socket to noval and rewire as follows: |  |  |  |
|  | 1X2A | E |  | No. 2 on octal 7 | $\begin{aligned} & \text { to No. } 2 \text { noval } \\ & \text { to } \end{aligned}$ |  |
|  |  |  |  |  |  |  |


| 1D5GP | 1N5GT | G | Parallel circuits - add 10 ohm $1 / 2$ watt resistor in series with filament circuit. |
| :---: | :---: | :---: | :---: |
|  |  |  | Series circuits - in addition to above resistors, shunt a 200 ohm 1/2 watt resistor across the combination. |
|  | 1 P 5 | G | Same as above. |
| $\begin{aligned} & 1 \times 2 \\ & 1 \times 2 \mathrm{~A} \end{aligned}$ | 1AX2 | E | It may be necessary to increase the filament current by removing the filament resistor or adding a turn to the filament loop. |
| 5AW4 | $\begin{aligned} & \text { 5U4 } \\ & \text { 5X4 } \\ & 5 \mathrm{~V} 4 \end{aligned}$ | G G G | No changes. |
| 5AZ4 | 5AW4 |  |  |
| 5R4GY | 5AW4 |  |  |
| 5 T 4 | 5AW4 |  |  |
| 5 U 4 | 5AW4 |  |  |
| 5V4 | 5AW4 |  |  |
| 5W4 | 5AW4 |  |  |
| 5X4 | 5AW4 |  |  |
| 5 Y 3 | 5AW4 |  |  |
| 5 Y 4 | 5AW4 |  |  |
| 5Z3 | 5AW4 |  |  |
| 5Z4 | 5AW4 |  |  |
| 6AB4 | 6AQ6 | P | Rewire as follows: |

Remove wires anchored on No. 5 and tape up.
Disconnect No. 2 if grounded.
No. 7
to No. 2
to 7
6 to 1
Connect Nos. 5 and 6 to chassis.


6AV6
P
6BF6
6BK6
6BT6 6BU6

6AF4 6AN4
6CF6
Pins 3 and 7 may be used as tie points for filament and high voltage filter resistors. with filament circuit. Series circuits - in addition to above resistors, shunt a 200 ohm 1/2 watt resistor across the combination.

## Rewire as follows:



Same as above. Parallel circuits only.

6AG5

| 6AH4-6AK5 |  |
| :--- | ---: |
|  |  |
| TUBE | SUB. |
| 6AH4 | 6BL7 |
|  | $6 B X 7$ | 6BX7

6F6 6K6 6L6 6U6 6V6 6W6 6SN7

12 AU7 12BH7

6AH6

6AM4
6AJ5
6CF6
6AJ8
12AH8

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE
PERF.
$\underset{\mathrm{E}}{\mathrm{E}}$
Parallel circuits only. Rewire as follows.

| No. 8 | to No. 3 |
| ---: | :--- |
| 2 | to 8 |



Connect together Nos. $3 \& 6,2 \& 5,1 \& 4$.


E
$\begin{array}{rr}\text { Parallel circuits only. } & \text { Rewire as follows: } \\ \text { No. } 8 & \text { to No. } 3 \\ 2 & \text { to } 8\end{array}$


Connect together Nos. $3 \& 6,2 \& 5,1 \& 4$.
E Parallel circuits only. Change socket to noval and rewire as follows:


No. 1
to No. 2


Connect together Nos. $1 \& 6,2 \& 7,3 \& 8,4 \& 5$.
G Parallel circuits only. Change socket to noval and rewire as follows:

| No. 1 | to No. 2 |
| ---: | :--- |
| 2 | to |
| 3 | to |
| 3 | to |
| 4 | to |
| 5 | 7 |
| 6 | to |
| 7 | to |
| 7 | 3 |

2
9
4
5
7
8
3


Nos. 1 and 6 are internal connections in the 6 CH 6 tube. Do not use these for tie points.

| 6AJ4 | 6AM4 | G | No changes. |
| :--- | :--- | :--- | :--- |
| 6AJ5 | 6 CF 6 | P | Parallel circuits only. No changes. |
| 6AJ8 | 12 AH8 | G | This will operate if pins $7 \& 9$ are connected together. <br> Rewire as follows: <br> Remove wires from No. 9 and put them on No. 7. |
|  |  |  | Remove wires from No. 4 (or 5) and put them on |
|  |  |  | No. 9. Connect No. 4 to No. 5. |



| TUBE 6AK6 | SUB. <br> 6AM5 | PERF. <br> G | CIRCUIT CHANGES NECESSARY <br> Parallel circuits only. Rewire as follows: |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| 6AK8 | 6 T 8 | E | No changes. |
| 6AM4 | 6 AJ4 | E | No changes. |
|  | 6AN4 | G | Change socket to 7 pin and rewire as follows: <br> All connections to Nos. 1, 3, \& 4 must go to No. 2. All connections to Nos. $6 \& 9$ must go to No. 6. Then as follows: <br> No. 2 <br> to No. 5 <br> to 1 <br> to or $/ 87$ <br> to 4 |
|  | 6Q4 | G |  |
| 6AM5 | 6AK6 | E | Heater current different, make necessary changes in series circuit. Rewire as follows: <br> Remove wires from No. 6 and tape up. <br> No. 6 to No. 7 <br> Connect Nos. 7 and 2 together. |
| 6AN4 | 6AF4 6T4 6AM4 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. <br> No changes. <br> Change socket to noval and rewire as follows: <br> Connections to No. 2 may be distributed between Nos. 1, 3, \& 4. <br> Connections to No. 6 may be split up between <br> Nos. 6 and 9. Then as follows: <br> No. 4 <br> ${ }_{5}^{1} \& 7$ <br> $\begin{array}{ll}\text { to No. } 8 \\ \text { to } & 7 \\ \text { to } & 5 \\ \text { to } & 2\end{array}$ |
| 6AQ5 | 6BM5 | E | No changes. |
| 6AS5 | 6BM5 | G | Parallel circuits only. Same as 6AS5 to 6AQ5. |
| 6AV6 | 6BT6 | G | No changes. |
| 6BA6 | 6CG6 | G |  |
| 6BC5 | 6CF6 | G |  |
| 6BJ6 | $\begin{aligned} & \text { 6BA6 } \\ & \text { 12BA6 } \end{aligned}$ | $\underset{\mathbf{E}}{\mathbf{E}}$ | Parallel circuits only. No changes. Series circuits only. No changes. |




6CG6-6CL6
TUBE SUB. 6CG6 6AM6

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE
PERF. CIRCUIT CHANGES NECESSARY
Rewire as follows:
Remove wires from No. 2.
No. 7 to No. 2


Wires removed from No. 2 connect to No. 6.

TUBE SUB. PERF.

6BE6
6BQ6GT
12AT7
$\mathbf{P}$

G

G

G


G
6BV7 6BW6 $6 B Y 7$ 6CK6

6M5

CIRCUIT CHANGES NECESSARY
Parallel circuits only. Rewire as follows:

| No. 8 |  | to No. 3 |
| :---: | :---: | :---: |
| $2 \& 9$ | to $\quad 8$ |  |
| 6 | to $\quad 2$ |  |



If Nos. 1 and 7 are tied together, leave as is; if No. 7 is grounded and No. 1 goes through a bias network, remove the ground from No. 7 and move leads from No. 1 to No. 7.

12AU7 E This substitution utilizes one half of the dual triode as the replacement tube. Change socket to noval and rewire as follows:

Remove and tape up any wires connected to Nos. 1, 4 and 6.

| No. 2 | to No. $4 \& 5$ |
| ---: | :--- |
| 3 | to 1 |
| 5 | to |
| 7 | to |
| 7 | to |
| 8 |  |



| 12AV7 | G | Same as 6J5 to 12AU7. Parallel circuits only. |
| :--- | :--- | :--- |
| 12AX7 | P | Same as 6J5 to 12AT7. |
| $12 \mathrm{AZ7}$ | G | Same as 6J5 to 12AU7. Parallel circuits only. |
| 12 BH 7 | G | Same as 6J5 to 12AU7. Parallel circuits only. |
| 6CL6 | G | Reverse 6CL6 to 6M5 procedure. |




| 12SK7-19Y3 |  | SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE |  |
| :---: | :---: | :---: | :---: |
| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| 12SK7 | 12SS7 | E | No changes, but in series circuits shunt 150 ohm 1 watt resistor across heater terminals, Nos. 2 and 7. |
| 12SQ7 | 26BK6 | G | Series circuits only. Same as $12 S Q 7$ to 12BK6. Add 300 ohm 2 watt resistor across Nos. 3 and 4. |
| 12SS7 | 12SK7 | E | Make necessary circuit changes to provide additional heater current. See page 12, Section 1. |
| 12V6 | 12A5 | G | Change socket to small 7 pin and rewire as follows: |
| 12X4 | $6 \times 4$ | E | No changes, but add a 20 ohm 5 watt resistor in series with the heater. |
|  | 6 X 5 | E | Same as 6X4 to 6X5, except to add a 20 ohm 5 watt resistor in series with the heater. |
| 14X7 | $19 \mathrm{T8}$ | G | Series circuits only. Change socket to noval and rewire as follows: |
|  | 19V8 | E | Series circuits only. Change socket to noval and rewire as follows: |
| 19AQ5 | 16A5 | G | Change socket to noval and rewire as follows: |
|  | 35B5 | G | Series circuits only. Some circuit changes may be necessary to provide the extra 15 filament volts. No other changes. |
| $19 \mathrm{J6}$ | 6 J 6 | E | Rewire as follows: <br> Disconnect heater terminals, Nos. 3 and 4. Connect these wires to a 125 ohm 3 watt resistor, which may be mounted out of the way. Use a 6 volt filament transformer to light the 6J6. |
| 19X3 | 19 Y 3 | E | No changes. |
| 19 Y 3 | 19X3 | E | No changes. |

TUBE

| 26CG6 | 26A6 | G |
| :--- | :--- | :--- |
|  | 12BA6 | G |
| 26D6 | $12 B E 6$ | $G$ |

E

E

12BA6

12L8GT

28D7 G
G

Rewire as follows:


No. 1
3 \& 7 6
to No. 7
to 2
to $\quad 1 \& 3$ or 9


No. 6 is heater tap. Do not use as tie point. Add 40 ohm 5 watt resistor in series with the filament.

G Change socket to 7 pin and rewire as follows:
No. 1

| 1 | to NO. 5 |
| :--- | :--- |
| $3 \& 7$ | to $1 \& 7$ |
| 4 | to |
| 5 | to |
| 5 | 4 |
| 6 | to |
| 8 | to |
| 8 | 6 |



Remove and tape up any wires connected to Nos. 2 and 9. In parallel circuits add a 40 ohm 2 watt resistor in series with one of the filament leads. In series circuits, shunt a 120 ohm 5 watt resistor across the filament leads.

Change socket to octal and rewire as follows:


No. 1
$3 \& 7$
to No. 3

| 4 | to | 2 |
| :--- | :--- | :--- |
| 5 | to | 7 |
| 6 | to | 8 |
| 8 | to | 4 |



Connections anchored to Nos. 2 and 9 may be placed on the free terminals of the octal socket.

Change socket to noval and rewire as follows:
No. 2 on octal


Change socket to loctal and rewire as follows:

| No. 1 on octal | to No. 7 on loctal |  |
| :--- | :--- | :--- |
| 2 | to | 6 |
| 3 | to | 2 |
| 4 | to | 4 |
| 5 | to | 3 |
| 6 | to | 1 |
| 7 | to | 8 |

No changes.
Same as 26A6 to 12BA6.
No changes, except to add 90 ohm 2 watt resistor in series with heater. (Parallel circuits only)

28D7-5670
TUBE SUB. PERF.

Rewire as follows:
Remove wires from Nos. 2 and 7 and connect them to a 330 ohm 10 watt resistor. Remove and tape up any wires on No. 1. No. 4 to No. 1
This will work if the requirements for proper operation of the gas rectifier are met. Change socket to octal and rewire as follows:

Remove and tapeup any wires connected to Nos. 1, 4 and 8.
No. 3 on loctal
6
to No. 3 on octal
to 5
to 8


The 6BY5 must be lit from a 6.3 volt 2.0 ampere filament transformer.


## SUBSTITUTING PICTURE TUBES IN TV RECEIVERS

## 1. Connecting the External Conductive Tube Coating to Chassis

When a picture tube that does not have an external conductive coating is substituted for one that has the external coating, it is generally necessary to install a metal finger to make contact with the coating in order to connect it to the chassis. Sometimes this finger is attached to the deflection yoke support bracket. Ordinarily a tube that does not have an external coating has a 500$\mu \mu \mathrm{f}$ capacitor connected from the anode lead to the chassis inside the high-voltage cage. It is normally not necessary to remove this capacitor when substituting a tube that has the external conductive coating.

## 2. Installing a Capacitor from the Anode Lead to the Chassis

When a tube that does not have the external conductive coating is substituted for one that has the external conductive coating, it is often necessary to install a capacitor from the anode lead to the chassis. In the substitutions listed here we have repeated the same value of $500 \mu \mu \mathrm{f}$. Ordinarily this will be satisfactory. In some cases this capacitor will not be necessary. In others best satisfaction may be had with capacitances as high
as $2,000 \mu \mu \mathrm{f}$. This is according to individual cases and can be determined by trial. The most convenient location for this capacitor is inside the highvoltage cage.

## 3. Dimensions

Before attempting any of the substitutions listed here, make sure the substitute tube will fit into the available space. In the magnetic types try to choose a substitute with a neck length similar to the original. Differences in face plate curvatures may make it necessary, in some substitutions listed, to change the mask.

## 4. Change in Anode Connector

Either the ball-type or cavity-type anode connector is used on picture tubes. Instructions specify when a change is necessary.

## 5. Replacement or Deletion of Ion Trap

It is necessary to replace the ion trap with the type required by the manufacturer of the substitute tube. Some tubes do not require an ion trap and are being substituted for others requiring either a single or dual ion trap. In these cases,
the instruction is "Remove ion trap." Other tubes requiring a single ion trap can be substituted for by installing a dual ion trap and vice versa. In these cases instructions are given. Some manufacturers of picture tubes are using a new type gun requiring a single ion trap in tubes that formerly used a gun requiring a dual ion trap. It is therefore important to check the individual manufacturer's specification on the substitute tube being used.

## 6. Electrostatic and Self-Focus Tubes

When using electrostatic or self-focus tubes as substitutions for magnetically focused tubes, it is necessary to remove the focus coil from the neck of the tube and replace it with a magnetic centering device. The focus coil may be left in the receiver circuit-wise, in which case it should be mounted in the cabinet in some position where it magnetic field has no effect on the picture. It may be replaced with a choke or resistor. The picture tube socket may have to be changed when it is necessary to bring out a lead from the focus electrode on the picture tube base except in the case of self-focus or automatic focus types. This lead should be connected to a d-c voltage point in the set which gives best focus. The voltage required normally lies between 50 and 350 volts. Self-focus or automatic focus tubes have a special gun structure within the neck of the tube designed
to focus the tube automatically without the use of an external focus voltage.

## 7. Substituting Electrostatic or Automatic Focus Types with Magnetic Types

When replacing electrostatic focus types with magnetic focus types, discard the magnetic centering device and install a permanent magnet focusing device. This must be mounted on the yoke support with suitable metal brackets. It is practical to replace an electrostatic focus tube using high-focus voltage with a type using low-focus voltage or a self-focus type. When doing this, it is desirable to remove the focus voltage rectifier as a safety measure.

## 8. Differences in the Face Plate

Differences in the face plate of the tube have little effect on whether or not they may be substituted. Dark-faced tubes give better contrast than white-faced tubes. Some tubes are frosted to decrease reflections and others have an aluminized back for better contrast and brightness. Aluminized tubes in some cases have higher anode voltage applied and this voltage should be reduced in accordance with manufacturers' specifications when other than aluminized tubes are substituted. When substituting aluminized tubes for white- or gray-faced tubes, sufficient voltage is usually available for satisfactory operation.

| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 7HP4 | 7QP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to cavity type. Change ion trap to single. |
| 7NP4 | 7WP4 | Connect external conductive coating to chassis. |
| 7QP4 | 7HP4 | Change anode connector to ball type. Connect external conductive coating to chassis. Change ion trap to double. |
| TWP4 | 7NP4 | No changes. |
| 8AP4 | 8AP4A | No changes. Substitute has dark face. |
| 8AP4A | 8AP4 | No changes. Substitute has white face. |
| 10BP4 | 10BP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & \text { 10BP4 } \\ & \text { 10BP4A } \end{aligned}$ | 10CP4 | Change anode connector to cavity type. Remove ion trap. |
|  | 10 EP 4 | Change anode connector to cavity type. |
|  | $\begin{aligned} & \text { 10FP4A } \\ & 10 \mathrm{FP} 4 \end{aligned}$ | Remove ion trap. |
| 10 CP 4 | $\begin{aligned} & \text { 10BP4 } \\ & \text { 10BP4A } \end{aligned}$ | Only where $1^{\prime \prime}$ greater length is available. Change anode connector to ball type. |
|  | 10EP4 | Only where $1^{\prime \prime}$ greater length is available. Change anode connector from ball to cavity type. Remove ion trap. |
|  | 10FP4 <br> 10FP4A | Change anode connector to cavity type. |
| 10EP4 | $\begin{aligned} & \text { 10BP4 } \\ & \text { 10BP4A } \end{aligned}$ | Change anode connector from ball to cavity type. |
|  | 10CP4 | Remove ion trap. |
|  | 10FP4 <br> 10FP4A | Change anode connector from ball to cavity type. Remove ion trap. |
| 10FP4 | 10FP4A | No changes. |
| 10FP4 <br> 10FP4A | $\begin{aligned} & \text { 10BP4 } \\ & \text { 10BP4A } \end{aligned}$ | Install double ion trap. |
|  | 10CP4 | Change anode connector to ball type. |
|  | 10EP4 | Change anode connector from cavity to ball type. Install double ion trap. |
| 10MP4 | 10MP4A | No changes. |
| 10MP4A | 10MP4 | No changes. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 12JP4 | $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | Connect external conductive coating to chassis. Change anode connector to cavity type. |
| 12JP4 | $\begin{aligned} & \text { 12LP4 } \\ & \text { 12LP4A } \end{aligned}$ | Only where $11 / 8^{n}$ greater length is available. Change anode connector to cavity type. Install double ion trap. |
|  | $\begin{aligned} & \text { 12QP4 } \\ & \text { 12QP4A } \end{aligned}$ | Install double ion trap. |
|  | 12RP4 | Install single ion trap. |
|  | 12TP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Install double ion trap. |
|  | 12VP4 <br> 12VP4A | Change anode connector to cavity type. Install double ion trap. |
|  | 12YP4 | Only where $1^{\prime \prime}$ greater length is available. Change anode connector to cavity. Install single ion trap. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12 KP 4 | 12KP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | 12JP4 | Change anode connector to cavity type. |
|  | $\begin{aligned} & \text { 12QP4 } \\ & \text { 12QP4A } \\ & \text { 12RP4 } \end{aligned}$ | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball. Install single ion trap. |
|  | 12TP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Connect $500-\mu \mu \mathrm{f}$, $20-\mathrm{kv}$ capacitor from anode to chassis. Install double ion trap. |
|  | $\begin{aligned} & \text { 12VP4 } \\ & \text { 12VP4A } \end{aligned}$ | Install double ion trap. |
|  | 12YP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Install single ion trap. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12LP4 | 12LP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & \text { 12LP4 } \\ & \text { 12LP4A } \end{aligned}$ | 12JP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball type. Remove ion trap. |
|  | $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | Remove ion trap. |
|  | $\begin{aligned} & \text { 12QP4 } \\ & \text { 12QP4A } \\ & \text { 12RP4 } \end{aligned}$ | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball type. Change ion trap to single. |
|  | 12VP4 <br> 12VP4A <br> 12TP4 | No changes. |
|  | 12YP4 | Change ion trap to single. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12QP4 | 12QP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & 12 \mathrm{QP4} \\ & 12 \mathrm{QP} 4 \mathrm{~A} \end{aligned}$ | 12JP4 | Remove ion trap. |
|  | $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | Connect external conductive coating to chassis. Change anode connector to cavity type. Remove ion trap. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| $\begin{aligned} & \text { 12QP4 } \\ & \text { 12QP4A } \end{aligned}$ | 12LP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. |
|  | 12LP4A | Connect external conductive coating to chassis. Change anode connector to cavity type. Install ion trap. |
|  | 12RP4 | No changes. |
|  | 12TP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Change ion trap to double. |
|  | $\begin{aligned} & \text { 12VP4 } \\ & \text { 12VP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. Only where $1^{n}$ greater length is available. Change anode connector to cavity type. Change ion trap to double. |
|  | 12YP4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Connect external tube coating to chassis. Change anode connector to cavity type. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12RP4 | 12JP4 | Remove ion trap. |
|  | $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. Change anode connector to cavity type. Remove ion trap. |
|  | $\begin{aligned} & \text { 12LP4 } \\ & \text { 12LP4A } \end{aligned}$ | Only where $11 / 2^{\prime \prime}$ greater length is available. Connect external conductive tube coating to chassis. Change anode connector to cavity type. Change ion trap to double. |
|  | $\begin{aligned} & \text { 12QP4 } \\ & \text { 12QP4A } \end{aligned}$ | No changes. |
|  | 12TP4 | Only where $11 / 2^{n}$ greater length is available. Change anode connector to cavity type. Change ion trap to double. |
|  | $\begin{aligned} & \text { 12VP4 } \\ & \text { 12VP4A } \end{aligned}$ | Only where $11 / 2^{\prime \prime}$ greater length is available. Connect external conductive coating to chassis. Change anode connector to cavity type. Change ion trap to double. |
|  | 12 YP 4 | Only where $11 / 2^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12TP4 | 12JP4 | Change anode connector to ball type. Remove ion trap. |
|  | $\begin{aligned} & \text { 12KP4 } \\ & \text { 12KP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. Remove ion trap. |
|  | $\begin{aligned} & 12 \mathrm{QP4} \\ & 12 \mathrm{QP} 4 \mathrm{~A} \end{aligned}$ | Change anode connector to ball type. Change ion trap to single. |
|  | 12RP4 |  |
|  | $\begin{aligned} & \text { 12VP4 } \\ & \text { 12VP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | 12YP4 | Connect external conductive tube coating to chassis. Change ion trap to single. Substitute is electrostatic focus. See No. 6 in picture tube article. |
| 12UP4 | 12UP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & \text { 12UP4 } \\ & \text { 12UP4A } \end{aligned}$ | 12UP4B | Change to single ion trap. |
| 12UP4B | 12UP4 <br> 12UP4A | Change to double ion trap. |
| 12VP4 | 12VP4A | No changes. Substitute has dark face. |


| TUBE | SUB. |
| :--- | :--- |
| $14 B P 4$ | $14 B P 4 A$ |

14CP4

14DP4

14EP4

| $14 \mathrm{FP4} 4$ | 14 BP 4 |
| :--- | :--- |
|  | 14 BP 4 A |
|  | 14 CP 4 |
|  | 14 EP 4 |

15AP4 15CP4

15DP4
16 CP 4

16LP4 16LP4A 16ZP4

15CP4

15AP4
15DP4
16CP4
16LP4
16LP4A 16ZP4

## SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

## CHANGES NECESSARY

No changes.

No changes.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis.

No changes.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis.

Connect external conductive coating to chassis.
Change ion trap to single.

Change ion trap to single.

No changes.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double.

Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis.

Connect external conductive coating to chassis.

Change ion trap to double.
Only where $1^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Install double ion trap.

Change ion trap to single.
Only where $1^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Install double ion trap.

Only where $2^{\prime \prime}$ greater length is available. Connect external conductive coating to chassis. Install double ion trap.

Change ion connector to ball type. Remove ion trap.
Change ion connector to ball type. Change ion trap to single.
No changes.
Only where $1^{\text {n }}$ greater length is available. Connect external conductive tube coating to chassis.

| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 15DP4 | 15AP4 | Install single ion trap. |
|  | $\begin{aligned} & 15 \mathrm{CP} 4 \\ & 16 \mathrm{CP} 4 \end{aligned}$ | Only where $1^{\prime \prime}$ greater length is available. Change anode connector to cavity type. Change ion trap to double. |
|  | $\begin{aligned} & \text { 16LP4 } \\ & \text { 16LP4A } \\ & \text { 16ZP4 } \end{aligned}$ | Only where $2^{\prime \prime}$ greater length is available. Connect external conductive tube coating to chassis. Change anode connector to cavity type. Change ion trap to double. |
| 16AP4 | 16AP4A | No changes. |
| 16AP4A | 16AP4 | No changes. |
| $\begin{aligned} & 16 \mathrm{AP} 4 \\ & 16 \mathrm{AP} 4 \mathrm{~A} \end{aligned}$ | 16AP4B | No changes. |
| 16 CP 4 | 15AP4 | Change anode connector to ball type. Remove ion trap. |
|  | 15 CP 4 | No changes. |
|  | 15DP4 | Change anode connector to ball type. Change ion trap to single. |
|  | $\begin{aligned} & \text { 16LP4 } \\ & \text { 16LP4A } \\ & \text { 16ZP4 } \end{aligned}$ | Only where $1^{\prime \prime}$ greater length is available. Connect external conductive tube coating to chassis. |
| 16 DP 4 | 16DP4A | No changes. |
| $\begin{aligned} & \text { 16DP4 } \\ & \text { 16DP4A } \end{aligned}$ | 16FP4 | Change anode connector to ball type. Change ion trap to single. |
|  | $\begin{aligned} & \text { 16HP4 } \\ & 16 \mathrm{HP} 4 \mathrm{~A} \\ & 16 \mathrm{JP} 4 \\ & 16 \mathrm{JP} 4 \mathrm{~A} \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | $\begin{aligned} & 16 \mathrm{MP} 4 \\ & 16 \mathrm{MP} 4 \mathrm{~A} \end{aligned}$ | Connect external conductive tube coating to chassis. |
| 16EP4 | $\begin{aligned} & 16 E P 4 A \\ & 16 E P 4 B \end{aligned}$ | No changes. |
| $\begin{aligned} & 16 \mathrm{EP} 4 \\ & 16 \mathrm{EP} 4 \mathrm{~A} \\ & 16 \mathrm{EP} 4 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & \text { 16AP4 } \\ & 16 \mathrm{AP} 4 \mathrm{~A} \\ & 16 \mathrm{AP} 4 \mathrm{~B} \end{aligned}$ | Only where $2-5 / 8^{\prime \prime}$ additional length is available. Change ion trap to double. |
| 16FP4 | $\begin{aligned} & \text { 16HP4 } \\ & \text { 16HP4A } \\ & \text { 16JP4 } \\ & \text { 16JP4A } \end{aligned}$ | Only where $1^{\prime \prime}$ greater length is available. Connect external conductive tube coating to chassis. Change anode connector to cavity type. Change ion trap to double. |
|  | $\begin{aligned} & \text { 16MP4 } \\ & 16 \mathrm{MP} 4 \mathrm{~A} \end{aligned}$ | Only where $2^{n}$ greater length is available. Connect external conductive tube coating to chassis. Change anode connector to cavity type. Change ion trap to double. |
| 16GP4 | $\begin{aligned} & \text { 16GP4A } \\ & \text { 16GP4B } \end{aligned}$ | No changes. |
| 16HP4 | 16HP4A | No changes. |
| $\begin{aligned} & 16 \mathrm{HP} 4 \\ & 16 \mathrm{HP} 4 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \text { 16JP4 } \\ & 16 \mathrm{JP} 4 \mathrm{~A} \end{aligned}$ | No changes. |
|  | $\begin{aligned} & \text { 16MP4 } \\ & \text { 16MP4A } \end{aligned}$ | Only where $1^{\prime \prime}$ greater length is available. No changes. |
| 16JP4 | 16JP4A | No changes. |
| $\begin{aligned} & \text { 16JP4 } \\ & \text { 16JP4A } \end{aligned}$ | $\begin{aligned} & \text { 16DP4 } \\ & \text { 16DP4A } \end{aligned}$ | Connect $500-\mu \mu \mathrm{f}, 20 \mathrm{kv}$ capacitor from anode to chassis. |
|  | $\begin{aligned} & \text { 16FP4 } \\ & \text { 16FP4A } \end{aligned}$ | Change anode connector to ball type. Change ion trap to single. |


| 16JP4-16RP4 | SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE |  |
| :---: | :---: | :---: |
| TUBE | SUB. | CHANGES NECESSARY |
| $\begin{aligned} & \text { 16JP4 } \\ & \text { 16JP4A } \end{aligned}$ | $\begin{aligned} & \text { 16HP4 } \\ & \text { 16HP4A } \end{aligned}$ | No changes. |
|  | $\begin{aligned} & \text { 16MP4 } \\ & \text { 16MP4A } \end{aligned}$ | Only where $1^{\circ}$ greater length is available. No changes. |
| 16KP4 | 16KP4A | No changes. |
| $\begin{aligned} & \text { 16KP4 } \\ & 16 \mathrm{KP} 4 \mathrm{~A} \end{aligned}$ | 16QP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |
|  | 16RP4 | No changes. |
|  | 16TP4 | No changes. |
|  | 16UP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16XP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |
| 16LP4 | 16LP4A | No changes. Substitute has dark face. |
| $\begin{aligned} & \text { 16LP4 } \\ & \text { 16LP4A } \end{aligned}$ | 15AP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball type. Remove ion trap. |
|  | 15CP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 15DP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball type. Change ion trap to single. |
|  | 16CP4 | Connect $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16ZP4 | No changes. |
| 16MP4 | 16MP4A | No changes. |
| $\begin{aligned} & \text { 16MP4 } \\ & \text { 16MP4A } \end{aligned}$ |  | Same as 16JP4 substitutes. |
| 16QP4 | $\begin{aligned} & \text { 16KP4 } \\ & 16 \mathrm{KP} 4 \mathrm{~A} \end{aligned}$ | Connect external conductive tube coating to chassis. Change ion trap to single. |
|  | 16RP4 | Connect external conductive tube coating to chassis. Change ion trap to single. |
|  | 16TP4 | Connect external conductive tube coating to chassis. Change ion trap to single. |
|  | 16UP4 | Change ion trap to single. |
|  | 16XP4 | No changes. |
| 16RP4 | $\begin{aligned} & \text { 16KP4 } \\ & 16 \mathrm{KP} 4 \mathrm{~A} \end{aligned}$ | No changes. |
|  | 16QP4 | Change ion trap to double. |
|  | 16 TP 4 | No changes. |
|  | 16UP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16XP4 | Install $500-\mu \mu \mathrm{f}, 20 \mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |

SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE

| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 16SP4 | 16SP4A | No changes. |
| 16SP4A | 16SP4 | No changes. |
| $\begin{aligned} & \text { 16SP4 } \\ & \text { 16SP4A } \end{aligned}$ | 16VP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to ground. Change ion trap to single. |
|  | 16WP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16YP4 | Change ion trap to single. |
|  | 16WP4A | No changes. |
| 16TP4 | $\begin{aligned} & \text { 16KP4 } \\ & \text { 16KP4A } \end{aligned}$ | Only where $1^{\prime \prime}$ greater leugth is available. No changes. |
|  | 16QP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |
|  | 16RP4 | Only where $1^{* \prime}$ greater length is available. No changes. |
|  | 16UP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16XP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |
| 16UP4 | $\begin{aligned} & 16 \mathrm{KP} 4 \\ & 16 \mathrm{KP} 4 \mathrm{~A} \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | 16QP4 | Change ion trap to double. |
|  | 16RP4 | Connect external conductive tube coating to chassis. |
|  | 16TP4 | Connect external conductive tube coating to chassis. |
|  | 16XP4 | Change ion trap to double. |
| 16VP4 | $\begin{aligned} & \text { 16SP4 } \\ & \text { 16SP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. Change ion trap to double. |
|  | 16WP4 | Change ion trap to double. |
|  | 16WP4A | Connect external conductive tube coating to chassis. Change ion trap to double. |
|  | 16YP4 | Connect external conductive tube coating to chassis. |
| 16WP4 | $\begin{aligned} & \text { 16SP4 } \\ & \text { 16SP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | 16VP4 | Change ion trap to single. |
|  | 16WP4A | Connect external conductive tube coating to chassis. |
|  | 16YP4 | Connect external conductive tube coating to chassis. Change ion trap to single. |
| 16WP4A | $\begin{aligned} & \text { 16SP4 } \\ & 16 \mathrm{SP} 4 \mathrm{~A} \\ & 16 \mathrm{VP} 4 \end{aligned}$ | No changes. <br> Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to single. |
|  | 16WP4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 16YP4 | Change ion trap to single. |

16XP4-17CP4A

| TUBE | SUB. |
| :--- | :--- |
| 16 XP 4 | 16 KP 4 |
|  | 16 KP 4 A |

16QP4
16RP4
$16 T P 4$

16UP4
16WP4A

16YP4

16ZP4

17AP4

17BP4

17BP4A
17BP4B
17BP4C

17CP4

17CP4A
17CP4

CHANGES NECESSARY
Connect external conductive tube coating to chassis. Change ion trap to double.

No changes.
Connect external conductive tube coating to chassis. Change ion trap to single.

Connect external conductive tube coating to chassis. Change ion trap to single.

Change ion trap to single.
Change ion trap to double.

Change ion trap to double.

Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis.
Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double.

Same as 16 LP 4 substitutes.

Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. No changes.

No changes.
Substitute type is self-focus electrostatic. See No. 6 in picture tube article.

Connect external conductive tube coating to chassis.
Connect external conductive tube coating to chassis.

Connect external conductive tube coating to chassis.
Substitute type is self-focus electrostatic. See No. 6 in picture tube article.

No changes.

No changes.

Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis.
No changes.
Substitute type is self-focus electrostatic.
See No. 6 in picture tube article.

No changes.

No changes.

| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 17FP4 | 17FP4A | No changes. |
| 17FP4A | 17FP4 | No changes. |
| 17FP4 <br> 17FP4A | 17KP4 | No changes. Focus voltage rectifier may be removed as a safety measure. |
| 17HP4 | 17HP4A | No changes. |
| 17HP4A | 17HP4 | No changes. |
| $\begin{aligned} & \text { 17HP4 } \\ & \text { 17HP4A } \end{aligned}$ | 17KP4 | No changes. |
|  | 17RP4 | No changes. |
| 17JP4 | 17AP4 | No changes. |
|  | 178P4 | Install $500-\mu \mu \mathrm{f}, 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | $\begin{aligned} & \text { 17BP4A } \\ & \text { 17BP4B } \\ & \text { 17BP4C } \end{aligned}$ | No changes. |
|  | 17KP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 17KP4 | $\begin{aligned} & \text { 17HP4 } \\ & \text { 17HP4A } \end{aligned}$ | Original type is self-focus. Substitute is external control electrostatic focus. See No. 6 in picture tube article. |
|  | $\begin{aligned} & \text { 17BP4 } \\ & \text { 17BP4A } \end{aligned}$ | Original type is self-focus. Substitute is magnetic focus. See No. 7 in picture tube article. |
| 17LP4 | 17LP4A | No changes. |
| $\begin{aligned} & \text { 17LP4 } \\ & \text { 17LP4A } \end{aligned}$ | 17SP4 | No changes. |
|  | 17VP4 | No changes. |
| 17QP4 | 17SP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
|  | 17UP4 | No changes. |
| 17RP4 | $\begin{aligned} & \text { 17HP4 } \\ & \text { 17HP4A } \end{aligned}$ | No changes. |
|  | 17KP4 | No changes. |
| 17SP4 | $\begin{aligned} & \text { 17LP4 } \\ & \text { 17LP4A } \end{aligned}$ | Substitute is external control electrostatic. See No. 6 in picture tube article. |
| 17UP4 | 17QP4 | No changes. |
| 17UP4 | 17SP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 17VP4 | $\begin{aligned} & \text { 17LP4 } \\ & \text { 17LP4A } \end{aligned}$ | No changes. |
|  | 17SP4 | No changes. |


| 19AP4-20CP4C |  | SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: |
| TUBE | SUB. | CHANGES NECESSARY |
| 19AP4 | 19AP4A | No changes. Substitute has gray face. |
|  | 19AP4B | No changes. Substitute has gray frosted face. |
|  | 19AP4C | No changes. Substitute has gray aluminum face. |
|  | 19AP4D | No changes. Substitute has clear frosted face. |
| 19AP4A ${ }_{\text {19AP4B }}$ |  |  |
| 19AP4B |  |  |
| 19AP4C |  |  |
| 19AP4D |  |  |
| 19DP4 | 19DP4A | No changes. Substitute has gray face. |
| 19DP4A | 19DP4 | No changes. Substitute has clear face. |
| $\begin{aligned} & \text { 19DP4 } \\ & \text { 19DP4A } \end{aligned}$ | 19FP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 19GP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to single. |
| 19EP4 | 19JP4 | No changes. |
| 19FP4 | $\begin{aligned} & \text { 19DP4 } \\ & \text { 19DP4A } \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | 19GP4 | Change ion trap to single. |
| 19GP4 | 19DP4 <br> 19DP4A | Connect external conductive tube coating to chassis. Change ion trap to double. |
|  | 19FP4 | Change ion trap to double. |
| 19JP4 | 19EP4 | No changes. |
| 20CP4 | 20CP4A | No changes. |
|  | 20CP4C | No changes. Substitute has treated face. |
|  | 20DP4 | No changes. |
|  | 20DP4A | Connect external conductive tube coating to chassis. |
|  | 20JP4 | Connect external conductive tube coating to chassis. Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 20CP4A | 20CP4 | Connect external conductive tube coating to chassis. |
|  | 20CP4C | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20DP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20DP4A | No changes. |
|  | 20JP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 20CP4C | 20 CP 4 | No changes. Substitute has treated face. |
|  | 20CP4A | Connect external conductive tube coating to chassis |
|  | 20DP4 | No changes. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 20CP4C | 20DP4A | Connect external conductive tube coating to chassis. |
|  | 20JP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 20DP4 | $\begin{aligned} & 20 \mathrm{CP} 4 \\ & 20 \mathrm{CP} 4 \mathrm{C} \end{aligned}$ | No changes. |
|  | 20DP4A | Connect external conductive tube coating to chassis. |
|  | 20CP4A | Connect external conductive tube coating to chassis. |
|  | 20JP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 20DP4A | $\begin{aligned} & 20 \mathrm{CP} 4 \\ & 20 \mathrm{CP} 4 \mathrm{C} \end{aligned}$ | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20DP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20JP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 20FP4 | 20GP4 | Connect external conductive tube coating to chassis. |
|  | 20JP4 | No changes. Focus voltage rectifier may be removed as a safety measure. |
| 20GP4 | 20FP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20JP4 | No changes. Focus voltage rectifier may be removed as a safety measure. |
| 20HP4 | 20HP4B | No changes. Substitute has treated face. |
| $\begin{aligned} & 20 \mathrm{HP} 4 \\ & 20 \mathrm{HP} 4 \mathrm{~B} \end{aligned}$ | 20HP4A | Connect external conductive tube coating to chassis. |
|  | 20JP4 | Connect external conductive tube coating to chassis. |
|  | 20LP4 | Connect external conductive tube coating to chassis. |
| 21EP4 | $\begin{aligned} & 21 \mathrm{EP} 4 \mathrm{~A} \\ & 21 \mathrm{EP} 4 \mathrm{~B} \end{aligned}$ | Connect external conductive tube coating to chassis. |
|  | 21KP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
|  | 21KP4A | Connect external conductive tube coating to chassis. Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 21EP4A | 21EP4B | No changes. Substitute is aluminized. |
| $\begin{aligned} & \text { 21EP4A } \\ & \text { 21EP4B } \end{aligned}$ | 21KP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
|  | 21EP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21KP4A | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 21FP4 | 21FP4A | Connect external conductive tube coating to chassis. |
|  | 21KP4 | No changes. |
|  | 21KP4A | Connect external conductive tube coating to chassis. |


| 21FP4A-27RP4 |  | SUPPLEMENT-RECEIVING TUBE SUBSTITUTION GUIDE |
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| 21FP4A | 21FP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21KP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21KP4A | No changes. |
| 21 KP 4 | 21KP4A | Connect external conductive tube coating to chassis. |
| 21KP4A | 21KP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 21WP4 | $\begin{aligned} & 20 C P 4 \\ & 20 C P 4 C \end{aligned}$ | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20CP4A | No changes. |
|  | 20DP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 20DP4A | No changes. |
|  | 20JP4 | Substitute is self-focus electrostatic. See No. 6 in picture tube article. |
| 21ZP4 | 21ZP4A | Connect external conductive tube coating to chassis. |
| 21ZP4A | 21ZP4 | Install $500-\mu \mu \mathrm{f}, 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 22AP4 | 22AP4A | No changes. |
| 22AP4A | 22AP4 | No changes. |
| 24 AP4 | $\begin{aligned} & \text { 24AP4A } \\ & 24 A P 4 B \end{aligned}$ | No changes. |
| 24AP4B | $\begin{aligned} & \text { 24AP4 } \\ & \text { 24AP4A } \end{aligned}$ | No changes. |
| 27EP4 | 27GP4 | No changes. |
|  | 27NP4 | No changes. |
|  | 27RP4 | No changes. |
| 27GP4 | 27EP4 | No changes. |
|  | 27NP4 | Connect external conductive tube coating to chassis. |
|  | 27RP4 | Connect external conductive tube coating to chassis. |
| 27NP4 | 27EP4 | No changes. |
|  | 27GP4 | No changes. |
|  | 27RP4 | No changes. |
| 27RP4 | 27EP4 | No changes. |
|  | 27GP4 | No changes. |
|  | 27NP4 | No changes. |

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## SUPPLEMENT—RECEIVING TUBE SUBSTITUTION GUIDE



# THIRD SUPPLEMENT <br> RECEIVING TUBE SUBSTITUTION G U I D E B O O K 

BY

H. A. MIDDLETON

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## FOREWORD

This Third Supplement to the Receiving Tube Substitution Guidebook, in addition to the original volume and the First and Second Supplements to it, is an accumulation of over 15 years of experience in substituting tubes in radio and television receivers and other electronic equipment. It is a never-ending process which we shall continue in an effort to keep this information as current as possible.

Most of these additional substitutions are for use in television receivers and therefore, because of their critical application in some cases, special consideration should be given your selection when you have a choice of substitutes. A stage-by-stage discussion of the most popular circuits used in television receivers is included in the First Supplement. If there is any question as to whether or not the stage being substituted is a critical one and which characteristics of the substitute should be given special consideration, take a moment to read the article covering the stage in question.

The information herein, in the large part, calls for substitutions only. It is not the object of these instructions to tell you how to improve radios, television receivers and other electronic equipment but rather to help you use the tubes you have, in order to replace those that are not available. Exceptions to the above statements are tubes especially designed as replacements of types where improvement is needed generally or for specific use such as 5881 for 6L6, 5 AW4 for 5U4G, 6CU6 for 6BQ6GT, and the same type numbers in ruggedized tubes designated by an additional ending letter, as 6SNTWGT. Types such as these are designed to improve the life of the tube, the efficiency
of the circuit in which they are applied, or both. Characteristics are generally identical to the type they replace. Elements are heavier duty or especially treated in order to withstand greater overloads and construction is more rugged.

Introduced in this Third Supplement is a EuropeanAmerican and American-European tube substitution guide. Due to the recent heavy influx of British and other European electronic equipment, the demand for a substitution guide for these tubes has been increasing steadily. This is due to the fact that in many instances European tubes are not readily available.

Also included in this supplement is a cumulative index indicating the volume and page where the tube you wish to substitute is located.

We have endeavored to list all the practical substitutions. Some, no doubt, have been omitted. When considering substitution, others not listed will likely come to mind. When this happens, write the tube number down immediately in the form used here and attach it in its proper place.

This supplement includes picture tube substitutions. It is recommended that before substitution of picture tube is attempted, a few moments be taken to read over the short article which precedes the picture tube section.

Phoenix, Arizona
June 1957
H. A. Middleton

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## RECEIVING TUBE SUBSTITUTIONS

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| OB3 | 1266 | E | No changes. |
| 1AB6 | 1AC6 | E | Parallel circuits only. No changes. |
| 1AC5 | 1AG4 | G | Change miniature socket to subminiature socket and rewire as follows: <br> Change pin No. 4 on miniature to F-pin on subminiature. <br> No. 2 <br> to G1 <br> to G2 <br> No. 7 <br> to P <br> No. 5 <br> to $\mathrm{F}+$ |
| 1AC6 | $1 \mathrm{AB6}$ | E | No changes. |
| 1AE5 |  |  | No practical substitute. |
| 1 AF 4 | $1 \mathrm{AJ4}$ | G | No changes. |
| 1AF6 |  |  | No practical substitute. |
| 1AG4 | 1AC5 | G | Reverse 1AC5 to 1AG4 procedure. |
| 1AG5 | 1AJ5 | G | No changes. |
|  | 1 AK5 | G | No changes. |
| 1AH4 | 1AK4 | E | No changes. |
| 1AH5 |  |  | No practical substitute. |
| 1 AH6 |  |  | No practical substitute. |
| 1AJ4 | 1AF4 | G | No changes. |
| 1AJ5 | 1AG5 | G | No changes. |
|  | 1 AK5 | G | No changes. |
| 1AK4 | 1AH4 | E | No changes. |
| 1AK5 | 1AG5 | G | No changes. |
|  | 1AJ5 | G | No changes. |
| 1AX2 | 1B3 | E | Change sock et to octal and rewire as follows: |
|  | 1X2 | E | No changes. Sus |
| 1B3 | 2B3 | P | No changes. |
| 1 C 3 | 1 E 4 | G | Change socket to octal and rewire as follows: <br> No. 1 on miniature <br> to No. 2 on octal $\begin{array}{ll} \text { to } & 3 \\ \text { to } & 5 \\ \text { to } & 7 \end{array}$ |
|  | 1LE3 | G | Change socket to octal and rewire as follows: |






4BQ7-4CX7

| TUBE | SUB. |
| :---: | :---: |
| 4BQ7 | 4 BC 8 |
|  | 4BK7 |
|  | 4BS8 |
|  | 4BZ7 |
|  | 4BZ8 |
|  | $4 \mathrm{CX7}$ |
| 4BS8 | 4BC8 |
|  | 4BK7 |
|  | 4BQ7 |
|  | 4BZ8 |
|  | $4 \mathrm{CX7}$ |

4BU8

| $4 \mathrm{BX8}$ | $4 \mathrm{BC8}$ |
| :--- | :--- |
|  | 4 BK 7 |
|  | $4 \mathrm{BQ7}$ |
|  | $4 \mathrm{BS8}$ |
|  | $4 \mathrm{BZ8}$ |
|  | $4 \mathrm{CX7}$ |

$4 \mathrm{BZ7} \quad 4 \mathrm{BC} 8$
4BK 7
4BQ7
4BS8
4BZ8 4CX7

4BC8 4BK7 4BQ7 4BS8 4 CX 7 4BC5 4BC8
UB.

THIRD SUPPLEMENT - RECEIVING TUBE SUBSTITUTION GUIDE

PERF.
CIRCUIT CHANGES NECESSARY
$\begin{array}{ll}\mathrm{G} & \text { No changes. } \\ \mathrm{G} & \text { No changes. } \\ \mathrm{G} & \text { No changes. } \\ \mathrm{G} & \text { No changes. } \\ \mathrm{G} & \text { No changes. } \\ \mathrm{G} & \text { No changes. }\end{array}$ together internally.

G No changes.
No changes.
No changes.
No changes.
No changes. Pins No. 8 and No. 9 are connected together internally.

No practical substitute.
G No changes.
G No changes.
No changes.
No changes.
No changes.
No changes. Pins No. 8 and No. 9 are connected together internally.

G No changes.
G No changes.
G No changes.
G No changes.
G No changes.
G No changes. Remove and tape any wires anchored on pin No. 9.
G No changes.
G No changes.
No changes.
No changes.
No changes. Remove and tape any wires anchored on pin No. 9.
G No changes.
G Rewire as follows:


G Rewire as follows:


Tie pins No. 8 and No. 9 together.


G Rewire as follows:
Tie pins No. 8 and No. 9 together.


G Rewire as follows:


Tie pins No. 8 and No. 9 together.


G Rewire as follows:


Tie pins No. 8 and No. 9 together.



| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |  |
| :---: | :---: | :---: | :---: | :---: |
| 5AX4 | 5AS4 | E | No changes. |  |
|  | 5AW4 | E | No changes. If transformer will stand 1.2 amperes more. |  |
|  | 5 T 4 | G | No changes. |  |
|  | 5U4G | G | No changes. |  |
|  | 5 U 4GA | E | No changes. |  |
|  | 5 U 4 GB | E | No changes. |  |
|  | 5X3 | E | No changes. If transformer will stand 1.3 amperes more. |  |
|  | 5 V 4 | E | No changes. |  |
|  | 5931 | E | No changes. |  |
| 5AZ4 | $5 \mathrm{AX4}$ | E | No changes. |  |
|  | 5V4 | E | No changes. |  |
|  | 5 Y 3 | E | No changes. |  |
|  | 5 Y 4 | G | Rewire as follows: <br> Change pin No. 2 to pin No. 7 |  |
|  |  |  |  |  |
|  | 5Z4 | E | No changes. |  |
| 5B8 |  |  | No practical substitute. |  |
| 5BE8 |  |  | No practical substitute. |  |
| 5BK7 | $\begin{aligned} & \text { 5BQ7 } \\ & \text { 5BZ7 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. No changes. |  |
| 5BR8 |  |  | No practical substitute. |  |
| 5BT8 |  |  | No practical substitute. |  |
| 5CG8 |  |  | No practical substitute. |  |
| 5CL8 |  |  | No practical substitute. |  |
| 5CM8 |  |  | No practical substitute. |  |
| $5 \mathrm{J6}$ |  |  | No practical substitute. |  |
| 5 T 4 | 5AS4 | E | No changes. |  |
|  | 5AW4 | E | No changes. |  |
|  | 5R4 | E | No changes. |  |
|  | 5U4 | E | No changes. |  |
|  | 5U4GA | E | No changes. |  |
|  | 5U4GB | E | No changes. |  |
|  | 5V4 | E | No changes. |  |
|  | 5931 | E | No changes. |  |
| 5T8 |  |  | No practical substitute. |  |
| 5U4G | 5AS4 | E | No changes. |  |
|  | 5AW4 | E | No changes. |  |
|  | 5U4GA | E | No changes. |  |
|  | 5U4GB | E | No changes. |  |
|  | 5 V 3 | E | No changes. |  |
|  | 5931 | E | No changes. |  |
| 5U4GA | 5AS4 | E | No changes. |  |
|  | 5AU4 | E | No changes. If transformer will stand 1.5 amperes more. |  |
|  | 5 AW4 | E | No changes. |  |
|  | 5R4GY | E | No changes. |  |
|  | 5T4 | E | No changes. |  |
|  | 5U4G | E | No changes. |  |
|  | 5 U 4 GB | E | No changes. |  |
|  | 5 V 3 | E | No changes. |  |
|  | 5931 | E | No changes. |  |





| 6BA8-6BH5 |  |
| :--- | :--- |
|  |  |
| TUBE | SUB. |
| $6 B A 8$ | $6 A U 8$ |
|  | $6 A W 8$ |
|  | $6 B H 8$ |
| $6 B C 4$ | $6 A J 4$ |


| 6BC5 | 3BC5 |
| :---: | :---: |
| 6BC8 | 4BC8 |
|  | 5BC8 |
|  | 6BK7 |
|  | 6BQ7 |
|  | 6BS8 |
|  | 6BZ7 |
|  | 6BZ8 |
|  | X155 |
| 6BD4A | 6BK4 |
| 6BD6 | $6 \mathrm{DA6}$ |
|  | 5749 |
| 6BE6 | 3BE6 |
|  | 6BY6 |
|  | 5750 |

6BE7
6BE8

6BG6
6BH5

THIRD SUPPLEMENT - RECEIVING TUBE SUBSTITUTION GUIDE

## PERF. <br> CIRCUIT CHANGES NECESSARY

G No changes.
G No changes.
G Rewire as follows:
Rewire as follows: Change pin No. 1 to pin No. 5


E
Parallel circuits oniy. Install 5-ohm 5-watt resistor in series with filament.

E Parallel circuits only. Install 3.5-ohm 5-watt resistor in series with filament.
Parallel circuits only. Install $1.5-0 h m 5$-watt resistor in series with filament.
G No changes.
No changes.
No changes.
No changes.
No changes.
No changes.
E No changes.
G Reverse 6DA6 to 6BD6 procedure.
G No changes.
E Parallel circuits only. Install 5-ohm 5-watt resistor in series with filament.
G No changes.
E No changes.
No practical substitute.
E Parallel circuits only. Install 1.5-ohm 5-watt resistor in series with filament.
Rewire as follows:
Change pin No.


G No changes.
G Change socket to miniature and rewire as follows:
Change pin No. 1


1
2
3
4
5
6
3
2
3
4
5
6
6
3
to pin No. 6 on miniature. to 1
6 on miniature.
1
2
3
4
5

6BJ6 (Cont.)

G Change socket to miniature and rewire as follows:
Change pin No. 1 to pin No. 6 on miniature.


2
3
4
5
6
3

| to | 1 |  |
| :---: | :---: | :---: |
| to | 7 | (1) (1) |
| to | 3 | (2) (0) |
| to | 4 | (1) (2) |
| to | 5 | sus |
|  |  |  |



$6 J 7$

6W7 7
7 C 7

5BR8

6AL6

6BR7

6C6
(Cont.)

G Parallel circuits only. Change socket to octal and rewire as follows:

Change pin No. 2 to grid cap on octal
2
3
4
5
7
8
9

|  |  |
| :--- | :--- |
| to | No. |
| to |  |
| to | 2 |
| to | 7 |
| to | 3 |
| to | 4 |
| to | 5 |



G Same as $6 B R 7$ to $6 J 7$ procedure.
G Change socket to octal and rewire as follows:

Change pin No. 2

| to pin No. | 6 on octal |
| :--- | :--- |
| to | 7 |
| to | 1 |
| to | 8 |
| to | 2 |
| to | 3 |
| to | 4 |


3
4
4
7
7
8
9

E Parallel circuits filament.

G Change socket to octal and rewire as follows:
Change pin No. 1 to pin No. 5 on octal

|  | Change pin No. 1 |  | 5 |  |
| :---: | :---: | :---: | :---: | :---: |
| (1) ${ }^{(1)}$ | 3 | to | 8 | (0)(5) |
| (1) 8 | 4 | to | 2 | (2) ${ }^{(3)}$ |
| (1) (0) | 5 | to | 7 | (1) (0) |
| OR16 | 7 | to | ca | sua |

E Rewire as follows:
Change grid cap on 6BS7 to pin No. 2.
G Change sock et to six pin.
Change pin No. 3 to pin No. 5


| TUBE | SUB. | PERF |
| :--- | :--- | :--- | :--- | :--- |
| 6BS7 |  |  |
| (Cont.) |  |  |




12AU7 G Parallel circuits only. Rewire as follows: Reverse wires connected to No. 5 and No. 9
6CG8 5CG8

6AT8

6X8

6CH6 6132

6 CH 7
6BC8 6BK7 6BQ7 6BS8 6BZ7 6BZ8 X155

No. 1
Rewire as follows:



E No changes.
G Tie pin No. 8 and No. 9 together.
G Tie pin No. 8 and No. 9 together.
Tie pin No. 8 and No. 9 together.
Tie pin No. 8 and No. 9 together.
Tie pin No. 8 and No. 9 together.
Tie pin No. 8 and No. 9 together.
Tie pin No. 8 and No. 9 together.
No practical substitute.



|  | Change pin No. ${ }_{3}$ |  | 7 |  |
| :---: | :---: | :---: | :---: | :---: |
| (1)0 | 4 | to | 3 |  |
| (3) 8 | 5 | to | 4 | (1) (3) |
| (1) (1) | 7 8 | to | 5 | $\left(\begin{array}{ll}\text { (1) } & \text { (1) }\end{array}\right.$ |
| ORIG | 8 | to | 2 | sue |

6BD6
6BJ6

G Same as 6DA6 to 6BA6 procedure.
G Parallel circuits only. Change socket to miniature and rewire as follows:


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6DB6 |  |  | No practical substitute. |
| 6DC6 | 6BZ6 | G | No changes. |
|  | $6 \mathrm{CB6}$ | G | No changes. |
|  | 6DC6 | G | No changes. |
| 6DE6 | 6BZ6 | G | No changes. |
|  | 6CB6 | G | No changes. |
|  | 6DE6 | G | No changes. |
| 6DG6 | 6K6 | G | Parallel circuits only. No changes. |
|  | 6V6 | G | Parallel circuits only. No changes. |
|  | 6W6 | E | No changes. |
| 6DN6 | 6BG6 | G | No changes. |
|  | 6CD6 | E | No changes. |
| 6DQ6 | 6BQ6 | G | No changes. |
|  | 6CU6 | G | No changes. |
| 6DT6 | 3DT6 | E | Parallel circuits only. Install 5-ohm 5-watt resistor in series with |
|  |  |  | filament. |
|  | 4DT6 | E | Parallel circuits only. Install 4.7 -ohm 5 -watt resistor in series with filament. |
| 6F6 | 1621 | E | No changes. |
|  | 1622 | E | Parallel circuits only. No changes. |
| 6H6 | 5679 | G | Reverse 5679 to 6 H 6 procedure. |
| 6 J 4 | 6J4WA | E | No changes. |
| 6 J 5 | 2C22 | G | Reverse 2C22 to 6J5 procedure. |
| 6 J 6 | 5964 | E | No changes. |
|  | 6101 | E | No changes. |
| $6 \mathrm{J7}$ | 1221 | E | Reverse 1221 to $6 J 7$ procedure. |
|  | 6059 | G | Reverse 6059 to 6J7 procedure. |
|  | 7000 | G | No changes. |
| 6K6 | 1621 | E | Parallel circuits only. No changes. |
|  | 5871 | G | No changes. |
| 6K7 | 5732 | E | No changes. |
| 6L6 | 1621 | G | Parallel circuits only. No changes. |
|  | 1622 | G | No changes. |
|  | 5881 | E | No changes. |
|  | 5932 | E | No changes. |
|  | 6550 | E | No changes. |
| 6M5 | 6BJ5 | G | Reverse 6BJ5 to 6M5 procedure. |
| 6N7 | 1635 | E | Parallel circuits only. No changes. |
| 6Q5 | 884 | E | No changes. |
| 6S7 | 5732 | G | Parallel circuits only. No changes. |
| 6SA7 | 5961 | E | No changes. |
| 6SB7Y | 5961 | G | No changes. |
| 6SG7 | 6006 | E | No changes. |
| 6SH7 | 6006 | G | No changes. |
| 6SJ7 | $\begin{aligned} & \text { 6SJ7WGT } \\ & 6006 \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{E}}$ | No changes. No changes. |



## 8AU8-12AQ5

THIRD SUPPLEMENT - RECEIVING TUBE SUBSTITUTION GUIDE




| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |  |
| :---: | :---: | :---: | :---: | :---: |
| 12D4 | 12AX4 | G | No changes. |  |
| 12DQ6 | 12AV5 12BQ6 12 CU 6 | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | Reverse 12AV5 to 12DQ6 procedure. <br> No changes. <br> No changes. |  |
| 12 F 8 |  |  | No practical substitute. |  |
| 12G4 | $\begin{aligned} & 12 \mathrm{H} 4 \\ & 12 \mathrm{~J} 5 \end{aligned}$ | $\underset{\mathrm{E}}{\mathrm{E}}$ | Remove, connect, and tape up any wires on pin No. 2. Change socket to octal and rewire as follows: |  |
|  | 14A4 | E | Change socket to octal and rewire as follows: |  |
| 12G8 |  |  | No practical substitute. |  |
| 12 H 4 | $\begin{aligned} & 12 \mathrm{G4} 4 \\ & 12 \mathrm{~J} 5 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. <br> Change to octal and rewire as follows: |  |
|  | 14A4 | E | Same as 14A4 to 12G4 procedure. |  |
| 12 J 5 | $\begin{aligned} & 12 \mathrm{G} 4 \\ & 12 \mathrm{H} 4 \end{aligned}$ | $\underset{\mathrm{E}}{\mathrm{E}}$ | Reverse 12G4 to 12 J 5 procedure. Reverse 12 H 4 to 12 J 5 procedure. |  |
| 12 J 8 |  |  | No practical substitute. |  |
| 12K5 |  |  | No practical substitute. |  |
| 12L6 | $\begin{aligned} & \text { 12W6 } \\ & 1632 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |
| 12R5 | 12W6 | G |  |  |
| 12SL7 | 2 C 52 | E | Parallel circuits only. No changes. |  |
| 12SN7 | 5814 | G | Parallel circuits only. Reverse 5814 to 12SN7 procedure. |  |
| 12 U 7 |  |  | No practical substitute. |  |
| 12V6 | 12CM6 | E | Reverse 12CM6 to 12V6 procedure. |  |
| 12W6 | $\begin{aligned} & 12 \mathrm{~L} 6 \\ & 12 \mathrm{R} 5 \\ & 1632 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. <br> Reverse 12R5 to 12 W 6 procedure. No changes. |  |
| 12 X 4 | 12BW4 | E | Reverse 12BW4 to 12Y4 procedure. |  |

14A4-25C5

| TUBE | SUB. | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 14A4 | 12G4 | E | Reverse 12G4 to 14A4 procedure. |
|  | 12H4 | E | Reverse 12 H 4 to 14A4 procedure. |
| $15 \mathrm{A6}$ |  |  | No practical substitute. |
| 15A8 |  |  | No practical substitute. |
| 16A5 |  |  | No practical substitute. |
| 17AV5 | 6AV5 | E | Parallel circuits only. Install 8.7 -ohm 25 -watt resistor in series with filament. |
|  | 12AV5 | E | Parallel circuits only. Install 7 -ohm 10 -watt resistor in series with filament. |
|  | 17DQ6 | E | Same as 12CU6 to 12AV5 procedure. |
| 17AX4 | $6 \mathrm{AX4}$ | E | Parallel circuits only. Install 18 -ohm 20-watt resistor in series with filament. |
|  | 12AX4 | E | Parallel circuits only. Install 10 -ohm 20 -watt resistor in series with filament. |
| 17C5 |  |  | No practical substitute. |
| 17CA5 | 6CA5 | E | Parallel circuits only. Install 9 -ohm 20 -watt resistor in series with filament. |
|  | $12 \mathrm{CA5}$ | E | Parallel circuits only. Install 10 -ohm 20 -watt resistor in series with filament. |
| 17DQ6 | 6DQ6 | E | Parallel circuits only. Install 9 -ohm 20 -watt resistor in series with filament. |
|  | 12DQ6 | E | Parallel circuits only. Install 10 -ohm 20 -watt resistor in series with filament. |
|  | 17AV5 | E | Same as 12CU6 to 12AV5 procedure. |
| 17H3 |  |  | No practical substitute. |
| 17 Z 3 | 17AX4 | E | Where space permits change socket to octal and rewire as follows: Change pin No. 4 to pin No. 8 on octal |
|  |  |  | $\begin{array}{ccc} 5 & \text { to } & 7 \\ 9 & \text { to } & 5 \end{array}$ |
| 18A5 |  |  | No practical substitute. |
| 19AU4 | 6AU4 | E | Parallel circuits only. Install 7 -ohm 30 -watt resistor in series with filament. |
|  | 19X3 | G | Parallel circuits only. Change socket to miniature and rewire as follows: |
|  |  |  |  |
| 19X3 | 19AU4 | G | Parallel circuits only. Reverse 19AU4 to 19X3 procedure. |
| 19X8 |  |  | No practical substitute. |
| 21A6 |  |  | No practical substitute. |
| 25AV5 | 25CU6 | G | Reverse 25CU6 to 25AV5 procedure. |
|  | 25DQ6 | G | Reverse 25DQ6 to 25AV5 procedure. |
| 25AX4 | 17AX4 | E | Parallel circuits only. Install 18 -ohm 10 -watt resistor in series with filament. |
|  | 25U4 | G | No changes. |
|  | 25W4 | G | No changes. |
| 25 C 5 | $\begin{gathered} \text { 25CA5 } \\ \text { (Cont.) } \end{gathered}$ | G | No changes. |






| 6063 | 6X4 | G | No changes. |
| :---: | :---: | :---: | :---: |
| 6064 | 6 AM6 | G | No changes. |
| 6065 | 6BH6 | G | Parallel circuits only. Rewire as follows: <br> Change pin No. 6 to pin No. $\begin{array}{r}7 \\ 7\end{array}$ |
| 6066 | 6AT6 | G | No changes. |
| 6067 | $\begin{aligned} & 12 \mathrm{AUT} \\ & 5814 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. Parallel circuits only. No changes. |
| 6072 | 12AY7 | G | No changes. |
| 6080 | 6AS7 | G | No changes. |
| 6095 | 6AQ5 6AQ5W 6005 | $\xrightarrow[\mathrm{G}]{\mathrm{E}}$ | No changes. No changes. No changes. |
| 6096 | $\begin{aligned} & \text { 6AK5 } \\ & 5654 \end{aligned}$ | $\underset{G}{E}$ | No changes. <br> No changes. |
| 6097 | $\begin{aligned} & \text { 6AL5 } \\ & 5726 \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. <br> No changes. |
| 6101 | 6 J 6 | G | No changes. |
| 6113 | 6SL 7 | G | No changes. |


| TUBE | SUB. | PERF. | CIRCUIT CHANGES NEC | ARY |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6132 | 6CH6 | G | No changes. |  |  |
| 6134 | $6 \mathrm{AC7}$ | G | No changes. |  |  |
| 6135 | 6 C 4 | G | No changes. |  |  |
| 6136 | 6AU6 | G | No changes. |  |  |
| 6137 | 6SK7 | G | No changes. |  |  |
| 6180 | $\begin{aligned} & \text { 6SN7 } \\ & 5692 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |  |
| 6186 | 6AG5 | G | No changes. |  |  |
| 6187 | 6AS6 <br> 6AS6W <br> 5725 | $\begin{aligned} & \mathrm{G} \\ & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. <br> No changes. <br> No changes. |  |  |
| 6189 | $\begin{aligned} & \text { 12AU7 } \\ & \text { 12AU7WA } \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |  |
| 6201 | $\begin{aligned} & \text { 12AT7 } \\ & 6060 \end{aligned}$ | $\mathrm{G}$ | No changes. No changes. |  |  |
| 6202 | 6X4 | G | No changes. |  |  |
| 6265 | 6BH6 | G | No changes. |  |  |
| 6350 | 12BH7 | G | Rewire as follows: <br> Change pin No. 2 | to pin No.  <br> to  <br> to 2 <br> to 8 <br>  7 |  |
| 6485 | 6AH6 | G | No changes. |  |  |
| 6550 | 6L6 | G | No changes. |  |  |
| 6661 | 6BH6 | G | No changes. |  |  |
| 6662 | 6BJ6 | G | No changes. |  |  |
| 6663 | 6 AL5 | G | No changes. |  |  |
| 6669 | 6AQ5 | G | No changes. |  |  |
| 6677 | 6CL6 | G | No changes. |  |  |
| 6679 | 12AT7 | G | No changes. |  |  |
| 6680 | 12AU7 | G | No changes. |  |  |
| 6681 | 12AX7 | G | No changes. |  |  |
| 7000 | 6 J 7 | G | No changes. |  |  |

# SUBSTITUTING PICTURE TUBES IN TV RECEIVERS 

## 1. Connecting the External Conductive Tube Coating to Chassis

When a picture tube that does not have an external conductive coating is substituted for one that has the external coating, it is generally necessary to install a metal finger to make contact with the coating in order to connect it to the chassis. Sometimes this finger is attached to the deflection yoke support bracket. Ordinarily a tube that does not have an external coating has a 500$\mu \mu \mathbf{f}$ capacitor connected from the anode lead to the chassis inside the high-voltage cage. It is normally not necessary to remove this capacitor when substituting a tube that has the external conductive coating.

## 2. Installing a Capacitor from the Anode Lead to the Chassis

When a tube that does not have the external conductive coating is substituted for one that has the external conductive coating, it is often necessary to install a capacitor from the anode lead to the chassis. In the substitutions listed here we have repeated the same value of $500 \mu \mu \mathrm{f}$. Ordinarily this will be satisfactory. In some cases this capacitor will not be necessary. In others best satisfaction may be had with capacitances as high
as $2,000 \mu \mu \mathrm{f}$. This is according to individual cases and can be determined by trial. The most convenient location for this capacitor is inside the highvoltage cage.

## 3. Dimensions

Before attempting any of the substitutions listed here, make sure the substitute tube will fit into the available space. In the magnetic types try to choose a substitute with a neck length similar to the original. Differences in face plate curvatures may make it necessary, in some substitutions listed, to change the mask.

## 4. Change in Anode Connector

Either the ball-type or cavity-type anode connector is used on picture tubes. Instructions specify when a change is necessary.

## 5. Replacement or Deletion of Ion Trap

It is necessary to replace the ion trap with the type required by the manufacturer of the substitute tube. Some tubes do not require an ion trap and are being substituted for others requiring either a single or dual ion trap. In these cases,
the instruction is "Remove ion trap." Other tubes requiring a single ion trap can be substituted for by installing a dual ion trap and vice versa. In these cases instructions are given. Some manufacturers of picture tubes are using a new type gun requiring a single ion trap in tubes that formerly used a gun requiring a dual ion trap. It is therefore important to check the individual manufacturer's specification on the substitute tube being used.

## 6. Electrostatic and Self-Focus Tubes

When using electrostatic or self-focus tubes as substitutions for magnetically focused tubes, it is necessary to remove the focus coil from the neck of the tube and replace it with a magnetic centering device. The focus coil may be left in the receiver circuit-wise, in which case it should be mounted in the cabinet in some position where its magnetic field has no effect on the picture. It may be replaced with a choke or resistor. The picture tube socket may have to be changed when it is necessary to bring out a lead from the focus electrode on the picture tube base except in the case of self-focus or automatic focus types. This lead should be connected to a d-c voltage point in the set which gives best focus. The voltage required normally lies between 50 and 350 volts. Self-focus or automatic focus tubes have a special gun structure within the neck of the tube designed
to focus the tube automatically without the use of an external focus voltage.

## 7. Substituting Electrostatic or Automatic Focus Types with Magnetic Types

When replacing electrostatic focus types with magnetic focus types, discard the magnetic centering device and install a permanent magnet focusing device. This must be mounted on the yoke support with suitable metal brackets. It is practical to replace an electrostatic focus tube using high-focus voltage with a type using low-focus voltage or a self-focus type. When doing this, it is desirable to remove the focus voltage rectifier as a safety measure.

## 8. Differences in the Face Plate

Differences in the face plate of the tube have little effect on whether or not they may be substituted. Dark-faced tubes give better contrast than white-faced tubes. Some tubes are frosted to decrease reflections and others have an aluminized back for better contrast and brightness. Aluminized tubes in some cases have higher anode voltage applied and this voltage should be reduced in accordance with manufacturers' specifications when other than aluminized tubes are substituted. When substituting aluminized tubes for white- or gray-faced tubes, sufficient voltage is usually available for satisfactory operation.

## PICTURE TUBE SUBSTITUTIONS

| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 7 CP 4 | 7DP4 | Change anode connector to cavity type. Connect external conductive coating to chassis. Change ion trap to double. |
| 7DP4 | 7 CP 4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. Change anode connector to ball type. Qemove ion trap. |
| 12 KP 4 | $\begin{aligned} & \text { 12ZP4 } \\ & 12 \mathrm{ZP} 4 \mathrm{~A} \end{aligned}$ | Install single ion trap. Install single ion trap. |
| 12LP4 | $\begin{aligned} & 12 \mathrm{ZP} 4 \\ & 12 \mathrm{ZP} 4 \mathrm{~A} \end{aligned}$ | Install single ion trap. Install single ion trap. |
| 12QP4 | 12 ZP 4 12 ZP 4 A | Change anode connector to cavity type. Connect external conductive coating to chassis. <br> Change anode connector to cavity type. Connect external conductive coating to chassis. |
| 12TP4 | 12ZP4 | Connect external conductive coating to chassis. Change ion trap to single. |
| 122P4 | 12 KP 4 <br> 12 KP 4 A <br> 12LP4 | Remove ion trap. <br> Remove ion trap. <br> Only where $1-1 / 8$ inch greater length is available. Change ion trap to double. |
|  | 12LP4A | Same as for 12LP4. |
|  | 12QP4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. Change annode connector to ball type. |
|  | 12QP4A | Same as for 12 QP 4. |
|  | 12 TP 4 | Only where $1-1 / 8$ inch greater length is available. Connect a $500-\mu \mu \mathrm{f}$ $20-\mathrm{kv}$ capacitor from anode to chassis. Change ion trap to double. |
|  | 12ZP4A | No changes. |
| 14 HP 4 | 14QP4 | No changes. |
| 14QP4 | 14 HP 4 | No changes. |
| 16AEP4 | 16 ABP 4 | No changes. |
| 17ATP4 | 17AVP4 <br> 17AVP4A | No changes. No changes. |
| 17AVP4 | 17ATP4 <br> 17ATP4A | No changes. No changes. |
| 17QP4 | 17YP4 | No changes. |
| 17YP4 | $\begin{aligned} & 17 \mathrm{QP} 4 \\ & 17 \mathrm{QP} 4 \mathrm{~A} \end{aligned}$ | No changes. <br> No changes. |
| 20HP4 | $\begin{aligned} & 20 \mathrm{HP} 4 \mathrm{D} \\ & 20 \mathrm{LP} 4 \\ & 20 \mathrm{MP} 4 \end{aligned}$ | No changes. <br> No changes. <br> No changes. |
| 20LP4 | $\begin{aligned} & 20 \mathrm{HP} 4 \mathrm{~A} \\ & 20 \mathrm{HP} 4 \mathrm{D} \\ & 20 \mathrm{MP} 4 \end{aligned}$ | No changes. <br> No changes. <br> No changes. |
| 20MP4 | $\begin{aligned} & 20 \mathrm{HP} 4 \mathrm{~A} \\ & 20 \mathrm{HP} 4 \mathrm{D} \\ & 20 \mathrm{LP} 4 \end{aligned}$ | No changes. <br> No changes. <br> No changes. |
| 21ACP4 | $\begin{aligned} & 21 \mathrm{ACP} 4 \mathrm{~A} \\ & \text { 21AMP4 } \\ & \text { 21AMP4A } \\ & 21 \mathrm{AQP} 4 \\ & 21 \mathrm{AQP} 4 \mathrm{~A} \\ & 21 \mathrm{BSP} 4 \end{aligned}$ | No changes. <br> No changes. <br> No changes. <br> Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. <br> Same as for 21AQP4. <br> No changes. |
| 21AFP4 | 21ASP4 <br> (Cont.) | No changes. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 21AFP4 | 21YP4 | Connect external conductive coating to ground. |
| (Cont.) | 21YP4A | Connect external conductive coating to ground. |
| 21ALP4 | 21ALP4A | No changes. |
|  | 21ALP4B | No changes. |
|  | 21ANP4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21ANP4A | No changes. |
|  | 21ATP4 | No changes. |
|  | 21ATP4A | No changes. |
| 21AMP4 | 21ACP4 | No changes. |
|  | 21ACP4A | No changes. |
|  | 21AMP4A | No changes. |
|  | $21 \mathrm{AQP4}$ | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21AQP4A | No changes. |
| 21AMP4A | $21 \mathrm{ACP4}$ | No changes. |
|  | 21ACP4A | No changes. |
|  | 21AMP4 | No changes. |
|  | 21AQP4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
| 21ANP4 | $21 \mathrm{ALP4}$ | Connect external conductive coating to chassis. |
|  | 21ALP4A | Connect external conductive coating to chassis. |
|  | 21ALP4B | Connect external conductive coating to chassis. |
|  | 21ATP4 | Connect external conductive coating to chassis. |
| 21AP4 | 21ZP4 | This substitute to be used only when changing from metal to glass picture tube. Mask opening must be enlarged. Change anode connector to cavity type. |
|  | 21ZP4B | Same as 21 AP 4 to 21 ZP 4 . Connect external conductive coating to chassis. |
| 21AQP4 | $21 \mathrm{ACP4}$ | Connect external conductive coating to chassis. |
|  | 21ACP4A | Connect external conductive coating to chassis. |
|  | 21 AMP4 | Connect external conductive coating to chassis. |
|  | 21AMP4A | Connect external conductive coating to chassis. |
|  | 21AQP4A | No changes. |
| 21AQP4A | $21 \mathrm{ACP4}$ | Connect external conductive coating to chassis. |
|  | 21ACP4A | Connect external conductive coating to chassis. |
|  | 21AMP4 | Connect external conductive coating to chassis. |
|  | 21AMP4A | Connect external conductive coating to chassis. |
|  | 21AQP4 | No changes. |
| 21ARP4 | 21ARP4A | No changes. |
|  | 21JP4 | No changes. |
|  | 21JP4A | No changes. |
| 21ARP4A | 21ARP4 | No changes. |
|  | $21 . J P 4$ | No changes. |
|  | 21JP4A | No changes. |
| 21ASP4 |  | Connect external conductive coating to chassis. |
|  | $21 \mathrm{XP} 4$ | Connect external conductive coating to chassis. |
|  | 21XP4A | Connect external conductive coating to chassis. |
|  | 21YP4 | Connect external conductive coating to chassis. |
|  | 21YP4A | Connect external conductive coating to chassis. |
| 21ATP4 | 21ALP4 | No changes. |
|  | 21ALP4A | No changes. |
|  | 21ALP4B | No changes. |
|  | 21ANP4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21ANP4A | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21ATP4A | No changes. |
| 21ATP4A | 21ALP4 | No changes. |
|  | 21ALP4A | No changes. |
|  | 21ALP4B | No changes. |
|  | 21ANP4 | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21ANP4A | Connect a $500-\mu \mu \mathrm{f} 20-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21ATP4 | No changes. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 21AUP4 | 21AUP4A | No changes. |
|  | 21AUP4B | No changes. |
|  | 21AVP4 | No changes. |
|  | 21AVP4A | No changes. |
|  | 21AVP4B | No changes. |
| 21AUP4A | 21 AUP4 | No changes. |
|  | 21AUP4B | No changes. |
|  | 21AVP4 | No changes. |
|  | 21AVP4A | No changes. |
|  | $21 \mathrm{AVP4B}$ | No changes. |
| 21AUP4B | 21AUP4 | No changes. |
|  | 21AUP4A | No changes. |
|  | 21AVP4 | No changes. |
|  | 21AVP4A | No changes. |
|  | 21 AVP 4 B | No changes. |
| 21AVP4 | 21 AUP4 | No changes. |
|  | 21AUP4A | No changes. |
|  | 21AUP4B | No changes. |
|  | 21AVP4A | No changes. |
|  | 21AVP4B | No changes. |
| 21AVP4A | 21 AUP4 | No changes. |
|  | 21AUP4A | No changes. |
|  | 21AUP4B | No changes. |
|  | 21AVP4 | No changes. |
|  | 21AVP4B | No changes. |
| 21AVP4B | 21AUP4 | No changes. |
|  | 21AUP4A | No changes. |
|  | 21AUP4B | No changes. |
|  | 21AVP4 | No changes. |
|  | 21AVP4A | No changes. |
| 21AYP4 | 21ASP4 | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21 XP 4 | No changes. |
|  | 21XP4A | No changes. |
|  | 21 YP 4 | No changes. |
|  | 21YP4A | No changes. |
| 21BSP4 | 21ACPYA | No changes. |
| 21JP4 | 21ARP4 | No changes. |
|  | 21ARP4A | No changes. |
|  | $21 \mathrm{JP4A}$ | No changes. |
| 21JP4A |  |  |
|  | 21ARP4A | No changes. |
|  | 21 JP 4 | No changes. |
| 21 MP 4 | 21 YP 4 | This substitute to be used only when changing from metal to |
|  |  | glass picture tube. Mask opening must be altered. Change anode connector to cavity type. |
|  | 21YP4A | Same as 21 MP 4 to 21 YP 4 procedure. |
| 21XP4 |  | Connect a $500-\mu \mu f 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21XP4A | No changes. |
|  | 21YP4 | No changes. |
|  | 21YP4A | No changes. |
| 21XP 4A | 21ASP4 | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
|  | 21 XP 4 | No changes. |
|  | 21 YP 4 | No changes. |
|  | 21YP4A | No changes. |
| 21YP4 | 21YP4A | No changes. |
| 21YP4A | 21YP4 | No changes. |


| TUBE | SUB. | CHANGES NECESSARY |
| :---: | :---: | :---: |
| 24BP4 |  | No practical substitute. |
| $24 \mathrm{CP4}$ | 24CP4A | No changes. |
|  | 24 QP 4 | No changes. |
|  | 24 TP 4 | No changes. |
|  | 24VP4 | No changes. |
|  | 24VP4A | No changes. |
|  | $24 \times P 4$ | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 24DP4 | 24DP4A | No changes. |
|  | 24YP4 | No changes. |
|  | 24ZP4 | No changes. |
| 24QP4 | 24 CP 4 | No changes. |
|  | 24 CP 4 A | No changes. |
|  | 24 TP 4 | No changes. |
|  | 24 VP 4 | No changes. |
|  | 24VP4A | No changes. |
|  | 24XP4 | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 24TP4 | 24 CP 4 | No changes. |
|  | 24CP4A | No changes. |
|  | 24QP4 | No changes. |
|  | $24 \mathrm{VP4}$ | No changes. |
|  | 24VP4A | No changes |
|  | 24XP4 | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 24VP4 | 24 CP 4 | No changes. |
|  | 24CP4A | No changes. |
|  | 24 TP 4 | No changes. |
|  | $24 \mathrm{VP4} 4$ | No changes. |
|  | 24XP4 | Connect a $500-\mu \mu \mathrm{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 24VP4A |  | No changes. |
|  | $24 \mathrm{CP} 4 \mathrm{~A}$ | No changes. |
|  | 24TP4 | No changes. |
|  | $24 \mathrm{VP4}$ | No changes. |
|  | 24XP4 | Connect a $500-\mu \mu \mathbf{f} 25-\mathrm{kv}$ capacitor from anode to chassis. |
| 24XP4 | 24 CP 4 | Connect external conductive coating to chassis. |
|  | 24CP4A | Connect external conductive coating to chassis. |
|  | $24 \mathrm{QP} 4$ | Connect external conductive coating to chassis. |
|  | $24 \mathrm{TP} 4$ | Connect external conductive coating to chassis. |
|  | $24 \mathrm{VP} 4$ | Connect external conductive coating to chassis. |
|  | 24VP4A | Connect external conductive coating to chassis. |
| 24YP4 | 24DP4 | No changes. |
|  | 24DP4A | No changes. |
|  | $24 Z \mathrm{P} 4$ | No changes. |
| 24ZP4 | 24DP4 | No changes. |
|  | 24 YP 4 | No changes. |
| 27AP4 |  | No practical substitute. |
| 27MP4 | 27EP4 | This substitute to be used only when changing from metal to glass picture tube. Mask opening may be altered. Change anode connector to cavity type. |
| 27SP4 | 27UP4 | No changes. |
| 27UP4 | 27SP4 | No changes. |
| 30BP4 |  | No practical substitute. |

## EUROPEAN - AMERICAN TUBE SUBSTITUTION

| EUROPEAN | AMERICAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| B36 | 12SN7 | G | No changes. |
| B65 | 6SN7 | G | No changes. |
| B152 | 12AT7 | G | No changes. |
| B309 | 12AT7 | G | No changes. |
| B319 | 7AN7 | G | No changes. |
| B329 | 12AU7 | E | No changes. |
| B719 | 6AQ8 | G | No changes. |
| D63 | 6H6 | G | No changes. |
| D77 | 6AL5 | E | No changes. |
| D152 | 6AL5 | G | No changes. |
| DA90 | 1 A 3 | E | No changes. |
| DAC32 | ${ }_{1} 1 \mathrm{H5}$ | E | No changes. |
|  | 1LH4 | G | Reverse 1LH4 to DAC32 procedure. |
| DAF91 | 1LD5 | G | Reverse 1LD5 to DAF91 procedure. |
|  | 1S5 | E | No changes. |
|  | 1 U 5 | G | Reverse 1U5 to DAF91 procedure. |
| DAF96 | 1 AH5 | E | No changes. |
| DC70 | 6375 | G | No changes. |
| DC80 | 1E3 | E | No changes. |
| DCC90 | 3A5 | E | No changes. |
| DD6 | 6AL5 | E | No changes. |
| DD7 | 6AL5 | G | No changes. |
| DF33 | 1 LC 5 | G | Reverse 1LC5 to DF33 procedure. |
|  | 1LN5 | G | Reverse 1LN5 to DF'33 procedure. |
|  | 1N5 | E |  |
| DF62 | 1AD4 | E | No changes. |
| DF91 | 1T4 | E | No changes. |
| DF92 | 1L4 | G | No changes. |
| DF96 | 1AF4 | G | No changes. |
|  | 1AJ4 | E | No changes. |
| DF904 | 1U4 | G | No changes. |
| DH63 | 6Q7 | G | No changes. |
| DH77 | 6AT6 | E | No changes. |
| DH149 | 7 C 6 | G | No changes. |
| DK32 | 1 A 7 | E |  |
|  | 1LA6 | G | Reverse 1LA6 to DK32 procedure. |
| DK91 | 1R5 | E | No changes. |
| DK92 | 1AC6 | E | No changes. |


| EUROPEAN | AMERICAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| DK96 | 1 AB6 | E | No changes. |
| DL33 | 3Q5 | E | No changes. |
| DL35 | 1 C 5 | E | No changes. |
| DL36 | 1Q5 | E | No changes. |
| DL91 | 154 | G | No changes. |
| DL92 | 3S4 | E | No changes. |
| DL93 | 3A4 | E | No changes. |
| DL94 | 3 Y 4 | E | No changes. |
| DL95 | 3Q4 | E | No changes. |
| DL96 | 3C4 | E | No changes. |
| DM70 | 1M3 | G | No changes. |
| DP61 | 6 AK5 | E | No changes. |
| DY30 | 1B3 | G | No changes. |
| DY80 | 1 X 2 A | G | No changes. |
| EA76 | 6489 | E | No changes. |
| EAA91 | 6AL5 | G | No changes. |
| EABC80 | $\begin{aligned} & \text { 6AK8 } \\ & \text { 6T8 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{G} \end{aligned}$ | No changes. <br> No changes. |
| EB34 | 6H6 | E | Parallel circuits only. No changes. |
| EB91 | 6AL5 | E | No changes. |
| EBC33 | 1639 | G | No changes. |
| EBC90 | 6AT6 | E | No changes. |
| EBC91 | 6AV6 | G | No changes. |
| EBF80 | 6N8 | E | No changes. |
| EC70 | 5718 | G | No changes. |
| EC80 | 6Q4 | E | No changes. |
| EC81 | 6R4 | E | No changes. |
| EC90 | 6 C 4 | E | No changes. |
| EC91 | 6AQ4 | E | No changes. |
| EC92 | $6 \mathrm{AB4}$ | E | No changes. |
| ECC33 | 6SN7 | G | Parallel circuits only. No changes. |
| ECC35 | 6 SL 7 | G | Parallel circuits only. No changes. |
| ECC81 | 12AT7 | E | No changes. |
| ECC82 | $12 \mathrm{AU7}$ | E | No changes. |
| ECC83 | 12AX7 | E | No changes. |
| ECC85 | 6AQ8 | E | No changes. |
| ECC91 | 6J6 | E | No changes. |




| EUROPEAN | AMERICAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| EM34 | 6 CD 7 | E | No changes. |
| EM80 | 6BR5 | E | No changes. |
| EN91 | 2D21 | E | No changes. |
| EQ80 | 6BE7 | E | No changes. |
| EY51 | 6X2 | E | No changes. |
| EY70 | 5641 | G | No changes. |
| EY80 | 6U3 | E | No changes. |
| EY84 | 6374 | E | No changes. |
| EZ35 | 6X5 | E | No changes. |
| EZ80 | 6V4 | E | No changes. |
| EZ81 | 6BW4 | E | No changes. |
| EZ90 | 6X4 | E | No changes. |
| GZ30 | 5Z4 | E | No changes. |
| GZ32 | 5V4 | E | No changes. |
| GZ34 | 5 U 4 | G | No changes. |
| H52 | 5U4 | G | No changes. |
| H63 | 6F5 | E | No changes. |
| HBC90 | 12AT6 | E | No changes. |
| HBC91 | 12AV6 | G | No changes. |
| HD14 | 1H5 | G | No changes. |
| HD30 | 3B4 | E | No changes. |
| HF93 | 12BA6 | E | No changes. |
| HF94 | 12AU6 | G | No changes. |
| HK90 | 12BE6 | E | No changes. |
| HL90 | 19AQ5 | E | No changes. |
| HL92 | 50 C 5 | E | No changes. |
| HM04 | 6BE6 | E | No changes. |
| HY90 | 35W4 | E | No changes. |
| KBC32 | 1H6 | G | Reverse 1H6 to KBC32 procedure. |
| KF'35 | 1E5 | E | No changes. |
| KK32 | $1 \mathrm{C6}$ | G | Reverse 1C6 to KK32 procedure. |
|  | $1 \mathrm{C7}$ | G | No changes. |
|  | 1D7 | G | Parallel circuits only. No changes. |
| KL35 | 1F4 | G | Reverse 1F4 to KL35 procedure. |
|  | 1F5 | G | No changes. |
| KT32 | 25L6 | G | No changes. |
| KT63 | $\begin{aligned} & 6 \mathrm{~F} 6 \\ & 6.57 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. No changes. |


| EUROPEAN | AMERICAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| KT66 | 6L6 | E | Parallel circuits only. No changes |
| KT81 | $7 \mathrm{C5}$ | G | No changes. |
| KTW63 | 6K7 | G | No changes. |
| L63 | 635 | G | No changes. |
| L77 | 6C4 | E | No changes. |
| LN152 | 6 AB8 | G | No changes. |
| LZ319 | 8A8 | G | No changes. |
| N14 | $1 \mathrm{C5}$ | G | No changes. |
| N17 | 354 | E | No changes. |
| N18 | 3Q4 | E | No changes. |
| N19 | 3V4 | E | No changes. |
| N77 | 6 AM5 | E | No changes. |
| N78 | $6 \mathrm{BJ5}$ | E | No changes. |
| N144 | 6AN5 | G | No changes. |
| N148 | 7 C 5 | G | No changes. |
| N152 | 21A6 | G | No changes. |
| N329 | 16A5 | G | No changes. |
| N359 | 21 A6. | G | No changes. |
| N709 | 6BQ5 | G | No changes. |
| PABC80 | 9AK8 | E | No changes. |
| PCC84 | 7AN7 | E | No changes. |
| PCC85 | 9AQ8 | E | No changes. |
| PCF 80 | $\begin{aligned} & \text { 8A8 } \\ & \text { 9A8 } \end{aligned}$ | $\underset{\mathrm{E}}{\mathbf{G}}$ | No changes. No changes. |
| PCF82 | $9 \mathrm{U8}$ | E | No changes. |
| PL21 | 2D21 | E | No changes. |
| PL81 | 21A6 | E | No changes. |
| PL82 | 16A5 | E | No changes. |
| PL83 | 15A6 | E | No changes. |
| PY80 | 19X3 | E | No changes. |
| PY81 | 17Z3 | E | No changes. |
| PY82 | 19Y3 | E | No changes. |
| QQV03-10 | 6360 | G | No changes. |
| QQV03-28 | 6252 | G | No changes. |
| QV05-25 | 807 | G | No changes. |
| SP6 | 6AM6 | E | No changes. |


| EUROPEAN | AMERICAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| TD03-10 | 5861 | G | No changes. |
| U50 | 5 Y 3 | G | No changes. |
| U52 | 5U4 | G | No changes. |
| U70 | $6 \times 5$ | G | No changes. |
| U78 | 6X4 | E | No changes. |
| U147 | 6X5 | G | No changes. |
| U149 | 7 Y 4 | G | No changes. |
| U154 | 19 Y 3 | G | No changes. |
| U319 | 19Y3 | G | No changes. |
| UF41 | 12AC5 | E | No changes. |
| UBC41 | 14 L 7 | E | No changes. |
| UCH42 | 14K7 | E | No changes. |
| W17 | 1 T 4 | E | No changes. |
| W63 | 6K7 | G | No changes. |
| W77 | 6065 | E | No changes. |
| W149 | 7B7 | G | No changes. |
| W179 | 6BY7 | G | No changes. |
| X14 | 1 A 7 | G | No changes. |
| X17 | 1R5 | E | No changes. |
| X18 | 1AC6 | E | No changes. |
| X63 | 6 A 8 | G | No changes. |
| X79 | 6AE8 | E | No changes. |
| X81 | 7S7 | G | No changes. |
| X148 | 7S7 | G | No changes. |
| Y61 | 6U5 | E | No changes. |
| Z14 | 1N5 | G | No changes. |
| Z63 | 6 J 7 | G | No changes. |
| Z77 | $\begin{aligned} & \text { 6AM6 } \\ & 6064 \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |
| Z152 | 6BX6 | G | No changes. |
| Z179 | 6BX6 | G | No changes. |
| ZD17 | 155 | E | No changes. |
| ZD19 | 1S5 | G | No changes. |
| 1F3 | 1 T 4 | E | No changes. |
| 1FD9 | 1S5 | E | No changes. |
| 1 P 10 | 3SF | E | No changes. |
| 6A7E | 6A7 | E | No changes. |


| EUROPEAN | AMERICAN | PERF. | $\quad$ CIRC |
| :--- | :--- | :---: | :--- |
| 6D2 | $6 A L 5$ | $G$ | No changes. |
| 6 F 12 | 6 AM 6 | G | No changes. |
| 8D3 | 6 AM 6 | E | No changes. |
| 30 C 1 | 8 A 8 | G | No changes. |
| 30 L 1 | 7AN7 | G | No changes. |


| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| OA2 | 150 C 2 | E | No changes. |
| OA4 | Z300T | E | No changes. |
| OB2 | 108C1 | G | No changes. |
| OD3 | 150 C 3 | E | No changes. |
| OE3 | 85A1 | E | No changes. |
| OG3 | 85A2 | E | No changes. |
| 1A3 | DA90 | E | No changes. |
| 1 A 7 | $\begin{aligned} & \text { DK32 } \\ & \text { X14 } \end{aligned}$ | $\begin{aligned} & E \\ & \mathrm{G} \end{aligned}$ | No changes. <br> No changes. |
| $1 \mathrm{AB6}$ | DK96 | E | No changes. |
| 1AC6 | $\begin{aligned} & \text { DK92 } \\ & \mathrm{X} 18 \end{aligned}$ | $\underset{\mathrm{E}}{\mathrm{E}}$ | No changes. <br> No changes. |
| 1 AD 4 | DF62 | E | No changes. |
| 1 AF 4 | DF96 | G | No changes. |
| 1 AH 5 | DAF96 | E | No changes. |
| $1 \mathrm{AJ4}$ | DF96 | E | No changes. |
| 1B3 | DY30 | G | No changes. |
| 1 C 5 | $\begin{aligned} & \text { DL35 } \\ & \text { N14 } \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{E}}$ | No changes. No changes. |

1C6 KK32 G Rewire as follows. Change socket to six pin.

|  | 2 | to | 3 |
| :---: | :---: | :---: | :---: |
| (3) 1 | 5 | to | 4 |
| (3) (3) | 4 | to | 5 |
| (1) (1) | 3 | to | 6 |
| ORIC | 6 | to | 7 |

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| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECE | ARY |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \mathrm{C7}$ | KK32 | G | No changes. |  |  |
| 1D7 | KK32 | G | Parallel circuits only. No changes. |  |  |
| 1E3 | DC80 | E | No changes. |  |  |
| 1E5 | KF35 | G | No changes. |  |  |
| 1F4 | KL35 | G | Rewire as follows: Change to five Change pin No. 1 | socket.  <br> to pin No. 2 <br> to 3 <br> to 4 <br> to 5 <br> to 7 |  |
| 1F5 | KL35 | G | No changes. |  |  |
| 1H5 | $\begin{aligned} & \text { DAC32 } \\ & \text { HD14 } \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{E}}$ | No changes. <br> No changes. |  |  |
| 1H6 | KBC32 | G | Rewire as follows: Change pin No. 6 to | id cap. |  |
| 1L4 | DF92 | G | No changes. |  |  |
| 1LA6 | DK32 | G | Rewire as follows: <br> Change pin No. 1 |  |  |
| 1LC5 | DF33 | G | Rewire as follows: <br> Change pin No. 1 | to pin No. 2 <br> to 3 <br> to 4 <br> to Cap <br> to 7 <br> to 7 |  |
| 1 LD 5 | DAF91 | G | Rewire as follows: <br> Change pin No. 1 <br> 4 <br>  | to $\operatorname{pin}$ No. 1 <br> to 3 <br> to 4 <br> to 5 <br> to 6 <br> to 7 |  |
| 1LH4 | DAC32 | G | Rewire as follows: | $l$  <br> to pin No. <br> to 3 <br> to 5 <br> to Cap <br> to 7 |  |
| 1LN5 | DF33 | G | Rewire as follows: <br> Change pin No. 1 |   <br> to pin No. <br> to  <br> to 3 <br> to 4 <br> to Cap <br> to 7 <br> to 7 |  |
| 1M3 | DM70 | G | No changes. |  |  |
| 1N5 | $\begin{aligned} & \text { DF33 } \\ & \text { Z14 } \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{E}}$ | No changes. No changes. |  |  |
| 1Q5 | DL36 | E | No changes. |  |  |


| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NEC | ARY |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1R5 | $\begin{aligned} & \text { DK91 } \\ & \mathrm{X} 17 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |  |
| 154 | DL91 | G | No changes. |  |  |
| 1S5 | $\begin{aligned} & \text { DAF91 } \\ & \text { ZD17 } \\ & \text { ZD19 } \\ & \text { 1FD9 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{G} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. No changes. No changes. |  |  |
| 1 T 4 | $\begin{aligned} & \text { DF91 } \\ & \text { W17 } \\ & \text { 1F3 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. <br> No changes. <br> No changes. |  |  |
| 1U4 | DF904 | G | No changes. |  |  |
| 1 U | D AF91 | G | Rewire as follows: <br> 4 | $\begin{aligned} & \text { to pin No. } 3 \\ & \text { to } \\ & \text { to } \\ & \text { to } \\ & 4 \\ & \hline \end{aligned}$ |  |
| 1X2A | DY80 | G | No changes. |  |  |
| 2D21 | $\begin{aligned} & \text { EN91 } \\ & \text { PL21 } \end{aligned}$ | $\underset{\mathrm{E}}{\mathrm{E}}$ | No changes. No changes. |  |  |
| 3 A 4 | DL93 | E | No changes. |  |  |
| $3 \mathrm{A5}$ | $\begin{aligned} & \text { DCC90 } \\ & \text { DL99 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{G} \end{aligned}$ | No changes. No changes. |  |  |
| 3B4 | HD30 | E | No changes. |  |  |
| 3 C 4 | DL96 | E | No changes. |  |  |
| 3Q4 | $\begin{aligned} & \text { DL95 } \\ & \text { N18 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |  |
| 3Q5 | DL33 | E | No changes. |  |  |
| 354 | $\begin{aligned} & \text { DL92 } \\ & \text { N17 } \\ & \text { 1P10 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. No changes. |  |  |
| 3V4 | $\begin{aligned} & \text { DL94 } \\ & \text { N19 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. No changes. |  |  |
| 5U4 | $\begin{aligned} & \text { GZ34 } \\ & \text { H52 } \\ & \text { U52 } \end{aligned}$ | $\begin{aligned} & \mathbf{G} \\ & \mathbf{G} \\ & \mathbf{G} \end{aligned}$ | No changes. <br> No changes. <br> No changes. |  |  |
| 5V4 | GZ32 | E | No changes. |  |  |
| 5 Y 3 | U50 | G | No changes. |  |  |
| 5Z4 | GZ30 | E | No changes. |  |  |
| 6A7 | 6A7E | E | No changes. |  |  |
| $6 \mathrm{A8}$ | X63 | G | No changes. |  |  |
| 6AB4 | EC92 | E | No changes. |  |  |
| $6 \mathrm{AB8}$ | $\begin{aligned} & \text { ECL80 } \\ & \text { SN152 } \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{E}}$ | No changes. No changes. |  |  |
| 6 AE8 | X79 | E | No changes. |  |  |
| 6AG5 | EF96 | G | No changes. |  |  |


| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6AJ8 | ECH81 | E | No changes. |
|  | DP61 | E | No changes. |
| 6AK5 | EF95 | E | No changes. |
| 6AK6 | EL91 | G | Reverse EL 91 to 6AK6 procedure. |
| 6AK8 | EABC80 | E | No changes. |
| 6AL5 | D77 | E | No changes. |
|  | DD6 | E | No changes. |
|  | DD7 | G | No changes. |
|  | D152 | G | No changes. |
|  | EAA91 | G | No changes. |
|  | EB91 | E | No changes. |
|  | 6D2 | G | No changes. |
| 6AM5 | $\underset{\text { N77 }}{\text { EL91 }}$ | E | No changes. |
|  | N144 | G | No changes. |
| 6AM6 | EF91 | E | No changes. |
|  | SP6 | E | No changes. |
|  | Z77 | G | No changes. |
|  | 6 F 12 | G | No changes. |
|  | 8D3 | E | No changes. |
| 6AQ4 | EC91 | E | No changes. |
| 6AQ5 | EL90 | E | No changes. |
| 6AQ8 | B719 | G | No changes. |
|  | $\text { ECC } 85$ | E | No changes. |
| 6AT6 | DH77 | E | No changes. |
|  | EBC90 | E | No changes. |
| 6AU6 | EF94 | G | No changes. |
| 6AV6 | EBC91 | G | No changes. |
| 6BA6 | EF93 | E | No changes. |
|  | HMO4 | E | No changes. |
| 6BE6 | EK90 | E | No changes. |
| 6BE7 | EQ80 | E | No changes. |
| 6BJ5 | N78 | E | No changes. |
| 6BM8 | ECL82 | E | No changes. |
| 6BN5 | EL85 | E | No changes. |
| 6BQ5 | EL84 | E | No changes. |
|  | N709 | G | No changes. |
| 6BR5 | EM80 | E | No changes. |
| 6BW4 | EZ81 | E | No changes. |
| 6BX6 | EF80 |  | No changes. |
|  | Z152 | G | No changes. |
|  | Z179 | G | No changes. |
| 6 BY 7 | EF85 | E | No changes. |
|  | W179 | G | No changes. |
| 6 C 4 | EC90 | E | No changes. |
|  | L77 | E | No changes. |
| $6 \mathrm{CA7}$ | EL34 | G | No changes. |


| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 6 CD 7 | EM34 | E | No changes. |
| 6CH6 | EL821 | G | No changes. |
| 6CJ6 | EL81 | E | No changes. |
| 6CK6 | EL83 | G | No changes. |
| 6CN6 | EL38 | E | No changes. |
| 6CQ6 | EF92 | E | No changes. |
| 6CS6 | EH90 | E | No changes. |
| 6 E 8 | ECH35 | E | No changes. |
| 6F5 | H63 | E | No changes. |
| 6F6 | KT63 | G | No changes. |
| 6H6 | $\begin{aligned} & \text { EB34 } \\ & \text { D63 } \end{aligned}$ | $\underset{G}{E}$ | Parallel circuits only. No changes. No changes. |
| 655 | L63 | G | No changes. |
| 6J6 | ECC91 | E | No changes. |
| $6 J 7$ | $\begin{aligned} & \text { KT63 } \\ & \text { Z63 } \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. No changes. |
| 6K7 | $\begin{aligned} & \text { KTW63 } \\ & \text { W63 } \end{aligned}$ | $\underset{\mathrm{G}}{\mathrm{G}}$ | No changes. No changes. |
| 6L6 | $\begin{aligned} & \text { EL37 } \\ & \text { KT66 } \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | No changes. <br> Parallel circuits only. No changes. |
| 6M6G | EL33 | E | No changes. |
| 6 N 8 | EBF80 | E | No changes. |
| 6P8G | ECH35 | E | Parallel circuits only. No changes. |
| 6Q4 | EC80 | E | No changes. |
| 6Q7 | DH63 | G | No changes. |
| 6R4 | EC81 | E | No changes. |
| 6SL7 | ECC35 | G | Parallel circuits only. No changes. |
| 6SN7 | $\begin{aligned} & \text { B65 } \\ & \text { ECC33 } \end{aligned}$ | $\begin{aligned} & \mathrm{G} \\ & \mathrm{G} \end{aligned}$ | No changes. <br> Parallel circuits only. No changes. |
| 6 T 8 | EABC80 | G | No changes. |
| 6U3 | EY80 | E | No changes. |
| 6U5 | Y61 | E | No changes. |
| 6 U 8 | ECF 82 | E | No changes. |
| 6 V 4 | EZ880 | E | No changes. |
| 6 X 2 | EY51 | E | No changes. |
| 6X4 | $\begin{aligned} & \text { EZ90 } \\ & \text { U78 } \end{aligned}$ | $\underset{\mathrm{E}}{\mathrm{E}}$ | No changes. <br> No changes. |
| 6 X 5 | $\begin{aligned} & \text { EZ35 } \\ & \text { U147 } \\ & \text { U70 } \end{aligned}$ | E G G | No changes. <br> No changes. <br> No changes. |


| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECESSARY |
| :---: | :---: | :---: | :---: |
| 7AN7 | B319 | G | No changes. |
|  | PCC84 | E | No changes. |
|  | 30L1 | G | No changes. |
| 7B7 | W149 | G | No changes. |
| $7 \mathrm{C5}$ | KT81 | G | No changes. |
|  | N148 | G | No changes. |
| 7 C 6 | DH149 | G | No changes. |
| 757 | X81 | G | No changes. |
|  | X148 | G | No changes. |
| 7 Y 4 | U149 | G | No changes. |
| 8A8 | LZ319 | G | No changes. |
|  | PCF80 | G | No changes. |
|  | 30C1 | G | No changes. |
| 9A8 | PCF80 | E | No changes. |
| 9AK8 | PABC80 | E | No changes. |
| 9AQ8 | PCC85 | E | No changes. |
| $9 \mathrm{U8}$ | PCF82 | E | No changes. |
| 12AC5 | UF41 | E | No changes. |
| 12 AT 6 | HBC90 | E | No changes. |
| 12AT7 | B152 | G | No changes. |
|  | B309 | G | No changes. |
|  | ECC81 | E | No changes. |
| 12AU6 | B329 | E | No changes. |
|  | ECC82 | E | No changes. |
|  | HF94 | G | No changes. |
| 12AV6 | HBC91 | G | No changes. |
| 12AX7 | ECC83 | E | No changes. |
| 12BA6 | HF93 | E | No changes. |
| 12BE6 | HK90 | E | No changes. |
| 12SN7 | B36 | G | No changes. |
| 14K7 | UCH42 | E | No changes. |
| 14L7 | UBC4 1 | E | No changes. |
| 15A6 | PL83 | E | No changes. |
| 16A5 | N329 | G | No changes. |
|  | PL82 | E | No changes. |
| 17Z3 | PY81 | E | No changes. |
| 19AQ5 | HL90 | E | No changes. |
| 19X3 | PY80 | E | No changes. |
| 19 Y 3 | U154 | G | No changes. |
|  | U319 | G | No changes. |
|  | PY82 | E | No changes. |
| 21A6 | N152 | G | No changes. |
|  | N359 | G | No changes. |
|  | PL81 | E | No changes. |


| 25L6-6489 | IRD | SUPP | MENT - RECEIVING TUBE SUBSTITUTION GUIDE |
| :---: | :---: | :---: | :---: |
| AMERICAN | EUROPEAN | PERF. | CIRCUIT CHANGES NECESSARY |
| 25L6 | KT32 | G | No changes. |
| 35W4 | HY90 | E | No changes. |
| 50C5 | HL92 | E | No changes. |
| 807 | QV05-25 | G | No changes. |
| 1639 | EBC33 | G | No changes. |
| 5641 | EY70 | G | No changes. |
| 5718 | EC70 | G | No changes. |
| 5840 | EF72 | G | No changes. |
| 5861 | TD03-10 | G | No changes. |
| 5899 | EF71 | G | No changes. |
| 6064 | Z77 | G | No changes. |
| 6065 | W77 | G | No changes. |
| 6252 | QQV03-28 | G | No changes. |
| 6267 | EF86 | E | No changes. |
| 6360 | QQV03-10 | G | No changes. |
| 6373 | EL70 | G | No changes. |
| 6374 | EY84 | E | No changes. |
| 6375 | DC70 | G | No changes. |
| 6487 | EF70 | G | No changes. |
| 6488 | EF73 | E | No changes. |
| 6489 | EA76 | E | No changes. |

## CUMULATIVE INDEX

The following indices contain all the tubes listed in the Receiving Tube Substitution Guidebook, including those given in the First, Second and Third Supplements, for which substitutions are given.

Where (0) precedes the page number, the substitution information is given on the page referred to in the original Receiving Tube Substitution Guidebook; where (1) precedes the page number, the substitution information is given on the page referred to in the First Supplement; where (2) precedes the page number, the substitution information is given on the page referred to in the Second Supplement; where (3) precedes the page number, the substitution information is given on the page referred to in the Third Supplement.

Page references to European substitutes for American tubes have been included under the respective American tube numbers, and are asterisked. Page references to American substitutes for European tubes are listed in the European Index.

## RECEIVING TUBES

| TUBE | PAGE | TUBE | PAGE | TUBE | PAGE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00A | (0)33 | $1 \mathrm{AB5}$ | (0)35 | 1B3 | $\begin{aligned} & (0) 36 \\ & (1) 14,15 \end{aligned}$ |
| 01A | (0)33 | 1AB6 | (3) $1,44^{*}$ |  | $\text { (2) } 1$ |
| 0A2 | (0)33 | 1AC5 | (0)35 |  | (3) $1,44^{*}$ |
|  | (3)44* |  | (3)1 | 1B4 | (0)36 |
| 0A3 | $\begin{aligned} & (0) 33 \\ & (1) 13 \end{aligned}$ | 1AC6 | (3)1, 44* | 1B5 | (0)36 |
| 0A4 | (0)33 | 1AD4 | (3)44* | 1B8 | $(0) 37$ |
|  | (3)44* |  |  |  |  |
| 0B2 | $\begin{aligned} & (0) 33 \\ & (3) 44^{*} \end{aligned}$ | $1 \mathrm{AE} 4$ | (0)35, 36 | 1-3 | $\begin{aligned} & (0) 37 \\ & (3) 1,2 \end{aligned}$ |
|  |  |  | $\begin{aligned} & (0) 36 \\ & (1) 14 \end{aligned}$ |  |  |
| 0B3 | $\begin{aligned} & (0) 33 \\ & (3) 1 \end{aligned}$ | 1 AE5 | (3)1 | 1 C 5 | (0)37 <br> (1)15 <br> (3)44* |
|  |  |  |  |  |  |
| 0C3 | (0)33 | 1AF4 | $\begin{aligned} & (0) 36 \\ & (3) 1,44^{*} \end{aligned}$ | 1 C 6 | $\begin{aligned} & (0) 37 \\ & (3) 44^{*} \end{aligned}$ |
| 0D3 | $\begin{aligned} & (0) 33 \\ & (3) 44^{*} \end{aligned}$ | 1AF5 | $\begin{aligned} & (0) 36 \\ & (1) 14 \end{aligned}$ |  |  |
| OE3 | (3)44* |  |  | $1 \mathrm{C7}$ | $\begin{aligned} & (0) 37 \\ & (3) 45^{*} \end{aligned}$ |
| 0G3 | (3)44* | 1AF6 | (3)1 | $1 \mathrm{C8}$ | (0)37 |
| 0 Y 4 | (0)33 | 1AG4 | (3) 1 | 1 C 21 | (0)37 |
| 0Z4 | $\begin{aligned} & (0) 33 \\ & (1) 13,14 \end{aligned}$ | 1AG5 | (3)1 | 1D3 | (3)2 |
|  |  | 1AH4 | (3)1 | 1D5 | (0)38 |
| 0Z4A | (0)33 | 1AH5 | (3)1, 44* | 1D5GT | (2) 1 |
| 1A3 | $\begin{aligned} & (0) 33 \\ & (3) 44^{*} \end{aligned}$ | 1AH6 | (3) 1 | 1D7 | $\begin{aligned} & (0) 38 \\ & (3) 45^{*} \end{aligned}$ |
| 1A4 | (0)33, 34 | 1 AJ 4 | (3) $1,44 *$ |  |  |
|  | (1)14 | 1 AJ5 | (3)1 | 1D8 | (0)38 |
| 1A5 | $\begin{aligned} & (0) 34 \\ & (1) 14 \end{aligned}$ | 1 AK4 | (3) 1 | 1E3 | (3)2, 45* |
| 1A6 | (0)34 | 1AK5 | (3) 1 | 1E4 | $\begin{aligned} & (0) 38 \\ & (3) 2 \end{aligned}$ |
| 1A7 | (0) 34,35 <br> (1)14 <br> (3) $44^{*}$ | 1 AX 2 | (3)1 | 1E5 | $\begin{aligned} & (0) 38 \\ & (3) 45^{*} \end{aligned}$ |


| TUBE | PAGE | TUBE | PAGE | TUBE | PAGE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 E 7 | (0)38 | 1LF3 | (3)2 | 1V | $\begin{aligned} & (0) 47 \\ & (1) 19 \end{aligned}$ |
| 1E8 | (0)38 | 1LG5 | (0)43 <br> (1)17 |  |  |
| 1F4 | (0)38 <br> (1)15 <br> (3)45* |  |  | 1V2 | (0)47 |
|  |  | 1LH4 | (0) 43 <br> (1) 17,18 <br> (3) $45^{*}$ | 1V5 | (0)47 |
|  |  |  |  | 1V6 | (3)2 |
| 1 F 5 | (0)38 (1)15 | 1LN5 | $\begin{aligned} & \text { (0) } 43,44 \\ & \text { (1)18 } \\ & \text { (3) } 45^{*} \end{aligned}$ | 1W4 | (0)48 |
|  | (3) $45^{*}$ |  |  |  | (1)19 |
| 1F6 | (0)38 | 1M3 | (3)2, 45* | 1W5 | (0)48 |
| 1F7 |  |  |  | 1X2 | (0)48 |
|  | (0)39 | 1N5 | (0) 44 <br> (1)18 <br> (3)45* |  | (1)19, 20 |
| 1G4 | (0)39 |  |  |  | (2)1 |
| 1G5 | $\begin{aligned} & (0) 39 \\ & (1) 15 \end{aligned}$ |  |  | 1X2A | (1)20 |
|  |  | 1N6 | (0)44,45 |  | $\begin{aligned} & \text { (2) } 1 \\ & \text { (3) } 46^{*} \end{aligned}$ |
| 1G6 | $\begin{aligned} & (0) 39 \\ & (1) 15 \end{aligned}$ | 1P5 | $\begin{aligned} & (0) 45 \\ & (1) 18 \end{aligned}$ | 1Y2 | (1)20 |
|  |  |  |  | 1Z2 | (0)48 |
| 1H4 | $\begin{aligned} & (0) 39 \\ & (1) 15 \end{aligned}$ | 1Q5 | (0)45 <br> (1)18 <br> (3) $45^{*}$ |  | (1)20 |
|  |  |  |  | 2A3 | (0)48 |
| 1H5 | $\begin{aligned} & (0) 39 \\ & (1) 15 \\ & (3) 45 * \end{aligned}$ |  |  |  | (1)20 |
|  |  | 1Q6 | (0)45 |  | (3)2 |
|  |  | 1R4/1294 | (0)45 | 2A4G | (0)48 |
| $1 \mathrm{H6}$ | $\begin{aligned} & (0) 39 \\ & (3) 45^{*} \end{aligned}$ | 1R5 |  |  |  |
|  |  |  | $\begin{aligned} & (0) 45 \\ & (3) 46^{*} \end{aligned}$ | 2A5 | (0)48 |
| 1J5 | $\begin{aligned} & (0) 39 \\ & (1) 16 \end{aligned}$ | 154 |  | $2 \mathrm{A6}$ | (0)48 |
|  |  |  | $\begin{aligned} & (0) 46 \\ & \text { (1)18, } 19 \\ & \text { (3)46* } \end{aligned}$ | 2 A 7 | (0)48 |
| 1 J 6 | $\begin{aligned} & (0) 39 \\ & (1) 16 \end{aligned}$ |  |  |  |  |
|  |  |  |  | 2AF4 | (3)2 |
| 1L4 | (0)39 <br> (1) 16 <br> (3)45* | 155 | (0)46 <br> (1) 19 <br> (3) $46^{*}$ | 2B3 | (3)2 |
|  |  |  |  |  | (3)2 |
|  |  |  |  | 2B5 | (3)2 |
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| 33 | $(0) 122$ $\text { (1) } 40$ | 48 49 | $(0) 129$ $(0) 129$ | 58S | (0)131 |

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| 5633 | (3)28 | 5725 | $\begin{aligned} & (0) 141 \\ & (3) 28 \end{aligned}$ | 5901 | (0)142 |
| 5634 | (3)28 |  |  | 5910 | (0) 142 |
| 5635 | (0)140 | 5726 | $\begin{aligned} & (0) 141 \\ & (3) 28 \end{aligned}$ |  | (0)142 <br> (3)29 |
|  |  |  |  | 5915 |  |
| 5636 | (0)140 | 5727 | (3)29 |  |  |
| 5637 | (3)28 | 5731 | (0)141 | 5930 | (3)29 |
| 5638 | (3)28 | 5732 | (3)29 | 5931 | $\begin{aligned} & (0) 142 \\ & (3) 29 \end{aligned}$ |
| 5641 | (3)50* | 5744 | (0)141 | 5932 | $(0) 142$ <br> (3) 29 |
| 5642 | (1)44 | 5749 | (3)29 |  |  |
| 5643 | (0)140 | 5750 | (3)29 | 5933 | (3)29 |
| 5646 | (0)140 | 5751 | (3)29 | 5961 | (3)29 |
| 5647 | (0)140 | 5751WA | (3)29 | 5963 | (3)29 |
| 5654 | $\begin{aligned} & (0) 140 \\ & (3) 28 \end{aligned}$ | 5783 | (0)141 | 5964 | (3)29 |
| 5670 | $\begin{aligned} & (0) 140 \\ & (2) 12 \\ & (3) 28 \end{aligned}$ | 5784 | (0)141 | 5965 | (3)29 |
|  |  | $5785 \quad(0) 141$ |  | 5992 | (3)30 |
| 5670WA | (3) 28 | 5787 | $(0) 141$ | $6005$ | (3) 30 |
| 5672 | (0)140 | $5812$ |  |  | (3)30 |
| 5676 | (0)140 | 5814 | (3)29 | 6006 | (3)30 |
| 5677 | (0)140 | 5823 | (0)141 | 6046 | (3)30 |
| 5678 | (0)140 | 5824 | $\begin{aligned} & (0) 141 \\ & (3) 29 \end{aligned}$ | 6057 | (3)30 |
| 5679 | $\begin{aligned} & (0) 140 \\ & (3) 28 \end{aligned}$ | 5838 | (3)29 | 6058 6059 | (3)30 (3)30 |
| 5686 | (0)140 | 5839 | (3)29 | 6060 | (3)30 |
| 5687 | (0)140 | 5840 | $\begin{aligned} & (0) 141 \\ & (3) 50^{*} \end{aligned}$ | 6061 | (3)30 |
| 5691 | (0)140 | 5847 | (0)141 | 6063 | (3)30 |
| 5692 | $\begin{aligned} & (0) 141 \\ & (3) 28 \end{aligned}$ | 5861 | (3)50* | 6064 | (3) $30,50^{*}$ |
| 5693 | (0)141 | 5871 | (3)29 | 6065 | (3)30, 50* |
| 5694 | (0)141 | 5879 | (0)141 | 6066 | (3) 30 |
| 5697 | (0)141 | 5881 | $\begin{aligned} & (1) 44 \\ & (3) 29 \end{aligned}$ | 6067 | (3)30 |
| 5702 | (0)141 | 5896 | (0)141 | 6072 | (3)30 |
| 5703 | (0)141 | 5897 | (0)141 | 6095 | (3) 30 |
| 5704 | (0)141 | 5898 | (0)142 | 6096 | (3)30 |
| 5718 | $\begin{aligned} & (0) 141 \\ & (3) 50^{*} \end{aligned}$ | 5899 | $\begin{aligned} & (0) 142 \\ & (3) 29,50^{*} \end{aligned}$ | 6097 | (3)30 |
| 5719 | (0)141 | 5900 | $\begin{aligned} & (0) 142 \\ & (3) 29 \end{aligned}$ | $\begin{aligned} & 6101 \\ & 6113 \end{aligned}$ | $\begin{aligned} & (3) 30 \\ & (3) 30 \end{aligned}$ |
| 5722 | (0)141 |  |  |  |  |

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| 6135 | (3)31 | 6374 | (3) $50{ }^{*}$ | 7000 | $\begin{aligned} & (0) 144 \\ & (3) 31 \end{aligned}$ |
| 6136 | (3)31 | 6375 | (3)50* |  |  |
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[^0]:    1J. F. Rider and S. D. Uslan, Encyclopedia on Cathode-Ray
    Oscilloscopes and Their Uses, John F. Rider Publisher, Inc., New York, N. Y., 1950, pp. 389-401.

[^1]:    (3)

    3C
    
    3G

[^2]:    Type GV hos TAF bnse.

[^3]:    With input choke of at least 20 herrys.
    ${ }^{1}$ With input choke of at le
    ${ }^{2}$ Tapped for pilof lomps.
    ${ }^{3}$ Per poin with cho
    ${ }^{5}$ With 100 ohms min. resistance In series with plate; witheut series resistor, maximum r.m.s. plate rating is 117 volits.

[^4]:    - Same as $872 \mathrm{AA} / 372$ excepl for heavy -duty push-type base. Filament connected to pins 2 and 3, plate to top cap.
    Choke input.
    Without panel lamp.
    - Using only ene-half of filament.
    ${ }^{10}$ Discentinued.

[^5]:    * Indicates VT number has been canceled.

[^6]:    * Indicates VT number has been canceled.

