

electronics today

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INTERNATIONAL
JUNE 1980 60p

DRUM SYNTHESISER PROJECT

Full Spec. Design



HOUSE WIRING
CASSETTE OPTIMISER
MAIN-LINE HI-FI!
LCD CHESS SET REVIEW

FREE INSIDE!
AUDIO DESIGNER'S HANDBOOK
CIRCUIT SECRETS UNFOLDED

... NEWS ... PROJECTS ... MICROPROCESSORS ... AUDIO ...

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

All kits also available as separate packs (e.g. P.C.B., component sets, hardware sets, etc.). Prices in FREE CATALOGUE.

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento, pitch bending, a VCO with shape and pitch modulation, a VCF with both low and high pass outputs and a separate dynamic sweep control, a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch detector, ADSR repeat, sample and hold, and special circuitry with precision components to ensure tuning stability amongst its many features. The kit includes fully finished metalwork, fully assembled solid teak cabinet, filter sweep pedal, professional quality components (all resistors either 2% metal oxide or 1/2% metal trim!) and it really is complete — right down to the last nut and bolt and last piece of wire! There is even a 13A plug in the kit — you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality fibreglass PCB printed with component locations. All the controls mount directly on the main board; all connections to the board are made with connector plugs and construction is so simple it can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready-built units selling for many times the price!

**COMPLETE KIT
ONLY
£168.50 + VAT!**

Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a multi-meter and a pair of ears!

**WE'VE MOVED!
NEW FACTORY UP!
PRICES DOWN!**



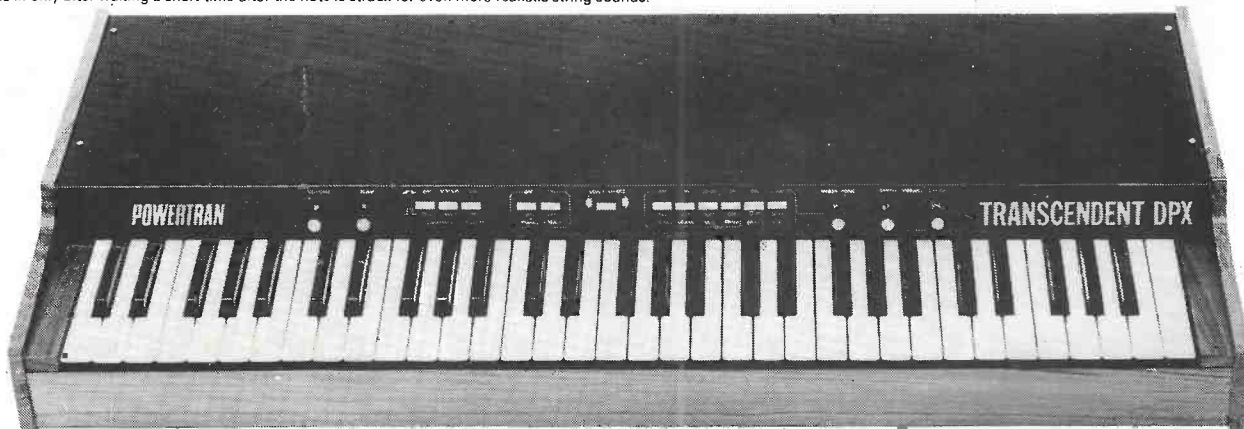
Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

**INCREASED CAPACITY AT OUR BIG NEW FACTORY
MEANS MANY PRICES DOWN! ALL OTHERS FROZEN!**

TRANSCENDENT DPX

**DIGITALLY CONTROLLED, TOUCH SENSITIVE, POLYPHONIC, MULTI-VOICE SYNTHESIZER
ANOTHER SUPERB DESIGN BY SYNTHESIZER EXPERT TIM ORR — PUBLISHED IN ETI**

The Transcendent DPX is a really versatile new 5 octave keyboard instrument. There are two audio outputs which can be used simultaneously. On the first there is a beautiful harpsichord or reed sound — fully polyphonic, i.e. you can play chords with as many notes as you like. On the second output there is a wide range of different voices, still fully polyphonic. It can be a straightforward piano or a honky tonk piano or even a mixture of the two! Alternatively you can play strings over the whole range of the keyboard or brass over the whole range of the keyboard or should you prefer — strings on the top of the keyboard and brass at the lower end (the keyboard is electronically split after the first two octaves) or vice versa or even a combination of strings and brass sounds simultaneously. And on all voices you can switch in circuitry to make the keyboard touch sensitive! The harder you press down a key the louder it sounds — just like an acoustic piano. The digitally controlled multiplexed system makes practical touch sensitivity with the complex dynamics law necessary for a high degree of realism. There is a master volume and tone control, a separate control for the brass sounds and also a vibrato circuit with variable depth control together with a variable delay control so that the vibrato comes in only after waiting a short time after the note is struck for even more realistic string sounds.



Cabinet size 36.3" x 15.0" x 5.0" (rear) 3.3" (front)

COMPLETE KIT ONLY £299.00 + VAT!

To add interest to the sounds and make them more natural there is a chorus/ensemble unit which is a complex phasing system using CCD (charge coupled device) analogue delay lines. The overall effect of this is similar to that of several acoustic instruments playing the same piece of music. The ensemble circuitry can be switched in with either strong or mild effects.

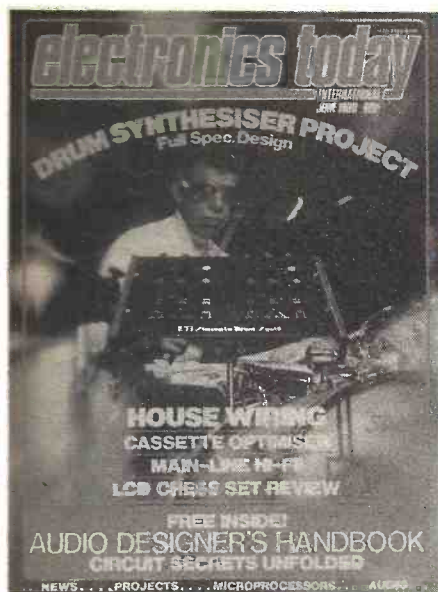
As the system is based on digital circuitry digital data can be easily taken to and from a computer (for storing and playing back accompaniments with or without pitch or key change, computer composing etc., etc.).

Although the DPX is an advanced design using a very large amount of circuitry, much of it very sophisticated, the kit is mechanically extremely simple with excellent access to all the circuit boards which interconnect with multiway connectors, just four of which are removed to separate the keyboard circuitry and the panel circuitry from the main circuitry in the cabinet.

The kit includes fully finished metalwork, solid teak cabinet, professional quality components (all resistors 2% metal oxide), nuts, bolts, etc., even a 13A plug — you need buy absolutely no more parts before plugging in and making great music! When finished you will possess an instrument comparable in performance and quality with ready-built units selling for over £1,200!

POWERTRAN

**ORDERING INFORMATION AND MORE KITS
INCLUDING THE BLACK HOLE ON PAGE 8**



Designer's handbook p.57



Check and mate p.49



Box o'Bangs p.84

electronics today

JUNE 1980 VOL 9 NO 6 INTERNATIONAL

FEATURES

- | | | |
|--------------------|----|----------------------------|
| DIGEST | 8 | The In place for news |
| HOUSE WIRING | 21 | Plugging the eighties |
| AUDIOPHILE | 28 | Cantilever contests |
| DESIGNERS NOTEBOOK | 39 | For stable people only |
| CHESS MACHINES | 49 | All set for LCD? |
| HANDBOOK | 57 | Could be all your own work |
| RAVEN ON | 79 | Hey Prestel! Instant info |
| MICROFILE | 93 | The word from Sinclair |
| TECH TIPS | 97 | The ideas circuit |

PROJECTS

- | | | |
|----------------------|-----|--------------------------------|
| FM LINE DISTRIBUTION | 15 | All music is main-line now |
| LINEAR OHMMETER | 34 | Resist it accurately |
| TAPE OPTIMISER | 44 | Getting the best bias |
| IR60 TRANSMITTER | 73 | Infra-red will send you |
| DRUM SYNTHESIZER | 84 | Easy to beat, never bettered |
| PCB FOIL PATTERNS | 114 | The other side of our projects |

INFORMATION

- | | | |
|------------------|-----|-----------------------------|
| ETI CHIP PENDANT | 13 | Get hung up on our offer |
| HE JULY | 38 | Future hobbling |
| ETI NEXT MONTH | 47 | July is lift-off month |
| MARKETPLACE | 77 | The place for Seiko seekers |
| COMPUTING TODAY | 95 | News of our micro-mag |
| ETI BOOK SERVICE | 101 | The finest fine-print |
| ETIPRINTS | 117 | The only rub-down to have |

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- | | |
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MITRAD

(MIDLAND TRADING COMPANY)

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BRITAIN'S FINEST SELLING RANGE

ZETRON

NEW ZETRON L.C.D. CALCULATOR NEW

Superb value in the economy range of LCD calculators. What more could you ask for? This marvel of the silicon chip era boasts the following:

Four basic functions, chain and mixed operations, constants for four functions, % calculations including discounts and mark-ups. Automatic accumulation in four functions.

★PLUS★

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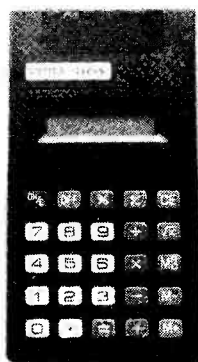
Memory facility

★PLUS★

Auto Power Off

(7 minutes)

ALL THIS FOR A MODEST £4.95



GENTS MELODY ALARM CHRONO DUAL TIME

Brand new Melody Alarm, Chrono. Constant display of hours, mins, secs, weekday, am/pm and mode square flag indication.

The chrono runs to a 1/10th sec (running horse style) split and lap mode facilities are standard. Dual timing facilities. The alarm system is unique in the fact that it plays the tune "Yellow Rose Of Texas" for 20 seconds.

The tune can be actuated at any instance by the press of a button. Backlight, infinitely adjustable stainless steel strap.

VERY PRICED

LOWLY

£17.75



NEW QUARTZ L.C.D. TIMER NEW

A new style timer incorporating split second accuracy. The timer is finished in a strong black plastic case with large L.C.D. readout of hours, mins and secs. A further optional display mode of month, date and weekday is available. The timer incorporates a 1/100th sec chronograph with numerous facilities.

(i) The timer can be frozen.

(ii) Two people can be timed simultaneously.

(iii) Split and lap mode facilities are available. A strong black cord is attached to the timer which aids movement at sporting events.



Battery replacement is made easy with a screw back.

OFFERED AT ONLY £19.95

GENTS FRONT BUTTON CHRONO ALARM

Latest style! Constant display of hours, mins, secs, am/pm, weekday and alarm indication. A further two optional display modes are available. The watch comprises of 7 digits, 12 function and is programmed to the year 2009. The alarm can be set to any time within 24 hours and operates for 30 sec. Back-light and a closely woven adjustable stainless steel strap finish the watch off with a really superb sleek look, only 8mm thick.

£13.25

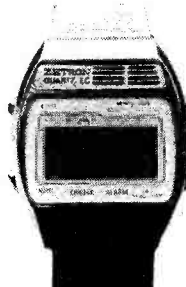


GENTS ALARM CHRONO (12/24 CYCLE)

A really superb watch and module. It can be set as a 12- or 24-hour watch with hours, mins, secs, am/pm and weekday indication always on display. A unique calendar is built into the watch. You can have month followed by date or date followed by month, it's entirely up to you. A 24-hour alarm can be set to any time within a 24-hour period.

The chronograph has a 12-hour capacity and runs at 1/10's. Split and lap mode facilities are available.

Battery hatch, mineral glass, long-life battery and a closely woven adjustable stain-



less steel strap finish the watch off with impeccable looks.

ONLY £16.50

LADIES COCKTAIL

Elegance and style for the lady with the discerning taste. In gold or silver finish with matching bracelet. Constant display of hours and mins with month, date, secs, auto calendar and back-light.

VERY SPECIAL £10.50



LADIES SUGAR COATED

Another superb ladies watch with that extremely popular sugar frosted finish. Links can easily be removed from the strap and the clasp has a spring mechanism built in to give a comfortable fitting. Constant display of hours and mins, with month, date, secs, auto calendar and back-light.

£10.50



GENTS CHRONOGRAPH

Probably the best looking chrono on the market. Constant display of hours, mins, secs with am/pm indication. Also month, date and weekday indication. 1/100th and 1/10th sec with split and lap mode facilities. Back-light, closely woven adjustable stainless steel strap.

SPECIAL £8.95



GENTS MELODY MULTI-CHIME ALARM CHRONO

Latest technology! Constant display of hours, mins and secs, weekday, date and month with mode and chime indication display. The musical alarm once actuated plays the tune "Oh Suzanna". Two further alarm systems are incorporated in this outstanding watch: (i) 24-hour alarm; (ii) count-down alarm. The watch can be set to chime on every full hour. A 1/100th sec chrono is standard to the watch. Can be switched off. Mineral glass face. The watch also has a battery hatch backlight and infinitely adjustable stainless steel strap.

VALUE AT £19.95



ZETRON

WHERE RELIABILITY, STYLE AND ELEGANCE REALLY COUNT

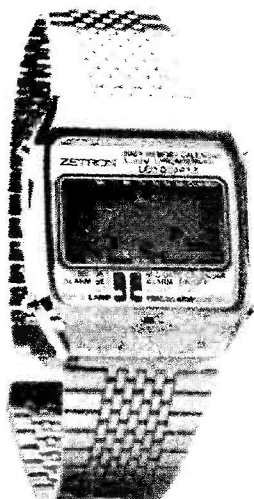
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MITRAD

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THREE OF THE FINEST SELLING WATCHES ON THE BRITISH MARKET

GENTS MEMORY CALENDAR ALARM CHRONO



A really successful watch incorporating all the latest technology.

Hours, mins, secs, weekday and snooze alarm indication on constant display.

A further two optional display modes are available, one being the calendar and month, which can be increased or decreased to give the appropriate month of the year.

A 1/106th second chronograph with split and lap mode facilities are built into the watch with a 12-hour capacity.

A 21-hour alarm with a 10-minute snooze function is also standard to this watch. A further feature is the backlight and fully adjustable stainless steel bracelet.

★
STAR VALUE
£19.95

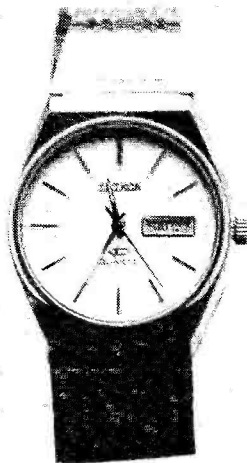
GENTS QUARTZ ANALOGUE

A truly superb timepiece with extreme accuracy. A choice of two colours on this outstanding watch are available, blue or white.

The calendar in the watch can be set to give a readout in either French or English with date indication being automatic.

An infinitely adjustable stainless steel strap is built in as part of the watch.

The watch is fitted with a long-life battery and comes with luminous markings to aid night-time vision.



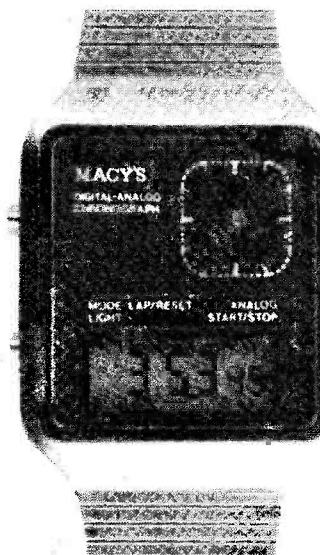
YES ONLY £19.95

GENTS DIGITAL ANALOGUE CHRONOGRAPH

Just look at this outstanding watch:

i) 6 functions (hours, mins, secs, month, date, week-day); ii) chronograph resolution; iii) automatic 4-year guarantee; iv) five buttons control all functions; v) back-light available.

ONLY £29.95 + P/P



The above watch is a new style digital analogue featuring complete up-to-date modern technology. The watch basically constitutes a traditional hand watch plus a modern digital watch, both battery powered.

Hours, mins and seconds are on constant display and with the press of a button, month, date and weekday is displayed.

This unique timepiece also has a chronograph built in which runs to a 1/100th sec, and has a 12-hour capacity. Features include: i) the chronograph can be frozen; ii) two people can be timed simultaneously, and iii) split and lap mode facilities are available.

The watch is finished off with an elegant infinite adjustable stainless steel strap.

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DISAPPOINTMENT !!!**

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WATFORD ELECTRONICS

THE DIGITAL FREQUENCY METER with a Difference



All these features and more, at less than half the price of an ordinary frequency meter. The DFM2000 has all its components including the displays, switches and transformer mounted on one double sided PC board. Assembly is simplicity itself especially since interwiring has been eliminated. This is a high quality design and will make a truly professional digital frequency meter that any constructor will be proud to own.

Price: Only £64.50 Kit (P&P 65p). Probes: Optional extra £8.75

Ready built and tested: £75.50 (65p p&p)

WATFORD'S BOOKSHOP CORNER (No VAT on Books) Switch Chip & You 250p Future With Microelectronics 400p Illustrating BASIC 250p Programming in for Business 690p Full ASCII Coded 56 Key KEYBOARD Type 756 Only £39.95 + and. data	BASIC Computer Games 500p Some Common BASIC Programs 750p 32 BASIC Programs for PET 950p Z80 Assembl. Lang. Programming 750p Z80 Microcomputer Handbook 690p 6502 Assembl. Lang. Programming 750p C202 Programming the 6502 750p Practical Intro. to PASCAL 400p TTL Cook-Book 700p CMOS Cookbook 750p (p&p please add 40p)	SWITCHES TOGGLE: 2A, 250V. 14p SPST 28p DPST 34p DPDT 38p 4 pole on/off 54p SUB-MIN TOGGLE SP changeover 69p SPST on/off 54p SPST biased 80p DPDT 6 lags 75p DPDT centre off 79p DPDT biased 115p ROTARY: Make your own multiway Switch. Adjustable Stop Shifting Assembly. Accommodate up to 6 Wafers 90p Mains Switch DPST to fit 40p Break Before Make Wafers. 1 pole/12 way. 2p/6 way. 3p/4 way. 4p/3 way. 6p/2 way. 56p Spacer and Screen 6p ROTARY (Adjustable Stop) 1 pole/2 to 12 way. 2p/2 to 6 way. 3 pole/2 to 4 way. 4 pole/2 to 3 way 43p ROTARY: Mains 250V AC. 4 Amp 52p	SLIDE 250V: 1A DPDT 14p 1A DPDT c/over 15p 1/2A DPDT 13p 4 pole 2-way 24p PUSH BUTTON DPDT Black Body 125p Red, Blue, Grn., Yell. 125p SRL Latching 125p SRM Momentary 125p MINI. Non Locking Push to Make 15p Push Break 25p Push to c/over 85p
ASTEC RF Modulators 250 Special Widebandwidth for Computers 470 Sound Modulator 250	DIL SWITCHES 4-way SPST 110 6-way SPST 120 8-way SPST 145 RELAYS RL6 SPCO 175 RL6B DPCO 215		

CRYSTALS 100KHz 323 455KHz 385 1MHz 323 1.008MHz 392 1.2MHz 392 1.6MHz 323 1.8MHz 323 1.968MHz 323 2.4576MHz 323 3.2768MHz 323 3.57954MHz 195 4.000MHz 290 4.032MHz 323 4.433619MHz 135 5.0MHz 395 5.185MHz 323 5.24288MHz 425 6.0MHz 323 6.5536MHz 200 7.680MHz 323 8.0MHz 392 8.86723MHz 323 9.375MHz 323 10.0MHz 323 10.74MHz 323 12MHz 392 14.3181MHz 300 18MHz 323 18.432MHz 323 20.0MHz 323 27.648MHz 323 38.6667MHz 350 48.0MHz 323 100.00MHz 323	TRANSFORMERS (Mains Prim. 220-240V) 6.0-6V. 9.0-9V. 12.0-12V 100mA 95p 3VA. 0.6V 0.6V (PCB mounting) 150p 8VA. 6V. 5A 6V. 5A. 9V. 4A 9V. 4A. 12V. 3A 21p 12V. 5A. 15V. 25A 15V. 25A 32p 12V. 4.5V. 1.3A 4.5V. 1.3A. 6V. 1.2A 6V. 1.2A 21p 12V. 5A 12V. 5A. 15V. 4A 15V. 4A. 20V. 3A 23p (20p p&p) 20V. 6A 23p (20p p&p) 24VA. 6V. 1.5A 6C. 1.5A. 9V. 1.3A 9V. 1.3A. 12V. 1A 12V. 1A. 15V. 8A 15V. 8A. 20V. 6A 32p (45p p&p) 20V. 6A 32p (45p p&p) 50VA. 6V. 4A 6V. 4A. 9V. 2.5A 9V. 2.5A. 12V. 2A 12V. 2A. 15V. 1.5A 15V. 1.5A. 20V. 1.2A 20V. 1.2A. 25V. 1A 25V. 1A. 30V. 8A 30V. 8A 365p (50p p&p) 100VA. 12V. 4A 12V. 4A. 15V. 3A 15V. 3A. 20V. 2.5A 20V. 2.5A. 30V. 1.5A 30V. 1.5A. 40V. 1.25A 40V. 1.25A. 50V. 1A 50V. 1A 695p (60p p&p). (N.B. p&p charge to be added above our normal postal charge.)	ALUM. BOXES WITH LID 3x2x1" 55 2 1/2x5 1/2x1 1/2" 75 4x4x1 1/2" 75 4x2 1/2x1 1/2" 75 4x5 1/2x1 1/2" 90 4x2 1/2x2" 80 5x4x2" 107 6x4x2" 110 7x5x2" 145 8x6x3" 185 10x7x3" 240 10x4x3x3" 228 12x5x3" 230 12x8x3" 275	PANEL METERS FSD 60x46x 35mm 0-500uA 0-100uA 0-500uA 0-1mA 0-5mA 0-10mA 0-50mA 0-100mA 0-500mA 0-1A 0-5A 0-25V 0-50V AC 0-300V AC 5" 445p each 4 1/2x3 1/2x1 1/2" 17 0-50uA 18 0-100uA 14 0-500uA 595p each
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VOLTAGE REGULATORS 1A TO3 +ve -ve 7905 220p 7912 220p 5V 7805 175p 7912 220p 12V 7812 175p 7912 220p 15V 7815 175p 7915 220p 18V 7818 175p 7918 220p 1A TO220 Plastic Casing 7905 65p 7912 65p 7915 65p 7918 65p 5V 7805 60p 7905 65p 7912 65p 7915 65p 7918 65p 12V 7812 60p 7912 65p 7915 65p 7918 65p 15V 7815 60p 7915 65p 7918 65p 24V 7824 60p 7918 65p 100mA TO92 Plastic Casing 7905 65p 7912 65p 7915 65p 7918 65p 5V 7805 30p 7905 65p 7912 65p 7915 65p 7918 65p 8V 78L82 30p 79L12 65p 79L15 65p 12V 78L12 30p 79L12 65p 79L15 65p 15V 78L15 30p 79L15 65p	OPTO LEDs with Clips 13 TIL209 Red 13 TIL211 Grn. 17 TIL212 Yel. 18 TIL220 2" Red 14 266 Green, Yellow or Amber 18 Square LEDs, Red, Green, Yellow 36 LD271 Infra Red 40 SFH205 Detector 58 TIL32 Infra Red 58 TIL78 Detector 70 BARGRAPH. Red 10 segments 225 LS400 255 OCP71 120 ORP12 63 ORP61 85 2N5777 45 ISOLATORS IL74 48 TIL111/2 85 TIL114 95 TIL117 110 Bargraph 225 7 Segment Displays TIL307 675 TIL312 3" CA 105 TIL313 3" CC 105 TIL321 5" CA 115 TIL322 5" CC 115 DL704 3" CC 99 DL707 3" CC 99 DL747 6" CA 180 FND357 Red 120 8" Orange CA 250 12x57 Red 150 3" Green CA 150 6" Green CA 215 3" Red CA 150 3" Green CA 150 LCD 3 1/2 Digit 875 LCD 4 Digit 975
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ETI Projects: Parts available for: Click Eliminator, DM500, 60W Amplifier, System. Send SAE plus 5p for list. LS202 345 LS221 120 LS240 225 LS241 225 LS242 232 LS243 232 LS244 225 LS245 270 LS247 135 LS248 135 LS249 135 LS251 130 LS253 130 LS255 115 LS258 120 LS259 180 LS261 450 LS266 75 LS273 180 LS275 320 LS279 88 LS280 250 LS283 190 LS290 130 LS293 130 LS295 215 LS298 215 LS299 420 LS300 175 LS302 175 LS320 270 LS323 450 LS324 200 LS325 320 LS326 320 LS327 315 LS346 185 LS347 150 LS348 190	LS352 185 LS353 185 LS355 65 LS366 65 LS367 65 LS368 65 LS373 180 LS374 180 LS375 150 LS377 199 LS378 185 LS379 215 LS384 50 LS385 420 LS386 85 LS390 140 LS393 140 LS395 210 LS396 199 LS398 275 LS399 230 LS445 140 LS446 190 LS490 150 LS668 105 LS669 105 LS670 270 LS673 750 LS674 850 CMOS 4000 18 4001 18 4002 24 4006 92 4007 22 4008 82 4009 40 4010 48	4011 24 4012 24 4013 45 4014 85 4015 85 4016 42 4017 82 4018 88 4019 48 4020 99 4021 95 4022 95 4023 25 4024 75 4025 25 4026 180 4027 48 4028 82 4029 105 4030 60 4031 225 4032 125 4033 175 4034 210 4035 125 4036 365 4037 115 4038 118 4039 360 4040 105 4041 80 4042 80 4043 95 4044 105 4045 175 4046 130 4047 98 4048 65 4049 45	4050 48 4051 80 4052 80 4053 80 4054 130 4055 135 4056 135 4057 1900 4058 575 4060 130 4061 1225 4062 995 4063 120 4064 58 4065 430 4066 26 4067 48 4068 30 4069 25 4070 25 4071 25 4072 25 4073 25 4075 25 4076 99 4077 48 4078 30 4079 88 4080 28 4081 48 4082 28 4083 90 4084 90 4085 90 4086 325 4087 99 4088 150 4089 150 4090 150 4091 150 4092 150 4093 150 4094 150 4095 150 4096 150 4097 150 4098 150 4099 150 4100 150 4101 150 4102 150 4103 150 4104 150 4105 150 4106 150 4107 150 4108 150 4109 150 4110 150
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£2 OFF!

SUPERB NEW KITS!

C300/ES200

high performance electronic ignition, to add power, economy, reliability, sustained smooth peak performance, instant all weather starting, to your car.

Surefire has sold in its thousands in ready made form from big name accessory firms, but it is now available in quality kit form to fit all vehicles with coil ignition up to 8 cylinders.

ES200. A high performance inductive discharge ignition incorporating a power integrated circuit (special selection): electronic variable dwell circuit (maximises spark energy at all speeds): pulse processor (overcomes contact breaker problems). Coil governor (protects coil). Long burn output. Negative earth only. Compatible with all rev. counters.

C300. In it's ready built form (C3000) it came top of all systems tested by an independent national authority July '79. A high energy capacitive discharge ignition incorporating a high output short circuit proof inverter, top grade Swedish output capacitor, pulse processor circuit, transient overload protection. Fast rise bidirectional output ideal for fuel injection, sports carburation, oily engines. Compatible with most rev. counters. (Low cost adaptors available for rare cases. Application list enclosed with each kit. Note: Vehicles with Smiths Jaeger rev. counters code RVI on dial will require adaptor type TCI).

What's in the kits. Surefire's own precision anodised aluminium extruded case. P.C. mounted security changeover switch, static timing light. Special selection Motorola semi-conductors. Capacitors, resistors etc. selected after 5 years experience. Glass fibre pcb, solder, complete down to last washer. Fully illustrated comprehensive instructions and full technical back up service.

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VAT and P & P inc

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C300: Pos	£17.95	£15.95	
C300: Neg	£17.95	£15.95	
Tacho Adapt. TCI		£3.90	

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DIGEST

Vending Over Backwards

A source of constant frustration to many people is vending machines. Invariably they have run out of what you want, or give you chicken soup flavoured coffee, or refuse to refund your money. The average vending machine certainly bears signs of the dislike its customers have for it, mostly in the form of dents, framed by boot marks. The wonderfully inscrutable Japanese have, of course, developed a cure in the form of the machine pictured here — not particularly beautiful to look at, but with a heart of gold. When the customer approaches it, a sensor picks up the infra-red rays emitted by

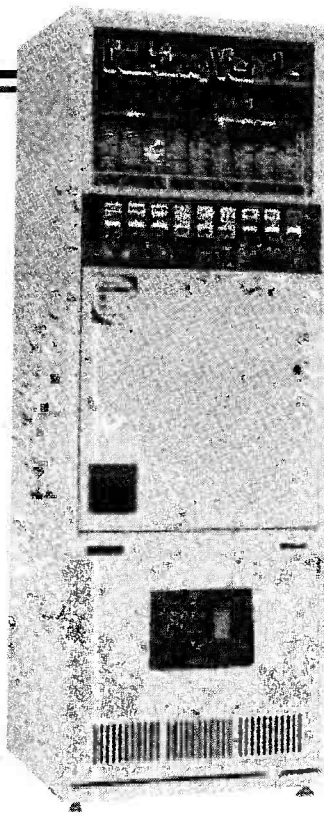
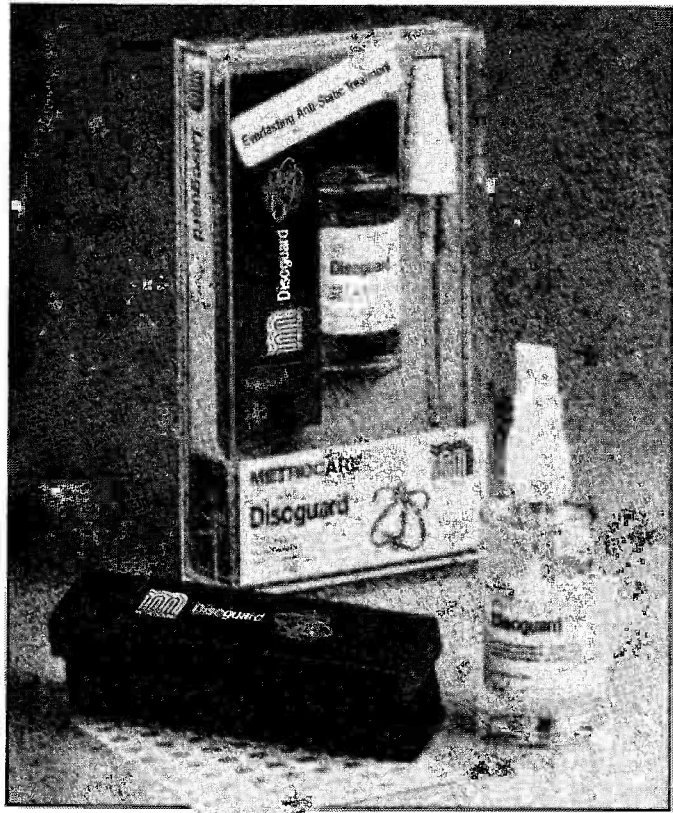
him, and a 'soft female voice' says "Welcome" and lists the merchandise in the machine. It also tells the customer when there is no change available, when items are out of stock and reminds him if he has not fed enough money into it for the item he requires. Finally the machine says a cheerful "Thank you" and reminds the buyer to pick up his change. This machine, although a novelty at the moment, has quite interesting possibilities, but there are no marketing plans for it as yet. Wouldn't it be nice to walk away from a vending machine, clutching exactly what you asked for and with the echoes of that warm welcome ringing in your ears? The system was developed by Mitshushita Reiki, a Mitshushita Electric subsidiary, which specialises in refrigeration equipment.

Ex-Static

'Diseguard' from Metrosound is an everlasting anti-static treatment for records. In the kit you find a spray pump, a bottle of 'special' fluid and a record cleaner for buffing.

The makers claim that there is no detectable change in sound quality except as we found that the treble sounds cleaner, as it

should. We extensively tested it of course, sneakily spraying some of the Editor's prized record collection, and then waiting for a response! In fact there were no adverse reactions, so we think this kit could prove quite useful to audiophile freaks. For £4.50 there is sufficient fluid in the kit to treat both sides of 40 LP records. For further information contact Metrosound, 4/10 North Road, London N7 9HN.



Solid Security

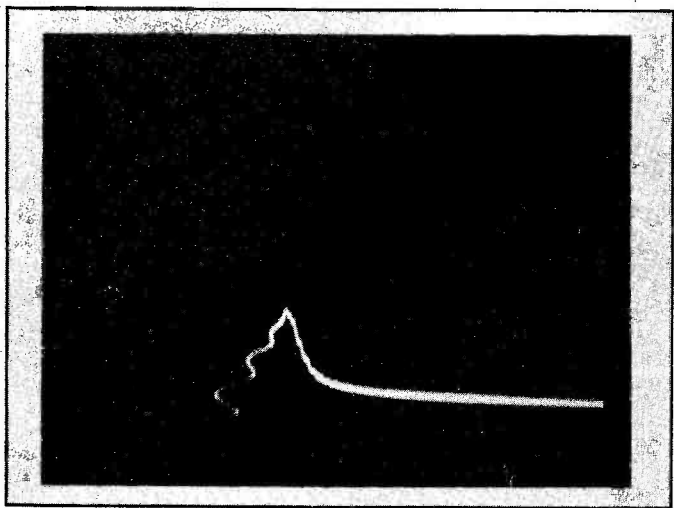
This is Clarke's Instruments Ltd motor driven door lock type 838. It is a remotely operated door lock, which is last to be released on strong doors that give public access to high security areas. After the dead locks have been unlocked by key, the door is held by the motor lock, whose double shear action gives 4 to 6 tonnes of shear strength. When relocking the door, the motor lock is first to be operated. The new microswitching system ensures greater reliability of operation and permits positive indication of full lock closure. Automatic locking of the door each time it closes can also be arranged. It is mains operated and needs no other power supply, great if you don't live in a high risk area for power cuts, although there is an integral manual emergency release on the inside of the door — unless of course, you're trying to get in! Further information is from Clarke Instruments Ltd, 91a High Street, Camberley, Surrey GU15 3RN.



Doctor Who

One of our readers, Mr. S. Knowles of Hampshire, sent us a scope picture he took whilst

designing with a Textronix 7403 on 500 nS/div with x10 expand. It seems he was looking for a pulse, but he may well have discovered the secret of time travel!



CHROMATHEQUE 5000



Panel size 19.0" x 3.5". Depth 7.3"

This versatile system featured as a constructional article in *ELECTRONICS TODAY INTERNATIONAL* has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least. You can run the unit as a straightforward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuitry which produces some superb random and sequencing effects. Each channel handles up to 500W and as the kit is a single board design wiring is minimal and construction very straightforward.

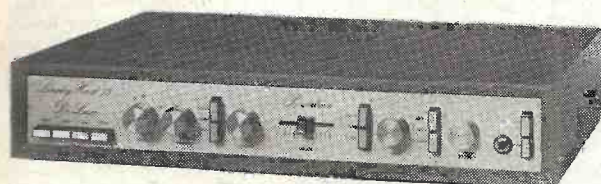
Kit includes fully finished metalwork, fibreglass PCB controls, wire, etc. — Complete right down to the last nut and bolt!

POWERTRAN 5 CHANNEL LIGHTING EFFECTS SYSTEM

COMPLETE KIT

ONLY

£49.50 + VAT!

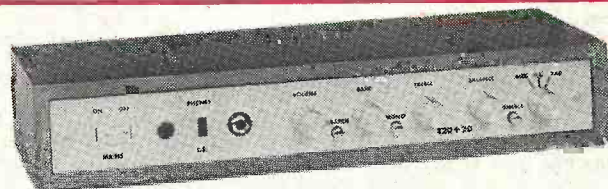


DE LUXE EASY TO BUILD LINSLEY HOOD 75W STEREO AMPLIFIER £99.30 + VAT

This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in *Hi-Fi News* and *Record Review* and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%.

Above 2 kits are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet, cable, nuts, bolts, etc and full instructions — in fact everything! Matching TUNERS and CASSETTE DECK — see our free catalogue!

All kits also available as separate packs (eg PCB, component sets, hardware sets etc). Prices in our FREE CATALOGUE.



T20+20 20W STEREO AMPLIFIER £33.10 + VAT

This kit, based upon a design published in *Practical Wireless*, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30-watt version of this kit (T30+30) is also available for **£38.40 + VAT**.

BLACK HOLE

LAST MONTH'S FRONT COVER FEATURE!

The BLACK HOLE designed by Tim Orr, is a powerful new musical effects device for processing both natural and electronic instruments, offering genuine VIBRATO (pitch modulation) and a CHORUS mode which gives a 'spacey' feel to the sound achieved by delaying the input signal and mixing it back with the original. Notches (HOLES), introduced in the frequency response, move up and down as the time delay is modulated by the chorus sweep generator. An optional double chorus mode allows exciting antiphase effects to be added. The device is floor standing with foot switch controls, LED effect selection indicators, has variable sensitivity input, has high signal/noise ratio obtained by an audio compander and is mains powered — no batteries to change! Like all our kits everything is provided including a highly superior, rugged steel, beautifully finished enclosure.

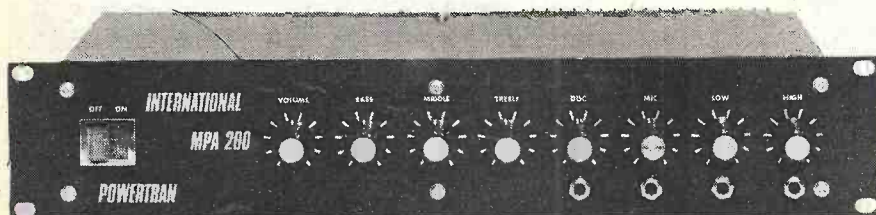
COMPLETE KIT ONLY £49.80 + VAT (single delay line system)

De Luxe version (dual delay line system) also available for £59.80 + VAT

MPA 200 100 WATT (rms into 8Ω) MIXER/AMPLIFIER

Featured as a constructional article in *ETI*, the MPA 200 is an exceptionally low priced — but professionally finished — general purpose high power amplifier. It features adaptable input mixer which accepts a wider range of sources such as microphone, guitar, etc. There are wide range tone controls and a master volume control. Mechanically the MPA 200 is simplicity itself with minimal wiring needed making construction very straightforward.

The kit includes fully finished metalwork, fibreglass PCBs, controls, wire, etc. — complete down to the last nut and bolt.



Panel size 19.0" x 3.5". Depth 7.3"

COMPLETE KIT
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Our pendant contains a (working — but what a shame to ruin it by wiring!) chip with quartz window, beautifully clasped in either silver or gold, depending just HOW generous you're feeling.

The price is pretty tasteful too and as the holder is emblazoned with the ETI logo, there is no better way of advertising the extent of your appreciation of the finer things in life.

In silver : **£30** all inc.

gold : **£69** all inc.



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Please send me silver/gold pendants. I enclose cheque/PO payable to Modmags for

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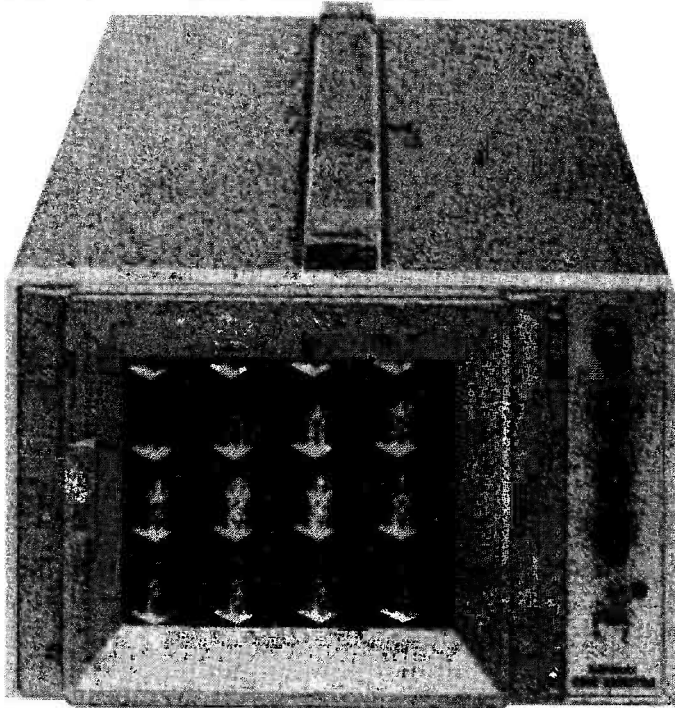
Allow 21 days for delivery.

Invasion Monitor?

Here is the model 606B display monitor from Tektrónix. It is a high resolution display for anyone needing critical sharpness for displays or display photographs. This monitor gives a spot size of only 0.079cm, and the manufacturers are aiming this at areas

such as medical multi-imaging and electron microscopy. For further information contact Tektronix UK Ltd, Beaverton House, PO Box 69, Harpenden, Hertfordshire.

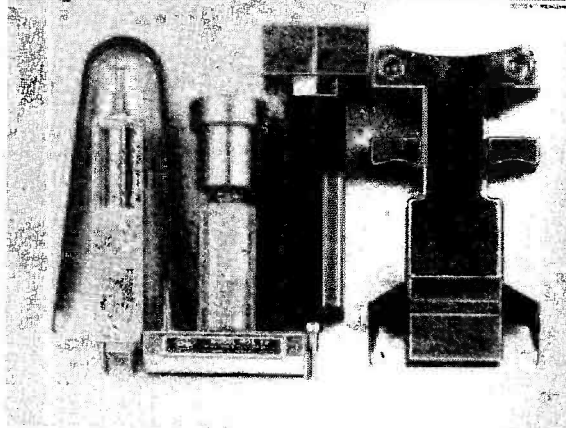
But what we'd like to know is what is being displayed on the screen! A free subscription to whoever out there can tell us what it is!



Instant Surgery

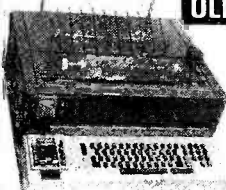
This may look like the surgical equipment of a mad doctor, but we are assured that this isn't its only function. Alternatively it can be used for DIP IC insertion and extraction. The kit has extractors for 14-16 pin

devices, 24-40 pin chips plus inserters for 14-16, 24-28 and 36-40 pin ICs. All the surfaces that could engage conductive surfaces are CMOS safe. It is available from OK Machine & Tool (UK) Ltd, Dutton Lane, Eastleigh, Hants SO5 4AA, and costs £22.35, a small price to pay for budding Dr. Frankensteins.





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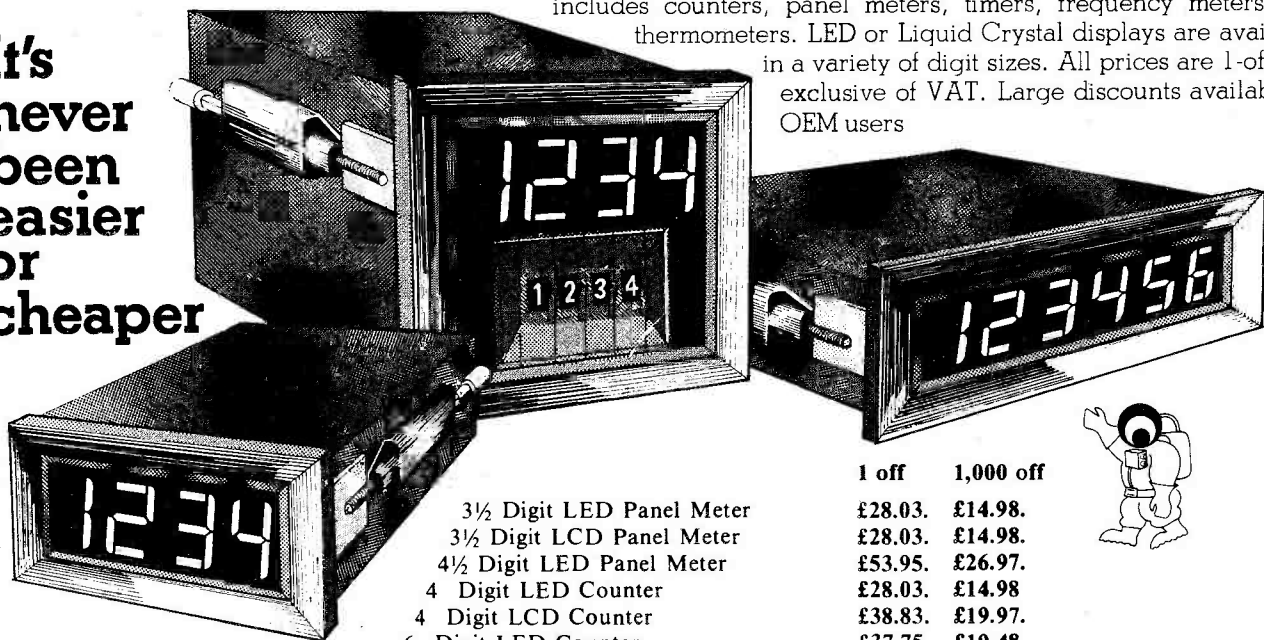
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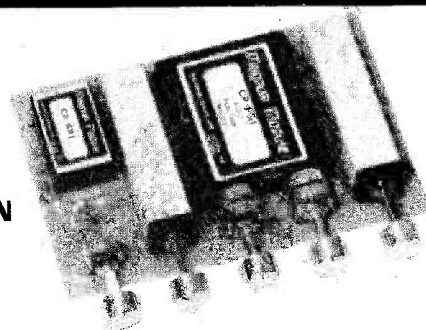
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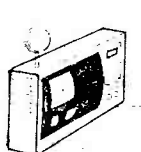


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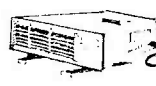
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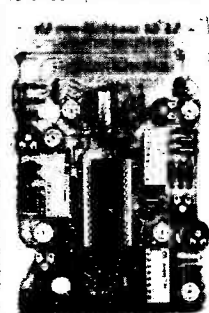
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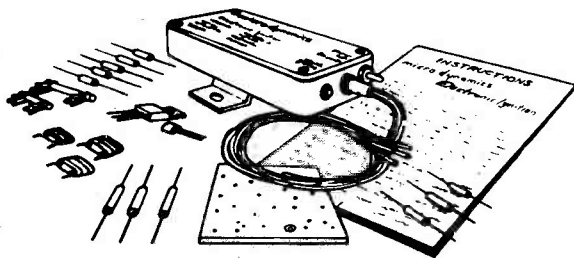
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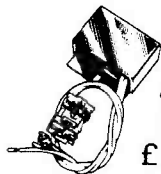


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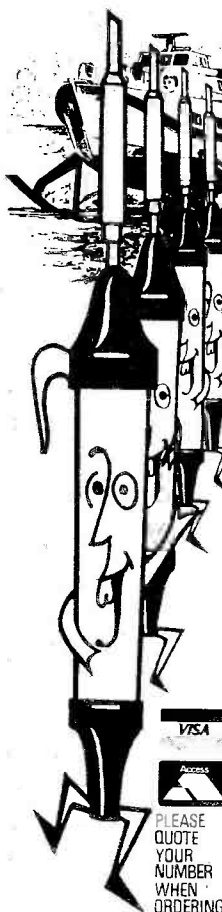
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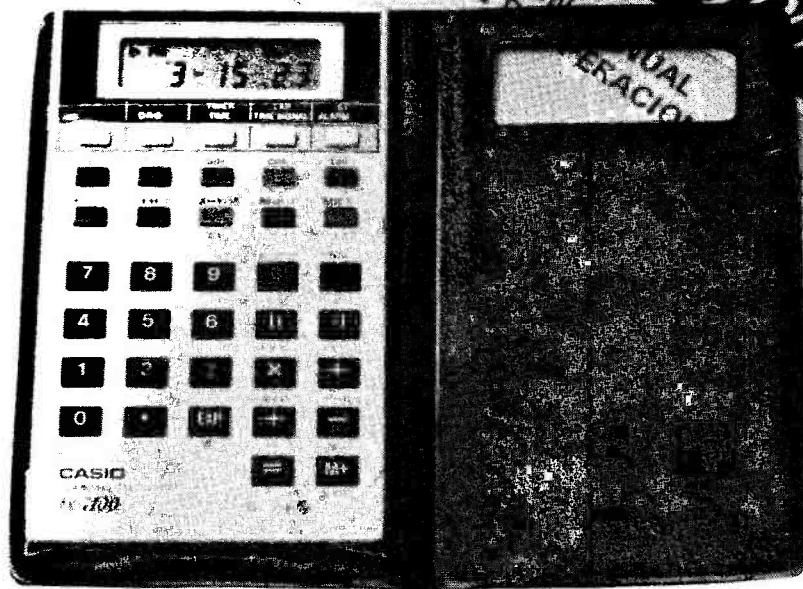
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Count On It



It was on a Monday morning that a small package arrived at ETI. It was greeted with the usual Monday morning enthusiasm — we ignored it—until suddenly... it went off. The entire ETI staff dived for cover (we needed an excuse for a lie down anyway),

but as ever, our intrepid telephonist saved the day by ripping open the package, and there, to our surprise... Yes, it was yet another member of the ever growing family of Casio, which has produced a new infant in the form of the fx-7100. A veritable baby, it measures 5mmH x 55mmW x 91.5mmD and weighs only 44gms. It incorporates a scientific calculator with 39 built-in functions, a continual display alarm clock accurate to 3 seconds a day under normal temperatures, a count-down alarm (repeater timer), a 1/100 sec stopwatch and an hourly on the hour time signal — a useful extra for clock-watchers (this had been the cause of the trouble that morning, and still causes the more somnambulant staff members to say 'wot dat?' every hour of the day).

The power consumption is 8mW, which gives a life of approximately 1 year for the two silver oxide batteries it uses. The package includes the usual data cards and a 70-page operation manual (cough). This little gem normally costs £27.95, or £24.95 from Tempus.

Metal Locator (March)

Well, the world famous ETI mistake maker has struck again, this time his mistakes were located (!) in the Metal Locator project from our March edition. These were many and varied so here goes: In figure 1 the circuit diagram, starting from the left, the unmarked resistor is R4 18k, at top centre V/2 is not +18V and underneath that R19 100k does not go to +18V but to Vs. IC4d should be labelled IC4a

and at bottom centre the common line to C2 470n, L1 and R2 15k should be connected to 0V. C18 10n and C20 470u should be transposed, and transistor Q9 is BC158. In figure 3, the component overlay, the tag which says White/WH should be White/BLK and the unmarked IC should be IC4, Q8 and Q9 should be transposed and the missing resistor value is R45. Track C17 should go to pin 13 and not to 12. Figure 4 connection for front panel, lead marked Blue/BLK should be Blue/WH.

Radio Control Protector (April)

We made an incorrect statement last issue with regard to the PPIM-4CH from Chromatronics. We said that their device

would not operate if one of the decoder outputs locked high. Well it does and we were wrong. Sorry Chromatronics.

B&B 1537 VCA Article

Here they are again. Errors. Hearing their ugly heads amongst the otherwise unsullied pages of ETI. But wouldn't you miss them if they weren't there?

The first error was on the schematic on figure 5. R6 and R9 should be shown as joined at pin 3 of the 1537A and R8 and R10 should be similarly joined at pin 6.

In figure 6, the trace connecting pins 1 and 2 of IC1 is slightly

obscured by the IC outline, so take note all of you out there who are making their own PC board!

Also the titles for figures 14 and 15 are exchanged and a non-inverting VCA configured as per figure 15 would have a minimum gain of unity, whereas the inverting VCA of figure 14 could attenuate to the common mode limits of the op amp used. OK?

DISPLAY ELECTRONICS ADVERTISEMENT — MAY ISSUE

Due to a printing error a photograph of the Super 77 Key Keyboard wrongly appeared under the 10W price chassis heading. We apologise for any inconvenience caused to our customers.

Sounds Interesting

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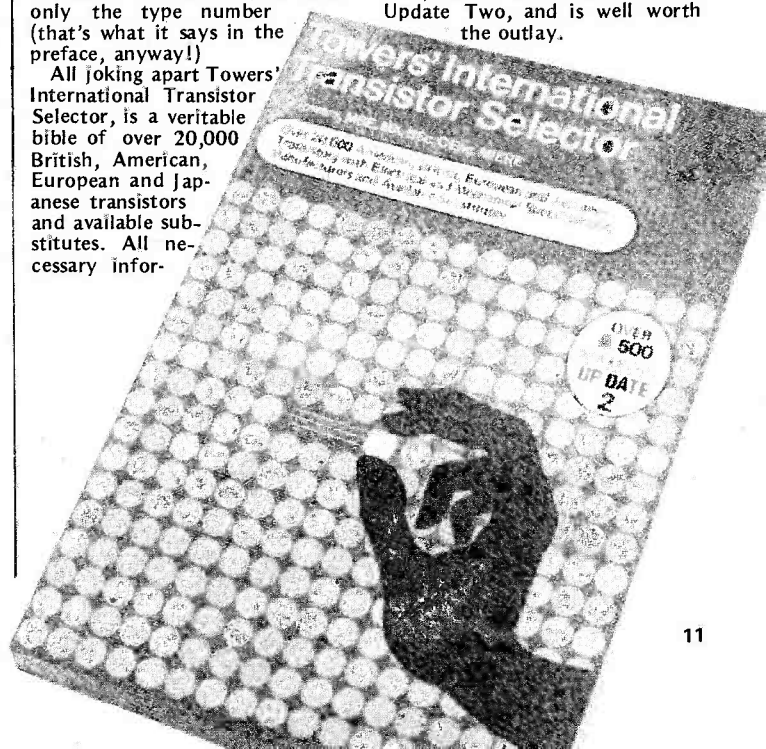
greater period of time. Aura Sounds assure us that the finished product is of superb quality, both sound and visual. Each kit comes complete with assembly manuals and they even supply the solder! The parts are in numbered containers so that the contents can be easily checked against the parts list. If you're interested contact: Aura Sounds, 14-15 Royal Oak Centre, Brighton Road, Purley, Surrey.

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If you deal with transistors — whether as a student, a hobbyist, a circuit engineer, a buyer, a teacher or a serviceman — you often want data on a specific transistor of which you know only the type number (that's what it says in the preface, anyway!)

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mation is shown in a neat tabular form including package outline, lead info., European and American equivalents etc, etc, etc. Published by W.Foulsham and Co. Ltd., this is the Revised Edition Update Two, and is well worth the outlay.



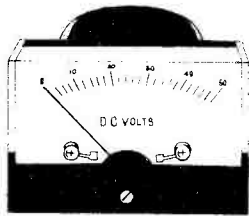


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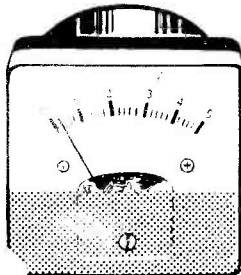
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ME10A	T31	0-2 AMP	
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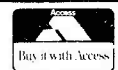
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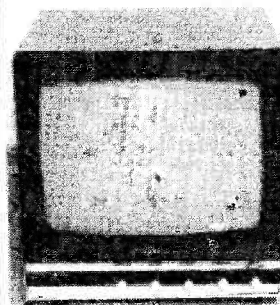
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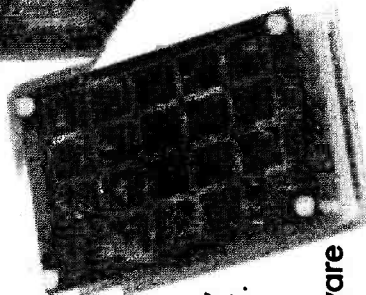
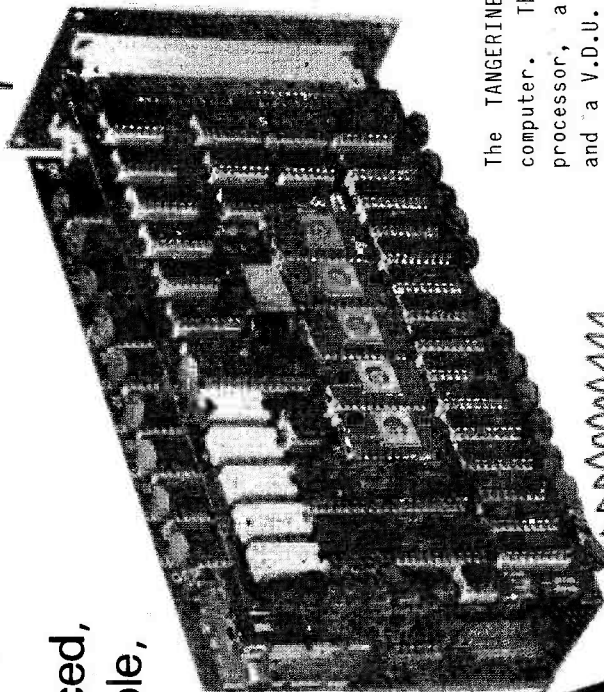
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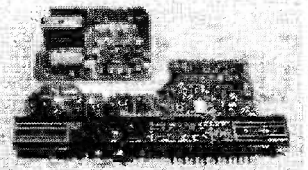
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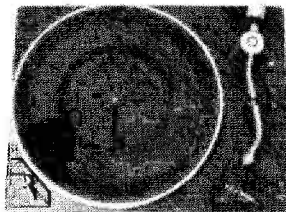
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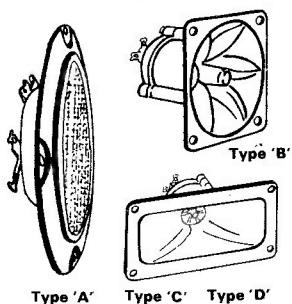
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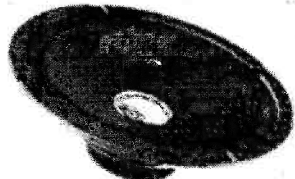
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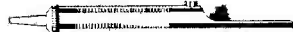
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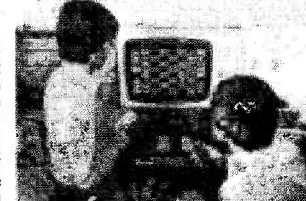
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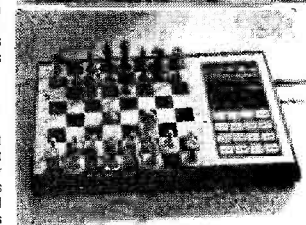
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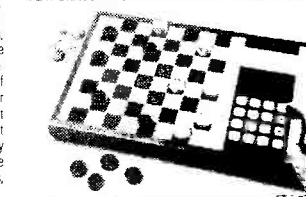
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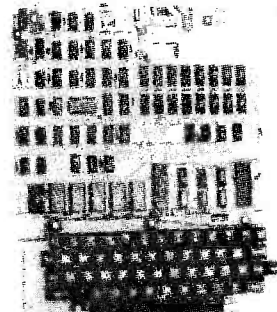
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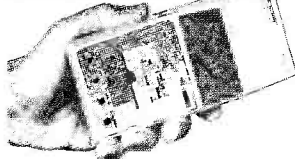
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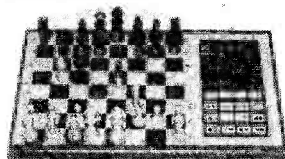


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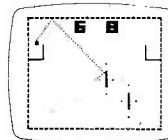
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PRINTED CIRCUIT MATERIALS

PC etching kits: — economy £2.42, standard £4.76, 40 sq ins pcb 45p, 1 lb FeCl £1.50, Etch resist pens: — economy 50p, dial 84p, Drill bits 1/32" or 1mm 34p, Etching dish 92p, Laminate cutter £1.20.

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AL30A £4.08, PA12 £8.38, PS12 £1.58, TS38 £2.70, S450 £25.06, AL60 £5.06, PA100 £17.33, SPMB0 £4.74, BMTB0 £6.06, Stereo 30 £21.57, AL80 £7.71.

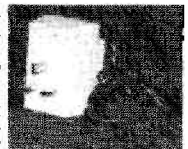


COMPONENTS

IN4148 0.09p, 1N4002 2.9p, 723 14 kit 33p, NE555 8 dil 24p, 741 8 dil 16p, bc547, bc549 4.9p, bc182, bc184, bc212, bc214, bc548 5.5p, tip31c, tip32c 36p, tip41c 40p, bd132 27p, plastic equiv bcv72 4.5p, fuses 20mm x 5mm cartridge .15, .25, .5, 1, 2, 3, 5Amp quickblow 1p, resistors 5% 1/4W £12 10R to 10M 1p, 0.8p for 50+ of one value, polyester capacitors 160V .015, .088mf 2.6p, 1mf 4.0p, .01mf 3.0p, .022, .033mf 3.3p, .047mf 3.5p, .15, .22, .33, .47mf 4.9p, polystyrene capacitors £12 63V 10 to 1000pf 3p, 1n2 to 10n 4p, ceramic capacitors 50V £5 22pf to 47n 2p, electrolytic capacitors 50V .5, 1, 2mf 5p, 25V .5, 10mf 5p, 16V 22, 33mf 5p, 47, 68mf 3.5p, 100mf 6p, 330, 470mf 9p, 1000mf 11p, zeners 400mw £24 2V7 to 33V 7p, preset pots subminiature 0.1W horiz or vert 100 to 4M7 7p, potentiometers 1/4W 4K7 to 2M2 log or 1m single 27p, dual 71p, 1/4" red LEDs 9.7p, ic sockets 8 dil 8.7p, 14 dil 10.1p, 16 kit 12p.

BATTERY ELIMINATORS

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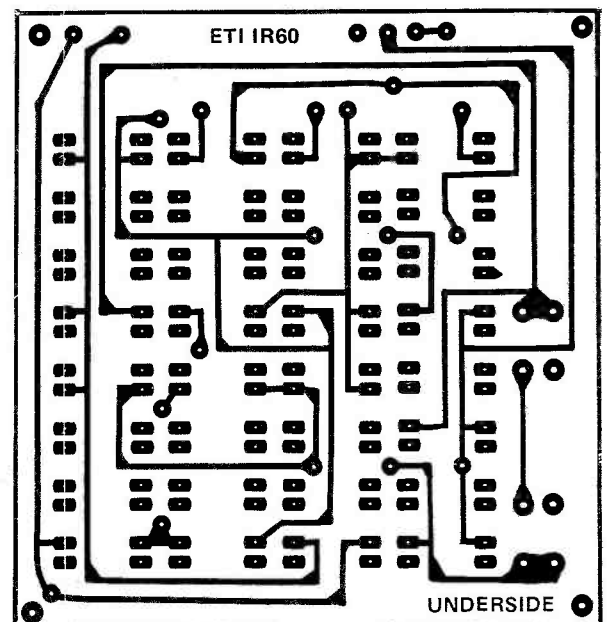
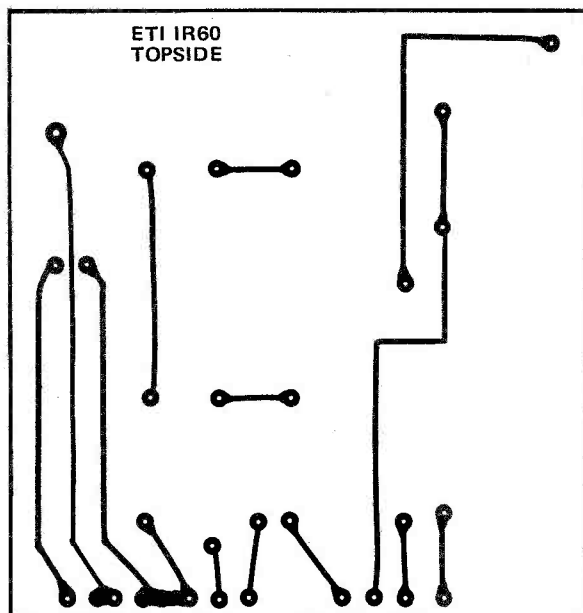
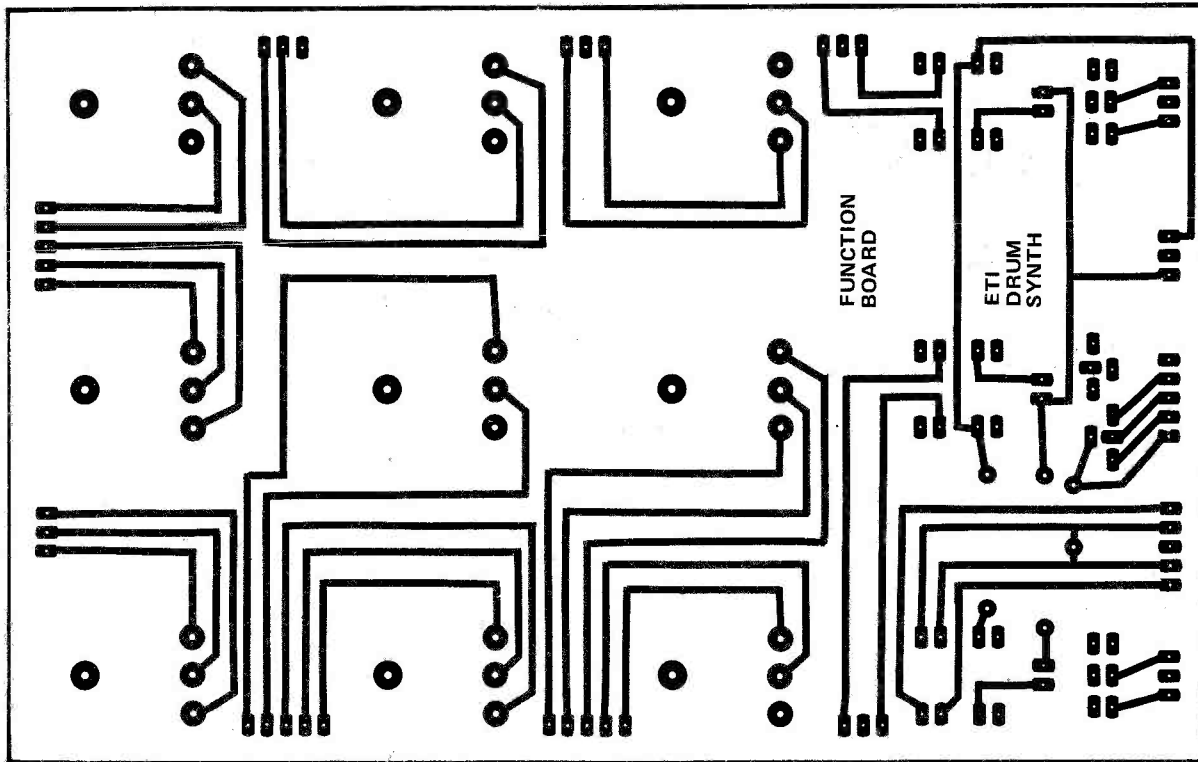
BATTERY ELIMINATOR KITS

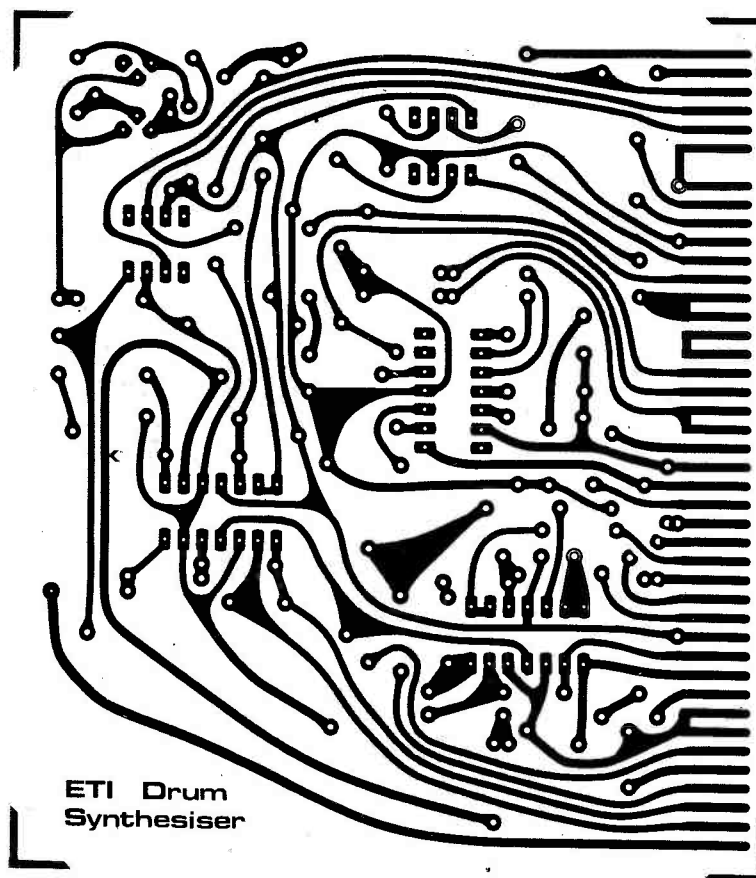
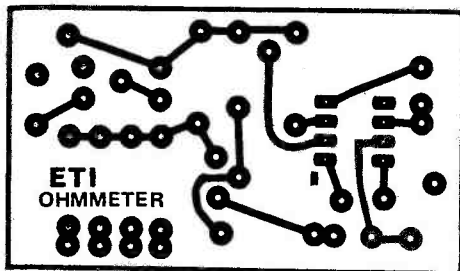
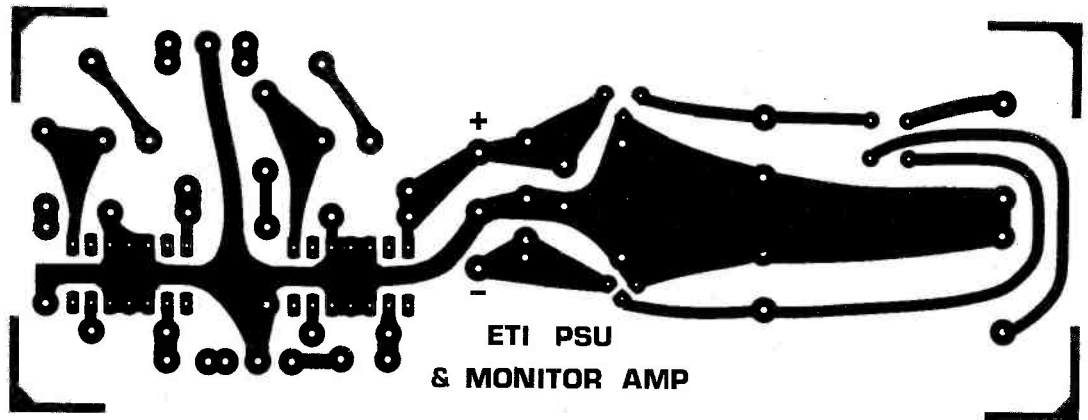
100ma radio types with press-stud connectors 4 1/2V £1.49, 6V £1.49, 9V £1.49, 4 1/2-4V £1.92, 6-8V £1.92, 9-8V £1.92, cassette type 7 1/2V 100ma with din plug £1.49, heavy duty 13-way types 4 1/2V/7 1/2V/11/13/14/17/21/25/28/34/42V 1A £5.52, 2A £8.80, car converter input 12V dc, output 6/7 1/2V/9V 1A stabilized £1.35.

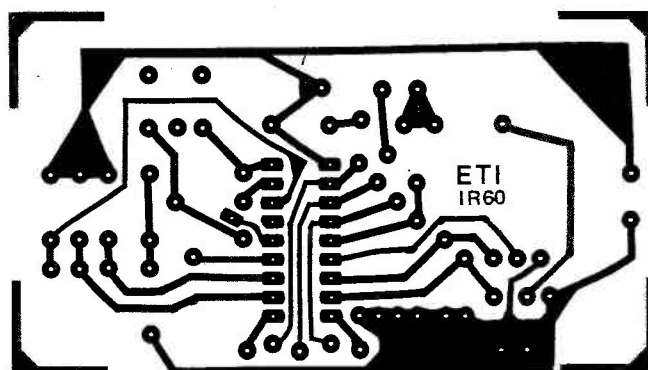
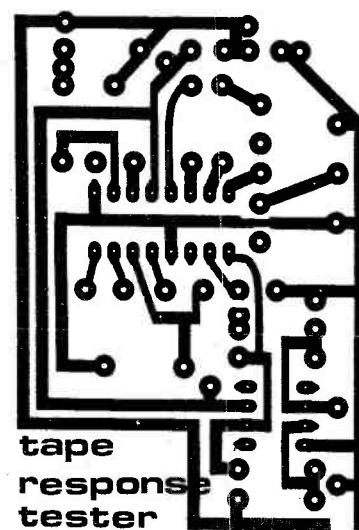
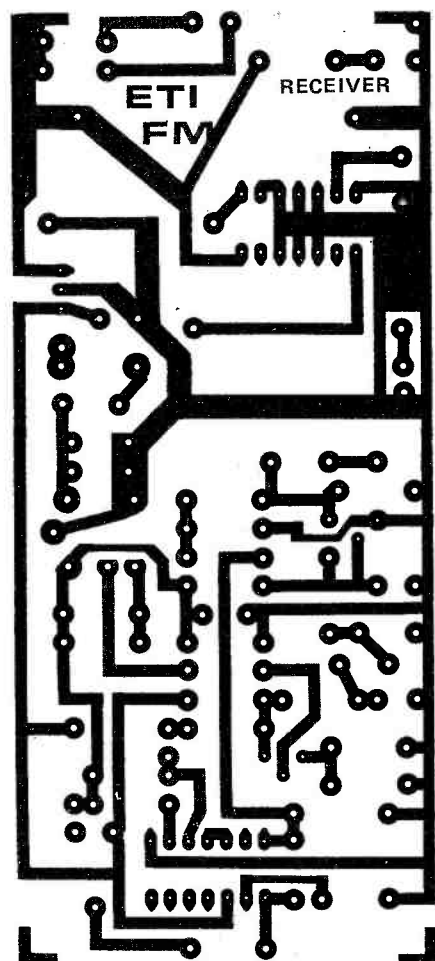
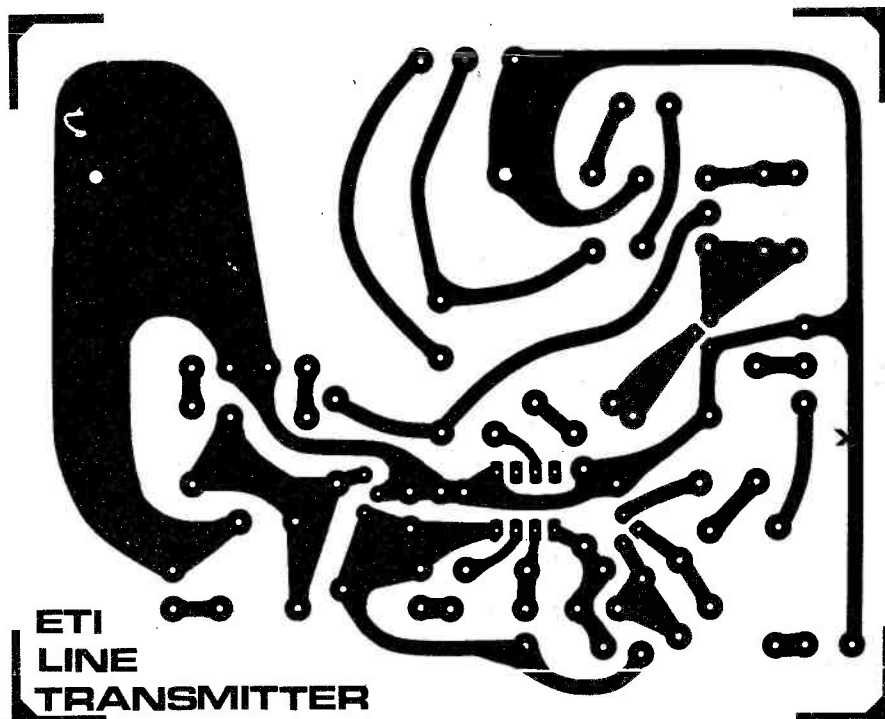
S-DECS AND T-DECS

S-Dec £3.79, T-Dec £4.59, u-DecA £4.69, U-DecB £7.16, 16 dil adaptor £2.31.

PCB FOIL PATTERNS







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ETIPRINTS are made from our original artwork ensuring a neat and accurate board. We thought ETIPRINTS were such a good idea that we have patented the system (patent numbers 1445171 and 1445172).

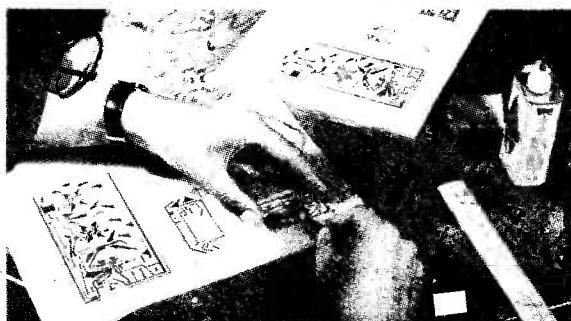
PARTS LIST

Shown below is the listing for the last year's ETIPRINTS.

Earlier sheets are available, ring Tim Salmon for details.

035	Oven Leakage Detector Pinball Wizard	Nov 79	038A	Long Period Timer Rain Alarm Touch Switch Flash Trigger Pseudo Random Noise Gen	Dec 79	049A	ETI 80 — VCO and VCLFO	Feb 80
036A	3 x Display Board Relay Activator Points Controller	Nov 79				040B	ETI 80 — PSU Tuning Fork Filter Coin Toss	Feb 80
036B	Data Distributor (double sided)	Nov 79	038B	Hum Filter Dice Logic Probe	Dec 79	041A	ETI Audiophile ETI VCA Signal Trace ETI HC Electromyogram	Mar 80
036C	Train Speed Controller Track Cleaner & Electronic Pot (double sided)	Nov 79	038C	Function Generator	Dec 79	041B	VCM Heater Controller	Mar 80
036D	Power Switch Selector (double sided)	Nov 79	039	Buffer Moving Coil Preamp Process Controller	Jan 80	042A	300W Amp Module	Apr 80
037A	Encoder (double sided)	Dec 79	039A	Hum Filter Logic Probe	Dec 79	033	Fuel Level Monitor, Alarm, Screen Controller Dynamic Noise Reducer	Sep 79
037B	Decoder (top side)	Dec 79	039B	Long Period Timer Rain Alarm Touch Switch Flash Trigger Pseudo Random Noise Gen	Dec 79	042B	Touch Dimmer, Battery Charger, RC Guardian (Top, Bottom) 1 & 2	Apr 80
037C	Decoder (bottom side)	Dec 79	039C	Function Generator	Dec 79	043	IR60 Preamps, Receiver, PSU, Servo Tester VU—PPM	May 80

HOW IT WORKS



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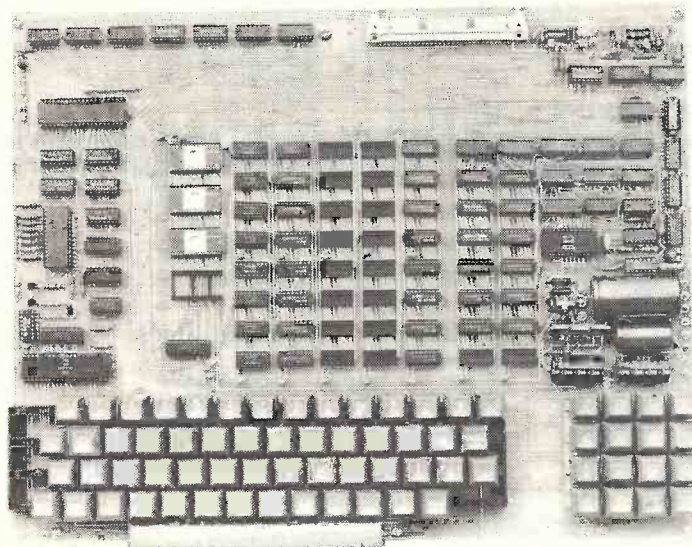
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		<p>ROTARY SWITCHES (water) 3P4W. 4P3W. 2P6W and 1P12W all 35p each.</p>	<p>MURATA TRANSDUCERS. REC/SENDER. MA4011 40KHZ £3.50 pair.</p>		
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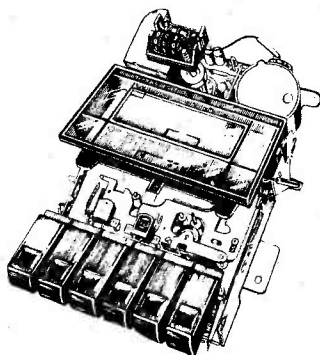
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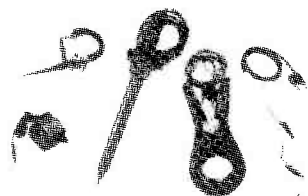
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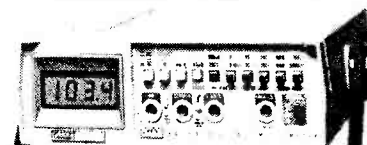
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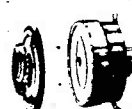
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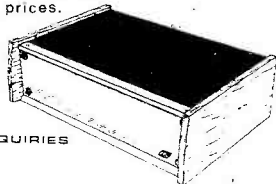
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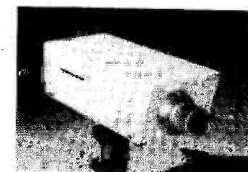
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AD INDEX

AJD Direct Supplies	112
Altek Instruments	109
Ambit International	83
Audio Electronics	14
Baringlock Ltd.	82
Baydis	25
Bi-Pak Semiconductors	20
BK Electronics	112
S&R Brewster	109
Butterworths	72
Calculator Sales & Service	71
Cambridge Learning Enterprises	70
Chiltmead	76
Chromasonics	48
Clef Products	71
Codespeed	42
Comp. Comp. Comp	123
Crimson Elektrik	82
Crofton Electronics	110
C.S.C.	19 & 105
Delta Tech & Co.	107
Display Electronics	100
Doram Electronics	26
E.D.A.	81
Electro-Tech Components	12
Electrovalue	14
Enviro Systems Ltd.	25

GMT Electronics	90
Greenbank	108
Greenweld	106
Happy Memories	105
Heathkit	109
Henry's Radio	46, 72, 91 & 110
ILP	36 & 37
Interface Components	41
Keelmore Ltd.	27
Kode Services	105
Lascar Electronics	102
LB Electronics	102
L&B Electronics	91
LSM Products	106
MacIn-Zand	104
Magnum Audio	103
Maplin	124
Marshall's	113
Metac	54 & 55
Micro-Circuits	104
Midland Trading Co.	4 & 5
Mighty Micro	107
Mountaineer	81
NIC Models	91

E. R. Nicholls	42
NTC	103
Polar Enterprises	42
Powertran Computers	118
Powertran Electronics	2 & 9
Progressive Electronics	42
Progressive Radio	119
Proton Electronics	82
J. W. Rimmer	38
R.T.V.C.	78
Science of Cambridge	32 & 33
Service Trading	92
Sinclair Electronics	71
C. N. Stevenson	56
Suretron	7
Swanley Electronics	113
Tandy	94
Tangerine	111
Target Electronics	110
Technomatic	13
Teleradio	91
Tempus	42 & 43
TK Electronics	103
Transam	96
Watford Electronics	6 & 7
West Hyde Developments	119
Wilmslow Audio	82

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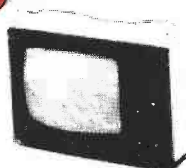


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7404	14p	74298	200p	4025	27p	9312	180p	3.75x1.75"	AD149	70p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7405	90p	74365	100p	4026	130p	9314	180p	4.7x1.75"	AD161/2	45p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7406	15p	74366	100p	4027	50p	9314	180p	4.7x1.75"	AD161/2	45p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7407	32p	74388	100p	4028	80p	9314	180p	4.7x1.75"	AD161/2	45p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7408	17p	74390	200p	4029	100p	9322	150p	Spot face cutter	BC109	11p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7409	19p	74393	200p	4030	55p	9334	380p	Pin insertion tool	BC117	20p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7410	15p	74490	225p	4031	200p	9368	200p	Wet Wirof Pin	BC147/8	9p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7411	20p	74508	225p	4032	180p	9370	200p	+ 2 wire spoils	BC149	10p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7412	20p	74509	14p	4033	110p	9374	200p	+ comb	BC157/8	10p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7413	20p	74502	14p	4034	285p			Combs	BC169C	12p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7414	50p	74503	18p	4037	115p				BC172	12p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7414C	50p	74504	18p	4038	120p				BC177/8	17p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7416	27p	74505	25p	4039	225p				BC179	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7417	27p	74506	22p	4040	100p				BC183/3	10p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7420	17p	74510	20p	4041	80p				BC184	11p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7421	40p	74511	40p	4042	80p				BC187	10p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7422	22p	74513	40p	4043	90p				BC212/3	11p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7423	34p	74514	72p	4046	110p				BC214	12p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7425	30p	74515	40p	4047	110p				BC237	15p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7426	40p	74520	20p	4047	100p				BC308	16p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7427	34p	74521	40p	4048	120p				BC337	16p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7428	17p	74527	38p	4049	50p				BC338	16p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7430	17p	74530	20p	4050	40p				BC461	36p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7432	30p	74532	27p	4052	80p				BC477/8	30p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7433	40p	74533	27p	4052	80p				BC516/7	70p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7434	40p	74534	27p	4052	80p				BC517	70p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7435	38p	74535	24p	4053	80p				BC548C	80p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7438	35p	74551	24p	4054	150p				BC549C	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7440	17p	74555	30p	4055	125p				BC557/8	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7441	70p	74573	50p	4056	135p				BC558C	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7442A	60p	74574	36p	4057	140p				BC559C	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7443	112p	74575	40p	4058	140p				BC570	70p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7444	112p	74576	45p	4059	140p				BC571/2	70p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7445	100p	74583	110p	4066	55p				BD131/2	22p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7446A	80p	74585	100p	4067	450p				BD135/6	54p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7447A	80p	74586	40p	4068	27p				BD139	58p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7448	80p	74590	40p	4069	200p				BD140	60p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7450	92p	74592	40p	4070	30p				BD189	18p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7451	17p	74593	60p	4071	25p				BD232	95p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7453	17p	74596	110p	4072	25p				BD235	75p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p	200p	
7454	17p	74597	45p	4073	25p				BD241	85p	BF259	36p	48p	2N3442	140p	40364	70p	40364	70p	40364	70p	40364	70p	10A 400V	200p	200p	200p		

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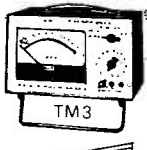
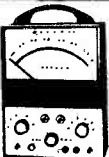
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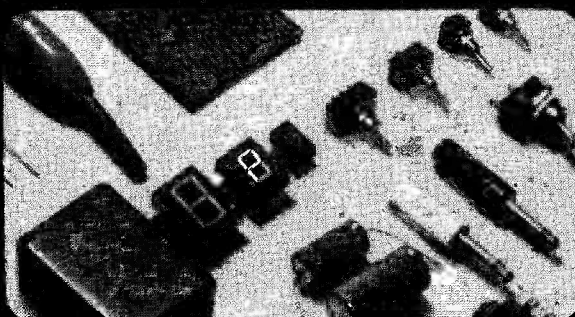
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FM MAINS DISTRIBUTOR

A system for distributing a Hi-Fi or other audio signal to any number of remotely-located speakers, using the mains wiring as the communication link.

This unusual project is designed to distribute an audio signal to any number of speakers that are remotely-located throughout a house or office building, using the mains wiring as the communication link. The system has an overall audio frequency response that extends to 20 kHz, with typically less than 0.5% total harmonic distortion and is designed to deliver a maximum of about 2 watts to each speaker. The system rejects all unwanted mains noise and has an overall audio sensitivity of about 10 mV for 2 watts output on each speaker.

The system comprises a single transmitter unit and any required number of remotely-located receiver/amplifier units. The transmitter unit generates a 200 kHz carrier signal, which is frequency modulated by the audio input signal and which the transmitter superimposes on the neutral line of the 230 volt AC mains wiring. At each receiver unit, this FM signal is picked up from the mains, is amplified, demodulated and the resulting audio signal is then fed to an external eight ohm speaker via a 2 watt power amplifier IC.

The transmitter and each receiver unit is provided with its own volume control. Each receiver unit is also provided with an automatic mute facility, which disables its audio output when the transmitter is turned off. All units are mains powered and simply plug into existing mains sockets via fused (1 amp) plugs, no other interconnections being required. All units incorporate a variety of safety features, but it is essential for correct operation that the mains sockets be wired in the correct polarity: each socket should thus be tested with a neon indicator or similar device before plugging a unit into place.

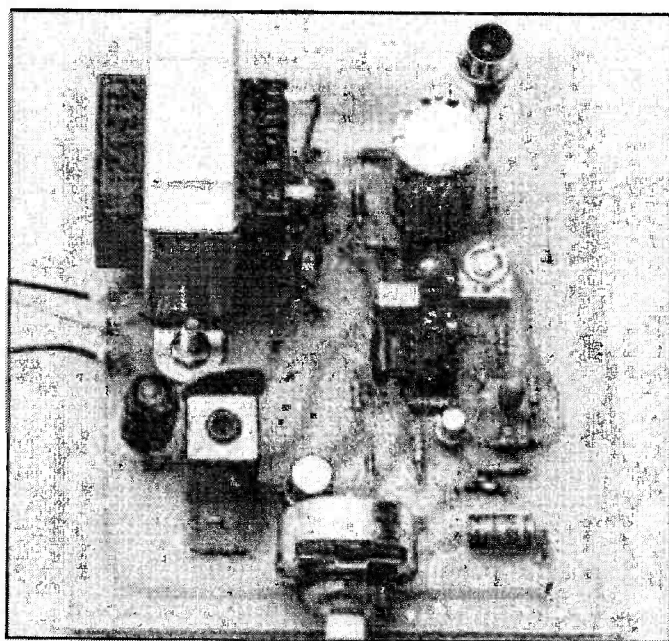
The Mains-Line system can readily distribute an audio signal throughout an entire house or office building and has a variety of practical applications. In the home, it can be used to transmit the output of a music centre or other audio source to all rooms in the building. Alternatively, the transmitter can be fitted with a microphone and pre-amp and used as a baby alarm, enabling the baby to be heard from any part of the house.

In an office, the transmitter can be coupled to a mixer unit and used to distribute music signals and announcements throughout the entire building without the expense of having to fit additional wiring.

Construction: The Transmitter

The entire transmitter unit, including the power transformer, is assembled on a single PCB. Construction should present few problems if the usual precautions are taken to ensure that all semiconductor devices and electrolytics are fitted in the correct polarity.

When construction is complete, set the core of L2 and the slider of RV1 to mid position. If you have a 'scope, give the



unit a functional check by checking that a signal of a few hundred mV at about 200 kHz is present across the output terminals of T2: set the frequency to precisely 200 kHz via RV1 and trim the core of T2 for maximum output.

You can, if you wish, case the complete unit; our own prototype is uncased, as it is intended to be built into an existing audio amplifier system.

Construction: The Receiver

Most of the receiver unit (except T1, RV2, SW1 and LED 1) is wired up on a single PCB. Construction should present few problems if the overlay is followed with care. When construction is complete, fit the PCB and remaining components into a suitable case and complete the interconnections to T1, RV2, SW1 and LED 1, as indicated on the overlay and the circuit diagram.

When construction is complete, set the core of T2 and the slider of RV1 to their mid position, connect the output of the unit to an eight ohm speaker and switch the unit on. With mute switch SW1 on, little noise should come from the speaker: with SW1 off, lots of 'white' noise should come from the speaker, indicating that the system is functional. If you have a 'scope, monitor pins 4-5 of IC1 and adjust RV1 to obtain a frequency of about 400 kHz.



HOW IT WORKS

The system is designed to transmit an audio signal to any number of remotely-located receiver/speaker units, using the mains wiring as the communication link. The transmitter produces a low-level 200 kHz carrier signal, frequency modulated by the audio signal, which it superimposes on the neutral line of the mains wiring. At each receiver unit, the carrier signal is picked up from the mains, amplified, demodulated and the resulting audio signal is passed on to a speaker via a 2 watt audio amplifier IC. The use of an FM link ensures a good audio response and excellent noise rejection.

System operation relies on the fact that the mains wiring is highly inductive and acts as a fairly high impedance to a 200 kHz signal. At this frequency, the wiring can be regarded as an inductive potential divider, with the power sub-station at its 'low' end. This 'divider' normally produces relatively little signal attenuation between power points that are separated by scores or hundreds of metres of wiring and can be used as an excellent built-in 'data link' in any home.

The Transmitter

IC2 is a voltage-controlled oscillator, or VCO. Its operating frequency is determined by the values of RV1-R4 and C8 and by the voltage on pin 5. With the component values shown, the VCO operates at a centre frequency of 200 kHz and produces a square wave output at pin 3. This output is used to drive common emitter amplifier Q1, which uses a standard IF transformer (T2) as its collector load; the centre frequency of T2 is shifted to 200 kHz by C3 and its 'Q' is reduced to a fairly low value (to give a broad-band response) by R2. The output signal on T2 secondary (pins 4 and 5) has an amplitude of a few hundred mV rms.

Audio input signals to the unit are fed to volume control RV2 via C11 and then subjected to about 20 dB of amplification via Q2. The output of Q2 is used to frequency modulate the VCO via C9 and pin 5. Consequently, the output of T2 is a 200 kHz 'carrier' signal frequency modulated by the audio signal. This output is coupled into the neutral line of the mains wiring via low-value capacitor C2 and current-limiting 'fuse' LP1. Note that one side of T2 output is wired to the Earth line of the mains, thereby ensuring that standing DC potentials of only a few volts exist between the primary and secondary windings of the transformer. C2 and LP1 ensure that the system will not be damaged if the output signal is accidentally fed to the live, rather than the neutral, side of the mains.

Q2 and IC2 are powered from a stabilised supply via IC1, a 12 volt regulator.

The Receiver

The 200 kHz frequency-modulated mains signal is picked up on the input of T2 via C2 and current-limiting 'fuse' LP1; D3 and D4 are used to limit the T2 signal amplitudes to a few hundred millivolts. T2 is tuned to 200 kHz via C3 and has its 'Q' reduced to a fairly low value via R4, to give a broad-band response. The isolated output signal of T2 is fed to the base of common emitter amplifier Q1 via current-limiting resistor R5.

The base of Q1 is biased to 4V5 via the R2-R3 divider network. Q1 is overdriven by the input signal and has its output clipped at about 6 volts peak-to-peak. The output of Q1 is fed to the pin 3 input terminal of IC1 via R8-C6-R9. IC1 is a phase locked loop and is used to demodulate the 200 kHz FM carrier signal. This IC contains a reference oscillator, which is set to the same centre frequency as the carrier via RV1-R13 and C11. The demodulated audio signal appears at pin 7 of IC1. C12-R14-C13-R15-C14 are used to filter out any vestiges of the carrier and the resulting 'clean' audio signal is passed on to volume control RV2 via C15. The output of the volume control is fed to 2-watt audio amplifier IC3 and is then passed on to an external eight ohm speaker via C17. Most of the circuit (other than IC3) is powered from a stabilised supply via IC2, a 12 volt regulator.

The receiver unit is provided with an automatic 'mute' facility, which kills the audio output in the absence of a carrier signal, via Q2 and its associated network. Q2 is wired across the input to the volume control and kills the audio signal when biased on. Q2 is biased from two independent sources. It is positively biased (biased on) via R11 and the R2-R3 potential divider and can also be negatively biased (biased off) from the output of Q1 via the C7-D5-D6-C8-R12 rectifier network. The values of R11 and R12 are chosen so that the negative bias is predominant and Q2 is turned off in the presence of a carrier signal that has sufficient strength to produce a peak-to-peak signal in excess of about 1V5 at Q1 collector. In the absence of a suitable carrier signal the negative bias falls to a negligible value and Q2 is turned on via R11.

The automatic mute circuit can be disabled by closing SW1, in which case the phase-locked loop tries to lock on to noise signals in the absence of a carrier and consequently produces very high noise levels at the output of IC3.

BUYLINES

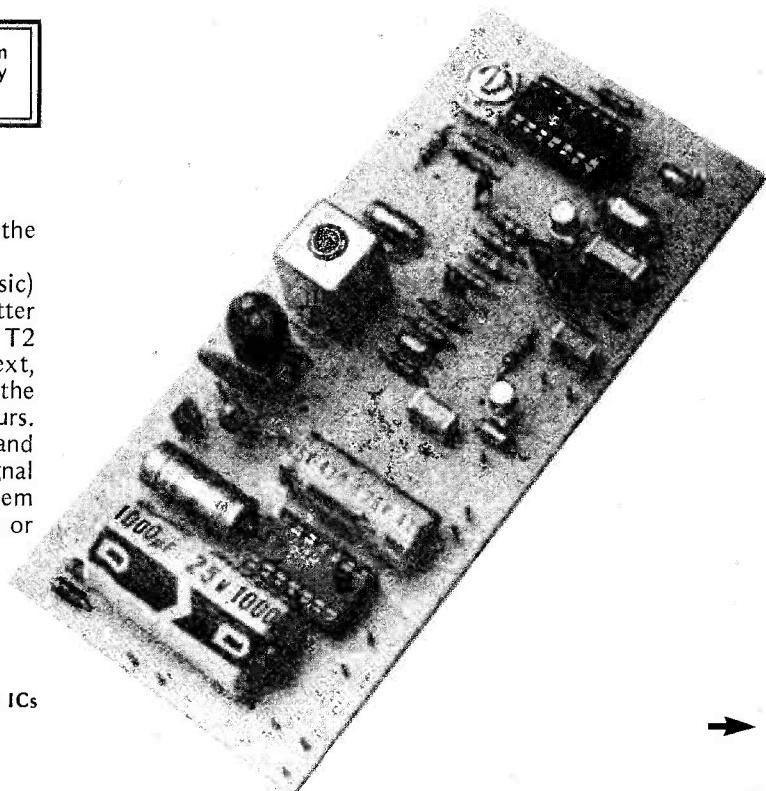
The Denco IF transformer used in this project is available from Watford Electronics. The other components should be readily obtainable.

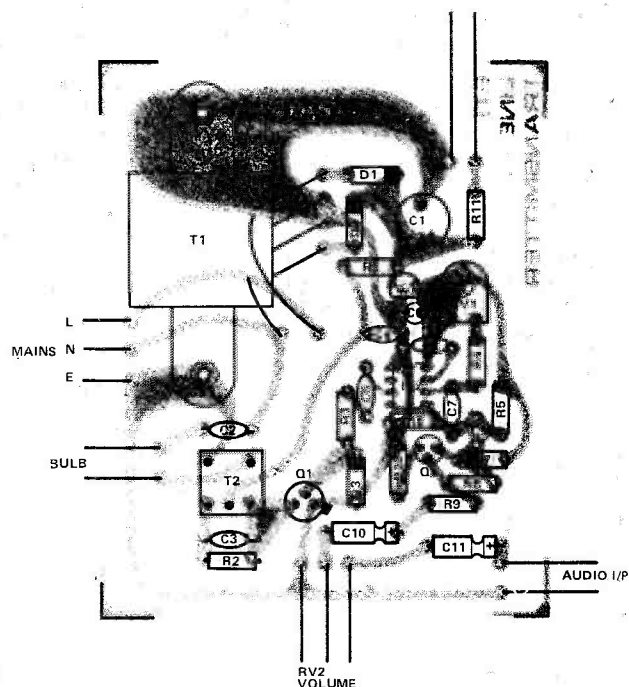
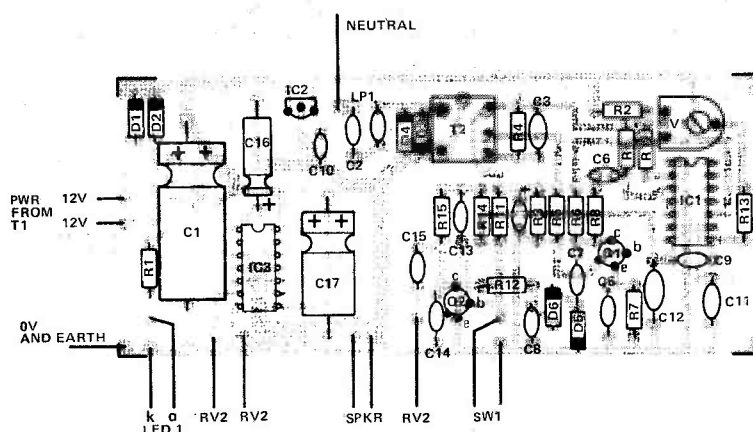
Setting Up The System

Access to a 'scope is needed when initially setting up the system, as follows.

Switch on both units and apply a suitable audio (music) signal to the input of the transmitter. Turn the transmitter volume control to zero, use the 'scope to monitor pin 2 of T2 in the receiver and adjust T2 core for maximum signal. Next, monitor pins 4-5 of IC1 in the receiver and set RV1 to the mid position at which locking to the 200 kHz carrier occurs. Finally, set the receiver volume control to mid value and adjust the transmitter volume control so that the music signal is heard at the receiver without apparent clipping. The system is then complete and ready for use throughout the house or office.

Right: a fully assembled line receiver PCB. Note the polarity of the ICs and polarised components.





12-0-12 transformer 6VA, 12V 100 mA bulb, T2 is Denco IFT
14, 8 ohm loudspeaker.

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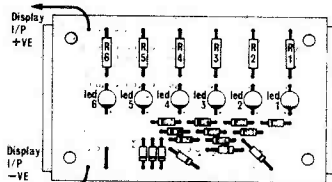
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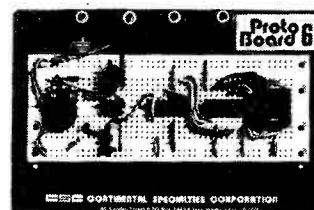
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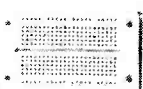
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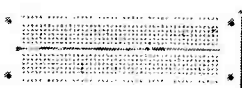
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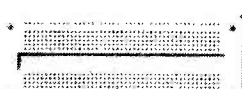
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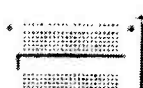
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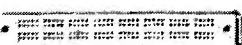
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AD140	£0.69	BC207	£0.13	BD177	£0.78	OC29	£1.09	2N2906	£0.19
AD142	£0.98	BC208	£0.13	BD178	£0.78	OC35	£1.09	2N2906A	£0.19
AD143	£0.86	BC209	£0.14	BD179	£0.86	OC36	£1.03	2N2906B	£0.21
AD149	£0.86	BC212	£0.10	BD203	£0.92	OC70	£0.28	2N2907A	£0.25
AD161	£0.40	BC212L	£0.10	BD204	£0.92	OC71	£0.17	2N2926G	£0.11
AD162	£0.40	BC213	£0.10	BD205	£0.92	TIC44	£0.33	2N2926H	£0.11
AD181	£0.40	BC213L	£0.10	BF457	£0.43	TIC45	£0.40	2N2926I	£0.11
162MP	£0.81	BC214	£0.10	BF458	£0.43	TIP29A	£0.46	2N2926J	£0.11
AF124	£0.35	BC214L	£0.10	BF459	£0.43	TIP29B	£0.46	2N2926K	£0.11
AF125	£0.35	BC227	£0.18	BF594	£0.35	TIP29C	£0.51	2N3053	£0.20
AF126	£0.35	BC238	£0.18	BF596	£0.32	TIP30A	£0.46	2N3054	£0.20
AF127	£0.35	BC251	£0.17	BF598	£0.28	TIP30B	£0.46	2N3055	£0.20
AF139	£0.40	BC251A	£0.18	BF599	£0.29	TIP30C	£0.51	2N3614	£1.15
AF186	£0.58	BC301	£0.32	BF797	£0.32	TIP31A	£0.46	2N3615	£1.21
AF239	£0.44	BC302	£0.33	BF800	£0.32	TIP31B	£0.48	2N3616	£1.21
AL102	£1.38	BC303	£0.32	BF829	£0.25	TIP31C	£0.51	2N3646	£0.09
AL103	£1.38	BC304	£0.44	BF830	£0.35	TIP32A	£0.46	2N3702	£0.09
AU104	£1.61	BC321	£0.16	BF834	£0.28	TIP32B	£0.48	2N3703	£0.09
AU110	£1.61	BC326	£0.17	BF835	£0.28	TIP32C	£0.51	2N3704	£0.08
AU113	£1.61	BC337	£0.17	BF836	£0.29	TIP41A	£0.51	2N3705	£0.08
BC107A	£0.09	BC338	£0.17	BF837	£0.25	TIP41B	£0.52	2N3706	£0.08
BC107B	£0.10	BC440	£0.35	BF838	£0.25	TIP41C	£0.55	2N3707	£0.08
BC107C	£0.12	BC441	£0.35	BFY50	£0.20	TIP42A	£0.51	2N3708	£0.08
BC108A	£0.10	BC450	£0.61	BFY51	£0.20	TIP42B	£0.53	2N3709	£0.08
BC108B	£0.11	BC461	£0.44	BFY52	£0.20	TIP42C	£0.55	2N3710	£0.08
BC108C	£0.12	BC477	£0.23	BFY53	£0.20	TIP2955	£0.69	2N3819	£0.21
BC109A	£0.09	BC478	£0.23	BP120	£0.44	TIS40	£0.25	2N3820	£0.08
BC109B	£0.10	BC479	£0.23	BP119	£0.44	TIS90	£0.21		
BC109C	£0.12	BC547	£0.12	20MP	£0.92	UT46	£0.23		
BC147	£0.08	BC548	£0.12	BRY39	£0.51	ZTX107	£0.12		

74 SERIES TTL

Type	Price	Type	Price	Type	Price	Type	Price	Type	Price
7400	£0.10	7427	£0.28	7473	£0.29	74110	£0.41	74165	£0.78
7401	£0.13	7428	£0.30	7474	£0.29	74111	£0.67	74166	£0.90
7402	£0.13	7430	£0.33	7475	£0.33	74118	£0.92	74174	£0.75
7403	£0.13	7432	£0.25	7476	£0.29	74119	£1.36	74175	£0.71
7404	£0.13	7433	£0.35	7480	£0.51	74121	£1.36	74176	£0.67
7405	£0.13	7437	£0.24	7481	£0.98	74122	£0.65	74177	£0.67
7406	£0.25	7438	£0.24	7482	£0.78	74123	£0.48	74180	£0.71
7407	£0.25	7440	£0.14	7483	£0.67	74136	£0.60	74181	£0.67
7408	£0.15	7441	£0.58	7484	£1.01	74141	£0.63	74182	£0.81
7409	£0.15	7442	£0.46	7485	£0.78	74145	£0.63	74184	£0.81
7410	£0.13	7443	£0.81	7486	£0.25	74150	£0.78	74190	£0.78
7411	£0.20	7444	£0.81	7487	£1.96	74151	£0.65	74191	£0.71
7412	£0.17	7445	£0.75	7490	£0.37	74152	£0.68	74192	£0.68
7413	£0.28	7446	£0.69	7491	£0.74	74154	£0.94	74193	£0.67
7414	£0.58	7447	£0.55	7492	£0.40	74155	£0.58	74194	£0.71
7416	£0.26	7448	£0.64	7493	£0.35	74156	£0.58	74195	£0.69
7417	£0.26	7450	£0.13	7494	£0.86	74157	£0.58	74196	£1.21
7420	£0.13	7451	£0.13	7495	£0.58	74160	£0.67	74197	£1.21
7421	£0.23	7453	£0.13	7496	£0.58	74161	£0.71	74198	£1.13
7422	£0.18	7454	£0.13	74100	£0.98	74162	£0.71	74199	£2.13
7423	£0.24	7460	£0.13	74104	£0.45	74163	£0.71		
7425	£0.22	7470	£0.29	74105	£0.44	74164	£0.78		
7426	£0.26	7472	£0.23	74107	£0.28				

CMOS ICs

Type	Price	Type	Price	Type	Price	Type	Price	Type	Price
CD4000	£0.16	CD4012	£0.22	CD4022	£0.94	CD4031	£2.30	CD4046	£1.50
CD4001	£0.22	CD4013	£0.48	CD4023	£0.22	CD4035	£1.38	CD4047	£1.00
CD4002	£0.18	CD4015	£0.94	CD4024	£0.75	CD4037	£1.09	CD4049	£0.55
CD4006	£1.06	CD4016	£0.49	CD4025	£0.22	CD4040	£1.01	CD4050	£0.55
CD4007	£0.09	CD4017	£0.94	CD4026	£1.38	CD4041	£0.87	CD4054	£1.27
CD4008	£1.06	CD4018	£0.98	CD4027	£0.58	CD4042	£0.83	CD4054	£1.27
CD4009	£0.52	CD4019	£0.48	CD4028	£0.78	CD4043	£1.01	CD4054	£1.27
CD4010	£0.55	CD4020	£1.04	CD4029	£0.98	CD4044	£0.94	CD4056	£1.52
CD4011	£0.22	CD4021	£0.94	CD4030	£0.55	CD4045	£1.61	CD4069	£0.20

LINEAR

Type	Price	Type	Price	Type	Price	Type	Price	Type	Price
CA3011	£1.13	CA3130	£1.07	NE536	£0.06	UA723C	£0.52	SL1414	£2.24
CA3014	£1.55	CA3140	£0.87	NE555	£0.09	72723	£0.52	TAA550B	£0.40
CA3018	£0.75	LM301	£0.33	NE556	£0.28	UA741C	£0.28	TAA550B	£0.40
CA3020	£1.96	LM304	£1.84	NE556	£0.69	72741	£0.28	TAA550B	£0.40
CA3028	£0.92	LM308	£1.15	NE556	£1.38	741P	£0.69	TAA550B	£0.40
CA3035	£1.61	LM309	£1.73	NE556	£1.73	UA747C	£0.23	TAA550B	£0.40
CA3036	£1.15	LM380	£0.98	NE567	£1.96	72747	£0.69	TAA550B	£0.40
CA3042	£1.13	LM381	£0.98	UA702C	£0.53	UA748	£0.40	TAA550B	£0.40
CA3043	£2.13	LM3900	£0.67	72702	£0.53	72748	£0.40	TAA550B	£0.40
CA3046	£0.81	MC1303L	£0.98	UA703	£0.29	748P	£0.40	TAA550B	£0.40
CA3052	£1.84	MC1304	£2.19	UA709	£0.29	SN76013N	£2.01	TAA550B	£0.40
CA3054	£1.27	MC1310	£1.09	72709P	£0.53	SN76023N	£2.01	TAA550B	£0.40
CA3075	£1.73	MC1312	£1.29	UA710C	£0.46	SN76110	£1.73	TAA550B	£0.40
CA3081	£1.73	MC1350	£1.38	UA711C	£0.37	SN76115	£1.73	TAA550B	£0.40
CA3089	£2.30	MC1352	£1.61	72711	£0.37	SN76660	£0.85	TAA550B	£0.40
CA3090	£4.14	MC1469	£3.39					TAA550B	£0.40
CA3123	£2.19	MC1496	£1.04					TAA550B	£0.40

THYRISTORS

Volts No.	Price	Volts No.	Price	Volts No.	Price	Volts No.	Price
10 THY600ma/10v	£0.17	50 THY1A/50	£0.30	50 THY1A/100	£0.32	50 THY1A/200	£0.37
20 THY600ma/20v	£0.18	100 THY1A/100	£0.32	200 THY1A/200	£0.37	400 THY1A/400	£0.44
50 THY600ma/30v	£0.23	200 THY1A/200	£0.37	400 THY1A/400	£0.44	600 THY1A/600	£0.52
100 THY600ma/100v	£0.29	400 THY1A/400	£0.44	600 THY1A/600	£0.52	800 THY1A/800	£0.57
200 THY600ma/200v	£0.44	600 THY1A/600	£0.52	800 THY1A/800	£0.57		
400 THY600ma/400v	£0.51						

LEDs

O/no	Size	Colour	Price
1501	125	RED	£0.10
1502	125	GREEN	£0.16
1503	125	YELLOW	£0.16
1504	2	RED	£0.10
1505	2	GREEN	£0.16
1506	2	YELLOW	£0.16
1509	2	CLEAR	£0.12

(Ill Red)

SUPER 'HY-Brite' Type

1521	125	RED	£0.11
1522	2	RED	£0.11
1514	ORP 12	Light dependent resistor	£0.70
1520	OC71	Photo transistor	£0.40

CLIPS

HOUSE WIRING

Ray Marston discusses house wiring systems of the past, present and future, presents some useful 're-wiring' aids and talks about some fascinating line-based gadgets for the '80s.

Modern house wiring circuits are designed to conform to regulations laid down in 1947, that far-distant time when valves were in vogue and the word 'electronics' was used only in Sci-Fi movies. Consequently, modern house wiring works fine when used to power simple devices like fluorescent lamps and electric toasters, but presents distinct problems if you want to use modern electronic lamp dimmers, FM power-line audio distribution systems, power-line remote control systems, or similar '1980s' devices.

If you happen to live in a house built before 1947, when 'modern' wiring was first introduced, it's a fair bet that your wiring is not only highly inefficient but is *downright dangerous*, with its rubber insulation perished to the point where total breakdown is imminent and the whole shambles is in danger of bursting into flames! So you'd better think about a rewiring. And if you are going to rewire, you may as well rewire for the '80s.

In the next few pages we'll tell you how 'modern' wiring systems work, explain the wiring needs of the '80s, give a few hints on how to conduct a rewiring job and tell you about some of the wiring-based electronic control and data distribution systems that you are likely to see in the next year or so.

Conventional Power Wiring Systems

Electric power is fed into the house from the outside mains and passes to the building's electricity meter. It is then fed to the individual household circuits via individual fuse units or, in the latest systems, via a multi-fused 'consumer' unit.

The household circuits are, for convenience, classified as three distinct types, (a) power circuits (feeding sockets, etc), (b) lighting circuits and (c) accessory circuits (individual heavy-duty circuits feeding immersion heaters, cooker panels, etc). Let's look first at 'power' circuits.

Old-style (pre 1947) electrical systems use a 'radial' system of power wiring, as shown in Fig.1. Here, each individual power socket or small group of sockets is treated as an individual circuit and is connected to the mains via its own specific fuse; often, the live and neutral lines of each circuit are individually fused.

Sometimes, different circuits have different fuse ratings (sometimes the cable gauges may also be different), so that an electric fire (for example) may work on one socket but blow the fuses (or the wiring) when connected to another socket.

The radial wiring system is clearly inefficient and requires the use of excessive amounts of cable and an excessive number of fuses.

'Modern' (post 1947) electrical systems use a 'ring' system of power wiring, as shown in Fig.2. Here, a power cable is run from the fuse box to the first (hall) socket, then sequentially to all of the sockets on (say) the ground floor and finally back to the fuse box again, so that a 'ring' of cable is formed. The ring is treated as a single circuit and provided with a single

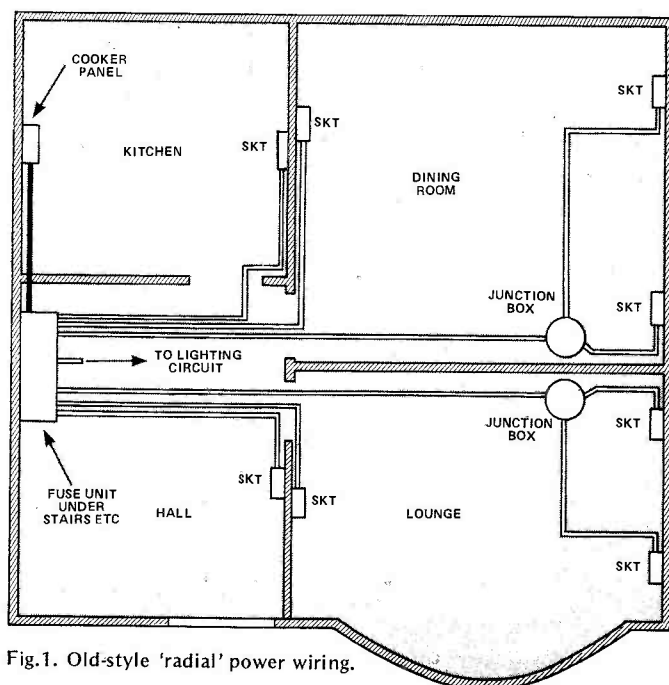


Fig.1. Old-style 'radial' power wiring.

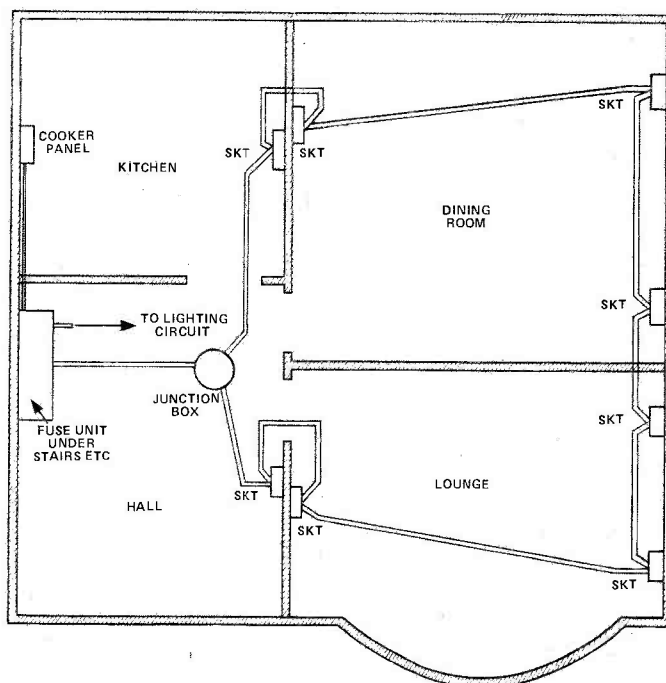


Fig.2. Modern-style 'ring' power wiring circuit. The 'ring' is shown here connected to the fuse unit via a junction box, but in practice the 'ring' may be connected directly to the fuse unit.

master fuse, but all socket plugs are individually fused. Most modern houses are provided with two ring circuits, one for each floor. On the upper floor, the ring may be connected to the fuse unit via a junction box and feeder cable.

The ring system is very efficient in the use of cable. Power is fed to each individual socket via both sides of the ring, which are thus effectively wired in parallel and share the socket current. This factor enables a relatively light gauge of ring cable to be used. In practice, 2.5 mm² PVC sheathed cable is used for ring circuits. Any number of sockets can be fitted on a ring serving a surface area of less than 100 m² (1000 ft²): the ring must be fitted with a 30 A (max) fuse and can handle up to 7.2 kW. The feeder cable to such a ring (if used) must be 4 mm² type.

Power Wiring For The 80s

The most important 'house wiring' innovation of the '80s will be the widespread use of the mains wiring as a high frequency (a few tens or hundreds of kHz) data link between different parts of the house. The live and neutral lines of the house wiring each contain very considerable lengths of cable and consequently have substantial inductance. The reactance of the wiring is negligible at 50 Hz but can be quite significant at frequencies of a few tens or hundreds of kHz.

High frequency signals can thus readily be superimposed

on the power wiring at any power socket in the house and can then be picked off again at any (or all) of the remaining sockets throughout the household.

Cable Music

You have two 'sets' of cables in the power wiring (earth-neutral and earth-live), giving you two independent data links throughout the house. One link can be used for distributing hi-fi signals via an FM system of the type described elsewhere in this issue. The other link can be used for distributing control data instructions to remote units: a 6-bit data word can be used to address any one of 16 different devices and convey up to four different instructions to those devices.

Figure 3 shows an example of the degree of control that can be obtained via a data-link system: only seven of the 16 available remote control channels are shown in use. On a cold and frosty morning you can, from the comfort of your bed, switch on the sump heater in the garage, activate the hi-fi distribution system and turn on the kettle and toaster in the kitchen. In the evening you can turn on the immersion heater and the electric blanket while sitting in your armchair in the lounge.

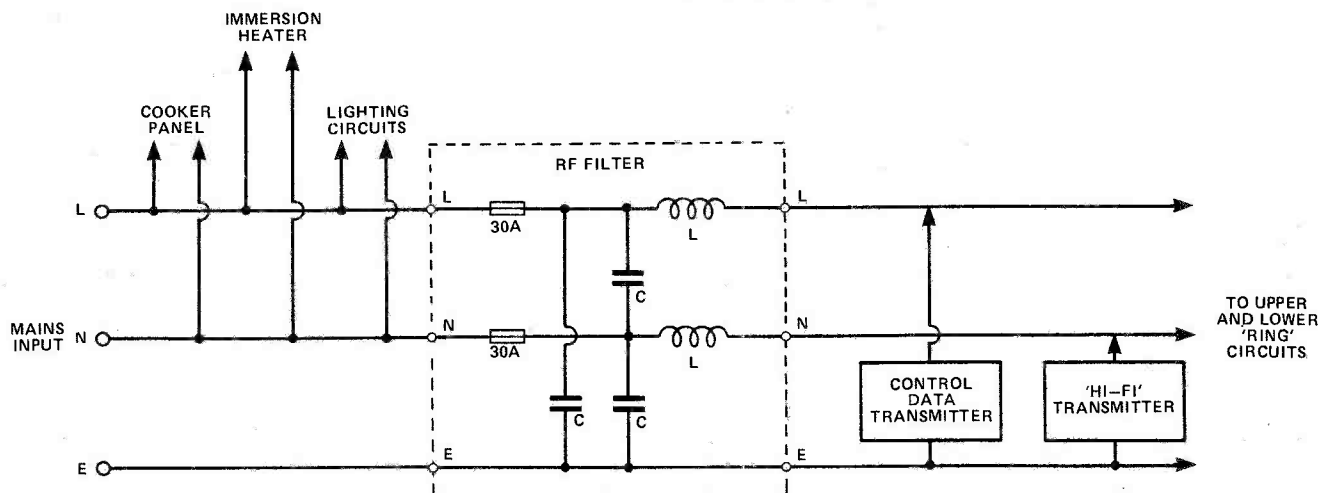
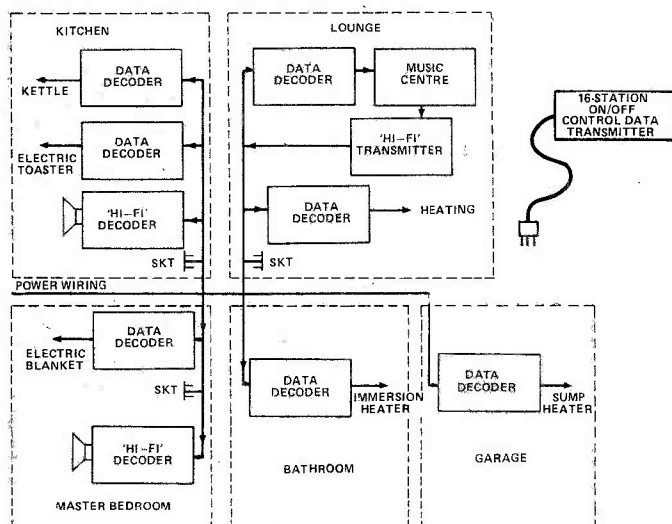
Absolute Luxury.

In the diagram we've shown a single 16-station transmitter unit that can be plugged into any convenient socket. In practice, you may prefer to have individual transmitter units permanently fitted into the lounge, kitchen and master bedroom. If you are really lazy, you can have a single 16-station infra-red transmitter unit that can pump signals into the mains via infra-red receiver/re-transmitter unit built into each room.

These high frequency distribution systems have considerable range and will work perfectly with all existing house wiring. This range is so great that signals can easily be picked up in neighbouring houses as well. If your neighbour happens to have a similar distribution system (it's a fair bet that he will within the next few years) the systems will interact. To overcome this problem you'll have to fit an efficient RF filter to the feeder lines, as shown in Fig.4, so that the unwanted external signals see the low impedances of the filter capacitors, while the signals on the internal rings see the high impedances of the filter inductors and do not escape.

Fig.3. (left) Hi-Fi signals are fed to all power sockets in the house via an FM distribution system. Kettles, toasters, heaters, etc can be activated from any room in the house fitted with a power socket via a 16-channel remote control system: only seven channels are shown in this diagram.

Fig.4. (below) When power-circuit data distribution systems become widespread, it will be necessary to fit efficient RF filters to the feeder lines of the ring circuits.



Ring For Roses

A major problem with the Fig.4 circuit is that suitable (30 A) filter inductors are not readily available at the present time. When planning a rewire for the '80s, space should, however, be left in the fuse box area for the eventual fitting of such a filter when suitable components become available. Note that high-current 'accessory' circuits such as the cooker panel and immersion heater are not fed by the filter: nor are the lighting circuits, which generate a good deal of electrical noise when used with lamp dimmers, etc.

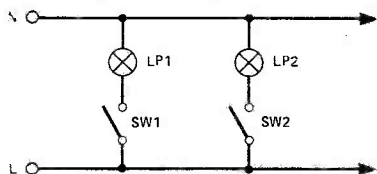


Fig.5. The basic lighting circuit (earth wiring not shown).

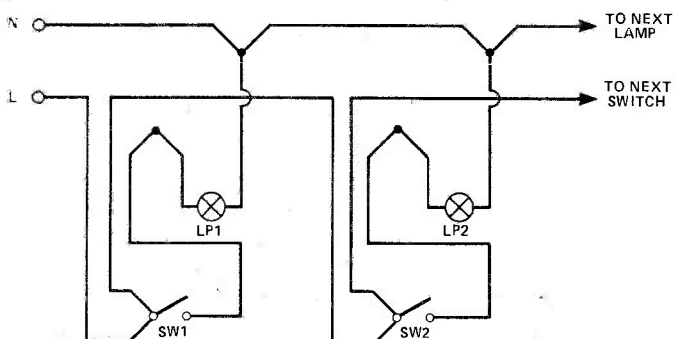


Fig.6. Old-style implementation of the lighting circuit (earth wiring not shown), with three wires (plus earth) running down to each switch.

In summary, then, power wiring for the '80s will take the form of 'modern' (post 1947!) ring circuits except that the feed line to the rings should be fitted with RF filters.

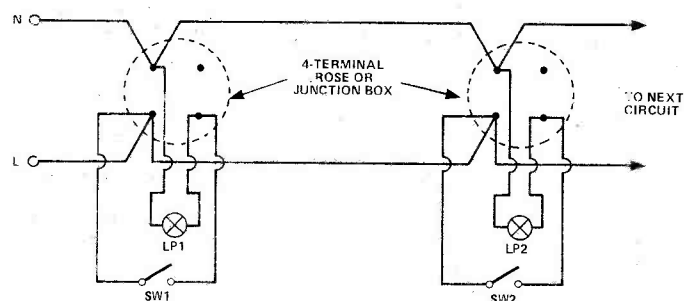


Fig.7. Modern-style implementation of the lighting circuit (earth wiring not shown), with two wires (plus earth) running down to each switch.

Conventional Lighting Circuits

The basic lighting circuit of a domestic system is deceptively simple, as shown in Fig.5. Note that the light switch is used to connect the lamp to the live side of the circuit, thereby ensuring that a shock cannot be received from the lamp holder (when changing a bulb) when the switch is open or off.

The physical implementation of the Fig.5 circuit is not a simple task. Fig.6 depicts the old-style (pre 1947) method of implementation, in which Neutral goes to one side of each lamp and the Live line is looped from one switch to the next. Note that this method requires three wires (plus Earth) to be run down to each switch. In practice, the old-style wiremen tended to disregard the 'polarity' rules and often switched the

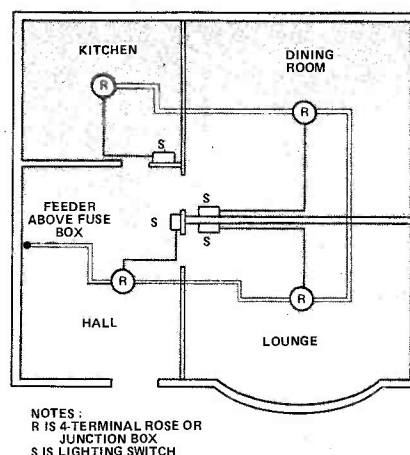


Fig.8. Typical ground-floor lighting circuit of a medium sized house.

Neutral line, so that the lamp holder remained permanently (and dangerously) 'live'.

Once again, the system in Fig.8 looks deceptively simple. In practice, the system may, if you are unlucky, take a full weekend to implement, particularly if you are changing the positions of light switches and have to cut new down-channels in the plaster to accommodate new cable runs.

Lighting The Way

Figure 9 shows the circuit and implementation of 2-way light switching. In practice 2-core, plus earth, cable is used to connect SW1 to the ceiling rose and 3-core plus earth is used to interconnect SW1 and SW2. A lot of channelling work may be required to implement the system. Note that changeover switches are required for 2-way switching.

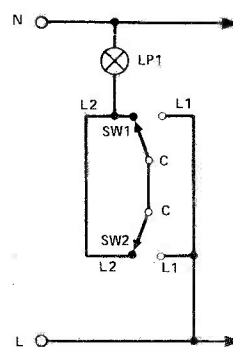
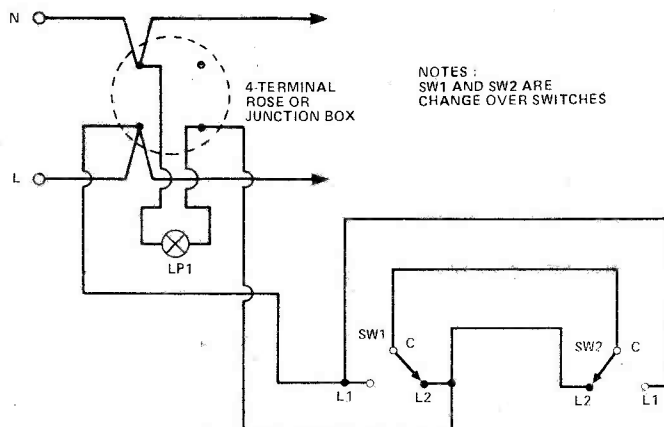


Fig.9. Circuit (left) and implementation (below) of modern 2-way light switching (earth wiring not shown). Note the large number of wires running down to the switches; in practice, a total of seven wires run down to SW1. The switching is shown in the OFF position.



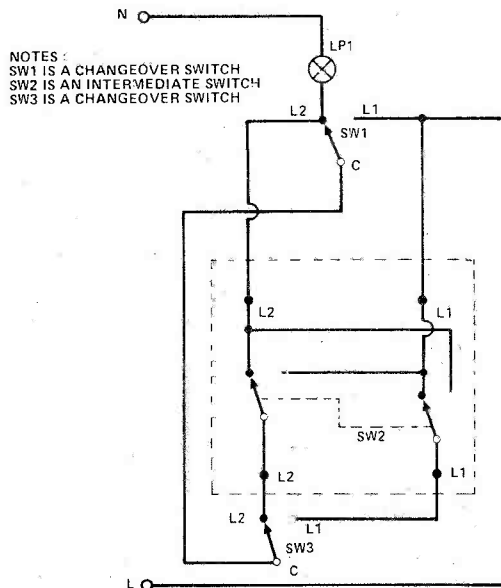
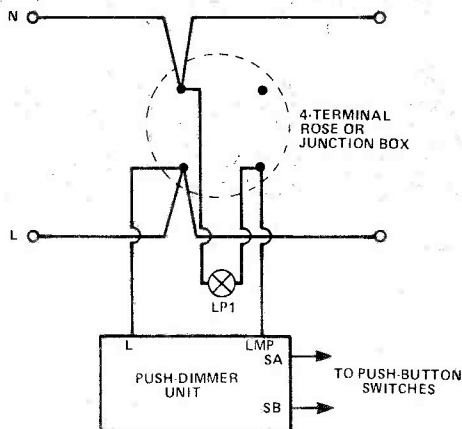


Fig. 10. The electrical circuit that is used in 3-way light switching.

Lighting Circuits

A major deficiency of 'modern' lighting systems is the physical difficulty that is involved in initially installing the light switch wiring or in converting the system to multi-way switching. An ideal '1980s' solution to this problem is offered by the push-button-activated lamp dimmer/on-off circuit of Fig. 11.



Note that the control (push-button) switches of the above circuit carry maximum currents of only a few mA and that any number of switches can be wired in parallel, enabling multi-way control to be readily implemented.

Ideally, this unit should be connected into the house wiring in a position that is close to the 4-terminal ceiling rose (but readily accessible for maintenance purposes): the push-button control switches should then be installed in the desired 'wall switch' positions and connected to the unit via low-power twin flex, shallowly buried in the plaster.

Note that the circuit uses components L1 and C1 for RFI suppression. All lamp dimmer circuits generate substantial RFI and should therefore incorporate suitable suppression networks: in practice, the very limited size of the conventional 'plaster-depth switch box' precludes the fitting of suitable filters, so most of today's 'manual' dimmer circuits generate unsuppressed RFI. A major advantage of the remote-controlled dimmer/on-off circuit of Fig. 11 is that its physical size is not significantly constrained, so excellent filtering can readily be incorporated.

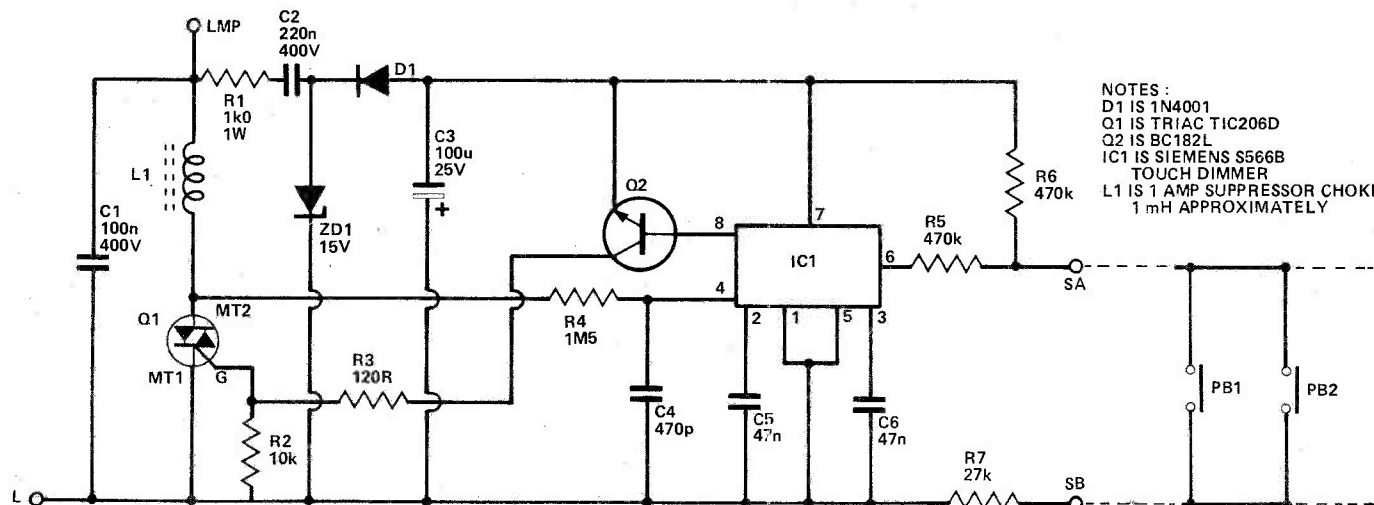
Practical Rewiring Hints

Electrical re-wiring is a technically simple but physically arduous and time consuming task. Floor boards have to be raised to gain access to the wiring and holes have to be drilled through joists and beams to facilitate wiring runs: plaster has to be channelled to accept new cable runs and must be remade afterwards.

Essential tools for the job include 2½" bolster chisels, a lump hammer and a decent power drill. Before starting the job, plan your new wiring layout with care, giving thought to the sensible positioning of new power sockets, light switches and ceiling roses. Your task may be simplified by using the conduit of the old wiring system.

Figs. 12 to 14 show some useful rewiring aids. The Fig. 12 and 13 circuits are used for tracing old wiring and conduit. The Fig. 12 wire tracer works on the magnetic-field detection principle and is used to trace 'live' wiring. The Fig. 13 circuit acts as a simple 'metal' detector and is used in conjunction with a hand-held pocket radio to trace cables, conduit and

Fig. 11. This push-button-activated dimmer/on-off unit (below) can accept any number of parallel-connected inputs and offers a state-of-the-art solution to the multi-way light-switching problem. The unit can be wired into the domestic lighting circuit (left).



plumbing. These two circuits are described in greater detail in the June '79 issue of ETI.

Finally, the Fig.14 'marker beacon' circuit is useful for indicating the loft or under-floor break-through positions of pilot holes drilled through ceilings when installing new feeder cable runs or when re-positioning ceiling roses.

The cable used for rewiring will be 1.0 mm T & E for the lighting circuits, 2.5 mm T & E for power rings and 4 mm T & E for the ring feeders. All metal switch boxes and metal conduit, etc, must be earthed; the earth cable must be connected to the earth line of the mains feeder into the house.

Fig.12. This wiring tracer works on the magnetic-field detection principle.

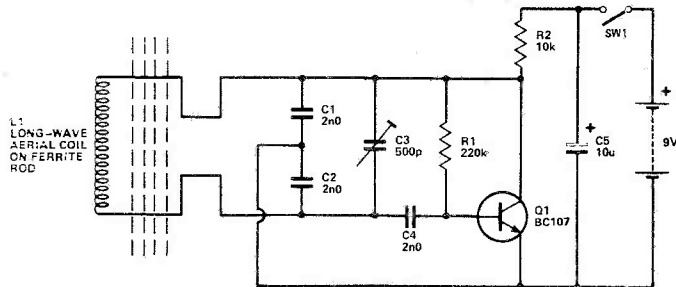


Fig.13. Circuit of a simple BFO-type mains and plumbing seeker; the unit is used in conjunction with a hand-held pocket radio.

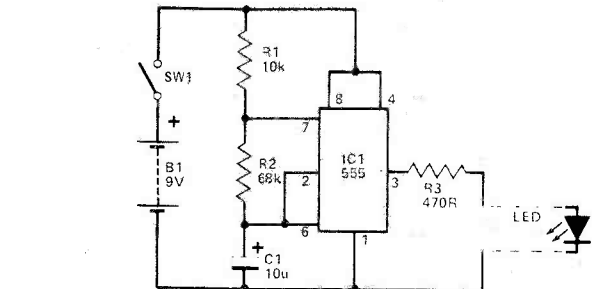
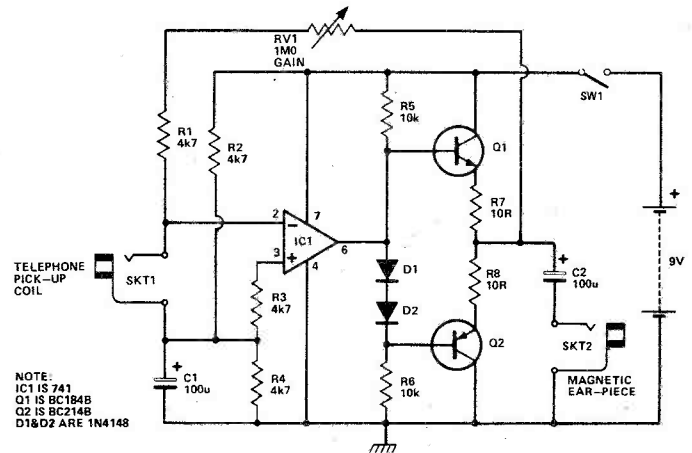


Fig.14. This 'marker beacon' circuit can be used to indicate the position at which pilot holes break through into dark places.

ETI

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0.8-9, 0.8-9	500 500	207	2.70	.70
0.8-9, 0.8-9	1A 1A	208	3.80	.70
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6	3	70	5.55	.90
8	4	108	7.40	1.15
10	5	72	8.20	1.15
12	6	116	8.80	1.15
16	8	17	10.80	1.25
20	10	115	13.80	1.45
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30 VOLT (Pri: 220-240V)

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6.0	117	11.05	1.15
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1.0	103	4.55	1.00
2.0	104	7.25	1.15
3.0	105	8.55	1.15
4.0	106	10.80	1.25
6.0	107	15.05	1.45
8.0	118	20.15	1.65
10.0	119	24.05	2.15

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Amps	Ref. No.	Price £	P&P
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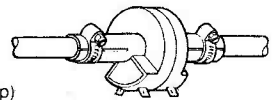
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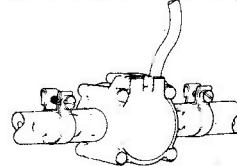
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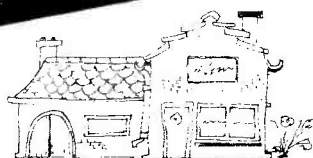
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ETI6



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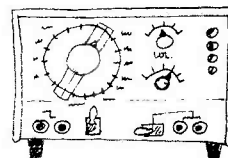
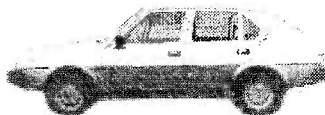
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AUDIOPHILE

Lost in a haystack full of needles (stylis?) Ron Harris presents a review of Shures new M97 cartridge range and compares two other two moving-magnets from Stanton and Ortofon.

I have to start this month with two apologies. The first goes to Videotone who had two pieces of equipment in my £300 system a while back. Seems that while the issue was going to press, they had their bright idea of going direct mail-order, with the result that their prices took a tumble. Being nice helpful people they rang me up to tell me this of course, but being the worlds worst file keeper I promptly lost the piece of paper with the facts scrawled across its tatty, crumpled face.

So, a little belatedly I admit, I have the somewhat unusual task of reporting a price FALL. GB2 loudspeakers can be purchased now for £60 and not the £100 or so they used to cost. The Coral 555E cartridge also comes down, from £25 to around £14. Good news indeed for those shopping in that area and reason enough for me to begin filing things properly.

My second apology goes to everyone, including me, who has the sense of beauty to appreciate the lovely Felicity Kendall. Last month's Audiophile was *supposed* to contain an excellent photograph of the lady, provided by Mr. Rickwood. Sometime between leaving my desk, bound for our printers, and reappearing in the issue, someone or something GOT to it, thing GOT to it.

When I find out *who*, there will be set abroad in the night such things that the miserable wretch will lie shivering and cowering in his repentance

Tale Of Four Cartridges

To hear some of the disciples speak, you could be excused for thinking that moving-coil cartridges were the only things fit to waggle a cantilever across a record. There are, however, not a few companies still producing some excellent units in the higher price brackets, whose coils remain remarkably static.

Immediate claims to such fame could be made by Shure, Goldring, Stanton, Ortofon, Empire and Grado. Units which earn such accolades might be V15 IV, 900 IGC, 881S, LM30, EDR9 and G2. Might be. That is what I determined to find out. The first two units, the Shure and Goldring, will be no strangers to Audiophile readers as both have been reviewed herein already. This month I have a report on the Stanton 881S and the Ortofon LM30H — SME style. Empire were invited to participate but still had not supplied an EDR9 by the time this magazine went to press. Should they ever awaken down there and one appears over my horizon you'll be hearing about. Until then — a pity.

As more than adequate compensation I can offer a first-ever review on two of the new Shure M97 series of pickups — the top model, the 97HE and the middle of the road M97EJ. Let's start with these Shures then.

V15's For All?

This new range from Shure is based upon the technology of their V15 IV model. All inherit the "dynamic stabiliser" affair from their predecessor — a carbon fibre brush set in damped pivots which rides ahead of the stylus and provides a

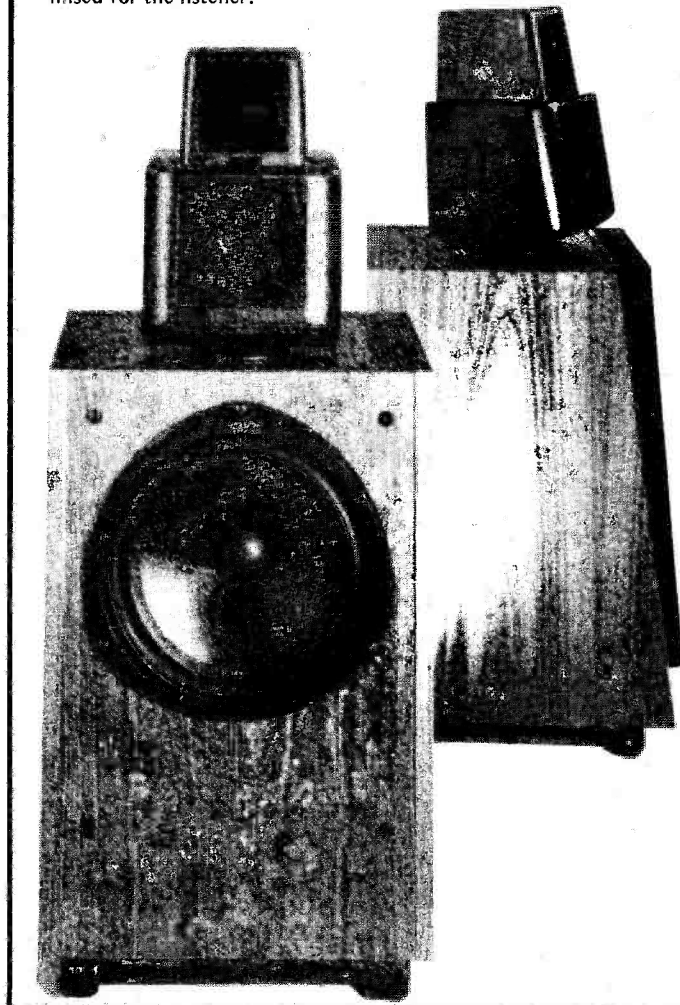
good deal of isolation from shock — and the 97HE model even has the same stylus contour as the V15 itself.

A feature which I am positively NOT going to test is their 'side-guard'. Shure claim that a 'lateral deflection assembly' allows the cantilever to accept impact in a sideways direction without damage, with the stylus simply withdrawing into the cartridge body. This might occur, say, when the cartridge hits the side of an LP accidentally, or is knocked across a record. Shure — I'll take your word for it, my courage fails me.

These are large cartridges, which look superb set up (in any arm). As usual for Shure the packaging and presentation is magnificent and the finish on the cartridges faultless.

The HE will take its place beneath the V15 IV in Shure's range, but with the incredible number of cartridges Shure now have on the market, it is difficult to be sure — and they show

Audiophile has acquired a new pair of reference speakers — KEF 105 II's, shown below and (in cutaway) right. These are probably the best speakers on the market today for home use. As you can see the 'head' contains the mid-range and HF units, each in its own little enclosure. This can be tilted and turned through a limited angle laterally, such that the stereo image can be optimised for the listener.



no signs of rationalising. More power to them if they can sell them all.

It should be said, though, that this M97 series is a significant step ahead of their other ranges in terms of sound quality and should outsell them all with ease. Originally I hadn't intended to include either of these two models in with the Stanton and Ortofon — after all the price is noticeably lower — but the HE performed well enough for me to think it worthwhile. In fact one of the surprises awaiting me amid this forest of cantilevers, was how close the M97HE came in performance to the exalted V15 IV!

Shure-fire Test?

Under test conditions both the M97s proved themselves worthy of their pedigrees. Both are top-flight performers in their respective classes and in fact the EJ is capable of tracking higher recorded velocities than the HE — but at a gram more weight. The HE cleared all my traps at 1g actual tracking force (the brush means that you set up for 0.5g more) and the EJ had an optimum force of 2.2g. Have a look at the table for more details of the results.

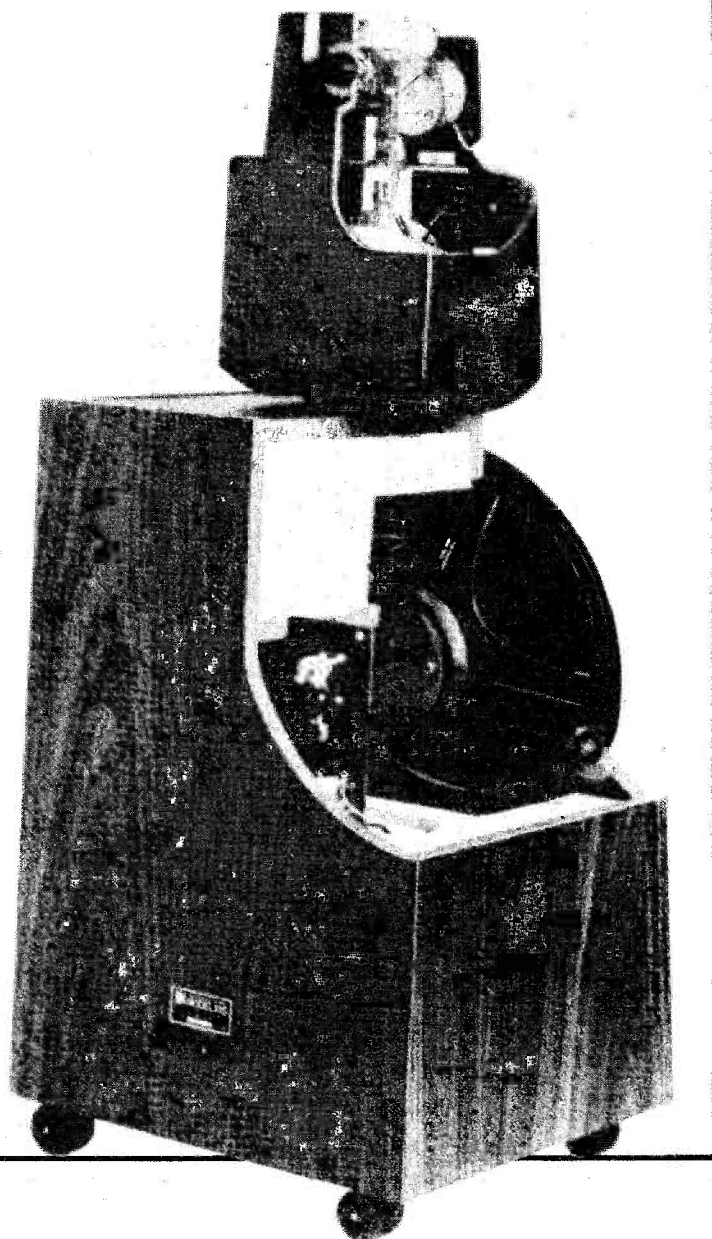
(Throughout these ramblings, "optimum tracking force" is that downforce at the stylus above which no improvement in tracing ability is obtained for increased weight). The 97EJ gave a creditable account of itself all around. Set up in a JVC QLA5R deck it performed very competently and gave a good

solidity to the sound, with a warm balance and smooth treble. It would match most good loudspeakers in the £100–£200 class that exhibit a clean top and its powerful bass could be a decided asset, especially to impercunious rock fans.

On the debit side it has a tendency to impose too much of itself upon the music at times and could be tipped over the edge into hardness (surprisingly) by very complex material. Still, these are minor effects — and more minor than you'd expect at the price. Not a serious worry and overall a good design, one which does credit to its designers.

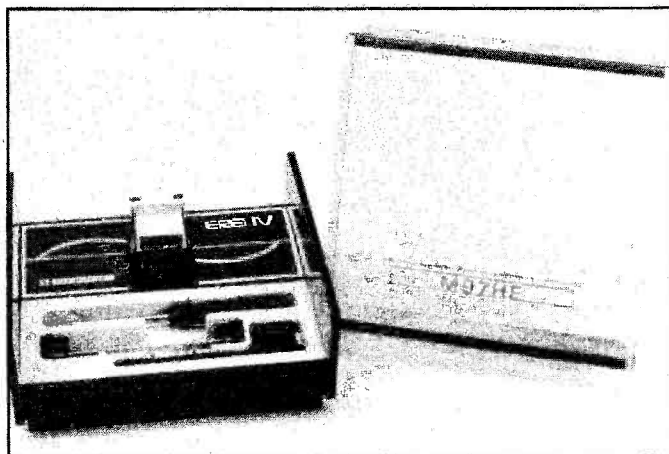
Set up in an SME III the M97HE played very well with all types of music. It is a good cartridge by any standards, having a smooth easy-to-listen-to approach to its task, and is tolerant of material of lesser stature than itself. As I said earlier it is very difficult at times to distinguish this pickup from the V15 IV — it has that same confidence in its own infallible tracking ability, never putting a diamond wrong. Distortion is low and the base possesses a good punch. Detail is well portrayed, but it is here that the V15 shines through with superior mid-range quality. A more refined performance is bought with the extra cash, it seems.

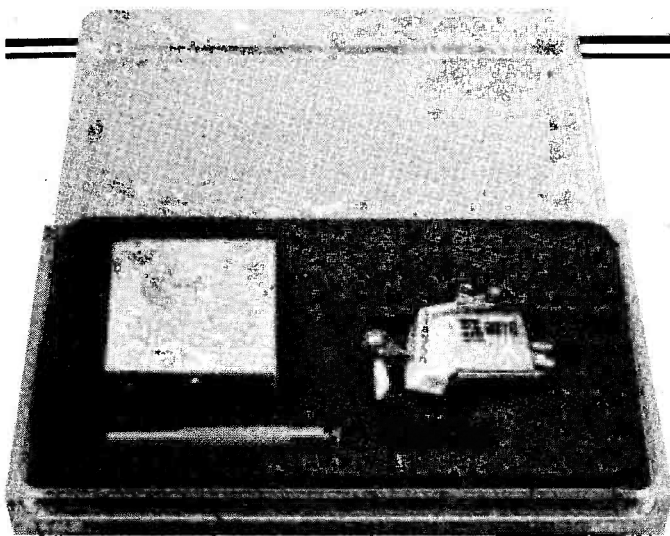
It would take a good system to justify the classier performance though, a careless matching of components could easily obscure the differences. Good enough then, I thought to bear comparison with the Ortofon and Stanton and so included the M97HE in the tests, about which you'll be hearing more later. Remember the price difference though.



Above: the Shure M97EJ and, below, the M97HE still reclining in its box. Both the cartridges are identical in appearance — so there was little point in showing photos of them both!

Note the dynamic stabiliser clipped down into position as a stylus guard on the EJ.





Stanton On It's Merits?

The Stanton 881S. Doesn't seem so long ago that the 681 and V15 III were considered the two best cartridges around — long were the nights spent arguing over the relative merits of the pair of them.

Stanton seem to have taken something of a low profile lately and this unit has never received the publicity it deserves. Having now auditioned it at greater length, I feel it has a lot to offer, albeit with a few vices amongst its virtues.

The 881S is also very well presented and its appearance is very striking indeed, with the silver finish and white stylus carrier. All preceded, of course, by the inevitable brush — and this I cannot refrain from condemning, both as a cleaner and an aid to the cartridge as a whole. Thank decibels it is at least removable.

At a time when great effort is being expended to *remove* static, and to ground any charges present on records; listen to Stanton's own description of how the brush does its work: —

"It operates on the principle that the rubbing action of the nylon bristles against the vinyl record surface creates an electrostatic charge which attracts dust particles like a vacuum cleaner".....Oh.

I'll bet it does. And charges up the record surface nicely too. (Dust sticks to LPs very well under charge conditions.) The stylus is trailing along just behind the brush — straight into that charged patch of vinyl prepared for it. What odds on increased snap, crackle and pop? Why, why, why, why, when you have a pickup this good, lumber it with a built-in static generator? I despair of humanity sometimes, I really do.

This is a well engineered unit, as the test results prove. Channel balance is beautifully maintained and resonances tightly controlled. As is Stanton's way, the cantilever is amazingly short and durable. The mass, minus brush, is about average.

The sound of the 881S is best described as rich and detailed. There always appeared to be a lot going on in the music, with the cartridge obscuring little of it. The bass is good but not as extended as it might be. Mid-range is sharp and clear but can be a little *too* sharp in the 2kHz — 5kHz range at times. Treble was well extended and crisp and overall the sound was well balanced and exciting to listen to.

A cartridge more than worth its asking price, but capable of being improved still further, I feel.

Ortofon/SME 30H

Now this is something really different. Part of the new ultra-low mass range from Ortofon, the Ortofon/SME 30H is the LM30H cartridge adapted for use with an SME Series III pickup arm. Adaptation here means 'building into'. A normal

Left: the Stanton 881S in its plush little box. That relatively huge container holds the fixing hardware for the Stanton cartridge, and everything else you want to hold in the headshell. What looks like a police whistle, in the foreground, is in fact a screwdriver. Very nice presentation.

CA1 arm has been shorn of headshell, and the 30H fitted as part of the new one.

The overall effect is to bring down the effective mass of cartridge and arm to 4.2g and create the most striking pickup around. It looks superb in operation.

Low mass like this has great advantage in the bass registers. Used in the SME, the system resonance — the frequency at which it is easiest to put a peak in the response — lies at 13Hz, which is too high to be effected by record warps, or ripples and too low to let acoustic feedback from the speakers influence it.

So much for the theory of it, in practice we have a very attractive, pencil slim, cartridge with built-in finger lift. Just about every aspect of operation has been well thought out. An alignment tool is provided for setting up the individually shaped cartridge for vertical tracing angle. Without it, it would be virtually impossible. Even the stylus guard will help with lateral balance adjustments! (Try and work *that* one out.)

In play the Ortofon proved to be as much of a contrast to the Stanton in sound as it had been in looks. The bass was nothing short of phenomenal. The extension went way down, more importantly though the energy was controlled very well, with no sign of looseness or tendency to 'boom'. The low mass and integrated head were responsible for this, I think. The mid-range was restrained but open. No sign of brightness or sharpness here. Some people would think it too bland I suppose, but then since when does 'neutral' mean 'striking'?

Overall the Ortofon presents a smoothly blended face to the world, with perhaps a slight veiling of the extreme high frequencies.

If ever there was a cartridge that was at home with a certain type of music, it is this one. On classical music of the symphonic variety, the Ortofon really soars. Things simply sound "in place" and natural. It is probably the best pickup I have ever heard on this type of material. The difference between its performance with say, Wagner and with the Floyd is very marked and not a little puzzling. On the former it is staggeringly good, on the latter — simply good.

Listen Here

It was this which started me off on what developed into a full blown comparison session, with the resultant exponential increase in people, equipment and headaches. All though the listening so far I had been using my usual cartridge as a reference against which to measure the others, simply because I am well used to it and know its foibles well enough.

The pickup in question is a Coral MC81 moving coil, which I have been in love with ever since reviewing it in these pages many LPs ago. I consider it one of the best around at any price and as it costs only about £48 these days, affording a head-amp is not the bank-robbing job it might be.

Anyway I digress. What transpired in the end was that I set up a listening -panel type of comparison between the Stanton, Ortofon, Shure M97HE and the Coral as reference.

I have not the space, or inclination, here to go on about the steps taken to ensure impartiality. They were taken, believe me. If you don't you're probably a PE reader anyway!

The rest of the disc playing system comprised. Technics/SMEIII configurations feeding a Lecson amplifier and being relayed to the waiting ears by that same pair of KEF 105 II loudspeakers. Some use was also made of a Sony TCK 55 II cassette.

Right: and below is the amazing Ortofon SME 30H. As you can see there is no real head-shell, just the cartridge itself. The unit looks extremely elegant in use, but the one thing they don't tell you is that it is so light that you need to remove ALL the lead weights from the SME III to balance it -- which means that you need more spacers.



After it was all over I took the scores, and 'normalised' the reference at 15 for everything, adjusting the other scores to create the (average) figures obtained below. (Table Two)

Material varied from Wagner to Rickie Lee Jones, via Grieg, Holst, Stravinsky, Thelma Houston, Sky, Alan Parsons and the inevitable Pink Floyd. Each listener was asked to mark the cartridge playing, out of 20, on the parameters shown in Table Two, without knowing which unit was operating.

Not much to choose really is there? The Shure comes out least well, but then its price bracket lies well below the other two and this is in reality a creditable showing indeed. As such I can confidently recommend both examples of the M97 range, secure in the knowledge that few (if any) will be disappointed with the purchase. Yet another nice one Shure.

The Stanton and the Ortofon are a different matter. Both provide ample evidence of the excellence obtainable

from moving-magnet methods, but are totally different in their sound balance.

They scored identically in this respect in the test, as you can see, so both are appealing designs.

The Ortofon is to be preferred for classical material and the Stanton for rock. Perhaps that, undoubtedly over-simplified statement is as close as I'll get to defining the differences for you. Comparing the two is entertaining stuff -- try it yourself if you plan to spend around £80 on a cartridge. The time will not be wasted and neither will the money!

Back to amps next month, with a look at an offering from Quantum Electronics. Their 102 pre-amp matched to the 110W per channel 204 power amp. You can obtain the units as either kits or ready-built equipment and amplifier modules are available separately. The main question is though -- what do they *sound* like?

Table One

	Stanton 881S	Ortofon/ SME 30H	Shure M97HE	Shure M97EJ
Output : 1kHz 5cm/sec	5mV	3.2mV	4.5mV	5mV
Channel Balance	< 1.5dB	< 2dB	< 1.5dB	< 2dB
Optimum tracking force	1.1g	1.3g	1g	2.2g
Frequency Response Limits, 20Hz-20kHz	±1dB	±2dB	±2dB	±2dB
Separation (LonR) 1kHz	32dB	30dB	35dB	28dB
Cartridge Weight	6.7g (inc brush)	10.5g (inc arm)	6.4g	6.4g
Recommended Loading	47k // 275p	47k // 400p	47k // 250p	47k // 250p
Typical selling price	£80	£85	£45	£27

Table One: objective test results. Note the Ortofon specified load is a good deal higher than normal, and a padding capacitor could be used to advantage here. Although its mass looks higher, it includes the pickup arm -- effective mass is actually close to 4g, well under the figures for the rest of the pickups.

Table Two : subjective results. These figures are the arranged responses gleaned from the listening panels individual markings.

Table Two

	Bass Extension	Bass Quality	Mid-range Quality	Rendition of Detail	Balance of Sound	Treble Extension	Treble Quality	Neutrality
CORAL MC81	15	15	15	15	15	15	15	15
STANTON 881S	17	14	12	14	14	14	13	13
ORTOFON 30H	18	15	14	14	14	10	12	15
SHURE M97HE	18	13	12	13	13	14	13	13

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- FREE course in BASIC programming and user manual.

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*Use a 600 mA at 9 V DC nominal unregulated mains adaptor. Available from Sinclair if desired—see coupon.

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The Sinclair ZX80 is not just another personal computer. Quite apart from its exceptionally low price, the ZX80 has two uniquely advanced components: the Sinclair BASIC interpreter; and the Sinclair teach-yourself BASIC manual.

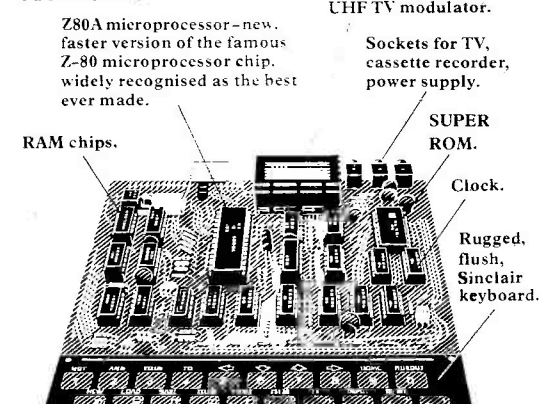
The unique Sinclair BASIC interpreter... offers remarkable programming advantages:

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ETI JUNE 1980

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Sinclair ZX80

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	Memory Expansion Board s. each one takes up to 3K bytes	12.00	
	RAM Memory chips – standard 1K bytes capacity.	16.00	
	Sinclair ZX80 Manual s. – manual free with every ZX80 kit or ready-made computer.	5.00	
NB. Your Sinclair ZX80 may qualify as a business expense.		TOTAL	£

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(ETI/6/80)

LINEAR OHMMETER

Well suited to either the lab or hobbyist bench this accurate little project will provide an inexpensive answer to many resistive problems.

This instrument is an inexpensive semi-precision ohm meter that can be used to give accurate readings of resistance from a few tens of ohms to one megohm. The unit has four decade ranges covering 1k to 1M full scale and has a full scale accuracy of 2% if low tolerance range resistors are used.

Conventional moving coil ohmmeters have non-linear scales which typically cover two to four decade ranges of resistance value on a single scale. With such a range of resistance it is impossible to obtain an accurate reading, especially at the higher values. To measure resistance values with reasonable accuracy, the usual method is to use a Wheatstone Bridge, often very expensive and time consuming.

By contrast, this ohmmeter gives resistance readings on a linearly calibrated scale and covers only a single decade of resistance on each switched range. The instrument thus gives inherently more accurate readings of resistance than multimeter type ohmmeters.



Construction

The ohmmeter can either be constructed as a completely contained unit, with its own moving-coil meter, as we have done, or it can be built as an add-on to an existing multimeter having a 1 mA DC range.

Take care with the polarity of the zener diode. The 301 op-amp cannot be substituted by a 741 as it has been selected for its low input current. The overall accuracy of the instrument is determined by the tolerance of the range resistors (R3 to R6) and the accuracy of the meter. If 1% or 2% resistors are used the accuracy of the instrument will be about two percent.

When the board assembly is complete, fit into the box and complete the wiring to the major components. If you are making an add-on version of the meter, fit a couple of screw terminals in place of the meter for connection to your multimeter.

Calibration

When construction is complete, switch the unit on and check that the LED lights up. If it doesn't, check the wiring and the polarity of the LED. When all is well connect an accurately known resistor (having a value within the range of the instrument) across the terminals and adjust the trimpot for the correct reading. The unit is then ready for use and should not require further calibration. You could purchase a 1k, 1% resistor specifically for this purpose.

BUYLINES

There are no components here which will prove difficult to obtain. Casing is not critical in the slightest, and all the mail-order advertisers within this issue should be able to provide all the bits and pieces required.

PARTS LIST

Resistors All ½W
(*see text)

R1	2k7 5%
R2	1k0 5%
R3	1k0*
R4	10k*
R5	100k*
R6	1M0*
R7	560k 5%
RV1	5k0 (minimum) vertical

Capacitors
C1

100p ceramic

Semiconductors

LED 1	TIL220
ZD1	5V1 400 mW
Q1	BC109, BC549
IC1	301

Miscellaneous

SW1 DPDT toggle switch, SW2 one pole four position wafer switch, M1 1 mA FSD meter, SK1, SK2 screw terminals.

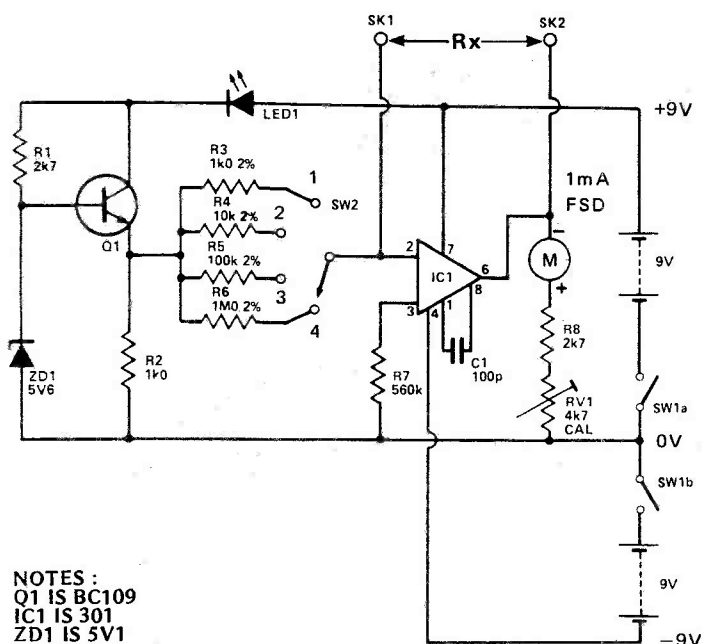
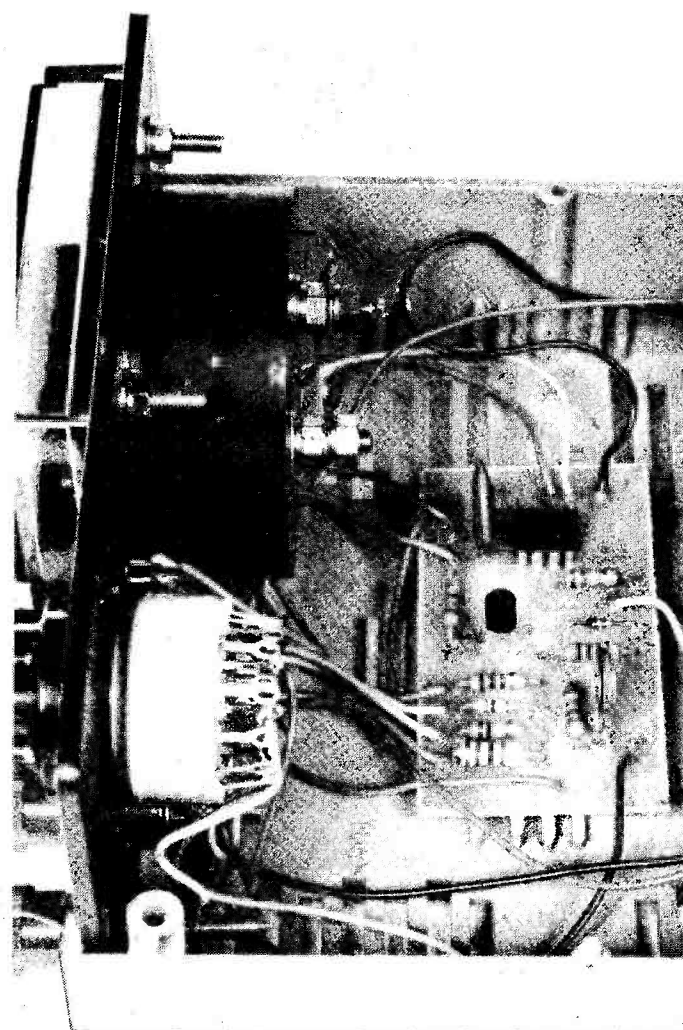


Fig.1. Full circuit diagram of the instrument.

HOW IT WORKS

The linear scale ohmmeter circuit is divided into two parts: a reference voltage generator and a readout unit that indicates the value of the resistor under test. The reference voltage generator section of the circuit comprises zener diode ZD1, transistor Q1, and resistors R1 and R2. The action of these components is such that a stable reference of about 5 V is developed across R2. This reference voltage is fed to the op-amp resistance-indicating circuit via range resistors R3 to R6.

The op-amp is wired as an inverting DC amplifier, with the 1 mA meter and R8—RV1 forming a voltmeter across its output, and with the op-amp gain determined by the relative values of ranging resistors R3 to R6 and by the negative feedback resistor R7. RV1 is adjusted so that the meter reads full scale when Rx has the same value as the selected range resistor. Under this condition the op-amp circuit has a voltage gain of precisely unity. Since the values of the reference voltage and the ranging resistors are fixed, the reading of the meter is directly proportional to the value of Rx, and the circuit thus functions as a linear-scale ohmmeter and has a full scale value equal to the value of the selected range resistor.



A peek inside at the PCB. Make sure it doesn't foul the range switch or meter.

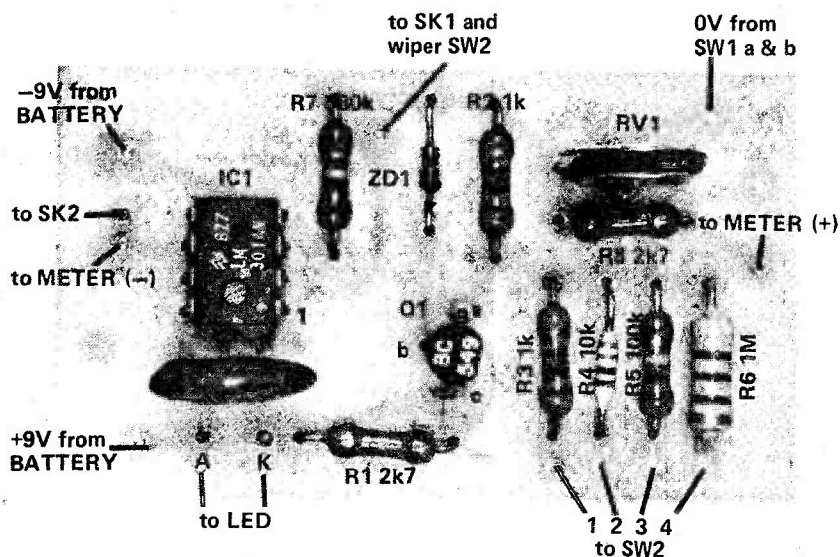


Fig.2. Component overlay.

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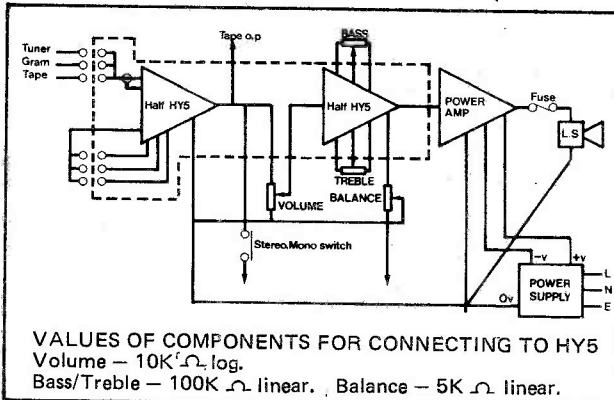
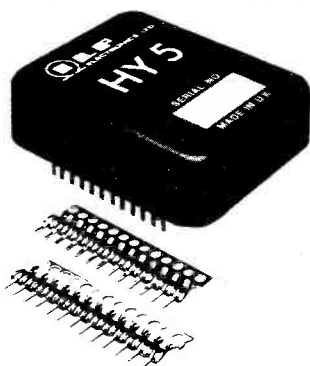
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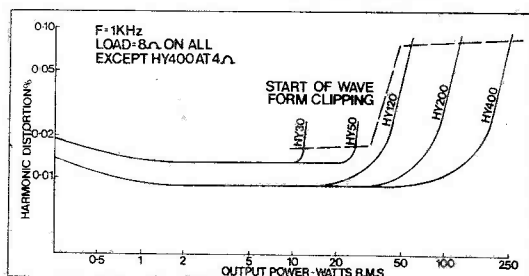
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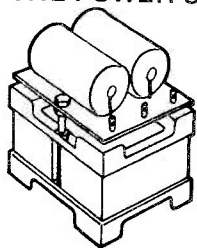
THE POWER AMPLIFIERS



Model	Output Power R.M.S.	Distortion Typical at 1KHz	Minimum Signal/Noise Ratio	Power Supply Voltage	Size in mm	Weight in gms	Price + V.A.T.
HY30	15 W into 8 Ω	0.02%	80dB	-20 -0 +20	105x50x25	155	£6.34 + 95p
HY50	30 W into 8 Ω	0.02%	90dB	-25 -0 +25	105x50x25	155	£7.24 + £1.09
HY120	60 W into 8 Ω	0.01%	100dB	-35 -0 +35	114x50x85	575	£15.20 + £2.28
HY200	120 W into 8 Ω	0.01%	100dB	-45 -0 +45	114x50x85	575	£18.44 + £2.77
HY400	240 W into 4 Ω	0.01%	100dB	-45 -0 +45	114x100x85	1.15Kg	£27.68 + £4.15

Load impedance — all models 4 - 16 Ω
Input sensitivity — all models 500 mV
Input impedance — all models 100K Ω
Frequency response — all models 10Hz - 45KHz - 3dB

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PSU 36	for 1 or 2 HY30's	£8.10 + £1.22 VAT
PSU 50	for 1 or 2 HY50's	£8.10 + £1.22 VAT
PSU 70	with toroidal transformer for 1 or 2 HY120's	£13.61 + £2.04 VAT
PSU 90	with toroidal transformer for 1 HY200	£13.61 + £2.04 VAT
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Next Month

The June issue will be on sale May 16th

THE RADIO CONTROL

Can it be true? Yes, of course it is, all the problems have been sorted out and next month we will be presenting what must be the last word in terms of simple to build, 2 channel proportional R/C systems.

The Tx, Rx units are based on just two, that's right, two, purpose-built ICs. External circuitry has been kept to an absolute minimum, consequently it will cost a fraction of a commercial system. Designed primarily for land-based vehicles, boats, cars etc it will enable even the most unskilled constructor to put together a really first-class R/C combo in just a couple of relaxed evenings.

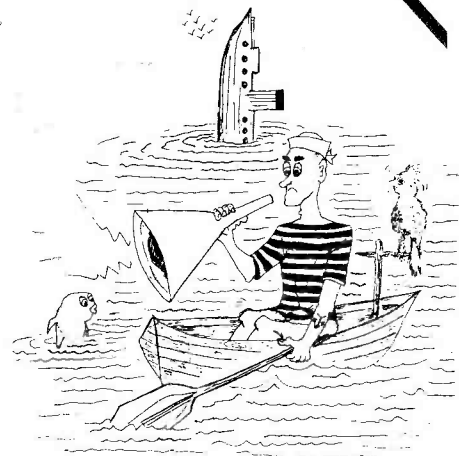
More than that we're not prepared to say, we are keeping the system under close wraps. We're sure it's going to revolutionise constructional radio control. Make sure you place your order early as the June issue is sure to be a sell-out. You have been warned!

CATALOGUE SURVEY

Do you buy components through the services of mail-order companies? If you do then you cannot afford to miss this survey into the various companies, the cost of their components, the service they offer and the quality of their catalogue. Who is the cheapest? Last year we came up with some pretty surprising results, find out if things have changed.

METRONOME

Don't miss a beat with this nifty, state-of-the-art little gadget. This revolutionary design has completely done away with cumbersome ICs. Yes, that's right, absolutely no Integrated Circuits. In fact we have used just four components and if that isn't state-of-the-art, what is?



FOG HORN

We're shore you'll build this circuit once you see it. But be warned your popularity will be at a very low ebb if you use it in the car. It is LOUD, very LOUD, so loud in fact, the only place you'll be able to use it is at sea.

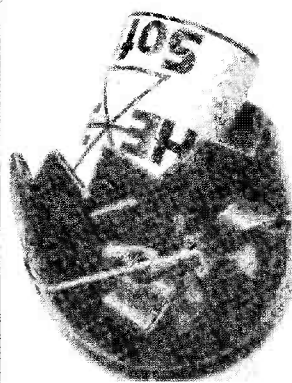
CITIZENS BANNED II

Next month is something of an anniversary for us. It will be exactly one year since we published our feature 'Citizens Banned'. In those twelve months we have carried the campaign for CB (sometimes struggling) into the open. Our petition (which around half our readers signed) gained Government recognition, generated national Newspaper, TV and Radio coverage and was the catalyst for forming CB clubs up and down the country. Something like 250 000 people are actively engaged in the campaign for legalisation MPs, Government Officials, Doctors, in fact everyone and anyone who wants the right for free speech.

In our second major feature we will be looking back over the past year and seeing how the campaign has fared.

EGG TIMER

Something really different for the gadget fans next month. Our Egg Timer is a solid-state version of the 'sand-in-a-glass' egg timer that has been around for hundreds of years. Shake it and set it down and depending upon whether you want a hard or soft boiled egg it will warble at the appointed time. No switches to worry about, is it magic? Find out next month.



POWERFETS

Some day all power transistors will be made this way

	CHAN	VDS max V	ID max A	PDISS max W	RDS(on) Type Ω	Case	Price
BD512	P	60	1.5	10	†(3.5)	T0202	85p
BD522	N	60	1.5	10	2.5	T0202	80p
VMP4	N	60	2.0	25	2.0	380-50E	1250p
VN10KM	N	60	0.5	1.0	4.0	T092†	55p
VN64GA	N	60	12.5	80	0.3	T03	750p
VN67AF	N	60	2.0	15	2.0	T0202	75p
2SJ49	P	140	7.0	100	1.0	T03	395p
2SK134	N	140	7.0	100	1.0	T03	395p

†1/p protected †our selection. VN/VM, 96-page Design Cat. 20p. Heat clips T0202 12p, T092 8p.

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733	50p	2SC1775(A) 120v 50mA, 17p		
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DESIGNER'S NOTEBOOK

Project editor Ray Marston discusses the uses and practicalities of voltage regulator circuits.

One of the most common and mundane tasks facing the electronics engineer is that of designing voltage regulator circuits, ie circuits that produce a stable and well defined DC output voltage over a wide range of load current variations. These circuits may vary from simple Zener networks, designed to provide load currents up to only a few mA, to fixed-voltage high current units for powering logic boards, etc, or to variable-voltage high current units designed to act as general-purpose pieces of test gear.

Zener Based Circuits

A Zener diode can be used to produce a fixed reference voltage by using the connections shown in Fig.1. Often, the supply voltage (V_{in}) may be subject to fairly wide variations, causing the Zener current to vary over a similarly large range. As long as V_{in} is always more than a few volts greater than the Zener voltage and provided that the Zener power rating is not exceeded this variation has only a moderate influence on the output voltage of the Zener, which typically has an effective output impedance of a few tens of ohms.

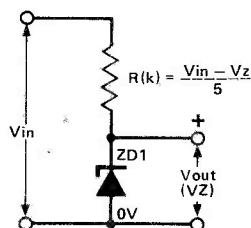


Fig.1. This basic Zener 'reference' circuit is biased at about 5 mA. A current of roughly 5 mA is passed through the Zener diode from the supply line via limiting resistor R.

A Zener can be used as a very simple voltage regulator, providing load currents up to a few mA, by merely selecting the value of 'R' as shown in Fig.2.

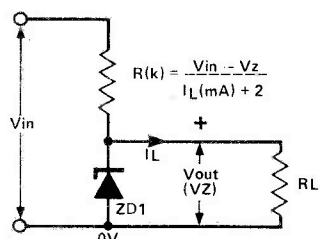


Fig.2. This basic Zener 'regulator' circuit can supply load currents of several milliamps. When the maximum load current is being drawn only 2 mA flows through the Zener. When zero load current is being drawn the Zener passes 2 mA plus the maximum designed load current and thus dissipates maximum power.

In most practical voltage regulator applications the Zener is simply used to apply a 'reference' voltage to a high-gain non-inverting buffer amplifier, which then supplies the required output power. The simplest example of this type of circuit is shown in the series-pass regulator circuit of Fig.3.

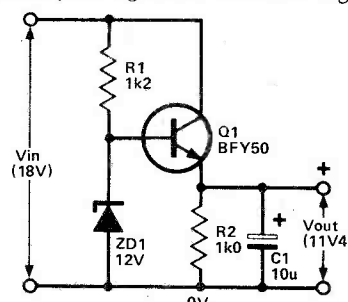


Fig.3. This series pass Zener-based regulator circuit gives an output of 11V4 and can supply load currents up to about 100 mA. Q1 is wired as a voltage follower, its emitter remaining at about 600 mV below its Zener-defined base voltage under all loading conditions. The Zener network provides the base drive current to Q1, this current being equal to the output load current divided by the current gain of Q1. Clearly, the higher the gain of the Q1 'buffer' stage, the better will be the output regulation of the circuit.

Op-Amp Regulators

One way of improving the regulation of the Fig.3 circuit would be to use a Darlington or Super-Alpha pair of transistors in place of Q1. An even better solution is to use the op-amp plus transistor buffer stage shown in Fig.4.

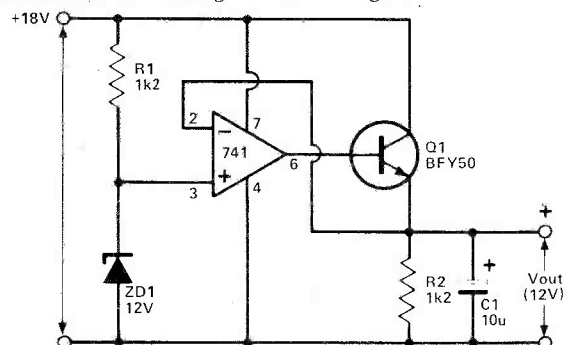


Fig.4. This op-amp based regulator gives an output of 12 V at currents up to 100 mA and gives excellent regulation. The op-amp and Q1 are interconnected as a unity-gain non-inverting DC amplifier with an overall current gain of about one million. The output voltage tracks within a few mV of the Zener reference value and the output impedance is less than one milli-ohm. The safe output current driving capacity of the circuit is limited to about 100 mA by the power rating of Q1; higher currents can be obtained if Q1 is replaced with a power Darlington transistor.

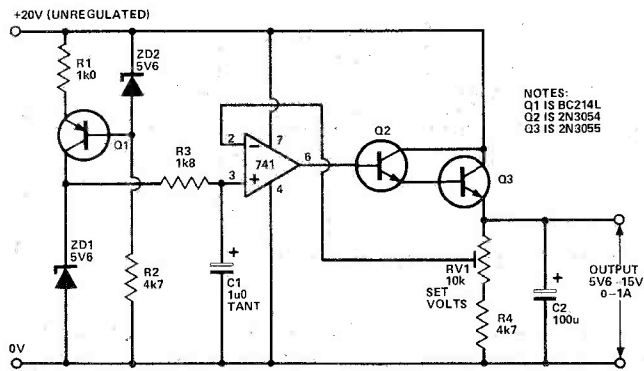


Fig.5. This variable-output 0-1 A circuit gives excellent regulation.

The performance of the basic op-amp circuit of Fig.4 can be improved in a variety of ways, some of which are shown in Fig.5. The first improvement that can be made is to make the Zener reference voltage (ZD1) independent of supply voltage variations by powering ZD1 from the output of constant-current generator Q1-R1-ZD2-R2. Next, the Zener noise can be eliminated by feeding the reference voltage to the op-amp via low-pass filter R3-C1. Thermal drift effects can be eliminated by making ZD1 a 5V6 type, with near-zero (actually about $-0.2 \text{ mV}/^\circ\text{C}$) temperature coefficient; the op-amp output voltage can then be set to the desired value (greater than 5V6) by using feedback components RV1-R4 to set the op-amp's voltage gain at some appropriate value.

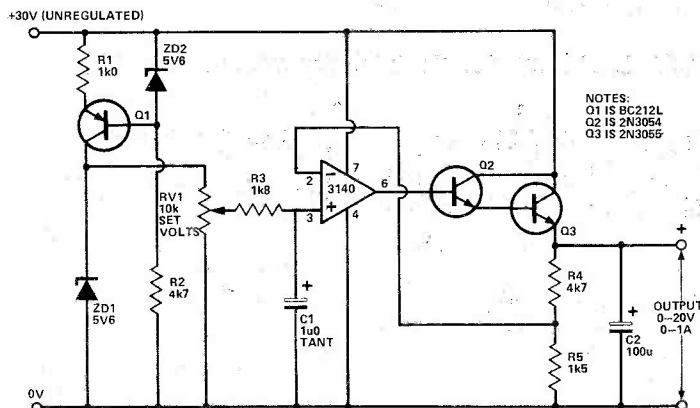


Fig.6. The output of this circuit is fully variable from zero to 20 V. The effective reference voltage is made variable from zero to 5V6 via RV1 and the op-amp is given a fixed voltage gain of about four via R4-R5. Note that a CA3140 op-amp, which can handle input signals down to ground volts, is used in this application.

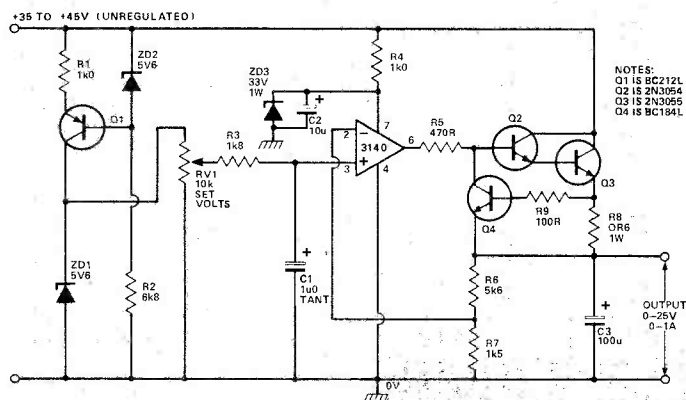


Fig.7. This 0-25 V, 1 A regulator has current limiting in its output stage with short-circuit or overload protection via Q4 and load-sensing resistor R8. The op-amp is protected against excessive supply rail voltages via R4 and ZD3.

Finally, the load current capacity of the circuit can be set to a fairly high value by using a Darlington-connected power transistor in the series-pass output stage.

Three Terminal Circuits

Three-terminal regulators are remarkably easy to use, as shown in the basic circuits of Figs.8 to 10, which show the connections for making positive, negative and dual regulator circuits respectively; the ICs shown in these examples are 12 V units, with current ratings of one amp. Note that a 270n or greater disc (ceramic) capacitor should be connected close to the input terminal of the IC and a 10u or greater electrolytic to the output.

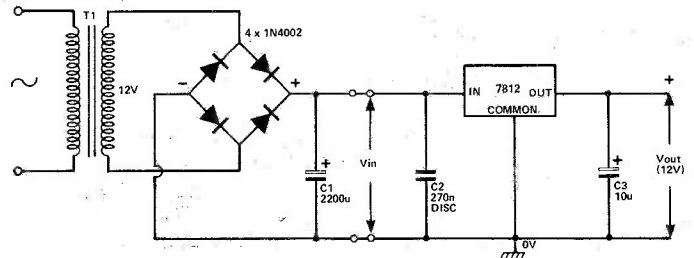


Fig.8. Connections for using a 3-terminal positive regulator IC, in this case a 12 V, 1 A type.

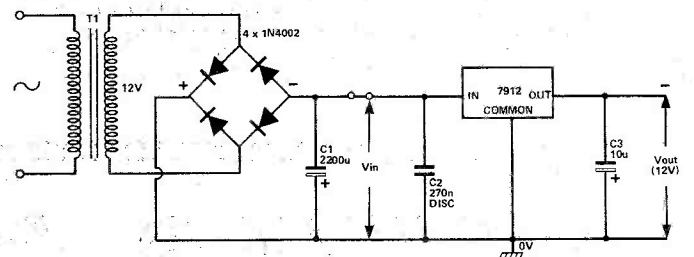


Fig.9. Connections for using a 3-terminal negative regulator IC, in this case a 12 V, 1 A type.

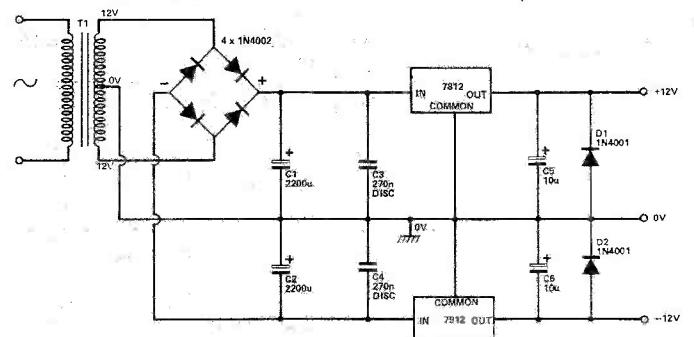


Fig.10. Complete circuit of a 12 V, 1 A dual power supply.

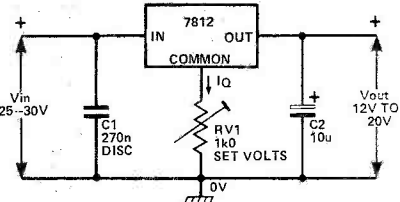


Fig.11. A very simple method of varying the output voltage of a 3-terminal regulator. The bias voltage is obtained by passing the IC's quiescent current (typically about 8 mA) through RV1. This design is adequate in most applications, although the output voltage obviously shifts slightly with changes in quiescent current.

The output voltage of a 3-terminal regulator is referenced to the 'common' terminal of the IC, which is normally grounded. Most regulator ICs draw quiescent currents of a few mA,

which flow to ground via the common terminal. The regulator output voltage can thus be raised above the designed value by simply biasing the 'common' terminal with a suitable voltage.

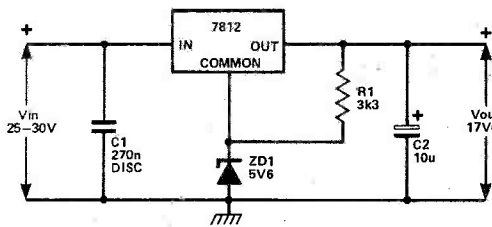


Fig. 12. The output voltage of a 3-terminal regulator can be increased by a fixed amount by wiring a suitable Zener in series with the common terminal.

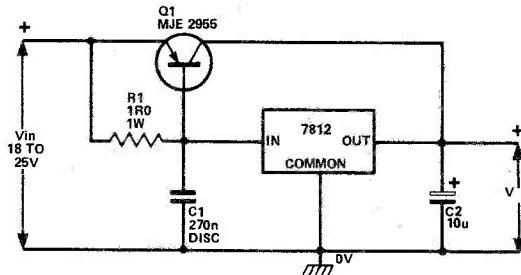


Fig. 13. The output current capacity of a 3-terminal regulator can readily be boosted via an external transistor. This circuit can supply 5 A at 12 V. At low currents insufficient voltage is developed across R1 to turn Q1 on and all of the load current is provided by the IC. At currents of 600 mA or greater sufficient voltage (600 mV) is developed across R1 to turn Q1 on, so Q1 provides all currents in excess of 600 mA.

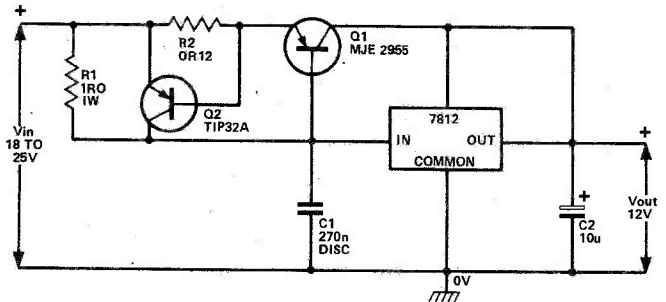


Fig. 14. This 5 A, 12 V regulator has overload protection provided via Q2.

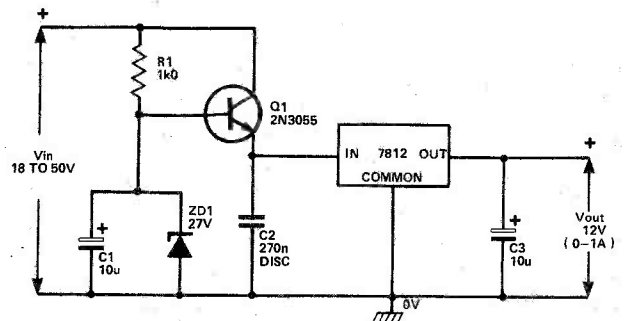


Fig. 15. This 12 V lamp regulator circuit is fully protected against excessive input supply line voltages.

ETI

Interface components

TRANSISTORS			OPTO			TRIACS			BRIDGES		
AC128	15p	BF200	29p	Leds		4A 400V	54p	with internal trigger diac.	74LS124	115p	
AC187K	30p	BF336	35p	125 Red	10p	4A 600V	60p		74LS132	89p	
AC188K	30p	BFX30	32p	125 Orange	10p	6A 400V	60p		74LS139	79p	
AC17	90p	BFX88	26p	125 Yellow	10p	6A 600V	60p		74LS151	89p	
AD149	55p	BFY50	13p	2 Red	10p	6A 600V	66p		74LS155	91p	
AF127	35p	BFY51	22p	2 Green	10p	6A 600V	66p		74LS156	89p	
AS17	120p	BFY64	28p	2 Clear	10p	8A 400V	66p		74LS157	89p	
AU113	150p	BFY90	56p			8A 600V	72p		74LS165	69p	
BC107	7p	BSX19	80p			10A 400V	72p		74LS168	139p	
BC108	7p	BSY95A	16p			10A 600V	84p		74LS174	99p	
BC108A	7p	BU204	149p			15A 400V	108p				
BC108C	7p	BU208	150p			15A 600V	126p				
BC135	15p	OC29	89p								
BC140	28p	OC43	50p								
BC141	30p	2N696	15p								
BC142	25p	2N930	20p								
BC143	28p	2N1132	19p								
BC147	6p	2N1304	40p								
BC147B	6p	2N1613	12p								
BC149	7p	2N1711	15p								
BC149C	7p	2N2217	20p								
BC159	9p	2N2219A	20p								
BC160	35p	2N2221	18p								
BC167A	10p	2N2368	15p								
BC178	12p	2N2369	14p								
BC179	12p	2N2894A	20p								
BC182	8p	2N2904A	15p								
BC182L	9p	2N2905	15p								
BC183	9p	2N2906	15p								
BC183L	9p	2N2926Y	10p								
BC184L	9p	2N2926B	10p								
BC186	20p	2N3442	102p								
BC212	9p	2N3702	8p								
BC212L	9p	2N3704	8p								
BC213B	8p	2N3705	8p								
BC327	13p	2N3708	8p								
BC328	13p	2N3709K	8p								
BC337	15p	2N3866	35p								
BC338	11p	2N3906	10p								
BC440	32p	2N4058	12p								
BC547	9p	2N4427	60p								
BC548	9p										
BC550	14p										
BC558	12p										
BCY33	99p	AA119	10p								
BCY34	99p	BA154	9p								
BCY39	229p	BA156	9p								
BCY58	16p	IN4001	4p								
BCY70	12p	IN4002	4p								
BCY71	12p	IN4003	5p								
BCY72	12p	IN4005	5p								
BF179	25p	IN4148	5p								
BF183	25p	IS44	3p								

DIODES			REGULATORS			TTL			CMOS		
AA119	10p		7805	57p		7400	9p		4000	14p	4072
BA154	9p		7812	57p		7401	9p		4001	14p	4073
BA156	9p		7815	57p		7402	9p		4002	14p	4076
IN4001	4p		7818	57p		7403	9p		4003	14p	4077
IN4002	4p		7824	57p		7404	10p		4004	14p	4081
IN4003	5p		7824	57p		7405	10p		4005	14p	4082
IN4005	5p		7824	57p		7406	30p		4006	14p	4160
IN4148	5p		7805	57p		7407	30p		4007	14p	4161
IS44	3p		7812	57p		7408	30p		4008	14p	4162
			7815	57p		7409	30p		4009	14p	4163
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			7824	57p		7494	30p		4094	14p	4248
			7824	57p		7495	30p		4095	14p	4249
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12 or 24 hour
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Time display



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Stainless steel. Mineral glass.
Water resistant. 5 YEAR BATTERY.

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83QS-41B Alarm Chronograph

S/S encased. Mineral glass. Water resistant. 3 YEAR BATTERY.

Hours, minutes, seconds, date, am/pm; or hours, minutes, alpha day, date am/pm. 24-hour alarm, hourly chimes.
Stopwatch from 1-10 second to 12 hours; net lap net lap and 1st and 2nd place. Nightlight.

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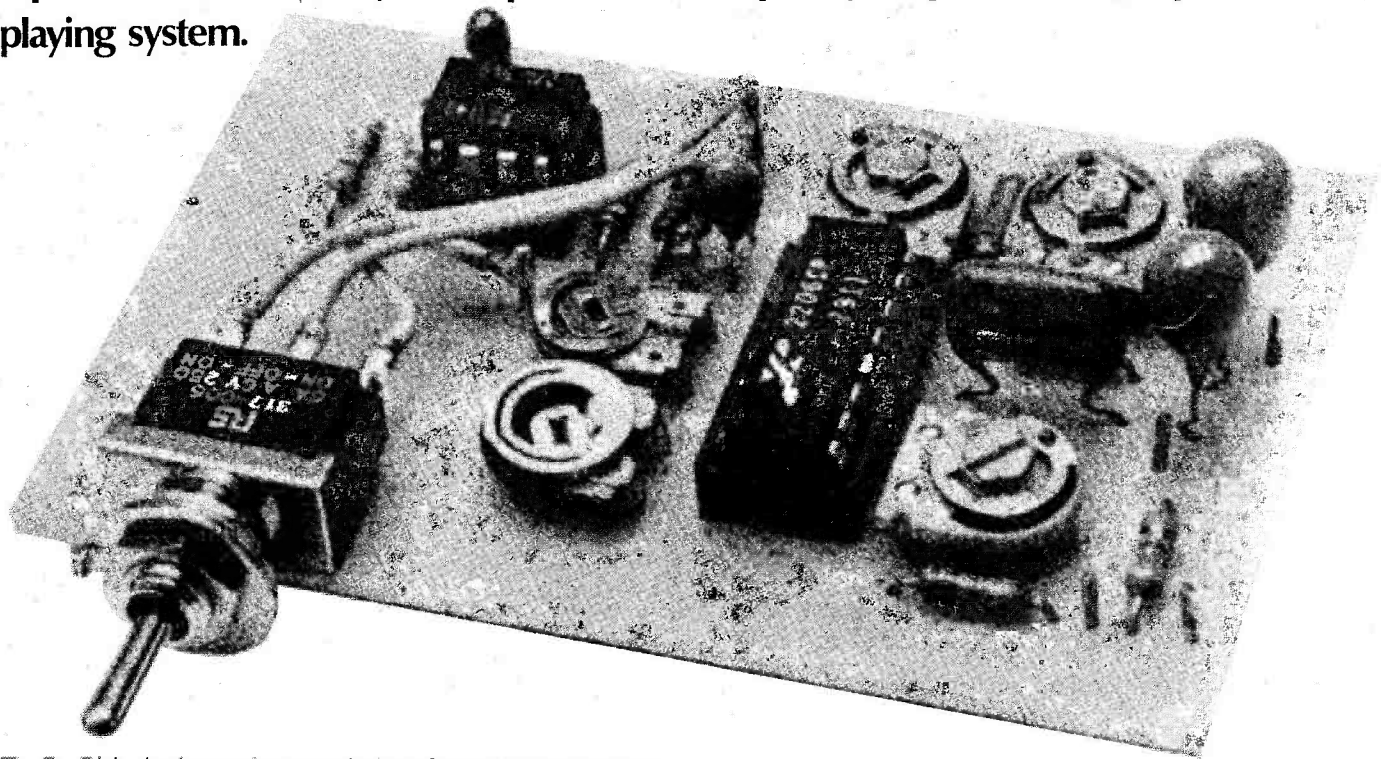
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TAPE RECORDER OPTIMISER

Don't be biased! Set up your tape recorder to make the most of those expensive tapes. This unit allows you to optimise the frequency response of any tape playing system.



With the increasing popularity of cassette tape systems, the search for perfect reproduction has led to the introduction of a wide variety of different magnetic media. Even when you use the correct tape for your machine, improvements to the sound may be made by slight adjustments of the bias control. Some decks feature this control on their front panels; even cheaper or older machines will have a bias preset potentiometer inside them somewhere.

Better Bias

This unit produces a 400 Hz and 8 kHz sinewaves of equal amplitude. By recording these using different bias settings, your system can be optimised for a maximally flat response or peaked for treble emphasis. The procedure is to record the two tones using a chosen bias setting then monitor the output levels on the VU meter. If desired, the bias can be adjusted to achieve the required response. If your deck does not feature a VU meter, you can use an oscilloscope instead. The high and low tones may be selected manually or will be produced alternately when the unit is switched to 'auto'. A frequency of about 0.3 Hz was chosen for this function. It can be simply altered by reselecting the value of C1.

Construction And Use

Our PCB design offers a convenient means of building up the unit (after all you need somewhere to put all those presets don't you!). Whatever method of construction you use, there are no special precautions to take except to watch out for the polarity of the semiconductors and tantalum capacitors.

An oscilloscope is an invaluable aid when setting up the unit. However, if one is not available, connect the output to a monitor amplifier and do it by ear. Preset RV5 should be set to mid position and RV3 to maximum resistance. With power applied, RV1 may now be adjusted to produce a 4 V peak to peak triangle waveform at pin 2, IC2. Then RV3 should be adjusted for the best sine wave. Small adjustments of RV5 may now be made to further improve the waveform. You should now have a fairly good sine wave of about 2 V peak to peak at pin 2, IC2.

The frequency of the two tones is set by adjustment of RV2 and RV4. A frequency meter makes this a doddle. If you do not have one, then R7, RV2 and R8, RV4 may be replaced by fixed resistors. The calculated values using C4, 10n are 250k (400 Hz) and 12k5 (8 kHz).

This simple project will help you get the very best from your audio system.

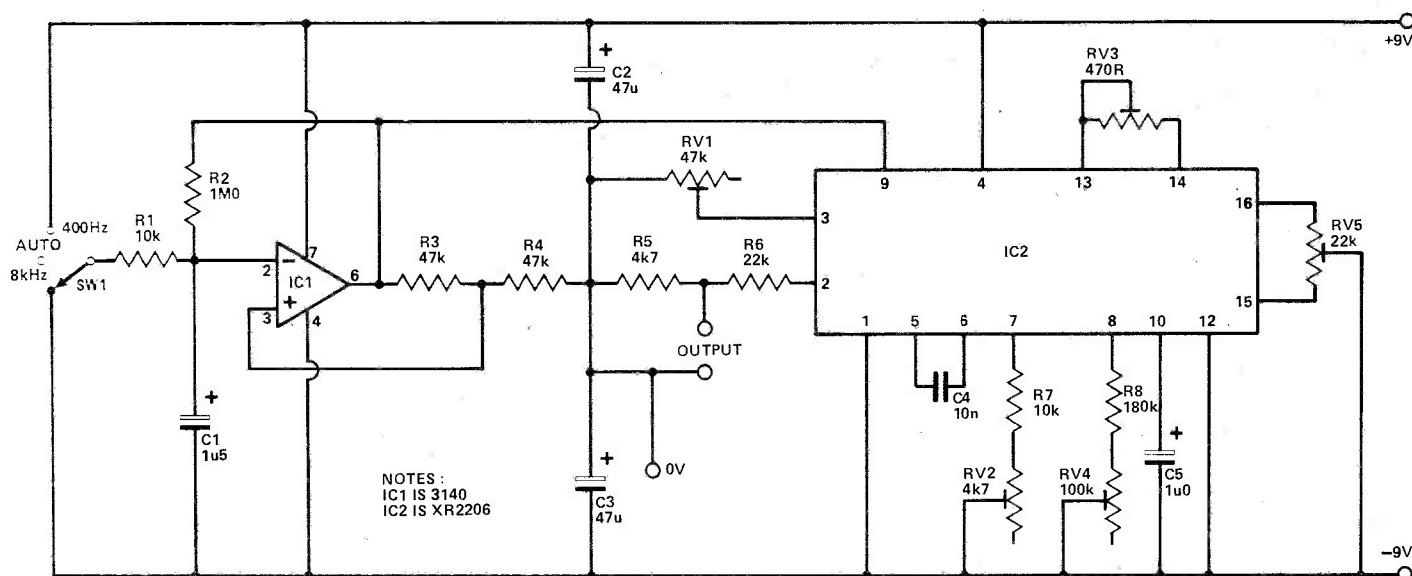


Fig.1. (above) Circuit diagram. RV2 and RV4 are used to set the frequency of the two tones.

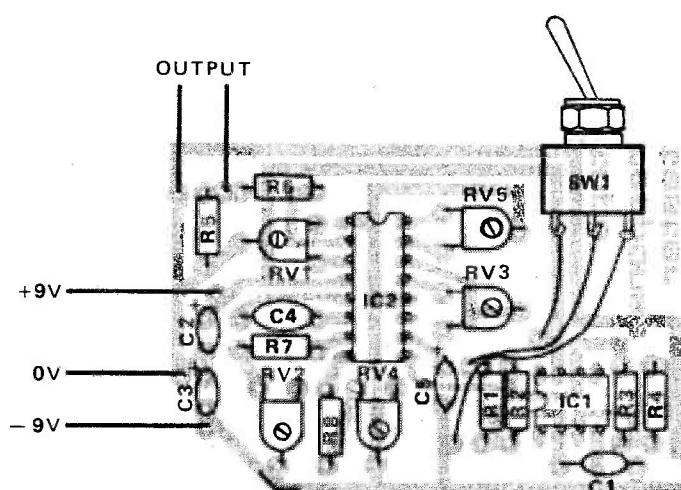


Fig.2. (left) Component overlay. The rate of switching between the two tones is set by C1 (0.3 Hz here, with C1, 1u5).

HOW IT WORKS

Most of the work is taken care of by IC2. This chip generates a triangle waveform which is shaped internally to produce the sine wave output. Frequency is controlled by the value of C4 and choice of resistance from pin 7 or 8 to the negative supply. Only one resistor is actively connected at any moment. Selection is achieved by controlling the voltage applied to pin 9. When the voltage at pin 9 is above two volts, or if the pin is open circuit, then the timing resistor connected to pin 7 is selected. When the signal at pin 9 drops below one volt, control is transferred to the resistor at pin 8.

Changeover is accomplished automatically by connecting the output of IC1, an op-amp configured as an astable oscillator, to pin 9. A high or low output can be 'forced' by switching R1 to either supply rail via SW1. With SW1 in the 'centre-off' position, the op-amp will switch at slightly less than 1 Hz producing alternating tones from the unit. Frequencies are set by adjustment of RV2 and RV4.

The output signal is developed across R5,6. Any convenient ratio may be chosen for these components to provide any desired output level up to a few volts peak to peak. A split supply was chosen as it facilitates circuit design. In any case IC2 needs at least a ten volt supply, precluding the use of a single battery. Current consumption is low and two PP3 type batteries provide a convenient source of power. Frequency stability with falling battery voltage is good and standard dry (Leclanche) batteries are quite adequate. Capacitors C2,3 provide overall decoupling.

PARTS LIST

RESISTORS

R1,7	10k
R2	1M0
R3,4	47k
R5	4k7
R6	22k
R8	180k

POTENTIOMETERS

RV1	47k min horiz preset
RV2	4k7 min horiz preset
RV3	470R min horiz preset
RV4	100k min horiz preset
RV5	22k min horiz preset

CAPACITORS

C1	1u5 tantalum
C2,3	47u tantalum
C4	10n polyester
C5	1u0 tantalum

SEMICONDUCTORS

IC1	3140
IC2	XR2206

MISCELLANEOUS

PCB, IC sockets, single pole centre-off change-over switch.

BUYLINES

The XR2206 is available from Technomatic Ltd or Stevenson Electronic Components. The other parts should be readily available.

NASCOM-2 MICRO-COMPUTER

FREE POWER SUPPLY
FREE 16K RAM Board

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Z80A 8 bit. This will run at 4 Mhz but is selected between 1/24/Mhz.

On-board, addressable memory. 2K 2K Monitor — Nas-sys 1. 1K Video RAM (MK 4118). 1K work space/User RAM (MK 4118). 8K Microsoft Basic (MK 3600 ROM). 8K Static RAM/2708E Pr.

Microprocessors Z80A. 8-bit CPU. This will run at 4MHz but is selectable between 1/24 Mhz. This CPU has now been generally accepted as the most powerful, 8 bit processor on the market.

INTERFACE

Keyboard New expanded 57 key Licon solid state keyboard especially built for Nascom. Uses standard Nascom, monitor controlled, decoding.

T.V. The iv peak to peak video signal can drive a monitor directly and is also fed to the on-board modulator to drive the domestic T.V.

I.O. On-board UART (Int. 6402) which provides serial handling for the on-board cassette interface or the RS232/20mA teletype interface.

The cassette interface is Kansas City standard at either 300 or 1200 baud. This is a link option on the NASCOM-2.

The RS232 and 20mA loop connector will interface directly into any standard teletype.

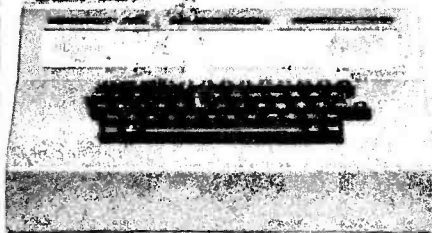
The input and output sides of the UART are independently switchable between any of the options — i.e. it is possible to house input on the cassette and output on the printer.

P/O There is also a totally uncommitted Parallel I/O (MK 3881) giving 16, programmable, I/O lines. These are addressable as 2 x 8 bit ports with complete handshake controls.

Documentation Full construction article is provided for those who buy a kit and an extensive software manual is provided for the monitor and Basic.

Basic. The Nascom 2 contains a full 8K Microsoft Basic in one Rom chip with additional features like DEEK, DOKE, SET RESET for simple programming.

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NASCOM-1
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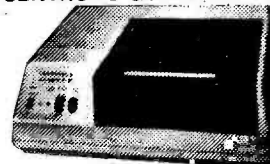
Carter 57 key ASCII keyboard. Conventional key board. 128 ASCII characters including control keys. Parallel output with strobe. Shift lock. + 5 V and -12 V DC. 12" x 5.5" x 1.5". Black keys with white legends.

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ETI JULY 1980

WHAT TO LOOK FORWARD TO
IN OUR JULY ISSUE! ON
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Next month ETI presents the definitive history of the spacecraft. Ian Graham - our permanently high spaceman - talks us through the hardware of the fastest man-made vehicles to date and takes a look at those which take flight only in our imaginations. For everyone who has looked up at the stars and longed.

Also next issue we have the long awaited Image Co-ordinator which will allow you to do things with your stereo image that your mother wouldn't approve of! Moreover Tim Orr follows up his Handbook of this month, with an article in similar vein, this time on his favourite subject, Active Filters, and out how to design them yourself in the July issue of ETI.

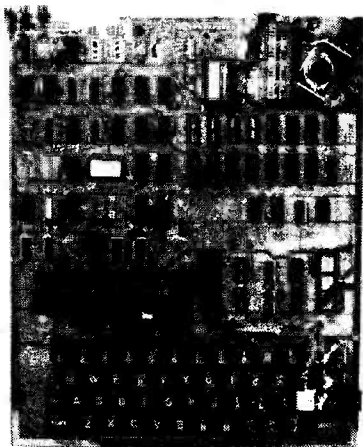
For the audio men there is our first look at one of the rising stars of hi-fi, the Quantum amplifier system. It can be bought as a kit, as modules, or as a fully built and working piece of equipment. As an example of their range we examine the 102 pre-amp and the 204 (110W per channel) power amp, stand by your speakers.

Articles mentioned herein are in an advanced state of preparation, however, circumstances may dictate changes to the final contents.

CHROMASONIC electronics

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4050 (200ns)	2.50	8212	2.00	CA3053	0.72	74LS01	0.18	74LS132	0.60	74LS289	4.50
4050 (350ns)	2.35	8216	2.08	CA3075	1.90	74LS02	0.18	74LS133	0.39	74LS290	0.91
4060 (300ns)	2.39	8224	2.77	CA3080	0.67	74LS03	0.19	74LS136	0.36	74LS293	0.91
4116	5.76	8228	4.13	CA3080E	0.67	74LS04	0.20	74LS138	0.65	74LS295	1.30
Static RAMS		8251	5.00	CA3081	1.30	74LS05	0.22	74LS139	0.65	74LS298	1.15
2102A	1.16	8253	6.93	CA3082	1.30	74LS08	0.20	74LS145	0.97	74LS348	1.39
2102A-2	1.16	8255	4.95	CA3086	0.45	74LS09	0.22	74LS151	0.81	74LS352	1.04
2111A-1	1.70	Baud Rate Generators		CA3089	1.75	74LS10	0.20	74LS153	0.52	74LS353	0.92
2112A-2	2.35	MC14411	5.87	CA3090Q	3.95	74LS11	0.20	74LS154	1.30	74LS362	4.21
21L02	0.98	MM5307	9.38	CA3097E	1.85	74LS12	0.18	74LS155	0.72	74LS365	0.47
2114	4.50	UARTS		CA3123E	1.70	74LS13	0.37	74LS156	0.72	74LS366	0.47
4035 (1000ns)	1.07	AY-5-1013	3.90	CA3130E	0.85	74LS14	0.65	74LS157	0.57	74LS367	0.47
4045 (250ns)	6.15	MM5303	5.04	CA3140E	0.38	74LS15	0.18	74LS158	0.57	74LS368	0.47
5257 (TMS4044)	6.93	TMS6011NC	3.55	CA3160E	1.00	74LS20	0.18	74LS160	1.09	74LS373	0.78
6810	3.48	2708 only £5.75 +VAT		CA3600E	3.69	74LS21	0.18	74LS161	0.69	74LS386	0.36
ROMS		Integrated Circuits		ICL7038A	3.57	74LS22	0.83	74LS162	1.16	74LS393	0.84
2513 (U.C.)	6.25	703 (8 pin)	0.95	ICL8038BC	8.82	74LS26	1.24	74LS163	0.69	74LS668	1.17
2513 (L.C.)	6.25	703 (14 pin)	0.35	ICL8038CC	3.40	74LS27	1.00	74LS164	1.06	74LS670	1.71
CPU		703 (16 pin)	0.35	ITT7120	1.90	74LS28	0.76	74LS165	0.72	8 x 4116 only £40.00 + VAT	
6800	5.90	703 (20 pin)	0.35	LMF351N	0.40	74LS29	1.75	74LS166	1.65	21L02 8 for £7.00	
8080	4.95	709 (8 pin)	0.35	LM301AH	0.80	74LS30	1.50	74LS168	1.71	16 for £13.00	
9900	26.05	709 (14 pin)	0.38	LM301AH	0.36	74LS32	1.00	74LS169	1.71	32 for £25.00	
Z80	9.00	709 (T099)	0.45	LM301AH	0.25	74LS33	1.00	74LS170	1.72	64 for £45.00 All excluding VAT	
6502	9.50	710 (8 pin)	0.36	LM307H	0.66	74LS37	3.97	74LS173	0.81		
E-PROMS		710 (14 pin)	0.38	LM307N	0.43	74LS38	3.97	74LS174	0.97		
1702AQ	5.16	710 (T099)	0.45	LM308N	0.95	74LS40	1.60	74LS175	0.97		
2708	5.75	711 (14 pin)	0.40	LM308	0.55	74LS42	1.20	74LS181	2.77		
2716	17.50	711 (T099)	0.87	LM308	0.55	74LS47	0.95	74LS188	0.44		
T.V. Controller		739 (14 pin)	1.80	LM318N	1.95	74LS48	3.20	74LS189	2.08		
SFF96364	10.50	741 (8 pin)	0.18	LM319H	2.25	74LS49	0.95	74LS190	0.86		
Buffers		741 (14 pin)	0.35	LM322N	3.87	74LS51	1.50	74LS191	0.86		
74365	0.52	741 (T099)	0.42	LM324N	0.50	74LS54	0.45	74LS192	1.04		
74366	0.52	747 (14 pin)	0.70	LM339N	0.50	74LS55	0.45	74LS193	1.04		
74367	0.52	748 (8 pin)	0.33	LM348N	0.90	74LS73	0.95	74LS194	0.86		
74368	0.52	748 (14 pin)	0.45	LM370N	2.90	74LS74	1.05	74LS195	0.87		
81LS95	1.25	753 (8 pin)	1.50	LM371H	2.05	74LS75	1.15	74LS196	0.97		
81LS96	1.25	AY-10212	5.80	LM373N	2.90	74LS76	1.98	74LS197	0.97		
81LS97	1.25	AY-15051	1.45	LM374N	2.90	74LS77	1.98	74LS200	0.81		
81LS98	1.25	AY-16721/6	1.95	LM377N	1.75	74LS78	0.80	74LS201	0.78		
8T26	1.90	AY-3-8500	5.00	LM378N	2.05	74LS83	0.80	74LS240	2.08		
8T28	1.90	AY-5-1224	2.40	LM379S	3.75	74LS85	1.90	74LS241	2.08		
8T95	1.57	AY-5-3507	4.15	LM380N	0.75	74LS86	1.05	74LS242	2.08		
8T96	1.57	AY-5-4007	6.30	LM381N	1.45	74LS91	0.97	74LS243	2.08		
8T97	1.57	CA3036	1.10	LM381AN	2.50	74LS92	0.69	74LS245	2.50		
8T98	1.57	CA3045F	1.40	LM382N	1.20	74LS93	0.60	74LS247	1.09		
		LM1820N	1.00	LM386N	0.78	74LS95	0.81	74LS248	1.09		
		LM1820N	1.00	LM387N	0.95	74LS96	1.16	74LS249	1.09		
		LM1820N	1.98	LM389N	0.95	74LS107	0.32	74LS251	0.96		
		LM1820N	1.98	LM725CN	2.25	74LS109	0.32	74LS253	0.92		
		LM1820N	1.98	LM1303N	1.00	74LS112	0.32	74LS257	0.92		
		LM1820N	1.98	LM1808N	1.95	74LS113	0.32	74LS258	0.92		
		LM1820N	1.98	LM1812N	5.40	74LS114	0.32	74LS259	1.39		
		LM1820N	1.98	LM1820N	1.00	74LS122	0.69	74LS261	4.50		
		LM1820N	1.98	LM1820N	1.00	74LS123	0.72	74LS266	0.37		
		LM1820N	1.98	LM1820N	1.98	74LS124	1.39	74LS273	1.70		

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SARGON AND THE LCD CHESS-SET!

The ultimate chess machine?

Well this must come pretty close. Ron Harris has been getting beaten regularly this month. Recovering some confidence he reports.

Sargon is the latest in the long line of chess playing boxes. It is neatly presented, with the keyboard and piece storage telescoping out from within the board itself. As with most of these offerings, the provided chessmen are abysmal. I really do not know why they bother providing them — surely anyone who can afford a machine like this will have their own decent set anyway?

I digress. Returning to the machine, it is a development of the well known 'Boris', an opponent I crossed pawns with some time ago. Sargon inherits the ability to comment on the games, albeit with a little more reticence. However the chess playing ability of Sargon is far superior to Boris, who would be hard pressed indeed to take a game from his offspring I suspect. (Response times being equal of course.)

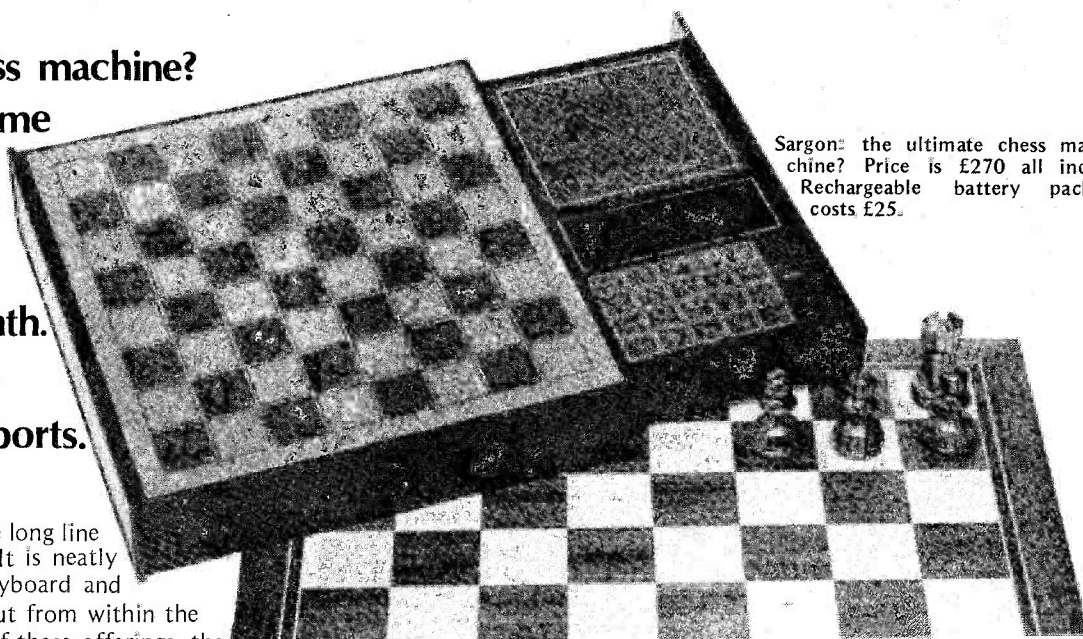
Model Modules

The basic concept of Sargon is a modular one. When the program is updated, changing the machine to a 'new' one means nothing more than unplugging the module and replacing it.

The keyboard is provided with different overlays to allow the machine to be used for pursuits other than chess. Backgammon and draughts are to be the first expansions, but here I shall restrict myself to the oldest wargame in history.

Features include a 'Restore' facility which allows you to replace the last move as though it had never happened — handy for training and cheating. A 'Best' button which cancels any random factor in Sargon's play and leads to a totally logical opponent. Frighteningly efficient, predictable (maybe — if you're good enough). Also there is a 'Hint' mode which allows you to obtain an idea of what to do next from the machine

Sargon: the ultimate chess machine? Price is £270 all inc. Rechargeable battery pack costs £25.



itself without having to listen to it if pride rises up and bites you at the last minute.

Fine thing pride. Makes you feel noble while Sargon cleans up your end of the board better than Domestos. Kills all known opponents. Dead. Naturally included are also full board review and alteration facilities.

Level With Me

Sargon is always on the level. Well some level or other, anyway. You set his response time by choosing a level from 0 (instant response) to 6 (postal chess). In between we have :—

Level one : 10 seconds
Level two : 20 seconds
Level three : 45 seconds
Level four : 2 minutes
Level five : 20 minutes

At two minutes thinking time Sargon is formidable indeed and will give a club player an energetic run for his pawns. I only ever beat the infernal thing once at this level — and I lost more than I won at level three.

Sargon is good. Very very good. At instant response it is better than the first generation chess machines and at level three becomes the best chess playing robot available for home use. For those who wish to trace it through I give an example game overleaf. Sargon set at Level 3 and plays Black. If you're interested in buying one, read it through — see if you would have done any better. I got a draw!



1.	E2 - E4	E7 - E5	21.	C1 - E3	B6 x E3
2.	G1 - F3	B8 - C6	22.	E1 x E3	C7 - C6
3.	B1 - C3	G8 - F6	23.	A1 - E1	D6 x E5
4.	F1 - C4	F8 - C5	24.	F4 x E5	E8 - E7
5.	F3 - G5	E8 - G8	25.	G5 - H3	D7 - H3
6.	E1 - G1	D7 - D6	26.	G2 x H3	F8 - D8
7.	D2 - D3	C8 - G4	27.	E5 - E6	E7 x E6
8.	D1 - D2	D8 - E7	28.	E3 x E6	E7 x E6
9.	C3 - D5	F6 x D5	29.	E1 x E6	D8 - C8
10.	C4 x D5	C5 - B4	30.	H3 - H4	G8 - F7
11.	C2 - C3	B4 - A5	31.	E6 - E3	C8 - B8
12.	D5 x C6	B7 x C6	32.	B2 - B3	B8 - E8
13.	F2 - F3	G4 - D7	33.	E3 x E8	E7 x E8
14.	D3 - D4	E7 - F6	34.	H1 - G2	E8 - F7
15.	D4 x E5	A5 - B6	35.	G2 - H3	F7 - F6
16.	G1 - H1	F6 x E5	36.	H3 - G4	F6 - E5
17.	F3 - F4	E5 - B5	37.	G4 - F3	C6 - C5
18.	F1 - E1	A8 - E8	38.	H2 - H3	D5 - D4
19.	E4 - E5	B5 - D5	39.	C3 x D4	E5 x D4
20.	D2 x D5	C6 x D5	40.	F3 - F4	D4 - C3

DRAW?

Figure 1. Playing Sargon at Level 3. Machine plays black. At the end of forty moves it's heading for a draw — providing neither of us does anything stupid!

Summing Totals

There is not much more to say. Sargon is a well presented games machine which is potentially expandable to better chess — or anything else a module appears for. As a player it is the best we've ever seen inside a ROM and will give any player food for thought. Its power is not to be scorned, consider it a toy and you're beat before you start. Tread carefully, oh ye of little faith, lest ye be divested of all manner of men!

Chess Champion

Just when I thought I'd done with chess (for this month at least) and was about to retreat back to wargaming, to regain a little composure, this box of tricks was placed mid-desk with its printer and LCD board — sufficiently interesting I think to hold off the counters a while longer and raise pawns once more.

Chess Champion is a dedicated chess machine. Expansion comes in the form of a printer, LCD board and game memory. A full chess clock will be added later.

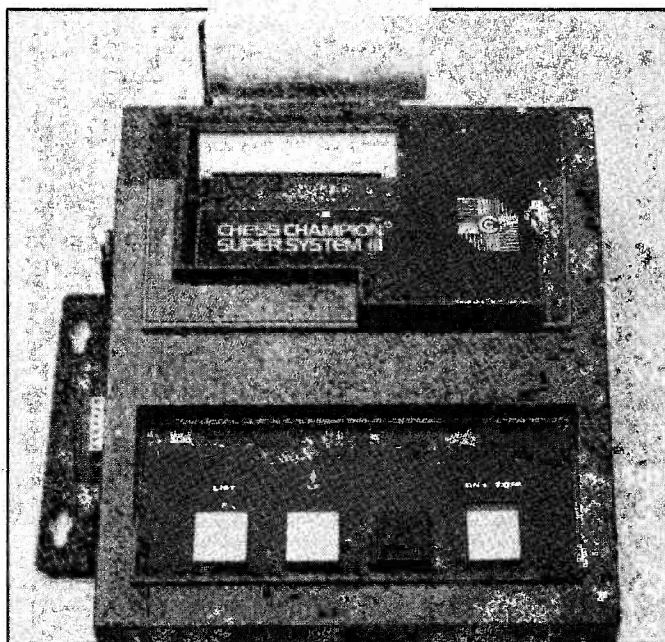
Rather than me trying to describe what it looks like, or has to offer, take a look at the photos. It features a fairly standard chess game keyboard with full board checking facilities. You can put back aught that has been removed — and remove what has not.

Display of move and status is via an LCD 'clock-type' display with piece verification symbol. Strength of game played is selected by varying response time. In seconds this time, not levels. In practice you have to double the time to get any appreciable increase in ability from the box.

Board Decision

As I can't see anyone using this unit without the LCD chessboard let me quickly add that to the consideration.

Packaged as a clip-on extra — the data bus edge connects — the board is powered from the main unit and is a complete chess set in itself. The chessmen are based around one symbol, which when displayed in its entirety is a Queen and assumes



The Chess Champion printer unit. Price : £104.95.

the guise of everything else as different segments are left unenergised. The photo shows how effective this can be.

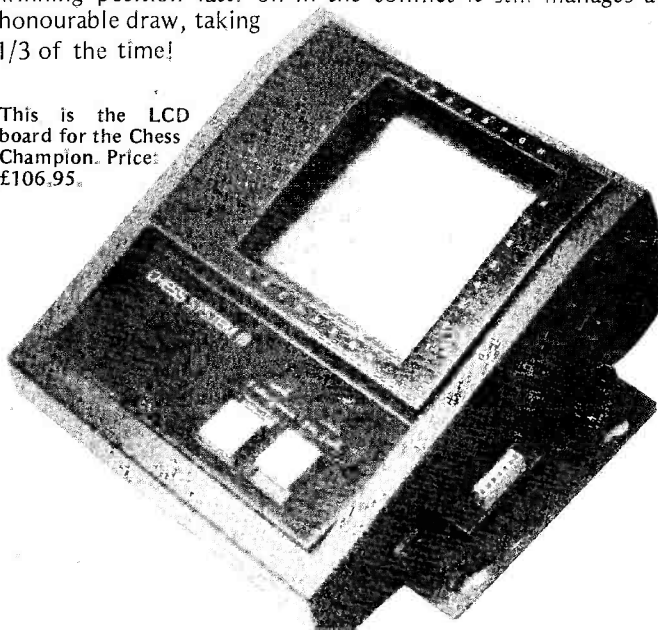
Backlighting is available when running from the mains and the board flashes a proposed move until the ENTER key is pushed. As the game progresses the board provides a continuous updated read-out and totally eliminates the need for a separate chess set with all the attendant errors of misinterpretation and mismanagement. Sheer magic! At last a self-contained intelligent chess set! I could forgive a lot of failings in the machine just for this beautiful facility.

As it happens there is little wrong with Chess Champion anyway. I disliked the sloppy keyboard and having to go through the involved key sequence to change level is frustrating, but so what? Sargon's board is touch-switched and an absolute pest. And you have to move men around to play it. Fair exchange?

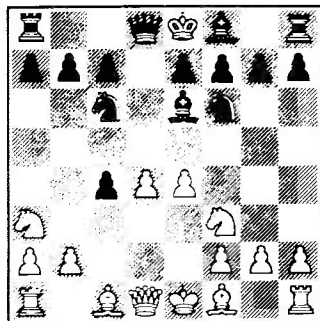
Mating Ritual

As a chess player, Chess Champion is no match for Sargon (at equal response). Witness the game below. Sargon is set to Level one (10 secs) and Chess Champion to 30 seconds response time. Although Sargon wastes what should have been a winning position later on in the conflict it still manages an honourable draw, taking 1/3 of the time!

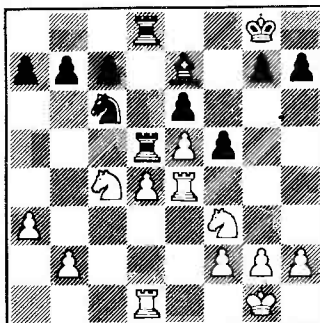
This is the LCD board for the Chess Champion. Price: £106.95.



1. D2-D4 D7-D5
2. C2-C4 D5xC4
3. G1-F3 B8-C6
4. B1-A3 C8-E6
5. E2-E4 G8-F6

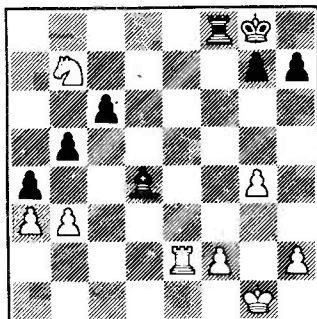


6. E4-E5 F6-E4
7. F1xC4 E6xC4
8. A3xC4 E7-E6
9. D1-D3 F8-B4
10. C1-D2 E4xD2
11. C4xD2 E8-G8
12. E1-G1 B4-E7
13. A2-A3 B4-E7
14. D3-C4 D5xC4
15. D2xC4 A8-D8
16. A1-D1 D8-D5
17. F1-E1 F8-D8
18. E1-E4 F7-F5

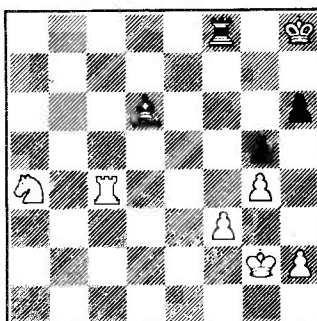


19. E5-F6 E7xF6
20. E4xE6 C6xD4

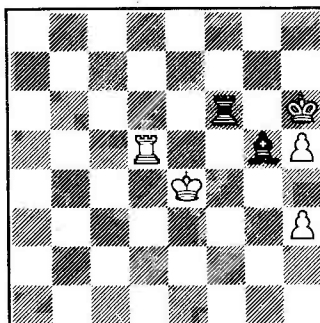
21. F3xD4 D5xD4
22. D1xD4 F6xD4
23. B2-B3 C7-C6
24. C4-D6 B7-B5
25. G2-G4 A7-A5
26. D6-B7 D8-F8
27. E6-E2 A5-A4



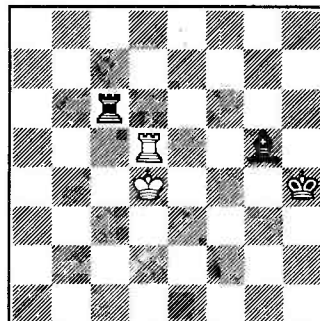
28. B3xA4 B5xA4
29. B7-A5 C6-C5
30. G1-G2 G7-G5
31. F2-F3 H7-H6
32. E2-E6 G8-H7
33. A5-C4 F8-A8
34. G2-F1 A8-B8
35. C4-B6 B8-F8
36. F1-G2 D4-B2
37. E6-E7 H7-H8
38. B6xA4 B2xA3
39. E7-C7 C5-C4
40. C7xC4 A3-D6



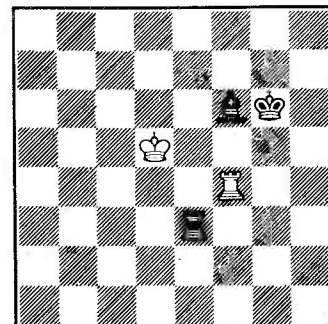
41. A4-B6 F8-E8
42. H2-H3 D6-F4
43. B6-D5 F4-D6
44. G2-F2 H8-G7
45. C4-C6 E8-E6
46. C6-C4 E6-E8
47. C4-C6 E8-E6
48. F3-F4 G5xF4
49. F2-F3 H6-H5
50. G4xH5 E6-H6
51. D5xF4 D6xF4
52. C6-C5 H6-F6
53. F3-E4 G7-H6
54. C5-D5 F4-G5



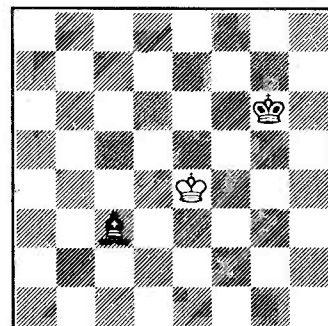
55. H3-H4 G5xH4
56. D5-C5 H4-G5
57. E4-E5 H6xH5
58. C5-D5 F6-C6



59. E5-D4 H5-H4
60. D5-F5 C6-E6
61. D4-D5 E6-B6
62. D5-C4 G5-F6
63. C4-C5 B6-E6
64. C5-D5 E6-B6
65. F5-F4 H4-H5
66. F4-C4 B6-B3
67. C4-E4 H5-G6
68. E4-F4 B3-E3



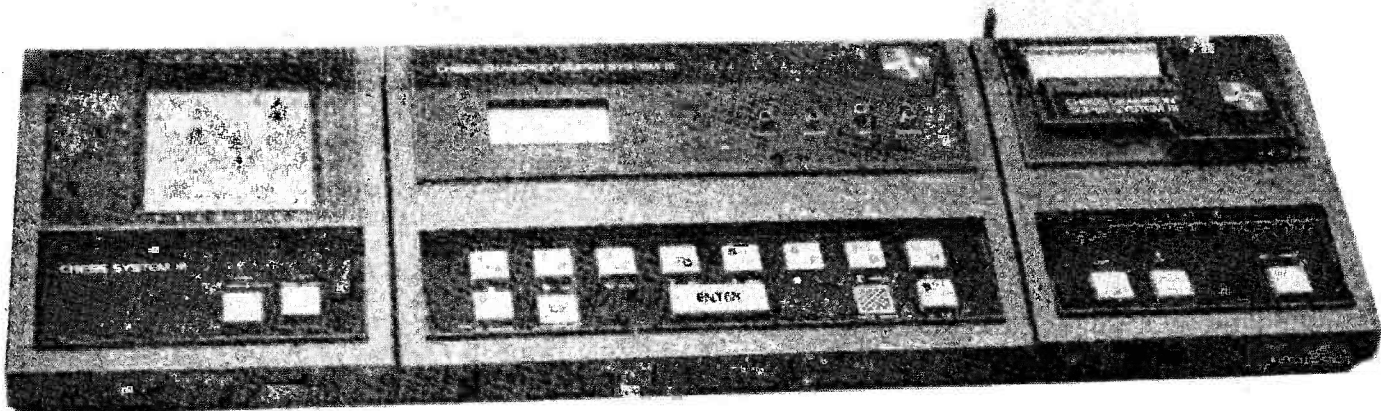
69. F4-E4 E3xE4
70. D5xE4 F6-C3



71. E4-D3 C3-E5
72. D3-E4 G6-F6
73. E4-D3 F6-F5
74. D3-E3 F5-G6

Figure 2 (above) the same between Sargon at 10 second response (white) and Chess Champion at 30 seconds. A draw in the end. Sargon should have won.

Below : the complete Chess Champion, with the LCD board in operation. Fascinating. The main unit will cost you £154.95 all inc. So Sargon costs about the same as the main unit plus LCD board in Chess Champion.



However, please don't think I'm decrying Chess Champion's ability. I wouldn't dare. With the possible exception of the Voice Challenger, I know of no other machine that could best it bar Sargon. Given a little longer Chess Champion will still pin you to the back rank should that be your desire.

It is just that it takes a little while to get over the advanced presentation (i.e. gadgets!) that comes as part of the system. Talking of which I haven't mentioned the printer yet, so let us rectify that immediately.

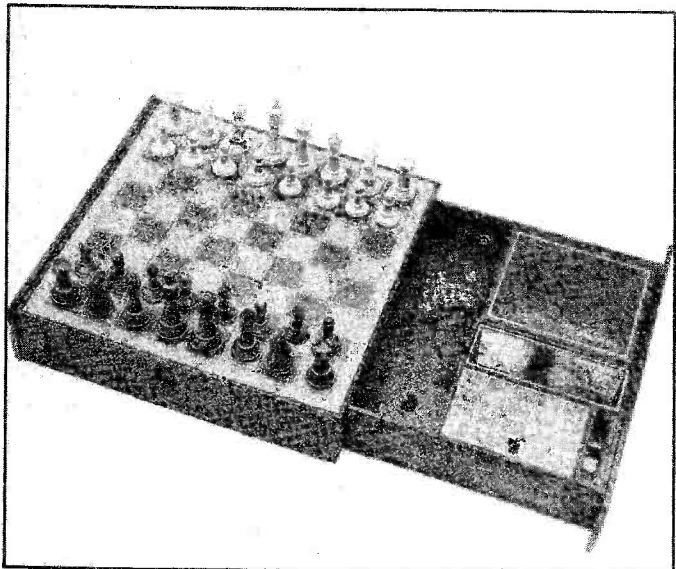
Packaged as another clip-on extra, the printer is a thermal unit with twenty characters per line capability. Shown below is the display of the full board which can be obtained, at any point during a game, by pushing LIST on the printer. Moves are recorded with a "symbol—move from—move to" sequence.

In order to give an example of the printer's output — and because I couldn't resist it — below I have given the ending from a game of Sargon vs Chess Champion at equal response times (20 secs). It's a massacre so don't look if you can't stand the sight of blood! (facing page).

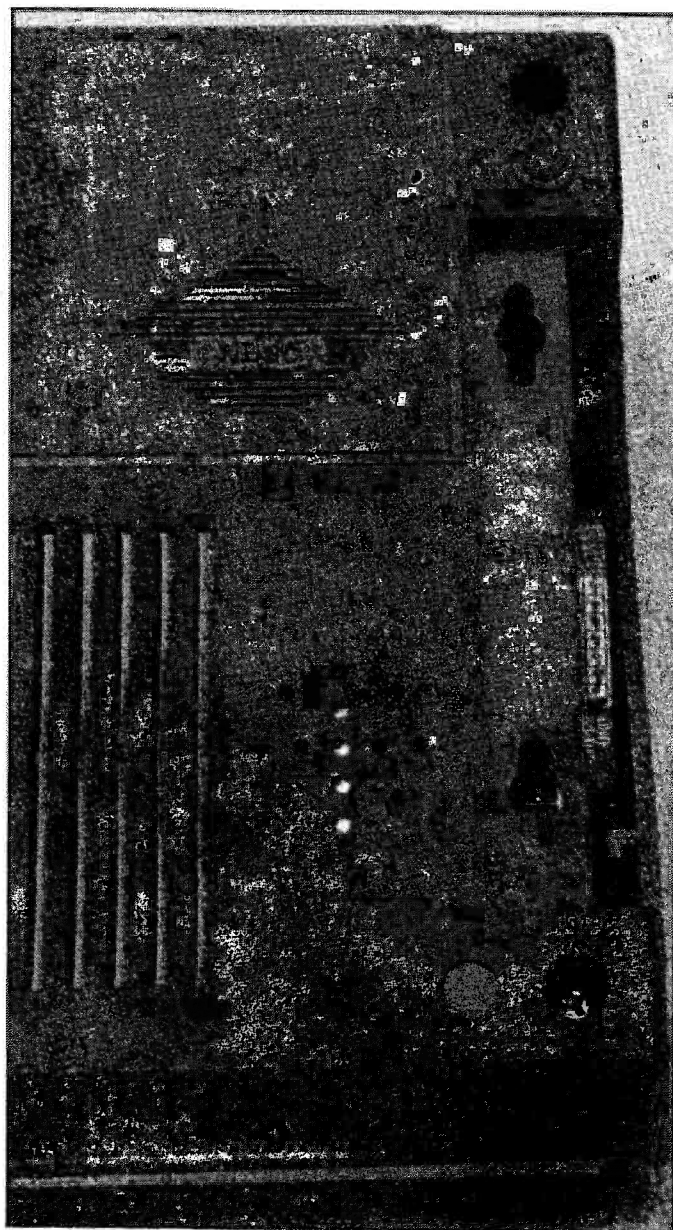


Above: the Chess Champion master unit with its clock-type display. To the right is shown the bus connection for the slave printer-board units.

Below: Sargon ready to play.



Above: Sargon ready to play.



Which Machine?

Choosing between the two is by no means straightforward. If you're a dedicated high-level chess player who will always use his own chess-set anyway, then Sargon will be your best choice for its superior playing ability. On the other hand the LCD board is a huge advantage (and error eliminator) and provided you don't mind waiting that extra time for equal ability Chess Champion is an attractive proposition.

The difference between the machines, in ability, diminishes as the thinking time is increased past 2 minutes, with Sargon always retaining the edge. For my own part I'd tend to go for Chess Champion as that still beats *me* often enough to be challenging and that board fascinates me! I dare say though Sargon will receive heavy support from the better players of this world.

My thanks to Kramer & Co. for lending us the machines for this article. Prices of the units from them are given in the captions.

[illegible]

Figure 3. Sargon vs Chess Champion (black) with both machines on 20 seconds think time. The print-out is courtesy of Chess Champ's printer.

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The slim but strong bracelet is fully adjustable and is available in a silver or gold finish.

M64 Mans dual time quartz alarm chronograph with 6 digits, 5 indicators and 22 functions.

For business people with overseas contacts and responsibilities this is the ideal watch.

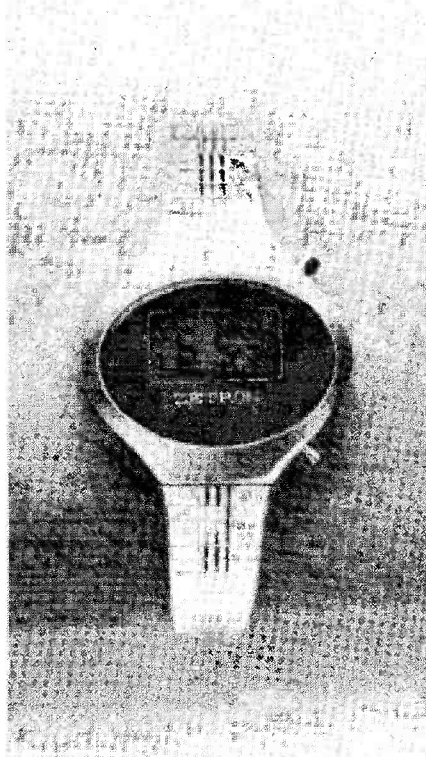
Local time is always visible, but in addition the watch can be set, and recall, a second time zone, in either 12 or 24 hour formats, and displays a day and date for each zone.

The chronograph/stopwatch displays up to 12 hours, 59 minutes and 59.9 seconds.

On command, the stopwatch display freezes to show intermediate (split/lap) time while the stopwatch continues to run and neither function affects the normal timekeeping.

The alarm can be set to any time within a 24 hour period.

To complete the functions, there is also a 4 year calendar and a fully adjustable stainless steel strap.



M18 £15.95 inc p & p
Ladies quartz LCD Fashion Watch



M64 £14.95 inc p & p
Mans dual time quartz alarm chronograph with 6 digits, 5 indicators and 22 functions.



£9.95 inc p & p

M15 Ladies quartz LCD Day Watch

This slender watch displays hours, mins, secs, day and date and has an auto calendar and a backlight.

Only 25mm X 20mm X 6mm thick this elegant watch has a bracelet, in silver or gold finish, and is fully adjustable to suit very slim wrists.



M17 Ladies quartz LCD Cocktail Watch

Only 6mm thick, the watch displays hours, mins, secs, day, date and has an auto calendar and backlight.

The fully adjustable bracelet has a bronze/gold or silver finish.

£13.95
inc p & p



M3 Mens quartz LCD with 6 digits and 11 functions

Only 7mm thick and with a fully adjustable stainless steel bracelet, this watch is ideal for all ages.

The normal functions are hours, mins, secs, day, date, and day of week.

But as a stop-watch, which does not affect normal timekeeping you also have 1/100th and 1/10th secs., split, lap and journey timing, a four year calendar and a backlight.

Also available is a solar version.

This is the same watch but incorporated is a solar energy panel which converts normal daylight into electricity.

During periods of darkness the watch instantly operates by battery without losing its accuracy.

£10.95
inc p & p



M30 Mens dual time melody alarm chronograph with count-down timer, 34 functions

A very impressive new watch at a superbly low price and with so many useful functions.

There are 5 independent working modes; normal watch, count-down alarm, alarm, dual time zone, 1/100th sec. chronograph.

In addition, the watch can display the day of the week in French, German or English.

The count-down timer can be used for a variety of applications from boiling an egg to reminding you your parking meter time has expired. Both the count-down alarm and the normal alarm have a clear musical tone.

For the businessman the time zone feature could be a real advantage. Just programme the second time zone and it will be permanently recorded for easy reference.

And as a stop-watch here's a great timepiece for sporting events and for timing recordings.

There's the conventional stop/start counter plus a lap timer which enables first and second places to be timed.

Longer timing intervals, such as journey times can be recorded while the watch is reading its normal time.

£19.95
inc p & p



M4 Mens quartz LCD alarm with 6 digits and 9 functions

A very useful watch with an effective, loud alarm but still only 8mm thick.

The normal functions are hours, mins, secs, date, day of week, four year calendar and a backlight.

In addition, there is a 24-hour alarm, a 5-minute snooze feature and a 4 second pre-alarm conference bleep.

The conference signal is a bleep, 4 seconds before main alarm to give advance warning and the option to cancel.

After the main alarm stops the snooze repeater alarm sounds 5 minutes later, unless previously cancelled.

£10.95
inc p & p

To complete the functions, there is also a 4 year calendar and a fully adjustable stainless steel strap.



M16 Mens dual time quartz alarm chronograph with 6 digits, 5 indicators and 22 functions.

This watch has the same functions as M64 except the time is in the 24 hour format only.

A solar version is available.

This is the same watch but incorporated is a solar energy panel which converts normal daylight into electricity.

During periods of darkness the watch instantly operates by battery without losing its accuracy.

Metac

ELECTRONICS & TIME CENTRES

Callers may buy from our shops in:
London, 327 Edgware Rd, W2 **Daventry**,
67 High St, **Northampton**, St. Giles Square.

To: Metac Electronics & Time Centres,
24-hour Despatch Centre, 67 High Street,
Daventry, Northants.

Please send me the following watches:

Model No. Quantity Colour if applic.

I enclose PO/Cheque for £
Barclaycard/Access No.

Name

Address

ET16

STEVENSON

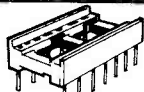
Electronic Components

OPTO

LED's	0.125in.	0.2in	each
Red	TIL209	TIL220	10p
Green	TIL211	TIL221	15p
Yellow	TIL213	TIL223	15p
Clips	3p	3p	
DISPLAYS			
DL704	0.3 in CC		130p
DL707	0.3 in CA		130p
FND500	0.5 in CC		100p

SKTS

Low profile
by Texas



8 pin	9p	18 pin	16p	24 pin	22p
14 pin	11p	20 pin	18p	28 pin	26p
16 pin	12p	22 pin	20p	40 pin	38p
3 lead T018 or T05 sct.					12p each.
Soldercon pins:					100 for 60p.

PCBS

VEROBOARD

Size in.	0.1in.	0.15in.	Vero
25 x 1	16p	—	Cutter 110p.
2.5 x 3.75	60p	53p	
2.5 x 5	70p	65p	Pin insertion
3.75 x 5	75p	75p	tool 150p.
3.75 x 17	275p	240p	
SS pins/100	45p	45p	
Fibreglass board, 203 x 95mm:			80p each.
Alfac	—	38p	per sheet.

RESISTORS

Carbon film resistors. High Stability, low noise 5%.

E12 series. 4.7 ohms to 10M. Any mix:			
each	100+	1000+	
0.25W	1p	0.9p	0.85p
0.5W	2p	1.5p	1.3p

Special development packs consisting of 10 of each value from 4.7 ohms to 1 Meg-ohm (650 res) 0.5W £8.50. 0.25W £5.30.

METAL FILM RESISTORS

very high stability, low noise rated at ¼W 1%. Available from 51 ohms to 330k in E24 series. Any mix:

each	100+	1000+
0.25W	4p	3.7p
		3.5p

POTENTIOMETERS

Preset vertical or horizontal 100 ohms - 1M 7p
Rotary 5K-2M2 Log or Lin single 30p
Rotary 5K-2M2 Log or Lin double 90p
Slide 60mm travel 5K-500K Log or Lin, single 60p
Suitable knobs for above with coloured caps in red, blue, green, grey, yellow and black. Rotary controls 16p each. Slide type 12p each.

MISC

Murata Ultrasonic Transducers	350p pair
64mm 8 ohm speakers	100p each
64mm 64 ohm speakers	100p each
SRB 17W soldering iron	430p each
Reel of 22swg solder (39.6m)	320p each
Desoldering tool	510p each
Precision screwdriver set	170p each
Titan Electric drill	1095p each
Miniature 606 and 909 at 100mA transformers	105p each

SWITCHES

TOGGLE		
Standard	SPST 36p	DPDT 50p
Miniature	SPDT 75p	DPDT 85p
Subminiature	SPST 58p	DPDT 78p
SLIDE		
Standard		DPDT 17p
Miniature		DPDT 16p
ROCKER (10A rating)		
SPST 34p each.	SPST	46p each.
ROTARY		
1P12W, 2P6W, 4P3W or 3P4W		51p each
Key operated DPDT (Yale key)		395p each
PUSH		
Non locking - push to make		16p each
- push to break		22p each
Locking - SPST		75p each
- DPDT		100p each

REGULATORS

100mA + ve	LM309K	140p
78L05 30p	LM317T	220p
78L12 30p	LM323K	480p
78L15 30p	LM723	40p
1A + ve		1A - ve
78L05 30p	7805	70p
78L12 30p	7812	70p
78L15 30p	7815	70p
		7905 85p
		7912 85p
		7915 85p

TRANSISTORS

AC127	22p	BC548	41p	TIP32C	60p
AC128	22p	BCY71	16p	TIP2955	66p
AC176	22p	BCY72	15p	TIP3055	53p
AD161	40p	BD131	40p	ZTX107	12p
AD162	40p	BD132	40p	ZTX108	12p
BC107	10p	BD139	33p	ZTX300	14p
BC108	10p	BD140	33p	ZTX500	15p
BC108C	12p	BFY50	23p	2N3053	25p
BC109	10p	BFY51	23p	2N3054	56p
BC109C	12p	BFY52	23p	2N3055	50p
BC147	9p	MJ2955	100p	2N3702	9p
BC148	9p	MPSA06	16p	2N3704	9p
BC177	16p	MPSA56	16p	2N3706	9p
BC178	16p	TIP29C	60p	2N3904	10p
BC182	10p	TIP30C	48p	2N3905	10p
BC182L	10p	TIP31C	50p	2N3906	10p
BC184	10p			2N5459	33p
BC184L	10p			2N5777	50p
BC212	10p	1N914	4p	1N4006	7p
BC212L	10p	1N4148	3p	1N5401	14p
BC214L	10p	1N4002	5p	BZY88ser.	8p
		1N4148	£1.50 per 100.		

CAPACITORS

POLYSTYRENE

High quality foil type. 63V working, 5% tol.
22pF to 100pF 7p each
1500pF to 0.01uF 9p each
TANTALUM BEAD
0.1, 0.15, 0.22, 0.33, 0.47, 0.68
1 & 2.2uF @ 35V 10p each
4.7, 6.8, 10uF @ 25V 18p each
22 @ 16V, 47 @ 6V, 100 @ 3V 22p each

MYLAR

0.001, 0.01, 0.022, 0.033, 0.047 4p each
0.068, 0.1 5p each

POLYESTER

Mullard C280 series
0.01, 0.015, 0.022, 0.033, 0.047, 0.068, 0.1. 6p ea.
0.15, 0.22 8p each
0.33, 0.47 12p each
0.68 17p each
1.0uF 22p each

CERAMIC

Plate type 50V. Available in E12 series from 22pF to 1000pF and E6 series from 1500pF to 0.047uF 2p each

MINIATURE TRIMMERS

Miniature film type, in 1.4pF - 5pF, 2pF - 22pF, 2pF - 22pF, 2pF - 10pF, 5.5pF - 65pF. 22p each

RADIAL LEAD ELECTROLYTICS

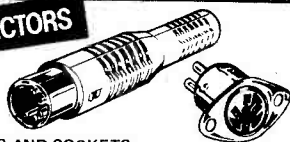
63V	0.47	1.0	2.2	4.7	10	6p each
			22	33	47	8p each
			100			16p each
			220			20p each
25V	10	22	33	47		6p each
			100			8p each
			220			12p each
			470			18p each
			1000			28p each

PACKS

Specially developed packs intended for development work.

¼W CF resistor, 10 each value E12 series 4.7 ohm to 1 Megohm (650 total) 530p each
¼W CF resistor, 10 each value E12 series 4.7 ohm to 1 Megohm (650 total) 850p each
¼W MF 1% resistor, 10 each value E24 series 51 ohms to 330K (930) 2950p each
Preset potentiometers 5 each value from 100 ohms to 1 Megohm (65) 390p each
Polyester capacitors 5 each value 0.01 to 2.2uF (170) 690p each
Ceramic plate capacitors 10 each value 22pF to 0.01uF (310) 575p each

CONNECTORS



DIN PLUGS AND SOCKETS

	plug	chassis socket	line socket
2 pin	8p	8p	12p
3 pin	12p	10p	12p
5 pin 180°	12p	11p	17p
5 pin 240°	14p	11p	22p

JACK PLUGS AND SOCKETS

	unscreened	screened	socket
2.5mm	10p	15p	8p
3.5mm	10p	16p	9p
Standard	16p	30p	19p
Stereo	23p	39p	22p

1mm PLUGS AND SOCKETS

Suitable for low voltage circuits, Red & Black. Plugs: 8p each. Sockets: 9p each.

4mm PLUGS AND SOCKETS

Available in blue, black, green, brown, red, white and yellow. Plugs 18p each. Sockets: 15p each.

CMOS

4000	20p	4023	25p	4054	120p	4502	120p
4001	25p	4024	55p	4060	120p	4507	60p
4002	20p	4025	20p	4063	120p	4508	330p
4006	90p	4026	160p	4066	60p	4510	90p
4007	25p	4027	45p	4068	25p	4511	90p
4008	100p	4028	90p	4069	25p	4512	90p
4011	25p	4029	100p	4070	25p	4516	90p
4012	20p	4031	220p	4071	25p	4518	90p
4013	40p	4033	150p	4072	25p	4520	110p
4014	85p	4036	350p	4073	25p	4527	165p
4015	90p	4039	350p	4075	25p	4528	100p
4016	40p	4040	110p	4076	90p	4529	160p
4017	70p	4041	85p	4077	25p	4531	150p
4018	90p	4042	80p	4078	25p	4532	125p
4020	110p	4043	95p	4081	25p	4538	160p
4022	100p	4046	110p	4082	25p	4543	170p
		4048	60p	4086	75p	4566	410p
		4049	50p	4093	60p	4568	120p
		4050	50p	4095	110p	4569	410p
		4051	80p	4098	120p	4581	320p
		4053	80p	4501	20p	4585	115p

LSTTL

74LS00	16p	74LS47	75p	74LS126	65p	74LS175	100p
74LS01	22p	74LS48	100p	74LS132	95p	74LS190	90p
74LS02	16p	74LS54	25p	74LS136	60p	74LS191	90p
74LS03	22p	74LS73	40p	74LS138	80p	74LS192	90p
74LS04	16p	74LS74	45p	74LS139	80p	74LS193	90p
74LS05	22p	74LS75	50p	74LS151	75p	74LS195	90p
74LS06	16p	74LS76	45p	74LS155	75p	74LS196	90p
74LS08	24p	74LS78	45p	74LS156	80p	74LS197	95p
74LS10	22p	74LS83	85p	74LS157	55p	74LS221	120p
74LS13	45p	74LS85	100p	74LS158	70p	74LS251	70p
74LS14	70p	74LS86	50p	74LS160	75p	74LS266	55p
74LS20	22p	74LS90	50p	74LS161	75p	74LS290	90p
74LS21	22p	74LS93	70p	74LS162	95p	74LS365	60p
74LS22	30p	74LS95	85p	74LS163	90p	74LS366	60p
74LS27	30p	74LS107	50p	74LS164	90p	74LS367	60p
74LS32	30p	74LS114	60p	74LS165	80p	74LS368	60p
74LS37	45p	74LS123	70p	74LS173	120p	74LS386	60p
74LS42	75p	74LS125	45p	74LS174	100p	74LS670	210p

TTL

7400	12p	7442	50p	7493	35p	74157	50p
7401	12p	7445	65p	7496	55p	74164	70p
7402	12p	7447	55p	74121	35p	74165	70p
7404	16p	7448	55p	74123	45p	74174	70p
7408	18p	7473	30p	74125	45p	74177	70p
7410	14p	7474	30p	74126	45p	74190	70p
7413	30p	7475	35p	74132	55p	74191	70p
7414	55p	7476	35p	74141	70p	74192	70p
7420	14p	7485	65p	74145	70p	74193	70p
7427	25p	7486	25p	74148	120p	74194	70p
7432	28p	7490	35p	74150	65p	74196	70p
		7492	35p	74154	80p	74197	70p

LINEAR

LINEAR	LM10	400p	LM3909	72p	TBA800	80p	
	LM301A	30p	LM3914	280p	TBA810S	110p	
	LM308	70p	LM3915	280p	TDA1008	350p	
	LM318	85p	LM3911	280p	TDA1022	630p	
	LM324	52p	LM13600	160p	TDA1024	120p	
	LM339	55p	MC1496	80p	TDA2020	360p	
	LM348	100p	LM1458	40p	TL071	75p	
	LM377	170p	LM1830	180p	TL072	135p	
	LM378	230p	MC3340P	135p	TL074	200p	
	CA3046	70p	MC3360P	135p	TL081	45p	
CA3080	75p	MM57160	650p	TL082	85p		
CA3130	90p	LM381	140p	NE531	110p	TL084	125p
CA3140	50p	LM382	120p	NE555	23p	TL170	60p
FX209	820p	LM383	200p	NE556	60p	XR2206	390p
ICM7555	100p	LM386	90p	NE566	120p	XR2207	450p
ICM7556	100A	LM387	120p	NE567	120p	ZN414	80p
LF347	135p	LM389	100p	NE570	420p	ZN419	150p
LF351	45p	LM391	100p	NE571	460p	ZN424	10A
LF353	85p	LM1310	140p	NE5537	POA	ZN425E	420p
LF355	92p	LM2917	280p	RC4136	100p	ZN460	360p
LF356	95p	LM2924	160p	SAD1024	1310p	ZN1034	230p
LF357	92p	LM3900	60p	SN76477	230p		

ETI

CIRCUIT DESIGN HANDBOOK

NO.1 : AUDIO AMPLIFICATION AND OSCILLATORS.



A step by step guide to doing it ALL yourself — by Tim Orr. This is the first of what will become an occasional series of easy to read reference works. Mathematics will be kept to a minimum with the emphasis upon producing practical circuits — quickly. Just the thing you always wanted, but thought no-one was ever going to produce! Future subjects will include radio circuitry, digital logic and signal processing.

SECTION ONE :

small signal and pre-amplifiers

SECTION TWO :

large signal, or power, amplifiers

SECTION THREE :

audio frequency oscillators

1. SMALL SIGNAL AND PRE-AMPLIFIERS

Preamplifiers are used to convert low level signals into higher level signals with low output impedances. The primary design considerations for preamplifiers are input impedance, signal gain, equalisation, noise performance and distortion. It is now possible to buy integrated circuits that will perform virtually all common preamplifier functions. Only rarely, (and with a lot of skill), will one be able to improve upon a monolithic 'best' solution with a discrete component design. However, it is necessary to fully understand the operation of the IC if optimum results are to be obtained.

The Op Amp Building Block

Most IC preamplifiers operate as op amps. They have a single or differential input, a low impedance output and a large frequency dependent voltage gain, (Fig.1). Note that the

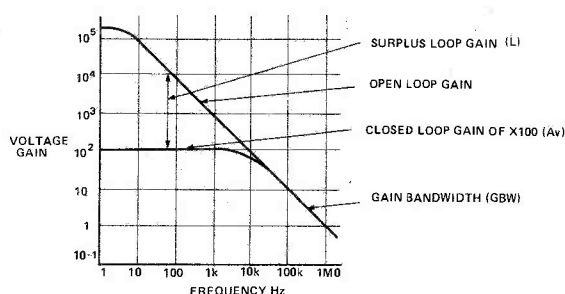


Fig.1. Typical frequency response for the 741 op amp.

open loop voltage gain rolls off at -6 dB per octave. By applying feedback around the op amp (closed loop), the gain is stabilised and is held constant by the resistor ratio until the device runs out of bandwidth. The difference between the open and closed loop gain is known as the surplus loop gain. This surplus loop gain is the negative feedback that is used to iron out non-linearities in the op amp. As the size of the surplus loop gain decreases with increasing frequency, the distortion and output impedance increase. Fig.2 compares the performance of inverting versus non-inverting configurations.

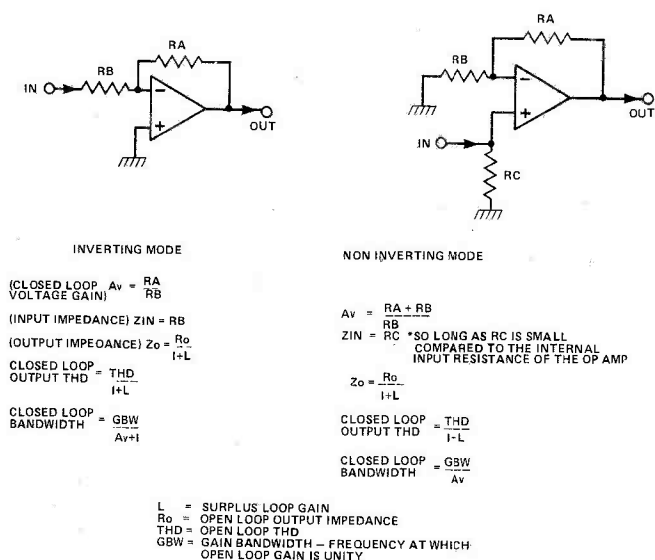


Fig.2. A comparison of the performance of inverting versus non-inverting configurations.

Note that for unity gain the non-inverting mode has twice the closed loop bandwidth of the inverting mode. Also note that the output impedance rises as the surplus loop gain decreases. This can cause a sharp increase in distortion when the op amp is driving a low impedance load at high frequency.

Design Example

Q. Design an amplifier with a gain of 60 dB, a closed loop bandwidth of at least 20 kHz and input impedance of 10 k.

A. First, try the inverting mode as shown in Fig.2.
 $Z_{in} = 10 \text{ k} = R_B$

$$A_v = 60 \text{ dB} = X1000 = \frac{R_A}{R_B}$$

$$\text{Therefore, } R_A = 10 \text{ k} \times 1000 = 10 \text{ M}$$

If we use a 741 then the input offset voltage will be multiplied by the closed loop gain. The offset is typically ± 1 to 5 mV. Therefore, the output offset will be ± 1 to 5 V! It is possible to null out the input offset (Fig.3a) with a preset. This circuit will not be very satisfactory.

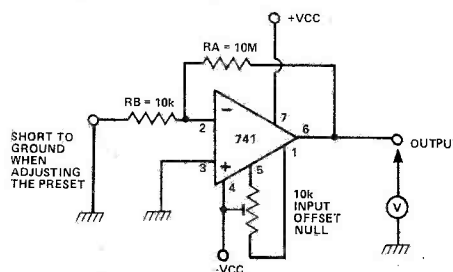


Fig.3a. The input offset can be null with a preset.

Its DC output offset will probably drift with temperature and time. If stable high DC gains are required then a 741 should not be used. A high performance instrument op amp should be selected in its place. Another problem in using the 741 is its 1 MHz gain bandwidth product. A closed loop gain of 60 dB will result in a closed loop bandwidth of 1 kHz, and not the 20 kHz needed. An op amp capable of giving 60 dB of gain at 20 kHz would need a gain bandwidth product of 20 MHz.

Although there are some op amps with this performance, they are generally difficult to stabilise and are relatively expensive. A cheap solution is to use two 741s, both with gains of 30 dB (x 33), (Fig.3b). The 741 has a bandwidth of 30 kHz at

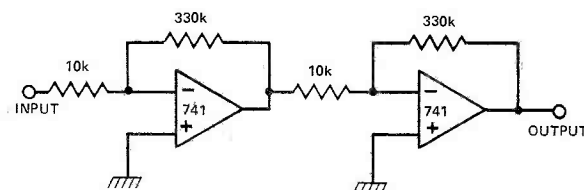


Fig.3b. A cheaper way to achieve higher gain at, say, 20 kHz without incurring a huge bandwidth is to use two 741s.

a closed loop gain of 30 dB. The DC offset still remains a problem, but it could be removed with a nulling preset on the first op amp. However, if the amplifier is to be used for audio then a DC response is not needed and so AC coupling can be used to reduce the final DC offset, Fig.3c. Yet another problem still exists. With the input short circuited the circuit would probably produce about 10 mV of noise at its output. The subject of noise will be dealt with later; suffice it to say that the 741 is not a low noise device. Low noise operation can be obtained by using one of the low noise op amps that are now available.

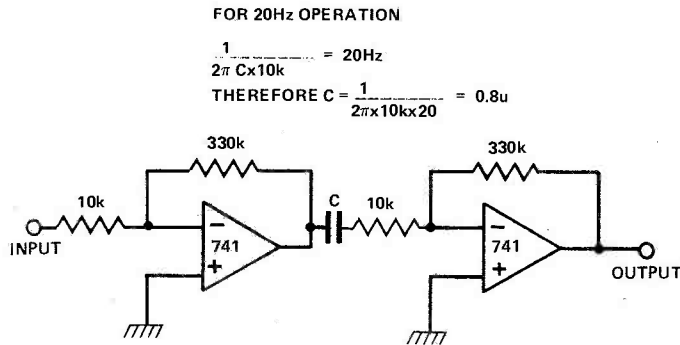


Fig.3c. AC coupling can be used to produce the final offset in audio applications.

Input Offset Voltage And Bias Current

When using op amps as DC amplifiers there are several sources of errors, Fig.4. The input to an op amp is usually an NPN differential pair. To make the device operate, a base current must be supplied (input bias current). Also, to balance the op amp the current through both transistors must be

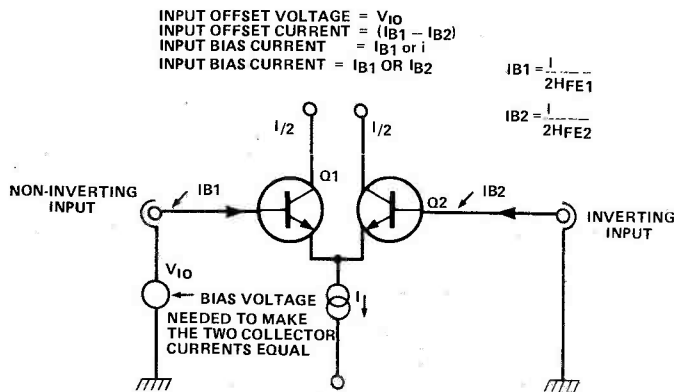


Fig.4. Typical differential op amp input.

equal. The transistor pair is 'matched' for parameters such as H_{fe} and V_{be} versus I_{CE} . However, small differences are caused by the manufacturing process, resulting in the base currents being different (input offset current) and also the base-emitter voltage parameter (input offset voltage). The input offset

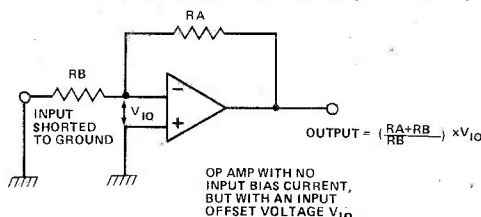


Fig.5. The effect of V_{IO} .

voltage is multiplied by the closed loop DC gain of the op amp (Fig.5) and the input bias current sets up a DC offset across any resistors it flows through (Fig.6). Typical parameters for the 741 op amp are; 2 mV (V_{IO}), 80 nA (IB) and 20 nA ($IB1-IB2$). These parameters vary from device to device and from manufacturer to manufacturer. The purpose of successful design is to produce circuits that are insensitive to these

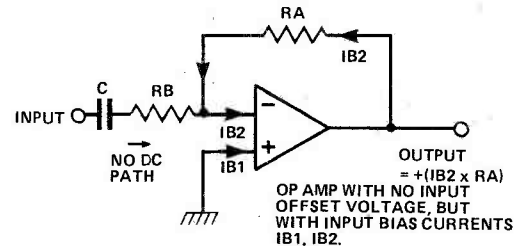


Fig.6. The effect of IB .

variations. Generally, for audio designs, the DC offsets may be eliminated by AC coupling and other methods (Fig.7). Note that the DC output offset may be reduced by inserting a resistor from the non-inverting input to ground. Without that resistor the DC offset may well have been ± 26 mV ($IB2 \times RA$) as opposed to ± 6.6 mV ($(IB1-IB2) \times RA$). A DC voltage on the output would generate a disturbing crackle when the level pot is adjusted.

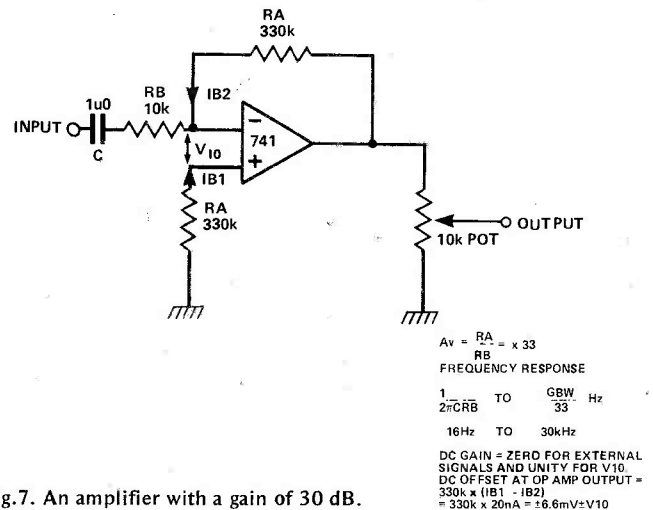


Fig.7. An amplifier with a gain of 30 dB.

Voltage Swing, Power, & Bandwidth

The voltage swing at the output of an op amp is limited in many ways, Fig.8. Most op amps can only swing within a few volts of either supply rail. Also, the speed at which the output voltage can move is limited by the slew rate of the device, which is typically 0V5 per microsecond for a 741. This is the limiting factor in designing amplifiers for high level large signal voltages.

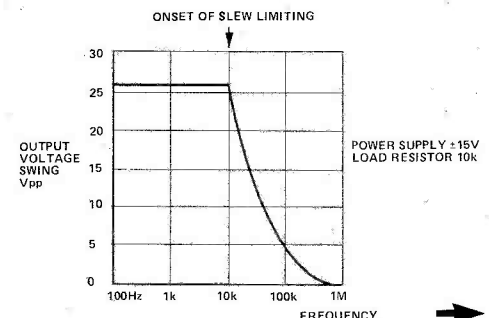


Fig. 8. Typical power bandwidth for a 741 op amp.

Design Example

Q. Design an amplifier with a gain of 4 to amplify a 50 kHz 5 V squarewave.

A. First try a 741, Fig.9. The required output swing is ± 10 V. The 741 can only move at 0V/uS and so in the half period of the square wave, it can only move 5 V. If the 741 is replaced with a faster device, the TL081 (13 V/uS) then a 'square' wave is produced. The TL081 would take approximately 1.5 uS to travel the 20 V distance, thus generating a

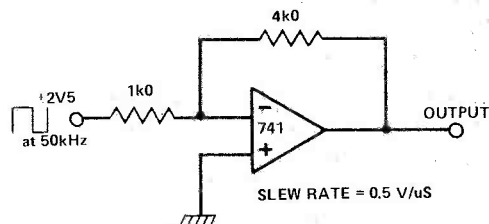


Fig.9. The difference in slew rate between a 741 and a TL081.

rise and fall time of 1.5 uS. Note, that if the resistors were increased in value to say 250 k and 1MΩ, then the squarewave output would ring. This is because the feedback would have to charge up the stray capacitance at the inverting input, thus generating a lag between the output and the feedback, which in turn would generate an overshoot.

Noise

Noise is always a problem in electronics. The presence of noise degrades the quality of the signal we are interested in. Everytime we amplify, process, transmit, record or replay a signal, noise is introduced thus worsening the signal to noise ratio. Some common signal to noise ratios are shown below.

Telephone 20 to 40 dB

Cheap cassette player 30 dB

Good tape recorder 60 dB

Professional studio equipment 80 dB

The calculations of noise produced by electronics is complex, but with a few short cuts it is possible to get some useable calculations.

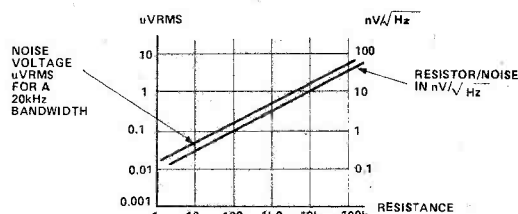


Fig.10. Thermal noise generated by a resistor.

All resistors generate noise due to thermal agitation (Fig.10). Noise is also generated when a voltage is applied to them. Manufacturers generally express this latter noise in uV/V typically 0.1uV/V for metal film devices. For most purposes resistor noise is not a dominating noise source although low level amplifiers perform slightly better with metal film devices. Keeping the resistor values low, helps to obtain low noise operation.

An op amp has several sources of noise generation, Fig.11. there are two noise current generators which both generate noise by flowing through the resistors in the circuit. The resistors themselves generate noise and there is an input voltage noise generator. The total output voltage E_o is given by

$$E_o = \left(\frac{R_A + R_B}{R_C} \right) \times \sqrt{(\text{noise voltage source})^2 + (\text{noise from } I_{n+} \text{Source})^2 + (\text{noise from } I_{n-} \text{Source})^2 + (\text{noise from } R_C)^2 + (\text{noise from } R_A // R_B)}$$

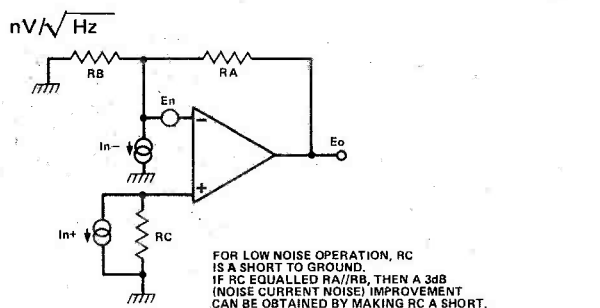


Fig.11. Model of op amp noise generation.

The noise performance curves for a low noise op amp, the SE5534, are shown in Fig.12a,b,c. Graph a shows the input noise voltage density, E_n (ie total RMS noise in a 1 Hz bandwidth at that particular frequency), as a function of frequency. To convert this input noise voltage, ($4nV/\sqrt{Hz}$) into an equivalent input noise generator, we must define the bandwidth of interest. As the noise spectrum is relatively flat above 100 Hz then we can say,

Fig.12a. The SE5534 low noise op amp input noise voltage density.

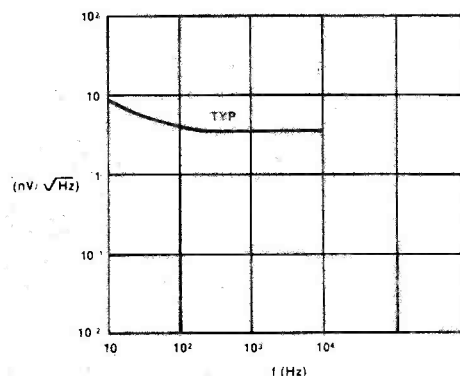


Fig.12b. The variation in total input noise density with source resistance for two frequencies.

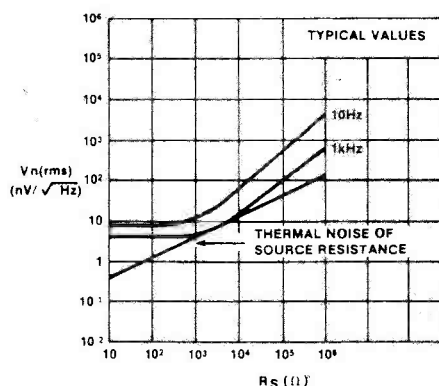
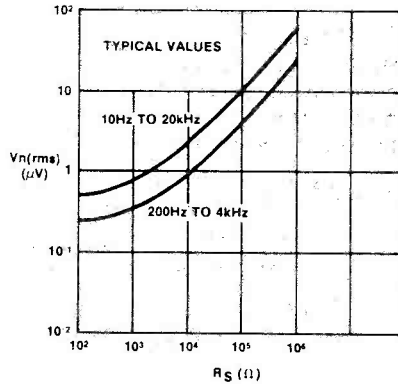


Fig.12c. The equivalent input noise voltage for two bandwidths as a function of frequency.



The equivalent input noise voltage $E_{in} = \sqrt{(E_n^2 \times \text{bandwidth}^2)}$
For 20 kHz bandwidth

$$E_{in} = \sqrt{(E_n^2 \times 20,000^2)}$$

$$E_{in} = (E_n \times 141) \text{ nV RMS}$$

$$\text{But } E_n = 4 \text{ nV}/\sqrt{\text{Hz}}$$

$$\text{Therefore } E_{in} = 4 \times 141 = 0.564 \text{ uVRMS (20 kHz)}$$

Design Example

Q. Calculate the output noise in a 20 kHz bandwidth for the circuit in Fig.13. Assume the voltage and current densities have a flat spectrum (which is not too far from the truth!).

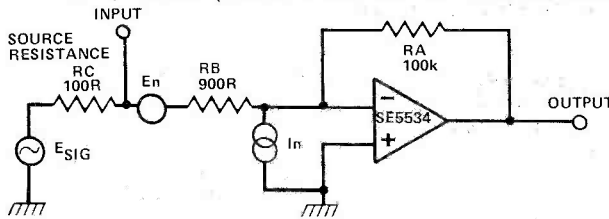


Fig.13. A low noise amplifier.

A. Calculate the individual noise sources.

Resistor Noise

Effective resistor is $RA/(RB+RC)$ 1k0

Therefore thermal noise (from Fig.13b) = $3 \text{ nV}/\sqrt{\text{Hz}}$

Noise Voltage

$$a = 4 \text{ nV}/\sqrt{\text{Hz}}$$

Noise Current

$$c = 0.5 \text{ pA}/\sqrt{\text{Hz}}$$

which sets up a noise voltage through $(RB + RC)$. This noise voltage is $0.5 \text{ pA} \times 1 \text{ k0} = 0.5 \text{ nV}/\sqrt{\text{Hz}}$

Therefore the total noise voltage

$$E_o = \left(\frac{RA+RB+RC}{RA+RB} \right) \times \sqrt{(4)^2 + (0.5)^2 + (3)^2}$$

$$= 101 \times \sqrt{16 + 0.25 + 9}$$

$$= 101 \times \sqrt{25.25}$$

$$500 \text{ nV}/\sqrt{\text{Hz}}$$

For 20 kHz bandwidth, the output noise = 500×141
= 70,500 nVRMS
= 70.5 uVRMS

A 7 mVRMS input signal from, say, a low impedance microphone would result in a 700 mVRMS output signal and give a S/N ratio of $20 \text{ Log } \left(\frac{700}{0.070} \right) = 80 \text{ dB}$

Note that most dominant source in this circuit is the noise generator E_n . As long as the input impedance levels are kept low, then it is the noise generator E_n on its own that can be used as a rule of thumb for calculating absolute and comparative noise performance. For high input impedance applications a FET op amp (with virtually no input noise current) should be used.

Noise Measurements

The noise current voltage psectrums of Fig.12 were measured using a mobile analysing filter (1 Hz bandwidth) plus an RMS meter. A simpler measurement can be performed using the system shown in Fig.14. This will measure the

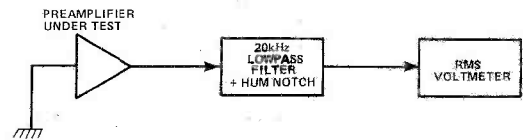


Fig.14. Noise measurement.

equivalent input noise in a specified bandwidth. The low pass filter should be high order device with a steep roll off slope. If a single pole low pass filter is used, then the RMS reading should be corrected by the following equation,

$$\text{'True' RMS noise (for a one pole lowpass filter)} = \frac{\sqrt{\text{measured RMS noise}}}{1.57}$$

(An RC 20 kHz low pass filter would be made from an 820 ohms resistor with a 10 nF capacitor to ground).

Sometimes the signal to noise ratio is quoted in dBA. This means that the noise measurement has been modified by an A weighted curved.

A short chart of op amp performance has been drawn up in Fig.17. It is difficult to compare device performance merely from the noise voltage at one frequency in the spectrum, as the noise spectrum shapes are different from device to device. It is best to refer to the manufacturing data sheet and then to actually breadboard the devices.

DEVICE	NOISE VOLTAGE AT 1kHz nV/√Hz	UNITY GAIN BANDWIDTH MHz	SLEW RATE V/μs
NATIONAL SEMICONDUCTORS LM381A	5.0 NOT OPTIMISED	15	4.7
SIGNETICS SE5534	4.0	10	13
SIGNETICS SE5534A	3.5	10	13
741	20 to 50 NOT USUALLY SPECIFIED	1 to 1.5	0.5
RAYTHEON RC4136	10	3	0.5
RAYTHEON RC4598	10	3	0.5
TEXAS TL071	18 *FET INPUT VERY LOW INPUT NOISE CURRENT 0.01 pA / √Hz	3	13
FERRANTI ZN455T	4.5 (Rs = 510R)	15	—

Fig.15. Op amp performance.

Biasing

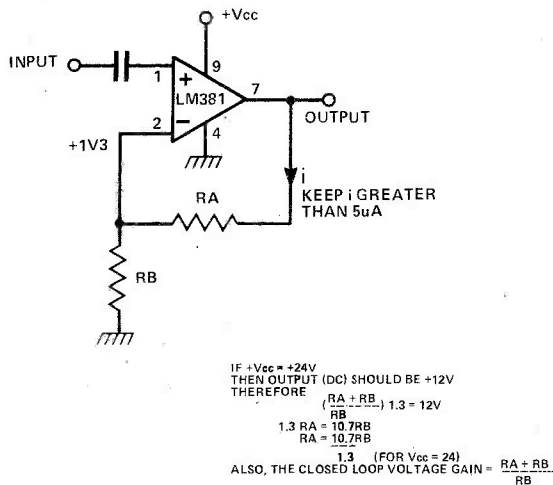


Fig.16. Biasing the LM381 (differential mode).

The base of Q1 is held at +1V3 by a pair of diodes. This preamplifier is often run from a single supply rail and a simple resistor network can be used to bias the output voltage to $\frac{1}{2} V_{cc}$ (Fig.16). Also a single ended amplifier can be constructed (Fig.17). The resistor pair RA, RB determines the DC output level and gain. To increase the AC gain resistor RB can be shorted to ground with a series R,C network.

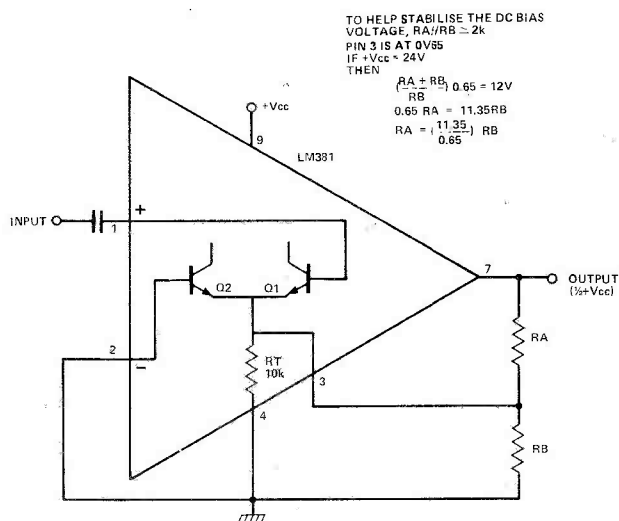


Fig.17. Single-ended biasing.

Design Example

Q. Design a preamplifier using the LM381 with a gain of 30 dB and a low frequency roll off of 20 Hz running from a +24 V power supply.

A. The design calculations are shown in Fig.18.

Record Preamplifier

When replaying a record from a magnetic cartridge it is necessary to have a preamplifier with an RIAA playback equalisation (Fig.19). A magnetic pick up generates a voltage

FIRST CALCULATE THE DC BIAS CONDITIONS
 $\frac{(RA + RB)}{RB} \cdot 1.3 = 12V$

$RA = 8.23 RB$
LET $RB = 10k$
THEN $RA = 82k$
THE AC VOLTAGE GAIN = X33

$\approx 1 + \frac{RA}{RC}$
THEREFORE $RC = \frac{RA}{32} = 2.56k$

LET $RC = 2k7$ (THE NEAREST PREFERRED VALUE)

THE LOW FREQUENCY ROLL OFF
 $f_L = \frac{1}{2\pi RC RC} = 20Hz$

THEREFORE $C3 = \frac{1}{2\pi \times 20 \times 2k7} = 3u0$

OUTPUT NOISE = 15uVRMS (APPROXIMATELY)

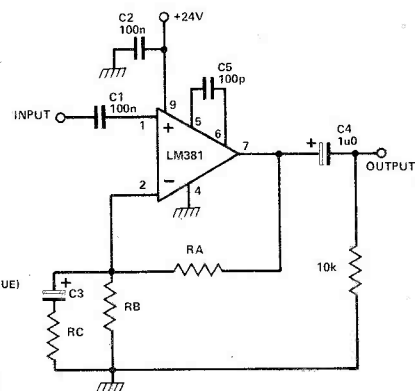


Fig.18. A 30 dB amplifier.

that is proportional to the velocity of the sideways movement of the stylus. So high frequencies produce large outputs and vice versa. Also, to assist replay electronics, the recording is given a 12 dB de-emphasis from 500 Hz to 2120 Hz. Thus, to restore a flat output it is necessary to equalise the signal from the pick up with an RIAA curve. As a rule of thumb,

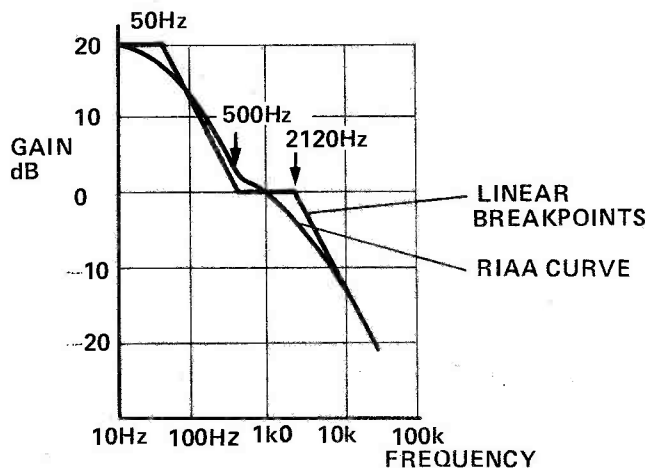


Fig.19. RIAA equalisation.

a typical magnetic pick up will generate 5 mVRMS at 1 kHz, although the recording level and make of pick up will effect this figure.

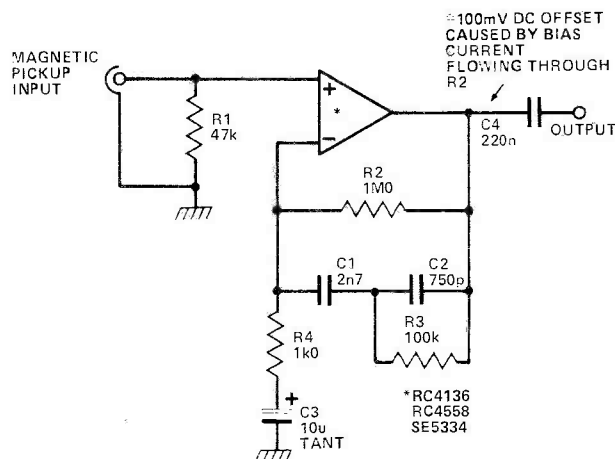


Fig.20. An RIAA-equalised preamplifier.

$$\text{Low frequency gain} = \frac{R2}{R4} = 60 \text{ dB}$$

$$\text{Low frequency rolloff} = \frac{1}{2\pi R4 C3} = 15 \text{ Hz}$$

$$50 \text{ Hz breakpoint} = \frac{1}{2\pi R2 C1}$$

The gain drops at -6 dB/octave beyond this point
500 Hz breakpoint $\frac{1}{2\pi R3 C1}$

Now the gain remains constant until the next breakpoint
AC gain at 1 kHz = $\frac{R3}{R4} = 40 \text{ dB}$

$$2120 \text{ Hz breakpoint} = \frac{1}{2\pi R3 C2}$$

The gain now falls at -6 dB/octave beyond this frequency.

A 5 mVRMS signal at 1 kHz will result in a 500 mVRMS (1V4 pp) at the preamplifier output. If the amplifier is powered from $\pm 12 \text{ V}$, then there is an overhead margin of

$$\left(\frac{\text{maximum output swing} = 20 \text{ V}}{\text{typical swing} = 1 \text{ V4}} \right) = 14,$$

which is 23 dB. The noise spectrum of the op amp will be multiplied by the RIAA curve which would complicate any noise performance calculations. However, an op amp with an equivalent input noise of 0.5 μV should give a signal to noise performance of better than 76 dB which is superior than that of the disc itself. Because of the large low frequency gain care must be taken to avoid mains hum pick up. Keep the input wiring away from the mains cables and transformers, use low noise screened cable and wire this cable as close as possible to the preamplifiers.

Problems

Often a preamplifier will pick up radio signals. Usually, the radio signal is picked up by the input wiring to the preamplifier and is rectified by the transistor input stage. Then it is amplified by the rest of the audio amplifier and you end up with permanent broad band radio reception. There are several solutions that can be tried, Fig.21. A low pass filter made from an LC or an RC section will attenuate the 'pick up' interference. These devices must be physically close to the op amp. If possible use a PCB ground plane. Also, a conductive metal screen (metal foil is often used) surrounding the preamplifier will help.

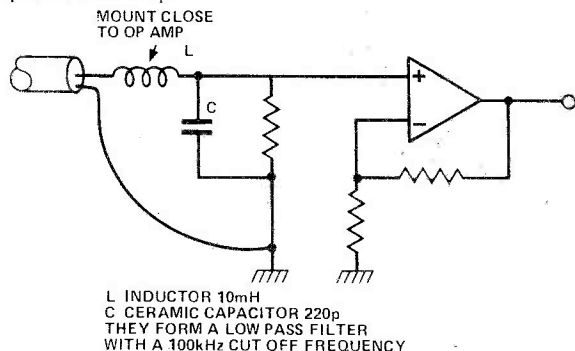


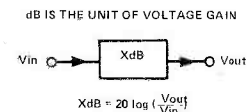
Fig.21. Removing RF interference.

Hum can also be a problem. If the hum is at 50 Hz then the source of it is probably magnetic. Check the wiring to see if any signals pass near to the mains section. Magnetic screening is difficult to implement. The best design solution is to put as much distance between the sensitive input and the mains

section as possible. If it is possible try rotating the mains transformer (using a gloved hand, the other hand in your pocket). Often the size of the hum can be reduced by re-orientating the transformer. If the hum is 100 Hz, then the source is either the supply rails or the power supply layout. A larger smoothing capacitor will reduce the power supply ripple. If the hum has a sharp buzz then the problem is probably the charging current pulses in the power supply. If the layout is bad, these current pulses generate voltage pulses that get added into the ground reference voltage, thus causing the hum.

Gain

When designing an audio system it is necessary to know what the normal signal level at any point will be and also the signal gains and attenuations of various units. It has been found that the most useful way to describe levels and gains is with the logarithm decibel, Fig.22. Signal gains in dB are additive. That is, a signal passing through a series of gains of +10, +20, -30, +6 dB will end up with an overall gain of +6 dB.



dB	APPROXIMATE RATIO
+60	1000
+40	100
+20	10
+10	3
+6	2
+3	1.4
+0	1
-3	0.7
-6	0.5
-10	0.33
-20	0.1
-40	0.01
-60	0.001

dBm	Vpp	VRMS
+20	21.9V	7.75V
+6	4.38V	1.55V
+0	2.19V	0.775V
-6	1.09V	0.387V
-20	0.219V	0.077V
-40	0.109V	0.0387V
-60	0.0545V	0.0194V

dBm IS THE UNIT OF VOLTAGE LEVEL
0dBm IS 1mW OF POWER INTO A 600R
LOAD

Fig.22. The dB and dBm story.

A typical audio system is shown in Fig.23. A low impedance microphone might typically give a -50 dBm output signal which will have to be given a 56 dB (x 600) gain to bring it up to line level (about +6 dBm). The line driver should

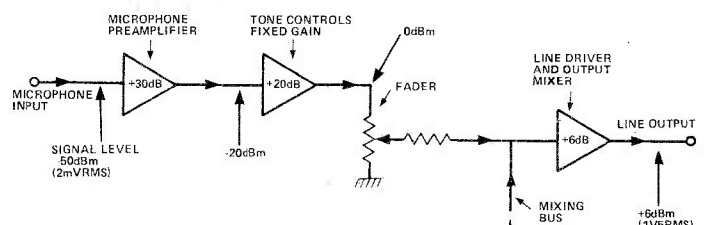


Fig.23. One channel of a mixing desk.

be capable of driving +20 dBm into 600 ohms at 20 kHz without generating significant distortion. Some line drivers are, in fact, capable of driving 30 ohm loads, but these units are small high quality power amplifiers. ➔

2. LARGE SIGNAL, OR POWER, AMPLIFIERS

A power amplifier must deliver power into a load without generating significant distortion or bursting into oscillation or burning itself out. Power amplifiers are, however, prone to all these effects and great care is needed during their design.

Power

Power is measured in watts and is defined as the product of $V_{RMS} \times I_{RMS}$ (Fig.1c), where RMS is the equivalent DC value. That is, a 2 Vpp sinewave has the DC value of 0V7. The 2 Vpp sinewave will generate as much heat in a load as a 0V7

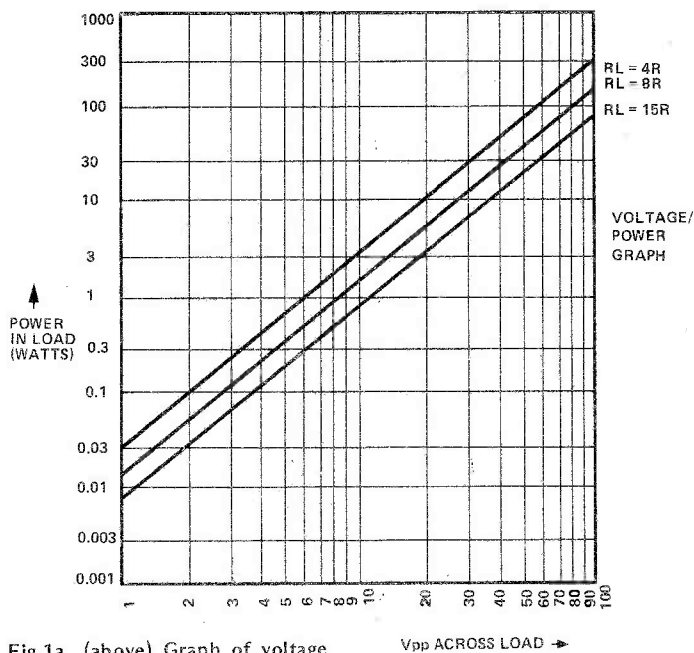


Fig.1a. (above) Graph of voltage against power.

	4R	8R	15R	RL
1V	0.031	0.015	0.008	
3V	0.28	0.140	0.075	
10V	3.125	1.562	0.833	
30V	28.15	14.062	7.50	
100V	312.5	156.25	83.33	
Vpp ACROSS RL	POWER IN RL			

Fig.1b. (left) The power dissipated in a load against drive voltage.

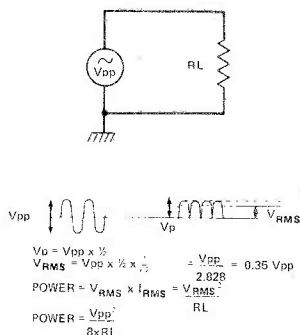


Fig.1c. (left) The measurement of power.

DC voltage. The chart in figure 1b shows the power dissipated in a load against drive voltage. If you have an amplifier that has a maximum output voltage swing of ± 10 V, then the maximum power output will be 12.5 watts into a 4 ohm load (from Fig.1a). Note that the amplifier must be able to deliver a peak current of 2.5 Amps. Whilst dumping power into the load, the amplifier will be dissipating heat itself. Most monolithic devices are documented with design graphs of output power versus amplifier dissipation of power efficiency. These will enable you to determine the amplifier's maximum power dissipation. As a rule of thumb, this equals the maximum sinewave power that can be dumped into the load. A 10 watt amplifier may have to dissipate a maximum of 10 watts of heat, although this level of dissipation would not be normal in general use. Manufacturers information usually gives the thermal resistance of the junction to case. If this was say $3^\circ\text{C}/\text{watt}$ then a 10 watt dissipation would raise the junction temperature by 30° above ambient (25° raising to 55°C). This is only true if the case temperature remains at ambient temperature, that is if the case is contact with an infinite heat sink. The heatsink may be anything from nothing (free air dissipation) to near infinite. It is important that the amplifier chip junction does not get very hot (above 100°C). The power chips of the amplifier age very quickly at elevated temperatures suffering from deteriorating characteristics and a short life time. This is why power amplifiers and power supplies are common failures in equipment. When the chip is heated up it expands. The chip is glued to its case and so by expanding it stresses the glue and eventually causes it to fracture. This thermal cycling increases the thermal resistance of the chip to the case and so the chip ends up operating at an even higher temperature.

Other heatsinking materials are used in the construction of power devices such as heat conducting plastics and pastes (Beryllium oxide). Manufacturers often provide design graphs of maximum dissipation versus temperature for various heatsink thermal resistances. These help to select an acceptable heatsink. Often if you are using the chassis as a heatsink it is impossible to calculate the temperature rise and it has to be done by trial and error. (As a rule of thumb I am satisfied if I can place my finger on the device for 5 seconds indicating that case temperature is no more than 80°C).

Distortion

A simple power amplifier is shown in figure 2. An op amp provides the voltage gain and a NPN, PNP transistor pair forms a current amplifier. Any distortions or nonlinearities are ironed out by the surplus loop gain of the op amp. The transfer characteristic of Q1,Q2 shows that there is a dead zone of

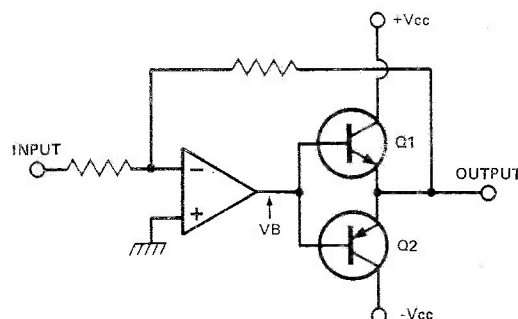


Fig.2. A simple power amplifier.

$\pm 0V6$ where neither transistor is ON. If a low frequency sine-wave is connected to the input (the op amp having a surplus loop gain of 1000 at this frequency) then the output will be a sine-wave with a small amount of crossover distortion. The distortion level will be

$$\frac{\pm 0V6}{1000} = \pm 0.6 \text{ mV.}$$

However, as the frequency is increased, the surplus loop gain will decrease causing the distortion to rise. At higher frequencies the slew rate of the op amp becomes noticeable (Fig.3). When the input signal crosses 0 V the output of the op amp has to change from $+0V6$ to $-0V6$. If the slew rate is $0V5/\mu\text{S}$ then the time taken to travel the $1V2$ distance is $2.6 \mu\text{S}$. Thus a $2.6 \mu\text{S}$ chunk of the signal is missing out of each half cycle. The problem may be overcome by biasing the

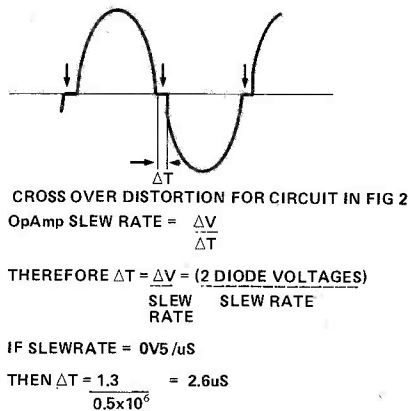


Fig.3. The effect of slew rate at higher frequencies.

two transistors so that they are both conducting. Then the crossover distortion becomes reduced to a reasonable level. The slew rate still needs to be considered. An amplifier delivering a 40 Vpp sine-wave at 20 kHz has a fastest slew rate of $2V5/\mu\text{S}$ (this represents a power of 25 watts into 8 ohms). If the amplifier has not enough slew rate the output will become distorted. Manufacturers generally provide graphs of distortion (THD) versus power output and frequency (Fig. 4). For the power curve, the onset of distortion is caused by the amplifier clipping at its power rails, whereas for the frequency curve the distortion rises as the surplus loop gain falls.

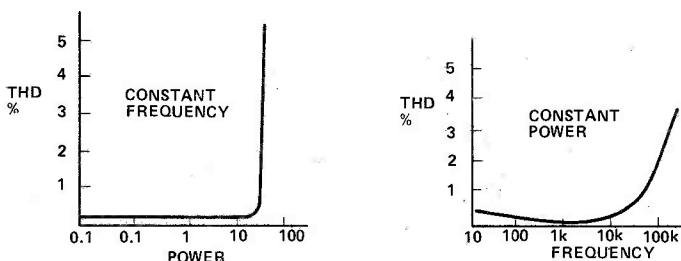


Fig.4. THD versus power and frequency.

Distortion is measured at various power levels and frequencies using the equipment shown in figure 5. A deep notch removes

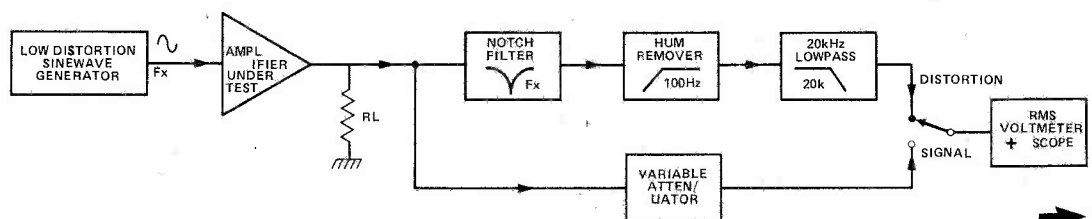


Fig.5. THD measurement.

the test sine-wave leaving behind the distortion products. Generally 0.1% THD is common for monolithic amplifiers.

Stability

Power amplifier performance is very similar to that of op amps. They have a large open loop gain that is stabilised by resistive feedback (Fig.6). Note that the amplifier described in this graph is normally inverting (180° DC phase shift) but that it suffers a phase shift as the frequency increases. The phase shift at the unity gain frequency is shown as the phase margin. If the phase margin falls to zero anywhere before the unity gain frequency then the amplifier will oscillate. This is simply because the loop phase shift will be zero at a loop gain of greater than unity, which are the conditions for an oscillation. A large phase margin is desirable.

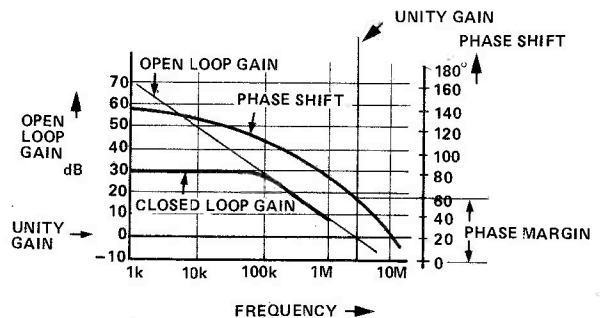


Fig.6. Gain and phase response.

Various techniques are available for preventing instability. Often a series RC network is connected from the amplifiers output to ground. This reduces the high frequency gain and thus reduces the unity gain frequency. Local power supply decoupling should be used. Current loops, whereby the output current generates a voltage in the signal ground wire which gets fed back to the input can cause bursts of high frequency oscillation. Also high input impedances can capacitively pick up the output signal and burst into oscillation. Increasing the closed loop gain may prevent some forms of instability, swearing will not! Figure 7 shows some typical instability problems.

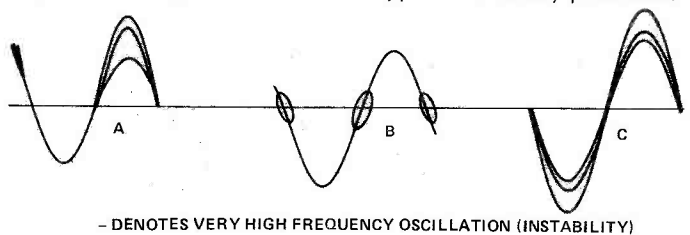


Fig.7. Instability; A, on one half cycle; B, at crossover; C, at all points.

- (a) The sine-wave oscillates on one half cycle. Really a power amplifier is two amplifiers, one half handling positive signals, the other, negative signals. Thus it is quite possible that the amplifier can be stable for negative signals but not positive ones.

- You may not hear the effects of high frequency oscillation but it does cause RF interference and generates waste power. It

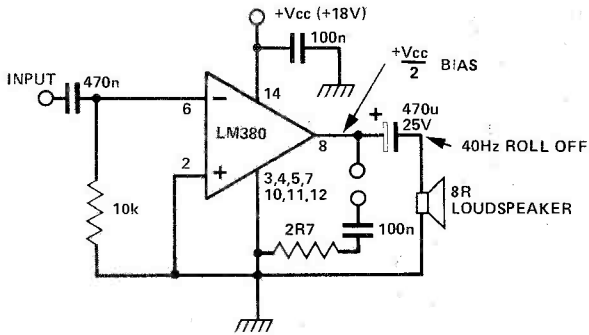
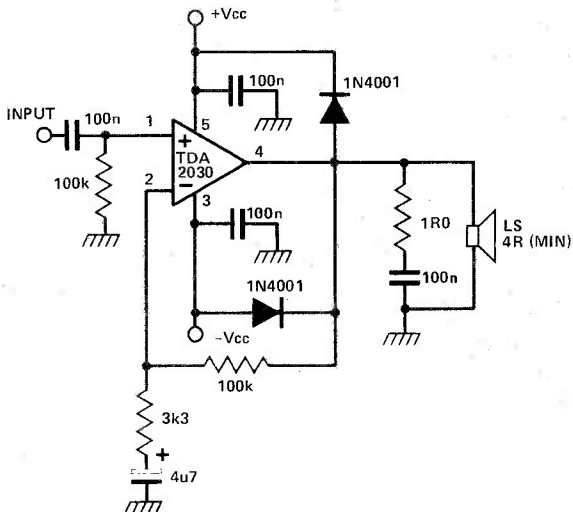


Fig.9. Medium power audio amplifier. The LM380 will work with a supply voltage range of 8 to 22 V. It can deliver 4 watts of power into 8 ohms at 20 V, although a good heatsink is needed for this level. The inputs are ground referenced and the output is automatically biased to $\frac{1}{2} V_{cc}$. The voltage gain is fixed at 34 dB. It also has a short circuit proof output and internal thermal limiting.



can burn out output stages and even loudspeaker crossovers.

The following five design examples demonstrate how to produce a solution to an amplifier problem. It is now possible to buy an amplifier for most general purpose uses. A wide selection of monolithic devices and modules cover the 0.25 to 100 watt power range. It is rare to have the time or the ability to improve upon this range. The art of designing is to select the most suitable solution on the basis of size, cost and performance.

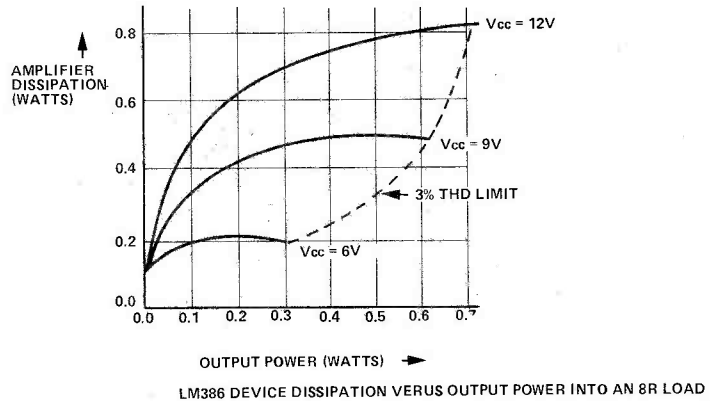
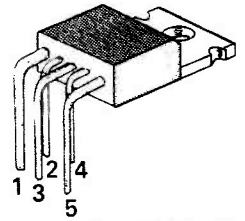
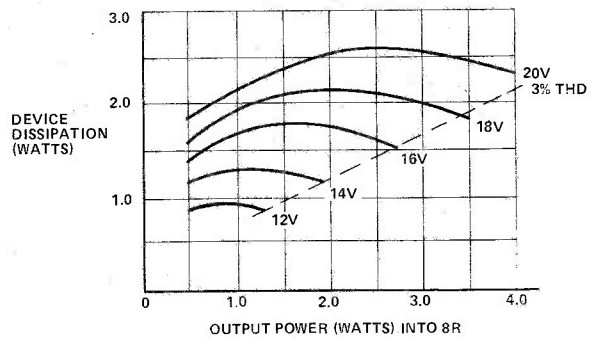


Fig.8. Low voltage, low power battery operated amplifier. The LM386N operates over a supply range of 4 to 12 V. It can deliver 0.7 watts into 8 ohms at 12 V, although, at this level, some heatsinking would be advisable. The typical battery drain is 4 mA. The voltage can be varied from 20 to 200, as shown it is 20. An AC short across pins 1 and 8 will increase the gain to 200. With a resistor in series the gain can be set to anything from 20 to 200. For gains greater than 20, a bypass capacitor (100n to ground from pin 7) should be used. Even with a supply voltage of only 4 V, there is an output voltage swing of greater than 2 V.



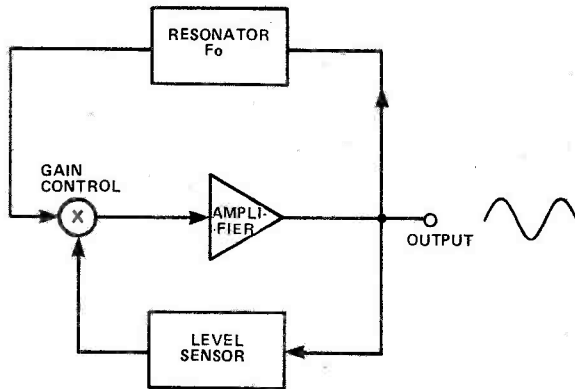
FEATURES

TO 220 PACKAGE – EASY TO HEATSINK
POWER SUPPLY RANGE ± 6 TO ± 18 V
QUIESCENT CURRENT 40mA
POWER OUTPUT 14 WATT (4R)
9 WATT (8R)
CLOSED LOOP GAIN 30dB

Fig. 10. 9 to 14 watt amplifier. The TDA2030 is a Hi-Fi audio amplifier which has short circuit protection and thermal shutdown. It can operate from supply rails of ± 6 to ± 18 V. At a ± 14 V supply the guaranteed output power is 12 watts into 4 ohms and 8 watts into 8 ohms. Harmonic and crossover distortion is low being typically 0.05% at 1 kHz for 7 watts of power output. The recommended closed loop gain is 30 dB. The two diodes protect the amplifier from back EMF voltages from the speaker.

3. OSCILLATORS

It seems to be a fact of life that amplifiers oscillate and oscillators won't! Generally there is little difference between the two. Both devices are amplifiers with feedback. The conditions for stable sinusoidal oscillation are shown in Fig.1. The higher the Q of the resonator the more stable is the resonant frequency, and the purer the sine wave. To stabilise



CONDITIONS FOR OSCILLATION
 * PHASE SHIFT AROUND LOOP = 0°
 * LOOP GAIN = UNITY
 * IF SINEWAVE FALLS BELOW SET AMPLITUDE, GAIN INCREASES
 * IF SINEWAVE INCREASES ABOVE SET AMPLITUDE, GAIN DECREASES

Fig.1. Conditions for a stable sine wave oscillator.

the signal level an automatic gain control circuit is used. This can be anything from simple diodes or thermistors to elaborate AGC systems. The smoothness with which the AGC works will determine the sine wave purity. A thermistor circuit might well introduce distortion at low frequencies by changing its resistance during one half cycle of oscillation. Very pure sine-wave oscillators (better than 0.001% distortion) employ slow acting AGC systems to control the loop gain.

Wien Bridge

The well known Wien Bridge oscillator is shown in Fig.2a. A frequency sensitive feedback network is constructed from R1, C1 and R2, C2. This network has a peak in its amplitude response which also corresponds to zero phase shift. At this frequency the attenuation is $\times 1/3$ and so to ensure oscillation

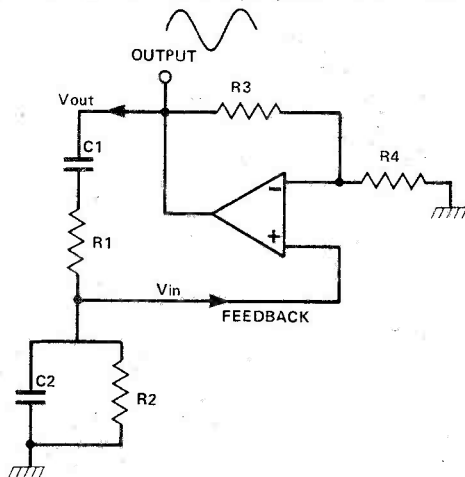


Fig.2a. A Wien Bridge oscillator.

the amplifier must have a voltage gain of at least $\times 3$. To stabilise the amplitude a thermistor is used in the feedback

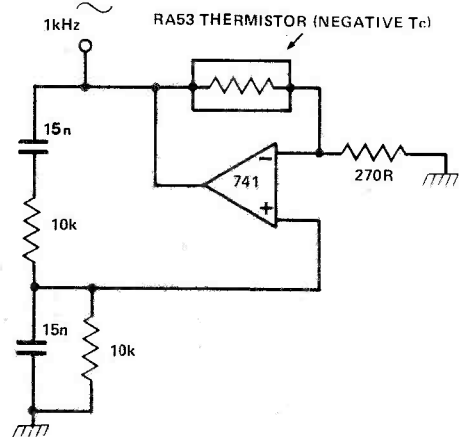


Fig.2b. To stabilise the amplifier a thermistor is used in the op amp feedback loop.

loop of the op amp. As the oscillation amplitude increases, the thermistor heats up, drops in resistance and so reduces the gain. The circuit suffers from amplitude bounce when the frequency is altered. Also, the op amp phase shift, which increases with increasing frequency, must be taken into consideration when designing this oscillator. Another sine wave oscillator is shown in Fig.3. This generates both sine and cosine outputs. The circuit is a state variable filter with posi-

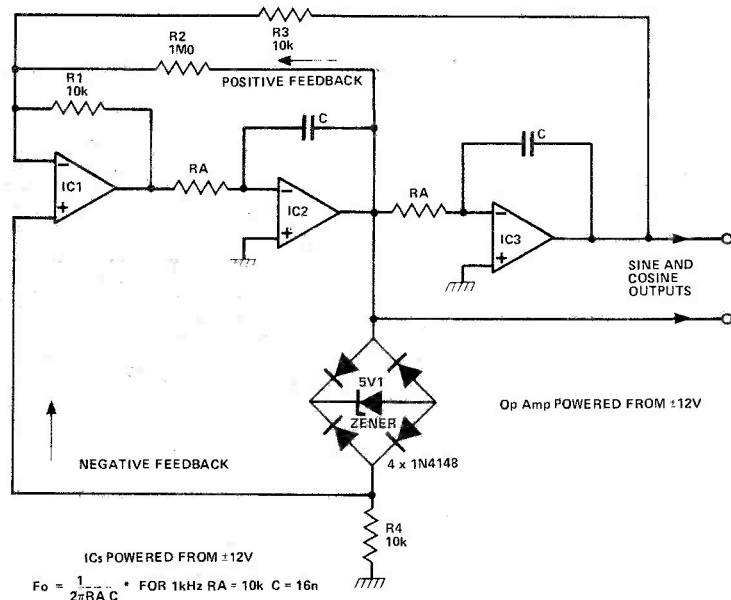


Fig.3. A state variable sine/cosine oscillator.

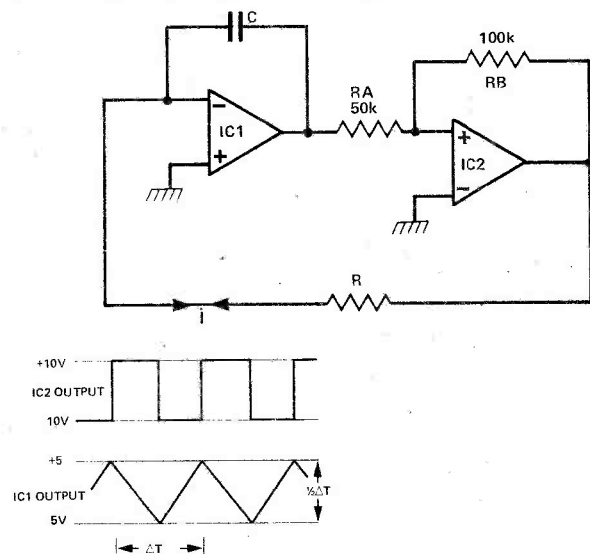
tive feedback (R2) to ensure oscillation and amplitude limiting (the diode bridge) to stabilise the sine wave level. The distortion may be trimmed by adjusting the amount of positive feedback. The oscillation frequency is set by RA and C.

A triangle/square wave oscillator may be constructed from a pair of op amps (Fig.4). IC1 is an integrator, the output of which ramps up and down between the hysteresis levels set by the Schmitt trigger, IC2. If the output of IC2 is set to $\pm 10V$ then the hysteresis level will be $\pm 10 \times \frac{RA}{RB}$ volts

The oscillation frequency and triangle symmetry is linearly proportional to the output swing of IC2. If a variable frequency oscillator is wanted, then resistor R can be connected to the wiper of a potentiometer fed from IC2 output.

Design Example

Q. Design a triangle oscillator with a 2 Vpp triangle output, oscillation frequency of 1 kHz, operating from ± 12 V power supplies, using circuit in Fig.4.



INVERTING INPUT OF IC1 IS A VIRTUAL EARTH
THEREFORE $i = \frac{10V}{R}$

CURRENT CHARGES AND DISCHARGES CAPACITOR C IN
THE INTEGRATOR GOVERNED BY THE RELATIONSHIP

$$C \frac{dV}{dt} = i$$

THEREFORE $\frac{dV}{dt} = \frac{i}{C} = \frac{10}{RC}$

$$\frac{dV}{dt} = \frac{\Delta V}{\Delta T}$$

SO, $\frac{1}{\Delta T} = \frac{dV}{dt} \times \frac{1}{\Delta V} = \frac{10}{RC \Delta V}$

WHERE $\Delta V = 20V$ AND $\frac{1}{\Delta T} =$ FREQUENCY OF OSCILLATION F_o

THEREFORE $F_o = \frac{1}{\Delta T} = \frac{10}{RC \times 20} = \frac{1}{2RC}$ Hz

Fig.4. A triangle/square wave oscillator.

A. Assume an output voltage swing at IC2 of ± 10 V.

For ± 1 V Hysteresis,

$$RA = \frac{RB}{10}$$

Let $RB = 100k$, then $RA = 10k$

$$F_o = 1 \text{ kHz} = \frac{1}{\Delta T} = \frac{i}{C \Delta V} = \frac{10}{C \times 20}$$

$$\text{Therefore } CR = \frac{10}{4 \times 1000} = 2.5 \times 10^{-3}$$

Let $C = 100n$

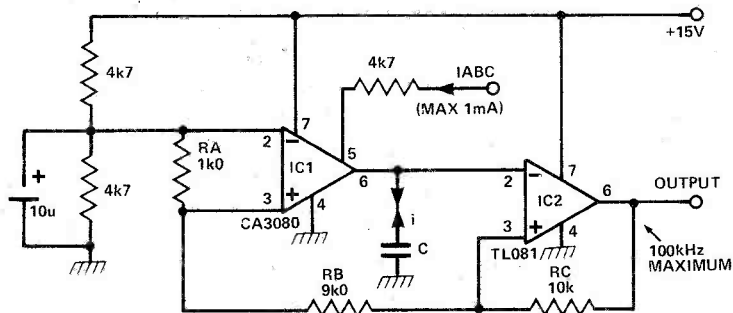
$$\text{Then } R = \frac{2.5 \times 10^{-3}}{10^{-7}} = 25k$$

$\frac{\Delta V}{\Delta T}$

Note that $\frac{\Delta V}{\Delta T}$ is 4000 V/sec. When designing this type of oscillator the slew rate of the integrator and Schmitt trigger need to be considered, although in this case virtually any op amp will be OK.

Linear VCO

A linear voltage controlled oscillator (VCO) is shown in Fig.5. This again is a triangle square wave oscillator although the squarewave is the only buffered output. The CA3080 is used as a current source for charging and discharging C. The charging current is equal to I_{ABC} , which is true for several



CURRENT i THAT CHARGES $C = I_{ABC}$
VOLTAGE AT PIN 3 IC2 IS A 6.5Vpp SQUAREWAVE
THEREFORE, THE TRIANGLE WAVEFORM IS ALSO 6.5Vpp
EQUATION FOR CHARGING C,

$$\frac{\Delta V}{\Delta T} = \frac{i}{C} = \frac{I_{ABC}}{C}$$

$$F_o = \frac{1}{\Delta T} = \frac{I_{ABC}}{C \Delta V} = \frac{I_{ABC}}{C \times 6.5 \times 2}$$

* IF $C = 680p$, $I_{ABC} = 250\mu A$,

$$\text{THEN } F_o = \frac{250 \times 10^{-6}}{680 \times 10^{-12} \times 6.5 \times 2} = 28.28 \text{ kHz}$$

Fig.5. A linear VCO.

decades of current. The Schmitt trigger uses a TL081 which has a slew rate of 13 V/ μ s. As the squarewave output voltage is 13 V then the rise and fall times are 1 μ s each. This enables the VCO to run at frequencies up to 100 kHz. As this frequency is approached the VCO loses its linearity, due to time delays in the circuits.

Another VCO is shown in Fig.6. This has two buffered outputs, a triangle and a square wave. Again, the oscillation frequency is dependent on the output voltage swing of the Schmitt trigger, IC2. However, if a stabilised power supply is used this circuit behaves very well. Superior performance can be obtained by replacing Q1 with a switching FET. The aberrations caused by saturation voltage and storage time are then removed. Also fast FET op amps will improve high frequency performance.

* ASSUME OUTPUT SWING OF IC2 IS $\pm 10V$
THEREFORE, IC2 SWING WILL BE $\pm 5V$

DURING HALF CYCLE A,

$$i_A = (V_{in} - 1/3 V_{in})$$

$$i_A = \frac{(V_{in} - 1/3 V_{in})}{R_1 + R_2}$$

$$i_A = \frac{V_{in}}{300k}$$

DURING HALF CYCLE B,

Q1 IS ON AND SO THE JUNCTION
OF R1,R2 IS SHORTED TO GROUND

$$i_B = \frac{1/3 V_{in}}{R_2} = \frac{V_{in}}{300k}$$

THEREFORE, THE CURRENT THAT CHARGES AND
DISCHARGES C IS THE SAME MAGNITUDE IN BOTH
HALVES OF THE CYCLE

$$\text{THEREFORE } \frac{\Delta V}{\Delta T} = \frac{i}{C} = \frac{V_{in}}{300k \times C}$$

$$\text{OSCILLATION FREQUENCY } F_o = \frac{1}{\Delta T} = \frac{V_{in}}{300k \times C \times \Delta V} = \frac{V_{in}}{300k \times C \times 20}$$

$$F_o = \left(\frac{V_{in}}{C} \times 0.166 \times 10^{-6} \right) \text{ Hz}$$

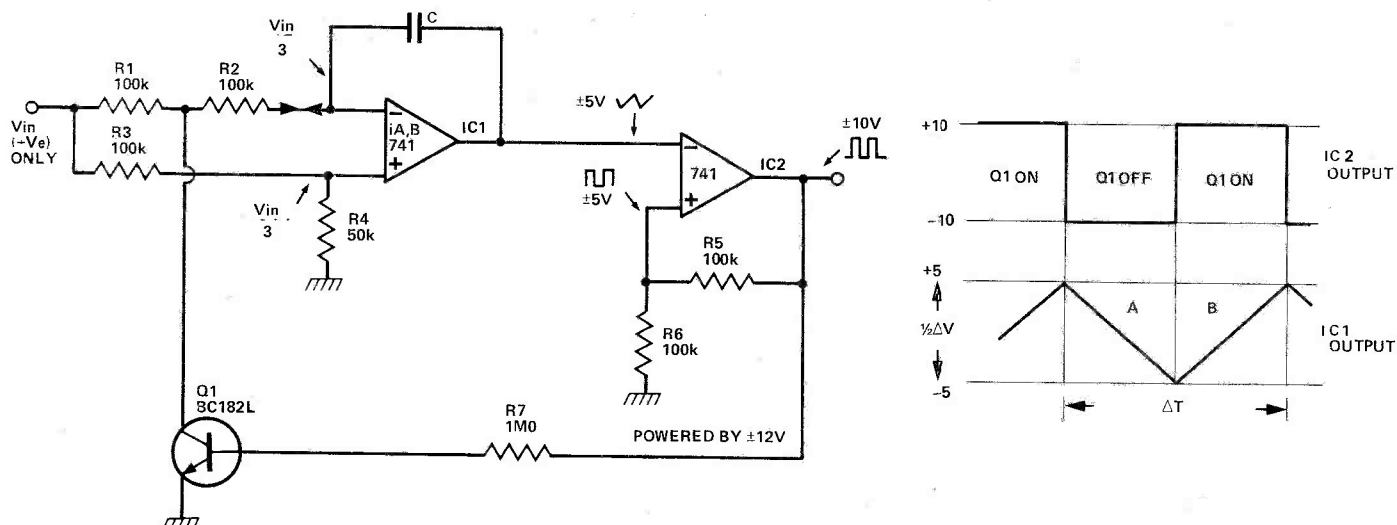


Fig.6. A linear triangle/square wave VCO.

The 555

The 555 timer chip (Fig.7) can be used as an oscillator (Fig.8). Capacitor C is charged up via RA and RB. When the voltage at pin 6,2 reaches $\frac{2}{3} V_{cc}$ the discharge transistor is turned ON. When the voltage falls to $\frac{1}{3} V_{cc}$ the discharge

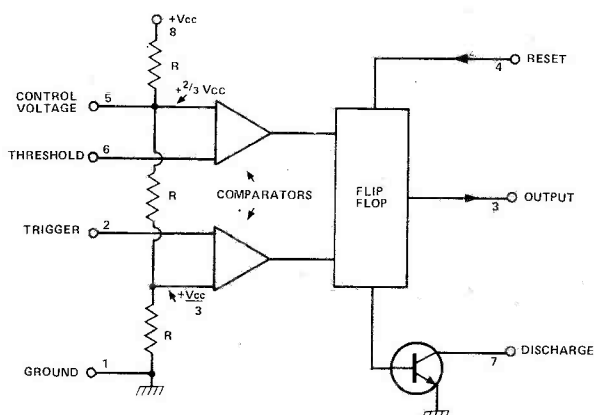


Fig.7. The timer chip.

transistor is turned OFF and the charging process repeats itself. As power supply voltage terms appear in both the numerator and denominator of the charging equation, it drops out and so the oscillation frequency is hardly effected

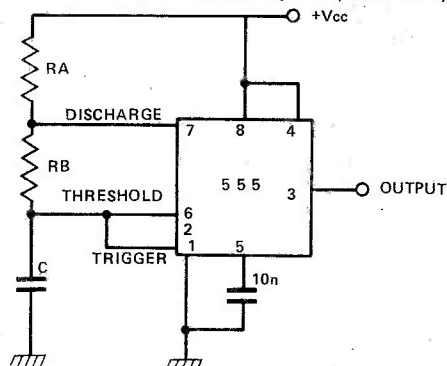


Fig.8. A simple oscillator based on the 555.

by supply voltage changes (typically $0.3\%V$). Also the temperature stability is good, typically $50 \text{ ppm}/^\circ\text{C}$.



A low power 555 oscillator is shown in Fig.9. This employs a CMOS version of the chip which consumes a mere $120 \mu\text{A}$. Capacitor C is slowly charged by current i and rapidly discharged by Q1.

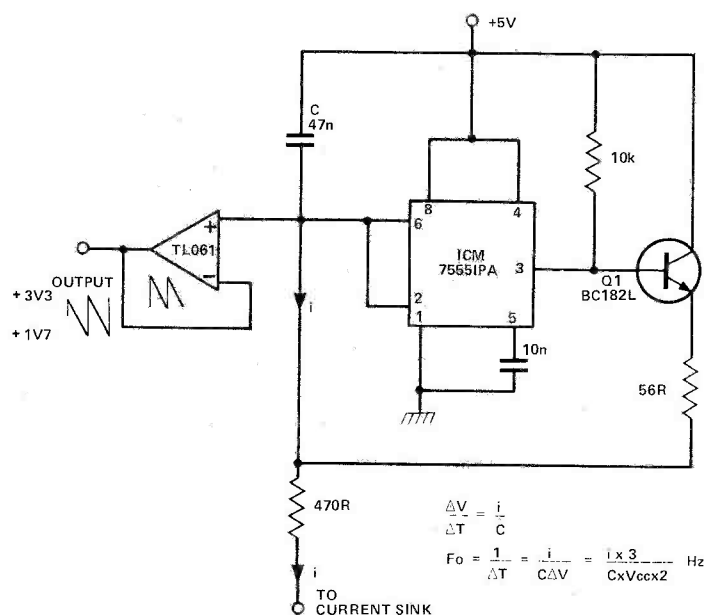


Fig.9. A linear VCO built around the ICM7555, the CMOS 555.

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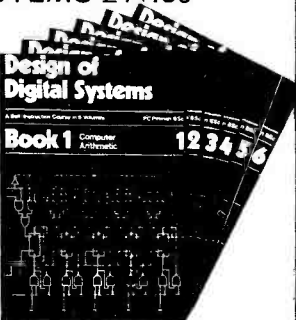
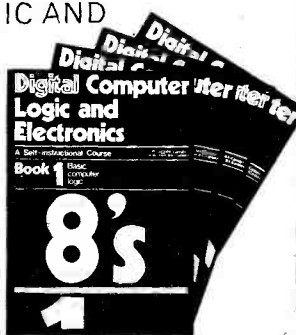
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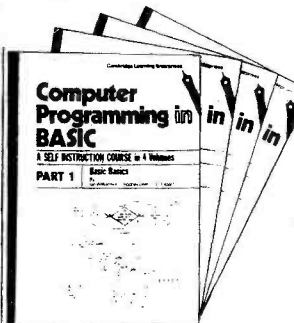
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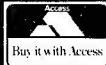
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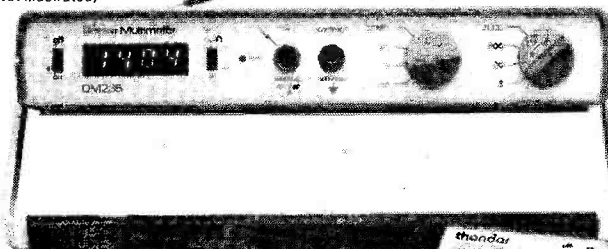


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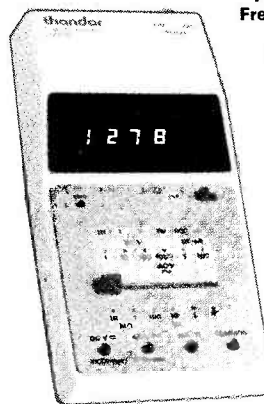
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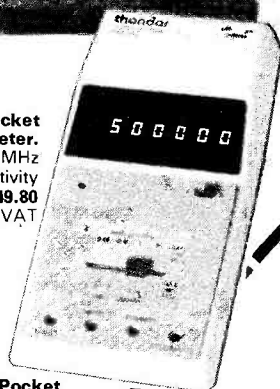
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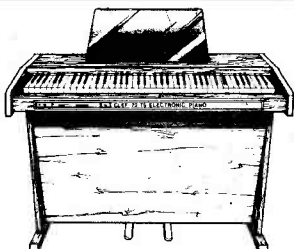
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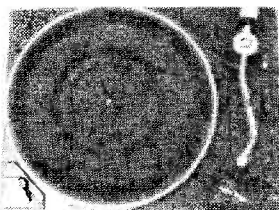
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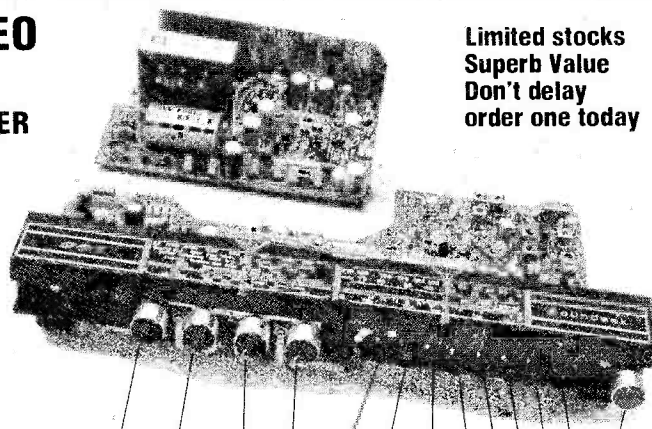
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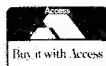
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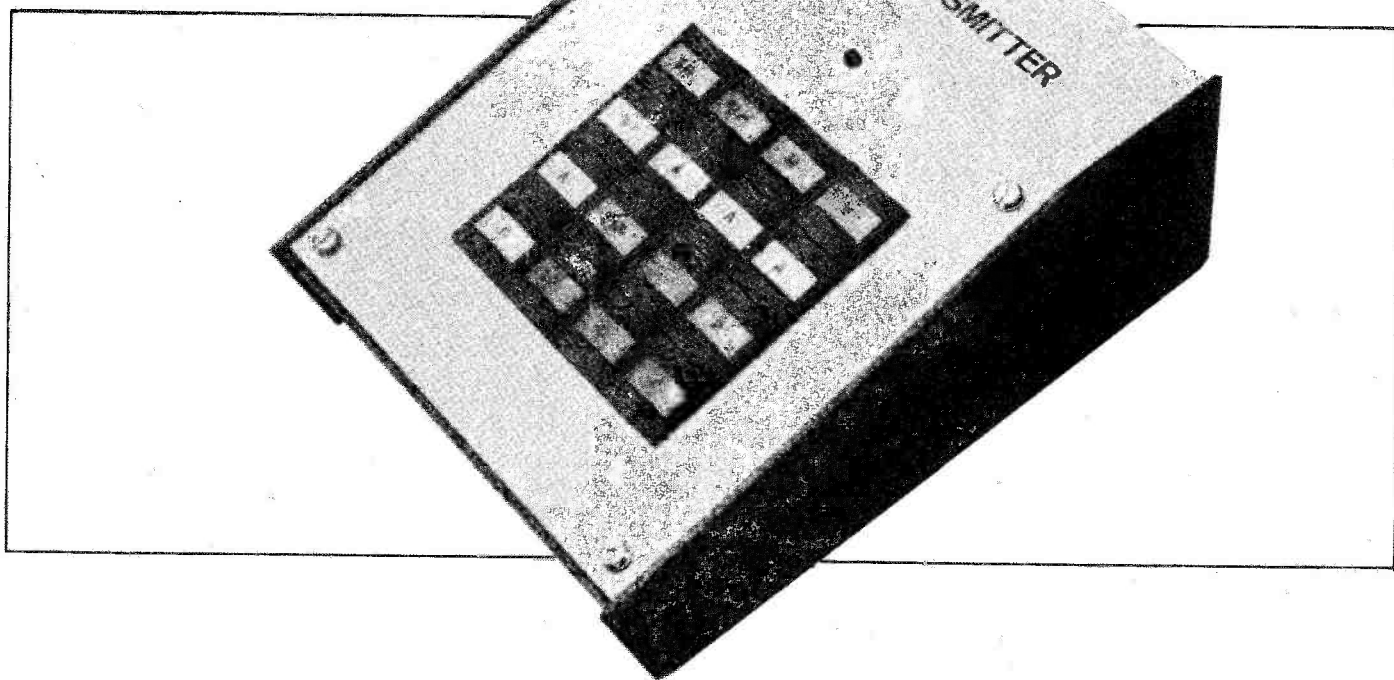
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INFRA-RED REMOTE CONTROL

This concluding part of our IR60 remote control project covers construction of the transmitter and setting up the system.



The transmitter circuit is constructed on two PCBs, a single-sided board being used to hold most of the electronic components and a double-sided board being used to hold the matrix of 16 keypad switches. The double-sided board is best tackled first.

The double-sided PCB has 16 pin-through connections, which are used to connect the tracks on different sides of the board and to make external connections. Start construction by fitting Veropins through these 16 positions, remembering to solder the pins on both sides of the board where appropriate. Next, solder diodes D1 to D4 into position on the PCB and then solder the bodies of the 16 keypad switches into place: the switch caps and bezels can now be snapped on to the switch bodies.

The completed keypad assembly can be mounted to the front panel of the transmitter case (see Buylines) via four 12mm x 6BA-tapped stand-off pillars, after first providing a suitable cut out in the front panel. Use ¼ inch 6BA screws to fix the four pillars to the PCB, then pass the keypad through

the cutout so that the switch tops protrude slightly and finally epoxy the four pillars to the back of the front panel.

The single-sided PCB can be built next. First, insert all Veropins and the single wire link. Next, fit the resistors, IC socket, semiconductors, capacitors and L1. Note that C1 is a PCB-mounting capacitor with its legs bent at right angles so that it lies flush on the PCB. The completed board can be fitted in the case with stickypads.

The two infra-red transmitter diodes can be fitted next. They are mounted through the back of the case, approximately 32 mms apart. Take special care to fit these diodes in the correct polarity.

The final stage of construction is the interwiring of the two boards and the LEDs, etc. Take special care here, particularly when wiring the switch board to the main circuit. The battery is wired directly to the transmitter circuitry and can be fitted into the case with stickypads.

When construction is complete, activate each of the 16 keypad switches in turn and check in each case that the front-

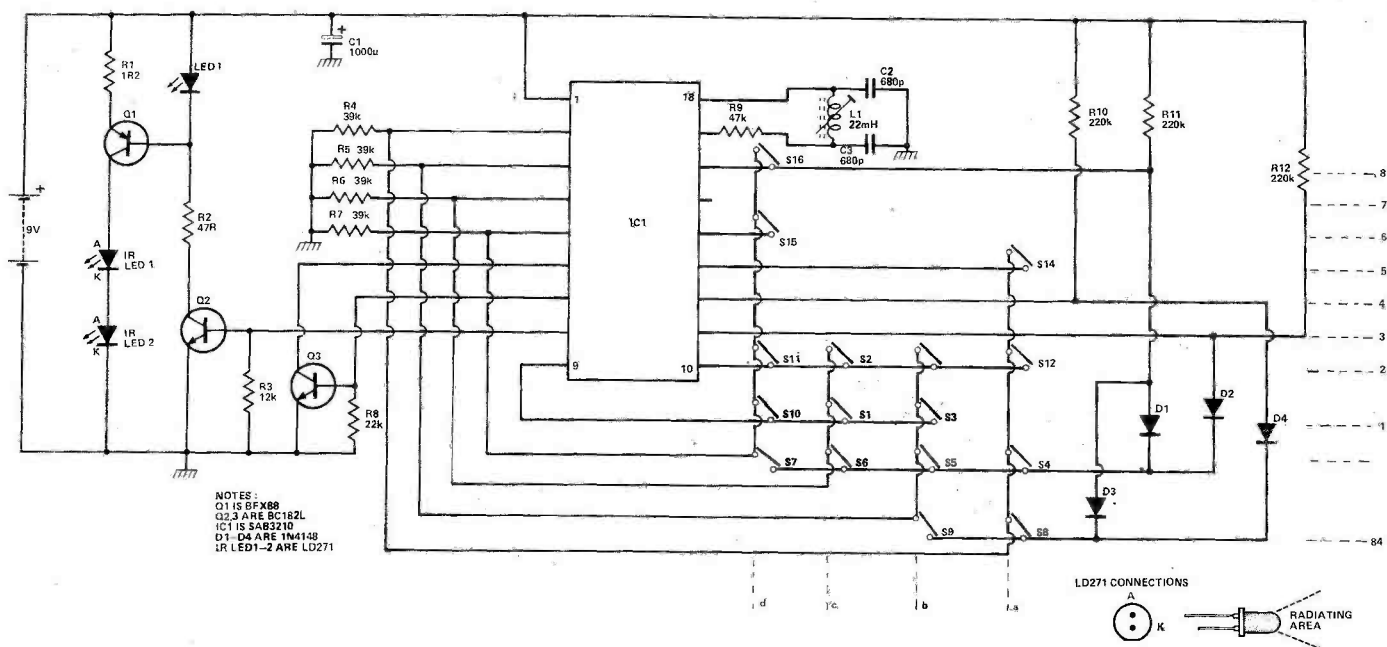


Fig.1. Circuit diagram of the IR60 transmitter unit.

HOW IT WORKS

The heart of the transmitter is IC1, a highly sophisticated P-MOS LSI chip. This chip receives input 'instructions' via an 8-row (pins 9 to 16) by 4-column (pins 2 to 5) matrix that can be activated via contact 'key' switches. The circuit is 'clocked' at about 60 kHz via the R9-L1-C2-C3 oscillator when the IC is active.

When the transmitter is in the quiescent state the IC is disconnected from the battery via turn-on transistor Q3 and the complete circuit (including the clock oscillator) is de-energised. Under this condition the entire circuit draws a total leakage current of only a few microamps from the supply battery. When any of the key switches are actuated, negative potential is applied to one of the 'row' pins via one of the R4 to R7 resistors and pin 7 goes high and turns Q3 on, thus energising the IC and its clock oscillator.

Whenever the IC is energised via a key-switch operation a keyboard scanner comes into operation, detects the 'code' of the actuated key and converts this information into a clock-related serial output code that appears on pin 8. This serial code signal is fed to the infra-red transmitter LEDs via Q2 and Q1.

The transmitter serial code is rather unusual. It consists of a start bit, followed by six information bits, which are read out in biphase code at half the clock frequency. 'Biphase' in this case means that a 'bit' prior to a clock reference point is read as a '0' and a 'bit' after a clock reference point is read as a '1'. The seven-bit serial code signal has a total 'frame' time of about 11 ms and is repeated at a time-base rate of about 130 ms throughout the duration of a key press. When the instruction key is released a single seven-bit 'end of signal' code frame is transmitted and the transmitter is then automatically deactivated again via Q3.

The serial output code from pin 8 is amplified by Q2 and is used to pulse constant-current generator Q1 on and off via R2 and LED 1. Q1 feeds 'on' pulses of several hundred milliamps to the two series-connected infra-red transmitter LEDs, this high current being supplied via storage capacitor C1. Although the PEAK IR LED currents are very high (thus ensuring a good operating range), the MEAN IR LED currents (averaged over one time-base period) amount to only 5 mA or so.

Considering that the transmitter will normally only be required to operate for about half a second per instruction, it can be seen that roughly 100,000 instructions can be transmitted from a single PP3 can be expected to transmit 250 instructions per day for roughly a year. Clever?

panel LED illuminates, indicating that a code signal is being transmitted. If the LED does not illuminate, re-check the circuit wiring.

Setting Up The IR60 System

When construction is complete, set the adjustable core of L1 in the transmitter and in the receiver to mid-position, place the transmitter a metre or so from the receiver and alternately operate transmitter buttons 1 and 2. With luck, receiver relay RLA will switch alternately on and off, indicating that the system is functioning correctly. If this action is not obtained, try twiddling the core of L1 in the receiver. If you still have no luck, use a 'scope to see if a coded signal is reaching the output of Q1 in the receiver: if not, recheck the transmitter circuitry and the polarity of IRD1 in the receiver.

Once you've got the system working, adjust L1's core in the receiver to find the extreme positions at which control is lost, then reset the core to half way between these two positions. You can then adjust RV1 in the receiver to obtain maximum possible range consistent with reliable operation: our prototype system gives a range of about 15 metres.

Finally, you can use a 'scope or voltmeter to monitor the individual outputs of the receiver while you check that they can be controlled via the transmitter buttons in accordance with the information given in Tables 1 and 2 last month. Your system is now complete and ready for use.

BUYLINES

The case for this project was chosen from the BIM Console range supplied by Boss Industrial Mouldings Ltd. (order code BIM600S Black).

A full kit of parts including the Mec switches (order SRM plus switch cap colour) can be obtained from Watford Electronics.

Ambit International are suppliers for L1, order as 87BN, 22 mH.

The SAB3210 transmitter IC is available from Electrovalue and Watford.

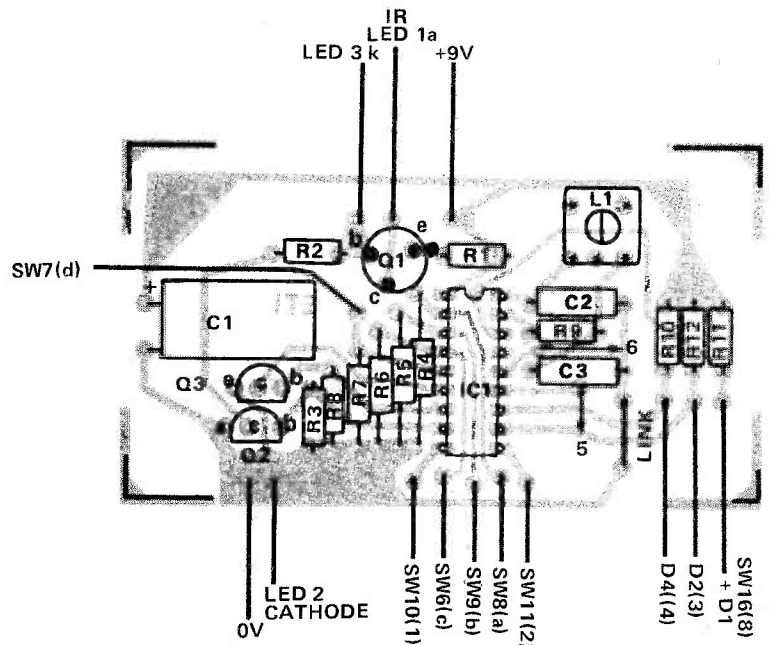
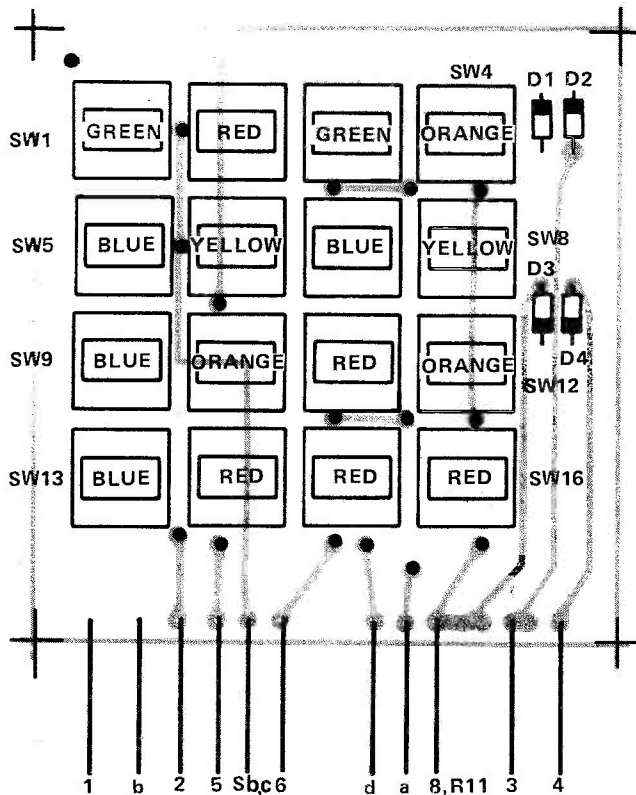


Fig.2. (left) Component overlay for the control board.

Fig.3. (above) Component overlay for the second board.

Fig.4. (below) The mounting positions of the controls on the double sided control board.

e.g. GREEN INDICATES COLOUR OF SWITCH CAP

● = PIN THROUGH

PARTS LIST

Resistors

R1	1R2
R2	47R
R3	12k
R4,5,6,7	39k
R8	22k
R9	47k
R10,11,12	220k

Capacitors

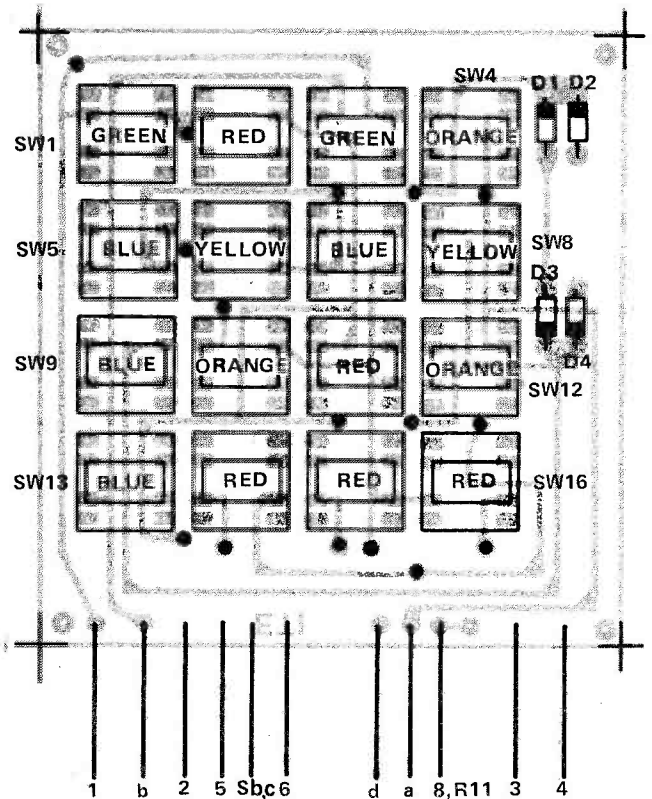
C1	1000u 16V electrolytic
C2,3	680p polystyrene

Semiconductors

IC1	SAB3210
Q1	BFX88
Q2,3	BC182L
IRLED 1,2	LD271
LED 1	0.125" dia. red LED
D1,2,3,4	1N4148

Miscellaneous

SW1-16 momentary switches (see Buylines), PP3 battery, case (see Buylines), L1 22 mH variable, Mec switch cap colour: green(2), red(5), orange(2), blue(4), yellow(2).



e.g. GREEN INDICATES COLOUR OF SWITCH CAP

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NOTE: For use with 4 to 8 ohms speakers p&p £2.55 **£13.95** with kit.

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RAVEN ON

Dave Raven takes the lid off his domestic computer scene and sounds alarm bells for the British computer scene.

Towards the close of 1979 it was announced in China that they had developed high speed emitter-coupled logic circuits that will permit construction of a super computer capable of 20 million operations per second. This is equivalent to ten times faster than any device they have produced to date. It was also announced that they would be exporting computers in the future.

Since this piece of breathtaking information must, by now, have brought you to the edge of your chair I will concentrate the mind further. The significance of China's declaration to enter the international computer market would be lessened if viewed in complete isolation and certainly does not pose any immediate threat to the western computer manufacturers. When, however, it is considered along with that of other emerging nations like Brazil, India and South Africa, who are all eager to develop independent computer industries, it serves to illustrate how different the international computer market will look at the end of the 1980's.

The USA, Europe, Japan, USSR and China will all be aiming to produce computer equipment for their 'in-house' requirements and also capture export markets.

The potential military role of computers is of major significance. However, other sectors of high technology such as telecommunications, aircraft, satellites and nuclear industry are all critical to the maintenance of an industrially based military complex.

Backing Britain

The ability of Britain to maintain our industries in all the above technological areas is vital if we wish to remain independent and it would surely be crazy if we were to waste the years of experience built up in this country in high technology only to import computers made in Brazil or China. Japanese computer manufacturers are already embarking on a long term programme to penetrate the USA computer market. This will be accomplished in much the same way as the establishment of cars in the UK; with good service centres and software requirements fully catered for.

In Britain, after seeing the end to our industry for manufacturing small motorbikes, we are now witnessing a slow take-over of the (cheap) family saloon market. Consumer electronic goods is of course well underway with virtually all the UK manufacturers killed off. Remaining are a few TV producers that will be fighting for their lives now that the PAL patents protection is soon to be lost.

The Video Story

Video Recorders could well reach the sort of sales levels which have been achieved by Colour TVs during the next ten years, since everyone with a TV has an application for a recorder. Guess how many of these quite straightforward pieces of hardware will be made in Britain, 12 million? 5 million? 1,000? How about 100? Sorry, not ONE. With the exception of a few home made models built in garden sheds and by lost souls in university development labs.

Watch This Space

Having debated involving myself in small computers for the last two years, I have at last purchased a home computer. The significance of this is that it is intended primarily for home use and, therefore, had to compete with other domestic demands on my home budget, as distinct from a business expense.

The decision to buy a home computer is not to be taken lightly, even at the knock down price of under £400, since this must be compared against other competing products which are just as attractive. My desire to buy a video recorder has not receded and the demands made by my wife for £400 worth of (quite unnecessary) furniture still continue. So what *was* the final overriding reason that made me rush out and buy a small computer?

Like most enthusiasts of electronics I usually desire new electronic goodies quite early in their evolution and home computers were to be no exception. All the products I have bought to-date such as TV games, digital watches, calculators etc, have all had clearly defined uses. However, a computer takes just a little more justifying as the following script shows:

Picture this domestic scene

Freak "Darling I have decided finally to buy a home computer".

Wife "That will be nice dear".

Freak "I have come to this decision after many months of careful thought and feel it will bring a greater understanding between man and machine. The involvement of the human brain with a computer will expand our memory capacity allowing us to be more creative thinkers".

Wife "That will be nice dear".

Freak "Through the tips of my fingers will be unleashed a storm of interlectual and statistical power man has not previously enjoyed. It can be incorporated with art, music, science, finance and with imagination it will probably iron my shirts".

Wife (looking slightly more interested) "That will be nice dear".

Freak (now standing looking out of the window with a glazed look on his face) "With the right level of software and peripherals it could organise many of our daily needs. A telephone link would enable it to order the shopping. Cooking, cleaning and remembering birthdays could all be carried out with the aid of a little robotics".

Wife "Darling is everything alright?".

Freak (not hearing) "With the right robotic design it could develop a human form. Feelings of compassion and warmth could be available to me at the press of a button. Love and understanding always there to satisfy my every whim".

Wife "But if the computer can be made to do all these things what will be my place in your life?".

Freak (now facing wife with manic expression) "And it all costs less than £400!"



The most frequent question asked by the few remaining people that have not yet bought a computer (sic) is — "What does one use it for?". Well, after going around the houses a few times, I can — with a little arm waving — come up with quite a convincing answer.

Life will of course continue without small computers. However, I doubt if small businesses will after a few more years. The pressures from larger competitors who use all the latest tools to beef-up their profit margins will force smaller competitors to follow suit. Don't ever kid yourselves that small companies are cheaper to operate. It requires nearly the same sized operation to print this one magazine as it does to print half a dozen. Ask the Managing Director of Modmags, if you don't believe me. Small computers can be used to speed the flow of management information required on a daily basis. They can put off the day when it is necessary to increase the size of office premises and produce more output without increasing staff numbers (not a bad objective when one considers that the birth rate is declining in Britain).

Joining The Revolution

Having extolled the virtues of computers and my fears that Britain may not enjoy the full fruits of their manufacture, I am rather excited by the future prospects of our own Prestel system. For once this very British innovation cannot easily be pinched and sold back to us at a cheaper price since it consists of a system rather than a single manufactured product.

My grateful thanks to Rediffusion Manager Tim Jaggard for allowing me to be present at a demonstration of both the Teletext and Viewdata systems. I must openly confess that although I am aware that much has already been written about these new systems, I have previously found it difficult to muster any interest. Perhaps this is because I am more familiar with Teletext, which interesting and useful as it is, remains an extension of the more traditional information services.

Clearly consumers in the next few years will demand Teletext as a standard on their TV sets in the same way that colour is now required. Viewdata (or Prestel), however, is a different ball game which links together a domestic telephone with the television and converts this to a traditional video display unit as used with a computer. At the press of a button connection is made through the GPO exchange to independent organisations who contribute information directly from their own offices.

The Post Office, who provides the Prestel computer and exchange equipment are not involved in editing or interfering in any way with the material supplied to the subscriber. The computer is capable of providing over one million pages of information which can also be of a highly confidential nature and only available to subscribers who have access to a certain code — for example, private company information to members of staff, bank statements, credit checks on potential customers for loans. On the direct selling side it is possible for subscribers to book tickets on planes, ships and trains using their credit cards. The possibilities for mail order are endless with customers buying directly after seeing TV adverts and not even leaving their front room.

Small Viewdata printers are available producing a hard copy of what you see on the screen. This is all British, you have to remind yourself, and according to the Post Office by 1986 Prestel services would be called on by 95 per cent of telephone users. One other interesting observation is of the uses which may be made of the three as yet unused Viewdata channels. I cannot see the problem in providing software and memory for use by the consumer — which would rapidly make redundant all the small home computers.

ETI

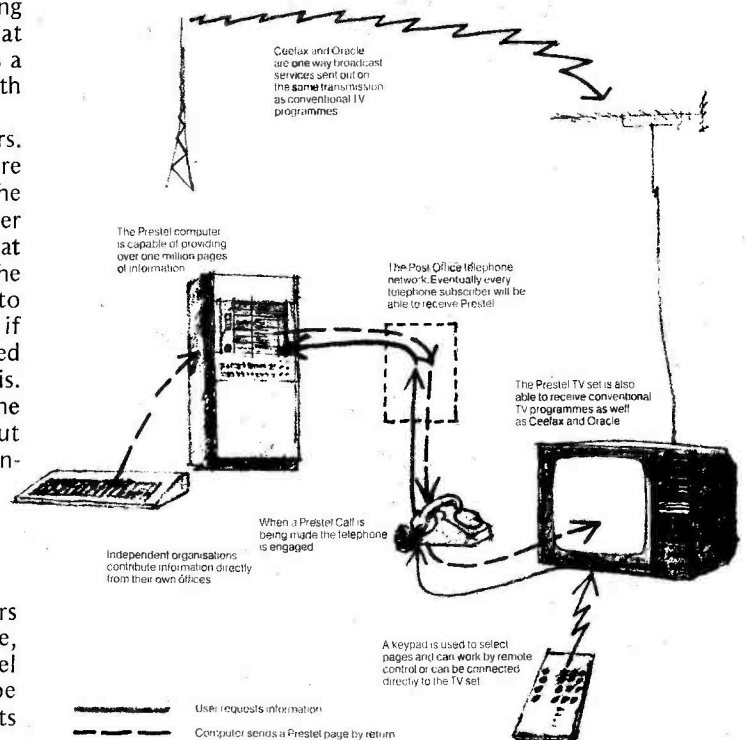


Fig.1. Ceefax and Oracle are broadcast in the same way as TV programmes. Prestel allows independent organisations to put information in. You receive it by telephone and the information is available on your telly at the touch of a button or two.



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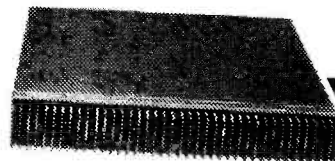
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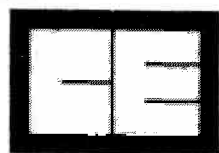
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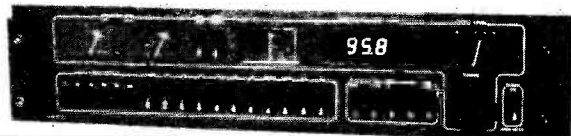
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Mark III A series 'Reference series' tuner modules£171.35 inc.
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A matching synthesiser unit will be made available later this year, and can be retrofitted to either version. All versions include digital frequency readout/clock, VU deviation meters, 6 preset stations, 10 turn pot manual tuning, toroidal PSU, output level adjustment, 110/240V AC input. Full alignment service available.

Power Amplifier

Style and performance - with a real 'belt and braces' PSU design.

After a couple of preview comments, it seems that many of you are waiting to hear about the matching HMOSFET power amplifier for the Mk III tuner. Well, it's out at last - complete with twin toroidal PSUs for comfortable 80W RMS per channel, over 100W peak, but limited by thermal shutdown of the HMOS. 10W-100W log LED output peak indicator, DC offset protection and switch-on pause relay. AC or DC input coupling, direct or relay protected output terminals. The works.

Only one version of this item: Complete kit£178.25 inc. Carr. £5.

Preamplifier

More features and facilities, thanks to DC switching and control design

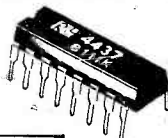
Previewing the most comprehensive audio preamplifier yet..... DC switching of 7 inputs, plus two tape in/out. 2 low pass, 2 high pass active filters, genuine volume related loudness, 1dB channel matching, with DC volume, balance, bass and treble controls. Suitable for bus/master control, tape dubbing, switched monitor etc. 80dB S/N+. THD -75dB or better. Pluggable PU equalization boards, tone control override. Price for complete unit about £149 ex VAT.

Semiconductors

Radio/Communications ICs

FOR COMPLETE LISTINGS - SEE OUR NEW PRICELIST

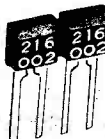
CA3089E	2.11	HA1197	1.61	SD6000	4.31
CA3189E	2.53	CA3123E	1.61	TDA4420	2.59
HA1137W	1.95	TDA1072	3.09	MC1330P	1.38
HA11225	2.47	TBA651	2.53	MC1350P	1.38
HA12412	2.81	TOA1090	3.51	KB4412	2.24
KB4420	1.95	TDA1220	1.61	KB4413	2.24
TBA1205	1.15	TDA1083	2.24	KB4417	2.53
KB4406	0.80	TDA1062	2.24	MC3357P	3.16



VARICAP DIODES.....

A section from our PL:

BA102	0.35	16:1 ratio AM tuning	
BB204	0.41	KV1215 9v triple	2.93
BB105	0.41	KV1211 9v dual	2.01
BB109	0.31	KV1225 25v triple	3.16
MVAM2	1.93	BB212 9v dual	2.25



POWER MOSFETS

100W PA's made simple

Since pioneering the 100W complementary MOSFET technique - Hitachi have developed a range of output devices and drivers that ought to revolutionise opinions and attitudes towards the design of all LF amplification systems. We have a new 48 page application note (£1.50 inc) and complete sets of parts, modules and now the new complete PA system (see above).

2SK133	120v N-ch 100W MOSFET	£6.33	2SJ48 Pch complement	£6.33
2SK135	160v N-ch 100W MOSFET	£7.29	2SJ50 Pch complement	£7.39

PA101B Kit for 100W MOSFET PA less Heatsink £16.10. (£23 inc heatsink/bkt)

ULTRA LOW NOISE PU PREAMPLIFIER

The HA12017 is the last word in PU preamps, and general low noise audio design. It is an SIL IC, with 86dB S/N in RIAA configuration, 10v RMS output capability, 0.002% typ THD at 10v RMS output (imagine the overload margin !!). It comfortably supercedes discrete circuit designs in terms of price/performance, and takes the art beyond the TDA1042's capabilities. (Replaces HA1457) £1.80 each - or an RIAA applications PCB with two ICs for £5.75. Complete with Rs/Cs £9.95.

Radio Control ICs

We have various RC ICs, including NE544 NE5044, and two new ones from OKI

KB4445	- 4 channel dig. prop. FM TX IC. 30mW out (amplifiable) -£2.30 inc
KB4446	- 4/5 ch. dig. prop FM RX IC. Suits KB4445 or RCME syst. £2.65
KB4445/6 pair:	£4.75. New 8 page data sheet 35p + SAE. More RC ICs in list

CMOS, LPSNTTL, TTL, MPU: Listings in the new pricelist.

Most CMOS is available in low volume - also LPSN. Standard linear and TTL OK.

Things like ICM7216B, ICL8038, 8080A, 6800P, 2708, NE555, NE556, etc

Coming Soon..... Contain yourselves, RF fans ! Not yet ready for a full launch until autumn, but previewed here:-

SSB transceiver system : 10kHz to 1000MHz !!

A modular VLF to UHF SSB TX/RX system at last. With the correct first mixer, the basic PCB covers 10kHz to 1000MHz - using LO fed from ext. source (Our 2 IC Mullard synth for instance) and RF PA for TX. OP. 0.2uV basic sensitivity in HF. Typ cost for HF synth SSB RX will be less than £200. Add an RF PA for full TRX for another £50. See one in our foyer, and marvel.

Please send an SAE with all enquiries. Phone orders by ACCESS - but minimum £5. Callers welcome

CATALOGUES 60p ea. all three for £1.60. PRICES SHOWN INCLUDE VAT. POST/PACKAGE CHARGE NOW 35p

ambit
INTERNATIONAL

200 North Service Road, Brentwood, Essex

TELEPHONE (STD 0277) 230909 TELEX 995194 AMBIT G POSTCODE CM14 4SG

Radio/Audio/Communications Modules

LW-MW-SW-DC tuned and switched

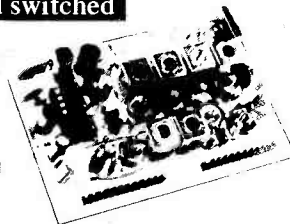
91072- All switching of bands by a single pin to gnd. Varicap tuned, with LO output for synth. MW/LW version or MW/LW plus 1 or 2 SW bands MW/LW: £15.58 +1SW £16.73

VHF Tunerheads

Europe's largest stock range for broadcast and communications. Probably also the world's - details in the catalogues and PL. Specials are also supplied in the region 30-220MHz.

Pilot Cancel PLL Stereo decoders

Again, Europe's widest range of stereo decoders including pilot cancel PLL types. The pic shows the 944378 - pilot cancel including post decoder 26/38kHz filtering and muting preamp output



944378-2
£26.45

Switched bandwidth FM IF strips

Broadcast FM IF strips for all occasions, including the new 911225 - with diode switched narrow filter option, ultra linear phase ceramic filters, 84dB S/N, and 0.04% THD (40kHz deviation). Plus usual things like AGC, AFC, dev. mute, level meter drive. £23.95 (supplied in screen can with 0.1 edge connection system) Also the 7230 hyperfi series - as the 911225, but with slope controlled AFC that operates in conjunction with signal level - and an extra IF amp stage for DXing.

Various digital frequency displays

The World's largest range of receiver DFM's is now joined by the DFM7 (shown) - and L shaped version of the DFM3 with remote display mount connector possibility. 1kHz SW resolution with 455kHz or 10.7MHz offsets, 100Hz res up to 3.9999MHz, and VHF to 299.99 MHz in 10kHz steps : £41.75



Components

Crystal Filters

Most popular types are available ex-stock, and in quantity.

10.7MHz	25kHz Channel spacing 8pole	£16.67
	12kHz	£17.82
	2.4kHz SSB	£19.78
	Monolithic dual roofing filter	£2.30
34.5MHz	1.3dB loss, 80dB stopband HF	
	first filter in synth. RX	£36.80
RC XTALS	FM pairs (no splits)	£3.74
	AM pairs	£3.57
USB/LSB	Xtals for 10.7SSB filter	£2.88 ea



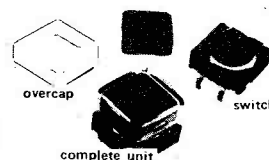
Piezo Sounders

The most efficient warning sounders yet

The latest thing in electro-acoustic efficiency. 1mA of drive from CMOS will give an SPL of 83dB - 10v RMS drive from CMOS uses 3mA for 100dB SPL at 4.8kHz (88dB at 1.65kHz) The data sheets shows various drive circuits, and give full specifications with regard to broadband responses and power consumption etc. 1 off 44p inc. 100 off 28.75p (25p ex vat)

Keyboard switches and caps

From the world's most widely used switch manufacturers - ALPS - come the biggest and best range of keyswitches, and data entry keyboard switches. The SC8B1101 is shown here, with the KT5 2-part cap (with clear top, to enable easy fitting of your chosen legend. Other types are available with built in LED, 90° mounting etc. SC8B1101: 17p, KT5: 16p - or 29p/pair



LCD CLOCKS

Clocks use 1.5v at 15uA only. DVM 9v/1mA

LCD DVM

CM161:	7mm LCD 12/24hr, alarms etc	£11.44 each
CM172:	13mm, 12hr, alarms, timer etc	£14.32 each
CM174:	13mm, 12hr, min/sec stopwatch	£14.32 ea
DVM 176:	ICM7106 based LCD 3 1/2 digit	£22.36 each



WHAT'S NEW at AMBIT

NEW PRICELIST/SHORTFORM:- 28 pages, FOC with A5 SAE pse

Bigger print than our recent one page list - and vastly extended

If you still need convincing to invest £1.60 in the cats, be mean and get this first.

POWER MOSFET APPLICATIONS HANDBOOK by HITACHI :

£1.50 each - or free with pairs of HMOS and the PA101B

Everything you should know about HMOSFET devices theory and applications.

Parts 1-3 AMBIT catalogues 60p ea, or £1.60 the lot.

DRUM SYNTHESISER

At last, ETI's own machine which peeoom-peeooms, bim-bams, whizees or boo-ooms in all its onomatopoeic glory. Here is Roger Shore's original design for the ETI staccato drum synth.

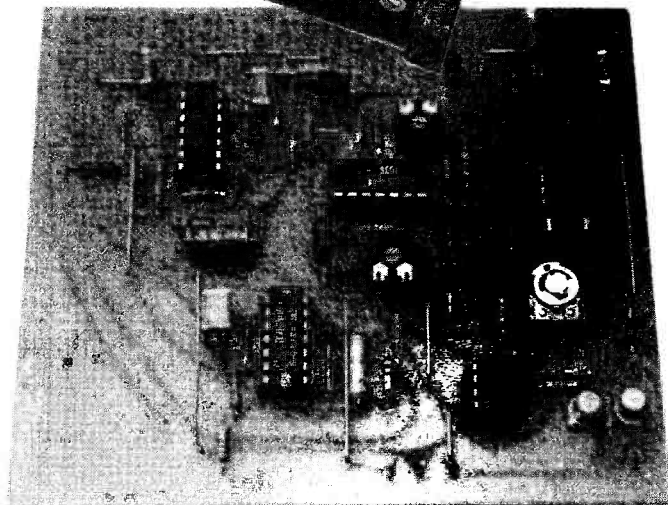


You've all heard the effect on disco or pop records. It was first heard about a year ago and since then, it seems, has grown in popularity so much that no decent, self-respecting drummer would let it be known that he hasn't got one. Mind you, they are only obtainable commercially at a price — £180 or so can buy you *one*. A fair price, the enquiring musician might muse in perspective, in order to keep up with the times and the modern music trends. A fair price indeed, until the even more enquiring technical musician takes the lid off and studies the electronic circuitry involved. That's exactly what we did! We decided that this new sound was one to be investigated with a future project in mind and so we took a good look at a major proportion of the available commercial units.

Our first conclusion was that somewhere along the line of manufacturer, middle-man and musician, somebody was ripping off somebody else — and, as usual, it is the end link in the chain having to pay more than the odds.

Our second conclusion was that we could probably do a better job — a design which out-performs available drum synthesisers in both quality and price.

A fairly conservative costing of all components and hardware for the project, which is a two channel synthesiser, forming a stereo output with the added facility of a monitor amplifier circuit to power a pair of stereo headphones (allowing setting up of the synth without being overheard) comes to



All 42 ways of the control board (above) are used. Cut a slot at pin 37 for identification.

around £60. This approximate price is inclusive of what we feel is a very nice housing (see Buylines) suiting the synthesiser down to a tee. A comparable price for a similar commercial unit is over £360 — OUCH.

The modular construction means that any number of channels can be built as required and perhaps the most enterprising of you out there can envisage a complete electronic drum kit of bass, snare, tom-toms, high hat and cymbals for about half the price of a standard kit. Of course the extra drum sounds of the synthesiser are also there as required.

The ETI Staccato is a mains powered device, none of those nasty batteries running out on you half way through a gig. A simple microphone or miniature loudspeaker acts as the trigger sensor and can be positioned inside an existing drum, on the underside of a simple wooden block or, as in the prototype, inside or underneath a practise drum pad. The drum pad is probably the ultimate as it means a permanent and compact method of holding the sensor whilst maintaining a good-looking and functional appearance.

Also featured is a sensitivity control which adjusts for a very wide range of trigger sensors and levels which means that virtually any combination of microphone, or speaker and holder will trigger the synthesiser.

The ETI Staccato Drum Synthesiser

Our aim was to incorporate a systematic approach to interwiring connections, therefore providing a unit that could easily be expanded. The most favoured compromise combined three PCBs; a power supply unit and monitor board, control-circuit and a function board which holds all PC mounting potentiometers, switches and LEDs for a single channel synth.

Begin construction by building the power supply unit and monitor PCB, insert all pins and wire links followed by IC sockets, resistors, diodes, capacitors and semiconductors. Next in line is the control circuit; follow the same procedure as above. Take care when you come to wire the edge connector as all of the 42 ways have been used right down to the last pin! A slot will need to be made at pin 37 of the circuit board to polarise the edge connector.

Construction

Before assembling the function board, it is wise to use it as a template for marking out the front panel. This will give a physical representation of the layout and will enable easy alignment of the potentiometers, etc after drilling. Mount all right angled, inter-PCB sockets (3 ways or 5 ways) around the edge of this board. Be sure to mount all potentiometers from the copper side of the PCB with their tags bent at right-angles. It is highly recommended that the specified switches are used (see Buylines) as they offer various switchable pinouts, especially in the case of SW3. To accommodate the switch bezel, a cutout of 14x14 mms is required. Finally to save any embarrassment whatsoever, check the orientation of all polarised components before switch on!

Now you've built the staccato drum synth how about joining a band? At least one hour's practice should put you 'on the road' — not necessarily to stardom!

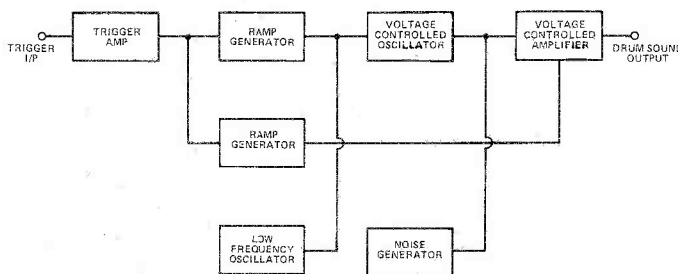
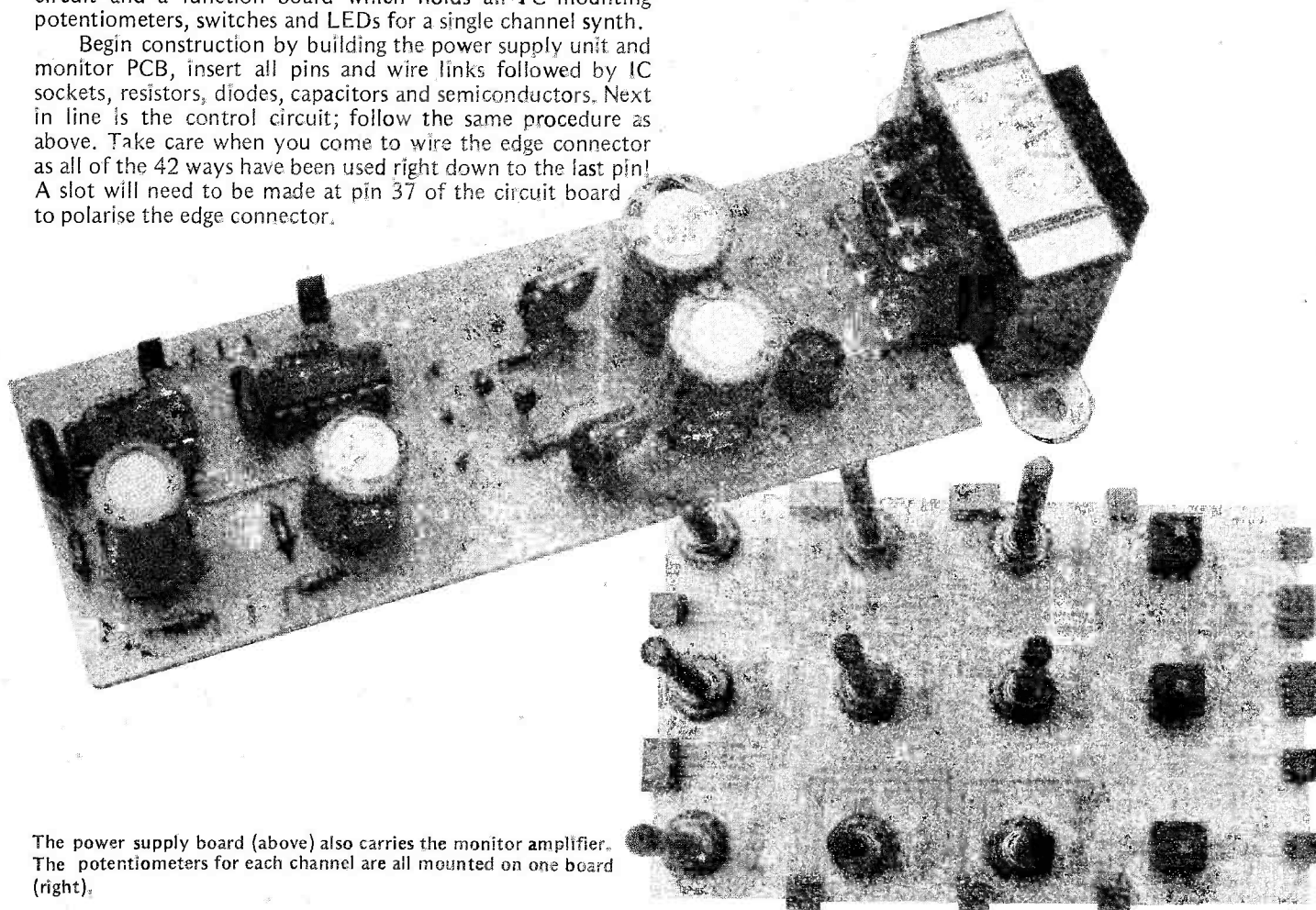
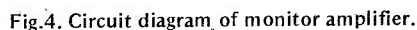
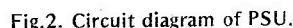


Fig.1. Block diagram of the ETI Staccato.



The power supply board (above) also carries the monitor amplifier. The potentiometers for each channel are all mounted on one board (right).

There are only three presets (RV5, 6 and 7) to adjust. Start by setting them all to mid-position then turn the noise control to minimum and switch the noise on. This effectively disconnects the sine filter from the circuit. Now switch the VCO to sine output. Switch the device on and adjust RV7 preset until a continuous signal is heard at the output. If an oscilloscope is available, adjust RV5 and 6 for minimum sine-wave distortion. If no oscilloscope is available, simply adjust



the presets for minimum audible distortion. This may seem somewhat haphazard, but the human ear is very discerning where sine distortion is concerned! Once the minimum distortion position has been established, it only remains to adjust RV7 until the signal just disappears from the output and that's it!

Now, the golden rule is to experiment. Apart from the sounds for which the drum synth is well known, a whole range



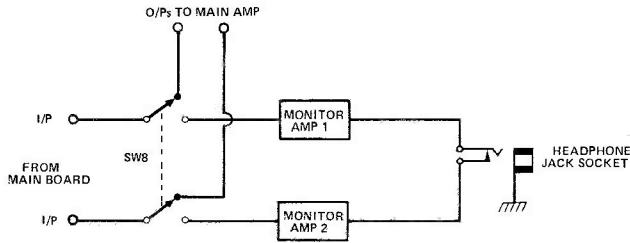


Fig. 5. Connecting details of monitor amplifiers.

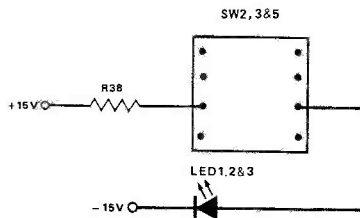
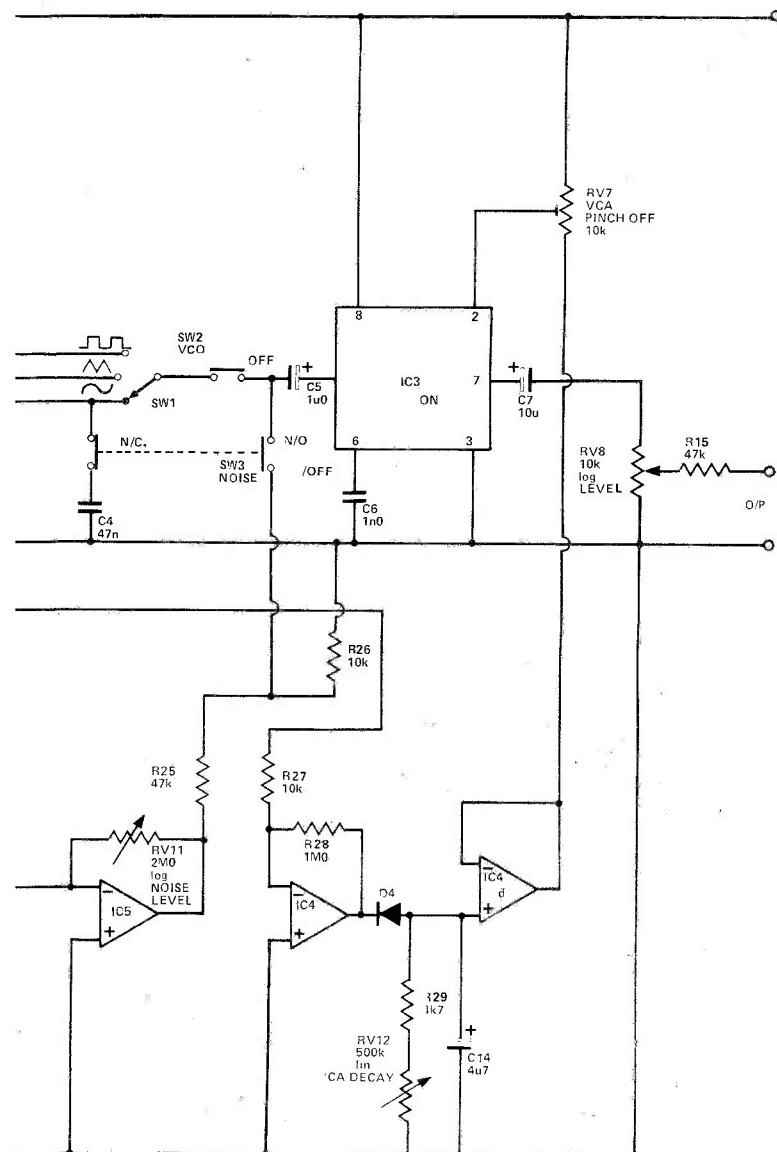


Fig. 6. Connecting details of switch LEDs.

Fig. 3. Circuit diagram of the ETI Staccato Drum Synth.



of strange and wonderful sounds is possible, particularly if the LFO and noise generator are used. Vibratos, warbles, chimes and gongs are obtained using the LFO. Surf, wind, applause, snare drums and cymbals are obtained using noise.

HOW IT WORKS

The block diagram (Fig.1) shows the main principle of operation of the synthesiser. It can be seen very simply as a voltage controlled oscillator followed by a voltage controlled amplifier. This means that the frequency of the final signal and its amplitude ie its pitch and envelope, are controlled by DC voltages derived from the original trigger. Two separate ramp generator circuits provide these DC voltages and all necessary parameters of these ramps are externally controllable. A low frequency oscillator can be applied to modulate the VCO if desired and a generator produces noise for cymbal or snare sound, etc.

The voltage controlled oscillator is based on the 8038 wave-form generator chip, IC2. Its frequency is varied by adjustment of the pitch control RV4, allowing the initial frequency to be set to the required level. Alternatively, the frequency can be controlled by a varying DC voltage applied via D3, from the VCO ramp to be described later. The oscillator works over the frequency range between about 10 Hz and 1k5 Hz. All three output waveforms available from the 8038, sine, triangle and square waves, are used.

The trigger for the synthesiser is provided by a microphone (virtually any microphone will do) fitted inside a suitable drum or holder, even a tin can will do! The signal from the microphone is differentiated by C1, R1, so that surrounding sounds do not cause false triggering. The pulse generated when the drum is struck is then amplified by IC1a, the gain being varied by RV1. The output of this amplifier is then rectified by D1 to provide a positive going pulse which is fed to further amplifiers IC1d and IC4c. These op amps are connected as inverting amplifiers to provide negative going pulses to drive the VCO and VCA ramp generators.

The anode of ZD1 is normally at zero volts and the cathode at +15 volts. When the output of IC1b is driven negative by a trigger pulse the cathode of D2 approaches zero. This negative-going pulse is rectified by D2 and charges C2 rapidly. C2 discharges through RV2 and R4, the value of RV2 varying the rate between a few milliseconds and several seconds. This DC ramp is buffered by IC1c connected as a voltage follower, to prevent RV3 affecting the C2, RV2 discharge time. As both ends of RV3 are normally at +15 volts, D3 is biased off. When the output of IC1c swings negative on receipt of the trigger, D3 is turned on and allows the ramp waveform to control the sweep input of the VCO. RV4 sets the lower frequency of the oscillator and as pin 8 goes more negative, the frequency rises. The range of this frequency sweep is determined by RV3 whose setting limits the negative swing of D3 cathode. However, C2 charges quickly and discharges more slowly. The characteristic falling sine sound of the drum synth is created at the output of the VCO. By use of RV4 pitch, RV3 pitch bend and RV2 slope a whole range of sweeps are possible.

The voltage controlled amplifier is based on the Motorola 3340 voltage controlled attenuator IC. The selected output from the VCO is fed to the IC and the output is fed to the volume control, RV8. The voltage controlling input is fed to pin 2 via RV7, which is preset so that with no trigger present there is no output. The VCA ramp generator functions in a similar manner to the VCO ramp generator. The base-emitter junction of Q1 is reverse biased to provide the noise source. This noise is amplified by Q2 and further amplified by IC5 whose gain is variable via RV11, determining the noise level to be fed to the VCA input.

Notice that when the noise is switched in, the sine filter, C4, is switched out. This is to ensure that when noise and sine are used together, this filter does not attenuate the useful part of the noise spectrum required. Although this marginally increases the sinewave distortion this is not noticeable above the deliberately introduced noise.

The low frequency oscillator uses IC4b as an integrator and IC4a as a Schmitt trigger, together making a triangle wave oscillator. The speed is varied by RV9 between about 0.5 Hz and 1 kHz, and the amplitude is varied by RV10. C9 can be switched in to integrate the triangle wave to provide a sinewave approximation for vibrato effects.

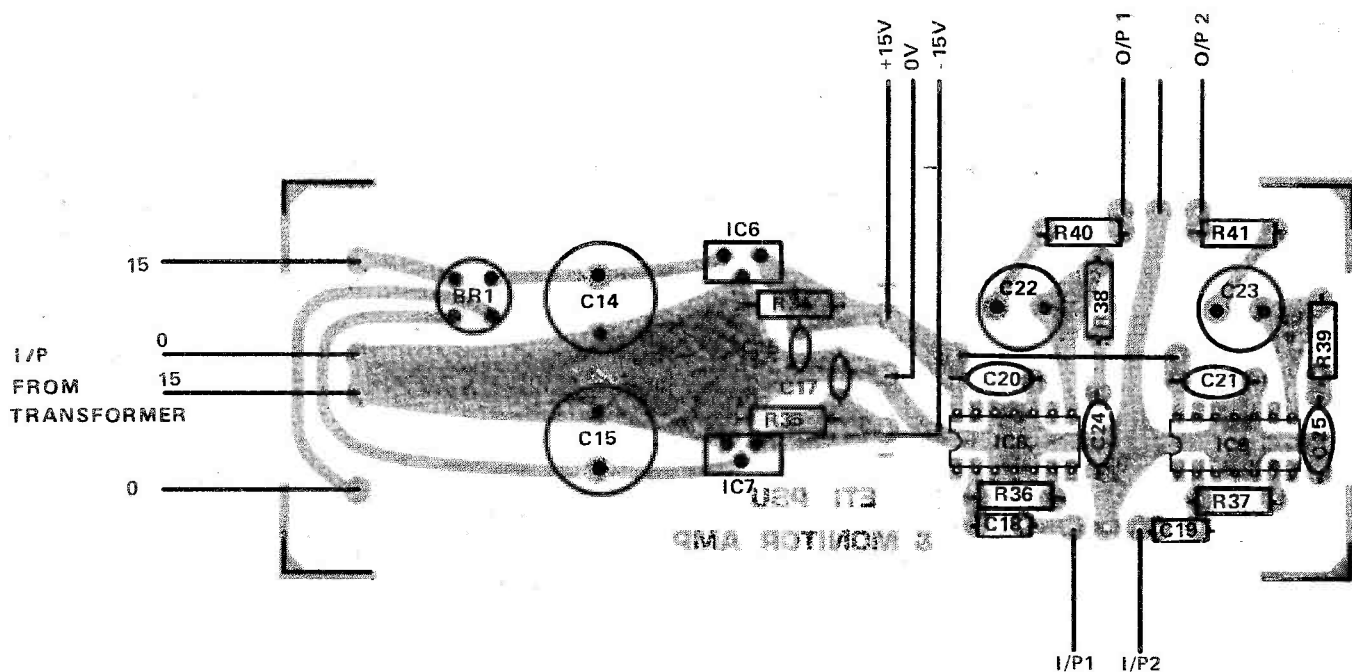
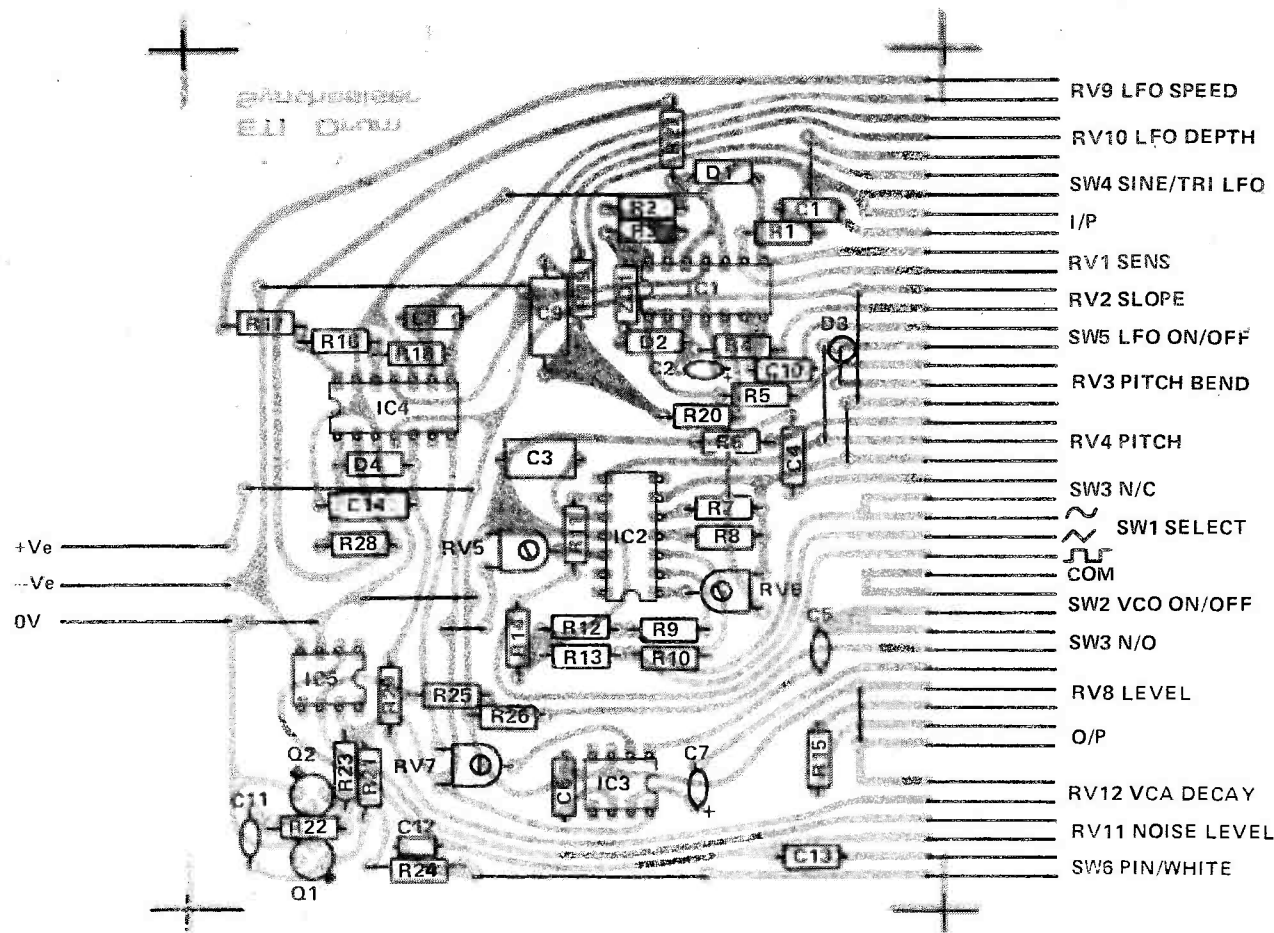


Fig.7. (above) Component overlay of the PSU and monitor amplifier board.

Fig.8. (below) Component overlay of the control circuit board. Take care when wiring the edge connector.



BUYLINES

A varied buylines, as certain components have been selected for easy construction. The exceptional case is part of a range (larger sizes available on request) supplied by Campbell Clarke Cabinets, 2 Arden Court, Church Road, Perry Barr, Birmingham, B42 2LF, Tel: 021-356-0890 — a very stylish wooden ended cabinet which is attractively priced at £11.50.

The MEC switches are only available from Watford Electronics (order code SRL plus colour of switch cap) along with the knobs. Also state cap colour when ordering the knobs. The micro toggle switches can be purchased from Marshall's. Electro-value stock the PC mounting potentiometers. For the inter PCB sockets, plugs and shells, Technomatic are suppliers. Our Remo practice drum pads were obtained from The Rhythm Box (Drum Store), 5 Denmark Street, WC2 8HLP, Tel: 01-240-3836. A crystal insert fits neatly inside these pads and acts as the trigger sensor.

PARTS LIST

Components For One Channel

Resistors

R1,2,4,5,12,13,14,18,	10k
20,24,26,27	1M0
R3,22,28	270k
R6	4k7
R7,8,19,23,25,29	22k
R9,10,16	220k
R11,21	47k
R15	1k0
R17	2k2 1W
R38	

Potentiometers

RV1,2	1M0 lin PCB mounting
RV3	250k lin PCB mounting
RV4	500k log PCB mounting
RV5,6	100k miniature horizontal cermet preset
RV7	10k miniature horizontal cermet preset
RV8	10k log PCB mounting
RV9,12	500k lin PCB mounting
RV10	100k lin PCB mounting
RV11	2M0 log PCB mounting

Capacitors

C1	4n7 polycarbonate
C2,5	1u0 tantalum 35V
C3	100n polyester
C4	47n polyester
C6,11,12	1n0 polycarbonate
C7	10u tantalum 35V
C8	470n polycarbonate
C9	10u 25V electrolytic axial
C10	100n polycarbonate
C13	22n polycarbonate
C14	4u7 16V electrolytic

Semiconductors

IC1,4	TL084
IC2	8038
IC3	3340
IC5	TL081
D1-D4	1N4148
ZD1	15V 400 mW
Q1,2	BC109
LED 1,2,3	0.125" dia red LEDs

Miscellaneous

SW1, DP 3 position slide switch (one pole used only) SW2,3,5, MEC 2 N/O, 2 N/C latching push button (see Buylines), SW4,6, SPST micro-miniature toggle, 43-way edge connector, 8 x 3-way right angle inter PCB connectors including plugs, sockets, shells, 5 x 5-way right angle inter PCB connectors including plugs, sockets, shells, case (see Buylines), 9 knobs, input and output sockets, 4 6BA tapped spacers (length), 4 6BA plastic spacers, trigger sensor, drum pads (if required), MEC switch cap colour green, blue and yellow, knob cap colour 3 blue 2 red, 2 green, 1 white, 1 yellow for a single channel drum synth.

Additional Components For Two Channels

Resistors

R30,31	22k
R32,33	1M0
R34,35	2R7
R36,37	150R

Capacitors

C14,16	1000u 25V PCB electrolytic
C15,17	1u0 16V tantalum
C18,19	68n ceramic
C20,21,24,25	100n polyester
C22,23	220u PCB electrolytic

Semiconductors

IC6	7815
IC7	7915
IC8,9	LM380
BR1	1A 50V bridge rectifier

Miscellaneous

T1 15.0-15 6VA transformer, SW7,8 DPDT miniature toggle, FS1 500 mA fuse, stereo jack socket, length of 3 core mains cable.

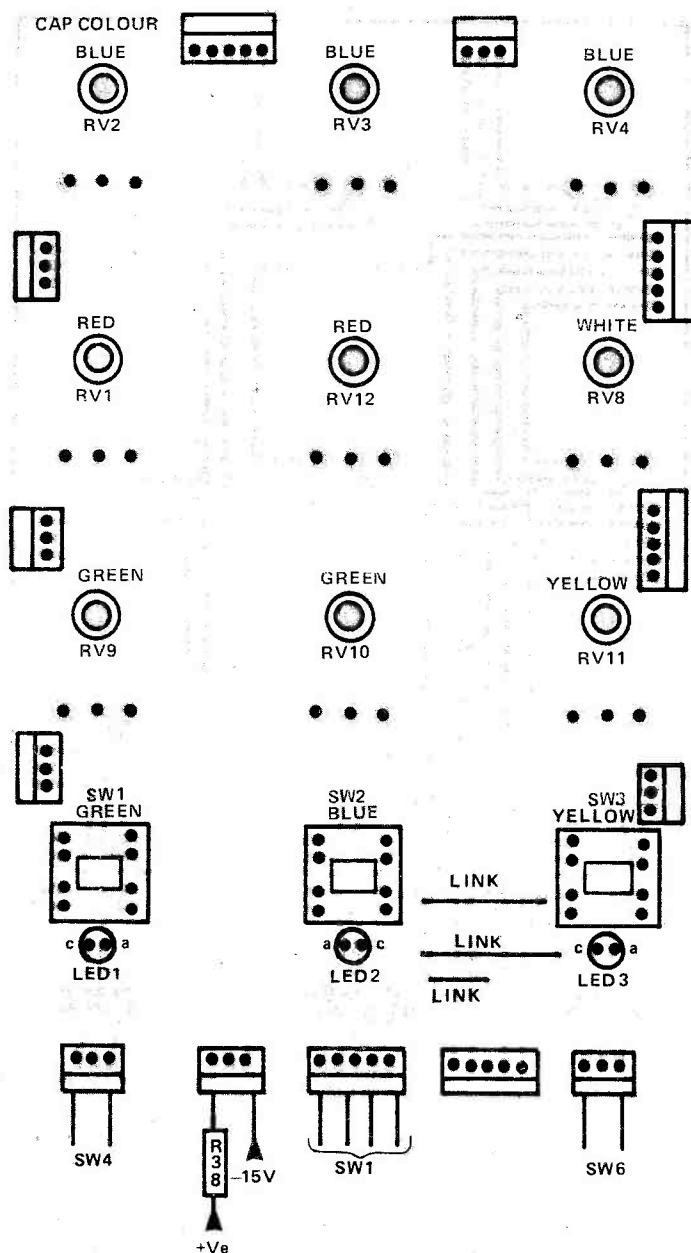
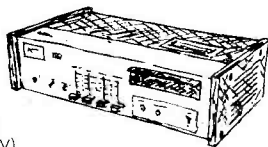


Fig.9. Component overlay of the function board.

Adastra PUBLIC ADDRESS EQUIPMENT Adastra

A40 P.A. CENTRE

All Solid State
Power: 40W Music
20W RMS
Mono Cassette Deck
Slider Controls
V.U. Meter
Inputs: 2 - Mic (1mV)
1 - Aux (100mV)
1 - Aux (15mV)

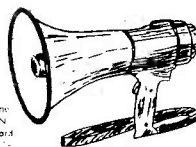


£220.80

The 'P.A. Centre' has fully comprehensive facilities making it unique equipment for multi-application use in audio, public address, sound and communication systems. Presentation is in a sleek video cabinet, with single slider deck and control facia, housing the 40W mono amplifier, cassette recorder, internal microphone and speaker. Outputs of 8, 16 ohms and 100V line enable a wide range of external loudspeaker systems and P.A. horns to be used; operation from A.C. mains and 12V car battery further increases the versatility of applications and location possibilities. The 'P.A. Centre' can be used as a mixer unit, and the internal condenser microphone or loudspeaker muted as required.

L81 10W MEGAPHONE

Power: 10W
Range: ½ mile
Batteries: 6 - 1½V

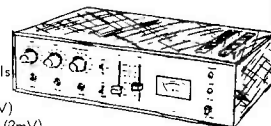


£89.70

Easy-to-use and hold, this lightweight megaphone has a range approaching ½ mile. Features ON/OFF switch incorporated in pistol grip and forward facing dynamic microphone. Solid-state 5 watt conductor circuit, powered by 6 x 1½V batteries. Attractive red and white case with carrying strap.

A56 50W A.C./D.C.

All Solid State
Power: 50W RMS
S.N.R.: 55dB
Rotary & Slider Controls
V.U. Meter
Inputs: 3 - Mic (0.5mV)
1 - Mag Phono (3mV)
1 - Aux (200mV)

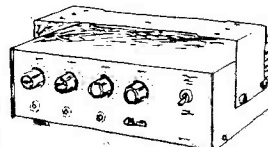


£117.30

The A-56 is a 50W A.C./D.C., all silicon solid state P.A. amplifier. Its outstanding performance and versatile operating features make it ideal for use in a wide range of applications, such as in schools, factories, restaurants and shopping centres. The amplifier is housed in a grey finished metal cabinet, well complemented with a black and silver front fascia panel. 3 low impedance microphone inputs are available. The third of these inputs is an alternative to 'auxiliary' or 'magnetic phono (R.I.A.A.)' inputs via a selector switch. A 3 position switch marked MUSIC, SPEECH is provided to give best cut. The pre-amplifier output is available through a 5-pin DIN socket, rear mounted. Since the 'auxiliary' input is through the same socket, it is possible to use a single connector for recording and playback from a tape recorder.

A55 MOBILE AMPLIFIER

All Solid State
Power: 20W RMS
S.N.R.: 60dB
Pos. or Neg. Earth
Car Mounting Bracket
Rotary Controls
Inputs: 2 - Mic (3mV)
1 - Aux (40mV)

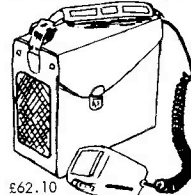


£69.00

Able to operate from both A.C. mains and 12V D.C. this is the ideal solid-state P.A. amplifier for installation in vehicles, caravans, boats, and for exhibitions, demonstration and display purposes. 3 inputs are conveniently front located, individually gain controlled and will accept two microphones plus ceramic or crystal cartridge, reed or tape recorder. Speaker output impedance of 4, 8, 16 ohms and 100V line allow for long and complex speaker runs. A two-way chrome mounting bracket stand is provided for easy fitting to dashboards, shelves, panels and control desks. The metal cabinet is finished in grey with black and silver front, incorporating gain controls, zone control and A.C. battery power switch with indicator lamp.

A60 SHOULDER P.A. SYSTEM

Power: 5W RMS, Range ½ mile
Batteries: 6 - 1½V



£62.10

This is a versatile, complete P.A. system essential for couriers and guides, public speakers, traffic and parking controllers, showground and display attendants and for countless publicity and promotion activities. The new leather-tone case with adjustable shoulder strap houses a solid-state amplifier, loudspeaker and storage for the 'press-to-talk' microphone on a self-coiling lead.

L83 MEGAPHONE (SEP. MIKE)

Power: 16W, Range: ½ mile
Batteries: 8 - 1½V

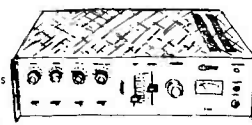


£69.00

High powered, yet compact and easy to carry and use, this solid state megaphone has a range of ½ mile. The noise cancelling microphone clips onto the base, has a convenient press-to-talk switch, and volume control and is fitted with a self-coiling lead extending to over 1½ metres. This sturdy constructed megaphone can be operated fitted onto a stand using the top hole provided, free standing on table and floor, and portably shoulder slung, or strap carried.

A70 PROFESSIONAL

All Solid State
Power: 175W RMS
S.N.R.: 55dB
Rotary and Slider Controls
V.U. Meter
Inputs: 4 - Mic (0.5mV)
1 - Mag Phono (3mV)
1 - Aux (200mV)



£276.00

Designed and developed to meet - and surpass - European performance standards, this P.A. amplifier boasts a power handling of 175W (R.M.S.). It is protected against short circuit output and incorrect battery connections. Each of the four input channels has its own rotary gain control and individual slide switch operating FLAVIO filters. Overall bass and treble levels are set by slide controls; overall volume level is obtained by observing the meter 2" V.U. meter and operation of the extra large Master control. Operation is from A.C. mains or from 24V D.C. 4 inputs are low impedance with a 3mV sensitivity; magnetic phono input with R.I.A.A. equalisation provided through a 5-pin DIN socket (3mV). An additional input accepts signals from turners, tape recorders etc. (200mV). Output matching is to 4, 8 and 16 ohms, 70V and 100V lines plus booster amplifier socket. The casing incorporates front grab handles and protective feet, and can be used free standing or rack mounted.

MICROPHONES - supplied c/w lead, jack plug, busby, U-bracket (if appropriate)

M12	CONDENSOR CARDIOD - 600 OHM	£26.43
M20	ELECTRET CONDENSOR, OMNI-DIRECTIONAL - 600 OHM	£13.80
M21	ELECTRET CONDENSOR, UNI-DIRECTIONAL - 600 OHM	£19.32
M30	DYNAMIC CARDIOD, BALL WINDSHIELD - 50K / 600 OHM	£28.98
M48	ELECTRET PAGING, CARDIOD. (CAST BASE) - 600 OHM	£26.22
M50	COMMUNICATIONS, OMNI-DIRECTIONAL. (HAND HELD) - 600 OHM	£ 6.90

MICROPHONE STANDS

M121	BANQUET STAND, CAST BASE - 11" TO 18½"	£ 7.66
M122	TRIPOD TABLE STAND, SCREW IN LEGS - 4½"	£ 5.11
M124	FOLDING FLOOR STAND - UP TO 60"	£14.49
M125	STUDIO FLOOR STAND, SCREW IN LEGS - UP TO 63"	£20.70
M129	SOLID BASE FLOOR STAND, CAST BASE - UP TO 54"	£17.25
M130	FLOOR STAND WITH CURVED BOOM, SCREW IN LEGS - UP TO 59½"	£31.05

MICROPHONE ACCESSORIES

M142	12" FLEXIBLE GOOSENECK STEM - CHROME FINISH	£ 3.80
M143	20" FLEXIBLE GOOSENECK STEM - CHROME FINISH	£ 4.83
M170	GOOSENECK FLANGE ADAPTOR - BLACK SPRAYED CASTING	£ 2.14
M1040	WINDSHIELD COVER (BUSBY) - MEDIUM (ENTRY 17MM DIA.) PER PAIR	£ 1.59
M1041	WINDSHIELD COVER (BUSBY) - LARGE (ENTRY 32MM DIA.) PER PAIR	£ 2.21

MIXER

M104	SIX CHANNEL STEREO MIXER AND PRE-AMPLIFIER - BATTERY POWERED (accepts high & low impedance microphones, and has R.I.A.A. input)	£62.10
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SPEAKER SYSTEMS - CABINETS

L106	10W, 8 OHM - BLACK FOAM FRONT, 'TEAK' FINISH, 8" DRIVER. PER PAIR	£35.19
L110	40W, 8 OR 16 OHM (SPECIFY WHICH) - BLACK 'VYNYDE' COVERING (fitted with metal corner protectors and complete with a slip-on cover)	£89.70



SPEAKER SYSTEMS - HORNS

L73	5W, 8 OHM WEATHERPROOF HORN, SUITABLE FOR VEHICLE USE	£14.15
L74	10W, 8 OHM METAL HORN	£26.97
L76	10W, 8 OHM WEATHERPROOF A.B.S. HORN	£12.42
L77	15W, 8, 660, 1K0, 2K0, 4K0, 100V LINE WEATHERPROOF ALUMINIUM	£27.60
L78	20W, 8, 500, 600, 1K0, 2K0, 100V LINE WEATHERPROOF ALUMINIUM	£47.40
L78-B	AS FOR L78, BUT 8 OHM IMPEDANCE ONLY	£28.75

CABLES

Z2	MICROPHONE CABLE, HEAVY DUTY, SINGLE, GREY (16/0.2mm centre conductor, 100m reel)	£21.95
Z25	FIGURE 8 FLEXIBLE, RIB POLARISED, GREY (13/0.2mm conductors, 100m reel)	£ 3.27
Z29	TWO CORE OVAL, GREY (16/0.2mm conductors, 100m reel)	£17.25
Z55	6 AMP MAINS LEAD, THREE CORE, ORANGE (24/0.2mm conductors, 50m reel)	£16.25
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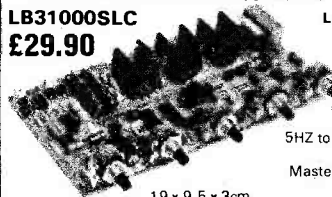
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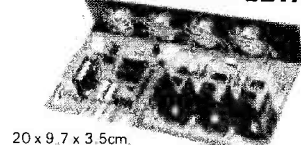
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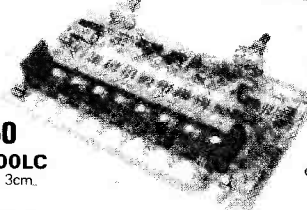
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1000w per channel. CMOS circuitry. Zero voltage fired. Can be footswitch triggered. Additional modules can be cascaded to form 16, 24, 32 chan. ect

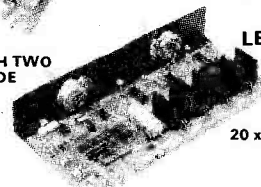
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LB81000LC
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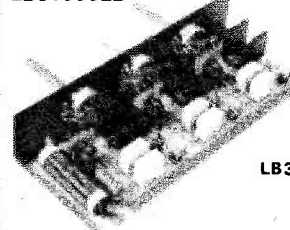
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LB31000LD £14.70 LB11000LD £6.70

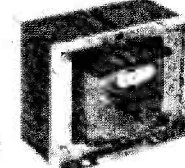
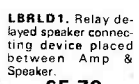


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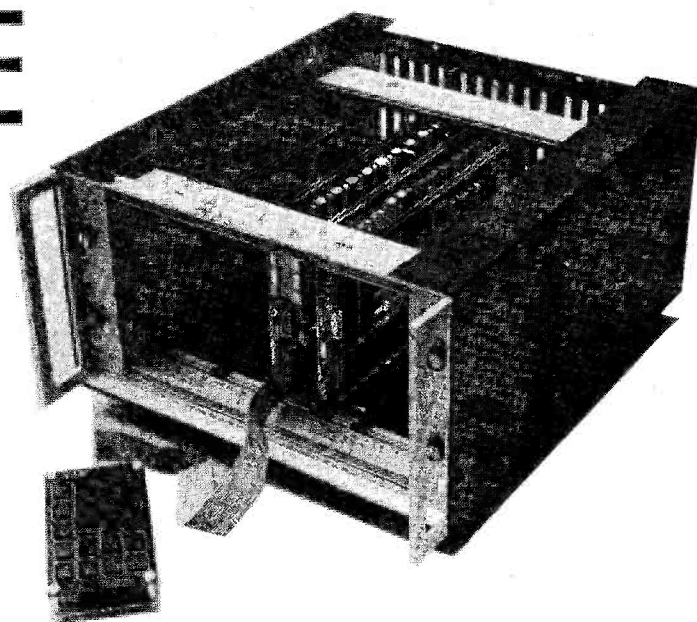
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MICROFILE

Henry Budgett leafs through the latest Vero catalogue to case his computer collection.



Welcome, once again, micro-fans to the world of small systems. I see that the ZX 80 topped the ratings for interest value last month, more on that in just a minute. Our busy network of spies has been burrowing deep into the fabric of both government and industry to bring you the following news items at great personal risk.

Micros For Schools

A mole, deep within the echelons of the Department of Industry, has revealed the existence of an intrepid plot to give microcomputers to schools. Naturally there is a catch, or 22, you have to enter a competition. Seriously though, a competition – in essay form – will be shortly announced for secondary schools with, currently, 100 British micros as prizes. Talks are being held with local industry and banking institutions in the hope that more finance – and hence more prizes – will be forthcoming. Your Headmaster should have received details by now and a full Press release will shortly be given so watch this space for further details wild horses wouldn't make us reveal what system is being considered!

The Case For Nascom

One of Microfile's more intrepid investigators recently emerged, smiling, from the latest Vero catalogue. It seems that the range of parts is so vast that you can box and house anything. The outcome of this is that if you order a 3D-N card frame you will be able to house your Nascom (1 or 2) for a mere £24.28. Added extras, such as modules, card fronts, Veroboards, edge connectors and a whole lot more can also be purchased along with a nice case to fit round it all.

Also discovered, and now in full-time use, is a card frame/case to house a Tangerine system along with all the extras such as a module to fit the necessary power supply into. This is a half width, extended System KM4C with card guides for International boards (whew). The same frame can also take Acorns by fitting Eurocard guides and an indirect connector plate. Subtle stuff all this, and much more fun than just asking for "the box"!

Research Into Sinclair

It appears that the author of this column may have been led a trifle astray during his research into the insides of the ZX 80. Shortly after the issue hit the streets a letter arrived from Clive Sinclair which refuted a number of points raised in the item. Here, in its entirety is the letter and readers who seek a fuller insight into the workings of the machine should either stifle their impatience or rush out and buy a copy of June Computing Today, which contains a full review.

Dear Mr. Harris,

The news item in the Microfile column of your April issue says some nice things about our ZX80 computer, for which many thanks, but unfortunately there are one or two errors of fact which I would like to correct.

The first is that the operating language is not Tiny BASIC but quite a powerful true BASIC with, we believe, better editing facilities and greater speed than any of our competitors.

Again, contrary to the news item the ZX80 has full machine code facilities. Although it is true that RAM extension is limited to 16K bytes, this is no small quantity when the tight packing the ZX80 achieves in its RAM is considered. Indeed, I suspect that more lines of BASIC can be accommodated on the ZX80 than on any of the competitors, all of which cost several times the price. At the other extreme the excellent Hewlett Packard machine costing around £3,000 accommodates a maximum of 32K bytes of RAM.

The final remark in the column doubts the practicality of adding new ROM's, extra languages and discs to the machine on the grounds that "the CPU is already rather overworked". The only thing the CPU does in our machine which it does not do in others is to drive the display, thereby saving integrated circuits, board area and costs, which is reflected in our selling price. It is not "overworking" the CPU in any sense as it would otherwise be idle during the display period.

A new plug-in ROM will soon be available at an additional cost of around £20, extending the maths. capability of the computer to include log. and trig. functions, and also increasing the data handling capacity and incorporating a floppy disc facility.

*Yours sincerely,
Clive Sinclair.*

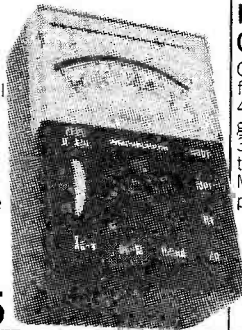
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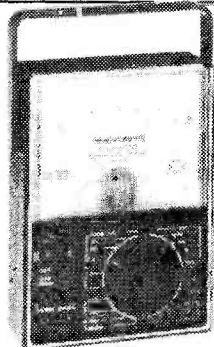


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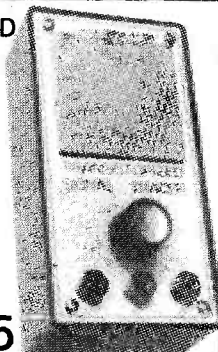
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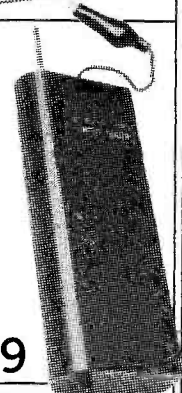
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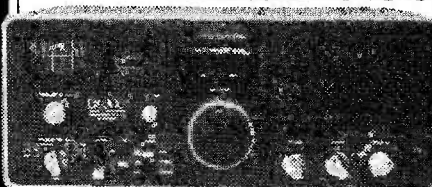
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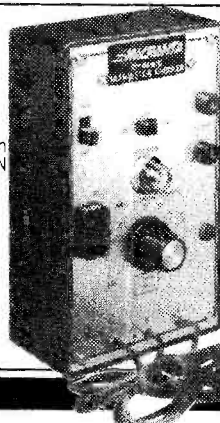
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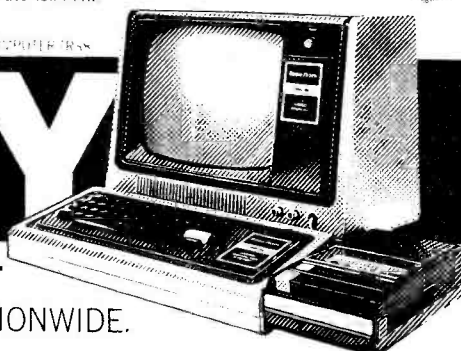
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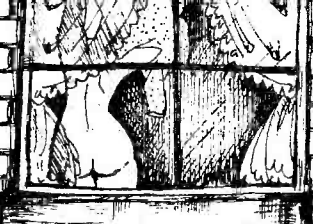


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RULES
NO?

LIVERPOOL
FOR THE
CUP

Another Brick In the Wall?

Why is this written on a wall?
Did it have to be so tall?
Read our next issue and find out.

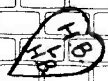
The Ultimate Systems Review

Never in the field of Personal Computing have so many systems come under the microscope in a single month. We shall be featuring at least six machines in a wide variety of categories from small business, through scientific down to low cost single boarders. Without giving it all away we will be following up on the HP85 in greater detail and also poking around in a newly launched system that is threatening to take the world by storm. After all, if we told you everything you wouldn't want to buy the next issue!

I.G.
L.H.

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Articles mentioned herein are in an advanced state of preparation, however, circumstances may dictate changes to the final contents.



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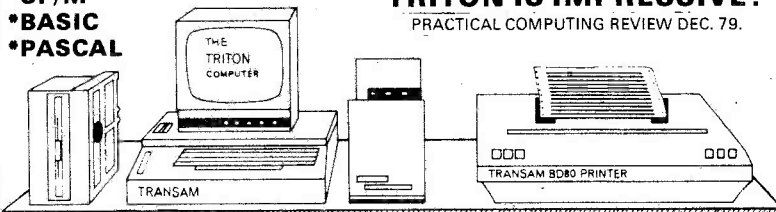
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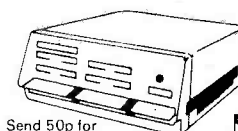
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SN74LS15N	25	SN74LS67N	80	SN74LS162N	115	SN74LS250N	145	SN74LS338N	132	8259	12.50	4044	7.00
SN74LS16N	20	SN74LS68N	95	SN74LS163N	90	SN74LS251N	125	SN74LS339N	140	8155	12.50	4045	7.00
SN74LS17N	26	SN74LS69N	120	SN74LS164N	150	SN74LS252N	140	SN74LS331N	365	8402	5.00	4050	7.00
SN74LS18N	26	SN74LS70N	175	SN74LS165N	170	SN74LS253N	95	SN74LS336N	57	8821P	4.50	2107	7.80
SN74LS19N	29	SN74LS71N	39	SN74LS166N	175	SN74LS254N	145	SN74LS330N	198	8850P	4.80	4116(58 for 8100)	8.00
SN74LS20N	35	SN74LS72N	39	SN74LS167N	185	SN74LS255N	39	SN74LS333N	150	8852P	5.50	4118	20.00
SN74LS21N	35	SN74LS73N	39	SN74LS168N	195	SN74LS256N	350	SN74LS335N	180	AY52376	11.50	280P10	8.00
SN74LS22N	25	SN74LS74N	44	SN74LS169N	195	SN74LS257N	140	SN74LS336N	170	MC14411	12.00	280CTC	8.00
SN74LS23N	27	SN74LS75N	44	SN74LS170N	250	SN74LS258N	95	SN74LS337N	175	M57109	12.43	280AP10	9.50
SN74LS24N	39	SN74LS76N	70	SN74LS171N	115	SN74LS259N	79	SN74LS339N	160	M57160	10.00	280ACTC	9.50
SN74LS25N	29	SN74LS77N	39	SN74LS172N	105	SN74LS260N	180	SN74LS340N	150	M57181	10.00	EPROMS	5.00
SN74LS26N	29	SN74LS78N	150	SN74LS173N	175	SN74LS261N	180	SN74LS341N	125	TM56011	5.00	1702	5.00
SN74LS27N	25	SN74LS79N	65	SN74LS174N	175	SN74LS262N	180	SN74LS342N	125	81LS05	1.80	5204	5.00
SN74LS28N	79	SN74LS80N	65	SN74LS175N	105	SN74LS263N	180	SN74LS343N	185	81LS06	1.80	2708	8.00
SN74LS29N	95	SN74LS81N	35	SN74LS176N	145	SN74LS264N	220	SN74LS344N	95	81LS07	1.80	2516	25.00
SN74LS30N	95	SN74LS82N	75	SN74LS177N	175	SN74LS265N	220	SN74LS345N	95	81LS08	1.80	2532	50.00
SN74LS31N	109	SN74LS83N	40	SN74LS178N	189	SN74LS266N	220	SN74LS346N	95	81LS09	1.80	2532	50.00

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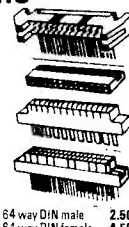
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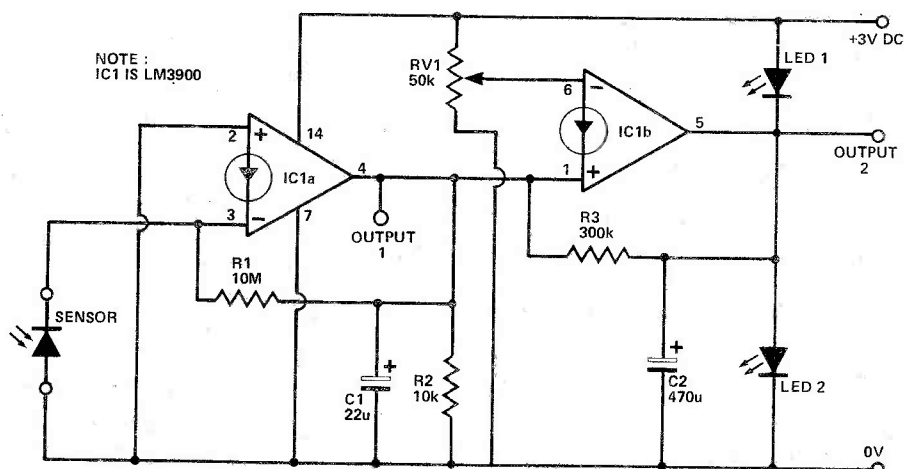
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TECH TIPS

Light/Temperature Indicator

M Miller, Reading

Using half a LM3900 quad Norton amplifier, either light or temperature can be monitored with this device. In the light monitoring mode a reverse biased LED was used (a clear type, not opaque) at output 1. The light value can be measured with a high impedance voltmeter, approximately 0-30 V FSD. RV1 sets a threshold voltage to IC1a, so that either LED 1 or LED 2 will be on depending on whether output 1 exceeds the threshold voltage or not. In the temperature mode a 1N4148 diode was used, also reverse biased. The amplifier outputs are the same as in the light monitoring mode.



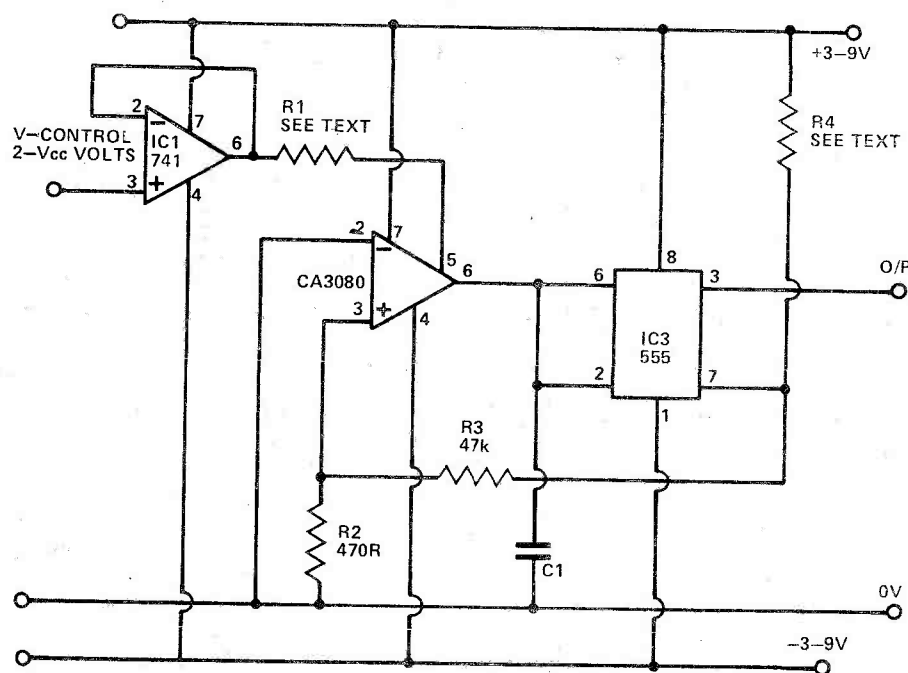
555 Voltage Control

S Draper, Lincoln

This circuit was developed to provide a cheap, reliable and accurate voltage controlled oscillator. It uses readily available components and the control over mark-space ratio common to other 555 circuits is retained. Frequency-voltage response is linear over approximately one decade making the circuit useful in timing applications. Operation is as follows:

IC1 buffers the input voltage and produces the control current for IC2. IC2 is an operational transconductance amplifier and produces an output current proportional to the control current multiplied by the differential input voltage. This output current is used to charge and discharge the capacitor C1 in the normal way. The equation for output high and output low times are given below:

$$\text{Output high time} = \frac{R1C1(47.5+R4)}{9024 V_{\text{control}}}$$



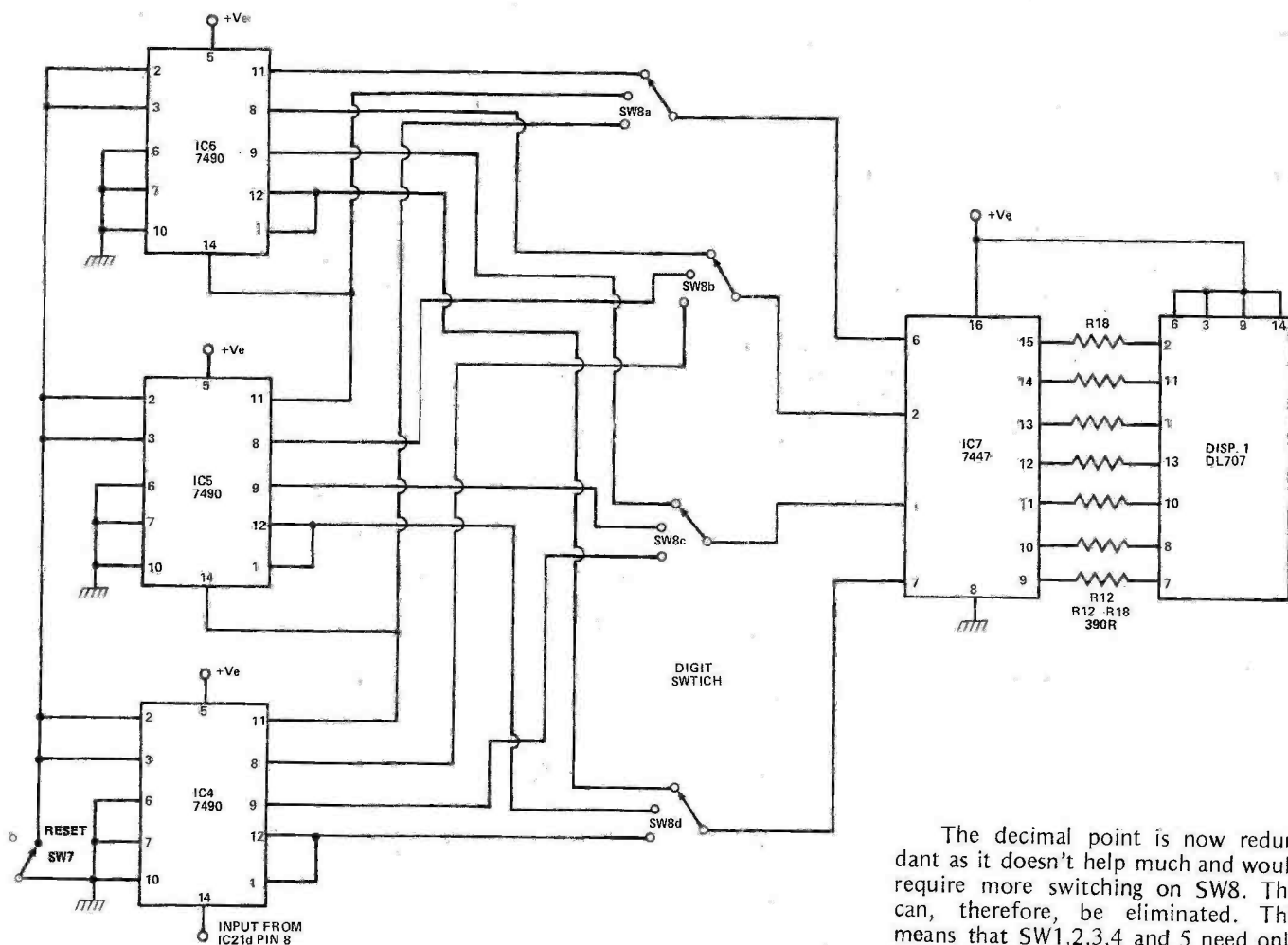
$$\text{Output low time} = \frac{R1C1}{192V_{\text{control}}}$$

where all resistances are in kilohms and all capacitances are in microfarads.

Current consumption is a miserly 10 mA from a 12 V supply making the unit suitable for battery power.

N.B. — R1 should not be less than 18 k.

Tech-Tips is an ideas forum and is not aimed at the beginner. We regret we cannot answer queries on these items. ETI is prepared to consider circuits or ideas submitted by readers for this page. All items used will be paid for. Drawings should be as clear as possible and the text should preferably be typed. Circuits must not be subject to copyright. Items for consideration should be sent to ETI TECH-TIPS, Electronics Today International, 145 Charing Cross Road, London WC2H 0EE.



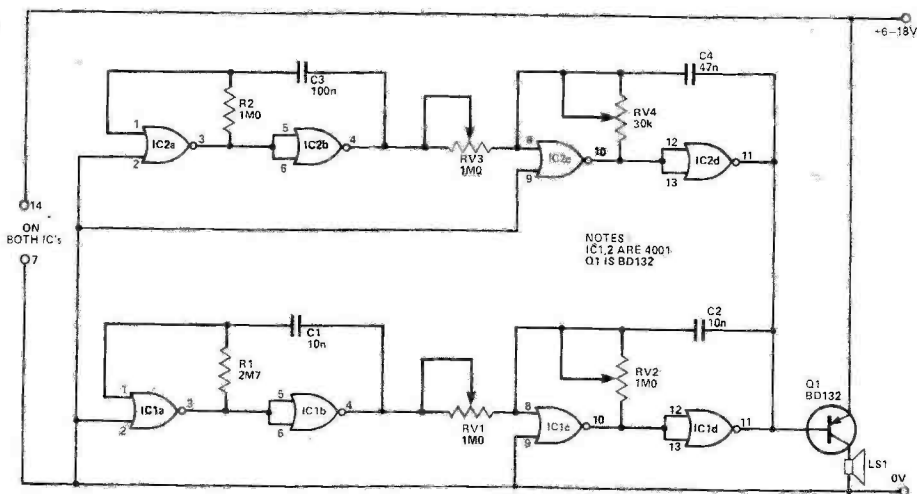
DFM Mods

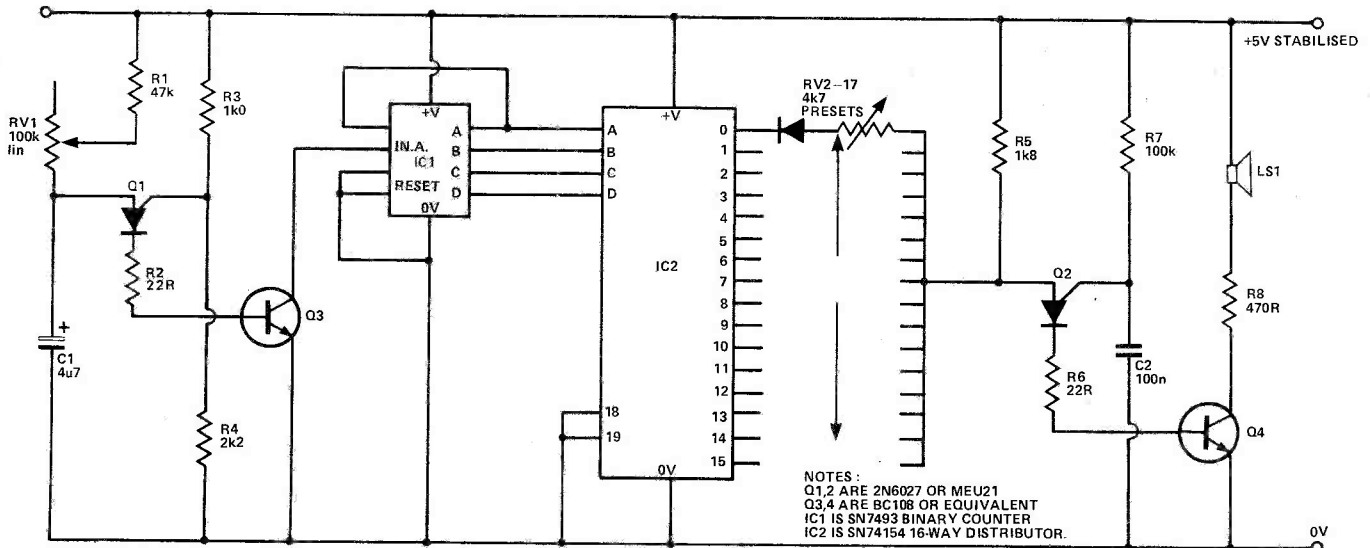
R Lea, Amersham

This is a simple, cost reducing modification to the DFM published in ETI June 1977. The need for three decoders and displays has been reduced to one.

The outputs from the counters (IC4-6) are switched via SW8 to a single 7447 decoder (IC7) driving a DL707 display. In use, the 'test' button on the original unit is pressed. When counting is complete, SW8 can be cycled through the digits to obtain a reading.

The decimal point is now redundant as it doesn't help much and would require more switching on SW8. This can, therefore, be eliminated. This means that SW1,2,3,4 and 5 need only be two pole, so they can all be incorporated one 2p 6w rotary switch, further reducing cost. These two modifications do make the meter slightly less convenient in use, but this is outweighed by the reduced cost. To modify the existing PCB the tracks to pins 1,2,6 and 7 of IC7 are cut and it is then a simple matter to insert SW8 as shown.





16 Note Sequencer

P Gatehouse, Buckingham

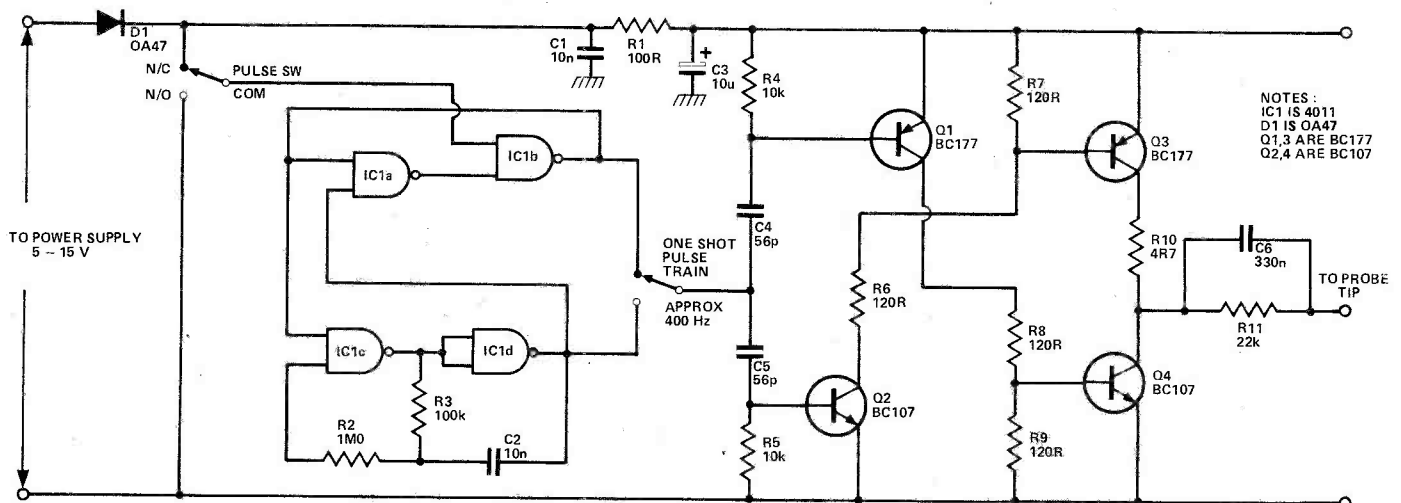
This circuit is designed to play a repeating sequence of 16 notes which are programmed by variable resistors. IC1 is a binary counter which runs off a PUT oscillator. The oscillator is built around Q1, which can be a 2N6027 or MEU21. The RC time constant connected to the anode charges up, causing the voltage at the anode to rise. At a certain voltage, controlled by R3 and R4, the PUT conducts. This allows the capacitor to discharge through Q3 as a good clean clock pulse. Q3 inverts the pulse to suit

the TTL requirements. The frequency of these events is easily changed by altering the time constant — a 100 k variable resistor was used.

IC1 generates a binary count on its four outputs — only if you ground both the reset terminals. IC2 selects a single output line for each of the sixteen possible input combinations. The result is that the presets are connected one-by-one, in sequence. Q1 is the audio frequency oscillator, whose frequency can be changed by altering the resistors which determine the anode voltage of the PUT. Don't be tempted to leave out the diodes in series with the presets as

they block the normally 'high' outputs from interfering with the selected 'low' output. The type of diode used is not critical. 1N914s are probably the best (and cheapest).

Interesting results can be obtained by connecting a fairly large capacitor to various parts of the gate terminal of the second (AF) oscillator. Connect the other terminal ground or positive line — watch the polarity, if it's electrolytic. Another oscillator can be connected to the same outputs provided it is fitted with diodes isolating it from the first oscillator. If the outputs are mixed, polyphonic effects are possible.



CMOS/TTL Pulser

C T Morris, Mid Glamorgan

For a small extra outlay, a pulse train facility can be added to the ETI Pulser that appeared in December 1975. The

NAND gates form an astable, which is gated by a flip-flop. When the pulse switch is pressed the flip-flop changes state and turns on the astable. Single shot or pulse trains are selected by a

change-over switch connected to the flip-flop and astable outputs.

The OA47 diode protects the pulser against reversal of the power supply leads.