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MANY MORE KITS ON PAGE 8


Single chip control system. p. 15


Sounds for Project 80. p. 79


From micro to tape in a flash. p. 63



## FEATURES

DICEST 7 You read it first here. SPOT DESIGNS 22 Six page circuits special. SPECIAL RELATIVITY $35 E=m c^{2}$ and all that AUDIOPHILE $48^{\circ}$ News from the top deck. TECH TIPS 59 Pages of your own designs. HEAD AMPLIFIER DESIGN 69 Match-making in your home. DESIGNER'S NOTEBOOK 73 Hot sensations on the test bench. ASTROLOGUE 84 A dialogue in astronautics. MICROBASICS 87 The anatomy of a micro.<br>ELECTRONICS TOMORROW 92 From mechanics to chips.

## PROJECTS

| FM RADIO CONTROL | 15 | One chip remote control. |
| ---: | :--- | :--- |
| FLASH TRICGER | 30 | Economical special effects. |
| VOCODER | $\mathbf{4 0}$ Orchestration par excellence! |  |
| FUZZISUSTAIN BOX | 53 Cuitar sounds you must have. |  |
| CASSETTE INTERFACE | 63 Extra-fast micro data transfer. |  |
| MONITOR AMPLIFIER | $\mathbf{7 9}$ Hear what Project 80 has to say. |  |
| FOIL PATTERNS | 108 | PCBs in black and white. |

## INFORMATION

NEXT MONTH'S ETI
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Remember, remember ETI November.
NEXT MONTH'S HE
33 The Hobby Electronics to come.

EDUORIAL. AND ADVERTEZAKNT OFFICE



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# computer kit. The Sinclair ZX80. 

Britain's first com

Price breakdown
ZX80 and manual: £69.52
VAT: £10.43
Post and packing FREE
Please note: many kit makers quote VAT-exclusive prices.
You've seen the reviews ... you've heard the excitement...now make the kit!

This is the $\mathbf{Z \times 8 0}$. 'Personal Computer World' gave it 5 stars for 'excellent value.' Benchmark tests say it's faster than all previous personal computers. And the response from kit enthusiasts has been tremendous.

To help you appreciate its value, the price is shown above with and without VAT. This is so you can compare the $2 \times 80$ with competitive kits that don't appear with inclusive prices.

## 'Excellent value' indeed!

For just $£ 79.95$ (including VAT and p\&p) you get everything you need to build a personal computer at home ... PCB, with IC sockets for all ICs; case; leads for direct connection to a cassette recorder and television (black and white or colour): everything!

Yet the ZX80 really is a complete, powerful, full-facility computer, matching or surpassing other personal computers at several times the price.

The ZX80 is programmed in BASIC, the world's most popular computer language for beginners and experts alike.

The ZX80 is pleasantly straightforward to assemble, using a fine-tipped soldering iron., It immediately proves what a good job you've done; connect it to your TV... link it to an appropriate power source ${ }^{\star}$. . and you're ready to go.

## Your $\mathbf{Z X} 80$ kit contains...

- Printed circuit board, with IC sockets for all ICs.
- Complete components set, inciuding all ICs-all manufactured by selected worldleading suppliers.
- New rugged Sinclair keyboard, touchsensitive, wipe-clean.
- Ready-moulded case.
- Leads and plugs for connection to domestic TV and cassette recorder. (Programs can be SAVEd and LOADed on to a portable cassette recorder.)
- FREE course in BASIC programming and user manual.
Optional extras
- Mains adaptor of 600 mA at 9 V DC nominal unregulated (availabie separately-see coupon).
- Additional memory expansion boards allowing up to 16 K bytes RAM. (Extra RAM chips also available-see coupon).

[^1]
## The unique and

 valuable components of the
## Sinclair ZX80.

The Sinclair $Z \times 80$ is not just another personal computer Quite apart from its exceptionally low price, the ZX80 has two uniquely advanced components: the Sinclair BASIC interpreter; and the Sinclair teachyourself BASIC manual.

The unique Sinclair BASIC interpreter offers remarkable programming advantages: - Unique 'one-touch' key word entry: the ZX80 eliminates a great deal of tiresome typing. Key words (RUN, PRINT, LIST, etc.) have their own single-key entry.

- Unique syntax check. Onily lines with correct syntax are accepted into programs: A cursor identifies errors immediately. This prevents entry of long and complicated programs with faults only discovered when you try to run them.
- Excellent string-handling capability-takes up to 26 string variables of any length. All strings can undergo all relational tests (e.g. comparison). The ZX80 also has string inputto request a line of text when necessary. Strings do not need to be dimensioned.
- Up to 26 single dimension arrays.
- FOR/NEXT loops nested up to 26 .
- Variable names of any length.
- BASIC language also handles full Boolean arithmetic, conditional expressions, etc.
- Exceptionally powerful edit facilities, allows modification of existing program lines.
- Randomise function, useful for games and secret codes, as well as more serious applications.
- Timer under program control.
- PEEK and POKE enable entry of machine code instructions. USR causes jump to a user's machine language sub-routine.
- High-resolution graphics with 22 standard graphic symbols.
- All characters printable in reverse under program control.
- Lines of unlimited length.

Fewer chips, compact design, volume productionmore power per pound!

The $Z \times 80$ owes its remarkable low price to its remarkable design: the whole system is packed on to fewer, newer, more powerful and advanced LSI chips. A single SUPER ROM, for instance, contains the BASIC interpreter, the character set, operating system, and monitor. And the $Z \times 80$ 's 1 K byte RAM is roughly equivalent to 4 K bytes in a conventional computer-typically storing 100 lines of BASIC. (Key words occupy only a single byte.)

The display shows 32 characters by 24 lines.
And Benchmark tests show that the ZX80. is faster than all other personal computers. No other personal computer offers this unique combination of high capability and low price.


ETI OCTOBER 1980


## ZX80 softwarenow available!

See advertisements in Personal Computer World, Electronics Today international, and other journals.

New dedicated software-developed independently of Science of Cambridgerefiects the enormous interest in the $\mathrm{ZX80}$. More software available soon-from leading consultancies and software houses

If the specifications of the Sinclair $Z \times 80$ mean little to you-don't worry. They're all explained in the specially-written 128-page book free with every kit! The book makes fearning easy exciting and enjoyable, and represents a complete course in BASIC programming-from first principles to complex programs (Available separately-purchase price refunded if you buy a $\mathrm{ZX8O}$ later.) A hardware manual is also included with every kit.

The Sinclair ZX80. Kit: £79.95.

## Assembled: £99.95. Complete!

The $Z \times 80$ kit costs a mere $£ 79.95$. Can't wait to have a ZX80 up and running? No problem! It's also available, ready assembled and complete with mains adaptor, for only $£ 99.95$

Demand for the $Z \times 80$ is very high: use the coupon to order today for the earliest possible delivery. All orders will be despatched in strict rotation. We'll acknowledge each order by return, and tell you exactly when your $\mathrm{ZX80}$ will be delivered. If you choose not to wait, you can cancel your order immediately. and your money will be refunded at once. Again. of course, you may return your $Z \times 80$ as received within 14 days for a full refund. We want you to be satisfied beyond all doubt - and we have no doubt that you will be

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# DIGEST 

## WatchOut

C or under $£ 44.95$ you too can own F a new Casio watch with cortinuous time readout, date display, full month, calendar information, professional grade stopwatch, plus alarm and time signal functions with a choice of tone pitch. What more can you ask fori And it's all in the 79CS51B Casio Stopwatch. A conventional LCD readout shows hour, minute, second, am/pm and date. Push a button to display year, month date and day. Press again for full calendar and cycle the display through earlier and later months if so desired. The automatic calendar is programmed from 1901 to 2099. As a stopwatch the 79CS51B has a running time of 12 hours and a measurement unit of one-tenth second. It handles normal start-stop timing, net timing, lap timing and first-second place timing. The watch will also sound an alarm at any preset time and/or signal every hour. One lithium battery will last about 15 months average use. For further in formation contact Casio Electronics Co Lid, 28 Scrutton Street, London EC2A 4TY.

## EMP - The Answer

A
Il our inquiries addressed to the Prime Minister, the Home Secretary and the Secretary of State for Defence on the Government's plans to cope with the Electromagnetic Pulse effect (EMP) in wartime eventually found their way to the same office somewhere in the depths of the Home Office. This is what HM Government has to say: 'Her Majesty's Government is aware of the phenomenon of EMP and its possible effects on communications systems. We take it into account in the design of civil and defence systems but cannot, of course, comment on the details of all the forms of EMP protection used.

The Home Office has given guidance to local authorities and other essential services concerned with the planning of communications systems for war, on the effects of EMP and about certain precautions that can be taken to reduce the risk of EMP damage to communications equipment.

The requirements for home defence communications are currently being reviewed and possible measures to protect them against the effects of EMP will be considered in the course of the review.'

So, it seems the Government and local authorities know all about EMP, but they aren't going to tell the likes of us.

In a statement to the Commons on August 7th, the Home Secretary (William Whitelaw) outlined
developments in Britain's civil defence programme. The UK warning and monitoring organisation is to improve its communications. Improvements are also to be made to the wartime broadcasting service to ensure the continuation of public broadcasting even after a large-scale attack (but no mention of EMP).

After a lengthy pronouncement on Central/Local Government cooperation in wartime, increased expenditure on equipment and services, greater involvement in civil defence by Central Government departments and finishing up with news of the refurbishment of our stocks of emergency fire appliances (Green Godesses?), Mr. Eric Heffer's immediate reaction was, "The right hon. Gentleman must be joking'.

We'll keep you posted on any further developments. Keep your letters coming. These given here are representative of those we have received so far. This article has stimulated a greater reader response than anything previously published in ETL. Most of our correspondents have understood the need for caution in our approach to publication.

The letter from Mr Keightley is particularly interesting and we are contacting Mr J. Pawsey MP to gather his views on the subiect. In addition investigations are under way to find out exactly what that "guidance to local authorities" referred to in the Home Office reply consists of and of how much use it has

## This Is A

 RecordingThe Compur 385 is a new tele phone answering machine from Agovox. It is a compact module which sits neatly under a conven tional telephone. The facilities available include a remote control electronic decoder which enables the machine to be telephoned from anywhere in the world and in structed to play back over the telephone any messages received from previous callers. The machine is also capable of recording both sides of a conversation and can be linked
proved to be. We hope to be able to report back next issue on the results of that investigation.

In the meanwhile keep your letters coming to us and why not follow Mr Keightley's example and write to your local MP? Maybe together we can overcome the vast governmental inertia and raise the heads above the sand just a little.

Dear Sir,
I think you should visit the inside of a NATO USA or British Radar Command Station.

We have in the UK high gain very large units operating on all bands ie:- VLF to UHF by a switching unit thus making jamming very hard because the unit sends out piano type signal and only receives back the same. All are sent out through banks of pure mechanical harmonic filters, that also process the received signal. The Front end is in liquid He and of the thermocouple type. Most of the units have a large valve content of the ECC82 size.

All cable passing through the 14 g sheet steel building shield have 80 to 120 bd RFI filters even the power cable. The building is bonded every four feet against RFI.

You will find that you can get an electric shock from nylon rigging seven miles out from the radar station such is the power.

Thank you for bringing your statement to the public and that many items are covered up, it would seem that the designers took into account EMP in the design of the radar system and my part was commissioning the 3000 kW cooling system.
P.S. Do you think I have time to scrap my TI51 III which is very limited and purchase and use a TI59 before EMP!
M.C. Wadlow

Project Engineer
to a standard recorder for retaining permanent records of calls. It is also fully compatible with existing dictating machines which utilise minicassettes and has a foot switch and head set available. Message lengths can be limited and a call counter enables easy location and logging of messages. The 385 is available for rent at between £3.72 and £6.46 depending on the type of rental contract or $\mathbf{E} \mathbf{5 0}$ for outright purchase. For further information contact The Sales Office, Agovox Limited, 4 Sydenham Road, London SE26 5QY.

## Dear Sir,

Congratulations on a most interesting article ("EMP"; ETI August 1980). The text was crisp and informative.

In view of the potential devastating effect of EMP, I feel that more people, both the public and industrialists should be made aware of this aspect of, perhaps, an inevitable nuclear war.

For my part, I have been largely unaware of EMP but feel that I may be able to at least inform engineers and managers in telecommunications.

Yours sincerely,
S.F. Gatley

Senior Electronics Engineer
Plessey Telecommunications

Dear Sir,
Thanks to ETI for an informative article on EMP.

I have drawn this article to the attention of Mr Jim Pawsey, the Member of Parliament for Rugby, who is also the secretary of the Civil Defence Committee in the House of Commons.

He informs me that he has tabled a question in the House on this matter after reading your feature

As you may know, a major statement on Civil Defence by the Home Secretary has been promised before the House rises on August 8th.

Incidentally, a range of devices which offer protection from EMP are being marketed by Suhner. These incorporate a Cerberus gas discharge tube in a coaxial (50R) line.

Yours faithfully,
M.R. Keightley, B.Sc., C8BLK

Bilton, Rugby,
Warwickshire

## TRANSCENDENT DPX

## DIGITALLY CONTROLLED, TOUCH SENSITIVE, POLYPHONIC, MULTI-VOICE SYNTHESIZER

Another superb design by synthesizer expert Tim Orr - published in Electronics Today International
The T APX a red sound - fully polyphonic ie you can play chords with as many notes as you like. On the second output there is a wide range of different voices, still fully polyphonic. It can be a straightforward piano or a honky tonk piano or even a mixture of the two! Alternatively you can play strings over the whole range of the keyboard or brass over the whole range of the keyboard or should you prefer - strings on the top of the keyboard and brass at the lower end (the keyboard is electronically split after the first two octaves) or vice versa or even a combination of strings and brass sounds simultaneously. And on all voices you can switch in circuitry to make the keyboard touch sensitive! The harder you press down a key the louder it sounds - just like an acoustic piano. The digitally controlled multiplexed system makes practical touch sensitivity with the complex dynamics law necessary for a high degree of realism. There is a master volume and tone control, a separate control tor the brass sounds and also a vibrato circuit with variable depth control together with a variable delay control so that the vibrato comes in only after waiting a short time after the note is struck for even more realistic strong sounds.


Cabinet size $36.3^{\prime \prime} \times 15.0^{\prime \prime} \times 5.0^{\prime \prime}\left(\right.$ rear) $3.3^{\prime \prime}$ (front)

## COMPLETE KIT ONLY £299 +vat

To add interest to the sounds and make them more natural there is a chorus / ensemble unit which is a complex phasing system using CCD (charge coupled device) analogue delay lines. The overall effect of this is similar to that of several acoustic instruments playing the same piece of music. The ensemble circuitry can be switched in with either strong or mild effects. As the system is based on digital circuitry digital data can be easily taken to and from a computer (for storing and playing back accompaniments with or without pitch or key change, computer composing, etc., etc.)
Although the DPX is an advanced design using a very large amount of circuitry, much of it very sophisticated, the kit is mechanically extremely simple with excellent access to all the circuit oards which interconnect with multiway connectors, just four of which are removed to separate the keyboard circuitry and the panel circuitry from the main circuitry in the cabinet boards which interconnect with multiway connectors, just four of which are removed to separate the keyboard circuitry and the panel circuitry from the main cirla (all resistors $2 \%$ metal oxide), nuts, bolts, etc., even a $13 A$ plug!

## POWEFTRAN TRANSCENDENT 2000

MANY MORE KITS ON PAGE 116. MORE KITS AND ORDERING INFORMATION ON INSIDE FRONT COVER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento pitch bending a VCO with shape and pitch The TAANCNCF with both low and high pass outputs and a separate dynamic sweep control, a noice generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch doder
The kit includes fully finished metalwork, fully assembled solid teak cabinet, filter sweep pedal, professional quality components (all resistors either $2 \%$ metal oxide or $1 / 2 \%$ metal film l, and it really is complete - righ 13 A plug in the kit - you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality fibreglass PCB printed with component locations. All the controls mount directly on the main board, all connections to the board are made with connector plugs and construction is so simple it can be built easily in a tew evenings by almost anyone capable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready-built units selling for many times the price.

```
COMPLETE KIT ONLY £168.50 + VAT!
```



An F-14 wing-tip camera catches a glimpse of the first airborne launch of the new upgraded version of the Phoenix air-to-air missile.

## On Target

How does Wasp find its targets? Two sensors are under evaluation - infra-red and millimetre radar. Millimetre radar has three main advantages over infra-red. Its high resolution enables tanks to be distinguished from trees and buildings, it uses very small antennae and it is relatively unaffected by adverse weather conditions.

If a group of the missiles are fired at a number of targets, they will each attack a different target. If they can find only one target, it suffers a severe case of overkill. Wasp has a range of six miles when fired from an aircraft with a ground speed of 500 MPH . Two rival versions are under development by Boeing and Hughes.

## AIM To Kill

Earlier this year the US Navy's new AIM-54C Phoenix air-to-air missile was successfully launched from an airborne F-14. It intercepted a drone aircraft target, passing well within the 'kill' range, if the missile had been armed. The Hughes AIM54C, an improved version of the AIM-54A, carries a new digital electronics unit which is more flexible and reliable than the analogue unit it replaces. It also has a more effective target detector.

This first successful interception was achieved over a greater range than was possible with its predecessors. The F-14 launching aircraft travelled subsonically head-on towards the supersonic QF-4 fighter drone. In this launch, the Phoenix was guided on to the target by radar returns from the F-14's weapon control system. Closer to the target, it can switch to its own active radar system.

The upgraded Phoenix will become the US Navy's primary longrange air defence weapon in the 1990s.

A spacesuit was destroyed by fire at the Johnson Space Centre in April. Fortunately there was no-one in the suit at the time, although a technician was badly burned. To avoid a recurrence, a review board has recommended several modifications to the high pressure oxygen system and seals.

GEOS-D, the latest in a series of Geostationary Operational Environmental Satellites, is due to join its two companions in Earth orbit as we go to press. The 12 feet high by seven feet in diameter spacecraft will be launched from Cape Canaveral on September 9th by a three stage Delta 3914 booster. Next month I hope to bring you an in-depth report on this latest weather satellite and the GEOS system.

In July's Digest we brought you the sad news that the Viking Lander 2's batteries had run out of juice. The latest news on the Viking population of Mars is that Viking Orbiter 1 has now reached the end of its supply of attitude control gas. Viking Lander 1 is the only member of the foursome that is still functional.

We now know that the first Space Shuttle launch has been postponed from November this year until at least March next year. Next month Astrologue will look into the political, financial and technical problems that have beset the Space Shuttle from the start.


> Something Bugging You?

With the increase in telephone tapping and boardroom bugging, Audiotel International have developed a simple to use, yet sophisticated successor to their Scanlock radio surveillance receiver. It is called the Scanlock Mark V8 and is a fast, easy means of detecting and locating an eavesdropping transmitter as well as being capable of routine 'sweep' searches of high level meetings rooms. Carried in a vehicle it can also locate any bleeper bug used for 'trailing'.

The Scanlock is not limited to the conventional radio receiver's range of $88-108 \mathrm{MHz}$. It covers the wider frequency spectrum of $10-1800 \mathrm{MHz}$ and its automatic 'sweep' mode scans this range four times a minute. Finally all that is necessary is to press the 'Locate' button and use the hand-held wand to guide you to where the bug is located. The kit is the size of a small briefcase, weighing 6.3 Kg , complete with spare battery pack. There is also provision for mains usage. For further information contact Audiotel International LId at Saddlers Court, Yately, Surrey, GU17 7RX.

## Video Pirates

V ictor Company of Japan (IVC), who developed the popular VHS system, are concerned with the increasing number of unlicensed "pirate" VHS blank cassettes that are being imported into the UK. In response, they have issued the following statement to their dealers. 1. JVC hold an exclusive patent of the design, construction and appearance of VHS cassettes in the UK. 2. JVC will protect their rights. 3. JVC is concerned about the importation of unlicensed VHS cassettes into the UK because of their inferior quality as well as their illegality.

## Show Time

Virtually every major electronic manufacturer 1 spoke to at this year's American Summer Consumer Electronics Show claims to be perfecting speech capable products, whilst only a handful are available.

The leader in voice technology manufacturing is Texas Instruments. Two years ago the firm unveiled the industry's first speech capable product, Speak ' $n$ ' Spell, and the consumer electronics world hasn't stopped talking about it since. This year, Tl introduced two other talking 'electronic learning aids' and is also predicting a bright future for its talking translator. The $\mathbf{\$ 3 0 0}$ unit offers approximately 500 spoken and displayed words.

If you don't know what type of video tape system you should be using brace yourself because more befuddlement is brewing. Early next year in the States two manufacturers, perhaps even three, mutually incompatible video disc players will be each shouting the virtues of their products whilst cleverly knocking the others.

Pictures that I have seen from the newest Pioneer, Magnavox, JVC and RCA players are all amazingly detailed and noisefree. The Magnavox and Pioneer machines play compatible twelve inch discs by bouncing a focused laser beam from a spiral track of microscopic pits etched onto the disc's reflective surface. A clear plastic coating makes the disc immune to dust and smudges from handling.

RCA's Selecta Vision video disc player has been completely over-
hauled since it was introduced and field tested several years ago. The basic playback principle is unchanged; a stylus electrode replaced every two or three years, senses a TV signal as electrical capacitance variations in disc grooves spinning at 450 rpm . Playing time was boosted to one hour per twelve inch disc side by doubling disc grooves to just under ten thousand per inch. Home tests show that dust and other groove conta mination from handling messed up pictures. So RCA's improved Selecta Vision has a sealed disc caddy.

JVC have illustrated a system that combines the low cost aspects of selectavision with the operating options of free flowing slow motion etc. of optical machines. Not only that JVC included options for a super hi-fi audio disc. It calls the whole package its VHDIAHD System (VideolAudio High Density).

Signals are stored as capacitance variations from minute pits in the conductive plastic. The stylus rests over central spiral tracks distributing pressure and minimising wear. (Stylus life is 2,000 hours, roughly 10 times RCA's).

Sony's newest addition to its Beta family of accessories is the Beta stack model AG300. The unit automatically ejects and loads up to 4 Beta Max video cassettes with record, playback and re-wind capabilities; this accessory can be used with the current Beta Max models SL5400 and SL5600 or with the programmable SL5600. When used with the regular Beta Max models it offers a maximum of 20 hours recording time. With a programmable unit the change allows a user to record separate programmes on separate cassettes: up to 4 events on different
channels and different days within a two week period.

A new company, Activision, has released four new cartridges to work with the Atari video computer system; they are dragster, chequers, boxing and fishing derby. The general opinion is that these cartridges have a far higher resolution and superior game content than any of the Atari manufactured units; is this why Atari is suing them for $\$ 20$ million? Anyway these cartridges will certainly be available in the UK via at least one well-known mail order house.

Good news for all you home computer owners. At last you can connect with the real world. Yes, the BSR System X10 is going to be available in January 1981. In case you are unfamiliar with the system here is a brief run-down. Just plug in the command console and various modules into the household supply outlets and you're ready to take control. No special wiring is needed. From one convenient location you can control a bedroom light, hall light, television, radio, stereo, porch light, back door light as well as lights in the dining room. The command console comes in two versions, either with or without a cordless controller. The lamp module receives signals from a command console to turn on, off, dim or brighten any incandescent lamp up to 300 W . The wall switch receives signals from the command console to turn on or off or brighten any light or lamp normally operated by a wall switch up to 500 $W$ and the appliance module receives signals from the command console to turn an appliance on or off.
are to be installed at 69 sites throughout 15 European countries. Installation started in July in Berlin and should be completed by the end of 1981.

The type 101 VDUs to be supplied were designed specifically for airline operations. They use Halleffect, contactless, solid state keys for maximum reliability and life expectancy. The VDU is part of an integrated terminal system including cluster control units and terminal drive units, which can support up to 128 terminals.

## Eagle Sounds

E agle International have just introduced their new consumer catalogue for 1980/81. Although it's only 20 pages long it covers a lof of ground - hi-fi separates and rack systems, portable radios, in-car entertainment systems, etc.

You can get hold of a free copy of this full colour guide to Eagle's wares by writing to Eagle International, Precision Centre, Heather Park Drive, Wembley HAO 1SU.

## Fly The Flag

$T$he familiar terminals in British Airways reservations offices are getting a bit long in the tooth. They're ten years old. A British company, Videcom, has won the $\$ 500,000$ contract for terminal replacement, against competition from three other contenders - one British and two American. Videcom supplied a substantial number of the existing BA terminals.

The 280 new keyboard VDUs
of VHS recorders for which IVC are otherwise responsible.

So, you've been warned. Beware of cheap tapes and what they might do to your machine.

$$
\begin{array}{ll}
\text { 4. These illegal cassettes originate } & \text { standard dimension, construction, } \\
\text { from Taiwan, Singapore and Hong } & \text { mechanical operation and electrical } \\
\text { Kong - there are no VHS cassette } & \text { performance. This mav affect the } \\
\text { making licensees in these countries, } & \text { overall performance and operation }
\end{array}
$$ thus VHS cassettes which are identified as being made in these countries will be subject to legal proceedings from JVC when. imported into the UK. 5. These unlicensed products generally do not conform to VHS



## WAIFOMD EIEGTROWICS 33/35 CARDIFF ROAD, WATFORD, HERTS, ENGLAND MAIL ORDER, CALLERS WELCOME

 Tel. Watford (0923) 40588/9ALL DEVICES BRAND NEW, FULL SPEC. AND FULLY GUARANTEED. ORDERS DESPATCHED BY RETURN OF POST. TERMS OF BUSINESS: CASH/CHEQUE/ P. 8 OR BANKERS DRAFT WITH ORDER. GOVERNMENT AND EDUCATIONAL
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POSTAGEAT COST. AIR/SURFACE. ACCESS ORDERS WELCOME.

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| DPOT centre off | 7\% |
| OPDT biased 1 | 11 6p |

## ELIDE 250 V <br> 1 APDDT <br> 1A OPDT c /over 14p <br> $\begin{array}{ll}1 / 2 A D P D T & 13 p \\ 4 \text { pole 2-way } & 24 p\end{array}$ <br> PUBH AUTTON RPDT Black Body Red. Blue. Grn. Yell. SRL Lutching 12sp SRM Momentary 12 sp <br> MINL. Non Locking $\begin{array}{ll}\text { Push to Makt } \\ \text { Push Break } & \text { 15p } \\ \text { 25p }\end{array}$

DIL SWITCHES (SPST
ROTARY: Make your own mulkiway Swith ROTARY: Maks your own multiway Switch
Adjustable Stop Shafting Assembly An Adjustable Stop Shatting Assembly. Accom-
modere up to 6 Weters modare up to 6 Waters Brask Before Make Wafers. 1 pole 12 way. Spacer and Screen Motanl: (Adjusteble stop) 1 pole/2 to 12 way, $2 p / 2$ to 6 way, 3
 -
caystás

## 100 KHz

 455 K1 MH
100

|  |  | 6-0.6V: 9.0.9V: $12.0-12 \mathrm{~V} 100 \mathrm{~mA}$ |
| :---: | :---: | :---: |
| 55\% | 323 | 3VA: $0-6 \mathrm{~V} 0-6 \mathrm{~V}$ (PCB mounting) |
| 155 KH | 333 323 | 9VA: 6 V .5 A 6Y-.6A; 9 V .4 A 9 V |
| MHz | 323 | 12V.3A: 15 V . 25 A 15V - 25 A |
| O08M | 305 | $12 \mathrm{~V}: 4.5 \mathrm{~V}-1.3 \mathrm{~A} 4.5 \mathrm{~V}-1.3 \mathrm{~A}: 6 \mathrm{~V}-1.2 \mathrm{~A} 6 \mathrm{~V}$ |
| 28MHz | 392 | $12 \mathrm{~V}-5 \mathrm{~A}$ 12V-5A: $15 \mathrm{~V}-4 \mathrm{~A}$ 15V:-4A: 20 |
| .6MHz | 323 | 20V.3A ${ }^{\text {a }}$ 238p 130 |
| .8MHz | 323 | 24 VA : $6 \mathrm{~V}-1.5 \mathrm{~A}$ 6-1.5A: $9 \mathrm{~V}-1.3 \mathrm{~A} 9 \mathrm{~V}$ |
| . 8432 MH | 382 382 | 12V-1A 12V.1A; 15V.8A 15V.8A |
| . 4576 MH | 382 | 20V-6A 3200 (55 |
| .2768M | 323 | 50VA: 6V.4A 6V.4A. 9V-2.5A 9V-2.5A: |
| .57954M | 186 | A: $20 \mathrm{~V}-1.24$ |
| . 000 MHz | 200 | - 30 V - ${ }^{\text {a }}$ |
| . 032 MHz | 323 |  |
| .433619M | 135 | 100VA: $12 \mathrm{~V}-4 \mathrm{~A} 12 \mathrm{~V} .4 \mathrm{~A}: 15 \mathrm{~V}-3 \mathrm{~A}$ |
| . 0 MHz | 385 | 20V-2.5A 20V-2.5A: 30V-1.5A 3 |
|  | 323 | A 4OV-1.25A; |
| .24288M | 428 |  |
| S.ON | $323$ | our normal postal charge.) |

6.0 MHz
6553 M
7.680 M
7.680 M
8.0 MHz
8.0 MHz
8.08333 M
8.86723
9.375 M
9.376 M
10.0 MHz
10.7 MHz
124 MHz

-


MasPann


## Audiophile Amplifier

We've collected together all the corrections to the Audiophile Amplifier project in one place for easy reference.

If you've experienced any trouble with RF oscillation causing overheating in the power amplifiers, connect a 1000 pF capacitor across the base-collector leads of Q12 and a second 1000pF capacitor across the base-collector leads of Q13 (power amplifier circuit diagram, p.56). As a safety measure, R10 can be increased to 47R to reduce drive current and prevent overheating without loss of performance.

R15, 115 (p.62, Fig.4) mount directly on SW6. In the Parts List on the same page, C 10 should be 12 nF
polyester (or carbonate). The toggle switch shown on the rear of the power amplifier case (p.63) is a selector switch for the two pairs of speaker output sockets we used. It is a dual, three position, centre-off switch. P.64, Fig. 6 - R1 (2k2) in series with LED 1 should be R3 ( 2 k 2 ). The unmarked lead in Fig.8, p. 65 (third one down) goes to T1. There are three connections only to the 0 V tag - C3/C4 junction, C103/C104 junction, LED 1 cathode. All other 0 $\checkmark$ connections are made to the 0 V junctions of the smoothing capacitors. In Fig. 9 on the same page, the foil pattern of the component overlay has been printed upside down.

In the Parts List on p.65, the power amplifier supply transformer should be 25-0-25 $V$ and the transformer for the preamp supply should be $15-0-15 \mathrm{~V}$.


## Shocking Truth

Static is a nuisance all of us experience at sometime or other Often it only appears to be an irritating and uncomfortable surprise; not often enough is it realised that static can damage expensive equipment and lead to fire and other hazards in a working environment. 3 M has produced a 14 -page booklet outlining these hazards and it is available from Keith Nunn, Static Control Systems Group, 3M United Kingdom, PO Box 1, Bracknell Berkshire, RG1211U.

## Kit Update

We're still receiving news of kits, in response to our kit survey, featured in the May issue. Partridge Electronics have introduced a 'Community Mixer Kit', which, they claim, is unique, in that it is the first complete mixer designed specifically for applications like hospital broadcasting. The design and straightforward construction take into account the limited budget available to buy equipment for voluntary broadcasting organisations.

The mixer has been designed in modular form, so that you can buy a basic mixer kit for $\mathbf{£ 2 5 0}+$ VAT (8 input) or $£ 300+$ VAT ( 12 input) plus your choice of meter kit (VU, PRVU or PPM) plus your choice of preamp kit (microphone, disc, tape, cassette, etc). Each preamp kit comes in one of two forms (with or without equalisation). If you have some
money to
spare, you can also buy a number of extras, such as an autofade unit or a telephone interface studio terminal unit.

For further details contact Partridge Electronics, 56 Fleet Road, Benfleet, Essex SS7 5JN.

Hart Electronics can supply a range of cassette recorder and amplifier kits. Two high quality Linsey Hood cassette recorder kits are available at $£ 81.50$ + VAT and $\mathbf{£ 9 4 . 9 0 ~ + ~ V A T ~ r e s p e c t i v e l y . ~ T h e ~ V F L ~}$ 910 vertical front-loading deck hardware used in the top range model is available separately at $£ 31.99$ + VAT. Two 30 W amplifier kits complete the picture. For further information contact Hart Electronic Kits, Penylan Mill, Oswestry
Shropshire.




FM Radio Control receiver board (topside)


FM Radio Control receiver board (bottom side)


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FM Radio Control
Page 15 missing

The KB4445 is an $\mathbf{I}^{2}$ L bipolar IC, comprising a 4 channel multiplexer encoder, RF oscillator with FM modulator (switch type) with a 30 mW RF output.

It is also provided with an undervoltage warning system using a flashing LED when the supply voltage drops below 4 V 4 from a nominal supply of 6 V .

The encoder section consists of a string of cascaded RC monostable time constants, determining the pulse width according to the position of the external control potentiometers.

Channel and frame times are similarly externally programmable. Specification

| Item | Min | Typ | Max | Comments |
| :--- | ---: | ---: | ---: | :--- |
| Power supply (V DC) | 4 | 6 | 12 | LED flashes at 4V4 |
| Consumption (mA) |  | 20 |  | Oscillator stopped |

The KB4445 adopts one of the most universal encoder formats and is thus widely compatible with existing FM systems. The 'on-board' RF section is intended to be used as a driver for an external output stage and where sufficient supply voltage is available, a single power MOSFET may be used to achieve power levels in excess of 2 W .

The external circuit shown on the applications diagram delivers approx $\mathbf{4 0 0} \mathbf{~ m W ~ R F ~ t o ~ t h e ~ a n t e n n a , ~ w h i c h ~ i s ~ s u f f i c i e n t ~ f o r ~ r e l i a b l e ~ c o n t r o l ~}$ over 200 m with the KB4446 at the receiver.

Pin 12 of the KB4445 is the switching point of the modulator and it should be noted that the modulation action is achieved by switching an external capacitor in series with the crystal. Thus the level of deviation (more accurately termed modulation 'on' offset) may be controlled by a trimmable value at this point in the circuit. The capacitors across pins 10 and 11 form the feedback of a Colpitts oscillator and thus also affect the order specification of the transmit crystal in conjunction with the capacitor selected at pin 12.

Adjustment of the capacitor at pin 12 is an essentially iterative adjustment, altering the output frequency at the same time as the deviation
level, so care must be taken when setting up inital values in this part of the circuit

Pin 13 of the KB4445 offers access to the modulator switch filter and may thus be tailored to provide optimum bandwidth by selection of an external value.

## KB4446 Receiver IC

Specification

| Item | Min | Tyr | Max | Remarks |
| :---: | :---: | :---: | :---: | :---: |
| Supply voltage (V DC) | 2.1 | 3.0 | 4.0 | LED flashes at 2V2 |
| Supply current (mA) | 15 | 20 | 25 | at 3 V |
| Receiver sensitivity ( dBu ) |  | 26 |  | $20 \mathrm{db} \mathrm{S/N}$ |
| Limiting sensitivity (dBu) |  | 40 |  |  |
| Detector output (8) (mV) |  | 300 |  | 60dBu input |
| $\mathrm{S} / \mathrm{N}$ at 60 dBu in (dB) |  | 40 |  |  |
| LED drive current (mA) |  | 5 |  | At Vcc. 2V2 |
| Std puise width (uS) |  | 200 |  |  |
| Channel (ms) |  | 1.5 |  |  |
| Frame (mS) |  | 20 |  |  |
| Output source current (uA) |  | 100 |  | Decoder outputs |
| Output sink current (mA) |  | 2.0 |  | Int. 20k |

The KB4446 receiver IC uses a third overtone (30pF parallel load) crystal in the local oscillator circuit, selected to be either 455 kHz high or low of the incoming transmitter frequency. Oscillator low is usually preferred.

The mixer output will match either LCC IF filtering or ceramic filter systems in much the same way as the MC3357P. A tuned IFT is however recommended at this point in the circuit, since most ceramic filters will offer little or no attenuation to the local oscillator present at this pin.

The detector uses a standard form of quadrature at pin 2 of the IC a $\mathbf{Q}$ of approx $\mathbf{8 0}$ will give results in the above table, although other values may be used if provision is left to include a damping resistor. The choice of the coil will determine the output for a given deviation - in this case $\mathbf{2} \mathbf{k H z}$ is used as the reference (ie $\mathbf{4} \mathbf{~ k H z}$ total displacement.)

The detector output is fed to a comparator at the decoder input, which provides immunity to noise effects present on the detected signal. The values selected for the inputs at pins 21 and 22 will reject most HF noise and are based on the frame and pulse timing stated here. Other values may be used with nor-standard forms of timing sequence.

A good quality capacitor should be used at pin 20 since this is the reset timing capacitor, setting the frame at approximately $\mathbf{2 0} \mathbf{~ m S}$ total with the values shown.


Fig. 3 (right) Block diagram of the FM Radio Control link.

Fig. 4 Circuit diagram of the transmitter, based on the KB4445 IC from



Fig. 5 Circuit diagram of the receiver, built round the KB4446 IC, also from то́ко.

## Supply And Demand

The KB4446 is designed to work on the exceptionally low voltage supplies (from 2 V 1 to 4 V ) to be precise. This is because the standard servo supply rail of 4 V 8 is subject to a lot of fluctuation and noise from the effects of the DC motors continually stopping and starting. Despite NiCad batteries being a very low impedance power source, there is nearly always some effect on the supply voltage when the start and stall current of average servos are being drawn, but the difference between 4 V 8 and the nominal 3V0 of the KB4446 is quite enough to permit stabilisation via a pass transistor

Both ICs contain an under voltage LED indicator to let you know when the power is approaching a dangerously low level. The indicator need not necessarily be a LED, as the output is available to drive a variety of alternative warning devices. A high efficiency peizo-ceramic resonator may be a more satisfactory system for outdoors applications where the light of a LED is easily flooded by sunlight. A suitable circuit is shown in Fig. 6.

## Construction

The PCB and layout (Fig. 7) of the receiver reveals very little, apart from the fact that you will need a steady hand and a fine point on your soldering iron. The receiver was designed to fit into a standard plastic case with the facility to easily swap crystals and servo connections, so some aspects of the layout are not perhaps as ideal as the RF purist would have chosen. Nevertheless, it works.

The transmitter PCB is a straightforward device, since it is not necesssary to apply the same size constraints. The board is designed to slot into a standard case made by Micron radio control

## Testing And Setting Up

The first thing to do is to ascertain that the transmitter is working. Those with access to an oscilloscope can check the data frame shape and size. Reference back to the internal


Fig. 6 This piezo-electric resonator can be used as a low power alarm instead of a IED.
layout of the KB4445 (Fig.4) shows that the modulating waveform is available at pin 12 of the IC.

Carry out such tests with the crystal removed, since the close proximity of a strong RF field will tend to distort the readings of better (wide bandwidth) oscilloscopes. The frame signal should be set to 20 mS using the preset on pin 1 of the KB4445. If you do not have the necessary equipment to check this, set the 50k preset approximately halfway. The control sticks should similarly be set halfway.

The crystal may now be plugged in and attempts be made to set up the RF output. The best way to to do this is with a spectrum analyser (and who hasn't got one these days ??). The next best thing is an absorption wavemeter, which is easily made by using a standard frequency coil and a small meter (Fig. 9).

This is standard procedure in many RC transmitters, although you must be careful where to dangle the pickup section, since it is possible to get misleading results due to localized RF fields that have very little in common with what's actually being transmitted by the antenna. By placing the pickup close by the output of the KB4445 at pin 15, it should be possible to get a reading without too much trouble. If not, the best thing to do is find someone with a known working 27 MHz transmitter and adjust your wavemeter for peak reading with this.

| TRANSMITTER Resistors $1 / 4 \mathrm{~W}, 5 \%$ |  |
| :---: | :---: |
| R1 | 1k5 |
| R2 | 22k |
| R3,4,5,6 | 8k2 |
| R7 | 6 k 8 |
| R8 | 390R |
| R9 | 10R |
| R10 | 15R |
| Potentiometers |  |
| RV1-4 | 220k linear |
| PR1 | 47k preset |
| Capacitors |  |
| C1,2,11,14,16 | 10n ceramic |
| C3-6 | 20n ceramic |
| C7 | 14035 V tantalum |
| C8,10 | 1 nO ceramic |
| C9 | 180p ceramic |
| C12,13,20 | 10u 16V electrolytic |
| C15 | 27p ceramic |
| C17 | 39p ceramic |
| C18 | 150p ceramic |
| C19 | 22n ceramic |
| C21 | 100p ceramic |
| TC1,2 | 27p trimmer |
| Inductors |  |
| RFC1 | 10 turns 32/36 SWG enamelled copper wire on ferrite |
| 11 | 1uH |
| L2,3 | MKXNA K3428 |
| 14 | KXN K3766 |
| Semiconductors |  |
| IC1 | KB4445 |
| Q1 | 2N3866 or 2N4427 |
| LED1 | any LED |
| Miscellaneous |  |
| X1 | 13.5740 MHz |
| PCB, Q1 heatsink, joystick pots (x2), telescopic antenna, case to suit |  |
| RECEIVER |  |
| Resistors 1/4W, 5\% |  |
| R1 | 470k |
| R2,3,7 | 1 k 0 |
| R4 | 1k5 |
| R5 | 1k8 |


| R6 | 470R |
| :--- | :--- |
| R8 | 270k |
| R9,10 | 33k |
| R11 | 820k |
|  |  |
| Capacitors |  |
| C1 | 27p ceramic |
| C2 | 1n0 ceramic |
| C3,4,14 | 10n ceramic |
| C5,6,7,13,15 | 100n miniature ceramic |
| C8 | 27p ceramic |
| C9 | 4n7 ceramic |
| C10 | 22n polyester |
| C11 | 560p ceramic |
| C12 | 1u0 6V tantalum |
| C16 | 22u 6V tantalum |
|  |  |
| Inductors |  |
| L1 | 113KN 2K241 |
| L3 | 199CC A127 |
| L4 | 5MMC 0124 |
| L5 | PCS 4201 |
| Semiconductors |  |
| lC1 | KB4446 |
| Q1 | BF274 or similar |
| Miscellaneous |  |
| CF1 | SFE27MA |
| F1A | CFM2 455D |
| F1B | NTK LFC6 |
| X1 | 26.640 MHz 3rd order T type |
| 7way servo connector block, PCB, case to suit. |  |
|  |  |

WAVE METER
Potentiometers
PR1 $\quad 47 \mathrm{k}$ preset

| Capacitors |  |
| :--- | :--- |
| C1 | $22 p$ (if required) |
| C2 | 10n |
| C3 | 27 p trimmer |

Semiconductors
D1 any Germanium diode

Miscellaneous
M1
11
100-500 uA MKXNA K3428

The antenna is a vital part of the output tuned circuit. It is an electrically 'short' transmission antenna, which creates a number of problems for the RF designer, the major one being that it is an integral consideration of the output tuning and so any adjustments really need to be made with the antenna in its finally intended form.'

As soon as the first coil peaks, the current drawn by the transmitter should go up fairly dramatically as the output stage begins to warm up. Keep dabbing a finger on the PA stage to check that it does not get too hot. Using the absorption wavemeter placed by the antenna about halfway up and as far away as possible whilst still getting a reading (about 1 m should be féasible), peak the coils in the transmitter.

## The Receiver

If you have access to a working FM transmitter, use it for setting up the receiver (remember to use the correct crystal pair).

An audio amplifier with high input impedance can be used to monitor the detector of the KB4446 on pin 1, so you can

hear what is going on whilst tuning up. An oscilloscope at this point will display the detected control 'frame' It should be the same as that appearing at pin 12 of the KB4445 transmitter IC.

By starting with the transmitter and receiver in close proximity, you should have no trouble in getting a signal with which to commence the alignment process. By progressively reducing this input signal and peaking the coils, you will reach an optimum that corresponds to about 2 uV input for a correctly assembled unit. The setting of the crystal oscillator coil (at pin 10 of the KB4446) is critical and may need retrimming as the alignment proceeds to make certain the receiver and transmitter are correctly aligned co-channel. One of the few drawbacks of the FM system is the need for a more carefully matched $R x / T x$ frequency than with AM. Stick to one particular make of crystals so that the loading requirements are the same.

Fig. 9 This absorption wavemeter can be used to set up the RF output.


## BUYLINES



Fig. 7 Component overlay of the receiver board (double sided).
(Right) The receiver circuit board (double sided). It's a bit of a squeeze, but it does all fit crystal is extra.

Ambit International can supply a kit of parts for the transmitter unit for $£ 6.80$ + VAT. The case hardware and crystal are extra. A complete kit of parts for the receiver is also available for $\mathbf{£ 8 . 0 0}+$ VAT. The

Ambit International, 200 North Service Road, Brentwood, Essex.


ETI OCTOBER 1980

Connect a servo to one of the output pins. It should work in response to adjusting the transmitter control. At least one commercial servo is a must, as this can then be used as a reference for the 1.5 mS channel pulse, ie with the controls at centre, the trimming should be adjusted so that the servo is at mid travel. If this is not possible, then a further preset may be needed in series with the control stick pots to bring them in range. If nothing at all happens with the servo connected, then it may be necessary to fit an external pull-up resistor on the output of the KB4446 (10k) to the supply rail of the servo amplifier IC.

Repeat the check on each channel and carry the transmitter down the garden whilst someone monitors the receiver and servos to ensure that adequate range can be achieved.

## Finally

Under no circumstances should any home-made RC equipment be fixed into a model aircraft and flown. Apart from rules preventing flying in parks, the dangers of propelling a few pounds of balsa and metal about at 4060 MPH demand that a much more cautious approach be adopted. The home made RC can be checked and verified in cars, boats and similar ground-based systems first, or you can have it professionally 'certified'. A licence is required and some experience and training in flying is essential.

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# Look out for the November issue on sale October 3rd. 



SPACE INVADERS

In the past few months we've seen all manner of Space Invaders games - from enormous pub machines to programs on tape cassette for home computers. We've spent many a long hour researching the game in pubs and clubs from Land's End (Watford) to John $\mathrm{O}^{\prime}$ Groats. Next month we present the ETI Space Invaders game for you to build. $\square$ Plug the lead into the back of your telly and sit back with the box of tricks on your lap. Off you go - blasting aliens out of existence (with full sound effects, of course). World War III's OK, but there's nothing like the real thing - ETI Space Invaders - a computer game with a trick or two up its sleeve, as you'll find out next month.


Photos courtesy of Twentieth Century Fox.

## FREE PCB

As we finish printing each issue of ETI with our John Bull set, we're sticking a free, gratis, no-more-to-pay printed circuit board on the cover. It has a million and one uses - you can prop up a wobbly coffee table, make a shower for the budgie . . . OR build the five projects we've designed for your free PCB. There's an RIAA equalised preamp, a 2 W amplifier, a touch doorbell, a light switch and a metronome. $\square$ We give you the PCB; we give you the project designs . . . it couldn't be easier.

## RADIOACTIVITY

Know your alpha, beta, gammas? If it's all just radiation to you, you could learn a thing or two from A.S. Lipson's excursion into that fantastic, frazzling, phenomenon of modem physics - Radioactivity. What makes something radioactive? What exactly is radioactivity? All will be revealed next month.

## EVEN MORE PROJECTS

Not satisfied with bringing you our amazing Space Invaders game and FIVE projects for your free board, we've also got a doorbell with a difference (it plays tunes) and a straightforward, no frills Bench Amplifier for your test bench. It's all in ETI November.

## AND THAT'S NOT ALL

Data Sheet puts in an appearance with all you need to know about a family of monolithic switched capacitor filter chips and a speech generator chip (a very clever little block of plastic). $\square$ Talking of blocks of plastic, voltage regulators this time - we look at a very simple discrete component regulator design (for when you don't have the necessary chip to hand then and there). $\square$ We know now that the Space Shuttle launch has definitely been postponed until at least next March. Astrologue explains why.

Articles described here are in an advanced state of preparation. However, circumstances may dictate changes to the final contents.

# SPOT DESIGNS <br> <br> Six pages of Spot Designs - a bumper bundle of tried and tested circuits <br> <br> Six pages of Spot Designs - a bumper bundle of tried and tested circuits with the ETI stamp of approval. 

 with the ETI stamp of approval.}

## Overload Current Trip

Most power supplies incorporate some form of protection circuitry so that an excessive output current cannot flow in the event of an overload. However, these protection circuits are often designed merely to prevent the supply circuitry from sustaining damage, and in the event of an overload permit a level of current flow that is sufficient to damage the circuit being powered. This overload current trip can be used between the powered equipment and the power supply and will cut off the supply almost instantly if a preset threshold current is exceeded. The trip current can be varied from just a few to a few hundred milliamps. The unit will work with supply voltages of $5-40 \mathrm{~V}$.

When power is first applied to the circuit, power FET Q1 will be biased hard into conduction by bias resistor R1. Power is, therefore, supplied to the load via Q1, D1 and R2. There will be a voltage drop across these components, and to some extent this varies with changes in the supply current. At low output currents there is likely to be a voltage drop of something in the region of 0 V 7 , but this increases to a volt or so at high currents.

RV1 is adjusted so that at output currents below the required threshold level the proportion of the voltage dropped across Q1, D1 and R2 (and fed to Q2's base terminal) is not sufficient to switch on Q2. If the threshold current is exceeded, the voltage fed to Q2's base is then adequate to switch the device on and it diverts the bias current that formerly went to Q1's gate terminal. Q1 then switches off and cuts the supply to the load. $\mathbf{Q} 2$ remains switched on as it receives a strong base bias from the positive supply through the load, current limiting resistor R3 and RV1. Once tripped, the circuit thus latches in the "off" state. It can be returned to the "on" state by clearing the overload and then briefly operating SW1 so that the supply is momentarily disconnected from the unit. When the supply is restored it then starts at the "on" state once again. C1 ensures that the circuit does always initially assume the correct state and it also helps to prevent spurious triggering of the unit.

When using the unit it should be kept in mind that about $1 \mathbf{V}$ is lost through the device and the output voltage from the supply must be adjusted to compensate for this. The current trip inevitably causes some loss of regulation efficiency, but this is only marginal. If the unit is to have a trip current of about 100 mA or more, R2 can be reduced to about 1R8 in order to maintain the low voltage drop and marginal degradation of regulation efficiency.


## Crystal Set

The most simple form of radio for receiving broadcast stations is the crystal set, or more precisely, a modern equivalent using a semiconductor diode to provide detection. This simple set covers the normal medium wave broadcast band, has an output for a crystal earpiece and, in most areas, should give reception of Radios 1, 2 and

(b) action of D1

(c) recovered audio signal
(a) received signal


NOTE:
L1 IS DENCO MW5FR FERRITE AERIAL OR SIMILAR.

3 at reasonable volume (plus any local radio stations where these are in operation on the medium waveband). It requires no battery or other form of power source since energy derived from the received transmission is used to drive the earpiece. However, this does bring the disadvantage of needing an external longwire aerial to operate the set, as an ordinary ferrite aerial does not give sufficient pick up.

The tuned circuit is formed by L1 and CV1. This selects the desired transmission and rejects other stations. CV1 permits full coverage of the normal medium wave broadcast band to be achieved. In order to obtain good volume from the unit it is necessary to directly couple the aerial to the tuned circuit. For the same reason it is necessary to take the output to the detector direct from the tuned circuit. This inevitably gives the set rather poor selectivity, but it should still be adequate in this respect.

The form of modulation used on the medium wave band is AM (amplitude modulation). This consists of varying the strength of the RF signal in sympathy with the amplitude of the modulating audio signal. D1 half wave rectifies the RF signal to leave only the positive half cycles. R1 and C1 are used to smooth the RF half cycles, but their time constant is too short to produce a steady DC output. Instead the output rises and falls in sympathy with the mean RF signal level, so that the original audio signal is recovered at the output and fed to the earpiece.

The only adjustment the finished unit requires is to slide the aerial coil (L1) along the ferrite rod to find a position that permits full coverage of the medium wave band. The coil is then taped or glued in this position. The smaller winding of the ferrite aerial is not required and is either removed or just ignored. The aerial should preferably be an outdoor type about 10 m or so long, but a few metres of hook-up wire fixed around the walls of a room or in a loft should give reasonable results.


## D.M.M. To Stopclock <br> Convertor

This simple add-on circuit can be used with a DMM switched to the 1 mA range to give a stopclock having a range of $0-99 \mathrm{~S}$ (or $0-199 \mathrm{~S}$ for a $31 / 2$ digit instrument). It can also be used with an ordinary analogue multimeter or panel meter, giving a range of $0-100$ S, but the resolution will be lower than with a digital instrument.

The unit relies on the fact that a linear rise in voltage is produced across a capacitor if it is fed with a constant charge current. The

capacitor (C2) must be a high quality type. The use of a tantalum bead component is, therefore, recommended. C2 cannot simply be charged from the supply lines via a resistor, since the voltage across the resistor would drop as the voltage across C2 increases. This would give a decreasing charge current as C 2 charges exponentially and the required linear voltage slope would not be produced. C2 is, therefore, charged from a conventional constant current source which is based on Q1. D1, D2, and R1 form a simple shunt regulator circuit which bias the base of Q1 approximately 1 V 3 below the positive supply potential. There is a voltage drop of about 0V65 across the base emitter terminals of Q1, giving about 0V65 across emitter resistor R3. This gives an emitter current of roughly 3 uA and, as the collector and emitter currents of a high gain device (such as the BC179 used in the Q1 position) are virtually identical, a constant charge current of about 3 uA is fed to C2 when SW1 is operated. This low charge current together with the fairly high value of $\mathbf{C} 2$ produces a suitably long time constant.

It is essential that the voltmeter circuit takes no significant current from C2 as this would affect accuracy and would result in a decaying reading at the end of a timing run. Operational amplifier IC1 is, therefore, used as a unity gain buffer stage which gives an in put impedance of about 1.5 million megohms and ensures that there is no significant loading on C2. PR1 enables the sensitivity of the voltmeter circuit to be adjusted to the correct level. In practice, SW1 is depressed for (say) $90 \mathbf{S}$ and then PR1 is adjusted for the appropriate reading on the DMM.
$\mathbf{S W 2}$ is a reset switch and this discharges C2 (via current limiting resistor $\mathbf{R 4}$ ) if it is briefly operated. SW3 is an ordinary on/off switch. The current consumption of the circuit is only about 4.5 mA .


## Quiz Monitor

This circuit is useful when playing "snap" or TV quizzes where the first person to have an opportunity of answering the question is the first to operate their push button switch. Operating it causes an indicator light to switch on and prevents the opponent's switch and indicator light from working. Thus, there is no doubt as to which push button switch was operated first.

The circuit is based on a CMOS 4001 quad two input NOR gate, but all of the gates have their two inputs connected together so that they, in fact, operate as simple inverters. The circuit has two identical sections, one for each player, each using two of the gates.

If we consider gates 1 and 2, at switch on C2 is in a discharged state and, therefore, takes the input of gate 1 low. This causes the output of gate 1 to go high, taking the input of gate 2 to the same state due to the coupling through R1. The output of gate 2 then goes low and feedback through R2 holds the input of gate 1 in its original low state, thus latching the circuit in this condition. LED 1 is driven from the output of gate 2 via current limiting resistor R3. At first it
will obviously be switched off. So will LED 2 which is the indicator light for the other player. It is driven from an identical arrangement. If PB1 is activated, the input of gate $\mathbf{2}$ is taken low, since it will be taken to the low output of gate 4 . This sends the output of gate 2 high, the input of gate 1 high (due to the feedback through R2) and the output of gate 1 low. The circuit will hold itself in this state even if PB1 is released. Operating PB2 will have no effect now, since this will merely connect the high output of gate 2 to the high input of gate 4, producing no changes in logic state. Thus the required blocking is obtained. Of course, if PB2 was operated first, LED2 would switch on and PB1/LED1 would be disabled, with the basic circuit action being the same as described above. The operating speed of the circuit is extremely fast and even with a very small gap between the two switches being operated, the unit is capable of determining which was operated first and there is no danger of both LEDs switching on.

The circuit is reset by briefly operating PB3 so that power is removed from the circuit and it starts once again from the beginning when PB3 is released. No onloff switch is required as the unit has a negligible quiescent current consumption.

## Simple Preamplifier

This preamplifier has two inputs; one for a magnetic cartridge and the other is an "Aux" input for a tuner, tape deck, etc. Although the circuit is very simple, it uses an IC which is specifically designed for this application and provides low levels of noise and distortion. The unit is suitable for stereo operation and both the required amplifiers are contained within a single LM382 IC.

The circuit diagram is for one channel only, but apart from the IC pin connections the other channel is identical. The numbers in brackets show the pin connections for the other channel. The supply connections of IC1 are common to both channels.

The LM382 has an internal biasing circuit which sets the quiescent output voltage at approximately 6 V and no discrete biasing components are required. C6 provides DC blocking at the output. When switched to the "Mag" mode, external feedback components are required in order to shape the frequency response characteristic of the amplifier in the required way. Bass cut and treble boost are applied to the signals transferred onto records so as to prevent excessive low frequency groove modulations and give an
improved signal to noise ratio. The preamplilfier must give corresponding bass boost and treble cut in order to give a flat overall frequency response to the system. C2, C3 and R1 are the discrete feedback components and the LM382 itself contains some feedback resistors. C4 and C5 provide DC blocking for two shunt resistors in the feedback network.

When switched to the "Aux" mode, most of the feedback components are not required and are switched out of circuit by SW1a and SW1c. C2 is left in circuit, but is superfluous. In this mode the circuit has a voltage gain of only about four and is really just operating as a buffer stage. SW1a connects the input of the amplifier to the appropriate input socket and C1 provides DC blocking at the input. Of course the input wiring must all be screened to prevent stray pick-up of mains hum, etc.

The current consumption of the circuit is about 12.5 mA . Due to the high supply ripple rejection of the LM382, it is not necessary to have a highly smoothed and decoupled supply.


(a)

## Combination Lock

A ost combination locks are based on the simple arrangement Mishown in (a). This merely consists of three ten way rotary switches wired in such a way that they will connect power to the relay or solenoid if the correct combination is set on them (6-4.5 in this case). This basic circuit is not often used in practice since it does not take very long to quickly adjust the switches through all the $\mathbf{1 , 0 0 0}$ possible combinations ( $\mathbf{0 - 0 - 0}$ to $\mathbf{9 - 9 - 9}$ inclusive) if it is done in a logical manner.

One of the simplest and best methods of overcoming this problem is simply to build a delay circuit into the unit so that power is not supplied to the solenoid or relay until the correct combination has been present for a few seconds. Quickly running through all the possible combinations is then ineffective at "cracking" the unit, as the delay circuit will prevent the unit from responding when the correct combination is briefly present. Anyone trying to "crack" the unit is very unlikely to succeed unless they know of the delay circuit and are prepared to devote a good deal of time to finding the correct combination.

Circuit (b) has an additional time delay circuit which is based on VMOS device Q1. When the correct combination is set on SW1 to SW3 and power is supplied to the circuit, C1 will be uncharged, giving zero gate bias to Q1. Q1 is, therefore, switched off and no significant current is supplied to the relay or solenoid which forms its drain load. C1 slowly charges via R1 and after about 4 S the charge voltage on C1 will be large enough to bias Q1 into conduction and switch on the relay or solenoid.

R2 discharges C1 when the unit is reset, so that it is quickly ready to operate properly once again. $R 2$ limits the maximum gate voltage of Q1 to only about half the supply voltage, but this is more than adequate to bias the device hard into conduction and is of no practical consequence. D1 suppresses the high back EMF produced across the relay or solenoid when it switches off and prevents possible damage to Q1.

(b)

## Reverberation Unit

This unit simulates the long reverberation time of a large hall (usually around 2 S or so) and can be employed as a musical effects unit or to improve certain types of home-recording. Reverberation is caused by sounds being reflected around the interior of a room and in the case of a large hall the sounds are usually reflected many times before losing sufficient energy to render them inaudible. This, coupled with the fairly long distances covered by the sound waves between reflections, gives the long reverberation time and reverberant sound of a large hall.

There are several ways of simulating reverberation, but the simplest and most commonly used is probably the springline based system. A springline consists of two transducers linked by one or two long springs. If a signal is fed into one transducer it produces a corresponding audio signal which is transmitted down the spring to the second transducer. Here it is reconverted into an electrical signal again. However, the sound signal travels down the spring relatively slowly, and the signal is reflected backwards and forwards
along the spring many times before it decays to an insignificant level. Thus, the output from the second transducer is a good simulation of natural reverberation.

In this circuit the input signal is fed to the low impedance input transducer of a short springline via an emitter follower which gives a reasonably high input impedance of about 10k or so. This uses Q1 in a conventional configuration. The output of the springline unit is fed to one input of a mixer circuit. This is based on IC1 and again uses a conventional and well known arrangement. There are substantial losses through the springline and so the mixer is designed to boost the output of the springline by over 46 dB (200 times). The other input of the mixer is fed with the input signal, but the high value of R5 gives only about unity voltage gain at this input, so that the main signal does not overwhelm the reverberation signal.

RV1 enables the amount of reverberation signal mixed into the main signal to be controlled. It can be reduced right down to zero by fully backing off RV1. SW2 can be used to cut out the main signal so that only the reverberation signal appears at the output, if desired. The only other control is on/off switch SW1. The current consumption of the unit is approximately 10 mA .


## Peak Level Indicator

D eak audio level indicators can be used in tape recorders, amplifiers, mixers, and other radio equipment to provide a visual overload warning, and unlike slower responding VU meters, they produce a proper response to fast transients. This circuit is based on the inexpensive 723 C device which, although primarily intended for use as a voltage regulator, can be adapted to work well in many other applications.

The 723 C has a highly stable 7 V (nominal) reference voltage available at pin 6 . This is coupled to the inverting input of an opera tional amplifier (which is also part of the 723 C device) via an at tenuator, R4,5. This gives a stable reference potential of a little over 2 V at the inverting input. The input signal is coupled by way of sensitivity control RV1 to a common emitter amplifier based on Q1 and fed to the non-inverting input of the operational amplifier by C2 and R6. Under quiescent conditions or with a negative going signal at Q1 collector, the non-inverting input will be at a lower potential than the inverting one, and the output of the amplifier will be low. If a
positive going signal reaches a high enough amplitude, though, the non-inverting input will reach a higher potential than the inverting one causing the output to go high. D1 is then switched on with a current that is determined by the output of the amplifier and which is largely independent of the supply voltage. Discrete resistor $\mathbf{R 8}$ actually sets the output current. The specified value gives a nominal 20 mA LED current. R7 provides positive feedback which ensures that D1 is either fully on or off. It also tends to hold D1 in the on state for slightly longer than would otherwise be the case, thus giving a clearer indication of a brief overload.

The unit can be adjusted to respond to input levels down to about 100 mV RMS, which should be more than adequate for all normal requirements. RV1 is adjusted for the lowest sensitivity that causes D1 to come on with an input signal level equal to the lowest overload level. Quiescent current consumption is only about 4 mA .


## I.F. Alignment Oscillator

This simple piece of test equipment can be very helpful when aligning or realigning an AM superhet receiver. It provides an output at $455 \mathbf{~ k H z}$, which can be modulated by an audio tone if the set is being adjusted for maximum AF output. The modulation can be switched off if the IF transformers are to be adjusted for maximum AGC voltage.

The circuit consists of two oscillators, Q1 and Q2 being used in the one which generates the 455 kHz signal and Q3 in the one which provides the modulation signal. Q1,2 are connected in a straightforward two stage, direct coupled, common emitter configuration. However, neither of the emitter resistors are bypassed in this case as only a low voltage gain is required. The input and output are in phase and positive feedback between the two is provided by ceramic filter CF1 (available from Ambit Interna-
tional). A significant amount of feedback is only provided at the 455 kHz operating frequency of the filter and so the circuit oscillates at this frequency.

A ceramic filter gives good frequency stability, requires no adjustment in order to produce the correct output frequency and is cheaper than using a crystal. C2 provides DC blocking at the output, although it should normally only be necessary to connect the "hot" output to the receiver, no chassis connection being necessary.

A straightforward phase shift oscillator is used to provide the modulation signal and the specified C-R values give an operating frequency of about 500 Hz . C3 and R6 couple this signal to the base of Q2 where it amplitude modulates the 455 kHz signal. SW1 can be used to cut the supply to Q3 and thus remove the modulation. Current consumption is about 2.5 mA with the modulation switched on and approximately 1.7 mA switched off.



## VMOS 10 Watt Amplifier.

$t$ first sight this circuit may seem to be a straight foward Class B design having an emitter follower, complementary output pair and Darlington Pair common emitter driver stage. However, the output devices are, in fact, complementary VMOS transistors used B0512/522

in the source follower mode the FET equivalent of the emitter follower). In most other respects the design is quite conventional.

R1 and R2 are used to bias the unit to give the optimum quiescent output potential and they provide overall negative feedback, which improves the quality of reproduction. D1 and C4 are bootstrapping components, enabling the gate drive voltage to Q3 to go above the positive supply potential, giving improved efficiency to the circuit. R3 is the main collector load for Q2 and PR1 is used to give a standing bias on the output transistors that gives a quiescent current consumption of about 25 mA . The thermal compensation circuitry normally used is totally unnecessary in this circuit, since VMOS devices do not suffer from thermal runaway. In fact the quiescent bias current will drop slightly as the output devices heat up, but not sufficiently to give rise to significant crossover distortion.

C2 and C5 provide DC blocking at the input and output respectively, while C1 is a supply decoupling component. C3 gives a degree of high frequency attenuation and aids the stability of the circuit.

Athough the current in the driver stage, only about 1 mA , may seem to be totally inadequate, it is in fact more than sufficient since .the VMOS devices have extremely high input impedances and consume no significant input current. This is one of their main advantages over bipolar devices. One disadvantage in this particular application is lower efficiency due to the higher threshold voltages and on resistance of VMOS transistors in comparison to bipolar devices. However, the circuit will give an output of 10 W RMS using a supply voltage of about 33 V or so (with a current drain of up to about 600 mA ). An input of about 500 mV RMS is needed for maximun output.
Note: The output devices do not have internal zener protection diodes and the appropriate handling precautions should be taken. These devices are available from I.W. Rimmer, 367 Green Lanes, Harringay, London, N4 1DY.

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# flash TRIGGER This versatile unit fits in your pocket - ready for use in a flash. 

Flash triggers have been with us for a few years now. This design offers all the usual features plus pocketability. Only a couple of cheap chips are used with a caseful (check the photos) of other components. Using the specified component values, the unit may be employed either as a direct slave or may introduce a delay variable between 10 ms and 200 mS . Other delay times may be achieved by a single component change.

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Our PCB design will enable you to build the unit into a compact case. A preset component was used for PR1, though a standard potentiometer can be substituted if you have room and require adjustable sensitivity. If you do use our PCB then construction will be straightforward. Just follow our drawings and PCB overlay. As usual, insert the low-profile components first taking care to orient the semiconductors correctly. If you do not have a BC184L, almost any other small NPN silicon transistor can be substituted. However, note the TO92A pin configuration which differs from that of many popular transistor types. We included a power 'on' LED indicator in our design next to the input socket. A word of warning: remember that the trigger leads of many flash guns may have a potential of up to 200 V across them. This is usually low current but may give the clumsy constructor a tingle. This versatile unit should find a place in every photographer's grab-bag, so if you are going to delay, do it ourway!


Fig. 2 Component Overlay.

## BUYLINES

All the electronic components should be readily available from your usual supplier or see the adverts in this issue. The Vero plastic box we used is their stock number 202-21027E.

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# Hobby Electronics 

## Next Month

## Kitchen Timer

This handy little gadget will soon take pride-of-place on the kitchen shelves. It'll accurately indicate periods of up to six and a half minutes in thirty second steps. All the components are easy to obtain and it shouldn't take more than a couple of hours to build.

## Freezer Alarm

Still in the kitchen, we've cooked up another winner for you with this little freezer alarm circuit. Should the temperature rise above a pre-determined level then the alarm will sound. Anyone who has ever seen a freezer full of unfrozen food will know how valuable this little project could be!

## Light Dimmer

Here's one for those afraid of bright lights. This all new dimmer circuit will fit into the standard light switch socket. It'll let you control your lighting from a harsh glare to a warm seductive glow, just right for those long winter evenings in front of the telly. It might even save a few bob on the electricity bill too!

## ON SALE SEPTEMBER 12th

## Doorbell

Just in case you've fallen asleep, safe in the knowledge your freezer's OK, the lights are low (courtesy the HE Light Dimmer), the meal was perfect (thanks to the HE Kitchen Timer), you'll be glad to know that the HE Nobell Doorbell will wake you up. This novel little circuit faithfully re-creates the sound of a mechanical doorknocker. No prizes for guessing why we called it the Nobell

## Temperature Controlled Soldering Iron

If we've tempted you into building any of these projects then you should know about our Temperature Controlled Soldering Iron project next month. You'll be able to build all of the projects. without worrying about burnt out bits anymore.

## Home Electronics

To round it all off we will be taking a look at some of the benefits electronics has brought to the home. The homely Tina Boylan looks at some of the gadgets on sale today and some of the labour saving devices we can expect in the next few years.

The items mentioned here are those planned but unforeseen circumstances may affect the actual contents.



# SPECIAL RELATIVITY 

# Einstein ranks as one of the giants of physics. A.S. Lipson looks behind the equations and tells the story of the special theory of relativity. 

In 1905, Einstein published three papers. It was the third of these which was concerned with special relativity. In this paper - "On the Electrodynamics of Moving Bodies" - he set out by making two apparently innocent assumptions; that the velocity of light as measured by some inertial observer does not depend on the velocity with which this observer is moving, but will only be affected if the observer is accelerating or decelerating (an inertial observer is one who travels with constant velocity, without accelerations or decelerations) and that the laws of physics as measured by the observer are also independent of his velocity. From these assumptions, Einstein produced - using the most beautifully simple arguments - conclusions that rocked common sense and upset people's basic ideas about space and time.

If the laws of physics, all laws of physics, are the same, no matter what the velocity of the observer measuring those laws is, then there is no way in which that observer can tell with what velocity he is moving, or even if he is moving at all, just by performing an experiment in his own reference system, which is moving along with him.

## Relative Motion

If, for instance, you are in a smoothly-running train, with all the windows covered over, and without noises from outside, such as the sounds of the wheels on the tracks, then you cannot tell by any means whether the train is in uniform motion, or standing still. However, should one of the windows be uncovered, so that you can see outside, you can then tell whether or not the train is moving by whether or not the buildings outside appear to be passing you at high speed.

Even so, information from the outside world can be very difficult to interpret sometimes. If your train is in a station, with another train on the line just next to it, then when your train pulls out, it can be very difficult to decide whether the motion you observe is due to the other train travelling slowly in one direction, or your own train travelling slowly the other way.

## Ether It's There Or It Isn't

Since Newton, there had been a running debate among physicists as to whether light consisted of a wave or a beam of particles. These days, it is believed that it actually consists of a sort of cross between the two, which is virtually impossible to visualise, but is extremely useful for explaining various phenomena. However, by the second half of the nineteenth century, everyone was pretty certain that it was a wave. Maxwell had predicted the theoretical speed of electromagnetic waves and it had turned out to be pretty nearly the same as the experimentally measured speed of light and that was that light was probably an electromagnetic wave. The one problem was that all other known waves travelled through a medium of some kind; sound waves through air, water waves


Fig. 1 To Bruce it appears that Barry's timescale is 'running slow. To Barry it appears that it is Bruce's timescale that is slow.
(obviously) through water, and so on. Light seemed to travel through a vacuum - for instance, from the Sun to the Earth. It didn't seem to need a medium. So they invented one; the ether

The ether supposedly filled all space, acting as a medium for light, but not interacting with matter. (So, for instance, it didn't slow down the Earth in its orbit around the Sun.) The fact that there was no experimental evidence for this ether did nothing to change physicists' minds.

Now we can see why Einstein's ideas were so radical and unpalatable to scientists of the time. He, a mere patent clerk at the time, was daring to challenge the scientific principles laid down by Isaac Newton, acknowledged as the greatest scientist of all time. What Einstein was saying was that there was no need for an 'absolute' reference system - or even for the concept of the 'ether'. In order to make these statements logically consistent, though, he had also to abolish the concept of absolute time

## Time

Time, according to the special theory of relativity, is dependent on velocity. This is best explained by giving an example. Consider two inertial observers, moving rapidly towards each other. For the sake of argument we can call them Bruce and Barry. Let us imagine that Bruce and Barry are approaching each other with a velocity $v$, and that each of them has a very accurate clock, which they carry along with them. Now according to relativity, if Bruce looks at Barry's clock and compares it with his own, it will appear to him that Barry's clock is running fractionally slower. Not only that; Barry himself will also be 'running slower' - his breathing, pulse rate, and so on will all have slowed down by just the same amount. In fact, it will appear to Bruce that Barry's time scale has slowed down! Well, if this is so, then it follows that it appears to Barry that Bruce's clock will be running fast. Or does it? Unfortunately not. If Barry looks at Bruce's clock, he will observe the same effect - that Bruce's clock is running slower; in fact, that Bruce himself will be running slower. Each of the two observers appears to the other to have a slower timescale.

## And That's Not All

Time wasn't the only thing that took a bashing from Einstein, though; he had something to say about space, as well. If you are travelling at high speeds, the way you perceive objects will also change. Originally, it was thought that relativity theory stated that objects appeared shorter at high speeds. In fact, this is not quite accurate. If objects moving at high speeds are looked at, then they actually appear rotated, rather than contracted in length. If the objects are measured, however, allowing for the travel time of light, then they do appear to be contracted. This decrease in length at high speeds is known as the 'Lorentz Contraction', after a scientist who suggested it (although for different reasons than those of Einstein) shortly before Einstein's paper, in 1895.

We can calculate the apparent length of an object and draw out a table of it against velocity. If $\mathrm{I}_{0}$ is the length of the object measured at rest, and $l$ is the length measured at some velocity $v$, then $I=I_{0} \sqrt{1-v^{2} / c^{2}}$, where $c$ is the velocity of light. In the table below, $v$ is expressed as a fraction of $c$, and $I$ as a fraction of $I_{0}$

| Velocity ${ }^{\text {d }}$ ) | $1 / 10$ | Velocity(v) | $1 / /_{0}$ |
| :---: | :---: | :---: | :---: |
| 0 | 1.0 | 0.9c | 0.4359 |
| 0.4c | 0.9165 | 0.95c | . 0.3122 |
| 0.8c | 0.6 | 0.99C | . 0.1411 |

You can see that, as $v$ gets close to $c$, the apparent length of an object drops dramatically, although at low speeds, less than 0.4 c , the effect is fairly small. In fact, this is why we don't notice relativistic effects in normal life and why it took a mind like Einstein's to point them out. Even the fastest speeds that we normally come across are such small fractions of the velocity of light that the relativistic effects are too small to be measured.


Fig. 2 Objects appear to grow shorter at high speeds.

## Time Dilation

The same arguments apply to the peculiar 'time dilation' effects we looked at earlier. At the sorts of velocities we are used to, the effects are too small to notice. Timescales, in fact, are related by exactly the same formulae as are lengths. Going back to Bruce and Barry, if $t$ is the time Barry measures by his own clock, then $t=t \sqrt{1-v^{2} / c^{2}}$

At this stage, it might appear, looking at the equations, as though, if we could reach the velocity of light; that is, if $v$ was equal to $c$, then time would appear to stop altogether and objects would appear to be so shortened as to be totally flat. In fact, this does not happen, and for a simple reason - the speed of light cannot be reached.

## Weight A Minute

Physics is concerned mainly with the study of four quantities and the interactions between them. These four quantities are distance, time, electric charge and mass. So far, we've seen that distance and time are both affected by high velocities. What about the other two? Well, electric charge doesn't seem to be changed, however fast you move it, but mass, on the other hand, can be very significantly changed.

The change that occurs is very similar to those with distance and time. If we measure the mass of something when it is at rest with respect to us as $\mathrm{m}_{0}$ - the'rest mass', as it is called - then when it is travelling relative to us with a velocity $v$, we will find its mass to be given by $m=m_{0} / \sqrt{1-v^{2} / c^{2}}$ and, hardly surprisingly, we see that this equation is strikingly similar to those giving time dilation and Lorentz contractions. The only difference being that $m_{0}$ is divided by $\sqrt{1-v^{2} / c^{2}}$ whereas $I_{0}$ and $t$ were multiplied by it.

The acceleration (that is, the rate of increase of velocity) of an object is given by the force applied to it, divided by its mass. Hence, as velocity increases, so does mass, and for a set applied force, acceleration becomes smaller. As v gets close to $c$, mass gets very close to infinity and the force needed to accelerate the body also gets higher and higher. To accelerate a body to the velocity of light would require an infinite force applied over a finite time, and hence would take infinite energy. Such an acceleration, then, is not possible. Although we can, in theory, get as close as we like to the velocity of light, we can never actually reach it.


Fig. 3 Mass increases at high velocities.

## So Where Does It All Come From?

All right. So an object's mass increases at it travels faster (Fig.3). Where does all this mass come from, though? Well, it originates in the energy that we put into the object while accelerating it and this is where what is possibly the best known equation in physics comes in:

$$
\mathrm{E}=\mathrm{mc}^{2}
$$

Energy equals mass times the square of the velocity of light. The extra mass actually is all the energy that was put into the acceleration. Because of this, when we slow the object down again, it loses all the excess mass, because in decelerating it, we extract all the energy again.

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## In the concluding part of the ETI Vocoder, Richard Becker deals with construction and setting up

Start construction with the power supply PCB and bolt this onto the rear panel with mica washers between the panel and transistors, which are on the underside of the board. Silicone grease will keep the washers in place during fitting. Wire up and check all is well when operating into 1 k 0 resistors as temporary loads.

Build up the rest of the boards. Use insulation on any links which touch the leads of components. On the LED PPM boards, fit the connector pins for the connector to the component side of the board for the excitation meter and the noncomponent side for the speech meter. Where there are jack sockets, solder short lengths of bare wire to the boards and fit both board and socket to the front panel before soldering the wires to the sockets, which then become firmly attached parts of the board assemblies. On the internal excitation board of the three controls with mounting frames fit to the underside of the board. The other four controls fit on the top side of the board. To get the correct spacing between the top and bottom controls the top ones are soldered to pins such that the tags just touch the top of the board.

## Split Supply

The analysis/synthesis board is split in two halves to simplify manufacture. When the two halves are completed, fit the boards to the panel by means of the controls. Fit wire links between the boards and solder the two halves together by use of a bared length of wire along the joint. Fit the spacers to the back of the board and drop it into the chassis so that it can sit

| PARTS LIST Slew Rate Control |  |
| :---: | :---: |
| Resistors all 2\% metal oxide |  |
| R1, 2 | 15k |
| R3, 6, 8 | 2k2 |
| R4, 5, 7 | 10k |
| R9, 10 | 47R |
| R11 | 220R |
| R12 | 470R |
| R13 | 1k0 |
| Potentiometer RV1 | 1M0 log with mounting frame |
| Capacitors |  |
| C1, 5 | 10n ceramic |
| C2, | 33 n polyester |
| C3 | 100p ceramic |
| C4 | 560p ceramic |
| C6, 7 | 22u 25 V |
| Semiconductors |  |
| IC1 | 556 |
| Q1 | 2N3904 |
| Q2 | 2N3906 |
| D1 | 1N4148 |
| LED1 | TIL220 |
| Miscellaneous <br> Footswitch, Footswitch box, stereo jack plug and socket, 5 way connector, IC socket |  |




Fig. 2 Component overlay of the slew rate control board.
on its back edge whilst wiring up and setting up. Link together with a stretched length of wire on the back of the board all the excitation input pins and also the other inputs and outputs (a total of seven rails).

Make up the wiring loom and connect up all the boards.

## HOW IT WORKS - Slew Rate Control

This is a pulse generator of variable mark/space ratio. IC1 is a $\mathbf{5 5 6}$ which is a dual timer. Pins $1-6$ form a $1 \mathrm{kHz} 2: 1$ markdspace ratio pulse generator, its frequency being determined by R1, R2, C2. Its output is used to trigger via C3 and a monostable built round pins 8-13. The width of the output pulse is determined by C4, resistors R3, RV1. The output is buffered by Q1. Q2 is the output driver, switching from + 11 V to -11 V . The freeze switch forces the output to -11 V thereby furning off all the FETs of the analysis/synthesis section. To isolate the heavy switching surges on the power rails from the rest of the machine the rails are decoupled by $\mathrm{R} 9,10,11$ and $\mathbf{C 6}, 7$.


## HOW IT WORKS - Input Amplifier

The preamplifier uses an RC4558, which is a low noise version of the 1458, for IC1. The overall gain of the stage is dependent on which input is used, being unity for SK2 and for SK1 it is 500 (speech) or 50 (excitation). The gain is distributed between IC1a and IC1b. If SK1 is used and SK2 is not, then amplified signal from IC1a is connected to RV1 via the switched contact SK2. Also R4 is connected to ground, through the other switched contact of SK2, giving IC1b a voltage gain of ten. If SK2 is used then IC1a is isolated and R4 is disconnected from ground making IC1b now have unity gain.

IC2 is a rather complex tone control stage giving, with a single control knob, treble boost with bass cut or bass boost with treble cut. R7, C5 and R9, C6 form high pass filters whilst R6, C3 and R11, C7 form low pass filters. When the wiper is clockwise the input of IC2 is connected to the input of the stage via C5, R7 whilst RV2 is in series with the feedback thereby boosting the gain at high frequencies. At the same time, bass from feedback path R11, C7, R10 is dominant over bass from the input, which has to pass through RV2. Therefore, the bass is cut. The opposite occurs when the wiper is anticlockwise.


Input amplifier board.

## Setting Up

Check the power lines are still correct when all the boards are connected, set all presets to the centre of their travel and apply a sinusoidal signal to the speech line input. (If no oscillator is available use the cheap little circuit shown.) Set the level to where the sixth LED up just flickers, corresponding to 400 mV . Measure the $A C$ voltage on pin 6 of IC1 channel 2. Adjust the frequency until the voltage reaches a peak, turn PR1 fully clockwise and turn it back slowly until 4 V RMS is measured at the resonant peak of the filter. Repeat this for the other analysis filters.

Connect a 56 R resistor between the bias rail and +12 V , turn the slewing rate control fully clockwise, check the pulse generator is operating by listening for a whistle when the input

## PARTS LIST - Input Amplifier


jack of an amplifier is placed near the slew rate control board, switch off the unvoiced detector, plug the oscillator into the external excitation HIGH input and set up channel 2 excitation filter as for the analysis filters (except that now the point to measure is pin 1 of IC7 and the potentiometer to adjust is PR5). With RV1 fully clockwise adjust PR2 so that 4 V RMS is also at the output of the OTA buffer (IC6 pin 8). Repeat this for the other filters including channels 1,14 where there is only PR2 to adjust.

Plug the vocoder into an amplifier, turn up all channel volume controls and the vocoder output control. Turn down the speech and the excitation inputs. Turn up one of the oscillators and adjust RV5 or RV6, as appropriate, so that the signal is heard to just disappear when the width control is anticlockwise. Repeat for the other oscillator.


Fig. 4 Component overlay of the input amplifier board.

Fig. 5 (below) Component overlay of the output amplifier board.


## PARTS LIST • Output Amplifier

| Resistors 1/4W 5\% |  |
| :---: | :---: |
| R1, 2, 4, 5, 6 | 22k |
| R3 | 33k |
| Potentiometers |  |
| RV1, 2, 3 | 10k log with mounting frames |
| Capacitors $\text { C1, } 2$ | 1u016V tantalum |
| Semiconductors IC1 | 1458 |
| IC2 | 741 |
| Miscellaneous Jack socket, 7 way connector, connector pins, IC sockets. |  |



Output amplifier board.

Fig. 7 Circuit diagram of the LED PPM display.



Fig. 8 Component overlay of the LED PPM display board.

## HOW IT WORKS - LED PPM Display

IC1 is a full wave rectifier with peak detector charging C2 to the peak voltage of the input signal. IC1 is a logarithmic display driver, the sensitivity of which is determined by R7, 8. The LEDs are at 3 dB spacing. The red LEDs illuminate when the filters overload. The LEDs have their own power supply.

PARTS LIST • LED PPM Display

| Resistors 1/4W 5\% |  |
| :---: | :---: |
| R1, 2, 3 | 100k |
| R4, 5 | 200k |
| R6 | 1k |
| R7 | 680R |
| R8 | 150R |
| Capacitors |  |
| C1 | 220n polyester |
| C2 | 470n polyester |
| C3 | 1u016V tantalum |
| Semiconductors |  |
| IC1 | TL082 or LF353 |
| IC2 | LM3915 |
| D1-4 | IN4148 |
| LED 1-7 | TIL211 (green) |
| LED 8-10 | TIL209(red) |
| Miscellaneous <br> 5 way connector, connector pins, IC sockets. |  |

## Noise Abatement

Remove the 56R resistor, turn down all the channel volume controls and the oscillators. Turn up the noise level to maximum, turn up channel 1 and adjust PR3 to the point just before the noise disappears. Repeat this for the other channels.

Disconnect the excitation and speech inputs from the analysis/synthesis board and temporarily connect the excitation to the speech input of the board so that noise can be applied to the analysis section. Turn up channel 1 and the noise control. Adjust PR4 for minimum breakthrough of the control
signal which will be heard as a low rumble. Repeat this for the other channels and then re-connect the inputs.

Turn on the voiced/unvoiced detector, apply a high frequency signal to the speech input and the V/UV LED will light up. Turn up all the channel volume controls and the noise control and noise will be heard. Adjust PR2 to halfway between the points where the noise is heard to start limiting. Turn down the noise control and adjust PR1 to the point where noise is just heard to disappear. Turn up the noise again and alter the frequency of the test oscillator. Adjust PR3 to where the noise level drops by about 6 dB , as indicated on the LED PPM, when the V/UVLED is illuminated.

## HOW IT WÖRKS - Power Supply

Raw positive DC is regulated by IC1. To reduce heat dissipation the current is shared with Q1 roughly in the proportion of R2 to R1. The negative supply is similar. The LEDs of the PPM meters have their own supply. This can be very raw indeed and smoothing capacitor C5 is very small. IC3 is used simply to limit the voltage and not regulate it.

Fig. 9 Circuit diagram of the power supply unit.


The power supply unit mounted on the rear panel.


Fig. 10 The job of wiring all the boards together is best tackled methodically and double checked by an impartial pair of eyeballs.

## PARTS LIST - Power Supply

## BUYLINES

Powertran Electronics, Portway Industrial Estate, Andover, Hampshire, are supplying a complete kit of parts for this project at E195.00 plus $\mathbf{1 5 \%}$ VAT. Delivery by Securicor is $\mathbf{£ 2 . 5 0}$ extra. Everything is included in the kit down to the last nut and bolt. They even give you a 'Freeze' footswitch and a test oscillator for setting it up!

| Resistors $1 / 2 \mathrm{~W}$ metal glaze |  |
| :---: | :---: |
| R1, 4 | 1R0 |
| R2, 3 | 3R3 |
| Capacitors |  |
| C1, 2 | 2200 u 25 V electrolytic |
| C3, 4, 6 | 1 uO tantalum |
| C5 | 22u 25V electrolytic |
| Semiconductors |  |
| D18 | 1 N4002 |
| IC1 | 7812 |
| IC2 | 7912 |
| IC3 | 7805 |
| Q1 | IIP 30A |
| Q2 | TIP 29A |
| Miscellaneous <br> Transformer $15-0.15 \mathrm{~V}$ at $1 \mathrm{~A}, 7 \mathrm{~V} 65$ at $0.4 \mathrm{~A}, 5$ way connector, connec ${ }^{\text {s }}$ tor pins, finned heat sinks, mica washers. |  |



Fig. 12 Component overlay of the power supply.

Fig. 11 Circuit diagram of the 100 Hz to $\mathbf{7 k H z}$ test oscillator.

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| 0-15-27, 0-15-27!1A:1A |  |  | 204 | 6.05 | 1.00 | Ampe | No. |  | Pap |
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# AUDIOPHIIE 

## Ron Harris returns to his roots - well almost - for a look at a very promising new Thorens TD 160 S turntable and has a severe shock in store for headphone owners!

Ashes to ashes. Dust to dust. Thorens to Thorens. Having launched off down the path to hi-fi many years ago in the august company of a TD 150 II turntable, it brought a whiff or two of nostalgia drifting back to lay hands on this new TD160S.

Thorens have received an indifferent press of late, mainly because some of their decks have failed to match the very high standards set in earlier days, by the 150 and 125 machines.

The standard 160 has been enthusiastically received, however, even by the usually isolationist 'cult' press. There was, though, a lot that could still be done to improve things and after some years of watching other people make money doing them, Thorens have decided enough is enough - and the TD160S is born.

## Vive La Difference

Compared to a standard 160, the 'special' is more solidiy constructed all around, has a massively heavy chipboard base, a better bearing system, thoroughly damped sub-chassis and improved suspension. The arm-board is also much heavier, but we'll come to that again later.

The standard Thorens mat has been dumped overboard and a much more sensible specimen is fitted in its place. The emphasis of the work has been upon suppression of resonance and isolation from feedback. I think the changes made show a clear enough improvement in the final sound to be immediately obvious in an A - B test, even in a crowded dealer's. Taking this into account, therefore, one is forced to consider the $160 S$ in a higher league entirely - so it was with the greatest of expectations that I approached the packing case

## Set Up By The Setting Up

The deck employs the (by now) well known Thorens three point spring suspension. This method of 'floating' a sub chassis away from the base on springs has been employed by Thorens for many years, long before either the Linn or the Ariston arose to dazzle the eyes of belt-driven enthusiasts. The intent is to isolate the turntable and arm assembly from the rest of the known universe. And very effective it is too, I may say.

However, this apparently ultimate solution is not without some practical drawbacks. Once the chosen arm is fitted, the whole assembly must be levelled by adjustment of the three springs, which are situated beneath the deck. Which means at every step:- removing the outer turntable, upending the deck, removing the base, replacing the outer turntable and checking with a spirit level. If it is still not right, then it's remove the outer turntable, upend the deck ...and so on and on ad frustratum maximum

Once this has been achieved, the arm leads must be arranged within the plinth so that they do not re-couple the subchassis to the base, thus negating a large portion of the benefit gleaned from the spring suspension. This is fairly straightforward at least, but with an SME the leads are very stiff indeed, making the adjustment critical. Naturally though, SME can supply a flexible link if your patience falls short of the task.

## Things That Go Bump In The Night

Mention of the magnificent SME brings me onto the subject of fitting said arm to this deck.
'Difficult' sums it up nicely.


Left: The 1605 with SMEN15 IV installed. Note the improved turntable mat and relatively small armboard. The base is much more massive than the standard version and the base-plate is of thick chipboard. A slot will need to be cut through this to clear an SME lead, however. The two small openings Thorens provide are simply not big enough!
Arranged across the deck are some of the pickups used in evaluating the 160S. Top to bottom these are: Goldring G900 ICC, Coral MC81, Empire 600 LAC and the elegant Ortofon/SME 30 H . The variation in type of sound between these units was most helpful in identifying which effects were caused solely by the 1605 !


Above: The Thorens sub-chasis with outer turntable removed. Note the position of the drive belt.

The 'new improved' arm-board fitted here - and the subchassis - have barely enough room to accept the SME III. Barely in this case means slightly less than $1 / 10$ th of a gnat's whisker. I would strongly advise any prospective owners of this combination to shell out the required sum of $£ 8.62$ and let SME send you a fully cut board. I assure you it is a miserly sum indeed, when weighed against the blood, sweat and tears you will expend trying to be a DIY hero. You have been warned.

Come to think of it, how about supplying the SME board with the 160S, eh Thorens? All else is but dross anyway!

Failure to line up the arm exactly will result in the pillar not clearing the sub-chassis cut-out, which is every bit as generous as the pickup board, or just as musically, bumping away at the base every time someone breathes on the turntable.

All in all then, an enthusiast's - or a dealer's - task. Patience is the order of the day and if you fancy a TD 160S, but don't fancy setting it up, then your friendly neighbourhood dealer should do it for you. If he doesn't, simply find another (more) friendly neighbourhood dealer.

## Down To Earth

Earthing the sub-chassis and arm means linking the earth of this to the base earth point beneath the turntable, from where a lead can be run to the amplifier - a point not well explained in the literature, I feel.

1 earthed my Decca cleaning arm to the same point to keep down the number of wires trailing around. I have heard it said that use of these' in-play' brush cleaners recouples the turntable in the same manner as a badly arranged output lead beneath the base. Frankly, I don't go along with that at all. If the tracking brush is set up properly to a very small down force, then I cannot see that it will affect matters significantly. During listening tests I tried to identify any audible effect produced by employing the brush and found only that it removed the dust! Really exciting that, huh?

## All Hands On Deck

Listening to the TD 160 S was carried out with an SME III on the arm-board, and a variety of cartridges, including a Coldring C900ICC and a Coral MC81. Also a Shure V15 IV was used on most comparisons as was an Ortofon/SME 30H. Regular readers will have seen this little lot before!

Incidently I have had some letters questioning my continued use of an SME III as a reference, when as one reader put it, "there are stacks of better arms around."

The answer to all these people lies in the fact that I personally don't think there are ANY better arms around.

The SME is an excellently engineered, universal pick-up arm, which is as neutral as any on the market and a damn sight easier to use than most. Don't be fooled into equating tedious setting up with final quality. It does not automatically follow. The SME is a dream to use and offers facilities that allow for useful optimisation of the pickup cartridge in use.


[^4]

Close-up of the arm pillar. There is not a great deal of room here so if you are fitting your own pickup - beware.


Above: The fixing of the sub-chassis suspension springs. The foam plugs have been sensibly removed on this model.

A small number of topend pick-ups have been specifically designed for arms other than the SME and will thus operate better in the designed-for carrier.

However, for universal application and sheer engineering excellence, I don't think anyone has gotten near SME yet!

So there.
Back to the plot. After the setting-up was finally concluded and the cartridges aligned I could gratefully sink into the armchair - brandy in hand - and, wiping the sweat from the editorial brow, settle down to some music.

The biggest surprise was the mid-range. With all the cartridges the 1605 produced a cleaner and clearer sound than I had heard from them before. Bass was firm and well-controlled, albeit with a nagging doubt concerning the extension. Treble was unimpeachable.

Continued listening has largely removed that doubt over the bass extension and I realised on a direct $A-B$ it was the reference deck that had a slight upper bass prominence compared to the Thorens, which set me onto the thought in the first place! Instructive things comparisons. Learn something new every time.

## A Right Little Belter

This comparison was set up with two SME III arms and two Shure V15 IV cartridges - and my warmest thanks to both firms for helping out at short notice so graciously - on the Thorens and the reference.

Even after several hours of this switching back and forth between decks I am left with nothing to be able to criticise in the TD 1605 sound! It comes very, very close to being the best turntable l've ever heard and even changing the mat for a GA Audio Soundisc failed to make any improvement. If anything it muddled up the mid-range detail. Some may find it a little bland methinks - but look ye to your references gentlemen!

Taking price into account, the 160 S is an excellent buy. It offers superb performance for its $£ 140$ price tag and should make prospective purchasers of decks twice the price stop and think very carefully indeed. To its price must be added, however, the need for precise setting up and a new arm-board! Still, with a good dealer neither should deter a single true audiophile.

An important addition to the ranks of hi-fi then, and I urge you to go and hear for yourself.


The reference cartridge for the comparisons was a Shure V15/IV.


Above: Close-up on the MDR-7 drive unit. The fine film driver is behind the mesh protection and can be clearly seen here. The foam earpads clip around the whole assembly and a spare set is provided.

## Big Brother Is Here!

Perhaps the best-selling headphones so far in 1980 have been the Sony MDR-3s. And quite right too, many of you will say. Good value for money, they certainly are, and up to the 21st of last month I would have said the best value under $£ 50$. Alas this is true no longer. There is now a unit on the market whose performance far surpasses the MDR-3, adding to it a wealth of bass extension and clarity, sufficient by far to justify an asking price of around $£ 30$. These new phones are little larger than the MDR-3 and not noticeably heavier. The fit is comfortable and the sound dynamic. Their name? Why the MDR-7 of course! What else?

Sirce they fell into $m y$ hands I have been using them in preference to $m y$ own Koss ESP-10 electrostatics a lot of the time - and there is no better recommendation than that.

Comparing against the ESP-10s shows the MDR-7s to have a better bass extension than the Koss and to be able to accept higher levels without distress. Their midrange is coloured with a slight warmth that can add a 'weight' to some music that is simply not there. The treble is smooth and goes a long way past your powers of hearing.

Overall, the sound is lively and detaiked without being intrusive. It is easy to listen through them to the music and the comfortable fitting greatly assists matters here.

The MDR- 7 will be widely available in this country from September 1st. At the same time an MDR-5 is being released which fills in the considerable gap in price between the three and the seven. I haverrt heard them, but on the strength of those on both sides of them, the MDR-5s should not disappoint

Sony apparently have no plans to bring out an MDR-9. At least not yet. At least that is what they tell me now. I can just see Audiophile in a years time. . .

## Conclusions

A nice production yet again. Well built and well presented. A spare set of earpads are included in the price - for when you forget to wash your ears - or just want a change of colour! Selling tag will lie around E30-35 and no doubt the MDR-7 will quickly repeat the sweeping success of its little brother. It deserves to do so, no doubt about it.


Above: The MDR-7 in use. Only one earpiece is adjustable, the other being fixed to a swivel joint to better aligh with the user's head. Cable entry is side-on and much more convenient than on the MDR-3 where it hangs awkwardly, stethescope-like, behind the ear pieces.

The MDR-7 is very comfortable in action, but must be precisely aligned with the ear for best performance.

## Odds And. . . Pieces Of Turf

Next month I hope to be able to offer you a complete cassette based - stereo system at a ludicrously low price. Negotiations continue to bring about an offer on the launch of a new range of budget hi-fi from regions east of Suez! The importers are Videotone and a pair of their excellent GB2 loudspeakers will provide the voice for the system. Everything else - amp, tuner and cassette deck bear a name you will not have heard before, Seoum, and offers 30 W RMS per channel, with good transient delivery, MC input, FM/AM with good sensitivity, LED level metering on tape and input power and best of all a good sound quality.

Price will be under $£ 300$ complete, so if you're looking for equipment in this price area hold on a little - you could save yourself some money!

Also next month I'll be starting to run some of your letters to Audiophile as a regular feature, be they queries or just communications! So if you've anything to say on matters even vaguely hi-fi let's hear from you.

The Audiophile enquiry service will still operate for anyone with a hi-fi problem. Don't forget to give details of the full system you're using and to mark the envelope for 'Audiophile'.

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# SUSTAIN FUZZ BOX 

# For that raunchy sound beloved of electric guitarists the world over, this simple little project is just the thing. 

Fuzz-tone is to guitar what salt is to meat - it adds flavour and body. The ETI Fuzz Unit has an added bonus in an inbuilt sustain circuit, adding a bit of extra spice to the idea. The device offers three distinctive sounds, in addition to the 'straight through' option: sustain, fuzz with sustain or fuzz without sustain.

## How We Did It

To explain how these sounds are realised, we have to consider the circuit diagram.

The input amplifier, IC1, gives the system some overall gain to boost the treble response and present the correct load impedance to the instrument. The mid-range gain is set to five, allowing 1 V peak-to-peak input signals before distortion and producing the largest possible dynamic range. The frequency response is flat from 20 Hz to about 2 kHz , after which an 8 dB step provides a gentle treble boost up to 20 kHz , where the response is rolled off.

Following the input stage is IC2a, one half of an NE571 compander IC configured as a conventional compressor with a fixed compression ratio of $2: 1$. This compression effectively halves the dynamic range of the incoming signal by attenuating high level signals and boosting low leyel ones; thus the signal hangs on - "sustains" - for much longer than it otherwise would. The compression also provides a constant level drive to the clipping stage, making the fuzz sound independent of the instrument output level.

The fuzz stage, Q1, is a high gain amplifier stage. Because of the high, constant drive from the compressor it is always driven into hard clipping, resulting in an output which is substantially a squarewave. The output of the fuzz stage is fed through a tone control which varies the quality of the sound by rolling-off the high frequencies - one of the reasons for the treble boost at the input stage was to ensure that there would be some high frequencies to roll-off at this point!

## Following Envelopes

The by now well-and-truly fuzzed signal is fed to the signal input of IC 2 b , the second half of the NE571 compander. This time the device is setup as an envelope follower with a signal input and a control input; the output of IC2b is whatever frequencies are applied to the signal input but with the amplitude envelope of the signal fed to the control input. It is this envelope follower, plus some simple switching, which makes the Fuzz Unit so versatile - of which more shortly!

A deliberate modification to the envelope follower ensures that IC2b shuts-off completely when the signal on the kontrol input falls below a certain level. This is a simple 'noise gate' function which prevents the amplification of low-level signals and noise, eliminating the hisses and buzzes of unwanted sounds and the squeals and howls of unexpected feedback! This function operates only when Fuzz function is selected.

The Fuzz Unit is capable of producing either sustain, fuzz with sustain, or fuzz without sustain. These variations are

achieved by selecting the appropriate output and the appropriate drive to the control input of the envelope follower.

The switching system is entirely electronic, so the guitar signal never leaves the box even if the footswitches themselves are a dozen yards away. The signal is not required to travel long lengths of cable and so is not attenuated or subject to interference. Also, single-pole non-audio type switches may be used, allowing a larger choice of switch types.

Two switch lines are used to control four electronic switches operating as two sets of change-over switches. One line controls A and B, (sustain on/off), the other controls C and D (fuzz on/off).

If neither fuzz nor sustain is selected, A and C are closed while B and D are open; the output of the unit is derived from the input pre-amplifier (so it will be a little louder and a little brighter than the guitar itself) via $A$ and $C$.

If sustain is selected $A$ and $B$ change over and the output is from IC2a.

## Selective Switching

Selecting fuzz closes D and opens C. Whether it is fuzz with sustain or fuzz without sustain now depends on the position of the sustain select switch. If sustain is selected the drive to the control input of the envelope follower is the compressed signal from IC2a; compression followed by expansion restores the amplitude envelope of the signal, so the output will have the dynamic characteristics of the original guitar sound, but will sustain for longer than usual. If sustain is not selected, the envelope follower control input is from the preamp. Therefore, the output of $I C 2 b$ is the original signal expanded. Because of the value chosen for C 7 and C 16 , the Fuzz Unit will produce a rather long'delayed attack' effect when in


## HOW IT WORKS

The input amplifier (IC1) is a CA3140, chosen for its low noise. The input impedance of the device is quite high, so the effective value is determined by the parallel combination of $R 1, R 2$; the values used give end impedance of 90 k . R1 and R2 can be as low as 10 k or as high as 1 M , as long as they are the same and within this range.

The bias for the CA3140 is filtered and regulated by R3, C2 and LED1; the LED also acts as a 'power on' indicator! The LED must be red as other colours have a different forward voltage. The stage gain of five is set by the ratio of R4 and R5, while C4, C5 and R6 tailor the frequency response.

IC2 is a dual gain control IC, NE571, which may be set-up to implement a number of signal processing functions. Each half of the IC consists of a full wave rectifier acting on the control input, a variable gain cell (signal input), an operational amplifier and a bias system. The blocks may be set-up as, for example, a compressor, an expander, a limiter or an envelope follower. The compression/expansion ratio is internally set at $2: 1$ while the attack and release times are determined by an external timing capacitor and an internal resistor, the attack-todecay time ratio is internally set at 1:5.

It is possible to vary both the compression ratio and the attack/ decay ratio by the use of complex external circuitry. However, the internally set values are adequate for the purpose of this gadget.

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Q1 is connected as an emitter follower in order to present a high input impedance to the guitar. C2, being relatively low capacitance, cuts out most of the bass and C3 with RV1 acts as a simple tone control to cut the treble and hence the amount of treble boost can be altered. Q2 is a simple preamp to recover signal losses in C2, C3 and RV1.

## Dimmer Decoder

## I. Henry, Kirkcowan

This circuit is an alternative decoder for the "ultrasonic remote control dimmer" project published in ETI June '79.

With this decoder, PB1,2 on the transmitter control two independent
channels. PB1 gives a pulsed input at $X$ and a high output is generated at IC1C; PB2 gives a high input at $X$ and a high output is generated at IC1d. IC2 is a dual JK flip-flop, but in this case the inputs have been connected to logic 1 and the outputs of IC1c,d connected to the clock inputs of the flip-flops. In this
configuration the outputs change state each time an input pulse is received, ie if A was at logic O and PB1 on the transmitter is pressed and released A will then be at logic 1 .

The outputs A, B can be used via some buffering arrangement to switch relays for remote control of lights, etc.


## Train Chuffer

c.s. Histed, Chislehurst

This circuit will produce a 'train chuffing' noise and might prove interesting to anybody with their own train layout.

The circuit consists of a white noise generator, which only switches
on with the 'high' part of the square wave output from the clock circuit. The frequency of the clock is adjusted with the 10 M pot and the output voltage of the clock is adjusted by the 100 k pot (these pots control the rate of chuff and the volume of the chuff).

The 2 M 2 pot controls the amount
of noise produced and the 1 k pot on the speaker controls the pitch of the average noise.

The circuit works by amplifying the amount of noise let through by the seemingly wrong way round diode and only letting the circuit be 'on' when the output of the clock is at logic 1.



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## 810S-35B ALARM CHRONOGRAPH

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# CASSETTE INTERFACE 

Use ETI's supersonic interface to store and retrieve digital data at an incredible 4800 bits per second. Design by Hugh Koanantakool.

Moderate-speed cassette systems running at speeds up to 1200 baud have been with us for some time, but unfortunately the standard setters seem to prefer a slower 300 -baud Kansas City standard. 300 -baud can be too slow if you have a lot of data to manipulate and is suitable only for software distribution. That is, once the original chunk of a software package has been implemented in a system, the user or owner could then make a copy of that piece of software for his (or her) normal use. This working copy should be running at the highest data-transfer rate that the owner can afford. In case of a failure in the fast working copy, the user can always fall back on the original master copy running at the slow rate. This design enables you to store and retrieve digital data using an unmodified cassette recorder at 4800 bits per second. The prototype proved to be as reliable as any 300-1 200 baud systems.

## Dropout

One reason for cassette load/save failures is tape dropout - momentary loss of playback signal due to the absence of, or damage to, the ferromagnetic coating somewhere on an imperfect tape; or due to bad contact between the tape and the tape head. In audio cassettes, the tape runs at 1.875 inches a second. Thus, for a 300 -baud KC (Kansas City) tape, a bit of data occupies approximately 0.00625 inches - how tiny! Any dropouts which are larger than that size will cause one or more bits of errors. The only practical solution is to use high quality cassettes which are certified or known to be originally free from dropouts. This applies to both 300 -baud and the fast 4800 -baud systems. From experience most tapes which are error-free at 300 baud can cope well at 4800 baud, but in the latter case, cassettes having good high-frequency specifications are preferred.

## How Good?

This design aims to surpass all existing cassette interfaces in both speed and reliability, given that it should require no more hardware than other systems to build one. It shouild run

well with an average tape recorder and cassette tapes which can cope with the KC standard or CUTS 1200-baud standard. There will be no timing adjustments. The system can be implemented on any existing serial, asynchronous communication channel and thus can be readily added to most home computers. If it becomes impossible to run the system at 4800 baud due to any reasons including those in my list of observations then you might have to slow down the data rate to, say. 2400 baud.

To do so you only have to slow down your UART (Universal Asynchronous Receiver and Transmitter) clock frequency. There is nothing else to adjust, thanks to the all-digital timing.

## Phase Encoding

There is nothing new or magic about the phase encoding format for data storage on magnetic tapes. Figure 1 illustrates how it works. A logic one is represented by the 5 V level and the zero by 0 V (Fig. 1b). Most tape recorders cannot record and playback slowly varying signals or DC . Therefore, a long series of ones or zeros will just come out the same if we attempt to connect the data signal (also called NRZ or Non-Return to Zero) directly to the recorder. This is because the data signal in NRZ format contains important information which is extended down to the very low-frequencies, beyond the frequency range of tape recorders.

Figure 1a shows a carrier wave oscillating at, in this case, 4800 Hz . The carrier is modulated by the data signal of Fig. 1 b by the following rules:
(a) The data signal is assumed to be synchronised to the carrier. This means their transitions (edges) are perfectly in a lignment.
(b) The carrier wave is inverted if data is a one and normal ie non-inverted if data is a zero. The resulting modulated carrier is shown in Fig. 1 c .
The phase encoded signal in Fig.1c is known to contain very little energy at low frequencies and can be recorded and played back with little distortion.

## Demodulation

Figure 1d shows the typical replay signal from the tape recording. Notice the rounding of all sharp edges - this is due to the high-frequency cut-off of the tape recorder. Also the high-frequency components of the signal will suffer from more attenuation than the low frequency components. By using some form of equalisation circuit, we can easily improve the signal into that shown in Fig.1e, which is now good enough for a slicer circuit to decide whether it is high or low. The sliced signal in Fig. 1 f is very similar to that of Fig. 1 c but it may or may not be inverted by the playback amplifier inside your recorder;
Construction of the board (left) should not pose any problems. The LED is on if there is no input or during normal data transfer and off if data transfer is about to take place or has just concluded.


Fig. 1 Timing diagram. The signal output is attentuated to about 100 mV (RMS), suitable for the mic input of most cassette recorders. A high pass filter is included to pre-compensate any loss in high frequency in the cassette. You may not need preemphasis capacitor $\mathbf{C 2}$ if you use a hi-fi deck.
pulse transitions may not be so precisely timed as in Fig.1c due to tape-speed fluctuations and it is more or less independent of the playback volume control setting. We then feed the signal of Fig. 1 f to a digital circuit (a demodulator), which recovers the data signal (Fig.1b) from the sliced signal (Fig.1f) and presents it to the UART receiver section.

## Implementation

You will probably need a "double standard" approach at least in the beginning so that tapes can be converted from the original slow rate to 4800 baud. The interface circuitry can be connected to your computer system using five wires:

- $\quad$ two power lines (common earth and the 5 V supply),
- two serial data lines (one for transmit(dump), one for receive(load)),
- one clock line running at $16 x$ the baud-rate, i.e. 76,800 Hz at 4800 baud.
The only assumption made is that your computer software could handle the UART at 4800 baud Some systems may not cope with a fast transfer rate. The serial I/O by program control instead of using a dedicated UART could be too slow, or maybe the VDU or TTY is not fast enough to dump some characters, eg filenames, in real-time. However, if you are using a memory-mapped VDU (PET, Superboard II, UK101, NASCOM, etc) or your system monitor buffers the load time messages in RAM, there is no problem, since no major hardware modifications are to be made and no software or data


Fig. 3 Adding the fast cassette interface to your system.
format to be changed. The fast system has been in use since March 1979, accumulating the bit error rate to better than 1 in 10. The tape conversion process is fairly straightforward; switch your system to the original interface, load the original tape to computer, switch to 4800 baud and record the same software onto a new cassette.


Fig. 4 Timing diagram.

## Postscript

After experimenting with various kinds of tape recorders it is sad to say that some cassette recorders just cannot cope with the 4800 -baud system. These recorders don't work with 300-1200 baud systems anyway, (or work with persistent troubles) and they can't even play back a continuous tone steadily! That is, if you record a tone and playback, it sounds so wobbly that anyone can detect its poor speed regulation.


## HOW IT WORKS

The upper part of Fig. 2 is the phase encoder. IC1 divides the UART clock signal by 16 to 1x baudrate. The UART data signal is then brought to synchronism to our local clock (carrier) by means of a D-type flip-flop (IC2a). This synchronisation circuit makes sure that data transitions at IC2a always take place at the rising edge of the local clock (at A). However, if the computer data and the local clock happen to be in synchronism already, (a random choice of 1/16), this D-type flip-flop might be in trouble. In reality, this "perfect" chance of trouble never occurs, since the UART's internal + $\mathbf{1 6}$ clock divider circuit works much faster than IC1, even though both are triggered by the same falling edges of the 16x clock. Thus it is sure to achieve perfect synchronisation.

The lower part of Fig. 2 shows the receiver/demodulator section of the system. First the signal from the recorder's ear-phone plug is fed to IC6 via C3. The values of C3 and R4 are such that any drop in level of the high frequency signal from an average cassette recorder is equalised. IC6 then slices through the average level of the equalised signal (Fig.1e). IC6 is wired as a Schmitt trigger circuit in order to suppress the background noise during playback. The output of IC6 is further buffered by IC5b. R9 and R 10 make sure that the op-amp signal is well within the input range of the CMOS gate, IC5b.

The sliced tape signal is then passed through IC3b, which is corfigured as a one-shot triggered by both positive and negative-goting transients. Its function is to generate a short pulse at point H whenever there is a level of transition at pin 10 of IC5b. The timing diagram is continued in Fig. 4 for the sake of explanation of the demodulation process. Pulses at H should be made as narrow as possible: anything shorter than 10 uS will be suitable. The pulse duration at H is proportional to the product of R11 and C5. The narrow H pulses reset the binary counter IC4, which is again clocked at 16x baud-rate. The counter outputs Q3 and Q 4 are NANDed so as to enable us to detect whether its count reaches 12 or more ( $\mathbf{1 1 0 0}$ to 1111 in binary notation). In other words, as long as the $H$ pulses are no more than 0.75 T apart, where T is the duration of one bit, the output of IC5a at I will always be a one. This is because the counter is always reset to zero before it counts to 12. At 4800 baud, T is $208 \mathbf{u S}$. Theoretically the H pulses are either 0.5 T or 1 T apart, corresponding to 8 and 16 counts respectively. Thus, discriminating the spacing interval by the threshold of 12 counts seems to be most logical, allowing some $\pm \mathbf{2 0 \%}$ tape speed fluctuation. In the other case, if the H pulses alif more than 0.75 T apart, we will get a negativegoing pulse at point J. If there are no pulses at $\mathbf{H}$ at all, as in the absence of the playback signal from the tape, the signal at J will be pulsed regularly at the baud-rate frequency with the mark-space ratio of 12:4.

From the timing diagrams (Figs. 1 and 4), we may conclude that a "change" of the carrier phase corresponds to a change in the original data stream. This change in turn corresponds to the larger sepalfation between successive $H$ pulses, equal to 1 . Subsequently, long separation of $H$ pulses is detected as a J pulse. We can, therefore, recover the original data signal from the J pulses by using IC2b, connected as a toggle flip-flop. It inverts its state upon receiving a J pulse. All seems to go well but we might still run into trouble if we happen to start IC2b wrongly and get all the data bits inverted, yet still obeying the change conditions discussed. Care must, therefore, be taken to ensure that the logic state of IC2b is always properly defined before data transfer can take place.

Fortunately, the asynchronous serial data transmission convention is such that on a UART getting ready to transmit, it always sends a series of marks (logic one). This means that we always have a steady tone recorded prior to the actual data signal. Therefore, we can preset IC 2 b to logic one before any transfer process commences. This function is carried out by means of IC5c and d. If the carrier is detected continuously for longer than 20 mS , the circuit will assume that this is a series of marks or logic one. It then resets IC2b accordingly. All subsequent data bits will then be demodulated with the correct polarity.

These properties are usually associated with cheap recorders. Users must avoid recorders with peak speed-fluctuations well over $\pm 20 \%$, our required tolerance. Poor speed-regulation of a new recorder is associated with the lack of motor-regulator circuit, but it can also happen to a more costly recorder if the pinch-roller has been deformed, eg by leaving the machine off in the play position for a long time.

To sum up, the 4800 -baud system may not work with all recorders due to the following reasons, in order of seriousness: (a) recorder transport mechanics - you need a recorder that can at least reproduce clean steady tone,
(b) tape quality: use tapes which are better than just a "low-noise one, eg "Super Dynamic", "High Frequen-
cy", etc, recorder bandwidth - you tend to get more bandwidth from a radio-cassette than a hand-held recorder.

If your system has an RTS line and you are using it to control the cassette's motor, then you may also use it to control the received data line of this interface as well. When there is no input signal from the recorder, the idling sequence at point L (Fig.2) is 1010101, which is a series of the valid ASCII ' $U$ ' characters causing over-run error in the UART. This error is normally reset by the tape loader routine before the data transfer takes place. A normal way of tape loading is to type into the computer, specifying a tape load command, start playing the cassette recorder until you hear the header tone (continuous 4800 Hz ) then type RETURN to start loading. The presence of the continuous tone is also indicated by the LED going off temporarily. However, if you happen to get a monitor which does not reset the UART (eg the UK101), then you need to get rid of the 1010101 . . . pattern by means of the RTS line. With RTS line low (no request for data transfer) the LED is also off and the data output line is kept high and no longer causes overrun errors.

----- = INSULATED LINK ON UNDERSIDE OF PCB
Fig. 5 Component overlay.
PARTS LIST

| Resistors 1/4W, 5\% |  | C2 | 560p ceramic |
| :---: | :---: | :---: | :---: |
| R1,2,14 | 4k7 | C4 | 22u 25V tantalum |
| R3 | 33k | C5,7 | 100p ceramic |
| R4,15 | 150R | C6 | 22n polycarbonate |
| R5,6 | 470R |  |  |
| R7 | $1 \mathrm{k5}$ | Semiconductors |  |
| R8,12 | 1 MO | IC1,4 | 4024B |
| R9 | 22k | IC2 | 4013B |
| R10,16 | 47k | IC3 | 40308 |
| R11 | 24k | IC5 | 4093B |
| R13 | 11k | IC6 | 3140 |
| R17,18 | 10k | Q1 | BC109 |
|  |  | D1 | 1N4148 |
| Capacitors $\mathrm{C} 1,3 \quad 100 \mathrm{nc}$ | ramic | LED1 | TIL209 |

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# HEAD AMP DESIGN 

## Videotone's Andy Sykes rounds off his head amp design guide with a few words on the dreaded mains hum.



The head amplifier design published in ETI in January is a good example of a differential input stage (Fig.1), which also makes use of a symmetrical output stage. A different approach is shown in Fig. 2, that of the Videotone H 300 amplifier. This is a refined version of the circuit in Fig 6 (last month) and is based on a simple parallel transistor pair.

Eight transistors are used for Q1 and two for Q2 and a bootstrap capacitor is employed to increase the open loop gain and so keep the distortion well below the noise level.

## Trickle Charge

The design also features switchable gain and input capacitance to allow many different cartridges to be catered for. The commercial unit is powered by a rechargeable battery which is put on trickle charge when the head amp is switched off. This neatly removes both the need tor a sophisticated mains power supply and the tedium of changing batteries.

## De-Thumper

Any output spikes produced on power up or down, so prevalent in other designs, are also eliminated by the use of a darlington pair to slowly raise and lower the supply rail when the power switch is operated. The time constant of this rise and fall is far greater than any others in the circuit and so the unit switches on and off without damaging your precious speaker cones if you inadvertently leave the volume turned up.

Another advantage of this particular configuration is that the feedback resistor provides the bias for the first stage so
that potentially noisy input bias resistors are not required. The common emitter second stage gives a low output impedance, which enables relatively long signal leads to be used and renders variations in main amplifier input impedances unimportant. The frequency response extends well up into the MHz region to reduce susceptability to RF pickup and note also the use of an inductor in the supply line. It also sounds good, though perhaps I am a little biased.

## Mains Hum

The final point to be discussed is the bane of any audiophile's life, the dreaded mains hum. Oh for the DC supplies of yester-year. As with any other piece of sensitive electronics great care with screening and earthing arrangements must be taken to keep the hum gremlins at bay. The ideal case would be made of Mu metal, an alloy with particularly good screening properties, but this is not very cosmetic. If your head amp is to stand any chance of holding its own against the acres of brushed aluminium which enclose the average $\mathrm{Hi}-\mathrm{Fi}$, a smart but substantial aluminium or steel case is the next best thing.

## Earth Loops

Connections to and from the head amp should be such that earth loops are avoided. Figure 3 illustrates one possible way of doing this, the turntable earth being separated from the signal earth to avoid hum pickup from the motor. It may also be necessary to tie the amplifier chassis down to a good earth

if it follows the modern trend of possessing a two-core mains cable. If your house wiring earth is not good enough, a passing water (not gas) pipe should be pressed into service, or even a length of copper pipe sunk into the back garden.

There is a case of a house with such bad earthing arrangements that the GPO telephone engineers not only resorted to sinking a rod in the garden, but instructed the occupants to water it before making a call in order to keep the telephone line from fading away.

## Mains-Shy

A certain amount of experimentation may be necessary to obtain the best position to site the Head Amplifier. Keep it and all signal leads away from potential sources of electromagnetic radiation such as mains cables, amplifier transformers and electric motors. I know that all this is pretty boring stuff which all good Hi-Fi buffs have known since they were knee high to a volume control, but introducing a Head Amp to your Hi-Fi does increase the system gain by a further factor of 30 and so precautions against hum pickup must be correspondingly greater.

If you do plump for a mains powered design, a separate case away from the amplifier circuit will almost certainly be required. This supply should be as well regulated and decoupled as possible (the use of the various IC voltage regulators here is highly recommended). Long supply leads are a potential source of RF pickup so remember to decouple at high frequencies as well on the supply line as near to the amplifier circuit as possible. Again the use of an inductor in the supply lines is recommended.

Fig.2 The Videotone H300 uses a different approach from the ETI design.


Fig.3. One possible way of avoiding earth loops.

## Memories are Made of This

So there we have it, an albeit potted guide to Head Amplifier design, but it should point budding designers in the right direction, avoiding the more obvious pitfalls. It is well worth the time and effort expended on producing a head amp because, although the sound extracted from the record groove by a good moving coil cartridge is not startling when compared to a moving magnet of similar price, it is the subtleties of reproduction that are conspicuous by their absence; once heard, always hankered after. Even my wife can tell the difference and her normal assesment of any piece of $\mathrm{Hi}-\mathrm{Fi} \mid$ bring home is based upon its ability to collect dust or support a plant pot. I am winning, though, slowly very slowly.

ETI

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# DESIGNER'S NOTEBOOK 

# Ray Marston devotes this month's 'Notebook' to a discussion of practical temperature-sensing switches, alarms and metering circuits. 

Temperature-sensitive circuits such as thermo-switches, alarms and electronic thermometers are amongst the most popular and common of all projects published in the technical Press. Such projects may use thermostats, thermistors or semiconductor devices as their basic temperaturesensing elements: each of these types of device has its own advantages and disadvantages and presents the electronics engineer with particular design problems. This month's 'Notebook' is devoted to a discussion of some of these problems.

## Thermostats

The easiest way to implement a thermo-switch project is to use a commercially available thermostat of the type used in central heating systems, for instance, as the switching element. These devices usually take the form of a bimetal strip that closes a pair of contacts when the temperature falls below a preset'trip' level, the level usually being variable over a limited range via a calibrated control.

The trip levels of these thermostats are usually accurate to within a degree or two and the devices give an adequate performance in most practical applications. They are simply wired in series with the switched load, as shown in Fig.1a, so that power is fed to the load when the temperature falls below the trip level.

You can reverse the action of a standard thermostat, so that power is fed to the load when the temperature rises above the trip level (contacts open) by using the simple circuit of Fig.1b. Here, when the contacts are closed the output of the inverting CMOS gate is driven low, so Q1 and the relay are off and zero power is fed to the load via the RLA/1 contacts. The circuit consumes a standby current (via R1) of only a microamp or so under this condition. When the thermostat contacts open, the input of the gate is pulled low via R1, so Q1 and RLA are driven on and power is connected to the load via the RLA/T contacts.

## Thermistor Circuits

Thermistors are simply resistive elements that are subject to fairly large changes in resistive value with small changes in temperature. They are ideally suited to use in sensitive or 'precision' thermal switching applications. The devices come in a variety of styles, but we'll concern ourselves here with inexpensive negative temperature coefficient (NTC) carbon-rod types only; a quick scan of component suppliers catalogues will show that these devices are readily available with a variety of resistance values at a variety of temperatures.

Figure 2 shows how you can use an NTC thermistor to make a precision under-temperature or 'frost' switch. Here, TH1 PR1 and R1-R2 are wired in the form of a bridge that is


Fig. 1 The effective switching action of a thermostat (a) can be reversed by using the circuit shown in (b).
almost balanced (via PR1) at the required trip temperature and the op-amp is wired as a voltage comparator with its output driving the relay via Q1. At temperatures below the trip level the pin 3 voltage of the op-amp output is driven to negative saturation and Q1 and the relay are driven on. At temperatures above the trip level the reverse action is obtained and the op-amp output is driven to positive saturation and Q1 and the relay are cut off.

The action of the Fig. 2 circuit can be reversed, so that the circuit acts as an over-temperature switch, either by transposing the pin-2 and pin-3 connections of the op-amp or, as in the case shown in Fig.3, by transposing the TH1 and PR1 positions.


Fig. 2 Precision under-temperature or 'frost' switch using thermistor sensor.

## Two Into One

Figure 4 shows how the above two circuits can be used together to make a combined over/under-temperature switch in which the relay turns on if the temperature (of TH1) goes above a limit set by PR3 or below a limit set by PR2.

Note in the above three circuits that TH1 can be any NTC thermistor that exhibits a resistance in the approximate range 500R to $9 \mathrm{k0}$ at the desired mean 'trip' temperature.

Finally, Fig. 5 shows how an NTC thermistor can be used to make a direct-output alarm-call generator that produces a powerful fixed tone if the TH1 temperature falls below a level


Fig. 3 Precision over-temperature switch using thermistor sensor.
preset via PR1. The op-amp is wired as a conventional astable (with its output boosted by Q1-Q2), except that PR1-TH1 act as a potential divider between the output and pin- 2 input of the op-amp and prevents the circuit from oscillating 'when the resistance of TH1 is below that of PR1. The action of the circuit can be reversed, so that it acts as an over-temperature alarm, by simply transposing TH1 and PR1. In either case, TH1 can be any NTC type that has a value in the range 2 kO to 2 MO at the required trigger temperature: the operating frequency of the astable can be changed by altering the C 1 value.

## Diode Sensors

Ordinary silicon diodes have junction temperature coefficients of about $-2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ when forward biased and can thus usefully be employed as temperature sensing devices. Major advantages of such diodes are that they give readily repeatable and consistent results and, because of their small masses, have fairly rapid thermal response times. A major

Fig. 4 Method of combining the Fig. 2 and 3 circuits to make a precision over/under temperature switch with independently adjustable upper and lower trip levels.

disadvantage is that their forward voltages are normally large compared to normal temperature-change values and are highly dependent on forward current: Typically, $V_{f}$ values may be 630 mV at 1 mA and 660 mV at 2 mA , giving a nominal 3 mV $\mathrm{V}_{f}$ change (equal to to a $1.5^{\circ} \mathrm{C}$ error) with a $10 \%$ change of forward current.

Figure 6 shows how a pair of 1 N 4148 (or similar) diodes can be used to make a differential temperature switch in which the relay turns on when the D1 temperature rises above that of $D 2$. The circuit is responsive to the relative, rather than the absolute, temperatures of the two diodes. PR1 enables the differential trip levels to be varied over a limited range.


Fig. 5 Direct output under-temperature alarm produces a powerful tone signal when temperature falls below a value preset by PR1. The circuit can be converted to an over-temperature alarm by transposing TH1 and PR1.

Fig. 6 This differential temperature switch uses diode sensors and turns RLA on when the D1 temperature rises above that of D2.

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# Sound out your collection of Project 80 synthesiser modules with this 10 W per channel stereo power amplifier. Design by Charles Blakey 

The 80-14 Stereo Power Amplifier is designed to be used in conjunction with the Project 80 synthesiser but with a few component changes it may also be used as a compact general purpose amplifier. The amplifier has an input impedance of 100 k and an output of 10 W per channel into 8 R with a maximum distortion of $0.5 \%$ (typically $0.1 \%$ ). For use with the synthesiser the input sensitivity is 1 V 2 RMS for the rated output and for the general purpose version the sensitivity is 250 mV RMS. A switched headphone output is incorporated, suitable for use with low impedance headphones.

The design is based on the TDA2030 which is a Class B amplifier with low harmonic and cross-over distortion. It incorporates power limiting circuitry, giving short-circuit protection, in addition to a conventional thermal shut down system. The choice is based on experience with the TDA2030, the fact that 10 W per channel is adequate for domestic or monitoring use, the need to keep heat generation to an acceptable level and, not least, to provide a compact module.

## Power Regulations

To obtain the 10 W per channel output it is necessary to use a 30 V supply; the maximum rating of the device is 36 V . Furthermore, synthesiser applications in particular can generate peak current demands and these factors dictated the use of a regulated +15 V supply and $D C$ coupling, of the speakers. The components for rectifying, smoothing and, regulating the power supply have been incorporated on the same $P C B$ as the amplifier. When used with the synthesiser this allows the same mains switch to be used as for the +15 V module supply (Project 80-1) and for the fuse and
transformer for the amplifier to be housed in the keyboard case. A miniature three pole connector may then be used to couple the $15-0-15 \mathrm{~V}$ unregulated supply to the module housing allowing the module to be rapidly removed from the case when required. Also by having the capacitors on the PCB the ground returns from the speakers are kept short.

## All Change

The component values shown in the circuit diagram are for the synthesiser version. For the general purpose amplifier the following component changes are required.

| R3,8 | wire links |
| :--- | :--- |
| R4,6,11,13 | 100 k |
| R5,12 | 3 k 3 |
| C6,11 | 4 u 7 PCB electrolytic |

## Construction

The module will fit onto the standard $9 \times 3$ inch panel and it can also be installed in a Teka Alba A23G case but as with the panel version the transformer will have to be external to the case. For the self-contained amplifier a case with minimum internal dimensions of width 220 mm , length 250 mm and height 90 mm is required.

Construction should be carried out in the following sequence. Make the one wire link with insulated wire then solder in the resistors, capacitors and the bridge rectifier. Next install the TDA2030s. Slide the heatsink under the TDA2030 and, after checking that the pins are still in place, bolt the IC and the heatsink to the PCB. Do not move the
heatsink once the IC has been soldered since this will stress the pins. The voltage regulators are now bolted to their heatsinks (the pins should protrude from the side having the greatest distance from mounting hole to edge) and the combined heatsink and IC held firmly against the PCB while the regulator is soldered in place. There is no need to isolate any of the ICs from their heatsinks, but it should be noted that the heatsinks for the negative regulator and the TDA2030s will be at negative potential. A small amount of heatsink compound between the IC and their respective heatsinks is desirable.

Next wire the PCB to the panel components. Screened wire should be used for the input leads which go from the input jack sockets to the rotary potentiometers and from the latter to the PCB. Do not common ground connections at the panel (except for the LEDs), but take them back to the appropriate connection hole on the PCB. Keep wiring as short and neat as possible. For the speaker leads it is preferable to use wire of at least equivalent to $16 / 0.2 \mathrm{~mm}$. R8 and 15 can be soldered direct to the switch and a lead taken from the other end to the headphone socket while R9 and 16 should be soldered direct to the headphone socket. Remember to take a ground return from this socket to the PCB.

Fig 1 (right) Circuit diagram of the power supply. BR1 is a 2 A bridge rectifier.
Fig. 2 (below) Circuit diagram of the stereo Monitor Amplifier (synthesiser version). See text for alterations necessary to make a general purpose amplifier.


HOWIT WORKS

The TDA2030 power amplifiers (IC3 and IC4) require few external components and the function of the latter for the left input is described. C5 AC couples the amplifier while R3 and R4 form an attenuating network to reduce the sensitivity for use with the Project 80 synthesiser and, in the absence of RV1, determine the input impedance. RV1 provides manual adjustment of attenuation. R5 and R6 set the closed loop gain and for the general purpose version ( $\mathrm{R} 4=100 \mathrm{k} ; \mathrm{R} 6=100 \mathrm{k} ; \mathrm{R} 5=3 \mathrm{k} 3$ ) the voltage gain is approximately 30 dB. C6 is for DC decoupling of the inverting input and adjusts the low frequency cut-off. R7 and C9 increase frequency stability while C3, C4 -(power supply) together with C7 and C8 are bypass capacitors which
also reduce the risk of oscillation.
SW1 allows selection of speaker or headphone outputs and for the latter R8 and R9 attenuate the output to a level suitable for low impedance headphones.

The power supply is a conventional regulated supply with a nominal +15 V and $1 \mathrm{A5}$ per rail which is sufficient for 8 R speakers at peak output of the amplifiers (about 13 W with $10 \%$ distortion). The regulators will also cope with 4 R speakers in combination with a suitable transformer. R1, R2 together with LED 1,2 give a visual indication of supply voltage to the amplifiers.


Fig. 3 Component overlay.

## PARTS LIST

| (Synthesiser version, 8R speakers) |  |
| :---: | :---: |
| Resistors $1 / 4 \mathrm{~W}$ carbon except where stated |  |
| R1,2 | 1k2 |
| R3,10 | 82k |
| R4,6,11,13 | 22k |
| R5,12 | 68R |
| R7,14 | 1R0, $1 / 2 \mathrm{~W}$ |
| R8,15 | 100R, 1/2 W |
| R9,16 | 8R2, 2W5 wirewound |
| Potentiometers |  |
| RV1,2 | 100k logarithmic |
| Capacitors |  |
| C1,2 | 2200 u 40 V electrolytic |
| C3,4 | 10u 25 V electrolytic |
| C5,10 | 100100 V PCB electrolytic |
| C6, 11 | 22u 25 V PCB electrolytic |
| C7,8,9,12,13,14 | 100n disc ceramic |
| Semiconductors |  |
| IC1 | LM340T-15 |
| IC2 | LM320T-15 |
| IC3,4 | TDA2030H |
| LED 1,2 | Red LED |
| 81 | 2 A bridge rectifier |
| Miscellaneous |  |
| SW1 | DPDT subminiature switch |
| SK1,2 | 3.5 mm jack sockets (phono sockets for GP version) |
| SK3,4 | 0.25 inch mono jack sockets |
| SK5 | 0.25 inch stereo jack socket |
| T1 | 50 VA transformer, dual 15 |
|  | V secondaries in series or 15-0.15 V type. |
| FST | Chassis fuse holder with 1 A fuse. |
| Heatsinks for IC1,2,3, and 4 |  |

A kit for the stereo amplifier is available from Digisound Limited, 13 The Brooklands, Wrea Green, Preston, Lancs PR4 2NQ for E22.20 inclusive of postage and VAT. The kit includes the PCB and all listed components except transformer and case/panel. Please specify synthesiser or general purpose version.

## Ironing

A final point to note is that comparatively heavy currents will flow through many of the connections and it is essential that they are properly soldered. The connections requiring most care are those to ground where the large foil area acts as a heatsink. This is eased by using a tinned PCB but even then it is necessary to place the soldering iron adjacent (not touching) to the lead to be soldered and allow the area to heat up sufficiently prior to heating the lead and applying solder to it.

After construction connect the transformer and switch on. Cently touch each IC in turn. These should remain cool, since the TDA2030 quiescent current to each is only of the order of 50 mA . The LEDs will indicate whether the power supply is functioning. If any of the ICs run hot at this stage check the component placement and condition of soldered joints. Next connect the speakers and if any hum is evident check the wiring from PCB to panel components. Finally connect the amplifier to an audio source to determine tha the module is functioning correctly.

Conventional $\mathrm{Hi}-\mathrm{Fi}$ speakers should not be used it conjunction with a synthesiser since single frequency tone of more than a few watts can damage treble speakers. Fo most purposes full range speakers with a nomina impedance of 8 R and a rating of 15 W will prove adequat


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# ASTROLOGUE 

# Over the years ETI has covered almost every aspect of spaceflight. Now in the new regular series lan Graham keeps you up to date with what's happening in the world of aerospace. 

0ne aspect of the European space programme suffered a serious setback in May this year, when the Ariane launch vehicle ended up in the Atlantic Ocean two minutes after embarking on its second test flight.

Ariane is the key to Europe's future independence from America and Russia in placing satellites in Earth orbit. It will vie with the American Space Shuttle for business. Although the European Space Agency (ESA) is supporting the development and testing programme, once the hardware is proven Ariane will have to pay its own way by charging customers to carry their payloads into orbit.

The 200 tonne, three stage rocket first took to the air in December 1979 at the fourth attempt. The first hold-up was caused by excessive pressure readings in one of the four first stage Viking 2 engines. In fact the engines were OK. The fault was in the pressure sensor.

During the second attempted launch a fault appeared in the on-board batteries. Again, a sensor was found to be responsible. Unfortunately, this malfunction caused further delay by damaging one of the third stage subsystems (helium pressurisation). When Ariane finally got off the ground, its performance exceeded the designers' predictions, to the relief of all concerned. Ariane was a success.

## Test Launch

The second test rocket blasted off from the Guiana Space Centre in French Guiana on May 23rd. Within a few seconds of lift-off, pressure in one of the four first stage engines began to fluctuate. Two of the remaining engines suffered the same rapid pressure variations, which set up vibration in the structure itself. Eventually, the rocket broke up and blew itself to pieces.

The wreckage has now been recovered from the Atlantic mud and investigators have found a small metal identification tag in a fuel injector in one of the engines, although it isn't known if the tag was lodged in the injector at launch or during the break-up. The investigators are also looking at several other possible causes. The next test flight, originally scheduled for November, has been postponed until the beginning of next year.

## Hughes' News

This is the first chance we've had to look at the new Hughes Aircraft Company Wasp anti-armour missile. It is one of a new generation of 'fire and forget' missiles; that is, once fired from an aircraft, the missile can carry on to its target without any guidance from the mother aircraft.

Of its predecessors, Maverick had to be targeted by the aircraft and could only be fired singly. Wasp can be fired either singly or in swarms of ten or more, but its over-riding advantage is that the aircrew do not have to identify a target before launch. The missile looks after all that itself. So, the aircrew can send a dozen Wasps on their way against a formation of enemy tanks and make for home without contacting the air defences. For that reason I'd guess Wasp will be a popular missile with the aircrew who will operate it.


In this artist's impression, a swarm of Wasps has been launched in the general direction of a formation of enemy tanks. The aircrew are already making for home. Each missile then seeks out a target and attacks.

The Hughes Aircraft Company's Wasp air-to-surface anti-armour missile. When the five feet long missile is launched, the wings flip out into the flying position.

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## MICROBASICS

# In the second part of our new series, Henry Budgett takes the mystique out of the inner workings of modern man's best friend and contemplates the bits and pieces necessary to make it all work. 

Having introduced the various component parts of a computer svstem in last month's episode I shall now move onto the actual microprocessor itself. Just as we divided the computer up into a number of parts so we may dissect the microprocessor. It is important to understand at this early stage that the much-vaunted micro is merely a very complex piece of electronic logic and is totally useless on its own without the ranks of qualified engineers, programmers and other allied trades, the supposedly mighty micro is an incomprehensible lump of high technology!

## Architectural Heritage

The average, general purpose computer can be divided into a number of discrete elements as we saw last month. One of these components is the Central Processing UnitorCPU and this can be sub-divided still further. The microprocessor is really a totally integrated central processing unit; it still needs all the other bits and pieces to make it perform as a computer. Some of the later designs do incorporate internal memory
areas and one or two even have self-contained programs, the new SC/MP chip from National Semi with the NIBL BASIC built in being a prime example.

The three main sections of the CPU are the registers, the ALU and the control circuitry.

Taking them in order we find that the registers are a group of storage units within the CPU. Some of these are available to the programmer, others are used solely by the processor as counters or storage locations. The most important of these is the Accumulator. This register is used to store the data to be processed by the ALU, a typical instruction being to add the contents of some memory location to the Accumulator and to hold the result in the Accumulator for further processing. Many of the current families have other general purpose registers for data storage - the 8080 has six for example.

## Flagging Already?

Closely associated with the Accumulator are a number of special registers called the flags. These are used to indicate the

Fig. 1 Block diagram of the internal areas of an 8000. The TEMP registers (*) are used by the CPU internally and cannot be accessed. Figures in brackets refer to the number of bits available in each register or latch.

status of the ALU after an operation. Typical flags are 'carry' showing that an arithmetical carry has occurred, 'overflow' which simply shows that the number has exceeded the word length of the Accumulator and a number of bits which indicate the sign of the result in the Accumulator. There is also one other register connected with the Accumulator and ALU and that is the index register. This holds any offsets used in addressing or indexing and its inclusion is machine dependent.

The processor also requires a number of special registers, the instruction register and the program counter being two typical examples. These both have a double word' capacity, that is they can hold a full sixteen bit address. The contents of the program counter are always one in front of the address currently being used. This is in order to allow subroutines to rejoin the program at the right place. When multiple subroutines are used, these addresses are held in a LIFO memory area called the stack. Some processors have a built-in stack which allows only a certain number of subroutines, whereas others use a dedicated area of memory, which can be, in theory, as large as you like.

All the stored information in memory is, until decoded, garbage. The instruction register performs two tasks in that it notonly holds the currently selected address contents but also decodes them to see if they are valid instructions or data. This is usually done by a mask programmed ROM (Read Only Memory) which has all the valid instructions stored in it. The reason for coding the instruction set into a 'microprogram' are twofold. Firstly, it makes the control circuitry much simpler and, secondly, one can, in theory at least, change the instruction set of one's processor. As an example of this there are some 20 extra codes built into the Z80 CPU that are not mentioned in the manuals. Apparently they are not all guaranteed to work on all Z80s. Anyone know what they are and what they do?

## Cycling Around

All the processes of control are under the charge of a central clock which synchronises the various happenings within the CPU. Some processors require a two phase clock, others a single phase, but in almost all cases the clock must be crystal
controlled. The reason for the accuracy needed is that, if one is to expand the system further than the basic CPU and its associated support circuitry, the clock must remain stable under variations of temperature and varying loads. Computer buses are fairly capacitive and can, over reasonable transmission distances, turn a nice square wave into a very unpleasant object indeed. The fundamental speed of the CPU is governed by the clock frequency. The original 8080 ran at 1 MHz and the 8080A, because of improved internal circuitry, runs at 2 MHz and will, therefore, process at twice the speed. However, and this is a common misconception, the actual CPU doesn't process at these speeds because of a number of reasons.

The most obvious reason is that the ALU is a serial device, that is it takes one bit at a time rather than processing the entire word. The second reason, which I will elaborate on in a minute, is that one has to perform a number of discrete operations within the chip just to get the information in a place where it can be processed and this takes time. All these operations are performed in cycles, the fundamental unit of time taken to fetch and execute a single instruction. On inspection of a data sheet on your chosen micro you will find this time quoted in terms of the number of clock cycles taken. All other instructions are then specified in the number of cycles that they take.

## State Visit

To further explain this concept of instruction cycles let's take a look at the various types. The basic. FETCH cycle, also known as the M1 cycle, is made up of four states. During the first three, the processor fetches the instruction from the memory location indicated by the program counter. The counter is at this point showing the current location and has not been incremented. The fourth cycle is taken up by decoding the instruction. An example of this is the instruction to add the contents of a register to the Accumulator. If we wish to access a memory location rather than a register, we will have to perform a memory read, which requires an extra machine cycle. Say we wish to add the contents of a given memory location to the contents of the Accumulator. The sequence of operations is as follows: the processor extracts the


Fig. 2 Functional block diagram of a CPU. This represents the minimal configuration you would expect to find. You could implement this (for fun) in discrete logic elements and see how it worked. It makes a good demonstration piece for schools and colleges.
single byte instruction from the memory location given in the program counter; this takes three states. This is decoded and the processor sends, as an address, the contents of its H and L registers. The data word returned during this cycle is held in a temporary register inside the CPU and we have now used six states. The final act of adding the temporary register contents to the Accumulator takes a further state making seven in all, or two cycles. The longest operation of all, in 8080 code, takes 16 states or five machine cycles.


Fig. 3 Timing diagram showing the various states that can make up a machine cycle: The vertical arrowed lines indicate information access states.

## The Ins And Outs

The final section of our look at the internals of a CPU is the connections you can make with the outside world. Cenerally, the CPU is housed inside a DIL package with some 40 legs. Under normal circumstances, assuming the standard eight bit CPU, we will have 16 pins for the address bus, eight pins for the data bus and 16 pins left to play with. Just what you do with them depends on the kind of CPU you have, but let's take a close look at the pins on an 8080.

Having already mentioned the address and data bus, we only need to say that the data bus is a bi-directional system and is capable of tri-state operation. It can assume a high impedance state, which is neither a logic zero nor one and this is used under some special circumstances, which will be mentioned next month. Four further legs can be allocated to power; the device needs $\pm 5 \mathrm{~V},+12 \mathrm{~V}$ and ground. Yet two more legs can be allocated to the required two phase clock, leaving us ten possible control signals to communicate the state of the device to the outside world. These are SYNC, DBIN, WAIT, HLDA, INTE, READY, HOLD, INT and RESET. Taking these in order, the SYNC indicates the first state of each machine cycle, thus acting as a synchronisation signal, hence the name. The DBIN signal tells the outside world that the CPU can accept data. It should be used to externally enable the
transfer. WAIT is an indication that the CPU has entered a WAIT state, triggered by pulling the READY line low before the second state time. This causes extra states to be added to the cycle time for as long as the READY line is held low. The process is often used in situations where the memory or device currently being accessed is slower than the processor.

Our next signal, WR, is provided for the synchronisation of external transfers. These include memory and I/O operations and it is the converse of DBIN. There now follows a group of controls, which are concerned with things called interrupts. An interrupt is the computer equivalent of a tap on the shoulder and is used by peripheral devices to tell the processor that they are ready to be looked at. The INT line must be set high to tap the computer on its shoulder, but this will only work if the INTE line has been enabled previously. Inside the CPU, the interrupt is signalled by a status bit being set and the external device must put its instruction onto the bus in order for any action to be taken. The HOLD line is concerned with direct memory access and as such we shall not dwell on this until next month. The HLDA is merely an indication that the CPU is in a HOLD state. Finally we have the RESET line which, as its name implies, does. The signal will restore the CPU to the first state of a machine cycle and it also clears the program counter. It is essential to start all the power up sequences with this signal otherwise you never know what you may find yourself doing! It is also worth noting for all those sceptics among you that pressing RESET does not destroy all your registers, it merely sets you back to the beginning without destroying your program unless the person who programmed the monitor on your system clears the memory as the first operation. Whoever said that programmers were logical anyway.


Pin designations of the 8080 . Developed by Intel, fathers of the micro, it is still regarded as the workhorse of eight bit processing. It also spawned the Z80, probably the most powerful eight bit chip using current technology.

## Coming Soon

Next month's slice of bits will investigate the thorny topic of memory devices and show you the way in the ROM-RAM jungle as well as telling you how to ignore your CPU altogether and really make things work fast.

## VIDEO MUSIC



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# ELECTRONICS TOMORROW 

# A spanner's not much help when your computerised fuel injection system dies. Dave Raven of Metac Electronics reports on the quality control that keeps your chips up to scratch, with a footnote on hand-held games. 

While we must welcome the arrival of new electronic circuitry in everyday products (cars, sewing machines, food mixers, etc), electronic failures always seem much worse and more difficult to put right. The difficulty now in making temporary repairs to an item, which has been transformed into a solid block of plastic containing a thick-film circuit, is underlined to the stranded motorist when he is out in the pouring rain.

My own recent experience of this occurred miles out in the countryside. I was directed with my faulty alternator to a small holding, miles from anywhere. The gentleman who attended to me was clearly an expert, despite outward appearances and disused cars littering his yard. A small workshop/caravan was crammed with used starter motors and dynamos. With the precision of a brain surgeon, he diagnosed my faulty alternator (a diode in yer alternator) and immediately commenced stripping it down and replacing the faulty component. With an elaborate piece of home made test equipment, which put Heath Robinson to shame, he tested the alternator on the bench under full load. While watching this rustic genius 1 felt assured that, even with the advent of microprocessors this man will survive. But what of all the other indispensable backyard mechanics who are willing to be called out on breakdowns at 9 am on a Sunday morning? If you happen to be equipped with an elaborate computercontrolled fuel injection system, then just try and sort that out mate.

## Quality Control

The whole elaborate procedure for the quality control of precision electronic equipment is now becoming of vital importance. If electronic products are to achieve the same reputation as earlier mechanical products, which appear to go on forever, it is necessary that they are produced to the same high standards. Electronic products properly tested can achieve very high levels of quality and reliability as any airline pilot or astronaut will testify. The term quality is used to express our level of satisfaction with either goods or a particular service which we use. The notion of quality becomes more ambiguous when we must express our satisfaction with a particular instrument after we have used it through several months. Even if the qualities noticed during the first few months have deteriorated, the product must remain within the specification during its useful life. The measurement of the deterioration of quality of a batch of instruments is when we start to examine the probability of failure or its reliability. A


Fig.1. The optimum reliability, considering the cost of the product and the cost of repair during the after-sales service period.
reliable instrument is one which maintains its performance throughout its useful life. A product's reliability can be defined within exact limits by the manufacturer and, naturally, the higher the product's reliability, the higher the price is. The reliability of an instrument is in the mathematical sense of the term - the probability of good functioning within clearly defined performances, in a given time period, under conditions of normal use. This reliability, in the form of probability, is expressed by the quotient of the number of instruments still working at the time of the test divided by the number of instruments initially put into service, when this latter tends towards infinity. The following formula can be used to calculate reliability:-
Reliability $=$ No. of instruments working correctly at time of test/No. of intruments initially put into service.

## Failure Rate

The other factor which is linked closely with reliability is the rate of failure. This parameter represents the speed with which the products cease to work correctly. The rate of failure in terms of time can be expressed graphically as a (bathtub) curve, which can be divided into three parts. The first part involves early failures which arise during the first few months. The second part involves random failures, with a constant rate of failure. No physical or chemical procedure can eliminate them and this is of prime importance to electronic products. The last part involves failures due to wear, signifying the end of a product's lifetime.

## Image Projection

The failures which occur during the first few months are particularly unwelcome, since they do much to tarnish a supplier's image. They are also very expensive to deal with. The reliability tests which a watch would need to undergo if we are to meet the requirements of the Swiss Industry Standards are divided into two categories:-

1. Performance and quality tests.
2. Accelerated life tests simulating wear.

## Testing Time

The example below is the type of performance that electronic watches must undergo if they are to reach an acceptable level of quality for the Swiss (and, indeed, Metac): Control for good functioning of all external controls accessible to the wearer, such as time setting, second stop, rapid corrector, etc; measurement of trimmer adjustment range in positive and negative areas; measurement of supply voltage at which the watch ceases to function correctly; measurement of current consumption and calculations of performance in terms of type of battery used; measurement of the performance deviation of the watch, expressed in seconds per day as a function of the supply voltage variation; determine the effects of temperature variation on the quartz crystal and the integrated circuit; measurement of the watch's resistance to thermal shocks and determination of the watch's resistance to magnetic fields.

Note: a watch can be termed anti-magnetic if it withstands without damage three passages in a magnetic field of 60 Oersted. A watch can be termed anti-shock if it withstands without damage two shocks corresponding to a fall from a height of one metre on a hard wood floor; the intensity of such a shock is around $5,000 \mathrm{~g}(1 \mathrm{~g}=$ unit of gravity acceleration).


Fig.2. The bathtub curve shows the rate of failure of a product in terms of time. 1. Early rate of failure; 2. Random failures, with a constant rate of failure;

## Hand-held Games

Electronic games have been with us now for the last three years and are continually growing in their sophistication. The early TV game chip with its four simple games proved to quickly become a bore and probably ended up in the bottom of the toy cupboard the day after boxing day. Space Invaders and the other microprocessor based games, which until now were only to be seen at fun-fairs and in the local pub, are soon to emerge as portable hand held games, which will easily fit into the Christmas stocking. The only viable way to produce really high technology microprocessor chips is in large volume. Once all the production problems are solved, the manufacturer starts to crank the handle and out spew millions of chips. Since rockets, machine tools, etc cannot consume very many chips in peace-time, the industry requires a volume product, which will soak up all this excess production.

## Software In Hand

Now that chip shortages (which probably held back this product last year) have been overcome, the relatively simple task of assembling hand-held games will ensure their success this Christmas in a big way. Over 500 different hand-held games are being produced. However, reports from the Far East indicate that only a small number are up to standard and will be acceptable to the UK market. Finding a suitable game, which does not quickly become a bore, is a major headache for designers. The chip manufacturers are Texas Instruments, AMI and General Instruments in the main and these companies expend a considerable effort in writing software for hand-held game microprocessors. It still remains a very high risk business, however, and manufacturers and importers will try hard to ensure that they do not have large stocks remaining after Christmas.

## Moving Pictures

Trends in hand-held games are in the direction of more LCD games than the LED type. These will last 20 to 30 hours compared to only three to five for LED ones. The use of fluorescent tube and larger memories are also expected developments. The drawback with LCD hand held games is that they must have a combination of driver and LCD display Companies in Hong Kong are working on this to produce the combination of chip and driver which makes players move on the display. The final touch will be a single chip direct drive microprocessor for LCD games. The standard type of LCD display has between 128 and 256 dots and the players and balls are mereblips on the screen. it is, however, hoped soon to produce a program of more than 600 dots and the LCD microprocessor will have drive capability with good resolu. tion. Hand-held game trends are also moving towards devices that produce sounds. An example of this is sound producing microprocessors, which produce musical sounds in toys and screeching wheels and engine sounds for toy cars.

## Tix

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the positively charged electrode thereby reducing its charge. The resulting fibre movement will be related directly to the quantity of radiation producing the ionisation, the fibre movement can thus be calibrated directly in roentigen units and the rate of movement of the fibre will be proportional to the roentgens received per unit time.

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shocks and deter magnetic fields.

Note: a watch can three passages in a magnetic field withstands without damage can be termed anti-shock if it of 60 Oersted. A warche two shocks corresponding to a fall from a height of one metre on a hard wood floor; the intensity of such a shock is around $5,000 \mathrm{~g}(1 \mathrm{~g}=$ unit of gravity acceleration).


Fig.2. The bathtub curve shows the rate of failure of a product in terms of time.
保 1. Early rate of tailure,

## Hand-held Games

Electronic games have been with us now for the last three years and are continually growing in their sophistication. The early TV game chip with its four simple games provertom quickly become a bore and probably ended up Space Invaders of the toy cupboard the day after boxing games, which until now and the other microprocen-fairs and in the local pub, are soon were only to be seen a hand-held games, which will easily fit into emerge as portable hand. The only viable way to produce to the Christmas $\begin{aligned} & \text { really high technology microprocessor chips is in large }\end{aligned}$ volume. Once all the production problems are solved, the manufacturer starts to crank the handle and out spew millions of chips. Since rockets, machine tools, etc cannot consume of chips. Since
very many chips in peace-time, the industry
product, which will soak up all this excess production.

## Software In Hand

Now that chip shortages (which probably held back this product last year) have been overcome, the relatively simple task of assembling hand-held games will ensure their success this Christmas in a big way. Over 500 depts from the Far East games are being produced. Humber are up to standard and will indicate that only a small number are up to sinding a suitable game, be acceptable to the l , which does not quickly manufacturers are Texas Instruments,
for designers. The chip m for designers. General Instruments in the main and these companies expend a considerable effort in writing software for hand-held game microprocessors. It still remains a very high risk business, however, and manufacturers and ocks remaining after Christmas.

## Moving Pictures

Trends in hand-held games are in the direction of more LCD games than the LED type. These will last 20 to 30 hour compared to only three to five for fluorescent tube and larger with LCD hand-held games developments. The drawback with LCD driver and LCD displa that they must have a combinatorking on this to produce th Companies in Hong Kong driver which makes players movec combination of chip and driver will be a single chip direct dri the display. The final LCD games. The standard type of LC microprocessor for 128 and 256 dots and the players a display has between on the screen. It is, however, hoped soon
balls are mere blips on produce a program of more than 600 dots and the L microprocessor will have drive capability with good resc tion. Hand-held game trends are also moving towards devi that produce sounds. An example of this is sound produc microprocessors, which produce musicaloy cars.
screeching wheels and engine sounds for toy cars.

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An F-14 wing-tip camera catches a glimpse of the first airborne launch of the new upgraded version of the Phoenix air-to-air missile,

## On Target

How does Wasp find its targets? Two sensors are under evaluation - infra-red and millimetre radar. Millimetre radar has three main advantages over infra-red. Its high resolution enables tanks to be distinguished from trees and buildings, it uses very small antennae and it is relatively unaffected by adverse weather conditions.

If a group of the missiles are fired at a number of targets, they will each attack a different target. If they can find only one target, it suffers a severe case of overkill. Wasp has a range of six miles when fired from an aircraft with a ground speed of 500 MPH . Two rival versions are under development by Boeing and Hughes.

## AIM To Kill

Earlier this year the US Navy's new AIM-54C Phoenix air-to-air missile was successfully launched from an airborne F-14. It intercepted a drone aircraft target, passing well within the 'kill' range, if the missile had been armed. The Hughes AIM54C, an improved version of the AIM-54A, carries a new digital electronics unit which is more flexible and reliable than the analogue unit it replaces. It also has a more effective target detector.

This first successful interception was achieved over a greater range than was possible with its predecessors. The F-14 launching aircraft travelled subsonically head-on towards the supersonic QF-4 fighter drone. In this launch, the Phoenix was guided on to the target by radar returns from the F-14's weapon control system. Closer to the target, it can switch to its own active radar system.

The upgraded Phoenix will become the US Navy's primary long-range air defence weapon in the 1990 s.

SHORTS

A spacesuit was destroyed by fire at the Johnson Space Centre in April. Fortunately there was no-one in the suit at the time, although a technician was badly burned. To avoid a recurrence, a review board has recommended several modifications to the high pressure oxygen system and seals.

GEOS-D, the latest in a series of Geostationary Operational Environmental Satellites, is due to join its two companions in Earth orbit as we go to press. The 12 feet high by seven feet in diameter spacecraft will be launched from Cape Canaveral on September 9th by a three stage Delta 3914 booster. Next month I hope to bring you an in-depth report on this latest weather satellite and the GEOS system.

In July's Digest we brought you the sad news that the Viking Lander 2's batteries had run out of juice. The latest news on the Viking population of Mars is that Viking Orbiter 1 has now reached the end of its supply of attitude control gas. Viking Lander 1 is the only member of the foursome that is still functional.

We now know that the first Space Shuttle launch has been postponed from November this year until at least March next year. Next month Astrologue will look into the political, financial and technical problems that have beset the Space Shuttle from the start.

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single byte instruction from the memory location given in the program counter; this takes three states. This is decoded and the processor sends, as an address, the contents of its H and L registers. The data word returned during this cycle is held in a temporary register inside the CPU and we have now used six states. The final act of adding the temporary register contents to the Accumulator takes a further state making seven in all, or two cycles. The longest operation of all, in 8080 code, takes 16 states or five machine cycles.
 Fig. 3 timing diagram showing the various states that can make up cycle: The vertical arrowed lines indicate information access states.

## The Ins And Outs

The final section of our look at the internals of a CPU is the connections you can make with the outside world. Cenerally, the CPU is housed inside a DIL package with some 40 legs. Under normal circumstances, assuming the standard eight bit CPU, we will have 16 pins for the address bus, eight pins for the data bus and 16 pins left to play with. Just what you do with them depends on the kind of CPU you have, but let's take a close look at the pins on an 8080 .

Having already mentioned the address and data bus, we only need to say that the data bus is a bi-directional system and is capable of tri-state operation. It can assume a high impedance state, which is neither a logic zero nor one and this is used under some special circumstances, which will be mentioned next month. Four further legs can be allocated to power; the device needs $\pm 5$, the required two phase clock, more legs can be allocated to trol signals to communicate the state of the device to the outside world. These are SYNC, DBIN, WAIT, HLDA, INTE, READY, HOLD, INT and RESET. Taking these in order, the SYNC indicates the first state of each machine cycle, thus acting as a synchronisation signal, hence the name. The DBIN signal tells the outside world that the CPU can accept data. It should be used to externally enable the
transfer. WAIT is an indication that the CPU has entered a WAIT state, triggered by pulling the READY line low before the second state time. This causes extra states to be added to the cycle time for as long as the READY line is held low. The process is often used in situations where the memory or device currently being accessed is slower than the processor.

Our next signal, WR, is provided for the synchronisation of external transfers. These include memory and I/O operations and it is the converse of DBIN. There now follows a group of controls, which are concerned with things called interrupts. An interrupt is the computer equivalent of a tap on the shoulder and is used by peripheral devices to tell the processor that they are ready to be looked at. The INT line must be set high to tap the computer on its shoulder, but this will ony work if the INTE line has been enabled previously. Inside the CPU, the interrupt is signalled by a status bit being set and the external device must put its instruction onto the bus in order for any action to be taken. The HOLD line is concerned with direct memory access and as such we shall not dwell on this until next month. The HLDA is merely an indication that the CPU is in a HOLD state. Finally we have the RESET line which, as its name implies, does. The signal will restore the CPU to the first state of a machine cycle and it also clears the program counter. It is essential to start all the power up sequences with this signal otherwise you never know what you may find yourself doing! It is also worth noting for all those sceptics among you that pressing RESET does not destroy all your registers, it merely sets you back to the beginning without destroying your program unless the person who programmed the monitor on your system clears the memory as the first operation. Whoever said that programmers were logical anyway.


Pin designations of the $\mathbf{8 0 8 0}$. Developed by Intel, fathers of the micro, it is s regarded as the workhorse of eight bit processing It also spalogy. probably the most powerful eight bit chip using current tecto.gy.

## Coming Soon

Next month's slice of bits will investigate the thorny th of memory devices and show you the way in the ROM-R jungle as well as telling you how to ignore your CPU altoge and really make things work fast.

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