

POWER PACKED — by POWERTRAN

Powertran's black boxes are packed with punch. Not only are they superb kits to buy and build they really do the job! Imaginative and ingenious design goes hand in hand with top quality materials and outstanding performance capability. With their smart black styling the kits harmonise visually as well as musically.

Your can built each unit independently for its set task and then gradually increase your array

until you have a complete bank of formidable controllable power.



Complete Kit - £49,90 + VAT



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100W amplifier. Its smart styling, professional appearance and performance, make it one of our most popular designs. With adaptable inputs the mixer accepts a variety of sources yet straightforward construction makes it ideal for the first-time builder. CHROMATHEQUE 5000

MPA 200 is a low price, high power

5-channel lighting system powerful enough for professional discos yet controllable for home-effects. Sound to light, strobe to music level, random or sequential effects - each channel can handle up to 500W yet minimal wiring is needed with our unique single-board

ETI VOCODER — 14 channels, each with independent level control, for maximum versatility and intelligibility; Two input amplifiers - for speech/excitation each with level control and tone control. The Vocoder is a powerful yet flexible machine that is interesting to build and thanks to our easy to follow construction manual, is within the capability of most enthusiasts.

SP2 200 twice the power with two of the reliable, durable and economic amps from the MPA200; fed by separate power supplies from a common toroidal transformer. Superb finish and quality components throughout – up to (even over!) the standard of high priced factory-built units.



Complete Kit - £97.50 + VAT





Digital Delay Line - our latest kit! With its ability to give delay times from 1.6 mSecs to up to 1.6 secs. Many powerful effects including phasing, flanging, A.D.T., chorus, echo & vibrato are obtained. The basic kit is extended in 400 mS steps up to 1.6 secs. Simply by adding more parts to the PCB. Comparewith units costing over £1,000! Complete kit (400 mS delay) £135. Parts for extra 400 mS delay £9.50p.





WORLD LEADERS IN ELECTRONIC KITS

- Money Back Guarantee If you are not completely satisfied with your Powertran Kit return it in original condition within 10 days for full refund.

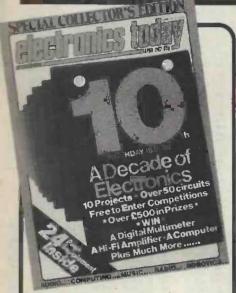
 Free Soldering Practice Kit To assist the beginner we will supply, on request with your first kit order, a free soldering practice kit with useful tips and
- illustrations.

 © Component Packs Most kits are available as separate packs (e.g. PC8 component sets, hardware sets etc). Prices in our FREE catalogue.
- Ordering Full ordering details, delivery service, and sales counter opening outside back of this issue.

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ITERNATIONAL APRIL 1982 VOL 11 NO 4



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ROBOT CONTROLLER PART 2 94 For producing PWM



SOLID STATE REVERB101 It's great-eat-eat-eat CAPACITANCE METER PART 2 108 We conclude with the construction SOUND EFFECTS 2118 Steam train and whistle GUITAR PRACTICE AMP121 Cheap, and keeps your neighbours cheerful FOIL PATTERNS This is where our boards find lodging

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We stock thousands more items. It pays to visit us. W Nearest Underground/BR Station: Watford High Stre Open Monday to Suturday: 9.00am to 6.00pm. Ample from the Company of the Company o	RD, HERTS, ENGLAND RS WELCOME 3. Telex: 8956095 D FULLY GUARANTEED. ORDERS DE IMS OF BUSINESS: CASH/CHEQU VERNMENT AND EDUCATIONAL INS ADE AND EXPORT INQUIRY WELCON LETT. OVERSEAS ORDERS POSTAGE. COME. K. Customers only. Unless stated otherwise, 15% to the total cost including p8p. (e are situated behind Watford Footbell Grounel. Lett. Order Linking space aveilable. (i) 10 52p; 4778p; 63V: 0.47, 1.0, 1.5, 2.2, 3.3 gp; 1000 70p. 50V: 47 12p; 68 20p; 220 24p; 10p; 25V: 1.5, 68 10, 22 8p; 33 pp; 47 8p; 1001 2700, 50p; 3300, 78p; 4700 92p; 16V: 40.47, 100, 31p; 2200 38p; 3300 74p; 4707 9p; 16V: 40.47, 100, 31p; 2200 38p; 3300 74p; 4707 9p; 16V: 40.47, 100, 31p; 2200 38p; 3300 74p; 4707 9p; 16V: 40.47, 100, 31p; 2200 38p; 3300 38p; 300 154p; 22 22n 12p; 33n, 47n, 68n p; 220 23p; 16V: 40.47, 100, 31p; 2200 38p; 3300 79p; 470, 500; 38p; 300 154p; 22 250V 100CPF/450V 100CPF/450	E	1.	MPSU06 55 MPSU06 55 MPSU05 60 MPSU156 60 MPSU156 60 MOSU56 60 MPU131 52 OC26 170 OC28/35 130 OC36/41 120 OC46/41 120 OC46/77 50 OC76/77 50 OC16/77 50 OC16/77 50 OC16/77 50 OC76/77 50 OC76	2 2100 74279 90 LS22 15 LS195	185 1990 2225 74 190 112 112 112 1130 130 130 130 130 120 140 140 150 160 170 170 180 170 170 175 185 195 195 195 195 195 195 195 195 195 19
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20 way 40p PLUGS Centronic parall TRANSFORMERS: Prim. 240V 6-0-6V; 9-0-9V; 12-0-12V 100m A 99p pob mounting, Miniature, Split Bobbin 3VA; 2x6V-0-25A; 2x9V-0.15A; 2x12V-0.12A; 2x15V-0.14 200p 8VA; 2x6V-0.5A; 2x9V-0.3A; 2x12V-0.25A; 2x15V-0.25A; 2x9V-0.3A; 2x12V-0.25A; 2x15V-0.5A; 2x9V-0.4A; 2x12V-0.3A; 2x15V-0.5A; 2x9V-0.4A; 2x12V-0.3A; 2x15V-0.5A; 2x15V-0.4A; 2x20V-0.3A; 2x15V-0.5A; 2x15V-0.4A; 2x20V-0.3A; 2x12V-0.5A; 2x15V-0.4A; 2x20V-0.3A; 2x12V-0.5A; 2x15V-0.4A; 2x20V-0.3A; 2x15V-0.5A; 2x15V-0.4A; 2x20V-0.3A; 2x15V-0.5A; 2x15	VOLTAGE REGUL 1A TD3 metal cast SV 7805 145p 12V 7815 145p 18V 7818 145p 18V 7818 145p 12V 7815 50p 18V 7815 50p 18V 7816 30p 8V 78162 30p 8V 78162 30p 12V 78112 30p 15V 78115 30p 15V 78115 30p 15V 78115 30p 15V 78115 30p	y 170p 250p 130p 130p 130p 130p 130p 130p 130p 13	500 pins 325p 28 w 28	SOCKETS 24 avy 820p: 40 25 wey 'D' CONNECTO Plug Pins 200p angle 210p atock many more Plugs Jumper Leads. avy 'D' CONNECTOR uper Lead Cable Assemt orig, Single End, Male orig, Single End, Male orig, Single Ended, M/r orig, Double Ended, M/r Annex SOLDERING III MY 420p: CX1	Socket 246p 275p 375p 560p 570p 1316p 1275p	6 185 MHz 300 5 242 288 380 6.1 44 MHz 240 6.5 53 6 MHz 200 7. 168 MHz 200 7. 168 MHz 200 8.8 87 23 MHz 200 10.2 4 MHz 200 12.0 MHz 200 12.0 MHz 200 12.0 MHz 200 13.0 MHz 200 13.0 MHz 200 13.0 MHz 200 13.0 MHz 200 27. 14 SM 200 27.	BUZZERS, miniature, solid-state 60; 9V & 12V 70p LOUGEPEAKERS Miniaturs, 0.3W: 8th 2in, 3 k in, 2 k in, 3in 80p 2 Win 40ti, 6411 or 80th 80p 2 Win 40ti, 6411 or 80th 80p 2 Win 40th 80p 2 Win 40th 80p 2 Win 40th 80p 2 Win 40th 80p 8 Bencher Posone, 8tt. Ideal for use in 8 osts, Caravans etc. 1 yes: TOSS12 & 813 525p Socket for above 40p ASTEC UHF MODULATORS Standard 6MHz Widebend 8MHz 425p ETI Autoranging Digital Cepacitance Meter, Ali parts available.
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Sinclair ZX81 Personal Comp the heart of a system that grows with you.

1980 saw a genuine breakthrough – the Sinclair ZX80, world's first complete personal computer for under £100. Not surprisingly, over 50,000 were sold.

In March 1981, the Sinclair lead increased dramatically. For just £69.95 the Sinclair ZX81 offers even more advanced facilities at an even lower price. Initially, even we were surprised by the demand – over 50,000 in the first 3 months!

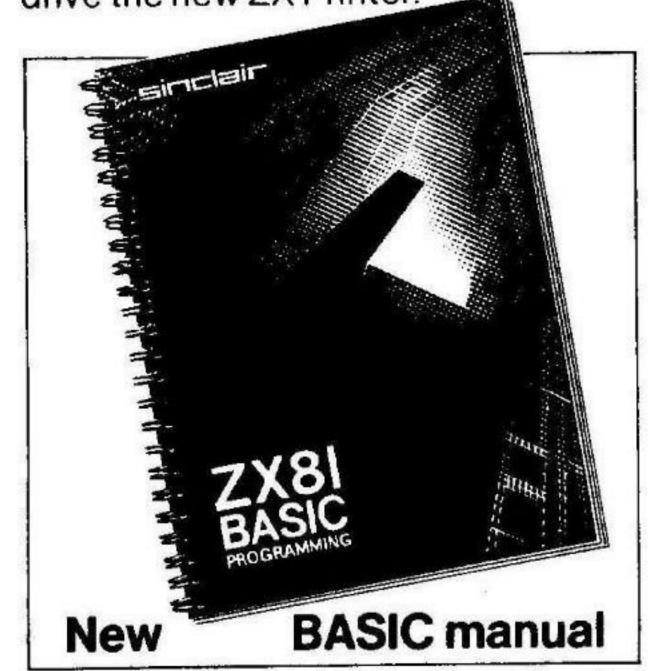
Today, the Sinclair ZX81 is the heart of a computer system. You can add 16-times more memory with the ZX RAM pack. The ZX Printer offers an unbeatable combination of performance and price. And the ZX Software library is growing every day.

Lower price: higher capability
With the ZX81, it's still very simple to
teach yourself computing, but the
ZX81 packs even greater working

capability than the ZX80.

It uses the same micro-processor, but incorporates a new, more powerful 8K BASIC ROM – the 'trained intelligence' of the computer. This chip works in decimals, handles logs and trig, allows you to plot graphs, and builds up animated displays.

And the ZX81 incorporates other operation refinements – the facility to load and save named programs on cassette, for example, and to drive the new ZX Printer.



Every ZX81 comes with a comprehensive, specially-written manual – a complete course in BASIC programming, from first principles to complex programs.

Kit: £49.95

Higher specification, lower price – how's it done?

Quite simply, by design. The ZX80 reduced the chips in a working computer from 40 or so, to 21. The ZX81 reduces the 21 to 4!

The secret lies in a totally new master chip. Designed by Sinclair and custom-built in Britain, this unique chip replaces 18 chips from the ZX80¹

New, improved specification

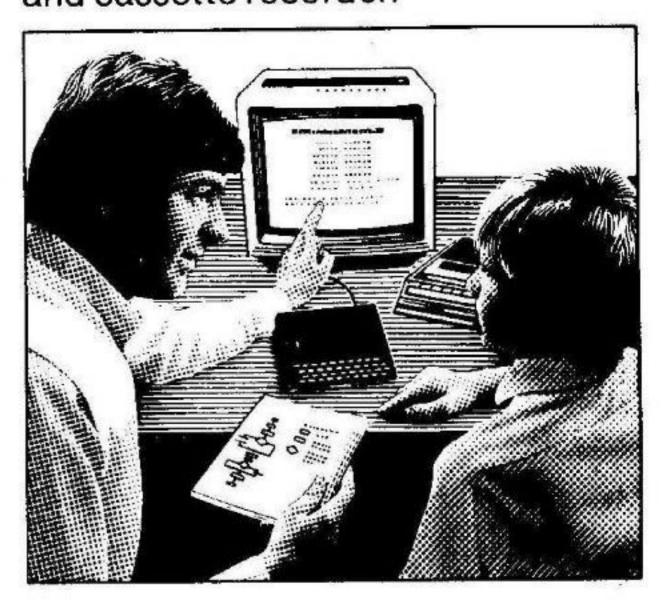
- Z80A micro-processor new faster version of the famous Z80 chip, widely recognised as the best ever made.
- Unique 'one-touch' key word entry: the ZX81 eliminates a great deal of tiresome typing. Key words (RUN, LIST, PRINT, etc.) have their own single-key entry.
- Unique syntax-check and report codes identify programming errors immediately.
- Full range of mathematical and scientific functions accurate to eight decimal places.
- Graph-drawing and animateddisplay facilities.
- Multi-dimensional string and numerical arrays.
- Up to 26 FOR/NEXT loops.
- Randomise function useful for games as well as serious applications.
- Cassette LOAD and SAVE with named programs.
- 1K-byte RAM expandable to 16K bytes with Sinclair RAM pack.
- Able to drive the new Sinclair printer.
- Advanced 4-chip design: microprocessor, ROM, RAM, plus master chip – unique, custom-built chip replacing 18 ZX80 chips.



Kit or built - it's up to you!

You'll be surprised how easy the ZX81 kit is to build: just four chips to assemble (plus, of course the other discrete components) – a few hours' work with a fine-tipped soldering iron. And you may already have a suitable mains adaptor – 600 mA at 9 V DC nominal unregulated (supplied with built version).

Kit and built versions come complete with all leads to connect to your TV (colour or black and white) and cassette recorder.





16K-byte RAM pack for massive add-on memory.

Designed as a complete module to fit your Sinclair ZX80 or ZX81, the RAM pack simply plugs into the existing expansion port at the rear of the computer to multiply your data/program storage by 16!

Use it for long and complex programs or as a personal database. Yet it costs as little as half the price of competitive additional memory.

With the RAM pack, you can also run some of the more sophisticated ZX Software – the Business & Household management systems for example.

Sinclair ZX8I

6 Kings Parade, Cambridge, Cambs., CB2 1SN. Tel: (0276) 66104 & 21282.

Designed exclusively for use with the ZX81 (and ZX80 with 8K BASIC ROM), the printer offers full alphanumerics and highly sophisticated graphics.

A special feature is COPY, which prints out exactly what is on the whole TV screen without the need for further intructions.

At last you can have a hard copy of your program listings - particularly

How to order your ZX81

BY PHONE - Access, Barclaycard or Trustcard holders can call 01-200 0200 for personal attention 24 hours a day, every day. BY FREEPOST - use the no-stampneeded coupon below. You can pay And of course you can print out your results for permanent records or sending to a friend.

Printing speed is 50 characters per second, with 32 characters per line and 9 lines per vertical inch.

The ZX Printer connects to the rear of your computer – using a stackable connector so you can plug in a RAM pack as well. A roll of paper (65 ft long x 4 in wide) is supplied, along with full instructions.

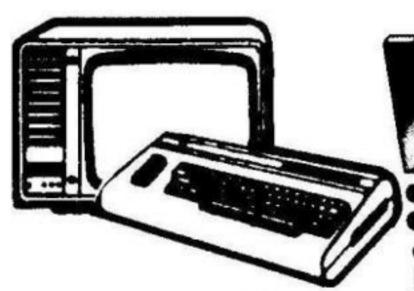
by cheque, postal order, Access, Barclaycard or Trustcard. EITHER WAY – please allow up to 28 days for delivery. And there's a 14-day money-back option. We want you to be satisfied beyond doubt – and we have no doubt that you will be.

Oty	Inclair Research Ltd, FREEPOST	, campeney, surrey, de	Code	Item price	Ordel Total £
-	Sinclair ZX81 Personal Compu ZX81 BASIC manual, excludes	ter kit(s). Price includes mains adaptor	12	49.95	
	Ready-assembled Sinclair ZX Price includes ZX81 BASIC ma	B1 Personal Computer(s). Inual and mains adaptor.	11	69.95	
	Mains Adaptor(s) (600 mA at 9	V DC nominal unregulated).	10	8.95	
	16K-BYTE RAM pack		18	49.95	
	Sinclair ZX Printer.		27	49.95	
	8K BASIC ROM to fit ZX80.		17	19.95	100
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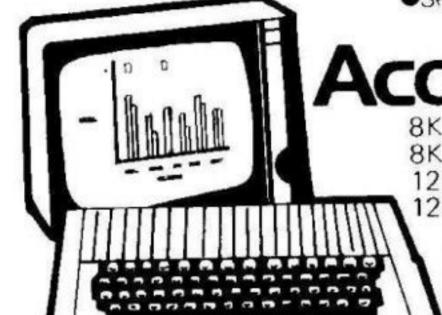


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FOR ALL BUSINESS SYSTEMS **ENQUIRIES:**-Phone Nick Rosenberg on Hastings (0424) 426844

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15 CASTLE STREET, HASTINGS, EAST SUSSEX TN34 3DY DEPT. ET4

NEWS:NEWS:NEWS:NEWS:NEWS:NEWS

DIGEST

ETI PRICE DECREASE

Readers will have no doubt noticed (painfully!) the cover price increase on this issue of ETI. We apologise for this, but are happy to say it is ONLY FOR THIS ISSUE and the price returns to 75p with the May issue.

The one-month jump was made necessary by the sheer size of this special issue. We hope you will agree it is worth it. If you could see the price of paper these days ... (moan,

Thank you for sticking with us through thick and thin... (and 10p!)

Tempus Fugit

It's felt a little uncomfortable working in the ETI office this month; must be something to do with the sackcloth and ashes we're wearing. During the last few issues several of our reviews have featured Casio products, but we have consistently failed to credit the company which lent us the review models. The kindly folk in question are Tempus of 38 Burleigh Street, Cambridge CB1 1DG and we'd like to thank them for all the help they've been giving us. Tempus are leading Casio specialists and if there's something from Casio you're having problems obtaining, they will doubtless be as nice to customers as they are to us.

Sun-Day Driving

A Volkswagon Dasher car is presently being tested carrying a roof-rack of AEG-Telefunken solar modules which convert solar energy directly into electric current. The small 160 W 'solar power plant' of the test car complements the dynamo and charges the battery. This means that fuel consumption can be reduced by approximately five percent. As yet the cost of manufacturing these solar panels makes them uneconomical to use, but with the rising prices of fuel, it is foreseeable that low-priced solar generators will enter the market. Not only that, future car generations will make increased use of electricity, for example with automatic startstop devices and pollution-free electrical energy for air conditioning in cars in warm countries. Great idea - but where will you put the luggage?



Tweeters That Go Cheap

Well, not just the tweeters, in fact. Mullard have a 40 W speaker system consisting of an 8" woofer as well as a high-power textile dome tweeter. They form part of a new low-price, two-way, self-build audio kit (whew!) being marketed by BK Electronics. The

BK Electronics crossover unit have been combined with spring-loaded terminals and recessed mounting panel. The complete system, when built into the 23 litre enclosure, is capable of handling 40 W comfortably. All this for the small outlay of £13.90 plus VAT and £1.50 carriage per kit! Get yours now from **BK Electronics Ltd, 37 Whitehouse** Meadows, Eastwood, Leigh-On-Sea. Essex SS9 5TY.



Heading For The | Electroware, Top

Headphones seem to be getting lighter and smaller these days, so Sennheiser, that well-known manufacturer of headphones, has decided to launch a pair of their own lightweight 'phones. The new model HD40 is soon to be released in the UK and weighs only 60 grammes with extremely light contact pressure. They can be supplied with either a three or seven metre lead, the seven metre variety incorporating a volume control in the lead so that you don't have to march all that way back to the amp if it's too loud. Another feature is that each ear-piece can be revolved on the headband by 90 degrees if you have a funny shaped head or if you want to store them compactly (!). The Sennheiser HD40 will be launched in the UK with a suggested selling price, including VAT, of £16.55. For those of you interested in technical specs; frequency response is 22 to 18,000 Hz, impedance is 600 ohms, characteristic SPL is 90 dB and distortion factor < 1.2%.

OK?

K Machine and Tool (UK) Ltd have launched a new division aimed at providing the electronics user with a really wide range of electronic hardware. All the products in the range will be available to everyone involved in building electronic equipment - that includes engineers, students, teaching staff, laboratory technicians and, not least, the hobbyist. The 40-page catalogue contains orious products selected from OK's bench tool range — plus some new items — and includes soldering irons, wire-wrapping kits, IC tools, PCBs, cases, enclosures, connectors, sockets and test instruments to name just a few. Electroware is distributed throughout the UK by leading electronic and computer stores. Catalogues are free, but send 30p for postage and packing. If you want any further information or one of their catalogues contact OK Machine & Tool (UK) Ltd, Dutton Lane, Eastleigh, Hants SO5 4AA.

Lack of ZX81 memory giving you headaches.?



The Memotech 64K Memopak

The growth of interest in computer use caused by the introduction of the Sinclair ZX81 has made new and exciting demands on the ingenuity of electronic engineers. At Memotech we have focused our attention on the design of an inexpensive, reliable memory extension.

The Memopak is a 64K RAM pack which extends the memory of the ZX81 by a further 56K. Following the success of our 48K memory board the new memory extension is designed to be within the price range expected by Sinclair users. It plugs directly into the back of the ZX81 and does not inhibit the use of the printer or other add-on boards. There is no need for an additional power supply or for leads.

The Memopak together with the ZX81 gives a full 64K, which is neither switched nor paged, and is directly addressable. The unit is user transparent and accepts such basic commands as 10 DIM A(9000)

0-8K ...Sinclair ROM

8-16K...Memopak memory which can switch in or out in 4K blocks to leave space for memory mapping.

12-16K...Memopak memory which holds its contents during cassette loads and allows communication between programmes.

16-32K...This area can be used for basic programmes and assembly language routines.

32-64K...32K of RAM memory for basic variables and large arrays.

With the Memopak extension the ZX81 is transformed into a powerful computer, suitable for business, leisure and educational use, at a fraction of the cost of comparable systems.



Memotech Ltd 3 Collins Street Oxford·OX4 1XL Tel·722102/3/4/5

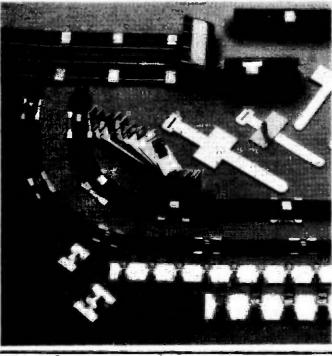
Please debit my BARCLAYCARD/ACCESS* account number:	Please rush me: 64K RAM, Assembled	Quantity	Price Tot	al
*Please delete whichever does not apply. Signature				+
Date	Stock Control Programme Payroll Programme		£ 25.00 £ 25.00	+
NAME		VAT	@ 15%	
To: Memotech Ltd., 3 Co	lins Street, Oxford, OX4 1XL	_ETI TO	OStage £2.0 OTAL (0865) 7221	_

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High-res Printing

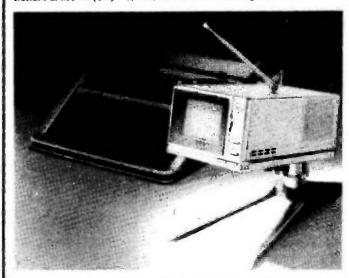
ew from Hi-Tek is the Facit 4542, a high-speed, highresolution printer which combines a new type of 'Flexhammer' printhead with advanced microprocessor control to make it equally suited to text printing, label or bar code production, and graphics output. Using 260-character-persecond bidirectional two-colour printing and a 14 x 9 dot-matrix format, the 4542 can produce a virtually unlimited range of characters as well as different grey scales in graphics applications. In normal text-printing applications, the 4542 features proportional spacing, justified right-hand margin and an extensive set of up to 512 characters in 11 national repertoirs with red/black, elongated and underlining facilities. For label printing, a variable-size option is

available which allows characters or bar codes to be generated in 95 different sizes from 2.52 mm up to 240 mm. Selection of size and position is easily controlled by software commands. In the graphics mode, scanning, semi-graphics and 10 levels of grey/red scale are available to illustrate reports with histograms, curves and diagrams, as well as generating half-tone illustrations in applications such as tomography, process monitoring and computer-aided design. The key to the versatility of the 4542 is the print-head, which consists of a set of nine stored-force flexible metal hammers mounted directly on a magnet armature. No adjustment or lubrication is necessary, wear is minimal, and a 'floating' mount means that the correct paper/print-head distance is always maintained irrespective of the paper thickness or number of copies. Further information is available from Hi-Tek Distribution Limited, Trafalgar Way, Bar Hill, Cambridge, CB3 85Q.



Small And Beautiful

ailed as 'the World's Smallest, Lightest and Lowest Power Consumption' television, the TH3-W3V from Matsushita certainly caught our editorial eye. Closer inspection revealed a colour TV set with a 3" colour picture tube, only 115 mm x 86 mm x 323.5 mm in size and 1.5 kg in weight. Power consumption is a mere 9.5 W and it operates on AC power, car batteries and on optionally available rechargeable batteries. Yet, despite its small size, it is equipped with video input/output terminals and operates as a colour monitor and a video tuner when connected to a video camera and a portable VTR, respectively. This 3" colour TV was faunched on to the Japanese market in mid-December 1981 at the approximate price of £200. It is due for launch in the U5 in June this year and, hopefully, will be seen in this country shortly after. Further details will be supplied by National Panasonic (UK) Ltd, 300/313 Bath Road, Slough SL1 6JB.



Sticky Clips

randauer adhesive cable clips from Stotron provide an inexpensive method of fixing round or ribbon cables to clean, dry surfaces. The range can handle round cables from just a few millimeters up to 19 mm and flat ribbon cables from 13 mm to 75 mm can be accommodated by a selection of clips with widths in stages of 6 mm. The adhesive is instant acting and polyethylene pads provide high levels of insulation, where necessary. Further information is available from Stotron Ltd. Unit 1, Haywood Way, Ivyhouse Lane, Hastings, East Sussex.

Video Victory

Thorn EMI have just announced that agreements have been signed with Telefunken and JVC to form a holding company for the manufacture of video consumer electronics products in Europe. Thomson-Brandt was originally intended as a fourth partner, but this was not possible. However, the three other parties hope an opportunity will arise for Thomson-Brandt to join the venture.

Products manufactured by the joint venture will include VHS video cassette recorders, VHD video disc players and video cameras.

BT Bill Beater

ollowing the success of the Telcost TNA25 from the Ansafone Corporation, it was decided that a single line unit should be manufactured. The new machine offers a range of functions which are all designed to save money by monitoring telephone use. Ansafone's single line Telcost 1 has features including a 24-hour clock display, which instantly shows the cost of a call as soon as a user is connected with a number dialled. The unit also has a built-in printer which records details of the call including cost and number dialled. It also prints out the date, time, machine identification number and the duration of the call. Telcost 1 has a built-in memory which retains information even if the machine is disconnected from a power source. It also gives a special security midnight printout each night which frustrates any attempts to conceal the day's telephone costs by the destruction of the daily printout sheet. The machine is virtually tamper-proof as the printout will indicate if it has been disconnected from the line at any time or if any information parameters have been changed. The machine has provision for it to be reprogrammed at any time to enable the user to keep in line with British Telecom unit rate charges and the date, time and identification number can be changed for any reason if the machine is moved to a new location. This desk-top unit is no bigger than a telephone and for an investment of around £249 could help to cut out the abuse of telephones in both large and small companies.



FRAPIC FRAPIC Tel: 0322 863494 Hillcroft House Station Road Eynsford, Kent DA4 0EJ





		Eynsford, Kent	DA4 0EJ
LINEAR CA3162E 450 LM377 150 LM3900 50 NE ★709 25 CA3189E 290 ★LM380 65 LM3909 70 NE ★741 14 ICL7106 790 ★LM381 100 LM3911 120 NE 748 35 ICL8038 320 LM382 120 ★LM3914 200 RC AY-3-1270 840 ICM7555 80 ★LM386 65 ★LM3915 200 SN AY-3-8910 700 ★LF351 40 LM387 120 LM13600 120 SN AY-3-8912 LF353 85 LM393 100 MC1310 150 IB 625 LF356 90 ★LM709 25 MC3302 150 IB CA3046 60 LM10 395 LM710 50 MC3340 135 IB CA3089 215 LM311 70 LM733 75 NE529 225 TB CA3190AQ 375 LM318 85	566 150 TAD1024 125 567 100 TLO71 45 571 425 TLO72 75 4136 90 TLO84 90 76018 150 XR2206 300 76477 150 ZN414 100 A641B11250 ZN423 195 A800 80 ZN424 135 A810 95 ZN425E 390 A820 80 ZN426E 330 A950 290 ZN426E 330 A950 290 ZN427E 650 A940 170 ZN428E 480 A1004 300 ZN1034E 200 A1008 320 A1010 225 A1022 560 4503 50 4532 95 4507 38 4534 495 4508 200 4538 110 4510 65 4543 110	An ideal opportunity for the beginner or the experienced constructor to obtain a wide range of components at reduced prices. WW 5% Resistor Kit. Contains 10 of each value from 4.7Ω to 1M (650 resistors) 480p. Ceramic Capacitor Kit. Contains 5 of each value from 22p to 0.01 (135 caps.) 370p. Polyester Capacitor Kit. Contains 5 of each value from 0.01 to 1uF (65 caps.) 575p each. Preset Kit. Contains 5 of each hor. Value from 100Ω to 1M (total 65 presets). 425p each. Nut and Bolt Kit. Total 300 items. 140p. 25 6BA ½" bolts 25 4BA ½" bolts 25 6BA ½" bolts 50 6BA nuts 50 6BA nuts 50 6BA nuts 50 6BA washers	Switches Submin. Toggle SPST 55p SPDT 60p *DPDT 50p Miniature toggle SPDT 80p SPDT centre off 90p DPDT 90p DPDT centre off 100p Standard toggle SPST 35p DPDT 48p * Miniature DPDT slide 12p * Push to make 12p Push to break 22p Rotary type adjustable stop 1P12W 2P6W, 3P4W, 4P3W all 55p each DIL switches 4 SPST 80p 6 SPST 80p 8 SPST 100p REGULATORS Positive * 78L05 25 79L05 65 78L12 30 79L05 65
4006 65 4022 70 4043 60 4067 395 4094 14 4007 17 4023 18 4044 65 ± 4068 15 4095 99 4008 58 4034 40 4046 70 4069 18 4097 34 4009 30 4025 18 4047 70 4070 18 4098 8 4010 35 ± 4026 96 4048 55 4071 18 4099 9 ± 4011 13 4027 30 ± 4049 28 4072 18 40106 5 4012 17 4028 55 4050 28 4073 20 40109 10 ± 4013 22 4029 75 4051 60 4075 20 40163 10 4014 60 4030 35 4052 70 4076 60 40173 10 4015 60 4031 170 4053 60 4077 25 40175 10 ± 4016 22 4034 170 4054 110 4081 18 40193 12	0 4512 70 4553 295 0 4514 180 4555 45 5 4515 180 4556 48 6 4516 75 4559 390 0 ★4518 45 4560 180 0 4520 70 4584 45 0 4521 200 4585 99 0 4526 80 4724 140 0 4527 90	CAPACITORS Polyester. Radial Leads. 250V 280 type. 0.01, 0.015, 0.022, 0.033, 6p; 0.047, 0.068, 0.1, 7p; 0.15, 0.22, 9p; 0.33, 0.47, 13p; 0.68, 20p; 1u 23p. Electrolytic Radial or Axial leads. 0.47/63V, 1/63V, 2.2/63V, 4.7/63V, 10/25V, 7p; 22/25V, 47/25V, 8p; 100/25V, 9p; 220/25V, 14p; 470/25V, 22p; 1000/25V, 30p.	78L 15 30 79L 15 65 ★ 7805 45 ★ 7905 45 ★ 7812 45 ★ 7912 45 7815 60 7915 60 LM309K 130 ★ LM323K 350 ★ LM317T 120 ★ LM723 40 PANEL METERS Sixe 60 × 46 × 35mm.
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LS TTL LS21 15 LS76 20 LS125 30 LS161 42 LS22 16 LS78 24 LS126 30 LS162 42 LS00 13 LS26 18 LS83 50 LS132 45 LS163 42 LS01 14 LS27 15 LS85 70 LS136 30 LS164 50 LS02 14 LS30 16 LS86 25 LS138 35 LS165 120 LS03 14 LS32 16 LS90 35 LS139 35 LS166 85 LS04 15 LS37 16 LS92 38 LS145 75 LS170 170 LS05 15 LS38 16 LS93 35 LS145 75 LS170 170 LS08 16 LS40 16 LS93 35 LS147 160 LS173 70 LS08 16 LS40 16 LS95 45 LS148 95 LS174 60 LS109 16 LS42 38 LS96 110 LS151 40 LS175 60 LS10 16 LS47 40 LS107 45 LS151 40 LS175 60 LS10 16 LS48 80 LS109 30 LS154 120 LS190 55 LS11 16 LS48 80 LS109 30 LS154 120 LS191 55 LS12 15 LS51 16 LS112 30 LS155 45 LS192 55 LS13 25 LS55 30 LS113 30 LS156 45 LS193 60 LS14 48 LS73 25 LS113 30 LS156 45 LS193 60 LS15 15 LS74 25 LS12 42 LS158 36 LS196 60 LS20 15 LS75 27 LS123 55 LS160 42 LS197 68	LS221 60 LS365 38 LS240 90 LS366 38 LS241 80 LS367 38 LS242 80 LS368 50 LS243 85 LS373 80 LS244 80 LS374 80 LS245 120 LS375 50 LS247 75 LS377 90 LS251 40 LS378 70 LS257 48 LS390 75 LS258 45 LS393 75 LS259 95 LS399 220 LS266 25 LS541 135 LS273 90 LS670 175 LS283 45 LS283 45 LS283 45 LS353 100	0-12, 0-12V @ 1A, 0-15, 0-15V @ 0.8A; 330p each (plus 60p carriage) Single 3 50VA 0-12, 0-12V @ 2A, 0-15, 0-15V @ 1.5A; 400p each (plus 70p carriage) Log or L 100VA 0-30, 0-30V @ 1.6A	Carbon track Log
AC125 35 ★BC159 8 BCY71 18 BFX85 25 TIP30A AC126 25 BC160 45 BCY72 18 BFX87 25 TIP30C AC127 25 BC168C 10 BD115 80 BFX88 25 TIP31A AC128 20 BC169C 10 BD131 35 BFY50 23 TIP31B AC176 25 BC170 8 BD132 35 BFY51 23 TIP31C AC187 22 BC171 10 BD133 50 BFY52 23 TIP32A AC188 22 BC172 8 BD135 50 BFY52 23 TIP32B AC188 22 BC172 8 BD135 50 BFY53 32 TIP32B AD142 120 BC177 18 BD136 30 BFY55 32 TIP32B AD142 120 BC177 18 BD136 30 BFY55 32 TIP32B AD149 80 BC178 18 BD137 30 BFY56 32 TIP32C AD149 80 BC178 18 BD138 30 BFY56 32 TIP33A AD161 40 BC179 18 BD138 30 BFY56 32 TIP33C AD162 40 BC182 10 BD139 35 BSX20 20 TIP34A AF124 60 ★BC182 10 BD139 35 BSX20 20 TIP34C AF126 50 BC183 10 BD204 110 BSY95A 25 TIP35C 14 AF139 40 BC183L 10 BD206 110 BU205 160 TIP35C 14 AF186 70 BC184 10 BD222 85 BU206 200 TIP36A 15 AF186 70 BC184 7 BF180 35 BU208 170 TIP36C 15 AF180 70 BC184 7 BF180 70 BC184 7 BC184	0 2N708 20 2N3866 90	New Telephone Order Service Now ordering from Rapid is even easier. Just telephone 0322 863494 with your requirements and your Access or Visa number for immediate despatch. Nothing could be more simple!	SOLDERING IRONS Antex CX 17W Soldering Iron 2 3mm and 4.7mm bits to suit 55p CX 17W element 190p Antex X25 25W Soldering Iron 3.3mm and 4.7mm bits to suit 55p X25 25W element 50lder pump desoldering tool 5pare nozzle for above 10 metres 22 swg solder TRIACS + SCRS
BC107B 10 BC212L 10 BF184 25 MJE340 50 TIP42A	45 2N2907 25 40362 50 75 2N2907A 25 40408 70 85 2N2926 9 40594 100	* 3mm green 12	SCRs C106D 30 400V 4A 60 400V 8A 70 400V 8A 70 400V 12A 99 400V 16A 105 CONNECTORS DIN Plug Skt 2 5mm 10p 10p 3 pin 12p 10p 3 5mm 47p 47p 5 pin 13p 11p Standard 16p 20p Phono 10p 12p Stereo 24p 25p Imm 13p 13p 4mm 18p 17p UHF (CB) Connectors
DIODES BY127 12 * 1N4001 3 OA47 10 1N4002 5 OA90 8 1N4006 7 OA91 7 1N4007 7 OA200 8 1N5401 15 OA202 8 1N5404 16 1N914 4 1N5406 17 CABLES 20 metre pack single core connecting cable, ten different colours 65p Speaker cable 10p/m Standard screened 16p/m Twin screened 24p/m 2.5A 3 core mains 23p/m 10 way ribbon 65p/m	VERO Verobloc 350p. Size 0.1 matrix 2.5 × 1" 22p 2.5 × 3.75" 75p 2.5 × 5" 85p 3.75 × 5" 95p	PCB MATERIALS Alfac PCB transfer sheets — please state type (e.g. DIL pads etc.) 45p Dalo etch resist pen 100p Fibre glass board 3.75" × 8" 75p Ferric Chloride 250ml bottle 100p	PL259 Plug 40p Reducer 14p SO239 Square chassis socket 38p SO239S Round chassis socket 40p IEC 3 pin 250V/6A Plug chassis mounting 38p Socket free hanging 60p Socket with 2m lead 120p
# 1N4148 2 400mW zen. 6p 10 way ribbon 20 way ribbon 120p/m EOXES Dimensions in inches. Aluminium. 3 × 2 × 1 70p 6 × 4 × 2 120p 6 × 4 × 3 150p 6 × 6 × 2 180p	VQ Board 160p Veropins per 100 Single sided 50p Double sided 60p Spot face cutter 105p	All prices exclude VAT. Please add to total order. Please add 50p carriage on all orders under £10 in value. Send cash/cheque/PO or Access/Visa number with your order. Send SAE for discounts list (free with orders). Official orders welcome from colleges, schools etc. Export orders no VAT, please add carriage. CRYST: 100KHz 200KHz 1MHz 1.008M 1.8432M 2.0M	5 0M 240 18 0M 240 200 18 432M 220 290 2 4576M 220 6 144M 180 19 968M 300 370 3 276M 240 7 00M 250 26 69M 300 300 3 579M 120 8 0M 170 27 145M 240 370 4 0M 150 10 0M 180 38 6667M 320 300 4 194M 150 12 0M 290 48 0M 220 270 4 43M 125 16 0M 240 116M 300

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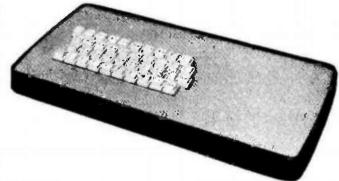
Grabbed By The Dooleys

Those tireless chappies down at Casio have taken time off from disguising BASIC computers and arcade games as pocket calculators and watches, and have turned their attention to the music scene. Although there is undoubtedly a market for top-flight organs and synthesisers amongst home musicians, many people will prefer something more modest for financial reasons, because the living room is too small or because they can't figure out what all the knobs do. At the other end of the scale (sorry), the type of hand-held organ made notorious by Rolf Harris is a little too limiting. With the Casiotone 701, Casio have not just produced a solution to this problem but a radically new type of instrument.

The CT-701 is not just a 61-key polyphonic (eight voice) minisynthesiser, but also contains an on-board computer that acts as a built-in sequencer; among other things. You can play along with the built-in rhythm unit, store your own music in memory and play it back automatically, or just load the machine with a Casio music score and let it get on with things by itself. The latter function is

quite extraordinary — Casio supply the music scores as bar codes and you read them into the machine using a light pen (like those at supermarket check-out desks). In melody guide mode you can even teach yourself to play the instrument, as LEDs above each key light up to tell you which note to play next.

Twenty preset sounds are available, such as pipe organ, flute, piano, oboe, bassoon etc, plus the synthesised drum sounds of the rhythm unit and the 'pneooum' sound so beloved by producers of disco records. Opinions of the preset sound quality vary from "beautiful" (Casio) through "very good" (an independent reviewer) to "too sharply filtered" (another independent reviewer). Since they can't agree and we haven't heard it (though, we're trying hard to get our mucky paws on one), you'll have to listen to one yourself before parting with any cash, but professional musicians seem to like it — the Dooleys use Casiotone mini-keyboards in their stage shows (fellow headbangers may not see this as a compliment). With so much packed into such a compact case (only slightly larger than the actual keyboard) and such a low price (about £500), Casio would certainly seem to have done it again.



ZX Revamp

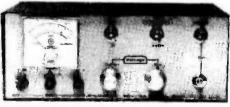
Tor those of you who are serious ZX-81 owners (is there such an animal?) or would simply like to disguise the machine, there is a professional standard keyboard and enclosure now available from Protos Computer Systems. The keyboard is the first of a range of peripherals to make the computer suitable for more heavy-duty use. The 40-key Sinclair coded board uses top quality mechanical contact type key switches with relegendable tops. A steel mounting board holds the keys firmly in position and a high quality printed circuit board completes the board's electrical circuit. Connection to the Sinclair board is made by a flexible connector which is a

push fit to the sockets provided on the ZX81. Access to the edge board connector is via a side port on the Protos enclosure and tape in/out, power and UHF connections are made through the rear. To fit the Protos entails removing the Sinclair board from the black ABS case it comes in and fixing it inside the Protos enclosure with four Phillips type screws. No soldering is required and all electrical connections are plug/socket connections provided either on the Sinclair or the Protos. Further details on this and other forthcoming peripherals can be obtained from Protos Computer Systems, Frome Computing, 20 Ashtree Road, Frome, Somerset BA11 2AS. Please enclose a large SAE with any enquiries.



renson Electronics, designers and manufacturers of power supplies for the Nuclear Research Industry have come up with a series of bench power units. The first unit in the series is priced at

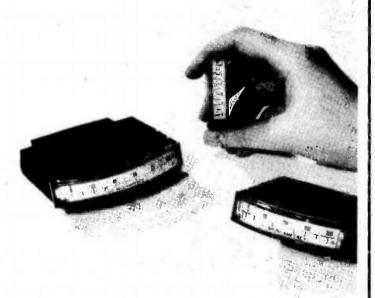
£59 and gives a variable stabilised output up to 30 V at 2 A in two ranges, has foldback re-entrant short circuit protection and current and voltage metering. This unit is also available in kit form at only £35 and further details are from Grenson Electronics Ltd, High March Road, Long March, Industrial Estate, Daventry, Northants NN11 4HQ.



Miniature Magnification New from Stotron Ltd is the

sew from Stotron Ltd is the Scope Mark III pocket microscope with stand. Priced at under E20 it is a useful tool for laboratories, schools, workshops, service engineers and the electronics, electrical, automotive, print and graphic trades, Uncle Tom Cobbley and all! It is 125 mm

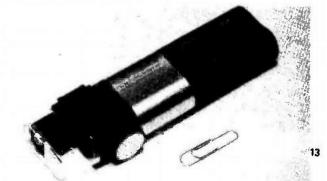
long, with 20x magnification and a graticule showing linear and angular measurements. Illumination is powered by standard 1V5 'pen-light' batteries and a microstand (with spring clips for sample slides) is available as an option so that the device can be used like a conventional microscope. Further details on this device are available from Stotron Ltd, Unit 1, Haywood Way, Ivy House Lane, Hastings, East Sussex.



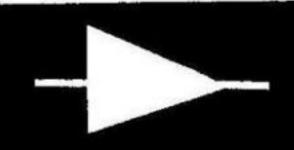
Thin Meters

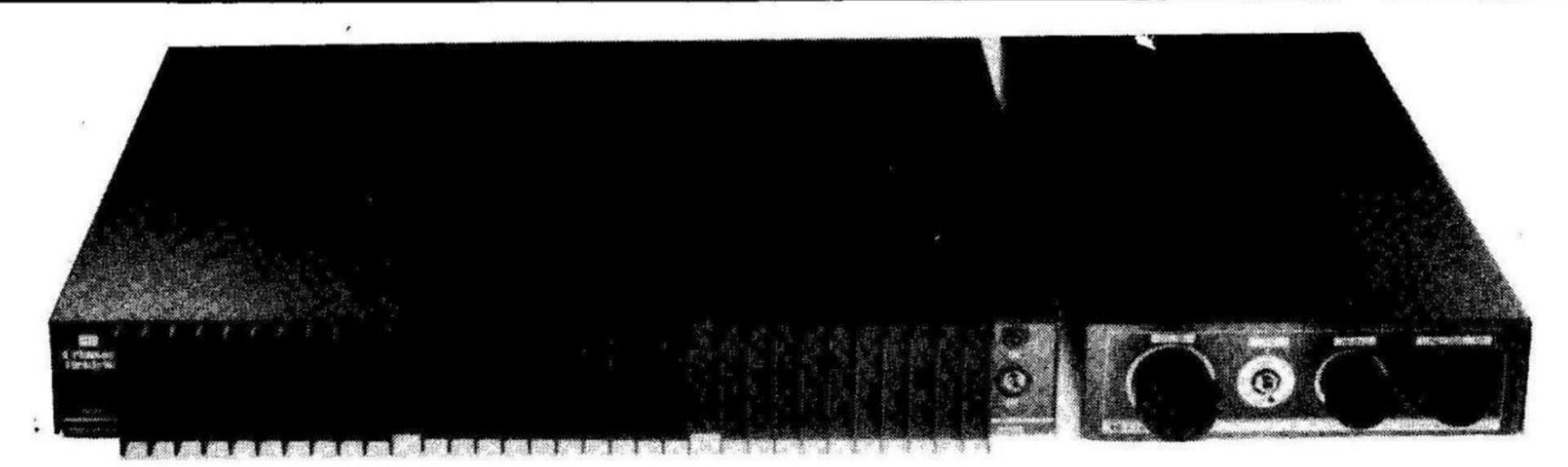
Sifam Ltd of Torquay in Devon are to market a range of very thin edgewise meters manufactured by General Electric of the USA. There are three sizes in the range with case widths of 38 mm, 63 mm and 89 mm and the units are scaled for vertical or horizontal presentation. The special feature of this design is the extreme thinness; the smallest has an overall depth of face of only 13 mm and the two larger sizes of about 17 mm. The smallest model has a rear-access zero set and a

simple spring-clip method of mounting. The two larger models have front access zero set at end of scale and a slide bracket form of mounting. They incorporate jewelled pivot movements with special high-torque magnets for reliable and accurate operation. The standard meters are available ex-stock from Sifam and have a maximum sensitivity of 50 microamperes. Scale markings can be produced to suit individual requirements. Further details of these and Sifam's own range of meters are available from: Sifam Limited, Woodland Road, Torquay, Devon TQ2 7AY.



New Products





HIFI STEREO AMPLIFIER KITS

From one of Britain's leading esoteric amplfier manufacturers comes an exciting new package of stereo amplifier kits, designed to offer all the advantages of true high fidelity but without the usual price penalty. These new kits offer the choice of moving magnet or moving coil inputs, 40 or 100 watts per channel, in fact, everyhthing that made the previous models so popular is imcluded but with added style, easier construction and a full two year warranty.

The New Range Consists of The CK 1010 Stereo Pre Amplifier

The CK 1404 WPC Power Amplifier The CK 1100 WPC Power Amplifier

CK 1010

This kit contains all the necessary parts to build a complete pre-amp. The main PCB is ready assembled and tested therefore construction is simply a matter of point to point wiring and mechanical assembly of the connections and controls to the pre punched chassis.

The CK 1010 takes its DC supply from the CK 1040, 1100 or, if using a different power amplifier a PSK power supply kit. Inputs for disc, tuner and tape are provided and an optional add-on moving coil input can be fitted to extend its versatility. (MC2K)

CK 1040

This is a nominal 40 watt per channel power amplifier kit which features our dual power supply and the DC output for the CK 1010. All components such as heatsinks, wire and connectors are protection and included circuit from short provided outputs.

CK 1100

Similar to the CK 1040 this model provides a nominal 100 watts per channel with extra heatsinking and thermal cutouts are provided as standard.

When correctly assembled these kits are guaranteed for two years.

"It would seem then that Crimson have maintained their position at the top of the commercial kitbuild field. There is no oriental amplifier I know of that can better the sound of this combination overall at any price and only a few - such as the KA-1000 (500 +) - are of comparable standard . . . I can say no more than that for £250 it (CK1010/MC2K/1100) is a bargain and one that becomes the reference point for kit amplifiers from now on."

ETI FEB 1982

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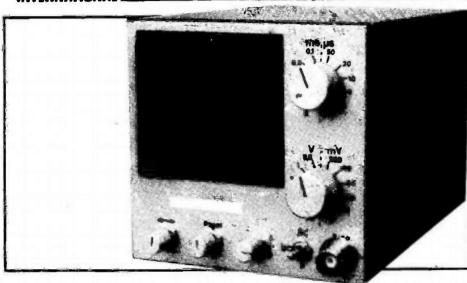
CK 1010 — RRP £90.00 SPECIAL PRICE £79.20 CK 1040 — RRP £119.00 SPECIAL PRICE £105.80 CK 1100 — RRP £149.00 SPECIAL PRICE £130.80 PSK — RRP £20.00...... SPECIAL PRICE £16.80

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INTERNATIONAL TO THE PARTICULAR OF THE PARTICULA



How would you like a 10 MHz oscilloscope about the size of a large lunchbox? Can't afford one? Then build this one — it's the main project in ETI next month.

SLOT CAR CONTROLLER

Let's not beat about the bush. Slot cars are fun. If you're as keen on slot cars and electronics as we are, you'll be equally appalled at the crude control systems provided in the basic sets. Naturally we decided something should be done about the situation and came up with this project. You can have controlled acceleration with overshoot, dynamic braking, 'electronic' fuel tanks — and all from quite a simple circuit. There'll also be some advice on how to tune your cars to get the ultimate in performance from them. A must to read for kids of all ages.

COLUMN LOUDSPEAKER DESIGN

Now this is good stuff. One of the bugbears of public address systems is acoustic feedback, which can be largely overcome by the use of a highly directional sound source. This directs the sound into the audience, where it's needed, and away from the microphone, where it isn't. This article describes the design of a novel column loudspeaker design that is cheap and highly effective.

ROBOT CONTROLLER PART 3

In next month's ETI we continue this series with the construction information for this month's analogue pulse width modulation controller, plus full details and a PCB for a dual digital PWM controller. This will not only be of interest to roboticists but to anyone who needs to control the speed of DC motors.

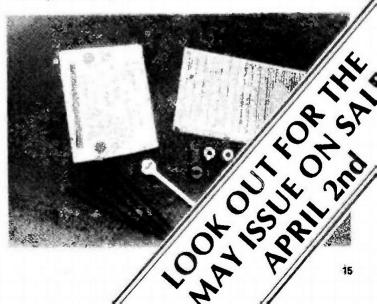
Articles described here are in an advanced state of preparation. However, circumstances may dictate changes to the final contents.

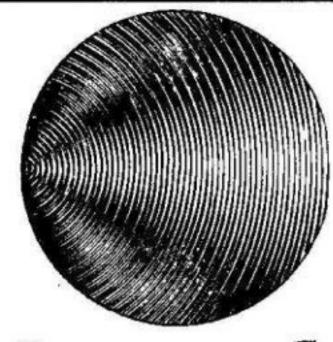
DVMEG

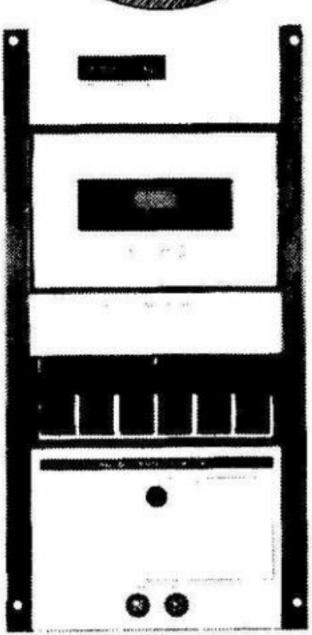
Any scholars out there will know that D is Roman for 500. Since V stands for volts, it will come as no surprise that this project generates 500 V to enable the leakage current through insulation to be tested using the built-in meter. In effect it is a high-voltage resistance meter for measuring values above about 1M0 — hence the last part of the name. We don't just throw these things together, you know!

BREADBOARDING SYSTEMS

There appears to have been a veritable explosion in the number of breadboarding and prototyping systems available to industry and the hobbyist; next month we'll be taking a look at some of them. Both solderwrap and insulation displacement techniques will be examined and we'll have an exclusive first review of a major new development from a leading manufacturer. Not to be missed!







The APPROVED B.K. ELECTRONICS TO APPROVED A SOUND CHOICE



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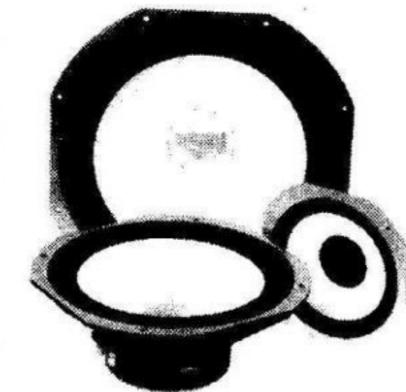
Features: Three digit tape counter. Autostop. Six piano type keys, record, rewind, fast forward, play, stop and eject. Automatic record level control. Main inputs plus secondary inputs for stereo microphones. Input Sensitivity: 100mV to 2V Input Impedance: 68K. Output level: 400mV to both left and right hand channels. Output Impedance: 10K. Signal to noise ratio: 45dB. Wow and flutter: 0.1%. Power Supply requirements: 18V DC at 300mA. Connections: The left and right hand stereo inputs and outputs are via individual screened leads, all terminated with phono plugs (phono sockets provided). Dimensions: Top panel 51/2in x 111/4in. Clearance required under top panel 21/4in. Supplied complete with circuit diagram and connecting diagram. Attractive black and silver finish.

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6 piano type keys

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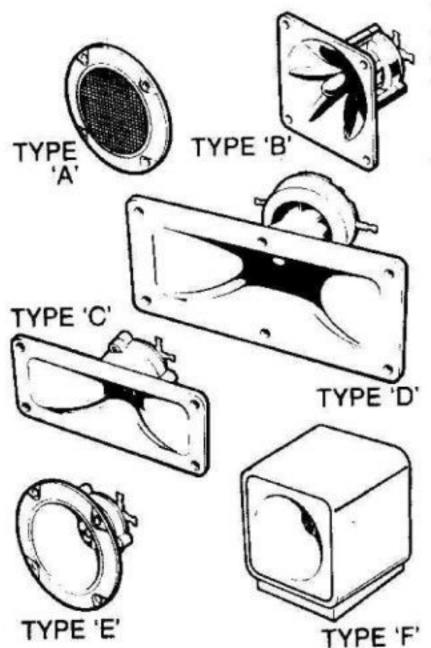


12" 100 watt R.M.S. Impedance 8 ohm, 50 oz. magnet. 2" aluminium voice coil. Resonant Frequency 25Hz. Frequency Response to 4KHz. Sensitivity 95dB. Price £23.70 each. £2.50 Packing and Carriage each.

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TYPE 'A' (KSN2036A) 3" round with protective wire mesh, ideal for bookshelf and medium sized Hi-fi speakers. Price £3.45 each.

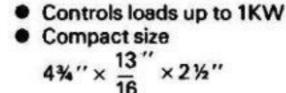
TYPE 'B' (KSN1005A) 31/2" super horn. For general purpose speakers, disco and P.A. systems etc. Price £4.35 each.

TYPE 'C' (KSN6016A) 2" × 5" wide dispersion horn. For quality Hi-fi systems and quality discos etc. Price £5.45 each.

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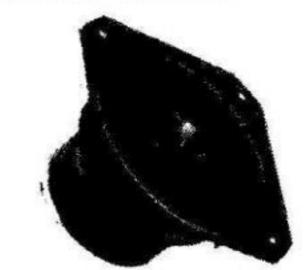
Fitted with attractive cast aluminium fixing escutcheons and mesh protective grills which are removable enabling a unique choice of cabinet styling. Can be mounted directly on to baffle with or without conventional speaker fabrics. All three units have aluminium centre domes and rolled foam surround. Crossover combines spring-loaded loudspeaker terminals and recessed mounting panel.

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Max. output power 100 watts R.M.S. (OMP100) Loads: (Open and short circuit proof) 4-16 ohms Frequency Response20Hz-25KHz ± 3dB Sensitivity for 100 watts 500mV at 10K 00.1%

T.H.D. Size: 360 × 115 × 80mm Prices: OMP 100W

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ELECTROMUSIC TECHNIQUES

Tim Orr, our tame electronic designer, emerged from his workshop this month just long enough to hand over this bundle of circuits for the ardent build-it-yourself musician.

rirtually all of the electronic music synthesisers that have been produced to date employ analogue circuits to generate the synthesised sounds. The process is known as subtractive synthesis, and operates by dynamically filtering out parts of the spectrum of a signal that is often rich in harmonics. The results are instant, easy to modify and relatively inexpensive to implement. It is not possible to produce an arbitrary output spectrum, and so it is very difficult to synthesise realistic copies of naturally generated sounds. This can be done using a digital technique known as harmonic synthesis, whereby the sound is constructed by precisely defining the amplitude and phase of each of the harmonics. These are then added together to produce the output. However, natural sounds are constantly varying and so the data defining all the harmonics must also vary. Harmonic synthesis can produce very realistic sounds and is in itself a powerful technique for generating completely new sounds, but the hardware is a combination of sophisticated microprocessor and digital technology and so is outside the scope of this article.

When we hear a sound we unconsciously analyse it for useful information; "Who wants another drink?" for example. Nobody knows how the human brain analyses incoming sounds, but it does it with incredible speed and sophistication. It can extract precise information from sounds (speech perception), it can experience pleasure from a rich harmony, or it can even learn to ignore certain sounds, such as a ticking clock. The brain is very good at perceiving pitch (or at least it thinks it is; it is also a fairly good liar); see Fig. 1. When you hear a pure tone you

will get a strong impression of its pitch. You will not be able to define its frequency in Hertz, but you will be able to remember its pitch. A sawtooth has a strong harmonic structure but even so you will get the same pitch perception. The ringing tone has virtually no energy at the fundamental frequency and yet it is still possible to correctly perceive the pitch of the signal, although it is more difficult than for the pure tone.

Most musical instruments produce a range of notes. Some instruments, like violins, can produce a continuous range of frequencies; because, unlike the guitar, there are no frets along the neck of the instrument. Keyboard instruments have fixed tuning; the piano, for example. The keyboard is an excellent choice for controlling a synthesiser, as it is easily converted so that it generates suitable electrical signals and it is widely accepted by musicians. Equal temperament tuning is used, that is there are twelve notes per octave and they are spaced at intervals of the twelfth root of two (that is 1.0594631) along an exponential curve, as in Fig. 2.

When You Hear The Tone...

The keyboard is used to define the fundamental pitch of a sound, but the actual shape of the waveform will determine its harmonic structure (Fig. 3). A sinewave is a pure tone and has no harmonics. A halfwave-rectified sine wave contains a fundamental plus a series of even harmonics. A fullwave-rectified sine wave is composed entirely of even harmonics. The squarewave and the triangle are both composed of a series of odd harmonics; in fact if you lowpass filter a square wave you can produce a triangle. The triangle is a fairly pure tone, with little of the energy in the waveform contained in its harmonics. The sawtooth is a rich waveform, having both odd and even harmonics.

The harmonic structure of all these waveforms extends to infinity, but the drawings only show the first 15 harmonics. If we call the harmonic number n, then the harmonic amplitude is easy to define. The rate at which the harmonic amplitude

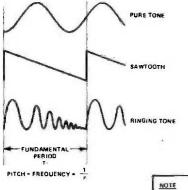
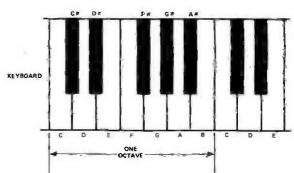


Fig. 2 (below) Keyboard layout with table showing equal temperament tuning.

Fig. 1 Pitch perception.

		NOTE	FREQUENCY (Hz)	RATIO
		C4	261.6	1.0000
		C4 #	277,2	1.0595
		04	293.7	1.1225
		D4#	311.1	1.1892
OTE	FREQUENCY (Hz)	E4	329.7	1.2599
D	27.5	FA	349.2	1.3348
1	56.0	F4#	370.0	1.4142
2	110.0	G4	392.0	1.4983
3	220.0	G4#	415.3	1,5874
A	440.0	A4	440.0	1.6818
5	890.0	A4#	466.1	1.7818
6	1760.0	84	493.9	1.8877
7	3520.0	C6	523.2	2.0000



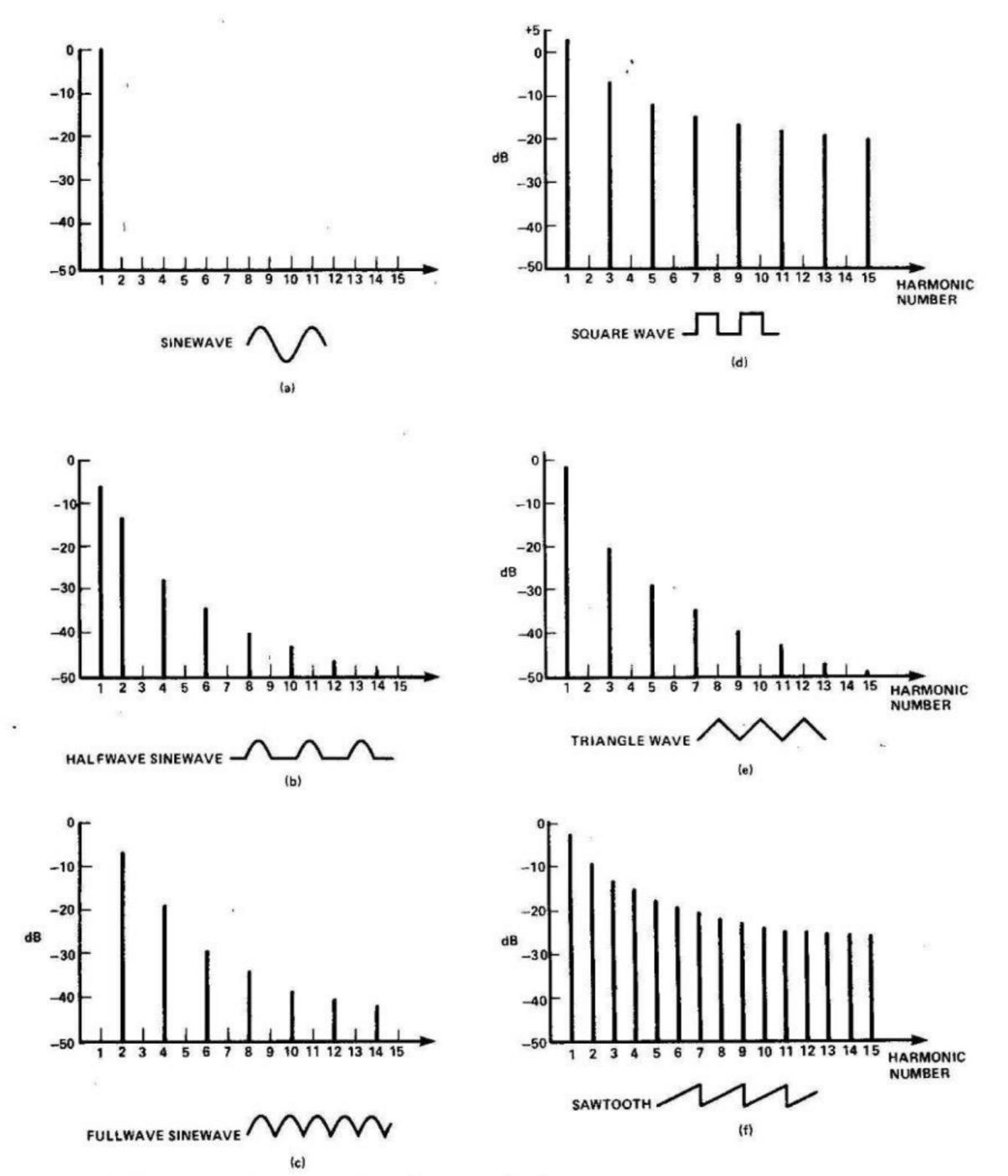


Fig. 3 Harmonic structure of various standard musical waveforms.

decreases is 1/n for the sawtooth and square wave and 1/n² for the half and fullwave rectified sine wave and the triangle. Figure 4 shows a sawtooth being constructed from harmonics. The sum of the harmonics is beginning to look like a sawtooth. As more harmonics are added (with the correct phase and amplitude) the sum will converge upon the correct sawtooth shape. An interesting effect can be produced by changing the mark/space ratio of the square wave. This modifies the odd harmonic spectrum and introduces even harmonics. The mark/space ratio is often dynamically modified as a synthesis process.

Frequency modulation is often employed in synthesisers to produce vibrato and other dramatic pitch change effects. Figure 5 shows some of the effects of frequency modulation. As the modulation depth is increased, frequency sidebands are generated. Their spacing and amplitude are determined by the modulation depth and the modulation and carrier frequencies. To precisely calculate them involves some complex maths and Bessel functions (which I have forgotten all about). To make matters worse, synthesisers usually use voltage controlled oscillators with an exponential transfer function, which tends to exponentially distort the sideband positions. But so what! Music synthesisers are all about making music and not the calculation of sidebands. If a particular electronic device produces a useful musical effect, then use it, don't analyse it.

The output from an oscillator is known as an excitation signal. This defines the pitch of the signal, and to a certain extent the harmonic content of the final signal. It is common practice to filter the excitation signal (Fig. 6). The frequency response of the filter is referred to as a formant. The formant modifies the harmonic spectrum of the excitation, producing a colouration

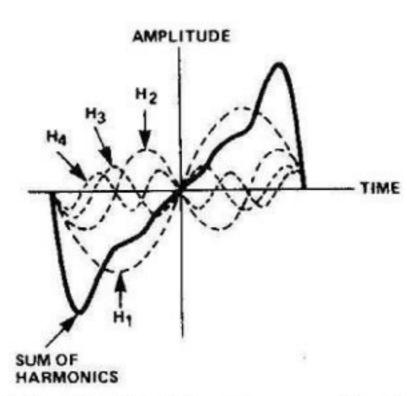


Fig. 4 Adding the first four harmonics to construct a sawtooth waveform.

FREQUENCY

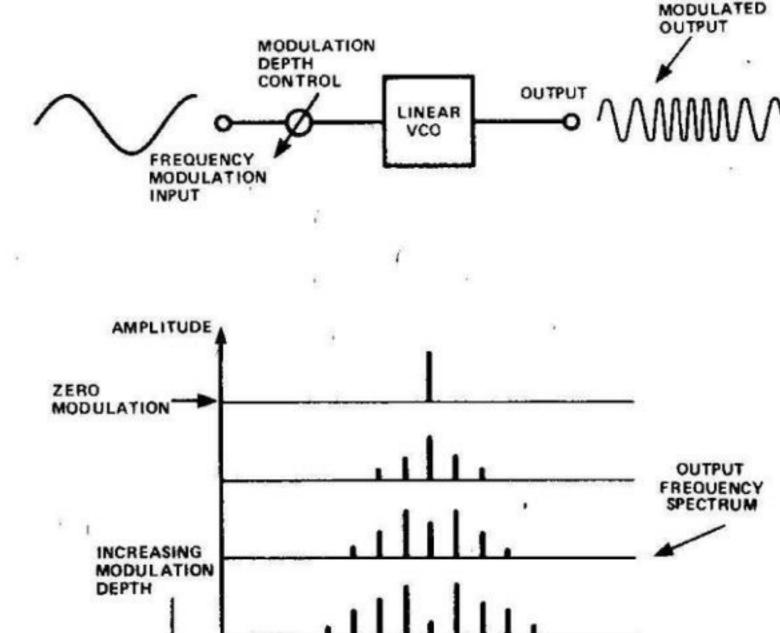


Fig. 5 The effects of frequency modulation.

FREQUENCY

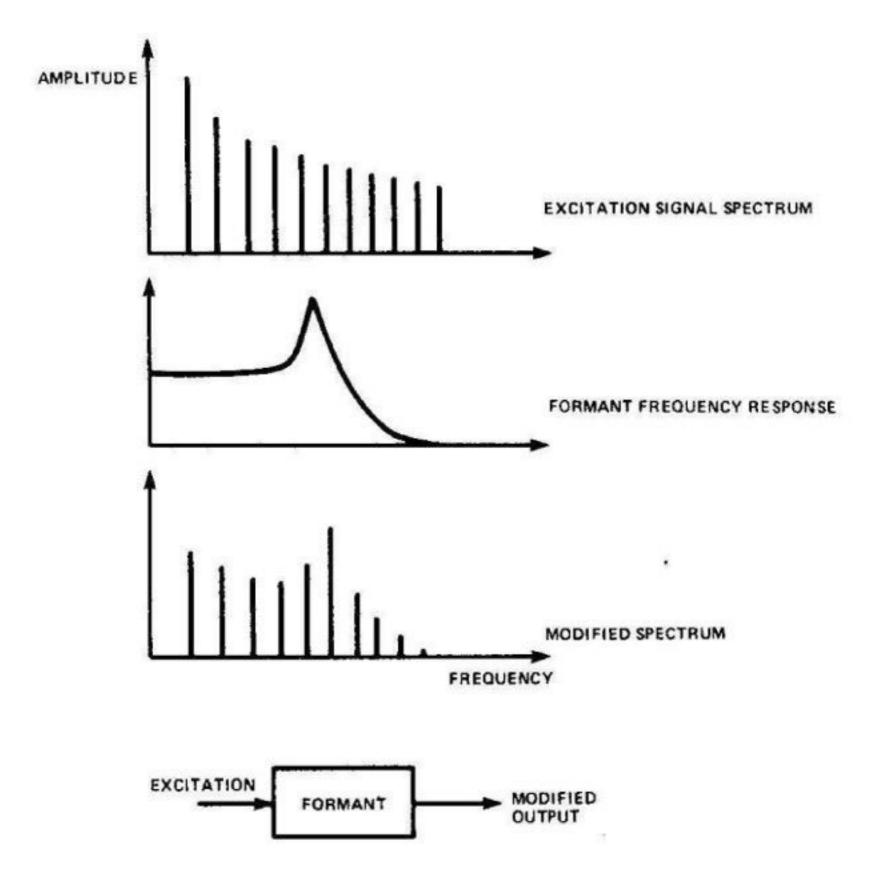


Fig. 6 The effect of filtering an excitation signal.

of the sound. The format is usually a mobile filter and this makes it possible to dynamically alter the sound colour. If the formant has a sharp resonant peak, then the output signal will ring as it passes the harmonics of the excitation.

Another parameter that characterises a sound is its

amplitude contour or envelope (Fig. 7). A sound that has a sharp attack and a slow release is similar to a plucked instrument. Other envelopes will make the sound seem like something else.

Building Blocks

Most synthesisers are constructed from standard building blocks, and most of these blocks are voltage controlled. This is a very powerful concept, because it enables you to control a unit with a combination of control voltages and/or audio signals. Building blocks can be patched together in any arbitary order to produce any system that is wanted. Some standard building blocks are detailed below.

Voltage Controlled Oscillator Used to generate the pitched excitation signals. Often a VCO will generate a wide range of waveforms. The control sensitivity is usually +1 V/octave. Therefore a one twelfth of a volt change will alter the oscillator pitch by one semitone. The exponential control law is a very powerful concept. If a VCO is being driven so that it produces a melody, then adding +1 V to the control input will transpose the melody up by one octave. Thus musical transpositions are very simple to produce. Often more than one VCO will be used, so that a rich chord is obtained.

Voltage Controlled Filter This is used as a formant for the excitation signal. The VCF is generally a lowpass filter, but it can often be a multi-mode device with lowpass, highpass, bandpass and notch responses. The VCF also has a Q (resonance) control. The control sensitivity is +1 V/octave for the frequency parameter, and undefined for the Q.

Voltage Controlled Amplifier The VCA controls the level of audio signals. The control law can be linear or logarithmic. The VCA is usually controlled by an ADSR unit and is employed to generate signal envelope contours. The device is a two quadrant multiplier.

Attack, Decay, Sustain, Release unit The ADSR is used to generate the signal envelope contour and also the VCF sweep waveform.

ETI APRIL 1982

Noise source Generates random noise, which can be used in the synthesis of non-pitched sounds such as explosions. Filtered or sampled noise can be used as a random control voltage.

Low Frequency Oscillator These oscillators are used to generate vibrato in the VCO or a filter sweep in the VCF.

Keyboard Musical control interface, generating pitch voltages of +1 V/octave and also a gate signal to indicate that a note is pressed. A monophonic keyboard only allows one note at a time to be pressed, but if more than one can be pressed simultaneously then the system is polyphonic.

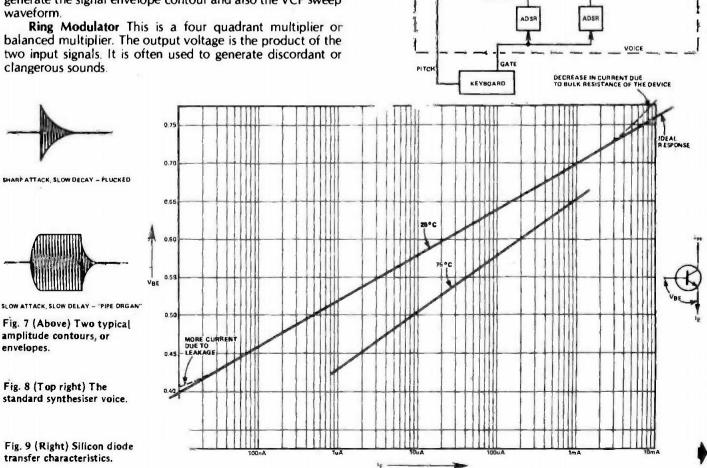
There are several other building blocks such as flangers, sequencers, frequency shifters, and pitch detectors, but there isn't enough space to deal with them.

Polyphonic synthesisers tend to be voice-based; ie all the building blocks are pre-routed to form a voice (Fig. 8). Modular systems are not pre-routed and have to be patched, either with lots of jack-to-jack patch leads or via a matrix patch board using patch pins. Patch leads are relatively inexpensive, but the leads get in the way and it is often difficult to see just what you have patched. Matrix patch boards are easy to understand, but they suffer from crosstalk and a large board (60 by 60) might cost £500!

vec

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LFO

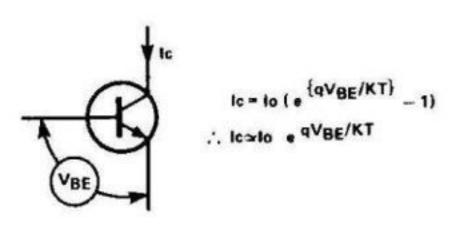


Diode Data

The silicon diode has an exponential transfer function, that is the diode current increases exponentially for linear increments in the diode voltage (Fig. 9). This can be used to turn linear changes from, say, a keyboard into exponential or musical intervals in a VCO. The required musical range is probably no more than 200 to 1 and so a suitable operating current would be 0.5 uA to 100 uA, thus avoiding the non-exponential parts of the curve. The silicon diode is temperature dependent (it is often used as a thermometer) and so great care must be used to avoid thermal problems. The junction voltage changes by $-1.9 \text{ mV/}^{\circ}\text{C}$, but a semitone change is equivalent to 1.5 mV,

therefore a 1°C change could result in a 1.27 semitone change in pitch! Figure 9 shows two temperature effects in operation; there is a large shift and the slope of the line changes.

Figure 10 illustrates the equations that determine the diode operation. Two facts emerge from these equations. First, an 18 mV change in V_{BE} will double the current I_{C} , and second, this parameter has a temperature coefficient of $-0.33\%/^{\circ}C$. Both the temperature problems can be resolved by using a circuit similar to that shown in Fig. 11. Transistor Q1 is run at constant current (12 uA) by the op-amp. Q2 is used as the exponentiator transistor. The emitter of Q2 is held at a voltage of about -0.006. Any voltage change at the base of Q2 will result in an exponen-



WHERE
IO IS THE EMITTER SATURATION CURRENT
K IS BOLTZMANNS CONSTANT
q IS THE CHARGE ON AN ELECTRON
T IS THE TEMPERATURE IN °K

HOWEVER, $\frac{KT}{q}$ IS 26mV AT 28.58 °C (301.73 °K IS ROOM TEMPERATURE). THEREFORE, Ic \simeq Io e $^{V}BE/26$ WHERE V_{BE} IS MEASURED IN mV

REARRANGING THE EQUATION,

26. In (lc) = VBE

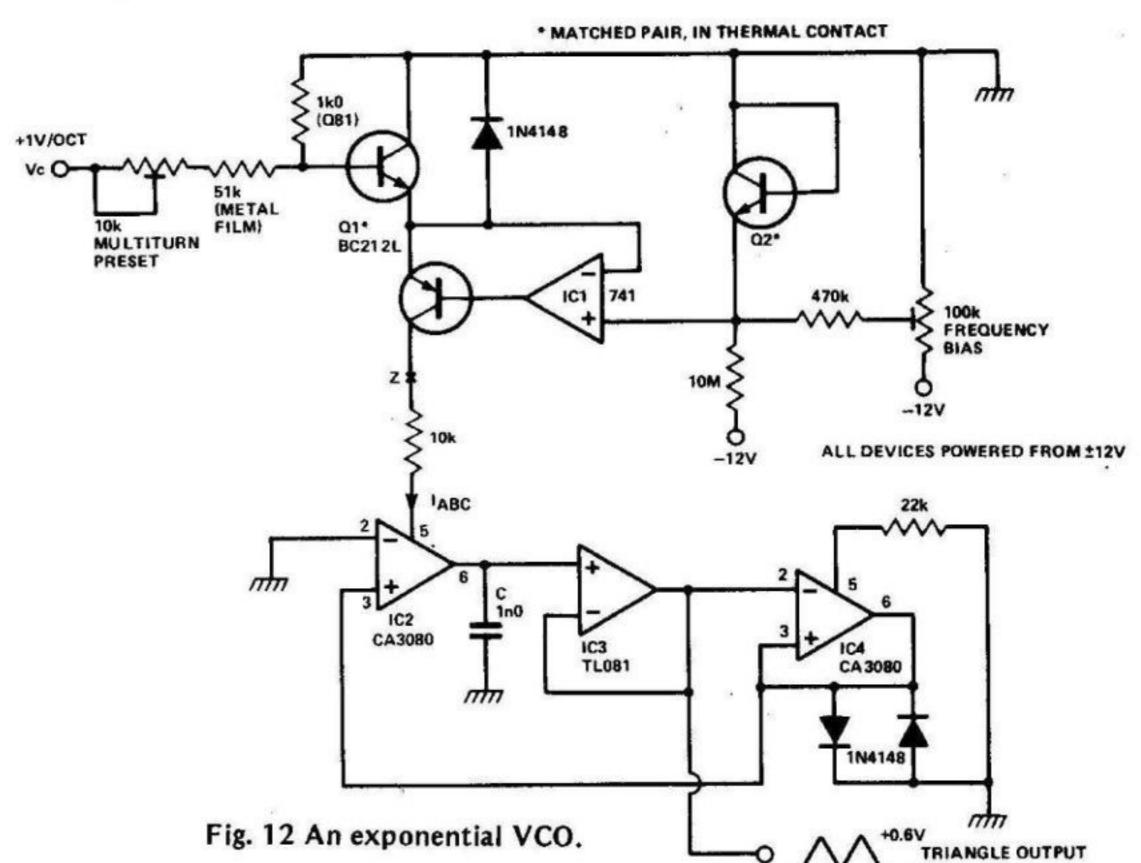
THEREFORE, AN OCTAVE CHANGE IN IC IS CAUSED BY A 18.021827mV CHANGE IN VBE (AT 28.58 °C). HOWEVER, IF THE TEMPERATURE WERE +1 °C HIGHER, THEN VBE WOULD HAVE TO BE INCREASED IN SIZE TO A NEW VALUE OF

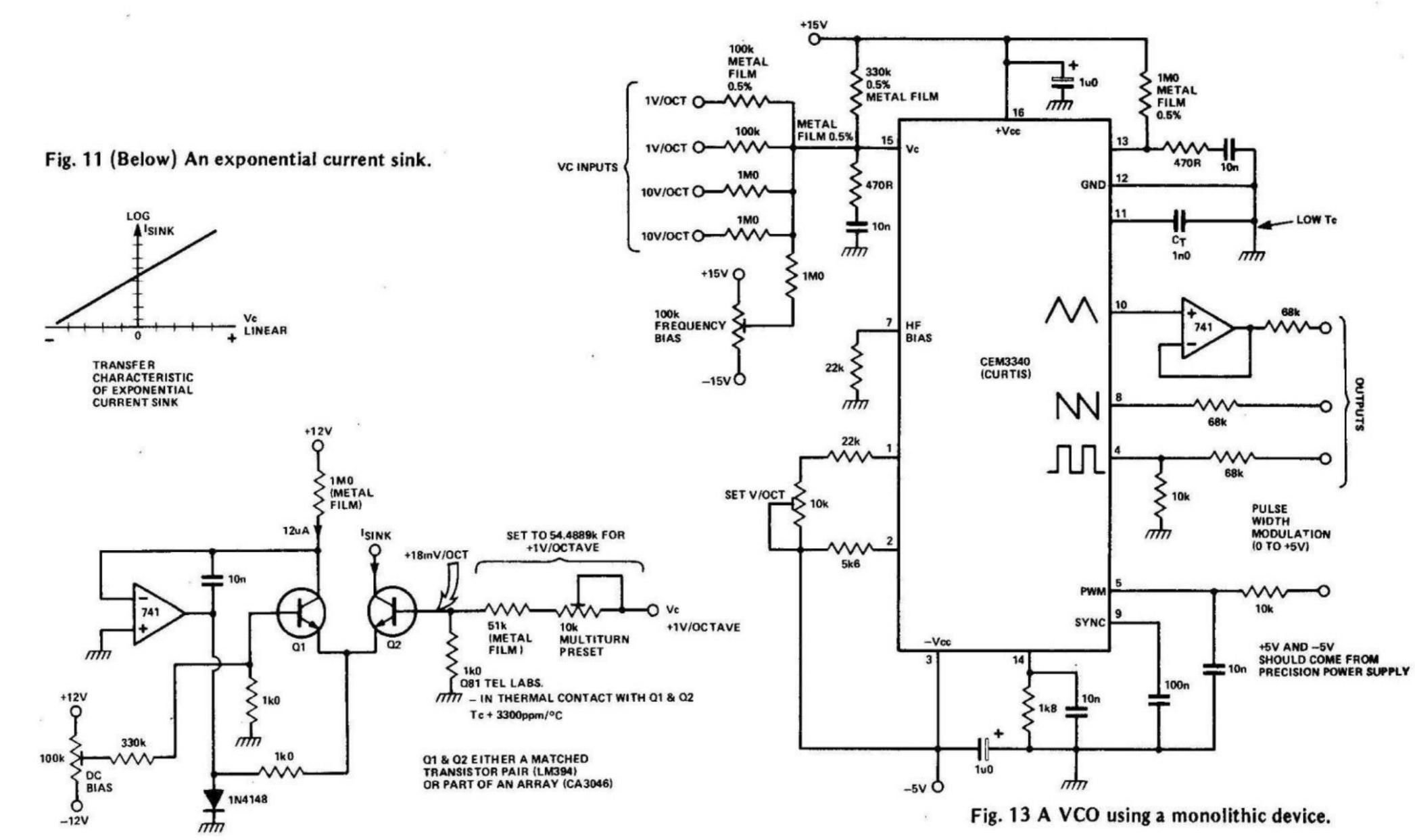
26 x (302.73)

SO, FOR AN OCTAVE CHANGE IN IC AT THE NEW TEMPERATURE, VBE MUST CHANGE BY 18.08155mV, AN INCREASE OF 0.059723mV. THIS CAN BE EXPRESSED AS A PERCENTAGE CHANGE PER °C:—

TEMPERATURE SENSITIVITY = 0.059/23 x 100 18.021827 = 0.33139%/ °C

Fig. 10 Exponential transistor characteristics.



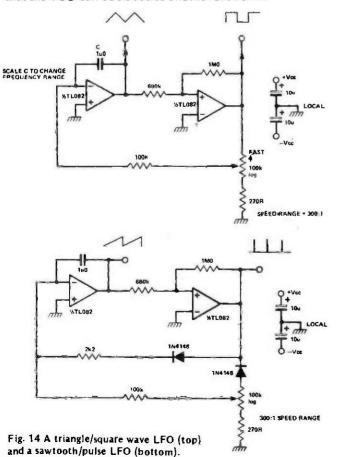


tial change in the collector current of Q2. Q1 and Q2 are in thermal contact and so any temperature change will effect both equally. Thus the $-1.9~\rm mV/^{\circ}C$ factor is cancelled out by Q1 acting as a compensating thermometer for Q2. The slope change is removed by using a temperature sensitive resistance (Q81 — Tel Labs) which has an equal but opposite temperature coefficient to the diode junction. This resistor is often in thermal contact with the matched transistors. If this circuit is connected to a linear current controlled oscillator, a musical VCO is produced.

VCO Circuits

Figure 12 is the circuit for an exponential VCO using an exponential current source. The oscillator is a standard triangle-square wave device. IC2 is a current-controlled integrator; the slow rate at its output is equal tol_{ABC}/C. This voltage is buffered by IC3 which drives a Schmitt trigger IC4. The output of IC2 ramps up and down between the two hysteresis levels which are determined by the two clamping diodes connected to the output of IC4. Any stray capacitance on the output of IC4 will slow down the Schmitt trigger and this will make the VCO go flat at high frequencies. Also the propagation time delay around the oscillator will cause a flattening out of the response at high frequencies. These effects can be nulled out but they may not even affect things if the VCO frequency is kept relatively low.

A very good VCO is shown in Fig. 13. It is a monolithic device, the CEM3340 from Curtis Electromusic Specialities Inc who make a range of electronic music devices. As can be seen, very few external parts are needed to implement the VCO. All the temperature compensation is performed inside the chip. Triangle, sawtooth and variable mark/space square wave outputs are simultaneously available. The mark/space ratio is a voltage controlled parameter. A sync input is also provided so that the VCO can be slaved to another oscillator.



LFO Circuits

A couple of LFO units are shown in Fig. 14. All four output waveforms can be usefully employed to sweep VCOs and VCFs. Often the waveforms are mixed together to produce strange frequency modulations. When the sawtooth is fed into one side of a ring modulator and noise into the other, a beat track can be generated; it sounds a bit like a cymbal being hit.

Noise Generators

In 'the old days' noise sources were made by amplifying the noise current of a diode junction that was zenering. These were a bit unreliable, and always involved selecting the device. However, noise can be generated digitally with a maximum length pseudorandom sequence generator (Fig. 15). The noise spectrum is relatively flat and always the same. If you slow down the clock rate you can get some interesting sounds; I think that this is used on some TV games. If a longer shift register is used, say 30 or 40 stages (the 4006 is 18 stages long), and the noise source is turned on, a tone is initially heard which gradually changes into noise as the sequence becomes more scrambled up. You can purchase a monolithic noise generator (pseudorandom); it is the MM5837 made by National Semiconductor, also sold by AMI with the part number \$2688.

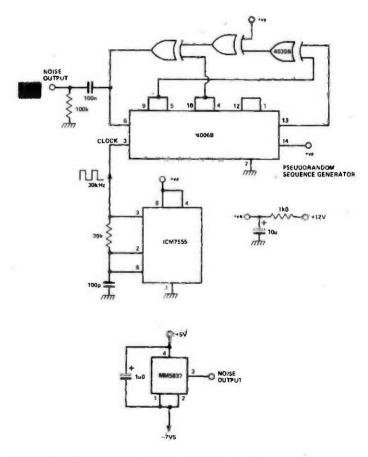


Fig. 15 A digital noise source (top) and a noise generator chip (bottom).

Five pages gone already, and we've still only scratched the surface of this fascinating subject. In part two next month, Tim Orr will continue his discussion of electromusic techniques with yet more circuit building blocks.

introducing

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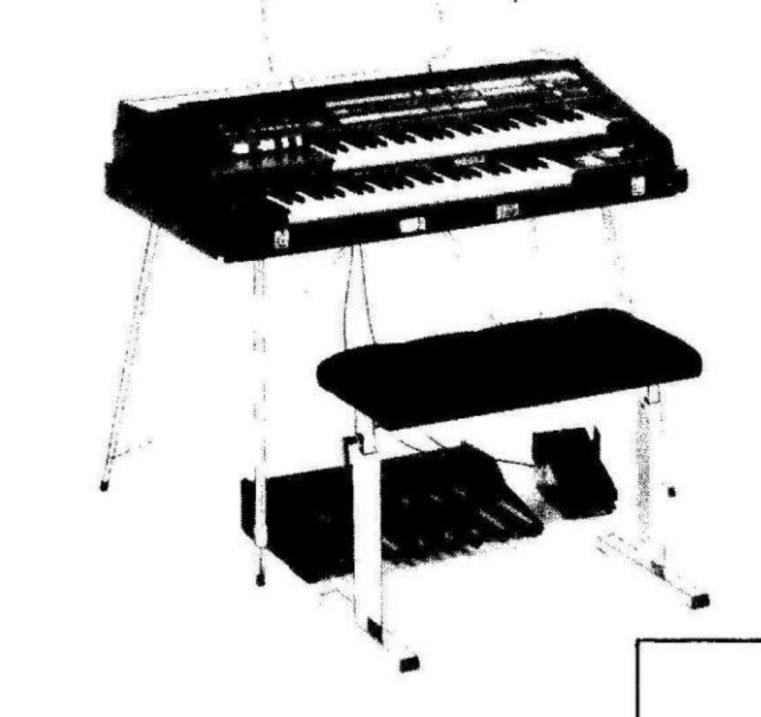
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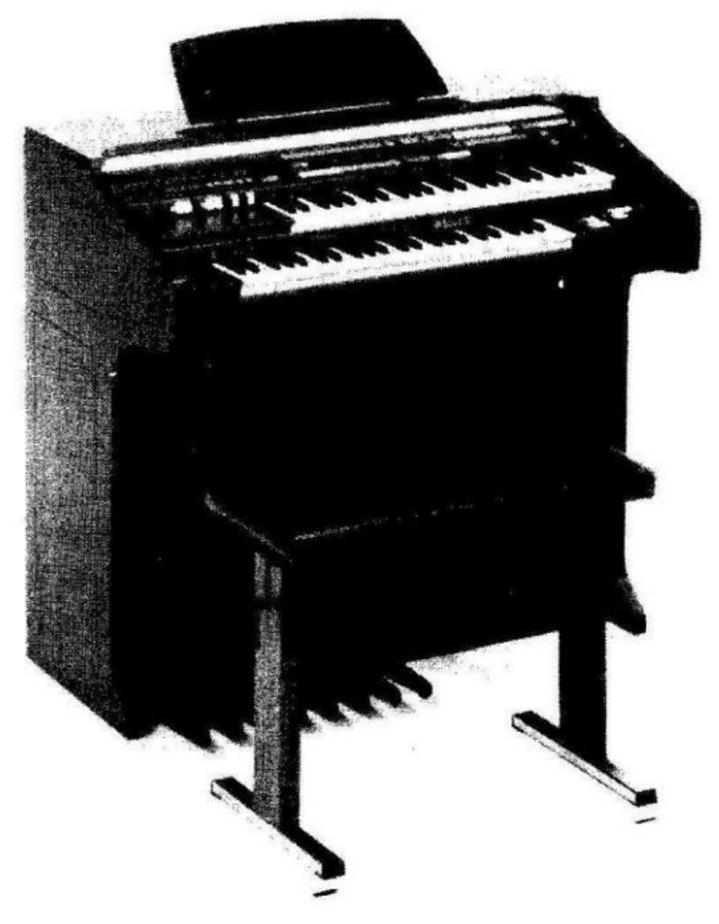


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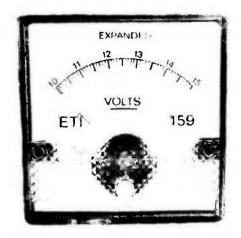
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ETI/4

ACCURATE VOLTAGE MONITOR



This simple, low-cost instrument can be built into power supplies or used as a portable or fixed 'battery condition' monitoring meter. Design by Simon Campbell and Roger Harrison.

ommon storage batteries to power nominal 12 V DC electrical systems have a terminal voltage that ranges from a little over 10 V when discharged to around 15 V when fully charged, the operating voltage being somewhere in the range 11V5 to 13V8. Lead-acid batteries, for example, may have a terminal voltage under rated discharge that commences at around 14V2 and drops to about 11V8. A 12 V (nominal) nickel-cadmium battery may typically have a terminal voltage under rated discharge that starts at 13 V, dropping to 11 V when discharged.

Equipment designed to operate from a nominal 12 V DC supply may only deliver its specified performance at a supply voltage of 13V8 — mobile CB and amateur transceivers being a case in point. Other DC operated equipment may perform properly at 12V5 but 'complain' when the supply reaches 14V5.

To monitor the state of charge/discharge of a battery, a battery-operated system or the output of power supplies, chargers, etc, a voltmeter which can be easily read to 100 mV over the range of interest (10 to 15 V) is an invaluable asset. This

project does just that.

The Circuit

An LM723 variable voltage regulator is employed to set an accurate 'offset' voltage of 5 V, and the meter (M1) plus the trimpot RV2 and R3 make up a 5 V meter, with the trimpot allowing calibration. The negative terminal of the meter is connected to the output of the 723 so that it is always held at 5 V 'above' the circuit negative line. The positive end

of the meter goes to a zener which will not conduct until more than 5 V appears between the circuit +ve and -ve lines. Thus the meter will not have forward current flowing through it until the voltage between the +ve and -ve rails is greater than 10 V, and will read full scale when it reaches 15 V (after RV2 is set correctly).

The meter scale limits may be adjusted by setting the output of the 723 higher or lower (adjusted by RV1) and setting RV2 so that the meter has an increased or decreased full-scale deflection range.

A variety of meter makes and sizes may be used.

Construction

Mechanical construction of this project has been arranged so that the PCB can be accommodated on the rear of any of the commonly available moving coil meter movements. We chose a meter with a 55 mm wide scale (overall panel width, 82 mm). A meter movement with a large scale is an advantage as it is considerably easier (and more accurate) to read than

HOW IT WORKS

The meter, M1, is a 1 mA meter with series resistance — made up of R3 and RV2 — so that it becomes a 0-5V voltmeter. The negative end of the meter is maintained at 5 V above the circuit negative line by the output of IC1, a 723 adjustable regulator. The positive end of the meter is connected to the circuit positive line via ZD1, a 4V7 zener diode. Thus, no 'forward' current will flow in the meter until the voltage between the circuit negative line and the circuit positive line is greater than 5 + 4.7 = 9V7.

Bias current for the zener is provided by a FET, Q1, connected as a constant current source so that the zener current is accurately maintained over the range of circuit input voltage. This ensures the zener voltage remains essentially constant so that meter reading accuracy is maintained.

The trimpot RV1 sets the output voltage of the 723. This determines the lower scale voltage. Trimpot RV2 sets the meter scale range, less resistance decreases it.

Diode D1 protects the circuit against damage from reverse connection.

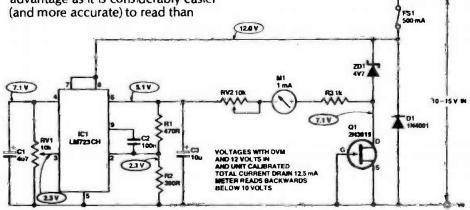


Fig. 1 Circuit diagram for the Voltage Monitor.

Having chosen your meter, drill out the PCB to suit the meter terminal spacing first. The components may then be assembled to the board in any particular order that suits you. Watch the orientation of the 723, ZD1, the FET and particularly D1. The latter is an 'idiot diode'. That is, if you have a lapse of concentration or forethought and connect your project backwards across a battery, the fuse will blow and not the project. Fuses are generally found to be cheaper than this project!

Seat all the components right down on the PCB as the board may be positioned on the rear of the meter with the components facing the meter. The size of C2 may give you a little trouble. Polyesters are generally too large and therefore unsuitable. We used a ceramic type capacitor — as commonly used on computer PCBs as bypasses. Alternatively, a 100n tantalum capacitor (+ ve to pin 2 of IC1) may be used. The actual value or type of capacitor is not all that critical.

We have used multiturn trimpots for RV1 and RV2 as they make the setting up a whole lot easier

Calibration

For this you will need a variable power supply covering 10 to 15 V and a digital multimeter (borrow one for the occasion).

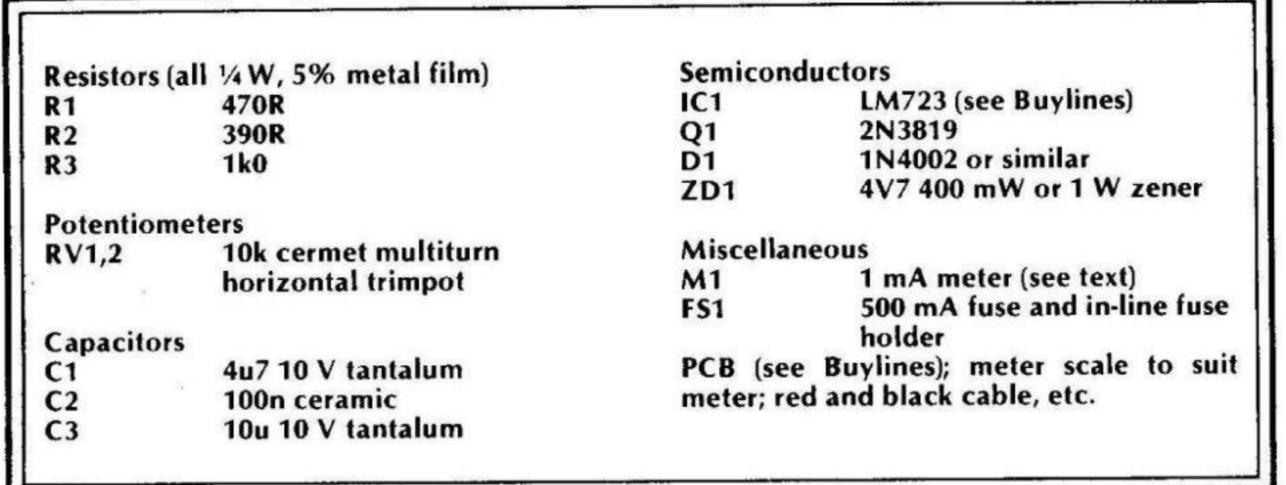
First set the 10 V point. Connect the digital multimeter across the power supply output and adjust the power supply to obtain 10.00 V. Set the mechanical zero on the meter movement to zero the meter's pointer. Connect the unit to the power supply output and adjust RV1 to zero the meter needle.

Next, set the power supply to obtain 15.00 V. Now adjust RV2 so that the meter needle sits on 15 V (full scale). Check the meter reading with the power supply output set at various voltages across the range. We were able to obtain readings across the full scale within ± half a scale reading (±50 mV). With a 2% FSD accuracy meter the worst error may be about ± one scale division.

BUYLINES_

Only one thing to comment on here; when you purchase your LM723 (or uA723 — same thing) make sure you get the version that comes in a T099 case, not the DIL version. The PCB is designed for the 10 pin version as shown in the overlay and the DIL type won't fit. Speaking of PCBs, as usual you can get it from us using the order form on page 44.

PARTS LIST



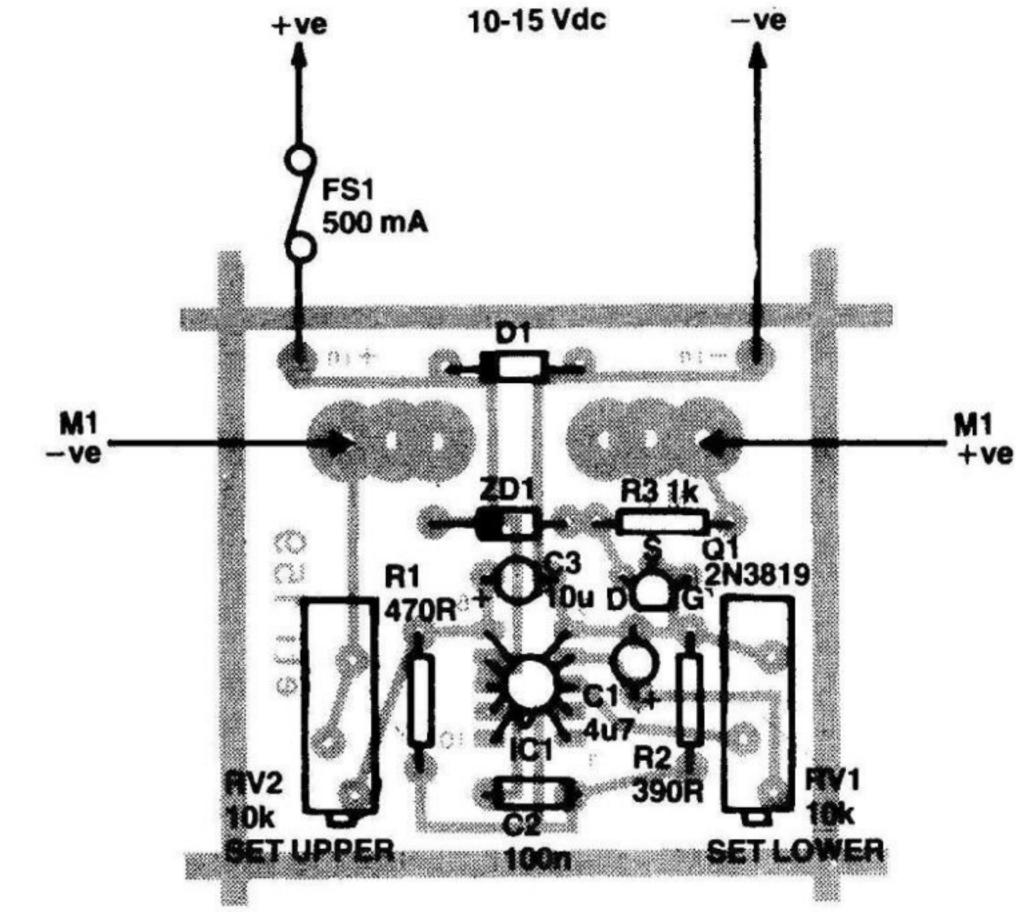


Fig. 2 Component overlay for the Voltage monitor. Note that IC1 is in a 10-pin T099 case.

BATTERY CONDITION AND TERMINAL VOLTAGE

The 12 V battery, in its many forms, is a pretty well universal source of mobile or portable electric power. There are lead-acid wet cell types, lead-acid gel electrolyte (sealed) types, sealed and vented nickel cadmium types, and so on. They are to be found in cars, trucks, tractors, portable lighting plants, receivers, transceivers, aircraft, electric fences and microwave relay stations — to name but a few areas.

No matter what the application, the occasion arises when you need to reliably determine the battery's condition - its state of charge, or discharge. With wet cell lead-acid types, the specific gravity of the electrolyte is one reliable indicator. However, it gets a bit confusing as the recommended electrolyte can have a different S.G. depending on the intended use. For example, a low duty lead-acid battery intended for lighting applications may have a recommended electrolyte S.G. of 1.210, while a heavy-duty truck or tractor battery may have a recommended electrolyte S.G. of 1.275. Car batteries generally have a recommended S.G. of 1.260. That's all very well for common wet cell batteries, but measuring the electrolyte S.G. of sealed lead-acid or nickel-cadmium batteries is out of the question.

With NiCads, the electrolyte doesn't change during charge or discharge.

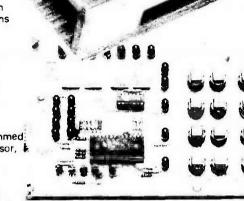
Fortunately, the terminal voltage is a good indicator of the state of charge or discharge. In general, the terminal voltage of a battery will be at a defined minimum when discharged (generally between 10 and 11 V), and rise to a defined maximum when fully charged (generally around 15 V). Under load, the terminal voltage will vary between these limits, depending on the battery's condition.

Hence a voltmeter having a scale 'spread' to read between these two extremes is a very good and useful indicator of battery condition. It's a lot less messy and more convenient than wielding a hydrometer to measure specific gravity of the electrolyte!

The charge and discharge characteristics of typical lead-acid and sealed NiCad batteries are given in the accompanying figures.

Micro-processor universal Timer

This incredibly versatile programmable timer can control up to 20 functions at accurately timed intervals over a period of a week. Originally developed for industrial and laboratory use it offers many interesting and exciting possibilities for the amateur constructor. Based on a pre-programmed TMS 1000 Microprocessor, & the unit provides a 24 hour clock with four independent relay controlled outputs with



a programmable period of one week. Up to 20 daily or weekly programmable functions can be set via a keyboard. Any of the timer functions can be assigned to control any one of the four relay outputs thus providing almost unlimited programming possibilities.

No previous experience of microprocessor programming is necessary since the manual explains all the possible operations, clearly and simply, enabling the inexperienced user to be fully conversant within one hour. Completed programme steps are indicated by LED's

The kit comes complete with printed panel and may be installed either as a 'built-in' or a 'free-standing' unit. A stabilised power supply mounted on a separate printed circuit board is supplied with the unit. It requires the addition of a 12V, 1A transformer. There is space on the board for up to four output control relays. One is supplied with the kit. Further relays maybe ordered separately as required. Price: (excluding wooden housing as illustrated) £48.37 inclusive of VAT and DELIVERED FREE on U.K. mainland.

APPLICATIONS

The programmable timer can provide central control of domestic electrical cooking, heating and entertainment equipment. The possibilities are limited only by the imagination of the user. Control of house lighting to discourage intruders; control of TV or audio equipment; sound or video recording control; automatic plant watering; automatic pet doors or feeding - are a few simple examples. For the professional or industrial user many uses in this area of process control will be found.

TECHNICAL DATA:

Power supply:
Mounted on separate pcb with space for up to four output
control relays. Requires 12V/1A transformer.

CONTROL SWITCHING:

Additional relays tone supplied with kit1 will switch 2Aa Additional relays may be ordered separately.

National relay, order no. HT 12V.

Siemans relay, order no. HT 1NV12.

MICROPROCESSOR:

TMS 1000 DISPLAYS:

12mm 7 segment LEO numerical display. LEO programme function indicators.

DIFFICULTY GRADE: 3

KIT NUMBER: K1682

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2.2 Watt mini amplifier Mono VU using LED's 7 Watt amplifier Dimmer 1000 Watt Dimmer 1000 Watt(deparasite) High precision stopwatch Microprocessor Universal timer 20 Watt monolithic ampliffer FM oscillator Stereo VU using LED's Universal mono pre-amplifier 60 Watt power amplifier

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Infra-red transmitter for tuner K2558 Tape/slide synchronizer 3 channel coloured light organ 20 cm display (common anode) 20 cm display (common cathode) 5-14V DC 1 Amp Universal power supply

Light computer Universal stereo pre-amplifier Stereo RIAA corrector amplifier Universal 4 digit up/down counter with comparator

Microprocessor doorbell with 25 tunes 40 Watt audio amplifier Electric drill speed control
Microprocessor-controlled EPROM

programmer (kit form) Microprocessor-controlled EPROM programmer (built and tested) Universal start/stop timer

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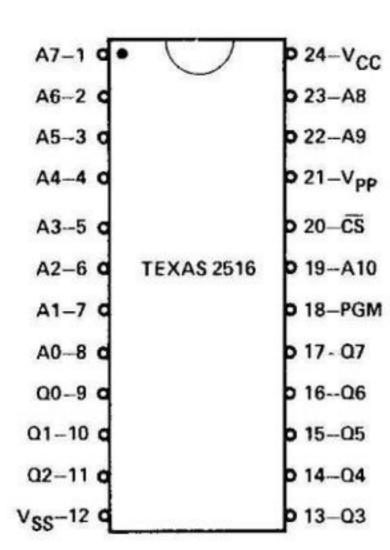
COMPUTER EXPANSION SYSTEM

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programmer and associated EPROM cards suitable for the machine code freak to store away those beloved extra routines or the space invaders freak to capture his aliens in 0's and 1's for life.

The first major consideration when designing an EPROM programmer is just what EPROMs should it be capable of blowing. There is more than just a little confusion here. There are two basic types of EPROM currently available — those that run off a three rail supply and those that run from a



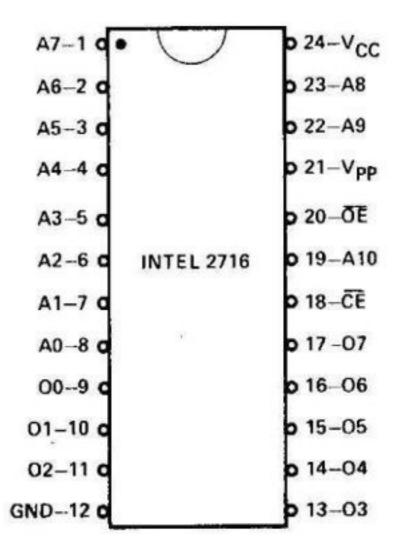


Fig. 1 You can program these EPROMs...

single +5 V rail. The two sizes of PROM most popular at the moment are 2K x 8 and 4K x 8. Aha! here manufacturers have had some fun. Intersil and others like calling their triple rail PROMs 2716 and 2732 whereas Intel make their 2716 and 2732 single rail; not to be missed out Texas try to settle the balance by nominating their EPROMs 2516 and 2532; both are single rail!

To clear up the matter our.
programmer will program single rail
EPROMs only, these being the most
popular. It will program the Texas 2516
2K x 8 EPROM and Intel 2716 2K x 8
EPROM as these are pin-for-pin
compatible (see Fig. 1). However, 2532

HOW IT WORKS.

PROM PROGRAMMER

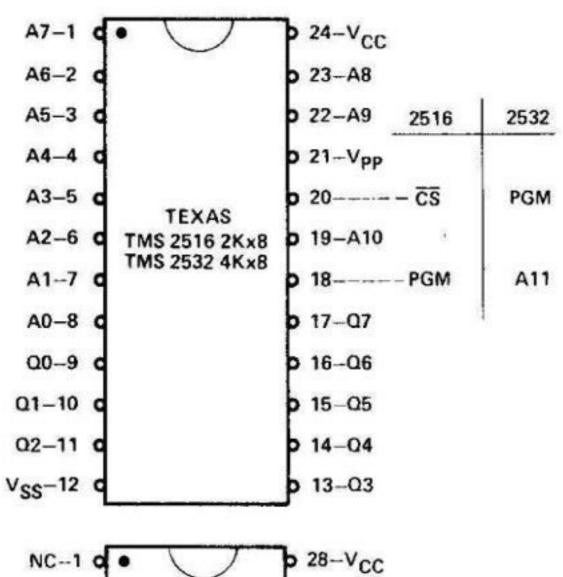
The heart of this board is two 6520 peripheral input-output chips — they serve to generate the address bus, the data and control signals for the chip being programmed.

R1 and C1 generate the power up reset; C4, 5 and 6 are included in for decoupling. The rather peculiar need of the V_{pp} pin for 0, +5 V and +25 V is met by the PSU and switching circuit. Transformer T1 supplies 30 V AC to the bridge which rectifies it and feeds it to smoothing capacitor C3. IC3 and ZD1 regulate this to + 25 V DC. C2 is included in the interests of stability. Transistors Q1 and Q2 handle the switching of V_{PP} between 0, 5 and 25 V. This output is then fed to the DIL switch and then to the V_{PP} pin of the EPROM to be programmed. Ports A and B of IC2 are used to generate the address bus - note A12 is connected to pin 1 of the EPROM (on a 28 pin basis) for use later with 2764 EPROMS. The data bus is generated by port A of IC1, while port B of IC1 generates the control for Vpp and the CS and PGM lines which are switched with A11 to the correct pins of the EPROM by the DIL switch.

Inputs to the 6520s are straight from the expansion sockets - ϕ 2 being used to enable the chips to reduce power consumption.

and 2732 4K x 8 EPROMs are not compatible and we have stuck to the 2532, as this then allows for use of the new 2764 8K x 8 EPROMs with the minimum alteration (see Fig. 2). If you wish to program 2764's then you must make the alterations to correct the OE/V_{PP} and CS lines. A12 has been brought to pin 1 and power (V_{CC}) to pin 28.

Selection of the type of EPROM you want to program is made by means of a quad DIL switch. This switch is unusual in that each section operates two oppositely biased single pole switches — this means it can be



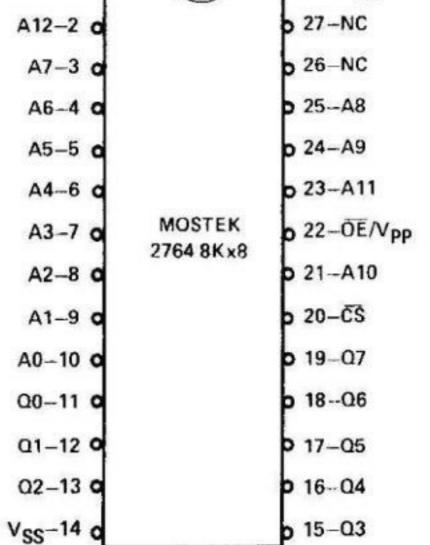


Fig. 2 ... or these ones.

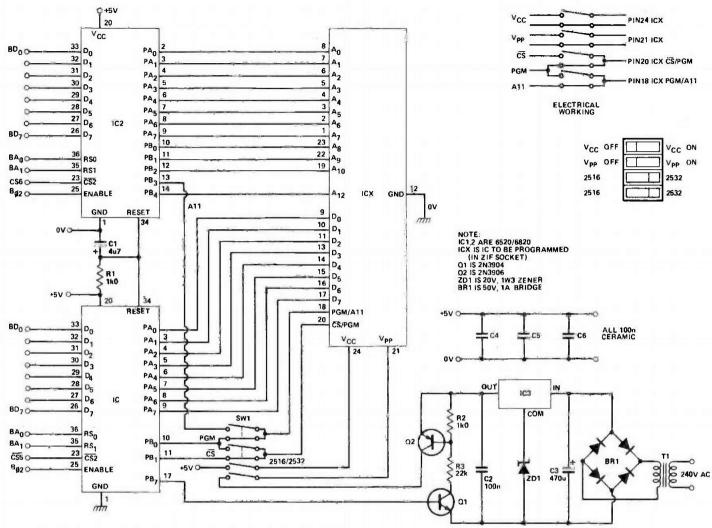


Fig. 3 Circuit diagram of the EPROM programmer, with details of SW1. ICX is the EPROM to be programmed.

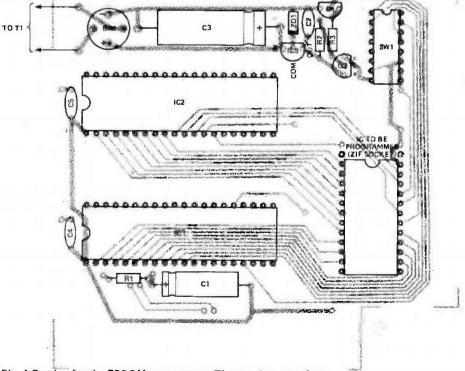


Fig. 4 Overlay for the EPROM programmer. The zero insertion force socket position has extra holes to allow for 2764s.

PARTS LIST.

PROM PR	OGRAMMER
Resistors (all ¼W, 5%)
R1,2	1k0
R3	22k
Capacitors	5
C1	4u7 25 V axial electrolytic
C2,4,5,6	100n ceramic
C3	470u axial electrolytic
Semicond	uctors
IC1,2	6520/6820
IC3	78L05
Q1	2N3904
Q2	2N3906
ZD1	20 V, 1W3 zener diode
BR1	1 A, 50 V bridge rectifier
Miscellan	eous
SW1	Quad DPST DIL switch
PCB (see B	uylines); DIL sockets;
	er (6 VA, 0-15-0-15)

used as a 4 pole changeover switch and makes it ideal for the job. Two of the four sections are used for chip power (+5 V) and the programming can be destroyed if V_{pp} is applied with V_{CC} disconnected. The other two sections are used to switch \overline{CS} , PGM and A11 to the correct pins of the ZIF socket according to whether a 2516 or 2532 is to be used.

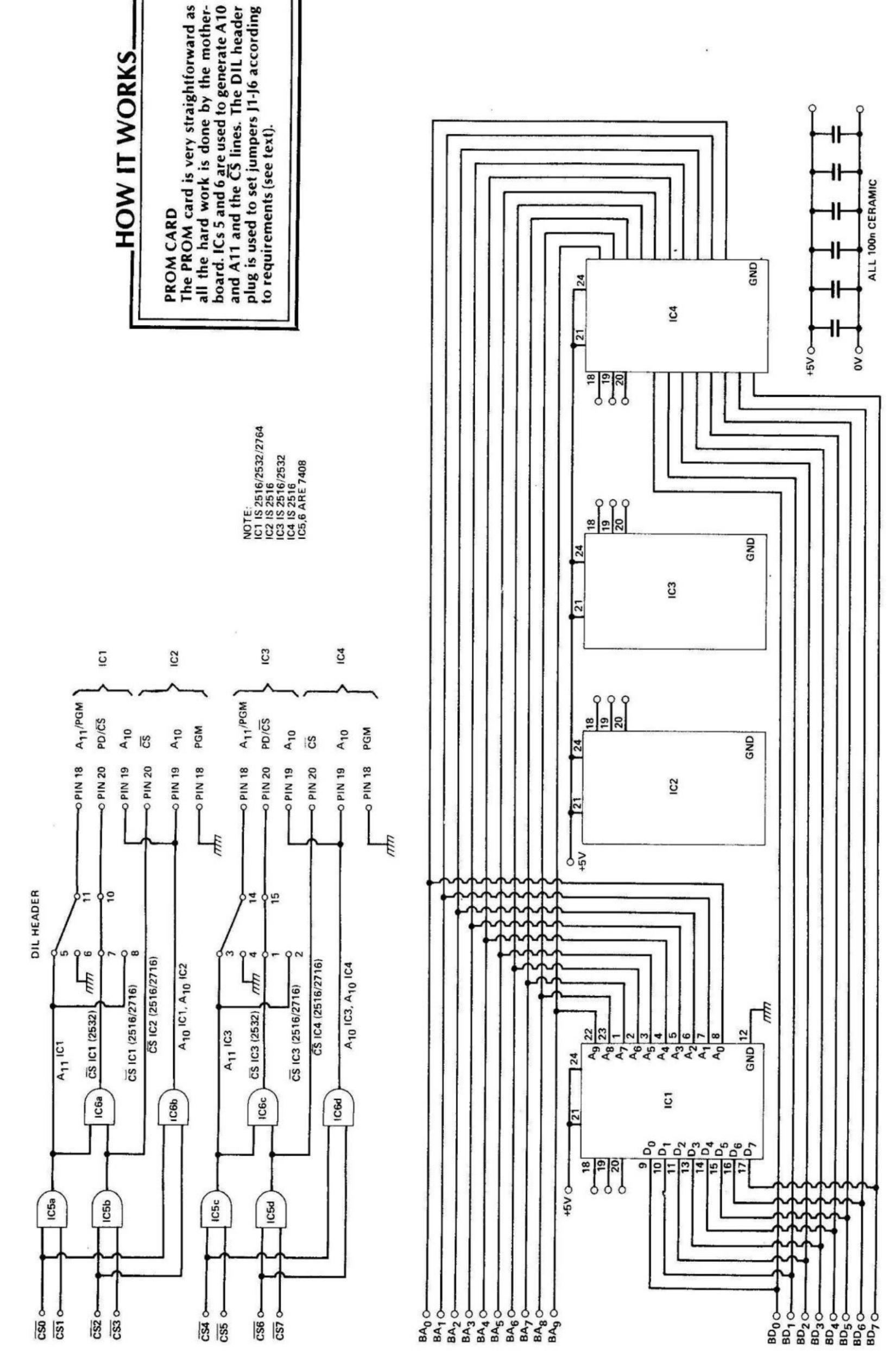
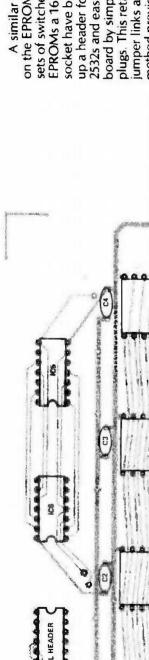


Fig. 5 Circuit diagram for the EPROM card. Links soldered to a D1L header select the correct signals for the various combinations of EPROMs — see Fig. 7 for details.



2532s and easily change the role of the plugs. This retains better flexibility than method previously considered. The DIL socket have been used. You can make on the EPROM card. As there are four A similar method has been used umper links and is cheaper than the neader plug can be wired as in Fig. 3. board by simply exchanging header up a header for four 2516s and two EPROMs a 16 pin header plug and sets of switches needed for four Refer to Fig. 7 for an

explanation of how the header plug is

wired

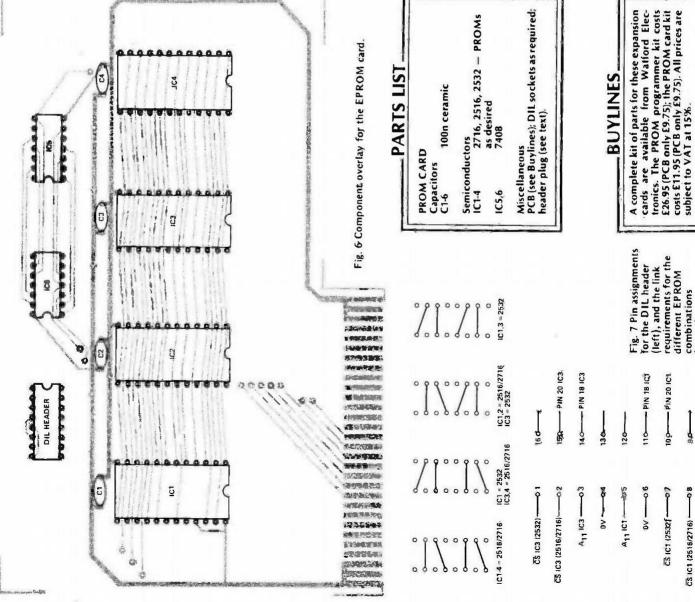
Construction

Construction of the two boards is overlays given here. Note that if you memory then simply break the connections CS5, CS6 to CS2 of the 6520 and re-make to the CS line you very straightforward — follow the want to move the card around in desire

bring the 30 V AC from the transformer computer that has supply rails of 0 and PCB to generate the V_{pp} voltage, it is about the only practical way from a using a transformer mounted off the Use two Veropins or similar to to the board — unfortunate as it is

Fit the 28 pin DIL socket at the IC1 position on the EPROM board. This is to allow experimenters to fit a 2764 8K

specifications. To mention one use: you customising your system to your own ROM and then while writing a BASIC When you have finished you will program simply renumber by calling could burn a renumber routine into have a very powerful means of the routine through the USR(X) chip at a later date. unction



above).

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2532 450ns

2732 450ns

2732 350ns

4116 200ns

4116 150ns

4118 200ns

4118 150ns

5516 200ns

6116 200ns

EF6845P

8195

8T97A

6116LP 200ns

6116LP 150ns

CRT CONTROLLERS

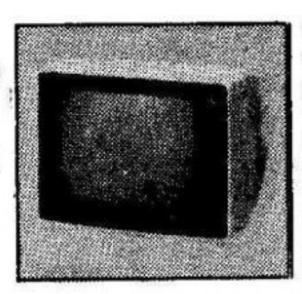
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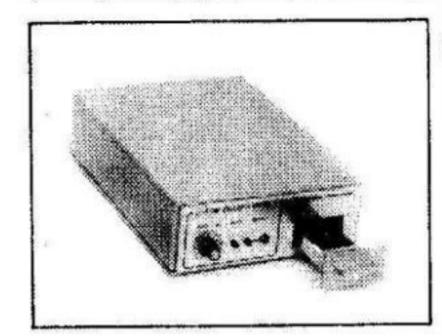
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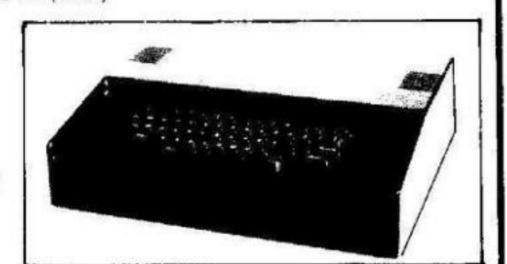


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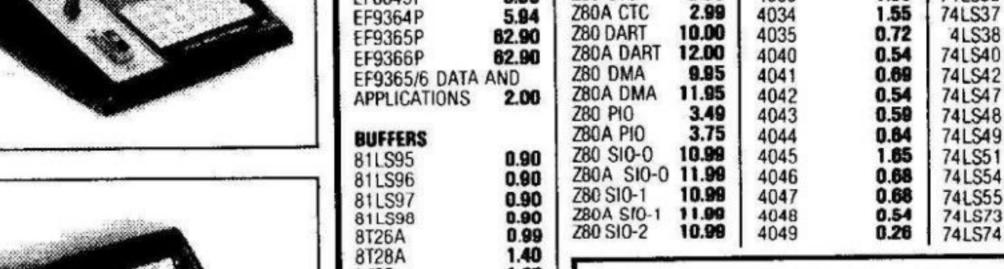
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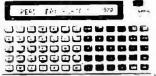
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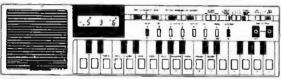


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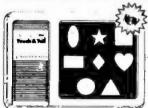
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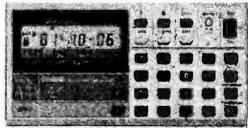
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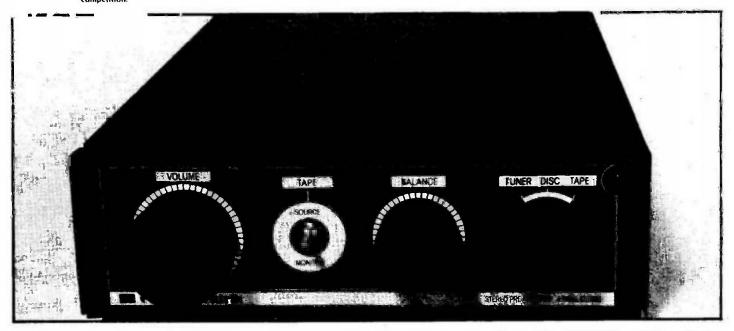
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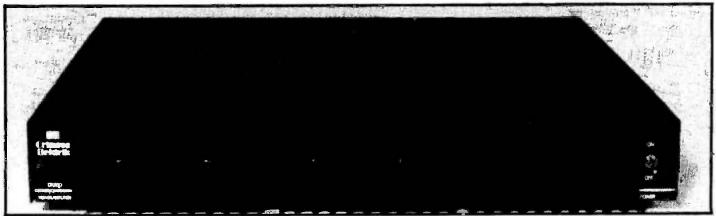
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This amp is designed particularly with music in mind. We anticipate usage often at only 50W to 100W average levels leaving 10dB of headroom.

PFA 500

This module uses 8 H-PAK powerfets and is designed to produce a continuous RMS output current of 25 amps and will run from a supply of up to ± 70 volts. The Unit will drive 250W continuous RMS into 8 ohms, 450W into 4 ohms, 600W into 2 ohms and 700W into 1 ohm.

Numerous features are included in the board to optimise efficiency. The H-Paks (thermally more efficient than TO3) are presented at ninety degrees to the P.C.B. so they can bolt directly onto the heatsink, instead of via the usual angle bracket. The resultant chip to heatsink thermal resistance is very low keeping junction temperatures down and efficiencies up. The Powerfet supply rails are kept separate from the rest of the amp. This enables the driver stage to be run from slightly higher rails resulting in larger undistorted output swings at little extra cost.

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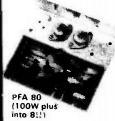
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Powerfets

Power Supply

So far 29 semiconductor manufacturers have invested in this new technology. Clearly powerfets

So far 29 semiconductor manusquiries in account of the circuitry in power amps, permitting are something special. Their enormous power gains eliminate conventional drive circuitry in power amps, permitting delightfully simple designs. Their freedom from secondary breakdown and their fulldenby to shuddown when thermally overstressed result in inherently stable and destruction proof output stages, not needing protection circuitry. And perhaps best of all, their lack of charge storage make them fast and responsive, producing amplifiers of wide bandwidth and low distortion even at high



PFA 120 (150W plus into BS

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Components available The PFA is perhaps the perfect realisation of the classic powerfet amp design. This superti PCB allows the use of either one or two pairs of output devices, providing easy expandability for those starting with the smaller system. (The eatia culput pair of the PFA120 results in lower distuttion and improved efficiency, particularly into low impedance loads). The components used in the PFA have been chosen with extreme care. The lowest noise input devices and lowest distortion gain stage devices were selected regardless of cost. 140V primartets were chosen against the more usual 120V to give improved safety margins.

Specification Bandwith	PFA80 10hz	PFA120 100KHz 1dB
RMS into 811	80W IVa = ± 50V)	120W (Va = ± 56V)
THD (20Hz 20KHz)	≈0 008	≤ 0 005
(KHz at rated	0.004 % Type	0.002 http://
SNR	12008	
Slew Rate	>70V µS	
Gan	X22	
Rin	30K	
Vs man	± 70V	
Cost		
(tuott)	£17.46	624.00 P B P 7
(kit)	£14.96	C21.66

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Specification
Output power RMS

20W into 8\$2 at : 22V 20W into 4\$2 at : 19V 0.02% at 1KHz IW to 12W 90dB

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Mains transformer for above 17 0 170 50VA 73 95 (P. & P. Et)

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Specification B W THD

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Cost
(built board less controls) (P. B. P. 40p)

20Hz-30KHz ± 1dB

85 dB (ref. 5mV RIAA) 106 dB (ref. 100mV flat) ± 20V 1V (clips at + 20dB)

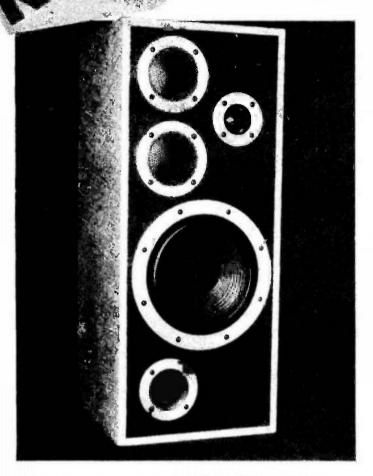
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Fancy a pair of Wharfedale E70s? Can't afford them? Then why not build 'em yourself?
Peter Freebrey underwent the mystic rites of woodworking and saved himself over £100.



or many years now there have been speaker manufacturers who have marketed kits for the 'do-it-yourself' audio enthusiast. At the present time there are several well known and respected firms supplying high quality kits. One such firm is Rank Hi Fi who manufacture the Wharfedale range. Their approach to this market is the Wharfedale Speakercraft series of drive units and crossovers, together with the constructional information necessary to duplicate their ready-built units using these same components. If the demand is there someone will supply that demand ... such is the case with Wilmslow Audio who sell kits of the cabinets to suit the Wharfedale units. This review follows the construction of the E70 system using the WE70 flat-pack cabinet kit.

Why build loudspeaker kits? Well, one obvious answer is to save money; often the cost of a kit is very much less than buying the completed unit. If you are reasonably competent at woodwork, it is perfectly feasible to start from scratch with just a large sheet of flooring grade ¾" chipboard. An electric power saw makes the job much easier and can also give a better edge to the cut. It is often the edges which concern people as they are going to be visible somewhere around the loudspeaker cabinet and it is easy to think that to get rid of the ugly sight of these will be difficult. This is not necessarily true; there are several ways in which unsightly edges may be hidden from view. The simplest answer is not only to buy a kit of speakers, crossovers, and so on, but perhaps to buy a ready-cut cabinet kit as well — this does not rid you of dealing with edges, but at least they are all cleanly cut!

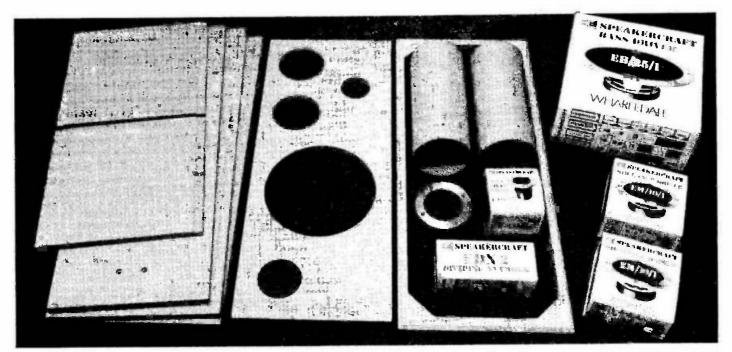
I had heard that Wilmslow kits were of a very high standard several people having commented upon the ease with which they went together. That sort of build-up sometimes takes a bit of living up to and I waited for the delivery of the WE70 kit with some uncertainty. When they arrived my initial reaction was favourable; all cuts were clean and the method of construction looked simple and sensible. The sides, top and base are rebated by about 1/2". This not only gives you a better mechanical joint, but also makes it almost impossible to get any voids or gaps which is good, acoustically speaking. It also means that with the minimum of care the cabinet will slot together into its correct shape with no unsquare corners or leaning sides. Included with the kit were two cardboard transmission tubes for the mid-range units, acoustic damping material, grille material (both black plastic foam for the reflex port and cloth for the front), nylon grille plugs and sockets, 3 mm wander plugs and sockets for loudspeaker lead connections, and the screws to fix the speaker units themselves. Last but not least there are written instructions on how to assemble the kit.

16 Steps To Heaven

Step one in the instructions is to examine the panels for transit damage. Presumably if any damage is noticed, Wilmslow Audio should be contacted as soon as possible. Step two is to remove all dust, etc from the panels. Any excess of wood dust from the sawing operation can only do harm so vacuum all surfaces. If there were any build-up of sawdust at the surfaces to be glued that sawdust could conceivably impair any glue joints and also cause the fit of the joints to be out of true.

Step three is to assemble the cabinet without gluing to check the fit. It is also suggested that panels be swapped around to find the optimum results. This step proved to be most encouraging... I assembled one unit (panels only) and held it together with just one turn of linen tape (no string please — it can bite into the corners of the chipboard and cause you extra work later). The cabinet felt as firm as a rock. No glue, just well-fitting joints. Thus encouraged I rapidly got on to step four, which was to paint the face of the baffle board matt black. I gave it a couple of coats of sanding sealer — not so much to get a 'de luxe' finish but to seal the wood surface. Chipboard is pretty thirsty stuff and you can use up a lot of paint if you do not seal the surface first. Just be careful not to get any of the sealer or paint on the edges, as this may affect the glue joint you have to make later.

Step five is to glue the midrange enclosures (transmission tubes) to the baffle boards, using plenty of glue to ensure an airtight seal. The baffle boards are recessed to take the cardboard tubes so it is easy to line up for position. I used Evostik Resin W, which is a PVA wood-working adhesive for all glue joints. It is easy to apply and may be cleaned off the hands/clothes as it is water soluble. Just don't put your speakers out in the rain! Light pressure to a PVA glued joint gives a better joint so I placed one of the side panels across the top of the four tubes to ensure a light even pressure. Rather than apply liberal amounts of glue in one dose I used sufficient so that a *small* bead of glue was squeezed out all around the tube. This was smoothed around with a handy finger and when dry a further fillet of glue was applied all round the tube/baffle joint. Four pieces of approximately 1" thick polyurethane foam are supplied which must be



glued to the rear (outside) end of the baffle tubes. Wharfedale recommend a hard rubber pad at this position but as this 1" foam is to be compressed to about 3/16" it probably is just as good.

Stepsix is probably the most critical point in the whole construction procedure, for at this point the cabinet panels are glued together. This entails gluing five of the six panels; the sixth (the side furthest from the mid-range enclosures) is placed in its position while the glue is setting but is not glued. This enables you to work inside the cabinet; fitting the crossover, acoustic wadding etc.

Wharfedale suggest that the acoustic wadding be attached to the inside of the panels before you reach this step. Wilmslow Audio suggest that the wadding be fixed after the panels have been glued. Although I only learnt of Wharfedales' suggestion after I had completed step six, I favour the Wilmslow approach for several reasons.

If the wadding is stuck/tacked or stapled to the panels before they are fitted together two things may happen: 1) some of the wadding may inadvertantly get caught between the panels and cause either an air gap or 2) force the cabinet to go together 'out of true'. Also, with the wadding in place you cannot inspect the inside corners to check that there is a continuous fillet of glue all along the joint.

If you choose the Wilmslow way you will have to cut the wadding to fit around the mid-range enclosures but in practice this proved to be a very simple task.

Getting A Grip

Holding the whole thing together while the glue sets is quite a teaser. I was fortunate to have a set of excellent clamps known as Jet System Clamps made by TMT Design Ltd of Learnington Spa. They cost about £10 per clamp but are worth their weight in gold for this type of job. The problem comes from the 1" thick foam stuck to the rear of the mid-range enclosures; this tends to force the back panel out of position. Wilmslow suggest either that clamps be used or that the joints be held firmly together with masking tape. It is possible with masking tape but only just; remember that unlike your trial fitting in step three, the foam pads are being compressed to about 3/16" and all but one panel has glue all along the edges and is quite capable of sliding all over the place! I bought a wide webbing strap from a camping shop to assist the initial stages of holding the four vertical panels approximately in place while I set up the clamps. The cost of the strap was wasted as I could not get enough tension in it to overcome the spring in the foam... a linen tape would have done just as well! If you are going to use masking tape then get someone to help apply the pressure to hold the front and back panels in position while you apply the tape. Lastly, cut up a thin polythene bag and place four pieces inside each corner of the panel that is not to be glued; it would be a shame if this stuck firmly to the rest of the panels by accident!

It is useful to have a rubber-faced hammer at this stage as, having clamped or taped the cabinet firmly together, you may wish to tap the panels firmly but lightly into position. A hammer and a block of wood do the trick just as well, but try not to mark or dent any edges. The places to look for out of true joints are the corners . . . remember once the glue has set there is nothing you can do, so a few light taps now can save the day. Wipe off excess glue with a damp cloth. Wipe from the centre of each panel out towards the edge; try not to get any glue smeared over the panels.

Having completed step six the rest of the construction is plain sailing. Step seven is simply to remove the loose side when the glue has set (leave for at least 24 hours). I then put a small fillet of glue all around the inside of all joints BUT not up to the edges where the last panel is to fit... we want it to go back from whence it came!

Step eight is to place the drive units and reflex port trims in the baffle board and mark accurately where pilot holes for the fixing screws are to be drilled. Although the chipboard is high density it has a fairly soft texture so it is well worth buying a new ½ " drill bit. This ensures the pilot holes are clean and in the right place . . . worn bits tend to wander! Although I'm sure it is unnecessary I drilled all my pilot holes just deep enough for the screws by slipping a small rubber sleeve over the drill bit at the right depth. No-one could accuse me of having any extra holes or air gaps here!

Step nine is to position the grille frame on the front of the cabinet with the cabinet lying on its back. Use masking tape to hold it in position and carefully drill a pilot hole through the grille and into the baffle board. I used a 1/16" drill bit and drilled four holes, one in each corner section of the grille frame. These holes can now be drilled out to the correct size to accept the nylon plugs and sockets that hold the grille in place. Wilmslow supply eight plugs/sockets for each grille but as Wharfedale suggested that four would be sufficient I chose the latter. It is far easier to line up four holes than eight! For the socket in the baffle board I used a 7/16" bit and for the grille a 7/32" bit. Don't forget to drill only from the rear of the grille and only to a depth of ¼-5/16". The 1/16" pilot hole may be filled with wood filler

but when the grille material is fitted I doubt that these holes can be seen. If you are happy with the finish on the baffle board then glue the sockets in now; if not, then wait until you have quite finished before fixing them in position. Do not stick the plugs in the grille until you have fixed the material in place. I used a quickset epoxy glue for these fittings.

Step 10 is to glue the black, acoustically transparent foam over the inside of the reflex port aperture. You can use either PVA glue or quickset epoxy, just be careful not to get any of the

adhesive on the foam where it is over the port.

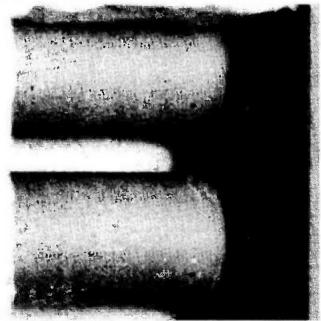
Step 11 is to position the crossover network inside the cabinet on the rear panel opposite the bass unit aperture. Before you screw it into position check that the leads from the drive units can reach their appropriate tags! Wharfedale recommend that the crossover has a piece of felt or foam between it and the panel to prevent any vibration rattles. Also in step 11 is the fitting of the input terminals through the rear panel. I smeared the threads on these sockets with some latex glue, again to ensure that there would be no air gaps. Solder the leads from the crossover to these terminals... make sure they are connected correctly, red to red and black to black!

Step 12 is to cut three 5" discs of wadding and place these in the mid-range tubes. The Wharfedale instructions that come with every Speakercraft unit specify that the packing density of this wadding should increase towards the back of the tube and that the tube should be completely filled with wadding. In view of this I cut two extra discs and fluffed out those towards the

front of the tube.

It's In The Bag

Step 13 is to line the inside of the cabinet with the acoustic wadding and glue the remaining side into place. Now comes the tricky bit — how do you slide the wadding up behind the midrange tubes? The wadding catches on the side panel and snags up behind the tubes! Easy — get a large polythene bag 12" or more wide and about 15" to 18" long, slide the wadding into the bag, slide the bag plus the wadding up behind the tubes and, lightly holding the wadding in place, pull out the bag. Cutting the wadding to fit round the tubes sounds fiddly but turned out to be quite easy. Cut the holes for the tubes smaller rather than larger as the wadding will easily stretch to fit comfortably in place. No wadding is required on the baffle board but don't forget to put wadding on the loose side panel before you glue it into place! The wadding may be tacked or stapled into place.



The wadding is tacked or stapled in place.

Step 14 is to attach the wires to the drive units — observing the correct polarity (if in doubt refer to the Speakercraft instructions and double-check every connection), and screw all units and ports to the cabinet. Wire up and fit the bass unit last as the bass aperture gives you ample room to work inside the cabinet connecting wires to the crossover. The wires from the mid-range units come through small holes in the tubes and these holes should be sealed after you have connected the wires to the crossover. The fitting of the drive units should only be started after the glue joints of the final side have thoroughly set and any glue fumes have completely cleared. The comment regarding fumes is highly pertinent if you are not using a water-based adhesive. There is a possibility that the fumes could affect certain plastics used in the construction of the drive units.

Step 15: You have two working loudspeaker systems, so connect them to your amplifier and sit back and enjoy your

favourite record.

Step 16: The cabinets are now ready for their final cosmetic treatment. There are a number of options open to you: they may be:

veneered either by you or a local cabinet-maker.

covered in iron-on veneer or plastic laminate.

 sealed and then painted (preferably sprayed) in colour of your choice.

 Wilmslow Audio also suggest the use of a 'Contact' type covering as these can be obtained in very realistic wood-grain finishes.

Whichever method you opt for you will probably have to attend to the cabinet edges/joints before you can proceed. Due to the small but noticeable tolerances in the cutting of the panels, the amount of glue and the pressure used during the construction, there are likely to be a few panels that are slightly proud of the edges that butt up to them. There are several ways to solve these problems but the simplest is to use one of the proprietary wood fillers. Which choice depends upon your choice of finish.

If the cabinets are to be covered in plastic laminate you can afford to use one of the more easily worked fillers such as Fine Surface Polyfilla, Alabastine or Plaster of Paris. If, on the other hand, you are going to cover them with 'Contact' or simply spray-paint them then I would suggest a tougher type of filler that is less likely to crack or crumble. My choice here would be one of the car body fillers — they are easier to sand than some of the loaded general-purpose fillers from the DIY shop. So you are less likely to sand away the wood from the cabinet instead of the filler!

The grille material must be stretched over the grille frames and either tacked/stapled or glued (or both) to the inside of the frame. The material supplied by Wilmslow Audio stretched easily and evenly; I smeared PVA glue over the rear faces of the frames (having first painted them black) and stapled the material in place while the glue set. When set I trimmed off the excess material (having removed the 50-odd staples) and ran another bead of the adhesive over the edge of the material.

Looking back on the construction of this E70 loudspeaker system using the WE70 flat-packs, I can only say that I am very satisfied with the way they went together. There were one or two instructions that could have been a little clearer but they have been covered in this article. Common sense would probably have solved any uncertainties but I chose to phone Rank Hi Fi to confirm my conclusions. The people I spoke to did not know that I was writing this review and so it is a pleasure to say the they could not have been more helpful. This entire project has been enjoyable from first to last.

-BUYLINES.

Wilmslow Audio self the complete WE70 package (flat pack, drivers and all components for two speakers) for E220 plus E8 carriage. Wilmslow Audio, 35/39 Church Street, Wilmslow, Cheshire SK9 1AS.

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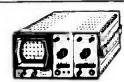
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PROJECT

AUTOMATIC CONTRAST METER

What's black and white and read all over? Answer — a photographic negative, providing you've built this simple and useful device. Design and development by Rory Holmes.

ontrast ratio is a very important quality of photographic negatives that must be assessed during the printing process, in order to select the correct grade of photographic paper. The contrast of negatives depends on the type of film used, the lighting conditions and the developing process; consequently five grades of printing paper are available to enable the full range of tones from black to white to be reproduced from any negative. Grade 1 is termed the softest and it is used with the highest contrast negatives. At the other end of the scale, grade 5 is the hardest paper, which will enhance the tonal variations of poor contrast negatives.

During the design stage of this project we experimented initially with two separate photodetectors which measured the instantaneous light difference between two points. There are a number of problems with this approach, as the photodiodes and their associated amplifiers must be carefully matched in light sensitivity.

Secondly, the lightest and darkest points of the image must be known exactly, and the two photodetectors need to be simultaneously positioned on these points while the reading is taken. This is an awkward business at the best of times, but especially so in a darkroom!

We considered that a different

approach was required and developed the circuit of Fig. 1 to overcome some of these difficulties. Only one photodetector is used and the peak positive and negative voltages obtained from different light levels are followed and stored independently by sample and hold circuits.

Now, as long as the photodiode is scanned at some time through the lightest and darkest points of the image, the peak detectors will memorize the maximum and minimum voltages, and thus provide a contrast measurement.

The photodetector input stage of our meter is rather unusual in its configuration. Photodiodes are usually

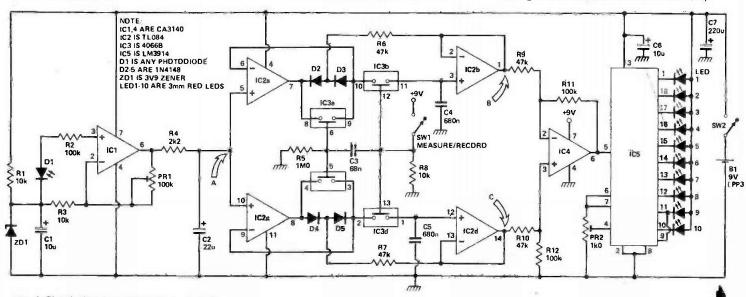


Fig. 1 Circuit diagram of the Contrast Meter-

used in the 'photovoltaic mode' where the photocurrent developed and measured is linearly proportional to the light intensity. Our input amplifier has an extremely high input impedance and thus measures the open circuit voltage generated by the photodiode. This voltage is logarithmically proportional to irradiance as the graph of Fig. 2 illustrates. This is a very convenient property since the sampling circuitry can now work on the log of the light level to provide maximum and minimum values. By simply subtracting these two values with a differential amplifier we obtain a voltage that is logarithmically proportional to the ratio of the maximum and minimum light levels, ie the contrast.

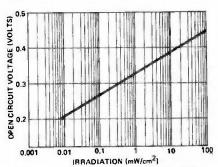


Fig. 2 Response of the photodiode used in this project.

Meter Made

The ETI contrast meter was intended primarily to determine the paper grade for a well balanced print; consequently a 10 LED bargraph type meter is sufficiently accurate for calibrating the five grades of paper. At today's prices this also works out somewhat cheaper than a moving coil meter and is less prone to damage. After calibration, the meter will be found very easy to use. It is switched on with the 'sample/hold' switch in the 'hold' position and placed down flat on the enlarger base with the photodetector probe anywhere in the image area. (The photodiode has been mounted in a separate probe with its amplifier in order to keep it as close to the focused image plane as possible. If it were much higher than this the detecting element would pass through an unfocused image, giving a false contrast reading).

Any red safety lights should be switched off before the reading is taken to avoid error since the photodiode is responsive at this wavelength. The sample/hold switch should now be moved to the sample position; this will clear any previous reading and start measuring light variations. Now the photodiode may be moved across the image and through the areas that look the brightest and darkest. This can be

done quite slowly thanks to the peak detectors' long memory time; however, several areas should be scanned to ensure the recording of the true maximum and minimum. The eye can be deceived quite easily by those cunning optical illusions lurking among the shades of grey!

During the scanning process the reading on the LED scale will increase and finally level-off at the true contrast ratio when the black and white peaks have been covered. Before removing the meter from the image area the sample/hold switch should be set to 'hold'. The meter will now be immune to further light variations and will continue to display the contrast reading for a considerable time, thanks to the even longer memory of the sample/hold circuitry!

A true ratio is provided by the meter and thus the contrast reading for a given negative will be independent of the light source intensity and enlargement size (photographic aberrations known as "circles of confusion" may produce sources of error under certain conditions). Negatives may thus be compared or matched for contrast.

Construction

The meter is built into a slim style plastic enclosure produced by ÖK Machine and Tool company. This houses the battery and main PCB on which all the parts are mounted. Since the light sensing element must be as close to the enlarger base plane as possible, we have mounted it externally on a separate small PCB with its associated amplifier. A probe to house the external sensor is made from a short length of aluminium channel extrusion. Figure 3 shows the

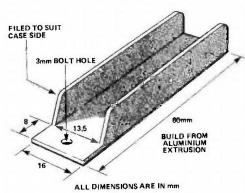


Fig. 3 Details for the aluminium extrusion that houses the photoprobe.

dimensions for the probe; if the aluminium channel proves difficult to obtain, a piece of the slotted aluminium extrusion used for commercial shelf-racking systems is ideal. This is available from most DIY

stores in short lengths with the required internal width. After filing or cutting to the right size, a piece of insulating tape should be stuck down on the inside to prevent shorting out the PCB. As shown in the diagram, a hole is drilled on the end for bolting it to the bottom of the case. This bolt should eventually be connected to circuit ground, thus providing screening for the photoamplifier. The two PCBs for probe and main meter circuits are laid out as one board, and should be sawn apart along the lines shown on the foil patterns.

For other construction arrangements, the circuit can be left as a single board, since the interconnections are already made.

Three wires are used to connect the two boards together as indicated on the overlay; these should pass through a small hole drilled in the case side where the metal probe case is bolted on. When the probe board is mounted and stuck down in its channel, a piece of thin aluminium sheet is cut to form a lid with appropriate holes for the photodiode and preset. (The photodiode case is internally connected to the cathode, so it must not short against the lid).

Calibration

Start with preset PR1 fully clockwise to set a gain of 1; also set PR2 fully anticlockwise, setting the voltage required to illuminate the lower end of the bargraph at zero. First, measure a high contrast negative that is known to require grade 1 paper for a good average contrast after developing. Initially a low contrast reading will be obtained, say about grade 4 or 5. Now, adjust PR1 anticlockwise to increase the gain of the photoamplifier. Take another measurement, when the contrast reading should be greater. Repeat this process until a grade 1 is consistently recorded.

Now select a negative with very poor contrast ratio, one known to require paper grade 5 for bringing out the contrast. Take measurements several times while adjusting only PR2 clockwise, until the bottom end of the scale illuminates at grade 5. The other contrast grades should now fall linearly between these points and can be checked for accuracy.

Although the bargraph display has a low resolution and accuracy, the rest of the metering circuit is obviously much better than this; consequently a moving coil meter could easily be added to measure the contrast voltage for those who may desire greater resolution.

HOW IT WORKS

The general circuit arrangement consists of photo-amplifier which feeds a voltage derived from varying light levels in an enlarger, to a pair of peak detectors. One follows the peak positive voltage and the other the peak negative voltage. The capacitors used for storing the voltage peaks in the followers also form part of sample and hold circuits which are then switched to 'hold' after measurement. Their outputs represent the maximum and minimum values of light intensity. A differential amplifier then computes the ratio of these values and the result is displayed on an LED bargraph meter.

IC1, a CA3140 CMOS op-amp, is used as the photodetector amplifier. It is configured as a non-inverting DC amplifier with a gain variable from unity to about 10, set by PR1. Although IC1 can have input and output voltages all the way to ground, this facility is not used owing to the driving requirement of the TL084 quad op-amp. This requires inputs at least 1 V above ground, and thus IC1's output is offset by a reference voltage of 3V9 provided by R1, ZD1 and C1. The anode of the photodiode is connected via R2 to the non-inverting ter-minal of IC1 which has an effectively infinite input impedance. Thus the open circuit voltage generated by the photodiode is amplified according to the gain set around IC1 and appears at the output on pin 6 added to the reference voltage.

The voltage at point A (ignoring the reference offset) will be logarithmically

proportional to the intensity of incident light, owing to the properties of the photodiode (see Fig. 2) R4 and C2 form a simple filter to remove 100 Hz ripple caused by AC mains bulbs. This voltage is fed directly to the peak detectors. These circuits are essentially the same, the difference being the polarity of the rectifier diodes. They operate in exactly the same way, and we shall deal only with the peak positive voltage follower.

Assume initially that the CMOS analogue switch IC3c is open and IC3d is closed. C5 will be connected to the output of op-amp IC2c via the rectifiers D4 and 5 (we can ignore the action of R7 for the moment). C5 will charge up via the rectifiers to the most positive voltage peak when the voltage at point A on the non-inverting terminal is greater than the capacitor voltage applied to the inverting terminal. The voltage held on C5 will droop over a period of time due to leakage current through the rectifiers D4 and 5 and the input bias current of IC2c. IC2c was chosen as a FET opamp with a low input bias current and R7 is included to reduce the diode leakage cur-

IC2d is connected to C5 as a straighte forward high impedance voltage follower to buffer the stored voltage. When the input voltage to IC2c at point A drops below the peak value, IC2c's output will go negative, reverse biasing D4. However, IC2d applies the capacitor voltage via R7 to the anode of D5, effectively removing

leakage current through D5.

The peak positive value of the signal at A thus appears at point C, and likewise the peak negative value at point B. When the analogue switch IC3d is now opened, C5 is disconnected from the peak detector and acts in conjunction with IC2d as a sample and hold circuit thus isolating the measured values from further light variations.

When SW1 is open, R8 and R5 hold the control pins 13 and 5 of IC3 low, opening both analogue switches. This is the 'hold' mode. When SW1 is now closed, the control pin 13 is taken high, switching to the 'sample' mode. C3 and R5 produce a positive pulse (about 50 mS) on control pin 5 to briefly short out D4 and D5, so resetting the peak detector to the current voltage at point A. When C3 has charged the IC3c switch will open again, allowing the peak detector to function.

IC4 is wired as a differential amplifier with a gain of 2, to subtract the voltage at point C from point B. Since these voltages are the log of the light levels, the output on pin 6 will represent the contrast ratio of

these light values. IC5 is a standard LED bargraph driver, the LM3914. The input voltage on pin 5 is converted linearly to illuminate one LED on a scale of 10. Full scale deflection (LED 10) is set internally at 1V2; the zero scale deflection is set by PR2 anywhere between 0V and 1V2 during the calibration process. C6, a 10 uF tantalum, is required for IC5 to ensure stability from oscillation.

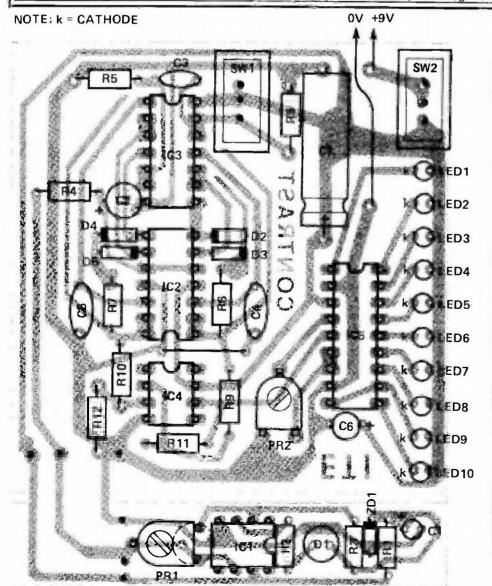


Fig. 4 (Left) Component overlay for the meter (showing the board uncut).

PARTS HIST

	PAKIS USI
Resistors (al	[¼ W, 5%)
R1, 3, 8	10k
R2, 11, 12	100k
R4	2k2
R5	1M0
R6, 7, 9, 10	47R
Presets	
PR1	100k subminiature horizon-
	tal preset
PR2	1k0 miniature horizontal preset
Capacitors	
C1	10u 35 V tantalum
C2	22u 25 V tantalum
C3	220u 16 V electrolytic
C4, 6	82n polycarbonate
C5	68 n ceramic
Semiconduc	
IC 1,4	CA3140
IC2	TL084
IC3	4066B
IC5	LM3914
D1	8PX65
D2, 3, 4, 5	
LED1-10	3 mm red LED
Miscellaneo	
SW1, 2	miniature slide switches
	ylines); PCB (see Buylines); B1 tery (preferably alkaline type).

BUYLINES.

The photodiode specified in the Parts List is the one used in our prototype, but any general purpose type should do. The case we used is a Pactec type HP, size 146 x 91 x 28 mm. The PCB is available from us using the order form on page 44 — price is £2.12.

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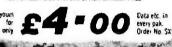
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DESIGNERS NOTEBOOK

Five into one does go. This month Don Keighley explains all about sampling and time-division multiplex systems, and looks closely at the advantages of pulse-width modulated telecommunications networks.

ampling is a process we can undertake if we want to combine many different signals on to a single transmission line. The transmission line can be of any type such as wire. radio, or optical. Combining several signals into one is called 'multiplexing' and can save the expense of having many separate lines. Sampling is used in a specific type of multiplexing called time-division multiplexing (TDM) which I'll explain later. The other form of multiplexing — frequency-division multiplexing(FDM) — is the basis of all standard radio transmissions. Each signal to be transmitted is mixed with a carrier wave (or radio frequency) on to a set frequency within the radio spectrum. Thus many signals can be transmitted and received by radio link — one on each defined frequency of the radio spectrum.

Figure 1 shows an illustration of sampling. In the figure, a sinusoidal signal (known as the message signal) has a series of values taken at regular intervals. These sample values can be used to represent the message signal. For instance, we can pass the actual DC values of the samples, ie their voltages, along the line. At the other end of the line the sample values, or pulses as they are usually called, are converted back into the message signal, simply by passing them through a lowpass filter. The filter removes the high frequency pulses and thus re-creates the envelope of the original message signal — as shown by the sinewave of Fig. 2.

One of the most important questions arising is — How often do we need to sample the message signal? It is obvious that if the signal is sampled too few times we won't be able to

reconvert the pulses into the message signal at the receiving end of the transmission line.

The minimum number of samples is given by the sampling theorem, which states that a message signal of bandwidth B Hz can be represented by a set of sample values taken at a frequency of 2B Hz. For example, an audio system has a frequency response of 20 Hz to 20 kHz. Its bandwidth is thus 20,000-20=19,980 Hz. The audio signal of the system can thus be represented if samples are taken at $2 \times 19,980$ Hz = 39,960 Hz.

But the *minimum* number of representative samples (2B Hz) isn't the *easiest* number of samples to convert back into the message signal. It's usual to take a greater number of samples because doing so makes the reconversion easier. To see why this is so we've got to take a look at the spectra of the transmitted samples and see how they differ when different sample frequencies are used. Figure 3 shows the possible spectrum of a message signal such as an audio signal. It's the sort of result you would see on the screen of a spectrum analyser. Frequency f_m is the maximum frequency contained in the signal. The lowest frequency contained is $0 \, \text{Hz}$ (the signal extends down to DC); so the bandwidth of the message signal is $f_m - 0 = f_m \, \text{Hz}$.

When the message signal is sampled at a frequency f, the overall spectrum looks something like that shown in Fig. 4 and consists of components at harmonics of the sampling frequency, with upper and lower sidebands around them, as well as the original spectrum of the message signal. In Fig. 4 you can see the sampling frequency, f, is more than twice f, — hence there is a gap between the highest frequency of the higher sideband of a

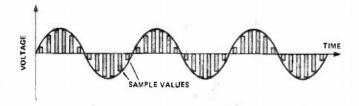


Fig. 1 A message signal can be represented by a series of sample values of the signal.

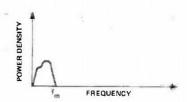


Fig. 3 Power density spectrum of typical audio signal. The higher frequency component in the signal is f_m . The signal extends down to θ Hz, so the bandwidth of the signal is f_m Hz.

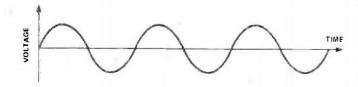


Fig. 2 If the series of sample values is passed through a lowpass filter the original message signal is recreated.

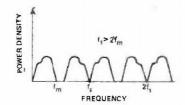


Fig. 4 Power density spectrum of an audio signal, sampled at a frequency of f_c . In this example, f_c is greater than $2f_m$.

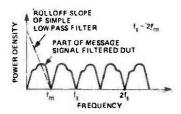


Fig. 5 Sampling frequency f_s equals $2f_m$. A simple lowpass filter may filter out some of the wanted message signal.

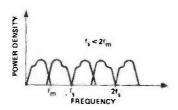


Fig. 6 Sampling frequency less than 2f_m. A lowpass filter cannot be used to recreate the original message signal.

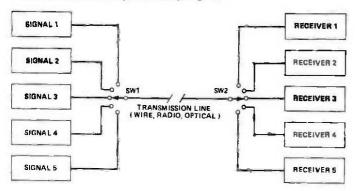


Fig. 7 A simple time-division multiplex (TDM) system.

component and the lowest frequency in the lower sideband of the next component, This gap between bands means that a simple lowpass filter can be used at the receiver to pass only the message signal and not the higher components: so the message signal is recreated.

With a sampling frequency of only $2f_m$ (Fig. 5) the highest frequency of one band and the lowest frequency of the next occur at the same point. A simple lowpass filter would filter out some of the message signal, as shown in the figure. A more complex lowpass filter (with a steeper roll-off slope) could be used to correctly recreate the message signal.

In Fig. 6, f, is less than 2f_m and, as you would expect, the spectrum shows how message signal and sidebands overlap. A lowpass filter cannot be used to recover the whole of the message signal without letting through part of the next sideband.

TDM Tricks

A simple TDM system is shown in Fig. 7, in block diagram form. Each signal to be transmitted is connected to an input of switch SW1. This switch, although shown in the diagram as a mechanical-type switch, will be of electronic construction in a real TDM system, so that a high switching speed can be obtained. The output signal from the switch is transmitted along the transmission line to switch SW2, which connects each receiver, in turn, to the line. Providing the switches are operating fast enough so that the sampling theorem is fulfilled ($f_x \ge 2f_n$) for all the message signals, everything is fine and we have five signals passing down one line.

The whole process of sampling and TDM is a form of modulation because only a representation of the message signal is transmitted, not the actual signal. And because pulsed samples of the message signal are transmitted, we call the process pulse modulation.

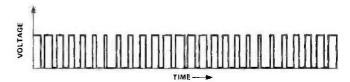


Fig. 8 Pulse-width modulation. The width of each pulse varies in accordance with the amplitude of the message signal.

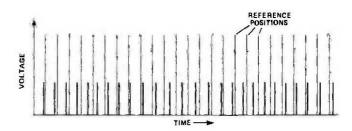


Fig. 9 Pulse-position modulation. Each pulse's position, with respect to a reference point, varies in accordance with the message signal amplitude.

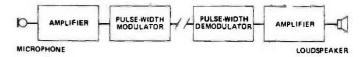


Fig. 10 A pulse-width modulation microphone/loudspeaker system.

There are various forms of pulse modulation which can be used in a TDM system, all relying on the fact that the original sample values control some property of corresponding pulses. The one just described uses the DC value (ie amplitude) of the pulses and is therefore known as pulse-amplitude modulation. Other forms of pulse modulation are: pulse-width modulation (where the width of the pulses is varied according to the sampled value) and pulse-position modulation (the position of the pulse, relative to a reference position, is proportional to the sample value). Figures 8 and 9 show examples of these pulse modulation systems and the sampling frequencies of both must follow the sampling theorem — the sampling frequency must be at least twice that of the message signal bandwidth. There is a final pulsed system, in which each sampled value is converted into a train of binary digits. This is, strictly speaking, a digital system and doesn't concern us here; however the system must still follow the sampling theorem.

Practical Matters

With careful design all the pulse modulation systems can give good results in TDM but perhaps the best — because it's easy to use, has a high immunity to interference and yet needs a minimum of component hardware — is pulse-width modulation (PWM). Figure 10 shows a block diagram of a PWM microphone/loudspeaker set-up — such as you might have in a multi-station intercom system or similar.

We can investigate the modulation and demodulation blocks in more detail, as in Fig. 11 and 12. Figure 11 shows a simplified pulse-width modulator. It consists of an oscillator to provide sampling pulses at a rate of over $2f_{mi}$, so that the sampling theorem is fulfilled. In a good quality audio modulator, the sampling rate is therefore over 40 kHz and the time between pulses must be $1/f_s = 25 \text{ uS}$.

The pulse duration is less than this, say 1 uS, and each pulse charges the capacitor C1 to full voltage. After charging, the capacitor is linearly discharged via the constant current source. The cycle repeats itself at every pulse. The capacitor's discharge rate is a product of the capacitor/constant current time constant, which should be about 2 uS. Comparator IC1 compares the ramp discharge with the incoming audio signal — when the non-inverting input voltage is above that of the inverting input

FEATURE: Designer's Notebook

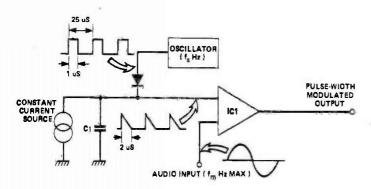


Fig. 11 A pulse-width modulator in detail.

the comparator output is high; when the non-inverting input is below the inverting input the output is low. Thus the output is high the instant of every sampling pulse, but falls low again after a time which is linearly related to the amplitude of the audio signal. In other words, the width of the pulse is modulated by the audio signal.

A pulse-width demodulator is shown in Fig. 12. A capacitor with a parallel constant current source is again used and the incoming width-modulated pulses cause a charge/discharge cycle similar to that in the modulator. The average DC level of charge across the capacitor is dependent on the width of the pulses — the wider the pulse, the higher the DC level. Buffer IC1 prevents loading of the voltage across the capacitor and the output is lowpass filtered by capacitor C2 to remove the sharp spikes of the sampling pulses, thus re-creating the original audio message signal.

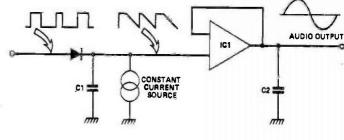


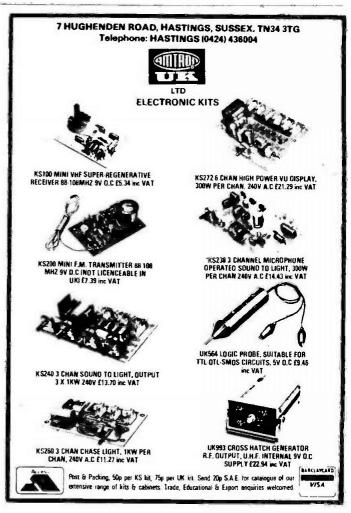
Fig. 12 A pulse-width demodulator can be built using the same basic components used in a pulse-width modulator.

The advantages of such a system aren't always immediately obvious, but you must remember that the audio signal is being represented by a pulse of nominal width 2 uS in a cycling time of 25 uS. This means that 12 different, high-quality audio signals can be time-division multiplexed down that transmission line simultaneously and without interference — and this is just a simple system. With a shorter nominal pulse width and more accurate modulators and demodulators, many more signals can be multiplexed on to a single transmission line.

It's all down to economics really. When you look at a large telecommunications system like the telephone network, there are literally thousands upon thousands of miles of expensive copper cable. By putting 100 telephone conversations down one line the overall cable cost is only 1/100th of that of a non-multiplexed system. Makes sense, doesn't it!

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SOUND EFFECTS 1: BOMB DROP

One of the attractions of the more sophisticated video games seen in 'fun' arcades these days is the realistic array of sound effects that go with the action — gunshots, bomb whistles and explosions, etc. Make some yourself with just one IC. Design by Phil Wait.

hose 'cannon shots' and explosions that go with the popular 'Space Invaders' video games and its variants add a measure of interest, feedback and stimulation to the action in which you participate on screen. Those sounds are electronically synthesised — that is, they consist of a complex mixture of waveforms that make up the required sound.

A 'bomb drop and explosion' is a remarkably complex sound when analysed carefuly. Looking at it simply, there is a descending tone followed by a burst of noise that dies away in intensity. The descending tone starts at quite a high pitch and is not a 'pure' tone (ie a sine wave). The explosion is a burst of noise that commences suddenly and dies away slowly in a recognisable way (usually exponentially). While it is possible to electronically produce very nearly an exact replica of a bomb drop and explosion, some compromises are acceptable to reduce the complexity and cost of the task and yet produce a recognisable replica of the sound.

To produce such sound using conventional components transistors, diodes, op-amps, resistors and capacitors — would require a whole legion of components. Fortunately, the IC maufacturers can come to our rescue here and much of the circuitry can be incorporated into a complex integrated circuit requiring the addition of a minimum of external components and the appropriate interconnections to synthesise the required sound. Generating a wide variety of sounds fortunately requires only a limited number of functional blocks, such as: a noise generator, voltage controlled oscillators, multivibrators, envelope generators (a sort of modulator), mixers and amplifiers. Tim Orr discusses such circuitry elsewhere in this issue.

Texas Instruments, the giant USbased component and equipment manufacturer, have designed a series of complex function ICs for various applications and among them is the SN76488 Complex Sound Generator. This chip contains both linear and digital circuitry and is intended for use in applications requiring audio feedback to the user — video games, pinball, alarms, toys, etc, or industrial indicators, feedback controls and the like. Power consumption is quite low, allowing battery operation, and only a single supply rail is required.

The SN76488 is contained in a 28-pin package and can be purchased for less than £5. It is quite a versatile chip, but we have chosen to describe how to obtain only two sound effects, these being a bomb drop and explosion, and a steam train and whistle. The former is described here; the latter appears on page 118.

Construction

Both the projects described use the one PCB design. Only the required components are assembled into the board according to each overlay diagram to obtain the required sound generator. Naturally enough, the polarity of the IC should be noted as well as the polarity of electrolytic and tantalum capacitors used. Commence construction by assembling the passive components, followed by the IC. This is not a CMOS device and no special care is required, apart from being careful not to bend any pins under the device when inserting it. If you wish, a socket may be used for the IC. This way, you can assemble both projects and purchase only one IC, swapping between the boards as you need to use them!

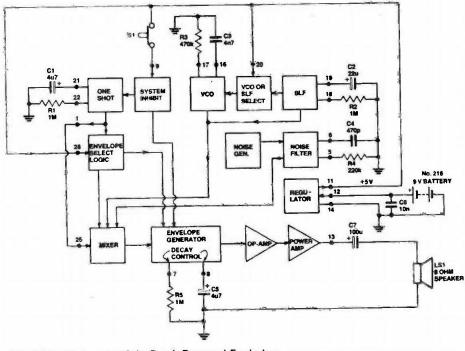


Fig. 1 Circuit diagram of the Bomb Drop and Explosion sound effects board.

Wiring to the switches, the speaker and the supply should be attached last.

The unit may be mounted in any convenient-sized box and the speaker mounted on the front. Alternatively, it may be wired into an existing piece of equipment. We'll have to leave these arrangements up to you.

Projectile Project

This produces a 'bomb drop and explosion' sound at the press of a button. Alternatively, the push-button PB1 could be replaced by a pair of relay contacts operated by a piece of equipment or a transistor (emitter to pin 9, collector to other side of PB1) that is turned on by a logic high applied to its base via a resistor.

This project is one of the most complex, using almost every functional block within the SN76488. Varying R3 and C3 a little will vary the pitch range of the 'bomb drop' (desending whistle), while varying R4 or C4 a little will alter the characteristics of the explosion. Note that it is generally easier to 'fine tune' things by varying the resistor values. The duration of the event can be varied by changing the value of either C1 or R1 and the decay of the explosion can be changed by varying R5 (varying C5 produces quite gross changes in the decay period).

Watch that you insert the link on the PCB in this one, located at the

'notch' end of the IC.

PARTS LIST.

14W, 5%
1M0
470k
20k

Capacitors C1,5 4u7 16 V PCB electrolytic

C2 22u 16 V tantalum
C3 4n7 ceramic
C4 470p ceramic

C6 10n ceramic C7 100u 16 V PCB electrolytic

Semiconductors IC1 SN76488 (see Buylines)

speaker; PP3 battery and clip.

Miscellaneous PB1 SPST push-button switch PCB (see Buylines); 50 mm diameter 8 ohm

BUYLINES

Very few components and very few supply problems with this one. The SN76488 is an improved version of the Texas SN76477 and can be obtained from Technomatic. The PCB will cost you £1.80 from our PCB Service; see page 44 for details.

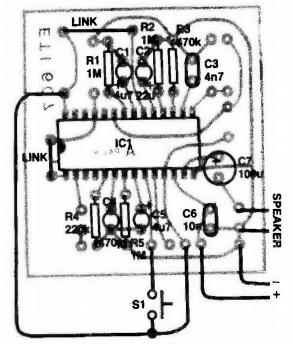


Fig. 2 Component overlay for the Bomb Drop board.



HOW IT WORKS

This unit employs most of the function blocks in the SN76488. The SLF provides a linearly increasing voltage waveform, or ramp, to the VCO, taking several seconds for the ramp voltage to rise from zero to maximum value. The causes the VCO to produce a tone which 'glides' down in pitch, making the 'bomb drop' effect. The explosion is generated by the Noise Generator/Filter and the Envelope Generator. It starts with a burst of noise, which dies away in intensity exponentially in a few seconds.

The whole sequence is triggered by operating the pushbutton, PB1. This applies a high (+5 V) to the input of the System Inhibit block, pin 9. This in turn triggers the One Shot and the Envelope Generator. At the commencement of the One Shot timing period, the One Shot triggers the SLF HI/LO Sync, starting the SLF, and the VCO does its things. At the end of the One Shot timing period the Envelope Select Logic becomes operative, the SLF is disabled and the

Envelope Generator commences to do its thing. The Mixer selects the VCO output at the start of the One Shot timing period and the Noise Generator/Filter output at the end of the One Shot timing period. Thus the two sounds are switched through to the audio output stage in sequence, the Envelope Generator modifying the noise so that it dies away, the time it takes to do so being controlled by the time constant of R5, C5.

The starting pitch of the VCO is determined by R3 and C3, the rate of rise of the voltage ramp produced by the SIF is determined by C2 and R2, while the One Shot timing period is determined by the time constant of C1 and R1. The frequency characteristics of the broad-band noise produced by the Noise Generator are modified by R4 and C4 connected to the noise filter control pins (5 and 6).

Audio output is coupled to the

Audio output is coupled to the loudspeaker via C7, a 100uF electrolytic

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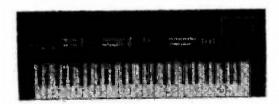
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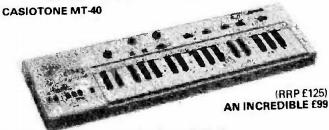
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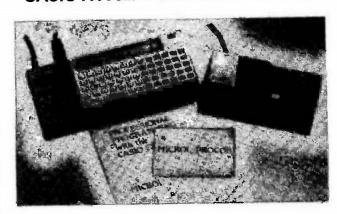
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READ/WRITE

Dear Mr. Ron Harris Sir,

We seem to have been hearing quite a bit about System A recently; technically it looks a rather nice amplifier. However, it's difficult to tell how good commercially-produced units are with only limited information available about them. So what about the other end of the problem - what does System A sound like, compared with other amplifiers? Unfortunately, I can't see any of the hi-fi mags doing a review of it, so - how about you doing one (totally unbiased, of course) please, pretty please? Come on, put your reputation on the line! Yours grovellingly,

M.R. Barrett, Hove. Certainly not. Someone might chop it

off! System A has a comparable sound to any of the more highly regarded

commercial units. Listening tests we have conducted over the months since the creature's completion, have shown it (the power amps) to have a more detailed and open midrange/top than ANY we have compared it to. The top commercial boxes - Threshold, Monogram, Carver, etc can exhibit a better bass control than the System A however, but as to whether or not that is important for your particular application (ie loudspeaker), I could not say (because you haven't told me what speakers you've got, have you?).

Anyone contemplating building a System A is welcome to write to us for advice on speaker matching.

Dear Sir.

I read with interest the articles in the July and August editions of ETI describing the construction of the System A Audio Amplifier, as I have been on the lookout for a high-quality class A amplifier design for some time. My particular interest in class A stems from the fact that I own a pair of Lowther loudspeakers — these units are almost ridiculously sensitive, requiring only some 10 W or so of input to produce the equivalent sound output of a conventional 100 W system. Given this sensitivity, most high quality class AB amps are only ticking over when driving a pair of Lowthers, and hence are working at the highest distortion end of their operating range. Hence the interest in class A, where no penalty is paid for operating the amplifier at low levels of power output. However, before going ahead and building the System A, I would like the answers to a couple of questions. Firstly, the July article heralds System A as "quite simply the best, designed to out-perform even commercial equipment." There is, however, no objective assessment or comparison to back up this claim, and before laying out the not insignificant construction cost, I would like to see the amplifier reviewed, preferably alongside its "competition" in the commercial amplifier field. Is this a possibility?

Secondly, the high power output of the System A seems more than a slight degree of overkill in the context of my

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BESSET.

Lowthers. Is it reasonable, therefore, to construct a lower power version of the power amp section? If so, what modifications should be made to the present design? Yours sincerely. T. Jeffree, Milton Keynes

Taking the two points you raise, in order; first we feel it is inappropriate for us to review our own product against anyone else's. (Would you believe us anyway?) 'Objective' would not be an appropriate word to apply to such a test.

System A has aroused a great deal of interest and we know that a large number of sets have been completed. There is probably, however, a larger number of people still who would tackle the project, if only they could get to hear one first! Accordingly any owners of a System A who would be prepared to let a fellow ETI reader have a listen, can write to us and we'll run the letters herein. Secondly the high power output of the amp will not be wasted, even on your Lowthers, it will simply provide you with more headroom - and hence a cleaner sound with better bass output on transients.

Dear Mr Harris,

I am writing for advice on the purchase of an amplifier and speakers combination. I list my present system below:

> Home-brew 10 W amp Ferguson (?) 3-way speakers (actually 2-way, 3-cone) Realistic 31-987 Graphic Equaliser Hitachi D-225 Cassette Deck Pioneer PL-300 turntable (the latest addition!)

The amplifier now ceases to be of any great use in terms of power. although quality is more than adequate (based on Bi-Pak AL30A). I have considered NAD3020. Pioneer SA410. and also the "Audiophile" amp, the MOSFET amps from IW Rimmer, and the Linsley-Hood kit from Powertran. The last three give me extra headroom, and I would like to feed them into AR18 speakers from Acoustic Research.

Basically, I would like your opinion on the Linsley Hood 75 De Luxe/AR18 combination, plus any comments on the other "possibles".

Also, the Pioneer PL300 I have just bought is certainly the best turntable I

have heard at the price (£79.95), and I can't help wondering why it gets so little attention. Perhaps you can fill me in?

Thank you for your valuable time, D. Crary. Ilford, Essex

PS When is Felicity Kendall to return to our screens?

The AR18 is a fine unit and if you like the sound of them, go ahead and buy yourself a pair. You haven't named your cartridge so I've no idea if it matches.

Ditch the equaliser, with decent speakers and amp, you won't need it!

As to amplifiers, from the units you mention the Linsley Hood power amps are the best bet, but the preamp of that unit is getting a bit long in the tooth now, although the sound quality is still very good by any standards. Have a listen to the Crimson CK1010/1100 setup before you decide, however, as it is in your price range and offers a highquality alternative.

The Pioneer PL300 I have not been able to listen to at any length and must thus refrain from commenting upon!

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INSTRUMENT PROBE

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ost readers would be aware that, when taking a measurement on electronic circuitry. the input impedance of the measuring instrument must be much greater than the impedance of the circuit to which it is attached, otherwise the accurary of the measurement suffers. The input impedance of the majority of oscilloscopes is generally 1M0 with a parallel capacitance of between 20pF and 40pF. For a wide variety of applications this is perfectly adequate and will suffice for measurements of frequencies up to 5 MHz or so. The input impedance of the CRO falls with increasing frequency owing to the falling reactance of the input capacitance. For example, a capacitance of 30pF — which may be made up of direct input capacitance plus cable capacitance — has a reactance of only 500 ohms at 10 MHz. The input capacitance also affects the rise time of the input — that is, the speed at which a 'step' input will rise from the 10% amplitude value to the 90% amplitude value.

The input impedance of an oscilloscope can be effectively raised, and the capacitance decreased, by using a 'stepdown' probe. For example, a 'x10' probe will generally have an input impedance of 10M and a parallel capacitance of between 5pF and 15pF. While this improves the input impedance there are two trade-offs. Firstly, unless elaborate (and expensive) compensation is employed, the rise time is degraded, and secondly, maximum sensitivity is decreased by a factor of 10. As Murphy's law would have it, your CRO will run out of grunt just when you need it most.

Taking the situation with digital counter/timers, we find similar problems. Those that operate beyond 30 MHz or 50 MHz generally employ a prescaler with an input impedance of 50 ohms — which is perfectly all right if you're working on low impedance circuits and/or with high signal levels. But there are those occasions when you need a high impedance input and a fast (high frequency) rise time. As with the CRO, this is where your

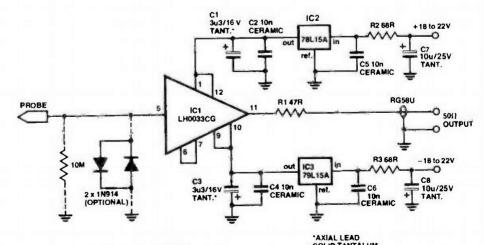


counter/timer runs out of grunt.

It's times like these you need this project; a x 1 active instrument probe using a special buffer IC with an input impedance of typically 100,000 megohms! — that's 10^{11} ohms — a very low input capacitance of around four to five picofarads, a fast rise time (around three nanoseconds) and a bandwidth of 100 MHz. Output impedance is around 50 ohms and the device is capable of driving capacitive loads up to several thousand picofarads. Thus it is eminently suited for use with high speed, wide bandwidth oscilloscopes and digital frequency meter/timers at frequencies up to 100 MHz. Output impedance is close to 50 ohms and it is thus suited to drive both high impedance instrument inputs and low impedance inputs (which are generally 50 ohms).

Design

It's all done inside a special IC an LH0033CG from National Semiconductors. This is described as a 'fast buffer amplifier'. (It has a companion designated LH0063, described as a 'damn fast buffer amplifier'!). The LH0033 is a direct coupled FET-input voltage follower/buffer (gain ≈1) designed to provide high current drive at frequencies from DC to over 100 MHz. It will provide ±10 mA into 1k0 loads (±100 mA peak) at slew rates up to 1500 V/uS, and the chip exhibits excellent phase linearity up to 20 MHz. No offset voltage adjustment is required as the unit is constructed using specially selected FETs and is laser-trimmed during construction. Input is directly to the gate of a



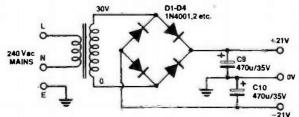


Fig. 1 Circuit diagram for the probe, C2 and C4 need to be ceramic
Fig. 1 Circuit diagram for the probe,

C2 and C4 need to be 10n ceramic chip or 1n0 ceramic disc or plate types. C5 and C6 need only be disc or plate ceramic. See 'Bypassing' over the page.

junction FET, operated as a source follower, driving a complementary output pair of bipolar transistors.

Regulated plus and minus supplies of 15 V each provide power to the IC. Low-power three-terminal regulators are used to keep the unit compact. An external unregulated supply of between 18 and 22 V at around 50 mA is required to power the probe.

The supply pins on the IC need to be well bypassed over a wide frequency range so that the IC can maintain its characteristics, and the construction has been specially arranged to achieve this. Axial lead solid tantalum capacitors are used to bypass the IC's supply pins at the lower frequencies, while low inductance ceramic capacitors are employed as bypasses for the higher frequencies. A double-sided fibreglass PCB is used to preserve the high frequency response and the high input impedance, and the layout is arranged to permit direct connection to the probe tip and provide low input capacitance.

However, the presence of the PCB substrate will degrade the input impedance, surprisingly enough, and you can drill out the area of board immediately beneath pin 5 of the IC and solder the pin directly to the probe tip. For those who wish to go 'all the way' (as Frank Sinatra sings), the plastic insulation of the probe tip can be replaced with a similar piece of Teflon — if you can afford it and have access to a lathe.

The maximum input voltage permissible, when driving a high impedance load, is plus or minus 15 V. When driving a 50 ohm load, maximum input voltage permissible is only plus or minus 10 V (limited by maximum output current). No input protection has been included. However, if you are only working with circuits where voltages are no greater than about 1 V peak-to-peak, protection can be added by putting two diodes back-to-back in parallel with the input, along with a 10M resistor. The maximum input voltage figures include any DC voltages present, plus the superimposed signal voltage

At this stage it is only fair to tell you that the LH0033CG is an expensive device (by comparison). But — compare the total cost of this probe to a similar commercially-made type and you won't catch your breath a second time!

Construction

The project is constructed on a small double-sided fibreglass PCB with

BYPASSING.

Supply lead bypassing is important in order that the LH0033 can operate correctly over the full bandwidth from DC to 100 MHz. To ensure this, the bypassing has been specially arranged and the techniques employed are probably unfamiliar to many readers.

The output circuit signal return path for the IC is via the ground and the two supply rails. Any significant impedance in series with this path (or paths) will subtract signal from the output load. Thus, the supply rail bypassing has to present an impedance which is a fraction (like one-tenth or better) that of the minimum output load impedance. Here, the minimum output load is about 100 ohms (R1 + 50 ohms instrument input impedance) and the supply bypassing impedance should ideally be less than 10 ohms across the frequency range.

The bypassing on each supply rail to the IC leads here takes advantage of the characteristics of three separate components to cover three sections of the frequency range.

From DC to around 100 kHz, each three-terminal regulator (IC2, IC3) has an output impedance well below one ohm, rising to four or five ohms at 1 MHz, as shown in Fig. 1. The two tantalum capacitors, C1 and C3, then take over.

Solid tantalum capacitors have a characteristic impedance that falls with frequency according to its value, which then 'flattens out' in the region around 500 kHz — 1 MHz, rising to a few ohms around 10 MHz, as can be seen in Fig. 2. Thus, C1 and C3 serve as effective bypasses across the range from around 100 kHz to around 10 MHz. Axial lead tantalum capacitors were chosen as their construction exhibits the slowest impedance rise following the minimum impedance value.

To provide bypassing over the decade from 10 MHz to 100 MHz, capacitors C2 and C4 have been specially chosen and positioned on the PCB. For the prototype, 'chip' ceramic capacitors were used. These tiny, 'naked' chips of ceramic with a capacitor embedded in them are probably the most effective bypass capacitors made. The leads and physical construction of all capacitors form an inductance which is

effectively in series with the capacitance of the component. The combined effect forms a series resonant circuit, the frequency of which (that is, the self-resonant frequency of the component) is mainly dependent on the length of the connecting leads, the particular construction of the capacitor and the way in which it is mounted. Ceramic chip capacitors, being a tiny block with connecting pads or surfaces on each end, have extremely low values of series inductance and thus very high self-resonant frequencies see Fig. 4. Now, any value of chip capacitor between 1n0 and 10n can be used for C2 and C4. The self-resonant frequency of a 1n0 chip capacitor is somewhat above 100 MHz (as per Fig. 4), but that of a 10n chip is between 40 MHz and 50 MHz. Now, this isn't a problem, for the chip's impedance falls with frequency as usual until near the self-resonant frequency where it falls rapidly, reaching a minimum at the self-resonant frequency. Above that frequency its impedance rises again, but is still low enough for effective bypassing.

Ordinary ceramic disc and plate capacitors behave in much the same way. The self-resonant frequency of a typical 5 mm diameter disc or 5 mm square plate capacitor depends on the lead length, as shown in Fig. 5. Thus, you could use 470pF or 1000pF (1n0) capacitors of this type for C2 and C4, provided you installed them on the underside of the board with absolute minimum lead length.



Fig. 3 Ceramic chip capacitors shown about actual size.

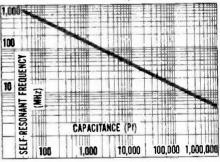
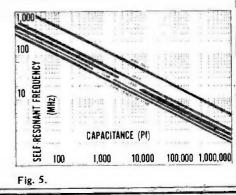


Fig. 4.



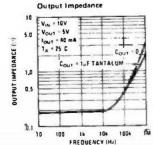
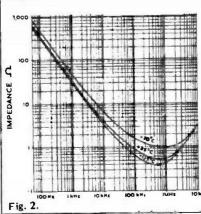


Fig. 1.



components mounted on both sides of the board. Commence by soldering in place the components that go on the top side of the board, leaving IC1 until last. Note that the positive leads of both C3 and C8 are soldered to the groundplane areas on both the top and the bottom sides of the board. Take care with the orientation of the tantalum capacitor, as well as IC2 and IC3. Having done that, solder C2, C4, C5 and C6 to the bottom side of the board. Now you can install IC1. You will have to juggle the legs a little. Push the can as far down on the board as you're able; its base should sit no more than 3 mm from the board.

Now that you have everything in place, check it all. It seems pretty simple, but Murphy's law will ensure that the simplest things have the

highest stuff-up rates!

All's well? — now you attach the output coax cable to the underside of the board, plus the DC input and ground (0 V) wires. But — before you do, slip the output end piece of the probe case over the cable and supply wires, push it down about 150 mm or so and then slip the case of the probe case down the wires. This saves slipping them over the other end of the whole business and sliding them all the way to the probe.

The probe tip can be attached and soldered in place last of all. Now you can screw it all together and attach the appropriate plugs to the other end of

the cable and supply wires.

With the construction completed, you can power up and try it out. Note that the transformer suggested in our power supply is but one of many suitable types. Any transformer that will deliver at least 26 V AC at a load of about 50 mA will suffice. Alternatively, any dual polarity DC supply having an output between 18 and 22 V at 250 mA will power the probe.

Note

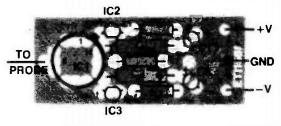
Always take care that you don't exceed the input voltage limitation; LH0033s are expensive.

BUYLINES

Ceramic chip capacitors and solid tantalum axial capacitors are a trifle unusual; however, they are stocked by C.T. Electronics (Action) Ltd, 267 & 270 Acton Lane, London W4 5DG. (They also stock the BNC plug should you have any problems there). We will be selling the double-sided board through out PCB Service — the order form is on page 44.

PARTS LIST

Semiconductors Resistors (all ¼ W, 5%) LH0033CG 47R R2, R3 IC2 78L15A 79L15A IC3 D1-D4 1N4001,2,etc. (if required) Capacitors 3u3 16 V solid tantalum Miscellaneous C1, C3 PCB (double-sided fibreglass); RG58U coax axial leads 10n ceramic block cable and BNC plug; T1 - (if required) C2, 4, 5, 6 C7, C8 C9, C10 10u 25 V tantalum 240 V to 30 V transformer or similar; op-470u 35 V electrolytic tional 10M/4W 5% resistor and 2 x 1N914 diodes; wire; probe housing. (if required)



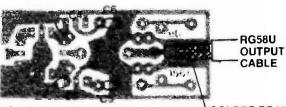


Fig. 2 Component overlays for the top of the board (top) and the bottom of the board (bottom!).

SOLDER BRAID TO COPPER

HOW IT WORKS.

This instrument probe employs a wideband hybrid voltage follower/buffer IC, the LH0033, with very close to unity gain, that features a very high input impedance and a low output impedance. It requires regulated, well-bypassed supply rails. Two three-terminal low power regulators provide plus-and-minus 15 V supplies from an unregulated input.

The internal circuit of the LH0033 is shown below. Basically, it consists of a FET input stage (Q1), operated as a source follower. The other FET, Q4, provides a constant current source for the source bias of Q1, while Q2 and Q3 are connected as diodes and provide bias for the bases of Q5 and Q6. Resistors R1 and R2 are laser trimmed in manufacture so that the IC meets the offset voltage specification. As Q1 has a constant current source load, the input impedance at the gate of Q1 is very low. The output of the source follower drives a complementary pair output stage, Q5-Q6. Thus the IC will have a very high input impedance, a very low output impedance and a gain very close to unity. With appropriate construction employed for the internal devices, the bandwidth over which the device will operate can be made very wide indeed. The -3dB point for the LH0033 is 100 MHz.

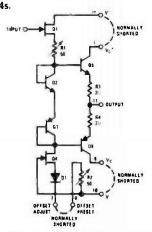
As the device is direct-coupled, DC levels will be maintained between input and output.

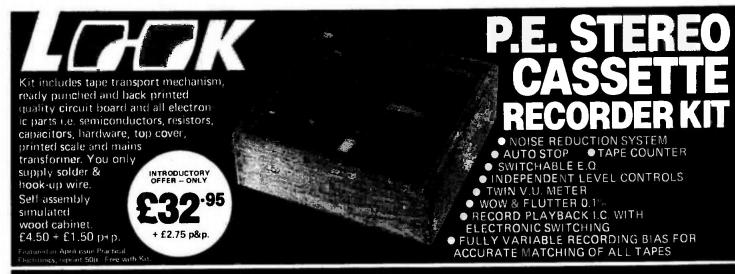
Bypassing requirements for the IC's supply leads are explained elsewhere in the article.

To provide regulated plus-and-minus 15 V rails for the IC, two three-terminal regulators are employed, a 78L15A for the positive rail and a 79L15A for the negative rail. These can supply up to 100 mA and have a very low output impedance up to

several hundred kilohertz, which is exploited for low frequency bypassing. Each supply rail requires an unregulated input of between 18 V and 22 V. Decoupling of the supply leads provided by R2/C7 on the positive rail and R3/C8 on the negative rail. The input terminal of each regulator is bypassed to prevent instability.

As the input voltage is limited to a maximum equal to the supply rails (high impedance load), input protection may be added in applications where only low level signals are being examined. As shown in the main circuit, this protection consists of two 1N914 diodes connected back-to-back in parallel with a 10 M resistor across the input. Signals above 1 V peak-to-peak will be clipped, preventing any damage to the IC. If very fast rise time signals are to be examined then better protection for the IC can be obtained by using hot-carrier diodes such as the HP 5082-2800 instead of the 1N914s.





STEREO AMPLIFIER KIT



- Feeturing latest SGS/ATES TDA 2006 10 watt output IC's with in-built thermal and short circuit protection.

 Multard Stereo Preamplifier Module.
- Attractive black vinyl finish cabinet, 9"x 8%"x 3%"
- 10+10 Stereo converts to a 20 watt Disco amplifier.

To complete you just supply connecting wire and solder. Features include din input sockets for ceramic cartridge, microphone, tape or tuner. Outputs - tape, speakers and headphones. By the press of a button it transforms into a 20 watt mono disco amplifier with twin deck mixing. The kit incorporates a Mullard LP1183 pre-amp module, plus power amp assembly kit and mains power supply. Also features 4 slider level controls, rotary bass and treble controls and 6 push button switches. Silver finish fascia with matching

nobs and contrasting cabinet. Instructions available, price 50p. Supplied FREE with kit.

SPECIFICATIONS: Frequency response Input sensitivity

Tone controls

Distortion

£16-50

Suitable for 4 to 8 ohm speakers 40Hz - 20KHz

40Hz - 20KHz P.U. 150mV. Aux. 200mV. Mic. 1.5mV. Bass * 12db @ 60Hz Treble * 12db @ 10KHz 0.1% typically @ 8 watts 220 - 250 volts 50Hz.

220 – 250 volts 50Hz.

8" SPEAKER KIT Two 8" twin cone domostic speakers, £4,75 per stereo pair plus £1,70 p&p, when purchased with amplifier, Available separately £6.75 & £1.70 p+p.

PRACTICAL ELECTRONICS

RADIO



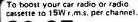
2 WAVE BAND, MW - LW

Easy to build.
 5 push button tuning.
 Modern design.
 6 watt output.
 Ready etched and punched PCB.
 Incorporates suppression circuits.
 All the electronic components to build the radio, you

All the electronic components to build the railor, you supply only the wire and the solder, featured in Practical Electronics. Features: pre-set tuning with 5 push button options, black illuminated tuning scale. The P.E. Traveller has a 6 watt output neg, ground and incorporates an integrated circuit output stage, a Mulfard IF Module LP1181 ceramic filter type pre-aligned and assembled, and a Bird pre-aligned push button tuning unit.

Suitable stainless steel fully retractable aerial (locking) and speaker (6"x 4"app.) available as a complete kit. £2.50/pack + £1.50 p&p.

RD AUDIO DIOBOOSTER



95 +£1.50 p&p.



125W HIGH POWER AMP MODULE

кіт: £10-50 воіст: £14-25

+£1.15 p&p

wer amp kit is a module for high power applications – disco units, guitar amplifiers, public address systems and even high power domestic systems. The unit systems and even high power domestic systems. The unit is protected against short circulting of the load and is safe in an open circuit condition. A large safety margin exists by use of generously rated components, result, a high powered rugged unit. The PC board is back printed, etched and ready to drill for ease of construction and the aluminium chassis is preformed and ready to use. Supplied with all parts, circuit diagrams and instructions. ACCESSORIES: Suitable mains power supply kit with

transformer: £7.50 plus £3.15 p&p. Suitable LS coupling electrolytic: £1.00 plus 25p p&p



SPECIFICATIONS:

Max. output power (RMS): 125W. Operating voltage (DC): 50 - 80 max. Loads: 4 - 16 ohms.

Loads: 4 - 16 oirms.
Frequency response measured @ 100 watts: 25Hz - 20KHz,
Sensitivity for 100 watts: 400mV @ 47K,
Typical T.H.D. @ 50 watts, 4 ohms: 0.1%,
Dimensions: 205 x 90 and 190 x 36 mm.

11-FI SPEAKERS

GOODMANS TWEETERS Bohm soft dome radiator tweet-er (3%"sq.) for use in up to 40W with 2 element crossove

£3.50 each (p&p £1) or £5.95 pair (p&p £2)

Complete with 2 Total impedance of system 4 ohms

£7.95 PER SET + €2.70 p&p

35 WATT MICRO 2-WAY SPEAKER SYSTEM Unit comprises one 50w (4"app.) Audax soft dome tweeter HD100. And one 5" Audax bass/midrange 35w driver HIFIIJSM. element crossover.

P.E. STEREO TUNER KIT

This easy to build 3 band stereo AM/FM tuner kit is designed in conjunction with Practical Electronics (July 81 issue). For ease of construction and alignment it incorporates three Mullard modules and an I.C. IF. System. FEATURES: VHF, MW, LW Bands, interstation muting and AFC on VMF. Tuning meter. Two back printed PCB's. Ready made chassis and scale. Aerial: AM - ferrite rod, FM - 75 or 300 ohms. Stabelised power supply with 'C' core mains transformer. All components supp-lled are to P.E. strict specification. Front scale size: 10½ x 2½" approx. Complete with diagram and instructions.

£17.95

Self assembly simulated wood cabinet sleeve to suit tuner only. Finish size: 11%"x8%"x3%". £3.50 Plus £1.50 p&p.



SPECIAL OFFER! TUNER KIT PLUS Matching I.C. 10 watt per channel Power amp kit. Multard LP1183 built pre-amp, suitable for ceramic pick-up and aux. inputs . • Matching power supply kit with transformer. • Matching set of 4 slider £21,95 controls for bass, treble and volumes. • £3.80 P&P.

TV SOUND

£11-45

+ £1.50 p&p.

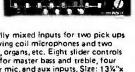


As featured in E.T.I. December '81 issue, Kit of parts including PCB, UHF tuner and selector switch with all components excluding case.

Transformer £1.50 + £1.50 p&p (p&p free on transformer if ordered with kit).
 Ready built LP1183 Module for simulated stereo operation.
 £1.95 + 75p p&p.

MONO MIXER AMP

+ £3,70 p&p.



50 WATT Six individually mixed inputs for two pick ups (Cer. or mag.), two moving coil microphones and two auxiliary or tape, tuner, organs, etc. Eight slider controls—six for level and two for master bass and trable, four Extra treble controls for mic. and aux inputs. Size: 13%'x 6%'x3%"app, Power output 50 watts R.M.S. (continuous) for use with 4 to 8 ohm speakers. Attractive black vinyl controls the property of the control of the controls of the control of the controls of the control of the controls of the control case with matching fascia and knobs. Ready to use

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Note: Goods despatched to UK postal addresses only. For further information send for instructions 20p plus stamped addressed envelope, All items subject to availablity. Prices correct at 31/1/82 and subject to change without notice. Please allow 7 working days from receipt of order for despatch.

ALL PRICES INCLUDE VAT AT 15%.

ALL CALLERS TO: 323 Edgware Rd, London W2. Telephone: 01-723 8432. Open 9.30 - 5.30pm. Closed all day Thursday. RTVC Limited reserve the right to update their products without notice.





Hands up all those who had trouble starting their cars during the recent appalling weather. Don't you wish your car was fitted with an electronic ignition to make the most of your battery, as well as increasing the life of your contact breaker and giving you more miles to the gallon into the bargain?

The prize in this competition is a Total Energy Discharge ignition unit designed by Electronize Design, a company with a great deal of experience in the field. The unit is supplied as a kit of parts and is easy to assemble.

To win this kit you have to answer these two questions:-

- (1) The standard ignition circuit, using a coil and contact breaker, has been fitted to virtually all mass produced cars for 60 years. Who designed it? (We'll accept surname only).
- (2) In a four-cylinder engine, firing the cylinders in the order 1-2-3-4 would lead to excessive engine vibration. Give one

firing sequence commonly used to overcome this problem.

Write your name, address and answers on the form on page 133 (there's no need to cut up this page) and send it to us by April 30th, 1982. (All right, you can put your hands down now!)

RULES

- Closing date is April 30th 1982, and all entries post-marked later than this date will be discounted.
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- entry.

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ACORN ATOM

K rom + 2K ram Kit £120, built £150, 12K rom + 2K ram kit £168, built £198, 4K expansion iom £25, lower supply £10 20

UK101 AND SUPERBOARD

UK101 with 1K and free power supply and modulator kit F120, bulk 1849. The below accessories suit both the UK101 and superboard: Estra ram f2.10 per K. 16K memory expansion complete kit f80, built 558. 32K memory expansion complete kit f80, built 568. 32K memory expansion kit f74, built f82, Cassette recorder f13, Eegmon f22.50, Wemon f13,95, Word processor program £10, Centronics interface kit £10. 610 expansion board £179. Casset ministroppy discorder with OOS £276. The below suit only superboard: Colour dealprior board built 646. Assembler £6 flort near £25. Guard band kit f10. Series 1 only 30 fines = 50 characters display expansion kit £14. UK101 display expansion kit £14.

NEW GENIE 1 £299

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PRINTERS



Buy any of the below and get a free interface kit and word processor program for UK101 or Superboard: Expan MX70 7259. Expan MX807 1739. Expan MX80F/T7 E49. OKI Microtine 80 E295. OKI Microtine 80 E295. OKI Microtine 82A E399. Centranks 737 E335. Saikosha GP80A E199

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kit £12.98. AY-3 8550 + kit £9.26.

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Postage £3.50 computers, £4.50 on Printers and 45p on other orders. Lists 27p Post free. Please add VAT to all Prices except those sections marked with a "which already include it. Overseas and official credit orders welcome."

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WIN THE NEXT **10 FREE!**



This is a special competition for our regular readers. We're offering a ten year subscription to ETI as a 'thank you' prize for supporting us this far. All the questions refer to back copies of our magazine and will be easy if you've kept the issues! (Surveys tell us that over 90% of readers keep ETI for longer than a year!) Index issues will be particularly useful, but will not give you all the answers. Fill in the coupon on page 133 — you don't need to ruin this issue — and don't forget your name and address! In the event that no one gets all the answers correct, the highest number of right answers will win. In the event of a tie, it will be the earliest postmark that takes the ten year subscription.

Read the questions carefully before answering.

- 1. Which issue was designated a "4 Channel Sound Special Issue"? _
- 2. Who edited the May 1973 issue of ET!?
- 3. What month did the first issue of ETI appear in Britain?
- 4. What makes March 1979 good theatre?
- 5. ETI published the first-ever TV games project. In which issue?.
- 6. Which IC is featured in the July 1976 "Data Sheet"?
- 7. The amplifier on the cover of the February 1982 issue has also appeared on a previous cover of ETI. Which one?

In 1979 who reviewed Star Chess for	1 E 1 1 6
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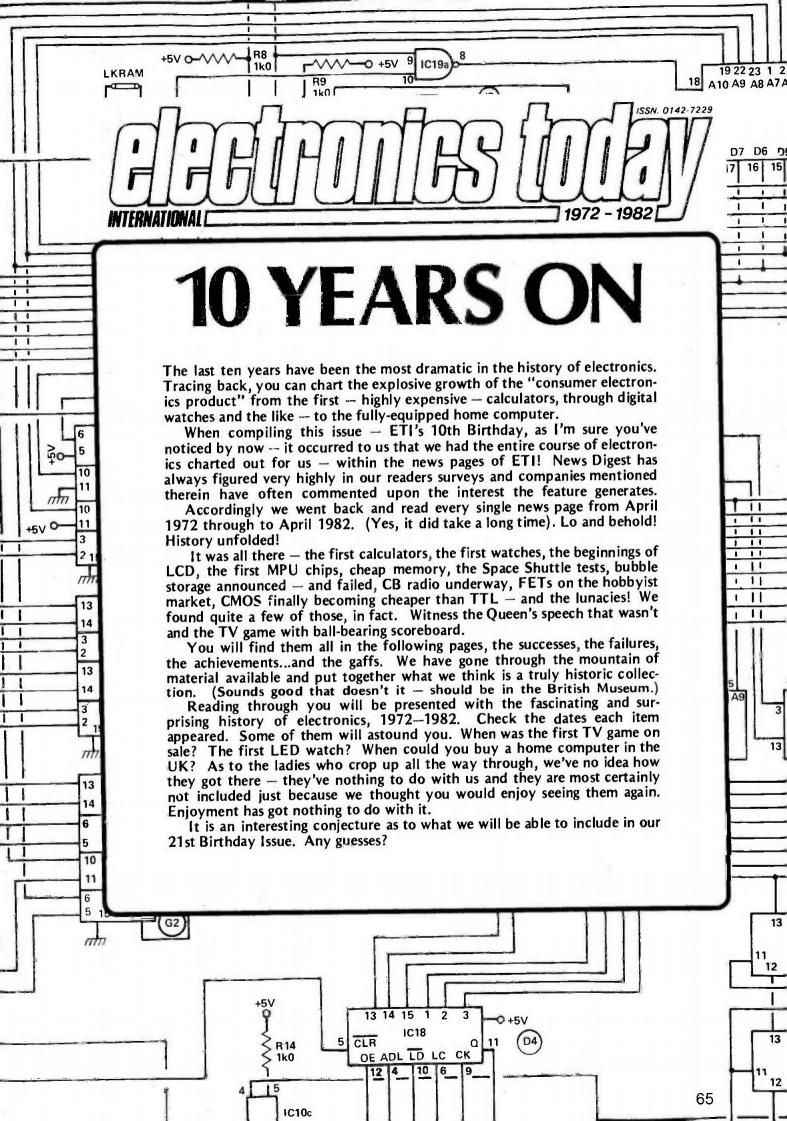
- 9. Who first wrote the series "Electronics Tomorrow"?
- 10. The 100 W Guitar Amplifier (the first one!) appeared when?
- 11. Microfile is the title of ETI's regular computing hardware section. In which issue did it first appear?
- 12. In what year did we publish a synthesiser, an LED multimeter and an FM tuner in successive months?
- 13. What was "The Beast"? ___
- 14. How many parts of the popular "Electronics It's Easy" series were published in ETI? _
- 15. How many editors has ET! had in the past years?
- 16. In October 1976, who was ETI's Assistant Editor?
- 17. Who designed the Transcendent DPX?
- 18. Which issue began "Project 80"?
- 19. The 4600 synthesiser is one of our all-time most popular projects. In which issue did the series begin?
- 20. DIY Polyphonic keyboards came to ETI when?

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TV GAMES COME OF AGE

It is just over two years since the first. TV games started to appear in pubs-since then a lot has happened in this field with a large number of small companies marketing various units by a variety of methods. Although the TV games have received a considerable

amount of publicity they have not yet caught on in a big way.

"No one who has ever played TV games has ever said anything derogatory about the concept", Richard Fairhurst of Videomaster Ltd., told ETI, "they may not like the price or the packaging but they always like the idea".

ETI NEWS NOV 1975

bbc get it taped

The BBC and 3M have collaborated to develop a new tape recording system claimed to provide 90 dB noise figure. The system will accommodate 32 tracks on one-inch tape at an undisclosed tape speed.

ETINEWS JULY 1973

PIEZOELECTRIC HEADPHONES

The Pioneer SE-700 are the first high fidelity headphones to use the piezo-electric effect. As the audio signals reach the headphones, the driver elements of ultra-thin aluminium-coated high-polymer film expand and contract accordingly, creating "breathing" motion. Tonal characteristics are comparable to those of the electrostatic type headphones, but the SE-700 require no matching transformer.

ETI NEWS MAY 1975



Doctor Who

One of our readers, Mr. S. Knowles of Hampshire, sent us a scope picture he took whilst

designing with a Textronix 7403 on 500 nS/div with x10 expand. It seems he was looking for a pulse, but he may well have discovered the secret of time travel!

ETI NEWS JUNE 1980

Pet Chip

This should appeal to those of you who spent your hardearned pennies on a 'pet rock,'

We recently received a letter from an anonymous dad who made an apparently trivial Christmas prest for his daughter. However, since then he has been inundated with orders.

ETI NEWS MARCH 1980

Mr A. Nonymous painted a face on one end of an IC (pet IC, you see) and made a matchstick cage for it complete with watch battery feeding bowl.

The chip should quickly LATCH on to its new OHM. As for feeding, a few BITS of CURRENTS a day should be AMPle. Just let it NOR away to its heart's content. You can teach it tricks.

Ta. Mr Nonymous. We haven't had a good groan in ages.

its a wide word

Intel, Zilog and Motorola are taking their places in the front rank on the grid for this years expected race to 16 bit MPU sales. All three have completed development, and will probably show the nature of

their teeth at next months US Solid State Circuits Conference. The pause between this and letting loose of the hounds as it were will almost certainly mean late autumn production.

On yer marksETI NEWS MARCH 1978

SHORTS

Every Ready — now called Berec — have released four rechargable consumer batteries, in the HP2, HP11, HP7 and PP3 varieties. Chargers are also available. An undoubted reaction to the phenominal loss of dry cell power these days.

Direct drive turntables yes. But direct drive MPUs? Also yes — now. The \$2000 is a new release from AMI which can drive flouorescent displays directly, with HT drive and 7-segment decoding on chip. Also on board 64 x 4 RAM and 1K ROM. Intended for low lost applications.

Ingersoll — the tick tock people — are into electronics. They have released three TV games, three clock radios, two Door Chimes, and a portable nicro cassette player. Photo, shows one of their new TV games, It must be Christmas.

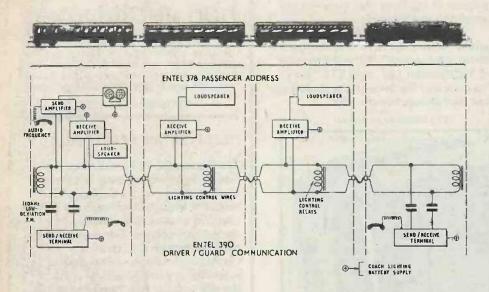
ETINEWS JAN 1979

Fairchild are making a big fuss about having their F16K Dynamic 16K RAMs available at last. Access times vary from 150 ns to 300 ns





TALKING IN TRAINS



British Rail's plans for 150 mph trains include improved communication systems between drivers and guards. Also planned are passenger address systems.

A range of equipment - known as EMTEL - has been designed specifically for this task by Britain's Nelson Tansley Ltd.

The main problem to be overcome was the impossibility of providing a special cable, running the length of the train, on which to carry the signals.

The equipment was therefore designed to accommodate any continuous circuit, for example, the control wires for the lighting relays which (in British Rail), are the only conductors always connected throughout any passenger train. In this case, departure from the ideal of a 600 ohm noise-free line is caused by the connexion across the wires of many relay solenoids, the impedance of which is not only complex, but variable.

ETI NEWS JULY 1972

LASER MISSILE INTERCEPTOR.

The US armed forces may soon have a laser missile interceptor. Air Force reports state that prototype deuterium fluoride lasers have been successfully tested at 'very very high' power outputs.

Power output is apparently so high that the laser beam burns straight through heavy gauge stainless nickel steel plate.

ETI NEWS JULY 1975

BIAS - AUTOSELECTION

Cassette tape recorders that have been designed specifically for use with chromium dioxide tapes require special bias switching facilities.

At present this is done manually. However the latest BASF 'SM' chromium dioxide cassettes have a notch on the rear of the cassette (in addition to the tab now used to prevent erasure of recorded material) and, hope BASF - and Philips who are backing the system - future cassette players will have a switch mechanism actuated by this tab to bring in the necessary bias circuitry.

ETINEWS APRIL 1972



It had to happen. The integrated circuit is so old that it has earned its place in a museum. Doesn't it make you feel old? The world's first IC, invented by Jack Kilby of Texas Instruments in 1958, is one of three exhibits on loan from TI in Dallas for the 'Challenge of the Chip' exhibition at the Science Museum. The other two are the first silicon exhibition at the Science Museum. The Stransistor and the first single chip microcomputer.

ETI NEWS MAY 1980

LIGHTING THE WAY

Many local authorities are now using a street lighting control system in which a photoelectric cell measures the light level and varies the input to a thick film heating element controlling a temperature sensitive switch. The street lights are therefore automatically switched on at dusk and off at dawn, which means that light is provided only when it is needed and ensures that electricity is not wasted.

GETTING READY FOR COMMERCIAL RADIO

Commercial radio is on its way: anyone doubting this should tune around the medium wave band where tests transmissions are already being conducted. Contracts for the supply of the transmitters and the aerials have been placed with EMI, the value of the order is put at £160,000.

ETI NEWS MAY 1973

shorts

Tandy is doing well with its home computer in the USA, and is expanding, both physically and financially, that side of the business.

 New from GI — the Cricket chip. The AY-3-8910 is a programmable sound generator and is controlled, software needing only a power sup-ply and clock to begin chirping or hooting or ...

Hong Kong King

Some numbers to tick off on your fingers. In the first six months of the year Hong Kong exported 16 million watches (worth £77m). These break down as 61% mechanical, 29% LCD and only 10% LED and quartz analogue com-

bined. Surprising LED figures eh?

Germany developed a sudden lust for these nontockers and their imports leapt up by 287%, putting them as the second largest consumers — behind the US and ahead of us! ETI NEWS NOV 1978

ETI NEWS OCT 1978

forget who

not?

You know we've quite forgotten why we used this photo at all. Now let's see something to do with TV games? Anyway the editorial desks have been bereft of nice lady photos lately - so this one appeared as an oasis amid the dusty filing trays.
P.S. Binatone the people

who make the box in front - don't ask what box or in front of what or we won't speak to you again claim to now taken over half the TV game market — the magic 51% in fact.

ETI NEWS NOV 1978

BE WARNED (IN A SMALL WAY!)

The Mini-Bleeptone 525 is a unit which provides a choice of two continous signals of up to 80dBa with current consumption ranging from 3-15mA.



Its applications are wide, being ideally suited as a fault indicator mounted onto portable equipment and instrument panels, or for localised warning of such things as intruders and/or fire

NEW LC DISPLAYS FOR WATCHES

A new series of Liquid Crystal displays have been announced by Beckman for digital watches. These display hours and minutes continually with either date or seconds, selected by a push-button. Contrast ratio is



20:1. power requirement is 1 microwatt so that even with constant readout battery life is over a year. LC modules are available for both 3V and 6V models and a CMOS compatible. Beckman Instruments Ltd., Queensway, Glenrothes, Fife, Scotland. ETI NEWS OCT 1978

Pocket Companion

Not just an electronic dictionary or a translator or an appointments diary or an encyclopedia, but something of all these rolled into one, the 'Brainbank' is hailed as the world's first pocket information and centre language laboratory.

Brainbank is programmed via a series of interchangeable. plug-in memory cells, so you have virtually unlimited information storage possibilities (armed with a bucket full of memory cells).

Each language cell, which contains 32K of ROM holds about 1200 of the most common

words, stored individually and in groups of up to fifty in categories such as travelling and food. The program also includes short phrases, automatically corrects spelling errors and explains words with double meanings (with its double entendre chip?).

The information centre's

heart is a Mostek 3870 microprocessor. Memory cells are currently available on diet and nutrition, first aid, taxation and a thesaurus. New cells will become available every month. A custom cell service is also available.

Brainbank will cost around £150 plus £20 or less for each additional cell. We will tell you more about this little marvel, when we can get hold of one to play with.





Computerised control and data recording equipment that can handle information from up to 413 different sources will be used in the development of Britain's tracked hovertrain — during its period of full-scale development.

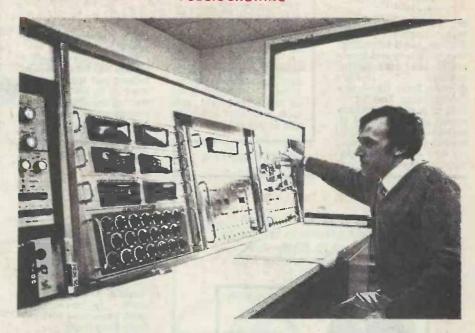
From this console, commands will be transmitted by radio to the hovertrain and radioed signals from the measuring instruments inside the vehicle will be received, recorded and analysed.

The 25-ton vehicle straddles the track and is supported approximately an inch above it by a system of fans employing the hovercraft principle. The linear motor consists of an aluminium strip set into the top of the track as the motor's "stator", and a complex set of electrical windings mounted inside the body shell. Power is picked up from a trackside rail.

The train made its first run over a mile of the track recently, watched by visiting experts and the press from several countries. It performed perfectly during the slow-speed run and is now expected to reach speeds of up to 90 mph during the next two months.

The hovertrain has been designed and constructed by Tracked Hovercraft

300 MPH HOVERTRAIN - PUBLIC SHOWING



ETINEWS APRIL 1972 (OUR FIRST EVER NEWS ITEM!)

Ltd., a company set up by Britain's National Research Development Council, and would be capable of providing a link between central

London and the airport planned for Foulness, its passengers completing the journey in quiet pollution-free comfort in about 20 minutes.

RED TAPE GAGS THE QUEEN!

In the wee small hours of January 19th 1903, Marconi established the first two-way communication across the Atlantic. Messages were exchanged between the American president Theodore Roosevelt and the British King Edward VII. To mark the 75th anniversary of this event, the Cornish Radio Amateur Club have organised a team of sixty local amateurs to run GB3 MSA (Marconi's Seventy-fifth Anniversary). The station was run 24 hours a day, from the

14th to the 22nd January, from the lounge of the Poldhu Hotel in sunny Cornwall — only metres away from the spot Marconi used.

Transmitting on 80m, 20m and 2m the team had already made 1 100 contacts in 51 countries when ETI contacted them on the 16th! All the equipment was owned by the club and its members and set up for the week specially. On the American side was another station, KM1 CC, based in Cape Cod. KM1 CC was run by

the local Barnstaple, Mass. radio club with the help of the Radio Club of America.

Now for the red tape. President Carter sent a message via KM1 CC and the Queen wanted to send a reply via GB3 MSA, just like Edward VII did back in 1903. The Home Office said that if she did, it would break a condition in all British amateurs licences — namely the one about not passing on messages from 3rd parties! So after 2 years preparation the Cornish Amateurs and the Queen were denied permission to reply to President Carter.

ETINEWS MARCH 1978

Something Bugging You?



With the increase in telephone tapping and boardroom bugging. Audiotel International have developed a simple to use, yet sophisticated successor to their Scanlock radio surveillance receiver. It is called the Scanlock Mark V8 and is a fast, easy means of detecting and locating an eavesdropping transmitter as well as being capable of routine 'sweep' searches of high level meetings rooms. Carried in a vehicle it can also locate any bleeper bug used for 'trailing'.

ed for 'trailing'.

The Scanlock is not limited to the conventional radio receiver's range of 88-108 MHz. It covers the wider frequency spectrum of 10-1800 MHz and its automatic 'sweep' mode scans this range four times a minute. Finally all that is necessary is to press the 'Locate' button and use the hand-held wand to guide you to where the bug is located. The kit is the size of a small briefcase, weighing 6.3 Kg, complete with spare battery pack. There is also provision for mains usage. For further information contact Audiotel International Ltd at Saddlers Court, Yately, Surrey, GU177RX.

CONCORDE BAN?

Whilst we are currently bombarded with PR material extolling the 'virtues' of the Concorde supersonic airliner it is interesting to note that in the USA Senator Alan Cranston has introduced a bill, co-sponsored by Senators Edward Muskie and Caliborne Pell, to prohibit overseas supersonic transports from landing at any US airports or flying over US territory at supersonic speeds.

The SSTs which carry less than half the passenger load of a 747 make ten times as much noise on take-off and landing. ETI NEWS JULY 1972

RICE LOGIC?

Later this summer — about June — National Semiconductor and Kellog's are to hook-up on a promotional deal. All Kellog cereal packets will carry coupons for reductions on National calculators. Barley credible is it not? ETI NEWS JULY 1976

electronics a show for the readboard renthusiast the seymour Hall will be last the seymour Hall will be last the seymour Hall will be last in London held a rea firm a exhibiting wire work it will be your diary mowher hetails contact would his if you letails contact would his if you letails contact Breadboard reference on P. Lig 8 ad. Taylistock

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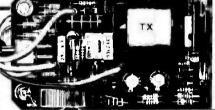


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contactless. Three position switch with Auxiliary back-up inductive circuit.

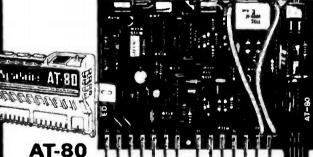
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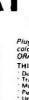
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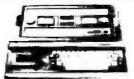
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WITH REMOTE CALL-IN BLEEPER

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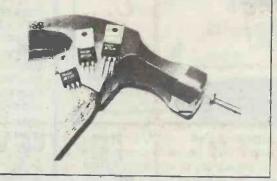
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hammer fet-ish

A new range of low cost VMOS power FETs in plastic have been introduced by Siliconix. These devices are aimed at replacing conventional bipolar transistors in a great many applications. This development in VMOS technology has cut the price of such devices by a third enabling them to compete directly with bipolar devices.



ETINEWS APRIL 1978

CALCULATOR CHIPS NOW LESS THAN £1

Calculator chips prices continue their inexorable fall in price. Latest prices in the USA for four function eight digit MOS chips are now as low as 40p to 80p. Even the complex scientific calculator chips are down to £6 or less compared to £20 this time last year.

MOS Technology Corporation for instance are selling a single chip scientific unit for £7.

ETINEWS JULY 1975

ETI NEWS DEC 1977

sailing into space

A 12 bladed solar sail spacecraft is a new candidate for mankind's first interplanetary shuttle. Designed to be employed in the 1980s its first use might well be a rendezvous with Halley's Comet in 1986.

The 'heliogyro' sail uses a helicopter type design with 12 'blades' composed of reflective aluminium plastic film, and deployed in two the space shuttle, centrifugal force would open the blades to their 41/2 MILE length. (They're 28ft. wide). The craft sits in the centre of the

The craft would be slowly spun by the sun's photon radiation, and complete a rotation every three minutes. A square sail, and hence windjamming to the stars, was rejected in favour of the blades, which now fight it out with an ion stream propulsion system for NASA consideration

ANTI-SKID CONTROL

The first standard i.c.'s designed specifically for the automotive market have been announced by Fairchild. Both are complex linear circuits developed over the past two years as 'custom' circuits before being added to the standard product line.

ETINEWS OCT 1973

ELECTRONIC CHEQUEBOOK CALCULATOR

A pocket calculator that will hold and display bank cheque account balances for a year or more is shortly to be announced by the US Mostek Corporation.

During the times that the calculator is 'off' data is stored in a static shift register (drawing a mere 100 microamps). This data is then clocked solely when access is required.

The unit is expected to retail for less than £16 and will be built into a plastic chequebook holder.

ETI NEWS JULY 1975

BUBBLING OVER

Next year Rockwell are hoping to launch their now developed one--megabit bubble memory price? One millicent per bit!

Their device can operate up to 300kHz and measures 10 x 9.5mm and is designed for a 1.8 micron bubble diameter. ETI NEWS SEPT 1977

ACC AFTER ONE YEAR

Now moving into its second year of existence the Amateur Computer Club has now formulised its activities into a constitution and has a membership of over 200. **ETINEWS AUG 1974**

Bowmar has Texas's range and is homing in. Texas are being sued for \$3 million by Bowmar who allege the supply of a large number of defective calculator keyboards.

culator keyboards.

National Strain S

The Government's hi-fi firm, Strathem are to launch their new SM2000 turntable in the autumn, which will replace the is not required. which will replace the SMA2 model. Once again the unit looks technically sound — maybe success at last for nationalised-fi? ETI NEWS OCT 1978

Power Cuts On The Way

n 1968 your 20 inch colour telly using 90° deflection would have consumed over 200 W. Now, the figure is around 65 W. A new development from Finland will further reduce that to about 40 W.

The system, which results in a reduction of about 40% in power consumption, has been incor-porated in the Salora G Series of portable colour sets. The design is basically a 90% efficient couple between the power supply and picture tube using an induction transfer system. The resultant cool running improves reliability and extends operational life.

The G Series, with its 16, 20 and 22 inch models, will operate from a standard 60A/hour 12 V battery for 15 hours, or from

mains for as long as you pay your bills. All the models feature automatic electronic tuning, fine tuning and memory plus add-on options for remoted control, 12 V battery and video frequency interface unit.

Salora products are available in the UK from Salora (UK) Ltd, 25A Techno Trading Estate, Swindon SN2 6EZ.



SPACE SHUTTLE ON THE TILES



Extremely pure silica glass has been manufactured for at least 40 years longer than jet aircraft have been around. Now it is to aid and abet the

ultimate aircraft the U.S. Space Shuttle. Made into tiles (composed of 96% silica glass) of which 34,000 are used, the material covers well over 70% of the surface of the Shuttle.

These tiles are incredible heat 'shedding' devices (see photo) and will be expected to withstand temperatures of up to 1260°C for 100 re-entries into the atmosphere. Previous heat shields were destroyed on re-entry.

Each tile is precisely milled to fit exactly against the curvature of the Shuttle body, thus making the composite craft as light as possible, and as aerodynamic as is feasible. This does however mean that no two of those 34,000 tiles are alike! Imagine the little man in a white coat with the job of fitting them to the aircraft - a huge 3-D jigsaw puzzle with only one solution out of 34,000 (i.e. 34,000 x 33,999 x 33,998...x 1) possibilities! Rather him than me.

ETI NEWS MARCH 1977

ORACLE ON AIR

ORACLE, ITV's Teletext system (see ETI, July 1975) began an on-air experiment on the ITV network on 30th June. Operating the experiment are two editorial teams and three computer systems. At ITN there is an editorial team (plus computer) for news and associated information. At London Weekend Television there will be an editorial team preparing public service and similar information pages, and the second computer. At Thames Television the third computer will be used to insert data into the network during the Monday to Friday broadcasting period with LWT taking over for the weekend transmissions. It is hoped that there will soon be sets with decoders in the main entrace lobbies of ITN House, London Weekend Television's South Bank Studios and Thames Television's Euston Studios, so that visitors can interrogate the system and see how ORACLE works.

ETI NEWS SEPT 1975

WATCHES FACE COLLAPSE!

Five companies have dropped production of digital watches, due entirely to the price war raging around the product. Gruen, Benrus, Armin Litronix and Gillette have decided the wrist borne digit is not for them. Those still there are sufferin too. Bulova are expected to make a loss this year. Gillette in fact pulled out before they pulled in, scraping well laid plans to burst into the 'marketplace' at the eleventh hour.

ETI NEWS SEPT 1977

solid state speech



If the latest goodie from Texas Instruments is as successful as we think it will be, the next generation will speak with an American accent! Called "Speak & Spell' it is a box that talks to the kids (with a 'standard' American accent),

and theoretically helps them pronounce new words correctly — it also compares how the kids spell the word with the correct (American) spelling, and indicates whether they gave the right answer.

ETI NEWS AUG 1978

£15 DOLBY RADIOS SOON?

Even the cheapest of domestic radio receivers may soon have Dolby circuitry inbuilt according to Alan Gregory of the Signetics Corporation, manufacturers of the NE545 Dolby IC

Gregory believes that the inclusion of the chip (which will be sold to manufacturers for less than a dollar will increase the price of domestic receivers by a pound at the most.

ETI NEWS APRIL 1975

SCREEN TEST

The UK is now Hong Kongs largest market for TV games. We absorbed 26% of their export in the field, some 523.506 items if you please, in the first eight months of this year. Germany finished second on 22% and the USA came third with 13%

Somewhat of a surprise, and a shame, that we take more than the States of these items. I always thought we had more taste.

ETINEWS JAN 1979

A POCKET CALCULATOR IN **EVERY HOUSEHOLD**

"By the mid-70's the pocket electronic calculator will be as much an essential part of the household as the transistor radio is now". This is the prediction made by Sinclair Radionics.

Recent market research confirms that increasing numbers of the population are becoming aware of the possible applications of pocket electronic calculators. This is most marked in the educational field, at school and college levels although considerable interest is also being shown on the domestic front by husbands and wives who are able to use a calculator to help control the family budget.

ETI NEWS DEC 1973

THE ENO OF THE AMP?

A British invention (three cheers!) could well mark the end of the amplifier as a circuit block. A new device called a 'voltage-to-current transactor can do everything an op-amp can - but better. Invented by Professor Gosling and Carl Brinker, the device contains no passive components at all, and consists of a network of transistors.

The advantages are that it integrates smoothly rather than as a series of steps, follows an input quicker and with a wider dynamic range, is smaller in chip form and uses less external components. A VCT can also double as a transformer!

ETINEWS OCT 1976

Blonde Bombshell

Now be honest with yourself aren't there times during those long cold winter days when you could do with one of these in your office. No, unfortunately I don't mean Blondie in the white pants. The blonde bombshells here are the brushed aluminium boxes of ITT Terryphone's new solid state intercom units.

The intercom, which doubles as a security and alarm system, consists of a master unit and from one to nine sub-units. The system is easily installed in many configurations.

Simple press-button-to-talk operation is featured on the master and sub-units. Each sub-unit can be called independently from the master unit, or all sub-units can be called simultaneously. Pressing the self-latching security button allows noises from children, equipment, burglars, etc to be picked up and transmitted to other parts of the premises. So, the intercom can be used as a security system in small businesses of a baby alarm at home.

Each sub-unit comes complete with cable and cable fixing pads for £20 each. The master unit costs £85 and comes with a mains plug and a screwdriver. Talking of Blondie - she can install an intercom in my office any time.

Further details of this system is available from ITT Terryphone, Station Approach, London Road, Bicester, Oxon

ETINEWS JAN 1980



FIELD EFFECT LC DISPLAYS

Siemens incorporate the field effect principle in their new liquid crystal displays with low operating voltages.



All the liquid crystal displays in field effect technology have dark symbols on a light background and are suitable for reflection operation. all with high contrast ratios, low operating voltage and low power draw. Such features allow the displays to be driven by CMOS and other ICs.

ETINEWS MARCH 1975

BANDING TOGETHER

The Editor, Electronics Today International, 36 Ebury Street, London SW1 W 0 LW.

We were most pleased to read the article "C.B. for Britain" in your July issue. The Citizens' Band Association is campaigning for the establishment of a VHF Citizens' Band in the UK and agrees with nearly all the points you make.

We have prepared a technical proposal for a VHF FM Citizens' Band which is being sent to the Home Office for discussion and contains a number of proposals to ensure that a British Citizens' Band suffers from few of the disadvantages of the American one. These proposals include:

1. Modulation shall he FM which avoids many problems of TVI, BCI and audio equipment break-in.

2. Each transceiver should contain an automatic identifying signal which is transmitted every time the transmit key is depressed. This means that anyone misusing Citizens' Band examination of the contains an automatic identification of the contains and the co

3. Transmission time should be limited to 75 seconds to prevent channels being monopolised.

Apart from the above, and a few purely technical proposals concerning standards which should be high enough to prevent interference to other services but not so unnecessarily high as to price Citizens' Band equipment out of the market, we believe that a British Citizens' Band should have a minimum of regulations.

Membership of the CBA is £1.50 p.a. for individuals and £5 for clubs.

Yours faithfully,

James M. Bryant, President, Citizens Band Association.

ETI NEWS OCT 1976

STEERING WHEEL? WOT STEERING WHEEL?



We had a very careful second look at this photograph, vowed to give up wine, women, and especially song, (for at least five minutes) then decided yes he was in the back seat, and yes the car was moving. Visions of a huge hoax flashed to the editorial mind frenzied navvies rushing about with the backdrop to simulate movement tiny men crammed into the wing mirrors steering via cunning Chinese arrangements of levers and gears. The. mind boggled.

Alas the answer is nought so scandalous. Quite simply an Australian electronics enthusiast has packed his car full of voice recognition and MPU circuitry to the end that it will now

obey verbal commands - even by walkie-talkie up to a range of 12 miles (Naturally it obeys only its owners voice).

The car has a CCTV system installed which enables the driver to see behind him - very useful in injon country. Infra red sensors pick up red traffic lights and brake the car automatically - no we're not joking. Radar ranging maintains a constant distance with respect to the car in front, and sensors apply the brakes should the car come too close to any object - even people.

All this makes it a better driver than most of us.

ETI NEWS NOV 1976

In a historic ruling, the US Supreme Court has confirmed that private individuals have the right to buy or make their own telephone equipment and connect it to the US telephone network.

Under the ruling it will be legal to hook

up as many devices as the user wishes — computer controlled systems, 'phone diverters, memory diallers, picturephones etc. etc. The only restriction is that the various bits must meet the relevant FCC requirements.

ETINEWS APRIL 1978

DIGITAL RECORDING

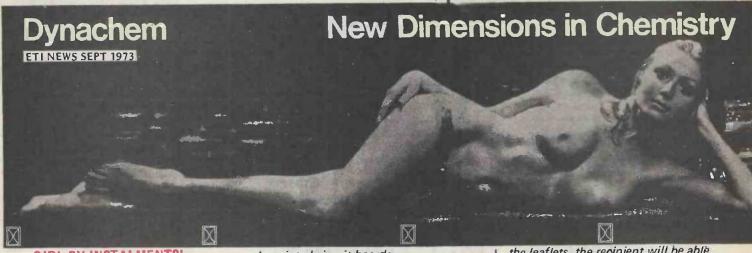
Japan's Nippon Columbia company have developed a digital recording technique. The new equipment, said to cost over £125,000 uses pulse code modulation.

Advantage of this technique is its virtual imperviousness to noise and distortion. Further details will be published as they come to hand.

ETI NEWS JAN 1973

LASER STICK FOR THE BLIND

A stick specially designed for blind persons gives the bearer a loud sonic signal in the event of impediment in his path at wrist height or above. The new device was commissioned by the Swedish Institute for the Handicapped and work on the project was initially financed by the Swedish Board for Technical Development (STU). The prototype stick comprises a 1.3-metrelong tube made of glassfibrereinforced plastic. To it is attached a gallium-arsenide laser, a midget transmitter and receiver, and an amplifier. The power source is a tiny nickel-cadium accumulator. The laser beam's trajectory is almost at right-angles to the stick's length, and as such sticks are normally held forward at an angle of about 45 degrees to the ground, the beam is directed both upward and forward. The laser sends about 1000 pulses per second and when one of these meets an object - such as a forry, car or a road sign - it is reflected back to the stick, where it is electronically transformed into a sonic warning signal to alert the bearer. ETI NEWS NOV 1972



GIRL BY INSTALMENTS!

Electronics manufacturers throughout Europe are receiving a series of unusual sales leaflets from a manufacturer of specialist chemicals used in the making of

printed circuit boards.

Dynachem are sending out four leaflets spaced at regular intervals. On the front of each will be printed a tantalising part of the company's DYNAGIRL, an exquisite young lady well worth a second look. By keeping the leaflets, the recipient will be able to build up a complete picture.

On the reverse sides will be information about the company's range of photo-resists, plating solutions, brighteners, cleaners and ancillary chemicals.

ZX81 HARDWARE

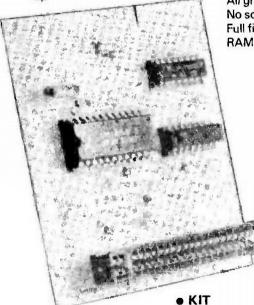
- KEYBOARD KIT 20.75 25.50 BUILT 10.30 CASE
- BUILT & FITTED IN 36.15 CASE



KIT 16.95 • BUILT 18.95

24 lines, in or out. Programmed by BASIC.





40 typewriter keys. All graphics etc shown. No soldering (built version) just plug in. Full fitting and assembly instructions supplied. RAM pack operation not effected.



16.95

18.95

Ready punched top. All screws supplied. Feet supplied. (For keyboard only, ZX81 does not fit inside).





CONNECTORS

• ZX81 23 WAY	2.95
MALE CONN	1.30
IN-OUT/MUSIC BD	3.00
• 24 WAY RIBBON CABLE	1.40
RAM PACK CONN	6.95

(Allows RAM pack to be mounted away from ZX81).

3 outputs. .01Hz to 2Mhz.

MUSIC BOARD

Programme by BASIC.

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	21041	155	86	-60	341p
	21047	156	86	80	407p
	21042	125	85	30	222p
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IPK screws		70	133	38	85p
	87	70 101	101	38	850
	AB8		70	38	850
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	#b10	101	64	51	850
	A811	101 76	51	25	850
	AB12	152	101	51	67p
	A813 AB14/2	127	89	64	99p
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Plastic ABS	20002	100	50	25	87p
	2004	121	66	40	106p
	2005	152	82	50	123p
	2006	192	113	51	216p
Plain Diecast					
Druggi	5001P	50	50	25	880
	5002P	100	50	25	110p
	5003P	113	63	31	130p
	5004P	121	66	40	150p
	5005P	152	82	50	196p
	5006P	192	113	61	305p
Grey painted Did	ocast				
21.04 hamiten Du	5001	50	50	25	116p
	5002	100	50	25	145p
	5003	113	63	31	190p
	5004	121	66	40	145p
1	5006	152	82	50	322p
	5006	192	113	61	4260

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Ways 2 3 4 5(180°C) 6	Plug 8p 14p 15p	8p 8p 14p 20p 19p	Ways 9 15 25 37	Sock 104p 147p 218p 315p	78p 106p 150p	130p 139p 152p 160p	

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(giving about 14V on full load)

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ETI NEWS SEPT 1981

Mini Discs

Philips, Sony and PolyGram have declared the Compact Disc Digital Audio System ripe for production. These companies are unanimous in the belief that this new

system will eventually replace the LP as we know it. PolyGram Records Operations and CBS/Sony have now put their productions on Compact Disc. It is not expected that the CD will be on the market before the autumn of next year.

STEREO CONTROL UNIT

Connect this unit to your existing power amplifier, and at your fingertips you will have a degree of control over the audio spectrum previously unattainable with conventional tone control systems. JVC's unique Model SEA-10 takes the full audio range of 20 to 20,000Hz and divides it up into five discrete frequency bands centred at 40, 250. 1000, 5000, and 15,000Hz. Each band can then be varied independently by ± 12dB using the professional type slider controls with 2dB click stops.



ETI NEWS JULY 1973



CARTRIDGE PERCUSSION UNIT

Bandmaster Limited of Gloucester Street, Glasgow, have designed a rhythm unit called the Powerhouse

which uses multi-track continuous tape loop to produce multi bar synchronised "live" percussion rhythms.

DIGITAL MULTIMETER FROM ADVANCE



The way things are going, the adjective 'digita!' will soon be dropped when talking about test gear. The advantages of digital readout are overwhelming compared to the standard meter (which has of course an analogue readout) and most new quality

test equipment utilises direct digital readout. One of the recently introduced DMM's is the Alpha from Advance Electronics; amongst the many attractive features is the price of £55.

ETI NEWS JUNE 1973.

MPG meter.....

A device called a Mileage Computer (what else?) from the Young Corporation in America is designed to produce a digital readout of miles per gallon being obtained from a vehicle at any given instant.

The device is composed of speed and distance sensors, fuel level indicator and calculator circuit. A sensor attached to the speedo picks up pulses every revolution to provide some of the info needed.

The MPG meter will sell at around \$20 in the USA. ETINEWS DEC 1977

COLOUR PREJUDICE?

Official figures for the number of homes with colour TV's, i.e. those with a license, have just exceeded 50% of the total. Some lesser mortals might well be tempted to conjecture how high the total would be if the un-licensed felons in our midst could be stood up and counted. Naturally we refrain from any such thoughts.

ETI NEWS DEC 1976

TELEPHONE COMPONENTS

High-standard telephony today relies on components and function elements whose design and properties render them equally suitable for use in completely different fields. Read-only memories, MT components, keylock connectors and automatic cutouts are some examples of such components.

The MT (magnetic-core transistor) component developed detection of switching criteria in dc signalling systems, has a magnetic core with a rectangular hysteresis loop to detect signals which are amplified by the transistor. The core and transistor circuits are operated at the same potential and the defined Yes/No statements can be evaluated electronically or via relay circuits.

ETINEWS APRIL 1973

PLASTIC BOXES

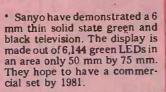
Vero Electronics Limited have recently become distributors for the Odenwalder Kunststoffwerk range of plastic products which include a range of plastic boxes. These are manufactured from high impact polystyrene, which is suitable for machining, engraving and silk screen printing. The upper portion of the box is coloured light grey and the lower portion, dark grey. The latter is provided with integral fixing points for circuit boards. The boxes can be free standing or wall mounting and should provide an attractive enclosure for reader's projects.

Vero Electronics Limited, Industrial Estate, Chandler's Ford, Eastleigh, Hants.
ETI NEWS JAN 1974



* Polaroid are about to release an automatic focusing camera that uses an ultra-sonic transducer to measure distance.

* Computers stores in the US are opening up literally every day — we have just heard that 700 have been identified by someone preparing an exhibition! In addition to those dedicated to Home computers, office equipment suppliers and camera shops are at the forefront when it comes to jumping on the bandwagon; even Macey's stores have now got a computer department in some of their stores.



* A radar based overspeed detector is in use in the U.S. of A, the unit measures your speed and lights up a neon sign saying YOUR SPEED IS ... REDUCE SPEED. The unit is very effective, only problem was the local hot-rodders using it to check their top speed! Problem solved by limiting display to 75 instead

ETI NEWS SEPT 1978

CMOS IN PLASTIC PACKAGES

Motorola Semiconductors have just announced that 39 devices from their standard CMOS logic family are now available in plastic packages. In the past, ceramic packages have been used for all CMOS devices

ETI NEWS SEPT 1973

FAIRCHILD TO MAKE CONSUMER PRODUCTS

The USA's Fairchild group are actively planning to enter the consumer products market, according to a usually reliable source.

Fairchild's first products are believed to be a low-end of the market one-chip hand-held calculator with 8-12 digits. However several industry commentors query Fairchild's ability to produce the necessary MOS chips, quoting Lester Hogan's (president of Fairchild) own description of his company's performance in the MOS field as 'disappointing'.

ETI NEWS JUNE 1974

SOVIET RADAR BLAMED FOR HIGH HEART DISEASE

A Russian radar tracking station near the Finnish town of Homaritsi may be responsible for a sharp increase in heart disease and cancer according to Dr. Milton Zaret, an American microwave expert.

The Finnish border towns have the highest rate of heart disease in the world and cancer has increased inexplicably.

ETINEWS JULY 1975

the little cb that santa forgot

Citizen Band radio manufacturers around the world are crying into their transceivers after Xmas. They expected a boost to sales to revive their drooping business, and it didn't materialise. Seems no-one wanted to contact anyone else — not even the reindeer.

ETI NEWS MARCH 1978

BLUE RESEARCH

Your choice of LED colours might include blue in the not so distant future. The new devices, being developed by Siemens, use silicon carbide and are predicted to have a forward voltage drop of 4 V at 50 mA.

ETINEWS OCT 1979



Watch This!

f you're sick of digital watches, how about taking a look at this watch from Casio. Its all analogue, but with a difference. It's fully electronic and has no moving parts. It uses LCD and has conventional hours, minutes and sweep seconds hands. The Model ANSGL is designed to be attractive and fashionable, face colour matches the synthetic strap. Hour positions are marked by standard Roman numerals and all the time settings and adjustments are handled by two buttons, keeping the compact gold-plated watch case simple and uncluttered. The display shows hour and minute hands, and seconds indication is by a third sweep hand or as a series of marks on the face edge to show accumulated seconds. Accuracy is to within 15 seconds a month. RRP is £27.95, but products of this type are often sold cheaper. Further information can be obtained from Casio Electronics Co Ltd, 28 Scrutton Street, London EC2A 4TY

ETI NEWS NOV 1981

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ET7 200V 4A Triacs — 6 for £1
ET7 200V 4A Triacs — 6 for £1
ET8 1500LF 40V PC mntg caps. 5 for £1
ET9 750LF 150V axial caps — 12 for £1
ET9 750LF 150V axial caps — 12 for £1
ET10 ½W 5% CF resistors, 20 each of these values: 2R2, 4R7, 6R8, 22R, 33R, 47R, 68R, 150R, 270R, 560R, 200R, 1k2, 1k5, 2k2, 3k3, 12k, 68k, 82k, 120k, 180k, 750k, 3M9, 6M6, 6M8, 10M. Total 500 for just £3.50
ET11 Mains transformer, 12—0—12V 50mA. 2 for just £1
ET12 100 1N4148 dlodes £2

STABILIZED PSU PANEL



A199 A versatile stabilized power supply voltage (0-30V) and current A) fully variable. Many uses inc bench PSU, Nicad charger, gen. purpose testing. Panel ready built, tested and calibrated. £7.75. Suitable transformer and nots £6.00. Full data supplied.

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The above PSU, transformer, pots, heat-sink, 0-30V and 0-2A meters, switch, terminels, neon and smart cabinet to mount it all in, plus wiring diagram & info.

JUST **£24.95**

MIXED LED PACK

All new full spec by Micro, Fairchild, etc. Red, Yellow, Green, Amber, Clear, 3mm & 5mm. Pack of 50 asstd £3.95; 250 £15

1W AMP PANELS

AUTI Compact audio amp Intended for record player on panel 95 x 65mm including vol control and switch, complete with knobs. Apart from amp circuitry built around LM380N or TBA820M, there is a speed control circuit using 5 transistrost young the properties of the p operation, connexion data supplied.

OP-AMP PSU KIT

A198 All parts + instructions to make a 50mA + 15, 0, -15V supply from mains input. Only £1.96

P.C. ETCHING KIT MkV

The best value in etching kits on the market — contains 100 aq ins copper clad board, Ferric Chloride, Etch resist pen, abrasive cleaner, two miniature drill bits, etching dish and instructions. All for £4.95.

PANELS

Z621 Panel with 16236 (2N3442) on small heat sink, 2N2223 duel trensistor, 2 BC108, dicides, caps, resistors, etc. 60p.
Z527 Reed relay panel — contains 2 × 6V 2\$030 or 2\$230, 6 × 400V ects + Rs. 50p.

74 series log. 2529 Pack of ex-computer panels containing 74 series log. Lots of different gates and complex logic. All ICs are marked with type

no. or code for which an identification sheet is supplied. 20 ICs £1.00; 100 ICs £4.00 A504 Black case 50 x 50 x 78mm with octal base. PCB inside has 24V reed relay, 200V 7A SCR, 4 x 5A 200V rects, etc. 60p.

CHEAP CHIPS

76477 Sound IC £1.25 2102A RAM 8 for £3 MK4027 shift reg. 8 for £6 uA78MG + volt reg £1.00 uA79MG - volt reg £1.20 74LS112 Dual Flip-Flop 8 for £1 TIL311 Hexadecimal display with decode 0—9 and A—F. With data £3.50.

DEVELOPMENT PACKS

These packs of brand new top quality components are designed to give the constructor a complete range so the right value is to hand whenever required. They also give a substantial saving over buying individual parts.

K001 50V ceramic plate capacitors, 5%, 10 of each value 22pF to 1,000pF, total 210 £4.80

X002 Extended range 22pF to 0.1. Values over 1000pF are of a greater tolerance. 10 of each value 22, 27, 33, 39, 47, 56, 68, 82, 100, 120, 150, 180, 220, 270, 330, 390, 470, 560, 680, 820, 1000, 1500, 2200, 3300, 4700, 6800, 01, 015, 022, 033, 047, 1

K003 C280 or similar Polyestar capacitors. 10 each of the following: 01, 015, 022, 033, .047, .068, .1, .15, .22, .33 and .47uF PRICE CS.40

.47uF PRICE E.5.40 K004 Mylar capacitors. Small size, vertical mounting 100V. 10 each of the following: .001, .0012, .0015, .0018, .0022, .0027, .0033, .0039, .0047, .0056, .0068, .0082, .01. Total 130 capacitors PRICE £4.70

K007 Electrolytic capacitors 25V working small physical size axial or radial leads. 10 each of the following: 1, 2.2, 4.7, 10, 22, 47, 100uF. Total 70 capacitors. PRICE

K008 Extended range, as above, also including 220, 470 and 1000uF all at 25V. Total of 100 capacitors. PRICE £6.35

K021 CR26 resistors or similar, miniature % watt carbon film 5%, as used in nearly all projects. 10 of each value from 10 ohms to 1M, E12 series. Total 610 resistors. PRICE £5.95

K041 Zener diodes 400mW 6%, 10 each of all the values from 2V7 to 36V. Total 280 zeners, PRICE £15.95

K051 LEDs. Pack of 60 comprising 10 each red, green and yellow 3mm and 5mm together with clips. PRICE £8.96

UHF TUNERS
GJE Sylvania F4720 Channels 21—69. Brand new, no data £3.00

VHF TUNERS

Type F3720 (CCIR) by Sylvania. Bargain at only £3.00.

RELAY/TRIAC PANEL MKII

Z537A PCB 100 × 75mm containing a weelth of components: 2 × 12V DPCD min relays. 5C146E 10A 400V ridac, 555 timer, 10 × 114401 diodes, 2NS061 5CR, 2 × 3mm LED 8 3 × 2N3704, R'a 67 C's — Amazing value — if bought separately, parts would cost around £811 Our price for the panel, just £1.50

LIE DETECTOR



Not a toy, this precision instrument was originally part of an "Open University" course, used to measure a change in emotional bilance, or as a "id detector, Full details of how to use it are given, and a circuit diagram. Supplied complete with probes, leads and conductive jelly. Needs 2 4 ½V batts. Overall size 155 x 100 x 100mm. Only £7,55 — worth that for the case and meter alone!

1000 RESISTORS £2.50

We've just purchased another 5 million preformed resistors, and can make a similar offer to that made two years ago, at the same pricell? K523 — 1000 mixed ¼ and ¼ W 5% carbon film resistors, preformed for PCB mntg. Enormous range of preferred values. 1000 for £2.50; 6000 £10; 20k £36

200 ELECTROLYTICS £4.00

K524 Large variety of values/voltages, mostly cropped leads for PCB mntg, 1—1000uF, 10—63V. All new full spec components, not chuck-outs!! 200 £4; 1000 £17.50

CAPACITOR BARGAINS

2200uF 100V cars 80 × 40mm dia 75p; 10/£5,59; 220uF 100V axial 5p; 100 £2,30; 1000 £16; 400 + 100uF 275V 102 × 44mm dia. 75p; 10 £5,50; 200uF 350V, 100 + 100 + 50uF 300V can 75 × 44mm dia. 40p; 10/£3; 100/£20; 100uF 25V Axial 53/100

2000/250V ad. 40p; 10/623; 100/620; 1000F 25V Axial 23/100.
0.339F 50V rad. £1.50/100, £12/1000 elec 22/F50V rad. £1.50/100, £12/1000 elec 22/F50V rad. £1.50/100, £12/1000 elec 22/F50V rad. £1.50/100/£12/1000 elec 22/F50V rad. £1.50/100/£150 100/£3; 4.7u/63V PC mrtg apma price 12/50/25V can 10/£1.50 100/£15 1500u/40V can 10/£3.50 100/£15 1500u/40V can 10/£5.50 100/£15 1000/£15 1000/£15 1000/£15 1000u/350V (100 + 100 + 50/300V talt in one can) 10/£5.00 100/£36.00

TOROIDAL TRANSFORMER

110mm dia × 40mm deep. 110/240V pri., Sec 18V 4A, 6.3V 1A, 240V 0,3A. Idaal for scopes, monitors, VDU's etc. Special low price £5.95

TRANSFORMERS

Mains primary, 50V 20A sec. £20.00 Mains pri. 110V 15A sec £30; 20A £40.00

DISC CERAMICS

0.22uF 12V 9mm dia, Ideal for decoupling, 100 for 22.75, 1000 £20.00 0.05uF 12V 15mm dia, 100 £1.50; 1000 £12.00 Pack of disc ceramics, assorted values and voltages — 200 for £1.00

1N4006 DIODES

Special purchase of 1A rects, Russian made. Packed in boxes of 300, £8.50 per box; 4 boxes £30.00; 10 boxes £75

AUDIBLE WARNING DEVICE

Solid state circuit drives high efficiency transducer to give high output. Voltage regd 6—18V. Can also be driven direct from TTL or CMOS. Module size 45 × 21 × 12mm. Comprehensive data supplied £150

NICAD CHARGER

Versatile unit for charging AA, C, D and PP3 batteries. Charge/test switch, LED indicators at each of the 8 charging points. Mains powered. 210 x 100 x 50mm. £7.95

ULTRASONIC ALARM - £14.95

Originally made to retail at over £50, these neat units housed in a 120 × 100 × 45mm case are brand new and boxed. They work by transmission of a 40kHz beam which responds to movement by detecting the Doopler freq. shift. Mains operated with internal buzzer and provided with data, these units are excellent value at only £14.95

SOLENOIDS AND RELAYS

W921 Solenoid rated 480 va 25% duty cycle, but work well on 24V 1700gm pull, (form travel) push or pull 27 × 18 × 15mm 55p W922 Mains 240V ac solenoid, 10% duty cycle, push or pull, 16mm travel. 50 × 20 × 16mm. Only 1.50 va 100 value.

E1.50
W895 9V DC relay 500R 5PCO 28' × 24 × 19, 50p
W895 9V DC relay 500R 5PCO 28' × 24 × 19, 50p
W7933 11 pin plug in relay, 240V ac, 3PCO 5A
contacts E2.50. Base £36p
W838 700R 24V 4PCO "continental" relay 35 ×
30 × 18, only 84p; 10/£7,00
W847 37R 5—10V relay, 5P 3A contact, PCB
mntg 11 × 33 × 20. 95p; 10/£7,50
W893 0mron LY4 mains relay, 4PCO 5A contacts.
£2.50

£2.50 W896 24V ac coil, but works well on 6V DC. 2 × 10A c/o contacts. Exequip, only 60p

AMAZINGI COMPUTER GAMES

PCB's for PEANUTS!!

A bulk purchase of PCB's from several well known computer games including Battleships, Simon, Logic 5 and Starbird enable us to offer these at incredibly low prices:

'STARBIRD'

Gives realistic engine sounds and tlashing laser blasts — accelerating engine noise when module is pointed up, decelerating noise when pointed dowin. Press contact to see flash and hear blast of lasers shooting. PCB tested and working complete with speaker and batt. (3) (needs PP3). PCB size 130 x 60mm. Only C2.59

'SIMON'

The object of this game is to repeal correctly a longer and longer sequence of signals in 3 different games, (Instructions Included). PCB contains chips, switches, lempholders and lamps, and is tested working, complete with speaker. Needs PP3 and 2 x HP11. PCB size 130 x 130mm. Only £3.95

COMPUTER BATTLESHIPS

"COMPUTER BATTLESHIPS"
Probably one of the most popular electronic games on the market. Unfortunately the design makes it impractical to test the PCB as a working model, although a may well function perfectly. Instead we have tested the sound chip, and sell the board for its component value: SN7847 sound IC; TMS1000 u-processor; that cflbs, R's, C'a etc. Siza 160 x 140mm. Only £1.50. Instruction book and circuit 30p extra "MICROVISION" Cartridges
These are a small PCB with a micro-processor.

these are a small PCB with a micro-processor chip, designed to plug in to the micro-processor chip, designed to plug in to the micro-sion console. Only snag is we don't have any consolest! However, they can be used as an oscillator with 4 different freq. Outputs simply by connecting a battery and speaker. Tested and working Iss an oscil with pin out data. PCB size 72 × 60mm.

ONLY 25p each!!

LOGIC 5 PANEL

Tested Logic 5 now sold out — but we have some PCB's with 10 LED's and chip on, but no keyboard. Not tested, 50p

ELECTRO-DIAL



Electrical combination lock — for maximum security — pick proof. 1 million combinations!] Dial is turned to the right to one number, lett to a second number, then right again to a third number. Only when this has been completed in the correct sequence will the electrical contacts close. These can be used to operate a relay or solenorid. Overall dia. 65mm × 60mm deep. Only of 6

Also availabe without combination — Only £3.95

1982 CATALOGUE

print, but the big new 1982/3 edition is now out of print, but the big new 1982/3 edition should be ready by late March '82 — Send 75p for your copy now!!

WHOLESALE LIST

We have in stock many millions of components—we supply shops, M/O companies, Schools, Industrial Users etc. Can we supply you, too? Our quantity (100+) prices for new full-spec components is very competitive. Ask for our free bulk-buyers list.

NEW CONTROL SYSTEM FOR SLR CAMERAS

Electronic shutter speed and exposure controls can now be built into single lens reflex cameras without mechanically modifying the camera bodies or

A new control system, developed by Matsushita Electrical Industrial Corporation, measures the light at a preset aperture (in less than two

milliseconds) and then sets exposure time accordingly. Control range varies from 0.0005 seconds to four seconds dependent upon lens aperture and film speed.

Prior to the Matsushita development, it was necessary to have a light measuring device accommodated behind the main lens - calculating light intensity with the lens held wide open. ETI NEWS JULY 1975

Elrad: ETT Germany.....

A new edition of ETI starts this month - Elrad in Germany. The name Elrad itself means nothing and is simply an amalgamation of electronics and radio. It is being published by Heinz Heise in Hanover and is edited ETI NEWS JAN 1978 by Udo Wittig

RIDING HIGH

The next step in America's space programme is the tesing of NASA's space shuttle. Landing tests are to be carried out in mid 1977, Amazingly the machine will be launched 'piggyback' from a Jumbo 747! Several



flights will be made to ensure stability before the shuttle is actually released. Trust Americans to build the worlds largest airliner and then carry people outside it! ETINEWS AUG 1976

COSMOS NOW CHEAPER THAN TTL FOR MAJORITY OF DIGITAL SYSTEMS

RCA has announced further price reductions in its CD4000 range of COS/MOS integrated circuits: The reductions range from 35% to 50%. The biggest price reductions have affected the more established MSI devices of the CD4000 range, with many types being reduced by over 50%.

As a result of the price cuts, many of the popular TTL devices are currently more expensive than the equivalent COS/MOS functions.

ETI NEWS SEPT 1975



CB2B

t long last a specification has A been published by the Home Office for the legalisation of Citizen's Band radio. Two frequencies will be allocated: 934.025 to 934.975 MHz and 27.60125 to 27.99125 MHz. For the 934 MHz (AM) frequencies the maximum power is 8 W (25 W ERP), 20 channels at 50 kHz channel spacing. Hand-held units are restricted to 3 W PEP. On the 27 MHz (FM) frequencies the maximum power is 4 W (2 W ERP), 40 channels at 10 kHz spacing. Frequency tolerance: ±1.5 kHz. Maximum frequency deviation: ±2.5 kHz. Adjacent channel power: -60 dB to 2 uW, spurious emission less than 50 nW.

PLAY-ALONG-WITH-RCA

Single chip I/O for video games is the laudible aim of messers. RCA. To be introduced in January the device is primarily a vertical and horizontal synching circuit designed for use with RCA's 1802 MPU. Price could well be around £12 when and if introduced into this country.

ETI NEWS DEC 1976

Right — now you've stopped staring at the picture can we proceed with this month's news. Thank you. Once again our old friends CBM have managed to get in on the act. The above watches yes watches — represent their

long-awaited entry into the digital watch market - with the 5,000 series. All three use a common module, with the casings making for a price range of £17.50-£21.00.

ETINEWS IAN 1977

TTL	-	74368 55p	4014	50p	LINEAR I.Cs	_	M83712	225p	60		MITE	5	MO	δÃ	RICRITO	- COM	NEAT	ION SYSTEMS
7401 7402	11p 11p 12p	74390 100p 74393 100p 74490 120p	4015 4016 4017	60p 3up 45p	AN103 AY1-0212 AY1-1313	200 p 600 p 668 p	MC1310P MC1458	150p 40p 350p	CPUs	MF		-	INTERF		NENTS	Con	JUM	PER LEADS
7403 7404	12p 12p 18p	74LS SERIES 74LS00 12p 74LS01 14p	4018 4019 4020	60 p 32 p 60 p	AY1-1320 AY1-5050 AY3-8910	320p 140p 600p	MC1496 MC3340P	70p 120p	1802CE 2650A 6502	700p £12 450p		400p 120p	AD558CJ AD561J	775p	32.768KH2 18 100KH2 30	Single of Double	end	146p 166p 240p 380p 210p 230p 345p 540p
7407	25p 25p 14p	74LS02 14p 74LS03 14p	4021 4022 4023	65p 70p 20p	AY3-8912 AY5-1224A	660p 240p	MC3403 MK 50398	90p 120p /50p 800p	6602A 6800 6802	800p 370p 4260	2111A 2112-A	300p 300p	AM25S10 AM26LS3 AM26LS3 DAC80	1 160p	200KHz 30 1 DMHz 32 1.008MHz 35	h 1		with Sockets 20pin26pin34pin40pin 160p 210p 270p 300p
7409 7410	15p 16p 20p	74LS04 15p 74LS05 15p 74LS08 16p	4024 4025 4026	40p 20p 130p	AY5-1315 AY5-4007D CA3028A	600p 520p 120p	MM57160 MN6221A	620p	6809 6809F 8035	£10 £15 750p	2114-2L 2114-4L 2147	160p 130p 450p	DM8131 DP8304 DS8832	375p 450p 260p	1,8432MHz 25 2,00MHz 25 .2,45760MHz25	Double 34 Way	end (18" Edge Cor	1290p 395p 490p 540p nn (36") One End £5.50 "M: £5. F: £5.50
7412 7413	20p 22p	74LS09 15p 74LS10 15p 74LS11 15p	4027 4028	32 p 60 p	CA3019 CA3046 CA3048	80p 70p 225 p	NE556	150p 20p 50p	8039 8080A 8085A	850p 350p 550o	4027-3 4044-45 4116-15	300p 450p 200p	DS8833 DS8836 DS8838	225p 160p 225p	2.5MHz 25 3.276MHz 15 3.5796MHz 10	D I	-	NNECTORS
7416	35p 25p 25p	74LS13 250 74LS14 40p 74LS20 15p	4029 4030 4031	75p 40p 170p	CA3069 CA3080E : CA3086	300p 72p	NE564 NE565 NE566	420p 130p 165p	INS8060 TMS9980 ZBO	£11 £20 370p	4116-20 4118-3 4118-4 4164-2	200p 500p 450p	LF13201 MC1488 MC1489	450p 66p 55p	3.686MHz 30 4.00MHz 15 4.794MHz 20	P Hearter	ady guk	Way Way Way Way 90p 200p 240p 270p
7421	17p 30p 20p	74L521 15p 74L522 16p 74L526 16p	4035	80p 295p	CA3089 CA3090AQ	48p 225p 375p	NE567 NE570 NE571	140p 425p 425p	Z80A Z80B 8068	450p £15 £19	5101 6116P 3	650p 300p 650p	MC3418 MC3446 MC3480	950p 300p 850p	4,43MHz150p 5 00MHz 17/ 4 43MHz 150	p E		90p 200p 240p 270p ONNECTORS Plug Skt
7423 7425	22p 28p 30p	74LS27 16p 74LS30 15p	4039 4040 4041	295p 56p 70p	CA3130E CA3140 CA3160E	90p 50p 100p	NE5534A PLLO2A RC4136	150p 500p 70p	SUPPO		6514-45 5810 7489	200p 210p	MC3486 MC4024 MC4044	500p 325p 325p	5.00MHz 175 8.0MHz 156 8.144MHz 256	p DIN 416 p Angled	122 × 32 2 × 32 W	Way 300p 350p ay 350p 400p
7427 7428	25p 30p 15p	74L532 16p 74L537 16p 74L538 16p	4042 4043 4044	56p 60p 70p	CA3161E CA3162 CA3189E	190p 450p 300p	RC4151 RC4558	200p 60p	3242 3245	800p 450p	74\$189 74\$201 74\$289	325p 350p 325p	MC14411 MC14412 MC4644	700p 900p 325p	7.0MHz 150 9.168MHz 171 8.00MHz 171 8.60MHz 171	P DIN 416	3 × 32 W	ay 450p sy 200p 200p
7432 7433	25p 27p	74LS42 38p 74LS47 40p 74LS51 15p	4046 4047 4048	70p 75p	CA3240 CA3260G DAC1408-8	120p 200p 200p	S5668 SAO1024A SFF96364	260p 1250p 800p	6522 6532 6821 6651	500p 775p 160p 660p	ROMs/PR	30Ms	MM58174 ULN20034 ULN20044 75017	4 100p	10.00MHz 26 10.7MHz 15 12MHz 260	P	A	please specify A+B or +C type! ADER PLUGS
7438 7440	27p 30p 17p	74LS55 30p 74LS73 25p 74LS74 16p	4049 4050 4051	55p 27p 27p 60p	HA1366 HA1388	196p 270p 860p	SN/6477 SP8515	350p 175p 750p	6845 6847	180p £10 £10	74S287 74S288	308p 226p 325p	75110 75112 75114	160p 160p 160p	13MHz 350 14,318MHz 176 15MHz 200	P Solder t	ype 1	4pin 16pin 24pin 40pin 50p 60p 100p 275p 130p 140p 200p 285p
7442A 7443	70p 36p 90p	74LS75 24p 74LS76 20p 74LS83 45p	4052 4053	80p 60p	ICL8038 ICM7555 LC7120	300p 80p 326p	TA7120 TA7204 TA7205	185p 195p 125p	6860 6852 6875	150p 250p 600p	745473 745474	650p 650p	75115 75150P 75154	160p 140p 140p	16.00MH ₂ 250 18.00MH ₂ 200 16.432 150			ONNECTORS
7448	60р 93р 46р	74LS85 65a 74LS86 20p 74LS90 28p	4055 4056	130p 125p 120p	LF347	325p 160p	TA7222 TA7310 TBA651	160p 160p 200p	8154 8155 8205	960p 800p 220p	745571	65 0 p 65 0 p 950p	75162 75324 75361	230p 375p 150p	19.968MHz 150 24MHz 175 26.690MHz 150		9	15 25 37 MALE
7451 7453	17p 17p 17p	74LS92 40p 74LS93 30p 74LS95 45p	4060 4063	500p 90p 100p	LF351 LF353 LF356P	48p 100p 95p	TBA800 TBA810 TBA820	90p 100p 90p	8212 8216 8224 8226	160p 160p 250p 250p	EPROMS 1702A 2708	500p 300p	75363 75365 75451/2 75453/4	150p 150p 72p	27.145MHz 200 38.6667MHz 175 48.0MHz 175	p angled	95p 160 _j F	230p 285p 426p EMALE
7460 7470	17p 17p 38p	74LA98 100p 74LS107 45p 74LS109 30p	4068	35p 400p 18p	LF357 LM10C LM301A	120p 425p 27p	TBA950 TCA220	300p 360p	8778 8243 8250	250p 450p 850p		300p £25	75491/2 8T26 8T28	72p 70p 120p 120p	55 5MHz 480 116.0MHz 300	anoted	126 176 100	240p 310p 500p
7473 7474	30p 30p 20p	74LS112 34p 74LS113 30p 74LS114 30p	4069 4070 4071	18p 18p 18p	LM310 LM318 LM319	120p 200p 225p	TCA940 TDA1004A TDA1008	200p 300p 320p	6251 6253 6256	350p 800p 360p	2532 2732 2716-300nS	650p 560p	8795 8797 81LS95	120p 120p 90p	KEYBOARD ENCODER		WITCH	All OKIO
7475 7476 7480	30p 30p 50p	74L5122 42p 74L5123 50p 74L5124 120p	4072 4073 4075	18p 20p 20p	LM324 LM3352 LM339	45p 140p 65p	TDA 1010 TDA 1022 TDA 1024	225p 560p 120p	8257 8259 8279 280PIQ	800p 800p 950p 300p	2732-300nS		81LS96 81LS97 81LS98 9602	120p 90p 120p 220p	AY-6-23/6 700- 74C927 500- MODULATOR:	Bway	120p 105p	24 pin £6 28 pin £8 40 pin £10
7482 7483A	70p 45p	74LS125 30p 74LS126 30p 74LS132 45p	4076 4081 4082	60p 16p 20p	LM348 LM358P LM377	75p 75p 175p	TDA 1034B TDA 1170 TDA 2002V	250p 300p 325p	ZBOAPIO ZBOCTC ZBOACTC	360p 360p 360p	UARTSa AY 3-1015P AY 5-1013P	300p	9637AP 2N425E-8 ZN426E-8	160p 350p	6MH2 UHF 375¢ 8MH2 UHF 460¢	E	DGE C	ONNECTORS 0.1 0.156
7484 1 7485 7486	90p 20p	74LS133 30p 74LS136 30p 74LS138 34p	4093	72p 150p 40p	LM380 LM381AN LM382	75p 180p 120p	TDA2020 TL071/81 TL072/82	320p 45p 75p	280ADART 280ADMA 280S101	800p £12 £12	IM6402	460p 300p	2N427E-8 2N428E-8 DISC CO	550p 500p	BAUD RATE GENERATOR	2 × 18 2 × 22 2 × 23	Way	160p 310p 170p 336p —
7489 2 7490A 7491	210p 26p 60p	74LS139 36p 74LS145 75p 74LS147 160p	4094 1 4095 4096	95p 95p	LM386 LM387 LM389	95p 120p 95p	TL074 TL084 TL094	130p 110p 200p	CONTRO		CHARAC		FD1771 FD1791	£2 £3	0 MC 14411 17	2 x 25 1 x 43 2 x 43	Way Way	210p 200p 260p — 350p —
7492A 7493A 7494	30p 30p 50p	74LS148 90p 74LS161 70p 74LS153 60p	4098	340p 90p 120p	LM393 LM394 LM709	100p 350p 36p	TL170 TL430C UAA170	50р 70р 170р	COM5037 SF96364 FMS9927 6845	£18 £9 £18 £10	GENERAT RO-3-2513U	TORS	FD1793 FD1795 FD1797	£3: £3	5 SAA5020 6			700p -
7495A 7496 7497 1	50p 45p 120p	74LS154 90p 74LS155 40p 74LS156 40p	40097 €1	90p 120p 120p	LM710 LM711	50p 70p	UA2240 UON6118 UDN6184	300p 320p 320p	6847 9365	C10 C50	RO-3-2513LC SN74S282AN	700p N [10	WD1691 WD2143		SAASOMO(1 C1		lasic Kit	N ATOM E120 Built £136 ed 12K + 12K £188
74100	85p 22p 40p	74LS157 35p 74LS158 36p 74LS150 40p		180p 180p 45p	LM733 LM741 LM747	100p 18p 70p	ULN2003 UPC575 UPC592H	100p 275p 200p	8 pin 99	18 pi	OCKETS BY 1 n 16p 24 pin n 18p 28 pin	1 24p	8 pin 2!	PSOCKI 5p 18 pir 5p 20 pir	ETS BY TEXAS n 50p 24 pin 7 n 60p 28 pin 8	0 ₁₂	p&p SEE AF	£2,50/unit PRIL PE FOR M VISION
74116 74118	90p 75p	74LS161 40p 74LS162 40p 74LS163 40p	40109 1 40163 1	100p 100p 120p	LM748 LM2917 LM3302	35p 200p 140p	UPC1156H XR2206 ZN414	275p 300p	16 pin 11s	22 pi	n 22p 40 pir	30p	16 pin 44	0p 22 pir	65p 40 pin 10	Op Phone to	or details	on Atom Accessories
74120 74121 74122	90p 70p 25p 45p	74LS164 48p 74LS165 100p	40174 40175	90p 100p 120p	LM3900 LM3909 LM3911	55p 95p 130p	ZN419C ZN423E	90p 225p 150p	TRANSIS A0161/2 BC107/8	45p 13p	BF X86/7	40p 27p 27p	TIP33A TIP33C TIP34A	70p 80p 90p	2N3054 6bp 2N3055 48p 2N3442 140p 2N3553 240p	3N140 3N141 3N201	120p 110p 110p	ZENERS 2 7V-33V 400mW 9p
74123 74125 74126	48p 40p 40p	74LS166 90p 74LS170 120p 74LS173 70p	40257 1 4502	70p 50p	LM3914 LM3915 LM3916	210p 225p 225p	ZN424F ZN425E ZN427E	135p 350p 625p	BC109C BC117 BC147/8 BC149	14p 20p 90	BFY50 BFY51/2	24p 24p	TIP34C TIP35A TIP35C	120p 120p 140p	2N3584 250p 2N3643/4 48p 2N3702/3 12p	3N204 40290 40361/2 40408	120p 260p 75p 90p	TRIACS PLASTIC
74128 74132	40p 45p 32p	74LS174 45p 74LS175 50p 74LS181 140p	4507 4508 2	40p 200p 85p	LM13600 M51513L M51516L	125p 300p 500p	ZN1034E ZN1040E	700p	BC157/8 BC159 BC169C	10p 10p 11p 12p	8FY56 8FY90 8RY39 85X19/20	33p 80p 45p 24p	TIP36A TIP36C TIP41A	140p 150p 50p	2N3704/5 12p 2N3706/7 14p 2N3708/9 12p	40409 40410 40411	100p 100p 300p	3A 400V 60p 6A 400V 70p 6A 500V 68p
74141 74142 2	65p 200p 70p	74LS190 60p 74LS191 60p 74LS192 60p	4511 4512	50p 65p 150p	VOLI	AGE RI	EGULATORS LASTIC		BC172 BC17778 BC179 BC182/3	12p 17p 18p 10p	BU104 BU105	225p 190p 250p	TIP42A TIP42C	66p 60p 65p	2N3773 300p 2N3819 25p 2N3820 40p 2N3823 50p	40594 40595 40673	120p 120p 75p	8A 400V 75p 8A 500V 95p 12A 400V 85p
74147 1	75p	74LS193 48p 74LS194 40p 74LS195 48p		75p 45p	5V 1A	+ ve 7805 7812	50p 7905 50p 7912	56p 66p	8C184 BC187 BC212/3	11p 30p 11p	8U109 2 BU126 1 BU180A	225p 150p 120p	TIP54 TIP120 TIP121	75p 75p	2N3866 90p 2N3902 700p	40871/2 DIODES	100p	12A 500V 105p 16A 400V 110p 16A 500V 130p
74151A 74153 74154	80p 45p 46p	74LS196 60p 74LS197 85p 74LS221 60p	4520 4521 1	70p	15V 1A 18V 1A	7815 7818 7824	55p 7915 56p 7918 55p 7924	60p 60p	BC214 BC237 BC327	12p 15p 16p	BU208 2	200p 200p 145o £6	T/P122 TIP142 TIP147 T#P2955	130p 130p 130p 78p	2N3905/6 16p 2N4037 65p	8Y127 8YX35.300 OA47	12p 20p 8p	T2800D 130p
74155 74156	70p 50p 50p	74LS240 70p 74LS241 70p 74LS242 80p	4527 4528	90p 75p 90p	5V 100mA 12V 100mA	78L05 78L12 78L15	30p 79L05 30p 79L12 30p 79L15	65p 70p 70p	BC337 BC338 BC461	16p 16p 25p 30p		350p 50p £4	TIP4055 TIS93 ZTX 108	70p 30p 12p	2N4123/4 27p 2N4125/6 27p 2N4401/3 27p 2N4427 90p	OA90/91 OA95 OA200	9p 9p 9p	3A 400V 100p BA 600V 140p 12A 400V 180p
74159 1 74160	50p 100p 60p	74LS243 80p 74LS244 66p 74LS245 90p	4534 5 4536 3	500p 300p 120p	OTHER REGULA LM309K 1A 5V		78HGKC	600p	BC477/B BC516/7 BC5478 BC548C	40p 14p	MJ2501 3 MJ2955	225p 90p 225p £4	ZTX300 ZTX452 ZTX500 ZTX502	13p 45p 15p 16p	2N4871 60p 2N5087 27p 2N5089 27p	OA202 1N914 1N916 1N4148	10p 4p 7p	16A 100V 180p 16A 400V 180p C106D 45p
74163	60p 60p	74LS253 40p 74LS253 40p 74LS257 45p	4539 1 4543 1	110p 100p 100p	LM317K LM317T IA Ad LM337T	325p 200p 225p	78HO5KC 78MGT2C 78GUIC	560p 140r 200p	BC549C BC557KB BC559C	12p 16p 14p	MJ4502 MJE340 MJE2955 MJE3055	60p 160p 70p 40p	2TX502 2TX504 2TX562 2TX652	16p 18p 60p	2N5172 27p 2N5191 90p 2N5194 90p 2N5245 40p	1N4001/2 1N4003/4 17/4005	4p 5p 6p 6p 7p 14p	MCR101 36p TIC44 27p 2N3525 130p
74165 74166	50p 65p 70p	74LS258 40p 74LS259 90p 74LS260 24p 74LS266 25p	4555 4556	50p 60p 80p	LM323K 3A 5V LM723 150mA A TL494	500 n	79GUIC 79HGKC TL497	225p 700p 300p	BCY70 BCY71/2 BD131/2	16 p 18 p 22 p 50 p	MPF103/4 MPF105	40p 30p 30p	ZTX752 VN65AF VN10RM	70p 72p 60p	2N5298 65p 2N5491 60p 2N5457/8 40p	1N4006/7 1N5401/3 1N5404/7	19p	2N4444 180p 2N5060 30p 2N5064 35p
74173	40р 100р 65р 60р	74LS273 70p 74LS279 45p	4569 1	100p	78S40 OPTO-ELECTRO 2N5777	300p	LM305AH DRP60	250p	BD135/6 BD139 BD140	40p 40p 40p	MPSA08 MPSA12 MPSA13	30p 50p 50p	2N697 2N698	80p 25p 46p	2N5459 40p 2N5480 60p 2N5485 44p	15920	9p	PCB MOUNTING RELAYS
74175 74176	60p 50p 70p	74LS283 450 74LS298 1600 74LS323 2500	4683 4684	45p	OCP71 ORP12	190p 120p	ORP61 TIL78	120p 120p 56p	BD189 BD232 BD233 BD235	60p 60p 75p 85p	MPSA42 MPSA43	50p 50p	2N706A 2N708 2N918	30p 30p 45p	7N5875 250p 2N6027 48p 2N6052 300p 2N6059 325p	BRIDGE RECTIFIERS	, 19p	6 or 12V DC Coil SPDT 2A 24V DC 160p
74178 19 74180	00p 50p 60p	74LS324 150p 74LS348 150p 74LS352 100p	14495 4	100p 100p	OPTO-ISOLATO ILD74 MC126	130p 100p	TIL111 TIL112	90p 90p	BD241 BD242 BD677	60p 60p 40p	MPSA56 MPSA70 MPSA93 MSPU06	32p 50p 40p 63p	2N930 2N1131/2 2N1613 2N1711	18p 36p 25p 25p	2N6107 65p 2N6247 190p 2N5254 130p	1A 100V 1A 400V 1A 600V	20p 25p 30p	6 or 12V DC coil DPDT 5A 24V DC 240V AC 200p
74182 74184A	90p 90p	74LS353 100p 74LS363 160p	748 SERIE 74500 74504	60p	ILO74 LEDS	190p 240p	T1L113 T1L116 0.2"	90p 90p	BF2448 BF2568	36p 50p	MPSU07 MPSU45 MPSU65	60ρ 90ρ 78ρ	2N2102 2N2160 2N2219A	70p 350p 25p 25p	2N5290 659 2SC1172 1509 2SC1306 1009	ZA 50V ZA 180V ZA 400V	30p 35p 45p	6 or 12V DC Coil SPDT 10A 24V DC 240V AC 225p
74186 54 74188 3	20p 00p 26p	74LS364 160p 74LS365 36p 74LS367 36p	74508 74532 74574	76p 90p 90p	0.125" TIL32 TIL209 Red	56p 11p	TIL220 Red TIL222 Gr TIL228 Yei	12p 15p 22p	BF257/8 BF337 BFR39 BFR40/1	30p 25p 25p	TIP29A TIP29C TIP30A	35p 40p 35p	2NZ2Z2A 2NZ369A 2N2484	25p	2SC1307 150p 2SC1957 90p 2SC1969 150p	3A 600V 4A 100V 4A 400V	60n 72p 95p 100p	
74191 ! 74192 !	50p 50p	74LS373 70p 74LS374 70p	74586 3 74586 1 745124 3	180p 180p	TIL211 Gr TIL212 Ye TIL216 Red	16p 18p 18	Rectangular LEDs (R, G, Y) NSB5881	30p 570p	BFR40/1 BFR79 RFR80/1 BFR96	25p 25p 25p 180p	TIP30C TIP31A TIP31C	40p 40p 45p	2N2646 2N2904/5 2N2906A 2N2907A	45p 25p 25p	2SC2028 96p 2SC2029 250p 2SC2078 200p	6A 50V 6A 100V 8A 400V	80p 100p 120p	RELAYS FOR ALL ETI PROJECTS AVAILABLE
74194 74195	50р 70р 60 р	74LS375 50p 74LS377 70p 74LS378 80p	745132 1 745133 745138 2	75p 225p	DISPLAYS 3015F	200p	TIL311 TIL312/3 TIL321/2	600p 110 130p	BFX29 BFX30	40p 27p	TIP32A TIP32C	45p 40p	2N2926 2N3053	25p 30p	2SC2612 250p 3N128 120p		200p 400p	EX STOCK
74197 74198 1	70p 80p 100p	74LS390 56p 74LS393 50p 74LS399 200p	74S139 2 74S157 2	225p 250p 300p	DL707 Red FND357	140p 140p 120p	7750/60 DAIVERS	140p 200p	The co	mple1e	microproces	sor dev	elopment	SOF system	for Engineers ar	d Hobbyists	. You	can develop your
74221 74258		74LS540 135p 74LS541 135p 74LS670 170p	745174 2 745175 3 745194 3	250p 320p 150p	FND500 FND507 MAN3640	90p 90p 175p	9368 9370 UON6118	250p 300p 323p	progran	nmes, v	renty, debug ROMULATOI	and co R. See	the review	in Sept.	il accept most +	SV EPROMS.		
74279 74283	50p 80p 75p	4000 SERIES 4000 12p 4001 14p	745241 4	100p		200p	FER #	320p			/IB £42			V ER	ASERS			141 £78
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	-1		JRNIEY	L				4	NR Uncl	. all col					terface, 2K moni 15% VAT ((Bs) £72 P&P £1

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CZECH ON CALCULATOR PRICES **ETINEWS MAY 1976**

A typical dour Czech day. The rain sleets across Prague. Somewhere in the back streets well away from the patrols and the populace, Ivan scuttles into a dingy corner shop.

There, amid the Western papers and naughty mags, he spots the

object of his desires.

Eyes alight he lifts the proscribed machine from the rack. and carries it reverently to the counter, behind which stands the owner

'How much?' he stammers.

hands shaking

Novus 650 comrade? To you, £172. Crossed the border this morning right under the army's noses." he looks around furtively, and leans across the counter.

whispering.

Interested in the REAL thing eh comrade? "Ivan nods. The man reaches below the counter and produces a battered show box. Ivan's eyes are wide by now, riveted to the lid as it lifts. Inside lies a full frontal scientific, a HP 45.

Ivan faints.

Now before you dismiss this as merely the alcoholic follies of the ETI staff, following a party, let us inform you dear reader, that whilst we may be guilty of slight embroidery, our flight of fancy is based on fact.

It seems our Eastern friends consider pocket calculators to be highly prized items, and will pay vast sums to acquire them. What would cost you or I £7, our Ivan would need £172 to own. For that HP 45 you could possibly get a weekend with Siberian Sue, belle of the Balkans.

The reason behind this black marketing and smuggling is that calculator ships are not produced behind the ferric curtain and the machines are banned from importers lists by the governments, to preserve foreign exchange as their value is so high.

I wonder how they count it?

FOUR CHANNEL DISCS

In the UK the EMI group have announced plans to release quadraphonic discs - using the CBS developed 'SQ Matrix' system - in April.

The company claims that the new discs will be fully compatible with existing stereo equipment.

ETI NEWS APRIL 1972

COMPUTER 'ON A CHIP' WITH CASSETTE TAPE

A new byte-orientated micro-computer with its own in-built cassette tape backing storage has been produced by Computer Electronics Ltd, of Saffron Walden, Essex, as part of its range of cassette tape data systems.



Believed to be one of the first 'processors on a chip' computers to be developed in this country, the complete computer fits on one of the company's standard printed circuit **ETINEWS AUG 1973**

CALLING ALL K9s, R202s, ROBBIES, C3POs, MICROMICE

etc, etc.....

ETI is very keen in getting a robot

dialogue going. Anyone out there on

the other side of the printers ink interested in robotics, especially anyone actually building robots

of WHATEVER complexity - should contact us here at ETI. If possible how about some photographs

of your machines? They may well be in line for an appearence in ETI. So come on, lets be hearing from you ALL of you - take pen in hand (or get the robot to do it) and write to

The Editor, ETI Magazine, 145 Charing Cross Road, London WC2. Mark your envelope "ROBOTS"

So we can deal with it with our usual machine - like_efficiency. ET! NEWS NOV 1979

TV GAMES LSI CHIP AVAILABLE SOON

Rumours have been abounding for about a year now that an LSI chip for television games was being developed.

We now have definite news that Logic Leisure, a British Company, have produced a chip which will produce four TV games, with two variations on each, giving eight permutations. There is score and sound facility. Type number is not yet known but the chip is suitable for both 625-line, 50Hz and 525-line, 60Hz.

It is hoped that the chip will be on sale in October and the price tag is going to be in the £10-£12 range (plus VAT). U.K. distributorship is in the hands of Television Sprots Co. Ltd., 6 Half Moon Street, Mayfair, London, WIY 7RA. ETI NEWS AUG 1975

ETI NEWS SEPT 1978

brief news

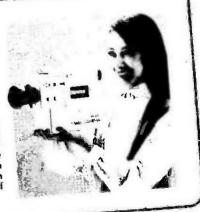
NASA have received weak signals from Skylab for the first time in four years. The possibility of sending it deeper into space is being considered.

* A study by the American National Institute for Occupational Safety and Health (Niosh) has con-cluded that VDUs in use in the offices of the New York Times are not responsible for cataracts developed by two copy editors working there.

Hitachi MAGic

itachi have developed an experimental colour video camera combined with a video tape recorder — provisionally christened the 'MAG Camera'. Using high density recording techniques, the combination is little bigger than an 8 mm sing camera. The carrette using mm cine camera. The cassette, using 1/4" tape, is almost as small as an audio cassette and allows two hours of recording/playback. The complete unit weighs only 2.6 kg, including a rechargeable battery pack. Watch this space for news on development of the MAG Camera.

ETI NEWS JAN 1981



From a firm called James Niell comes the Micro 2000 to rise into our News Digest with carefully measured precision. This instrument gets our vote for the best innovation of the year already! A digital micrometer no less.

As you can see from the picture, it actually reads out a measurement in seven-segment format. Goodbye verniers. It has so many features and advances, it is perhaps best simply to list them.

Accuracy to ± 0.002 mm., with a 'constant force' spindle and selfcalibration facility. As soon as it is switched on, the 2000 self zeros.

The zero reset means that it can be used as a comparator against a known standard, and variations from that can

BRITISH? PRECISELY!



be read directly. Also in awkward situations, the instrument can be

zeroed, utilised, and then removed to be read. **ETINEWS IUNE 1977**

Sat 54

Well, it was Satcom 3 actually, but the plot is reminiscent of that old, old American telly series. The Car 54 in this case, however, was an RCA communications satellite, last heard of in December, 22,000 miles above mother Earth.

If anyone finds a communications satellite answering to the name of Satcom 3, send it to RCA, nto us. Mind you, if it has gone up in a puff of smoke, it has probably burned up on its way back to Earth. NASA quick to assure us that it won't cause another Skylab incident. So, you needn't dust off your anti-Skylab umbrella, yet. ETI NEWS MARCH 1980

Text To Talk

KurzwellComputer Products of Cambridge, Massachussetts has developed a machine to turn written text into speech.

The machine contains an optical scanner, a small computer, a small synthesiser and a loudspeaker unit.

The page to be read is placed over the scanning unit which then converts the written text to digital signals for the computer. The computer then converts them into bruos

ETINEWS APRIL 1980

junk calls

From the land that brought us Muzak and MPUs comes the Junk call — the same as Junk mail but verbal! A machine is being used to dial up to 1,000 numbers a day and make a prerecorded sales pitch, unlike junk mail there is no way of knowing when the call will be junk or not. By dialing up numbers from 0001 to 9999 the machine annoys everybody who answers on a particular exchange, even if you hang up it holds the line open until the pitch is finished - this has caused emergency calls to be delayed in some cases.

Ten states are considering legislation to curtail the activ ities of the machines. However they intend to exempt charities, pollsters and politicians. Some people want an electronic 'no thanks' sign to be developed, although nobody is quite sure how it would work. What next?!

ETI NEWS SEPT 1978

HP AT A (CALCULATED) LOSS:

Hewlett-Packard - renowned for their up-market calculators, are apparently running this section of the business at a loss. Equipment and other activities are keeping then in the black, and H.P. cite the delays occurring on the introduction of new models as the cause for this. Also named as a culprit is "severe price erosion in the pocket calculator marketplace". Pick the bones out of that ye rivals of the beast.

ETI NEWS NOV 1976

ELECTRONICS ENGINEERS' SALARIES FALL BEHIND

*A computer system cap

A computer system cap-ble of controlling the lighting and heating in up lighting hundred buildings to one hundred buildings to one set up in London has been set up in London has been set up in London by Honeywell. The system called BOSS, is the called BOSS, is the its kind in the UK.

ETINEWS MAY 1978

The 'Survey of Salaries', published by the Management Survey Centre this August, shows that the salaries of electronic engineers working for large companies have stagnated whilst other engineers' salaries have increased. Senior chemists have done best - their salaries have increased 3-4 times more quickly than the average.

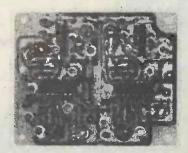
For a senior professional in development (with major responsibilities) the median salary is £4,174; for electronic engineers in particular the median at this level is £3,720.

ETI NEWS OCT 1973

ANRS INTEGRATED INTO A SINGLE IC CHIP

In 1972, JVC first introduced their Automatic Noise Reduction System (ANRS) into their top-range cassette decks. Since then, ARNS has been incorporated into a wide range of tape decks. Recent improvements however, in cassette deck quality and the possibility of "noise-reduced" FM broadcasts have meant improvements in the quality of noise reduction systems and the application of these systems to components other than cassette tape decks.

To meet these new requirements. JVC has recently completed the development of the ANRS IC.



ETINEWS OCT 1975

CEEFAX AND ORACLE SYSTEMS

COMBINED

The BBC and IBA, together with BREMA and the Broadcasting Department of the Home Office have agreed on a unified system of data broadcasting.

Until now the BBC have been working on CEEFAX, the IBA on ORACLE. Both systems allow a TV viewer to select at will from a number of different 'pages' of information and put these onto his screen.

ETI NEWS JULY 1974

A Preview from the Next Issue of

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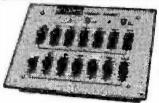


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4-channel STEREO DISCO MIXER

Switchable phono/line i/ps. Cross fade on decks. P.F.L. on deck i/ ps. Master volume control. Mains operated.

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7 hand/channel. Tape monitor button. 12DB boost and cut (each band). Mains operated.



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6 mlc l/ps. 2 stereo line i/ps Slide volume control for each Stereo/mono control output.

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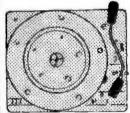
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AUDIOPHILE

Soon burglars won't be bothering to nick your whole hi-fi; they'll just take the cartridge. This month Ron Harris reviews two new pickups, one with a gemstone cantilever and the other a work of modern art.

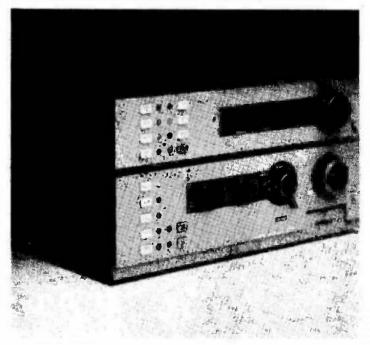
ews just in of a new piece of British circuitry genius. This is a new protection circuit, soon to be added to a famous manufacturer's product, which is claimed to make an amplifier totally invulnerable electrically.

Totally in this case means "even from 240 V mains at input or output". Ultra-fast relays are set at the output and on the supply lines to the PCB. These are driven from the new circuit, which has as its final stage a voltage amp with an incredibly high slew rate. This ensures a high speed of operation for the relays.

Out Of Phase

The protection circuit operates like this: if an amplifier is suddenly faced with a massive input signal, the ratio of the feedback signal to input will drop dramatically. A comparator senses the change and a 'low-feedback' signal is generated. This by itself is sufficient to trip the supply relays, so that the overload cannot be passed on to the output stages, thus destroying them — and probably the speakers.

A second block within the circuitry watches the supply rails and any surges which are outside the requirements of normal drive will trip the protection circuit, since this is a "low-feedback likelihood situation" as the designer puts it. Great play is made of the fact that the music signal and the feedback voltage are in anti-phase at the point of comparison, so no interaction within the buffer is likely. 'Anti-phase reset', as it is called, thus introduces no colouration. Hence the protection reset of the relays can occur either in the case of low feedback-to-signal ratio, or in event of an "overload likelihood". I suppose this is where the somewhat pompous title of the circuit is derived — Anti-Phase Reset In Low Feedback (Or Overload) Likelihood.



Shure MV30HE

A dedicated offshoot of the renowned V15 IV design, the MV30HE is for use in the SME Series III or IIIS only. The cartridge is built into a SME carryarm such that no headshell is used, or needed.

The moving components are those of the V15, save that no damper is provided. The cartridge body is all new, however, and quite a few problems it must have given them getting the coils and poles into a body as slim as this. The design is so arranged that the point of bearing intersection and the stylus line up parallel to the record. This will tend to aid stability in the replay of warped records.

As in the V15 a hyperelliptical stylus is used, which will give lower distortion results than either a spherical or elliptical tip. Tip mass is commendably low and output level is on a par with the V15 IV

Once fitted into the SME the MV30HE looks very smart indeed is and visually extremely classy!

Testing an Armful

In the lab the MV30HE had an easy time passing just about every test. It tracks as well as the V15 IV and measures slightly better. There is no higher technical accolade than that. The LF resonance came out — surprisingly — at around 16 Hz, a little higher than optimum in my opinion. Best values are somewhere around 10-12 Hz so as not to affect extreme LF reproduction. Best tracking was obtained at around 1.0 g, and no improvement was forthcoming for increased force.

Frequency response was boringly perfect at 20 Hz — 20 kHz ± 1.3 dB with a separation figure of 27 dB at 1 kHz. Compliance measured very high at 34 cu, so only the smallest damping paddle is required. It is required however — see later.

Instructive Stuff

The instruction booklet is worth a special mention. It is a straight 'copy' of the SME style, right down to the little diagrams with ticks and crosses for right and wrong answers. Some sort of deal has been struck here, methinks!

One point that I just have to mention here; I could not,

At long last Quad have released their new tuner, the FM 4. It was shown for the first time at the Audio 82 exhibition in Swiss Cottage recently. Designed to match the Quad 44 control unit (preamp to the rest of us) the FM - only unit has digital tuning and seven pre-set stations. Programme locations are stored in memory.

A tuning knob has been retained in preference to a set of pushbuttons, since Quad say it is easier to use.

Brief Specification:

Full limiting	1 V	IF Rejection
S/N (1 V input)	7 dB (stereo)	AM Supression
Distortion (1 KHz)	0.15%	Image Rejection
Canture Ratio	2.5 dB	Crosstalk (1 KHz

100 dB 60 dB 80 dB





APRIL 1982

Dynavector Karat Ruby

Both this month's cartridges are unusual in their own way, Dynavector's Karat is notable for its gemstone cantilever. This 2.5 mm long piece of single-crystal ruby is cut with a laser to accept the stylus (diamond) and then allowed to cool, thus fixing the stylus in place. The length is remarkably short, since Dynavector say that the less material the stylus information has to pass through, the higher will be the fidelity of the output.

Wave propagation through a medium is something not many of us take up as a hobby, but someone down at Dynavector must have it all well sussed! Apparently this equation:-

$$\frac{EI}{m}\,\frac{\partial^4 y}{\partial x^4} + \frac{\partial^2 y}{\partial t^2} - \rho \frac{EI}{m}\,\left(\frac{1}{E} + \frac{\gamma}{G}\right)\,\,\frac{\partial^4 y}{\partial x^2 \partial t^2} + \frac{\rho^2 \gamma}{mG}\,\frac{\partial^4 y}{\partial t^4} = \hat{0}$$

$$C_B = \alpha \sqrt{2\pi f} \left\{ 1 - \frac{1}{4} \beta \frac{2\pi f}{\alpha^2} + \frac{1}{4} \delta (2\pi f)^2 + \frac{1}{4} \delta (2\pi f)^2 \right\}$$

where E = Young's modulus; I = secondary moment of section area; G = shear modulus; m = mass per unit length of a cantilever; p = density of the cantilever material; x = distance from the end of the cantilever; y = flexural displacement of the cantilever; r = constant; t = time.

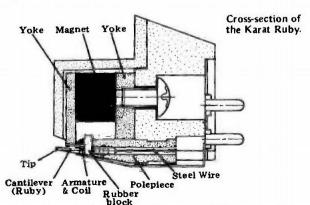
sums up the vibrational behaviour of a cantilever under dynamic conditions. It can also be used to prove that rigid materials, such as ruby and diamond, make for better cantilevers than boron, berylium and the rest.

(There is a 'big brother' to the Ruby, which has a diamond cantilever and costs around £450 as opposed to the Ruby's £100. If I can persuade the ever-helpful Dynavector into lending one I hope to report on the differences soon. Maybe if I say "please"...?)

Temperate Zones of Test

Another piece of original thinking has gone into solving the problem of temperature dependence and damping material. The only rubber used in the Karat is to prevent the cantilever taking its jewelled self up into the body whilst playing records. Normally the pivot damping in a cartridge is accomplished by a rubber block and this is prone to suffer from changes in temperature and slow deterioration as it ages — the Karat suffers neither of these weaknesses.

In fact, due to the short rigid construction of the cantilever, the Ruby requires no damping at all.



Under test the Karat showed a ruler flat response from 100 Hz to 30 kHz of under ± 0.5 dB! It was only 1 dB down at 30 Hz and separation measured an excellent 24 dB at 1 kHz and a more than adequate 18 dB at 20 kHz. Stylus resonance fell at 49 kHz and in the SME Series III (what else?). LF resonance was well placed at 12 Hz, below audibility and above warps.



Tracking was exemplary for a moving-coil unit — at 1.75 g it tracked all my test bands perfectly; the first moving coil to do so. Bias was set for 2.0 g, a high value, but one that worked well. In actual use the Karat was never caught out by any recorded information.

If at this point you're looking around the pages in search of the usual response graphs, don't bother — I haven't included any. If you really want to see a straight line, go buy a ruler. Dishearteningly disappointing for us cynics.

Listening Out

As the Karat Ruby matches the SME Series III so well, it was left in that arm all through the listening test. One brief excursion into a Linn Itokk showed the two to be completely incompatable in my opinion, as the sound stage broke up and the bass became so loose as to be positively flapping! Strange that, as both are capable of much better and there is little on paper to point to such obvious mutual abhoration.

The loudspeakers used were my trusty KEF 105 II's fed by a variety of amplification from Crimson, Monogram and Trio. Source equipment remained at Thorens 160S/SME III throughout.

On the very first LP side I played with the Ruby it was obvious that here was something special. The sound is so detailed and open, with such tight control of the bass that it makes you sit up and take notice of the music. This is a cartridge that will be much appreciated by reviewers, as it is so easy to listen through for long periods.

In fact there is little I can say against the Karat. It is a trifle recessed — I cannot account for this impression from the lab results, however, but it remains a definite impression — but is so relaxed and balanced a sound that none but the most obnoxious could find aught to quibble with. The sound quality reminded me greatly of the Ortofon MC30, but with greater resolution of complex passages and a more extended bass end.

At around £100 the Karat Ruby is an excellent bargain. Even accounting for the required step-up device, this pickup is required listening for anyone in the market. I have no hesitation in saying that it out-performs many units costing much, much more and will give more musical pleasure than just about any other cartridge I know.

Mind you, I haven't heard the Karat Diamond yet... but can it really be worth £350 more? On this evidence I would doubt it! (Pause while Dynavector work out whether this is a compliment or an insult....)

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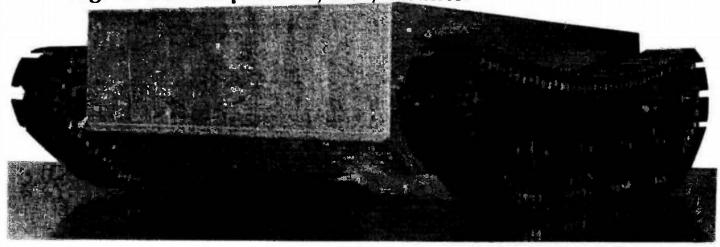
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ROBOT MOTOR CONTROL

This month we feature a control board for last month's motor driving board. This is part 2 in a series of DIY robot modules — collect them all! Design and development by Rory Holmes.



n this second part of the series on the ETI intelligent programmable mobile we shall describe the design of an analogue pulse width modulator for controlling the motor driver stage featured last month. We shall also take a brief look at some of the modules being offered later in the series which can be added in stages to enhance the motorised vehicle. The intention is to build up to a complete computerised mobile.

A lot of flexibility has been allowed for in the actual use and configuration of the modules, as we are well aware that constructors interested in this type of project have firm ideas of their own on the final form and capabilities of their mobile. Construction and interconnection details for all the modules we are presenting will be given along with guidelines to a range of applications.

The facilities we have planned for the mobile will continue with the digital motor control and an on-board programmable computer for overall control of other modules. A light-weight manipulator arm complete with teaching arm has also been designed, for mounting on the front of the mobile. It is powered by four radio control servo motors and the electronics interface between the servos and computer will be described

along with details of the arm mechanics. Optical proximity detectors for object sensing, and infra-red tachogenerators for speed sensing will also be featured on the ETI mobile.

It is hoped that the designs will also prove useful as stand-alone modules for individual use in other applications. Optical proximity detectors, for example, have numerous applications in batch counting, limit sensing, detection, alarms and so on.

The digital pulse width modulator in next month's issue will find many uses in the control of analogue functions; how about a computer interfaced to a pulse width modulated optical data link, for analogue information transmission? Our version will control two pulse width modulated channels, with a resolution of one part in 256, via an eight bit data port; modulation being achieved solely by logic to satisfy the all-digital purists.

Optical Proximity Detectors

These have been designed as small independent units with as much in-built versatility as possible. The circuitry is housed in a short length of aluminium tube axially aligned in the detector direction, with three external

connecting points; ground, positive supply, and an open collector digital output. A number of detectors can thus be easily mounted in strategic locations. All circuit operating parameters are independent of the supply voltage, which can be anywhere between 5 and 35 V at a current of 20 mA.

The proximity switch works on the principle of transmitting and detecting a modulated infra-red beam. The infra-red transmitter receives 1 A peak current pulses, of 10 uS duration, with a modulation frequency of 1 kHz. The 100:1 duty-factor thus achieved allows high currents to be used to increase the detection range, while reducing the average supply current to only 10 mA.

The sensor can be set by a preset pot, accessible through a small hole, to detect an object at any distance in the range 1 cm to 35 cm.

A small amount of hysteresis is introduced into this switching distance to ensure clean switching thresholds and stability of the output signal. The use of tuned detector amplifiers provides excellent infra-red interference rejection.

Analogue Speed Control

The analogue speed control has

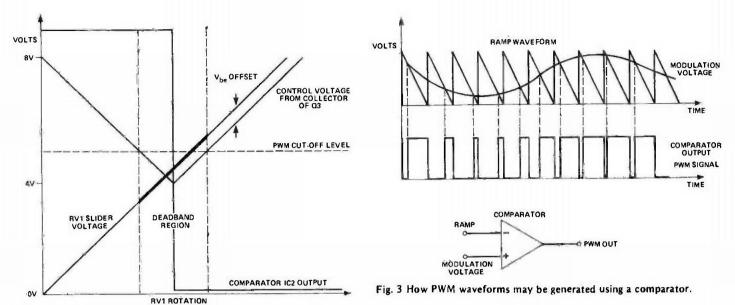


Fig. 1 Various voltages associated with the circuitry around Q3. The control voltage is measured at point A in Fig. 5.

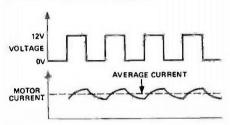


Fig. 2 PWM motor driving waveforms for last month's circuit.

been devised for manual control of the main traction motors; it provides two pulse width modulated signals suitable for the motor driver amplifier.

The circuit is designed to provide a linear control-voltage-to-pulse-width relationship for greater flexibility in application, and to simplify the addition of speed feedback velocity control.

The modulator can be built either single or dual, and the manual control section, if not required, is easily omitted. Speed control is achieved via two remote potentiometers, allowing speed to be set in either forward or reverse directions independently for each traction drive.

Since both motors are controlled via switching amplifiers from the same battery supply, it is important to reduce the peak currents that are drawn. This can be achieved by offsetting the phase of the switching waveforms relative to each other, such that at 50% duty cycle modulation, power

BUYLINES.

No problems here with any of the components specified — most mail order companies who advertise in the magazine will be able to supply everything. We can supply the PCB — see page 44 for details.



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The circuit for the dual analogue pulse width modulator is shown in Fig. 5; it will be seen that each channel is identical with the exception of the circuitry around the CMOS gates IC1 and IC4. As described earlier the two switching waveforms must be the same frequency and synchronized 180° out of phase, to distribute the motor current peaks more evenly through the cycle. This is achieved by synchronizing both pulse generators to a master clock based around IC1a and b. A 20 kHz square wave is generated by this conventional astable arrangement and its frequency, set by R1 and C1, is fairly independent of supply variations.

The output of IC1d at pin 6 provides a buffered square wave in the same phase as the output on pin 10 of IC1b. C2 and R3 differentiate the positive-going edge of the square wave to produce a very short logic low pulse at the output of Schmitt inverter gate IC1c. In similar fashion C9 and R16 produce a logic high pulse coinciding with the negative-going square wave edge. IC4b further inverts this signal to a logic low pulse. Two separate trains of 500 nS negative-going pulses are thus provided in the correct phase relationship for resetting the charging cycle of two sawtooth oscillators as described below.

The pulse width modulators are iden-

tical from here on and we shall refer to the topmost circuit for description. Voltage controlled pulse width modulation is, in principle, very simple; a ramp waveform (sawtooth) is applied to one input of a comparator and the modulation voltage to be encoded is applied to the other, producing the required PWM squarewave at the comparator output. Figure 3 illustrates this operation.

Due to the design requirement of a linear relationship between control voltage and pulse width, a constant current source formed from Q2 is used to generate the linear ramp waveform. LED1 and the baseemitter junction of Q2 are forward biased by R6 and together define a temperaturecompensated voltage across R7 which in turn defines a constant emitter and collector current of about 1 mA. C3 is charged up negatively from this current, until the negative-going reset pulse arrives from inverter IC1c. This pulse turns Q1 hard on for a very short period (500 nS), during which C3 is completely discharged, taking the ramp voltage back to +8 V. This process repeats at the clock frequency of 20 kHz, providing a negative-going sawtooth of about 3 V peak-to-peak referenced to the V rail.

IC3b, the comparator used to perform the modulation, is an LF353 dual op-amp,

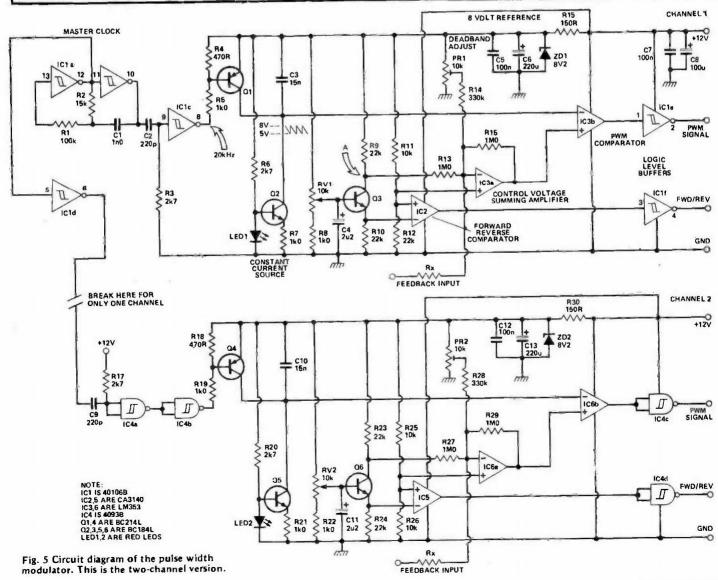
chosen for its large bandwidth and high slew-rate. The inverting terminal on pin 2 is fed from the ramp waveform, while the non-inverting terminal is fed from op-amp IC3a, an inverting amplifier configured to sum control voltage inputs relative to a 4 V reference.

The potential divider R11 and R12 provides the 4 V reference to the non-inverting terminal of IC3a, and the control voltage applied to R13 at point A is summed relative to the 4 V. An offset voltage set by PR1 is also summed at the inverting terminal of IC3a, and is used to bring the control voltage into the correct operating range and for setting a deadband region on the manual control pot RV1.

The output of op-amp 1C3b (and indeed most others) will not swing to the full supply rail voltages, so the inverter gate IC1e is used to buffer the square wave to

full CMOS logic levels.

The manual control system included in this circuit enables a single potentiometer to control the speed in both forward and reverse directions. When the pot is at centre travel, and for a certain deadband around this point, the motor must be stopped and no switching pulses should occur (ie the PWM signal is continuously low). As the pot is turned in either direction from its midpoint, the pulse width should in-



crease and this requires a positive-going input voltage to the summing amplifier IC3a. The forward/reverse logic level should also change state as the pot moves through its midpoint. Q3 provides the necessary voltage transfer function from the pot RV1 to the control voltage summing amplifier, as explained graphically in Fig. 1.

The emitter and collector resistors of Q3 are both equal and the base voltage is taken directly from the slider of the manual control pot RV1. The output voltage is taken from the collector of Q3 to feed the summing amplifier, and will be held at +8 V via R9 when Q3 is switched off. As the slider of RV1 moves toward the centre of travel, the base voltage rises, slowly turning on Q3 and lowering the collector voltage.

When Q3 is turned hard on as RV1 reaches its mid-point, R9 and 10 will form a potential divider giving 4 V as the minimum control voltage. Further increase of base voltage can now only increase the emitter and collector voltages back up to the positive rail, reaching a maximum at one V_{be} drop from the +8 V rail.

During the above process the voltage on the emitter of Q3 rises from zero to the same maximum voltage, and is fed to the inverting terminal of IC2, a CA3140 used as a comparator. The other comparator input receives 4 V derived from the potential divider R11 and R12. This provides the required forward/reverse signal that corresponds to each half of the control pot. tnverter gate IC1f buffers the output of IC2.

C7 and C8 provide supply decoupling for both channels, while C5 and C6 provide further smoothing for the 8 V zener regulator formed by R16 and ZD1. This 8 V reference rail is used for two reasons; firstly to allow for fluctuation in the 12 V battery power supply that would otherwise affect the output pulse width, and secondly to ensure that the op-amp supply voltage is well above the maximum input voltage.

The resistor marked as Rx in the circuit shows where a speed feedback voltage will be added to the controller to close the velocity control loop. An infra-red tachometer module to directly sense the traction speed will be described later in the

If the manual control input is not required, the components associated with this can be simply omitted (ie RV1, R8, R9, R10, C4, Q3, IC2 and their equivalents in the other channel). Control voltages may now be fed to the unconnected end of R13, where a variation of 3 V, set by PR1 to be anywhere in the range 0 V to 8 V, will provide 100% control of the output pulse width. Forward/reverse switching must also be applied to the input of IC1f on pin 3.

Construction and setting up with interconnection details for the motor driver will be described next month.

PARTS LIST.

Resistors (all 14W, 5%) 100k 15k R3,6,17,20 2k7 R4,18 470R R5,7,8,19, 21,22 1k0 R9,10,23,24 22k R11,12,25,26 10k 1M0 R13,15,27,29 R14,28 330k R16,29 150R

Potentiometers

10k linear RV1,2 PR1,2 10k linear miniature horizontal preset

Capacitors

1n0 ceramic C2,9 220p ceramic 15n polycarbonate 2u2 35 V tantalum C3, 10 C4, 11 C5, 7, 12 100n ceramic

C6, 13 C8 220u 16 V axial electrolytic 100u 25 V axial electrolytic

Semiconductors

40106B IC1 IC 2, 5 CA3140 IC3,6 LF353 IC4 4093B Q1,4 BC214L Q2,3,5,6 LED1,2 RC1841 red LED

8V2 400 mW zener diode **ZD1.2**

Miscellanous PCB (see Buylines)

will be switched alternately to each motor. This spreads the current peaks more evenly over the switching cycle.



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SUPERIOR QUALITY CARBON					, -0.	100.		- Z JL	and the same of		
FILM RESISTORS, HI STAB LOW NOISE X W 19Ω-1ΜΩ 5% E24	per Clad Glass PCB × 3 75 72p Single Sided	2N2848 60p 21 2N2875 2.20 21	N3977A 36p N3900 26p	2N5194 1,34 2N5209 24p 2N5210 25p	40608 2.44 40622 1.45 40625 60p	BC178 22p	BC415 3	6p BOX14 6p BDX18 0p BDX32	1.30 BSX19 1.59 BSX20 3.47 BSX21	26p MPSL01 26p MPSL51 48p MPSU01	42p 48p
75 W 1032-10M 2 5% E24 3p 2.5 1 1W 1032-10M 2 5% E12 6p 3.75	# 3.75 80p 420 × 195mm	2N2891 2,28 21 2N2892 3.00 21	N3902 6,65 N3903 15p	2N5219 25p 2N5220 15p 2N5221 25p 2N5222 28p	40626 3.20 40631 1.90 40632 2.12	BC178A 24p BC178B 25p BC179 23p	BC418 3	2pl BDY17	2.00 BSX26 2.50 BSX27 2.89 BSX28	80p MPSU04 78p MPSU05 86p MPSU05	84p 1.32 65p
METAL OXIDE/FILM 3.75 RESISTORS 4.78	× 17 2.50 130p × 17 3.30 420 × 245mm × 17 4.20 195p	2N2905 28p 21 2N2905A 29p 21	N3905 15p N3906 15p	2N5223 15p 2N5224 38p	40635 1.35 40637 2.90 40643 1.80	8C179C 27p	BC441 3 BC460 3 BC461 3	3p BDY23 2p BDY25 3p BDY38	3.75 BSX29 3.75 BSX39 1.74 BSX60	80p MPSU07 MPSU51 75p MSON 166	56p 75p 88p 64p
stability. Extremely low noise Trac 0.4W 1052-1MΩ 2% E24 Sp One	Soard 1.58 Ferric Chlorida k Cutter 1.15 60% Solution Insertor 1.59 Bottle £1.50	2N2906A 30p 21 2N2907 25p 21	N3962 30p N3964 1.42	2N5225 25p 2N5226 25p 2N5227 25p	40673 95p 40622 1.80 40671 1.00	BC182 11p BC182A 12p BC1828 13p	BC479 34 BC516 44	9p 80Y54 0p 8YD55 0p 8DY56	1.98 BSX61 2.09 BSX76 2.35 BSX77	50p MPSU56 MPSU57	1.20
13/10 CHARLES 14 9p 100 8	Pins .50 bloc 3.78 Sitem Collet	2N2920 2.94 2 N2920 15p 21	N4031 55p N4032 55p	2N5232 30p 2N5232A 32p 2N5245 37p 2N5246 40p	40872 1.00 AC125 35p AC126 25p AC127 25p	BC182L 12p BC182LA 13p BC182LB 14p	8C547 13	0p 80Y57 3p 80Y58 4p 80Y60	5.26 BSY24 8.15 BSY25 2.80 BSY26	1.00 MFR450A MRF453	39.95 24.10 27.65
0.2212 8 212 E12 T1p Pen Spen	+ Spool 3.06 on professional s Spool 72p studio equipment	2N2925 15p 2 2N2926 10p 2i	N4037 43p N4058 10p	2N5247 45p 2N5248 46p	AC128 25p AC132 39p	BC183A 11p BC183A 11p BC183B 12p	BC5478 12 BC548A 12	2p BDY82 3p BDY92	2.30 BSY29 2.34 BSY39 3.76 BSY54	70p MRF475 47p MRF477 40p MRF477	40 80 7.55 21.95
2 3W 6 2211 - 33031 E12 28p 100	Standard spindles VACI Axial Please specify	2N3011 25p 21 2N3019 50p 21	N4060 12p N4061 10p	2N5249 48p 2N5266 2.88 2N5293 98p 2N5294 1.28	AC151 51p AC152 45p AC153 55p AC153K 64p	BC183C 13p BC183L 12p BC183LA 13o	BC549 13	96 BF119 36 BF121	38p BSY65 1.00 BSY95A 75p BU104	25p MRF604 3.0 NKT124	12.32 7.29 63p
LOW NOISE Mini Vert 14p 10n5	2 2nF 23p gray or black F, S 2nF 26p 15mm	2N3054 56p 21 21N3055CSF 60p 21	N4064 1,50 N4069 1,80	2N5298 1.37 2N5298 1.28	AC176 27p AC175K 37p	BC183LC 14p BC183LC 14p BC184 11p	BC549C 15		70p BU105 80p BU109 39p BU126	1.70 NKT126 3.00 NKT126 1.66 NKT128	49p 47p 42p
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470nF 560nF27p 22nF, 33nF, 470nF 680nF 12p 47nF, 68nF, 470nF	58p 3 16V £1,05	2N3567 55p 2N 2N3568 50p 2N	V4402 38p 2 V4403 30p 2	N8121 54p N6122 56p	8C108C 14p BC109 13p BC109B 14p BC109C 15o	BC250 18p BC250 22p BC250A 23p	80116 2.5 80121 2.2 80124 1.5	BF256B BF256C BF257	43p ME4104 45p ME6001 30c ME6002	25p NKT16229 25p NKT20329	64p 59p 38p
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SILVER MICA CAPS 1% 600V Cerrent costed Extremely stable Content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes may be seen as the content of the good makes as t	Chrome Bezel ris 75p	2N3607 28p 7N 2N3632 9.88 2N	14901 3.62 21 14902 3.62 21	N6132 83p N6133 1.14 N6134 1.36	8C118 25p 8C119 38p 8C121 82p	BC252B 23p BC252C 24p BC253 22p	BD140 446 BD142 2.46 BD153 1.28	BF274 BF324		56p OC41 58p OC43 2.3 OC44 2.40 OC76	80p 70p 82p
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120pF 220pF 25p 47 83 8p 191711 250uF 470pF 30p 47 100 9p Low	Radial Variety in UK. If you den't Voltage tee what you want please	2N3642 25p 2N 2N3643 15p 2N 2N3644 28p 2N	4907 3.20 21 4908 3.70 21	N6290 1,10	BC134 36p BC135 45p BC136 45p BC137 39p	BC256A 25p BC256A 27p BC257 25p	BD160 3.80 BD181 1.76 BD182 2.50	BF363 BF450	35p M.#802	2.79 OC82D 3.54 OC83 4.46 P346A	50p 70p 75p 58p
TANTALUM 1 100 8p 10 BEADS 1 500 400 27	V phone or write 16 5p as this is not 10 5p 8 last list	2N3645 336 2N 2N3646 29p 2N 2N3682 15p 2N	14901 1.95 3/ 14913 2.59 3/ 14914 2.69 3/	N128 1.99 N138 3.50	BC137 38p BC138 55p BC140 33p BC141 37p	8C257A 27p BC258 24p BC258A 25p BC258B 26p	BD183 2.70 BD187 1.09 BD201 1.30	BF457 BF458	35p MJ900 45p MJ901 MJ1000	3.10 A20108	2:14 1.88 27p
.1/35V 17p 2.2 25 8p 22 .22/35V 17p 2.2 63 8p 47 .33/35V 17p 2.2 100 11p 47	16 7p 2N404 1,50 10 7p 2N914 20p 16 8p 2N916 39p	2N3691 18p 2N 2N3692 20p 2N	4915 2.95 3 4918 48p 3 4917 47p 3	N140 2.37 N143 2.85	BC142 33p 8C143 34p 8C147 11p	8C259 25p 8C2598 26p 8C259C 27p	BD202 1.35 BD204 1.44 BD220 1.00 BD221 966	BFR39 BFR40	52p MJ1001 25p MJ1800 25p MJ2500 25p MJ2501	3.60 SC108	27p 27p 35p 69p
.47/35V 17p 22 350 30p 100 .88/35V 17p 3.3 25 30p 100 1.0/35V 17p 3.3 40 11p 20 2 2/16V 17p 3.3 40 11p 20	70 9p 2N917 55p 16 10p 2N918 33p 10 11p 2N929 35p	2N3694 300 2N 2N3702 10p 2N	4919 1.28 31 4920 1.34 31	N154 2,56 N200 6,93	BC147A 12p BC147B 13p BC147C 18p	BC280 30p BC260B 32p BC280C 33p	BD223 1,00 BD224 95p BD232 1,11	BFR80	25p MJ2985	1.00 T P30A 3.30 T P30C	69p 46p 68p 44p
2.2/35V 22p 4.7 16 8p 470 3.3/35V 22p 4.7 25 8p 470	16 12p 2N929A 45p 10 17p 2N930 20p 16 18p 2N930A 30p	2N3704 90p 2N- 2N3706 10p 2N-	4922 1.29 40 4923 1.34 40	0250 2.42 0251 2.77	8C148 11p BC148A 12p BC148B 13p	BC261 33p BC261A 34p BC261B 35p	8D233 70; 8D234 72; 8D235 720	BFS21A 4	50 M.02701 .96 MF4502 00 M.9F340		44p 52p 44p
4.7/35V 24p 4.7 63 12p 1000 6.8/25V 25p 4.7 100 14p 2200 6.8/35V 25p 10 25 250	10 20p 2N1731 25p 16 24p 2N1132 25p 10 34p 2N1302 65p	2N3707 10p 2N4 2N3708 10p 2N4 2N3709 10p 2N4	4926 95p 40 4927 95p 40	0264 2.63	8C148C 13p 8C149 11p 8C149B 12p	BC261C 36p BC262 31p BC262A 32p	BD236 76p BD239A 67p BD239C 64p	BFT19 1	.10 MJE375 .65 MJE371 RB MJE371		52p 44p 58p 1.80 1.68
10/16V 25P 10 40 12P	/Speaker 2N1308 75p	2N3710 10p 2N4 2N3711 10p 2N4 2N3712 2.00 2N4	4964 27p 40 4966 25p 40 4966 25p 47	0311 97p	BC153 23p	BC262B33p BC262C 34p BC263 30p BC263B 31p	BD240A 59p BD240C 73p BD241A 61p BD241C 57p	BFY66 2 BFW10 1	.48 M	710 -1941A 3 65 TIP41C 3 65 TIP42A	64p 78p
22/6.3V 26p 22 63 18p Twin 2	amp 14p 2N1370 58p 7 amp16p 2N1420 56p 7 amp16p 2N1483 2 96	2N3713 2.86 2N4 2N3714 2.98 2N4 2N3715 3.31 2N4	4967 25p 40 4968 25p 40 4969 31p	0313 T.891	6C157 11p	BC263C 32p BC264 40p	BD241C 67p BD242A 65p BD242C 70p BD243A 72p	DESMAS 3		71P50	78p 69p 80p 1.20
32/16V 32p 22 100 21p 33/10V 38p 47 25 14p 3 Core 47/6 3V 43e 47 40 17e	18p 2N 1485 3.47	2N3724 750 TAIL	5011 9.37 40 5030 44p 40	0324 1.86 0325 2.46 0326 1.98	BC158 11p.	8C284B 42p 8C266 35p 8C266A 36p 8C266B 37p	BD243C 85p BD244A 82p BD244C 1.00	8FW90 1 9FX12 1 8FX13	00	1.00 - 1954	2.30 2.60 74p 90p
Feedthrough 68 25 Mg	86p 2N1702 3,20 2N1711 35p 2N1889 50p	2N3732 2.88 2NE 2'N3734 1.30 2NE	5036 1.60 40 5038 1.95 40	0347 1.40 0348 1.95	BC159 11p BC159A 12p	BC300 45p BC301 44p	BD245A 1.74 BD245C 1.30 BD246A 1.20	BFX19 BFX20 BFX29	00e 177 C. 00p 179 C. 00e 170 C. 00e 170 C. 00e 17	1.40 TIP112 1.16 TIP115 59 TIP117	90p 81p 95p 86p
1000pF 500V /p 100 16 14p 8 Core	33p 2N1890 50p 38p 2N1893 30p 46p 2N1974 1 50	2N3725 2.46 2N5 2N3738 2.90 2N6 2N3740 2.38 2N5 2N3741 2.75 2N5	6086 36p 40 6087 39p 40	0361 50p 0362 50p	BC160 42p	BC303 47p BC304 46p BC307 13p	BD249A 2.00 BD249C 2.31	BFX30 BFX34 1 BFX37	50e	116 TP115 TS9 TIP117 45p TSP120 TSP123 40p TSP123	88p 1.00 1.20
MINI FILM MULLARD 100 63 25p TRIMMERS 100 100 30p Screen	ZNZIUZ 350	2N3766 2.90 2N5 2N3767 3.19 2N5 2N3731 1.75 2N5	5126 48p 1 40	0364 2.90 0372 1.80	BC167 12p BC187A 13p BC1676 13p BC168 12p	BC307B 16p BC307B 12p	BD250A 2 11 BD250C 2.48 BD433 79p BD434 79p	BFX68	DE WEFFE		1.00 1.20 1.27 7.50 1.60
14-5-59F (800MHz) 23p 220 16 17p Storeo 2-10pF (800MHz) 27p 220 25 22p Mint 5 220 25 25 Mint 5			5126 38p 40 5129 30p 40 5130 37p 40	0374 2.84 0389 1.24	BC1688 13p	BC308A 13p BC308B 14p BC309 14p	BD435 81p BD436 81p	BFX87	10e 1/253640	27g T!P135 40c T!P137 50c T!P140	1.60 1.80 1.95
2-22pF (400MHz) 29p 220 63 30p 4 Core 5-5-65pF 330 16 19p 4 Core	20,2217 38p 20,2218 33p 20,2218 33p 20,2218 33p 20,2218 33p 20,2219 20,2219 20,2219 20,2220 20,2221 20,2220 20,2221 20,2220 20,2221 20,2220 20,2221 20,2	2N3790 2.73 2N5 2N3791 2.47 2N5	5131 22p 40	0392 1,20 0394 1 10 0406 1,39		BC309 14p BC309A 15p BC309B 16p BC309C 17p BC317 16p	BD437 88p BD438 88p BD439 90p BD440 91p	BFY18 1	3a 7 56: 7 .06 7 56: 8 .15 MP56:30	67p 71P142 47p T1P145 37p 71P147 32p T1P2955	1.80 1.95 2.25 2.16 2.48 77p
630VOC 250VAC 470 16 270 17 Core		2N379 210 2N5	5136 38p 40 5137 23p 40 5138 30p 40		BC170B 17p BC170C 18p	BC318 15p BC320 25p	BD441 91p BD442 93p BD529 1,20	EREVIO 1	20 MP\$6562	200 E (153/	92P
POLYESTER 470 25 280 CAPS 470 40 33P Asri 15nF 18p 470 100 600 500 500 R	2N2223A 4.15 2N2303 1.10 inl Cable 1.N2368 30p G58A 36p 2N2369 19p HF 36p 2N2369A 20p	2N382) 1.84 2N5	5139 48p 40 5140 25p 40	0410 1.80 1 0411 3.00 1	BC171 12p BC171A 15p BC171B 15p	BC327 14p BC328 14p BC337 15p	BD535 75p BD536 75p	BFY51	10 MPS6562 20 MPS6562 00 MPS616 MPS616 MPS616 50 MPS613 50 MPS613 MPS614 50 MPS616	22p 11545 28p 11546 28p 11547	40p 66p 86p 49p
18nF 18p 470 100 60p 5032 R 22nF 18p 1000 16 30p 75Ω U 47nF 32p 1000 25 38p 75Ω V	71 ZNo W 20€2405 88a M	2N3826 78p 2N6	5175 58n ac	0422 2.85 0467A 1.72 0513 1.75	BC172A 15p	BC347 20p BC350 20p	BD538 80p BD538 80p BD539 80p	BFY53 BFY56 BFY56A	15p MPSA12 16p MPSA16 55p MPSA18 MPSA20 16p MPSA43	46p 11548 30p 11549 65p 11550	66p 60p
160nF 37p 1000 40 46p 30032 2 220nF 40p 2200 16 40o Re	2N2411 3.60	2N3854 44p 2N5 2N3855 30p 2N6	5183 1 OD 40	0594 1.156	BC172C 16p BC173 15p BC173B 16p	BC382L 30p BC382L 30p BC383 30p	BD540 1.10 BD540 85p BD540C 1.20	II BEY77 8	MPSA43 MPSA55 MPSA56 MPSA56	60p TIS51 50p TIS52 28p TIS53	65p 70p 97p
Fully enclosed 2200 63 1340 10 Way	anded 2N2483 25p 2N2484 26p 1665 2N2484 26p	2N3856 46p 2N8 2N3858 31p 2N8	5189 1.15 40 5189 1 00 40	0600 2.58 1 0601 2.36 1 0602 1.68	BC173C 16p BC174 21p BC174A 24p BC174B 24p BC174B 24p BC175 75p	BC383L 30p BC384 30p BC384L 30p	8D675 72p 8D676 77p 9D677 78p BD678 83p BD711 1 32	BFY80 S	MPSA55 MPSA56 MPSA65 MPSA66 MPSA66 MPSA70	30p TIS54 40p TIS55 47p TIS58	86p 66p 92p
F3 Suries 4700 18 75p 24 Way 109 Ω 18Ω 25 90p 45 Way		2M3858 31p 2N5 2N3859A 31p 2N5 2N3860 31p 2N6	5181 70p 40	0 6 03 2.06 I	BC175 75p	BC407 3Dp BC408 24p BC409 30p	BD578 B3p BD711 1.32 BD712 1.32	BSW41 5 BSW67 1 BSW70 1	MPSA70 MPSA92 00 MPSA93	450 T1560 66p T1562 66p T1564	42p 44p 67p

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TIS91 30p TIS92 30p TIS93 640	1N1204A 1,00 1N1206 1,20 1N3063 36o	PW06 (600) 90p 25 amp type	VA109B 40p VA109B 40p VA1100 40p	LM305H 88p LM307H 1.05 LM307N 58p	NE531N 1.50 NE543N 2.50 NE544N 1.80	TDA2571 4 TDA2581 3	.10 74185 1.2 .40 74186 4.9 .75 74188 3.3	74LS373 79p 74LS378 75p	74C918 2.50 74C920D 8.50	4534 E.00 4536 3.10	6875 6.30 8131 3,78 8154 9.59	HEATSINKS CLIP-ON
VN10KM 60p VN48AF 84p VN66AF 85p	1N3085 48p 1N3492 1.86 1N3493 2.20	Metal clad with hole K01 (100) 2.20	VA1103 40p VA1104 90p VA1108 40p	LM308AH 3.15 LM308AN 2.14 LM308H 96p	NE555 20p NE556 67p NE558 1.43	TDA2591 4. TDA2600 6	.70 74190 72 .73 74191 72 .15 74192 72	p 74LS390 70p 74LS393 60p	74C922 4.50 74C923 6.00 74C925 6.00 74C926 6.58	4538 1,20 4539 1,20 4543 1,10 4553 2,90	8155 8.00 8212 1.80	TO1 (AC128) 18p TO5 (BFY51) 18p TO18 (BC109)
ZTX107 10p ZTX108 10p ZTX109 10p	1N3493R 2.20 1N3602 36p 1N3604 45p	K02 (200) 2.30 K04 (400) 2.80 K06 (600) 3.40	VA110940p VA1110 40p VA1181 40p	LM308N 88p LM309K 2.80 LM310H 1.96	NE560 4.99 NE562 5.13 NE565 1.25	TDA2640 3. TDA3000 2.	.50 74193 72 .64 74194 72 .76 74195 63	p 74LS396 1.99 p 74LS398 2.80	74C928 6.00 74C929 6.20	4555 80p 4556 60p 4560 2.00	8223 1.80 8224 2.60 8226 2.50	18p TQ220 (TIP29) 38p
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ZTX314 24p ZTX320 35p ZTX330 35p	1N4007 10p 1N4009 20p 1N4148 8p	400 500mW E24 Series 2 4-47V 10p	RESISTORS (VDRs) E298ZZ05 35p	LM320 — See 79XX Series Volt, Requistors	SAS560 1.65 SAS570 1.6S SAS580 2.20	XR2206 3. ZN414 1.	.00 74LS04 14	74LS869 2.10	4009 37p 4010 39p 4011 15p	6502 4.65 6900 3.95 6802 4.90	8259 8.00 8279 8.95 8304 4.50	charges HP2 (1,2ÅH)2,25 HP2 (4AH) 4,99
ZTX341 28p ZTX500 14p ZTX501 14p	1N4150 18p 1N4448 22p 1N4517 22p	1.3 Wait E24 Series	E298ZZ06 35p E299DDP116 40p E299DDP116 40p	LM324N 50p LM337K 4.76 LM337MP 1.66	SAS590 2.20 SFF96364 8.28 SL610C 4.00	ZN1034 2. ZN1040 7.	.00 74LS10 15	0	4012 18p 4013 30p 4014 58p	6809 10.96 8035 7.44 8060 10.90		HP1 (1,2AH) 1,10 HP11 (1,2AH) 4,20
ZTX502 14p ZTX503 17p ZTX504 24p ZTX510 34p	1N5172 30p 1N5176 94p 1N5400 12p	2.5 Watt	E299DDP120 46p E299DPP216 40p E299DDP218 40p	LM337T 1.99 LM339AN 1.60 LM339N 51p	SL611C 4.00 SL612C 4.00 SL620C 6.00	ZTK33 8	39p 74LS12 15 39p 74LS13 15 74LS14 48 74LS15 16	p 74S02 80p	4015 60p 4016 27p 4017 48p	8080A 3.75 8085A 5.60 8900 57.75	8832 2,60 8833 2,35 9097 3.00	Chargers TYPE H. Adjustable to 6
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Small Signal 2N5080 30p 2N5081 32p	1N5626 6Zp 1N5627 68p 1S44 10p	33V, 51V, 62V. 58V 1.25	E296EDA262 40p E296EDA262 40p E296EDA265 40p	LM376N 66p LM377N 1.56 LM378N 3.40 LM379S 6.80	AN76013N 1,95 SN76023N = SN76033N SN76033N 2,95	7410 1 7411 2	5p 74LS40 25 21p 74LS42 39	74S112 90p 74S113 1.00	4028 60p 4029 75p 4030 38p	2114 1,17 2532 4,69 2708 3.00 2716 (5V) 2.50	ZN428E8 6.25	Please anguire about types not listed
2N6062 350 2N6063 37p 2N6084 40p	15131 40p 15134 68p 15421 1.00	10W Pos. Stud Following voltages only	E298ED A268 40p E299DDP336 40p E299DDP338 40p	LM380N14 75p LM380N8 75p LM381AN 2.26	SN76110 2.25 SN76115 2.65 SN76116 2.75	7413 2	21p 74LS47 40 25p 74LS51 16 33p 74LS64 22	p 74\$132 1.80 p 74\$133 1.00	4031 1.96 4032 1.40 4033 1.90	4027 3.00 4044 7.00 4060 9.50	REGULATORS ISee elso Linear ICsi	32.768KHz 3.00 100KHz 3.00 200KHz 3.60
BR101 75p BRY39 46p BRY55 100 66p BRY55-300 67p	1S421R 1.00 1S940 10p 1S941 11p	7V6, 13, 18, 20, 24, 27, 30, 33, 68, 82, 91, 100,	E299DDP340 40p E299DDP342 40p E299DDP344 40p	LM381N 1.40 LM382N 1.25 LM383T 3.40	SN76226 - 3.45 SN76228 2.90 SN76477 1.70	7417 2 7420 1 7421 2	74LS54 22 25p 74LS55 18 22p 74LS73 28 15p 74LS73 20 12p 74LS74 20	74\$139 2.35 74\$140 2.50	4034 1.61 4035 78p 4036 3.00	4116 (200ns) 96p 4118-3 5.00 4164 8.40	- Positive 100mA 78L05A 30p	1.00MHz 3.28 1.008MHz 3.50 2.00MHz 2.60
BRY56 BOP TIC44 35p TIC47 BOP	15961 22p AA118 28p	20W Poe. Stud	E299DD P346 40p E299DD P348 40p E299DD P350 40p	LM384N 1.40 LM386N1 88p LM386N4 1.20	SN76550 80p SN76666 2 90	7422 2 7423 2 7425 2	20p 74LS75 30 74LS76 30 25p 74LS78 30 25p 74LS80 1.2	p 74S157 2.76	4037 1.30 4038 1.22 4040 54p	5204 7,50 6116 6,60 6514 3,30	78L12A 30p 78L15A 30p 78L24A 30p	2.097152MHz 3.50 3.2768MHz 3.00
4, 6 & 12 Amps Tours to 220	AA129 57p AA144 25p AAY30 44p AAY33 46p	(BZY93 series) E24 values 7V5-75V 2.00	E299DDP352 40p E299DPP354 40p LINEAR IC4	LM388N 1.32 LM391N60 1.70 LM391N80 1.93	SO41P 1.60 SO42P 1.60 TA7120 2.20	7426 3 7427 2 7428 2	74LS83 50 74LS85 80 74LS85 24	745188 3.50	4041 69p 4042 60p 4043 61p	6810 1,99 7489 2.86 74189 4.00	100mA To5 78L05CH 80p 78L12CH 80p	4,00MHz 3.00 4,194394MHz 3.00 4,433619MHz
Suffix: A = 100V 8 = 200V, C = 300V	AAZ17 27p BA100 22p BA102 25p BA115 25p BA133 40p	OPTO ELECTRONICS 2N5777 180	AN103 2.20 AY1-0212 6.60 AY1-1313 6.90	LM392N 76p LM393N 96p LM394H 3.80	TA7204 2.76 TA7205 2.20 TA7222 2.30	7430 1 7432 3	IBP 74LS90 35 30p 74LS92 38 30p 74LS93 35 26p 74LS95 1.0	p 745194 3.50 p 745200 4.76	4844 70p 4845 1,20 4846 88p	74LS289 4.00 ,4S188 3.50 74S287 3.30	78L15CH 80p 78L24CH 80p 500mA T0202	1.45 5.00MHz 3.50 6.00MHz 2.75
D = 400V M = 600V	BA115 25p BA133 40p BA138 30p	2N5777 78p 2N5778 88p 2N5779 1.00 4N25 1.10	AY1-1320 3.20 AY1-5050 1.40 AY1-1270 8.70	LM396K 13.52 LM709N8 64p LM709CH 1.00	TAA263 1,50 TAA300 3.95	7438 2 7440 1	74LS96 1.0	0 745225 5.60 0 745261 3.00	4047 68p 4048 50p 4049 29p	74S288 2.50 2ERO	7805M 47p 7812M 47p 7815M 47p	6.9375MHz 3.50 8.00MHz 2.75 10.00MHz 2.75
TIC108A 48p TIC108B 47p 4A TIC108C 48p	BA138 30p BA142 20p BA144 15p BA155 15p	BP100 1.40 BP104 1.00 BPX25 4.74	AY3 8910 7.20 AY3 8912 6.80	LM710CH 89p LM710CN 52p LM711CH 1.38	TAA320 2.05 TAA350 3.60 TAA521 1.50	7442 3 7443 8	38p 74LS109 28 38p 74LS112 33 30p 74LS113 31	745287 3.71 745288 3.71	4060 29p 4051 56p 4062 88p	INSERTION DIL SOCKETS (24 pin 6 26	7824M 47p 1 Amp T0220 7805T 50p 7812T 50p	18.00MHz 2,75 20.00MHz 3.25 27.648MHz 2.60
TIC 106D 59p TIC 106M 68p	BA155 15p BA156- 38p BA182- 40p BA201 18p BA202, 25p	BPA40 8,76	CA3000 4.90 CA3001 4.95	LM711CN 80p LM723CH 1.21 LM723CN 40p LM725CH 3,40	TAA522 2.47 TAA550 73p TAA560 2.35	7445 6 7446 - 6	80p 74LS114 31 80p 74LS122 41 55p 74LS123 50	p 745301 3,99 p 745470 5.75	4063 58p 4064 1,20 4056 1,18	-40 pin 11.37	7815T 60p • 7824T 50p • 1,5 Amp T03	48 00MHz 3.00 100 00MHz 6,50 5.5 MHs
TIC116A 84p TIC116B 80p 8A TIC116C 71p TIC116D 73p	BA316 25p BA317 25p	BPX61 3.48 BPX63 2.93	CA3005 3.16 CA3007 4.92 CA3010 1.30	LM725CN 3,30 LM733CN 77p LM741CH 96o	TAA570 2.35 TAA621AX1 2.75 TAA661A 1.60	7448 4 7450 1	10p 74LS124 1,2 14p 74LS125 30 74LS126 31	0 74S473 12.50 p 74S474 4.26 p 74S475 13.10	4056 1,30 4059 5,50 4060 98p 4063 90p	including COMPUTER SUPPORT	7805K 1.40 7812K 1.40 7815K 1.40	Ceramic filter90p VALVES
TIC116M 80p	BAV10 16p	BPX86 4.15 CQX13 40p	CA3012 1.76 CA3013 4.12 CA3014 2.35	LM741CN 20p LM741CN14 80p LM747CN 70p	TAA661B 1.70 TAA700 2.66 TAA930 2.60 TAA930B 2.63	7453 1 7454 1	15p 74LS132 46 15p 74LS138 25 14p 74LS138 36	74S571 9,00 74S573 9.00	4086 34p 4087 3.80	ADC0800 22.50 ADC0816 14.90 ADC0817 10.06	7824K 1 40 Nagative	DY86/67/802 1.32 ECC82 1.22
TIC126B 72p 12A TIC126C 73p TIC126D 77p	BAV20 15p BAV49 15p BAX13 10p BAX16 11p	CQX33 48p	CA3015 2.62 CA3018 759 CA3018A 2.00	LM748CH 1.00 LM748CN 39p	TAA970 2.45 TAA991D 2.45 TAD100 2.00	7470 7472	74LS145 75	74H01 1.45	4068 17p 4069 18p 4070 19p 4071 19p	AY5-2376 12.00 ICM7555 30p INS1671 20.00	100m A T092 79L05 70p 79L12 70p	ECC83 1.22 ECC84 1.22 EF86 1.80
TIC128M 96p	BAY38 20p BAY44 16p BAY93 10p	LD3/A 12p LD52A 12p	CA3020 2.00 CA3020A 3.90 CA3021 3.20	LM1304N 2.50 LM1305N 3.10 LM1307N 2.75	TBA120AS 75p TBA331 1.50	7474 7475	23p 74LS151 35 38p 74LS153 60	74H05 1.66 74H10 1.46	4072 20p 4073 15p 4075 20p	INS1771 20.00 INS1791 34.00 MC1466L 8.50	79L15 70p 500mA T0202 7905M 55p	EL34 2.50 EL84 2.50 K T66 10.76
SIEMENS THRISTORS 1.2 emp plestic	B8103B 70p B8103G 70p B81048 80p	LD57A 16p LD52C 30p LD56C 30p	CA3022 3.12 CA3026 1.52 CA3028A 1.21 CVA30289 2.53	Flaire 900 400b	TBA395 1.65 BTA396 1.60 TBA450 1.96	7480 4 7481 1	08 74LS155 40	74H20 1.46 74H21 1.46	4078 60p 4077 49p 4078 23o	MC1488 75p MC1489 75p MC4024 3.25 MC4044 3.25	7912M 55p 7915M 55p 7924M 55p	KT88 12.50 PC900 1.76 PCC84 3.00 PEC85 3.40
Bet 80106 (100V) 80p Bet 80113 (200V) 70p	88104G 80p 88105 82p 88105A 87	LD80A 18p LD86A 22p	CA3029 1.44 CA3030A 2.97 CA3033 B.44	LM1496 1.08 LM1600 3.24 LM1801 3.47 LM1812 6.00	TBA460 1.61 TBA500 2.97 TBA5000 3.11	7483 7484 7485	741 S161 44	P 74H40 1.65 P 74H61 1.76 P 74H53 1.65 P 74H54 1.46	4081 20p 4082 20p 4085 66p	MK50250 10.00 MK50398 6.25	1 Amp T0220 7906T 60p 7912T 60p 7915T 60p	PCC89 1.89 PCF86 2.30 PCF201 3.00
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4.7 emp plastic Bat 80206 (100V) 80p Bat 80213 (200V)	8Y127 22p 8Y134 52p 8Y182 1.26 8Y188A 65p	LD466 1.45 LD468 1.66 LD471 27p	CA3041 3.47 CA3042 3.47 CA3043 3.92	LM1830 2.76 LM1845 4.12 LM1848 2.89	TBA5200 2.75 TBA630 2.65 TBA5300 2.74 TBA540 2.72	7492 7493	74L5164 49 74L5165 1.1 30p 74L5168 2.3 30p 74L5169 2.4	74H62 1.75 56 PM TTL 30100 100	4095 90 p 4096 90 p	MM57160 9.00 MM57161 9.00	7912K 2.20 7915K 2.69 7924K 2.69	PCL85 2 20 PCL86 2 10 PCL805 2 20
9,10 Bat B0246 (700V) 2,00	BY206 36p BY207 36p BY223 1.56 BY297 48p	LD476 1.20 LD478 1.45 LD479 1.56	CA3046 69g CA3047 4.10 CA3048 2.90	LM1872 4.75	TBA540Q 2.85	7495 7496		12 301.08 6.00 10 301.14 5.20 10 301.24 5.20 20 301.70 1.30 20 301.70 1.30	4097 3.20 4098 87p 4099 90p For higher	RO2513LC 7.50	Variable L200 (2A Pos)	PFL200 2.99 PL504 2.11
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97119 1.70 87120 1.50 87121 1.30	8YW12-200 1.40 8YW12-400 2.00 8YX10 36p 8YX50-200R 2.00	RPY63 2.86	CA3060 4.05 CA3062 13.84 CA3065E 4.62	LM3301 1,60 LM3302 960	TBA700 2.34 TBA7000 2.43	74116	40p 74LS193 50 96p 74LS194 41 75p 74LS195 50 98p 74LS196 55 70p 74LS197 66	5p 74C00 27p 5c 74C04 29p 74C14 89p 5p 74C20 28p 5p 74C20 28p 5p 74C20 36p 74C30 36p 74C48 140	45 CMOS 4502 B0p 4503 50p	SAA5050 8 50 SAA5052 8.50 TMS6011 4.25	LM337MP 1.73	PLUGS & SOCKETS UHF PL259 lypes
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	03 0.50	40085 0.99 I		74160N 0.55	74LSN			0.50	74C14	0.55	8216 1.95
4009 0.25 450			7470N 0.28	74161N 0.55	•	74L S125N 0.24	74LS260N		74C20	0.20	8224 3.50
4010 0.30 450		40098 0.54	7472N 0.27	74162N 0 55	74LS00N 0.10	74LS126N 0.24	74LS266N	0.22			
4011AE 0.24 450		40106 0.69	7473N 0.28	74163N 0.55	74LS01N 0.10	74LS132N 0.42	74LS273N	0.70	74C30	0.20	
4011 0.11 450		40160 1.05	7474N 0.28	74164N 0.55	74L S02N 0.11	74LS133N 0.24	74LS275N	3.20	74C32	0.20	8255 5.40
		40161 1.05	0.20	74165N 0.55	74LS03N 0.11	74LS136N 0.20	74LS279N	0.35	74C42	0.80	
			0.00		74LS04N 0.14	74LS138N 0.30	74LS280N	2.50	74C48	1.03	6800/6809
4015 0.50 451		40162 1.05	7476N 0.30	74166N 0.70			74L S283N	0.42	74C73	0.50	
4016 0.22 451		40163 1.05	7480N 0.26	74167N 1.25		74LS139N 0.30 74LS145N 1.20 74LS151N 0.30	74L 5290N	0.50	74C74	0.50	6800P [2.90]
4017 040 451		40174 1.05	7481N 0.20	74170N 1.25	74LS08N 0.12	74LS151N 0.30	74L5290N		74076	0.48	68A00 4.25
4019 0.38 451	14 1.25	40175 1.05	7482N 0,75	74173N 1.10	74LS09N 0 12	74LS15IN 0.30	74L 5293N	0.40	74083	0.98	68B00 4.65
4020 0.55 451		40192 1.08	7485N 0.75	74174N 0.75	74LS10N 0.12	74LS153N 0.27	74LS295N	1.50			6802 3.50
4021 0.55 451		40193 1.08	7486N 0.24	74175N 0.75	74LS11N 0.12 74LS12N 0.12	74LS154N 0.88	74LS298N	0.76	74C85	0.98	6809 (8.75
4022 0.55 451		40194 1.08	7489N 1.05	74176N 0.75	74LS12N 0.12	74LS155N 0.35	74LS365N	0.32	74C86	0 26	6810 1.25
			7490N 0.30	74177N 0.75	74LS13N 0.20	74LS156N 0.37	74LS366N	0.34	74C89	2.68	
	. 0.00		7491N 0.55	74178N 0.90	74LS14N 0.30	74LS157N 0.30	74LS367N	0.32	74C90	0.80	68A10 1.85
4024 0.33 452		TTL N			74LS15N 0.12	74LS158N 0.30	74LS368N	0.35	74C93	0.80	68910 2.04
4025 0.15 452			7492N 0.35	74179N 1.35			74LS373N	0.70	74C95	0.94	6820 1.95
4026 1.05 452		7400N 0.10	7493N 0.35	74180N 0.75	74LS20N 0.12	74LS160N 0.37 74LS161N 0.37	74LS373N	0.70	74C107	0.48	6821 1.25
4027 0.26 452	28 0.85	74C1N 0.10	7494N 0,70	74181N 1.22	74LS21N 0.12				74C 151	1.52	68A21 2.10
4028 0.50 452		7402N 0.20	7495N 0.60	74182N 0.70	74LS22N U.12	74LS'62N 0.37	74LS375N	0 40		1.32	68821 2.25
4029 0.55 453		7403N 0.11	7496N 0.45	74184N 1.20	74LS26N 0.14	74LS163N 0.37	74LS377N	0.85	74C 154	2.26	6840 4.25
4030 0.35 453		7404N 0.12	7497N 1.40	74185N 1.20	74LS27N 0.12	74LS164N 0.40	74LS378N	0.65	74C157	1.52	68A40 4.55
		7405N 0.12	74100 1.10	74188N 3.00	74LS28N 0 15	74LS165N 0.80	74LS379N	0.60	74C160	0.80	
					74LS30N 012	74LS166N 0.80		2.50	74C161	0.80	68840 4.65
4040 0.50 45		7406N 0 22			74LS32N 0.12	74LS168N 0.70		2.05	74C162	0.80	6850 1.50
4042 0.50 453		7407N 0.22	74105 0.62	74191N 0.55		74LS169N 0.85		0.29	74C 163	0.80	68850 2.13
4043 0.50 453	39 0.80	7408N 0.15	74107 0.26	74192N 0.55	74LS33N 0.15	74LS170N 0.80		0.68	74C164	0.80	6852 2.95
4043AE 0.93 454	43 0.80	7409N 0.15	74109N 0.35	74193N 0.55	74LS37N 0.15				74C165	0 84	68A52 2.75
4044 0.60 454	49 3.50	7410N 0.12	74110N 0.54	74194N 0.55	74LS38N 0.14	74LS173N 0.80		0.61		0 72	
4046 0 60 455		7411N 0.18	74111N 0.68	74195N 0.55	74LS40N 0.13	74LS174N 0.4		2.10	74C173		68852 2.95 68488 5.25
4047 0.68 459		7412N 0.19	74112N 1 70	74196N 0.55	74LS42N 0.30	74LS175N 0.41		1.99	74C174	0.72	3.23
		7413N 0.27	74116N 1.98	74197N 0.55	74LS47N 0.35	74LS181N 1.05	74LS398N	2.75	74C175	0.72	
			74118N 0.85		74LS48N 0 45	74LS183N 1 75	74LS399N	2 30	74C192	0.80	Z80 series
4050 0.24 455					74LS49N 0.55	74LS189N 1 2		1.40	74C193	0.80	
4051 0.55 459		7416N 0.27	74119N 1 20	74199N 1.00		74LS190N U.4	74LS447N	1.95	74C195	0.80	Z80A 13.75
4052 0.55 459		7417N 0.27	74120N 0.95	74221N 1.00	74LS51N 0.13	145010011	145344114		74C200	4.52	Z80ADRT 7.50
4053 0.55 459	59 3.50	7420N 0.13	74121N 0.34	74246N 1.50	74LS54N 0.14			1.10	74C221	1.06	Z80APIO 3.50
4054 1.30 456		7421N 0.28	74122N 0.34	74247N 1.51	74LS55N 0.14	74LS192N 9.4		1.05			
4055 1.30 456		7423N 0.22	74123N 0.40	74248N 1.89	74LS73N 0 21	74LS193N 0.4		1.05	74C901	0 38	
4056 1.30 456		7425N 0.22	74125N 0.40	74249N 0.11	74LS74N 8.16	74LS194N 0.3	74LS670N	1 70	74C902	0.38	Z80ASIO/2 11.00
			74126N 0.40	74251N 1.05	74LS75N 0.22	74LS195N 0.3			74C903	0.38	Z80ASIO/9 9.95
4059 5.75 450		7426N 0.22			74LS76N 0.20	74LS196N 0.5			74C904	0 38	Z80CTC 4.00
4060 0.75 450		7427N 0.22	74128N 0.65		74LS78N 0.19	74LS197N 0.61		1 70	74C905	5 64	Z80ACTC 4.50
4063 1.15 456	69 1.70	7430N 0.12	74132N 0.50	74273N 2.67		74LS200N 3.4		3 40	74C906	0.38	ZB001 65 00
4066 0.30 45	72 0.22	7432N 0.23	74136N 0 65	742 ⁷ 8N 2.49	74LS83N 0.40			1 49	74C907	0.38	2000
4067 4.30 456		7437N 0.22	74141N 0 45	74279N 0.89	74LS85N 0.60	74LS202N 34				0.84	
4068 0.18 45		7438N 0.22	74142N 1 85	74283N 1.30	74LS86N 0.14	74LS221N 0.5		5 78	74C908		PROM
		7440N 0.14	74143N 2.50	74284N 3.50	74LS90N 0.32	74LS240N 0,8		1 59	74C909	1.52	
		7441N 0.54		74285N 3.50	74LS91N 0.28	74LS241N 0.8	4116/3	1.49	74C910	3 62	2708 2.00
4070 0.16 45					74LS92N 0.31	74LS242N 0.7		12.50	74C914	0.86	2716 (3.00
4071 0.16 45		7442N 0.42	74145N 0 75	74290N 1 00	74LS93N 0.31	74LS243N 0.7		9.00	74C918	0.98	2532 OA
4072 0.16 45		7443N 0.62	74147N 1.50	74293N 1 05		74LS244N 0.6		11.25	74C925	4 32	
4073 0.16 470	02 4.50	7444N 0.62	74148N 1 09	74297N 2 36	74LS95N 0.40			12.50	74C926	4 32	2732 £4.00
4075 0.16 47		7445N 0.62	74150N 0.79	74298N 1 85	74LS96N 1.20	74LS245N 0.8		12.50		4.32	1
4076 0.55 479		7446N 0.62	74151N 0.55	74865N 0.85	74LS107N 0 25	74LS247N 1.3			74C927	4,32	

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SOLID STATE REVERB UNIT

Where have all the spring lines gone? Gone to lesser projects in other magazines, that's where. Meanwhile we present this cheap, simple, but high-quality unit using solid state technology.

Design by Charles Blakey.



t last — a reverberation unit which is not a pseudo echo effect and does not suffer from the defects of spring line devices. The unit described below will interface with virtually any preamplified signal and is ideal for direct use with most musical instruments or for incorporating in the 'echo-send' line of mixers. The design has been made possible by a new 3328-stage bucket brigade device having six tapped delays and capable of producing a useful reverberation time of about three seconds.

Sound emitted in an enclosed space will be subjected to both simple and multiple reflections from internal surfaces. Since these surfaces are at varying distances, the time for these reflections to occur and then decay by absorption will vary. The effect is a build-up of sound known as reverberation. When playing a musical instrument in the home, small studio or some other venue, the decay time can be very small coupled with a high absorption loss; the result is a weak sound when compared to recorded music or to live music played in a large hall

Until now the only low-cost method of simulating acoustic reverberation has been the use of spring lines. These units, however, are prone to vibration, require a high

power consumption for effective driving and are prone to producing distorted resonant peaks. Furthermore it is not possible to adjust the reverberation time and in many instances a short reverberation can be very effective. Another option has been available for some years, namely, the use of bucket brigade devices to electronically delay signals. While claims have been made for reverberation effects based on these products, a realistic unit would require at least three dual 512-stage BBDs. such as the Reticon SAD1024A. The cost and complexity of the latter approach puts it beyond the reach of the average constructor.

Beyond The Pail

The reverberation unit utilises the MN3011, which is the latest in a series of bucket brigade devices for audio applications to come from National Panasonic. They are all fabricated in PMOS and for a start you can forget most of what you may have read about the disadvantages of PMOS BBDs. It is a fact that they are somewhat limited in clocking speed (10 kHz to 100 kHz) and also have a limited bandwidth, typically 10 to 12 kHz. The latter, however, is not usually a limitation since the bandwidth is often restricted

by the desire for long delay times. What makes the series ideal for audio applications is their low insertion loss, low distortion and excellent signal-to-noise ratio and for the MN3011 the specified values are 0 dB, 0.4% and 76 dB respectively.

The IC is unusual in that it has 12 pins but is the length of a normal 18-pin package; the functional block diagram and pinout for the MN3011 is shown in Fig. 1. As is normal with such devices it requires two power supplies, V_{DD} and V_{CC} ; the former may be up to 18 V with respect to ground while V_{GG} should be $\pm 1 \text{ V}$ higher than V_{DD} Bucket brigade, or charge coupled, devices are analogue shift registers which operate by sampling the input signal at a rate determined by an external clock. The signal level at the time of sampling is stored on an internal capacitor; this charge is then clocked down a series of capacitors by means of internal switches. The transfer process is accomplished by a dual clock whose outputs are in antiphase and so are alternately opening and closing adjacent switches. It will be apparent that the slower the clock speed the longer the delay. Since the devices operate at high clocking speeds the input signals are faithfully reproduced at the output.

The most interesting feature of the

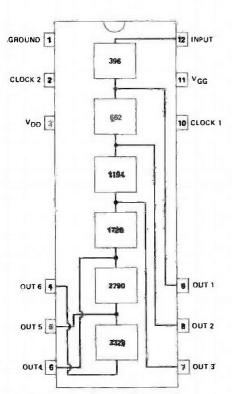


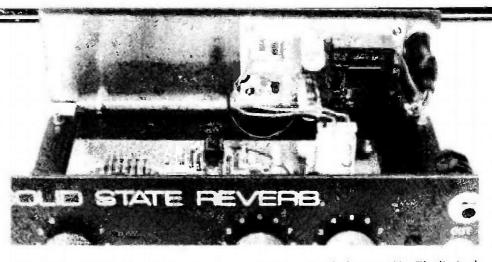
Fig. 1 Pinout and internal layout of the MN3011. The centre three pins on each side of this 18 pin package are absent.

MN3011 is that it has six tapped delays and Fig. 1 shows the number of stages for each tapping. The tappings are not evenly spaced since otherwise the reverberant sound would have a distinct flutter. If the device was being clocked at 10 kHz then the delays from outputs one to six would be 19.8, 33.1, 59.7, 86.3, 139.5 and 166.4 milliseconds respectively. If these delay times are mutiplied by 0.33 then one obtains the equivalent room path length for one trip, ie the longest delay is equal to a room length of 55 metres (181 feet). Reverberation time is usually measured as the time taken for the power to decay to one millionth of its initial level (60 dB down). For the present design the time was measured for the output level to fall to one hundredth of its initial level (-40 dB) and at the longest delay this was found to be about three seconds.

Blocks 'n Clocks

The block diagram of the circuit for the reverberation unit is shown in Fig. 2. First there is the dual clock driver, which is another National Panasonic device, the MN3101. It has an oscillator, divider and wave form shaping and produces the dual clock pulses required by the MN3011. It reduces component count and is lower in cost than other alternatives, such as a 4007. A further advantage is that it also generates the required V_{GG} voltage.

The unit will operate satisfactorily



with any input signal greater than 280 mV RMS and higher input signals are attenuated by the input potentiometer. The signal is also reduced by half in amplifier A1 and inputs higher than 140 mV to the first filter are indicated by a LED peak detector circuit. Although the MN3011 will accept signal levels up to 780 mV before the distortion value stated earlier is exceeded, it will become apparent that the effect of reverberation can lead to reinforcement of signals and consequently this has to be allowed for. The only preset in the circuit is used to apply a bias voltage to the signal. The precise value of this voltage is not very critical in the current design and the object is to keep the signal at a level where it will not be distorted or clipped within the BBD.

The main problem with BBDs is the inability to completely cancel out the clock pulses and these can form audible cross products with the input signal. In order to prevent this foldover distortion, the bandwidth of the input signal should be limited to between a half and a third of the clock frequency. Filter F1 in Fig. 2 is a lowpass filter with a cut-off frequency of 3.6 kHz. This may seem rather low but in fact it is equivalent to the upper reverberation limit of most spring lines and the BBD scores in respect of low frequency responses since springs usually give rise

to 'booming' below 100 Hz. The limited bandwidth is compensated by mixing the original signal with the reverberated signal at the output stage. The filtered signal goes to the MN3011 and the six output stages are summed to give a composite signal with different delay times. This signal is again filtered with a lowpass filter with a cut-off frequency of 3.6 kHz, to remove residual clock glitches, prior to mixing with the original signal at the output amplifier, A2.

The most important feature. however, is that the signal from the longest delay is returned, slightly attenuated, to the input and subjected to further delays. This is the reverberation effect and with the times given earlier the sound will simulate the effect of the first reaching a surface 55 metres away (assuming slowest clocking rate) and then being reflected back as well as being reflected from other surfaces closer than the 55 metre surface. The whole process is repeated until the original delayed signal and its reflections die away. In the meantime new signals are being recycled and the overall effect is a build-up of sound reverberation.

Construction

The construction is very straightforward but the following precautions should be observed. First,

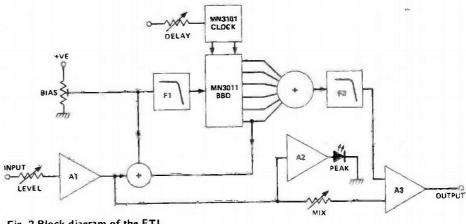


Fig. 2 Block diagram of the ETI Solid State Reverberation unit.

BUYLINES

The PCB and a kit of components for the reverberation unit is available for £32.00, inclusive of postage and VAT, from Digisound Limited, 13 The Brooklands, Wrea Green, Preston, Lancs PR4 2NQ. The power supply may also be obtained for an inclusive price of £7.00. As the PCBs are copyright they will not be available from our PCB Service; however, the foil patterns are reproduced at the back of the magazine. National Panasonic do not distribute active components in the UK and the ICs may only be obtained from Digisound.

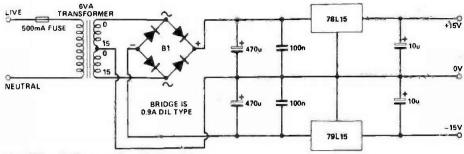


Fig. 4 Circuit diagram of a suitable PSU for this project.

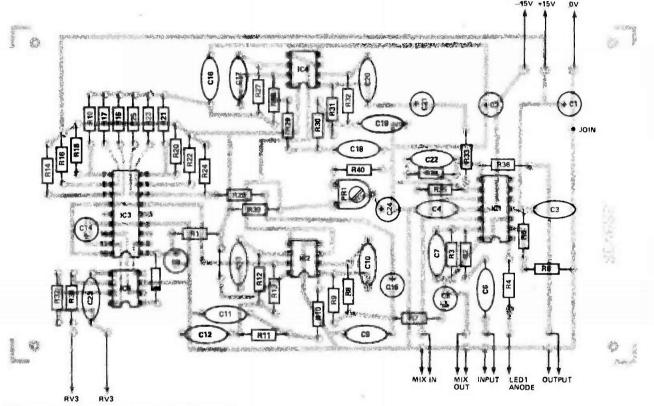


Fig. 3 Component overlay for the reverberation units

make sure you get the correct orientation of the ICs which are clearly shown on the component overlay. Second, the MN3011 is a CMOS device and with the advent of 'B' series devices we have all become rather careless as regards handling such ICs. For the MN3011, however, take the precaution of working on a grounded

DCII DARTS HIST

Capacito	rs					
C1,2	470u 35 V PCB electrolytic					
C3,4	100n polyester					
C5,6	10u 35 V PCB electrolytic					
Semicon	ductors					
IC1	78L15					
IC2	79L15					
BR1	0A9 DIL type					
Miscella						
PCB (se	ee Buylines); PCB-mounting					
	ner (15-0-15, 6 VA); 500 mA main: chassis-mounting holder.					

Nation and	PART PART	S LIST	
Resistors (Al R1	1 ¼ W 5% except where stated) 10R ½ W	PR1	47k miniature horizontal preset
R2,5,7,9,			
13,32,33,39	100k	Capacitors	
R3,34	51k	C1,2	10u 35 V PCB electrolytic
R4	330R	C3,4	100n polyester
R6	1k3	C5	22u 35 V PCB electrolytic
R8,12,27,31	33k	C6	220n polyester
R 10, 29, 37	47k	C7,10,13,	
R11, 30	56k	20,22	220p połystyrene
R14,16,18,20		C8,14,15,	
22,24	56k 1%	21,24	3u3 63 V PCB electrolytic
R15	100k 1%	C9,11,12;	
R17	110k 1%	18,19	2n7 polystyrene
R19	120k 1%	C16	2n2 polystyrene
R21	130k 1%	C17	270p polystyrene
R23	150k 1%	C23	33p polystyrene
R25	160k 1%		
R26	200k	Semiconduc	ctors
R28	82k	IC1	TL074
R35	18k	IC2, 4	LM358
R36	1k0	IC3	MN3011
R38	36k	IC5	MN3101
	68k	D1	1N4148
R40	DOK	LED1	5 mm red LED
D. 4 4 4		Miscellaneo	•
Potentiomet		SK1,2	mono jack sockets
RV1	100k logarithmic		ylines); IC sockets; case (Ve
RV2	10k logarithmic	order no. 91	
RV3	470k linear	order Bo. 9	1-20/ 30).

metal surface, such as a piece of aluminium foil, do not insert the IC with the power on and do not use a soldering iron on the PCB with the IC installed.

The PCB supplied with the kit has a ground plane to reduce interference from and to other electronic equipment as well as to reduce noise. This feature allows greater freedom in locating the unit, eg it does not have to be housed in a separate metal case. A ground plane comprises a metallized surface on the component side except for small areas around the holes for the components. Ensure that the component leads do not touch the ground plane - which is not difficult and preferably solder the resistors and axial capacitors in place with a thin piece of card between the component and the board so that the former are not in physical contact with the ground plane. After soldering the card is removed. The latter step is not essential. The one wire link must be made with insulated wire. The ground plane has to be connected to the 0 V line and some 15 mm from where the latter is connected to the PCB there is a hole marked 'join'. A piece of wire should be placed through this hole and soldered on both sides of the PCB.

The PCB has been laid out such that the BBD and clock are as far away as practical from the signal input and output. This separation should be maintained if the unit is housed in a

box and all wiring should be kept as short and as neat as practical, with the audio connections being made with miniature screened cable.

The unit requires a ± 15 V power supply and the current consumption is a miserly 13 mA at ± 15 V and 9 mA on the ± 15 V line. If a separate power

supply is required then a suitable PSU is shown in Fig. 4. A PCB-mounted transformer is preferred, and it should be mounted as far away from the BBD as practical. The photographs show the unit inside a Vero 'G' range case with internal dimensions of approximately 218 x 138 x 50 mm.

HOW IT WORKS

The input signal is attenuated by RV1 and also by the inverting amplifier built around IC1a which has a gain of about 0.5. From IC1a the signal goes three ways. A comparator built around IC1b forms a peak detector to indicate optimum signal level, while RV2 and R35 allow mixing of the original signal with the reverberated signal in the inverting amplifier configured around IC1c. The component values in this section are such that equal proportions of the two signals may be mixed. Finally the signal also passes to two active filters constructed around IC2 which have a 12 dB/octave roll-off for each stage and a cut-off frequency of 3.6 kHz.

From the above filter stages the signal passes into the MN3011 and the six delay outputs are summed by the resistor network formed by R14 to R25. Note that the shorter the delay, the less the attenuation. From the longest delay (pin 4) the signal goes via R25 back to the input of the filter and thus provides recycling of the delayed signal in order to generate a true reverberation effect. The reverberated signal is filtered by two active filters constructed around IC4 and these have the same characteristics as the input filters. Between the active filter stages some passive filters have also been

added to increase the roll-off; the loss in these filters is compensated by increasing the gain of the active filters.

The dual clock for the MN3011 is provided by IC5 and with the components shown, the clock frequency may be manually varied with RV3 over the range 10 kHz to 100 kHz, allowing maximum first pass delays from 16.64 to 166.45 milliseconds. Pin 8 of ICS provides the V_{GG} voltage for the MN3011. Since both IC3 and tC5 are P-channel CMOS it would be normal to operate them from a -15 V supply. Voltages are, however, relative and by connecting + 15 V to the ground pin and ground (0 V) to the V_{DO} pin they will operate happily with positive signal inputs. R1 and C5 prevent clocking signals getting back into the power lines. The filters are also operated from a single + 15 V supply and this avoids any problems which may arise from excessive bipolar signals, ie they will be clipped at + 15 V or ground and not damage the BBD. The bias voltage required by the BBD and the filters is primarily to allow them to accept bipolar signals; this voltage is provided by the resistive divider using components R39, PR1 and R40 and is applied to the non-inverting input of the filter op-amps.

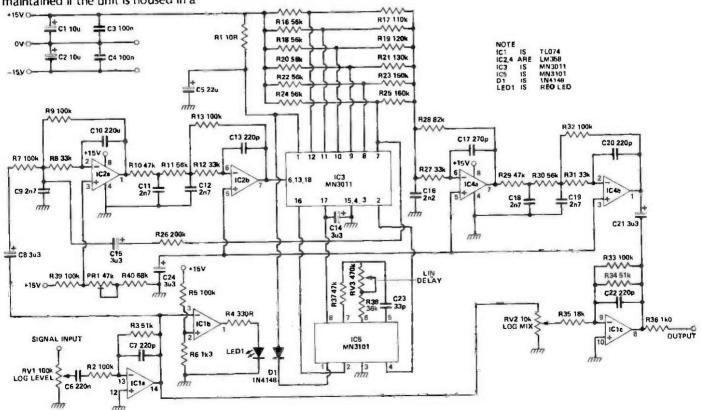
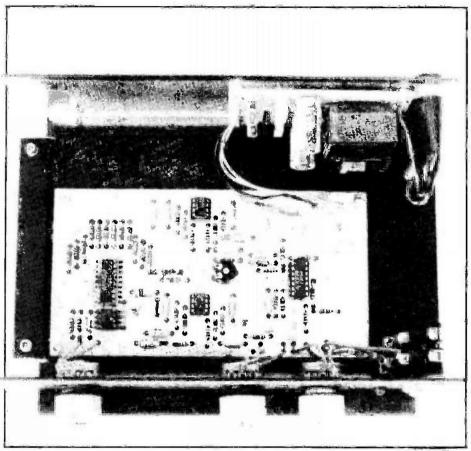


Fig. 5 Circuit diagram for the ETI Reverb.

Setting Up And Use

The only setting up required is adjustment of PR1. If a sinewave source is available then the latter may be used as the signal source and PR1 adjusted by ear, or with an oscilloscope, for minimum distortion. Alternatively measure the voltage at the junction of PR1 and R40 and adjust PR1 to give a reading of 6V2.

The unit has a signal-to-noise ratio of better than 60 dB but this requires that it is operated with the peak indicator LED just glowing or occasionally illuminating. The output level will vary from about 0V5 to 1 V RMS, depending on the amount of mixing of the original signal, and these levels should ensure adequate response from most amplifiers, mixers, and so on. In other words, by keeping input signals at maximum level the amplifier setting will be such that during periods of no signal the residual noise will not be obtrusive. This is common practice with recorders, many of which have much lower signal-to-noise ratios.



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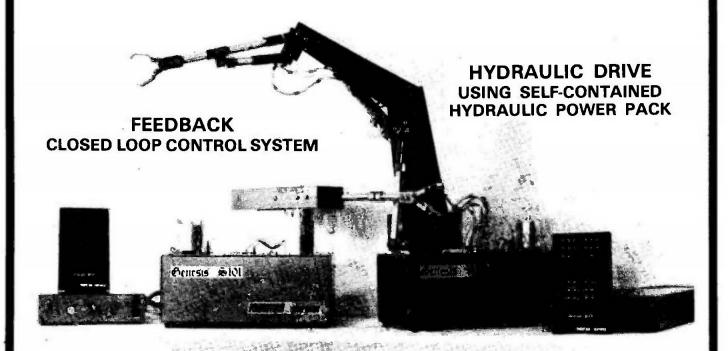
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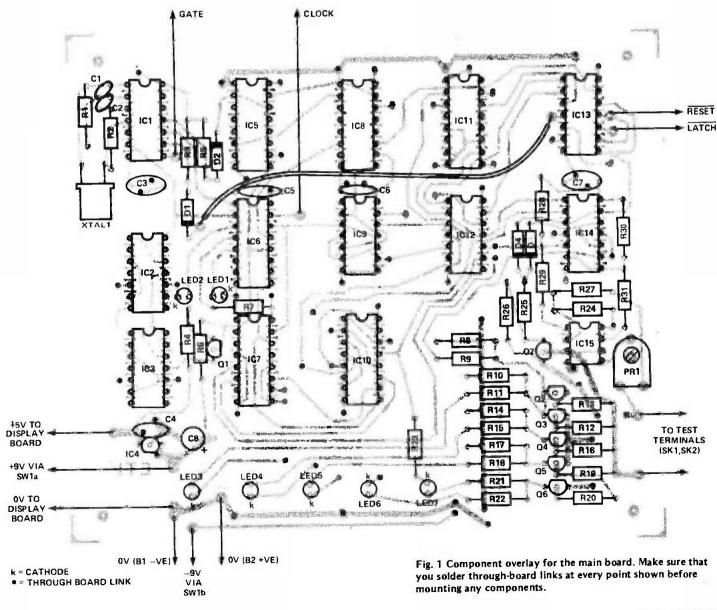
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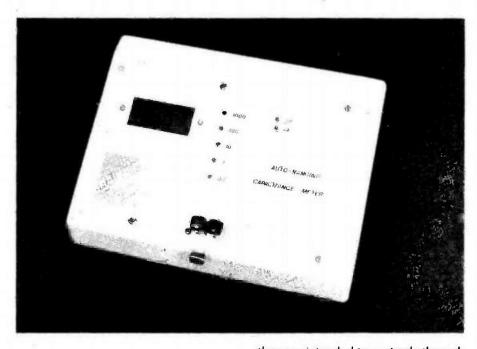
Design and development by Phil Walker.



his is a fairly complex project and should only be attempted by those with a good deal of constructional experience. It is well worthwhile checking the PCB for shorts between tracks before doing anything else. Ensure that there is a hole through the board under the PR1 position to facilitate adjustment later.

Put links through the board at all positions marked with a dot on the overlay and solder on BOTH sides of the board. The other components may now be inserted into the board preferably using sockets for all the ICs except IC4 and IC15. IC4 is a T092-type package 100 mA regulator and does not need a socket, while IC15 may foul PR1 if a socket is used.

The LEDs should not be fitted until the board is test-fitted in position as



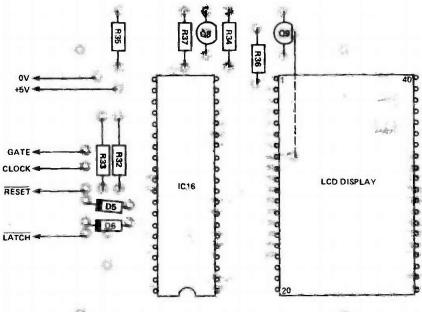


Fig. 2 Component overlay for the display board. Insert the link under the display first.

they are intended to protrude through the panel as indicators. Attach power supply wires and fit up to the panel, position the LEDs and solder in position.

Assemble the display board components and attach the logic and power supply wires from the main board. Wire the remaining power leads via the on/off switch to the battery connectors and attach the two boards to the front panel using pillars or long bolts and lock nuts. Our prototype just fitted into a slope fronted instrument case made by Vero Industries (see Parts List).

BUYLINES.

Very few unusual components in this project; all the logic is standard CMOS. The ICM7224 and the LCD display is stocked by Watford Electronics, while the LF353 is available from Rapid Electronics. The two PCBs can be obtained from our PCB Service, advertised on page 44.

			PARTS LIST		
R1,2 R3,4,5, 28-37 R6,25 R9 R10,14,17,	4W, 5% except where stated) 470R 15k 4k7 10k	Capacitors C1 C2 C3-7 C8	10p ceramic 1n0 ceramic 100n ceramic 100u 10 V tantalum	IC15 IC16 Q1,7,8,9, Q2-6 Q3-7 D1-6 LED1-7	LF353 ICM7224 BC182L BC212L BC212L 1N4148 miniature green LEDs
R11,15,18, 22,23 R12 R13 R16 R19 R20 R24,27 R26	100k 1k0 100R 1% 1M0 5% or better 1k0 1% 10k 1% 10k 1% 27k 2% 1k8 27k 2%	Semicondu 1C1 1C2,3 IC4 IC5,8 IC6 IC7 IC9 IC10 IC11 IC12	ctors 74LS04 74LS90 78L05 4518B 4053B 4029B 4013B 4051B 4049B 4012B 4012B	sockets; dis tery and co	miniature 10 MHz crystal DPDT toggle switch press terminals (one red, one black) Buylines); 3½ digit LCD display; IC play socket (if required); PP9 bat- nnectors; PP3 battery and connec- ting hardware; case (Vero 220 x
PR1	47k miniature horizontal preset	IC14	4001B		ping front box, order no. 65-2523E).

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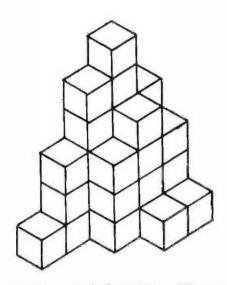
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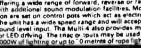
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TECH TIPS

Frequency-To-Phase Controlled Power Supply

Dilbay Singh (B.Tech), Crawley

The circuit shown in the diagram was initially designed to obtain a phase-controlled power supply to use with a ¼ horsepower stepping motor. The phase angle can be varied over the complete

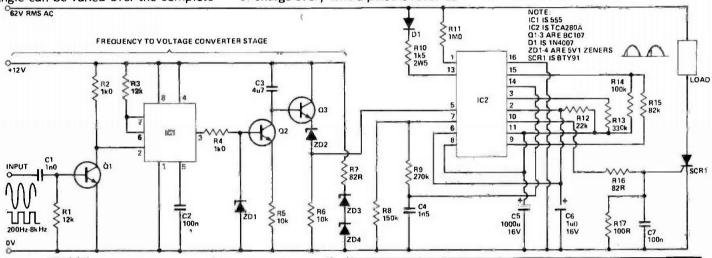
cycle period and is dependent on the frequency of the input. Clearly the circuit can be used to control resistive loads such as lamps or motors.

The first stage of the circuit consists of a frequency-to-voltage converter. C1, R1, and Q1 effectively differentiate and amplify the input signal waveform to provide triggering pulses for the 555 timer, which is used in the monostable mode. The output of the monostable is used to charge C3 by a constant amount of charge every time a pulse is received

at the base of Q2. The voltage across C3 acts as an input to the common collector stage formed by Q3. The voltage across C3 is DC-shifted by means of the zener diode ZD2 to a suitable value, providing the input to the trigger IC (the Mullard TCA280A). The TCA280A provides the phase control signal for the gate of the thyristor.

A triac may be used in place of the thyristor, if phase-controlled AC is required.

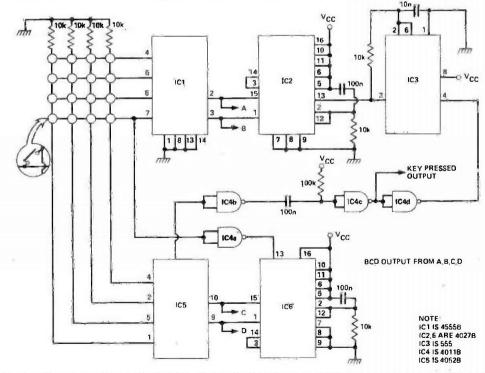
The component values shown are suitable for providing phase control using frequencies in the range 200 Hz-8 kHz on the control input. The firing angle can be varied from 0° at 8 kHz to 170° at 200 Hz.



Fully Debounced Keyboard

Graham Kyte, Bexleyheath

This circuit produces a debounced output whenever a key is pressed. Each matrix point is scanned in turn and the output of the 4052 data distributor goes high when a pressed key is detected. This stops the scanning oscillator (555) for about 10 mS and a 'key pressed' output is produced, thus enabling the BCD output to be stored in a latch or otherwise made use of. The use of CMOS ICs enables current consumption to be minimised, making the circuit suitable for operation in a car. The circuit is easily modified for a larger number of keys by using an eightway data distributor (with relevent counter made from three J-K flip-flops rather than the two as used here).





Remote Camera Release

Geoffrey Ammon, Welling

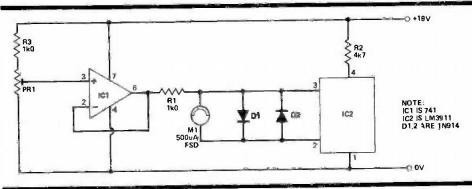
When taking photographs from a distance, a pneumatic remote release is normally used. These will only work over a limited distance and it is not always possible to tell if the camera has operated. This simple circuit uses a low current trigger circuit to operate the camera and provides a visible indication that the camera or flashgun has worked correctly.

The circuit operation is as follows. When the remote release push-button PB1 is operated, a current flows via the extension lead, which may be a 100 metres or more in length, to switch transistors Q3 and Q4. This combination provides the load current of up to 2 A for the camera release solenoid. When the flashgun fires, light falling on the CdS cell

CL703 R2 CL703 R2 CL703 R2 CL TO TO TO THE TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL T

causes a current pulse to appear at the base of Q1. When Q1 switches on it will discharge C2, extending the pulse duration to about one second. While C2 is charging Q2 will be turned on, causing a large enough current to flow in the extension lead to operate LED1. If a flashgun is

not used, the camera flash contacts (SW1) may be connected to bypass the CdS cell and remotely operate the indicator LED1.

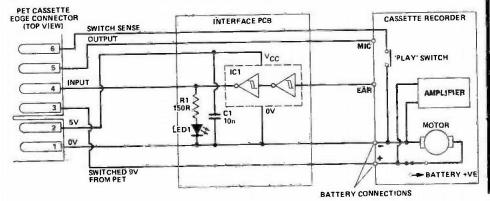


Cheap PET Cassette

D.J. Cocker, Portsmouth

In view of the price of the Commodore cassette unit, the following adaptation may be of interest. I have been using this arrangement for some time and have experienced very few problems. In order to signal the PET when the PLAY key has been pressed, a switch mus be incorporated into the cassette key assembly—a small microswitch is ideal. This is an improvement on the Commodore unit,

in which any key activates the switch, leading to confusion and ambiguity. The 'signal present' LED is very useful in locating the start and end of the data tape. The cassette recorder is supplied with power from the PET, batteries only being required for fast forward and rewind functions — a switch should be fitted to facilitate this. When the PLAY key is depressed, the PET has control of the tape motor. It may be found necessary to disable any tone control circuitry or AGC which may be fitted in the cassette recorder. Any suitable TTL Schmitt gate may be used as IC1.



Room Thermometer

J. P. Macaulay, Crawley

With the advent of the LM3911 temperature controller IC the task of measuring temperature has become simple in the extreme. The internal circuitry of this device comprises a temperature sensing element, an op-amp and a stable reference voltage. The device gives, in its simplest form, a stable 10 mV change in output for every 1° change in temperature over the range —25 to 85°C. For the application of room thermometer it is only necessary to utilise part of this range from, say, 0° —50°C. The circuit to be described measures this range.

The figure shows the complete circuit of the thermometer. The meter, a 500 uA FSD type, is connected between the output and inverting input of the internal op-amp. Resistor R1 connects the inverting input to the output of the 741 op-amp. This is used with 100% AC and DC feedback to form a unity gain voltage follower with a current output capacity of several milliamps. The input of the 741 is connected to the slider of PR1 which in turn is connected across the stable supply voltage produced by the IC. D1 and D2 protect the meter from overrange temperatures and thus protect its delicate movement from harm.

Once completed, a calibration can be made with a room thermometer of known accuracy. Simply leave the equipment in the room for 10 minutes or so for its own temperature to stabilise and then adjust PR1 until both thermometers read the same; the calibration is now complete.

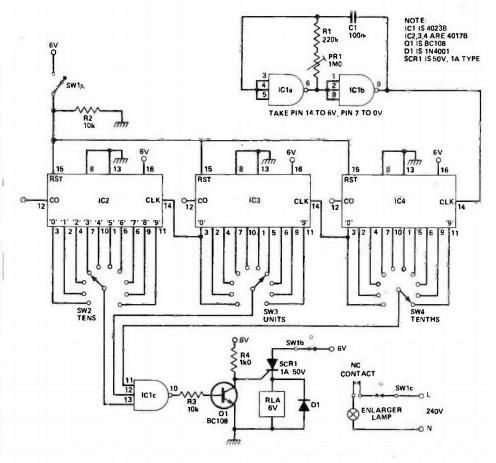
Enlarger Timer

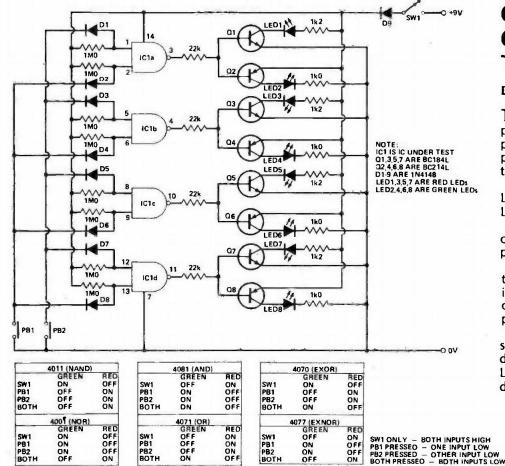
C. E. Basson, South Africa

The circuit of the enlarger timer can time periods from 0 to 99.9 seconds in 0.1 second steps. PR1, C1, R1, IC1a, b form an oscillator that feeds a 10 Hz signal to the first 4017 counter stage. Either the 'carry out' or '0' outputs of IC2 and IC3 can be used to feed the next stage, as the frequencies are the same and the positive-going edges of the pulses appear at the same time. Outputs '0' to '9' go high in sequence as the pulses are received at the 'clock in'. The desired time is selected by SW2, SW3 and SW4.

Q1 is used as an inverter and with the NAND gate it performs the same function as an AND gate. As soon as the desired time is reached, all the inputs on the gate will be high and this will trigger SCR1. The relay will be turned on and switch off the enlarger lamp. The lamp will remain off until the circuit is reset.

The circuit can be resetted by closing SW1a and opening SW1b and SW1c. SW1a will reset the 4017s and keep them in the reset condition. SW1b will remove the current from SCR1 to reset it. SW1c prevents the light from going on when in the reset condition. When SW1 is switched back to normal, the light will go on and remain on for the desired time.





Comprehensive CMOS Logic Gate Test Rig

David Ian, Surrey

This simple test rig will check out all possible functions of any type of dual input CMOS logic gate allowing, for example, a faulty gate to be pinpointed so that the rest of the IC may still be used.

Each gate is provided with a green LED to indicate a high output and a red LED to show a low output.

Use a 14-pin holder for the IC and orientate the LEDs to relate to their appropriate gate.

SW1 connects power and a logic 1 to all inputs: press A to put a 0 onto one input of each gate; B puts 0 onto the other inputs; A and B togther force all inputs low.

A milliammeter in series with a 9 V supply should only indicate the current drawn by the LEDs, ie about 7 mA per LED. An appreciably higher reading indicates a completely faulty IC.

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6821 1.1			164	.46	3.579MHz	1.00
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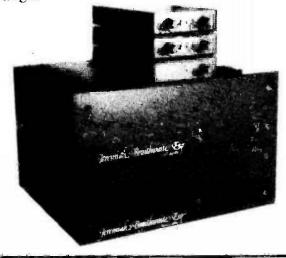
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First, let A\$ = STR\$(the product of 7K (in decimal) and the standard audio bandwidth). We'll use this later. Now, add the UK AC mains frequency to yellow/violet/red and divide by the number of our modular synth project. Divide the result into VAL(RIGHT\$(A\$,4))-VAL(MID\$(A\$,5,3))/LEN(A\$)Add to this result the difference between our office street number and the TTL prefix. Multiply by the log (to base 10) of the sum of the digits of a CMOS quad EXNOR IC divided by the number of pins on a 555. Finally, add the decimal number represented in binary by 10111.

If you've managed all that (hint - people who know BASIC well have an advantage), write the answer on the entry form (page 133) with your name and address and send it to us by April 30th 1982. Answers to six decimal places, please.

RULES.

- Closing date is April 30th 1982, and all entries post-marked later than this date will be discounted. The coupon provided in the magazine must be used. Photocopies are NOT acceptable. Employees of ASP and their relatives are not eligible for

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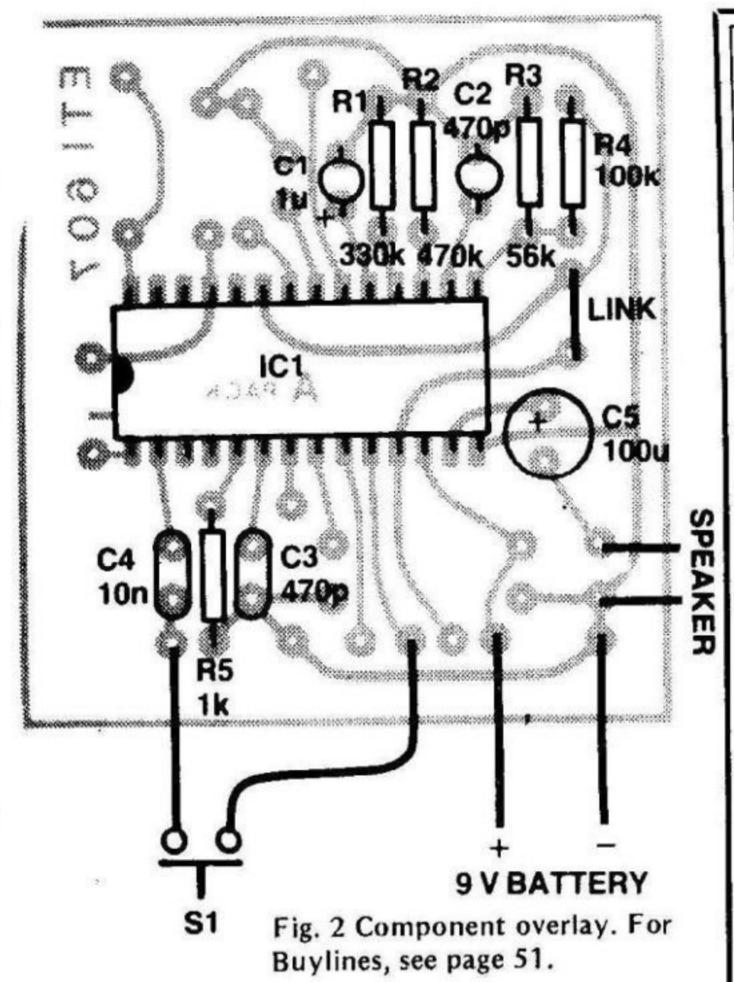
 The judges' decision is to be considered final and no correspondence will be entered into concerning the

SOUND EFFECTS 2: STEAM TRAIN

Railway modellers looking for something special to improve their layout need look no further. Our second sound effect project simulates a steam train and whistle. Design by Phil Wait.

ahh, the nostalgia! If you're young at heart, old in years, or both, then this is for you — a steam train (chuff-chuff) and whistle. The electronic construction details are given on page 50 in the bomb drop project; but for that authentic touch, deft constructors can also fashion a cow-catcher out of tinned copper wire to attach to the unit!

The chuff-chuff runs continuously once power is applied and the whistle sounds when the push-button is pressed. The VCO is used to provide the whistle while the SLF modulates the noise generator/filter output to produce the steam train's chuff-chuff sound. The chuff-chuff rate may be varied by changing the values of R1 and C1, while the chuff-chuff sound may be varied by changing the values of R2 and C2. For a special effect, you can control the chuff-chuff rate manually by replacing R1 with a 1M0 potentiometer.



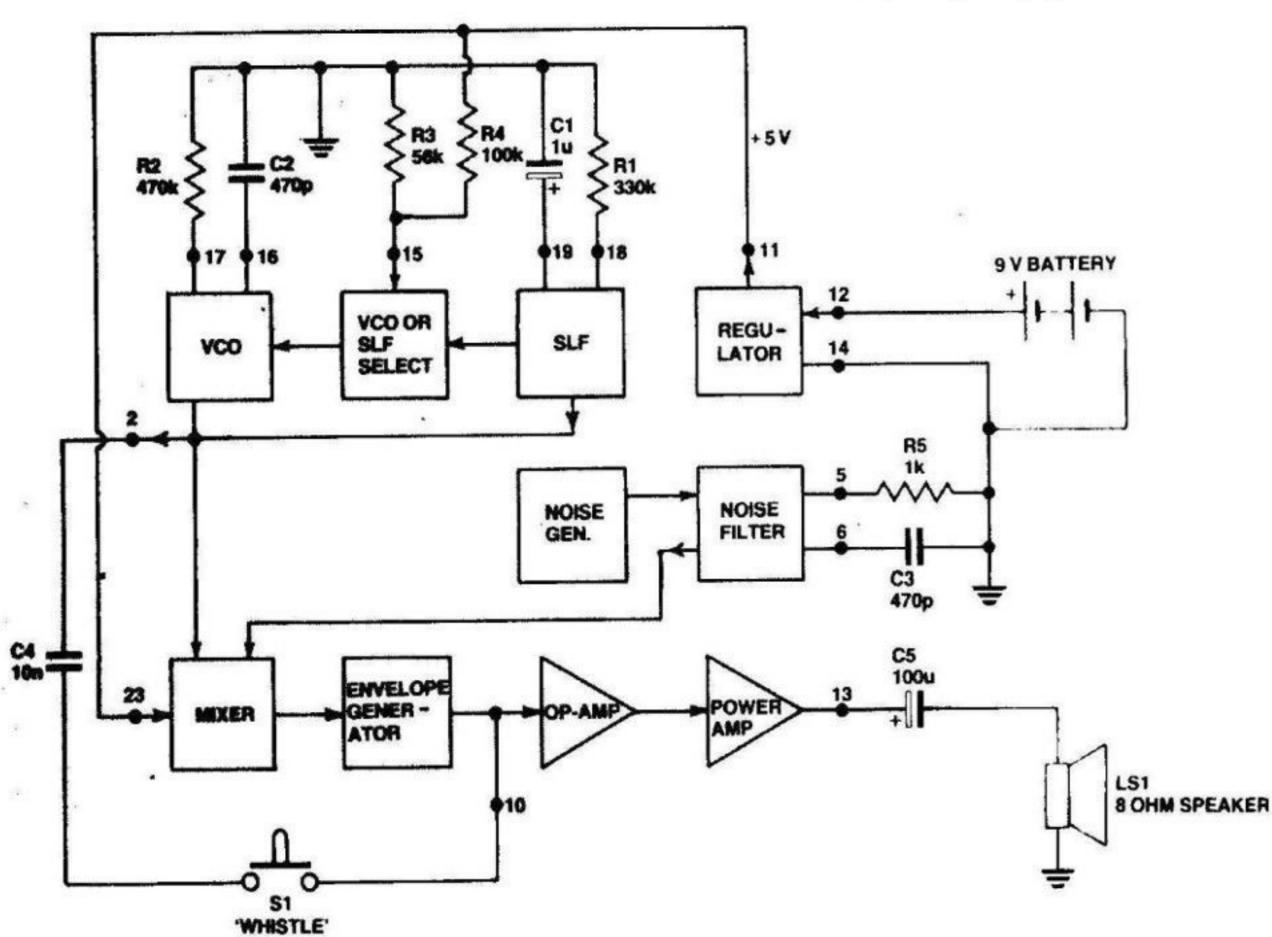


Fig. 1 Circuit diagram of the Steam Train and Whistle unit.

HOW IT WORKS

In this unit the Noise Generator/Filter is employed to produce the basic 'steam engine' sound, this being modulated by the SLF to produce the 'chuff-chuff' so characteristic of steam locomotives. The whistle is produced by the VCO, which is set to a particular non-varying pitch, and the output is switched into the audio input pin to produce the whistle.

The broadband noise from the Noise Generator is modified by the Noise Filter, the frequency characteristics being determined by R5 and C3 connected to the Noise Filter Control pins (5 and 6). The Noise Filter Output is fed via the Mixer and the Envelope Generator (which doesn't function here) to the audio output stages. The SLF square wave output effectively modulates the noise to produce a noise burst followed by a silent period, then another noise burst. Thus the chuff-chuff sound is produced. This sound is continuous whilst power is applied to the unit.

A resistive divider, R3/R4, provides about 1V8 at the VCO frequency to a convenient pitch within its range, providing a suitable pitch for the whistle. The VCO output is coupled to the audio input (pin 10) via C4 and the push-button, PB1. When PB1 is pressed, the whistle is heard over the chuff-chuff sound.

The SLF frequency is determined by C1 and R1, while the combination of R2/C2 and the voltage on pin 15 determines the VCO frequency. Output to the loudspeaker is coupled via C5, a 100uF electrolytic capacitor.

PARTS LIST

Resistors	(all 1/4 W, 5%)
R1	330k
R2	470k
R3	56k
R4	100k
R5	1k0
Capacito	
C1	1u0 16 V tantalum
C2, 3	470p ceramic
C4	10n ceramic
C5	100u 16 V PCB electrolytic
Semicon	ductors
IC1	SN76488 (see Buylines)
Miscella	nous
PB1	SPST push-button switch
	Buylines); 50 mm diameter 8 ohn PP3 battery and clip.

Having trouble containing yourself?

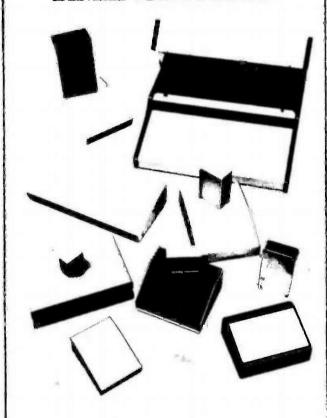
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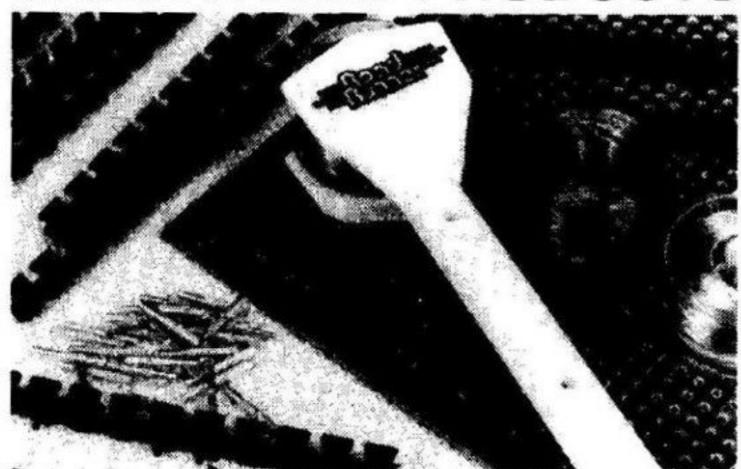
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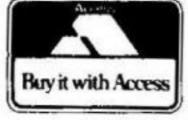
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GUITAR PRACTICE AMPLIFIER

Simple construction, low cost, good performance and super neighbour relations are the features of this project! Design and development by David Tilbrook.



This project has been designed to enable guitarists to put in long hours of practice and still keep that high power amp in the cupboard, where it belongs! It is a compact amp capable of about 7 W into a 4 ohm load. This is enough power for practice purposes and just think of the greatly improved relations you will have with your neighbours.

We were in a considerable quandary as to how to present the project, whether it should be done as a complete practice unit with inbuilt speaker or simply as an amplifier to be connected to an external speaker. Finally we chose a compromise. The PCB has been designed in such a way that it can be used as a totally selfcontained unit. The heatsinks for the output stage have been mounted on the PCB so that the only components separate to the board are the power transformer, 240 volt power switch controls, input and output jacks. We have shown the project mounted in its own box with power transformer but it should be a simple matter to construct the whole unit inside a small loudspeaker cabinet.

The unit has two inputs so that two guitars can be mixed together using the relative settings of the two input level controls. A preamp output enables your main high power amp to be driven from the guitar practice amp using the practice amp as foldback.

We provided the PCB with the necessary circuitry for a battery input but you might elect not to use this feature. If so diode D8 and the battery switch can be omitted with points 'A' and 'C' connected together by a wire link

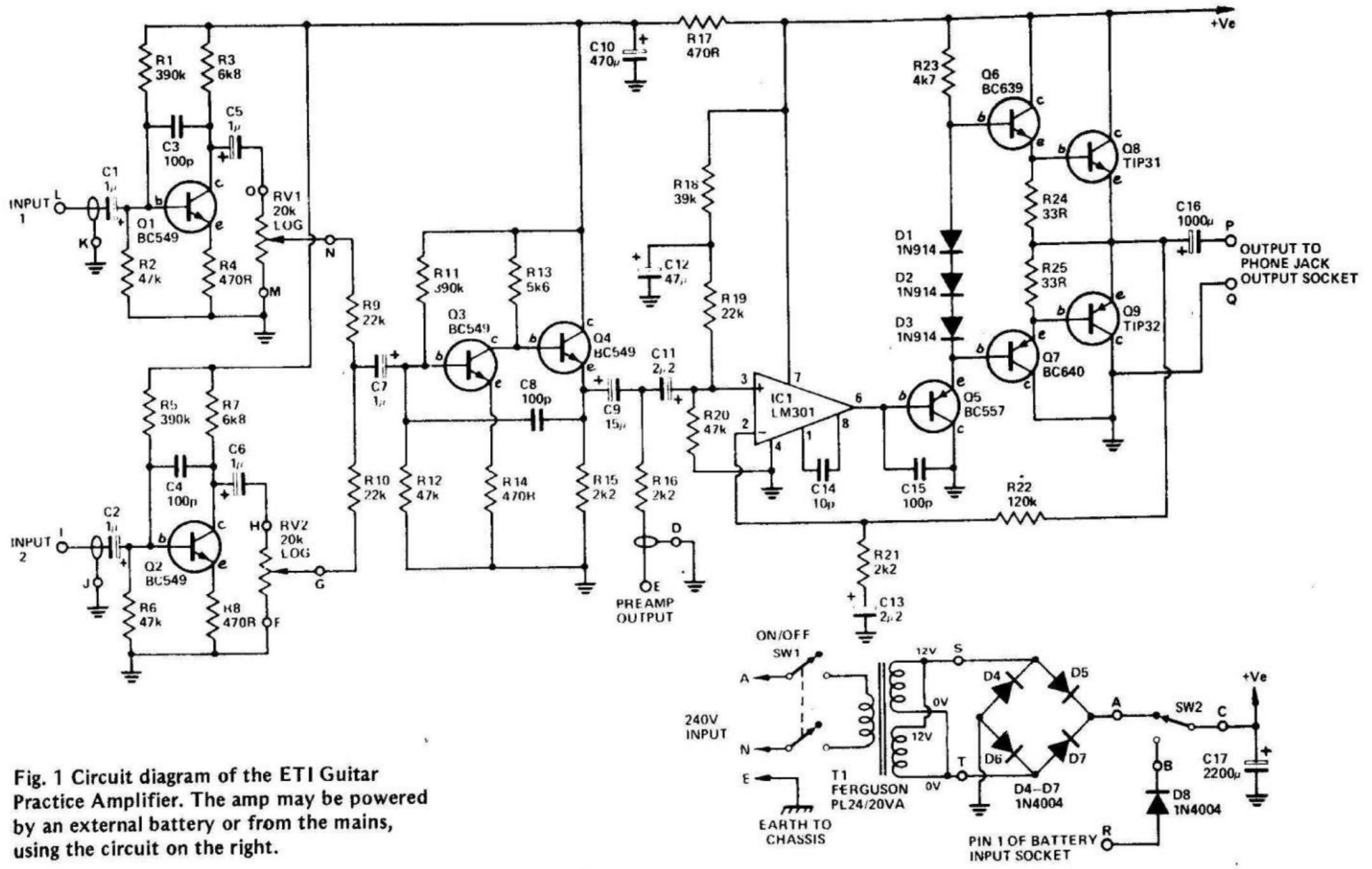
Construction

Construction of the project is reasonably simple since it is almost entirely devoted to construction of the PCB. Start as always by mounting the resistors and non-polarised capacitors. Mount the tantalum and electrolytic capacitors next, being careful to orient them correctly. These components could be irreparably damaged if inserted the wrong way around. Mount the LM301 IC, transistors and diodes, again being careful to insert these the correct way round.

Finally the output devices can be mounted. Although the transistors are in TO220 packages, our PCB is laid out to accept heatsinks drilled for TO3 transistors. The overlay and photograph should make the construction method clear. Cut the centre (collector) lead off. This lead is connected to the case of the transistor internally, so in this case, electrical connection is made through the mounting screw that also serves to hold the heatsink in place. Place the heatsinks on the PCB and secure with the lower nut and bolt (not used to mount the transistors). There is only one right way round. Bend the leads of the output transistors and, using a small amount of thermal compound, mount the transistors with the leads protruding through the PCB.

Secure each transistor with a nut and bolt through both the transistor 'flag' and heatsink. Use a star washer between the head of the bolt and the copper pad on the PCB to ensure good electrical contact. Now the base and emitter leads can be soldered to their pads.

The prototype unit was constructed in a steel box measuring



HOW IT WORKS.

The two input stages formed around Q1 and Q2 are identical. Resistors R1, R2 and R4 form a very stable biasing configuration around Q1. The gain of this type of circuit is determined by the values of R3 and R4 (specifically, the gain is R3/R4). The load impedance on the output of the input stages is in parallel with R3, effectively decreasing the total value of impedance from collector to ground. Remember that, as far as signal is concerned, the positive supply rail is a short circuit to ground, since it is connected to ground through C17, a 2200uF capacitor. When all these factors are taken into account the gain of the first stage is about 10 since the impedance from collector to ground is about 4k7.

The signal, which should now be around 200 mV, is then applied to the input of the second stage through potentiometers RV1 and RV2. The 22k resistors R9 and R10 prevent the output of one of the stages being shorted to ground when the other is turned right down.

The second stage works in exactly the same manner as the input stages, resistors R11, R12 and R14 forming the bias network for Q3. The voltage present on the collector of Q3 is around 9 V which is approximately half the supply voltage. This is used to bias Q4 which is an emitter follower. This type of amplifier has no voltage gain but provides a low output impedance to drive the preamp output socket. Q3 has a gain of approximately 10. If the volume controls RV1 and RV2 are used in their middle positions, the voltage out will be around one tenth of the voltage at their inputs since these are logarithmic pots. So, the signal voltages into Q3 should be in the order of 20 mV. This will be amplified to a level of 200 mV and applied to the input of the power amp. The power amp has been designed to deliver full power with an input voltage of 300 mV, so the amp should be easily driven to

full output with usable settings.

Since this is a guitar amplifier, it will spend most of its life hard into clipping. The output stage had to be robust! The basis of the output stage is the LM301 op-amp. This device gives all of the voltage gain in the power amp. The output IC1 is fed through a voltage follower Q5. This has no voltage gain and, like Q4, serves to decrease the impedance feeding the output stage. The three diodes, D1, D2 and D3, maintain 1V8 between the bases of Q6 and Q7. Each of these transistors will drop approximately 0V6 across their base-emitter junctions. This leaves a total of 0V6 to be dropped by the two 33R resistors, R24 and R25. Since these are of equal value they will each drop 0V3 and hold this voltage across the base-emitter junctions of the two output transistors Q8 and Q9. As these transistors require 0V6 to turn on they will remain off until the applied signal voltage causes the voltages on their bases to rise above 0V6. The extra 0V3 needed to turn on the output devices will be supplied by a mere 10 mA of current through the 33R resistors. Resistor R22 forms a feedback loop around the entire output stage to decrease distortion, stabilise the DC output voltage and set the overall gain of the power stage (a process too difficult to go into here).

The op-amp will at all times attempt to make the DC voltage at the output equal to that voltage set up on its positive input. This voltage is determined by the potential divider formed by R18, R19 and R20. Since this is also the main input to the power amp any noise which might be on the positive supply rail (and supplies can get very noisy sometimes!) will be communicated directly to the input of the power amp, only to be amplified and applied to the loudspeaker. Capacitor C12 prevents this from happening by bypassing to ground any noise above a frequency of around 0.1 Hz.

approximately 250 x 210 x 80 mm. Mount the pots and switches on the front panel, using the pot and switch nuts to secure the front escutcheon if you have one. Mount the output and battery input sockets on the rear panel. If you are using a battery input socket use something different to the output socket (which is usually a two-pin DIN socket or a 6.5 mm jack socket) to avoid confusion.

Mount the power transformer and make the 240 V connections. The mains lead should be terminated immediately inside the case into a terminal block and the earth lead secured firmly to the chassis by a solder lug bolted to the case using a star washer. This lead must be the longest. A length of 240 V cable should be used between the terminal block and the power switch. Wire the transformer to the power switch as shown in the circuit diagram, then wrap the whole switch with insulation tape or enclose in large diameter heat-shrink tubing so that no 240 V connection is exposed.

Finally, the fully-loaded PCB can be secured into the case using short metal spacers. If Veropins are used, all the connections to the board can be made after the board has been mounted. Connect the front panel controls, rear panel sockets and input sockets, using short lengths of shielded cable to make the connections to the two inputs and preamp output.

PROJECT: Guitar Practice Amp

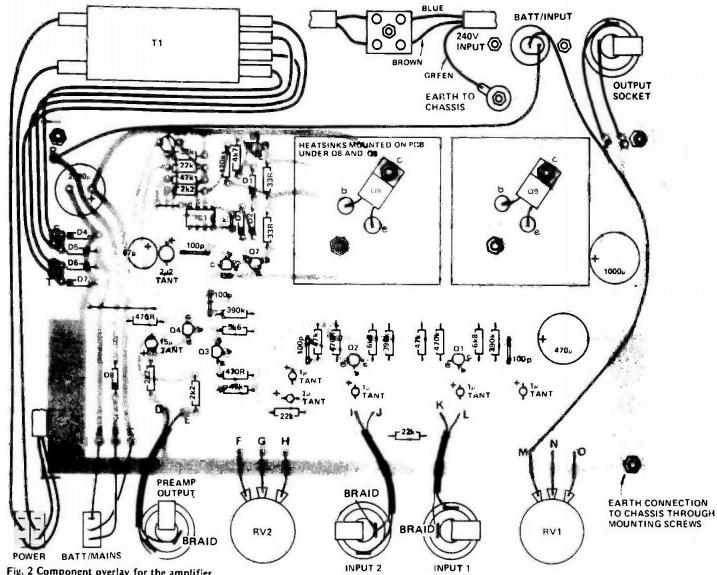


Fig. 2 Component overlay for the amplifier. The original design used a BC639/BC640 complementary pair for Q6 and Q7, and these are shown on the overlay, but they may prove hard to obtain. Consequently the PCB we will be supplying is laid out for a BC140/BC160 pair, which have different pad layouts - the b,c and e pads are etched onto the board for your guidance.

Powering Up
Make a final check of the wiring and PCB. If all is well, apply power. A slight turn-on thump should be heard at the moment of turn-on. If the 'Input 1' volume control is now wound up, some hiss should be heard from the loudspeaker. Do the same check on the other input. There is no set-up procedure since the power amp stage is operating in class B and requires no bias adjustment.

BUYLINES.

Lots of nice, standard, easy-to-obtain components in this project, so you shouldn't encounter any problems with supply. The PCB will be available fro our PCB Service at the price listed on page 44.

PARTS LIST.

Resistors (a	II ½W, 5%)	C16	1000u 25 V PCB electrolytic
R1,5,11	390k	C17	2200u 25 V PCB electrolytic
R2,6,12,20	47k		
R3,7	6k8		
R4,8,14,17	470R	Semicon	ductors
R9,10,19	22k	IC1	LM301
R13	5k6	Q1-4	BC549 or BC109
R15,16,21	2k2		BC557 or BC179
R18	39k	Q5	
R22	120k	Q6	BC140
R23	4k7	Q7	BC160
R24,25	33R	Q8	TIP31
	338	Q9	TIP32
		D1-3	1N914
D-4- 4'-		D4-8	1N4004
Potentiome			
RV 1,2	22k logarithmic		
		Miscella	neous
		SK1-4	mono jack sockets
Capacitors		SK5	DIN socket (or other type —
C1,2,5,6,7	1u0 35 V tantalum		see text)
C3,4,8,15	100p disc ceramic	SW1	DPDT toggle switch (mains
C9	15u 16 V tantalum		rated)
C10	470u 25 V PCB electrolytic	SW2	DPST toggle switch
C11,13	2u2 35 V tantalum	Transform	mer (1-2-0-12-0, 20 VA); TO3 type PCB-
C12	47u 25 V PCB electrolytics		g heatsinks; PCB (see Buylines); case
C14	10p disc ceramic		nounting hardware.

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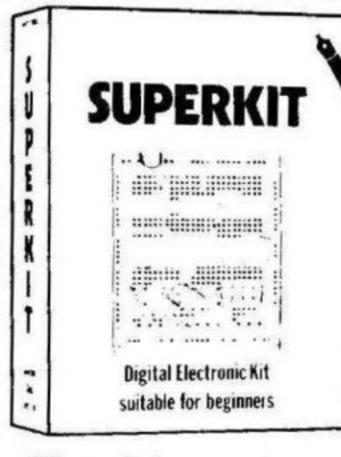
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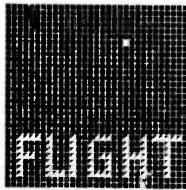
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SWITCHES DIL 3-wy SPST 200 DIL 3-wy SPST 300 DIL	VEHO BOARD (0.1' copper clad)								AF126	25p				250			POTENTIO-
DIL 3 way SPBT		LM13600 140p							AF139	35p						111	METERS
DIL 9 way SPDT 30p					8p LS95	50p											(with 2A / 250)
DIL F vay SPST TOTATY 24/250V OPST 9mm bush REGITARY 24/250V	DIL 3 way SPDT													22p			DP switch) Linear:
Mag	DIL 7 way SPST																47K 470K
Authorst 180			LAIMIST - SOD												2N4061	6р	Log: 5K
April														46p			22K 47K
SLIDE 14/250V PPDT 70 N8555 22b 7818 52b 4023 15p L8251 50b 74110 52b 80119 35b TIPSEB 135b 135b 135b 135b 135b 135b 135b 135b														127n			100K
SLIDE 34/50V DP 3 way or 1A/250V with 1 throw panel cultout 1 to 1652 400m 9705 58p 4025 140 150 150 150 150 150 150 150 150 150 15					7p LS221						BD139						5 for 100p
SLIDE 3A+50V DP 3 way or 1A/250V NESC2 400p NP 3P 58p A027	SLIDE 1A/250V DPDT											35p		50p		Sub	01.105
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0.00 cmm of 10 Mohams E17																	1A/250V
PRESETS (miniature horizontal) TAAS21 280p TAAS21 280p	NESISTONS (MW 5% carbon film)	NE567 160p	7915 62p		111											1	10 for 40p
1000 chms to 1400 htms 5-0 178.65	PRESETS (minute servents)	TAA621 280m				rip;			BC149	7p						1	3A/50V
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According to the property of	100K Linear precision 40 turn 30u				5P 7405	44-1									15A/600V		CERMET
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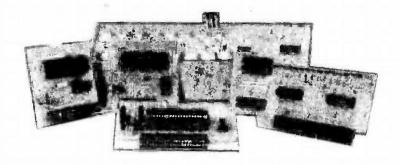
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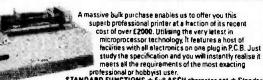
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RIPOLAR Standard, with heatsinks

		DIST	ORTION					
Model Vo	Output power Walts rms	TH.D Typ at IkHz	I M D. 50Hz/7kHz 4 1	Supply voltage Typ/Max	Size mm	Wi gms	Price inc. VAT	Price 8x VA1
HY 30	15w/4 8Ω	0 015%	<0 006%	+18±20	76×68×40	240	€8 28	€7 29
HY 60	30w/4-8Ω	0 015%	< 0.006%	-25:30	76×68×40	240	19 58	£B 33
HY 120	60w/4 BΩ	0.01%	<0 006%	- 35. 40	120 × 78 × 40	410	£20.10	£17 48
HA 500	120w/4-8s?	0 01%	<0.006%	+45±50	120×78×50	515	124 39	£21 21
HY 400	240w/492	0.01%	<0.006%	± 45±50	120 × 78 × 100	1025	£36 60	£31 83

BIPOLAR Standard, without heatsinks

HY 120P	60w/4-8sz	0 01%	<0.006%	+35+40	120 × 26 × 40	215	£17 83	£15 50
HY 200P	120w/4-8Ω	0 01%	<0.006%	+45+50	120×26×40	215	£21 23	€18 46
HY 400P	240w/412	0.01%	<0.006%	+45+50	120×26×70	375	£32 58	£28 33

Protection: Load line momentary short circuit (typically 10 sec.) Slew rate $15V/\mu s$ Rise time $1\mu s$ S/N ratio 100db. Frequency response (-3dB) 15Hz-50kHz. Input sensitivity 500mV rms. Input impedance $100k\Omega$. Damping factor ($8\Omega/100Hz$)>400.

HEAVY DUTY with heatsinks

Model No	Output power Watts rms	DIST TH D. Typ at 1kHz	OATION M D 50Hz/7kHz 4.1	Supply voltage Typ/Max	Sizemni	Wigns	Price inc. VAT	Price ex VAI
HD 120	60w/4-852	0 01%	< 0.006%	+35+40	120×78×50	515	125 85	£22 48
HD 200	120w/4-852	0.01%	<0.006%	: 45:50	120 × 78 × 60	620	£31 49	€27.38
HD 400	240w/412	0 01%	<0.006%	+45+50	120×78×100	1025	£44 42	£38 63

HEAVY DUTY without heatsinks

					120×26×50			
HD 200P	120w/4-812	0 01%	<0.006%	+45+50	120×76×50	265	£27 17	F73 63
HD 400P	240w/452	0 01%	<0.006%	+45+50	120×26×70	375	£39 42	£34 28



Protection: Load line. PERMANENT SHORT CIRCUIT (ideal to disco/group use should evidence of short circuit not be immediately apparent). The Heavy Duty range can claim additional output power apparent). The Heavy Dury range can claim additional output power devices and complementary protection circuitry with performance specs as for standard types

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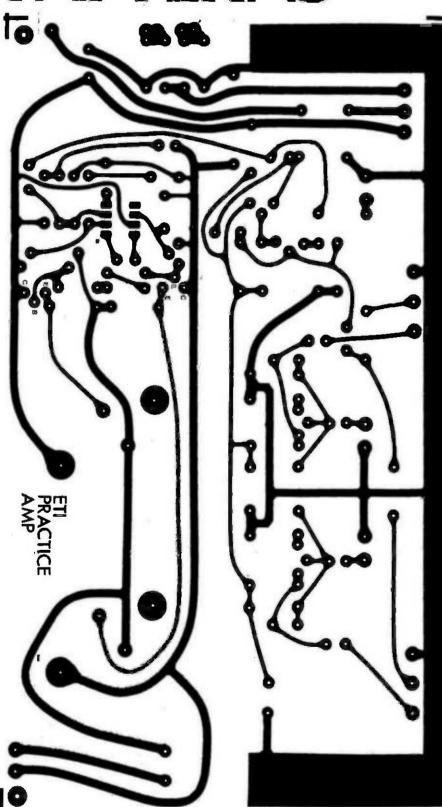
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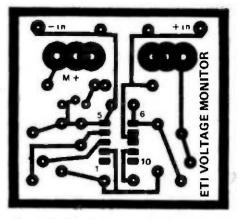
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12p 12p 14p 18p 33p 50p 50p 19p

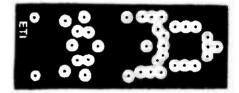
LS02 LS02 LS03 12p 15p 15p

PCB FOIL PATTERNS



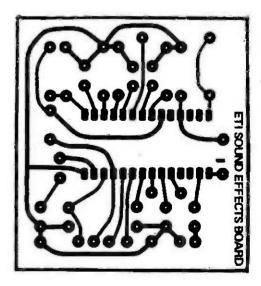


Above: the PCB for the Voltage Monitor.





Above: the two foils for the double-sided 100 MHz High Impedance Probe PCB.



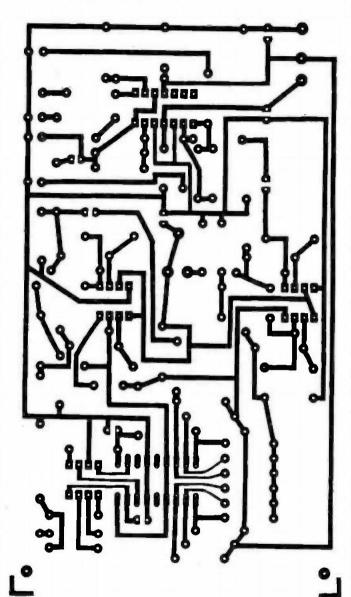
Above: the board for the two sound effects projects,

Left: the board for the Guitar Practice Amplifier. Please note the alteration to the pad layout for Q6 and Q7.

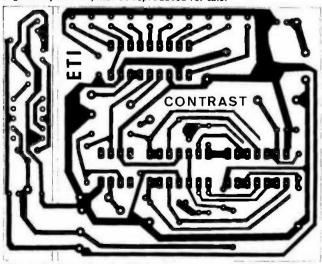
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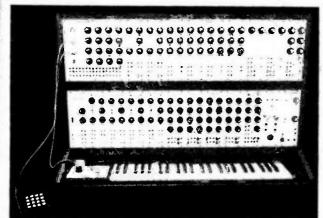
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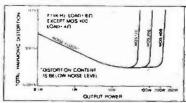
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MOS 400	240w/4Ω	<0 005%	<0.006%	±55±60	120×78×100	1025	€52 20	£45 39

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MOS 120P	60w/4-8s2	< 0.005%	<0.006%	±45±50	120×26×40	215	£26.82	£23 32
					120×25×80			
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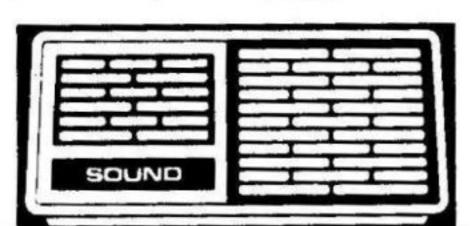
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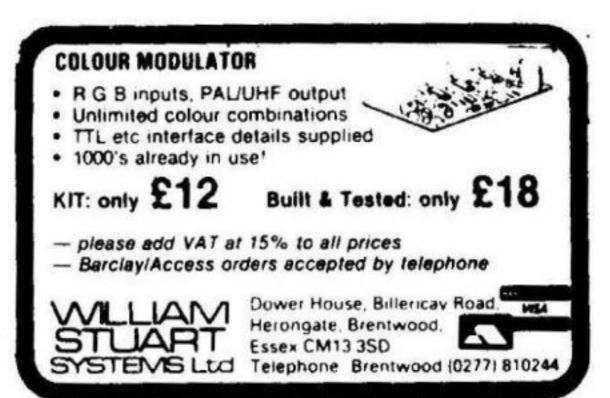
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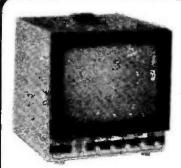
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HY 9	Stereo pre-amp	Two channels mag cartridge, mic + volume control	10 mA	£7.71	€6 70
HY 12	Моло рге-атр	Modes two signals into one, with bass/mid- range/freble controls	10 mA	£7.71	£6 70
HY 66	Stereo pre-amp	Two channels, with Inpuls for mic/mag, cartridge/lape/tuner/auxiliary, with volume/bass/trebie/balance	20 mA	£14.02	£12.19
HY 69	Mono pre amp	Two input channels mag cartridge mic, with mixing and volume/treble/bass controls	20 mA	£12 02	£10 45
HY 71	Dual stereo pre-amp	Provides four channels for mag_cartridge/mic with volume control	20 mA	£12 36	£10.75
HY 73	Guitar pre-amp	Provides for two guitars (bass + lead) and mic with separate volume/bass/freble and mixing.	20 mA	£14 09	£12 25
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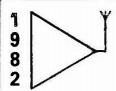
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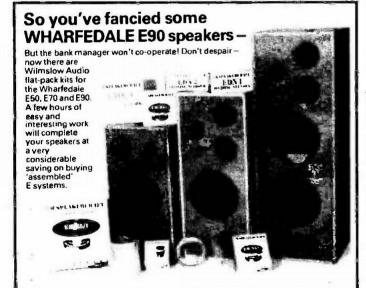
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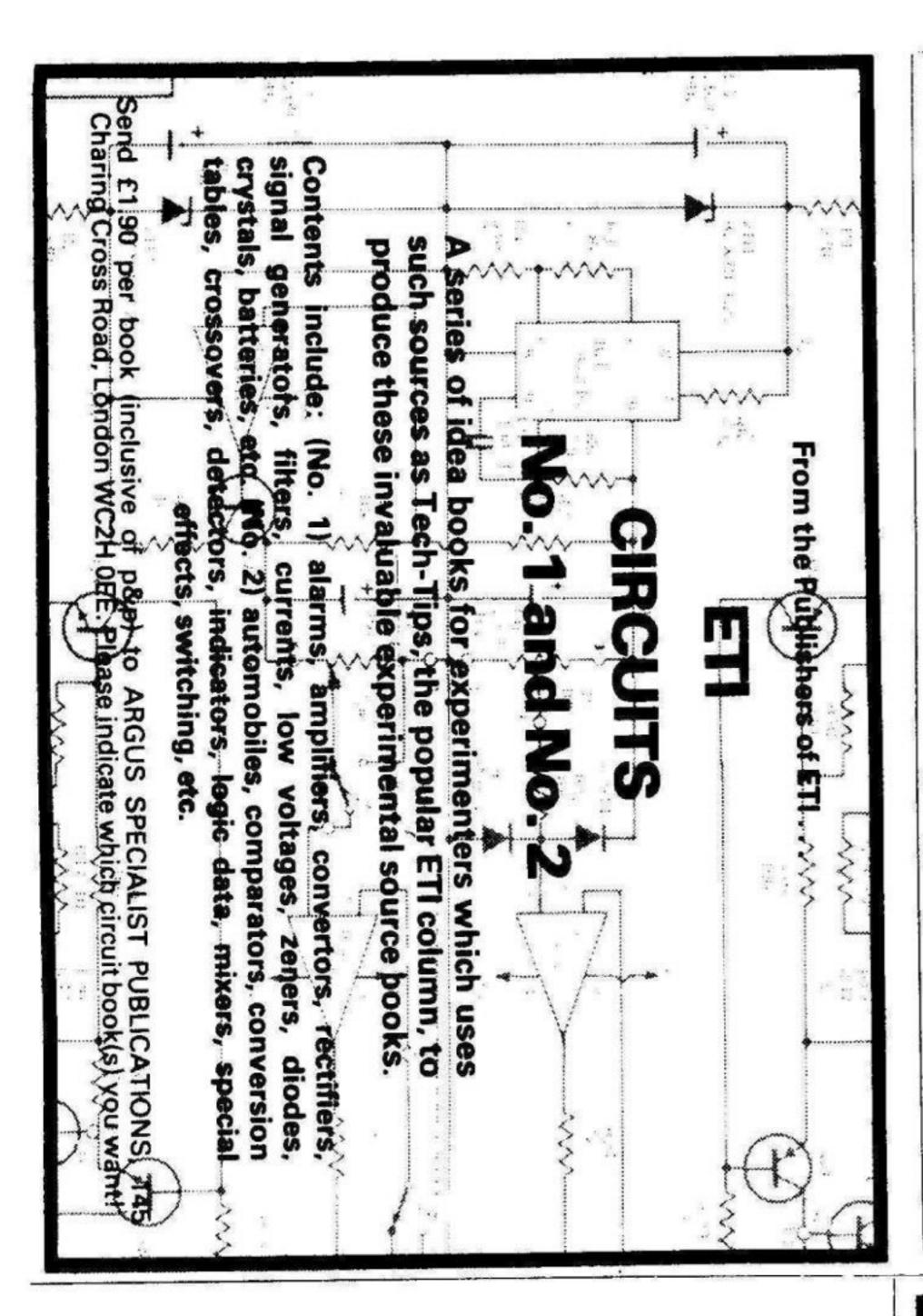
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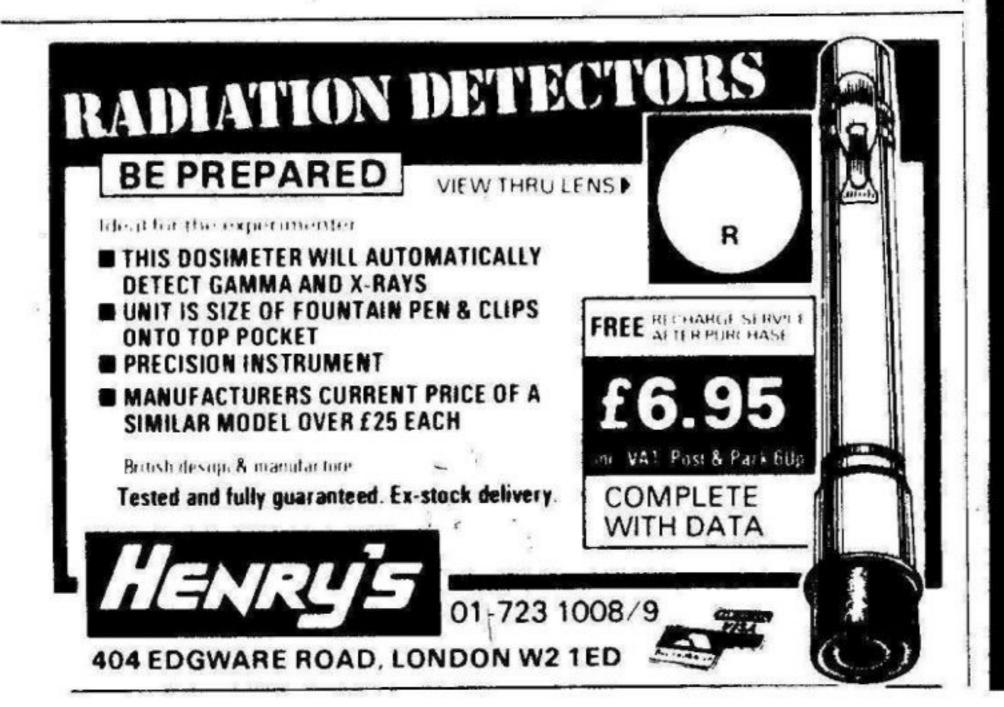


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MÉTEORS-your starship is cruising through space when you meet a meteor storm. How long can you dodge the deadly danger?

LIFE - J.H. Conway's 'Game of Life has achieved tremendous popularity in the computing world. Study the life, death and evolution patterns of cells.

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GOLF - what's your handicap? It's a tricky course but you control the strength of your shots.

Cassette 2-Junior Education: 7-11-year-olds For ZX81 with 16K RAM pack

CRASH-simple addition-with the added attraction of a car crash if you get it wrong.

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TRAIN-multiplication tests against the computer. The winner's train reaches the station first.

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COMBAT - you're on a suicide space mission. You have only 12 missiles but the aliens have unlimited strength. Can you take

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Cassette 5 - Junior Education: 9-11-year-olds For ZX81 (and ZX80 with 8K BASIC ROM)

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