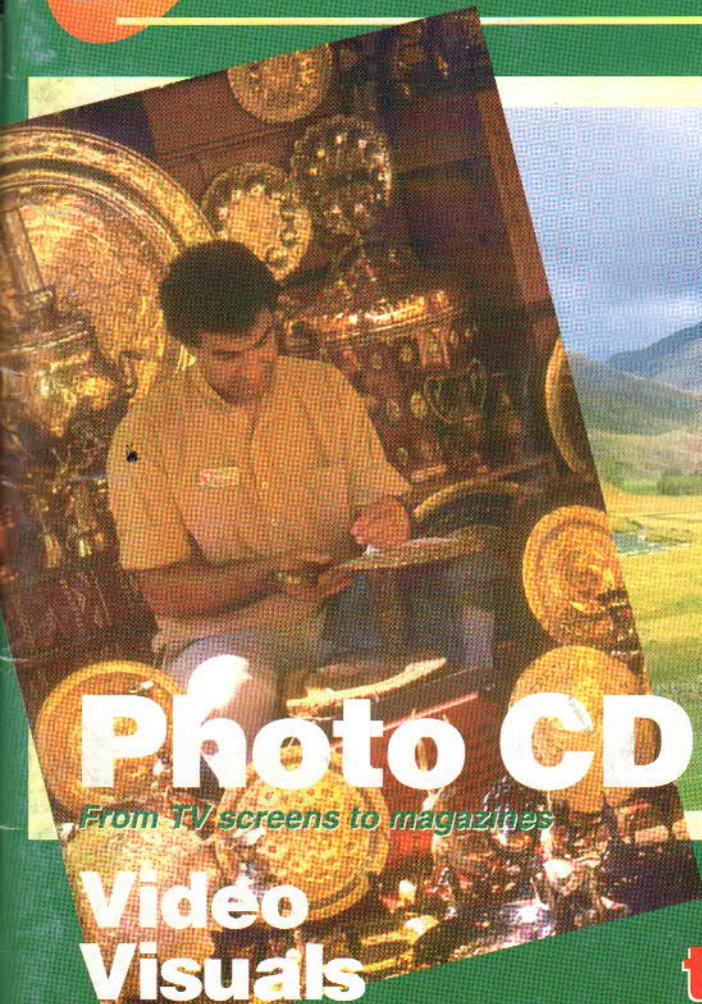


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**SCHOOL STRIPPERS** We have quite a few of the above units which are 'returns' as they are quite comprehensive units they could be used for other projects etc. Let us know how many you need at just 50p a unit (minimum 10).

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**FIBRE OPTIC CABLE** Made for Hewlett Packard so pretty good stuff! you can have any length you want (min 5m) first 5m £7 REF: MAG7 thereafter £1 a metre (ie 20m is £22). REF: MAG1 Max length 250m.

**SNOOPERS EAR?** Original made to clip over the earpiece of telephone to amplify the sound-it also works quite well on the cable running along the wall! Price is £5 REF: MAG5P7

**DOS PACKS** Microsoft version 3.3 or higher complete with all manuals or price just £5 REF: MAG5P8 Worth it just for the very comprehensive manual! 5.25" only.

**DOS PACK** Microsoft version 5 Original software but no manuals hence only £3 REF: MAG3P6 5.25" only.

**FOREIGN DOS** 3.3-German, French, Italian etc £2 a pack with manual 5.25" only REF: MAG2P9

**MONO VGA MONITOR** Made by Amstrad, refurbished £49 REF: MAG49

**CTM644 COLOUR MONITOR** Made to work with the CPC464 home computer. Standard RGB input so will work with other machines. Refurbished £59.00 REF: MAG59

**JUST A SMALL SELECTION** of what we have - to see more get our 1994 catalogue (42p stamp) or call in Mon-Sat 9-5.30

**HAND HELD TONE DIALERS** Ideal for the control of the Response 200 and 400 machines. £5 REF: MAG5P9

**PIR DETECTOR** Made by famous UK alarm manufacturer these are hi spec, long range internal units. 12v operation. Slight marks on case and unboxed (although brand new) £8 REF: MAG8P5

**WINDUP SOLAR POWERED RADIO** AM/FM radio complete with hand charger and solar panel! £14 REF: MAG14P1

**COMMODORE 64** Customer returns but ok for spares etc £12 REF: MAG12P2 Tested and working units are £69.00 REF: MAG69

**COMMODORE 64 TAPE DRIVES** Customer returns at £4 REF: MAG4P9 Fully tested and working units are £12 REF: MAG12P5

**COMPUTER TERMINALS** complete with screen, keyboard and RS232 input/output. Ex equipment. Price is £27 REF: MAG27

**MAINS CABLES** These are 2 core standard black 2 metre mains cables fitted with a 13A plug on one end, cable the other. Ideal for projects, low cost manufacturing etc. Pack of 10 for £3 REF: MAG3P8 Pack of 100 £20 REF: MAG20P5

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**MICROWAVE TIMER** Electronic timer with relay outputs suitable to make enlarger timer etc £4 REF: MAG4P4

**PLUG 420?** showing your age? pack of 10 with leads for £2 REF: MAG2P11

**MOBILE CAR PHONE** £5.99 Well almost! complete in car phone excluding the box of electronics normally hidden under seat. Can be made to illuminate with 12v also has built in light sensor so display only illuminates when dark. Totally convincing! REF: MAG6P6

**ALARM BEACONS** Zenon strobe made to mount on an external bell box but could be used for caravans etc. 12v operation. Just connect up and it flashes regularly! £5 REF: MAG5P11

**FIRE ALARM CONTROL PANEL** High quality metal cased alarm panel 350x165x80mm. Comes with electronics but no information £15 REF: MAG15P4

**SUPER SIZE HEATSINK** Superb quality aluminium heatsink. 365 x 183 x 61mm. 15 fins enable high heat dissipation. No holes! £9.99 REF: MAG10P1P

**REMOTE CONTROL PCB** These are receiver boards for garage door opening systems. You may have another use? £4 ea REF: MAG4P5

**LOPTX** Line output transformers believed to be for hi res colour monitors but useful for getting high voltages from low ones! £2 each REF: MAG2P12 bumper pack of 10 for £12 REF: MAG12P3.

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REF: MAG50

ISSUE 3 VOLUME 1

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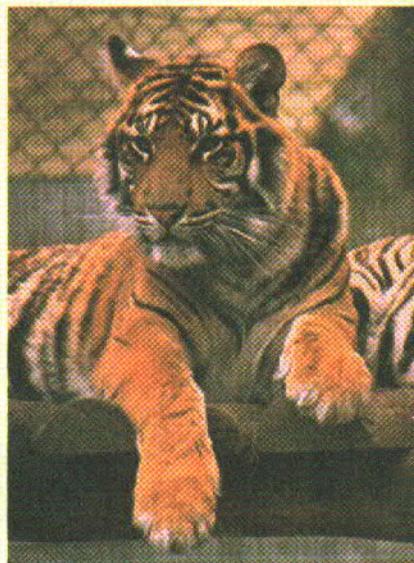
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# ...of CDs and Electric Transport

In this 'CD' issue we have some goodies to give away, namely over 100 4D audio Compact Disc recordings from Deutsche Grammophon with over 72 minutes of recorded music and Two Kodak Photo CD/audio players. Our feature on Photo CD demonstrates the processes and the hoped-for popularity at home and in the commercial sector of this latest technology.

To take part in the competition for the CD players we suggest you turn to page 12 and for more information on how to get your free CD take a look at the 4D article on page.

## Electric transport

It has long been the dream of many entrepreneurs to produce the electric car with equivalent performance characteristics of an internal combustion engine fuelled by petrochemicals. The attractions in today's ecological climate are obvious, but it seems the researchers are finding it more difficult to progress along conventional development lines. The results of this show only small increases in usable car range and 'the outage time' for electric refuelling has been a huge sticking point.

Although the Oxford project for placing a few electric buses onto the streets has to be applauded for the minor inroads made to cleaning up our cities, it has no major technological advances to offer. Let's hope the initiative will pay off.

**Paul Freeman-Sear**

# NEWS



## Inmarsat high speed datalink

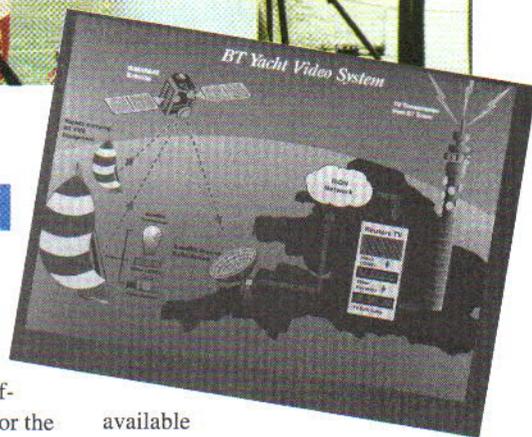
British Telecom Martlesham Heath has rolled up its sleeves to provide two state-of-the-art transmission systems for the Whitbread Round The World Yacht Race.

Inmarsat-C satellite terminals, part of a tracking and information system tested last year in the British Steel Challenge Race, are on each yacht, linked to Global Positioning System (GPS) receivers. The yachts transmit their positions six-hourly via the Inmarsat to the Race HQ in Southampton. British Telecom software then compares the new position with previous information to compute course and speed.

The GPS is accurate to about 50 metres, so that yachts can be individually tracked even in a group.

The energy-efficient transceivers draw a mere 15 watts and provide two-way communication more reliably than HF radio in high southern latitudes. A "panic button" can be pressed to send an alert to rescue services in an emergency.

For the first time, high-quality TV footage from the yachts will be



available almost - if not quite exactly - as it happens. Ten of the 15 yachts carry advanced custom electronics to convert video camera signals to compressed digital data for transmission via an Inmarsat-A High Speed Data (HSD) link.

The pictures are compressed on a specially adapted BT videoconferencing codec at 384 or 768 Kbits per second and stored in the codec's computer. In favourable conditions, the picture files are transmitted at 64 kbit per second via the Inmarsat link.

Normally TV pictures sent via the high speed data pathway, 2000 times narrower than usual for TV transmission, would not be of broadcast quality. But taking around 12 minutes to send a compressed two-minute video clip allows the narrow-band high-speed link to send the picture data to another codec at Reuters TV in London, where it is uncompressed and played out at its original coded rate for editing or immediate transmission.

Every care is taken when compiling the magazine. However, the publishers cannot be held legally responsible for errors in the magazine or from loss arising from those errors. Any errors discovered will be published in the next available edition of the magazine.

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# Eurosats TV Wrangle

For years, European bureaucrats and broadcast companies have been wrangling over which satellite broadcasting format will be the European standard. In the meantime, those companies who couldn't afford to wait and see which way the wind was blowing have got on and used the best standard available. There were arguments about what that was, too, but the then-Sky TV, satellite operator SES, and Canal Plus went ahead using PAL-type transmission standards, using a telecomm satellite which was not covered by the EC directives. The rest is history.

The European Commission eventually came up with the D2-MAC standard (after the D-MAC standard, a leading contender in earlier discussions) and tried to enforce it in the industry,

offering grants for the transition period and hoping that it would provide the basis for wide-screen broadcasting (expected to start in 1994) and high definition television (HDTV) arriving in 1995. But they delayed too long, and satellite tv was already a fact.

Now it looks as though the wrangling is at an end. Recently 80 European companies signed an agreement to co-operate with each other in the search for a standard agreeable to all of them, without the intervention of the European Directive, any Commission money, or further delays. The European Launch Group (ELG) accepts that de facto standards are already in use and that future developments will need to dovetail with these, starting with digital television and following with HDTV. Membership and participation in the group is voluntary, so there will be no enforcements to distract operators from their primary aim of broadcasting, but everyone recognises

the need to avoid VHS/Betamax-type format wars wherever possible in the very cost-intensive environment of international broadcasting.

The UK has more representatives signing than any other country. Japanese companies with manufacturing facilities in the UK, including Sony, JVC and Toshiba, have signed, which is a good omen for development and manufacturing of new systems in the UK. Amstrad, Pace and Cambridge Industries, major receiver suppliers, have signed, indicating that they both expect to stay with satellite broadcasting as it developed. British Telecom is absent, but it is felt to be unlikely that they will be totally uninvolved.

It's been reported that the US counterparts of the European satellite companies are not forging ahead in drawing up their own standards. If Europe can get its act together, it may find itself with a marketable technical lead in the field.

## Electric buses for Oxford

The city of Oxford, like many busy modern towns with medieval town centres, has a car problem. The citizens want cars out of the city centre, and visitors want to get in and out without running themselves ragged in the process. It's a long-term problem.

A recent strategy, small scale but interesting, is the introduction of four fully electric buses on the round-town and station routes. The first vehicles of their kind in the UK, the buses hold 18 passengers each, have a top speed of 40mph, and no diesel fumes. The project

is a joint initiative between Southern Electric and Oxfordshire County Council. The buses were designed by electric vehicle specialists International Automotive Design of Worthing and built to the long-wheelbase Optare MetroRider spec by Optare of Leeds.

The batteries, used in packs of six and specially made for the project, will recharge overnight at the bus depot and more importantly, with a full recharge time of 12 hours and a range of only 55 miles - will top-up at a special charger alongside Oxford railway station,

whence they will be collecting many of their fares. Regenerative braking will also help to keep the batteries running. Use of cheap-rate electricity should cost the buses about 4p per mile, allowing a flat-rate 30p fare, cheaper than the current minimum on many Oxford hopper buses. Headlights, indicators and the other interior electrics run on a standard 24V lorry battery as normal.

It's hoped that the new buses will speed up passenger circulation in the city centre and improve communications with the railway station, vital in a city which encourages visitors and shoppers but actively discourages cars. The city's extensive park-and-ride facilities were described by a denizen of the local countryside with deliberate irony as "an adventure". Anything which makes Oxford access less adventurous will be welcomed.

Oxford has changed its tune in the last 70 years since poet A D Godley wrote, in 1914, on meeting the first buses roaring up the High Street:

Et complebat omne forum  
Copia Motorum Borum.  
How shall wretches live like us  
Cincti Bis Motoribus?  
Surrounding itself with Omnibuses  
now seems to be Oxford's hope for the future.



## Graphical user interfaces for the blind

In the process of investigating the necessity for making computer graphical user interfaces accessible to blind and partially-sighted computer operators, the European project "Textual and Graphical User Interfaces for Blind People (GUIB)" has developed a keyboard/terminal which integrates synthesised speech, braille, and non-speech sound signals. The project's efforts to represent the intensely visual, highly-packed information-carrying nature of graphical user interfaces is still in an experimental stage but enough progress has been made to fill a booklet, *Access to Graphical User Interfaces*, by John Gill, summarising the research so far.

GUIs are rapidly becoming more popular with computer operators, especially those who have never interacted directly with the operating system, or who found the strings of text commands needed too difficult to remember. Unlike a decade ago, most of today's users are non-specialists glad to have a set of icons standing between them and the operating system. Unfortunately, working in text has a big advantage for non-sighted operators: it can be rendered quickly in audible speech. This is not the case with graphics, and blind or partially-sighted users are finding that they need the help of colleagues or other work-rounds to interact with GUI screens. Often they are unable to do so.



## Cellphone contract

All the signs are that Mitsubishi does not expect its portable cellphones to slow down. The company has just signed up former Grand Prix racing driver and BBC Grand Prix commentator Jonathan Palmer's

The GUIB project has looked into the use of different, symbolic, partially symbolic, or simply easily differentiated abstract sounds to represent the screen contents and the position of the mouse pointer as it moves around the screen. One experiment has involved a "sound screen" of five small loudspeakers to position a sound signal according to the position of the mouse pointer on the screen. Trials have found that three-dimensional sound space, now in common use in virtual reality systems, differentiates sounds better and gives a stronger indication of position, even though the visual image is apparently only two-dimensional.

### Applied design at the front end

One aim of the project is to develop a method which can be applied to new GUIs as they appear, instead of waiting for each package to become established and then developing a translator for it. In the waiting period, visually disabled operators could fall behind a reasonable operating speed and lose work and their jobs. The project is funded by the Commission of the European Communities, involving organisations from six European countries, including the RNIB in the UK. Research however is also being drawn from the USA, where many of the GUIs are written, and

dealership for its telecomms products. The already-bruised award-winning MT-7 and a new relation, the MT-8, out later this year, are included in the agreement. The dealership, Jonathan Palmer FOneTime, is a new division of the IPM organisation. The telecomms division will operate nationwide service on portables and transportable telephone systems, with aftersales service and backup alongside Mitsubishi, and possibly installation and backup at a later date.

Jonathan Palmer is now with the McLaren racing team, working on the 231 mph McLaren F1. Jonathan Palmer PromoSport has evolved the Cellnet Driver Challenge road safety promotion competition, which tried the driving skills of 3000 competitors last year. The MT-7 analogue ETACS cellphone was one of the first in its field to offer the TACS-2 specification, and PIN code identification against unauthorised use. Trophy winner in the call security section of the Cellnet Caesar Awards, the MT-7 also won two Merit prizes, including one for user documentation. Next: the World Land Speed Record?

and Japan.

The booklet is available from the Royal National Institute for the Blind, 224 Great Portland Street, London W1N 6AA.

## More powerful DSP chips

Analog Devices' new ADSP-21060 single-chip digital signal processor is being announced as industry's most powerful 32-bit DSP to date, a fully-integrated, high-performance, floating-point signal computer. The first DSP available in the Super Harvard Architecture Computer (SHARC - And yes, there is a fin on the logo) class, the ADSP-21060 is out to tear off its chunk of the market before the crowd gets there, flashing an impressive array of features. Built around the high-speed ADSP-21020 floating-point core, a dual-port 4-megabit SRAM with two serial ports, and external parallel port and a 10-channel direct memory access I/O controller, the ADSP-21060 carries a very high I/O bandwidth alongside very fast data processing. When the 3.3 volt versions is available, the total power consumption of the system will be less than current computers.

Super Harvard Architecture is a step up from DSP/Harvard Architecture and effectively allows multi-chip functionality on a single chip to a higher degree than before. The new DSP is reckoned to deliver two to ten times for performance of current top-end signal processing chipsets, and can link up to six ADSP-21060 units "gluelessly" with one host, cutting the need for interfacing logic.

## Applications

The new chip is being aimed particularly at communications, speech, audio and video applications in the growing demand for digital comms, but graphics imaging, number processing and instrumentation get a mention as well. Interestingly, Analog Devices' cost comparisons show a higher initial cost for the chip over other top-end DSP chips, but a lower overall cost for a complete system, supported by the large number of peripheral functions integrated onto the chip. The specification includes instruction

# Land Speed record challenge by electric vehicle

Four GCSE pupils from St. Richard's RC School in Bexhill-on-Sea, Sussex are attempting to break the land speed record for lightweight electric vehicles with a car they have developed themselves. The team have received technical help and support from Lotus and the Motor Industry Research Association, which opened its aerodynamic wind-tunnel to test and adapt the car's streamlining.

Test driver Rudy Thomann of Lotus

will be driving the car, which reached 120 mph during test drives at Greenham Common. The record for electric vehicles below 500kg is 100.242mph, so the St. Richard's car seems set to walk it.

The car uses thin-plate lightweight lead acid batteries by Deta. The car's 60 horse-power, 96-volt Nelco motor draws 600 amps and takes virtually the whole charge from the battery in 70 seconds, giving the engine a 30 percent extra kick of power.

execution time of 25 nanoseconds, 40 MIPS processing speed with peak MFLOPS of 120 (80 sustained), and 128K internal RAM, in 1.59 square inch surface-mount package. For layout engineers, that's 74 MFLOPS per square inch, double the capacity of the nearest competitor.

One application which may benefit from fast, highly integrated processors like the ADSP-21060 is real-time speech recognition by computers, with all that implies for man/machine interaction, speed and remote control.

# Cellphone falls off motorbike and lives - Batteries don't

It seems that the much-unloved portable cellphone is expected to undertake tougher assignments than sitting in a first-class carriage with a yuppie annoying fellow-travellers these days. For instance, a Mitsubishi MT-7 portable, already an award-winner for other aspects of its performance, survived an unscheduled exit from a motorbike on the fast lane of an unnamed motorway in the British Isles.

It appears the article, pocketed by its owner, biker/businessman John Caudwell, accidentally eased its way out of his leather racing suit as he zipped along the fast lane.

The phone bounced several times before - fortunately - coming to rest on the hard shoulder, from which its owner was able to retrieve it, no doubt in the process of trying to ring its maker to ask for a transfer. The LCD covering was smashed, the antenna was kinked, the casing severely gouged. When we saw the photograph we thought - they've dropped that one! The mast and battery

were never recovered. But still the phone leapt into life when connected to a new battery.

Now we discover that Caudwell Communications is the UK's largest cellular phone distributor. They should know something about the machinery's survival rate in the field. Says John Caudwell: "The toughness, durability and performance capabilities of the Mitsubishi phone speak for themselves. The MT-7 survived a gruelling test, the result of which is most amazing." It might be tempting fate a bit to put this into the advertising, but it's nice to know that



next time you hurl your telephone at the wall, it stands a good chance of bouncing back to you.

The only Achilles heel seems to be - as ever - the battery technology. Perhaps a little more work on keeping the module locked in place.

# Signal to NOISE

A selection of your views and thoughts

I am new to Electronics in Action and therefore wish to comment. I find this monthly very stimulating, remember I am 69 years old and have been in electronics all my life, and I welcome a change of monthly. I thoroughly agree with the letter about teaching science. I could add more such thoughts, the bright scholars are led into the Arts such that they can attain more GCSEs more easily and enhance the name of the school. We need more champions of electronics to enthuse people!

On a different note, can I ask for articles on organ voices, I have programmed many of these on synthesizers, and have constructed many formants but I cannot as yet obtain a voice anything like the Wurlitzer or Blackpool organ. I find all magazines ignore this area. Perhaps you might mention why.

**H W C Hollings**  
Witney  
Oxon

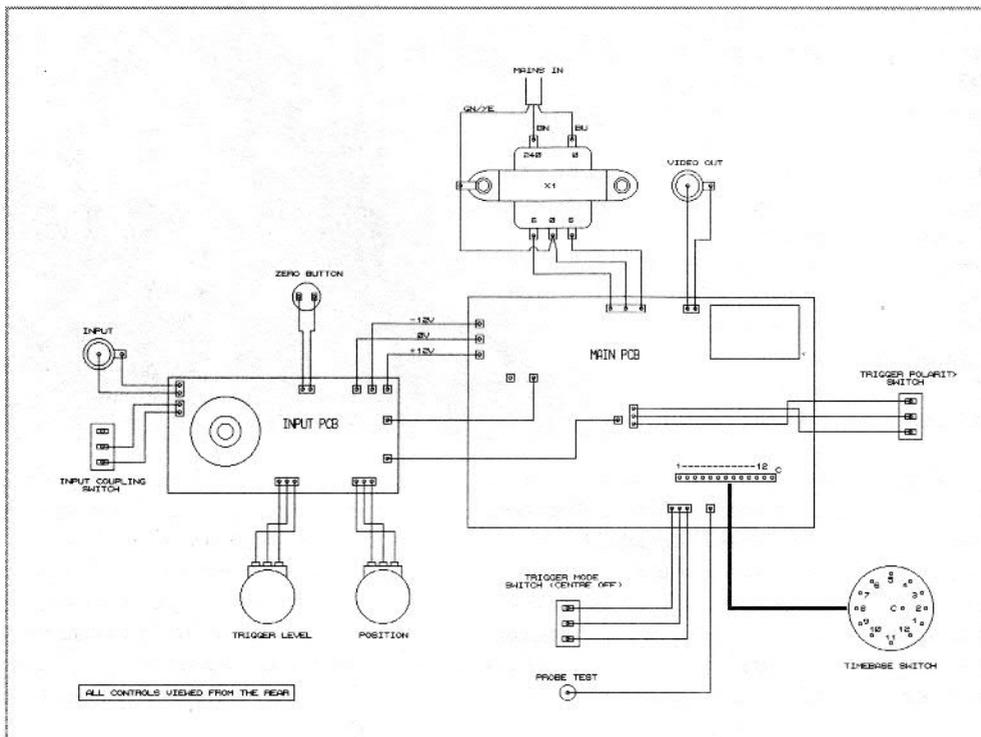
*Thank you for your comments. I have also spent some time in teaching and I'm afraid the answer to why more young people go for the Arts, apart from the financial incentive, is deep rooted. It certainly does not help to have the vast majority of politicians with an Arts based education totally ignorant of Science and Technology. The course of British society tends to lead from those that govern us. Given the right incentives, science presented in a stimulating way in schools can lead to far more exciting challenges and new discoveries. Taking a sideways look at our world in the way it works instead of taking the established way of conservative development could, in the words of the now famous phrase 'boldly go where no man or woman has gone before'- or should I say go boldly....?*

*On to your other point, we could have the answer to your question when we ask 'our man from Yamaha' to come up with a solution. Hold on for a few editions and we will see what can be done .....unless of course any reader out there has some answers. - Ed.*

I have enjoyed reading your magazine especially the test equipment section as I am taking my CG Part 2 year two and I need just the right type of equipment as you have had in your magazine in the last two issues.

I only took up electronics as I was classed disabled and I like helping old age pensioners with their electrical problems that are within my scope. I really like the telescope idea and I am thinking of building one for my own use. Keep up the good work especially the test equipment and you will have a loyal reader for all your future issues. Good Luck to you.

**K G Pullen**  
Swansea



Owing to unforeseen circumstances the interwiring diagram for The Telescope (featured in our October and November issues) was omitted. We apologise for this oversight and reproduce it here.



**Helen Armstrong reports on the growing attraction of seeing pictures on 'CD'**

**L**ike 110mm film, electronic stills photography was a great idea which signally failed to ride 35mm off the range. New formats often survive their inception to fill a niche - even a major niche - but only a few become popular standards. Philips Compact Cassettes were a success in the audio field from the early '70s. Since then, only Compact Disc - another Philips project - has made it as a 'must have' audio format.

So what have CDs to do with stills photography? More to the point, what have audio CDs to do with stills photography? Dodging the latter question for now, it's possible that photographic compact disc, or Photo CD, by its Kodak name, could become the next popular photo format. One: Compact Disc has proved itself in one medium already; two: Photo CD has one foot firmly in a very established camp - it employs standard 35mm film and ordinary mechanical cameras as its picture source.

The difference is that the developed images can be stored digitally - on a Photo Compact Disc - or made into prints in the usual way. You can opt for either or both from the same set of negatives or slide transparencies. The images are scanned to a very high resolution, so good-quality thermal enlargements can be taken from the PCD files as well. And while PCD Players, which provide the output signal for televisions, need to be matched to local TV standards, the discs (unlike video-tapes) do not. A PCD can be played anywhere.

**Everyone smile for the Compact Disc**

Photo CD Players are designed for connection to domestic televisions, but discs can also be read by Compact Disc Interactive (CD-I), and by certain CD-ROM players for interfacing to a computer. The standards referred to are the CD-R (recordable CD) 'orange book' standard for CD recording and CD-ROM-XA (Extended Architecture) 'bridge' standard on delivery. The aim is flexibility of use on present and future viewing media. To this end - Kodak thinks of it as 'future-proofing' - each image is stored in five different image files allowing increasing resolutions. To further maximise storage efficiency, each file draws data from the lower ones, instead of duplicating. The net effect is that a television can display the images at its own maximum resolution - the best that can normally be achieved by video camcorders and Electronic

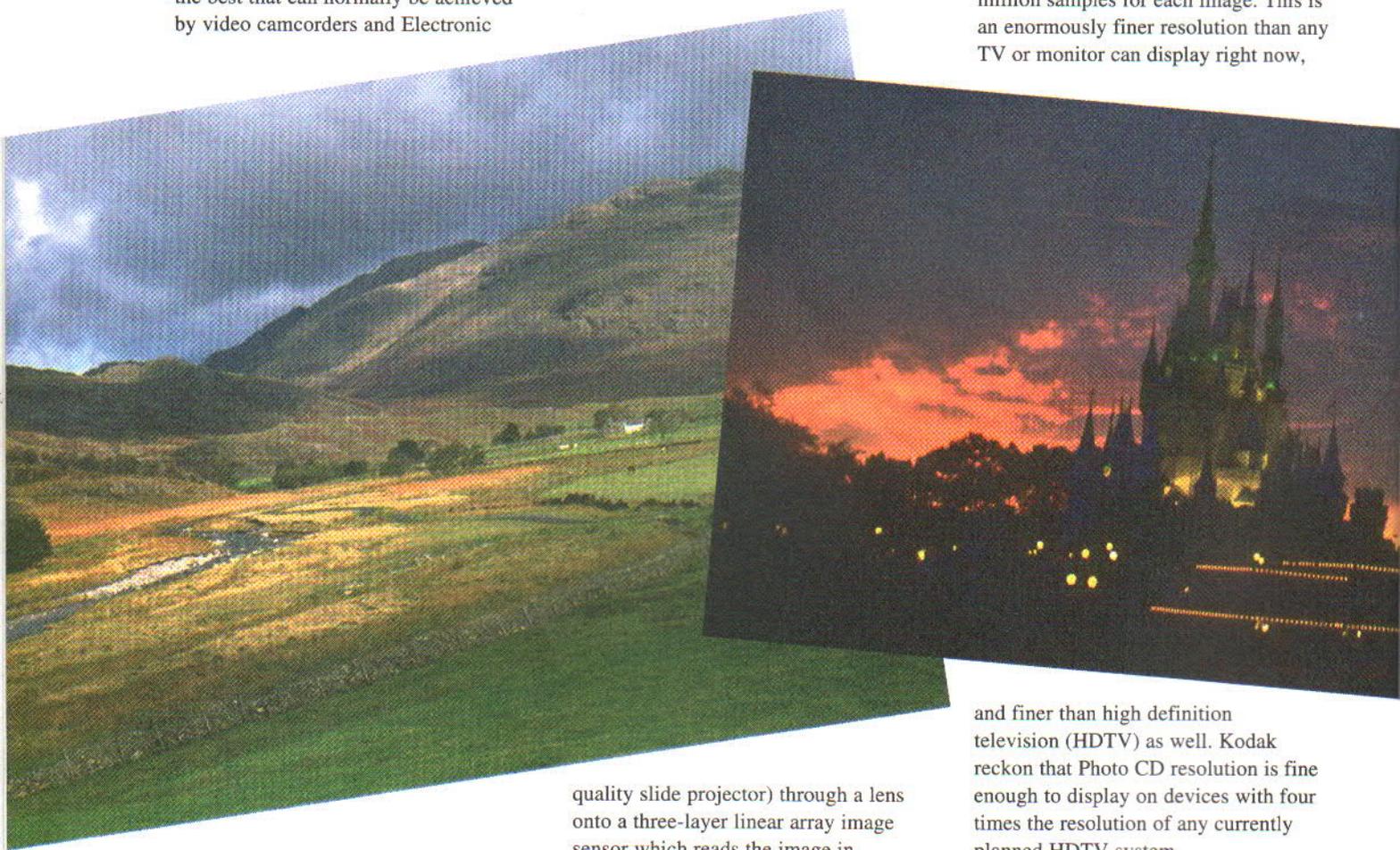
begins after the 35mm film has been processed into negative or slide strips in the normal way. This is different from disk- or ramcard-based photography, where the pictures are video-encoded and can be played back immediately, but it has a considerable advantage in quality. 35mm film originals give a much higher-resolution than video or current image-sensor photography, and the image-transfer allows a high standard of accuracy, with colour balance adjustment where needed, substantially capturing the photographic quality of the original.

### Primary Hues

The film is scanned in a PCD Film Scanner, projected (this part of the machine is like a self-contained high-

groups of three density values between 1 and 256, one each for R, G and B, are allocated to each pixel (picture element).

Digital sampling divides up the information contained in the analogue original into fine slices or packets ('quantisation'). Quantised data is stored in bytes of memory. One byte can only contain so much detail, so the more finely the information is divided, the less information each byte will have to carry and the more precisely each detail can be defined. PCD scanning samples a 35mm image on a grid of 3,072 pixels across by 2,048 vertically, giving over 6 million pixels over a postage-stamp sized area. The RGB is in three separate layers, each with 6 megabytes of colour intensity information, giving over 18 million samples for each image. This is an enormously finer resolution than any TV or monitor can display right now,



Stills Cameras - but as higher-resolution formats arrive, the same images can be displayed at higher resolutions. Photo CD intends to be robust in a world where formats come and go like yo-yos.

In fact, the format has been around for a couple of years, but early 1994 expects a considerable extension of processing facilities, which will in eventually turn Photo CD into a 'mini-multimedia' format which can be customised with sound and text to order.

The electronic processing only

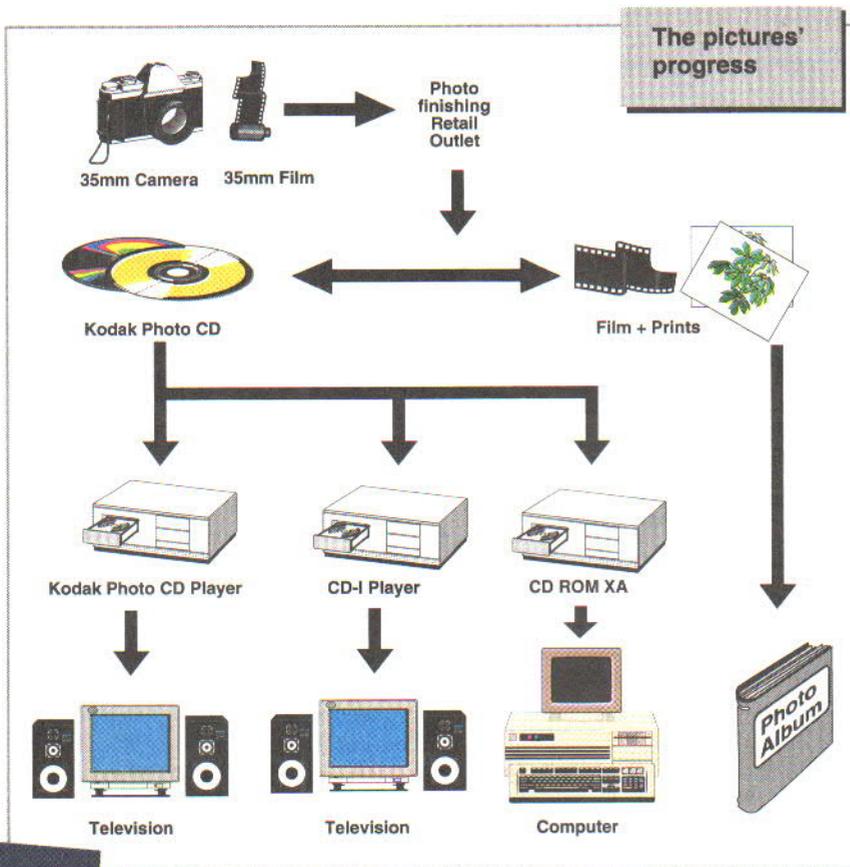
quality slide projector) through a lens onto a three-layer linear array image sensor which reads the image in horizontal lines of red, green and blue densities. (The density is the intensity value of the colour in question.) The scanner reads the additive (projected light) primaries red, green and indigo (blue), rather than the subtractive (colour pigment) primaries, magenta, yellow and cyan, used for printing. A television set uses the RGB primaries (coded in a rather different form) to build up its picture.

As the analogue film image is sampled and quantised into bytes,

and finer than high definition television (HDTV) as well. Kodak reckon that Photo CD resolution is fine enough to display on devices with four times the resolution of any currently planned HDTV system.

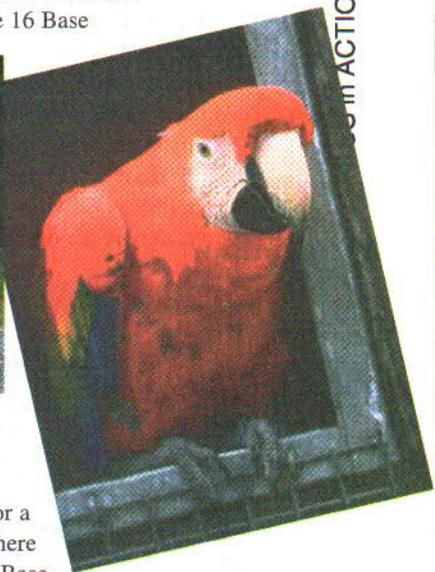
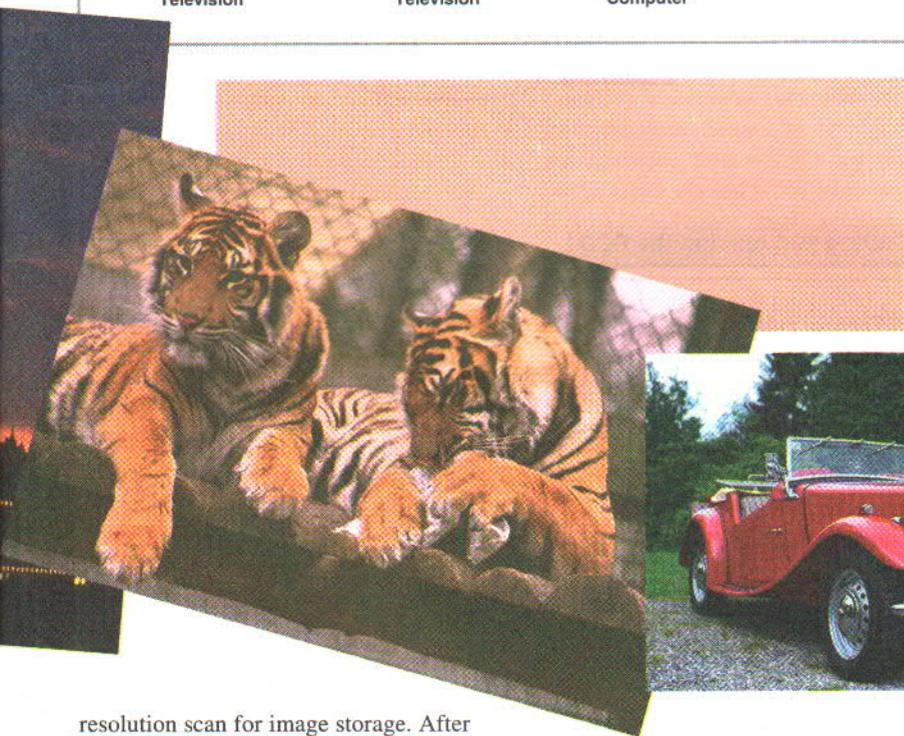
Because the picture information is stored digitally as groups of numeric values, signal distortion is kept to a minimum, and each playback or reproduction is as exact as the previous one. CDs are no longer thought to be virtually immortal, but they do have very good survival capabilities.

The Photo CD scanning process actually makes two scans, a low-resolution scan for checking, for example, whether the image is horizontal or vertical, and a high



Television passed historically through a luminance-only stage before colour signals were added, so the PhotoYCC format can produce output signals in composite video (broadcast television), S-Video (Y/C, higher-quality video) or RGB (higher-quality video and computer monitor) signals.

The data for each image is then 'packed' into batches of five files offering increasing resolution depending on the use of the image. 16Base (3.14 megabytes, compressed), for thermal prints and high quality enlargements; 4Base (.62 MB, compressed), for HDTV; Base (.563 MB, uncompressed) with 512 lines of 768 pixels, for TV and monitor display; Base/4 (.141 MB) for low resolution display, and Base/16 (.035 MB) for 'thumbnail' display. The files are stored hierarchically: the Base file is the central building block, and the more detailed 16 Base and 4 Base files draw some information already stored in files below them, saving memory space. Compression to about 25 percent of the original file size allows quick retrieval of the image. Greater compression would need more complex algorithms, more processing time (and more complex and more expensive machinery) and carry a greater risk of data loss. The compression allows each disk to store around 100 still images. Only the highest two files are compressed: the 16 Base



resolution scan for image storage. After scanning, the information is passed to the PCD Data Manager, a dedicated workstation based on a Sun Microsystems computer. Software in the Data Manager uses an automatic colour balance algorithm to check and correct the images for overall exposure and colour balance. At this stage, custom processes like cropping, zooming, rotating and other image manipulations - montaging or adding text and graphics - can be done on request. The images are then recorded onto the Photo Compact Disc.

The colour encoding uses a Kodak-developed scheme called PhotoYCC

which takes the 12-bit RGB data from the PCD Reader and splits it into luminance (Y, the monochrome brightness scale, which the human eye is most sensitive to, and which carries most of the image detail) and chrominance (C, colour) information at 8 bits per channel. Separating the Y and C allows maximum file compression in areas carrying the minimum detail. The dynamic range (difference between the lightest and darkest details) captured by the system is reckoned at 350:1 or better, far more than is needed for any current video system.

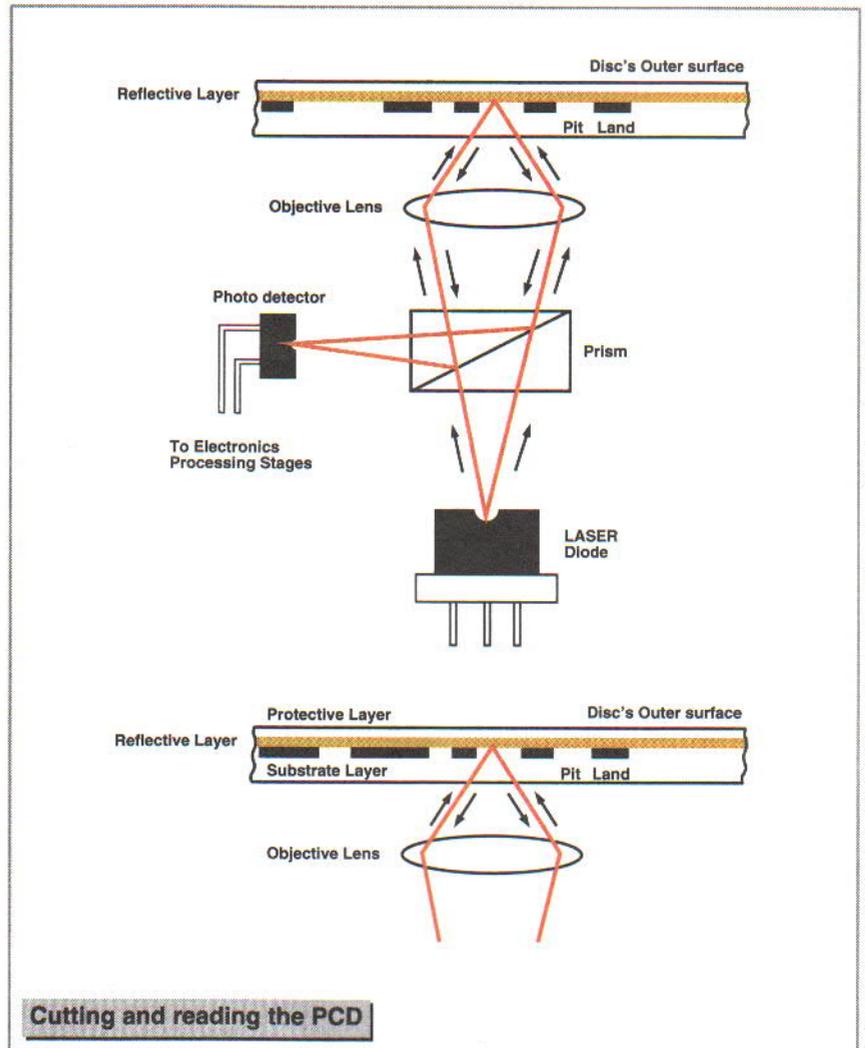
file consumes most of the storage space for a given image. There are optional 64 Base and 256 Base files for larger film formats.

The image discs themselves have a gold layer with very high reflectivity instead of the 'silver' layer of audio CDs. These discs can store 640 megabytes of data, a capacity far above a computer hard disk. The accuracy of the lasers which cut and play back compact disks is much finer than the magnetic computer read-heads.

Photo CDs are not over-writable: they use WORM (write once, read many times) technology. But they are 'Multi Session'. Once the disc is recorded from your film by the photo developers, it can't be over-recorded or erased. However, you can take a partly-filled disc back to the shop with further films until it's topped up. After all - who takes 100 photographs at once? Kodak advise that it's best to record large batches of images in one session, but this is for price efficiency. You can also choose which images you want to keep from your negatives or conventional prints, and have the disc made up to your selection. Image collections can be arranged and themed like an album, and are provided with a printed inlay sheet with numbered mini-images as an index.

### Finely focused beam

The disc is cut by a PCD Writer in much the same way as an audio CD. A finely focused laser beam, guided by data from the Data Manager, attacks a layer of light-sensitive dye on the blank disk to form 'pits' which expose the gold reflective layer beneath. The read laser in the user's PCD Player scans those pits and feeds the resulting digital information back to its processor to transmit to the television screen. The picture information can be manipulated by the PCD Player: cropped, rotated or panned. High resolution allows zooming up without jagged edges. PCD Players also handle hi-fi audio, offering high end facilities including bitstream, so ordinary audio CDs can be played on them, and users can look forward to having Photo CDs with added music and commentary in the fullness of time.



Cutting and reading the PCD

Thermal enlargements can be made straight from the disc at the processing shop. The RGB primary information is read off and used to calculate the subtractive primary values for printing. A PCD printer has somewhat over 2,000 elements to give a good-quality continuous tone print. The detail should

be comparable to that of a photographic print rather than that of a glossy magazine cover.

This is not an idle comparison, because the print industry is now heavily computerised, and the ability to load and edit images digitally is being taken for granted. The transport and



2

# Kodak

Electronics in Action in association with Kodak are giving two lucky winners the chance to be proud owners of Kodak Photo CD players. All you have to do is answer the 3 easy questions on the right and tell us what sort of projects and features you would like to see in future issues of Electronics in Action. We will draw the winners out of a large hat on 20<sup>th</sup> December 1993

Closing date for entries  
15<sup>th</sup> December 1993

reproduction of high-quality photographs for printing is expensive; CDs are light and tough, and can carry a large number of digitally-encoded images. Many publishers and image libraries already use 35mm PCDs, and Kodak are set to provide the same facilities for larger commercial formats such as 120mm. Larger formats need larger file sizes, but with or without image compression, there is no problem in packing a number of large high quality images onto a 640MB disc.

In early 1994 Kodak expect to be offering a 'Portfolio' service. Graphics designers can edit originals from their own PCDs as a Macintosh computer file using proprietary Kodak software which is now being tested. Text, graphics, audio and the ability to branch through various information paths will be available, and when these have been combined to the designer's satisfaction a bureau will write a new combined-medium CD using the original PCD and computer files as the data source.

### In-House Images

In the further future, designers and training managers will be able carry out these processes in-house to produce their own complex image files or interactive sound and vision CDs. Hardware and software companies including Apple, Microsoft, Hewlett-Packard, Adobe and Aldus are already endorsing PCD. It can already be read by Compact Disc-Interactive (CD-I), the sound and visual system widely used for training and cataloguing and other tasks needing sound/visuals branching, and by CD-ROM-XA, which can be used to interface with a computer. (PCD does

not read CD-I software.) Many CD-ROM drives are not compatible with Photo CD, but as the PCDs only need some CD-ROM-XA capabilities, they can be read by certain CD-ROM players supporting Mode 2 data transfer.

Several manufacturers now make Mode 2 Form 1, Multisession-compatible CD-ROM drives which support Photo CD. Check with your dealer that your CD-ROM drive has this capability if you want to go into PCD by that route. PCD Players themselves have considerable interactive and branching facilities and may be more economic than fully-fledged CD-I for some applications. This is mainly of interest to commercial users who want to manipulate and edit images or sequence them with sound and text. Home computers don't usually have enough memory to access and manipulate large high-resolution image files, but this is changing fast with low-cost hard disks. Already, the lower-resolution PCD images are read and manipulated with software like Photoshop. Once edited in their low resolution form, the image files can be handed to a bureau as guide-files to make the same changes on the high-resolution file, from which a new print can be taken. As and when prices come down a little further, small companies and serious home users will be looking at this.

Kodak is offering Photo CD Access Developer Toolkit software, under license to themselves, to enable software developers to embed the ability to handle full quality PCD images into their own software. Another, small, application, CD Access Software, allows the YCC-coded PDC files to be

converted to TIF, PICT, EPS and other image formats in existing applications. If this is what you want to do and you have any doubts about compatibility with the destination format, Kodak can advise you.

Photo CD is expensive for the home photographer. PCD Players have come down about 30% to around £199, and the discs themselves cost around £5. Processing costs more than conventional prints. A lot will depend on the attractions of the compact disc - compact, convenient, long-lasting and accurate in reproduction - and the amusement of viewing sessions round the TV, sequencing, zooming, panning and rotating with the remote control while family and friends boo and hiss. It's also easy to overlook that the players also play audio CDs, so anyone considering compact disc, or replacing a player, might look at the photographic possibilities. CDs don't fade, tear or crumple, and as long as the medium hasn't been physically wrecked, copy PCDs suffer no loss of quality. Eventually, sound and graphics should be available for the home user, but this is still a long way off for simple price reasons.

For the commercial user, though, PCD holds the attraction of reduced costs by bypassing certain processes which are necessary at the moment, and gives more control over the end result.

Try out your reactions: a photographer friend comes around and whips a shiny disk from her top pocket. It could be her latest photomontage, the new Lemonheads album, or her holiday snaps.

# Photo CD players to be won

- 1 In which year did George Eastman invent the box camera?  
a 1988  
b 1888  
c 1588
- 2 What is the standard film size found in most cameras?  
a 35mm  
b 35m  
c 35km
- 3 What does WORM stand for?  
a Waste Optimising Read Memory  
b Window Operating RAM Management  
c Write Once Read Many times

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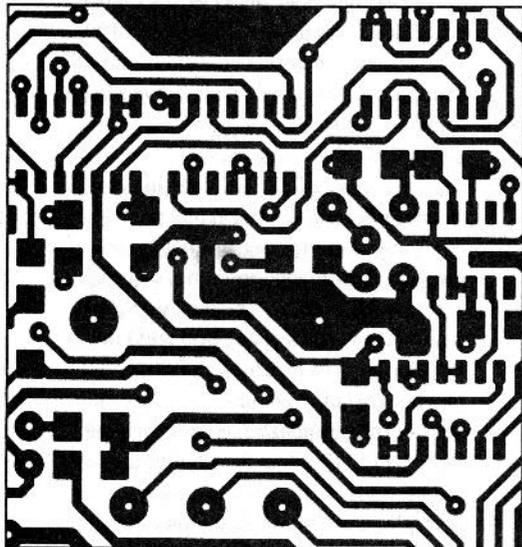
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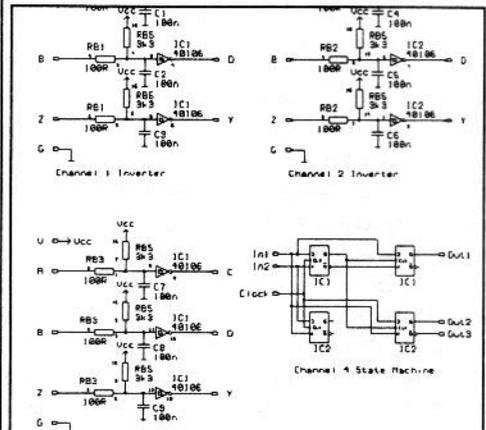
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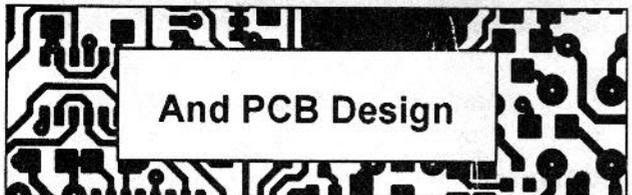
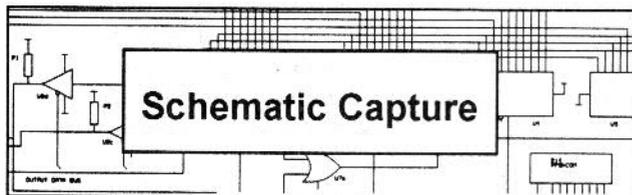


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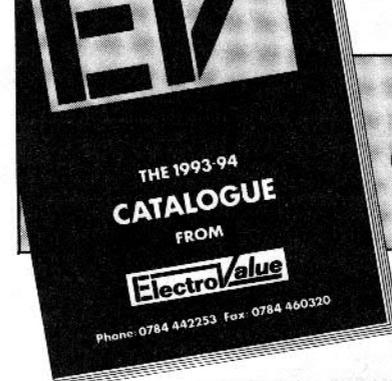
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Part 2

# The Switcher

This month Mike Meechan looks at the construction of this audio solid state switcher.

Last month, we looked at the analogue and local control side of things as far as The Switcher (our solid-state audio routing module) was concerned. Before we move onto the VCA section, the constructional side of the two main boards (which were presented last month) must first be finalised. Interested parties might like to note that the overlay and parts list for the relay switching option associated with the main board will be presented at the end of the series. On a related note, it is relevant to mention that when the system was first developed, the price differential between the relay version and the solid-state version was minimal. However, in recent months, the price of the SSM 2412 has shot up astronomically, from around £3.00 a year ago to around £8.00 at the time of writing. This has serious repercussions on the overall cost of a switching unit intended for eight inputs, although the cost of said unit is still substantially less when compared to buying a preamp with a commensurate number of facilities of similar quality.

## A-Z of the PCB

A brief look at the two appropriate component layouts of the front panel board and main analogue board (solid state version), depicted in Figures 1 and 2 respectively, show that extensive use of a ground plane has been made. A

short word about the need for this. When digital control and high quality analogue (audio) circuitry come together, what can have been a workable system on breadboard can quickly become a nightmare of gigantic proportions when the design is committed to printed circuit board.

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*In an ideal world we'd use completely separate and isolated supplies for audio and digital circuitry*

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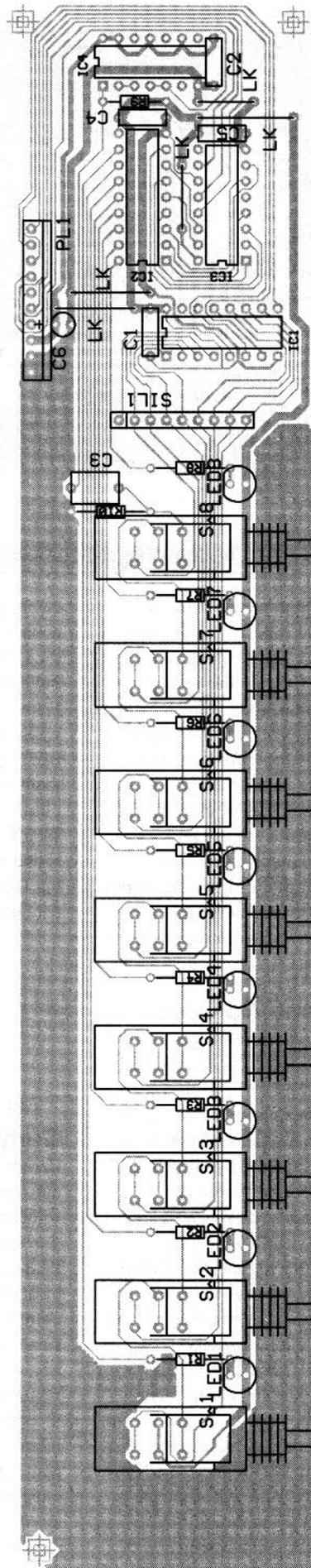
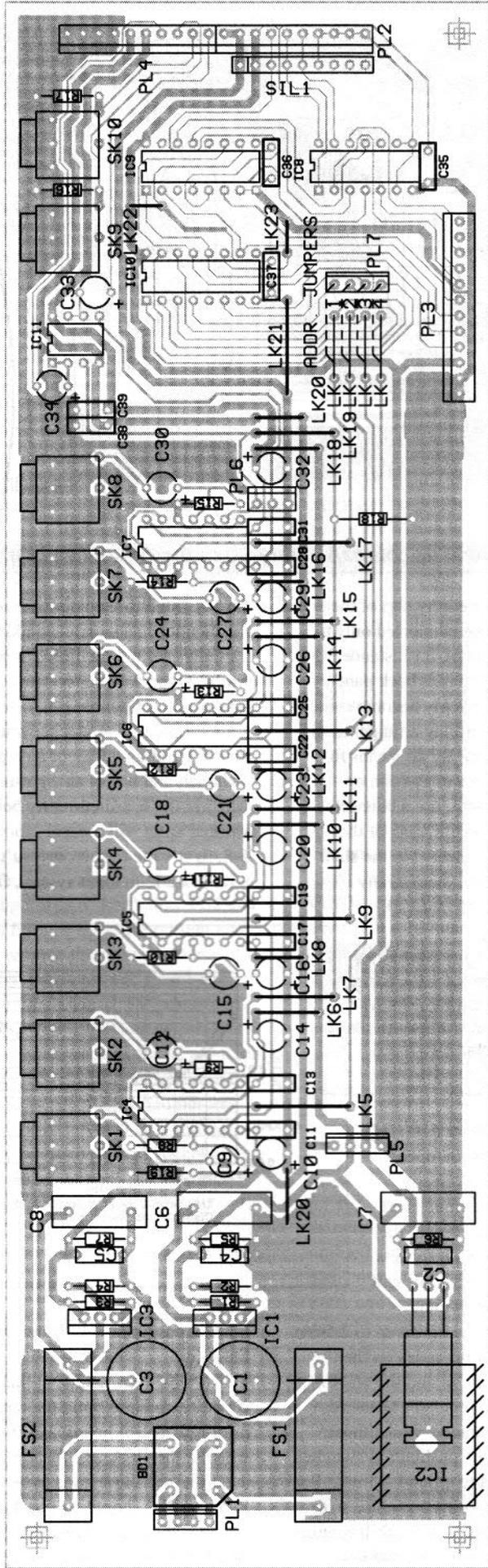
As digital outputs change state, there is a transient need for energy. On a positive transition, this current sourcing comes from the positive supply rail, and on a negative transition, the ground line sinks current. Inadequate supply decoupling at appropriate frequencies (up to about 50kHz), or narrow supply or ground tracks, will produce noticeable resistance and a digital pulse of energy throughout the system can create upset. In audio, this manifests itself as an audible click or a splat on the output. Fat tracks mean much lower resistance

and a ground reference which ostensibly remains where it is (ie at 0V) irrespective of how much current is flowing through it at any instant. Good supply decoupling in the immediate vicinity of each IC on the board, and hefty positive rails eradicate the problem on the supply side of things.

In an ideal world, we'd use completely separate and isolated supplies for audio and digital circuitry, and either connect them only at the system star earth, and adhere rigidly to this earthing philosophy throughout the rest of the board, or use opto-isolators to control things to keep things separate.

A halfway-house measure, (which is used in many commercial products where economics are top of the designer's list), is to use a limited star-earth arrangement. With this PCB topology, logic and audio supplies are kept separate except at one point, and a ground follows signal arrangement is used, with high impedance signals sharing a common earth return, and low impedance signals likewise, the various busses connecting only at the star earth. The boards shown here are a veritable pot-pourri of the above, but the system works, and any switching clicks are at or around the system noise floor.

Whilst on this subject, the relay version compounds any errors in this area of design by a very large order of magnitude, since electromechanical



**Fig.1 (left) Main Analogue Board/ PSU Component Positioning (Inputs 1-4)**

**Fig.2 (right) Front Panel Switch Board/Decoder Component Positioning**

**Designed on Boardmaker 2 from Tsien (UK)**

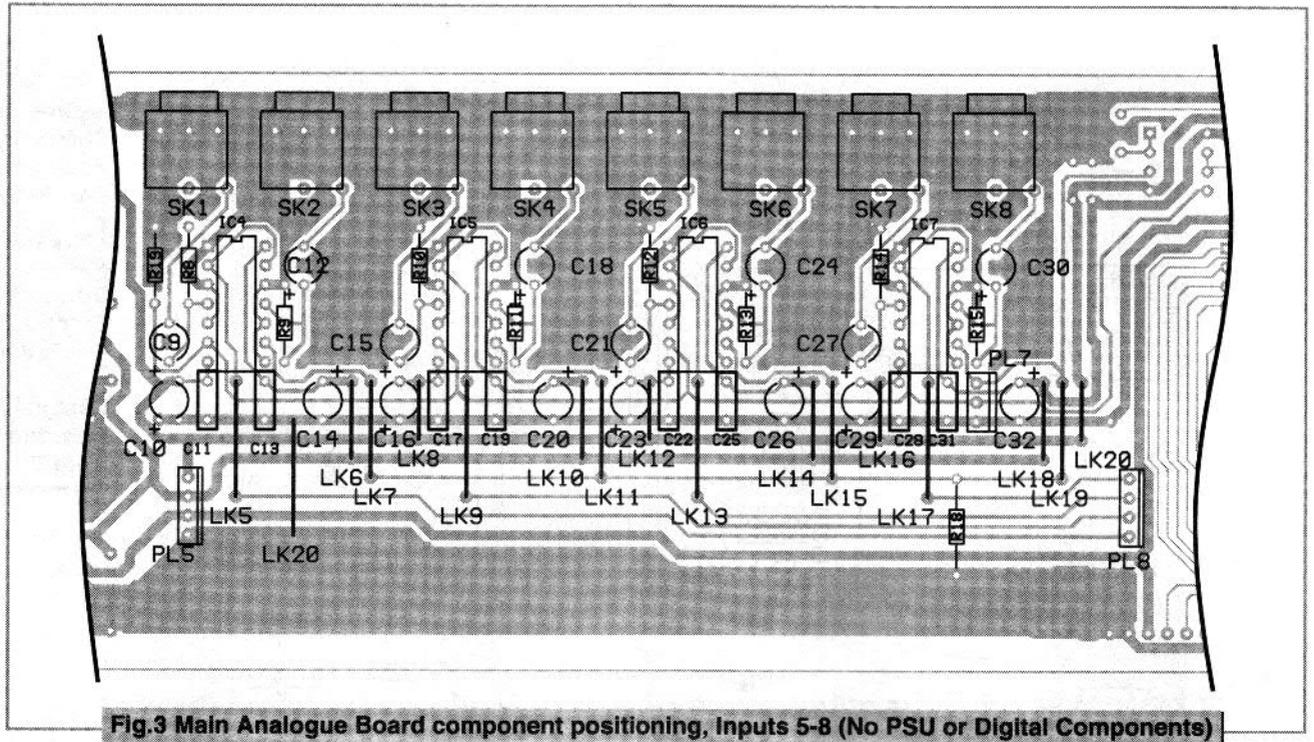


Fig.3 Main Analogue Board component positioning, Inputs 5-8 (No PSU or Digital Components)

devices are predominantly inductive. They absorb and expel a lot of energy as they are energised or de-energised. This energy has an effect similar to that caused by the transitions of logic gates, but it can be more devastating to any audio signals in close proximity because of the inherently larger currents involved. For this reason, track layouts are especially critical where relays and audio are mixed on the same board. We'll cover this subject in greater depth when we come to look at the relay version of The Switcher in next month's issue.

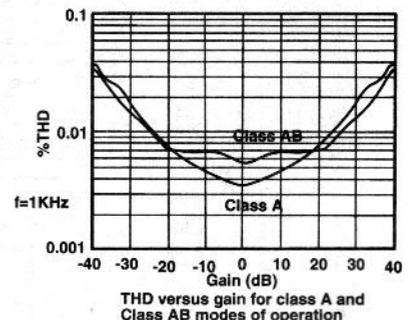
### All Mods and No Cons

The PCB's have been designed with specific components in mind. Certain substitute parts WILL fit, whilst others will not. As an example, the particular ALPS pushbutton switches used could be omitted and replaced by other DPDT non-latching types and could be connected to the board using a flying lead/Veropin-style of arrangement. Lead layout for the digital side of things isn't too critical, although any leads should be kept as short as possible. The PCB-mounting phono connectors, whilst not to everyone's taste, provide an uncomplicated, fast and cheap way of terminating audio signal sources. Again, these could be omitted, replaced instead by screened lead, DIN sockets (YUK!), 1/4" jack sockets, XLR's, banana plugs or whatever takes your fancy. Interwiring on the audio side is inherently less tolerant of gross modification than the digital part is.

Consequently, the earthy part of the connectors must be connected only to the PCB - it must not, for instance, be bolted to a metal chassis back panel. Hum loops very quickly become evident where slapdash earthing arrangements like these are used. By all means fit them first to a piece of Paxolin or plastic, or better still, use a connector such as an XLR where none of the signal pins are connected to the shell, but DO NOT attach them to any conducting, earthed material.

first be fitted to the board, since some of the components which are added later partially obscure the links, or make the fitting of them at a later date a downright impossible task. Before fitting links LK1-4, decide whether you're building a four or an eight input switcher, and if it is an eight-input one, whether the board currently being worked upon will control Inputs 1-4, or 5-8. If it's the former, or you're content with just a four-input system, fit the

Fig.4 Distortion graph showing differences in characteristics of class A & AB operation



### Component Stuffing

Certain holes must be opened out - enlarged - before any soldering can be commenced. The holes associated with the PCB-mounting phono sockets must all be enlarged to around 2mm in diameter although some versions may require up to 2.5mm holes. The mounting holes on the perimeter of the PCB, and the one for mounting the 5V regulator heatsink, require 3mm clearance, whilst those associated with the pushbutton switches must be enlarged to around 1.5mm. For all of the drilling operations, use sharp (brand new) drill bits and a drill running at 2000rpm or higher. We can now begin soldering. All of the links must

links in positions 1-4. If not, leave the links out.

In a similar vein, decide at this juncture if you're going to build the optional infra-red control board, and if so, whether the VCA will feature as part of it. If the VCA system is to be fitted, PL4 and PL2 should be fitted later. If not, two short links connecting Pins 7 and 8, and 9 and 10 respectively, should be soldered in place. These carry both

channels' Audio In and Out signals. As an aside, there are wire links on the board than I would normally desire, but single-sided boards are cheaper double-sided ones, and so, in the interests of economy, pure aesthetics have been sacrificed somewhat.

Next, fit all of resistors and follow with the DIL sockets. Capacitors next, soldering the smaller ones before moving on to the electrolytics and suchlike. (The smoothing capacitors, C1 and C3 associated with the power supply section are the last components to be fitted to the audio board). Plugs and sockets, fuseholders, the bridge rectifier, regulator IC's and heatsink, (and pushbutton switches on the front panel board), are the penultimate fixture. Again, the number and identity of plugs fitted will depend upon the options chosen. The various overlays show this pictorially. LED's come last on the front panel board. Verify that these, particularly, are correctly orientated with regard to polarity - once the leads are bent to their required shape and cropped to length, any mistakes are effectively irreparable.

We are now ready to test the main analogue board. A 15-0-15 transformer must be connected, via a suitable 4-way Minicon socket, to PL1. Power up and check for a DC voltage of around 19V on the input side of fuseholder FS1 and -19V on FS2. If these are present and correct, remove the primary source of power and insert 250mA slow blow fuses into the holders. Re-power and check that -17V is present on pin 7 of each of the DIL sockets for IC's 4-8, pin 4 of IC11, and that +17V is present on pin 14 of the first-mentioned holders, and pin 8 of IC11. (No IC's should presently be fitted to their sockets). Check also for +5V on pin 14 of the sockets for IC8, and pin 16 of the sockets for IC9 and 10.

If all is well, disconnect power and plug

| PARAMETER                       | MEASUREMENT CONDITIONS                  | UNITS    |
|---------------------------------|-----------------------------------------|----------|
| Equivalent Input noise          | f=1KHz                                  | 14nV/Hz  |
| Gain Bandwidth product          | VCA Configuration                       | 12MHz    |
| Slew Rate                       | VCA Configuration                       | 10V/us   |
| Gain Constant                   | Ratio of Outputs                        | -28mV/dB |
| Control Feedthrough (untrimmed) | Class A 60Hz Sine wave causing          | -10mV    |
|                                 | Class AB                                | -1mV     |
| Maximum attenuation             | f=1KHz, Vcontrol=+4V                    | 100dB    |
| Noise                           | Class A, Rb=30K, BW=20-20KHz, AV=0dB    | -85.5dB  |
|                                 | Class AB', Rb=150K, BW=20-20KHz, AV=0dB | -94.5dB  |
| Total Harmonic Distortion       | Class A, AV=0dB, Vin=+10dBu@f=1KHz      | 0.007    |
|                                 | AV=+/-20dB, Vin=+10dBu@f=1KHz           | 0.0115   |
|                                 | Class AB', AV=0dB, Vin=+10dBu@f=1KHz    | 0.007    |
|                                 | AV=+/-20dB, Vin=+10dBu@f=1KHz           | 0.017    |

**Fig.5 Table of SSM 2018 VCA performance specifications**

front panel PCB into the main board. Re-apply power and with reference to the circuit diagram shown last month, verify for the presence or otherwise of the supply voltages on the appropriate pins of each of the DIL IC sockets. Once this has been done to your complete satisfaction, remove power and fit all of the IC's into their correct sockets. Re-apply power and verify the operation of the switches/LED's, ie that pressing a particular pushbutton cancels the previous selection and causes its associated LED to light. Next, connect a stereo audio source to each of the inputs in turn and check that audio is present on the output sockets when the relevant source is selected as an input. (If you're going to be building the VCA/Remote Control board, and have fitted plugs PL4 and PL2, bridge pin 7 to pin 8, and pin 9 to pin 10 using wire links. This establishes an audio path from the output of IC11 to sockets SK9 and SK10). Both boards can now assume to be tested and complete.

### More than Four Inputs?

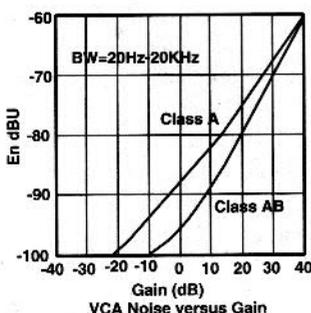
For inputs 5-8, a second main analogue board must be constructed. This is identical in all aspects to the first, but for the fact that all of the components associated with the power supply are omitted. Furthermore, links LK1-4 are also omitted, as are PL4 and PL2, IC's 8-10, and their associated decoupling capacitors and resistor arrays. Two 4-way Minicon socket/lead/socket assemblies transfer power (via PL5) and control signals (via PL7) between the two boards, whilst a 3-way socket/lead/

socket assembly (PL6) connects the audio output of the second board to the stereo bus that is IC11's input. Figure 3 shows an overlay of a board constructed in this fashion. The links LK1-4 are replaced instead by a 4-way plug PL8. In this way, the Q5-8 outputs from the BCD-decimal decoder IC on the main board are connected to the board carrying Audio Inputs 5-8 and used to actuate the solid state switches thereon.

### Voltage Controlled Amplifiers

We are now ready to take a preliminary theoretical look at the VCA side of the optional digital remote control part of the system. The remote control boards - transmitter and receiver - as well as the constructional element of both of these boards - VCA and infra-red transmitter/receiver - occupies the final part of this saga.

The VCA section of The Switcher uses a studio-standard VCA from our friends at Analog Devices. Its performance is markedly different from some of the consumer IC's marketed for this purpose, since it was designed to be included as part of the fader automation systems of recording desks, or into the panning or equalisation sections of said equipment. It should be noted that any impairment perpetrated in the mixing console electronics is irreparable - it follows that noise and distortion characteristics of semiconductors destined for inclusion in mixer electronics must, in many instances, be in the vanguard, performance-wise, of devices currently available. This is whilst combining such characteristics with a cost which makes the component attractive from the point of view of economics. The SSM 2018 manages to achieve respectable figures in all of the places that matter ie noise, distortion, and cost. A table of these and other



**Fig.6 Noise graph showing differences in characteristics of class A & AB operation**

**Fig.7 SSM 2018  
Simplified Internal  
Architecture**

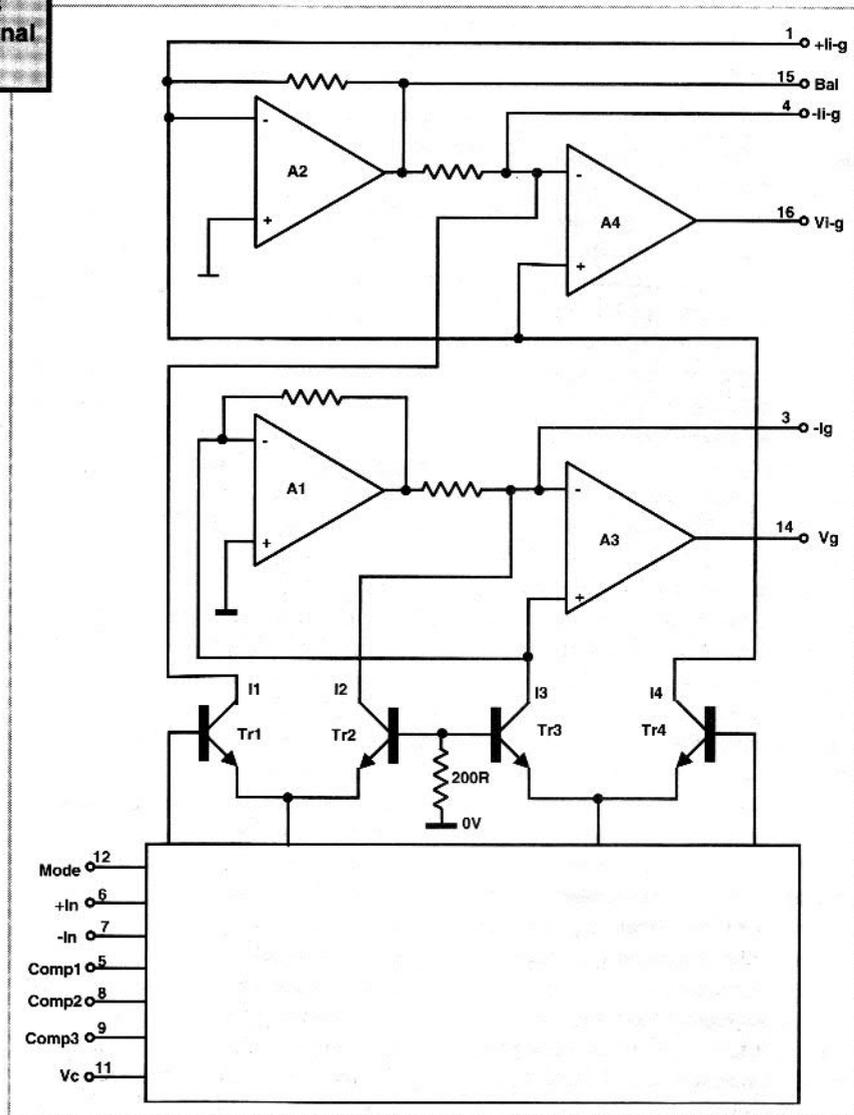
important characteristics is shown in Figure 5

The SSM 2018 VCA can be configured to operate in Class A, Class AB or anything in-between. Running the output devices in different modes of operation can become important in critical, high fidelity applications, since these different classes of biasing the VCA output stage alter the way it performs as regards noise and distortion. We'll discuss the differences presently. Also, because of the complexity of the VCA family of devices, and because we expect so much of them, sonically, in a decent application, we'll look rather thoroughly at what is going on inside this innocuous-looking IC before we get down to the nitty-gritty of the actual Switcher VCA circuitry itself.

### A Background History

Surprising though it might seem, there are only five manufacturers of VCA's in the world. Many of the individuals concerned with the development and perfection of the VCA have become legends in the pro-audio industry - their successes in this field can be measured by the fact that their surnames adorn many of the upper echelon class of audio FX and processors. The designers and patentees of VCA's have long since abandoned the R and D labs where they started their careers and gone on to head the corporate empires which manufacture these goodies. Because, between them, these five companies hold all of the key patents, there are a number of similarities between the competing types. In many respects, there is little or nothing to choose from, performance-wise, between the top-of-the-range offerings from each of the manufacturers. The Analog Devices IC is the only one freely available from electronic retailers such as Maplin and RS, the others being the exclusive domain of the big boys of the pro-audio industry and distributed only through specialist audio component retail outlets.

The only other quality VCA available through the recognised hobbyist component supply channels is another Analog Devices IC, the AD 7110KN. This is marketed as a "digitally-controlled CMOS audio attenuator". It accepts a 6 bit binary code and translates this into an attenuation setting. Signal-to-noise



ratio available from this IC is 100dB, whilst distortion hovers around the 0.00125% mark. There is, sadly, a high price to pay for such outstanding performance - about £24.00 per IC.

As far as the choice of the 2018 is concerned, it shouldn't be taken as an indication that the SSM series of VCA's are in any way inferior to these other, mysterious, aloof and hard-to-find types - it performs quite meritoriously in all aspects important to professional users and audiophiles. As I said earlier, I shall not even bother mentioning the so-called "consumer" VCA/tone control/preamplifier IC's intended for inclusion in less demanding domestic hi-fi applications - distortion figures of around 0.5% make them a rather unpalatable proposition - there is absolutely no place for their fitting in any system with pretensions towards fidelity of any size, shape or form...

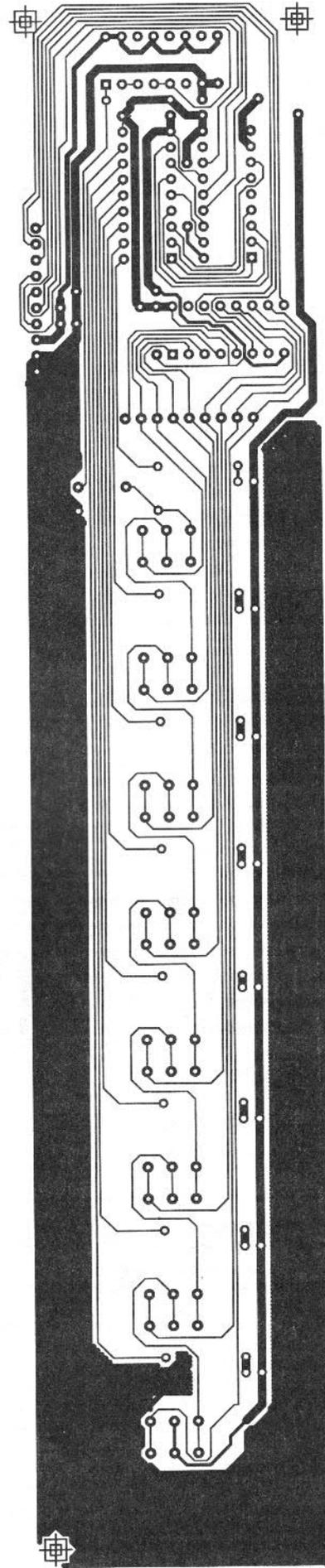
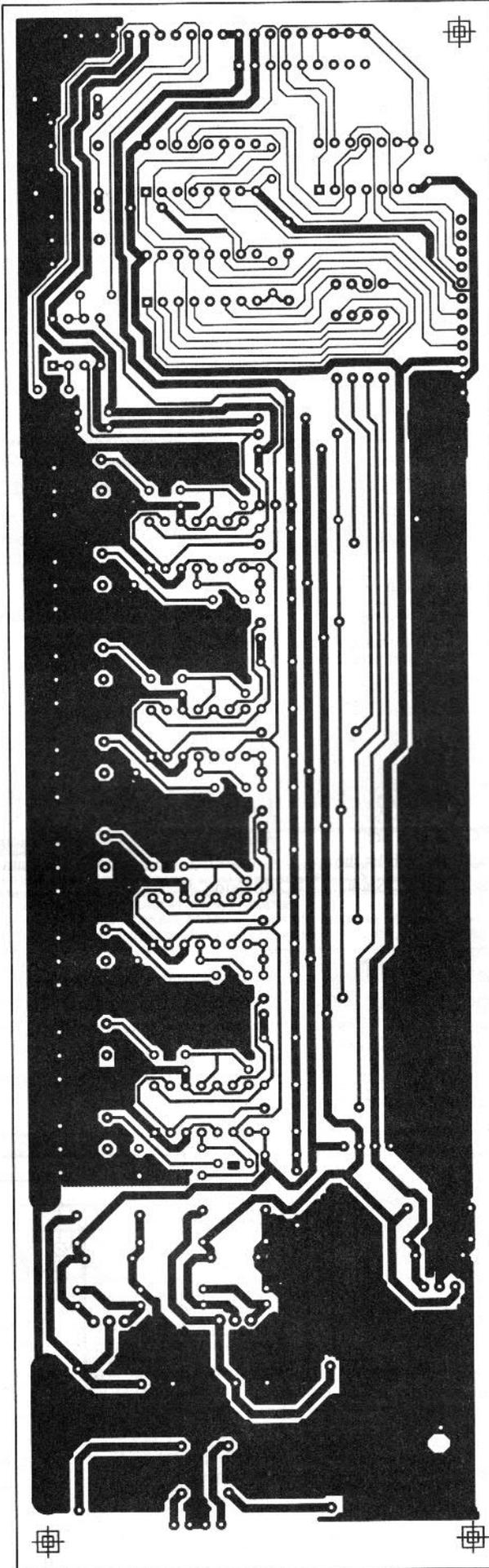
### Is "A" Top of the Class?

As in any amplifier or related circuit, Class A means that the output devices operate with a constant bias current,

while Class A-B operation means that the bias current varies continuously and proportionately to the absolute magnitude of the input signal.

Typically in these configurations, high operating currents reduce distortion but worsen noise. This results because of the way in which semiconductor noise mechanisms work.

In essence, noise remains constant and distortion low in VCA devices operated in pure Class A. See Figure 5. Because the noise remains at a fixed level irrespective of the magnitude of the input signal, it is, of course, worst when low level signals are being handled (signal-to-noise ratio is compromised). With Class A-B, noise is worst with large-level input signals (more bias current flowing through the VCA's internal resistances and so greater noise voltages developed across them). As signal level drops, so does noise level, so the signal-to-noise ratio is ostensibly constant for a widely differing range of input levels. Distortion, however, is worsened, since the bias current is continuously altering. The value of this



bias current is chosen as a compromise between good all-round noise performance and decent distortion performance at various operating levels.

## Types of VCA's

As well as different operating modes, there are currently also two different ways of implementing the voltage-controlled attenuation (or amplification) function. One uses a method known as "current-steering", the other, "log-antilog". Since the SSM 2018 VCA - the one which this project uses - employs BOTH methods, we'll look at each in turn.

Current-steering, (also known more popularly as variable transconductance), divides current to reduce system gain. No attenuation is possible although the logarithmic nature of the process means that the large dynamic range span necessary for high quality audio signal handling is available from any IC using this kind of design architecture. These types give their best when attenuating a signal, performance failing slightly at or near unity gain.

The other type, log-antilog, as we might expect, operates in a completely different manner, and so gives its best under different operating conditions. Log-antilog types work by subtracting current from, or adding it to, the logarithm of the input signal current. An anti-logging function converts the current back to its original form. This method of operation means that the log-antilog type can give gain as well as attenuation. In contrast to the current-steering types, log-antilog types give best performance when operating at unity gain ie no attenuation.

## The Analog Devices SSM 2018

The extremely flexible chip architecture of the SSM 2018 features inputs and

outputs which can be configured for both differential and single-ended signals, with each able to further be configured for current or voltage modes of operation. All of the important input and output ports - audio in, audio out, and control in - are buffered. This improves performance whilst reducing external parts count when compared to other similar, competing devices. The IC has two voltage outputs and three current outputs available, the current outputs being able to deliver 750uA when operated from a bipolar 15V supply. Feedback resistors can be used to convert these currents, internally or externally, into voltages. One external resistor,  $R_B$ , programmes the gain core bias current and determines Class A, A-B or intermediate operation. This current must be derived from the positive supply rail and be of the order of 90-500uA for correct operation, since its omission cause the output signal to appear half-wave rectified. Figure 7 shows the unusual internal chip architecture.

The best noise performance is achieved in Class AB, although this is at the expense of a slight increase in distortion. This increase is much lower than other contemporary devices and small enough to be ignored in all but the most demanding distortion-free applications. This is borne out when distortion figures in Class A-B are compared to those achieved whilst the device is operating in Class A. Such

noise/distortion characteristics are quite unusual, since low distortion AND low noise cannot normally be achieved. Historically, Class A-B was always the preferred mode of operation when low noise was of the greater concern, whilst Class A found a niche where a low distortion VCA system was required. The programmability of the IC allows the distortion/noise performance to be optimised for a given application. Intermediate Class operation yields an excellent compromise between the low noise of Class A-B and the superior distortion characteristics of Class A operation. As a final thought on the Class Wars, Class A-B gives better control feedthrough rejection than other classes.

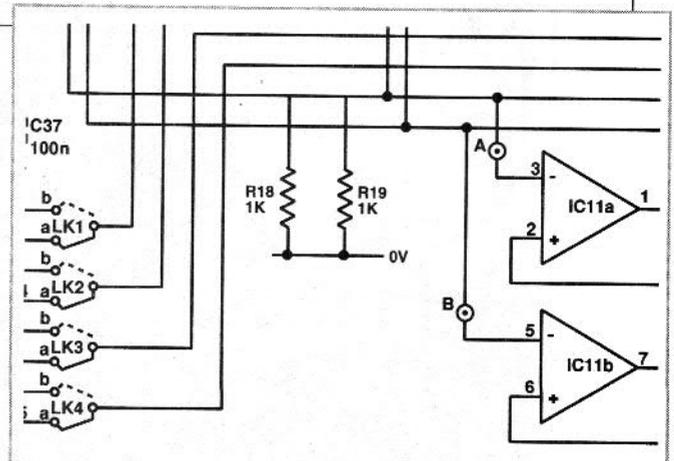
Next month, we describe in detail the various parts important to the unique operation of the SSM 2018, and then go on to divulge how it is used in our application. As a closing thought, if you're one of the subjectivist brigade who hates any superfluous semiconductors in the audio pathway, adding noise and distortion that wasn't present in the original signal, you might prefer the relay version in the final part when we'll present overlays and diagrams for this cheaper-by-thirty-pounds-version.

## References

Analog Devices SSM 2018 Voltage Controlled Amplifier/OVCE Data Sheet, Revision A

# Clang

In last months installment of The Switcher, two resistors - R18, 19 both 1k in value, were missing from Fig.12 Switcher main analogue/PSU board circuit diagram and the parts. They should be connected as shown in the abbreviated circuit diagram shown below.



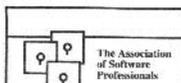
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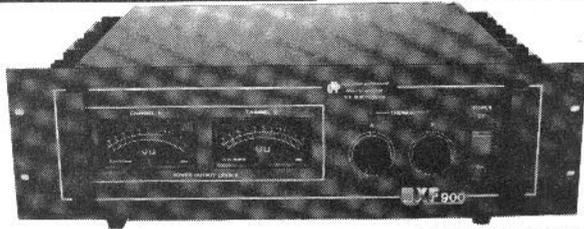
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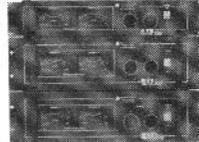
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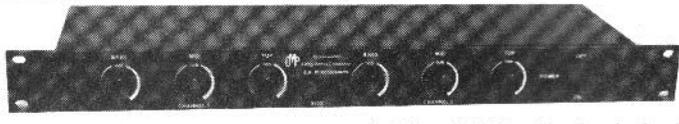
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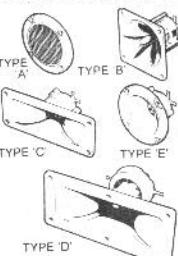
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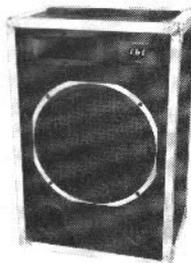
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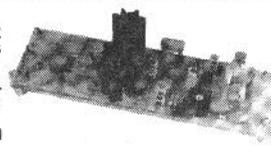


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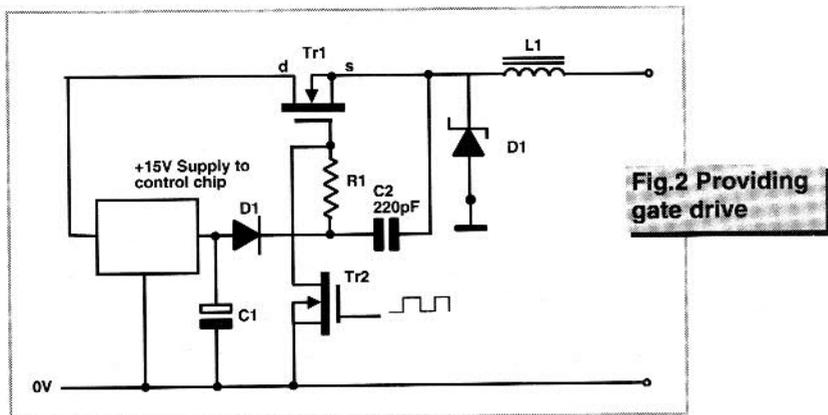
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**Fig.2 Providing gate drive**

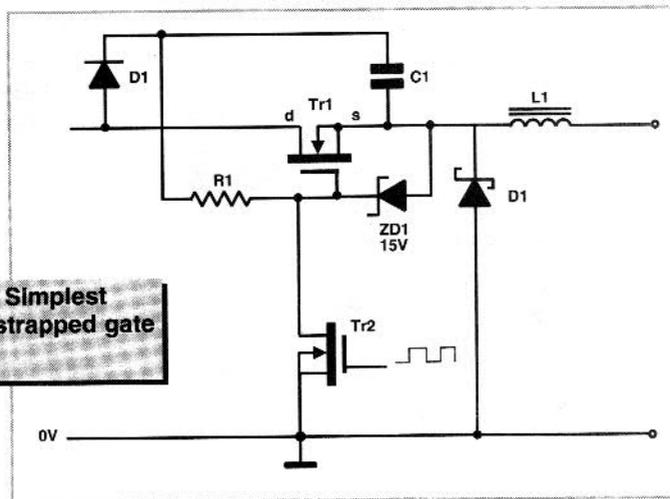
I will describe the circuit in detail, because it is almost identical to one which I have used in the past as a constant current battery charger, and it works well if the PCB is laid out properly, with good earth tracking.

The control chip, a UC3843, provides a constant frequency, variable mark:space ratio drive signal in response to its current and voltage feedback signals. It is a current mode controller, which means that its primary control method is to switch off the output drive when the current signal has ramped to its limiting value each cycle. The limiting value of current is set by an internal reference, and reduced as a function of the feedback voltage potted down from the output. The oscillation frequency is set by the value of R9 and C5, while the maximum on to off ratio of the output is set by C5 and the fixed discharge current inside the chip.

Because this circuit can operate with greater than a 50% on-time, it is necessary to feed a proportion of the oscillator ramp into the current feedback point to prevent sub-harmonic oscillation. TR5 buffers the ramp into the relatively low impedance point, while the proportion of ramp fed back is set by the ratio of R12 in series with VR1 to R8.

The derivation of the current feedback makes interesting use of the FET. The important property of the FET in this case is that the source current is equal to the drain current (i.e. the gate current is zero). If the offset adjustment, VR2, is set so that the inverting and non-inverting inputs of IC2 are at the same voltage (with no current flowing through TR6 no current flows through

R1), then any voltage drop across R1 (caused by a current through R1), will result in an extra current through R14. This must flow through TR6 in order to maintain the op-amp in balance. Note that the feedback is to the non-inverting



**Fig.3 Simplest bootstrapped gate drive**

input of IC2, because of the inversion in TR6. The net result of all this is that if R12 in series with VR1 is set to the same value as R14, then whatever voltage appears across R1 will also appear on the current sense input of IC1.

The purpose behind this apparent complexity is to avoid the necessity for a current sense resistor in the zero volt line of the supply. Such a resistor would have to be inserted directly to the right of the ground connection of IC1, and would cause incorrect voltage feedback signals.

**Gate switching**

The drive output of IC1 switches TR4 via a current limiting resistor, R11. This marginally slows down the switching of TR4, but is necessary to limit the peak output current of IC1 to its specified maximum value.

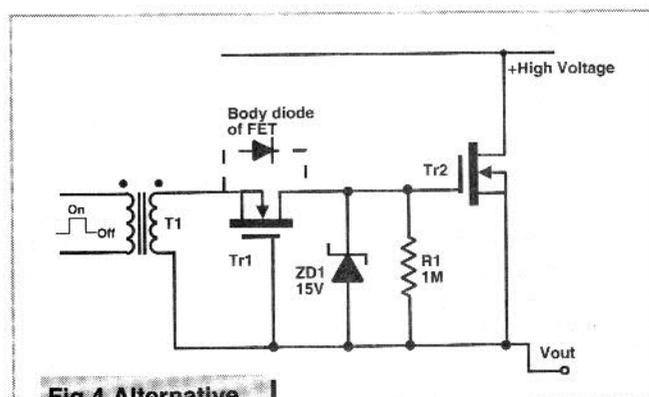
When TR4 switches on, TR3 also switches on.

This switches off TR2, and switches on TR1. In order for TR1 to switch on fully, it is necessary for the gate voltage to be raised above the power supply's input voltage. The charge to do this is provided by C1. It is charged up to the power supply input voltage when TR1's source is at 0V, and whose top end is therefore raised to double the power supply input voltage when the source reaches the input voltage. If the input voltage is more than about 15V, then the voltage on C1 will be too high and must be limited by ZD1 and R3 to prevent damage to TR1. If the power supply input voltage exceeds about 25 volts, the dissipation in R3 and ZD1 can become significant. It is certainly necessary to calculate the value of R3 to minimise the dissipation at the expected input voltage of the supply, while maintaining adequate gate drive. However, the higher the value of R3, the slower the switching of TR1, and if the input voltage is raised, at some stage the point will be reached where if R3 is raised high enough to prevent ZD1 over-dissipating, TR1 will not switch on fast enough, and will itself dissipate heavily.

If it is so difficult to provide sufficient gate drive voltage for an N channel MOSFET, you may wonder why a P channel device should not be used instead. The reason is that, for a given die area (and hence cost and gate capacitance) an N channel device can switch on to a lower resistance. N channel devices also tend to be sturdier, cost for cost.

**Control supply**

When this design is running, the power for IC1 is drawn from the output. Although during power-up, C4 is charged from the input via R5, and when it reaches an adequate voltage IC1

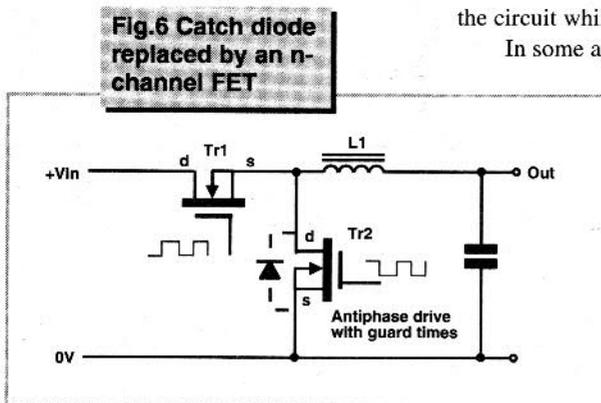


**Fig.4 Alternative form of gate drive**

starts to operate. R5 will not pass enough current to operate IC1 continuously, so it is necessary that the supply output is powered up before C4 has discharged.

However, there may be situations in which this means of powering the control chip is unsuitable. This supply can be used to feed the bootstrap capacitor if a separate small linear voltage regulator is used to power the control chip. So the FET gate voltage is what the FET requires without the need to dissipate power in a resistor and a zener diode. This much simpler method of providing gate drive to TR1 is illustrated in Figure 2.

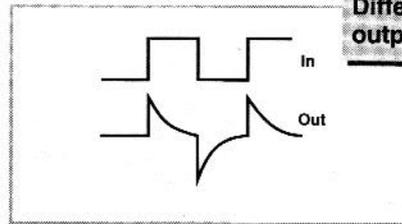
In cases where the input voltage is known, does not vary much, and is not far above 15V, the even simpler arrangement of Figure 3 can be used. This arrangement works well for input



voltages in the range 10-20V, and becomes increasingly inefficient at higher voltages. At input voltages lower than 10, the on-resistance of TR1 will be slightly higher, with serious inefficiency setting in at around 6V. If a lower input voltage must be used, then a special logic level FET may be used for TR1. This type of FET is more expensive than run of the mill MOSFETs, because its processing is optimised to make it switch on fully with gate drives of less than 5V.

### Isolated drive

An alternative form of gate drive is shown in Figure 4. Because the gate drive is coupled via an isolating transformer, it does not matter at what voltage the FET is sitting relative to the voltage of the control circuit. In this design, an extra MOSFET is used to control the gate drive, so that the power FET remains switched either on or off even if the drive signal from the pulse transformer disappears. This is necessary because, if a small low-inductance pulse transformer is used, a



square wave input drive may result in a differentiated output drive as illustrated in Figure 5.

On a positive edge, the body diode of TR1 switches, charging up the gate capacitance of TR2, and switching that on. When there is no voltage on the output of T1, then TR1 does not conduct in either direction. A negative edge on the output of T1 turns on TR1 and discharges the gate capacitance of TR2, thus switching it off. The gate of TR2 is protected from overvoltage by ZD1, and static charge is leaked away by R1, to minimise the likelihood of damage to the circuit while it is switched off.

In some applications, it is

necessary to add a fixed capacitor in parallel with R1, to hold TR2 on for longer in the absence of a drive pulse. If really long on-times are required, it may even be necessary to omit R1 altogether.

There is one particular snag to

using this gate drive technique, which may render it unsuitable for use in a buck regulator. If it is possible for the control chip to stop giving drive pulses altogether, in a circumstance when the power FET should be switched off, it can happen that noise or interference causes the power FET to be left switched partly on. In the conventional buck regulator design, if the pass transistor is on when it should be off, then the control chip will not generate any drive pulses, and, with a circuit such as that of Figure 4, the pass transistor will turn off very slowly as the charge is leaked away through R1. Therefore, it is clear that this type of gate drive should only be used in designs where gate drive pulses will always be present.

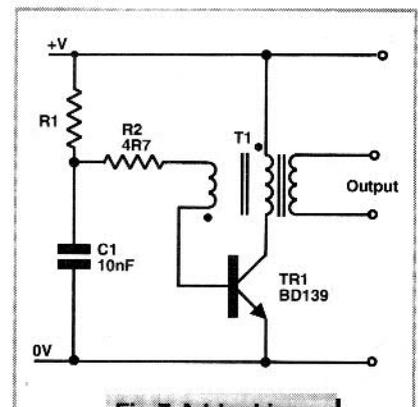
There is one final buck regulator variation, in which power MOSFETs can find a further application. The circuit fragment of Figure 6 shows the catch diode (the equivalent of D1 in Figure 1), replaced by an n-channel FET. In this design, when TR1 switches off, the body diode of TR2 will start to

**Fig.5**  
Differentiated  
output drive

conduct the current in L1. After a sufficient guard time to make sure that TR1 is completely switched off, TR2 is switched on. If TR2 has been chosen correctly, it has a very low on-resistance, and so imposes a much lower voltage drop than does any normal diode, even a Schottky. This technique is called synchronous rectification, and was originally used with electromechanical power supplies using vibrating contacts instead of power transistors, to drive a step-up transformer, and vibrating contacts in phase to rectify the output. These were used in ancient valved mobile radios.

When it is time for TR1 to switch on again, TR2 must be switched off sufficiently in advance to avoid the possibility of current flowing via TR1 and TR2 directly to ground. However, for most of the diode conduction cycle the voltage drop can be arranged to be negligible. In some very critical designs, a Schottky diode will be connected in parallel with TR2 to maintain a low voltage drop while TR2 is switched off, and to avoid the problems of slow switch on associated with some MOSFET body diodes. Certain MOSFETs are specifically designed for use in this application, and the switching time of the body diode in such MOSFETs is fully specified.

This sort of design is relatively



**Fig.7** A blocking  
oscillator design

expensive and is only useful when it makes a crucial contribution to the overall efficiency of the system. In effect, the voltage drop in the catch diode, while it is on, is added in series with the output voltage. So for example, if the output voltage were 6.3V, then a diode drop of 0.7V would impose a 10% loss during the time the diode was conducting.

The criteria for synchronous rectification to be worthwhile are that

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the output voltage of the supply shall be low, efficiency is high, and the output diode is switched on for a significant fraction of the operating cycle. In particular, this is useful in high-current 5V supplies, and medium or high current 3.3V supplies (now becoming common in notebook computers). The criterion for the diode to be on for a large part of the cycle is that the input voltage is significantly higher than the output voltage. This is simple common sense, because, if the input voltage was equal to the output voltage, the pass transistor would be on all the time and the diode would be on none of the time.

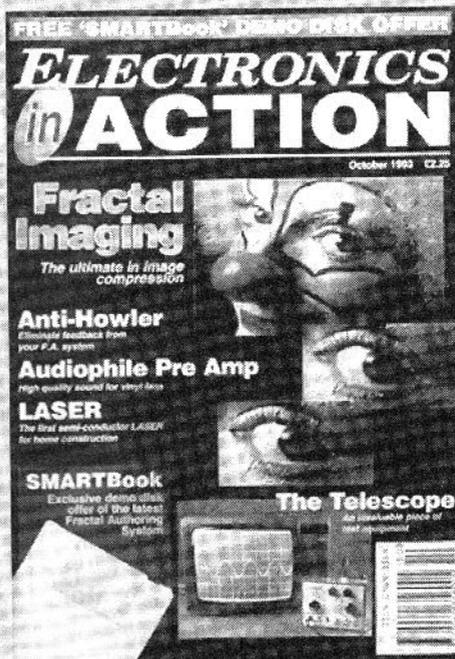
## Blocking oscillator

By way of contrast, Figure 7 shows an application for which, in my experience, a bipolar transistor is much better suited than a MOSFET. In this design, feedback is provided by transformer coupling between collector and base-winding, and the frequency is set (approximately!) by the time constant of R1 and C1. This is what it does: when power is first applied, C1 charges through R1 until TR1 starts to switch on. As soon as it starts to switch on, extra base drive is applied by the base winding, so it switches on harder.

It remains switched hard on with its base current supplied by the base winding on T1, until the base current demanded from C1 has discharged the capacitor to the point that there is insufficient voltage on the base winding of T1 to keep TR1 switched on. TR1 then starts to switch off, and in doing so the flow of current in the base winding is reversed which turning it off.

The operation of the circuit is based on a flow of current. A simple MOSFET implementation of this would involve the gate drive being derived from a current flow through a zener diode, with the switching device turning off when the sum of the capacitor voltage and the winding voltage fell below the gate threshold of the FET. The zener would dissipate heavily and the efficiency of the circuit would be low. For a simple and effective implementation of a blocking oscillator, a bipolar transistor seems best.

That's all for this month. In the final part next month, I shall cover high-powered analogue signal switching, reverse battery protection, a micro power voltage regulator and a transformer-coupled flyback converter. A MOSFET power amplifier project is also planned. Class A, B, or D? I haven't decided yet.



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## Hurry while stocks last!

**You may photocopy the coupon if you do not want to spoil the magazine**

# Technoshop

**E**lectronics in Action in co-operation with The Technology Exchange Ltd, the international technology matchmaking service based in the UK, will be bringing you each month a selection of technology partnership opportunities to which you are invited to respond.

The Technology Exchange, which was formed in 1985 as a not-for-profit technology sourcing service to industry, holds a bi-annual 'Technoshop' Technology Transfer Fair at Heathrow Airport and several 'Techmart' Fairs overseas for the United Nations (UNIDO).

For this issue of Electronics in Action, we continue to present business opportunities from European firms seeking technology partners in the UK indicating on each item whether it is an offer or a request for products or technology.

If you believe that you would qualify to be the partner for any firms described in these profiles, please write to The Technology Exchange quoting the item number and code letters at the head of the entry saying how you wish to respond and enclosing information on your own organisation and its products or services.

The only cost associated with this process is a simple £10 plus VAT introduction fee for each entry to which you respond. For this we will send you the information which we hold on the entry, transmit your response to the source of the entry and invite them to send you more detailed information about themselves and their entry.

The code letters on the entry number indicate the country where the partner is located as follows:-

## Code Letters

**TO/TR** - UK  
**GOM** - Belgium  
**SOFAD** - Spain  
**GR** - Greece  
**DTO** - Denmark  
**IDA/E** - Ireland  
**PME** - Portugal  
**SG/SGT** - Italy  
**A/ANG/DP** - France  
**B** - Bulgaria  
**ZO/ZL/TVA** - Germany

## Offer/Request BG 14 Computer Array Processors

Bulgarian producer offers FPS-compatible Array Processors 60 x 30 x 70 (H, W, D) attached to IBM PC/AT and converting it into a minisupercomputer workstation with 60 MIPS, 12 MFLOPS, up to 1 GigaByte dynamic memory, FFT 1024 complex points - 4.75mS at a fraction of the price of RISC computers. The company looks for licences and know-how in this field.

## Company Sale ANG F 1 Printed circuits

Manufacturer of printed circuits (metal and multilayer hole) generally in small quantities for industrial electronics, data processing, telephone and avionics manufacturers, seeks investment or company sale.

## Offer ANG F 8 Expert system generator

New expert system generator designed for use in companies where users are not familiar with such software. Enables such users to set up programs for decision making in a couple of days instead of a few months as with traditional systems. Distributors sought.

## Offer/Request ANG F 13 Position and movement sensors (Trajectory Metering)

Manufacturer of position and movement sensors used for monitoring industrial robots, human movement for medical and sports applications, mobile platforms and simiar, offers products for distribution and will consider joint-ventures with suitable companies.

## Offer ANG F 24 Micro-terminals for data collection processing

Manufacturer of software and data processing terminals including portable data loggers for the control and monitoring of production processes seeks reciprocal marketing arrangements and may consider offering manufacture of their products in Europe.

## Request SOF 9015 IBM Software

Spanish firm dealing in IBM medium and host systems is seeking development tools and specific software for those systems.

## Offer SG 90002 Electronic systems

An Italian specialist in the development of electronic systems and general purpose automation systems for the automotive and aviation industries offers technology and know-how exchange and sub-contracting.

## Offer/Request SG 911200 Component manufacture

A company producing a variety of electrical and electronic products including magnetic disk boxes, dot matrix printer leads, radio telecommunications and electronic components including circuit boards, seeks commercial and/or technical know-how exchange plus partners for CEC R & D programmes.

## Offer SG 911215 Oliodynamic motors

Manufacture of oliodynamic motors (high speed, low speed and variable speed) based on axial pistons with fixed and variable cylinders from 50 cm<sup>3</sup> to 6,200 cm<sup>3</sup>, seeks distributors for their products. Potential partners should already be involved in the oliodynamic industry as the products are normally an integral part of the original equipment.

## Offer TO 148 Data cable test equipment

This easy to use 8 channel test set is British Telecom approved and is specified for use with computer data cabling and telephone cabling installations. It is powered by a PP3 battery and gives an instant indication

Please respond directly to:  
**The Technology Exchange Ltd**  
**Wrest Park**  
**Silsoe**  
**Bedford**  
**MK45 4HS**

or **Fax:** 0525 860664

**Phone:** 0525 860333

The payment of £10 plus VAT (£11.75) per item should be sent with your requests.

without manual intervention of the state of cabling terminations. Unterminated, wrongly or badly terminated conductors, inter-conductor shorts and earthed conductors are clearly shown. It will be of universal interest to installers and commissioning engineers. Investment partner sought for a 64 channel model, currently at prototype stage.

#### **Offer TO 154** **Range of high efficiency** **fluorescent lighting units**

A range of attractive fluorescent lighting units designed for ease of installation and tube replacement. High frequency electronic ballasts ensure instant start up without flicker using high efficiency tubes and special reflective films. The units are BRECON approved. Each unit is individually switched and can be changed from down lighting to architectural uplighting, either manually or by an infra-red signal. A manufacturing licence is offered for this range which is designed for low cost manufacture and assembly using aluminium extrusions.

#### **Offer TO 163** **Compact brushless DC** **pancake motor**

This ultra slim brushless DC pancake or doughnut motor has been developed for computer peripherals and is only 12 mm thick and 100 mm in diameter. It has a hollow rotor with 40 mm through hole making it suitable for through shaft and servo applications. Especially suitable for hazardous environments with inherent electrical safety. Manufacturing licence offered.

#### **Offer TO 215** **Imaging in opaque fluids**

A wide dynamic range analogue data collection system which is used with ultrasonic transducers for imaging in opaque fluids. Subsequent computer analysis prepares a two dimensional image containing three dimensional information. Manufacturing agreement/joint venture.

#### **Offer TO 216** **Computer linking system**

A patented in-house computer linking system which has virtually no memory, time, or priority overheads. The system links mini-computers, PC's and peripherals in a way which allows access to any computer or peripheral. All protocols are handled by the system for ease of interrogation and file transfer.

#### **Offer TO 217** **Video system for robot** **positioning**

This automated equipment and control system design is used for non-contact high accuracy dimensional analysis from a video image by embedded transputer array. The information generated is used for positional control of an industrial robot - initially developed to remove fuel pins from nuclear fuel sub-assemblies, but the system may be modified for other robot assembly applications.

#### **Offer TO 253** **Computer/Peripheral sharing** **and interconnection**

This PC computer and peripheral sharing system is designed for the interconnection of up to 8 peripherals (printers, plotters, modems etc) with a maximum of 24 computers. The system acts as line driver, serial/parallel converter, automatic printer sharing switch, peripheral grouping system, port contention switch and multiplexer. A manufacturing agreement is offered.

#### **Offer TO 254** **Private telecommunication** **network services**

The UK company specialises in project management of private network systems from strategic and feasibility studies to network design and cost reduction. They prepare and adjudicate ITT's, design cabling systems, troubleshoot, compile OR's and assist with training and recruitment of operators.

#### **Offer TO 255** **A hypermedia computer** **software mechanism for** **information management**

WEB is a new approach to managing information based on a concept of threads which represent particular topics of interest to the user. Information can be linked to a number of relevant threads to allow users to model their ideas. The first product WEB - Information Assistant runs in a multi-window environment on IBM PC and compatibles. Information can be keyed in or imported as a text file and moved from point to point within a WEB or between WEBs providing a powerful HYPERTEXT environment for general information. Links to the users existing word processor, spreadsheet etc.

#### **Offer TO 258** **Cable coupling transformer for** **audio, digital and** **communication systems**

Compact, low cost, coupler will operate round a line pair to enable insertion and/or retrieval of digital or speech information anywhere along a cable length without any physical contact. It is the equivalent of a sliding plug and socket and can be used for telephone sharing, additional loud speakers to extend hi-fi or public address systems. It will cancel common mode noise and since it does not penetrate the cable insulation or sheathing it can be used outdoors, underwater or in hazardous or chemical environments.

#### **Offer TO 260** **Intelligent computer software** **desk and organisation system** **with hard copy binders and a** **computer data transfer system** **and connecting cables**

Filocept is an intelligent desk and organiser which integrates an automatic preset spreadsheet, database, address book, note book, calendars, diary and information sheets producing hard copy in A4 and organiser formats. Printercept enables files including pictures and text to be imported from any computer to any other computer which is made to appear like a printer.

#### **Offer TO 262** **Miniature passive infra-red** **motion detector**

This miniature infra-red motion detector consists of a pyroelectric polymer film and an electronic circuit. The motion detector will switch on a load for a given period of time eg an external light and activate an alarm based on changes in temperature or movement and can also be incorporated into a coded radio transmitter security guard system covering six protected zones. A speech synthesis trespassing alarm version can give a pre-programmed audible warning or welcome message of up to 12 seconds in duration. The low power consumption of the sensor enables modules to operate for up to one year on a single 9 volt PP3 battery.

#### **Offer/Request TO 272** **Computer-based vision and** **sensor systems for the control** **of machine operations**

A company working in the above fields have developed a flexible vision inspection system which incorporates a standard unit with flexible software

which should replace the need for designing individual systems for each customer. It can be easily programmed by relatively unskilled operators and used for many purposes. The company seeks collaboration with OEMs who's products encompass vision systems but who's expertise does not extend to the vision technology.

**Offer/Request TO 282  
Telephone call screening  
device**

A low cost call screening system used on an attended telephone to avoid and deter any unwelcome telephone callers. It can be operated manually by the call recipient and is suitable for use in the home or small business. This product should interest manufacturers of call answering machines and security systems. A patent sale, licence or joint-venture would be considered.

**Offer/Request TO 302  
Micro-code voice encryption  
modules for security in  
telephone conversations**

Various implementations of a voice encryptor on a single system integrated circuit. The modules are highly reliable of low cost, and low power consumption and are easily installed to new or existing telephones or radios. Originally designed as a thick film hybrid, a single chip design is available. An investment partner is required.

**Offer/Request TVA 6  
Broadband communications**

Specialist research and development company for broadband technology, cell relays, signalling software, ATM cells, etc. Company seeks R & D partners for further developments either as joint-ventures or contracts. Consultancy is offered in ATM technology and the sale of existing boards is also offered.

**Offer TVA 8  
Low Voltage control equipment  
and intelligent motor  
protection**

Distributors or licence manufacturer required for a range of low voltage electrical control equipment including vacuum contactors, relays and circuit breakers. Also intelligent motor protection which predicts the lifetime usage of the motor aiding preventative maintenance.

**Offer TVA 10  
CAD-CAM Software for  
maximum efficiency and speed  
in materials usage**

Software design for maximum efficiency in materials usage subject to cutting and punching. Calculates best use of materials by maximising product layout on sheet. Will maximise process for entire line in multiple products which need to be cut from sheets of varying thicknesses. Also appropriate for paper punching and construction, wood cutting and marble cutting.

**Offer TVA 11  
Modular satellite systems**

Licensed manufacture and distribution offered for modular satellite systems used, for example, in hotels for 'pay TV'. Distributors should be able to offer technical services in satellites, TV control, data communications and installation, as well as an after sales service. Manufacturers should be working in a relevant sector and be capable of surface mounting of chips.

**Offer TVA B 17  
Cable system manager for  
large manufacturing plants**

Cable system manager for all types and mixes of cable (electrical, co-axial, optical, etc) including capacity planning for cable runs and automatic monitoring and switching of telecommunications. Joint venture required to customise product for individual EEC markets.

**Request TVA 17  
Multimedia software**

A German company seeks joint venture partner with knowledge of multimedia systems, particular for use in manufacturing industry. Company should have good knowledge of image storage and picture retrieval.

**Offer TVA 26  
Portable data storage device**

Mobile handheld storage device with wide variety of uses from inventory stock control in warehouses to production of parking tickets for Police. Can be used in conjunction with memory cards and a light pen and will drive a separate printer. Licence offered for manufacture as well as distribution rights.

**Offer TVA A 34  
Portable solar powered solar  
cooling system**

Portable cylindrical solar powered and cooled dewar vessels ideal for mobile

use in laboratory, human and veterinary medicine. Particularly appropriate for vaccination campaigns in developing countries. Incorporates a temperature sensor and display, overheat protection and a power failure device.

**Offer/Request ZO 7  
Microelectronics**

A company specialised in microelectronics covering research, production, distribution and servicing in the fields of 3-dimensional micro-structures of metal, plastic and ceramics (eg. fibre-chip couplers, micro coils, micro plugs), seeks cooperation leading to licensing-in technology, reciprocal distribution and purchase of shares in their company.

**Offer/Request ZO 25  
Microelectronics**

Manufacturer of software tools for visualising processes on the PC, hardware and software of sensor technology based on SMD and hybrid technology, especially ultrasound and wireless data transmission, seeks distributors for above products. The company also requests contracts for the development of similar hardware and software.

**Offer ZO 34  
Electronic data processing**

A company who's activities include the repair of electronic assemblies (PCB's) and mechanical components (Printers only), software development and storage supervision, are seeking a distributor or wholesaler interested in Japanese spare parts and repair of Japanese EDP printers.

**Offer/Request ZO 38  
Microelectronics for  
communications**

A company specialising in ASIC design support, training, support for object-oriented programming as well as the development of high-speed silicon bipolar circuits and with a patent pending for a switching network component in BiCMOS technology, seeks a partner for joint development of circuits for mobile communications and optical telecommunications.

**MORE  
NEXT  
MONTH**

# MAILTECH

## ELECTRONIC COMPONENTS

**PROJECT BOXES** A range of high quality boxes moulded in black high impact ABS, easily drilled or punched to produce a professional looking end product

| TYPE | W   | L   | H  | PRICE |
|------|-----|-----|----|-------|
| T2   | 75  | 56  | 25 | £0.77 |
| T4   | 111 | 57  | 22 | £0.92 |
| MB1  | 79  | 61  | 40 | £1.35 |
| MB2  | 100 | 76  | 41 | £1.47 |
| MB3  | 118 | 98  | 45 | £1.71 |
| MB4  | 216 | 130 | 85 | £5.19 |
| MB5  | 150 | 100 | 60 | £2.35 |
| MB6  | 220 | 150 | 64 | £3.95 |
| MB7  | 177 | 120 | 83 | £3.42 |
| MB8  | 150 | 80  | 50 | £2.22 |

All sizes are in millimetres

**MICRO SWITCH** roller arm operation spdt 40p each

**MINIATURE TOGGLE SWITCHES**

|             |          |                                        |          |
|-------------|----------|----------------------------------------|----------|
| spdt        | 60p each | spdt 3 position c/off                  | 70p each |
| dpdt        | 70p each | dpdt 3 position c/off                  | 80p each |
| spdt biased | 60p each | spdt 3 position c/off biased both ways | 70p each |
|             |          | dpdt 3 position c/off biased one way   | 80p each |

**MINIATURE PUSH TO MAKE SWITCH**

**DIL RELAYS** 5 volt dp/changeover 12 volt dp/changeover 60p 10 for £5.00 80p 10 for £6.00 £1.20 each

**RELAY** 10 amp contacts sp/changeover 12 volt coil

**CAR HORN RELAY** in metal can with fixing lug, s/pole on 10 amp contacts £1.00 each 6 for £5.00

**20 AMP RELAY** dp on 12 volt coil £1.50 each 4 for £5.00

**REED RELAY** 12 volt 50p each 10 for £4.00

**240 VOLT AC RELAY**, 3-pole c/o 10 amp contacts £1.50 each 4 for £5.00

**SEMICONDUCTORS - TRANSISTORS - ICs - DIODES - REGULATORS - ETC**

**VOLTAGE REGULATORS**

1 amp 7805/7812/7815 all 33p each, 7905/7912/7915 all 39p each

2 amp 7805/7852/12 54p each

100mA 78L05/78L12/78L15 all 26p each, 79L05/79L12/79L15 all 29p each

Adjustable LM317T 47p each, LM723 29p each, L200 £1.28 each

Transistors TIP2955 70p each, TIP 3055 70p each

2N3053 29p each, 2N3055 70p each, 2N4403 28p each, 2N3819 40p each

**MICRO IC'S** - 280A CPU £1.20; 280A PIO £1.50; Z80B SIO-1 £4.00

**OPTO DEVICES - LEDES - ETC**

5mm rnd red/yellow/green/amber 10p each 12 for £1.00 any mix

5mm rnd high brightness red/green 20p each 6 for £1.00 any mix

5mm rnd flashing red 60p each, yellow/green 70p each

5mm rnd bi-colour 35p each, tri-colour 45p each

LED mounted in chrome bezel red, yellow or green 30p each, 4 for £1

LED mounted in a black bezel red only 25p each, 5 for £1.00

**PLASTIC BEZEL** for 5mm rnd leds 10 for 40p

High brightness bi-colour i.e.d., rectangular, red/green, two leads 40p each

**RESET TIMER PCB**

Gives a timed relay closure following a momentary input. Requires 12V d.c. supply SP c/o relay output LED indication. 19 different time intervals from 25sec to 35min 20sec. £5.98 each.

**UNIVERSAL BELL TIMER**

10 or 20 minute bell cut off + ve or - ve trigger\* timed relay contacts. £4.96

**ALARM CONTROL UNIT**

Single zone alarm control unit built into a domestic light switch box. Ideal for home, caravan, boat, garage, shed etc.

Facilities: - Normally closed loop for pir sensors, door/window contacts etc. Normally open loop for pressure mats. 24-hour loop for personal attack button Visual indication that the system is operational.

Automatic entry/exit delay.

Automatic system reset.

Alarm output cmos logic level.

**PRICE COMPLETE WITH FULL INSTRUCTIONS** £8.95

**Miniature Piezo Siren** 12V DC 100dB with mounting bracket. £4.23

**Internal Piezo Siren** 12V DC 100dB mounted in white plastic box 114 x 114 x 44mm. £4.70

**EX INSTALLATION SENSORS** tested working.

Type 1. Measures 180 x 112 x 70mm with walk test led, relay output and tamper protection. 12 volt dc supply required £8.50 each

Type 2. As above but a smaller unit 123 x 62 x 50mm £11.75 each

Type 3. Ceiling mounting passive, infra red sensor 360° detection, 12V d.c. supply relay output, tamper circuit and pulse count option. Data supplied. £15.70 each

**DOOR/WINDOW CONTACTS**

Surface or flush mounting, white £1.10 each

**JUNCTION BOX** white 6 way 60p

**DUAL TECH SENSOR** Microwave and passive infra-red combined. Separate led indication for each function. Measures 120 x 75 x 50mm. 12 volt d.c. supply. Relay output. Tamper protection. £29.95 each

**ALARM CONTROL PANEL ST3000**

\*Wire free alarm control panel, detectors communicate with the panel by means of radio transmitters\*. Speech synthesis for programming and general operating guidance\*. Built in user programmable telephone dialler\*. Up to 32 transmitters can be used\*. Programmable exit/entry and bell timers\*. Programmable user codes\*. Full installation data supplied, the only thing that has to be handwired is the output to the siren/bell unit (not supplied)\*. These control panels cost over £300.00. Yours for only £59.95.

Suitable **PASSIVE INFRA SENSOR/TX** £25.85

Battery operated, available in 8m range, 10m range or 25m range.

**UNIVERSAL TX**

For connection of normally open or closed contacts e.g. door/window switches, pressure mats etc. £17.63

**CRYSTAL OSCILLATORS**

4.0 mhz ALL £1.50 each

7.5 mhz £1.71

12.0 mhz OR £5.19

18.432 mhz 4 FOR £2.35

33.33 mhz £5.00

**'D' CONNECTORS**

plug socket cover

9 pin 30p 30p 35p

15 pin 40p 40p 35p

25 pin 50p 50p 40p

**SPECIAL OFFER PROJECT BOX**

In white high impact ABS 50 x 70 x 25mm 60p each 10 for £5.00

## BREADBOARDS - CAPACITORS - SOLAR CELLS - HEATSHRINK - ETC

**SOLAR CELL** 2 volt 150mA max, size 60 x 100mm £1.35 each 5 for £6

**BNC SOCKETS** 50 ohm single hole fixing 50p each 10 for £4.00

**MERCURY TILT SWITCH**

Standard on/off £1.00 each

4 Contact (Directional) £1.50 each

**PIEZO VIBRATION SENSOR**

with data sheet £1.00 each

**BREADBOARD**

173 X 65mm 840TP £5.25 each

**TEXTOL ZIF SOCKET**

28 pin zero insertion socket £5.95 each

**6 VOLT NI-CAD PACK** 5AA NI-CADS, fast charge type £3.95

**CAPACITOR** 10,000 mfd 25 volt with fixing clip 60p each

**EPROMS 27C256 - 30 27C512 - 25.** Once programmed but never used eprom. Mounted on a plastic carrier, can easily be removed from the carrier or used with a low insertion force socket.

**27C256** £1.00 each 6 for £5.00 **27C512** £1.20 each 5 for £5.00

Suitable low insertion force socket 28 pin 40p each 3 for £1.00

**MULTITURN PRESETS** 20mm RECT, 500R, 1K, 5K, 10K, 20K, 50K, 100K 1MO. 40p each, 3 for £1.00

**CAR CIGAR LIGHTER ADAPTER (DUAL SIZE)**

mounted on two metres of cable £2.00 each

**100db PIEZO SOUNDER**

2KHz note, 3-12V d.c. 40Ma, 45mm dia. x 26mm £1.76 each

**VIBRATION SENSITIVE ALARM BOARD WITH PIEZO SOUNDER**

Originally a bike alarm. There is a short delay after activation then the piezo sounder operates for a preset period. £3.76 each

or the above alarm board with custom designed case, fixing clip and keyswitch £9.95

**INFRA-RED BREAK BEAM** Transmitter and receiver p.c.b. with 2 lens assemblies. 12V d.c. supply. These are ex-installation units and are not guaranteed to be working. £4.96 pair

**RECHARGEABLE BATTERIES**

AA (HP7) 600 mA £1.02 each C (HP11) 1200 mA £7.64 each

D (HP2) 1200 mA £2.40 each PP3 8.4V 100 mA £4.77 each

**FLOURESCENT LIGHT INVERTOR.** Drives an 8 watt tube directly from 6V d.c. Data supplied £4.50 each

## £1.00 BARGAIN PACKS

### SUB-MINIATURE TOGGLE SWITCHES

P.C.B. Mounting

BO1 S.P. on 4 for £1.00

BO2 D.P. on 3 for £1.00

BO3 3 x D.P. 3 pos. centre off

BO04 DIL SWITCHES 4-way S.P. on 3 for £1.00

BO05 DIL SWITCHES 8-way S.P. on 2 for £1.00

BO06 DIL SWITCHES 12-way 90° sp on 2 for £1.00

BO07 12 x PP3 BATTERY SNAPS

BO08 1 x CAPACITOR 1 FARAD 5.5 VOLT 20mm dia. x 7mm high

BO09 INSTRUMENT KNOBS (0.25" SHAFT) High quality grey plastic knob, collet fixing 15mm dia. 5 for £1.00

BO10 as above but 29mm dia. 3 for £1.00

BO11 4 x MAGNETIC EARPIECE 8 ohm with 3.5mm plug

BO12 4 x 28-WAY TURNED PIN DIL SOCKET

BO13 15 x 12 VOLT WIRE-ENDED LAMPS

BO14 8 x 2 PIN DIN PLUGS screw terminal connection

BO15 2 x LIGHT DEPENDENT RESISTOR Less than 200 ohms in daylight, greater than 10 megohms in darkness

BO16 1 x KEYPAD 20-key in 5 x 4 matrix bubble type switch contacts

BO17 2 x PIEZO BUZZERS approx 3 to 20 volt d.c.

BO18 5 x 78M12 VOLTAGE REGULATORS positive 12V 500mA

BO19 4 x TL082CP bi-fet op-amps

BO20 20 x ASSORTED LEDES full spec. various shapes and sizes

BO21 3 x INFRA-RED DIODE TX/RX PAIRS made by Honeywell (no info)

BO22 4 x CONSTANT CURRENT LED 5mm round, red 2-18V d.c. or a.c. nominal 14mA

BO23 50 x IN4148 diode

BO24 2 x INFRA-RED TRANSISTOR PPT5133

BO25 5 x DIACS

BO26 3 BDX33C 10 amp 100V npn transistor

BO27 12 x 2N3702 Transistor

BO28 12 x 2N3904 Transistor

BO29 12 x BC337 Transistor

BO30 4 x LM317T Variable regulator mounted on a small heatsink

BO31 2 x MAN6610 2 digit 0.6" 7 segment display Com anode, amber

BO32 3 x PHONO TO PHONO LEAD 63cm long

BO33 15 x RECTANGULAR RED LEDES 6 x 6 x 2mm stackable

BO34 1 x PHOTO SENSITIVE SCR mounted on a PCB, data sheet supplied

BO35 4 x IEC Panel Mounting Mains Plug Snap fix

BO36 5 x ASSORTED PIEZO TRANSDUCERS

BO37 5 LENGTHS OF HEATSHRINK SLEEVING 8mm dia. 400mm long

BO38 25 x CERAMIC DISC CAPACITORS 0.1 mfd 63V

BO39 15 x MONOLITHIC CERAMIC CAPACITORS 0.1 mfd 63V, in a dil package

BO40 25 x ASSORTED ELECTROLYTIC CAPACITORS PCB mounting useful values

BO41 25 ASSORTED PRE-SET RESISTORS

BO42 6 x 3-5mm LINE JACK SOCKETS (mono)

BO43 6 x 3-5mm JACK PLUG (mono)

BO44 8 x 3-5mm CHASSIS SOCKET (mono)

BO45 2 x TRIACS 800 volt 8 amp

BO46 12 x BC213L Transistor

BO47 12 x MIN SLIDE SWITCH dpdt

BO48 15 x MIN CERMET TRIMMER POTS (good range of values)

BO49 1 x PCB WITH TWO LARGE LEDES 15mm square, one red and one green

BO50 1 x 12V DC RELAY 4-pole c/o with plug in base

BO51 4 x LM324 quad op-amps

BO52 4 x 555 Timer

BO53 5 x 741 op-amp

BO54 25 x IN4001 diode

BO55 20 x IN4007 diode

BO56 1 x SLOTTED OPTO

BO57 1 x DAC08 Digital to analogue convertor with data

BO58 4 x OPTO ISOLATOR

BO60 3 x C106D Thyristor

BO61 5 x 78M05 VOLTAGE REGULATORS positive 5 volt 500mA

Please use order code when ordering the bargain packs.

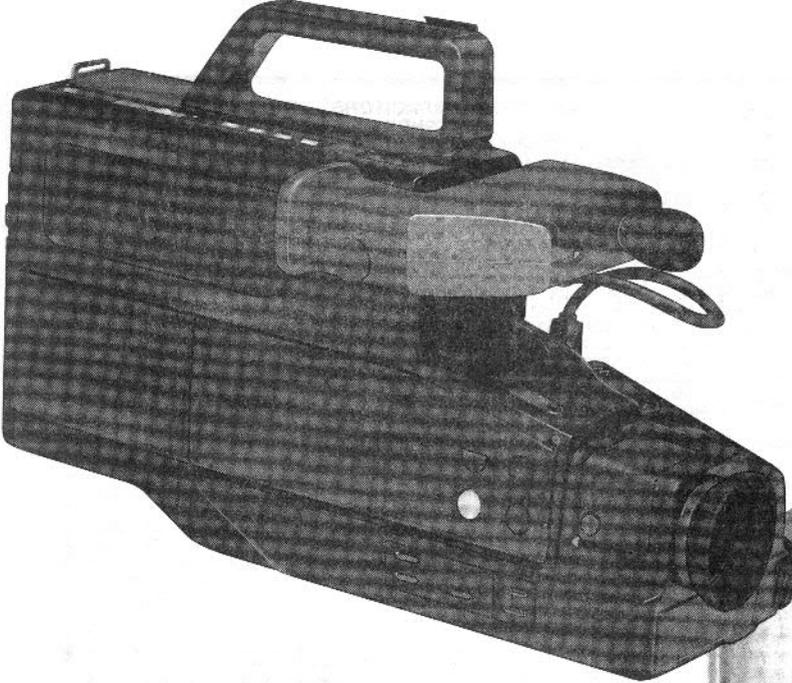
Please make cheques and postal orders payable to Mailtech.

All prices include VAT.

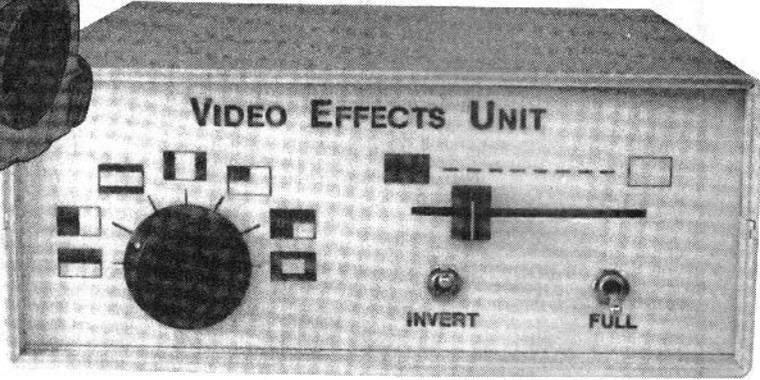
Please add 75p postage to all orders.

At the moment it is not possible to have a full telephone answering service. But we will have the phone definitely manned on Tuesdays, Wednesdays and Thursdays between 10am and 4pm.

Dept EA, Mailtech  
PO Box 16 Ludlow  
Shropshire SY8 4NA  
Tel:058 474475

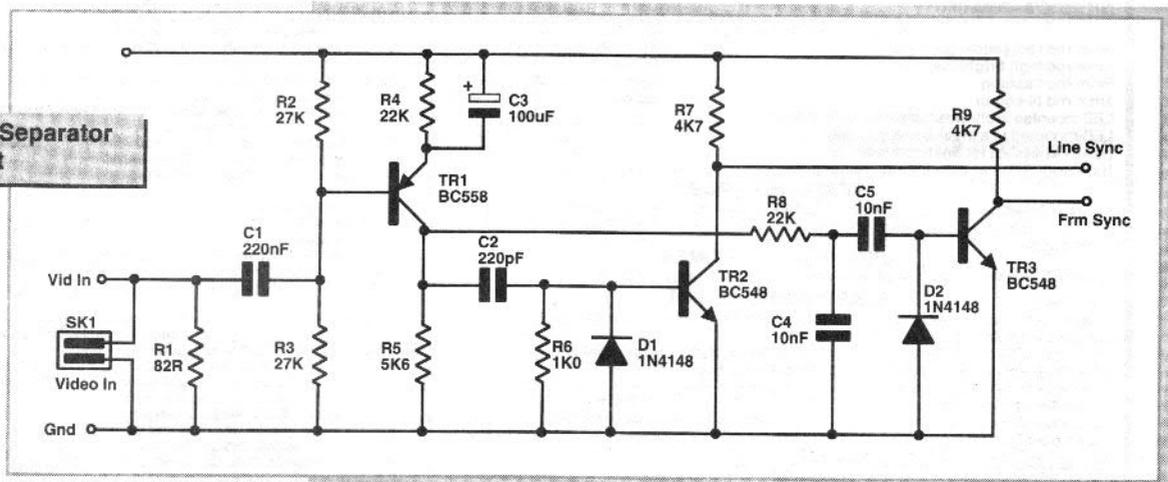


Improve your video editing with this low cost unit! Another ingenious design from Paul Stenning



# Video Visuals

ELECTRONICS in ACTION 32 DECEMBER 1993



**Fig.1 Sync Separator circuit**

**T**here are many times when I enjoy producing my own video compilations of music tracks. This normally involves recording a few hours of music videos from TV and other music programmes, then copying selected tracks onto another tape.

One problem is joining the tracks. Since the inevitable talking over the beginning and end of the track has to be removed, it results in a rather untidy continuity between tracks. A similar situation occurs when editing camcorder tapes and the like.

Digital AV mixers are available commercially, but these normally cost as much as a good video recorder, and so are rather expensive for home use.

### The Works **A**

The complete circuit diagram is shown in Figures 1,2,3,4 and 5. Although this may initially appear complicated, the operation is reasonably straightforward.

On the circuit diagram and in the following description, a '-' after a signal name indicates that the line is active low.

The unit works by selectively blanking the picture. To achieve this, parts of the video signal are

replaced with a voltage level corresponding to black. Monostables and control logic are used to select the portions of the signal to blank.

The video signal enters the unit via SK1, and is terminated by R1. The circuit around TR1 removes the sync portion of the video signal. C2 and R5 convert this to short pulses, which are buffered by TR2. The longer frame sync pulses are able to pass through R9 and C4, and are buffered by TR3.

The Video Effects Unit presented here has a more modest specification, with a more modest price tag!

It should be possible to construct this unit for about £40 including the

case. Setting up is straightforward, and no test equipment is required. Some of the companies and individuals who produce wedding videos could put this unit to good use!

Fig.2 Line and frame delays

**The Works**

The two control voltages are used to control the delay of monostable ICs 2, 3, 5 & 6. These monostables are based around the 7555 IC, which is the CMOS version of the popular NE555. This device was chosen because its delay can be adjusted by an external voltage on pin 5 - this alters the threshold voltage. The level of the control voltage reaching each IC is adjustable over a limited range by the 10K preset pots to allow for component tolerances.

However since the charging waveform on the timing capacitor is exponential, the control voltage does not change the delay in a linear fashion. To overcome this, the timing capacitor is charged from a constant current source, giving a linear sawtooth waveform and therefore linear control of the delay. The constant current source, consisting of a transistor, two diodes and two resistors, gives a (reasonably) constant 60µA charging current for the timing capacitor.

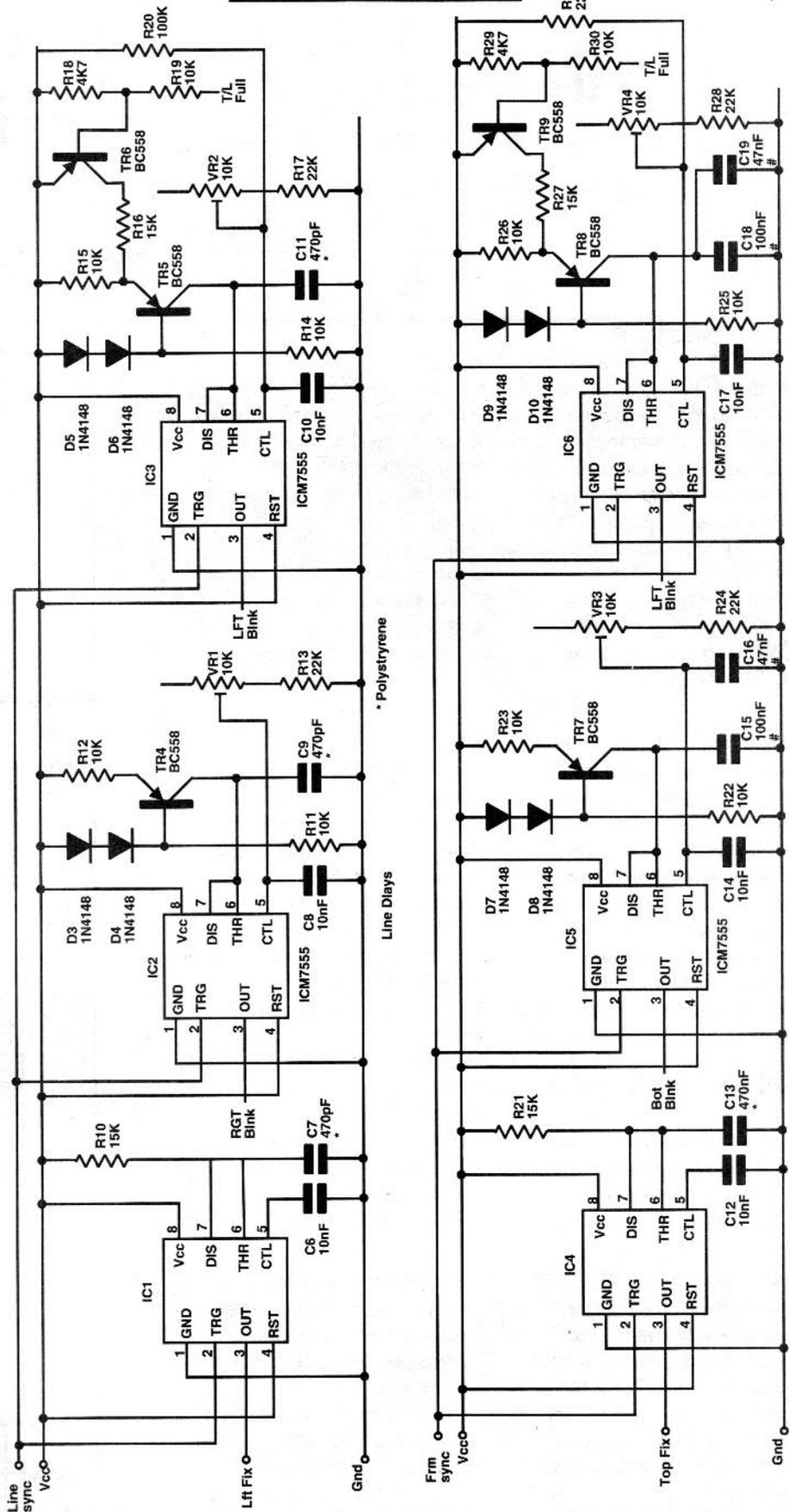
The above arrangement is repeated four times. In the case of IC3 and IC6 an additional transistor can switch a second resistor in parallel with the constant current control resistor, increasing the current and hence reducing the delay. This facility is used for those patterns where the top and bottom, and/or both sides of the screen are blanked, and the delay from the left or top only has to reach the centre.

IC2 and IC5 are controlled from the reduced and reversed control

voltage from the second half of IC11. This gives a control range from the right or bottom of the screen to the centre.

Two additional monostables (IC1 and IC4) give fixed delays for the left

and top of the screen. These are used to ensure that the colour burst and frame sync pulses are not blanked.

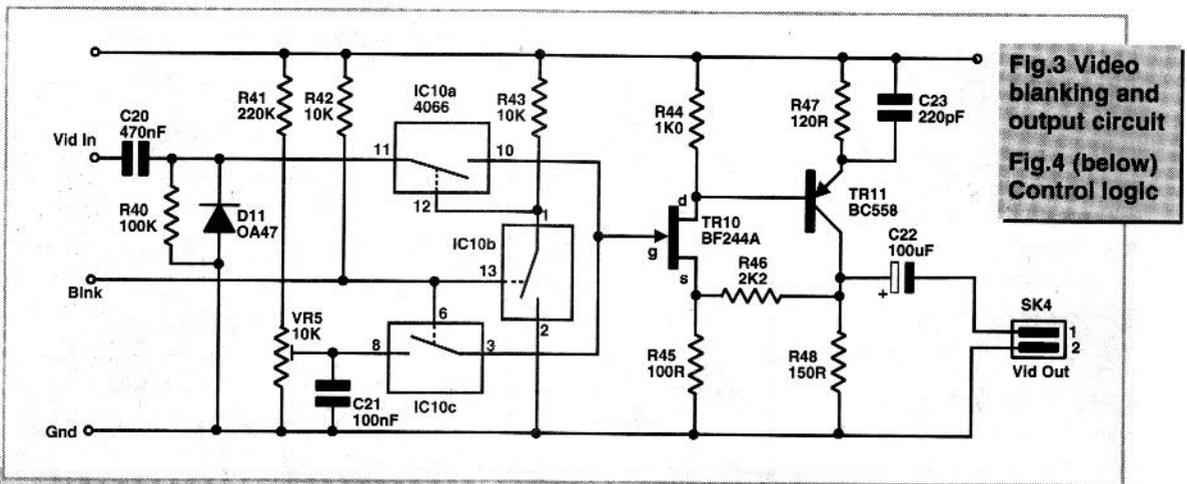


\* Polystyrene

Line Delays

# Polyester/Mylar

Frame Delays



**Fig.3 Video blanking and output circuit**  
**Fig.4 (below) Control logic**

**The Works C**

The BLANK- signal mentioned earlier controls a changeover analogue switch arrangement that switches either the complete video signal, or a DC voltage equivalent to Black level, to the output buffer amplifier. The changeover analogue switch is constructed from a pair of gates in the 4066 (IC10), by using a third gate as an inverter. The incoming video

signal is held with the negative tips of the sync pulses at about 0V by D11 and C20. VR5 sets the DC level for the blanked signal.

The circuit requires a regulated supply of 12V DC at 50mA, this is derived from a 7812 regulator circuit. C29-C33 are decoupling capacitors that are distributed around the PCB.

The unit enables the picture to be wiped to black at the end of a track, and then restored at the beginning of the next track. The recording video recorder would be paused once the picture is black, and the pause released just before fading in the next section.

A 'Full' switch is provided to show the picture when the unit is faded - this is useful for finding the beginning of the next section once the recording machine is paused.

**The full wipe or just the half!**

The unit offers seven wiping effects, all of which are also available in inverted form giving a total of fourteen, these are illustrated in Figure

8.

As described this unit does not fade the sound, however, it would be a simple matter to add a second slider control next to the existing one, and operate both simultaneously. Further comments on this option are given later.

The unit only allows the wiping of one video input to black. Due to sync problems it is not possible to mix two video signals without incorporating the expensive digital techniques contained in commercial products. Broadcasters and professionals use a gen-lock system where all equipment is controlled by one external sync generator, however, domestic video equipment

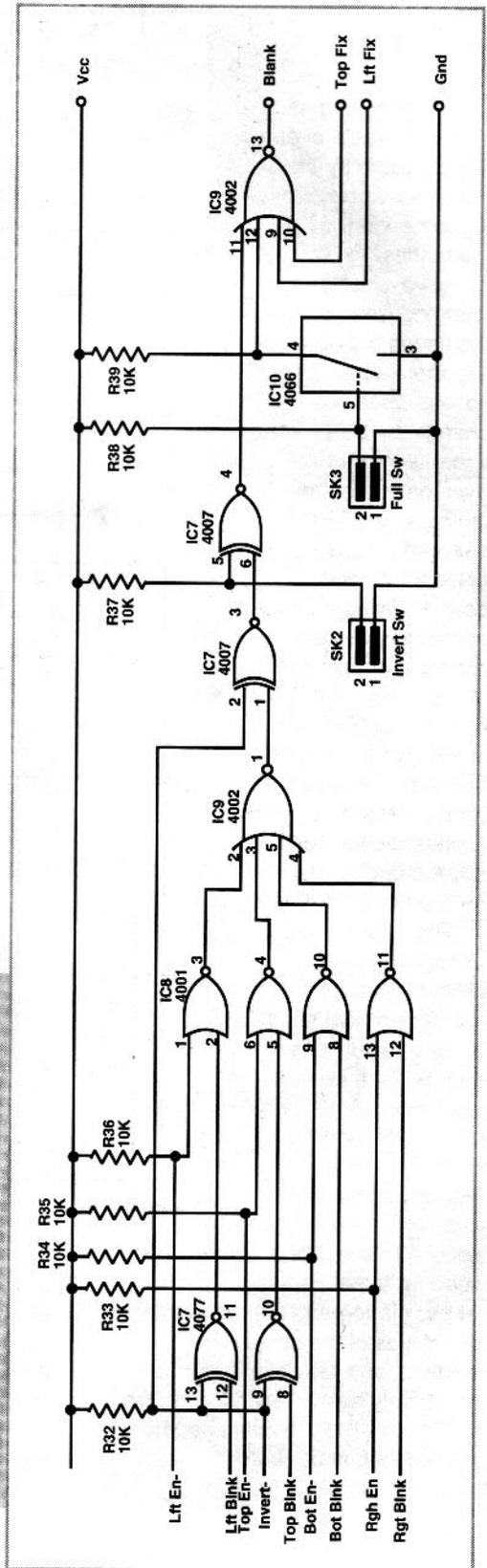
**The Works D**

We now have all the control signals. The next stage is to select which are used, and how they are used, to achieve the selected blanking pattern. This is the job of the Control Logic, which is in turn controlled by the Control Switching.

The first two gates in IC7 (an exclusive NOR gate) are controlled by an INVERT- line from the control switching, and allow the signals from the top and left delay monostables to be inverted. The four gates of IC8 (NOR) allow each of the outputs

from the monostables to be individually selected. The outputs from these are combined with a four input NOR gate, IC9.

The output of this passes to the third gate in IC7, which is controlled by the INVERT- signal. This is followed by the last gate in IC7, which is controlled by the front panel Invert switch. IC9 combines the output from this with the fixed delay signals from IC1 and IC7, and the inverted signal from the Full switch, to form the BLANK- signal.



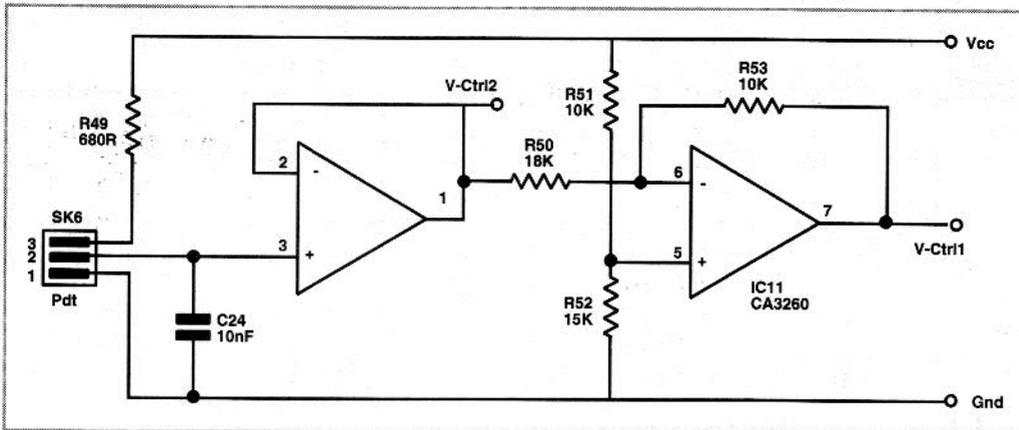


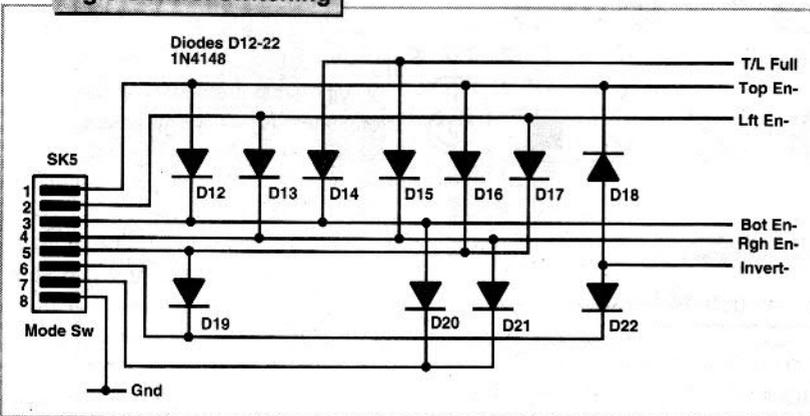
Fig.5 Control amp

**The Works E**

The voltage from the control pot is buffered by half of IC11. This is then inverted by the second part of IC11, and the level reduced to give an output range of 11V to 5V for an

input range of 0V to 11V. Note that the pot is a dual device with the tracks wired in anti-parallel. The front panel Invert switch selects which wiper is connected to IC11.

Fig.6 Control switching



**The Works F**

The operation of the above logic is controlled by the mode switch, via D12-D22 which act as basic logic. The truth table of switch position against control logic levels is shown in table 1. Note that the control lines are pulled high (1) by resistors, the diode logic and switch pull the appropriate lines low (0).

|                 | Mode Switch Position |   |   |   |   |   |   |
|-----------------|----------------------|---|---|---|---|---|---|
|                 | 1                    | 2 | 3 | 4 | 5 | 6 | 7 |
| TOP EN-         | 0                    | 1 | 0 | 1 | 0 | 0 | 0 |
| BOT EN-         | 1                    | 1 | 0 | 1 | 1 | 1 | 0 |
| CONTROL LFT EN- | 1                    | 0 | 1 | 0 | 0 | 0 | 0 |
| LINE RGH EN-    | 1                    | 1 | 1 | 0 | 1 | 1 | 0 |
| T/L FULL        | 1                    | 1 | 0 | 0 | 1 | 1 | 0 |
| INVERT-         | 1                    | 1 | 0 | 0 | 1 | 0 | 0 |

does not support this system. In any case mixing two signals would require three video recorders, which is probably excessive by domestic standards!

**Construction.**

The circuit is constructed on a single sided PCB, 157mm x 134mm, which is available from the EIA PCB service. Component positioning is shown in Figure 6. Before commencing construction, the three PCB mounting holes and the fixing hole for IC12 should be enlarged to 3mm.

The 31 link wires should be fitted first, followed by the other components in the usual size order. D11 is a germanium device and extra care should

be taken to ensure it does not get too hot. The holes for the off-board connections (shown as SK1 to SK7) should be fitted with terminal pins or suitable 0.1" pitch connectors.

The PCB was originally designed for low cost ceramic disc capacitors. However when testing the prototype, it was found that these were not suitable for the monostable timing components. C7, C9 and C11 should be polystyrene types - the leads of these may need to be formed to fit the PCB. C13, C15, C16, C18 and C19 must be polyester or mylar types; polyester types are available in 0.2" pitch to suit the PCB.

IC sockets may be used for the ICs, however the ICs are fairly cheap and

could be soldered directly into the PCB if preferred. In this case they should be fitted last and due care taken to avoid static damage.

The prototype was constructed in a plastic case, 190mm x 165mm x 68mm. A suitable overlay for the front panel is shown in Figure 9. This may be photocopied and fixed to the front panel with clear self-adhesive vinyl ('sticky-backed-plastic' as Blue Peter call it!).

The interwiring is shown in Figure 7. Screened wire should ideally be used for the video signals, but since the cable runs are short this is not essential. Normal hookup wire or coloured ribbon cable may be used for the remainder of the low voltage connections. Take care when soldering to the slider pot as the connection pins are not very tough!

No mains power switch or fuse is necessary, however, a three-amp fuse must be fitted in the mains plug. A suitable cable clamp should be fitted to the case where the mains lead enters. The mains cable may then be connected directly to the transformer tails with a choc-block connector. Since the unit is not earthed, the transformer must be fitted with nylon screws.

**Testing.**

Initially set VR1-VR4 fully clockwise, and VR5 to the centre position. Set the slide control fully to the left, the Effect switch to position one, the Full switch to the off (upper) position and the Invert switch to the lower position. Connect the unit between two video recorders and connect a television or monitor to the second video recorder.

Switch the unit on. If a test meter is available check the regulated supply

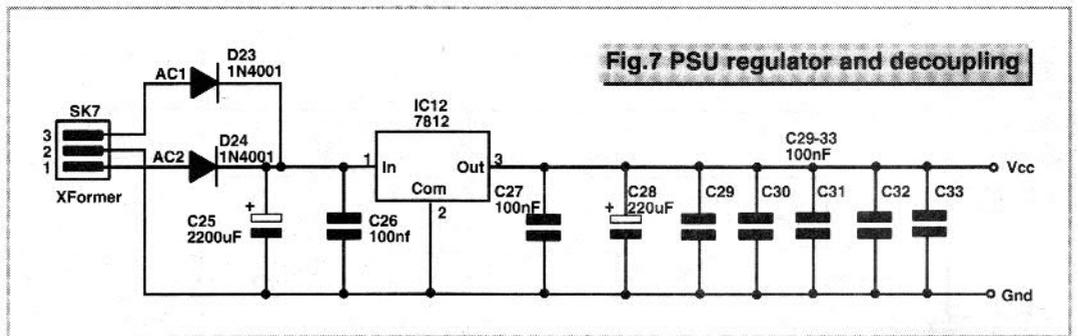


Fig.7 PSU regulator and decoupling

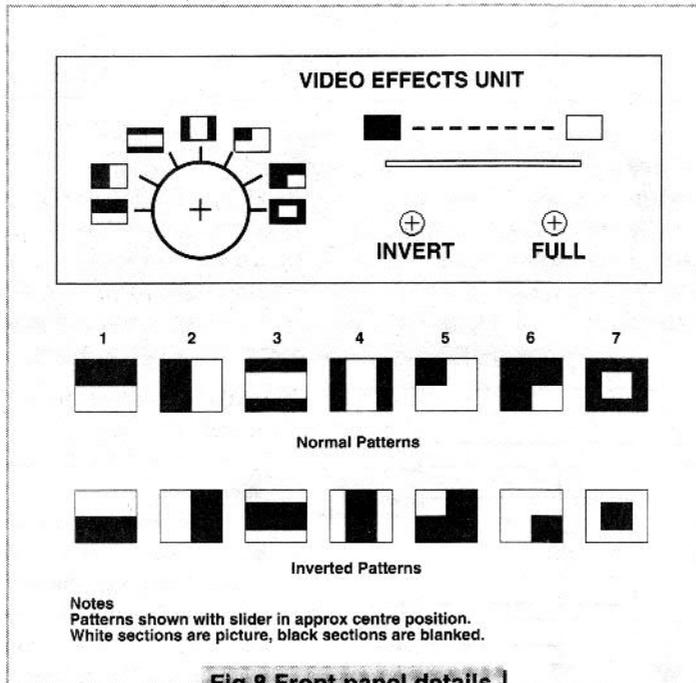


Fig.8 Front panel details

is indeed 12V. The picture on the TV should be blank. Move the slider to the right, and more of the picture should appear as it is moved.

With the slider fully to the right, adjust VR4 to remove the whole black section at the bottom of the screen. If the control is adjusted too far the picture will flicker and may roll. Set the control just before the onset of the flickering.

Now set the Effect switch to position two, and adjust VR2 for no blanking on the right side of the screen. If this control is adjusted too far alternate lines on the screen will be blank; adjust to the point just before this occurs. Check that with the slider fully to the left the whole picture is blank. Careful adjustment of VR2 should give the desired results at both ends of the slider's range.

Set the Invert switch to the upper position and the Effect switch to position three and adjust VR3 as described previously. Set the Effect switch to position four and adjust VR1. In both cases check the operation of the slider control.

With the screen partially blanked, adjust VR5 so that the blanked portion is black. If a testcard is available (try

unused satellite channels) this will provide a suitable black reference. If VR5 is set too far anti-clockwise the picture may roll or pull on some settings of the controls.

Finally check the operation of all the controls. If the unit was constructed with care no problems should occur.

## Options.

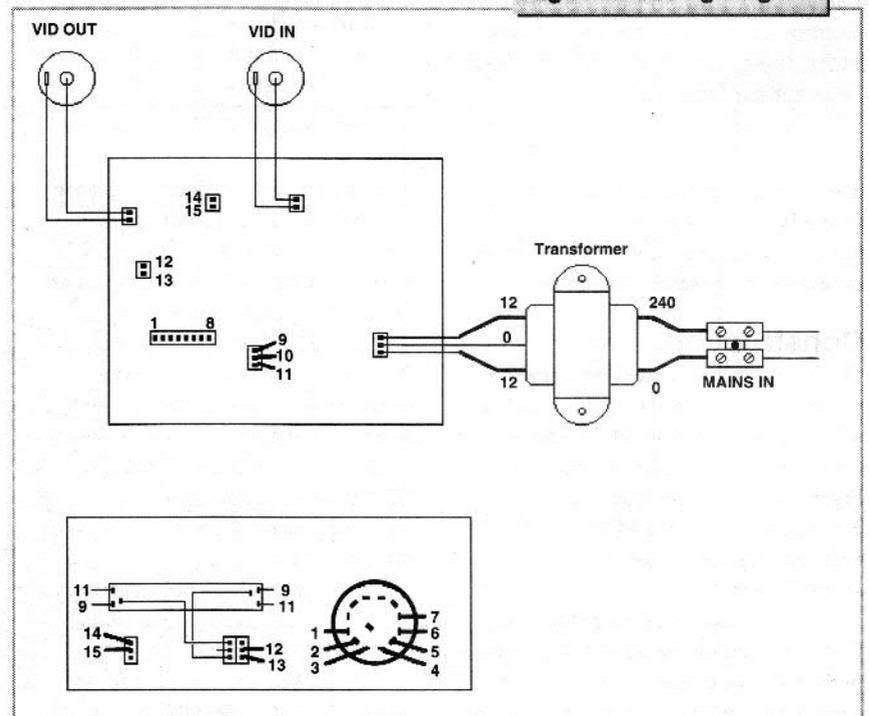
The following suggestions are aimed at experienced constructors, and have not been tested by the author.

This unit does not fade the sound. However if a second dual slide pot (10K Log) is placed next to the existing one on the front panel, the two controls may then be operated simultaneously. This second control is then wired as a passive attenuator in the audio line(s) between the two video recorders. Some constructors may like to construct a mechanical linkage between the two, and have only one control knob.

A possible problem with this arrangement is that the automatic recording level system in the video recorder might try to raise the volume while it is faded. This point should be checked with the equipment being used.

Many people will want to carry out their video editing from the sofa with the aid of the remote controls. The front panel controls on this unit may be mounted separately from the remainder of the circuit, and connected by a length of thin 12 core cable. Not true remote control perhaps, but better than lying on a cold floor for hours!

Fig.9 Interwiring diagram



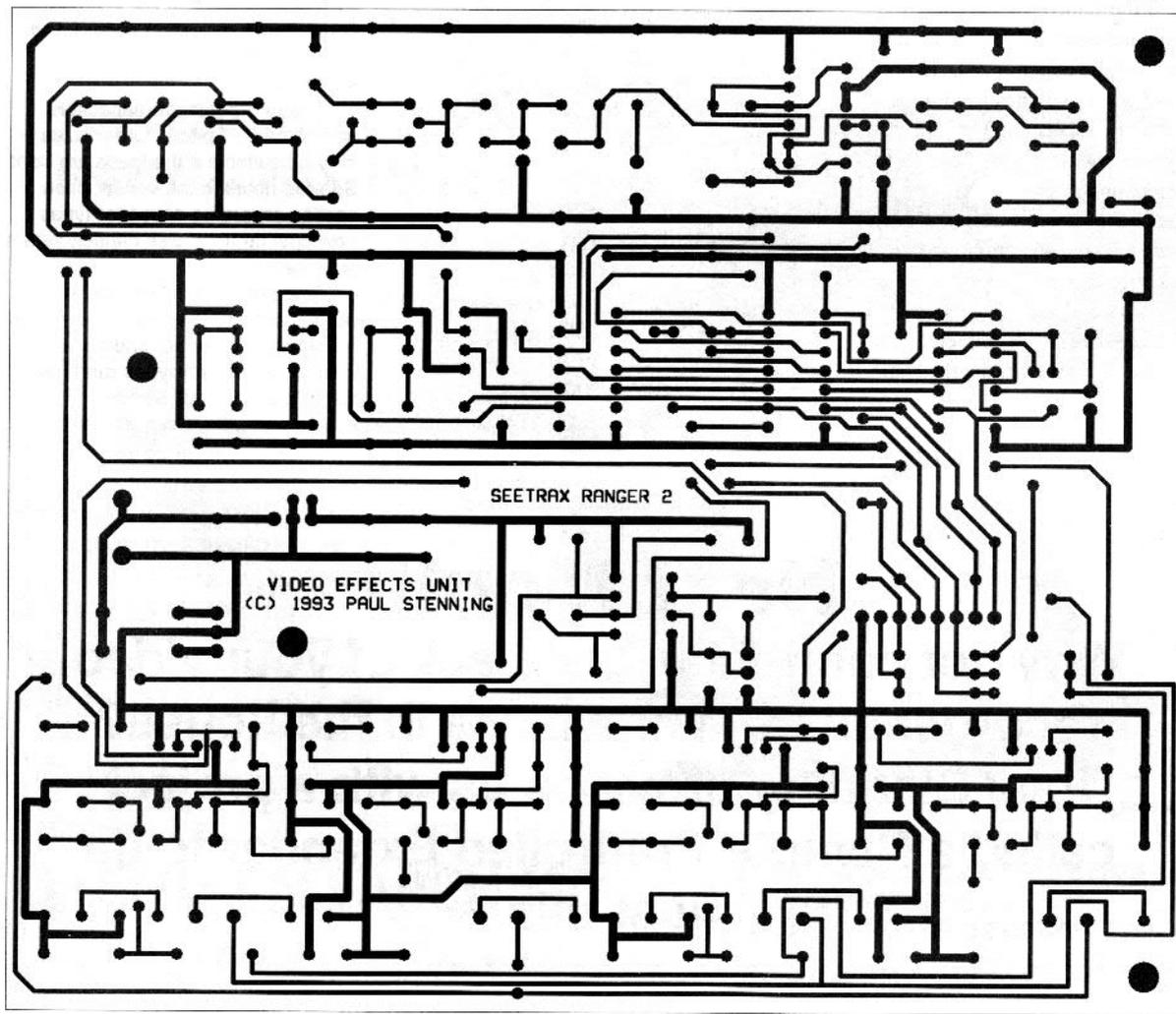
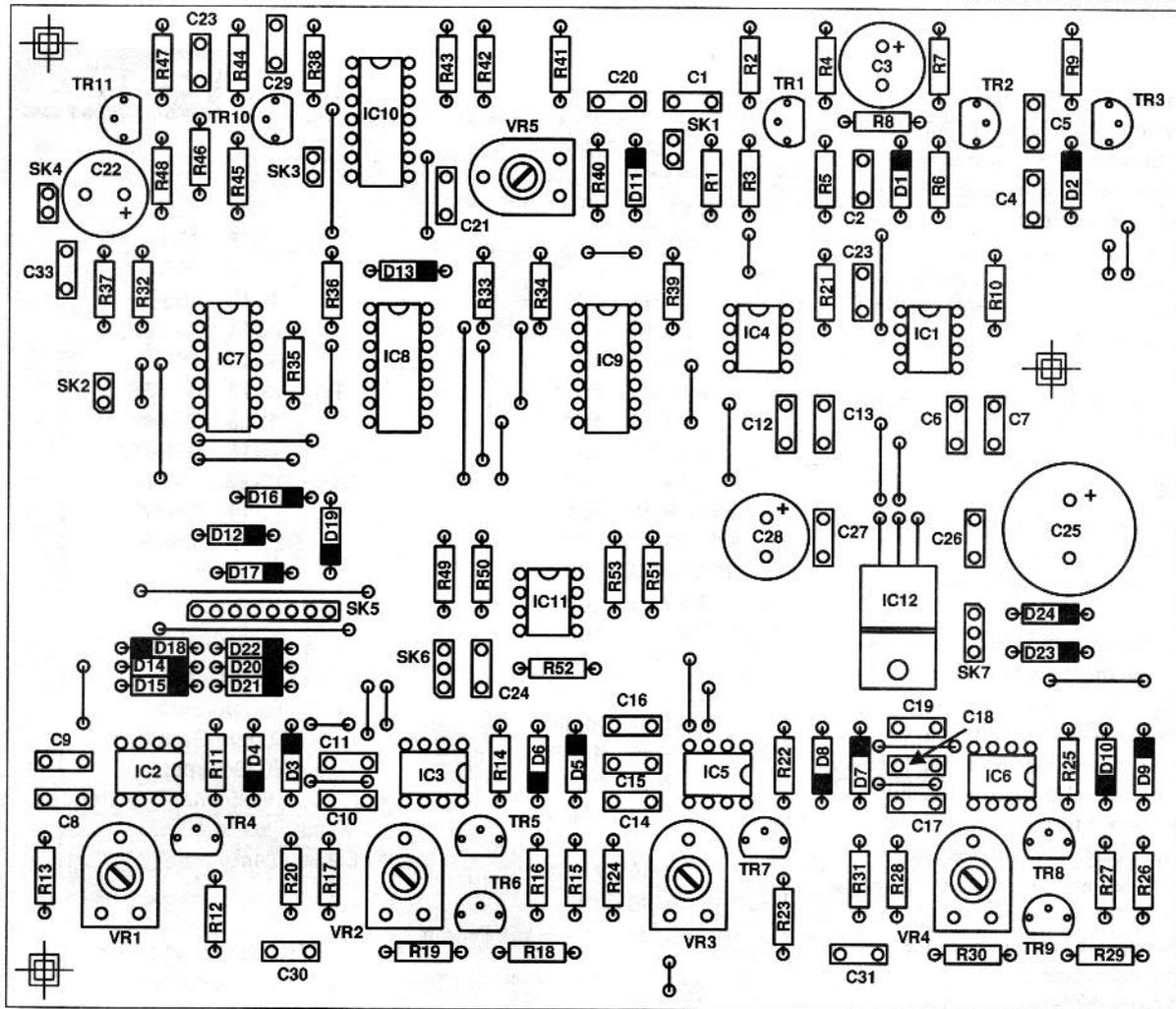


Fig.10 Component positioning and foil

If a second video monitor is available it may be useful to connect this in parallel with the input to this unit, so that the input and output can be monitored independently. In this case R1 should be omitted since the line will be terminated by the input impedance of the monitor. The input impedance if this unit without R1 will be about 10K. This does not apply if the second monitor is a television connected via the aerial socket.

## In Use

The unit is connected in the video link between two video recorders, or between a camcorder and a video recorder.

In normal use the effect required is selected, and the slider is set to the left. The recording unit is set to Record/Pause mode. When the section to be recorded is played, the pause should be released and the slider moved steadily to the right. When the end of the section approaches, the slider is moved steadily back to the left and then the recording machine can be paused again. A new effect may then be selected and the whole process repeated.

When the Effect and Invert switches are operated the picture may flicker. If the same effect is used at the beginning and end of a section then no problems will be experienced. However if either of these switches need to be operated while recording, the Full switch should be turned on first, and off again afterwards.

The Full switch may also be useful for monitoring and searching on the playback machine, while the recording machine is paused.

With your editing complete, your holiday videos may never be the same again!

### Resistors (all 0.25W 5%)

|               |                  |
|---------------|------------------|
| R1            | 82R              |
| R2,3          | 27K              |
| R4,8,13       | 22K              |
| R17,20        | 22K              |
| R24,28        | 22K              |
| R5            | 5K6              |
| R6,44         | 1K0              |
| R7,9          | 4K7              |
| R18,29        | 4K7              |
| R10,16        | 15K              |
| R21,52        | 15K              |
| R11,12,14     | 10K              |
| R15,19,22     | 10K              |
| R23,25,26     | 10K              |
| R30,32-39     | 10K              |
| R42,43        | 10K              |
| R51,53        | 10K              |
| R27           | 12K              |
| R20,40        | 100K             |
| R31,41        | 220K             |
| R45           | 100R             |
| R46           | 2K2              |
| R47           | 120R             |
| R48           | 150R             |
| R49           | 680R             |
| R50           | 18K              |
| VR1-5         | 10K Horiz Preset |
| Slide Control | 10K Dual Lin Pot |

### Capacitors

|           |           |
|-----------|-----------|
| C1        | 220n      |
| C2,23     | 220p      |
| C3,22     | 100µ/16V  |
| C4-6,8    | 10n       |
| C10,12,14 | 10n       |
| C17,24    | 10n       |
| C7,9,11   | 470p      |
| C13,16,19 | 47n       |
| C15,18,21 | 100n      |
| C26,27,29 | 100n      |
| C30-33    | 100n      |
| C20       | 470n      |
| C25       | 2200µ/25V |
| C28       | 220µ/16V  |

### Semiconductors

|             |         |
|-------------|---------|
| IC1-6       | ICM7555 |
| IC7         | 4077    |
| IC8         | 4001    |
| IC9         | 4002    |
| IC10        | 4066    |
| IC11        | CA3260  |
| IC12        | 7812    |
| TR1,4-9,11  | BC558   |
| TR2,3       | BC548   |
| TR10        | BF244A  |
| D1-10,12-22 | 1N4148  |
| D11         | OA47    |
| D23,24      | 1N4001  |

### Additional Items

- PCB
- Case
- 1 Pole 12 Way switch
- DPDT Toggle Switch
- SPST Toggle Switch
- Two BNC Sockets
- 12-0-12V 250mA Transformer
- Mains Flex
- Cable Clamp

### Where to get things

The PCB is available from the EIA PCB service.

The slide control pot was supplied by Maplin. Note that M2 x 12mm countersunk mounting screws and 6mm spacers must be purchased separately.

The non-polarised capacitors should be 0.2" pitch. Other sizes may be suitable if the leads are bent. See the notes in the construction section regarding capacitor types. Low cost ceramic disk capacitors are suitable.

Since the unit is likely to be permanently connected to the mains, a 250mA transformer should be used. The 100mA types run fairly hot at a continuous 50mA.

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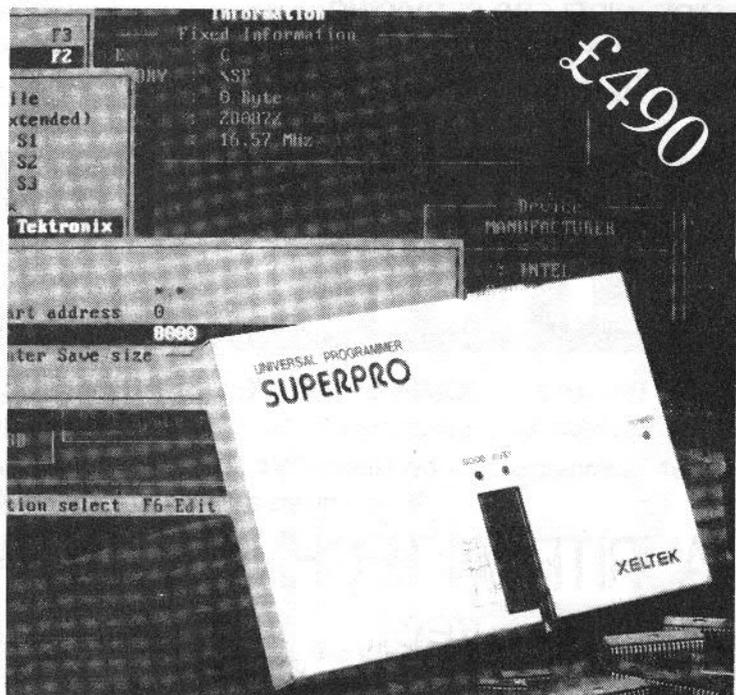
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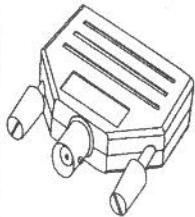
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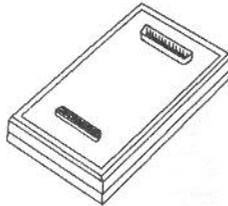
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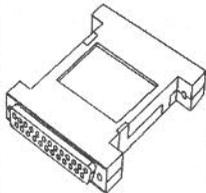
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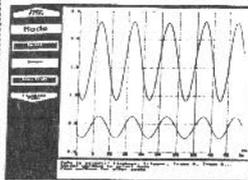
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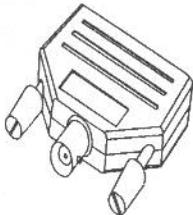
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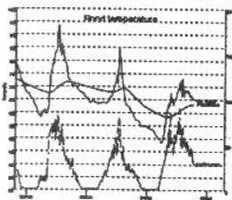
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| Spectrum analyser        | ●      | ●      | ●      |        |
| Audio sampling           | ●      |        | ●      |        |
| Chart recorder emulation |        | ●      |        | ●      |
| Temperature measurement  | ●      | ●      | ●      | ●      |
| Pressure measurement     | ●      | ●      | ●      | ●      |
| Chromatography           |        |        |        | ●      |
| Automotive monitoring    |        | ●      |        | ●      |
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| Education                | ●      | ●      | ●      | ●      |

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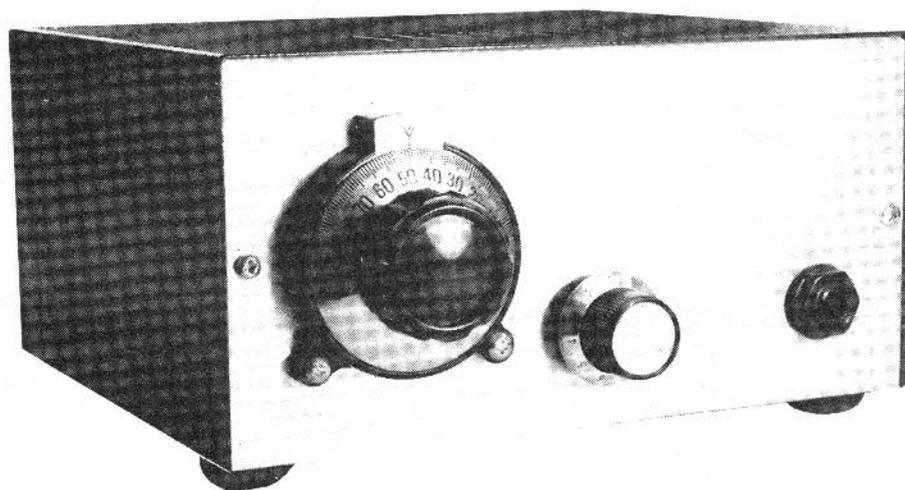
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# Listening on 15 metres

A direct conversion receiver by David Silvester G4TJG



which all of the other RF circuits are tuned. Other than the first RF stage that mainly provides isolation of the antenna from any oscillator feedback in the mixer, all the gain occurs at audio frequencies. For the AF gain we use a number of op-amp circuits and a power IC to drive either headphones or a small loudspeaker. Tuning can be performed without any test gear, although it is advisable to try to use a frequency counter to set up the oscillator scanning range. At a later date I plan to add a digital frequency display to the design, providing that the performance is not degraded by the addition.

## Mode of Operation

The receiver has been built on two PCBs separating the oscillator from the rest of the receiver. The oscillator is contained in a separate aluminium box within the receiver's main case to both provide a stable environment for the oscillator and prevent spurious inputs to the main PCB. Output has been set up

commercial communications receivers are expensive. Setting up the receiver would be impossible without the necessary test gear to inject the intermediate frequencies for alignment of the tuned frequency amplifier stages.

By accepting a number of limitations I was able to use the direct conversion principal to allow a receiver

**A**mateur radio receivers are expensive, or should I say the ones that you can buy are expensive, and this will put off people who are interested in radio but cannot afford a commercial receiver. The reason is shown Figure 1. After the RF input stage, the oscillator and mixer convert the incoming frequency to

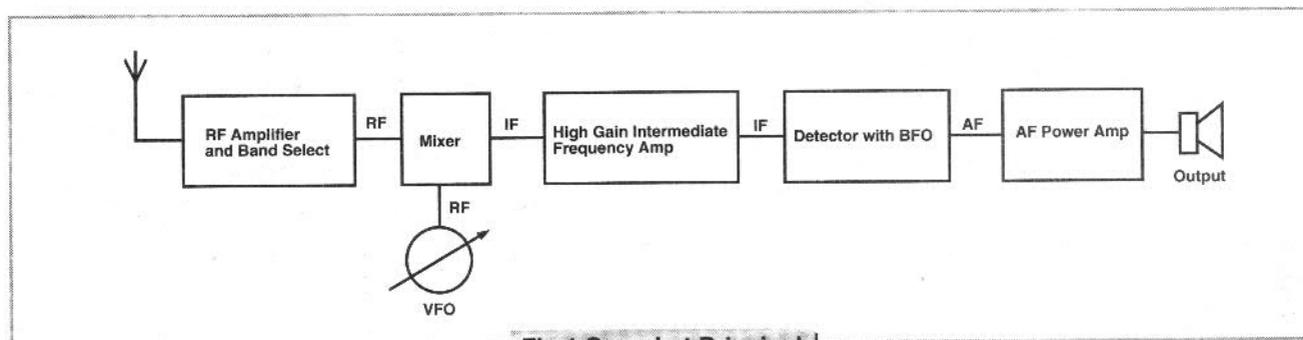


Fig.1 Superhet Principal

another radio frequency. This intermediate frequency is amplified before conversion to an audio signal in the detector. The last stage is the power amplifier that drives the receiver's loudspeaker. This is the layout of a very simple single conversion superhet receiver. Many commercial receivers use dual conversion, dual oscillators and two intermediate stages. There will also be a range of RF input filters for the bands of interest. It is little wonder that

to be built at home, since the design substantially reduces the alignment difficulties. The saving in complexity of the communications receiver, building for a single frequency band, and constructing at home brings the cost of the receiver to around £70.

Figure 2 shows the basic layout of a direct conversion receiver. There is now only a single oscillator running at the incoming 'received' frequency to

for headphones as this allows the constructor to use the receiver without annoying the other members of the family, although a loudspeaker can be used if a single resistor is shorted out. I have used all the circuits myself previously, and they have proved to be reliable and easy to set up. Many have been adapted from articles in either 'Solid State Design for the Radio Amateur' or 'QRP Classics', both published by the ARRL.

## Circuit Description

The VFO

The oscillator is of the standard series-tuned Clapp type, named as are all oscillator designs after the man who first proposed the circuit. Oscillator stability is vital in the receiver if the radio is to fulfil its function. While common in the valve era, the Clapp oscillator has been forgotten in semiconductor designs. The advantage of the Clapp circuit over the Colpitts or the Hartley is that the inductance of the coil in the Clapp oscillator is around twice that in the alternatives, which eases the physical design problems in this area at higher frequencies. Also the stability of the circuit is increased with the higher inductance. This circuit in Figure 3 was designed to allow other frequencies of operation and therefore contains a few component spaces that are not used in the 15 metre (21MHz) receiver but may be required in other frequency bands. L1 with the series capacitance of C1 and C2 forms the tuned circuit. The tuning capacitor is connected across 'Conn1' to 'Conn2' and may be either of two values. Using a 25pF capacitor results in a tuning range slightly less than the full 15 metre amateur band but makes tuning easy as the tuning control is less sensitive. This may be suitable for those constructors interested in either the SSB or CW portion of the band. For the full band a 50pF tuning capacitor should be used, but this will result in coarser tuning control. Final adjustment of the range is carried out with C1 and C2. Two variable capacitors have been used to distribute the RF current for oscillator stability and allow ease of tuning. The full oscillator range can be set from around 15MHz to about 26MHz. With the two capacitors set around the half meshed position, 21MHz is achieved.

The upper section with ZD1 and IC1 provides highly stable supply voltages, essential if the oscillator is to have an output frequency that remains stable enough for SSB or CW listening. The circuit around Q2 is a buffer stage with enough amplification to allow the correct drive level at the output.

The final stage of Q3 to Q6 is a high impedance to 50 ohm B class RF buffer, designed so that the double balanced mixer SBL-1 on the main PCB gets the correct drive impedance level.

## The Main PCB

The rest of the circuit is constructed on a single PCB on which the upper layer acts as a groundplane with the signal

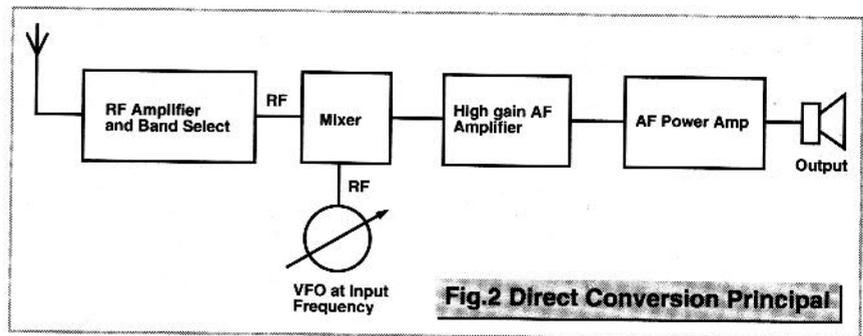
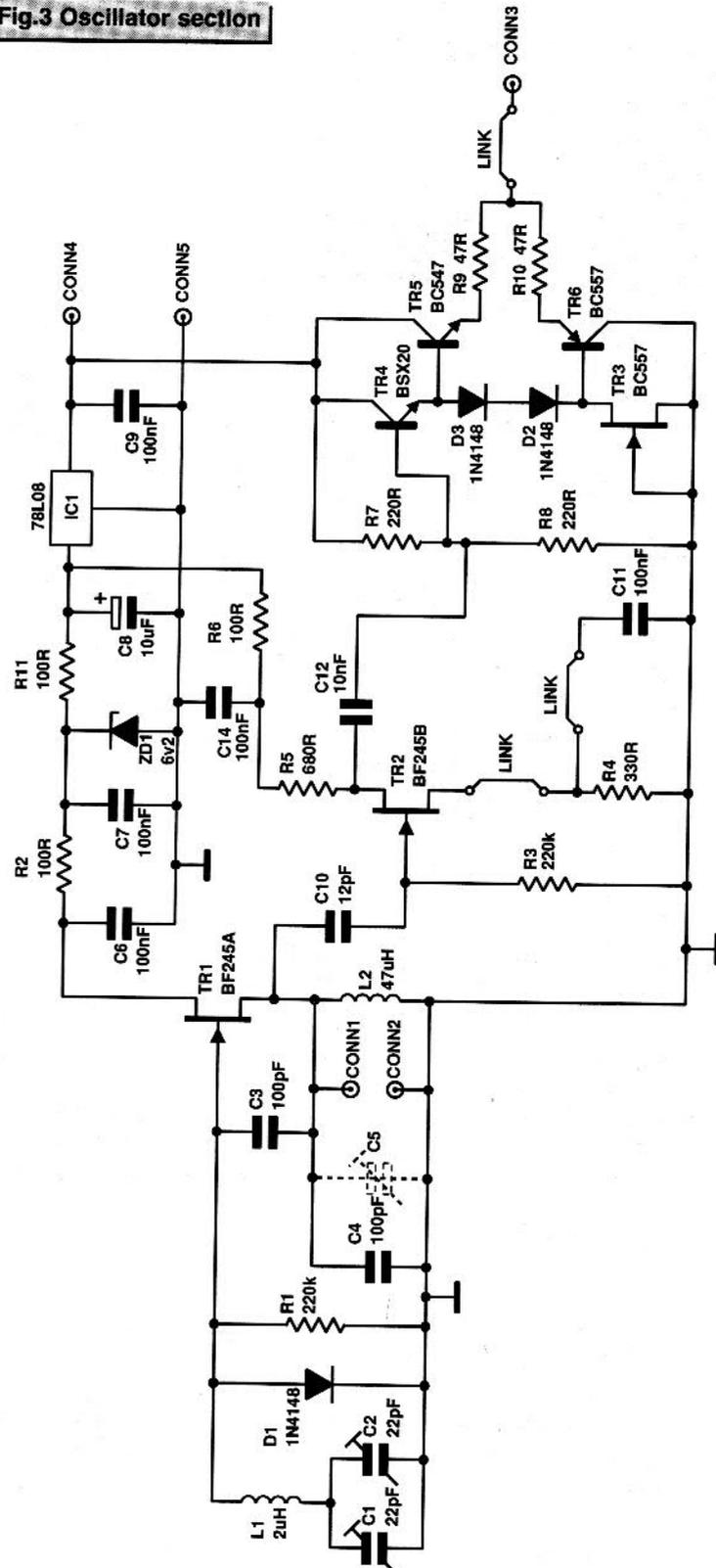


Fig.2 Direct Conversion Principal

Fig.3 Oscillator section



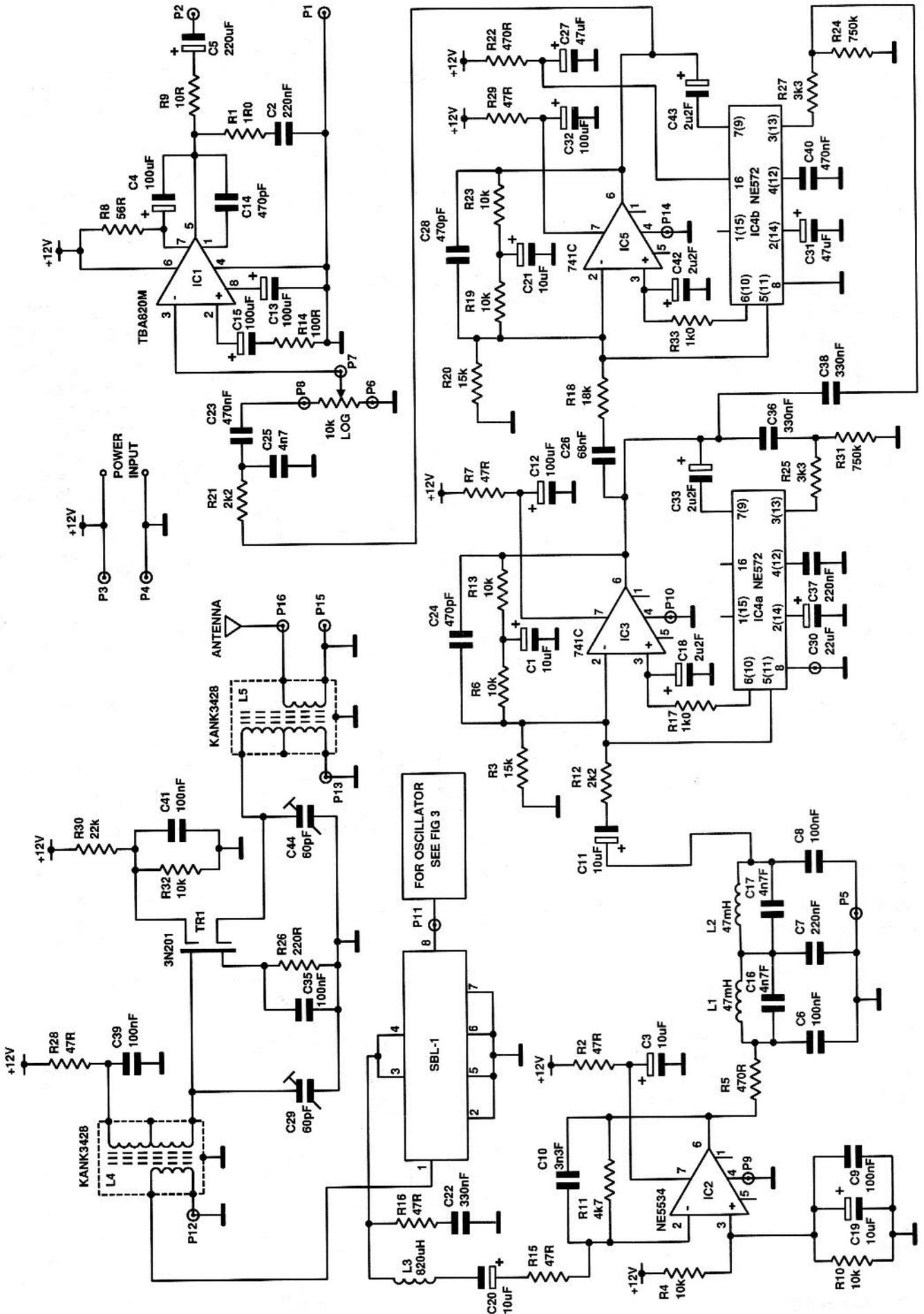


Fig.4 15m Receiver Circuit

tracks on the lower layer. Again, this PCB has been designed for use with several different frequency bands, so that in the RF section some components may be missing. These are noted in the parts list. Figure 4 is the schematic for the main PCB.

There are 17 pins on this PCB, some of which connect the lower PCB track to the upper groundplane. Others are for off-board connections. The rest connect both the lower tracks and the upper groundplane, or go to off-board wires. The circuit around L5, L4 and Tr1 is the RF input amplifier buffer stage. This feeds the RF input of the Double Balanced Mixer SBL-1 where the sum and difference frequencies are generated. The difference is an audio frequency and is selected out by the circuit of L3, C20 and R15 (the input to the first op-amp stage). All the rest of

and IC5. This is an AF gain-controlled amplifier in which IC4 provides a variable feedback resistance to the inverting op-amp circuits of IC3 and IC5. This circuit was originally proposed by DF4SQ in the Autumn 1991 issue of SPRAT. (This magazine, which comes with membership of the G-QRP club, is a mine of information for designing simple radio circuits). These circuit units give an automatic gain control action that prevents the variability of the incoming signals resulting in the listener tearing off the headphones in pain when a strong signal is received.

## Construction

### The VFO

The VFO is built on a single sided PCB, as stray capacitances between an upper groundplane and signal tracks on the

keeping the second winding to the right of the first. This is the natural way for a right handed person to wind the core. Left handed persons should start with the short wire towards them and wind keeping the long end to the left. Continue for the full 22 turns, so that the wire passes through the toroid centre 22 times. Distribute the turns evenly around the core. If the winding is correct, when you look at the core with the wires pointing away from you, the upper wire should be to the right of the lower. See L1 on Figure 5. If the wires need to cross over to fit in the holes, or the core does not fit exactly with the position in Figure 5, then you will need to start the coil winding again from scratch. If all is OK then scrape back the insulation on the wire and solder L1 to the VFO PCB. There should be no difficulties with the rest of the building of the VFO PCB. Note that C5 and C13 are not used in this design as the PCB was laid out for use at other frequencies as well as the 15 metre amateur band shown here. Equally L3 is not used, but a shorting wire is installed in its place. Should the constructor desire, pads are available to scale the VFO for many frequency bands without modification. The only criteria for the double balanced mixer is that it receives 5mW of power at 50 ohms, equivalent to around 2V peak to peak at the output pin 'Conn3'. Put this board aside for the mechanical construction stage.

### The Main Receiver PCB

The main PCB is a double sided board in which the upper layer is used solely as a groundplane. During construction you will need to cut back the holes around most of the components to prevent shorting to ground. The kit PCB will be cut back during processing. However, the main PCB has 17 connections, labelled P1 to P17. The separate table lists the types, and the solder connections that the three types need. In some cases the upper groundplane MUST NOT BE CUT BACK or a faulty connection will result.

Let us start from a home constructed PCB. In this case it is only necessary to etch the lower surface while protecting the other side as a full groundplane. Drill all the holes at 0.8mm except the connectors which are 1mm. Locate the position of the five ICs and cut back the groundplane around the holes for all of them. Insert and solder down IC sockets for each IC. These provide a good reference point for the rest of the layout. Using the

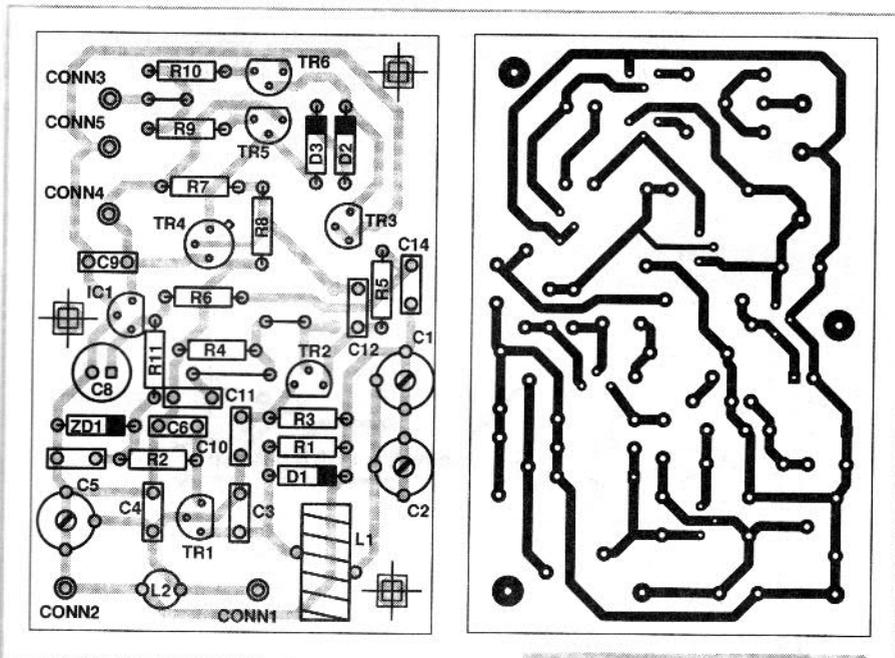


Fig.5 Oscillator component overlay and foil

the signals are shorted to a 50 ohm 'waste' line of R16 and C22. As the 3dB cut-off of the two circuits is the same, the mixer should see the fixed 50 ohm impedance that it needs for correct operation. IC2 is a very low noise op-amp circuit with an inverting input layout and a gain of times 100. For this device, you can substitute a slightly noisier LF351 or TL071 op-amp.

L1, L2 and the associated circuit form a high cutoff low pass AF filter to attenuate any signals outside the 3.3kHz SSB band. The final stage around IC1 is the power amplifier driving the headphones or loudspeaker. For loudspeaker operation R9 should be shorted out.

This leaves the circuit around the two halves of IC4 with the op-amps IC3

lower layer are very variable, causing oscillator frequency instability. Locate the five off-board connections 'Conn1 to Conn5' and solder in the terminal pins. Drill holes for the PCB stand-offs where the large pads are shown.

The main inductor L1 is wound on a T50-6 toroidal core. Take about 2ft (60cm) of 26SWG (0.018 inch or 0.045mm) enamelled copper wire. Gently pull this straight and place the toroid on the wire leaving about 4 inches (10cm) for one of the connections. With this short end pointing away from you, take the longer end and wind this around the toroid and through the hole again from below

separate table fit and solder the connections, being extremely careful over those that have the upper groundplane cut back. I have used a 1/8 inch (3mm) drill mounted in a file handle to cut back the groundplane. The upper groundplane acts as a good thermal heatsink as well as a good electrical conductor, so that you need a large soldering iron to prevent cold joints. A better option is to invest in a temperature controlled soldering iron. With a large bit they have enough power to get a good solder joint to the groundplane but the bit can be changed to a small one to protect the semi-conductors that have to be soldered in at a later stage. It is unlikely that the amateur will need to buy another iron, for many years, such is the reliability of the temperature controlled unit.

Having got to this stage the rest of the holes can have the groundplane cut back from them. Drill holes for the PCB stand-offs. Now we come to the PCB construction proper. Of the components shown in Figure 6 only C34 and C45 are missing as they are not needed in the 15 metre receiver. Space has been left for them should the receiver be built for other frequency bands.

Due to the crowded nature of the PCB and since the semiconductors can be plugged in at the final stage it is best to start from the centre near P10. By taking care to select components, it is possible to build the PCB without ending in a position where it is very difficult to solder a component blocked by others. In Figure 6 many of the components are shown with a stub wire, such as C3 in the upper left corner. This is a radial electrolytic capacitor which has the negative wire pulled to the side for soldering to the upper groundplane, while the positive terminal passes through the PCB to a pad on the lower surface. Figure 7 shows the side view.

When connecting the coils L4 and L5 the case sides are pulled out and soldered to the upper surface. Take your time over construction, as a lot of care is needed. When complete hold the PCB for final construction.

### Final Assembly

Take the main case and remove all the panels. The slow motion drive should be fitted to the left of the front panel so that the outside ring is about 1/4 inch (5mm) from the left fixing screw. Drill the necessary holes and fix the drive to the front panel. There is a small screw to prevent rotation of the drive on the inside of the front panel and two screws

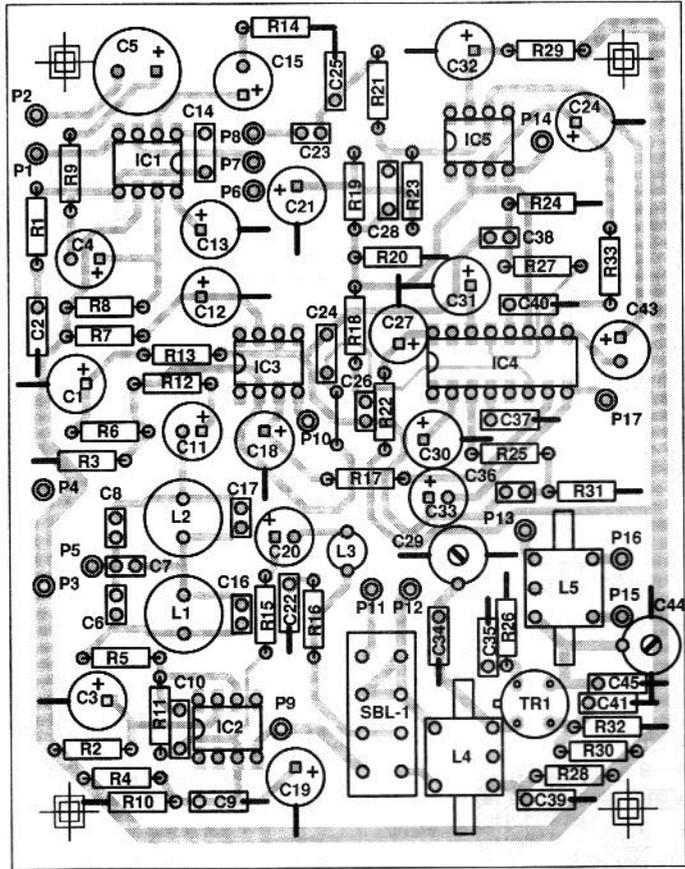
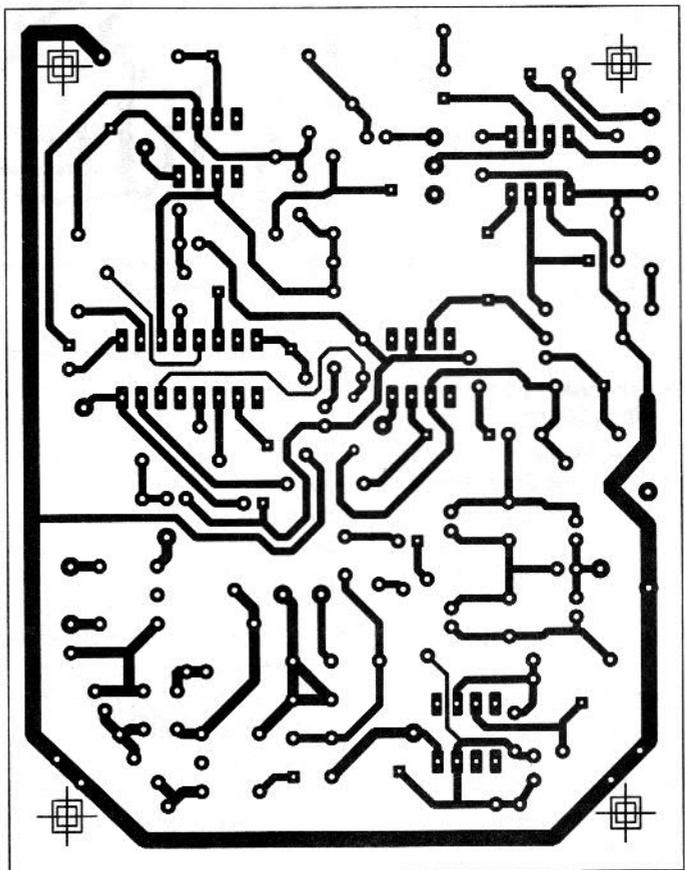


Fig.6 Main board component overlay and foil  
Note connections to ground plane on top surface



## Oscillator Section

### Resistors

(all 0.25w metal film)

- R1,3 220K
- R2,6,11 100R
- R4 330R
- R5 680R
- R7,8 22R
- R12 shorted out

### Capacitors

(All with 15V rating or greater) Lead spacing in brackets is in inches. **THIS SPACING IS VITAL IF COMPONENTS ARE TO FIT IN THE ALLOTTED SPACES.**

- C1,2 22pF Variable
- C3,4 100pF (0.2) polystyrene
- C5, C13 Not used
- C6,7,9,11,14 100nF (0.2)
- C8 10µF (0.1)
- C10 12pF
- C12 10n

### Semiconductors

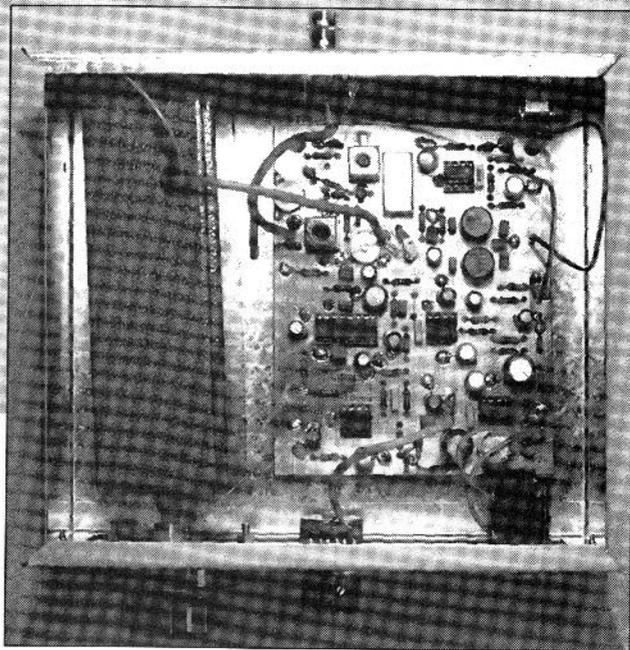
- Tr1 BF245A. Other BF245 Idss groups may be substituted but with modified gain and stability.
- Tr2,3 BF245B. Note for Tr1 applies
- Tr4 BSX20 or 2N2222
- Tr5 BC547 or equivalent
- Tr6 BC557 or equivalent
- D1,2,3 1N4148
- ZD1 6.2V 400mW zener diode
- IC1 78L08 8 volt regulator

### Inductors

- L1 22 turns of 26SWG enamelled copper wire wound on a T50-6 core [Circuit Part No. T50-6] approx. 2µH
- L2 47µH Toko 7BS series Part No. 283AS-470J [Circuit]
- L3 Shorted out, not used in the 21MHz oscillator

### Additional Items

- Case - See component list of main receiver
- Grommet
- Small Coax - I could not source the preferred 50ohm
- Tuning capacitor: See text for value required by the constructor. Either 25pF or 50pF
- PCB as in Figure 5
- Terminal Pins (5 needed) see text for important note on use
- PCB Stand-offs (4 needed) [Circuit LCBSB401A]
- Hookup wire



through the panel from the front. The external screws will be M3, needing 3mm holes in the panel. With the front panel in place, mark and drill holes for the volume control and the PO pack plug that is the headphone connector. Ream out as necessary, then remove all of the items from the front panel, but screw the front panel onto the main case bottom for the next stage.

Take the aluminium box, and on the short side nearest the front panel (see photo of the inside for orientation) draw a line on the outside down the centre, with the box lid towards the right. Place the aluminium box in the main case and align this line with the hole for the slow motion drive; then draw a horizontal line at the centre, making sure that the aluminium box is pushed squarely against the main case's base. Due to the way that the aluminium box is made, the sides are not perpendicular to the top and bottom so that the rear end of the box will lean closer to the main case's left-hand panel. Where the two lines cross on the aluminium box drill a hole for the tuning capacitor and fit it into the aluminium box. Now refit the slow motion drive to the front panel. Fit the

tuning capacitor with the vanes towards the bottom of the main case. This eases the wiring of the VFO PCB to the tuning capacitor. Connect the drive shaft from the tuning capacitor to the hole on the shaft from the slow motion drive and fasten the locknut. If all has gone well, the aluminium box will rest against the bottom of the main case. Carefully measure a distance from the left hand edge of the main case to the centre of the aluminium box and drill two holes through the base of the main case and the aluminium box. The two may now be secured together. I used a pop riveter in the prototype although screws are acceptable. When done, check that the zero position of the slow motion drive corresponds to the fully meshed plates of the tuning capacitor, as this results in a higher read-out number corresponding to a higher frequency. Final wiring is very simple. Glue the

VFO PCB onto the aluminium box with the terminal pins 'Conn1' and 'Conn2' closest to the tuning capacitor. Connect 'Conn1' to the grounded rotating plates of the capacitor and 'Conn2' to the fixed plates with tinned copper wire. A small hole in the top of the aluminium box and a protecting grommet takes the power supply (+12v to 'Conn4' and ground to 'Conn5' and a piece of the small 75ohm coax connected to 'Conn5' and 'Conn3' with the centre wire going to 'Conn3'. If a frequency counter is available, it is advisable to set the scanning range of the VFO by setting C1 and C2. Without this aid the vanes on both should be set to half meshed, with final tuning done from off air signals.

Stick the main PCB into the main case on the stand-offs. Drill holes in the back panel of the main box for the BNC connector that connects to the antenna

and the power socket. Power is supplied to the PCB via P3 (+12V) and P4 (Ground). The VFO coax wire connects to P11 (central signal wire) and P12 (screen). The headphone connector goes to P1 and P2 with P1 as the ground and therefore the connection on the PO jack closest to the panel. The aerial connects from the BNC to P15 and P16 with P15 being the ground connection to the screen. Finally, plug in the ICs.

## The Aerial

The aerial I used is a very simple affair. My back garden is just long enough to take a 20 metre dipole on the diagonal, so for the 15 metre receiver I set up a dipole antenna with longer guy wires. The aerial is made from strong PVC-covered copper wire available from a local radio shop and has an insulating unit in the centre to which the feeder is connected. This is a section of 75ohm twin feeder that can fit through the window seal without damage. Between the feeder and the coax to the radio itself is a simple balun. This consists of a toroidal ferrite core, T72-26, wound with a pair of 26SWG wires that have been twisted together. One end is connected to the balanced feeder and the other end with coax to the receiver. Everything should now be ready. Grit

your teeth and apply power to the radio. There should be a noticeable difference in output volume of the background hash with and without the aerial. This is a good sign as it shows the receiver noise is below the background which forms the limit for the reception. None of the components should become warm at any time. Try tuning for a signal. If one can be heard, use this to set the positions of C29 and C44 for the loudest signal. If nothing is available then a rough guide to the settings of these variable capacitors can be made by tuning for the largest difference in noise with and without the aerial connected. The 15 metre band is subject to strong propagation variations and may be silent on occasions. However, its saving grace is that it is open for long distance communications at some time in the day. If the band is open, then signals will be strong. In southern England contact with South America is not unusual. I used an American station in New York to tune up the receiver at around 18:00 GMT.

The construction of amateur radio equipment is addictive, you may end up with your own call sign and a low power (QRP) transmitter/receiver rig of your own.

## Main PCB Connections

### P1, P4, P6, P12, P15

These are terminal pins. In all cases the groundplane MUST NOT be cut away from the upper surface. During soldering both the lower and the upper groundplane are soldered to the pin to allow both a ground connection to the lower track and a grounded pin for an off board connection.

### P2, P3, P7, P8, P11, P16

These terminal pins carry live signals to or from the PCB. They are only connected to the lower layer, so it is important to cut back the groundplane around the pin to give isolation from ground.

### P5, P9, P10, P13, P14, P17

These are by PCB connector pins. They connect the upper groundplane to the lower layer in situations where it is difficult to arrange direct connection from the component. They are pushed well home, then soldered onto the lower pad and the upper groundplane.

G-QRP Club and SPRAT magazine  
Rev. George Dobbs G3RJV  
St. Aidan's Vicarage  
498 Manchester Road  
ROCHDALE  
Lancs OL11 3HE

## Parts

### The Main Receiver

#### Resistors

(all 0.25w metal film)

|           |                    |
|-----------|--------------------|
| R1        | 1R0                |
| R2,7,15   | 47R                |
| R16,28,29 | 47R                |
| R3,20     | 15K                |
| R4,6,10   | 10k                |
| R13,19    | 10k                |
| R23,32    | 10K                |
| R5,22     | 470R               |
| R8        | 56R                |
| R9        | 10R                |
| R11       | 4K7                |
| R12,21    | 2K2                |
| R14       | 100R               |
| R18       | 18K                |
| R26       | 220R               |
| R17,33    | 1K                 |
| R24,31    | 750K               |
| R25,27    | 3K3                |
| R30       | 22K                |
| RV1       | 10K log volume pot |

#### Capacitors

(All with 15V rating or greater) Lead spacing in brackets is in inches. **THIS SPACING IS VITAL IF COMPONENTS ARE TO FIT IN THE ALLOTTED SPACES**

|                  |                    |
|------------------|--------------------|
| C1,3,11,19,20,21 | 10µF (0.1)         |
| C2,7,37          | 220nF (0.1)        |
| C4,12,13,15,32   | 100µF elect (0.15) |
| C5               | 220µF elect (0.2)  |
| C6,8,9,35,39,41  | 100nF (0.1)        |
| C10              | 3n3F (0.2)         |
| C14,24,28        | 470pF (0.2)        |
| C16,17,25        | 4n7F (0.1)         |
| C18,33,42,43     | 2u2F elect (0.1)   |
| C23,40           | 470nF (0.1)        |
| C26              | 68nF (0.1)         |
| C27,31           | 47µF elect (0.1)   |
| C29,44           | 60pF variable      |
| C30              | 22µF elect (0.1)   |
| C34,45           | unused See text    |
| C36,38,22        | 330nF (0.1)        |

#### Additional Items

Through PCB connector pins (6 off)  
Terminal Pins (11 off) see text for important note on use  
4 by 8 pin IC sockets  
1 by 14 pin IC socket  
PCB as Figure 6  
PCB Stand-offs (4 off) [Circuit LCBSB401A]  
Small 75 ohm coax – I could not source the preferred 50 ohm coax.  
BNC Chassis socket and Free plug. For lower cost a TV connector may be used  
Aluminium box, Main Case  
Slow motion Dial Drive  
Hookup wire  
Stereo headphones as used on a Sony Walkman type stereo system  
Small socket to fit the above headphones  
Power connector for the 12V supply

#### Inductors

|       |                                          |
|-------|------------------------------------------|
| L1,2  | 47mH Toko 10RB series Part No.181LY-473J |
| L3    | 820µH Toko 7BS Series Part No.283MS-821J |
| L4,5  | Toko MKANK3428R                          |
| SBL-1 | Double Balanced Mixer SBL-1              |

#### Semiconductors

|       |                                       |
|-------|---------------------------------------|
| Tr1   | 3N201, 3SK85 or most dual gate RF FET |
| IC1   | TBA820M                               |
| IC2   | NE5534 low noise op-amp See Text      |
| IC3,5 | 741C op-amp                           |
| IC4   | NE572                                 |

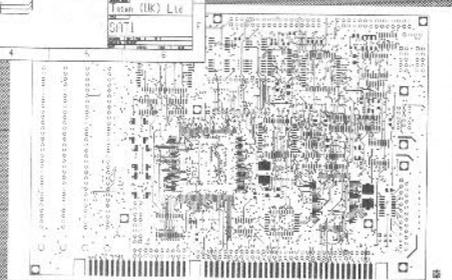
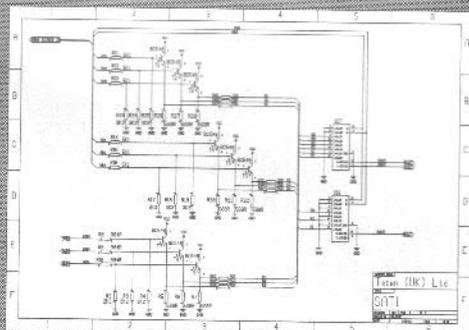
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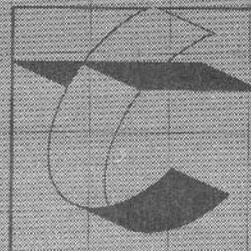
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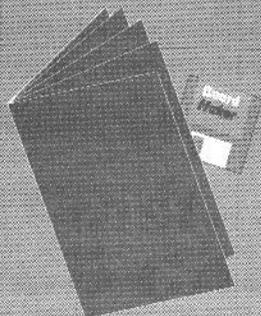
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### How Green is your city? Public transport

Are your buses electric or diesel powered? Of the few electric buses around, can we improve upon their efficiency with better electronic control systems, better electrical storage or further ways of reducing friction to give a longer range? Is there a better way at converting electrical energy into motion rather than using electromagnetic repulsion? If the main problem is one of running out of portable electrical energy ie dead batteries, can the supply be remote and without connecting wires (remember trams and trolley buses used wires and rails). Is there a method of picking up the energy from under or by the side of the road without physical contact?

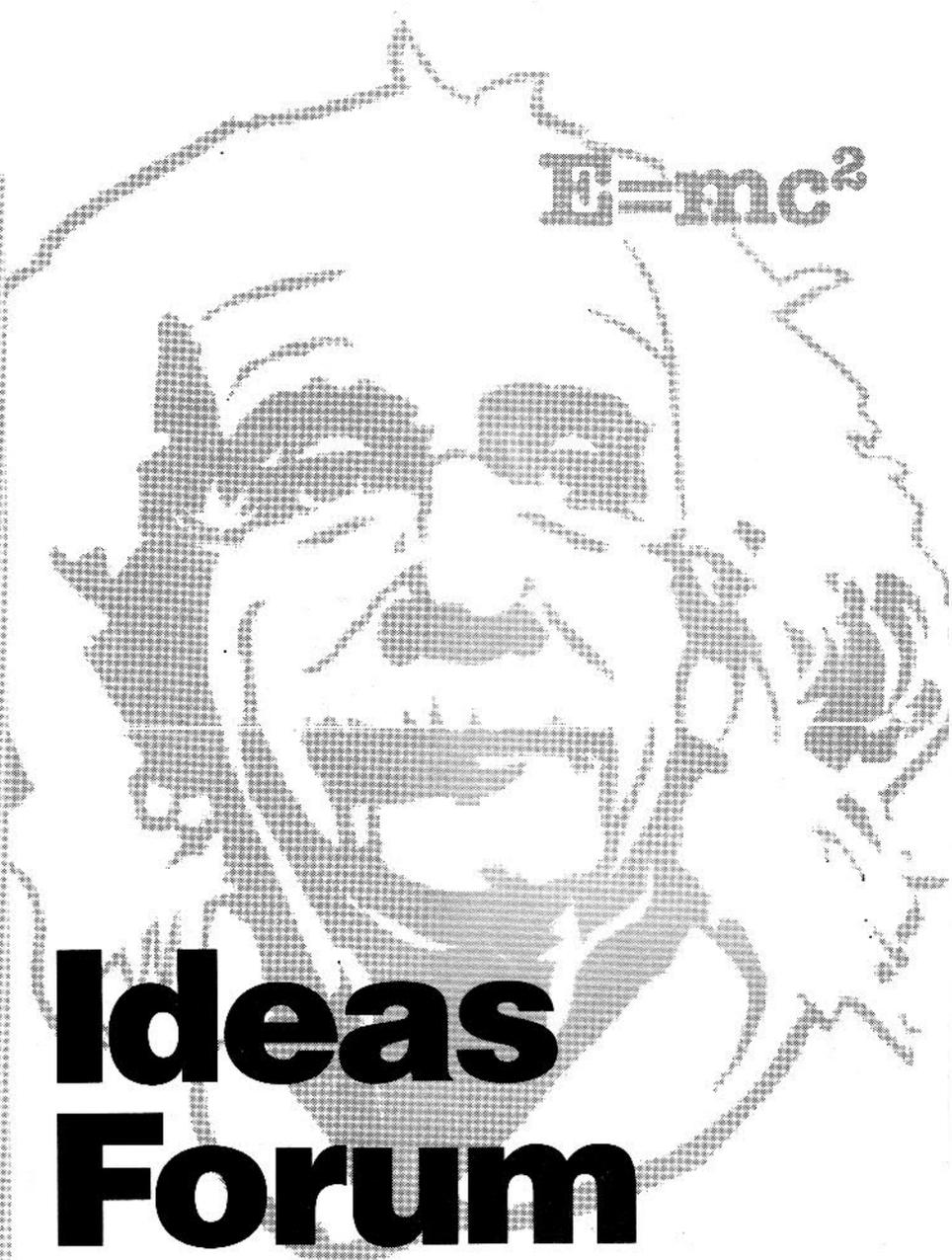
### Reducing Pollution

Can electrostatic dust precipitators be converted for use in removing particulates from conventional car exhausts?

### Noise pollution

Traffic and engine noise is a problem. Many cars are now quiet inside, but can we apply the same noise reduction to external sound emissions. Is there a way to reduce the high/low alternating gas pressure from moving cylinders that creates the engine sound before it leaves the exhaust?

Can the oscillations be down or up converted to sub or supersonic frequencies? A more radical approach - why have an oscillatory reciprocating motion engine anyway - Is there a way of producing an automobile engine from a continuous force rather than impulses as in a four cylinder engine? Can the rocket or Jet engine be tamed to run on normal roads? What about using high velocity air for thrust? Air in-air out giving no pollution? Could Noise cancelling electronics be used to deaden sound?

$$E=mc^2$$


# Ideas Forum

**Time once again to expand these ideas and put some thoughts to paper. This is Electronics in Actions' monthly brainstorm column.**

**E**ver wondered what to do with your spare time? Why not examine the ideas to the left and see if they can provide a spark of an idea that you can develop into something worthwhile. It could be that you are at home, school, college or university and have to make an electronic or allied project for your coursework and you are wondering what to do.

This is an ideas page and is intended to be a regular feature. As soon as you think or know the idea can be

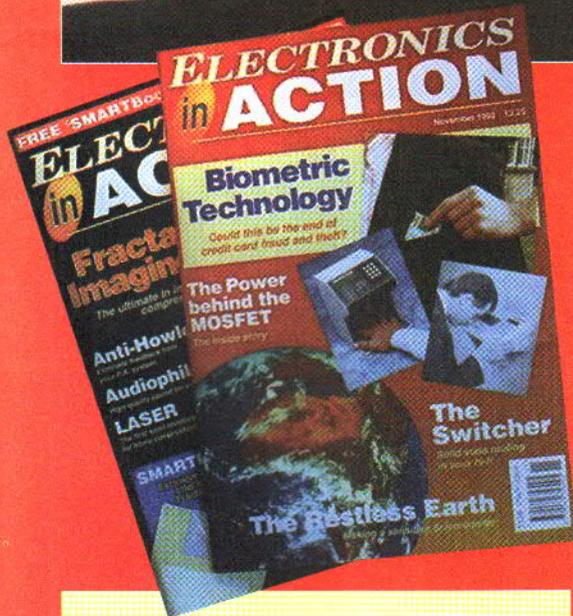
achieved by yourself, and it might be a variation on these themes, get a working prototype together. If you think others might like to see your efforts in print, send it in with the details to us and we will seriously consider publishing it. You will of-course be rewarded for your efforts in print. The ideas seen here may even be a cause to write in to our letters page to discuss the ideas you have.

Some of them may well have been designed and built at high commercial level and high cost but it may be you have thought of a quick and easy route to achieving the same end and at much lower cost. The exercise here could also lead to other less costly innovative ideas.

The ideas do not appear in any particular order so keep a look out every month. Very soon Electronics in Action could be printing lists of 'Centres of Excellence' where it would be the place to be for an informal chat and to openly discuss these and other ideas in a sort of brainstorming session.

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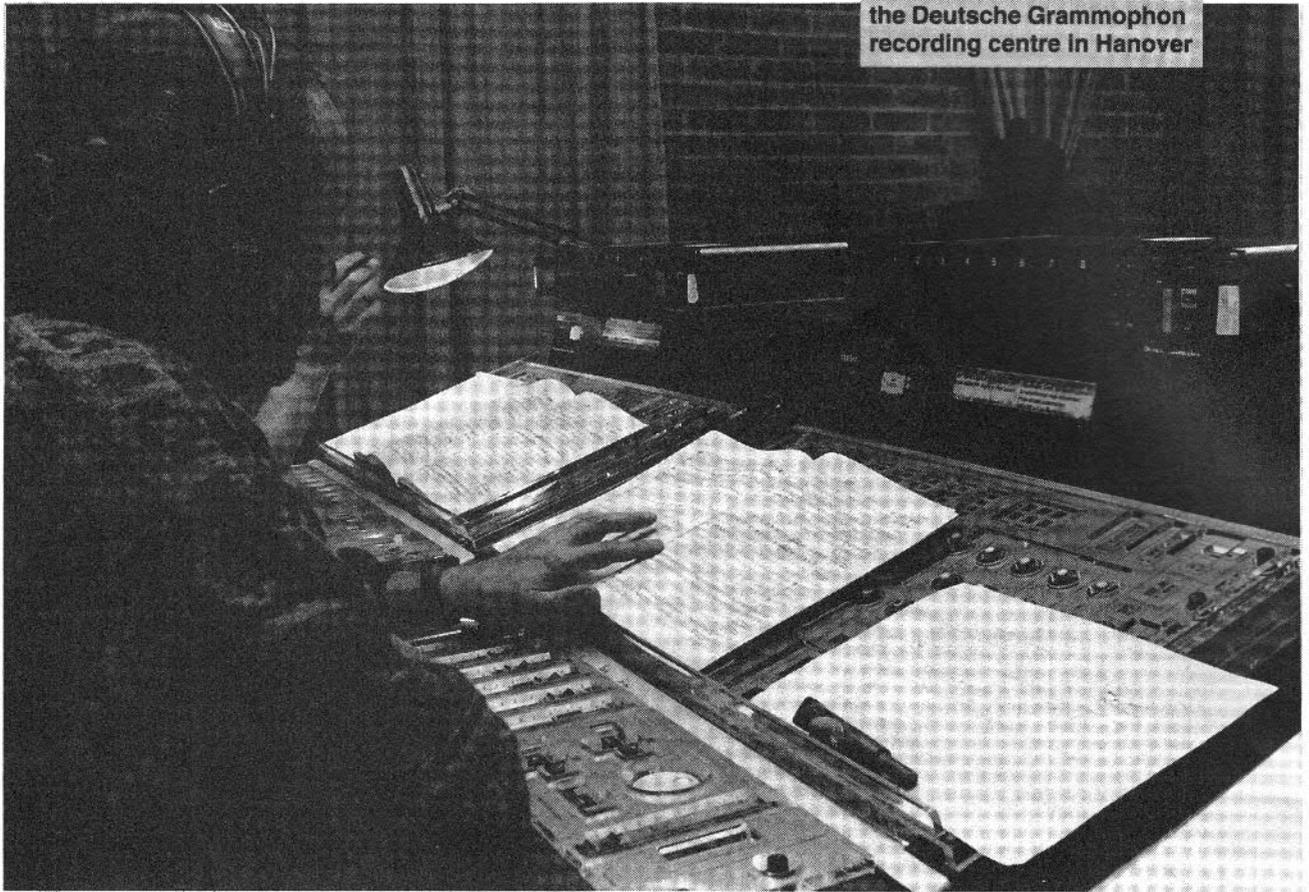
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Klaus Hiemann, director of  
the Deutsche Grammophon  
recording centre in Hanover



# Welcome to the fourth dimension

**4D Audio Recording is the world's first fully digital mobile professional recording system. Keith Grant reports from Hamburg.**

**F**or an engineer, even a sound engineer, to declare that the aim of recording technology should be that it should become inaudible, might seem incomprehensible. But listen to the sound of a group of players while they are being recorded and then listen to the recording and you will realise that the degrading effect of the recording technology is indeed audible.

When Klaus Hiemann, Director of the Deutsche Grammophon Recording Centre in Hannover, therefore declares

that the technology used to make a recording should be inaudible, he means that its effect should not be to audibly degrade the musical signal that first enters the microphone. Sadly however it is so often the case that, even with digital recording, metres of microphone cable, recording console signal paths and multiple conversions, of analogue signal to digital audio and digital audio back to analogue signal, throughout the recording, mixing and mastering processes, do just that.

The development of a recording system that could offer freedom from the effects of the recording process itself was a dream that Klaus Hiemann held for many years, convinced that the digital recording medium would eventually evolve beyond the simple development of a storage system for the same analogue recording signal chain. 4D Audio Recording is the materialization of that dream and although much publicity has surrounded the claims for its technical achievements

it is The Recording Centre's principals of acoustic engineering, under Hiemann's Directorship, that has shaped the development of the world's most sophisticated mobile location recording system, transferring laboratory standards of system performance into the field.

"It has always been my goal as director of The Recording Centre to make the recording process as imperceptible as possible, but the less noticeable the technology is to the listener, the more complex it has to be on the inside," explains Hiemann.

The shift to digital technology was a worldwide phenomenon. We were suddenly confronted with a recording process we scarcely knew.

"In the beginning we found it very 'cold' and later, that view proved to be correct because the equipment was not advanced enough. Almost immediately we discovered flaws in the analogue-to-digital and digital-to-analogue converters, so we sought to improve them, so the analogue musical signal could be shifted to the digital level with a greatly reduced distortion."

Along with the rest of the classical recording companies, Deutsche Grammophon continued to record digitally while constantly seeking to refine the available equipment. What became increasingly clear to the company's Audio Development team, from the early 80s onward, was the scale of improvement that was going to be required. The years following the rush into digital recording

also saw a break with the tradition of developing in-house technology.

The Recording Centre (like Decca in the UK) had always striven, to develop its own equipment, believing that the technology required could not be found commercially."

The development of dedicated analogue recording equipment was an entirely different proposition to the R & D investment required to produce the fully digital recording signal chain that DG had identified as a primary requirement of the next generation classical recording systems. A development partner was found in Yamaha. Their research department in Japan was already tackling the development of the powerful digital processing technology.

In Yamaha we found a real willingness to create technology with our particular needs in mind.

In co-operation with Yamaha, we were able to develop new improved analogue-to-digital converters which led us into high-bit technology, shifting the analogue music signal to the digital level with much greater than 16-bit precision, with greatly reduced levels of distortion. The next objective was to be able to mix the microphone signals as cleanly as possible. We worked with Yamaha to develop a new generation of completely digital mixing consoles.

Around the same time Hiemann appointed a young digital audio communications engineer, Stefan Shibata, to head the Audio Development team charged with

replacing the entire audio signal chain with a completely integrated digital processing system, incorporating the new Yamaha converter and console technology. The 4D Audio Recording programme was officially under way.

A 21-bit variant of Yamaha's Delta-Sigma floating digital D/A converter system, offered both a technical and a musical performance exceeding anything previously possible. Extensive listening tests and technical measurements were made before the system was selected. The high bit resolution allowed a signal to noise and performance dynamic range far in excess of 16-bit technology but more important still to Hiemann it enabled the elimination of so much of the distortion inherent in the 16-bit standard, regarded as woefully inadequate, almost from the outset, by so many engineers. The resolution with 21 bit conversion is much higher and far closer to the original waveform of the music.

Replacing the analogue signal chain meant they had to be sited on the recording stage, as opposed to in the control room along with the mixing console and digital recorder. Siting the converters on the stage would allow short microphone cable runs. "Experience has shown us that it is much better to convert the analogue signal, almost as soon as the microphone has picked it up. This ensures a cleaner mix, and above all, one free from technical interference and from other sounds bouncing around theatres and concert halls. Since the signal is converted into digital, it is no longer subject to undesired interference."

High bit converters of this quality made new demands on microphone head amplifier design, to ensure that what remained in the way of analogue processing did not impose a bottle neck on the digital signal chain. Given that the converters were assembled in an eight channel arrangement an eight channel head amp was suggested. A remote facility was also required but with no compromise on quality. An extensive search found no suitably spec'd devices on the market and the decision was taken to design and manufacture one in-house.

Design criteria included external power supply (maximum signal to noise performance), transformerless input, distortion-free gain switching with relays, gain setting and display and channel group indication, remote protocol with extensive acknowledgment and error



Yamaha Digital mixing desk used in 4D recording

reporting features, asynchronous serial communication on RS422 (midi/4 Baud default) and interface with PC based remote control software for up to six eight channel units to a system. Signal path components were selected on the basis of extensive measurement and listening tests. "We have developed our pre-amplifiers to satisfy the ears subjective expectations. They have been designed, above all, with the goal of 24 bit recording in mind."

The eight channel configuration of both the converters and head amps allowed an eight channel 'stagebox' to be devised, housing both devices as well as the required electronics to allow these stageboxes to operate in synchronization with the digital consoles and control room based computer aided control systems. The demands of location recording mean that the stagebox may have to be placed anywhere up to 200 yards from the control room. A critically engineered error-free transmission system was designed and built by DG's engineers to ensure that the kind of system performance obtained under laboratory conditions could also be realised.

The 'Digital Network', a galvanically separated, multicore transmission line, carrying bi-directional 24 bit AES/EBU audio channel, digital transfer data, remote control data for the microphone head amplifiers, and other communication data, took two years to engineer and construct.

The DMC1000 digital consoles are usually configured three to a system, although larger systems of up to six consoles are possible and occasionally required. These operate with extremely sophisticated operational software, developed specially for Deutsche Grammophon by Yamaha.

Recording with a high bit signal, i.e. one greater than 16 bit, of course raises the problem of incompatibility with all the digital consumer playback

formats which all adhere to the 16 bit standard. In order to master such high bit signals for consumer release it is however possible to employ requantizing noise shaping techniques, in order to redither the signal down to 16 bit. While it will never completely mirror the quality of a 21 bit master tape, noise shaping a high bit signal can result in achieving a better sound performance than that of the standard 16 bit medium. The resultant improvement in the sound of a standard CD, played back on a standard CD player, can represent a readily perceived quantum leap in sound quality.

In employing noise-shaping techniques (termed Authentic Bit Imaging), an extensive program of experimentation and empirical testing has led to refinements that build on the pure mathematical precepts of noise-shaping, as defined in the pioneering

### *The improvement in the sound of a standard CD can represent a readily perceived quantum leap in sound quality*

work of Dr. Stanley Lipshitz. This has produced interesting and often surprising results which have led Deutsche Grammophon to conclude that no single noise-shaping curve is appropriate to all types of program material. In the course of their analysis of requantizing techniques Deutsche Grammophon have experimented with changing filter techniques, the varying of different parameters and the use of correlated and non-correlated noise generation. Consequently Deutsche Grammophon have developed curves appropriate to particular types of music.

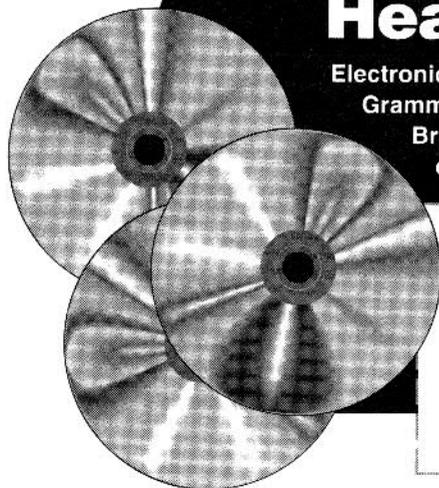
After five years of development, Hiemann took the prototype 4D Audio Recording system out to record a session. "As the man responsible for pushing through the development of the system, it was only fair that I should take the responsibility and possible risk of trying it out." In fact the system worked first time, as it has done so ever since; a level of reliability not necessarily associated with the implementation of digital audio even in the 'fixed' studio environment. The first officially badged 4D Audio Recording was released in March this year although several had already been released onto the market using the system. Now all recordings used the new technology.

Initially it was not possible to store the high bit signal as DG awaited the availability of 24 bit capable recorders, requantizing therefore having to occur before the signal hit tape. Operation is now with 24 bit Nagra D recorders with evaluation of Sony's new 24 bit MOD (magneto-optical drive) system due to commence. By November a propriety 'scrambler' developed by the DG engineering team will also allow full 24 bit recording with conventional Sony digital multitrack recorders. The use of 24 bit recording allows for the future development of 24 bit A/D conversion and the implementation of 4D as a fully 24 bit system. 24 bit is recognised as representing the limit of human hearing.

There are now six fully operational 4D mobile recording rigs traversing the globe and all inhouse digital editing and mastering suites are all fully 4D compatible. Future system development revolves around the continued push towards a fully 24 bit recording chain and the problems inherent in current microphone technology that this will require to be solved; but that's another story, to be told at a later date.

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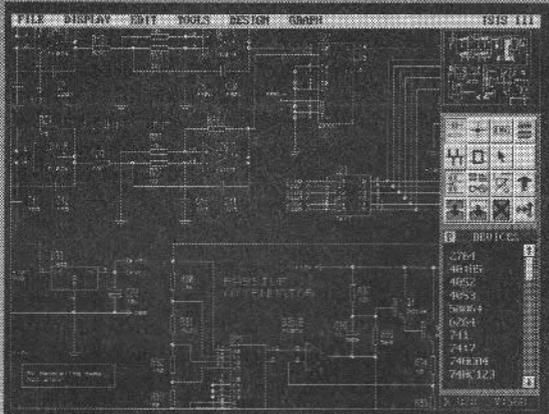
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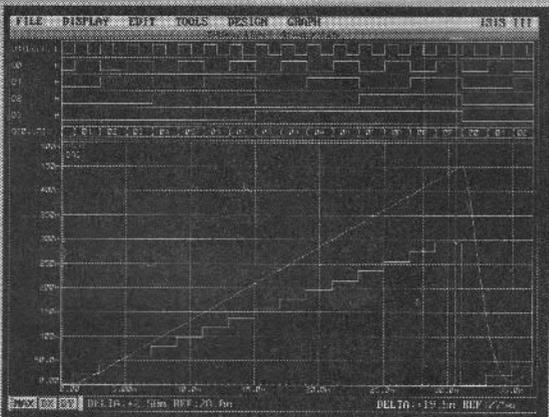
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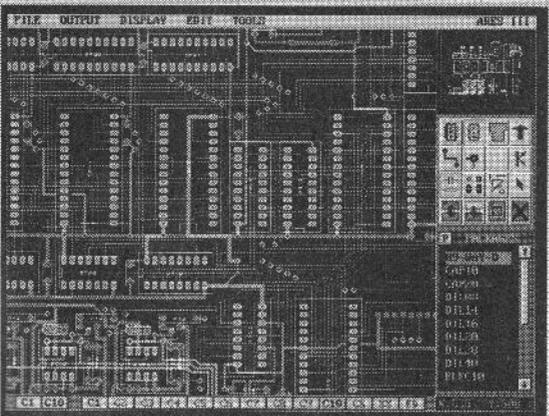
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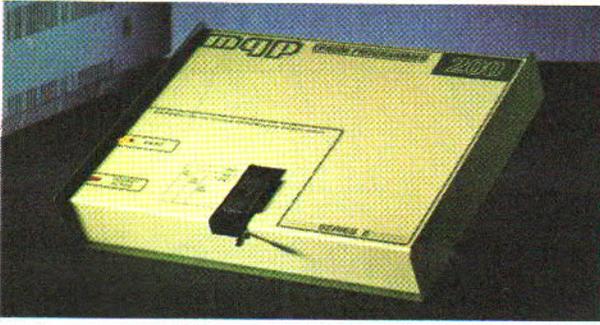
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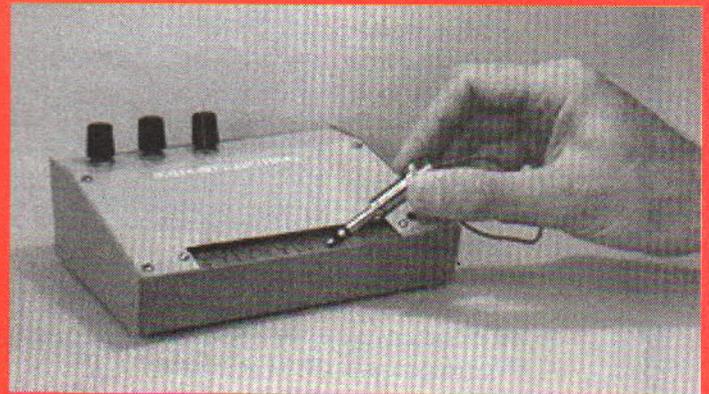
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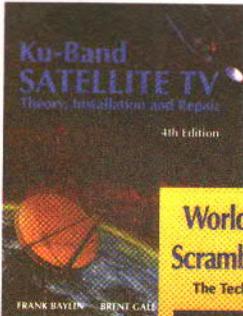
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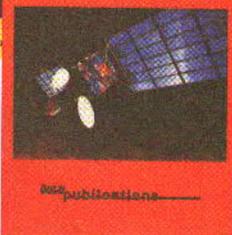
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# Back to the Sixties...

...Using 90s technology. Bathe your audience in nostalgia with an auto panning stereo tremolo unit. Music to our ears from Dan Coggins

I have been asked countless times by my guitar-toting friends where they can buy a 'tremolo pedal' for their instrument.

Oddly, these are hard to find - which seems strange when it is enjoying a new-found popularity, especially with 'indie' groups.

Tremolo is an old-fashioned effect, found originally on late 1950s guitar amplifiers of the valve variety. It can best be described as a 'stuttering' effect (or used more discreetly, a 'shimmering' effect.) However, only vintage-style

amplifiers feature it (as a rule), and designs for tremolo circuits have been absent from the pages of electronic magazines for some years. Hence this design.

I might be accused of taking 'money for old rope' here, but this design has a difference - it's stereo! It can also work in mono, of course, giving the classic sound that many a sixties' hit was built on. The design uses modern ICs to capture these sounds in a compact pedal with low battery consumption.

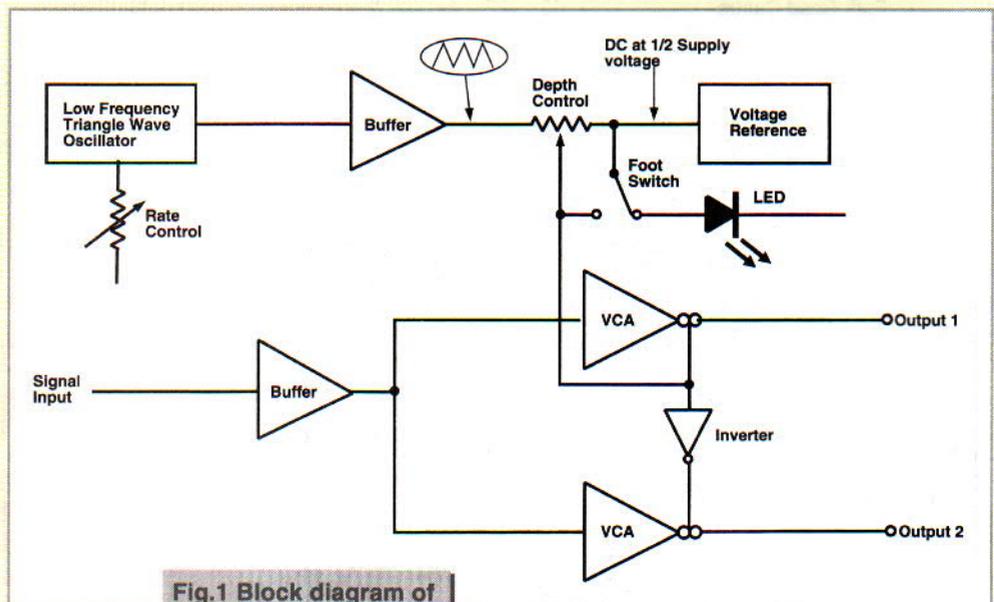


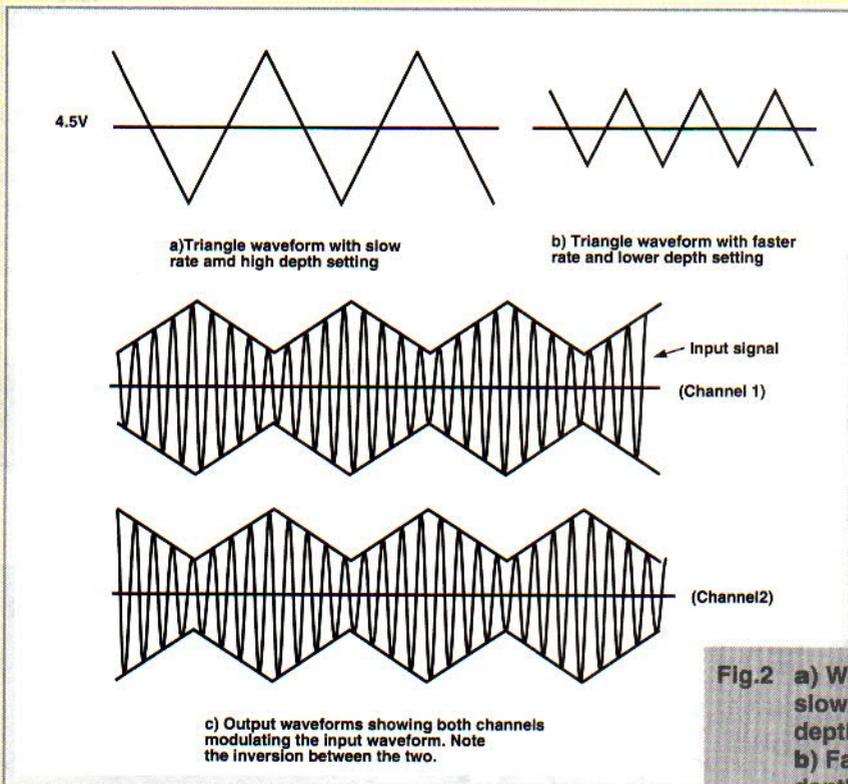
Fig.1 Block diagram of the stereo tremolo unit

## Design Considerations

As with any musical effect pedal, a small portable sturdy box, containing a substantial footswitch and having low-current battery operation is the general requirement. This pedal has those very features and is simple to use.

Although chiefly associated with guitars, tremolo effects can be used on most signal sources with interesting results. Indeed, I tested the prototype by feeding Radio One through the input - a vast improvement!

To this end, a high input impedance and a reasonably flat



**Fig.2** a) Waveform with slow rate and high depth setting  
 b) Faster rate and low depth setting  
 c) Output showing both channels modulating the input waveform. Note inversion

## The Circuit

For convenience, I shall refer to the circuit in two halves, namely the Low Frequency Oscillator (LFO) and the Voltage Controlled Attenuator (VCA) circuit. In the LFO circuit:- IC1 is a TL064 quad JFET op-amp package, giving low current consumption and good performance at low cost. Here, all four of its op-amps are used in the LFO circuit only, which is good practice from a noise viewpoint.

First, we require a split supply for the LFO (and the VCA circuit, too). IC1a buffers the 4.5V produced by R1 and R2, both acting as a potential divider. This voltage is decoupled 'fore and aft' by capacitors C1 and C2. This provides a low impedance 4.5V rail necessary to run the LFO and VCAs. Good

decoupling is essential to prevent breakthrough of the LFO control waveform to the signal path.

IC1b is configured as a simple triangular wave oscillator, with C3 as its timing capacitor.

C3 charges and discharges alternately through the resistance set by RV1. With series resistor R6 assigning a maximum rate of oscillation of 5Hz approximately, the rate control RV1 will vary this rate down to around 0.3Hz. The voltage appearing across C3 is a triangle wave, buffered by IC1c to feed the control

frequency response are important features to have. This is achieved by buffering the input signal as it enters the circuit.

Low current consumption is achieved by using JFET op-amps which use only hundreds of microamps, typically. The overall design uses about 3mA, and so is kind to a PP3 battery. Of course, a power supply may be used and a socket wired in to accommodate this, if so desired.

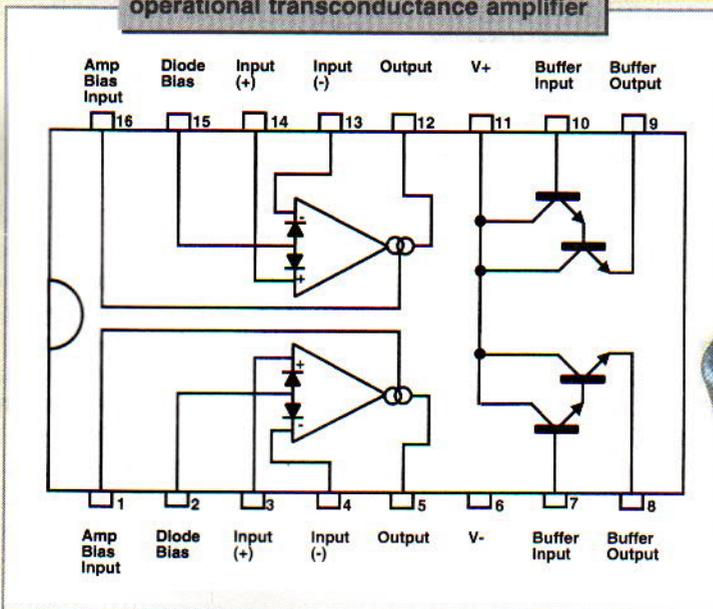
A substantial die-cast case is used to screen and protect the circuit, in the arduous conditions it is likely to endure between a stage and someone's pounding foot! A lot of time was spent agonising over a suitable switching

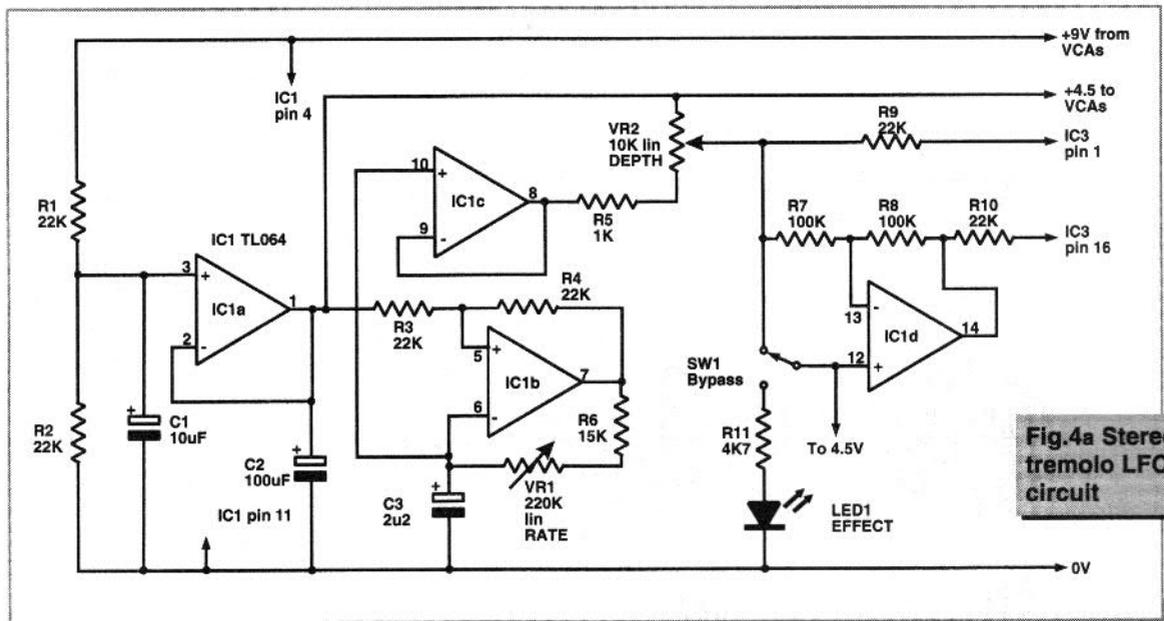
arrangement to bypass the effect.

The arrangement chosen gives very noise-free operation from a mechanical switch, as well as switching on an LED when the effect is in operation to alleviate confusion and to show up a dying battery.

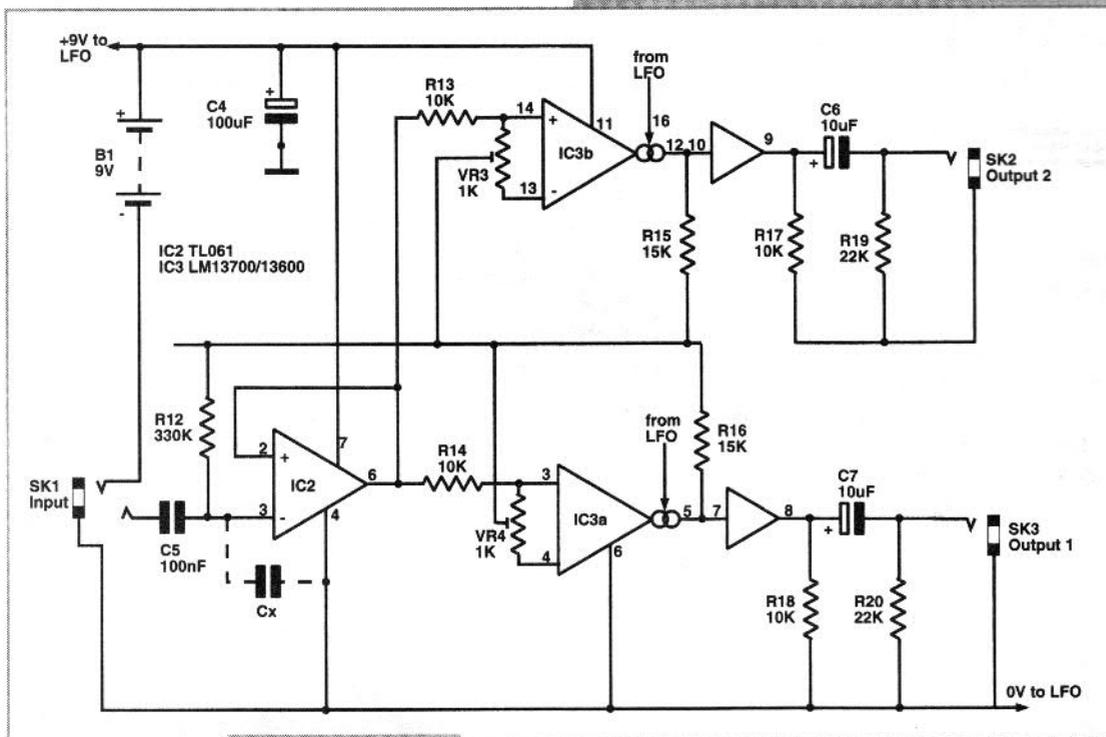
Many methods of coupling oscillators to audio signal paths were investigated in this design - it's difficult to be successful in reconciling good performance with low noise. Having abandoned the use of opto-isolators, a design utilising voltage controlled attenuators was implemented.

**Fig.3** The LM13700 (LM13600) dual operational transconductance amplifier





**Fig.4a Stereo tremolo LFO circuit**



**Fig.4b VCA circuit**

inputs of the VCAs (see Figure 2a & 2b).

R5 is included to protect the output of IC1c from excessive loading when the footswitch is closed across RV2 on its higher settings. RV2 is the 'depth' control which varies the amount of modulating waveform fed to the VCAs. The penalty of including R5 is to limit the maximum depth of modulation, but the effect will still sound quite powerful despite this.

At RV2's minimum setting (or when it is effectively shorted by the footswitch) the VCAs are held at half-supply with zero applied modulation. This allows the original signal from the instrument to pass through to the output unmodified, and the unit is therefore

### The Works

Refer to Figure 1. An input signal from a musical instrument, such as a guitar, bass or keyboard is buffered and fed to two identical electronic attenuators. When an adjustable waveform is fed to these, as a control voltage, the amplitude of the instruments' signal is modified. A

'bypassed'.

With the effect 'on', the LED (D1) is lit when the other contact of the footswitch is closed. It runs from 4.5V via current limiting resistor R11, which passes only 0.5mA through the LED, yet giving reasonable visibility in ambient light. IC1d is an inverting buffer, which reverses the phase of the waveform applied to the second VCA - this gives

triangle waveform will give us a 'tremolo' effect. With just one of the two outputs connected, a tremolo sound will be heard. With both outputs connected to separate amplifiers a stereo 'panning' effect is heard. This stereo effect is achieved by feeding opposite phase waveforms to either attenuator. When the footswitch is pressed to cancel the effect, both attenuators are fixed to the same 'zero' DC control voltage, giving identical outputs of the original input signal at the same level, without any audible effects.

This unit is useful for buffering high impedance sources, such as electric

guitar pick-ups, as the buffer stage is always in the signal path (with unity gain), preventing undesirable treble-losses in the signal, due to cable length. And it provides a convenient means of running two amplifiers or signal chains from a common source.

the stereo effect when two separate amplifiers are used (when one output gets louder, the other gets quieter and vice-versa, according to control settings). See Figure 2c. When the effect is bypassed (or depth is zero) both VCAs will have the same half-rail control voltage, hence giving identical in-phase unmodified outputs to both amplifiers.

## VCA Circuit

In the VCA, the input signal is buffered by IC2, a TL061 - again chosen for its low current consumption and reasonable noise level (the TL071 is superior for audio, but will use more current; in this design, the LM13700 IC produces most of the noise - the S/N ratio of this design is 60dB, approximately - (so the use of a TL061 is justifiable). R12 sets the input impedance, suitably high for musical instruments, with no treble loss. Cx is shown dotted in the event that the unit may pick up radio signals after dark.

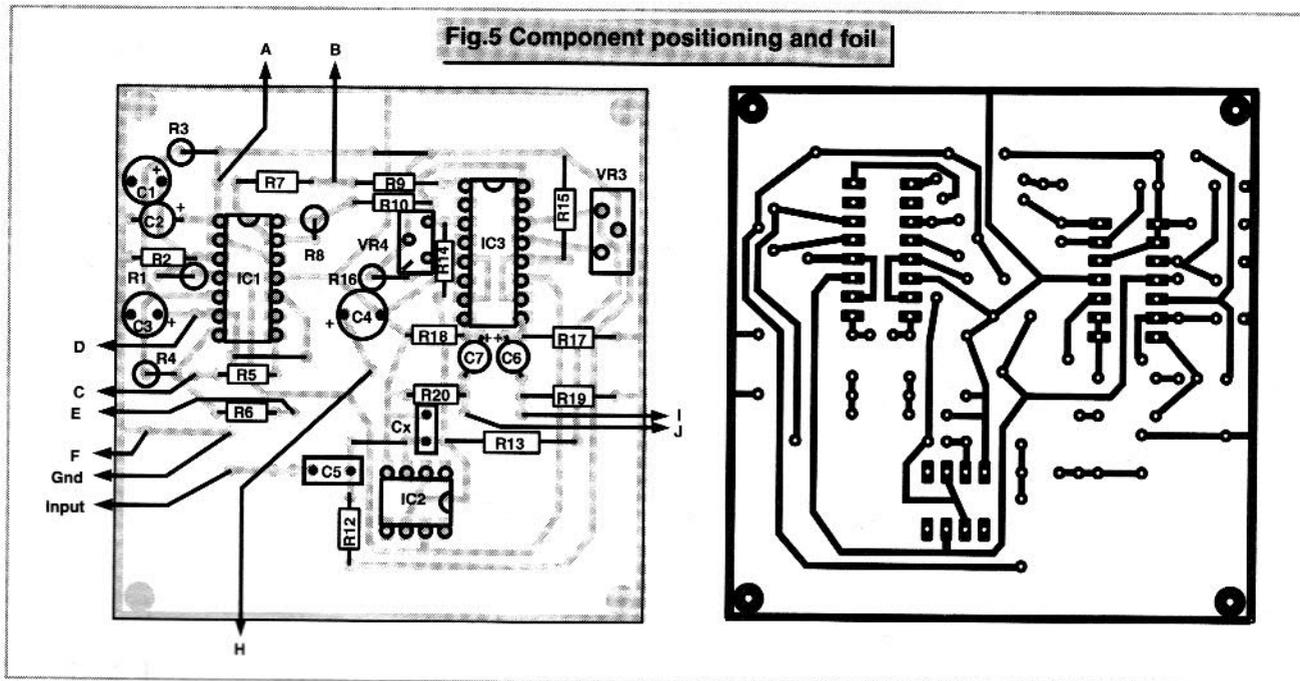
output buffer, which is internally matched to the characteristics of its op-amps. Pins 9 and 8 are loaded by the resistors R17 and R18 and the audio signals coupled to the output sockets by C6 and C7. Resistors R19 and R20 provide a charging path for these capacitors, thus eliminating 'thump' when connecting up to an amplifier. The trimmer resistors RV3 and RV4 are used to null out any control signal breakthrough, by balancing the input stages of each transconductance op-amp.

diameters. Drill out the other holes to size, as shown in Figure 6. The PCB can be mounted on the inside of the lid. Once all the holes have been checked to fit their respective components, rub-down letters can be used to label the controls and sockets. Several coats of clear lacquer (as found in motor factors) may now be applied to protect it.

## Setting Up and Testing

When you are content with your wiring and everything has been checked over carefully, connect the battery with an

Fig.5 Component positioning and foil



If this problem arises, try using a polystyrene capacitor of around 470pF. If this fails, increase the value until the RF is eradicated, but remember that too high a value may cause treble loss with high impedance sources - experimentation is the best way to solve this!

The buffered signal is coupled by R13 and R14 to each VCA IC3 is an LM13700 dual Operational Transconductance Amplifier. It has many uses (filters, pulse width modulators, electronic stereo volume controls, etc.) and here both of its op-amps are configured as voltage controlled amplifiers (or more correctly, voltage controlled attenuators). By applying a varying voltage to the control pins (1 or 16) the amount of attenuation applied to the audio signal can be controlled. As this is a transconductance op-amp, an output current is produced which in turn develops a voltage across resistors R15 or R16. This voltage is buffered by the LM13700's own internal darlington

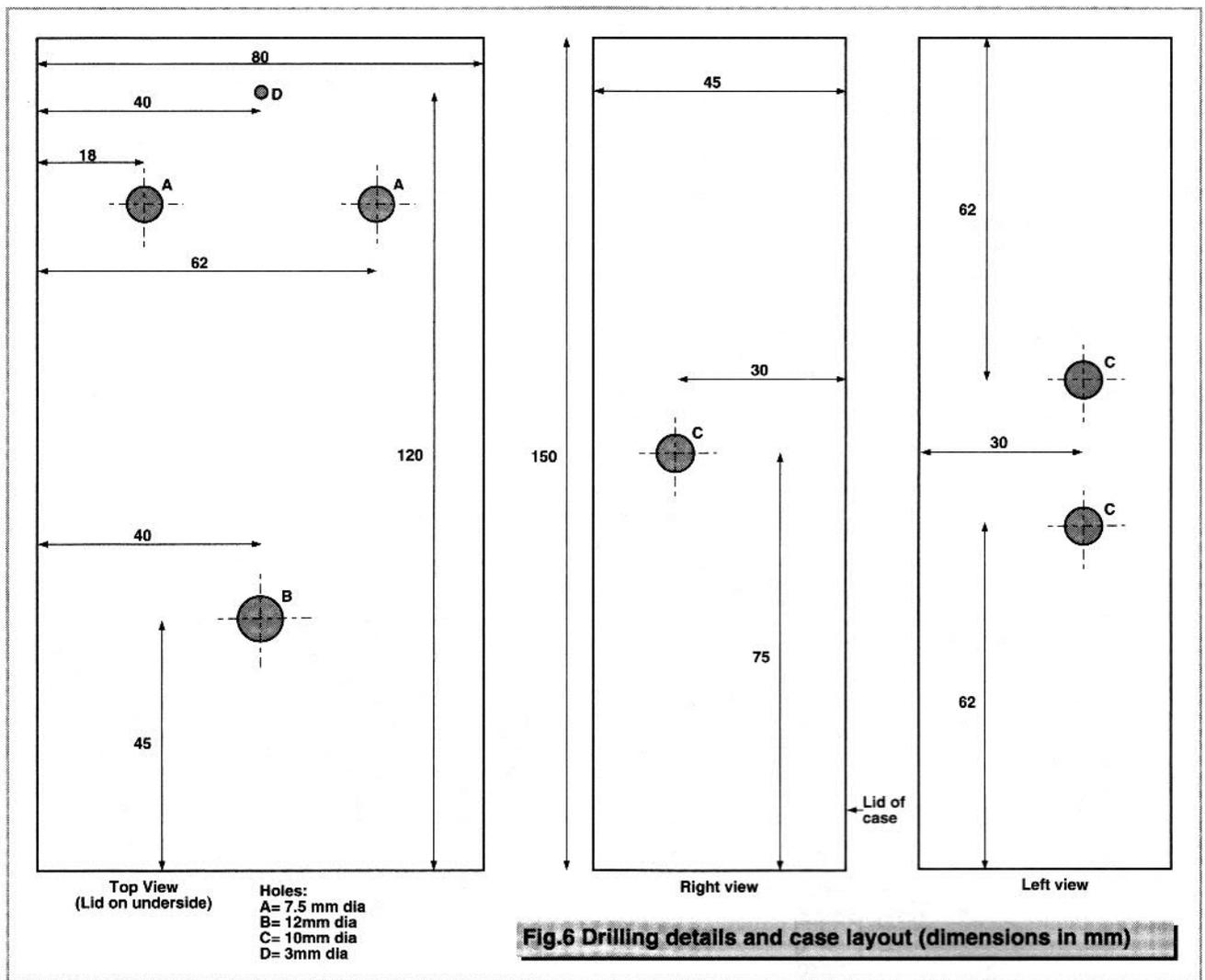
## Construction

Start by assembling the PCB. Begin with the resistors - double checking their values with a multimeter will help to prevent any inexplicable faults later on! Next fit the capacitors - be sure to fit them the correct way round. Solder in the ICs - again, checking for orientation. Refer to the overlay diagram (Figure 5) for assistance.

Connect all the flying leads to the PCB and use colour-coding if possible, to pre-empt any possible wiring nightmares! Ensure that screened cable is employed for the input socket connection. This piece of wire makes the difference between a quiet pedal and a noisy one. It is only necessary to solder the screen at the PCB end. If moulded plastic sockets are used, then connect the nearest contact of the case to one of the potentiometer housings for a suitable ground.

Using the case specified, mark out the holes using a centre punch and use the 3mm drill for the LED hole (D) to make pilot holes for the larger

ammeter in series. Plug a 1/4 inch mono jack into the input and observe that the current reading should be between 2 and 3mA approximately. If your reading differs much from these figures, disconnect the battery and check your wiring and assembly again, especially the ICs and capacitors. Always unplug the input jack when not using the unit - it doubles as the on-off switch, and will eventually drain the battery if neglected. With both controls set fully clockwise, connect a cable between one of the output sockets and your amplifier. Ideally, short the terminals on your mono input jack to effectively ground the input stage (alternatively, turn down the volume control on your instrument). Press the footswitch so that the LED is lit, then turn up the volume on your amplifier until it registers a 'thumping' noise. Depending on which output socket you have connected your amplifier to, adjust RV3 or RV4 until this noise disappears. Repeat the process for the other output - there is a critical point on both trimmers where the



cancellation occurs, so adjust slowly. If the oscillator can still be heard, check the layout of your wiring and the grounding of the input connections. A low level of hiss may be noticeable on either setting of the footswitch, and this should not be confused with oscillator noise.

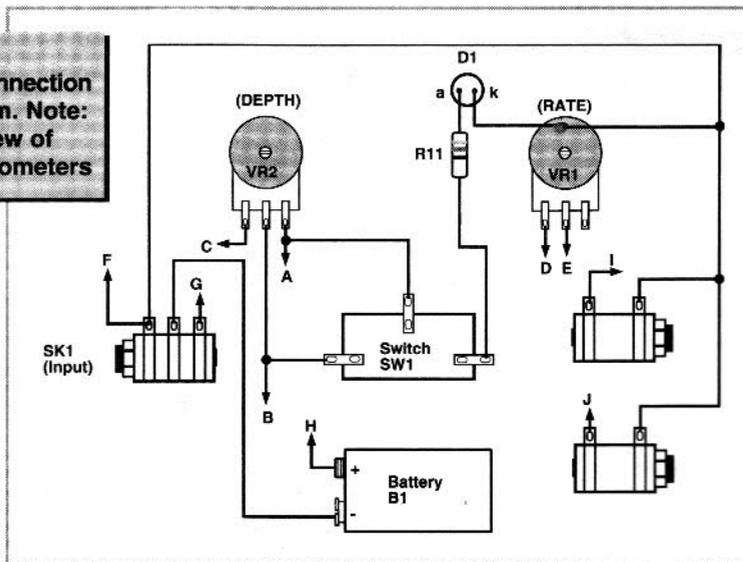
The stereo tremolo unit is now ready for use

### The Twang's the Thang

Hopefully, the stereo tremolo effect should be self-explanatory. The rate control adjusts the speed of the effect, and the depth control adjusts the intensity of it. With an amplifier connected to each output (it's an expensive game) the most dramatic 'panning' effect will be heard at low rate settings, with full depth. Stereo imaging can be produced by using a high rate with the depth control set to about  $\frac{3}{4}$ . Experiment to find the sounds that please you the most.

When used in mono (as a standard tremolo) the rate control may seem a bit 'cramped' at one end. Ideally an anti-log potentiometer would be employed, but these are scarce and costly. A log

**Fig.7 Interconnection diagram. Note: rear view of potentiometers**



pot could be used instead, with the opposite track connection used to provide smoother rate control, albeit back-to-front. This appears to be counter-intuitive, but is worth consideration. If you only intend to use the tremolo in mono (one amplifier) then change the value of the rate pot to 100K. A 220K pot is specified to accommodate lower rates for stereo 'panning' effects, and would be worth changing to improve its 'sweep'.

### Afterthoughts

Other effects may be obtained from this circuit by modifying the VCAs to operate as VCFs which could give 'auto-wah' effects, or as a dynamic filter to simulate the sound of a rotating 'Leslie' speaker.

If the unit is to be used at line level (0dBu/775mV) or greater, then some modifications must be made. IC3 has optional linearising diodes at its inputs to facilitate greater headroom and lower

# Parts

distortion figures. This is at the expense of available gain and has not been used in this design. If you wish to modify the unit, tie pins 2 and 15 to 9V with 15K resistors and increase the values of R15 and R16 to compensate for gain loss.

If the LED is considered to be too dim try reducing the value of R11 to 3K3 or less. Do remember the pay off will be a substantial increase in current consumption when the effect is switched on. Generally, the smaller the LED the greater the perceived intensity of light - large LED's appear to diffuse low light levels to a greater extent. Connecting a second oscillator producing an even slower triangle wave will give interesting effects, if it too is connected to the control pins of the VCAs. By skewing the triangle waveform it is possible to achieve 'backwards guitar' simulation, by offsetting the voltage to the oscillator. It's tricky to implement, as it causes erratic rate control if it is altered and can be difficult to interface with the VCAs to give a consistent overall gain, but it sounds good.

## REFERENCES

National Semiconductor data sheet for the LM13700.

### Resistors (all 5%, 1/4W):

- R1,2,3,4 22K
- R5 1K
- R6 15K
- R7,8 100K
- R9,10 22K
- R11 4K7
- R12 330K
- R13,14 10K
- R15,16 15K
- R17,18 10K
- R19,20 22K
- RV1 220K linear potentiometer
- RV2 10K linear potentiometer
- RV3,4 1K miniature vertical preset

### Capacitors

- C1,6,7 10u/16V PCB type electrolytic
- C2,4 100u/16V PCB type electrolytic
- C3 2u2/16V PCB type electrolytic
- C5 100n polyester or similar
- Cx see text

### Semiconductors

- IC1 TL064 quad JFET op-amp
- IC2 TL061 JFET op-amp
- IC3 LM13700 (or LM13600) dual transconductance op-amp
- D1 3mm miniature red LED

### Additional Items

- S1 SPST heavy duty footswitch SK1 stereo 1/4" jack socket
- SK2,3 mono 1/4" jack socket
- B1 9 volt (type PP3)

### Battery clip

Case (150 x 80 x 45mm - BIMBOX type 5005)  
 Rub down letters, Knobs, Wire, Screened cable, Solder  
 Spray lacquer, PCB (This can be ordered through EIA)  
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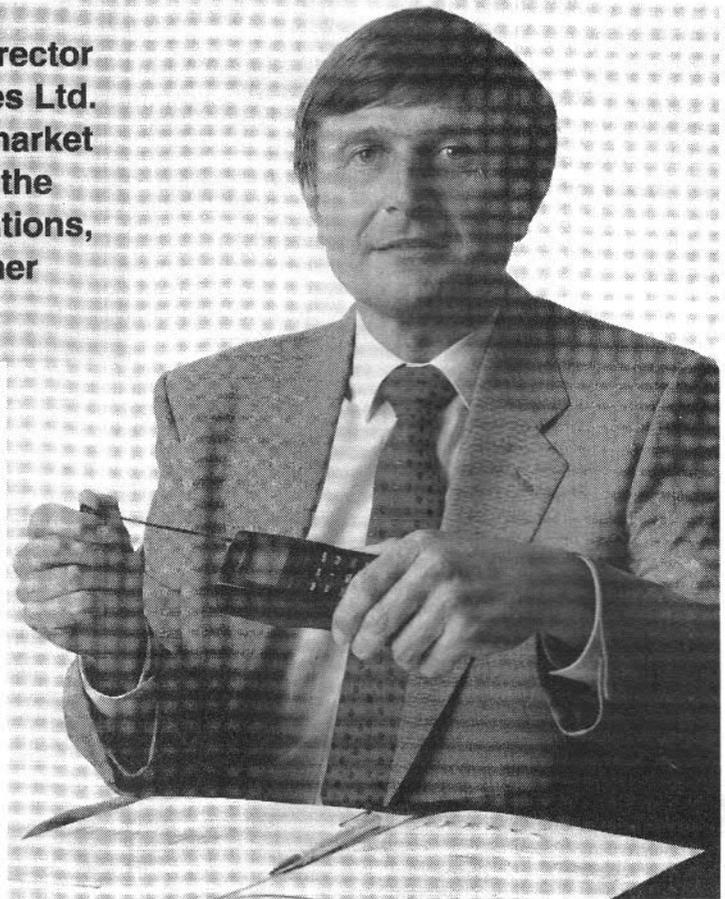
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# Future View

**Robin Saxby, Managing Director of Advanced RISC Machines Ltd. talks about the emerging market for portable products at the cross roads of communications, computing and consumer electronics**



## Historical Background

Following on from the pioneering work by Charles Babbage on computer architecture, the first practical computers were produced in the UK and USA during the second world war. The invention of the transistor in 1948 by William Shockley, Walter Brattain and John Bardeen at US Bell labs and the integrated circuit (IC) by Robert Noyce and Jack Kilby independently in the USA in 1959, fuelled the start of the mainframe digital revolution in the early 60's. IBM introduced the 360 mainframe computer (so called because it was intended to turn the world through 360 degrees) in 1964 and quickly became one of the world's largest corporations. At the same time and through the mini skirt era of the sixties the mini computer companies started to be successful with the emergence of DEC.

The microprocessor, invented in 1971 by Ted Hoff was originally designed for calculators. In 1975 Intel thought that their microprocessors were only suitable for controllers such as those used in traffic lights. But in parallel with this hardware activity, Paul Allen and his friend Bill Gates were working away in Albuquerque to write a version of BASIC that could run on a microprocessor. This work demonstrated that Intel's new invention had the potential to be the brain of a truly serious computer. In 1976 on April Fools day, Steve Jobs and Steve Wozniak who had written a BASIC for another microprocessor from MOS

Technologies, founded Apple Computer and launched the Apple I. This computer had characteristics of good performance and low cost as it consisted of a circuit board which connected to an ordinary TV set. Apple's sales accelerated when Visicalc, the first spread sheet, invented by Dan Bricklin, was coded to run on the Apple II by his friend Bob Frankston. Then IBM entered the PC business in the mid 70s and along with all the clone companies fuelled the explosive growth of Microsoft and Intel.

## Meanwhile...

In Cambridge UK at 3pm on the 26th April 1985 a couple of British computer scientists, Steve Furber (Now ICL Professor of Computer Engineering at Manchester University) and Roger Wilson (now Chief Scientist at Acorn Computers) with a small team of engineers:- Mike Muller, Robert Heaton, Tudor Brown, Jamie Urquhart, Dave Flynn, Dave Howard and Jim

Sutton received samples of the world's first commercially exploited RISC chip which was manufactured by VLSI technology and called the ARM.

Unlike later RISC chips of Sun SPARC and MIPS which were designed for the highest performance, the ARM was designed to squeeze the maximum performance possible within the constraints of a tight cost budget. In semiconductor terms manufacturing cost is directly proportional to chip size. The ARM was used in Acorn's award winning Archimedes computers which in world terms were not well known except within a small techno-cult community. This cult community extended into California's silicon valley in the USA and the engineering laboratories of some major Japanese electronics corporations.

## Foundation of Advanced RISC Machines Ltd.

On November 28th 1990, twelve engineers from the original chip and software design team of Acorn were spun out into the independent company



examples which are entering the market today and will be totally pervasive by the year 2000.

**Personal Digital Assistants (PDAs)**

The first volume product in this category known as Newton™ was launched by Apple in Boston USA at the beginning of August 1993.

Today it is an "intelligent organiser" with address book, diary, calculator, to do list and note taker built in. I will briefly describe how you use it and its benefits;

Fitting into the palm of your hand you write onto a liquid crystal display (LCD) screen 80mm by 120mm with a plastic pen, as Newton™ converts your scrawl into readable text. Faxes and electronic mail can be sent from it and Newton keeps a good track of your personal priorities and actions. Because writing with a pen is so natural and as Newton is light weight, you use it everywhere and continually, ensuring that the most current data is stored in Newton's memory. As you meet people who have changed their job or phone number, you immediately up date your information and put new appointments in your calendar. Newton also helps you to make new friends who are very keen to see how the hand writing recognition works. I find waitresses in restaurants I visit are most fascinated by the device. Application programmes are supplied on 85mm by 55mm flash memory cards. Examples are:-

- Leisure:-** Time Out Guide to London,
- Business:-** the Fortune 500 top

Advanced RISC Machines (ARM) Limited. ARM Ltd's strategic goal is to establish the ARM as the leading processor for new emerging markets at the cross roads of computing, communications and consumer electronics. I was fortunate in being recruited to lead this outstanding team and to develop the International business of ARM. ARM Ltd's founders were Acorn Computers, Apple Computer and VLSI Technology Inc. Latterly NIF (Nippon Investment and Finance) which is Japan's second largest venture company became ARM's fourth investor.

**New Market Opportunities**

The Electronics Industry is currently undergoing rapid change with an increasing number and breadth of products being introduced that will change the way we live, work, learn and play. This transformation is occurring to improve the way that humans interact with machines and each other. Faced with the environmental challenges to reduce pollution, save fuel and costs, people are moving into an era where working effectively and remotely from home is now possible with the help of electronic mail, remote computer access, portable computers, mobile phones and fax machines. Distance learning with full media availability (sources of books, newspapers and films on CD and via cable) is extremely straight forward and

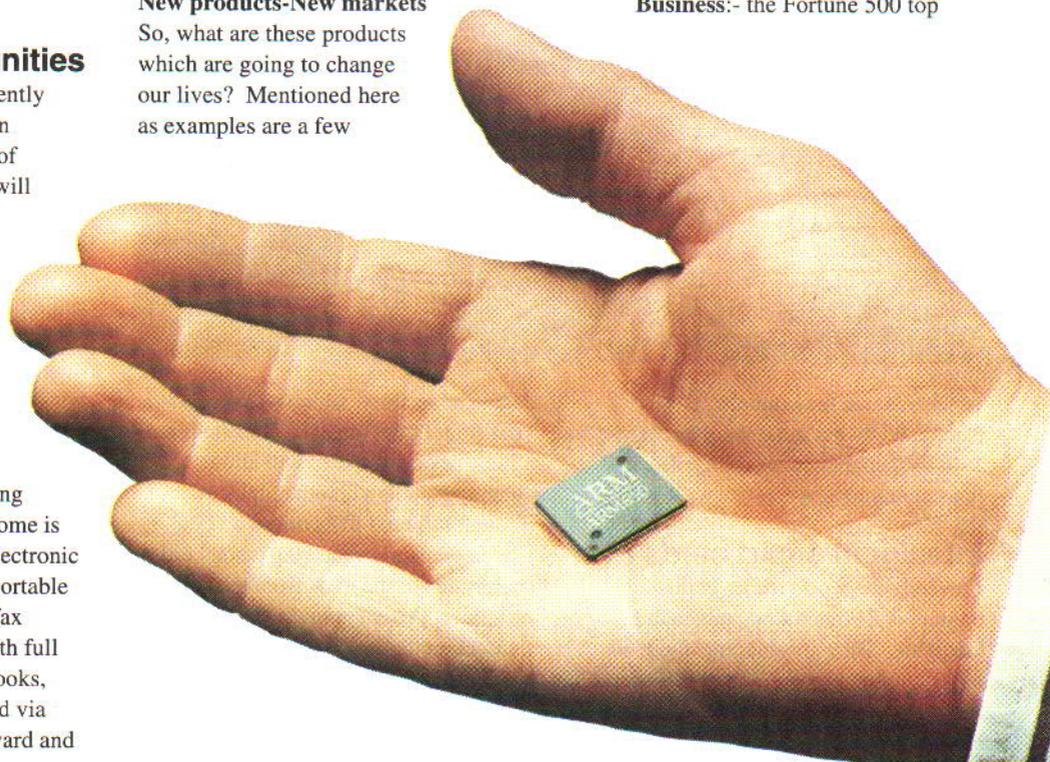
fun to use. Leisure media products offer high quality sound and 3D graphics capability. Dial up of information available in the best reference libraries of the world will be available at the touch of a button and at a low cost.

**Product Needs**

New classes of intelligent products share common themes of being cost effective, light weight, highly intuitive to use, very powerful and yet running from batteries for a long time, making them fully portable.

**New products-New markets**

So, what are these products which are going to change our lives? Mentioned here as examples are a few



businesses in the world, spread sheets, financial calculations

**Education:-** scientific calculators, the periodic table of the elements. foreign languages

**Personal:-** talking and moving pictures of your family

These application programmes can also be down loaded from central computers through telephone or radio links.

Newton™ also has an infra red link by

card. The information stored in memory is equivalent to monetary units and their main application is for public telephone booths especially in France. After use of say 50 units, they expire and can be thrown away.

The intelligent card of the future will store all your personal information, such as passport, current bank account balance and health details. It will be a personal smart card with a very high



which you can for example electronically exchange business cards with the people you meet. Apple call this beaming.

### Intelligent smart cards

Currently the world leader in this product is a French Company called Gemplus. They are shipping about 60 million units per year globally. Today's cards consist of an 8 bit microprocessor and memory mounted on a thin flexible

degree of security, which will recognise your finger print or voice. Inserted into a PDA device, the card will allow communication with other devices through infra red links or radio. For example imagine receiving a hotel bill transmitted to the PDA from the hotel's computer. After approving the transaction through, applying your signature on the PDA, the card would transfer money from your bank account to the hotel proprietor's account.

### New multi media games and education machines

In October 1993, Matsushita (National Panasonic) started shipping in the USA, an Interactive Multiplayer™ designed by "The 3DO Company" of California. This is an advanced CDROM device which can play audio and photo CD, movies, games and education programmes through your television set. By attaching a camcorder to the machine, you can input a picture of yourself so that you become the cartoon animation character in the game you are playing. It is the high quality sound, 3D graphics and interactive capability that makes this product different from other entertainment machines on the market today. When this device is attached through cable to a central station it may also be used for home shopping and interactive TV applications.

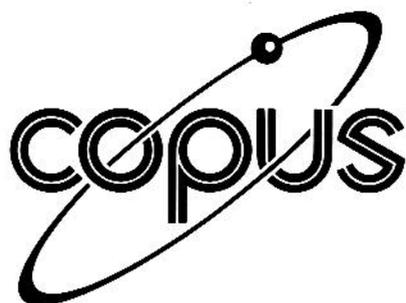
### Complete mobile phone capability

The GSM (global system mobile) and PCN (personal communication network) phone systems have recently started service in central London and Germany. These systems offer light weight and potentially lower cost portable voice and data global telephone capability. Eventually these systems will work anywhere in the world making communication easy wherever you are.

### Product vision for the year 2000

I imagine a product integrating all of the above capabilities being available by the year 2000. It would be light-weight and portable, be interactive with its users and have a high resolution colour LCD screen. It would also provide smart card security features and have PDA type intelligence (also with voice recognition) to be able to communicate globally by having access to the cable and satellite television network and access to data services through radio links.

This device becomes your TV set, note book, games machine, phone, fax, computer, organiser, language tutor, cinema rolled into one. Technologically this is possible, the only question, is how much will it cost? With the rate of progress of technology, and mans ingenuity, I think that such a device will be a high volume consumer product in this time frame. Most probably there will be families of devices for different applications.



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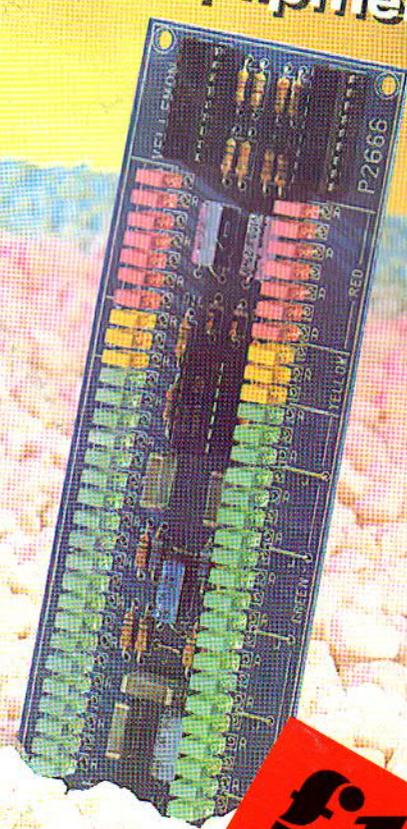
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