

An exciting hobby.... for everyone

PAGE 11

JULY 74

20p

# everyday electronics

## TELEPHONE CALL CHARGE CALCULATOR

Australia 40c  
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ALL  
INEXPENSIVE  
AND EASY TO  
BUILD

## AUTOMATIC LIGHT LEVEL CONTROLLER



**FREE** ENTRY  
COMPETITION

*Your last chance  
to win a...*

**Multimeter**

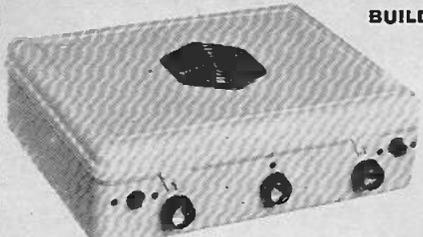
**GENERAL PURPOSE  
5WATT AMPLIFIER**



# NEW EDU-KIT MAJOR

COMPLETELY SOLDERLESS ELECTRONIC CONSTRUCTION KIT.

BUILD THESE PROJECTS WITHOUT SOLDERING IRON OR SOLDER.



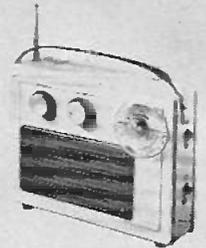
- ★ 4 Transistor Earpiece Radio ★ Signal Tracer ★ Signal Injector ★ Transistor Tester NPN-PNP ★ 4 Transistor Push Pull Amplifier ★ 5 Transistor Loudspeaker Radio MW/LW ★ 7 Transistor Loudspeaker Radio MW/LW ★ 5 Transistor Short Wave Radio ★ Electronic Metronome ★ Electronic Noise Generator ★ Batteryless Crystal Radio ★ One Transistor Radio ★ 2 Transistor Regenerative Radio ★ 3 Transistor Regenerative Radio ★ Audible Continuity Tester ★ Sensitive Pre-Amplifier.

Total Building Costs

**£7.23** P P & Ins. 44p.  
(Overseas P & P £1-85p.)  
(+ 10% VAT 72p)

- ★ 24 Resistors ★ 21 Capacitors ★ 10 Transistor ★ 21 loudspeaker ★ Earpiece ★ Mica Baseboard ★ 3 12-way connectors ★ 2 Volume controls ★ 2 Slider Switches ★ 1 Tuning Condenser ★ 3 Knobs ★ Ready Wound Coils ★ Ferrite Rod ★ 6 yards of wire ★ 1 yard of sleeving, etc. ★ Parts price list and plans 50p (FREE with parts).

## NEW ROAMER NINE



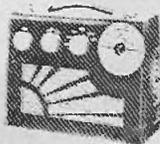
WITH V.H.F. INCLUDING AIRCRAFT

Nine Transistors, 9 Tunable wavebands as Roamer Ten, built in ferrite rod aerial for MW/LW. Retractable chrome plated telescopic aerial for V.H.F. and SW. Push Pull output using 600 mw transistors. 9 Transistors and 3 diodes, tuning condenser with V.H.F. section, separate coil for aircraft, moving coil loudspeaker, volume ON/OFF and wavechange control. Attractive all white case with red grille and carrying strap. Size 9 1/2" x 7" x 2 1/2" approx. Parts Price list and Plans 30p (FREE with parts)

Total Building Costs **£6.95** P P & Ins. 44p.  
(Overseas P & P £1-85p.)  
(+ 10% VAT 69p)

## ROAMER TEN

with V.H.F. including aircraft, 10 Transistors. Latest 4" 2 watt Ferrite Magnet Loudspeakers, 9 Tunable Wavebands, MWL, MWE, LW, SW1, SWE, SW3, Trawler Band, V.H.F. and Local Stations also Aircraft Band, Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be angled and rotated for peak short wave and V.H.F. listening. Push Pull output using 600 mw Transistors. Car Aerial and Tape Recording Sockets. 10 Transistors plus 3 Diodes. Gauged Tuning Condenser with V.H.F. section. Separate coil for Aircraft Band. Volume on/off, Wave Change and tone Control. Attractive Case in black with silver blocking. Size 9" x 7" x 4". Easy to follow instructions and diagrams. Parts price list and plans 30p (FREE with parts). Total building costs **£8.50** P P & Ins. 52p  
(Overseas P & P £1-85) (+ 10% VAT 85p)



## NEW EVERYDAY SERIES

Build this exciting New series of designs  
E.V. 5 6 Transistors and 2 diodes. MW/LW. Powered by 4.5 volt Battery. Ferrite rod aerial, tuning condenser, volume control, and loudspeaker. Attractive case with red speaker grille. Size 9" x 5 1/2" x 2 1/2" approx. Parts price list and Plans 15p. Free with parts.  
Total Building Costs **£2.95** P P & Ins. 30p  
(Overseas P & P £1-25p.)  
(+ 10% VAT 29p)



E.V. 6 Case and looks as above. 6 Transistors and 3 diodes. Powered by 9 volt battery. Ferrite rod aerial, 3" loudspeaker, etc., MW/LW coverage. Push Pull output. Parts price list and Plans 15p. Free with parts.  
Total Building Costs **£3.60** P P & Ins. 30p  
(Overseas P & P £1-25p.)  
(+ 10% VAT 36p)

E.V. 7 Case and looks as above. 7 Transistors and 3 diodes. Six wavebands. MW/LW, Trawler Band, SW1, SW2, SW3, powered by 9 volt battery. Push Pull output. Telescopic aerial for short waves. 3" loudspeaker. Parts price list and easy build plans 20p. Free with parts.  
Total Building Costs **£4.08** P P & Ins. 31p  
(Overseas P & P £1-85) (+ 10% VAT 40p)

## ROAMER EIGHT Mk 1 NOW WITH VARIABLE TONE CONTROL

7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mw transistors. Car aerial and Tape record sockets. Selectivity switch. 8 transistors plus 3 diodes. Latest 4" 2 watt Ferrite Magnet Loudspeakers. Air spaced gauged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9 x 7 x 4 1/2 approx. Easy to follow instructions and diagrams. Parts price list and plans 25p (FREE with parts).  
Total Building Costs **£6.98** P P & Ins. 47p  
(Overseas P & P £1-85) (+ 10% VAT 69p)



## "EDU-KIT"



Build Radios, Amplifiers, etc from easy stage diagrams, Five

units including master unit to construct

Components include:  
Tuning Condenser; 2 Volume Controls; 2 Slider Switches; Fine 5" Tone Moving Coil Speaker; Terminal Strip; Ferrite Rod Aerial; Battery Clips; 4 Tag Boards; 10 Transistors; 4 Diodes; Resistors; Capacitors; Three 1/2" Knobs. Units once constructed are detachable from Master Unit, enabling them to be stored for future use. Ideal for Schools, Educational Authorities and all those interested in radio construction. Parts price list and plans 25p (FREE with parts).

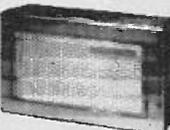
Total Building Costs **£5.50** P P & Ins. 35p  
(Overseas P & P £1-85) (+ 10% VAT 65p)

## ROAMER SIX Case and looks as Trans-Eight

6 Tunable Wavebands: MW, LW, SW1, SW2, SW3, Trawler band plus an Extra Medium waveband for easier tuning of Luxembourg etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. Six Speaker, 8 stages—6 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 x 6 1/2 x 2 1/2 approx. Plans and parts price list 25p (FREE with parts).  
Total Building Costs **£3.98** P P & Ins. 31p  
(Overseas P & P £1-85) (+ 10% VAT 39p)

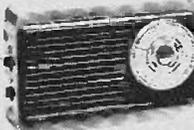
## POCKET FIVE

3 Tunable waveband. M.W./L.W. and Trawler Band. 7 stages, 5 transistors and 4 diodes, super-sensitive ferrite rod aerial, moving coil loudspeaker, attractive Black and Gold Case. Size 5 1/2" x 1 1/2" x 3 1/2" approx. Plans and parts price list 15p. (Free with parts).  
Total Building Costs **£2.50** P P & Ins. 26p  
(Overseas P & P £1-25p) (+ 10% VAT 25p)



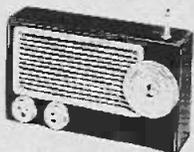
## TRANSONA FIVE

Wavebands, transistors and speaker as Pocket Five. Larger Case with Red Speaker Grille and Tuning Dial. Plans and parts price list 15p (Free with parts).  
Total Building Costs **£2.75** P P & Ins. 26p  
(Overseas P & P £1-25p) (+ 10% VAT 27p)



## TRANS EIGHT

8 TRANSISTORS and 3 DIODES  
6 Tunable Wavebands; MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. Six Speaker, 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9 x 5 1/2 x 2 1/2 approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and plans 25p (FREE with parts).  
Total Building Costs **£4.48** P P & Ins. 33p  
(Overseas P & P £1-25) (+ 10% V.A.T. 44p)



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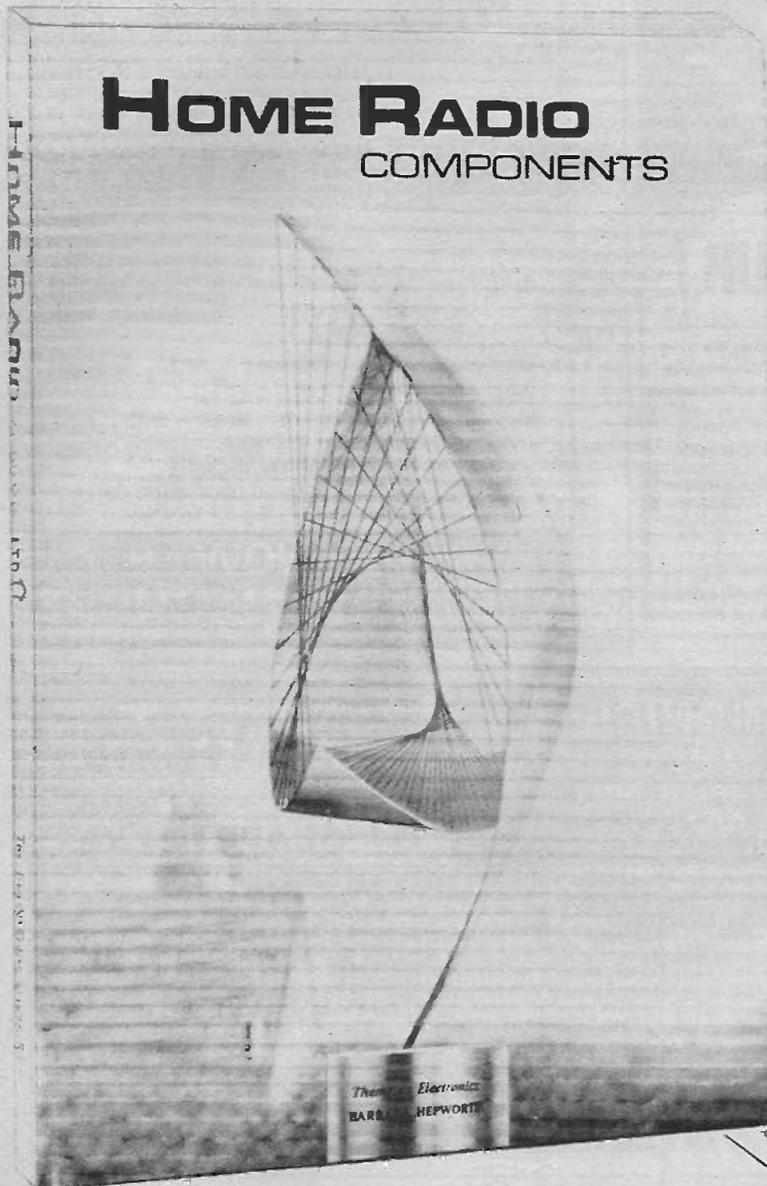
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## Beginner's Guide To Electronics

3rd Edition

T.L. Squires and C.M. Deason



This book describes as simply as possible the basic concepts in electronic engineering and the various components used in electronic equipment so that the reader gains an understanding of the terms used and the practical side of the subject. Prominence throughout has been given to the transistor and the integrated circuit.

- Provides a 'short cut' for those wishing to obtain a quick acquaintance with modern electronics
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**PLEASE ADD 10% VAT**

### RESISTORS

1W Iskra high stability carbon film—very low noise—capless construction.  
1W Mullard CR25 carbon film—very small body size 7.5 x 2.5 mm.

### 1W 2% ELECTROSIL TRS.

Power watts	Tolerance	Range	Values available	1-99	Price	100+
1	5%	4-7Ω-2.2MΩ	E24	1-3p	1-1p	1-1p
	10%	3-3MΩ-10MΩ	E12	1-3p	1-1p	1-1p
1/2	2%	10Ω-1MΩ	E24	3-5p	3p	3p
	10%	1Ω-3-9Ω	E12	1-3p	1-1p	1-1p
1/4	5%	4-7Ω-1MΩ	E12	1-3p	1-1p	1-1p
	10%	1Ω-10Ω	E12	8p	7p	7p

Quantity price applies for any selection. Ignore fractions on total order.

### DEVELOPMENT PACK

0-5 watt 3% Iskra resistors 5 off each value 4-7Ω to 1MΩ.  
E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70.

### POTENTIOMETERS

Carbon track 5kΩ to 2MΩ, log or linear (log 1W, 1in 1/2W).  
Single, 14p. Dual gang (stereo), 49p. Single D.P. switch 28p.

### SKELETON PRESET POTENTIOMETERS

Linear: 100, 250, 500Ω and decades to 5MΩ. Horizontal or vertical P.C. mounting (0-1 matrix).  
Sub-miniature 0-1W, 5p each. Miniature 0-25W, 7p each.

### SMOKE AND COMBUSTIBLE GAS DETECTOR—GD1

The GD1 is the world's first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide, methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Full details and circuits are supplied with each detector. Detector GD1 £2. Kit of parts for mains operated detector, including GD1 but excluding case £5.60. Suitable case £1.50. Kit of parts for 12 or 24V battery operation, including GD1 and PC Board £7.70. As above for PPG battery £8.90. Note: the battery operated kits incorporate our patented circuit to minimise battery drain—typically 90mA for 24V.

### PRINTED BOARD MARKER

97p  
Draw the planned circuit onto a copper laminate board with the P.C. Pen allow to dry, and immerse the board in the etchant. On removal the circuit remains in high relief.

### MULLARD POLYESTER CAPACITORS C296 SERIES

160V: 0-01μF, 0-015μF, 0-022μF, 0-033μF, 0-047μF, 0-068μF, 3p, 0-1μF, 3p, 0-15μF, 4p, 0-22μF, 5p, 0-33μF, 6p, 0-47μF, 7p, 0-68μF, 11p, 1-0μF, 13p.

### MULLARD POLYESTER CAPACITORS C290 SERIES

250V P.C. mounting: 0-01μF, 0-015μF, 0-022μF, 3p, 0-033μF, 0-047μF, 0-068μF, 3p, 0-1μF, 4p, 0-15μF, 0-22μF, 5p, 0-33μF, 6p, 0-47μF, 8p, 0-68μF, 11p, 1-0μF, 13p, 1-5μF, 20p, 2-2μF, 24p.

### MYLAR FILM CAPACITORS 100V: 0-001μF, CERAMIC DISC CAPACITORS

0-002μF, 0-005μF, 0-01μF, 0-02μF, 3p, 0-04μF, 100μF to 10,000μF, 2p each.  
0-05μF, 0-023μF, 0-1μF, 4p.

### ELECTROLYTIC CAPACITORS

(μFv) 1-63, 1-5/63, 2-2/63, 3-3/63, 4-7/63, 6-8/40, 6-8/63, 10/25, 10/63, 15/16, 15/40, 15/63, 22/10, 22/25, 22/63, 33-6-3, 33/16, 33/40, 47/4, 47/10, 47/25, 47/40, 68/6-3, 68/16, 100/4, 100/10, 100/25, 150/6-3, 150/16, 220/4, 220/6-3, 220/16, 330/4, 5p, 47/63, 100/40, 150/25, 220/25, 330/10, 470/6-3, 7p, 68/63, 150/40, 220/40, 330/16, 1000/4, 1p, 470/10, 680/6-3, 11p, 100/63, 150/63, 220/63, 1000/10, 12p, 470/25, 680/16, 1500/6-3, 13p, 470/40, 680/25, 1000/16, 1500/10, 2200/6-3, 18p, 330/63, 680/40, 1000/25, 1500/16, 2200/10, 3300/6-3, 4700/44, 21p.

### SOLID TANTALUM BEAD CAPACITORS

0-1μF	35V	2-2F	35μV	22μF	16V
0-22μF	35V	4-7F	35μV	33μF	10V
0-47μF	35V	6-8F	25μV	47μF	6-3V
1-0μF	35V	10F	25μV	100μF	3V

### VEROBOARD

2 1/2 x 3 1/2	0-1	0-15
2 1/2 x 5	24p	20p
2 1/2 x 8	28p	28p
3 1/2 x 3 1/2	28p	28p
3 1/2 x 5	32p	32p
17 x 2 1/2	85p	67p
17 x 3 1/2	120p	108p
17 x 3 1/2 (plain)	76p	52p
17 x 2 1/2 (plain)	—	41p
2 1/2 x 3 (plain)	—	12p
2 1/2 x 3 1/2 (plain)	—	11p
Pin insertion tool	62p	62p
Spot face cutter	52p	52p
Pkt. 50 pins	20p	20p

### JACK PLUGS AND SOCKETS

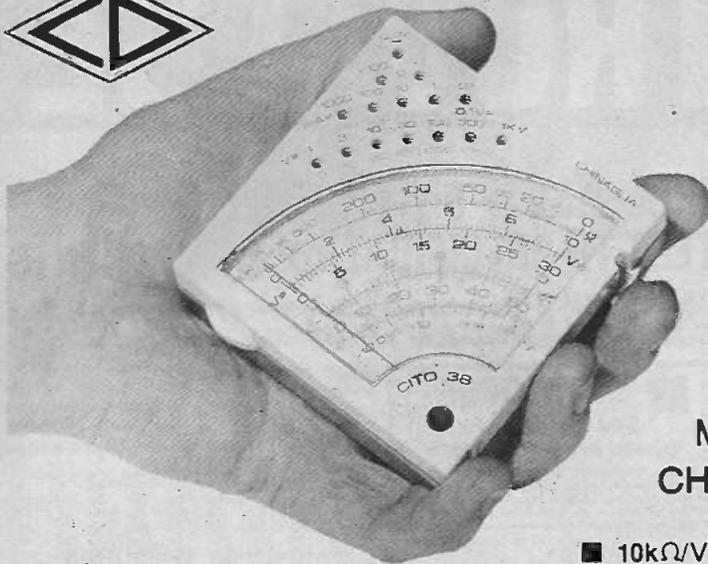
Standard screened	28p	2-5mm insulated	12p
Standard insulated	18p	3-5mm insulated	12p
Stereo screened	40p	3-5mm screened	18p
Standard socket	20p	2-5mm socket	11p
Stereo socket	30p	3-5mm socket	11p

### D.I.N. PLUGS AND SOCKETS

2 pin, 3 pin, 5 pin 1800, 5 pin 2400, 6 pin, 7 pin  
Plug 12p. Socket 8p.  
4 way screened cable, 25p/metre.  
6 way screened cable, 30p/metre.

### BATTERY ELIMINATOR

8V mains power supply. Same size as PP9 battery. £1-70



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THE TRULY POCKET  
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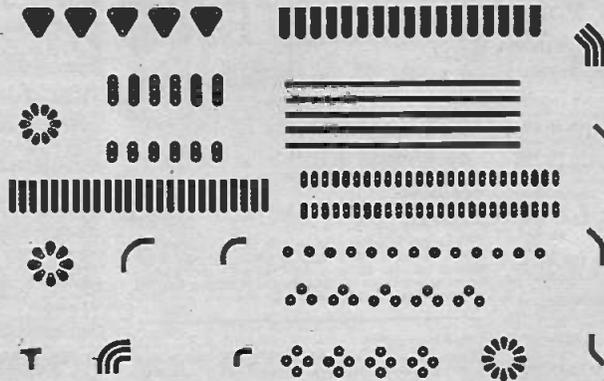
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Acid resistant transfers for direct application to P.C. Board. This is a new approach to printed circuit board manufacture, giving a professional finish with all details that an electronics engineer would require, including all drilling positions automatically marked.

Ideal for single unit boards or small quantities. All at a very low cost—for example an average 6" x 4" layout would cost less than 30p, and the time taken under one hour, including etching to complete.

The system is simple, briefly it consists of 10 sheets of self adhesive acid resistant transfers made in required shapes—i.e. edge connectors, lines, pads, dual in line I.C.'s, 8-10-12, T.O.5 Cans, 3-4 lead transistors, etc., etc., which only require pressing into the required positions on the printed circuit board before etching.

The printed circuit transfer system is a genuine offer to the public and industry. A full money back guarantee is sent with each order, trade prices on application.

### List of Prices

Complete system including post and VAT .....	£2.00
Individual sheets .....	22p
Sample sheet .....	22p
Copper laminate (boards) size 6" x 4½" 6 sheets.....	50p
(with six months guarantee)	

Printed circuit board PCB transfer systems patent applied for.

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and semi-conductors of many types from simple diodes to ICS photo-sensitive devices, threshold switches, etc. etc.  
**MINITRON DIGITAL INDICATORS**  
3415F Seven segment filament, compatible with standard logic modules, 0-9 and decimal point; 9mm characters in 16 lead DIL (some alphabetical symbols available) £1-20  
Suitable BCD decoder driver 7447 £1-15  
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**DALY ELECTROLYTIC**  
In cans, plastic sleeved  
1000µF/25V 28p 1000/50 41p  
5000/100 £2-91 2000/50 57p  
5000/25V 62p 5000/50 £1-18  
2200/100 £1-56

### POLYESTER TYPE C-220

Radial leads for P.C.B. mounting. Working voltage 250V d.c.  
0-01, 0-015, 0-022, 0-033, 0-047 ea. 3p  
0-068, 0-1, 0-15 ea. 4p  
0-22, 5p; 0-21 7p; 0-47 8p; 0-68 11p; 1-0 14p;  
1-5 21p; 2-2 24p

### SILVERED MICA

Working voltage 500V d.c.  
Values in pFs—2-2 to 820 in 32 stages ea. 6p  
1000, 1500 7p; 1800 8p; 2200 10p; 2700, 3600 12p;  
4700, 5000 15p; 6800 20p; 8200, 10,000 25p

### TANTALUM BEAD

0-1, 0-22, 0-47, 1-0 MFF 35V. ea. 14p  
2-2/16V, 2-2/35V, 4-7/16V, 10/6-3V ea. 14p  
4-7/35V, 10/16V, 22/6-3V ea. 18p  
10/25V, 22/16V, 47/6-3V 100/3V ea. 20p

### POLYCARBONATE

Type B42540 Working Voltage—250V  
Values in mF:  
0-0047; 0-0068; 0-0082; 0-01; 0-012; 0-015 ea. 3p  
0-018; 0-022; 0-027; 0-033; 0-039; 0-047; 0-056  
0-068; 0-082; 0-1 ea. 4p

### CERAMIC PLATE

Working voltage 50V. d.c.  
In 26 values from 22pf to 6800pF, each, 2p

### POTENTIOMETERS

**ROTARY CARBON TRACK.** Double wipers for good contact and long working life.  
P-20 SINGLE linear 100ohms to 4-7megohms, ea. 14p  
P-20 SINGLE log. 4-7Kohms to 2-2megohms, ea. 14p

JP-20 DUAL GANG lin. 4-7Kohms to 2-2megohms, ea. 48p

JP-20 DUAL GANG log. 4-7Kohms to 2-2megohms, ea. 48p

JP-20 DUAL GANG Log/antilog 10K, 22K, 47K, 1 megohm only ea. 48p

JP-20 DUAL GANG antilog 10K only 48p

2A DP mains switch for any of above 14p extra.

Decades of 10, 22 and 47 only available in ranges above.

Skeleton Carbon Presets Type PR, horizontal or vertical 6p each.

### SLIDER

Linear or log. 4-7K to 1 meg. In all popular values ea. 36p

Ecutcheon plates, black, white or light grey, ea. 10p

Control knobs, blk/wh/red/yel/grn/blue/dk. grey/lt. grey ea. 7p

### JACKS AND PLUGS

Sockets

2-circuit unswitched S1/SS 12p

2-circuit 1/2 break contacts S1/BB 15p

3-circuit unswitched (Not GPO) S3SSS 17p

3-circuit with 3 break contacts S3/BBB 20p

2-circuit with chrome nut and black/white/red/green or grey unswitched S3/SS 16p

with 2 break contacts S5/BB 20p

Miniature 3.5mm 2-circuit, (black) 2 br. cont S6/BB 9p

### PLUGS

2 circuit screened top entry P1 24p

side entry SEP1 36p

Line socket mono 231 40p

Line socket stereo 244 45p

3 circuit unscreened, bl/grey/wh. P4 48p

2 circuit, unscreened, bl/wh/red/bl/grn/grn P2 18p

3 circuit screen top entry P3 53p

side entry SEP3 55p

Miniature 3-5mm 2-circuit screened P5 13p

Min. 3-5mm 2-circ. unscrnd. various colours P6 10p

## EV CATALOGUE

### 2nd printing

(Green and buff cover)

112 pages, thousands of items; illustrations; diagrams; much useful technical information. The 2nd printing of this catalogue has been updated as much as possible on prices. It costs only 25p, post free and includes a refund voucher for 25p for spending when ordering goods list value £5 or more.

### INSULATED SCREW TERMINALS

In moulded polypropylene, with nickel plate on brass. With insulating set, washers, lag & nuts. 15A/250V in blk/brown/red/yel/grn/bl/grn/wh. Type TP.1, ea. 14p  
Suitable plugs Type TP4, 4mm each 7p  
Type TP2, 2mm each 4p

### ZENER DIODES

Full range E24 values: 400mW: 2-7V to 33V, 14p each; 1W: 5-8V to 32V, 21p each; 1-5W: 4-7V to 75V, 48p each, 20V: 7-5V to 75V, 69p each. Clip to increase 1-5W rating to 3 watts (type 266F), 5p.

### RESISTORS

Code	Watts	Ohms	1 to 9	10 to 99	100 up
C	1/3	4-7-470K	1-3	1-1	0-9 nett
C	1/2	4-7-10M	1-1	1-1	0-9 nett
C	3/4	4-7-10M	1-5	1-2	0-97 nett
C	1	4-7-10M	3-2	2-5	1-92 nett
MO	1/2	10-1M	4	3-3	2-3 nett
WW	1	0-22-3-9	9	9	8
WW	3	1-10K	7	7	6
WW	7	1-10K	9	9	8

Codes: C—carbon film, high stability, low noise.

MO—metal oxide, Electrofit TR5, ultra low noise.

WW—wire wound, Plessey.

Values: All E12 except C 1/3, C 1/2, and MO 1/2.

E12: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades.

E24: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

Tolerances: 5% except WW 10% ±0-05Ω under 10Ω and MO 1/2 2%.

Prices are in pence each for quantities of the same ohmic value and power rating. NOT mixed values. (Ignore fractions of one penny on total value of resistor order). Prices for 100 up in units of 100 only.

### VEROBOARD

Copper clad 0-1 matrix—2-5 x 3-75 ins. 30p; 3-75 x 3-75 ins.—30p; 2-5 x 5 ins.—30p; 3-75 x 5 ins.—33p.

Copper clad 0-15 lin. matrix 2-5 x 3-75 ins.—20p;

3-75 x 3-75 ins.—30p; 2-5 x 5 ins.—30p; 3-75 x 5 ins.—36p.

Vero spot face cutter (any matrix) 48p.

0-040 pins (for 0-1 matrix) per 100—38p.

0-052 pins (for 0-15 matrix) per 100—36p.

### APPOINTED STOCKISTS FOR SIEMENS QUALITY PRODUCTS

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Telephone Egham 3603 Telex 264475 Shop hours 9-5.30 daily: Sat. 9-1 p.m.

**NORTHERN BRANCH:** 680, Burnage Lane, Burnage, Manchester M19 1NA  
Telephone (061) 432 4945 Shop hours 9-1 p.m. 2-5.30 daily: Sat 9-1 p.m.

**U.S.A. CUSTOMERS** are invited to contact ELECTROVALUE AMERICA, P.O. Box 27, Swarthmore PA 19081.

### ELECTROLYTICS

Axial Lead	µF	3V	6-3V	10V	16V	25V	40V	63V	100V
0-47	—	—	—	—	—	—	11p	11p	8p
1-0	—	—	—	—	—	—	—	—	8p
2-2	—	—	—	—	—	11p	—	—	8p
4-7	—	—	—	—	—	—	8p	8p	8p
10	—	—	—	—	—	8p	8p	8p	8p
22	—	—	—	—	—	8p	8p	8p	10p
47	8p	—	—	—	—	8p	8p	8p	10p
100	9p	8p	8p	8p	8p	8p	8p	8p	10p
220	8p	8p	9p	10p	10p	11p	17p	24p	28p
470	9p	10p	10p	11p	13p	17p	24p	45p	—
1,000	11p	13p	13p	17p	20p	25p	41p	—	—
2,200	15p	18p	23p	26p	37p	41p	—	—	—
4,700	26p	30p	39p	44p	58p	—	—	—	—
10,000	42p	46p	—	—	—	—	—	—	—

### KNObS

In a great variety of modern types, for 1/4" shaft, from plastic to solid aluminium as well as pointer and numbered types.

### CONNECTORS

DIN from two way to 7 way plugs and sockets, phono types mains connections, etc. etc. Page 88 in Catalogue 7

### BAXANDALL SPEAKER KIT

As designed by P. J. Baxandall and described originally in "Wireless World." Simple to assemble, fantastically good results and a greater money saver. Carries 10 watts RMS, 15 ohms impedance. Size 18in x 12in x 10in. Complete kit, including pack-flat cabinet, £14-90.

The size and weight of this product obliges us to charge 70p cart cost of carr. In U.K.

Equaliser Assembly, £2-30

Loudspeaker Unit 59RM109, £2-45

Cabinet Kit (to Baxandall design), £10-45.

Cross-over choke for additional woofer to above £1-30

As designed by P. J. Baxandall and described originally in "Wireless World." Simple to assemble, fantastically good results and a greater money saver. Carries 10 watts RMS, 15 ohms impedance. Size 18in x 12in x 10in. Complete kit, including pack-flat cabinet, £14-90.

The size and weight of this product obliges us to charge 70p cart cost of carr. In U.K.

Equaliser Assembly, £2-30

Loudspeaker Unit 59RM109, £2-45

Cabinet Kit (to Baxandall design), £10-45.

Cross-over choke for additional woofer to above £1-30

## This is EV Service

### DISCOUNTS

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### PACKING AND POSTAGE FREE

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All goods are sold on the understanding that they conform to manufacturers' specifications and satisfaction is guaranteed as such—no rejects, 'seconds' or sub-standard merchandise is offered for sale.

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All postal communications, mail orders etc. to Head Office at Egham address, Dept. EE7. S.A.E. with enquiries requiring answers.



### SWR METER Model SWR3

Handy SWR meter for transmitter antenna alignment, with built-in field strength meter. Accuracy 5%. Impedance 52. Indicator 100uA DC. Full scale 5 section colorable antenna. Size 145 x 50 x 60mm.

**OUR PRICE £4.25** P&P 25p

### AT201 Decade ATTENUATOR

Frequency range 0-200kHz. Attenuator. 0-1110dB, 0.1dB steps. Impedance 600 ohms. Input power maximum 300mW. Size: 130 x 90 x 66mm.

**OUR PRICE £12.50** P&P 37p

### TRANSISTORISED I.C.R. A.C. BR/8 MEASURING BRIDGE

A new portable bridge offering excellent range and accuracy at low cost. Resistance: 6 ranges: 0.1 ohm-11.1 megohm ± 1% Inductance: 1 microhenry-111 henries ± 2% Capacity: 6 ranges: 10pF-1110 mFD ± 2% Turns Ratio: 6 ranges: 1:1/1000-1:11100 ± 1% Bridge Voltage at 1,000cps. Operating from 9-volt battery. 100 microamp meter indication. Size 7 1/2" x 6" x 2"

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### TE16A TRANSISTORISED SIGNAL GENERATOR

5 ranges, 400kHz to 30 MHz. An inexpensive instrument for the handy man. Operates on 9V battery. Wide easy to read scale. 800kHz modulation. Size: 148 x 148 x 92mm. Complete with instructions and leads.

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### MODEL TE20 RF SIGNAL GENERATOR

Six bands. 120kHz-260MHz. Dual output RF terminals. Separate variable audio output. Accuracy ± 2%. Audio output to 6V. Power requirements: 106-120V, 220-240V A.C. Size: 193 x 295 x 150mm. Complete with test leads etc.

**OUR PRICE £17.50** P&P 40p

### TE-200 RF SIGNAL GENERATOR

Accurate wide range signal generator covering 120 kHz-800 MHz x 6 bands. Directly calibrated. Variable R.F. transmitter audio output. Xtal socket for calibration. 220/240V a.c. Brand new with instructions. Size 140mm x 215mm x 170mm.

**OUR PRICE £17.50** P&P 30p

### TE22 SINE SQUARE WAVE AUDIO GENERATOR

Sine 20cps to 200kHz on 4 bands. Square 20 cps to 20 kHz. Output impedance 500 Ohms. 200/250V A.C. operation. Supplied brand new guaranteed, with instruction manual and leads.

**OUR PRICE £24.95** P&P 37p

### ARF 300 AF/RF SIGNAL GENERATOR

All transistorised compact fully portable. AF sine waves 18Hz to 220 kHz. AF square waves 18Hz to 100k Hz. Output Square/Sine waves 10V. P.F. 100kHz to 200kHz. Output 1V maximum. 220/240V A.C. operation. Complete with instructions and leads.

**OUR PRICE £37.50** P&P 60p

### MODEL MG100 SINE SQUARE WAVE AUDIO GENERATOR

Range 19-220,000Hz Sine Wave 19-100,000 Hz Square Wave. Output Sine or Square wave 10V. P. to P. Size 180 x 90 x 90mm Operation 220/240V. A.C.

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### PS200 Regulated POWER SUPPLY UNIT

Solid state. Variable output 5-20V DC up to 2 Amp. Independent meters to monitor voltage and current. Output 220/240V A.C. Size: 190 x 136 x 98mm.

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### POWER RHEOSTATS

High quality ceramic construction. Windings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range of sizes. Single hole fitting. 3/4" diameter shafts. Bulk quantities available.

1W 10/50/100/250/500/1000 Ohms **£1.15** P&P 10p

50 Watt 10/25/50/250/500/1000/2500/5000 Ohms. **£1.62** P&P 10p

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### YAMABISHI VARIABLE VOLTAGE TRANSFORMERS

Excellent quality at low cost. Input: 230V 50/60Hz. Output 0-260V. MODEL S260 BEACH MOUNTING

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2.5A £12.00 35p

5A £17.50 27p

8A £30.35 30p

10A £33.75 75p

12A £29.50 75p

20A £85.00 125p

25A £95.00 130p

40A £120.00 150p

MODEL S260B PANEL MOUNTING

1A £10.00 30p

2.5A £12.00 35p

### BV05 Vernier TUNING OIAL

App. 7:1 ratio planetary drive vernier dial. Log scale 0-180 degrees. Blank scales 1-5. Dial size 78 x 76mm. Overall size 190 x 117 x 41mm. Deep including knob and coupling. 3/4" diam. shaft

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MW 1-6 60x60mm **£6.50** P&P 15p

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### CP110 CHASSIS PUNCH SET

Carefully machined top grade steel. Contains 1/2", 5/8", 3/4", 1" and 1 1/8" punches complete with gripper and accessories.

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### HITACHI FLUORESCENT LANTERN L1901

A portable battery operated lantern ideal for home, motoring, camping etc. Approx. 10" tall. Provides brilliant light from a 1.5W battery (not supplied).

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Master and two sub-stations. Can be used on desk or wall mounted. Complete with cable and batteries.

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SKYFON 100mW **OUR PRICE £24.95** per pair  
P302 Two Channel 300mW **OUR PRICE £82.50** per pair  
P1003 Three Channel 1 Watt **OUR PRICE £71.25** per pair  
P&P 50p per pair  
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Features: 24 hour alarm setting, on/off and auto alarm 'sleep' switch. Illuminated rotary dial with hours, minutes and seconds. Automatically turns off radio, light etc. and with auto-switching will turn on again when required. 240V A.C. operation. Switch rating 250V-3 Amp.

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### SINCLAIR IC12 INTEGRATED CIRCUIT AMPLIFIER

complete with printed circuit mounting board. **OUR PRICE £2.35** P & P 15p

### LH025 STEREO HEADPHONES

Light weight head-phones with padded ear pieces. 4-15 ohms 20-20,000Hz. Complete with 6' lead and plug. **OUR PRICE £1.97** P&P 30p

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Sensitive magnetic headset with soft ear pads. Impedance 2,600 ohms (600 ohms DC). Frequency response: 200-4,000Hz. **OUR PRICE £2.25** P&P 30p

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Low cost with excellent response. Foam rubber cups. Adjustable headband. 8 ohms impedance. Frequency response 20Hz-18kHz. Complete with cable and stereo jack plug. **OUR PRICE £2.60** P&P 30p

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Volume control for each channel. 4-16 ohms impedance. Frequency response 20Hz-18kHz. Complete with 10ft. coiled lead and jack plug. **OUR PRICE £4.97** P&P 30p

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Moving coil. Ideal for language teaching, communications etc. Headphone impedance 16 ohms. Microphone impedance 200 ohms. **OUR PRICE £5.95** P&P 30p

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Tannoy 12" DR/8 Bass Speakers 8 ohms 30 watt. Heavy duty, ideal for Hi-Fi P.A. Group. **OUR PRICE £12.60** P&P 60p.

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Matched pair of stereo bookshelf speakers. Deluxe teak veneered finish. Size: 358 x 228 x 130mm. 8 ohms. 8 watts RMS. 16 watts peak. Complete with Din lead. **OUR PRICE £12.95** P&P 50p

### FM TUNER CHASSIS

6 transistor high quality tuner. Size only 153 x 101 x 63mm 3 IF stages. Double tuned discriminator. Ample output to feed most amplifiers. Operates on 9V battery. Covers 88-108MHz. Ready built, ready for use. Fantastic value for money. **OUR PRICE £8.95** P&P 20p

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6 transistor high quality unit - 3 IF stages and double tuned discriminator. For use with most amplifiers. Covers 88-108MHz. Powered by 9V battery. **OUR PRICE £13.50** P&P 30p

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8 digit display. Four functions plus logarithms to base 10, arith, sine, cosine, tangent, arcSine, arcCosine and arcTangent. Complete with instructions, case and batteries. Rec. Price £49.00. **OUR PRICE £44.50** P & P 25p plus VAT

### SINCLAIR SYSTEM 2000 STEREO AMPLIFIER AND TUNER

Amplifier output 8 watts per channel RMS. Distortion less than 0.06%. Silicon transistors. Two pick-up plus radio and tape inputs. tape output and scratch filter. Excellent Value. **OUR PRICE £28.50** P & P 60p.

### AMPLIFIER

Amplifier output 8 watts per channel RMS. Distortion less than 0.06%. Silicon transistors. Two pick-up plus radio and tape inputs. tape output and scratch filter. Excellent Value. **OUR PRICE £28.50** P & P 60p.

### FM TUNER

Excellent selectivity and sensitivity. Twin dual-varicap tuning. 4 pole ceramic filter. 18 transistor stereo demodulator giving 40 dB separation. Distortion 0.2% output. Fantastic Value. **OUR PRICE £28.50** P & P 60p.

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P28 Power Supply..... £7.98  
Transformer for P28..... £4.05

### SINCLAIR Project 80 Packages

2 x 240/Stereo 80/P25..... £25.00  
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POST & PACKING 35p each.

### MP7 MIXER-PREAMPLIFIER

5 Microphone inputs each with individual gain controls enabling complete mixing facilities. Battery operated. Size: 235 x 127 x 76mm. Inputs: Mic, 3 x 2mV 50k; 2 x 3mV 600 ohms. Phono, Mag. 400V 50k; Phono Ceramic 100mV 1 Meg. Output 250mV 100k. **OUR PRICE £8.97** P&P 20p

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### Post and Packing 15p per kit.

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AT25 Window wiper robot..... £5.82  
AT30 Photo cell switch unit..... £5.70  
AT50 400V triac light dimmer/speed control..... £4.80  
AT56 2,200W triac light dimmer/speed control..... £6.80  
AT60 1 channel light control..... £7.80  
AT65 3 channel light control..... £14.55  
GP304 Circuit board..... £4.94  
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GP312 Circuit board..... £11.45  
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### 1021 Stereo Listening Station

For balancing and gain selection of loudspeakers with additional facility for stereo headphone switching. Two gain controls, speakers on-off slide switch, stereo headphone socket. **OUR PRICE £2.25** P&P 15p

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C90 £1.87 £3.00 £7.08  
C90 £2.24 £4.25 £10.00  
C120 £2.73 £5.17 £12.24

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TYPE 5 10 25  
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CR90 £5.32 £10.46 £22.22

### AUDIOTRONIC 8 TRACK CARTRIDGES

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40M 85p £4.00 £7.50  
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### AUDIOTRONIC AHA101 Stereo Headphone Amplifier

All silicon, transistor amplifier operating from magnetic, ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9V battery. (INPUTS: 5mV and 100mV). OUTPUT: 50mV per channel. **OUR PRICE £8.50** P&P 20p

### EA41 REVERBERATION AMPLIFIER

Self contained, transistorised, battery operated. Simply plug in microphone, guitar etc. and output to your amplifier. Volume control and depth of reverb on control. Walnut cabinet. 184 x 77 x 108mm. **OUR PRICE £7.50** P&P 20p

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Size: 85 x 64mm

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100uA	£3.85
200uA	£3.70
500uA	£3.65
50-0-500uA	£3.75
100-0-1000uA	£3.70
1mA	£3.65
5mA	£3.65
10mA	£3.65
50mA	£3.65
100mA	£3.85
500mA	£3.65
1A DC	£3.65
5A DC	£3.65
10A DC	£3.65
5V DC	£3.65



10V DC	£3.65
20V DC	£3.65
50V DC	£3.65
15V AC	£3.65
30V AC	£3.75
VU Meter	£3.90

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Size: 100 x 80mm

50uA	£4.80
100uA	£4.80
500uA	£4.30
50-0-500uA	£4.50
100-0-1000uA	£4.45
1mA	£4.30
1A DC	£4.30
5A DC	£4.30
20V DC	£4.30
50V DC	£4.30
300V DC	£4.30



150V AC	£4.45
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VU Meter	£4.90

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Size: 90 x 34mm

50uA	£4.15
100uA	£4.10
200uA	£4.05
500uA	£3.90
50-0-500uA	£4.10
100-0-1000uA	£4.05
1mA	£3.95
300V AC	£3.85
VU Meter	£4.30



## MODEL ED107 EDUCATIONAL METER

Size: 100 x 90 x 150mm including terminals

A range of high quality moving coil instruments ideal for school experiments and other bench applications. 3" mirror scale. The meter movement is easily accessible to demonstrate internal working.



50uA	£8.50
100uA	£7.90
50-0-500uA	£7.90
1mA	£7.60
1-0-1mA	£7.60
1A DC	£7.60
5A DC	£7.60
10V DC	£7.60
15V DC	£7.60

20V DC	£7.60
50V DC	£7.60
300V DC	£7.60
500mA/5A DC	£8.60
5V/50V DC	£8.60
5V DC	£8.60
15A DC	£8.60
1A/15A DC	£8.60

## CLEAR PLASTIC MODEL MR 85P

Size: 120 x 110mm

50uA	£5.45
100uA	£5.40
200uA	£5.35
500uA	£5.25
50-0-500uA	£5.40
100-0-1000uA	£5.35
1mA	£5.20
10-1mA	£5.20
5mA	£5.20
10mA	£5.20
50mA	£5.20
100mA	£5.20
500mA	£5.20
1A DC	£5.20
5A DC	£5.20
15A DC	£5.20
30A DC	£5.40
10V DC	£5.20
20V DC	£5.20
50V DC	£5.20
150V DC	£5.20



300V DC	£5.20
15V AC	£5.30
30V AC	£5.30
5A AC	£5.20
15A AC	£5.20
30A AC	£5.20
1A DC	£5.20
5A DC	£5.20
10A DC	£5.20
20A AC	£5.20
30A AC	£5.20

\*Items with asterisk are Moving Iron type, all others are Moving Coil

## CLEAR PLASTIC MODEL SD830

Size: 110 x 83mm

50uA	£4.30
100uA	£4.25
200uA	£4.20
500uA	£4.15
50-0-500uA	£4.25
100-0-1000uA	£4.20
1mA	£4.10
5mA	£4.10
10mA	£4.10
50mA	£4.10
100mA	£4.10
500mA	£4.10
1A DC	£4.10
5A DC	£4.10
10A DC	£4.10
5V DC	£4.10



10V DC	£4.10
20V DC	£4.10
50V DC	£4.10
15V AC	£4.10
30V AC	£4.20
VU Meter	£4.40

## CLEAR PLASTIC MODEL MR 45P

Size: 50 x 50mm

50uA	£3.20
100uA	£3.15
200uA	£3.10
500uA	£3.05
50-0-500uA	£3.15
100-0-1000uA	£3.10
1mA	£2.95
5mA	£2.95
10mA	£2.95
20mA	£2.95
50mA	£2.95
100mA	£2.95
500mA	£2.95
1A DC	£2.95
5A DC	£2.95
10V DC	£2.95
20V DC	£2.95
50V DC	£2.95
300V DC	£2.95
15V AC	£3.05
30V AC	£2.95
50A AC	£2.95
100A AC	£2.95
200A AC	£2.95
300A AC	£2.95

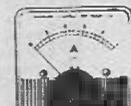


300V AC	£3.05
S Meter 1mA	£2.95
VU Meter	£3.40
1A AC	£2.95
5A AC	£2.95
10A AC	£2.95
20A AC	£2.95
30A AC	£2.95

## CLEAR PLASTIC MODEL MR 38P

Size: 42 x 42mm

50uA	£3.10
100uA	£3.05
200uA	£3.00
500uA	£2.85
50-0-500uA	£3.05
100-0-1000uA	£3.00
1mA	£2.80
1-0-1mA	£2.80
2mA	£2.80
5mA	£2.80
10mA	£2.80
20mA	£2.80
50mA	£2.80
100mA	£2.80
150mA	£2.80
200mA	£2.80
300mA	£2.80
500mA	£2.80
750mA	£2.80
1A DC	£2.80
2A DC	£2.80
5A DC	£2.80
10A DC	£2.80
3V DC	£2.80
10V DC	£2.80
15V DC	£2.80



20V DC	£2.80
50V DC	£2.80
150V DC	£2.80
300V DC	£2.85
500V DC	£2.85
750V DC	£2.80
15V AC	£2.90
50V AC	£2.90
150V AC	£2.90
300V AC	£3.00
S Meter 1mA	£2.80
VU Meter	£3.20

## CLEAR PLASTIC MODEL SD460

Size: 59 x 46mm

50uA	£3.80
100uA	£3.45
200uA	£3.40
500uA	£3.35
50-0-500uA	£3.45
100-0-1000uA	£3.40
1mA	£3.40
5mA	£3.30
10mA	£3.30
50mA	£3.30
100mA	£3.30
500mA	£3.30
1A DC	£3.30
5A DC	£3.30
10A DC	£3.30
5V DC	£3.30



10V DC	£3.30
20V DC	£3.30
50V DC	£3.30
300V DC	£3.30
15V AC	£3.45
30V AC	£3.45
50A AC	£3.45
VU Meter	£3.65

## CLEAR PLASTIC MODEL MR 65P

Size: 85 x 78mm

50uA	£3.95
100uA	£3.85
200uA	£3.80
500uA	£3.75
50-0-500uA	£3.85
100-0-1000uA	£3.80
100-0-5000uA	£3.70
1mA	£3.70
1-0-1mA	£3.70
5mA	£3.70
10mA	£3.70
50mA	£3.70
100mA	£3.70
500mA	£3.70
1A DC	£3.70
5A DC	£3.70
10A DC	£3.70
15A DC	£3.70
20A DC	£3.70
30A DC	£3.85
50A DC	£4.05
50V DC	£3.70
10V DC	£3.70
15V DC	£3.70
20V DC	£3.70
50V DC	£3.70
150V DC	£3.70



300V DC	£3.70
15V AC	£3.80
30V AC	£3.80
150V AC	£3.80
300V AC	£3.90
500V AC	£3.80
S Meter 1mA	£4.10
VU Meter	£3.70
1A AC	£3.70
5A AC	£3.70
10A AC	£3.70
20A AC	£3.70
30A AC	£3.70
50A AC	£3.70
100A AC	£3.70
200A AC	£3.70
500A AC	£3.70

## BAKELITE MODEL S80 Enlarged Window

Size: 80 x 80mm

50uA	£4.50
100uA	£4.45
200uA	£4.40
500uA	£4.35
50-0-500uA	£4.45
100-0-1000uA	£4.40
1mA	£4.20
10A DC	£4.20
5A DC	£4.20
20V DC	£4.20
50V DC	£4.20
15V AC	£4.40
30V AC	£4.20
300V AC	£4.30
VU Meter	£4.70



S Meter 1mA	£3.30
VU Meter	£3.80
1A AC	£3.30
5A AC	£3.30
10A AC	£3.30
20A AC	£3.30
30A AC	£3.30

## CLEAR PLASTIC MODEL MR 52P

Size: 60 x 60mm

50uA	£3.70
100uA	£3.50
200uA	£3.45
500uA	£3.40
50-0-500uA	£3.50
100-0-1000uA	£3.45
1mA	£3.30
5mA	£3.30
10mA	£3.30
50mA	£3.30
100mA	£3.30
500mA	£3.30
1A DC	£3.30
5A DC	£3.30
10V DC	£3.30
20V DC	£3.30
50V DC	£3.30
15V AC	£3.40
30V AC	£3.40
300V AC	£3.40



S Meter 1mA	£3.30
VU Meter	£3.80
1A AC	£3.30
5A AC	£3.30
10A AC	£3.30
20A AC	£3.30
30A AC	£3.30

## BAKELITE MODEL MR 65 Size: 80 x 80mm

25uA	£5.25
50uA	£4.00
100uA	£3.95
500uA	£3.65
50-0-500uA	£3.95
100-0-1000uA	£3.90
1mA	£3.60
10mA	£3.60
50mA	£3.60
100mA	£3.60
500mA	£3.60
1A DC	£3.60
2A DC	£3.60
5A DC	£3.60
10A DC	£3.60
15A DC	£3.60
30A DC	£3.60
50A DC	£3.80
5V DC	£3.60
10V DC	£3.60
15V DC	£3.60
20V DC	£3.60
50V DC	£3.60
150V DC	£3.60



300V DC	£3.60
30V AC	£3.60
50V AC	£3.60
150V AC	£3.60
300V AC	£3.60
500V AC	£3.60
VU Meter	£4.10
1A AC	£3.60
5A AC	£3.60
10A AC	£3.60
20A AC	£3.60
30A AC	£3.60
50A AC	£3.60
100A AC	£3.60
200A AC	£3.60
500A AC	£3.60

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33 TOTENHAM CT. RD.	01-636 2605
42/45 TOTENHAM CT. RD.	01-636 0845
87 TOTENHAM CT. RD.	01-580 3739
257/8 TOTENHAM CT. RD.	01-580 0670
3 LISLE ST. WC2	01-437 8204
34 LISLE ST. WC2	01-437 9155
118 EDGWARE RD. W2	01-723 9789
193 EDGWARE RD. W2	01-723 6211
207 EDGWARE RD. W2	01-723 3271
311 EDGWARE RD. W2	01-262 0387
346 EDGWARE RD. W2	01-723 4453
382 EDGWARE RD. W2	01-723 4194
109 FLEET ST. EC4	01-353 5812
152/3 FLEET ST. EC4	01-353 2833

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## EX COMPUTER BOARDS

Packed with transistors, diodes, capacitors and resistors—COMPONENT VALUE £1.50. 3 for ONLY 55p + p & p 30

**SPECIAL ONE.** As above PLUS Power Transistors ONLY 45p each + p & p 15p

**STABILISED POWER MODULES**  
Complete with circuit diagrams, etc. 59p each + p & p 15p

**PAKOLITE BOARDS** 7 1/2" x 9" approx. 4 for 80p + p & p 20p.

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16 1/2 x 4" approx. 2 for 65p

## DECON-DALO 33PC Marker

Ethc resistant printed circuit marker pen 90p each

## VEROBOARDS

Packs containing approx. 50± ins. various sizes, all 1-matrix 65p

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RF Chokes  
CH1. 2.5mH 25p CH2. 5.0mH 25p  
CH3. 7.5mH 25p CH4. 10mH 25p  
CH5. 1.5mH 25p

## COILS

DRX1 Crystal set 81p DRB2 Dual range 45p

## COIL FORMERS & CORES

NORMAN 1/2" Cores & Formers 7p  
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## SWITCHES

DP/DT Toggle 25p SP/ST Toggle 18p

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1 1/2" and 20mm, 100mA, 200mA, 250mA, 500mA, 1A, 1.5A, 2A  
QUICK-BLOW 4p ea. ANTI-SURGE 5p ea.

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Crystal 3.5mm plug 33p  
8 ohms 2.5mm plug 22p  
8 ohms 3.5mm plug 22p

## DYNAMIC MICROPHONES

B1223. 200 ohms plus on/off switch and 2.5mm and 3.5mm plugs £1.60

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H1012 £1.87

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K4007. 60 ohms Imp. Insertion loss 3dB £1.21

## CAR STEREO SPEAKERS

(Angled) £3.85 per pair.

## BI-PAK

CATALOGUE AND LISTS  
Send S.A.E. and 10p.

## INSTRUMENT CASES



(Black Vinyl covered)

No.	Length	Width	Height	Price
BV1	8"	4"	2"	90p
BV2	11"	6"	3"	£1.20

## ALUMINIUM BOXES

BA1	5 1/2"	4"	1 1/2"	42p
BA2	4"	4"	1 1/2"	41p
BA3	4"	2 1/2"	1 1/2"	41p
BA4	5 1/2"	4"	1 1/2"	47p
BA5	4"	2 1/2"	2"	41p
BA6	3"	2 1/2"	1 1/2"	34p
BA7	7"	5"	2 1/2"	68p
BA8	8"	6"	3"	84p
BA9	6"	4"	2"	54p

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18 BALDOCK ST., WARE, Herts. (A10)

Open Mon.-Sat. 9-5.30 p.m. Tel. 61592

## BIB HI-FI ACCESSORIES

### De Luxe Groov-Kleen

Model 42 £1.84

Chrome Finish Model 60 £1.50



Ref. 36A. Record/Styleus Cleaning Kit 28p

Ref. 43. Record Care Kit £2.35

Ref. 31. Cassette Head Cleaner 54p

Ref. 32. Tape editing Kit £1.54

Model 9. Wire Stripper/Cutter 83p

Ref. P. Hi-Fi Cleaner 81p

Ref. 32A. Styleus Balance £1.38

Ref. J. Tape Head Cleaning Kit 51p

Ref. 34. Cassette Case £1.27

Ref. 55. Hi-Fi Stereo Hints & Tips 32p

## ANTEX SOLDERING IRONS

X25. 25 watt £1.93

OCN 240. 15 watt £2.15

Model G. 18 watt £2.15

8K2. Soldering Kit £2.88

STANDS: ST1 £1.21. ST2 77p

SOLDER: 18SWG Multicores 7oz 82p

22SWG 7oz 82p. 18SWG 22ft 25p

22SWG Tube 22p

## ANTEX BITS AND ELEMENTS

Bits No.

102 For model CN240 3/32" 38p

104 For model CN240 3/16" 38p

1100 For model CCN240 3/32" 38p

1101 For model CCN240 3/8" 38p

1102 For model CCN240 1/2" 38p

1020 For model G240 3/32" 38p

1021 For model G240 1/8" 38p

1022 For model G240 3/16" 38p

50 For model X25 3/32" 38p

51 For model X25 1/8" 38p

52 For model X25 3/16" 38p

## ELEMENTS

ECN 240 £1.16 EOCN 240 £1.33

EG 240 £1.16 EX 25 £1.16

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V.A.T. included in all prices. Please add 10p P. & P. (U.K. only). Overseas orders—please add extra for postage.

## NEW COMPONENT PAK BARGAINS

Pack No. Qty. Description Price

C1 250 Resistors mixed values approx. count by weight 0.55

C2 200 Capacitors mixed values approx. count by weight 0.55

C3 50 Precision Resistors 1%, 2% mixed values 0.66

C4 75 1/4 W Resistors mixed preferred values 0.55

C5 5 Pieces assorted Ferrite Rods 0.65

C6 2 Tuning Gangs, MW/LW VHF 0.55

C7 1 Pack Wire 60 metres assorted colours 0.55

C 8 10 Reed Switches 0.55

C 9 3 Micro Switches 0.55

C10 15 Assorted Pots & Pre-Sets 0.55

C11 5 Jack Sockets 3 x 3.5m 2 x Standard Switch Type 0.55

C12 40 Paper Condensers preferred types mixed values 0.55

C13 20 Electrolytics Trans. types 0.55

C14 1 Pack assorted Hardware—Nuts/Bolts, Grommets etc. 0.55

C15 4 Mains Slide Switches 0.55

C16 20 Assorted Tag strips & Panels 0.55

C17 10 Assorted Control Knobs 0.55

C18 4 Rotary Wave Change Switches 0.55

C19 3 Relays 4-24V Operating 0.55

C20 4 Sheets Copper Laminate approx. 10" x 7" 0.55

## PLUGS AND SOCKETS

### SOCKETS

PS 35 DIN 2 Pin (Speaker) 0.06

PS 36 DIN 3 Pin 0.10

PS 37 DIN 5 Pin 180° 0.10

PS 38 DIN 5 Pin 240° 0.10

PS 39 Jack 2.5mm Switched 0.09

PS 40 Jack 3.5mm Switched 0.10

PS 41 Jack 1/2" Switched 0.17

PS 42 Jack Stereo Switched 0.96

PS 43 Phono Single 0.06

PS 44 Phono Double 0.06

PS 45 Car Aerial 0.10

PS 46 Co-Axial Surface 0.09

PS 47 Co-Axial Flush 0.14

### INLINE SOCKETS

PS 21 D.I.N. 2 Pin (Speaker) 0.13

PS 22 D.I.N. 3 Pin 0.17

PS 23 D.I.N. 5 Pin 180° 0.17

PS 24 D.I.N. 5 Pin 240° 0.17

PS 25 Jack 2.5mm Plastic 0.10

PS 26 Jack 3.5mm Plastic 0.12

PS 27 Jack 1/2" Plastic 0.24

PS 28 Jack 1/2" Screened 0.28

PS 29 Jack Stereo Plastic 0.28

PS 30 Jack Stereo Screened 0.82

PS 31 Phono Screened 0.14

PS 32 Car Aerial 0.15

PS 33 Co-Axial 0.17

## PLUGS

PS 1 D.I.N. 2 Pin (Speaker) 0.11

PS 2 D.I.N. 3 Pin 0.12

PS 3 D.I.N. 4 Pin 0.15

PS 4 D.I.N. 5 Pin 180° 0.14

PS 5 D.I.N. 5 Pin 240° 0.15

PS 6 D.I.N. 6 Pin 0.15

PS 7 S.I.N. 7 Pin 0.15

PS 8 Jack 2.5mm Screened 0.10

PS 9 Jack 2.5mm Plastic 0.09

PS 10 Jack 3.5mm Screened 0.12

PS 11 Jack 1/2" Plastic 0.13

PS 12 Jack 1/2" Screened 0.18

PS 13 Jack Stereo Screened 0.99

PS 14 Phono 0.06

PS 15 Car Aerial 0.15

PS 16 Co-Axial 0.10

## CABLES

CP 1 Single Lapped Screen 0.06

CP 2 Twin Common Screen 0.06

CP 3 Stereo Screened 0.06

CP 4 Four Core Common Screen 0.23

CP 5 Four Core Individually Screened 0.30

CP 6 Microphone Fully Braided Cable 0.10

CP 7 Three Core Mains Cable 0.07

CP 8 Twin Oval Mains Cable 0.06

CP 9 Speaker Cable 0.04

CP 10 Low Loss Co-Axial 0.10

## CARBON POTENTIOMETERS

Log and Lin

4.7K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M

VC 1 Single Less Switch 0.14

VC 2 Single D.P. Switch 0.28

VC 3 Tandem Less Switch 0.44

VC 4 1K Lin Less Switch 0.14

VC 5 100K Log anti-Log 0.44

## HORIZONTAL CARBON PRESETS

0.1 watt 0.06 each

100, 220, 470, 1K, 2.2K, 4.7K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M, 4.7M

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2N3045. Silicon Power Transistors NPN. Famous manufacturers out-of-spec devices free from open and short defects—every one abel 115w. T03. Metal Case.

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0.01UF 400V. 5p. each  
500UF 50V. Elect. 10p each

## RECORD STORAGE/CARRY CASES

7 1/2" EP. 18 1/2" x 7" x 8". (50 records) £2.10  
12" LP. 13 1/2" x 7 1/2" x 1 1/2". (50 records) £2.95

## CASSETTE CASES

Holds 12. 10" x 3 1/2" x 5". Lock & Handle. £1.30

## 8-TRACK CARTRIDGE CASES

Holds 14. 13" x 5" x 6". Lock & Handle. £1.95  
Holds 24. 13 1/2" x 8" x 5 1/2". Lock & Handle. £2.70  
COLOURS: Red, Black and Tan—Please state preference.

## REPANCO TRANSFORMERS

240v. Primary. Secondary voltages available from selected tappings 4v, 7v, 8v, 10v, 14v, 15v, 17v, 19v, 21v, 26v, 31v, 33v, 40, 50 and 25v-0-25v.

Type	Amps.	Price	P & P
MT50/1	1	£1.93	30p
MT50/1	1	£2.42	35p
MT50/2	2	£3.30	40p

## CARTRIDGES

ACOS GP91-18C. 200mV at 1.2cm/sec £1.18  
ACOS GP92-1. 280mV at 1cm/sec £1.65  
ACOS GP96-1. 100mV at 1cm/sec £2.65  
TTC J-2005. Crystal/Hi Output 95p  
TTC J-20 10C Crystal/Hi Output Compatible £1.30  
TTC J-206 CS Stereo/Hi Output £1.60  
TTC J-2105 Ceramic/Med. Output £1.84

## CARBON FILM RESISTORS

The E13 Range of Carbon Film Resistors. 1/8th watt available in PAKS of 50 pieces, assorted into the following groups—

R1	50 Mixed 100 ohms-820 ohms	40p
R2	50 Mixed 1K ohms-8.2K ohms	40p
R3	50 Mixed 10K ohms-82K ohms	40p
R4	50 Mixed 100K ohms-1 Meg. ohms	40p

THESE ARE UNBEATABLE PRICES—LESS THAN 1p EACH INCL. V.A.T.

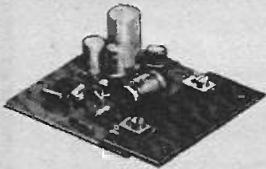
## BI-PAK SUPERIOR QUALITY LOW - NOISE CASSETTES

C60. 32p C90. 41p C120. 52p

# -the lowest prices!

## BI-PAK QUALITY COMES TO AUDIO!

### AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	$P_o = 3 \text{ WATTS } f = 1\text{KHz}$	0.25%
LOAD IMPEDANCE	—	8 - 16 $\Omega$
INPUT IMPEDANCE	$f = 1\text{KHz}$	100 k $\Omega$
FREQUENCY RESPONSE @ 3dB	$P_o = 2 \text{ WATTS}$	50 Hz - 25KHz
SENSITIVITY FOR RATED O/P	$V_s = 25\text{V. } R_L = 8 \Omega f = 1\text{KHz}$	76mV. RMS
DIMENSIONS	—	3" x 2 1/4" x 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. ( $R_L = 8 \Omega f = 1 \text{ KHz}$ )	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.

#### AUDIO AMPLIFIER MODULES

AL 10. 3 watts RMS £2.10  
AL 20. 5 watts RMS £2.59  
AL 30. 10 watts RMS £3.01

#### POWER SUPPLIES

P8 12. (Use with AL10 & AL20) 83p  
SFM 80. (Use with also AL30 & AL50) £3.25  
FRONT PANELS SP 12 with Knobs £1.10

#### PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20) £4.35  
PA 100. (Use with AL30 & AL50) £13.15

#### TRANSFORMERS

T461 (Use with AL10) £1.38 P & P 15p  
T538 (Use with AL20) £1.93 P & P 15p  
BMT80 (Use with AL30 & AL50) £2.15 P & P 25p

#### PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with ceramic cartridges while the auxiliary input will suit most magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm x 84mm x 35mm.

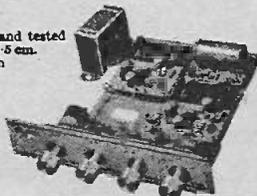
Frequency response—  
20Hz - 20KHz (-3dB)  
Bass control—  
 $\pm 12\text{dB at } 60\text{Hz}$   
Treble control—  
 $\pm 14\text{dB at } 14\text{KHz}$   
\*Input 1. Impedance  
1 Meg. ohm  
Sensitivity 300mV  
†Input 2. Impedance  
30 K ohms  
Sensitivity 4mV

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ALL PRICES INCLUDE V.A.T.

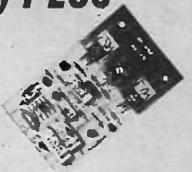
### The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch volume control, balance, bass and treble controls, Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power: 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 20Hz-25KHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control  $\pm 12\text{dB at } 60\text{Hz}$  typically 0.25% at 1 watt. Treble con.  $\pm 14\text{dB at } 14\text{KHz}$ .



£14.45

### NOW WE GIVE YOU 50w PEAK (25w R.M.S.) PLUS THERMAL PROTECTION! The NEW AL60 Hi-Fi Audio Amplifier FOR ONLY £3.95



- Max Heat Sink temp. 90°C.
- Frequency Response 20Hz to 100KHz
- 0.1% Distortion
- Distortion better than 1% at 1KHz
- Supply voltage 10-35 volts
- Thermal Feedback
- Latest Design Improvements
- Load—3, 4, 8 or 16 ohms
- Signal to noise ratio 80dB
- Overall size 63mm x 105mm x 13mm

Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

### STABILISED POWER MODULE SPM80



AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 1.5 amps at 35 volts. Size: 63mm x 105mm x 30mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including—Disco Systems, Public Address Intercom Units, etc. Handbook available 10p PRICE £3.25

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### STEREO PRE-AMPLIFIER TYPE PA100

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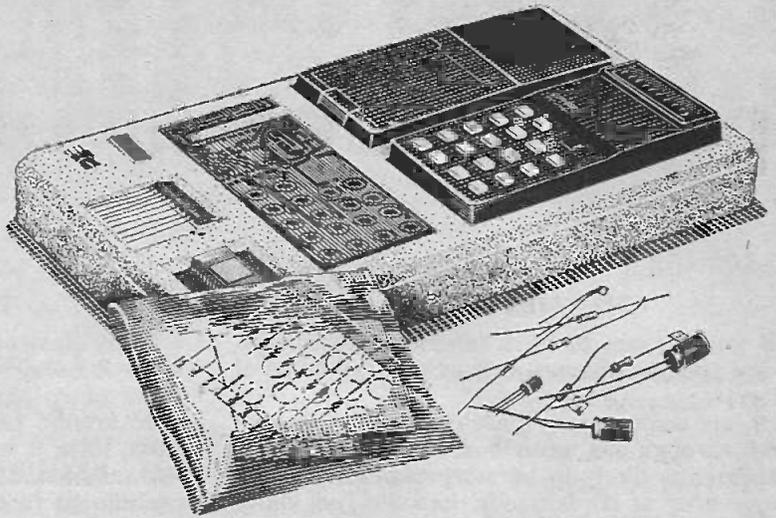


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6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.



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If you just use your Sinclair Cambridge for routine arithmetic – for shopping, conversions, percentages, accounting, tallying, and so on – then you'll get more than your money's worth.

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How? It's all explained in this unique booklet, written by a leading calculator design consultant. In its fact-packed 32 pages it explains, step by step, how you can use the Sinclair Cambridge to carry out complex calculations.

# sinclair

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Everyday Electronics, July 1974

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# everyday electronics

PROJECTS...  
THEORY.....

## ON THE PHONE

If you happen to be a telephone subscriber, one of this month's projects cannot fail to be of interest.

Of all those many unwelcome missiles that shoot through the letter box at quarterly intervals none is likely to be more unpredictable in the severity of its demands than the Post Office bill for telephone service.

"Surely we can't have made all those calls?" are the first words to be gasped by the unbelieving recipient following examination of the account. The customary dire warnings to all members of the household to moderate their conversations in future are then made—but have little lasting effect, as the next bill will undoubtedly show.

Strange how those minutes tick away. And at today's rates the charges rapidly mount up. What is required is some means to monitor the total call charge ticking up as one speaks. This, we are happy to say, is now possible with the *Telephone Call Charge Calculator* described in this issue.

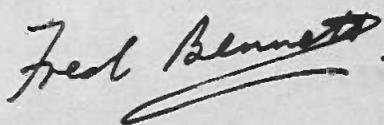
A useful aid to have beside the 'phone, an ever-present reminder of the accumulated call charges and (let's hope) a deterrent or moderating influence for the more loquacious members of the family.

## TRY IT AND SEE

Many devices essential in electronics as we know it today were not in existence a mere 20 years or so ago. The magnet, in contrast, has been around rather longer: in its natural lode-stone form it was in use about 4,000 years ago. An understanding of magnetism is an essential prelude to further study into electronics principles. So this venerable yet humble and commonplace device receives top billing in the opening articles of our new series *Physics Is Fun!*

These articles, specially prepared for beginners, are intended to amuse and instruct by means of simple experiments anyone can carry out at home. The expense involved will be nil, or very nearly so. For this is one special and exceptional occasion when we advocate the seeking out an use of "junk" material.

Just try the experiments and you'll quickly discover that the title of this series is perfectly true.

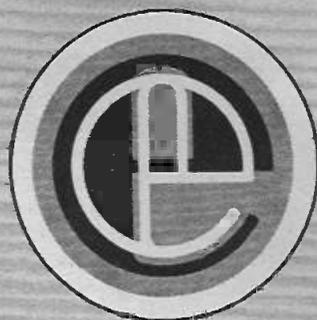


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# EASY TO CONSTRUCT SIMPLY EXPLAINED

VOL. 3 NO. 7

JULY 1974

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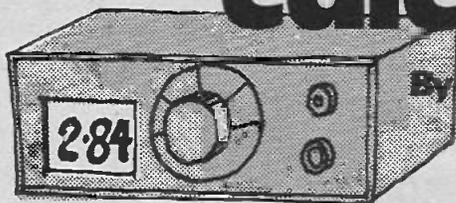
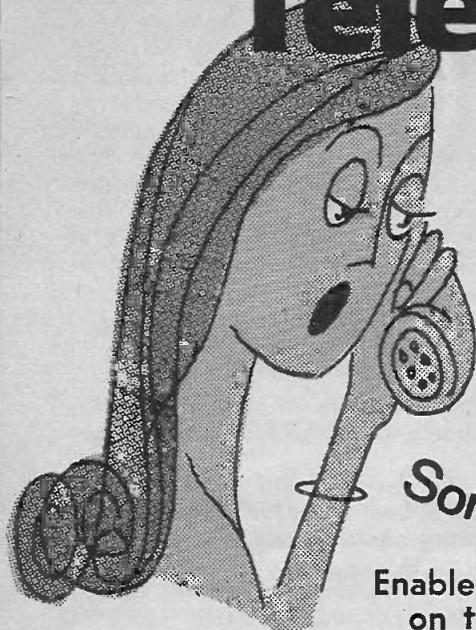
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# Telephone call charge calculator



By **BRIAN W. TERRELL** B.Sc.

Sorry - can't afford another second....

Enables you to keep a watchful eye on the mounting telephone bill.

WITH the ever-increasing cost of living, it is the wise person who keeps a controlling eye on his (or her) bills as they are mounting up and puts funds aside regularly to meet the bills, so that when they do arrive he is adequately prepared for the amount demanded.

As far as electricity and gas bills are concerned, these can be easily estimated since there are dials and meters that the consumer can read and note. With the telephone bill it is not so easy since there are no dials to be read by the user and the cost of a telephone call depends on three factors:

1. Time spent on the telephone
2. Time of day the call is made
3. The distance of the call

With all these factors to take into consideration, the calculation of the costing of calls becomes complex and tedious.

The Telephone Call Charge Calculator does all the calculating for you electronically, and automatically gives you a running total of all calls placed, thus enabling the cost of all self-dialled calls over any period to be noted and allowed for.

## CHARGES

The relation between the three factors mentioned above and the cost of a call is summarised in Table 1 which is reproduced from the latest Post Office leaflet entitled "New Charges for Telecommunications Services".

It is seen from Table 1 that times for all calls are normalised to a unit of one penny (1p)—see later; that is to say, depending on the call made, one penny buys a fixed amount of time and this is charged whether the whole time is used or

Table 1: Time bought for 1p for trunk and local dialled telephone calls from STD exchanges.

Peak Mon-Fri 9am-noon	Standard Mon-Fri 8am-9am noon-6pm	Cheap Every night 6pm-8am and all day Sat and Sun	Code
24	40	90	a
8	10	40	c
(seconds)			
<b>Local calls</b>	Mon-Fri 8am-6pm All other times	3min 12min	1 2

not. For example, if a "c" call is made during the "peak" period, and the call lasts for 18 seconds, the cost is three pence.

## THEORY

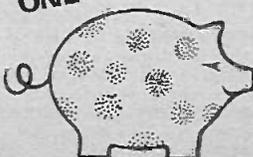
The block diagram of the unit is shown in Fig. 1. It consists of a pulse generator whose

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\*Based on prices prevailing at time of going to press



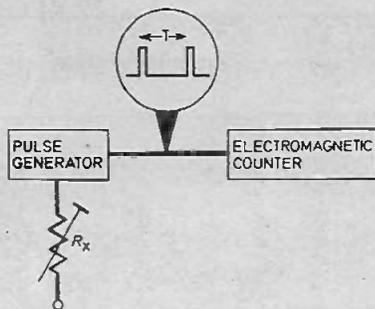


Fig. 1. Block diagram of the unit.

periodic time ( $T$ ) can be controlled by selecting value of  $R_x$  these values being trimmed so that the periodic times of the pulses are made equal to the fixed times depicted in Table 1.

The pulses are then fed to an electromagnetic counter which causes its readout to advance by one unit for each pulse received.

### INTEGRATED CIRCUIT

The heart of the unit is the versatile timer i.c. known as the "555". It is used in the astable multivibrator mode, see Fig. 2, and thus forms the pulse generator.

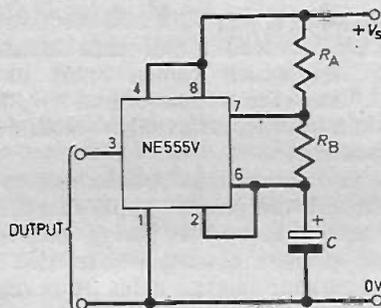


Fig. 2. The 555 timer i.c. wired as an astable multivibrator.

On connecting the positive supply voltage, the capacitor begins to charge up through the series combination  $R_A + R_B$ . When the potential at pin 6 reaches two-thirds the supply voltage, the internal circuitry of the i.c. switches and the capacitor begins to discharge through resistor  $R_B$ . When the potential at pin 6 drops to one-third the supply voltage, the internal circuitry resets and re-charging starts immediately. This action is repeated for as long as the supply is connected.

The output is at pin 3 and the voltage here can have only two values, these being either equal to the positive supply voltage or zero. While the capacitor is charging the output is equal to the supply voltage, when the capacitor is discharging the output is zero. This action is shown graphically in Fig. 3.

The reasons for using the 555 i.c. are two-fold; firstly construction is made very simple and secondly the most important, the frequency

( $1/T$ ) of the multivibrator is virtually independent of the supply voltage which can range from 5 to 15V. Also, the frequency is virtually unaffected by temperature over its range of 0 to 70 degrees centigrade. The choice of operating voltage depends on the type of electromagnetic counter used; the type used in the prototype had a coil impedance of 500 ohms and operates from a voltage in the range 12 to 24 volts. With the transformer specified, an output of 15V is available which satisfies both counter and i.c.

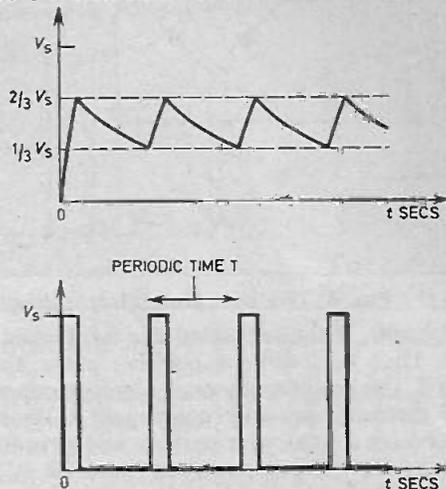


Fig. 3. (top) Charging and discharging of the timing capacitor as a function of time and (bottom) the corresponding output at pin 3.

### CIRCUIT DESCRIPTION

The complete circuit diagram of the Telephone Call Charge Calculator is shown in Fig. 4. It can be either mains or battery operated depending on the choice of the constructor. If battery operated, components T1, D1-D4, C1 and LP1 should be omitted. A suitable battery supply is three bell batteries type 126 wired in series.

The power supply consists of a readily available Friedland bell transformer and uses the 8V tappings. On full wave rectification by the diode bridge D1-D4 and smoothing by capacitor C1, a 15V d.c. supply is available.

The pulse generator has been described earlier (Fig. 2); the basic difference between the two circuits is the addition of the steering diodes D6 and D7. With these diodes, the charging time of the capacitor C2 is proportional to  $R_{10}$  and the discharge time proportional to the series combination of  $(R_1 + VR_1)$ ,  $(R_2 + VR_2)$  etc, depending on the position of S2.

This arrangement is necessary so that the charging time can be made rapid (in the order of 120 milliseconds) and the first pulse must be produced and operate the counter at the instant of switch on.

The electromagnetic counter is connected directly across pin 3 and ground, and D5 prevents the back e.m.f. produced when the counter

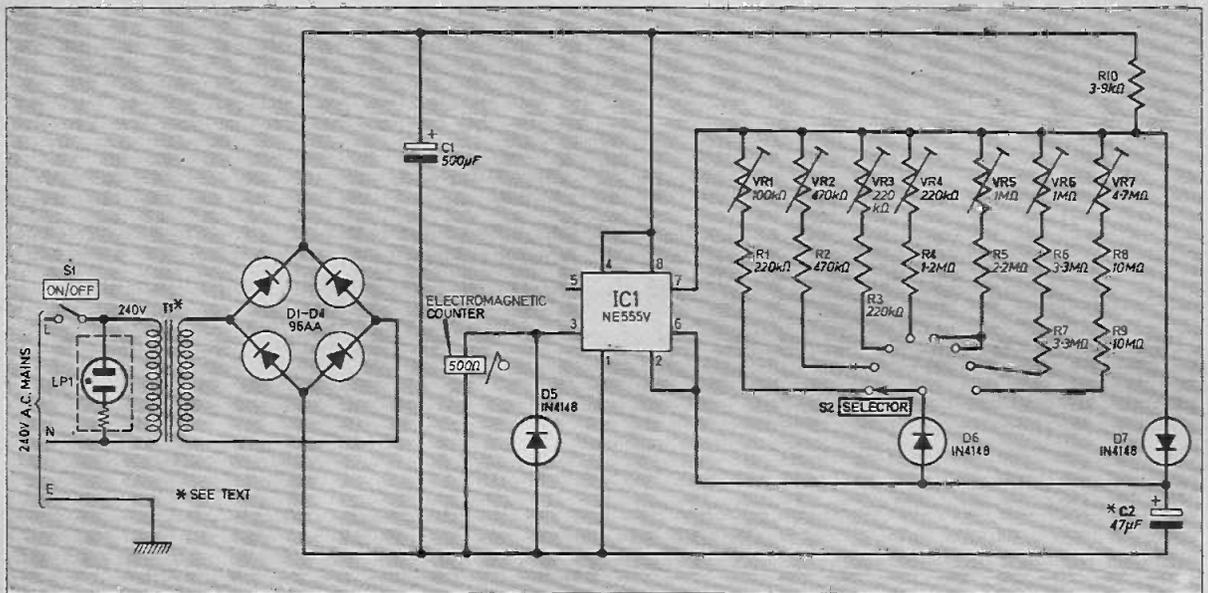


Fig. 4. The complete circuit diagram of the Telephone Call Charge Calculator.

switches off, from damaging the i.c. output transistor. Thus each time a positive pulse appears at pin 3, the counter advances by one count.

The discharge resistor (previously  $R_B$ ) has been replaced by a bank of resistors and presets, R1-R9 and VR1-VR7 respectively, and S2 is incorporated so that a fixed discharge time can be readily selected. The seven discharge paths are calculated so that the discharge times are in accordance with Table 1.

The charge ( $t_c$ ) and discharge ( $t_d$ ) times can be calculated from the following formulae:

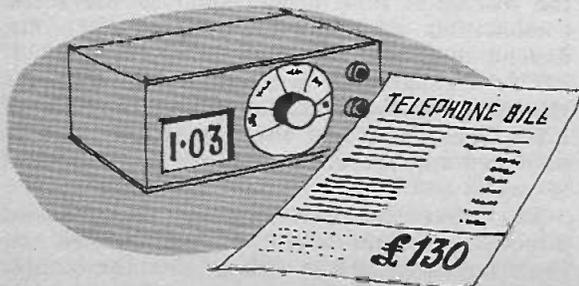
$$t_c = 0.7 \times R_{10} \times C_2 \text{ and this has been fixed at approx. } 0.1 \text{ sec.}$$

$$t_d = 0.7 \times R_x \times C_2 \text{ where } R_x \text{ can be } (R_1 + VR_1), (R_2 + VR_2) \text{ etc.}$$

### TIMING CAPACITOR

For accurate long time delays, capacitor C2 ideally needs to be a low leakage type with low tolerance such as 20 per cent or better. Values for the discharge resistors were calculated based on a 20 per cent capacitor. Normal electrolytic capacitors may be used but may need a higher value preset than that detailed, depending on the leakage factor.

The capacitor used in the prototype was obtained from a surplus computer panel and was a tantalum type.



A 25V working electrolytic chosen at random functioned satisfactorily.

### CONSTRUCTION DETAILS

The prototype unit was built in a commercially available p.v.c. covered metal case measuring 150×130×75mm which comes apart as two "U-sections". This case size should be considered as the minimum to comfortably accommodate all the components.

There are two component boards, one to take the timing circuit and power supply components (board A), and a second to carry the timing resistors and presets (board B). In this way, should the telephone charge rates be revised in the future, it will only be necessary to remove board B to update the device.

Begin construction by drilling the fixing holes in the boards and then making the breaks along the copper tracks as detailed in Figs. 5 and 6. Now assemble and solder the components in positions indicated paying attention to diode and capacitor polarities. Veropins are used on board B.

An 8 pin d.i.l. socket should be used for IC1 as this facilitates easy removal and replacement should this be necessary. Also, using a socket eliminates possible damage from the heat of the soldering iron. When complete, recheck for possible errors and insert the i.c. in its holder, paying attention to polarity indicated by a notch at one end. Do not attach the flying leads.

Next, with reference to Fig. 7 the case should be prepared to accept the counter, S2, S1 and LP1, all of which are mounted on the front face. The case should then be drilled to accept all the other component fixings, and a hole made in the rear face to suit a grommet through which the mains cable is passed.

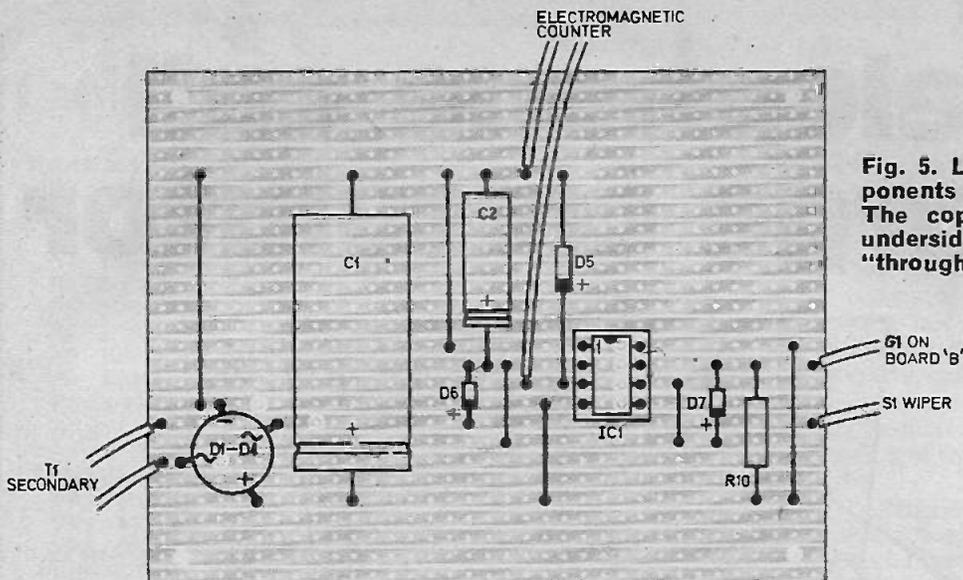


Fig. 5. Layout of the components on the main board. The copper strips on the underside are shown tinted "through" the board.

Two small aluminium brackets are required, one to hold board B in position and the other to secure the counter to the case.

With the exception of board B, secure all the components and board A in place as indicated in the photograph and wire up as shown in Fig. 7. Thoroughly check all the wiring and when fully satisfied, secure board A in place using 4BA nuts, bolts and spacers. A piece of stiff cardboard interposed between the case and each board will eliminate possible shorting against the case.

Three-core mains cable should be used and led out at the rear of the case via a rubber grommet. The mains lead should be fitted with a fused plug. A suitable earthing point is board B fixing bracket via a solder tag.

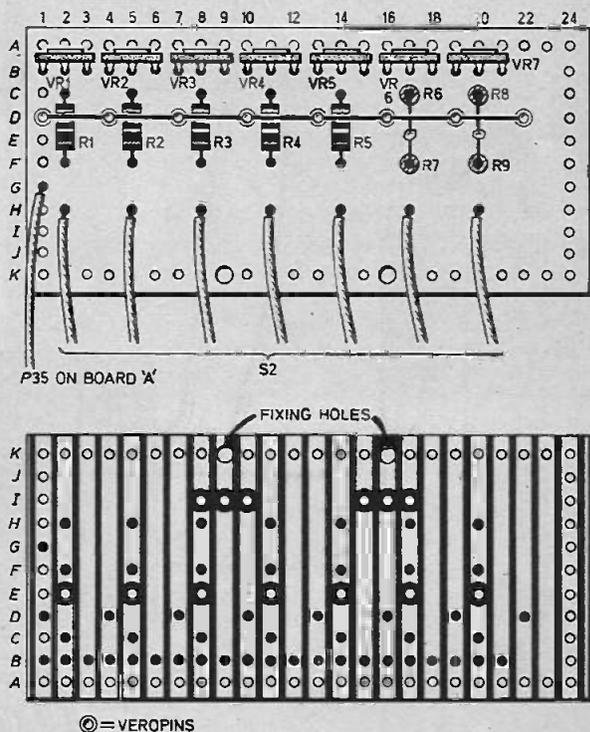
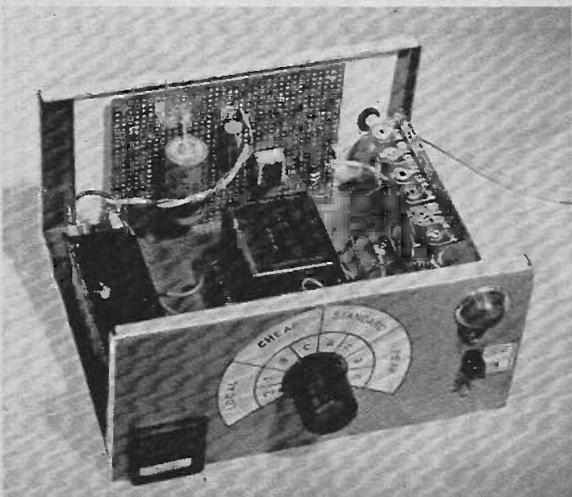


Fig. 6. Layout of the components on board B. Note the use of Veropins.

knob fitted. The pointer should be made to read "peak c" with S2 set so that (R1+VR1) are in circuit. Set all the potentiometers at their mid-way positions and plug into the mains.

Switch on at S1; the neon should illuminate and the counter should click and its readout advance by one. If this does not happen switch off immediately and check the circuit wiring etc.

Assuming all is well, switch off; obtain a timing device such as a stop watch or clock with



Photograph of the finished unit with lid removed.

## CALIBRATION

A dial should now be drawn up and glued around S2 as shown in photograph and a pointer

# Telephone call charge calculator

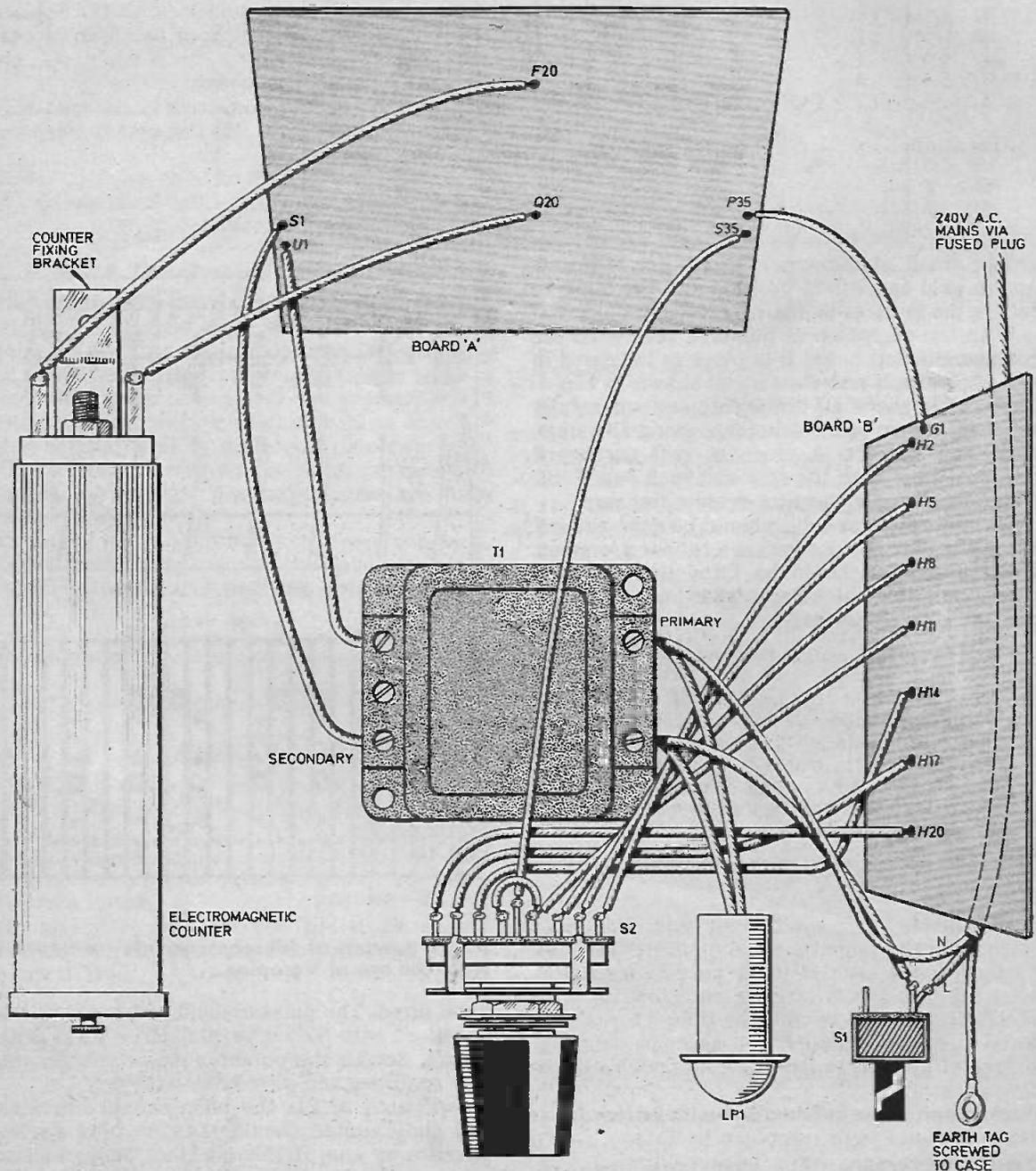


Fig. 7. The complete wiring up details of the unit.

## Components . . . .

### Resistors

- R1 220k $\Omega$
- R2 470k $\Omega$
- R3 220k $\Omega$
- R4 1.2M $\Omega$
- R5 2.2M $\Omega$
- R6 3.3M $\Omega$
- R7 3.3M $\Omega$
- R8 10M $\Omega$
- R9 10M $\Omega$
- R10 3.9k $\Omega$

All  $\frac{1}{4}$ W carbon  $\pm 5\%$  tolerance

### Potentiometers

- VR1 100k $\Omega$
- VR2 470k $\Omega$
- VR3 220k $\Omega$
- VR4 220k $\Omega$
- VR5 1M $\Omega$
- VR6 1M $\Omega$
- VR7 4.7M $\Omega$

All miniature carbon vertical skeleton types

### Capacitors

- C1 500 $\mu$ F 16V elect.
- C2 47 $\mu$ F 10V elect.—see text

### Semiconductors

- D1-D4 96AA  $\frac{1}{2}$ A 50 p.i.v. bridge rectifier or similar
- D5, 6, 7 1N4148 (3 off)
- IC1 NE555V timer i.c. 8-pin d.i.l.

### Miscellaneous

- S1 mains on/off slide or toggle
- S2 1-pole 8-way wafer
- LP1 mains neon with built-in resistor
- T1 Friedland mains bell transformer—see text

Electromagnetic counter type 14A or similar having a minimum coil resistance of 200 ohms that will operate at 15V; 8-pin d.i.l. socket; Veroboard: 0.1in. matrix 35 holes by 27 strips; 0.15in matrix 11 holes by 24 strips; Veropins; solder tag; length of three-core mains cable; 4BA fixings; knob; case.

SEE  
**SHOP  
TALK**

second hand, and switch both unit and stop watch on at the same time and measure the time it takes for the counter to advance by a further count after its initial turn on count. Preset VR1 should be adjusted so that the time interval between successive counts is 8 seconds. Turning the preset in a clockwise direction decreases the timing period.

All other settings should be adjusted in a similar manner with reference to Table 1.

When all ranges have been calibrated and checked, a dab of glue or nail varnish should be applied to each preset to prevent the latter being disturbed from their set positions.

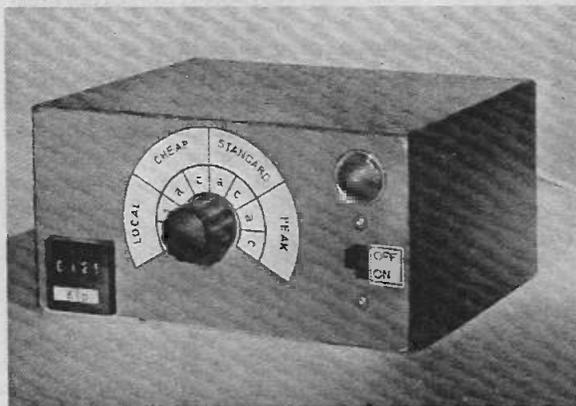
## USING THE UNIT

The unit should be situated within easy reach of the telephone when in use. When wishing to cost a call, the call code should first be determined from the Dialling Instructions booklet as an "a", "c" or local call; switch S2 is then set to this code according to rate for the time of day i.e. cheap, standard, peak, 1 or 2 (see Table 1).

The call should then be dialled and the unit switched on at the instant of "getting through"; the unit should be switched off as the receiver is replaced. The difference in the counter readings before and after the call is made, will give the cost of the call in pence.

Alternatively, the counter can be read regularly, say once a week and the weekly telephone bill determined.

In the Dialling Instructions booklet (issued pre-Oct 1973) there are some calls coded "b", these should now be changed to "c".



Photograph of completed unit.

## REVISION OF CHARGES

Since the charges at present are normalised to a 1p unit, the counter display can be read directly in pounds and pence. If in the future the basic unit changes from 1p the readout will give the number of units used.

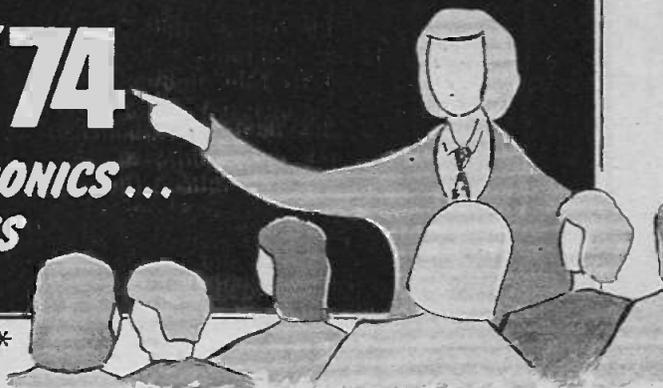
Also, if the rates are later revised, the timing resistors will need replacing, values being calculated using the formula given above.



# TEACH-IN '74

FOR BEGINNERS IN ELECTRONICS ...  
THEORY AND EXPERIMENTS

TUTOR: PHIL ALLCOCK\*



## LESSON 10 Transformer, Reed Relay, Loudspeaker and Unijunction

THE ratio of the numbers of turns on the coils is an important quantity since it can be used to measure the amount by which the input voltage or current is transformed (i.e. stepped up or down).

### RATIO

The Friedland transformer, which is used later in the Tutor Board experiments, is designed to be connected to the normal mains supply on the primary side and to supply 3, 5 or 8 volts from the secondary side.

The mains supply provides the current to magnetise the core and since the supply is a.c. the resulting magnetic flux is continuously varying. The varying flux links equally with the primary and secondary coils and each coil will have a voltage induced in it, just as in the case of the alternator coil.

Since the changing flux is common to all coils the rate of change of flux linkage will only depend on the number of turns on each coil. The situation is illustrated in Fig. 10.1 and if we assume that  $N_1=3000$  and  $N_2=100$  the primary flux linkage will be  $3000\Phi$  whereas the secondary flux linkage will be  $100\Phi$ . ( $\Phi$  represents the rate of change of magnetic flux.)

We know that voltage is proportional to the rate of change of flux linkage so we can write:—  
(primary current)  $\times$  (primary turns) =  
(secondary current)  $\times$  (secondary turns)

The first equation tells us that  $\Phi = \frac{240}{3000}$  and substituting this in the second equation we get—

$$\text{Secondary voltage} = \left(\frac{100}{3000}\right) 240 = 8 \text{ volts.}$$

The ratio 100:3000 is the "step down" turns ratio going from the primary coil to the secondary coil. Note that the coil with least turns also has the least voltage. The turns ratio thus determines the output voltage for a given mains supply voltage at the primary (input) coil. If this same transformer was connected to a mains supply of say 210 volts the output voltage would be reduced:

$$\text{Output voltage} = \left(\frac{100}{3000}\right) 210 = 7 \text{ volts.}$$

### TRANSFORMER ON LOAD

If a resistor or some other form of load is connected to the secondary a secondary current must flow due to the existing secondary voltage.

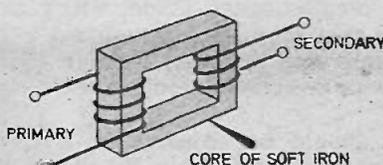
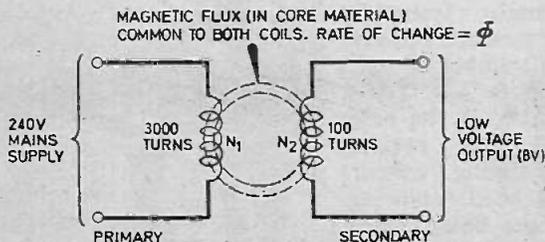


Fig. 10.1. Flux linkage in a simple transformer, and illustration of a simple transformer system.

\* North Staffordshire Polytechnic (Any communications arising from the Teach-In '74 series must be addressed to Everyday Electronics, Fleetway House, Farringdon Street, London E.C.4).

To keep the magnetisation of the core at its correct level, so that the primary induced voltage is equal to the mains supply voltage, extra current must be taken from the mains supply to compensate for the flow of secondary current.

Since the magnetic effect of each current depends on the product of the current magnitude and the number of turns through which it flows, the transformer flux "constancy" requires that:

$$(\text{primary current}) \times (\text{primary turns}) = (\text{secondary current}) \times (\text{secondary turns}).$$

Thus the current ratio also depends on the turns ratio but this time the least turns is associated with the greatest current. If our load is 100 ohms an 8 volt output would give a secondary

current of  $\left(\frac{8}{100}\right)A = 80\text{mA}$ . The corresponding

primary current would be  $\left(\frac{100}{3000}\right)80\text{mA} = 2\frac{2}{3}\text{mA}$ .

If these are the r.m.s. values, the power dissipation in the load will be 0.64 watts and a similar power is taken at the primary side since

$$240\text{V} \times \frac{8}{3}\text{mA} = 640\text{mW}.$$

Our transformer is 100 per cent efficient simply because we have not allowed for any of the losses that occur in practice due to coil resistances, core heating and magnetisation. For our purposes we can neglect these losses and use the following simple relationship for all our calculations:

$$\left(\frac{\text{primary turns}}{\text{secondary turns}}\right) = \left(\frac{\text{primary voltage}}{\text{secondary voltage}}\right) = \left(\frac{\text{secondary current}}{\text{primary current}}\right)$$

## REED RELAY

Another component that uses the magnetic effect of a current is the reed relay. The reed switch is usually encapsulated in a thin glass tube and consists of two (or sometimes three) blades made of magnetic material. The tips of the blades are usually gold plated to form a low resistance contact.

If the reed switch is exposed to a suitable magnetic field from a current-carrying coil or a permanent magnet the blades become magnetised and the contacts attract each other. If the magnetic field is sufficiently strong the contacts will close whilst the field is present. The reed switch with outer coil is known as a reed relay, and a wide variety of different types are now available.

Some switches have three blades to form a "change-over" contact. One of the characteristics of these switches is that the contacts can "bounce" when the relay is operated. This means that the contacts do not settle down to their

operated positions immediately but undergo a series of momentary closures before final closure. The effect is due to the bouncing of contacts and can depend on the strength of the magnetic field used.

In some systems this "bounce" cannot be tolerated and precautions must then be taken to minimise its effects. In the experiments this month a simple "make" contact switch is used to demonstrate the action of the reed relay using an easily wound relay coil.

## RELAY TRANSIENTS

If an inductor, reed relay coil or transformer winding carries a steady current (d.c.) the resulting magnetic field will be constant. When the current is switched off the magnetic flux must fall to zero and must therefore generate an induced voltage in the coil due to the changing flux linkage. Since the rate of change can be very high, large induced voltages can be produced which might cause damage to semiconductor devices if not protected.

A typical situation in which a reed relay coil is connected in the collector circuit of a transistor is shown in Fig. 10.2. If the transistor is saturated when on, the collector current will be limited by the resistance of the reed relay coil which in this case is one kilohm. When the transistor is switched off the collapsing magnetic flux, linked with the coil turns, produces an induced voltage that makes the collector end of the coil positive with respect to the other end.

By connecting a suitable diode D1 across the coil, as shown dotted, this voltage spike can be limited so that excessive voltage does not appear at the transistor collector. The diode provides a current path whilst the field collapses and the energy previously stored in the magnetic field is lost by power dissipation in the coil.

In some circuits, resistance is included in series with the diode to limit the current flow. The waveforms in Fig. 10.2 show the effect of the diode. Note that the induced voltage is established in a direction that tries to maintain the relay current in its original direction.

By using similar reasoning it can be seen that if we switch a current on and off and the current flow is via, say, a transformer winding, then a large voltage can be produced at a second winding if a suitable turns ratio is employed. This is of course the same principle as that used in the well established method of generating the high voltage pulses for the spark plugs of a car-engine.

## LOUDSPEAKER

One further component using magnetic effects is the moving coil loudspeaker. Just as the coil of a moving coil meter is made to turn by the interaction of a permanent magnet field and the field of the current-carrying coil, so the cone of

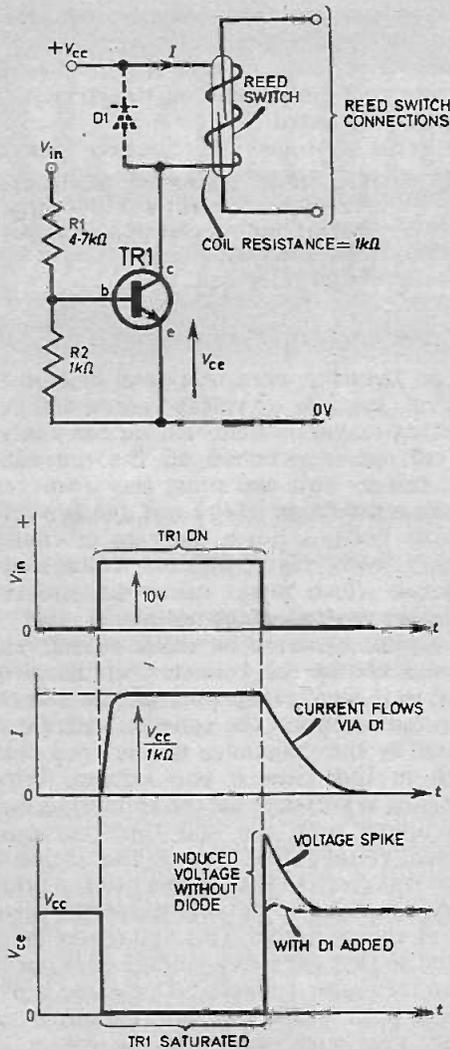
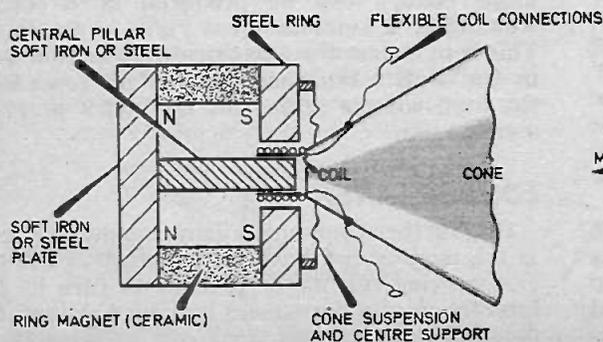


Fig. 10.2. Transistor operated reed relay with associated waveforms.

a loudspeaker is displaced by a similar interaction. In this case the moving coil is attached to the base of the cone and the cone movement generates variations in air pressure which we observe as sound, see Fig. 10.3.



It is apparent from what we have said so far that devices employing magnetic effects are very common in electrical and electronic engineering. Some of these devices are specialised and need not concern us now. However the main features of the electromagnetic effects have been illustrated and it is usually a straightforward matter to apply the basic ideas to other devices such as buzzers, horns and motors.

## OTHER SEMICONDUCTOR DEVICES

In addition to the diode and bipolar transistor, covered in earlier lessons, a wide variety of semiconductor devices exist and some of these will be used in the experimental circuits that have been planned for the remaining parts of the Teach-In series. The first of these devices is the so called unijunction transistor which was originally known as a double-base diode.

Like the bipolar transistor it has three connections but there the resemblance ends. The device we have selected is the TIS43 and we shall deal specifically with this type, but other types of similar ratings are available and may be tried if these are available.

## UNIUNCTION OPERATION

The unijunction behaves in some respects like a voltage-sensitive switch. The device connections are known as emitter (e), base No. 1 (b1) and base No. 2 (b2) and these are illustrated together with the circuit symbol in Fig. 10.4. Notice that the arrow head on the emitter symbol points towards the connection known as base No. 1 (b1).

As far as the b1, b2 connections are concerned the device behaves just like a resistor made of lightly doped n-type silicon material. The use of light doping means that the resistance of the device between the points b1 and b2 is relatively high, typically 10 kilohms, due to the restricted number of free electrons available.

The connections to the silicon at b1 and b2 are "non rectifying" i.e. they do not behave like a diode, but the emitter connection which is formed part way along the silicon material is in

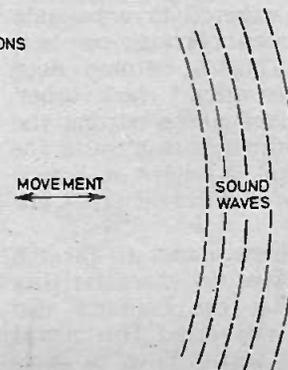


Fig. 10.3. Construction of a loudspeaker using the moving coil principle.

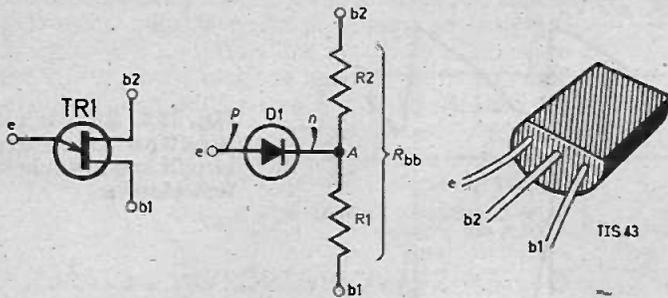


Fig. 10.4. Detail of the unijunction transistor, circuit symbol, equivalent circuit and mechanical details.

fact a normal *pn* junction and so the equivalent circuit for the unijunction is as shown in Fig. 10.4.

Point A represents the region at which the emitter junction is formed and R1, R2 represent the resistance of the material between this point and the base connections b1, b2. In use, a voltage  $V_{bb}$  is developed across the effective potential divider formed by R1 and R2 as shown in Fig. 10.5 and this makes point A positive with respect to b1. If the total resistance is  $R_{bb} = (R1 + R2)$  then we can define our first useful parameter as

$$\eta(\text{eta}) = \frac{R1}{R_{bb}} = \text{intrinsic stand-off ratio.}$$

This rather fancy title need not frighten anyone—it is simply the ratio of the resistance R1 to the total resistance  $R_{bb}$  and is particularly useful since the voltage at A is given by  $\eta V_{bb}$ . Since the voltage level at A is important to the subsequent mode of operation it is useful to realise that  $\eta$  must always be less than unity and is typically about 0.6 for the TIS43 transistor.

Thus if  $V_{bb}$  was set to +10 volts the voltage at point A would be +6 volts (measured with respect to the b1 terminal). Let us now consider the test circuit of Fig. 10.5 in which the emitter is connected to a variable voltage supply via a current limiting resistor  $R_e$ .

If we had suitable instruments available we could measure the current  $I_e$  and the voltage  $V_{eb1}$  for various settings of the variable voltage supply  $V_{ee}$ . With  $V_{bb}$  connected and  $V_{ee}$  set at zero a small leakage current would flow via the diode because of the positive voltage at point A. As we increase  $V_{ee}$  this leakage current would reduce until at point Z, on the characteristic shown in Fig. 10.5, the current would be zero.

For this zero current condition the emitter-base voltage  $V_{eb1}$  must be equal to the voltage at point A so that the voltage across the diode

is zero. Thus the voltage at point Z is

$$V_{eb1} = \eta V_{bb} = \text{voltage across R1,}$$

and  $I_e = 0$ . If we increase  $V_{ee}$  further the voltage  $V_{eb1}$  will continue to rise until the diode starts to conduct. This is a critical point on the characteristic (X) and is known as the **peak point**.

As the diode starts to conduct the number of current carriers in the R1 section of the device increases and this has the effect of increasing the conductivity of the silicon in this region. The resistance R1 thus tends to fall and this causes a further increase in diode current.

The resulting characteristic is shown by the curve between X and point Y, and this latter point is usually known as the **valley point**. Once the peak point is reached the transition from X to Y is very rapid and does not require any change in  $V_{ee}$ . The increased emitter current is limited by the external emitter resistor  $R_e$  and if the transistor reaches the region to the right of the valley point the circuit will remain in this new condition until the  $V_{ee}$  supply is disconnected or reduced to a much lower value.

If  $R_e$  is made sufficiently large the current  $I_e$  will not reach the valley current and the circuit can then be made to oscillate by adding a single capacitor to the emitter circuit.

## OSCILLATOR

The complete oscillator is shown in Fig. 10.6 where it can be seen that the same battery is used for the two supply voltages i.e.  $V_{bb} = V_{ee}$ . The resistance in the emitter is made variable, by VR3, and has a minimum value determined by R1. A second variable resistor VR1 is used as a potentiometer in the b1 lead to derive an output voltage waveform.

The capacitor C1 charges via the resistances and VR3 and the capacitor voltage ( $V_c$ ) rises exponentially as described in earlier lesson material. When the critical peak voltage ( $V_p$ ) is

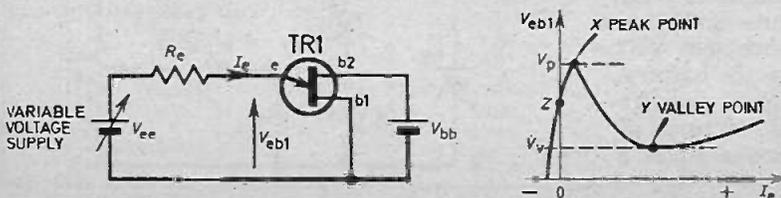


Fig. 10.5. Unijunction operating characteristics.

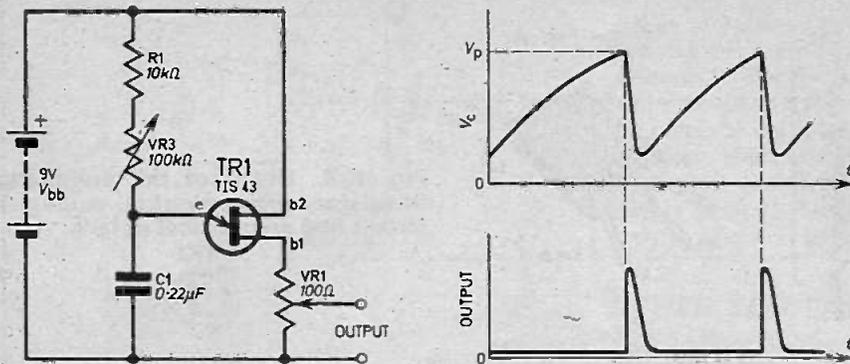


Fig. 10.6. Simple uni-junction oscillator circuit and associated waveforms.

reached the transistor switching action is initiated and  $V_c$  falls rapidly. If the total emitter resistance is large enough the final emitter current will be limited to less than the valley point current and the capacitor will start to recharge again.

Every time the capacitor discharge occurs a pulse of current flows via VR1 and this produces a series of voltage pulses at the output. Since the charging of C1 depends on the time constant C1 (R1+VR3) the frequency of the pulses can be controlled by VR3. The waveforms shown in Fig. 10.6 illustrate the circuit behaviour. Note that the voltage  $V_p$  is given by

$$V_p \approx 0.5 + \eta V_{bb}$$

where the forward voltage of the emitter diode has been taken as 0.5 volts. Since  $V_p$  depends on both  $\eta$  and  $V_{bb}$  the frequency will also depend on these two quantities.

Next month we shall investigate some of the features of field effect transistors.

## TUTOR BOARD EXPERIMENTS

### Test No. 20

Remove the cotton from the plastic spool (as listed in the May 1974 issue) by winding it onto a piece of cardboard so that it is not wasted. Carefully wind the enamelled wire onto the spool until it is full. The start end can be fixed with sticky tape, to stop it slipping, and it will help if someone can support the bobbin of wire on a knitting needle whilst the coil winding is in progress. Fasten the end of the wire with tape to complete your relay coil.

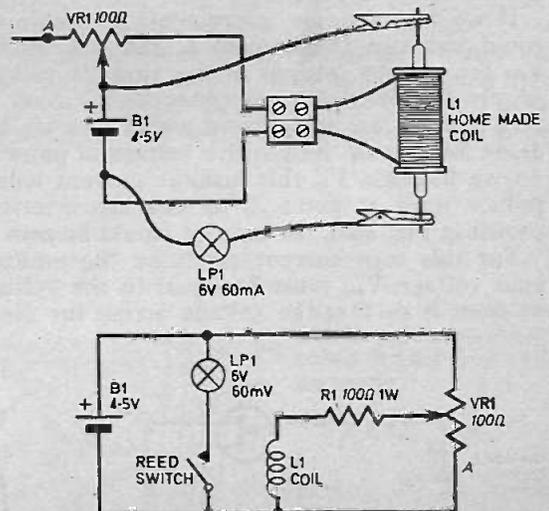
Use the circuit of Fig. 10.7 to check that your reed switch operates. The potentiometer VR1 can be used to vary the coil current—note that your coil will have a low resistance and VR1 helps to limit the current taken from the battery. The prototype coil used a plastic spool approximately 1½ inches long and a coil of 400 turns of 30 s.w.g. wire. The coil resistance was about 3 ohms.

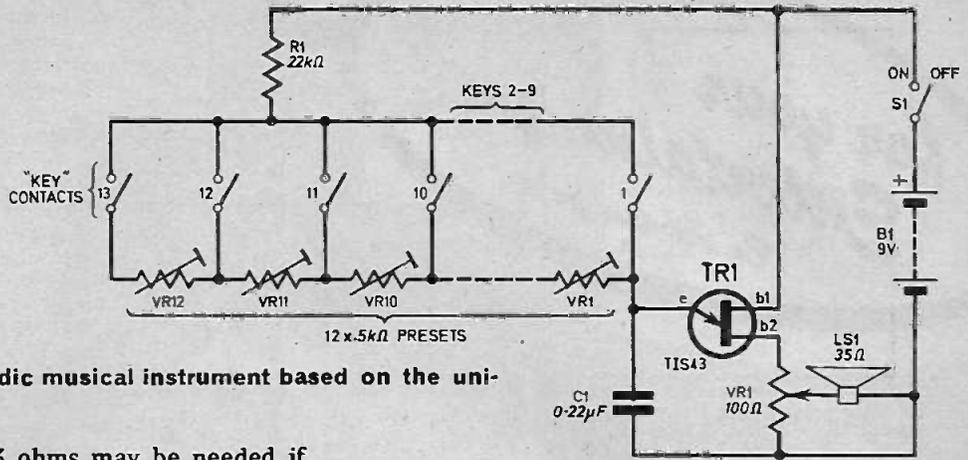
The 6-RSR-A reed switch requires 20 to 40 ampere-turns to give reliable operation and with 400 turns this means a current of 50 to 100mA. By noting the position of the potentiometer VR1 at which the relay operates it may be possible to estimate the operating current for your coil. Once operated the current must be reduced to about half the operating value to ensure that the relay contact opens again.

If the range of adjustment is insufficient using the 100 ohm potentiometer an additional resistor of 100 ohms, 1W, can be used to reduce the coil current using the circuit modification shown in Fig. 10.7. With this arrangement the maximum current is limited to about 45mA but the current can be reduced to zero.

If a larger number of turns is used the operating and release currents will be correspondingly reduced. A coil of at least 400 turns is recommended. An accurate measurement of operating and release current can be made by measuring the voltage drop across the 100 ohm fixed resistor but because of the limited maximum current not all coils can be tested this way.

Fig. 10.7. Reed relay test circuit and modification.





**Fig. 10.9. Simple melodic musical instrument based on the unijunction oscillator.**

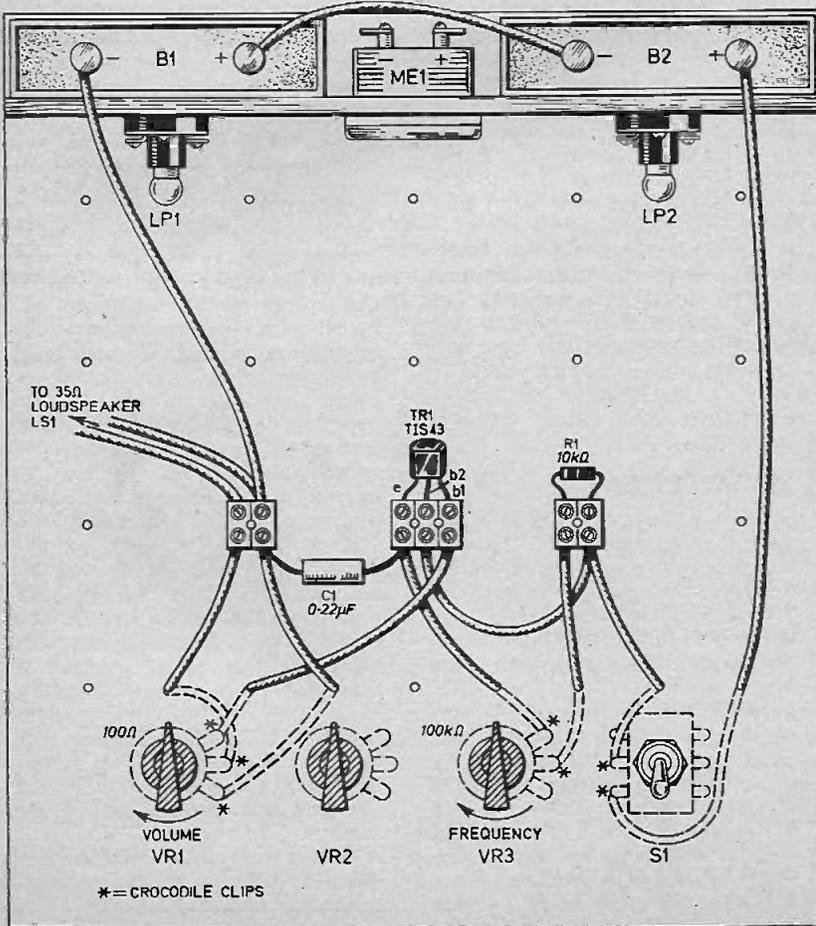
A resistor of say 33 ohms may be needed if the reed switch requires 40 ampere-turns to operate and a coil of 400 turns is used. (Note: A resistor of 33 ohms is not available in the existing component collection. Three 100 ohm resistors can be connected in parallel as an alternative if these are available, or a higher voltage (9V) could be used. Do not try to operate the lamp circuit from the full 9 volts as this will probably ruin the lamp! If your relay coil does not work, try winding a coil with more turns. Remember, patience is a virtue!)

**Test No. 21**

Build the unijunction oscillator (Fig. 10.6) on the Tutor Board using the layout shown in Fig. 10.8. Connect the loudspeaker (35 ohms) to the output terminals and listen to the sound produced as VR3 is varied. Adjust the 100 ohm potentiometer (VR1) to give a suitable volume level from the loudspeaker. Note that the lowest frequency occurs when VR3 is set to its maximum value of 100 kilohms. If you have a piano or other musical instrument in the home try to estimate the frequency range covered as VR3 is varied.

It is possible to build a simple musical instrument using this oscillator. All that is required is to switch in different resistors by means of "contacts" as shown in Fig. 10.9. The mechanical arrangement for such an instrument is left to the ingenuity of the reader. The overall "pitch range" can be changed by using a different value for capacitor C1. Doubling C1 halves the frequency of all notes.

The output at the 100 ohm potentiometer can be fed to an amplifier, if required, via a 0.22μF series capacitor.



**Fig. 10.8 Layout and wiring of Fig. 10.6 on the Tutor Board.**

# For your Entertainment...

By Adrian Hope

ONLY a few years ago the only electronics used for entertainment in most homes was a radio set, a simple black and white TV set running on an indoor aerial, and a mono record player. Now many people are almost literally ankle deep in exotic electronic gear. And daily they are subjected to the temptation of buying yet more.

Matching one piece of new equipment with another so that both work properly is no mean feat and I'll bet that all over the country, or the world for that matter, there are expensive electronic arrangements producing such had results that the owner would have been far better off with what he had before.

Some times the fault is with the equipment, some times with the setting up and some times local conditions are responsible for poor results. Whatever the cause the effect is little or no entertainment for anyone. The idea of this column is to offer a few practical suggestions on buying and using equipment which really is primarily *For Your Entertainment*.

## CONTINENTAL ENTERTAINMENT

Cheap holidays in Spain and the Balearic Islands beckon all the year round. So a few thoughts on the electrical facts in Spanish life should not come amiss. Also many people, myself included, like the idea of a little music or world news being available on tap in the privacy of our hotel room.

Palma, Majorca has a local f.m. studio which broadcasts in the English language every evening and into the night on 96.6MHz. The programming is mostly good popular music, for instance in the Sinatra bracket, and reception is fine in the coastal area around

Palma. But because the station is low strength (1 kilowatt transmitter power) and the island very mountainous, you will be hard pressed to receive it in any other part of Majorca.

This radio station is, incidentally commercial and one of the few in the world that you can visit any time you like. This is because the "studio" is a Palma bar called "My Own Place" run by American expatriate Riki Lazaar. Buy the local English language newspaper (The Majorca Bulletin) for further information.

Elsewhere in Spain there is little, if any, English language f.m. radio so you will need to rely on the medium and long wave bands for your listening. And this is where the plot starts to thicken. Although Radio Algeria should come in loud and clear on the long wave band with some light music every night, it is in many concrete hotels likely to be a weak signal and drowned out by local interference. The prime source of this interference is hard to tie down but may well be thyristor-controlled circuitry for dimming lights or controlling heaters or drive motors for lifts and airfans.

## INTERFERENCE

The interference problem is bad enough in England, but in Spain it is even worse and reception of m.w. and l.w. may be impossible. This is probably because even new modern hotels being built there are electrically wired with little or no earthing. This is not only potentially dangerous, but it also means that any interference which is created for instance by a motor, a thermostat or a thyristor control will have the best possible chance of pervading the hotel wiring system, which then acts as one glorious aerial.

I have stripped down several

hotel wall sockets and switches in Spain and never yet found any earthing, even in stone-floored bathrooms where unshielded two-pin sockets are provided with astonishing lack of common safety sense. Shocks received from lift switch panels also suggest that their high-power drive motors may be unearthed. And even the toilets in some new Spanish hotels are flushed by heavy duty electric solenoids. Small wonder that a.m. radio reception is so poor!

Of course f.m. radio is largely immune to interference of this type, but as we have already seen, there is relatively little f.m. to be received. So anyone going on holiday to Spain and wanting to be sure of some music in their hotel room, will need to take not only an f.m./a.m. radio, but also a cassette player with some pre-recorded cassettes. That way if there is no local f.m. station and local interference blots out everything on the a.m. bands, taped music can come to the rescue.

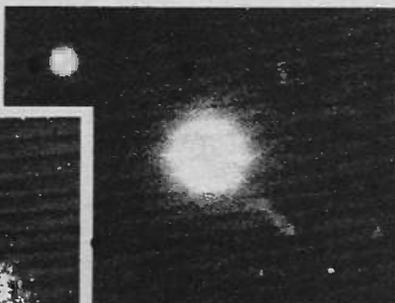
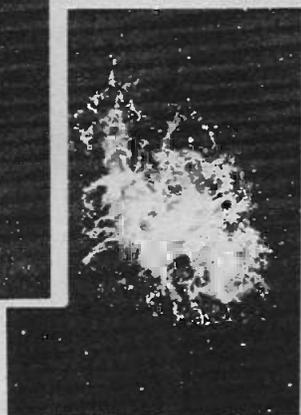
## VOLTAGE

Incidentally, the mains supply voltage in Spain is now a nominal 220 volts a.c., with the plug sockets of standard continental two-pin type. The pins of the plugs to fit these sockets are smaller than those on British two-pin plugs and are spaced apart by 2cm.

Although adapters to convert British plugs to continental size are cheap in most Spanish shops, the hotels often charge an exorbitant price so it may be worth buying one in England. And don't be too bothered if you run equipment such as a shaver, hair dryer or radio off the mains and find its performance erratic.

Although mains voltage is nominally 220 volts it fluctuates like mad, often down to around 190 volts. In this country a 6 per cent change only is allowed by law i.e. 15 volts either way. All over Spain there is a roaring trade in voltage stabilisers for use with television sets. So if you see a television in a bar and it has a mysterious white boxed gadget standing on top, the chances are that it's a stabiliser. This keeps the voltage to the set steady and prevents the picture size from shrinking.

In fact a few days with Spanish electric makes the British system a joy to live with.



*The Andromeda Galaxy  
The Crab Nebula  
The Quasar 3c 273*

*(United States Information Service)*

# RADIO ASTRONOMY AT JODRELL BANK

BY S. McCLELLAND

**E**VERY second of the day and night, many types of electromagnetic radiation impinge on the earth from outer space. Although we can see some of this—the starlight—most is invisible and it was totally unknown until the advent of radio astronomy.

This fascinating science probes every secret of our amazing universe through this newly-discovered "window". To do this, it uses highly-complex instruments such as the radio telescopes at Jodrell Bank, Cheshire where Manchester University's Nuffield Radio Astronomy Laboratories are based. This article will briefly look at these telescopes and the purpose for which they were built.

## A NEW WINDOW ON THE SKY

The science of radio astronomy is young even compared to the relatively brief life of radio communication. Indeed, it was not until 1931 that Karl G. Jansky, an American engineer working on the problems of radio interference, discovered a background static in his equipment and deduced from its nature that it must originate in space. Although he published the results of his important work little notice was taken of it.

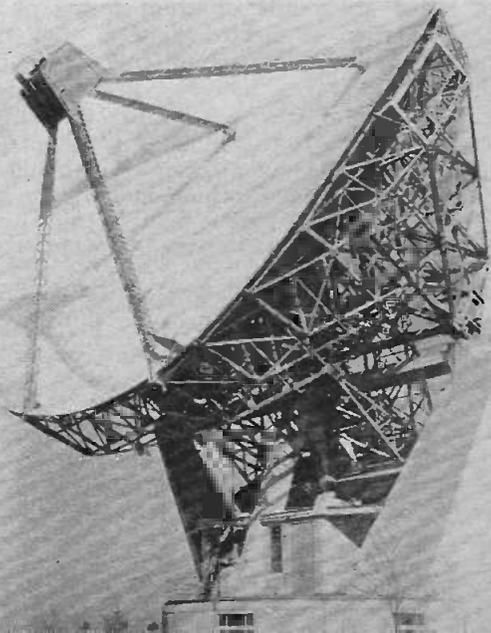
In fact, only an American radio amateur named Grote Reber followed up Jansky's discoveries by building a small parabolic dish aerial in his garden. He used it to discover that areas of our galaxy were strong radio sources. However it became apparent that, contrary to expectations, only our sun, among all the normal stars in the sky, had a definite radio output

associated with it. This is because of its proximity.

The second world war provided an impetus to radio astronomy and the subject was re-examined. Among the post-war researchers in England was a physics lecturer at Manchester University named Bernard Lovell.

Interested in the detection of the cosmic rays and meteors which continually bombard our planet, he was allowed to set up his equipment on a site free from man-made electrical interference at the botanical department of the University—a place called Jodrell Bank.

Jodrell Bank mark II radio telescope. (Jodrell Bank)



## THE GROWTH OF JODRELL BANK

The work of Bernard Lovell with fairly elementary equipment was so successful that he was allowed to build larger and more efficient radio telescopes. Eventually he realised that to make further progress a giant, fully-steerable radio telescope with a parabolic dish 250 feet in diameter, was required.

The magnificent design of, and supervision work on, the telescope was carried out by H. C. Husband and Co., of Sheffield.

Construction of the telescope commenced in 1952, and it was finished in the International Geophysical Year of 1957. About half of the £700,000 cost was borne by the Department of Scientific and Industrial Research (now the Science Research Council), the bulk of the remainder being very generously met by Lord Nuffield and the Nuffield Foundation.

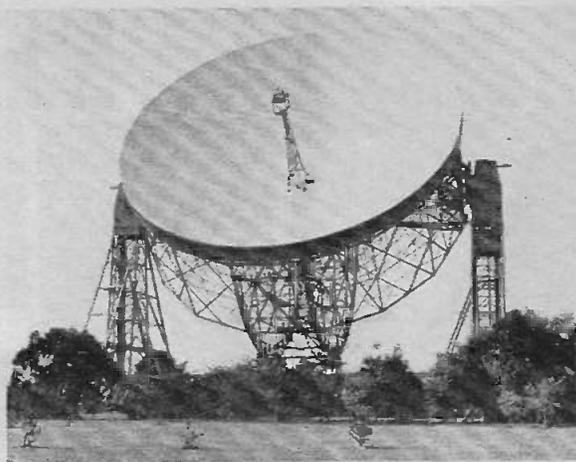
Any existing doubts about the value of the telescope were disposed of in an immediate and spectacular way, when the instrument showed its great versatility by being the first Western device to detect and track the carrier rocket of the first space satellite—the Russian Sputnik I. Great successes, also in the field of tracking, continued to be achieved at Jodrell Bank, notably with the American Pioneer space probes, and the first man-made object to hit the moon—the Russian Lunik II.

Today, Jodrell Bank has become world famous through these events, but it still remains primarily a radio astronomical station with a very small percentage of its research time being devoted to tracking. In the past decade, it has been greatly involved with the discoveries of the so-called “new” astronomy—especially the fantastic quasars and pulsars.

## THE RADIO TELESCOPE

The light and radio waves which originate from space are really different forms of the same radiation — electromagnetic radiation. Some methods of receiving them are thus similar. Radio waves, however, are very much longer than light waves—typically ten million times, and those from about one centimetre to many metres in wavelength can easily penetrate the earth's atmosphere which hinders the passage of light waves. This means that radio astronomical observations can be made through cloud and mist, etc.

However, because of the dissimilarity in wavelengths, radio telescopes have to be much larger in order to achieve the resolving power—or distinguishing power—of a comparable optical telescope. Hence the collecting area, the parabolic dish, of the big telescope (called the mark IA) at Jodrell Bank is 250 ft. in diameter. This steel bowl weighs over 1,000 tons, and the giant mass of steel which supports it weighs roughly twice as much.



This photograph gives some idea of the size of the Jodrell Bank Mark IA telescope. (Jodrell Bank)

Modifications recently carried out on the telescope have resulted in a lower working wavelength, namely 11 centimetres. The instrument has a large working range and is thus very versatile in operation. Indeed, it is this versatility which has contributed to the great success of the telescope. It is also fully steerable, still one of the largest of this kind in the world, and it can be pointed to any area of the sky.

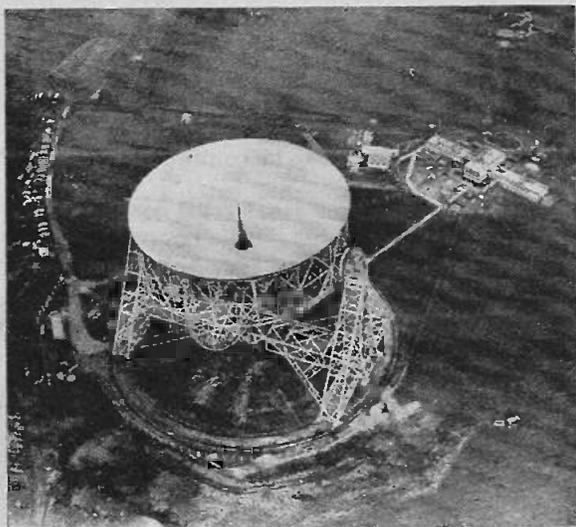
This is achieved by using computer-controlled electric motors to drive the complete telescope in azimuth (i.e. to the various points of the compass) and the bowl alone in elevation (i.e. tilt) through two huge racks that were salvaged from the gunnery equipment of the *Royal Sovereign* battleship. These are housed at the top of the two bowl support towers, 180 feet above the ground.

Radio waves which are collected by the bowl are focused on to the aerial at the dish's centre. Here, a very sensitive receiver amplifies the weak signals and they are passed to the control building and converted to binary form for analysis by a computer. This can print out its results on punched tape for further reference or make pen-recordings of signal intensity in the area of sky studied.

This is the nearest the radio astronomer can get to having a “picture” of the source, but his observations are usually combined with those made by an optical telescope in the same area to build up a complete knowledge about it.

## OTHER TELESCOPES

Besides the mark IA, Jodrell Bank also has a mark II instrument. This is a smaller and more recent instrument with an unusual dish shape (see photograph) and it is used for lower wavelength work.



**Aerial view of the Jodrell Bank telescope.**

A similar telescope, the mark III, has a mesh dish and is stationed near Nantwich.

These instruments, besides being independent, can be used together, the output from each telescope being combined in a special way to effectively produce a very large radio telescope. The complete arrangement is known as an interferometer. Interferometers have been constructed between a Jodrell Bank telescope and instruments at places as far ranging as Malvern in Worcester, to Onsala, Sweden and Arecibo, Puerto Rico.

The remaining instruments at Jodrell Bank include a 50 foot telescope for lunar radar and miscellaneous work and another 50 foot "az-el" telescope for tracking space probes.

### **THE NEW TELESCOPE**

In December 1972, it was announced that the University of Manchester is to build another radio telescope on a site near Welshpool, in Wales. The diameter of its dish will be 375 feet, making it the largest of its type in the world. It also means that the telescope's resolving power will be considerably greater than that of the present mark IA.

### **THE RADIO SKY**

There are several varieties of radio sources in the sky, and Jodrell Bank has been concerned with almost every type, ranging from the radio "noise" areas of the sun and the planet Jupiter to the incredibly distant objects in the farthest reaches of the universe.

A great feat of radio astronomy has been the mapping of our galaxy. This is because the internal structure of the atoms of hydrogen gas of which the galaxy is largely composed can undergo a slight energy change. This change

gives rise to a radio signal on a unique wavelength of 21cm, which can be detected by radio telescopes such as those at Jodrell Bank, so the distribution of hydrogen in our galaxy can be mapped. Also, the fact that the hydrogen line, as it is called, is sometimes slightly shifted in frequency due to the Doppler effect, means that the hydrogen gas and, therefore the galaxy, is in motion.

Such investigations have helped to build up a picture of our galaxy as being a gigantic, slowly rotating disc with spiral arms. It is indeed huge—about 100,000 light years across (a light year is the distance light travels in one year: it is about six million million miles)—and probably contains in the region of 100,000,000,000 stars.

Our sun, one of that number, is insignificantly placed away from the centre. The whole galaxy is probably quite similar to the Andromeda galaxy—also a nearby radio source, but still over two million light years away.

Other very interesting and mysterious radio sources exist in the sky which emit radio signals by different methods. These include the radio galaxies and the intriguing quasars and pulsars.

Quasi-stellar objects or quasars for short are certain, very small, star-like objects which emit incredible amounts of radio and optical energy. Evidence from the latter tends to suggest that they are enormously distant, but until the true distance is actually ascertained, quasars will continue to be a central problem in astronomy. The radio telescope at Jodrell Bank has played an important part in the discovery of the quasars.

Another of the amazing phenomena that have been discovered by the science of radio astronomy in the past ten years are the pulsating radio sources or pulsars. As their name suggests they emit bursts of radio and sometimes, light-energy. Perhaps the most famous example of a pulsar is that in the Crab Nebula.

This is a glowing cloud of gas which is thought to contain an incredibly dense neutron star. The latter could give rise to the radio pulses as a consequence of its spin. Although its origination is unclear, astrophysicists believe that the Nebula and the neutron star are remnants of a star which just blew itself up in a gigantic explosion or supernova which was observed by Chinese astronomers in 1004 A.D.

In this field, too, Jodrell Bank has made a very significant contribution by discovering many new pulsars.

### **RADIO ASTRONOMY AND OUR UNIVERSE**

The aim of radio astronomy is to discover by its singular techniques more about the universe—its formation, evolution and end, if any, and its true nature. These are some of the most

important questions of all. A great advantage with observational astronomy in general is that not only vast gulfs of space but also of time, can be surpassed.

This is because even light and radio waves, the messengers of the events which we observe in the sky, can take an enormous time to cross the distances involved. Thus, the farther we can probe into space, the farther we also probe back in time, perhaps even towards the possible creation of the universe. This is why the nature of distant galaxies and quasars is of great importance to the astronomer.

Radio astronomy is helping scientists to decide between the various theories of the creation of the universe. These include the widely held

“big bang theory” that suggests that at one time in the distant past all the matter in the universe was concentrated at one point before being scattered by a colossal explosion. Another theory, that of the “steady state” considers the matter in the universe to be continuously created as the universe expands.

In radio astronomy’s brief life of 40 years almost paralleled by the development of Jodrell Bank, many questions have been answered, but many more have been unearthed. However, in the future, as in the past, we can be sure that Jodrell Bank will number among those prominent establishments providing the knowledge so necessary to mankind’s understanding of the universe. □



### Loudspeaker Connection

Could you tell me how to connect two 60 watt loudspeakers together to give a total power rating that will handle 100 watts.

This is simply done by putting the two loudspeakers either in series or parallel but remember that you must match the output impedance of your amplifier. If your loudspeakers are twice the impedance of your amplifier then connect them in parallel; if they are each half its impedance put them in series. If each of your loudspeakers has the same impedance as your amplifier then you cannot use this simple technique because it is impossible to produce a good match without the use of a transformer.

Remember to keep the phasing correct; when connecting the speakers in parallel connect like terminals together. For series connection, unlike terminals should be linked.

### Preferred Values

Some of your advertisers show resistors categorised as E12 and E24 series. I would be pleased if you could explain what this means.

As you must be aware, resistors are supplied with preferred values. There are 12 different values within a decade of  $\pm 10$  per cent tolerance resistors. These

are 1.0, 1.2, 1.5, 1.8, 2.2, 2.7, 3.3, 3.9, 4.7, 5.6, 6.8, 8.2 and multiples of ten on these values. The values have been carefully selected so that the upper 10 per cent tolerance of the lower value approximately equals the lower 10 per cent tolerance of the next higher value—this is how the rather strange selection of values comes about. This is called the E12 series of values.

There is a similar series for  $\pm 5$  per cent tolerance devices—called E24—and there are twenty-four different values within a decade as follows: 1.0, 1.1, 1.2, 1.3, 1.5, 1.6, 1.8, 2.0, 2.2, 2.4, 2.7, 3.0, 3.3, 3.6, 3.9, 4.3, 4.7, 5.1, 5.6, 6.2, 6.8, 7.5, 8.2, 9.1. Note that the same tolerance law applies except that now it is  $\pm 5$  per cent.

### Circuit Supply

Please would you tell me how it is possible to vary the current of a circuit whilst keeping the supply voltage constant?

For a fixed supply voltage circuit current is set by the total circuit resistance. In the simplest case this would comprise a set of resistors in series. The only way of altering the current is to alter the value of one or more of the resistors. In a more complicated case the current in question might be the collector or emitter current of a transistor and in this instance the circuit current can be controlled via the transistor’s base current.

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# SEMICONDUCTOR PRIMER

By A. P. STEPHENSON

## 16 ■ TESTING TRANSISTORS

The instruments available for testing transistors, and how an AVO can be used both for testing and sorting out *pnp* from *npn* types.

Various transistor-test sets are manufactured, some quite simple, others bristling with knobs, dials and switches and capable of measurements on almost any transistor.

For transistor manufacturers they are no doubt very useful for testing  $h_{fe}$ ,  $h_{oc}$ ,  $h_{rc}$ ,  $h_{ie}$ , noise,  $f_T$  etc. For the small workshop, the capital investment in one of these spectacular instruments is seldom justified.

By the time the voluminous instruction manuals are studied, the various knobs twiddled, the dial readings laboriously checked, the poor technician is mentally exhausted and too weak to insert the transistor.

In most cases, it is only required to find out if a suspect transistor is working at all, or definitely unserviceable. An AVO meter (on resistance range) is quite adequate. Three tests are required.

(a) Resistance between base and emitter

should be *LOW* with leads one way round but *HIGH* the other way. The difference should be at least 10:1.

(b) As (a) above but between base and collector.

(c) A test across emitter and collector should be *HIGH* either way round. The actual reading in ohms will vary widely between serviceable transistors even of the same type and there is little point in attempting figures—it is only the *ratio* which is important. (Note: it is unwise to use the very high ohms range in case the highest battery voltage causes damage).

Unknown transistors can be sorted into *pnp* or *npn* by this method.

Put RED lead of AVO to base and BLACK lead to emitter. If reading is low ohms, the transistor is *pnp*. (This appears to contradict normal *pn* junction theory until it is remembered that an AVO on ohms range is delivering a small *negative* voltage from its RED lead and a *positive* voltage from its BLACK lead).

## 17 ■ VARIOUS BIASING METHODS

The simple diagrams of Fig. 17.1 (a-e) illustrate the various methods of setting the d.c. bias conditions in a class A amplifier operating in the common-emitter mode.

- Simple, economical on current, but gain sensitive to  $h_{FE}$  production spreads, temperature and supply voltage, seldom used.
- The inclusion of the emitter resistor  $R_E$  helps to reduce the sensitivity of the stage to temperature, supply voltage and  $h_{FE}$  spreads. Also, the input impedance is higher due to the series negative feedback across  $R_E$ . Unfortunately, the gain is lowered as well as the output swing.
- Instead of an emitter resistor a direct voltage negative feedback action is provided by  $R_F$ . Has a similar effect on reducing sensitivity as well as the gain. Also the amount of feedback is fixed by the bias required on base. Output swing not affected.
- Has all the advantages of (b) but the potential divider  $R_1, R_2$  provides a much steadier base bias. Unfortunately the extra resistor  $R_2$  provides an additional load across the signal. However, this circuit is the most widely used in general amplifier design.
- Similar to (d) but the emitter as well as the base, is fed by a potential divider. The extra stability of this circuit must be paid for in extra current drain through  $R_3, R_4$ .

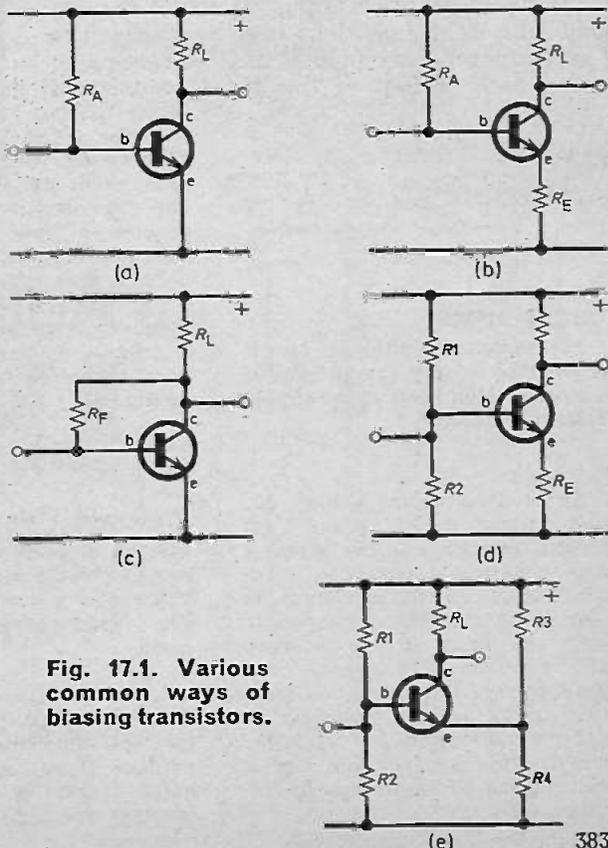


Fig. 17.1. Various common ways of biasing transistors.

**T**HANKS to the selection of semiconductors, such as relatively cheap triacs and high-tension transistors which are at present on the market, it is possible to design a simple device to automatically control light level in household or similar uses.

With regard to the fact that there are a large number of non-fluorescent light sources in use, this light controlled device was designed to control a luminous intensity over a very wide range and at the same time automatically hold a pre-set light level.

### DESIGN CONSIDERATIONS

As the only practical solution, without visible flickering effect, a phase shift system was chosen although this system is known to have some disadvantages, such as the necessity for interference suppression circuitry and the deformation of the supply waveform. These disadvantages are caused by the fast triac switching.

The circuit described is not expected to be connected to the mains in large quantities where consumption exceeds 200 watts. Due to the large number of light dimmer units using the same principle and working satisfactorily it was not necessary to develop a new control principle.

Light dimmers at present on the market are characterized by manual adjustment of required light level only. These dimmers are without any automatic readjustment of luminous intensity of the light source according to actual requirement (the light conditions may be changed in a very short period such as in the evening or during dark periods of the day in connection

with weather changes). In such cases normal circuits require readjustment of light level or the user must be satisfied with an unsuitable light level.

In some cases it would be desirable to switch some of the lights in the house on whilst the house is unoccupied. To fulfil this condition the light must be switched on when leaving the house. In the case of the controller to be described a constant level of light will be automatically kept.

### ADJUSTMENT

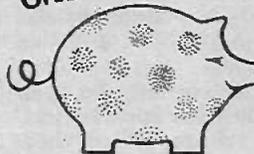
In manually controlled dimmers the adjustment of a very low light level becomes critical and from a certain point practically impossible due to instability of the mains voltage and the inaccuracy of triac switching circuits.

Another disadvantage of manually controlled dimmers is the use of potentiometers for control of the phase-switching triac circuit. These potentiometers, which are in some designs loaded with high currents, are the reason for many faults and instability after a certain time of use.

To avoid the disadvantages of presently manufactured dimmers the described device was designed, this unit solves these problems for an

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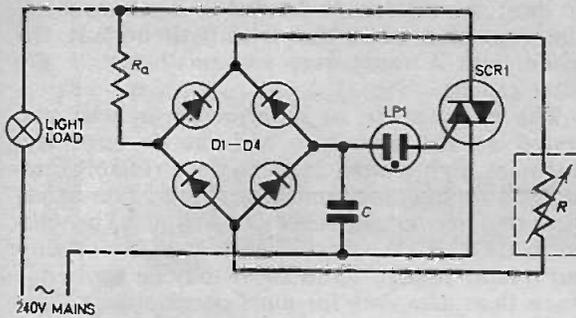
excluding case

\*Based on prices prevailing at  
time of going to press

# Automatic Light Level Controller

By M. DVORAK

**A dimmer unit with the ability to automatically keep a pre-set light level.**



**Fig. 1. Basic dimmer circuit with the inclusion of a bridge rectifier.**

acceptable price. The design incorporates the following points. (1) A photoresistor in the dimmer unit to enable automatic control of luminous intensity. (2) The use of an iris instead of potentiometer to control the light passing to the photoresistor. (3) Increase of stability at low light levels by the introduction of negative optical feedback.

### BASIC CIRCUIT

It is necessary to avoid oscillation of the light source, caused by positive feedback, of about 8Hz between the dimmer unit and the controlled light source. The oscillation can be avoided by moving the oscillation frequency to a higher level so that it is not noticeable, however, this is practically impossible due to the necessity of the use of standard incandescent lamps connected to the mains.

Another possibility is to use an electronic filter designed to suppress the frequency band of about 8Hz in the light controlled circuit. This

filter appears to be very effective and oscillation can be eliminated by a relatively simple circuit. One of the disadvantages is the necessity to filter the low frequency by means of a large (25 $\mu$ F) electrolytic capacitor connected to a d.c. transistorised circuit.

The use of transistors is additionally suitable to match the high resistance of the chosen photoresistor in darkness and thus to increase the light sensitivity of the complete unit. To fully control the light source the triac should be switched by transistors, thus the internal conversion from a.c. to d.c. was designed.

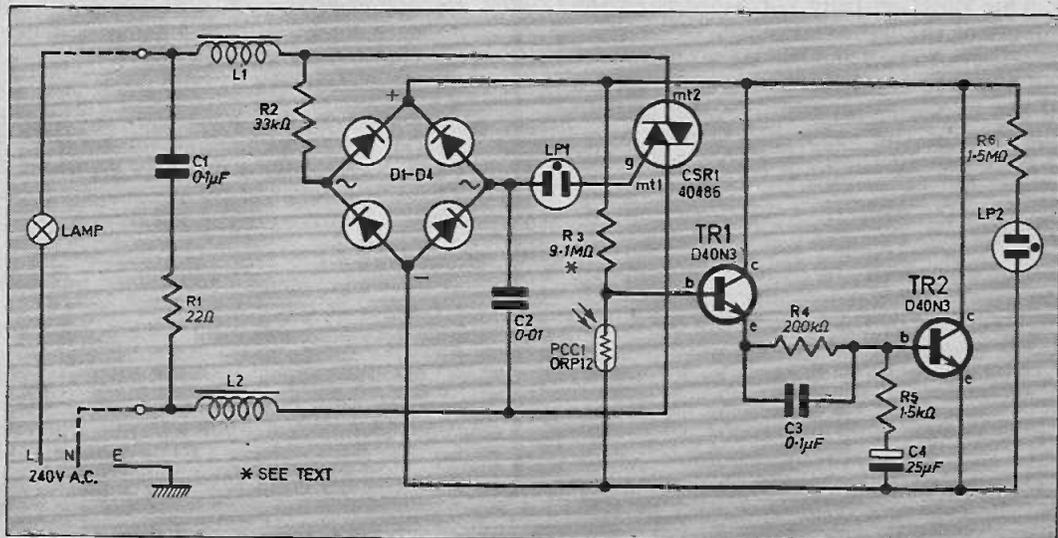
The solution, which is simple, consists of a bridge-rectifier, connected with the circuit of the controller as shown on Fig. 1. This circuit is connected on the principle of currently designed dimmer units, the neon lamp is fired by the RC phase control circuit. The current passing through resistor R is d.c. and it is therefore possible to replace resistor R by a transistor circuit. Resistor  $R_a$  limits the maximum current when the resistance in circuit (R) is reduced to a low value.

### CIRCUIT OPERATION

The readily available photoresistor type ORP 12 has a high "dark resistance" and in order to match this high resistance transistor TR1 (Fig. 2) is connected as an emitter follower to maintain high sensitivity. The frequency filter formed by C3 and C4 is connected to the base of TR2 which works as a variable resistor. Overall frequency response characteristic of this stage is shown in Fig. 3.

The frequency and phase response around 8Hz is not excessively critical but it is not recommended to alter substantially any value in the filter circuit. The entire filter was designed to match the expected range for different types of light sources.

**Fig. 2. Complete circuit of the Automatic Light Level Controller.**



In some cases after a sudden change of light level a sort of damped oscillation can be observed on the luminous intensity of the controlled light source. This effect is caused by the imperfection of the low frequency filter and lasts about one second. It does not visibly affect normal conditions of the dimmer unit in use.

The 25 $\mu$ F capacitor C4 is across a low voltage and a 12V type is quite sufficient for this purpose. Resistor R2 (9.1 megohm) is not always available and it may be necessary to use two resistors of 4.7 megohms connected in series. The transistors TR1 and TR2 should be 300V types of low collector dissipation, the most suitable transistor is the D40N3 designed for power line connection. If this is not available a BF259 can be used.

### REFERENCE LIGHT SOURCE

The light level is controlled by an iris in front of the photocell a substitute light source (neon LP2) in front of the photoresistor is necessary because with the iris fully open it would not be possible to set a completely dark level. The internal light source serves as a commanding light during the period in which the main light is turned fully off.

Without the use of this arrangement it is not possible to set up an extremely low light level which could be dependent on the sensitivity of the unit and its distance from the light. So that this arrangement cannot reduce the light sensitivity of the unit, by adding a constant light level, the signal lamp must be placed in such a way that it will not effect the photoresistor until the iris is almost fully opened and the controlled light is dimmed.

This neon is connected across the d.c. side of the bridge-rectifier; if the lamp is fully dimmed the voltage across the neon is high and the neon lights to its maximum. If the lamp is half on the neon lamp is automatically turned off in consequence of a high voltage drop across the dimmer. This function fully corresponds to the requirements of the light reference.

It is necessary to position the signal neon with regard to the photoresistor and iris in such a way that the unit suits all requirements of light regulation and at the same time would allow the unit to switch off the light source by means of the iris.

### R.F. FILTER

Interference caused by the unit appears mostly on wireless frequencies because of switching of high current by the triac in the controlled light circuit. To suppress this interference the unit employs an r.f. filter, formed by L1, L2, C1 and R1.

In the prototype unit the suppression coils used (L1, L2) were readily available ready-wound TV type chokes capable of passing two amperes. The capacitor C1, 0.1 $\mu$ F must be 400V

a.c. working and resistor R1 (22 ohms) is used to limit the voltage peaks due to discharging of the capacitor when the triac switches, at the same time it suppresses any oscillation in the filter circuit.

The filter, made as described was used and tested on the prototype and interference frequencies higher than 100kHz were reliably suppressed. On medium and short wave radio bands virtually no interference appeared. The disadvantage of this filter is a low load capacity but a lamp load of up to 200W may be applied—more than adequate for most situations.

### CONSTRUCTION

The complete unit can be housed inside any suitable case—it is a good idea to use a plastic case to provide good insulation but a metal case can be used provided the case is connected to the mains earth via three-core lead and plug fused at one amp.

Commence construction by cutting a length of tagboard to size and wiring up the components as shown in Fig. 4. The wires to LP2 should be about 150mm long so that LP2 can be positioned correctly as described earlier, LP2 is glued to the lid of the unit when finally positioned.

When mounting PCC1 it must be positioned slightly above all the other components on the board with its front on the same plane as the tagboard.

The wiring to the mains should be normal twin flex or—if a metal case is used—three-core wire.

## Components . . . .

### Resistors

R1 22 $\Omega$	R4 200k $\Omega$
R2 33k $\Omega$	R5 1.5k $\Omega$
R3 9.1M $\Omega$	R6 1.5M $\Omega$
All $\pm 5\%$ $\frac{1}{4}$ W carbon	

SEE

**SHOP  
TALK**

### Capacitors

C1 0.1 $\mu$ F 400V a.c. metalized paper
C2 0.01 $\mu$ F 250V metalized paper
C3 0.01 $\mu$ F 250V metalized paper
C4 25 $\mu$ F elect. 12V

### Semiconductors

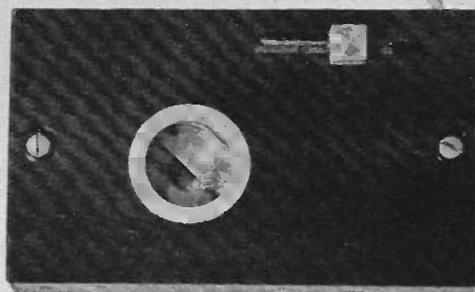
D1-D4 400V 0.5A bridge rectifier
CSR1 40486 triac or any 400V 2A triac
TR1 D40N3 or BF259 silicon npn
TR2 D40N3 or BF259 silicon npn

### Miscellaneous

LP1,2 neon lamps 80V type—no series resistor (2 off)
L1,2 2 amp chokes type TV2 (2 off)
PCC1 ORP12 light dependent resistor.
11 way double sided tagboard, stand off spacers, 4BA fixings, wide based insulated knob, 6mm diameter bolt with nut, aluminium for iris, felt to shade PCC1, case (size depends on tagboard used), wire.

# Automatic Light Level Controller

By M. DVORAK



Photograph of the completed unit, the iris and part of LP2 can be seen through the aperture.



Fig. 3. Overall frequency response characteristic of the transistor stage.

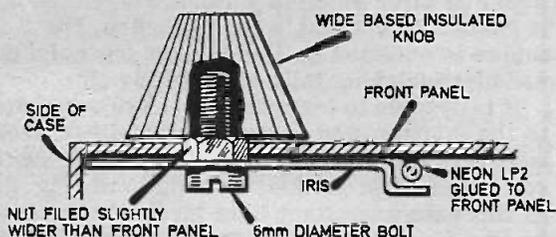
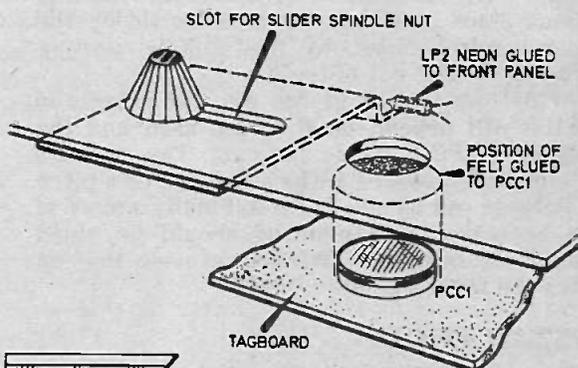
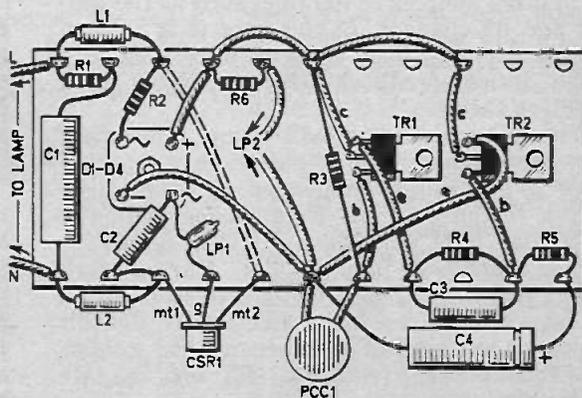


Fig. 5. (above and above right). Construction and fixing of the iris and LP2.

Fig. 4. (right) Construction of the Automatic Light Level Controller on a single tagboard. PCC1 must be mounted as described in the text.



Having completed the tagboard it should be placed in the case and mounted so that it is insulated, using stand off spacers and nylon bolts. With the board mounted the position of PCC1 should be marked on the lid and a hole cut as shown in Fig. 5.

## IRIS

The iris is constructed from 22 s.w.g. aluminium with two bends, as shown in Fig. 5, so that the neon LP1 is covered by one side of it. It is important that the leads to the neon are completely insulated so that they cannot touch the iris or case (if metal) and also that the control knob used is an insulated type with a sunken grub screw attachment.

The iris must be made the correct width so that it covers the whole of the aperture plus LP2 and also touches the side of the case nearest PCC1. This prevents the iris from twisting around since it is only fixed to the lid by the slider control, fixed to the spindle passing through the slot cut in the lid.

Actual dimensions of the iris and cutouts in the lid will depend on the case used and the position of PCC1 inside the case. The aperture hole must be covered with cellophane or a piece of Perspex can be glued into it. Finally a piece of felt or other thick material should be glued around the outside of PCC1 to provide shading when the iris is closed.

## INSTALLATION

The unit can replace the light switch for a single room but its fixing position will not necessarily be where the light switch was previously situated. It is essential to take into account some principles which result from the function of devices of this sort. The following analysis shows which principles are to be dealt with.

(1) Placing the dimmer unit very close to the light source a very strong negative feedback will come into effect, the iris will be usually fully closed and the whole device will become insensitive to other sources of lighting, such as the daylight and its changes. In this case it is easy to adjust a very low level of light, in consequence of the optical feedback which operates as a stabilizing factor.

(2) Another extreme will come into effect when the dimmer unit is placed in a position where it is strongly influenced by other light sources. In this case any insignificant change of the outside light will cause a strong alteration in the controlled light source. During dark periods the dimmer unit will try to work to its full capacity and it will be much more difficult to adjust a low level of light because the stabilizing effect of the feedback will not operate sufficiently.

It is not practical to install the dimmer unit in a place where the photoresistor could be shaded

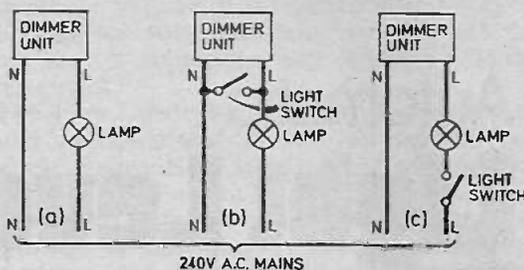


Fig. 6. Methods of connecting the unit to the supply and load (a) no mains switch (b) in parallel with switch (c) in series with switch.

by any movement in the room. Because PCC1 is very sensitive it would be affected by such changes and the intensity of operated light source would change as a result. A similar effect will take place where the dimmer unit is used for operating the light level in shop windows, when the unit is facing outside light. In this case for instance cars passing-by would cause a change of the light intensity if their lights were directed onto the shop window.

The dimmer is very useful for operating the light intensity level when table lamps are used. In this case the unit automatically levels the light during dark periods of the day. It is not suitable for use with fluorescent lights.

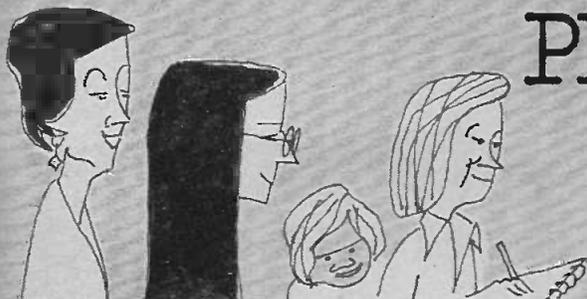
## CONNECTION

The unit can be connected to the light source in one of three different ways, in Fig. 6a the unit is connected without a mains switch, the light source is operated by the dimmer iris only, this includes switching fully on and fully off.

It is possible to leave the automatic regulation to the dimmer, and in case of immediate necessity to switch the light fully on the light switch can be wired in parallel with the unit (Fig. 6b). In this case a constant light level can be set up by the iris and the lamp can be turned fully on if required by the switch.

In Fig. 6c the dimmer unit is connected in series with the mains switch this results in complete disconnecting of the light source by the switch with automatic regulation of the light level being controlled by the dimmer unit. It is also possible to achieve a complete switching off by means of adjusting the iris to its end position.

The functional model was tested in various conditions for 7 months without any faults whatsoever and no interference of radio reception was noticed. As no potentiometer is used in the dimmer unit, a longer life is expected in comparison with the dimmers which are at present on the market. The neon LP2 can provide a small amount of external light, so that the knob can easily be found in the dark (this will not be the case if the circuit of Fig. 6c is used and the switch used to turn off the lamp). □



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By Derrick DAINES



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We are going to describe simple and practical experiments in a language that all can understand. These experiments will enable you to discover for yourself the fundamental laws of physics that govern our hobby and give rise to the often bewildering tricks that we get up to in designing circuits. This is in fact the BASIC basic series!

If we are ever to get a start in electronics, we must accept, various laws, but later we run into difficulties because we do not fully understand the reason for those laws. However, here we present you with a series of experiments designed especially to give you the most basic understanding possible; an understanding that will stand you in good stead in future years.

Please do carry out the experiments. Seeing and doing will fix facts in your mind far more effectively than just reading. Besides, it is more fun, and these experiments should give you plenty of that.

Finally, keep a little notebook. It doesn't matter what sort, nor how you keep it—what IS important is that after you have finished experimenting and just before you turn to something else, you jot down in your own words what the experiment has taught you. Again, this will help to fix it in your mind and later, when you browse through your notebook, the experiments will come alive again.

## THE MAGNETIC FIELD

Take a magnet—any magnet; bar, horseshoe, pot, anything. (Many fine magnets are to be had for the asking from car-breakers' yards or out of old TV sets). Sprinkle a few pins on the table and slowly lower the magnet towards them. Notice that the magnet does not have to actually touch the pins, but that when the magnet is some distance away, the pins leap up to cling to the magnet. "So what?" you say. So this—we are so familiar with this extraordinary event that we don't stop to think about it.

**Magnetism stretches out  
into space**

Silently, invisibly, magnetism reaches out to grab the pins. Isn't it odd that little old ladies who are uneasy at the very idea of silent, invisible electricity, will use a magnet to pick up pins?

If magnetism stretches out into space, there ought to be a way in which we can map it—find out what shape it is and how far it goes. Well, there is a way. Put your magnet firmly on the table and place a sheet of cartridge paper over the top. Now you need some iron-filings. You can buy these, but it's cheaper to drag your magnet round underneath a bench. Or why not actually file a piece of iron?!!

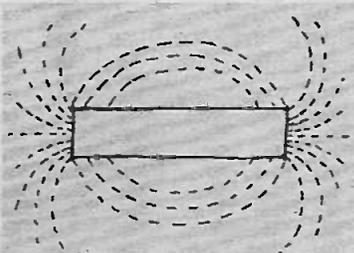


Fig. 1: Iron filing pattern obtained with a bar magnet.

Sprinkle the filings evenly over the paper and tap the paper very gently. The filings will arrange themselves into a pattern conforming to the shape of the magnet field. The actual shape of this pattern will depend upon what sort of a magnet you have. If it is a bar magnet, the shape will be as in Fig. 1. If a horseshoe, as in Fig. 2. (Pot magnets and ring magnets are not really suit-

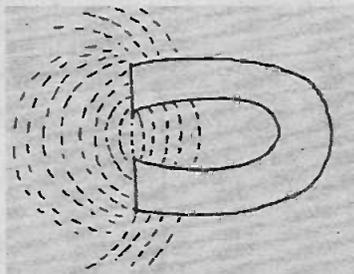


Fig. 2. A Horseshoe magnet will produce this filing arrangement.

able for this experiment.) If you tap too hard or too long, the filings will travel across the paper to cluster over two areas of the magnet—but only two.

**The centre of the magnet  
does not attract the filings**

We say that the magnetic field (and the magnet) is polarised—that is, they have a North pole and a South pole. Strictly speaking, we should call them North-seeking and South-seeking, as the next experiment shows.

If you have a bar-magnet, hang it up by a fine thread. After swinging about for some time, the magnet will eventually settle down in a North/South orientation. Mark one end with a piece of chalk and swing the magnet again. However many times you do it, the marked end will always finish up pointing in the same direction. This of course is what a compass does. Again—so what?

Well, ask yourself this question—you know that the compass points North/South, but is this because the Earth is attracting the compass, or because the compass is attracting the Earth? In other words, in the compass/Earth relationship, is one of the pair active and the other passive? If so, which?

**Answer next month.**

# General Purpose 5 Watt AMPLIFIER

By Tom Mason

For use with electric musical instruments, record player, radio and tape deck.



**A**N AMPLIFIER is probably one of the most popular projects for the amateur electronics constructor for it can find many applications both in the home and as a test amplifier on the work bench.

The General Purpose 5 Watt Amplifier described here can be used to amplify the signals from record players fitted with ceramic or crystal cartridges, radio tuners, tape decks, musical instruments such as electric guitar and organ, microphones, and in the workshop for testing prototypes requiring an amplification stage.

The quality is not claimed to be up to hi fi standard, but nevertheless is good enough to be acceptable to most listeners; maximum available output power is 5W r.m.s.

## SEPARATE UNITS

The complete amplifier as shown in Fig. 2 uses three integrated circuits, IC1, IC2 and IC3 and can be split into two distinct sections: (1) the battery powered preamplifier and tone controls, consisting of operational amplifiers IC1, IC2 and local components, and (2) the mains powered power amplifier IC3.

If desired, the two sections can be built and used independently of each other; some constructors may not wish to include the tone control and preamplifier stages into their amplifier in which case these should be omitted and input fed directly to capacitor C5.

The sensitivity of the main amplifier is 80mV for full output into a 16 ohm load, and this is suitable for most of the audio devices listed above, but for those with a lower signal output, down to 5mV, maximum output will only be obtained with a suitable preamplifier stage.

## OPERATIONAL AMPLIFIERS

The preamplifier and tone control stages each use differential operational amplifiers type 741;

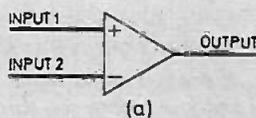
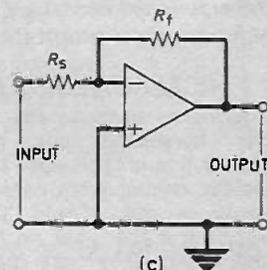
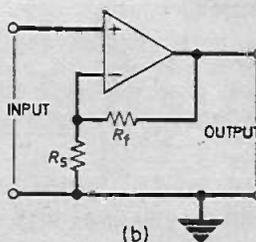


Fig. 1. Feedback arrangements for differential operational amplifiers.



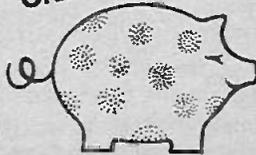
these are two-input devices, one inverting (-) and one non-inverting (+) and are symbolised as shown in Fig. 1a. The output voltage of these devices is proportional to the difference in voltage between the two inputs.

In audio work they can be used in two basic modes as shown in Figs. 1b and c. The gain of the system is controlled by the choice of feedback resistor  $R_f$  and source resistor  $R_s$ , both external components, and it can be shown that for Fig. 1b.

$$\text{gain} = \frac{\text{output voltage}}{\text{input voltage}} = \frac{R_f + R_s}{R_s}$$

$$\text{and Fig. 1c, gain} = \frac{R_f}{R_s}$$

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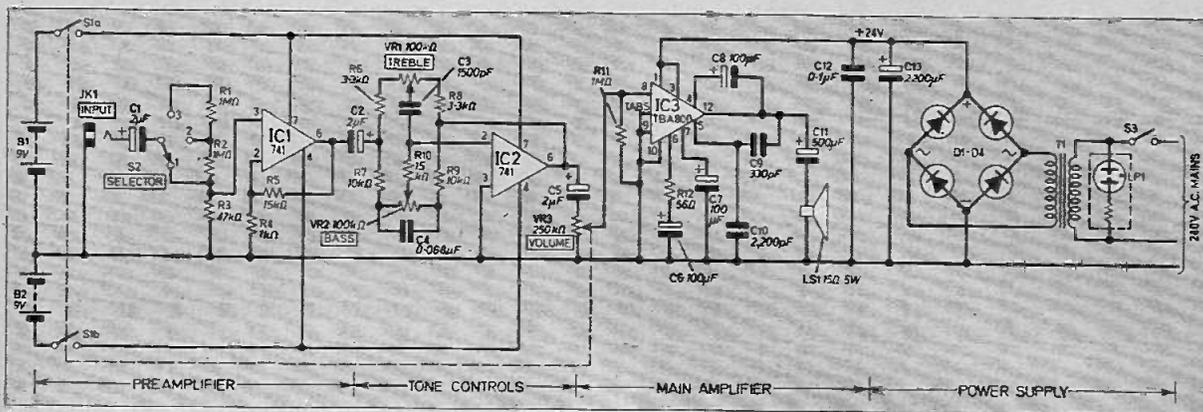


Fig. 2. The complete circuit diagram of the General Purpose 5W Amplifier.

### CIRCUIT DESCRIPTION

The complete circuit diagram of the General Purpose 5 Watt Amplifier is shown in Fig. 2. The main amplifier i.c. TBA800 can be powered by a supply in the range 5 to 30 volts (depending on load) and can be terminated in an 8 to 16 ohm loudspeaker to give output powers up to 5W r.m.s. (with suitable heatsink).

It was decided to use a 15 ohm loudspeaker (since this is more readily available than a 16 ohm one) to obtain 5 watts. This necessitates a 24 volt supply, which in the prototype is mains derived via T1 which steps down the mains voltage to approximately 17V; diode bridge D1-D4 gives full-wave rectification and the output from the bridge is smoothed by capacitor C13 to give a 24V (approx.) supply to pins 1 and 3 of IC3.

The prototype used a mains transformer with a secondary rated at 16V 1A. Any similarly rated transformer will do; current consumption at maximum output is about 600mA.

Input to IC3 is at pin 8 from the wiper of potentiometer VR3 (volume control) which is connected across the output of IC2. The output is a.c. coupled to the loudspeaker by capacitor C11.

Other circuit components around IC3 should be evident to readers from the pin identification drawing of Fig. 3.

### PREAMPLIFIER

Input to the preamplifier is via d.c. blocking capacitor C1 and selector switch S2, the position

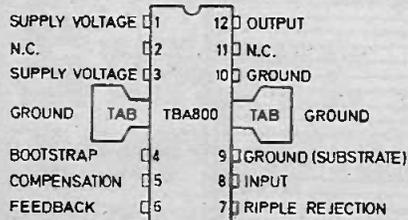


Fig. 3. Pin identification for the TBA800.

of the latter being chosen to suit the amplitude of the input signal.

The resistor chain, R1, R2 and R3 form an attenuator network, the voltage appearing across R3 being applied to IC1 input (pin 3). The value of these resistors has been calculated such that (1) 5mV at position 1 (2) 100mV at position 2 (3) 200mV at position 3 causes 5mV to be present at the input to IC1 which is connected in the mode of Fig. 1b. Thus the gain of the first stage is approximately 16.

### TONE CONTROLS

Output from IC1 is fed to the tone control circuitry, IC2 and local components, via C2.

The tone control employed is a Baxandall-type network that gives both boost and cut of treble and bass. Inspection of Fig. 2 will show that IC2 is connected in the mode of Fig. 1c, but since capacitors are now in circuit, the "resistances" equivalent to  $R_t$  and  $R_b$  are now frequency

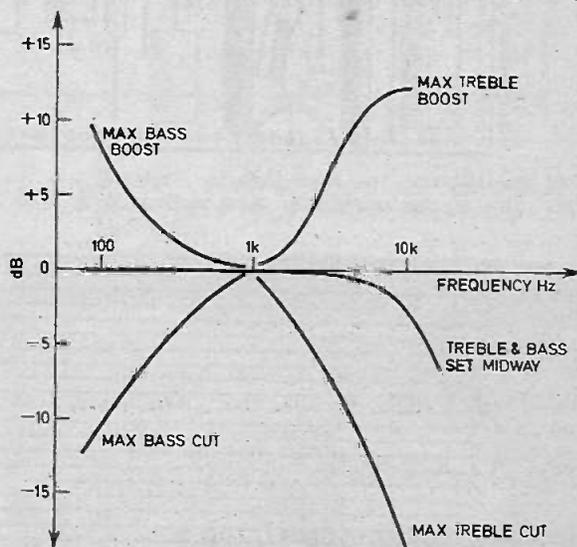


Fig. 4. Performance graphs for the tone control stage.

dependent i.e. they are impedances.

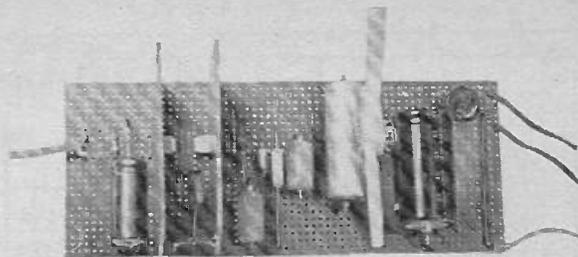
When VR1 and VR2 are set to their midway positions, the gain of this stage is unity for all frequencies; also, the gain for a frequency of 1kHz is unity for all settings of the tone controls (within component tolerances). All other frequencies are boosted or cut as the controls are rotated. This is standard practice. The performance of the tone controls is shown graphically in Fig. 4.

### MAIN AMPLIFIER BOARD

The main amplifier is constructed on a piece of 0.1in. matrix Veroboard size 58 holes by 24 strips. The layout of the components on the top side of the board and the breaks along the copper strips on the underside are shown in Fig. 5.

Begin by making all the cut-outs and drilling the fixing holes and then with the exception of IC3, position and solder the components and link wires to the board as shown in Fig. 5.

The heatsinks for IC3 are made from two pieces of copper clad board size 65mm x 50mm



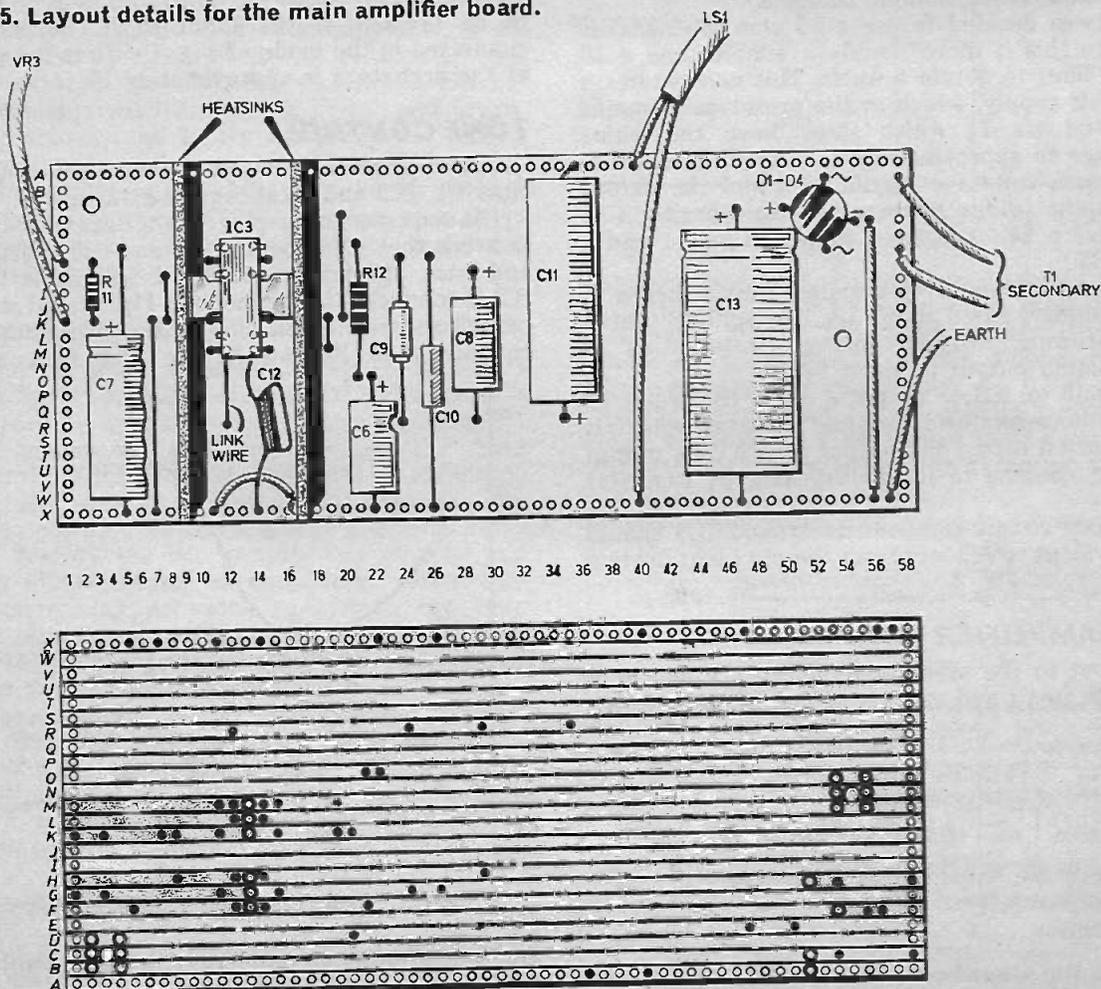
Completed main amplifier board.

which are soldered to the heatsink tabs on the i.c. These tabs should be very carefully straightened using a pair of pliers and then about 4mm of each end bent up vertically.

The i.c. should then be positioned and soldered to the board paying attention to polarity (pin 1 is marked on the body of the i.c.). The two heatsink boards should now be soldered to the tabs so that they rest on the component board and stand vertical. Now connect the link wire between ground and heatsink.

The flying leads to the loudspeaker should now be soldered in position. In the prototype, 200mm of twin-cored mains cable was used.

Fig. 5. Layout details for the main amplifier board.



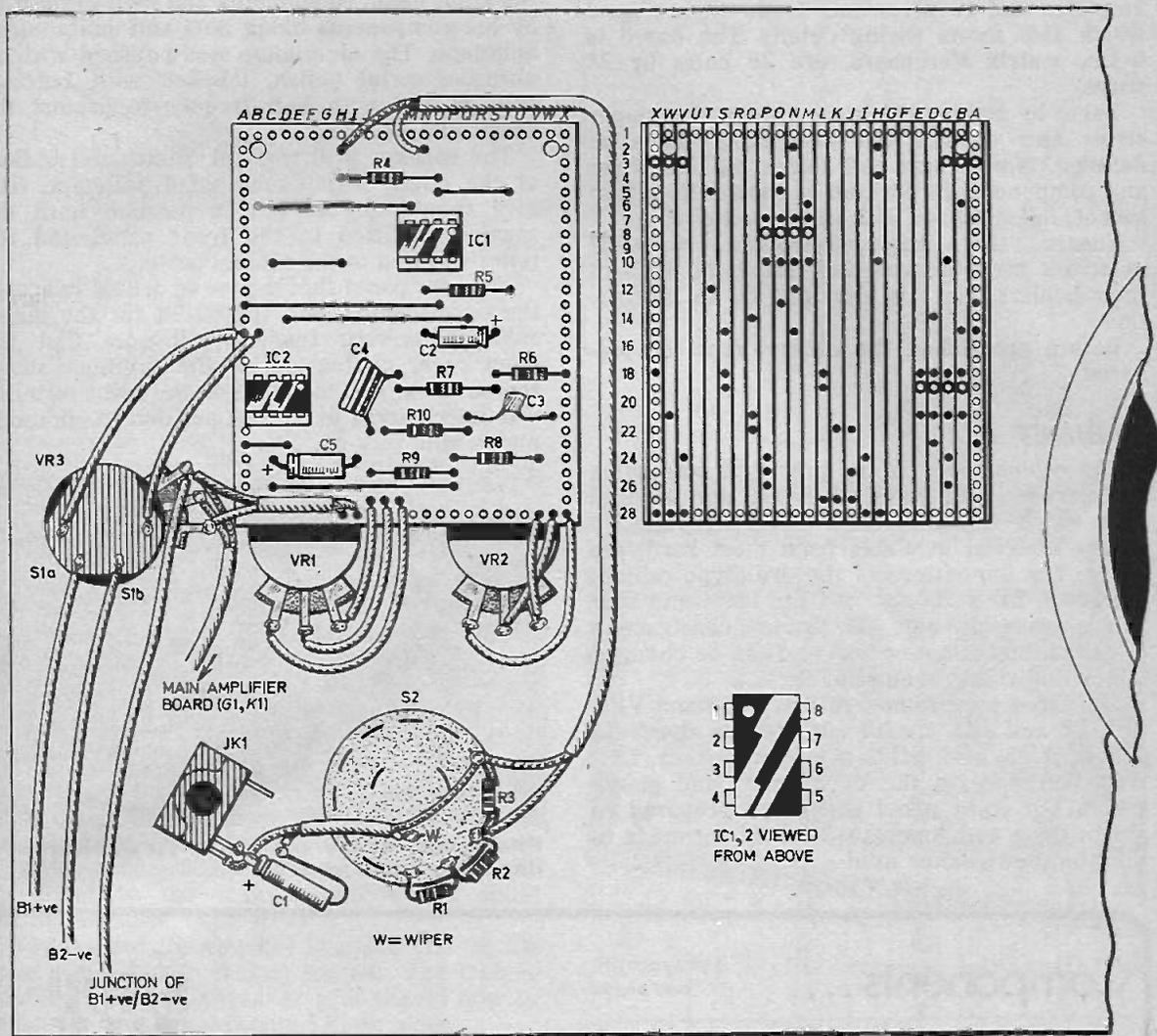
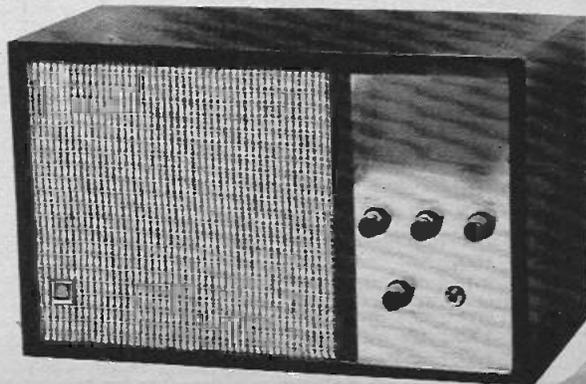


Fig. 6. The layout of the components on the preamplifier board and wiring up details.

Below: photograph of completed unit showing new position of mains neon indicator.

# General Purpose 5 Watt AMPLIFIER



## PREAMPLIFIER BOARD

The layout of the components for the pre-amplifier and tone controls is shown in Fig. 6 which also shows wiring details. The board is 0.1in. matrix Veroboard size 28 holes by 24 strips.

Begin by making the breaks along the copper strips and drilling the two fixing holes as detailed. Next insert and solder all link wires and components in position as shown. Note that sockets are used for both integrated circuits.

Ensure that the electrolytic capacitor polarities are observed and insert the i.c.'s in their holders, pin 1 is identified by an indentation.

Before proceeding the cabinet must be prepared.

## CABINET

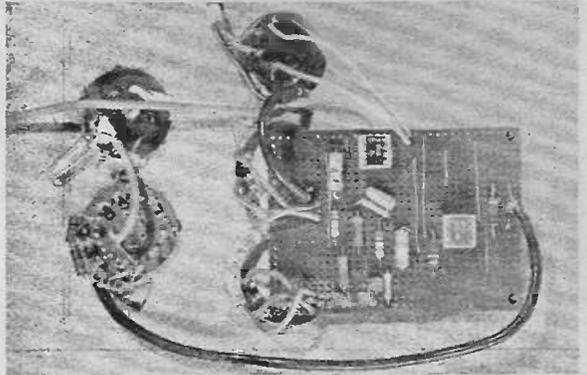
The cabinet used in the prototype was home made from 12mm thick chipboard and covered with black Contact which is a self-adhesive plastic material available from most hardware shops. The dimensions of the prototype cabinet are 380 x 230 x 200mm and the front and rear panels are removeable. The size and construction of the cabinet is not critical and can be changed to suit individual requirements.

The three potentiometers VR1, VR2 and VR3, LP1, S2 and JK1 are all mounted on the front panel which also holds the loudspeaker LS1. With reference to the illustrations and photograph, the front panel should be prepared to accept these components with a cut-out made to suit the loudspeaker used.

In the prototype a fascia was made from a thin sheet of aluminium which is drilled to suit the front panel components and held in position by the components fixing nuts and double-sided Sellotape. The aluminium was polished with an abrasive metal polish, labelled with Letraset and sprayed with hair lacquer to protect the sheen and lettering.

The speaker grill was cut to size and backed at the edges with double-sided Sellotape. The grill should not be put in position until the speaker is fitted to the front panel and the latter screwed to the cabinet battens.

The rear panel should now be drilled to accept the on/off switch and the outlet for the mains cable. Observant readers will note that the front cover photograph of the amplifier shows the on/off switch mounted on the front panel. It was later moved to its new position to eliminate mains hum pick-up.



Photograph of the completed preamplifier section mounted in position.

## Components . . . .

### Resistors

R1 1M $\Omega$	R5 15k $\Omega$	R9 10k $\Omega$
R2 1M $\Omega$	R6 3-3k $\Omega$	R10 15k $\Omega$
R3 47k $\Omega$	R7 10k $\Omega$	R11 1M $\Omega$
R4 1k $\Omega$	R8 3-3k $\Omega$	R12 56 $\Omega$

All  $\frac{1}{4}$ W  $\pm$  10% carbon

### Potentiometers

VR1 100k $\Omega$ lin. carbon
VR2 100k $\Omega$ lin. carbon
VR3 250k $\Omega$ log. carbon with ganged d.p.d.t. switch

### Capacitors

C1 2 $\mu$ F 10V elect.	C8 100 $\mu$ F 15V elect.
C2 2 $\mu$ F 10V elect.	C9 330pF
C3 1500pF	C10 2200pF
C4 0.068 $\mu$ F	C11 500 $\mu$ F 15V elect.
C5 2 $\mu$ F 10V elect.	C12 0.1 $\mu$ F
C6 100 $\mu$ F 6V elect.	C13 2200 $\mu$ F 25V elect.
C7 100 $\mu$ F 25V elect.	

### Integrated Circuits

IC1, 2	741 differential operational amplifier, 8-pin d.i.l. (2 off)
IC3	TBA800 5W audio amplifier

### Miscellaneous

D1-D4	$\frac{1}{2}$ A 50 p.i.v. type 96AA or similar
S1	d.p.d.t.—see VR3
S2	1-pole 3-way wafer
S3	mains on/off toggle
LP1	mains neon with built-in resistor
JK1	standard jack socket
T1	mains/17V 1A secondary—see text
LS1	15 $\Omega$ 5 watts
B1, B2	9V PP3 (2 off)
0.1in. matrix Veroboard:	58 x 24 strips (main amplifier), 28 holes x 24 strips (preamplifier); 8-pin d.i.l. sockets (2 off); copper clad board—p.c.b.—for heatsinks; screened lead; knobs (4 off); small wood screws for fixing boards; length of three-core mains lead; materials for cabinet.

SEE  
**SHOP  
TALK**

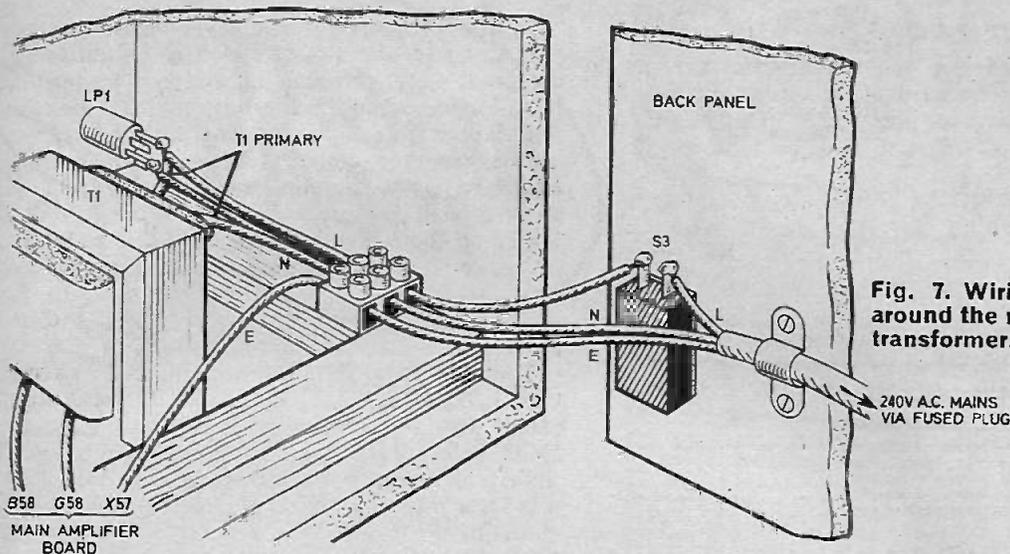


Fig. 7. Wiring up details around the mains transformer.

## ASSEMBLY

Place all the front panel components in position and wire up to the preamplifier board as shown in Fig. 6; using small wood screws secure the board to a short length of batten on the front panel. Ensure that the board does not touch VR1 and VR2. Screened lead must be used where shown.

Two PP3 9V batteries were found suitable to power the preamplifier and these should be wired up to the switch on VR3 and fixed to the side of the cabinet with a suitable bracket.

Solder about 200mm of screened lead to VR3 for input to the main amplifier and about 150mm of mains cable to LP1.

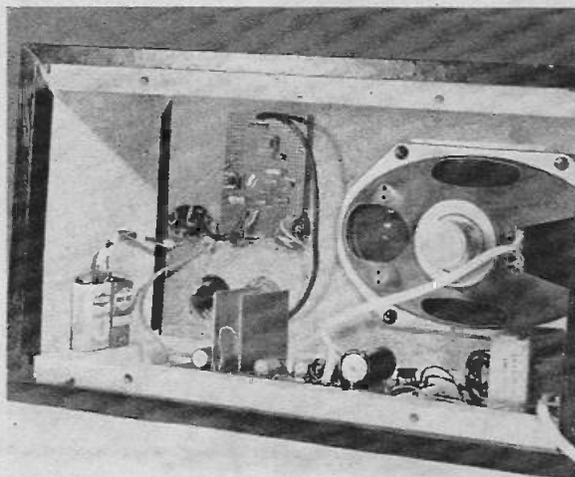
Now secure the speaker in place and fix the front panel to the cabinet battens. The treated labelled fascia and speaker grill should now be attached. Insert and secure LP1 in place.

Use two woodscrews to hold T1 firmly to the cabinet base and then wire up the primary to S3, LP1 and terminal block as shown in Fig. 7. Connect T1 secondary, the earth lead and screened input lead to the main amplifier board. All that remains is to solder the lead to the speaker and secure the board to the base. Screw on the back cover and the unit is complete.

Connection to the mains should be via a fused plug containing a 500mA fuse.

## IN USE

The main amplifier is switched on at S3 located on the rear panel (indicated by the illumination of LP1) and the preamplifier at S1 ganged to VR3 (volume). Input is via a jack socket—which may be changed to suit existing plugs—and should be via screened lead for best results.



Photograph of the prototype with rear panel removed.

## SPECIFICATION

OUTPUT	5 watts r.m.s. into 15 ohms
SENSITIVITY	1. 5mV r.m.s. into 47 kilohms
	2. 100mV r.m.s. into 1 megohm
	3. 200mV r.m.s. into 2 megohms
TONE	Boost Cut
	Bass +9dB -11dB at 100Hz Treble +12dB -20dB at 10kHz
FREQUENCY RESPONSE	Within $\pm 3$ dB from 20Hz to 13kHz

If in doubt as to the amplitude of the input signal set S2 to least sensitive position, (3), and adjust so that volume control gives widest range. For input signals greater than 200mV, the attenuator should be modified to suit. □

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Safety Stand £2.44

Prices Correct May 1974  
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Readers' Bright Ideas; any idea that is published will be awarded payment according to its merit. The ideas have not been proved by us.

Since cabinets for loudspeakers on the infinite baffle system must have two main features, i.e. they must be perfectly air tight and they must be made of something which prevents the passage of sound, then I suggest that when cabinets have been made from wood, a coat of rubberised underseal for cars would be a good idea as it would seal any small holes and even the pores of the wood and, as it says on the container, it is a very good sound insulator.

J. Beever,  
Chippenham, Wilts.

I wish to submit, for possible publication in the Bright Ideas column, a design for a simple and inexpensive cordless electric soldering iron.

A miniature insulated three-pin mains plug is fitted to the soldering iron lead, the lead is cut about 2cm away from the point where it leaves the iron, it is then fitted into the plug which is Araldited to the iron, a matching socket is fitted to the bench and connected to the mains. This system relies on the fact that when the iron is hot it will remain hot for a long enough time for one or more joints to be completed.

M. Renshaw,  
Sheffield, Yorks.

An idea which may be of interest to readers concerns the use of nails when trying small circuits: Instead of drilling elaborate boards or using turret board, both of which due to the time and trouble in their making, not to mention the cost, have to be cleaned afterwards for re-use, simply mark the circuit diagram on to a piece of scrap wood, and then tap 10mm long brass brads in at all the junctions and solder the components and wires on to these. I make less mistakes this way, when I'm in a hurry. With the parts removed the board can become firewood once again, or in the case of rough projects for the garage etc. can be made into the back of the box quite easily.

P. Stokes,  
Lowestoft, Suffolk.

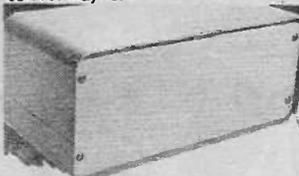
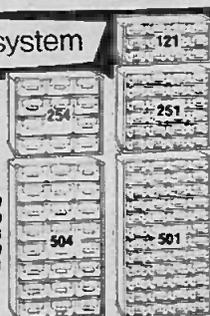
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Mod-305	£5.69	11"	4 1/2"
Mod-306	£6.58	11"	6"

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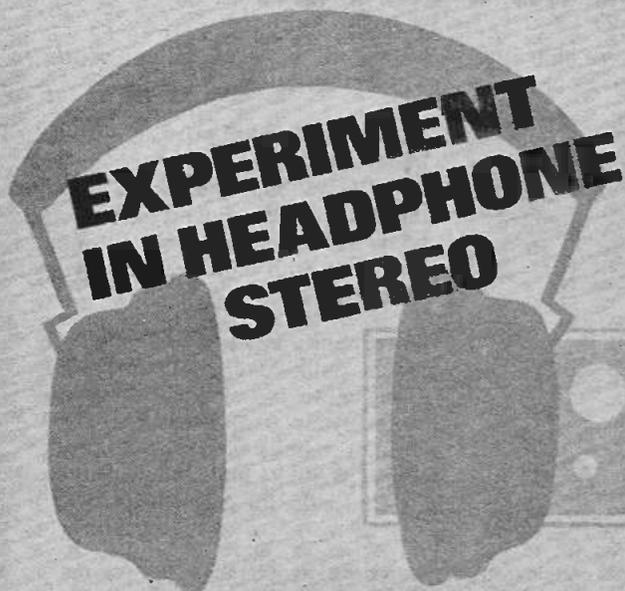
Width	Depth	Height	No.	Case cost	Extra for alu panel
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8"	6"	7"	867	£6.64	35p
9"	7"	5"	975	£8.64	35p
12"	7"	7"	1277	£7.42	26p
12"	7"	7"	1277	£8.11	—
16"	12"	7"	16127	£10.52	58p
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# NEXT MONTH...



When listening to stereo material through headphones one tends not to get the impression of a continuous sound stage in front of you. This simple experimental circuit sets out to try and overcome this problem, it also provides alternation to give a comparable speaker to phones level, and a balance control.

## RADIATION MONITOR

Consisting of a very simple circuit powered by a small battery, this monitor is portable and can be used for field work or demonstration purposes. Despite the simple circuit the unit is as commercial units using six tubes.

## HEADS OR TAILS

An electronic version of "heads and tails". The unit is inexpensive and employs an integrated circuit for ease of con-



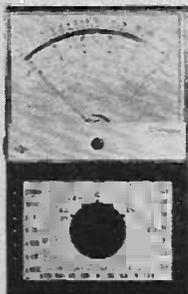
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# FREE ENTRY

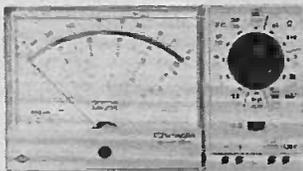
# COMPETITION

## ... WIN A CHINAGLIA MULTIMETER!

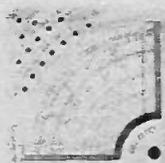
Here is your second and last chance to try for one of these high quality multimeters. Thirteen meters are being presented as prizes in this exciting free competition, open only to Everyday Electronics readers.



First prize, a Chinaglia Dino electronic multimeter which utilises f.e.t.s. to provide a d.c. input impedance of 200k $\Omega$ /V and an a.c. impedance of 20k $\Omega$ /V. This instrument has 33 ranges, all with high accuracy and costs over £28.



Second and third prize, a Chinaglia Minor multimeter with a sensitivity of 20k $\Omega$ /V on d.c. and 4k $\Omega$ /V on a.c. ranges. This instrument is a versatile pocket-sized instrument, having 25 ranges all with high accuracy. It sells for over £13.



Ten runner-up prizes, a Chinaglia Cito pocket multimeter designed specifically to provide a low cost instrument for everyday use. Sensitivity 20k $\Omega$ /V on d.c. ranges and 2k $\Omega$ /V on a.c. ranges. With 24 high accuracy ranges the Cito sells for over £10.

### HOW TO ENTER

Place the eight multimeter features, given below, in what you consider to be their order of importance to the average reader working on typical Everyday Electronics constructional projects.

For example, if you consider that "A.C. current ranges" is the most important of them all, write "C" in the box marked 1st on your entry coupon; the key letter of your choice goes into the second box and so on for all eight.

### IMPORTANT

All entries must be with us by Monday 22nd July 1974—the closing date. Regular readers submitting last month's entry coupon as well, may send both in the same envelope.

- A Anti-parallax mirrored scale.
- B Degree of accuracy.
- C A.C. current ranges.
- D Resistance ranges beyond 1M $\Omega$ .
- E Clearly marked, well arranged controls.
- J High sensitivity (ohms/volt).
- K Large, easy to read scale.
- L Overload Protection.

### COMPETITION RULES

There is no entry fee, but each attempt must be fully completed in ink on the proper printed coupon cut from Everyday Electronics, and bear the entrant's own full name and address.

Every accepted entry will be examined and the first prize, as described, will be awarded to the entrant who, in the opinion of an expert panel of judges, and in any one attempt, has shown the most skill and judgement in listing the eight features in order of importance. The other prizes will be awarded to the senders of the 12 next best attempts in order of merit. No entrant may win more than one prize.

In the event of a tie or ties for any of the prizes, a further eliminating contest will be conducted by post between the tying competitors to determine such winners in winning order.

Any entry which does not comply with the printed instructions or is received after the closing date will be disqualified, as will any received mutilated or illegible, incomplete, bearing alterations, or with more than one key letter in each space. No responsibility will be accepted for entries lost or delayed in the post or otherwise.

The judges' decision, and that of the Editor of Everyday Electronics in all other matters affecting the competition, is final and legally binding. No correspondence can be entered into.

The competition is open to all readers in Great Britain, Northern Ireland, and the Channel Isles except employees (and their families) of IPC Magazines, the printers of Everyday Electronics or of Chinaglia (U.K.) Ltd.

The winners will be notified, and the result announced in the earliest possible issue of this magazine.

Mulberry Walk, London, S.W.3

Everyday Electronics, July 1974

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| H41 | 2   | Sil Power transistors comp pair BD131/132                   | 55p |
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| B86 | 100 | Sil. Diodes sub. mln. IN814 and IN816 types                 | 55p |
| H34 | 15  | Power Transistors, PNP, Germ. NPN Silicon TO-3 Can.         | 55p |
| H67 | 10  | 3819N Channel FETs plastic case type                        | 55p |

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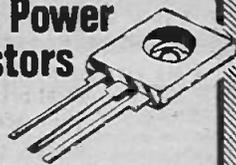
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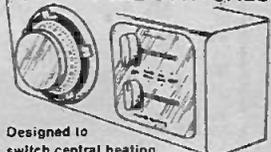
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**New products and component buying for constructional projects**

# SHOP TALK

By Mike Kenward

WE often get letters from readers asking how to get started in constructional electronics and we usually reply by saying buy a kit for one of our more simple projects—some of the advertisers sell them—and build it to the details shown, this way we know the unit works and that the reader will be starting at a fairly elementary level. However there is another way of constructing items—a way which requires very little skill and no soldering, you can build things and learn something with no fears of damaging components and when you are proficient you can gradually change to normal construction methods. The new way—with an Electroni-Kit.

Some time ago we were supplied with a SR4A kit which we tried out (the electronic machine-gun is good but fortunately failed to injure anyone!) and eventually passed on to the son of a staff member for further "trials". The unit has proved to be quite good and has

**The Electroni-Kit ST100 kit—good value for value for money.**



provided hours of fun and entertainment as well as education.

The biggest advantage is that youngsters can build many projects without help and without the need for tools, cases or soldering irons. The kits are not cheap but are worthwhile and cost from £8.80 to £33.95 including V.A.T. They provide many designs to build and the components can be used over and over again. There is no reason why almost any design should not be constructed and tested once the user became able to lay out the design.

Details from Electroni-Kit Ltd., 408 St. John's St., London EC1.

## **General Purpose Amplifier**

The parts for the *General Purpose 5 Watt Amplifier* should all be readily available, only the speaker is likely to provide any difficulty and this is an R. S. Components type which can be ordered from them by almost any dealer. The speaker unit must be a 15 or 16 ohm type.

Some notes on one or two other parts will not be amiss, the 741 integrated circuit should be obtained in the eight-pin dual-in-line (d.i.l.) case—most of them are this type nowadays. The transformer used can be any type with a mains primary and secondary rated at about 17V at 1A, various types are available from suppliers and prices vary considerably.

In the prototype one of the tags on the input selector switch has been used for component mounting (earth), if your switch is a single pole three way type it will not have this extra tag and the connection will have to be self supporting—this will be quite satisfactory in this application.

## **Telephone Call Charge Calculator**

The most important part in the

*Telephone Call Charge Calculator* is probably the counter—the bit that actually shows what your wife has spent, provided you can convince her to use the unit! As far as we know this counter is only available from Henry's Radio. If you find one anywhere else make sure that it is a 12V to 24V type (the 24V only types will not work on the 15V supply) and the coil resistance is in excess of 200 ohms.

The 555 timer integrated circuit should be obtained in the eight pin d.i.l. case, once again most of them are these days anyway. We always advise readers to use sockets with integrated circuits since they can be damaged by soldering and are difficult to remove without special tools once they are soldered in.

## **Light Level Controller**

We recommend the use of a plastic case for the *Light Level Controller* and advise readers to take note of the points concerning insulation as mentioned in the text.

The triac listed is a 6A 400V device but is reasonably priced at about 90p and is more than adequate for the maximum permissible lamp load imposed by the suppression coils. Other types of triac can be used provided they are rated at least 400V at 2A (to avoid overheating—no heatsink is fitted), remember other types may have different cases and wire configurations.

The transistors are high voltage types and have few direct equivalents. A. Marshall (London) Ltd., 42 Cricklewood Broadway, London NW2 3ET can supply two BF259s for £1.35 including V.A.T and postage.

## **Transistor Assisted Ignition**

We have been informed by Marshall's that due to the very large number of orders they have received for the semiconductor for the *Transistor Assisted Ignition* they have run out of stock of the TIP49 transistor.

Unfortunately their suppliers have already put back the quoted delivery date (in April) by approximately three months and it could be quite a few weeks before Marshalls can supply the outstanding orders. Readers' money will be refunded on request or the orders will be held until a supply is available.



## Blow for Bagpipes

Just a few comments about the *Electronic Bagpipes* article of the May issue of *EVERYDAY ELECTRONICS*.

Firstly there appears to be an error in the second full paragraph of column 2 page 254 in that the references to positions 1 and 3 of the switch are interchanged. Position 1 gives vibrato, whilst position 3 gives "bagpipes", or so it seems to me from Fig. 1. Incidentally I do not think that the Scottish folk will like it one bit to read the part that says that "in position 3 it becomes a

pleasing sound not unlike an organ".

I suspect that the author is Tom Richardson of North Shields former fellow of the Electronic Organ Constructors Society, and next time I see him, I must pull his leg about this, should we say, "praising with feint damns", or left handed compliments.

However I do think that the article would have been improved by the inclusion of a few dimensions, and perhaps an extra elevation, in Fig 3. Also by the inclusion of a musical stave showing the exact compass to be aimed at (because the "spread" of unijunctions can alter the tuning), together with much more precise instructions for the tuning of the drones than is given in the closing paragraph.

James W. Robson  
Newcastle upon Tyne.

*We thank you for pointing out the error in our text namely that in the above mentioned paragraph, positions 1 and 3 should be transposed. We apologise to any Scottish readers who may have been offended.*

*As far as "more information" is concerned we think sufficient has been given to successfully construct the unit. We would be interested in readers' comments on this point.*

## Suppression

I feel that I must make a few comments on the reply given in your *Help* column of the May issue of *EVERYDAY ELECTRONICS*, concerning automobile interference.

If carbon leads are fitted (as the practice seems to be these days) the standard way of suppressing these leads is to replace the carbon h.t. lead between the coil and distributor with a length of copper h.t. lead, and insert a "cut-lead suppressor" 1½ inches from the coil end of the lead.

The h.t. coil is suppressed with a 1µF not 0.1µF capacitor as stated, and is fitted to the ignition, or SW side of the coil. The same value 1µF is fitted to the alternator, or dynamo. In either case it is advisable to disconnect the battery.

Hoping you will correct these errors made in a future issue of your otherwise excellent magazine.

A. N. Choat  
Medway Sound Service  
Rainham.

## Amateur Exhibition

I was very interested to see in the May issue of *EVERYDAY ELECTRONICS* the discussion by Mr. Paul Young on page 270 in *Counter Intelligence*. I am pleased to say that I can answer Mr. Young's plea as the British Amateur Electronics Club is holding a B.A.E.C. Amateur Electronics Exhibition at the Shelter, The Esplanade, Penarth, from July 20 to July 27 next.

I am expecting many exhibits from members in all parts of the country, so that there should be a very good cross-section of both original exhibits and designs taken from your excellent magazine. All readers are welcome.

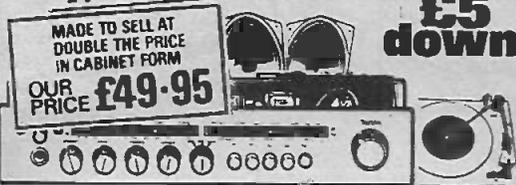
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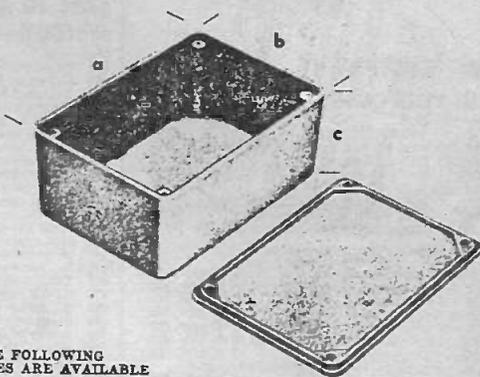
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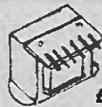
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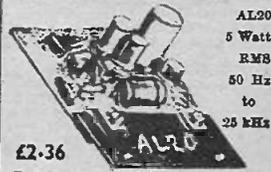


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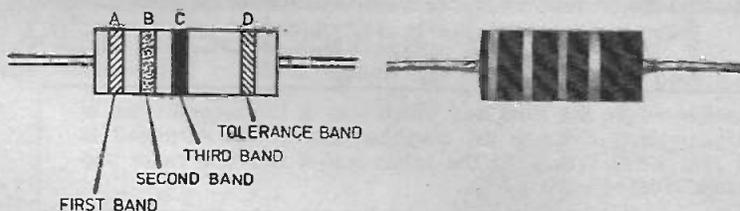


# KNOW YOUR COMPONENTS...

## Hints & Tips for the Novice Constructor

By Ron Adams

THE beginner in electronics often has difficulty in identifying components, component values (sometimes coded), polarities, etc. This "information page" has been formulated to help in this area and begins this month with the most common component—the resistor.



### The Resistor

The obviously important thing to watch on this device is the ohmic value, depicted by a colour code. At least all resistors—excepting some high stability types, which have the value printed on the body—have a colour coding of bands or dots, see Table 1.

If you don't know your colour code, then keep it written on a card next to you when constructing your projects. You will save yourself a lot of headaches and time by putting the right resistors in circuit. Not to mention the damage to components that can result.

The other thing to watch carefully is the current rating. Remember that you can put a half watt resistor in place of an eighth watt resistor, but not vice versa.

The wattage of the resistors can usually only be found from the size and type of resistor and various types and sizes with wattage ratings are also shown in full-sized silhouettes below.

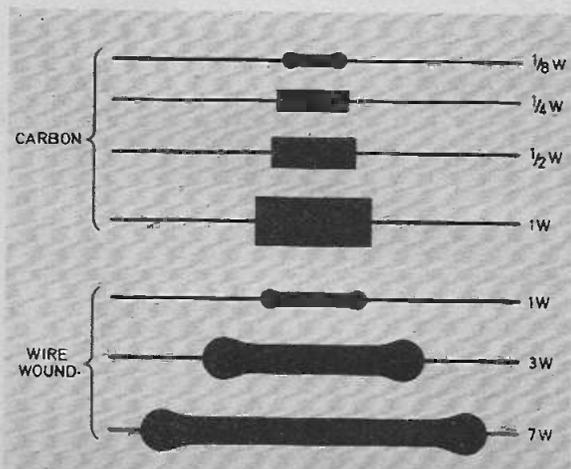


Table 1: Resistor Colour Code

Colour	1st digit (A)	2nd digit (B)	Multiplier (C)	Tolerance $\pm$ per cent (D)
Black	—	0	1	—
Brown	1	1	10	1
Red	2	2	100	2
Orange	3	3	1,000	3
Yellow	4	4	10,000	4
Green	5	5	100,000	—
Blue	6	6	1,000,000	—
Violet	7	7	10,000,000	—
Grey	8	8	100,000,000	—
White	9	9	1,000,000,000	—
Gold	—	—	0.1	5
Silver	—	—	0.01	10

No fourth band indicates a  $\pm 20$  per cent tolerance.

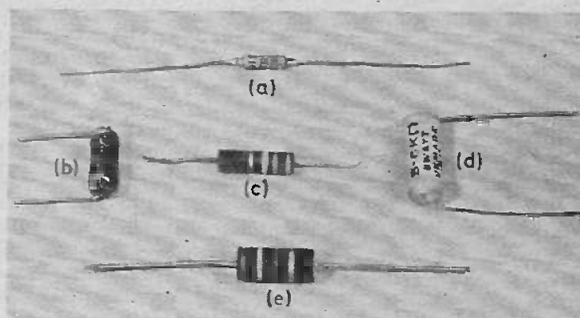
A fifth band is sometimes used, colour salmon pink, to indicate high stability (hi-stab) resistors.

Also, it is surprising how many people think that a resistor is polarised and has to be put in circuit one way only—it isn't and can be put in either way round.

### Colour Code Example

A resistor coded as A—red, B—violet, C—yellow, D—gold indicates a value of 470 kilohm  $\pm 5$  per cent.

Next part: capacitors.



Above. A selection of resistors. (A) high stability (B) enamelled wirewound (C) and (E) carbon composition (D) high voltage wire wound. Left. Size and wattage of common types.

# DOWN TO EARTH

By GEORGE HYLTON

"I connected up the *Fuzz Box* which was in the second issue of *Everyday Electronics* to my amplifier and I was surprised to find that when I touched the input lead I heard a radio programme. Please explain."

This kind of experience isn't at all uncommon. It explains why audio pre-amplifiers have "unnecessary" capacitors in them which have no appreciable effect on their audio performance. They are there to prevent "break-through" of unwanted r.f. signals picked up by the input leads.

## HUMAN AERIAL

In the dear old days when even medium wave receivers had to have an aerial wire plugged in at the back, many of us found out that a finger touched on the aerial terminal was a useful temporary substitute. Not that anybody spent his evenings standing by a set with a finger poked into it, but it was a handy trick for testing purposes.

The human body may not be a very efficient aerial, but it does pick up strong radio signals. That explains how the radio-frequency signals got into the *Fuzz Box*. What it doesn't explain is how they were converted to audio, in other words how they were "detected."

## RECTIFICATION

Detection is rectification—the conversion of the r.f. carrier into d.c. Fluctuations in the r.f. strength appear as fluctuations in the d.c. output. The fluctuations are caused deliberately at the

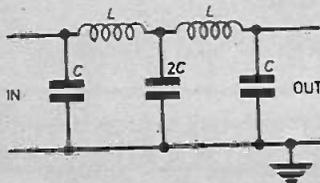


Fig. 1. A low-pass LC filter.

transmitter, by "modulating" the r.f. carrier with the audio programme, and rectification recovers the audio.

Now, rectification is normally carried out by diodes, and there are no diodes in the *Fuzz Box*. So how does it rectify?

## DISTORTION

Well, rectification is a form of distortion, in which the positive half-cycles, say, are allowed to pass and the negative ones are suppressed. Even if the process is incomplete, and the unwanted half-cycles are only partially suppressed some degree of rectification still takes place. In the *Fuzz Box* this kind of distortion is deliberately introduced to provide the "fuzz" effect, so it's not surprising that r.f. signals are detected by it.

The question is, how to eliminate the r.f. breakthrough, if it is bad, without at the same time eliminating the "fuzz" effect.

## LOW-PASS FILTER

The obvious method is to put a low-pass filter in the input circuit, so as to allow audio signals to pass but attenuate radio-frequency signals. In theory, an LC filter (Fig. 1) is most effective, but the chokes are apt to be bulky and expensive.

If the lowest radio frequency is far above the highest audio frequency the less efficient but cheaper RC filter is adequate.

In the U.K., the 200kHz long wave transmitter (Radio 2) is likely to be the lowest dangerous radio frequency (unless you live near one of the v.l.f. navigational aid transmitters). The highest audio frequency of interest is 10kHz, since "fuzz" in the form

of harmonics of higher frequencies is beyond the limit of human hearing, and anyway most of the "fuzz" tends to be at much lower frequencies than even 10kHz. So a filter which attenuates 10kHz slightly is the best bet, since it will attenuate 200kHz at least 20 times more.

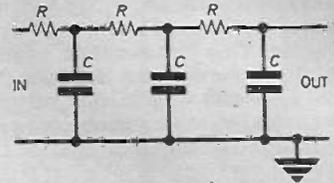


Fig. 2. A three-section low-pass RC filter.

The values of R and C and the number of filter sections needed are a matter for experiment, but a three-section filter as shown in Fig. 2, with R=10 kilohms and C=1,500picofarads should function satisfactorily. Neither value is critical, but ceramic or mica capacitors are better than paper or plastic types. The rated capacitor working voltage is not important here.

## SCREENING

The filter should, along with the rest of the *Fuzz Box* components, be enclosed in an earthed metal box for screening, and connected to the amplifier with a screened lead. Quite short lengths of unscreened lead can pick up enough r.f. to cause interference, particularly if the source is a short-wave one such as the local television transmitter.



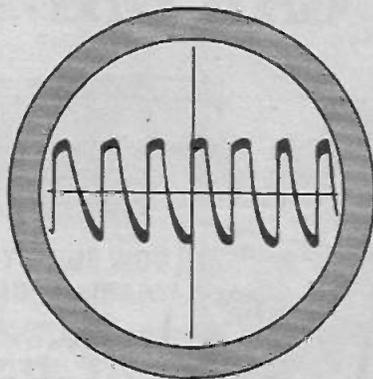
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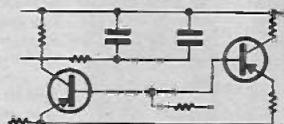
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*NOTE:* The ability to solder on a printed circuitboard is necessary to complete this kit successfully. Circuit diagram and comprehensive instructions 55p. free with kit.

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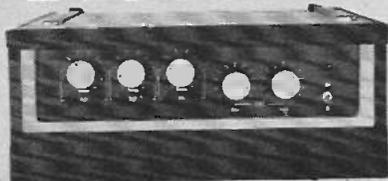
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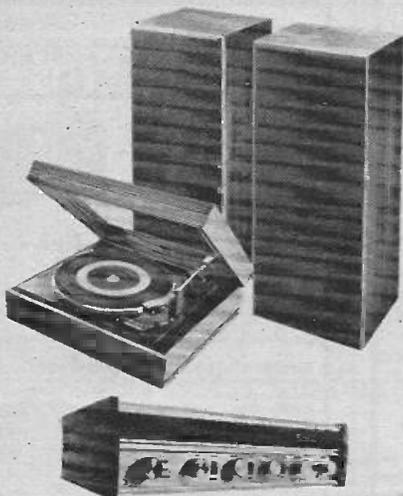


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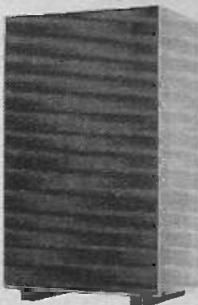
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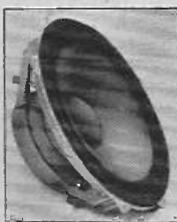
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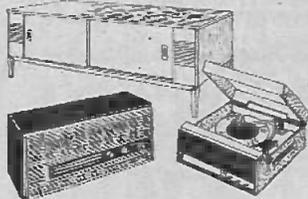


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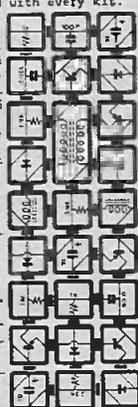
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47µF 6p	10µF 6p	1µF 6p
100µF 6p	22µF 6p	2.2µF 6p
220µF 8p	47µF 6p	4.7µF 6p
330µF 10p	100µF 8p	6.8µF 6p
470µF 10p	220µF 10p	10µF 6p
1000µF 11p	470µF 13p	6.8µF 6p
1500µF 20p	680µF 20p	10µF 6p
2200µF 24p	1000µF 22p	22µF 6p
	2200µF 39p	68µF 10p
	5000µF 68p	100µF 11p
16 VOLT	40 VOLT	150µF 13p
15µF 6p	220µF 19p	220µF 19p
33µF 6p	6.8µF 6p	330µF 22p
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## AUDIO BARGAINS STEREO DECODER



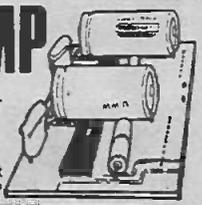
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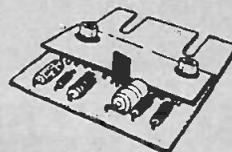
A ready built unit, ready for connection to the I.F. stages of existing F.M. Radio or Tuner. A tell tale light can be connected. The unit is a small printed circuit, no further alignment necessary. A L.E.D. is recommended as the indicating light, suitable device available from us at 36p. Instructions included

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Pre-assembled printed circuit boards 2" x 3" available in stereo only, will fit .15 edge connector.

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Instruction leaflet supplied with all units. Post and packing and VAT included in prices.

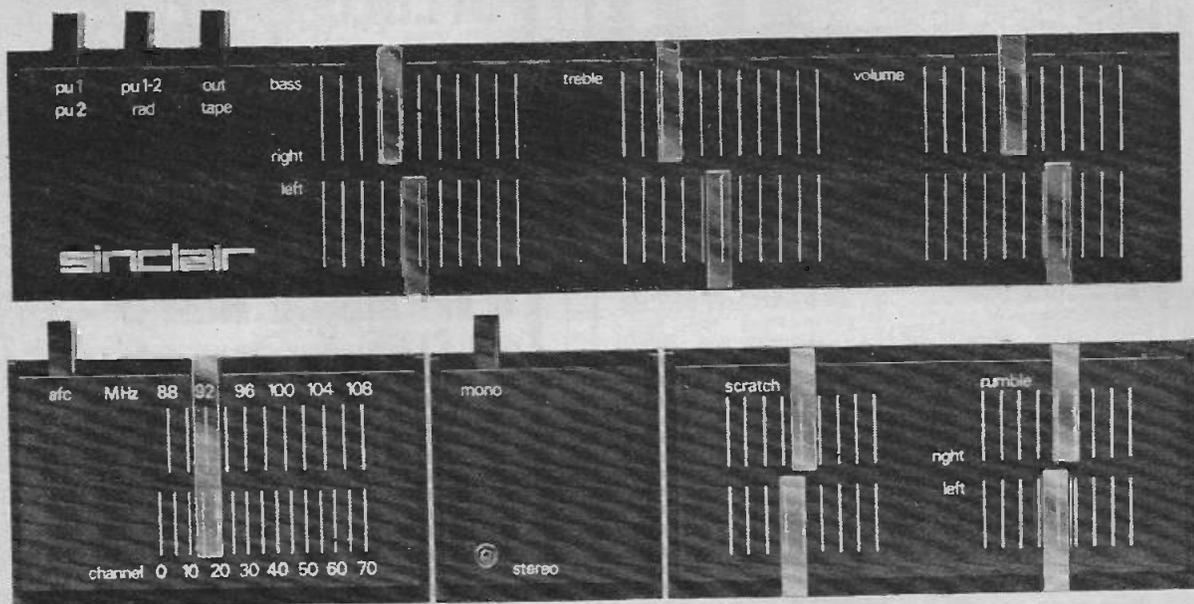
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# Sinclair Project 80

exciting



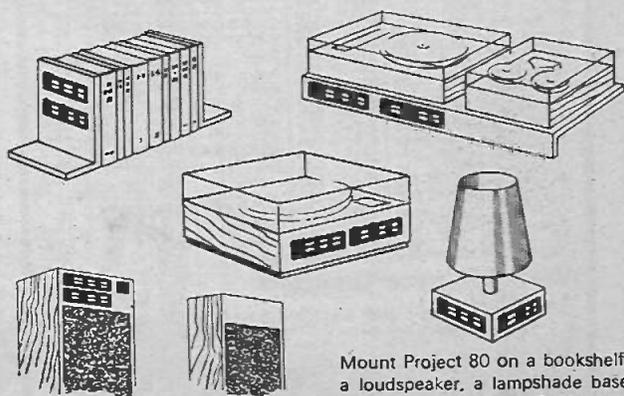
only  $\frac{3}{4}$ " deep x 2" high

Living with hi-fi takes on new meaning with Sinclair Project 80. The electronics of these revolutionary new modules are all contained within elegantly designed matching cases no more than three-quarters of an inch deep. They are designed for mounting on any appropriate flat surface by means of 6BA bolts extending from the rear of each module and which pass through suitably drilled holes. Connections are taken away out of sight in a similar manner. The possibilities opened up by Project 80 are endless – superb hi-fi systems can be installed in ways hitherto only dreamed about and never before made practical. No more cutting out and shaping to put modules in position. A few holes drilled with the aid of templates supplied and the job is done. Now you need never again be faced with problems of keeping the hi-fi from clashing with carefully thought-out furnishing schemes. (That will surely please wives!) Slider controls have been introduced in place of knobs and all modules in the range incorporate new up-dated circuitry with emphasis on performance standards and built-in protection against overload and shorting. The aim was to re-think modular construction completely – to make it infinitely more versatile, even simpler and more reliable – the result – Project 80 – another triumph for Sinclair, and the most exciting construction modules ever.

the slimmest, most elegant hi-fi modules ever made

## Typical Project 80 applications

System	The Units to use	Units cost
Simple battery record player	Z.40	£5.45 +54p V.A.T.
Mains powered record player	Z.40, PZ.5	£10.43 +£1.04 V.A.T.
30W. RMS continuous sine wave stereo amp.	2 x Z.40s, Stereo 80; PZ.6	£30.83 +£3.08 V.A.T.
50W (8 Ω) RMS continuous sine wave de luxe stereo amp.	2 x Z.60s, Stereo 80; PZ.8	£33.83 +£3.38 V.A.T.
Indoor P.A.	Z.60, PZ.8	£14.93 +£1.49 V.A.T.



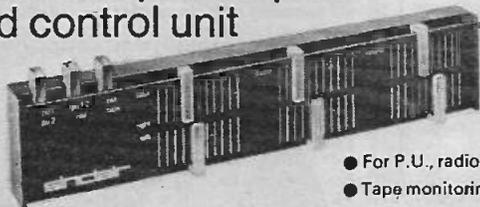
Mount Project 80 on a bookshelf, a loudspeaker, a lampshade base, a false wall with two Q.16 loudspeakers... almost anywhere.

Everyday Electronics, July 1974

Project 80 FM tuner, decoder, and A.F.U. may be added as required

# new thinking in modular hi-fi

## Stereo 80 pre-amplifier and control unit



- For P.U., radio and tape
- Tape monitoring switch
- Simplest ever fixing

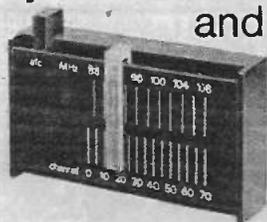
Each channel has its own separate tone and volume controls operated by sliders, enabling ideal environmental matching to be obtained. A virtual earth input stage forms part of the up-dated circuitry that ensures the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied.

### TECHNICAL SPECIFICATIONS

Size - 260 x 50 x 20mm (10 1/2 x 2 x 3/4 ins)  
 Finish - Black with white indicators and transparent sliders  
 Inputs - Magnetic pick-up 3mV RIAA corrected; Ceramic pick-up 300mV  
 Radio 300mV; Tape 30mV  
 Signal/noise ratio - 60dB  
 Frequency range - 20Hz to 15KHz ± 1dB; 10Hz to 25KHz ± 3dB  
 Power requirements - 20 to 35 volts  
 Outputs - 100mV + AB monitoring for tape  
 Controls - Press button for tape, radio and P.U. Sliders for volume, bass (+ 12dB to - 14dB at 100Hz) treble (+ 11dB to - 12dB at 10KHz)

R.R.P. £11.95 +£1.19 V.A.T.

## Project 80 FM tuner and stereo decoder



- Twin dual varicap tuning: 4 pole ceramic filter; switchable A.F.C.
- On the decoder, solid state stereo indicating beacon.

Making the Project 80 F.M. tuner and decoder available separately gives a wider choice of systems and saves money where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40dB channel separation with 150mV output per channel. Both units may be used with other than Project 80 systems.

### TECHNICAL SPECIFICATIONS OF TUNER

Size - 85 x 50 x 20mm (3 1/2 x 2 x 3/4 ins)  
 Tuning range - 87.5 to 108 MHz  
 Detector - I.C. balanced coincidence for good A.M. rejection  
 One I.C. equal to 26 transistors  
 Distortion - 0.2% at 1 KHz for 30% modulation  
 4 pole ceramic filter in I.F. section  
 Aerial impedance - 75 Ω or 240-300 Ω  
 Sensitivity - 4 microvolts for 30dB quieting  
 Output - 300 mV for 30% modulation  
 Power requirements - 23 to 33 volts

### DECODER

Size - 47 x 50 x 20mm (1 7/8 x 2 x 3/4 ins)  
 One 19 transistor I.C.

R.R.P. £11.95 +£1.19 V.A.T.

R.R.P. £7.45 +0.74 V.A.T.

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If, within 3 months of purchasing any product direct from us, you are dissatisfied with it, your money will be refunded on production of receipt of payment. Many Sinclair appointed stockists also offer this guarantee. Should any defect arise in normal use, we will service it without charge.

## Z.40 & Z.60 power amplifiers totally short-circuit proof



Z.40



Z.60

Intended for use in Project 80 installations, these modules readily adapt to an even wider range of applications. Both incorporate built-in protection against short circuiting and risk of damage from mis-use is greatly reduced.

### Z.40 TECHNICAL SPECIFICATIONS

Size - 55 x 80 x 20mm (2 1/4 x 3 1/4 x 3/4 ins) 9 transistors  
 Input sensitivity - 100mV  
 Output - 15 watts RMS continuous into 8 Ω (35v)  
 Frequency response - 10Hz - 100KHz ± 1dB  
 Signal/noise ratio - 64dB  
 Distortion - at 10 watts into 8 Ω less than 0.1%  
 Power requirements - 12 to 35 volts

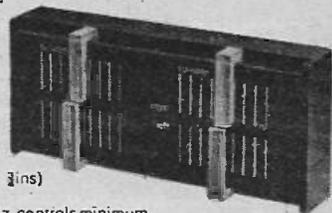
### Z.60 TECHNICAL SPECIFICATIONS

Size - 55 x 98 x 15mm (2 1/4 x 3 7/8 x 3/4 ins) 12 transistors  
 Input sensitivity - 100-250mV  
 Output - 25 watts RMS continuous into 8 Ω (45V).  
 Distortion - typically 0.03%  
 Frequency response - 10Hz to more than 200KHz ± 1dB  
 Signal/noise ratio - better than 70dB  
 Built-in protection against transient overload and short circuiting  
 Load impedance - 4 Ω min; max. safe on open circuit

Z.40 R.R.P. £5.45 + 0.54 V.A.T.; Z.60 R.R.P. £6.95 + 0.69p V.A.T.

## Project 80 active filter unit

Makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls applied to each channel make it easier to obtain ideal stereo balance.



### TECHNICAL SPECIFICATIONS

Size - 108 x 50 x 20mm (4 1/4 x 2 x 3/4 ins)  
 Voltage gain - minus 0.2dB  
 Frequency response - 36Hz to 22KHz controls minimum  
 Distortion - at 1 KHz - 0.03% using 30V supply  
 HF cut off (scratch) - 22KHz to 5.5KHz, 12dB/oct. slope  
 LF cut off (rumble) - 28dB at 20Hz, 9dB/oct. slope

- For scratch and rumble control
- Transistorised active circuitry

R.R.P. £6.95 +0.69 V.A.T.

## Power supply units

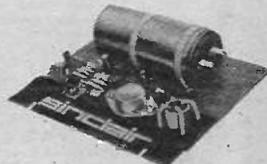
### PZ.8

Stabilised. Re-entrant current limiting makes damage from overload or even direct shorting impossible. Normal working voltage (adjustable) 45V.

R.R.P. £7.98 + 0.79p V.A.T.  
 Without mains transformer

PZ.5 30V unstabilised  
 R.R.P. £4.98 + 0.49p V.A.T.

PZ.6 35V, stabilised  
 R.R.P. £7.98 + 0.79p V.A.T.



# sinclair

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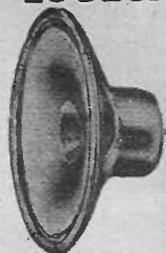
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2N915	0-741	2N3905	0-24	BC1107	0-18	BD123	0-32		
2N918	0-47	2N3906	0-27	BC1093	0-15	BD124	0-67	8D1L	0-46
2N923	0-30	2N4036	0-63	BC1099	0-19	BD131	0-40	14D1L	0-38
2N1302	0-19	2N4037	0-42	BC113	0-13	BD132	0-50	LM747	1-00
2N1303	0-19	2N4058	0-16	BC115	0-15	BD135	0-43	LM7488DIL	
2N1304	0-24	2N4059	0-09	BC116	0-15	BD136	0-49		
2N1305	0-24	2N4060	-0-11	BC116A	-0-18	BD137	-0-35	14D1L	0-73
2N1306	0-33	2N4061	-0-11	BC117	-0-21	BD138	-0-43	MC1303P	1-26
2N1307	0-22	2N4062	-0-11	BC118	-0-18	BD139	-0-71	MC1310	1-26
2N1308	0-25	2N4126	0-20	BC119	0-29	BD140	0-81	MC1458CP1	
2N1309	0-36	2N4289	0-13	BC121	0-23	BDY20	1-05		
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2N1671B	1-72	2N4921	0-73	BC132	0-30	BF117	0-43	MJ490	0-98
2N1671C	4-32	2N4922	0-84	BC134	0-18	BF119	0-58	MJ491	1-38
2N1711	0-45	2N4923	0-83	BC135	-0-11	BF121	-0-25	MJE340	0-42
2N1907	5-50	2N5172	0-12	BC138	0-15	BF123	0-27	MJE2955	1-12
2N2102	0-50	2N5174	0-22	BC137	0-15	BF125	0-25	MJE3055	0-88
2N2147	0-70	2N5175	0-26	BC138	0-24	BF152	0-20	MP8111	0-32
2N2148	0-94	2N5176	0-32	BC141	0-34	BF153	0-32	MP8113	0-47
2N2160	0-60	2N5190	0-32	BC141	0-34	BF153	0-32	MP8112	0-40
2N2192	0-40	2N5191	0-95	BC142	0-23	BF158	0-23	MP1102	0-39
2N2192A	0-40	2N5192	1-24	BC143	0-21	BF159	0-27	MPSA05	0-25
2N2193	0-40	2N5195	1-46	BC145	0-21	BF160	0-23	MPSA06	0-26
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2N2194A	0-73	2N5257	0-49	BC148	0-13	BF163	0-32	MPSA58	0-27
2N2194B	0-30	2N5458	0-43	BC149	0-42	BF165	0-30	NE555V	0-96
2N2194C	0-60	2N5459	0-49	BC153	0-18	BF167	0-21	NE560	4-48
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2N2219A	0-60	40362	0-50	BC157	0-14	BF177	0-29	NE565A	4-48
2N2220	0-45	40363	0-61	BC158	0-13	BF178	0-35	OC23	2-56
2N2221	0-40	40334	0-56	BC160	0-14	BF179	0-43	OC28	0-78
2N2221A	0-40	40395	0-65	BC167B	0-13	BF181	0-34	OC35	0-80
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2N2368	0-31	40407	0-33	BC168C	0-11	BF183	0-40	OC71	0-12
2N2369	0-37	40408	0-50	BC169B	0-13	BF184	0-38	OC72	0-13
2N2369A	0-41	40409	0-47	BC170	0-13	BF185	0-17	OC81	0-26
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2N2905A	0-56	40601	0-67	BC183	0-09	BF199	0-18	SC41D	1-32
2N2906	0-31	40602	0-53	BC184	0-11	BF225J	0-40	SC45D	1-89
2N2906A	0-37	40603	0-53	BC184	0-11	BF225J	0-40	SC46D	1-98
2N2907	0-40	40604	0-56	BC184L	0-11	BF237	0-22	SC50D	2-30
2N2907A	0-45	40636	1-10	BC186	0-25	BF238	0-22	SC51D	2-69
2N2924	0-14	40669	1-90	BC187	0-27	BF244	0-16	SL414A	1-80
2N2925	0-11	40673	0-12	BF245	0-12	BF246	0-33	SL623	0-59
2N3053	0-32	AC1107	0-25	BC208	0-11	BF246	0-43	TA A263	0-10
2N3054	0-60	AC113	0-16	BC212K	0-10	BF247	0-23	TA A350	2-10
2N3055	0-75	AC117	0-20	BC212L	0-16	BF254	0-16	TA A621	2-03
2N13390	0-28	AC126	0-25	BC214L	0-21	BF255	0-17	TA A661B1	3-20
2N3391	0-23	AC127	0-25	BC237	0-09	BF257	0-46	TAD100	1-50
2N3391A	0-29	AC128	0-25	BC238	0-06	BF259	0-59	Filler	0-25
2N3392	0-13	AC151V	0-14	BC239	0-09	BF259	0-59	TA A271	0-64
2N13393	0-13	AC152V	0-17	BC281	0-20	BF251A	2-30	TBA641B	2-25
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2N3402	0-18	AC153K	0-25	BC253	0-23	BF561	0-27	TBA810	1-50
2N3403	0-18	AC154	0-20	BC257	0-09	BF598	0-29	TIL209	0-35
2N3440	0-16	AC176	0-18	BC258	0-06	BF599	0-30	TIP29A	0-49
2N3441	0-97	AC176K	0-25	BC259	0-13	BF630	0-25	TIP30A	0-58
2N3442	1-69	AC187K	0-23	BC261	0-20	BF44X	2-33	TIP31A	0-82
2N3414	0-10	AC188K	0-34	BC262	0-18	BF633	2-48	TIP32A	0-74
2N3415	0-10	AC189	0-24	BC263	0-23	BF638	0-30	TIP33A	1-01
2N3416	0-16	AC191	0-27	BC300	0-12	BF638	0-24	TIP34A	1-51
2N3417	0-21	AC192	0-32	BC301	0-34	BF639	0-20	TIP34A	1-51
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2N3641	0-17	AD142	0-50	BC307A	0-10	BFY18	0-35	TIP42A	0-90
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2N3703	0-12	AD150V	0-45	BC309A	0-10	BFY20	0-35	TIP305S	0-60
2N3704	0-14	AD150	0-53	BC308B	0-09	BFY29	0-29	TIP305S	0-60
2N3705	0-12	AD161	0-45	BC309	0-10	BFY50	0-23	TX300	0-12
2N3706	0-09	AD162	0-45	BC309A	0-10	BFY51	0-19	TX302	0-20
2N3707	0-13	AD161	pr	BC309B	0-10	BFY52	0-21	TX500	0-15
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