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by Tom Duncan

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Adventures With Electronics. £1-75.

Component Pack £16-72 less battery.

## ADVENTURES WITH MICROELECTRONICS

Same style as above book; 11 projects based on integrated circuits—includes: dice, two-tone doorbell, electronic organ, MW/LW radio, reaction timer, etc. Component pack includes a Bimboard, 1 plug-in breadboard and the components for the projects.

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## DOING IT DIGITALLY

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KIT: £18-97. Headphones extra £3-28.

## TEACH - IN - 80

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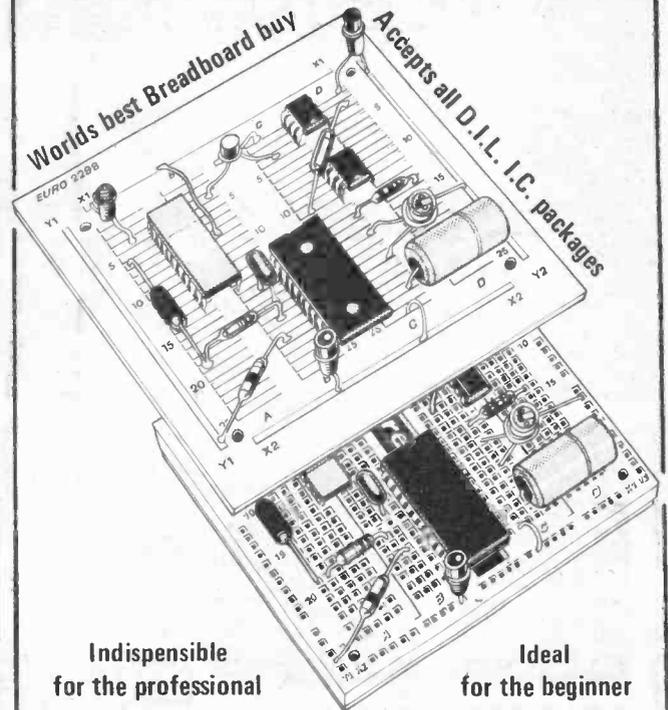
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You've seen the reviews...you've heard the excitement...now make the kit!

This is the ZX80. 'Personal Computer World' gave it 5 stars for 'excellent value.' Benchmark tests say it's faster than all previous personal computers. And the response from kit enthusiasts has been tremendous.

To help you appreciate its value, the price is shown above with and without VAT. This is so you can compare the ZX80 with competitive kits that don't appear with inclusive prices.

### 'Excellent value' indeed!

For just £79.95 (including VAT and p&p) you get everything you need to build a personal computer at home...PCB, with IC sockets for all ICs; case; leads for direct connection to a cassette recorder and television (black and white or colour); everything!

Yet the ZX80 really is a complete, powerful, full-facility computer, matching or surpassing other personal computers at several times the price.

The ZX80 is programmed in BASIC, the world's most popular computer language for beginners and experts alike.

The ZX80 is pleasantly straightforward to assemble, using a fine-tipped soldering iron. It immediately proves what a good job you've done; connect it to your TV...link it to an appropriate power source\*...and you're ready to go.

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- Printed circuit board, with IC sockets for all ICs.
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The unique Sinclair BASIC interpreter offers remarkable programming advantages:

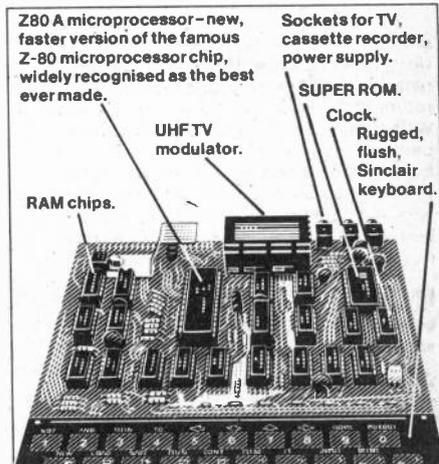
- **Unique 'one-touch' key word entry: the ZX80 eliminates a great deal of tiresome typing. Key words (RUN, PRINT, LIST, etc.) have their own single-key entry.**
- Unique syntax check. Only lines with correct syntax are accepted into programs. A cursor identifies errors immediately. This prevents entry of long and complicated programs with faults only discovered when you try to run them.
- Excellent string-handling capability—takes up to 26 string variables of any length. All strings can undergo all relational tests (e.g. comparison). The ZX80 also has string input to request a line of text when necessary. Strings do *not* need to be dimensioned.
- Up to 26 single dimension arrays.
- FOR/NEXT loops nested up to 26.
- Variable names of any length.
- BASIC language also handles full Boolean arithmetic, conditional expressions, etc.
- Exceptionally powerful edit facilities, allows modification of existing program lines.
- Randomise function, useful for games and secret codes, as well as more serious applications.
- Timer under program control.
- PEEK and POKE enable entry of machine code instructions. USR causes jump to a user's machine language sub-routine.
- High-resolution graphics with 22 standard graphic symbols.
- All characters printable in reverse under program control.
- Lines of unlimited length.

### Fewer chips, compact design, volume production—more power per pound!

The ZX80 owes its remarkable low price to its remarkable design: the whole system is packed on to fewer, newer, more powerful and advanced LSI chips. A single SUPER ROM, for instance, contains the BASIC interpreter, the character set, operating system, and monitor. And the ZX80's 1K byte RAM is roughly equivalent to 4K bytes in a conventional computer—typically storing 100 lines of BASIC. (Key words occupy only a single byte.)

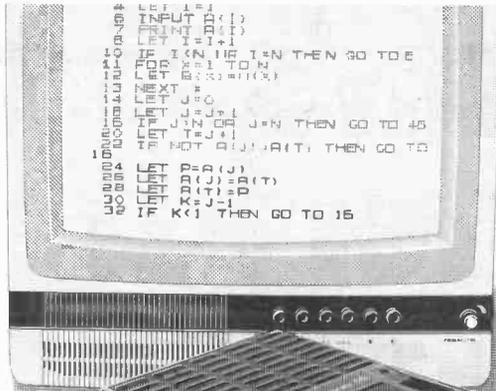
The display shows 32 characters by 24 lines. And Benchmark tests show that the ZX80 is faster than all other personal computers.

No other personal computer offers this unique combination of high capability and low price.



Everyday Electronics, October 1980

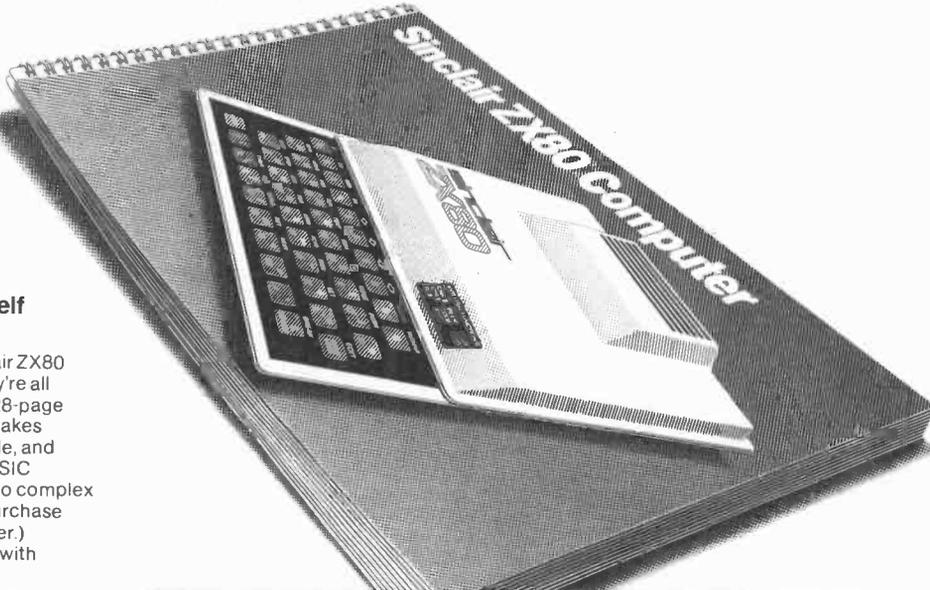
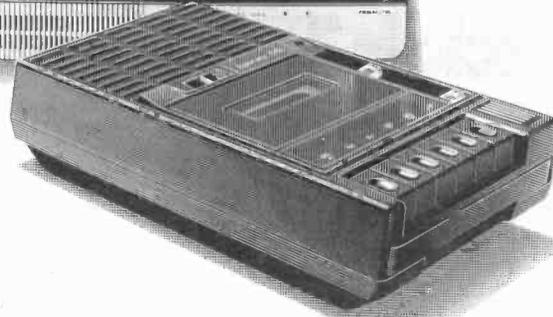
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See advertisements in Personal Computer World, Electronics Today International, and other journals.

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# sinclair

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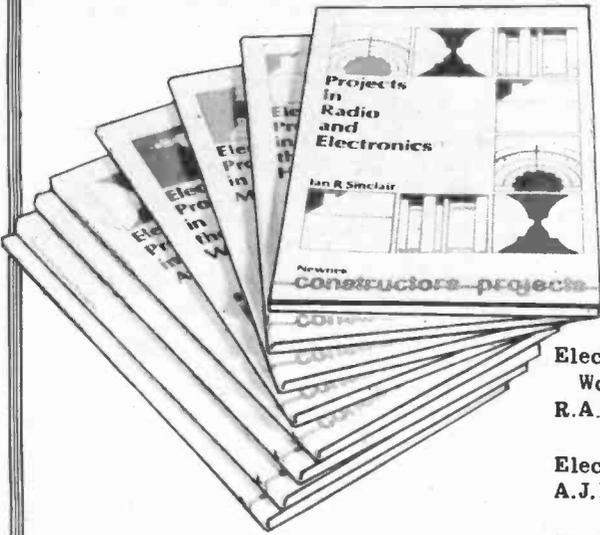
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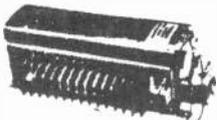
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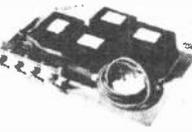
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## 6 WAVE BAND SHORT WAVE RADIO KIT

Bandsread covering 13.5 to 52 metres. Based on circuit which appeared in a recent issue of Radio Constructor. Complete kit, includes case materials, six transistors and diodes, condensers, resistors, inductors, switches, etc. Nothing else to buy, if you have an amplifier to connect it to or a pair of high resistance headphones. Special price to get this kit off the ground, is **£11.95** inc VAT and postage.

## 3" EDGEWISE PANEL METER

0-25 MA moving coil made for the G.P.O. A very useful instrument especially when panel space is limited. **£2.50** + 38p.

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Japanese made full vision perspex front, flush mounting. Price **£3** + 45p.

## 12v SUBMERSIBLE PUMP

Our drill pump is useful, but this new one is even more so. Just join to your car battery, drop it into the liquid to be moved and up it comes, no messing about, no priming, etc. and you get a very good head. Suitable for water, paraffin and any non-explosive, non-corrosive liquid. One use if you are a camper, make yourself a shower. Price **£6** + 80p. A free gift, first 100 purchasers will get tap with built in switch and length of plastic tubing.

**E.H.T. MAINS TRANSFORMER** with inductance control, normal primary, secondary output by our equipment, 3-5 kv, 3 mA. E.H.T. voltage can be varied by applying a DC voltage to the lower normally unused bobbin. We are not sure how much the voltage may be increased or decreased but using a 9 volt battery we seem to get a rise or fall of about 50 volts. Ex unused P.S.U.'s. Price **£2** + 30p. Post 40p.

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All the parts to make up the beginners model. Price **£2** + 30p. Crystal earpiece 57p + 8p. High resistance headphones (give best results) **£3.25** + 50p. Kit includes chassis and front but not case.

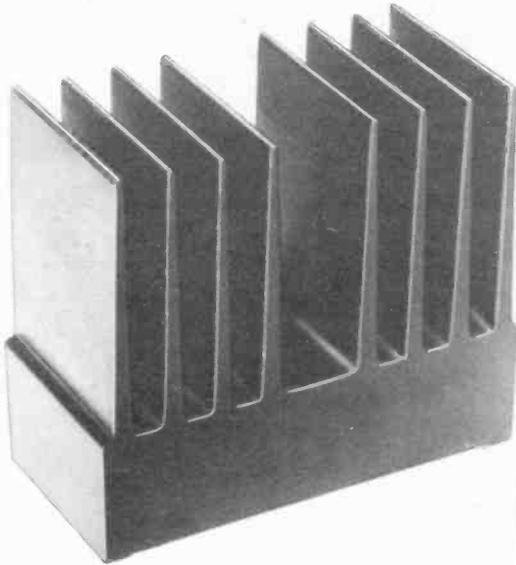
## RADIO STETHOSCOPE

Easy way to fault find—start at the aerial and work towards the speaker—when signal stops you have found the fault. Complete kit **£4.25** + 65p.

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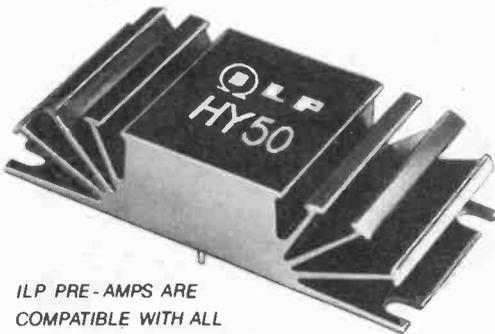
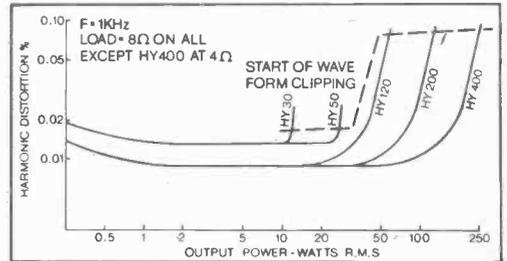
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ILP POWER AMPS AND PSUs

Model	Output Power R.M.S.	Distortion Typical at 1KHz	Minimum Signal/Noise Ratio	Power Supply Voltage	Size in mm	Weight in gms	Price + V.A.T.
HY30	15 W into 8 Ω	0.02%	100dB	-20 -0 +20	105x50x25	155	£6.34 + 95p
HY50	30 W into 8 Ω	0.02%	100 dB	-25 -0 +25	105x50x25	155	£7.24 + £1.09
HY120	60 W into 8 Ω	0.01%	100 dB	-35 -0 +35	114x50x85	575	£15.20 + £2.28
HY200	120 W into 8 Ω	0.01%	100 dB	-45 -0 +45	114x50x85	575	£18.44 + £2.77
HY400	240 W into 4 Ω	0.01%	100 dB	-45 -0 +45	114x100x85	1.15Kg	£27.68 + £4.15

Load impedance - all models 4 Ω - ∞  
Input sensitivity - all models 500 mV  
Input impedance - all models 100K Ω  
Frequency response - all models 10Hz - 45 KHz - 3dB

## POWER SUPPLY UNITS



ILP Power Supply Units with transformers made in our own factory are designed specifically for use with ILP power amplifiers and are in two basic forms - one with circuit panel mounted on conventionally styled laminated transformer, for smaller PSU's - in the other, for larger PSU's, ILP toroidal transformers are used which are half the size and weight of laminated equivalents, are more efficient and have greatly reduced radiation.

PSU 30 ± 15V at 100mA to drive up to 12 x HY6 or 6 x HY6i6] £4.50 + £0.68 VAT

THE FOLLOWING WILL ALSO DRIVE ILP PRE-AMPS

PSU 36 for 1 or 2 HY30's £8.10 + £1.22 VAT

PSU 50 for 1 or 2 HY50's £8.10 + £1.22 VAT

PSU 60 with toroidal transformer for 1 HY 120 £9.75 + £1.46 VAT

PSU 70 with toroidal transformer for 1 or 2 HY120's £13.61 + £2.04 VAT

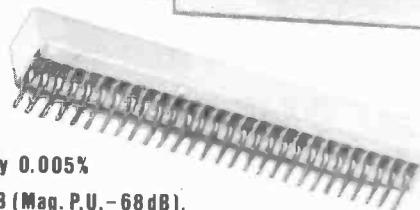
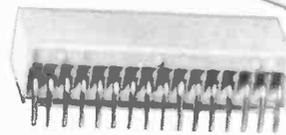
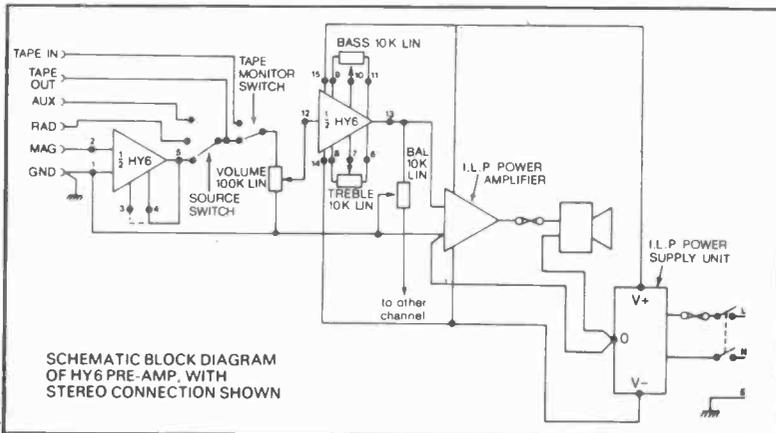
PSU 90 with toroidal transformer for 1 HY200 £13.61 + £2.04 VAT

PSU 180 with toroidal transformer for 1 HY400 or 2 x HY200 £23.02 + £3.45 VAT



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**HY6** mono  
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**HY66** stereo  
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Connectors included

B6 Mounting Board  
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B66 Mounting Board  
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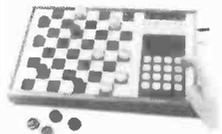


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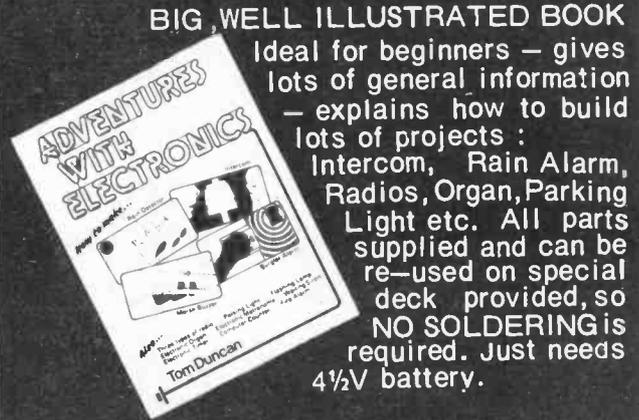
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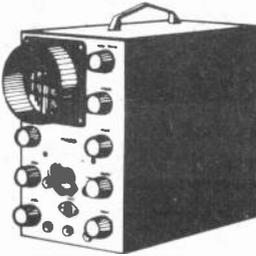
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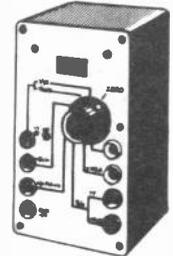
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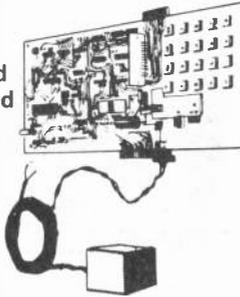
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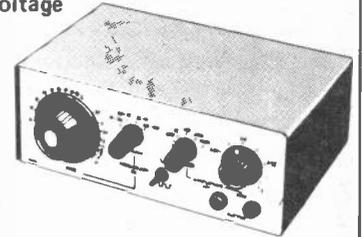
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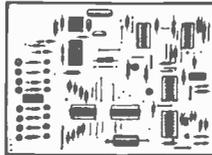


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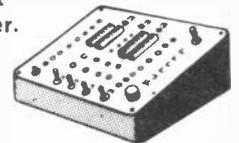
Note:— for full benefit with this kit a C.R.O. is desirable although circuits can be built without one.



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## LK6 LOGIC DEMONSTRATION PANEL

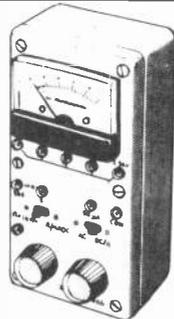
Basic introduction to computer technology; AND and OR gates; NOR and NAND; Data line selector; Truth tables; AND and INVERT gate; Half and Full Adder; Latches; Flip-Flops; Shift register; Binary coded decimal counter. Over 16 experiments are performed with panel. Battery operated.



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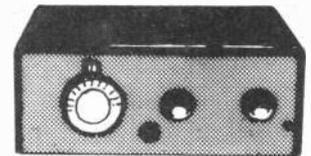
Basic multi range test meter kit with 20,000 ohm/volt sensitivity. Ranges: D.C. and A.C. volts 0-5, 0-25, 0-100, 0-500; 2.5kV. D.C. 0-5mA, 0-500mA, 0-50 $\mu$ A Resistance 0-50K; 0-5M. Size 150 x 75 x 50mm.



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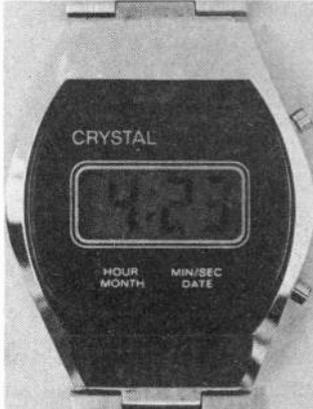
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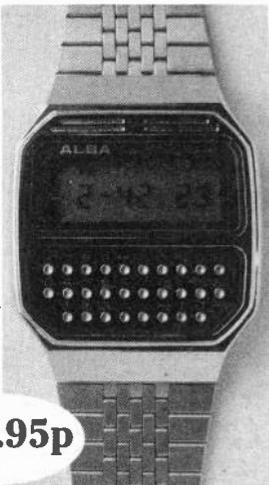
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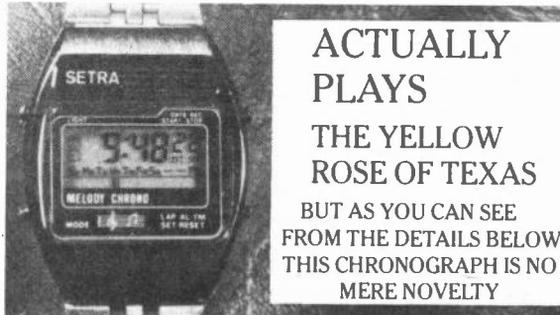


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HEF4017	57	HEF4066	62	HEF4532	150	LM381AN	198	2N2646	46	BC548	11	
HEF4014	105	HEF4067	475	HEF4534	638	LM3900N	75	2N2926G	13	BC549	12	
HEF4016	57	HEF4068	22	HEF4539	138	MC3403P	156	2N3053	19	BC557	15	
HEF4017	100	HEF4069	22	HEF4585	122	NE531	131	2N3054	55	BC558	15	
HEF4018	100	HEF4070	22	HEF4724	214	NE536T	250	2N3055	55	BCY70	15	
HEF4019	58	HEF4071	23	HEF4097	113	NE555M	20	2N3702	9	BCY71	15	
HEF4020	112	HEF4072	23	HEF4098	92	NE568N	86	2N3704	9	BD131	39	
HEF4021	107	HEF4073	23	HEF4106	78	NE568N	171	2N3705	10	BD132	39	
HEF4022	103	HEF4076	130	HEF4160	149	NE570N	485	2N3773	297	BD139	39	
HEF4023	22	HEF4077	22	HEF4192	149	NE571N	505	2N3819	22	BD140	39	
HEF4024	74	HEF4078	23	<b>Voltage Regulators</b>				RC4136	148	2N3850	39	
HEF4025	22	HEF4081	23	Dipped Type, C280/352 Style				TC136	148	2N3850	39	
HEF4026	244	HEF4082	23	Moulded Type, 10.2mm Pitch				TD1022	713	2N6457	39	
HEF4027	57	HEF4085	80	LM3800AIK1				119	TD1034B	239	2N6459	35
HEF4028	89	HEF4086	80	LM3800AIK2				119	TL081C	84	BFY59	50
HEF4029	113	HEF4093	63	UA723CN				42	TL084CN	156	BC107	14
HEF4030	58	HEF4094	219	UA7815CU				78	UA741CN	20	BC108	14
HEF4031	250	HEF4104	206	UA7815CU				78	UA741CT	47	BC109	18
HEF4033	138	HEF4502	114	Zener Diodes				BC109	14	BC109	18	
HEF4040	107	HEF4505	714	400mW CV7-C33				BC109B	19	TIP41C	54	
HEF4041	94	HEF4508	230	8Y288/BZ X79				BC109C	20	TIP242C	76	
HEF4042	83	HEF4510	135	+ Voltage				BC148	10	TIP2955	75	
HEF4043	100	HEF4511	157					BC158	10	TIP3055	60	
								BC177	17	TIP543	36	

**GMT SELL PA EQPT.** PLEASE SEND AN SAE FOR DETAILS

CAPACITORS				Electrolytic Axial				Polyester Radial Leads				Electrolytic Radial Leads				
-10% to +50% Tol.				Order Code	Cap 352				Cap 350				Cap 354			
10F V 18 26 40 63				Order Code	Dipped Type, C280/352 Style				Dipped Type, C280/352 Style				Dipped Type, C280/352 Style			
1.0				1.0	Moulded Type, 10.2mm Pitch				Moulded Type, 10.2mm Pitch				Moulded Type, 10.2mm Pitch			
1.8				1.8	352 300				352 300				352 300			
2.2				2.2	.001				.001				.001			
3.3				3.3	.0015				.0015				.0015			
4.7				4.7	.0022				.0022				.0022			
6.8				6.8	.0033				.0033				.0033			
10				10	.0047				.0047				.0047			
15				15	.0068				.0068				.0068			
22				22	.01				.01				.01			
33				33	.015				.015				.015			
47				47	.022				.022				.022			
68				68	.033				.033				.033			
100				100	.047				.047				.047			
150				150	.068				.068				.068			
220				220												
330				330												
470				470												
880				880												
1000				1000												
1500				1500												
2200				2200												

RESISTORS				Carbon Film, Fixed				Metal Film, Fixed				Metal Glaze, Fixed			
0.25W, E24 Values, 10R-10M, 5% Tol.				0.5W, E24 Values, 10R-10M, 5% Tol.				0.5W, E24 Values, 10R-10M, 5% Tol.				0.5W, E24 Values, 10R-10M, 5% Tol.			
2 each Res RD4				8 each Res MR30				8 each Res MR30				16 each Res VR37			
100/100 (Mult 10/Value)				16 each Res PR52				16 each Res PR52				16 each Res VR37			
0.5W, E12 Values, 10R-4M7, 10% Tol.				16 each Res PR52				16 each Res PR52				16 each Res VR37			

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MAINS TRANSFORMERS				Plastic Boxes - Best Industrial Mouldings				Diectest Boxes			
Secondaries may be connected in series or parallel to give wide voltage range				Moulded Box and Close Fitting Flanged Lid				Decast Box and Flanged Lid			
Primaries 0.220, 240V				ABS Box, CW Brass Bushes, and Lid in Orange				Aluminium Box and Lid in Natural Finish			
BVA - Clamp Type Construction				L112 W82 D31				L113 W83 D31			
Approx 18% Regulation F C 54, W36, W35				L150 W80 D50				L152 W82 D50			
0.4-5V, 0.4-5V Secondaries				L190 W110 D80				L192 W113 D81			
0.5V, 0.6V				Plastic Boxes with Metal Lids				200-21089J			
0.12V, 0.12V				Recessed Top Box				200-21072D			
0.15V, 0.15V				ABS Base, CW Brass Bushes, in Orange				200-21078C			
0.20V, 0.20V				1mm Aluminium Top Panel Finished Grey				200-21078H			
20VA - Clamp Type Construction				L85 W58 D29				200-21084E			
Approx 18% Regulation F C 70, H48, W46				L111 W71 D42				203-21013A			
0.4-5V, 0.4-5V Secondaries				L81 W58 D53				203-21015F			
0.5V, 0.6V				Diectest Boxes				200-21087G			
0.12V, 0.12V				Decast Box and Flanged Lid				200-21017H			
0.15V, 0.15V				Aluminium Box and Lid in Natural Finish				200-21341D			
0.175V, 0.175V								200-21339F			
0.20V, 0.20V								200-21340G			

G.M.T. ELECTRONICS KITS				F.E.I. POWER AMPLIFIER OUTPUT MODULE KIT			
FIXAL TELETEXT KIT				ONE AMP POWER SUPPLY MODULE KIT - FIVE VOLTS			
TELETEXT DECODER + REMOTE CONTROL KIT				ONE AMP POWER SUPPLY MODULE KIT - TWELVE VOLTS			
PAL ENCODER/MODULATOR KIT				MODEL INERTIA CONTROLLER MK I - SLOT RACKER			
DOPPLER RADAR ALARM KIT				MODEL INERTIA CONTROLLER MK II - TRAIN (HAND UNIT)			
				MODEL INERTIA CONTROLLER MK III - TRAIN (CONSOLE UNIT)			

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AUTOFADE	(ZB66)	May 80	£10-25
VARICAP RADIO	(ZB1)	Sept 79	£8-50
TRANSISTOR TESTER	(ZB2)	Sept 79	£5-00
4-STATION RADIO (No Case)	(ZB22)	May 80	£14-00
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OPTO ALARM	(ZB41)	Nov 79	£8-00
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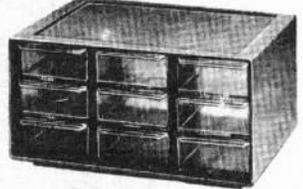
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180V: 39pF, 100n, 150n, 220n 11p; 330n, 470n 18p; 680n, 1 $\mu F$  22p; 1 $\mu 5$ , 2 $\mu 2$  32p; 4 $\mu 7$  36p.  
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**TAG-END TYPE:** 450V: 100 $\mu F$  180p; 70V: 4700 165p; 64V: 3300 150p; 2500 110p; 50V: 3300 135p; 2200 99p; 40V: 4700 130p; 4000 92p; 3300 85p; 2500, 2200 80p; 2000 + 2000 120p; 30V: 4700 110p; 25V: 15000 195p; 6400 120p; 4700 100p; 3000 85p; 2200 60p.

**TANTALUM Bead Capacitors**  
35V: 0.1 $\mu F$ , 0.22, 0.33, 0.47, 0.68, 1.0, 2.2, 3.3, 4.7, 25V: 10, 20, 22p; 6.8, 15V: 2.2, 4.7, 10, 20p; 15V: 22 $\mu$  32p; 100 58p; 220 70p; 10V: 15, 22, 33, 30p, 3V: 100 32p.

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100V: 0.001, 0.002, 0.005, 0.01 $\mu F$  7p  
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0.1 $\mu F$  8p 50V: 0.47 12p

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2.5-8pF, 3-10pF, 10-40pF 22p  
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5V 7805 145p 7905 220p  
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18V 7818 145p  
1A TO220 Plastic Casing  
5V 7805 80p 7905 85p  
12V 7812 80p 7912 85p  
15V 7815 80p 7915 85p  
18V 7818 80p 7918 85p  
24V 7824 80p 7924 85p  
100mA TO92 Plastic Casing  
5V 78L05 30p 79L05 85p  
6V 78L06 30p  
8V 78L08 30p  
12V 78L12 30p 79L12 85p  
15V 78L15 30p 79L15 85p  
CA3085 95 LM325N 240 TDA1412 150  
LM3001H 170 LM327N 240 78H05+5V/5A 595  
LM309H 140 LM327N 240 78H05+5V/5A 595  
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6.1/36.1 775p 25 50 pF 250p  
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"DP" VALVE TYPE RFC 5  
Range 1 to 5 Bl., RFC7 (19mH) 133p  
Rd., V. Whl. 106p RFC 13, 14, 15;  
6-7 B.Y.R. 95p 16; 17 110p  
1.5 Green 130p IFT 18/1-6 116p  
'T' 1 to 5 Bl., V.I., IFT 18/465 132p  
Rd., Wht. 130p TOC 1 110p  
B9A Valve Holder MW5F 112p  
35p MW/LW5FR 134p

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2 $\frac{1}{2}$  x 3 $\frac{1}{2}$  66p 59p 34p  
2 $\frac{1}{2}$  x 5 75p 69p  
2 $\frac{1}{2}$  x 7 86p 92p 65p  
2 $\frac{1}{2}$  x 11 296p 260p 178p  
4 $\frac{1}{2}$  x 17 387p 280p  
Pkt of 35 pins 20p  
Spot face cutter 107p  
Pin insertion tool 147p

**DIODES**  
A A129 25 Range 2V7 to 39V  
BA100 25 39V 400mW  
BY126 12 12 8p each  
BY127 12 Range 3V3 to 33V, 1-3W  
CRO33 158 15p each  
OA 48  
OA47 18  
OA70 12  
OA71 12  
OA81 18  
OA85 15  
OA90 8  
OA91 8  
OA95 8 (plastic case)  
OA200 4 1A/50V 20  
OA202 0 1A/100V 22  
IN914 4 1A/200V 25  
IN916 5 1A/400V 29  
IN4001/2 5 1A/600V 34  
IN4003 8 1A/50V 35  
IN4004/5 6 2A/50V 35  
IN4006/7 7 2A/100V 44  
IS44 20 2A/200V 46  
3A/100V 18  
3A/400V 20 2A/600V 85  
3A/600V 27 4A/800V 120  
3A/1000 30 6A/100V 73  
6A/200V 78  
6A/400V 85  
12A/100V 60  
12A/200V 70  
12A/400V 80  
12A/600V 95  
12A/800V 130  
16A/100V 95  
16A/200V 104  
16A/500V 158  
25A/800V 295  
25A/1000V 48  
T2800MD 120

**ZENERS**  
Range 2V7 to 39V 400mW  
Range 3V3 to 33V, 1-3W  
15p each  
NOISE  
ZSJ 180

**BRIDGE RECTIFIERS**  
(plastic case)  
1A/50V 20  
1A/100V 22  
1A/200V 25  
1A/400V 29  
1A/600V 34  
2A/50V 35  
2A/100V 44  
2A/200V 46  
2A/400V 53  
2A/600V 85  
2A/800V 120  
4A/800V 120  
6A/100V 73  
6A/200V 78  
6A/400V 85  
12A/100V 60  
12A/200V 70  
12A/400V 80  
12A/600V 95  
12A/800V 130  
16A/100V 95  
16A/200V 104  
16A/500V 158  
25A/800V 295  
25A/1000V 48  
T2800MD 120

**TRIACS**  
3A100V 48  
3A200V 49  
3A400V 54  
6A100V 54  
8A100V 54  
8A200V 54  
8A400V 64  
8A600V 68  
12A100V 60  
12A200V 70  
12A400V 80  
12A600V 95  
16A100V 95  
16A200V 104  
16A500V 158  
25A800V 295  
25A1000V 48  
T2800MD 120

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TTL 74	74126	55 LS54	30 LS873	750	4095	105	ICM7217A	796
	74128	74 LS55	30 LS874	850	4095	105	ICM7555	890
	7401	12 74132	70 LS63		4097	350	LD10	452
	7402	12 74136	85 LS73	40	4098	115	LF356	390
	7403	14 74141	85 LS74	48	4099	190	LM10	190
	7404	14 74142	195 LS75	48	4100	125	LM300H	170
	7405	18 74143	350 LS76	45	4102	24	LM301A	23
	7406	48 74144	350 LS77	45	4106	125	LM308	70
	7407	48 74145	40 LS83	105	4107	22	LM318	185
	7408	22 74147	180 LS85	105	4108	82	LM324	180
	7409	22 74148	145 LS86	45	4109	40	LM339	48
	7410	10 74150	150 LS90	50	4110	48	LM348	80
	7411	25 74151	75 LS91	125	4111	24	LM380	80
	7412	20 74153	75 LS92	75	4112	24	LM381	143
	7413	14 74154	140 LS93	75	4113	45	LM382	123
	7414	62 74155	75 LS95	118	4114	85	LM458	40
	7415	31 74156	80 LS96	180	4115	85	LM459	60
	7417	31 74157	75 LS107	45	4116	42	LM390N	75
	7420	10 74159	185 LS109	75	4117	82	LM391	120
	7421	38 74160	99 LS112	80	4118	88	LM391A	240
	7422	28 74161	99 LS113	85	4119	48	LM391S	240
	7423	22 74162	99 LS114	48	4120	90	M23A A	143
	7425	30 74163	99 LS115	48	4121	105	MC1310	780
	7426	44 74164	120 LS124	180	4122	95	MC1312P	190
	7427	32 74165	120 LS125	60	4123	25	MC1488	88
	7428	38 74166	153 LS126	60	4124	75	MC1489	90
	7430	20 74167	240 LS132	95	4125	25	MC1494	350
	7432	28 74170	230 LS133	30	4126	180	MC1495	595
	7433	30 74172	100 LS136	45	4127	48	MC1498	92
	7437	35 74173	120 LS138	60	4128	440	MC1710	76
	7438	30 74174	105 LS139	90	4129	105	MC3340P	620
	7440	20 74175	82 LS151	96	4130	60	MC3360P	120
	7441	74 74176	80 LS153	85	4131	225	MC3401	82
	7442	71 74177	90 LS155	96	4132	125	MC3403	135
	7443	120 74178	148 LS157	70	4133	128	MCFC040	67
	7444	160 74180	140 LS160	80	4134	210	MCFC040	878
	7445	110 74181	290 LS158	85	4135	125	MM50388	635
	7446	132 74182	280 LS161	85	4136	125	MM50388	635
	7447	99 74184	145 LS162	110	4137	115	NE518	210
	7448	99 74185	145 LS163	106	4138	110	NE543	210
	7450	20 74188	239 LS164	115	4139	360	NE544	185
	7451	20 74190	155 LS165	155	4140	105	NE555	22
	7452	20 74191	155 LS166	125	4141	80	NE555	35
	7454	20 74192	135 LS170	225	4142	80	NE555	35
	7456	20 74193	135 LS173	285	4143	105	NE555	325
	7470	41 74194	105 LS175	110	4144	85	NE562	410
	7472	31 74195	185 LS181	295	4145	175	NE564	433
	7473	40 74196	150 LS183	208	4146	130	NE565	128
	7474	34 74197	150 LS184	220	4147	80	NE565	188
	7475	56 74198	195 LS189	120	4148	120	NE565	188
	7476	41	LS190	120	4149	45	NE565	188
	7478	45	74LS	125	4150	48	NE565	188
	7480	120	LS200	135	4151	125	NE565	188
	7481	120	LS201	135	4152	125	NE565	188
	7482	64	LS202	135	4153	125	NE565	188
	7483	64	LS203	135	4154	125	NE565	188
	7484	121	LS204	135	4155	125	NE565	188
	7485	121	LS205	135	4156	125	NE565	188
	7486	121	LS206	135	4157	125	NE565	188
	7487	215	LS207	135	4158	125	NE565	188
	7488	57	LS208	135	4159	125	NE565	188
	7489	57	LS209	135	4160	125	NE565	188
	7490	57	LS210	135	4161	125	NE565	188
	7491	57	LS211	135	4162	125	NE565	188
	7492	57	LS212	135	4163	125	NE565	188
	7493	57	LS213	135	4164	125	NE565	188
	7494	57	LS214	135	4165	125	NE565	188
	7495	57	LS215	135	4166	125	NE565	188
	7496	57	LS216	135	4167	125	NE565	188
	7497	100	LS220	135	4168	125	NE565	188
	7498	100	LS221	135	4169	125	NE565	188
	7499	100	LS222	135	4170	125	NE565	188</

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# Projects... Theory... and Popular Features ...

The busiest season for constructors is now upon us and we open this new season with an eight-part series *I.C.s Explained*. The first four parts will be devoted to linear devices, the remaining four to digital i.c.s.

That's not all. As back-up, we are giving every reader a specially prepared chart *Guide To Popular Linear I.C.s*—free with this issue.

In general, electronics is becoming more and more to mean microelectronics. This is as evident in the constructor's field as elsewhere. The integrated circuit upon which microelectronics is based has risen to a position of paramount importance in designs for the home constructor. In quantity used, the i.c. already tends to be on parity with the transistor, which used to be the key active component in the average circuit.

Anyone who was building electronic circuits before the i.c. came on the scene will appreciate the tremendous changes this device has brought about during the course of the last decade. Electronic circuit design has been transformed—and greatly to the advantage of the constructor. An i.c. takes little more time and effort to solder in position than a transistor yet it introduces an increase in actual operational circuitry of 10 to 10,000 times, or even more, compared to that built around a single discrete transistor.

Integrated circuits are produced in great variety. They can be broadly

divided into two classes: linear and digital. They range from comparatively simple devices incorporating, for example, a single operational amplifier or a set of logic gates, right up to those large-scale integration devices such as microprocessors which form the heart of complete computing systems—and which have recently been caught in the glare of large-scale publicity as harbingers of a new technological and social revolution.

Many of the available integrated devices are of immediate interest and usefulness to the constructor. Our new series will identify some of the most important i.c.s and explain their functions and provide suggestions for their use in practical circuits.

Those who are unfamiliar with the integrated circuit (or microchip—to use one of the popular names for this device) are recommended to read first the scene-setting article *Introducing Microcircuits*. This will prepare the ground for our series *I.C.s Explained*.

We hope a large number of new recruits will "join-up" this autumn and so swell the ranks of electronics constructors. It's a grand hobby, and it keeps you up with the technological times!

*Fred Bennett*

Our November issue will be published on Friday, October 17. See page 645 for details.

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# ELECTRONICS

VOL. 9 NO. 9

OCTOBER 1980

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GUIDE TO POPULAR LINEAR I.C.s

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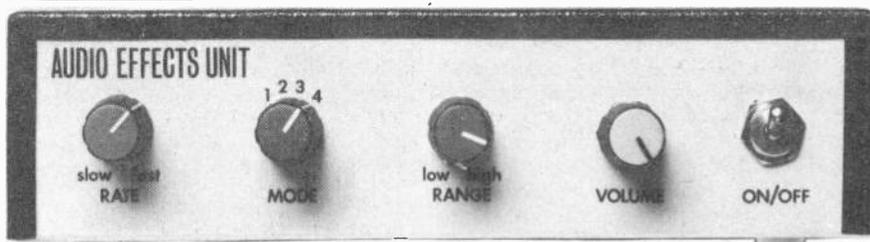
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THE RIGHT FORMULA  
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made easy

# audio EFFECTS UNIT

BY P. BAILEY



# FOR WEIRD SOUNDS

WITH THE ever increasing cost of commercially produced electronic sound effects units, it is becoming increasingly economical for the electronics hobbyist to construct his own.

The unit to be described basically reproduces siren tones, but with careful manipulation of the controls, it can produce a whole variety of sounds. It can be built for a fraction of the cost of a ready made unit, and could be of use in home movie-making, tape recording, plays and discos.

## OSCILLATOR PRINCIPLE

The circuit is based on the NE556 i.c. This is a "dual timer" i.c. and contains two NE555 timers in one 14

pin d.i.l. package. In this application both of these timers have been connected as astable multivibrators using basically the conventional circuit shown in Fig. 1, which shows the circuit for just one half of the 556.

When the power is first applied, capacitor  $C_T$  starts to charge up towards  $V_{CC}$  via  $R_A$  and  $R_B$ . This continues until the voltage on  $C_T$  reaches  $\frac{2}{3}V_{CC}$  at which point the threshold or, pin 2 senses this and switches on the discharge path, pin 1, which was formerly in a high state, to ground potential thus effectively grounding the junction between  $R_A$  and  $R_B$ . This allows  $C_T$  to discharge to ground via  $R_B$ . But when the voltage on  $C_T$  falls to  $\frac{1}{3}V_{CC}$  the trigger input, pin 6 senses this

and drives pin 1 high again, thus allowing  $C_T$  to charge up again towards  $\frac{2}{3}V_{CC}$  at which point the whole discharging process repeats itself. This charging/discharging of  $C_T$  will repeat *ad infinitum* with the  $C_T$  voltage varying between  $\frac{1}{3}$  and  $\frac{2}{3}V_{CC}$ .

Each time  $C_T$  is charged the output, pin 5, is driven high thus providing a pulse waveform. Thus by making  $R_B$  a variable resistor, and giving  $R_A$  and  $C_T$  set values, we have a variable frequency oscillator.

## MODULATING VOLTAGE

An additional feature of the NE556 is that the oscillation frequency can be varied using a control voltage. This is shown in Fig. 1 as a modulating voltage  $V_M$  being fed into the control voltage pin, pin 3. This varies the width of the output pulses, while leaving the spaces between them constant so effectively varying the frequency. The higher the voltage fed to pin 3 the lower the frequency.

So if we have an audio frequency oscillator and we use low frequency waveforms to modulate its pitch via its control voltage input, then we can produce a variety of siren type sounds; the particular siren type dependent on the modulating waveform's shape. This is the principle of the unit described below.

## CIRCUIT DESCRIPTION

The complete circuit diagram of the Audio Effects Unit is shown in Fig. 2. The low frequency oscillator is built around IC1a, half of the 556 i.c.  $C_1$  is the timing capacitor and is charged via  $R_2$  and  $R_3+VR_1$ . It is discharged via  $R_3+VR_1$ . The frequency range at the high end is limited by  $R_3$ , but the frequency range can still be varied from about 0.72Hz to about 12Hz.

The mode of operation is selected by  $S_1$  and this determines the shape and type of modulation signal sent to the audio oscillator. The switch positions are summarised as follows.

*Position 1:*  $S_{1a}$  is not connected to anything;  $S_{1b}$  is connected to the

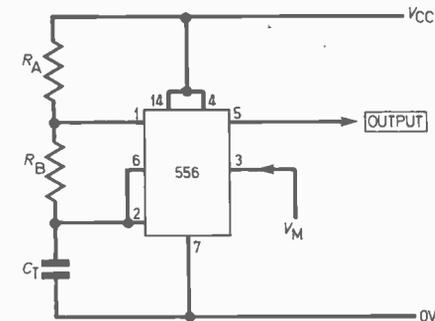


Fig. 1. Circuit diagram of basic astable multivibrators using one half of a 556 timer i.c.

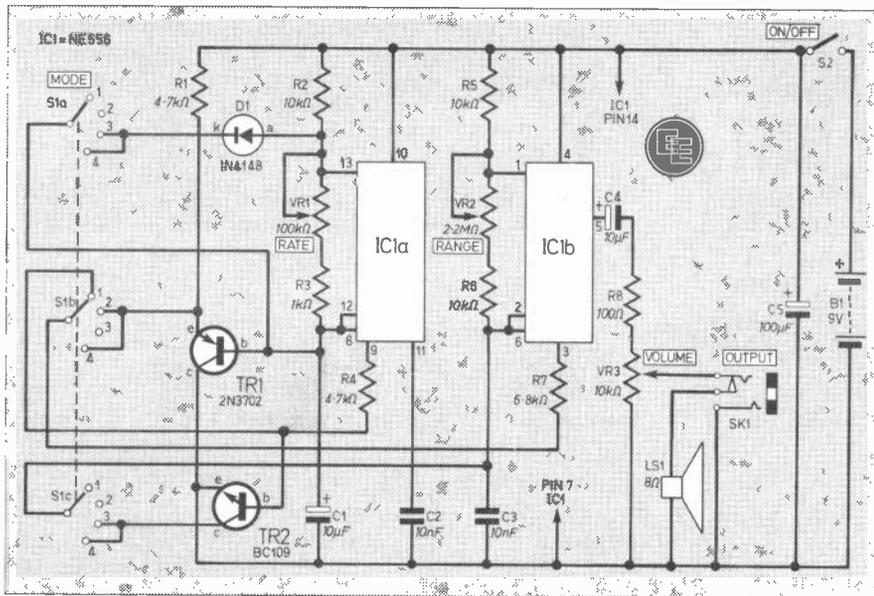


Fig. 2. Complete circuit diagram for the Audio Effects Unit.

low frequency oscillator output; S1c is not connected to anything. Thus a square wave is fed to the audio oscillator causing it to alternate between two tones.

**Position 2:** S1a is not connected to anything; S1b is connected to the emitter of TR1 which has been set up as an emitter follower (buffer) for the voltage on C1 so producing a ramp waveform that is the charge/discharge curve of C1; S1c is unconnected. Thus a roughly triangular wave is fed to the audio oscillator causing it to glide between two tones.

**Position 3:** S1a is connected to D1 which is thus connected across R3 and VR1. This has the effect of causing C1 to charge quickly via R2 and VR1; S1b is unconnected; S1c is connected to the collector of TR2. This is switched on and off by the low frequency oscillator output and so, since the output is a series of short pulses, TR2 switches the audio oscillator on and off by shorting out its timing capacitor for short intervals. Thus the audio oscillator produces a pulsed, steady tone.

**Position 4:** S1a is connected to D1 as before; S1b is connected to TR1 which in this case is producing a reverse sawtooth wave due to the action of D1 on the charging times; S1c is connected to TR2 as before so as to switch the audio oscillator off during the charging of C1. Thus the audio oscillator produces a tone which rises steadily, stops and then rises again starting from its original pitch.

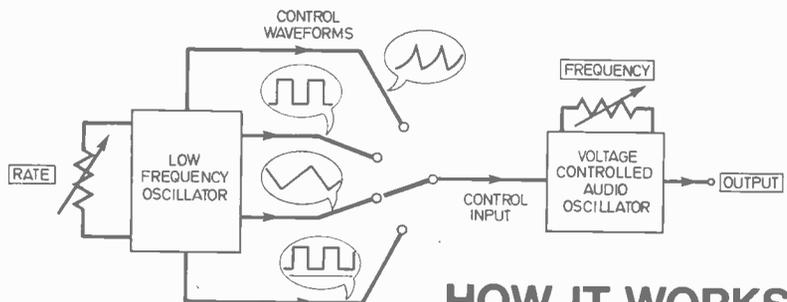
### AUDIO OSCILLATOR

The audio oscillator is built around IC1b section of the 556 and its frequency is variable via VR2 with R6 setting an upper limit.

This oscillator works in exactly the same way as the low frequency section described above, but has only one waveform, a square wave taken from its output at pin 5, and it can be manually adjusted over a frequency range of approximately 32Hz to 4kHz.

The purpose of R8 is to limit the current drawn from the output which although it can source or sink well over 100mA, can easily be damaged by a short across the output when VR3 is at full volume.

This resistor also allows the output to directly drive a miniature loudspeaker of virtually any impedance without damage. In the prototype an eight ohm miniature speaker was used but other values should work equally well.

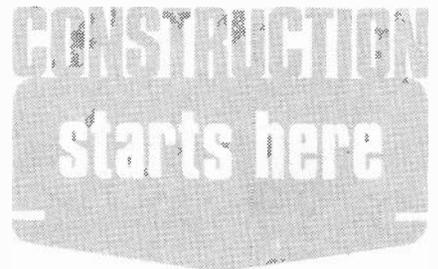


### HOW IT WORKS

A low frequency oscillator based round a simple timer i.c. produces square waves at frequencies between about 1Hz and 12Hz. These are processed to produce different control waveforms.

A second timer i.c. is wired to provide a voltage controlled audio oscillator and the waveforms derived from the first oscillator are fed to its control input to provide a wide range of special sound effects.

The output is via a switched jack socket and it has been arranged such that the internal speaker is normally on but is disconnected by the entry of a plug in the output socket. Either the socket or the speaker could be omitted if not required.



### CASE

The prototype unit was housed in a two-part metal case size 200×125×50mm which had a removable vinyl covered top which was held in place by two screws. This gave a pleasant, smart, compact appearance, but any other metal or plastic case would do just as well providing it had room for the battery and the speaker, if one is being used.

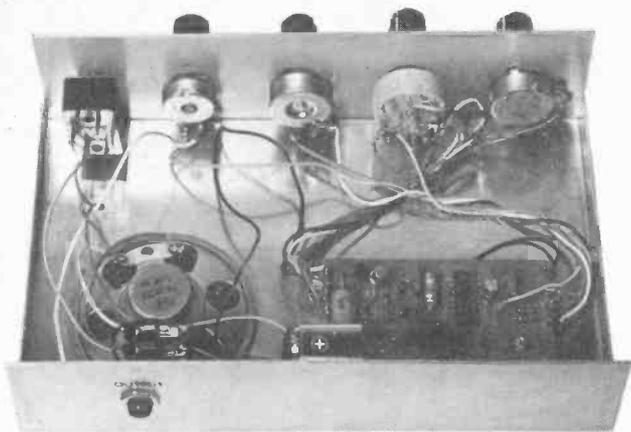
Four small self-adhesive feet or similar should be fixed to the underside of the case to stop it sliding about during use.

The case, once drilled, can be lettered using Letraset or similar rub-down lettering and then given a protective coat or two of clear varnish. The type sold in aerosols is ideal for this.

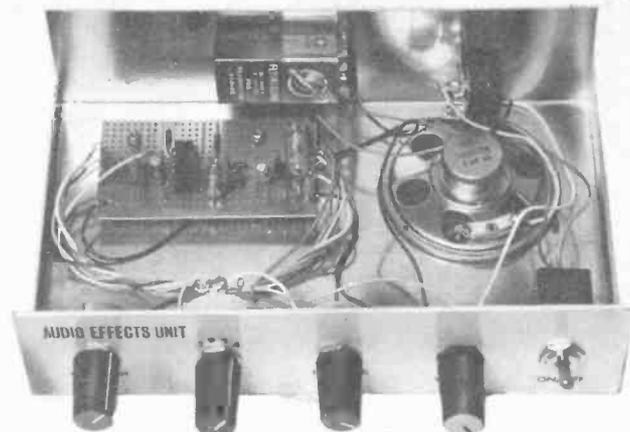
If a loudspeaker is fitted inside then it is advisable to drill holes in the case to allow the sound to escape.

### CIRCUIT BOARD

The majority of the components are mounted on a piece of 0.1 inch



Completed Audio Effects Unit showing wiring to front panel controls.



Finished unit with top cover removed showing suggested positioning of the battery, circuit board and loudspeaker.

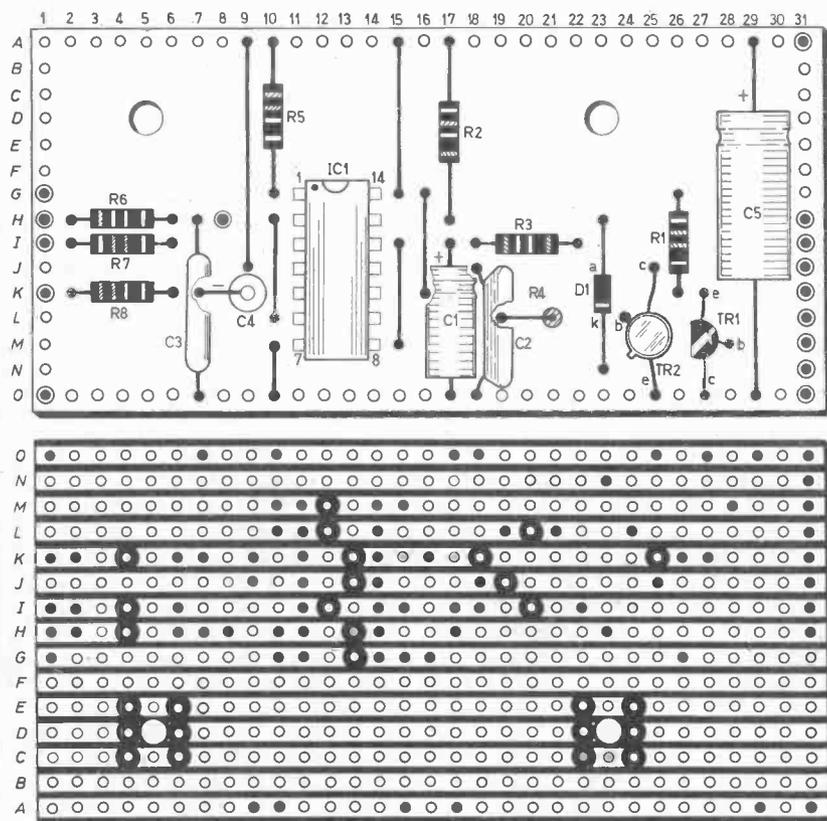


Fig. 3. Component layout on the stripboard together with details of breaks to be made along the copper strips on the underside of the board.

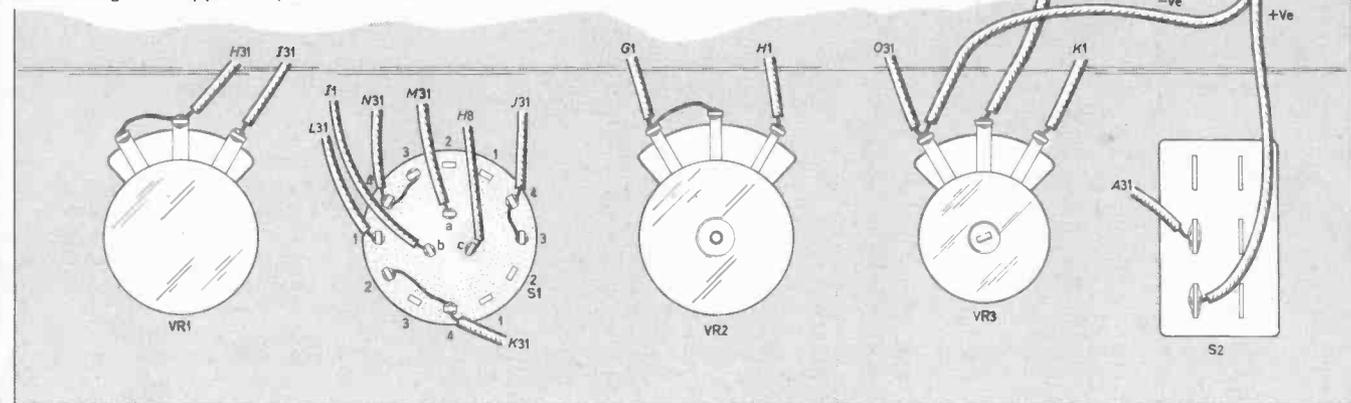
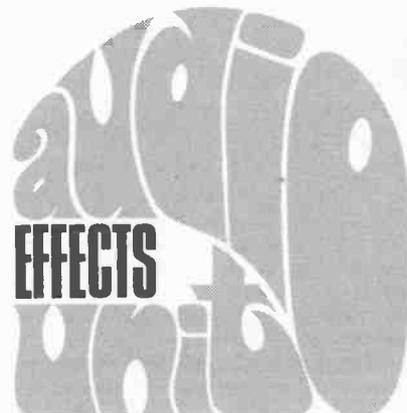


Fig. 4. Interwiring for the offboard components and wiring details to the circuit board.



matrix stripboard size 15 strips by 31 holes. There should be no constructional problems with the circuit board but be careful not to leave out any of the breaks in the copper strips.

The component layout and interwiring are shown in Figs. 3 and 4. First of all mount the resistors and capacitors then the diode and the two transistors. Although the i.c. is not of the delicate CMOS type a socket would be an advantage in easing replacement of the i.c. should this become necessary, and also it avoids the possibility of overheating during soldering.

Soldercon pins were used in the prototype but a 14 pin d.i.l. socket would do just as well. When soldering the diode and the transistors, care should be taken not to overheat them and it is recommended that a heat-shunt should be used.

### WIRING UP

To ease the job of connecting flying leads to the circuit board, single ended Veropins could be used and in this case the pin should be pushed through from the copper side so that its head comes up against the strip it is to be soldered to. After soldering the pin, the wire should be wrapped around it and then soldered in place.

The circuit board in the prototype was mounted on the base of the box

TABLE 1

Rate	CONTROL SETTING		SOUND PRODUCED
	Mode	Range	
Half-way	1	Half-way	British police siren
Minimum	2	Three-quarter-way	U.S.A. police siren
Maximum	2	Maximum	Canary
Quarter-way	3	Three-quarter-way	Heart beat monitor
Half-way	4	Three-quarter-way	"Star Trek" red alert

using 6BA bolts with nuts to suit, and 10mm plastic spacers.

Be careful when wiring up the rotary switch and follow the layout diagram in Fig. 4 to avoid confusion.

The speaker, if used, can be fitted in place using Araldite or a similar adhesive and applying it around the metal edge of the speaker, being careful not to get any on the cone.

The battery in the prototype was secured using a double-sided self-adhesive pad, but double-sided tape or a suitably bent metal strip could be used instead.

### TESTING AND USING

Check that all the components have been inserted the right way round especially the i.c. If all seems well, then with the RANGE and RATE controls at around mid-position, the MODE switch in position 1 and the

VOLUME control at maximum, switch on.

A two-tone sound should be clearly heard from the loudspeaker or amplifier (whichever is being used). If nothing can be heard switch off immediately and recheck all the wiring particularly the wiring to the VOLUME control because this may have been reversed. Check also to see if the battery is flat.

Assuming that the unit is working now turn the MODE switch to position 2. The sound should now waver about a steady pitch. If this is functioning correctly, modes 3 and 4 can be similarly checked; position 3 should give a beeping sound, and position 4 should give a whooping sound.

### IN USE

If these tests are successful then the unit is operating correctly and is ready for use. The unit has a wide range of applications as a sound-effects source since it can produce many different sounds.

Some control settings have been given in Table 1 for producing a small variety of effects and these can obviously be modified by experimentation with the controls. Note that to produce the canary effect the RANGE control should be moved quickly back and forward about a position near the maximum setting.

Finally, if a louder sound is desired than is obtained using the given component values then the value of R8 may be reduced providing that the total value of R8 plus the speaker impedance (with VR3 at maximum volume position) is kept above about 80 ohms.

This is to avoid drawing too much current from the output of IC1, since if this is done then permanent damage may occur.

Also, if any alteration to R8 is to be made, bear in mind that the louder the sound from the speaker, the more current there is being drawn from IC1, and consequently the more current is being drawn from the battery, and a larger battery may be required to give reasonable life.

With the component values shown, a PP3 battery and an 8 ohm speaker, the prototype provided a good volume and the battery lasted for many long periods of use.

## COMPONENTS



### Resistors

R1 4.7kΩ  
R2 10kΩ  
R3 1kΩ  
R4 4.7kΩ

All 1/4W carbon ± 5%

R5 10kΩ  
R6 1GkΩ  
R7 6.8kΩ  
R8 100Ω

See  
**Shop  
Talk**

page 635

### Potentiometers

VR1 100kΩ carbon log.  
VR2 2.2MΩ carbon lin.  
VR3 10kΩ carbon log.

### Capacitors

C1 10μF 25V elect.  
C2 10nF polyester C280  
C3 10nF polyester C280  
C4 10μF 25V elect.  
C5 100μF 16V elect.

COMPONENTS  
approximate  
cost  
**£9**

### Semiconductors

IC1 NE556 dual timer i.c.  
TR1 2N3702 pnp silicon  
TR2 BC109 npn silicon  
D1 1N4148 small signal silicon diode

### Miscellaneous

S1 3-pole, 4-way rotary switch  
S2 s.p.s.t. toggle  
SK1 standard mono switched jack socket  
LS1 8 ohms, miniature moving coil loudspeaker  
B1 9V type PP3  
Stripboard, 0.1 inch matrix 15 strips by 31 holes; metal case 200 × 125 × 50 mm;  
14 pin d.i.l. socket for IC1; four knobs; stranded wire for interconnections;  
battery connector; 6BA nuts bolts and spacers (2 off each).



By T. R. de Vaux-Balbirnie

cut costs by  
building our

# PHONE CALL CHARGE JOGGER

WITH telephone bills flowing freely again, many readers must be examining ways of saving money. Rather than to cut down on the number of calls, choosing the best time of day and eliminating gossip can do a great deal to reduce telephone bills. The circuit described here is a very simple and cheap affair which gives an indication when a fixed sum, presently 3·5p when the call is dialled on your own phone, has been spent.

It has a built-in "nuisance factor" in the form of a button which is pressed to reset the circuit and to initiate a further timing period. Of course, direct connections to the telephone system are prohibited so savings will only be made with the goodwill and co-operation of the user who may choose not to switch the unit on in the first place!

It is probable, however, that members of the family will not be setting out to waste money—they just need a simple jog to remind them of the mounting cost.

There are commercial instruments which "clock up" the cost digitally. There have also been published designs for similar sophisticated circuits which use advanced techniques to give an accurate account of the

cumulative cost. These are excellent but tend to be expensive. A cynic might suggest that it would take years to recover their cost in terms of the savings achieved.

By contrast, the present design is cheap and very simple to construct. It does not boast accuracy and uses a simple lamp to indicate when the time is up.

## USING THE JOGGER

The device is used in the following way. Before the call is made the correct time period is selected according to the distance and the time of day. At the present time there are four distance factors—Local (L), Medium Distance (a), and Long Distance (b). The fourth is a Channel Islands charge and, with apologies for those making calls to these parts, this is not included.

The charge system allows for three rates according to the time of day—Peak, Standard and Cheap. With three distance factors and three time factors there should be nine possible call times available for the 3·5p unit. In fact, there are only eight as two of them coincide. Nine positions have been included for convenience and the possibility of later non-coincidences. The various periods are set out in

Table 1 below but further details may be obtained from the Telephone Dialling Codes booklet supplied to subscribers by the Post Office.

TABLE 1: Time in seconds obtained for 3·5p as a function of call distance and time of day. This applies to calls dialled on your own phone. V.A.T. is to be added to the total cost.

Distance Time	(L) Local	(a) Up to 56km	(b) Over 56km
PEAK Mon-Fri 9am-1pm	120	30	10
STANDARD Mon-Fri 8am-9am 1pm-6pm	180	45	15
CHEAP All other times	480	180	60

The selection of these times could be made by using nine separate switches or by a 9-position rotary switch. The author, however, used the cheap alternative of nine miniature sockets and a plug on a wandering lead which could be placed in the appropriate position. The plug will normally be left in the most frequently used socket.

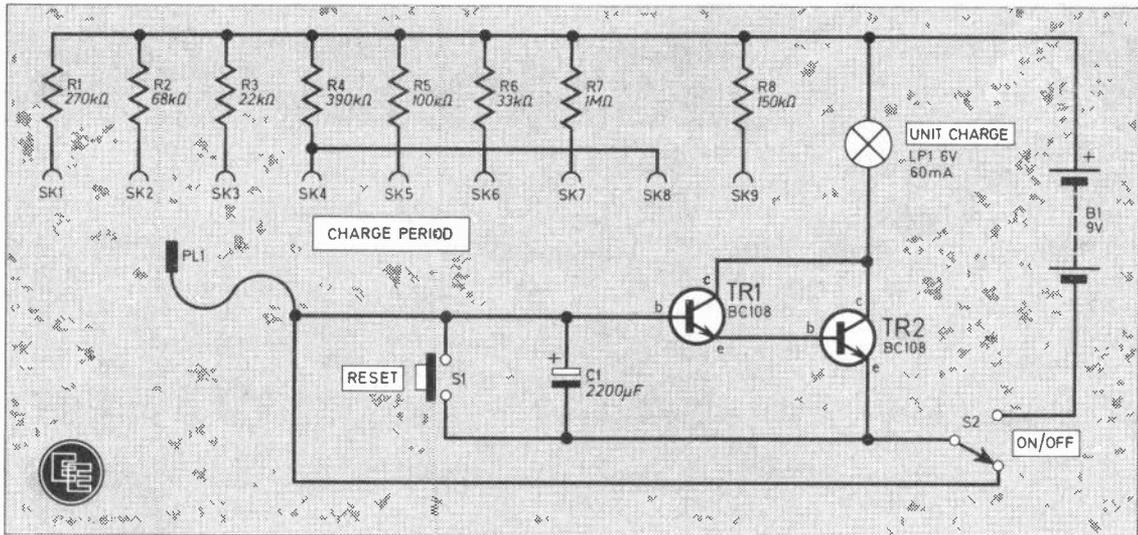


Fig. 1. The complete circuit diagram for the Phone Call Charge Jogger.

With the correct selection made, the unit is switched on. When the call is established, the reset button is pressed momentarily. When the first 3.5p has been used the panel light will come on. To monitor further 3.5 pence worth the reset button is pressed as required. For local cheap rate calls there will be little nuisance value as the intervals will be 8 minutes or so but for the more expensive calls the nuisance factor will be much greater and the mounting cost demonstrated in quite a frightening way!

### CIRCUIT DESCRIPTION

The circuit (Fig. 1) consists of two high-gain transistors TR1 and TR2 connected as a "Darlington pair" which produces a very high gain transistor equal to the product of the individual gains. When the circuit is switched on, C1 charges up through one of eight resistors selected by the control panel. The rate of charge will depend on the value of the resistor—the higher the value the more slowly will the capacitor charge. At a certain point the voltage across C1 will be sufficient to turn on TR1. This turns on TR2 which causes the panel lamp to illuminate. The push-button switch S2 is used to discharge C1 and initiate another timing cycle. It will be noted that the on-off switch is placed in the negative battery line. This is necessary because this switch is also used to discharge C1 whilst the unit is "off."

### COMPONENTS

Electrolytic capacitors like C1 are a necessary evil in this type of circuit. Any particular component is unlikely to have its nominal value and the manufacturer's tolerance is typically -25 per cent to +100 per cent. In

fact it is likely to be well within these limits. All the same, some capacitors could lead to quite significant differences in the timing periods.

On testing, if this is found to be the case, then the easiest course of action is to re-specify the unit cost i.e. the time bought for, perhaps, 2p or 4p instead of 3.5p. The latter unit was originally chosen because the Post Office base their calculations on this at present!

One point to watch is that a newly purchased capacitor or one which has been stored for a long period is likely to be deformed to some extent. It should be found that the time intervals settle down to steady values after a few operations. It is normal for the lamp to come on slowly, especially for the long time intervals.

The timing resistors R1-R9 in the circuit diagram can be cheap carbon components with 10 per cent tolerance. In theory, better results would

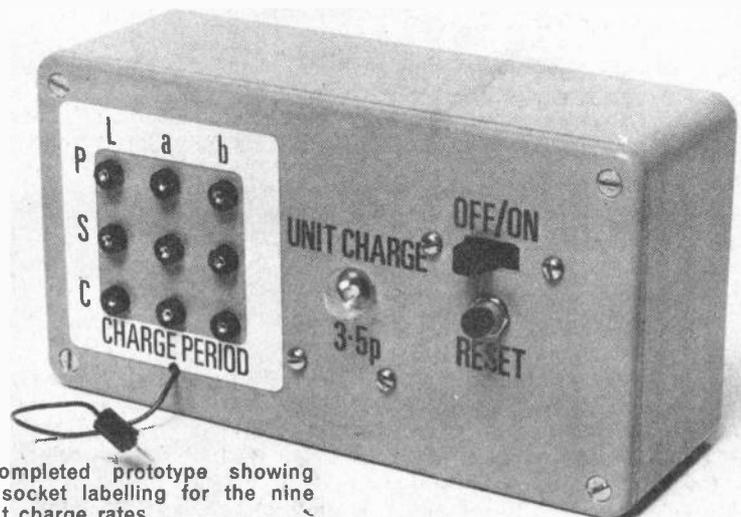
be obtained, especially in the long term, by using more expensive resistors with 5 per cent or better tolerance.

In terms of cost the benefit would not be worthwhile and in practice the cheap type worked satisfactorily with reasonable accuracy.

As well as buying a good quality component for C1, it is necessary to buy good transistors. Cheap "out of spec" transistors may have insufficient gain to work properly in the circuit.

The panel light for the prototype was just a lamp pushed through a rather tight hole with direct soldered connections. This saves cost but some constructors will wish to improve the appearance of the panel by using a proper lampholder.

A cheap plastic box was bought for the prototype but there are generally boxes lying around the house which could be used. The size of this box



The completed prototype showing matrix socket labelling for the nine different charge rates.

## COMPONENTS

### Resistors

- R1 270k $\Omega$
  - R2 68k $\Omega$
  - R3 22k $\Omega$
  - R4 390k $\Omega$
  - R5 100k $\Omega$
  - R6 33k $\Omega$
  - R7 1M $\Omega$
  - R8 150k $\Omega$
- All  $\frac{1}{4}$ W carbon  $\pm$  5%

See  
**Shop  
Talk**

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### Capacitor

- C1 2200 $\mu$ F 15V-elect.

### Transistors

- TR1, 2 BC108 silicon *n*p*n* (2 off)

### Miscellaneous

- S1 push-to-make, release-to-break button switch
  - S2 s.p.d.t. slide switch
  - LP1 6V 60mA m.e.s. bulb
  - SK1-9 1mm panel mounting sockets (9 off)
  - PL1 1mm plug
  - B1 9V type PP9—see text
- Tagpanel 10-way miniature; case, plastic size 150 x 75 x 50mm, Bimbox type BIM 2005/15 or similar

Guidance only  
Approx. cost

**£2.75**  
excluding  
case

# PHONE CALL CHARGE JOGGER

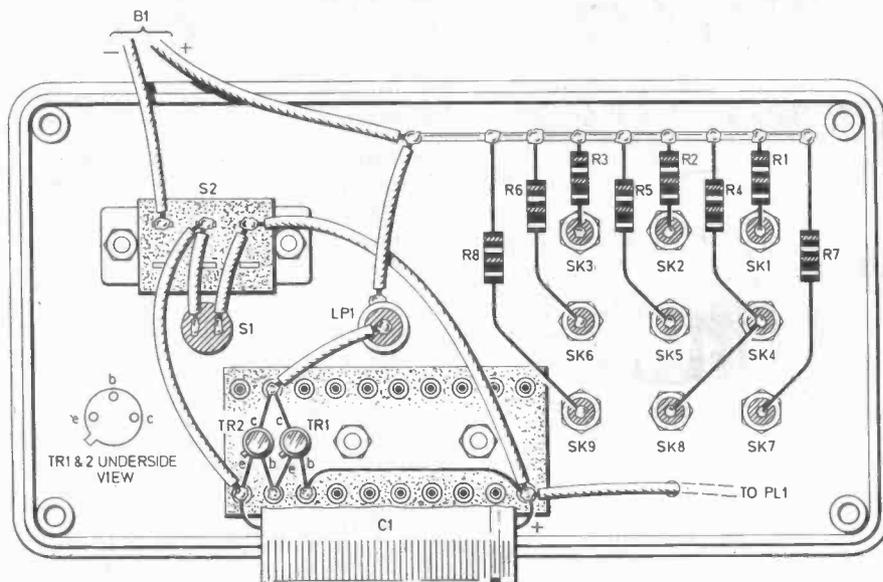


Fig. 2. Shows the method of assembly and interwiring where the case lid is used for mounting all components. Note the link wire on the tag-board. This method is not critical and may be readily changed to suit other case dimensions. The lamp can be mounted in a holder to improve the appearance.

will determine the kind of battery which will be used. It would not be wise to use a small battery like a PP3. This would not give good service. If a larger 9 volt battery like a PP9 could be fitted into the box then this would be a good choice. An alternative would be two 4.5 volt "flat" cycle lamp batteries connected in series. These can be placed separately in the box and manoeuvred into position. It should be noted that the panel lamp is a 60mA (0.06A) type. A higher cur-

rent rating like 200 or 300mA is not advised.

## WIRING UP

The components in the prototype were all secured to the lid of the case as seen in Fig. 2. Begin by drilling the holes to suit these components and their fixings and fit these to the lid with the exception of the tag-panel, and wire up as shown.

The resistors are connected to the correct socket (see Fig. 2) at one end

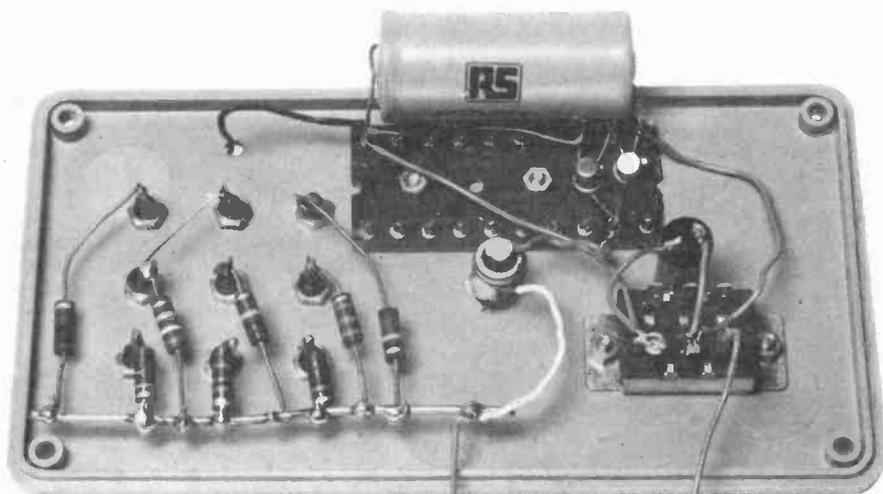
and the other ends are hooked around a common busbar and securely soldered. The ends leading to the sockets must not touch one another—if they cannot be routed in such a way that this will not happen then the wire ends should be protected by means of sleeving. Insulation stripped from wire of suitable diameter makes excellent sleeving.

The rest of the circuit was built on a small piece of tag-panel to the layout shown in Fig. 2. It is in no way critical, however, and constructors may use tagboard or other boards which may be available. Secure the completed tag panel to the lid and complete the interwiring.

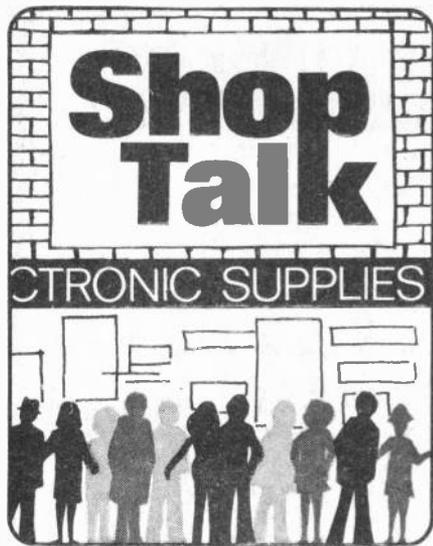
Attach suitably terminated leads to form the battery supply leads and connect to the battery of your choice (see above). With PL1 connected and plugged into SK3 (long distance peak call) the lamp should light after 10 seconds from turning on at S2. Pressing S1 should cause the lamp to extinguish to come on again after a further 10 seconds.

Repeat and check times for all the other positions to see that they agree with Table 1. If so, the unit can be fitted in the case and the top panel labelled as shown in the photograph, and protected from the effects of fingermarks.

After initiating the family in its use it just remains to wait for reduced bills!



The completed prototype ready for connecting to the batteries and installation in the case base.



By Dave Barrington

## Soldering Iron

With the new season upon us many of our readers must be taking stock of their workshop tools and components and making a shopping list of requirements for the months ahead.

Top priority must be the soldering iron. Is the bit still serviceable? Does it handle well? Is the iron rated correctly? Most important, should the selection of bit sizes be changed or added to?

There are many irons to choose from at widely differing prices. Choice will obviously be dictated by the amount of money you can afford but we recommend you purchase the best possible. A little extra outlay now will more than pay for itself over the years. Most of our advertisers carry fairly large ranges and stocks of irons and will be only too pleased to offer advice.

For most work encountered in *Everyday Electronics* an iron rated between 15 and 25 watts should be adequate. For bit sizes we would suggest a selection of 2, 3 and 4mm preferably of the latest iron plated type, for long life. A good choice is the Litesold range manufactured by Light Soldering Developments Ltd., and the Midget range from S. & R. Brewster Ltd.

Try to choose an iron that is lightweight, well balanced, easy to handle and has an adequate length of mains cable. Some irons are fitted with lightweight flexible cable that will not "pull" on the iron when in use.

Some irons come complete with a protective stand. If this is not included we strongly recommend the purchase of this item as it will save many a burnt cable and other disasters through carelessness or forgetful use.

If you decide to purchase and use an iron without a stand we suggest you choose one with a built-in hook or "anti-roll collar" so that when placed on the work surface the iron bit stands proud of the worktop.

At the top end of the market there are what is commonly known as "solder stations". These are usually made up of a low voltage temperature controlled iron, ideal for delicate work, an integral stand, with a wiping sponge for cleaning the iron

tip and a mains derived low voltage, via a transformer, supply.

The use of the transformer isolates the iron bit from the mains which can be essential in some MOS work.

## Solder Station

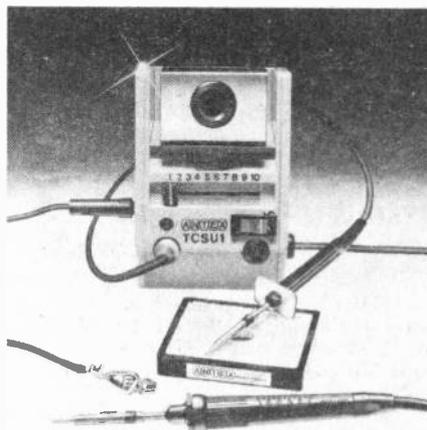
One such thermostatically controlled station is the new version of the Antex TCSU1.

The soldering station is provided with either the miniature CTC 40 watt iron or the XTC 50 watt model. Both irons are fitted with burn free cable terminated with 5 pin DIN plugs for connection to the 24 volt supply from the station.

Thermocouples sense the bit temperatures which is kept at a preset level (between 65 and 420°C) by a slide control on the front facia of the stand. A range of three iron coated bits are included which are a slide fit on the stainless steel shafts of the irons. A removable sponge tray is also included.

A particular feature of the TCSU1 is the inclusion of an anti-static earth socket to help protect MOS devices from damage. Also, by employing zero switching such evils as magnetic fields and spikes are claimed to be eliminated.

Further details, price and stockists can be obtained from Antex Electronics Ltd., Dept EE, Mayflower House, Plymouth, Devon.



The Antex TCSU1 soldering station.

## Catalogue

It is claimed that over 400 new product lines have been added to existing ranges in the new Verospeed Autumn '80 components catalogue, which just by glancing through we can well believe. Printed circuit board mounting rotary switches, batteries and chargers, test leads, cases and integrated circuit sockets are just some of the ranges that have been extended.

Two features of this excellent 114-page catalogue which appeal are the inclusion of two pages of "Bargain Basement" items and, more important, the inclusion of all prices against each entry (less VAT). It is hoped that all prices will be held for the period of the catalogue, until January 1981.

Copies of the Verospeed Autumn '80 Catalogue can be obtained from Verospeed Ltd., Dept EE, Stansted Road, Boyatt Wood Industrial Estate, Eastleigh, Hants SO5 4ZY.

## CONSTRUCTIONAL PROJECTS

### Call Charge Joggler

A double-pole double-throw slide switch should be used for the Off/On switch in the *Call Charge Joggler* as this is the more commonly stocked item. The rest of the components for this project are readily available.

### Midget Radio

The compression trimmer capacitor C2 called for in the *Midget Radio* is stocked by Home Radio (Components) Ltd. The spindle for this trimmer is made specially for Home Radio.

The aerial coil used in the prototype model was MW 5FR from Denco (Clacton) Ltd., This aerial coil, and the transformer, can also be purchased from Home Radio, Maplin and Watford Electronics.

The t.r.f. radio i.c. ZN414 is available from most component stockists as are the rest of the components for the radio.

### Darkroom Timer

The only item likely to cause any concern in the *Darkroom Timer* is the small biased toggle switch. This is available from Watford Electronics and is listed in their "miniature" toggle switch range.

The relay used is the common miniature "continental" type carried by most advertisers. This may be supplied with more than one set of contacts but only one set need be wired in circuit.

### Bicycle Alarm

Although the prototype *Bicycle Alarm* used a reed switch and coil it was felt that a relay would be more suitable. Any relay with a coil resistance of 150 ohm or greater and capable of operating at 9V will suffice. The miniature continental relay with an 185 ohm coil is capable of operating down to approximately 5.5V and would seem useable here.

The Delta bleeper alarm from J. Bull (Electrical) Ltd., gives off a most piercing sound and at 75p each seem to be most reasonable. However, any 6 to 12V d.c. buzzer can be used.

### Audio Effects Unit

We cannot foresee any buying problems for the *Audio Effects Unit*. Note when ordering components that two log. (logarithmic) potentiometers are specified as you may find you are supplied with all linear types.

### Dusk--Dawn Relay

Readers should have no difficulty in locating components for the *Uniboard: Dusk--Dawn Relay*. The relay used is the common miniature continental type rated at 12V 185 ohm coil with 2-pole change-over contacts rated as required.

### Iron Heat Control

We do not expect any purchasing problems for the *Iron Heat Control*. The triac for this circuit is available from Home Radio for the sum of 75p, including postage and packing.

We have been informed that Home Radio are also able to supply all parts, including the case.

# UNIBOARDS

SIMPLE  
TRANSISTOR  
DESIGNS

By A.R. Winstanley

7

## DUSK-DAWN RELAY

**T**his article describes the construction of a device which illuminates a lamp automatically as the night approaches. This three-transistor design operates a changeover relay when the amount of light falling onto a photocell has reached a defined level.

The circuit is powered from a 9 volt rail and whilst this could be derived from dry batteries, the unit described here has been designed to operate from the 9 Volt Power Supply which appeared in Part 3 of this series.

### CIRCUIT DESCRIPTION

The circuit diagram of the Dusk-to-Dawn Relay is shown in Fig. 1. Light-dependent resistor PCC1 is remotely located and detects the ambient light level. Together with R1 and VR1 (the SENSITIVITY control), the l.d.r. forms a potential divider, so that the voltage at the base of TR1 is dependent upon the amount of light falling onto PCC1.

During the daytime the resistance of the l.d.r. is low—in the order of 20 ohms—and so the voltage at TR1 base is high; conversely as night-time approaches, the resistance of the ORP12 increases, so lowering the voltage at TR1 base.

TR1 and TR2, together with associated resistors, form a circuit configuration called a Schmitt Trigger. This circuit is designed to suddenly switch over at a predetermined setting even though the input signal (i.e. the voltage at the base of TR1) may change over only very slowly.

This snap-over action makes the circuit ideal for operating a lamp when the ambient light level is slowly reducing. The Schmitt Trigger functions as follows.

Consider a night-time situation where the resistance of PCC1 is high—say 500 kilohms or so (although it could be considerably higher). Assuming that VR1 is set to midway, the voltage at the base of TR1 works out at only 150mV. This means that TR1 must be off since the base needs to be 650mV more positive than its emitter for the device to switch on. TR2 is therefore permitted to switch on as base current is able to flow through R2. A voltage then develops across R3 (and also R4); this effectively reverse-biases the base-emitter junction of TR1 and this component remains firmly biased off.

### INCREASING LIGHT LEVEL

As the resistance of PCC1 falls (the ambient light level increasing) the voltage at TR1 base will rise until TR1 starts to switch on.

At this point, the collector of TR1 falls, taking TR2 base with it. The effect of this is that TR2 starts to turn off. In so doing, the emitter of TR2 is sent to 0V, as is TR1 emitter. This increases the forward bias on the base-emitter junction of TR1, so enabling TR1 to switch on harder.

As it does this TR2 is forced to switch off even further, thereby causing TR1 to conduct more. This regenerative action, once started, causes TR1 to switch on hard very rapidly, with a consequent switching out of circuit of TR2.

This is the action of the Schmitt Trigger: a very gradual change in the resistance of the l.d.r. results in the circuit "snapping over" very quickly.

As night-time approaches once more, a reverse avalanche takes place resulting in TR1 switching off and TR2 conducting.

TR3 is a *pn*p transistor coupled to the collector of TR2 by R5. When TR2 is on, TR3 is also conducting. This operates RLA, the contacts of which complete the mains circuit to the lamp. Diode D1 also illuminates, signifying that the relay is operating. TR3 serves as a power output stage which prevents loading of the basic Schmitt circuit.

The ratings of the relay contacts must be carefully observed: the specified relay will switch mains loads of up to 3A (750 watts), and this should satisfy most domestic applications.

CONSTRUCTION  
starts here

### CIRCUIT BOARD

The circuit is built onto a standard-sized piece of 0.1in matrix strip-board measuring 10 strips by 24 holes. The l.d.r. and power supply are connected by means of two 3.5mm jack sockets. The Dusk-to-Dawn Relay unit itself was housed in a plastic box which measured 150 × 80 × 50mm.

If desired, there is no reason why the power supply cannot be housed in the same case. A larger case than specified may then be required.

Component layout on the circuit board and complete wiring details are shown in Fig. 2. Two 6BA clearance holes are drilled to take the supporting hardware, and then the circuit board is assembled in the normal manner. Take care regarding the orientation of the transistor leads: do not overheat them and ensure that D2 is soldered in the right way round.

Complete the low-voltage wiring using stranded connecting wire as shown. The l.e.d. is mounted on the front panel using the special mounting clip normally provided with it; the relay can be secured in place with a piece of double-sided adhesive foam.

Basic interwiring is also shown for the mains circuitry. In this respect it is important that the soldering to the relay tags is of a high quality. Also mains connecting wire of the appropriate specification (3 amps at 250V) must be employed.

The photocell was soldered to a small piece of tagstrip and twin core flex terminated in a 3.5mm jack plug was used to connect this to the main unit, see Fig. 2.

Setting up comprises simply adjusting the preset, VR1 to about midway and then repositioning it if necessary until the desired switching point is achieved with the l.d.r. sited in its operating position. □

# COMPONENTS

## Resistors

- R1 5.6k $\Omega$
- R2 15k $\Omega$
- R3 68 $\Omega$
- R4 680 $\Omega$
- R5 3.3k $\Omega$
- R6 680 $\Omega$
- All  $\frac{1}{2}$ W 5% carbon

See  
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## Semiconductors

- TR1, 2 BC108 npn silicon (2 off)
- TR3 BFX88, BFX30 or 2N2905A pnp silicon
- D1 TIL220 light emitting diode
- D2 1N4148 silicon
- PCC1 ORP12 light dependent resistor

## Miscellaneous

- VR1 22 kilohm miniature horizontal preset
  - RLA 12V relay, coil resistance 185 ohm Continental with 3A 250V c.o. contacts
  - SK1, 2 3.5mm jack sockets, (2 off)
  - PL1 3.5mm jack plug
- 0.1 inch stripboard, 10 strips  $\times$  24 holes; case—BIM2005/15; i.e.d. clip; twin-core flex; tagstrip; mains wire; stranded hook-up wire; 6BA hardware.

Approx cost      Guidance only

**£4.00** excluding case

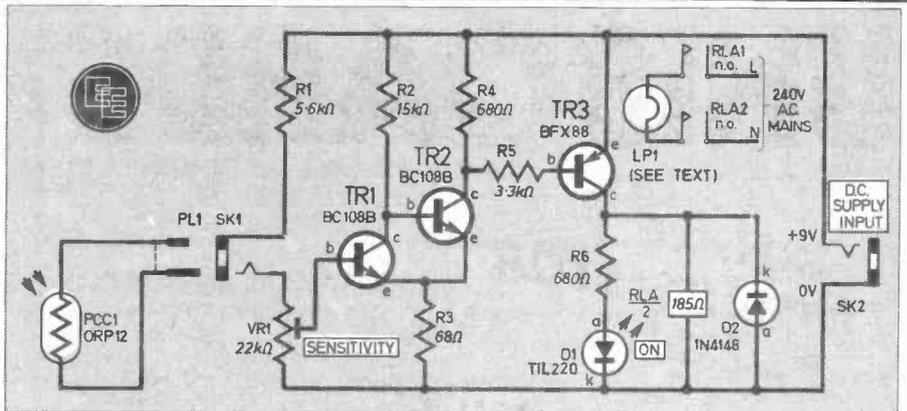
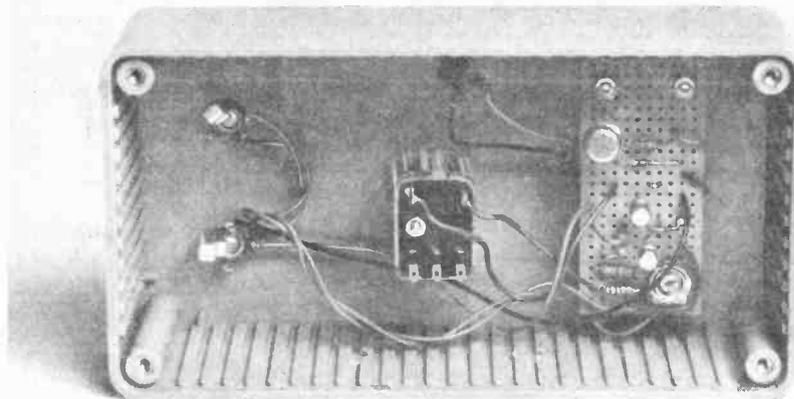


Fig. 1. The circuit diagram of the Dusk-Dawn Relay unit. The power supply may be from battery or the 9V Power Supply Unit featured earlier in this series.



The partially assembled prototype requiring connections from the relay contacts to the lamp and 240V a.c. mains.

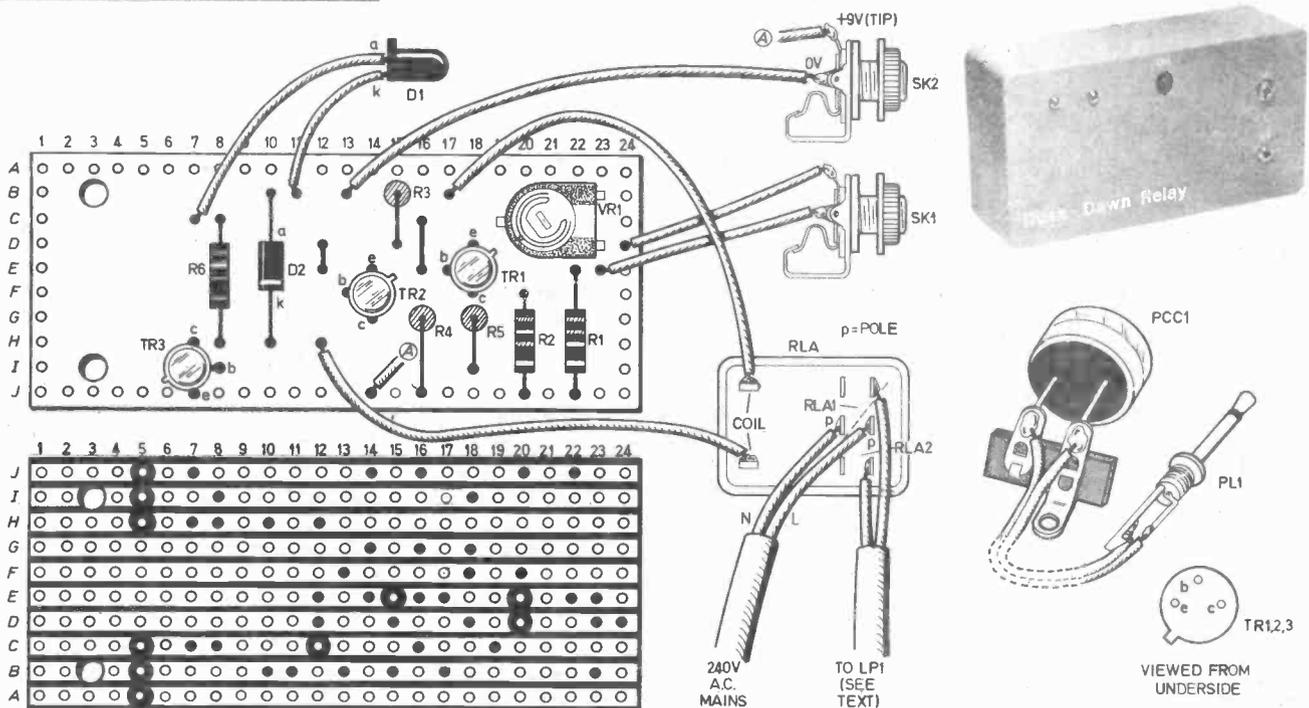


Fig. 2. The layout of the components on the topside of the stripboard, breaks to be made along the copper strips on the underside and wiring up to the off-board components. Also shows 240V a.c. mains connections to the controlled lamp via the relay contacts. The contact arrangement will vary between relay types and should be verified before connection. Seen right is the method used for mounting the light dependent resistor.

**R**ICHARD was choosing a switch for his new project. Looking through the pages of the catalogues, he thought that it would be easy. Unfortunately, he just became increasingly confused. The easy part was the cosmetic one—deciding on a rocker switch rather than the toggle variety. It was the contact current ratings which really confused him so he came along for advice.

"I could understand it if there was just one figure given for the current rating", he said in dismay—"but there are two; one for a.c. use and one for d.c. Apart from that, there is a different figure given for switching current and carrying current. To top it all, there is a warning to de-rate in the case of inductive loads—I feel like giving up!"

Though confusing I told him that these ratings must not be taken lightly. To exceed one could seriously reduce the life of the switch. Some manufacturers do give only one current rating and although this seems easier it can lead to misuse.



I explained that at the instant of the contacts "breaking" a spark is produced. This tends to burn the contacts. If a.c. is used the spark tends to go out as the current falls to zero on each half cycle. With d.c. the spark will only go out when the contacts move too far apart to support it. This usually takes longer. For

this reason, switches usually have a higher a.c. rating than for d.c. Some switches are not recommended for d.c. use at all because the contacts do not move fast enough.

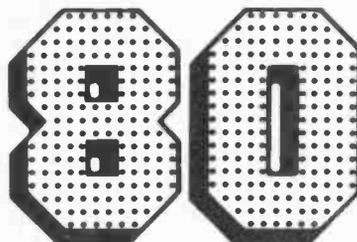
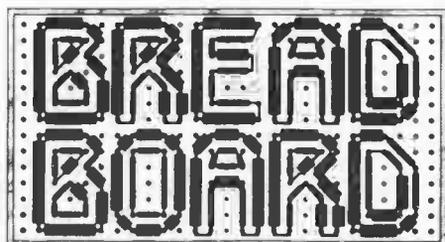
I went on to say that where coils form part of the load—chokes, transformers, motors, and so on, then larger sparks could be expected. It would then be wise to halve the rating at least.

His point about current carried and current switched was interesting. With the contacts "made" the current could be allowed to rise significantly above the "switched" value.

I rounded off our talk by telling him that switches are better mechanically than they are electrically. With no load, a switch will give far more operations before it fails than on full load. Here, burnt contacts will limit its life.

Although it may cost more, a switch should be generously rated. Good quality switches have an inbuilt "safety margin" which cheap ones might not and I warned Richard not to buy a dubious component.

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 27th Nov — THURSDAY — 10am-8pm  
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# FOR BEGINNERS

## STRIPBOARD

LOOKING at the constructional articles in EVERYDAY ELECTRONICS, the newcomer will discover that most projects are built on pieces of stripboard. This is a plastics board with copper strips on one side, and perforated with holes, at 0.1 inch intervals. This is a popular method of construction, and is recommended to the beginner.

The size of board used for a particular project is expressed in terms of number of strips and number of holes. For example, "Stripboard: 0.1 inch matrix 25 strips x 18 holes." Refer to Components Lists for further examples.

This board, also known under the proprietary name *Veroboard*, is available from most component stockists in a variety of sizes. The board can be cut to any required size with a small hacksaw or jewel saw. The smallest size supplied is 10 strips x 24 holes. This is adequate for many smaller circuits, as is demonstrated by our *Uniboards Series*.

In all our constructional articles we provide (1) a circuit diagram (2) a diagram showing the layout of all components on the top side of the

stripboard and — usually — (3) an underside view showing any breaks that have to be made in the copper strips. Though where the number of breaks involved is small, they may be indicated in (2) by an "X" enclosed in a circle. Breaks are easily made, using a drill bit and rotating by hand, or there is a special tool for this purpose which can be obtained from retailers (Fig. 1a).

In these diagrams, the strips are given a letter reference and the holes are numbered. This facilitates location and co-relation of connection points at both sides of the board.

It is usual to mount all components on the board, except those that happen to be too large physically, and certain items such as controls and switches which need to be mounted on a front panel or on the top of the enclosing case.

Flexible wiring is used to connect such components to the appropriate points on the board. All such interwiring is usually illustrated in the diagram.

## PRINTED CIRCUIT BOARD

Other methods are also used for mounting circuit components. Printed circuit boards are commonly used for mass produced commercial equipment, and this same technique has been in wide use amongst private constructors for many years. One does of course have to get familiar with

the technique and then practise, to achieve good results.

A wiring pattern, unique to a particular circuit, is produced as a copper image on a plastics board by an etching or masking process. This operation can be undertaken by the individual and special kits for making printed circuit boards (p.c.b.s) can be purchased from certain advertisers.

(A detailed article describing the procedure will appear in a future issue of EVERYDAY ELECTRONICS.)

## PLAIN PERFORATED BOARD

Another quite simple and popular method is the use of plain perforated plastics board—this is like stripboard minus the strips.

Special terminal pins (Veropins), tapered to give good fit, are pushed into the appropriate holes in the board to provide anchoring points for components. The snag is that connecting wires have to be soldered between pins to make all the necessary link-ups, in the absence of copper strips (Fig. 2).

All the above mentioned methods of assembling circuit components will be found amongst EE Projects, from time to time. The newcomer should study these constructional articles, noting particularly the layout diagrams.

Since every component and every connection is clearly shown, the "non-electronic" person can go ahead with confidence and build up one of the simpler projects according to these diagrams. Knowledge of exactly how the circuit functions is not essential, for this purpose.

Once a small project has been tackled and successful results obtained, the newcomer will be additionally inspired to learn more about circuit theory and there will always be articles and features in EE to help explain the basics of electronics, both theoretical and practical.

Good luck, all you new constructors.

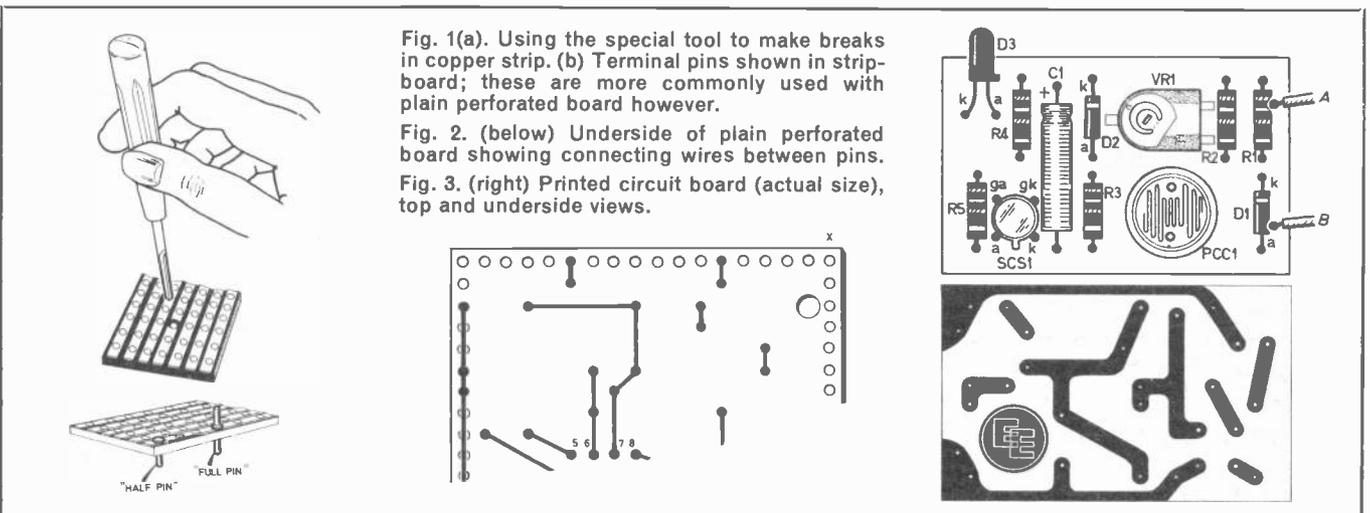


Fig. 1(a). Using the special tool to make breaks in copper strip. (b) Terminal pins shown in stripboard; these are more commonly used with plain perforated board however.

Fig. 2. (below) Underside of plain perforated board showing connecting wires between pins.

Fig. 3. (right) Printed circuit board (actual size), top and underside views.



By M. P. Horsey

# BICYCLE ALARM



**B**ICYCLES are becoming increasingly expensive, and the ease with which they can be stolen is a major problem for every cyclist. A simple, inexpensive yet effective device was therefore needed to protect a bicycle against the thief, or "joy rider".

As with all alarm systems, care must be taken to ensure the alarm cannot be triggered accidentally (if the bicycle fell over for instance), and it was decided to use a fairly conventional wire link system to disable the cycle.

More unusual is the owner's method of de-activating the alarm. Instead of the usual key and lock switch, a less expensive and more novel method was devised using a miniature jack plug "coded" with a suitable resistor.

The alarm is then "tuned" to recognise this resistor, the jack plug replacing the key.

The alarm cannot be de-activated using a metal object instead of the jack plug, as the resistance is clearly incorrect. Of course, the alarm could be defeated by a dishonest person, with a knowledge of electronics, armed with the correct equipment, who happens to want to steal a bicycle protected by this particular device.

This combination is thought to be unlikely!

## OPERATION

The alarm is operated as follows. When not in use, the wire link,

actually screened cable, is connected via the 3.5mm jack plug. To set the alarm, the 2.5mm "key jack" is plugged in, the 3.5mm plug removed, looped through a wheel (or better still, a nearby fixed object), and replaced in its socket. The key jack may now be removed and the alarm is set.

If the wire link is removed or cut, the alarm will sound and cannot be silenced by replacing the link. The only way the alarm can be silenced is by using the key jack.

To de-activate the alarm, the key jack is inserted, the link removed from around the wheel and plugged in again. The key jack is now removed to avoid unnecessary current drain.

## CIRCUIT DESCRIPTION

Since the alarm will be set continuously, current consumption is a major consideration. The circuit is therefore based on a CMOS integrated circuit, the CD4011. This consists of four NAND gates, each with two inputs.

With the component values indicated, current consumption is less than one microamp with the link plugged in, and rises to about 1.5mA during the short periods when the key jack, PL1/R1, is used. The current will of course be much higher if the alarm is triggered, but this should not happen often.

The circuit is in two sections (see Fig. 1). Gates a and b of IC1 are wired through presets VR2 and VR1 respectively. If the key jack is missing, the inputs at gate a will be low, and its output logic 1.

The inputs into gate b will be logic 0 at pin 5, and logic 1 at pin 6, and its output logic 1. Assuming the presets are set correctly, as described later, if the key jack socket is shorted, the inputs to gate a will be logic 1, and its output 0.

The inputs to gate b will now be logic 1 at pin 6, and logic 0 at pin 5 resulting in its output being at logic 1.

## KEY JACK

Thus the output from gate b will be high whether the key jack socket SK1 is open, or shorted. If, however, a resistance of say 1 kilohm is connected via the key jack, the presets can be arranged so that the potential from preset VR2 maintains the input to gate a low, but the potential from preset VR1 is sufficient to cause an input to pin 5 at logic 1. Since pin 6 is now high as well, the output of gate b falls to zero.

To summarise, if the key jack is unplugged or shorted the output from gate b is at logic 1. If a key jack plug containing the correct resistance is used, the output from gate b is at logic 0.

This output is fed to gate c, such that a zero output from gate b will ensure that the output of gate c is at logic 1, regardless of the state of its other input. This in turn will ensure that the output from gate d is zero, and the alarm cannot sound.

If the key jack is removed, or shorted, the output from gate c is now dependant upon its other input. This is arranged with R2 and R3 as a potential divider, such that the input to pin 9 is logic 1, if the loop connected via SK2/PL2 is removed, and logic 0, with the loop connected.

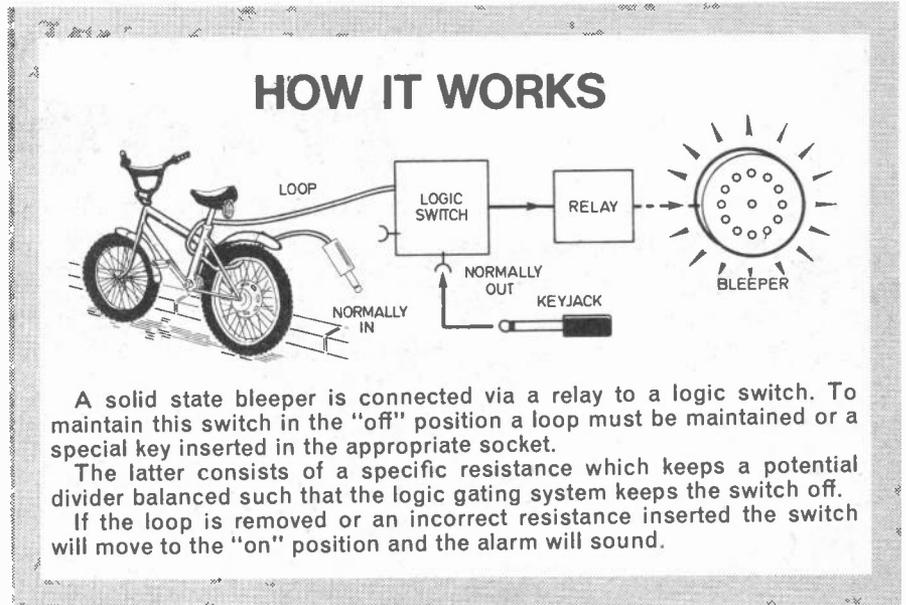
Thus if the loop is connected pin 9 will be low and the alarm cannot sound. Removing the loop will cause pin 9 to rise to logic 1, and with both inputs to gate c high, its output will be zero, and the output of gate d will be high.

Diode D1 will maintain pin 9 at logic 1 even if the loop is replaced, and therefore the alarm can only be silenced by using the key jack.

### WARNING DEVICE

The output from gate d is fed to TR1 via R4 and this in turn operates a relay with diode D2 to protect the transistor. The relay will allow virtually any type of warning device to be used, providing its power requirements are within the limits of the relay contacts and battery.

The prototype used a reed relay, driving a "solid state buzzer", a small device, with a very loud sound! However virtually any small relay will do. Its resistance should be higher than 150 ohms, and it should be able to operate on nine volts.



### CIRCUIT BOARD

The circuit is arranged on 0.1 inch matrix stripboard, measuring 20 strips by 25 holes (see Fig. 2). Begin by making breaks in the copper track where shown, ensuring that all traces of loose copper are removed. An i.c.

socket is essential, and this should be soldered into place, followed by the wire links, ensuring enough space is left for the presets.

The other components should now be soldered into place, finishing with the transistor which together with the diodes and electrolytic capacitor, should be the correct way round.

Next the battery leads, relay connections and jack sockets can be connected. The wire link is connected as shown in Fig. 2. Good quality screened cable is suggested, since although the outer screen is not used, it is the most difficult to cut and rejoin.

A potential thief would not know that only the inner core was in use, and whilst it would be possible to devise a cunning system to enable both inner and outer cores to be used, using extra i.c. gates, the extra circuitry would not seem justified.

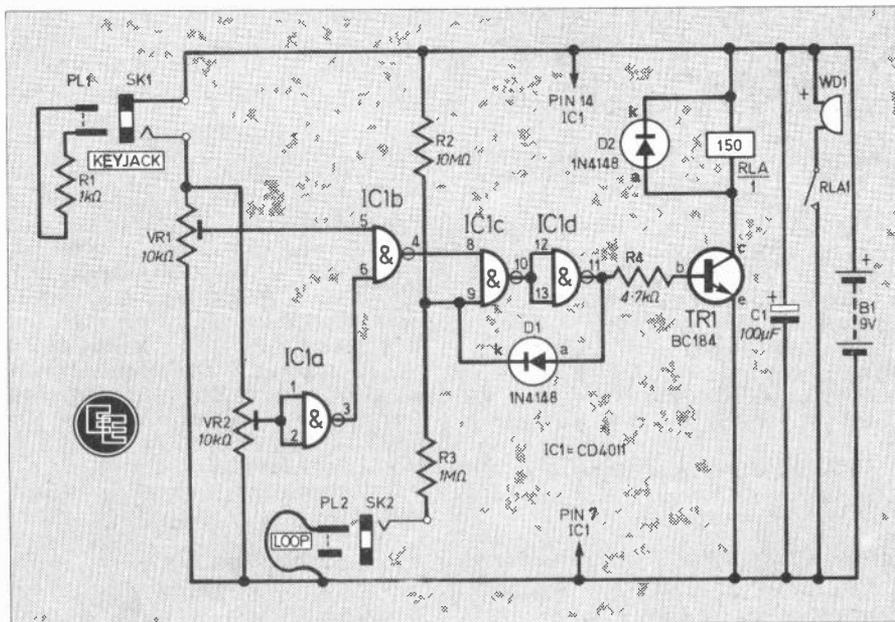
The inner core is joined to location B4 on the stripboard, and terminates at the 3.5mm jack plug. At this stage the board should be carefully inspected for bridged tracks, dry joints and faulty component positions.

### CMOS I.C.

If all is well, the i.c. may be removed from its protective packaging and, without touching its pins placed into its socket. Make sure it is inserted correctly. This may well be the most difficult operation of the project! Static electricity on your body, especially if wearing man-made fibres, or if standing on a nylon carpet, may possibly damage the i.c. if the pins are touched.

Finally the key jack is constructed, using a 2.5mm jack plug, fitted with a suitable resistor. A 1 kilohm type is suggested, although alternative values in the same region could be tried. Careful setting of the presets can make the circuit fairly selective.

Fig. 1. The complete circuit diagram for the Bicycle Alarm.



# BICYCLE ALARM

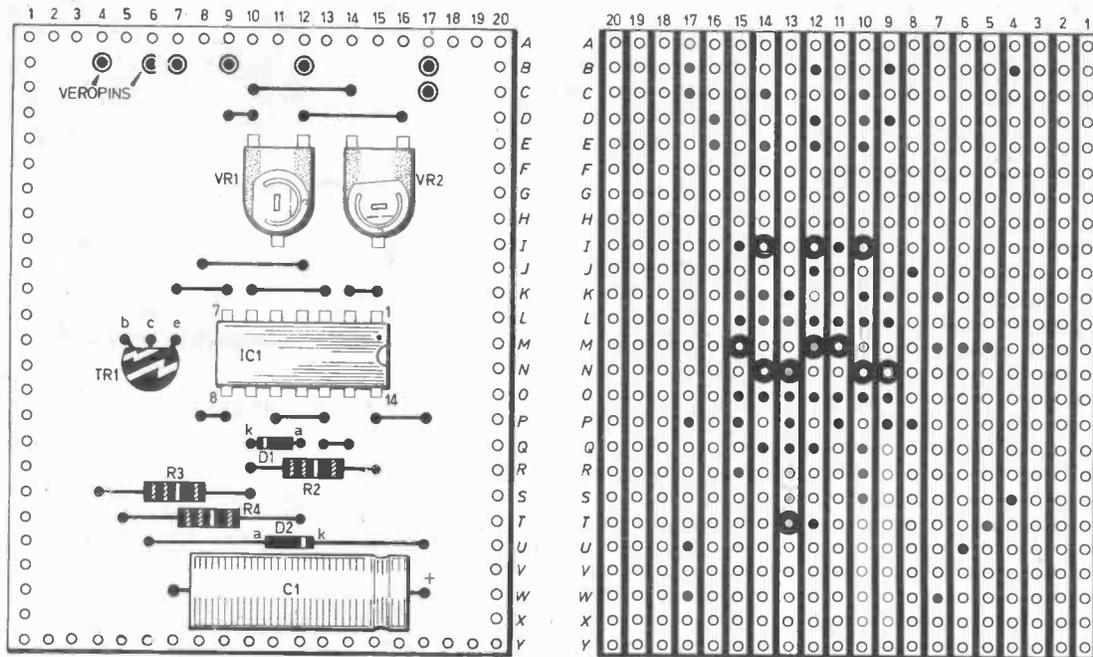


Fig. 2. The layout of the components on the top side of the board and on the right, the breaks to be made along the copper strips on the underside. Note the use of single-sided Veropins for connecting board to other components.

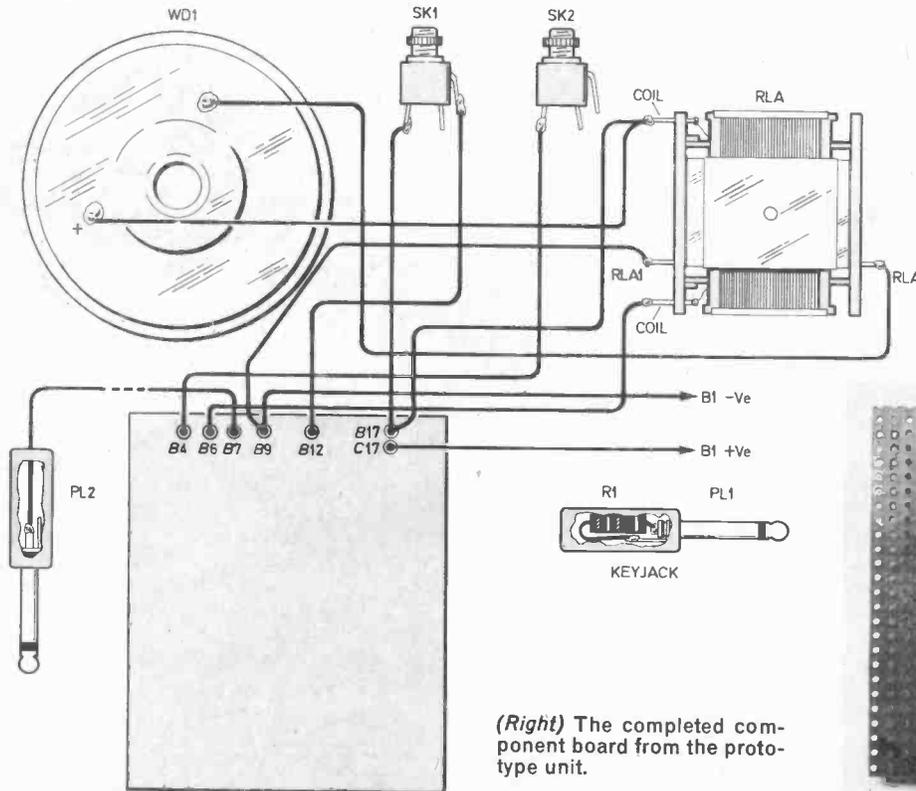
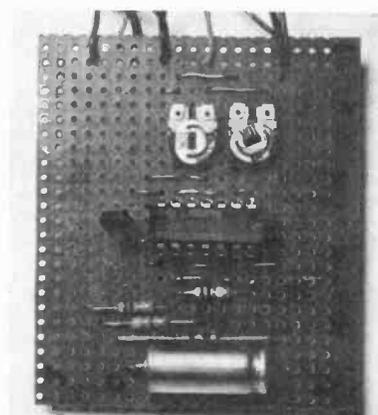


Fig. 3. (Left) Full wiring details between circuit board and the remainder of the components. This shows the coil/reed switch assembly used in the prototype which may be replaced by a standard relay as specified in the components list.



(Right) The completed component board from the prototype unit.

## THE CASE

Some thought must be given to the case as several factors must be taken into account that are not normally considered. The case must be large enough to house the battery, circuit board and bleeper. It must be strong enough not to invite tampering, be watertight, and not easily opened, except by the owner to very occasionally change the battery.

The prototype was fixed under the saddle, in such a way that it would be very difficult to remove. Although a metal case was used originally, one with rounded corners is far more appropriate.

The container used in the prototype was not weather-proof and had sharp protruding corners. Obviously this would be a great disadvantage and we would recommend a plastic or die-cast box with rounded corners instead. Suitable types would be the Bimbox type BIM 2005/15 or a Verobox type 202-21030K.

This can be sited in any convenient place on the cycle using U-clamps or alternatively fixed securely in the saddle bag with the wire loop protruding from the side.

Having decided which way it will fit to the cycle, the case should be drilled *underneath* to allow the sound from the bleeper to penetrate. Care must be taken not to allow rain to enter the case, and the hole for

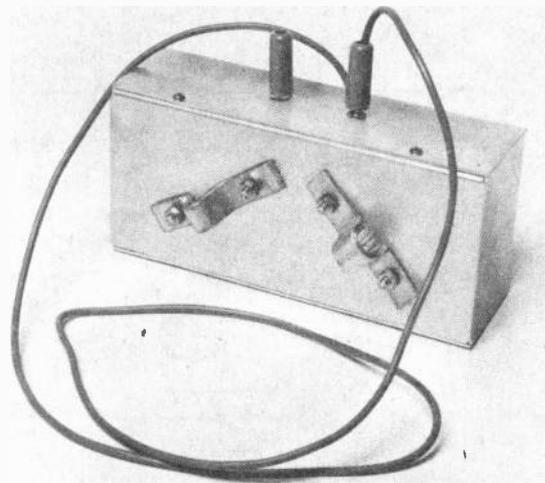
the wire link should also be drilled at the base. The jack sockets are mounted at the rear.

## ASSEMBLY

The parts are then assembled inside using any convenient method. In the prototype "superglue" was used to mount the bleeper and relay, and small self-adhesive rubber feet (cut in half) were used to mount the circuit board and create a battery compartment.

Finally the case is fitted to the cycle as securely as possible. Extra security may be obtained by means of a microswitch wired in series with the wire link, and arranged so that any attempt made to undo the case, opens the switch, and triggers the alarm.

As a final precaution against rain entering via the 2.5mm socket (which is left for long periods without a jack plug in place), a small piece of acetate sheet or similar material may be glued just above the socket, so



The completed alarm showing the fixing brackets and the "key and wire loop jack plugs in position.

that it hinges over the opening.

A final word of warning: ensure that when riding the cycle, the wire link is safely stowed away so that it cannot foul the wheel.

## SETTING UP

Turn preset VR2 fully clockwise. Remove the link, and plug in the key jack. Connect the battery and observe the relay (or bleeper if connected). Adjust preset VR2 until the relay is

## COMPONENTS

### Resistors

- R1 1k $\Omega$
- R2 10M $\Omega$
- R3 1M $\Omega$
- R4 4.7k $\Omega$
- All  $\frac{1}{4}$ W carbon  $\pm$  5%

See  
**Shop  
Talk**  
page 635

### Potentiometers

- VR1 10k $\Omega$  miniature horizontal preset
- VR2 10k $\Omega$  miniature horizontal preset

### Capacitor

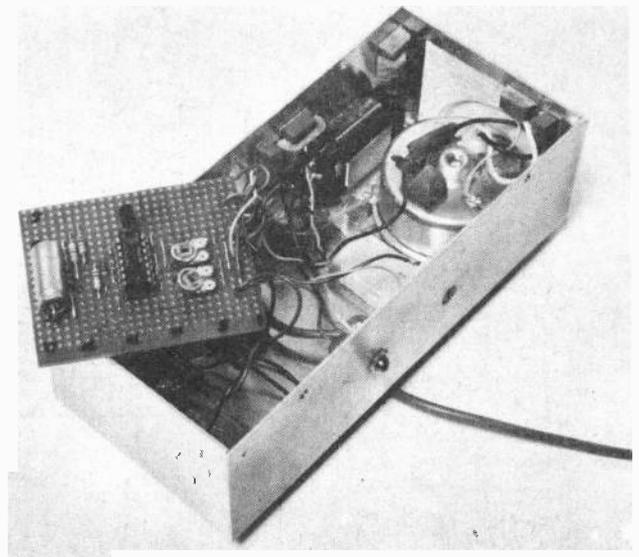
- C1 100 $\mu$ F 16V elect.

### Semiconductors

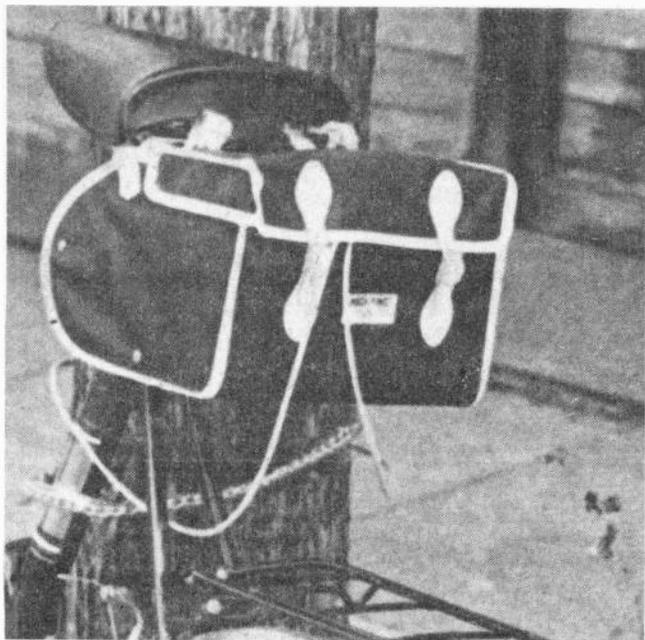
- IC1 CD4011 CMOS quad 2-input NAND gate
- TR1 BC184 *npn* silicon
- D1, 2 1N4148 small signal silicon diode (2 off)

### Miscellaneous

- SK1 2.5mm jack socket
  - SK2 3.5mm jack socket
  - PL1 2.5mm jack plug
  - PL2 3.5mm jack plug
  - RLA miniature 9V relay, coil resistance 150 ohms, one set of normally open contacts
  - WD1 9V solid state buzzer ("Delta Bleeper" from J. Bull Ltd or similar)
  - B1 9V battery, PP7 type
- Plastic case, 150 x 80 x 50mm, Bimbox type BIM 2005/15, die-cast box, or similar; 0.1 inch matrix stripboard 20 strips by 25 holes; battery connectors; interconnecting wire; screened cable for loop; mounting hardware to fix unit to bicycle; rubber feet or other fixings to secure circuit board and battery inside case.



**COMPONENTS**  
approximate  
cost **£8** including  
case



The loop shown in position, securing the bicycle to the tree together with a conventional chain security system. The Bicycle Alarm is mounted securely to the saddle bag.

just off, that is bleeper not sounding. Remove the key jack. The relay should now switch on.

Next short circuit the key jack socket, and turn preset VR2 anticlockwise slowly until the relay just

switches on again. If the short circuit is removed, that is the key jack socket is left open circuit, the relay should remain on. The relay should only switch off when the key jack is inserted.

Having become familiar with this procedure, more accurate and selective settings can be achieved by using a higher resistance than one kilohm instead of an open circuit, and a resistance lower than one kilohm instead of the short circuit.

Now that the presets are set, plug in the key jack and connect the wire link. Remove the key jack.

The relay should remain off. Removing the link should activate the relay. If the link is replaced, the relay should remain on due to the action of diode D1. The only way it can be deactivated is by replacing the key jack.

## TROUBLE SHOOTING

If the circuit does not perform correctly, check again for bridges, dry joints, and incorrect breaks in the tracks. Check the positions of all the components and if all is well use a voltmeter to check the voltage actually reaching the i.c. (positive pin 14, negative pin 7).

With both presets turned fully clockwise, and neither jack inserted, pin 3 should be high (nearly 9V), pin 4 high, pin 10 low (about zero), and pin 11 high. If the key jack is inserted and the presets turned fully anti-clockwise, pin 3 should be low, pin 4 high, pin 10 low and pin 11 high.

Next turn preset VR2 fully clockwise, and VR1 fully anti-clockwise. Insert the key jack only. Pin 3 should be high, pin 4 low, pin 10 high and pin 11 low. Finally connect the loop wire. This should have no effect on the previous readings. However if the key jack is withdrawn, pin 3 should still be high, pin 4 high, and pin 11 low. (The voltage at pin 10 should not be measured, as in so doing, its state may well be changed.)

These tests should locate the faulty section of the circuit. If all the readings were satisfactory, the fault must lie in R3, TR1, or the relay circuit. Having found the problem, and cured it, do not forget to reset the presets as described earlier. ✧



## Mail Order

Continuing my remarks on the subject of the purchase of components by Mail Order, I would like to make some further suggestions. I will assume that you have equipped yourself with four or five reputable catalogues, and you are ready to start.

If you have studied them carefully you will have noted particularly what each one does not stock, or in what areas choice is limited. You will now be in a position to say that you will order transistors from dealer A, variable capacitors from dealer B and so on. Now, you can commence sending out your orders.

To avoid the risk of repeating myself I will make the following points.

- (1) Always print your name and address clearly in block capitals.
- (2) If the items in the catalogue have catalogue numbers, be certain to quote them.

- (3) If the firm sends you their order form, make sure you use it.
- (4) Make sure you send the correct money and it's not a bad idea to allow a little extra for inflation.

Many firms work on a fixed rate of postage, and the way to make this work in your favour, is to send one large order, instead of several small ones.

Remember that in to-day's economic climate most of us are operating with the minimum of staff, and the sort of thing that depresses us, is the customer who writes in and says, "In 1975 in Everymans Electronics, there was a circuit for a *Super Burper*, please quote me for all the parts". The poor old dealer knows it will give him at least forty minutes work, and he will also probably discover during his investigations that there is at least one vital part that is no longer available.

It is, therefore, quite obvious he is wasting his time. Even if this is not the case, the chances are, that the customer will

probably decide that it is too dear and change his mind.

## Delivery Time

How quickly can you expect your goods once you have posted your order? If we assume you write your order on Sunday afternoon, it will be collected Monday and your supplier might have it by Tuesday. If he is really efficient, and has everything in stock, he might get it out the same day, but he probably cannot afford first class post, so it will probably arrive at your home Thursday or Friday.

I have, of course, assumed a set of ideal conditions, which do not always apply. If you are a real enthusiast, and I am sure you are, if only in the making, none of this will worry you, because you will plan ahead all the time.

First of all you will get together all the parts for project number one, and then while you are building this, you will select project number two, and begin ordering the parts for this. Unless you are very unlucky, you will have assembled all you require for project two, before you have finished project one.

I think it is worth while mentioning here that many firms will grant credit facilities which means you can order your requirements by telephone, a time saver.

I would like at this juncture to tell our many friends in Southern Ireland, that since they detached their currency from ours, we have to pay 70p on each cheque or postal order, they send us, to have it cleared by the English Banks. If therefore I receive £1.35 made up of two Irish Postal Orders, and if I try and cash them, I wind up minus five pence!

# NEXT MONTH



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# Everyday ELECTRONICS

NOVEMBER 1980  
ISSUE ON SALE  
FRIDAY, OCTOBER 17

# Everyday News

## OPEN TO COMMENT

The latest chapter in the fiery debate on the need for a UK Citizens Band radio service (CB) was given added fuel with the publication recently of the Government's Green Paper *Open Channel—a discussion document*.

The message from the document is clear, the Government is in favour in principle of the introduction of a personal short range radio system in this country provided certain conditions can be met.

The Home Office is recommending a frequency allocation somewhere above 928MHz to achieve minimum interference problems.

### Frequency Allocation

Why 928MHz? After careful studies the document says "that the 27MHz band used for CB abroad and for illegal transmissions in the UK is inappropriate for this country. This is because the band is already allocated to legitimate uses, such as hospital paging systems and model control. Moreover, other services such as broadcasting, emergency services communications, old people's alarms and aircraft landing system outside the band can also be affected by illicit 27MHz use."

The paper went on to state that in addition to the rising demand for use of the spectrum, there are other constraints on frequency policy grounds. "We must take into account our international obligations when choosing a frequency, and it would be useful if we could choose one with at least some prospect of international standardisation".

Great importance is stressed in the timescale that a suitable frequency can be allocated to the Open Channel. Although it has been suggested that the redundant 405-line television service, bands 41-68MHz and 174-216MHz, could be used it points out that it will be some years, probably 1986, before any other services can be located here.

Equipment used should have a range of 15km (10 miles) in open countryside, but obviously in built-up city areas the range would be considerably less—probably down to "line-of-sight" (3 to 5km). For social services such as car to car in traffic jams,

ship to shore from small pleasure boats and between groups of climbers and walkers this should prove adequate. Hand portable equipment should be capable of communications over 1 to 2km in large cities.

The document concludes that the only suitable frequency band is in the new mobile radio allocation around 900MHz. The United States and Canada are giving serious considerations to setting up an up-market range to its existing service, and authorities in Western Europe are also strongly interested. This would give British manufacturers a chance to export.

If a frequency above 928MHz were selected, interference could be kept to a minimum, since there would be no direct frequency relationship between the Open Channel service and the television services, although this frequency may still cause interference to some users of TV and hi fi equipment.

The Government are going to look further into the problems of frequencies before making a final decision.

### Controls

The document proposes that there should be close technical control of manufacturers of Open Channel transmitters to ensure high standards of manufacture.

It also proposes that users should pay an annual licence fee to operate certified sets. As the system would have to be self financing the cost of the licence would probably be related to the present amateur radio licence fee, presently £6.40.

### Summary

The Government is, in principle, in favour of the introduction in the UK of a freely available personal two-way radio communication to be known as Open Channel. This would be of limited range and rather different from what is thought of as "citizens band" radio in other countries.

The discussion paper is intended to help people to understand what Open Channel would involve and to balance its benefits and

drawbacks and would like to receive readers comments.

Copies of *Open Channel—a discussion document*, can be obtained from the Officer in Charge, Home Office Supply and Transport Branch, Royston Road, Caxton, Cambs CB2 8PN.

All comments should be sent by 30 November 1980 to the Radio Regulatory Dept, Home Office, Waterloo Bridge House, Waterloo Road, London SE1 8UA.

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All aspects of CB Radio, so popular in Germany, were discussed during this years *Hobby Electronics Show '80* held in Stuttgart, West Germany. (To date we have not received their final findings.)

This years exhibition for practical electronics and micro-computers had a special "Action Centre" where visitors were able to see displays of amateur radio, CB radio, tape/slide synchronisation and special model railway exhibits. During the past year radio controlled cars and model ships controlled by microprocessors have come to the fore and these were strongly represented.

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### HOME COMPUTERS

The purchase by Lasky's of *Micro-digital* of Liverpool has brought Lasky's into the home computer market. Apple computers, distributed by *Micro-digital*, will be retailed through Lasky's 40 UK stores and backed up by *Micro-digital's* programming experience.

### INMOS LIVES

Inmos is to get its second £25 million tranche for the establishment of a UK micro-electronics plant for high-volume memory products.

The Inmos preference for the plant to be sited in Bristol near their technology centre has been overruled, and the new factory is expected to be built in South Wales and to provide 2,000 new jobs over the next three or four years.

### AWARD FOR FLOWERS

An award that will annually mark the contribution of one engineer to telecommunications science and engineering was launched by British Telecom recently.

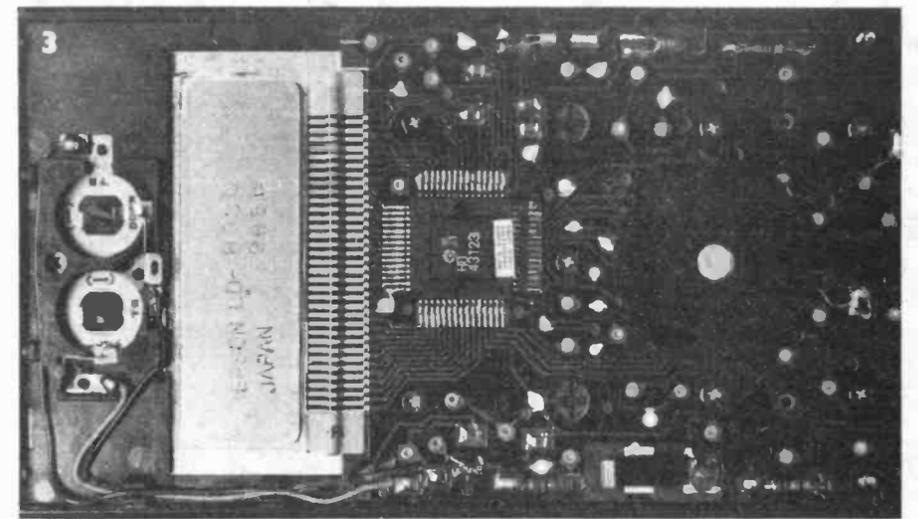
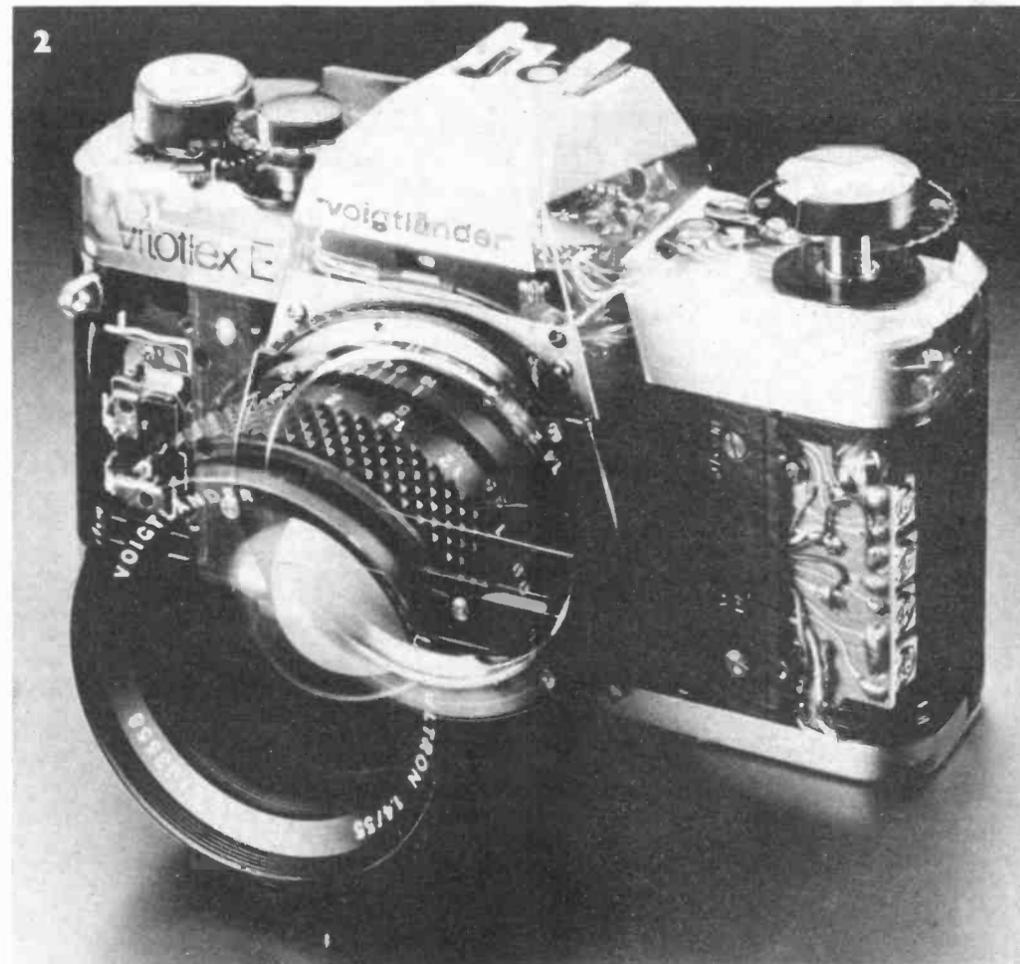
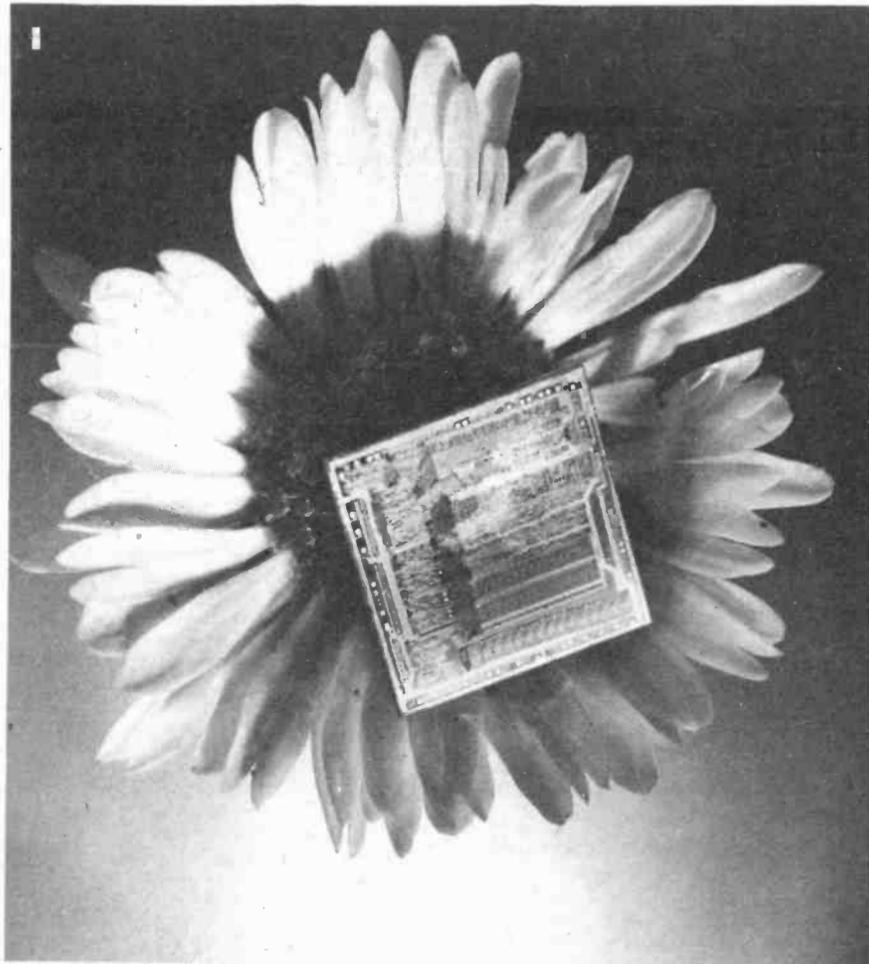
Called the Martlesham Medal, its first recipient was Dr. Tommy Flowers, the man who invented Britain's and possibly the world's first computer and the acknowledged father of electronic switching.

The award, to mark outstanding achievement in telecommunications, will be presented annually to former or present members of British Telecom.

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The much heralded 64K RAM is finally available to the general market. *Crellon Electronics Ltd*, a leading electronic component distributor, hold an advance stock of the *Motorola MCM6665L25*.

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a verbal warning by synthesised speech of an impending fault and will be able to keep a record of the servicing. (The microprocessor is an i.c., albeit a rather complex and larger device than the more commonplace i.c.)

The great advantage of the use of integrated circuits is that they enable complex circuits to be made in a small volume at much lower cost than would be possible using separate transistors, diodes, resistors and capacitors. Integrated circuits have already had a great effect upon our lives, but the impact will be still greater in future years.

#### INSIDE THE I.C.

Inside its protective package an integrated circuit contains a miniature silicon chip on which a large number of individual electronic components (transistors, diodes, resistors and capacitors) have been fabricated by automated photographic masking techniques. Thus a single monolithic integrated circuit can contain most of the components required for a circuit to perform a certain purpose.

Unfortunately it is not possible to fabricate certain components on a

BY J.B.DANCE M.Sc.

# introducing MICROCIRCUITS

#### WHAT'S IN A WORD

The uninitiated may well be confused by the jargon surrounding electronics. A striking example is the term *Silicon Chip*, and its aliases, as employed by the media.

So let us clarify the terminology before anything else.

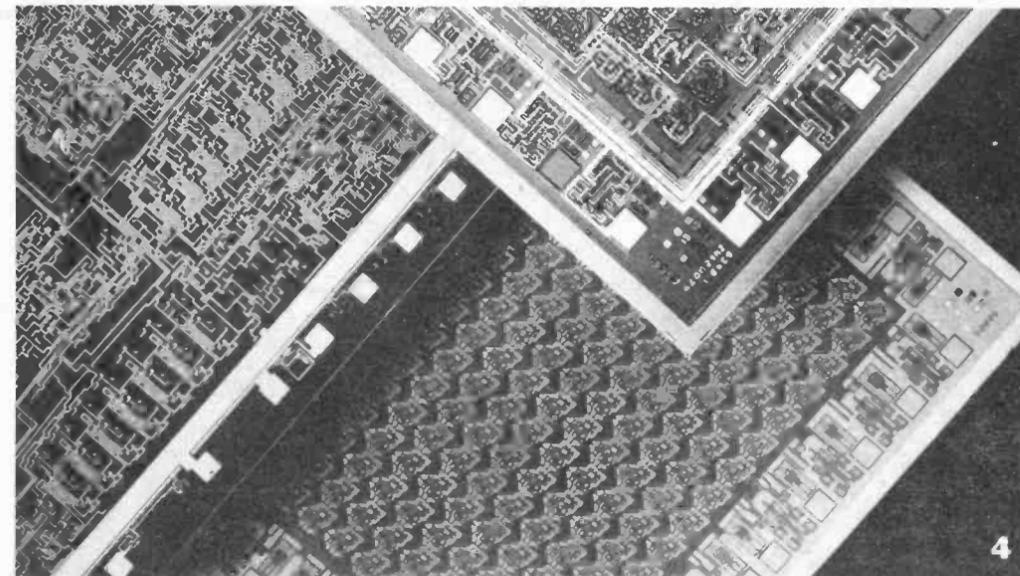
During the past twelve months or so, much publicity has been given to one of the chief marvels of electronic technology. This is an electronic component manufactured on a tiny piece of silicon and incorporating a complete circuit. It is popularly referred to as a *Silicon Chip*, *Microchip* or *Microcircuit*, or sometimes more simply as just "the chip". All these terms are apt, but in technical circles these devices are commonly known as *Integrated Circuits*.

Integrated circuit is generally abbreviated to "I.C." In text this appears as i.c., while in circuit diagrams and component lists such devices are identified with a reference number preceded by IC (capitals), for example: IC1, IC9.

INTEGRATED circuits are widely used in all types of modern electronic equipment. They are employed in large numbers in computers, in modern electronic telephone exchanges and in almost all professional electronic equipment, as well as in military and space vehicle equipment.

Extensive use is also made of integrated circuits in the consumer equipment we meet in everyday life, such as electronic calculators, washing machines, watches, electronic camera shutters, record player circuitry, radio and television receivers and in ancillary television equipment such as teletext, Prestel, television games and computer displays.

It is certain that new designs of car will contain more integrated circuits. The more expensive vehicles will include microprocessor control of many functions; indeed, the microprocessor will even be able to provide



1. A silicon chip containing the complete circuit for a 16-bit microprocessor, on a wild daisy. (Ferranti)

2. Microcircuits allow automatic selection of shutter speed and aperture size. (Ferranti)

3. A single i.c. with few external components found in a modern calculator.

4. Final stages of the Ferranti ULA process: (left) uncommitted state, (top) interconnect mask, (right) committed ship. (Ferranti)

silicon chip. For example, it is not possible to make capacitors of even a moderately large value on the chip, so when such a capacitor is required, a connection is brought out from the chip to a suitable external capacitor. Similarly inductors are not made on a chip, so external inductors must be employed in radio tuning circuits, and the like.

In addition, user-interactive components such as loudspeakers, light emitting diode displays, variable capacitors and variable resistors must be external to the chip.

Strangely enough the microscopically small circuit on a silicon chip is usually considerably more complex than a similar circuit designed for the same application using separate or discrete individual components. This is because the cost of incorporating a few extra components on a silicon chip is negligible when averaged out over the large number of integrated circuits of that type which the manufacturer expects to sell. It makes sound economic sense to add extra "on-chip" components if this will avoid the necessity for an external component which cannot be fabricated on the chip.

Although we have been talking about silicon chips (from which all current production devices are fabricated), it is interesting to note that integrated circuit manufacturers have great hopes for the future of devices employing gallium arsenide chips.

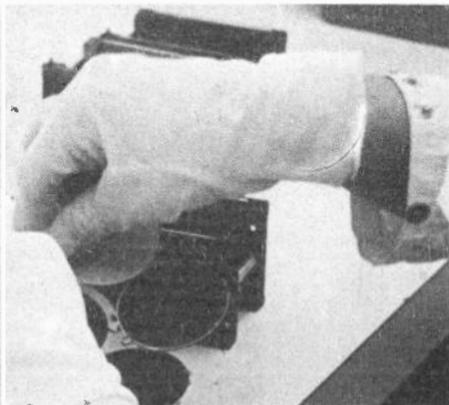
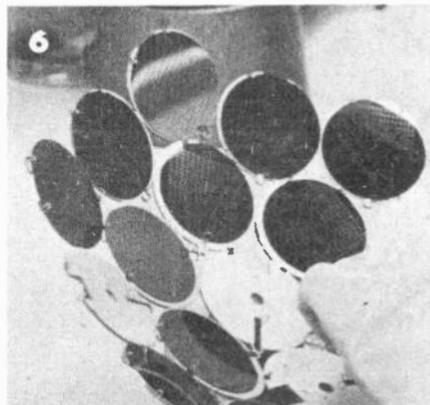
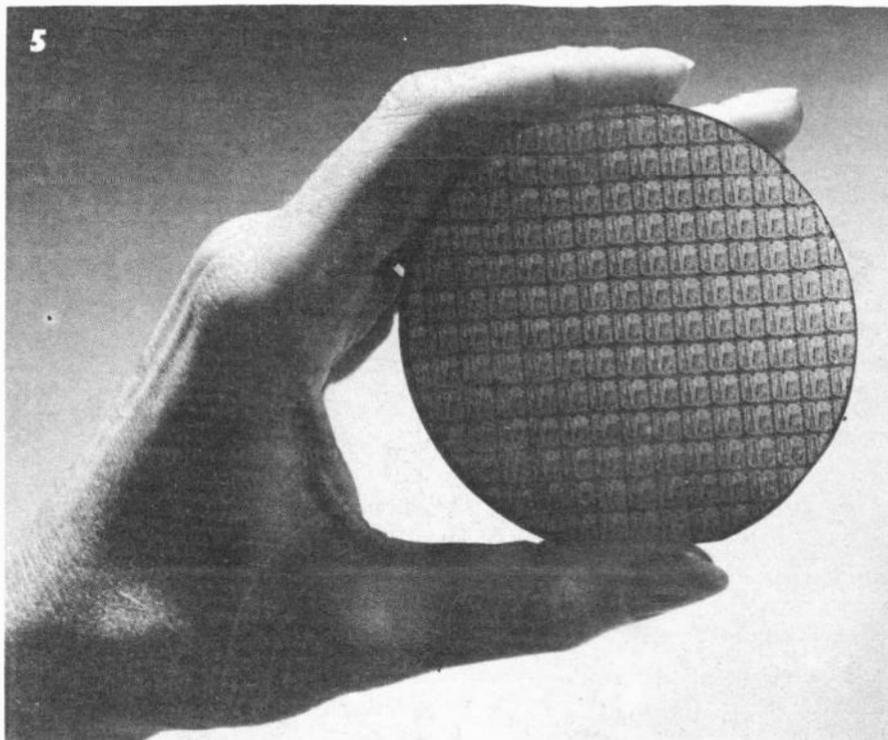
#### MAIN ADVANTAGES

One of the main advantages of integrated circuit technology is that all of the connections within the chip are made quite automatically by photographic masking techniques during production. This is a vital consideration in these days of high labour costs when the expense of wiring up an electronic circuit using discrete components is very high.

In addition, the connections made automatically inside an integrated circuit are very reliable over the lifetime of the device—far more reliable than the connections made by a person using a soldering iron.

Although it is true that external connections have to be made to an integrated circuit with solder in the normal way, the numbers of these connections is very small compared with the number of connections made automatically inside the device. Thus the failure rate in equipment due to the failure of an external soldered connection is very low.

The constructors of electronic equipment can save a great deal of space through the use of integrated circuits, since the numerous components in each of these devices are included on a single chip. This is a vital consideration in such varied



applications as space vehicles and electronic watches.

#### COST

It is very expensive to set up the masks and equipment required to produce a new type of integrated circuit, but once the production line is in operation the cost of producing each additional device of that type is extremely small. Thus the cost of a device depends mainly on the estimated sales volume.

In practice one finds that many of the simpler integrated circuits retail at prices only about two or three times that of a cheap transistor in spite of the fact that they contain perhaps a hundred components. Complex devices containing thousands or even tens of thousands of devices on a single chip are naturally more expensive, but are very cheap for the job they can do.

#### PACKAGING

Each silicon chip must be enclosed in a suitable package to prevent damage by contamination with moisture or dust and to facilitate external connections. Some of the cheapest integrated circuits are supplied in dual-in-line packages which consist of a black plastic body with connecting pins on each side of the body bent downwards at right angles to the body. The two lines of pins on each side of the body give rise to the name dual-in-line (d.i.l.).

Circular metal can packages with wire connections coming from the base are also common. The wires of this transistor-type package are arranged in a circle and in some cases these are preformed to be d.i.l.

Various other type of package are also employed, for example, when a device must be able to dissipate a high power level, a package which

## ... from the World of Electronics



#### Police/Fire Change

One of the effects of new frequency allocations following last year's World Administrative Radio Conference is that broadcasting on v.h.f. is to be expanded up to 180MHz.

Britain's police and fire service radio will now have to be re-equipped for new wavebands at an estimated cost of £50 million at today's prices. The programme, however, will not start until near the end of the decade as the new frequency allocations are not effective until 1990.

Due to expansion of business and increase of personnel Transam, the computer specialists, have moved to new premises opposite the Ministry of Defence at 59/61 Theobalds Road, London WC1.

Production of the Triton and Tuscan computers will be increased with TCL software, a subsidiary of Transam, expanding its own activity to include more emphasis on applications software.

#### Home Cameras

Japanese manufacturers are working on all-solid-state lightweight TV cameras using charge-coupled devices (CCD) for use in the home.

A market of 2 million cameras is forecast as a follow-on to the expected boom in VTRs. CCD cameras at reasonable cost could be available by 1983 according to some industry pundits.

#### GLOBAL RADIO

Global radio cover, which will enable ships anywhere in the world to contact the mainland, is now possible through a new arrangement made by British Telecom with the Japanese telephone authority.

The arrangement just reached expands the Marisat system which provides communications with ships through satellites. It means that telephone and telex

Mullard Ltd, have supplied a Signetics "Super-Twin" video games development system to Century Electronics Ltd, Oldham. It forms part of a major games development facility which has been set up by Century Electronics, representing an initial investment of around £60,000 over the next six months.

#### Infrared Security

A new type of coded identity card is used on the latest Plessey time-control and security-access equipment. It uses a coded filter layer embedded in the card which responds to an infrared beam of light.

It is claimed that the card is far more tamper-proof and difficult to duplicate than the magnetically coded cards now in common use.

#### Telematics

Telematics is a new word for the 1980s and beyond. It has been coined to describe the convergence of telecommunications, computers and related equipment as in the electronic office, electronic mail and electronic information systems.

The telematics market has the biggest and fastest growth potential for the future.

users in the UK will now be able to reach ships in the Indian Ocean via the Japanese satellite earth station at Yamaguchi, south west of Hiroshima.

Over 300 ships are now equipped with Marisat global satellite communications equipment. Any of these ships can be telephoned ship-shore without the annoying fading and distortion common to conventional radio transmission.

#### Licences Cancelled

Radio-controlled model and metal detector hobbyists will no longer need official licences to operate their equipment when regulations exempting users are introduced by the Government within the next few months. Neither will licences be required by users of pipe locators.

This does not absolve in any way the 150,000 users of metal locators/cable finders from the need to obtain permission to enter, search and dig land and to keep off protected archaeological and other sites when treasure hunting.

#### ANALYSIS

##### THE SPOKEN WORD

It must be nearly 50 years ago that the Girl with the Golden Voice emerged from a competition among the many thousands of telephone operators then employed. She had the distinction of recording the time at intervals for the whole 24 hours for the GPO Talking Clock, a sensation at that period. People used to dial TIM (there were letters as well as figures in those days) just for the delight of hearing a beautifully modulated voice with precise diction.

At London's Heathrow Airport this old-established principle is being revived in a new application called Automatic Volmet, a continuous weather-reporting service transmitted by radio for the benefit of pilots and navigators. Existing Volmet services at all major airports throughout the world use live announcers, all speaking English which is the international language for air traffic.

As may be imagined, there are many and varied accents which frequently lead to difficulty in comprehension. How sensible, then, to introduce a "standard" Volmet voice world-wide, which would soon become familiar to aircrew of all nationalities.

The voice of Automatic Volmet is that of Colonel John West, lately of Her Majesty's Royal Signals. There was no competition to discover this new Golden Voice. He just happened to be on the spot as marketing manager of the Military Communications Division of Marconi Space and Defence Systems who designed Automatic Volmet.

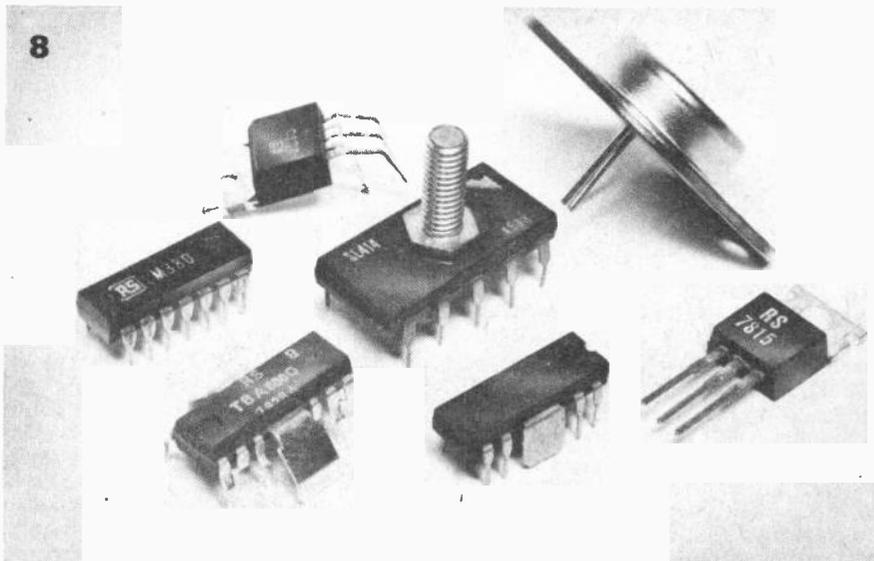
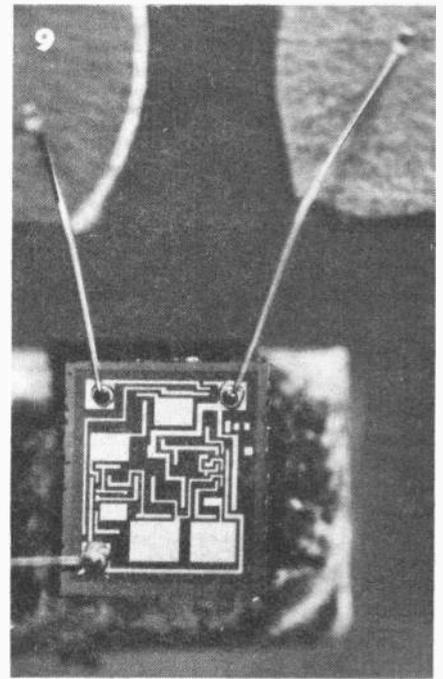
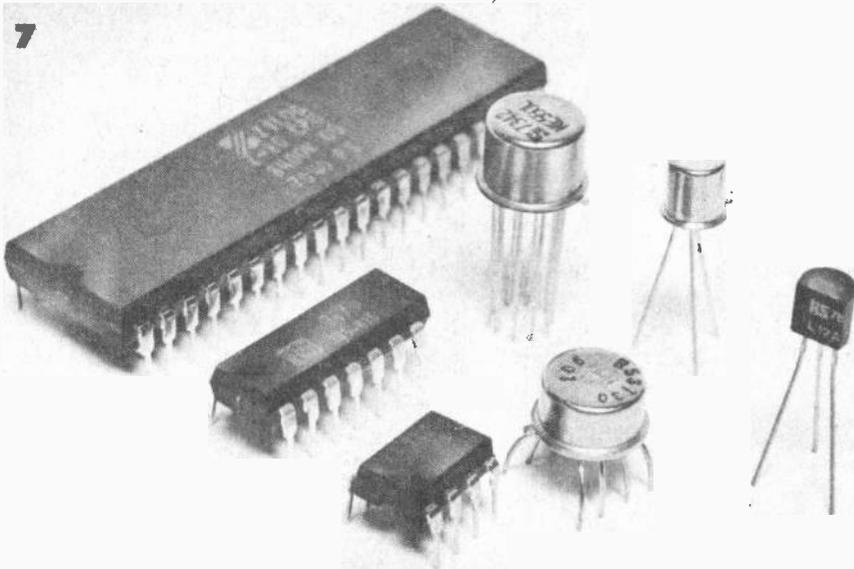
Nonetheless, all agree that his voice is well matched to the application. He has recorded all the standard meteorological phrases, words and figures which have been digitized and stored in a computer memory so that any combination can be selected at will for transmission.

The Heathrow system allows weather reports from selected groups of airports to be transmitted simultaneously over four radio channels. The weather data arrives by telex and is automatically converted by the equipment to a number code which controls the voice output from the computer memory, thus providing automatic and instant up-date of the Volmet transmissions without human intervention.

Note that Automatic Volmet uses a real voice, that of John West. It could be argued that a really slick up-to-date system should dispense with an old-fashioned human voice and use artificially generated synthesized speech. This may yet come when clarity and vocabulary are adequate. But for the time being the John West voice is the best solution and far superior to the "Donald Duck" sound so common in present synthesized systems.

I note, however, that Texas Instruments who pioneered low-cost speech synthesis in their Speak & Spell teaching aid four years ago are now releasing chips to other manufacturers and have embarked on a massive development programme for exploitation of solid-state speech technology. So we may reasonably expect that before long we hobbyists will be using the technique in construction projects.

Brian G. Peck



5. A "slice" of silicon containing many identical i.c.s.—the chips. (Plessey)

6. One of the many stages in the i.c. manufacturing process. Protective clothing is worn in a clean room. (Plessey)

7. Some of the more common packages for encapsulating low power i.c.s.

8. Audio power amplifier and voltage regulator power packages, most with means for easy connection to heatsinks.

9. The common ZN414 radio i.c. showing connection between chip and the device leadouts. (Ferranti)

can be bolted to a heat sink is employed. In many cases the same basic integrated circuit is made available in various types of package.

### SOCKETS

Sockets are readily available for dual-in-line devices and somewhat less readily available for circular metal can type devices. Although the cost of using a socket is comparable with the cost of the cheaper integrated circuits, the constructor will find that it is much easier to change devices when a socket is employed than when a dual-in-line device has been soldered directly into a circuit board.

However, great care should be taken when inserting or removing devices from sockets or damage can occur. Insertion and extraction tools are available for this. Devices can be easily removed from a socket by in-

serting a thin screwdriver blade under each end of the body of the device in turn so as to lift it gently out of the socket. If any pins of the device are bent, they should be carefully straightened with forceps and pliers.

### LINEAR AND DIGITAL

Most integrated circuits can be conveniently classified as either linear or digital types.

Digital devices usually employ binary logic in which the voltage or current at each point in the circuit can have only one of two possible values at an instant. Calculators and electronic watches are examples of products using digital circuits.

Linear integrated circuits operate with voltage and current levels of any value between certain limits. For example, the output of a power amplifier driving a loudspeaker can

have any voltage or current level up to a certain maximum value. This output voltage is proportional to the voltage at the input of the amplifier, so if the output voltage is plotted against the input voltage, a straight line or *linear* graph is obtained. This is the reason why circuits such as power amplifiers are known as linear devices.

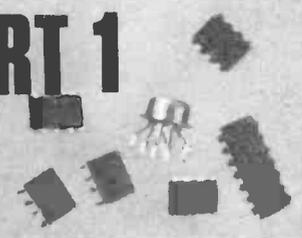
The circuit designer has a vast array of linear devices from which he can select the type most suitable for his needs. Some manufacturers offer thousands of linear products. Linear devices are used for voltage regulation, in timing circuits and in many types of consumer circuits for radio and television.

However, the operational amplifier or "op-amp" is probably the best known of all linear devices. Audio amplifiers are a type of op-amp designed for a specific purpose. □

NEW SERIES

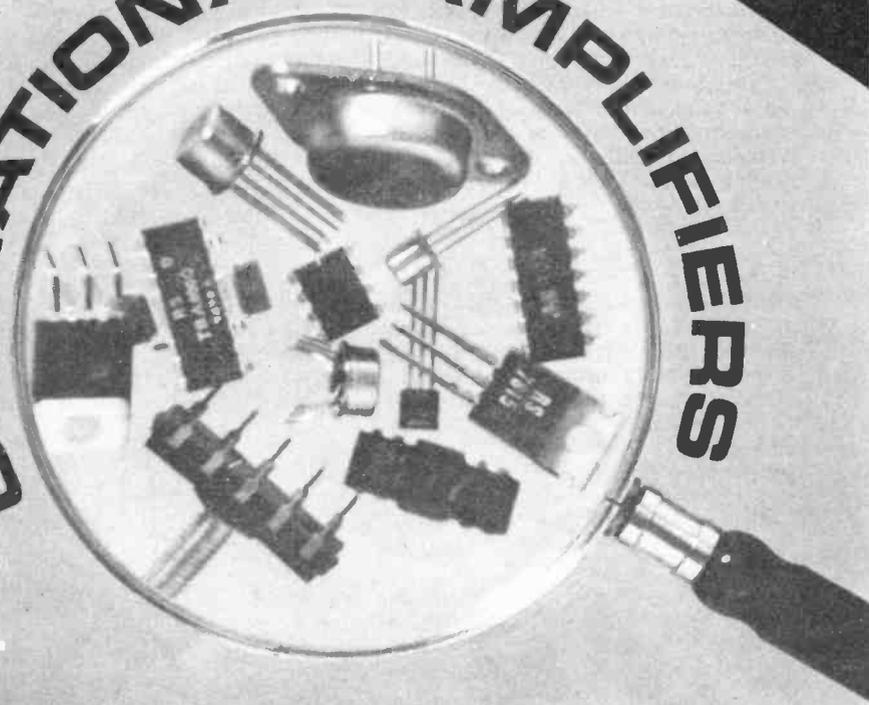
# ICs

## EXPLAINED PART 1



by J.B.DANCE M.Sc.

# OPERATIONAL AMPLIFIERS



OPERATIONAL amplifiers were originally high gain amplifiers operating down to zero frequency which were used in analogue computers to perform mathematical operations, such as addition, integration, etc. Discrete components were used in the early operational amplifiers, but nowadays it is far easier and cheaper to employ an integrated circuit.

Modern operational amplifiers are used for a very wide variety of purposes, although the name operational amplifier is still retained. They are best regarded as gain blocks. The cheapest operational amplifiers are readily available at some tens of pence, but some high performance "instrumentation amplifier" types are priced at tens of pounds.

The purchaser of an operational amplifier can use it in circuits without knowing about the details of its internal design; this is the type of approach we shall adopt.

### EARLY DEVELOPMENT

The first linear monolithic device was marketed about 1962, but the first device with a reasonably high performance was the Fairchild  $\mu A709$  which was introduced in 1965. This device is still a fairly well-known operational amplifier which is available from most of the large semiconductor manufacturers.

Linear devices are therefore little more than fifteen years old—but what an impact they have made in recent years! Initially linear devices were expensive and strange to circuit designers, but they are now very common.

### BASIC CIRCUITS

Operational amplifiers have a very high voltage gain, typically of the order of 50,000 (94dB); this *open loop voltage gain* ( $A_{VOL}$ ) is measured with no feedback applied. In practical circuits the gain is reduced by employing a negative feedback loop, this

reduced gain being called the *closed loop voltage gain*.

The advantage of using a high gain amplifier with the gain reduced by negative feedback is that the properties of the circuit, including the gain, depend only on the values of the external components and not on the performance of the amplifier itself which will vary from device to device.

### INVERTING AMPLIFIER

A basic inverting operational amplifier circuit is shown in Fig. 1.1, the operational amplifier itself being represented as a triangle on its side with the output at one of the points. The word "inverting" means that the output is in opposite or anti-phase with the input; in other words, as the input becomes more positive, the output becomes more negative and vice-versa. For simplicity, the power supply connections to the amplifier are not shown in Fig. 1.1.

There are two inputs to the operational amplifier itself, the one marked "+" being the non-inverting input and the one marked "-" being the inverting input. As the signal input is fed to the inverting input in Fig. 1.1, the output is out of phase with the input.

If the input voltage to  $R_1$  rises by a very small amount say  $V_i$ , this will tend to raise the voltage at the inverting input and the output voltage

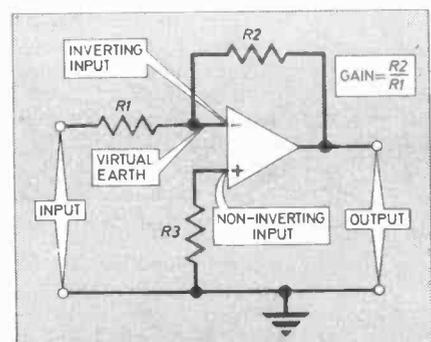


Fig. 1.1. The basic inverting operational amplifier circuit. Power supply lines have been omitted for clarity.

therefore falls. This fall in voltage is fed back through  $R_2$  and tends to cancel the increase in the input voltage which produced it.

The gain of the amplifier itself is extremely high and therefore the fall in the output voltage,  $V_o$ , will be large enough to almost cancel the rise in voltage at the input of the amplifier. Thus the input of the amplifier remains virtually at earth potential and is known as a "virtual earth" point.

## GAIN

The impedance at the two inputs is so high that they take hardly any current. A current therefore flows from the input through  $R_1$  and  $R_2$  to the output. As the potential of the

close to earth potential and the above reasoning will then be invalid.

Ideally  $R_3$  should be approximately equal to the value of  $R_1$  in parallel with  $R_2$  so as to minimise the effect of the small amplifier input currents flowing in the resistors. The input resistance of the circuit is almost exactly equal to the value of  $R_1$ , since the right hand side of this resistor remains at about ground potential.

## THE 741

The type 741 operational amplifier device is suitable for use in this type of circuit, typical component values for various voltage gains being shown in Table 1.1. It should be noted that the *bandwidth* (the frequency at

amount which we will call  $V_o$ . Part of this latter rise is fed back to the inverting input. The inverting and non-inverting input voltages must rise by almost equal amounts or the difference between them will be multiplied by the very high gain of the 741 device and cause a large change in the output voltage.

The voltage fed back to the inverting input is equal to  $V_o$  multiplied by  $R_2/(R_1+R_2)$ , since  $R_1$  and  $R_2$  form a normal voltage divider. Equating the two input voltages gives

$$V_1 = V_o \frac{R_2}{R_1 + R_2}$$

Hence,

$$\text{Gain} = \frac{V_o}{V_1} = \frac{R_1 + R_2}{R_2} = 1 + \frac{R_1}{R_2}$$

Table 1.1 Gain and Bandwidth for the circuit of Fig. 1.1.

Gain Factor	Gain (dB)	$R_1$ (k $\Omega$ )	$R_2$ (k $\Omega$ )	Bandwidth (kHz)
1	0	10	10	1000
10	20	1	10	100
100	40	1	100	10
1000	60	0.1	100	1

Table 1.2 Gain and bandwidth for the circuit in Fig. 1.2.

Gain Factor	Gain (dB)	$R_1$ (k $\Omega$ )	$R_2$ (k $\Omega$ )	Bandwidth (kHz)
10	20	9	1000	100
101	40	10	100	10
1001	60	100	100	1

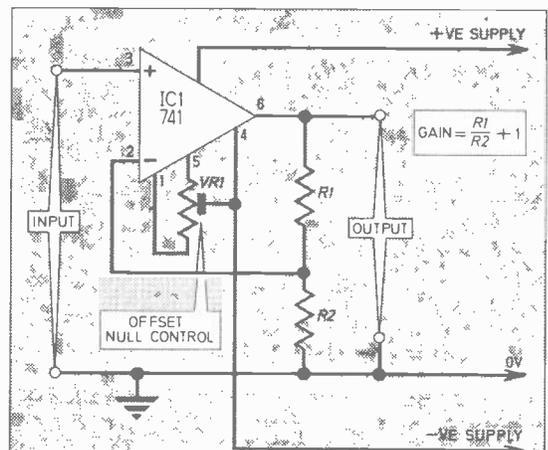


Fig. 1.2 A non-inverting amplifier circuit using the common 741 type op-amp. The preset VR1 allows the quiescent output voltage level to be adjusted.

input is nearly zero, the current passing through  $R_1$  is  $(V_1/R_1)$  and the current through  $R_2$  is  $(V_o/R_2)$ . These two currents are approximately equal, since the amplifier input takes little current.

Hence

$$\frac{V_1}{R_1} = \frac{V_o}{R_2}$$

and

$$\text{Gain} = \frac{V_o}{V_1} = \frac{R_2}{R_1}$$

Thus the gain of the whole circuit is determined by the ratio of these two resistor values. Indeed, one of the advantages of this type of amplifier is that the low frequency gain remains constant and can easily be adjusted by choosing suitable values of  $R_1$  and  $R_2$ .

The gain of the amplifier itself should be much greater than the closed loop gain of the circuit or the inverting input will not remain very

which the gain reduces to one half of its low frequency value, a measure of the maximum useable frequency) decreases with increasing gain. This type of circuit may be employed as an audio amplifier or for other purposes within its frequency limitations.

Both positive and negative power supply lines are required when the 741 is used in this type of circuit. Normally  $\pm 15V$  supplies are used, but if lower supply voltages are employed, the maximum swing of the output voltage is more limited.

## NON-INVERTING AMPLIFIER

In the operational amplifier circuit shown in Fig. 1.2, the input voltage is applied to the non-inverting input of the 741 device. The output is therefore in phase with the input. Initially we will ignore VR1.

If the input voltage rises by a very small amount  $V_1$ , this will cause the output voltage to rise by a small

If  $R_1$  is much larger than  $R_2$ , the gain is approximately equal to  $R_1/R_2$ .

This type of circuit has a much higher input impedance than that of Fig. 1.1. Ideally the impedance of the input source should equal  $R_1$  in parallel with  $R_2$  in order to minimise gain errors due to the amplifier input currents.

## PINNING

The pin connections for the 741 shown in Fig. 1.2 are for the 8-pin dual-in-line package or for the circular metal (TO-99) package. This device is also available in a 14-pin dual-in-line package with a different pin numbering.

The potentiometer VR1 connected between pins 1 and 5 allows the quiescent voltage at the output to be adjusted to zero. Typical component values are shown in Table 1.2 for various gain values.

## THE 709

The 741 device contains a 30pF capacitor formed on the silicon chip which reduces the gain at high frequencies and ensures stability. However, the earlier 709 device does not have this internal capacitor and external capacitors must be used to provide "frequency compensation" and stability.

A typical inverting amplifier using the 709 is shown in Fig. 1.3; it may be compared with the basic 741 circuit of Fig. 1.1. The pin numbers shown are for the 14-pin dual-in-line encapsulation, but the 709 is also available in a circular metal can (TO-99) and an 8-pin d.i.l. package with different connections.

## FREQUENCY COMPENSATION

The components C3 and R4 provide input frequency compensation, whilst C4 provides compensation in the output section of the device. The component values may be selected as in Table 1.3 for various values of the circuit gain. It should be noted that the bandwidth obtainable at high gain is considerably greater than with the 741 circuits.

The 741 device includes protection against short circuiting of the output by a circuit which limits the output current to about 25mA. The resistor R5 is included in the output of the Fig. 1.3 circuit to limit the 709 output current, since there is no short circuit protection in this device. There are no provisions for the adjustment of the offset voltage in the 709 in the way VR1 is used in Fig. 1.2.

Small capacitors C1 and C2 are included in the power supply lines in Fig. 1.3 to provide high frequency decoupling. They should be used in

all operational amplifier circuits in addition to the electrolytics in the power supply unit. Although the electrolytics provide a high capacitance for low frequency decoupling, they have a high inductance and do not provide satisfactory decoupling at high frequencies. C1 and C2 should be mounted close to the integrated circuit.

The power supply for the Fig. 1.3 circuit may be  $\pm 15V$ , in which case outputs of up to about  $\pm 14V$  may be obtained. Smaller supply voltages may also be used when smaller output voltage swings are satisfactory.

Table 1.3 Gain and bandwidth for the circuit in Fig. 1.3.

Gain Factor	Gain (dB)	R1 (k $\Omega$ )	R2 (k $\Omega$ )	R3 (k $\Omega$ )	R4 (k $\Omega$ )	C3 (pF)	C4 (pF)	Bandwidth (kHz)
1	0	10	5	10	1.5	5000	200	450
10	20	10	9.1	10	1.5	500	20	700
100	40	10	10	1000	1.5	100	3	600
1000	60	1	10	1000	0	10	3	300

The input voltage swings should be limited to  $\pm 5V$  at the device inputs. A high or low input voltage to the 709 can cause the output to "latch up" and not return to its normal value when the input voltage is removed, but this cannot occur with the 741.

## COMMON MODE

If an input signal is applied to both the inverting and non-inverting inputs, it will have a relatively small effect on the output voltage; this type of signal is known as a *common mode input*, as opposed to the normal *differential input* which is applied only to one of the inputs.

It should be noted that the voltage difference between the two inputs can

be only a fraction of a millivolt or the output will approach one of the supply line voltages. Even if the two inputs are joined to ground, the output voltage of a practical amplifier is not zero. The difference between the input voltages required to make the output voltage zero is known as the *input voltage offset*; it is typically a few millivolts.

## SENSITIVE MICROAMMETER

A simple and instructive use of the 741 device involves its use as a sensitive microammeter. The circuit of

Fig. 1.4 provides a full scale deflection for an input current of  $1\mu A$ . The potentiometer VR1 sets the zero of the scale when the input current is zero.

When a current of  $1\mu A$  flows into the input of the circuit and passes through R1, it will develop 1mV across this resistor. This 1mV is amplified by the gain of the circuit, namely, by  $R2/R1=200$  to produce an output voltage of 200mV. If the combined resistance of the meter and VR2 is 2 kilohm, the current passing through the meter will be  $100\mu A$  and a full scale deflection will be obtained.

## INVERTING MODE

The amplifier is used in the inverting mode and therefore if pin 2 be-

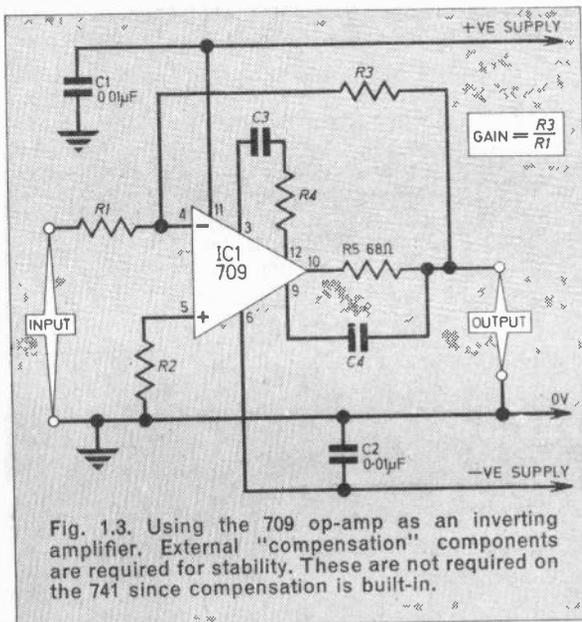


Fig. 1.3. Using the 709 op-amp as an inverting amplifier. External "compensation" components are required for stability. These are not required on the 741 since compensation is built-in.

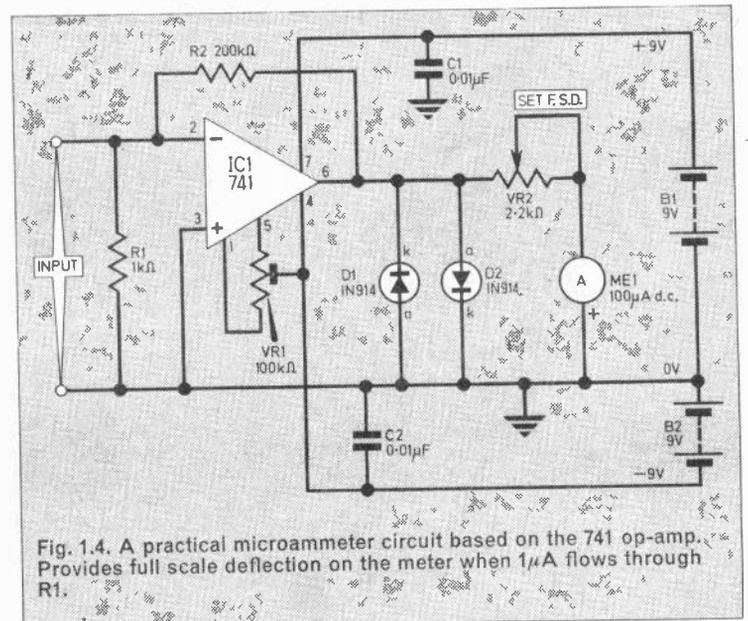


Fig. 1.4. A practical microammeter circuit based on the 741 op-amp. Provides full scale deflection on the meter when  $1\mu A$  flows through R1.

comes more positive, the output becomes more negative, which explains why the meter is connected with its negative side to pin 6. If desired, however, a centre reading 100-0-100 $\mu$ A meter may be used for measuring input currents which flow in either direction.

The two diodes D1 and D2 protect the meter against overloads. Similarly diodes may be placed across the resistor R1 to protect the 741 input circuit.

This circuit can be calibrated by feeding a current of 1 $\mu$ A into it and

adjusting VR2 for a full scale deflection. Such a current can be obtained by using a supply of exactly 10V and connecting it through an accurate 10 megohm resistor to the input.

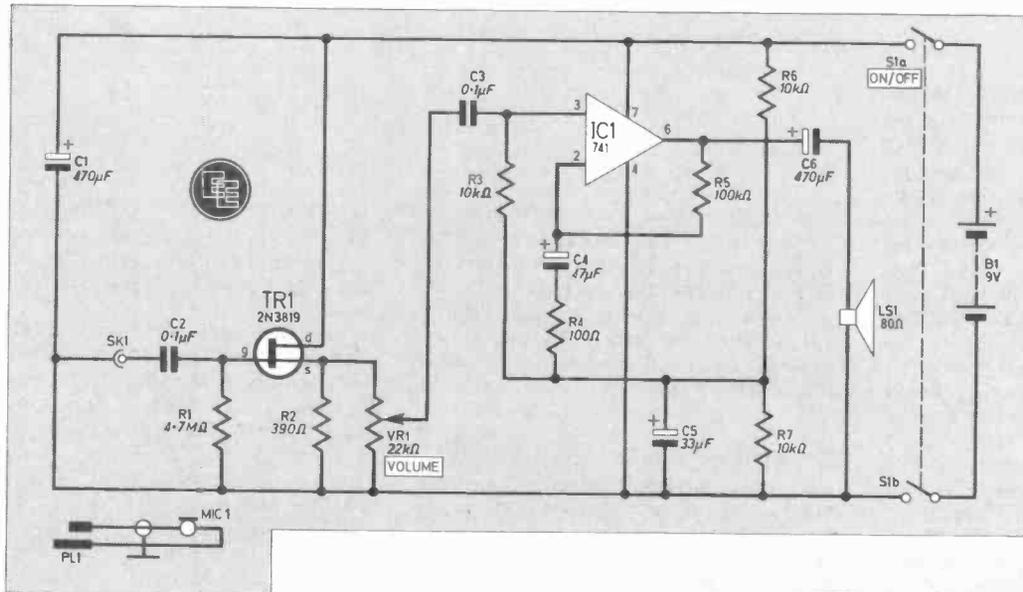
This same circuit can be used as a meter having a full-scale deflection of 1mV.

-15V, but two 9V batteries may be used. It is always wise to connect 0.01 $\mu$ F capacitors from each of the power supply lines to ground to reduce the chance of instability; these capacitors should be wired directly across the operational amplifier connections using wire which are as short as possible.

### POWER SUPPLIES

The circuits described require balanced power supplies. Ideally these should be stabilised at +15V and at

Next month. Part 2 of this series will continue with a discussion of other amplifier devices, including those used for practical audio circuits.

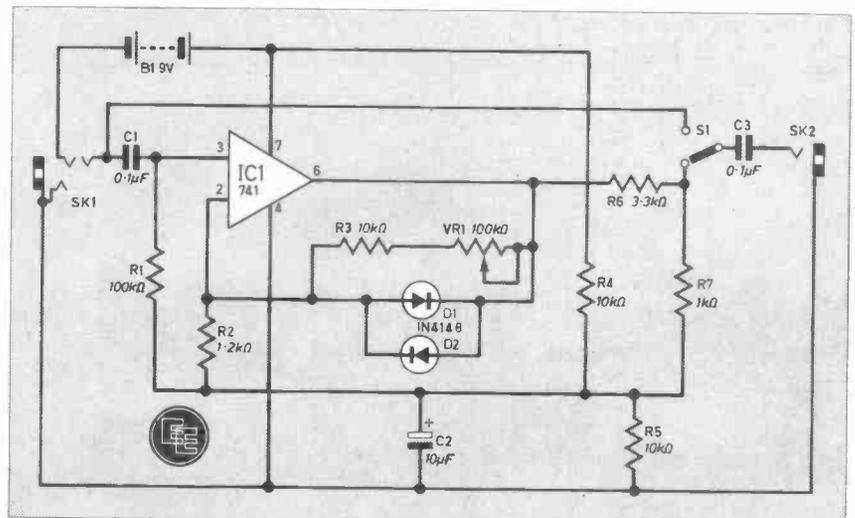


**TWO  
FOR  
YOU  
TO  
TRY**

Fig. 1.5. The circuit diagram for a simple Baby Alarm using a 741 op-amp. The microphone needs to be a crystal type. This circuit can also be used as a high impedance sensitive amplifier. (Previously published in EE November, 1979).



Fig. 1.6. The circuit diagram for a Fuzz Box sound effects unit for guitar based on a single 741 type op-amp. (Previously published in EE December 1978).



# LETTERS

## Patterns On Film

Will you please advise me on a problem I have concerning the making of printed circuit boards. I am unsure of the exact way to go about it. I know I can get the patterns (transfers), the board with an all-over coating of resist and the ferric chloride. I am also aware of ink resist pens to be applied direct to the board. The problem is that I had the idea that one could transfer the pattern to the board by some sort of photographic process, but I do not know how to go about this.

I dare say that I have missed an article on this topic in E.E.

F. A. Craig  
Maidstone, KENT

*Photographic means for producing p.c.b.s is just one of the many options available to the home constructor and detailed descriptions of the various methods are published from time to time in the pages of E.E. Such a feature is likely to appear in the near future.*

What is required here is an actual-size master of the p.c.b. pattern on film or transparent paper, for example tracing paper. This can be realised with the aid of rub-down transfers on the film (or paper) which is laid over the actual-size pattern appearing in the article, and copied. Long or intricate interconnections are best produced with p.c.b. tape or Indian ink.

The finished pattern is placed on top of the photo-resist coated board and held flat to this by use of a piece of plate glass for example, and then exposed to ultraviolet light for between 5 and 10 minutes. The action of the u.v. light on the resist is to soften the exposed areas and make them soluble in a developer (sodium hydroxide solution) leaving exposed the regions of copper to be etched in the normal way.

Photography can also be used to reproduce the pattern on film by "taking a picture" of the pattern and having the negative enlarged and reversed (black on white) to the required size.

## Spurious Alarm

I have recently completed the construction and installation of the *Intruder Alarm* published in the May 1979 issue of *EVERYDAY ELECTRONICS*. Having made this circuit for elderly relatives, I now find myself in the embarrassing position of being told by them that the alarm is being triggered on after it has been set at night when the bedroom light is switched off prior to their retiring for the night. At all other times the alarm functions perfectly.

Can you offer an explanation for this and possibly a remedy?

J. R. H. Hunter  
Eastwood, NOTTS

*A number of constructors of this project have experienced similar false triggering, but not, we hear, as a result of lights being turned off (or on) but have traced the triggering time to co-incide with the turning on or off of refrigerators, deep-freezers and washing machines. This could be due to the voltage spikes that are produced when inductive loads, such as the electric motors in these appliances, are turned on or off.*

*If the Intruder Alarm is on the same "loop" as one or more of these household items, then these voltage spikes can find their way along the supply line into the Alarm and to the gate of the thyristor in this circuit causing it to turn on.*

*These spikes can be induced in other loops in the building if the loops run parallel for any appreciable distance. If possible the Alarm should be plugged into a loop not containing any of the above appliances—although this may not be possible in modern houses. You will need to experiment, trying different sockets around the home. In Mr. Hunter's case, it could be that his lighting wiring runs parallel with that to the socket powering the unit.*

*It was a constructor who found a remedy for this and informed us. Two additional capacitors are required: a 0.1 $\mu$ F*

*mounted across the terminal block, positions 5 and 6, and a 2.2 $\mu$ F connected across pins 1 and 2 of SK1, positive to pin 2 completely eliminated false triggering of this nature.*

## Contact Please

I am a fifteen year old electronics fan looking for pen friends all over the world.

I correspond in German and English and these are some of my hobbies: Programming TI calculators, I possess a TI58C, and I am active in short wave listening (SWL).

If any readers would like to contact me my address is:

Christian Munker,  
V. Ketteler-Strasse 50,  
5060 Bergisch Gladbach 2,  
West Germany.

Christian Munker  
West Germany

## Electronics Club

I recently visited GB on an invitation of an English town band. We even had the great honour to play exclusively for Queen Elizabeth II in Buckingham Palace.

I am interested in musical engineering and bought the June/July 1980 issue of *EVERYDAY ELECTRONICS* for the *Autowaa* and *Autophase* effect units.

I just want to correct one mistake in the abbreviations list (p.437) concerning the use of "DIN".

DIN does not mean Deutsche Industrie Nummer (German industry number).

DIN is equivalent to ASA (have a look on cameras!) and means Deutsche Industrie Norm(en) (German standard(s) of industry) generally used with a following number, for example DIN45 500 (Hi-Fi Equipment).

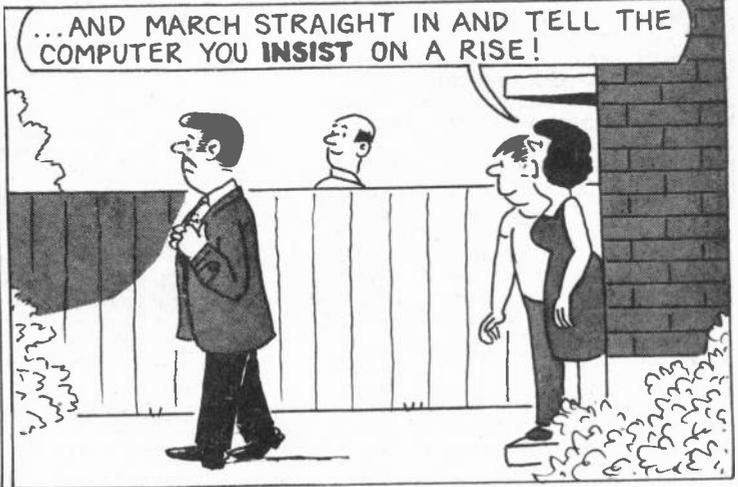
I have founded a constructors club for electronic instruments, including musical and synthesiser projects. We also exchange cassette recordings with our ideas on (in German). There is now a section concerning personal computers.

We would be grateful to hear from any similar clubs in Great Britain. Please write to Manfred Bertuch, Werneweg 58, D-4400 Munster, West Germany.

W. Habermehl  
West Germany

## JACK PLUG & FAMILY...

BY DOUG BAKER



# RADIO WORLD

By Pat Hawker, G3VA

## Companionship

Back in 1976, after looking at CB in the United States and just when the lobby for it was beginning to build up in the UK, I wrote: "The Home Office Radio Regulatory Division should surely be encouraged to explore how modern two-way radio systems could be extended to the public domain for such purposes as traffic information and "companionship" and for the original concept of assisting the private citizen in the conduct of his personal affairs or business activities.

On the other hand there is a strong argument for firmly channelling the hobbyist into amateur radio, where he belongs, with its self-training and technical investigations, possibly by provision of temporary "novice" or "beginner" licences, but with a built-in incentive to progress to the standard licences. Short-range radio has reached the stage where the public at large can benefit by the facilities it provides—is it not time that the UK licensing authorities recognise this?"

Since then, CB in the States has passed its peak (and the industry is now losing rather than making money); the British amateur radio examination has become "multiple-choice" with a much higher pass-rate; illegal 27MHz operation is widespread (though not so much as some claim) and this indeed forms part of its appeal to some enthusiasts; and the CB lobby has grown vocal and respectable.

## Open Channel

On August 5, the Home Office finally published its 14-page "Open Channel—a discussion document" (available free of charge from: Officer-in-Charge, Home Office, Supply and Transport Branch, Royston Road, Caxton, Cambridge CB2 8PN—is it a coincidence that the Post Code should be CB?). Comments are invited by November 30.

There is however little reason to suppose that Open Channel (the name the Government prefers) will be with us legally for many months to come. Not the least because of the considerable problem presented to industry by the need to develop equipment for the proposed, unexpectedly high, frequency band of around 928MHz.

It is this ultra high frequency that has caused the proposals to be coolly received by many enthusiasts. Yet, in many respects, the Home Office document (and the additional information revealed at the press conference by Mr Timothy Raison, Minister of State for Home Affairs) are worthy of careful consideration, and are by no means as illiberal or as restrictive as some commentators would have us believe.

Indeed, frequency apart, the proposals come near to meeting those 1976 suggestions of mine. The aim clearly has been

to produce a system that would cause minimal interference to the public's reception of radio and television broadcasts; minimal interference to other users of the radio spectrum (including public and private communications systems, radio amateurs, etc); yet not ruling out any of the "fun" or socially-useful elements of CB.

What is proposed is a band about 1MHz wide, representing a nominal forty 25kHz-wide channels or twenty 50kHz-wide channels and a licence requirement (hopefully under £10 per annum) but without any official call-signs. Equipment will not need to be formally "type approved" (a process that adds considerably to the cost of normal business radio) but makers would certify that it was in accordance with a Home Office technical specification (not yet formulated); otherwise there would be minimum restriction on, or supervision of, the use made of the facilities.

On the other hand, if Parliamentary time permits, the Wireless Telegraphy Acts may be modified to make it illegal to sell (or advertise for sale) equipment for the 27MHz band, and the Home Office intend to continue to endeavour to enforce the existing regulations against 27MHz operation (and the import of 27MHz equipment).

## Range

The document acknowledges that lower frequencies have been advocated, including not only 27MHz but also around 225MHz and 450MHz. It does not consider the recent suggestion that a channel in Television's Band I (41 to 68MHz) should be used when the 405-line service finally closes, but in any case this is not due to happen until about 1986.

The document argues strongly that the lower frequencies could and would give rise to interference problems, either with existing 27MHz service (radio paging and radio control of models) or with services, including television on nearby or harmonic frequencies. This is indisputable, although some would argue that the assessment of the risks involved for 225 or 450MHz is rather over-stated.

It admits that 928MHz would normally provide only "line-of-sight" range and that in city streets hand-portable or vehicle-to-vehicle range would often be restricted to under a mile. Reference is made to various tests which indicate that this high frequency is capable of providing an effective mobile radio service. Indeed it could be argued that amateur results on a considerably higher frequency (1300MHz) show that under some circumstances (temperature inversions, etc) Open Channel contacts over hundreds of miles should be possible, while hill-top to hill-top ranges should be considerable even under normal conditions.

## Cost of Service

The most telling argument *against* 928MHz is the economic one. Current u.h.f. power transistors (or alternatively varactor frequency multiplier chains) capable of providing say 5 watts output at this frequency, with crystal-controlled stability, are not far short of being "state of the art" and cost prohibitive—and all such devices can easily be destroyed.

If the Home Office is prepared to accept (at least for an initial period) self-excited "super-regenerative" type equipment, cost could be kept to reasonable proportions. Another possibility might be the development of mass-produced low cost SAW (surface-acoustic-wave) oscillators although that still leaves the problem of power amplification.

For the Australian CB allocation at 250MHz, Philips developed a 5-watt mobile transceiver with frequency synthesiser. This design (modified for the UK amateur band at 432MHz) is sold in the UK by Catronics for about £250 (including VAT). It would be difficult (some would say "impossible") to produce an equivalent 928MHz unit even for a larger market without significant extra cost. In other words it might be realistic to expect an Open Channel mobile unit at a cost of say £300 to £400, with extra care also being needed in such matters as coaxial plugs, sockets and cables.

Would this price Open Channel out of the market? There is some evidence that some illegal 27MHz units, selling at say £100 to £150 overseas, have been changing hands in the UK at prices not unlike that indicated for Open Channel.

## Not a Shamateur band

The Home Office make it clear that they want to avoid creating a shamateur-type band: the document states categorically: "If an individual wishes to use sophisticated equipment to communicate over long ranges and make international contacts, he should become a licensed radio amateur by taking the appropriate examination."

The frequency of 928MHz is being considered for auxiliary CB purposes in the USA, Canada and some other countries. The flaw in this argument is that any narrow-band equipment for 928MHz is almost bound to be "sophisticated". In 1947 the USA initiated CB in the band 460 to 470MHz but little use was made of CB until 27MHz was authorised in 1958.

Using 928MHz would be a challenge—but it is to be hoped that the Home Office proposals will be given serious consideration and not just dismissed as unrealistic. It is very unlikely that the Government will ever be persuaded to legalise 27MHz CB in the UK.

ACTUAL SIZE



# mini i.c. RADIO

By F. G. Rayer

**T**HE radio described here is pocket-sized with internal ferrite aerial and speaker. There is space available in the case to fit a socket to suit an 8 ohm earpiece if this is required. This was not included on prototype.

In order to accommodate the 38mm diameter speaker, standard 9V battery, and other items in the small case, the number and size of com-

ponents must be kept small. Building then presents no particular difficulty.

## CIRCUIT DESCRIPTION

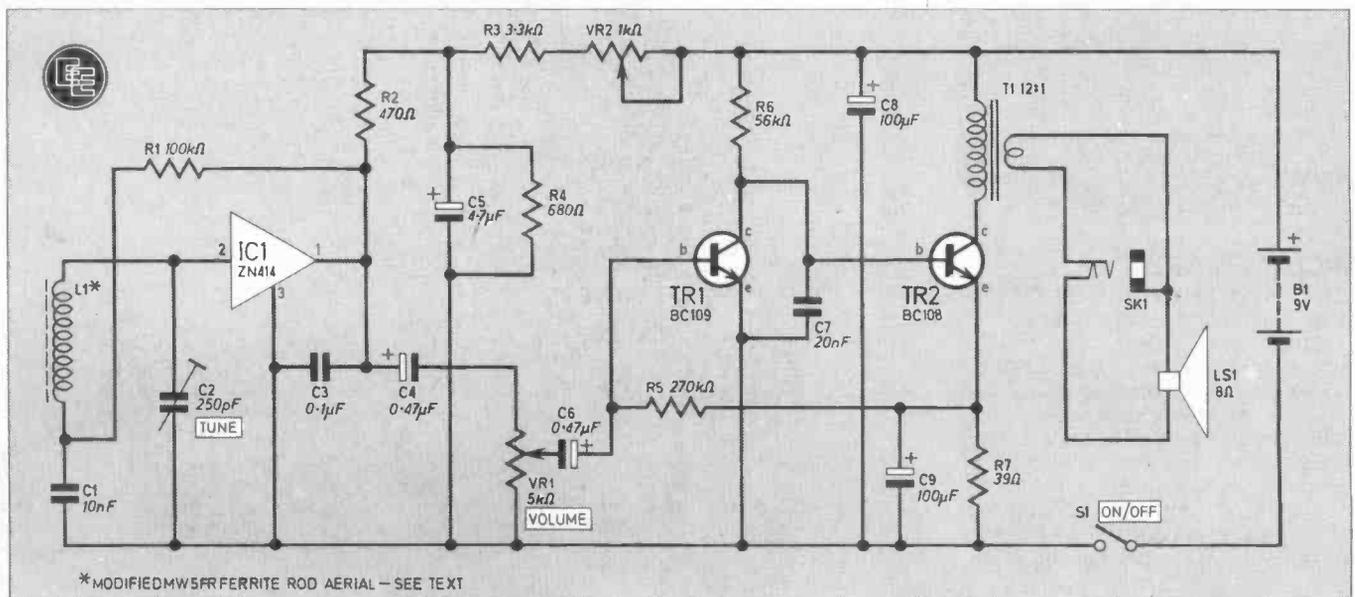
The circuit diagram appears in Fig. 1. The well-known ZN414 i.c. is used which has a series of r.f. amplifiers, detector, and a.g.c. and needs few additional components. The ferrite rod winding L1 is tuned by the com-

pression trimmer C2.

RF input to IC1 is at 2, with audio output at 1, and feedback via R1. The output load resistor R2 receives its supply from the potential divider R3, and R4 with VR2. The latter allows setting for optimum results.

The supply should be between 1.2V and 1.6V but it is found that an unnecessarily low voltage reduces sensi-

Fig. 1. The complete circuit diagram for the Mini I.C. Radio. The optional earpiece socket SK1 is not included on the prototype.



tivity, while if the voltage is too high instability tends to develop. Should VR2 be omitted, R3 should be 3.9 kilohm, but there is then no means of adjusting operating conditions in this way.

Audio signals are routed via C4 to the volume control VR1. This control is necessary as otherwise it is possible to overload the following amplifier section with strong signals. Transistors TR1 and TR2 form a simple but high gain amplifier, d.c. stabilised by feedback via R5. TR2 drives the speaker through the midget transformer T1.

### NOTE ON COMPONENTS

All components should be readily available. The case is in fact made from two Vero cases from the General Purpose Plastic Box range with the lids not being used. The remaining two halves were held securely together by means of "oval" nails pushed into the lid fixing holes. This allows easy access to the inside of the radio for battery replacement.

Due to limited space within the case small-sized components are required, in particular the capacitors. C4 and C6 are required to be tantalum types, and the remaining electrolytics should be as small as possible. The transformer is the type usually used in push-pull circuits and has a ratio 6+6:1, the centre-tap being unused.

L1 is a ready-wound medium-wave winding provided also with a base coupling coil, and as the latter is not required here the few turns of this coil are unwound and removed. The MW5FR as supplied has a 5 inch long ferrite rod. This must be cut to be 2 inches long. C2 is a compression trimmer fitted with a 1/4 in. dia spindle to allow tuning via a knob.



### CIRCUIT BOARDS

Two circuit boards are used in this design, and each have components mounted on both sides. The smaller board accommodates the external controls and is secured to the larger by a small right-angled bracket.

The larger board sits between the two halves of the case and held in position by these and the "oval" nails.

Prepare the larger board, 18 strips × 27 holes. The corners needs to be rounded exactly following the shape

## COMPONENTS

### Resistors

R1	100kΩ	R5	270kΩ
R2	470Ω	R6	56kΩ
R3	3.3kΩ	R7	39Ω
R4	680Ω		
All 1/4W carbon ± 5%			

### Potentiometers

VR1	5kΩ miniature enclosed pre-set—knob operation type
VR2	1kΩ miniature horizontal skeleton pre-set

### Capacitors

C1	10nF disc ceramic
C2	250pF compression trimmer with spindle (Home Radio)
C3	0.1μF polyester or ceramic
C4	0.47μF tantalum bead
C5	4.7μF 6V elect.
C6	0.47μF tantalum bead
C7	20nF disc ceramic
C8	100μF 10V elect.
C9	100μF 6V elect.

### Semiconductors

IC1	ZN414 t.r.f. radio i.c.
TR1	BC109 npn silicon
TR2	BC108 npn silicon

### Miscellaneous

S1	miniature s.p.s.t. toggle
L1	m. w. aerial coil type MW5FR including a ferrite rod (Denco)
T1	miniature push-pull output transformer type LT700
LS1	8 ohm miniature moving coil loudspeaker about 38mm diameter
Stripboard: 0.1 inch matrix 27 holes × 18 strips, 18 holes by 7 strips; case Vero type 202-21025K General Purpose Plastic Box (2 off—see text); control knob; PP3 battery clips.	

See  
**Shop  
Talk**

page 635

**COMPONENTS**  
approximate  
cost **£7**

of the case and holes drilled to align with the fixings. Also make the cut-outs to allow VR1 and C2 to project through the larger board, the bracket fixing holes and the breaks along the copper strips on the underside.

Begin construction with the smaller board making the necessary breaks along the copper strips (as shown in Fig. 2a). The stripboard positions holding S1 and VR1 tags will need

to be enlarged. Fit these and C2 to the board and cut C2 tags short. Remember to attach a small bracket to the board via C2 fixing stud/nut. Bolt the two boards together.

### CASE PREPARATION

Take one half of the case and drill holes so that C2 spindle, S1 and VR1 can pass through. The large board



The completed prototype with lid removed showing the nails that hold the two sections together.

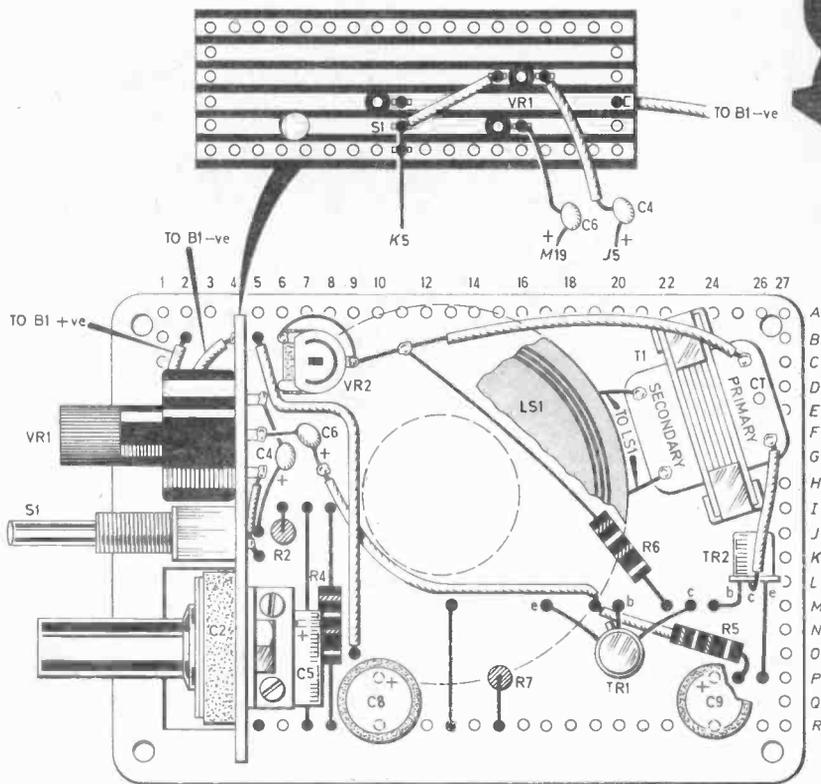
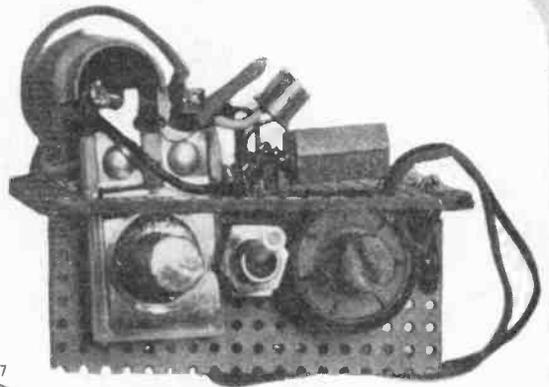


Fig. 2a. The layout of the components on the topside of the stripboard. Only a small section of the loudspeaker has been drawn for clarity. The cone of course faces out of the page. Note the small bracket holding the controls fitted to the second smaller piece of stripboard, details of the latter shown at the top of diagram.



End elevation of the circuit board showing components mounted on both sides, with the smaller board fixed in place.

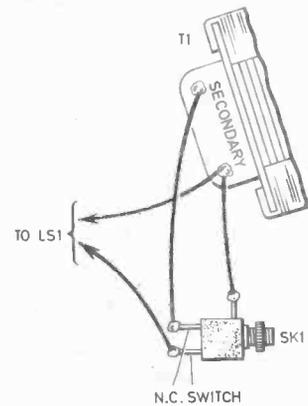


Fig. 3. Modification to be made to Fig. 2b to include an earpiece socket.

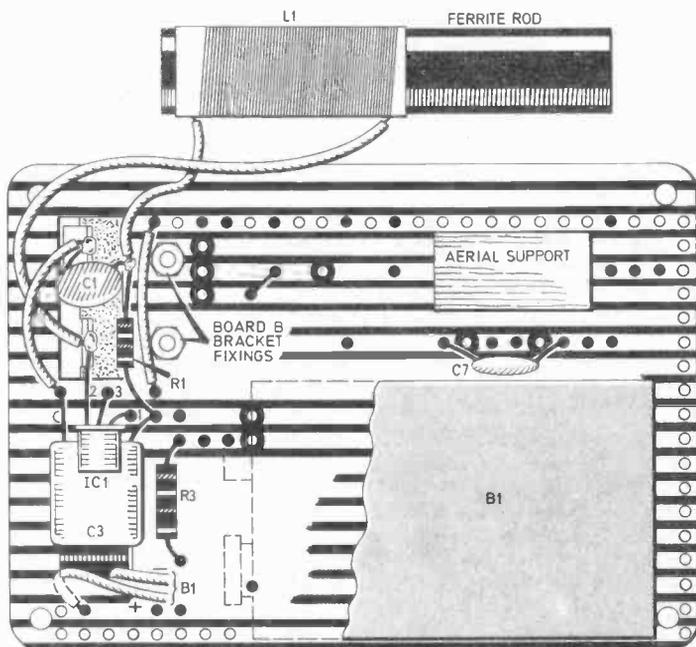
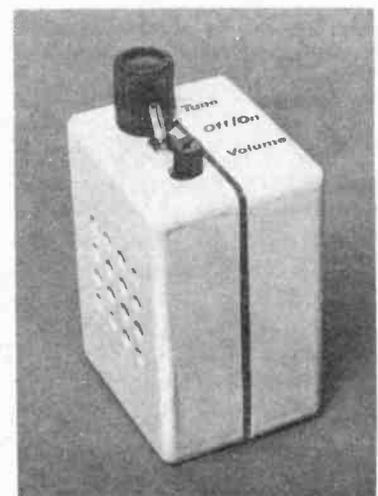
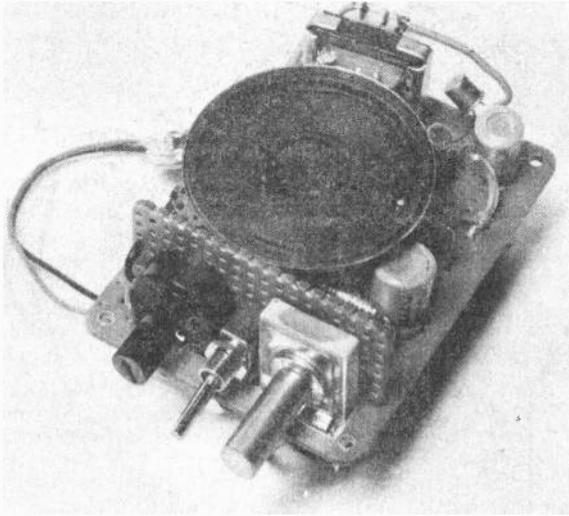


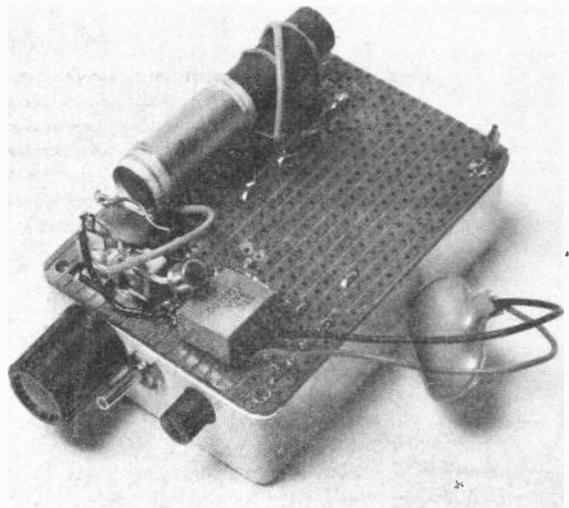
Fig. 2b. The underside of the stripboard showing breaks to be made and position of the components mounted directly to the copper strips. The aerial support is held in place by an elastic band or cord which also secures the ferrite rod in place.

# mini i.c. RADIO





The completed prototype circuit board prior to installation in the lower half of the case. The fixing for the trimmer capacitor holds the L-shaped bracket to the smaller board.



Final stage of assembly. The battery sits on the copper side of the stripboard and held in place by double-sided adhesive foam. This also insulates the battery case from the board.

should lie flat on this section of the case.

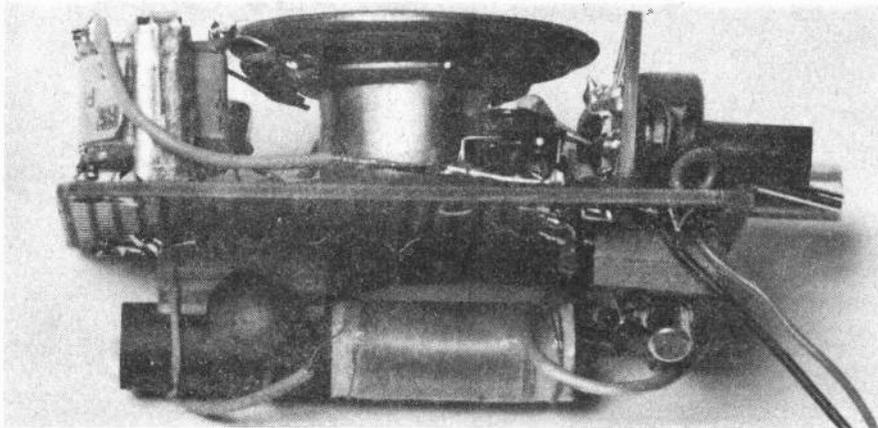
Accurate positioning of the holes can be simplified by drilling them a little smaller, then enlarging with a round file, adjusting the position meanwhile if necessary. C2 and VR1 spindles should clear the holes. S1 hole should be a close fit. Later, one nut is put inside the case on S1, and one on outside, to help hold this part of the receiver secure.

Drill a grid of small holes in the case where the speaker will finally sit, about 3mm in diameter.

When the finished receiver is assembled, the components in Fig. 2a, with speaker, fit permanently in one half of the case. A small piece of card is glued between the speaker and the board. This will press the speaker against the front of the case. The speaker is fitted to the circuit board, so that this can be checked or tested easily as a unit.

The reverse side of the board (Fig. 2b) carries the ferrite aerial, and leaves space for the battery. So only

Side view of the completed circuit board showing in detail the method used for mounting the aerial and its support.



the case back need be removed to replace the latter.

### COMPONENT ASSEMBLY

Component layout on the top side of the board and inter-board wiring is seen in Fig. 2a. Carry out assembly and check that components and connections will be clear of the speaker. The latter should not be fitted until all the wiring is finished. It is then cemented to the folded card (see above), which is, in turn, cemented to the circuit board, with cone upwards to be beneath the holes in this half of the case.

If there is any free space between the speaker and case, when fitted in this way, cut a piece of card to go between the two, with a hole to match the speaker cone, and fit (glue) this inside the case. If wished, there is space for an earphone jack socket on the end of the case.

The remainder of the components are mounted on the underside of the circuit board as shown in Fig. 2b.

A small block of wood with groove is cut to raise the ferrite rod about 6mm above the board. With the ferrite rod/coil assembly in place (elastic or cotton round the rod and through holes of the board will secure the rod) connect the wire ends of L1 to C2/IC1 pin 2 and R1/C1.

Finally attach PP3 battery leads, feeding through the slot as shown. The shaft of C2 may need to be shortened to allow the small tuning knob to be close to the case end.

### ADJUSTMENT

Band coverage can be modified to some extent by moving L1 on the ferrite rod. A suitable position should be found with L1 level with the end of the rod.

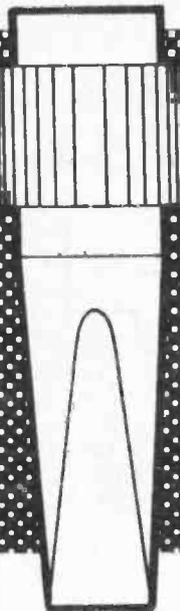
Initially have VR2 set at about mid-way. Later, VR2 can be adjusted so that a high resistance meter shows about 1.3V across C5, or so that instability does not arise at any tuning position of C2. VR2 may be reached by drilling a clearance hole in the board, beneath VR2 for a narrow-blade screwdriver, or it can be set before fitting either part of the case.

Note that the case should be present for proper loudspeaker reproduction, and that it is necessary to turn VR1 back, with strong signals, to avoid overloading and distortion.

The case sections, with board, fit together with the four metal pins (nails) in the corner holes. To change the battery, the back section only is removed, and this is best done by inserting a knife or similar tool so that the back can be lifted away. Foam adhesive tape can be used to hold the battery in place or a thin piece of foam sponge between battery/board, and battery/case will achieve the same result. □

# IRON

# HEAT CONTROL



by A. Sproxtton

A SOLDERING iron will become unnecessarily hot when there is some delay in making joints, and these are usually small so that not much heat is carried away. This causes damage to the bit, and also increases the danger of harm to circuit boards or components. The controller described here is particularly intended to avoid these difficulties.

In use, the heat controller is placed in series with the iron, and is adjusted for the temperature required.

## CIRCUIT DESCRIPTION

The circuit diagram for the Iron Heat Control unit is seen in Fig. 1. Control is obtained by use of a triac, CSR1. Current at mains voltage is fed to the iron element through the triac. This device is normally in the off state, where it exhibits an open circuit. When it receives a trigger on its gate terminal, the triac turns on (short circuit) for the remainder of the half-cycle in which it was triggered.

Thus by choosing the point at which triggering occurs one is able to select the power delivered to the iron and

hence the temperature of its bit. In the circuit of Fig. 1, the triggering point is controlled by the charging time of C1 via R1 and VR1. When the voltage level across C1 reaches the striking voltage of the neon LP1, the neon lights and passes current into the gate of CSR1 turning it on. Thus, the iron bit temperature is controlled by the setting of VR1.

For maximum heat, the triac conducts for virtually the whole of the a.c. cycle. To reduce heat, the triggering angle is reduced, and the triac is then conducting for only a part of each half cycle, so that average power to the iron falls.

With this circuit, the neon was found preferable to a diac, and it also acts as a panel indicator showing that power is on for the iron. When the neon is not lit, no power is available.

Current is drawn from a mains plug receiving power from the usual outlet, and the iron is in turn connected to the controller. Note that the earth conductor E, and neutral N, run without interruption from the mains plug and cord to the iron circuit. The triac control is placed in the Live (L) conductor.

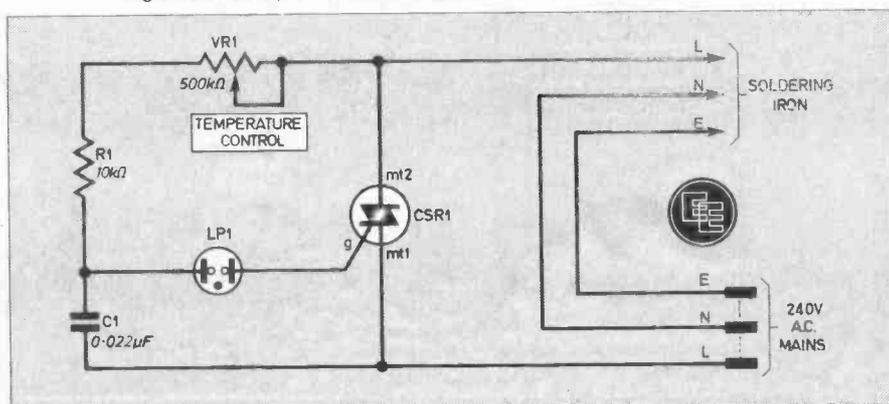
## ASSEMBLY

No circuit board is required in the construction. Some of the components are mounted on the metal front panel of the case and point-to-point wiring employed. The prototype used a standard panel neon with integral limiting resistor. This must be removed. Pull off the neon cover, unsolder and take away the resistor, and solder the free neon lead to the holder tag.

The arrangement of the components on the case lid is shown in Fig. 2. The triac used in the prototype and shown in Fig. 2 has an isolated body which is bolted directly to the metal panel. This also acts as a heat-sink for CSR1. If other non-isolated body types are used, a mica washer with insulating bush(es) should be used.

Stud, TO-3 and TO-66 types are not suitable because at least one terminal would be exposed, but the flat plastic packages are, such as the TIC206D and the TIC226D. These have their metal tabs connected to one terminal and should thus be fitted with mica

Fig.1. The complete circuit diagram of the Iron Heat Controller.



## COMPONENTS

- R1 10kΩ 1W carbon ± 10%
  - VR1 500kΩ lin. carbon
  - CSR1 ECC704 or other mains/3A triac (see text.)
  - C1 0.022μF plastic or ceramic
  - LP1 panel neon without limiting resistor (see text)
- Tag-type terminal strip, 3-way with extended mounting tag; case, plastic with metal lid or all metal (see text), size approx. 115 × 75 × 50mm used in prototype; control knob; mains cable; rubber grommets (2 off); 6BA fixings.

Approx cost Guidance only

£2.50 (see page 635)

washer/bush. Precautions should also be taken to keep its terminals clear of the case.

Note that the panel is earthed via one of the tags on the terminal strip by the earth conductor of the mains cable. This is essential.

The mains cable runs from a 3-pin plug fitted with a 2A or 3A fuse. If a non-fused plug is to be used, a panel fuseholder should be added and fitted to the case. It passes through a grommet in the back of the case. Earth and Neutral leads are soldered directly to the E and N tags of the tag strip. Live runs directly to mt1 of the triac.

Take the plug off the soldering iron cable, and pass the flex through the front grommet; E and N conductors connect to E and N at the terminal tag strip, and L to mt2 of the triac. Take care to follow the correct E, N and L connections.

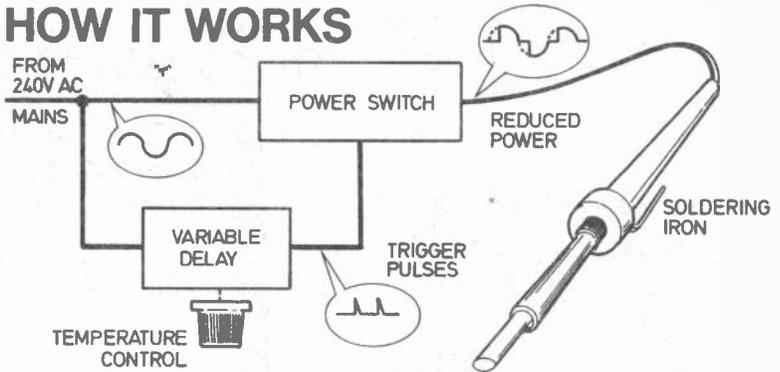
The assembly was fitted into a plastic case. A metal case can be used and earthed with the panel.

## IN USE

To test the unit an a.c. voltmeter may be clipped to the N and L tags of the tag strip. Rotation of VR1 should give a smooth control of voltage, from about 50V minimum up to nearly the full mains voltage.

For average small intermittent work with a 15W to 25W iron, a setting of about 150V should prove to be satisfactory, but this can of course be adjusted as found best in practice.

## HOW IT WORKS



Mains voltage is applied to the power switch which is either a short or open circuit. The mains is also used to derive a pulse from the variable delay network in order to trigger the power switch on, i.e. from open to a short circuit.

The position of the trigger pulse with respect to the mains zero crossing point determines the amount of power delivered to the soldering iron. Thus, very early triggering in the half cycle yields maximum power whereas very late triggering gives minimum power to the iron.

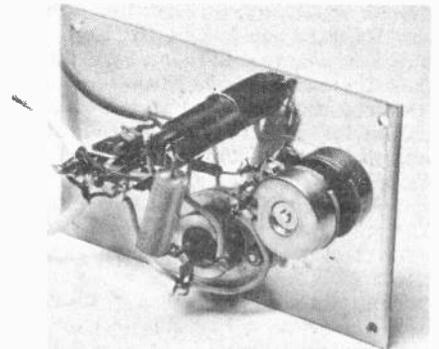
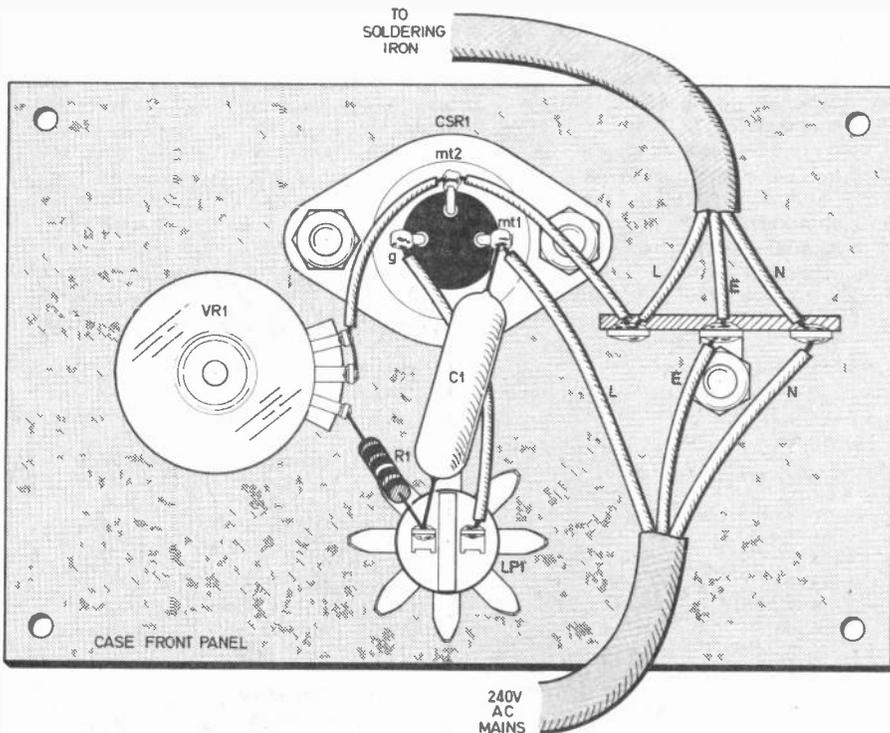
The shaded regions in the "switched" main cycle are proportional to the power delivered.

## MODIFICATIONS

Due to the way in which the circuit operates, maximum power setting of VR1 provides a little under the full mains voltage. This slight reduction was not found of any importance. It is easy to fit a small mains type toggle switch to the panel for maximum or full power, if wished. This switch should be connected from L of the mains cord to L of the iron cir-

cuit, thereby eliminating (short circuiting) the triac when it is closed.

In use, no troublesome interference was noticed, this being in part due to the low power. Various forms of interference suppression are available such as a 22nF 550V capacitor with a 22 ohm 1/2W resistor in series, from mt2 to mt1 of the triac. A similar capacitor from L to E may also be used.



Above shows completed panel of the prototype; (below) finished unit.

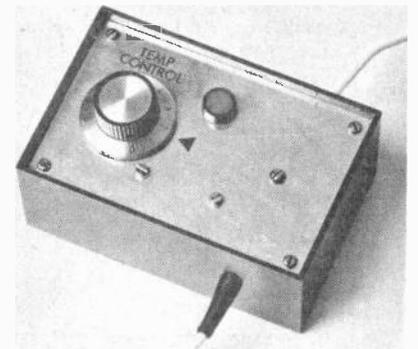
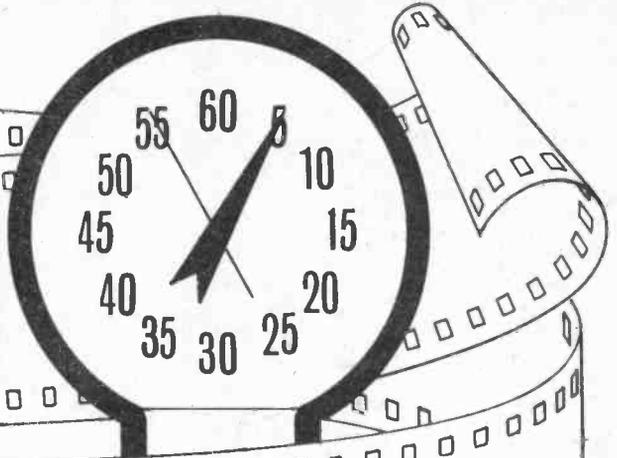


Fig.2. Layout of the components on the case lid and complete interwiring details.

# DARKROOM

# CONTROLLER

BY S. IBBS



**B**Y FAR the most useful piece of equipment in a photographic darkroom is a timer for the enlarger. Using this, a high standard of accuracy can be guaranteed, and good quality photographs depend on high standards.

The large majority of photographers prefer to use a test strip technique to establish the right exposure, rather than using an enlarging meter. This is because a meter is dependent on standard light values, which are almost impossible with different negatives, of different subjects, on different films, taken at different times.

The project here described provides a versatile, accurate enlarging timer that not only controls the safe-light as well as the enlarger (to make initial focussing and framing easier) but includes a red l.e.d. that produces a very short pulse of light every second.

This makes standardisation of test print exposures very simple. The circuit is relatively easy to construct, very reliable, and has eased life considerably for the author.

## THE CIRCUIT

The full circuit of the Darkroom Controller is shown in Fig. 1. It can

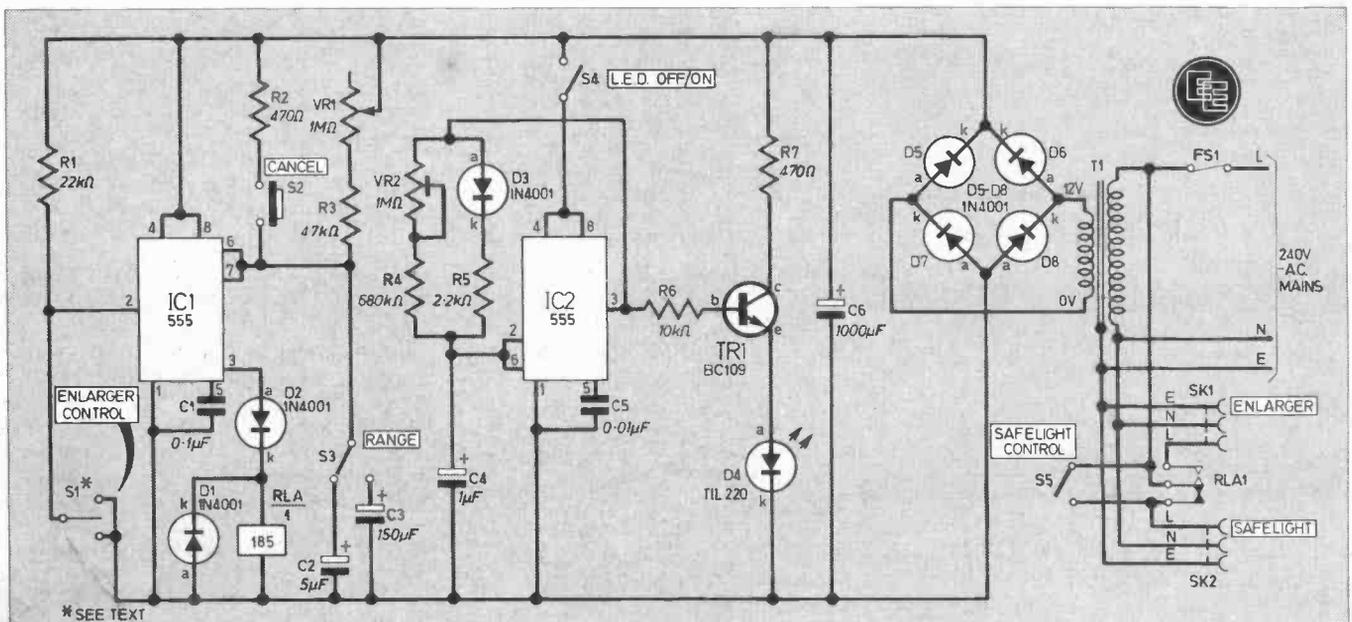
be seen that this consists of two NE555 timer i.c.s. The first one, IC1, is wired as a monostable and timing is initiated by grounding pin 2.

This causes capacitor C2 or C3 to start charging up and pin 3 to produce a high output thus activating the relay.

When the charge on the capacitor has reached two thirds of the supply voltage, the i.c. rapidly grounds pin 7 thus discharging the capacitor and taking pin 3 "low" again.

The time taken for all this to happen depends on the value of the capacitor and the setting of VR1. The particular values chosen for this pro-

Fig. 1. Complete circuit diagram for the Darkroom Timer.



ject give a timing range from zero to about fourteen minutes.

If we wish to keep pin 3 high all the time then pin 2 should be kept at ground potential. The switch S1 is provided for this purpose.

## RELAY

The relay connected to pin 3 of IC1, has one set of change-over contacts and these are wired into the live lead of the enlarger and safe-light.

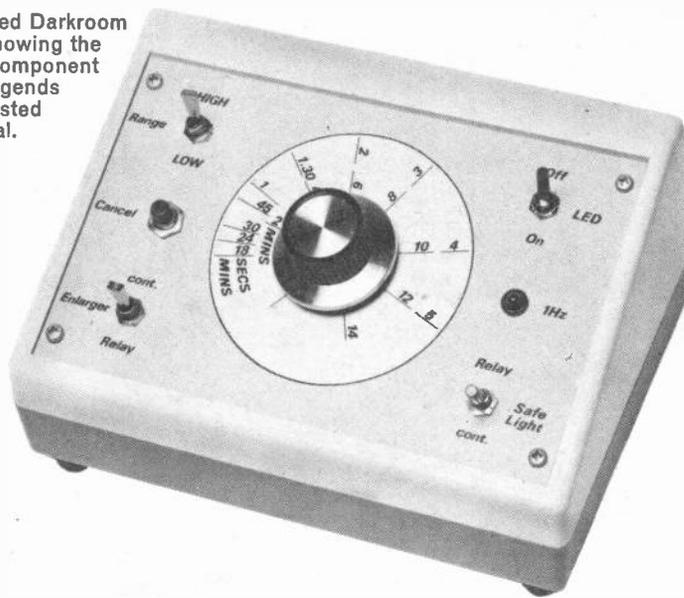
In normal conditions the enlarger is off and the safelight is on, but when the relay coil is activated the contacts change over and the enlarger comes on and the safelight goes off.

There is also a further switch, S5, to override the relay contacts connected to the safelight.

## TIMING SIGNAL

The second timer IC2 is provided to give an accurate timing signal. Here we have a 555 i.c. connected in the astable mode. The time period is set by C4 and the VR2, R4, R5, D3 combination and should be adjusted

The completed Darkroom Controller showing the front panel component layout and legends with a suggested calibrated dial.



so that D4 flashes on and off at the rate of one short pulse every second. This must be a red l.e.d. as this is the colour that most photographic papers are least sensitive to.

Transistor TR1 is used as a buffer to prevent the l.e.d. from drawing too much current through the i.c.

The power supply to the control circuitry is very basic and consists simply of full wave rectified d.c. derived from the mains via step-down transformer T1 and diode bridge D5-D8, with just one smoothing capacitor, C6.

## COMPONENTS



### Resistors

R1	22k $\Omega$	R5	2.2k $\Omega$
R2	470 $\Omega$	R6	10k $\Omega$
R3	47k $\Omega$	R7	470 $\Omega$
R4	680k $\Omega$		
All $\frac{1}{4}$ W carbon $\pm$ 5%			

### Potentiometers

VR1	1M $\Omega$ carbon linear
VR2	1M $\Omega$ miniature vertical preset

### Capacitors

C1	0.1 $\mu$ F polyester type C280
C2	5 $\mu$ F 16V elect.
C3	150 $\mu$ F 16V elect.
C4	1 $\mu$ F 16V elect.
C5	0.01 $\mu$ F polyester type C280
C6	1000 $\mu$ F 16V elect.

### Semiconductors

IC1, 2	NE555 timer i.c. (2 off)
TR1	BC109 npn silicon
D1-D3	1N4001 or other low power silicon diodes (3 off)
D4	TIL220 red l.e.d.
D5-D8	1N4001 50V 1A silicon diodes (4 off)

### Switches

S1	s.p.d.t. toggle, centre off with one pole biased off
S2	push-to-make, release-to-break switch
S3	s.p.d.t. miniature toggle
S4, 5	s.p.s.t. miniature mains rated toggle (2 off)

### Miscellaneous

T1	mains primary with 12V 100mA secondary
RLA	miniature 12V relay, 185 ohms coil resistance with one set of single-pole changeover contacts.
SK1, 2	three pin Bulgin mains socket type P650 (2 off)
FS1	5A cartridge fuse and panel mounting holder
Stripboard, 0.1 inch matrix, 24 strips by 48 holes; sloping front case 171 x 121 x 37mm, Verocase 202-21033A or similar; knob; five amp mains cable; inter-connecting wire; 6BA nuts and bolts for fixing transformer and circuit board.	

See  
**Shop  
Talk**

page 635

COMPONENTS  
approximate  
cost **£11** excluding  
case

**CONSTRUCTION**  
starts here

## CIRCUIT BOARD

The prototype is built on 0.1 inch stripboard, 24 strips by 48 holes. This requires several link wires, so follow the layout diagram in Fig. 2 carefully, and construction should cause no problem.

The two i.c.s can be mounted in Soldercon pins, although low profile sockets can be used if preferred. The board is then bolted to the bottom of the box, as is the miniature transformer. The relay can be glued directly to the circuit board or fixed using double-sided adhesive tape.

When doing the interwiring, check at each stage of construction to make sure that you have made no mistakes. The relay used has changeover contacts so a live mains lead is taken to the centre contact, and a wire is taken from the terminal normally connected to the safelight.

A switch is also wired across these two terminals so that mains can be fed direct to the safelight, bypassing the relay.

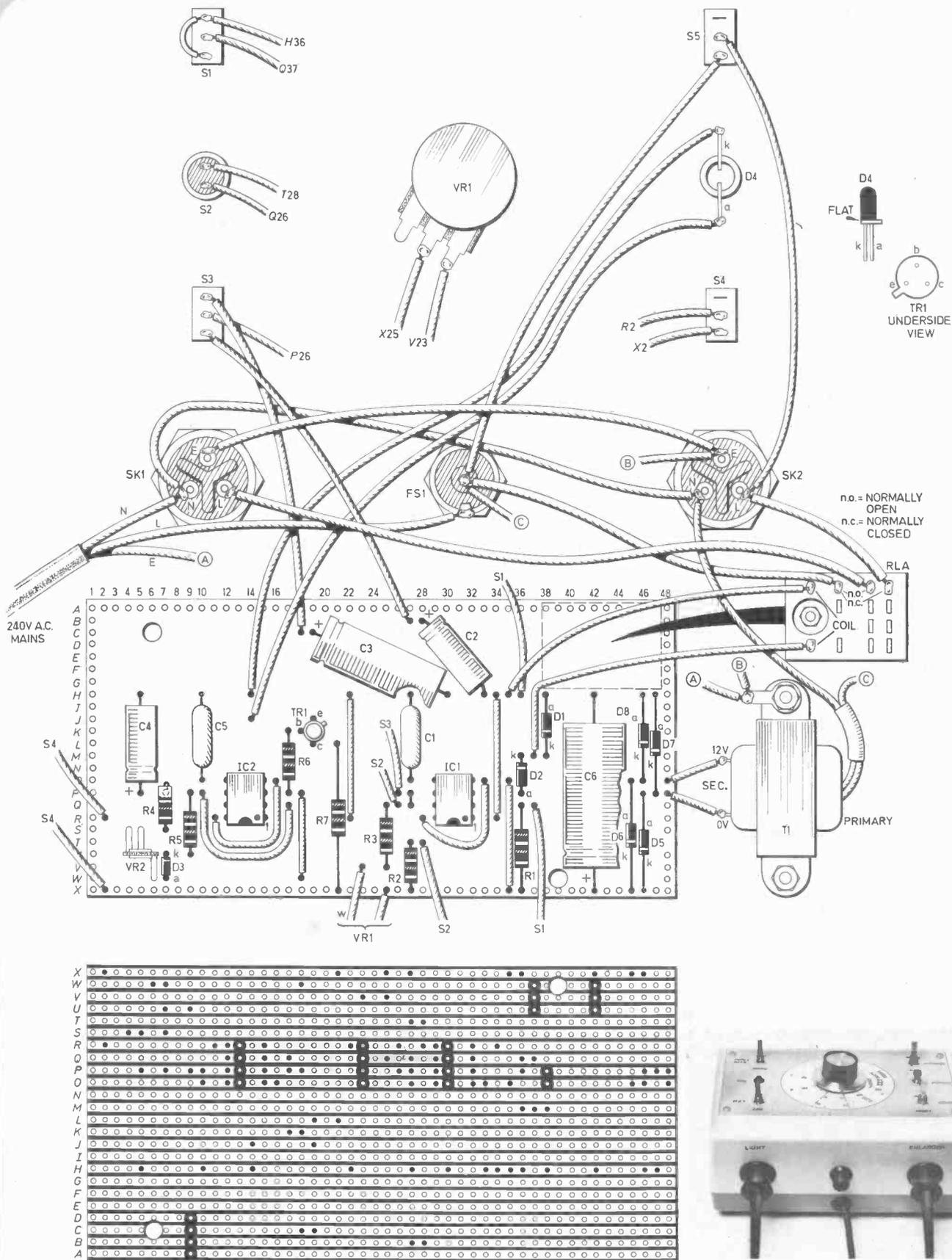
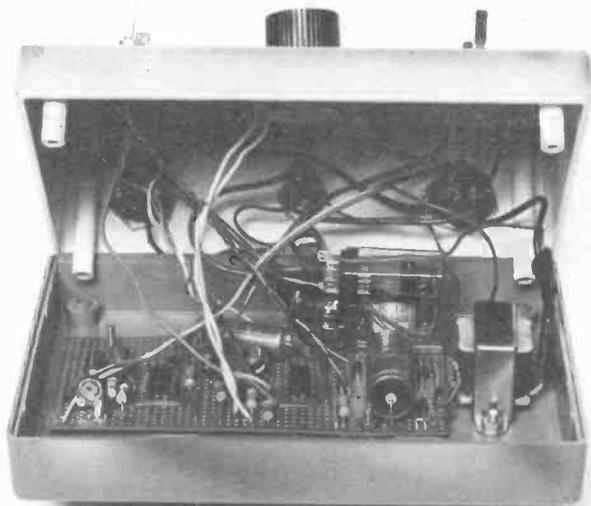
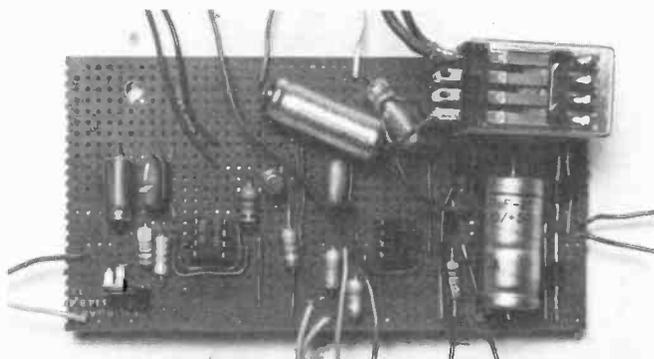


Fig. 2. Circuit board component layout on the topside, details of breaks to be made in the copper strips on the underside and all interwiring to off board components.

Arrangement at the rear of the case showing positioning of the lights and enlarger plugs and sockets.



The sloping front cover half of the case lifted clear to show positioning of the circuit board, transformer and relay. When completing the final wiring to front panel controls and rear sockets make sure that all leads are long enough to facilitate the removal of front section of the case.



The finished prototype circuit board for the Darkroom Timer. The relay wiring may differ according to type finally selected. Low profile integrated circuit sockets may be used in place of the Soldercon pins if preferred.

The switch S1 deserves some comment. It is a single-pole, double-throw type and is biased to the centre "off" position on one of the poles. This means that it can be left in the "on" position if pushed say up, but cannot be left in the "on" position if pushed down but reverts to the centre "off" position as soon as finger pressure is released.

### CASE

The prototype was housed in a sloping front box, size 171 x 121 x 37mm. The Verocase number 202-21033A would be ideal although any similar case would suffice. Drill the front panel and mount all the switches. The rest of the components can then be mounted in position as

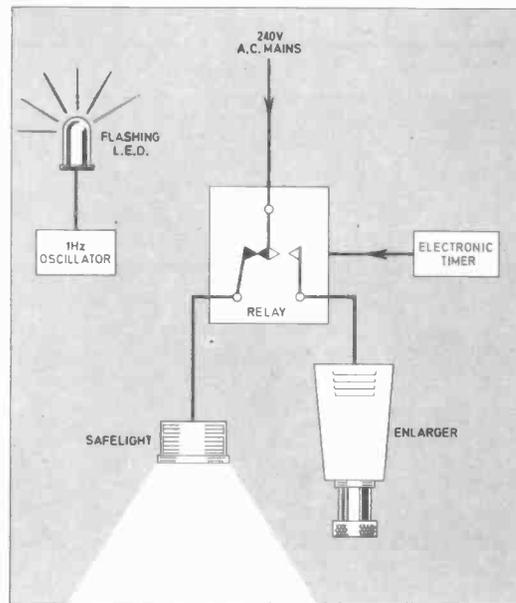
in Fig. 2 and when interwiring is complete, calibration and checking should be carried out.

### CALIBRATION

The preset VR2 should first be adjusted until D4 flashes at a rate of precisely 1Hz. Having done this we can then proceed to calibration of the main timing circuit.

Accuracy of calibration for the main timing control VR1 will determine the final accuracy of the timer, so it is best to take care to set the two ranges properly (using pencil marks). Check that all the controls are working.

With the SAFELIGHT switch set on RELAY, and the relay activate switch (S1) used in the push-to-make mode,



## HOW IT WORKS

A single timer i.c. is wired as a monostable and its output controls a relay.

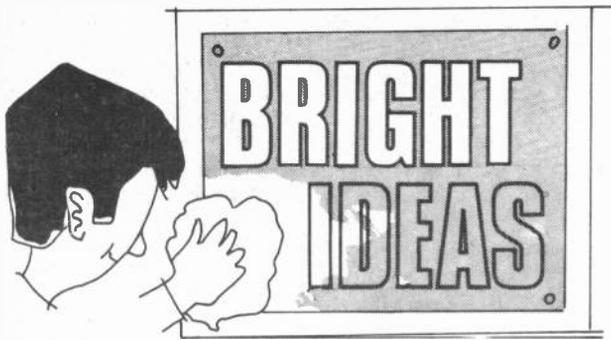
In normal conditions the safelight is on and the enlarger off. When the timer is activated the relay changes over and the enlarger comes on and the safelight goes off.

A second timer i.c. is wired so as to switch a l.e.d. on and off at a frequency of 1Hz. This can be used to time exposures reliably and consistently.

the light should go out, and the enlarger come on for the timed period.

This period can be terminated at any time by the CANCEL button. Moving the relay activate switch to the unbiased position (CONTINUOUS) should make the enlarger turn on continuously, and the SAFELIGHT switch S5 should turn the safelight on continuously independent of the relay. ✧

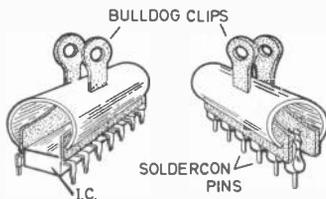




Readers' Bright Ideas; any idea that is published will be awarded payment according to its merit. The ideas have not been proved by us.

### SOLDERING AID

During construction of the *TTL Test Bed* (October 1978) I found that the Soldercon pins were inclined to break away from their frame when every second one was bent up in order to fit alternate pins on the stripboard. You were then left with a lot of loose pins.



I found that by using a "Bulldog" paper clip it made an excellent holder while you soldered the pins in position. A small size "Bulldog" clip will hold six pins while you solder them in position, see diagram.

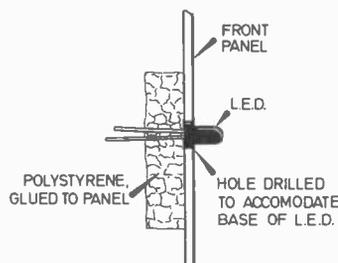
I also use these paper clips while soldering 14 pin and 16 pin i.c.s in position. I find they make an excellent heat shunt as the tension of the clip ensures good contact with each of the pins.

Jerry Murphy, Eire

### POLYSTYRENE L.E.D. MOUNTING

I have on occasions been confronted with the problem of mounting single l.e.d.s onto the fascia panels of projects. Bearing in mind the cost of specialised holders I have come up with the idea of mounting a small piece of polystyrene (e.g. ceiling tile) behind the panel and using the gripping action of the polystyrene to hold the components.

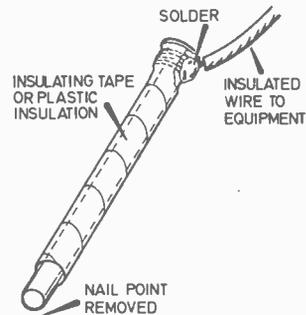
D. E. Kingston,  
Lowestoft,  
Suffolk.



### SIMPLE PROBE

I have made the *Continuity Tester*, which was published in the January issue of *EVERYDAY ELECTRONICS*. I have found that commercially made probes are not cheap, so I have devised a simple substitute. This can easily be made from the contents of a "spares box".

A nail with the point filed away is the basis of the probe, see diagram. A length of suitable wire is then taken with about 25mm of copper exposed. The area that is to be soldered is cleaned, then "tin" the clean area of the nail with a hot soldering iron. The solder should remain if the surface is clean enough.

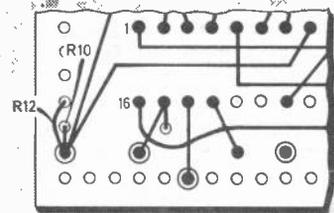


The exposed end of the wire is wrapped around the tinned area of the nail and then soldered. When the joint is cool, it is covered with an appropriate colour of insulating tape or plastic insulation sleeving. The remaining end of the wire should then be taken to a plug or equipment.

This is *only a low voltage probe*, it should *not* be used for mains voltages.

J. Moulder (Age 13), Dumgoyne, Scotland.

PLEASE  
TAKE  
NOTE



#### Cricket Game (August 1980)

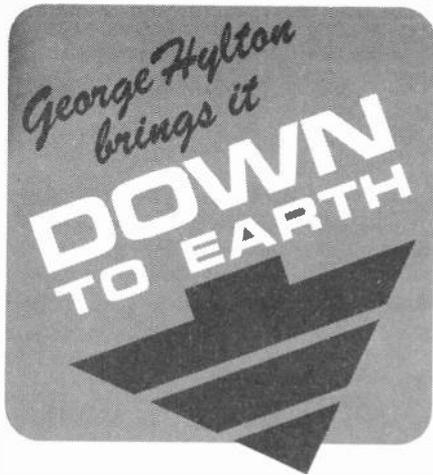
The underside wiring of Board B is incomplete, the common connections to ground of resistors R10 and R12 being omitted. The completed wiring is shown above.

There are some unused sections (gates and flip-flop) in i.c.s IC4, IC6 and IC9. As these are CMOS devices, the unused inputs should be strapped to the appropriate power supply rail. If this is not done, the i.c. may become very hot and possibly overheat and be damaged. As a result excessive current will be drawn from the supply making battery powered systems uneconomical.

The unconnected pins should be connected as follows: IC4 pins 8, 9, 10 and 11, IC6 and IC9 pins 8, 9, 12 and 13 to the 0V supply rail.

#### Autophase (June/July 1980)

An additional break on the underside of the stripboard is required at location C16.



## Keeping Things In Proportion

**O**DD LOOKING numbers abound in electronics. Why do resistors and capacitors have values like 27 ohms and 560pF? Why not have a nice round numbers like 30 and 600? Why do so many test meters these days have scales of 0 to 31·6? In this article the odd numbers are found to be rather less odd than they first appear but still not quite without mystery.

Let's take those multimeter scales first. When I was a lad meters had scales 0 to 10, 0 to 100, and so on. Some had intermediate scales as well but these were always simple multiples of the basic 0 to 10, etc. My old Avometer, for instance, has scales of 0 to 100 and 0 to 400 and the same scale divisions serve for both. But 0 to 31·6? Never!

The choice of this odd-looking intermediate range, 0 to 31·6, is quite sensible. It springs from a commendable anxiety to minimise one kind of error. This is the "reading error" which stems from the fact that the human eye cannot make very fine discriminations of the position of a pointer. Practical meter scales seldom have more than a hundred small divisions because it is difficult to read markings if they are spaced too closely. Experience shows that at normal viewing distances and with average eyesight a hundred small divisions is the practical limit.

## Limits

This has a direct bearing on the accuracy obtainable from a pointer type of indication. I'm not thinking of the accuracy of the meter itself, but of the eye's ability to make use of it. Let's assume that the meter itself is absolutely accurate. Even so, the eye can only read off what it says to within certain limits. This is what then fixes the achievable accuracy.

Let's assume that a meter can be read to the nearest small scale division. A meter scaled 0 to 100V can then be read to the nearest volt. If the true voltage is 99·5V but you read this as

99V or 100V the reading error is 0·5V which is an error of one half of one per cent and for most purposes is perfectly tolerable.

But if the voltage were 10·5V and you read it as 10V or 11V the error, still only half a scale division, now amounts to 5 per cent, which may be serious.

## Best Compromise

The answer, of course, is to switch to a lower voltage range. If the meter has a 0 to 20V range then each small division is now worth 0·2V, and if you read 10·6V instead of the true 10·5V the error is under 1 per cent. However, with scales of 0 to 20V and 0 to 100V you are still in trouble with a voltage like 21V, which is of scale for the 20V range but still quite low down on the 100V range. An error of 0·5V at 21V is about 2·4 per cent. Given that a meter can have one intermediate range between its 0 to 10 and 0 to 100 ranges, what is the best compromise for accuracy? That is what range value gives, on average, the smallest reading errors?

## Thirty-one Point Six

The answer is 0 to 31·6. This figure is arrived at because it bears the same proportionate relation to both the other ranges. Actually 31·6 is only an approximation. My pocket calculator says the true figure is 31·6227766. Let's call it 31·6 for short! If you multiply 10 by 3·16 you get 31·6. It's less obvious that if you then multiply the 31·6 by 3·16 you get 100. And if you start with a lowest range of 0 to 1 and go on multiplying by 3·16 you end with ranges which go: 1, 3·16, 10, 31·6, 100, 316, 1000 . . . etc. By turning to the next lowest range when the pointer lies too low on the scale for accuracy you can now always reduce your reading error to less than a third of what it was.

The meter manufacturer must now print two basic scales, 0 to 31·6 and 0 to 100, since the same markings can't be used for both. But all the voltage and current ranges can share these two scales. If the meter also has an ohms scale and a decibels scale the total is still only four scales so the dial is still relatively uncluttered and easy to read. Moreover the only mental arithmetic required is simple multiplication or division of the scale numbers by 10, 100, or 1000. With scales like 0 to 10, 0 to 20, and 0 to 50 you get into difficulties with mental arithmetic when faced with the problem of deciding what the true voltage is when the pointer is at say 33 on the 0 to 100 scale but the meter is actually set to its 0 to 50V range. I do, anyway.

## Constant Proportion

Mind you, there are cases when this principle of forming a set of ranges by multiplying by a constant factor like 3·16 (which is the square root of 10, by

the way) can't be applied. A common example is the measuring oscilloscope. This has a ruled graticule over its screen and only one set of rulings can be used since two lots, superimposed, would be confusing to the eye. You are stuck with a single scale and have to use intermediate ranges which fit it. This leads to sets of ranges like 0 to 10, 0 to 20, 0 to 50, 0 to 100..... etc., where each range is roughly twice the previous one. In other words you apply the constant proportion principle as nearly as you can but compromise by sacrificing true constancy to convenience in reading.

## Component Values

The same basic principle gives rise to those odd-looking component values, like:

10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82, 100, 120...etc.

It may seem more reasonable to use a range like 10, 20, 30, 40, but this gives a very poor selection of values at the low end. If you needed 15pF but all you could buy was 10 or 20pF you'd have to settle for an error of 5pF, which is 33 per cent. The 10, 12, 15, 18 series is designed so that this "selection error" is never more than about 10 per cent anywhere in the range. To ensure this, each successive value is greater than the last by the same percentage, about 20 per cent in this case.

This series is called E12 because there are 12 standard values before the same basic numbers start repeating, or in other words there are 12 values per decade. (In the series printed above, the 10 marks the start of one decade and the 100 the start of the next.) For greater choice there is also an E24 series with 24 values per decade and an E48 with 48, but E12 is by far the commonest with component stockists.

Actually the traditional E12 values given above are not quite right. My pocket calculator tells me that each value should be 1·211527659 times the previous one. Using this figure and rounding off the answers gives the series:

10, 12·1, 14·7, 17·8, 21·5, 26·1, 31·6, 46·4, 56·2, 68·8, 82·5.....

While most of these correspond with traditional E12 when taken to two significant figures there are a few in the middle which don't. Thus the traditional 33 should really be 32 which is nearer to 31·6. (Yes, it's the magic number 31·6 again!) Similarly the traditional 27 should be 26 and 39 should be 38. I don't know why the traditional values are wrong. Perhaps some knowledgeable reader will tell me. But the errors are too small to have much effect on the usefulness of the series. The maximum selection error is still only a shade over 11 per cent (and occurs when what you need is 24·5 and what you have to settle for is 22 or 27).

# WORKSHOP MATTERS

By Harry T. Kitchen

## Receiver Sensitivity

Last month we looked, rather briefly, at dummy aerials and the necessity of using cables of the correct impedance. I mentioned the importance of e.m.f. and p.d. and it is important to have a good understanding of all these factors if one is going to be involved in precision measurement as opposed to simply connecting an oscillator or signal generator (sig-gen) to the receiver and hoping for the best.

For measuring the sensitivity of receivers it is essential that the sig-gen—forget the simple oscillators—shall deliver an accurately calibrated output voltage, the source impedance of which should match the source impedance of the aerial with which the receiver is normally used, though this is normally the same as the input impedance of the receiver.

At the frequencies that most of us are likely to be involved in, receivers are regarded as voltage sensitive, and their sensitivities are generally specified in appropriate terms; for a given a.f. output (in milliwatts) the receiver sensitivity in microvolts is quoted. But Europe, including the UK, differs from the USA.

European practice is to state the sensitivity in terms of source e.m.f. available via the specified source impedance. The receiver impedance, and hence the p.d. developed across it, is generally unknown. In the USA it is customary for the p.d. to be developed across a matched load to be quoted. In essence the two methods are the same provided they are suitably qualified:  $15\mu\text{V}$  e.m.f. or  $7.5\mu\text{V}$  p.d.

## EMF and PD

We can now look at e.m.f. and p.d. in some detail. Bear in mind that there is little difference apart from terminology, and that either can be used provided it is made clear which, and that the two are not mixed in any way.

The generator is usually represented as a source voltage in series with its own internal resistance; the pictorial method is to show the source as a circle containing a sine wave symbol, in series with a resistance, the whole being contained within a rectangle. Two leads, sometimes with arrows to show direction of current, connect to the receiver's input impedance, represented by a resistance, sometimes labelled as  $R_i$ .

If the attenuator is calibrated in terms of e.m.f., as most are, it means that the source resistance appears in series with the e.m.f. and must be allowed for whilst measurements are made. If a matched receiver input resistance is involved, what happens? We have, in effect, two series resistances with the output taken from their junction, and therefore only half the e.m.f. will appear across  $R_i$ , giving us the example quoted earlier, i.e.  $15\mu\text{V}$  e.m.f. or  $7.5\mu\text{V}$  p.d.

If  $R_i$  is very much higher, say is infinite, then no voltage will be "lost" across the source resistance, and e.m.f. will equal p.d. If  $R_i$  is very low, most of the voltage will be "lost" across the source resistance and e.m.f. will greatly exceed p.d. Hence, the necessity of keeping the two units separate.

## Source Impedance

The source impedance of generators is specified, and with the required accessories is typically 50 or 75 ohms, and is single ended, with one side connected to earth. If a floating output is required, with neither end connected to earth, but with a centre tap that is, then the output impedance is commonly 300 ohms. Load resistances, or impedances to be precise, of 50 ohms, 75 ohms and 300 ohms will result in the p.d. being half the e.m.f.

However, the input impedance of a receiver is not precise, nor is it fixed, but varies with frequency. When measuring receiver sensitivity at widely differing frequencies it is quite possible to obtain erroneous results if the input impedance is not compensated for. This is commonly achieved by a "dummy" aerial interposed between the generator and the receiver and is fairly effective from 150kHz to around 30MHz.

Another common source of error is to use connecting cables of varying impedance to connect generator to receiver. What happens is that voltage standing waves are set up and, in very simple terms, we get sum and difference effects, so that at times the standing wave aids the signal and at others it tends to cancel it.

In short, you disregard generator source impedance, receiver input impedance, and cable impedance at your peril!

## Generator Efficiency

The generator efficiency is not constant but decreases with increasing frequency. Some method is essential for feeding the attenuator with a constant signal. This is frequently achieved by varying the oscillator supply voltage; increasing it causes the oscillator to oscillate more vigorously and so compensate for the increase in frequency.

This setting up of output voltage is most commonly effected by monitoring it with a thermocouple type meter. A thermocouple is substantially unaffected by frequency being a heat operated device, and the meter carries little more than a pre-set mark to which the pointer is adjusted by the "Set R.F." control.

Essentially very simple and reliable, the system has just one drawback: if the output terminals are short-circuited together, at maximum output on the attenuator, the thermocouple can be destroyed

by the excess current that is caused to flow. Most high quality generators are inhibited such that maximum output can only be selected after a special catch has been disengaged.

## Variable Modulation

Variable depth of modulation is essential for checking detector distortion in receivers. The oscillator can be directly modulated, but it is preferable for an intermediate, or buffer, stage to be modulated, as this reduces the amount of f.m. in the signal. The a.f. oscillator will work at 400Hz or 1kHz, but should be capable of being disconnected from the circuit so that a plain unmodulated, or c.w. (continuous wave) signal is possible.

External modulation should be possible as this extends greatly the usefulness of the instrument. The depth of modulation can be only properly checked on an oscilloscope and is outside our terms of reference; we must, perforce rely on the manufacturer if we lack a 'scope.

## Conclusions

There is rather more to sig-gens than meets the casual enquirer, and it has been possible to do no more than arouse the potential user's interest, and caution, in the belief that this will encourage him to carry out further, more detailed, research.

Returning, briefly, to e.m.f. and p.d., it should have been mentioned earlier that some very high quality a.f. generators are also so calibrated, and therefore the loads applied should be considered very carefully before relying on in-built attenuators and output meters.



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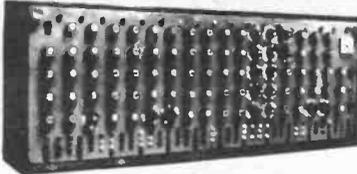
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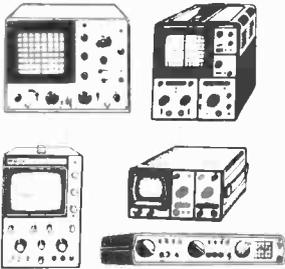
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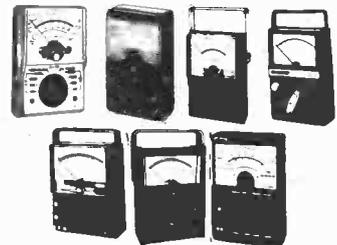
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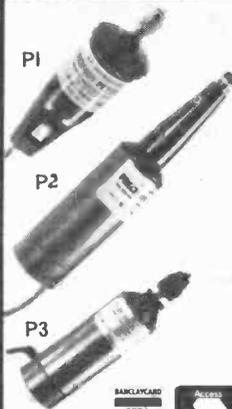
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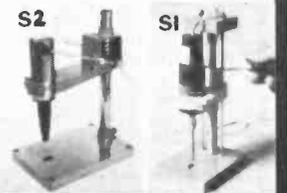
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 Operating voltage (DC) 50-80 Max.  
 Loads 4-16 ohms  
 Frequency response Measured at 100 watts 25Hz-20kHz  
 Sensitivity for 100 watts 400mV @ 47k  
 Typical T.H.D. @ 50 watts 4 ohms load 0.1 %  
 Dimensions 205 x 90 and 190 x 36 mm

The P.E. power amp kit is a module for high power applications—disco units, guitar amplifiers, public address systems and even high power domestic systems. The unit is protected against short circuiting of the load and is safe in an open circuit condition. A large safety margin exists by use of generously rated components, the

output stage uses four 115 watt transistors normally only two would be used, result, a high powered rugged unit. The PC Board is backprinted, etched and ready to drill for ease of construction, and the aluminium chassis is preformed and ready to use, supplied with all parts and circuit diagrams.

125 watt power amp kit

**£9.50** plus £1.00 p&p

## ACCESSORIES

Suitable L.S. coupling electrolytic

**£1.00** plus 20p p&p

Suitable Mains Power Supply Unit

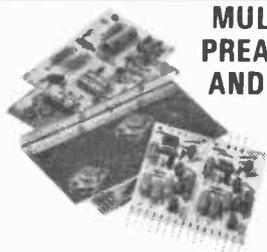
**£7.50** plus £2.75 p&p

ACCESSORIES available only when purchasing packs.



AS FEATURED IN PRACTICAL ELECTRONICS OCTOBER ISSUE

## DIY STEREO BARGAIN PACKS FEATURING FAMOUS BUILT MULLARD PREAMP MODULES



### MULLARD STEREO PREAMP MODULES AND TWO 12 WATT POWER AMP KITS.

In easy to build form P.C.B.s backprinted, etched and drilled ready to use.

### BUILD A 12 WATTS PER CHANNEL STEREO AMPLIFIER ACCESSORIES AND L.S. KIT EXTRA (not available separately)

**£6.00**

DIY PACK 1 2 x power amp kits LP1182/ preamp module, suitable for ceramic and auxiliary inputs.

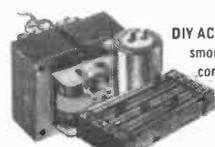
**£6.00** plus £1.10 p&p

DIY PACK 2 2 x power amp kits LP1184 preamp module suitable for magnetic ceramic and auxiliary inputs.

**£8.50** plus £1.15 p&p

DIY SPEAKER KIT Two 8" x 5" approx. 4 ohm bass.

**£3.50** plus £1.70 p&p



DIY ACCESSORIES Mains transformer smoothing capacitor rectifier 4 x slider controls, for base, treble and volume.

**£3.00** plus £1.60 p&p

ACCESSORIES: Available only at time of purchase of Bargain Packs

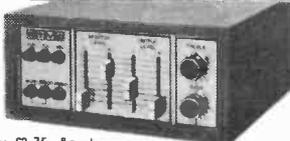
### 12 + 12 WATT AMPLIFIER KIT

**NOTE:** for use with 4 to 8 ohms speakers. With up-to-the-minute features. To complete you just supply screws, connecting wire and solder. Features include din input sockets for ceramic cartridge, microphone, tape or tuner. Outputs—tape, speakers and headphones. By the press of a button it transforms into a 24 watt mono disco amplifier with twin deck mixing. The kit incorporates a Mullard LP1183 pre-amp module, plus 2 power amplifier assembly kits and mains power supply. Also featured 4 slider level controls, rotary bass and treble controls and 6 push button switches. Silver finish fascia panel with matching knobs. Easy to assemble teak simulate cabinet and ready made metal work. For further information instructions are available price 50p. Freq with kit. Size 9 1/4" x 8 3/4" x 4" approx.

**NOTE:** for use with 4 to 8 ohms speakers.

**£13.95** plus £2.55 p&p

BSR chassis record player deck with manual set down and return, complete with stereo ceramic cartridge.

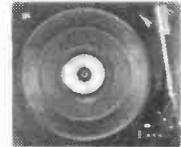


**£8.50** plus £2.75 p&p when purchased with amplifier available separately **£10.50** plus £2.75 p&p.

**TWO WAY SPEAKER KIT.** 2 Philips 8" approx speakers **£4.75** per stereo pair plus £1.50 p&p when purchased with amplifier available separately **£6.75** plus £1.50 p&p.

**ALSO AVAILABLE** Stereo magnetic pre-amp conversion kit all components including P.C.B. to convert your ceramic input on the 12 + 12 amp to magnetic. **£2.00** when purchased with kit featured above. **£4.00** separately inc. p&p.

BSR Manual single play record deck with auto return and cueing lever. Fitted with stereo ceramic cartridge 2 speeds with 45 rpm spindle adaptor ideally suited for home or disco use.



**£12.25** OUR PRICE plus £2.75 p&p

### PHILLIPS RECORD PLAYER DECK GC037

Hi Fi record player deck, 2 speed, damped cueing, auto shut-off, belt drive with floating sub chassis to minimise acoustic feedback. Complete with GP401 stereo magnetic cartridge—**LIMITED STOCK. UNBEATABLE OFFER AT**

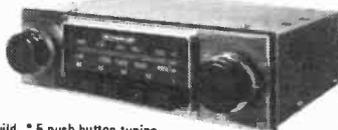


**£27.50** complete plus £2.75 p&p

**OFFER!** SAVE MONEY by purchasing 12 + 12 amp kit, BSR record deck and speaker kit together for only **£25.50** p&p £4.50.

### PRACTICAL ELECTRONICS CAR RADIO KIT (Constructors pack 7)

**£10.50** plus £1.75 p&p



- \* Easy to build \* 5 push button tuning
- \* Modern styling design \* All new unused components
- \* 6 watt output \* Ready etched & punched P.C.B.
- \* Incorporates suppression circuits \* Now with tape input socket

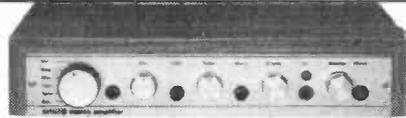
All the electronic components to build the radio, you supply only the wire and solder as featured in the Practical Electronics March issue. Features: Pre-set tuning with five push button options, black illuminated tuning scale, with matching rotary control knobs, one, combining on/off volume and tone-control, the other for manual tuning, each set on wood simulated fascia. The P.E. Traveller has a 6 watts output, neg ground and incorporates an integrated circuit output stage, a Mullard IF module LP1181 ceramic filter type, pre-aligned and assembled and a Bird pre-aligned push button tuning unit. The radio fits easily in or under dashboards. Complete with instructions.

#### CONSTRUCTORS PACK 7A

Suitable stainless steel fully retractable locking aerial and speaker (approx. 6" x 4") is available as a kit complete **£1.95** p&p £1.00

NOTE: Constructor's pack 7A sold complete with radio kit **£15.20** including p&p.

FEATURED PROJECT IN PRACTICAL ELECTRONICS.



### 30 + 30 WATT STEREO AMPLIFIER BUILT AND TESTED

Viscount IV unit in teak simulate cabinet, silver finished rotary controls and pushbuttons with matching fascia, red mains indicator and stereo jack socket. Functions switch for mic magnetic and crystal pickups, tape and auxiliary. Rear panel features fuse holder. DIN speaker and input socket 30 + 30 watts. RMS 60 + 60 watts peak for use with 4 to 8 ohm speakers. Size 14 1/2" x 10" approx.

READY TO PLAY **£32.90** plus £3.30 p&p



323 EDGWARE ROAD, LONDON W2 21A HIGH STREET, ACTON W3 6NG

ACTON: Mail Order only. No callers ALL PRICES INCLUDE VAT AT 15% All items subject to availability. Price correct at 14/8/80 and subject to change without notice.

For further information send for our instruction booklet **20p** plus stamped addressed envelope.

Persons under 16 years not served without parent's authorisation.

### BARGAIN OFFER!!



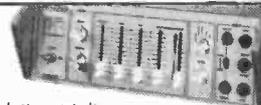
#### ARISTON PICK UP

Ariston pick-up arm manufactured in Japan. Complete with headshell. Listed price over £30.00

**£11.95** plus £2.50 p&p

### 100 WATT MONO DISCO AMPLIFIER

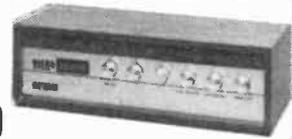
Brushed aluminium fascia and rotary controls. Size approx 14" x 4" x 10 1/2". Five vertical slide controls, master volume, tape level, mic level, deck level. PLUS INTER DECK FADER for perfect graduated change from record deck No. 1 to No. 2, or vice versa. Pre fade level controls (PRL) lets YOU hear next disc before fading it in. VU meter monitors output level. Output 100 watts RMS 200 watts peak.



**£76.00** plus £4.00 p&p

### 50 WATT MONO DISCO AMPLIFIER

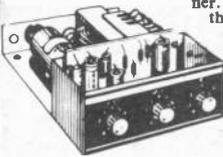
Size approx 13 1/2" x 5 1/4" x 6 3/4". 50 watts rms. 100 watts peak output. Big features include two disc inputs, both for ceramic cartridges, tape input and microphone input. Level mixing controls fitted with integral push-pull switches. Independent bass and treble controls and master volume.



**£30.60** plus £3.20 p&p

Personal Shoppers EDGWARE ROAD LONDON W2 Tel: 01-723 8432. 9.30am-5.30pm. Closed all day Thursday ACTON: Mail Order only. No callers GOODS DESPATCHED TO MAINLAND AND N. IRELAND ONLY

**SUPERSOUND 13 HI-FI MONO AMPLIFIER**



A superb solid state audio amplifier. Brand new components throughout. 5 silicon transistors plus 2 power output transistors in push-pull. Full wave rectification. Output approx. 13 watts r.m.s. into 8 ohms. Frequency response 12Hz-30KHz ± 3db. Fully integrated pre-amplifier stage with separate Volume, Bass

boost and Treble cut controls. Suitable for 8-15 ohm speakers. Input for ceramic or crystal cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and tested, with knobs, escutcheon panel, input and output plugs. Overall size 3" high x 6" wide x 7 1/4" deep. AC 200/250V. PRICE £18.40, P. & P. £1.60.

**HARVERSONIC MODEL P.A. TWO ZERO**



An advanced solid state general purpose mono amplifier suitable for Public Address system, Disco, Guitar, Gram, etc. Features 3 individually controlled inputs (each input has a separate 2 stage pre-amp). Input 1, 15mV into 47k. Input 2, 15mV into 47k (suitable for use with mic. or guitar etc.). Input 3, 200mV into 1 meg. suitable for gram, tuner, or tape etc. Full mixing facilities with full range bass & treble controls. All inputs plug into standard jack sockets on front panel. Output socket on rear of chassis for an 8 ohm or 16 ohm speaker. Output in excess of 30 watts music power. Very attractively finished purpose built cabinet made from black vinyl covered steel, with a brushed anodised aluminium front escutcheon. For ac mains operation 200-240 volts. Size approx. 12 1/4in wide x 5in high x 7 1/4in deep. Special price £29.00 + £3.00 carriage and packing.

**"POLY PLANAR" WAFER-TYPE, WIDE RANGE ELECTRO-DYNAMIC SPEAKER**

Size 1 1/2" x 14 1/2" x 1 1/2" deep. Weight 19oz. Power handling 20W r.m.s. (40W peak). Impedance 8 ohm only. Response 40Hz-20KHz. Can be mounted on ceilings, walls, doors, under tables, etc., and used with or without baffle. Send S.A.E. for full details. Only £8.80 each + p. & p. (one £1.20, two £1.50).

**STEREO MAGNETIC PRE-AMP.** Sens. 3mV in for 100mV out. 15 to 35V neg. earth. Equ. ± 1dB from 20Hz to 20KHz. Input impedance 47K. Size 1 1/2" x 2 1/2" x 1" H. £3.20 + 22p P. & P.

**MAINS OPERATED SOLID STATE AM/FM STEREO TUNER**

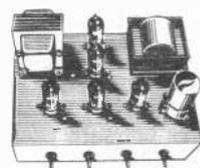


200/240V Mains operated Solid State FM/AM Stereo Tuner. Covering M.W. A.M. 540-1605 KHz VHF/FM 88-108 MHz. Built-in Ferrite rod aerial for M.W. Full AFC and AGC on AM and FM. Stereo Beacon Lamp

Indicator. Built in Pre-amps with variable output voltage adjustable by pre-set control. Max o/p Voltage 600mV/ RMS into 20K. Simulated Teak finish cabinet. Will match almost any amplifier. Size 8 1/4" w x 4" h x 9 1/4" d approx.

LIMITED NUMBER ONLY at £29.00 + £2.00 P. & P. 10/14 WATT HI-FI AMPLIFIER KIT

A stylishly finished mono-aural amplifier with an output of 14 watts from 2 EL84s in push-pull. Super reproduction of both music and speech with negligible hum. Separate inputs for mike and gram allow records and announcements to follow each other. Fully shrouded section wound output transformer to match 3-15 Ω speaker and 2 independent volume controls, and separate bass and treble controls are provided giving good lift and cut. Valve line-up 2 EL84s, ECC83, EF86 and EZ80 rectifier. Simple instruction booklet. 50p + SAE (Free with parts). All parts sold separately. ONLY £18.40, P. & P. £2.00. Also available ready built and tested £22.50, P. & P. £2.00.



**STEREO DECODER MK.II** SIZE 1 1/2" x 2 1/2" x 1 1/2" ready built. Pre-aligned and tested for 10-16V neg. earth operation. Can be fitted to almost any FM VHF radio or tuner. Stereo beacon light can be fitted if required. Full details and instructions supplied. £7.00 plus 25p. P. & P. Stereo beacon light if required 40p extra.

Mullard LP1159 RF-IF module 470kHz £2.50 + P. & P. 40p. Full specification and connection details supplied. Pye VHF FM Tuner Head covering 88-108MHz, 10.7 MHz I.F. output. 7.8V + earth. Supplied pre-aligned, with full circuit diagram with precision geared F.M. gang and 323PF + 323PF A.M. Tuning gang only £3.40 + P. & P. 60p.

**VYNNAIR & REXINE SPEAKERS & CABINET FABRICS** app. 54 in. wide. Our price £2.30 yd. length. P. & P. 70p per yd. (min. 1 yd.). S.A.E. for samples.

**HARVERSONIC SUPERSOUND 10 + 10 STEREO AMPLIFIER KIT**

A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integral pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. Very simple to modify to suit magnetic cartridge—instructions included. Output stage for any speakers from 8 to 15 ohms. Compact design, all parts supplied including drilled metalwork, high quality ready drilled printed circuit board with component identification clearly marked, smart brushed anodised aluminium front panel with matching knobs, wire, solder, nuts, bolts—no extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Power output: 14 watts r.m.s. per channel into 5 ohms. Frequency response: ± 3dB 12-30,000Hz Sensitivity: better than 80mV into 1M Ω; Full power bandwidth: ± 3dB 12-15,000Hz. Bass boost approx. to ± 12dB. Treble cut approx. to -16dB. Negative feedback 18dB over main amp. Power requirements 35v. at 1.0 amp. Overall Size 12" w. x 8" d. x 2 1/2" h.

Fully detailed 8 page construction manual and parts list free with kit or send 50p plus large S.A.E.

AMPLIFIER KIT . . . . . £14.95 P. & P. £1.20 (Magnetic input components 33p extra)  
POWER PACK KIT . . . . . £6.20 P. & P. £1.50  
CABINET . . . . . £6.20 P. & P. £1.50

SPECIAL OFFER—only £25.80 if all 3 items ordered at one time plus £2.80p. & p. Full after sales service

Also avail. ready built and tested £32.20, P. & P. £2.80.

**HARVERSONIC STEREO 44**

A solid state stereo amplifier chassis, with an output of 3-4 watts per channel into 8 ohm speakers. Using the latest high technology integrated circuit amplifiers with built in short term thermal overload protection. All components including rectifier smoothing capacitor, fuse, tone control, volume controls, 2 pin din speaker sockets & 5 pin din tape rec./play socket are mounted on the printed circuit panel, size approx. 9 1/2" x 2 1/2" x 1" max. depth. Supplied brand new & tested, with knobs, brushed anodised aluminium 2 way escutcheon (to allow the amplifier to be mounted horizontally or vertically) at only £10.40 plus 90p P. & P. Mains transformer with an output of 17v a/c at 500mA can be supplied at £2.15 + 70p P. & P. if required. Full connection details supplied.

All prices and specifications correct at time of press and subject to alteration without notice.

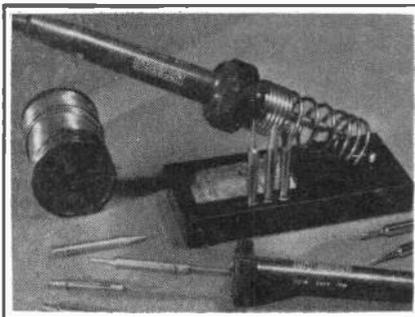
PLEASE NOTE: P. & P. CHARGES QUOTED APPLY TO U.K. ONLY. SEND SAE WITH ALL ENQUIRIES.

**HARVERSON SURPLUS CO. LTD.** (Dept. E.E.) 170 MERTON HIGH ST., LONDON, S.W.19. Tel.: 01-540 3985  
A few minutes from South Wimbledon Tube Station. Open 9.30-5.30 Mon. to Fri. 9.30-5 Sat. Closed Wed.

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New 'L' series irons, designed to latest safety standards. Outstanding performance, lightweight and easy maintenance. New non-roll GRP safety handles. Ceramic and mica insulated elements enclosed in stainless steel shafts.

Fully earthed with screw connected 3-core leads. Interchangeable, non-seize copper bits.



**MODEL LC18 18 watts**

Lightweight, high-performance iron for all soldering from calculators to T.V. sets. Fitted with 3.2 mm copper bit and complete with

spare bits 1.6, 2.4 and 4.7 mm. £6.31 including p&p and VAT. 240 volts standard but also available 12 and 14 volts. Iron only £4.66 including P&P and VAT.

**MODEL LA12 12 watts**

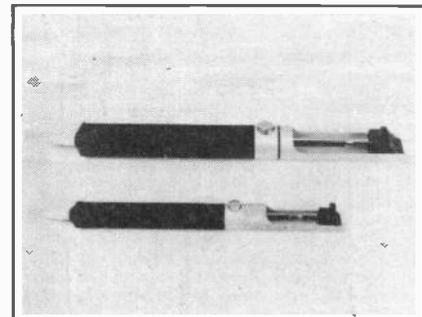
Similar to LC18 but with extra slim shaft and bits for fine work. Fitted with 2.4mm copper bit and complete with spare bits 1.2 mm and 3.2mm. £5.58 including p&p and VAT. 240 volts standard also available 6, 12 and 24 volts. Iron only £4.61 including P&P and VAT.

**No. 3 SAFETY SPRING STAND for LC18 & LA12**

Complete with sponge and location for spare bits £4.41 including P&P and VAT.

**LOLA DE-SOLDERING PUMPS**

Removes solder from pcb joints quickly, with no fuss. Simple one-handed operation leaves other hand free to hold soldering iron heat source. Needs no external power. Has replaceable PTFE nozzle. Thousands in daily use in major manufacturing companies. Two sizes to choose from.



**Lola A** 215 mm long x 20 mm dia. £6.89 (including VAT, P&P)

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937	55p	4030	50p	6505	795p
944	65p	4031	195p	6800	695p
946	55p	4033	145p	6802	995p
947	55p	4035	104p	8080A	525p
962	55p	4036	290p	8085A	1095p
9099	90p	4037	105p	Z80	795p
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7404	17p				
7409	18p				
7410	18p				
7412	18p				
7413	28p				
7420	16p				
7430	18p				
7432	25p				
7440	16p				
7442	68p				
7448	75p				
7473	32p				
7474	32p				
7475	40p				
7476	40p				
7490	35p				
7492	50p				
7493	50p				
7496	45p				
74121	35p				
74123	45p				
74154	90p				
74157	55p				
74122	45p				
74125	50p				
74195	100p				
74196	100p				
74283	140p				
74290	120p				
74365	90p				
74365	90p				

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74LS11	30p				
74LS12	30p				
74LS14	60p				
74LS15	38p				
74LS20	19p				
74LS30	30p				
74LS32	25p				
74LS40	26p				
74LS42	56p				
74LS47	78p				
74LS48	85p				
74LS49	95p				
74LS107	40p				
74LS123	69p				
74LS125	50p				
74LS132	79p				
74LS138	69p				
74LS151	75p				
74LS153	155p				
74LS155	65p				
74LS161	78p				
74LS163	90p				
74LS164	90p				
74LS168	190p				
74LS174	99p				
74LS175	99p				
74LS195	87p				
74LS221	110p				
74LS244	175p				
74LS245	325p				
74LS251	120p				
74LS257	110p				
74LS290	95p				
74LS293	120p				
74LS366	57p				
74LS373	70p				
74LS374	170p				
74LS375	140p				
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74LS393	135p				
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74LS195	87p	S/D Inverted Bus	2995p		
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74LS251	120p	S/D Inverted Bus	3495p		
74LS257	110p	FD1793 B-01			
74LS290	95p	D/D True Bus	5495p		
74LS293	120p	FD1794 B-01			
74LS366	57p	S/O True Bus	3495p		
74LS373	70p	FD1795 B D/D Inverted Bus, side select	5995p		
74LS374	170p	FD1797 B D/D True Bus, side select	5995p		
74LS375	140p				
74LS377	188p				
74LS393	135p				
74LS490	140p				
74LS700	260p				

74LS		SUPPORT DEVICES	
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74LS164	90p	6522	795p
74LS168	190p	6531	895p
74LS174	99p	6551	1095p
74LS175	99p	6810	375p
74LS195	87p	6820	425p
74LS221	110p	6821	425p
74LS244	175p	6850	425p
74LS245	325p	6852	425p
74LS251	120p	8212	395p
74LS257	110p	8214	450p
74LS290	95p	8216	395p
74LS293	120p	8224	395p
74LS366	57p	8228	395p
74LS373	70p	8251	395p
74LS374	170p	8253	1125p
74LS375	140p	8255	495p
74LS377	188p	8257	1050p
74LS393	135p	8259	1325p
74LS490	140p	8522	795p
74LS700	260p	P20 P14 12VLT	595p
		Z80 CT	595p
		Z80A P10	695p
		Z80A CTC	695p
		Z80 DMA	1995p
		Z80 DMA	395p
		Z80 S10/1	2995p
		Z80 S10/0	3495p
		Z80 S10/1	2995p
		Z80 S10/2	2995p
		Z80 S10/2	3495p

74LS		INTERFACE LINEAR	
74LS163	90p	MC1488	90p
74LS164	90p	MC1489	90p
74LS168	190p	DM8123	125p
74LS174	99p	75150	125p
74LS175	99p	75154	125p
74LS195	87p	75182	195p
74LS221	110p	75322	250p
74LS244	175p	75324	325p
74LS245	325p	75325	325p
74LS251	120p	75361	350p
74LS257	110p	75365	295p
74LS290	95p	75451	50p
74LS293	120p	75491/2	75p
74LS366	57p	8728	175p
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74LS221	110p		
74LS244	175p		
74LS245	325p		
74LS251	120p		
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74LS175	99p		
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74LS221	110p		
74LS244	175p		
74LS245	325p		
74LS251	120p		
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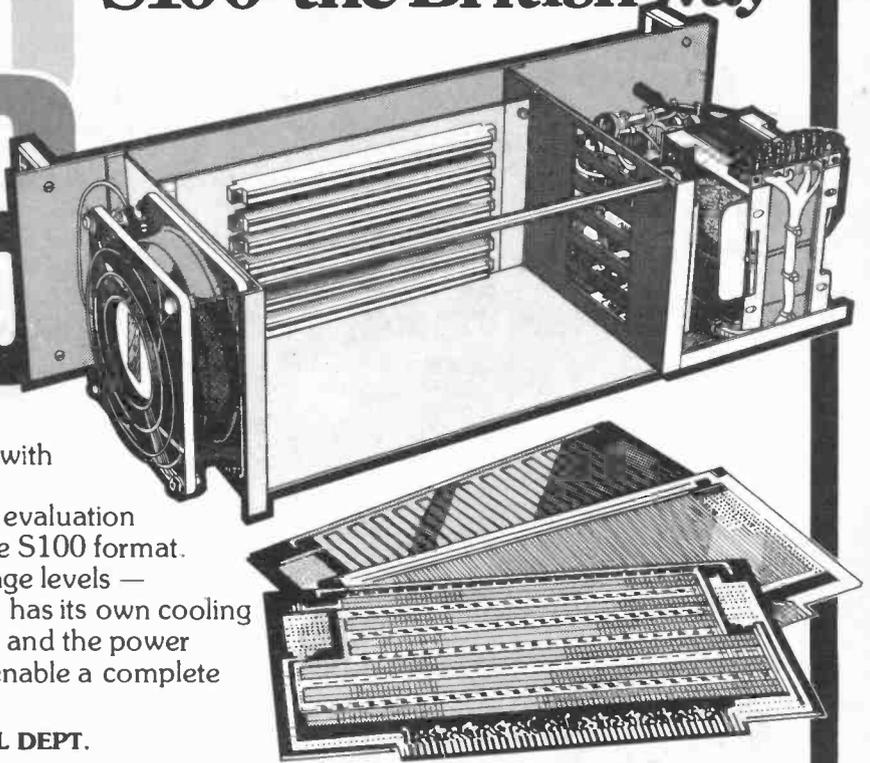
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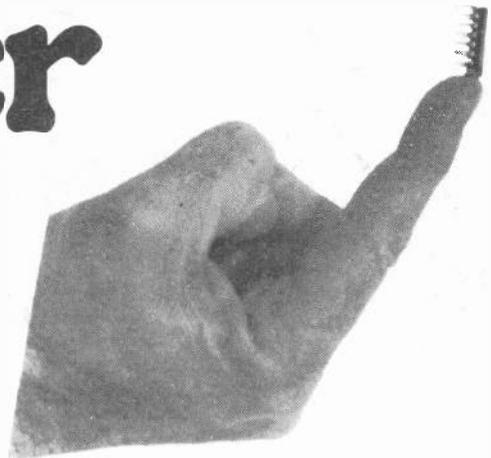
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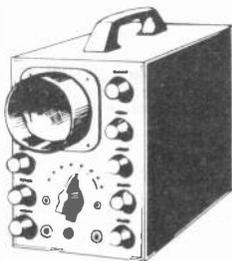


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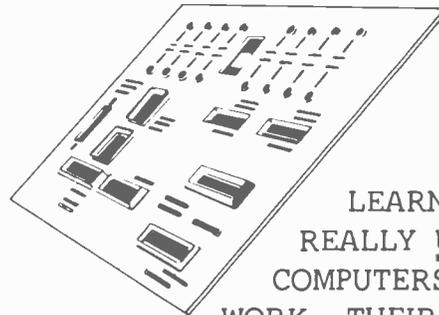
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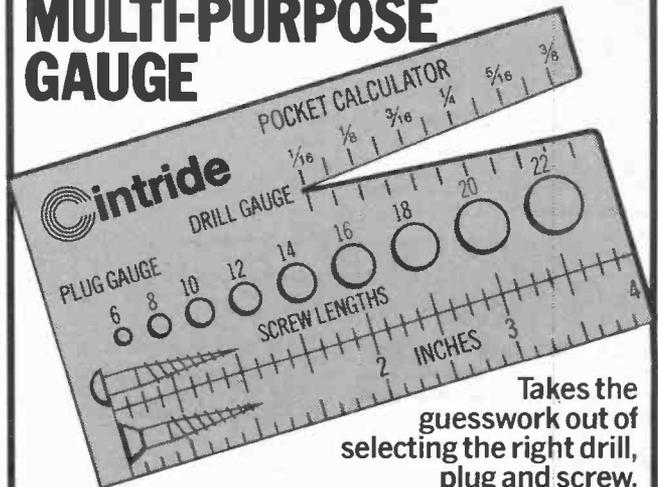
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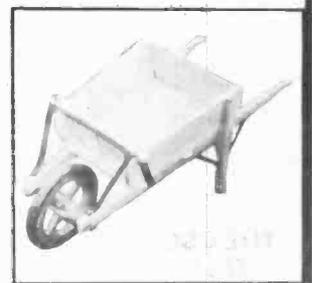
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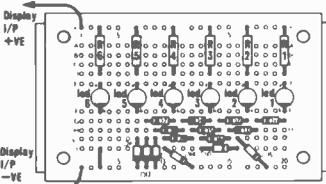
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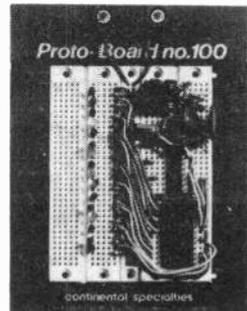
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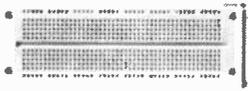


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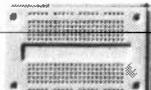
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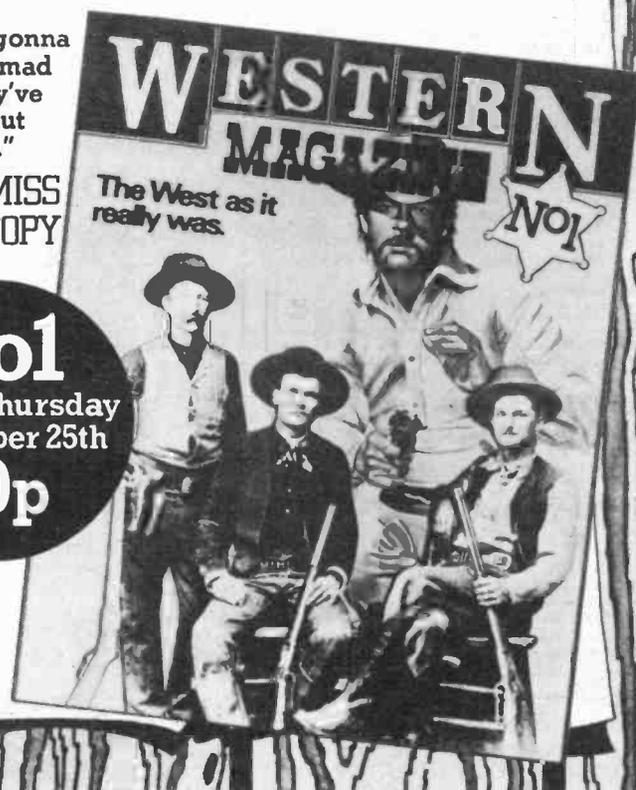
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**INDUSTRIAL ELECTRONICS:** Are you an electronic wireman/tester or prototype wireman? Have you had an apprenticeship followed by at least 5 years practical experience? If so we can offer you employment as an instructor with good promotion opportunities and pensionable security at Bristol and Swindon Skillcentres. Starting salary £6,000 p.a. rising by two increments to £7,110 p.a. For more information contact Miss A. Curran MSC TSD, 11 Park Place, Clifton, Bristol. Telephone Bristol 20661.

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## ELECTRONIC COMPONENTS

### MULTIMETER "NYCE" MOD. 360 TRCX TS/2567-00

Mirror backed view of pointer to avoid parallax errors in readings. Shock proof movement. Diode and Fuse protection. Sensitivity 100,000 Ohms/Volt.

**Technical Specification:**  
Ranges: D.C. Voltages: 0-0.25-2.5-10-50-250-1000V. A.C. Voltages: 0-5-10-50-250-1000V. D.C. Currents: 0-10 $\mu$ A-2.5mA-25mA-500mA-10 Amps. A.C. Currents: 0-10 Amps. Resistances:  $\times 1 \times 10 \times 1000 \times 10,000$  Ohms. Decibels: -10dB + 16dB + 62dB. Special measurements using two torch batteries of 1.5 Volts for Transistors. HFE 0-1000/ICO 0-50/A. Capacities: 5pF-30pF, 30pF-0.01uF, 0-01-50uF.  
Dimensions: 180  $\times$  140  $\times$  80 mm. **£39.25**

### MULTIMETER "NYCE" Mod. ETU 5000 TS/2561-00

50,000 Ohms/Volt. Range Doubler Switch. Mirror backed view of pointer to avoid parallax errors in readings. Ruby mounted movement—shock proof. Diode protection.

**Technical Specification:**  
Ranges: D.C. Voltages: 0-125-250 mV, 0-1-25-2.5-5-10-25-50-100-250-500-1000V. A.C. Voltages: 0-5-10-25-50-125-250-500-1000V. D.C. Currents: 0-5-10-25-50-100 Volts. D.C. Currents: 0-25-50 $\mu$ A-0.2-5-5-25-50-250-500 mA, 0-5-10 Amps. Resistances: 0-2K-20K-200K Ohms, 0-2M-20 Megohms. Centre of scale 10 Ohms. Decibels: -20+62dB in 8 ranges.  
Accuracy: D.C. Voltages: 125 mV - 2.5 V  $\pm$  4%, 500-1000V  $\pm$  3%. A.C. Voltages:  $\pm$  4% of full scale. D.C. Currents:  $\pm$  4%. Resistances:  $\pm$  3% of scale length.  
Sensitivity: D.C. Voltages & Currents: 50 K Ohms/Volt (V-A/2), 25 K Ohms/Volt (V-Ohm-A), 10 K Ohms/Volt (V-A/2). A.C. Voltages: 5 K Ohms/Volt (V-Ohm-A).  
Internal power supply: 1.5 volt battery (Pentorch), 9V Rectangular battery.  
Dimensions: 170  $\times$  124  $\times$  50 mm. **£16.60**

### MULTIMETER "NYCE" Mod. 304 TS/2562-00

Movement Ruby Mounted—shock proof. Complete with Case.

**Technical Specification:**  
Ranges: D.C. Voltages: 5-25-250-500V. A.C. Voltages: 10-50-500-1000V. D.C. Current: 250 $\mu$ A-250mA. Resistances: 0-600 K Ohms.  
Sensitivity: D.C. Voltages: 4,000 K Ohms/Volt. A.C. Voltages: 2,000 K Ohms/Volt.  
Internal Power Supply: 1.5 Volt battery (Pentorch).  
Dimensions: 90  $\times$  60  $\times$  30mm. **£5.80**

### MULTIMETER "NYCE" Mod. ETU-2000 TS/2560-00

20,000 Ohms/Volt. Mirror backed view of pointer to avoid parallax errors in readings. Ruby mounted movement—shock proof.

**Technical Specification:**  
Ranges: D.C. Voltages: 0-0.8-15-60-300-600-1200V. A.C. Voltages: 0-15-60-150-600-1200V. D.C. Currents: 0-60 $\mu$ A-0.3-30-300 mA. Resistances: 0-2K, 0-20K, 0-200K Ohms, 0-2 Megohms. Decibels & A.C. Voltages: -20+62dB, 0-15-60-150 V, 0-600 V.  
Accuracy: D.C. Voltage  $\pm$  3% of reading. A.C. Voltage:  $\pm$  4% of reading. D.C. Current:  $\pm$  3% of reading. Resistance:  $\pm$  3% of scale length.  
Db Accuracy & A.C. Accuracy:  $\pm$  4% of reading.  
Sensitivity: D.C. Voltages: 20 K Ohms/Volt. A.C. Voltages: 10 K Ohms/Volt.  
Decibel Scale Sensitivity: 10 K Ohms/Volt.  
Internal power supply: 1.5 Volt battery (Pentorch).  
Dimensions: 142  $\times$  100  $\times$  38 mm. **£10.15**

### MULTIMETER "NYCE" Mod. ETU 100—TS/2564-00

1000 Ohms/Volt. Mirror backed view of pointer to avoid parallax errors in readings. Ruby mounted movement—shock proof.

**Technical Specification:**  
Ranges: D.C. Voltages: 0-15-150-500-1000V. A.C. Voltages: 0-15-150-500-1000V. D.C. Currents: 0-1-150 mA. Resistance: 0-100 K Ohms (Centre scale 2.5 K Ohms).  
Accuracy: D.C. Voltages:  $\pm$  4% of reading. A.C. Voltages:  $\pm$  5% of reading. D.C. Currents:  $\pm$  4% of reading. Resistances:  $\pm$  4% of scale length.  
Sensitivity: D.C. Voltages: 1 K Ohm/Volt. A.C. Voltages: 1 K Ohm/Volt.  
Internal Power Supply: 1.5 Volt battery (Pentorch).  
Dimensions: 90  $\times$  63  $\times$  33mm. **£4.60**

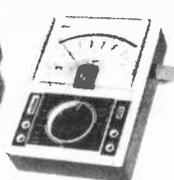
### MULTIMETER "NYCE" Mod. VF-25W TS/2566-00

20,000 Ohms/Volts. Versatile and Compact. Range Doubler Switch. Ruby mounted movement—shock proof.

**Technical Specification:**  
Ranges: D.C. Voltages: 0-0.25-2.5-5-25-150-500V, 0-0.5-5-50-300-1000V. A.C. Voltages: 0-15-150-500V, 0-30-300-1000V. D.C. Currents: 50 $\mu$ A-100 $\mu$ A, 0-2-5-250mA, 0-5-500mA. Resistances:  $\times 1 \times 100 \times 1K-32$  Ohms at centre of scale.  
Accuracy: D.C. Voltages & Currents:  $\pm$  3% of reading. A.C. Voltages:  $\pm$  4% of reading. Resistances:  $\pm$  3% of scale length.  
Sensitivity: D.C. Voltages: 20 K Ohms/Volt, 10 K Ohms/Volt. A.C. Voltages: 10 K Ohms/Volt, 5 K Ohms/Volt.  
Internal Power Supply: 1.5 Volt battery.  
Dimensions: 108  $\times$  79  $\times$  25 mm. **£13.25**



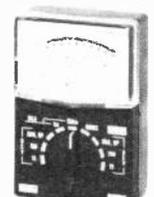
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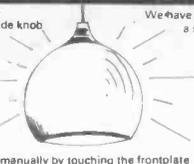
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We have designed the light dimmer unit to fit a standard wall box, the transmitter to fit your hand and the price to fit your pocket.

In two years' time everyone will be selling remote control dimmers but you can have your TDK300K kit NOW for only £14.30 for the dimmer unit and £4.20 for the transmitter. For the more athletic of you, the TD300K is still available at £6.50 and the TDE/K at £2.00.

DON'T FORGET to add 40p P&P and 15% VAT to your total purchase.



### REMOTE CONTROL COMPONENTS

LD271 IR Emitting Diode	36p
SF4205 Photodiode Detector	95p
SL430 IC Pulse Amp.	£1.70
SL490 32 command encoder/transmitter	£2.40
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ML925 16 channel receiver 4 momentary binary o/p	£1.40
ML925 16 channel receiver 4 latched binary o/p	£1.40
ML925 16 channel receiver 4 latched binary o/p	£1.40
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These ICs can be used with Infra red, ultrasonic or radio links, depending on range, cost and speed of operation.

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SN76477 Complex Sound Generator	£2.52
TBA800 5W Audio Amp.	68p
TBA810AS 7W Audio Amp.	£1.00
TDA1024 Zero Voltage Switch	£1.20
TDA2020 20W Audio Amp.	£2.85
ZN1034E Timer	£1.80

All ICs supplied with data sheets. Data Sheets only 10p each device.

### MINI KITS

These kits form useful subsystems which may be incorporated into larger designs or used alone. Kits include PCB, short instructions and all components.

**MK1 TEMPERATURE CONTROLLER / THERMOSTAT**  
Uses LM3911 IC to sense temperature (80°C max) and triac to switch heater. 1KW £4.00

**MK2 SOLID STATE RELAY**  
Ideal for switching motors, lights heaters, etc. from logic. Opto-isolated with zero voltage switching. Supplied without triac. Select the required triac from our range. £2.60

**MK3 BAR/DOT DISPLAY**  
Displays an analogue voltage on a linear 10-element LED display as a bar or single dot. Ideal for thermometers, level indicators, etc. May be stacked to obtain 20 to 100 element displays. Requires 5-20V supply. £4.75

**MK4 PROPORTIONAL TEMPERATURE CONTROLLER**  
Based on the TDA 1024 Zero voltage switch, this kit may be wired to form a "burst fire" power controller or a "proportional temperature" controller enabling the temperature of an enclosure to be maintained to within 0-5°C. 3KW £5.55

**MKS MAINS TIMER**  
Based on the ZN1034E Timer IC this kit will switch a mains load on (or off) for a preset time from 20 minutes to 35 hours. Longer or shorter periods may be realised by minor component changes. Maximum load 1KW. £4.50

### BOXES

Moulded in high impact ABS. Supplied with lids and screws. Black or white.

B2 95 x 71 x 35mm	85p
B3 115 x 95 x 37mm	95p

### RESISTORS

<b>ZENER DIODES</b>		<b>1W 220hm-10M</b>	
400mW 3-3V-30V	8p	Pack of 10 (one value)	10p
1-3V 7-5-30V	15p	10 packs (10 values)	80p

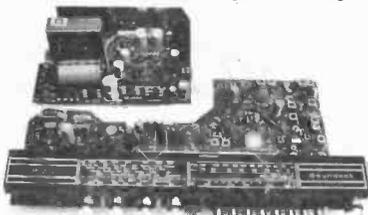
### TRIACS

<b>400V Plastic Case (Texas)</b>			
3A	49p	16A	95p
8A	58p	25A	190p
12A	80p		
6A with trigger			80p
8A Isolated tab			65p
Diac			18p

### FM/AM STEREO TUNER AMPLIFIER CHASSIS

Originally designed for installation into a music centre. Supplied as two separate built and tested units which are easily wired together. 240 volts A/C operation. Note Circuit diagram and inter-connecting wiring diagrams supplied.

**Rotary Controls** Tuning, volume, balance, treble and bass.  
**Push Button Controls** Mono, Tape, Disc, A.F.C., FM(VHF), LW, MW, SW.  
**Power Output** 7 watts RMS per channel into 8 ohms (10 watts music)  
**Tape Sensitivity** output typically 150mv. Input 300mv for rated output.  
**Disc Sensitivity** 100mv (ceramic cartridge).  
**Stereo Beacon Indicator** LED or bulb.  
**Size Tuner**—2½" x 15" x 7½" approx. Power amp.—2" x 7½" x 4½" approx.  
Price £22.00 + £2.50 Postage and Packing.



### J.V.C. TURNTABLE CHASSIS

J.V.C. Turntable supplied complete with an Audio Technica AT10 stereo magnetic cartridge.

★ 'S' shaped tone arm. ★ Belt driven. ★ Full size 12" platter. ★ Precision calibrated counter balance weight 0-3 grms). ★ Damped cueing lever. ★ Anti-skate (bias) device. Nylon thread weight. ★ Cut out template supplied. Size—12½" x 15½" (approx).  
Price £29.90 + £2.50 Postage and Packing.



### B. K. ELECTRONICS (Dept. EE)

37, Whitehouse Meadows, Eastwood, Leigh-on-Sea, Essex, SS9 5TY.  
★ S.A.E. for components list etc. ★ Official orders welcome.  
★ All prices include V.A.T. ★ Mail order only.  
★ All items packed (where applicable) in special energy absorbing PU foam.

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## Complete Audio/Tuner Kits



### Mk III FM Tuner series

Carriage for Mk III tuner £3 inc

The Mark III series FM tuner has been updated, and now includes a centre zero tuning meter as standard. The instruction manual has been meticulously revised, enabling easy assembly by constructors of various levels of experience - a preview copy may be purchased for £1.00.

Mark III A series 'Reference series' tuner modules .....£171.35 inc.  
Mark III B series 'Hyperfi' modules, with switched IF BW, pilot cancel decoder .....£198.95 inc.

A matching synthesiser unit will be made available later this year, and can be retrofitted to either version. All versions include digital frequency readout/clock, VU deviation meters, 6 preset stations, 10 turn pot manual tuning, toroidal PSU, output level adjustment, 110/240v AC input. Full alignment service available.

### Power Amplifier

Style and performance - with a real 'belt and braces' PSU design.

After a couple of preview comments, it seems that many of you are waiting to hear about the matching HMOSFET power amplifier for the Mk III tuner. Well, it's out at last - complete with twin toroidal PSUs for comfortable 80W RMS per channel, over 100W peak, but limited by thermal shutdown of the HMOS. 10W - 100W log LED output peak indicator, DC offset protection and switch-on pause relay. AC or DC input coupling, direct or relay protected output terminals. The works. Only one version of this item: Complete kit .....£178.25 inc. Carr. £5.

### Preamplifier

More features and facilities, thanks to DC switching and control design

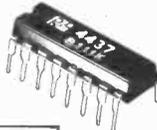
Previewing the most comprehensive audio preamplifier yet..... DC switching of 7 inputs, plus two tape in/outs. 2 low pass, 2 high pass active filters, genuine volume related loudness, 1dB channel matching, with DC volume, balance, bass and treble controls. Suitable for bus/remote control, tape dubbing, switched monitor etc. 80dB S/N+, THD -75dB or better. Pluggable PU equalization boards, tone control override. Price for complete unit about £149 ex VAT.

## Semiconductors

### Radio/Communications ICs

FOR COMPLETE LISTINGS - SEE OUR NEW PRICELIST

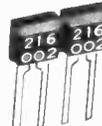
CA3089E	2.11	HA1197	1.61	SD6000	4.31
CA3189E	2.53	CA3123E	1.61	TDA4420	2.59
HA1137W	1.95	TDA1072	3.09	MC1330P	1.38
HA11225	2.47	TBA651	2.53	MC1350P	2.24
HA12412	2.81	TDA1090	3.51	KB4412	2.24
KB4420	1.95	TDA1220	1.61	KB4413	2.24
TBA120S	1.15	TDA1083	2.24	KB4417	2.53
KB4406	0.80	TDA1062	2.24	MC3357P	3.16



### VARICAP DIODES.....

A section from our PL:

BA102	0.35	16:1 ratio AM tuning
BB204	0.41	KV1215 9v triple 2.93
BB105	0.41	KV1211 9v dual 2.01
BB109	0.31	KV1225 25v triple 3.16
MVAM2	1.93	BB212 9v dual 2.25



### POWER MOSFETS

100W PA's made simple

Since pioneering the 100W complementary MOSFET technique - Hitachi have developed a range of output devices and drivers that ought to revolutionise opinions and attitudes towards the design of all LF amplification systems. We have a new 48 page application note (£1.50 inc) and complete sets of parts, modules and now the new complete PA system (see above).

2SK133 120v N-ch 100W MOSFET £6.33 2SJ48 Pch complement £6.33  
2SK135 160v N-ch 100W MOSFET £7.29 2SJ50 Pch complement £7.39  
PA101B Kit for 100W MOSFET PA less Heatsink £16.10. (£23 inc heatsink/bkt)

### ULTRA LOW NOISE PU PREAMPLIFIER

The HA12017 is the last word in PU preamps, and general low noise audio design. It is an SIL IC, with 86dB S/N in RIAA configuration, 10v RMS output capability, 0.002% typ THD at 10v RMS output (imagine the overload margin !!). It comfortably supercedes discrete circuit designs in terms of price/performance, and takes the art beyond the TDA1042's capabilities. (Replaces HA1457) £1.80 each - or an RIAA applications PCB with two ICs for £5.75. Complete with Rs&Cs £9.95.

### Radio Control ICs

We have various RC ICs, including NE544 NE5044, and two new ones from OK!

KB4445 - 4 channel dig. prop. FM TX IC. 30mW out (amplifiable) - £2.30 inc  
KB4446 - 4/5 ch. dig. prop FM RX IC. Suits KB4445 or RCME syst. £2.65.  
KB4445/6 pair: £4.75. New 8 page data sheet 35p + SAE. More RC ICs in list

### CMOS, LPSNTTL, TTL, MPU:

Most CMOS is available in low volume - also LPSN. Standard linears and TTL OK.

Listings in the new pricelist.

Things like ICM7216B, ICL8038, 8080A, 6800P, 2708, NE555, NE556, etc

Coming Soon.....

Contain yourselves, RF fans! Not yet ready for a full launch until autumn, but previewed here:-

### SSB transceiver system : 10kHz to 1000MHz !!

A modular VLF to UHF SSB TX/RX system at last. With the correct first mixer, the basic PCB covers 10kHz to 1000MHz - using LO fed from ext. source (our 2 IC Mullard synth for instance) and RF PA for TX. OP. 0.2uV basic sensitivity in HF. Typ cost for HF synth SSB RX will be less than £200. Add an RF PA for full TRX for another £50. See one in our foyer, and marvel.

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## Radio/Audio/Communications Modules

### LW-MW-SW-DC tuned and switched

91072 - All switching of bands by a single pin to gnd. Varicap tuned, with LO output for synth. MW/LW version or MW/LW plus 1 or 2 SW bands MW/LW: £15.58 +1SW £16.73



### VHF Tunerheads

Europe's largest stock range for broadcast and communications. Probably also the world's - details in the catalogues and PL. Specials are also supplied in the region 30 220MHz.

### Pilot Cancel PLL Stereo decoders

Again, Europe's widest range of stereo decoders including pilot cancel PLL types. The pic shows the 944378 - pilot cancel including post decoder 26/38kHz filtering and muting preamp output



944378-2  
£26.45

### Switched bandwidth FM IF strips

Broadcast FM IF strips for all occasions, including the new 911225 - with diode switched narrow filter option, ultra linear phase ceramic filters, 84dB S/N, and 0.04% THD (40kHz deviation). Plus usual things like AGC, AFC, dev. mute, level meter drive. £23.95 (supplied in screen can with 0.1 edge connection system) Also the 7230 hyperfi series - as the 911225, but with slope controlled AFC that operates in conjunction with signal level - and an extra IF amp stage for DXing.

### Various digital frequency displays

The World's largest range of receiver DFM's is now joined by the DFM7 (shown) - and L shaped version of the DFM3 with remote display mount connector possibility. 1kHz SW resolution with 455kHz or 10.7MHz offsets, 100Hz res up to 3.9999MHz, and VHF to 299.99 MHz in 10kHz steps : £41.75



## Components

### Crystal Filters

Most popular types are available ex-stock, and in quantity.

10.7MHz	25kHz Channel spacing 8pole	£16.67
	12½kHz	£17.82
	2.4kHz SSB	£19.78
	Monolithic dual roofing filter	£2.30
34.5MHz	1.3dB loss, 80dB stopband HF first filter in synth. RX	£36.80
RC XTALS	FM pairs (no spilt)	£3.74
	AM pairs	£3.57
USB/LSB	Xtals for 10.7SSB filter	£2.88 ea



### Piezo Sounders

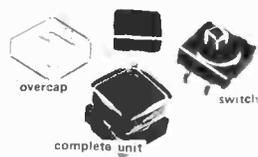
The most efficient warning sounders yet

The latest thing in electro-acoustic efficiency. 1mA of drive from CMOS will give an SPL of 83dB - 10v RMS drive from CMOS uses 3mA for 100dB SPL at 4.8kHz (88dB at 1.65kHz) The data sheets shows various drive circuits, and give full specifications with regard to broadband responses and power consumption etc. 1 off 44p inc. 100 off 28.75p (25p ex vat)



### Keyboard switches and caps

From the world's most widely used switch manufacturers - ALPS - come the biggest and best range of keyswitches, and data entry keyboard switches. The SCM81101 is shown here, with the KT5 2-part cap (with clear top, to enable easy fitting of your chosen legend. Other types are available with built in LED, 90° mounting etc. SCM81101 : 17p, KT5 : 16p - or 29p/pair



### LCD CLOCKS

Clocks use 1.5v at 15uA only - DVM 9v/1mA

### LCD DVM

CM161: 7mm LCD 12/24hr, alarms etc £11.44 each  
CM172: 13mm, 12hr, alarms, timer etc £14.32 ea  
CM174: 13mm, 12hr, min/sec stopwatch £14.32 ea  
DVM 176: ICM7106 based LCD 3½digit £22.36 each



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### POWER MOSFET APPLICATIONS HANDBOOK by HITACHI

£1.50 each - or free with pairs of HMOS and the PA101B

Everything you should know about HMOSFET devices theory and applications.

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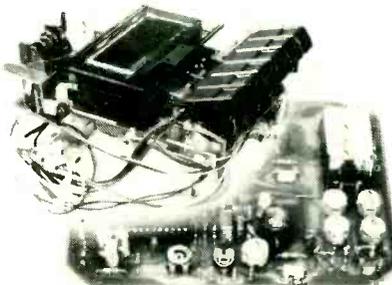
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