

EVERYDAY

SEPTEMBER 1996

**PRACTICAL**

# ELECTRONICS

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Writes the time  
"in the air"



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*"Power consumption"*  
indicator for boats,  
caravans, etc.

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DELAY/FLANGER**  
Simple musical  
effects unit

**MAX038 WAVEFORM  
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timing or p.c.b. making

**Plus** **INGENUITY UNLIMITED**  
NEW TECHNOLOGY UPDATE

**CIRCUIT SURGERY FOX REPORT** NET WORK - *The Internet Page*



**THE No. 1** MAGAZINE FOR  
ELECTRONICS TECHNOLOGY  
& COMPUTER PROJECTS



**MOONSHINE BIBLE** 270 page book covering the production of alcohol from potatoes, rice, grains etc Drawings of simple home made stills right through to commercial systems. £15 ref MS1

**NEW HIGH POWER MINI BUG** With a range of 800 metres or more and up to 100 hours use from a PP3 this will be popular! Bug measures less than 1" square! £28 Ref LOT102.

**SINCLAIR C6 MOTORS** We have a new ones available without gearboxes at £50 ref LOT25

**BUILD YOUR OWN WINDFARM FROM SCRAP** New publication gives step by step guide to building wind generators. Armed with this publication and a good local scrap yard could make you self sufficient in electricity! £12 ref LOT81

**PC KEYBOARDS** PS2 connector, top quality suitable for all 286/386/486 etc £10 ref PCKB 10 for £65.

**TRACKING TRANSMITTER** range 1.5-5 miles, 5,000 hours on AA batteries, also transmits info on car direction and motion! Works with any FM radio. 1.5" square. £65 ref LOT101

**ELECTRIC DOOR LOCKS** Complete lock with both Yale lock and 12v operated deadlock (keys included) £10 ref LOT99

**GALLIUM ARSENIDE FISHEYE PHOTO DIODES** Complete with suggested circuits for long range communications/switching £12 complete.

**SURVEILLANCE TELESCOPE** Superb Russian zoom telescope adjustable from 15x to 60x! complete with metal tripod (impossible to use without this on the higher settings) 66mm lense, leather carrying case £149 ref BAR69

**WIRELESS VIDEO BUG KIT** Transmits video and audio signals from a miniature CCTV camera (included) to any standard television! All the components including a PP3 battery will fit into a cigarette packet with the lens requiring a hole about 3mm diameter. Supplied with telescopic aerial but a piece of wire about 4" long will still give a range of up to 100 metres. Single PP3 will probably give less than 1 hours use. £99 REF EP79. (probably not licensable!)

**CCTV CAMERA MODULES** 46X70X29mm, 30 grams, 12v 100mA, auto electronic shutter, 3.6mm F2 lens, CCIIR, 512x492 pixels, video outputs 1v p-p (75 ohm) Works directly into a scart or video input on a tv or video. IR sensitive. £79.95 ref EF137.

**IR LAMP KIT** Suitable for the above camera enables the camera to be used in total darkness! £5.99 ref EF138.

**REMOTE CONTROLLED DATA TD1400 MODEM/VIEWDATA** Complete system comprising 1200/75 modem, auto dialler, infra red remote keyboard, (could be adapted for PC use?) psu, UHF and RGB output, phone lead, RS232 output, composite output. Absolute bargain for parts alone! £9.95 ref BAR33

## 9 WATT CHIEFTAN TANK LASERS

Double beam units designed to fit in the gun barrel of a tank, each unit has two semi conductor lasers and motor drive units for alignment, 7 mile range, full circuit diagrams, new price £50.00/00? us? £349. Each unit has two gallium Arsenide injection lasers, 1 x 9 watt, 1 x 3 watt, 900nm wavelength, 28vdc, 600hz pulse frequency. The units also contain an electronic receiver to detect reflected signals from targets, five or more units £299 ea. £349 for one. Ref LOT4.

**TWO WAY MIRROR KIT** Includes special adhesive film to make two way mirror(s) up to 60"x20". (glass not included) Includes full instructions. £12 ref TW1.

**NEW LOW PRICED COMPUTER/WORKSHOP/HI-FI/RCB UNITS** Complete protection from faulty equipment for everybody! Inline units fits in standard IEC lead (extends to 750mm), fitted in less than 10 seconds, reset/test button, 10A rating, £6.99 each ref LOT5. Or a pack of 10 at £49.90 ref LOT6. If you want a box of 100 you can have one for £250!

**RADIO CONTROLLED CARS FROM £6 EACH!!!!** All returns from famous manufacturer, 3 types available, single channel (left, right, forwards, backwards) £6 ref LOT1. Two channel with more features £12 ref LOT2.

**THOUSANDS AVAILABLE RING/FAX FOR DETAILS!** **MAGNETIC CARD READERS** (swipes) £9.95 Cased with flyleads, designed to read standard credit cards! they have 3 wires coming out of the head so they may write as well? complete with control electronics PCB. just £9.95 ref BAR31

**WANT TO MAKE SOME MONEY? STUCK FOR AN IDEA?** We have collated 140 business manuals that give you information on setting up different businesses, you peruse these at your leisure using the text editor on your PC. Also included is the certificate enabling you to reproduce (and sell) the manuals as much as you like! £14 ref EP74

**PANORAMIC CAMERA OFFER** Takes double width photographs using standard 35mm film. Use in horizontal or vertical mode. Complete with strap £7.99 ref BAR1

**COIN OPERATED TIMER KIT** Complete with coin slot mechanism, adjustable time delay, relay output, put a coin slot on anything you like! TV's, videos, fridges, drinks cupboards, HiFi, takes 50p's and £1 coins, DC operated, price just £7.99 ref BAR27

**ZENITH 900 X MAGNIFICATION MICROSCOPE** Zoom, metal construction, built in light, shrimp farm, group viewing screen, lots of accessories. £29 ref ANAYLT.

**AA NICAD PACK** Pack of 4 tagged AA nicads £2.99 ref BAR34

**PLASMA SCREENS** 222x310mm, no data hence £4.99 ref BAR87

**NIGHTSIGHTS** Model T2S4 with infra red illuminator, views up to 75 metres in full darkness in infrared mode, 150m range, 45mm lens, 13 deg angle of view, focussing range 1.5m to infinity. 2 AA batteries required. 950g weight £199 ref BAR61. 1 years warranty

**LIQUID CRYSTAL DISPLAYS Bargain prices,** 16 character 2 line, 99x24mm £2.99 ref SM1623A  
20 character 2 line, 83x19mm £3.99 ref SM2020A  
16 character 4 line, 62x25mm £5.99 ref SMC1640A

**TAL-1 110MM NEWTONIAN REFLECTOR TELESCOPE** Russian. Superb astronomical scope, everything you need for some

serious star gazing! up to 160x magnification. Send or fax for further

## WOLVERHAMPTON BRANCH NOW OPEN AT WORCESTER ST WILMINGTON TEL: 01902 22039

details £249 ref TAL-1

**CENTRAL POINT PC TOOLS** Award winning software, 1,300 virus checker, memory optimiser, disc optimiser, file compression, low level formatting, backup scheduler, disk defragmenter, undelete, 4 calculators, Dbase, disc editor, over 40 viewers, remote computing, password protection, encryption, comprehensive manual supplied etc £25 ref lot 97 3.5" disks.

**GOT AN EXPENSIVE BIKE?** You need one of our bottle alarms, they look like a standard water bottle, but open the top, insert a key to activate a motion sensor alarm built inside. Fits all standard bottle cameras, supplied with two keys. SALE PRICE £7.99 REF SA32.

**GOT AN EXPENSIVE ANYTHING?** You need one of our cased vibration alarms, keyswitch operated, fully cased just fit it to anything from videos to caravans, provides a years protection from 1 PP3 battery, UK made. SALE PRICE £4.99 REF SA33.

**DAMAGED ANSWER PHONES** These are probably beyond repair so just £4.99 each. BT response 200 machines. REF SA30.

**COMPUTER DISC CLEAROUT** We are left with a lot of software packs that need clearing so we are selling at disc value only! 50 discs for £4, that's just 8p each!! (our choice of discs) £4 ref EP66

**IBM PS2 MODEL 160Z CASE AND POWER SUPPLY** Complete with fan etc and 200 watt power supply. £9.95 ref EP67

**DELL PC POWER SUPPLIES** 145 watt, +5, -5, +12, -12, 150x150x85mm complete with switch, flyleads and IEC socket. SALE PRICE £9.99 ref EP55

**1.44 DISC DRIVES** Standard PC 3.5" drives but returns so they will need attention SALE PRICE £4.99 ref EP68

**1.2 DISC DRIVES** Standard 5.25" drives but returns so they will need attention SALE PRICE NOW ONLY £3.50 ref EP69

**PP3 NICADS** Unused but some storage marks. £4.99 ref EP52

**DELL PC POWER SUPPLIES** (Customer returns) Standard PC psu's complete with fly leads, case and fan +12v, -12v, +5v, -5v SALE PRICE £1.99 EACH worth it for the bits alone! ref DL1. TRADE PACK OF 20 £28.95 Ref DL2.

**GAS HOBS AND OVENS** Brand new gas appliances, perfect for small flats etc. Basic 3 burner hob SALE PRICE £24.99 ref EP72. Basic small built in oven SALE PRICE £79 ref EP73

**RED EYE SECURITY PROTECTOR** 1,000 watt outdoor PIR switch SALE PRICE £8.99 ref EP57

**ENERGY BANK KIT** 100 6"x6" 6v 100mA panels, 100 diodes, connection details etc. £69.95 ref EF112

**PASTEL ACCOUNTS SOFTWARE**, does everything for all sizes of businesses. Includes word processor, report writer, windowing, networkable up to 10 stations, multiple cash books etc. 200 page comprehensive manual. 90 days free technical support. (01342-326009 try before you buy!) Current retail price is £129, SALE PRICE £9.95 ref SA12. SAVE £120!!

**COMPLETE PC 200 WATT UPS SYSTEM** Top of the range UPS system providing protection for your computer system and valuable software against mains power fluctuations and cuts New and boxed, UK made Provides up to 5 mins running time in the event of complete power failure to allow you to run your system down correctly. LAST FEW TO CLEAR AT £49 SAVE £30 ref LOT61

**BIG BROTHER PSU** Cased PSU, 6v 2A output, 2m o/p lead, 1.5m input lead, UK made 220v. SALE PRICE £4.99 REF EP7



Check out our  
WEB SITE

<http://www.pavilion.co.uk/bull-electrical>

**RACAL MODEM BONANZA!** 1 Racal MPS1223 1200/75 modem, telephone lead, mains lead, manual and comms software, the cheapest way onto the net! all this for just £13 ref DEC13.

**4.5mw LASER POINTER, BRAND NEW MODEL NOW IN STOCK!**, supplied in fully built form (looks like a nice pen) complete with handy pocket o/p (which also acts as the on/off switch.) About 60 metres range! Runs on 2 AAA batteries. Produces thin red beam ideal for levels, gun sights, experiments etc. Just £39.95 ref DEC49 TRADE PRICE £28 MIN 10 PIECES

**BULL TENS UNIT** Fully built and tested TENS (Transcutaneous Electrical Nerve Stimulation) unit, complete with electrodes and full instructions. TENS is used for the relief of pain etc in up to 70% of sufferers. Drug free pain relief, safe and easy to use, can be used in conjunction with analgesics etc. £49 REF TEN/1

**PC PAL VGA TO TV CONVERTER** Converts a colour TV into a basic VGA screen, complete with built in psu, lead and swave. Ideal for laptops or a cheap upgrade. Supplied in kit form for home assembly. SALE PRICE £25 REF SA34

**EMERGENCY LIGHTING UNIT** Complete unit with 2 double

\*SOME OF OUR PRODUCTS MAY BE UNLICENSABLE IN THE UK

## BULL ELECTRICAL

250 PORTLAND ROAD, HOVE, SUSSEX.  
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FAX 01273 323077

E-mail [bulk@pavilion.co.uk](mailto:bulk@pavilion.co.uk)

bulb floodlights, built in charger and auto switch. Fully cased. 6v 8AH lead acid req'd. (secondhand) £4 ref MAG4P11

**YUASHA SEALED LEAD ACID BATTERIES** Two sizes currently available this month. 12v 15AH at £18 ref LOT8 and 6v 10AH (suitable for emergency lights above) at just £6 ref LOT7

**ELECTRIC CAR WINDOW DE-ICERS** Complete with cable, plug etc SALE PRICE JUST £4.99 REF SA28

**AUTO SUNCHARGER** 155x300mm solar panel with diode and 3 metre lead fitted with a cigar plug. 12v 2watt. £8.99 REF SA25.

**MICRODRIVE STRIPPERS** Small cased tape drives ideal for stripping, lots of useful goodies including a smart case, and lots of components. SALE PRICE JUST £4.99 FOR FIVE REF SA26

**SOLAR POWER LAB SPECIAL** You get TWO 6"x6" 6v 130mA solar cells, 4 LED's, wire, buzzer, switch plus 1 relay or motor. Superb value kit SALE PRICE JUST £4.99 REF SA27

**RGB/CGA/EGA/TTL COLOUR MONITORS** 12" in good condition. Back anodised metal case. SALE PRICE £49 REF SA16B

**PLUG IN ACORN PSU** 19v AC 14w. £2.99 REF MAG3P10

**13.8V 1.9A PSU** cased with leads. Just £9.99 REF MAG10P3

**UNIVERSAL SPEED CONTROLLER KIT** Designed by us for the C5 motor but ok for any 12v motor up to 30A. Complete with PCB etc. A heat sink may be required. £17.00 REF: MAG17

**PHONE CABLE AND COMPUTER COMMUNICATIONS PACK** Kit contains 100m of 6 core cable, 100 cable clips, 2 line drivers with RS232 interfaces and all connectors etc. Ideal low cost method of communicating between PC's over a long distance utilizing the serial ports. Complete kit £8.99. Ref comp1.

**VIEWDATA SYSTEMS** made by Philips, complete with internal 1200/75 modem, keyboard, psu etc RGB and composite outputs, menu driven, autodialler etc. SALE PRICE £12.99 REF SA18

**AIR RIFLES .22** As used by the Chinese army for training purposes, so there is a lot about! £39.95 Ref EF78. 500 pellets £4.50 ref EF80.

**PLUG IN POWER SUPPLY SALE FROM £1.60** Plugs in to 13A socket with output lead, three types available, 9vdc 150mA £1.50 ref SA19, 9vdc 200mA £2.00 ref SA20, 6.5vdc 500mA £2 ref SA21.

**VIDEO SENDER UNIT.** Transmits both audio and video signals from either a video camera, video recorder, TV or Computer etc to any standard TV set in a 100' range! (tune TV to a spare channel) 12v DC op. Price is £25 REF: MAG15 12v psu is £5 extra REF: MAG5P2

**\*MINIATURE RADIO TRANSCEIVERS** a pair of walkie talkies with a range up to 2 km in open country. Units measure 22x52x155mm including cases and ear pieces. 2xPP3 req'd. £30.00 pr. REF: MAG30

**\*FM TRANSMITTER KIT** housed in a standard working 13A adapter!! the bug runs directly off the mains so lasts forever! why pay £700? or price is £15 REF: EF62 (kit) Transmits to any FM radio.

**\*FM BUG BUILT AND TESTED** superior design to kit. Supplied to detective agencies, 9v battery req'd. £14 REF: MAG14

**TALKING COINBOX STRIPPER COMPLETE WITH COIN SLOT MECHANISMS** originally made to retail at £79 each, these units are designed to convert an ordinary phone into a payphone. The units have the locks missing and sometimes broken hinges. However they can be adapted for their original use or used for something else??! SALE PRICE JUST £2.50 REF SA23

**GAT AIR PISTOL PACK** Complete with pistol, darts and pellets £12.95 Ref EF82B extra pellets (500) £4.50 ref EF80

**6"X12" AMORPHOUS SOLAR PANEL** 12v 155x310mm 130mA. SALE PRICE £4.99 REF SA24

**FIBRE OPTIC CABLE BUMPER PACK** 10 metres for £4.99 ref MAG5P13 ideal for experimenters! 30 m for £12.99 ref MAG13P1

MIXED GOODIES BOX OF  
MIXED COMPONENTS WEIGHING 2 KILOS  
YOURS FOR JUST £6.99

**4X28 TELESCOPIC SIGHTS** Suitable for all air rifles, ground lenses, good light gathering properties. £19.95 ref R77.

**GYROSCOPES** Remember these? well we have found a company that still manufactures these popular scientific toys, perfect gift or for educational use etc. £6 ref EP70

**HYPOTHERMIA SPACE BLANKET** 215x150cm aluminised foil blanket, reflects more than 90% of body heat. Also suitable for the construction of two way mirrors! £3.99 each ref O/L041

**LENSTATIC RANGER COMPASS** Oil filled capsule, strong metal case, large luminous points. Slight line with magnifying viewer. 50mm dia, 86gm. £10.99 ref O/K604

**RECHARGE ORDINARY BATTERIES UP TO 10 TIMES!** With the Battery Wizard! Uses the latest pulse wave charge system to charge all popular brands of ordinary batteries AAA, AA, C, D, four at a time! Led system shows when batteries are charged, automatically rejects unsuitable cells, complete with mains adaptor. BS approved. Price is £21.95 ref EP31.

**TALKING WATCH** Yes, it actually tells you the time at the press of a button. Also features a voice alarm that wakes you up and tells you what the time is! Lithium cell included. £7.99 ref EP26

**PHOTOGRAPHIC RADAR TRAPS CAN COST YOU YOUR LICENCE!** The new multiband 2000 radar detector can prevent even the most responsible of drivers from incurring their licence! Adjustable audible alarm with 8 flashing leds gives instant warning of radar zones. Detects X, K, and Ka bands, 3 mile range, 'over the hill' 'around bends' and 'rear trap facilities. micro size just 4.25"x2.5"x.75". Can pay for itself in just one day! £79.95 ref EP3.

**3" DISCS** As used on older Amstrad machines. Spectrum plus 3's etc £3 each ref BAR400.

**STEREO MICROSCOPES BACK IN STOCK** Russian, 200x complete with lenses, lights, filters etc etc very comprehensive microscope that would normally be around the £700 mark, our price is just £299 (full money back guarantee) full details in catalogue

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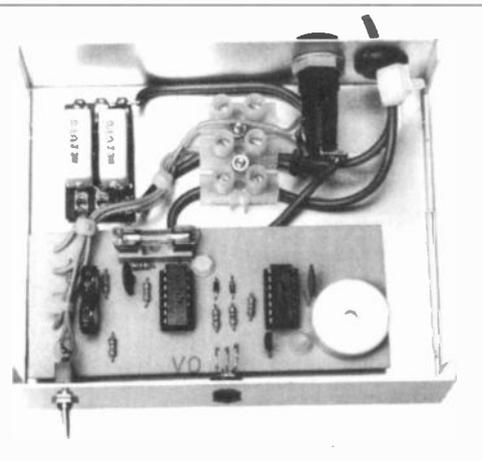
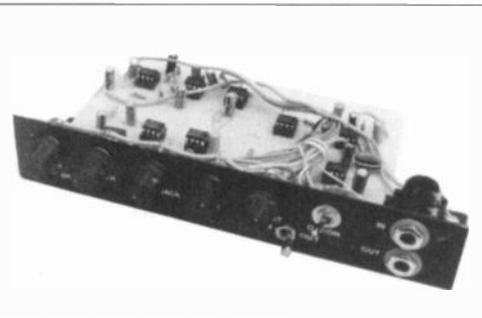
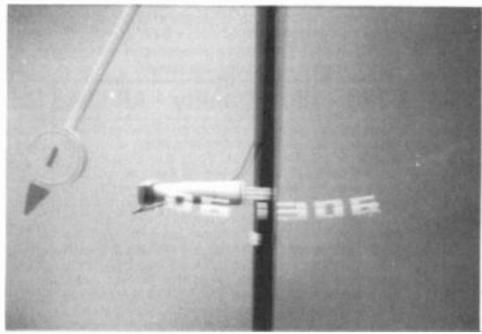
VOL. 25 No. 9 SEPTEMBER 1996

EVERYDAY

PRACTICAL

# ELECTRONICS

The No. 1 Magazine for Electronics, Technology  
 and Computer Projects



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Our October '96 Issue will be published on Friday, 6 September 1996. See page 659 for details.

Everyday Practical Electronics, September 1996

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- ANALOGUE DELAY AND FLANGER** by John Chatwin 670  
 There could be a short delay to improving your musicality!
- SIMPLE EXPOSURE TIMER** by Andy Flind 684  
 Make light work of exposure timing for printing p.c.b.s or photos
- PIC-TOCK PENDULUM CLOCK** by John Becker 697  
 Time don't mean a thing if it ain't got that swing!
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 How not to get the wind up about draughts blowing holes in your budget
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 Keep a colourful watch on caravan and boating battery power consumption

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 Safely handling lead-acid batteries; the Great NiCad Debate continues; alkaline cell tabbing
- INTERFACE** by Robert Penfold 690  
 Transistor tester interface for PC parallel ports
- INGENUITY UNLIMITED** hosted by Alan Winstanley 710  
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 Advice to beginners on choosing suitable projects and how to build and check them
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# THE ORIGINAL SURPLUS WONDERLAND!

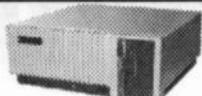
THIS MONTH'S SELECTION FROM OUR VAST EVER CHANGING STOCKS

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## LOW COST PC's -

### SPECIAL BUY 'AT 286'

40Mb HD + 3Mb Ram



LIMITED QUANTITY only of these 12MHz HI GRADE 286 systems MADE IN THE USA to an industrial specification, the system was designed for total reliability. The compact case houses the motherboard, PSU and EGA video card with single 5 1/4" 1.2 Mb floppy disk drive & integral 40Mb hard disk drive to the front. Real time clock with battery backup is provided as standard. Supplied in good used condition complete with enhanced keyboard, 640k + 2Mb RAM, DOS 4.01 and 90 DAY Full Guarantee. Ready to Run!  
Order as HIGHRAE 286 **ONLY £129.00** (€)

Optional Fitted extras: VGA graphics card **£24.95** (€)  
1.4Mb 3 1/2" floppy disk drive (instead of 1.2 Mb) **£19.95**  
Wordperfect 8.0 for Dos - when 3 1/2" FDD option ordered **£22.50**  
NE2000 Ethernet (thick, thin or twisted) network card **£29.00**

## LOW COST 486DX-33 SYSTEM

Limited quantity of this 2nd year, superb small size desktop unit. Fully featured with standard SIMM connectors 30 & 72 pin. Supplied with keyboard, 4 Mb of RAM, SVGA monitor output, 256k cache and integral 120 Mb IDE drive with single 1.44 Mb 3.5" floppy disk drive. Fully tested and guaranteed. Fully expandable.  
Many other options available - call for details. **£399.00** (€)

## FLOPPY DISK DRIVES 3 1/2" - 8"

5 1/4" or 3 1/2" from only £18.95!

Massive purchases of standard 5 1/4" and 3 1/2" drives enables us to present prime product at industry beating low prices! All units (unless stated) are BRAND NEW or removed from often brand new equipment and are fully tested, aligned and shipped to you with a 90 day guarantee and operate from standard voltages and are of standard size. All are IBM-PC compatible (if 3 1/2" supported on your PC).

3 1/2" Panasonic JU363/4 720K or equivalent RFE	£24.95 (€)
3 1/2" Mitsubishi MF35C-L 1.4 Meg. Laptop only	£25.95 (€)
3 1/2" Mitsubishi MF35C-D 1.4 Meg. Non laptop	£18.95 (€)
5 1/4" Teac FD-55GFR 1.2 Meg (for IBM PC's) RFE	£18.95 (€)
5 1/4" Teac FD-55F-03-U 720K 40/80 (for BBC's etc) RFE	£29.95 (€)
5 1/4" BRAND NEW Mitsubishi MF501B 360K	£22.95 (€)
Table top case with integral PSU for HH 5 1/4" Flopp or HD	£29.95 (€)
8" Shugart 801/801 8" SS refurbished & tested	£195.00 (€)
8" Shugart 810 8" SS HH Brand New	£250.00 (€)
8" Shugart 851 8" double sided refurbished & tested	£250.00 (€)
Mitsubishi M2894-63 8" double sided NEW	£275.00 (€)
Mitsubishi M2896-63-02U 8" DS slimline NEW	£285.00 (€)
Dual 8" cased drives with integral power supply 2 Mb	£499.00 (€)

## HARD DISK DRIVES

End of line purchase scoop! BRAND NEW NEC D2246 8" 85 Mbyte drive with industry standard SMD interface, replaces Fujitsu equivalent model. Full manual. Only £299.00 or 2 for £525.00 (€)

3 1/2" FUJIK-309-26 20mb MFM I/F RFE	£59.95 (€)
3 1/2" CONNER CP3024 20 mb IDE I/F (or equiv RFE)	£59.95 (€)
3 1/2" CONNER CP3044 40mb IDE I/F (or equiv RFE)	£69.00 (€)
3 1/2" RODIME RC3057S 45mb SCSI I/F (Mac & Acorn)	£185.00 (€)
3 1/2" WESTERN DIGITAL 850mb IDE I/F Brand New	£149.95 (€)
5 1/4" MINISCRIBE 3425 20mb MFM I/F (or equiv) RFE	£49.95 (€)
5 1/4" SEAGATE ST-238R 30 mb RLL I/F Refurb	£69.95 (€)
5 1/4" CDC 94205-51 40mb HH MFM I/F RFE tested	£69.95 (€)
5 1/4" HP 9754B 850 Mb SCSI RFE tested	£89.00 (€)
5 1/4" HP C3010 2 Gbyte SCSI differential RFE tested	£195.00 (€)
8" FUJITSU M2322K 160Mb SMD I/F RFE tested	£195.00 (€)

Hard disc controllers for MFM, IDE, SCSI, RLL etc. from £16.95

## THE AMAZING TELEBOX

Converts your colour monitor into a QUALITY COLOUR TV!!



TV SOUND & VIDEO TUNER CABLE COMPATIBLE

The TELEBOX is an attractive fully cased mains powered unit, containing all electronics ready to plug into a host of video monitors made by makers such as MICROVITEC, ATARI, SANYO, SONY, COMMODORE, PHILIPS, TATUNG, AMSTRAD etc. The composite video output will also plug directly into most video recorders, allowing reception of TV channels not normally receivable on most television receivers\* (TELEBOX MB). Push button controls on the front panel allow reception of 8 fully tuneable 'off air' UHF colour television channels. TELEBOX MB covers virtually all television frequencies VHF and UHF including the HYPERBAND as used by most cable TV operators. A composite video output is located on the rear panel for direct connection to most makes of monitor or desktop computer video systems. For complete compatibility - even for monitors without sound - an integral 4 watt audio amplifier and low level Hi Fi audio output are provided as standard.

TELEBOX ST for composite video input type monitors	£36.95
TELEBOX STL as ST but fitted with integral speaker	£39.50
TELEBOX MB Multiband VHF/UHF/Cable/Hyperband tuner	£69.95

For overseas PAL versions state 5.5 or 6 MHz sound specification.  
\*For cable / hyperband reception Telebox MB should be connected to a cable type service. Shipping code on all Teleboxes is (B)

## DC POWER SUPPLIES

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PHILIPS HCS31 Ultra compact 9" colour video monitor with standard composite 15.625 KHz video input via SCART socket. Ideal for all monitoring / security applications. High quality, ex-equipment fully tested & guaranteed (possible minor screen burns). In attractive square black plastic case measuring W10" x H10" x 1 3/4" D. 240 V AC mains powered.  
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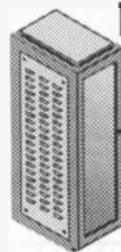
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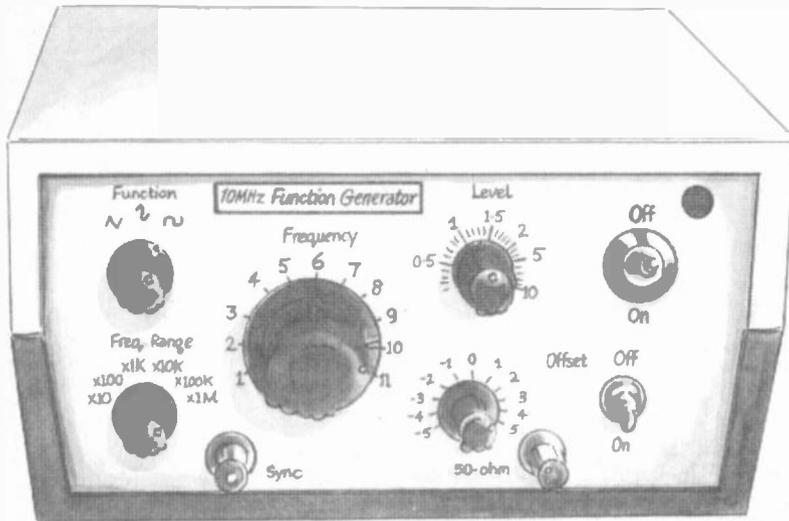
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## 10MHz FUNCTION GENERATOR

This straightforward project uses the MAX038 chip described in this issue to provide sine, square and triangle output waveforms from 10Hz to 10MHz in six switched ranges.

Together with the multimeter and the oscilloscope, a "function generator" is one of the

most useful pieces of equipment an electronics enthusiast can possess. It generates signals over a wide range of frequencies, and gets its name from the fact that it can also provide various output waveforms. Usually these are triangular waves and squarewaves in addition to the basic sinewaves, and users soon discover the value of these for testing different types of circuit. Squarewaves, for example, are useful when checking for overshoot and ringing, whilst a triangular waveform is handy when looking for amplifier "crossover" distortion. Often the output can have a variable d.c. "offset" voltage added to the a.c. signal. This too has various applications, an example is a 5V squarewave output with a 2.5V positive offset which would be suitable for directly driving many logic inputs.

## DIRECT CONVERSION RECEIVER FOR TOP BAND AND EIGHTY METRES

Interested in amateur radio? Want to listen in to amateur transmissions from around the world? If so this design is for you. As an introduction to shortwave listening on the amateur bands this direct conversion receiver probably represents the easiest type of d.i.y. receiver to build. It can resolve the single sideband (SSB) voice and Morse (CW) signals which most stations use.

## VIDEO FADE TO WHITE

Video fader projects have appeared in EPE in the past, and these have all provided a conventional fade out to a black screen. This video fader is slightly different in that it provides a fade out to a white screen, or to a preset grey level if preferred. This gives the home video producer a few more creative possibilities from a circuit that is only marginally more complex than an equivalent fade-to-black circuit.

## A BRIEF HISTORY OF GREAT EXPERIMENTERS

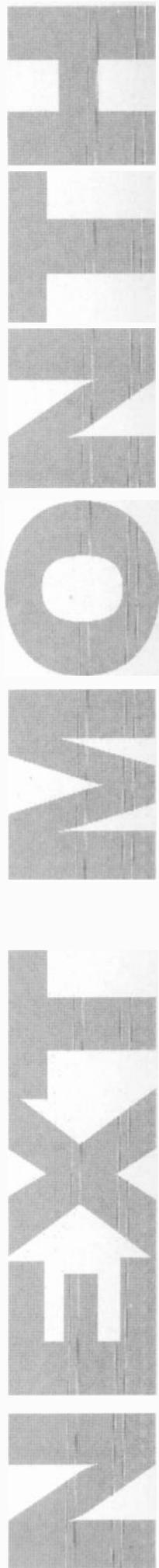
This fascinating series describes the work of the major electrical and magnetic experimenters, the emphasis being on the fact that experimentation was, and is, a necessary requirement for the study of any science. The series covers the work of such famous experimenters as Gilbert, Galvani, Volta, Ampere, Ohm, Faraday etc.

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#### Single-Ended Class "A" Headphone Amplifier

Most modern high fidelity amplifiers either do not have a headphone output facility, or this may not be up to the highest standard.

The new Hart "Chiara" has been introduced as an add-on unit to remedy this situation, and will provide two ultra high quality headphone outlets. This is the first unit in our 2000 Range of modules to be introduced through the year. Housed in the neat, black finished, Hart Minibox it features the wide frequency response, low-distortion and "musicality" that one associates with designs from the renowned John Linsley Hood.

Both outputs will drive any standard high quality headphones with an impedance greater than 30 ohms and the unit is ideal for use with the Sennheiser range. A signal link-through makes it easy to incorporate into your system and two extra outputs, one at output level and one adjusted by the Volume control are available on the back panel. The high level output also makes a very useful long-line driver where remote mounted power amplifiers are used. Power requirements are very simple and can be provided by either of our new "Andante" power supplies. Use the K3565 to drive the "Chiara" on its own, K3550 if driving other modules as well.

Volume and Balance controls are provided and as befits any unit with serious aspirations to quality these are the ultra high quality Alps "Blue Velvet" components.

Very easily built, even by beginners, since all components fit directly on the single printed circuit board and there is no conventional wiring whatsoever. The kit has very detailed instructions, and even comes with a roll of Hart audiograde silver solder. It can also be supplied factory assembled and tested.

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### NEW BOOK

#### "Audio Electronics"

And now, hot off the press, yet another classic from the pen of John Linsley Hood. Following the ongoing enormous success of his "Art of Linear Electronics" the latest offering is the all-new edition of "Audio Electronics", now entirely re-written by the master himself.

Underlying audio techniques and equipment is a world of electronics that determines the quality of sound. For anyone involved in designing, adapting or using digital or analogue audio equipment understanding electronics leads to far greater control over the reproduced sound.

The subjects covered include tape recording, tuners, power output stages, digital audio, test instruments and loudspeaker crossover systems. John's lifetime of experience and personal innovation in this field allow him to apply his gift of being so familiar with his subject that he can write clearly about it and make it both interesting and comprehensible to the reader.

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To fulfil the need for ultra high quality controls we import a special range of precision audio pots in values to cover most quality amplifier applications. All in 2-gang stereo format, with 20mm long 6mm diam. steel shafts, except for the 50K Log which is 25mm x 6mm. Overall size of the manual pot is 27W x 24H x 27Deep, motorised versions are 72.4mm Deep from the mounting face. Mounting bush for both types is 8mm diameter.

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**K1450** Kit, complete with all parts ready to assemble inside the fully finished 228mm x 134mm x 63mm case. Kit includes full, easy to follow, assembly instructions as well as the Hart Guide to PCB Construction, we even throw in enough Hart Audiograde Silver Solder to construct your kit.....£111.58  
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**PAXOLIN PANELS**, size 6" x 6", approximately 1/16" thick, pack of two. Ref: D103.  
**13A SOCKET**, virtually unbreakable, ideal for trailing lead. Ref: D95.

**PIEZO BUZZER** with electronic sounder circuit. 3V to 9V D.C. operated. Ref: D76.

**DITTO** but without internal electronics, pack of two. Ref: D75.  
**LUMINOUS ROCKER SWITCH**, approximately 30mm sq. pack of two. Ref: D64.

**ROTARY SWITCH**, 9-pole 6-way, small size and 1/4" spindle. pack of two. Ref: D54.

**FERRITE RODS**, 7" with coils for Long and Medium waves, pack of two. Ref: D52.

**DITTO** but without the coils, pack of three. Ref: D52.  
**SLIDE SWITCHES, SPDT**, pack of 20. Ref: D50.

**MAINS DP ROTARY SWITCH** with 1/4" control spindle, pack of five. Ref: D49.

**ELECTROLYTIC CAP**, 800µF at 6-4V, pack of 20. Ref: D48.  
**ELECTROLYTIC CAP**, 1000µF + 1000µF 12V, pack of 10. Ref: D47.

**MINI RELAY** with 5V coil, size only 26mm x 19mm x 1mm, has two sets of changeover contacts. Ref: D42.

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**FIGURE-8 MAINS FLEX**, also makes good speaker lead. 15m, Ref: 1014.

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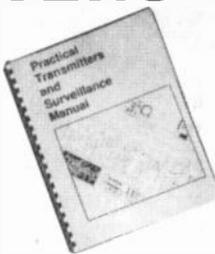
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Current gain = 150  
 Emitter Resistor = 1k  
 Input Impedance = 151k

$$Z_{in} = (150 + 1) \cdot R_e$$

The software is completely self-contained, explanatory text and calculations are laid out in additional Windows, enabling you to see the effect of changing component values, one-at-a-time within the formulae. Graphics, text and calculations can be 'pasted', in colour into text documents for a hard copy reference.

Loaded  $V_{out} = 7.268V$   
 Load = 10k  
 $R2 \parallel Load = 3k19$

$$V_{out} = V_{in} \cdot \frac{R2}{R1 + R2}$$

Effect of connecting a load across R2.

$$V_{out} = V_{in} \cdot \frac{R2 \parallel Load}{R1 + (R2 \parallel Load)}$$

|| means in parallel

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REVIEWED IN AUGUST ISSUE of EPE!

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$V = 50V$   
 $R = 100\Omega$   
 $L = 500mH$   
 $C = 100\mu F$   
 $f = 50Hz$   
 $X_L = 157R1$   
 $X_C = 31R82$   
 $I_R = 500mA$   
 $I_L = 318.3mA$   
 $I_C = 1.571A$   
 $I = 1.6486A$   
 Phase  $\phi = 68.4502^\circ$   
 $Z = 37R06$

$$I_R = \frac{V}{R}$$

$$I_C = \frac{V}{X_C}$$

$$I_L = \frac{V}{X_L}$$

$$\phi = \tan^{-1} \frac{I_C - I_L}{I_R}$$

$$Z = \frac{R + jX_L - jX_C}{\sqrt{X_L^2 + X_C^2 + R^2 - 2X_L \cdot X_C}}$$

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1 of 8 Latches.

\* means don't care.  
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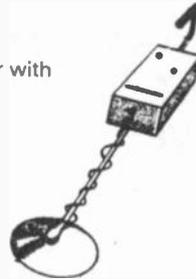
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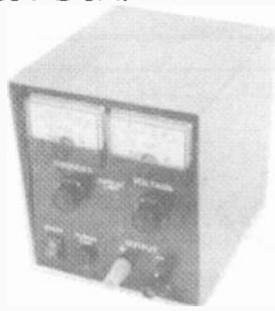
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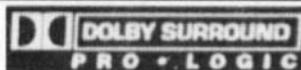
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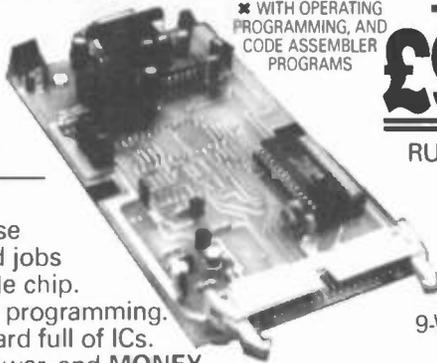
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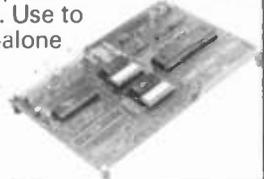
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# EVERYDAY PRACTICAL ELECTRONICS

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## PROJECT DEVELOPMENT . . .

The introduction to our *PIC-Tock Pendulum Clock* project this month gives some insight into how this design came about. With so many projects in each issue and the need to keep coming up with new ideas we always welcome suggestions for unusual projects. Of course we get quite a few sent in "out of the blue", or readers ask us if we have ever published anything for a thingamawoit? Provided we feel these ideas will be of interest to a good proportion of readers then we try to publish something.

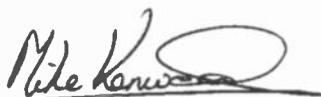
There are, of course, a number of requests that are not achievable for various reasons - for instance it is simply not worth trying to build your own video recorder or worse, camcorder. The cost of the mechanics - even if you could get hold of them - on a one off basis would outweigh the price of a new, guaranteed commercial unit and few readers would have the test gear necessary to test and fault find such an item anyway.

## . . . AND REDEVELOPMENT

Of course, we do rehash ideas from time to time, particularly when we can come up with an improved, more versatile or less expensive design, etc. We are presently working on one or two of these ideas for future issues. One of them is a full specification Theremin. The *Simple Theremin* we published in the September '95 issue has been very popular and Jake Rothman is now finalising the design for a fully specified instrument with pitch and volume control. This has also led to work on an add-on MIDI interface for the instrument. We are sure that both of these projects will be very popular developments of a previous design. We expect to publish the Theremin in the November issue if things go to plan.

We have now published three different Mind Machines from Andy Flind, each one being a major improvement on the previous design. Andy is also now working on an improved TENS Unit (TENS stands for Transcutaneous Electrical Nerve Stimulation) that we hope will be published in the next few months. His previous *Simple TENS Unit* and *Advanced TENS Unit* have been amongst the most popular designs we have ever published and we know from your letters and comments that they have brought relief to hundreds of pain sufferers.

As technology marches on at an ever increasing pace it is possible to improve on old ideas (and to come up with new ones like the PIC-Tock) and we will continue to bring you a wide range of interesting projects.



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# ANALOGUE DELAY AND FLANGER

JOHN CHATWIN

*Simply add the characteristic flanging sound to your guitar effects repertoire.*

IF ANY single effect characterises the sound of the modern electric guitar, it is probably the flanger. Ever since the widespread availability of cheap analogue delay lines, the effect has become realistically pedal sized. It has been taken up by guitar players in all styles, from pop to classical, and is used to enrich the sound of many other electronic instruments.

Anyone who is not sure exactly of the effect that a flanger produces will certainly have heard it used on countless records. It can range from a sort of epic tonal sweep, like phasing, through to a fast bubbling vibrato. A classic flanged guitar sound was used by Andy Summers on the 1980's *Police* records. These days it is a great basic effect, along with "chorus", which is similar, for beefing up guitars and keyboard instruments.

The original flanging effect was produced accidentally – according to the mythology – in some recording studio when an engineer inadvertently put his finger on the flange of a tape deck that was playing back onto another machine. This had the effect of slowing down the tape fractionally until he removed his finger.

When the faulty recording was played back in sync with the original, the slowed down section was, of course, played back at a relatively faster speed. This created an interesting cross modulation effect, which became known as flanging. However, until

"straight" version of the sound to create the effect.

In flanging, the delay required is only very small, no more than 15ms or so, which means that relatively simple analogue delay lines can be used. Generally speaking, analogue delays are now not used much in audio applications for anything over about 50ms because of the noise and distortion they can introduce.

With the short delays needed for flanging, though, they can produce very accept-

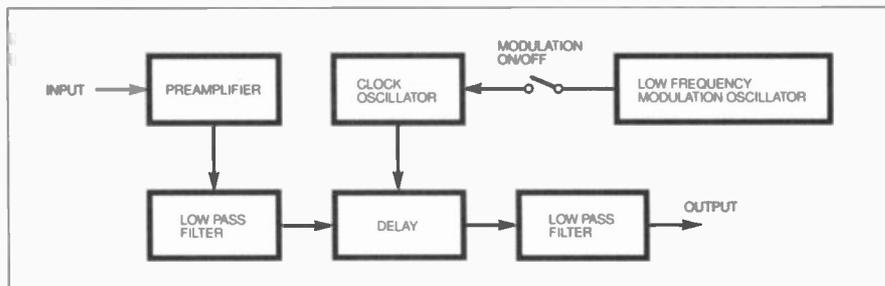
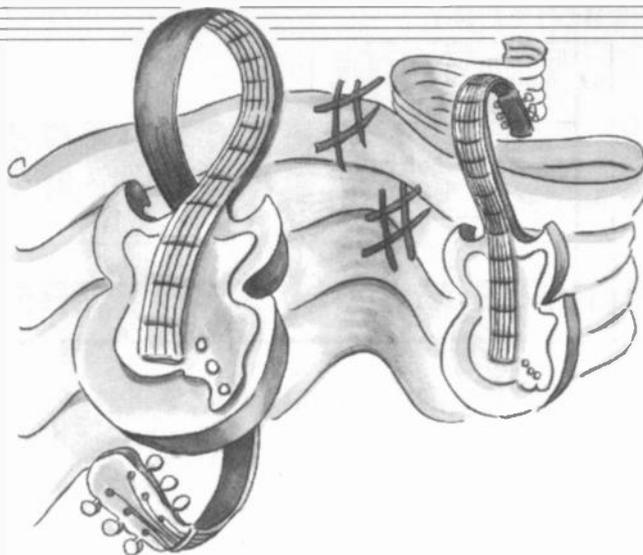


Fig. 2. Block diagram of the Analogue Delay and Flanger.

it could be produced by purely electronic means, its generation was really limited to the recording studio.

Electronic flangers work by slowing down and speeding up signals passing along a delay line. This causes the required de-tuning, which can then be mixed with a

able results. It has to be said, however, that most high quality flangers and chorus pedals now employ digital delay lines, and are correspondingly quieter.

## PASS THE BUCKET

Analogue delay lines operate by using a form of shift register which is driven by a timing circuit or clock. Within the shift register are tiny capacitors which store samples of charge relating to the level of an input signal. The input is fed into the first capacitor and then the charge is progressively shifted from capacitor to capacitor within the i.c. in synchronisation with the clocking signal.

This type of system is sometimes called a "bucket brigade delay" or BBD, because of the way information is passed along it. A typical BBD chip might have around 500 or 1000 stages. In this circuit, the MN3207 delay chip has 1024 stages.

Some analogue delay chips include an on-board clock but the MN3207 has a partner chip, the MN3102, which provides the clock signal and the gate supply voltage required by the MN3207. As can

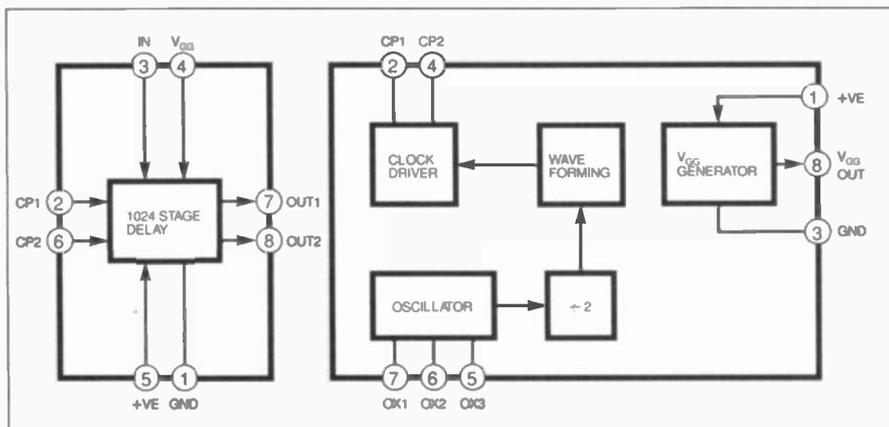


Fig. 1. Functional block diagram for the MN3207 delay line (left) and MN3102 clock generator devices.

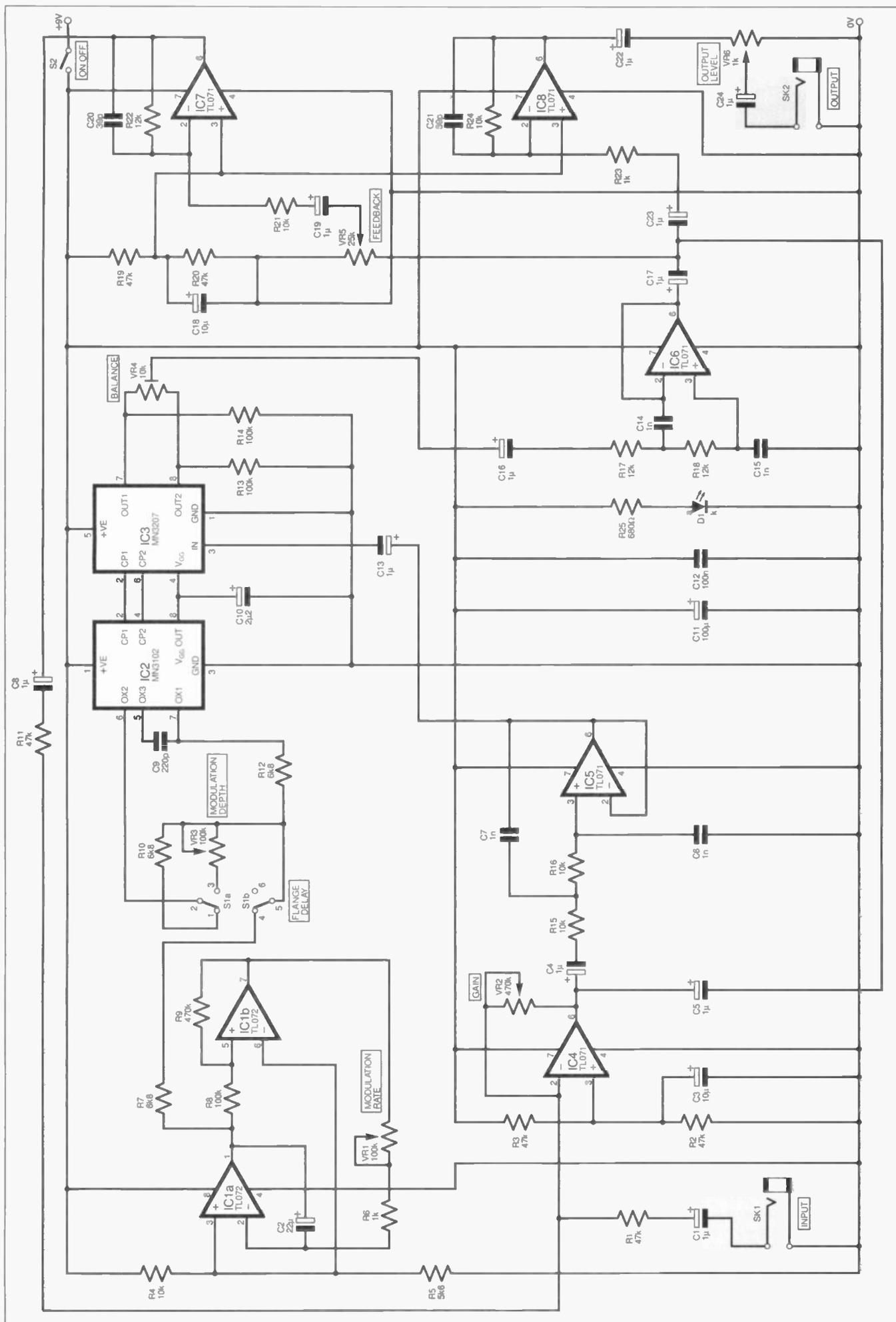
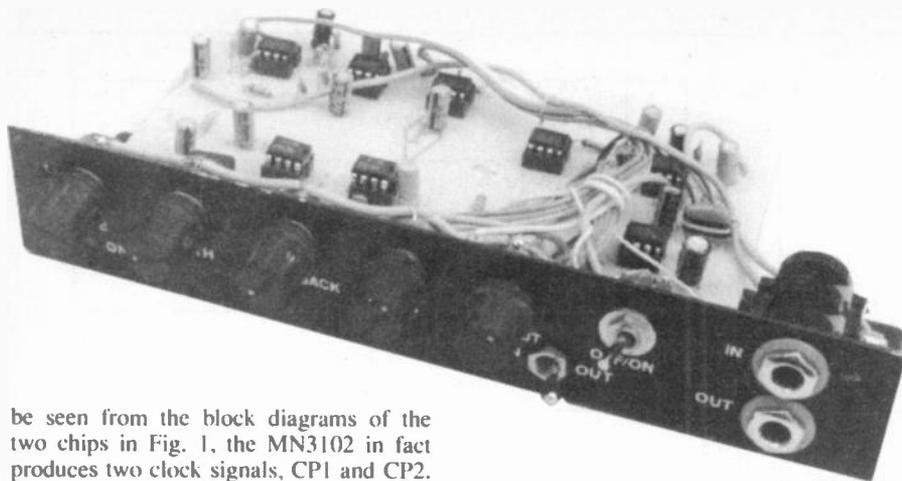


Fig. 3. Complete circuit diagram for the Analogue Delay and Flanger.



be seen from the block diagrams of the two chips in Fig. 1, the MN3102 in fact produces two clock signals, CP1 and CP2. These operate at half the frequency of the master oscillator, and are out of phase with one another.

The frequency at which the clock runs determines the delay time and, to some extent, the quality of the output signal, as it also controls the rate at which the input signal is sampled and passed along the register. The MN3102 will operate at a rate anywhere between 10kHz and 100kHz, which provides an audio signal delay of 2.56ms to 25.6ms with the MN3207. It also allows for the clock frequency to be varied according to an external modulation signal.

## BLOCK DIAGRAM

It can be seen from the block diagram in Fig. 2 that the Flanger/Delay unit consists of six main parts: input preamp, input filter, delay, clock oscillator, low frequency modulation oscillator and an output filter.

The circuit diagram for the complete unit is shown in Fig. 3. Signals enter the circuit via the d.c. blocking capacitor C1 and are passed to the low noise inverting amplifier IC4.

The gain of this stage is controlled by the potentiometer VR2. In essence, this allows the circuit to be matched to a variety of input signal levels from various sources, such as guitars, keyboards or microphones. The unit could also be incorporated into a public address (PA) system or guitar amplifier effects loop.

From IC4 output pin 6, signals are fed into a two-pole 15kHz active low pass filter, based around IC5. The filter is required to remove any high frequency signals before they get to the delay line, as it would be unable to process them correctly, and they would tend to increase levels of noise and distortion.

From IC5, signals enter the delay line IC3, the MN3207 BBD chip. The MN3102 clock generator is IC2. The two clock signals from IC2 pins 2 and 4 are connected directly to IC5 pins 2 and 6, respectively. The  $V_{gg}$  gate supply voltage from IC2 pin 8 to IC3 pin 4 is decoupled by capacitor C10.

The basic clock frequency of IC2 is set by capacitor C9 between pins 5 and 7, and the resistance between pins 6 and 7. In this circuit, the timing capacitor is 220pF, but for other applications its value could range from around 39pF to 240pF.

Between them, op.amps IC1a and IC1b form the low frequency modulation oscillator (LFO) which produces a triangle wave output at a frequency controlled by potentiometer VR1 and capacitor C2. With

the component values shown, VR1 enables the frequency to be varied from around 0.3Hz to about 4Hz, which gives a good usable range of fast and slow flanging.

The output from the LFO is channelled through resistor R7 to the selector switch S1. This switch allows you to use the LFO to modulate the clock frequency produced by the MN3102 – to automatically create the flanging effect – or to manually change the delay rate using VR3, thus creating an echo effect. With the switch in the modulation position, VR3 is disconnected, and the modulation voltage is applied through the potential divider formed by resistors R12 and R10.

If you do not require the echo effect option and just want to use the circuit as a flanger, the LFO can be connected as shown in Fig 4. This avoids the need for switch S1 and potentiometer VR3.

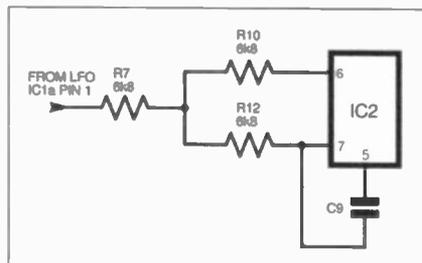


Fig. 4. Connecting the LFO without modulation switch S1.

The output from the delay line is via IC3 pins 7 and 8. Potentiometer VR4 provides a mid-point, and can be adjusted to give the best response. Correct balance of the two signals being summed at VR4 may not be a problem unless you use the clock at very low speeds. From the wiper of VR4 the signal is passed to IC6, which is another low pass filter. This removes the high frequency clock noise that is superimposed on the audio signal by the delay circuitry.

From IC6, the processed signal is sent to IC8, which is wired as a low gain (about  $\times 10$ ) buffer. Via capacitor C5, an unprocessed version of the audio signal from the output of the first preamp, IC4, is also fed to IC8. From IC8 the combined signal is then sent through the level control potentiometer VR6 to the output socket SK2.

Potentiometer VR5, connected to the combined signals from IC4 and IC6, is the control that sets the amount of signal routed back to the input of IC4. VR5 can be used to maximise the resonant qualities of the flanging effect, as it allows the circuit to be operated close to maximum

feedback level. In the delay mode, VR5 allows the creation of repeat echoes.

## POWER SUPPLY

Power for the circuit can be provided by a 9V supply, such as a PP3 battery. The actual voltage is not critical and the circuit will probably work with voltages from around 6V to 15V. The power supply lines are decoupled by capacitors C11 and C12. Light emitting diode (l.e.d.) D1 provides power-on indication, with its current limited by resistor R25.

The centre rail voltage for the non-inverting input of IC4 is provided by resistors R2 and R3. IC7 and IC8 share a mid-rail voltage provided by R19 and R20.

## CONSTRUCTION

Component layout and tracking details of the printed circuit board are shown in Fig. 5. This board is available from the EPE PCB Service, code 111.

## COMPONENTS

### Resistors

R1 to R3, R11,	
R19, R20	47k
R4, R15, R16,	
R21, R24	10k
R5	5k6
R6, R23	1k
R7, R10, R12	6k8
R8, R13, R14	100k
R9	470k
R17, R18, R22	12k
R25	680 $\Omega$

All 0.25W 5% carbon film or better.

### Potentiometers

VR1, VR3	100k rotary carbon lin. (2 off) (see text)
VR2	470k rotary carbon lin.
VR4	10k preset, horiz.
VR5	25k rotary carbon log.
VR6	1k rotary carbon log.

### Capacitors

C1, C4, C5,	
C8, C13, C16,	
C17, C19,	
C22 to C24	1 $\mu$ elect. radial, 16V (11 off)
C2	22 $\mu$ elect. radial, 16V
C3, C18	10 $\mu$ elect. radial, 16V (2 off)
C6, C7,	
C14, C15	1n ceramic disc (4 off)
C9	220p ceramic disc
C10	2 $\mu$ 2 elect. radial, 16V
C11	100 $\mu$ elect. radial, 16V
C12	100n polyester
C20, C21	39p ceramic disc (2 off)

### Semiconductors

IC1	TL072
IC2	MN3102
IC3	MN3207
IC4 to IC8	TL071 (5 off)
D1	red l.e.d. and clip

### Miscellaneous

S1	d.p.d.t. min. toggle switch (see text)
S2	s.p.s.t. min. toggle switch
SK1, SK2	standard mono jack socket, 0.25in (2 off)

Printed circuit board, available from the EPE PCB Service, code 111; 8-pin d.i.l. socket (7 off); knob (5 off); connecting wire; solder, etc.

Approx Cost  
Guidance Only

£28

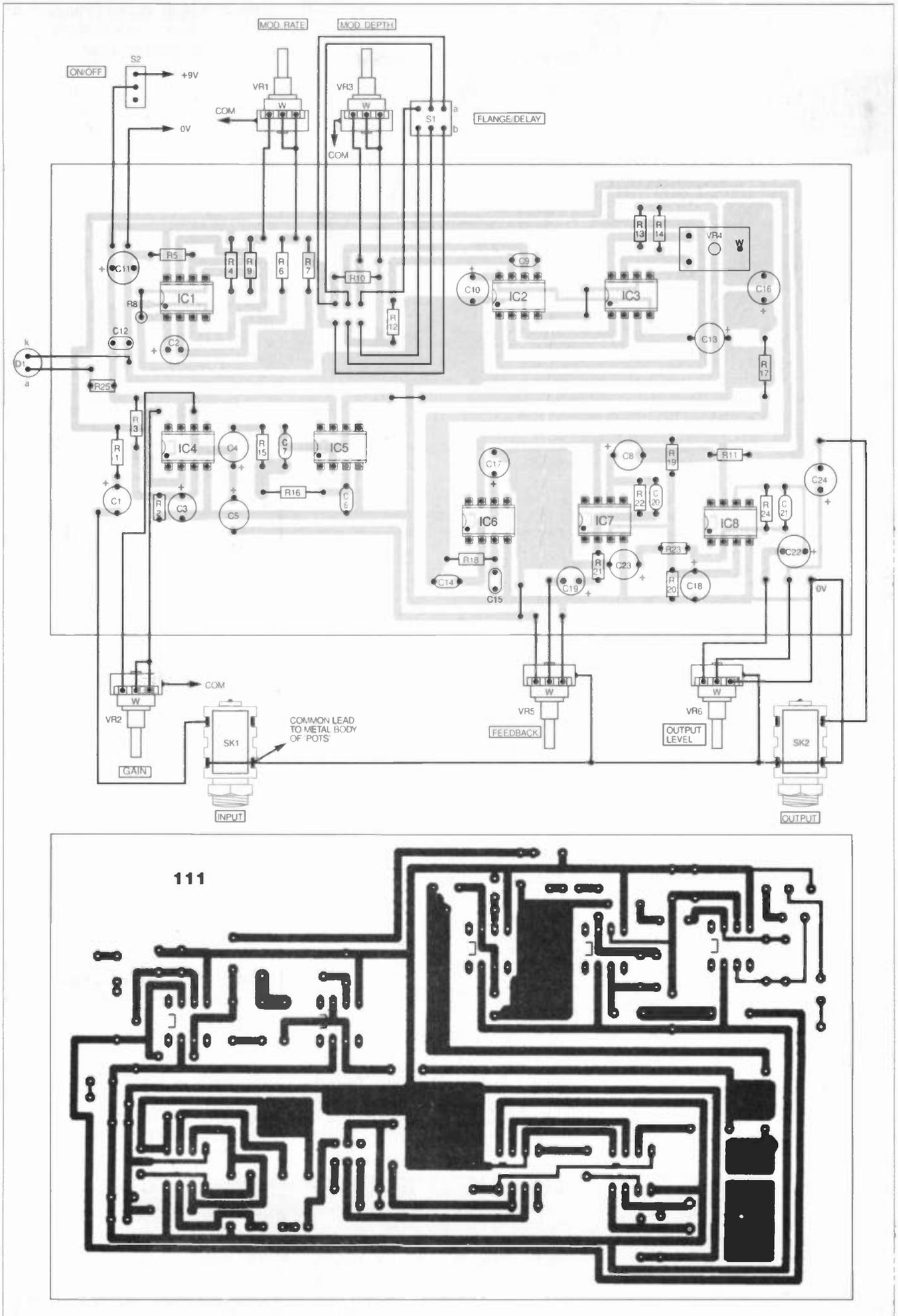
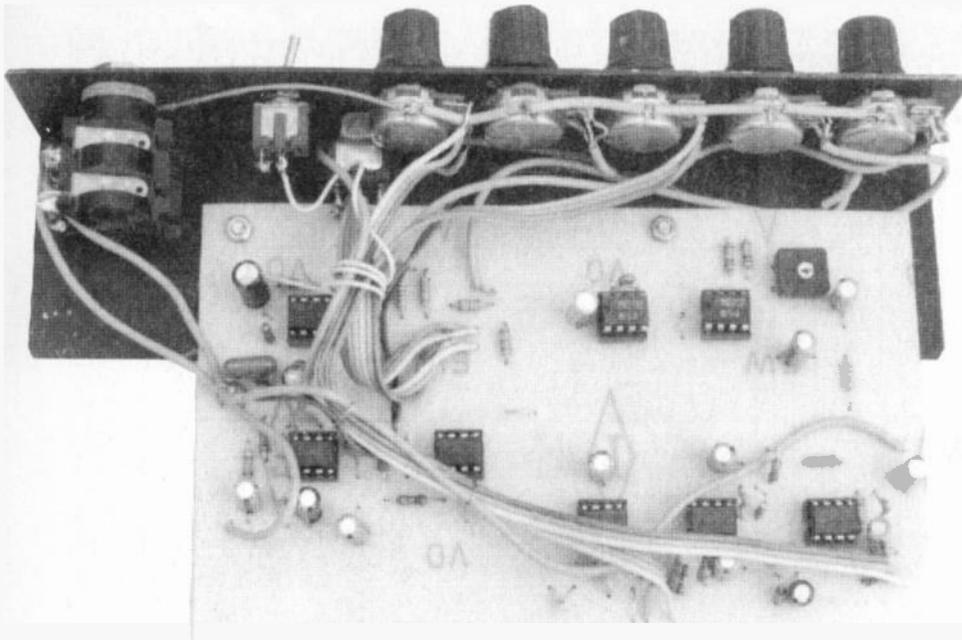


Fig. 5. Details of the printed circuit board component layout and wiring, plus full-size underside copper foil master track pattern. *Everyday Practical Electronics, September 1996*



The additional wiring to the potentiometer bodies ensures satisfactory screening by connecting them to the 0V point on the jack socket.

Assembly of the p.c.b. should be quite straightforward as the components are well spaced out. Take the usual precautions against heat damage, and solder the resistors and wire links in first. Check the polarity of the polarised components, and use sockets for all the i.c.s. The i.c.s. should not be inserted until after all the other construction has been completed.

Connections to the potentiometers can be made with thin multi-strand wire. Do not use solid-core wire as it will tend to break at connection points if it is moved about too much during assembly. All connections to the p.c.b. should be as short as possible to minimise noise pick-up. However, as long as you use an earthed metal case, noise should not be too much of a problem.

## SETTING-UP

Setting up the unit is very simple. Plug a guitar into the input, and take the output to a normal guitar amplifier.

Completely turn down the volume controls on the amplifier, and the level and feedback controls on the flanger. Connect a PP3 battery to the circuit, switch on S2 and check that the l.e.d. comes on. Turn up the volume on the amplifier slightly, then bring up the output level control on the Flanger and listen for a slight background hiss. This will usually indicate that the unit is working.

If you cannot hear anything unusual (like the sound of chips expiring!), turn up the input level and check that a signal on the input turns up at the output. With

## BY-PASS SWITCH

If the Flanger is going to be used as a musical effects unit, you will need a way of turning it on and off without having to disconnect the power, which can cause horrendous noise spikes unless you disconnect the output first. This can be a bit impractical!

The standard way of arranging an effects by-pass switch is shown in Fig. 6. This method disconnects both the input and output of the active circuit when the by-pass switch is operated, which eliminates switching noise.

The circuit also incorporates a stereo input jack socket wired as an overall power on/off switch. Again, this is common practice in manufactured effects pedals, and does away with the need for a power switch. When a normal mono guitar or instrument lead is plugged into the input socket, the earth sleeve shorts across the first two connections and connects the negative terminal of the battery to the negative supply rail.

The only drawback with this arrangement is that you must remember to pull out the input lead if the unit is not going

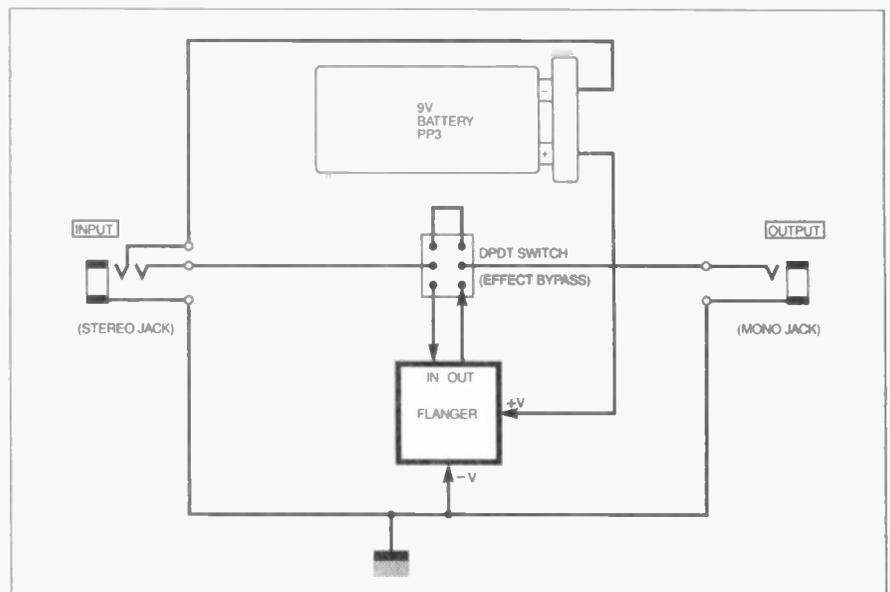


Fig. 6. How to wire the unit to a by-pass switch.

switch S1 set for Delay, you should hear short echo effects, with VR3 controlling the length of the delay. In this mode, VR1 has no effect.

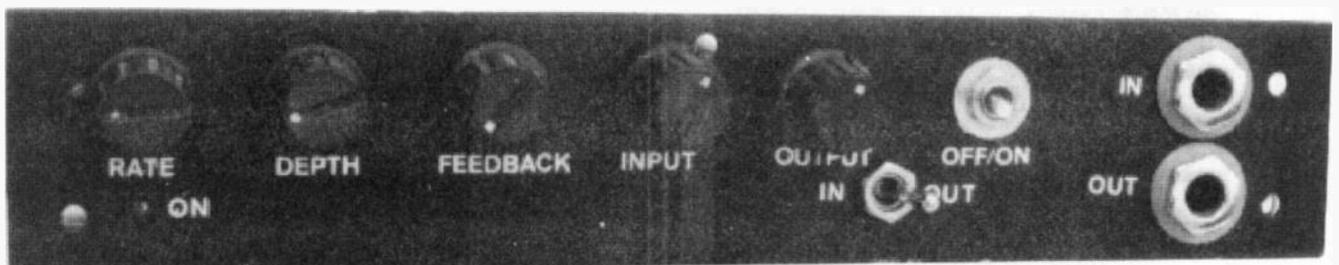
With switch S1 set to Flanging, the flanging rate can be controlled by VR1, but with VR3 having no effect.

Use the input level, output level and feedback controls to get the best effect. If there is a background whining from the clock circuit, try adjusting the preset VR4 to balance it out, though it may still be just audible if the unit is used with a very sensitive amplifier.

to be used for a while, otherwise the battery will run down.

## CASING THE UNIT

Assuming that all is well, the unit can be mounted in a case. The prototype unit was actually mounted in a large case which also houses other effects units. A metal case is recommended so that the circuit will be well screened. If you must use a plastic case, try screening the inside with tin foil, but remember that unless the case or screen is connected to earth, it may make noise levels worse.



**Is your PCB design package not quite as "professional" as you thought? Substantial trade-in discounts still available.**

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## BoardMaker

*BoardMaker1 - Entry level*

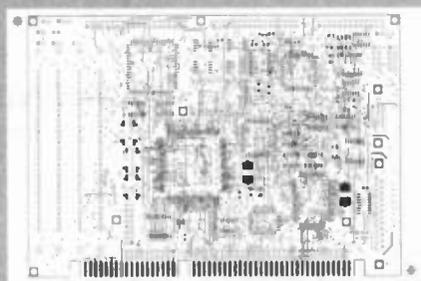
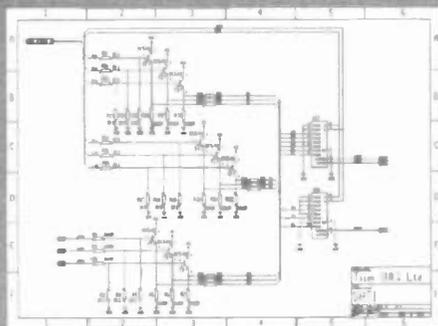
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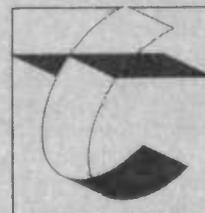
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## MORE SPENDING ON BRITISH INNOVATIONS

CBI reports good prospects for sensors and electronic tagging  
— by Hazel Cavendish

**B** RITISH companies spent more on innovation in the last two years than in the previous five, according to an Innovation Trends Survey run by the CBI and the NatWest Innovation and Growth Unit. 487 manufacturers and 200 non-manufacturers took part in the survey.

Manufacturers spent 6.2 per cent of their turnover on innovation last year, while non-manufacturers reported 10.6 per cent, in both cases showing a marginal drop from record 1994 figures but showing a healthy increase in the opening years of the decade. Most encouraging was the increase in collaboration between manufacturing and academics shown by an analysis of the Government's *Technology Foresight* programme.

### Patents Falling

A more disappointing statistic to emerge from the survey was the significant fall in the number of manufacturers committed to patenting. This fell from 77 per cent in 1994 to 62 per cent last year and was echoed by a 10 per cent drop for non-manufacturers.

John McClelland of IBM, who took part in the Foresight exercise, had previously drawn attention to the small number of American patents registered by the UK since 1980, pointing out that this was an indication of just how badly Britain lagged because Government and Industry were spending too little on research.

He warned that, in modern industry, it is "patent or perish". Budgets had been trimmed to an unacceptable level when it took five million dollars of research to come up with one patentable notion.

Another Foresight panel urged that the amount of R&D devoted to telecommunications and information technology should be substan-

tially increased, and the Computers panel called for greater investment in "leading-edge technologies".

As a result of the survey's sector reports, the Department of Trade and Industry is putting £36m into supporting research in six fields with long-range market opportunity and scientific potential. Two of these fields are sensor and automation technology, and communications and computers.

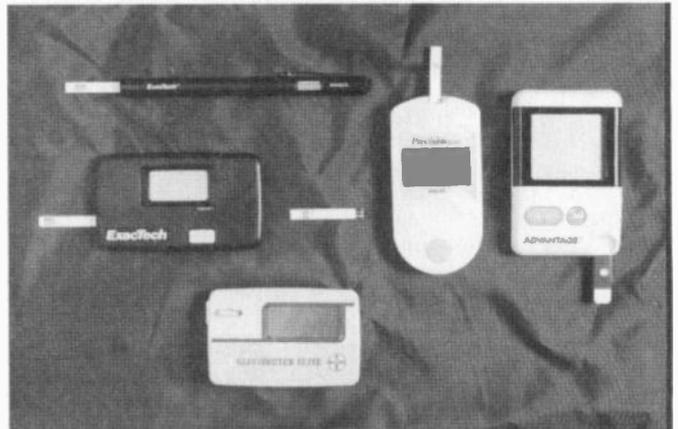
### Cranfield's Sensor Success

Cranfield University, which celebrates its fiftieth anniversary this year, was chosen in the '80s for a Leverhulme Trust-sponsored chair in biotechnology - the engineering of medicine - because of its excellent links with industry.

Subsequently, their Biotechnology Centre has developed sensors which detect bacteria in water, including the detection of waterborne diseases such as Legionella, and a fermentation monitor which is able to measure the growth of micro-organisms in foods such as yoghurt, bread and beer, enabling improved control of fermentation processes.

Professor Tony Turner, head of the Biotechnology Centre, says bio-sensors have a great future in health care with their ability to both detect and monitor illnesses in the early stages.

He believes tiny sensors could be used in private homes, connected to personal computers, able to throw up medical conditions which can then be reported to the



Biosensors for home blood-glucose measurement. None are of British manufacture, even though they could have been.

patient's doctor. This will greatly reduce the doctor's load in making patients' visits necessary only when the sensor shows that something is wrong.

"In health care in future we will be looked after in our homes, secure in the power of complete diagnostic systems and continuous monitoring, all based on our computers", he says, adding that recent research with sensors has shown that improved monitoring can

greatly reduce the complications of diabetes.

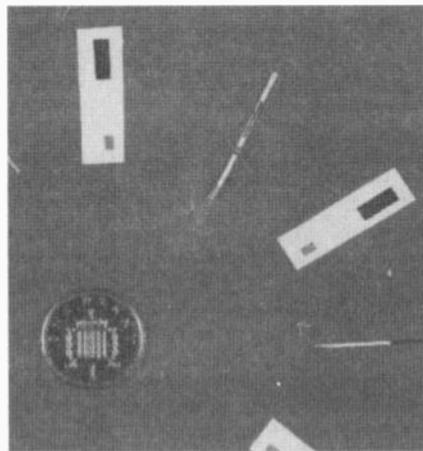
His Centre's development of sensor technologies is the basis of all three of the best-selling devices used by diabetics to measure blood sugar levels before meals, but he is disappointed that British industry's failure to follow up on his department's research has resulted in three foreign market leaders making millions of dollars annually, based on a Cranfield sensor. The sensors shown in the photograph above originated from the USA and Japan.

### Tagging Growth

Electronic tagging is another growth area of considerable potential. This has many applications in addition to the familiar plastic rectangles attached to merchandise in stores which sound off a daunting alarm when we thoughtlessly pluck a garment from a rail for personal inspection.

St James's University Hospital in Leeds introduced baby-tagging following the abduction of Abbie Humphries from the Queen's Medical Centre in Nottingham in 1994.

Unfortunately this development has been beset by



Prototype printed biosensors produced at Cranfield University for lactate measurement. Lactate measured in vivo or in vitro gives an indication of fitness in, for example, human athletes or race horses.

problems caused by interference from other equipment, or because the tagging devices were originally designed for different environments.

St James's actually abandoned the experiment and reverted to other security measures, but Queen Charlotte's Hospital in London and Edinburgh Royal Infirmary's Simpson Memorial Maternity Pavilion have expended much time and effort to fault-proof their systems. Hospitals have so much electrical machinery that innumerable things can set off the alarms, including vacuum cleaners and television sets.

Now a real opportunity for electronic tagging companies has come up as a result of the BSE problem. Europe requires a tagging system for cattle, and a National Cattle Database Working Group is considering the matter while several British electronic companies are working feverishly to produce the answer, said to be worth £42 million annually to the company that can deliver the goods with the minimum delay.

It is to be hoped that for once Britain will win this lucrative prize ahead of Europe and the Far East.

## PRECISION CAPPING

THOSE needing to accurately measure capacitance values should consider the latest digital capacitance meter from Seme Ltd. The DKM190 is capable of measuring capacitors in range from 1pF to 20,000µF with an accuracy of 0.5%.

The instrument is operated from a 9V battery, with a running time of approximately 200 hours (depending on the type of battery used). If the power falls below the operating voltage, the low voltage warning symbol is displayed.

With its wide capacitance measuring range, this instrument can be employed in all fields of electrical and electronic engineering, particularly in radio and television design and repair workshops.

The meter is supplied with a carry bag, test leads, battery and instruction manual, at a price of £73.

For further information, contact Seme Ltd., Dept. EPE, Unit 2, Saxby Road Industrial Estate, Melton Mowbray, Leics LE13 1BS. Tel: 01664 65392.



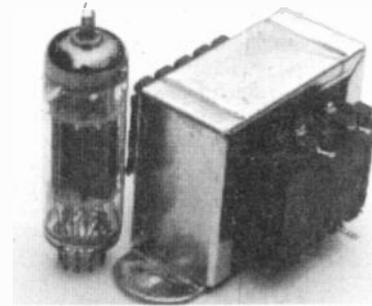
## Valve Transformers

A RANGE of transformers specially designed to meet the needs of the resurgent valve market has just been launched by Variable Voltage Technology Ltd. Aimed at the electronics and amateur radio enthusiast, the new VTM range is manufactured to traditional requirements, but using modern methods and materials, including high grade annealed copper wire and high quality grain-orientated laminations.

The VTM transformers have been designed to give a low flux density to ensure reduced external magnetic fields. They meet the requirements of EMC (electromagnetic compatibility) and low voltage directives.

Frame or vertical mounting types can be specified and are available for the following applications: mains transformers for HT circuits with or without filament windings; filament transformers; mains smoothing chokes; output transformers; grid coupling transformers.

As a specialist transformer design and manufacturing company, VVT can customise its standard range of transformers to meet non-standard requirements. For more information, contact Variable Voltage Technology Ltd., Dept. EPE, Unit 24, Samuel Whites Estate, Medina Road, Cowes, Isle of Wight, PO31 7LP. Tel: 01983 280592.



## Your Flexible Friend

P.I.D.A., the Professional Instrument Distributors Association, has advised us that a new flexible a.c. current probe has been introduced. The probe is ideal for irregular shaped conductors with difficult access.

Compatible with any digital multimeter, chart recorder or oscilloscope, LEM-flex is claimed to be the most versatile measuring device of its type, providing wrap-around flexibility with two standard current ranges to each unit.

Compact, light and portable, it has the added benefits of a wide bandwidth, one per cent accuracy, electrical isolation and rugged durability.

Standard models from P.I.D.A. are available in lengths of 61cm, 91cm and 122cm, with dual ranges of 30A/300A, 300A/3000A and 600A/6000A.

For further information, contact P.I.D.A., Dept. EPE, 3 Brackenley Court, Embsay, N. Yorks BD23 6PX. Tel: 01756 799737.

## SCHOOLS ONLINE

The "Schools Online" project – a pilot study to promote structured education via the Internet – will be expanded from 60 to over 200 participating schools with an extra £450,000 funding from the DTI if teachers and sponsoring companies want it to go ahead. Science and Technology Minister Ian Taylor has recently announced.

Phase two will aim to further develop the Internet skills of teachers and students, provide accreditation for participating teachers, produce best practice case studies for UK-wide distribution, continue mentor support from sponsors, and disseminate the lessons to all schools in the UK.

Initial evaluation shows that the DTI's project has been a "significant contribution to understanding the information super-highway".

Speaking at the "Schools Online" conference in Birmingham, Ian Taylor said: "Information and communications technology have the potential to make a massive contribution to how our children learn and equip themselves for life and work in the next century."

"The key has been the development of software to

support better use of the Internet in schools' teaching. Schools can now go on-line via the standard telephone, but higher capacity connections are now being marketed to schools."

Further information is available from Tom King, Schools Online Project Manager, tel: 01924 378111.

## REVEILLEZ!

French car makers, Renault, are developing a device which will wake drivers up if they are nodding off behind the wheel. A small infra-red camera system continually monitors the driver's eyelids and measures how long they are closed. If they stay shut too long an alarm sounds.

Drowsiness is said to be the second commonest cause of accidents involving heavy lorries and coaches in France. Renault feels that its system can help prevent a significant number of accidents. The majority of drivers asked are in favour of the concept.

The system will be operational on an experimental basis early in 1997 and is likely to be adapted for cars as well.



## KEELOQ CODE HOPPER

Microchip has added a further product to its family of KEELOQ code hopping devices. Keeloq devices provide rock-solid security in remote keyless-entry systems using r.f., infrared or microwave transmissions.

The new HCS200 operates over a voltage range of 3.5V to 13V and has three button inputs providing up to seven functions. Using a complex non-linear algorithm that combines a programmable 28-bit serial number with a 64-bit encryption key, the device generates a 32-bit hopping code that changes with each successive transmission and eliminates the possibility of unauthorised access.

Simultaneously announced is the *Silicon Solutions for Security* guide which provides technical solutions for a range of security applications, including remote keyless entry, alarm and access control, smart cards and personal communications products. The guide offers designers a valuable head start that can significantly reduce development time and cost.

For more information, contact Arizona Microchip Technology Ltd., Dept. EPE, Unit 6, The Courtyard, Meadowbank, Furlong Road, Bourne End, Bucks SL8 5AJ. Tel: 01628 851077.

## TIME-BOMB 2000

*Innovations in EPE* August 1996 briefly reported on the potential problems for business computer systems which may crash with the "00" of the millennium date change.

A recently received press release from the Department of Trade and Industry (DTI) confirms that the pending problem is real and not just a media story befitting April 1st or the Summer Silly Season.

Apparently, the UK has taken the initiative over the millennium date change within Europe. The Minister for Science and Technology, Ian Taylor, says that he has "asked senior representatives of interested parties in industry and the Bank of England to discuss remedial action with me and encouraged the Computing Software and Services Association to set up a task force to examine the action that can be taken in conjunction with users.

"Government departments have also been asked to draw up an action plan to show how they will deal with the problem internally and to assess how much of a problem there might be for any industrial sectors they sponsor. Within the DTI the Information Society Initiative will provide advice for companies.

"If the time-bomb is to be stopped from exploding we all need to start planning now", he added.

The DTI advise that the Computer Services and Suppliers Association has available a directory of organisations providing specialist Millennium skills and products. To obtain the directory contact: Nicki Blinkhorn at CSSA on 0171 405 2171. Alternatively, the directory is available on the CSSA's WWW site at: <http://www.cssa.co.uk/cssa/new/Mmillen.htm>.

## Soldering On

Vann Draper Electronics are introducing what they describe as "an extremely competitive range" of soldering stations. The range initially comprises three models, the SL20, SL30 and SL916, priced at £59, £69 and £349, respectively.

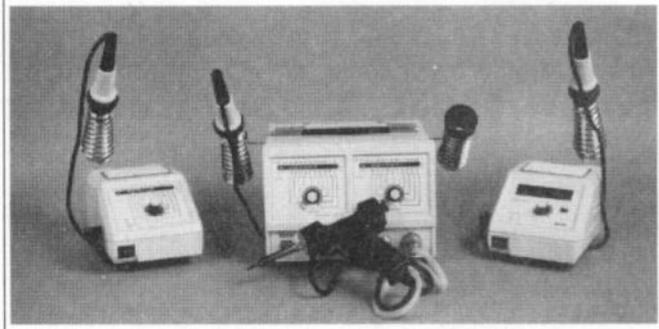
The SL20 is an electronic temperature controlled soldering station with a plug-in 24W soldering pencil. Temperature is fully adjustable between 150°C to 420°C with a 12-l.e.d. bargraph indication for actual temperature and heat-on mode.

The SL30 provide similar facilities to the SL20 except with a higher temperature range of 160°C to 480°C and a digital readout of both the preset and actual temperature.

The SL916 is a combined soldering and desoldering station with independent temperature control of both the soldering iron and desoldering gun allowing simultaneous use of both.

Whilst the SL916 is probably best suited to professional electronics users, the SL20 and SL30 should be considered as possible additions to the workshop of any serious electronics hobbyist.

For more information, contact Vann Draper Electronics Ltd., Dept. EPE, Unit 5, Premier Works, Canal Street, South Wigston, Leics LE18 2PL. Tel: 0116 277 1400.



## Catalogues Abound

We have received the latest catalogues from *Alpha*, *Mauritron* and *Rapid* all of which are worth adding to your library.

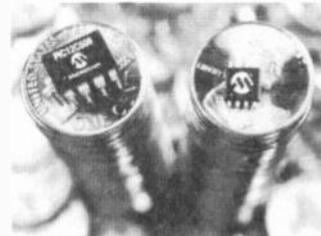
Alpha Electronics (Southern) Ltd. have a good range of electrical and electronics test and measuring equipment. They are members of the PIDA (Professional Instrument Distributors Association) and are based at Dept EPE, Unit 16, Wren Industrial Estate, Coldred Road, Parkwood, Kent, ME15 9XN. Tel: 01622 690187.

Mauritron Technical Services, as we are sure you are well aware, have an enormous range of service manuals and technical books, available for most equipment, of any make, age or model, most of which are also available on CD-ROM. Mauritron are at 8 Cherry Tree Road, Chinnor, Oxon OX9 4QY. Tel: 01844 351694.

Rapid Electronics' 400+ page catalogue offers an enormous range of electronic products, right

across the spectrum, including passives, actives, electro-mechanicals etc. It is another major catalogue which ought to be on your shelves. There is a £3 charge for it, but it's well worth it. Write to Rapid at Dept EPE, Heckworth Close, Severalls Industrial Estate, Colchester, Essex CO4 4TB. Tel: 01206 751166.

A fourth catalogue received is from a company whose products were previously unknown to us - Hogg Laboratory Supplies. It does not have a lot directly to do with hobbyist electronics, but is nonetheless likely to be of interest to all you broadly-inventive experimenters. Amongst the subjects covered are general laboratory apparatus, chemicals, microscopes, anatomical models, biology, environmental science etc. For more information, write to Hogg Laboratory Supplies Ltd., Dept EPE, Sloane Street, Birmingham B1 3BW. Tel: 0121 233 1972.



## 8-PIN PICS

More news from Microchip highlights their introduction of the world's first 8-pin microcontrollers.

The new PIC12Cxxx 4-bit one-time-programmable (OTP) microcontrollers pack Microchip's powerful RISC-based PIC16/17 architecture into an 8-pin package. As well as offering mathematical and Boolean performance not available on most 4-bit microcontrollers, the low pin count of the new OTP family makes it extremely cost-effective and flexible.

The first two family members, the PIC12C508 and PIC12C509, feature 512 words of program memory with 25 bytes of user RAM, and 1024 words of program memory with 41 bytes of user RAM, respectively.

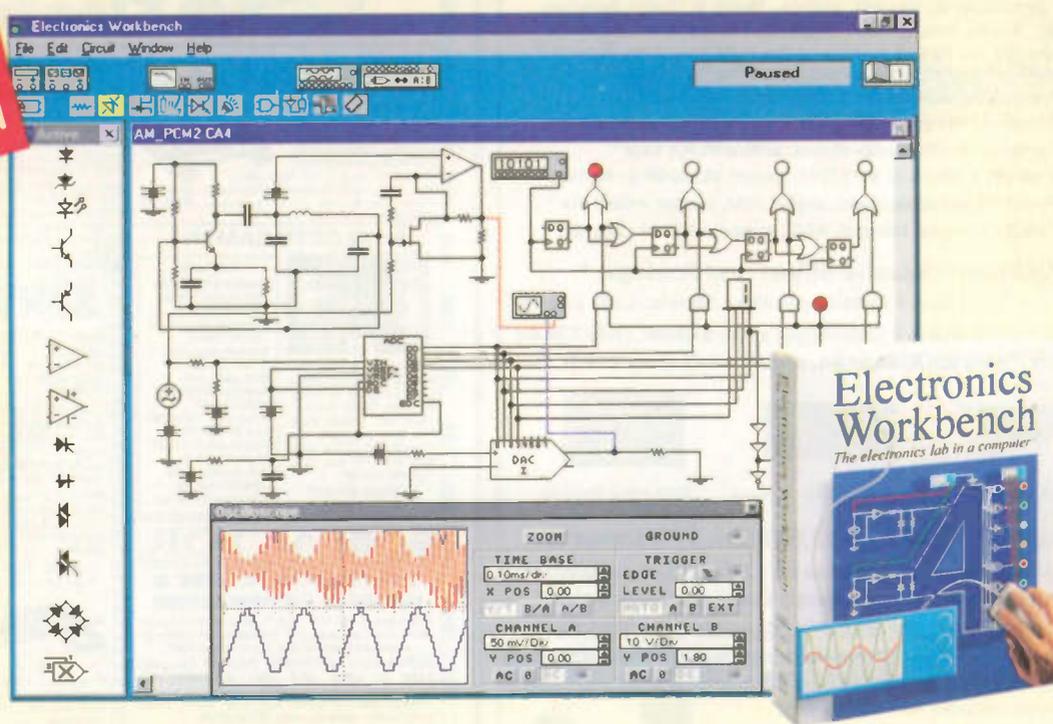
Both devices provide six I/O with on-chip oscillator, 33 single-word instructions, full-speed 1µs instruction cycle at 4MHz. There are seven special function hardware registers, 2-level deep hardware stack, 8-bit real-time clock/counter with 8-bit programmable prescaler, watchdog timer, direct i.e.d. drive, low 2.5V-5.5V operating voltage and less than 2mA power consumption at 5V/4MHz.

In other words, these are astonishingly powerful little chips. It's a shame, though, that they are not also available in EEPROM versions allowing in-circuit development of control software.

For more information, contact Arizona Microchip Technology Ltd., Dept EPE, Unit 6, The Courtyard, Meadowbank, Furlong Road, Bourne End, Bucks SL8 5AJ. Tel: 01628 851077.

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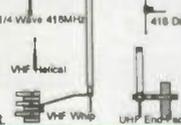


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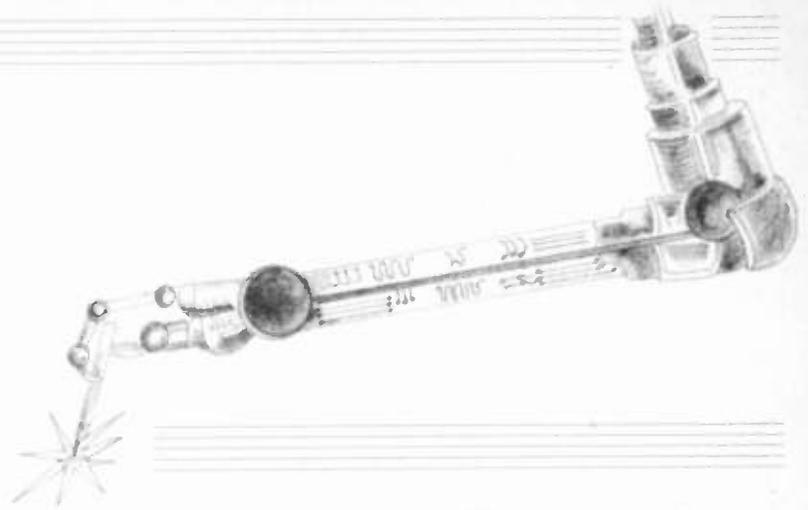
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# CIRCUIT SURGERY

ALAN WINSTANLEY



Our monthly "Surgeon" gives some sound advice on handling lead-acid batteries, helps out with a boat owner's electrical woes, offers more on the chemistry of NiCad charging, and warns about over-hot batteries.

I feel a "battery special" coming up this month, so let's dip our toes into the briny with a question from Mr. Oliver Lazarus of Oxford, who asks:

Help! I'm moving into a boat where all electricity will be supplied by two 12V lorry batteries, powered by a petrol generator, with the help of a wind generator, too. My experiences so far of using 12V appliances on these batteries have been both smelly and expensive!

Could you give me some tips and advice so that I can safely live a life afloat, in one piece? Also, how do I connect lower voltage units to a 12V battery? With a transformer for instance? Thanks!

Connecting to a 12V lorry lead-acid battery poses many hazards. Obviously there is the immediate risk of accidentally reverse-connecting the load, this may damage an unprotected unit beyond repair (as I think you found out with your stereo).

There is massive capacity within a 12V car or lorry lead-acid battery to provide enormous currents (many hundreds of amps, instantaneously) and it is potentially quite easy to burn out any wiring, causing an electrical fire if the battery was wrongly connected. How well the appliance would withstand a reverse supply, depends on what protection it includes, if any. In-line fuse protection is a good idea, and the fuse should be connected as close as possible to the battery's +12V terminal so that the full length of wire is protected.

## Explosive

Lead acid batteries (if not of the "sealed gel" type) may emit hydrogen gas which will become explosive when mixed with air. If you cause a spark near the battery's cells, then in extreme circumstances a battery explosion could result, causing serious personal injuries. (Have I put you off setting sail, yet? Sorry.)

Sparks may be caused by twiddling with the battery terminal connections when a load is already connected to the battery. It is safest to switch off all (heavy) loads, cover the battery with a damp cloth, and ensure good ventilation, when adjusting it for any reason.

Burns may also be caused by wearing a metal watch strap, for example, or using a spanner or screwdriver blade carelessly.

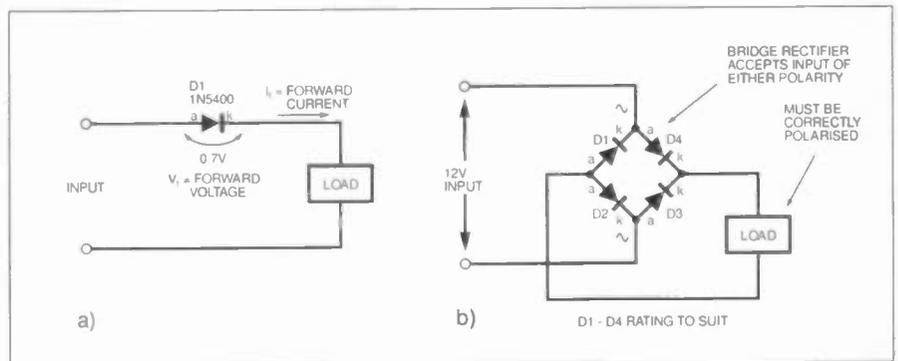


Fig. 1. Reverse polarity protection.

This may accidentally cause a short circuit through the metal, causing serious wrist burns as 200-300 amperes flow merrily through.

A rectifier, if added inside the appliance, will guarantee that no current will flow if the supply is connected the wrong way round, see Fig. 1a. The rectifier should have a "forward current rating" (symbol,  $I_f$ ) to enable it to cope with the current which will be drawn under normal operation. You will lose about 0.7V across the rectifier but this shouldn't matter.

You could also consider a resettable thermal trip which acts like a fuse, but

pressing a button resets it again. Maybe use one thermal trip a few inches away from your battery +12V terminal.

It's possible to add a simple "bridge rectifier" - maybe inside the appliance - which will guarantee that whichever way you connect the battery, it will work correctly. It's a neat idea but you will then lose about 1.4V, which I don't think would be a problem with, say, a stereo or other appliance. Fig. 1b shows how.

To "step down" from 12V d.c. to, say 6V or 7.5V d.c. you can't actually use a transformer since these work with pulses or a.c. only. The easiest way is to use a

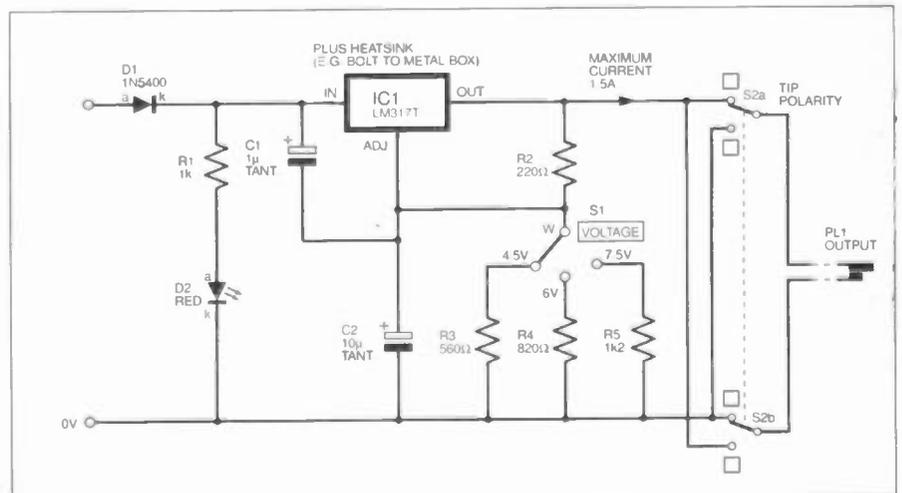


Fig. 2. Mini power source from 12V batteries.

regulator chip, see Fig. 2 which shows a unit capable of offering different voltages to operate low voltage appliances from a 12V battery. Regulators including the LM317 type are current-limiting, short circuit proof, over-heat proof though they are still not indestructible. This circuit will provide up to 1.5A. IC1 should be heat-sunked, perhaps by bolting it with an insulating kit, to a metal box.

## Battery Monitor

I've sketched an l.e.d. voltmeter (Fig. 3) which may help you to keep an eye on your 12V battery. This uses an LM3914 bargraph display, IC1, adapted to measure its own supply, so you simply wire it directly across the 12V supply voltage (right way round – watch pins 2 and 3 carefully!). Ten light-emitting diodes D1 to D10 will indicate the applied battery voltage, ranging from 1.5V to 15V.

The i.c. contains ten internal comparators connected totem-pole-like, each sinking current through a light-emitting diode. They compare an internal reference voltage against the chip's input voltage, at pin 5. I've set the i.c. reference voltage with resistors R3 and R4 to just under 5V. This means that one l.e.d. will light for every 500mV (5V reference/10 stages) increase in the signal.

To enable this to be used to read a 12V battery (the chip's own supply rail, in this case), resistors R1 and R2 are included as a divider: an input of roughly +15V will cause D1 to light. When the voltage gradually falls, l.e.d.s D2-D10 will progressively illuminate. The circuit is set as a "moving dot" display. Connect pin 9 to the positive rail for a bargraph display (not recommended because of the current consumption).

Since the ten outputs are effectively constant-current sinks, the l.e.d.s. will glow at a level independent of the changes in the supply rail: they won't dim when the rail drops. However, the first two or three display l.e.d.s. (D8-D10) are superfluous in this application, because the LM3914 won't operate correctly below a rail of about +5V; I showed them only in case you want to adapt the design for other applications, otherwise you can omit them. Anything much less than 10V or so indicates you've a real problem with your battery!

## Dial Light

Another feature I've added is a "Dial Light" switch. When S1 is closed, each l.e.d. is grounded through a high value resistor, and will glow faintly. One l.e.d. will glow much more brightly when it's displaying the voltage level. The value of resistor depends on the l.e.d. you use – up to 33k or so for high-brightness types is fine. Light-emitting diodes are easily discerned in murky locations but are best mounted out of direct sunlight. Different colours may be used for an at-a-glance check, too. Maybe caravanners and campers will find the circuit of use, as well. I gave more LM3914 hints and tips in December 1995's *Circuit Surgery*. The *Power Check* project in this issue might also be of interest to you.

In general, almost everybody takes a lead-acid battery for granted but they make extremely dangerous foes if treated incor-

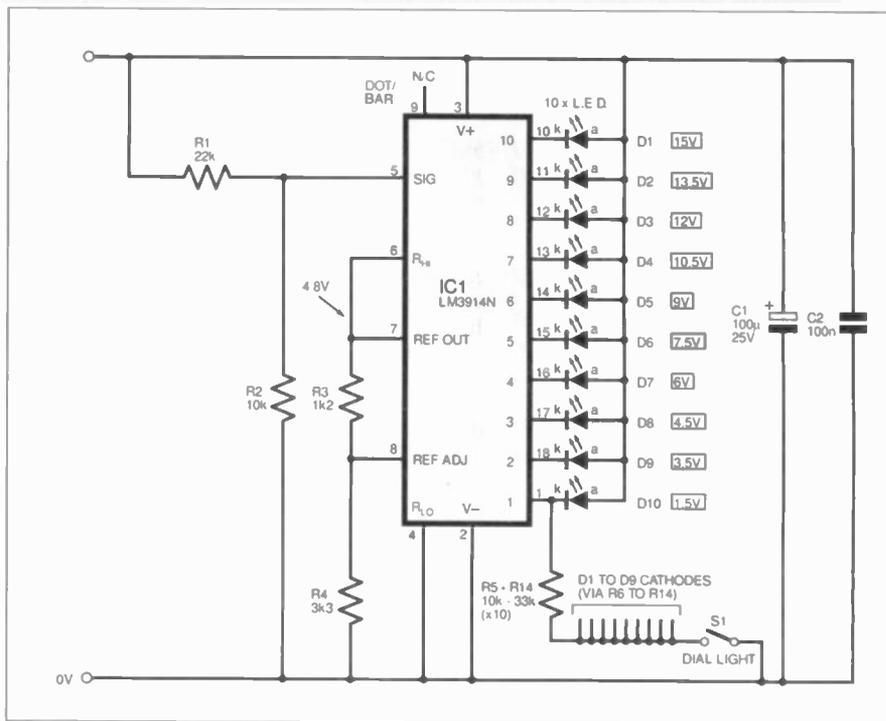


Fig. 3. Car/boat battery voltmeter.

rectly or casually. I have seen the results of a battery explosion and the consequent burns caused to an acquaintance, so I would urge that they are treated with the utmost respect. The present range of sealed-gel batteries (e.g., as made by Yuasa) are expensive, and can't match the capacity of a car/lorry battery, but use a far safer technology in every respect. Thanks for the question and *bon voyage!*

## The Great NiCad Debate

This morning, whilst preening myself in front of the mirror and wondering what to write about next, my rechargeable electric shaver went "flat". Probably the most topical subject of any, because everyone from RC modellers to mobile phone owners use them, the care and use of Nickel-Cadmium cells and batteries (multiple cells) continues to arouse debate!

Readers might recall earlier *Circuit Surgery* columns which dealt with the supposed "memory effect", more correctly called *voltage depression*. To the man in the street, it's when his NiCads go flat more quickly than they used to.

Voltage depression is caused by larger cadmium crystals forming on the cadmium electrode inside the cell when re-charging. This increases the internal resistance of the NiCad and creates an unwanted voltage drop. We'd prefer to see a *smaller* crystalline structure with smaller boundaries which lowers the internal electrical resistance. Larger cadmium crystals become progressively harder to re-form during recharging, so the problem escalates.

Although NiCads have a definite life-span anyway, voltage depression is caused solely by a poor charge/discharge regime on the part of the user, and has been manna for mobile phone salesmen selling spare batteries.

Behaviour likely to spell doom to NiCads include: *light or partial cycling*, because the cadmium deep within the cadmium plate never fully forms into

cadmium hydroxide during discharge. Recharging is supposed to convert it back again, into cadmium, but partial cycling leads to an underlying growth of those unwanted large cadmium crystals. The more you do it, the worse it gets.

*Deliberate and excessive trickle charging/overcharging* is bad news which also means "large crystals". Have you ever noticed how, the more you try to charge something – you leave it on overnight, then all day too, then for several days, and you *still* get less charge? Your cells have got "voltage depression".

*High temperatures* also spell death as this promotes the growth of larger cadmium crystals inside. Overcharging can lead to high temperatures too. Actually, temperature is probably the most overlooked factor, and very possibly the most critical one! If your cells become at all hot, you've overcharged them.

"*Deep discharging*" is questionable. It may help to convert some "deep" cadmium crystals, which may have grown through partial or light cycling, into cadmium hydroxide. Many say it does nothing beneficial at all.

Deliberate deep-discharging to 0V is futile and a complete waste of time, or so the current thinking says. Forget what the mobile phone salesman said about discharging your NiCad battery to "zero".

Other views say that it's good to discharge cells heavily once in a while but not fully down to 0V. Most seem to agree though, that you should never do this to a *battery* (containing several cells), because you run the risk of reverse-charging some of the cells.

## Recover those NiCads

Poor performance may however be reversible. The aim of re-conditioning a "forgetful" NiCad is to destroy those large cadmium crystals and replace them with small "microcrystals" instead. If you treat them more sympathetically again, they will quite often recover.

Vary the charge/discharge cycles. Charge for no more than 15 hours or whatever the manufacturer recommends, to avoid overcharging. When you can measure it, commence recharging when the cell has fallen to absolutely no less than 0.5V per cell. A constant-current load may help, but it has to be used in a controlled manner.

Most importantly, do not overcharge them for long periods. Smaller discharge phases, with "proper" recharging in between, will contribute to a healthy life. In trying to recover a cell, the bottom line is – just start to use them properly again, *more often*.

According to the latest thinking, although the value of 1.0V is often quoted as the critical cut-off voltage, below which a NiCad should not fall, this figure is less "gospel" than we previously thought. I think the best current advice is not to discharge them to zero ever, (*definitely not*, in the case of a multiple-cell battery) but consider a value of about 0.5V to 0.6V per cell the minimum terminal voltage.

The problem is that during discharge, the cell's quite steady discharge curve suddenly plummets as its terminal voltage aims like a bomb towards 0V (see *Circuit Surgery*, February 1996, page 145). So if you do find yourself with a cell reading

about 0.5V or so, it is unwise to continue with its use and you should commence re-charging.

I am afraid that NiCad battery owners have more of a problem, because cells need to be "re-conditioned" individually and unless you can access the 1.25V cells themselves, any battery overcharging or excessive discharging may cause an individual cell to reverse, and you may not be able to recover the battery.

The information was variously supplied by engineers at NASA, Hewlett Packard, Varta, and Steve Walz in Silicon Valley, and appeared in the sci.electronics newsgroups. See our *Net Work* column for more pointers to Internet sites relevant to electronics enthusiasts.

## Hot Battery

From *Jon Jacobs*, by E-mail came the following query related to alkaline batteries.

*Do you know of any home-brew method of attaching those nasty tabs to alkaline batteries? Can it be done with a MIG welder for example, or simpler? Thanks for any help.*

I've never actually seen alkaline cells with tags fitted to the terminals, though it's not unusual to see Nickel-Cadmium cells with tags. MIG welding, or any other form of welding, is a definite no-no, I'm afraid.

The intense temperatures reached in such a short time will cause great damage and it would be dangerous to attempt this. The battery terminals are, I think, nickel plated, and on NiCads at least, they seem to be spot-welded during production.

I'm afraid I can't see any way you could attach the tabs except by maybe soldering both surfaces and gingerly trying to "sweat" them together with a soldering iron. Have plenty of freezer aerosol handy! But I'm not even sure whether ordinary lead/tin solder will "take" to the surface. I do however know that you can solder wires to some batteries (such as coin cells). Maybe try soldering wires directly to the battery. *You must take extreme care not to apply excessive heat, though. Any ideas, anyone?*

## Surgery Calls

If you have any questions to ask, or comments to make, please write to Alan Winstanley, *Circuit Surgery*, Wimborne Publishing Ltd., Allen House, East Borough, Wimborne, Dorset, BH21 1PF, United Kingdom. E-mail [alan@epemag.demon.co.uk](mailto:alan@epemag.demon.co.uk)

We cannot guarantee an individual reply nor undertake to answer questions on commercial equipment but we try to help whenever possible. See you next month.



## Analogue Delay/Flanger

Looking for parts for the "bucket brigade" *Analogue Delay/Flanger* project proved to be a fairly straightforward exercise and most items are commonly stocked by component advertisers. The exceptions to this are, of course, the low voltage delay line and clock generator/driver i.c.s. which may not be carried by your local supplier.

Some analogue delay chips have an in-built clock function, but the MN3207 delay has a partner i.c. (MN3102) which provides the necessary clock signal and gate voltage. Both these i.c.s are currently stocked by *Maplin*, codes UR67X (MN3207 delay) and UR68Y (MN3102 clock/driver).

The choice of case is left to individual choice, but it should be a metal type to give some "screening" to the circuit and help cut down on any possible noise pick-up. Also, it is good practice with any audio circuits to use screened leads for wiring the input and output sockets to the p.c.b.

The Delay/Flanger printed circuit board is available from the *EPE PCB Service*, code 111.

## Simple Exposure Timer

One or two points need to be repeated concerning the construction of the *Simple Exposure Timer*. The most important being: *Be aware that when testing the unit potentially lethal mains voltages are present and extreme care must be taken during this operation.*

The wattage and voltage rating indicated in the "comp. list" for certain components are *minimum* ratings and must be as specified or greater. The 2W metal film resistor should be stocked by most component advertisers.

However, the "continuous" mains rated capacitor and transient suppressor may be a little difficult to find. If problems do arise, the ones in the model came from *Maplin*, codes JR36P (IS Cap) capacitor and HW13P (Supp 250L) suppressor.

When purchasing the transistor check the pinout connections as the various versions of BC184's have differing pin line-ups. One with the suffix L was used here. The printed circuit board is available from the *EPE PCB Service*, code 113 (see page 731).

## PIC-Tock Pendulum Clock

A few problems could arise when searching for components for the *PIC-Tock Pendulum Clock*.

The Sharp spectrally matched infra-red emitter diode type GL380 and special detector phototransistor type PT380 are specific to this design and, as far as we are aware, no alternatives are available. These are RS devices and can be purchased through *Electromail (01356 20455)*, their mail order operation, or any *bona-fide* RS stockists. Quote codes 195-489 (GL380) and 195-502 (PT380).

Supplies of the PIC16C84 EEPROM microcontroller are now plentiful and no problems should be encountered in obtaining this device. The same applies to the crystal.

The PIC microcontroller needs to be programmed and the *Simple PIC16C84 Programmer*, described in our Feb '96 issue, together with a PC-compatible computer is ideal for the job. (Regrettably, the Feb '96 issue, is "sold-out" and we can only supply photostats of the article – see page 722.)

A software source (ASM) and object file (.OBJ) for *PIC-Tock* is available on a 3.5in disk from the *EPE* Editorial Offices for the

sum of £2.50 (Overseas – surface mail £3.10; airmail £4.10). It can also be downloaded from our Internet ftp site address: [//ftp.epemag.wimborne.co.uk](ftp://ftp.epemag.wimborne.co.uk)

The small printed circuit board, which also needs cutting to provide the diode emitter p.c.b., is available from the *EPE PCB Service*, code 109. Probably your best source for the required "hardware" will be your local "plumbing" depot.

## Draught Detector

Not too many problems were encountered when tracking down components for the *Draught Detector* project. The positive temperature coefficient thermistors came from *Electromail (01356 20455)*, order code 158-272 (disc thermistor 80°C).

The potentiometer installed in the prototype model is a wirewound type usually used as a "loudspeaker volume control." This came from *Maplin*, code FX40T. The small buzzer also came from the same source, code KU58N.

The printed circuit board is available from the *EPE PCB Service*, code 112.

## Power Check

It is most important that constructors stick to the 3W or greater wirewound power resistors specified in the *Power Check* project. It is also important that they be mounted separately, on a small tagboard, to the main p.c.b.

Quite a number of component advertisers still stock tagboards and tag-strips, but make sure you mount it well clear of the base of the case. Due to resistor heating, when high currents flow, a metal box should be used to house the circuit.

**You must use 10A minimum rating wiring where indicated in the article.**

Tri-colour 5mm l.e.d.s are widely stocked and should be easily obtainable. Low-voltage 3V to 24V, p.c.b. mounting, buzzers should also be readily available. Try *Maplin*, code KU58N.

The printed circuit board is obtainable from the *EPE PCB Service*, code 110.

# SIMPLE EXPOSURE TIMER

ANDY FLIND

Make light work of timing the precision exposures for p.c.b. making or darkroom printing.

A FREQUENT workshop task for the author is the making of small printed circuit boards. The usual procedure for this is to prepare the artwork, have it copied onto transparent acetate and then expose through this onto photo-sensitive coated board using an ultraviolet light box. Developing and etching in the usual manner then produces a finished board ready for drilling and assembly.

Since the light box was not fitted with a timer, it was decided to construct one as their use is far more convenient than standing over the process with a stopwatch, and produces more consistent results.

It should be pointed out that the presence of live mains in this circuit renders it potentially hazardous. Consequently, it should only be built by constructors with sufficient experience to recognise and avoid the dangers. However, practically all of it can be tested using a safe, low voltage d.c. power supply.

## TIMING RANGE

Commercial light box timers usually have a range extending to at least twelve minutes. It seemed sensible to provide the home-produced one with something similar, yet the optimum exposure in most cases appears to be about two and a half minutes. Because of this, it was decided to provide an "expanded" control, with the first couple of minutes spread over half the scale for fine adjustment, with the remainder progressively compressed.

Whilst the design was in progress, the author's daughter acquired a photographic enlarger, and it soon became apparent that a small modification would result in a timer suitable for controlling this as well.

The usual exposure used in photographic printing is less than a minute, although some enlarger timers extend beyond two minutes. With the expanded control, it is possible to provide a two-minute scale with finer control over the first minute. In fact, the timer shown in the photographs is the "photographic" version, as the UV timer has been built into the light box.

## TIMING ACCURACY

Although timer circuits using electrolytic capacitors for long periods are not uncommon, this is not always the best approach because of the wide tolerance in the values of these components. This makes it difficult to design a reliable and "repeatable" circuit. Additionally, the leakage currents associated with electrolytics may also affect timing performance if they are used with high-value resistors.

Where a period in excess of a minute is required, it is much better to use an oscillator with a relatively short period and then to count a set number of these periods using a divider circuit. This was the method chosen for this design.



## SCALING UP

Expanding a portion of the control scale presented an interesting design challenge. A linear potentiometer produces a linear variation of period in many oscillator circuits, but substitution of a logarithmic pot produces too much expansion for this design.

An interesting point about log pots is that the "law", if measured and plotted as a graph, is not usually the smooth curve that might be expected. In fact, it often consists of just two straight-line sections with a sharp connecting "knee", presumably reflecting the fact that most manufacturers make tracks from just two types of resistive compound! Other pot laws are available, but not often to home constructors.

It is possible to construct an oscillator where the period is proportional to the reciprocal of the control position - in fact this would be a linear frequency control - but again this provides excessive compression.

Using a dual-ganged linear pot, though, with the wiper of the first connected to the top of the second, it is possible to produce a voltage with an approximate "square law" control function, which gives about the right degree of scale compression.

The design aim, therefore, was to produce an oscillator with a cycle period proportional to this voltage.

## CIRCUIT DIAGRAM

The complete circuit diagram for the Simple Exposure Timer is shown in Fig. 1.

In this circuit, op.amp IC1b and timer IC2 form a voltage controlled oscillator circuit having its frequency varied by the dual-ganged potentiometer VR1.

The power supply, about 12V, is divided by two and buffered by op.amp IC1a. Between them, VR1a and VR1b then tap the output of IC1a to produce the required control voltage.

Resistor R3 effectively swamps any variations in VR1 value, preventing them from altering the lowest control voltage as set by R4 and R5. The values of these resistors are chosen to give a ratio between the highest and lowest voltages of 32.5:1, which sets the timing range from 0.4 to 13 minutes, ensuring cover of the intended range of 0.5 to 12 minutes.

The control voltage does not conform exactly to a square law because of the way in which VR1b loads VR1a, but it is fine for the purpose of this design. Resistor R7 and capacitor C2 remove any noise present on the control voltage.

## COMPARATIVE REFERENCE

Op.amp IC1b is used as a comparator. Capacitor C1 charges in exponential fashion from VR2 and R6 until the voltage across it reaches the selected control voltage from VR1b. When it does so, the output of IC1b goes low, triggering timer IC2 which then delivers a 2.5ms pulse from output pin 3. This is used to discharge C1 via transistor TR1. The output from IC2 is therefore a series of pulses with the period between them controlled by the voltage from VR1.

The frequency used is quite low, between 1.5Hz and 35Hz. This means that the 2.5ms reset pulse forms only a small part of each cycle, yet is long enough to ensure complete discharge of C1. VR2 provides overall trimming adjustment for calibration.

From IC2, the output pulses are applied through resistor R10 to the clock input of binary counter IC3. This counts the pulses until the selected output goes high, thus blocking the clock signal via diode D1.

Pin 15 of IC3 is the 11th counter output, so 1024 clock pulses are counted before this goes high. Provision is made on the printed circuit board (p.c.b.) to select two other outputs, one from pin 12 for use as a two-minute timer and one from pin 4 for assisting with calibration.

## GATED OUTPUT

The final output of the circuit is controlled by quad NOR gate IC4. The first two gates of this, IC4a and IC4b, are connected to form a set-reset flip-flop. When the circuit is first energised, a positive pulse from C5 via D2 to IC4a pin 1 causes IC4a output pin 3 to go low and IC4b output pin 4 to go high, the "off" state. This ensures that the output is not immediately energised when the unit is plugged in.

The high output of IC4b pin 4 charges C4 through R13. When Start switch S1 is pressed, the charge on C4 positively pulses IC4b input pin 6, causing output pin 4 to go low and output pin 3 to go high, the "on" state. At the same time, the pulse resets counter IC3 via its input pin 11.

Capacitor C4 will not be recharged until the output returns to the "off" state, ensuring that if switch S1 is held down or

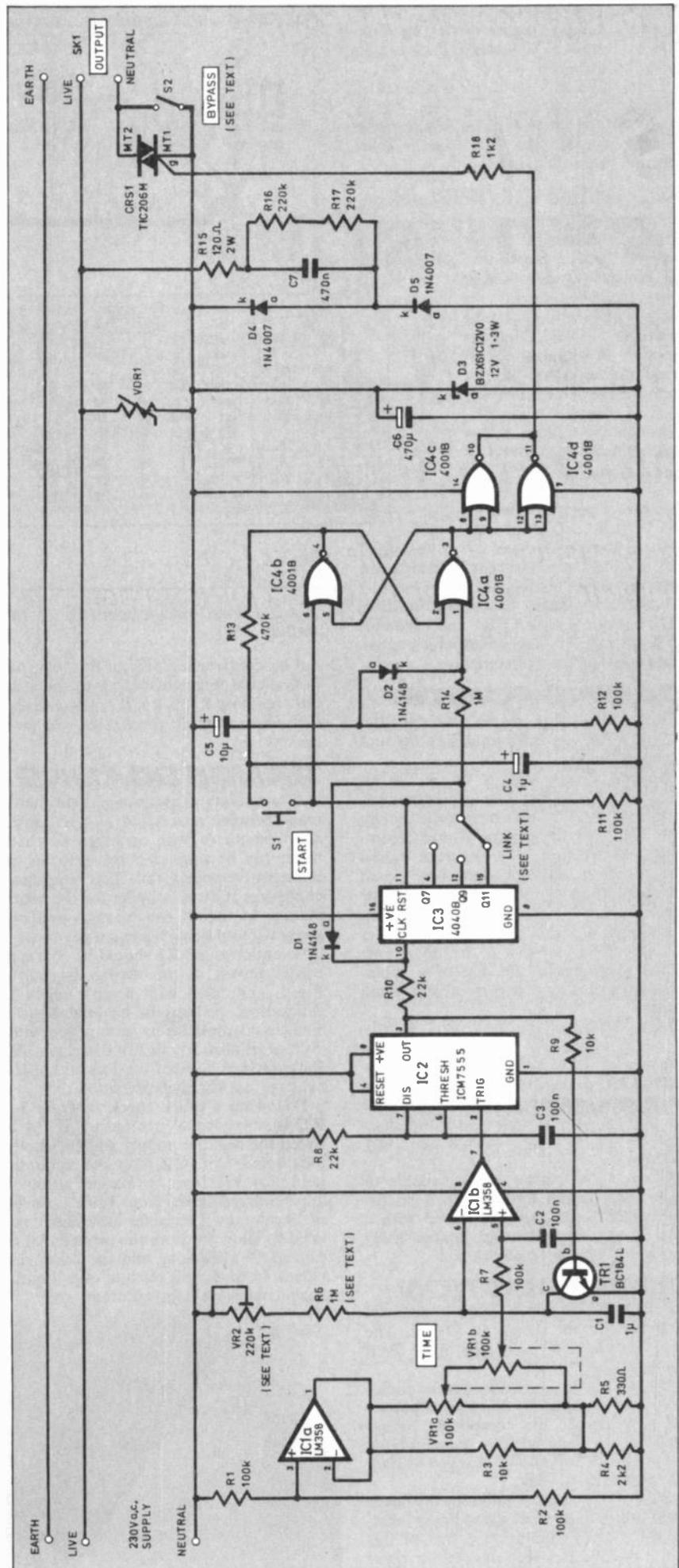


Fig. 1. Complete circuit diagram for the Simple Exposure Timer.

accidentally pressed again before timing is complete, the output time will not be affected. Timing ceases when the link-selected output of IC3 goes high and resets IC4a through R14.

Gates IC4c and IC4d are connected in parallel as inverting buffers for driving triac CSR1 through R18. A negative gate current is used since the triac is more sensitive to this than to positive.

## POWER SUPPLY

Power for the main circuit is provided by a capacitive mains dropper circuit. In essence, the a.c. current through capacitor C7 is virtually constant at about 35mA, set by the mains supply voltage and the reactance of C7. In the positive direction, this current flows through diode D4. In the negative direction, it is used to charge C6 via D5, although the voltage across this is limited to about 12V by Zener diode D3.

Apart from the small amount of power drawn by the circuit, most of the current flowing through C7 is "reactive" and does not generate heat or add to the electricity meter reading!

Varistor (voltage dependent resistor) VDR1 protects triac CSR1 and capacitor C7 from high voltage spikes which sometimes occur on the mains supply.

## CASING POINTS

Before discussing p.c.b. assembly and testing, a few words about casing the unit are appropriate.

Housing of the unit is up to the individual constructor. The prototype was fitted into the UV light box itself, though with hindsight the author would recommend construction in a separate plastic case, using it with the light box as an accessory. In most instances, this would be much simpler.

Although a mains power output socket was mounted in the case of the unit shown in the photographs, the use of a cable-mounted socket may be preferable to some readers.

Many enlargers are constructed mostly of metal and likely to be used in the presence of water and chemicals. Consequently, it is important to ensure that the earth is properly connected through the unit. Also, the case used should at least be splash proof, even if not fully waterproof.

Many of the plastic cases available to home constructors have a lipped lid fitting, which could easily be sealed with a drop of silicone sealant or similar. Fully waterproof cases are also available.

## CONSTRUCTION

Details of the p.c.b. components and track layouts are shown in Fig. 2. The p.c.b. is available from the *EPE PCB Service*, code 113.

The first step in construction is the choice of version required. If the twelve-minute one is required, the component values listed will be suitable. For a two-minute unit preset VR2 should be changed to 100k and resistor R6 to 680k.

Since *EPE* readers undoubtedly have better things to do than spend hours locating the control calibration points of this unit, a method has been devised for rapid calibration with a DVM (digital voltmeter)

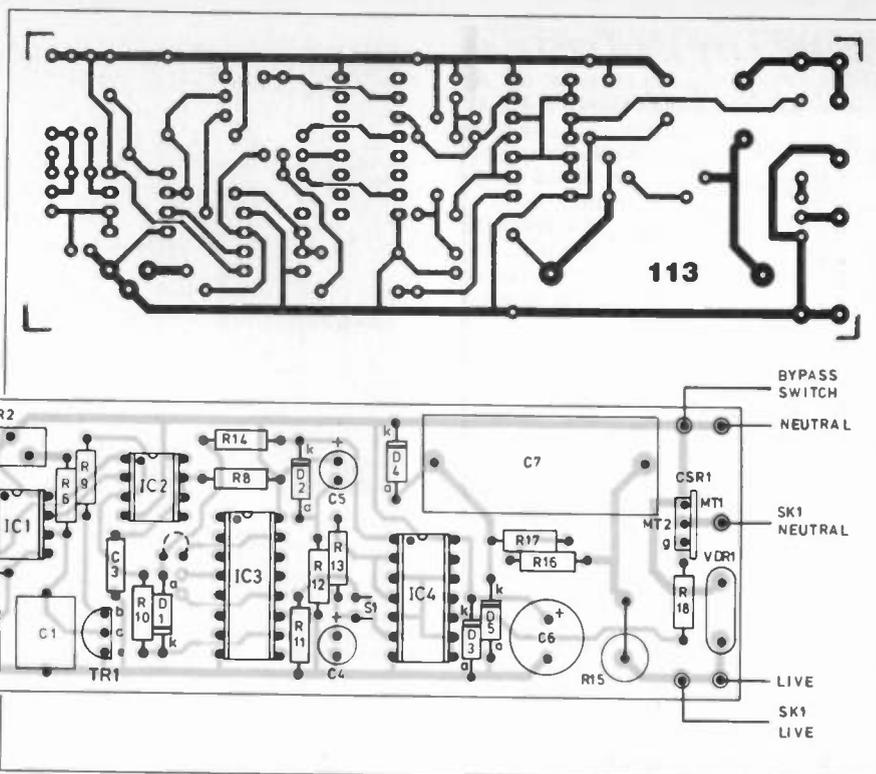


Fig. 2. Printed circuit board component layout and full size copper foil track master-details.

during construction. To do this, construction should begin by fitting to the board only resistors R1 to R5, R7, plus capacitor C2 and op.amp IC1 (preferably with an i.c. socket).

## RANGE SCALING

A temporary connection should then be made between pins 6 and 7 of IC1 with a short length of wire arranged so that a meter can be connected between this and the negative supply rail. This temporarily configures IC1b as a buffer for the control voltage so that it can be measured by a meter without being loaded in any way.

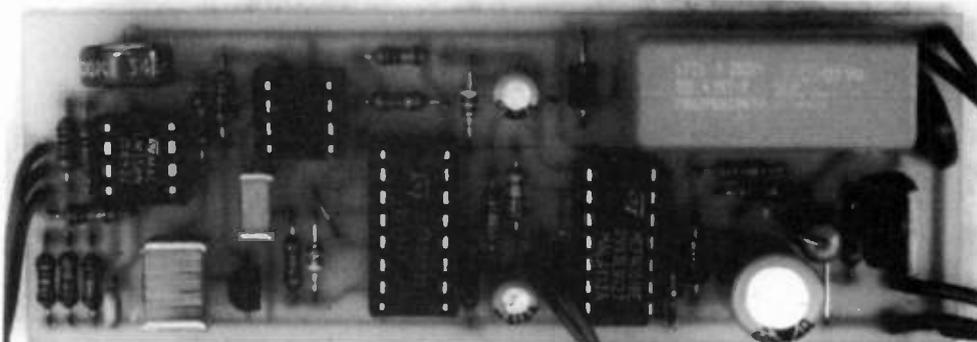
Potentiometer VR1 should be connected up as shown in the wiring diagram of Fig. 3, and fitted with a scale ready for calibration, perhaps in its final housing. The circuit should now be supplied with a voltage set as nearly to 12V d.c. as possible. Batteries can be used for this, although a bench power supply is preferable.

Following a quick check that pin 1 of IC1 is supplying 6V, connect a DVM between the negative supply and the shorted pins 6 and 7 of IC1. Now the calibration points of VR1 can be marked using the appropriate columns from Table 1, for two or 12 minutes. The tables have been calculated to allow for both the exponential nature of C1's charging and the 2.5ms reset pulses. In trials, this method of calibration has proved simple and accurate.

### Timer Calibration Tables

12 minute version		2 minute version	
Mins	Volts	Secs	Volts
0.4	0.227	4	0.214
0.5	0.290	5	0.277
0.75	0.446	7.5	0.433
1	0.599	10	0.587
1.25	0.751	12.5	0.739
1.5	0.900	15	0.889
2	1.193	20	1.182
2.5	1.478	25	1.468
3	1.756	30	1.747
3.5	2.026	35	2.018
4	2.289	40	2.282
4.5	2.546	45	2.539
5	2.795	50	2.789
6	3.275	60	3.269
7	3.729	70	3.725
8	4.160	80	4.157
9	4.568	90	4.566
10	4.956	100	4.954
11	5.322	110	5.321
12	5.670	120	5.670
13	6.000	130	6.000

One "end point" of VR1's rotation should be marked so that if the knob is subsequently removed it can easily be refitted correctly. Following this procedure, the connection between pins 6 and 7 of IC1 should be removed.



# COMPONENTS

## Resistors

R1, R2,	
R7, R11,	
R12	100k (5 off)
R3, R9	10k (2 off)
R4	2k2
R5	330Ω
R6	1M (680k for 2-min timer)
R8, R10	22k (2 off)
R13	470k
R14	1M
R15	120Ω 2W metal film
R16, R17	220k (2 off)
R18	1k2

All 0.6W 1% metal film, except R15

## Potentiometers

VR1	100k dual rotary, lin. carbon.
VR2	220k sub-min. preset, vertical (100k for 2-min timer)

## Capacitors

C1	1μ polyester layer
C2	100n resin dipped ceramic
C3	100n polyester layer
C4	1μ radial elect., 100V
C5	10μ radial elect., 50V
C6	470μ radial elect., 35V
C7	470n suppression type, 250V a.c. working

## Semiconductors

D1, D2	1N4148 signal diode (2 off)
D3	BZX61C12V0 Zener diode, 12V 1.3W
D4, D5	1N4007 rectifier diode, 1A 1000V (2 off)
TR1	BC184L <i>n</i> p <i>n</i> transistor
CSR1	C206M triac, 4A 600V
IC1	LM358 dual op.amp
IC2	ICM7555 CMOS timer
IC3	4040B 12-stage binary ripple counter
IC4	4001B quad 2-input NOR gate

## Miscellaneous

S1	min. push-to-make switch
VDR1	varistor (transient suppressor) for 250V a.c. operation

Printed circuit board, available from the *EPE PCB Service*, code 113; 8-pin d.i.l. socket (2 off); 14-pin d.i.l. socket; 16-pin d.i.l. socket; plastic case, 130mm x 68mm x 45mm (see text); pointer knob; 13A mains plug and socket to suit application; optional s.p.c.o. mains-rated toggle switch (see text); connecting wire; solder, etc.

Approx cost guidance only

**£18**

Excl. case and mains connector

The rest of the components can now be fitted to the board with the exception of Zener diode D3 and triac CSR1.

Note that resistor R15 is a 2-watt type. Its purpose is to limit the momentary surge that occurs if the unit is plugged in at the precise instant where the mains voltage is high, for which a reasonably rugged component is needed to withstand it.

## DIVISION FACTOR

The division factor should be set with a link as shown in Fig. 4. For a two-minute timer this will be to IC3 pin 12 for a count of 256 pulses. For a twelve-minute timer, first temporarily connect the link to IC3 pin 4 for 64 pulses.

Having connected switch S1, the circuit can be powered again from the 12V supply,

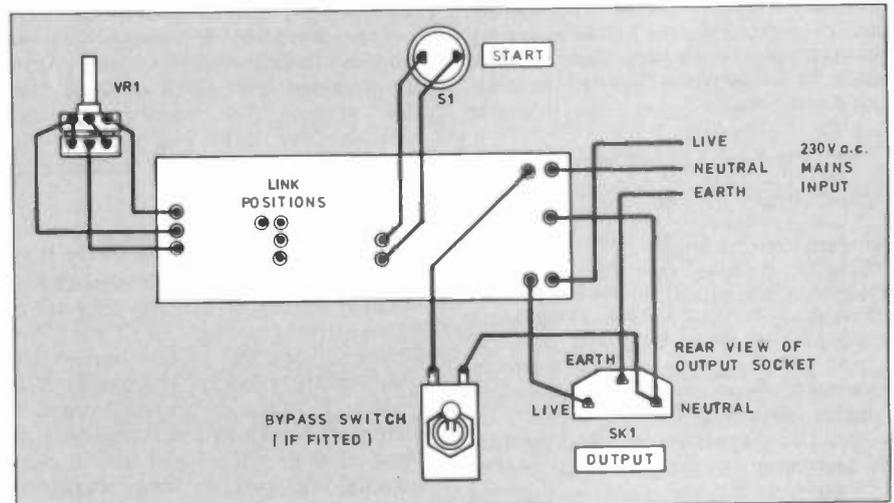
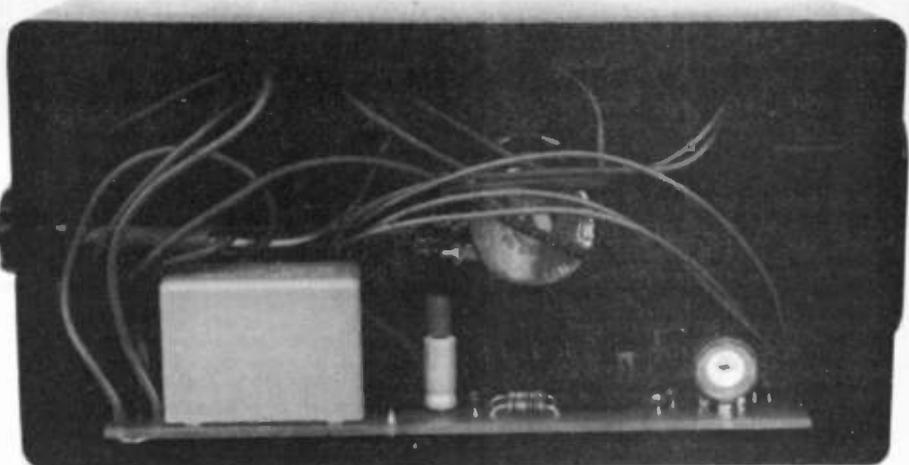


Fig. 3. P.C.B. and off-board component wiring diagram.

with a meter connected between negative and the junction of R18 and the combined output at IC4c and IC4d. The output should normally be high, going low for a time when S1 is pressed.

For a two minute timer, VR1 can be set to one or two minutes and VR2 adjusted to give the correct output time. For a twelve minute unit, the temporary connection to IC3 pin 4 means that all scaled values are divided by sixteen, so the 12 minute setting will actually correspond to a period of 45 seconds. This speeds the adjustment of VR2 considerably, after which the link can be fitted permanently to the "Pin 15" position for correct times.

## MAINS TESTING

Following these adjustments, diode D3 and triac CSR1 can be fitted and the unit tested with a mains supply and a suitable load, such as a 100W lamp. At this point, of course, the unit becomes potentially dangerous to handle and appropriate precautions must be observed.

For safety reasons, a suitably rated fuse, of 3A or lower, should be used in the plug

associated with the unit. Power handling is limited to a couple of hundred watts by the fact that the triac is not provided with a heatsink, but one could easily be fitted if the application required it. For most UV light boxes and enlargers though, this power will be more than adequate.

Where the timer is to be used with a photographic enlarger, bypass switch S2 will be required to allow adjustment and focusing of the enlarger. This can be connected across the triac as shown in Fig. 3.

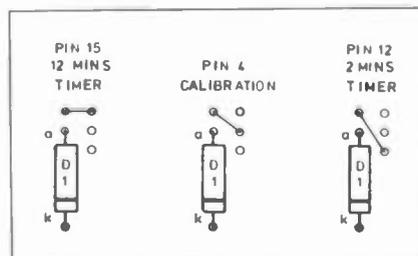
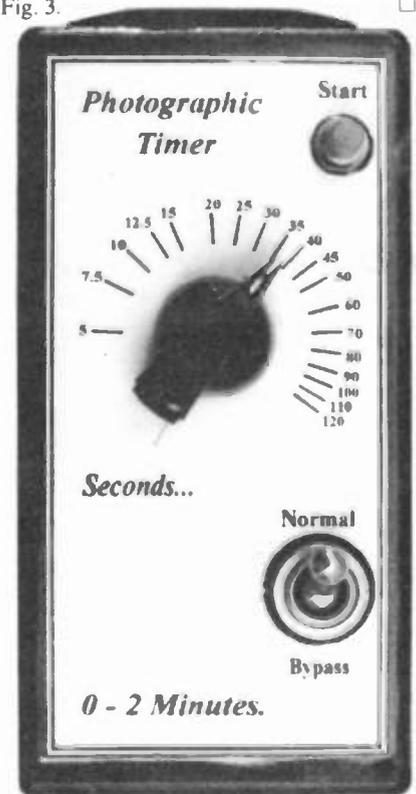


Fig. 4. Division factor links.



0 - 2 Minutes.

# New Technology Update

*New developments in charge coupled device technology are likely to result in further miniaturisation of electronic cameras – Ian Poole reports.*

**C**HARGE coupled devices (c.c.d.s) are being widely used in image sensing applications. They were originally invented in the early 1970s at Bell Labs, where the transistor was invented. Since their invention, development of c.c.d.s has been led by the Japanese. As a result, their cost has fallen dramatically. Coupled to this, reliability has risen and power consumption fallen.

Now c.c.d.s are widely used in image sensing applications. Naturally one of their main uses is for camcorders where the market has grown enormously in the last few years. There is also a wide variety of other uses for these devices where visual images are needed. Everything from the new PC vision conferencing to various forms of automatic inspection and other image sensing applications.

C.C.D. arrays form an ideal method of capturing an image. Being highly integrated, they are very cost effective and occupy comparatively little space. They often enable manufacturers to miniaturise their equipment, or to build in further features.

Despite this success story there are still many areas for improvement. A number of ideas are being investigated which may enable far greater flexibility to be achieved. It may even be possible for a single chip to contain all the major electronic components for a television camera.

## Operation

As the name indicates, c.c.d.s depend upon the generation and transfer of charge for their operation. They include a capacitor as part of the basic circuit. In most devices these days the capacitor is a buried channel MOS capacitor for each pixel integrated onto the chip. It is fabricated by growing an *n*-type region onto the *p*-type substrate. Other areas are also grown. The gate for the MOSFET is grown by first laying down a region of silicon dioxide and then placing some highly doped and conductive silicon on top.

When light falls onto the capacitor, the photons cause electron/hole pairs to be generated. The electrons migrate towards the *p*-type substrate whilst the holes accumulate in the capacitor.

With holes forming a charge in each of the capacitors proportional to the amount of light, it only remains for this to be transferred out. After exposure, the charge has to be transferred serially from one cell to the next in a form of shift register.

Once the charge has been transferred from the light sensitive capacitors into the shift register, the capacitors are reset, ready for their next exposure.

When the charge in the register reaches the exit point from the device it is converted to a voltage by an amplifier circuit. As the charges from the different cells reach the exit from the device the varying voltages represent the light levels across the device and the image is successively built up.

## New Developments

The major problem with these charge coupled sensors is that the data has to be transferred to the end of each row before it can be passed out of the c.c.d. into any further processing electronics. Then a considerable amount of electronic manipulation is required. In view of their widespread use in camcorders, the cost of many c.c.d.s is around £10, whereas the cost of the associated processing circuitry may be around the £50 mark.

This limitation could be overcome if each pixel could be accessed individually. The main problem in achieving this is the large number of connections which would be needed.

However, if all the electronics for the camera was integrated onto the same chip, this problem would be overcome. Also, by placing all the electronics for a camera onto one chip, costs could be reduced by considerable proportions. This approach is now becoming a reality in view of the fact that connections of less than one micron can be made in a semiconductor chip.

## Accessing Pixels

To achieve this, a number of new developments have been made allowing the charge of each pixel to be transferred individually. As the image sensor or photogate element generates a charge, this has to be converted to a voltage before it is interfaced to any other circuitry. In one development this is achieved using a field effect transistor circuit for each pixel. Four transistors are used for each site, and they provide all the readout, selection and reset functions.

A number of chips have been made using a 256 × 256 matrix. So far the performance has lived up to expectations giving sufficient light to voltage conversion. The only area where it cannot compete with c.c.d.s at the moment is in the resolution which has been

achieved. However it is not anticipated that there will be any major problems in extending the level of integration and obtaining a larger matrix in the future as techniques are refined.

At the moment only the analogue functions are integrated onto the chip. To enable the full range of functions to be performed further work is progressing to give an analogue to digital conversion and also functions like automatic exposure and an electronic shutter.

## Future Rewards

Although the initial work to enable all these functions to be contained on the one chip will cost money, the rewards are likely to be very large. The obvious use for them is within camcorders and the market for these is expanding all the time. Here, placing all the functions on one chip will reduce costs as well as the size of the cameras.

In addition to the camcorder market there are many other uses. With all the electronics on a single chip, the size of complete cameras will fall by significant amounts. This will allow cameras to be used in many monitoring applications where it might not have been possible before. They will be able to be used in a number of process monitoring applications, allowing visual inspection of different areas of a manufacturing process.

## Still Cameras

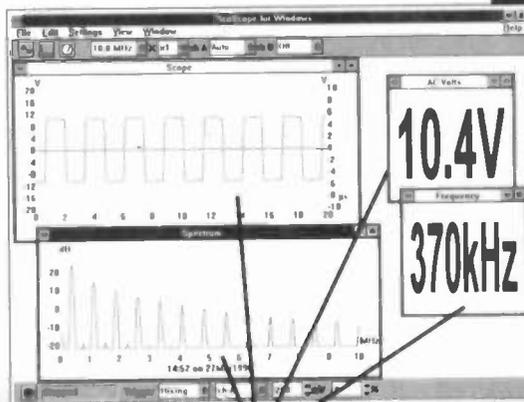
They could also find uses in still cameras. Although electronic cameras are not widely used yet, their use offers many advantages in terms of flexibility. Pictures can be instantly viewed on an l.c.d. screen, down-loaded into computers and processed accordingly. Even for the home user this is likely to become more commonplace.

Prints can also be made on the variety of printers which are widely available now. It would be possible to down-load the output of a camera into a computer and print out the results without the need for sending the film off or taking it to the local chemist.

The single chip camera would help to reduce costs of the whole camera and bring them more into the reach of the public at large. All of these possibilities mean that work being undertaken on these new camera i.c.s is likely to pay large dividends in the future.

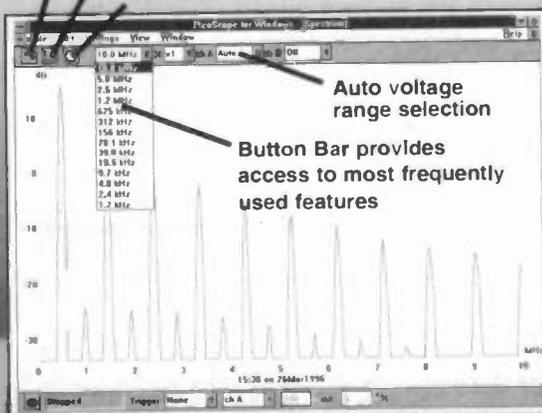
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# INTERFACE

## Robert Penfold



**M**ANY readers will no doubt have noticed that a growing range of so called "virtual" measuring instruments based on PCs are coming onto the market. The basic idea of a virtual instrument is to replace a complex piece of measuring equipment using some relatively simple hardware plus a PC and suitable software.

Most of the commercially produced units and software are quite complex. Typical systems on offer include twin beam storage oscilloscopes, logic analysers, and spectrum analysers, complete with on-screen controls that are operated via the mouse.

### Testing, Testing

It is difficult for the do-it-yourself computer enthusiast to compete with this type of thing. The hardware part of the system is not necessarily that hard to tackle, but the software side of the system usually requires a great deal of development time and an expert programmer.

This is not to say that it is impossible to undertake test gear projects based on a PC. There are certainly plenty of possibilities for those who are willing to settle for relatively simple systems.

The piece of test equipment featured here is a transistor tester that provides digital readout via the screen of the PC. It interfaces to the host PC's printer port, and either port one or port two can be used. Both *npn* and *pnp* bipolar transistors can be tested, but the system is not usable with any form of field effect transistor (f.e.t.).

Most transistor testers operate on the basis of feeding a fixed base current to the test device, and then measuring the collector current. This is convenient

in that the collector current is proportional to the current gain of the test transistor. Consequently, there is no difficulty in having direct readout of current gain on an analogue or digital display.

A drawback of this method is that the current gain is not measured at a specific collector current. The lower the gain of the component under test, the lower its collector current.

Current gain of transistors varies significantly with changes in collector current, and in general a lower operating current gives reduced gain.

device can be calculated from the base current reading, but one is not directly proportional to the other. The lower the base current, the higher the current gain of the test component. The scaling is not just reverse reading, but is also non-linear.

In a computer based system this is not really of any consequence, since the software can provide a few simple calculations to provide a direct readout of current gain. It is basically just a matter of dividing the fixed collector current by the base current reading from the interface.

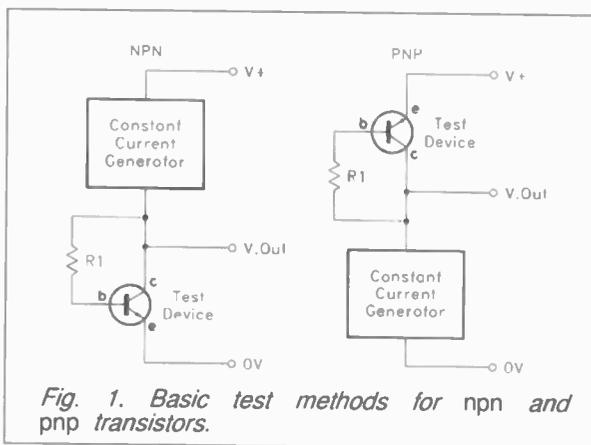


Fig. 1. Basic test methods for npn and pnp transistors.

This tends to give unrealistically low readings on low gain devices, and could give the impression that a component is sub-standard when it is actually "up to scratch".

This tester gives low gain devices a "fair hearing" by using a fixed collector current and a variable base current. The basic idea is to have a circuit that automatically adjusts itself to provide the base current that just supports the collector current in use. The gain of the test

The test device is biased into conduction via resistor R1 connected between its collector (c) and base (b) terminals. Provided the value of R1 is low enough, it will supply a base current that just supports the collector current set by the constant current generator circuit.

An excessive base current is avoided by a negative feedback action. An increased base current results in a lower collector voltage, which reduces the base current. In effect, the collector voltage automatically adjusts itself to provide

### Self Adjusting

The basic arrangement used in the interface, which feeds into the PC's printer port via a simple analogue to digital converter, is shown in Fig. 1. If we take the *npn* circuit first, the collector (c) of the transistor is fed from a constant current generator. The current used must be one that gives reasonable gain from higher power transistors, but it must not be so high as to risk damaging low current devices. This system uses a current of 10 milliamps, which seems to give good results in practice.

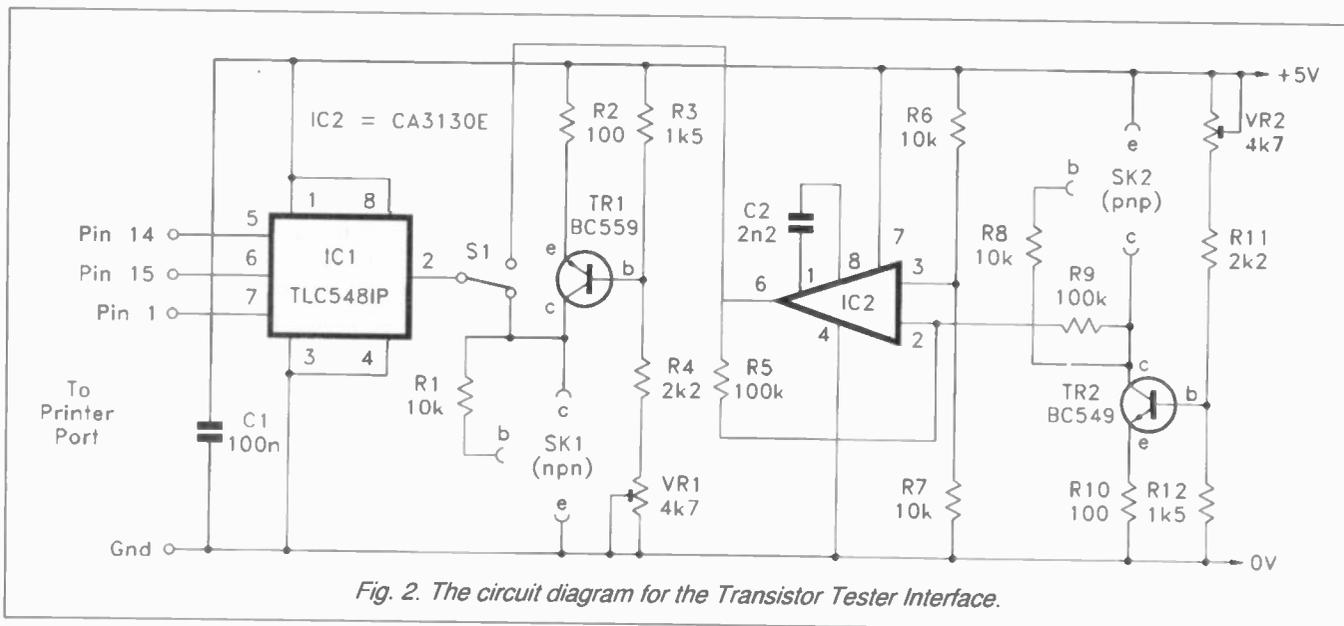


Fig. 2. The circuit diagram for the Transistor Tester Interface.

the correct base current for the test device.

### Calculating Gain

In order to calculate the gain of the test transistor it is merely necessary to measure the base current, and then divide the collector current by this figure. In practice it is quite difficult to measure the current flow through resistor R1 using a computer.

It is easier to take the indirect approach and measure the collector voltage. This is equal to the voltage across R1, plus the (approximately) 0.7V developed across the base-emitter junction of the test transistor. Deducting 0.7V from the collector voltage gives the voltage across R1, and Ohm's Law can then be used to calculate the base current.

One slight flaw in this method of testing is that although the collector current is constant, the collector voltage varies significantly from one test device to another. Fortunately, this is of no great importance, since the gain of a transistor is little affected by variations in collector voltage.

The *pnp* test circuit is essentially the same as the *nnp* type, but with a change of supply polarity. This brings a slight problem in that the output voltage is referenced to the positive supply rail, and not the 0V "earth" rail. This is not a major obstacle though, and either hardware or software can be used to compensate for this factor.

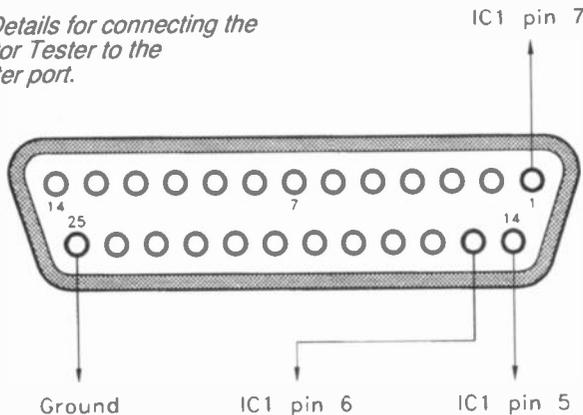
### Listing 1: Transistor Tester Program

```

10 REM transistor tester program
   (TLC548 A/D converter)
20 CLS
30 LOCATE 8,25
40 PRINT "DC CURRENT GAIN"
50 OUT &H37A,1
60 OUT &H37A,3
70 OUT &H37A,2
80 X = INP(&H379) AND 8
90 X = X*16
100 OUT &H37A,3
110 OUT &H37A,2
120 Y = INP(&H379) AND 8
130 Y = Y*8
140 X = X + Y
150 OUT &H37A,3
160 OUT &H37A,2
170 Y = INP(&H379) AND 8
180 Y = Y * 4
190 X = X + Y
200 OUT &H37A,3
210 OUT &H37A,2
220 Y = INP(&H379) AND 8
230 Y = Y * 2
240 X = X + Y
250 OUT &H37A,3
260 OUT &H37A,2
270 Y = INP(&H379) AND 8
280 X = X + Y
290 OUT &H37A,3
300 OUT &H37A,2
310 Y = INP(&H379) AND 8
320 Y = Y/2
330 X = X + Y
340 OUT &H37A,3
350 OUT &H37A,2
360 Y = INP(&H379) AND 8
370 Y = Y/4
380 X = X + Y
390 OUT &H37A,3
400 OUT &H37A,2
410 Y = INP(&H379) AND 8
420 Y = Y/8
430 X = X + Y
440 OUT &H37A,3
450 X = X * 2
460 OUT &H37A,1
470 X = X - 69
480 X = 10000 \ X
490 LOCATE 10,30
500 IF X < 25 THEN PRINT " "
510 IF X < 25 GOTO 50
520 PRINT X
530 GOTO 50

```

Fig. 3. Details for connecting the Transistor Tester to the PC printer port.



### The Circuit

The full circuit diagram for the Transistor Tester Interface appears in Fig.2. The analogue-to-digital converter is based on the TLC548 serial converter. This chip, and its use with a PC printer port, was covered in the November 1995 issue of *EPE*. Refer to the *Interface* article in that issue if you require detailed information on the converter. All you really need to know here is that it has an input voltage range of zero to five volts.

Transistor TR1 is used in the constant current generator for the *nnp* test circuit. Preset potentiometer VR1 is adjusted to give one volt across resistor R2. If slightly reduced accuracy is acceptable, simply replace resistor R4 and VR1 with a fixed resistor of 3.3 kilohms (3k3) in value.

Resistor R1 is the base bias resistor, and a value of 10 kilohms is a very convenient one. If the readings from the converter are doubled, this gives a range

of returned values from 0 to (roughly) 500, which equates to a base current range of 0 to 500 microamps ( $\mu$ A).

The *pnp* test circuit has TR2 as the constant current source. Here, preset VR2 should be adjusted to give one volt across resistor R10. A software inversion can be provided by deducting the returned value from 255.

This circuit provides a hardware inversion, which avoids the need for *nnp/pnp* switching in the software. The inversion is provided by IC2 which acts as a unity gain inverting amplifier. This stage works fine using a CA3130E, but is unlikely to work at all using most other operational amplifiers. Switch S1 provides *nnp/pnp* switching, and it simply switches the output of the appropriate circuit to the input of the converter.

To keep things simple, separate test sockets are used for the two types of transistor. However, an extra three poles

on switch S1 would enable one socket to be shared between the two sections of the unit.

Note that IC2 is a CMOS device, and that it therefore requires the standard anti-static handling precautions. The resistors, apart from R3, R4, R11 and R12, should have a tolerance rating of one percent.

### Software

The accompanying GW BASIC listing reads the port, calculates the current gain, and prints it on the screen. Most of the program is concerned with reading the port, and is essentially the same as the listing provided in the November 1995 issue (see *Back Issues* page).

Some lines added onto the end of the original program work out the current gain, print the answer on the screen, and loop the program indefinitely. Lines 500 and 510 detect very low readings of under 25, and blank the display. This gives a blank display with no test device connected, or if the test component has a gain of under 25.

The port addresses used in the program are for printer port one. If the system is used with printer port two, addresses &H379 and &H37A should be changed to &H279 and &H27A respectively (e.g. "OUT &H27A,1" at line 50). There is no built-in means of breaking out of the loop, but the usual "Control - Break" combination will halt the program.

In use the system seems to work very well, giving more plausible results than most testers when testing lower gain and (or) higher current devices. One drawback of this system is that it has lower resolution at high gains than at low gains, but it still gives perfectly acceptable results with high gain devices.

# MAX038 WAVEFORM GENERATOR

ANDY FLIND

*At last there is a waveform generator which offers greater advantages over the familiar 8038 device.*

**D**EDICATED waveform and "function generator" i.c.s have been around for many years now. Some of the simpler ones offer only square and triangular output waveforms but at least one, the well-known 8038, also has a sine wave output which makes it a good basis for the design of versatile signal generators.

It is fairly complex to design with, though, and a successful circuit generally needs quite a few preset adjustments for acceptable performance. In addition, its maximum frequency is quite low. Although one manufacturer quotes a top speed of 1MHz, in practice the 8038 usually begins to struggle beyond 200kHz and, where good waveforms are required, it is preferable to regard 100kHz as the maximum. A faster waveform generator i.c. has been overdue for some time.

## EASY TO USE

With the introduction of their new MAX038 waveform generator i.c., Maxim have at last filled this need. Like the 8038, the MAX038 provides all three output waveforms but it is much easier to use and has some interesting new features that increase its versatility.

The most important characteristic, however, is speed. Maxim claim over 20MHz, and the author's experience shows that it is indeed capable of this with little degradation of any of the output waveforms.

At 10MHz the outputs are excellent, even the square wave! At around £15 it is not a cheap i.c., but it looks set to become the new industry standard, so in time this price may well fall. Meanwhile, it is still inexpensive in view of the performance of which it is capable.

At the time of writing, the device is available in both surface-mount and standard dual-in-line (d.i.l.) packages. The 20-pin d.i.l. version will probably be the one encountered by most readers and its pinouts are shown in Fig. 1.

## OPERATIONAL TOUR

A good way to describe the operation of this new i.c. is to begin with a brief description of its internal architecture, and continue with a tour of the external connections giving detailed descriptions of their functions. A simplified diagram of the internal structure is shown in Fig. 2.

The control current regulator converts signals from three inputs to a control current which passes to the oscillator. This is of the relaxation type, where a capacitor is repeatedly charged and discharged between two preset limits, with currents set by the input control current. The outputs from the oscillator are a triangle wave from the capacitor and a square wave from the comparator used for switching between charge and discharge.

Sine waves are obtained by modifying the triangle wave in a shaping circuit. The three waveforms then go to a selection switch which is controlled by logic levels

applied to two waveform control inputs, and the one chosen passes through a buffer amplifier to the output.

Three further functions are provided by the device. A very fast comparator, driven from the triangle wave, produces a logic level sync output for driving synchronised external circuitry. A phase detector with an external input can be used for phase-locking the oscillator to an external signal, possibly using division, to construct a phase-locked loop. Finally, a 2.5V reference source is provided for use in generating input control voltages for the current generator.

## POWER SUPPLIES

Dual power supplies of +5V and -5V are needed, with a tolerance of 0.25V and currents of about 45mA from both. The simplest way to provide these is from 7805 and 7905 positive and negative regulators. The 1A versions are preferable to the 100mA type because they will usually dissipate a small amount of heat and it is much easier to attach heatsinks to the 1A devices.

The MAX038 has its positive supply input at pin 17 and the negative supply input at pin 20. Pins 2, 6, 9, 11, 15 and 18 are all ground connections and must all be

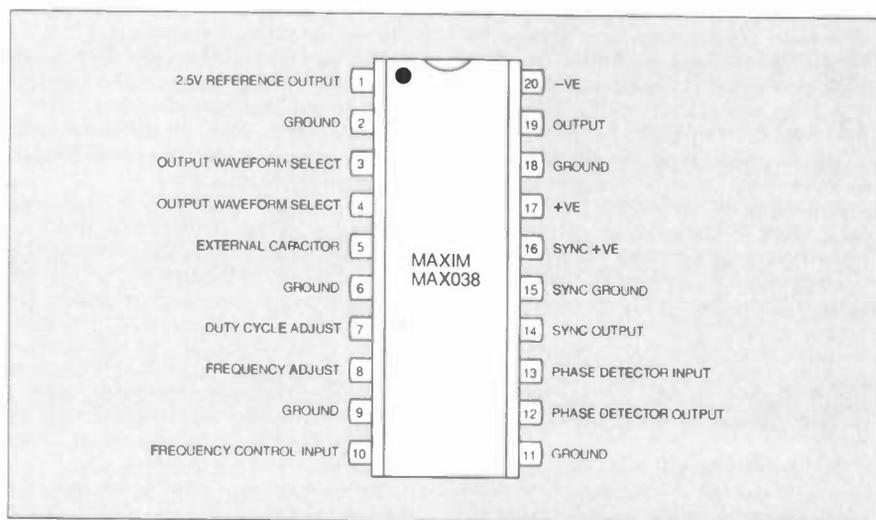


Fig. 1. Pinouts of the d.i.l. version of the MAX038.

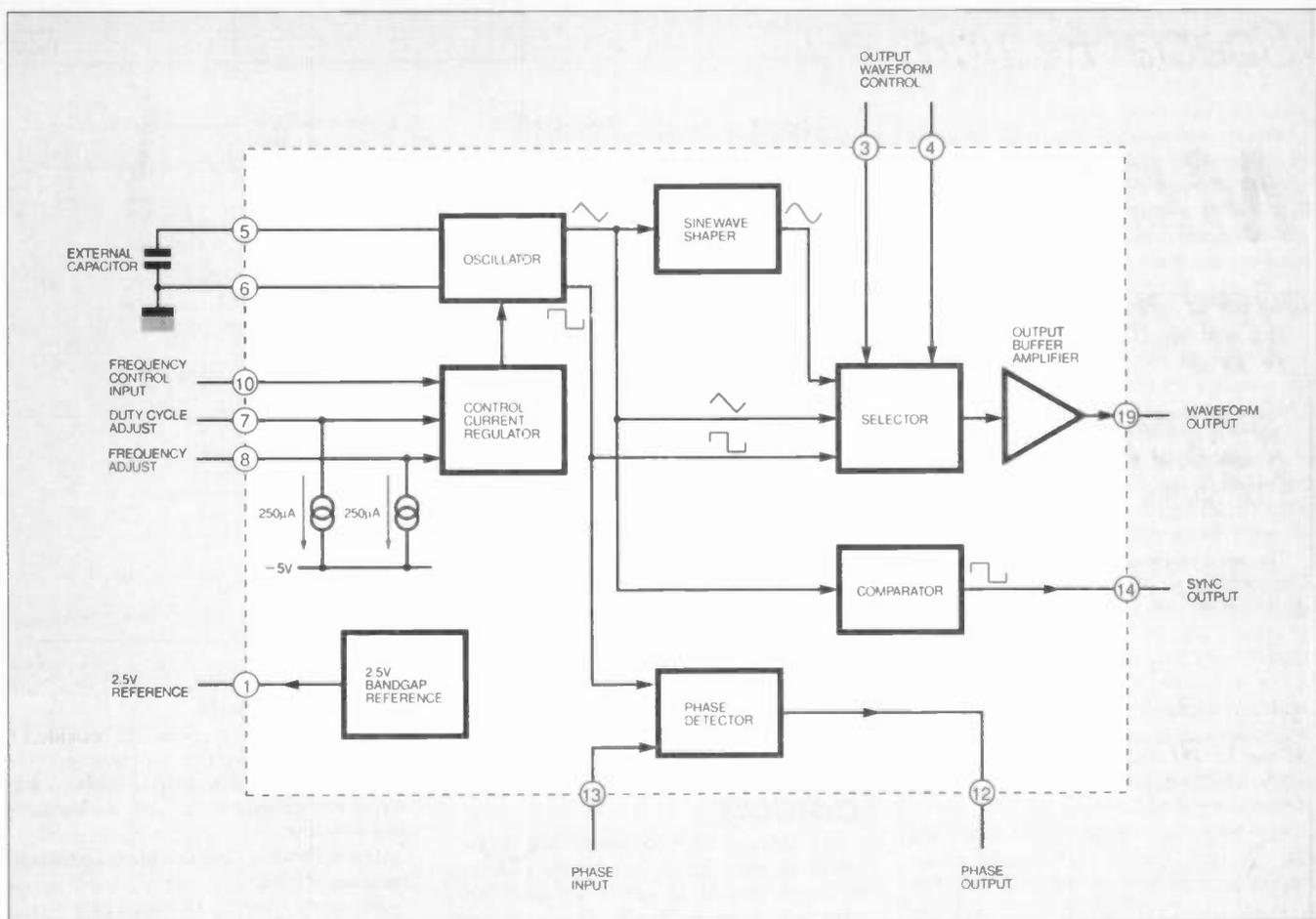


Fig. 2. Internal structure of the MAX038 waveform generator. Positive power supply input is at pin 17 and negative at pin 20.

connected to ground. Both supplies should be decoupled to ground by capacitors placed as close to the supply pins as possible. Maxim recommend the use of 1nF ceramic capacitors in parallel with 1µF tantalum bead types for decoupling.

They also suggest an alternative of 1µF ceramics, but these are large and expensive, so most designers will probably opt for the first combination.

Pins 15 and 16 are separate supply connections for the internal comparator for the sync output. If this is not needed, it can be disabled by simply leaving pin 16 unconnected, saving supply current and eliminating the possibility of stray coupling between the sync and main outputs.

It is necessary that pin 15 should always be grounded, however, otherwise the comparator will distort the triangle and sine outputs. If pin 16 is powered, a small series resistor of about 100 ohms should be used together with local decoupling capacitors.

## OTHER PINS

The functions of the remaining pins are as follows:

Pin 1 provides a 2.5V d.c. output from a bandgap reference source. The data sheet states that up to 4mA can be drawn from this output but, with two examples tested by the author, currents in excess of 1mA caused a voltage drop.

This is seriously bad news since the reference is also used by the i.c.'s internal circuits and dragging it down in this way causes severe waveform distortion and frequency changes.

The message is clear; either avoid using it, or buffer it with an op.amp. With a regulated positive 5V supply available,

most applications can use this instead. A small decoupling capacitor can be used between pin 1 and ground at pin 2.

Pins 3 and 4 are the output waveform selection inputs which should be held at ground (low) or +5V (high). Their input impedance is quite high, so they can be pulled high or low with 10kΩ resistors and enabled or disabled with very simple switching.

The easy way to follow their action is as follows: if both are low, the output is a squarewave; if just pin 3 is high, it is a triangle wave; but if pin 4 is high it will be a sine wave regardless of the state of pin 3.

Pin 5 is the connection for the external frequency determining capacitance. The other end of this is grounded and it should be placed as close as possible to pins 5 and 6. Many designs using pin 5 will have several frequency ranges provided by switching between suitable capacitors, so the wiring of this part should be kept as short as possible.

Pin 7 is for control of the output duty-cycle, or symmetry. It has an internal constant current "sink" to the -5V supply so it should never be left open circuit. If duty-cycle adjustment is not required, it can be connected directly to ground and the duty-cycle will then be almost exactly 50:50.

If it is needed, varying the voltage at pin 7 between ±2.3V will alter the duty cycle between 15 per cent and 85 per cent with little change of frequency. If this input is controlled through a resistor, the effect of the current sink must be taken into consideration, but it can be driven by a low impedance source, such as an op.amp output.

Pin 8 is for modulation or fine adjustment of output frequency. Its use is similar to that of pin 7 in that it also has an internal 250µA current sink and can be grounded if not required. Where it is used, compensation must be made for the effect of the sink. Varying this input between ±2.4V alters the nominal frequency by ±70 per cent.

## FREQUENCY CONTROL

Pin 10 is the main frequency control input. Current fed into this pin together with the value of the capacitor at pin 5 controls the output frequency, which can be calculated roughly from:

$$F \text{ (Hertz)} = I_{in} \text{ (amps)} / C \text{ (farads)}$$

which translates usefully to:

$$F \text{ (MHz)} = I_{in} \text{ (}\mu\text{A)} / C \text{ (pF)}$$

Although the input to pin 10 is a current, this input behaves in a manner sometimes referred to as a "virtual earth", meaning that whatever current is fed into it, its voltage is always zero or ground potential.

This means that if a resistor is connected in series with it, the input current will be directly proportional to the applied voltage, turning it into a linear voltage-controlled input. Values of input current can be from 2µA to 750µA, with a preferred range of 10µA to 400µA.

Pins 12 and 13 are the output and external input of an exclusive-OR type phase detector. This produces rectangular pulses from pin 12 having their width dependant on the phase of the external input, as compared to the internal one. These can

be converted to a d.c. voltage with a simple resistor and capacitor low-pass filter, and then coupled back to pin 8 to form a phase-locked loop for locking the frequency to an external signal.

Maxim recommend that both of these pins should be grounded if not used. This may sound odd for the output, but it appears to have only a limited current capability and grounding it probably helps avoid stray coupling to other parts of the circuit.

## OUTPUTS

The sync output from pin 14 is a logic level (ground to +5V) output for driving external circuitry, especially TTL or CMOS. It has very fast rise and fall times, so where it is used careful layout is needed to avoid stray coupling into the main output. If it is not needed, it can be left open-circuit together with the positive supply point for its comparator, pin 16.

The main output is provided at pin 19. This will be a sine, square or triangle waveform as selected by the levels applied to pins 3 and 4, and it always has an amplitude of 2V peak-to-peak.

The output has a very low internal resistance, a maximum of 0.2 ohms is quoted, and it can supply up to 40mA. This allows the use of low-impedance following circuitry which makes it easier to maintain performance at high frequency.

Typically, the output may be connected into a 1k $\Omega$  carbon potentiometer for amplitude control, followed by a very fast amplifier having sufficient gain to achieve the maximum amplitude required.

## TEMPERATURE COEFFICIENT

One special operating mode is worth mentioning. Apparently the internal frequency adjusting circuit behind pin 8 adds a small temperature coefficient to the operating frequency. If this pin is grounded through a 12k $\Omega$  resistor, the internal current sink will develop -3V at pin 8, which causes the internal circuit to disconnect itself.

This has two effects. Firstly, the temperature coefficient is improved. Secondly, the output frequency set by the input current and external capacitor is doubled, although the manufacturer hastens to point out that this does not double the ultimate output frequency of which the i.c. is capable! Most applications probably will not be critical enough to need this mode, however.

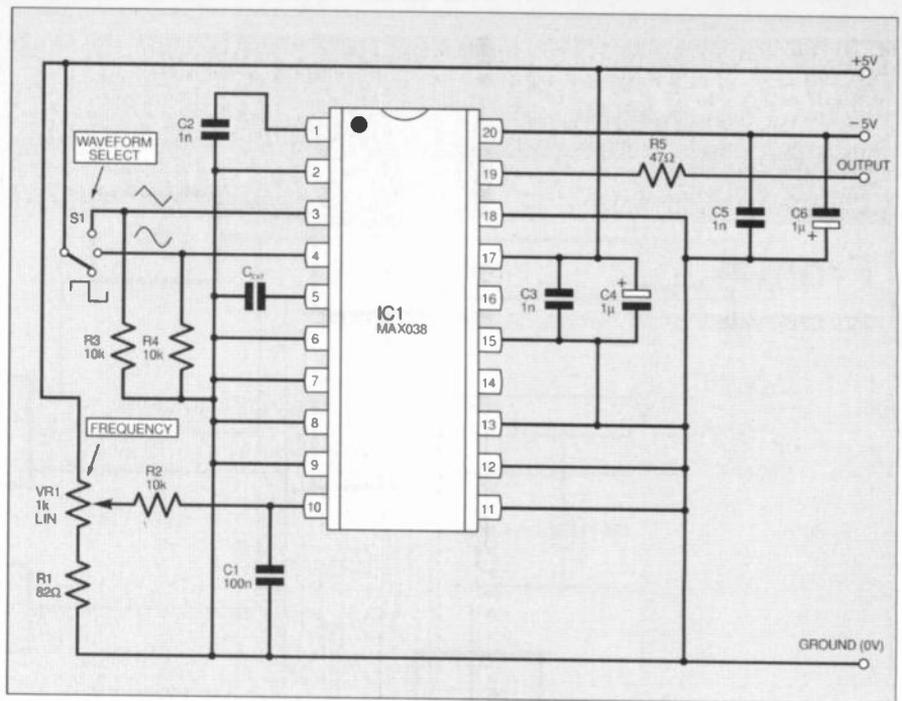


Fig. 3. Experimental circuit using the MAX038.

## EXPERIMENTAL CIRCUIT

For enthusiasts who would like to experiment with this device for themselves, a simple circuit to get it up and running is shown in Fig.3. The only real problem with the MAX038 is that inherent in its sheer speed. Breadboarding can be difficult as stray coupling and reflected signals in mismatched bits of wire can produce all sorts of odd effects.

Whilst these usually disappear when the circuit is rebuilt with a good printed circuit board layout, it is possible that other more serious design defects will actually have been masked by them! This may lead to more trial and error than usual when working with this device.

Maxim suggest careful layout on a double-sided ground-plane p.c.b. for best results. In practice, a single-sided p.c.b. seems to work well, providing it has plenty of copper areas at ground potential, good decoupling and guard tracks around signal paths carrying rectangular waveforms, especially that from the sync output.

Such effort is well worthwhile, since circuits having far greater performance

than those constructed with older waveform generator i.c.s are undoubtedly now possible.

The following component recommendations are offered:

Resistors - 0.6W, 1% metal film

C1, C2, C3 and C5 - ceramic disc

C4 and C6 - tantalum bead, 35V

C<sub>ext</sub> - as required for frequency, between 47pF and 4 $\mu$ 7F, polyester or polystyrene.

## SOURCE

MAX038CPP waveform generator i.c.s can be obtained from RS Components (trade only - tel: 01536 201201) or Electromail (retail outlet for RS - tel: 01536 204555), order code 810-396.

It is also available from Maplin (tel: 01702 554161) order code DT25. Maxim will also supply it directly against credit card orders (tel: 01743 303388).

## NEXT MONTH

A practical and very versatile 10MHz waveform generator project using the MAX038 will be published in our October issue.

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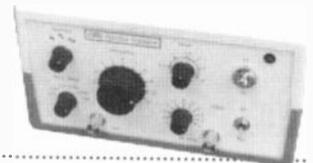
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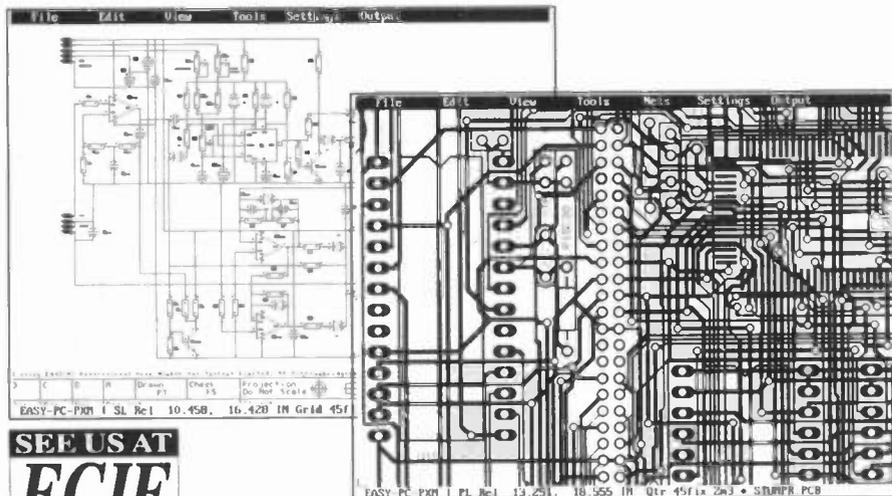
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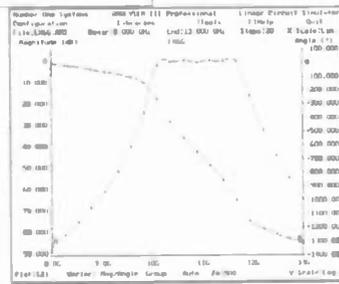
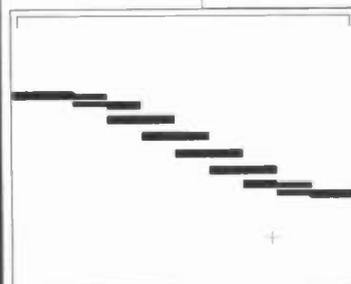
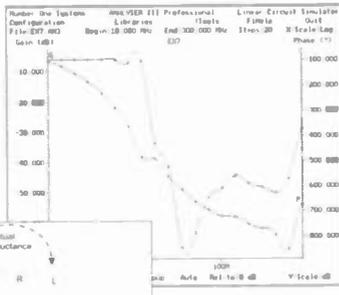
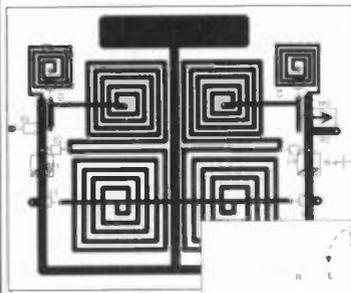
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# FOX REPORT

by Barry Fox



## Reality of Stonehenge

Exactly as the marketing pundits predict, the Internet is turning into a marketing tool. Goods, services, magazines and entertainment are all on offer. Sometimes you pay to receive, other times you are getting advertisements for something that someone is trying to sell.

The most exciting claims and promises are made by people who have never actually set up a PC, connected to the Internet and downloaded data. If they had rolled up their sleeves and done it themselves, they could never deliver their spiel with a straight face.

English Heritage looks after Stonehenge and has tied up with Intel and Californian software company Superscape to put a "virtual reality" Stonehenge model on the Internet.

"Millions of people round the world will be able to walk virtually through the stones" promised EH Chairman Sir Jocelyn Stevens, and EH archeologists when the system was launched at the London Planetarium.

The demo did look impressive, as well it should have done. The computers used were £20,000 Intergaphs, with ganged pairs of 200MHz Pentium processors and 128MB of RAM. The Internet site was coming from a hard disc, not down a phone line.

But by being a bit pushy I did get a demo from a laptop, connected to the Internet site ([www.intel.com](http://www.intel.com)) by phone line and 28-8K modem. It worked very well because Superscape's Viscap software plays a clever trick. Instead of relying on a constant flow of graphics data down the line, it downloads a VR model into the PC and then needs only nibbles of data to control motion.

## Fit of Peak

That night I tried it at home. In fact I tried night after night for several weeks. Getting the system up and running is, I would guess, comparable to climbing Mt Everest with one leg tied behind your back.

Stonehenge works only on a Windows PC, not an Apple Mac. You can of course thank Intel's involvement for that. Superscape's Viscap software will only work with the Netscape Web Browser. Tough luck if you have Mosaic (e.g. if you use CompuServe) or Microsoft's Explorer (e.g. you are on the Microsoft Network).

If you know what you are doing, you should be able to dial into the Internet using either of these services, and then overlay Netscape. This works with MSN but not CompuServe.

The one man I found inside the whole of English Heritage who has actually set up the system himself (and not

surprisingly he's in charge of EH's office computer network) thinks this is something to do with "routers being too clever".

You cannot buy Viscap on a disc. It is still in Beta version. So you must download it from Superscape's site on the Internet. This took me half an hour, even on an ISDN line. So expect it to take over an hour on an ordinary line.

Viscap will only "plug into" Netscape Version 2 or later. Last year's Ver 1.2 is no-no. So that's more downloading to do, or more discs to buy.

If you are running Windows 3.1 you will need the 16-bit version, but Windows 95 needs 32-bit. Viscap then needs the Win 32s software extension if you have 16-bit Windows 3.1.

(I hope this is all clear, because I shall be asking questions at the end!)

## Games On The Line

For game playing, E-ON, "Entertainment On-Line", promises game play from the Internet ([www.e-on.com](http://www.e-on.com)) "for as little as £5.99 per month".

Subscribers get the chance to play "a range of hit games, including the very best from ... Sony/Psychosis, Virgin, Gametek, US Gold and Gremlin Interactive". Founder Mark Bernstein said at the UK launch in July, that the system is "as easy to use as a TV".

But this claim rang rather hollow after the show biz presenter had gone through a long puff about "doing it live, down a phone line through a modem", when the on-screen demonstration was very clearly coming from a disc. Backed by a team of experts controlling the computers he finally plucked up courage to go live on-line. Surprise, surprise, the system crashed.

Fortunately a row of PCs set up elsewhere in the room were all working live on-line, through consumer modems. Game play, for instance on *Tank Warrior*, looked surprisingly smooth.

## Childs Play

"Yes, but wait and see what happens if the service is successful, and several thousand kids are all trying to access the service on Saturday morning", said one industry consultant.

Perhaps more to the point, what happens when parents start getting the bills that their kids are running up by playing games on-line, rather than off ROM disc?

The £5.99 per month subscription fee only applies if the subscriber uses one of the Internet services with which E-ON has deals. These include America On

Line, Easynet, UK OnLine and Pipex Dial.

Just to make sure you are concentrating, Superscape has wrongly labelled the Viscap file that comes down the line. So when the instructions say Run Runme.exe, they actually mean Run Runme106.exe.

After literally weeks of carefully following instructions, spotting the Runme error and getting error messages like "Netscape not found", I finally did something wrong and got a sight of Stonehenge on my PC screen.

By then I had lost all interest in the system and wanted only to lock all EH's top management into a room with a few PCs and not let them out until they either visited Stonehenge or admitted that the system was as ready for launch as a car with the engine still packed as a kit of parts.

If the game player goes through any other service provider, for instance CompuServe, the price rises to £9.99 per month. Internet service providers charge at least £10 a month, often nearer £15, or up to a couple of pounds an hour after a few hours free time per month.

Then there is the cost of making the local BT call into the Internet. If the calls are made over the weekend, then the price is 60p per hour. On weekday evenings BT charges 5p for every three minutes, which is £1 per hour. If the kids are on school holiday, playing games during the day at BT's local peak rates, the cost is 5p per 75 seconds, which works out at £2.40 per hour.

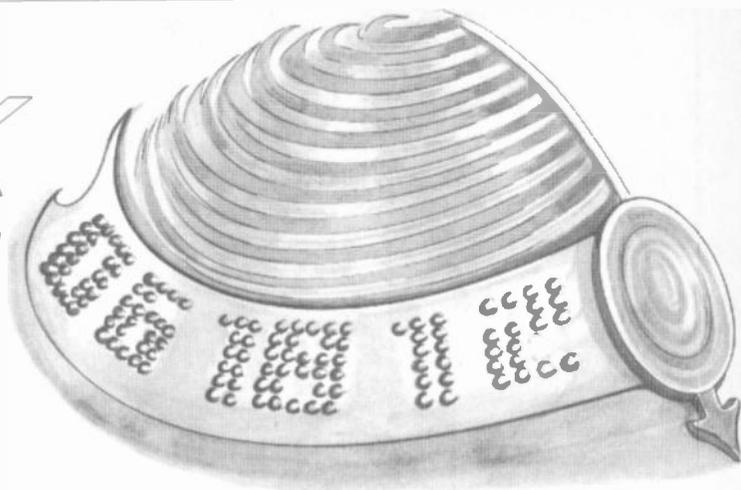
Once you have subscribed and before you play games, you must download a large file of control software. E-ON warns that this will take 45 minutes even with a 28-8k modem. But at least this is a one-off load.

## Paying the Price

Once up and running, a game addict can easily run up local call charges of £10 a week. Add to that at least £10 a month for Internet access plus at least £6 for the E-ON subscription, and you start to get a feel for the kind of money involved in accessing on-line entertainment services.

You also see why so many companies are now trying to get a slice of the action. But with so many companies looking for slices, a lot of them must fail. No-one knows who, which is why so many are trying to find a place on the bandwagon.

# PIC-TOCK PENDULUM CLOCK



**JOHN BECKER**

*Have a swinging time building this "magic" clock!*

**T**HERE is no denying it, the PIC-Tock Pendulum Clock is simply a novelty! Blatantly, there are much easier ways of telling the time, most of us wear them on our wrists, or mount them on the wall. But why do things the dull way if there's a more fun way of doing them?

First design thoughts were about how the PIC-Tock could be made different to the two inspirations. As will be seen, the principal difference is that the PIC-Tock uses a suspended pendulum display. It is also programmed as a 24-hour clock.

The *Spacewriter* referred to above is a handheld "wand" waved in front of an awe-struck viewer who sees the message "MERRY XMAS" drawn in light across space. The *Science Museum* design also consists of a wand. This, though, is mounted on a stand and pivoted at the base. When the wand swings, the lighted message drawn in space shows the current time.

These are seemingly astonishing feats, since each wand is simply a tube containing a single column of light emitting diodes. When stationary, there appears no way that they could show a message.

## PERSISTENT VISION

The answer lies in the phenomenon that led to the creation of the cinema, persistence of vision. The human eye "stores" an image briefly beyond the point at which the image source is removed. This can be illustrated by the large X in Fig. 1.

With the page you are now looking at well lit, hold it in your hand and stare at the X. Now close your eyes quickly. You should find that for a second or two, and sometimes longer, the image of the X remains "trapped" in the eyes. If the X is sufficiently well lit, its latent image can almost be "studied" while your eyes remain closed.

The image will quickly fade as the retina nerves of the eyes return to normal.

**Scene:** EPE HQ – Editor's office.

**On the desk:** *EPE* December '94 open at *Spacewriter* messagemaker, and *Science Museum* catalogue advertising lever-arm clock.

**J.B.** (queryingly): "Which, perhaps, inspired the other?"

**M.K.** (knowingly): "Neither, the principle's historic."

**J.B.** (memorably): "Ah!"

**M.K.** (suggestively): "Could you design a spacewriter clock?"

**J.B.** (technically): "Probably..."

**M.K.** (directorially): "Do it!"

So began a train of thought that led to the *PIC-Tock Pendulum Clock*.

Blinking the eyes open and closed again repeats the process. If eyelids could move fast enough, repeated rapid blinking would give the brain the sensation that the eyes are viewing a scene continuously with no intervening periods when it is shut off by the eyelids.

Eyes can't actually blink that fast and so a flickering scene of alternate brightness and semi-darkness is experienced. However, with eyes remaining open, if the room light is turned on and off more rapidly than the retina nerves allow the scene to fade, a continuous viewing of the scene will be experienced.

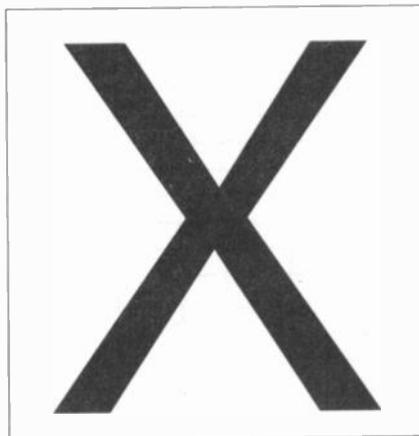


Fig. 1. Using the letter X to demonstrate "persistence of vision".

This is precisely the way that a cinema film projected onto a blank surface is viewed as a moving image, except that it is a shutter that turns the projector light on and off. On each occasion, a different stationary image is projected and any positional differences between consecutive images of almost identical scenes are seen as movement.

The *Spacewriter*, the *Science Museum Clock* and the PIC-Tock wands are designed so that when they are moved through an arc, the lights flash in different patterns at each position through the arc. Retaining the image of each pattern flash, the viewer's

eyes are made to believe that the sequence of flashes is one long flash in which the several patterns are simultaneously seen as a coherent message.

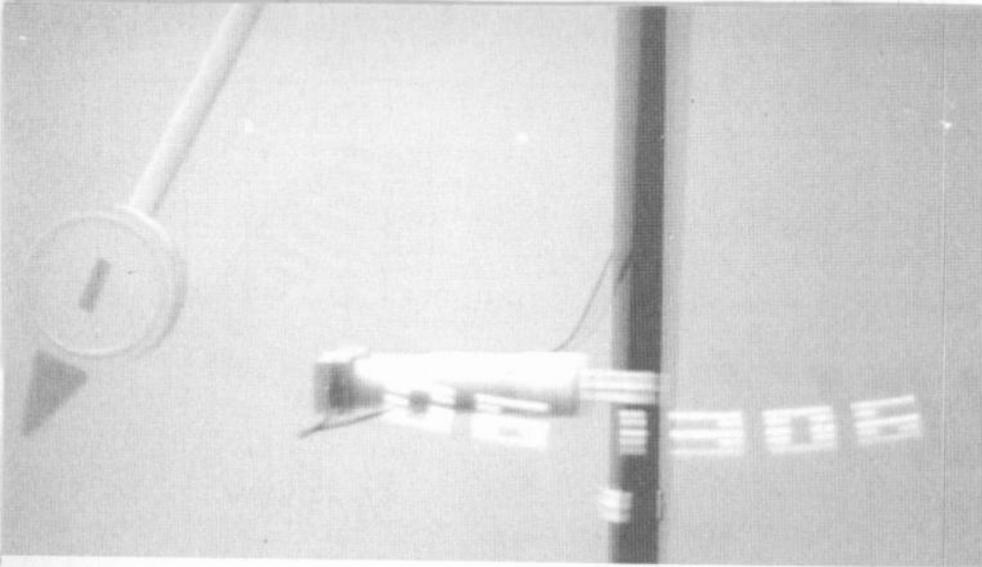
## LIMITATIONS

The patterns could be arranged to show any simple message, whether it is in text or numbers. Even a simple picture could be "drawn" by a wand with enough lights. Vertically, there is no limit to the number of lights that can be used to make up the pattern, other than that imposed by practicality.

Horizontally, though, the number of flashes that can occur is dictated by the time between the start of the sequence and its end. Too long a time will result in the eye "forgetting" the starting pattern before the ending pattern is shown. Effectively, the total period should last for no more than about a *quarter* to *half* a second.

There are also limits to the distance between the positions of the starting and ending patterns. Too short a distance and the images will be too closely superimposed for the overall pattern to be distinguished. Too long a distance will result in each pattern flash appearing as streaks of light, again making the overall pattern difficult to interpret. Also, with a lengthy swing, the eye tries to follow the lights and so the effect is lost, all that is seen is a vertical line whose individual segments are flashing.

Obviously, then, these practicalities constrain the amount of data that can be



Swinging the pendulum past the infra-red beam triggers the time in "thin air".

conveyed by a horizontally moving sequence of flashing lights arranged as a single vertical column.

With the *Spacewriter*, the message had to be restricted to show "MERRY XMAS" rather than "MERRY CHRISTMAS". To simply tell the time, however, a six-digit number is perfectly readable, two digits for hours, two for minutes and two for seconds.

Thus, the technique is well suited to use as a clock display, as the PIC-Tock Pendulum Clock proves.

## MICROCONTROLLER

The complete circuit diagram for the PIC-Tock Pendulum Clock is shown in Fig. 2. As can be seen, there is not a lot to it! Most of the work is done by the PIC16C84 microcontroller, IC1, and the software programmed into it.

This particular microcontroller is the EEPROM version of the PIC family manufactured by Arizona Microchip. It has previously been described in two *EPE* articles, the *Simple PIC16C84 Programmer* and the *PIC-Electric Meter*, both in the February '96 issue. (We regret that this issue is now completely out of print and only photostat copies of these articles are available - see page 722 - Ed.).

Being an EEPROM (Electrically Erasable Programmable Read Only Memory) device, the PIC16C84 can be repeatedly reprogrammed several thousand times. It does not need to be erased by ultra-violet light between each reprogramming routine.

It contains two input/output ports, the first having five lines, RA0 to RA4, the second having eight lines, RB0 to RB7. Any of the lines can be set through software as an input or output. As discussed in the manufacturer's data book, some of the lines can be used as interrupt inputs, although this fact is not taken advantage of in PIC-Tock.

The device can be software-configured for any one of four oscillation modes:

- RC Resistor-capacitor oscillator
- XT Standard crystal/resonator (100kHz to 4MHz)
- HS High-speed crystal/resonator (4MHz to 10MHz)
- LP Power saving low frequency crystal (32kHz to 200kHz).

Here, the XT mode is used, in which the oscillation frequency is generated around the 3.2768MHz crystal X1, in conjunction with capacitors C2 and C3, and resistor R6.

## COUNTING TIME

Using an internal counter, the 3.2768MHz master frequency is subdivided to trigger a register flag at intervals of approximately 100th of a second. The precise count is varied periodically during the software routines to compensate for manufacturing tolerances of the exact crystal frequency.

Each time the register flag is triggered, counters representing seconds, minutes and hours are incremented as appropriate, as happens in an ordinary digital clock.

## SEGMENTED TIME

The contents of the clock counters are converted to a format suitable for driving the five l.e.d.s (light emitting diodes) D1 to D5. Using an internal look-up table, at each 100th of a second count, the format is determined by which portion of the time is to be shown.

There are six digits associated with the time display: units of seconds; tens of seconds; units of minutes; tens of minutes, units of hours and tens of hours. Since the l.e.d. pattern displayed has to also take into account the fact that the time has to be viewed while the pendulum is swinging, each digit has to be split into vertical segments.

PIC-Tock has been designed so that the time is displayed when the pendulum swings from left-to-right. Consequently, the vertical segments of the digits must also be turned on and off in the same order.

For the sake of simplicity in this design, the digits have been split into three vertical segments, each consisting of five l.e.d. bits, as illustrated by the ten digits represented in Fig. 3.

The l.e.d.s are turned *on* when the output port line is taken "low", shown as a zero (0), and *off* when the line is "high", shown as a one (1). For clarity, the outline of each number is represented by the black trace line in the 15-bit block.

Take digit zero (0), for example. The left hand column of the digit consists of five (0)s, therefore the l.e.d.s show a vertical line when this format is output to them.

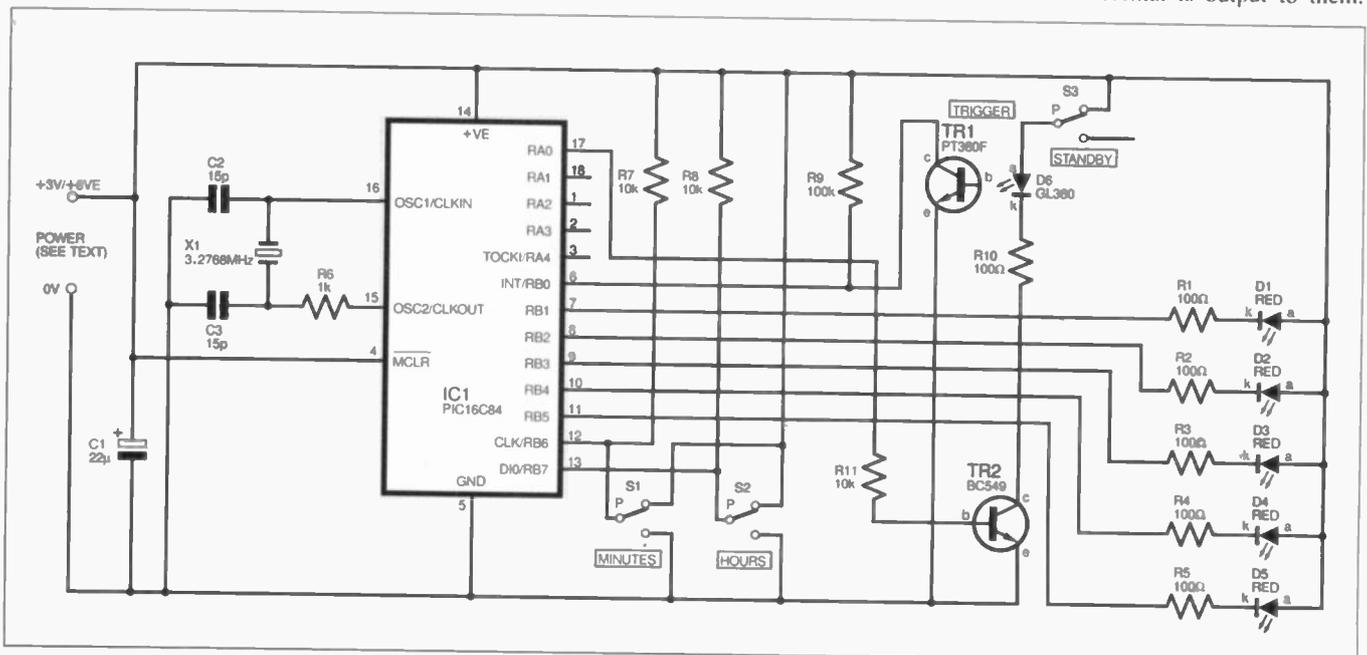


Fig. 2. Complete circuit diagram for the PIC-Tock Pendulum Clock. Note that switch S3 is optional.

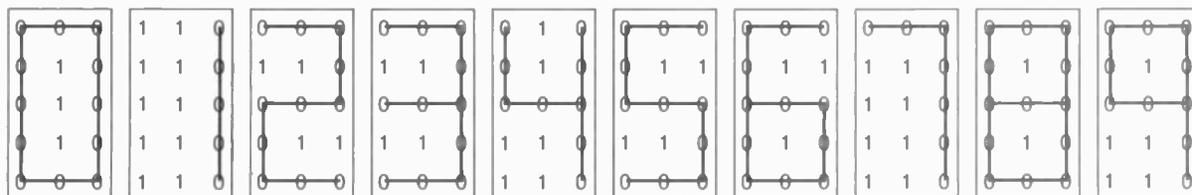


Fig. 3. Logic formatting sequence for producing the numerals zero to nine using five l.e.d.s.

In the second column, only the top and bottom l.e.d.s are turned on for this output format. Column three is the same as column one, a vertical line.

When these columns are triggered in sequence during the pendulum swing, because of "persistence of vision", the eyes respond as though they have simultaneously seen a left hand vertical line, top and bottom horizontal lines and a right hand vertical line. In other words, the outline of a zero (0) will be seen.

Studying the other blocks in Fig. 3 shows how the digits one to nine are similarly made up. For other applications, the bit patterns could be changed so that letters of the alphabet are displayed, although they would need to be a mixture of upper and lower case characters, and not all could be realistically generated using a 3-bit by 5-bit pattern.

When several digits are displayed consecutively, the program inserts a blank between them by momentarily turning off all the l.e.d.s.

## SYNCHRONISATION

Obviously, the commencement of the time display sequence has to be synchronised to the pendulum swing. This is achieved by using an infra-red (IR) emitter and sensor pair. The IR emitter, diode D6, is placed at a fixed point to the left of the pendulum's vertical rest position. The sensor, TR1, is housed in the circuit box mounted at the end of the pendulum.

When the pendulum is at rest, sensor TR1 cannot detect the infra-red output from the emitter D6. However, when the pendulum is swinging, each time the sensor crosses the IR beam emitted from D6, a logic 0 (low) pulse is generated across resistor R9.

Through port line RB0 (IC1 pin 6), software continually monitors the logic status at the junction of resistor R9 and collector (c) of transistor TR1. When a logic 0 pulse is detected, the l.e.d. display routine is started.

Once triggered, the display routine triggers the l.e.d.s appropriately until all six clock digits have been displayed, at which point they are turned fully off until the next trigger pulse is received. Each l.e.d. pattern is turned on for 100th of a second, the whole sequence taking approximately 0.2 seconds.

## L.E.D. SWINGING

In operation, the pendulum is first pulled, by hand, beyond the left of the emitter diode D6 position. It is then released and the display sequence is triggered as soon as the swing takes the sensor left-to-right past the emitter diode

D6. The sequence is displayed fast enough so that it is complete before the pendulum reaches the end of its swing.

Now under control of gravity, the pendulum swings back, right-to-left, past D6 towards its release position. It then again swings from left-to-right, once more triggering the display routine. The process is repeated for as long as the pendulum's energy can take it back past the infra-red emitter.

Each swing, of course, is shorter than the last, and so the display width is seen to shrink in size. Its height remains the same, though. Eventually, the swing becomes too short for the display to be triggered, and the pendulum gradually comes to rest.

Unavoidably, each time the sensor passes the emitter on the return swing from right-to-left, the display sequence is again triggered, resulting in a flipped-over (backwards) view of the time.

Early on in the design, attempts were made to write the software so that the display would not be triggered on the return swing. The results proved to be unreliable, caused by the system's uncertainty about the triggering phase when the pendulum's energy only just managed to bring it within the vicinity of the emitter's beam.

Whilst the use of an additional sensor to detect swing direction could have overcome this problem, the extra complexity and current consumption was felt to be unjustified.

Anyway, as PIC-Tock is a novelty clock, backwards viewing of the time can be regarded as part of the novelty! Indeed, by mounting the emitter diode D6 near the pendulum's rest position, rather than well to one side, the effect can be set so that both viewing directions can be seen for similar lengths of time.

## ENERGY SAVING

The "clock" may be powered from any d.c. power source, either regulated or from a battery, between 3V and 6V. In order to save power while it is not being viewed, two design features have been included, one software, the other mechanical.

The software aspect causes the infra-red emitting diode, D6, to be turned on only very briefly at each 100th of second. At this time, output line RA0 (IC1 pin 17) is taken high, switching on transistor TR2, which in turn switches on D6. The turn-on period is just slightly longer than the pulse width needed for the sensor TR1 to satisfactorily respond to the infra-red beam.

This technique cuts down the long-term power consumption by D6, to nearly one hundredth of that if it were constantly turned on. As limited by resistor R10, it draws around 30mA from a 5V supply.

Secondly, an optional Standby switch, S3, has been included so that D6 can be

switched off for extended periods when the clock does not need to be viewed.

With a supply of 5V, power consumption is approximately 1.7mA when all the l.e.d.s are turned off. When turned on, each l.e.d. draws about 25mA to 30mA.

## TIME SETTING

Initial setting of the time is done by switches S1 and S2. Once per second, software monitors port lines RB6 and RB7 (IC1 pins 12 and 13). With the switches in the Off position, a logic 1 (high) is present on both lines. If either switch is turned On, the corresponding port line goes low (logic 0).

When this fact is detected, the relevant minutes or hours counter is incremented by one. When the hours counter reaches 24, it resets to zero. The minutes counter resets to zero when it reaches 60. Each time the minutes are incremented, the seconds are reset to zero.

While either counter is being incremented, the l.e.d.s are turned on and display the logic values of the counter's

## COMPONENTS

### Resistors

R1 to R5,		
R10	100Ω (6 off)	
R6	1k	
R7, R8,		
R11	10k (3 off)	
R9	100k	

All 0.25W 5% carbon film or better.

### Capacitors

C1	22μ radial elect., 16V
C2, C3	15p polystyrene (2 off)

### Semiconductors

D1 to D5	min. 3mm red l.e.d. (5 off)
D6	GL380 infra-red emitter diode
TR1	PT380F infra-red receiver transistor
TR2	BC549 npn transistor
IC1	PIC16C84 EEPROM microcontroller (see text)

### Miscellaneous

X1	3.2768MHz crystal
S1 to S3	min. s.p.c.o. toggle switch (3 off)

Printed circuit board, available from the EPE PCB Service, code 109; 18-pin d.i.l. socket; plastic circular box, 68mm diameter x 26mm deep (see text); diecast box, size 89mm x 34mm x 26mm; materials for pendulum and support (see text and Fig. 5 to Fig. 7); connecting cable and wire; solder, etc.

Approx Cost  
Guidance Only

£19

excl. hardware

first five bits, confirming that the count is being changed. The l.e.d.s remain on briefly after the controlling switch has been turned off.

If both switches are on together, priority is given to the Hours switch S2, the Minutes switch S1 being ignored.

### TIMING ACCURACY

In theory, the crystal X1 should oscillate at its stated frequency, in this case 3.2768MHz. In practice, it probably will not.

This is due to several factors, such as the manufacturing tolerance, the load imposed on it by IC1, the capacitance values of C1 and C2, and temperature. All of these factors can affect the accuracy of any real-time clock.

The software has been written so that, with the exception of temperature, the disruptive factors can be compensated for.

At first, it had been assumed that by making either C1 or C2 a variable capacitor, the crystal frequency could be trimmed with fair precision. For reasons unknown, and despite experimenting with various component values and configurations, it was found that the inclusion of a variable capacitor could actually cause the oscillator to become unstable. Consequently, it was omitted from the final design and compensatory parameters were written into the software instead.

These parameters involve periodically changing the primary count length from the basic value of 100, to a value above or below it, as appropriate. For example, to perhaps occasionally count to 99 or 101 before incrementing the seconds count. This count change can be applied after so many seconds or minutes or hours, or at intervals involving all three.

Whilst it would have been possible to add additional switches to set the compensatory values while the clock was running, this would have severely increased the software complexity. It would have also required additional wires to be run up through the pendulum arm to the control box at its head. This could have proved difficult because of the restricted width of the pendulum tube.

Consequently, a less-than-ideal compromise has been adopted, which requires the microcontroller IC1 to be programmed twice. Once for an initial run of about 24 hours, and then again with compensatory values having been written into the source code when the clock's actual rate is known.

### Listing 1: Correction Calculation Program

```

10 REM PICCALC4 - PIC-TOCK PENDULUM CLOCK CALCS 30DEC95
20 XTAL=3276800!:REM CHANGE THIS NUMBER FOR ANY FUTURE CORRECTION CALC
30 CLS:LOCATE 4,1:PRINT"IS CLOCK RUNNING FAST OR SLOW [F/S]?"
40 A$=INKEY$:IF A$<>"f" AND A$<>"s" THEN GOTO 40
50 IF A$="f" THEN A$="FAST":F=-1:ELSE A$="SLOW":F=1
60 PRINT "BY HOW MANY SECONDS ";A$;" IN 24 HOURS":INPUT B$:S=VAL(B$)*F
70 T=60*60*24:B=S+T:E=B*100/T:XTALERROR=XTAL-((E*XTAL)/100)
80 XTAL=XTAL+XTALERROR:CLK=XTAL/4:SCALE=CLK/32:RTCC=SCALE/256
90 DIV=32768!:PRINT:PRINT "XTAL IS RUNNING AT";XTAL;"Hz"
100 PRINT"MAKE A NOTE OF THIS NUMBER IN CASE FURTHER CHANGE NEEDED"
110 B=INT(XTAL/(DIV*100))*(DIV*100):C=(XTAL-B)/(DIV*100)*T
120 SECERROR=XTAL:ERRORTOTAL=XTAL:DAYMULT=100*T:PRINT
130 MULT=1:A$="EACH 1 SEC=":B$="1ST":C$="CLKCNT":GOSUB 210
140 CLKCNT=SECCORRECT
150 MULT=60:A$="EACH 1 MIN=":B$="2ND":C$="MINCRT":GOSUB 210
160 MULT=60:A$="EACH 1 HR =" :B$="3RD":C$="HRSCRT":GOSUB 210
170 MULT=24:A$="EACH 1 DAY=":B$="4TH":C$="DAYCRT":GOSUB 210
180 PRINT"XTAL PULSES YEAR ERROR":DAYERROR*365:PRINT
190 PRINT"NOTE THE 4 ($..) NOS & SET SOURCE CODE FILE ACCORDINGLY"
200 PRINT:END
210 SECERROR=ERRORTOTAL*MULT:SECCORRECT=INT(SECERROR/DIV)
220 C=SECCORRECT*DIV:ERRORTOTAL=SECERROR-C:DAYMULT=DAYMULT/MULT
230 DAYERROR=ERRORTOTAL*DAYMULT/DIV:HEXFACT=CLKCNT+SECCORRECT
240 PRINT"ERROR AFTER "B$;" CORRECTION =" :ERRORTOTAL;"XTAL PULSES"
250 PRINT "CORRECTION ";A$;SECCORRECT,"SET "C$=" $";HEX$(HEXFACT)
260 RETURN

```

Regrettably, this technique means that only readers who have a suitable PIC16C84 programmer can build the time corrected PIC-Tock Pendulum Clock, since it is not practical to arrange a commercial double-programming source for the chip. However, the inexpensive *Simple PIC16C84 Programmer* previously mentioned is ideal for the job and can be used by anyone having access to a PC-compatible computer.

### SOFTWARE

The software source and object codes for the PIC-Tock Pendulum Clock are available on a 3.5in disk from the *EPE* Editorial offices for £2.50 (overseas £3.10 surface, £4.10 airmail). Prices include postage. Or download (free) from our Internet site: [//ftp.epemag.wimborne.co.uk](http://ftp.epemag.wimborne.co.uk).

### CORRECTION CALCULATION

To establish the correction factors needed, the program in Listing 1 should be used. It can be run from GW-Basic or QuickBasic.

First, the microcontroller IC1 is programmed with the correction factors set to a default value already written into its source code. These factors assume that the oscillator is running at precisely 3.2768MHz and that no correction is needed.

The clock is now run for a reasonable period, say 24 hours, and the number of seconds that it has gained or lost

during that time noted. If the period is not exactly 24 hours, calculate the number of seconds that would be gained or lost in 24 hours. Decimal places are permitted.

Run the Correction Calculation Program. It will ask whether a gain or loss has occurred and then ask for the number of seconds by which the clock is wrong. It then calculates correction values which will be actioned at the end of four strategic intervals: every second, every minute, every hour, and every 24 hours.

The resultant values are shown in hexadecimal alongside the name of the program variable to which they relate. Note them down, then from the normal software used for writing text, substitute the values into the PIC-Tock source code (the section to look for has the label PUTCRT:)

For example, the default values are:

CLKCNT = \$64, MINCRT = \$64,  
HRSCRT = \$64, DAYCRT = \$64

and the substitution values might be:

CLKCNT = \$64, MINCRT = \$68,  
HRSCRT = \$91, DAYCRT = \$75

The section of source code which needs changing is shown in Listing 2, in which the default and example substitution values are tabulated.

Save the source code file, and then assemble it into an object code file (.OBJ) in the usual way. After which, reprogram the chip from this file data.

Should the clock precision later be found to be still fractionally wrong, the process can be repeated. This can be done by adding the original and later error values together and calculating accordingly.

Alternatively, when the first calculation is done, note the quoted crystal rate as calculated and shown, then substitute its value in place of the original default crystal value (XTAL = 3276800!) in the Basic program.

**Listing 2:**  
**Section of source code (label PUTCRT:) showing default and example correction timing values.**

DEFAULT CODE	CODES VAL/REG	CORRECTED CODE	CODES VAL/REG
MOVW	\$64	MOVW	\$64
MOVWF	CLKCNT	MOVWF	CLKCNT
MOVWF	CNTVAL	MOVWF	CNTVAL
MOVW	\$64	MOVW	\$68
MOVWF	MINCRT	MOVWF	MINCRT
MOVW	\$64	MOVW	\$91
MOVWF	HRSCRT	MOVWF	HRSCRT
MOVW	\$64	MOVW	\$75
MOVWF	DAYCRT	MOVWF	DAYCRT

Now just the latest clock seconds error (still over a 24 hour period) can be used to calculate the new correction factors.

## CONSTRUCTION

Details of the printed circuit board (p.c.b.) topside component layouts and full size copper foil track masters are shown in Fig. 4. This board is available from the *EPE PCB Service*, code 109.

Commence construction by using a small hacksaw to separate the board into its three sections: the main board; the infra-red sensor board and the unused section. If using the suggested box, trim off the corners of the main p.c.b. as indicated to allow it to fit inside the box. The four drilled holes at the corners of the p.c.b. are to ease mounting in other boxes.

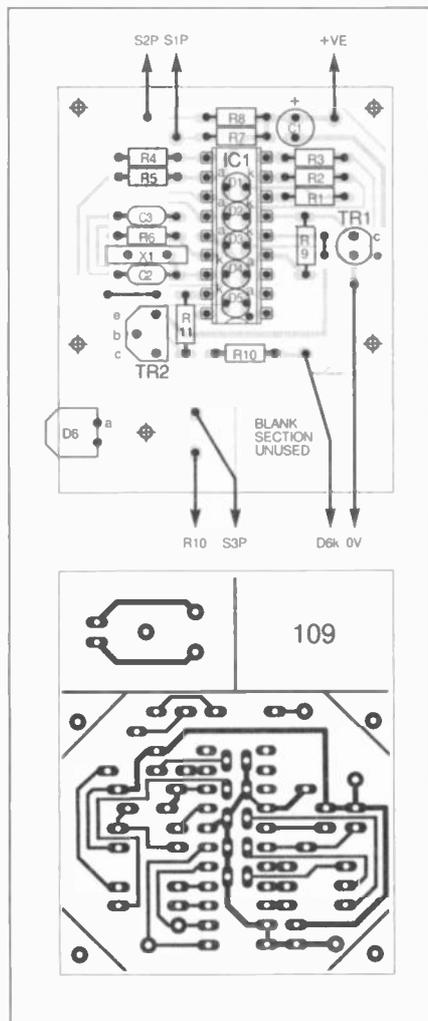
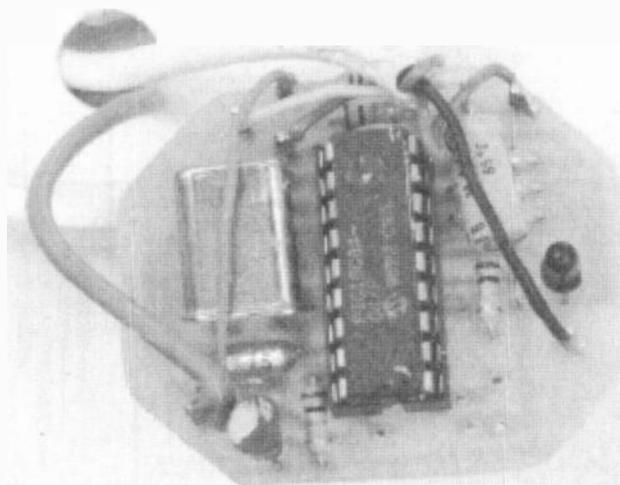


Fig. 4. Printed circuit board component, layout and full size p.c.b. foil master. This board is cut to produce two p.c.b.s.

Now assemble the main board. The i.e.d.s D1 to D5 are mounted on the *track side* and should be dealt with first. From the track side, push their leads into the holes as far as they can go, making sure that their polarities are correctly positioned.

With a small-tipped soldering iron, *carefully* solder them to their track pads. Just solder one side first, allowing them to be properly aligned before soldering the other side. Trim off the excess lead lengths, on the topside, very close to the board.

Fit the i.c. socket, two small on-board link wires, resistors and capacitors C2 and C3. Mount capacitor C1 (correctly polarised) and crystal X1 so that their



Completed main printed circuit board showing the crystal and small radial electrolytic carefully mounted vertically over the other components.

bodies lie flat across their neighbouring components, see photograph. Fit TR1 and TR2, again ensuring correct orientation.

Finally, insert 1mm terminal pins for the off-board wires. Thoroughly check the assembly with a magnifying glass, looking especially for problematic soldering around the i.e.d.s and i.c. socket pins.

Now solder the infra-red emitting diode D6 to its small sub-board, lying it flat with the board.

## DISPLAY BOX

For the prototype model, the p.c.b. is mounted in a small circular plastic box which had previously contained a powerful "Gentleman's Relish" anchovy paste! It is available in different sizes and the one chosen measures externally about 68mm maximum diameter and is about 26mm deep.

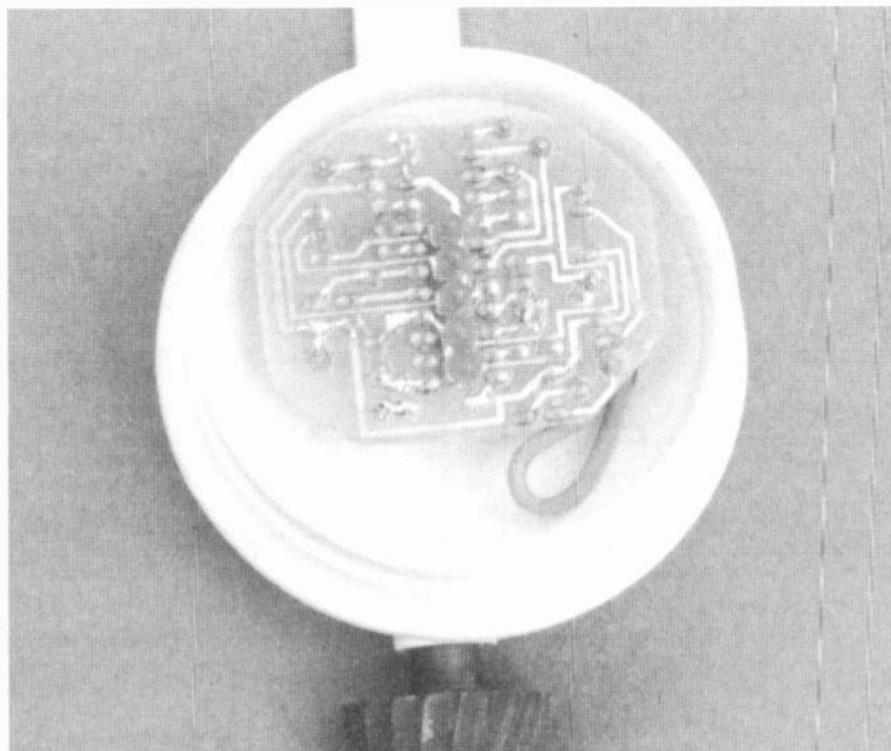
Three holes are needed in its concave base: for sensor vision, cable entry and pendulum shaft mounting. The lid needs a central slot through which the i.e.d.s protrude. The plastic is a bit brittle, so work on it with care.

Because of the unusual concave interior of the box, it was decided not to attempt bolting the p.c.b. to it. Instead, a chunk of Blu-Tack was used to hold the p.c.b. in place.

## PENDULUM ARM

Look at the photographs of the pendulum assembly and then relate them to the schematic details shown in Fig. 5 to Fig. 8.

The pendulum arm itself is made from an oval metal tube. Its actual measurements, given in Fig. 5, are not critical and anything similar could be used. The



The completed p.c.b. mounted inside the circular case, using Blu-Tack, showing the i.e.d.s soldered on the track-side.

original started life as part of a *Harrison Drape Net Curtain Track*, intended for a window width of 0.61m to 1.02m (24in to 40in) – curtaining shops stock them. Just its outer slider was used, with the plastic end plug removed.

Holes were drilled in the tube, suitable for mounting-shaft insertion at the top, cable exit towards the bottom, and a nearby display-box mounting hole. Before drilling the latter, though, it is suggested that the box is temporarily stuck to the shaft with Blu-Tack until the preferred position is found, this being a matter of taste.

For added weight, in order to give greater swing momentum, a pyramidal woodworking hole enlarger was pushed into the bottom end of the pendulum shaft. Other weights could be substituted, if a suitable fixing method can be devised.

### PIVOT PARTS

Mechanics are not the author's best subject! As usual, these have been done according to what spare bits there are around the house and which can be successfully bodged! Again, as usual, plumbing materials and electronic parts have been conscripted into action (both are in plentiful supply at *Chez B...*), for the pendulum's pivot and mounting support.

Details of the pivot assembly are shown in Fig. 6. The pivot shaft, which passes

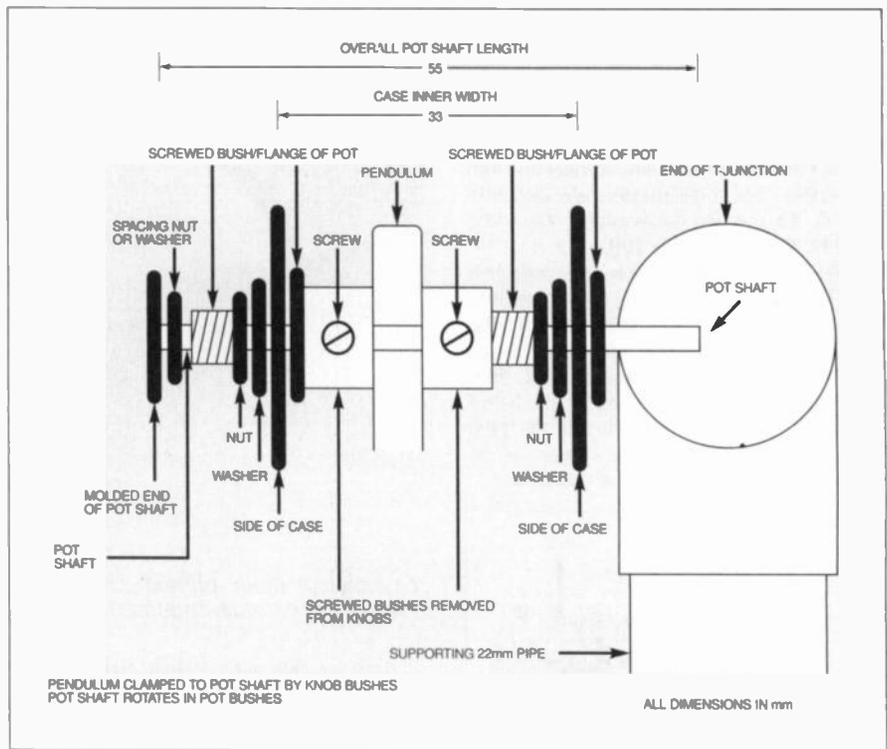


Fig. 6. Pendulum pivot head assembly and dimensions.

through the top of the pendulum arm, is the plastic shaft removed from a mono potentiometer (any value will do!).

The flanged bushes, nuts and washers were also taken from pot assemblies. The screwed brass bushes were cut out from two spare plastic rotary knobs.

These parts were assembled inside a small, suitably drilled, diecast metal box, taking care that the arrangement swung smoothly from side to side, but with minimal sloppiness fore and aft. If better parts can be found in a local model shop, use them.

Inconveniently, the diecast box had slightly sloping sides. This required the use of thin wooden wedges (not shown in Fig. 6) between the rear side and the plastic plumbing T-tube to which the box was bolted. The wedges were cut so that the pendulum arm and its shaft were satisfactorily positioned vertically to ensure a swing with least friction (they were vandalised from clothes pegs!).

### SUPPORTING STRUCTURE

As shown in Fig. 7, the pendulum support structure is principally constructed from 22mm diameter plumbing pipe. Since the structure is only used to support the pendulum pivot mechanism at the top, plus the mount for infra-red l.e.d. D6, alternative techniques could be used. For example, the pivot box could be bolted directly to a wall, as could D6.

In the illustrated method, the pivot box is bolted to a plumbing T-junction, into which the vertical pipe is pushed. The latter is then fixed to a wall using ordinary pipe clips. The same type of clip is used in connection with mounting diode D6.

Two mounting positions for the infra-red l.e.d. D6 are shown in Fig. 7. The preference is for the position on the end of the horizontal shaft. This places emphasis on viewing the time in the normal direction and provides an amount of uniformity

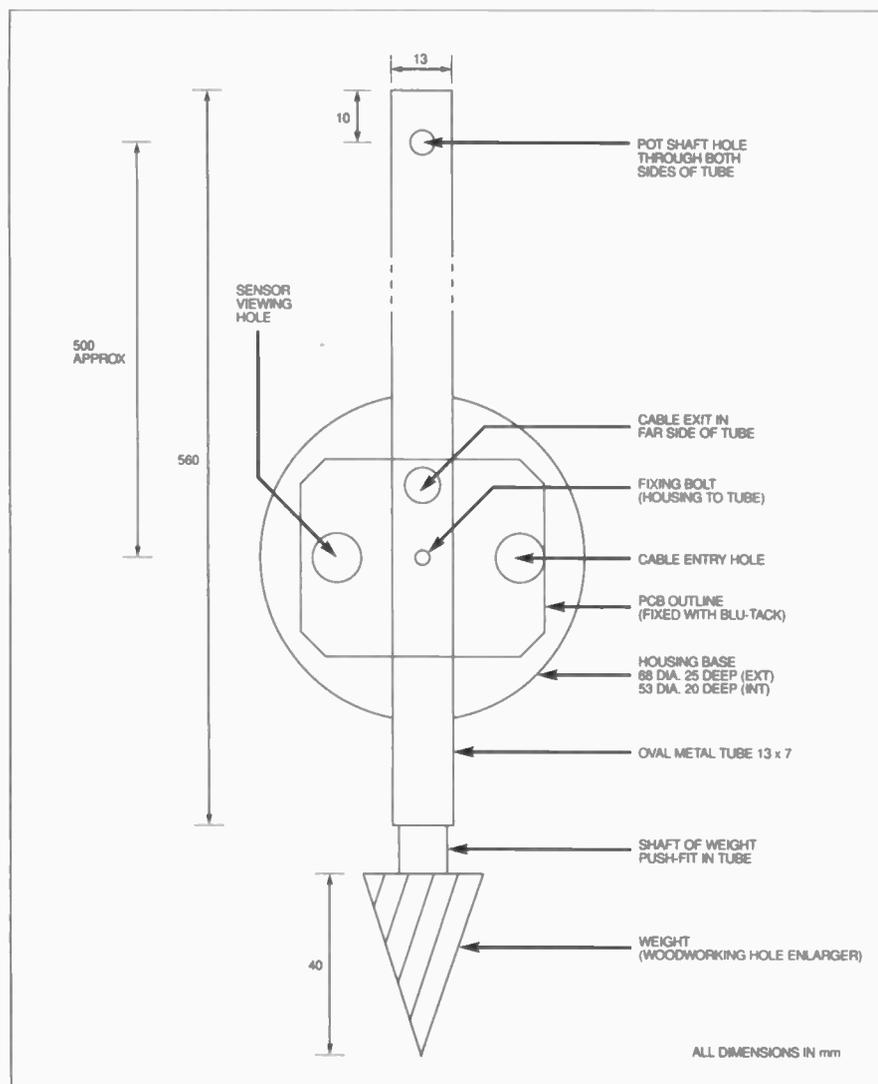


Fig. 5. Pendulum arm assembly and dimensions.

in the width of the display to either side of the central position. Be aware, though, this relationship varies as the pendulum swing arc shortens.

The second position, with D6 near the central column, allows the time to be read in both swing directions, with it being displayed "backwards" on the return to the left beyond the centre. Be aware here that the apparent width of the digits will be greater near the central column than towards the end of the swing. This happens because the pendulum is slowing down as it nears the end of its arc.

All plumbing parts for the pendulum support may be copper or plastic. A mixture of both was used in the prototype since they were already owned.

Prototype pendulum pivot head case (right) and infra-red emitter support arm (below).

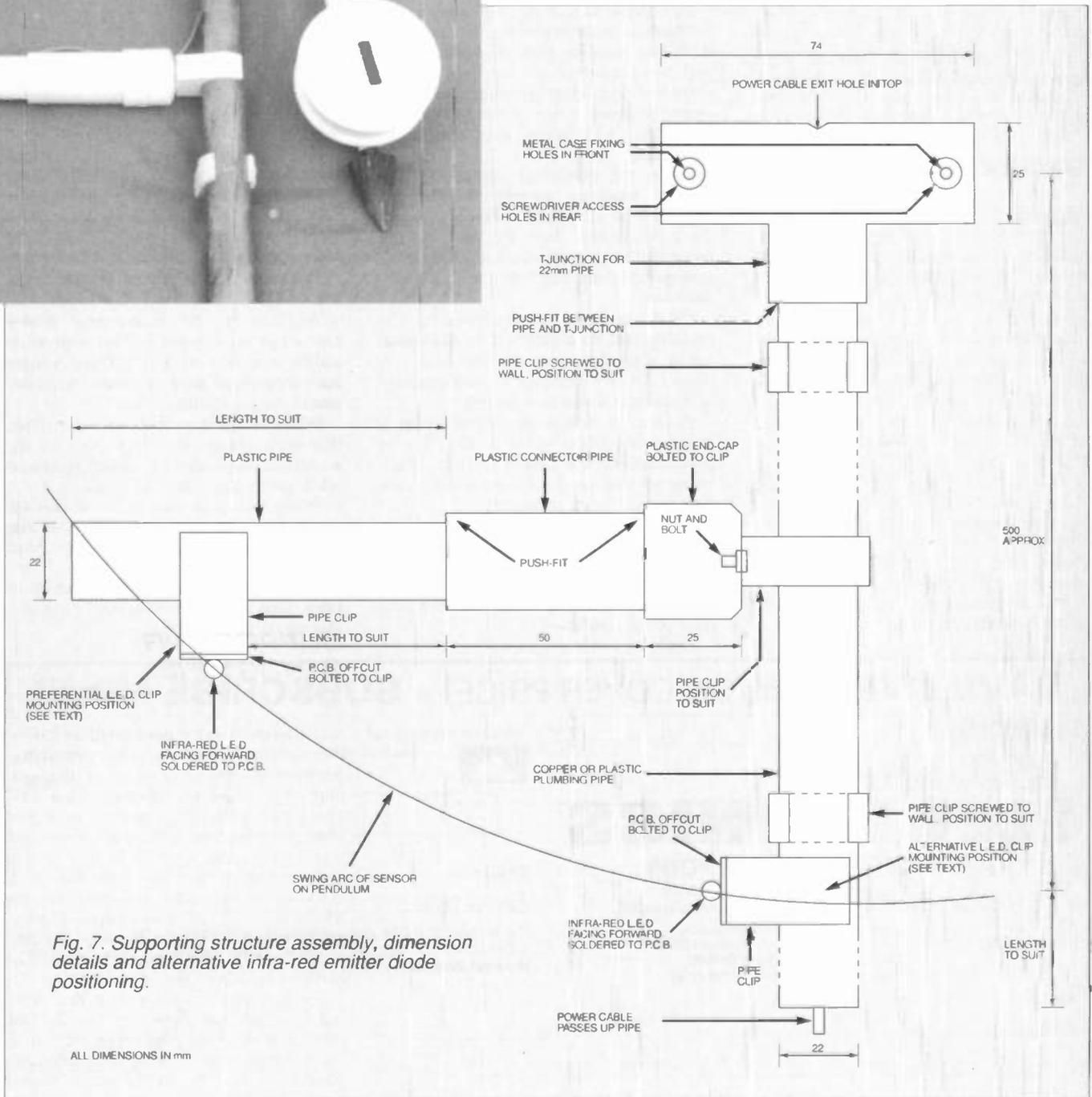
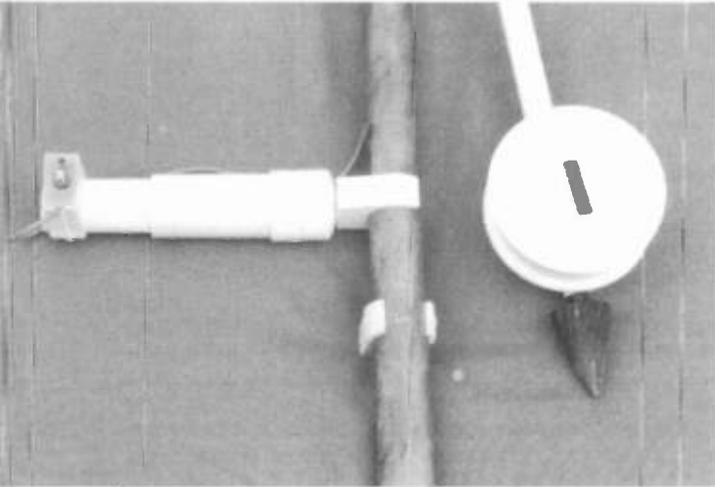
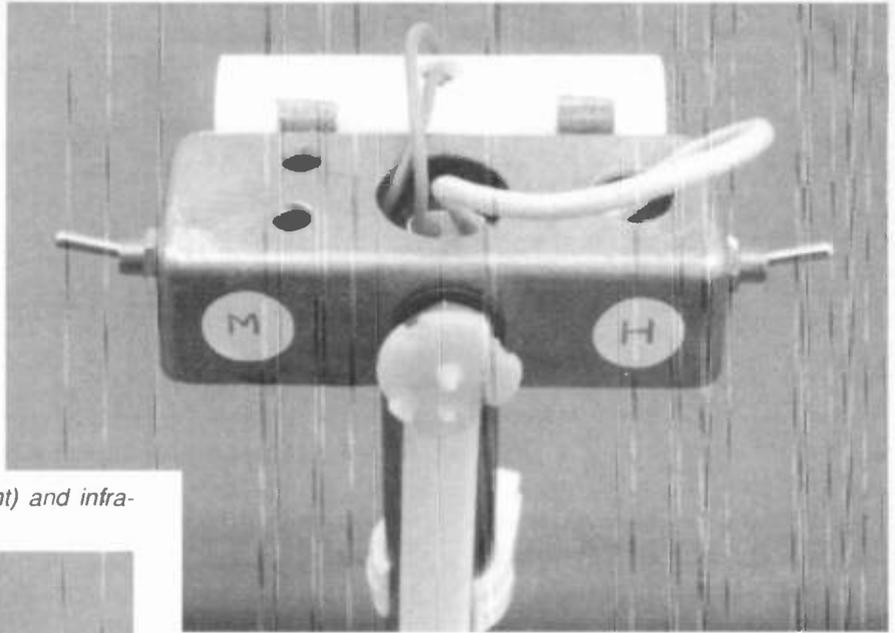


Fig. 7. Supporting structure assembly, dimension details and alternative infra-red emitter diode positioning.

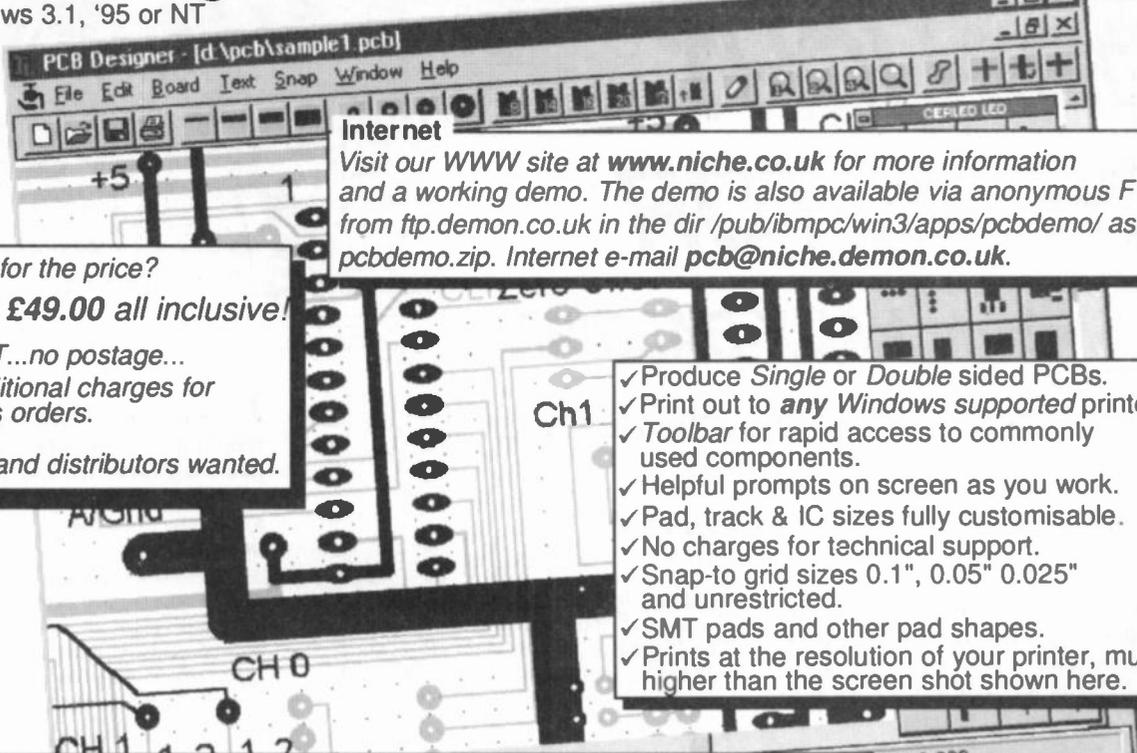


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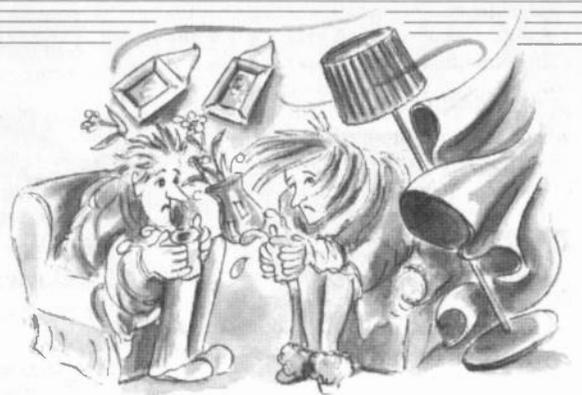
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# DRAUGHT DETECTOR



TERRY de VAUX-BALBIRNIE

Sniff out those unwanted draughts with this money-saving project.

**M**OST people now realize the importance of providing efficient insulation in their homes. However, the simpler expedient of eliminating draughts is often overlooked and this can represent a considerable waste of energy.

Once sources of draughts have been found, they may be sealed at very little cost using materials obtained from any DIY store.

## TRICKY SITUATIONS

The project presented here is a self-contained unit which helps to locate draughts around the home. In use, the Draught Detector is moved slowly around likely places such as the edges of window frames and doors. When the sensor detects a draught, a buzzer sounds.

This is more effective than checking with the hand and is easier to use in awkward situations. The unit may even be attached to a long cane so there is no need to crawl around on the floor or to stand on a chair to reach out-of-the-way places.

The maximum sensitivity can be judged from the fact that the prototype unit is

triggered by blowing at the sensor at a distance of about one metre (3ft approx.). For this reason, resourceful readers are certain to find alternative uses for this circuit.

key components are R2 and R4 – these form a pair of identical *positive temperature coefficient* (p.t.c.) thermistors. The working substance in a p.t.c. thermistor is a mixture of barium, lead and strontium titanates.

It is essential to use this particular type of thermistor (see *Shop Talk*), the more common *negative* (n.t.c.) variety would not be suitable here. Whereas the latter type *reduces* its resistance with increasing

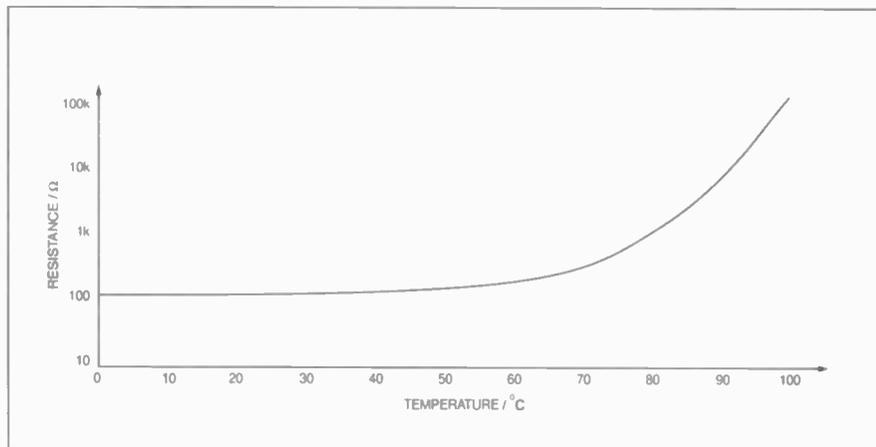


Fig. 2. Graph showing the rising resistance with an increasing temperature.

## CIRCUIT DESCRIPTION

The complete circuit diagram for the Draught Detector is shown in Fig. 1. The

temperature, the positive temperature coefficient one shows a *rising* resistance.

The specified thermistors have a resistance of around 100 ohms at temperatures below 60°C. Above this, the resistance rises sharply and at 100°C reaches 100 kilohms – a thousandfold increase (see Fig. 2). The temperature at which the resistance becomes about one kilohm (1kΩ) (in this case, 80°C) is called the *threshold* or *critical* temperature.

With switch S1 on, current flows from the nominal 18V supply consisting of two 9V batteries connected in *series* to the rest of the circuit. The thermistors R2 and R4 are included in a pair of potential dividers.

The first comprises fixed resistor R1 in the upper arm and thermistor R2 in the lower one. The second consists of potentiometer VR1, connected in series with fixed resistor R3, in the upper arm and thermistor R4 in the lower one.

With room temperature below 60°C, the current in the thermistors will be 150mA approximately and sufficient for them to self heat. They will then approach the threshold temperature within a few seconds.

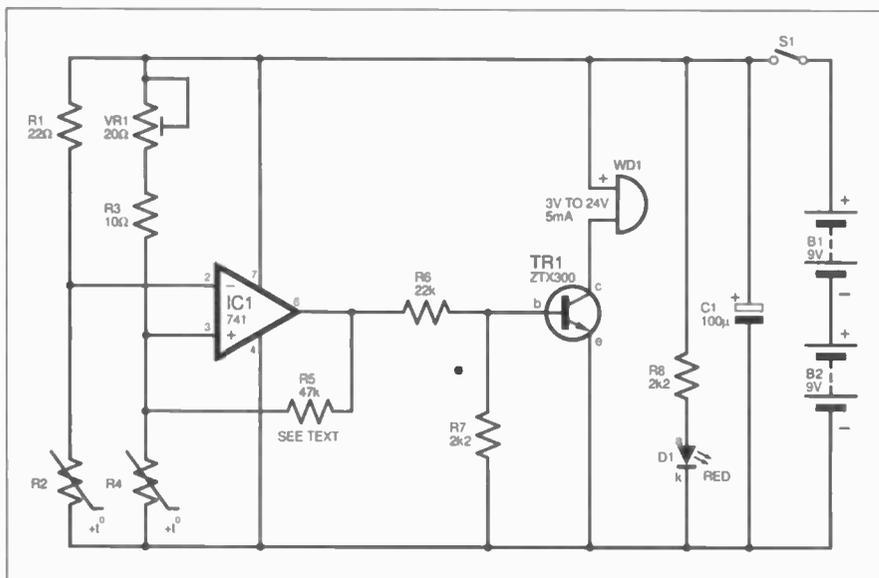


Fig. 1. Complete circuit diagram for the Draught Detector.

However, the rapidly rising resistance causes the current to fall and there will be a reduced heating effect. The temperature of the thermistors will therefore stabilize when the energy supplied equals the heat emitted from the surface. This will happen when the temperature reaches about 75°C, corresponding to a resistance of some 500 ohms.

## DETECTION

In the absence of a draught, each thermistor will be surrounded by a blanket of warm air. However, thermistor R4 is arranged so as not to receive any draught impinging on the detector R2.

When a draught is detected, the warm air around R2 is disturbed and this thermistor is cooled slightly. This results in a lower resistance and hence a falling voltage being developed across it. It is this voltage change which operates the circuit.

Operational amplifier IC1 is configured as a *voltage comparator*. When the voltage applied to its non-inverting (+) input, pin 3, exceeds that at the inverting (-) one, pin 2, the output (pin 6) is *high*. In other cases it is *low*. The voltage across R2 is applied to pin 2 while that across R4 is applied to pin 3.

## WELL BALANCED

In use VR1 (Balance control) is adjusted so that, with no draught present, the voltage at pin 3 will lie a little below that at pin 2. The op.amp will therefore be *off* and hence transistor TR1 will be off also. With no collector (c) current flowing, the buzzer WD1 will remain silent.

When a draught is detected by R2, the voltage at pin 2 will fall below that at pin 3 and the op.amp will switch on. This *on* state will operate the transistor, with base (b) current entering via resistor R6 and WD1 sounds.

Using a pair of thermistors in a balanced circuit like this makes it reasonably immune from deviations in the operating point caused by changes in ambient temperature. It also prevents problems when the device is moved during the course of use since this will inevitably cause a draught.

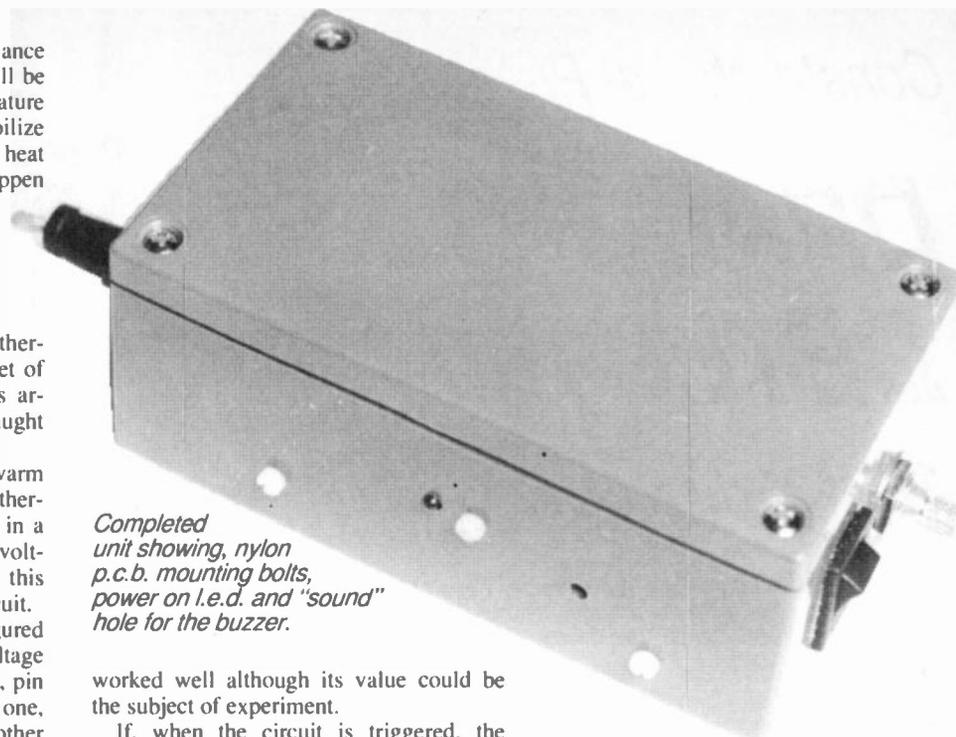
Any such changes will have an equal effect on both thermistors and the voltages applied to the op.amp inputs will rise or fall in sympathy. The relative status of the inputs - in theory anyway - will therefore depend only on the cooling effect of R2 caused by draughts impinging on it.

Small changes in supply voltage due to the batteries ageing will have no effect since, again, the relative state of the inputs will remain unchanged. Of course, when the batteries run down to the point where they cannot maintain sufficient heating effect in the thermistors they will need to be replaced.

## NICE AND WARM

Resistor R5 applies a little positive feedback to IC1. This helps to provide a sharp switching action. Thus, at the point where the device switches on, thermistor R2 will need to warm up a little more for it to go off again.

This causes the buzzer to begin sounding sharply instead of with a "chirp" as might otherwise happen. The value stated



Completed unit showing, nylon p.c.b. mounting bolts, power on l.e.d. and "sound" hole for the buzzer.

worked well although its value could be the subject of experiment.

If, when the circuit is triggered, the buzzer fails to go off again this could be because the resistance of R5 is too low. The value could be raised or the circuit tried with the resistor removed altogether. Light emitting diode D1 indicates the switched-on state with resistor R8 limiting the current to a safe working value.

The circuit needs a power supply of between about 14V and 18V. In the prototype, this was provided by two 9V alkaline PP3 batteries housed inside the case. These will give very good service in occasional use.

At the instant of switching on, there is a current surge of about 300mA. However, this falls rapidly and stabilises at only 50mA or so.

## CONSTRUCTION

Construction of the Draught Detector project is based on a single-sided printed circuit board (p.c.b.) and the topside (component view) is shown in Fig. 3, together with the underside copper foil master. This board is available from the *EPE PCB Service*, code 112.

Begin by drilling the three mounting holes. Mount the i.c. socket and resistors. Follow with the electrolytic capacitor, transistor, buzzer and l.e.d. (taking care over the polarity of these latter components). The l.e.d. should be mounted using most of the length of its end leads so that its tip stands 18mm above the p.c.b.

Solder pieces of stranded connecting wire to the points labelled "VR1" and "S1". Connect the negative wire of one of the battery snap connectors to the point marked "Batt (-)".

Next, shorten the thermistor end leads - R2 to a length of about 8cm and R4 to 6cm. Solder them to the positions shown on the circuit board. Insert IC1 in its holder, observing the orientation.

## CASE DETAILS

Drill three holes in one side of the box to correspond with the mounting holes in the p.c.b. Make holes for On/Off switch S1 and potentiometer VR1 in an end panel.

Drill a hole in the opposite end panel of the box for the sleeved grommet through

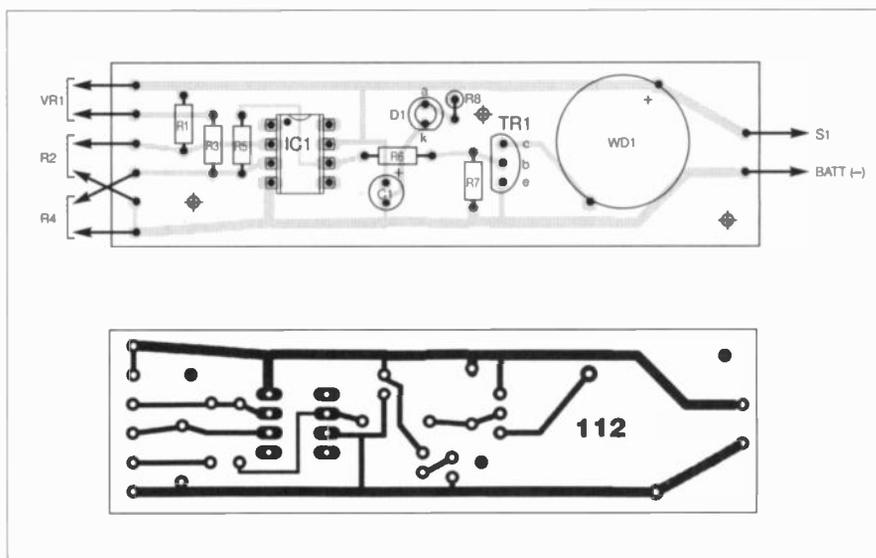


Fig. 3. Draught Detector printed circuit board component layout and full size underside copper foil master pattern.

# COMPONENTS

See

## TALK Page

### Resistors

R1	22Ω
R2, R4	disc thermistor, positive temperature coefficient 80°C @ 1kΩ (2 off)
R3	10Ω
R5	47k
R6	22k
R7, R8	2k2 (2 off)
All 0.25W 5% carbon film	

### Potentiometer

VR1	20Ω wirewound vol. control
-----	----------------------------

### Capacitor

C1	100μ radial elect. 25V
----	------------------------

### Semiconductors

D1	3mm red l.e.d.
TR1	ZTX300 npn silicon transistor
IC1	LM741CN op.amp

### Miscellaneous

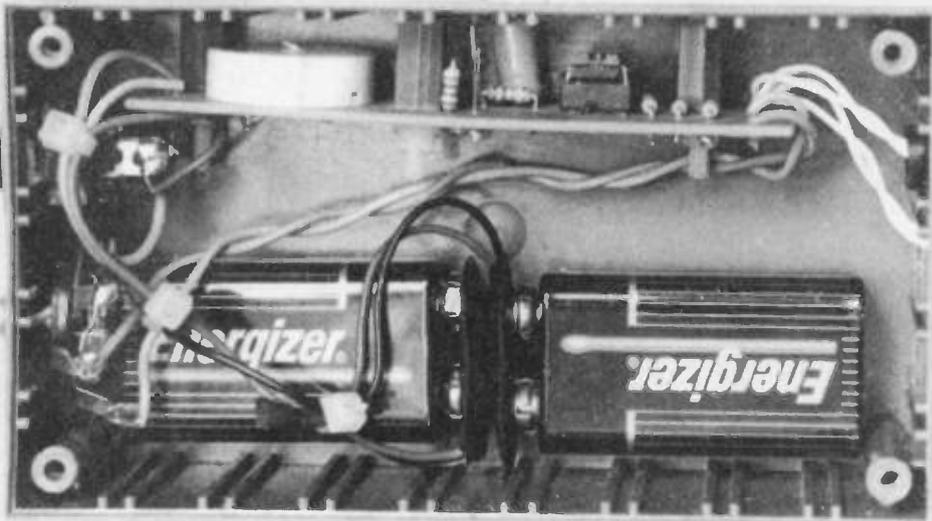
WD1	piezo buzzer, p.c.b. mounting, 3V to 24V 5mA operation
B1, B2	PP3 alkaline battery and snap connector (2 off each)
S1	miniature s.p.s.t. rocker switch

Printed circuit board available from EPE PCB Service, code 112; plastic box, size 125mm x 70mm x 49mm; 8-pin d.i.l. socket; p.c.b. spacer (3 off); sleeve exit grommet; knob (if needed); sleeving; wire, solder, etc.

Approx Cost  
Guidance Only

**£20**

excluding batts.



Layout of components inside the Detector case. The two sensor thermistors can be seen on the right, with the draught "detector" R2 protruding through the sleeved exit grommet. The "balance" thermistor is carefully bent away from the detector as shown.

which thermistor R2 leads pass (see photographs). This grommet is not essential but it improves the appearance of the finished project and provides some protection. Drill a smaller hole nearby for thermistor R4 leads.

Measure the position of l.e.d. D1 and drill a hole in the side so that, when the circuit board is in position, the l.e.d. will protrude through it. Similarly, on the same side panel, measure the position of buzzer WD1 and drill a hole for the sound to pass through.

Mount the internal components. Note that the potentiometer specified for VR1 needs no control knob and may be adjusted using its knurled extension. However, it is of a standard size so a knob may be fitted if desired.

## INTERWIRING

Mount the printed circuit board using 15mm long plastic stand-off insulators and nylon fixings. If metal nuts and bolts are used, take care that no short circuits are formed with the board copper tracks.

Referring to Fig. 4, complete the point-to-point wiring. Take care over the connections to the battery connectors — these are wired in series. The common

connection should be insulated using p.v.c. tape or a piece of heat shrinkable sleeving.

The exact method of arranging the thermistors could be a useful subject for experiment. However, the following guidelines will be found useful.

Random air movements such as those caused by moving the unit from place to place should equally affect both thermistors. This means that R4 should be fairly close to R2.

It is important that the draught to be detected falls only on thermistor R2. Note that R2 should protrude through the sleeved rubber grommet sufficiently for the sensitive blue spot to show.

In the prototype unit, R4 leads were bent out of the way as shown in the photograph above. The sensitive parts of the thermistors must not touch the box, the grommet or anything else since this would disturb the self-heating effect and cause unreliable operation.

## TESTING

With switch S1 in the *off* position, attach the battery connectors and secure the batteries to the base of the box using Velcro fixing pads or small brackets. Fit the lid.

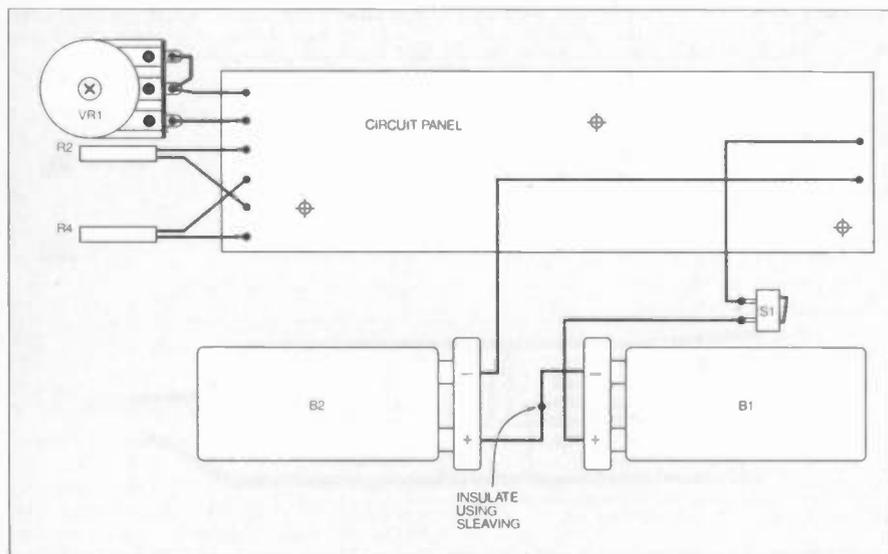


Fig. 4. Details of the interwiring from the Draught Detector printed circuit board to the off-board components.

Adjust Balanced control VR1 fully clockwise and switch on. The l.e.d. D1 should light and the buzzer remain off. If the buzzer sounds, it is likely that the outer (track) connections to VR1 have been made in the opposite sense so turn the spindle completely anti-clockwise instead.

Wait for at least 30 seconds to allow the thermistors to thermally-stabilise. Rotate Balance control VR1 slowly to the point where the buzzer sounds then take it back so that it is *just* silenced. This is the most sensitive position.

Now blow *very gently* on thermistor R2 (it may be necessary to shield R4 from the draught using a piece of paper) — the buzzer should sound and go off again a few seconds later. If this test works satisfactorily the unit may be put into service.

In use, VR1 should be kept adjusted to give the sensitivity required. If it is set too finely, once triggered the buzzer WD1 will sound for a long time or even fail to go off altogether.

Another consequence is that triggering is likely to occur with random draughts. A little practice will soon find the optimum setting.

When a harsh draught has been detected, it will take some time for the unit to recover and be ready to detect another. When there is a general lack of sensitivity and an excessive recovery time, this is a sign that the batteries need to be replaced.

Happy sniffing! □

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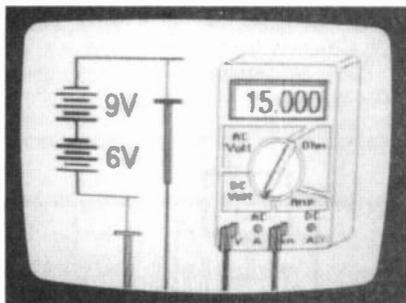
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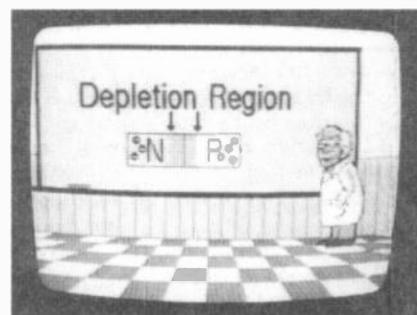
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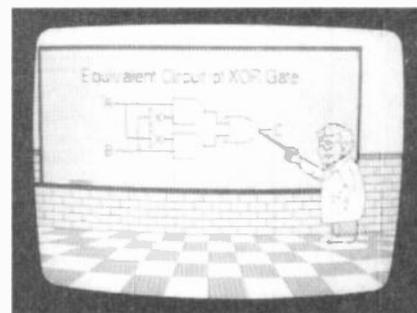
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## “Custom Ferrari” — for boy racers!

In order to add some realism to a model sports car, I designed the simple circuit of Fig. 4 which can be built into virtually any type of toy car, battery operated or not. The design uses a CD4020 14-stage binary counter to operate l.e.d. “Turn Indicators” (D5 to D8), “tail-lights” (D9 to D10) and “Headlights” (D11 to D12).

The counter IC1 is clocked by a unijunction oscillator based around TR1. The red tail-lights and the yellow headlights draw a small current supplied constantly by resistors R7 and R8. For added realism, this current is supplemented through resistors R1 and R2 which gives an impression of headlights “dipping” and tail-lights “braking”.

The model’s turn indicators flash whenever they are enabled and so the cathodes (k) of D5 to D8 are taken to another output (Q3, pin 7) of IC1. Taking their anodes (a) positive, via resistor R3/R4 and the relevant counter output, they flash at the rate determined by Q3. The result is that one set of indicator lights flash, then the other side, followed by both!

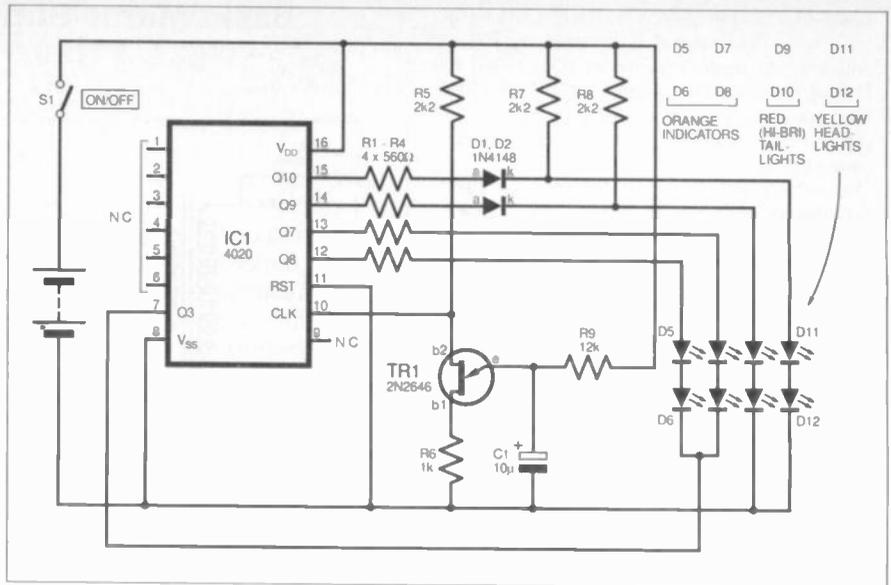


Fig. 4. Lighting and indicator circuit for model cars.

The circuit is powered by a PP3-type or MN1604 9V battery and a small slide switch S1 can be mounted on the vehicle’s underside.

David Geary,  
Blackheath,  
London.

## 555 Astable Frequency Meter – out for a count

The circuit shown in Fig. 5 is a simple digital frequency meter which I designed to indicate the frequency in Hertz of an astable 555 timer. It could perhaps be adapted for other uses.

An npn transistor, TR2, is connected to the 555 astable to be measured, as shown inset, and the output signal obtained is “hooked” to the main circuit via transistor TR1 collector (c). Two CMOS 7555 timers, IC3 and IC4, are wired as monostables and these will

trigger via R6/C1 when the Display switch S1 is closed. The period of IC3 is adjustable using VR1 whilst IC4 times for a fraction of a second.

Upon closing S1, IC4 sends a reset signal to IC1 and IC2, which are two decade counters each driving a 7-segment common cathode l.e.d. display directly. IC3 then drives transistor TR1, which allows pulses generated by the 555 “under test” to be fed into pin 1 (Clock) of IC2, the first decade counter.

Monostable IC3 needs to be trimmed such that it triggers for approximately 100ms. Pressing switch S1 then allows “100ms worth” of pulses to clock up on the display, and simply multiplying the result by ten will yield the value in Hertz. It would be feasible to cascade several counters to show a higher range of frequencies.

Nick Dossis,  
Middlewich,  
Cheshire.

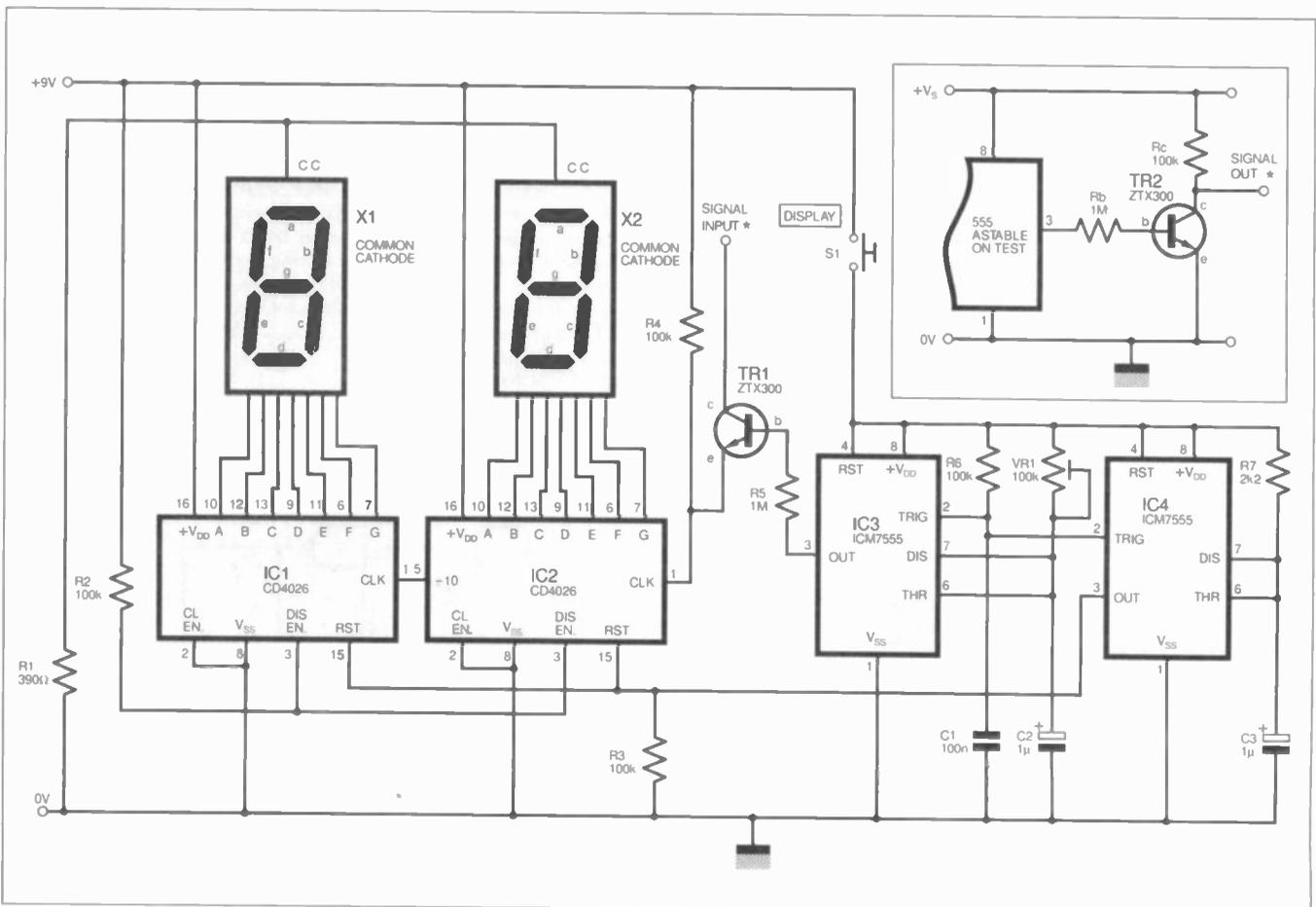


Fig. 5. Circuit diagram for a simple digital frequency meter for 555 astable.

More I/U on page 725

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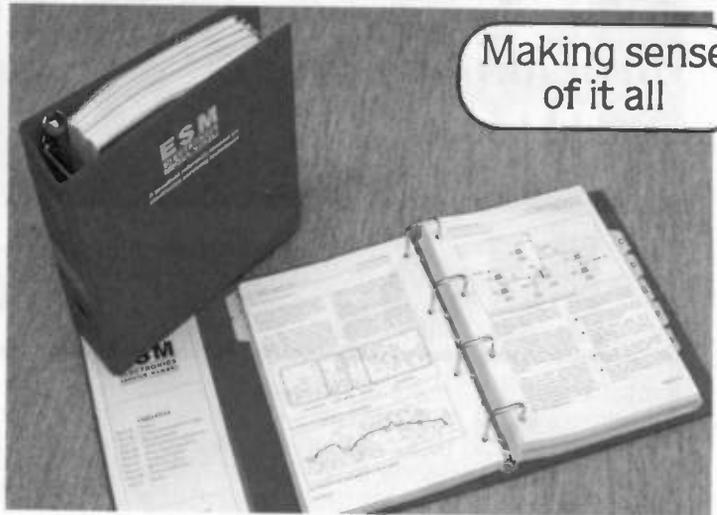
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# Ohm Sweet Ohm

Max Fidling

## Fatal Attraction

The month of August brings the prospect of the dreaded "Annual Garden Fete", held in the grounds of the local Vicarage. This money-raising venture has yet to hit the big time in terms of lasting entertainment value, but the Boss likes it, so that's all that matters, and I get dragged along whether I like it or not, every year.

Indeed, this rigmarole had occurred for many years now and against my better judgment I'd been volunteered by the Boss into lending a hand at this grand social event. Hence the word had eventually got round that I was a bit of an electronics boffin. This appealed especially to the Reverend, who as a sideline, operated the *Church Bells* discotheque, another of his madcap moneyspinners, and in the past I'd helped him with the odd electrical repair, bodged together resourcefully as I usually do!

This year was to be no exception, because the Rev. had asked me if I could help fix a fault on his small public address system, which he intended to use at the Fete. "No problem, Max will happily do it!" the Boss had volunteered.

So, that Sunday morning found me hurriedly finishing off the job in the shack. It would have been nice, I explained to my cat, Piddles, whilst soldering up the microphone's jack plug, and squirting *ElectroLube* into the volume control, if they'd at least tip me a few quid for my toils, but no, it's the same old story - complete mug, do it for nothing, lifetime guarantee, what's the world coming to, etc., I moaned to an unreceptive audience (one cat).

## Cool Cat . . .

I switched the soldering iron off and pondered gloomily, whilst fumbling with the microphone. A quick test was, I suppose, a good idea so I plugged everything

together, microphone, loudspeaker and all, and switched on.

Now for some fun. I'd always fancied myself as a singer, and now was a good time to practise. I told the moggie, as I cranked up the "level" control and warbled into the microphone with a fine rendition of *Elvis Presley*.

"... Yeah-aye, I'm all shook up!!" echoed the shack to fifty watts of musical entertainment. The window rattled in sympathy but Piddles looked on, unmoved by my taste in tunes. Everything seemed fine so the P.A. was made ready for the big day out as we prepared for the Fete.

Arriving early, I hastened over to see the Reverend and between us we installed it around the garden, using an extension lead from the Vicarage for power. Everyone in the merry band of workers then received their orders from the Vicar's wife, and my eyes rolled skywards as I was handed the job of the "Mousey Mousey" Stall. The Boss smirked.

## . . . Hot Mouse

Devoid of anything remotely electronic, the dreaded Mousey Mousey Stall was the pits. It consisted of a short length of drainpipe with an outlet at the bottom. The idea was that the merry "punter" for 20p, waited with a rubber mallet at the drainpipe's exit, whilst I dropped a stuffed toy mouse in at the top. The player had to clobber the mouse as soon as possible when it exited.

Little did they know that the mouse contained a quarter pound of solid lead, taken from the church roof, and would pelt out of the tube faster than a whippet on steroids! This inside knowledge was about the only satisfaction I derived from the job.



So a whole afternoon of stuffing the mouse down the drainpipe finally drew to a close as I counted up the loot and handed it in to the Rev.'s wife. The Boss looked on, proudly telling everyone how I'd just fixed the sound system in the nick of time and saved the day. Time for the day's results, as an expectant hush permeated around the villagers.

## Ohm Sweet Ohm

Grabbing the microphone, the Reverend started his usual Garden Fete speech, thanking everyone individually (excluding myself, I noticed) for their help, as his voiced echoed around the garden. At precisely the point where he started to read out the profits, the sound went dead!

Tapping the microphone and twiddling the controls had no effect! The Reverend blanched, quickly switched it off then raised his voice and continued shouting the results ever more hoarsely to a hushed crowd.

The Boss glared over at me, but I'd already started to flee through the garden gate, whistling a tune and wandering in the direction of home, the shack and the cat. I mean, what do they expect for free? I ask you.

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# Techniques

## ACTUALLY DOING IT!

by Robert Penfold

If you talk to someone who is contemplating the construction of their first project, but is a bit reluctant to actually buy the parts and give it a try, the reason for their hesitation is almost always the same. They are worried that they will not be able to get the finished unit to work, and that the money spent on the components will be wasted.

### Something Simple

As I have pointed out many times before, the chances of getting modern projects to work first time are excellent. The first-time constructor needs to choose his or her project very carefully, but provided a sensible choice is made, and things are not rushed, there is little risk of the finished unit failing to work. The best type of project to choose is one which is fairly simple and straightforward. The larger the project, the greater the chances of a mistake being made.

I would also suggest that the project should be built on a ready-made custom printed circuit board (p.c.b.). This is not a cynical attempt to plug the *EPE PCB Service*. A custom printed circuit board is the easiest construction method. Making your own boards is not too difficult, but there are plenty of new skills to be learnt even without any unnecessary additions to the list. If you are interested in p.c.b. production, this can be mastered once you have some experience of project construction.

It is better to choose a project that does not present any major problems as far as the mechanical side of construction is concerned. You will have plenty to occupy your mind when dealing with the electronics. Awkward aspects of the mechanical side of construction will be an unwelcome distraction.

Only choose battery powered projects that do not involve any connections to the mains supply. The mains supply is potentially lethal, and is certainly not a suitable starting point, particularly for younger constructors.

### Understandable

Make sure that you select a project which has a function that you fully understand. It is not that unknown for a letter to be received from a reader who is having problems with a project, where it soon becomes quite clear that the reader had slightly (or completely) misunderstood the purpose of the project! This is admittedly quite rare these days, but from time to time a

reader still "gets hold of the wrong end of the stick". Choose something straightforward, like a simple household gadget, car project, or a very basic piece of test gear.

When you first attempt project construction there is a great temptation to start building some weird and wonderful device, but to do so would almost certainly be a mistake. It is better to start with something reasonably simple and straightforward, even if it is not of any great use to you when finished. You should learn a lot from building it, have some fun in the process, and it should be a good confidence builder.

### Can't Stand the Heat

I suppose that project constructors have to regard an occasional problem project as an inevitable part of the hobby. You can minimise the number of projects that give problems by building every project carefully and methodically, but we all make mistakes from time to time. Sooner or later you are almost certain to be faced with a project that fails to work first time.

There are three main causes of newly constructed projects failing to work. An error by the constructor, an error in the article describing the project, or a faulty component. A faulty component is probably the least likely cause, since modern components are thoroughly tested and very reliable. Even if you spend many years building hundreds of projects it is quite likely that you will never be sold a "dud" component.

If there is a problem with a component, it is more likely that it has become damaged during project construction, or possibly on its way to you in the post. In most cases any physical damage will be plain to see. It is not advisable to use any component that has any physical damage beyond a few superficial scratches. Even if a damaged component is basically functioning, its accuracy and reliability will almost certainly have been impaired.

Components are most at risk when they are being soldered onto the circuit board. Beginners are often a little slow and hesitant when producing soldered joints, and this can result in overheating. Fortunately, most modern electronic components are quite resilient, and are not easily damaged by excessive heat.

Even if a resistor or capacitor is overheated to the point where it becomes

discoloured, it might actually still work properly. However, if a project fails to work, it obviously makes sense to replace any components that show signs of heat damage, or any other form of physical damage.

Probably the passive components that are most at risk are the box style capacitors which do not have a plastic casing. These open style capacitors are now somewhat tougher than the original components of this type. Even so, with many of them it is not too difficult to detach one of the leadout wires.

The fact that a leadout has broken away from the case will normally be self evident, but this is not always the case. If there is outward pressure on the leadout wires when one of these capacitors is soldered into place, one of the leads can effectively be desoldered and part company with the casing. However, with both leads firmly soldered in place, everything may appear to be perfectly all right unless the component is carefully scrutinised. *(We have found polystyrene capacitors to be occasionally subject to similar problems. Ed.)*

### Semiconductors

Semiconductors are the components that are most vulnerable to heat damage. It is quite possible to overheat practically any semiconductor without any physical signs of damage becoming apparent. Integrated circuits, with their numerous pins to connect, are more vulnerable than the more simple semiconductors.

Unless the designer states otherwise, a holder (i.e. socket) should always be used for integrated circuits. The holders are soldered to the circuit board, and the integrated circuits are plugged into the holders once the circuit board is otherwise complete. This avoids soldering direct to the pins of the integrated circuits, and avoids any risk of overheating them.

Germanium semiconductors are more vulnerable to heat damage than the much more common silicon variety. The only germanium devices in common use today are a few types of diode, such as the OA90 and OA91. Obviously extra care should be taken when dealing with these.

Some semiconductors, including a fair percentage of integrated circuits, are vulnerable to high voltage static charges. The article should always give a warning if a project uses static sensitive components. While many "old hands" largely ignore the standard handling precautions when dealing with the cheaper static sensitive devices, beginners should always rigidly adhere to them. Experienced constructors can soon sort out what is wrong in the event that a device is accidentally "zapped". Beginners could spend a great deal of time and effort in locating the source of the problem.

### User Error

By far the most common cause of projects failing to work, including my

own efforts, is an error on the part of the constructor. In theory we should all thoroughly check each newly constructed masterpiece before it is switched on. In reality we are usually too impatient to do much checking, if any. If a new project fails to work, switch off immediately and do all the meticulous checking that you should have done already!

The most likely causes of problems are components connected the wrong way round, and badly soldered joints. If a component is connected the wrong way round, checking the board against the printed circuit overlay should soon reveal the problem. Go through the layout component by component, making sure that every component is in the right place, and (where appropriate) fitted the right way round.

Work through the components methodically, making sure that none are overlooked. Remember to check the wiring to the off-board components, including the battery clip. It is quite easy to get a crossed-over wire here, so carefully check that each wire runs between the right two points.

Avoiding and detecting "dry" joints was covered in the January 1996 issue of *EPE*, so we will not go over the same ground again here.

### Clean and Check

Accidental short circuits between copper pads due to solder splashes and trails are another common cause of problems. These are easily produced, and are less obvious than you might think, as they tend to blend-in with the numerous soldered joints.

Also, solder trails are often minute, and can be covered over by the smallest amount of excess flux. Any large pieces of solder should be easily spotted, but a close visual inspection will be needed in order to find most of these short circuits.

Start by cleaning the underside of the board. This will clear away any loose pieces of solder, together with excess flux that might otherwise obstruct your view of any solder trails. Special cleaners are available, but simply brushing the underside of the board using something like an old toothbrush seems to do the job perfectly well.

Unless you have very good close-up vision you will need a reasonably powerful magnifying glass in order to spot the smallest solder blobs and trails. Most photographic shops can supply an 8X loupe (also known as a "lupe"), and these are excellent for detailed checking of boards.

The entire underside of the board should be checked meticulously, but pay extra attention to areas of the board where there are a large number of joints in close proximity to one another. With stripboard the short circuits often seem to occur at the ends of tracks, or where there is a row of breaks in the strips, so pay extra attention to these parts of the board.

### Continuity Error

Without a reasonable amount of technical knowledge and some test equipment it is not really possible to undertake comprehensive fault finding. A simple multimeter or even just a continuity tester is still "worth its weight in gold" though, and something that you should obtain sooner rather than later.

A continuity tester merely lights an l.e.d. and (or) sounds a buzzer when there is a short circuit across the test prods. Ideally you need one that is not "fooled" into indicating a short circuit by diode junctions in the circuit under test. Most modern circuits are riddled with these junctions, with many of them hidden away inside integrated circuits. Many multimeters have a continuity tester facility that can use a low test voltage so that diode junctions are ignored.

In days gone by it was common to use a continuity tester that consisted of a battery and a torch bulb, but this type of tester is not appropriate to modern circuits. The problem is simply that the current drawn by a torch bulb is high enough to "zap" many integrated circuits, and some other semiconductors. An old style continuity tester can soon inflict several pounds worth of damage on any circuit board you test with it!

### Simple Tester

The simple l.e.d. equivalent shown in the circuit of Fig.1 is a much better choice. This operates at a current of only about two milliamps, which is sufficient to give reasonable brightness from a high efficiency l.e.d., but is far too low to cause any damage. The circuit will respond to forward-biased diode junctions, but the l.e.d. will switch on at only about half the normal brightness.

With a continuity tester, or a multimeter that has a built-in facility of this type, it is possible to check that there are no short circuits between tracks, or breaks in tracks, and that on/off switches open and close properly, etc. With a multimeter set to a voltage range you can check that the battery voltage is correct, and that the supply is

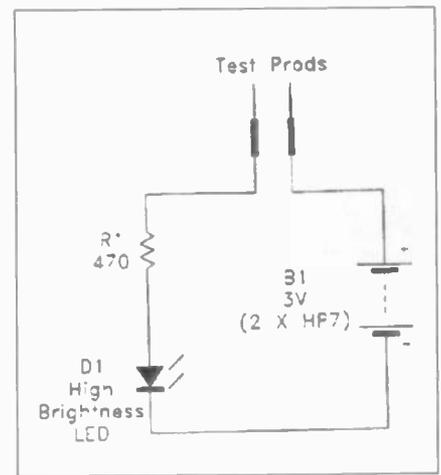


Fig. 1. Circuit for a simple but "safe" continuity tester.

getting through to each part of the circuit correctly. Basic tests of this type are usually sufficient to locate the cause of the problem.

### If All Else Fails

If a couple of thorough checks of the project fails to show up any problem, the last resort is to contact the publisher or designer of the project. Mistakes in *EPE* are few and far between, but they do occur occasionally. Check for corrections in subsequent issues of the magazine, or write in with a stamped addressed envelope asking if there are any corrections. If you think that there is an anomaly in the article (two R23s and no R24 for example), contact the publisher for the correct information rather than guessing and hoping.

It is much easier to help readers locate faults if they supply us with some information, rather than simply saying "I built project X and it does not work". Does the project do anything at all? In the case of an amplifier for example, does it produce a distorted output signal, noise, a weak output signal, or nothing at all?

A multimeter is more than a little helpful here, because it enables you to provide the circuit designer with a list of test voltages at various points in the circuit. Remember to state the type of multimeter you used to take the measurements (digital, 20k/volt analogue, etc.).

Probably the most important thing when dealing with a faulty project is to be positive about it. Remember that if the components are all present and correct, and everything is wired up properly, the project *will* work.

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# POWER CHECK

TERRY de VAUX-BALBIRNIE



Keep costs in tow, build a tri-colour power consumption indicator for caravans and boats.

**M**ANY outdoor enthusiasts rely on a 12V "leisure" battery as a source of energy – perhaps for a caravan or boat. As many know to their cost, indiscriminate use of power can result in a flat battery much sooner than expected.

Children, especially, tend to be as liberal in their use of battery power as they are with the mains at home.

## HAPPY HOLIDAY

It is surprising how many different pieces of electronic equipment may be operated from a 12V d.c. supply and this puts greater demands than ever on a low-voltage system. It is not uncommon for people to mix business with pleasure and operate a laptop computer and printer while taking a break "away from it all". Gone are the days when the battery was used only for lighting and an electric water pump was a luxury.

This project monitors the current being drawn from the battery. By doing so,

economies can be made and the time obtained from one charge maximised. Note that an indication of current may be regarded as a measure of power because the voltage is reasonably constant. This being so, power is proportional to current.

An ordinary ammeter would do the job but this does not easily attract attention and is not readily interpreted at a distance. Also, it would be difficult asking a young child to respond to its reading. In any case, actual current values are not needed – it is sufficient to know if the consumption is simply low, medium or high.

## GO GREEN

In this system, the display is provided by a tri-colour l.e.d. This shows green for a low demand, yellow for a medium one (acceptable for a temporary heavy load such as a water pump) and red to indicate excessive use and the need to switch appliances off straight away. When red shows, an audible signal is also given.

The circuit is built in a small metal box with the l.e.d. mounted on the front panel. A piece of terminal block inside is used to make the connections to the external system.

**This circuit must not be used in installations using more than 10A.** Having said that, though, the values at which the colours operate are freely adjustable.

In the prototype unit, a current below 2A was judged to be *low*, between 2A and 4A *medium* and more than 4A *high*. With these criteria, by keeping green at least 30 hours of operation would be obtained from a standard 60Ah (amp.hour) battery.

## TWO-IN-ONE

Tri-colour l.e.d.s are really two l.e.d.s in one. There is one red and one green unit contained side by side in a milky white translucent package. When *both* are illuminated, the display is yellow. This is a simple example of two primary colours being added together to produce a secondary one. Thus, the three colours mentioned earlier are made possible.

The device has three leads. One is the common cathode (k) connection while the other two (both of them anodes) are responsible for the red and green sections. Do *not* connect the device to a battery to watch it work. The current must be limited

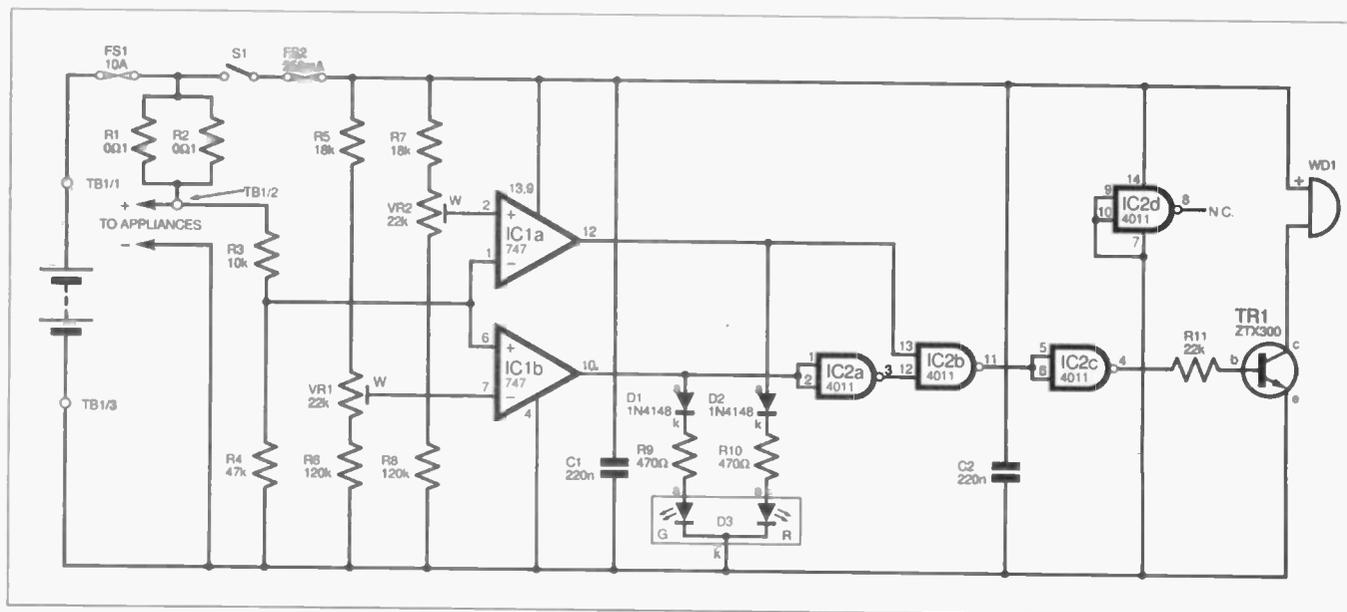


Fig. 1. Complete circuit diagram for the Power Check. Note that resistors R1 and R2 are 3W types.

to 30mA maximum and a series resistor is required for each section. The device will be ruined if it is connected directly – *you have been warned!*

## CIRCUIT DESCRIPTION

The complete circuit diagram for the Power Check is shown in Fig.1. The chief component is the dual operational amplifier, IC1a and IC1b, with the two sections configured as a window comparator.

The heavy-duty battery power feeding the appliances – lights, TV, etc. – flows through fuse FS1 and resistors R1 and R2 connected in parallel. There is, therefore, a voltage drop produced across them. This is important as will be seen presently.

When the current is at the maximum allowed value (10A) the power dissipated is about 5W. The use of two resistors connected in this way provides sufficient power rating while obtaining the correct value, in this case 0.05Ω. Fuse FS1 will blow if the maximum current is exceeded.

## MAKING PREDICTIONS

As predicted by Ohm's Law ( $V = I \times R$ ), for each amp of current flowing through resistors R1 and R2, there will be 50mV dropped across them. In normal leisure use, it is not expected that much more than 5A will be drawn from the supply and for this the voltage drop would be 250mV (i.e. 0.25V). This is unavailable to the appliances but is too small to have any noticeable effect.

Suppose the supply voltage has the nominal value of 12V. With 5A flowing, this would mean that 11.75V would appear across the appliances. In fact, the supply voltage will fall as the battery discharges. This will make no difference to correct operation of the circuit and this point will be explained in further detail later.

Let the voltage drop across R1/R2 be  $D$ -volts. The voltage appearing across the appliances will therefore be  $(12-D)$  volts. This is scaled down to about 80 per cent of its value by the potential dividing action of resistors R3 and R4. The result is henceforth referred to in the text as the "monitored voltage".

## MONITORED VOLTAGE

The monitored voltage is applied to both the inverting input of IC1a (pin 1) and the non-inverting input of IC1b (pin 6). Meanwhile, preset potentiometers VR1 and VR2 apply adjustable voltages to the inverting input of IC1b (pin 7) and the non-inverting input of IC1a (pin 2), respectively. Fixed resistors R5 to R8 limit the range of adjustment of the presets to that needed for correct operation.

Suppose the switching points are chosen to be those suggested earlier – green up to 2A, yellow up to 4A and red for any current higher than this. Presets VR1 and VR2 would be adjusted so that their sliding contacts (wipers) provide 9.45V to IC1b pin 7, and 9.55V to IC1a pin 2, respectively. Note that these voltages do not need to be measured – they will follow naturally during the setting-up process.

The output of an op.amp is high (on) if the non-inverting (+) input voltage

exceeds the inverting (–) one. Consider the case where 1A flows, a low current as required, perhaps, by a single light. There will be a 50mV drop across resistors R1/R2 and therefore a voltage of 11.95V across the appliance, 80 per cent of which gives a monitored voltage of about 9.6V.

Since this is greater than the 9.55V already existing at IC1a pin 2, IC1a output pin 12, will be low. The red l.e.d. section, which is fed from this via diode D2 and current-limiting resistor R10, will therefore be off. The monitored voltage is also greater than that at IC1b pin 7, so IC1b output pin 10 will be high and the Green l.e.d. will be on, being fed through diode D1 and current-limiting resistor R9.

## MORE OR LESS

Now, suppose a current of 3A is drawn. The voltage across the appliance will fall to 11.85V and this will result in a monitored voltage of 9.5V. This is now less than the voltage at IC1a pin 2 and so this op.amp will be on and with it the red l.e.d. However, it is still greater than the voltage at IC1b pin 7 so this op.amp will also be on and hence the green l.e.d. will also be on. With both l.e.d.s on, there will be a Yellow display.

Suppose the current now rises to 6A. The voltage across the appliance will fall to 11.7V and this gives a monitored voltage of 9.4V. Since the voltage at IC1a pin 2 exceeds this, the red l.e.d. remains on. However, it is also less than the voltage at IC1b pin 7 so this op.amp goes off, and with it the green l.e.d. This leaves a Red display.

Diodes D1 and D2 connected in series with the l.e.d. sections prevent any tendency for them to glow slightly when nominally off. This could happen because when the power supply voltage is about 12V, the low state for the outputs of a type 747 op.amp is around 2V, and this is roughly the level at which an l.e.d. will begin to operate.

The voltage across a forward-biased diode is about 0.7V so the output is effectively reduced by this amount. This brings it well below the l.e.d. turn-on voltage.

The supply voltage will fall a little in the normal course of battery discharge.

However, since all the op.amp inputs are derived from potential dividers, they will all fall in unison. This means that the switching levels will remain reasonably constant.

## BE LOGICAL

An audible warning is required when *only* the red l.e.d. is on (i.e. not when yellow is displayed). This is a simple logic problem and may be solved with an arrangement of logic gates. A high output is needed when IC1 pin 10 (green feed) is low and IC1 pin 12 (red feed) is high. A possible arrangement to provide this function is shown in Fig.2, but in this simple application, it is a clumsy method because it uses two different types of gate.

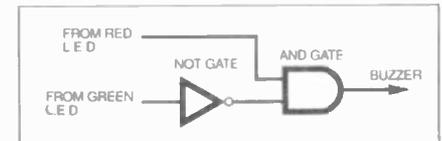


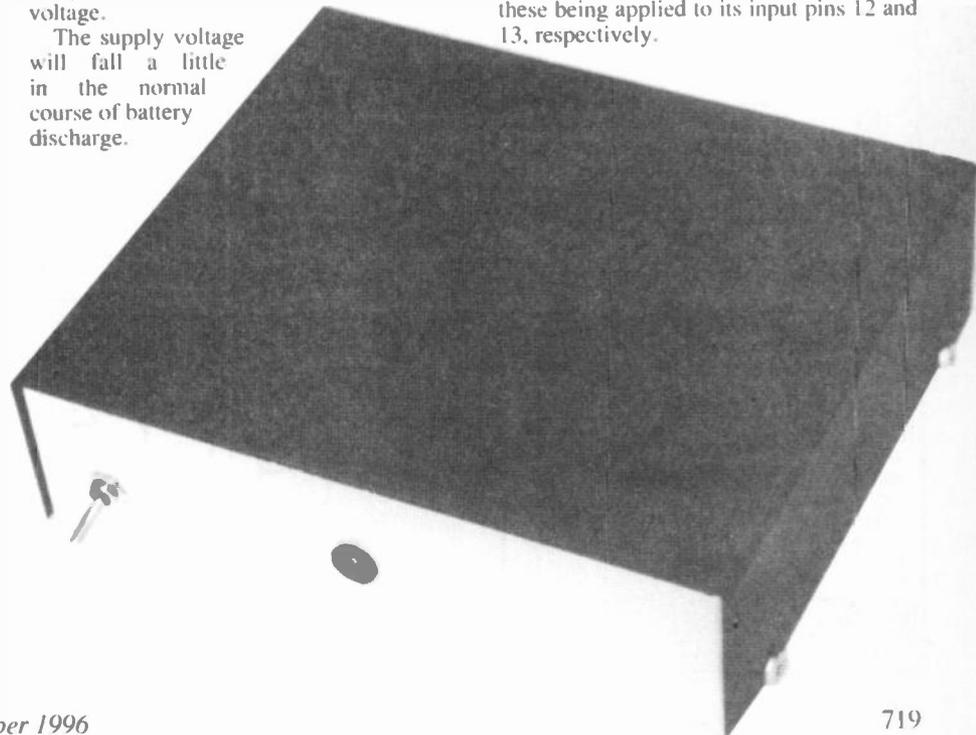
Fig. 2. One possible method of providing a logic signal to trigger the "red" warning buzzer. This uses two different types of gate and was rejected in favour of a single quad 2-input NAND gate i.c. in this circuit.

A more practical way of solving the problem is to use a single quad 2-input NAND gate chip (this contains four identical NAND gates) arranged as shown in Fig.1. Three of the gates are used (IC2a, IC2b and IC2c) and one (IC2d) is left unused.

The two inputs of IC2a (pins 1 and 2) are connected together to form an inverter (NOT gate). This inverts the incoming signal obtained from IC1 pin 10, thus, while green shows, a low signal is output from IC2a pin 3.

Ideally, an AND gate should now be used, but we only have NAND gates available here. So two of these are used together to create an AND function.

First, IC2b is used as a proper NAND gate, and then its output is inverted by IC2c. NAND gate IC2b receives signals from IC2a pin 3 and from IC1 pin 12, these being applied to its input pins 12 and 13, respectively.



Only if both of IC2b's input pins are high simultaneously will its output pin 11 change from high to low. This condition only prevails when the outputs of IC1a and IC1b cause the red l.e.d. to be on and the green l.e.d. to be off. In this situation, the output of IC2c at pin 4, being an inversion of IC2b's output, is high.

Output pin 4 of IC2 is fed via current-limiting resistor R11 to the base (b) of transistor TR1. When IC2c pin 4 is high, TR1 is turned on, so operating the audible warning device (solid state buzzer) WD1 in the collector (c) circuit.

The unused gate, IC2d, has its two inputs tied to the 0V line since unused CMOS inputs should not normally be left unconnected.

## CONSTRUCTION

Most of the Power Check circuit is built on a single-sided printed circuit board (p.c.b.), details of which are shown in Fig.3. This board is available from the *EPE PCB Service*, code 110.

The pair of power resistors, R1 and R2, are mounted separately on a piece of tag board. This is because they become hot when a high current flows and this could damage unprotected components nearby. For this reason, *do not use a plastic box for this project.*

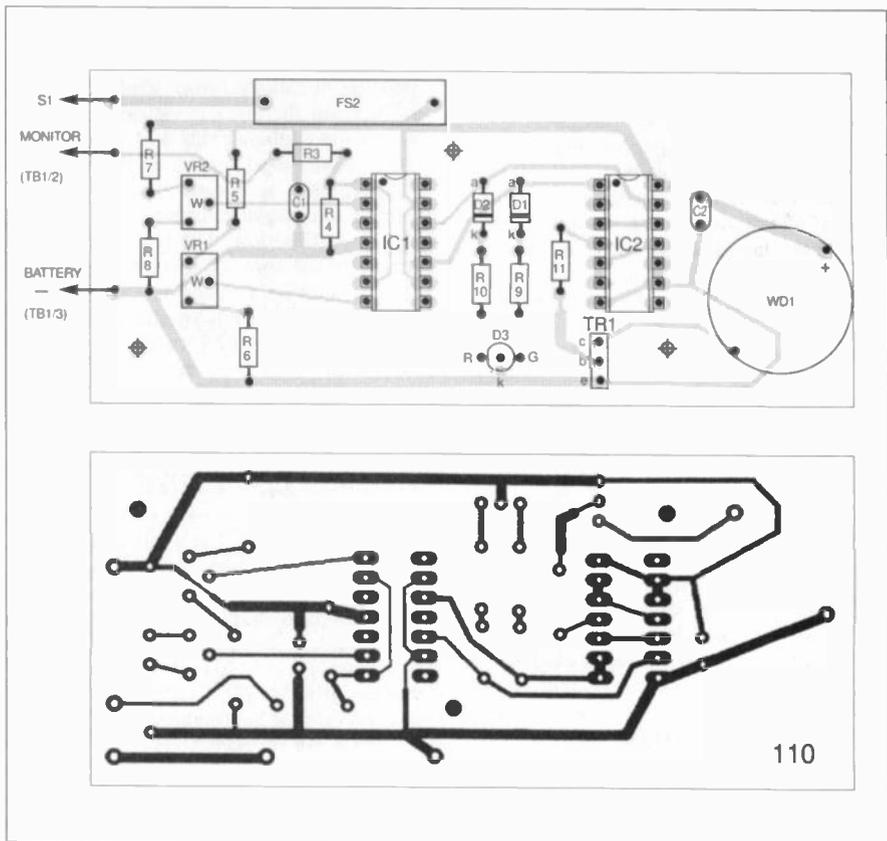


Fig. 3. Printed circuit board topside component layout and full size underside copper foil master pattern.

Begin construction by mounting fuseholder FS2 and the two i.c. sockets (but do not insert the i.c.s themselves yet) on the p.c.b. Add the passive components - the resistors (including the preset potentiometers) and capacitors.

Solder the buzzer into position - this is polarity-sensitive and the correct orientation is usually marked on the plastic body underneath. Add the transistor and diodes, also being conscious of their correct polarity.

Gently bend the leads of the tri-colour l.e.d. D3 at right angles and solder them to the p.c.b. so that the body points forward as shown in the photograph. Note that the centre lead is the common connection and the shorter one operates the green section.

Adjust the wiper (sliding contact) of both presets to approximately mid-track position. Solder 10cm pieces of stranded connecting wire to the points marked "S1", "monitor" and "battery -".

## CASE

Refer to the photograph and drill three holes in the base of the box to correspond with those in the circuit board. Drill holes for the terminal block and for the tag-board, to be used for mounting resistors R1 and R2.

Drill a hole in the front panel for the l.e.d. clip and one for the switch. Drill a hole in the rear panel for fuseholder FS1 and one for the wires to pass through to the terminal block via a rubber grommet.

## COMPONENTS

### Resistors

R1, R2	0 $\Omega$ 1 (0.1 ohms)	See
	3W (2 off)	
R3	10k	TALK Page
R4	47k	
R5, R7	18k (2 off)	
R6, R8	120k (2 off)	
R9, R10	470 $\Omega$ (2 off)	
R11	22k	

All 0.25W 5% carbon film, except R1 and R2.

### Potentiometers

VR1, VR2 22k min. preset, vert. (2 off)

### Capacitors

C1, C2 220n ceramic disc (2 off)

### Semiconductors

D1, D2	1N4148 signal diode (2 off)
D3	tri-colour l.e.d., 5mm, plus mounting clip
TR1	ZTX300 npn transistor, or similar
IC1	LM747 dual op.amp
IC2	4011B quad 2-input NAND gate

### Miscellaneous

WD1	piezo buzzer, p.c.b. mounting, 5mA 3V-24V d.c.
S1	min. toggle switch (or rocker or slide switch)
FS1	10A 20mm fuse, plus 20mm panel mounting fuseholder
FS2	250mA fuse, plus 20mm p.c.b. mounting fuseholder

Printed circuit board available from the *EPE PCB Service*, code 110; aluminium case, size 125mm x 105mm x 35mm; 14-pin d.i.l. socket (2 off); 15A screw terminal block - 3 sections required; tag board - 6 tags required; 10A rated wire; light-duty stranded connecting wire; cable ties; grommet; solder, etc.

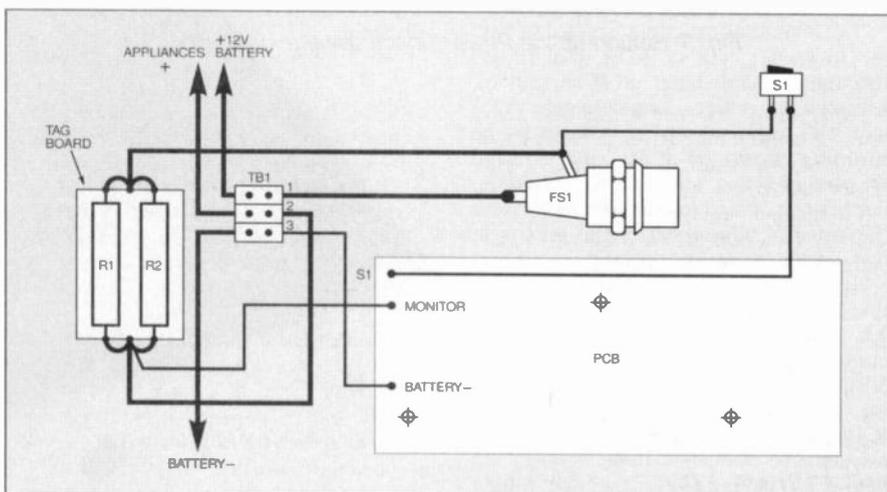


Fig. 4. Interwiring details between the printed circuit board and off-board components. Note that heavy-duty 10A wire must be used where indicated by thicker leads.

Approx Cost  
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£20

## EXTENSION

Solder power resistors R1 and R2 to the piece of tagboard as shown in the photograph and Fig.4, leaving some space between them. Solder the link wires to their ends so that they are connected in parallel.

Mount the tagboard assembly on plastic stand-off insulators so that it is kept 5mm clear of the bottom of the box. This is because the tag connections on the underside are not insulated.

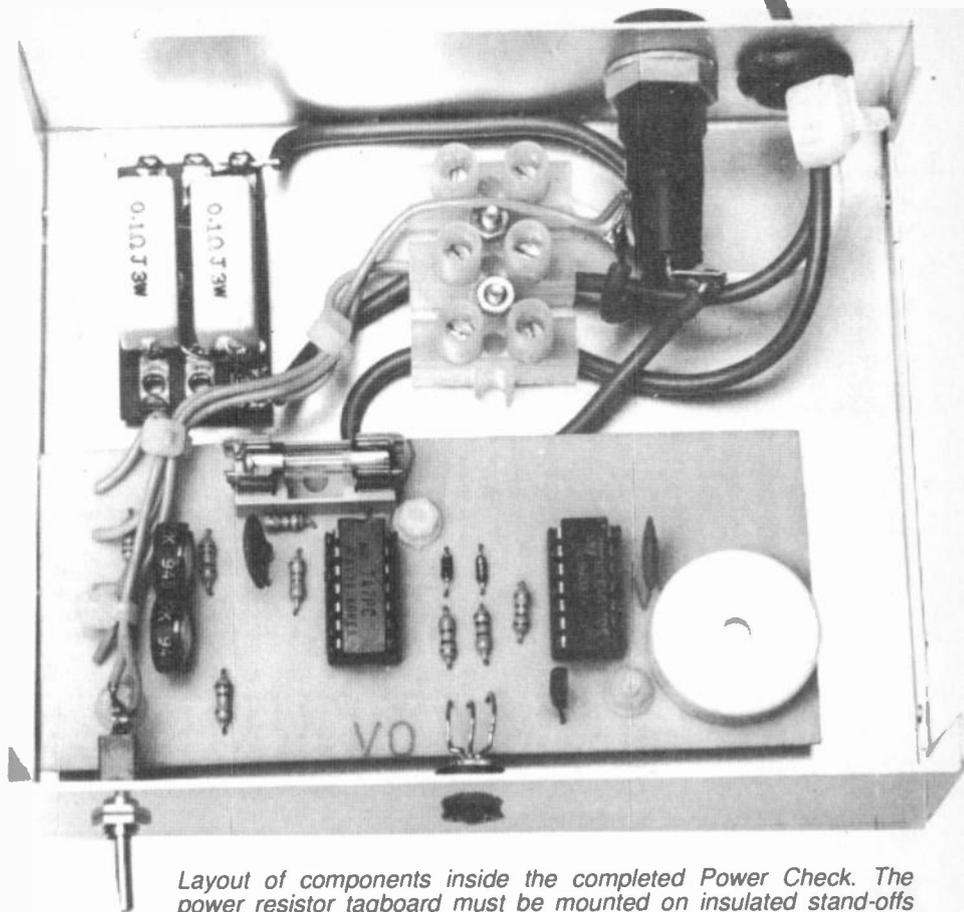
Mount the terminal block TB1, fuseholder FS1 and the toggle switch. Attach the circuit board using plastic stand-off insulators on the bolt shanks to keep the underside connections on the p.c.b. 5mm clear of the box. At the same time, engage the l.e.d. in its mounting clip and secure it.

Refer to Fig.4 and complete the internal wiring. No wires should touch resistors R1 and R2 since these become hot in operation. Note that all wiring drawn with thick lines must be of 10A rating *minimum*.

You now need to locate the main feed wire from the battery positive terminal. This needs to be cut at a convenient point. The free end leading directly to the battery positive terminal is connected to the terminal block point TB1/1, while that leading to the appliances is connected to TB1/2.

The wires may be extended to reach a convenient place for the main unit but such extensions must be kept as short as possible. Also, the wire used must be appropriate to the maximum current being drawn. If this procedure is not observed, there could be an excessive voltage drop along the new wiring and a consequent reduction in current to the appliances, and the wiring could get hot!

The connection to TB1/3 is made to the battery negative terminal using light-duty stranded wire. Apply some strain relief to



Layout of components inside the completed Power Check. The power resistor tagboard must be mounted on insulated stand-offs above the base of the case and heavy-duty wires used where indicated (thicker leads) in Fig. 4.

meters usually have a suitable high range. If no such ammeter is available, the circuit may, of course, be set up by common sense. If using an ammeter, include it in the circuit as shown in Fig.5.

Begin with a partially-discharged battery. Switch on S1 and operate appliances

## IN USE

Fit the lid of the case, checking to avoid trapped wires and short circuits. If the audible warning is not loud enough, drill a matrix of small holes in the top section of the box above buzzer WD1 position.

If the unit is operated close to its upper current limit for any significant time, resistors R1 and R2 will become very hot. This should not cause a problem, but it would be a good idea to check that the case does not become excessively hot. If necessary, drill some ventilation holes above the tag board position. Working below 5A, the case should remain cool although R1 and R2 will still become fairly hot.

Switch S1 operates the warning circuit. However, if it is switched off, the appliances will still work. This may be useful for items which may be switched on while the user is out or at night, for example.

The Power Check circuit requires a maximum of 80mA (with Yellow showing) so it imposes little load on the system. However, there is no point in using it when it is not required.

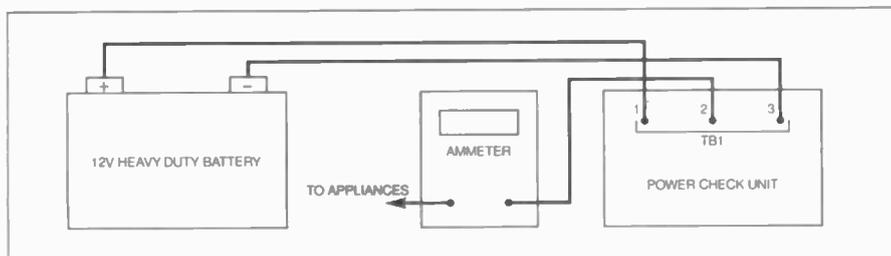


Fig. 5. Setting-up the Power Check using an ammeter.

the wires inside the case where they enter through the grommet. In the prototype this was done by securing a large cable tie around them.

IC1 requires no particular handling precautions. However, IC2 is a CMOS device and could possibly be damaged by static charge which might exist on your body. For this reason, before unpacking IC2, touch something which is earthed (such as a water tap, or soldering iron metal parts – when cold!). This will remove the static charge. Insert both i.c.s into their holders, observing the correct orientation.

## SETTING-UP

For adjustment to specific current values, an ammeter (multimeter set to the 10A d.c. range) will be needed. Digital

such as lights so that the required low current limit is obtained. Adjust preset VR1 so that the display just turns from green to yellow. Switch on more appliances until the upper limit is reached. Adjust preset VR2 so that the display just changes from yellow to red – the buzzer should sound. Repeat and check the settings.

Note that when an appliance is switched on it is quite usual for there to be a momentary surge of current. This is particularly true of filament lamps, fluorescent lights and motors such as those used in water pumps. Do not be surprised, therefore, if a green display gives a transient yellow response or a yellow display becomes red for an instant and the buzzer gives a ‘chirp’.



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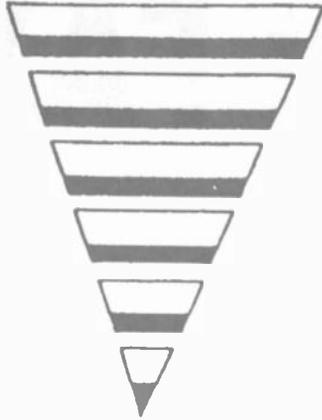
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# DOWN TO EARTH



George Hylton

## CASCADING OPERATIONAL AMPLIFIERS

THE GAIN of an operational amplifier (op.amp) can be very high – up to several million. Very few practical applications call for such a high gain and it's usual to reduce it by applying negative feedback.

This allows the gain to be set to any required figure below the "inner" (open-loop) gain. It also increases the range of frequencies over which the gain is constant.

## NOISE

The laws of physics dictate that noise is always present in practical circuits. The amount of noise depends on many factors, including temperature and bandwidth. In many practical applications (audio, radio) it's hard to make the noise at the input of an amplifier less than about a microvolt.

If the gain is one million then a microvolt at the input gives a volt at the output. To drown the noise the input signal should be a thousand times larger, say one millivolt. If this were amplified by a million the output would be a kilovolt.

Nobody needs this much (not in the average home, at least) and in practice you can't get it because the circuit overloads and limits the signals. In a word, practical, usable gains are relatively low.

Reducing gain by negative feedback can't reduce the input noise but the output noise undergoes the same reduction as the gain. Let's put in some numbers.

An audio power amplifier may need an input signal of 100mV. A typical audio signal of 1mV then needs to be preamplified by 100. Some signals may be under 1mV but gains of more than 1000 are seldom needed.

## D.C. ERRORS

Trouble can arise if the d.c. gain of an op.amp is high. The amplifier has two

input terminals (inverting (-) and non-inverting (+)).

Ideally these should be at exactly the same d.c. voltage. In practice they aren't. There's a difference, called the "input offset voltage".

For a cheap op.amp this might be 5mV. This acts like a d.c. input signal and gets amplified. Thus a d.c. gain of 1000 turns it into 5000mV (5V) at the output.

This is a serious shift in level. It will at the very least limit the a.c. output voltage swing and at worst may stop the amplifier from working at all.

If your supply voltage is 5V then an attempt on the circuit's part to shift the working point by the same amount just pushes the output as hard up to the supply rail voltage as it can go. Even much smaller d.c. shifts cause premature overload and consequent peak clipping. Steps must be taken to keep the d.c. gain well below the a.c. gain.

same as at the input, which is normally negligible.

In practice the improvement may not be as much as this simple reasoning predicts. There is an additional source of error in the shape of d.c. flowing in resistor R2.

Some d.c. does flow! It's the "input bias current" and though small it has an effect when R2 is large.

In my tests, one of the four op.amps of an LM324 i.c. gave a shift in d.c. output voltage of 120mV when R2 was changed from zero to ten megohms (10M). This implies an input bias current of typical 12 nano-amps. However, the LM324 data quote a typical bias current of 20nA (which would give 200mV d.c. shift) and a maximum bias (at 25°C) of 250nA, which would give a nasty shift of 2.5V.

A remedy is to insert equal resistance in the other input lead (shown dotted in Fig. 1). When I did so the additional d.c. error at the output fell to 14mV.

In fact, 10M is ridiculously high for this op.amp. In real life you would use a much lower resistance or an op.amp with a much lower bias current, e.g. one with f.e.t. inputs.

There is a price to be paid for using the low-resistance solution. To preserve the l.f. response capacitor C1 must be made larger, increasing cost and bulk.

## SPACE SAVING

Even if you don't mind the cost, the space taken by blocking capacitors can be an embarrassment on a crowded circuit board. For this reason, as well as for cost reduction designers try to minimise the number of capacitors.

The easiest way is to use op.amps with low offset voltage and low input bias current. Bias is small in f.e.t.-input amplifiers, but very low offset voltage calls for special chips which are expensive. Offsets down to about a microvolt are available, but they cost a lot more than the 30p (pence) or so you pay for an LM324.

The simplest and cheapest way of connecting one op.amp to the next is *direct coupling* (Fig. 2). Here the voltage error of the first stage is reduced by a combination of capacitive input coupling and resistance equalisation (R3).

The resulting d.c. error at its output (shown here as 5mV) is fed to the next stage. This amplifies it (tenfold) to

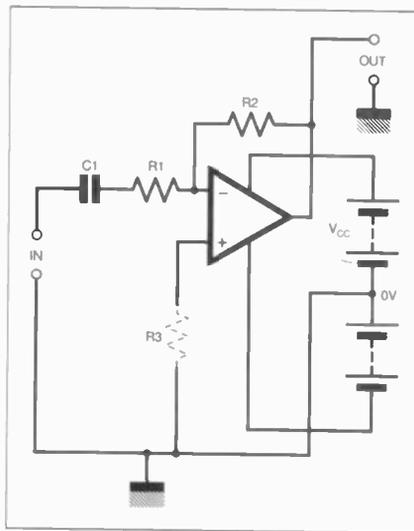


Fig. 1. Blocking capacitor C1 ensures that d.c. negative feedback is maximised.

## CAPACITIVE COUPLING

The insertion of d.c. blocking capacitors in a.c. paths can reduce the effective d.c. gain drastically. In Fig. 1 capacitor C1 ensures that the full d.c. output voltage is fed back via resistor R2 to the inverting terminal. This reduces the d.c. gain to 1, which means that the d.c. error at the output is the

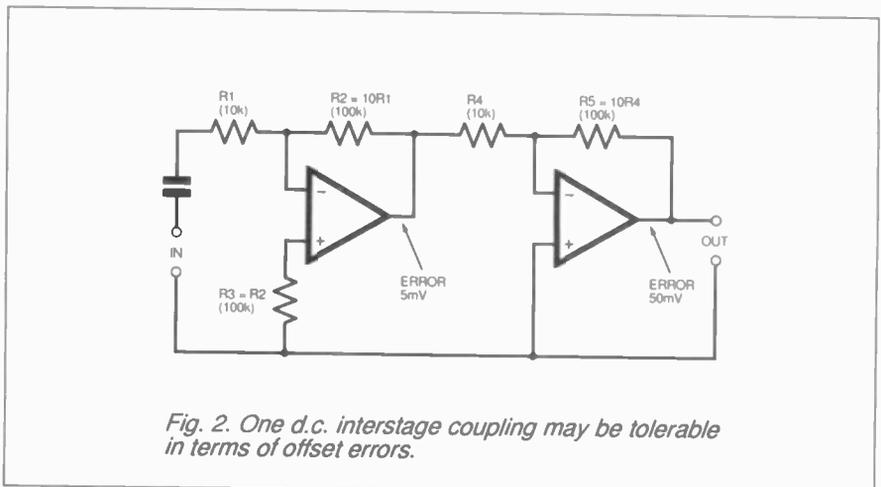


Fig. 2. One d.c. interstage coupling may be tolerable in terms of offset errors.

50mV but this may well be tolerable. Clearly, the situation is worsened if the second-stage gain is higher.

**MULTISTAGE FEEDBACK**

If a gain of 1000 is required, 5mV input offset error becomes 5V output error if nothing is done about it. One possibility is to use overall d.c. feedback to reduce the d.c. gain while leaving the a.c. gain at 1000.

In Fig. 3 the three cascaded inverting stages produce overall inversion, hence d.c. feedback via resistors R7 and R8 is negative. Signal frequencies are shunted off by capacitor C2.

There is one unwanted effect. Operation is delayed by a few seconds after switch-on, as C2 charges. If, to minimise the delay, C2 is reduced there is a reduction in gain at the low-frequency end. Compromise is necessary.

For the record, I found that 10µF gave a -3db point at 300Hz and 100µF gave -3dB at 20Hz. To give bass cut

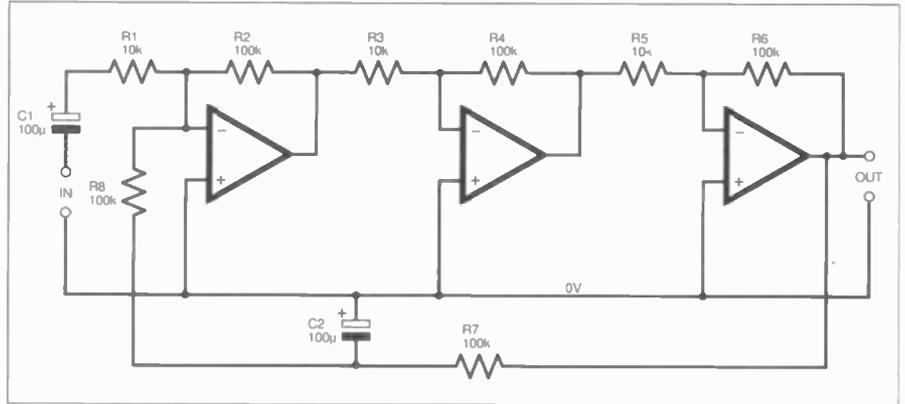


Fig. 3. Overall d.c. feedback stabilises the whole amplifier.

C2 can be made deliberately small, but may cause a hump in the l.f. response or even instability.

My initial tests used the LM7324 but

it is rather noisy. The TL084 gave equally good results from the d.c. point of view (very small overall d.c. error) despite its poorer offset error.

# INGENUITY UNLIMITED

Continued from page 712

**Model Fire Engine -**

“Blue Watch”

**S**TILL on the theme of model vehicles, Fig. 6 was designed as a circuit to add both a blue flashing light sequence plus a two-tone siren effect, to a model fire engine. IC1 is a quad NAND Schmitt trigger and IC1a provides a low-frequency waveform which is inverted by IC1b.

Thus, complementary outputs are obtained which drive transistors TR1 and TR2. These driver transistors operate D1 and D2 which are two blue l.e.d.s. The model had a blue translucent moulding on its roof and yielded a surprisingly realistic effect.

The outputs from IC1a and IC1b are also used to control gated astables IC1c and IC1d, which are set to oscillate at different frequencies to simulate a typical British two-tone siren sounded by WD1, a piezo disc. Battery B1 should be an alkaline or rechargeable 9V type since the current consumption is relatively high. S1 was a slide switch fitted on the rear of the vehicle. The sounder is optional!

David Geary,  
Blackheath, London.

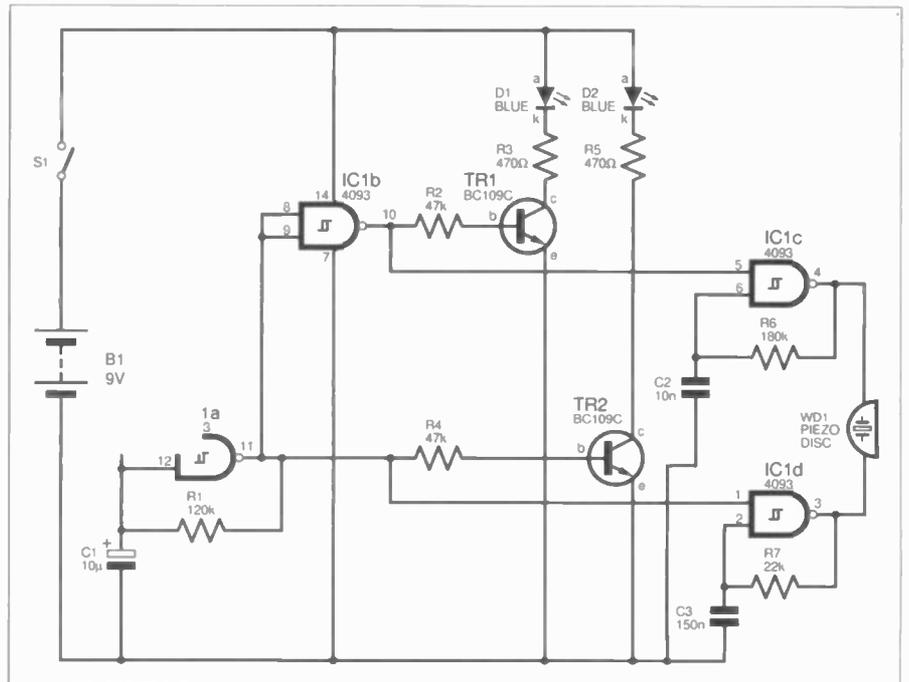


Fig. 6. Circuit for a blue l.e.d. flasher/siren for a model fire engine.

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Although nearly a century has passed since Marconi's first demonstration or radio communication, there is still research and experiment to be carried out in the field of antenna design and behaviour.

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### DESIGN YOUR OWN CIRCUITS

See ELECTRONICS TEACH-IN No. 6 above left.

# TESTING, THEORY, DATA AND REFERENCE

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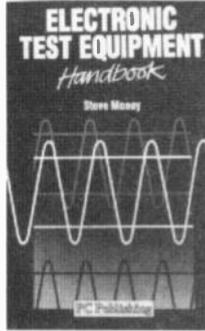
Hans-Günther Steidle

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The wonders of electronics multiply unceasingly and electronic devices are creeping relentlessly into all walks of modern life. As with most professions, ours too has a language of its own, ever expanding and now encompassing several thousands of terms. This book picks out and explains some of the more important fundamental terms (over 700), making the explanations as easy to understand as can be expected of a complicated subject and avoiding high-level mathematics.

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Geoff Phillips

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Owen Bishop

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D. Weale

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The topics covered in this book include: the basic concepts of logic circuits; the functions of gates, inverters and

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119 pages

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R. M. Marston

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They may be designed to produce outputs with sine, square, triangle, ramp, pulse, staircase, or a variety of other forms. The generators may produce modulated or unmodulated outputs, and the

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The manual is divided into eleven chapters, and

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R. A. Penfold

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# AUDIO AND MUSIC

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F. A. Wilson, C.G.I.A., C.Eng., F.I.E.E., F.I.E.R.E., F.B.I.M.

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BP258	Learning to Program in C (revised edition)	£4.95	BP336	A Concise Users Guide to Lotus 1-2-3 Release 3.4	£5.95	BP396	Electronics Hobbyists Data Book	£5.95
BP259	A Concise Introduction to UNIX - Revised Edition	£4.95	BP337	A Concise Users Guide to Lotus 1-2-3 for Windows	£5.95	BP398	Sage Instant Accounting Explained	£5.95
BP261	A Concise Introduction to Lotus 1-2-3 (revised edition)	£3.95	BP341	MS-DOS 6 Explained (covers V6.2)	£5.95	BP399	Windows '95 One Step at a Time	£4.95
BP262	A Concise Introduction to WordPerfect (revised edition)	£3.95	BP343	A Concise Introduction to Microsoft Works for Windows	£5.95	BP400	Windows 95 Explained	£5.95
BP264	A Concise Advanced User's Guide to MS-DOS (revised edition - covers version 6.2)	£4.95	BP345	Getting Started in Practical Electronics	£4.95	BP401	Transistor Data Tables	£5.95
BP273	Practical Electronic Sensors	£4.95	BP346	Programming in Visual BASIC for Windows	£5.95	BP402	MS - Office One Step at a Time	£5.95
BP274	A Concise Introduction to SuperCalc5	£4.95	BP349	Practical Opto-Electronic Projects	£4.95	BP403	The Internet and World Wide Web Explained	£5.95
BP276	Short Wave Superhet Receiver Construction	£2.95				BP405	MS Works for Windows 95 explained	£5.95
BP281	An Induction to UHF VHF for Radio Amateurs	£4.99				BP409	MS Office 95 one step at a time	£6.99
BP284	Programming in QuickBASIC	£4.95						

IF NO PRICE IS SHOWN THE BOOK IS OUT OF PRINT (O.O.P.)  
SEE PREVIOUS PAGE FOR FULL ORDERING DETAILS

## PCB SERVICE

Printed circuit boards for certain EPE constructional projects are available from the PCB Service, see list. These are fabricated in glass fibre, and are fully drilled and roller tinned. All prices include VAT and postage and packing. Add £1 per board for airmail outside of Europe. Remittances should be sent to **The PCB Service, Everyday Practical Electronics, Allen House, East Borough, Wimborne, Dorset BH21 1PF. Tel: 01202 881749.** Cheques should be crossed and made payable to *Everyday Practical Electronics* (Payment in £ sterling only).

NOTE: While 95% of our boards are held in stock and are dispatched within seven days of receipt of order, please allow a maximum of 28 days for delivery - overseas readers allow extra if ordered by surface mail.

Back numbers or photostats of articles are available if required - see the *Back Issues* page for details.

Please check price and availability in the latest issue.

Boards can only be supplied on a payment with order basis.

### Special KNOCK DOWN SALE of PCBs.

We have a few p.c.b.s left from past projects these are being offered at the knock down price of **£1.00 each - no matter what size they are (some of these boards are worth over £9.00 each)** while stocks last. This price includes VAT and UK post - overseas orders please add 50p postage (or £1 per board for airmail postage).

Audio Lead Tester 641; Hand Tally, main board 699 and display board 700; Modular Disco Lights - Masterlink 752 - Dimmer Interface 765; Knockerbox 775; Auto Nightlight 779; Car Electric Window Enhancer, 821; Electronic Fire, 820; Electronic Snooker Scoreboard, 832; Bike Odometer (pair of boards), 836/7; Amstrad PCW A to D Converter (double-sided), 838; Kettle Alert, 843; Linear Power Supply (double-sided), 844; Microphone Pre-Amp module, 846; RIAA Pre-Amp module, 847; 20 Metre Receiver, 848; 1W Stereo Amplifier, 851; Auto Alarm, 854; 10W+10W Stereo Power Amplifier Amplifier, 852a - Power Supply, 852b; Whistle Controlled Light Switch, 860; Battery to Mains Inverter - U.P.S. charger board, 862.

Any of the above for just **£1 each inc. VAT and p&p.**

Back numbers or photostats of articles are available see the *Back Issues* page for details.

**£1.00 EACH inc. VAT and p&p**

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CCD TV Camera - Control Board (double-sided, plated-through-hole)	865	£15.00
Telephone Ring Detector	<b>APR '94</b> 864	£4.72
CCD TV Camera Combined Video, Test & Ext Plug Boards	866a/e	£11.00
Frame Grab Control (double-sided p.t.h.)	867	£15.00
EPE SoundAC PC Sound Board	868	£4.77
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Display Board	870	£18.00
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Stereo Noise Gate	873	£6.14
Simple TENS Unit	875	£5.84
Capacitance/Inductance Meter	876	£6.44
Advanced TENS Unit	<b>JUN '94</b> 877	£6.56
Digital Water Meter - Scaler	878	£11.19
Counter/Display	879	pair
L.E.D. Matrix Message Display Unit		
Keypad	872	£5.19
PC interface	880	£5.82
Microprocessor Smartswitch	881	£5.61
Microcontroller P.I. Treasure Hunter	882	£6.60
Print Timer	<b>JULY '94</b> 874	£5.82
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Simple NiCad Charger	884	£4.98
Stereo HiFi Controller - 1 Power Supply	886	£5.66
Stereo HiFi Controller - 2	<b>AUG '94</b>	
Main Board	887	£7.39
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Dancing Fountains - 1 Pre-amp	889	£5.28
Pump Controller	890	£5.41
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6802 Microprocessor Development Board	894	£9.15
Dancing Fountains - 2	<b>SEPT '94</b>	
PC-Compatible Interface (double-sided)	892	£10.90
Automatic Greenhouse Watering System	895	£5.33
Seismograph - 1 Sensor/Filter	896	£6.23
Clock/Mixer	897	£5.87
3-Channel Lamp Controller	899	£8.17
Seismograph - 2	<b>OCT '94</b>	
PC-Compatible Interface (double-sided)	898	£10.72
Visual/Audio Guitar Tuner	900	£7.55
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Active Guitar Tone Control	907	£4.50
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Video Modules - 1 Simple Fader	910	£5.12
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Rodent Repeller <b>DEC'94</b>	913	£6.26
EPE Fruit Machine	914	£8.14
Video Modules -2 Horizontal Wiper	916	£6.23
Vertical Wiper	917	£6.35
4-Channel Audio Mixer	918	£6.20
Spacewriter Wand	921	£4.00
Universal Digital Code Lock	922	£6.25
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System Mains Power Supply	920	£4.98
Magnetic Field Detector	923	£5.77
Model Railway Track Cleaner	924	£5.11
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The Ultimate Screen Saver <b>FEB'95</b>	927	£5.66
Foot-Operated Drill Controller	928	£5.73
Model Railway Signals	929	£5.96
12V 35W PA Amplifier	930	£12.25
Multi-Purpose Thermostat <b>MAR'95</b>	931	£6.30
Multi-Project PCB	932	£3.00
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Audio Amplifier		
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Switch On/Off Timer		
Continuity Tester		
Auto Battery Charger	934	£5.36
National Lottery Predictor	935	£5.34
R.F. Signal Generator - R.F./Mod. <b>MAY'95</b>	936	£6.48
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MIDI Pedal	938	£7.78
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PIC-DATS Development System (double-sided p.t.h.)	940	£9.90
EPE HiFi Valve Amplifier - <b>JUNE'95</b>		
Phase splitter	941	£6.71
PIC-DATS 4 -channel Light Chaser	942	£7.90
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Low-Range Ohmmeter Adaptor <b>SEPT'95</b>	926	£5.55
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Boot Control Unit	953	£10.52
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Treble Booster		
Infra-Red Controller/Alarm (2 boards required)		
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Multiple Project PCB <b>NOV'95</b>	932	£3.00
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Current Tracer		
Distortion Effects Unit		
Digital Delay Line	958	£8.04
50Hz Field Meter	959	£8.32
Temperature Warning Alarm (Teach-In '96)	960	£6.15
Stereo "Cordless" Headphones <b>DEC'95</b>		
Transmitter	961	£8.04
Receiver	962	£7.66
EPE Met Office - Sensor/Rainfall/Vane	963/965	£11.33
Spiral transparency free with above p.c.b.		
Light-Operated Switch	966	£6.37
Modular Alarm System (Teach-In '96)	967a/b	£7.12
Audio Meter and Amplifier	968	£5.99

PROJECT TITLE	Order Code	Cost
EPE Met Office - <b>JAN'96</b>		
Computer Interface (double-sided)	964	£7.69
Audio Signal Generator	969	£6.58
Mains Signalling Unit, Transmitter and Receiver	970/971 (pr)	£9.09
Automatic Camera Panning (Teach-In '96)	972	£6.63
Printer Sharer	973	£9.93
Analogue Frequency Meter <b>FEB'96</b>	957	£6.70
Vari-Speed Dice (Teach-In '96)	974	£5.69
Mains Signalling Unit - 2		
12V Capacitive PSU	975	£6.07
PIC-Electric Meter - Sensor/PSU- Control/Display	977/978 (pr)	£9.90
Multi-Purpose Mini Amplifier <b>MAR'96</b>	976	£6.12
PIC-Electric - Sensor/PSU - Control/Display	977/978 (pr)	£9.90
High Current Stabilised Power Supply	979	£6.62
Mind Machine Mk III - Sound and Lights	980	£7.39
Infra-Zapper Transmitter/Receiver (Teach-In '96)	981/982 (pr)	£8.01
Mind Machine Mk III - Programmer <b>APRIL'96</b>	983	£7.36
Bat Band Converter/B.F.O.	984a/b	£5.80
Hearing Tester	985	£6.87
Event Counter (Teach-In '96)	986	£8.39
B.F.O. and Bat Band Converter <b>MAY'96</b>	984a/b	£5.80
Versatile PIR Detector Alarm	988	£6.76
Mind machine Mk III - Tape Controller	989	£6.70
Midi Analyser	992	£6.74
Countdown Timer (Teach-In '96)	993	£9.44
Sarah's Light <b>JUNE'96</b>	996	£7.17
Home Telephone Link	997 (pr)	£10.72
PuLStar	998	£6.60
VU Display and Alarm	999	£7.02
Ultra-Fast Frequency Generator <b>JULY'96</b>		
and Counter - Oscillator/L.C.D. Driver	994/995 (pr)	£12.72
Timed NiCad Charger	100	£6.99
Single-Station Radio 4 Tuner	101	£7.02
Twin-Beam Infra-Red Alarm - Transmitter/Receiver		
Games Compendium	102/103 (pr)	£10.50
	104	£6.09
Mono "Cordless" Headphones <b>AUG'96</b>		
- Transmitter/Receiver	990/991 (pr)	£10.16
Component Analyser (double sided p.t.h.)	105	£12.18
Garden Mole-Ester	106	£6.07
Mobile Miser	107	£6.36
Bike Speedo	108	£6.61
PIC-Tock Pendulum Clock <b>SEPT'96</b>	109	£6.31
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Analogue Delay/Flanger	111	£7.95
Draught Detector	112	£6.22
Simple Exposure Timer	113	£6.63

## EPE PRINTED CIRCUIT BOARD SERVICE

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# SURFING THE INTERNET

# NET WORK

ALAN WINSTANLEY



**A**T LAST! We have more and more readers gaining access to the Internet and we also receive numerous enquiries, especially from the USA, asking about us, who we are, what kind of material we carry and how much we cost. A World Wide Web site is often the best way to answer these and other queries and so we're pleased to announce the opening of our own WWW pages, which will be found on <http://www.epemag.wimborne.co.uk>. This will just have opened up by the time you read this.

We plan to "grow" the site to meet the needs of our readers. The site will be constantly updated with new material as it takes shape, including back issue information, subscription and ordering details, plus pointers to other sites which we hope will help readers everywhere.

We are also uploading PIC source files to our new file area <ftp://ftp.epemag.wimborne.co.uk> where you will also find the very latest version of my own UK Sources FAQ, a file of well over 200 names, addresses, URL's, phone numbers etc. of UK based electronics related products and services.

In association with the Dept. of Electronic Engineering, the University of Hull, England, we plan to link with the University to bring you the latest developments in research and education over at Hull, which will be of interest to students and hobbyists worldwide.

Every year students at Hull undertake a "design and build" project. This year the students will be working in "companies" to design and build a computer-controlled "Mouse Organ". All resources for the project will be web based, and we'll post a running commentary on how the "companies" are going. Last year's project, to design a digital telephone, resulted in a formation of a company called "Lemon" (after the "Orange" mobile phone network) with the catch phrase "The Future is Bleak, the Future is Lemon".

It's going to be great fun! Please join us and keep checking our progress regularly. We'll keep you posted with developments, in *Net Work* and immediately on our web site itself. And of course, if you have any comments, let us know. E-mail to [alan@epemag.demon.co.uk](mailto:alan@epemag.demon.co.uk) or write to us at the Editorial address.

## Turnpike Trauma

When choosing an Internet Service Provider (ISP), it's well worth investigating the type of mail on offer, and confirming what particular software package an ISP might recommend for you to handle their mail service. Some service providers (e.g. BT Internet, CompuServe, Pipex and AOL) provide you with their own access software as part of the package, so there's no problem for most users. With others, e.g. Demon, you're on your own to choose whichever package you prefer.

E-mail comes in two flavours, and you'll hear both names mentioned from time to time. SMTP (Simple Mail Transfer Protocol) is favoured by some ISP's including Demon Internet Services. The good part is that SMTP mail is formatted as `<username>@domain.name`. With my own domain name of [epemag.demon.co.uk](mailto:epemag.demon.co.uk), I can set up as many usernames as I wish, at no extra cost, and my SMTP software will sort it all out on my PC when received. Mail delivery is controlled by your ISP you (hopefully) get the lot when you dial in – but it is sorted by your software.

POP3 (Post Office Protocol) mail just sits on the ISP's server, and you dial in to download it onto your own machine. POP3 mail generally stays on the server until you decide to delete it.

The free software *Pegasus* is excellent at choosing and handling incoming POP3 mail: but it doesn't handle incoming SMTP mail. Many folks prefer to use SMTP (or, are given it anyway) but POP3 is useful in applications where one user needs one mailbox only, or where users need to dial in from other locations.

## Mail-lite

Turnpike software is supposedly capable of handling "multiple" mailboxes (usernames). Or so they said on their Web pages, in their manuals and in their software Help files. What they fail to tell you is that it doesn't handle *multiple* POP3 mailboxes but only one single one.

When it came to the crunch, Turnpike let us down badly when we configured an E-mail system for our new domain. We expected Turnpike to handle all of our POP3 mailboxes just as it does SMTP mail. When we actually pressed the "Add" button to add the next POP3 username onto the system, up popped a message saying "Multiple mailbox collection – sorry not yet". No greyed out or disabled button, nothing.

We were peeved to find buried deep in the small print of one Turnpike Help screen, a note saying "Add not available in this version." Turnpike offered our money back "if we thought we had been misled".

Turnpike is an odd package, seemingly aimed at network users, but with various bits disabled as they adapt it for single user, single machine use. They wouldn't say when (or even if) it will handle multiple POP3 mail, and they respectfully suggested that I should have read the disclaimer label on the box, which says that "it does what it does".

Perhaps Turnpike should have changed its Web site and Help files accordingly to say what it doesn't do, as well. None the less, I still recommend it for use with SMTP mail including Demon's, or single user POP3 mail. It includes Netscape V1.22 as well. More interestingly, Turnpike (a.k.a. Locomotive Software – remember the Amstrad PCW?) was purchased by Demon Internet Services last December, and Locomotive was hived off.

On another note, there is a lot to be said for picking a smaller, local ISP and we're glad to say we're very happy with Total Connectivity Providers Ltd. in Southampton (tel. 01703 393392) who have national local dial-in and provide our E-mail and newly launched world wide web and ftp sites. POP3 is their mail standard, by the way. See <http://www.tcp.co.uk>.

## Browsing

Time to fire up your WWW browser – check these URL's! As always, addresses were checked at the time of going to press but may sometimes move. Engineers dealing with EMC and other thorny regulations might try the web page of *Approval Magazine* which resides at <http://www.compulink.co.uk/~Approval>. It gives one or two pointers. Also the Institute of Electrical Engineers have their own web page at <http://www.iee.org.uk>.

A very impressive World Wide Web site handling almost anything to do with integrated circuits, is the famous *Chip Directory*, which you should definitely bookmark as a resource. It's at [http://xs4all.nl/~ganswijk/chipdir/chip\\_dir.html](http://xs4all.nl/~ganswijk/chipdir/chip_dir.html). An increasing number of semiconductor data sheets are available on-line (needing Adobe Acrobat reader) from *Premier Farnell* in Leeds, now the world's largest catalogue-based component distributor, who will be found on <http://www.farnell.co.uk>.

Batteries are next, and <http://www.duracell.com> is where you'll find technical data on those famous copper-coloured tops, button cells, photography batteries and more. It's a slow, graphics laden site but well worth the stopover. I found the (American) Energiser site less worthwhile; <http://www.eveready.com> describes their latest battery tester product but is again graphics-heavy.

Still on batteries, to go hand-in-hand with this month's *Circuit Surgery*, get the NiCad FAQ from Steve Walz's FTP site at <ftp://ftp.armory.com/pub/user/rstevew/nicadfaq.zip> (13k). You'll see other interesting files there too.

Finally, welcome aboard to *Henry's Radio* in London, very old established component suppliers whose modest web site is on <http://www.henrys.co.uk>. See you next month for more *Net Work*.

## DC TO DC CONVERTERS

DRM58 input 10-40vdc output 5v 8A £15  
DRM128 input 17-40vdc output 12v 8A £50  
DRM158 input 20-40vdc output 15v 8A £50  
DRM248 input 29-40vdc output 24v 8A £40  
DRS123 input 17-40vdc output 12v 3A £20  
DRS153 input 20-40vdc output 15v 3A £20  
DRS243 input 29-40vdc output 24v 3A £15

## SOLID STATE RELAYS

CMP-DC-200P 3-32vdc operation, 0-200vdc 1A £2.50  
SMT20000/3 3-24vdc operation, 28-280vac 3A £4.50  
SMT20000/4 3-24vdc operation, 28-280vac 4A £5.00  
ZRA6025F 28-280vdc operation, 28-280vac 25A £7.00

**200 WATT INVERTERS** Nicely cased units, 12v input 240v output 150watt continuous, 200 max. £49 ref LOT62.

**6.8MW HELIUM NEON LASERS** New units, £65 ref LOT33

**COIN SLOT TOKENS** You may have a use for these? mixed bag of 10 tokens £10 ref LOT20.

**PORTABLE X RAY MACHINE PLANS** Easy to construct plans on a simple and cheap way to build a home X-ray machine! Effective device, X-ray sealed assemblies, can be used for experimental purposes. Not a toy or for minors! £65 set. Ref F/XPJ.

**TELEKINETIC ENHANCER PLANS** Mystify and amaze your friends by creating motion with no known apparent means or cause. Uses no electrical or mechanical connections, no special gimmicks yet produces positive motion and effect. Excellent for science projects, magic shows, party demonstrations or serious research & development of this strange and amazing psychical phenomenon. £45 set Ref F/TKE1.

**ELECTRONIC HYPNOSIS PLANS & DATA** This data shows several ways to put subjects under your control. Included is a full volume reference text and several construction plans that when assembled can produce highly effective stimuli. This material must be used cautiously. It is for use as entertainment at parties etc only, by those experienced in its use. £15 set Ref F/EH2.

**GRAVITY GENERATOR PLANS** This unique plan demonstrates a simple electrical phenomena that produces an anti-gravity effect. You can actually build a small mock spaceship out of simple materials and without any visible means - cause it to levitate. £10 set Ref F/GRA1.

**WORLDS SMALLEST TESLA COIL/LIGHTENING DISPLAY GLOBE PLANS** Produces up to 750,000 volts of discharge, experiment with extraordinary HV effects, 'Plasma in a jar', St Elmo's fire, Corona, excellent science project or conversation piece. £5 set Ref F/BTC1/LG5.

**COPPER VAPOUR LASER PLANS** Produces 100mw of visible green light. High coherency and spectral quality similar to Argon laser but easier and less costly to build yet far more efficient. This particular design was developed at the Atomic Energy Commission of NEGEV in Israel. £10 set Ref F/CV1.

**VOICE SCRAMBLER PLANS** Miniature solid state system turns speech sound into indecipherable noise that cannot be understood without a second matching unit. Use on telephone to prevent third party listening and bugging. £6 set Ref F/V59.

**PULSED TV JOKER PLANS** Little hand held device utilises pulse techniques that will completely disrupt TV picture and sound works on FM too! DISCRETION ADVISED. £8 set Ref F/TJ5.

**BODYHEAT TELESCOPE PLANS** Highly directional long range device uses recent technology to detect the presence of living bodies, warm and hot spots, heat leaks etc. Intended for security, law enforcement, research and development, etc. Excellent security device or very interesting science project. £8 set Ref F/BHT1.

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**MYSTERY ANTI GRAVITY DEVICE PLANS** Uses simple concept. Objects float in air and move to the touch. Defies gravity, amazing gift, conversation piece, magic trick or science project. £6 set Ref F/ANT1K.

**ULTRASONIC BLASTER PLANS** Laboratory source of sonic shock waves. Blow holes in metal, produce 'cold' steam, atomize liquids. Many cleaning uses for PC boards, jewelry, coins, small parts etc. £6 set Ref F/ULB1.

**ULTRAHIGH GAIN AMP/STETHOSCOPIC MIKE/SOUND AND VIBRATION DETECTOR PLANS** Ultrasensitive device enables one to hear a whole new world of sounds. Listen through walls, windows, floors etc. Many applications shown, from law enforcement, nature listening, medical heartbeat, to mechanical devices. £6 set Ref F/HGA7.

**ANTI DOG FORCE FIELD PLANS** Highly effective circuit produces time variable pulses of acoustical energy that dogs cannot tolerate. £6 set Ref F/DOG2.

**LASER BOUNCE LISTENER SYSTEM PLANS** Allows you to hear sounds from a premises without gaining access. £12 set Ref F/LLIST1.

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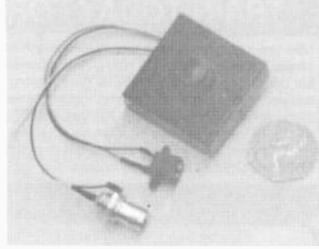
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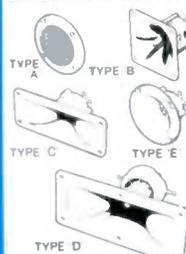


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**TYPE 'D' (KSN1025A)** 2" x 6" wide dispersion horn. Upper frequency response retained extending down to mid-range (2KHz). Suitable for high quality Hi-Fi systems and quality discos. Price £9.99 + 50p P&P.  
**TYPE 'E' (KSN1038A)** 3½" horn tweeter with attractive silver finish trim. Suitable for Hi-Fi monitor systems etc. Price £5.99 + 50p P&P.  
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**PRICES: 150W £49.99 250W £99.99**  
**400W £109.95 P&P £2.00 EACH**

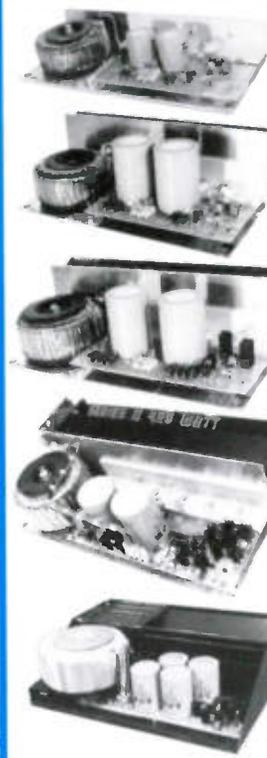
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**ALL POWERS INTO 4 OHMS**

**Features:**  
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**THOUSANDS OF MODULES PURCHASED BY PROFESSIONAL USERS**



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**OMP/MF 200 Mos-Fet** Output power 200 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor >300, Slew Rate 50V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB. Size 300 x 155 x 100mm.  
**PRICE £64.35 + £4.00 P&P**

**OMP/MF 300 Mos-Fet** Output power 300 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor >300, Slew Rate 60V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB. Size 330 x 175 x 100mm.  
**PRICE £81.75 + £5.00 P&P**

**OMP/MF 450 Mos-Fet** Output power 450 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor >300, Slew Rate 75V/uS, T.H.D. typical 0.001%, Input Sensitivity 500mV, S.N.R. -110 dB, Fan Cooled, D.C. Loudspeaker Protection, 2 Second Anti-Thump Delay. Size 385 x 210 x 105mm.  
**PRICE £132.85 + £5.00 P&P**

**OMP/MF 1000 Mos-Fet** Output power 1000 watts R.M.S. into 2 ohms, 725 watts R.M.S. into 4 ohms, frequency response 1Hz - 100KHz -3dB, Damping Factor >300, Slew Rate 75V/uS, T.H.D. typical 0.002%, Input Sensitivity 500mV, S.N.R. -110 dB, Fan Cooled, D.C. Loudspeaker Protection, 2 Second Anti-Thump Delay. Size 422 x 300 x 125mm.  
**PRICE £259.00 + £12.00 P&P**

**NOTE: MOS-FET MODULES ARE AVAILABLE IN TWO VERSIONS: STANDARD - INPUT SENS 500mV, BAND WIDTH 100KHz. PEC (PROFESSIONAL EQUIPMENT COMPATIBLE) - INPUT SENS 775mV, BAND WIDTH 50KHz. ORDER STANDARD OR PEC.**

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  - 6" 60WATT EB6-60TC (TWIN CONE) HI-FI, MULTI-ARRAY DISCO ETC.** RES. FREQ. 38Hz, FREQ. RESP. TO 20KHz, SENS 94dB. PRICE £10.99 + 1.50 P&P
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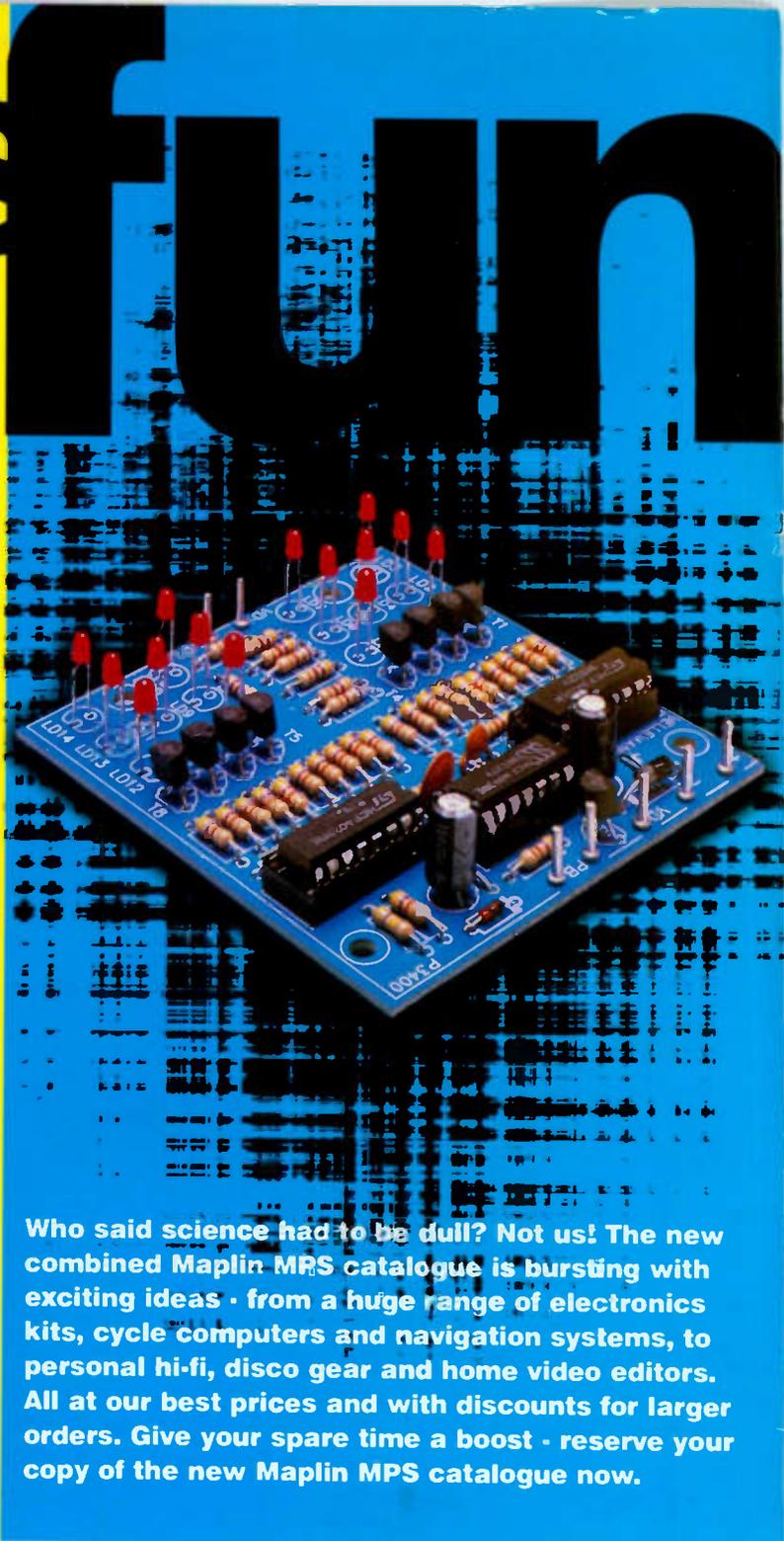
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