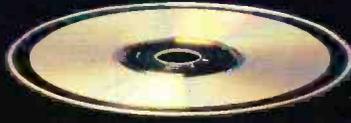


DECEMBER 1982-FEBRUARY 1983

PRICE 60p

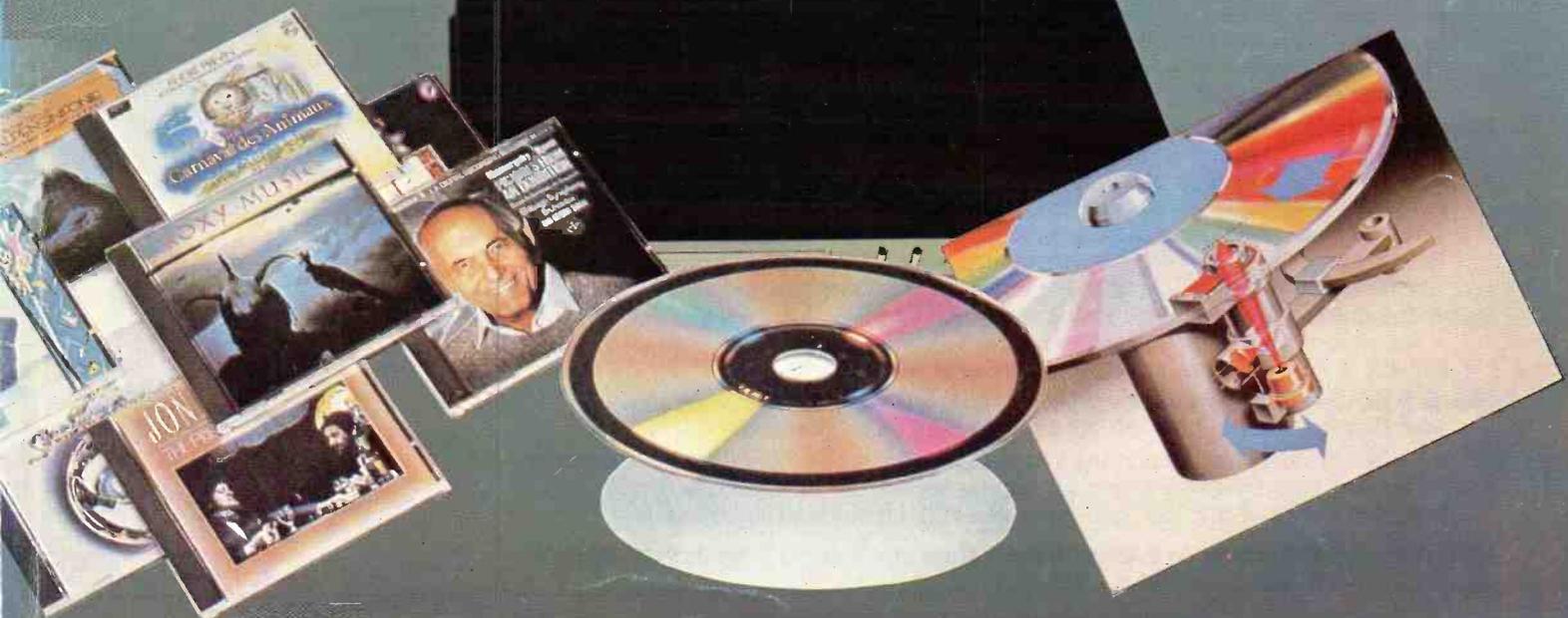
Electronics

THE MAPLIN MAGAZINE



**AS HI-FI TAKES A GIANT
STEP FORWARD WE ASK —
HAS THE LP HAD ITS CHIPS?**

**CCITT STANDARD MODEM
CENTRAL HEATING CONTROLLER
SOUNDS GENERATOR FOR ZX81
BURGLAR ALARM PANIC BUTTON
AND MANY MORE!**



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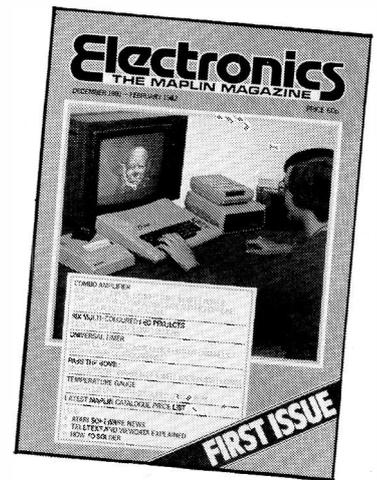
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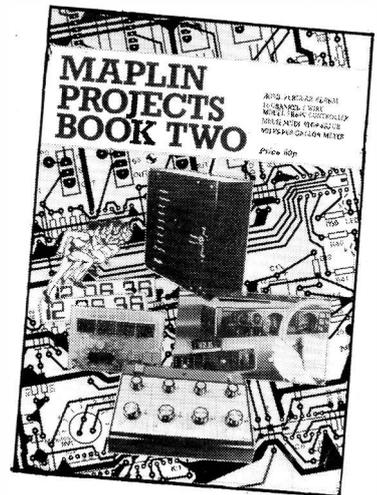
Digital Multi-Train Controller. Our superb digital train controller can control up to 14 locomotives individually on the same track. Any four loco's can be controlled simultaneously. The unit has automatic short-circuit protection and because it uses digital control a DC supply is present all the time for carriage lighting etc. The locomotive modules will fit in most modern 00-scale engines. Complete construction details.

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Radar Doppler Intruder Detector. Home Office type-approved microwave unit gives coverage adjustable from about 2m to 20m. May be used on its own, or with our Home Security System.

Model Train Controller Remote Control Facilities. Full details of infra-red, radio or wired remote control units for our Digital Multi-Train Controller.

Issue 3 also included features on the VIC20 Colour Computer, Working with Op-Amps Part 2, Making Your Own PCB's and our regular feature series: Basically BASIC, Starting Point, news of the Atari computer and video game and lots more.

All this for just 60p. Order As XA03D (Maplin Magazine Volume 1 No 3) Price 60pNV



A NEW CATALOGUE FOR 1983

At the same time that this magazine hits the news stands our new catalogue for 1983 will be available. It will be on sale in all branches of W.H. Smith from about 17th November for just £1.25. For 392 pages this represents a page-for-page price increase of just 2% over two years. Considering that inflation topped 15% a year during that period, we're sure you'll agree that the Maplin catalogue is still incredible value for money.

Consequently in this issue of the magazine, the price list in the centre has been re-ordered for use with the new catalogue. If you don't have a copy yet, you can still use the price list with your old catalogue by looking under the appropriate section heading. If the item you are looking for is no longer in the list then it has probably been discontinued as only a few items have been moved from one section to another.

In the new year our dial-up service will be available allowing you to access our computer stock file. In the meantime a service is available that will allow you to test out the modem project. Just dial (0702) 552941 and you will be able to access our computer. The computer is usually available from 9 a.m. to 7 p.m. Mondays to Fridays. For our trade customers we are introducing a new service that will provide quantity prices if required. If you want to buy the quantity (shown in brackets in the price list) or more then we can offer very competitive prices. And the more you buy, the better the price will be. Take advantage of our quantity price discounts now. Just write to or phone our sales desk.

We've got dozens of exciting new projects lined up for 1983 as well. The most popular project from our first year was the ZX81 Keyboard and our other computer add-on projects were also extremely well-received. We will therefore have lots of new projects on this theme through 1983. In addition we have lots of other novel projects under development and we're sure you'll find your new subscription well worth the money.

Electronics

THE MAPLIN MAGAZINE

November 1982 to February 1983 Vol.2 No.5

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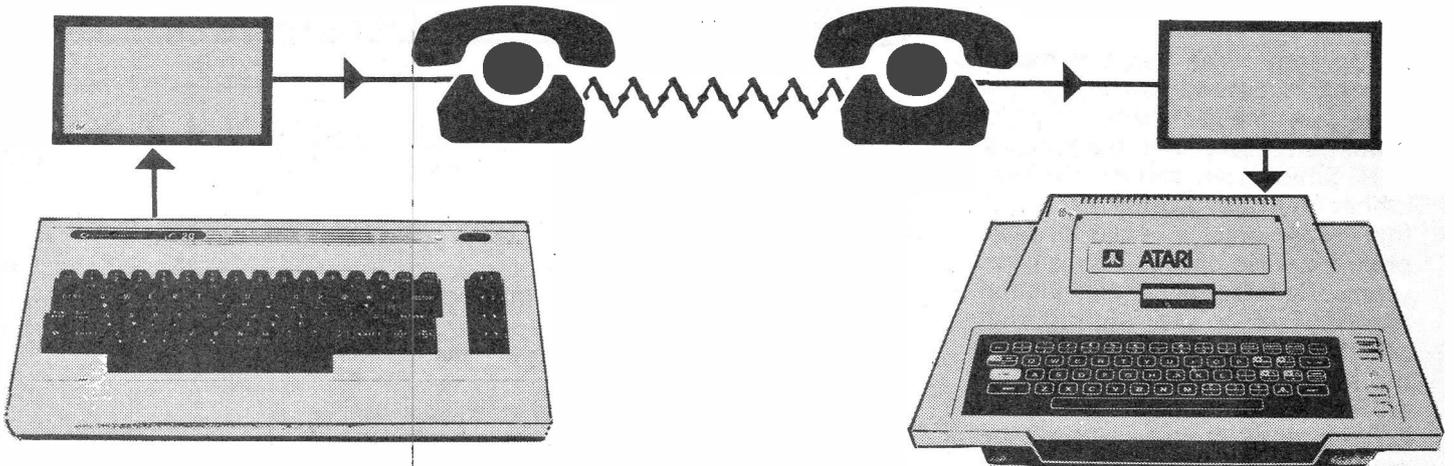
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THE MAPLIN MODEM



- ★ CCITT standard MODEM
- ★ Communicate with other computers
- ★ Easy-to-build
- ★ Exchange programs with other computer users

by Harold Godwin

This modem will enable a home computer or VDU to communicate with other computers using CCITT standard tones, over the telephone. This means that you will be able to exchange programs with other people and in particular have direct access to the Maplin computer to order components etc. A modem works by converting the data input of marks and spaces, to two different audio frequencies. These audio tones are transmitted down the phone line to the other end where they are converted back to a digital signal by the modem.

So that data can be sent in both directions, four different frequencies are used, two for each direction. In order that two modems can communicate, one must be switched to the originate mode, which transmits 980 and 1180 Hz, and the other must be switched to the answer mode and transmits 1650 and 1850 Hz. Each modem receives the alternate pair of frequencies to those which it transmits.

The lower frequency is the mark

condition in each case and it is usual for the terminal that makes the call to be switched to the originate mode. To prevent interference between the two directions of communication, filters are needed to pass the required frequencies in each direction. Although the frequency shift is only 200Hz, the required bandwidth of these filters depends upon the baud rate. At a baud rate of 300 baud and sending alternate marks and spaces, the first sidebands occur ± 150 Hz from the carrier which is located midway between the mark and space frequencies. Therefore the minimum bandwidth for the filters is 300Hz.

Unfortunately a signal passing through a filter is delayed in time. All frequency components of the signal should be delayed equally, or jumbling and smearing of the data occurs. This is known as intersymbol or interbit interference. Minimising the delay distortion minimises the interbit interference. This is relatively easy over the centre 2/3 of the passband, but keep-

ing the delay constant near the band edges is difficult, if not impossible to achieve. For this reason the bandwidth is widened. To maintain minimum delay at 300 baud requires an overall bandwidth of 400Hz. The overall performance of the modem is mainly dependant on the response of the filters, particularly the receive BPF (band pass filter).

Circuit

Two specialised IC's are used in this modem, the first is the 4412VP which is used to generate the required frequencies from a 1 MHz crystal. This IC is capable of transmitting American or CCITT standard frequencies, but pin 14 is earthed for the CCITT standard. The IC is switched between originate and answer by earthing pin 10 for the originate mode. The following pins are permanently earthed. Pin 15 which enables internal pull up resistors, reset pin 5, and pin 13 to inhibit a 2100 Hz tone which is normally transmitted for disabling line echo suppressors. Pin 12 is a carrier disable pin, no tone is

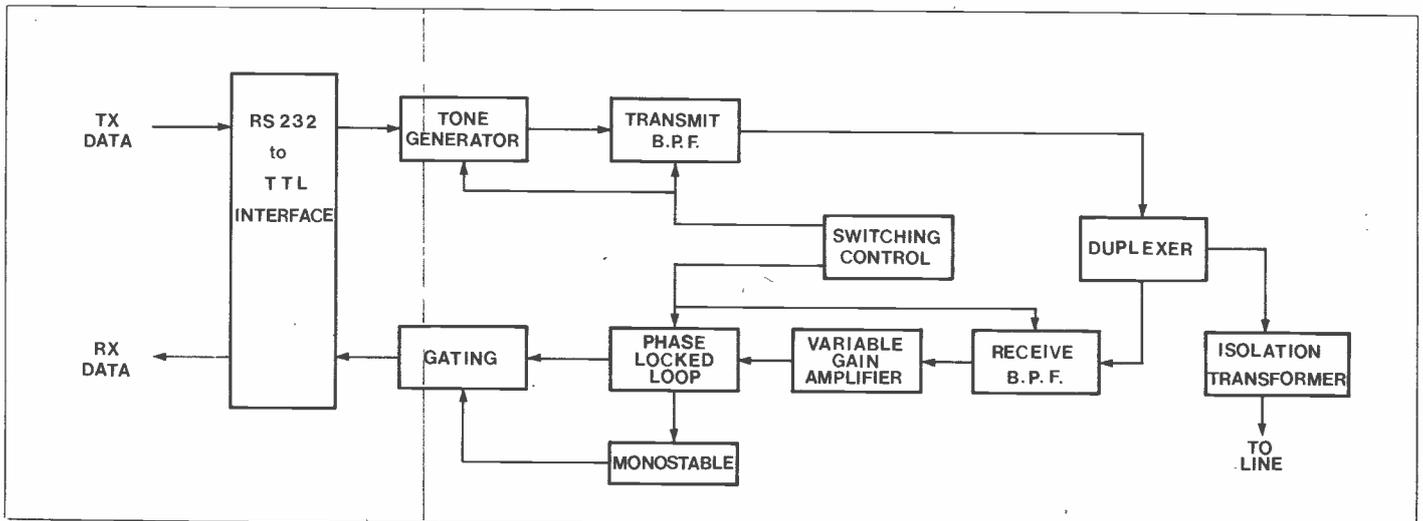
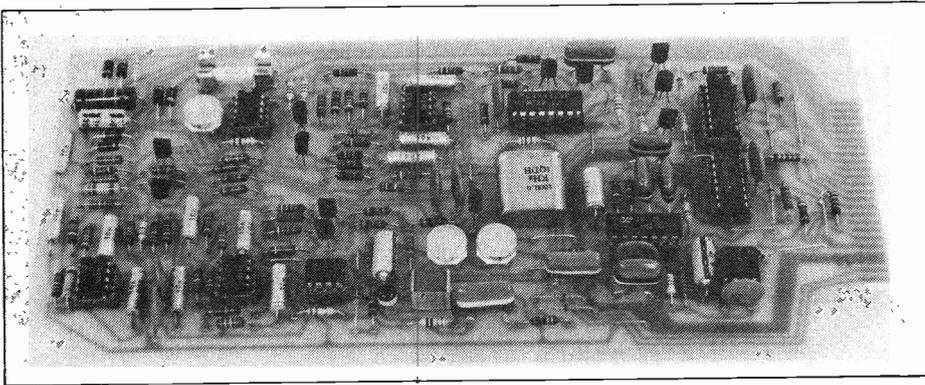
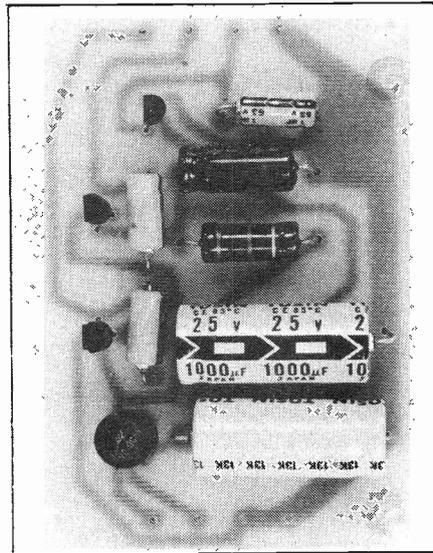


Figure 1. Modem block diagram



transmitted when this is earthed, but this facility is not used at present. Data is input to the IC on pin 11 and the audio tone is output on pin 9. The modulator output is an approximated stepped sine wave of 8 amplitude levels. Although each step is optimised so that the waveform has a maximum amount of signal energy at the fundamental frequency, a large number of harmonics are produced. For this reason, and to limit the transmitted bandwidth, the output is buffered by TR1 and passed through the transmit filter. The transmit filter, consisting of IC2 and associated components, is switched between originate and answer frequencies by TR3, 4, and TR1 switches the 4412VP.

There are two methods of connecting a modem to the phone system, acoustic coupling or direct electrical connection. Acoustic coupling has the advantage of being electrically isolated and easy to connect. However, there are problems, one is trying to exclude room noise, particularly if operating in a noisy environment. Another is the fact that the transmit tones will be heard in the telephone receiver considerably louder than the tones that are trying to be received. Although the receive filter would reduce this, there is a problem when operating in the originate mode. When transmitting a mark frequency of 980Hz, harmonic distortion (mainly from the carbon microphone of the handset) produces a second harmonic of 1960Hz. As this is close to the receive band of 1550 to 1950Hz, the receive filter provides little rejection and this interferes with the received signal. For these reasons it was decided to connect the modem to the phone line via a



British Telecom approved transformer.

Duplexer

The transmit filter output and receive filter input are connected to the line via a duplexer and isolation transformer. This allows the received signal to pass to the receive filter, properly couples the transmit signal to the line, terminates the line and attenuates the transmit signal appearing at the receive filter input. For maximum attenuation $R16 = R17$ and $RV3$ should equal the line impedance. $RV3$ is adjusted for maximum attenuation of the transmit signal. Although the line impedance is nominally 600 ohms, it will have a reactive as well as a resistive component. Therefore the duplexer should be considered as providing about 10db of attenuation, although in many cases better results will be obtained. D1 and D2 protect the

modem from voltage surges from the line.

Receive filter

The receive filter consists of IC4, 5 and associated components. It is switched between the originate and answer frequencies by TR5 to TR8. It is an 8 pole Chebyshev filter and provides 35db of attenuation of the alternate channel. The overall gain of the filter is about 20db (less when receiving 1550 to 1950Hz). Close tolerance components are required for the filters and the resistor values are made up from two resistors in the majority of cases. IC6 is used as a variable gain amplifier to adjust for different receive levels. The output signal is rectified by D3 and used to control TR9 which acts as a variable impedance, adjusting the proportion of the output signal fed back to pin2. D4 and D5 limit the signal fed to IC7 to about 1.5V p to p.

Phase locked loop

Originally it was planned to use the demodulator section of the 4412VP to decode the received tones. Unfortunately the demodulator has been optimised for 200 baud when receiving CCITT tones, so in order to work at 300 baud it was decided to use an XR2211. This IC is a phase locked loop system especially designed for data communication. Referring to the block diagram for this IC, the input signal applied to pin 2 is amplified, limited and fed to the loop phase detector and quadrature detector. The output from the loop phase detector, at pin 11, is a DC voltage proportional to the phase difference between the VCO (voltage controlled oscillator) and the input signal. This voltage is filtered by C18, R46 and applied to pin 12 to control the VCO frequency. This locks the VCO onto the input signal and the control voltage at pin 11 is dependant on the incoming frequency over the tracking range of the VCO.

The control voltage is filtered by R45, C23 and compared with an internal reference voltage. As the input frequency changes the control voltage above and below the reference voltage, the data output on pin 7 changes. The reference voltage is decoupled by C22 on pin 10, and C19, R47, R48, RV1, RV2 determine the free running frequency of the VCO, which is set midway between the mark and space frequencies. The VCO frequency is switched between originate and answer mode by TR10.

The quadrature phase detector compares the VCO and the input frequency and outputs a voltage when the VCO is locked to the input frequency. This voltage is filtered and drives the lock detect outputs. IC8 is a monostable which drives the lock detect LED and is gated with the data output from IC7. This allows data to be received only while the VCO is in lock and prevents spurious data filling the screen when there is no input signal.

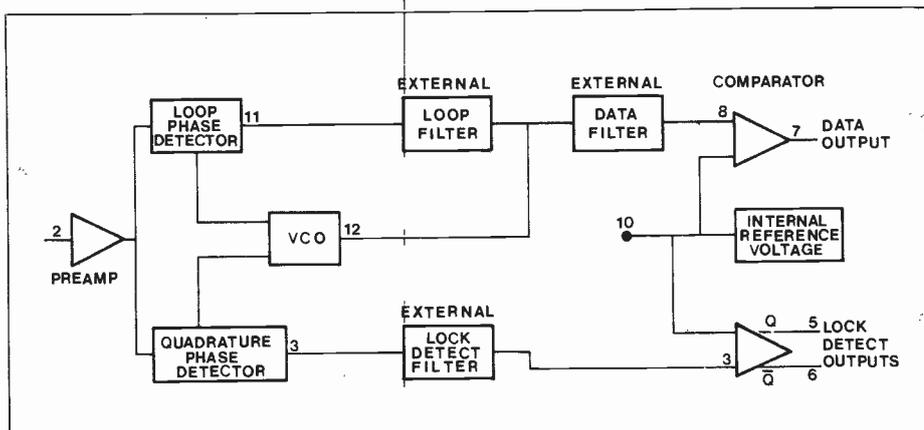


Figure 2. XR2211 block diagram

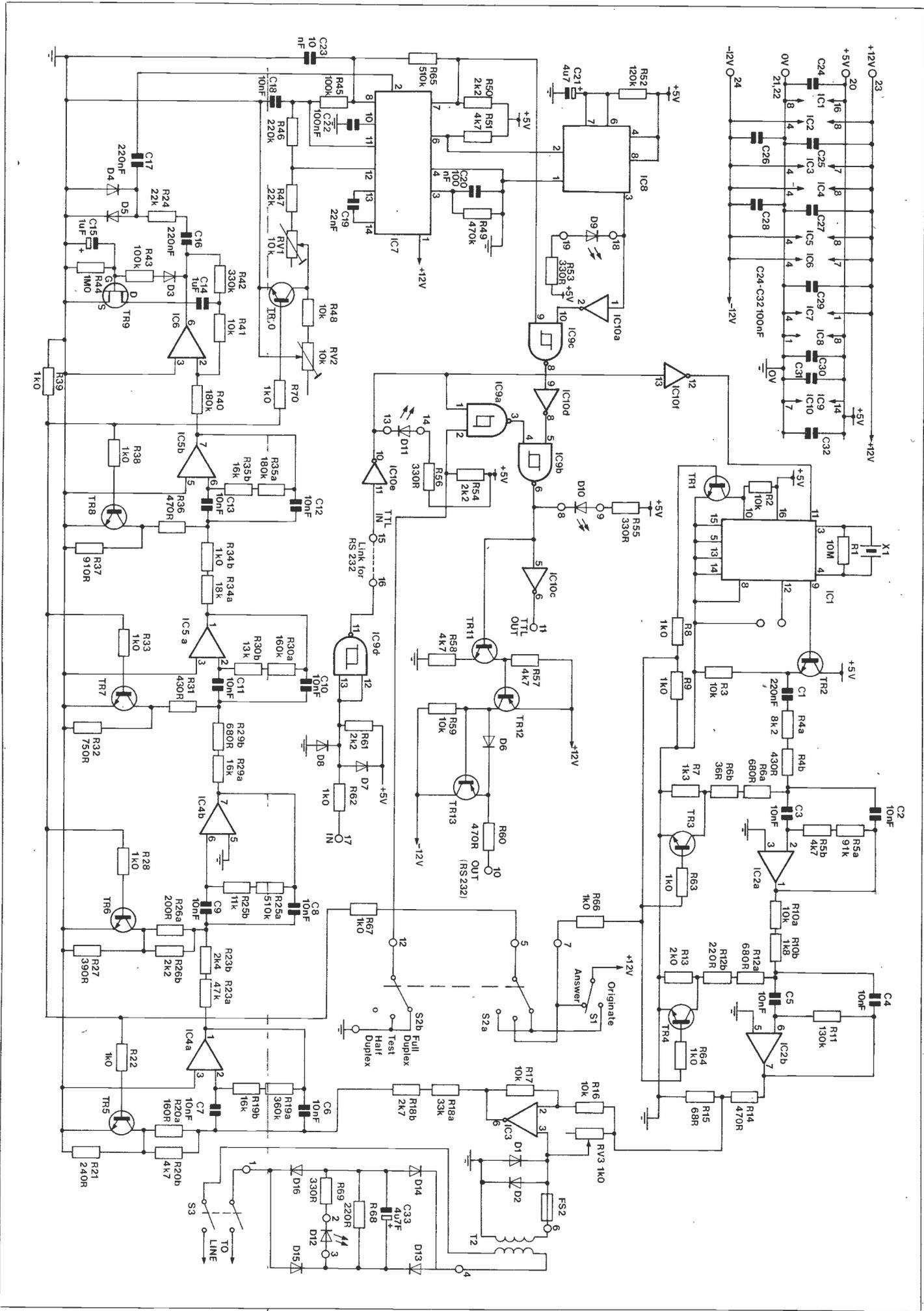


Figure 3. Modem main cct diagram

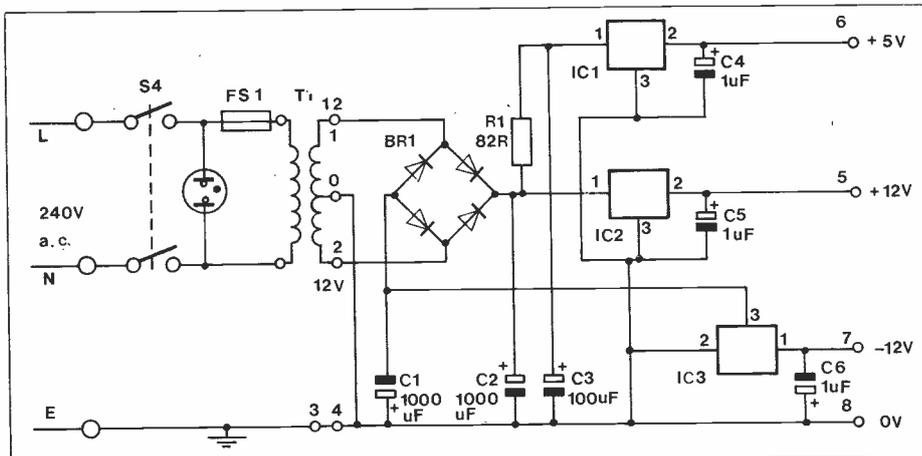
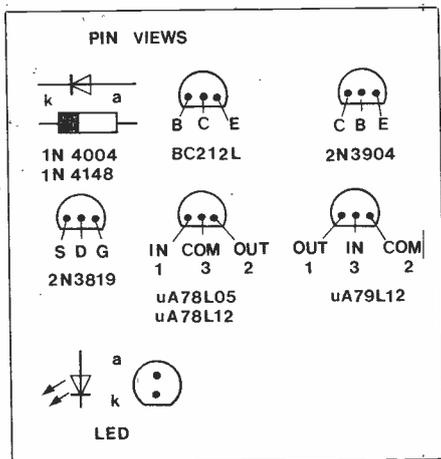


Figure 4. PSU circuit diagram

S1 switches the modem between originate and answer modes, and S2 switches between full-duplex, half-duplex and test positions. Full-duplex working allows data to be sent in both directions at the same time. Normally this means that the data received at the far end is sent back to the sender on the alternate channel. This is displayed on the senders terminal so that it can be seen exactly what was received at the far end. If the data is not echoed back, the modem can be switched to half duplex. This connects the transmit data via IC9a to the receive direction so that the transmitted data is displayed as well as that received. Obviously data cannot be sent in both directions at the same time as garbled information would be displayed. Note also that a mark condition must be received from the other end to allow the local data to be received via IC9b. The test position switches the BPF and IC7 to receive the same frequencies that are being transmitted locally. This allows the modem to be checked in local via the duplexer. This position could also be used to monitor a simplex transmission, when no signal is being received from the other end. D10 and D11 monitor the receive and transmit data respectively and are lit for a mark condition. IC10c

drives the TTL output and TR11 to TR13 convert TTL levels to RS232 interface voltages of +/-12V. At the transmit side D7 and D8 limit the RS232 voltages and IC9d gives TTL level out. The strap must be connected if the RS232 input is used, otherwise IC10 pin 11 is the TTL input. The power supplies of +5V, +12V and -12V are supplied by the three low power regulators and associated components. R1 reduces the power dissipation in the +5V regulator.

Construction

There are two PCB's to be assembled, the main modem board and the power supply unit. These are printed with the component overlay to make assembly easier. Starting with the modem board, the resistors should be fitted first. It is suggested that the values are checked against the circuit diagram, as a wrong value in the filters would affect the response and would be difficult to find. Next the capacitors should be fitted, checking that C15, C21 and C33 are the correct way round.

It is recommended that IC holders are used and these are fitted next, but the IC's not yet inserted. The leads to the 1MHz crystal are bent so that the crystal lies flat against the PCB. The

transistors and diodes are fitted next, checking that they are the correct type and the correct orientation. This leaves just the potentiometers, fuseholder and wire links to be fitted as shown on the legend. The power supply board is assembled in the same way, following the PCB legend.

A suitable case should be chosen from the wide range available that can take the two PCB's and transformers. The front panel should be drilled for the four LED's and switches. The fuse FS1 could be mounted on the front panel or at the back as desired. The 2 transformers should be mounted apart from each other to avoid mains hum. Two connecting sockets will be required to connect to the line and the computer. These are left for the constructor to choose.

The modem PCB plugs into a 24 way connector and is wired up as shown in fig. 5. Lengths of sleeving should be used over the socket connections to prevent short circuits. It is important that the feet are the correct way round, to prevent the PCB being plugged in the wrong way. When the wiring has been completed, the fuses can be inserted and the modem powered up without the IC's in. The power supply voltages should be checked to each IC socket and if correct, the modem switched off. Allow a few minutes for the capacitors to discharge and then insert the IC's and the modem can be tested.

Setting up and Using the System

The modem can be used with any computer that has a RS232 serial interface or the TTL inputs can be connected direct to a UART, if this is available, as on the Maplin VDU. Only 3 wires are needed between the computer and the modem, Tx, Rx data and 0 volts. If using the TTL inputs, these should be kept reasonably short. With S3 unoperated, connect the 2 line connections across the phone line. Normally there are 3 wires from the phone that connect to a terminal block on the wall. The line wires are the Red and the White.

The modem is most easily set up with an oscilloscope as follows. All signals are measured as peak to peak

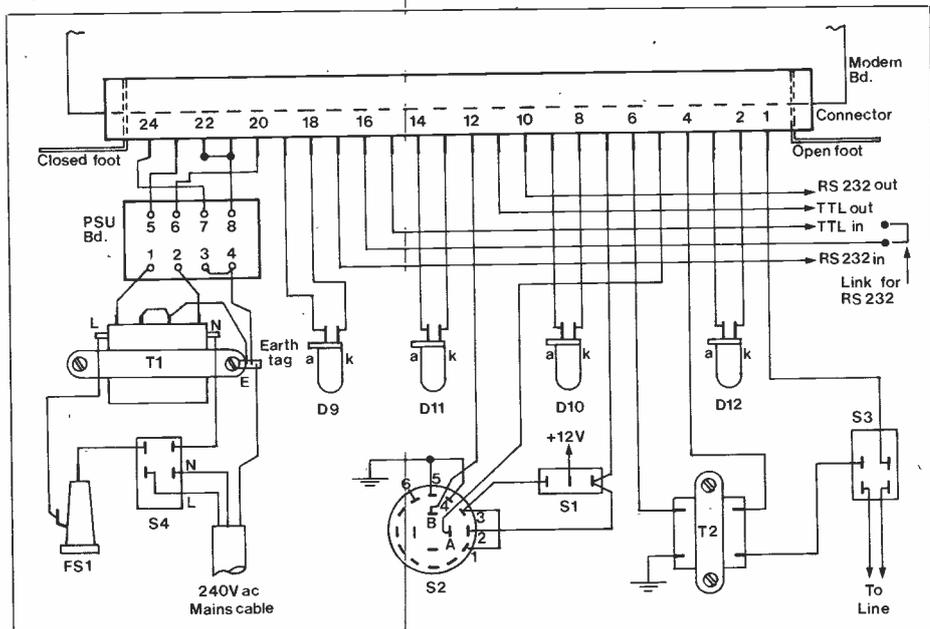


Figure 5. Wiring diagram.

voltages. The signal at TR1 emitter should be a stepped sinewave of 800 mv. The frequency should change if S1 is operated and if the data input is changed. Check the level at IC2B, pin 7. This should be about 8V when S1 is switched to originate, and 6V for answer mode. Dial a '1' from the phone to clear dialtone, operate S3, replace the handset, and D12 should light, showing that the phone line is being held by the modem. Note that no calls can be received while S3 is operated. People ringing the number will get engaged tone. Switch to originate mode and S2 to test. Measure the signal at IC5B pin 7 and adjust RV3 for a minimum signal at this point. Check the signal level at IC3 pin 3 to be around 500mv p to p. Restore S3 to normal and D12 should darken. IC7 has to be adjusted so that the free running frequency is midway

between the mark and space frequencies. The easiest method is as follows. Switch to answer mode and test position, sending alternate marks and spaces, adjust RV1 for equal mark-space ratio at IC7 pin 7. Switch to originate mode and adjust RV2 for equal mark-space ratio. Note RV1 must be adjusted before RV2, as RV2 setting is dependant on RV1. Alternate marks and spaces can be sent by sending the ASCII code for 'U' continuously. The repeat key can be used on a VDU or a short program written for the computer that puts the computer in a loop and outputs ASC(U) to the serial port. The modem is now set up and is used as follows. With S3 normal and D12 unlit, dial the number required. When the number is answered, you must decide which end will be in the originate mode and whether half

or full duplex working will be used. Switch the modems accordingly and operate S3 at both ends. The handsets can now be replaced at each end and data sent in each direction. The carrier lock LED will light when the tone is received from the other end and the receive data LED shows the data received. When you have finished, S3 must be restored to normal to clear down the call. When calling a British Telecom modem with automatic answer-in, the call will be answered after a few rings and then 1650Hz will be sent. Your modem should be switched to originate and a mark sent back within about 10 seconds or else the modem at the far end will clear down and you will have to call again. Normally when your mark is received, a signing on message is sent giving instructions on using the system.

PARTS LIST FOR MODEM MAIN PCB

Resistors - All 0.4W 1% carbon unless specified

R1	10M		
R2, 3, 10a, 16, 17, 41, 48, 59	10k	8 off	(M10M)
R4a	8k2		(M8K2)
R4b, 31	430R	2 off	(M430R)
R5a	91k		(M91K)
R5b, 20b, 51			
57, 58	4k7	5 off	(M4K7)
R6a, 12a, 29b	680R	3 off	(M680R)
R6b	36R		(M36R)
R7	1k3		(M1K3)
R8, 9, 28, 33, 34b, 38, 39, 62, 63, 64, 70, 22, 66, 67	1k0	14 off	(M1K0)
R10b	1k8		(M1K8)
R11	130k		(M130K)
R12b	220R		(M220R)
R13	2k0		(M2K0)
R14, 36a, 60	470R	3 off	(M470R)
R15	68R		(M68R)
R18a	33k		(M33K)
R18b	2k7		(M2K7)
R19a	360k		(M360K)
R19b, 29a, 35b	16k	3 off	(M16K)
R20a	160R		(M160R)
R21	240R		(M240R)
R23a	47k		(M47K)
R23b	2k4		(M2K4)
R24, 47	22k	2 off	(M22K)
R25a, 65	510k	2 off	(M510K)
R25b	11k		(M11K)
R26a	200R		(M200R)
R26b, 50, 54, 61	2k2	4 off	(M2K2)
R27	390R		(M390R)
R30a	160k		(M160K)
R30b	13k		(M13K)
R32	750R		(M750R)
R34a	18k		(M18K)
R35a, 40	180k	2 off	(M180K)
R37	910R		(M910R)
R42	330K		(M330K)
R43, 45	100k	2 off	(M100K)
R44	1M0		(M1M0)
R46	220k		(M220K)
R49	470k		(M470K)
R52	120k		(M120K)
R53, 55, 56	330R	3 off	(M330R)
R68	220R 1W 5% carbon		(C220R)
R69	330R ½W 5% carbon		(S330R)
RV1, 2	10k cermet	2 off	(WR42V)
RV3	1k0 cermet		(WR40T)
Capacitors			
C1, 16, 17	220nF polyester	3 off	(BX78K)
C2-13	10nF polystyrene 1%	12 off	(BX86T)
C14	1uF polycarbonate		(WW53H)
C15	1uF 63V electrolytic axial		(FB12N)
C18, 23	10nF polyester	2 off	(BX70M)
C19	22nF polystyrene 1%		(BX87U)
C20, 22	100nF polyester	2 off	(BX76H)

C21, 33	4 7 63V electrolytic axial	2 off	(FB18U)
C24-32	100nF ceramic disc	9 off	(BX03D)
Semiconductors			
D1, 2, 13-16	1N4004	6 off	(QL76H)
D3-8	1N4148	6 off	(QL80B)
TR1, 8, 10, 11	2N3904	10 off	(QR40T)
TR9	2N3819		(QR36P)
TR12, 13	BC212L	2 off	(QB60Q)
IC1	4412VP		(QQ39N)
IC2, 4, 5	1458	3 off	(QH46A)
IC3, 6	uA 741 8 pin	2 off	(QL22Y)
IC7	XR2211CP		(QY43W)
IC8	NE555		(QH66W)
IC9	74132		(WH03D)
IC10	7404		(QX40T)

Miscellaneous

X1	PC board 1MHz MP crystal Veropin 2141 Fuse clips	1 pkt 2 off	(GB09K) (FY79L) (FL21X) (WH49D) (WR01B)
FS2	Fuse 20mm 250mA		

POWER SUPPLY

Resistors			
R1	82R 1W 5% carbon film		C82R
Capacitors			
C1, 2	1000uF 25V elect. axial	2 off	(FB83E)
C3	100uF 25V elect. axial		(FB49D)
C4, 5, 6	1uF 63V elect. axial	3 off	(FB12N)
Semiconductors			
IC1	uA78L05		(QL26D)
IC2	uA78L12		(W077J)
IC3	uA79L12		(W086T)
BR1	W005		(QL37S)

Miscellaneous

	PC board Veropin 2141	1 Pkt	(GB10L) (FL21X)
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ADDITIONAL PARTS REQUIRED

S1	Switch (Sub. Min Toggle A) SPST		(FH00A)
S2	Switch rotary 3B (BBM)		(FF76H)
S3	Switch (Sub. Min. Toggle E) DPDT		(FH04E)
S4	Switch dual rocker neon		(YR70M)
	Safuseholder 20		(RX96E)
FS1	Fuse 20mm 1A		(WR03D)
T1	Transformer		(WB10L)
T2	Transformer (Line Isolating)		(BK57M)
D9, 10, 11, 12	LED red	4 off	(WL27E)
	LED clip	4 off	(YY40T)
	Edge conn. 124		(FL85G)
	Edge conn. G		(FL91Y)
	Edge Conn. H		(FL92A)

A complete kit of parts is available for this project.
Order As LW99H (Modem Kit). Price £39.95.

IMPROVED TIMER CONTROL

by J. A. Fryer

This is an explanation of a very simple circuit change for 555 or 7555 timers that improves the precision and stability of variable control over frequency ranges up to 4:1, by adding one extra resistor.

The circuit can be adjusted to work over higher ratios but low-end drift grows exponentially; a need for a wide range of control can be satisfied economically by using this circuit in a 2:1 range to clock a binary counter IC with stage switching with no loss in precision. This extension also allows very low frequencies to be generated without hard-to-obtain or less stable large component values.

These very useful low-cost timer IC's get their intrinsic clock stability at a fixed frequency because they are controlled by internal reference voltages of $1/3$ and $2/3 V_{CC}$ from a chain of three nominally equal resistors: these drift, but they drift together very closely and the ratio controls the device. This idea can be applied to external control components, so that the maximum to minimum frequency ratio is set by a pair of resistors, and any drift in a low-cost control potentiometer does not affect output. The pot. can be changed at wear-out while preserving the frequency scale, which turns out to be almost linear in frequency.

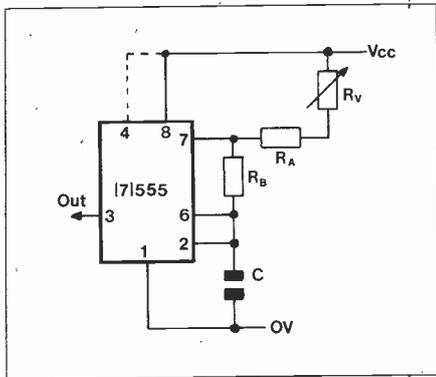


Figure 1. Simplest circuit.

The usual circuit, with a simple frequency control R_v , is shown in Fig. 1. The times of the two part-cycles are

$$C \times R_B \text{ for discharge, and}$$

$$1.46 \frac{C(R_B + R_A + R_v)}{B A v}$$

$$1.46 \text{ for charge}$$

of capacitor C. These add and invert frequency:-

$$f = 1.46 \text{ Hz (megohms, microfarads)}$$

$$C(R_A + R_v + 2R_B)$$

$$A v B$$

The basic device accuracy is $\pm 2\%$, with a little more if V_{CC} changes, and a temperature coefficient of 50 parts per million (or ppm) per degree C. In clockwork terms that is 4.32 seconds per day per degree, a performance not given by clockwork at IC prices.

Trying to use a low-cost pot. for R_v causes immediate problems: at $\pm 20\%$, frequency at the low end is in a 40% band at worst; the pot.

drift will exceed that of all the other parts; the scale is linear in period, not frequency, and gets very cramped at one end for high control ratios. There are ways to reduce these problems, but the only way to achieve precision is to use a high-cost potentiometer, and a good one will cost more than a crystal.

Another approach is to use the device "control" terminal (pin 5), which lets an external voltage force the $2/3V_{CC}$ reference down for a faster cycle or up towards V_{CC} for a slower one. This works, but for stability a lot

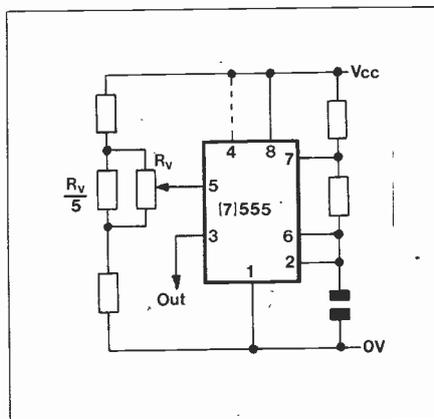


Figure 2. "Control" system.

of power is needed from the external voltage source. The internal resistors are of silicon, with a $\pm 50\%$ production spread, a worse temperature drift than carbon pots., and a quite high voltage variation. An external resistor chain has to "swamp" these variations by having less than one-tenth the resistance of the internal chain for a start. If the external system includes a 20%-grade pot., its variations need another factor of at least five in waste current. With nominal IC chain totals of 15Kohm and 150K (555 and low-current 7555), a design has to start at 300 or 3000 ohms, and less for any real stability. However, the terminal is useful for very wide but not very steady control. Figure 2 shows a fully-padded circuit, which can be simplified with a high-grade pot.

In this "control" mode, capacitor C is charged towards V_{CC} as in the original circuit but the upper trip level is varied. This principle can be inverted, keeping the trip point at $2/3$ but altering the charging level at source to something less than V_{CC} . If a 70% source were used, C would take several time-constants to reach 67% instead of less than one. There is a control limit at a source of 67%: below this the cycle never completes, and close to it drift and noise become problems. The inverted circuit works quite well for small ranges of control, and is shown in Figure 3.

The extra resistor R_C has been added, and R_v moved. At the high and low ends of the control range the pot. is obviously not in circuit. The top frequency is set by R_A and R_C in parallel, and at the low end C is charged towards a fraction $R_C / (R_C + R_A)$ of V_{CC} . The control ratio is given by the resistor ratio in a slightly awkward index equation, which is easier to use when tabulated.

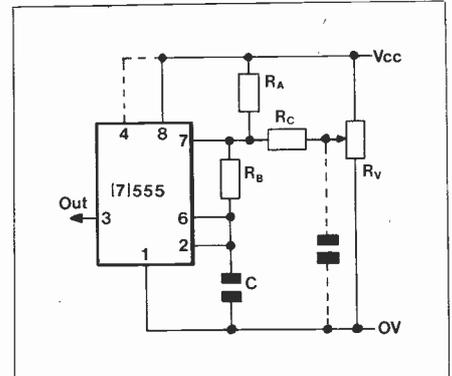


Figure 3. Modified circuit.

At intermediate control settings there is clearly going to be some steady change between the two extremes, and without making one more condition it is not clear what form it takes. This extra condition is that R_v must be well below R_C ; when this is so, the actual value of R_v hardly affects the frequency equation, only its setting fraction of V_{CC} . The pot. can be $\pm 20\%$ and subject to drift without disturbing operation.

The condition is easy to achieve: R_C is already at least $2R_A$, and R_A can be kept very high except at very high frequency. Values of half a megohm will accommodate a 20K pot. with no difficulty, and there is improved stability but not the power loss of the standard "control" system.

There is an equation for frequency against V_{CC} fraction, which is slightly logarithmic. Solving it shows that control is very nearly linear: better than 2% error at 2:1, less than 5% at 4:1. These are about the limits for low-cost pots. with a 0.5 dB or 6% specification. If there is a need for something better, a slightly better pot. has to be used, and it then makes sense to correct the theoretical curvature by one more resistor from ground to slider, which gives total correction at 3 points on the scale.

The table here gives the most useful design ratios:-

F_{max}/F_{min}	R_C/R_A		R_A/R_T
	Theory	Actual	
2	3.500	3.3 + 0.2	1.30
3	2.500	2.3 + 0.2	1.435
4	2.21..	2.15 + 0.15	1.453

The R_A/R_T column is a design aid; the whole of the table assumes R_B is very low compared with R_A . If it is not, stability is not affected, but the frequency ratios are changed and need to be worked out for the actual values, or found on plug-board. If a need for a long pulse makes R_C too close to $2R_A$, it is better to use a dual IC package with one half as a fixed monostable triggered by the variable half with low R_B .

The design calculations are just as for fixed frequency use except for R_C .

- (1) Set F_{max} and the wanted control ratio.
- (2) The original design formula is turned over into the form

$$C \times R_T = F_{max} \text{ Hz, Mohm, microfarads}$$

$$1.46$$

Continued on page 15

COMPACT DISC DIGITAL AUDIO

A NEW WORLD STANDARD

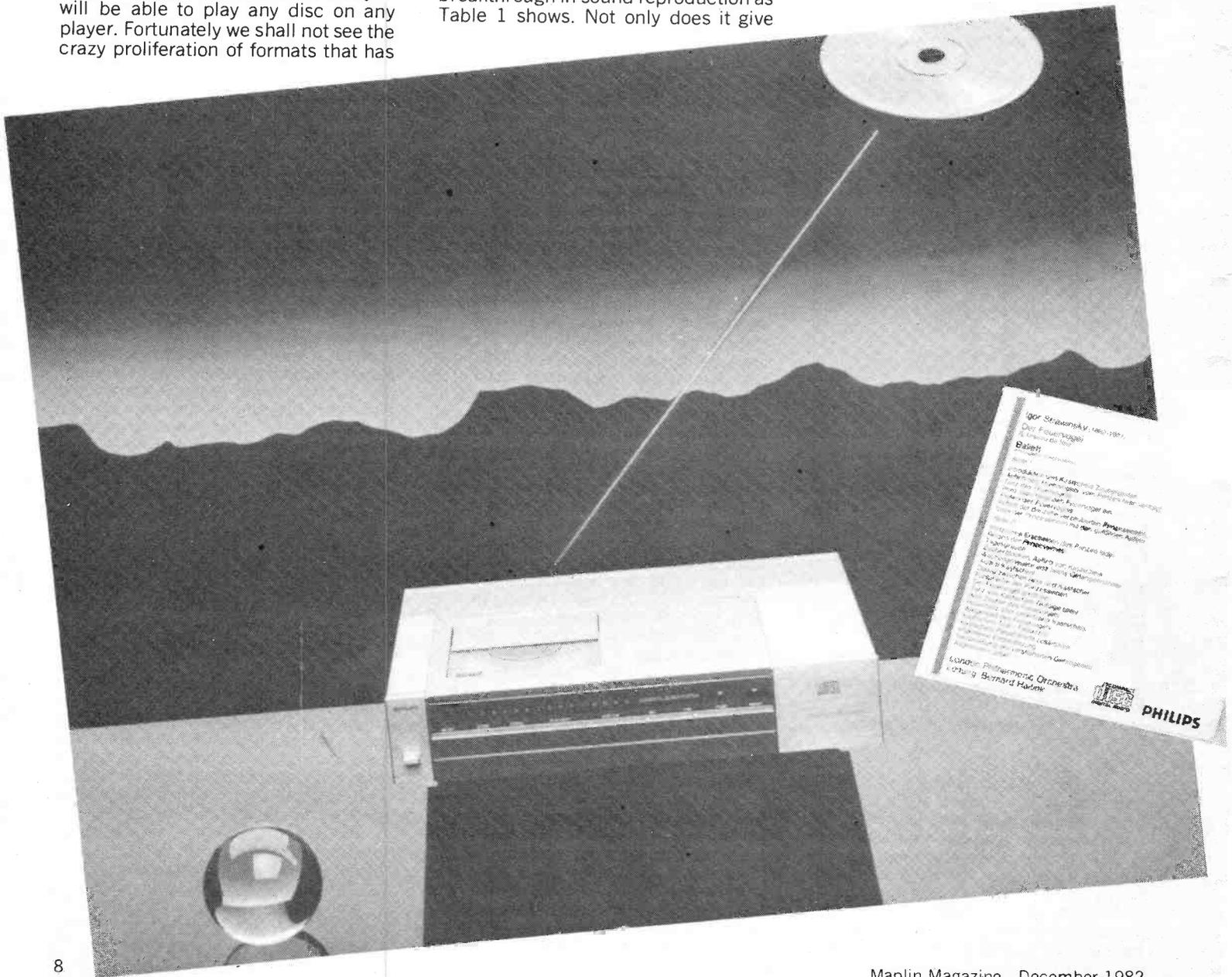
Compact Disc is due to be launched by Philips and several other manufacturers in March 1983 along with about 200 different discs mostly from the Philips group labels. Philips got together with the Japanese electronics giant, Sony, some years ago and the two companies then worked together to create the final format. Philips have now licensed several other manufacturers to make players for Compact Disc and this has ensured that there is only one digital disc system so that you will be able to play any disc on any player. Fortunately we shall not see the crazy proliferation of formats that has

A revolutionary new sound reproduction system that could mark the beginning of the end for the LP, will be launched in the UK in March 1983. Developed over many years by Philips, the Dutch electronics company, the new system is called Compact Disc Digital Audio.

bugged the infant video industry - VHS, Betamax and the two Philips formats, to say nothing of Laservision.

The new system is clearly a major breakthrough in sound reproduction as Table 1 shows. Not only does it give

almost perfect sound reproduction, but the disc itself is extremely hard wearing. It can be handled quite freely without being damaged at all unlike the microgroove LP which seemed to acquire extra pops and clicks every time you looked at it, let alone touched it. In fact, you could drill a small hole through a Compact Disc (up to about a tenth of an inch (2.4mm) diameter and when played again, there would be no audible difference. Since the discs will



cost about £8 to £10 each, only a little more than the cost of a good quality classical LP, not many people will be in a hurry to try this out, but it does serve to illustrate just how impervious to damage the Compact Disc is.

Immunity to ordinary handling is achieved by coating the surface on which the data are stored with a layer of transparent plastic. How immunity is given to gaps in the data stream caused by opaque dust, scratches or even holes in the disc we will describe later.

Pocket-sized Discs

The disc itself is relatively small, about 4¾ inches (120mm) diameter and comes in a 5 inch square plastic pack with a hinged lid. "Sleeve" notes will be printed on a removable piece of card in the lid of the box. At first almost all the discs available will come from Philips companies: Polydor, Mercury, Deutsche Grammophon, Barclay, Casablanca, London, Archiv, Fontana, RSO, Polystar, Decca and of course Philips. The major American record companies are refusing to pay Philips the royalty they are requesting on each disc made, but since it is only 3 cents (about 1.75 pence) and there is considerable pressure from the world's top recording artists to have their material available on Compact Disc, there will doubtless be a compromise sooner or later and within a couple of years we should see most LPs available on Compact Disc as well, as soon as they are released.

The disc will hold one hour of audio information on one side. At the present time, the label covers the other side, but it could be used to hold a second hour of recording though the space left for a label (a 17 millimetre (¾ inch) wide band around the hole in the middle) is rather small! The disc could also hold quadraphonic or surround sound information encoded into

Frequency range	20Hz to 20kHz	30Hz to 20kHz
Dynamic range	>90dB	<55dB (at 1kHz)
Signal to noise ratio	>90dB	60dB (approx.)
Channel separation	>90dB	35dB (max)
Harmonic distortion	<0.005%	0.2%
Wow and flutter	Nil	0.03%
Playing time	60 minutes	20 minutes per side
Resistance to damage	Very high	Very low
Wear on disc and pick-up	None	Some
Instantaneous track selection	Yes	No
Can be moved at will whilst playing	Yes	No
Sensitive to microphony, shock or vibration	No	Yes
Pocket sized disc	Yes	No

Table 1. Comparison of Compact Disc with conventional 12 inch LP.

four channels, though a different player would be needed.

The surround sound player would, however, still be able to play existing stereo Compact Discs in stereo, while surround sound discs would have a message encoded into the data which would tell the surround-sound player to switch into four-channel mode.

First Models

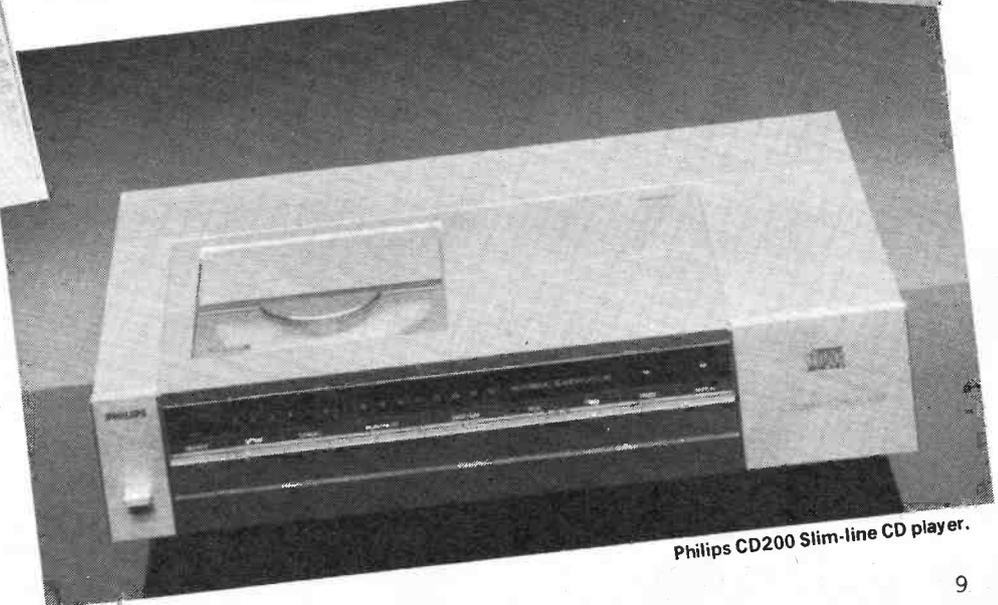
The first generation of players to come on the market can be broadly divided into two types. The Japanese

models which use an analogue filter in the output and the European models which, in the main, use a more sophisticated digital filter. The use of a digital filter, since it is physically far smaller than an analogue filter, has enabled Philips to make the smallest player on the market. Coded the CD100, this player will sell for about £400. It will also be available under the Marantz name, since Marantz are wholly owned by Philips. It measures just 320mm wide by 75mm high by 255mm deep (12½ x 3 x 10 inches).

Philips claim that the digital filter

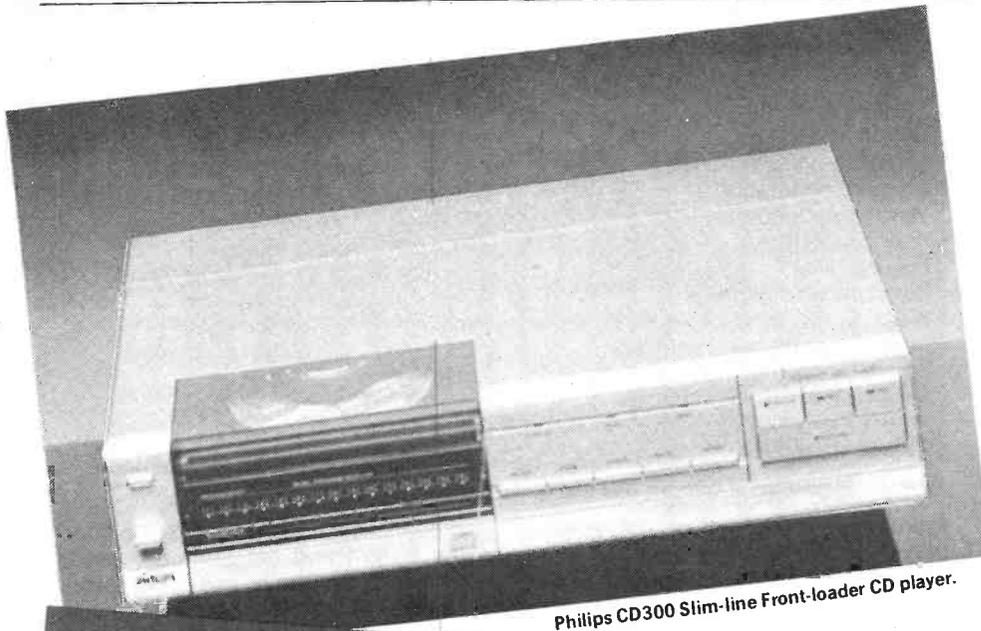


Philips CD100 Super CD player.



Philips CD200 Slim-line CD player.





Philips CD300 Slim-line Front-loader CD player.



Example of a CD player with vertical styling.

gives superior results to the analogue filter and is more stable and reliable. We will take a look at exactly how the filters work later.

All the players will enable you to select the order in which you want the tracks played, or allow you to pick your favourite track and have it play instantaneously (a boon for deejays) and repeat the selection as many times as you wish.

LED's on the player, light to show which track is playing and a button allows you to skip to the next track if you don't like the one that's playing. There is a fast search mode, either reverse or forward which will help you find your favourite passage, on for example a classical record, where there may not be separate tracks as such. A pause control is also provided.

Subcoded Messages

Some players will display the elapsed time on a track or how much time is left till the end of the disc. Some companies are planning to market players which when linked to a TV set will display the name of the track playing, or the text of the song, or any other information, the disc manufacturer wishes you to see. Or the information may be displayed on LED's, on the player itself.

But most of that is for the future. At the beginning all the players will be fairly similar in the features they offer. The main differences will be in the styling and here there are 3 main choices. There will be top-loaders, front-loaders where the disc is placed in a tray that pops out, and vertical players.

Once you've got your player home, you'll be able to plug it directly into the



All tastes from pop to classics will be covered in the first selection of music available on Compact Disc.

Maplin Magazine December 1982

radio or aux input on your amplifier. And then... perfection, or very nearly. At last you will be able to hear the full dynamic range of a symphony orchestra or your favourite pop group. No longer will the sound of a full orchestra be compressed lest the tracks on the LP get so wide they run into one another, or the sound of a single violin be enhanced by close-miking to ensure that the sound exceeds the inherent noise level of the LP material. Now you can hear it in your own home exactly as the composer and conductor meant it to be. From an inky black silence right up to the majesty of an orchestra at full crescendo, that is if your neighbours and your loudspeakers can take it.

Latest Technology

So how is all this magic possible on a disc 120mm diameter and just 1.2mm thick (4 $\frac{3}{4}$ inches by less than a twentieth of an inch). In the broadest sense it is made possible thanks to the recent advances in digital and laser technology and the incredible scales of integration now possible in single IC's.

The first step is to turn the analogue signals to be recorded into digital signals and there are already quite a number of recording studios which use digital techniques. The digitising system used is called pulse code modulation (PCM). The incoming analogue signal is sampled about once every 22 microseconds and the voltage level detected at that instant, compared against a library consisting of 65,536 levels. Each level has a different 16-bit code and the code for the level nearest the one detected is output. Thus each stereo channel generates a data stream of 705,600 bits every second.

The sampling rate is actually

COMPACT
disc
DIGITAL AUDIO

Compact
Cassette

Logo of the new system with the logo of Philips last world-beating idea. The Compact Cassette has virtually wiped out reel-to-reel and cartridge tape players in domestic applications, despite their technical superiority. This time the technical superiority is all on Philips' side.

44.1kHz and is this high because it is essential that it is at least twice the maximum frequency required, 20kHz. Having so many levels available (over 65,000) means that the code describing the voltage is extremely accurate. The difference between the actual voltage and the voltage described by the code will be heard as noise. This noise is called quantisation noise. The best signal to noise ratio possible is equal to $6n + 1.8$ dB where n is the number of bits. So in our case the signal to noise ratio will be $(6 \times 16) + 1.8$ or 97.8dB, an order of magnitude better than the best (though rarely achieved) signal to noise ratio possible with an LP.

High Speed Data

The two stereo channels are now combined into one data stream, each 32 bits comprising one left and one right channel sample for the same instant. Thus channel separation is virtually total since each group of 16 bits is completely independent of any

other group. This data stream comprising 1.4112 million bits per second is however not suitable as it stands to put onto the disc for several reasons.

The data will be put onto the disc by a laser that will burn a tiny pit about 0.2 micrometres (μ m) deep and 0.6 μ m diameter (about 24 millionths of an inch) for each binary zero into the surface of a very thin layer of aluminium embedded in the plastic.

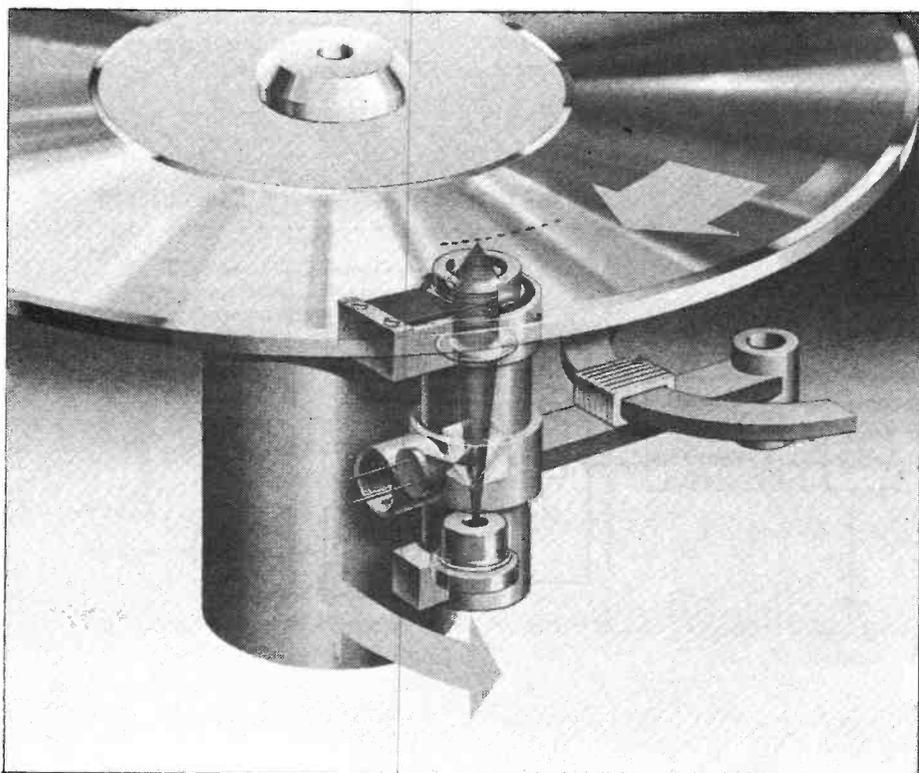
The data will be read by shining a very fine infra-red light beam onto the disc. The pits will scatter the light in all directions whilst the flat aluminium between the pits will reflect the light like a mirror. An infra-red detecting diode will register zero if no light is received (from the pits) and one, when the light is reflected back.

8 To 14 Modulation

The data are recorded in a spiral starting about 25mm from the centre of the disc and continuing to a point about 59mm from the centre. Since there is no contact between the disc and the reading system, the servo-controlled reader can only keep on the correct track if successive zeros are closer together than the pitch of the track. The distance between each track is 1.6 μ m so if there were two or more ones together the servo would find it difficult to decide where the track continued and could easily continue on the wrong track after a long sequence of ones.

A second reason why the data cannot be put onto the disc as it is, is that after a long sequence of ones the optical detector will have been flooded for a long time and may not turn off fast enough to detect the first zero following a sequence of ones. The detector will read the data at the high speed required much more reliably if the total spectral power is kept low.

The third reason is that since the size of a data bit anywhere on the disc is the same, there are fewer bits in one revolution at the centre of the disc than at the outside. So the disc must spin faster at the beginning (the centre) than at the end when data is being read from the outer tracks. When reading data at the centre the disc spins at about 500 rpm and at the outside about 200 rpm. In order to get the rotation speed



The disc spins in an anti-clockwise direction as viewed from the side read by the laser.

exactly right, it must be possible to detect the bit rate from the data.

It turns out that all these requirements are met if there are at least two zeros between any successive ones and never more than ten zeros at one time. There are 16,384 different patterns of 14 bits of which 277 meet the requirements of not less than two zeros between each successive 'one'. Of those, 21 have more than ten consecutive zeros, leaving exactly 256 that meet all the requirements. This is a very convenient number, since there are 256 different patterns of eight bits as well.

The data streams from the 16-bit converters are split into 8-bit sections and each 8-bit byte is converted into a 14-bit word using a look-up table stored in ROM. Three merging bits are added at the end of each 14-bit word so that words can be joined together without violating the two to ten zeros constraint. These bits contain no information and are skipped by the decoder.

Making The Frames

The data are now arranged into frames each starting with a 24-bit synchronisation pattern and containing twelve 16-bit data words (24 14-bit words after encoding) representing 6 stereo samples, four 16-bit error correction parity words (eight 14-bit words after encoding) and one 8-bit control and display word (one 14-bit word after encoding). With three merging bits between each of the 33 14-bit words, one after the sync pattern and one at the end there are a total of 588 bits in each frame.

The eight bit control and display words can contain information, for instance to mark the pause between tracks to implement search and repeat functions, or to indicate remaining or elapsed playing time, titles or composers etc.

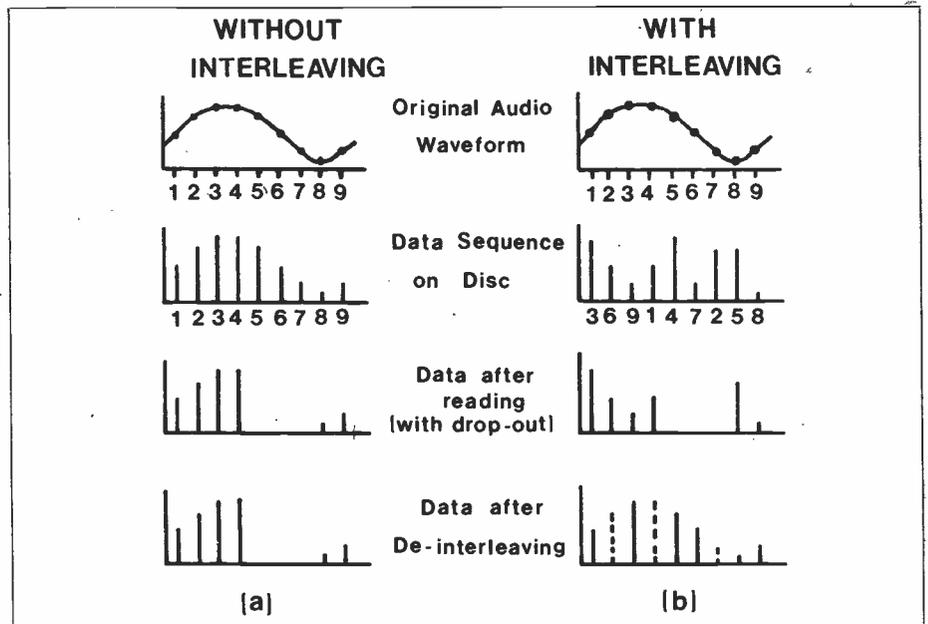


Figure 1. Principle of interleaving as used in Compact Disc's error correcting system.

No. of Bits	Type of Data	Total No. of Bits
24	Synchronisation Pattern	24
3	Merging Bits	3
14	Control and Display Bits	14
3	Merging Bits	3
14	Audio Data Bits	Repeated 12 times 168
3	Merging Bits	
14	Error Correction/Parity Bits	Repeated 4 times 56
3	Merging Bits	
14	Audio Data Bits	Repeated 12 times 168
3	Merging Bits	
14	Error Correction/Parity Bits	Repeated 4 times 56
3	Merging Bits	
Total number of bits per frame		588

Figure 2. One frame of 588 bits in the format in which it is recorded onto the disc.

Before the data are put into frames the audio data are rearranged in time. This interleaving coupled with the parity words forms a powerful error

correction system that can correct a loss of up to 3,500 successive bits and compensate by interpolation, a loss of 12,000 successive bits. The principle of

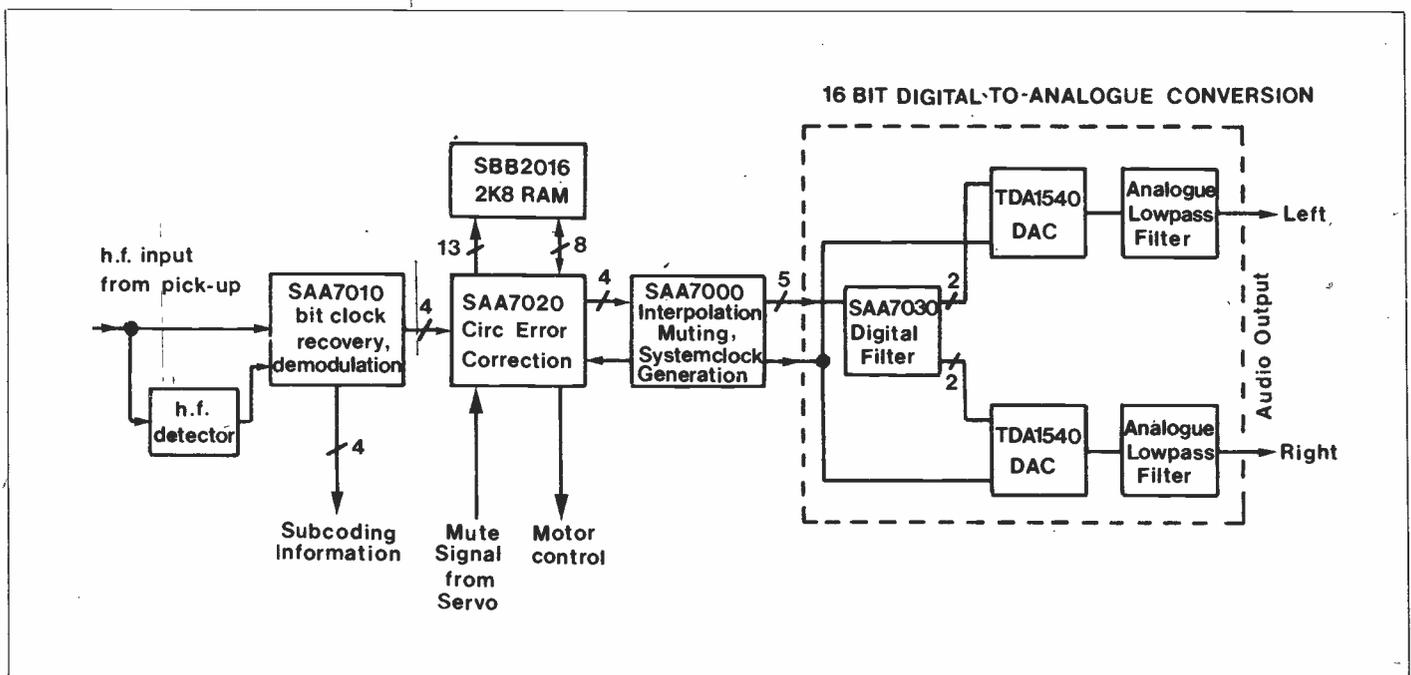


Figure 3. Block schematic of the Compact Disc decoder.

this system, known as a Cross Interleave Reed-Solomon Code (CIRC) is shown in Figure 1.

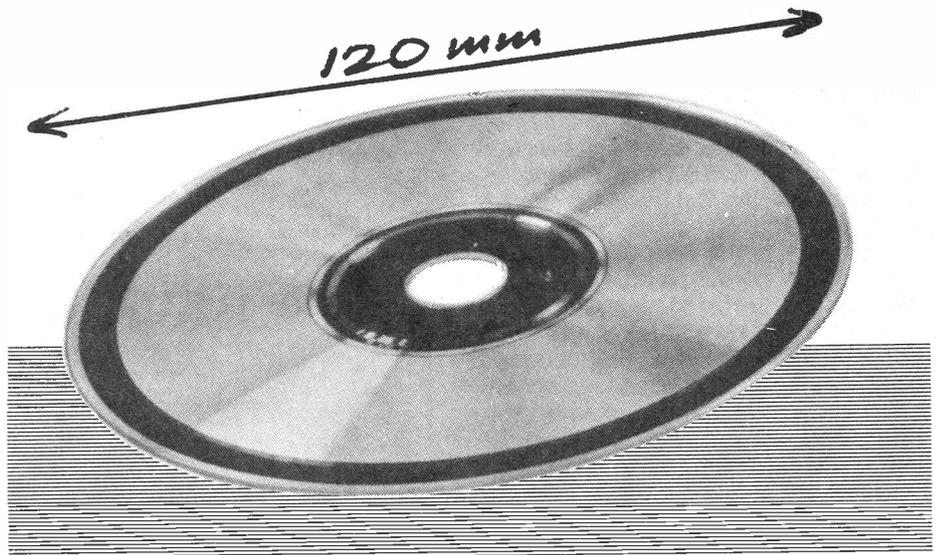
In 1a three consecutive words are missing making it difficult or even impossible to replace the missing words and be certain they are correct. In 1b, however, after de-interleaving, the missing words are spread out in time and there are now only single errors which can be easily corrected.

This then is the form the data take that are recorded onto the disc (see Figure 2). It is now the job of the Compact Disc player to recover the data from the disc and reconstruct the original stereo audio signals.

Reading The Data

The player contains an Aluminium Gallium Arsenide solid-state laser diode which emits infra-red light at a wavelength of 780nm, just outside the visible spectrum. The light passes through a half-silvered mirror and then a lens which focusses the beam onto the disc. When a digital "one" occurs in the data, the light is reflected back along the transmission beam, but deflected at right-angles when it hits the half-silvered mirror. The deflected beam then strikes a photodiode which registers the pulse of light. This whole optical system is carried on a servo controlled arm which gradually moves across the disc from the inside to the outside.

The high frequency (hf) data stream is recovered from the disc at the rate of 4.3218 million bits per second. The output from the photodiode is first amplified and filtered then passed to the input of the demodulator IC, SAA7010. See Figure 3. The incoming signal is first squared-up by a level detector and Schmitt trigger and then passed to a phase locked loop which regenerates the bit clock. The voltage



Playing side of a Compact Disc. The other side is covered by the label.

controlled oscillator of the phase locked loop operates at 8.6436 MHz, twice the incoming data rate, from which a 4.3218MHz master clock for all internal timing is derived.

The incoming data are clocked into a shift register within the SAA7010 until the unique synchronisation pattern is detected. Each subsequent 14-bit word is then held in a latch and converted back to the corresponding 8-bit word by a logic array. The first 8-bit word contains the control and display information and is passed to a microcomputer which can deal with the data in whatever way a particular manufacturer desires as explained earlier. The next thirty-two 8-bit words are passed to the error correction IC, SAA7020.

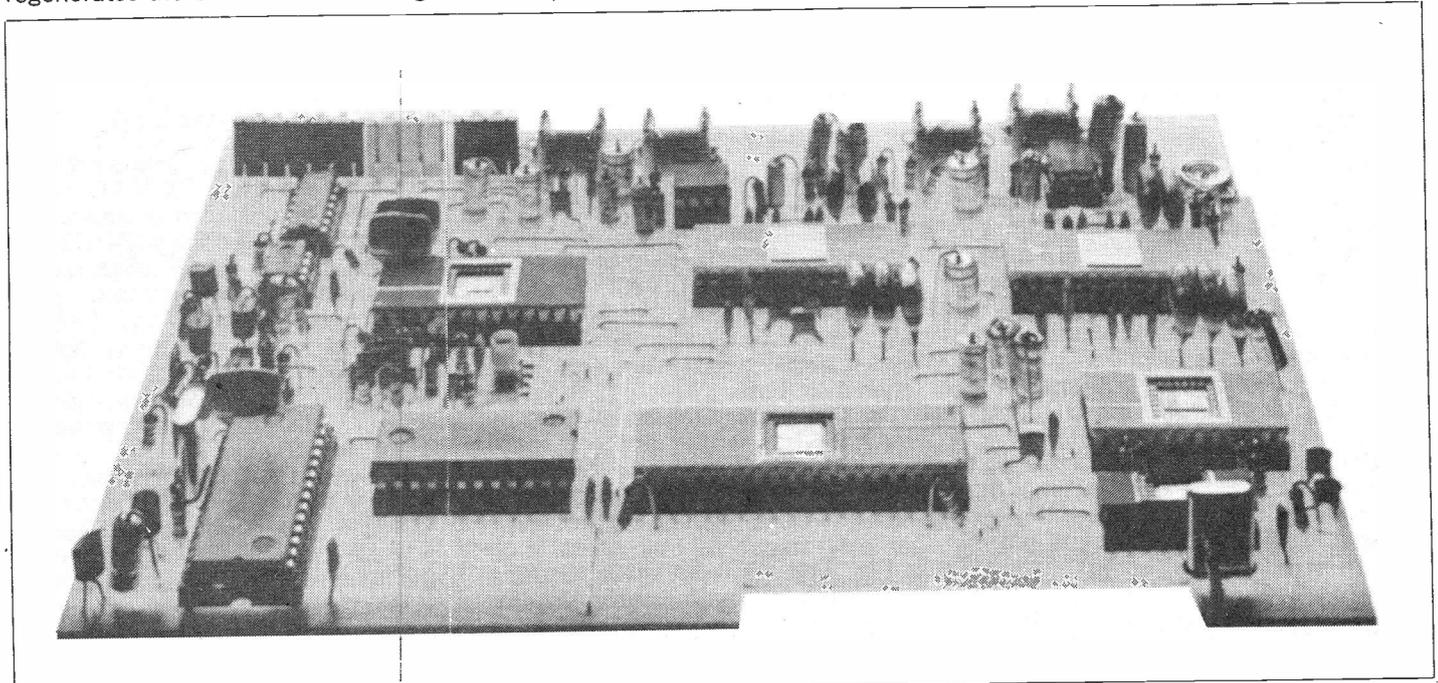
Before going on to this IC, we will just mention the hf detector shown in Figure 3. When the amplitude of the hf signal is small, for example, during loss of data, the hf detector switches off the phase and frequency detectors in the SAA7010 and this prevents the phase locked loop locking onto noise which

would otherwise have caused clock jitter.

Data entering the SAA7020 are stored in a shift register and a first-in-first-out (FIFO) register. The FIFO acts as a jitter reduction circuit and since it can compensate for up to ± 2.25 frames, totally eliminates wow and flutter in the system. The data rate at the output of the SAA7020 is determined solely by the clock signal from a crystal oscillator. Any difference between this frequency and the frequency derived from the detected bit rate, generates an error signal which controls the speed of the motor driving the disc.

Reed-Solomon Decoders

The data are now de-interleaved by storing the 32 words of one frame in a 2K by 8 RAM along with the 28 output words of the first Reed-Solomon decoder. This decoder can correct one erroneous word, but if more than one



This single small circuit board contains nearly all the electronic circuitry in a Compact Disc player, yet it can process data at a rate of 4 million bits per second and convert it to perfect audio.

word is shown by the first four parity words to be incorrect then the 28 words (the first four parity words now being discarded) are written back to the RAM unchanged, and a flag is set which marks the 28 words of this frame as unreliable. If the data was correct or corrected, the 28 output words are written back to the RAM but the flag is not set. The output words of the first decoder are further de-interleaved by means of the RAM and fed to a second Reed-Solomon decoder. This decoder can correct up to two erroneous words, and the correct or corrected frame of 24 words (the second four parity words now being discarded) is written back to the RAM. If the data are still incorrect a second flag is set and the uncorrected word returned to the RAM.

After 30 stereo samples have been stored in the RAM the first sample is output from the SAA7020 in a 16-bit burst followed by an 8-bit interval then a second 16-bit burst and so on. If a sample is incorrect a flag is passed with it. If two consecutive errors are detected a flag is sent in the 8-bit interval as soon as it is detected, that is 30 samples before it is actually passed on to the interpolation and muting IC, SAA7000.

Muting Bad Data

Serial data from the SAA7020 are entered into a shift register and the left and right channels then descrambled. If there are no unreliable data flags then the data passes through the SAA7000 unchanged. If a single unreliable sample is flagged then the SAA7000 reinstates the missing sample by linear interpolation. If a flag arrives in one of the 8-bit intervals, the SAA7000 immediately starts to reduce the value of the samples so that they will produce a zero volume audio output after 30 samples. As soon as the flag stops appearing in the 8-bit intervals, the SAA7000 starts to increase the value of the samples until they return to their true value after 30 samples. This system ensures that incorrect samples are never heard and is gradual so that clicks are not heard in the output.

Since muting will not occur until 12,000 consecutive bits are lost, this should not be a common occurrence and even then should be of such a short duration that it will be scarcely noticeable. For example, 24,000 consecutive bits lost will cause muting for less than one hundredth of a second.

The output of the SAA7000 is now 16-bit words for right and left channels exactly as they were when they were original encoded by the 16-bit analogue to digital encoders at the time of recording. It is now only necessary to regenerate the original analogue information from the 16-bit codes.

Digital To Analogue Conversion

In the Japanese players the 16-bit codes are fed to a 16-bit digital to

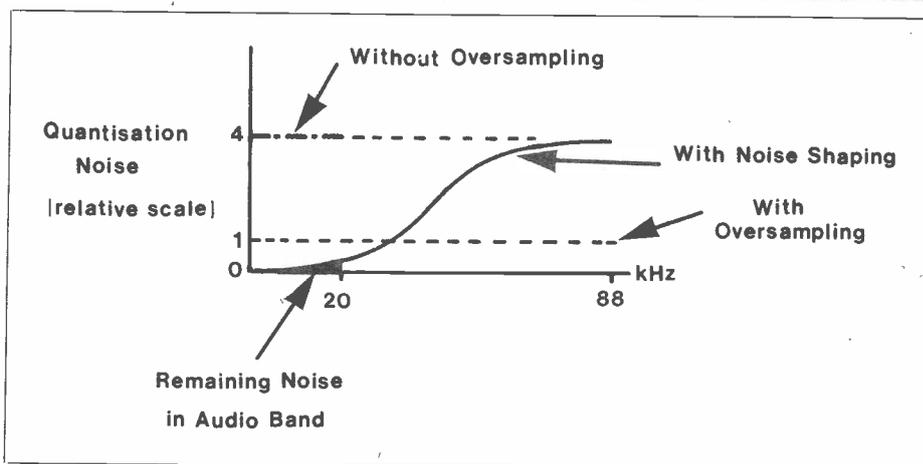


Figure 4. How 16-bit signal-to-noise ratio is obtained from a system using 14-bit DAC's.

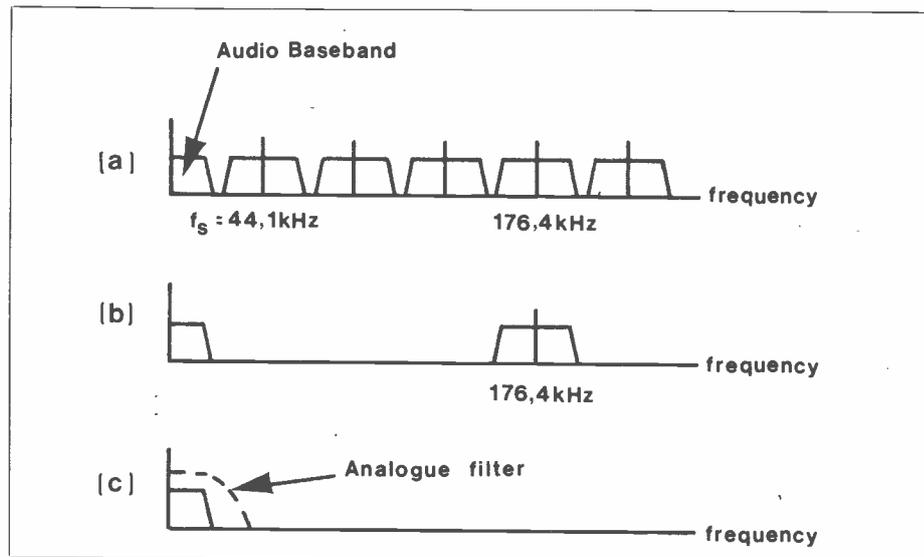


Figure 5 (a) Frequency spectrum of output of 16-bit DAC. (b) Frequency spectrum of output of SAA7030. (c) Frequency spectrum of output of TDA1540.

analogue converter (DAC) and the resulting analogue signals filtered using a complicated analogue filter. This filter can cause phase distortion in the audio signal and will reduce the slew rate. In addition, 16-bit DAC's and the complex filter are both expensive.

In most of the European players and in all Philips models a more sophisticated system is used which does not suffer from any of the problems mentioned above. A relatively cheap 14-bit DAC is used, yet the signal-to-noise ratio is only about 1dB worse than the 16-bit system (97dB instead of 97.8dB) it has only a simple low-cost analogue filter which does not affect the phase response of signals under 20kHz and does not reduce the slew rate. In addition, it virtually eliminates intermodulation distortion.

In this system the outputs of the SAA7000 are fed to a digital oversampling filter, SAA7030. The two 16-bit data streams (left and right) are fed into shift registers which quadruple the sampling frequency from 44.1kHz up to 176.4kHz. Quadrupling the sampling frequency also quadruples the effective audio bandwidth, from 22kHz up to 88kHz and the noise is spread out with it. See Figure 4. Since 75% of the noise is now above the audio band, it can be suppressed by filtering.

The 16-bit words entering this digital filter are output as 28-bit words and stored in an accumulator. The most significant 14-bits are then output to a 14-bit DAC. The SAA7030 contains two identical filters, one for each stereo channel and there are two identical 14-bit DAC's, again, one for each channel.

Simple Filters

A 14-bit DAC will give a signal-to-noise ratio of about 84dB. Oversampling and digital filtering add about 6dB to that figure. In addition the SAA7030 contain a noise shaper which redistributes the quantisation noise so that more noise occurs in the 22kHz to 88kHz region than in the audible region. This noise shaper adds a further 7dB to the signal-to-noise ratio giving a total of 97dB, almost the same as for a 16-bit system.

The 14-bit digital samples now arrive at a rate of 176.4kHz at the DAC, TDA1540. The input data are used to activate 14 switches which determine the output current. This output current is held between conversions by latching a flip-flop in the DAC. The hold function results in an output response which has a null at 176.4kHz where the first harmonic of the sampling frequency would otherwise have occurred.

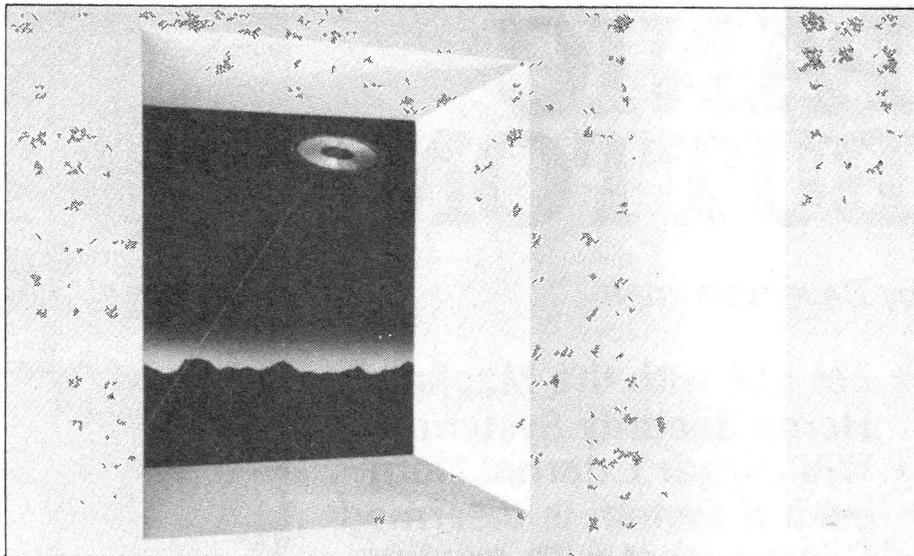
Thus with reference to Figure 5(c), it is clear to see how a very simple analogue filter can now be used to filter off any remaining frequency components outside the audio band. On the other hand Figure 5(a) shows that a very high order filter will be needed to filter out the spectral lobe stretching from 22kHz to 66kHz, generating all the problems inherent in high order filters as previously described. Also since the sampling frequency is so close to the audio band some intermodulation distortion will occur in the audio band! In the oversampled system, intermodulation products are well outside the audio band.

The current output of the TDA1540 is converted to a voltage by an NE5532 dual op-amp. This op-amp is also used as the filter which is a third order low-pass Bessel filter with a cut-off frequency of 30kHz. A Bessel filter is used as it has a linear phase response. The output of the filter is a 1V rms max. voltage which can be connected to any hi-fi amplifier.

The End Of The LP

When Compact Disc is launched most of the potential purchasers will be those who already have expensive hi-fi systems. For them £400 is comparable with the cost of a top quality cartridge, tone-arm and turntable. And the superb quality possible will be irresistible.

However, the Compact Disc is inherently very simple to make. The Laser and servo system are far less complex



than the mechanics of a video tape recorder and the simple circuit board containing just twelve IC's and a few other components is very easy to make. Once production gets into full swing, prices are bound to fall and I would be surprised if they are not under £200 within two years.

Clearly, as the price falls and the numbers of discs around increases, more and more people will choose a Compact Disc player rather than an inferior record-player. There is little doubt that the days of the LP are numbered. Within 10 years the LP will have gone the way of the 78. And just as LP's are available now containing the best of the music recorded on 78's usually after re-recording from the old

masters, so Compact Discs will be released containing the old favourites originally released on LP's. And that will be the final nail in the coffin for the LP.

But I for one will not be mourning the LP too much. The exasperating imperfections of the LP will at last be a thing of the past. The launch of Compact Disc heralds the new era in hi-fi, with the near-perfect reproduction that enthusiasts have been striving for over the years. But there is already signs of discontent in the hi-fi magazines, with die-hards questioning the quality of Compact Disc. In the meantime the rest of us can just sit back at last and listen to the music itself uninterrupted by the pops, clicks and bangs of those dreadful LP's!

IMPROVED TIMER CONTROL

Continued from page 7

and the time constant found. R_T is the effective timing resistance of R_A and R_C in parallel.

(3) Pick a trial value of C, and find R_T to match it. As a guide, keep C low and R high within reason: C under 1 nF makes strays important, R over about 470K may present problems of selection from a limited standard range. If both C and R look too high at low frequencies, consider using a fast oscillator and divider: this could be more stable, smaller and cheaper with no waiting for special-value parts.

(4) Use the table to get R_A from R_T , and then work out R_C as well. These are not directly usable values: there are called "design centre values", before allowing for adjustment of tolerances.

(5) Tolerancing:-

IC	±2%
V_{CC} effect	±0.25% for 0.25V regulator offset

C	±1%
R	±1%

Worst-case sum = 4.25%

There is no need to use 1% parts; other grades can be just as stable, but they alter the tolerance sum.

Take away the tolerance allowance from the design centre R_A , and compare this result with available preferred values. If close, just continue; if far away, either:

(a) try a different C.

(b) use the next lower value and add the difference to the adjuster design

or (c) try a sum of two fixed resistors: a small extra one need not be of 1% grade for 1% results.

When settled, allow twice the tolerance fraction of R_A as the necessary range of adjustment, adding on any rounding-up if R_A has been reduced much to a standard value. (6) Check the required adjuster range against standard values, remembering the adjuster may be ±20% itself. With a design using wide-spec. parts, the adjuster may end up very large, and selecting a fixed resistor on test for part of the adjustment will improve stability.

So far this is exactly what is done for a fixed-frequency oscillator with the standard circuit.

(7) R_C needs an adjustment allowance first of all equal to R_A 's, and then an extra 5-6% for worst-case IC tolerances. With 1% parts, this means taking 10% from the design centre R_C , and allowing for up to 20% adjustment range.

One of the resistor adjustments can be replaced by capacitor adjustment, but often a full range of parts is not available.

When built, setting-up is easy enough: adjust R_A at F_{max} , then R_C at F_{min} , and repeat to overcome a slight interaction.

There are no special layout problems: six plugboards and two PCB's have worked well, despite trying to bundle wires and adding short antennas to suspect points. Take "reset" (pin 4) to V_{CC} if not in use; for the 555, 100nF and 10nF supply and "control" de-

coupling. The 7555 does not need supply decoupling, and usually control will behave without it. If the control pot. is remote, prepare to decouple the DC end of R_C . Otherwise, just keep everything cool and check V_{CC} regulation for real stability. If in doubt, use a local 78L05 with steady load.

The output will drive two standard loads — 74/LS/ALS/CMOS — via 470-820 ohms; a resistor helps in any later fault diagnosis and prevents faults spreading through a system, if speed is not critical.

The expected stability can be found in worst-case from the component sums:-

IC	±50 ppm per degree C
V_{CC}	negligible, 78L05
C	- 150 ppm/degree (polystyrene)
R	± 100 ppm/deg.C

and it is very unlikely drift will exceed 0.1% for a 5 degree case temperature change. This is about as good as can be had from an RC oscillator with no oven or special components.

For interest, R in the circuit can be replaced by two fixed resistors: their junction with R_C is then a good linear FM input terminal for a 20% voltage swing. A dual IC can be used for sweep — with care not to upset its timing — or frequency shift keying. A simple D-to-A converter allows other codings.

Their 4:1 circuit makes a very useful metronome with a range of 70-280 pulses per minute: good as clockwork and easier to set, with more range.

PANIC BUTTON

by Dave Goodman

- ★ For use with the Maplin Home Security System
- ★ Will trigger External Horn even if system is disarmed
- ★ Can be reset with existing alarm unit keyswitch



This project has been designed specifically in response to the many requests we have had for a 'Panic Button' addition to our Home Security System.

The requirement is for a button placed close to the front or back doors, inside the home, or even by the bedside. In any emergency pressing the button would trigger the alarm, setting off sirens, lamps, etc., and hopefully attracting attention and dissuading potential burglars. The Panic Button PCB caters for up to four switches, which should prove adequate for most applications, and complete instructions are given for connection to the Burglar Alarm PCB.

Circuit Description

With reference to figure 1, two diodes, D1 and D2, are wired to the spare change-over contacts on the Burglar Alarm keyswitch (figure 3). Either of these diodes will always be forward biased, allowing D3 only to conduct when the contact changes over. The keyswitch contacts are break-before-make, so that during switching a positive pulse appears at D3, which will,

in turn, trigger the monostable IC1b and IC1c. This lengthened trigger pulse forward biases D4 and resets the latch IC1d and IC1e.

The output from IC1d is held low by R9 and a high output from IC1e. This may be thought of as a loop. IC1a and

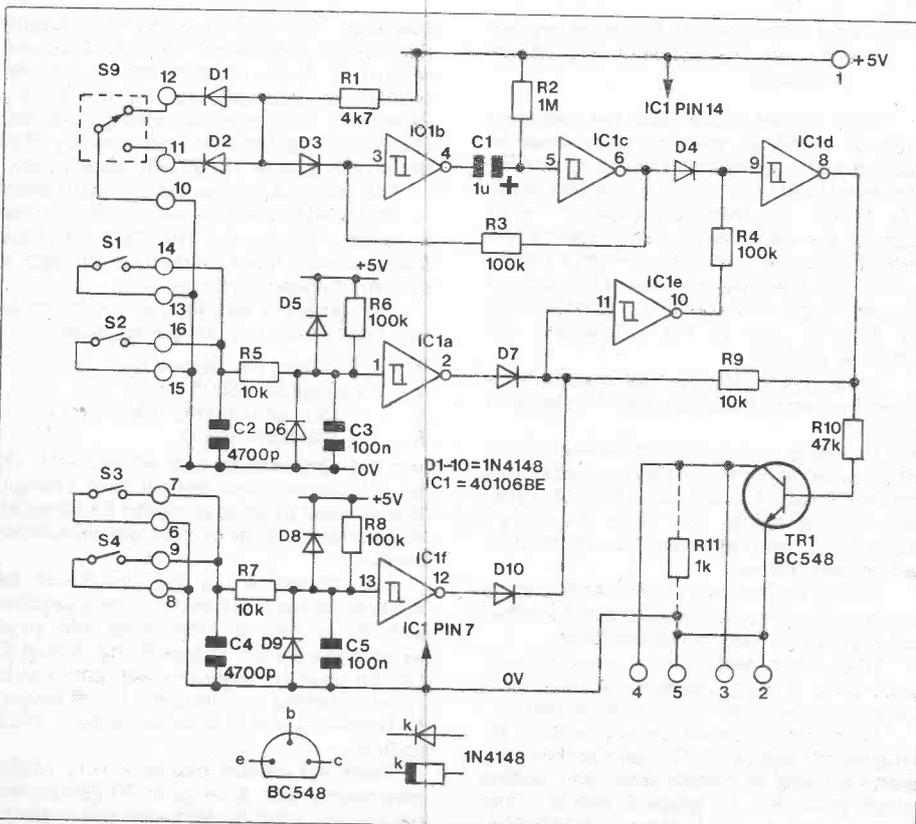


Figure 1. Circuit diagram

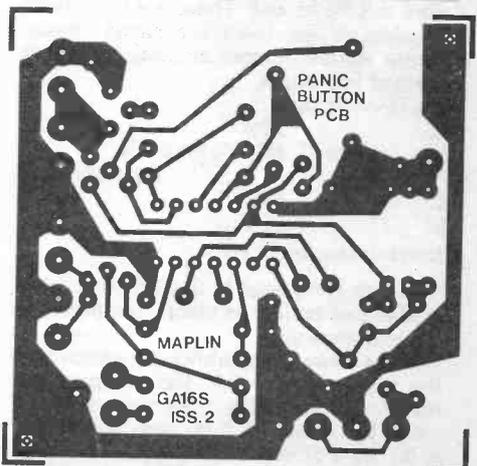
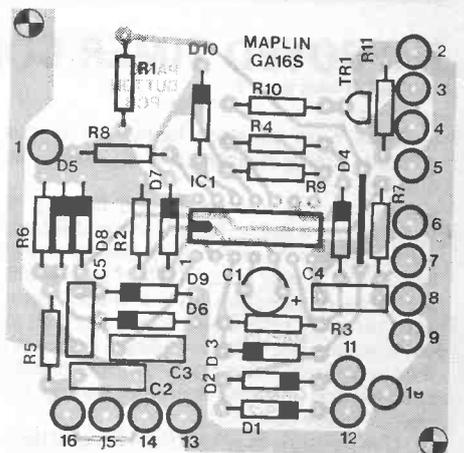


Figure 2. PCB layout and legend

WORKING WITH OP-AMPS

by Graham Dixey C.Eng., M.I.E.R.E.

Filtering is the act of separating what is wanted from what is unwanted. In electronics this usually means some form of separation on the basis of signal frequency. In the simplest case, signals are divided into two 'bands' known as 'low frequencies' and 'high frequencies', separated quite arbitrarily by the 'cut-off' frequency. The fact that capacitive reactance depends upon frequency is often used to obtain such separation. This idea leads to simple filters of the 'inverted-L' type, known as 'low-pass' and 'high-pass' filters; these, together with their characteristics, are shown in Figure 1.

The characteristics of these simple filters show that, soon after the cut-off frequency is reached, the filter cuts off with a constant slope which is never greater than -6dB/octave (i.e. -20dB/decade). This is a basic limitation where a high degree of separation is required. Also, there is no gain at all, even at the wanted frequencies. These filters are said to be 'passive'. By using the op-amp with its high gain and differential inputs, filters can be designed to have real gain and high degrees of rejection of the unwanted frequencies: these are known as 'active filters'.

The Op-amp as an Active Filter

To see how the op-amp can be used as the basis for an active filter, consider a now familiar circuit; the inverter. This is shown in Figure 2, where the circuit is drawn twice (a) and (b), each case illustrating how either the input component or the feedback component can be represented by a 'block' which could contain literally anything. For example, if these components are a resistor R1 and another resistor R2 respectively, the circuit is then just an inverting amplifier with a gain of R2/R1, this gain being quite independent of frequency, at least within the limitations of the op-amp itself. But, if either block contains frequency-conscious components, then the situation will be entirely different. The gain of the amplifier will vary with frequency and in such a way that it is under the designer's control by his choice of network components, either at the input or in the feedback path or both. Thus, a number of different configurations for active filters are possible, based on this idea.

The Twin-tee Selective Amplifier

One example of a frequency-conscious network is the twin-tee filter. This has the characteristic that at a particular frequency, given by $f=1/(2\pi RC)$, its impedance is very high. If the impedance of the network is called Z2 and it is used in the feedback path, then it will give a gain of Z2/R1 (if the input circuit is a simple resistor of value R1); this gain will be a maximum at the frequency quoted above. The circuit is obviously selective and in fact behaves rather like a high-Q resonant circuit, but at low frequencies instead of radio frequencies. The frequency that it selects depends upon the values of R and C used in the twin-tee network. A

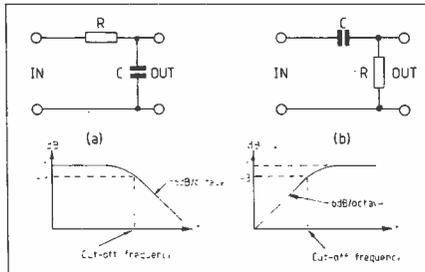


Figure 1. Simple RC Filters: (a) Low-pass filter (b) High-pass filter.

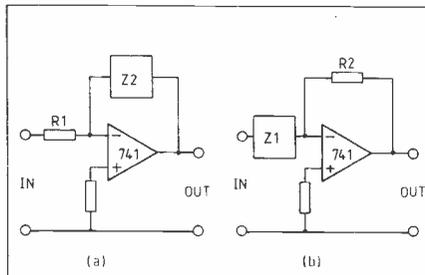
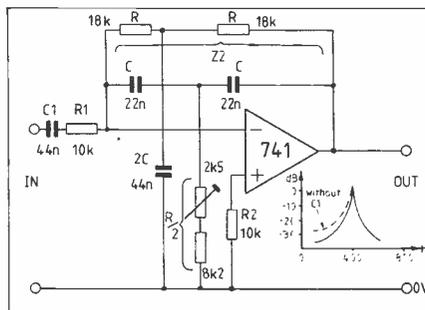


Figure 2. The Basic Idea of an Active Filter.



selective amplifier of this type is shown in Figure 3, together with a sketch of relative output (in dB) as a function of frequency, for a design frequency of 400 Hz. To use the amplifier at some other frequency, it is only necessary to assign new values to R and C (giving new values to R/2 and 2C at the same time of course). The R/2 branch should contain a pre-set part since the circuit selectivity is best when the resistance of this branch is actually slightly less than the nominal value of R/2 calculated. The selectivity can be improved further by adding a little 'bass-cut'. This is provided by the series input capacitor C1, a value equal to 2C being about right. Using 22nF for C, 2C becomes 44nF; this value can be realised by wiring two 22nF capacitors in parallel or, alternatively, opting for the nearest preferred value of 47nF. The latter choice may well be close enough.

The Twin-tee Rejector

Instead of selecting a frequency at the expense of all others, the opposite course of action may be taken. The circuit is then made to reject just one frequency and to pass all others (ideally anyway). The obvious way of doing this is to place the twin-tee network in the input of the op-amp, calling its impedance Z1 now, which will give a very low

value of gain, R2/Z1, the feedback network being a simple resistor R2. This gain is a minimum at a frequency given by the formula already quoted, as is fairly obvious. A possible circuit is shown in Figure 4, additional components being provided so that the gain 'off the centre frequency' is defined by R2/R1 (giving unity gain in this case) as well as giving some degree of control over the shape of the rejection curve. For example, increasing the value of R2 increases the gain away from the centre frequency but does so at the expense of the sharpness of the curve. At the centre frequency, the situation is more complex because then R3 comes into play as well; it also has some effect on the sharpness of cut-off but, if its value is made too large, use of RV to obtain maximum rejection of the centre frequency is more difficult. It is a point worth experimenting with. For the values given in Figure 4 and a design frequency of 400 Hz, a sketch of the characteristic with RV adjusted as well as possible is also shown.

For both of these twin-tee filters, note that the sharpness of cut-off is considerably greater than that of the simple filters mentioned earlier.

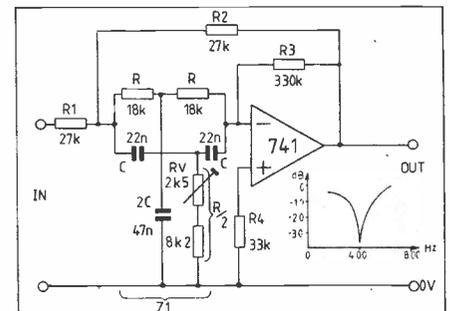


Figure 4. A 400Hz Twin-tee Rejector Amplifier.

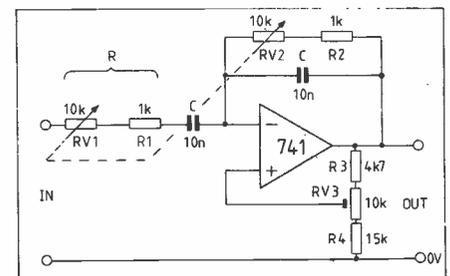


Figure 5. A Tuned Acceptor Amplifier (Wien Network).

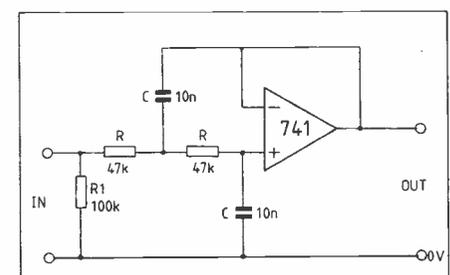


Figure 6. Second-order Low-pass Filter.

The Wien Acceptor Amplifier

An acceptor amplifier is a useful circuit in that it allows analysis of a complex signal i.e. one containing a number of harmonics, which can then be separated into its constituent parts and each measured individually. An obvious example of this is the measurement of harmonic distortion in audio signals. If the fundamental frequency

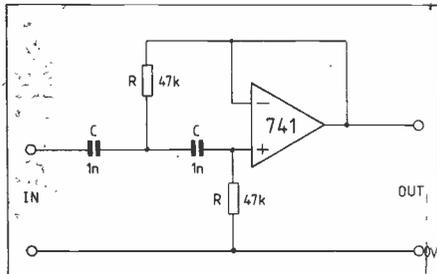


Figure 7. Second-order High-pass Filter.

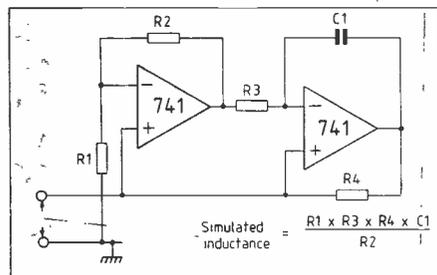


Figure 8. The Gyrator Circuit.

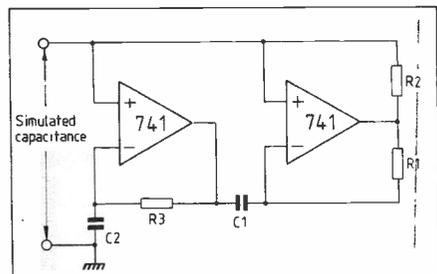


Figure 9. The FDNR (Frequency-Dependent Negative-Resistance) Circuit.

and harmonics of a distorted signal are selected separately by a filter, each can be measured by an electronic voltmeter to give information about the percentage of the various components in the signal. Obviously, such a filter must be variable and the twin-tee is not particularly useful in this application because of the need to vary three components at once. For this reason, the Wien network is a better proposition and a selective amplifier based on this approach is shown in Figure 5.

The circuit uses positive feedback from the output to the non-inverting input, and negative feedback from the output to the inverting input. The amount of positive feedback can be controlled by RV3 and is independent of frequency. On the other hand, the negative feedback is provided by the Wien network and therefore depends upon frequency. If RV3 is adjusted correctly, both types of feedback cancel out at one particular frequency, given by $f=1/(2\pi RC)$, and the gain of the circuit is very high. At all frequencies above and below this value, the negative feedback predominates and the gain is low. With the values of R and C given in Figure 5 the circuit can be tuned to accept any frequency in the range 1.6-12.5kHz. Switching values of C would allow several ranges to be covered.

Low-pass and High-pass Filters

Both the circuits of Figure 6 and Figure 7 are known as 'second order' filters because they double up on the use of the previously mentioned inverted-L filter sections. As a result, the ultimate cut-off slope is 12dB/octave instead of being only 6dB/octave. The circuits are arranged to give unity gain over the passband but substantial attenuation outside the passband.

The filter elements for Figure 6 and Figure 7 are R and C and, for the single inverted-L section, the cut-off frequency (-3dB) is obtained when $R=1/(2\pi fC)$ which, by transposition, means that the cut-off frequency $f=1/(2\pi RC)$. However, the use of two identical sections means that the attenuation is actually -6dB at this frequency so that the true -3dB frequency is rather different than give by the above formula for a single section.

For example, in Figure 6, the cut-off frequency for a single section works out at 339Hz but the actual value obtained for the second order circuit is nearer 200Hz.

Similarly for the circuit of Figure 7 while the cut-off frequency for a single section works out at 3.386kHz, the actual cut-off frequency for the second order circuit was found to be about 5kHz.

An Alternative Approach

So far each active filter presented has consisted of a well-known passive filter used in conjunction with an op-amp, the filter type being quite clearly identifiable e.g. as in the Wien circuit.

Now a completely different approach will be demonstrated which shows even more

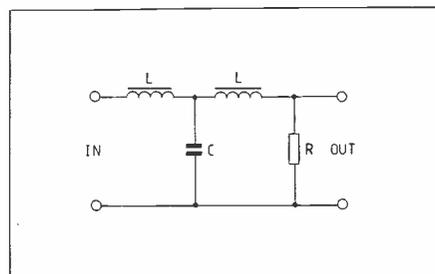


Figure 10. A Low-pass Passive RLC Filter.

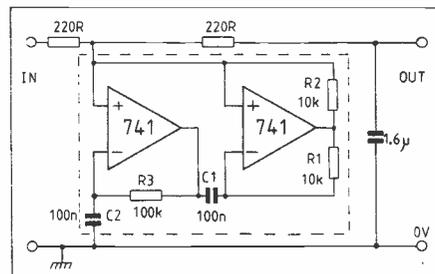


Figure 11. Design for a FDNR-based Low-pass Active Filter.

clearly the clever tricks that can be played with the aid of op-amps.

The starting point is the idea that inductors and capacitors can be 'simulated' by any circuit that produces a 'lagging' or 'leading' phase angle between applied voltage and the resulting current respectively. To illustrate the first case, Figure 8 shows how two op-amps can be connected to produce a 'gyrator' circuit or simulated inductor. This apparent inductor appears between the terminals shown and the major advantage is that a costly, heavy and bulky component is replaced by a handful of small, cheap ones; also the inductance value is readily changed. Thus, any real filter that contains

an inductor could contain a gyrator circuit instead. However, inductors in LCR filters are often in series with the signal and the gyrator simulates an inductor which has one terminal earthed, a slight disadvantage.

This limitation of the gyrator is overcome by the circuit arrangement of Figure 9, which is known as the 'frequency-dependent negative-resistance' circuit or just FDNR for short. This circuit simulates a capacitor but, and here is the clever bit, when a passive filter normally comprised of L, C and R is synthesised by a circuit arrangement based on the FDNR, not only is C replaced by the FDNR but R is replaced by a capacitor C' and L is replaced by a resistor R', the following relations being used to find the component values in the synthesised circuit.

$$\text{New capacitance } C' \text{ (Farads)} = 1/R$$

(R in ohms)

$$\text{New resistance } R' \text{ (Ohms)} = L$$

(L in Henries)

Note that the final synthesised circuit contains no inductors, just resistance, capacitance and FDNRs.

The component values for the FDNR circuit to replace a given value of capacitance C are obtained from the relation,

$$C = (R1 \times R3 \times C1 \times C2)/R2$$

(capacitance values in Farads, resistance values in Ohms).

What this implies is that it is possible to design any conventional filter based on R, L and C and then translate the required passive values into those for the FDNR circuit, using the relations given above. To conclude, an example of a design using this approach will now be given.

Low-pass FDNR Filter

Figure 10 shows a T-filter using high value series inductors. Such components are inconvenient because of cost, weight, size, etc., and the use of an FDNR-based filter allows them to be eliminated. Suppose that the filter is to cut off at 500Hz, the values of the passive components being found from the following two simple formulae.

$$(1) \text{ Cut-off frequency} = 1/(\pi\sqrt{2LC})$$

$$(2) R = 2L/C$$

As a starting point, let L be equal to some arbitrary value and then evaluate C for the cut-off frequency of 500Hz; if C turns out to have a ridiculous value then choose another value of L and try again. Suppose L is 200H, then the formula (1) gives a value of C of about 1nF, a perfectly reasonable value. Now R can be evaluated from formula (2) and is found to be 632k.

Thus, for the passive circuit, the values are L = 200H; C = 1nF and R = 632k. These are the values that must now be transformed into the values for the synthesised circuit.

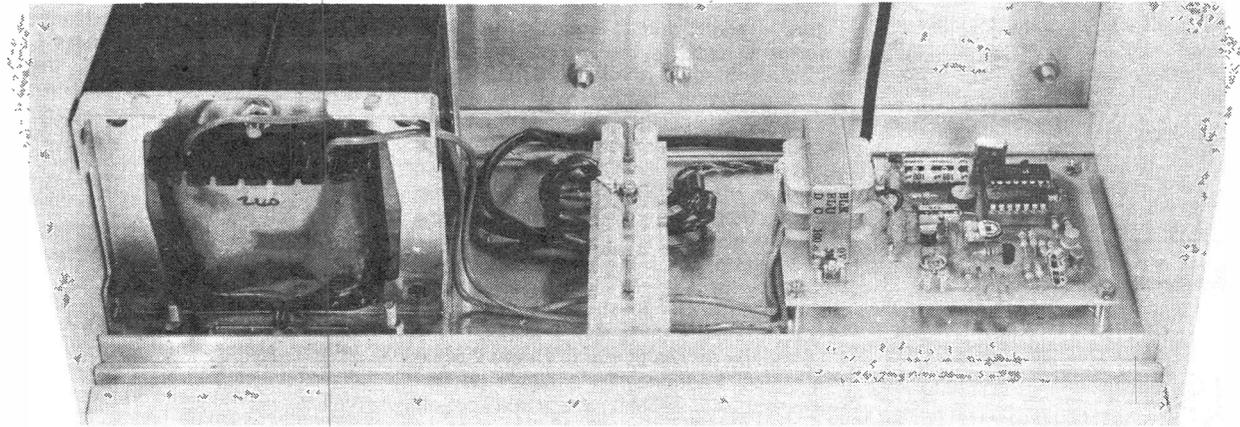
Thus, for the FDNR-based circuit, $C' = 1/(632 \times 10^3) = 1.6\mu\text{F}$; $R' = 200$ ohms and the values for the FDNR circuit are related by the expression

$$C = 1 \times 10^9 = (R1 \times R3 \times C1 \times C2)/R2$$

Again an initial choice has to be made. Suppose that a guess is made at reasonable values for the numerator e.g. R1 = 10k; R3 = 100k; C1 = C2 = 100nF, this leaves R2 as the only unknown and by substituting these values into the expression just given and transposing it, R2 is found to be 10k, which is perfectly reasonable. It is obvious that a certain amount of judgement and/or experience is invaluable in this sort of design. The complete circuit is shown in Figure 11.

This example has been presented to illustrate the unique nature of this type of active filter design. The same type of approach can be applied to other circuits employing passive components.

220/240V AC INVERTER



by Dave Goodman

- ★ Runs small domestic appliances such as televisions, hi-fi and lights
- ★ Supplied from a standard 12V car battery
- ★ Ideal for camping and caravanning

Now that winter is well on its way, bringing the threat of power cuts, a standby power source can be extremely useful. Central heating pumps can be kept running, or the family can be entertained by connecting a television to the inverter.

The need is for a 220-240V AC (50Hz) supply at 100 Watts to be

derived from a 12V car battery. The power available should be adequate for most small domestic appliances, providing that their total power requirement is less than 100W.

Circuit description

The crystal X1 and IC1 produce a stable 100Hz square wave, which is

further divided by IC2 to give two 50Hz waveforms, one of which is 180 degrees out-of-phase with the other.

The transistors TR1 and TR2 both drive the MOSFETs TR5-8, which alternately switch the windings of T2 to the 12V battery supply. D4 and D5 become forward biased if the battery is wrongly connected, blowing the fuse FS1. D6

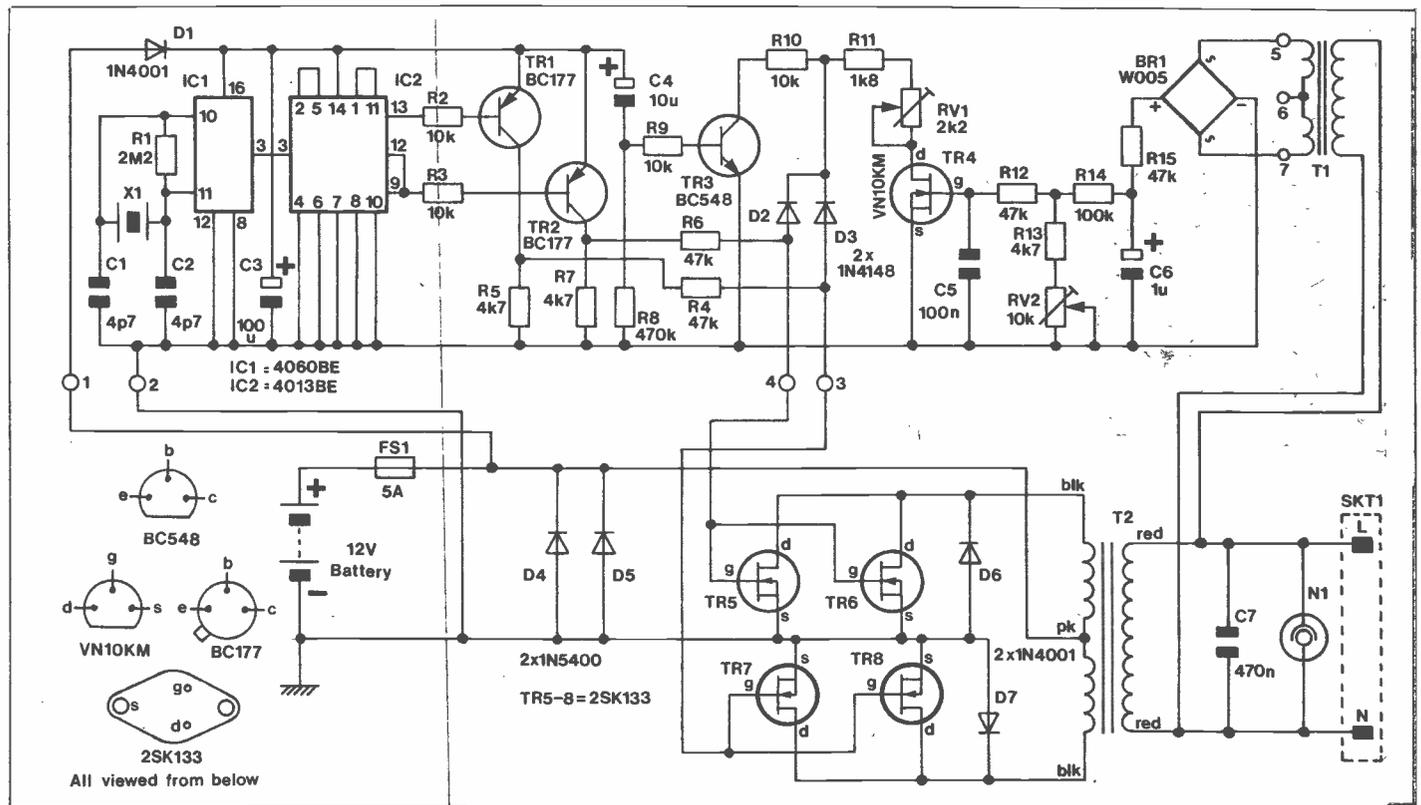


Figure 1. Inverter circuit diagram.

and D7 prevent reverse voltage spikes, developed across T2 primary windings, from damaging the MOSFETs. Transformer T2 has been specially developed for use in this system, and steps up the voltage on its primary windings from 17.5V rms to 250V rms across the secondary. Because of the fast switching action that use of the MOSFETs provides, the waveform appearing at T2 secondary under load is a good square wave, whose high harmonic content may cause problems with some equipment connected to it. C7 removes many of the upper harmonics, 'rounding off the edges' of the square wave and producing a more sine wave like waveform.

To produce a high power output, T2 turns ratio is about 20:1. With reference to the primary voltage (17.5V) this would produce 350V rms with small loads connected to T2. To control this voltage T1 monitors the supply output, producing 12V AC across pins 5 and 7 for 250V input. This voltage increases to 15V AC for 350V input, and is rectified by BR1 to produce a small DC biasing voltage at TR4 gate. TR4 acts as a voltage controlled resistor in this circuit, and the drain to source resistance decreases in proportion to a positive value voltage applied to its gate. RV2 and associated resistors determine the bias voltage to TR4. With

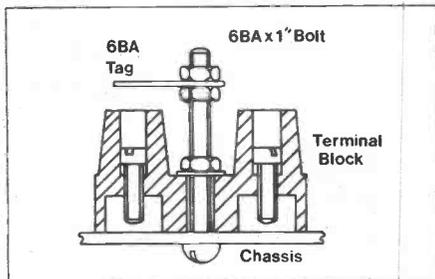


Figure 3. Chassis connection

TR4 low resistance diodes D2 and D3 both conduct, and the drive signals to the MOSFETs TR5-8 is reduced. With reduced drive T2 output voltage drops, and the monitoring voltage drops, causing TR4 to increase in resistance. D2 and D3 start to turn off, to a point where the drive to the MOSFETs is maintained and held, so the output from T2 is determined by RV2. This monitoring circuit can be likened to A.V.C. (Automatic Voltage Control). When first switched on no voltage output appears from T2 for a short period of time, this is due to the conduction period of the MOSFETs and primary windings.

When a voltage first appears C6 starts to charge, and TR4 bias is developed as before, therefore the A.V.C. being delayed allows an initial 350V AC to appear at the output. TR3 prevents this surge voltage by conducting immediately a battery is connected. D2 and D3 are forward biased by R10, and the drive signals from TR1 and TR2 are reduced. When C4 is charged, via R8, TR3 then switches off. This charge time allows the A.V.C. to be developed, and the T2 output voltage gradually rises to 240V over a one second period. The

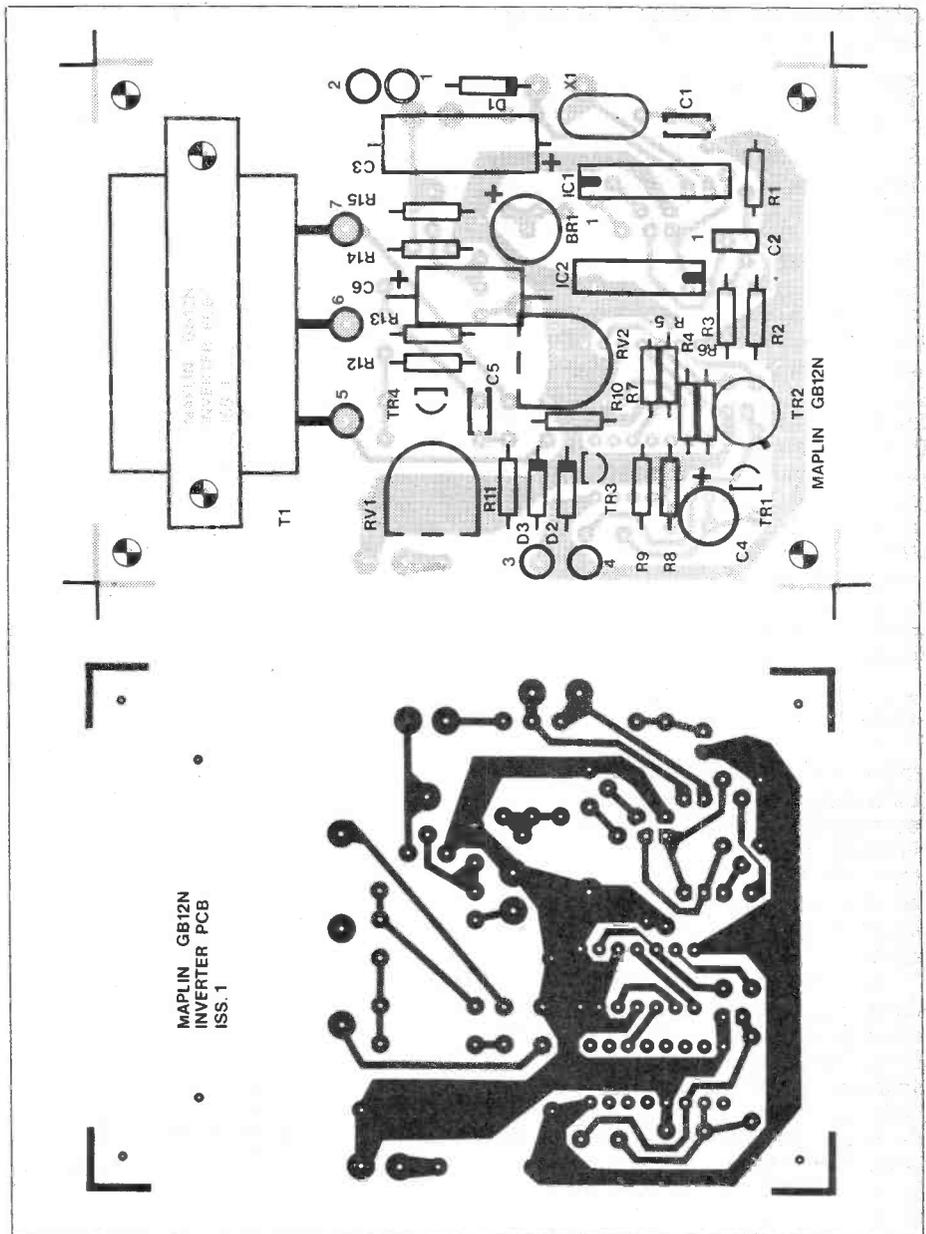


Figure 2. Legend and artwork

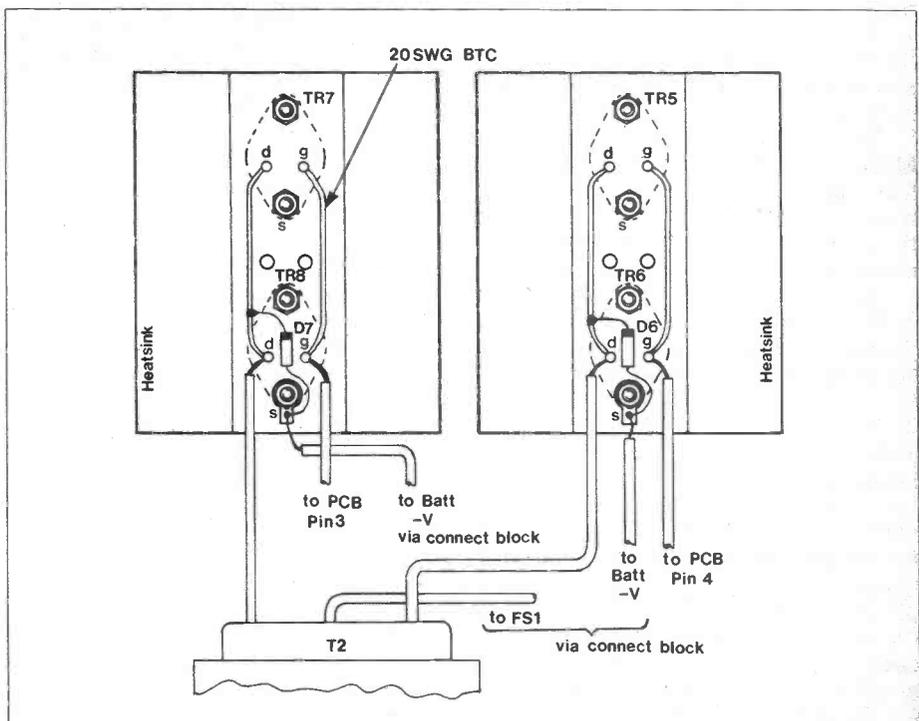


Figure 4. Heatsink and MOSFET assembly

Testing

Set RV1 fully clockwise and RV2 to halfway. Insert a 5A fuse into the holder. Remember you are dealing with 250V AC and that you should treat this with the same respect you would have for normal mains supply. Connect the battery. If you have an ammeter capable of reading up to 15A DC connect this in series with the battery positive and red connecting lead. Neon N1 should come on and the transformer may quietly buzz. The supply current should be approximately 500mA with no load connected.

Connect a voltmeter set to read 250V AC across the 13A mains socket. There should be about 250V AC present. Turn RV2 fully clockwise. The reading should drop to 190V AC, and neon N1 may flash. Turn RV1 fully anticlockwise and the voltage reading should increase to 280/300V AC. This proves the A.V.C. is working correctly. Note that these voltage readings may vary from unit to unit. Next you will need a 15W pygmy lamp and a 60/100W lamp.

Remove the battery supply and plug a 15W lamp into SK1. Turn RV1 fully clockwise again and reconnect the battery. Both neon and lamp will flicker. Turn RV2 anti-clockwise until there is a reading of 250V AC on the meter. Now remove the 15W lamp. The reading should stay at 250V AC. If it does not, turn RV1 anti clockwise until it does. This sets up the required voltage of 250V (RV2) and the A.V.C. (RV1). Connect a 60/100W lamp to SK1. The reading will drop down to 230/240V, but all is well. If you check the battery supply current now a reading of between 7 and 10A DC can be expected! The inverter is now working.

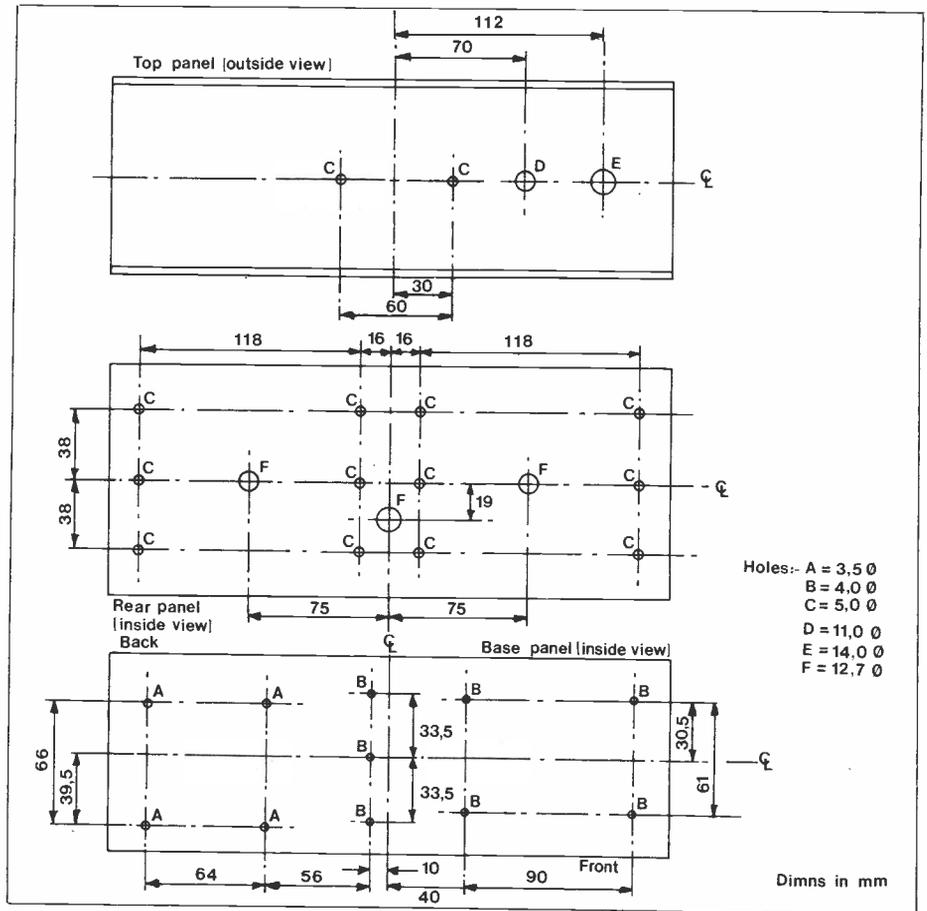


Figure 6. Chassis and drilling sizes

Finally, slot the top panel in place, followed by the blank black front panel. Fit the metal extrusion into both panels and screw to the side plates. The assembly is now complete.

The prototype has been used successfully on televisions, spot lamps, hi-fi, tuner, cassette recorders, soldering irons and AC induction motors, although the latter requires high battery

current. Some time switches or synchronous motors may not run correctly on this system, and a high current choke may need to be connected in series with T2 primary centre-tap to produce a waveform suitable for operating such appliances. This will be a matter for experimentation, and outside the scope of this article.

INVERTER PCB PARTS LIST

Resistors: All 0.4W 1% Metal Film

R1	2M2		
R2,3,9,10	10k	4 off	(M2M2)
R4,6,12,15	47k	4 off	(M10K)
R5,7,13	4k7	3 off	(M47K)
R8	470k		(M4K7)
R11	1k8		(M470K)
R14	100k		(M1K8)
RV1	2k2 Hor-sub min Preset		(M100K)
RV2	10k Hor-sub min Preset		(WR56L)
			(WR58N)

Capacitors			
C1,2	4p7F Ceramic	2 off	(WX40T)
C3	100uF 25V Axial Electrolytic		(FB49D)
C4	10uF 35V P.C. Electrolytic		(FF04E)
C5	100nF Minidisc		(YR75S)
C6	1uF 63V Axial Electrolytic		(FB12N)
C7	470nF IS Cap		(FF58N)

Semiconductors			
D1	1N4001		(QL73Q)
D2,3	1N4148	2 off	(QL80B)
TR1,2	BC177	2 off	(QB52G)
TR3	BC548		(QB73Q)
TR4	VN10KM		(QQ27E)
IC1	4060BE		(QW40T)
IC2	4013BE		(QX07H)

Miscellaneous			
BR1	W005		(QL37S)
X1	Crystal 3.2768 MHz		(FY86T)
T1	6-0-6 Sub-min Transformer		(WB00A)
	14 Pin DIL Skt		(BL18U)
	16 Pin DIL Skt		(BL19V)
	Veropin 2141	1 pkt	(FL21X)
	Inverter PCB		(GB12N)

ADDITIONAL PARTS LIST

Semiconductors			
D4,5	1N5400	2 off	(QL81C)
D6,7	1N4001	2 off	(QL73Q)
TR5-8 inc.	2SK133	4 off	(QQ36P)

Miscellaneous			
T2	Inverter transformer		(XG29G)
FS1	5 amp fuse x 1 1/4"		(WR15R)
	Safe fuseholder 1 1/4"		(RX97F)
SKT1	Single skt unswitched		(HL68Y)
N1	Square neon red		(RX81C)
	Terminal block 15A		(HL54J)
	Heatsink 10 DNDR	2 off	(FL55K)
	Surface Pattrns 29mm single		(YB15R)
	Charger clip	2 off	(HF26D)

4BA solder tag	2 off	(BF28F)	Bolt 6BA x 1"	3 off	(BF07H)
6BA solder tag		(BF29G)	Nut 6BA	9 off	(BF18U)
Bolt 2BA x 1/2"	12 off	(BF00A)	Washer 6BA	7 off	(BF22Y)
Nut 2BA	14 off	(BF16S)	Spacer 6BA x 1/4"	4 off	(FW34M)
Washer 2BA	14 off	(BF20W)	Systoflex 2mm Ø 150mm		(BH06J)
Bolt 4BA x 1/2"	12 off	(BF03D)	20A cable blk	1M	(XR57M)
Nut 4BA	12 off	(BF17T)	20A cable red	1M	(XR59P)
Washer 4BA	10 off	(BF21X)	Large grommet	3 off	(FW60Q)
Csk bolt 2BA x 1/2"	2 off	(LR54J)	20 SWG B.T.C.	500mm	(BL13P)
Bolt 6BA x 1/2"	4 off	(BF06G)	BOX NM3		(YK43W)

A complete kit of all parts excluding the case is available for this project. Order As LW95D (Inverter Kit). Price £49.95. The case suggested for this project is the NM3, shown on page 71 of our 1983 catalogue. Order As YK43W.

STARTING POINT

by R. Penfold

Introducing the fundamentals of electronics for the constructor.

UJTs, FETs and SCRs

In this final article in the "Starting Point" series we will consider some of the semiconductor devices which have not been covered by previous articles in the series. The devices that will be discussed here are unijunction transistors (UJTs), junction field effect transistors (Jfets), VMOS transistors, and silicon controlled rectifiers (SCRs).

UJTs

Unijunction transistors used to be quite popular, but are not often used in new designs due to the availability of inexpensive integrated circuits such as the 555 timer device which give more predictable results and greater versatility. Unlike other forms of transistor a UJT cannot be used as an amplifier, and these devices are in fact normally only used as the basis of relaxation oscillators. A UJT is analogous to two resistors and a silicon diode connected in the manner shown in Figure 1. The total resistance through the resistors is several kilohms and the upper resistor is normally somewhat lower in value than the lower one.

A UJT is used in the oscillator configuration shown in Figure 2, and this

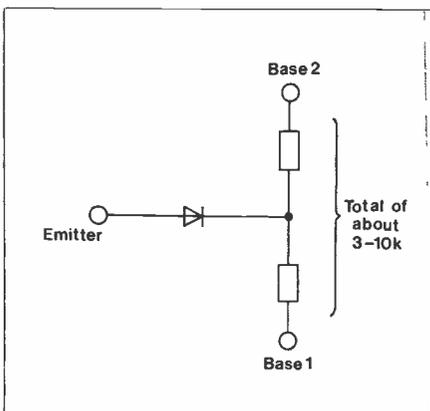


Figure 1. A UJT is analogous to this circuit.

provides three output waveforms (which are shown in the diagram). A UJT is a three terminal device like ordinary bipolar types, but the terminals have different names, these being base 1, base 2 and emitter. In the circuit of Figure 2 there is initially an extremely high input impedance at the emitter of Tr1 as there is effectively a reverse biased silicon diode here, and C1 is therefore free to charge by way of R1. When the charge on C1 reaches something in the region of 65 to 90% of the supply voltage (depending on the particular device used), the voltage at the emitter becomes slightly higher than the voltage at the junction of the two resistances within the UJT, and the silicon diode then becomes forward biased.

At this point a current flows into the

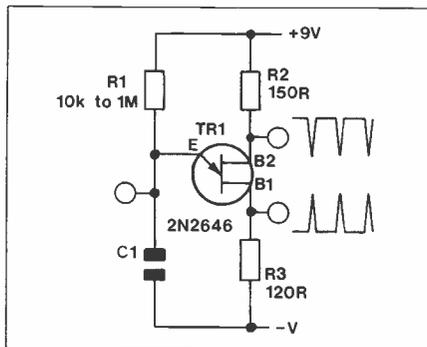
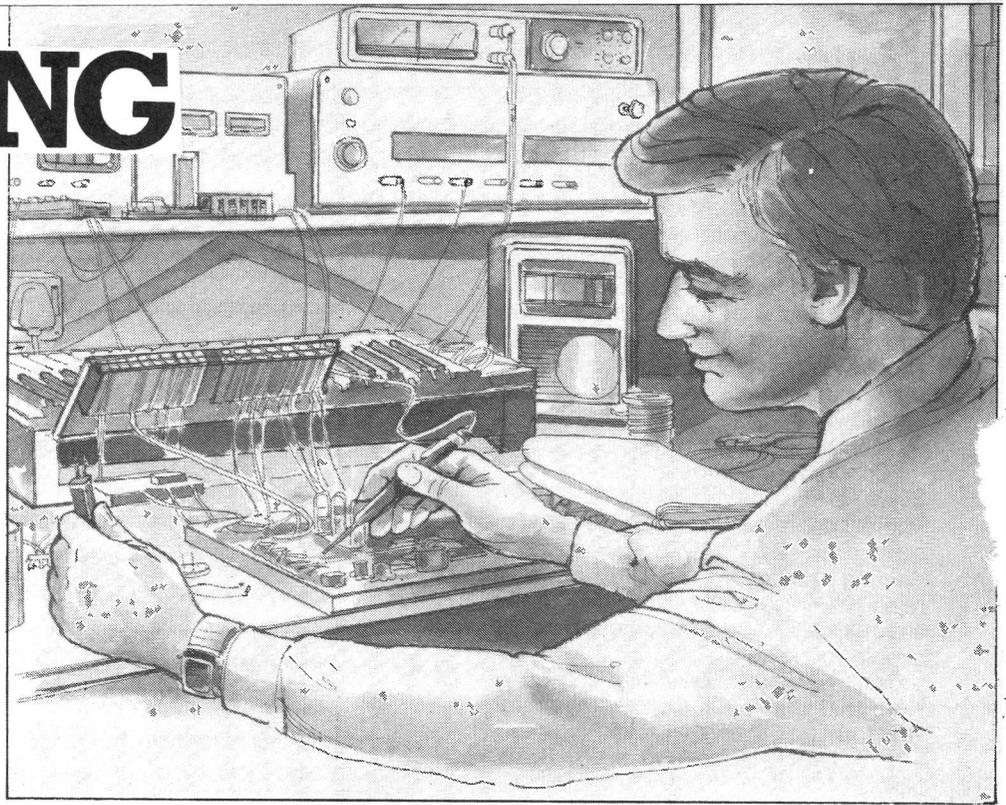


Figure 2. A UJT relaxation oscillator and output waveforms.

emitter of the device, and a regenerative action within the UJT causes the input impedance to the emitter to fall to a very low level. At the same time the resistance between the base 1 and base 2 terminals falls substantially. C1 largely and rapidly discharges into the emitter of Tr1 until the charge voltage is no longer high enough to sustain the regenerative action, and the device then reverts to its original state. C1 then starts to charge again, and this process continues with a nonlinear sawtooth waveform being produced across C1. This signal is at a fairly high impedance, especially if R1 has a high value. As C1 discharges, positive pulses are produced at the base 1 terminal and negative pulses are generated at the base 2 terminal. These are both at a low impedance.

It is important to realise that you cannot produce a UJT by simply connecting two resistors and a diode in the configuration shown in Figure 1. A UJT actually consists of a bar of silicon which forms the two resistances, with a single semiconductor junction on the bar to form the diode. It is from this single junction that the name unijunction is obtained. Two resistors and a diode connected in the manner shown in Figure 1 will not produce the regenerative action required to trigger the UJT to the on state.

R1 should not have a value of less than about 10k or it will supply enough current to hold Tr1 in the on state and oscillation will be blocked. Similarly, if R1 is made more than about 1 megohm in value it will not supply

enough current to trigger Tr1 properly, and oscillation will not take place. Another point to bear in mind is that R2 and R3 must be very low in value or they will prevent the circuit from operating.

Jfets

The three terminals of a Jfet are called the gate, drain, and source, and these roughly correspond to the base, collector, and emitter of bipolar transistors. Jfets are depletion mode devices, and they require bias circuits that are subsequently different to those employed with bipolar transistors. However, like bipolar transistors they can be used in three amplifying modes which are

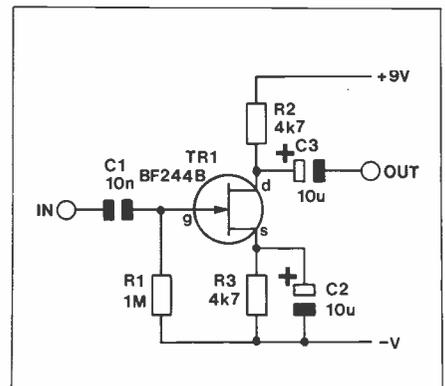
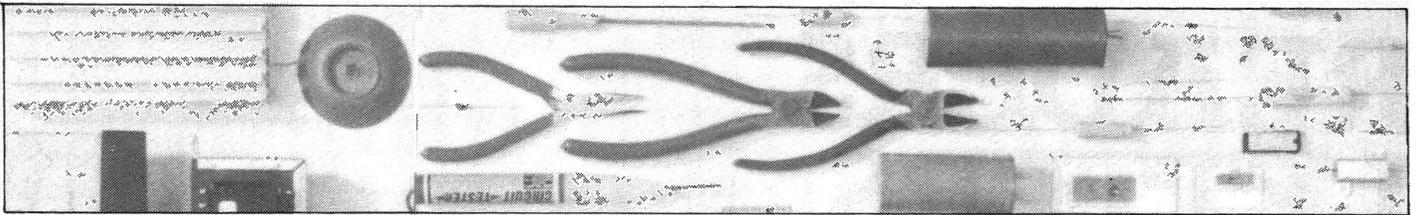


Figure 3. A simple JFET common source amplifier.

the common source, common drain (or source follower), and common gate modes. The equivalent bipolar configurations are the common emitter, common collector (or emitter follower), and common base modes respectively.

Figure 3 shows the circuit diagram of a simple common source amplifier which helps to highlight the difference between Jfet and bipolar devices. Whereas ordinary transistors are normally switched off and require a forward bias to enable them to be used as amplifiers, Jfets are normally in the on state and require a reverse bias in order to partially switch them off so that they can act as linear amplifiers. In Figure 3 the gate of Tr1 is biased to the negative supply potential by R1, while R2, the drain to source



resistance of Tr1, and R3 form a potential divider across the supply lines. The potential developed across R3 takes the source terminal of Tr1 about two or three volts positive, and the gate is therefore about two or three volts negative of the source and has the required reverse bias.

An important difference between bipolar and field effect devices is that the latter have a very high input impedance and consume very little input current. The input impedance of a Jfet is typically about one thousand megohms at low frequencies (the input capacitance gives reduced input impedance at high frequencies), and some field effect devices have an input impedance of over a million megohms. The gain of a field effect transistor is not therefore specified as a certain current gain since such a figure would be of little practical value, but instead it is the transconductance that is specified. This relates the

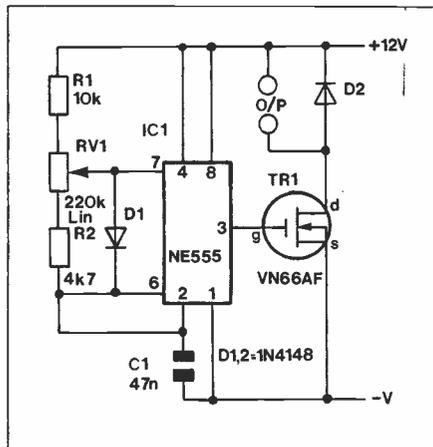


Figure 4. A motor speed controller using a VMOS transistor.

change in input voltage to the change in output current, and in data sheets "gm" is the abbreviation often used for transconductance.

Transconductance is usually specified in milli-mhos, and this unit is equal to a one volt change in input potential giving a change in output current of 1 milliamp. Transconductance is equal to output current divided input voltage which is the opposite of the formula for finding resistance in ohms, and it is from this that the name 'mho' is derived. Milli-mho is sometimes abbreviated to m Ω . Transconductance is sometimes specified in micro-mhos, and this unit is simply a thousandth of a milli-mho. A Jfet has a gm of something in the region of 2 to 7 mhos.

The circuit of Figure 3 has a voltage gain of only about 20dB (ten times) which is only about a tenth of the voltage gain obtained using a high gain bipolar transistor. However, by making R1 high in value a high input impedance can be achieved with a figure of approximately 1 megohm being obtained in this case. This is about one hundred times higher than the input impedance achieved using a high gain bipolar transistor.

The BF244B is an N channel device which is comparable to an npn bipolar device. There are also P channel devices such as the 2N3820, and these have the same circuit symbol apart from the arrow in the gate part of the symbol, and this points in the opposite direction for a P channel type.

VMOS devices

Until recently there were no field effect power devices available to the amateur user, and there were in fact no really practical power f.e.t.s. at all. Power Jfets are now produced, but are difficult to use and are not available to amateur users. There are other types of power f.e.t. though, and the most common type is the VMOS transistor.

These are enhancement mode devices, and are similar to bipolar transistors in that the device is cut off with a gate bias voltage of zero, and does not begin to conduct until a gate potential of about 0.8 to 2 volts is reached. Like all field effect devices, the input impedance of VMOS transistors is very high and they are voltage rather than current operated. They have transconductance figures which are much higher than those of Jfets, and they obviously need to be since they are power devices which might need to control output currents of a few amps with an input voltage change of just a few volts. Most VMOS devices have a gm of about 250 mhos, which means that a 4 volt change in the input potential gives a 1 amp change in output current! High power types have gm values in excess of 1000.

VMOS transistors can be used in the output stages of audio power amplifiers and other high power linear applications, and their freedom from secondary breakdown and thermal runaway plus their excellent high frequency response make them in many respects ideal for such applications. They are also useful for switching applications such as the simple pulse type motor speed controller circuit of Figure 4. VMOS transistor Tr1 can be driven direct from the output of the 555 timer I.C. without the need for any current limiting resistor since Tr1 is

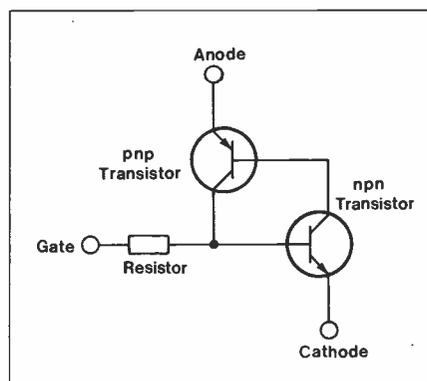


Figure 5. An SCR is analogous to this circuit.

voltage and not current operated. For the same reason there is no need to have a low impedance drive circuit capable of supplying a few hundred milliamps, and although the VN66AF can handle drain currents of up to two amps it can be driven from a fairly high impedance source (such as a CMOS logic device) unless the input frequency is quite high. The input capacitance of most VMOS transistors is only about 50pF and it is really only at radio frequencies that the input impedance of these devices falls to a fairly low level.

VMOS transistors are susceptible to damage by high static voltages and many types (including the VN66AF) have a 15 volt zener protection diode connected between the gate and source terminals. Obviously the

gate potential should not be allowed to exceed 15 volts or a high input current could flow with the device being damaged in consequence.

Power MOSFETs are another type of high power field effect devices. They are primarily intended for use in very high quality audio power amplifiers, and designs of this type have been featured in previous issues of this magazine.

S.C.R.s

Silicon controlled rectifiers or "thyristors" as they are popularly known, are switching devices and cannot be used for linear amplification. These are analogous to the circuit shown in Figure 4.

Initially both transistors will not receive any base current and will be switched off, but if a forward bias of about 0.6 volts is applied to the gate terminal the npn transistor will begin to conduct and supply a base current to the pnp transistor. This device then supplies a base current to the npn transistor, and a regenerative action results in both transistors switching hard on. They

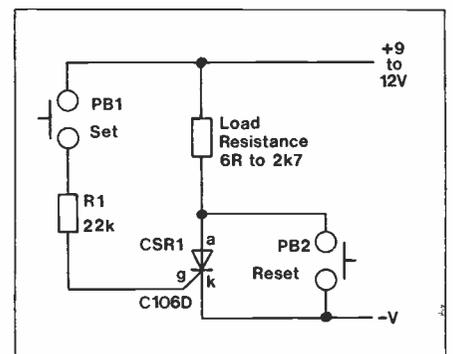


Figure 6. A simple bistable circuit using an SCR.

remain in this state even if the forward gate bias is removed, and the device conducts between the anode and cathode terminals with a voltage drop of about one volt or so between the two.

The simple bistable circuit of Figure 6 demonstrates the basic properties of an S.C.R. Power will not be supplied to the load until PB1 is operated and a gate current is fed to CSR1 through current limiting resistor R1. The C106D device specified for CSR1 is a sensitive device which requires a gate trigger current of no more than 0.2mA, but most thyristors require a trigger current of as much as 20 or 30mA. When PB1 is released CSR1 remains switched on provided the current through the load is high enough, and the hold-on current for the C106D is no more than 3mA. Again this is lower than the figure for most types, and a hold-on current of about 20 to 35mA. is more common. Apart from a few special types it is not possible to switch off a thyristor by reverse biasing the gate, and the only way to switch off the device is to take the anode to cathode current below the hold-on level. In this circuit this is achieved by momentarily operating PB2 so that the current flow is briefly diverted from CSR1.

A triac is similar to a thyristor, but it will operate with gate and load voltages of either polarity (they can even be of opposite polarity). Triacs are mainly used to control A.C. loads in applications such as lamp dimmers and drill speed controllers.

READERS LETTERS

CB Transceiver

Dear Sir,
After receiving the last issue of my year's subscription to the 'Maplin Magazine' I must say that I am very pleased with the projects and articles that have been published over the year.

However, I am slightly disappointed that the '2m/CB transceiver' project which was to be published in the first year has not yet appeared — nor is it due to appear in issue 5! After all, it was originally on the strength of this project that I subscribed to the magazine.

I wonder if it would be possible to inform readers, in the magazine, when this project is likely to appear.

CHRIS WALKER
Darwen, Lancs

When we first conceived this project, there was a great deal of interest in CB, but over the months interest has waned considerably. Also we were surprised at the cheapness of the ready-made transceivers and it is unlikely that our kit would have been competitive. In the meantime, prices have fallen even further, making our potential project of less and less interest. In view of these factors we decided not to go ahead with the project. However, most of the design work that was done will be utilised in a new major radio project that we are hoping will be ready for issue 7.

Centripetal Not Centrifugal

Dear Sir,
Many of my pupils take your magazine; I myself do not, but I am sure it is an excellent publication. My pupils assure me of this.

However, I do not feel that your article featuring Fig. 1 of the September issue shows a gross error on basic physics. In the diagram mentioned you show a satellite orbiting the Earth in which there are two equal and opposite forces acting on it. Such a satellite would not orbit the Earth but would move in a straight line to infinity, or until it encountered something, in accordance with Newton's first law. Your satellite should have an unbalanced centripetal force, equal to the force of gravity. The centrifugal force shown in your diagram should not exist. There is no such thing!

D. STIRZAKER
St. Benedict's School,
London

BBC Micro vs Atari

Dear Sir,
I was very annoyed to see how you replied to a letter in the June-August edition of the Maplin Magazine. I am referring to what you said about the BBC micro.

Certainly, the BBC micro could be used as a business machine. This is because of its extremely good operating system and basic interpreter, and its superb facilities for expansion. But this does not make it unsuitable as a home computer, for which it was originally designed.

As for your comment about software backup, you are totally wrong here. The BBC micro will have a far better software backup than any other home computer in a short while. This is because the BBC are showing programs for the BBC micro on CEEFAX (and you do not have to buy the special equipment to load it directly if you don't mind a bit of typing. Also, the features I mentioned which make the BBC Micro suitable for business will also attract software writers and companies to produce software for it. I know this because the school I go to has a BBC micro and I have been able to compare it with the Commodore PETS we have. I also know some very unsatisfied owners of Commodore VICs and can assure J. G. Ashdown that the BBC Micro is by far the best home computer available at the moment.

Remember that any magazine which misleads its readers in this way concerning a very good British-made computer is doing serious damage to the British economy.

E. T. GRIMLEY EVANS
Gosforth, Newcastle-on-Tyne

We never said the BBC Micro was not a good machine; it is an excellent machine. What we did say was that for home use, the Atari is a much better proposition. Much is made of the vaunted Tube on the BBC micro that allows a second processor to be added so that computing can be separated from input/output work (i.e. keyboard, VDU, printer, cassette, disk, user ports). Great!

The Atari, however, already has three chips other than the 6502 which do all this and more. One of them called ANTIC is a true microprocessor with its own program, that handles screen displays. Another is the GTIA chip that also assists ANTIC with screen displays and handles the comprehensive sound system. The third chip is called POKEY and this deals with I/O from the keyboard, paddles and other peripherals. Each of these chips is as complex as the 6502 itself.

On software, the BBC micro just doesn't stand a chance of ever having the back-up that Atari has. In America more than 30 software houses in addition to Atari themselves are writing for Atari. And they've already produced well over a hundred different titles. More titles are coming fast and furious as software houses adapt Apple programs for Atari (Atari is now outselling Apple in the States). In addition there are over a hundred titles available through APeX (the Atari Program Exchange). The few letters writing for the BBC just don't stand a hope of ever catching up.

And anyway what sort of software is being planned for the BBC Micro: Unix, UCSD Pascal, Fortran, Cobol, LISP. With the exception of Pascal and LISP, the others are not suitable for home use. They're big, business or university, multi-user systems and Cobol and Fortran only come into their own on giant programs.

On the other hand Advanced BASIC, Forth, LISP, Tiny-C and Pilot are

already available for the Atari and are languages that can be used at home to give meaningful results. Everything about the BBC micro is BIG. So if you want a giant system at home and can afford it, you may be pleased with the BBC micro, but don't expect the basic machine to be able to do what the Atari can do for the same price or you'll be very disappointed.

Additions To 25W MOSFET Amp

Dear Sir,
Congratulations to Dave Goodman on designing the Superb 25W MOSFET Amp, however I have a couple of questions about the design.

Firstly, why were DIN input sockets used, as nearly every piece of hi-fi equipment is supplied with leads terminating in phono plugs. DIN sockets and plugs are generally only used in tape record/playback leads. Secondly, why wasn't a source/monitor switch provided as this enables quick comparison between the music source and the recording. Also having this switch prevents oscillation when the record control is depressed on the tape deck while having the input switched to tape.

I realise these additions would have meant extra wiring and components not mounted on the PCB, but surely the improvement in convenience would make it worthwhile. Thank you for an otherwise good project.

R. JONES
Buckden, Cambs

It is relatively easy to make simple phono to DIN adaptors, but much more difficult to fit phono sockets on the back panel and wire them to the circuit board. Each phono socket makes just one connection whereas a DIN can make two or more, so they take up more space and require more complex holes with screw-heads showing unless a sub-panel is used. The extra space used would have made it difficult to fit the remote control unit.

Extra facilities could have been provided of course, but a source/monitor switch is just one of many. Any of them would have added to the cost and complexity, and these we wished to avoid.

Universal Timer Builder

Dear Sir,
Thank you for the third issue of your magazine in which you include a request for more letters, so we hereby oblige! First I agree with most of your customers/readers that your delivery service is very good, which, as well as the goods, is what we pay for. I, too, like the magazines for the wide variety of subjects dealt with.

Recently I completed L. H. Harrold's "Universal Timer" which is now working well, but, my goodness, the trouble I had with those wretched 10 way sockets!* I was getting all sorts of horrific effects until I bent each pin and coated them with solder. Couldn't you sell a made up version?

Also I had to find an old metal meter case to house the unit in order to heat sink the mains transformer. It gets pretty warm!

By the way, I found that a 13 amp outlet socket on a surface mounting box with the relay panel housed in a further box bolted underneath it is excellent for each remote controlled-point.

Yes thank you. I'm glad I joined the club and look forward to our future.

D. C. EMMERSON
Northampton

Atari Is A Dinosaur

Dear Sir,
Your reply to J. G. Ashdown on the BBC Micro left me speechless. How you can call a £645 dinosaur a "home computer" is beyond me. Just look at the popular computing press and show me where the adverts are for Atari software (apart from yours). I belong to the East Antrim Computer Club and none of our considerably large membership has ever seen an Atari. Many of us have sold our machines to buy BBC Micros and ZX Spectrums. I used to own an 8K PET before I bought my BBC Model B and so the mere mention of "Commodore back-up" had me in fits of laughter. £396 for a single disc drive for the VIC? Come on Maplin, just who do you think you're kidding. Seriously though, I honestly believe your choice of machines leaves much to be desired and unless Atari/VIC prices fall dramatically then you will be left with egg on your faces.

ALLISTER MURPHY
Carrickfergus
Co. Antrim

We have to agree that Atari's own marketing of their computers has, up to now, been abysmal. But since you've never seen an Atari how can you compare it with others? I can tell you that its streets ahead of the BBC micro and the ZX Spectrum (see our reply to Mr. Grimley Evans letter below). We stock the Commodore VIC20 as a lower cost alternative to the Atari, though we agree that their disc drive is overpriced, but you can't say they have no back-up - they even publish their own magazine packed with programs and information.

Suggestions For New Stock

Dear Sirs,

Might I suggest a few additions to your excellent range of electronic components?

(1) 4mm plugs with 4mm cross-hole (I believe they are called "Bunch Plugs"). (2) I.C.s CA 3130 and CA 3140 in DIL package. (3) 10M 1% resistors. Circuits for electronic multi-meters often specify them. (4) 2mm plugs with tips long enough to suit multimeters such as the Super-tester 680R etc.

While writing, I would like to thank you for replacing the faulty 'scope probe so promptly a month ago.

L. W. DEWHURST
Leamington Spa, Warwickshire

CIRCUIT MAKER

Simple NiCad charger

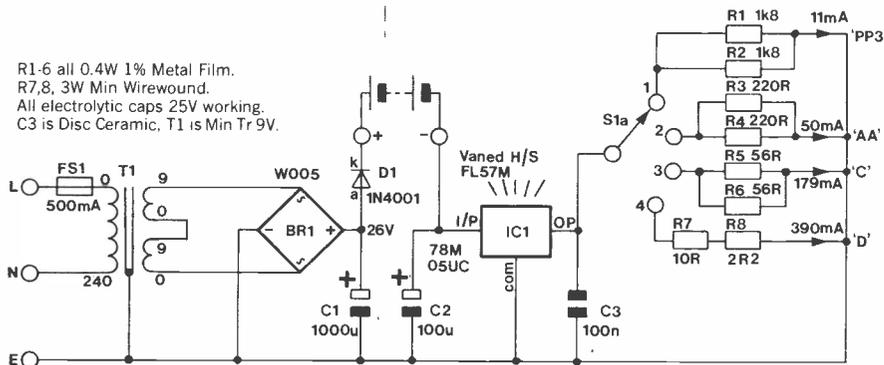
J. R. Smith, Paignton, Devon

Most commercial NiCad chargers have connections for the A to D range of cells, but do not include PP3 type batteries. This circuit will charge from 1 to 6 standard 1.2V NiCads or one PP3 type in ten hours. If more than one cell is being charged then they should be connected in series, and the charging connection is made between positive and negative pins at IC1 input.

Switch S1 selects the appropriate range for the cell to be charged, and this must be chosen before applying mains power.

Resistors R1 to 8 determine the current flowing through IC1, which is a constant voltage regulator. The total current flowing through the NiCad will therefore be resistor (load) current and IC1 drive current (3 to 4mA). Bolt the IC onto a suitable heatsink when charging C or D type cells.

R1-6 all 0.4W 1% Metal Film.
R7,8, 3W Min Wirewound.
All electrolytic caps 25V working.
C3 is Disc Ceramic, T1 is Min Tr 9V.

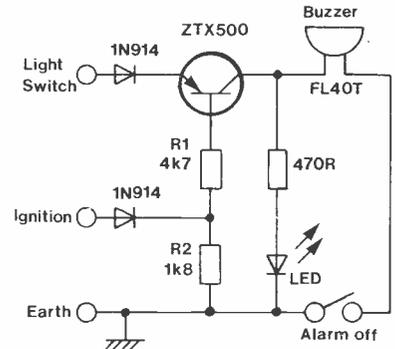


Simplified car lights reminder

J. M. Dunnett, Prestatyn, Clwyd

This circuit uses less components than the one published in Issue 1.

With the ignition off, the base of the transistor is held sufficiently low via R1 and R2 to cause it to conduct. If the lights are also on, 12V from the lighting circuit will pass through the conducting transistor and activate the buzzer.



If the ignition is switched on, the transistor base is taken high, it no longer conducts, and the alarm ceases.

The switch and LED are optional and are intended to cater for situations where the lights have to be left on with the ignition off.

ATARI VIDEO GAME

NEW CARTRIDGES FOR ATARI VIDEO GAME

Over the next three months, five new cartridges will be released by Atari for the Video Game Console.

Star Raiders

At last the most popular of Atari's Computer games becomes available for the Video Game. A vicious star battle in the glory of 3D, this game will be even more popular than Pac-Man or Space Invaders. The cartridge comes complete with its own keypad controller. For one player only, a joystick controller is also required.

Order As BC53H (VCS Star Raiders) Price £29.95

ET - The Extra-Terrestrial

ET needs your help! The lovable little alien is stranded on the planet Earth, and just like in the movie, he needs an interplanetary phone to contact his friends for rescue. Help him find the parts he needs. Call Elliott to guard him and help ET return to the planet he loves. Contains 3 games, played with a joystick controller.

Order As BC54J (VCS ET) Price £29.95

Volleyball

Superb graphics on this the first of Atari's new series of Sports Games offering a high degree of realism.

Order As BC55K (Volleyball) Price £29.95

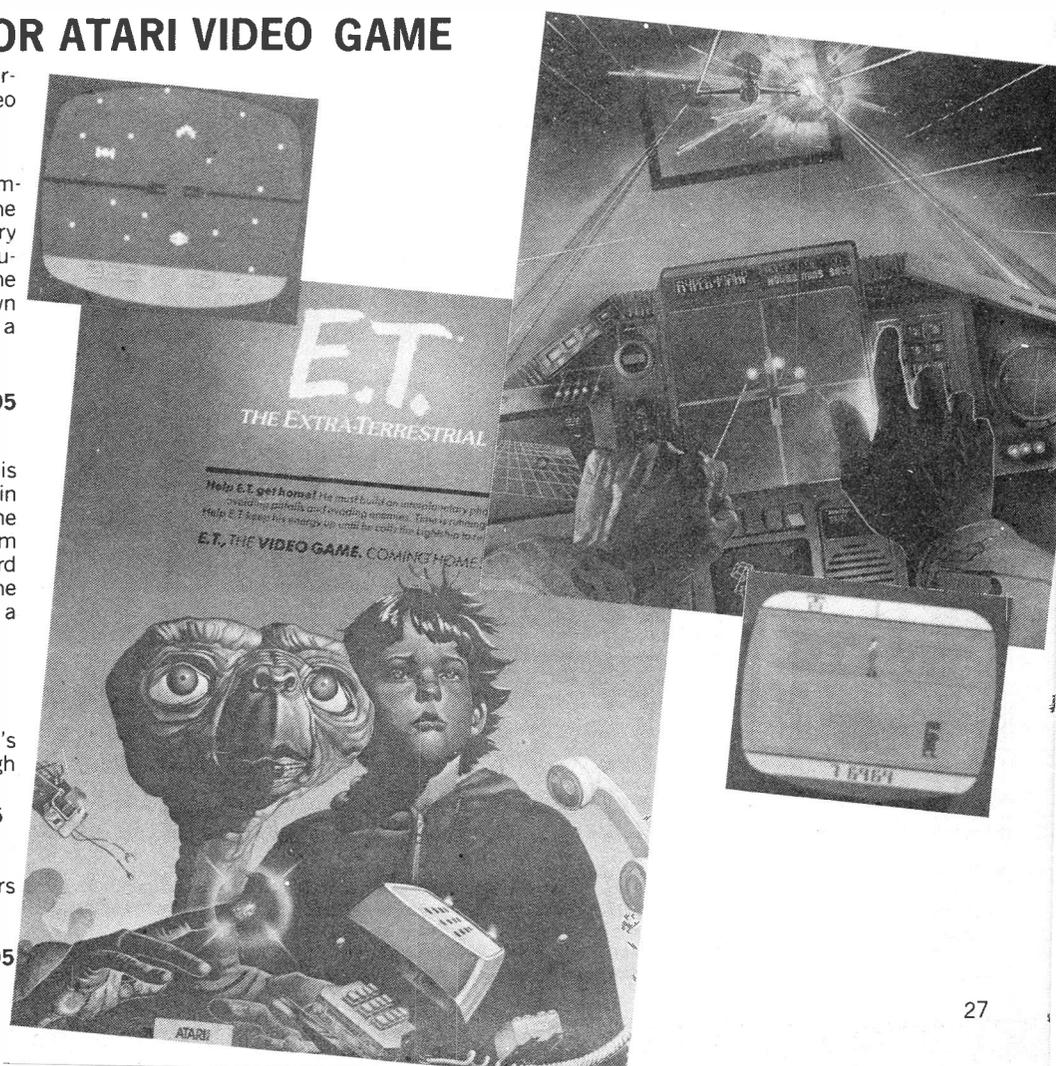
Also Coming

Due for release in January 1983 are Raiders Of the Lost Ark and Frog Pond.

Order As AC76H (Raiders Of Lost Ark) Price £29.95

BC56L (Frog Pond) Price £29.95

December 1982 Maplin Magazine



PRICE LIST

All prices shown in this price list are valid from 15th November 1982 to 12th February 1983

Please note new telephone number for Sales Only (0702) 552911

Prices shown in this list include VAT at 15% where applicable. Items marked NV are rated at 0% and the price shown applies both to inland and export orders. Overseas customers should add up the total cost of all items except those marked NV and deduct 13% to arrive at the total price excluding VAT. Alternatively multiplying the total price (except NV items) by 0.87 will give the total price excluding VAT. Please add extra for carriage on all overseas orders. Carriage will be charged at cost.

Although postage charges to customers living in the Republic of Ireland and in the UK, but not on the UK mainland, are the same as to mainland addresses we regret that we must levy an additional charge of £5 on each order containing any items marked "Delivery by Carrier".

Will customers from the Republic of Ireland please add 40p and then 35% to the cost of their order now that the Irish pound is not equivalent to sterling, to cover the rate difference and negotiation fees. We will refund any difference; please state cheque or credit note. Alternatively if you pay by bank draft drawn in pounds sterling on a London bank, then you need add nothing extra. Bank drafts drawn in pounds sterling on a London bank should be readily available from your local bank.

All prices are for the unit quantity shown in the catalogue (unless shown otherwise on this list) i.e. each, per pack, per metre etc. All prices include postage and packing. There is a 50p handling charge which must be paid on all orders having a total value of under £5.00.

The price list is intended for use with our 1983 catalogue and applies to all mail orders. Prices in our shop are generally lower on heavy items as mail order prices include postage and packing costs.

Copies of manufacturers' data sheets are available for most IC's - price 40p each.

Prices charged will be those ruling on the day of despatch

1983 Catalogue Page No.	VAT inclusive PRICE	1983 Catalogue Page No.	VAT inclusive PRICE	1983 Catalogue Page No.	VAT inclusive PRICE	1983 Catalogue Page No.	VAT inclusive PRICE
Page 15		X053H Mast Bracket Type 8	£8.50 (B)	Page 25		BOOKS	
X022Y Pirate Attack Poster	£1.00NV (D)	X054J Mast Bracket Type 8	£12.75 (A)	RK48C 8-Section Antenna	£1.15 (D)	Page 29	
X012N Maplin Poster	£1.00NV (D)	BW44X Mast Bracket Type 14	£4.65 (C)	RK49D 6-Section Antenna	£1.15 (D)	WA27E Basic Elec & DC Ccts.	£12.64NV (A)
AERIALS		BW45Y Loft Bracket EM4	£2.65 (C)	LB10L Telescopic Aerial 1.22m	£3.30 (C)	WA28F Basic AC Ccts.	£10.95NV (A)
Page 20		X056K Lashing Kit Type 4	£2.85 (B)	Y032W TVI Filter	£3.25 (B)	RL27E Book NB147	£6.95NV (B)
X022A Mushkiller FM224	£12.25 (A)	X056L Lashing Kit Type 6	£1.95 (A)	RH64U Aerial Rotator	£39.95 (A)	WG10L Book JW787	£7.34NV (B)
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X025C Mushkiller FM244T	£17.80 (A)	X058N Lashing Kit Type 9	£12.24 (A)			RL31J Book NB157	£4.35NV (C)
X027E Mushkiller FM264T	£24.50 (A)	X0600 Mast D	£3.75 (C)			RL29G Book NB152	£2.56NV (C)
X028F Mushkiller FM284T	£30.50 (A)	X061R Mast E	£7.45 (B)			RR02C Book NB245	£4.99NV (C)
X029G Trucolour TC10 Grp A	£10.50 (A)	X062S Mast G	£15.95 (A)			RK46A PCB Mounting 3.6V Bat.	£2.82NV (C)
X030H Trucolour TC10 Grp B	£9.40 (B)	X063T Mast M	£5.79 (B)				
X031J Trucolour TC10 Grp C/D	£9.94 (B)	BW46A Masthead UP1300/W	£10.90 (A)			Page 30	
X032A Trucolour TC10 Grp E	£9.94 (B)	BW49D Masthead UP1300/V	£11.94 (A)			XW31J Book MM639	£1.95NV (D)
X032K Trucolour TC13 Grp A	£11.85 (A)	BW50E Power Unit PU1240	£14.65 (A)			XV12N Book NB386	£4.10NV (C)
X033L Trucolour TC13 Grp B	£12.20 (A)	Page 23				RH85V Book NB048	£3.90NV (C)
X034M Trucolour TC13 Grp C	£11.45 (A)	YK73Q Amp XB11U	£15.80 (A)			WG71N Book BP94	£2.10NV (C)
X035O Trucolour TC18 Grp A	£13.95 (A)	BK06G Amp VX18	£16.95 (A)			XW00A Book FT882	£5.90NV (A)
X036P Trucolour TC18 Grp B	£13.85 (A)	Y022Y Xtra Set Amp	£14.45 (A)			WA44X Understanding Auto Elec.	£4.95NV (A)
X037S Trucolour TC18 Grp C/D	£13.25 (A)	W036P Plugpak 200	88p (E)			RL13P Book NB099	£2.55NV (B)
X037A Trucolour TC18 Grp E	£13.25 (A)	BW51F Diplexer UF20	£5.55 (B)			WQ21X Book NB344	£6.08NV (A)
Page 21		BW52G Splitter CS1000	£8.95 (B)			RF19V Book NB286	£4.20NV (A)
X038R Extragain XG5	£16.50 (A)	BW53H Splitter SB20	DIS			RL06G Book NB0740	£4.74NV (A)
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X040T Extragain XG8 GroupB	£23.50 (A)	Y023A Splitter CS200	£4.45 (C)			RL02C Book NB059	£5.15NV (A)
X041U Extragain XG8 GroupC	£21.50 (A)	H877U Surface Co-Ax Outlet	75p (E)			RH04E Book BP6	85pNV
X042V Extragain XG8 Wdbnd	£21.95 (A)	Page 24				Page 31	
X043W Extragain XG14 GroupA	£35.50 (A)	BW54J Sfc Dble Co-Ax Outl	£4.38 (C)			RQ23A Book BP53	£3.20NV (A)
X044X Extragain XG14 GroupB	£36.35 (A)	BW55K Flush Co-Ax Outlet	75p (E)			RH21X Book BP27	65pNV (A)
X045Y Extragain XG14 GrpC/D	£34.85 (A)	BW56L Fish Dbl Co-Ax Outl	£2.65 (C)			RH53H Book BP160	FEB
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BW43W Mast Bracket Type 2	£2.55 (C)	Y020X Ferrite Rod 810	29p (E)			WA21X Understanding Dip Elec.	£4.95NV (A)
		Y021X Ferrite Rod 814	46p (F)			WG11M Book JW748	£5.65NV (A)
		Y022Y Ferrite Rod 101	45p (F)				
		Y023A Ferrite Rod 102	69p (F)				
		LB12N MW/LW Aerial	£2.35 (C)				

NYA Not yet available
 NA Not available
 DIS Discontinued
 TEMP Temporarily out of stock
 OOP Out of print
 FEB Out of stock, new stock expected in month shown
 † While stocks last
 NV Indicates that item is zero rated for VAT purposes

*The Aerial Rotator is not supplied with cable. Use 4-core Mains XR48C. Make no connection to terminal 2 of the controller. The wire from terminal 3 of the controller must be connected to terminals 2 and 3 at the rotator.

TRADE QUANTITIES

The letter in brackets after the price indicates the minimum quantity of that item you can buy and qualify for a trade price. If you buy less than the quantity shown then the price is that shown. If you want to buy the quantity shown or more of that item, then please contact us for a trade price. If no trade quantity is shown, then the price shown is the best price we can offer regardless of the quantity. Trade quantities shown for wires or cables of any type is in metres, not reels or parts of metres. Trade quantities for nuts, bolts, washers, Hiatts etc. refers to the number of packs, i.e. to qualify for a trade price on Tag 2BA for example (trade quantity 500), you will need to order 500 packs which is equal to 5000 tags.

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(A)	Trade quantity	5
(B)	Trade quantity	10
(C)	Trade quantity	25
(D)	Trade quantity	50
(E)	Trade quantity	100
(F)	Trade quantity	250
(G)	Trade quantity	500
(H)	Trade quantity	1000

TRADE QUANTITIES

The letter in brackets after the price indicates the minimum quantity of that item you can buy and qualify for a trade price. See table at start of price list. If you buy less than the quantity shown then the price is that shown. If you want to buy the quantity shown or more of that item, then please contact us for a trade price. If no trade quantity is shown, then the price shown is the best price we can offer regardless of the quantity.

Trade quantities shown for wires or cables of any type is in metres, not reels or parts of metres. Trade quantities for nuts, bolts, washers, Hiatts etc. refers to the number of packs, i.e. to qualify for a trade price on Tag 2BA for example (trade quantity 500), you will need to order 500 packs which is equal to 5000 tags.

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WG22Y	Book JW567	£19.35NV	Page 44	WA600	Book FT1075	£6.15NV	XW98G	Book FT1070	£7.85NV	WA81C	Making Most of ZX81	£7.85NV	YK42W	Instrument Case NM2	£11.95 (A)
WG87U	Book BP101	£6.5pNV	WA600	Book FT1075	£6.15NV	RO02C	Book Sybex C207	£14.25NV	WG83E	Book JW413	£5.95NV	YK43W	Instrument Case NM3	£12.90 (A)	
RO25C	Book NB278	£4.78NV	WA59P	Book FT1391	£7.60NV	WA91Y	Book NB223	£5.80NV	WA93E	Book NB223	£5.80NV	YK44X	Instrument Case NM4	£14.50 (A)	
RO97H	Book NB076	£6.55NV	TR04E	Book FT1185	£9.99NV	WA93E	Book NB223	£5.80NV	YK45G	Get Acquainted ZX81	£5.40NV	YK45A	Instrument Case NM5	£14.90 (A)	
RL17T	Book NB115	£2.75NV	RR00A	Book NB195	£4.55NV	Page 54			WA85G	34 ZX81 Games	£4.55NV	YK46B	Instrument Case NM6	£10.90 (A)	
RO26D	Book NB319	£5.98NV	WX34M	Book NB471	FEB	WA92A	Book NB129	£5.80NV	WA79I	Explosion Games ZX81	£5.70NV	YK47B	Instrument Case NM7	£13.50 (A)	
Page 35			WX54J	Book NB439	£4.85NV	WA402C	Advanced 6502 I/Face	£11.45NV	WA80B	20 ZX81 Projects	£5.70NV	YK48P	Console 103	£10.95 (A)	
RR28F	Book NB2028	£14.25NV	WX59P	Book BP91	£2.15NV	WA57M	Book HD177	£6.89NV	WA42V	30-Hour BASIC	£6.62NV	YK49Q	Console 108	£16.45 (A)	
WA29G	Book BP51	£1.05NV	WX92A	Book WDXG	£5.55NV	WG10C	Book FT1330	£6.89NV	WA38R	Book BP109	£1.95NV	YK50Q	Blue Case 227	£4.45 (C)	
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RB25C	Book BP225	£1.45NV	Page 45			XW80B	Book D302	£11.95NV	WG99H	Book MM973	£7.45NV	YK41U	Blue Case 235	£5.40 (B)	
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WA09K	Opto Theory/Practice	£7.50NV	WG95D	Book FT1305	£7.45NV	W006G	Book Sybex L2	£9.24NV	WB86T	Sanitar Machine Cde	£9.85NV	YK48P	Blue Case 237	£7.90 (B)	
WA08J	TI Opto Data	£5.25NV	WG93B	Book FT1235	£9.45NV	W010A	Prog Your Spectrum	£6.55NV	W020C	Spectrum Programmer	£6.65NV	YK49Q	Blue Case 233	£7.70 (B)	
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Page 36			WG58B	Book FT1185	£5.95NV	W030D	Spectrum Games Book	£6.55NV	WA78K	20 Prog For Spectrum	£7.85NV	YK51L	Wood-End Case 1426	£13.95 (A)	
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WG93G	Guide To Solar Elect	£2.95NV	WA97F	Book NB156	£6.85NV	Page 56			WA03D	Peak, Poke Byte & RAM	£6.25NV	Page 72			
RR03D	Book NB201	£3.96NV	RO33L	Book BP52	£2.25NV	XW72P	Book C280	£13.55NV	LH56L	Potting Box Min	13p (G)	FW19V	Feet Cab	8p (H)	
RR27E	Book NB2026	£4.15NV	WA61R	Book FT1409	£7.55NV	RO17T	Book Sybex M15	£7.83NV	LH57M	Potting Box Small	19p (G)	FW39N	Stick-on Feet	18p (G)	
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Page 37			RG66W	Book BP96	£2.10NV	WG21X	Book HD167	£6.95NV	YK49F	Castor Feet	£24.50 (A)	YR61K	Castor Feet	£24.50 (A)	
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WA53H	Book BP20	£2.25NV	RG66W	Book BP96	£2.10NV	XW71N	Book M4	£13.25NV	YK49H	Castor Feet	£24.50 (A)	YR63K	Castor Feet	£24.50 (A)	
RR17T	Book BP23	£1.95NV	RG66W	Book BP96	£2.10NV	Page 57			YK49I	Castor Feet	£24.50 (A)	YR64K	Castor Feet	£24.50 (A)	
RO28F	Book BP48	£1.92NV	RG66W	Book BP96	£2.10NV	XW05E	Book MM286	£4.85NV	YK49J	Castor Feet	£24.50 (A)	YR65K	Castor Feet	£24.50 (A)	
WA34M	Book BP92	£1.75NV	RG66W	Book BP96	£2.10NV	RL45T	Book HD106	£10.91NV	YK49K	Castor Feet	£24.50 (A)	YR66K	Castor Feet	£24.50 (A)	
RO29G	Book BP49	£1.65NV	RG66W	Book BP96	£2.10NV	WG13P	Book JW204	£6.75NV	YK49L	Castor Feet	£24.50 (A)	YR67K	Castor Feet	£24.50 (A)	
WG67X	Book BP98	£2.25NV	RG66W	Book BP96	£2.10NV	WA69A	Microsoft Basic Book	£8.95NV	YK49M	Castor Feet	£24.50 (A)	YR68K	Castor Feet	£24.50 (A)	
WA35D	Book BP99	£1.95NV	RG66W	Book BP96	£2.10NV	XW04E	Book FT1055	£4.63NV	YK49N	Castor Feet	£24.50 (A)	YR69K	Castor Feet	£24.50 (A)	
WA36P	Book BP103	£1.95NV	RG66W	Book BP96	£2.10NV	WG99G	Book HD534	£6.95NV	YK49O	Castor Feet	£24.50 (A)	YR70K	Castor Feet	£24.50 (A)	
WG57M	Book FT1300	£12.99NV	RG66W	Book BP96	£2.10NV	WG39N	Book JW412	£7.00NV	YK49P	Castor Feet	£24.50 (A)	YR71K	Castor Feet	£24.50 (A)	
WG28F	Book BP83	£2.10NV	RG66W	Book BP96	£2.10NV	WG47A	Book JW415	£6.95NV	YK49Q	Castor Feet	£24.50 (A)	YR72K	Castor Feet	£24.50 (A)	
Page 38			RG66W	Book BP96	£2.10NV	WA16E	TI Sftware Dptment	£14.92NV	YK49R	Castor Feet	£24.50 (A)	YR73K	Castor Feet	£24.50 (A)	
RB21X	Book BP221	£1.45NV	RG66W	Book BP96	£2.10NV	RO41U	Book NB528	£6.60NV	YK49S	Castor Feet	£24.50 (A)	YR74K	Castor Feet	£24.50 (A)	
RR12G	Book BP22	£1.50NV	RG66W	Book BP96	£2.10NV	WG67X	Book JW279	£11.75NV	YK49T	Castor Feet	£24.50 (A)	YR75K	Castor Feet	£24.50 (A)	
RR19V	Book NB864	£2.80NV	RG66W	Book BP96	£2.10NV	Page 58			YK49U	Castor Feet	£24.50 (A)	YR76K	Castor Feet	£24.50 (A)	
RF08J	Book BP39	£1.90NV	RG66W	Book BP96	£2.10NV	WG37S	Book HD138	£8.85NV	YK49V	Castor Feet	£24.50 (A)	YR77K	Castor Feet	£24.50 (A)	
RR30H	Book BP37	£1.92NV	RG66W	Book BP96	£2.10NV	WA70M	Little BASIC Style	£6.95NV	YK49W	Castor Feet	£24.50 (A)	YR78K	Castor Feet	£24.50 (A)	
RO50F	Book NB074	£5.99NV	RG66W	Book BP96	£2.10NV	WA72P	Book JW932	£7.85NV	YK49X	Castor Feet	£24.50 (A)	YR79K	Castor Feet	£24.50 (A)	
XW67X	Book BP98	£2.25NV	RG66W	Book BP96	£2.10NV	WA64U	Pascal for Humans	£4.50NV	YK49Y	Castor Feet	£24.50 (A)	YR80K	Castor Feet	£24.50 (A)	
WA35D	Book BP99	£1.95NV	RG66W	Book BP96	£2.10NV	WG03D	Book P310	£10.75NV	YK49Z	Castor Feet	£24.50 (A)	YR81K	Castor Feet	£24.50 (A)	
WA36P	Book BP103	£1.95NV	RG66W	Book BP96	£2.10NV	WG21J	Book B250	£10.92NV	YK49A	Castor Feet	£24.50 (A)	YR82K	Castor Feet	£24.50 (A)	
WG57M	Book FT1300	£12.99NV	RG66W	Book BP96	£2.10NV	WG52K	Book P320	£12.15NV	YK49B	Castor Feet	£24.50 (A)	YR83K	Castor Feet	£24.50 (A)	
WG28F	Book BP83	£2.10NV	RG66W	Book BP96	£2.10NV	XW24B	Book HD124	£7.65NV	YK49C	Castor Feet	£24.50 (A)	YR84K	Castor Feet	£24.50 (A)	
Page 39			RG66W	Book BP96	£2.10NV	RO43X	Book HD682	£8.38NV	YK49D	Castor Feet	£24.50 (A)	YR85K	Castor Feet	£24.50 (A)	
WG50E	Book NB500	£3.95NV	RG66W	Book BP96	£2.10NV	WA68Y	Discover FORTH	£11.80NV	YK49E	Castor Feet	£24.50 (A)	YR86K	Castor Feet	£24.50 (A)	
WG18U	Book HD748	£1.75NV	RG66W	Book BP96	£2.10NV	WG25C	Book JW609	£13.45NV	YK49F	Castor Feet	£24.50 (A)	YR87K	Castor Feet	£24.50 (A)	
WG35D	Book NB893	£5.46NV	RG66W	Book BP96	£2.10NV	Page 59			YK49G	Castor Feet	£24.50 (A)	YR88K	Castor Feet	£24.50 (A)	
WG94C	Book FT1349	£9.45NV	RG66W	Book BP96	£2.10NV	XW93R	Book C300	£12.45NV	YK49H	Castor Feet	£24.50 (A)	YR89K	Castor Feet	£24.50 (A)	
WA49D	Book BP104	£2.45NV	RG66W	Book BP96	£2.10NV	WG15R	Book JW55R	£10.34NV	YK49I	Castor Feet	£24.50 (A)	YR90K	Castor Feet	£24.50 (A)	
WG91Y	Book FT1261	£5.45NV	RG66W	Book BP96	£2.10NV	WG90P	Book HD154	£10.34NV	YK49J	Castor Feet	£24.50 (A)	YR91K	Castor Feet	£24.50 (A)	
RL30H	Book NB153	£5.95NV	RG66W	Book BP96	£2.10NV	WG19V	Book HD180	£5.85NV	YK49K	Castor Feet	£24.50 (A)	YR92K	Castor Feet	£24.50 (A)	
WA50E	Book BP106	£2.15NV	RG66W	Book BP96	£2.10NV	WG38R	Book JW410	£4.75NV	YK49L	Castor Feet	£24.50 (A)	YR93K	Castor Feet	£24.50 (A)	
LY04E	Book BP44	£2.10NV	RG66W	Book BP96	£2.10NV	WG48C	Book HD162	£10.20NV	YK49M	Castor Feet	£24.50 (A)	YR94K	Castor Feet	£24.50 (A)	
XW38R	Book NB480	£4.75NV	RG66W	Book BP96	£2.10NV	WA71N	BASIC for Scientists	£12.95NV	YK49N	Castor Feet	£24.50 (A)	YR95K	Castor Feet	£24.50 (A)	
RO27E	Book BP90	£2.10NV	RG66W	Book BP96	£2.10NV	WG60Q	Book HD762	£10.37NV	YK49O	Castor Feet	£24.50 (A)	YR96K	Castor Feet	£24.50 (A)	
Page 40			RG66W	Book BP96	£2.10NV	Page 60			YK49P	Castor Feet	£24.50 (A)	YR97K	Castor Feet	£24.50 (A)	
RB23A	Book BP223	£1.45NV	RG66W	Book BP96	£2.10NV	XW94C	Book FT1095	£4.52NV	YK49Q	Castor Feet	£24.50 (A)	YR98K	Castor Feet	£24.50 (A)	
WG130H	Book BP65	£1.75NV	RG66W	Book BP96	£2.10NV	RL48C	Book HD112	£9.68NV	YK49						

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XR43W Extra Flex Green	20p (G)	BH05F Systoflex 1mm Yellow	6p (H)	BX25C Polystyrene 33	8p (H)	FF46A SW Trim 60pF	£6.15 (B)	FF48B SW Trim 100pF	£6.10 (B)
XR44X Extra Flex Red	20p (G)	BH06G Systoflex 2mm Black	9p (H)	BX26D Polystyrene 47	8p (H)	FF49D SW Trim 150pF	£5.50 (B)	FF50E Dilecon 300pF	£4.45 (C)
XR45Y Extra Flex Yellow	20p (G)	BH07H Systoflex 2mm Blue	9p (H)	BX27E Polystyrene 68	8p (H)	FF51F Dilecon 500pF	£4.35 (C)	FF57J FS Crystal 100kHz	£4.55 (C)
XR58Y Min Extra Flex Black	15p (G)	BH08K Systoflex 2mm Red	9p (H)	BX28F Polystyrene 150	8p (H)	FF62S FS Crystal 1MHz	£5.95 (B)	FF78K FS Crystal 10MHz	£2.95 (C)
XR69A Min Extra Flex Red	15p (G)	BH10L Systoflex 2mm White	11p (H)	BX30H Polystyrene 220	8p (H)	FF77J FS Crystal 1MHz	£4.45 (C)	FF82S FS Crystal 10MHz	£2.95 (C)
XR22Y EHT Wire	32p (G)	BH11M Systoflex 2mm Yellow	9p (H)	BX31J Polystyrene 330	8p (H)	FF80F MP Crystal 1MHz	£4.45 (C)	FF81C MP Crystal 2.4576MHz	£1.80 (D)
BL11M Strappg Wire 16swg	82p (G)	BH12N Systoflex 4mm Black	15p (H)	BX32K Polystyrene 470	8p (H)	FF82M MP Crystal 4MHz	£1.80 (D)	FF83E MP Crystal 6.144MHz	£1.25 (D)
BL12N Strappg Wire 18swg	87p (G)	BH14Q Systoflex 4mm Green	15p (H)	BX33L Polystyrene 560	8p (H)	FF84F MCR Cryst Brown Pairs	£2.95 (C)	FF85G MCR Cryst Green Pr	£2.95 (C)
BL13R Strappg Wire 20swg	92p (G)	BH15S Systoflex 4mm Red	15p (H)	BX34M Polystyrene 680	8p (H)	FF86G MCR Cryst Orange Pr	£2.95 (C)	FF87G MCR Cryst Blue Pr	£2.95 (C)
BL14Q Strappg Wire 22swg	94p (G)	BH16S Systoflex 4mm White	15p (H)	BX35Q Polystyrene 1000	8p (H)	FF88G MCR Cryst Yellow Pr	£2.95 (C)	FF89G Colour TV Crystal	£1.20 (C)
BL15R Strappg Wire 24swg	96p (G)	BH17T Systoflex 4mm Yellow	15p (H)	BX36P Polystyrene 1500	8p (H)	FF90G PC Elect 0.47uF 100V	11p (G)	FF91G PC Elect 1uF 100V	11p (G)
BL16S EC Wire 14 swg	70p (G)	BH21X Systoflex 6mm Black	17p (H)	BX37S Polystyrene 2200	8p (H)	FF92G PC Elect 2.2uF 63V	10p (G)	FF93G PC Elect 4.7uF 63V	10p (G)
BL24B EC Wire 18 swg	79p (G)	BH43W Systoflex 10mm Black	17p (H)	BX38R Polystyrene 3300	8p (H)	FF94G PC Elect 10uF 63V	12p (G)	FF95G PC Elect 22uF 16V	12p (G)
BL25C EC Wire 20 swg	86p (G)	BH43W Systoflex 10mm Black	17p (H)	BX39N Polystyrene 4700	8p (H)	FF96G PC Elect 47uF 63V	14p (G)	FF97G PC Elect 100uF 10V	12p (G)
BL26D EC Wire 22 swg	89p (G)	BH43W Systoflex 10mm Black	17p (H)	BX40T Polystyrene 5600	8p (H)	FF98G PC Elect 100uF 63V	22p (G)	FF99G PC Elect 220uF 16V	22p (G)
BL27E EC Wire 24 swg	93p (G)	BH43W Systoflex 10mm Black	17p (H)	BX41U Polystyrene 6800	10p (G)	FF100G PC Elect 470uF 25V	25p (G)	FF101G PC Elect 100uF 25V	27p (F)
BL28F EC Wire 24 swg	£1.05 (D)	BH43W Systoflex 10mm Black	17p (H)	BX42V Polystyrene 10000	14p (G)	FF102G PC Elect 220uF 63V	25p (G)	FF103G PC Elect 470uF 63V	25p (G)
BL29G EC Wire 26 swg	£1.07 (D)	BH43W Systoflex 10mm Black	17p (H)	BX43X Polystyrene 15000	19p (G)	FF104G PC Elect 100uF 10V	27p (F)	FF105G PC Elect 220uF 16V	27p (F)
BL30H EC Wire 28 swg	£1.07 (D)	BH43W Systoflex 10mm Black	17p (H)	BX44Y Polystyrene 22000	19p (G)	FF106G PC Elect 470uF 25V	27p (F)	FF107G PC Elect 100uF 25V	27p (F)
BL340T EC Wire 30 swg	£1.07 (D)	BH43W Systoflex 10mm Black	17p (H)	BX45Z Polystyrene 33000	25p (F)	FF108G PC Elect 220uF 63V	27p (F)	FF109G PC Elect 470uF 63V	27p (F)
BL41U EC Wire 32 swg	£1.12 (D)	BH43W Systoflex 10mm Black	17p (H)	BX46A Polystyrene 100	27p (F)	FF110G PC Elect 100uF 10V	27p (F)	FF111G PC Elect 220uF 16V	27p (F)
BL42V EC Wire 34 swg	£1.16 (D)	BH43W Systoflex 10mm Black	17p (H)	BX47B Polystyrene 150	27p (F)	FF112G PC Elect 470uF 25V	27p (F)	FF113G PC Elect 100uF 25V	27p (F)
BL43X EC Wire 36 swg	£1.25 (D)	BH43W Systoflex 10mm Black	17p (H)	BX48C Polystyrene 220	27p (F)	FF114G PC Elect 220uF 63V	27p (F)	FF115G PC Elect 470uF 63V	27p (F)
BL44X EC Wire 38 swg	£1.25 (D)	BH43W Systoflex 10mm Black	17p (H)	BX49D Polystyrene 330	27p (F)	FF116G PC Elect 100uF 10V	27p (F)	FF117G PC Elect 220uF 16V	27p (F)
BL45Q EC Wire 40 swg	£1.50 (D)	BH43W Systoflex 10mm Black	17p (H)	BX50E Polystyrene 470	27p (F)	FF118G PC Elect 470uF 25V	27p (F)	FF119G PC Elect 100uF 25V	27p (F)
BL61R EC Wire 42 swg	£1.49 (D)	BH43W Systoflex 10mm Black	17p (H)	BX51F Polystyrene 680	27p (F)	FF120G PC Elect 220uF 63V	27p (F)	FF121G PC Elect 470uF 63V	27p (F)
BL62S EC Wire 44 swg	£2.20 (C)	BH43W Systoflex 10mm Black	17p (H)	BX52G Polystyrene 150	29p (F)	FF122G PC Elect 100uF 10V	27p (F)	FF123G PC Elect 220uF 16V	27p (F)
BL63T EC Wire 48 swg	£4.95 (C)	BH43W Systoflex 10mm Black	17p (H)	BX53H Polystyrene 330	29p (F)	FF124G PC Elect 470uF 25V	27p (F)	FF125G PC Elect 100uF 25V	27p (F)
XR39N Z-Wire	14p (G)	BH43W Systoflex 10mm Black	17p (H)	BX54J Polystyrene 470	29p (F)	FF126G PC Elect 220uF 63V	27p (F)	FF127G PC Elect 470uF 63V	27p (F)
XR60Q Hi-Z Loudspeaker Cable	36p (G)	BH43W Systoflex 10mm Black	17p (H)	BX55K Polystyrene 680	29p (F)	FF128G PC Elect 100uF 10V	27p (F)	FF129G PC Elect 220uF 16V	27p (F)
YG08J Lit. Speaker Leads	£8.99 (B)	BH43W Systoflex 10mm Black	17p (H)	BX56L Polystyrene 1000	29p (F)	FF130G PC Elect 470uF 25V	27p (F)	FF131G PC Elect 100uF 25V	27p (F)
XR06G Ribbon Cable 10-Way	60p	BH43W Systoflex 10mm Black	17p (H)	BX57M Polystyrene 1500	29p (F)	FF132G PC Elect 220uF 63V	27p (F)	FF133G PC Elect 470uF 63V	27p (F)
XR07H Ribbon Cable 20-Way	£1.20	BH43W Systoflex 10mm Black	17p (H)	BX58N Polystyrene 3300	29p (F)	FF134G PC Elect 100uF 10V	27p (F)	FF135G PC Elect 220uF 16V	27p (F)
XR67X Ribbon Cable 30-Way	£1.80 (D)	BH43W Systoflex 10mm Black	17p (H)	BX59P Polystyrene 4700	29p (F)	FF136G PC Elect 470uF 25V	27p (F)	FF137G PC Elect 100uF 25V	27p (F)
XR65V IDC Cable 12-Way	£2.11	BH43W Systoflex 10mm Black	17p (H)	BX60Q Polystyrene 6800	29p (F)	FF138G PC Elect 220uF 63V	27p (F)	FF139G PC Elect 470uF 63V	27p (F)
XR630H Flexible Cable 7-Way	£4.20	BH43W Systoflex 10mm Black	17p (H)	BX61R Polystyrene 10000	29p (F)	FF140G PC Elect 100uF 10V	27p (F)	FF141G PC Elect 220uF 16V	27p (F)
XR47B Twin Mains DS Black	28p (G)	BH43W Systoflex 10mm Black	17p (H)	BX62S Polystyrene 15000	29p (F)	FF142G PC Elect 470uF 25V	27p (F)	FF143G PC Elect 100uF 25V	27p (F)
XR00A Twin Mains DS White	28p (G)	BH43W Systoflex 10mm Black	17p (H)	BX63T Polystyrene 22000	29p (F)	FF144G PC Elect 220uF 63V	27p (F)	FF145G PC Elect 470uF 63V	27p (F)
XR61R Twin 6A Mains Orange	49p (E)	BH43W Systoflex 10mm Black	17p (H)	BX64U Polystyrene 33000	29p (F)	FF146G PC Elect 100uF 10V	27p (F)	FF147G PC Elect 220uF 16V	27p (F)
XR62S Twin 6A Mains Black	35p (E)	BH43W Systoflex 10mm Black	17p (H)	BX65W Polystyrene 47000	29p (F)	FF148G PC Elect 470uF 25V	27p (F)	FF149G PC Elect 100uF 25V	27p (F)
XR02C Min Mains White	36p (E)	BH43W Systoflex 10mm Black	17p (H)	BX66W Polystyrene 68000	29p (F)	FF150G PC Elect 220uF 63V	27p (F)	FF151G PC Elect 470uF 63V	27p (F)
XR03D C6A Mains Black	56p (E)	BH43W Systoflex 10mm Black	17p (H)	BX67M Polystyrene 100000	29p (F)	FF152G PC Elect 100uF 10V	27p (F)	FF153G PC Elect 220uF 16V	27p (F)
XR04E C6A Mains White	56p (E)	BH43W Systoflex 10mm Black	17p (H)	BX68G Polystyrene 150000	29p (F)	FF154G PC Elect 470uF 25V	27p (F)	FF155G PC Elect 100uF 25V	27p (F)
XR05F C6A Mains Orange	70p (E)	BH43W Systoflex 10mm Black	17p (H)	BX69H Polystyrene 220000	29p (F)	FF156G PC Elect 220uF 63V	27p (F)	FF157G PC Elect 470uF 63V	27p (F)
XR09K HD Mains Black	80p (E)	BH43W Systoflex 10mm Black	17p (H)	BX70A Polystyrene 330000	29p (F)	FF158G PC Elect 100uF 10V	27p (F)	FF159G PC Elect 220uF 16V	27p (F)
XR10L HD Mains White	80p (E)	BH43W Systoflex 10mm Black	17p (H)	BX71B Polystyrene 470000	29p (F)	FF160G PC Elect 470uF 25V	27p (F)	FF161G PC Elect 100uF 25V	27p (F)
XR11M HD Mains Orange	90p (E)	BH43W Systoflex 10mm Black	17p (H)	BX72C Polystyrene 680000	29p (F)	FF162G PC Elect 220uF 63V	27p (F)	FF163G PC Elect 470uF 63V	27p (F)
XR24B Cotton Mains	94p (E)	BH43W Systoflex 10mm Black	17p (H)	BX73D Polystyrene 1000000	29p (F)	FF164G PC Elect 100uF 10V	27p (F)	FF165G PC Elect 220uF 16V	27p (F)
BL71N Stretchflex JA	£1.05 (D)	BH43W Systoflex 10mm Black	17p (H)	BX74E Polystyrene 1500000	29p (F)	FF166G PC Elect 470uF 25V	27p (F)	FF167G PC Elect 100uF 25V	27p (F)
BL72P Stretchflex 6A	£4.95 (C)	BH43W Systoflex 10mm Black	17p (H)	BX75F Polystyrene 2200000	29p (F)	FF168G PC Elect 220uF 63V	27p (F)	FF169G PC Elect 470uF 63V	27p (F)
XR48C 4-Core Mains	£1.05 (E)	BH43W Systoflex 10mm Black	17p (H)	BX76G Polystyrene 3300000	29p (F)	FF170G PC Elect 100uF 10V	27p (F)	FF171G PC Elect 220uF 16V	27p (F)
XR49D 1.0mm TE Cable	43p (E)	BH43W Systoflex 10mm Black	17p (H)	BX77H Polystyrene 4700000	29p (F)	FF172G PC Elect 470uF 25V	27p (F)	FF173G PC Elect 100uF 25V	27p (F)
XR50E 1.5mm TE Cable	48p (E)	BH43W Systoflex 10mm Black	17p (H)	BX78J Polystyrene 6800000	29p (F)	FF174G PC Elect 220uF 63V	27p (F)	FF175G PC Elect 470uF 63V	27p (F)
XR51F 2.5mm TE Cable	65p (E)	BH43W Systoflex 10mm Black	17p (H)	BX79L Polystyrene 10000000	29p (F)	FF176G PC Elect 100uF 10V	27p (F)	FF177G PC Elect 220uF 16V	27p (F)
XR52G 6mm TE Cable	£1.75 (E)	BH43W Systoflex 10mm Black	17p (H)	BX80A Polystyrene 15000000	29p (F)	FF178G PC Elect 470uF 25V	27p (F)	FF179G PC Elect 100uF 25V	27p (F)
XR53H 1mm Trpl & ECC Cbl	74p (E)	BH43W Systoflex 10mm Black	17p (H)	BX81B Polystyrene 22000000	29p (F)	FF180G PC Elect 220uF 63V	27p (F)	FF181G PC Elect 470uF 63V	27p (F)
XR54R Min Screened	75p (E)	BH43W Systoflex 10mm Black	17p (H)	BX82C Polystyrene 33000000	29p (F)	FF182G PC Elect 100uF 10V	27p (F)	FF183G PC Elect 220uF 16V	27p (F)
XR12N Cable Single Black	19p (G)	BH43W Systoflex 10mm Black	17p (H)	BX83D Polystyrene 47000000	29p (F)	FF184G PC Elect 470uF 25V	27p (F)	FF185G PC Elect 100uF 25V	27p (F)
XR13P Cable Single Grey	19p (G)	BH43W Systoflex 10mm Black	17p (H)	BX84E Polystyrene 68000000	29p (F)	FF186G PC Elect 220uF 63V	27p (F)	FF187G PC Elect 470uF 63V	27p (F)
XR14Q Cable Single White	19p (G)	BH43W Systoflex 10mm Black	17p (H)	BX85F Polystyrene 100000000	29p (F)	FF188G PC Elect 100uF 10V	27p (F)	FF189G PC Elect 220uF 16V	27p (F)
XR16S Single Mic Cable	42p (G)	BH43W Systoflex 10mm Black	17p (H)	BX86G Polystyrene 150000000	29p (F)	FF190G PC Elect 470uF 25V	27p (F)	FF191G PC Elect 100uF 25V	27p (F)
XR18U Low Noise Scnd	42p (G)	BH43W Systoflex 10mm Black	17p (H)	BX87H Polystyrene 220000000	29p (F)	FF192G PC Elect 220uF 63V	27p (F)	FF193G PC Elect 470uF 63V	27p (F)
XR19V Low Co-Ax Cable	42p (G)	BH43W Systoflex 10mm Black	17p (H)	BX88J Polystyrene 330000000	29p (F)	FF194G PC Elect 100uF 10V	27p (F)	FF195G PC Elect 220uF 16V	27p (F)
XR36T URG R Cable	55p (E)	BH43W Systoflex 10mm Black	17p (H)	BX89L Polystyrene 470000000	29p (F)	FF196G PC Elect 470uF 25V	27p (F)	FF197G PC Elect 100uF 25V	27p (F)
XR08J Twin Mic Cable	82p (E)	BH43W Systoflex 10mm Black	17p (H)	BX90A Polystyrene 680000000	29p (F)	FF198G PC Elect 220uF 63V	27p (F)	FF199G PC Elect 470uF 63V	27p (F)
XR20W Lapped Pair	21p (G)	BH43W Systoflex 10mm Black	17p (H)	BX91B Polystyrene 1000000000	29p (F)	FF200G PC Elect 100uF 10V	27p (F)	FF201G PC Elect 220uF 16V	27p (F)
XR21X Cable Twin	29p (G)	BH43W Systoflex 10mm Black	17p (H)	BX92C Polystyrene 1500000000	29p (F)	FF202G PC Elect 470uF 25V	27p (F)	FF203G PC Elect 100uF 25V	27p (F)
XR23A Cable Quad	38p (G)	BH43W Systoflex 10mm Black	17p (H)	BX93D Polystyrene 2200000000	29p (F)	FF204G PC Elect 220uF 63V	27p (F)	FF205G PC Elect 470uF 63V	27p (F)
XR25C Multi-Core 4-Way	60p (E)	BH43W Systoflex 10mm Black	17p (H)	BX94E Polystyrene 3300000000	29p (F)	FF206G PC Elect 100uF 10V	27p (F)	FF207G PC Elect 220uF 16V	27p (F)
XR26D Multi-Core 6-Way	65p (E)	BH43W Systoflex 10mm Black	17p (H)	BX95F Polystyrene 4700000000	29p (F)	FF208G PC Elect 470uF 25V	27p (F)	FF209G PC Elect 100uF 25V	27p (F)
XR27E Multi-Core 9-Way	86p (E)	BH43W Systoflex 10mm Black	17p (H)	BX96G Polystyrene 6800000000	29p (F)	FF210G PC Elect 220uF 63V	27p (F)	FF211G PC Elect 470uF 63V	27p (F)
XR28F Multi-Core 15-Way	86p (E)	BH43W Systoflex 10mm Black	17p (H)	BX97H Polystyrene 10000000000	29p (F)	FF212G PC Elect 100uF 10V	27p (F)	FF213G PC Elect 220uF 16V	27p (F)
XR46A Multi-Core 25-Way	£1.74 (E)	BH43W Systoflex 10mm Black	17p (H)	BX98J Polystyrene 15000000000	29p (F)	FF214G PC Elect 470uF 25V	27p (F)	FF215G PC Elect 100uF 25V	27p (F)
XR54J Multi-Core 36-Way	£2.31 (E)	BH43W Systoflex 10mm Black	17p (H)	BX99L Polystyrene 22000000000	29p (F)	FF216G PC Elect 220uF 63V	27p (F)	FF217G PC Elect 470uF 63V	27p (F)
XR65W 4-Wire Phone Cable	21p (G)	BH43W Systoflex 10mm Black	17p (H)	BX00A Polystyrene 33000000000	29p (F)	FF218G PC Elect 100uF 10V	27p (F)	FF219G PC Elect 220uF 16V	27p (F)
XR55K 7-Core Trailer Cable	£1.19 (E)	BH43W Systoflex 10mm Black	17p (H)	BX01B Polystyrene 47000000000	29p (F)	FF220G PC Elect 470uF 25V	2		

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RX61R Holder MES Red	£1.45 (D)	WL59Q Opto-Isolator	69p (E)	BY25C Mar Key Tab Diap 16'	DIS	F180B Pin 0266 Pk of 10	25p (F)
RX76H Dmd LES Lhd Red	35p (F)	WY62S Dual Opto-Isolator	£1.58 (D)	BY26D Mar K Tab Dbar Acc	£3.45	F181C Pin 1657 Pk of 10	25p (F)
RX77D Dmd LES Lhd Green	35p (F)	Y633T Quad Opto-Isolator	£2.96 (C)	BY27E Mar K Tab Dbar Solo	£3.45	R194C Verowire Kit	£6.95 (B)
RX78D Dmd LES Lhd Red	35p (F)	WQ70M Darlington Isolator	74p (E)	BY28F Mar Key Tab Dule 8'	£3.45	HY16S Verowire Pen	£4.95 (E)
RX79L Dmd LES Lhd White	35p (F)	Y644U SCR Isolator	£2.12 (C)	BY29G Mar Key Tab Flute 1'	£3.45	HY17T Verowire Spool	99p (E)
RX80D Dmd LES Lhd Yellow	35p (F)	Q010L Triac Isolator	£1.55 (D)	BY30H Mar Key Tab Flute 2'	£3.45	FY33L Verowire Comb	8p (H)
RX86X Fit-Tp LES Lhd Blu	35p (F)	Y666W Infra-Source	38p (F)	BY31J Mar Ky Tb File 2/2/3	DIS	FL28D Track Pin	85p (E)
RX86Y Fit-Tp LES Lhd Grn	35p (F)	YH71N Photocoupler TIL100	31p (F)	BY32K Mar Key Tab Flute 4'	DIS	FL28F 4-Way Tag	12p (G)
RX69A Fit-Tp LES Lhd Red	35p (F)	Q101L Triac Isolator	£1.55 (D)	BY33L Mar Ky Tb File 5/1/3'	DIS	FL29G Mounting Strip	32p (F)
FF66W Fluted Lhd Amber	30p (F)	Y666W Infra-Red Sensor	31p (F)	BY34M Mar Key Tab Flute 8'	£3.45	FL11M Tag Board	94p (E)
FF67X Fluted Lhd Clear	30p (F)			BY35Q Mar Ky Tab Flute 16'	£3.45	YL11M Vero Plugboard	£4.38 (C)
FF68Z Fluted Lhd Green	30p (F)			BY36P Mar Ky Tb Frch Hrn 8'	£3.45	H084F Verobloc Bracket	63p (E)
FF69A Fluted Lhd Red	30p (F)			BY37S Mar Key Tab Gndk 8'	£3.45	BY38T Engineer's Design Kit	48p (F)
Y000A LES Cover Amber	6p (H)			BY38R Mar Key Tab Gedkt 16'	£3.45	BK63T Verobloc Kit	£4.82 (C)
Y001B LES Cover Blue	6p (H)			BY40T Mar Key Tab Horn 8'	£3.45		
Y002C LES Cover Green	6p (H)			BY41U Mar Key Tab Mx 16'	DIS		
Y003D LES Cover Purple	6p (H)			BY42V Mar Key Tab Obee 8'	£3.45		
Y004E LES Cover Red	6p (H)			BY43M Mar Key Tab Obee 16'	£3.45		
Y005F LES Cover White	6p (H)			BY44X Mar Key Tab Pdl Sus	£3.45		
Y006G LES Cover Yellow	6p (H)			BY45Y Mar Key Tab Piano	£3.45		
BK52G Min Neon Red	30p (F)			BY46A Mar Ky Tb Prsts Cntd	£3.45		
BK53H Min Neon Green	30p (F)			BY47E Mar Ky Tb Prsts To Rr	£3.45		
BK54J Min Neon Amber	29p (F)			BY48D Mar Key Tab Reverb	£3.45		
BK55K Min Neon Red	29p (F)						
BK56L Min Neon Green	29p (F)						
BK57M Min Neon Amber	29p (F)						
BK58N Min Neon Red	29p (F)						
BK59P Min Neon Green	29p (F)						
BK60Q Min Neon Amber	29p (F)						
BK61R Min Neon Red	29p (F)						
BK62S Min Neon Green	29p (F)						
BK63T Min Neon Amber	29p (F)						
BK64U Min Neon Red	29p (F)						
BK65V Min Neon Green	29p (F)						
BK66W Min Neon Amber	29p (F)						
BK67X Min Neon Red	29p (F)						
BK68Y Min Neon Green	29p (F)						
BK69Z Min Neon Amber	29p (F)						
BK70A Min Neon Red	29p (F)						
BK71B Min Neon Green	29p (F)						
BK72C Min Neon Amber	29p (F)						
BK73D Min Neon Red	29p (F)						
BK74E Min Neon Green	29p (F)						
BK75F Min Neon Amber	29p (F)						
BK76G Min Neon Red	29p (F)						
BK77H Min Neon Green	29p (F)						
BK78I Min Neon Amber	29p (F)						
BK79J Min Neon Red	29p (F)						
BK80K Min Neon Green	29p (F)						
BK81L Min Neon Amber	29p (F)						
BK82M Min Neon Red	29p (F)						
BK83N Min Neon Green	29p (F)						
BK84O Min Neon Amber	29p (F)						
BK85P Min Neon Red	29p (F)						
BK86Q Min Neon Green	29p (F)						
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BK90U Min Neon Amber	29p (F)						
BK91V Min Neon Red	29p (F)						
BK92W Min Neon Green	29p (F)						
BK93X Min Neon Amber	29p (F)						
BK94Y Min Neon Red	29p (F)						
BK95Z Min Neon Green	29p (F)						
BK96A Min Neon Amber	29p (F)						
BK97B Min Neon Red	29p (F)						
BK98C Min Neon Green	29p (F)						
BK99D Min Neon Amber	29p (F)						
BK00E Min Neon Red	29p (F)						
BK01F Min Neon Green	29p (F)						
BK02G Min Neon Amber	29p (F)						
BK03H Min Neon Red	29p (F)						
BK04I Min Neon Green	29p (F)						
BK05J Min Neon Amber	29p (F)						
BK06K Min Neon Red	29p (F)						
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BK09N Min Neon Red	29p (F)						
BK10O Min Neon Green	29p (F)						
BK11P Min Neon Amber	29p (F)						
BK12Q Min Neon Red	29p (F)						
BK13R Min Neon Green	29p (F)						
BK14S Min Neon Amber	29p (F)						
BK15T Min Neon Red	29p (F)						
BK16U Min Neon Green	29p (F)						
BK17V Min Neon Amber	29p (F)						
BK18W Min Neon Red	29p (F)						
BK19X Min Neon Green	29p (F)						
BK20Y Min Neon Amber	29p (F)						
BK21Z Min Neon Red	29p (F)						
BK22A Min Neon Green	29p (F)						
BK23B Min Neon Amber	29p (F)						
BK24C Min Neon Red	29p (F)						
BK25D Min Neon Green	29p (F)						
BK26E Min Neon Amber	29p (F)						
BK27F Min Neon Red	29p (F)						
BK28G Min Neon Green	29p (F)						
BK29H Min Neon Amber	29p (F)						
BK30I Min Neon Red	29p (F)						
BK31J Min Neon Green	29p (F)						
BK32K Min Neon Amber	29p (F)						
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BK34M Min Neon Green	29p (F)						
BK35N Min Neon Amber	29p (F)						
BK36O Min Neon Red	29p (F)						
BK37P Min Neon Green	29p (F)						
BK38Q Min Neon Amber	29p (F)						
BK39R Min Neon Red	29p (F)						
BK40S Min Neon Green	29p (F)						
BK41T Min Neon Amber	29p (F)						
BK42U Min Neon Red	29p (F)						
BK43V Min Neon Green	29p (F)						
BK44W Min Neon Amber	29p (F)						
BK45X Min Neon Red	29p (F)						
BK46Y Min Neon Green	29p (F)						
BK47Z Min Neon Amber	29p (F)						
BK48A Min Neon Red	29p (F)						
BK49B Min Neon Green	29p (F)						
BK50C Min Neon Amber	29p (F)						
BK51D Min Neon Red	29p (F)						
BK52E Min Neon Green	29p (F)						
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BK56I Min Neon Amber	29p (F)						
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BK61N Min Neon Green	29p (F)						
BK62O Min Neon Amber	29p (F)						
BK63P Min Neon Red	29p (F)						
BK64Q Min Neon Green	29p (F)						
BK65R Min Neon Amber	29p (F)						
BK66S Min Neon Red	29p (F)						
BK67T Min Neon Green	29p (F)						
BK68U Min Neon Amber	29p (F)						
BK69V Min Neon Red	29p (F)						
BK70W Min Neon Green	29p (F)						
BK71X Min Neon Amber	29p (F)						
BK72Y Min Neon Red	29p (F)						
BK73Z Min Neon Green	29p (F)						
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BK77D Min Neon Amber	29p (F)						
BK78E Min Neon Red	29p (F)						
BK79F Min Neon Green	29p (F)						
BK80G Min Neon Amber	29p (F)						
BK81H Min Neon Red	29p (F)						
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BK83J Min Neon Amber	29p (F)						
BK84K Min Neon Red	29p (F)						
BK85L Min Neon Green	29p (F)						
BK86M Min Neon Amber	29p (F)						
BK87N Min Neon Red	29p (F)						
BK88O Min Neon Green	29p (F)						
BK89P Min Neon Amber	29p (F)						
BK90Q Min Neon Red	29p (F)						
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BK92S Min Neon Amber	29p (F)						
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BK95V Min Neon Amber	29p (F)						
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BK99Z Min Neon Red	29p (F)						
BK00A Min Neon Green	29p (F)						
BK01B Min Neon Amber	29p (F)						
BK02C Min Neon Red	29p (F)						
BK03D Min Neon Green	29p (F)						
BK04E Min Neon Amber	29p (F)						
BK05F Min Neon Red	29p (F)						
BK06G Min Neon Green	29p (F)						
BK07H Min Neon Amber	29p (F)						
BK08I Min Neon Red	29p (F)						
BK09J Min Neon Green	29p (F)						
BK10K Min Neon Amber	29p (F)						
BK11L Min Neon Red	29p (F)						
BK12M Min Neon Green	29p (F)						
BK13N Min Neon Amber	29p (F)						
BK14O Min Neon Red	29p (F)						
BK15P Min Neon Green	29p (F)						
BK16Q Min Neon Amber	29p (F)						
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BK18S Min Neon Green	29p (F)						

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RK25C Stereo Amp Heatsink	£1.25 (D)
XG16S Stereo Amp Woodwork	£6.25 (B)
XG15R Stereo Amp Chassis	£5.95 (B)
GA71N Stereo Amp PCB	£4.60 (C)
GA78K Stereo Amp SW PCB	£5.5p (E)
LRW1N 25W Stereo Amp Kit	£49.95 (A)
RK36P Switch Panel	£1.20 (D)
GA97F Stereo Amp IR Decoder	£2.75 (C)
GA99H Sio Amp IR Controller	£1.40 (D)
LR77J Amp Remote Cntrl Kit	£26.95 (A)

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QY25C 2716/M4	£10.50 (A)
GB04E E.L.C. Board	£2.95 (C)
GB05F Connect PCB	£3.80 (C)
GB06E T/E Motherboard	£2.75 (A)
GB07H T/E PSU PCB	£4.50 (C)
LRW80B Dig-Tel ELC Kit	£24.95 (A)
LRW81C Dig-Tel Connect Kit	£9.95 (B)
LRW82D Dig-Tel Main Kit	£67.50 (A)

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XG06G Burglar Alarm Box	£12.50 (A)
XG07H Ext Horn PCB	£14.50 (A)
LR59P Burglar Alarm PSU PCB	£2.40 (C)
GA45Y Burg Alarm Main PCB	£6.75 (B)
GA46A Break Contact PCB	£1.95 (D)
GA47B Ext Horn PCB	£1.60 (D)
LRW57M Burglar Alarm Kit	£44.95 (A)
LRW58N Train Receiver 2 PCB	£1.25 (D)
LRW58N Ext Horn Kit	£29.95 (A)
GA81C Channel/PSU PCB	£1.85 (D)
GA82D Extra Channel PCB	£1.35 (D)
LRW73D RTX3 Doppler Kit	£39.95 (A)
LRW74E Radar Chn/PSU Module	£13.95 (A)
LRW75S Radar Extrich Module	£4.50 (C)

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GB00A Ultrasonic Xvr PCB	£1.60 (D)
GB01D Ultrasonic F PCB	£1.60 (D)
LRW83E Usonic Xceiver Kit	£12.25 (A)
LRW84F Usonic Interface Kit	£2.50 (C)
XF44X Magnum Booklet	50p (V)
Y044X Magnum 1 PCB	£2.95 (C)
Y045Y Magnum 2 PCB	£2.95 (C)
Y072P Magnum Mod Chng PCB	£1.65 (D)
GA79L Multi-circuit Board	£1.25 (D)

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LY94C HiFi Amp Sel Mthr PC	£4.20 (C)
FL95D HiFi Amp Sel PCB	£3.47 (C)
FL96E HiFi Amp Egl Mthr PC	£2.95 (C)
FL97D HiFi Amp Egl PCB	£1.97 (D)
FL98C HiFi Amp Pk Det PCB	£1.97 (D)
FL99H HiFi Amp PSU PCB	£2.15 (C)
XX32K H/Phones Slt Brckt	59p (E)
XY21X HiFi Amp Chassis	£22.10 (A)
XY22Y HiFi Amp Screen	£1.85 (D)
XY23A HiFi Amp Fr Panel	£10.99 (B)
XY24B HiFi Amp Cover Black	£6.95 (B)

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MX48C MES33	40p (V)
FL94C HiFi Amp Sel Mthr PC	£4.20 (C)
FL95D HiFi Amp Sel PCB	£3.47 (C)
FL96E HiFi Amp Egl Mthr PC	£2.95 (C)
FL97D HiFi Amp Egl PCB	£1.97 (D)
FL98C HiFi Amp Pk Det PCB	£1.97 (D)
FL99H HiFi Amp PSU PCB	£2.15 (C)
XX32K H/Phones Slt Brckt	59p (E)
XY21X HiFi Amp Chassis	£22.10 (A)
XY22Y HiFi Amp Screen	£1.85 (D)
XY23A HiFi Amp Fr Panel	£10.99 (B)
XY24B HiFi Amp Cover Black	£6.95 (B)

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LRW57M Burglar Alarm Kit	£44.95 (A)
LRW58N Train Receiver 2 PCB	£1.25 (D)
LRW58N Ext Horn Kit	£29.95 (A)
GA81C Channel/PSU PCB	£1.85 (D)
GA82D Extra Channel PCB	£1.35 (D)
LRW73D RTX3 Doppler Kit	£39.95 (A)
LRW74E Radar Chn/PSU Module	£13.95 (A)
LRW75S Radar Extrich Module	£4.50 (C)

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GB00A Ultrasonic Xvr PCB	£1.60 (D)
GB01D Ultrasonic F PCB	£1.60 (D)
LRW83E Usonic Xceiver Kit	£12.25 (A)
LRW84F Usonic Interface Kit	£2.50 (C)
XF44X Magnum Booklet	50p (V)
Y044X Magnum 1 PCB	£2.95 (C)
Y045Y Magnum 2 PCB	£2.95 (C)
Y072P Magnum Mod Chng PCB	£1.65 (D)
GA79L Multi-circuit Board	£1.25 (D)

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MX48C MES33	40p (V)
FL94C HiFi Amp Sel Mthr PC	£4.20 (C)
FL95D HiFi Amp Sel PCB	£3.47 (C)
FL96E HiFi Amp Egl Mthr PC	£2.95 (C)
FL97D HiFi Amp Egl PCB	£1.97 (D)
FL98C HiFi Amp Pk Det PCB	£1.97 (D)
FL99H HiFi Amp PSU PCB	£2.15 (C)
XX32K H/Phones Slt Brckt	59p (E)
XY21X HiFi Amp Chassis	£22.10 (A)
XY22Y HiFi Amp Screen	£1.85 (D)
XY23A HiFi Amp Fr Panel	£10.99 (B)
XY24B HiFi Amp Cover Black	£6.95 (B)

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FO63T Curved Demagnetiser	£3.85 (C)
BR27E Elec Head Demag	£8.95 (C)
WY91Y Splicing Block	£1.85 (D)

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LR13P HQ Mixer PCB No 2	£1.96 (D)
LR14Q HQ Mixer PCB No 3	£1.55 (D)
LR15R HQ Mixer PCB No 4	£1.39 (D)
LR34M HQ Mixer PCB No 24	£1.98 (D)

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GB00A Ultrasonic Xvr PCB	£1.60 (D)
GB01D Ultrasonic F PCB	£1.60 (D)
LRW83E Usonic Xceiver Kit	£12.25 (A)
LRW84F Usonic Interface Kit	£2.50 (C)
XF44X Magnum Booklet	50p (V)
Y044X Magnum 1 PCB	£2.95 (C)
Y045Y Magnum 2 PCB	£2.95 (C)
Y072P Magnum Mod Chng PCB	£1.65 (D)
GA79L Multi-circuit Board	£1.25 (D)

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GA26D Dig Tacho Main PCB	£1.75 (D)
GA27E Dig Tacho Dsply PCB	£1.25 (D)
GA19V Batt Mon PCB	£1.20 (D)
GA98G Car Burglar Alarm PCB	£1.10 (D)
LRW87K Car Burglar Alarm Kit	£6.95 (B)
GA40T Car Aerial Bster PCB	£1.35 (D)

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HR15R Ctrdg Goldring G850	£5.70 (B)
HR16S Ctrdg Goldring G800	£7.45 (B)
HR16V Ctrdg Goldring G800H	£9.85 (B)
Q039N Ctrdg Goldring G800E	£11.95 (A)
FQ04T Ctrdg Tenorel T2001D	£4.85 (C)
FQ41U Cdg Tenorel T2001E	£11.29 (A)
RK98G Ctrdg Tenorel TMC101	£9.95 (A)
BK64U TMC10 Replacement	£19.95 (A)

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U Micro Res	3p (H)
B Econ Res 1R to 8R2	2p (H)
E Econ Res 1M2 to 10M	2p (H)
M 1M to 8R2 (1%)	12p (H)
M 1M to 1M (1%)	2p (H)
M 1M to 1M (10%)	12p (H)

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LR24V HQ Mixer PCB No 9	£1.78 (D)
LR24V HQ Mixer PCB No 29	£2.95 (C)
LR25C HQ Mixer PCB No 10	£1.85 (D)
LR26D HQ Mixer PCB No 14	£1.87 (D)

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GA74R Train Receiver 1 PCB	£1.35 (D)
LRW61R Train Common/PSU Kit	£27.50 (A)
LRW62S Train Control Kit	£6.45 (A)
LRW63T Train Rcvr ML926Kit	£5.95 (B)
LRW64U Train Rcvr M1926Kit	£5.95 (B)
LRW65V Train Rcvr M1927Kit	£5.95 (B)
LRW69A Train Rcvr M1927Kit	£5.95 (B)

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XF52G E&MM October 1981	£1.00 (V)
XF53M E&MM November 1981	£1.00 (V)
XF54J E&MM December 1981	£1.00 (V)
XF55K E&MM January 1982	£1.00 (V)
XF56L E&MM February 1982	£1.00 (V)
XF57M E&MM March 1982	£1.00 (V)
XF58N E&MM April 1982	£1.00 (V)
XF59P E&MM May 1982	£1.00 (V)
XF60Q E&MM June '82	£1.00 (V)
XF61R E&MM July 1982	£1.00 (V)
XF62S E&MM August 1982	£1.00 (V)

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HR25C Stylus GP91SC DD	£1.85 (D)
HR26V Stylus Sanyo ST26	£5.50 (B)
BK07H Stylus ATN3400	£1.85 (D)
HR13J Stylus GP104 DD	£1.85 (D)
HR66W Stylus Acos SM6	£4.95 (C)
BK08J Stylus ATN71	£5.50 (B)
HR27C Stylus ADC R5030	£4.95 (C)
BK09K Stylus ATN3710	£4.95 (C)
BK10L Stylus Toshiba N501	£5.50 (B)
XY09K Stylus AT70	£4.95 (C)
BK19N Stylus DS107AL	£4.95 (C)
HR68V Stylus VMB ST104	£5.50 (B)
HR39N Stylus BSR TC8 D	£1.50 (D)
HR71N Stylus BSR ST4 DD	£1.85 (D)
HR42V Stylus BSR ST10	£1.85 (D)
HR45Y Stylus BSR ST15	£1.85 (D)
HR47B Stylus BSR ST17 DD	£1.85 (D)
HR48V Stylus BSR ST104	£1.85 (D)
BK11M Stylus Hitachi E100	£5.50 (B)
BK12N Stylus JVC DT31	£5.50 (B)
XY12N Stylus Garrard GA150	£10.50 (A)
HR76H Stylus D110E	£5.50 (B)
HR76V Stylus D110H	£2.95 (C)
HR78C Stylus D110SR	£1.95 (D)
HR49D Stylus D120SR	£2.45 (C)
HR78K Stylus Hitachi ST101	£4.95 (C)
HR79L Stylus Hitachi ST103	£6.75 (B)
HR80V Stylus Hitachi ST104	£6.75 (B)
XY14J Stylus JVC DT21S	£4.95 (C)
FQ54J Stylus JVC DT33	£4.95 (C)
BK14Q Stylus Trio STY111	£4.95 (C)
HR81C Stylus LV65977D	£1.50 (D)
HR82V Stylus NP EP525	£2.25 (C)
HR84F Stylus NP EP525	£5.50 (B)
XY16S Stylus NP EP533	£5.50 (B)
XY17T Stylus Philip AG3306	£1.85 (D)
HR87U Styl Philips GP200DD	£1.85 (D)
HR88V Stylus Philips GP203	£1.25 (D)
XY18U Styl Philips GP213	£5.10 (B)
HR90X Styl Philips GP400	£5.10 (B)
XY19V Styl Philips GP400Mk2	£4.95 (C)
XY20W Styl Philips GP401Mk2	£6.75 (B)
BK15R Stylus EP207	£6.75 (B)
HR91V Stylus Sanyo ST104	£4.95 (C)
HR96E Stylus DM500/7	£4.95 (C)
XY22Y Stylus Sanyo ST10J	£4.95 (C)
HR95D Stylus Sansui SN28	£4.95 (C)
XY23A Stylus Sansui SN41	£4.95 (C)
HR97C Stylus Sanyo ST104	£4.95 (C)
HR97F Stylus Sanyo 2611	£4.95 (C)
FQ48C Stylus Sanyo ND128	£2.20 (C)
XY25C Stylus Sharp STY101	£4.95 (C)
HR98G Stylus Sharp 706	£4.95 (C)
FQ49D Stylus Sony ND133	£1.85 (D)
BK16S Stylus Sony ND133	£5.50 (B)
HR61R Stylus Sonotone V100	£4.95 (C)
XY26D Stylus Sonotone V101	£4.95 (C)
FQ45Y Stylus 2509	£1.85 (D)
HR95V Stylus ST40C DD	£1.85 (D)
HR95H Stylus SKA40 DD	£1.85 (D)
BK17T Stylus Sony ND114	£5.50 (B)
BK18U Stylus ND200	£6.75 (B)
XY27E Stylus Sony XL15	£4.95 (C)
XY28F Stylus Sony ND126	£4.95 (C)
FQ49D Stylus Sony ND133	£5.50 (B)
FQ50F Stylus Sony ND134	£2.95 (C)
FQ52G Stylus N2001ED	£6.75 (B)
XY30H Stylus Tetrad 51	£2.25 (C)
FQ33H Stylus Toshiba NSC	£2.20 (C)
XY31J Stylus Toshiba N55	£4.95 (C)
XY32K Stylus Toshiba N58	£4.95 (C)
XY21X Stylus Toshiba N550	£4.95 (C)

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C Std Res	3p (H)
X Colour Wheel	25p (F)
X See Me	2p (H)
T See Me	2p (H)
M W/W Res	29p (F)

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HQ68Y 50W Hi-Fi PCB	£2.96 (C)

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XF11M Stereo Synth Book	£2.00 (V)
XF12S MES12S	FREE
XF37S MES2C	FREE
XF42B MES15	15p (V)
XF44X MES15B	FREE

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XF63T E&MM September 1982	£1.00 (V)
XF64U E&MM October 1982	£1.00 (V)
XF61R E&MM Projects Vol 1	£1.00 (V)
XA00A Maplin Mag Subscripn	£2.40 (V)
XA01C Projects Book One	60p (V)
XA02D Projects Book Two	60p (V)
XA03E Projects Book Three	60p (V)
XA04F Projects Book Four	60p (V)

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YB47B Record Care Ct C106	£4.95 (C)
LY06G Cleaning Arm C100	£3.25 (D)
YB81C Cleaning Cloth C104	78p (E)
FR48C Dust-Off C101	89p (E)
WY82D Cleaner C92	£4.65 (C)
XY93B Stylus Microscope	£2.45 (C)
WY83E Stylus Brush C103	12p (D)
FR46A Stylus Cleaner C95	22p (D)
WY85V Stylus Cleaning Fluid	58p (E)
FR52G Anti-Static Fluid C99	49p (F)
LY10L Anti-Stat Mat C119	£1.95 (D)
LY04E Anti-Stat Gun	£5.25 (B)
FR49D Stylus Balance PK1	£2.45 (C)
FR50E Gram Speed Indicator	9p (H)

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L 7W W/W	29p (F)
H 10W W/W	39p (F)
I 15W W/W	£1.65 (D)
V HV Res 1M 33M	12p (D)
V HV Res 47M	25p (F)
BL64U Constantan 28 swg	£3.25 (C)
YY12N Resnet 100R	85p (E)
YY13P Resnet 100K	85p (E)
YY14Q Resnet 470R	85p (E)
YY15R Resnet 1k	85p (E)
YY16S Resnet 2k2	93p (E)
YY17T Resnet 4k7	95p (E)
YY18U Resnet	

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BW08J Edge Knob Small Grey	8p (H)	BR45Y AS314	33p (F)	QH16S BZ88C12	9p (H)	QH71N DA90	9p (H)	QL85C IN5406	20p (G)
BW09K Edge Knob Large Bk	8p (H)	QB21X AY 1-0212	£8.20 (B)	QH17T BZ88C13	9p (H)	QH72P OA91	8p (H)	QL86T IN5407	19p (G)
BW10L Edge Knob Large Grey	8p (H)	QH52G AY 1-1320	£4.99 (C)	QH18U BZ88C15	9p (H)	QH73Q OA95	8p (H)	QL87U IN5408	19p (G)
FW04A Pot Lin 1k	45p (F)	QH51F AY 1-5050	£1.99 (D)	QH19V BZ88C16	9p (H)	QH74R DA200	8p (H)	QL88W I5921	9p (H)
FW01B Pot Lin 4k7	45p (F)	QH12Z BA243	£8.30 (B)	QH20W BZ88C18	9p (H)	QH75S OA202	13p (G)	QH46A 1458C	45p (F)
FW02C Pot Lin 10k	45p (F)	QH13Z BA243	£8.30 (B)	QH21X BZ88C20	9p (H)	QH76S OA202	13p (G)	OR00A 2N697	49p (F)
FW03D Pot Lin 22k	45p (F)	QH14Z BA243	£8.30 (B)	QH22Y BZ88C22	9p (H)	QH77S OA202	13p (G)	OR01R 2N706	35p (F)
FW04E Pot Lin 47k	45p (F)	QH15Z BA243	£8.30 (B)	QH23A BZ88C24	9p (H)	QH78S OA202	13p (G)	OR03D 2N708	35p (F)
FW05F Pot Lin 100k	45p (F)	QH16Z BA243	£8.30 (B)	QH24B BZ88C27	8p (H)	QH79S OA202	13p (G)	OR09K 2N1711	39p (F)
FW06G Pot Lin 220k	45p (F)	QH17Z BA243	£8.30 (B)	QH25C BZ88C30	9p (H)	QH80S OA202	13p (G)	OR10L 2N1893	32p (F)
FW07H Pot Lin 470k	45p (F)	QH18Z BA243	£8.30 (B)	QH26D CA3046	72p (E)	QH81S OA202	13p (G)	OR11M 2N2219	31p (F)
FW08J Pot Lin 1M	45p (F)	QH19Z BA243	£8.30 (B)	QH27E CA3089E	£2.70 (C)	QH82S OA202	13p (G)	OR12R 2N238A	22p (F)
FW09K Pot Lin 2M2	45p (F)	QH20Z BA243	£8.30 (B)	QH28F CA310T	£1.10 (D)	QH83S OA202	13p (G)	OR13P 2N2484	31p (F)
FW21A Pot Log 4k7	45p (F)	QH21Z BA243	£8.30 (B)	QH29G CA3140T	£1.10 (D)	QH84S OA202	13p (G)	OR14Q 2N2646	55p (E)
FW22Y Pot Log 10k	45p (F)	QH22Z BA243	£8.30 (B)	QH30H CI06D	42p (F)	QH85S OA202	13p (G)	OR15R 2N2647	95p (E)
FW23A Pot Log 22k	45p (F)	QH23Z BA243	£8.30 (B)	QH31J BC107B	14p (G)	QH86S OA202	13p (G)	OR16S 2N2904	31p (F)
FW24B Pot Log 47k	45p (F)	QH24Z BA243	£8.30 (B)	QH32K BC108C	14p (G)	QH87S OA202	13p (G)	OR17T 2N2905	31p (F)
FW25C Pot Log 100k	45p (F)	QH25Z BA243	£8.30 (B)	QH33L BC109C	16p (G)	QH88S OA202	13p (G)	OR18U 2N2906	36p (F)
FW26D Pot Log 220k	45p (F)	QH26Z BA243	£8.30 (B)	QH34M BC1119	24p (F)	QH89S OA202	13p (G)	OR19V 2N2907	26p (F)
FW27E Pot Log 470k	45p (F)	QH27Z BA243	£8.30 (B)	QH35Q BC1199	24p (F)	QH90S OA202	13p (G)	OR20W 2N29260r	12p (G)
FW28F Pot Log 1M	45p (F)	QH28Z BA243	£8.30 (B)	QH36P BC1399	40p (F)	QH91S OA202	13p (G)	OR21X 2N2926e	12p (G)
FW29G Pot Log 2M2	45p (F)	QH29Z BA243	£8.30 (B)	QH37S BC1340	34p (F)	QH92S OA202	13p (G)	OR22Y 2N2926Gn	12p (G)
		QH38R BC1411	37p (F)	QH38R BC1411	37p (F)	QH93S OA202	13p (G)	OR23A 2N2926	26p (F)
		QH39N BC142	34p (F)	QH39N BC142	34p (F)	QH94S OA202	13p (G)	OR24B 2N3054	6p (E)
		QH40A BC154	27p (F)	QH40A BC154	27p (F)	QH95S OA202	13p (G)	BL45Y 2N3055	75p (E)
		QH41B BC161	36p (F)	QH41B BC161	36p (F)	QH96S OA202	13p (G)	OR25C 2N3525	£1.85 (D)
		QH42C BC168	11p (G)	QH42C BC168	11p (G)	QH97S OA202	13p (G)	OR26D 2N3702	11p (G)
		QH43D BC177	21p (G)	QH43D BC177	21p (G)	QH98S OA202	13p (G)	OR27E 2N3703	11p (G)
		QH44E BC184	11p (G)	QH44E BC184	11p (G)	QH99S OA202	13p (G)	OR28F 2N3704	11p (G)
		QH45F BC191	40p (F)	QH45F BC191	40p (F)	QH00S OA202	13p (G)	OR29G 2N3705	12p (G)
		QH46G BC204	15p (G)	QH46G BC204	15p (G)	QH01S OA202	13p (G)	OR30H 2N3706	14p (G)
		QH47H BC209C	14p (G)	QH47H BC209C	14p (G)	QH02S OA202	13p (G)	OR31J 2N3707	12p (G)
		QH48J BC212L	11p (G)	QH48J BC212L	11p (G)	QH03S OA202	13p (G)	OR32K 2N3708	11p (G)
		QH49K BC215L	11p (G)	QH49K BC215L	11p (G)	QH04S OA202	13p (G)	OR33L 2N3709	11p (G)
		QH50M BC218	10p (G)	QH50M BC218	10p (G)	QH05S OA202	13p (G)	OR34M 2N3711	11p (G)
		QH51N BC225	10p (G)	QH51N BC225	10p (G)	QH06S OA202	13p (G)	OR35P 2N3712	£1.95 (D)
		QH52P BC231	10p (G)	QH52P BC231	10p (G)	QH07S OA202	13p (G)	OR36P 2N3713	£2.70 (C)
		QH53R BC238	10p (G)	QH53R BC238	10p (G)	QH08S OA202	13p (G)	OR37Q 2N3714	65p (E)
		QH54T BC245	10p (G)	QH54T BC245	10p (G)	QH09S OA202	13p (G)	OR38R 2N3903	17p (G)
		QH55V BC252	10p (G)	QH55V BC252	10p (G)	QH10S OA202	13p (G)	OR40T 2N3904	17p (G)
		QH56W BC259	10p (G)	QH56W BC259	10p (G)	QH11S OA202	13p (G)	OR41U 2N3905	15p (G)
		QH57X BC266	10p (G)	QH57X BC266	10p (G)	QH12S OA202	13p (G)	OR42V 2N3906	14p (G)
		QH58Y BC273	10p (G)	QH58Y BC273	10p (G)	QH13S OA202	13p (G)	OR43W 2N3907	12p (G)
		QH59Z BC280	10p (G)	QH59Z BC280	10p (G)	QH14S OA202	13p (G)	OR44X 2N4060	12p (G)
		QH60A BC287	10p (G)	QH60A BC287	10p (G)	QH15S OA202	13p (G)	OR45Y 2N4061	17p (G)
		QH61B BC294	10p (G)	QH61B BC294	10p (G)	QH16S OA202	13p (G)	OR46A 2N4062	12p (G)
		QH62C BC301	10p (G)	QH62C BC301	10p (G)	QH17S OA202	13p (G)	OR47B 2N4871	69p (E)
		QH63D BC308	10p (G)	QH63D BC308	10p (G)	QH18S OA202	13p (G)	OR48C 2N5459	36p (F)
		QH64E BC315	10p (G)	QH64E BC315	10p (G)	QH19S OA202	13p (G)	OR49D 2N6073	£1.20 (D)
		QH65F BC322	10p (G)	QH65F BC322	10p (G)	QH20S OA202	13p (G)	OR50E 2N6074	£3.55 (C)
		QH66G BC329	10p (G)	QH66G BC329	10p (G)	QH21S OA202	13p (G)	OR51F 2N6075	£1.20 (D)
		QH67H BC336	10p (G)	QH67H BC336	10p (G)	QH22S OA202	13p (G)	OR52G 2N6076	£1.20 (D)
		QH68J BC343	10p (G)	QH68J BC343	10p (G)	QH23S OA202	13p (G)	OR53H 2N6077	£1.20 (D)
		QH69K BC350	10p (G)	QH69K BC350	10p (G)	QH24S OA202	13p (G)	OR54J 2N6078	£1.20 (D)
		QH70L BC357	10p (G)	QH70L BC357	10p (G)	QH25S OA202	13p (G)	OR55K 2N6079	£1.20 (D)
		QH71M BC364	10p (G)	QH71M BC364	10p (G)	QH26S OA202	13p (G)	OR56L 2N6080	£1.20 (D)
		QH72N BC371	10p (G)	QH72N BC371	10p (G)	QH27S OA202	13p (G)	OR57M 2N6081	£1.20 (D)
		QH73O BC378	10p (G)	QH73O BC378	10p (G)	QH28S OA202	13p (G)	OR58N 2N6082	£1.20 (D)
		QH74P BC385	10p (G)	QH74P BC385	10p (G)	QH29S OA202	13p (G)	OR59P 2N6083	£1.20 (D)
		QH75Q BC392	10p (G)	QH75Q BC392	10p (G)	QH30S OA202	13p (G)	OR60Q 2N6084	£1.20 (D)
		QH76R BC399	10p (G)	QH76R BC399	10p (G)	QH31S OA202	13p (G)	OR61R 2N6085	£1.20 (D)
		QH77S BC406	10p (G)	QH77S BC406	10p (G)	QH32S OA202	13p (G)	OR62S 2N6086	£1.20 (D)
		QH78T BC413	10p (G)	QH78T BC413	10p (G)	QH33S OA202	13p (G)	OR63T 2N6087	£1.20 (D)
		QH79U BC420	10p (G)	QH79U BC420	10p (G)	QH34S OA202	13p (G)	OR64U 2N6088	£1.20 (D)
		QH80V BC427	10p (G)	QH80V BC427	10p (G)	QH35S OA202	13p (G)	OR65V 2N6089	£1.20 (D)
		QH81W BC434	10p (G)	QH81W BC434	10p (G)	QH36S OA202	13p (G)	OR66W 2N6090	£1.20 (D)
		QH82X BC441	10p (G)	QH82X BC441	10p (G)	QH37S OA202	13p (G)	OR67X 2N6091	£1.20 (D)
		QH83Y BC448	10p (G)	QH83Y BC448	10p (G)	QH38S OA202	13p (G)	OR68Y 2N6092	£1.20 (D)
		QH84Z BC455	10p (G)	QH84Z BC455	10p (G)	QH39S OA202	13p (G)	OR69Z 2N6093	£1.20 (D)
		QH85A BC462	10p (G)	QH85A BC462	10p (G)	QH40S OA202	13p (G)	OR70A 2N6094	£1.20 (D)
		QH86B BC469	10p (G)	QH86B BC469	10p (G)	QH41S OA202	13p (G)	OR71B 2N6095	£1.20 (D)
		QH87C BC476	10p (G)	QH87C BC476	10p (G)	QH42S OA202	13p (G)	OR72C 2N6096	£1.20 (D)
		QH88D BC483	10p (G)	QH88D BC483	10p (G)	QH43S OA202	13p (G)	OR73D 2N6097	£1.20 (D)
		QH89E BC490	10p (G)	QH89E BC490	10p (G)	QH44S OA202	13p (G)	OR74E 2N6098	£1.20 (D)
		QH90F BC497	10p (G)	QH90F BC497	10p (G)	QH45S OA202	13p (G)	OR75F 2N6099	£1.20 (D)
		QH91G BC504	10p (G)	QH91G BC504	10p (G)	QH46S OA202	13p (G)	OR76G 2N6100	£1.20 (D)
		QH92H BC511	10p (G)	QH92H BC511	10p (G)	QH47S OA202	13p (G)	OR77H 2N6101	£1.20 (D)
		QH93I BC518	10p (G)	QH93I BC518	10p (G)	QH48S OA202	13p (G)	OR78I 2N6102	£1.20 (D)
		QH94J BC525	10p (G)	QH94J BC525	10p (G)	QH49S OA202	13p (G)	OR79J 2N6103	£1.20 (D)
		QH95K BC532	10p (G)	QH95K BC532	10p (G)	QH50S OA202	13p (G)	OR80K 2N6104	£1.20 (D)
		QH96L BC539	10p (G)	QH96L BC539	10p (G)	QH51S OA202	13p (G)	OR81L 2N6105	£1.20 (D)
		QH97M BC546	10p (G)	QH97M BC546	10p (G)	QH52S OA202	13p (G)	OR82M 2N6106	£1.20 (D)
		QH98N BC553	10p (G)	QH98N BC553	10p (G)	QH53S OA202	13p (G)	OR83N 2N6107	£1.20 (D)
		QH99O BC560	10p (G)	QH99O BC560	10p (G)	QH54S OA202	13p (G)	OR84O 2N6108	£1.20 (D)
		QH00P BC567	10p (G)	QH00P BC567	10p (G)	QH55S OA202	13p (G)	OR85P 2N6109	£1.20 (D)
		QH01Q BC574	10p (G)	QH01Q BC574	10p (G)	QH56S OA202	13p (G)	OR86Q 2N6110	£1.20 (D)
		QH02R BC581	10p (G)	QH02R BC581	10p (G)	QH57S OA202	13p (G)	OR87R 2N6111	£1.20 (D)
		QH03S BC588	10p (G)	QH03S BC588	10p (G)	QH58S OA202	13p (G)	OR88S 2N6112	£1.20 (D)
		QH04T BC595	10p (G)	QH04T BC595	10p (G)	QH59S OA202	13p (G)	OR89T 2N6113	£1.20 (D)
		QH05U BC602	10p (G)	QH05U BC602	10p (G)	QH60S OA202	13p (G)	OR90U 2N6114	£1.20 (D)
		QH06V BC609	10p (G)	QH06V BC609	10p (G)	QH61S OA202	13p (G)	OR91V 2N6115	£1.20 (D)
		QH07W BC616	10p (G)	QH07W BC616	10p (G)	QH62S OA202	13p (G)	OR92W 2N6116	£1.20 (D)
		QH08X BC623	10p (G)	QH08X BC623	10p (G)	QH63S OA202	13p (G)	OR93X 2N6117	£1.20 (D)
		QH09Y BC630	10p (G)	QH09Y BC630	10p (G)	QH64S OA202	13p (G)	OR94Y 2N6118	£1.20 (D)
		QH10Z BC637	10p (G)	QH10Z BC637	10p (G)	QH65S OA202	13p (G)	OR95Z 2N6119	£1.20 (D)
		QH11A BC644	10p (G)	QH11A BC644	10p (G)	QH66S OA202	13p (G)	OR96A 2N6120	£1.20 (D)
		QH12B BC651	10p (G)	QH12B BC651	10p (G)	QH67S OA202	13p (G)	OR97B 2N6121	£1.20 (D)
		QH13C							

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Q038R 40175BE	£1.25 (D)	WHO1B 7412J	42p (F)	QH48C MC3302P	80p (E)	Page 319	
Q074R 40181BE	£1.99 (D)	YF48C 74LS123	62p (E)	QY14Q UAA170L	£2.50 (C)	QY44X Insulator T03	18p (G)
QW75S 40182BE	85p (E)	YF49D 74LS125	33p (F)	YJ30H 74C917	£8.85 (B)	QY45Y Insulator P	14p (G)
QW75H 40192BE	£1.25 (D)	YF50E 74LS126	33p (F)	Y9000 Crystal 6.5536MHz	£2.98 (C)	WR24B Kit T03	8p (H)
QW77J 40193BE	80p (E)	WHO1D 74LS132	55p (E)	Y939B ICM7045PI	£14.20 (A)	WR25C Kit T066	9p (H)
QW78K 40194BE	80p (E)	YF51F 74LS132	45p (F)			WR27E Kit S055	9p (H)
QW79L 40257BE	£1.10 (D)	YF52G 74LS136	32p (F)			WR26D Kit T0126	5p (H)
QX34M 40673	£1.75 (D)	YF53H 74LS138	38p (F)			WR23A Kit (P) Plus	6p (H)
QW93B 4116 250ns	£1.45 (D)	YF54J 74LS139	44p (F)			XX14Q Soldercons	90p (E)
QW95F 4118 250ns	£4.45 (C)	YF65V 74LS152	75p (E)				
X011B 4136	75p (E)	WHO6G 74LS157	47p (F)				
QW80B 4151	89p (E)	YF55K 74LS145	£1.65 (D)				
Q006G 4164 250ns	£5.99 (B)	QX89W 74LS150	80p (E)				
X020C 4195	£1.45 (D)	WHO7H 74LS151	65p (E)				
QX30H 4416BE	£1.92 (D)	YF59L 74LS153	43p (F)				
QW10C 4502BE	£1.19 (D)	YF59M 74LS153	49p (F)				
Q041U 4503BE	95p (E)	WHO8J 74LS154	78p (E)				
QW82D 4508BE	£2.10 (C)	YF58N 74LS154	98p (E)				
QW83E 4510BE	68p (E)	YF59P 74LS155	37p (F)				
QX31J 4511BE	68p (E)	YF60Q 74LS156	57p (E)				
QW84F 4512BE	85p (E)	YF61R 74LS157	35p (F)				
QW85G 4514BE	£1.20 (D)	YF62S 74LS158	49p (E)				
QW86T 4515BE	£1.20 (D)	WHO9K 74LS160	67p (E)				
QW87U 4516BE	49p (F)	YF63T 74LS160	49p (F)				
QX32K 4518BE	85p (E)	YF64U 74LS161	49p (F)				
QW88V 4520BE	78p (E)	YF65V 74LS162	51p (E)				
Q042V 4521BE	£2.88 (E)	YF66W 74LS163	49p (F)				
Q043W 4522BE	£2.58 (E)	WH10L 74LS164	66p (E)				
Q044X 4526BE	95p (E)	YF67X 74LS164	55p (E)				
QW88V 4527BE	£1.15 (D)	YF68Y 74LS165	£1.40 (D)				
Q045Y 4529BE	£1.19 (D)	YF69A 74LS166	£1.95 (E)				
QW89W 4532BE	£1.10 (D)	YF70M 74LS168	£1.20 (D)				
QW90X 4555BE	50p (E)	YF71N 74LS169	99p (E)				
QW91Y 4556BE	58p (E)	YF72P 74LS170	£2.99 (E)				
Q049D 4568BE	£3.15 (C)	YF73Q 74LS173	65p (E)				
Q051F 45100BE	£1.25 (E)	WH11M 74LS174	81p (E)				
Q052G 5W Zener 5V6	£1.27 (D)	YF74R 74LS175	62p (E)				
X36P 5W Zener 8V2	£1.27 (D)	YF75S 74LS175	58p (E)				
YH31J 5101-1L	£3.48 (C)	YF76H 74LS180	£2.95 (E)				
OR55K 6345S2	£4.95 (C)	YF77K 74LS190	58p (E)				
Q004E 6402	£2.58 (B)	YF78U 74LS191	58p (E)				
Q002C 6502	£2.58 (B)	WH12N 74LS192	70p (E)				
QW94C 7106	£7.90 (B)	WH12P 74LS193	70p (E)				
QW95D 7107	£7.95 (B)	QX90X 74LS193	66p (E)				
QX37S 7400	17p (G)	YF81C 74LS193	65p (E)				
YF00A 74LS00	17p (G)	YF81P 74LS193	55p (E)				
QX38R 7401	17p (G)	YF82Q 74LS194	85p (E)				
YF01B 74LS01	17p (G)	YF83E 74LS195	45p (F)				
QX39N 7402	17p (G)	WH14Q 74LS196	48p (F)				
YF02C 74LS02	21p (G)	YF85G 74LS197	63p (E)				
QX74R 7403	20p (G)	YF86T 74LS221	99p (E)				
YF03D 74LS03	17p (G)	YF87U 74LS241	99p (E)				
QY24B 74503	68p (E)	YF88V 74LS241	99p (E)				
QX40T 7404	21p (G)	YF89W 74LS242	99p (E)				
YF04E 74LS04	20p (G)	YF90X 74LS243	89p (E)				
QX41U 7405	21p (G)	Q056L 74LS244	£2.87 (E)				
YF05F 74LS05	20p (G)	YF92A 74LS251	£2.87 (E)				
QX75S 7406	29p (F)	YF93B 74LS253	53p (E)				
QX76H 7407	29p (F)	YF95D 74LS257	52p (E)				
QX42V 7408	21p (G)	YF96E 74LS258	55p (E)				
YF06G 74LS08	22p (G)	YF97G 74LS261	£2.25 (C)				
QX77J 7409	17p (G)	YF99H 74LS266	32p (F)				
YF07H 74LS09	22p (G)	YH00A 74LS273	£1.32 (D)				
QX43W 7410	17p (G)	WH01B 74LS279	40p (F)				
YF08J 74LS10	22p (G)	YH02C 74LS283	70p (G)				
QX44X 7411	24p (F)	YH03D 74LS290	£1.30 (D)				
YF09K 74LS12	22p (G)	YH09V 74LS292	£1.10 (A)				
YF10L 74LS12	17p (G)	YH04E 74LS293	96p (E)				
QX45Y 7413	28p (F)	QY40T 74LS297	£1.10 (A)				
YF11M 74LS13	31p (F)	YH05T 74LS298	£1.25 (C)				
QX46A 7414	42p (F)	YH07H 74LS299	£4.25 (C)				
YF12N 74LS14	17p (G)	YH08J 74LS323	£6.75 (B)				
YF12P 74LS15	17p (G)	YH09K 74LS363	£2.35 (C)				
QX78K 7416	31p (F)	WH11M 74LS365	99p (F)				
QX79L 7417	30p (F)	YH13P 74LS367	62p (E)				
QX47B 7420	23p (G)	YH14Q 74LS368	43p (F)				
YF14Q 74LS20	21p (G)	YH15R 74LS373	£1.15 (D)				
QX74T 7421	40p (F)	YH16S 74LS374	£1.30 (D)				
YF15R 74LS21	20p (G)	YH17P 74LS377	£1.82 (D)				
YF16S 74LS22	17p (G)	YH18U 74LS378	£1.40 (D)				
QX80B 7425	28p (F)	YH19V 74LS378	£1.40 (D)				
QX81C 7426	22p (G)	YH20W 74LS379	£2.40 (C)				
YF17T 74LS26	29p (F)	YH21X 74LS390	£1.45 (D)				
QX49D 7427	29p (F)	YH22Y 74LS393	£1.40 (D)				
YF18U 74LS27	29p (F)	YH23A 74LS395	£1.35 (D)				
YF19V 74LS28	44p (F)	YH24B 74LS398	£1.99 (D)				
QX50E 7430	36p (F)	YH25C 74LS399	£2.50 (C)				
YF20W 74LS30	36p (F)	Q059P 74LS600	N/A				
QX51F 7432	36p (F)	QY41U 74LS601	£1.72 (A)				
YF21X 74LS32	21p (G)	QY42V 74LS602	£4.56 (C)				
YF22Y 74LS33	40p (F)	Q061R 74LS608	N/A				
YF23A 74LS34	21p (G)	Q062S 74LS610	N/A				
QX82D 7438	22p (G)	WH02C 74LS629=74LS124	£1.49 (D)				
YF24B 74LS38	22p (G)	YH29G 74LS670	£3.95 (C)				
QX53H 7440	24p (F)	YH30T 74LS674	£4.25 (C)				
YF25C 74LS40	40p (F)	YH31J 5101-1L	£3.48 (C)				
QX54J 7442	48p (F)	QW11M 2102 450ns	£1.95 (D)				
YF26D 74LS42	42p (F)	QW04Y MC6810AP 450ns	£1.86 (D)				
QX55K 7447A	55p (E)	QW12N 2114 450ns	£1.30 (D)				
Q052G 74LS47	65p (E)	QW03B 4121 250ns	£2.45 (C)				
Q053H 74LS48	68p (E)	QW42V MC4027 250ns	£1.88 (D)				
QX83E 7451	22p (G)	QW93B 4116 250ns	£1.45 (D)				
YF27E 74LS51	70p (E)						
YF28F 74LS54	30p (F)						
QX56L 7470	36p (F)						
QX57M 7472	35p (F)						
QX58N 7473	32p (F)						
YF30H 74LS73	32p (F)						
QX59P 7474	32p (F)						
YF30H 74LS74	26p (F)						
QX60Q 7475	35p (F)						
YF32K 74LS75	32p (F)						
QX61R 7476	32p (F)						
YF33L 74LS76	28p (F)						
QX62S 7481	£1.75 (E)						
QX85G 7483	50p (E)						
QX63T 7485	77p (E)						
YF35Q 74LS85	70p (E)						
QX64U 7486	28p (F)						
YF36P 74LS86	36p (F)						
QX65V 7489	£3.10 (C)						
QX66W 7490	35p (F)						
YF38R 74LS90	32p (F)						
QX86T 7491	£1.20 (D)						
QX67X 7492	32p (F)						
YF39N 74LS92	36p (F)						
QX68Y 7493	35p (F)						
YF40T 74LS93	36p (F)						
QX69A 7494	39p (F)						
QX70M 7495	48p (F)						
YF41U 74LS95	89p (E)						
QX87U 7496	50p (E)						
QX71N 74LS107	41p (F)						
YF43W 74LS107	53p (E)						
YF44X 74LS109	34p (F)						
YF45Y 74LS112	64p (E)						
YF46A 74LS113	40p (F)						
QX72P 74118	£2.30 (C)						
QX73Q 74121	33p (F)						
WH00A 74LS122	68p (E)						
Q054J 74LS122	72p (E)						

TRADE QUANTITIES

The letter in brackets after the price indicates the minimum quantity of that item you can buy and qualify for a trade price. See table at start of price list. If you buy less than the quantity shown then the price is that shown. If you want to buy the quantity shown or more of that item, then please contact us for a trade price. If no trade quantity is shown, then the price shown is the best price we can offer regardless of the quantity. Trade quantities shown for wires or cables of any type is in metres, not reels or parts of metres. Trade quantities for nuts, bolts, washers, Hiatts etc. refers to the number of packs, i.e. to qualify for a trade price on Tag 2BA for example (trade quantity 500), you will need to order 500 packs which is equal to 5000 tag

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X082D	Fone C1285TC 16R £28 45 (A)	L001B	Profess Morse Key £5 40 (B)
X083E	C15 Bass 8R £57 80 (A)	HY00A	Tooch Pads Rect 22p (G)
X084F	C15 Bass 16R £57 80 (A)	HY01B	Tooch Pads Tri 27p (F)
X828F	Power L/S Cabinet £49 00 (A)	YR88V	Solenoid 12V £4 75 (C)
		YR93W	Solenoid 240V AC £4 85 (C)

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AF33L	Mini Speaker System £45 50 (A)
AF34M	5W Spkr in Cab £9 95 (B)
AF35Q	15W Spkr Pair £33 40 (A)
AF35U	20W Spkr Pair £63 00 (A)
AF32K	PA Spkr in Cab £21 99 (A)
XY79L	Ceiling Speaker £11 75 (A)
YL15R	Bracket Minor 5 £6 50 (B)
YL16S	Bracket Beck 100 £13 90 (A)
YK54J	Wallcamps Duo 220 £15 95 (A)

SWITCHES RELAYS

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FH97F	SPST Ultra Min Toggle 66p (E)
FH98G	SPDT Ultra Min Toggle 69p (E)
FH99H	DPDT Ultra Min Toggle 75p (E)
FF70M	Sub-Min Toggle 80p (E)
FH01B	Sub-Min Toggle B 89p (E)
FH03D	Sub-Min Toggle D £1 06 (E)
FH04E	Sub-Min Toggle E 99p (E)
FH05F	Sub-Min Toggle F £1 29 (D)
FH07H	Sub-Min Toggle H £1 25 (D)
FF72P	4-Pole SPST Toggle £2 35 (C)
FH08J	Toggle Sw 60p (E)
YL01B	Toggle Switch Cover 47p (F)
FH10L	Std Toggle SPST £50p (E)
FH11M	Std Toggle SPDT 57p (E)
FH12N	Std Toggle DPDT 77p (E)
FH13P	10A SPST Toggle £1 15 (D)
BK33L	10A SPDT Toggle £1 15 (D)
FH17T	H/D Toggle Type 4 £4 25 (C)
FH18U	H/D Toggle Type 7 £1 95 (D)
FH19V	H/D Toggle Type 8 £4 40 (C)
FH20W	H/D Toggle Type 9 £4 30 (C)

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FH13P	Duck Bill Toggle 55p (E)
YK53C	Chrome Bar 96p (E)
YK64U	Min Rocker SPST 69p (E)
YK65V	Min Rocker DPDT £1 15 (D)
FH30H	SPST Rocker 39p (F)
FH31J	SPDT Rocker 49p (F)
YR63Y	Rocker Neon 65p (E)
YR69A	Rockers Sw DP 69p (E)
FH34M	DPDT Rocker 98p (E)
YR70M	Dual Rocker Neon £1 10 (D)
BH58M	Co-ax Switch SO239 £66 99 (B)
BH59P	Co-ax Switch PL239 £66 99 (B)
XK26D	DIL Switch SPST Dual £1 20 (D)
XK27E	DIL Switch SPST Octl £1 50 (D)
XK28F	DIL Switch SPST Sgl 95p (E)
XK29G	Rotary SPST Quad £2 95 (E)
F747R	Rotary SW2B 70p (E)
F748S	Rotary SW4 70p (E)
F749T	Rotary SW8 70p (E)
F750U	Rotary SW12 70p (E)
F751V	Rotary SW6 70p (E)
F752W	Rotary SW3 75p (E)
XK45Y	Switchpot 1p 12w 85p (E)

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F83E	Thumbwheel Decmal £4 95 (C)
F84F	Thumbwheel BCD £4 55 (C)
BK49D	End Checks 35p (F)
BK50E	Dial Stops 35p (F)
YR71T	Push Wheel BCD £5 45 (B)
YR72U	Push Wheel End Checks 99p (E)
FH40T	Key Switch £3 60 (B)
FH57M	Rotary Mains 71p (E)
FH95D	Roller Microswitch £1 55 (D)
FH46A	Maka Shaft £1 10 (D)

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FH47B	Maka Water 1p 12w £1 06 (E)
FH48C	Maka Water 2p 6w £1 06 (E)
FH49D	Maka Water 4p 3w £1 10 (D)
FH50E	Maka Water 6p 2w £1 17 (D)
FH52G	Maka Water 1p 12w MB 75p (E)
FH53H	Maka Water 2p 6w MB £1 05 (D)
FH54I	Maka Water 4p 3w MB 79p (E)
FH55K	Maka Screen 5p (H)
FH57U	Click Switch 30p (F)
FH58V	Click Cap Black 18p (G)
FH59W	Click Cap Blue 18p (G)
FH60X	Click Cap Green 18p (G)
FH61Y	Click Cap Grey 18p (G)
FH62Z	Click Cap Ivory 18p (G)
FH63A	Click Cap Red 18p (G)
FH64B	Click Cap White 18p (G)
FH65C	Click Cap Black 18p (G)
FH66D	Click Key Black 24p (F)
FH67E	Keyboard Switch 23p (G)
FH68F	Keypad 1 Position 18p (G)
FH69G	Keypad 2 Position 29p (F)
FH70H	Keypad 3 Position 56p (E)
FH71I	ASCII Transparency 13p (D)
FH72J	Switch Contact Sheet £1 49 (D)

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FF77J	SP Slide 12p (G)
FH35Q	Sub-Min Slide 15p (G)
FF79L	Long Chrome Slide 22p (G)
FH39P	Std Slide Switch 15p (G)
FH38R	4-Pole Slide 15p (G)
FH59P	Push Switch 17p (G)
YR67Q	HQ Push Switch 39p (F)
FH60Q	Break Push 23p (G)
FH61R	Motor-Start Press 43p (F)
FH62S	Lge Red Push Button 49p (E)
FH63T	Square Push Black 77p (E)
FH64U	Square Push Green 77p (E)
FH65V	Square Push Red 77p (E)
FH66W	Square Push Yellow 77p (E)
FH67X	Square Psh Lk Black 75p (E)
YH43W	Square Psh Lk Red 75p (E)
YH44X	Square Psh Lk Yellow 75p (E)

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FH41U	Pushlock SPDO £1 20 (D)
FH42V	Pushlock DPDO £1 45 (D)
FH43W	Press Switch 28p (F)
FH92A	Press Toe Sw Type 1 £1 20 (D)
BK31J	Press Toe SPST 2 £1 39 (D)
FH93B	Press Toe Sw Type 2 £1 95 (D)
FH94C	Foot Switch 15p (G)
FH95D	Mains Push £1 10 (D)
LB91Y	Flasher Unit 2-Way £5 75 (B)
LQ00A	Beginners Morse Key £1 90 (D)

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L001B	Profess Morse Key £5 40 (B)	LH06B	Clamp Meter £26 90 (A)
HY00A	Tooch Pads Rect 22p (G)	YK36P	Low Cost DMM £29 95 (A)
HY01B	Tooch Pads Tri 27p (F)	YK32K	Multimeter DD601 £39 95 (A)
YR88V	Solenoid 12V £4 75 (C)		
YR93W	Solenoid 240V AC £4 85 (C)		

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FH67X	Latchswitch 2 pole 46p (F)
FH68Y	Latchswitch 4 pole 52p (F)
FH69A	Latchswitch 6 pole 59p (E)
FH70M	Latchswitch 8 pole £1 45 (D)
FH71N	Latchswitch 10 pole £1 25 (D)
BW11M	Latchsoft 2 pole 60p (E)
BW12N	Latchsoft 4 pole £1 20 (D)
FH72P	Latchswitch 6-way 32p (F)
FH74R	Mains Latchswitch £1 59 (D)
FH75S	Latchbracket Single 13p (F)
FH76H	Latchbracket 2-way 38p (F)
FH77I	Latchbracket 4-way 45p (F)
FH78J	Latchbracket 6-way 52p (F)
FH79K	Latchbracket 8-way 64p (E)
FH80L	Latchbracket 10-way 69p (E)

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FL31J	Rd Latchbutton Black 14p (G)
FL32K	Rd Latchbutton Green 14p (G)
FL33L	Rd Latchbutton Grey 14p (G)
FL34M	Rd Latchbutton Red 14p (G)
FL36P	Rd Latchbutton Chrm 22p (G)
BW13P	Sm Latchbutton Black 11p (G)
BW14Q	Sm Latchbutton Chrm 33p (F)
FH61R	Rct Latchbutton Bk 14p (G)
FH62S	Rct Latchbutton Grey 14p (G)
FH63T	Rct Latchbutton Red 14p (G)
FH64U	Rct Latchbutton White 14p (G)
FH65V	Magiclatch Bttm Bk 23p (G)
FH66W	Magiclatch Bttm Org 42p (F)
FH67X	Magiclatch Bttm Ylw 49p (F)
BW15R	Latchbutton Blue 35p (F)
BW16S	Latchbutton Green 45p (F)
BW17T	Latchbutton Orange 45p (F)
BW18U	Latchbutton Yellow 39p (F)

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BK47B	Micro-Min Relay 60p (E)
YK53C	Ultra-Min Relay SPDT £1 95 (E)
YK54D	Ultra-Min Relay DPDT £1 49 (D)
BK48C	Ultra Min Ry 6V DPDT 95p (E)
YK59E	3A Min Relay 99p (E)
YK59F	10A Mains Relay £1 65 (D)

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YK59G	5A Mains Relay £3 20 (C)
YK59H	12V 30A Relay £2 15 (C)
YK59I	Open Relay 12V £3 25 (C)
FX24B	Open Relay 12V £3 88 (C)
FX26D	2p Sub-Min Relay 6V £3 45 (C)
FX27E	2p Sub-Min Relay 12V £3 45 (C)
FX30H	4p Sub-Min Relay 12V £3 99 (C)

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FX48C	Power Relay 12V £3 95 (C)
FX49D	Power Relay 230V AC £4 25 (C)
YH20W	Relay Flat 12V £2 40 (C)
FX50E	Relay Flat 6 to 3V £1 98 (D)
FX51F	Reed Relay 9 to 12V £2 15 (C)
FX58V	Di Reed Relay 1p 5V £1 95 (D)
FX59W	Di Reed Relay 1p 12V £2 15 (C)
FX60X	Di Reed Relay 2p 5V £3 95 (C)
FX61Y	Di Reed Relay 2p 12V £3 95 (C)
FX93B	Di Reed Rly 1p C/012V £7 60 (B)
FX68Y	Reed SW Compact 89p (E)
FX69A	Reed SW Standard £1 75 (D)
FX70M	Reed SW Miniature 69p (E)
FX71N	Magnet Small 38p (F)
FX72P	Magnet Large 88p (E)

TEST GEAR

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FH19V	Test Prod Black 45p (F)
FH20W	Test Prod Red 45p (F)
FH51X	Probe Clips 98p (E)
YK57M	Probe Black 42p (F)
YK58N	Probe Blue 38p (F)
YK59P	Min Probe Green 42p (F)
YK60Q	Min Probe Red 42p (F)
YK61R	Min Probe Yellow 42p (F)
FH30H	Pistol Probe Black 99p (E)
FH31I	Pistol Probe Red 99p (E)
FH22Y	Lc-Cost Test Probe 74p (E)
FH32K	Moulded Test Probe 79p (E)
FH33L	4mm T 89p (E)
FH93B	Test Lead Kit £2 75 (C)
FY73Q	Logic Probe £9 50 (B)
FY88V	Continuity Probe 99p (E)

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FL61R	Signal Injector £5 99 (B)
FY74R	IC Test Clip £2 35 (C)
YK60Q	Scope Probe BNC £1 93 (A)
YK61R	Lc-Cost Scope Probe £3 75 (C)
XB82D	Single Beam Scope £167 90 (A)
	Carr in UK with XB82 £8 45

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XB83E	Dual Beam Scope £286 00 (A)
	Carr in UK with XB83 £9 45 (B)
YK38R	Low-Cost Counter £49 90 (A)
LH05F	Transistor Test HFE £15 20 (A)
YB82D	LCR Bridge £25 30 (A)

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YB81C	Seasure Sig Gen £26 75 (A)
YK40T	Seasure CMOS Tester £34 95 (A)
YW93B	Low Cost Multimeter £4 85 (C)
FL60Q	Pocket Multimeter £7 50 (B)
YB83E	Small Multimeter £15 95 (A)

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YK35Q	Multimeter 2050 £11 95 (A)
YK37S	Ultra Dibr Multimeter £19 95 (A)
YW66Y	Multimeter Type 320 £16 25 (A)
LH93B	Tact-Band Multimeter £23 95 (A)
YB87U	100K Multitester £44 00 (A)

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YB84F	Microtest 80 £19 09
YB85G	Supertester 6800 £28 96
YB86T	Supertester 6800 £37 80

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LH06B	Clamp Meter £26 90 (A)	FY53H	Mini Vice £3 85 (C)
YK36P	Low Cost DMM £29 95 (A)	LH79L	Reliant Kit £21 95 (A)
YK32K	Multimeter DD601 £39 95 (A)	BW03D	Reliant Drill £7 60 (B)
		BW02C	Titan Drill £11 25 (A)

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YK34M	Auto Range Meter £54 50 (A)
LH95D	DMM 100 £68 61 (A)
YK01F	Rf Frequency Meter £69 95 (A)
YB04E	Grid Dip Meter £45 00 (A)

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XY75S	Ham Multimeter £31 95 (A)
WY18U	SWR Meter 310 £10 75 (A)
WY19V	SWR Meter 200 £12 95 (A)
WY21X	SWR Meter 178 £24 95 (A)

TOOLS	
Page 368	
LH15Y	Hobby Box £3 45 (C)
FR25R	Storage Drawer 98p (E)
BR48C	Hex Trimmer 24p (F)
BR51F	Trim Tool 45p (F)
BR52D	Presd Trimmer 72p (E)
BR50E	Trim TTS 60p (E)
BK34M	Trim Tool Set £1 25 (D)
FY07H	Min Screwdriver Set 85p (E)
BR58N	Jewellers Screwdriver £2 30 (C)
BK44X	Pce S/Driver Set £6 45 (B)

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BR79L	Intrchbl Scrvr Set £1 69 (D)
YH92A	Ratchet Socket Set £5 99 (B)
YH93B	Utility Set £4 49 (C)
YK74R	Min Screwdriver 10p (G)
BR52G	Small Screwdriver 34p (F)
BR53H	Large Screwdriver 36p (F)
YH94T	Driver 20p (F)
FY12N	Driver S5 89p (E)
FY13P	Driver S6 63p (E)
BK35Q	Driver S7 £1 25 (D)
BK36P	Driver S8 £2 25 (C)
FY20W	Podzidrvr P1 £1 49 (D)
FY17T	Podzidrvr P2 99p (E)
BK37S	Podzidrvr 3 £1 15 (D)
BK38R	Podzidrvr 4 £2 25 (C)
BR71N	Mains Tester 60p (E)

Page 370	
LH75S	Spiraldriver £4 25 (C)
FY20W	Box JT End Cutter £6 95 (E)
WY04E	Cushioning Dvr Set £5 84 (B)
FY19V	Low Cost Min Cutters £4 25 (C)
BR75S	Ins Min Cutters £6 93 (B)
BK42W	Slant Edge Cutters £6 75 (B)
FY21X	Box Combined Pliers £3 99 (C)
FY21Y	Low-Cost Cutters £2 25 (C)
FY76H	Large Low Cost Cutts £3 75 (E)
FR74R	Box Cutters £5 95 (E)
FR72Y	Box J Side Cutters £7 60 (B)
FR73Z	Side Cutters S55 £4 50 (D)
WY67X	Twizers 19p (G)

Page 371	
BK43W	Pearl Catcher £1 75 (D)
FY20W	Low Cost Min Pliers £3 90 (C)
BR78K	Ins Min Snipe £5 72 (B)
BK41U	Hooked Pliers £6 75 (B)
BR77J	Bright Pliers £4 39 (C)
FY20W	Low Cost Pliers £3 99 (C)
FY26D	Box Combined Pliers £3 99 (C)
FR73Q	Long Snipe Pliers £7 49 (B)
BR90X	Box Radio Pliers £

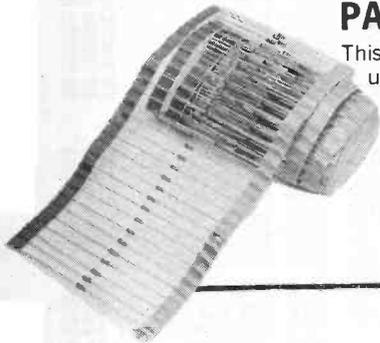
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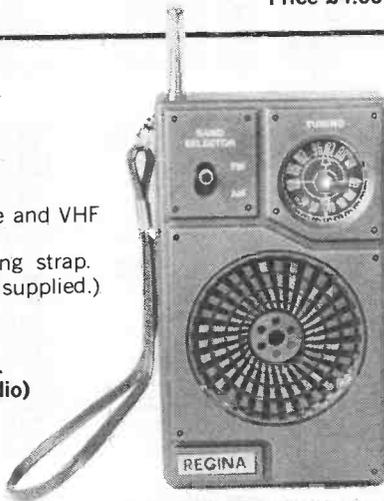
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Price £3.95



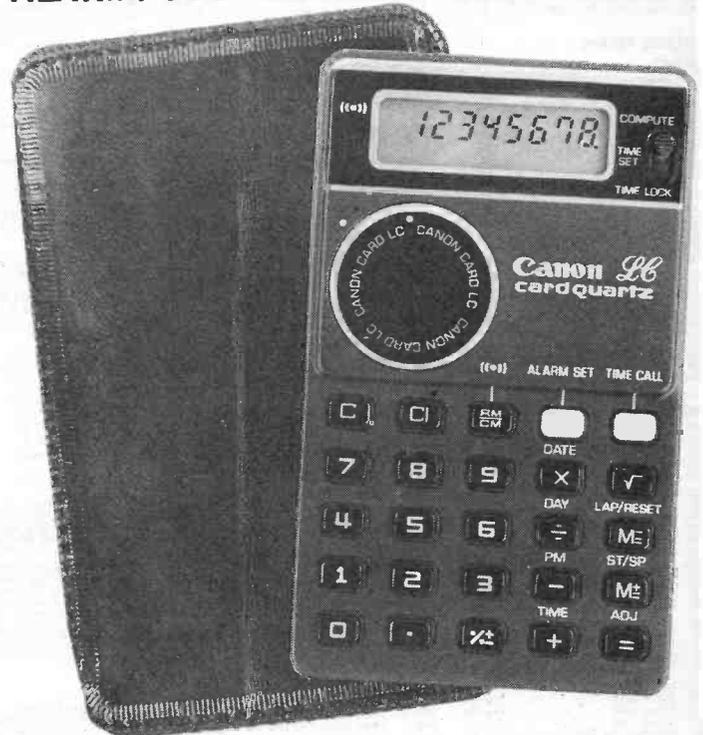
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CANON ULTRA-SLIM TIME/DATE/ALARM/STOPWATCH CALCULATOR



A special end-of-catalogue offer that is strictly while stocks last!

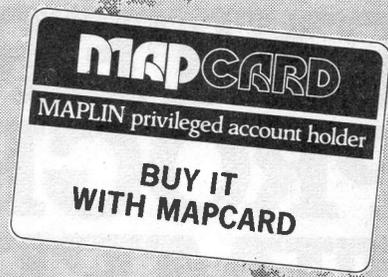
An ultra-slim 8-digit calculator with memory that also incorporates a quartz-crystal and functions: as a clock with hours, minutes, day and date displayed; as an alarm clock which beeps discreetly when a preset time is reached and as a stopwatch with hours, minutes, seconds and tenths of seconds displayed. It will fit easily into an inside pocket or handbag as it is less than 1/16 in. thick. The device has a liquid crystal display and battery life will be about one year. The day, date, time display is normally operating continuously and after use as a calculator, if not returned to clock mode manually, it will return automatically after 10 to 20 minutes.

Specification

- Timepiece
- Quartz crystal frequency: 30, 720Hz
- Accuracy: Better than ±30 seconds per month (at 25°C)
- Display: Date, day of week, hours, minutes, flashing seconds indicator, AM/PM.
- Alarm: Electronic beep signal. Display shows when alarm is set.
- Stopwatch
- Measuring unit: 1/10 second
- Measuring range: To 9 hours, 59 minutes, 59.9 seconds
- Types of measurement: Standard; Lap time displayed while count continues; Stop count and restart; Two sets of times with simultaneous start.
- Calculator and General Display: 8-digit liquid crystal with minus, overflow and memory signs.
- Types of calculation: Addition, subtraction, multiplication, division, percentages, square roots, chain multiplication and division, constants, powers, add-on and discount calculations, sum and difference of products and quotients, calculations requiring memory.
- Power source: One lithium battery (LF1/2V) (3V DC 0.6mW)
- Battery life: 1 year (with intermittent calculator use)
- Size: 94 x 56 x 2.9mm
- Weight: 36gms (including battery)

Supplied complete with batteries, wallet and instruction booklet.
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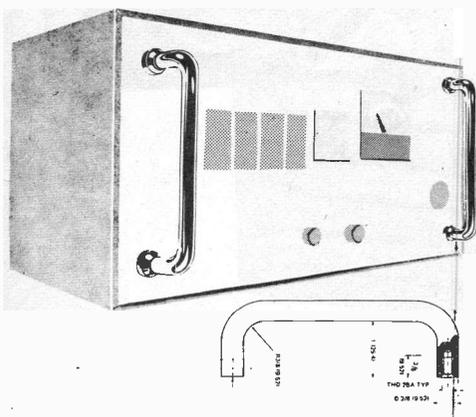
MAPLIN NEWS



THE ONE'S THAT GOT AWAY

We regret that the following items were inadvertently omitted from the 1983 Maplin catalogue. They appeared in the 1981/2 edition, and will be reinstated in 1984. Prices can be found in our current price list under the relevant section heading. We apologise for any inconvenience that this causes.

INSTRUMENT CASE HANDLE



Mild steel handles fine chromed (on nickel on copper). Two sizes available: Fixing hole centres 3 3/4 in. (95.2mm, SMALL) or 6 in. (152.4mm LARGE).

Order As FX00A (inst Handle Small)
FX01B (Inst Handle Large)

FERRULE



A chrome plated brass ferrule is also available to suit INST. HANDLE.

Order As FX02C (Ferrule)

CIGARETTE LIGHTER EXTENSION LEAD



An extension lead with plug at one end to fit the cigarette lighter socket in a car and socket at other end to accept cigarette lighter plug. Approx. 1.7m of lead.

Order As YB68Y (Car Lighter Ext. Lead)

GUITAR STRINGS



A set of replacement steel guitar strings for electric and acoustic guitars, round wound. Pack contains an extra 1st and 2nd string (total 8 strings).

Order As LB60Q (Guitar Strings Steel)

December 1982 Maplin Magazine

INTEREST FREE CREDIT EXTENDED (APR = 0%)

Following the incredible success of our Interest Free Credit scheme in its first months of operation, we are pleased to announce its indefinite extension.

So if you have an order containing over £120 of computer hardware, then buy it on credit — interest free. Here's how it works.

In our shops

1. Phone the branch of your choice and give them your order (must include at least £120 worth of computer hardware). We will also have to ask you some personal financial questions in order to fill up our credit application form.
2. We will phone you back within 48 hours to let you know whether your application has been approved.
3. Any time after this, you may visit the shop to collect the goods. You must bring with you some form of identification (e.g. driving licence, credit card) and sign the form that we filled in on your behalf. A deposit of 10% will be required.
4. A further 10% will be payable every month for a further 9 months equalling the total cash price for the goods.

By mail-order

1. Send your order to us (which must include at least £120 worth of computer hardware) and mark clearly on it "Interest Free Credit Terms". Enclose 10% of the value of the goods with your order.
2. We will send you by return of post, a credit application form.
3. Complete the form and post it in the stamped addressed envelope supplied.
4. When approved we immediately despatch your goods to you.
5. One month after goods despatched the

first 10% payment becomes due, and thereafter a further 10% is due monthly for a further 8 months, equalling the total cash price for the goods.

Example

A VIC20 computer could be yours for just £16.99 down and £17 per month for nine months.

Interest free credit terms are only available in the U.K., not in Northern Ireland, Isle of Man and Channel Islands.

OUR COMPUTER WOULD LIKE TO TALK TO YOU

We hope to launch a brand new service in early 1983, allowing you, through your Modem, to talk directly to the Maplin computer. You will be able to access our stock file to check stock levels, then place your order, using any of the credit cards that we accept to pay for it. A few seconds later your order will be printed out, then collected and posted to you.

However, until we can make this available, you will still be able to call our computer on 0702 552941, and a message on our computer will tell you if your Modem is working correctly. If our computer is not operational, you will hear only a ringing tone. This part of the service will be ready for use in late November.

CORRIGENDA

ISSUE 1

Page 4. On Combo RCB overlay D6 above R67 should read D4.

Page 6. Fig. 8, Dimns. given for 'B' holes on Front View are incorrect, mount PCB in 'A' holes and drill through fixing holes for correct positions.

ISSUE 3

Page 3. Fig. 2, SK2 Pin numbers are incorrect, from left to right they should read 1, 2, 4, 6, 8, 7, 5, 3. Note the PCB is correct.

ISSUE 4

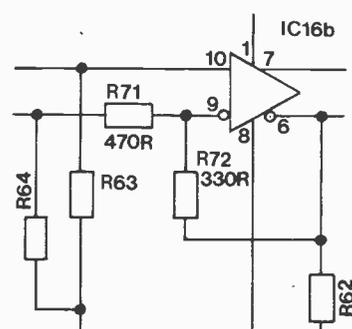
Page 5. Digi-tel Motherboard cct. There are 4 Diodes shown below R1 to 11 without cct references, their designations are D31 to 34, working from top to bottom; Pin 15 on Skts 1-4 goes to IC's 7, 8, 9 & 10 Pin 2 not 15 as shown; Veropin 48 should be connected to collector of TR2 not to IC4 Pin 10; Veropin 55 has been omitted and joins to IC19 Pin 11.

Page 41. Frequency Counter: Fig. 2, R47 value is 10M.

Page 42. Fig. 3, on IC7 Pin 10 goes to D13.

Page 43. Fig. 6, R65 value is 1k; R71 & R72

have been added thus:—



Page 44. Fig. 7, for better performance IC14 has been changed to SP8680, but please note that the circuit and PCB require no modifications, the order code (QY18U) is also unchanged. Some early kits may still contain the 11C90, however.

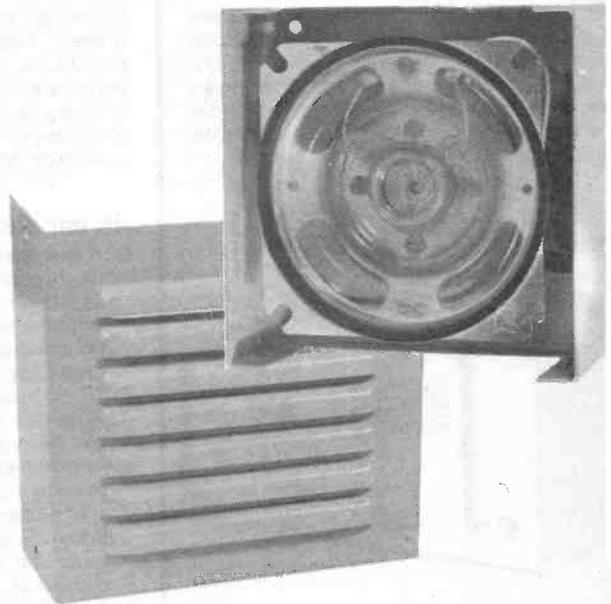
Page 45. Main Parts List: Add R71 to 470R (Qty 8), Add R65 to 1k (Qty 9), Delete R47 from 1M (Qty 1), Delete R65 from 47k (Qty 1), Add R47 value 10M, Add R72 value 330R; Diode 1N4148 Qty should be 24.

Page 57. ZX81 I/O Port: Fig. 1, IC1 Pin 9 goes to A10.

EXTERNAL HORN PROGRAMMABLE TIMER

by Dave Goodman

- ★ Three timing settings from 2 minutes to 2½ hours
- ★ Switch over from sounder to flashing beacon when time is up
- ★ Directly replaces the previous external horn PCB
- ★ Two wire control with tampering detection



New recommendations concerning the use of burglar alarm sounders have recently been introduced, and apply only to sirens or bells fitted outside protected premises, not to those used internally, unless they are likely to be audible outside. The ruling comes under the noise pollution title, and requires that alarm sound indicators cease to function after a seventeen minute running period from switch-on. Presumably the alarm would, or should, have been raised within this time, and the appropriate authorities notified, making further ear-blasting and nerve-shattering decibels unnecessary. So that it is not forgotten that the alarm system has been activated a

flashing lamp or beacon can be switched on which will flash away until reset. Perhaps eye pollution will become a problem in the future!

Specification

A timer project has been designed for use with the Home Security System (see March issue) which will directly replace the previous External Horn PCB. Any type of siren, bell, or sounder requiring 12V at no more than 1A DC can be used, and in addition a lamp or beacon rated at 12V and less than 1A DC can be switched on after a preset time-out period has elapsed. One of three timing periods (see table 1) ranging from 2 minutes to 2½ hours can

be programmed by removing or adding two wire links as required.

A 12V battery supply is needed to power this system, and batteries, siren, and PCB will all fit into an external horn cabinet. Unfortunately, this PCB is larger than the previous one, and the mounting holes in the cabinet lid will not align with it, so a further two 6BA holes are required. The lamp may be fitted to the cabinet, or wherever it will be readily visible.

Circuit Description

R1 terminates a two wire loop connection from the mother board in the main alarm. Removal of R1 from the circuit, either by shorting or open

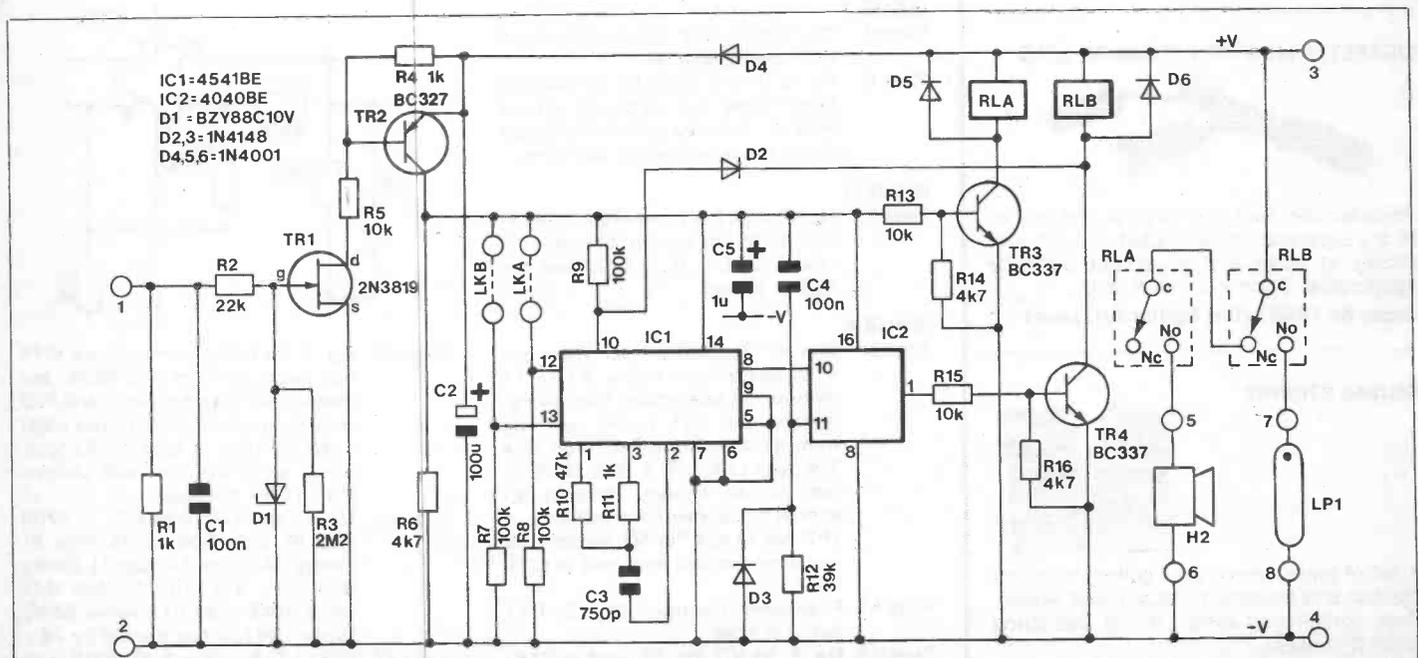


Figure 1. Circuit diagram.

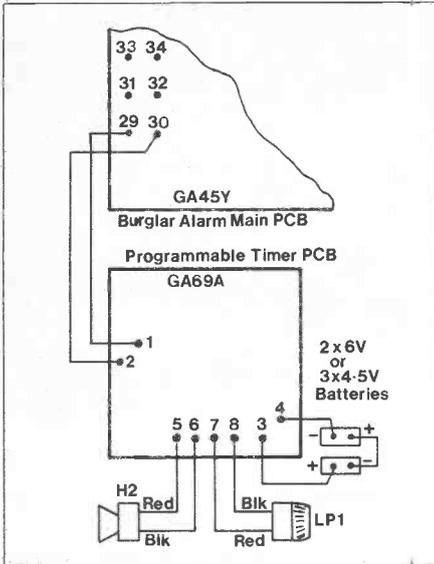


Figure 2. PCB layout and overlay.

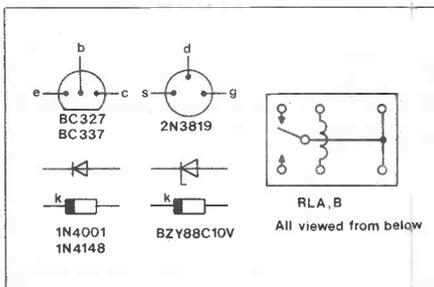
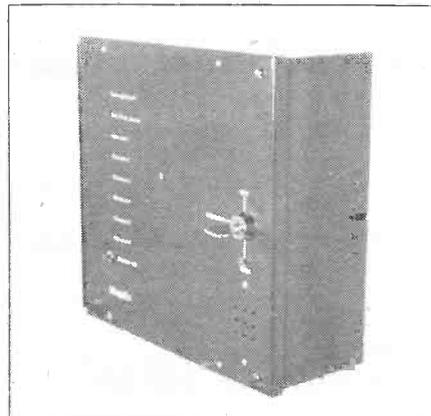
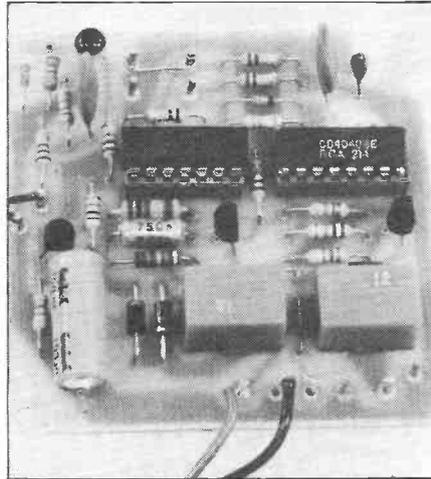


Figure 3. Wiring to main burglar alarm PCB.

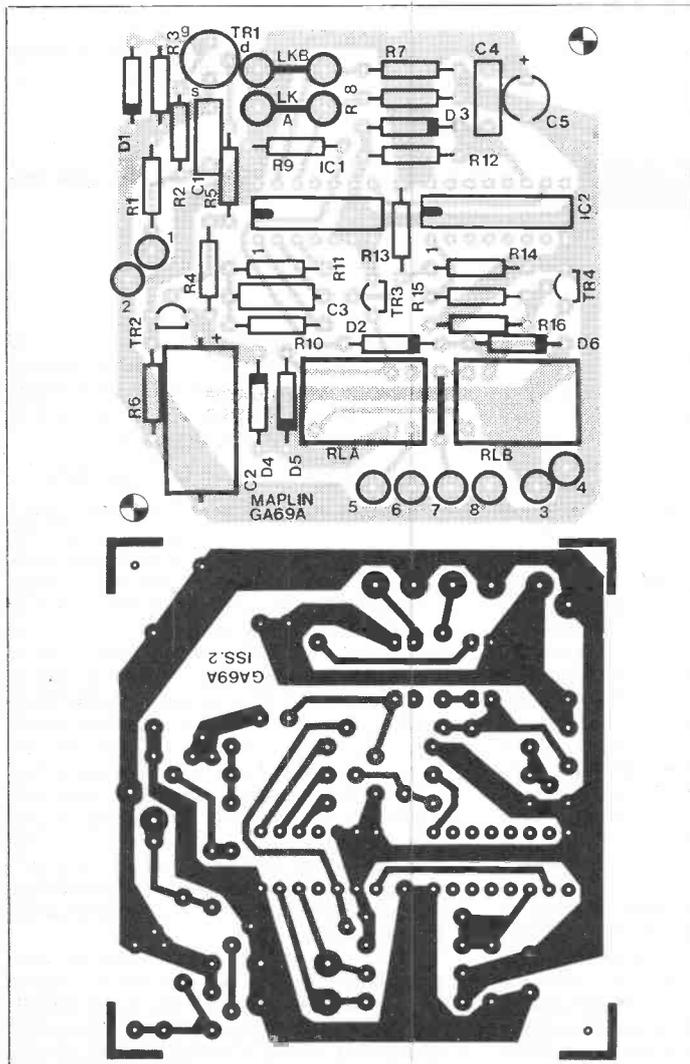


circuiting the loop, will trigger the main alarm (described in the March issue). TR1 is an N-type J-FET device, and requires a negative potential between gate and source to prevent drain current flow. With Pin 1 or 2 disconnected, R3 holds TR1 gate to ground, allowing drain current to flow.

C1, R2 and D1 help prevent RF and voltage spikes, that may be introduced along the length of connecting cable used, false triggering the timer. Now, with TR1 conducting, the voltage drop across R4 and R5 is sufficient to allow TR2 to conduct, and connect the battery positive rail, via D4, to the supply rail. R13 monitors the positive supply rail, and TR3 immediately conducts, switching RLA, and allowing the siren connected between pins 5 and 6 to operate for a period of time (generated by IC1 and 2).

IC1 is a programmable timer, with an internal clock and four dividing stages. Clock frequency is set by R10, R11 and C3 to 16.5kHz, which is divided down by one of three stages set by links from the positive rail to pins 12 and 13 (Table 1). The Q output at pin 8 requires further dividing, and is applied to a 12 stage ripple counter, IC2. C4 and R12 apply a reset pulse to IC2, ensuring that all twelve dividing stages will

Continued on page 43



PROGRAMMABLE TIMER PARTS LIST

Resistors - All 0.4W 1% metal film unless specified.

R1, 4, 11	1k	3 off	(M1K)
R2	22k		(M22K)
R3	2M2		(M2M2)
R5, 13, 15	10k	3 off	(M10K)
R6, 14, 16	4k7	3 off	(M4K7)
R7, 8, 9	100k	3 off	(M100K)
R10	47k		(M47K)
R12	39k		(M39K)

Capacitors			
C1, 4	100nF Disc Ceramic	2 off	(B*03D)
C2	100uF 25V axial electrolytic		(FB49D)
C3	750pF 1% polystyrene		(BX55K)
C5	1uF 35V Tantalum		(WW60Q)

Semiconductors			
D1	BZY88C10V		(QH14Q)
D2, 3	1N4148	2 off	(QL80B)
D4, 5, 6	1N4001	3 off	(QL73Q)
TR1	2N3819		(QR36P)
TR2	BC327		(QB66W)
TR3, 4	BC337	2 off	(QB68Y)
IC1	4541BE		(QQ47B)
IC2	4040BE		(QW27E)

Miscellaneous			
RLA, B	Ultra-min relay SPDT	2 off	(YX94C)
	Veropin 2141	1 Pkt	(FL21X)
	14 pin DIL skt		(BL18U)
	16 pin DIL skt		(BL19V)
	Programmable timer P.C.B.		(GA69A)
LP1	12V 50mA Beacon		(YK39N)

Printed below are the parts needed for the External Horn Case. (If required):

H2	Electronic siren		(XG14Q)
B1, 2	6V lantern battery	2 off	
	Case		(XG07H)
	Grommet Small		(FW59P)
	No. 6 self-tapping screws x 1/8"	10 off	(BF67X)
	Bolt 6BA x 1/4" (for P.C.B.)	2 off	(BF06G)
	Washer 6BA	4 off	(BF22Y)
	Nut 6BA	4 off	(BF18U)
	Spacer 6BA x 1/4"	2 off	(FW34M)
	Bolt 6BA x 1/4" (for Siren)	2 off	(BF05F)
	Wire to suit		

A kit of parts is available for this project. It does not include the Beacon which must be ordered separately if required, nor does it include any of the parts listed below.

Order As LW98G (Programmable Timer Kit) Price £6.95

WIRES AND WHEREFORES

by Christopher Roper

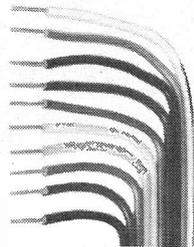
On first sight, a casual glance through the local electronic retailers catalogue usually reveals a bewildering assortment of wires and cables which are available to the amateur enthusiast. With such a wide choice, difficulty may be experienced in choosing the right wire for the job in hand, but armed with a few facts it is relatively simple to decide on the appropriate cable. Having said this it should be borne in mind that the average length of wire is itself something of a technological feat; as I hope this article will show.

Cables and wires usually fall into one of several groups, dictated by their usage; e.g. power cables, signal cables etc, although there is often some overlapping between groups. Consider cables in general. Looking through the appropriate catalogue pages usually reveals several descriptive facts and figures relating to number of strands per core, current ratings, voltage ratings and, in the case of screened cables and some multicore cables, a figure for capacitance is usually given. The figure quoted for the number of strands is given in two parts, e.g. 7/0.2 or 16/0.2. The first number gives the number of strands within the core and the second number gives the diameter of each strand in millimeters. Therefore a wire which is listed as being 7/0.2, has seven strands each of which has a diameter of 0.2mm.

The maximum voltage rating is the maximum potential that can be applied across the conductor's insulation without it breaking down due to electrical stress. For obvious reasons this rating should not be exceeded. The current rating is the maximum current that the conductor should be allowed to carry, but although this should never be exceeded it is often necessary to derate this value under certain conditions. The factors which determine the current capacity of a conductor, apart from its cross sectional area and the type of insulation surrounding it, are its proximity to other current carrying conductors, the ambient air temperature and the type of equipment that it is built into.

The amount of heat generated by current flowing in the conductor, should not be allowed to exceed the temperature rating of the insulation and as the number of individually insulated conductors which are loomed together, is increased, the heat dissipation is decreased. Further restriction of the cables, such as within an enclosed chassis, will further lower the heat dissipation.

When dealing with the above situations it is often necessary to have some form of guide as to the amount by which the current capacity of the cables should be derated. For example, a loom consisting of thirty or more individual conductors may need to have the current rating of each conductor derated by as much as 50%. These considerations can become important when dealing with projects such as hi fi amplifiers and the like, which draw appreciable amounts of current.



Ribbon cable with end fanned-out (XR06G).



Multi-strand single core wire 7/02 (BL00A).



Heavy-duty mains cable 3-core (XR10L).



Cotton-covered rubber mains cable 3-core (XR24B).



Single-core audio screened cable (XR15R).



High-frequency co-axial cable (XR19V).

Screened Cables

Current flowing in a wire can cause other problems, apart from those already mentioned. Consider for example, screened cables. These are usually used when outside interference sources can be troublesome. The cable screen is usually connected to zero volts or ground and helps to minimise interference induced signals, as well as helping to contain the transmitted signal. Capacitive effects within screened cables dictate to some extent their usage. The inner insulation of the cable acts as the dielectric of a capacitor, with the screen and the inner conductor acting as the capacitor plates. The capacitive effects which are produced can result in a finite time delay being imposed on the transmitted signal. In general terms a cable with a lower capacitance is more suitable for audio and radio frequencies; bearing in mind that the measure of capacitance in both cases is in pico farads i.e. 100-300pf/m.

Capacitive effects can also cause problems between two individually insulated conductors, which are in close proximity, when one or both are carrying alternating currents; under certain circumstances it is possible for signals being carried in one lead to become superimposed on those being carried in the other lead. The use of screened cables in this situation will help to

minimise the effect, although this is not always the answer, especially when dealing with power supply leads. In this case it is best to avoid running power supply cables and signal leads within the same loom.

High Frequency Cables

Certain conductors are designed specifically to carry very high frequencies. On first sight it might seem that a conductor with virtually zero resistance will carry high frequency signals as efficiently as it will carry low frequency signals, but this is not the case. The effective resistance of a conductor increases with frequency, and at high frequencies its resistance may be many times greater than its low frequency resistance. As the signal frequency increases, the signal current tends to flow more within the surface layers of the conductor and less within its central core, giving rise to the phenomenon known as 'skin effect'. The explanation for skin effect is fairly straightforward, when one considers the effect on a conductor which is within its own associated magnetic field.

A current flowing in a conductor produces lines of magnetic flux which actually exist within the conductor itself and there is a greater concentration of flux lines nearer the centre of the conductor than at the surface layers. From this it follows that in a multi strand conductor, the individual con-

ductor nearest the centre of the bundle has induced within it a greater back e.m.f. (electromotive force) than one nearer the outside. This greater induced e.m.f. results in a greater inductive reactance which is effectively an increase in its resistance. At low frequencies this inductive reactance is negligible, but at much higher frequencies it can become troublesome.

The most commonly used cable for high frequency work, i.e. VHF and UHF is Co-ax. This is similar to the screened cables usually with a centre stranded section of copper wires in a polythene insulation covered with a braided screen. However, the spacing between the core and screen is accurately defined which produces capacitances usually around 50-60 pF/m, i.e. much less than screened cables and also maintains a more consistent impedance level.

A less common method of overcoming high frequency problems is to plate the conductor with silver. The silver has a lower resistance than the copper, which offsets the increase in the relative resistance of the conductor as the signal frequency increases. As the frequency rises, more and more of the current will flow in the silver so that the resistance remains fairly constant over a wide range of frequencies.

For specific purposes where a large number of conductors are required all carrying high frequency signals. Litz wire (Litzendraht) can be used. This type of cable has individually insulated strands which are wound around its neighbours in such a way that each occupies the centre of the bundle in succession. This type of wire comprises 3, 9 or 27 strands which are all plaited together in this manner.

Which Wire?

The majority of cables and wires that are available, are based on perhaps half a dozen different designs. At the bottom of the table are the relatively simple single cored, multi-strand conductors such as 10/0.1mm and 7/0.2mm, which, for their respective sizes, have useful current carrying capacities. They are ideal for most projects and as general hook-up wire.

Ribbon Cable

A logical development of this type of wire is ribbon cable. Ribbon cable is usually comprised of ten or twenty individually insulated and colour coded conductors which are bound together lengthways so as to form a ribbon of cable. It may be split into any number of ways and any single conductor may be branched off at any point. It is useful where space is limited as it lies flat against any chassis. Some types of ribbon cable are designed so as to be fitted with multipin plugs which fit neatly into standard IC sockets. This is useful for compact interconnections between circuit boards.

A further development of ribbon cable is interboard jumper cable. This is similar to ribbon cable but is designed specifically for interconnecting circuit boards.

For low to medium power applications, 16/0.2mm is a good general sized wire with a current carrying capacity of about 3 amps. This, alongside with 7/0.2mm is a useful choice for the amateur workbench. For myself, these two wire sizes form the bulk of my stock and although the amount on the wire rack is dependant on the types of projects being built, it is useful to have several metres of each colour.

Screened

There are many types of screened cable, ranging from single cored to multi-cored, and from single screened to multi-screened. As mentioned before capacitive problems with these types of cables, tends to make the appropriate choice more difficult. As a general guide for the spares box, a few metres each of single core, twin cored and four core should be useful; but this will obviously depend again on the individual requirements.

Mains Cables

The choice of cable suitable for making external mains connections to equipment is one that requires special attention. Whilst overloading the internal wiring of equipment may lead to the rapid demise of its component parts in a puff of smoke, overloading a mains cable can have consequences which cannot be overstressed. The wires and cables already mentioned should never be connected to the mains directly; with the possible exception of 16/0.2mm in certain cases, and then only within the equipment itself. To comply with British Standards mains cables must have two separate insulation layers.

Apart from acting as an insulator, it must be capable of withstanding a certain amount of general abuse, and in many cases, the equipment that the cable is fitted to, has a bearing on the type of insulation that is used. For most applications PVC or rubber insulated mains cable of suitable current rating, is probably sufficient, but where there is a possibility of accidental contact with hot appliances, e.g. irons, toasters, fires, etc., it is advisable to use one of the cotton covered heat resistant type.

EXTERNAL HORN PROGRAMMABLE TIMER

Continued from page 41

function, and a positive-going output at pin 1 operates TR4 and relay RLB.

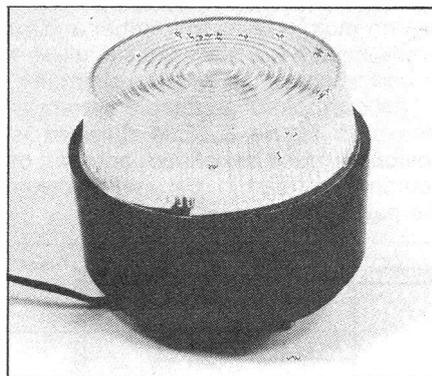
The timing sequence must now be inhibited in this mode, otherwise RLB will switch off and on after each timeout period, and D4 stops this by preventing IC1 pin 8 from changing state. RLB contacts, changing over, will remove the battery supply from the siren and reconnect it to pin 7, hence the beacon will flash until the control loop is restored, either by resetting the main burglar alarm, or by the batteries running down.

Time Period	Link
2 mins	Link B
2hrs 30mins	Links A & B
17 mins	No Links

Table 1: Program Table

Assembly

Refer to figure 2 and the parts list for building this project. You may commence construction by bending and inserting resistors R1 to 16 and diodes D1 to 6. Note that D1 is a zener diode, and different from the others. Fit capacitors C1 to 5, you will see that C2 and C5 are polarised, and must be fitted the correct way round. Finally, fit transistors TR1 to 4, and relays RLA and B, both IC holders, and all the Vero pins. Solder all the components into place,



clean, and inspect the track for shorts and dry joints. When you are completely satisfied with your handiwork, proceed with testing before putting into use.

Testing

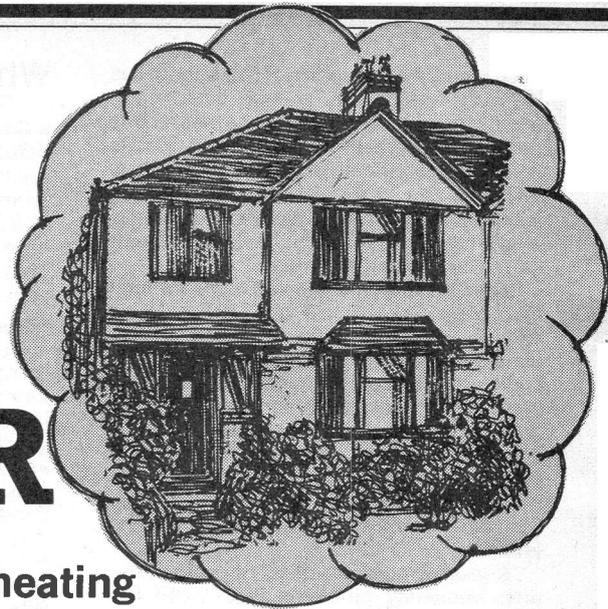
Preliminary checks can be made with a meter set to resistance range. Measure between pins 3 and 4 (supply rails), there should not be a shortcircuit here. Measure between one of the supply rail pins of LKA or LKB and pin 4, again there should not be a short circuit. Wire the PCB to the burglar alarm as shown in figure 3, and connect to a suitable 12V battery supply. Two 6V lantern type or three 4.5V batteries are recommended for use with the project, because quite high currents can be drawn by bells or sirens.

The beacon listed in the parts list gives a very bright flash once a second, but only draws 50mA, so battery life is extended. It is not necessary to make connection to a siren or lamp at this stage, as both RLA and B give an audible click when operated. Remove the wire from pin 1 and you should hear RLA click on. If you have placed a link in LKB you will have to wait two minutes before RLB clicks on. The next step is to connect both siren and lamp to repeat the tests after remaking the connection to pin 1. Ensure correct polarity of the four connecting wires, red is positive and black negative (figure 3). The system is now ready for use.

Usage

Fit the timer PCB into your external horn cabinet. If you already have an external horn PCB it must now be discarded as this new system completely replaces the old unit. Two new holes are needed, but the existing spacers, nuts, and bolts can be used for mounting. If you do not possess our external horn cabinet, see parts list for details. Connect the batteries and siren, you will need a length of two-wire cable for connection to the lamp if fitted externally. Connect up to the Burglar Alarm and the system is complete.

DIGITAL CENTRAL HEATING CONTROLLER



- ★ Works with either gas or oil-fired central heating
- ★ Designed to work reliably and without adjustment over long periods of time
- ★ Eliminates wasteful standing losses within the boiler
- ★ Saves you money

by Chris Bearman

Ever rising fuel costs are tending to make most of us seek ways in which to reduce our energy consumption, particularly in the home. Many firms offer us their wares with the promise of lower fuel bills in the future, usually these take the form of some type of insulation, be it draught exclusion, wall and loft insulation or double glazing. One area which has its fair share of economy suggestions is the central heating system. At present there are thermostatic radiator valves, and zone control valves to name but two.

The digital central heating controller was designed with two basic views in mind. First, to help to make the system more economical, and second, to make the controls more convenient to operate. The controller was designed

around a basic gas fired central heating system, but it could work just as well with an oil fired boiler. The controller directly activates two motor valves, a pump and a boiler. The 'primary' water route through the boiler should be pumped to allow the controller to operate correctly. Some types of heating system use what is called a 'gravity primary' which does not require a pump to heat the water in the hot water cylinder. This type of system probably has no motor valves in it either and so would need a few alterations to allow it to work successfully with the controller.

An example of a suitable system is shown in Figure 1. This diagram is obviously much simplified, and can of course be altered in many ways to suit the particular application.

Circuit description

It can be seen from the circuits (Figures 2, 3 and 4) that there are two sets of control buttons. One set is mounted on the control box (usually near to the pump and motor valves) and the other set is at a convenient remote location. In a two storey house the water cylinder is found upstairs, so the remote control set is probably best mounted in the kitchen.

The remote switches S1-4 activate the LEDs in the opto-coupler D14, hence giving isolation to the logic inputs. Either the outputs of the couplers, or the operation of switches S5-9, act on the inputs of the latches in IC1. These inputs may also be acted on by the operation of the timer circuitry, IC2

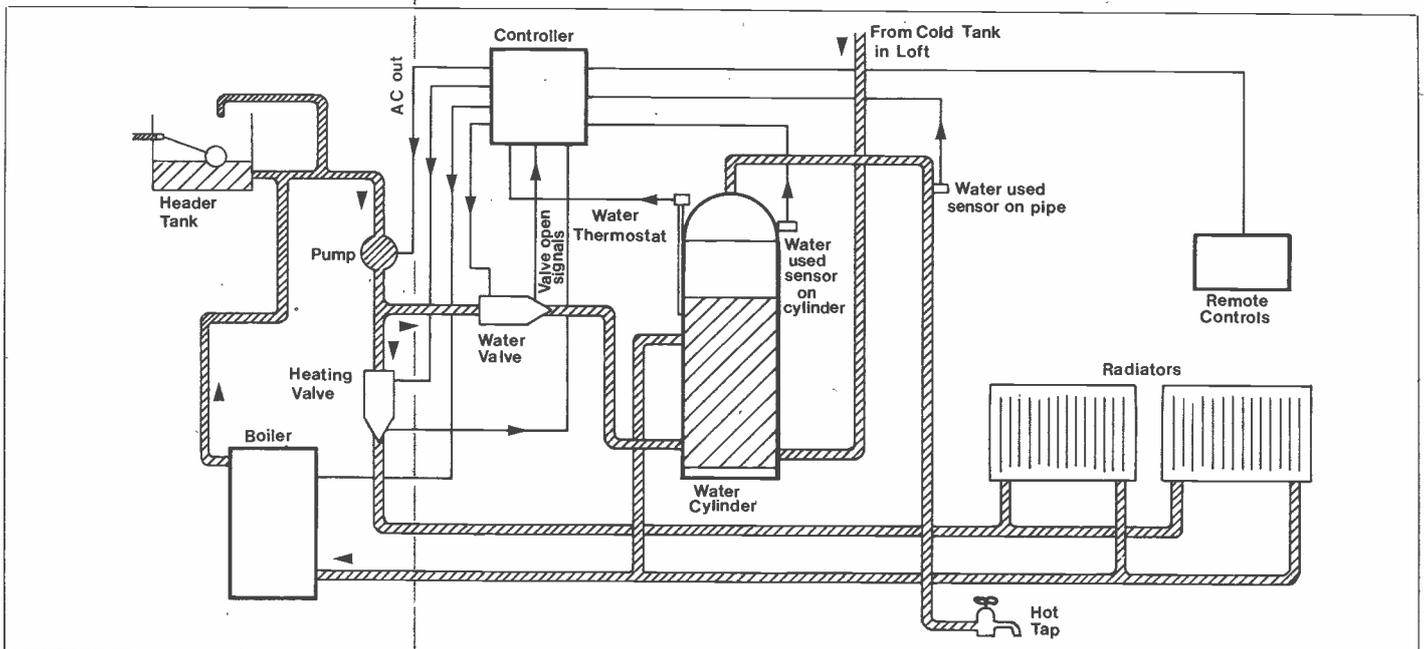


Figure 1. Outline of a typical heating system.

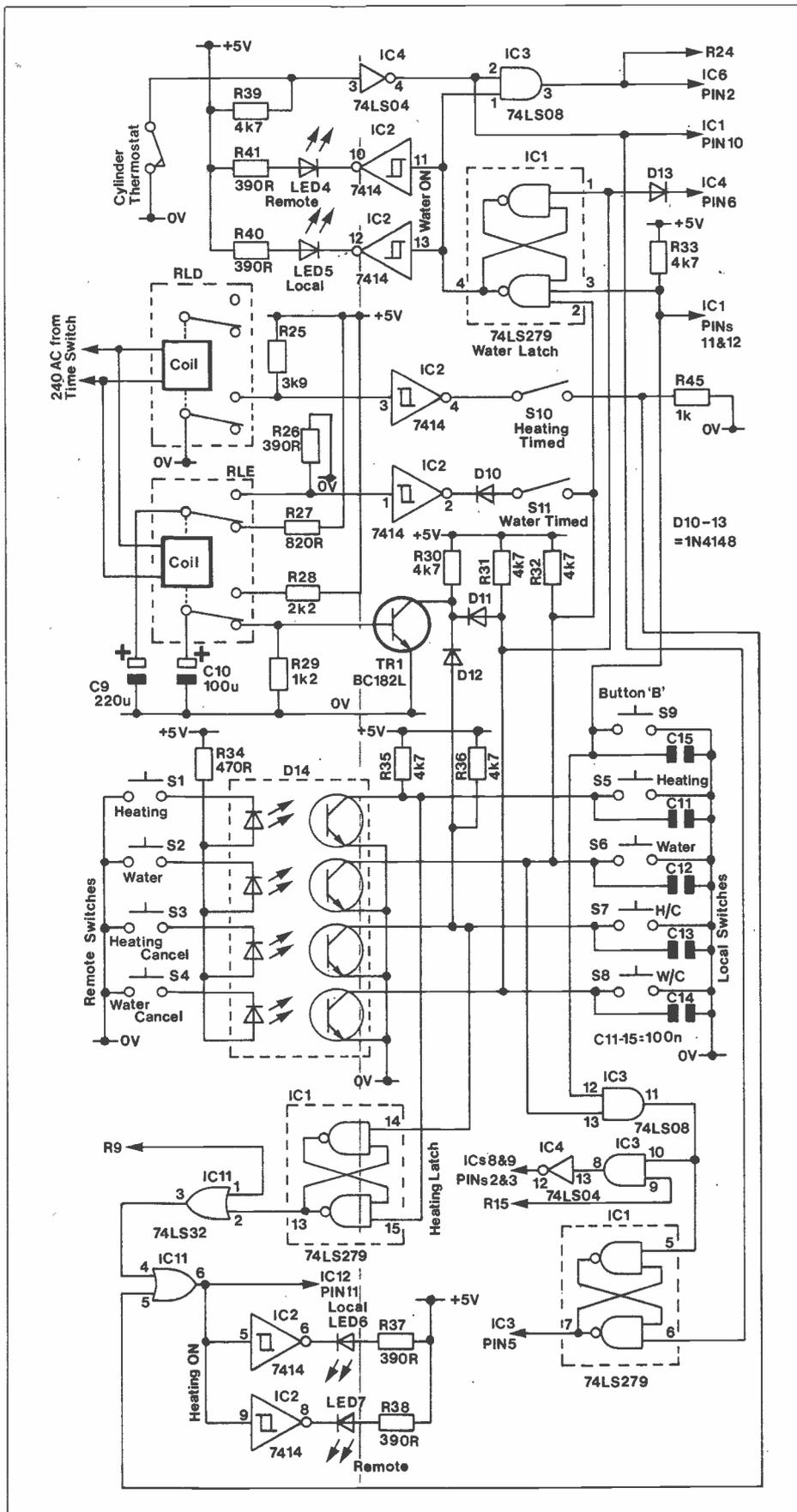
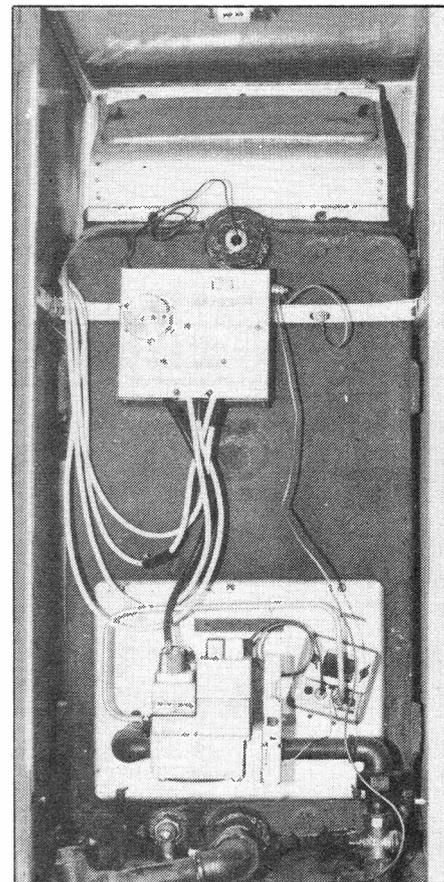


Figure 2. Circuit diagram.

and TR1. A standard inexpensive plug-in type timer may be used to operate the A.C. Relays RLD and E, hence allowing timed operation of the water, the heating or both. Switches S10 and S11 enable the circuitry to the latches.

When Pin 2 of water latch IC1 is taken low, the two 'water on' indicators are activated, one on the control box

and the other on the remote panel. If the cylinder thermostat shows the water temperature to be below the set level, the output of IC3 will go high, enabling TR4 and so operating the water valve via RLC. Once open, the inbuilt switch in the valve will take pin 11 of IC4 low, enabling input 3 of IC6. Pin 6 of IC6 then activates both the pump and the boiler



via IC4, transistor TR2, and relay RLA.

It can be seen that two thermistor sensors are attached to inputs 12 and 13 of Op Amp IC7. One of these is attached to the hot water pipe leaving the water cylinder, and the other is attached to the cylinder itself. These form the 'Water Used' circuitry. The preset RV1 is adjusted so that when the hot water pipe has cooled down, (in relation to the cylinder) i.e. no hot water has been run off for some time, the output on pin 14 will go high. This disables the reset lines of the counters IC8 and IC9. When the water in the cylinder is up to temperature IC4 pin 4 will go low thus forcing pin 7 of latch IC1 to go high. Clock pulses from the slow clock IC10 will now reach the input of the counter IC8. When no hot water is used for some time, the output of IC7 pin 14 will go high, thus allowing the counters to time out. After a period of about half an hour or so, assuming that the 'water' button is not depressed again, and that no hot water is used, pin 11 of IC9 will go high thus clearing down the water latch IC1; at this point the 'water' indicator will go out.

Heating may be turned on by pressing either of the two 'H' buttons. It may also be set to come on 'timed'. The buttons act upon input Pin 15 of the heating latch IC1 and cause output 13 to go high. This output is taken to Pin 2 of the 'OR' gate IC11. The other input of the 'OR' is from the frost-stat circuitry, IC7.

Both the frost-stat and the room thermostat share the same thermistor, sited to control the temperature of the heating in the house. The output of the thermistor is taken to pins 2 and 6 of the 3403 (IC7). One of the Op-amps is

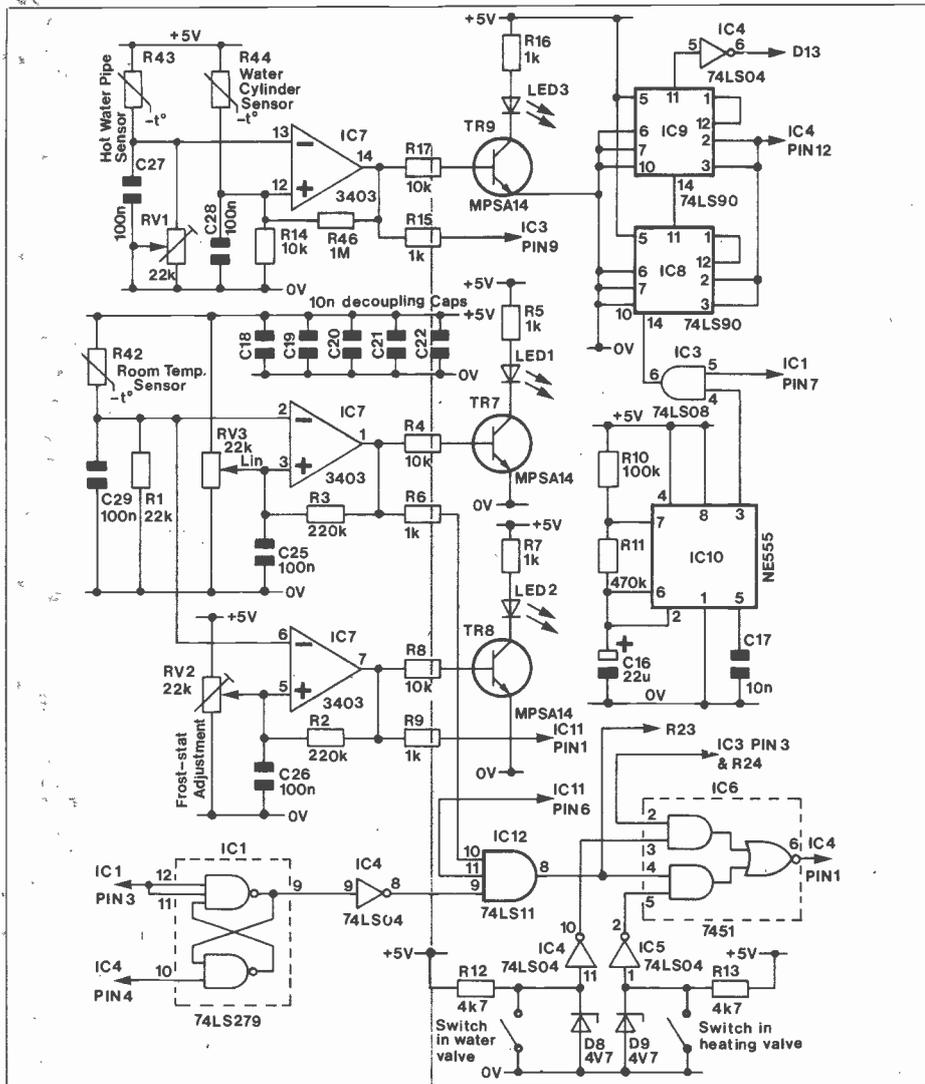


Figure 3. Circuit diagram.

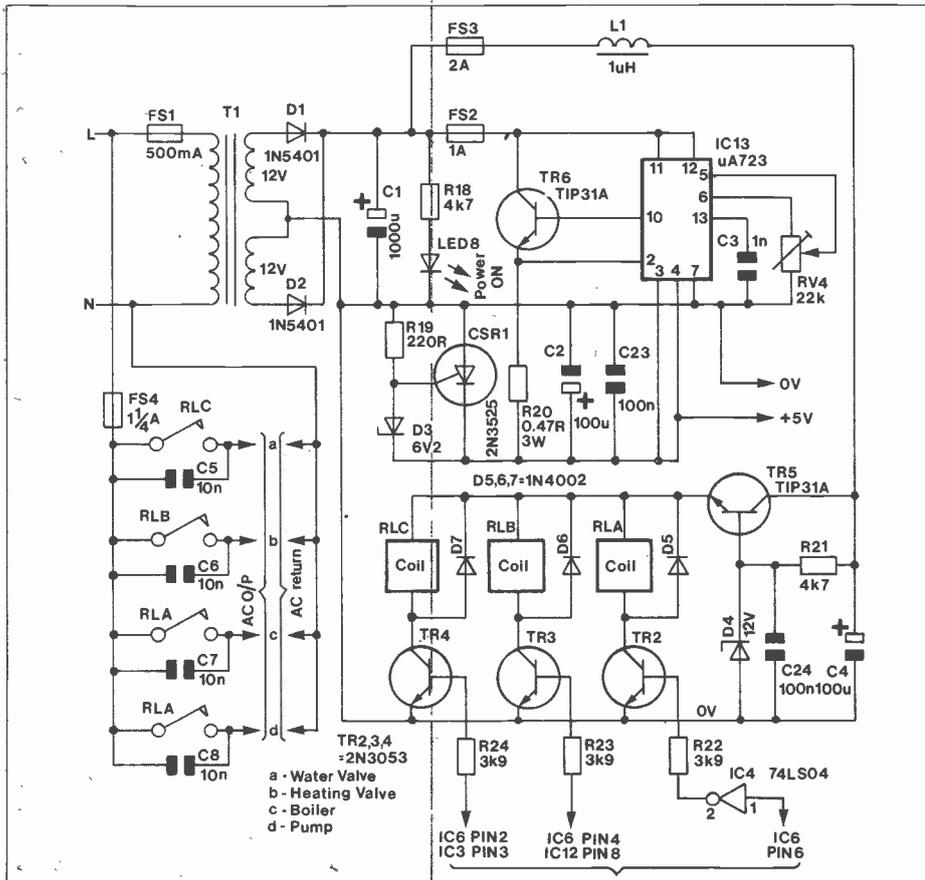


Figure 4. Circuit diagram.

adjusted by an external knob on the control-box (RV3) for the desired room temperature. The other is adjusted by a pre-set (RV2) to the desired lower-level temperature which will activate the heating. It will be noticed that the heating does not have to be on for this to operate, hence the premises may be left unoccupied with no fear of frozen pipes during a cold spell.

The output of the 'heating timed' circuitry is taken to Pin 5 of the next 'OR' gate (IC11) and so to the 74LS11 (IC12), on Pin 11. If the other inputs 10 and 9 are high, the output on Pin 8 will activate the heating motor valve via TR3 and relay RLB. Input 10 of the 74LS11 is taken from Pin 1 IC7 which is acting as the room thermostat. The other input, Pin 9, is fed from the output of latch IC1.

The 'B' button is found only on the control box and is used to give a priority to water heating when the central heating is also being used, for instance when a bath is needed. Switch S9 (B) causes the water latch to operate via Pin 3 of IC1. Pins 11 and 12 of IC1 are also taken low, thus causing the output IC4 pin 8 to go low. This has the effect of shutting down the heating on a temporary basis (as it does when the roomstat is up to temperature). It is restored eventually when the cylinder thermostat reaches the desired temperature, so taking Pin 10 of the latch low and re-activating the heating.

It will be noticed that the system design eliminates 'standing losses' with the boiler, which occur in the majority of central heating systems. This is when the boiler 'short cycles' by itself on it's own thermostat even when no heat is required by the radiators or the hot water.

System power

The electronics are supplied with the necessary +5 volts from a 723 voltage regulator, IC13, and a series pass transistor TR6. A separate feed is taken off the bridge rectifier to a simple regulator TR5, D4, to give around 12 volts for the operation of the relays. This supply is isolated to a degree by means of the choke L1 and the capacitor C4. The +5 volts is protected from over-voltages by an ordinary cro-bar circuit, D3 and CSR1. Three fuses are used to give protection to the low voltage supplies, these are FS1, FS2 and FS3.

It is preferable to run a separate lead from the mains plug to the relay contacts which supply the voltages to the external devices, this is to reduce the likelihood of mains-originated interference problems. If mains interference poses a serious problem (this all depends on the other devices using the ring main supplying the controller) then the best solution will probably be found in a small mains filter.

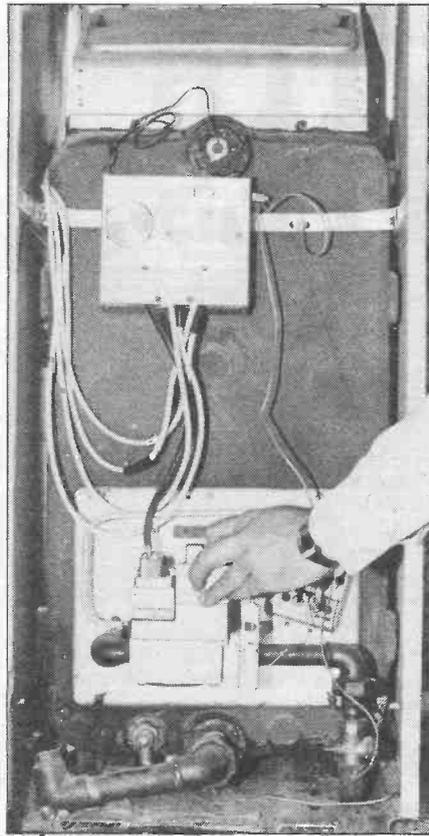
When constructing the controller, the logic must be assembled away from the mains transformer and the relays. Transistors TR5 and TR6 must be mounted on adequate heatsinking; TR2, TR3 and TR4, each need only be fitted with a small cooling fin. The cable

from the remote controls should not be run alongside of any mains cabling to reduce the possibility of any noise being induced onto the supply rails.

Setting up

It will be noticed that at various places in the circuitry, indicators have been fitted. These are invaluable for setting up the unit, and are of future use when adjustments to the settings are required.

Before first powering up the unit, the +5V adjustment should be set to its midway position, along with all of the other pre-sets. Now apply power to the unit and adjust RV4 to give +5 Volts. To calibrate the room thermostat, an ordinary thermometer is required. Set the thermometer up close to where the room thermistor (R42) is mounted, and after allowing ten minutes or so for it to stabilise, note the reading on it. Now turn the room thermostat (RV3) adjustment fully counter-clockwise and note that the room-stat indicator LED 1 is on. (It matters not whether any of the buttons have been pressed). The control should be now rotated clockwise till the indicator goes out. This point on the scale should be marked with the temperature on the thermometer. It will be necessary to turn the heating on (H button) after the thermostat control has been turned up to check for the correct operation of the heating valve, the pump, and the boiler. When the room temperature has risen by a few degrees, it will be possible to add another value onto the thermostat scale using the same method as be-



fore. It should be possible to add further points to the scale by dividing the distance between the two points by the number of degrees rise in the room temperature.

An immersion heater type thermostat may be used to sense the temperature in the water cylinder. It should be firmly attached in an upright posi-

tion to the top or the hot water cylinder (inside of the insulating jacket) and set to the temperature required by means of the adjusting control at the top. To adjust the 'water used' pre-set RV1, it will be first necessary to bring the water in the cylinder up to temperature by depressing the 'W' button. Check for correct operation of the motor valve, the circuitry and indicators, and when up to temperature note the position of the pre-set RV1 which causes the time out enable indicator LED 3 to extinguish. Run out half a sinkful of hot water and note the new setting of the pre-set. The final position will be somewhere between the two of these marks. Initially set the pre-set two thirds of the way back to the first mark and observe that if no further hot water is used, the indicator comes on after a period of five to fifteen minutes. The longer it takes for the indicator to come on after the last water was used, the longer before the start of the timeout.

The frost-stat is the most difficult to adjust in that the temperature of the thermistor has to be reduced to around five degrees C. The setting may be obtained by adjusting it two thirds of the way down the scale and waiting for the colder weather. Two settings at the lower end of the scale should enable a similar calibration to be carried out as was done with the room-stat.

*Note that a lot of the components have been very conservatively rated, this being felt necessary to ensure that the unit will run cool and reliably as it is likely to be left switched on for very long periods of time.

CENTRAL HEATING CONTROLLER PARTS LIST

Resistors: All 0.4W 1% metal film unless specified

R1	22k		
R2,3	220k	2 off	(M220K)
R4,8,14,17	10k	4 off	(M10K)
R5,6,7,9,15,16,45	1k	7 off	(M1K)
R10	100k		(M100K)
R11	470k		(M470K)
R12,13,18,21,30			
31,32,33,35,36			
39	4k7	11 off	(M4K7)
R19	220R		(M220R)
R20	0.47R (3W wirewound)		(W0.47)
R22,23,24,25	3k9	4 off	(M3K9)
R26,37,38,40,41	390R	5 off	(M390R)
R27	820R		(M820R)
R28	2k2		(M2K2)
R29	1k2		(M1K2)
R34	470R		(M470R)
R42,43,44	VA1055S Thermistor	3 off	(FX21X)
R46	1M		(M1M)
RV1,2,4	22k Hor-sub min preset	3 off	(WR59P)
RV3	22k lin pot		(FW03D)

Capacitors			
C1	1000uF 63V axial electrolytic		(FB84F)
C2,10	100uF 25V axial electrolytic	2 off	(FB49D)
C3	1nF polycarbonate		(WW22Y)
C4	100uF 63V axial electrolytic		(FB51F)
C5,6,7,8	10nF suppression cap.	4 off	(FF53H)
C9	220uF 16V axial electrolytic		(FB61R)
C11,12,13,14,15,23,24,25,26,27,28,29	100nF disc ceramic	12 off	(BX03D)
C16	22uF 25V axial electrolytic		(FB30H)
C17,18,19,20,21,22	10nF disc ceramic	6 off	(BX00A)

Semi-conductors

D1,2	1N5401	2 off	(QL82D)
D3	BXY88C6V2		(QH09K)
D4	BXY88C12V		(QH16S)
D5,6,7	1N4002	3 off	(QL74R)
D8,9	BXY88C4V7	2 off	(QH0GG)
D10,11,12,13	1N4148	4 off	(QL80B)
D14	Quad Opto-Isolator		(YY63T)
CSR1	2N3525		(QR25C)
TR1	BC182L		(QB55K)
TR2,3,4	2N3053	3 off	(QR23A)
TR5,6	TIP31A	2 off	(QL15R)
TR7,8,9	MPSA14	3 off	(QH60Q)
L1	1uH choke		(WH29G)
IC1	74LS279		(YH01B)
IC2	7414		(QX46A)
IC3	74LS08		(YF06G)
IC4,5	74LS04	2 off	(YF04E)
IC6	7451		(QX83E)
IC7	3403		(QH51F)
IC8,9	74LS90	2 off	(YF38R)
IC10	NE555V		(QH66W)
IC11	74LS32		(YF21X)
IC12	74LS11		(YF09K)
IC13	uA723 (14 pin)		(QL21X)

Miscellaneous

T1	12V toroidal		(YK10L)
FS1	Fuse 500mA anti-surge		(WR18V)
FS2	Fuse 1A		(WR03D)
FS3	Fuse 2A		(WR05F)
FS4	Fuse 1.25A anti-surge		
LED 1-8 inc	LED red	8 off	(WL27E)
RLA,B,C	5A mains relay	3 off	(YX98G)
RLD,E	2-pole changeover relay (coil 240V AC)	2 off	(FX49D)
S1-9 inc	SP make push button switch	9 off	
S10,11	SP make min toggle/slide switch	2 off	

SAY IT WITH SATELLITES

by Mike Wharton

Part 2

The first part of this series took a broad view of the historical development of the communications satellite. This is an area of rapid change, with new satellites continually being put into orbit, and some old ones coming back down to Earth! Since the beginning of this year, 9 Russian Cosmos and 1 Ekran satellite have been launched from Plesetsk and Baikonur. These include military navigation and surveillance satellites and one direct-broadcast satellite put into a geostationary orbit. The Americans have not been idle either, with an RCA Satcom 4 and a Western Union Westar 4 being launched into a geostationary position from Cape Canaveral. Of the ones that come down, virtually all burn up in the Earth's atmosphere on re-entry, so there is little danger of being hit by falling satellite debris. Such a fate for the satellite is not inevitable, but depends on the altitude and shape of the orbit. If the altitude is much below 500km., then the drag due to the outermost parts of the atmosphere gradually takes effect and the orbit decays, becoming lower and slower, until the satellite finally burns up in the denser parts of the atmosphere. Some satellites have small rocket motors which are used to carry out manoeuvres in space, either to alter the angle of the orbit or adjust the altitude. Usually, any data produced by satellites is beamed back to Earth by radio, but some of the Russian surveillance satellites are able to dump photographic material in re-entry canisters just before they burn up. This method is used by their low flying 'photosats', which often streak across the target area at altitudes as low as 160km. Such orbits decay very quickly and these satellites have to be replaced about every fortnight.

Those satellites placed in a geostationary orbit, 36,000km. out in space, may last for many years before they finally fail; such failures are usually due to faults developing in the satellite because of the extremely harsh conditions of outer space. The satellites are subjected to the full intensity of the sun's rays on one side and the bitter cold of space on the shaded side. In order to even out the temperatures and keep the internal electronics within reasonable limits, the satellite is given a slow spin to spread out the heating effect. Also, reflective metal foil is used to deflect some of the sun's heat, or electrical heaters used to maintain the stability of particularly sensitive parts of the craft. Part of the telemetry from the satellite monitors the various components and the craft may be manoeuvred to ensure a proper temperature balance. Despite these precautions, some satellites still fail due to impact by micro-meteorites. These are small pieces of inter-stellar debris, some no larger than a pin-head, which travel through space at colossal speeds and can punch a hole through the satellite. Especially, vulnerable are the solar arrays, which offer a large target area; if critical parts of these are damaged then the satellite is deprived of

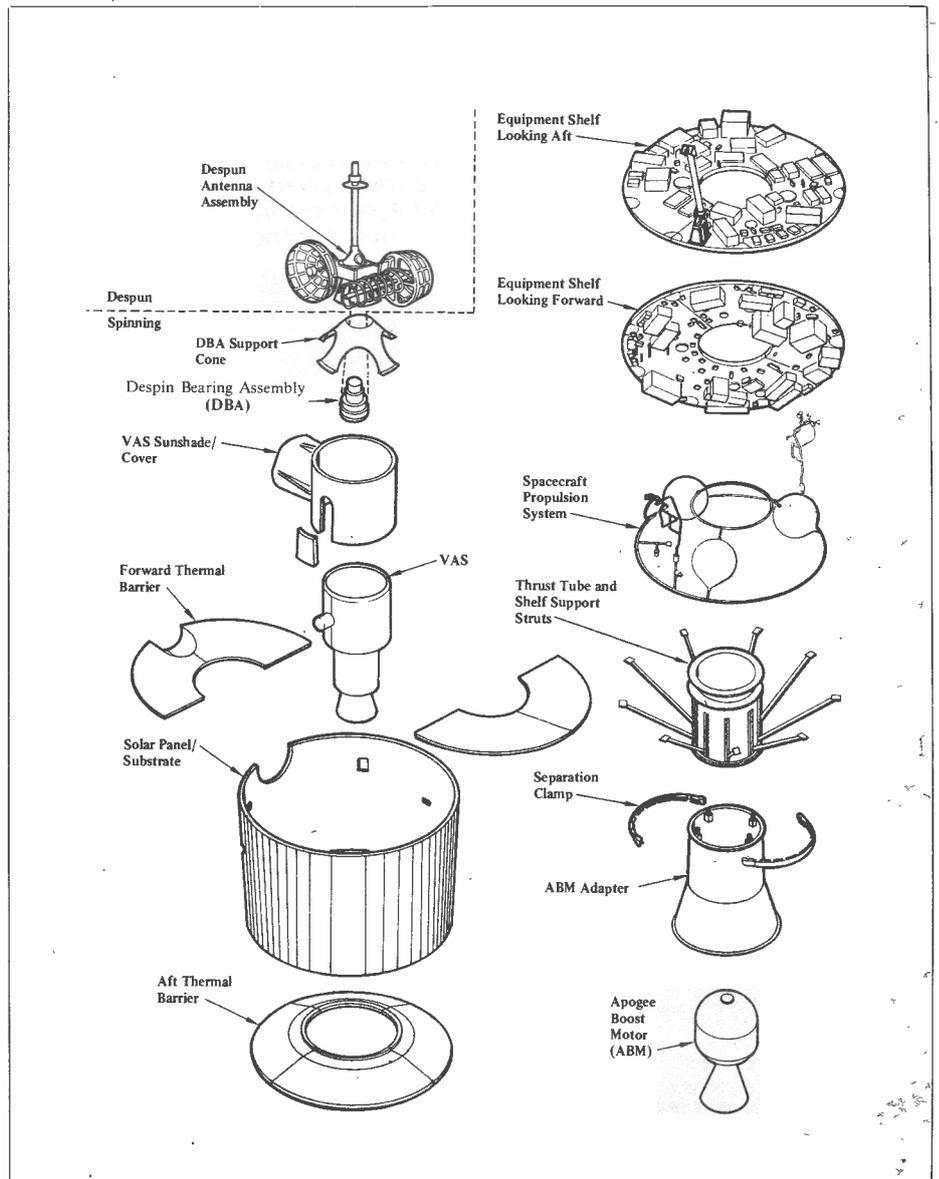


Figure 1. GOES modular assembly.

electrical power, and can then only operate until its internal batteries run down.

GOES weather satellites

The internal construction of a satellite will naturally depend on the job it is intended to do; they range in complexity from that of Echo 1, simply a large balloon launched by NASA for bouncing off radio signals, to those like GOES (Geostationary Operational Environmental Satellite). This satellite is operated by the American National Oceanic and Atmospheric Administration (NOAA). Figure 1 shows the various parts of this particular satellite, which is used mainly for investigations into the physics of the Earth's atmosphere. The most important parts of such a satellite are the imaging sensors, of which GOES carries two, the Visible and Infra-red Spin Scan Radiometer, (VISSR), and the Visible and Infra-red Spin Scan Radiometer Atmospheric Sounder, (VAS), which is a more sophisticated version of the VISSR. The VAS telescope and operation are shown in Figure 2. Imaging is achieved by scanning a focussed spot over the Earth. Light from the surface enters the telescope at right angles to its optical axis via the flat scan mirror, which is provided with an angular positioned stepping mechanism. The scanned pattern, after processing, resembles a conventional TV picture. East-west scan lines are achieved by rotation of the spinning satellite and the lines are moved by the stepped

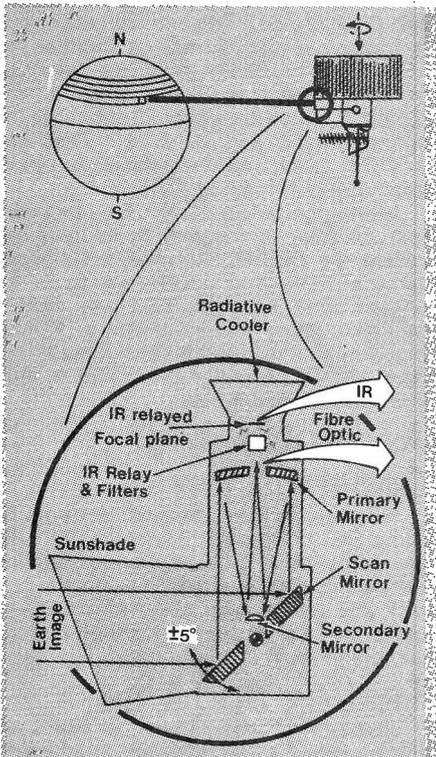
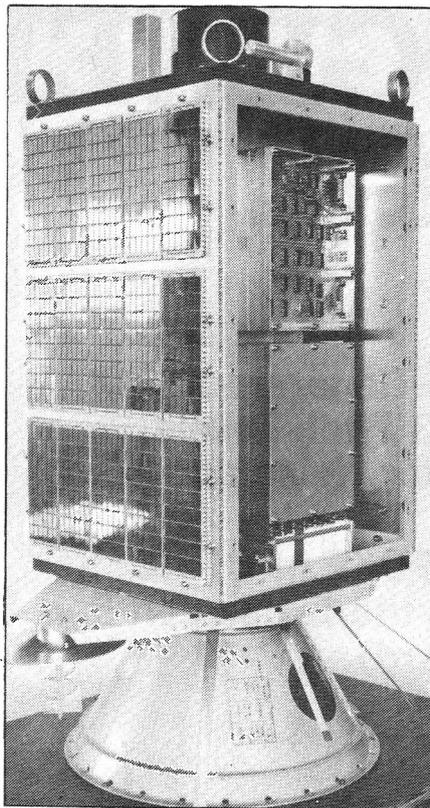


Figure 2. VAS telescope optics.

mirror to scan north-south. The data from these sensors can be used for detecting the amount of water vapour in the atmosphere and producing temperature profiles, as well as visible-light and infra-red pictures. All of this information is used by meteorologists to help predict weather patterns and gain some insight into the mechanisms which drive the atmospheric weather machine. One way in which these images are transmitted is as WEFAX, or weather facsimile. By suitably decoding such transmissions it is possible to feed them into a facsimile copier and obtain pictures of the visible field of view. This is by no means a straight-forward task, but there are ways of obtaining a 'satellites-eye-view' of the world which are easier using an Amateur satellite.

December 1982 Maplin Magazine



UOSAT/OSCAR 9

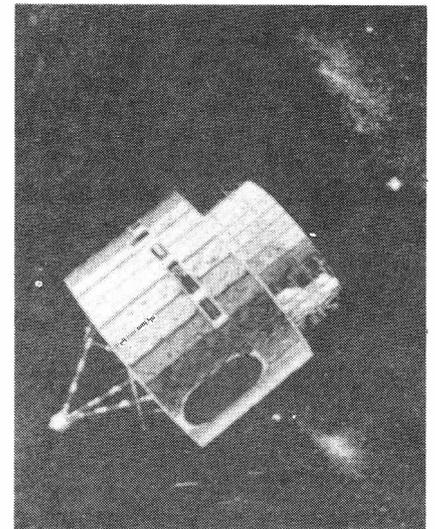
TV of the future

The direct-broadcast satellites are rather different in their mode of operation, being used primarily to re-transmit signals beamed at them from ground stations. They contain a number of devices called transponders, which receive the incoming up-link signal, amplify it, and then re-transmit it back towards Earth, usually on a different frequency. By the use of specially designed transmitting antennae the down-link signal may be directed to a particular area within the satellite's field of view, called the 'footprint'. Although nowhere near as powerful as ground-based broadcast stations, which often have transmitter powers measured in hundreds of kilo-watts, their unique vantage point in space is more than sufficient compensation. The usual problems associated with terrestrial radio communication, such as limited range, obstruction by high ground or buildings, reflections which cause ghosting in TV pictures or interference between the ground wave and the sky wave which introduces multi-path distortion, simply do not exist with satellite reception. Thus it is not necessary to have high-powered transmitters with omni-directional antennae, and there are no areas of weak signal due to hills and valleys. The only disadvantage is that special high frequency receiving dish antennae and tuners are needed, and these are quite expensive at the moment, although with improvements in this area of semi-conductor technology and equipment design they may be expected to become much cheaper. Also, by using a sufficiently high down-link frequency, and 12 GHz is likely for L-sat, the proposed European D-B satellite, a receiving dish of less than a metre diameter may be used. It is likely that an interim solution will be to set up neighbourhood schemes, where one large dish and frequency converter could be used to satisfy a number of normal, domestic TV receivers.

Amateur satellites

For those interested in becoming involved in satellite communications, possibly

the easiest and most rewarding way is through Amateur satellites. Many readers will be aware of the existence of Radio Amateurs, whose activities provide a worldwide service and who operate on nationally and internationally agreed frequency bands. As a group they have been responsible for many advances in the understanding of radio, such as the nature of the propagation of radio waves. One of their latest ventures has been to become involved in producing a number of satellites for Amateur use, and the whole activity from design through to launch has been co-ordinated by AMSAT. This is a group comprised of Radio Amateurs who are interested in satellites and their use in the field of amateur radio communication. Although the organisation originated in America, there is a very well established branch in this country, called AMSAT-UK. The satellites they operate, known as OSCARs, are used to facilitate radio communication between all parts of the world. Although not as complex as commercial satellites, for an amateur group to have put a number of such satellites upaloft is no mean feat. The usual mode of operation is as a transponder, mentioned earlier. Here, though, the frequencies are in the more manageable HF and VHF bands. The up-link is on 145 MHz and the down-link on 29 MHz, and to make the best use of the limited power available transmissions are on SSB (Single Side Band). The Russians, never ones to be left out, launched several of their own amateur satellites at the end of last year.



GOES weather satellite

Known simply as R-S satellites, they operate in a similar manner to the OSCARs.

The next article in this series will examine in more detail the operation of the AMSAT OSCARs, particularly OSCAR 9 or UOSAT, which has been produced as the result of a joint venture with the University of Surrey and a number of British companies. Also, methods of predicting the appearance of these satellites from orbital data will be explained and the design of a suitable receiver for OSCAR 9/UOSAT transmissions given.

Appendix

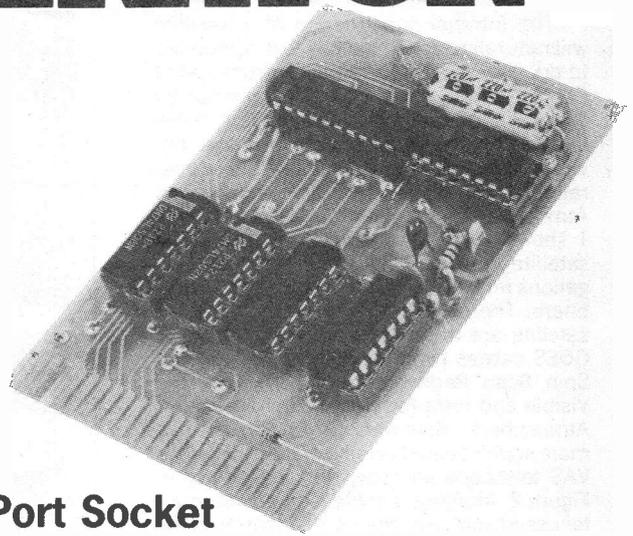
Anyone interested in obtaining more information on AMSAT-UK should write, enclosing a stamped addressed envelope, to:

AMSAT-UK, 94, Herongate Road, Wanstead Park, London, E12 5EQ.

Information on Amateur Radio may be obtained from: The Radio Society of Great Britain, 35, Doughty Street, London, WC1N 2AE.

SOUND GENERATOR for the ZX 81

by Dave Goodman



- ★ 3 Programmable Tone Generators
- ★ Noise Generator with 3 Pitch Levels
- ★ Separate Attenuators for Noise and Tone Generators
- ★ Entry from PEEK and POKE in BASIC
- ★ Connects Directly into the Expansion Port Socket (or into the motherboard)
- ★ Single Address Access

This sound generator is a worthy addition to our ZX81 hardware projects. Almost infinite possibilities for sound and noise effects that can be added to your own programs for greater realism.

Circuit Description

ICs 1, 2, and 3 are connected to the computer address lines A1 to A15. This means that all addresses up to 65534 may be presented, so a decoder is required to examine all lines, but only to respond to a

particular address. The address code used here is 16370, which lies between the 16360 and 16380 used in our I/O port project. A0 is not used, so a further address of 16371 exists.

A negative going address decode pulse appears at the output of IC2, and is used to latch data into IC4 and enable IC6. To avoid corruption of data into IC6 the output of IC4 must be latched to the data code before IC6 is enabled.

Buffers IC5a and b delay the enable pulse

just enough to allow IC4 to latch before enabling IC6. IC6 pin 4 READY line controls the duration of the WRITE ENABLE (pin 5) and CHIP ENABLE pulse for correct circuit operation, via IC5c. R1 and C1 smoothe the +5V supply, to keep noise spikes down to a minimum, and audio output is taken from IC6 pin 7, via low pass filter R3 and C2, to the output pins 1 and 2. IC5d buffers the 3.22MHz clock, and prevents lengthy track runs from crashing the ZX81.

Most important is D1. You may be aware that because of incomplete address decoding, the ZX81 ROM is repeated between address 8193 and 16383, which is an unused area between ROM and system variables. These addresses can be POKEd providing that the ROM is deselected at that time, and D1 conducts when A13 is high, freeing this area for use.

Assembly and Construction

Insert all track pins and both vero pins. Fit all six DIL sockets, R1, 2, and 3 and C2. Fit disc ceramics C3 to C7 and C1 and C8 noting the polarity markings. Insert all ICs the correct way round, then clean the PCB and make the final inspection for short circuits and dry joints.

Testing and Use

If you do not possess a mother board you will require a 2 x 23 way socket to solder onto the PCB edge connector, otherwise plug into your motherboard. The signal is insufficient to drive a loudspeaker direct, as it is only 300mV in amplitude, so you will need an external amplifier and speaker connected to pins 1 (signal) and 2 (screen). Switch on the ZX81 and a cacophony of noise should be heard. Run the following test program:-

```

10 REM TEST PROGRAM
15 LET A = 16370
20 INPUT B
25 POKE A, B
30 GOTO 10
    
```

Press RUN then NEWLINE and input the following codes followed by NEWLINE after each code: 159 191 223 255 (you should hear the tones disappearing one by one until all the signals are off) 144 128 64. A low frequency tone of approximately 98Hz (G2)

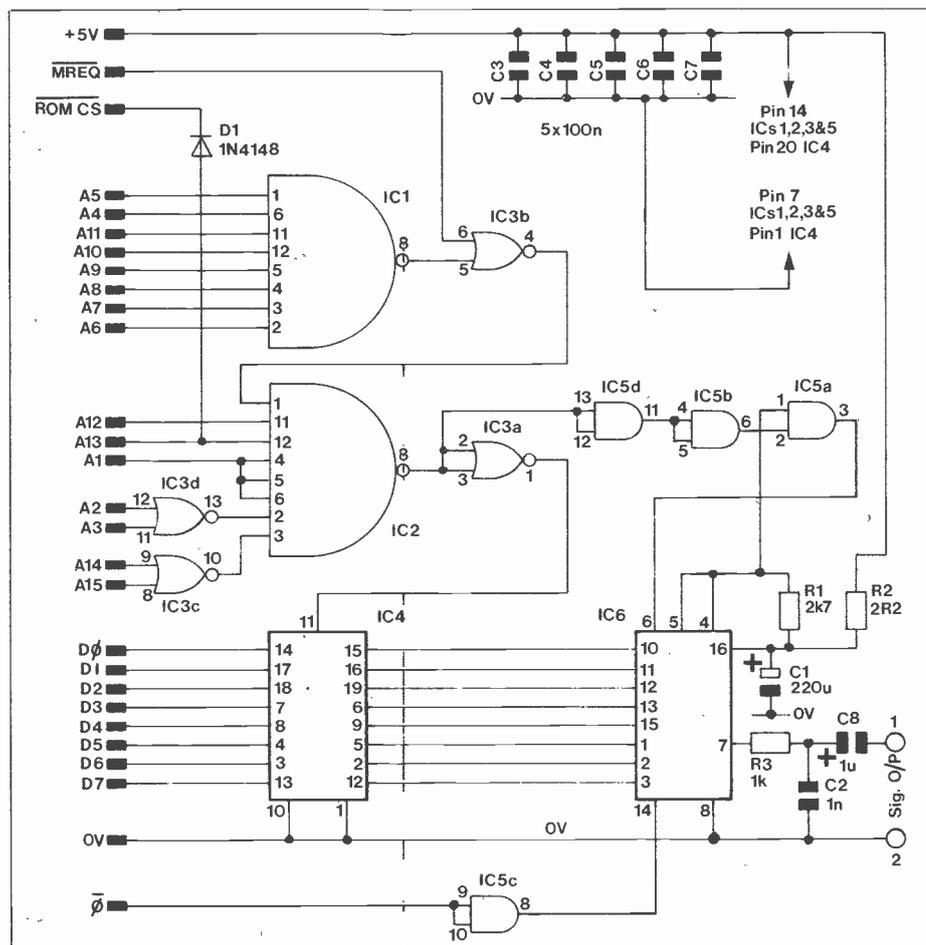


Figure 1: Circuit diagram

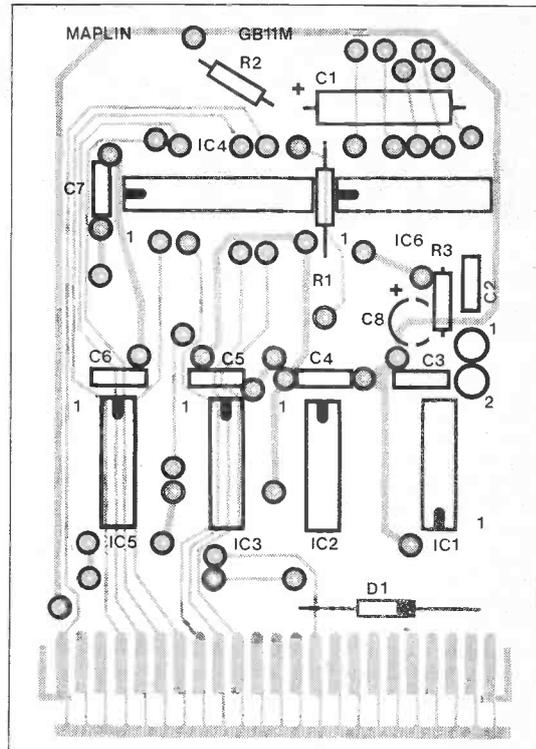
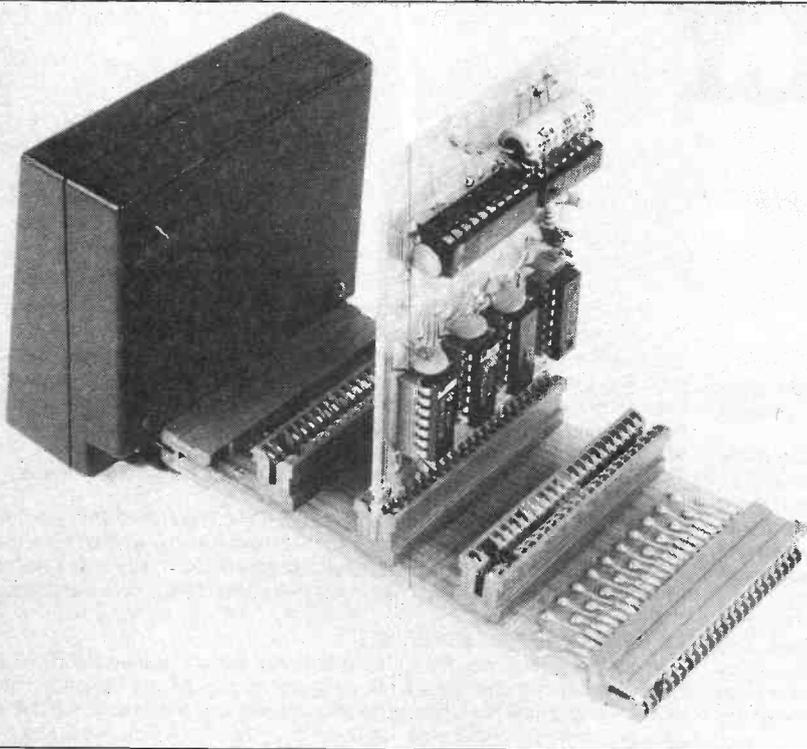


Figure 2: Overlay and artwork

TONE GENERATOR	ACCESS CODE	FREQUENCY RANGE	ATTENUATION CODE
1	128	64(G2) to 1(G8)	144 to 159 (OFF)
2	160	64(G2) to 1(G8)	176 to 191 (OFF)
3	192	64(G2) to 1(G8)	208 to 223 (OFF)
White Noise	228	High pitch	240 to 255 (OFF)
White Noise	229	Med. pitch	240 to 255 (OFF)
White Noise	230	Low pitch	240 to 255 (OFF)
Pulse (spike)	224	480Hz	240 to 255 (OFF)
Pulse (spike)	225	240Hz	240 to 255 (OFF)
Pulse (spike)	226	120Hz	240 to 255 (OFF)

should be heard. Any number between 1 and 64 may now be entered and the appropriate tone should be audible. Refer to the following listing for access codes and settings.

To input data into tone generator 1 only, first enter the required volume level from the attenuation codes. The first code given is maximum volume, e.g. Tone generator 1 = 144 and attenuation levels are in 15 x 2dB steps down to 159, which is fully off. Next enter the tone generator access code, which in this example is 128, followed by the required frequency. The frequency range covers 98Hz (G2) up to 6.3kHz (G8) in 64 steps, code 1 being the highest frequency and code 64 being the lowest, so enter 64. The entered codes are now 144, 128, 64, which is tone generator 1 producing an

output of 98Hz at full volume. As a Tone Generator access code was entered after the attenuator, the frequency can be changed as desired, but if an attenuator code is now entered, 144 to 159 in this example, the frequency can only be altered by entering the access code, 128, again, and then a frequency code.

Keep in mind that when a register is accessed it will remain 'on line' awaiting further update input codes. Access to Tone Generators 2 and 3 is in the same manner, except that the codes are different. If you enter 144, 128, and 64 to set up a tone in Generator 1, then enter 176, 160 and 32. Two tones will now be heard, with Generator 2 an octave above Generator 1. Entering a frequency code will now only alter Generator 2.

Pulse and noise effects require attenuation codes and an access code only. Once the attenuation level has been set noise and pulse codes are entered and are immediately audible.

Tone Generator 3 can be used to control either noise or pulse registers and code 231 followed by 192 allows control of white noise pitch by entering 1 to 64. Similarly, code 227 followed by 192 allows control of a 480Hz pulse tone by entering 1 to 64, and the lowest frequency possible is 6Hz.

Obviously, the best way to understand the system is to use it, therefore a few simple programs are given for assistance, shown at the end of this article. When writing music programs remember that G2 to G8 spans 73 notes and control only covers 64 notes, therefore higher frequency notes tend to become sharper in relation to the lower octaves.

Run these programs in SLOW mode:—

```

10 REM ZMD878DMZ      10 REM PHOTON BLAST
   MD878DM182.*2     15 LET A = 16370
   8ZMD878DM5MI      20 POKE A, 159
   EDFJMZMD878DM     25 POKE A, 191
15 LET A = 16370      30 POKE A, 223
20 LET B = 16514      35 POKE A, 148
25 FOR J = 1 TO 48    40 POKE A, 240
30 FOR I = 1 TO 15    45 POKE A, 231
35 NEXT I             50 POKE A, 192
40 POKE A, (PEEK B)  55 FOR J = TO 30 STEP 2
45 LET B = B+1        60 POKE A, J
50 NEXT J             65 POKE A, 128
55 GOTO 10            70 POKE A, J
                       75 POKE A, 192
                       80 NEXT J
                       85 POKE A, 159
10 REM GUN SHOT      90 POKE A, 228
15 LET A = 16370      95 POKE A, 247
20 POKE A, 159        100 INPUT C$
25 POKE A, 191        110 GOTO 10
30 POKE A, 223
35 POKE A, 240
40 POKE A, 23
45 FOR J = 24 TO 255  Press NEWLINE to fire.
50 POKE A, J          To remove back-
55 NEXT J              ground hiss, delete line
60 INPUT E$           90 and change line
65 GOTO 10            95 to POKE A, 255.
After RUN press
NEWLINE to fire.

```

ZX81 SOUND GENERATOR PARTS LIST

Resistors: All 0.4W 1% Metal Film

R1	2k7	(M2K7)
R2	2R2	(M2R2)
R3	1k	(M1K)

Capacitors

C1	220uF 10V axial electrolytic	(FB60Q)
C2	1nF ceramic	(WX68Y)
C3-7 inc.	100nF minidisc	(YR75S)
C8	1uF35V tantalum	5 off (WW60Q)

Semiconductors

D1	1N4148	(QL80B)
IC1,2	74LS30	(YF20W)
IC3	74LS02	2 off (YF02C)
IC4	74LS373	(YH15R)
IC5	74LS08	(YF06G)
IC6	76489AN	(YH33L)

Miscellaneous

	14 pin dit skt	4 off (BL18U)
	16 pin dit skt	(BL19V)
	20 pin dit skt	(HQ77J)
	Veropin 2141	(FL21X)
	Track pin	1 pkt (FL82D)
	ZX81 Sound Gen. PCB	(GB11M)

A complete kit of parts is available for this project. Order As LW96E (Sound Gen. Kit). Price £10.95.

For constructors who may wish to use the Sound Generator in addition to other external hardware, a mother board is available, called the ZX81 Extend board (GB08J) and will accept the Sinclair 16k RAM pack and up to 3 plug-in modules. In addition to the PCB you will require 4 PC Edge Connectors (RK350)

BASICALLY BASIC

Graham Hall, B.Sc.

Part 14

Files

BASIC has three methods of supplying data to a program:

1. The INPUT statement — the user interacts with the computer while the program is running. Each time the program is run new data is requested and is input from the terminal.
2. The READ, DATA and RESTORE statements — the READ statement directs the program to read from a list of values built into a data block by a DATA statement. In terms of program execution time, it is much more efficient to use READ and DATA statements than INPUT statements because the user does not have to interact with the program when it is run. The RESTORE statement enables the same data to be used more than once during the execution of the program.
3. The file statements — data can be accessed from or written to a uniquely named file which is separate from the main program. The computer system stores a file on peripheral devices such as disks or magnetic tapes. As the file is stored under its own name separate from the program which created it, different programs can use the file name to make that file's data available.

The use of the INPUT, READ, DATA and RESTORE statements has already been described. Now the BASIC statements used to create a file, place data into it, and make it available to a program are described. Since files are externally stored and program independent, their configuration and characteristics such as size and data access depend on the computer system and peripheral device that you use. For these reasons the description to follow will be general and serves only as an introductory explanation. For a specific and more complete description refer to your systems user guide.

Most personal computer systems use 'sequential files'. These files are usually terminal — format files in which the contents consist of a collection of ASCII characters stored in lines of various lengths exactly as they would appear on the terminal. A sequential file is one in which the data assigned to the file is arranged one item after another from the beginning of the file. To retrieve an item from the file all items preceding it must be retrieved first. Some systems also allow virtual array files and record files to be created but these will not be described here.

All versions of BASIC have statements to:

- i) create a new file and to assign it a unique name,
 - ii) place data into a file (writing to a file),
 - iii) access data from a file (reading a file),
 - iv) close a file which has previously been opened by a program.
- These will now be described.

Creating and Opening a File

The OPEN statement enables a new file, or an existing file, to be opened and associated with a file number which establishes a communication channel between the program and the file. Some versions of BASIC only allow one file at once to be used by a program so it is not required to associate a file number since this will be a system default.

Usually the OPEN statement performs several functions which include naming the file, designating the operations to be performed and opening a communication channel. An example of this would be:

```
10 OPEN "string" {FOR INPUT } AS FILE # expression
                {FOR OUTPUT }
```

The OPEN "string" component of this statement either references a file which already exists, in which case the file name enclosed within quotation marks is used to locate the file or names a new file. The file name is a string of alpha-numeric characters enclosed within quotation marks. Usually it must be less than a certain maximum number of characters depending on the system being used. It could also be a string variable.

The FOR INPUT or FOR OUTPUT component of the open statement is optional — one or neither of these portions can be used. When the FOR INPUT option is used BASIC opens the file specified as the file name and allows the data it contains to be used by the program. An error message is returned and displayed on the terminal if BASIC tries to open a file which does not exist. The FOR OUTPUT option creates a new file and allows the program to write data to it. If neither is specified BASIC searches for a file with the name specified in "string". If the file is found it is opened; otherwise a new file assigned to that name is created.

The AS FILE # expression portion of the OPEN statement associates the file and the program with a common communication channel. This enables the file, which is stored on a peripheral device, to be associated with the current program which is in the computer's main memory area. The location associated with the file name is called a channel number and is specified in the expression part of the AS FILE # portion. This location can then be accessed by the program.

The following examples show how the OPEN statement is used:

```
20 OPEN "SUBJECT" FOR INPUT AS FILE # 1
```

This statement opens the file named SUBJECT. The FOR INPUT portion shows that the file already exists and that the data is to be read from the file. The AS FILE # portion establishes communication channel 1 as the link between the program in main memory and the file on a peripheral device.

```
20 OPEN "INFORM" AS FILE # 3
```

This statement causes BASIC to search for the file named INFORM. If the file exists it is opened and the program can access its data; if the file is not found a new file is created and assigned to the file name INFORM. The program can then write data to this file. The file is accessed by channel number 3.

```
10 OPEN "RESULTS" FOR OUTPUT AS FILE # 2
```

This statement creates a new file which is assigned to the file name RESULTS. The FOR OUTPUT portion of the statement notifies BASIC that this is a new file to which data can be written. The AS FILE # 2 portion of the OPEN statement establishes communication channel 2 as the link between the program in main memory and the file on a peripheral device.

Some versions of BASIC have different OPEN statements to open a file for reading and to open a file for writing. For example, to open a file to accept data the statement could be WOPEN (write open) but to open a file to retrieve data the statement could be ROPEN (read open). This depends on the system you are using and will be explained in the user's guide for your system.

Closing a File

All files opened by a program should be closed before the program terminates execution. Unless they are closed the file may become 'corrupt', that is some of the contents may be spuriously altered or destroyed. The CLOSE statement is used to close a file and dissociate it from a communication channel. After a file has been closed it cannot be accessed until it has been re-opened.

The general format of the CLOSE statement is:

```
line number CLOSE ([ ] expression list)
```

where expression list may be one file number or a list of opened file numbers separated by commas. The part of the CLOSE statement shown within square brackets is usually optional. If no expressions are specified all files opened by the program are closed.

The following examples illustrate the use of the CLOSE statement:

```
10 CLOSE # 1:REM CLOSE FILE ASSOCIATED WITH CHANNEL 1
```

```
20 X=3
```

```
30 CLOSE 2,X,3+2:REM CLOSE FILES 2,3&5
```

```
40 CLOSE:REM CLOSE ALL FILES
```

Writing to a File

To write data to the terminal the BASIC PRINT statement is used. The PRINT statement can also be used to write data to a file. The general format is:

```
PRINT (#) channel number, list
```

where channel number can be the communication channel number associated with a file that has been opened with the OPEN statement or zero. If zero is specified the output is to the terminal. The # character preceding the channel number is usually optional. List can be any numeric or string expression or a numeric or string variable. Each item in the list must be separated with a comma or a semicolon. Also the first item in the list must be separated from the channel number by a comma.

The following short program opens a file called EXAMPLE for output and then writes the string "FIRST LINE OF FILE EXAMPLE" to the file when the program is executed.

```
10 OPEN "EXAMPLE" FOR OUTPUT AS FILE # 1
```

```
20 PRINT # 1, "FIRST LINE OF FILE EXAMPLE"
```

```
30 CLOSE # 1
```

```
40 END
```



The same result would be achieved by assigning the string to a string variable and then printing the string variable, i.e. line 20 could be substituted with the lines:

```
15 LET M$ = "FIRST LINE OF FILE EXAMPLE"
20 PRINT # 1, M$
```

The next section shows how this data can be retrieved from the file.

Reading from a File

To input data to a program from the terminal the BASIC INPUT statement is used. The INPUT statement can also be used to retrieve data from a file to use as input to the program. The general format is: INPUT (#) channel number, list

where channel can be the communication channel number associated with a file previously opened using the OPEN statement, or zero. If zero is specified the input is from the terminal as for the program INPUT statement.

List can be a single string or numeric variable or a list of variables separated by commas. Also the first item in the list must be separated from the channel number by a comma. The '#' character preceding the channel number is usually optional.

The INPUT # statement line that retrieves data from a file must duplicate the format of the PRINT # statement that wrote the data. Also the type of variable used to store the retrieved data must correspond to the type of data item being retrieved. When the INPUT # statement is to request more than one data item, the data must have been written to the file separated by a string constant comma. This is because the INPUT # statement reads data in the file in the same manner as a program INPUT statement (where the data following a DATA statement is separated by commas). For example, the statement which writes the integers 1 and 2 and the string "THREE" to the file assigned to channel number 1 is:

```
10 PRINT # 1, 1, ",", 2, ",", "THREE"
```

The program line retrieving this data would be:

```
20 INPUT # 1, A, B, Z$
```

When this statement is executed the first data item retrieved from the file is assigned to the variable A, the next to variable B and finally the string is assigned to the string variable Z\$. These variables can then be used in other BASIC statements to perform any desired operation on the data within the program.

The following programs demonstrate how data can be written to and retrieved from a file using BASIC file statements.

```
10 REM FILE EUROTEMPS TO BE WRITTEN TO
20 OPEN "EUROTEMPS" FOR OUTPUT AS FILE # 1
30 READ P$, C, F
40 IF P$ = "" THEN GOTO 130
50 PRINT # 1, P$, ":", C, ":", F
60 GOTO 30
70 DATA "LONDON", 18.7, 65.7
80 DATA "AMSTERDAM", 21.0, 69.8
90 DATA "EDINBURGH", 17.8, 64.0
100 DATA "PARIS", 22.8, 73.0
110 DATA "MUNICH", 22.8, 73.0
120 DATA "", 0, 0
130 PRINT # 1, P$, ":", C, ":", F
140 CLOSE # 1
150 END
```

RUN

December 1982 Maplin Magazine

The program consists of the following lines:

Line 10 — The REM statement serves only as a comment. The characters after REM are ignored.

Line 20 — The OPEN FOR OUTPUT statement creates a new file and assigns it the name "EUROTEMPS". The AS FILE # 1 portion establishes communication channel number 1 as the link between the program in main memory and the file on a peripheral device.

Lines 30, 70 to 120 — The READ statement on line 50 is associated with the DATA statements on lines 70 to 120. When it is executed the READ statement assigns data from the DATA statements to the variables P\$, C and F. Each data line is a string followed by two numeric constants.

Lines 40, 120 — The end of the data is signalled by a null string followed by two zeros. The IF THEN statement tests the string assigned to P\$ to see if it is null. If the condition is true the program control is directed to the CLOSE statement on line 140 which closes the file. Some versions of BASIC have file statements which test whether the end of the file has been reached. If this facility was available on your system it would not be necessary to set up a dummy data item to signify the end of file.

Line 50 — The PRINT # statement writes the variables P\$, C and F to the file associated with channel 1. The data is written to the file separated by string constant commas. This is to enable the data to be retrieved using the INPUT # statement.

Line 60 — The GOTO statement repeats lines 30, 40 and 50 to write all the data contained in the DATA statements to the file.

Line 130 — The PRINT # statement writes the null string and zeros to the file.

Line 140 — The CLOSE statement closes the file EUROTEMPS and disassociates it from communication channel 1.

Line 150 — The END statement signifies program completion.

To write the data to the file EUROTEMPS the program must be executed by typing RUN. After program execution is complete the data contained in the file EUROTEMPS can be made available to any BASIC program.

A program to retrieve the data contained in the file EUROTEMPS is:

```
10 REM DATA TO BE RETRIEVED FROM FILE EUROTEMPS AND
    DISPLAYED ON THE TERMINAL
20 OPEN "EUROTEMPS" FOR INPUT AS FILE # 1
30 INPUT # 1, C$, C, F
40 IF C$ = "" THEN GOTO 70
50 PRINT C$, C, F
60 GOTO 30
70 CLOSE # 1
80 END
```

RUN

LONDON	18.7	65.7
AMSTERDAM	21.0	69.8
EDINBURGH	17.8	64.0
PARIS	22.8	73.0
MUNICH	22.8	73.0

The program consists of the following lines:

Line 10 — The REM statement serves only as a comment.

Line 20 — The OPEN statement causes BASIC to locate the file EUROTEMPS on the peripheral storage device. The FOR INPUT portion of the statement shows that the file already exists and that the data it contains is to be retrieved. AS FILE # 1 associates the file with communication channel number 1.

Line 30 — The INPUT # statement reads the data items from the file and stores them in variables. This duplicates the format of the PRINT # statement on line 50 of the program that created the file. That is, the variables match in type and number, and a comma separates the data items in the file. If this was not the case, BASIC would display an error message when the program is executed.

Line 40 — The IF THEN statement tests for the end of the file. The last data line written to the file consisted of a null string followed by two zeros. When a null string is retrieved from the file the condition is satisfied and the program is directed to the CLOSE statement on line 70.

Line 50 — The PRINT statement outputs the contents of the file as stored in the variables C\$, C and F to the terminal. The variables are separated by commas so each argument is output to its own field. The output from the program is shown after the RUN command.

Line 60 — The GOTO statement repeats lines 30, 40 and 50 until all of the data are read.

Line 70 — The CLOSE statement closes the file EUROTEMPS and disassociates it from communication channel number 1.

Line 80 — The END statement signifies program completion.

BASIC programs are also stored in files. The BASIC commands to store and retrieve programs in files from a peripheral device (the SAVE and LOAD, or OLD commands) have been described previously. There are also BASIC commands to delete files which are no longer required.

INTERFACING MICROCOMPUTERS

Using Parallel Input/Output Ports

by Roy Waters BSc., MSc., C.Eng., F.IEE.

The Function of Parallel Interface Adapters

Introduction

This article deals with how to interface projects to a microcomputer and to program the complete system.

There are two modes of transmission of data between computers and peripherals (external equipment), *serial* and *parallel*. Inside the computer all data transfers are in parallel mode, that is each bit of each data word is assigned a separate line. Serial data transfer, where only one wire is used and the data bits are transferred one after the other is used principally along telephone lines and in other situations where relatively long distances are involved.

For our present purpose we shall consider *parallel* data transfers; the more usual and convenient way of connecting equipment to computer. However, it is still necessary to interpose special circuitry between external equipment and the computer data bus (i.e. the data lines, usually eight in a small computer). See Figure 1.

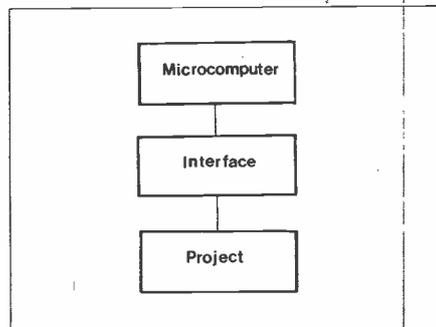


Figure 1. An Interface is necessary between computer and project.

The Need for an Interface Adapter

Data messages from a computer data bus only last for the order of 1 μ s, also data messages to a computer are only allowed to last for about 1 μ s on the data bus otherwise the system would probably crash.

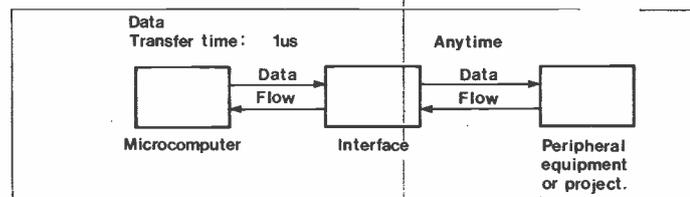


Figure 2. The data transfer rate is modified by the interface.

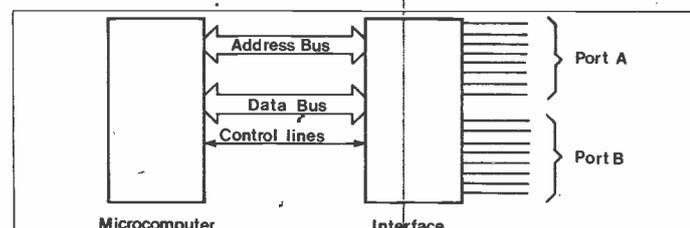


Figure 3. The interface provides two 8-bit data lines for input or output of data.

The functions of the interface device are therefore:

- to capture the data from the computer in a register and retransmit it to the external circuitry "at leisure"
- to hold data from the external source ready for the computer to "snatch it" very quickly
- to perform these operations only when instructed to do so by the computer program.

See Figure 2.

Interface systems

The interface system, Figure 3, will comprise connections to the computer address and data buses and a few control lines. It will provide two 8-bit sets of input/output lines to connect to external equipment.

Most of the work is done by a single IC package. Such packages (or "chips") are appropriately called Peripheral Interface Adapters (PIA), Parallel Input Output (PIO) or Versatile Interface Adapters (VIA), the latter includes timers and serial I/O facilities also which we shall not need to deal with at present.

A few additional logic gates are required to enable the user to choose an address which will not conflict with other operations on his particular computer.

Most current micro computers use micro processors and support devices in the 6800, 6500 or Z-80 families. All of these families have interface packages, but generally speaking they are interchangeable i.e. they will work with other micro processors, but pin-outs and programming will vary.

The following are a selection of such interface adapters. The numbers suggest the families from which they derive: 6820, 6821, Z-80 PIO, 6520, 6522 and 8154. The INS 8154 is related to the 8060 SC/MP but is frequently used with other micro processor systems.

These devices are all similar in principle of operation and use. The 6821 will be considered in particular as it is comparatively easy to understand and use.

Construction of an Interface System

Connections to the Computer

Some microcomputers already have an interface adapter fitted (or a socket for one) with parallel Input/Output ports available from the board edge. If your computer has this facility you may like to skip the following constructional details and concentrate on the programming in the next section. However, that which follows will assist greatly in the understanding of interface adapters even if your computer has a different one from the type specifically dealt with here.

If your computer does not have an interface facility which is readily accessible, read on. You will learn how to construct your own interface system so that your computer may be connected and used with your own projects. Note, however, that your computer must provide the following:

- Access to the Address Bus, the Data Bus and certain control lines (i.e. all these lines must be brought out to the board edge or to a socket to facilitate connection.)
- A wiring or board layout diagram or clear markings on the board identifying clearly the connections.
- A memory map.

If you are proposing to purchase a micro-computer make certain that the one you choose either has these facilities or already has an Interface Adapter (or socket for one) on board. At this stage you may not think of connecting your own circuits to the computer, proposing to use it only for programming, games, calculations or business accounts. However, if you dabble in electronics at all you will soon want to involve your computer, when you realise its potential in this context. Connecting your own circuitry is really quite simple and there is no fear of damaging the computer if appropriate instructions are followed.

Address Decoding

Interface Adapters are accessed via the

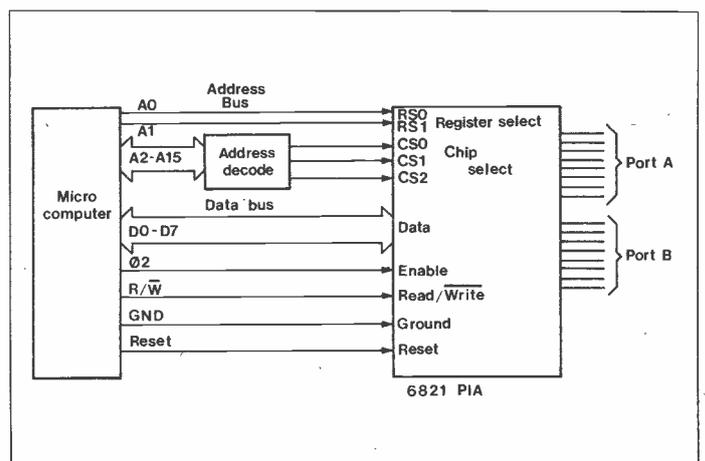


Figure 4. Essential connections between microcomputer and interface adapter.

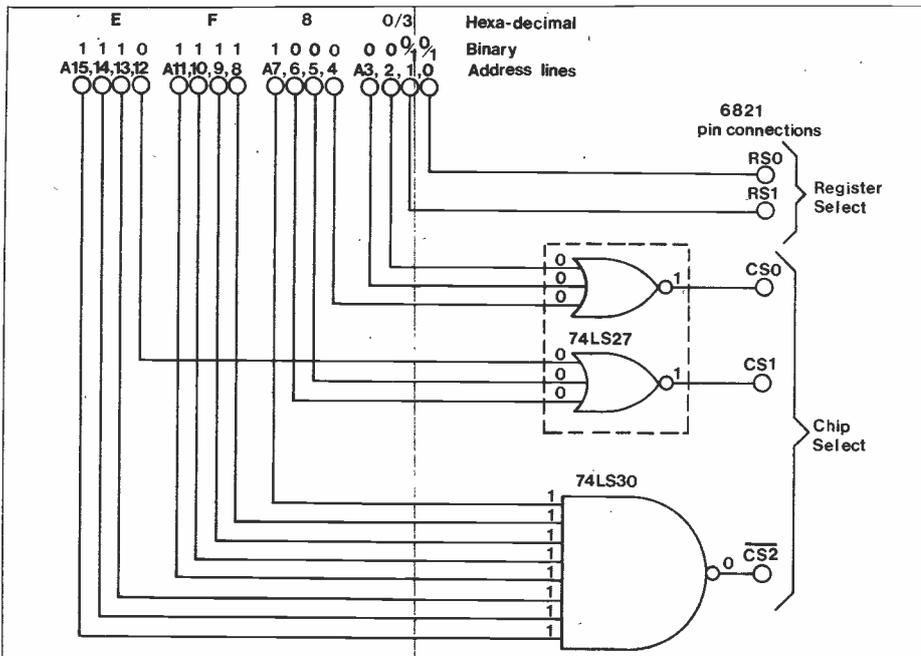


Figure 5. Address decoding.

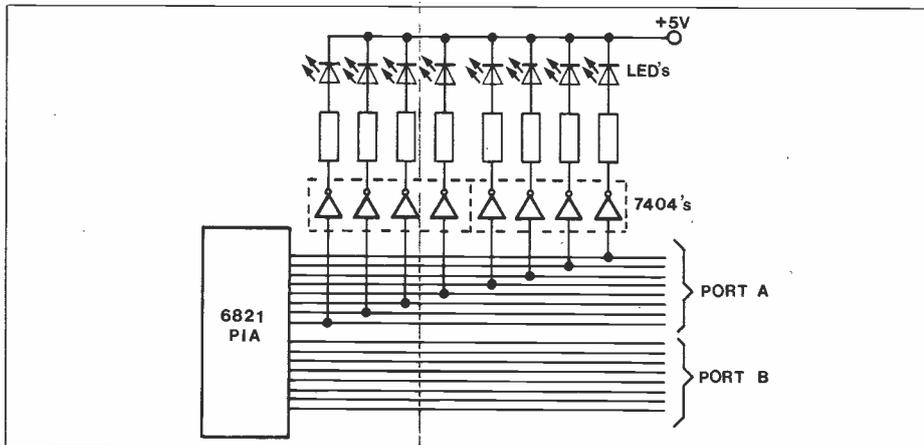


Figure 6. Optional output display.

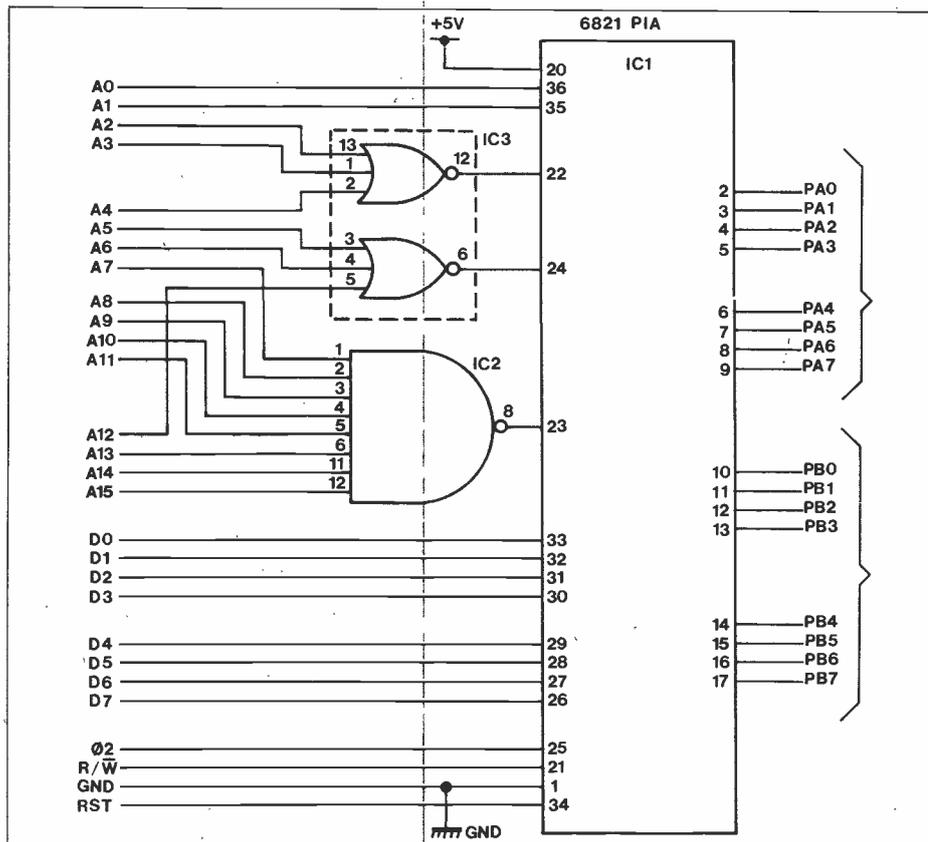


Figure 7. Complete connection diagram of Peripheral Interface Adapter.

Address Bus like RAM or ROM memory and are allocated one or more specific addresses. The address bus lines are therefore connected either directly to the Interface Adapter or through an address decoder.

As indicated in Figure 4 all connections are made directly from the microcomputer to the 6821 PIA except for the address lines. Most of the address lines are decoded externally, using TTL logic gates. These should be from the LS range to minimise bus loading.

One possible arrangement is indicated in Figure 5. To minimise the number of address decoder IC chips to two, utilising all three Chip Select pins on the PIA, a good choice is: 1-74LS30 8-input NAND 1-74LS27 Triple 3-input NOR

Using the NAND gate and two of the 3-input NOR gates provides for 14 address line inputs, eight of which must be High and six Low to enable the 6821 PIA.

The combination shown in Figure 5 gives the PIA addresses as EF80, EF81, EF82 and EF83 (four addresses are necessary to program this PIA, as we shall see later).

With these suggested TTL IC's, any address combination may be used which results in eight address lines being High (1) and six Low (0). A few examples are indicated in Table 1. From this Table note the following:

1. In each example the two least significant digits are XX, because they are always connected, not to the decoder gates, but directly to the PIA pins RS0 and RS1. The next two address lines, A2 and A3 are always designated 0, so that when programming the PIA the least significant four bits will always be 0000, 0001, 0010, 0011 in binary, that is 0, 1, 2, 3 in hexadecimal.
2. The total of 1's is always 8.
3. The total of 0's is always 6.

Hexadecimal:	E	F	8	0/3
Binary:	1110	1111	0100	00XX
or	E	F	4	0/3
	1110	1111	0010	00XX
or	C	C	F	0/3
	1100	1100	1111	00XX
or	C	E	E	0/3
	1100	1110	1110	00XX

Table 1. Some alternative address combinations.

Memory Map

Which address decode combination should be used? Before sticking a pin in to decide this, you must study carefully the memory map of your computer. This will almost certainly be designated in hexadecimal and will indicate the "areas" of address memory already allocated for specific functions, e.g. RAM user memory, operating system in ROM, display, etc. You must choose an address within an empty area. As almost all microprocessors used in small microcomputers have 16 address lines giving 65,536 discrete addresses there should be plenty of available addresses from which to choose.

In addition to the Address and Data bus, line connections and a common Ground it will be noted that R/W and Ø2 connections are made to the PIA. The R/W Read, not Write signal indicates to the PIA whether the computer wishes to read from or write to the PIA. Ø2, the Phase Two clock signal is the timing strobe to ensure that data transfers only take place after the correct address signals have been set up and decoded.

The Input/Output Ports

Each individual bit pin of the two 8-bit Ports can be programmed as either an input or an output by the computer program.

These I/O Ports are all TTL compatible, that is to say they may be connected directly to drive TTL logic gates or be driven by TTL devices. For our present purpose it is sufficient to generalise and say that each Port pin may either be fed from a standard TTL gate or feed one standard TTL gate input (not necessarily 'LS' series TTL).

Since it is comparatively easy to drive any electrical circuitry from TTL and to feed any signals into TTL it follows that the computer can drive or be driven from any electrical circuitry, via the PIA.

More will be said about connections to the Ports in following articles on projects using them. However, for the present purpose of developing and testing the system and learning how to program it, it is very useful to be able to read the state of each Port line. This may be done by connecting LED's as indicated in Figure 6. The input of any standard TTL device may be connected to a Port pin and the output will sink enough current to illuminate a LED adequately using a resistor of between 270 and 330R. If TTL Hex. Inverters are used, a LED will be ON when a logic 1 (High) signal is present on the corresponding Port pin.

For test purposes, when checking Ports as inputs the pins may be connected to Ground or +5V for logic 0 or 1 respectively.

Power Supply

A +5V stabilised supply must be fed to the 6821 PIA and the two decoder TTL gate chips. The total current requirement will be about 110mA. There may well be enough reserve in your computer power supply. However, if indicator LED's also have to be supplied from this source a further 12mA per LED must be taken into account. In this case you are advised to connect 100nF capacitors directly across the 6821 and TTL decoder supply pins, and really it is advisable to do this anyway.

A separate stabilised power supply unit may be used and may well supply any project that is interfaced to the computer as well. There is no problem here, but remember to common the Ground of this supply to that of the computer, but do NOT connect the two +5V lines.

Circuit Diagram

The circuit shown in Figure 7 assumes the PIA address to be EF80/EF83. Remember the Address line connections may be changed to obtain different addresses.

Board Layout I 6821 PIA Only

The board, Figure 8, accommodates the circuit of Figure 7 providing two 8-bit parallel output ports.

A reset button has been included as there might be difficulty locating the computer reset connection. It will be found more convenient not to common the computer and interface RESET lines, since either may then be reset without the other. For testing and many circuit operations it may be found unnecessary to use the manual reset on the interface. The software routine of initialising the ports virtually does this. However, it may be useful as a safety stop button, particularly if the interface is driving motors or servo-systems.

The Veroboard layout has been designed for ease and minimum construction work, and will only take an hour or two to put together. It is suggested that IC sockets be

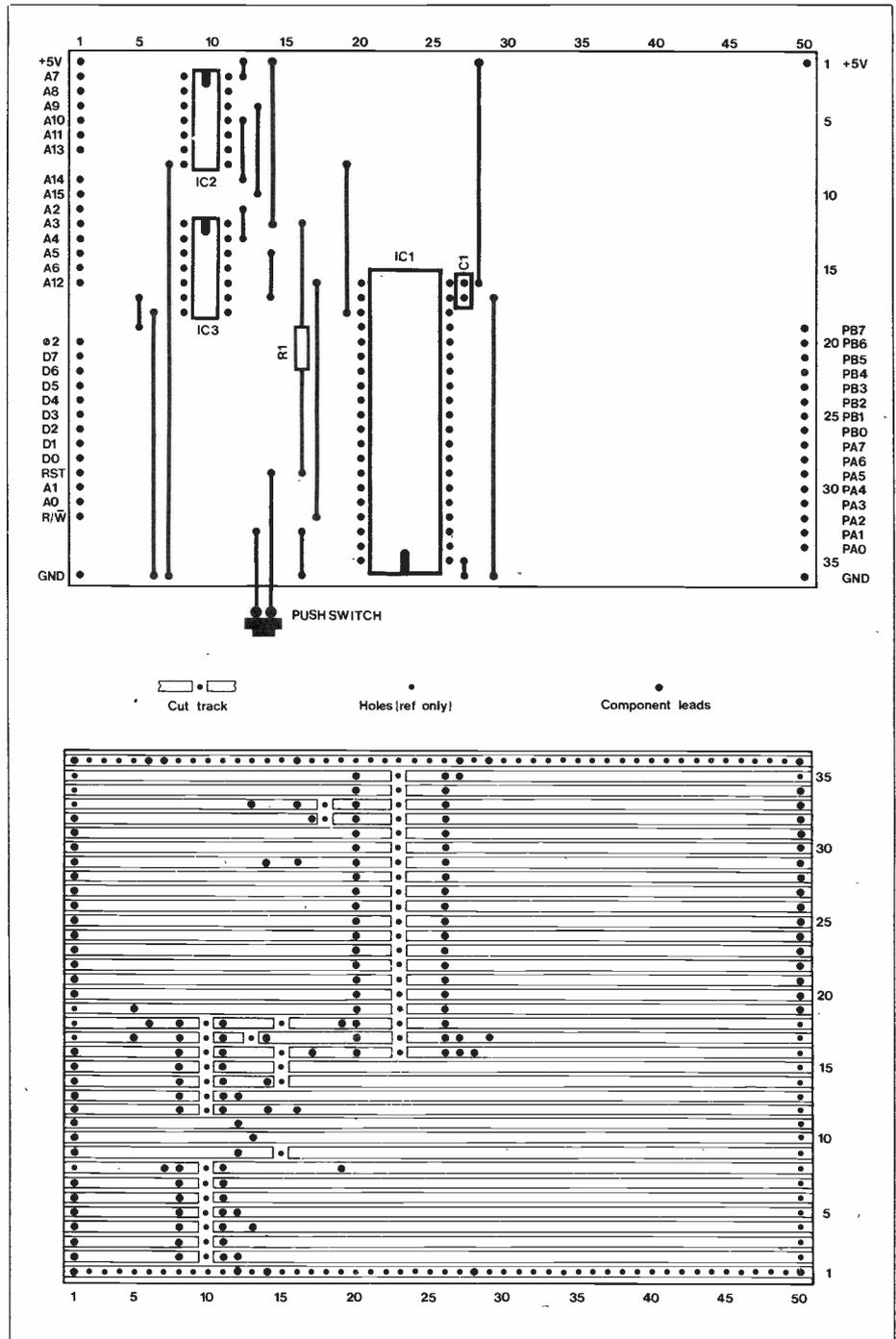


Figure 8. Veroboard layout for 6821 only.

used. These do not object to excessive soldering heat and should you have a fault on an IC it is easily replaced. Certainly use a socket for the PIA package which is relatively expensive and also remember to take the usual static precautions (earth yourself whilst handling).

IMPORTANT NOTE. Observe that the 6821 is mounted "upside-down", i.e. with the identifying mark and pin 1 near the Ground line. The other IC's are mounted with the identifying mark towards the top of the board, i.e. nearer to the 5V rail of the board. The reason for this is so that the 6821 inputs are now on the left and the outputs on the right. The address decoders are mounted so that address lines connect conveniently from the left also.

For ease of construction all vertical connections may be made with uninsulated tinned copper 24 swg wire.

The components have been kept to the left of the board so that, if the larger Veroboard is used (see parts list) there is room to add other circuits to the right, for example LED indicators.

Connections to the Veroboard. The quickest and most convenient connections are made using 0.1in. pitch edge connectors plugged into the board edge. 1/0.6 single strand wire can usually be plugged straight into sockets on a computer board for test purposes. Ribbon cable to a plug which will marry to the computer connector is advisable as a long term arrangement.

Board Layout II 6821 PIA and LED Indicators

LED's can be temporarily connected to the Ports via 7404's as buffers with the aid of a socket breadboard.

As a more permanent feature, it is very useful if a lot of development work is to be done, to connect the LED's on to the PIA interface board as shown in Figure 6.

The advantages are:

1. A visual indication of the state of the Ports.
2. Additional Buffered Outputs (B00 through B07) capable of sinking 6mA per

output with the LED's or 16mA if the LED's are disconnected (48mA if 7416's are used).

- A visual indication of the input signals to the Port, assuming the input circuit can sink the 1.6mA required by the 7404's.

For board and LED economy only eight LED's are shown. By making the vertical connections to the Port lines via Veropins with insulated hook-up wire, it is an easy soldering job to swap between Port A and Port B as the need arises.

PARTS LIST Interface only

R1	4k7	M4K7
C1	100n	YR75S
IC1	6821	WQ46A
IC2	74LS30	YF20W
IC3	74LS27	YF18U
DIL socket	40 pin	HQ38R
DIL socket	14 pin	2 off BL18U
Vero 10347		FL09K

or a smaller board if no extra circuits are to be used on board: FL10L (Vero 10348)

Additional items for the indicators

R2 thru R9	300R	8 off S300R
D1 thru D8		8 off WL32K
IC4,5	7404	2 off QX40T
	2141	FL21X

Programming Interface Adapters

Simplified Functional Diagram

The simplest use of all Interface Adapters for parallel port input/output operations consists of programming the computer to place data on the port lines or read data from the port lines. Most of these devices have additional facilities which are useful but more complex to use. In the interests of simplicity we shall omit these facilities at present.

The simplified functional diagram, Figure 10 is relevant to all parallel I/O adapters as far as their simplest mode of operation is concerned.

The least significant 2, 3 or 4 address lines go straight to the adapter, allowing 4, 8 or 16 discrete addresses to be allocated to programming and using the adapter. Higher order address lines go via the external address decoder to the Chip Select pins. It will have been noted from Figure 4 that the 6821 has only two address pins, allowing four addresses only. These addresses and the data sent to them are decoded by the PIA and fed to four Registers on the right of Figure 10.

Each 8-bit Data Direction Register, DDRA and DDRB (for Ports A and B) determines whether each corresponding bit in the 8-bit Data Registers DRA and DRB shall be an input or an output.

0 defines as an input
1 defines as an output

Example: If DDRA is loaded with 15 (decimal), that is 0F (hex) or 0000 1111 (binary) then —

DDRA: 0 0 0 0 1 1 1 1
DRA: PA7 PA6 PA5 PA4 PA3 PA2 PA1 PA0
← inputs → ← outputs →

The process of defining the Data Direction is referred to as initialisation of the adapter.

The process of initialisation and writing data to a port is precisely the same as writing data to a specified memory location. Similarly reading data from a port is the same as reading data from a specified memory location.

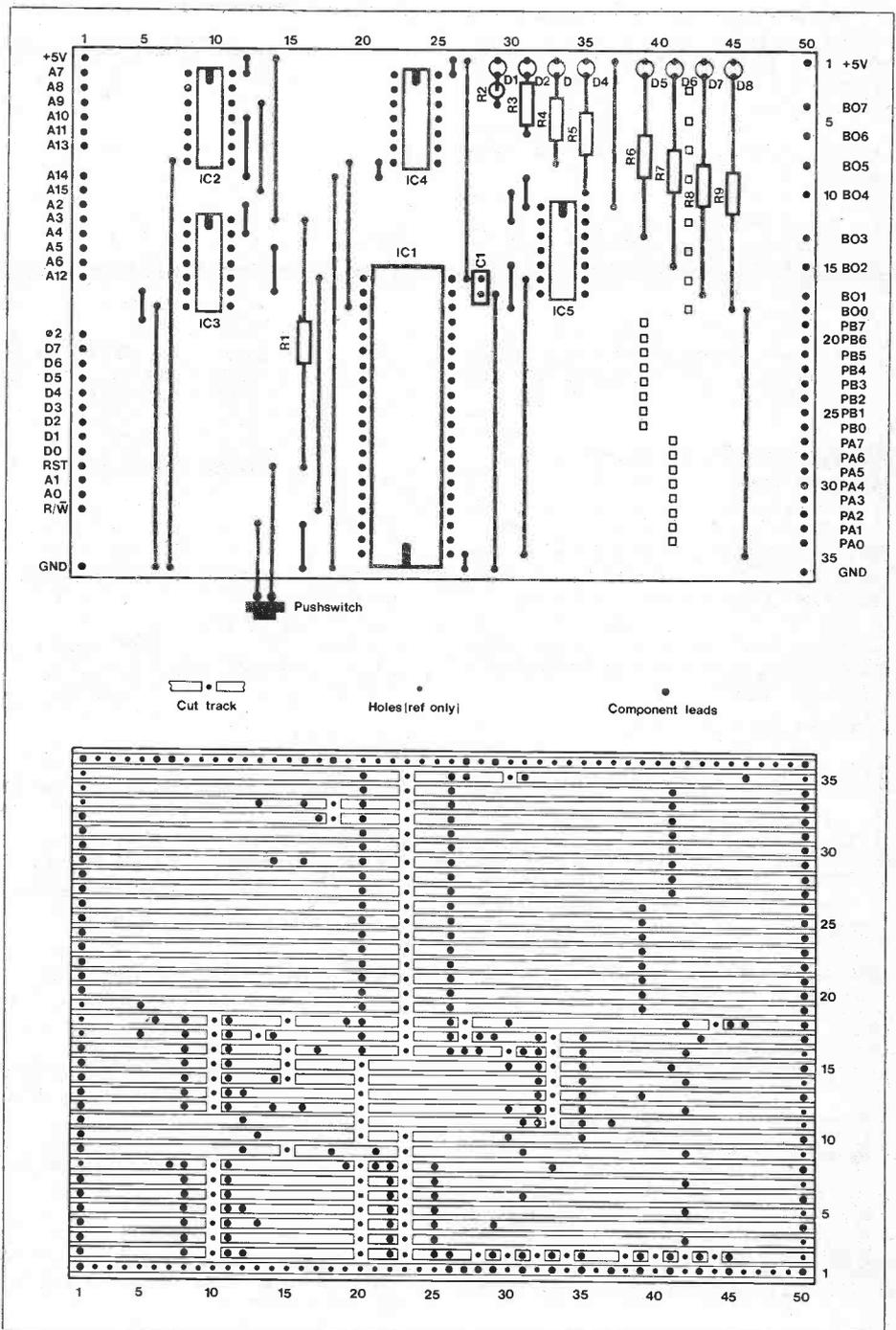


Figure 9. Veroboard layout for 6821 with LED indicators.

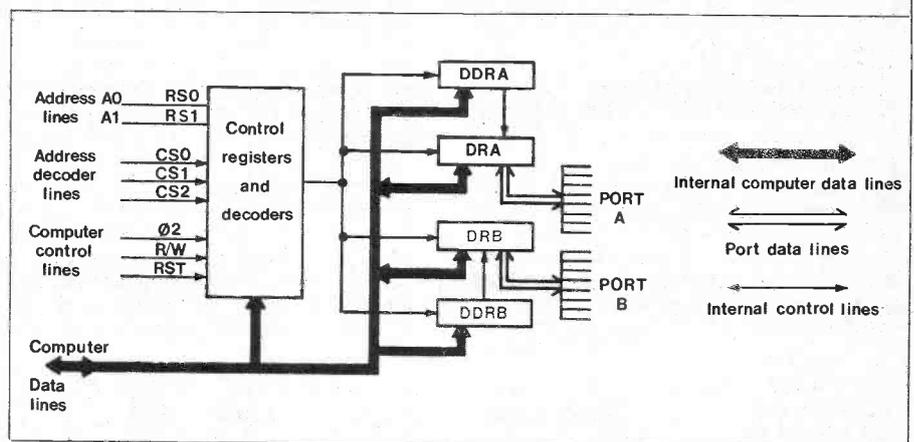


Figure 10. Simplified functional diagram of the Peripheral Interface Adapter.

References

- "Microcomputer Components" — Motorola R6500 Hardware Manual
- Inc 1979. R6500 Software Manual — Rockwell International.
- "Superboard II Users Manual" — Ohio Scientific Inc. Microcomputer Components — Motorola.

The computer may be programmed to perform these functions in machine code, Assembly Language or in a High Level Language (usually BASIC in the case of microcomputers).

It is, of course, much easier to program in BASIC. However, the BASIC interpreter MUST:

Either have the POKE and PEEK instructions to enable specified address locations to be accessed (some microprocessors use symbols instead of the words Poke and Peek but the effect is the same).

Or have BASIC statements enabling the user to write subroutines in machine code in order to access specified addresses.

To Program Port A as all Output lines

The following assumes that the address decoder has been connected for addresses EF80/EF83. If some other address has been wired this must be used, but note the least significant character will be the same.

For Port A to be all outputs the following locations must be addressed and loaded with data as follows, and in the sequence shown in Table 2.

Example Suppose in the table that nn=A6 (Hex)

This is 1010 0110 (binary).

Then a High (nominal 5V) signal would appear on pins PA7, PA5, PA2 and PA1.

A Low signal would appear on pins PA6, PA4, PA3, PA0.

Once the first three lines in the above programming sequence have been run to initialise the Port, the operation of loading Port A with data:

Location	Data
EF80	nn

may be repeated for different values of nn, giving different output patterns.

Programming the PIA in 6502 Machine Code

If your computer uses a 6502 microprocessor, you are using PIA addresses EF80/EF83 and you can use Page 4 (04) of memory for your programs, then the program shown in Table 3, will load the output binary pattern 1101 0011 (D3 in hex) on to the Port A pins.

Programming in BASIC

Using BASIC all Hexadecimal numbers must be converted to decimal numbers first, unless your version of BASIC allows direct usage of Hexadecimal numbers (some do).

The following BASIC program will load the output binary pattern 1101 0011 (D3 hex.) on to the Port A pins.

EF80 (hex.)=61312 (decimal)

D3 (hex.)=211 (decimal)

FF (hex.)=255 (decimal)

(Note that some BASIC interpreters use symbols instead of the words POKE and PEEK, in which case the following program will need to be modified.)

	Remarks
30 A=61312	
40 B=A+1	
50 POKE B,0	EF81=0
60 POKE A,255	EF80=FF
70 POKE B,255	EF81=FF
80 POKE A,211	EF80=D3
90 END	

A good check that all port lines are working correctly is to connect LED's to all lines and write a BASIC program to count and output data to the Port from 0 to 255.

Location (Hex)	Contents (Hex)	Remarks
EF81	0	Next instruction to DDRA
EF80	FF	DDRA loaded 1111 1111 1111 1111
EF81	FF	Next instruction to DRA
EF80	nn	Loads the binary pattern equivalent to nn on to Port A pins.

Table 2

Location	Contents	Mnemonic, Data	Comments
0400	A9,0	LDA IMM 0	
0402	8D,81,EF	STA Abs	EF81=0
0405	A9,FF	LDA Imm FF	
0407	8D,80,EF	STA Abs	EF80=FF
040A	8D,81,EF	STA Abs	EF81=FF
040D	A9,D3	LDA Imm D3	
040F	8D,80,EF	STA Abs	EF80=D3

Table 3

This can follow the above program thus:

```

80 INPUT T
90 FOR X=0 TO 255
100 POKE A,X      Write X to Port A
110 FOR Y=1 TO T
120 NEXT Y        Time Delay,
                  function of T

130 NEXT X
140 END

```

Try out the program with T=200. Alter the value of T to obtain a count speed slow enough to observe each count.

To Program Port A as all Inputs

To do this the Data Direction Register A (DDRA) must be loaded with all zeros.

Location (Hex)	Contents (Hex)	Remarks
EF81	0	Next instruction to DDRA
EF80	0	DDRA loaded with 0000 0000 0000 0000
EF81	FF	Next instruction to DRA
EF80	—	Read from this location

The following BASIC program will read the binary pattern of signals connected to Port A and print out the decimal equivalent. (With some versions of BASIC the program can be modified to print out in hexadecimal, making it easier to check the binary equivalent.)

```

20 A=61312
30 B=A+1
40 POKE B,0      EF81=0
50 POKE A,0      EF80=0
60 POKE B,255    EF81=FF
70 M=PEEK(A)     Read EF80
80 PRINT M
90 END

```

Before running this program connect the Port A output pins as follows:—

PA0,1,2,4 to 5V.
PA3,5,6,7 to Ground
giving a binary pattern of 0001 0111 (17 (hex.) 23 (decimal))
After RUN the printout should be 23.
Check with other input patterns.
In the above program replace the last line with 90 GOTO 70
then as you change the connections the new output will appear on the screen.

Summary of Programming Instructions for the 6821 PIA

In Table 4 XXX represents the first three hexadecimal characters of the PIA address. If this has been wired as EF80/3 then XXX=EF8.

Mix of Inputs and Outputs

To find the correct data to load into the Data Direction Register proceed as follows:

1. Decide which Port lines are to be inputs and which outputs.
2. Tabulate thus:—

Port bit:	7	6	5	4
Input or Output:	in	out	in	in
Corresponding DDR:	0	1	0	0
Hex. Equivalent:	4			
Port bit:	3	2	1	0
Input or Output:	out	out	in	in
Corresponding DDR:	1	1	0	0
Hex. Equivalent:	C			
(for example)				

Note For INPUT load 0
For OUTPUT load 1

Therefore, in this example instead of loading FF or 0, 4C must be loaded at the appropriate instruction.

	Address	Data	Remarks
Port A.	XXX1	0	Next instruction to DDRA
Either	XXX0	FF	All lines outputs
or	XXX0	0	All lines inputs
	XXX1	FF	Next instruction to DRA
Either	XXX0	nn	Write data nn to Port A
or	XXX0	—	Read data from Port A
Port B.	XXX3	0	Next instruction to DDRB
Either	XXX2	FF	All lines outputs
or	XXX2	0	All lines inputs
	XXX3	FF	Next instruction to DRB
Either	XXX2	nn	Write data nn to Port B
or	XXX2	—	Read data from Port B

Table 4

To initialise Port B for the above input/output pattern load the following:—

```

XXX3 0 Next instruction DDRB
XXX2 4C Defines inputs/outputs
XXX3 FF Next instruction DRB
XXX2 To access Port B
  
```

It is advisable to use Port B for mixing inputs and outputs. This Port has Tri-state buffers, so connections to the lines designated as outputs will not affect input readings. However, it is not very likely that lines designated as outputs will acquire a voltage of any significance from external sources so if it is necessary for BOTH Port A and Port B to have a mix of I/O there should be no trouble.

BASIC Program to Read/Write Port B

Suppose the following is required:—

```

Port B Bit: 7 6 5 4 3 2 1 0
Designation: Inputs Outputs
DDR B: 0 0 0 0 1 1 1 1
Port to output: 0 0 1 1
DDR B=OF(hex.)=15(decimal)
DR B=03(hex.)=3(decimal)
EF82(hex.)=61314
20 A=61314 EF82
30 B=A+1
40 POKE B,0 Next instruction to DDRB
50 POKE A,15 Define I/O bits
60 POKE B,255 Next instruction to DRB
70 POKE A,3 Load 0011 in outputs
(3 decimal)
80 D=PEEK (A) Read Port B
90 PRINT D
100 END
RUN
  
```

If the Port B input lines have input signals as follows:—

```

PB7 PB6 PB5 PB4
0 1 0 1
  
```

then the printout would be 83 (decimal) i.e. 53 (hex.)

The PEEK statement reads all 8 bits of the Port. In this case it reads the value 3 (decimal) previously POKEd to the 4 output bits, plus 80 (decimal) present on the input lines.

In general the PEEK statement will read the signals on the Input lines plus the latest value to be POKEd to the output lines. This is because once a signal has been POKEd to the outputs it is held on the output lines of those bits of the Data Register programmed as Outputs until it is updated.

A number POKEd to a Port containing bits programmed as inputs will not affect these input lines.

At first reading the programming of I/O Ports may appear a little complicated. The easiest way to learn to program a PIA is to build the system, connect LEDs and signals to the Port lines and try it out.

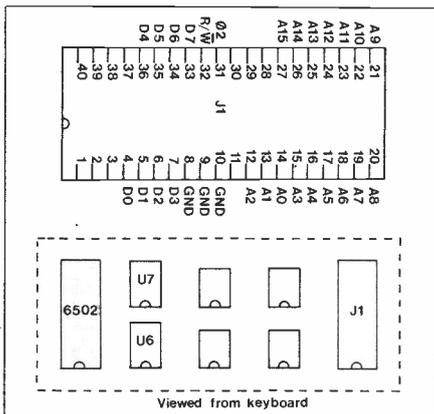


Figure 11. Superboard II J1 socket designations and location of sockets.

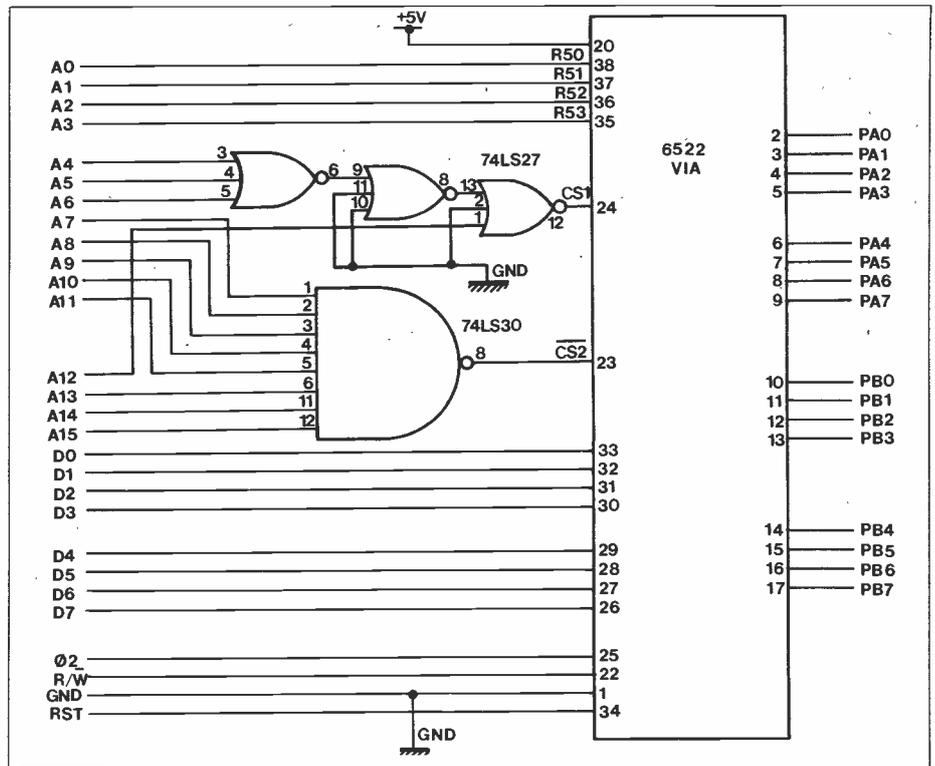


Figure 13. Circuit diagram when using the 6522 VIA.

Appendix A For owners of Superboard II or UK101 microcomputers

These microcomputers are readily connected to the interface system described above. However, some owners of Superboard II may feel they have insufficient information to proceed with confidence.

All the necessary bus outputs are connected to the 40-pin socket, designated J1 at the bottom right hand side of the board. The pin connections are shown in the diagram, Figure 11. Note that all DIL sockets and IC's on the Superboard II are "upside-down" when viewed from the keyboard and pin 1 is in the bottom right-hand corner of the socket.

Temporary connections to J1 may be made by pushing 1/0.6 solid-core wire into the sockets, but you are recommended to use a 40-pin DIL "Header socket" and use multicore ribbon cable to connect the interface system as a more permanent feature.

If 8T28 data direction buffers are NOT fitted in positions U7 and U8 (16-pin sockets, lower centre of board) there is no connection between the computer Data Bus and the designated sockets on J1.

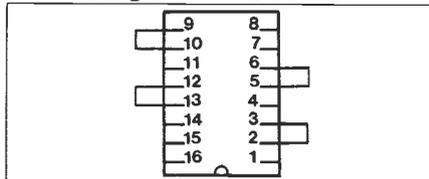


Figure 12. Superboard II connections for sockets U6 and U7.

You are advised NOT to use 8T28 buffers as the Superboard connections may not hold these in the Tri-state (high impedance), but in the Read Mode when quiescent. In this mode any signals applied to the external data bus connections may cause a system crash. Instead it is necessary to use jumpers to connect relevant input and output pin sockets of the U7 and U8 DIL sockets, as indicated in Figure 12. These connections may be made with 1/0.6 solid-core wire (again note that the socket connections are "upside-down"). The connections for U7 and U8 are identical.

Appendix B Use of other Interface Adapters

Owners of microcomputers using interface adapters other than the 6821 should find programming details in their computer manuals. Alternatively data sheets should provide the programming information necessary, although sometimes a little difficult for the newcomer to understand.

6522 Versatile Interface Adapter

Information on this device is included here as a number of microcomputers use it. Some constructors may prefer to pay a little extra for an adapter having two timers and a serial interface as well as the parallel ports.

Circuit Diagram

It will be noted that the circuit diagram, Fig. 13, is almost identical to that of Fig. 7. The 6522 pinouts are slightly different and address lines A2 and A3 are connected directly to the VIA. In the software programming that follows these lines will be zero always, however by connecting them to the address bus the Timers and the Serial I/O may also be used.

Programming the 6522 for Parallel I/O

The three most significant hex. address characters depend upon the address decoder connections and will vary from one system to another.

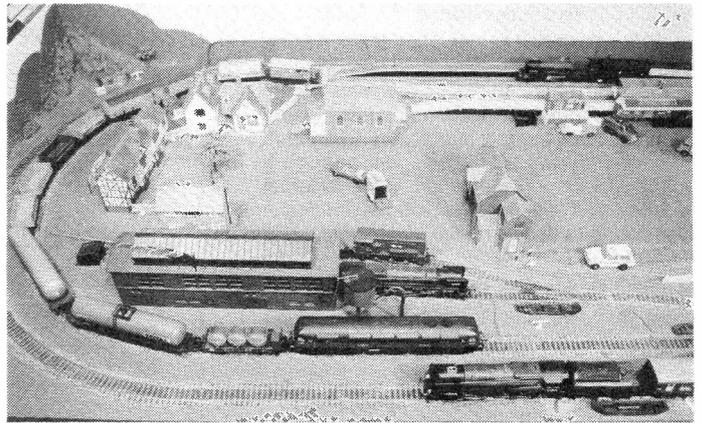
All sixteen variants of the least significant hex. character are used for programming the adapter i.e.: XXX0 thru' XXXF. For Parallel I/O only XXX0 thru' XXX3 are used.

	Address	Data	Remarks
Port A	XXX3	pp	Initialise DDRA
	Either XXX1 or XXX0	nn —	Write data to Port A / Read Data from Port A
Port B	XXX2	pp	Initialise DDRB
	Either XXX0 or XXX0	nn —	Write data to Port B / Read data from Port B

The data pp initialises bits as outputs or inputs 1 for output 0 for input in the same way as for the 6821.

MODEL TRAIN PROJECTS

- ★ Train Head and Tail Lamp Control
- ★ Automatic Loop Control
- ★ Track Circuiting



by Robert Kirsch

This article describes several circuits that may be added to a layout using the digital control system described in issues 2 and 3 of Electronics (order numbers XA02C and XA03D). These circuits have been in use on the authors 00 gauge outdoor layout for some time, and have been found to improve the realism and enjoyment of the railway greatly.

Train Head and Tail Lamp Control

This circuit enables the head and tail lamps to be operated automatically from the receiver unit fitted in the locomotive and controlled by the direction of travel.

This unit may be fitted to dual ended locomotives to enable the headlamps to light only in the direction of travel, or to a complete train that is to operate in both directions, for example an H.S.T. set, providing white lights at the front and red lights at the rear whichever way the train is moving.

The circuit is fed from the output of the decoder in the receiver module described in issue 2 figure 5.

When a receiver is selected by the control unit and the speed control advanced, pulses appear at one of the two outputs of the decoder, the num-

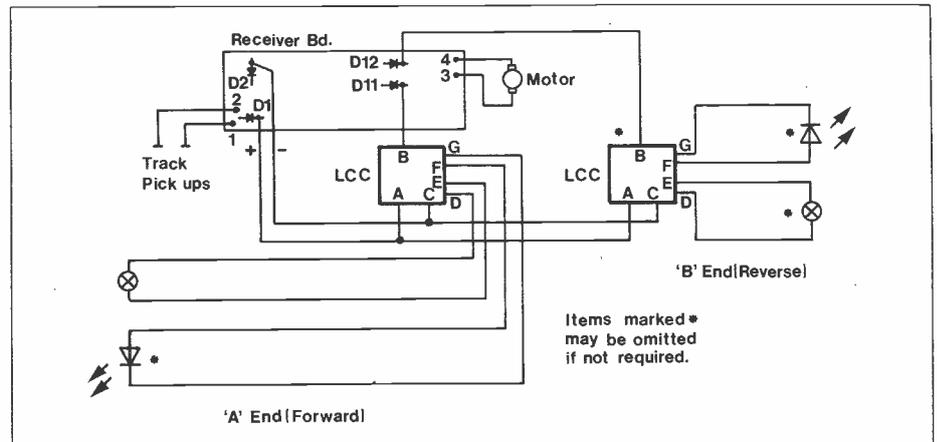


Figure 2. Typical locomotive installation

ber of pulses being dependent on the speed setting. These pulses are fed via R1 and D1 (figure 1) to C1, causing it to charge rapidly. It is prevented from discharging when the input goes low by D1 being reverse biased.

The voltage developed across C1 is used to turn TR1 on, via R2, and in so doing causes current to flow through the lamp in the collector circuit. R3 reduces the voltage to enable a 12V lamp to be used. The lamp and the LED are effectively in series across the supply, so that when TR1 is on the LED is extinguished, and when it is off the LED will light via the resistance of the bulb filament. The lamp will not light because the LED only draws about

10mA as R4 is in series with it.

Installation

Examples of installation for various applications are shown in figures 2 and 3. It will be seen that to control headlamps at both ends of a locomotive two control circuits will be needed. In the case of a complete train it is necessary to electrically couple all vehicles together. This is useful as it enables several track pick-ups to be made along the length of the train, also making carriage lighting possible.

Three wires are required to enable headlamp control. A bridge rectifier and control circuit are required at the non-driving end of the train, the pulse

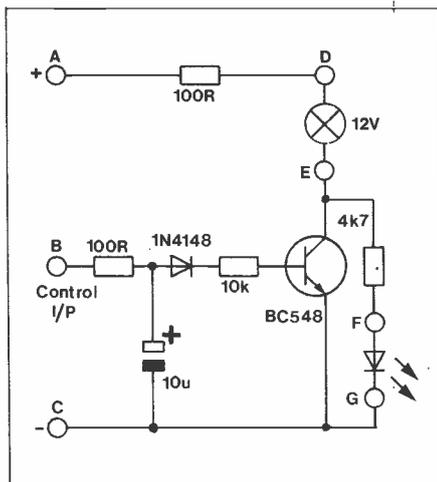


Figure 1. LCC schematic

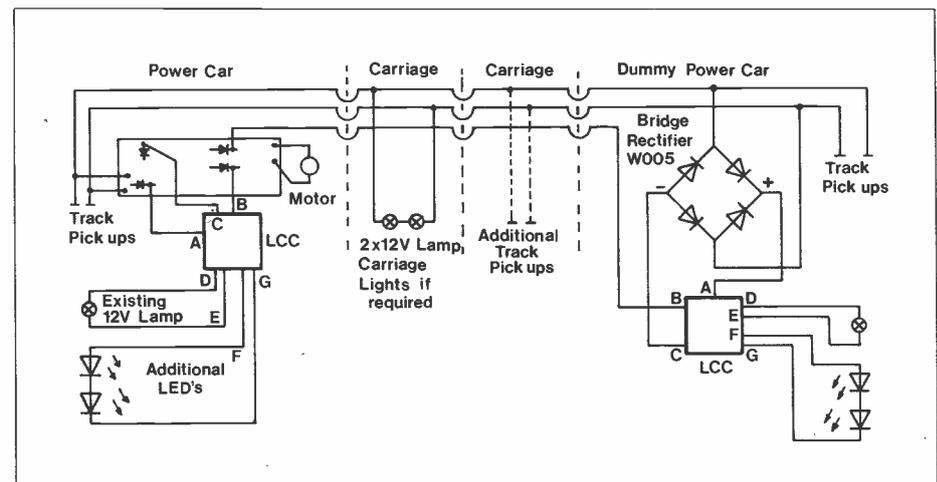


Figure 3. Installation in HST set

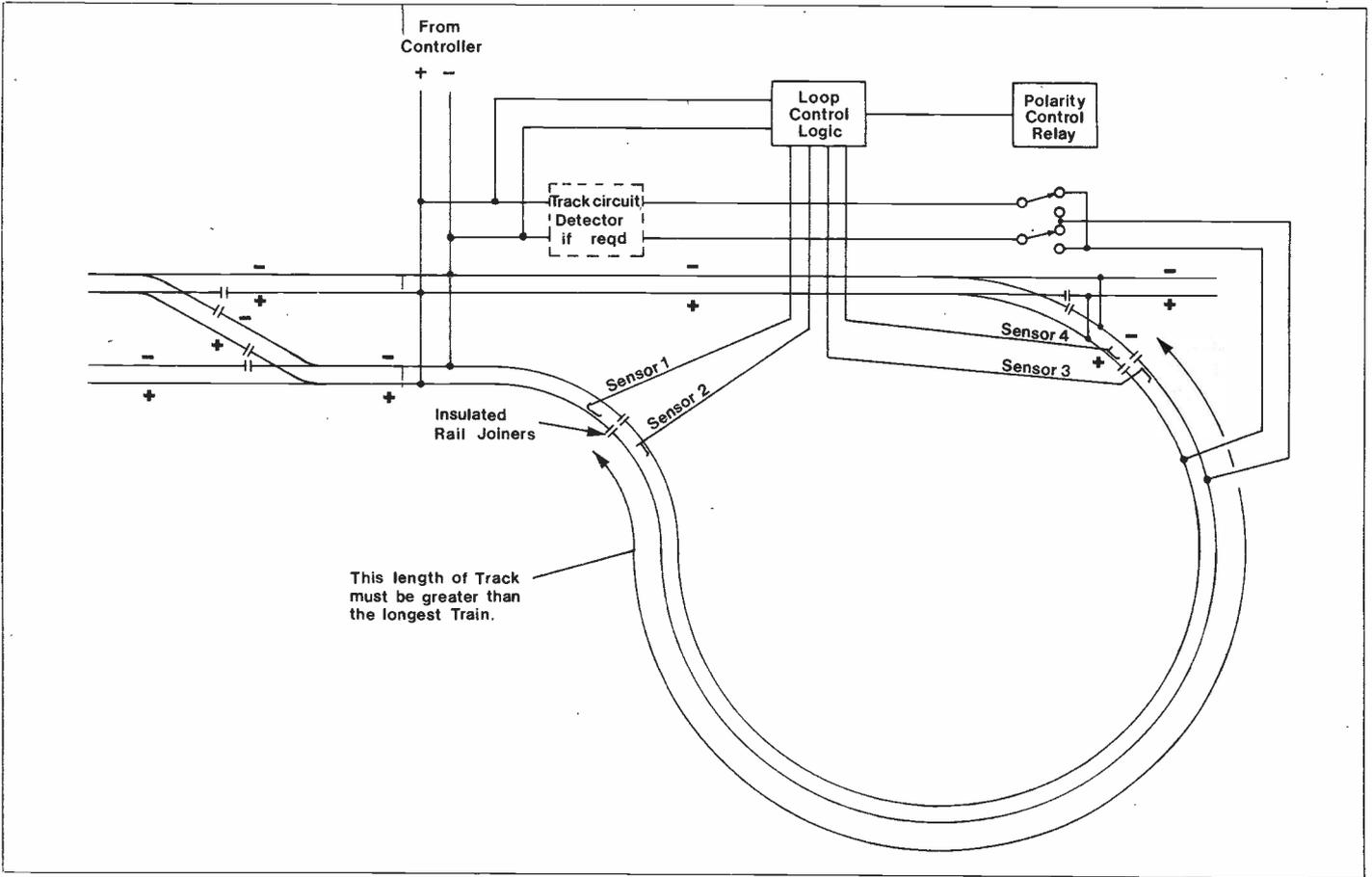


Figure 4: Loop control schematic.

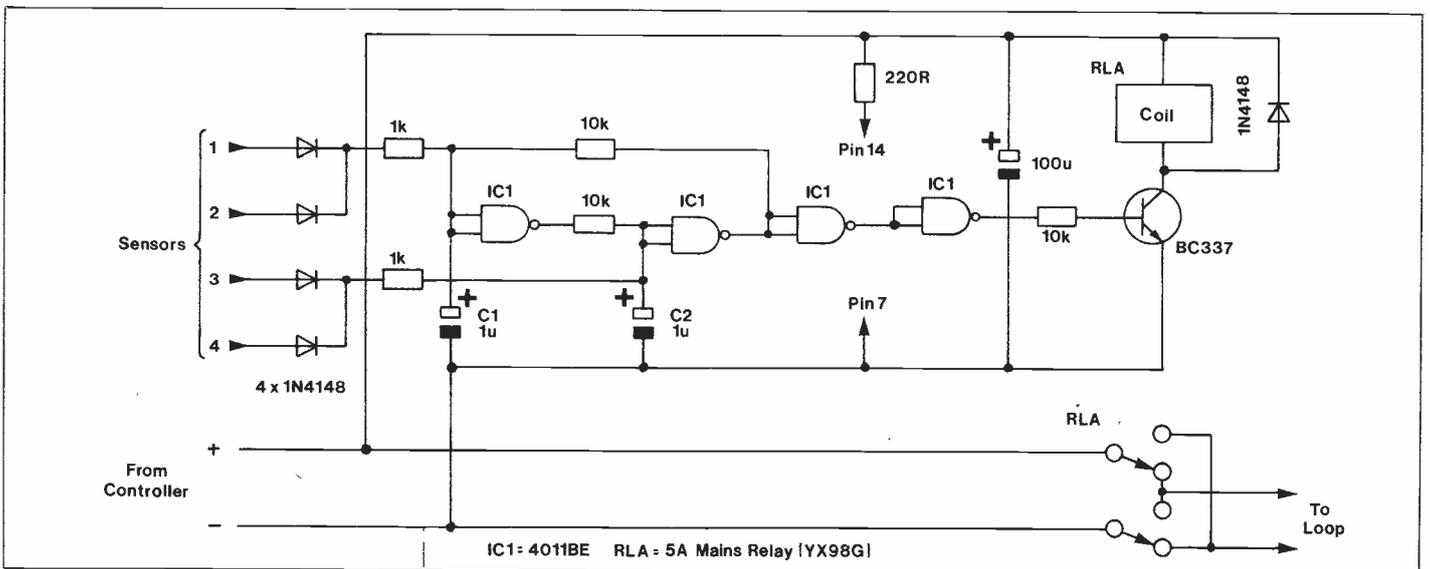
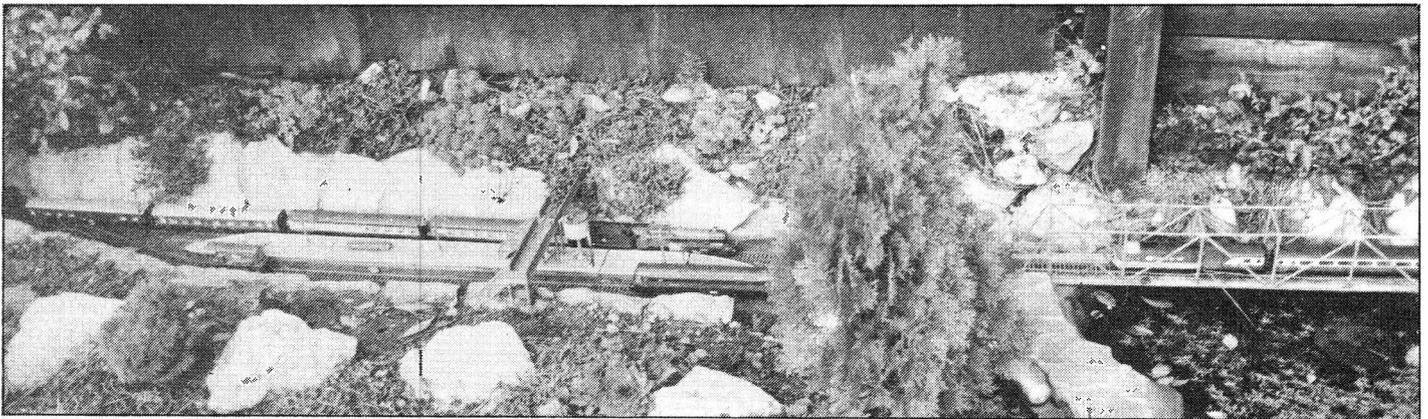
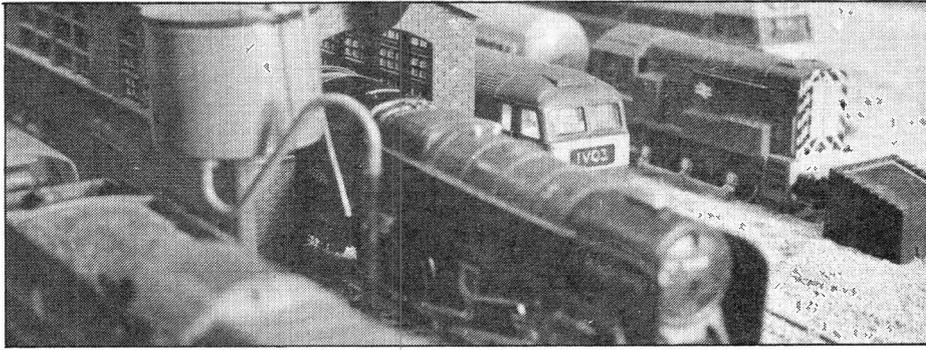


Figure 5: Loop control circuit.



signals being fed on the third wire. A very flexible type of wire should be used between carriages, and the wire used in telephone cords has been found suitable for 00 gauge applications. Enough slack must be left to allow for negotiation of sharp curves. A single lamp may be used for the headlamps, and flexible light guide (XR56L) can be used to transfer the light to the front of the vehicle. The ends of the light guide may be shaped into a lens by holding it near a heat source and allowing the plastic to melt and form a small dome. Two LEDs may be used if required by connecting them in series, although it may be necessary to try several LEDs before

installation, to ensure that they are both of the same brightness.

Automatic Loop Control

Loops on model railway systems present a problem due to the conflict of track polarity when entering or leaving the loop. The system described here automatically detects when a train is entering or leaving the loop and sets the polarity accordingly. The receivers used in locomotives are fed from a bridge rectifier, and are therefore not affected by the change in polarity of the track, thus there is no pause during switching.

Figure 4 shows a typical loop arrangement with the four sensors, two placed at each end of the loop. These sensors are simply made from gold plated wire and arranged so that the wheel flanges of the train make contact between one running rail and the sensor wire. This arrangement has been found very reliable in practice, and may be used in other applications where accurate train position detection is required.

Figure 5 shows the circuit of the automatic loop control and it can be seen that a positive input from any of

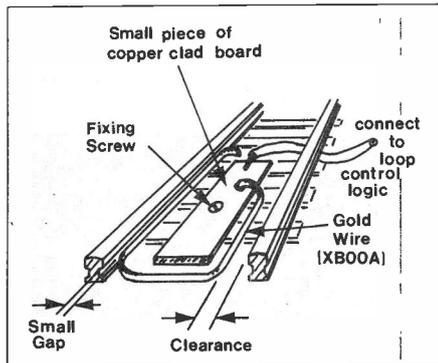


Figure 6: Track sensor detail.

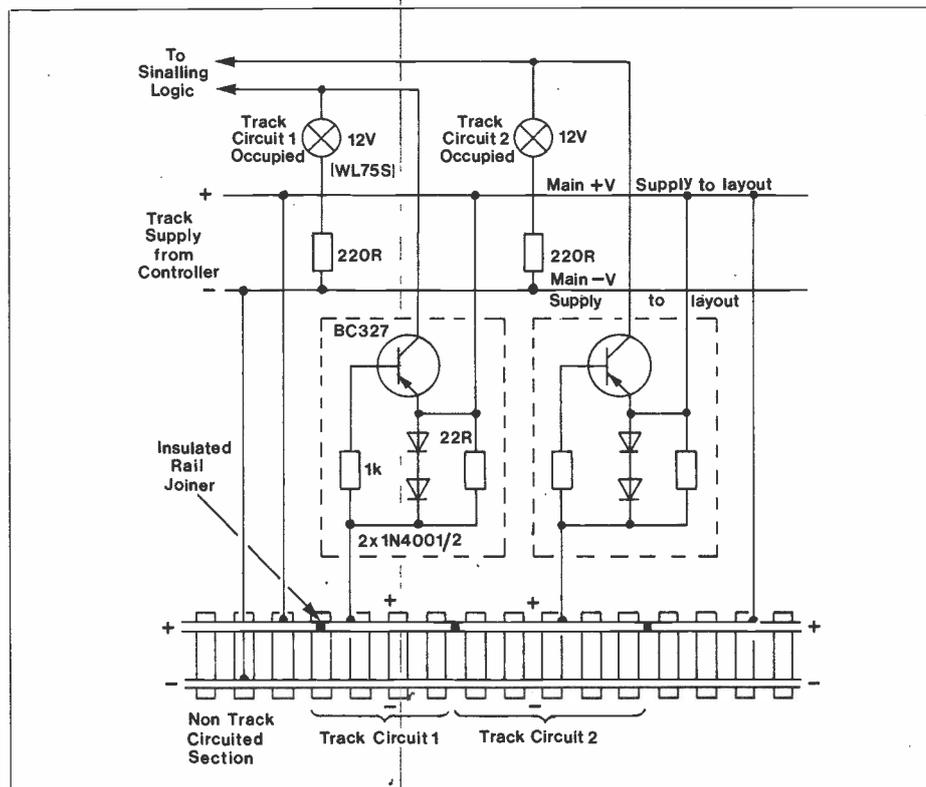


Figure 7: Track circuiting.

the track sensors will cause the bi-stable, formed by gates 1 and 2 of the IC; to change to one state or the other, depending on the sensor activated. The inputs from the sensors are decoupled by C1 and C2, to prevent false operation due to inevitable voltage spikes found on model railway systems.

Installation

The system should be installed referring to figure 4 as a guide, but do not worry at this stage about the polarity of the connections to the loop section. When the sensors are in position check their operation by shorting them to the appropriate running rail with a screwdriver blade, to ensure that sensors 1 and 2 cause the relay to operate and 3 and 4 cause it to release.

The polarity can now be tested by driving a train into the loop, if the protection circuit on the controller trips as soon as the train enters the isolated section the connections to the loop must be reversed, and a further test carried out to ensure that all is now correct. It will be noted that the distance between the two inner sensors must be greater than the longest train that is likely to use the loop, to prevent both sets of sensors being activated at the same time.

Track Circuiting

The circuit shown in figure 7 provides a means of detecting when a train is in a particular section of the track. This information may be used to provide an indication on a track layout diagram, as well as being interfaced with signalling equipment.

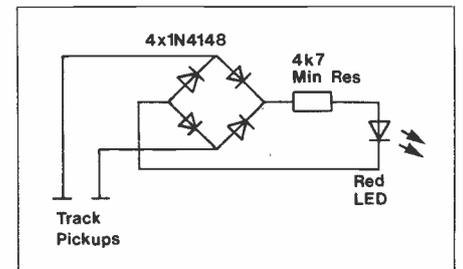


Figure 8: Tail lamp circuit.

The individual sections of track which need to be equipped must be isolated at both ends on the positive rail only, and fed by the common supply from the controller via the detector circuit. A single wire feeds from each detector and is connected via a 12V bulb to the negative supply (EARTH). The lamp lights when current is drawn from the track due to TR1 (figure 7) being turned on by the volt drop across D1 and D2. The two diodes only allow a reduction of about 1.4V, and do not affect the operation of the system. It should be noted that only vehicles that draw current through their wheels will be detected by the track circuiting so it is necessary to provide track pickups at both ends of the train. This may be accomplished by connecting a resistor of about 470 ohms between both wheels on an axle of the last vehicle, or a tail lamp may be provided using the circuit shown in figure 8.

CLASSIFIED

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SINCLAIR DIGITAL Multimeter £50. Tandy AM/FM stereo tuner £30. Linear 5 watt stereo amplifier £10. All in good working order. Lathaen, 19 Schimel St., Sunderland, Tyne and Wear.

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OFFERS PLEASE for any of the following. Maplin ASCII keyboard and interface, Cherry stereo phones, Foster dynamic microphone, unused TTL logic circuits. Ralph, 14 Knightley Rd., Exeter EX2 4SR. Tel: (0392) 75896.

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HANDBOOK including circuit for Eddystone EC10 communications receiver. £2.20. 4 Greathead Road, Leamington Spa, Warwickshire, CU32 6ES

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REGA R200 arm. SME 3009 arm. Technics SU300 M.C. cartridge and head amp. Fri Mk II cartridge and FRT-3 transformer. Sony EL7 El-cassette Deck. Offers. Dave Ebchester 561212 (N. England).

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For the next issue your advertisement must be in our hands by 5th January 1983.

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WANTED. TRANSISTORS C1389 or C1417 or knowledge of equivalents. Tel: Chelmsford 69009.

WANTED SERVICE manual for Teletypewriter D52 oscilloscope. P. Midgley, 17 Glenthorne Avenue, Yeovil, Somerset BA21 4PG. Tel: 71739.

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MECCANO WANTED, including wheels, pulleys, cogs, axles, motors, angle strips, brackets, nuts, bolts, etc. etc. A. Askew, 86 Katherine Road, Thurcroft, Rotherham, S. Yorks S66 9HR

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WANTED 4 PCBs BB55K to build 2 Maplin Dynamic Noise Filters. Offers to A.R.C. Crawford, BM Box 6422, London WC1N 3XX

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MAPLIN 5600s synthesiser for sale. Complete component schedule. Requires only some inter-board wiring to complete very high standard of construction. Any good offer considered. Tel: Harpenden 61695 or Staverton 434.

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YAMAHA CS-5 synthesiser for sale. Excellent condition £195. Tel: Wilmslow (0625) 526517.

MAPLIN BASIC organ (single 49 note keyboard). Complete but not working. For sale as I'm too thick to do the fault finding! £60. Phone: Walsall 28911. Ask for Mark Neal.

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ACORN ATOM. 12K RAM. 12K ROM. All leads, manual + PSU included. £190. Dave, 2 Western Villas, Church Rd., Kennington, Ashford, Kent. Tel: (0233) 23077.

ATARI 800 16K plus Basic programme recorder. 2 joysticks. Missile Command. Star Raiders, Jaw Breaker, Darts, Jigsaws, Galaxians. Fully boxed and in mint condition. Bargain — £450. Tel: 01-764 1504 (evenings).

AVENGERS CARTRIDGE for VIC-20 computer. As new, in box. £15 or nearest offer. Write to Miss Lorna Findlay, The Manse, St. Monans, Fife, Scotland.

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ZX81 + 16K RAM + tape recorder and TV. Lots of software. £70 o.n.o. Tel: 0634 721062 (evenings only).

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TWO MICROCOMPUTERS one 16K ZX81 with Maplin Keyboard. One 8K UK101. Both with software. Offers phone: (06615) 3258. After 6p.m.

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PSI COMP 80 Computer, 36K RAM, full ASCII keyboard, own PSU and VDU. Well made steel case. Cost over £400. Offers around £200 o.n.o. Tel: Derby (0332) 810543.

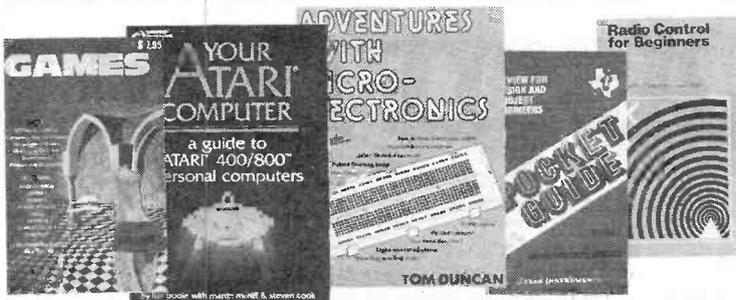
EIGHT 2114 200ns. Two 74LS138. Thirty D.I.L. sockets. ZX81 edge connector. 75ml pcb. Photo resist lacquer. All unused. £9.50 for lot. Also details for making expandable memory for ZX81 from above components. Tel: Chris, (0254) 771303.

ZX81 INVERSE video m/c routine controlled by Basic. Requires 8K ROM + 16K RAM. Send 90p + s.a.e. K. E. Rayner; 25 Mill View, Gazeley, Newmarket, Suffolk CB8 8RN.

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GA16S	Panic Button PCB	Price £1.25	LW96E	Sound Generator Kit	Price £10.95
GA69A	Programmable Timer PCB	Price £1.49	LW97F	Panic Button Kit	Price £4.50
GB09K	Modem Main PCB	Price £4.99	LW98G	Programmable Timer Kit	Price £6.95
GB10L	Modem PSU PCB	Price £1.75	LW99H	Modem Kit	Price £39.95
GB11M	Sound Generator PCB	Price £2.25	QQ39N	4412VP	Price £8.00
GB12N	Inverter PCB	Price £1.99	QY43W	XR2211CP	Price £4.45
LW95D	Inverter Kit	Price £49.95	XG29G	Inverter Transformer	Price £22.50

MAPLIN'S TOP TWENTY BOOKS



1. (1) De Re Atari (WG56L) (cat. P62).
2. (-) Atari Computer Operating System User's Manual and Hardware Manual. (WA46A) (cat. P62).
3. (-) Games for the Atari by S. Roberts (WA47B) (cat. P62).
4. (11) Towers' International Transistor Selector Update 2 by T. D. Towers (RR39N) (cat. P32).
5. (-) Digital Integrated Circuit Pocket Guide (WA18U) (cat. P34).
6. (10) Electronic Synthesiser Projects by M. K. Berry (XW68Y) (cat. P50).
7. (8) Programming the 6502 by Rodnay Zaks (XW80B) (cat. P54).
8. (5) Power Supply Projects by R. A. Penfold (XW52G) (cat. P38).
9. (13) Cost Effective Projects Around the Home by John Watson (XW30H) (cat. P41).
10. (6) Newnes Radio and Electronics Engineers Pocket Book (RL06G) (cat. P30).
11. (-) Linear Integrated Circuit Pocket Book (WA19V) (cat. P32).
12. (14) Projects for the Car and Garage by G Bishop (XW31J) (cat. P30).
13. (9) IC555 Projects by E. A. Parr (LY04E) (cat. P39).
14. (-) Adventures With Micro-Electronics by Tom Duncan (XW63T) (cat. P30).
15. (-) The Art of Programming the 1K ZX81 by M. James and S. M. Gee (WA56L) (cat. P64).
16. (3) How To Identify Unmarked ICs by K. H. Recorr (WG87U) (cat. P34).
17. (-) Atari Sound and Graphics by Herb Moore, Judy Lower and Bob Albrecht (WA39N) (cat. P62).
18. (12) Remote Control Projects by Owen Bishop (XW39N) (cat. P43).
19. (-) Electronic Music Projects by R. A. Penfold (XW40T) (cat. P50).
20. (-) Radio Control for Beginners by F. G. Rayer (XW66W) (cat. P43).

These are our top twenty best-selling books based on mail-order and shop sales during August, September, and October 1982. Our own publications and magazines are not included. We stock over 450 different books relating to electronics or computing, and the full range is shown on pages 29 to 65 of our 1983 catalogue. For prices see page 29 of this magazine.

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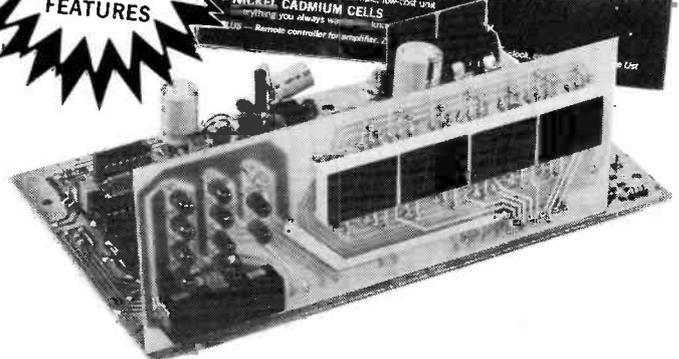
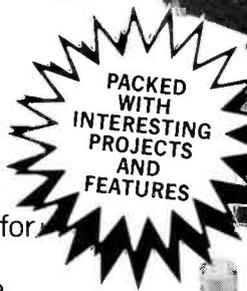
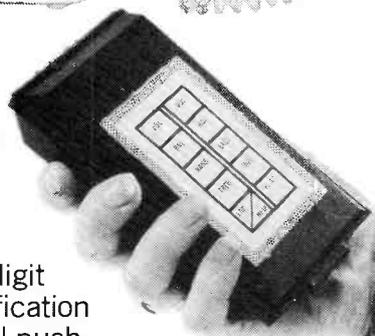
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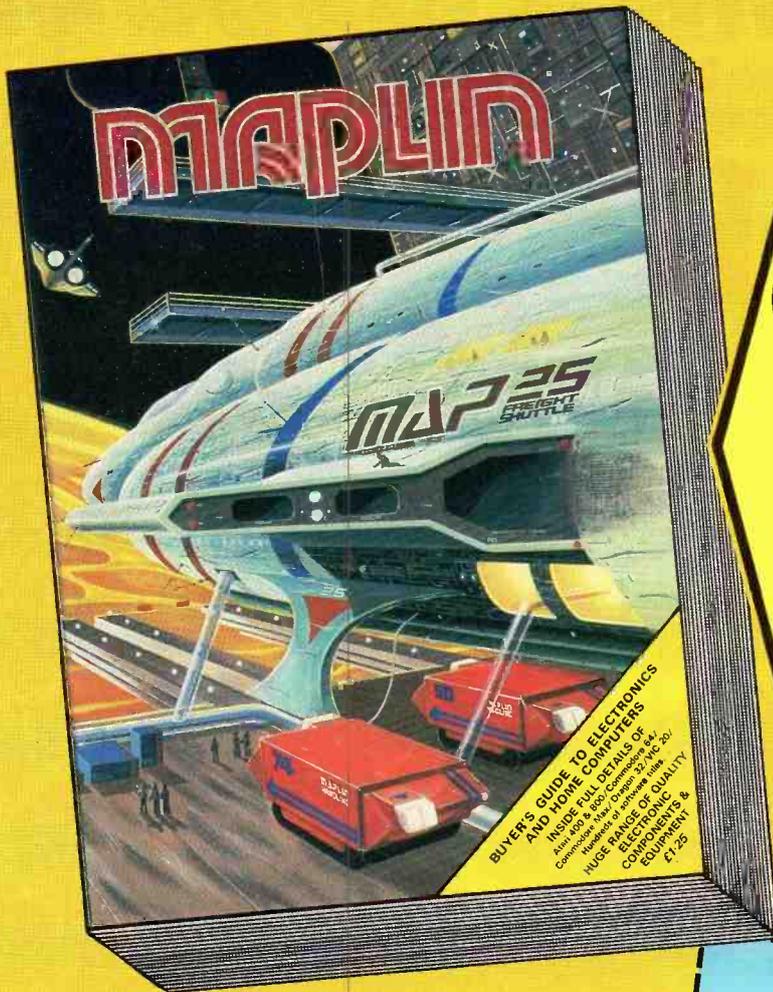
Other Projects and Features

Also in issue 4, an I/O Port for your ZX81, a Car Burglar Alarm, and features on Satellite Communications, Nickel-Cadmium Batteries, and all our usual articles.

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