

# THE MARCONI REVIEW

*Volume XXIII Number 136 First Quarter 1960*

The Marconi Review is published four times a year  
Annual subscription £1. Single copies 5s. Postage paid to any part of the world  
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## The Aerial Papers in this Issue

It is a curious fact that the Radio Antenna tends to be somewhat of a Cinderella in the telecommunication family; certainly young engineers are inclined to be much persuaded that the study of aerials is a worth-while activity and every whit as fascinating as transistors or the electronic amazes of computer work.

Every radio installation begins or ends with an antenna and no other element in the signal chain contributes more significantly to the performance of the system as a whole. It is for this reason that aerial investigations of all types figure largely in the programme of the Marconi Research Laboratory.

Radar aerials have received particular attention because of the difficulty of meeting the stringent operational requirements demanded by the Civil Air Traffic Control authorities as well as by the military. This work has led to aerials of large aperture, high gain and patterned directivity combined with low side lobes. The testing of such aerials has posed some difficult problems of measuring technique, instrumentation, mechanical handling and harsh economics. Some of these points are touched upon in the three papers contained in this issue; in addition, the papers seek to show that the large antenna is a vital tool in the radio survey of the universe around us—it is, in fact, the radio telescope whose influence on astronomy during the last decade has been so dominant.

E. EASTWOOD

# AERIAL INVESTIGATIONS

## USING NATURAL NOISE SOURCES \*

By E. EASTWOOD, Ph.D, M.Sc, M.I.E.E.

*Radio frequency noise from the sun was first observed as an interfering signal on certain longwave RAF and Army radars in 1942. Since that time a number of observations on the noise arising from the active sun have been made on radars operating at various frequencies, but it is only with the development of receivers of increased sensitivity, fed by aerial systems of high gain, that the quiet sun is now observed as a matter of routine.*

*The following article describes experiments which utilize the quiet sun as a noise source at varying angles of elevation, in order to establish the radiation diagrams of the high performance radars required to provide the operational environment demanded by modern aircraft.*

*The sun is a variable noise source and during its brief periods of enhancement spectacular radio and radar effects may sometimes result. A description is given of observations at 215 Mc/sec made on the active sun of October 27, 1955 when evidence was obtained which suggests that a moon reflected signal was also obtained.*

*Records are presented to illustrate the enhancement of the sun at sunrise on July 14th 1959. This event was followed by the reception of signals on July 15th 1959, which may be explained in terms of auroral activity consequent upon the arrival at the earth of charged particles emitted by the active sun.*

### Introduction

The discovery by Jansky<sup>(1)</sup> in 1931 that radio noise was reaching the earth from the general direction of the Milky Way did not lead, as might be supposed, to the immediate detection of radio waves emanating from the sun. It was to be expected that such electromagnetic radiation would be emitted from the sun in accordance with black body theory, but it was not until 1944 that Reber<sup>(2)</sup> succeeded in demonstrating the presence of solar radiation at a wavelength of 1.87 m followed in 1945 by Southworth<sup>(3)</sup> account of his experiments at 10 cm<sup>(3)</sup>. The intensity of the solar radiation flux at these wavelengths proved to be in rough agreement with the level expected from a black body at 6,000°K.

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\* The first part of this paper is based upon a lecture given in Copenhagen in October, 1958 to the Avionics Panel of the Advisory Group on Aeronautical Research and Development to N.A.T.O.

Direct proof of the emission of radio noise from the active sun had been made as early as 1942, however, when a number of Army and Air Force Metric Radar Stations reported an increased noise level coming from a bearing corresponding to and moving with the sun. The phenomenon was analysed by J. S. Hey<sup>(4)</sup> of the Army Operational Research Group and correlation of the radio effect with the movement of a large sunspot across the solar disc was convincingly demonstrated.

A detailed study of the radio effects accompanying the marked sunspot activity of February 1946 was made by Appleton and Hey<sup>(4)</sup> when useful observations were again made at various service radar stations, in addition to the detailed measurements made by Hey and his group on radar derived equipment. These measurements covered the wavelength band 10 cm-1.5 m and established the radio phenomena accompanying the occurrence of a major sunspot disturbance.

As noted in the paper by Appleton and Hey<sup>(4)</sup> the RAF contribution to this series of observations was made by the author, assisted by Mr. F. Phipps and Mr. H. Crossland, and employed the 60-Group radar stations operating in the 10 cm 1.5 m and 10-15 m wavebands. For the 10 cm observations the Type 14 plan position sets and Type 13 nodding height finders were used, but no increase in noise level was observed on these equipments when their beams traversed the sun. The CH sets in the 10-15 m band showed an increased noise level on the A-Type displays which were employed, and it was possible to DF this signal by the usual radiometer technique to show that the bearing corresponded with the bearing on the sun. The 1.5 m GCI equipments showed enhanced noise on the A-scope trace when the aerial beam swept through the azimuth of the sun, and the increase in the noise could be roughly measured from the A-scope, or by monitoring the second detector current when the aerial was stopped on the sun's bearing.

The methods of elevation measurements employed by the CH and GCI sets proved difficult to apply on the solar noise signal, but were sufficient to show that the signal source moved in elevation roughly in accordance with the sun's motion.

It is interesting to remember that, during these experiments, no trace of the sun's noise could be seen upon the PPI of the GCI set, and even the A-scope observations were possible only during the active period of the sun; efforts to observe the quiet sun upon the CH and GCI equipments were unsuccessful.

### Parameters of the Wartime GCI Radar

The wartime GCI set of the RAF operated on a frequency of 209 Mc/s and had an effective noise figure of 19 dB due to the degradation introduced by the capacity switching network and the duplexer. The low cover aerial

consisted of four bays; each bay was made up of four full-wave, horizontal dipoles, i.e. thirty-two half-wave dipoles placed  $\frac{\lambda}{8}$  in front of a wire mesh reflecting screen. Thus the free space power gain of the array, after allowance for feeder losses, was 19 dB. The horizontal beam width was in the order of  $12^\circ$ . PPI observations were made upon a double layer screen of rather poor afterglow characteristics so that little signal integration was possible. Signal amplitude measurement was made from an A-scan tube having a phosphor of similar afterglow properties.

The set noise corresponding to the noise figure of 19 dB is  $3.18 \times 10^{-17}$  watts/Mc/s while the power available at the receiver from the solar noise flux at the earth's surface, corresponding to black body radiation from the sun at a temperature of  $6,000^\circ\text{K}$  and for an aerial gain of 19 dB is  $7.06 \times 10^{-17}$  watts/Mc/s. If we allow for the effective increase of gain produced by the earth's reflection, the noise power at the peak of the lobe is four times this figure, i.e.,  $2.8 \times 10^{-16}$  watts/Mc/s. Thus the solar noise was down on the set noise by a factor of 1,000, and was not visible except during periods of extreme enhancement of the solar activity. If black body theory were obeyed, the effective temperature would have to rise well above  $10^6$  °K for a noise signal to be visible.

### Solar Noise Observations at 215 Mc/s with PPI Recording

During some recent experiments upon a modified 1.5 m type radar, solar noise signal was observed as a matter of routine upon the PPI during those hours of the day when the sun was rising or setting through the lower ground interference lobes of the aerial, whilst a period of increased solar activity around October 27th 1955 gave some spectacular solar noise signals upon the PPI. It is these observations which have prompted the present appreciation of the sun as a noise source in radar antenna studies.

For comparison with the parameters of the 1.5 m radar given above the present experimental equipment operated on a frequency of 215 Mc/s and had a noise figure of 8 dB so that the level of background noise in the receiver was  $2.5 \times 10^{-14}$  watts/Mc/s. The aerial was an array of horizontal half-wave dipoles distant  $\frac{\lambda}{8}$  from the screen as before, but increased in number from thirty-two to ninety-six. The gain now appears as 24 dB after due allowance for feeder losses. The black body flux presented to the aerial for a surface temperature of  $6,000^\circ\text{K}$  and at a frequency of 215 Mc/s yields a solar noise power available at the receiver of  $2.12 \times 10^{-16}$  watts/Mc/s (free space) which corresponds to  $8.4 \times 10^{-16}$  watts/Mc/s at the first interference maximum. This signal is 14 dB down on the set noise

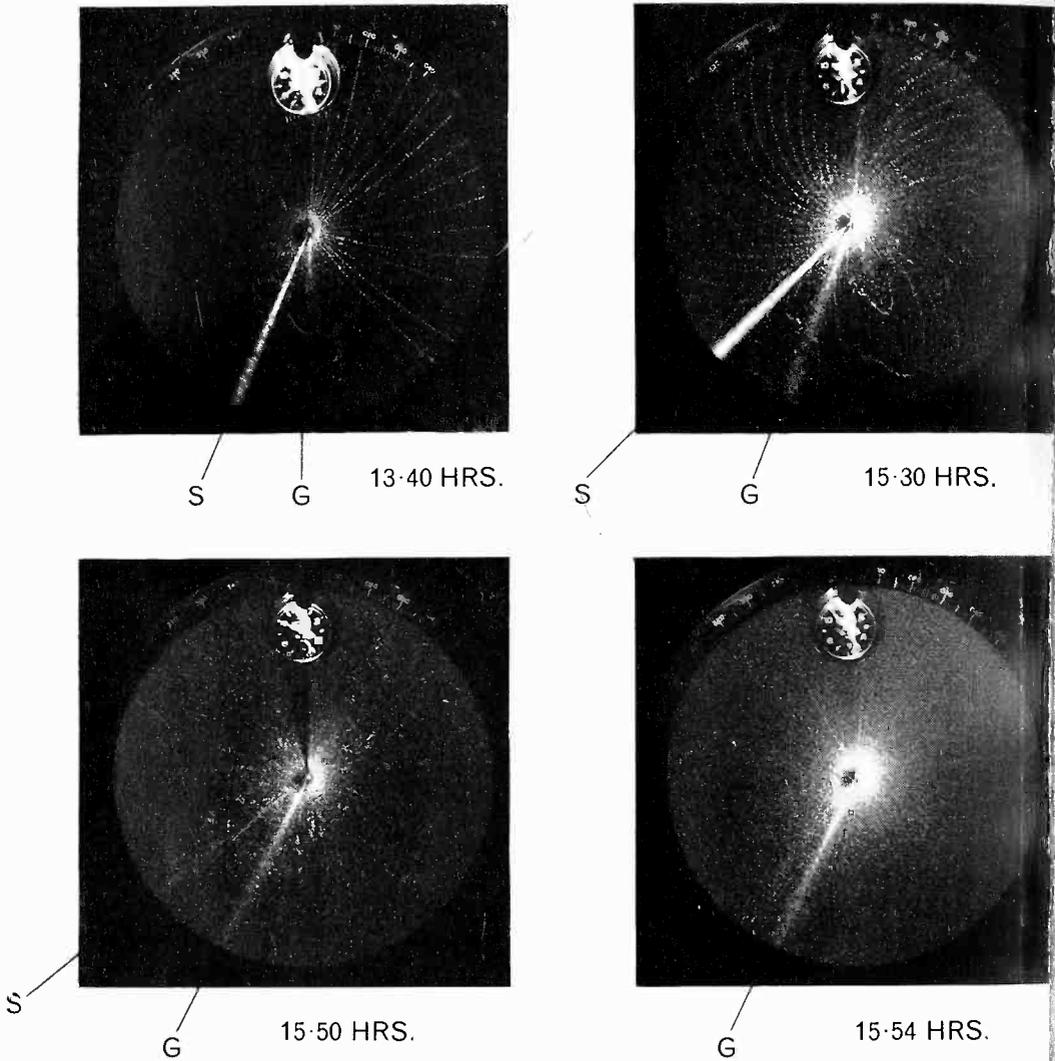
Nevertheless, a clearly discernible noise signal is painted on the PPI at the bearing corresponding to the sun, and moves in azimuth in accordance with the sun's diurnal motion. The character of the signal and the change of bearing with time is clearly shown in Fig. 1. The ratio  $\frac{\text{polar noise amplitude}}{\text{set noise amplitude}}$  for the record at 15.20 hours GMT was measured on an A-scope as  $4/1$ , which is 26 dB above the flux expected for a black body at  $6,000^{\circ}\text{K}$ .

These radar observations confirm in a simple and vivid way the conclusions of the radio astronomers<sup>(5)</sup> that the radio emission from the sun demands an effective temperature much higher than the  $6,000^{\circ}\text{K}$  of the photosphere, or that a radiative process other than provided by black body theory is involved.

Improvements in receiver noise figure and aerial gain have both contributed to the success of this simple technique of PPI display of solar noise signals, but if comparison is made of the power ratio  $\frac{\text{solar noise}}{\text{set noise}}$  for the two sets, i.e. an increase of 16 dB, it will be seen that a further important contribution to solar noise detection comes from the integrating property of the modern phosphor screen. The PPI record was photographed from a cathode ray tube which employs a magnesium fluoride phosphor, having an afterglow characteristic corresponding to a decay time of 30 secs. to 10% intensity after a single excitation. The CRT spot diameter is in the order of half a millimetre, so that for an aerial turning speed of 4 r.p.m. and a time base repetition frequency of 250 pps, integration of the signal over four or five traces was obtained; in the radar case for these same operating conditions it is usual for ten paints on an aircraft track to be seen on the tube at any instant.

### **Solar Diagram Measurements at 215 Mc/s with the Sun as a Noise Source**

Techniques of measuring and recording the horizontal polar diagrams of directional radar aeriels are now highly developed and make use of both CW and pulsed sources in combination with CRT or pen type recorders. In the case of wide aperture aeriels, however, observance of the usual Rayleigh criterion results in large source to aerial distances and generators of not negligible expense. It, therefore, appeared worthwhile to test the usefulness of the sun as a noise source in this type of measurement, particularly as such a technique would permit observations of the horizontal diagram to be made at the various angles of elevation which are of interest operationally.



*Fig. 1. Solar noise signal on PPI of metric radar*

The first simple approach was to photograph the PPI response as in Fig. 1, and to make a density plot of the negative using a Hilger recording densitometer. The record is shown in Fig. 2; a normalized plot of the horizontal pattern of the aerial taken by the usual oscillator method is shown for comparison. Substantial agreement between the main lobe will be noted, also the correct positioning of the side lobes. The amplitude of the side lobes relative to the major lobe are clearly in error, and on further consideration it appeared that accurate measurement of side lobe amplitude would require correction for (a) the smoothing introduced by the sun's movement during the time necessary to build up a PPI picture

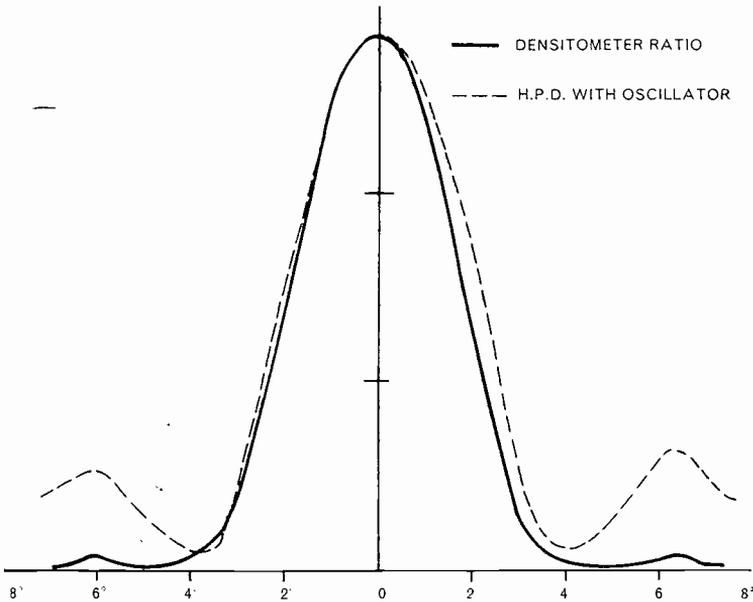
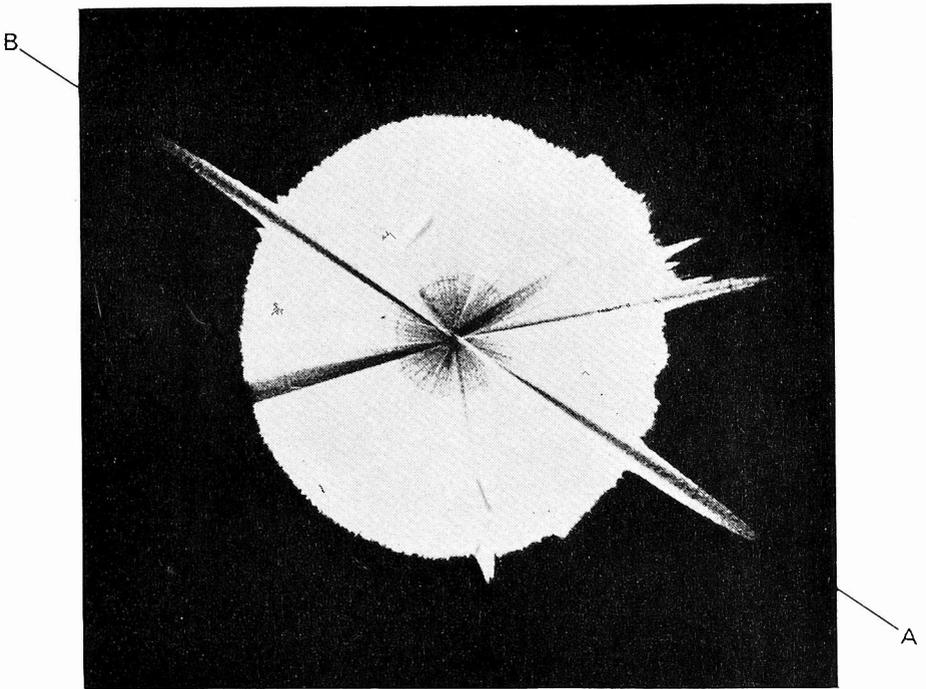


Fig. 2. Horizontal polar diagram of 215 Mc/s aerial

sufficient density, (b) the finite aperture of sun, (c) saturation in the phosphor, (d) the  $\gamma$  characteristic of the film. Solution of these difficulties would hardly be economic in an application of this type where accurate techniques already exist but the simple photographic method is obviously not without interest.

Later experiments have used a technique developed by Mr. M. H. Griffin of the Baddow Laboratories in which the solar noise is integrated during the trace time, i.e. 4 milli-seconds for 250 pps trace repetition frequency, and this integrated signal is applied to the normal sweep amplifier driving the rotating deflection coils of the PPI. The record on the cathode ray tube now consists of a sequence of radial lines of length proportional to the integrator output. Fig. 3 shows an interesting example of this type of record in which the solar noise responses corresponding to frequencies of 202.5 Mc/s and 250 Mc/s respectively are derived from two arrays mounted back to back on a common turning gear, and switched automatically to the display every half revolution. (See Fig. 4.)

The same method was also applied to measure the peak signal on successive sweeps of the aerial through the sun for the purpose of measuring the radiation diagram of the aerial in the vertical plane. The method has also been used for studying the direction and amplitude of interfering



*Fig. 3. Solar noise signals at 202.5 Mc/s and 250 Mc/s*

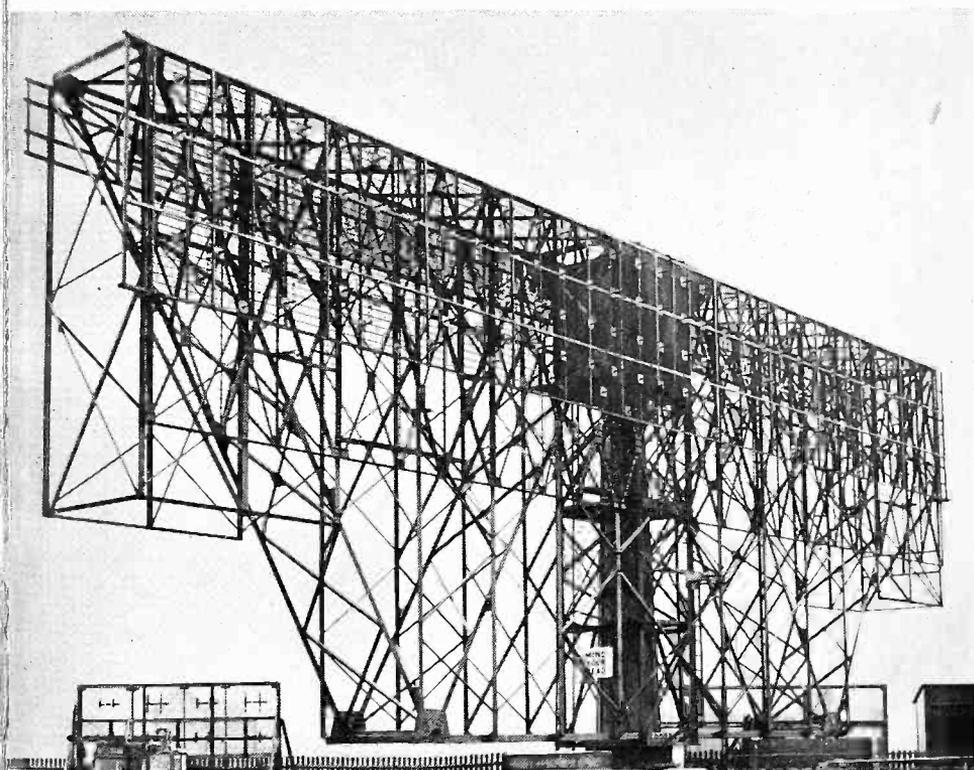
signals, but applies equally to the sun as shown. The form of the horizontal diagram is again clearly seen and it will be apparent that the peak amplitude can be readily measured for each sweep of the aerial which permits the rate of change in amplitude of the solar noise signal with angle of elevation to be measured. The vertical plane radiation diagram calculated for the experimental aerial is shown in Fig. 5. It has proved possible to reproduce the angular positions of the maxima and minima on this diagram exactly when due allowance has been made for the sun's aperture but the amplitude of the second lobe has tended to appear enhanced relative to the first lobe, suggesting attenuation at the lower angle of elevation due to the increased path length through the ionosphere and the atmosphere.

One interesting result which has come out of this work has been the determination of the effective position of the earth reflection plane. During the war the GCI stations were used to measure the altitudes of hostile aircraft by the amplitude comparison of signals derived from aerials at different mean heights. It was, therefore, a matter of considerable importance to know these aerial heights accurately. It was considered that the effective heights would be a function of the particular soil terrain and

type of cultivation, and so much effort was expended in determining the position of the earth's effective reflecting surface. Such experiments, although widely conducted, were contradictory and it was necessary to accept, perforce, the height of the arrays as measured in the usual way. The present experiments have employed an infinitely distant source and were ideally suited to establishing the effective height of the aerial by measurement of the positions of the maxima and minima. These measurements have failed to show a reflection plane which differs from the position of the earth's surface as ordinarily determined. It should be added that the site in question is located on flat arable land having a clay subsoil, and is typical of the wheatlands of Essex.

### Solar Noise Signals Observed on Microwave Radars

Improvements in receiver techniques at microwave frequencies combined with the introduction of the high gain arrays required to provide both the radar cover and resolving power demanded by modern military aircraft,



*Fig. 4. Experimental array for metric radar, 202-250 Mc/s*

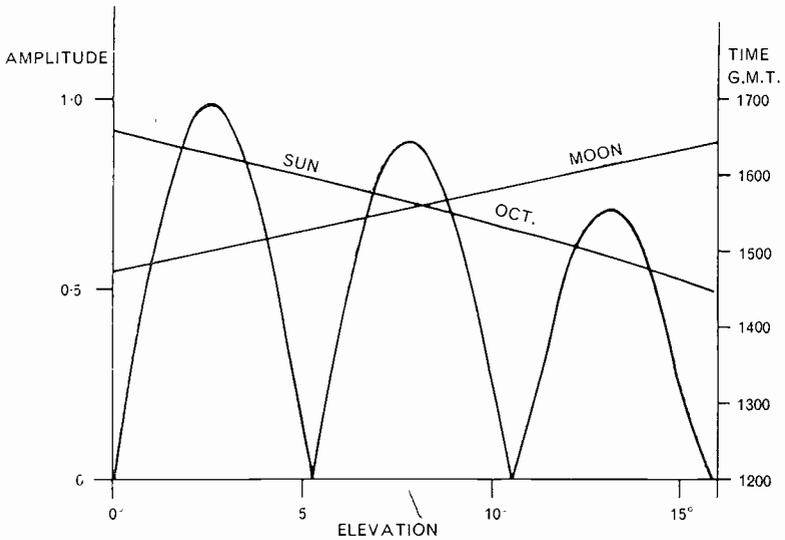
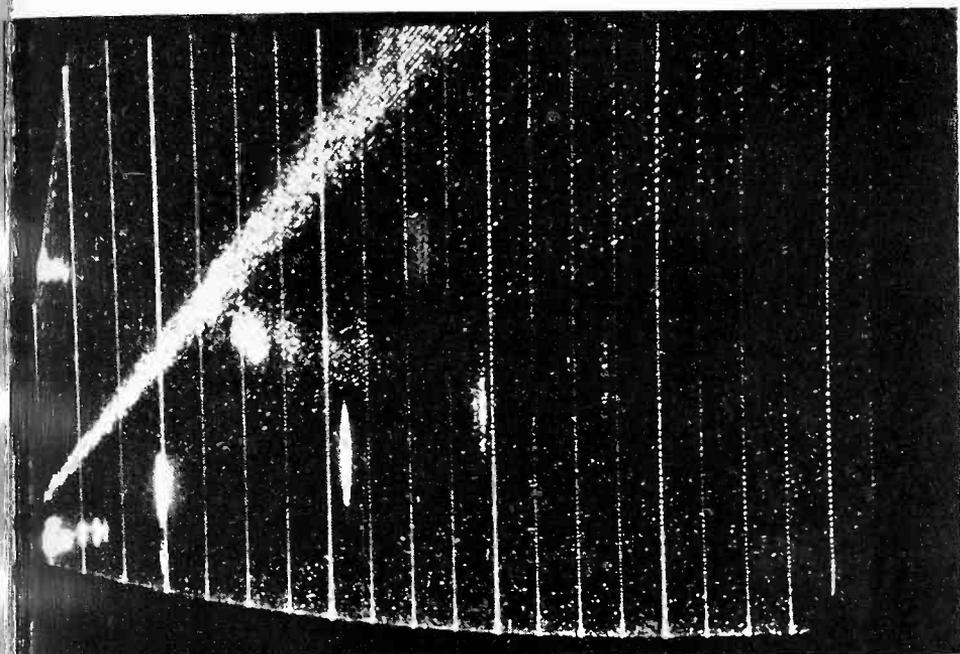


Fig. 5. Ground reflection interference pattern of four-stack array (215 Mc/s 25' mean height)

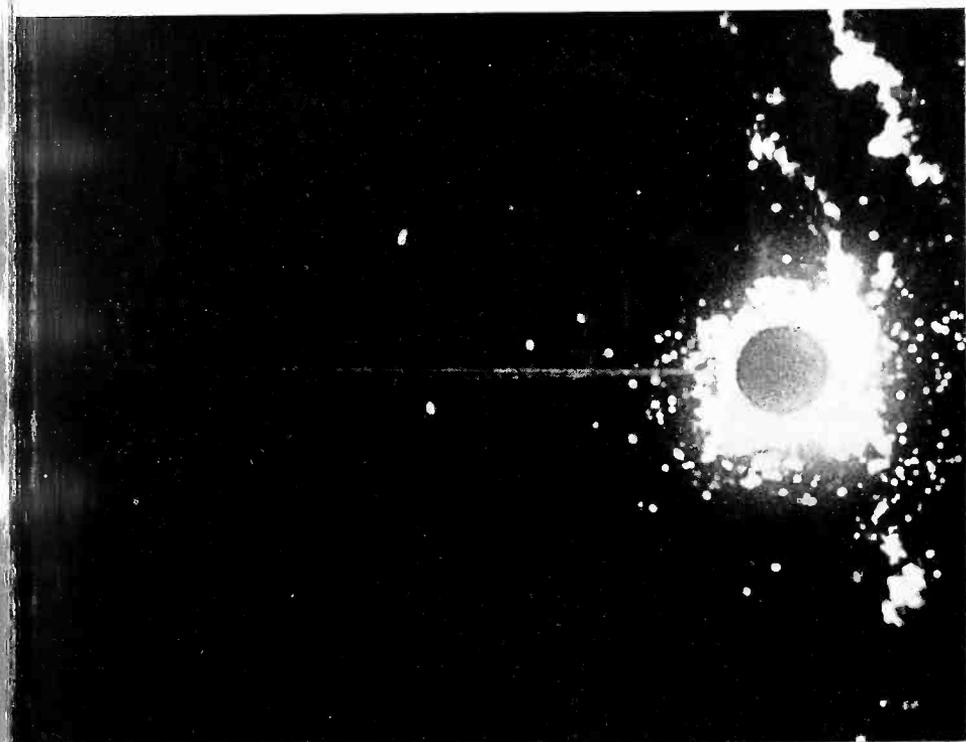
have caused the solar noise echo to be a familiar feature of the PPI at sunrise and sunset. Thus, in the case of an S-band nodding height finder the sun's signal is clearly visible on the range-height display shown in Fig. 6. In this particular equipment the aerial gain is 41 dB and the receiver noise figure 9 dB so that the noise power available to the receiver on the assumption of black body radiation from the sun with surface temperature  $6,000^{\circ}\text{K}$  would be 5 dB down on the set noise. Nevertheless the solar signal is always visible on this equipment when its azimuth corresponds to the bearing of the sun.

Again, in the case of a surveillance L-band equipment the aerial gain is 40 dB and the noise figure yielded by the Travelling Wave Tube receiver is 8 dB so that black body radiation from the sun at  $6,000^{\circ}\text{K}$  would also be 5 dB down on the set noise, and a daily solar signal would not be anticipated. In fact, however, the solar noise signal is observed at sunrise and sunset every day and is so constant in form and amplitude that careful appreciation has been made of its application in antenna studies.

The TWT receiver is normally operated in association with an image rejection filter, but Fig. 7 shows the noise signal in the PPI with the filter temporarily removed. It will be seen that the signal is divided into two. This apparent splitting is an interesting diffraction grating effect and arises from the dispersive property of the linear array; the signal and its image differ in frequency by twice the IF and are therefore observed at different angles. When the image rejection filter is restored into the circuit the image signal disappears from the tube.



*Fig. 6. S-band solar noise signal as recorded by a nodding height finder*



*Fig. 7. L-band solar noise signal on the PPI*

In this particular equipment the horizontal beam width of 39 minutes of arc is comparable with the angle subtended by the sun's disc, but the accuracy with which the horizontal polar diagram of the array can be traced suggests that the effective diameter of the sun as an L-band noise source is considerably less than the 32 minutes of arc of the optical disc. Since the position of the sun is accurately known in elevation and azimuth, it has proved most helpful to use the noise signal in checking the setting up of the radar in azimuth, and this method will surely be of great value at many sites where accurate azimuthal alignment of a radar from a suitably located permanent echo or beacon is difficult. The checking of the absolute elevation accuracy of a nodding height finder is similarly difficult but in the experimental evaluation of the S-band equipment mentioned above we have found the sun to be an adequate source of signal of known angular elevation as is evidenced by Fig. 6. In this figure the angle scale is greatly expanded which exaggerates the apparent beam width.

### Vertical Polar Diagram Measurements

To those responsible for Air Defence planning, the characteristic of a surveillance or control radar which is of greatest interest is the vertical polar diagram, but measurement of radar performance is unfortunately an operation which is difficult to make accurately, economically, and conveniently. While the horizontal polar diagram of a radar can be plotted without difficulty, the vertical polar diagram is not so easily determined and the difficulty of the measurement increases with the size of the antenna and with the angular extent of the vertical cover which it is desired that the radar system shall provide.

It has appeared in the past that there was no really satisfactory alternative to mounting the array with its normally vertical axis in an horizontal position and so establishing the required diagram as in an ordinary horizontal polar diagram measurement, using a remote oscillator and rotation of the reflector. While this method is satisfactory for small antennas, and we have successfully used this technique for aeriels with apertures up to 32', it requires expensive mounting tackle and great care has to be exercised if the reflector is not to be distorted in the process. For the really wide apertures of modern search radars, the method is prohibitively expensive.

An alternative approach is to explore the diagram yielded by the centre section only of the array mounted in the above manner. In the case of a linear array, feeding into a cylindrical reflector, this method would appear to be reasonably satisfactory, but for a double curvature reflector it is obviously less so.

In our experimental evaluation of large antennas we have also made use of CW oscillators carried by captive balloons and by helicopter, but the

work has been slow and tedious and has required much repetition in order to invest the result with significance. In particular, the observations to be made in the high angle cover region have required the source to be brought much too close to the antenna, and so the accuracy of measurement has been prejudiced in that part of the cover which it is most desired to explore, in order to confirm that the optimum power distribution and positioning of a primary feed have been achieved.

It is ultimately necessary to resort to controlled test flights with aircraft, but while such flights are inevitable in order to establish the final performance diagram of the complete system, it is most undesirable to use aircraft flights for antenna polar diagram measurements.

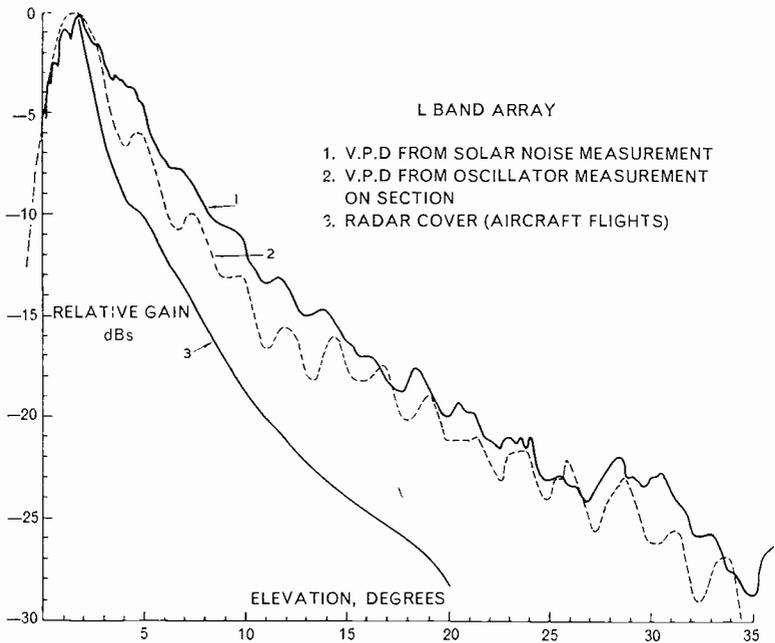
The observations described in the preceding section had shown that a noise signal could be received from the quiet sun by a microwave radar, and was of sufficient intensity to permit accurate measurements to be made of the variation of signal amplitude with angle of elevation of the sun. It was thus an obvious step to explore the possibility of using the sun as a standard noise source for the exploration of radar aerial vertical polar diagrams.

In the experimental evaluation of a large L-band antenna the amplitude of the solar noise signal has been measured and recorded photographically, using the integrator and radial scan technique described earlier, also using a back-off diode with current amplitude displayed on a long persistence C.T. The noise amplitude has been recorded against time, which has permitted correlation with the known angle of elevation of the sun. All details of the measuring technique finally adopted are given in an article appearing on page 21 of this issue of *The Marconi Review* by J. M. H. Scanlan.<sup>(6)</sup>

The measurements have been taken over a number of days in both the morning and evening and have proved to be remarkably reproducible.

Fig. 8 is shown a plot of the solar noise signal against the angle of elevation for an array of 25' vertical aperture designed to provide a secant squared pattern. Also plotted in the figure are the two vertical polar diagram curves derived respectively from the aircraft trials of the complete radar and from oscillator measurements on a section of the cylindrical reflector of this radar, when mounted horizontally on a turntable.

The general correlation between the measurements on the aerial section and on the solar signal is good, and much superior to the results obtained with captive balloon and helicopter borne oscillators. The agreement between the solar noise curve and that resulting from the aircraft test flights is reasonably satisfactory at low angles of elevation, but shows significant discrepancies at high angles. Further detailed work has shown



*Fig. 8. Vertical polar diagram of L-band array*

that a satisfactory explanation of these differences is to be found in the scattering diagram associated with the particular test aircraft.

The solar noise method is thus clearly established as a reproducible, accurate, and economic technique for exploring the radiation patterns of microwave aerials in those cases where the total gain of the antenna is such as to provide a signal of adequate amplitude; it is especially suited to the S and L-band surveillance radars of today.

It is well known that the vertical aperture of a microwave radar can never be such as to provide a bottom edge to the pattern, so sharp as to eliminate completely the possibility of a ground interference pattern. The solar noise method fails to reveal the detail of such a pattern, since the angular aperture of the solar disc is wide compared to the interference lobes. In consequence, the interference pattern is smoothed out. The solar noise method, however, does permit the low elevation pattern to be explored for different azimuths of sunrise and sunset, and so allows the effect of the terrain to be assessed.

### **Galactic Noise Observations on a Metric Radar**

The PPI records reproduced in Fig. 1 clearly show the diurnal motion of the solar noise signal marked with an S. The photographs also show the

presence of a second signal marked G which also partakes of the same diurnal motion as the sun's signal, but continues to be visible on the tube face long after the sun has set.

Observations were taken over a period of a month and showed that the signal was losing in azimuth relative to the G-signal by about  $1^\circ$  per day. From the difference in right ascension of the sun and this unknown source, also from the polar diagram of Fig. 5, it was recognized that this signal was indeed coming from the general direction of the galactic centre. This detection of noise from the galaxy is not, of course, novel, but it is interesting and remarkable to see Jansky's original observation reproduced simply and directly upon a radar PPI; the maximum intensity of the Jovian source at a frequency of 160 Mc/s corresponds to a flux of  $5 \times 10^{-17}$  watts/sq.m/Mc/s at the earth's surface<sup>(7)</sup>.

### "Radio Moonshine" at 215 Mc/s

In the afternoon of Thursday, October 27th 1955, a test flight programme was in progress to establish the performance of the 215 Mc/s radar described in an earlier paragraph. The tests were being conducted by Mr. G. F. Slack, Mr. R. F. O'Neill and the author. The presence of a solar noise signal having the appearance of Fig. 1 upon the PPI when the sun's elevation corresponded to the lower lobes of the radiation diagram, was a phenomenon with which we were thoroughly familiar. Reference to Fig. 5 will show that on the date in question the sun would be passing through the centre of the third lobe at approximately 14.45 hours. We did not usually see the sun in the third lobe, but on this occasion a signal was seen which expanded in azimuth to fill  $90^\circ$  of the tube face by the time the sun was in the maximum of the first lobe, i.e., about 4 p.m. From the detailed measurements of the horizontal polar diagram it was concluded that the noise power centred on 215 Mc/s received from the active sun for a short period on this date was at least 25 dB above the level normally received.

Confirmation of this state of the sun was received on the subsequent days when transatlantic communications were reported disrupted by the arrival at the earth of the corpuscles emitted by the active sun. Further evidence was also provided by routine measurements of solar noise at 75 Mc/s made at certain radio-astronomical laboratories. These results suggested that the sun's activity was about 23 dB above normal. In addition short duration peaks were recorded superimposed on the enhanced noise background, and which rose to 10 dB or more above the mean level<sup>(8)</sup>.

For a brief time during the period 15.20-16.00 of this day a noise signal was observed to paint upon the PPI along a south easterly bearing. This signal was very faint indeed but persisted over about twenty sweeps of the aerial (five minutes). Preoccupation with the test flight prevented

careful observation of this noise signal, except to make a rough tracing on paper of its position relative to the angular centre of the sun's signal. Visual observation of the moon on conclusion of the flight showed it to be in the same general direction as had been noted for the strange noise signal, and so the possibility was recognized that this signal might result from reflection from the moon of the enhanced noises radiation from the sun, i.e., that "radio moonshine", on 215 Mc/s had been observed.

Measurement of the above tracing returned an angle of  $134^\circ$  for the angular position of the unknown signal relative to the sun's bearing. Extraction of the corresponding angle for the moon from the Nautical Almanac for the approximate time in question gave  $135.2^\circ$ . This was rather exciting agreement having regard to the crudeness of the tracing and the difficulty of estimating the axis of the solar signal upon the PPI.

Much the best test of the lunar origin of the signal would have been to have measured the time variation of the bearing, but the short duration of the signal and preoccupation with the test flight prevented this. In the absence of this information we can only try to estimate the relative amplitudes of the "lunar" and solar signals and then compare their ratio with the attenuation that might be produced by the lunar path of transmission.

As noted earlier, the average level of the solar signal on the afternoon of October 27th 1955, was in the order of 25 dB above the level normally prevailing which is usually about 10 dB above set noise. The "moon" signal was only about 1 dB above set noise, thus this signal as seen on the PPI was 34 dB down on the solar signal. A further attenuation factor arises on account of the different angle of elevation of the sun and moon at the moment in question and with respect to the vertical diagram of the array. On Fig. 5 are plotted the angle of elevation—time curves for the sun and moon respectively. It will be seen that over the period 15.20-16.00 hours there is a wide uncertainty as to the effect of the antenna gain function in the vertical plane, but the curves clearly suggest that it was most unlikely that the ratio could have exceeded 20 dB.

These considerations indicate that the "moon" signal as presented to the antenna could not have been more than 54 dB down on the solar signal and may well have been only 34 dB down having regard to the symmetry of the sun and moon curves of Fig. 5, relative to the second lobe. It remains to examine whether these ratios could be compatible with the attenuation introduced by the moon path.

The intensity of the solar flux presented to the moon at any instant is sensibly equal to that obtaining at the earth and so the attenuation introduced by the moon reflection appears as  $10 \log \frac{\sigma}{4\pi R^2}$  dB; where  $\sigma$  is the

echoing area of the moon in square metres and  $R$  metres is the distance of the moon from the earth.

If we assume that the reflectivity of the moon is unity and that all the energy incident upon it is radiated isotropically, then  $\sigma = \pi r^2$ , where  $r$

is the radius of the moon. We have, for the attenuation,  $10 \log \frac{\pi r^2}{4 \pi R^2}$ ,

with  $r = 1,080$  m and  $R = 230,000$  m; this leads to a value of 52 dB.

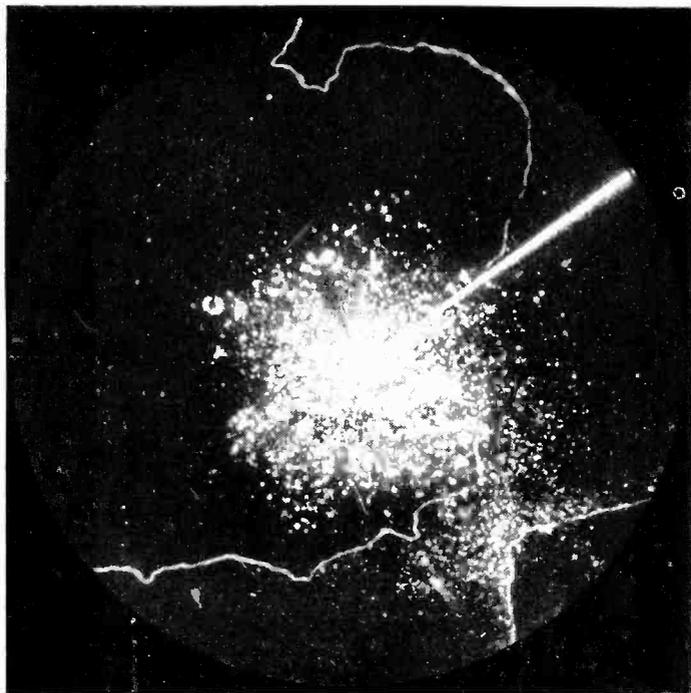
A recent survey of information on the radio reflection coefficient of the moon given by Dr. F. Graham Smith <sup>(9)</sup> at the I.A.U./U.R.S.I. Conference (1959) showed that the cross section of the moon is about  $0.1\pi r^2$ . The attenuation in this case is then 62 dB.

If the higher echoing area of the moon be taken, the calculated attenuation of 52 dB suggests that the lunar reflection of the enhanced solar noise could have yielded a detectable signal on the PPI when the moon was at the elevation corresponding to the maximum of the second lobe. The attenuation figure of 62 dB exceeds the upper limit of the signal ratio by 8 dB. Under these circumstances the moon could have yielded a reflected signal detectable on the PPI only during a burst of solar noise above the enhanced level. Such short duration bursts do indeed occur.

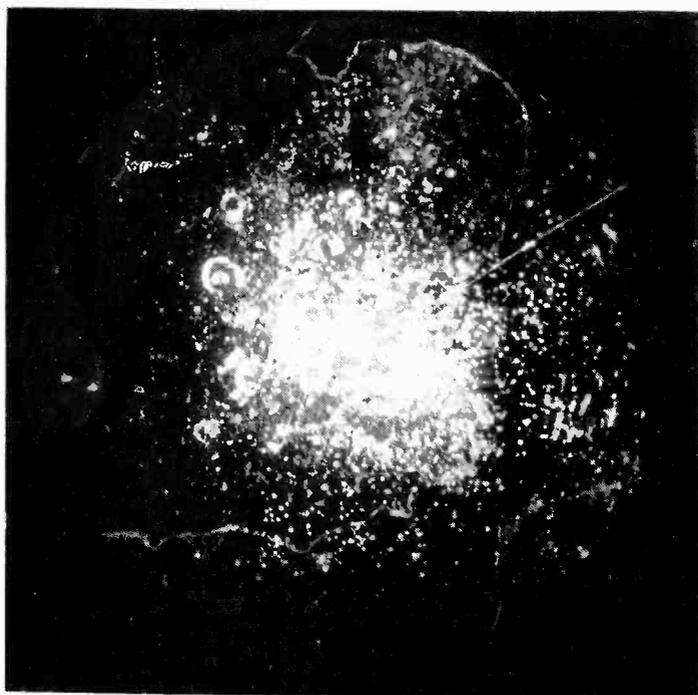
Taking the evidence as a whole, viz., correct bearing of the moon, enhanced sun, freedom of the site from spurious reflection and finally the polar diagram effects, it appears likely that the noise signal of unknown origin observed on October 17th 1955 was due to reflection by the moon of the noise radiated by the sun. This evidence is certainly not conclusive, although much superior to that advanced by Steinberg and Zisler in 1949<sup>(10)</sup> who claimed confirmation of a lunar reflection even though the noise signal was only 18 dB down on that from the sun. "Radio moonshine" is indeed difficult to detect and measure—which is perhaps only to be expected; perhaps our work will help to make a future identification of moon reflections more likely by concentrating attention on possible lunar reflections during solar bursts. Errors such as those of Steinberg and Zisler<sup>(10)</sup> or of Kraus<sup>(11)</sup> would then be avoided. It should then be possible to obtain information on the nature of the moon's surface by observing the reflection coefficient over a band of frequencies.

### Observations at 1,300 Mc/s on the Enhanced Sun; Auroral Effects

The performance of an L-band radar against a solar noise signal has already been discussed; the sun is clearly shown on the PPI at sunrise and



*Fig. 9a. Enhanced solar noise at 1,300 Mc/s*

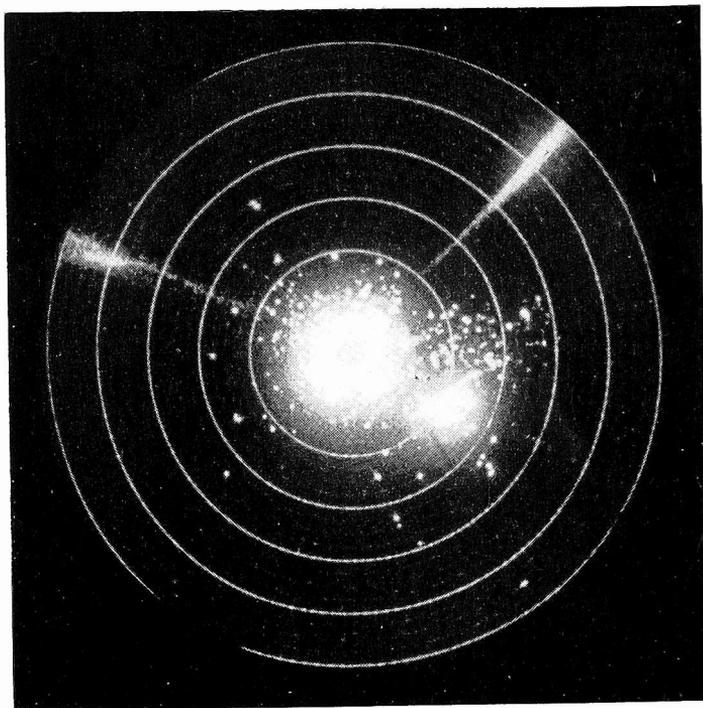


*Fig. 9b. Normal solar noise at 1,300 Mc/s*

at sunset when its elevation corresponds to the peak in the radiation diagram of the antenna.

During sunrise observations conducted on July 14th 1959, the radial noise pattern from the sun was particularly intense. This enhancement of the solar noise signal is shown in Fig. 9. The sun was visible on the PPI for a period of 1 hour 20 minutes, as compared to the usual time of 40 minutes for this period of the year. From a knowledge of the sun's elevation and the curves given in Fig. 8, it was concluded that the sun was displaying an activity of 15 dB above the normal.

As discussed in the preceding section, such an outburst of intensive solar activity is followed by disruption of radio communications on the earth. The noise emitted by the sun travels with the velocity of light, but the charged particles which are simultaneously ejected travel much slower and only arrive at the earth some 6 to 30 hours after the disturbance. On arrival the particles interact with the earth's magnetic field and tend to stream into the upper atmosphere in the general region of the geomagnetic poles. In the descent from the upper atmosphere these high energy particles create channels of ionization. It is during the later recombination processes that the optical emissions are produced which constitute the aurora. The



*Fig. 10. Auroral effect on L-band radar*

randomness of these electron processes also ensure that radio noise emitted, while the presence of the electron cloud with densities of up to  $10^8$  electrons per c.c. permits radar scattering.

On the afternoon of July 15th 1959, i.e., 34 hours following the solar burst reported above, anomalous echoes were observed upon the PPI of the L-band radar. The tube was photographed by Mr. J. D. Bell and Fig. 1 reproduces one of the cine frames. There can be little doubt that the effects recorded on this picture are due to auroral scattering, the aurora having been produced by arrival of the particles emitted during the solar eruption of the previous day.

### Acknowledgements

The experiments reported in this article have formed part of the programme of the Marconi Research Laboratory and the author would like to acknowledge the assistance received from all his colleagues in the Research Group.

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# SOME MEASUREMENTS ON RADAR AERIALS, USING STELLAR NOISE

By M. J. B. SCANLAN, B.Sc, A.R.C.S.

*The measurement of the radiation patterns, especially in the vertical plane, of large radar aerials is often a matter of considerable difficulty. Work with scale models or with sections of an array can give some guidance, especially in the design stage, but some check upon the complete aerial is often felt to be desirable. Test flights are costly, tedious and often inconclusive, since they involve the aircraft echoing area, which may vary rapidly with aspect and angle of elevation, and which in any case has only a statistical significance. It is thus difficult to correlate results obtained in this way with scale model or section experiments. Another method is therefore required, and is in fact readily available. This uses solar noise radiation as a test signal, and has been used with great success, requiring only readily available apparatus to give a great deal of the required information. A short account of the sun as a noise source is given here, together with a description of the experiments so far carried out, and an indication of how sensitivity can be improved, using radio astronomy techniques.*

## The Sun as a Noise Source

Since Southworth's first observations on the sun as a microwave source in 1942 (ten years after Jansky had founded radio astronomy), a vast mass of data has been accumulated showing that the sun's radio spectrum is very complex, not easily to be summarized in a short article. However, if we are interested only in wavelengths commonly used in radar, say from 3 to 50 cms, it is perhaps possible to give a reasonably simple account, which does not, however, pretend to replace the comprehensive surveys available elsewhere<sup>(1)</sup>.

Continuous recordings of solar radiation at many frequencies are made at various observatories; examples from 1948 are given by Pawsey and Bracewell<sup>(1)</sup>, and some 1958 observations at 2,800 Mc/s<sup>(2)</sup> are shown in Fig. 1. Such records enable two components in the microwave solar spectrum to be distinguished. There is firstly the quiet sun component, given by the minima of the fluctuations. This is thermal radiation originating in the corona at temperatures much higher than that of the photosphere. The power radiated varies by a factor of two or three from sun spot minimum to maximum: if the sun were a black body, of the size

of the photosphere, the temperature required to give the quiet sun component at sun spot minimum is given very roughly by

$$T_d = 4 \times 10^5 \lambda \quad (1)$$

where  $T_d$  is in degrees and  $\lambda$  is in metres

For example, measurements in England and in Canada on the same day in 1954 gave temperatures of  $42,200^\circ$  and  $43,300^\circ$  at  $10.8 \text{ cms}^3$ . The spectrum of the quiet sun is also shown in Fig. 7.

Over and above the quiet sun component, Fig. 1 shows the presence of the so-called slowly varying component. This has an irregular period of rather less than a month and is in general roughly equal at its maximum power to the quiet sun component. This flux variation is seen to be well correlated in period and amplitude with sun spot activity and is thought to have a thermal origin in disturbances associated with the spots. Since the area covered by spots is very small (a few thousandths of the sun's disc) the effective temperature of the disturbances (if the effect is indeed thermal) is clearly very high.

A third type of solar emission may be distinguished, namely "bursts". Three classes of "bursts" may be distinguished<sup>(1)</sup>: those associated with flares, noise storms associated with sunspots, and isolated bursts with no certain optical counterpart. Of these only the first need concern us here since the other two are restricted to metric wavelengths. This type of

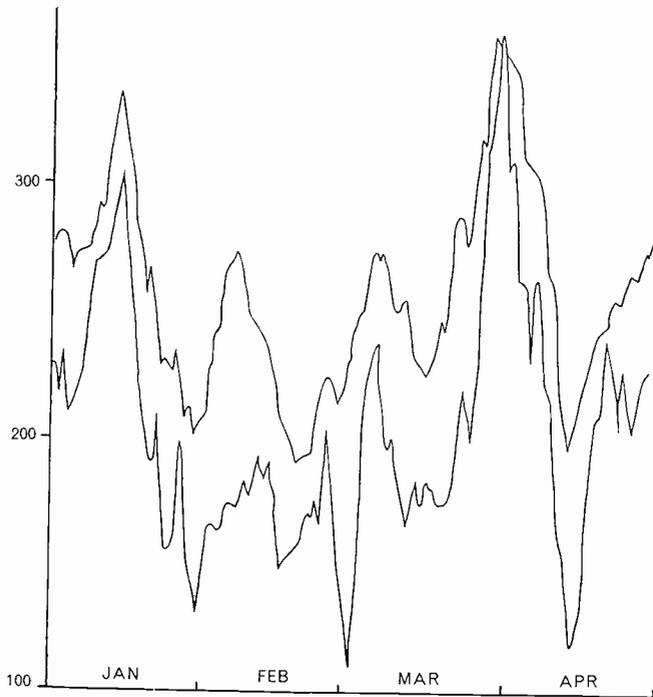


Fig. 1. 2,800 Mc/s solar Flux (units  $10^{-22} \text{ watts m}^{-2} (\text{c/s})^{-1}$ ) and Zurich Sun Spot Number (lower curve) for 1958

first is shortlived (a few minutes only in general), but may be very intense, especially at the longer wavelengths; fortunately, very large solar flares are rare, even at sunspot maximum.

It will be clear, even from the oversimplified discussion given so far, that the sun cannot be regarded as a black body radiator. Nevertheless, it is often convenient to treat it as such, and to use the Rayleigh-Jeans formula to connect the power received with the apparent disc temperature. From the size of the sun, and of the earth's orbit around it, it is easily shown that the power flux  $S$  received on either polarization at wavelength  $\lambda$  is given by

$$S = \frac{0.94 \times 10^{-27} T_d}{\lambda^2} \text{ watts meters}^{-2} (\text{c/s})^{-1} \quad (2)$$

where  $T_d$  is the apparent disc temperature which is given roughly by (1) for the quiet sun at sunspot minimum. It should be remembered, however, that (1) underestimates the temperature, perhaps by six times or more, when the slowly varying component and the sun spot cycle are both at maximum.

### The Detection of Solar Noise

The noise power due to the receiver and aerial may be expressed as

$$p = k[(N - 1) T_0 + T_A] \text{ watts (c/s)}^{-1} \quad (3)$$

where  $k$  is Boltzmann's constant,  $N$  is the receiver noise factor,  $T_0$  and  $T_A$  are the room and aerial temperatures. A measurement of noise factor gives  $N$ , while the change in noise output when the receiver is connected to the aerial and to a matched termination at room temperature gives  $T_A$ . Hence  $p$  is known: for centimetric radar receivers and aerials at present in use, its value cannot be much less than  $2 \times 10^{-20}$  watts  $(\text{c/s})^{-1}$ , since  $N$  is typically about 5 and  $T_A$  about 100-200°K. This situation, in which the noise factor is dominant, may be overcome by the advent of masers and parametric amplifiers. It is unfortunate that, since the larger radar aerials "see" the ground and the atmosphere, the aerial temperature is higher than if they looked into space, so that the advantage of a very low noise receiver is to some extent lost. Masers have already been used in radio astronomy<sup>(4)</sup> but it seems doubtful, for radar aerials at least, if the greatly increased complexity, as compared with a parametric amplifier, is worth while.

Given a receiver noise power of  $2 \times 10^{-20}$  watts  $(\text{c/s})^{-1}$  what is the minimum detectable signal? In the absence of gain fluctuations, this depends on the receiver bandwidths before and after the detector. A large pre-detector bandwidth and a narrow post detector bandwidth give the

average value of a large number of random noise events, which are therefore smoothed out. The smoothing factor is the square root of the ratio of the bandwidths and can easily have a value 1,000, enabling a signal of  $2 \times 10^{-23}$  watts  $(\text{c/s})^{-1}$  to be theoretically detectable. If this figure is to be realized, however, the gain of the receiver must be held constant to better than 0.1%; gain fluctuations, even with the greatest care over power supplies, are in fact the limiting factor in the sensitivity of so-called straight systems. Apart from this limitation, the bandwidth desiderata outlined above may conflict with a requirement to measure the variation of a phenomenon with time or with frequency.

The gain stability limitation can be considerably eased by radiometer techniques, originally used by Dicke<sup>(5)</sup>. Here, the receiver is switched rapidly (say thirty times a second) between the aerial and a matched termination, so that (if these have the same temperature) only gain fluctuations at the switching frequency, which are much smaller than in a straight system, are recorded. The Dicke radiometer is widely used in radio astronomy, especially at the shorter wavelengths: it has perhaps reached a peak in the work of Drake and Ewen<sup>(6)</sup> who were able to detect changes of  $0.01^\circ$  in aerial temperature, although their receiver had a rather poor noise factor.

A variation of Dicke's technique by Ryle and Vonberg<sup>(7)</sup> is mainly used at metric wavelengths and will not be discussed here.

It is fortunately true that the sun is so powerful a source that a straight system will often give polar diagrams of great value, especially when, as now, the disc temperature is considerably higher than the minimum value given by<sup>(1)</sup>; for example at  $\lambda = 10$  cms, the power received from the quiet sun, is from (1) and (2), about  $4 \times 10^{-21}$  watts meter<sup>-2</sup>  $(\text{c/s})^{-1}$ , so that an aerial of effective aperture 1 metre<sup>2</sup> will collect a signal about 20% of the receiver noise, several times the minimum detectable signal even with a straight system.

### Some Measurements Using Solar Noise

After considerable time and effort had been expended on the measurement of the vertical polar diagram of a large radar aerial by means of test flights with rather equivocal results, attention was turned to the possibility of using solar noise, which was readily visible on the displays every day, as a test signal. Preliminary calculations were based on figures given by Ryle<sup>(8)</sup>, and showed that more of the polar diagram would be measurable than was available from test flights, where high angle results were limited by permanent echoes. The first experiments led to a few minor modifications, mainly aimed at greater convenience and speed, and the final experimental method was as follows. Preliminary calculations were made and graphs drawn of the sun's elevation and azimuth for the

few hours before sunset: the accuracy required is not great (say  $1/10^\circ$  in elevation and  $1^\circ$  in bearing) and daily calculation of a few points was referred to the use of tables, none of which list low angles of elevation. The graphs of the sun's azimuth were mainly of use in searching for the first weak signals as the sun came down into the beam: the elevation curves are, of course, required for the final vertical polar diagram results. The receiver used was a normal radar receiver consisting of a broadband

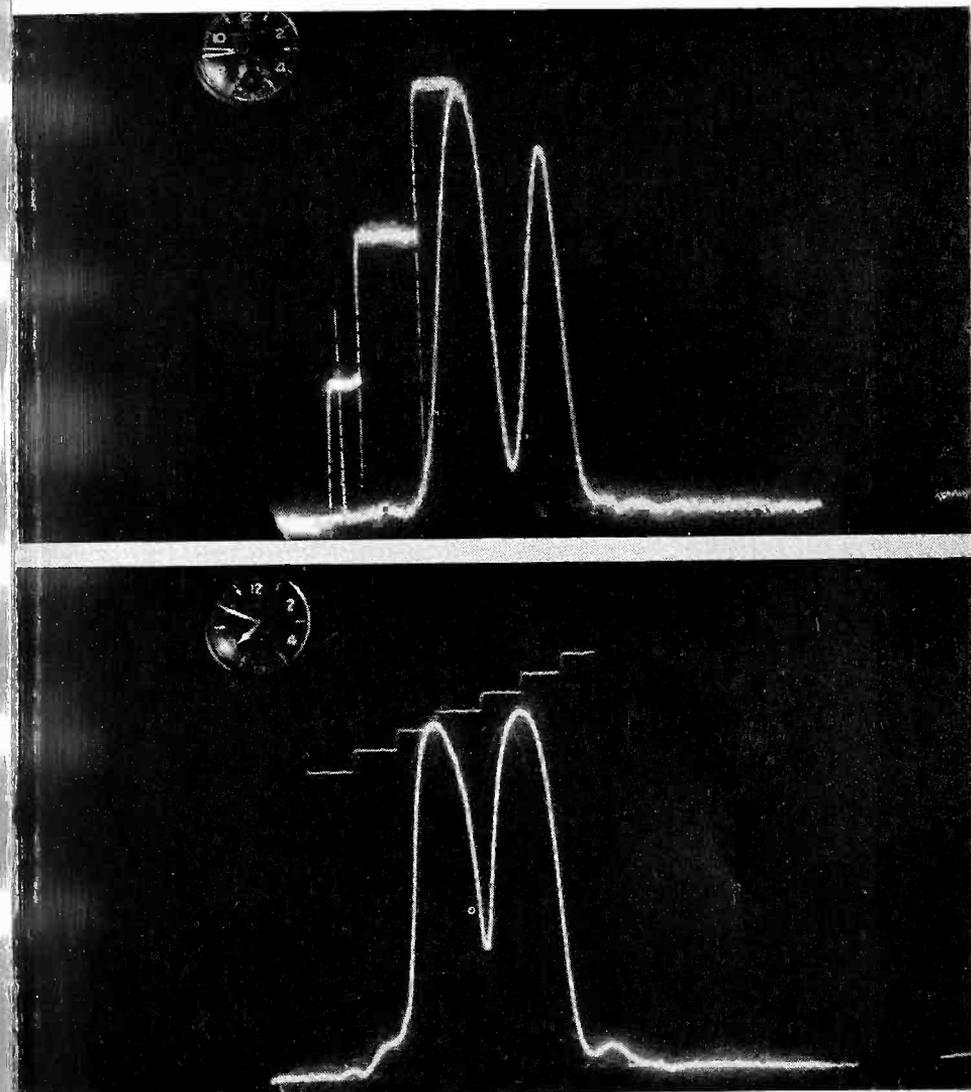
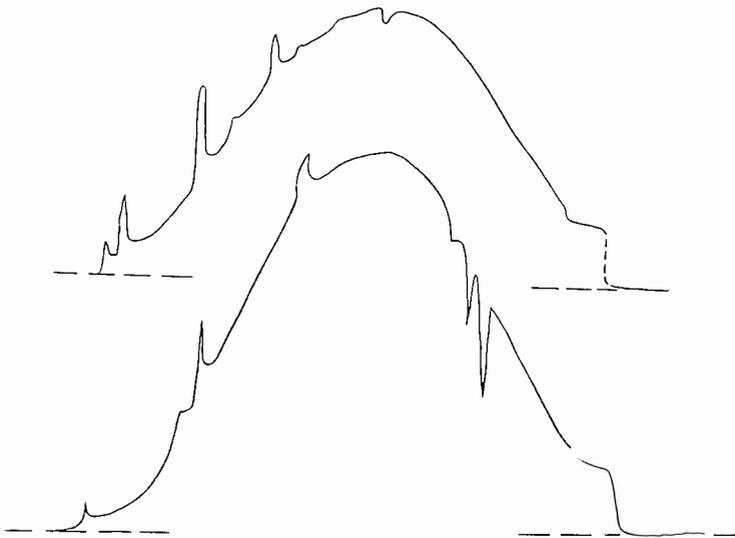


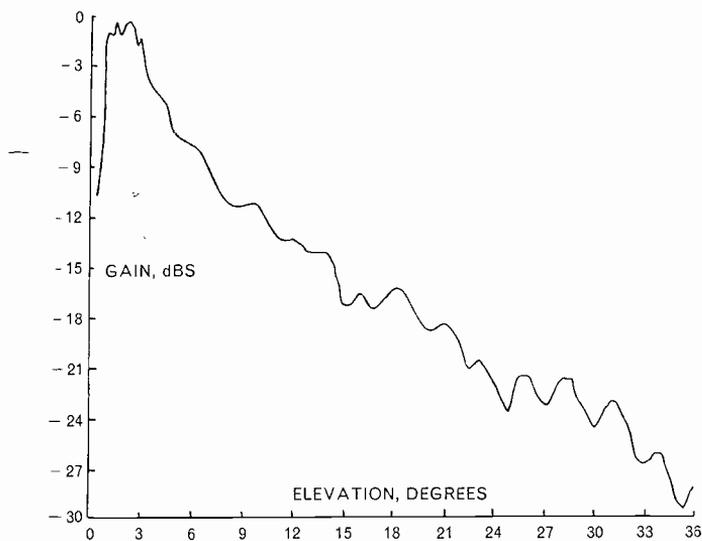
Fig. 2. Sun signals received as the aerial beam sweeps through the sun's azimuth. Sun's elevation  $12^\circ$  (upper) and  $2.6^\circ$ . Also visible are 1 dB calibration markers, and (lower photo) side lobes of the horizontal polar diagram

crystal mixer followed by a high gain IF amplifier and a crystal detector. Noise factor and aerial noise experiments gave a noise temperature of  $1,000^{\circ}$  at the receiver input. A proposal to put the receiver at the end of the aerial's linear array rather than below the rotating joint in an effort to save the losses (about  $1/2$  dB) in the joint and associated waveguide runs, was not carried out, as vibration effects and loss of flexibility offset the small advantage to be gained. An increase in IF bandwidth, while obviously desirable to reduce noise fluctuations, was judged not to be worth while: on the other hand, considerable care was taken with power supplies to the receiver in an effort to reduce gain fluctuations. The AC mains were regulated before going to stabilized power packs for HT supplies, and 6 volt batteries were used for valve heaters, firstly for the head amplifier only, finally for all receiver heaters.

The receiver second detector current was used as a measure of received signal. At first, the standing current was backed off and any increase used to deflect a sensitive galvanometer; later the detector output was fed to a DC amplifier, whose output was taken to a pen recorder and to an A-scope. The A-scope, equipped with a slow time-base and an afterglow tube, was photographed during every sweep of the aerial through the sun's azimuth while the pen record was used only as a check and for identification purposes. Typical A-scope photographs are shown in Fig. 2: They show the increase in signal received (in the form of a horizontal polar diagram of the aerial) as the aerial is swept through the sun's azimuth. The double



*Fig. 3. Pen recordings of sun signals with aerial stationary. Departures from smooth curves are caused by vibrations of aerial in wind*



*Fig. 4. The vertical polar diagram of a radar aerial, measured using solar noise*

peaks result from the combination of a linear array, whose "squint" depends on frequency, and a superhet receiver with no RF stage. Calibration of the system was conveniently achieved by increasing the gain in 1 dB steps (using an IF attenuator between the head and main amplifiers) at frequent intervals: such 1 dB calibration steps are easily visible in Fig. 2. The validity of the calibration is easily checked by the injection of a known amount of noise. It was found that photographs could easily be taken at 30 second intervals, if required, corresponding to a change in elevation of about  $0.1^\circ$ . It would not be difficult to reduce this interval, which, however, is probably small enough for most purposes.

Two tracings of pen recordings are shown in Fig. 3. These were taken as the sun moved through the stationary aerial, and each record covers five minutes or so. The small excrescences on the curves are presumably due to slight shifts or vibrations of the aerial in the wind.

Calculation of results is easy if laborious. Each photograph gives the time (and hence the sun's elevation) and a deflection due to the sun's noise. These deflections are easily converted, via the calibration marks, to relative power received, which is proportional to aerial gain, provided that the sun's noise output is constant during the experiment. Any significant contravention of this condition (due to a burst) may well be obvious from the results but is easily eliminated in any case by a repeat experiment on another day. Fig. 4 shows a vertical polar diagram taken in this way in May 1958. It differs from another curve taken the next day by a maximum

of about 1 dB. Such close correspondence gives great confidence that the random errors, at least, have been largely eliminated.

### **Some Measurements at 600 Mc/s**

The experiments so far reported involved a fairly elaborate system, most of which is nevertheless readily available on radar sites. However, in November 1958 a requirement arose to measure, and compare, the vertical polar diagrams of two 600 Mc/s radar aerials on a rather remote and less well equipped site. In this case, the aerials were turned by hand, the rising sun was used (the aerials were obscured when looking towards the setting sun) and the equipment was simple, almost crude. It consisted of the normal radar receiver with its second detector current backed off to zero. Any noise signal was observed as a deflection on a sensitive microammeter. The conditions of the experiment are reflected in the results which show that the low angle measurements are missing in both cases; this was caused by poor visibility, lack of bearing information, and a signal so much larger than expected that it was at first taken for interference. Unfortunately there was no opportunity to repeat the measurements. The results (Fig. 5) show the earth reflection patterns of the aerials very well and agree with theoretical predictions based on aerial aperture and mean height.

### **Measurement of Aerial Gain**

The measurements discussed so far do not require a knowledge of the sun's temperature, but only that this be constant for the duration of an experiment. A measurement (using solar noise) of the gain of a large radar aerial, on the other hand, does require a knowledge of the sun's temperature, which may be obtained at some frequencies from the published figures (which are always well in arrear) or failing this, from a measurement with an aerial of known gain. This method, of course, amounts to a comparison of the gain to be measured with the known gain, with the sun as signal source, so that its temperature need never be calculated explicitly. It has already been pointed out that an aerial of very modest size will gather enough signal to give reasonable accuracy and the problem of making a microwave aerial of known gain has been dealt with by several authors<sup>(9)</sup>. Since the comparison standard aerial will be relatively small, less accuracy will be required in pointing it at the sun than with a larger array. On the other hand, care must be taken that the sun is sufficiently high for ground reflection effects to be neglected, which may mean that the main array and the gain standard cannot receive strong sun signals simultaneously.

In order to check the gain of the large aerial whose vertical polar diagram is given by Fig. 4, a gain horn was made having a gain of 20 dBs.

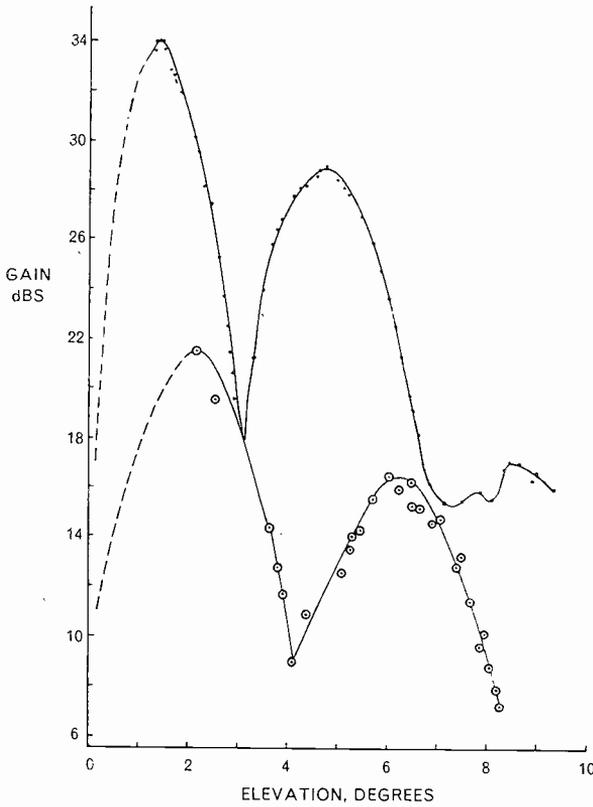


Fig. 5. Vertical polar diagrams of two 600 Mc/s radar aerials

This was of quite manageable size but gave a good sun signal. In practice, measurements were made on the large array, then on the gain horn, then gain on the large array, all in one day. The large array measurements gain agreed well with those of Fig. 4, although the measurements were some months later, and a figure for the maximum gain of the large array resulted. It is thought that this result could not be achieved by other means.

**Some Possible Sources of Error**

Corrections to vertical polar diagrams and gain measurements will be required, especially at small angles of elevation, to take account of atmospheric attenuation and refraction, which is greater at radio wavelengths than for light<sup>(10)</sup>. The finite size of the sun's disc will mask ground reflection effects if the lobes of the ground reflection pattern are smaller than 1/2°, as they were, for example, in the case of Fig. 4. Moreover, if the horizontal beam width is comparable with 1/2°, the aerial will receive less signal than from a point source giving the same flux density as the

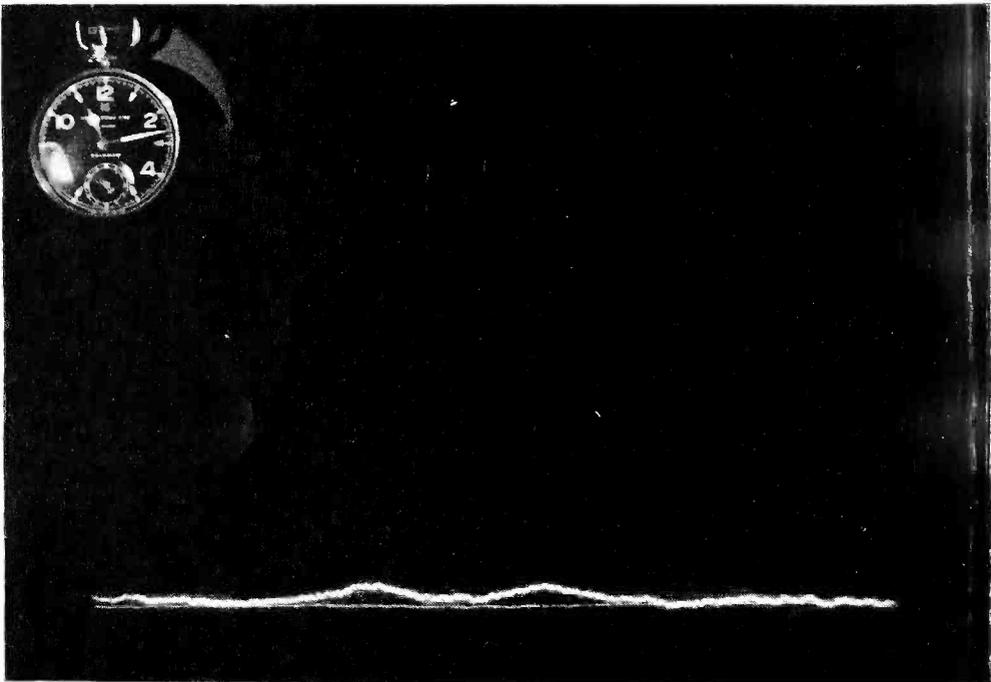
sun so that a small correction to gain measurements may be required, since the comparison aerial, being smaller, will see the sun as a point source.

### **The Advantages of the Solar Noise Methods**

The difficulties of other methods of measuring the VPD of a large radar array have already been mentioned; the solar noise method alone gives the required result, and this without any apparatus external to the radar. There is no difficulty, as there is on an aerial test site, in keeping transmitter and receiver in tune. There are no problems of squint as there are when measuring sections of the array on a test site. The frequency characteristics of the aerial array may be explored relatively quickly, and, finally, the sun provides almost the only practical source for gain comparison measurements.

### **Other Radio Sources**

It is natural to inquire whether any others of the thousands of radio sources so far catalogued may not be easily detectable with radar aerials. The advantages would be considerable, since the other sources are generally



*Fig. 6. Signals received from the radio source Cygnus A as the aerial beam sweeps through its azimuth. 11.13 B.S.T. 26th August 1958*

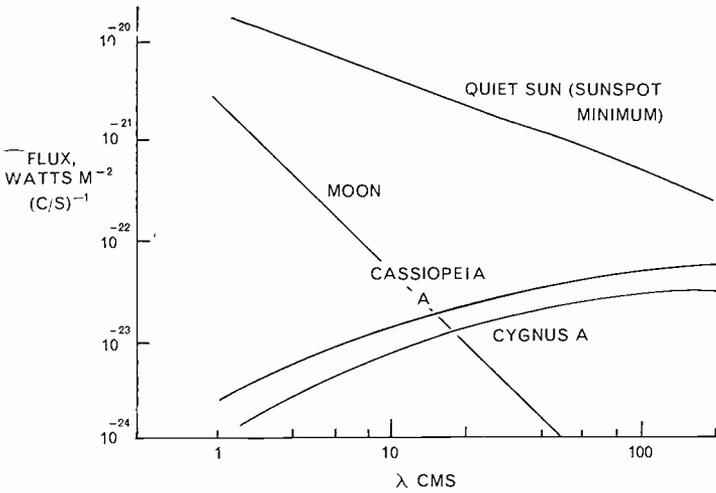


Fig. 7. Spectra of the more powerful radio sources

smaller in angular size and more constant in radio power output, even if the absolute value of this output is not known to better than 10 or 15%. However, it turns out that only the most powerful sources can be detected by any aerial of reasonable size and a straight receiver at microwave frequencies. Since the strongest of all sources, Cassiopeia A (RA 23h 1m 12s, Dec. 58° 32') never comes below 20° in elevation in this latitude (51.5° N), it is not detectable by radar aerials having their maximum gain at low angles. However, the second most powerful source, Cygnus A (RA 14h 57m 45s, Dec. 40° 35') has a minimum elevation of less than 3°, even allowing for refraction, and may be detectable on the largest aerials. This source is among the most interesting in the sky. It was the first discrete source detected and appears to consist of two spiral galaxies in collision and to emit as much power in its radio as in its near-visible spectrum. Its strength as a radio source is such that it could still be detected at 30 times its estimated distance of  $3 \times 10^8$  light years, although it would then be out of reach of the largest optical telescope. Fig. 6 shows a photograph of the response from this source, whose spectrum, together with that of the quiet Sun, Moon and Cassiopeia A, is shown in Fig. 7. The next most powerful sources are considerably weaker than those already mentioned and will not be detectable by straight methods on any but exceptionally large radar aerials until very low noise receivers become available.

The Moon is an interesting special case. Its microwave temperature appears to be constant with frequency at about 200°, and does not vary so much as would be expected with lunar phase. It should be easily detectable with a straight system at wavelengths of 10 cms or less.

## Conclusion

An account of solar radiation at microwave wavelengths and of a simple experimental method for its detection and use in the measurement of the vertical polar diagrams and gain of large aerials such as those used for radars, has been given. Typical results are shown and attention is drawn to other radio sources which may be detectable.

## Acknowledgements

The author wishes to thank Dr. E. Eastwood, Chief of Research, Marconi's Wireless Telegraph Co. Ltd., for permission to publish this paper.

Very many of his colleagues contributed to the success of the experiments, but especial thanks are due to Miss A. P. Darwent and Messrs. G. Downie, E. Bowan and D. Thorn.

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# AERIAL CALIBRATION BY SOLAR NOISE USING POLAR DISPLAY

By M. H. CUFFLIN, B.Sc, (Hons)

*During the summer of the International Geophysical Year 1957, some experimental investigations were made at Bedell's End, near Chelmsford, with two objects in view. One was the possibility of using the radio noise of the sun as a suitably remote source for plotting the vertical polar diagram of an aerial. The other was an attempt to repeat an observation made by Dr. E. Eastwood\* at the radar station at Trimley in Suffolk in 1955, of a suspected deflection from the moon during a very intense eruption of solar noise. This, it was felt, would be an interesting contribution by Marconi's Wireless Telegraph Company to the world-wide work of the I.G.Y.*

*The usefulness of the first aim was successfully demonstrated and has since been applied in the Company's research work. This article is largely concerned with the experimental equipment used and the reasons for particular circuit arrangements, with a description of some interesting records.*

*The second object of the work was not achieved. Normally, the level of the solar radiation was insufficient, but on the one occasion when the sun was in an enhanced state of activity the moon was not in a position suitable for observation.*

## Initial Experiments

Following development and engineering work on a VHF radar the Company was left in possession of a metric radar aerial mount with driving mechanism, and a moving coil type console with PPI display. On the aerial frame were mounted, back-to-back, two experimental aerial arrays, one operating on 202.5 Mc/s, the other on 250 Mc/s.† The 202.5 Mc/s array comprised twelve horizontal dipoles arranged end to end in a single stack approximately  $\lambda/8$  in front of a wire mesh reflector. This gave effectively twelve maximum lobes in elevation, while the main horizontal beamwidth was  $4.5^\circ$ . The 250 Mc/s aerial contained four stacks, each of sixteen horizontal dipoles, fixed vertically one above the other, also 8 in front of a wire mesh reflector. This gave effectively only three maximum lobes with a main beamwidth of  $3.5^\circ$  azimuth. For comparison the theoretical lobes are shown in the table overleaf.

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\*Chief of Research, Marconi's Wireless Telegraph Company.

†Refer to Dr. Eastwood's article "Aerial Investigations Using Natural Noise Sources," p. 4, page 9.

Aerial Lobe No.	1	2	3	4	5	6	8	9	10	11	12
202.5 Mc/s	2.43°	7.3°	12.3°	17.3°	22.5°	27.9°	33.6°	39.7°	45°	54°	64°
250 Mc/s	2.3°	6.9°	11.5°	(16.3°)	—	—	—	—	—	—	—

The 202.5 Mc/s aerial offered a wide angle of reception in elevation, while the 250 Mc/s aerial was "low-looking." It was obvious that the latter would only be effective during a period from one-and-a-half to two hours after sunrise or before sunset.

To make convenient use of the two aerials a head amplifier and mixer for each aerial were installed in the cabin on the aerial column, the output of each being at the IF, 50 Mc/s. A remotely controlled relay switch permitted either output to be presented to the main IF amplifier as required.

In the early observations, a normal PPI form of presentation was used. The noise from the sun appeared as a narrow band, brighter than the general receiver noise, as shown at A in Fig. 1. Unfortunately, as the sun changed its position in elevation and passed into the aerial minima, it became increasingly difficult to discriminate between receiver and solar noise and the precise observation of the minima was impossible. The elevation of the sun was obtained by recording the time of a particular

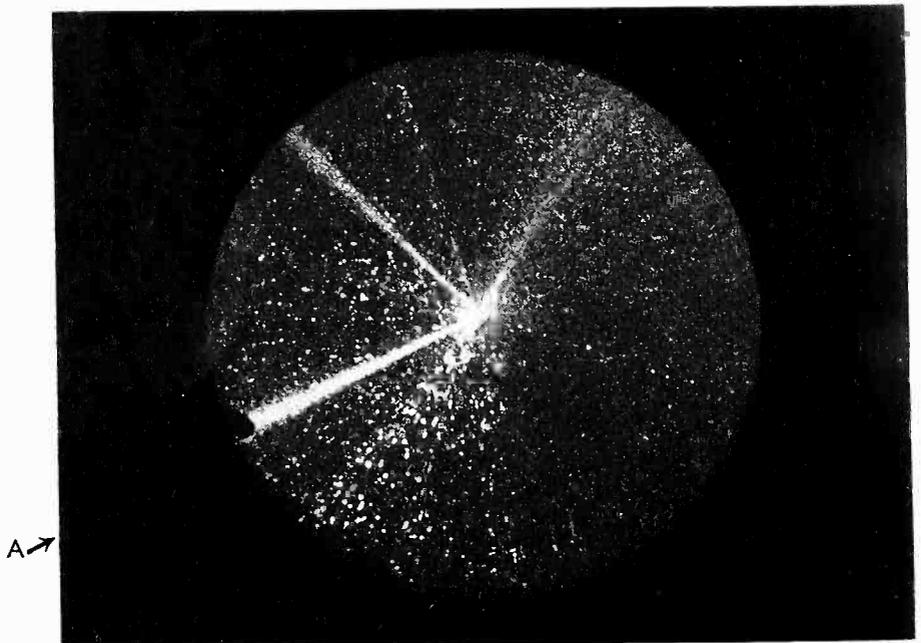


Fig. 1. PPI Record

ment and calculating the angle with the aid of nautical tables. This was more accurate and reliable than direct measurement with the aid of a theodolite, which needed some skill and an extra person to make observations, and was, of course, useless on cloudy days.

### Integrating display

The poor resolution of the noise minima on the PPI display led to the introduction of a modified display which overcame this handicap and provided the beginnings of a useful instrument with other possible applications.

The modification abolished the normal PPI with its constantly repeated radial time base. Instead a radial scan was developed whose length was related to the received signal strength. As the aerial rotated, followed by the rotating deflector coil assembly, a bright polar pattern was drawn on the cathode ray tube screen, consisting of a large number of straight radial lines of varying lengths emanating from the centre. It was now very easy to see when received signals faded to a minimum. Even signals well below receiver noise caused a visible increase in the scan radius.

If two signals,  $n_1$  representing receiver background noise, and  $n_2$  solar noise, are added, the resultant is

$$N = \sqrt{n_1^2 + n_2^2}$$

then, the scan radius were proportional to the signal,  $R_1 = k \cdot n_1$  for normal receiver noise and  $R_2 = k \cdot \sqrt{n_1^2 + n_2^2}$  for added solar noise.

For  $n_2 = n_1$ ,  $R_2 = R_0 \sqrt{2}$  i.e., 41% increase in radius.

For  $n_2 = n_1/4$  i.e., 12 dBs below receiver noise.

$$R_2 = R_0 \sqrt{1 + \frac{1}{16}}$$

$$\cong R_0 (1.03) \text{ i.e., } 3\% \text{ increase in radius.}$$

This illustrates the enhanced sensitivity of observations of the minima. This signal integrator was achieved with a few simple modifications. The schematic diagram of the whole system is shown in Fig. 2. The grid resistance,  $R$ , of the Miller integrator was connected to the rectified signals from a diode following the video amplifier. No signal brightening was applied to the grid of the cathode ray tube although a blanking pulse removed the flyback trace. The integrating period was approximately 800 microseconds at a repetition period of 4,000 microseconds, i.e., at 50 c/s. During the integration period the rate of change of the integrator output varied instantaneously with a change of input signal, although the signal excursion, and hence length of scan, depended on the average signal

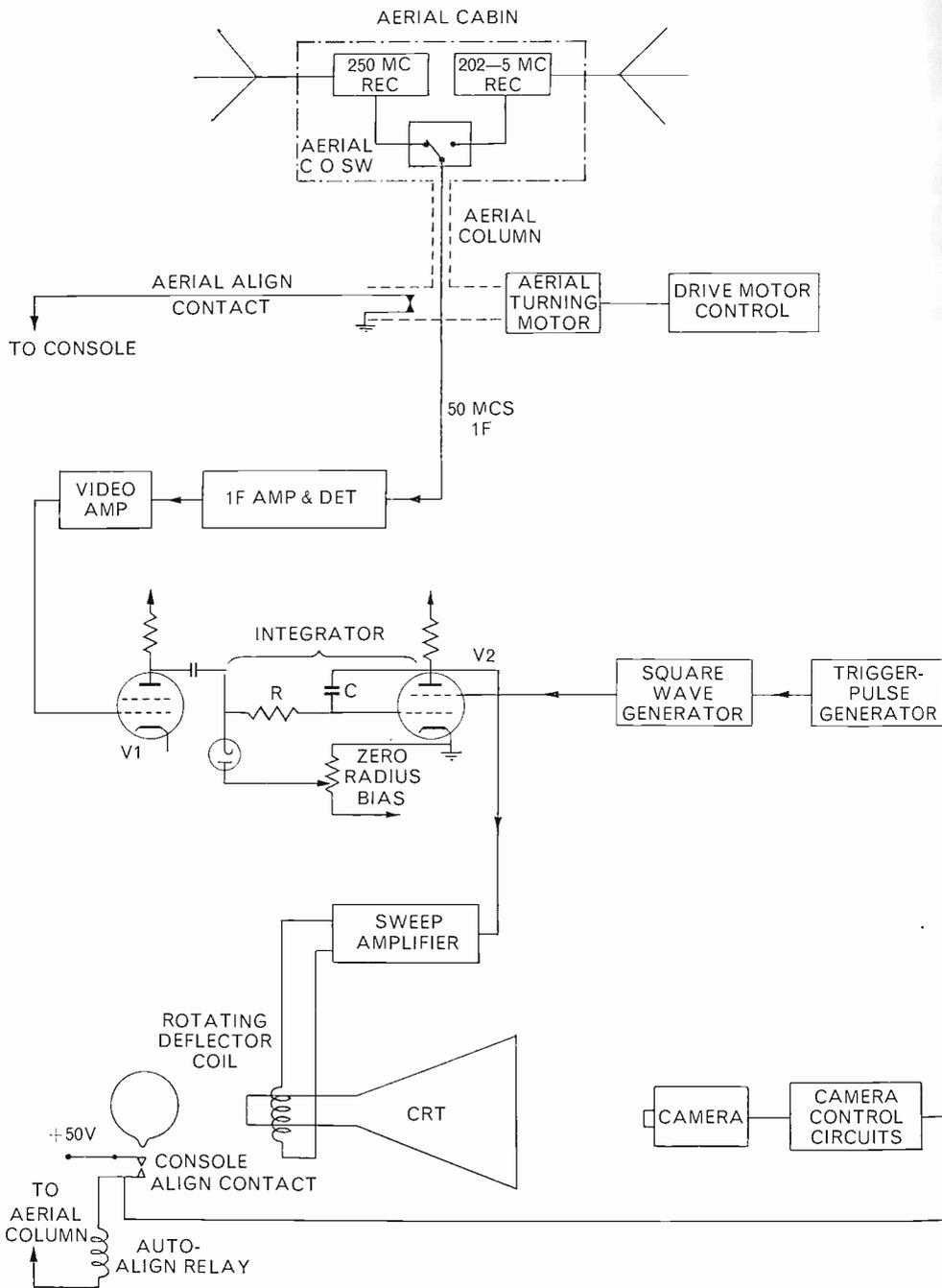


Fig. 2. Block diagram of integrating display

uring the period. It can, therefore, reasonably be said that the response frequency of the system was limited to 250 c/s. There was, therefore, no practical delay between a signal arriving on the aerial and its recording on the cathode ray tube screen.

A minor defect of the original Miller integrator was the initial instantaneous potential drop at the anode, caused by the excursion of grid potential from zero bias to near cutoff potential at the start of the controlling square-wave. This caused a minimum radius of scan when no signals were applied to the integrator. It was overcome as shown in Fig. 2 by a small negative bias, almost to cutoff value, applied via the rectifying diode.

Although no precise measurement was made to obtain the linearity of input v. output, a simple test with a signal generator showed approximate linearity over a 10:1 input range, with a change of radius of the scan from 1 inch to 0.5 inch. It was realized that several factors could influence the performance including the linearity of the various stages of the receiver, the video rectifier and deflection amplifier. It would be possible to reduce the overall number of stages by feeding the output of the second detector directly to the integrator, avoiding demodulation and video amplification with their attendant distortions, but it was inconvenient in this experiment due to the distance between various sections of equipment.

It was found convenient, to obtain a point of reasonable radius for the polar noise, so to adjust the receiver gain that the background noise generated a disc about half the maximum diameter. For stronger signals the noise radius could be reduced.

### Automatic Camera Control

The circuit of the camera is shown in Fig. 3. The "prime mover" used in controlling the camera was the auto-align contact in the console. When the aerial and moving coil drive were running in correct alignment, the auto-align contact closed over an arc of  $5^\circ$  as the aerial "aspect" passed through the North bearing. The contacts controlled a DC supply of 50 volts. The moment of initial contact was used for camera timing. However, in attempting to use this initial closure to trigger an all-electronic circuit it was found that random noise and hum pick-up due to long auto-align control leads, and occasional contact bounce, resulted in hopelessly erratic triggering. It was found more reliable to use relays, to isolate the auto-align circuit from the trigger circuit, and to derive timed transfer pulses to operate a Decatron Switch Valve GS10C, as a decade counter.

In the circuit, relays A/2 and B/1, with their associated circuits, were connected that they operated sequentially when the 50V supply was applied to A/2 via the  $2 \mu\text{F}$  condenser on the closing of the auto-align contact. This input, being of low impedance and having a long time

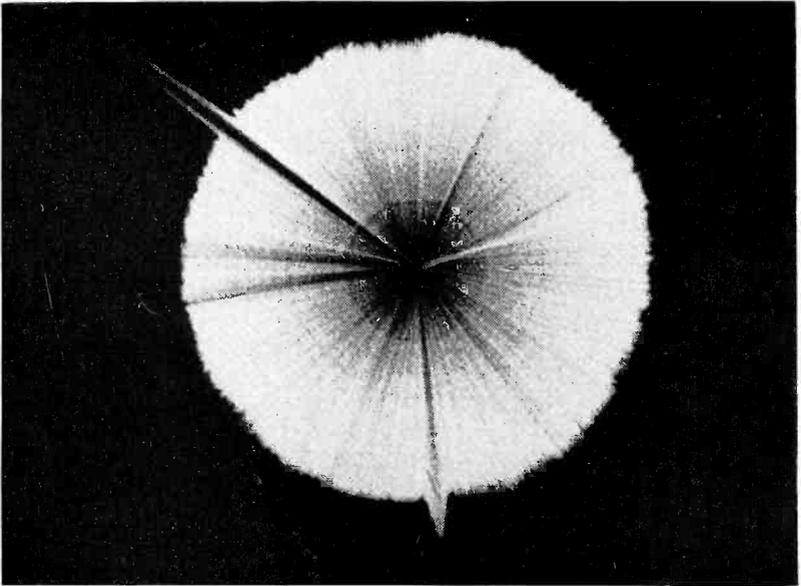


constant, smoothed any irregularities due to contact bounce and ignored hum and random noise. Charges, accumulated during the "waiting" period on the  $0.1 \mu\text{F}$  condensers, were discharged by contacts A2 and B1 and caused transient negative pulses in sequence to appear on the Geatron guide electrodes. The glow discharge thus transferred from one cathode to the next at each revolution of the aerial and remained on that cathode for one revolution. When on cathodes one or six, the camera would be switched on.

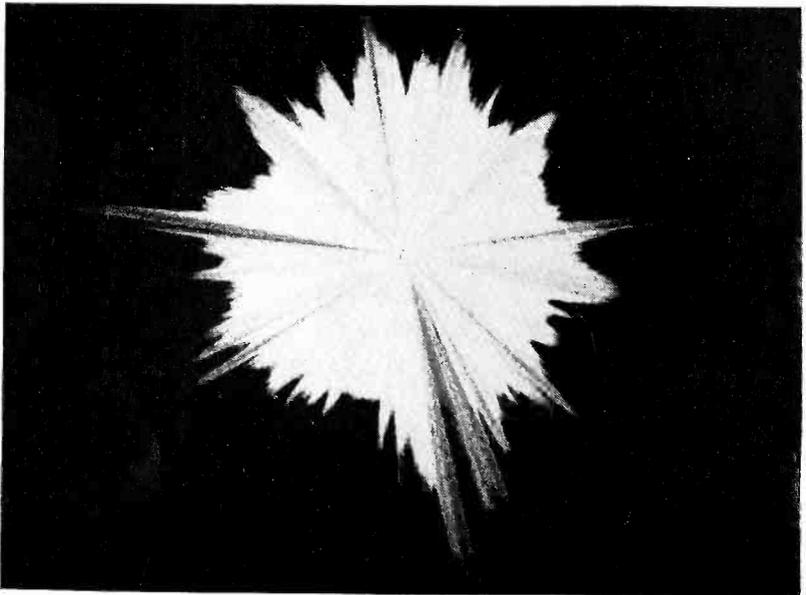
The same principle of a stored charge was used for "zero re-set." Closing of push button switch S2 earthed the "live" side of a  $0.1 \mu\text{F}$  condenser (charged via the  $8\text{M}\Omega$  resistor). This applied a very large negative transient to cathode "O", which thereby seized the glow discharge and set the counter to zero, awaiting the next transient of the auto-align cam. This was very convenient when it was desired to start a recording at a given time or to record a series of phenomena on each rotation. Normally the counter would permit the camera to operate for only one rotation in five or ten according to the position of switch S1. This was to reduce consumption of recording film, when slow moving events, such as the transit of the sun, were being recorded. This automatic camera control would permit a continuous watch up to ten or twelve hours with little more than supervisory attention.

### Typical Records

A number of records were taken including extended periods of up to two hours before sunset. It was possible to determine minima, i.e. the passage of the sun through the minima in the vertical polar diagram of the aerial, to an accuracy of  $\pm 1$  minute of time. This corresponded to a vertical angle accuracy of  $\pm 7.5'$  depending on the rate of climb or fall of the sun for the time of day. In any such measurement the sharpness of the observed minimum must depend on the relative width of the actual minimum compared with the effective angle subtended by the sun. The optical diameter of the sun is about  $32'$  of arc, varying slightly with the season. From the point of view of the radio aerial the diameter is less than the optical diameter, particularly when a burst of energy arises occasionally from a small area such as a sun spot. These bursts are relatively uncommon, however, and any use of the sun for aerial calibration should allow for a number of measurements to obtain an average. In general, the more lobes that exist in an aerial diagram, the sharper, in terms of dBs/degree are the minima. The sun will therefore straddle the minima, which will apparently be less obvious. It will be equivalent in effect to the passage of an opaque shutter over the surface of the sun. If the width of the shutter is less than the solar diameter, some radiation will always pass, and there will never be absolute darkness.



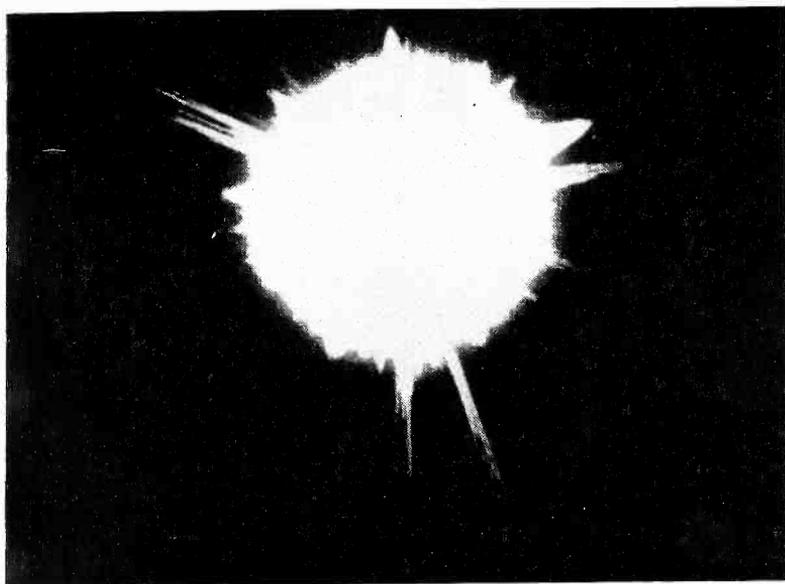
*Fig. 4. Record of Quiet Sun, 250 Mc/s*



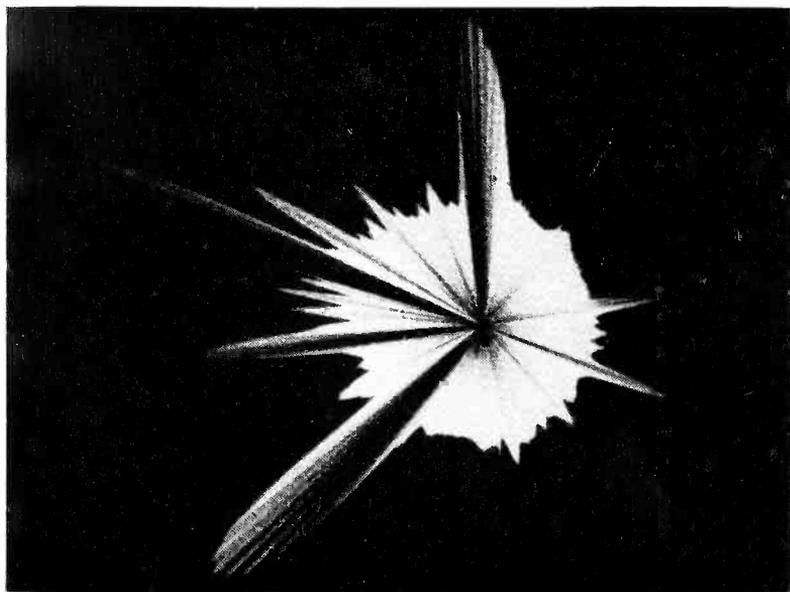
*Fig. 5. Record of Radar Jamming 202.5 Mc/s*

Typical extracts from records are shown in Fig. 4 to Fig. 8. Fig. 4 shows a quiet background of receiver noise with a sharp peak due to solar noise. The small peak was from a weak CW transmitter on 250 Mc/s.

Fig. 5 shows severe jamming from radars on 202.5 Mc/s. The peak



*Fig. 6. Record during thunderstorm*



*Fig. 7. Record of "Polar diagram" due to CW source on 202.5 Mc/s*

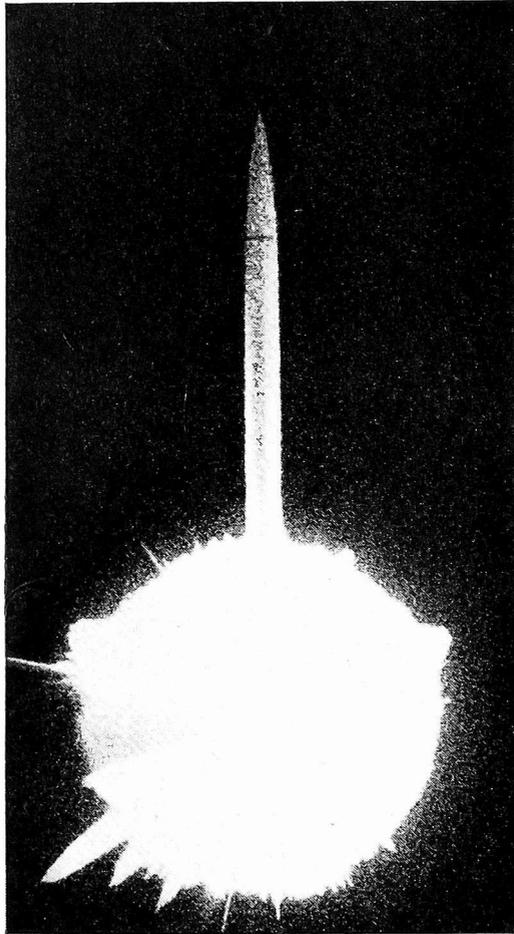
energy is such that they were received on all side lobes of the receiving aerial. Four or five radars were involved.

Fig. 6 was recorded during a summer thunderstorm. Although the central area was marred by halation due to over-exposure of the film,

very sharp pulses were recorded due to lightning flashes. Some idea of the duration of these flashes can be obtained from the aerial speed, which was about 3 r.p.m. Flashes occurred every few seconds. The angular position of the peaks did not correspond to the bearing of the flashes; their power was sufficient to break through, whatever direction the main aerial beam was pointing. It was also noticed that the general noise increased during the onset of the storm. This may have been caused by precipitation charges from the rain striking the aerial.

Fig. 7 is a record of a CW transmission of considerable power, with the receiver gain reduced. A polar diagram of the receiving aerial was thus obtained.

Fig. 8 is a record of a greatly increased solar noise radiation, with several small interfering signals from radar sources.



*Fig. 8. Record of abnormal solar noise, 202.5 Mc/s*

### Example of Aerial Check Using Minima

Observations made with the 202.5 Mc/s aerial gave maxima and minima as follows:

Min. at elevation	36.8°	(sine = 0.6000)
Max. „ „	39.7°	(sine = 0.6388)
Min. „ „	42.5°	(sine = 0.6756)
Max. „ „	45.7°	(sine = 0.7157)
Min. „ „	50.5°	(sine = 0.7710)

It was uncertain which order of maxima and minima were recorded but these were deduced from the equation for the elevation of minima,

$$\text{Sine of elevation angle} = \frac{n\lambda}{2h}$$

where  $\lambda$  = wavelength,  $h$  = effective height of aerial,  $n$  = order of minimum, taking the minimum at zero elevation as  $n = 0$ .

For the minimum at 36.8°  $\frac{n\lambda}{2h} = 0.6000$

and for the minimum at 50.5°

$$\frac{(n + 2)\lambda}{2h} = 0.7710$$

thus, 
$$\frac{n}{0.600} = \frac{n + 2}{0.771}$$

giving  $n = 7$  for the minimum at 36.8°.

At 202.5 Mc/s,  $\lambda = 1.48$  metres. Substituting these values in the equation,

$$0.600 = \frac{7 \times 1.48}{2h}$$

thus, 
$$h = 8.65 \text{ m.}$$

$$= 28.4 \text{ feet.}$$

This corresponded well with the known height to the centre of the aerial of 28.5 feet, and indicated the accuracy obtainable. It also indicated that as far as the flat farmland site of Bedell's End was concerned, it was correct to assume the "reflecting plane" as being the actual surface of the ground.

### Conclusion

The experiments succeeded in proving that the noise radiation from the sun can be used to plot the vertical polar diagram of an aerial. The work

was not carried to the extent of evolving a method of finding the relative gain in the various lobes. There is no doubt that if the input signal had been constantly compared, by a "chopper" method, with a local signal source, giving standard levels as marker rings, the gain could be measured accurately over extended periods. This method could be easily adapted to become a means of plotting the polar diagram of any aerial in any plane, using a reasonably distant CW source.

### Acknowledgements

The author expresses his appreciation to his colleagues, Mr. R. F. O'Neill and Mr. A. Smith, for their assistance in the practical work and to Dr. D. H. Shinn for supplying data on the movements of the sun and moon.

## BOOK REVIEWS

RADIO ENGINEERING HANDBOOK. *Edited by Keith Henney*  
McGraw-Hill Book Co. Ltd. Price £9 14s.

No fewer than thirty-four specialists combined under the editorship of Keith Henney to produce this, the fifth edition of a handbook which made its first appearance in 1933. In the subsequent twenty-six years, radio engineering has developed to such an extent that scarcely any aspect of our lives remains unaffected by it; it is, therefore, not perhaps to be wondered at that even an 1,800 page book such as this, comprising upwards of a million words (it would take three days and nights to read it at an average rate of 250 words per minute), leaves large areas of detail unexplored. Neither is it surprising that the quality varies substantially from chapter to chapter, for the task of editing such a work can be nothing less than formidable.

Nevertheless, the prospective buyer is entitled to expect a work of more than average merit for the £9 14s. at which it is priced, and it is with this consideration that this review must be concerned.

The list of contents shows that, after an introductory chapter entitled "Basis of Radio-communication Engineering," in which is presented a sketch of the fundamental principles involved, the book can be divided into four main sections covering broadly: Circuit Elements and their Properties (eleven chapters), Measurements (two

chapters), Circuits, including aeriels (six chapters), and Systems (eight chapters). Each chapter is the work of a different author (or authors); this is all too obvious as what little overall editing has been attempted has resulted in considerable overlapping of subject matter and no obvious uniformity of treatment. Indeed the Handbook conveys an impression of haphazard assembly, apart from the broad pattern indicated by the chapter headings. This haphazardness can be illustrated by an example taken from Chapters 2, 3, and 4, which deal, respectively, with Resistance, Inductance, and Capacitance. It might be supposed that with these at his elbow the designer would have all the fundamental information required to design resistor, inductors, and capacitors to meet his special needs. Yet, in fact, data on wires and resistance materials are lacking from Chapter 2, which deals at length chiefly with many aspects of proprietary types of resistor (that this may be indicative of the adequacy of the proprietary range for any conceivable application is, surely, beside the point).

The chapters on Inductance and Capacitance adopt a more rational approach and are generally satisfactory.

Here, then, we see some of the problem

in which the editor of a work such as this is placed — how free a hand is he to give his associates, to what extent should he impress his own personality upon the book; what should he include in detail, what in broad outlines; what subjects should be reserved for bibliography; how far should he strive for uniformity of presentation, how may he avoid an impression of incoherence? The success or otherwise of the work depends on making the right compromises, just as in any branch of creative endeavour.

In the opinion of the reviewer this work, both in conception and in sheer weight of words as it is, fails through editorial in-

decision. It is a book which will, very properly, find its way into the reference sections of libraries, and it will on occasion provide the seeker with an adequate survey of some aspect of radio engineering; more often it may suggest references for further reading from its relatively meagre bibliography; seldom is detailed design information of the kind one might reasonably expect in so highly priced a book to be found.

In short, a book priced at £9 14s. must be of exceptional quality if it is to justify its publication; Mr. Henney's work fails by this standard, notwithstanding the galaxy of the talent he has had at his disposal.

## GUIDE TECHNIQUE DE L'ELECTRONIQUE PROFESSIONNELLE

1st Edition 1959. General Editor: Robert Domenach

Published by Publeditec-Domenach, Paris. 2 Vols. 5,500 Fr.

is not enough to know how to make and do things well, but for continued success it is essential to advertise that knowledge. This is the theme of the *Guide Technique de l'Electronique Professionnelle*, neatly summarised in a preface by: "*Savoir faire, bien faire . . . il faut aussi: faire savoir.*"

Its purpose is to put before the new European Common Market the achievements and potentialities of the French Electronics Industry, in all its branches.

The two volumes of the Guide are to some extent usable independently. The main volume contains the presentation of the achievements and the vast amount of advertising. These sections are attractively illustrated and catalogued in colour and are interesting, even fascinating. The smaller volume contains the classified reference lists and business directories, and a few sample checks showed that a user could find the answer to his enquiry in a few seconds. This avoids a long search through 500 pages of distracting advertising, a feature which will be of value to many, whether business executive, sales and purchasing departments, or design and engineering staff. This tried use, however, could result in the two volumes becoming separated, which would create inconvenience. It is a pity, also that such excellent material is contained in rather cheap and easily damaged covers.

The sections dealing with French achievements, and the classified subject lists and

directories are in French, English, German and Italian. Advertising is in French and English. The Guide thus becomes an illustrated technical glossary in four languages, which many users may find of value, apart from its main function. The sections mentioned are, for the most part, well, if freely, translated into English, but unfortunately, some advertisers have very poor translations, a few making nonsense.

There are rather too many English printing errors, some of which are amusing, as, for example, in the second preface, where "production drive" is printed as "production dive."

In general, it is easier to read those catalogue sections where the English text is separated from the French in blocks of smaller type, rather than those which are interleaved line by line.

It is a little surprising to find much American equipment advertised under a guide to French Electronics, since a sales agency cannot be an industry in the sense claimed by the Guide. However, the influence of the U.S.A. is seen in the classified lists where "valves" refers entirely to mechanical types. Radio valves must be sought under "tubes" and tubes appear under "piping."

The editors have chosen to adopt the American usage of words; a note, in parentheses, where this occurs might be of use for English readers.

## PRINCIPLES AND PRACTICE OF RADAR (SIXTH EDITION)

by *H. E. Penrose and R. S. H. Boulding*. George Newnes Ltd. Price 50s.

The authors have attempted, like many others, to cover a very wide subject in one book without the use of mathematics, to such an extent that this book must be classed as one belonging to the Popular Press Category.

There may have been justification in the early 1920 period to develop the theory of transmission lines from a resistance ladder network but, today, there can be little justification for such an approach in an appendix to a book such as this, particularly when it is followed by an appendix on waveguides.

Although in many places the authors state that the reader is assumed to be familiar with the more usual radio circuits they find it necessary to run through basic principles but in such a skimpy manner as to be of little or no value to the reader.

Some 280 pages out of a total of 800 are given over to description of actual equipment manufactured by some six British manufacturers. This description is clear and quite detailed but it is puzzling to find that circular polarization and MTI are dealt with in this section rather than under the "Principles" section.

The preface states that "later developments such as lenses, slot aerials, slot arrays, and the Cosecant Squared aerial have been added" but not more than one page is given to any of the above subjects. Fortunately, they have all been very fully covered in the literature since the war.

The phraseology is in many instances difficult to follow. For example when the student has mastered the meaning of the title of Chapter IX "Rectangular pulses having a definite time duration and the development of high voltage high power time control pulses at low and high level" he will then have to struggle through several explanations followed by "In other words" or "That is to say . . .".

From reading the book it is impossible to obtain a clear understanding of impedance matching. If the simple calculations on matching a cathode follower into a coaxial cable, page 134, had been taken a little further and the useful power into the cable load calculated it would be realized that the matching exercise was a very effective

method of putting energy where it is not wanted. The authors do not make it clear why matching is desirable in this case. The last paragraph on page 140 is equally misleading particularly when it is appreciated that the most common type of high power pulse modulator, i.e., the artificial line and thyatron modulator, has very poor regulation.

When the authors state that the alternative to a hard valve modulator, which they state has an upper limit of 27 kV operating potential, is a spark gap they neglect completely high power modulator developments during the last ten years. To brush aside the thyatron in one line in Chapter IX and half a page on page 330 is doing the brilliant work of many physicists a gross injustice. At the present day the rotary or stationary spark gap is probably only used in isolated cases for laboratory test purposes, and it would be next to impossible to find one in a piece of service equipment.

The operating cycles of a number of multivibrator circuits are clearly dealt with in Chapter X but a fully worked out example would have been useful.

Although over fifty pages are given to Time Base Circuits and Display Units, no reference is made to Fixed Coil Displays and the many additional facilities that can follow.

Certain errors exist in the illustrations. For example the dots and crosses in Fig. 1 (4) indicating the magnetic field are incorrect and should be of a similar pattern to that indicated in Fig. 11 (c). The distance of the magnetic coupling loop from the end of the guide in Fig. 14 (b) should be  $\lambda_2$  and not  $\lambda_4$  as indicated.

From the general form of the waveguide illustrated in Fig. 18 (a) and 18 (b) one would expect the equivalent dipole radiators to radiate with the same polarization. The meaning to be conveyed by Fig. 18 (a) is not clear.

As an introduction to Chapter XXIX on "Typical Radar Installations" the author discusses two systems, intended to illustrate the application of general principles upon which radar systems are worked out. The all important principle of the relationship between peak transmitter power, pulse

length, aerial gain, receiver noise factor and effective target area, more commonly referred to as "The Radar Equation" seems to have been forgotten.

The above remarks criticize, in detail, the points which immediately strike the reader. Summarizing, it may be said that

Principles and Practices of Radar gives the reader an introduction to the elements of small radars.

It does not deal with the more complicated modern systems and particularly the highly complicated data handling side of modern radar.

#### EXPERIMENTAL RADIO ENGINEERING by E. T. A. Rapson

Isaac Pitman and Sons Ltd. Price 12s. 6d.

Experimental work that is so necessary in any radio engineering course will be complemented very usefully by carrying out measurements and experiments outlined in this volume. As the author is head of the Department of Electrical Engineering at Southall Technical College, he is in a favourable position for planning such work. In general, the experiments are graded, and the student is likely to find that a three or four year course at a technical college will take him over the ground covered by the experiments roughly in the order given in the book. Starting with series and parallel circuits and coupled circuits, measurements of the static characteristics and dynamic characteristics of valves are described. A number of experiments in connection with amplifiers, demodulators and oscillators are then given and also attenuators and filters. The Appendix Section XIII contains seven experiments with cathode ray tubes, time base applications.

The range of experiments is surprisingly wide for a book of this size. This is possible because of the abbreviated style of the book and to the complete absence of theory. Nevertheless, each experiment is adequately explained for the engineering student; and component values are stated. Most students will find the component values a great time saver, but the reviewer is not

entirely in favour of helping an experimenter much in this respect: an intelligent student should know how to work out his own values.

Conclusions to be deduced from the experiments are outlined in thirty pages at the back of the book and these form a most valuable aid to the experimenter. So much so, indeed, that the omission of conclusions in respect of the experiments on transistors and the Foster Seeley frequency discriminator is unfortunate, especially as these are so important in the design of present types of radio receivers.

By and large, the experiments represent current practice but it is surprising to find some relating to the split anode magnetron. The Randall and Boot cavity magnetron superseded the split anode magnetron in 1941, and has been used almost exclusively in industry ever since. During revision, the opportunity should also have been taken to include measurements on the ratio detector which is used so extensively in F.M. receivers. The experiment on the amplitude discriminator is of little more than academic interest.

As a contribution to the literature for training radio engineers, this book is admirable. It is certainly worthy of a place in the library of every serious minded student.

#### RADIO CIRCUITS by W. E. Miller, revised by E. A. W. Spreadbury

Isaac Pitman and Sons Ltd. Price 15s.

Enough circuits are always interesting and intriguing to an engineer, a beginner often finds them baffling, especially when presented with a diagram of a complete receiver. In the present Volume the authors dissect the radio receiver and group together the various partial-circuits encoun-

tered in different types of receiver. The explanatory notes are written in an elementary style that will suit the tyro and which presuppose no technical knowledge on the reader's part.

*Radio Circuits* is far too ambitious a title for this little volume, for the authors have

dealt only with broadcast receivers—communication receivers are not even mentioned. The broadcast receiver is broken down into such small divisions that there are thirty-eight chapters in the 170 pages. Indeed, the book tends to be disjointed because of this. For example, the aerial input circuits are covered by three chapters: "Aerial Input Circuits," "Tuned Input Circuits" and "Band Pass Coupling." The subject is nevertheless well treated at the level stated and the reader is introduced briefly, but logically, to the various stages starting at the "front end." Nine pages (three chapters) are devoted to A.G.C., and the different types of push-pull circuits are outlined. Negative feedback, tuning indicator devices and transistor receivers are each dealt with in a separate short chapter. The concluding section of thirteen pages is devoted to F.M. receivers.

It is a pity that the text was not cleared

of "deadwood" during the revision. A chapter is included, for example, on "Early F.C. Circuits" which describes some frequency changer circuits that have not been used in broadcast receivers since the early 'thirties. In another part of the book, several tuning indicators are described that have become obsolete since the middle 'thirties when the cathode ray indicator made its bow. The elementary reader will also be somewhat confused to be told on page thirty-one that additive mixers are not much used, and then to find that additive mixing is employed almost exclusively in transistor receivers and F.M. receivers. In neither case, however, is an explanation of the additive mixing process given.

These are minor criticisms of a useful volume on broadcast receiver circuits which provides an introductory description of a wide range of circuits used in present day models.

## PRINCIPLES OF FREQUENCY MODULATION

by *B. S. Camies*. Iliffe and Sons. Price 21s.

Frequency modulation is a subject that has received attention from a number of technical authors in recent years. This latest book on the subject is intended to appeal to engineers and amateurs in providing a survey of the art in its various applications.

The first three chapters form a theoretical explanation of frequency modulation and include one on frequency modulation in relation to interference. The reviewer considers this chapter to be the best in the book. Various types of interference are considered, including that due to the valves and circuits, and the treatment is comprehensive for a book of this size.

Frequency modulated generators are briefly described in Chapter 4, the various types including the frequency modulated quartz (FMQ) system. No acknowledgement is made to the Marconi Company as originators and patentees of the FMQ system nor is mention made of the extensive use by the BBC of transmitters based on this system. However, acknowledgement is given to Armstrong for his design of modulator. Reference might have been made to the serrasoid system which, although not in favour in this country, has been used in the United States.

FM receivers are dealt with in two chapters, one being devoted to FM detec-

tion. These provide a sound practical description of the FM receiver, and current types of discriminators, e.g. the Foster Seeley and the ratio detector are adequately dealt with. Some confusion is likely to arise from the circuit shown on page 93 which purports to illustrate the ratio detector arranged to provide AGC. The only difference between this circuit and the one given on the page facing it is that the polarity of the reservoir capacitor has been reversed. The diodes themselves should also, of course, have been reversed.

The non-broadcast applications include the use of klystrons and the application of FM to radar, including Doppler radar and FM radar. This is the least detailed part of the book but should be regarded as an introductory outline. The ten-page section on radar, for example, starts at very first principles of pulse radar and includes four pages on Doppler radar and two on FM radar.

The author's clear and direct style renders the text easy to follow, while the numerical examples included in the text will aid in the more elementary type of design calculations. The author has succeeded in his object and has produced a volume that will be a useful and practical guide to the less advanced engineer and student.

## FUNDAMENTALS OF RADIO TELEMETRY by Marvin Tepper

John F. Rider Inc. Price \$2.95

Radio telemetry is an art that has come very much to the fore in recent years, mainly because of the spectacular advance in guided missile techniques and earth-bound satellites. Telemetry itself, however, is not a new art, having been the hunting ground of inventors since before the turn of the century. Probably the best known example of radio telemetry is the radio sonde which has been employed by the Air Ministry since the middle 1930's. It is fitting that, in view of the wide topical interest displayed, a book should be produced, such as the one under review, that purports to explain to the layman some of the intricacies of the subject.

The author has attempted to present an overall picture of the radio telemetric art as applied to a large range of equipments. This is a very ambitious object for so small a book, especially bearing in mind the complex nature of such aspects of telemetry as data handling and digital techniques. However, the volume is not intended to do more than the most elementary description and this probably is the reason for the inclusion of so many illustrations of cartoon type for the purpose of explaining even the most rudimentary features. In fact, a good half of the book consists of these illustrations.

The ground covered ranges from an introductory chapter on first principles, through multiplexing, data handling to the radio telemetry associated with missiles and satellites. A typical telemetric receiving station is described and a large chapter on recovering and recording the data. Page 93 virtually terminates the text but there follows a very useful bibliography (five pages) and also two appendices giving the United States standards on telemetry for guided missiles and magnetic recorders and reproducers.

It is not apparent to whom the book is directed, as the author does not seem to be able to make his mind up whether he is writing for a reader who is sufficiently knowledgeable to be able to assimilate, without explanation, the theoretical diagram (on page 22) of a six-valve transmitter for phase or frequency modulation; or for a tyro who cannot count and therefore has to be presented with a picture (page 43) of three specimen recording tapes showing respectively two, seven and fourteen recording tracks.

As an introduction to radio telemetry, this book may appeal to a layman who enjoys strip cartoons, but an engineer will seek his knowledge in more profound and balanced texts.

## NEAR NETWORK ANALYSIS by S. Seshu and N. Balabanian

McGraw-Hill Book Co. Price £4 14s.

In the last five years, a profusion of books has appeared in the U.S.A., dealing with electric network analysis and synthesis. Most of these are edited versions of lecture notes used in graduate courses at Universities. The amount of material covered in them is roughly the same and this makes it very difficult for a prospective student to judge their relative merits.

The authors of the present book are well known in specialist circles from papers on network topology and frequency transmutation respectively. They make a justified claim that their book attempts to show both out the transition between steady state or frequency and transient or time

responses, as exemplified in the two classic works in these respective areas: Guillemin's *Communication Networks* and Gardner's and Barnes' *Transients in Linear Systems*. The text is written very lucidly; the flow of argument is easy to follow making it a valuable textbook. However, the diversity of aims causes the authors occasionally to stop the argument almost in mid-stream, in order to start with a new chapter. This is especially evident in the second half of the book where feedback, stability and filter theory are considered.

It is assumed that the reader is acquainted with the elements of the complex variable theory, Laplace transforms and elementary

network analysis. The first four chapters deal with the fundamental concepts (loop and node systems of equations, elementary topology, etc.); the discussion on network elements is very illuminating—see, for example, discussion on relationship between perfect and ideal transformers.

The next two chapters deal with the steady state and the transient responses, containing among others an excellent treatment on steady state response to a general periodic excitation and on relationship between frequency and time responses. Chapter 7 concerns the analytic properties and representation of network functions. The so called Bode relations form the backbone of the argument. The authors follow here, very successfully, the treatment given by Guillemin in his *Mathematics of Circuit Analysis*. Complete and separate procedures are provided for calculation of network functions from given magnitude, angle or real part. It is a pity, however, that very little is said on how to obtain suitable initial functions, satisfying given requirements within some approximation. The potential analogue method, discussed here, has many obvious limitations, while nothing is said on the least square approximation, Tchebysheff's polynomials and other well-known mathematical tools.

The following two chapters deal with the elements of the quadripole (two-port networks) theory, especially with various matrix representations; the scattering matrix is clearly represented. The Foster Reactance Theorem and Cauer's modification for RL and RC networks are also included here.

Chapter 10 contains elementary feedback and stability theory. The signal-flowgraph technique is very ably explained. The discussion on the stability criteria, however, could have been profitably extended: the Hurwitz continuous fraction test, when performed with limited accuracy, is often unreliable even misleading.

The last chapter, on image parameter and filter theory, is least satisfactory with scanty treatment of the determination of image parameters. Also, no attempt is made to correlate results of chapter 7 with a synthesis procedure. A short appendix gives elements of complex variable and Laplace transformation theory.

In spite of these criticisms this is a very valuable contribution to the network literature and a convenient tutorial tool; original and daring in treatment and scope, clear exposition, a stimulating stepping stone to more complicated and difficult aspects of the theory.

## AN APPROACH TO ELECTRICAL SCIENCE

by Henry G. Booker. Published by McGraw-Hill Publishing Co. Ltd. Price 74s.

When the author of this book went to Cornell University he had already gained a wide reputation for his original outlook in presenting and applying electromagnetic theory. The appearance of this new treatise is therefore of particular interest to those who have to teach the fundamentals of electrical science, for the author has aimed at getting the best of all worlds by steering his way between the outlooks usually adopted by the electrical engineer, the physicist and the mathematician.

Following the physicist he begins with a discussion on electric charges and fields, but when he comes to consider magnetic fields he favours the viewpoint of the electrical engineer except that instead of working in terms of ampere turns per metre he shows that it is desirable to express the field in amperes per metre. Here he brings to bear

his war-time experience of teaching radio to graduates in other subjects who had thought of magnetic fields as they occur in wave-guides and cavities rather than in solenoids.

The treatment essentially relates electro-magnetic phenomena to the presence of electric charges which are static or in motion. Forces on a charge which are the result of its motion are said to be of magnetic origin and the concept of magnetic flux is introduced by considering the movement of charges in the space between the inner and outer conductors of a cylindrical transmission line carrying a steady current. The idealized magnetic pole and the properties of magnets are then eventually derived almost as a by-product instead of being used to establish the existence and nature of magnetic fields.

The book claims to present a unified and consistent description of electro-magnetism which can be used as a basis for teaching the subject to a student who may have any knowledge of other approaches. Such it is extremely well thought out and ably argued and it lends itself naturally to the use of a single system of units.

It is difficult, however, to avoid the impression that the treatment is too facile, as it dispenses very largely with the experimental basis of the historical approach and replaces it with statements that are made to appear almost self-evident. It is interesting speculation whether in principle the knowledge of electromagnetic theory could have been developed in the way this book implies.

Possibly the author could have done better service to his cause by writing a shorter book more especially for teachers to help them to re-think the knowledge of the subject that they already possess. As it is, the book sets out to be not only a new approach but also a self-contained textbook producing a great deal of standard procedure. As such it is almost tedious in its detail; for instance it discusses network theorems in basically the same way three times, first for capacitors, then for resistors and finally for inductors, though in his

preface the author seeks to justify this emphasis on the embracing nature of Kirchhoff's laws.

An attractive feature of the book is a set of summarizing exercises at the end of each chapter designed specifically to make the student prove to himself that he has understood the chapter, while at the end of the book are eighty pages of problems. The author has aimed at making the mathematics as simple as possible, and for this reason although he makes some use of vector algebra he stops short of using vector analysis.

He promises a sequel in which vector analysis will be used as a vehicle of thought in oscillation theory in contrast to the mere use of complex numbers as a tool for calculation. Here presumably he will deal in detail with wave theory which is only touched on in the present book. This further work will be eagerly awaited as it is certain to be even more original and stimulating. Meanwhile, although this "approach to electrical science" may not prove to be an ideal textbook, it will be an invaluable source of information to which many will continually refer, and not least those who are concerned with research and development work who need from time to time to refresh their ideas on the fundamentals of electromagnetism.

#### VO-WAY RADIO by Allan H. Lytel

Graw-Hill, 1959. Price 74s.

This book deals in a practical way with equipment for radio telephone communication between road vehicles and fixed stations, using the frequency band 30—50 Mc/s. Such equipment is much less used in Europe than in America, where over one and half million transmitters are in use. In U.S.A. this equipment may be repaired and tested only by licensed operators, the licensing requirements for these licences being outlined in the first chapter. The widespread use of mobile radio in America creates a demand for qualified service engineers, and the non-mathematical approach in the book is directed to those readers rather than to the design engineer. The subject matter is almost entirely descriptive of existing commercial apparatus, with numerous illustrations. The introductory chapter sketches mobile communication systems and explains their purpose,

with some advice about meeting the equipment regulations and licensing requirements. The basic differences between frequency- and amplitude-modulation are explained with numerous diagrams and almost without mathematics. The core of the book is composed of descriptions and explanations of frequency- and amplitude-modulated transmitters and receivers, with more attention to the former. The space devoted to single-sideband modulation is generous, considering that such methods have not yet been commercially introduced in the mobile service.

Most of the aeri-als used in the mobile service are described and illustrated, with informative polar diagrams showing their directional properties. The fundamental principles to be used when selecting an aerial are scarcely mentioned and half of the introductory material about aeri-als is

inexplicably reserved for the final section of the chapter.

There is no indication how far selective calling of a single station in a network has been implemented in U.S. but examples of both tone and impulse systems are described in detail, specific equipments being singled out for treatment. It is surprising that resonant reeds are not mentioned. Vibrator and transistor oscillator power supplies are clearly explained without unnecessary detail.

Installation and servicing will constitute the main duties of the readers to whom the book is addressed. The important "do's and don'ts" of installation will be useful to the beginner, but it is doubtful whether the description of the tools and methods of the service engineer can compare with personal instruction and extensive bench experience.

The printing and illustrations are done in the excellent way which one expects in McGraw-Hill publications. It cannot be said that the material justifies this care. Some sections are a jumble of sentences, apparently derived from apparatus instruc-

tion books, with an ample sprinkling non-precise terms, which lead to difficult reading. Modulation and sidebands can be introduced without mathematics with clearly explained vector diagrams; in this book the explanation is poor and some of the vector diagrams are so unorthodox as to be incomprehensible. Of 277 well-printed illustrations, many are quite uninformative. One photograph of mobile radio equipment and one paragraph could convey the information of the seventeen photographs in Chapter 1, mostly showing happy truck drivers leaning, microphone in hand from their driving cabs. How many readers will benefit from Figs. 9—14, which show how to knock the cover off one particular piece of equipment?

A book intended for relatively non-technical readers probably needs more care in choice of material and presentation than one directed to highly skilled engineers. Perhaps the ten years which the author took to complete the book have somewhat to do with the confused impact which was made on the reviewer.

#### RADIO AND ELECTRONIC COMPONENTS Sir Isaac Pitman and Sons Ltd.

Vol. III Fixed Capacitors *by G. W. A. Dummer*. Price 45s.

Vol. IV Variable Capacitors and Trimmers *by G. W. A. Dummer*. Price 32s. 6d.

The first two volumes of this series, dealing with fixed and variable resistors, which were noticed in *Marconi Review* No. 123 have been followed by the two now under review. The same general arrangement has been followed. The first twenty or so pages of general information are common to both volumes, thus avoiding cross referencing. This is followed by a brief review of the types of component available, based in the case of Vol. III on dielectric material and, in Vol. IV on application and by methods of measurement of characteristics appropriate to each class.

Succeeding chapters deal with the various types in detail, the last two covering possible faults and future developments respectively.

Both volumes include a very extensive bibliography and a comprehensive comparison chart which facilitates selection of a particular purpose. Service-type components have been chosen as representative of the large number of types available; this does not detract from the worth of the books which constitute a valuable source of reference, not only to the components themselves, but to characteristics and properties of materials used.