#  <br> ELECTRONICS 

## cyill

 C 6 - $0^{0000}$

$$
0 \text { O }
$$ of damage to expensive transistors and integrated circuits, when soldering? Use Antex low-leakage soldering irons

## 220-240 Volts or $100-120$ Volts <br> Model X25

The leak age current of the NEW $\times 25$
is only a few microamps and cannot harm the most delicate equipment even when soldered "live" Tested at 1500 v . A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder" any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages. Fitted long-life iron-coated bit $1 / 8^{\prime}$ 2 other bits available $3 / 32^{\prime \prime}$ and $3 / 16^{\prime \prime}$.

PRICE: $£ 1.75$ (rec. retail) Suitable for production work and as a general purpose iron

## Model CCN <br> 220 volts or 240 volts

The 15 watt miniature model CCN also has negligible leakage. - Test voltage 4000 v . A.C. Totally enclosed element in ceramic shaft. Fitted long-life iron-coated bit $3 / 32^{\prime \prime}$ 4 other bits available $1 / 8^{\prime \prime}, 3 / 16^{\prime \prime} 1 / 4^{\prime \prime}$ and $1 / 16^{\prime \prime}$ PRICE: $£ 1.80$ (rec. retail)

OR Fitted with triple-coated, (iron, nickel and Chromium) bit $1 / 8^{\prime \prime}$
PRICE: $£ 1.95$ (rec. retail)

Totally enclosed element in ceramic and steel shaft Bits do not "freeze" and can easily be removed

A SELECTION OF OTHER SOLDERING EQUIPMENT.

## MODEL CN

Miniature 15 watt soldering iron fitted $3 / 32^{\prime \prime}$ ironcoated bit. Many other bits available from 3/64" to $3 / 16^{\prime \prime}$. Voltages $240,220,110,50$ or 24
PRICE: $£ 1.70$ (rec. retail)

## MODEL CN2

Miniature 15 watt soldering iron fitted with nickel plated bit $3 / 32^{\prime \prime}$. Voltages 240 or 220
PRICE. $£ 1.70$ (rec. retail)

$1-$


MODEL G
18 Watt miniature iron, fitted with long life ironcoated bit $3 / 32^{\prime \prime}$. Voltages 240,220 or 110. PRICE. $£ 1.83$ (rec. retail)

MODEL SK. 1 KIT
contains 15 Watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit, 2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$, heat sink, solder, stand and "How to Solder" booklet. PRICE £2.75
(Rec. retail)
MODELSK. 2 KIT contains 15 Watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit, 2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$
 heat sink. solder and booklet "How to Solder

## MODEL

MES.KIT Battery-operated 12v. 25 watt iron fitted with $15^{\prime}$ lead and 2 heavy clips for connection to car battery. Packed in strong plastic wallet with book let "How to Solder." PRICE $£ 1.95$
(Rec. retail)
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Our March issue will be published on Friday, February 9, 1973

[^0]
# The revolutionary new Supertester 680R. Buy it for what it is. Or buy it for what it can be. <br> itself a high quatity test meter with eighty ranges on a 128 mm mirror backed scale. it is also the basis of a complete measurement system. With the addition of the appropriate accessories it can measure a wide range of values including light, temperature, gauss and phase sequence. And there are other accessories to greatly extend the 680R's range. The 680R System offers many advantages over conventional test meters including tremendous versatility and economy. <br> ACCESSORIES TO CONVERT THE SUPERTESTER 680R TO THE FOLLOWING: Amperclamp : Signal Temperature <br> <div class="inline-tabular"><table id="tabular" data-type="subtable">
<tbody>
<tr style="border-top: none !important; border-bottom: none !important;">
<td style="text-align: center; border-left-style: solid !important; border-left-width: 1px !important; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top-style: solid !important; border-top-width: 1px !important; width: auto; vertical-align: middle; " class="_empty"></td>
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<td style="text-align: center; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top-style: solid !important; border-top-width: 1px !important; width: auto; vertical-align: middle; ">Probe</td>
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<td style="text-align: center; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top: none !important; width: auto; vertical-align: middle; ">Covering the range</td>
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<td style="text-align: center; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top: none !important; width: auto; vertical-align: middle; ">$30^{\circ} \mathrm{C}$ to $200{ }^{\circ} \mathrm{C}$</td>
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</tr>
<tr style="border-top: none !important; border-bottom: none !important;">
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| :--- |
| 500 A [1195 |</td>
<td style="text-align: center; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top: none !important; width: auto; vertical-align: middle; ">Stgrals</td>
<td style="text-align: center; border-right-style: solid !important; border-right-width: 1px !important; border-bottom-style: solid !important; border-bottom-width: 1px !important; border-top: none !important; width: auto; vertical-align: middle; " class="_empty"></td>
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</tbody>
</table>
<table-markdown style="display: none">|  | Injector | Probe |
| :---: | :---: | :---: |
| For measut. | producing | Covering the range |
| ing a.c | 1 kHz and | $30^{\circ} \mathrm{C}$ to $200{ }^{\circ} \mathrm{C}$ |
| currents from | 500 kHz | £1195 |
| 250mA 10 &lt;br&gt; 500 A [1195 | Stgrals |  |</table-markdown></div> <br> Gauss PhaseSequence ElectronicVoltmeter Transistor Meter Indicator 

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4. 

## LASKYS SUPER

 NEW YEAR OFFER PRICE
## THIS IS THE FIRST PAGE OF THE GREAT Bl-PAK SECTION

## BRAND NEW FULLY GUARANTEED DEVICES



## NEW COMPONENT PAK BARGAINS

Pack

| No. | Oty. | Description |
| :---: | :---: | :---: |
| C 1 | 250 | Resistors mized values approx. count by weight |
| C 2 | 200 | Capacitors mixed values approx, count by weight |
| C 3 | 50 | Precision Resistors $1 \%, \cdot 01 \%$ mixed values |
| C 4 | 75 | th W Resistors mixed preferred values |
| C 5 | 8 | Pieces assorted Ferrite Rods |
| C 6 | 2 | Tuaing Gangg, MW/LW VHF |
| C 7 | 1 | Pack Wire 50 metres assorted colours |
| C 8 | 10 | Reed 8witches |
| C 9 | 3 | Micro Switches |
| C10 | 15 | Assorted Pots \& Pre.Sets |
| 11 | 5 | Jack Sockets $3 \times 35 \mathrm{~m} 2 \times$ Standard 8witch Trpe |
| $\mathrm{Cl2}$ | 40 | Paper Condensers preferred types mixed values |
| C13 | 20 | Electrolytics Trans. types |
| C14 | 1 | Pack assorted Hardware-Nuts/Bolts, Grommets |
| C15 | 4 | Mains Toggle ${ }_{\text {Switches, }} 2 \mathrm{Amp} \mathrm{D} / \mathrm{P}$ |
| C16 | 20 | Assorted Tag Strips \& Panels |
| C17 | 10 | Assorted Control Knobs |
| C18 | 4 | Rotary Wave Change Switches |
| C19 | 3 | Relays 6-24V Operating |
| C20 | 4 | Sheets Copper Laminate approx. $10^{*} \times 7^{*}$ | on pack Nos. $\mathrm{Cl}_{\mathrm{T}} \mathrm{C} 2, \mathrm{C} 19, \mathrm{C} 20$

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Each Kit contains two Amplifier Modules, 3 watts RMS, two loudspeakers, 15 ohms, the pre-amplifier, transformer, power supply module, front panel and other accessories, as well as an illustrated stage-by-stage instruction booklet designed for the beginner. Further details available on 5 , request.



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100 \& 0.25 \& 0.33 \& 0.47 \& 0.47 \& 0.50 \& 0.58 \& 0.63 \& 1.40 <br>
200 \& 0.35 \& 0.37 \& 0.49 \& 0.49 \& 0 \& 57 \& 0.611 \& 0.75 <br>
\hline

 

200 \& 0 \& 35 \& 0.37 \& 0 \& -49 \& 0.49 \& 0 \& 57 \& $0 \cdot 61$ \& 0.75 <br>
400 \& 0.43 \& $0-47$ \& 0 \& 56 \& $0-58$ \& 0 \& 67 \& 0 \& -75 \& 0.93 <br>
\hline
\end{tabular} 4000.43

6000.53
$\begin{array}{llllllllll}800 & 0.63 & 0.57 & 0.68 & 0.68 & 0.77 & 0.97 & 1 & .25 & - \\ 800 & 0.68 & 0.70 & 0.80 & 0.80 & 0.90 & 1.20 & 1.50 & 4.00\end{array}$
SIL. RECTS. TESTED

PIV 300 mA 750 mA IA 1.5 A 3 A 10A 30 A $\begin{array}{llllllll}50 & 0.04 & 0.05 & 0.05 & 0.07 & 0.14 & 0.21 & 0.60 \\ 100 & 0.04 & 0.06 & 0.05 & 0.13 & 0.16 & 0.29 & 0.75\end{array}$ | 100 | 0.04 | 0.06 | 0.05 | 0.13 | 0.16 | 0.23 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.65 |  |  |  |  |  |  |
| 200 | 0.05 | 0.09 | 0.06 | 0.14 | 0.20 | 0.24 | $\begin{array}{llllllll}200 & 0.05 & 0.09 & 0.06 & 0.14 & 0 \cdot 20 & 0.24 & 1 \cdot 00 \\ 400 & 0.06 & 0.13 & 0.07 & 0.20 & 0.27 & 0.37 & 1.25 \\ 600 & 0.07 & 0.16 & 0.10 & 0.24 & 0.34 & 0.45 & 1.86\end{array}$ $\begin{array}{llllllll}8000.67 & 0.16 & 0.10 & 0.2 & 0.34 & 0.45 & 1.86 \\ 800 & 0.10 & 0.17 & 0.11 & 0.25 & 0.37 & 0.55 & 2.00\end{array}$ $\begin{array}{llllllll}10000.11 & 0.25 & 0.14 & 0.30 & 0.46 & 0.63 & 2.50\end{array}$ $\begin{array}{llll}0.38 & 0-67 & 0 & -75\end{array}$

| TRIAC8 |
| :--- |
| VBOM 2A 6A | TO-1 T0 10 A FULL RANGE VOLER DIODES RANGE 8-33V. 400 mV (DO-7

 Case) 18p ea. 1\%W (TopStud) 25p ea. All fully teated $5 \%$ tol and
narked. State voltage rnarked.
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| 1 |

10 amp POTTED BRIDGE RECTIFIER
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ORP60, OliP61 40p eac GENERAL PURPOSE NPN SILICON SWITCHING TRANS. TO-18 SLM. TO 2N700/8. BSY27/28/05A. All unable
devlces no open or ahort
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25 up 15 p each.

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| :---: | :---: | :---: |
| Q1 | 20 Red spot transistors PNP | 0. 50 |
| Q2 | 16 White «pot R F. transistors PNP | 0.80 |
| Q3 | 4 OC 77 type transistors | 0.50 |
| Q4 | 6 Matched transistors OC44/45/81/8 | 30 |
| Q5 | 4 OC 75 transistors | 0.80 |
| Q5 | 5 OC 72 transigtors | 0.50 |
| Q7 | 4 AC 128 tranaistors PN P high gain | 0.50 |
| Q8 | 4 AC 126 tramistors PNP | $0 \cdot 50$ |
| Q9 | OC 81 ty de transiators |  |
| Q10 | 7 OC 71 type transistors |  |
| Q11 | 2 AC 127/128 Complementary pairs PNP/NPN |  |
| Q12 | 3 AF 116 type transistors | 0. 50 |
| Q13 | 3 AF 117 trpe transistors | 0.60 |
| Q14 | $30 \mathrm{O} 171 \mathrm{H}, \mathrm{F}$. type transistors |  |
| Q15 | 7 2N2926 Bil. Epoxy transistors mixed colourg |  |
| Q16 | 2 get880 low noise Gerinanium |  |
| Q17 | 5 NPN $2 \times$ ST. 141 \& $3 \times 8 T .140$. | 0. 50 |
| Q18 | 4 MADT*\& $2 \times$ MAT $100 \& 2 \times$ MAT 120 | $0 \cdot 50$ |
| Q19 | 3 MADT'S $2 \times$ MAT $101 \& 1 \times$ MAT 121 |  |
| Q20 | 4 OC 44 (iermanium transistors A.F | 0.50 |
| Q21 | 4 AC 127 NPN Germanium transisto |  |
| Q22 | 20 N KT transistors A.F. R.F. coded | 0. 80 |
| Q23 | 10 OA 202 silicon hiodes sub-min |  |
| Q24 | 8 OA 81 diodes | $0 \cdot 80$ |
| Q25 | 15 IN914 Silicon dioles 75 PIV 75 ma |  |
| Q26 | 8 OA95 Germanium dioles bub-min INi9 ............................. | $0 \cdot 50$ |
| Q27 | 2 10A PIV Silicon rectiffers I8425R | $0 \cdot 30$ |
| Q28 | 2 Slicon wower rectifiers BFY 13 | 0. 80 |
| Q29 | 4 silicon transiators $2 \times 2 \times 296$, $1 \times 2 \mathrm{~N} 697,1 \times 2 \mathrm{~N} 698$ | 0.50 |
| Q30 | 7 sllicon switch transistors 2N706 NPN |  |
| Q31 | 6 Silicon switch transistors 2N708 | - 50 |
| Q32 | 3 PNP Bilicon transistors $2 \times 2$ N1131, <br> $1 \times 2 \mathrm{~N} 1132$ | O. 50 |
| Q33 | 3 silicon NPN transistors 2NiJII | 0.50 |
| Q34 | 7 silicon NPN transistors 2Na369. 500 MHz (cole P397) | $0 \cdot 50$ |
| Q35 | 3 Silicon PNP TO-5. $2 \times 2$ N2904 \& $1 \times 2 \mathrm{~N} 290 \mathrm{~K}$ | 0.50 |
| Q3a | $72 \mathrm{~N} 3646 \mathrm{TO}-18$ plastic 300 MHz NPN | 0.50 |
| Q37 | 32 N 3053 NPN Silicon tranaistors |  |
| Q38 | 7 NPN transistors $4 \times 2 \mathrm{~N} 3703, \triangleleft \times$ | $0.50$ |

ELECTRONIC SLIDE-RULE
The MK Slide Rule. designed to simplify Elec Conne calculations features the following acales:-
of Frequency and Wavelength Calculation of $L$, i and fo of Tuned Circuite Reactance and Self Inductance. Area of Circles. Volnme of Cylinders. Reaistance of Conductora Weight of Condurtors. Decibel Calculations Angle Functiona. Natural Logs and 'e' Functiona Multiplication and Division. Equaring, Cubing and A वuare Koots. Conversion of kW and Hp A must for every electronic engineer and enthusi
ast. Size: $2 \mathrm{~cm} \times 4 \mathrm{~cm}$. Complete with care and ast. Size: 2
ingtructions.

GENERAL PURPOSE GERM. PNP Coded GPloo. BRAND NEW TO.3 CABE POSS REPLACE. $-00^{25-28-29-30-35-36 . ~ N K T ~}$
404-405-406-430-451-452-453. T13027-3028,
$2 N^{2} 250 A-$ 2N456A-457A-458A, 2N511 A \& B. 2G220-222, ETC YCBO 80 V VCEO 50 V IC 10 A PT. 30 WATTS H $30-170$.
PRICE

43p each $\quad 40 \mathrm{p}$ each $\quad 100 \mathrm{up}$

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 HFE trpe $20 / 1 \mathrm{~T}$ 5MHZ.OUR PRICE EACH
$\frac{50 \mathrm{p}}{\mathrm{AD} / 61 / 162}$
100 up
40 p

## 115 WATT SIL

 POWER NPN50p EACli

SILICON 50 WATTS WATCEED NPN/PNP BIP 19 NPN TO-3 Plastic. BIP 20 PNP. Brand new OUB PRICE PE 50/IC 10A. HFE type 100/ft 3 mHZ $1-24$ prs. 60p $\quad 100$ prs. 60p

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Manufacturers Fall Onts which include Functional and Part-Functional Units These are classed as 'out-of-spec' from the maker's very rigid siecifications, but PakNo. Contentı Price Pak Ko. Contents Price $\mathrm{UICOO}=12 \times 7400 \quad 0.50$ $\mathrm{UIC01}=12 \times 7401$
$\mathrm{UIC02}=12 \times 7402$
U .50
$\mathrm{UIC}=12$ $\begin{array}{ll}\mathrm{UIC} 02=12 \times 7402 & 0.60 \\ \mathrm{UIC} 03 & =12 \times 7403 \\ 0.60\end{array}$ each.

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| :--- | :--- | :--- |
| Price each | 45 D | 40 p |

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2N3820
> 2N3820
> 2N3821
> 2N3823
> $\begin{array}{ll}350 & 2 N 5458 \\ 500 & 2 N 5459\end{array}$
> 80p MPF105
$\begin{array}{ll}\mathrm{UICO4}=12 \times 7404 & 0.50 \\ \mathrm{UIC} 05=12 \times 7405 & 0.50\end{array}$ $\begin{array}{ll}\mathrm{UIC} 06=8 \times 7406 & 0.50 \\ 0.50\end{array}$ $\begin{array}{ll}U 1 C 00 & =8 \times 7406 \\ \text { UIC1 } & 0.50 \\ =12 \times 7410 & 0.50 \\ U & 0.50\end{array}$

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UIC43 $\begin{array}{ll}\mathrm{HC} \\ \mathrm{HC}\end{array}=5 \times 74=743$ $\begin{array}{ll}\text { TIC44 }=5 \times 7444 & 0.50 \\ \text { UIC45 }=5 \times 750 \\ 0.50\end{array}$

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SN7401 SN7402<br>SN74 SN SN03<br>SN7404 SN7403 SN7 SN 7407<br>SN 7407 SN 7406 SN 7409<br>SN7709 SN7410 SN74<br>SN7412 SN7413<br>SN7416 SN7417<br>SN7417 SN7420 SN7422 SN 7423<br>SN7423 SN 2429 SN<br>SN7428 SN $N 440$ SN<br>$\mathrm{SN} N 432$ SN 743 l SN 7437<br>SN7437 SN $N$ N43<br>SN740 SNT441 SN74<br>SN744 SN7444 SN744<br>SN744S SN7446 SN747<br>SN 7448 SN 7450<br>SN74S4 SN7460<br>SN7470 SN7472<br>SN7472 SN7473 SN74<br>SN7474 SN7475 SN74<br>SN 7476 SN 7480 SN 7491<br><br>SN744 SN748S SN748is

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| 8P2014-51.2018 | 48 | 23-9 | 45p |  | ${ }_{\text {RP93 }}$ | 13 p | 12 p | 110 |
| 8P7016-S1.7018 | 48 | 50 | 45p | HP919 | $13 p$ | 12 p | $11 p$ |
| 8P7026-S1.7026 | 4 p | 50 p | 45p | 8P9\% | 14 p | 12 p | $11 p$ |
| BP702-72702 | 53p | $4{ }^{40}$ | ${ }^{40} \mathrm{p}$ | BP944 | 1.9 | 12p | 110 |
| BP709-727.39 | \%p | 3 P | *p | ${ }_{\text {H Proy }}$ | $25 p$ | 24 p | $22^{p}$ |
|  | 34 p | ${ }_{4}{ }_{4}$ | 40 | KP946 | 120 | 110 | 10p |
| BPFIO- ${ }^{\text {BPA }}$ | 450 | 4.4p | 400 | 4P948 | 250 | 24. | 220 |
| BP741-52741 | 750 | $0^{\circ}$ | sop | AP991 | 65 p | 0 p | 53 p |
| 世47036-世A703 | 28 p | $26 p$ | $24 p$ |  | 11p | $1{ }^{19}$ | ${ }^{10 p}$ |
| TAA263- | 700 | 60p | 55 p | APso9? | 40 p | \% | 35 p |
| TAAP93- | คp | 75p | 70p | ${ }_{4}^{41 p 9094}$ | *p | 40 | ${ }^{35}$ |
| TAABSO ${ }^{\text {S }}$ (1000 | 170p | 159\% | 1.50 p |  | 40 | 3 p | 3 spp $1.5 p$ |
| S.Cis FA 10002 |  |  |  | Deviser may quanlity price un applasation | $\begin{aligned} & \text { te mixed } \\ & \text { larger }{ }^{\text {a }} \\ & \text { (DTi } 930 \end{aligned}$ | qualif antily Serie, | y for price unly) |



## BI-PAK DO IT AGAIN! 50W pk 25w (RMS)

$0.1 \%$ DISTORTION! HI-FI AUDIO AMPLIFIER

## THE AL50

* Frequency Response 15 Hz 100,000-1dB.
$\Rightarrow$ $\qquad$
15
* Distortion-better than $1 \%$ at 1 KHz .
$\star$ Signal to noise ratio 80 dB .


## ONLY

23.250 each

* Supply voltage $10-35$ Volts.
$\star$ Overall size $63 \mathrm{~mm} \times$ $105 \mathrm{~mm} \times 13 \mathrm{~mm}$.

Tatlor made to the moat atringent specifications using top qually components and incorporating the latest solid atate circuitry and ALBO, was concelved to fill the need for all your A.F. amplification needs.
FULLY BUILT - TESTED - GUARANTEED.


## STABILISED POWER MODULE SPM80

AP80 is especially designed to power 2 of the AL50 Anplifers, up to 15 watt (r.m.s.) per channel simultaneously. This module embories the latent componenta sircuit protection. With the addition of the Mains Transformer MT80, the unit will provide outputs of up to 1.5 ampe at 35 volts. Size: $63 \mathrm{~mm} \times 105 \mathrm{~mm} \times 30 \mathrm{~mm}$. These unlts enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:-Disco Systems, Public Adiress, ntercom Units, etc. Handbook avallable, 10p PRICE £2.95

TRANSFORMER BMT80 £1.95 p. \& p. 25p.

## STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet atill the greatest value on the market, the PA100 stereo pre-amplifier has been concejved from the latest circuit teconlques. Designed for use with the Al50 power ampliffer syatem, thls quality made unit incorporatea No less than eight silicon planar transisto
Three switched stereo inputs, and rumble and scratcb filters are featurea of the PAl00. which also has a STEREO/MONO awitch, volume, balance and continuously varlable bass and treble controls.
gPECIPICATION Frequency Response
Inputs : 1. Tape Head $\quad 1.25 \mathrm{mV}$ into $50 \mathrm{~K} \Omega$
2. Radio, Tuner
1.25 mV into $50 \mathrm{~K} \Omega$
1.5 mV into $50 \mathrm{~K} \Omega$

All Input voltagea are for an output of 250 mV . Tape and P.U. inputs equalised to RIAA curve within $\pm 1 \mathrm{~dB}$. from 20 Hz to 20 KHz . Base Control
$\pm 15 \mathrm{~dB}$ at 20 Hz
$\pm 100 \mathrm{~Hz}$
8 KHz
better than - 65 dB
$+28 \mathrm{~dB}$
+35 volts at 20 mA
ONLY E11.95
SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT 80 \& 1 PA100 ONLY £23-00 FREE p. \& p.


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| NKT713 | 27p | BC107 | 8 | NKT128 | 18 p | NKT261 | ${ }^{19} \mathrm{p}$ |
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This unit generates stepping pulses ( 50 V d C .) at intervals of 6 puises per min to 120 pulaes per min -continuously variable Can be used for Automatic
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PC1 150 mW Audio Amplifier
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Resistors, 50p. 10 mF 64 V Electrolytic Caps, 5 for 25 p ; 12 for 50 p. 640 mF 16 V Electrolytic Caps 3 for 50 p ; 7 Mr 60 p . 10 mF 63 V WIMA non-electrolytic, 15 p each. $(3200$ grf $10 \mathrm{~V}, 15 \mathrm{p} ;)$ for $38 \mathrm{p} ; 5$ for 60 p . SEMICOTNDETORS
Any 6 of the following, 50 p , or 10 en each. OC7I, BFY50, 2 N 3702 , CV8615, BSY95A, NTG885, 2N930, OA8I, $2 \times 1$ N914. (OR P60 50p)

## CONSTRUCTORS' ITEMS

Subminiature Omron I2V d.c. relays mounted on CCF board, 3 for $60 p$, P\&P 9p; mounted on CCT board with components, 2 fo-60p, Pap-7 GPO Relays, various 200s $2-7000 \Omega$, 30p each. Uni electors, 10 pole, 25 way, El each, P\&P 25p. Heavy Duty Foot Ped Is, 50p, P\&P 20p. 6 V 5 digit High Speed Counters, E1,50, 15p P\&P.

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£2.50 each-ideal for spares, motor, power pack, record/replay, electronics with mike $\mathbf{〔 3 . 2 5}$,

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Mains-13V 2.5A and $15 \mathrm{~V} 0.75 \mathrm{~A} \in 1.45,20 \mathrm{p}$ P\&P. Mains-I 13 V IA 12 $0.5 \mathrm{~A}, \mathrm{£1.25}, 20 \mathrm{P} P \& P$. Mains-13V 5 A and 24V 2A, £2, 25p. P\& Mains-24V 100 mA and $6 \mathrm{~V} 100 \mathrm{~mA}, 75 \mathrm{p}, 10 \mathrm{p}$ P\&P.
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$0.33,7 p ; 0.47,8 p ; 0.68,10 \mathrm{p} ; 1.0,13 \mathrm{p} ; 1.5,20 \mathrm{p} \cdot 2.2,23 \mathrm{p}$. 160V: ( $\mu \mathrm{F}) 0.01,0.015,0.022,2 \mathrm{2p} ; 0.047,0.068,3 \mathrm{p} ; 0.15,0.22,4 \mathrm{p} ; 0.33,5 \mathrm{p}$;
$0.47,6 p ; 0.68,1.0,10 p$.
$400 \mathrm{~V}:(\mu \mathrm{F}) 0.001,0.0015,0.0022,0.0033,0.01,2 p ; 0.015,0.033,3 p ; 0.068,4 \mathrm{p}$. MINIATURE ELECTROLYTIC MULLARD C426 SERIES (5p each) ( $\mu$ F/V) $0.64 / 64,1.6 / 25,4 / 4$ ), $8 / 40,10 / 40,10 / 64,16 / 40,20 / 64,25 / 25,32 / 10$, 40/16, 64/10, 80/16, 80/25, 100/6.4, 125/16, 200/6.4, 200/10, 320/6.4, 125/10. MULLARD C437: ( $\mu \mathrm{F} / \mathrm{V}$ ) 64/64, 9 p ; 160/25, 9p; 160/40, 11 p ; 640/6.4, 9p $1600 / 6 \cdot 4$, 14p.

ELECTROLYTIC CAPACITORS. Tubular and large can ( $\mu$ F/V) 2.5/50, 3p; $4 / 10,10 / 25,16 / 15,20 / 25,25 / 15,25 / 25,40 / 6,64 / 10,200 / 6$,
$250 / 10,4 \mathrm{p} ; 10 / 6,10 / 50,25 / 50,32 / 50,50 / 10,64 / 25,100 / 25,50,50 / 50,64 / 40$ $\begin{array}{ll}250 / 10,4 p ; 10 / 6,10 / 50,25 / 50,32 / 50,50 / 10,64 / 25,100 / 25,5 p ; & 50 / 50,64 / 40, \\ 250 / 15,1,000 / 3,6 p ; 100 / 50,250 / 25,400 / 10,500 / 10,500 / 12,640 / 10,1.000 / 6,\end{array}$
 1,000/50, 35p; 2,000/25, 25p; 2,500/25, 30p; 2500/50, 55p; 3,000/50, 65p;
5,000/50, 85p. 5,000/50, 85p.
CERAMIC PLATE CAPACITORS

750V: (pF) 5, 10, 25, 40, 70, 220, 2tp; ( $\mu$ F/V) $0.0047 / 30,0.01 / 350,2 p$ $0.047 / 30,3 \mathrm{p} ; 0.1 / 30,4 \mathrm{p} ; 0.1 / 100,5 \mathrm{p} ; 22 \mathrm{pF}-1000 \mathrm{pF} 50 \mathrm{~V}$, EI2 Series; 1500 pF $0.022 \mu \mathrm{~F} 50 \mathrm{~V}$, E6 Stries 2 p each.
CARBON FILM RESISTORS $\ddagger W 5 \%, 10$ ohms- $2 \cdot 2 M, 1 p$ each, or 100 for
55p.
S5P. SPECIAL RESISTOR KITS ( 1 W $5 \%$ CARBON FILM) 10 E 12 Kit: 10 of each El 2 value, 10 ohms- 1 M , a total of $610,62-80 \mathrm{net}$ $\overline{\text { VEROBOARD }} \begin{array}{lllll}0.1 & 0.15 & \text { IN400I } & \text { op }\end{array}$


# NIFTD FROM ADCOLA THE BEST IN SOLDERING KITS Styrene packed with see-through top 



## Contents

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# Sinclair Project60 

# Active Filter Unit <br> (A.F.U.) 

Built and tested post free $£ 5.98$

The value of an efficient filtering system cannot be over emphasized in these days of very high quality reproduction since there are so often occasions where its use can mean the difference between comfortable and uncomfortable listening. On the low pass side the Sinclair A.F.U. will effectively reduce hiss from radio or tape, cut out heterodyne whistles on A.M. reception, greatly reduce record surface noise and other imperfections; on the high-pass side it will cut out motor rumble and other spurious low frequency intrusion. The unit is for use between pre-amp (including tape pre-amps) and power amplifiers, and operates in two sections, both stereo. The cut-off frequencies are continuously variable, and since attenuation in the rejection band is rapid ( 12 dB /octave) there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is as easy to mount as the stereo 60 pre-amp/control unit which it matches in styling, along with the Stereo FM Tuner.

## SPECIFICATIONS

The A.F U employs two Sallen and Key type active filter stages. one rumble (high pass) and one scratch (low pass). The two stages use complementary iransistors io minimise distortion.
Supply voltage: 15 to 35 volts Current 3mA maximum.
Gain at $1 \mathbf{k H z}$ : Filters flat 098 ( -0.2 dB )
HF cut off: ( -3 dB ) variable from 28 kHz to 5 kHz at 12 dB /octave.
LF cut off: ( -3 dB ) variable from 25 Hz to 100 Hz at 12 dB /octave.
Distortion: at 1 kHz ( 35 volt supply) $0.02 \%$ at rated output.

## Super IC. 12 mesertece circum <br> high fidelity amplifier

sistor circuit contained within a 16 lead DIL package. and the finned heat sink is sufficient for all requirements. The Super IC. 12 is compatible with Project 60 modules which would be used with the $\mathrm{Z}$..50 and $\mathrm{Z}$.30 amplifiers. Complete with free manual and printed circuit board.

## SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). 6-8 . Frequency Response: 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total Harmonic Distortion: Less than $1 \%$. (Typical $0.1 \%$ ) at all output powers and frequencies in the audio band $(28 \mathrm{~V})$ Loed Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90 dB ( 1.000 .000 .000 times) after feedback Supply Voltage: 6 to 28 V . puiescent cur-, rent: 8 mA at 28 V . Size: $22 \times 45 \times 28 \mathrm{~mm}$ in cluding pins and heat sink
Manual available separately 15 p postfree.

Having introduced Integrated Circuits to hi-fi constructors with the IC. 10 . the first time an IC had ever been made avallable for such purposes. we have followed it with an even more efficient version. the Super IC. 12 . a most exciting advance over our qrigjnal ynit. This needs verv few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up. F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC make possible: It is the equivalent of a 22 tran-


## Project 605

The easy way
to buyand
build


Project 60
Project 605 is one pack containing: one PZ5. two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. T患us all soldering an hunting for the odd part is eliminated. You will be able to add further Project 60 nodules as they become a wailable pdapted to the Project 605 method of connecting Complete Project 605 pack with
£29.95 comprehensive manual, post free
le a superb 30 Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.

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# the world's most advanced high fidelity modules 

## Z.30 \& Z.50 power amplifiers

The $Z .30$ and $Z .50$ are of advanced design using silicon epitaxial planar transistors to provide unsur passed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at 15 w ( $8 \Omega$ ) and all lower outputs. Whether you use $Z .30$ or $Z .50$ amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such. however, that $Z .50$ s and $Z .30$ may be used in a far wider range of applications.
SPECIFICATIONS ( 2.50 units are interchangeable with 2.30 s in all applications).- Power Outputs Z. 3015 watts R.M.S. into 80 hms using 35 volts: 20 watts R.M.S. Into 3 ohms using 30 volts
$\mathbf{Z . 5 0} 40$ watts R.M.S. into 3 ohms using 40 volts 30 watts R.M.S. into 8 ohms using 50 volts
Frequency response: 30 to $300,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$. Distortion: $0.02 \%$ into 8 ohms. Signal to noise ratio: better Frequal oh ns impedance. Fize: $14 \times 80 \times 57 \mathrm{~mm}$.


## Stereo 60 Pre-amp/control unit

Built testedand guaranteed.
Designed specifically for use on Project 60 systems. the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxıal planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount.
SPECIFICATIONS-Input sensitivities: Radio - up to 3 mV . Mag. pu. 3 mV correct to R.I.A.A. curve $\pm 1 \mathrm{~dB} 20$ to 25.000 Hz . Ceramic p.u. - up to 3 mV : Aux - up to 3 mV . Output: 250 mV . Signal to nolse ratio better than 70 dB Channel matching: withın 1 dB . Tone controls: TREBLE +12 to -12 dB at 10 KHz : BASS better 12 dB a 10 H z Front panel: brushed alumınıum with black knobs and controls. Size: $66 \times 40 \times 207 \mathrm{~mm}$


## Project 60 Stereo F.M. Tuner

The phase lock loop princıple was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now. Sinclair have applied the principle to an F.M. tuner with fan tastically good results. Other advanced features include varicap dıode tuning. printed circuit colls, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.
 SPECIFICATIONS-Number of transistors: 16 plus 20 ml .C. Tuning range : 87.5 to 108 MHz . Sensitivity: $7 \mu V$ for lock-in over full deviation. Squelch level: Typically $20 \mu V$. Signal to noise ratio: $>65 \mathrm{~dB}$. Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}$ ( $\pm 1 \mathrm{~dB}$ ). Total harmonic distortion: $015 \%$ for $30 \%$ modulation. Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M S. maximum Operating voltage: $25-30 \mathrm{VDC}$. Indicators: Stereo on: tuning. Size: $93 \times 40 \times 207 \mathrm{~mm}$

## Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ. 5 for normal Z.30 assemblies and PZ. 6 or $P Z .8$ where a stabilised supply is essential.

PZ. 530 volts unstabilised $£ 4.98$ PZ. 635 volts stabilised $\mathbf{£ 7 . 9 8}$ PZ. 845 volts stablised (less manstransformer) $\begin{array}{ll}\text { (less mains transformer) } & £ 7.98 \\ \text { PZ.8 mainstransformer } & \mathbf{£ 5 . 9 8}\end{array}$

Typical Project 60 applications

| System | The Units to use | together with | Units cost |
| :---: | :---: | :---: | :---: |
| Simple battery record player | 2.30 | Crystal P.U., 12 V battery volume control, etc. | £4.48 |
| Mains powered record player | Z.30, PZ.5 | Crystal or ceramic P.U. volume control, etc. | £9.45 |
| 12W. RMS contınuous sine wave stereo amp. for average needs | ```2x Z.30s, Stereo 60;PZ.5``` | Crystal. ceramic or mag. P.U., F.M. Tuner, etc. | £23.90 |
| 25 W . RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times Z .30 \text { s, Stereo } \\ & 60 ; \text { PZ. } 6 \end{aligned}$ | High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck. etc. | £26.90 |
| 80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms) | $2 \times 2.50$ s, Stereo 60: PZ.8, mains transformer | As above | £34.88 |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic.. guitar. speakers, etc.. controls | £19.43 |
| F.M. Stereo Tuner (£25) \& A.F.U. (£5.98) may be added as required. |  |  |  |
|  |  |  |  |



## Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd. you are dissatisfied with it. your money will be refunded at once. Many Sinclair appornted Stockists also offer this same guarantee tn co-operation with Sinclair Radionics Ltd.
Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Shouid any defect arise n normal use we will service it at once and without any harge 10 you if it is returned within wo vears from the date harge to you. of purchase. Outside this period of guarantee a small charge (typically $£ 1.00$ ) will be made. No charge is made for postage by surface mail. Air Mall is charged at cost

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$0 \cdot 2 \mu \mathrm{~F}, 5 \mathrm{p} .0 .33 \mu \mathrm{~F}$ ELECTROLYTIC CAPACITORS-MULLARD C426 SERIES
 $6.4 / 6 \cdot 4,2 \overline{0} / 64,50 / 54,100 / 5 \cdot 4,200 / 4 \cdot 4.3 \div 0 / 54,4 / 10,16 / 10,3: / 10,14 / 10,125 / 10,200 / 10$,


MULLARD C437 SERIES
 $640 / 10,1,20 / 4,1,000 / 64.4,600 /-3,12 p .140 / 44,250 / 40,400 / 2-\overline{3}, 540 / 14,2,000 / 4,1,000 / 10$, $1,600 / 64,2,500 / 2 \pi .15 \mathrm{p} .950 / 64,400 / 40,640 / 23,3,200 / 4,1.000 / 16,1,600 / 10,2,500 / 64$

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Despite miniaturisation and close packing, the extent of the circuitry involved in a sophisticated design may add up to a large and unwieldly piece of equipment. In such cases-and the present signs are that they will become more and more commonplace - the answer probably lies in unit or modular construction. This is a well-established practice in large commercial equipments. Now it is beginning to merit serious consideration in the home constructor field, for particular designs.

The modular form of construction can be seen as a further development of the plug-in circuit board arrangement, with carefully selected and clearly definable parts of the overall system assembled within mechanically independent units. The modular system offers a number of advantages. In some instances individual modules belonging to a system may be capable of serving other functions, either while remaining within the parent rack or cabinet, or as free-standing and independent units pressed into service at short notice for some ad hoc experiment or demonstration, for example.

The additional cost in hardware is therefore likely to be fully recompensed by the greater versatility provided by the constituents that go to make up the whole system. The maximum possible utilisation of valuable equipment can be assured. Operational flexibility is, of course, another important attribute of modular construction, as well as greater facility for the subsequent updating or improvement of particular sections of the system in the light of technical progress.

The P.E. Sound Synthesiser demonstrates some of the most valuable and desirable features of the modular approach. This project is certainly ambitious, in amateur terms; yet such is the current interest in the synthesis and manipulation of sound for all manner of divergent uses, that the popularity of this instrument is not in doubt. And it has this additional attraction: many of the modules have other possible applications, alone or in association with other equipment, outside the confines of the main system. The Sound Synthesiser series of articles can be considered in the whole-relating to one large and comprehensive design with great capabilities. Alternatively, the series may be viewed as a collection of separate designs, many of these having interesting possibilities as solo units in the wide and appealing field of creative and experimental sound.-F.E.B.

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## The latest in circuit integration.....



## 

## By F. R. HEATH b.Sc. (Hons.) (Ferantit Lta.)

NEW CDI integrated circuit technology has enabled Ferranti engineers to produce the smallest radio i.c. device in the world that offers a satisfactory alternative to the superhet. This article will take a brief look at the CDI techniques used to produce this device and then describe in full how you can build a high quality medium and/or long wave portàble radio of superior quality for modest cost.

For the constructor there is, at least, a rest from some of the tedious coil-winding operations so often necessary in radio construction. There is no recourse to expensive alignment equipment, as no setting up is required.

This article does not aim to stress an overall small size, such as in a matchbox radio, because the majority of constructors will want a radio with a speaker and cabinet, ferrite'aerial, and room for a long lasting battery. To make full use of the superior sound quality available from the radio i.c. these items are essential. Anybody wishing to make a "micro-radio" or a medium and long wave tuner for an existing hi-fi system, will be able to adapt from the design in this article.

The "P.E. Triffid" design has been tried in most parts of the British Isles, from Exeter to Edinburgh, and gives good results on stations which are of normally reasonable signal strength for the area. The only problem (occurring with all t.r.f. designs) is when the receiver is being used very close to the transmitter. In such a case rotation of the rod aerial is necessary to find a null. Although desgined for reception of BBC Radio 1, 2, 3 and 4, the set works well on many foreign stations, especially Radio Luxemburg.

## COLLECTOR DIFFUSION ISOLATION (CDI)

CDI is a new bipolar integrated circuit manufacturing technique which possesses the following inherent advantages:

1. Simplicity of processing
2. High component density
3. High switching speed
4. Low supply volts.


Fig. 1. Cross section view through a CDI transistor

CDI in its basic form, as developed by Bell Laboratories, was limited to a 3 V supply voltage. Ferranti carried out a major development programme to achieve a 5 V process for compatability with current logic i.c. systems.

The processes involved in the production of CDI devices are much simpler than for standard bipolar techniques. Only five masks are required which compare directly with MOS processing; four less than for conventional bipolar i.c. processes. The transistor size is much smaller due to the self isolating properties of CDI, and much thinner ( 1 micron) epitaxial layers can be used in processing.

This simplicity is of direct importance in achieving low cost and yielding large quantities, both factors being passed on to the consumer as cheaper i.c.s.

A cross-section of a CDI transistor is shown in Fig. 1. Buried $n$ regions are diffused into a $p$-type substrate wherever transistors, diodes or resistors are required. A thin, high resistivity $p$-type epitaxial layer is then grown over the slice.

Table 1: BASIC CDI TRANSISTOR CHARACTERISTICS

| $V_{\text {cbo }}$ | 7.5 volts |
| :---: | :---: |
| $\mathrm{h}_{\text {fe }}$ |  |
| $\mathrm{f}_{\mathrm{T}}$ | 1 GHz |
| $\mathrm{R}_{\text {sat }}$ | 10 ohms |
| Voftset | 5 mV . |
| lcbo | 1.0 pA |
| $\mathrm{h}_{\text {fe }}$ (inverse) | 20 |
| $\mathrm{C}_{\text {b }}$ | 0.3 pF |

A block diagram of the radio chip is shown in Fig. 2. Basically, the circuit is a 10 transistor t.r.f. tuner which will operate from 150 kHz to 3 MHz and requires about 1.3 volts power supply. Audio output is typically 30 mV r.m.s.

The i.c. requires the minimum of external circuitry and effective a.g.c. action is available. Distortion from the chip is very low (typically $2 \%$ ), which is three or four times better than in an average superhet. Current requirements for the i.c. are approximately 0.5 mA and the characteristics are shown in Fig. 3 and 4 and in Table 2.

Fig. 2. Block diagram of the interior circuitry of the ZN414 with associated tuned circuit and a.g.c. components


Isolation, deep collector contact, interconnection crossunders, and definition of base and resistor areas are all achieved by a single selective $n_{+}$diffusion through this epitaxial layer. The isolating $n_{+}$diffusion completely surrounds each buried layer island, complete isolation being provided by the $p$-type epitaxial layer and the substrate between the $n_{+}$ diffused regions. The $p$-type epitaxial layer which is completely enclosed is used to form transistor bases and $p$-type resistors (medium value resistors 2 k S 2 to $50 \mathrm{k}(2)$.
Another $n_{+}$diffusion defines the transistor emitters, and can also be used for low value resistors. Contact holes are then cut and the basic aluminium interconnection pattern is evaporated onto the device.
The parameters of CDI devices are shown in Table 1.

## RADIO CHIP DESIGN

The design of the ZN414 radio chip began in November 1970. A basic circuit was produced and then "breadboarded" using discrete CDI devices. As in many basic t.r.f. designs, instability was the major problem. Intensive development work culminated in a design that is stable provided certain external requirements are satisfied.

Many prototype experimental circuits were tried and found to be capable of excellent quality. The first i.c. radio was working in July 1971. The present day radio chips are predictable and consistent.


Table 2:
MAIN CHARACTERISTICS OF THE ZN414

Supply volts
Temperature range
Supply current
Frequency range
R.F. input impedance

Output impedance
Sensitivity
Power gain
$1.1-1.5$ volts 0 to $+70^{\circ} \mathrm{C}$ 0.5 mA maximum $200 \mathrm{kHz}-3 \mathrm{MHz}$ $1.5 \mathrm{M} \Omega$ typical $500 \Omega$ typical $100 \mu \mathrm{~V}$ r.m.s. 70 dB typical


Fig. 3. Graph of voltage gain showing the effective a.g.c. region


Fig. 5. The integrated circuit is driven from a constant voltage source of 1.3 volts derived from a 9 volt supply

## HIGH QUALITY RADIO SET

To obtain the best possible results from the ZN414, certain rules must be adhered to. All leads in the radio circuitry must be .kept short, and the i.c. should preferably be soldered flush to a printed circuit board. The aerial coil should have a high $Q$ or selectivity will suffer.

The only problem occurs when a very strong station swamps the front end. Here, rotating the set until a null is found will solve the problem. A demonstration radio gave better reception of Radio Luxemburg than a superhet, not because selectivity was better, but because the superhet gave out so many whistles and shrieks that any pleasure from the programme was impossible to achieve.

One other important requirement is to keep the a.g.c. resistor within the range 470 to $1,000 \mathrm{ohms}$,

A typical case used to house the P.E. Triffid receiver

and for best selectivity keep to the lower end. This means that if the radio is powered from a 9 V battery, then a constant voltage source is needed to derive the 1.3 volts necessary. This is done using the circuit shown in Fig. 5.

Fig. 4. shows that the gain of the chip falls off at long wave frequencies. For this reason, a switch is fitted to increase the supply volts (and consequently increase the gain of the chip) on long wave so that the volume is kept approximately the same when the different bands are selected. Fig. 5 shows the circuit changes needed to accomplish this.

## AMPLIFIER AND CASE

The output amplifier and loudspeaker should be of good quality to do justice to the signal from the receiver. Several i.c. amplifiers were tried. All gave some results, but most were tricky to stabilise and did not give the quality needed. For this reason a discrete amplifier was used, low power output at 500 mA being suitable for a personal radio. Low cost and battery power consumption are kept to a minimum making this receiver suitable for the inexperienced radio constructor.

Cabinet and speaker design is dependent on personal taste so the following constructional details deal mainly with the circuitry aspect. Most constructors will want to design their own housing for the unit, and there are many cases available to cater for those who do not like woodwork.

The case must not contain large metal parts near to the ferrite rod, as this will damp the $Q$ of the coil.

## AMPLIFIER DESCRIPTION

The amplifier is not claimed to be a revolutionary design: rather it is intended to be easily built, and of good enough performance to match the radio i.c., whilst maintaining battery current economy and using inexpensive transistors.

The circuit in Fig. 6 shows a class-AB amplifier with a constant current source (TR4) enabling a

NOTE: The earthy side of VC1 (moving section) musi be connected to C1/R16


Fig. 6. The complete circuit diagram of P.E. Triffid receiver
higher voltage gain from the drive stage TR2. The current in TR4, and consequently the quiescent current taken by the circuit, is around 5 mA . This $p n p$ current source was found to reduce distortion in the circuit. The voltage gain at 1 kHz is approximately 80, thus the input sensitivity for full output ( 5.7 volts before clipping) is 70 mV .

The value of R13 may be lowered to give less bias voltage at the expense of distortion. Replacing it with a wire link is recommended if other output transistors are used, or any modifications are tried, as this prevents the possibility of thermal runaway

If a reduced ouput power is acceptable, ZTX300 and ZTX500 may be used as the output pair, or BFS60 and BFS96; both sets give good results. Distortion with the standard circuit is one per cent at 1 kHz and 2 volts peak output, mainly second harmonic. No crossover distortion can be seen on an oscilloscope trace at 20 kHz , indicating that distortion is due mainly to non-linearity in the whole amplifier rather than to crossover "spikes"

No heatsinks are necessary with the recommended output pair. Three layouts of the circuit were tried, all were stable and gave similar results.

The amplifier is certainly of good enough performance to use as an amplifier for an f.m. tuner, or record player, and experimenters can easily modify the circuit to switch in to another function or functions.

## CONSTRUCTION AND LAYOUT

Provided the layout is carried out as described earlier, almost any method of construction can be used. However, a printed circuit board is recommended as it offers reliably consistent results.
The combined amplifier and radio circuit is shown in Fig. 6, the p.c.b. pattern and layout in Fig. 7. Apart from essentially sound soldered joints, two further precautions must be observed: wires from the coil-capacitor tuned circuit must be kept away
from other circuitry, especially the battery leads and loudspeaker leads; the volume control must be $10 \mathrm{k} \Omega$ or greater, if it is not to affect the a.g.c. characteristics.


Layout of components on a printed circuit board

Resistors

| R1 | $56 \mathrm{k} \Omega$ | R8 | $1 \mathrm{k} \Omega$ | R15 | $1 \Omega 1 W$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| *R2 | $56 \mathrm{k} \Omega$ | R9 | $3.3 \mathrm{k} \Omega$ | R16 | $100 \mathrm{k} \Omega$ |
| *R3 | $680 \Omega$ | R10 | 10k $\Omega 2 \%$ | R17 | $10 \mathrm{k} \Omega$ |
| *R4 | $1 \mathrm{k} \Omega$ | R11 | 1k $\Omega 2 \%$ | R18 | $22 \mathrm{k} \Omega$ |
| R5 | $100 \mathrm{k} \Omega$ | R12 | $27 \Omega$ | R19 | $220 \mathrm{k} \Omega$ |
| R6 | $220 \mathrm{k} \Omega$ | R13 | $100 \Omega$ |  |  |
| R7 | $10 \mathrm{k} \Omega$ | R14 | $1 \Omega 1 \mathrm{~W}$ |  |  |

## Potentiometer

VR1 $10 \mathrm{k} \Omega$ volume control with switch (S3)

## Capacitors

C1 $0.01 \mu \mathrm{~F}$
C2 $0.22 \mu \mathrm{~F}$
C3 $4 \mu \mathrm{~F}$ elect 10 V
C4 $25 \mu$ F elect 10 V
C5 $500 \mu \mathrm{~F}$ elect 10 V
C6 47pF disc ceramic
C7 $0.01 \mu \mathrm{~F}$ polyester
C8 $250 \mu \mathrm{~F}$ elect 10 V
C9 $0.1 \mu \mathrm{~F}$ polyester
VC1 200 pF single gang tuning

Integrated Circuit
IC1 ZN414 (Ferranti)
Transistors

| TR1, 2, 3 | ZTX109 (3 off) |
| :--- | :--- |
| TR4 | ZTX504 |
| TR5 | ZN1132 |
| TR6 | ZT1711 |

## Diodes

$$
\begin{array}{ll}
\text { D1 } & \text { KS047A } \\
\text { D2 } & \text { ZS142 }
\end{array}
$$

## Tuning Coil

L1 85 turns +250 turns 28 s.w.g. enamel wire wound on $\frac{3}{8}$ in dia. 6 in ferrite rod (see text)

## Miscellaneous

LS1 $8 \Omega$ loudspeaker
B1 9V battery style PP9
Printed circuit board (see Fig. 7)
Case and tuning scale


Fig. 7. Component layout and printed circuit board pattern (full size)


Fig. 8. Coul winding details and waveband selection



Fig. 9. A tone control circuit is inserted in the position of R4 as shown here with another capacitor

## TUNING COIL

If the tuning range is tending towards the low frequencies, then fewer turns are needed on the coil. For a 6 in ferrite rod with the coil feeding a 200 pF tuning capacitor, about 85 turns of close wound enamelled copper or litz wire are needed; 28s.w.g. wire is suitable, but nothing is critical here, and adjustments are easy. It is better to wind more turns (say 100) and then remove some until the correct tuned frequency spread is reached. Litz wire gives highest $Q$ coils and is highly recommended.

Constructors who wish to wind a long wave coil and fit a wave-change switch will find that, with the values above, the coil will need about 250 turns. Multilayering is best, but again this is not critical. Fig. 8 shows the long wave components necessary.

The type of ferrite rod affects the inductance, as does the type of wire, but it is easy to adjust the coil to suit the requirements of the rod obtained. Do not expect to adhere rigidly to the specified coil details for optimum results.

## TESTING

Building the circuit should present no problems if carried out in the following manner:

1. Build up the amplifier unit and volume control, and test it on suitable inputs. If no signal generator is available, see if a hum is produced when the input is touched. The output (before $C 5$ ) should be at 4.5 volts $\pm 0.5$ volts.
2. Wire up the radio drive circuit and put a $3.3 \mathrm{k} \Omega \Omega$ resistor between emitter of TRI and earth. This should have 1.3 volts $\pm 0.2 \mathrm{~V}$ across it.
3. Wire up the radio i.c. and test.

Interior of receiver showing the printed circuit board mounted on a plain board which also has the tuning capacitor, volume control and aerial mounted on it


If instability is encountered, the following procedure is used.
(a). Short the tuning capacitor out, if instability continues then the radio supply voltage may be incorrect.
(b). Radio frequencies generated in the amplifier may be feeding back to the i.c. To cure this a 47 pF capacitor may be fitted across the $220 \mathrm{k} \Omega$ resistor, and /or a $30 \mu \mathrm{H}$ choke placed in the supply before R9. (The link on the board is replaced by the choke.)
(c). Leads to the tuning circuit may need re-routing.
(d). If instability continues then replacing R 2 by a 47 k ! resistor, and replacing the link above R 2 with a $20 \mathrm{k} \Omega 2$ preset, will facilitate greater control of radio supply voltage. This has an additional advantage; as the battery ages and its voltage drops, the set will still give good results (down to 6 volts with this preset in circuit.)
Happily, none of these problems occurs if neat systematic working is done, and normally the radio should work first time.

## TUNING INDICATOR

A tuning indicator is very simply added to the set by inserting a $0-1 \mathrm{~mA}$ (or $0-500 \mu \mathrm{~A}$ ) meter between TR1 emitter and the top end of R3. This should read approximately 0.3 mA with no signal, but should read higher as one tunes through a station. The maximum reading indicates that the station is properly tuned, and depending on the signal strength, should give a reading around 0.5 mA .

In normal circumstances this receiver should not drift and once set, the tuning should not need to be altered.

## TAPE RECORDER OUTPUT

Provided the circuitry of the tape recorder has an input impedance of several tens of kilohms, a screened lead can be taken from the "top" end of the volume control to the tape recorder input socket most suited for a 100 mV flat response input signal. Care that the bias circuitry does not interfere with the radio is needed, so a fairly long lead is recommended.

## TONE CONTROL

Fig. 9. shows a recommended tone control, which in its extreme position gives a $6 \mathrm{~dB} /$ octave roll-off above 1 kHz . To fit the tone circuit, the connection between C3 and R4 has to be cut. Apart from this the board is adaptable for the modification.


# Biological Amplifier 

HIS month we describe the construction of a brain rhythm frequency meter and cardiophone.

## BRAIN RHYTHM FREQUENCY METER

The circuit in Fig. 8 can be employed to identify different brain rhythms, and will demonstrate, for example, how alcohol intake affects alpha frequency.

A signal taken from output 1 of the pre-amplifier is amplified by TR3 and squared by the Schmitt trigger TR4 and TR5. Differentiator C15 and VR4 converts the square wave into an a.c. signal of amplitude proportional to frequency. This is rectified and smoothed by D3, D4, and C16, with the resulting d.c. current being measured by ME2. VR4 calibrates the instrument, and VR3 adjusts sensitivity.
The frequency range covered by ME2 is $0-20 \mathrm{~Hz}$, and capacitor C 8 in the pre-amplifier can be switched into circuit by S3 to give additional top-cut for noise and interference rejection, see Fig. 2.
In addition to the frequency meter, a voltage controlled unijunction oscillator TR7, gives an audio output into 8 ohm headphones of frequency proportional to the subsonic brain rhythm frequency, so that the user can sense changes of rhythm with his eyes closed. TR6 controls the charge rate of the unijunction emitter capacitor C17.
If interest is centred on either beta, theta, delta, or slow alpha rhythms, the centre frequency of the preamplifier can be modified according to the capacitor value listed in Fig. 3. Alternatively, a three-pole four-way wafer switch can be used to select twin-T filter capacitance values.

## CONSTRUCTING AND USING THE FREQUENCY METER

Constructional details of the frequency meter output module are shown in Fig. 9. A suggested layout in a metal box, similar to that used for the alphaphone, will be found in Fig. 10. Cl 6 is mounted on the meter terminals.

Plug headphones into SK4, leave the head electrodes disconnected from SK1 and SK2, and set VR1 and VR2 to minimum resistance, and VR3 and VR4 to maximum resistance. Switch on the



## COMPONENTS . . .

## ADDITIONAL COMPONENTS FOR FREQUENCY METER

Fig. 8. Wiring of the pre-amplifier to the frequency meter circuit to measure brain rhythm rates
Resistors

| R22 | 10 k , | R26 | 2.7 k ( | R30 | $2.7 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R23 | 100 k ¢ | R27 | $1 \mathrm{k} \Omega$ | R31 | $1 \mathrm{k} \Omega$ |
| R24 | 10ks 2 | R28 | $22 \mathrm{k} \Omega$ | R32 | $100 \Omega$ |
| R25 | $1 \mathrm{k} \Omega$ | R29 | 10kS |  |  |
| All $\pm 10 \% \frac{1}{2}$ watt carbon |  |  |  |  |  |

Potentiometers
VR3 $500 \mathrm{k} \Omega$ sub-min horizontal pre-set
VR4 $10 \mathrm{k} \Omega$ sub-min horizontal pre-set
Semiconductors

| TR3 | BC108 | TR6 | OC71 |
| :--- | :--- | :--- | :--- |
| TR4 | BC108. | TR7 | 2N2646 |
| TR5 | BC108 | D3, D4 | IGP5 or OA91 |

## Capacitors

C14 $2 \cdot 2 \mu \mathrm{~F}$ tantaium 35 V
C15 $2 \cdot 2 \mu \mathrm{~F}$ tantalum 35 V
C16 $1,000 \mu \mathrm{~F}$ elect. 3 V
C17 $0.01 \mu \mathrm{~F}$ polyester

## Meter

M2 $100 \mu \mathrm{~A}$ edgewise type level indicator

## Switches

S3 single-pole, on-off sub-miniature
S4 3-pole, 2-way wafer

## Socket

SK4 3-pole jack

## Batteries

B6, B7, B8 9 volt styie PP3 (3 off)

## Miscellaneous

8 ohm mono or stereo headphones, electrodes, battery connectors, metal box.


Fig. 9. Layout and wiring of the frequency meter board


Fig. 10. Suggested layout of components for the brain rhythm frequency meter circuit shown in Fig. 8
instrument and listen for a steady low note in the phones. Advance VR3 until the audio note just starts to rise slightly.

If an accurately calibrated audio oscillator with an output of around 30 millivolts r.m.s. at 10 Hz is available, connect this to the pre-amplifier input via a 10 megohm resistor, with a 10 kilohm resistor shunting SK1 and SK2. Set VRI for a steady deflection of meter ME2, and adjust VR4 for a half full scale reading, corresponding to 10 Hz .

In the absence of an audio oscillator, set up the frequency meter for alpha rhythms (with head electrodes on a subject who can generate steady alpha rhythms) and adjust VR4 for a mean meter reading of 10 Hz . With the eyes open. ME2 should fluctuate between $2-7 \mathrm{~Hz}$, indicating the presence of random brain noise and low level theta.

As an experiment, measure a subject's alpha frequency and then ask them to have a drink (alcoholic). After $15-30$ minutes the alpha frequency should fall by several hertz. A whole range of experiments can be conducted with the frequency meter, such as mental reactions to various stimuli, or the effect of dreams on sleep rhythins.

## ELECTRODE SITING

With previous projects the earthed electrode (SK2) was sited on the forehead so that eyeblink signals
could be used to test equipment in the absence of alpha rhythms, but in some investigations eyeblink pulses can be a nuisance. Alpha, theta, and delta signals are best obtained from the back of the head, with the earthed electrode positioned an inch or two from the live electrode. For beta signals the electrodes can be placed on the forehead or near the cheeks. but watch for noise generated by facial muscles and eyes.

If the earthed electrode is placed on the neck, or other parts of the body, while observing brain rhythms, a strong heartbeat pulse will be superimposed, tending to block the brain signals.

## CARDIOPHONE

Stress situations, like running for a bus, attending an interview, sitting an exam, or appearing before an audience, are usually attended by an obvious increase in heartrate, but during the course of an uneventful day the heart also responds to numerous minor stress situations which normally pass unnoticed.

By making the heartbeat clearly audible, it is possible to detect these subtle changes, and perhaps learn to control them. This is really an example of bio-feedback. If the heart speeds up slightly in response to some unconscious stimulus, you become aware of it and seek to reduce it.

Conversely, it may also be possible to induce an artificial state of excitement by consciously trying to increase heartrate, and thereby cause more adrenalin to be released into the system.

In the cardiophone circuit (Fig: 11) transistor TR8 is in series with the emitter supply to astable multivibrator TR9 and TR10. In the absence of a heartbeat signal, TR8 base is grounded (by R16, Fig. 3) and the multivibrator is therefore switched off. Diode DI in the pre-amplifier, rectifies a heartbeat signal and applies a positive going pulse to TR8 base, thus switching on TR8 and the multivibrator. and causing a 300 Hz audio "bleep" tone to be heard in the earpiece X 1 .

Switch S5 in Fig. 11 gives additional top cut to suppress mains borne interference.

Brain rhythm frequency meter. The coaxial socket provides a connection to the visual feedback unit


Fig. 11. The pre-amplifier used with a cardio-phone circuit


Fig: 12. Layout and wiring of the cardiophone output module

## COMPONENTS

## ADDITIONAL COMPONENTS FOR CARDIOPHONE

Resistors

| R33 | $1.5 \mathrm{k} \Omega$ |
| :--- | :--- |
| R34 | $22 \mathrm{k} \Omega$ |
| R35 | $22 \mathrm{k} \Omega$ |
| R36 | $1.5 \mathrm{k} \Omega$ |
| All $\pm$ | $10 \% \frac{1}{2}$ watt carbon |

## Capacitors

C18 $0.03 \mu \mathrm{~F}$ polyester
C19 $0.03 \mu \mathrm{~F}$ polyester

## Transistors

TR8 BC108
TR9 BC108
TR10 BC108

## Earpiece

X1 150 ohm magnetic

## Switches

S5 Single-pole, on-off sub-miniature toggle
S6 3-pole, 2-way wafer

## Batteries

B9, B10, B11 9 volt style PP3 (3 off)
Socket
SK5 3.5 mm 2 pole jack
Miscellaneous
Electrodes
Battery connectors
Metal box (see text)


Fig. 13. Circuit of the visual feedback lamp driver

## COMPONENTS . . .

```
            ADDITIONAL COMPONENTS FOR
            VISUAL FEEDBACK LAMP DRIVER
Resistors
    R37 1MS2
    R38 10k\Omega
    R39 470\Omega
    R40 100\Omega
    R41 4.7k\Omega
    R42 10\Omega
    All }\pm10%\frac{1}{2}\mathrm{ watt carbon
```


## Potentiometer

VR5 $500 \mathrm{k} \Omega$ sub-miniature horizontal mounting preset

## Capacitor

C20 $0.25 \mu \mathrm{~F}$ miniature polyester
Transistors
TR11 BC108
TR12 BC108
TR13 AC128
Switch
S7 Single-pole, on-off toggle or slide
Lamps
LP1, LP2 6V 60mA m.e.s.
Battery
B12 9 volt style PP9


Brain rhythm frequency meter. The coaxial socket provides a connection to the visual feedback unit


Fig. 14. The method of mounting the lamps in plastics lens sunglasses

## CONSTRUCTING AND USING THE CARDIOPHONE

The cardiophone output module circuit board (Fig. 12) may be housed, along with the preamplifier module, in a metal box similar to that used for previous projects. Socket SK 5 must be insulated from the box.

Electrodes for use with the cardiophone can either be positioned a few inches apart on the left side of the chest, or one on each wrist, and held in place with elastic straps.

Set VR1 to minimum gain, and VR2 to wideband, with S5 open circuit. Plug earpiece X1 into SK5, the electrode leads into SK1 and SK2, and switch on. If no heartbeat "bleep" is heard, advance VR1. When the heartbeat is masked by interference, close S5, and adjust VR1 and VR2 for a clear signal.
Try using the cardiophone with a friend who is driving a car. The "bleep" rate will increase when negotiating roundabouts, traffic lights, and congested streets, and will rise sharply when overtaking.

## VISUAL FEEDBACK

The lamp driver circuit in Fig. 13 can be employed as an external unit to extend the scope of previous projects. An output taken from the pre-amplifier (output 1 ) is amplified to a level sufficient to flash two low consumption filament lamps (LP1 and LP2) which are mounted close to the eyes in a pair of cheap plastics lens sunglasses; see Fig. 14.

When driven by brain rhythms, visual feedback will produce an interesting variety of "strobe" effects while leaving the ears free to, say, listen to music or other sound sources.

If the lamp driver circuit is housed in a small plastics box, it can be coupled to the alphaphone, alphameter, frequency meter, or cardiophone, via screened cable to a coaxial socket which connects with pre-amp output 1 . VR5 is adjusted so that both lamps just glow when there is no signal. Setting up instructions are otherwise the same as for previous projects.

Note: pin 12 in the case interwiring diagram in Fig. 5 (last month) should be designated pin 11 to agree with the practical circuit.



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| 61 | 100 | 5 | 12 | $10.2 \times 8.9 \times 8.3$ |
| 30 | 200 | 9 | 8 | $12.0 \times 10.3 \times 10.0$ |
| 62 | 250 | 12 | 4 | $9.5 \times 12.7 \times 11.4$ |
| 55 | 350 | 15 | 0 | $14.0 \times 10.8 \times 12.4$ |
| 63 | 500 | 27 | 0 | $17.1 \times 11.4 \times 15.9$ |
| 92 | 1000 | 40 | 0 | $17.8 \times 17.1 \times 21.6$ |
| 128 | 2000 | 63 | 0 | $24.1 \times 21.6 \times 15.2$ |

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& \text { PRIMAMY 200-250 VOLTS I2 AND/OR } 24 \text { VOL }
\end{aligned}
$$

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\begin{aligned}
& \text { LOW VOLTAGE SERIES (ISOLATED) } \\
& \text { PRIMAMY } 200-250 \text { VOLTS } 12 \text { AND/OR } 24 \text { VOLT RANGE } \\
& \text { Ref. Amps. Weight Size } \mathrm{cm} \text {. Secandopy Windings } P \text { \& } \\
& \text { No. } 12 V 24 V \text { ib oz }
\end{aligned}
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& \text { Ref. Amps. Weigh } \\
& \text { No, } 12 \mathrm{~V} 24 \mathrm{~V} \text { ib } \\
& 1110.50 .25 \\
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$$
\begin{array}{lll}
10.5 & 0.25 \\
130 & 0.5
\end{array}
$$

$$
\begin{array}{rr}
71 & 2 \\
18 & 4 \\
70 & 6 \\
108 & 8 \\
72 & 10 \\
17 & 16 \\
115 & 20 \\
187 & 30 \\
226 & 60
\end{array}
$$

$$
\begin{array}{cc}
t & \\
0.85 & 2 \\
1.01 & 2 \\
1.33 & 2 \\
1.86 & 3 \\
2.24 & 4 \\
2.48 & 5 \\
2.94 & 5 \\
4.54 & 5 \\
5.78 & 6 \\
10.67 & 8 \\
19.61
\end{array}
$$

| Amps. | Weight is oz | Size cm. | VOLT RANGE Secondary Taps |  |
| :---: | :---: | :---: | :---: | :---: |
| 0.5 | 14 | $8.3 \times 3.7 \times 4.9$ | 0.12-15-20.24-30V | 1.01 |
| 1.0 | 20 | $70 \times 6.4 \times 6.0$ |  | 1.35 |
| $2 \cdot 0$ | 32 | $8.9 \times 7.0 \times 7.6$ | . | 2.01 |
| 3.0 | 46 | $10.2 \times 8.9 \times 8.6$ | . | 2.48 |
| 4.0 | 60 | $10.2 \times 10.0 \times 8.6$ | ", ", | 2.94 |
| 5.0 | 68 | $12.1 \times 10.0 \times 8.6$ | '* | 3.68 |
| 6.0 | 78 | $12.1 \times 10.0 \times 10.2$ | " | 4.36 |
| 8.0 | 100 | $14.0 \times 11.7 \times 10.0$ | .. | 5.64 |
| 10.0 | 122 | $14.0 \times 10.2 \times 11.4$ | ". ${ }^{\text {\% }}$ | 7.14 |
| Amps. | Weigh | Size cm. ${ }^{50}$ | VOLT RANGE Secondary Tops | $P$ |
| 0.5 | 16 Oz | $7.0 \times 7.0 \times 5.7$ |  |  |
| 1.0 | 210 | $8.3 \times 7.3 \times 7.0$ | ,. | 1.94 |
| 2.0 | 50 | $10.2 \times 8.9 \times 8.6$ | , .. | 2.69 |
| 3.0 | 60 | $10.2 \times 10.2 \times 8.3$ |  | 3.65 |
| 4.0 | 94 | $12.1 \times 11.4 \times 10.2$ |  | 4.83 |
| 6.0 | 124 | $12.1 \times 11.1 \times 13.3$ | .. | 7.1467 |
| 8.0 | 189 | $13.3 \times 13.3 \times 12.1$ | $\cdots$ | 9.3297 |
| 100 | 1912 | $16.5 \times 11.4 \times 15.9$ |  | 11.68 |



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[^3]

## Audio Frequency Discriminator By G.F.A. HOFFMAN de VISME

ACIRCUIT for distinguishing between two notes whose frequencies are very close together and whose amplitudes may differ greatly is shown in Fig. 1. The operation of the circuit does not depend on the use of filters, and notes of any frequency may be distinguished by simple potentiometer adjustment.

The circuit was designed for a project in which it was necessary to distinguish between notes differing in frequency by as little as 20 Hz , the mean frequency of the notes lying in the range 300 to 1500 Hz . The amplitudes of the notes could differ by as much as a factor of ten, and the notes themselves were not free of distortion. In addition, a certain amount of acoustic noise was present during the experiment.

The requirement was that when the higher pitched note was sounded a bistable should be set, and when, after an unspecified period of silence, the lower pitched note was sounded the bistable should be reset. There was no need for undue speed in the response of the bistable since each note was sounded for some seconds.

Whilst audio frequency filters can be devised to meet the above demands, there are well known difficulties with these as regards the realisation of high $Q$ at low frequency and as regards tuneability, and sensitivity to signal amplitude. The method described below is a simple alternative which achieves the required objectives without the use of filters or counting techniques.

Although originally designed for a project involving acoustic measurements such a circuit could be used in a variety of practical situations. For example it could be used to enable the driver of a moving vehicle to switch on (and switch off) a stationary warning light of some kind by sounding notes of appropriate frequencies. Alternatively an operator could use the circuit to control a model railway


Fig. 2. Trip circuit switching levels and waveforms
acoustically, or, by sounding horns of different frequency, a motorist could open and close his garage doors from his driving seat.

Although the circuit as described here consists of discrete components, every part of it except the emitter followers and pump circuit is realisable using standard integrated circuit modules. In this form the circuit could be made extremely compact.

## PRINCIPLE OF OPERATION

Fig. 1 is a block diagram of the circuit. The audio signal, after amplification, is squared by a Schmitt trigger circuit to yield a wave with sharp leading and trailing edges. The squared signal is applied to a diode pump circuit designed to give a d.c. output


Fig. 3. Circuit diagram of the a.f. discriminator

as nearly as possible proportional to the signal frequency. Thus if a note $A$ is sounded a voltage of, say, 4 volts appears at the output of the pump circuit, while if a higher pitched note $B$ is sounded a voltage of, say, 5 volts appears there. It is required, therefore, that the bistable, if set, should be reset by the 4 volts signal due to note A , and if reset, it should be set by the 5 volt signatl due to note $B$.

To achieve this the pump circuit output is applied simultaneously to two trip circuits. The switching levels of these are so arranged that when note $A$ is sounded only Trip I switches, while when note B
is sounded both are switched. The signals from these trips are then used as the reset and set signals, respectively, of a bistable whose output controls a relay. In order to ensure that the bistable remains set after note $B$ has ended the switch-off level of Trip 2 is made lower than the switch-off level of Trip 1. In this way the set signal produced by Trip 2 lasts until after the reset signal from Trip 1 has ended.

Fig. 2 shows the waveforms from Trip 1 and Trip 2 and the corresponding bistable output, resulting from notes $A$ and $B$ respectively.


Fig. 4. Trip circuit and bistable outputs from selective discriminator


## CIRCUIT FEATURES

Fig. 3 shows the circuit of the discriminator using all discrete components. Most of the circuitry is conventional, but suitable circuit values are included for the benefit of readers.

The only features worthy of note concern the pump circuit. To ensure a reasonably linear voltagefrequency characteristic from this stage capacitive loading of the previous stage must be small, hence the relatively small coupling capacitor $(0.022 \mu \mathrm{~F})$, and a transistor must be used in the place of the usual shunt diode. Adequate sensitivity then demands a fairly large shunting resistor ( $47 \mathrm{k} \Omega$ ), which therefore necessitates the inclusion of an emitter follower between the pump circuit and the trip circuits.

A large value $(16 \mu \mathrm{~F})$ is used for the reservoir capacitor to slow down the speed of the response of the pump circuit and so minimise its sensitivity to background noise.

## PERFORMANCE

The discrimination attainable by the above circuit was found to depend to a large extent on the purity of the notes used as signals. The following table shows how the pump circuit output varies with signal frequency, the signal being provided by a signal generator rather than a microphone:

| Frequency (Hz) | 300 | 400 | 500 | 600 | 700 |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Pump circuit output (volts) | 2.7 | 3.6 | 4.5 | $5 \cdot 3$ | $6 \cdot 1$ |

By setting the switch-on and switch-off levels of Trip 1 to $3 \cdot 8$ and $3 \cdot 1$ volts, respectively, and those of Trip 2 to $5 \cdot 3$ and 1.6 volts, respectively, it was possible to distinguish signals of frequency 590 Hz and 600 Hz with complete reliability. Using a good quality microphone and real notes generated by a
loudspeaker the performance was almost as good $(570 \mathrm{~Hz}$ and 590 Hz$)$ even though the notes from the speaker were noticeably distorted. With a poor (carbon) microphone, however, the discrimination was much poorer due to frequency jitter at the output of the squarer.

## BAND-PASS FILTERING

The above principle may readily be extended to provide selective discrimination, whereby, if A, B and $C$ are notes of successively higher pitch, $A$ or $C$ reset a bistable which has been previously set by B. In this case three trip circuits are used, the switching levels of Trip 1 being arranged to lie within those of Trip 2, which in turn lie within those of Trip 3. As shown in Fig. 4, note A causes only Trip 1 to switch, note B causes Trip 1 and Trip 2 to switch, while note $C$ causes all three to switch.

When notes $A$. $B$ and $C$ are sounded in turn the trip circuit outputs pursue sequences as shown in the following table. The 'required output $Q$ from the bistable is shown alongside, the symbol $Q^{\prime}$ representing "the previous value of $Q$ ":

| OUTPUTS | Note A | Note B | Note C |
| :--- | :---: | :---: | :---: |
| Trip 1 | 010 | 01100 | 0111000 |
| Trip 2 | 000 | 00110 | 0011100 |
| Trip 3 | 000 | 00000 | 0001110 |
| Bistable (Q) | $Q^{\prime} 00$ | $Q^{\prime} 0111$ | $Q^{\prime} 010000$ |

From this table it is easy to deduce that the reset signal for the bistable has to be $\overline{\mathrm{T}}_{1}$ (the inverse of the Trip 1 output), while the set signal has to be $\overline{\mathrm{T}}_{2}+\mathrm{T}_{3}$ (i.c. the inverse of the Trip 2 output OR the Trip 3 output).


BY FRANK W. HYDE

## SATELLITE CAMERAS

Cameras that have been developed and used with such great success on satellites and other spacecraft have been mainly devoted to the obtaining of high definition. Similarly with television cameras where the task is much more difficult, the British company EMI have made a major contribution in this field. They developed a low light tube which was used in the ESRO TD-I spacecraft launched in March 1972. and was part of a French experiment to map gamma rays from the galaxy. It was the first time that a European camera tube has been used in space.
The tube, known as the Ebitron. was developed at Hayes, Middlesex. by EMI Central Research Laboratories. it is an intensifier vidicon tube measuring 160 mm by 64 mm and is claimed to be the smallest tube of its type in the world. It formed the "seeing" part of the camera designed by the French company Engins Matra. The camera with its associated equipment is quite light. the camera itself weighing only 1.8 kg .

The EMI tube was chosen because of its small size. low weight and its ability to "see" in near darkness. Its ease of operation, fast response. low light requirement made it ideal for recording the sparks caused in a gas chamber by the passage of gamma rays.

As gamma rays pass through the gas filled chamber the gas becomes ionised leaving trains of sparks These are short lived (a few millionths of a second only) and of low intensity.

A series of mirrors is arranged so that two sides of the chamber can be viewed by the Ebitron thus enabling a three dimensional image to be obtained. The information is
stored and transmitted to earth stations for analysis by computer.

The $T D-I$ is the first satellite to scan the whole sky and also the first to be able to operate in full daylight. The picture of the sky is built up over a period of six months from a polar orbit of some 500 km altitude. The satellite is one of the most advanced in operation put into space. It was launched on a ThorDelta rocket from the Western Test Range in California.

## ECOLOGICAL STUDIES FROM SPACE

Aboard the Earth Resources Satellite which was launched in July 1972 were cameras designed by RCA for high resolution TV. These cameras can detect crop deseases and pollution sources in the course of making their scanning passes.

The system which consisted of three cameras was designed by the Astro-Electronics Division of RCA at Princeton. N. Jersey. They have produced a picture which is some ten times sharper than the kind that appears on home television sets.

Each camera uses 4,000 horizontal scanning lines for the building of a picture. From a height of some 900 km each camera will be able to view the same area of $180 \mathrm{~km}^{2}$. Each camera observes in a different part of the spectrum, one in red, one in infra-red and the third in green. After transmission to Earth the three images are combined and the composite picture can then be studied.
It is perhaps worthwhile to point out that this technique was used ten years ago by Ian Whitacker when studying the moon. Later other astronomers used the same technique.
Now its use has been extended to the study of the environment and has proved exceptionally valuable. Already the diseased areas of various food crops have been photographed, as well as silt movement from estuaries into the sea and the direction of ocean currents have also been mapped.
One of the advantages of this kind of photography is that the altitude of the satellite gives orthographic pictures so that the proper spacial relationships are directly seen. No corrections are required to show the real condition without the spacial distortion that arises from ordinary mapping.

As the orbit of the satellite is synchronised with the Sun the same lighting conditions exist for, each area viewed, thus avoiding distortions that appear when using other methods of carrying cameras aloft which are subject to changing angle of the light of the Sun. The full significance of this aspect can be appreciated when it is understood that only 72 per cent of the habit-
able land has been mapped in detail and of this more than 50 per cent of those that exist are out of date.

The new mapping will now fill in this gap, and not only that, each area will be mapped 18 to 20 times a year.

## INDIA AND SPACE ACTIVITY

India has been very active in the field of space development. as well as in radio astronomy. There are plans afoot to build the first allIndia satelite for launch in 1974.

It is expected that the launch vehicle will be Russian and will carry a satellite weighing about 100 kg . There will be three experiments on board which have been designed by ISRO (India Space Research Organisation) and will be built entirely in India.

Development is also proceeding on a design for a carrier vehicle expected to be ready by the end of 1974. It is a four stage design similar to the Scout rocket. It will be capable of putting a 40 kg package into orbit at about 400 km altitude.

It is planned that the first firing be made to gain experience. Later launchings will carry on-board experiments. This will be worked up eventually to a coverage for educational purposes.

By 1974 India will have access to the NASA satellite ATSF which will be launched in 1973. This will enable India to have the facility to cover some 5,000 villages for educational purposes. India will design and manufacture the small and rugged battery receivers needed and also the 10 ft diameter aerials made of chicken wire.

There are two major satellite communications stations in India one at Avi and the other at Ahmedabad. The dishes at these sites are 30 m dia. Most of the research is carried out at the National Aeronautical Laboratories in Bamgalore. There are divisions there covering Aerodynamics, Propulsion, Materials. Electronics, Instrumentation and Structures.
India suffered a severe blow with the death of their leading scientist Vikam Surabhai in 1971. However. such was the nature of his forward planning that India has today a very successful space research team.
India has contributed quite considerably already to the space programmes of other countries. From the launching sites at Thube near Travandram, which is U.S. sponsored. several hundred launchings have taken place. Rockets. probes. and satellites of British. French. Russian and Indian origin have already been launched from there.

A new site now being completed. the Shrihameola Range, will extend India's future space activities even further.

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## VALENCE ELECTRONICS

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# report from <br> AUSTRALIA 

## BY J.M.WALDIE

## FM BROADCASTING

The Australian Broadcasting Control Board has been enquiring into the desirability of $\mathrm{f} . \mathrm{m}$. radio in Australia and has now issued its findings in a 100 -page volume entitled "Frequency Modulation Broadcasting' '. The board examined some 150 written submissions and 70 formal exhibits, and employed its Technical Services Division to carry out an examination "of every technical problem considered to be possible' $"$.

The upshot of this deliberation is to recommend that f.m. broadcasting should be introduced, and this has been endorsed by the Government.

This is, in fact, the third time that official committees in one form or another have examined f.m. radio in Australia. The first was in 1942 and resulted in the installation of four experimental transmitters, operating in Sydney, Melbourne, Brisbane and Adelaide in 1948.

## OBJECTIONS

In 1957, the board conducted a public enquiry and found "very real practical objections to the introduction of f.m. broadcasting''. The four stations, which by then were transmitting for some 80 hours weekly using substantially the same material as was included in the more serious of the then two $A B C$ programmes, were closed down in 1961 to allow for expansion of the television services from 10 to 13 channeis.

This situation, in which the v.h.t. band is more or less saturated with television and other services, provided a large headache for the enquiry just completed. It was preferable to use the v.h.f. band for the projected radio service for obvious reasons: the technology was well known and the signal propagation would be relatively high. However, this meant the abolition or re-allocation of one or more television channels with obvious disadvantages and the possible need to use bandwidths of as low as 0.4 MHz .

The alternative was to use the u.h.t. band, which is relatively uncluttered, but this, too, has disadvantages: no other country uses u.h.t. for f.m., and standardisation should be the aim; the technology
was virtually unknown; the coverage obtainable would be lower than with v.h.f.

However, the die is now cast: the recommended bandwidth (allowing 20 stations to cover each area) is 40 MHz and the suggested frequency range is $470-510 \mathrm{MHz}$. Local manufacturers have three years in which to decide on the technical standards for u.h.f. reception and transmission.

## PLANS FOR THE FUTURE

The aim is to provide two national stations, one to transmit the current $A B C$ network for provincial and country areas, and the second, citybased, to provide a second "fine music', network. Commercial stations will also be licensed. Finally, a new type of station will be introduced, on a non-profit basis, to cater for the needs of minority groups. All these stations can transmit stereophonically.

It has been suggested, with just a hint of patriotism, that Australia's venture into u.h.f. broadcasting might just be the shot in the arm that the local manufacturers claim is needed. It will be interesting to see if the Japanese will produce a u.h.t.$\mathrm{f} . \mathrm{m} . / \mathrm{a} . \mathrm{m}$. receiver for the Australian market by 1978 .

## AUDIO SHOW

There can be no doubt that hi-fi enthusiasts (at least in Sydney) have an extremely large selection of equipment available to them, if the 1972 Audio Show, held in Sydney on August 9-13, is any guide. It is equally true to say that the average buyer can not be badly off; the manufacturers and importers, in conjunction with Australian hi-fi, must be conscious of a considerable interest to stage an exhibition of this magnitude.

The show actually covered three floors of a moderately large multistorey motel. The ground floor was relegated to 16 large (silent) displays; two upper floors were used to demonstrate, in over 40 individual suites, the complete range from any one manufacturer or selected combinations.

More than half the equipment shown originated in Japan, with all the major names being present. British exhibitors included Garrard
(the Zero 100 deck was used in many stands), Wharfedale, KEF (who have, along with Leak and Goodmans, commenced local production), Plessey, BSR, and B\&W.

## NEW DEVELOPMENTS

Interesting new developments for the cassette enthusiast included the new Sony deck (TC 165) with automatic and continuous reverse facilities, several new decks with inbuilt Dolby, including National, TEAC, Kenwood and Pioneer, and a C 180 cassette, and an endless loop cassette, both from TDK.

There were many four-channel units demonstrated, but by far the most impressive was one line-up consisting of a four-track TEAC 3340 deck, feeding two JVC PST 1000 stereo graphic equalisers, in turn feeding two phase linear power amplifiers whose 2,800 watts (r.m.s.) output was handled by four ESS transmission line speakers-and this in a room measuring about $12 \mathrm{ft} \times 15 \mathrm{ft}$ ! Cost-about $£ 4,000$, but trade-in's are acceptable.

## OPTICAL <br> COMMUNICATIONS

Australian communications may benefit from a new joint venture by Amalgamated Wireless (Australasia) Ltd., and the Tribophysics Division of the Commonwealth Scientific and Industrial Research Organisation (CSIRO). The CSIRO have developed a new type of optical fibre, consisting of a liquid-filled hollow glass tube.
Although finer than a human hair, the fibre could transmit more information than existing wide-band microwave and coaxial communication links. Using a helium-neon injection laser as a light source, for example, it is claimed that, using the new fibre, previous disadvantages of signal loss over long distances using light guides are overcome.

The system has been made available to the Australian Post Office for its research laboratories to evaluate the fibre's potential in the development of Australia's Telecommunications network.

It is certainly a far cry from that eventful day in 1870 when John Tyndall showed that light could be borne by a liquid around corners.


THE realisation of music and allied effects by means of a variety of electıonic devices has been possible for a good many years. The electronic organ, for examp"e, was becoming rapidly accepted a ciecade before World War II. Of the vast range of electronic instruments now available, however, there are a few which are not aligned to operate around a conventional chromatic scale. Thus, for the performer, the appeal of such instruments would be based primarily on the effect of tone quality, ease of playing and novelty in design.

For the composer, however, the abundance of electronic instruments does little more than provide a range of alternatives to supplement or replace standard instruments of the orchestra Out of such a situation the idea of musique concrete was born. This technique enabled composers to create and experiment with sound forms generated naturally or unnaturally by such unlikely scurces as dustbins, rattling teacups, conversation or malplayed musical instruments. Some workers incorporated a system of manually operated oscillators, both groups linking their sound sources to one or more disc cutters or, later, tape recoiders.

The task of creating and blending discrete tones into a coherent and recognisable musical work involved so much laborious effort that musique concrete established the reputation of being more of a technical exercise than a creative art form. Thus the publication of Moog's designs for voltage controlled amplifiers and oscillators about eight years ago was hailed with enthusiasm in many quarters of the musical world.

Moog's designs crystallised the ideas and requirements expressed by a number of serious composers winose creativity was hampered and frustrated by the confines of the accepted musical disciplines. The possibilities of, and extensions to, Moog's original circuits have led with great rapidity to the inception of a series of variably complex devices having the generic label of 'synthesiser".

## THE SYNTHESISER DEFINED

What exactly is a synthesiser? The word "synthesis" is defined as the building up of separate elements into a connected whole and this, very succinctly, describes the function of the synthesiser with respect to the formation of sound structures.
Essentially the instrument consists of a number of sound sources and sound treatments which may be combined together in an enormous diversity of ways to produce an equally varied range of sounds in a number of applications.

1. As a live performance instrument. A considerable company of popular artists and groups use a synthesiser, in one form or another, as a standard item of equipment either to supplement their normal methods of sound treatment or to play as an instrument in its own right.
2. As a sound effects unit. The use of the synthesiser is by no means restricted to musical circles and it is equally at home "producing" creaking doors, artillery fire, explosions, dripping water, birdsong and a virtually unlimited range of sounds similar to those featured in and popularised (for some) by the "Dr Who" series. Thus the tape recording enthusiast, amateur dramatic society, cine club and so on could easily find the synthesiser becoming a useful and indispensible tool.
3. As an audio-visual teaching aid (in conjunction with a good oscilloscope) the synthesiser can provide an invaluable insight into the fundamentals of electronic and acoustic waveform phenomena. In this respect there is a large potential field of application.

## IMITATIVE OR UNIQUE

The term synthesiser carries the implication, for some, that the instrument is of an essentially imitative nature and/or that the sounds produced by it are ersatz. With regard to the former criticism, the degree of control which may be exercised in a well designed synthesiser is such as to allow it to imitate a wide range of musical instruments very effectively.
For the sound effects man, the ability of the instrument to produce imitations of a wide range of naturally occurring sounds is a feature which cannot be lightly set aside.

In answer to the second criticism which implies that the sound forms produced by the synthesiser are, in a sense, unreal-nothing could be further from the truth. The nuance and timbre imparted by the synthesiser to a fundamental tone is no less real than the nuance and timbre imparted, to the same tone, by, say, a trumpet or a violin. In practice, the purity and exactitude of the tonal permutations made available by the synthesiser are frequently inspiring and possess a beauty which is peculiarly their own.


Fig. 1. Block diagram of a voltage controlled oscillator

## VOLTAGE CONTROL

Various forms of voltage control have been known and exploited for a number of years but the application of the principle to the control of synthesiser circuits results in the appearance of a number of unique features. By way of illustration one could scarcely choose better than a form of voltage controlled oscillator based on the design published by Dr Moog. Fig. 1 shows such a device in block form.

The relaxation oscillator is driven by an operational amplifier the output current of which is proportional to the exponential of the input. As the output current increases so also will the rate at which the charge on capacitor " C " reaches the unijunction breakdown voltage. Thus the frequency is increased.

The unijunction sawtooth is fed to a series of waveform shaping circuits which provide a useful number of "in phase" outputs. By means of this system relatively wide frequency ranges may be obtained without the necessity of switched RC or inductively tuned networks.
The general principle of voltage control may similarly be applied to almost any parameter in any of the devices built into the synthesiser, e.g. amplifier gain, filter bandpass or band reject characteristics, degree of reverberation and so on. There are a number of distinct advantages in so doing, these are:

1. Signal and control paths are quite separate from one another. Thus a device may be remotely controlled without compromising the signal in any way.
2. Devices can control one another in a continuously variable manner without the necessity of complicated, expensive and limited-range switching circuits. In certain circumstances a device may control or limit its own output by using part of the signal output as feedback to the control input.
3. By provision of high input impedance to the control circuits each controlling device has a potentially large "fan-out" capability thus making multiple parameter control a possibility.
A specific example of voltage control is given later in this article and will serve to underline the flexibility and versatility of the system.

## SYNTHESISER DESIGN

In designing a synthesiser care has to be taken to ensure that the system does not become so complex that it is impossible to operate effectively.

Consequently it is necessary to define the requirements of the instrument and to specify the means by which these requirements may be met. In this respect a form of modular construction offers the distinct advantage that one may start with a simple system and increase the size and complexity as and when required.

As a general rule most sounds have a fairly complex structure comprising a fundamental tone, one or more overtones or harmonics and, in some cases, an element of noise. It is usually the fundamental tone which dominates the sound structure and which provides the primary means by which the sound is observed.


The author's prototype synthesiser is shown above. Below is the final version built in modular form and housed in a Vero metal case


Another important feature concerns the way in which the sound structure is presented. The rapidity with which the sound becomes audible, the maximum volume attained and the rate at which the sound dies away together constitute a pattern, known generally as an envelope, which contributes very largely to the recognition of the sound. Variation in the rapidity of attack and the rate of decay of an otherwise unchanging sound structure can make an enormous difference to the auditory effect of the sound on an observer.

Two other factors play an important part with respect to the recognition of sound. These are timbre and nuance. Timbre is defined as the characteristic quality of sounds produced by each particular instrument or voice, depending upon the number and character of the overtones while nuance relates to the delicacy, or shade of meaning, of a sound.

## ACHIEVING THE REQUIREMENTS

It is a relatively straightforward matter to provide hardware to meet three of the above requirements, i.e. fundamental tones may be provided by one or more oscillators; variation in sound presentation is achieved by means of an envelope shaper while
timbre may be varied by selective filtering and additive mixing, either separately or in combination, together with a degree of reverberation.

Control of nuance cannot, however, be achieved by the application of a discrete piece of hardware but is controlled by the inter-adjustment of practically all the parameters involved in any particular sound structure.

## PROGRAMMED MODULES

The hardware so far considered covers the basic necessities of sound formation but offers nothing that cannot be obtained from a selection of signal generators, reverberation amplifier and integrator, all of which are easily obtainable as discrete units and in a variety of forms. The next stage, therefore, is to devise a means whereby the principal function of the modules may be voltage controlled and to provide the means by which they may be programmed to produce a range of tone patterns or rhythms. Automatic programming may be achieved by provision of one or more ramp or random voltage generators.

If these latter devices are, themselves, made programmable then the possible control signal permutations, with only a small number of modules, becomes

## SPECIFICATION

Stabilised Power Supply $+15 \mathrm{~V} / \mathrm{O} /-15 \mathrm{~V}$ at 750 mA per rail. Max. ripple at $\mathbf{1 2}$ per cent overload is less than 15 mV .

Two Input Amplifiers
Gain variable from unity to $\times 50$.
Two Ramp and Pulse Generators
Frequency range (a) 0.01 Hz to 15 Hz .
(b) 0.05 Hz to 30 Hz .

Manual and voltage control. Output voltage is 4 V nominal ramp and -4 V nominal pulse.

Two Triangular/Square Wave Oscillators
Frequency range (voltage control) less than 1 Hz to 16.5 kHz . Frequency range (manual control) 5 Hz to 10 kHz . Output voltage: Triangular 350 mV p-p. Square IV p-p.

Two Output Amplifiers Variable gain with manual and voltage control. Panning facility between channels. Input level 500 mV . Maximum voltage gain +13dB.

## Reverberation Amplifier

Variable gain manually controlled. Voltage control of reverberation. Unity gain with reverberation out. Frequency range of spring line -3 dB at 80 Hz and 4 kHz . Input level 500 mV .

## Ring Modulator

Four quadrant multiplier based on integrated circuit. Frequency response effectively flat from d.c. to greater than 150 kHz . Input levels $2 \times 500 \mathrm{mV}$ max. Output level 800 mV max.

## Tone Control

Tuneable active filter. Effective slope 7dB/octave. Overlapping bass and treble ranges allow extreme effects to be obtained.

## Envelope Shaper

Produces an envelope of variable shape and period derived from internal constant voltage source and external trigger. May be triggered manually. Output waveforms variable from pulse, sawtooth, trapezoid, and triangular.

## Noise Generator

Provides up to 3.5 V white noise. Control of colouration by means of tuneable low pass filter.

## Sample and Hold

Random voltage generator which can double as an additional ramp generatos. Produces staircase waveforms of formal or random nature. Clock output is provided for synchronisation purposes. Output level - 6 V max.

## Differential Amplifier

Provides additive and/or subtractive mixing facilities. Output level proportional to sum and/or difference of the four inputs provided, maximum 26 V p-p.

## Inverter

Similar to above but with only two inverting inputs.

## Meter Unit

A meter with precision rectifier circuit to read a.c./d.c. signals in two ranges, 0.5 V and 1 V .


Fig. 2. Block diagram of the synthesiser
very wide indeed. If the frequency range of the ramp generators is sufficiently wide they may themselves be considered as sound sources and used for the direct provision of rhythms.
Similarly. with the control signal suitably attenuated and running at a frequency of between $6-8 \mathrm{~Hz}$, a single ramp generator may be used to provide a vibrato modulation to an oscillator thus adding greatly to the interest content of discrete tones.


Synthesiser keyboard with separate sustain, vibrato and oscillator units mounted on the left

## ADDING A KEYBOARD

Perhaps the simplest method of programming the oscillators is by the addition of a keyboard. Since keying provides a range of control voltages to the oscillator the keyboard itself may be considered to be a manually operated staircase generator.

The keyboard may also be used to provide gating and synchronising pulses to initiate treatment or shaping sequences each time a key is depressed.

## SOUND TREATMENTS

The only sound treatment so far given any degree of consideration is that of reverberation. There are. however, a number of others which can provide very useful extensions to the facilities offered by the synthesiser. Up to now the accent has been on synthesis by addition, but, equally, one can synthesise by subtraction.

In this latter case the starting point is a complex sound, such as white noise. from which the required elements are obtained by filtration. There is thus a place for one or more notch and/or band-pass filters the actual characteristics of which may be varied by means of voltage control.

On the simpler side there is also a place for a form of tone control of sufficient range to enable extreme effects to be investigated.

## INTERFACING

Finally, it is necessary to consider the best means of interfacing the synthesiser with external equipment so that it may accept as wide a range of inputs as possible without distortion and, on the output side, provide a similar widely compatible drive.
A block diagram of the synthesiser to be described is given in Fig. 2.
The idea of external connection compatibility for all modules was believed to be a prime requirement in view of the possibility that many constructors may wish to build only a limited number of the


The basic modular form of construction that will be used throughout the series modules to be described as additions to existing synthesiser projects. In view of this situation it may seem somewhat paradoxical to provide modules labelled input and output amplifiers.

In point of fact these can be connected in virtually any position in a chain of modules the main limitation being due to the possible saturation of the amplifiers due to the input levels being exceeded.

The final stages of the output amplifiers are crosscoupled by "panning" controls thus enabling stereo and "floodsound" effects to be investigated.

## INTERCONNECTIONS

Referring again to Fig. 2, it will be noted that many of the modules are shown with interconnections made between them.

Of the three most widely used systems of module interconnection the one most suited to the modular concept is that in which individual devices are coupled by means of patch cords. The great disadvantage of this system is that a complicated patch can render the front panel controls almost inaccessible.

With a view to relieving this situation modules may be connected internally in the manner in which they are most likely to be used. The actual method of internal connection is really a matter of the individual constructor's preference, those connections shown in Fig. 2 being intended as a guide rather than a mandatory requirement.

## BUILDING THE SYNTHESISER

Full constructional details will be given on building the synthesiser shown and an outline specification of the instrument appears in this article.

Extensive use has been made of the 741 operaional amplifier since the use of these devices invariably simplifies design and construction in comparison with circuits in which discrete semiconductors are employed. Furthermore, the 741 offers the feature of unconditional stability under almost any operating condition and is protected internally against "latch-up" and output short circuit and is readily available at economic prices from a variety of sources.

The only test equipment requirement is for a good oscilloscope, particularly during the setting up stages. Ideally the scope should be d.c. coupled but, failing this, a high resistance voltmeter will suffice to monitor the v.l.f. performance of the various modules.

Next month, constructional details for the stabilised p.s.u. will be given.

## NEXT MONTH

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## TAPE LINK:...

Bring hi-fi quality to your tape deck with this quarter track stereo tape link.
It features separate record and replay amplifiers using modern circuit technology to give low distortion and noise, and accurate replay characteristics.
Tape speeds of $1 \frac{7}{6}, 3 \frac{3}{4}$ and $7 \frac{1}{2}$ inches per second are catered for, and a switch is included for single track mono operation. Setting up requires only minimal circuit adjustments.

## SIENAL INEECTOR TRACER

Using a digital integrated circuit in a linear mode makes this Signal Injector and Tracer cheap and easy to build. Extremely useful for fault finding on radios, amplifiers and other audio equipment. A simply built r.f. probe makes the Tracer suitable for high frequency detection.


## PRACTICAL

## GREAT LEAP FORWARD

The year 1973 should be good for Solartron and the Schlumberger Group, of which Solartron is the U.K. member. I hear that the French companies in the Group have now virtually completed a rationalisation programme in which what was once a rag-bag of smallish companies has now been consolidated into major groupings of considerable strength.

In Britain, Solartron's Farnborough plant was as busy as I'd ever seen it when I called in last month. The Master Series, a range of a dozen digital voltmeters launched earlier this year, was described to me as having made a major impact in the market place with revenues already ahead of schedule. But the big new field is in radio frequency instrumentation and Solartron will be offering equipment for use up to 40 GHz .

Another new Solartron activity is frequency synthesizers. This activity was previously concentrated in the Munich plant but now Farnborough engineers are involved in a joint development programme and new models will probably be manufactured in both locations.

Another bright product line is the realistic tank gunnery simulator known as "Simfire" for which Solartron recently won a Ministry contract worth $E 1.4$ million following successful field trials by the 15th/19th Hussars in Germany. The system uses a low-power pulsed laser beam to simulate the firing of the shell and its trajectory. The target is fitted with detectors and if a hit is detected it triggers off a pyrotechnic display on the "killed" vehicle.

Solartron is spending plenty of cash on $R$ and $D$ to bring themselves into a leading position in Europe. Most companies think themselves pretty progressive if they plough back 10 per cent into $R$ and $D$. The Solartron figure is currently running at 14 per cent on the instrument side of the business.

The biggest Schlumberger business, though, is still in oilfield instrumentation. Worldwide there are 30,000 employees operating in 50 countries.

## LES FOLIES

One of the brightest of the new generation of electronic industry entrepreneurs, Tom Jermyn, has a keen eye for the ladies, in a strictly business sense of course. His company, Jermyn Industries, manufactures semiconductor accessories such as i.c. sockets, transistor pads and heatsinks for which there is a world-wide sale.

Nearly three years ago he set up a sales office in Munich, soon to be followed by another in San Francisco and now he has opened his third in Paris. They all have one
thing in common-all are managed by ladies, and all of them good lookers.

Heading up the Paris office (appropriately located in the rue de Londres!) is multi-lingual Stella Bornstein who now joins Lore von Kleist, Munich, and Janice Pascoe, San Francisco. Stella is as yet untested, having only just started, but Janice and Lore have easily outpaced the performance of the local agents they replaced, Lore for example having built up the German business to 50 per cent of the present Jermyn U.K. turnover.

The point of this story is not so much the girls but how some of our more thrusting companies are getting around the world and really selling.

Incidentally, Jermyn is expanding manufacturing facilities bevond simple semiconductor accessories. Latest product is a 300 W triac-controlled light dimmer which fits neatly in place of the common square MK liạht switch. The dimmer, desianed bv Jermyn enaineers. is also available in kit form for home constructors.

## NEW LINE ON DEFENCE

Defence contracts may be getting harder to come by but they are still very big business. A new lineup of Thorn Automation, the Kelvin Hughes and Aviation divisions of Smiths Industries, and Scott and Electromotors, will be in a stronger position to bid for contracts under the group name Defence Equipment. Between them they employ 11,000 people and have combined assets of $£ 164$ million and a turnover of $£ 440$ million.

One reason for the link-up is said to be the reduction in size of Ministry R and D establishments and the farming out of work to the larger companies.

## IN TRIPLICATE

Despite all the trials and tribulations experienced during the commissioning of the new air traffic control system at West Drayton, Marconi Radar Systems has finally handed over the $£ 5$ million complex-after a year of operational trials. The triplicated MYRIAD computer systems operate independently to give a reliability such that the system is only out of action for less than thirty seconds in five years.

Another Marconi achievement was the $£ 1.5$ million system for Eurocontrol based at Bretigny, near Paris. This has now also been handed over. Marconi led the international consortium which included Standard Elektrik Lorenz of Germany, and S.A.I.T. Electronics of Belgium. Altogether Marconi has completed 38 major ATC installations in the last decade.

# ELECTRONORAMA 



Goonhilly 3, Britain's new £22 million satellite-communication aerial, is significantly different from the two earlier aerials at the Post Office's earth station on Goonhilly Downs. It is specifically intended for tracking satellites in geo-stationary orbit, whereas Goonhilly 1 was deslgned for tracking fast-moving satellites, and Goonhilly 2 for both sub-synchronous and synchronous orbiting satellites.

## REFLECTOR

The $29.6-\mathrm{m}$ diameter reflector of Aerial 3, although larger than those of aerials 1 and 2 ( 26 m and 27.4 m respectively) for improved performance, is considerably lighter, due to the use of 2 mm aluminium sheet for the reflecting surface, instead of stainless and mild steel. The sub-reflector can be tilted under the control of an hydraulic system to deflect the aerial beam by up to 25 minutes of arc in azimuth or elevation without moving the main reflector.

## DRIVE EQUIPMENT

Movement of the main reflector about each axis is effected by twin driving units each having two electric motors. Solid-state control devices are used instead of rotating machines as on aerials 1 and 2.

When the satellite starts to move out of the beam, error signals appear and activate the servo systems which steer the beam to eliminate the tracking error. Tracking can be accomplished by movement of the main reflector with the sub-reflector locked in a central position, or alternatively by movement of the sub-reflector


only
Goonhllly 3 is currently transmitting two and receiving 11 telephony carriers, although it is capable of being expanded ultimately to receive 33 carriers. The transmit carriers are radiated in the band 5.930 to 6.420 GHz and recelved in the 3.705 to 4.195 GHz band.

When required, Goonhilly 3 transmits and receives two television carriers, one for vision, the other for sound. It can also operate a transmit and receive contingency carrier arrangement to support services lost during failure of a transatlantic cable.

## RECEIVING SYSTEM

The received signals pass through flexible waveguide to one of a pair of low-noise parametric amplifiers, cooled to $15^{\circ} \mathrm{K}\left(-258^{\circ} \mathrm{C}\right)$ by a closed-cycle gaseous-helium cryogenic system (botlom left).

The signal from the LNAs, further amplified by 400 B in a tra-velling-wave-tube amplifier, passes by waveguide down the centre of the king post to a rotating waveguide joint, and is then carried in the waveguide to the central control building (boltom right).



The board to be described this month is the all important ADDER board which forms the heart of the arithmetic section of the calculator. The name ADDER is a shortened name for what is really an adder/subtractor with carry store, but before going into the design of the board in detail it is necessary to recall some of the principles of binary and B.C.D. addition and subtraction.

## BINARY ADDER

The principles involved in a simple single stage binary full-adder are fairly well known in this, the computer age, but for the sake of completeness it is as well to run over them again here.

Fig. 8.1. shows the logic diagram of a typical binary adder which generates a SUM and Carry output from the three inputs termed a, b, and Carry in. The word "typical" is quite meaningful in this connection because a circuit to perform binary addition can be made up in a number of different ways, the end result being the same, no matter which gating arrangement is used.

The performance of this sort of array is best described in terms of a truth-table which lists the circuit's output response to all possible input conditions, and the truth-table for the ADDER is also given in Fig. 8.1. If any reader is unfamiliar with the basic rules of binary addition, studying the truthtable will tell all.


Fig. 8.1. Single binary full adder stage. The truth table defines all the outputs for all combinations of inputs


Fig. 8.2. A parallel binary adder to add two four-bit words. Each of the stages in this adder is identical to that shown in Fig. 8.1

## PARALLEL BINARY ADDER

A binary adder stage like that of Fig. 8.1 is of limited use as it stands, being capable of adding together only a single pair of binary digits and a carry, whereas most sums a machine is asked to solve would stretch to a number of pairs of such digits. The simplest way to extend the capabilities of this circuit is to use a number together to form a parallel adder like the one in Fig. 8.2.

Each pair of binary digits in the two numbers to be added has its own adder circuit with the carry connected in series down the chain. This method of addition is widely used in binary computers but suffers from the disadvantages of large scale component use and slow propagation of the serial carry which has to "ripple-through" to the last stage before the addition is complete.

A circuit arrangement which only uses a single adder stage to add two n-bit numbers is quite possible if the addition is carried out sequentially, i.e. one pair of digits at a time, in a system such as that shown in Fig. 8.3. This method of binary addition is called "serial addition" and requires a store to "remember" the carry from a previous addition so that it may be added in with the next.
The two basic addition methods are both employed in Digi-Cal, with some special modifications to allow operation in the B.C.D. code.


Fig. 8.3. Basic serial binary adder/subtractor. The ADD/SUBTRACT unit presents either the true or complemented output from the $X$ REGISTER to the adder under the control of the FUNCTION CODE A signal

## SUBTRACTION

Once the truth table required of a binary subtractor has been worked out it is quite easy to design a simple logic circuit to perform the operations required, but in practice this is very seldom done, because, by making the number to be subtracted negative, i.e. by complementing it, it is possible to achieve the effect of subtraction in an adder circuit of the types already described.
The principles underlying this method of subtraction are quite straightforward and it can be readily appreciated that adding a negative number is the same as subtracting a positive one. Turning a positive binary number into a negative equivalent is simply achieved by inverting all its digits so that all the ones become zeros and vice versa, and then adding a one in the least significant position, for example

| binary three | 0011 |
| :--- | :--- |
| becomes | 1100 plus 1 |
| equals | 1101 |

To show that this process does generate a negative equivalent we can add the result to say binary four:
binary four 0100
plus binary thirteen 1101 (complement of binary three)

$$
\text { equals } \quad \overline{0001} \text { which is correct }
$$

Note that the carry digit from the most significant stage is disregarded, being only an indication of whether the result is positive (as in this case) or negative (if no carry results).

The operation of these principles in a practical circuit can be seen in Fig. 8.3 which is a serial adder system with subtraction carried out by simply feeding the inverted version of the x register output to the ADDER. and arranging for a carry to be preset into the store before the start of the clock pulse series.

## M.S.I. ADDERS

The TTL medium scale integration process has been used to produce several different binary adder circuits ranging from the very flexible SN7480 single, full adder to the compact SN7483 cricuit which contains four complete adders arranged as a four-bit parallel adder. It is this latter device which is used
in the 'Digi-Cal adder circuitry, where the four-bit length lends itself well to use with the binary coded decimal (B.C.D.) arithmetic process.

The SN7483 is used as a basic building block in the adder to be described and before venturing into the intricacies of B.C.D. addition and subtraction it is best to become familiar with its construction and operation in its intended role as a parallel binary arithmetic unit.

The equivalent logic circuit of the SN7483 is shown in Fig. 8.4 and comparison of this logic with Figs. 8.1 and 8.2 will show that this device is connected to add together two, four-bit binary numbers with a carry in to the first (least significant) stage. termed $C_{0}$, and a carry out from the final (most significant) stage termed $\mathrm{C}_{4}$.


Fig. 8.4. The internal logic of the SN7483 four bit binary adder i.c.

The two four-bit words to be added to indicate the termed A and B with a suffix I to 4 to indicate the significance of each bit. The carry circuit delays have been reduced as far as possible by internal connection, the use of high-speed type gating, and the elimination of unnecessary inversion circuitry, so that the addition time is kept below 100 ns .

## BINARY VERSUS B.C.D.

The numbers stored in the registers of Digi-Cal are represented by groups of four binary digits conforming to the Binary Coded Decimal (B.C.D.) code. This code is not complicated since it is identical to straight binary except that only the values 0 to 9 inclusive are allowed in each four-bit group instead of the values 0 to 15 .
With straight binary the word length can be any convenient value, depending on the quantities to be represented, each increment to the word length increasing the range of representable quantities by a factor of two.
In the B.C.D. system however the binary word length must not exceed four bits, and the value of each four-bit word must not exceed 9. Capacity is increased by adding extra four-bit B.C.D. words, each of which increases the range of representable quantities by a factor of ten. As an example of the contrast between the two systems:

$$
\begin{aligned}
& \left.\begin{array}{l}
0110 \\
1001 \quad \text { equals } 6 \\
01101001
\end{array}\right\} \text { in straight binary equals } 105 \\
& 0110,1001 \text { in B.C.D. equals } 69
\end{aligned}
$$



Fig. 8.5. Basic practical B.C.D. adder with a carry store flip-flop

The use of B.C.D. in calculators is desirable because of the simplicity in interfacing the logic with old fashioned human operators who insist on thinking in the decimal number system.

## B.C.D. ADDITION

When two four-bit B.C.D. words and a possible B.C.D. carry bit are added together in a parallel binary adder a total of 19 different (four-bit + carry) sums can be produced. Since the largest quantity representable in the B.C.D. code is 9. it is obvious that the nine most significant sums will require correction, and will be responsible for the generation of a B.C.D. carry bit. A moment's thought reveals that the correction required by sums from ten to 19 is the subtraction of ten, e.g.

7 plus 6 equals 13
subtract $\quad 10$
equals $\quad 3$ plus a carry to the next decade.
As we have seen already, the subtraction of ten is readily achieved by adding its complement, which is 0110 , or 6 if you prefer, and so the problem reduces to that of detecting sums in excess of nine so that the subtraction can be initiated.

The basic circuit of the B.C.D. adder used in DigiCal is shown in Fig. 8.5. Here the two B.C.D. words are added in ADDER $A$ in the conventional binary fashion, the detection for sums in excess of nine being performed by gates GI, 2, 3, and 4 . If any such sum is detected G4 feeds a carry to the carry-store
flip-flop and inserts 0110 into adDer b where it is added to the sum from adDer a.

The output from the second adder is the corrected versions of sums over nine, but if a carry is not required because the sum is less than or equal to nine, ADDER B passes the sum from ADDER a through to its output in an unmodified form due to the addition of 0000 instead of 0110 .

## CARRY DETECTION LOGIC

The performance of gates G1, 2, 3 and 4 in detecting sums in excess of nine can be taken for granted if the reader prefers, but for those who would like to know how the gating arrangement was arrived at, and who have some previous logic experience, the design was carried out as follows.
The carry out from adder a is a ready made indication that the sum is in excess of 15 , which reduces the problem to that of detecting sums of between 10 to 15 inclusive. To determine the gating required, the sums in question are plotted on a Karnaugh map, as shown in Fig. 8.6.

The Karnaugh map is just a special way of drawing a truth table to make it easy to see what gating will be required to generate a specific function. It has the property that where adjacencies occur in the plots, the particular value, or values which change between the plots can be eliminated from the resulting logic equation.
As can be seen in Fig. 8.6 there are two distinct groups of plots, 10, 11. 14. 15, and 12, 14, 15, 13. In the first group the terms $\Sigma_{1}$ and $\Sigma_{3}$ change, and can be eliminated. In the second group the terms $\Sigma_{1}$ and $\Sigma_{2}$ change, resulting in the required gating function of ( $\Sigma_{2}$ AND $\Sigma_{4}$ OR $\Sigma_{3}$ AND $\Sigma_{4}$ ) OR (Cout).

This function could be realised using two twoinput AND gates and a three-input or gate, but as the standard gating function of TTL is NAND it is possible to invert $C_{\text {out }}$ NAND $\Sigma_{2}$ and $\Sigma_{4}$ and $\Sigma_{3}$ and $\Sigma_{4}$, and feed these inverted functions to a further NaND gate which carries out the NOR function because of the inverted nature of its inputs.


Fig. 8.6. The Karnaugh map used to determine the gating required to detect the sums from 10 to 15 inclusive

## B.C.D. SUBTRACTION

The B.C.D. adDer just described cannot be used for subtraction as it stands, and the method of addition of complements is complicated by the fact that it is not the straight binary complement which is required, but the decimal complement which can be defined as 10 minus the number to be subtracted. In practice the generation of the "tens complement" causes problems with the carry logic, and it is preferable to generate the "nines complement" by subtracting from nine and then use the carry logic to add in a 1 .
The generation of the "nines complement" of the data from the $z$ Register requires the addition of the circuit shown in Fig. 8.7, which employs yet another SN 7483 quad adder.
The principle behind this "nines complementer" is that the binary complement of the input data is added to binary nine to produce nine minus $z$, but since the binary complement of a number is its inverted version plus 1 , in practice the circuit adds the inverted $z$ data to binary 10 thus taking care of the extra 1 required by the complement.

The inversion of the $z$ data is carried out in an SN7486 quad exclusive-or gate, which, when connected as shown, allows a true version of the input data through to the output when the common control input is a logic 0 , and an inverted version when the control is a logic 1 .

This useful property of exclusive-or gates, along with the fact that it is the control input which inserts the required 1010 into the adder, allows the "nines complementer" to either pass the $z$ data unmodified when FUNCTION CODE A is a logic 0 indicating an addition is required, or pass the "nines complement" of the $z$ data when the function code a line is a logic I indicating that subtraction is required.


Fig. 8.7. B.C.D. nines complementer. This generates the output 9 minus $Z$ when subtraction is required


Fig. 8.8. Complete circuit diagram of the ADDER board

The details of the subtraction process are quite hard to grasp at first but the process may be easier to understand after working through the following example (right).
Note that the borrow function which would be generated if the answer to a subtraction is negative is stored in the carry store in the opposite sense to that of a carry in addition, i.e. a 1 stored means no borrow, and vice versa.

## FULL CIRCUIT DIAGRAM

The complete circuit of the Digi-Cal adder/subtractor is shown in Fig. 8.8. This circuit is made up of a combination of the ADDER and COMPLEMENTER circuits already covered, with the addition of IC104 and gating for the Carry Store preset/CLEAR input.

| A Register data | 1000 | (equals 8) |
| :--- | ---: | :--- |
| B Register data | 0110 | (equals 6) |
| Carry store | 1 | No borrow from <br> previous subtraction |
| Function Code A | 1 | Subtraction |

## START ADDITION

Invert z data 1001
Add to $1010 \quad 0011$
Add to a data plus
carry input 1100
Add 0110
B.C.D. carry generated

Equals 2, the required answer

## COMPOLENIS . . .

## ADDER BOARD

Capacitors
C33 $10 \mu \mathrm{~F} 15 \mathrm{~V}$ elect.
C34 $0.047 \mu \mathrm{~F}$
Integrated Circuits
IC100 SN7486
IC101-IC103 SN7483 (3 off)
IC104 SN7408
IC105 SN7410
IC106 SN7400
IC107 SN7474
Printed Circuit Board
Type DL109/22 (Shirehall)
$1 \mathrm{ClO4}$ is an SN7408 quad AND gate which is connected as an a register data inhibit, requiring its common enable input to be a logic 1 before the a data is allowed through to the ADDER.

The purpose of this i.c. is to allow flexibility in the programming possibilities and, particularly, to inhibit data recirculation when the a REGISTER data is being normalised after a multiplication sequence.

The normalisation process was covered last month. and readers may recall that after multiplication, the A data are shifted to the right by the number of decimal places selected on the thumbwheel.

If the inhibit gates were not fitted the data which were to be discarded during normalisation would
recirculate and appear at the most significant end of the a register. The enable input is controlled by the programme.

The purpose of the gating in the Carry store preSET and Clear inputs is to allow for the fact that a BORROW is stored in the opposite sense to a CARRY, requiring the store to be preset before a subtraction, and cleared before an addition. Since there is a single Carry store clear signal from the programme, the FUNCTION CODE A input is used to control two, two-input nand gates which steer the Clear signal to the correct side of the Carry store flipflop.

The only other part of the circuit worthy of note is the CARRY SENSE output which is used to inform other parts of Digi-Cal of the state of the CARRY store, one of its uses being to stop subtractions when a borrow is produced after any tenth clock pulse during division, i.e. it senses when the A REGISTER contents are negative.

## CONSTRUCTION

The construction and wiring of the ADDER board is quite straightforward since the circuit is housed on the usual Dualine card, in this case a DL109/22.

On this board almost all of the connections are carrying high speed data signals which must have a high integrity, and for this reason it is necessary to keep wiring as short as possible to minimise problems caused by line reflection

The component layout and edge connector wiring is shown in Figs. 8.9 and 8.10

## ADDER BOARD



Fig. 8.9. Layout of the components on the DL109/22 printed circuit board


Fig. 8.10. Function of the edge contacts for the ADDER board

## TESTING

Checking out this board in isolation is relatively easy since it is possible to check the sum responses to various dummy control and data inputs. The data values can be inserted by wiring each of the four data lines from the separate sources to ground, or leaving them open circuit, to simulate a particular B.C.D. number.

Providing the enable and function code a lines are also properly activated, a B.C.D. answer should appear on the SUM outputs from IC103, and a CARRY/BORROW signal at the D input of IC107. The Carry store clear input can also be tested in combination with FUNCTION CODE $A$, monitoring the result at the Q or $\overline{\mathrm{Q}}$ output of the flip-flop.

Constructors who have followed the assembly sequence suggested will also be able to try the first complete calculations on their machine by judicious application of dummy control signals which would normally emanate from the programme.

Numbers entered into the ENTRY REGISTER can be transferred to the $z$ REGISTER by operation of the (cleared) a REGISTER by momentarily grounding the start clock input to board cb. This process requires a large number of temporary control signals to be wired in, and may be daunting to some readers: the prospect has been suggested only to enable the more adventurous to experiment with the way the programme board (to be described next month) will be required to carry out the process of addition and subtraction automatically. Those who do attempt this type of test will learn a great deal about the intimate workings of Digi-Cal.

Note: In Part 4 (Oct. 72), Fig. 4.2, C13 on IC21 should be marked C9, and C8 should be $10 \mu \mathrm{~F}$ not $22 \mu \mathrm{~F}$

## COMPUTER '72

Taking both the Grand and National Halls at Olympia. the COMPUTER 72 exhibition (December 4 to 8) attracted over 200 international companies who had data processing services to offer. The organisers of this show, the Business Equipment Trade Association. described its purpose as "explaining the benefits of electronic data processing to commercial and industrial management". thus the exhibition presented services rather than the actual hardware itself, though peripherals were much in evidence.

One of the most attractive stands was that of the Post Office. The display was a symbolic representation of their Datel services in multicoloured plastics. with some exhibits showing data transmission techniques of the past.

On the hardware side. Hewlett-Packard presented their new minicomputer. Model 30. This computer is no larger than a good sized teletype terminal and provides an economical alternative to time-sharing, operating in BASIC. the language most used for time-shared systems. It has an internal cassette store with a capacity of 24.000 numbers. Its readout is via an 80 character alphanumeric display, though a printer is an optional extra.

As well as the main exhibition some light relief was provided by Honeywell who presented the winning entries to the Observer Colour Magazine children's "Paint-a-Computer" competition. Also on display was the Honeywell/Roland Emett forget-me-not computer. On the NCR stand a simulated game of cricket was being played through one of their computers and results were presented as the "game" progressed.

The bringing together of a large nuumber of companies in this way is obviously a great service to management and the success of this and future shows is assured.

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NON-IPACT printer capable of writing 1,000 lines per minute is being developed by R.C.A. for the U.S. Army. The new printer uses a laser to transfer digital communications alphanumerics onto ordinary paper.

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Through its data interface the MTR can receive any type of digital signal from a wide variety of sources including satellite ground terminals. It can receive this information at the rate of 20,000 words per minute.

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## 5 OPERATIONAL AMPLIFIERS WITH POWER STAGES

SOME instrumentation or audio applications may require a greater output current capability than that provided by an integrated circuit on its own. The simplest way to achieve this is to include an emitter follower inside the feedback loop, as in Fig. 5.1.

Since the output is compared with the input the effect of the 0.7 volts base-emitter bias voltage is reduced by the feedback. If the input is zero then the output of the integrated circuit will be 0.7 volts, allowing the output of the arrangement to remain at zero, as shown in the diagram. Short circuit protection can be given by R3 and the gain is determined by R1 and R2 in the usual way.

Since this is a class-A circuit it is not suitable where load currents of hundreds of milliamps are required, and other booster circuits must be designed on the lines of class-B audio power stages. A straightforward class-B output stage is shown in Fig. 5.2.

## UNITY GAIN OUTPUT PAIR

When load currents of several amps are needed a higher current gain output stage is required; one possible combination for one half of an output stage is shown in Fig. 5.3. It has several advantages, including good d.c. stability, and consists of two common emitter stages with 100 per cent negative feedback from the collector of the power transistor to the emitter of the driver transistor. This gives an overall voltage gain of unity and a high current gain.

For a positive going signal TR1 conducts, increasing the drive to TR2 which also conducts. Hence both transistors operate in class-B, apart from a small quiescent current.

For a collector current of 30 mA it was found that a typical silicon power transistor required a baseemitter bias voltage of 0.56 V . This seems lower than might be expected for a silicon transistor until we remember that 30 mA is a small part of the 5 A or so to which a power transistor can be driven.
(Indeed it is the range of currents over which a power stage has to be driven that causes many of the problems associated with this area).


Fig. 5.1. An operational amplifier with a class-A emitter follower output


Fig. 5.2. An operational amplifier with a class-B output stage


Fig. 5.3. One section of a class-B, unity gain, high current, output stage

The base-emitter voltage of the driver transistor was 0.65 V for a 5 m A collector current, and this becomes the input bias voltage required under quiescent conditions. For the other combination of a pnp driver and an npn power transistor the bias was 0.71 V , and these values are typical.

## PRECAUTIONS IN MEASURING CURRENTS

The quiescent current of the output transistor can only be measured in its collector lead if the d.c. conditions are not to be disturbed. Alternatively,
the change in total supply current can be measured as the bias resistor is increased and the power transistor conducts.

Great care should be taken in making such tests because one careless move could result in a damaged meter or a heavy current through the transistors. A current limited power supply provides an extra measure of safety.

## 30 WATT POWER AMPLIFIER

If the unity gain power stage previously discussed is used, then the maximum output swing is limited to about 20 V peak-to-peak from the integrated circuit. This would provide up to 5 watts into 8 ohms. Where more power is required the output stage can be modified to provide a small gain, five times is enough.

A complete power amplifier circuit is shown in Fig. 5.4. The required voltage gain is provided by the integrated circuit, supplemented by the output stage, while current gain is provided by the class-B output stage. The small signal driver transistor and the potentiometer allows the quiescent current to be set.

With the potentiometer at maximum resistance the transistor is bottomed and no current flows in the output stage. As the slider is brought towards minimum resistance the transistor takes less current and the collector current of the ouput transistors can be set to (say) 50 mA .
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load allows a good low frequency response without using a large coupling capacitor. However, it could be argued that we have moved it back to the supply to obtain the centre tap.

The a.c. feedback sets the gain to 26 times or 28 dB . If the BC184 transistor is mounted on the same heat sink as the power transistors, it will tend to compensate for variations in quiescent current if they become warmer. The 330 ohm resistors limit the maximum drive if the load is accidentally shorted. When used as shown in the diagram the BC184 can be considered simply as a low value impedance.

Since in these circuits the power stages appear inside the feedback loop, extra care must be taken with frequency compensation to achieve closed loop stability. Measurements on a prototype show that distortion should be better than 0.2 per cent at 30 watts at 1 kHz .

## CONSTRUCTION

It is essential that the $10 \mu \mathrm{~F}$ capacitor is a low leakage tantalum type because if a leakage current flows through this component there will be a d.c. offset at the output which could cause a quiescent current to flow in the load.

The output offset voltage could be measured before the load is connected, or if a small d.c. current flows through the load as it is connected, this would be indicated by an unbalance in the current drawn from each supply. The offset should be small, less than 10 mV . Each power transistor should be mounted on a heat sink of thermal resistance $2 \cdot 8^{\circ} \mathrm{C} /$ watt or better. Each driver transistor should also have a small heat sink.

## CONCLUSIONS

The final circuit given for a 30 watt power amplifier should be regarded as experimental because it has not been fully toleranced as regards transistor and integrated circuit variations. Some adjustment might be necessary for the 10 pF capacitor in order to obtain the best possible square wave at 10 kHz . For instrumentation applications the circuit can easily be direct coupled so that its response extends down to d.c.

## Part 6 will look at basic memory circuits



SEMICONDUCTOR DIODE LASERS
By R. W. Campbell and F. M. Mims
Published by Foulsham.Sams
192 pages, 9 in $\times 5 \frac{1}{2}$ in. Price $£ 1.90$

O'ptoelectronics is a field which is attracting a great deal of attention at the present time but semiconductor diode lasers are still very much in the development stage. Though the large manufacturers are producing them it appears that the price is still a prohibitive factor in their widespread use. One of the authors points out that "laser specifications of recent years should generally be reasonably accurate" showing that even the manufacturers are still not totally confident in the devices.

This new book originating in America (but with the usual Foulsham-Sams introduction for English readers) is thus directed more towards the researcher and experimenter than the constructor.

The opening chapters give a description of the development of the laser diode with a description of light generation processes in both lasers and ordinary light emitting diodes (l.e.d.s). For those who have not met semiconductor lasers before, they differ from 1.e.d.s in that they emit coherent light in an intense beam. The structure of lasers is different from 1.e.d.s and they are usually used in the pulsed mode. mode.

Probably the main interest in the book will be in the practical laser diode driving circuits. Perhaps the most interesting design is of a laser transmitter and receiver using pulse frequency modulation which can be used for voice communication at up to $3 \frac{1}{2}$ miles range. Of course, sophisticated optics are needed to achieve such a range and this side of the design is not neglected.
For the interested amateur or the researcher this book provides an excellent introduction to semiconductor lasers and the techniques needed to use them.
S.R.L.

## SEMICONDUCTOR DATA HANDBOOK

Published by the General Electric Company, U.S.A. $\mathbf{1 , 5 3 8}$ pages, $8 \frac{1}{2} \mathrm{in} \times 10 \frac{1}{2} \mathrm{in}$. Price $\mathbf{E 2 \cdot 3 0}$.

THIS massive 1.538 page handbook embraces the full range of semiconductor devices manufactured by the General Electric Company. It contains data sheets, circuits application tips and hints, equivalent and device selector guides and indexes to application notes and technical publications.

Devices covered include silicon and germanium transistors from small signal to power types; signal and tunnel diodes and power rectifiers; unijunction switches and triggers; s.c.r.s and triacs; optoelectronic devices; voltage regulators, differential and Darlington amplifiers; selenium components; transistor and diode chips; military and high reliability types and associated mounting hardware.

The Semiconductor Data Handbook can be obtained from Jermyn Distribution, Vestry Estate, Sevenoaks, Kent.

# PNTENTE 

Ele:CTRONIC METRONOME

In BP 1280117 Andre Paquet of France details a simple but probably reliable electronic metronome for producing synchronised sound and light signals.
In his circuit (see Fig. 1) the inventor uses a bi-stable multivibrator which can be switched from one of its states to the other by a time constant circuit R1, VR1, C1. In fairly conventional manner the capacitor C1 is charged via R1, VR1 to a voltage $V$ (defined by R3 and R4) at which TR1 and TR2 transistors conduct. In this state the capacitor C 1 discharges and a negative pulse is passed via C 2 to the multivibrator. There follows a change of state of the multivibrator which energises the coil L1 and the lamp LP1 and the coil L2 and the lamp LP2 alternately in a "flip-flop" manner.

In one design the coils attract cores which strike a metal plate to produce a sound output. In another design, a sound output is produced by a loudspeaker connected in series with a thyristor controlled by an RC circuit.

Regulation of the rance of frequency to be covered is by adjustment of the frequency control VR1. The other adjustment is of the absolute value of the frequency at a predetermined point on the potentiometer-usually this is the minimum frequency required.

The main advantage claimed is that as the value of a potential $U$ on the base of TR1 is defined with respect to $V$ by $\frac{R 4}{R 3+R 4}$ the period $P$ between switching operations will depend only on the slope of the exponential of the charging
curve of the capacitor C1, i.e. on (R1 + VR1) $\times$ C1, which is adjustable, of course, by means of the potentiometer.

Thus (discounting leakage currents) the frequency of switching of the multivibrator is independent of the voltage of the power source and thus the metronome will not speed up or slow down according to battery condition.

## COUVTING STACKED ARTICLES

WHEN flat articles such as envelopes, paper sheets or packages are stacked, counting them can be extremely difficult. The main problem is that very low contrast gradients exist between adjacent stacked articles and so photoelectric sensing devices produce such poor signal-to-noise ratios that the final count is hopelessly unreliable.

One way round the problem is simply to weigh the stack and another proposal has been to enhance the signal from the photoelectric sensors by some means, such as a high pass filter. But so far (at least according to Spar. tanics Limited, of llinois, USA, in BP 1 280 311) the overall results have been poor.

In this new British patent Spartanics suggest counting the discontinuities between adjacent stacked articles by an array of sensors having an effective thickness less than that of the stacked articles.

The sensors are photoelectric and (see Fig. 1) an area of the stack of articles is illuminated by means of a lens focusing light from a d.c. source. The axis of illumination ( $x 1$ ) is adjustable so as to give the maximum contrast possible at the article edges. A pair of cross coupled photoelectric

## BP 1280117

Fig. 1


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RADIO COMP SPEClilis



A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.
This is YOUR page and any idea published will be awarded payment according to its merits.

## SOUND/LIGHT MODULATOR

READERS may be interested in my version of a sound/light modulator shown in Fig. 1. It is entirely adjustable and works out to be very cheap compared with other modulators which incorporate frequency band splitters and sync pulse generators.

Sensitivity is controlled by VR1, and resistor R1 is to protect the transistor in the instance of the bulb filament shorting. The value of RI was 100s? rated at $\frac{1}{2}$ watt which can be lowered depending on the bulb used. A 6 V 0.06 A or 0.1 A bulb can be used quite satisfactorily.


Fig. 1. Circuit diagram of the sound/light modulator. The value of R2 was found to vary between 15 to 27 kilohms according to the load

If a microphone is to be used it should be of the carbon type and connected in the circuit as shown (dotted) in Fig. 1

If the circuit is to be built in a cabinet or case the lamp should be positioned approximately $\frac{1}{2}$ in away from the l.d.r. (ORPI2).

For a load greater than 500W the handling current of the thyristor should be increased. The potentiometer VR2 controls the brilliance of lamp LP2.

This circuit is open to a great deal of experiment, for instance three circuits could be built with the potentiometer in each adjusted to different stages to make a three channel unit.
The input is completely isolated from the mains. C. Walker,

London, S.W. 9

## TOUCH SWITCH

THE circuit in Fig. 1 detects voltage changes caused by the proximity of the hand on a sensitive plate or contact, causing a relay to operate. The characteristics of the circuit may be tailored to a particular application by choice of component values.

Typical component values are shown in Fig. 1. The transistors and diodes are general purpose silicon types. The relay coil resistance should be about 700 ohms to 1.5 kilohms, and the supply should be easily capable of operating the relay but not exceeding 25 V .

Resistor R1 may be decreased to about 2.7 megohms if the circuit is required to operate only when contact is made to the input by one's fingers. Conversely, as a proximity detector the value of the resistance may be increased.

If the battery drain is an important factor, the resistor R2 may be increased so that the quiescent current is only a few microamps. Sensitivity may be increased by reducing the value of $R 2$. If the sensitivity is increased too much the relay will remain permanently operated.

If the circuit is required to remain operated for some time after triggering, the value of Cl may be increased. The delay before the relay releases is
about one second per microfarad. As the capacitor is charged up through R2, it may be necessary to reduce the value of $R 2$ to give speedy operation.

The circuit may be used in a wide variety of applications such as burglar alarms, doorbells, practical jokes, and is particularly useful for switches which have to be found in the dark.
P. K. Webb,

Malvern, Worcs.


Fig. 1. Circuit diagram of a simple proximity switch
ltems mentioned in this feature are usually available from electronic equipment and com ponent retailers advertising in this magazine However, where a full address is given enquiries and orders should then be made direct the firm concerned.

## CATALOGUES

It is at this time of the year that we take stock of all of our component catalogues and usually receive all the new editions. Judging by the amount of catalogues we have already, received and those acquired during the past year it seems a good time to mention just some of the many excellent catalogues in our files.

It seems that as more and more components are becoming available generally, particularly the more specialised types, as electronic tech niques forge ahead so we are receiving a greater number of catalogues and firms are tending to specialise in particular fields.

Typical of this trend is LST Components who, through the component explosion, have found it increasingly difficult to maintain their excellent personal service to both the home constructor and the trade. Not wanting to lower their high standards they recently formed a new company called Arrow Electronics Ltd., to deal exclusively with the home consumer market. The parent company is now dealing with the trade only.

The new company have recently issued an excellent catalogue containing items from i.c.'s to switches. Copies of the catalogue can be obtained from Arrow Electronics Ltd., 7 Coptfold Road, Brentwood. Essex.
Another firm who tends to specialise. in this case in integrated circuits. is Bywood Electronics. Their catalogue lists such items as a Digital Clock Chip, LSI Calculator i.c.'s and several LED devices (including liquid crystal types).

The Bywood catalogue is available from Bywood Electronics, 181 Ebberns Road. Hemel Hempstead. Hertfordshire.

From the other side of the coin GSPK (Sales) Ltd., who are well known trade distributors, have recognised the vast demands for components from the consumer side and have set up a special retail counter at their office. Also, they issue a very good mail order catalogue and are offering a great many
of their components which are not normally available to the constructor, unless ordered in large quantities, on a one-off basis.
Copies are available from GSPK (Sales) Ltd., Hookstone Park, Harrogate. Yorkshire.
A catalogue we strongly recommend to our readers is the Audio Pack Trade Reference Catalogue from Tape Recorder Spares Ltd. This catalogue costs 35 p , including postage. and covers over 600 items marketed under the name of "Audio Pack".
The catalogue seems to cover practically every conceivable arrangement for connecting up audio equipment. A special section is devoted to Garrard spares.
This catalogue is certainly an excellent audio spares reference source and should be very near the top of any "Catalogues Wanted" list. Copies are available from Tape Recorder Spares Ltd., 206-210 Ilderton Road, London SE15 INS.

Finally, as proof of the component growth Home Radio Components have had to completely change the format of their catalogue.

The new 240 -page catalogue contains over 8,000 items, 1,500 illustrations and still maintains the usual high standards of previous editions. The cost of the catalogue is 75 p , including postage, but contains 10 redeemable vouchers worth 5 p each when used as directed.

Included with the catalogue is a price supplement which will be updated from time to time and each page will have the date stamped on it. At the bottom of the price supplement is a note to the effect that "when the supplement is six months old 10 per cent should be added to any item purchased and a new supplement be requested". Upon investigation it was pointed out that this was to avoid any unnecessary delay in dispatching of orders. Any difference between the remittance and the current price of goods ordered will be returned as a credit note with the option of a cash refund.

The Home Radio catalogue is probably one of the most useful reference sources for components on the market and copies can be obtained from Home Radio (Components) Ltd., 240 London Road. Mitcham. Surrey CR 4 3HD.

## SYNTHESISER MODULES

Commencing in this issue is the first part of the P.E. Synthesiser which we are sure will generate tremendous interest amongst our readers. This synthesiser will be described in great detail over the next few months and each circuit function will be described and complete constructional details given.
For those readers who do not wish to understand or construct


Two of the Dewtron synthesiser modules from D.E.W. Ltd.
each individual circuit as the series progresses but prefer to connect up "black boxes" (modules) then the Dewtron Project X Synthesiser modules from D.E.W. Lid., may be worth looking into.
The Project X modules are completely sealed units which have a two year guarantee against failure and their range includes a voltage controlled oscillator, sample, hold and envelope shaper unit and a ring modulator module. The Project X Synthesiser is in NO way connected with the P.E. Synthesiser.

A list of modules and other musical effects units with prices are available from D.E.W. Ltd.. 254 Ringwood Road. Ferndown, Dorset.

## SLIDER CONTROLS

Whilst on the subject of effects units we often get requests for the slider type of controls which are used extensively in effects units. To, date, these type of controls have been difficult for the home constructor to obtain and a compromise has had to be made by using standard rotary potentiometers.

A range of slider potentiometers is now available direct from DJ Electronics (Hackney) Ltd. or from most component retailers. The sliders, complete with knob and fixing screws, are available as single or double gang types in both logarithmic and linear configurations.

A range of mounting plates are available separately and enable the constructor to make up numerous configurations. The plates are offered as single-way, double or triple-way.

The cost of the sliders are expected to be 6lp for single gang types; and 81p for double gang. The mounting plates will cost 25 p for single-way, $36 p$ for double-way and 45p for three-way.

Addresses of nearest stockists can be obtained from DJ Electronics (Hackney) Ltd., 122 Balls Pond Road. London. N1 4AE.


Slider control from DJ Electronics


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MICROPHONE MIXER (Apr. 69)-S/c's, Rs, Cs, Pots. $\mathbf{C 2} 20$. Slider Pots and Knobs extra, $11 \cdot 15$. PCB ( 34 in $\times 44$ in)-holds pocs, 6120
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Finds exposure, controls ciming, stabilises mains voltage.
S/c's, SCR, LDR, Rs Cs, Pots. Relay Sw, T/former, 67.60 .
$\mathrm{S} / \mathrm{c}$ 's, SCR, LDR, Rs, Cs, Pots, Relay, Sw, T/former, 6760 . PCB ( $3 \frac{1}{2}$ in $\times \mathrm{S} \frac{\mathrm{t}}{\mathrm{in}}$ ) also holds pots, relay, Keyswitch, $\mathbf{1 1} 20$.
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## SOME OTHER DESIGNS AVAILABLE

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 (St MW
C. 2.7W STEREO AMPLIFIER (Radio Constructor July 71 )

Rs, Cs, Pots. I.C's complete with heatsinks, 67.50 . PCB (4tin $\times 5$ in) -1
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## YOU MUST HEAR

## miniWISE audiLECT YOUR PERSONAL TUTOR

Get PLEASURE from your CAREER or HOBBY through ORGANISED TUITION. YOUR PERSONAL TUTOR will give you rapid UNDERSTANDING-the key to SUCCESS in your own HOME and at your own SPEED Your FUTURE in RADIO, TV or ELEC. TRONICS could EASILY be much BRIGHTER. FOR DETAILS OF THIS UNIQUE METHOD just send us your name and address MINIWISE PRODUCTS
FREEPOST (P), BLETCHLEY, BUCKS.
INCLUDE ONLY £ $1 \cdot 20$ TO OWN A TRIAL LESSON* on a C90 cassette or L.P. Tape (state which)

* Your money INSTANTLY REFUNDABLE if not $100 \%$ convinced that this can be the turning point in your hobby or career


## the natural way to learn



| INPUT 230/240Y a.c. 50/60 OUTPUT |  |
| :---: | :---: |
| VARIABLE 0 | 260 V |
| All Typas |  |
| from to 50 mm | np from stock. |
| SHROUDED TYPE |  |
| 1 amp [ 7.00 | $20 \mathrm{amp}, 649.00$ |
| $2.5 \mathrm{mmp}, 18.05$ | 25 a mp, $¢ 58.00$ |
| $5 \mathrm{amp}, 611.75$ | $37.5 \mathrm{mmp}, 682.00$ |
| 10 amp, 622.50 | $50 \mathrm{amp}, \mathbf{8 8 . 0 0}$ |
| $15 \mathrm{mmp}, 625.00$ |  |

Panel Mounting) $\frac{1}{2}$ amp, $\mathbf{4 . 7 5}$. OPEN TYPE DOUBLE ENDED BLOWER UNIT Powerful, continuously rated, 2 -speed.
Blades easily removable. Either 6 or
$\mathbf{1 2}$ volt D.C. opperation. PRICE
\&1.75. P. \& P. 25p.
12 VOLT D.C. MOTOR
Powerful I amp. REVERSIBLE motor. Speed 3,750 r.p.m. removable) giving approx. final speed of ither 125 r.p.m. or 240 r.p.m. Size: $4 \frac{1}{4}$ in

ONSTANT SPEED, PRECISION MADE ${ }^{6}$
750 pole armature, ballrace bearing 2,750 r.p.m. Length 2 it, Dia. Hi , Shaft ength is load 350 mA . Ideal for portable REVERSIBLE SPLIT PHASE MOTOR 250 r.p.m., $100-115 / 210-240 \mathrm{~V}$ A.C., 2 in . $\times$ lin. 1deal powerful for size, including small capacitor. 75p
post paid.
PARVALUX TYPE SD19 $230 / 250$ VOLT A.C REVERSIBLE GEARED MOTORS Position of drive spindle adjustable to 3 differ ubstantial cast alum ment. Tested and in first-class running order A really powerful motor maker's price. $£ 6 \cdot 30$. P. \&


PARVALUX Type: SDI.S
86896/OJ
$230 / 250 \mathrm{~V}$ A.C. 50 r.p.m. $7 \mathrm{lb} /$ in. Continuously rated. TYPE: SDI.S/89400/OM
 $30 / 250$ A.C. 50 r.p.m. $22 \mathrm{fb} / \mathrm{in}$ The above motors are new and unused.
PARVALUX TYPE SD2. 200/250 VOLT A.C./D.C. HIGH SPEED MOTOR Speed 9,000 r.p.m. approx. or 3,200 variable speed over a wide range used in conjunction with ou Dimmer Switch, illustrate
PRICE \&1.75. P. \& P. 25D.
600 WATT DIMMER SWITCH.
Easily fitted. Fully guaranteed by
makers. Will control up to 600 W of ali
lights except fluorescent at mains
voltage. Complete with simple in-
structions. E3 incl. P. \& P.

## 24-HOUR TIMER

Can be adjusted to give a switching delay of berween $\frac{1}{t} \mathrm{hr}$. to 24 hrs .
Driven by $200 / 250 \mathrm{~V}$. C . synchronous notor. $15 \mathrm{amp} \mathrm{s} / \mathrm{o}$ contacts. Mfg. C Led. Supplied with scale calibrated $0-10$ (2 hrs
per division). Brand New. \&i.75. P. \& P. 25p.
HONEYWELL PROGRAMME TIMERS
240V. A.C. S r.p.m. mocor Each cam operating a c/o ing inumerable combinations Ideally suited for machinery ontrol, automation, erc. Also in the field of entertain ment, for chaser lights
15 cam model 65.75
5 cam model $\mathbf{6 5 . 7 5}+\mathbf{2 5}$ p. P. \& $P$
2 cam model with 15 r.p.m. motor $£ 1.75+25 p$ SIMPLE 12 CAM PROGRAMMER with 4 adjustable cams and 8 that may be profiled to All Mail Orders-Callirs-Ample Parking
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CHISWICK, LONDON W4 5BB Phone 01-995 1560

36V 30 AMP. A.C. or D.C VARIABLE L.T. SUPPLY UNIT INPUT 220/240V A.E. VARIABLE 0-36
Fully isolated. Firted in robust metal case with Volt meter. Ammeter Panel Indicator and handles
Lab. or Industrial use. E6B plus $E 2$ P. \& P
MOTOROLA MAC $11 / 5$ PLASTIC Now available EX STOCK Supolied and applications

STROBE! STROBE! STROBE!
Build a Strobe Unit, using the latest type Xenon
white light fiash tube. Solid state timing and EXPERIMENTERS' ECONOMYY ORET
Sp Speed adjustable I to 30 flash per sec. All S.C.R. Unijunction Xenon Tube and inseructions 66.30 , plus 25 p P. \& P

NEW INDUSTRIAL KIT
Ideally suitable for schools, laboratories, etc Roller sin princed circuit. New trigger coil approx. 1 output of Hy -Lygh
Price f 10.50 P. \& P. 50 p .
HY-LYGHT STROBE MK III
Designed and produced for use in large rooms halls and the photographic field and utilises coil. Speed adjustable $0-20$ f.p.s. Light ourput approx. greater than many (so called 4 Joule Strobes.
THE 'SUPER' HY-LYGHT KIT proven Hy-Lyghtes trobe light output of our well - Heavy duty power supply - Variable speed from I-13 flash per sec. Reactor control circuit producing an intense ever before a Strobe Kit with so HIGH an output at so LOW a price.
ATTRACTIVE, ROBUST, FULLY VENTI LATED METAL CASE specially designed for the Super Hy-Lyght Kit including reflecto
$£ 7.00 \mathrm{P}$. \& P. 45 p . For Hy-lyght Kitincluding reflector. ©4.00. Finch POLISHED REFLECTOR Ideally suited for above Strobe kits. Price 53p.


RAINBOW STROBEFOUR LIGHT CONTROL MODULE
ofrer a mains operated fully isolated short variable flash rate. It will operate four of our Hy-Lyght or Super Hy-Lyght Serobes in either 1, 2, 3, 4 sequence; $2+2$; or all together filters. Modules can be connected together to operate 8 or 12 Strobes. Will work on long runs of up to 50 yards, so that your Strobes of module is $5 \times 6$ for maximum effect. Size your own equipment, or into a separate case. Thoroughly tested and reliable. Complete with full connection instructions. Price:

Complete with oil
filled colour wheel.
100 watc lamp. 200 /
240 V AC. Features
fical system. $f 18.50+$
COLOUR WHEEL


BIG BLACK LIGHT
400Wars. Mercury vapour designed to absor Exight and transmit powerful source of Innumerable industrial applieations also ideal for stage,
display, discos, etc PF ballas display, discos, etc. P.F. ballast is essential with these bulbs.
Price of matched ballast and Price of matched ballast and Spare bulb \&7.00, P. \& P. 30p BLACK FLUORESCENT U.V. TUBES
$\qquad$

Superior Quality Precision Made NEW POWER RHEOSTATS

## 100 WATT. I ohm, 10A; 5 ohm

 4.7A; 10 ohm, 3A; 25 ohm, 2A $500 \mathrm{hm}, 1.4 A_{i} 100 \mathrm{ohm}_{1} 1 \mathrm{~A}$ 250 ohm, $7 \mathrm{AA}, 500$ ohm, $0.45 \mathrm{~A} ; 1 \mathrm{k0} 290 \mathrm{~mA}$ $5 \mathrm{kn}, 230 \mathrm{~mA} ; 2.5 \mathrm{~kg}, 2 \mathrm{~A} ; 3.5 \mathrm{k} \Omega, 5 \mathrm{~kg}, 140 \mathrm{~mA}$ Diameter 3tin Shaft teneth tin, dia. 数in. All a 50 WATT. 1/5/10/25/50/100/250/500/1/1.5/2.5/5kn All at \&1.15 azch. P. \& P. 7tD25 WATT. $10 / 25 / 50 / 100 / 250 / 300 / 500 / 1 / 1 / 5 / 2 \cdot 5 / 3 \cdot 5$ kn. All at 90p each. P. \& P. 7tp
Black Silver Skirted knob calibrated in Nos. 1.9
RELAYS SIEMENS, PLESSEY, Etc. MINIATURE RELAYS Col.(1)

Col. (2) Working
d.c. volts

Col.
Contracts
Col. (4)
Price
HD= Heavy duty Post paid.

| 52 | $3-6$ | $2 \mathrm{c} / \mathrm{o}$ |
| :---: | :---: | :---: |
| 410 | 10-18 | $4 \mathrm{c} / \mathrm{o}$ |
| 600 | 12-24 | $4 \mathrm{c} / \mathrm{o}$ |
| 700 | 16-24 | 4M2B |
| 700 | 16-24 | $4 \mathrm{c} / \mathrm{o}$ |
| 700 | 15-35 | $2 \mathrm{c} / \mathrm{OHD}$ |
| 700 | 16-24 | 6M |
| 700 | 6-12 | $1 \mathrm{c} / \mathrm{oHD}$ |
| 700 | 20-30 | $6 \mathrm{c} / \mathrm{O}$ |
| 1,250 | 24.36 | $4 \mathrm{c} / \mathrm{o}$ |
| 2,500 | $36-45$ | 6M |
| 2,400 | 30-48 | $4 \mathrm{c} / \mathrm{o}$ |
| 9,000 | 40-70 | $2 \mathrm{c} / 0$ |
| 15k | 85-110 | 6 M | 63p*

$73 p^{*}$
$78 p^{*}$
$63 p^{*}$
$78 p^{*}$
$73 p^{*}$
$65 p^{*}$
$50 p^{*}$
$75 p^{*}$
$63 p^{*}$
$63 p^{*}$
$50 p^{*}$
$50 p^{*}$
$50 p^{*}$
12 VOLT D.C. RELAY 140 ohm coil
Type 1 : Three sets e/o contacts rated at 5 amps. 78p Type 2 : One set of clo contacts 60 p incl $P$. Type 3: 4-8 volt, 3 c/o HD, 67 ohm coil. 78 p DIAMOND H' 2

## RELAYS (Unused)

PRICE: 50p. P. \& P. 10p. ( 100 lot 40 including P. \& P.
230 YOLT A.C. RELAYS MFG. KEY SWITCH One set c/o contacts rated at 7.5 amps. Bored MINIATURELATCHING RELAY Manufactured by Clare-Elliotr Ltd. Type F. 2 c/o per manent latching in either direction. Coil 1150 ohm


UNISELECTOR SWITCHES
NEW

"HONEYWELL" PUSH BUTTON, PANEL MOUNTING MICRO SWITCH ASSEMBLY 10 amps 240 V . A. C. Black knob lin fixing hole in. ONE bank 30p; \& ${ }^{40 \mathrm{P} \text {. Quot. }}$

HONEYWELL' LEVER OPERATED
MICRO SWITCH
cacts. Types N39, N95, N100,
PRICE: 10 for $\mathbb{E} 1-90$ incl. P. \& P.


## INSULATION TESTERS NEW!

 Test to liE.E. Spec. Rugged metalconstruction, suitable for bench or field work. constant speed clurch. Size L.8in, W. 4 in, H.6in, weight 61 b .
l,000V, 1.000 megohms, $E 34.00$ carriage paid.
$500 \mathrm{~V}, 500$ megohms, $\mathbf{6} 28$ incl. P. \& P


50 in I ELECTRONIC PROJECT KIT 50 easy to build Projects. No soldering, no Meter, Relay. Transformer. plus a host of othe components and a $56-p a g e$ instruction leaflet Sound Level Meter, 2 Transistor Radio, Amplifier

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## TRANSFORMERS

all with 0-250
MM6 6V, $500 \mathrm{~mA}+6 \mathrm{~V}, 500 \mathrm{~mA}$ MM12 $12 \mathrm{~V}, 250 \mathrm{~mA}+12 \mathrm{~V}, 250 \mathrm{~mA}$ MM20 $20 \mathrm{~V}, 150 \mathrm{~mA}+20 \mathrm{~V}$, 150 mA
L.T. 1.29 plus 13p p. \& P .

LT1 $6.3 \mathrm{~V}, 1.5 \mathrm{~A}-75 \mathrm{p}$ plus 18 pp . \& $p$. LT2 $6.3 \mathrm{~V}, 3 \mathrm{~A}-87 \mathrm{p}$ plus $26 \mathrm{p} p$. \& $p$.
LT3 $12 \mathrm{~V}, 1.5 \mathrm{~A}-87 \mathrm{p}$ plus 26 p p. \& p . LT4 12 V , 3A- El 1.32 plus 30 p LTS 9-0-9V, 0.5A-75p plus 21p LT6 12-0-12V, IA-95p plus 26p Multi-tapped

MT30/2 0-12-15-20-24-30V, 2A| MT60/1 | (1.95 plus 30p p. \& F p. |
| :--- | :--- |
| 20-30-40-60V, IA- |  | MT60/2 0-5-20-30-40-60V, 2ACharger $\quad \mathbf{2 . 9 5}$ plus 34p p. \& $p$

 CT/02 2A- 1.10 plus 30 p p. \& p.
CT/03 4A- 1.60 plus 30 p p. \& CT/03 4A- 1.60 plus 30p p. \&
Speaker Matching 3-8-16
Example: $16 \Omega$ speaker to 8 , amplifier. 90 p plus 20 p p. \& p.

SEMICONDUCTORS, etc. Zeners-400mW, 15p: 1.5W, 221pp C.D.R.ORP12, $56 p$

Bridge rectifier- 40 P. ${ }^{\text {P/ }}$ 50 p
Bridge 50p
Transistor sockets-7p
D.1.L. I.C. sockers-14 pin. 20p $16 \mathrm{pin}, 20 \mathrm{p}$
N4001-50 P.I.V. 1.0A. 6p
N4002-1
I 100 P.I.V., I OA,
Ip
IN4003-200 P.IV., I.OA, 8p
IN4005-400 PI.V. I OA, op
IN 400 P.I.V. $1.0 A$, I2p
ALUMINIUM BOXES
with lids and serews $\quad$. Price p. g p.
 GB8: tin 4 in litin 38p 15p

GB9. lin 2tin litin 38p 13p $\begin{array}{lll}\text { GBio. Stin 4in 1tin 44p } & 18 p \\ \text { GBil } \\ \text { GBil } 4 \text { in 2tin } 2 i n & 38 p & 13 p\end{array}$ | GBil | $4 i n$ | $2 \frac{1}{2} i n$ | $2 i n$ | $38 p$ |
| :--- | :--- | :--- | :--- | :--- |
| GBi2 | $3 i n$ | $2 i n$ | $1 i n$ | $33 p$ |
| GBi3 | $6 i n$ | $4 i n$ | $2 i n$ | $52 p$ |
| $18 p$ |  |  |  |  |

 GB15 8in 6in 3in 81p 26p GBI6 l0in 7in. These sizes fir


EQUIPMENT CASES in plain aluminium with sloping front panel
Type H. W. D. Pricep. \& SFP $2 i n$ stin $2 \operatorname{tin} 45 \mathrm{p}$ 12p $\begin{array}{lllll}\text { SF2 } & \text { 2in } 7 \operatorname{tin} & 3 \operatorname{tin} & 60 p & 16 p \\ \text { SF3 } & \text { 2in } 9 \text { in } & 4 \frac{1}{2} i n & 75 p & 19 p\end{array}$ tove - enamelted silver-grey ham-
mer finished, 25p mer fa.

CONSOLE CASES
in plain aluminium, ideal for mixers Type W. A B C Dprice p. ap. $\begin{array}{lllllll}\text { GB20 } & 8 & 9 & 3+2 & 3 & \& 1.42 & 30 p \\ \text { GB21 } & 10 & 9 & 312 & 3 & E 1.58 & 30 p\end{array}$ $\begin{array}{lllllll}\text { GB2 } & 12 & 9 & 3 \frac{1}{2} & 3 & \text { E1.58 } & 30 \mathrm{p} \\ \text { GB2 } & 12 & 9 & 3 \frac{1}{2} & 3 & \text { El.72 } & 30 \mathrm{D}\end{array}$


VEROBOARD

| Size | $\begin{gathered} 01 \\ \text { matrix } \end{gathered}$ | $\begin{gathered} 0.15 \\ \text { matrix } \end{gathered}$ |
| :---: | :---: | :---: |
| 2tin $\times$ 3tin | 22p | 16p |
| 2 $\operatorname{in}$ in $\times 5 \mathrm{in}$ | 24p | 25p |
| 3tin $\times$ 3tin | 24p | 25p |
| $3 \frac{1}{1} \mathrm{in} \times 5 \mathrm{in}$ | 27p | 29p |
| $17 \mathrm{in} \times 2 \mathrm{im}$ | 75p | 57p |
| $17 \mathrm{in} \times 3$ 3in | ¢ 1 | 75p |

ELECTROLYTICS

| $1 \mu \mathrm{~F}$ | 450 V | 19p | 1,000 F | 25 V | 27p |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \mu \mathrm{~F}$ | 450 V | 20p | 1,000 ${ }^{\text {F }}$ F | 50 V | 42p |
| $4 \mu \mathrm{~F}$ | 350 V | $14 p$ | 2,000 F | $25 V$ | 39p |
| $8 \mu \mathrm{~F}$ | 450 V | 17p | 2,000 $\mu \mathrm{F}$ | 50 V | 53p |
| $16 \mu \mathrm{~F}$ | 450 V | 18 p | 2,500 ${ }^{\text {F }}$ | 25. | 45p |
| $25 \mu \mathrm{~F}$ | 25 V | 7p | 2,500 ${ }^{\text {F }}$ | 50 V | 60p |
| $25 \mu \mathrm{~F}$ | 50 V | 10p | 3,000 F | $25 V$ | 48p |
| $32 \mu \mathrm{~F}$ | 450 V | 27p | 5,000 ${ }^{\text {F }}$ | $25 V$ | $60 p$ |
| $50 \mu \mathrm{~F}$ | 50 V | 10p | $5,000 \mu \mathrm{~F}$ | 50 V | (1) 10 |
| $100 \mu \mathrm{~F}$ | $25 V$ | 10p | 8-8 $\mu \mathrm{F}$ | 4SOV | $18 p$ |
| $100 \mu \mathrm{~F}$ | 50 V | 11p | $8-16 \mu \mathrm{~F}$ | 450 V | 20p |
| $250 \mu \mathrm{~F}$ | 25. | 14p | 16-16 $\mu \mathrm{F}$ | 4S0V | 27p |
| $250 \mu \mathrm{~F}$ | 50 V | 17p | $16-32 \mu \mathrm{~F}$ | 450 V | $63 p$ |
| $500 \mu \mathrm{~F}$ | 25 V | 18p | 32-32 $\mu \mathrm{F}$ | 450V | 49p |
| $500 \mu \mathrm{~F}$ | 50 V | 25p | $50-50 \mu \mathrm{~F}$ | 3 SoV | ${ }^{38}$ p |

MINIATURE ELECTROLYTICS

| $1 \mu \mathrm{~F}$ | 63 V | 6p | $47 \mu \mathrm{~F}$ | 16 V |
| :---: | :---: | :---: | :---: | :---: |
| $2.2 \mu \mathrm{~F}$ | 63 V | 6p | $47 \mu \mathrm{~F}$ | 25 V |
| $3.3 \mu \mathrm{~F}$ | 63 V | ${ }^{6 p}$ | $68 \mu \mathrm{~F}$ | 16 |
| $4.7 \mu \mathrm{~F}$ | 63 V | 6p | $100 \mu \mathrm{~F}$ | 10 |
| $8 \mu \mathrm{~F}$ | 40 V | 7 p | $220 \mu \mathrm{~F}$ | 16 |
| $10 \mu \mathrm{~F}$ | 25 V | ${ }^{6 p}$ | $330 \mu \mathrm{~F}$ | 16 |
| $10 \mu \mathrm{~F}$ | $64 V$ | $7{ }^{7}$ | $470 \mu \mathrm{~F}$ | 10 |
| $16 \mu \mathrm{~F}$ | 40 V | $7 p$ | 1,000 ${ }^{\text {F }}$ | 16 |
| $33 \mu \mathrm{~F}$ | 16 V | 6p | 1,500 F |  |

## CASSETTE OWNERS

For Philips and similar cassecte recorders.
PUI2 Power unit for connection to
$2 V+$ or - E car electrica
systems, giving $7 \frac{1}{2} V$, stabilised $\mathbf{£ 3 . 2 5}, ~$
output.
PUI4 As zbove but switched for $\mathbf{\$ 5 . 1 0}$
PP75 Mains power supply. output $\mathbf{f |} 95$
All units are complete with cable and plug.

## CASSETTES

Top quality British made, low noise, complete with transparent ibrary cases $-\overline{0}$
C60-40p; C90-55; C120-70

BATTERY ELIMINATORS current equipment
PP96 Input 240 V a.c. Output 6 V d.c
Price $\mathrm{fl}: 50$ plus $12 \mathrm{p} \mathrm{p}$.\& F p.

## ILLUSTRATED CATALOGUE

Post Free
15p

CONTROLS, Log. or Lin.
Single, less switch, $15 p$
Single, D.p. switch, ${ }^{4} \mathrm{p}$
Tandem, less switeh, 40
$5 \mathrm{k} \Omega$, $10 \mathrm{k} \Omega, 25 \mathrm{k} \Omega$. $50 \mathrm{k} \Omega$. $100 \mathrm{k} \Omega$, $250 \mathrm{k} \Omega$. $500 \mathrm{k} \Omega, 1 \mathrm{Mn}, 2 \mathrm{Mn}$

## RESISTORS

 AW, 1fp;iW, 4p; 2W, 6p$5 \mathrm{~W}, 10 \mathrm{p}$; $10 \mathrm{~W}, 12 \mathrm{p}$

## SWITCHES

Toggle switches, standard size
SW20-S.P.S.T. 18p; SW21-D.P.D.T. 23p. Push Button, miniature, SWI-I3p.
Wafor switches (rotary)-24p each
SW4-1 pole, 12 way. SW5-2 pole, 6 way SW6-3 pole, 4 way. SW7-4 pole, 2 way SW8-4 pole, 3 way

## BONDED ACRYLIC FIBRE

B.A.F. wadding, I8in wide, lin thick. The ideal lining for speaker enclosures. 30p per
yard. p. \& p. one yard I 2 p; each extra yard 4 p

TYGAN tod quality loudspeaker covering material. Please send 6p for samples, sizes and prices.

## MAGNETIC COUNTERS

Brand new, neat, 48 volt
Brand new, neat, 48 Vo
5 digit counters. 60 p

| PLUGS |  |  |  |
| :---: | :---: | :---: | :---: |
| Car aerial | 14 p |  |  |
| Co-axial <br> D.I.N. 2 pin (speaker) | $10 \mathrm{p}$ |  |  |
| D.iN. 3 pin | 13 p | 15 |  |
| D.IN. 4 pin $180^{\circ}$ | 14 p |  |  |
|  | $13 p$ 150 |  |  |
| D.I.N. 6 pin | 15 p |  |  |
| Jack, 2 tmm unscreened | 9p |  |  |
| Jack. 24 mm screened | 10 p |  |  |
| Jack, $3 \frac{1}{2} \mathrm{~mm}$ unscreened Jack, $3 \frac{1}{2} \mathrm{~mm}$ screened | 12p | -x (1) |  |
| Jack, tin unscreened | 12 p |  |  |
| Jack, din screened | 20p | SOCKETS |  |
| Jack, stereo, unscreened | ${ }^{20 p}$ | Car aerial | $\mathrm{l}_{8 \mathrm{p}}^{8}$ |
| fack, stereo, screened | ${ }^{35 p}$ | Co-axial, flush | 9 p |
| Phono, plated met | 12 p | D.I.N. 2 pin (speaker) | 10 p |
| Wander, red or black | ${ }^{3} \mathrm{p}$ | D.I.N. 3 pin | $9 p$ |
| Banana 4 mm , red or black | 6 P | D.IN. ${ }^{\text {D }}$ pin, $180^{\circ}$ D.I.N. 5 pin, $240^{\circ}$ | 9p ${ }^{\text {p }}$ |
| LINE SOCKETS |  | $\begin{aligned} & \text { Jack, } \frac{2}{2} \frac{2 m m}{\text { Jack, }} 3 \frac{2}{2 m m} \end{aligned}$ | 10 p |
| Caraerial | 14 p | Jack, din unswitched | 15 p |
| C.I.N. 2 pin (s | 178 | Jack, tin switched | 17 p |
| D.IN. 3 pin | 16 p | Jack, stereo, switched Phono, single | ${ }^{24} 5$ |
|  | 16p | Phono, 2 on a strip | $7 p$ |
| D.IN, 5 pin, $240^{\circ}$ | 150 | Phono, 3 on a strip | p |
| Jack, $3 \frac{1}{2} \mathrm{~mm}$ | 15p | Phono, 4 on a strip | 10p |
| Jack, tin screened | 49p | Wander, single, red or black | 5p |
| Jack, stereo, screened | 34 p | Wander, twin str | 7 p |
| Phono, plated metal | 14 p | Banana 4mm red, or black | 6p |


| CAPACITORS |  |  |  | $0 \cdot 0027_{\mu} \mathrm{F}$ | $\begin{aligned} & 500 \mathrm{~V} \\ & 500 \mathrm{~V} \end{aligned}$ | $S / M$ | 15p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.2pF | 500 V | S/M | $71 p$ |  | 125 V | Cer. | 6p |
| $3 \cdot 3 \mathrm{pF}$ | 500 V | S/M | 710 | $0.0033 \mu \mathrm{~F}$ | 500 V | Poly. | $6 p$ |
| 5 pF | 500 V | S/M | 7 ¢ ${ }^{\text {P }}$ | $0.0033 \mu \mathrm{~F}$ | 1,000V | MDC | 6p |
| 10 pF | 125 V | P.S. | 5p | $0.0036 \mu \mathrm{~F}$ | 500V | S/M | 15p |
| 10 pF | 500 V | S/M | 71 p | $0.0047 \mu \mathrm{~F}$ | 125 V | P.S. | 9 p |
| 15 pF | 125 V | P.S. | 5p | $0.0047 \mu \mathrm{~F}$ | 500 V | Poly. | 6 p |
| 15 pF | 500 V | Cer. | 4 p | $0.0047 \mu \mathrm{~F}$ | 500 V | S/M | 20p |
| 18 pF | 500 V | S/M | $71 p$ | $0.0047 \mu \mathrm{~F}$ | 1,000V | MDC | 6 p |
| 22pF | 125 V | P.S. | 5p | $0.005 \mu \mathrm{~F}$ | 100 V | Mylar | 3p |
| 22pF | 500 V | S/M | 7 p | $0.005 \mu \mathrm{~F}$ | 500 V | Cer. | 5 p |
| 25pF | 500 V | $S / M$ | 71 p | $0.0068 \mu \mathrm{~F}$ | 125 V | P.S. | 101p |
| 27 pF | s00V | Cer. | 4 p | $0.0068 \mu \mathrm{~F}$ | 500 V | S/M | 30p |
| 33 pF | 125 V | P.S. | 5p | $0.0068 \mu \mathrm{~F}$ | 500 V | Poly. | 6p |
| 33 pF | Soov | S/M | 710 | $0.0082 \mu \mathrm{~F}$ | 125 V | P.S. | $101 p$ |
| 39pF | 500 V | S/M | $71 p$ | $0.0082 \mu \mathrm{~F}$ | 500 V | S/M | 30p |
| 47 pF | 125 V | P.S. | $5 p$ | $0.01 \mu \mathrm{~F}$ | 18 V | Dise | 4p |
| 47pF | 500 V | Cer. | $4 p$ | $0.01 \mu \mathrm{~F}$ | 125 V | P.S. | $101 p$ |
| 50 pF | 500 V | S/M | 7 tp | $0.01 \mu \mathrm{~F}$ | 160 V | Poly. | 4 p |
| 56\%F | 500 V | S/M | 7 P | $0.01 \mu \mathrm{~F}$ | 250 V | M.F. | 3 p |
| 68 pF | 125 V | P.S. | 5p | $0.01 \mu \mathrm{~F}$ | 400 V | Poly. | 3 p |
| 68 pF | 500 V | S/M | 7 p | $0.01 \mu \mathrm{~F}$ | 500 V | Cer. | $5 p$ |
| 75 pF | 500 V | S/M | 7 P | 0.0114 F | 500 V | 5/M | 10p |
| 82pF | 500 V | S/M | 7 P | $0.01 \mu \mathrm{~F}$ | 600 V | MDC | 7 p |
| 100 pF | 125 V | P.S. | 5 p | $0.01 \mu \mathrm{~F}$ | $1,000 \mathrm{~V}$ | MDC | 9 p |
| $100 p \mathrm{~F}$ | 500 V | S/M | 7 p | $0.015 \mu \mathrm{~F}$ | 160 V | Poly. | $3 p$ |
| 100 pF | Soov | Cer. | 5p | $0.015 \mu \mathrm{~F}$ | 400 V | Poly. | 3 p |
| 120 pF | 500 V | S/M | $7 \frac{1 p}{}$ | $0.02 \mu \mathrm{~F}$ | 100V | Mylar | $3 p$ |
| 150pF | 125 V | P. 5. | ${ }^{5 p}$ | $0.022 \mu \mathrm{~F}$ | 18 V | Disc | $5 p$ |
| 150pF | 500 V | S/M | 7 P | $0.022 \mu \mathrm{~F}$ | 250 V | M.F. | 3 p |
| 150pF | 500 V | Cer. | 5 P | $0.022 \mu \mathrm{~F}$ | 400 V | Poly. | 3 p |
| 180pF | 500V | $5 / \mathrm{M}$ | $71 p$ | $0.022 \mu \mathrm{~F}$ | 600V | MDC | $71 p$ |
| 200pF | 500 V | S/M | $7 \frac{1}{5 p}$ | $0.022 \mu \mathrm{~F}$ | 1,000V | MDC | 10p |
| 220pF | 125 V | P. S. | ${ }_{5 p}$ | 0.033 $\mu \mathrm{F}$ | 250 V | M.F. | 4p |
| 220pF | 500 V | Cer. | 5 p | $0.033 \mu \mathrm{~F}$ | 400 V | Poly. | 4 p |
| 250pF | 500 V | S/M | 8 p | $0.047 \mu \mathrm{~F}$ | 12V | Disc | 6 p |
| 270pF | 500 V | Cer. | 5 p | $0.047 \mu \mathrm{~F}$ | 180 V | Poly. | 3 p |
| 300 pF | 500 V | $5 / M$ | 8 p | $0.047 \mu \mathrm{~F}$ | 250 V | M.F. | $3 p$ |
| 330pF | 125 V | P.S. | 5 p | $0.047 \mu \mathrm{~F}$ | 400 V | Poly. | 4 p |
| 330pF | 500 V | 5/M | 8 p | $0.047 \mu \mathrm{~F}$ | 600 V | MDC | 8 p |
| 390 pF | soov | S/M | 8p | $0.047 \mu \mathrm{~F}$ | 1,000V | MDC | 10 p |
| 470 pF | 125 V | P.S. | 5p | $0.1 \mu \mathrm{~F}$ | 30 V | Dise | $6 p$ |
| 470pF | 750 V | Dise | $5 p$ | $0.1 \mu \mathrm{~F}$ | 250 V | M.F. | 4 p |
| 500 pF | 500 V | 5/M | 8 p | $0.1 \mu \mathrm{~F}$ | 400 V | Poly. | 5p |
| S60pF | 500 V | S/M | 8 p | $0.1 \mu \mathrm{~F}$ | 600 V | MDC | 10p |
| 680pF | 125 V | P.S. | 6 p | $0.1 \mu \mathrm{~F}$ | 1.000 V | MDC | 14p |
| 680pF | 500 V | S/M | 8 p | $0.15 \mu \mathrm{~F}$ | 250 V | M.F. | 5p |
| 820 pF | 500 V | 5/M | 8 p | $0.22 \mu \mathrm{~F}$ | 160 V | Poly. | $6 p$ |
| $0.001 \mu \mathrm{~F}$ | 100V | Mylar | 3 p | $0.22 \mu \mathrm{~F}$ | 250 V | M.F. | 5 p |
| $0.001 \mu \mathrm{~F}$ | 125 V | P.S. | ${ }^{6 p}$ | $0.22 \mu \mathrm{~F}$ | 400 V | Foil | 10p |
| $0.001 \mu \mathrm{~F}$ | 400 V | Poly. | 3 p | $0.22 \mu \mathrm{~F}$ | 1,000V | MDC | $15 p$ |
| $0.001 \mu \mathrm{~F}$ | 500 V | S/M | 10p | $0.33 \mu \mathrm{~F}$ | 250 V | M.F. | ap |
| $0.001 \mu \mathrm{~F}$ | 500 V | Cer. | 5p | $0.47 \mu \mathrm{~F}$ | 250 V | M.F. | 8 p |
| $0.001 \mu \mathrm{~F}$ | 1,000V | MDC | 6 p | $0.47 \mu \mathrm{~F}$ | 400 V | Foil | 15p |
| $0.0015 \mu \mathrm{~F}$ | 400 V | Poly | ${ }^{3} \mathrm{p}$ | $0.47 \mu \mathrm{~F}$ | 1,000V | MDC | 25p |
| $0.0015 \mu \mathrm{~F}$ | 500 V | S/M | 10p | $1.0 \mu \mathrm{~F}$ | 250 V | M.F. | 15p |
| $0.0015 \mu \mathrm{~F}$ | 500 V | Cer. | ${ }^{5 p}$ |  |  |  |  |
| $0.0018 \mu \mathrm{~F}$ | 500 V | S/M | 10p | Note |  |  |  |
| $0.002 \mu \mathrm{~F}$ | 100 V | Mylar | 3 p , | $S / \mathrm{M}=$ | er mi | \% |  |
| $0.002 \mu \mathrm{~F}$ | 500 V | Cer. | 5p | P.S. $=$ p | ystyrene | 21\% |  |
| $0.0022 \mu \mathrm{~F}$ | 125 V | P.S. | $6 p$ | MDC | c. ratin | $=300 \mathrm{~V}$ |  |
| $0.0022 \mu \mathrm{~F}$ | 500 V | S/M | 10 p | M.F. $=$ | ullard m | . foil. |  |
| $0.0022 \mu \mathrm{~F}$ | 1,000V | MDC | 6 p | Cer. $=$ ce | eramic. | . |  |

## (IP) IL.P. (Eseatenestuc

## THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highiy improved odule achieves true High Fidelity with a dramatic reduction in distortion (iypically $0.05 \%$ at KHz into 8 ohms! ! and is electronically and mechanically compatible with the HY40.

With this important improvement the HY 41 retains all of the quality characteristics found in he earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete保 power amplifier of extremely high perstmand industry.
HI-Fi but also for public address systems and industry. HY 4 t and its various applications including
The free manual gives a full circuit diagram of the complete stereo amplifier
Like its predecessor the HY41 is based on conventional and proven circuit techmiques developed over recent years.
OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts
R.M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30 K ohms at 1 KHz .
VOLTAGE GAIN: 30 db at 1 KHz
TOTAL HARMONIC DISTORTION: less than $0.15 \%$ (typical $0.05 \%$ )
at 1 KHz
FREOUENCY RESPONSE: $5 \mathrm{~Hz}-50 \mathrm{KHz}+1 \mathrm{db}$
SUPPLY VOLTAGE: + 22.5volts D.C
SUPPLY CURRENT: $\overline{0} .8$ amps maximum.
PFIICE: inc. comprehensive manual, P.C. board, five extra components and P. \& P.:-
MONO: $£ 4.90$
STEREO: $£ 9.80$

## UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the desired function is achieved by use of a multi-way switch or by direct interconnection.

Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16-25 Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo pre-amplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

## INPUTS

Magnetic Pick-up (within $\pm 1 \mathrm{db}$ RIAA curve) $2 \mathrm{mV} .47 \mathrm{~K} \Omega$
Fape Replay texternal components to suit head) $4 \mathrm{mV} .47 \mathrm{~K} \Omega$
Microphone (flat) $10 \mathrm{mV} .47 \mathrm{~K} \Omega$
Ceramic Pick-up lequalized and compen-
satable) $20-2000 \mathrm{mV}$. variable.
Tuner (flat) 250 mV . $100 \mathrm{~K} \Omega$
Auxiliary 1250 mV . $47 \mathrm{~K} \Omega$
Auxiliary $22-20 \mathrm{mV}$. $100 \mathrm{~K} \Omega$

OUTPUTS
Main Pre-amp output 500 mV .
Direct tape output 120 mV .
ACTIVE TONE CONTROLS (Bexendall)
Treble $\pm 12 \mathrm{db}$
Bass + 12 db
INTER̄NAL STABILIZATION
Enables the HY5 to share an unregulated
supply with the Power Amplifier.
SUPPLY VOLTAGE
16-25 volts
PRICE: MONO: $£ 3.60$
STEREO: £7. 20

## POWER SUPPLY PSU45

The versatile P.S.U. 45 is designed to supply your HY41's + HY5's in stereo or mono format.

Specification
Input: 200-240 Volts.
Output: $\pm 22.5$ Volts at 2 amps
Overall Dimensions: L. $7^{\prime \prime} ;$ D. 3.8"; H. 3.1 ${ }^{\prime \prime}$
PRICE: 4.50 inc. $P$. \& P.

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## BEDFORD ELEGTRONIGS <br> 2 GROVE PLACE, BEDFORD <br> (continuation of Lurke Sereet)

Tel.: Bedford 51961
MULLARD C296 POLYESTER FILM CAPACITORS
$400 \mathrm{~V}=0.001,0.0015,0.0022,0.0033,0.0047,21 \mathrm{p}, 0.0068,0.01,0.015,0.022$, 12p, 3p. 0.047, 0.068, 0.1, 4p. 0.15, 5ip, 0.22, 7p. 0.33, 101p. 0.47 $160 \mathrm{~V}: 0.01,0.015,0.022,0.033,0.047,0.068,3 \mathrm{p}, 0.1,3 \neq \mathrm{p}, 0.15,4 \mathrm{p}, 0.22$ 41p. $0.33,51 p . \quad 0.47,7 p . \quad 0.68,10 \mathrm{p} .10,12 \mathrm{p}$.

MULLARD C280 METALLISED FILM CAPACITORS 250V
$0.01,0.015,0.022,3 p .0 .033,0.047,0.068,31 p .0 .1,4 p, 0.15,0.22,41 p$. $0.33,6 p . \quad 0.47,71 p .0-68,10 \mathrm{p} .10,12 \mathrm{p}, 1-5,18 \mathrm{p} .2 \% 21 \mathrm{2}$.

CERAMIC CAPACITORS 50V (Square plaquette body) CERAMIC CAPACITORS 50V (Square plaquette body)
E12 Series 22pF-1,000pF, IIp. E6 series $0.0015-0.01,2 p$. E6 series 0.015 -
0.047 , 2 pp .

HIGH VOLTAGE CAPACITORS IO00V d.c. (300V a.c.)
$0.001,0.0022,0.0033,0.0047,7 \mathrm{p}$. $00068,0.01,0.022,10 \mathrm{p} .00 .047,01,12 \mathrm{p}$.
$0 \cdot 22,20 p . \quad 0.47,22 p$.
POLYSTYRENE CAPACITORS $125 V, 21^{\circ}$
Values in PF: $5,10,15,22,33,47,56,68,100,150,220,330,470,560,680,820$ 1000, 3ip.

SOLID TANTALUM RESIN DIPPED BEAD CAPACITORS $\mu$ F/V; $0.1 / 35,0.22 / 35,0.47 / 35,1 \cdot 0 / 35,2 \cdot 2 / 35,4.7 / 35,10 / 6 \cdot 3,10 / 16,10 / 25$, 22/16, 47/6.3, $100 / 3,15 p$.

MULLARD 015/016/017ELECTROLYTICS (Replaces C426/C437) $\mu F / V: 1 / 63,1.5 / 63,2 \cdot 2 / 63,3.3 / 63,4-7 / 63,6 \cdot 8 / 63,10 / 25,10 / 63,15 / 10,15 / 63$, $22 / 25,22 / 63,33 / 16,33 / 40,47 / 10,68 / 16,100 / 4,100 / 10,100 / 25,150 / 16,220 / 16$,
 $1500 / 6 \cdot 3,11 \mathrm{p}, 10220 / 63 \cdot 470 / 40$
$1500 / 16,2200 / 10,3300 / 6 \cdot 3,18 p$.
RESISTORS
ISKRA TYPE
MULLARD I/3W
MULLARD $1 / 5 \mathrm{~W}$ METAL FILM IW WIREWOUND 2.5 W WIREWOUND 2.5 W

[^4]PRACTICAL ELECTRONICS "SCORPIO" ELECTRONIC IGNITION SYSTEM


This Capacisor-Discharge Electronic Ignition system was described in the November and December issues of for incorporating in any 12 V ignition system in cars, boats, go-karts, etc. of either pos. or neg, earth and up to six cylinders. The original coil, plugs, points and contact-breaker capacitor fitted in the vehicle are used. No extra or special com ponents are required.
Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better highspeed performance, quicker engine wanomy. Eliminatesproved fue ecoct-breaker point burning and che need to adiust point and spark-plue gaps with precision. Construction of the unit can easily be completed in an evening and
installation should take no longer than half an hour. A complete complement of components is supplied with each kit together with ready-drilled roller-tinned professional quality fibre-glass wownd transformer and fullymachined die-cast case. All components are availabie separately. Case size 7 itn $\times 4 \frac{1}{2}$ in $\times 2$ in. approx.
Complete assembly and wiring manual $25 p$, refundable on purchase
of kit. Price: : $10 \cdot 50$ plus 50 p P. \& P

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This unic represents a natural pro gression from our phenomenally befores the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency sig nals into a three-coloured light display; the colour depending on the frequency of the signal and the incensity on the loudness of the audio source
The unit is constructed on professional fibre-glass princed-circuit wave triac circuitry. There full master-level control together wish independent sensitivity controls for each channel. The original minimum ambient light level controls have been redesigned permitting thei use as faders; allowing dimming from max. to zero at the turn of knob. R.F.I. suppression is now incorporated as standard as well as
provision for D.J. "Pulse. Flash " provision for D.J. "' Pulse. Flash
controls. The choice of two inputs enables operation from wo inputs and low power amplifiers Max power 1.5 kW per channel ax power
240 V a.c.
Complete assembly built and tested Size 9 in $\times 7$ in $\times 3 i n$. Price 25 carr. paid

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 EZ80 as acetifict. Twis dalal potentionetera are provided for bass and treble control, giving hass and treble boost and cut. A dual volume control is used.
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$\begin{array}{llll}\text { BN7408 } & 0.20 & 0.18 & 0.18 \\ \text { SN7409 } & 0.45 & 0.42 & 0.35 \\ \text { BN7410 } & 0.20 & 0.18 & 0.16 \\ \text { SN7411 }\end{array}$
$\begin{array}{llll} \\ \text { BN7411 } & 0.23 & 0.22 & 0.20 \\ \text { BN7412 } & 0.42 & 0.40 & 0.35 \\ \text { BN7413 } & 0.30 & 0.24 & 0.25\end{array}$
$\begin{array}{llll} \\ \text { BN7413 } & 0.30 & 0.27 & 0.25 \\ \text { SN7417 } & 0.30 & 0.27 & 0.25 \\ \text { N } 7417 & 0.30 & 0.27 & 0.25\end{array}$
$\begin{array}{llll} \\ \text { BN7420 } & 0.30 & 0.27 & 0.25 \\ \text { SN7422 } & 0.48 & 0.44 & 0.18 \\ \text { SN7423 } & 0.48 & 0.44 & 0.40\end{array}$

|  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| SN7425 | 0.48 | 0.44 | 0.40 | SN |
| SN7427 | 0.48 | 0.40 | 0.35 | S |
| SN7． | 0.39 | 0.35 |  |  |


|  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| SN7．428 | 0.50 | 0.45 | 0.42 | SN7493 | 0.75 | 0.70 |
| SN | 0.85 |  |  |  |  |  |
| SN7430 | 0.20 | 0.18 | 0.18 | SN7495 | 0.80 | 0.75 |
| 0 | 0.70 |  |  |  |  |  |

$\begin{array}{lllllllll}\text { SN7432 } & 0.20 & 0.18 & 0.16 & \text { SN7495 } & 0.80 & 0 & 75 & 0.70 \\ \text { SN7433 } & 0.70 & 0 & 39 & 0.35 & \text { SN7496 } & 1.00 & 0.97 & 0.95 \\ \text { SN } & \text { SN } \\ \text { SN }\end{array}$


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AAY42 | 15 p | BC169C | 12p | BY100 | 15p | 0445 | 150 | V405A | 25p | － N 3440 | 75p |
| AAZ13 | 10p | BC18： | 10p | HY126 | 15p | OC57 | 50 p | ZTN108 | 12p | 2N3442 | 1.25 |
| AC107 | 35p | HC214 | 15p | BY127 | 15p | 0 OCl 1 | 15p | ZTX300 | 12p | 2N3525 | 75p |
| AC126 | 25p | ВСY32 | $75 p$ | BYZ13 | 35p | $0 \mathrm{Cl2}$ | 25p | ZTX301 | 15p | 2N3614 | 59p |
| AC127 | 25p | BCY 34 | 35p | C106D | 65p | $0 \mathrm{OC}^{7} 7$ | 45p | 2TX302 | 18p | 2N3615 | ${ }^{75 p}$ |
| AC128 | 25p | BCY 39 | 1.00 | （1ET111 | 55p | OC81 | 26 p | ZTX341 | 20 p | 2 N 3702 | 10 p |
| AC176 | 25 p | 13CY42 | 30p | CET115 | 55p | 0088 | $25 p$ | ZT |  |  | 10p |
| AC187 | 25p | BCY43 | 25p | GET880 | 45p | OC140 | 55 p | ZTX503 |  |  | 10p |
| AC188 | 25p | BCris5 | 250 | LM 309 K |  | OC170 | 25p |  |  |  | 180 |
| ACY17 | 30p | BCY70 | 15p | （T03） | 1.87 | 0 O 171 | $80 p$ | 2N 404 | 20p | 2N3771 | 175 |
| ACY20 | 20p | BCY71 | 20p | MATl－ 2 | 25p | OO200 | 45p | 2N527 | 35p | 2N3773 | 200 |
| ACY＇21 | 20p | BCY7 ${ }^{\text {a }}$ | 15p | MJE340 | 50p | OC201 | 75p | 2 N 695 | 15p | 2N3790 | 2.25 |
| ACY39 | 55p | BCY87 | 2.99 | MJ E370 | 70p | $0 \mathrm{OC202}$ | 80 p | 2N697 | $15 p$ | \％ 38819 | 35p |
| AD140 | 50p | BCZIL | 50p | MJE520 | 75p | OC203 | 50p | 2N706 | 10 p | 2N3820 | 50p |
| AD149 | 50p | B1124 | 80p | MJE 295 |  | 0 OCP 71 | $1-25$ | 2N930 | 20 p | 2N3866 |  |
| AD161 | 35p | BD131 | 75p |  | 110 | ORP12 | 50p | 2N987 | ${ }^{45 p}$ | ${ }_{2}^{2 N 3903}$ |  |
| A 1162 | 35p | BD132 | 80 p | M | 5 | ORPP60 | 40p | 2N1131 | 25p $25 p$ | 2， N 4061 |  |
| AF1］7 | 20p | BF115 | 25p |  | 75p | P346A | 20 p | 2N1302 | 25p | ${ }_{2} \mathrm{~N} 40 \mathrm{H}$ ． |  |
| AFP124 | 50 p 250 | ${ }_{13 F 173}$ | $25 p$ $25 p$ | MP | 40p 20p |  | 45p | 2N1304 | 22p | ${ }^{2} \mathrm{~N} 412$ | 15p |
| AFF124 | 20 p 30 p | 13F173 | 250p | NKT21 | 640 p | RAS | $\mathrm{AF}^{\text {P }}$ | 2 N 1305 | 22D | ${ }^{2} \mathrm{~N}+87$ | 35p |
| AF189 | 40p | BF180 | 30p | NKT217 | 7 40p |  | 55p | ${ }_{2} \mathrm{~N} 13137$ | ${ }^{25 p}$ | 2 N 545 | 30p |
| AF＇239 | 4UD | BF194 | 15p | NKT403 | 370 p | TAA963 | 75p | 2 N 1308 | 25p | $2 \mathrm{NS77}$ | 55p |
| AsY27 | 30p | BP195 | 15p | NKT404 | 450 p | TIL209 | 39p | 2N1613 | 20p | 28001 |  |
| AsY28 | 25p | ［3FSh1 | 25p | 0.45 | 50p | TIP29a |  | 2N1671 | 1.00 | 28012 | 0.00 |
| BA102 | 30p | Fs98 | 25p | OAl0 | 35p | TIP30A |  | 2N $214 \%$ | 75 p | ${ }^{2} 88018$ | 0 |
| BA115 | 7 | BFX13 | 25p | 0481 | 10p | TIP31A |  | 2N2160 | 39p | ${ }^{2} 88301$ | D |
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| $\begin{gathered} \text { OCI } 70 \text { Mullard } 25 \mathrm{p} \\ 25+20 \mathrm{p} \\ 100+118 \mathrm{p} \\ 500+155 \\ 1000+13 \mathrm{p} \end{gathered}$ | $\begin{array}{r} 25+8 p \\ 100+7 p \\ 1000+8 p \\ 1000 \\ \hline 0 \end{array}$ |
| :---: | :---: |
| Byi27 Mullard 15p | AD161，ADI62 35peach25 |
| 25＋ 12 p |  |
| （100 +10 p |  |
| 1000＋ |  |
|  |  |
| $25+8$ | 2N3053 20p |
| 25 100 $+8 p$ $+8 p$ | $\begin{array}{r} 25+18 p \\ 100 \pm+15 p \\ 1000 \pm+12 p \\ 1000 \end{array}$ |
|  |  |
| $1000+$ Sp |  | TRIACS

$$
\begin{gathered}
\text { OC35 Muilard } 50 \mathrm{p} \\
25+45 \mathrm{p} \\
1000+30 \mathrm{p} \\
500+35 \mathrm{p} \\
1000+30 \mathrm{p}
\end{gathered}
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$$
\begin{aligned}
& x \\
& \mathrm{~B} \geqslant / \\
& \mathrm{B}
\end{aligned}
$$

$$
\begin{aligned}
& x=1 \\
& B \geqslant / 05 \\
& B \geqslant / 100
\end{aligned}
$$

$$
\begin{array}{lr}
x=1 \\
\mathrm{~B}=/ 20 & 50 \\
\mathrm{~B}^{2} / 100 & 100 \\
132 / 200 & 200 \\
B_{2}^{2} / 200 & 600 \\
B^{2} 2 / 1000 & 1000
\end{array}
$$

$$
\begin{aligned}
& B 2 / 100 \\
& 132 / 200 \\
& 102 / 600
\end{aligned}
$$

$$
\begin{aligned}
& \mathrm{B} \cdot 11000 \\
& \text { FOUR AMP }
\end{aligned}
$$

$$
\begin{aligned}
& \text { SILICON CONTROLLED } \\
& \text { RECTIFIERS }
\end{aligned}
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THERMOSTAT WITH PROBE
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Gur Ref. No. P301, 6 switches some of whict are changeover types. All rated at 10A. Operated
by motor which makea 1 rev every 3 mina. by motor which

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Made by G.E.C. Normal type with approx. 1 in of $3 / 8$ apindle. Standard fixing in stack. Brand new tocks available.
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OCPF0-ideal for burglar alarms and similar applica-
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## EXIT

One of our customers easily our hox signs can aigns. Thene are to exit ted having a 20 W fiuorescent lamp with coar plastic. Directly onto this you can atick down the letters available at most stationers. There $\mathfrak{j}$ room inside the box for a battery and low volt amp in the case of power failure. Size of aign is 2 ft high $\times 14 \mathrm{in}$ wide $\times 5 \mathrm{in}$ deep. Solidly mad roln sheet steel and hammer finished in enamel. Price 53.50 plus 50 p carriage per 200 miles.
6 PIN PLUG AND SOCKET
And nietal case with flex grip for one end, this ther part fitting to the equipment. Price 40 p per paír-10 pairs as-60.
LIGHT DIMMERS
We regret that through increased costs our 1 kW model has now to be increased to $\$ 2.95$

## LIGHT DIMMER BOX

Another festure we can supply is box and 13 A socket, this makes dimmer suitable for control of portable lights and equipment. This price is 450 extra.

## TAPE HEADS

We are gradually obtaining nore information bout the Truvox tape heads we have, we are ingenlous way so that winding may be coupled either in parallel or in seriea depending whether high or low impedance is required. We also have matching erase heads and now offer these in pairs, 1 record and 1 erase head. Price of th track 45p per pair, 4 track 75 p per pair. Pai

REED SWITCH COILS
These are solenoids wound on moulded tormera of the correct shape and dimensions to tak standard reed switches. They have printed circui board mounting. 8 ix types avaitsble:-
RCl takes 1 reed-Operates $10-15 \mathrm{~V}$ - 600 ohm 80 m
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Miniature mains driven blower centrifugal type blower unit by Woods, powerful but specially induction motor with specially buil tusnone bearings. Overall size of blower is spprox. 4 in $\times 4!$ in $x 4 i n$. When mounted by its flange air is blown into the equipment but to suck air out mount it from the centre using a clamp, ideal for cooling electrica equipment, or fiting into a cooker hood. nlm drying etc., etc. A real bargain at $81-85$.
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This is a fully gereened intermediate frequency module for amplification and detection of f.m. signala at 10.7 HMz and a.m. signals at 470 kHz . The first stage is used as an
i.f. amplifter for f.m. and a sell oscillating mixer for a.m

100 for $268 \cdot 50$. With connection diagram.
TANGENTIAL HEATER UNITS


This heater unit is the very latest type, most and blower heaters costing \& 15 sitd in Hoover have a few only. Comprises motor, impeller 1, 2 and 3 kW and with thermal ang switching 1,2 and 3 kW and with thermal aafety cut-out Can be fitted into any metal lined case or cabinet Only need control switch, $\mathbf{8} \mathbf{8} 50$. 2 KW Model as above except $2 \mathrm{kilowatts}$, Don't miss this. Control $8 w i t c h, 85 \mathrm{p}$. P. \& P. 40 p

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Made by smitha these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13 A nocket. 2 completely adjustable time periods per 24 hours, 5 A change-over contacts will switch cl rcuit on or off during these periods


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