

Why take the risk?

of damage to expensive transistors and integrated circuits, when soldering?

Use Antex low-leakage soldering irons

220-240 Volts or

0-240 Volts or 100-120 Volts Model X25

The leakage current of the NEW X25 is only a few microamps and cannot harm the most delicate equipment even when soldered "live". Tested at 1500v. A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder" any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages.

Fitted long-life iron-coated bit 1/8". 2 other bits available 3/32" and 3/16".

Totally enclosed element in ceramic and steel shaft Bits do not "freeze" and can easily be removed

PRICE: £1.75 (rec. retail) Suitable for production work and as a general purpose iron

Model CCN 220 volts or 240 volts

The 15 watt miniature model CCN. also has negligible leakage. Test voltage 4000v. A.C. Totally enclosed element in ceramic shaft. Fitted long-life iron-coated bit 3/32"

> 4 other bits available 1/8", 3/16" 1/4" and 1/16"

PRICE: £1.80 (rec. retail)

OR Fitted with triple-coated, (iron, nickel and Chromium) bit 1/8"

PRICE: £1.95 (rec. retail)

A SELECTION OF OTHER SOLDERING EQUIPMENT.



Miniature 15 watt soldering iron fitted 3/32" ironcoated bit. Many other bits available from 3/64" to 3/16". Voltages 240, 220, 110, 50 or 24 PRICE: £1.70 (rec. retail)

MODEL CN2

Miniature 15 watt soldering iron fitted with nickel plated bit 3/32". Voltages 240 or 220. PRICE. £1.70 (rec. retail)



18 Watt miniature iron, fitted with long life ironcoated bit 3/32". Voltages 240, 220 or 110. PRICE. £1.83 (rec. retail)



contains 15 Watt miniature iron fitted with 3/16" bit, 2 spare bits 5/32" and 3/32", heat sink, solder, stand and "How to Solder" booklet.

> PRICE £2.75 (Rec. retail)

MODEL SK.2 KIT

contains 15 Watt miniature iron fitted with 3/16" bit. 2 spare bits 5/32" and 3/32",

heat sink, solder and booklet"How to Solder



PRICE £2.40 (Rec. retail)

MODEL

MES.KIT Battery-operated 12v. 25 watt iron fitted with 15' lead and 2 heavy clips for connection to car battery. Packed in strong

plastic wallet with booklet "How to Solder." PRICE £1.95

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VOLUME 9 No. 2 FEBRUARY 1973

CONSTRUCTIONAL PROJECTS	
P.E. TRIFFID I.C. RADIO by F. R. Heath An easy to build inexpensive portable a.m. radio using the latest integrated circuit	120
BIOLOGICAL AMPLIFIER by D. Bollen A brain rhythm frequency meter and a cardiophone	126
P.E. SOUND SYNTHESISER—1 by G. D. Shaw A comprehensive and versatile instrument for the experimenter in sound	140
P.E. DIGI-CAL—8 by R. W. Coles Logic and construction of the adder board	148
GENERAL FEATURES	
AUDIO FREQUENCY DISCRIMINATOR by G. F. A. Hoffman de Visme Use of switching circuits for frequency separation	133
DESIGNING WITH I.C.s—5 by A. Foord Operational amplifiers with power stages	157
INGENUITY UNLIMITED Proximity Switch—Sound/Light Modulator	165
NEWS AND COMMENT	
EDITORIAL—The Whole And The Parts	119
SPACEWATCH by Frank W. Hyde Ecological studies from space and India's space programme	136
REPORT FROM AUSTRALIA by J. M. Waldie F.M. Broadcasting proposals—Sydney audio show—Optical communications	139
REPORT FROM AUSTRALIA by J. M. Waldie F.M. Broadcasting proposals—Sydney audio show—Optical communications INDUSTRY NOTEBOOK by Nexus What's happening inside industry	139 146
F.M. Broadcasting proposals—Sydney audio show—Optical communications INDUSTRY NOTEBOOK by Nexus	
F.M. Broadcasting proposals—Sydney audio show—Optical communications INDUSTRY NOTEBOOK by Nexus What's happening inside industry ELECTRONORAMA	146
F.M. Broadcasting proposals—Sydney audio show—Optical communications INDUSTRY NOTEBOOK by Nexus What's happening inside industry ELECTRONORAMA Focus on the new satellite-communication aerial at Goonhilly NEWS BRIEFS	146 147
F.M. Broadcasting proposals—Sydney audio show—Optical communications INDUSTRY NOTEBOOK by Nexus What's happening inside industry ELECTRONORAMA Focus on the new satellite-communication aerial at Goonhilly NEWS BRIEFS Computer '72—High Speed Printer using a Laser BOOK REVIEWS	146 147 154

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AC107		AD162 AD161 8	0.88	BC148 BC149	0.10	BD137	0.45	BF188	0.40	OC19	0.35	2G371	0.16	2N2219	0.20	2N3054	0.46	2N4059	0.10
AC118		AD161 6		BC150	0·12 0·18	BD138 BD139	0 · 50 0 · 55	BF194 BF195	0·12 0·12	OC20 OC22	0 · 63 0 · 38	2G371B 2G373	0·12 0·17	2N2220 2N2221	0.22	2N3055 2N3391	0.50	2N4060 2N4061	0·12 0·12
AC117	7K 0.20		0.55	BC151	0.20	BD140	0 - 60	BF196	0.14	OC23	0.42	2G374	0.17	2N2222	0.20	2N3391A	0.16	2N4062	0-12
AC125		ADT140		BC152	0.17	BD155	0.80	BF197	0.14	OC24	0.56	2G377	0.30	2N2368	0.17	2N3392	0.14	2N4284	0.17
AC126		AF114 AF115	0-24	BC153 BC154	0.28	BD175 BD176	0-60	BF200 BF222	0 · 45 0 · 95	OC25 OC26	0·38 0·25	2G378 2G381	0·16 0·16	2N2369 2N2369A	0.14	2N3393 2N3394	0-14	2N4285 2N4286	0·17 0·17
AC127		AF116	0.24	BC157	0.18	BD177	0-65	BF257	0.45	OC28	0.50	2G382	0.16	2N2411	0.24	2N3395	0.17	2N4287	0.17
AC128	3 0 - 17	AF117	0.24	BC158	0 12	BD178	0.65	BF258	0.60	OC29	0.50	2G401	0.80	2N2412	0.24	2N3402	0.21	2N4288	0.17
AC132		AF118	0.35	BC159	0.12	BD179	0.70	BF259	0.85	OC35	0 · 42	2G414	0.30	2N2646	0.47	2N3403	0.21	2N 4289	0.17
AC134 AC137		AF124 AF125	0·30 0·25	BC160 BC161	0 · 45 0 · 50	BD180 BD185	0 - 70 0 - 65	BF262 BF263	0 - 55	OC36 OC41	0·50 0·20	2G417 2N388	0·25 0·85	2N2711 2N2712	0 · 21 0 · 21	2N3404 2N3405	0.28	2N4290 2N4291	0·17 0·17
AC141		AF125	0.28	BC167	0.12	BD186	0.65	BF270	0.35	OC42	0.24	2N388A	0.55	2N2714	0.21	2N3414	0.15	2N4291 2N4292	0.17
AC141		AF127	0.28	BC168	0 12	BD187	0.70	BF271	0.30	OC44	0.15	2N404	0.20	2N2904	0.17	2N3415	0.15	2N4293	0.17
AC142		AF139	0.30	BC169	0.12	BD188	0.70	BF272	0.80	OC45	0.12	2N404A	0.28	2N2904A		2N3416	0 - 28	2N5172	0.12
AC142 AC151		AF178 AF179	0·50 0·50	BC170 BC171	0·12 0·14	BD189 BD190	0·75 0·75	BF273 BF274	0·35 0·35	OC70 OC71	0 10	2N524 2N527	0·42 0·49	2N 2905 2N 2905 A	0.21	2N3417 2N3525	0·28 0·75	2N5457 2N5458	0.32
AC154		AF180	0.50	BC171	0.14	BD195	0.85	BFW10	0.60	OC72	0.14	2N598	0.42	2N 2906	0.15	2N3646	0.09	2N5459	0.40
AC158	0.20	AF181	0 45	BC173	0.14	BD196	0.85	BFX 29	0.27	OC74	0.14	2N599	0-45	2N2906A	0.18	2N3702	0.10	28301	0.50
AC156		AF186	0 · 45	BC174	0.14	BD197	0.90	BFX84	0 . 22	OC75	0.15	2N696	0.12	2N2907	0.20	2N3703	0.10	28302A	0.42
AC157		AF239 AL102	0·87 0·65	BC175 BC177	0.22	BD198 BD199	0·90 0·95	BFX85 BFX86	0·30 0·22	OC76 OC77	0·15 0·25	2N697 2N698	0·13 0·24	2N2907A 2N2925	0.22	2N3704 2N3705	0·11 0·10	28302 28303	0 · 42 0 · 55
AC166		AL103	0.65	BC177	0.19	BD200	0.95	BFX87	0.24	OC81	0.15	2N699	0.85	2N2923 2N2924	0.14	2N3705 2N3706	0.09	28304	0.70
AC167	7 0.20	A8Y26	0.25	BC179	0.19	BD205	0.80	BFX88	0.22	OC81D	0.15	2N706	0.08	2N2925	0.14	2N3707	0.11	28305	0.84
AC168		ASY27	0.80	BC189	0.24	BD206	0.80	BFY50	0.20	OC82	0.15	2N706A	0.09	2N2926 (2N3708	0.07	28306	0.84
AC169		ASY28 ASY29	0 · 25 0 · 25	BC181 BC182	0.24	BD207 BD208	0·95 0·95	BFY51 BFY52	0.20	OC82D OC83	0.15	2N708 2N711	0.12	2N2926 (0.12	2N3709 2N3710	0.09	28307 28321	0·84 0·56
AC177		ASY50	0.25	BC182L	0.10	BDY20	1 00	BFY53	0.17	OC84	0.20	2N717	0.35	2142820 (0.11	2N3711	0.09	28322	0.42
AC178	0 . 28	ASY51	0 25	BC183	0.10	BF115	0.24	BPX25	0.85	OC139	0.20	28718	0.24	2N2926 (0)	2N3819	0.28	28322A	0.42
AC179		A8Y52	0.25	BC183L	0.10	BF117	0.45	B8X19	0.15	OC140	0.20	2N718A	0.50	0310000	0.10	2N3820	0.50	28323	0.56
AC180		ASY54 ASY55	0 · 25 0 · 25	BC184 BC184L	0·12 0·12	BF118 BF119	0.70	BSX 20 BSY 25	0·15 0·15	OC169 OC170	0.25	2N726 2N727	0·28 0·28	2N2926 (0·10	2N3821 2N3823	0·35 0·28	28324 28325	0.70
AC181		ASY56	0.25	BC186	0.28	BF121	0.45	BS Y 26	0.15	OC171	0.25	2N743	0.20	2N2926 (2N3903	0.28	28326	0.70
AC181		ASY57	0.25	BC187	0.28	BF123	0.50	BSY27	0.15	OC200	0.25	2N744	0.20		0.10	2N3904	0.30	28327	0.70
AC187		A8Y58	0.25	BC207	0.11	BF125	0 - 45	BSY28 BSY29	0.15	OC201 OC202	0.28	2N914 2N918	0.14	2N3010	0.70	2N 3905	0.28	28701	0·42 0·40
AC187		ASZ21 BC107	0 - 40	BC208 BC209	0·11 0·12	BF127 BF152	0·50 0·55	BS Y 29	0·15 0·18	OC202 OC203	0 · 28 0 · 25	2N918 2N929	0·30 0·21	2N3011 2N3053	0·14 0·17	2N 3906 2N 4058	0 27	40361 40362	0.45
AC188		BC108	0.09	BC212L	0.11	BF153	0.45	BSY39	0.18	OC204	0.25	2N930	0.21	2210000		211 20110		40002	•
ACY1		BC109	0.10	BC213L	0.11	BF154	0.45	BSY +0	0.28	OC205	0.35	2N1131	0.20						
ACY1		BC113 BC114	0·10 0·15	BC214L BC225	0·14 0·25	BF155 BF156	0.70	BSY41 BSY95	0 · 28 0 · 12	OC309 P346A	0·40 0·20	2N1132 2N1302	0·22 0·14		DIOL	ES AND I	RECTIE	IERS	
ACY2		BC115	0.15	BC226	0.35	BF157	0.55	B8 Y95 A	0.12	P397	0.42	2N1302	0.14	A A 119	0.08	BY133	0.21	OA10	0.35
ACY2	1 0.20	BC116	0.15	BCY30	0.24	BF158	0.55	Bu105	2.00	OCP71	0.43	2N1304	0.17	AA120	0.08	BY164	0.50	OA47	0.07
ACY2		BC117	0.15	BCY31	0.26	BF159	0.60	CILLE	0.50	ORP12	0.43	2N1305	0·17 0·21	AA129	0.08	BYX38/3		OA70	0.07
ACY2		BC118 BC119	0·10 0·30	BCY32 BCY33	0·80 0·22	BF160 BF162	0-40	C400 C407	0 30	ORP60 ORP61	0·40 0·40	2N1306 2N1307	0.21	AAY30 AAZ13	0 · 09 0 · 10	BYZ10	0 42	OA79 OA81	0.07
ACY2		BC120	0.80	BCY34	0.25	BF163	0.40	C424	0 20	ST140	0.12	2N1308	0.23	BA100	0.10	BYZII	0.30	OA85	0.09
ACY3		BC125	0 12	BCY70	0.14	BF164	0.40	C425	0.50	ST141	0.17	2N1309	0.23	BAH6	0.21	BYZ12	0.30	OA90	0.06
ACY3		BC126 BC132	0 18 0 12	BCY71 BCY72	0·18 0·14	BF165 BF167	0 - 40	C426 C428	0.35	TIS43 UT46	0.30	2N1613 2N1711	0 · 20 0 · 20	BA126 BA148	0·22 0·14	BYZ13 BYZ16	0 · 25 0 · 40	OA91 OA95	0.06
ACY3		BC132	0.12	BCZ10	0.20	BF173	0.22	C441	0.30	2G301	0.09	2N1889	0.32	BA154	0.12	BYZ17	0.35	OA200	0.08
ACT3	6 0.28	BC135	0.12	BCZ11	0.25	BF176	0.35	C442	0.30	2G302	0.19	2N1890	0.45	BA155	0.14	BYZ18	0.35	OA202	0.07
ACY4		BC136	0.15	BCZ12	0.25	BF177	0.35	C444	0.85	2G303	0.19	2N1893	0.37	BA156	0.13	BYZ19	0.28	8D10	0.05
ACY4		BC137 BC139	0·15 0·40	BD121 BD123	0 · 60 0 · 65	BF178 BF179	0.80	C450 MAT100	0 22	2G304 2G306	0.24	2N2147 2N2148	0·72 0·57	BY100 BY101	0·15 0·12	CG62 (Eg) OA9	1	SD19 IN34	0 - 05
AD13		BC140	0.80	BD123	0.60	BF180	0.30	MAT101	0.20	2G308	0.35	2N2160	0.80	B¥ 105	0.17	(136) OV9	0.05	IN34A	0.07
AD14	0 0.48	BC141	0.30	BD131	0.50	BF181	0.30	MAT120	0.19	2G309	0.35	2N2192	0.35	BY114	0.12	CG651		1N914	0.06
AD14 AD14		BC142 BC143	0.80	BD132 BD133	0 · 60 0 · 65	BF182 BF183	0·40 0·40	MAT121 MPF102	0.20	2G339 2G339A	0.20	2N2193 2N2194	0 35 0 35	BY 126 BY 127	0·14 0·15	(Eq) OA7 OA79	0. 0.08	1N916 IN414B	0 · 06 0 · 06
AD14		BC145	0.45	BD135	0.40	BF184	0.25	MPF104	0.37	2G344	0.18	2N2217	0.22	BY128	0.15	OA5	0.35	18021	0.10
AD16		BC147	0.10	BD136	0.40	BF185	0.30	MPF105	0.37	2G345	0.16	2N2218	0.20	BY130	0.18	OA58L	0 - 21	18951	0.08

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pages out

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C 8	10	Reed Switches	0.50				
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100 0 25	0.33	0.47	0.47	0.50	0.58	0.63	1.40
200 0 35	0.37	0.49	0.49	0 57	0.61	0.75	1.60
400 0 43							
600 0 - 53	0.57	0.68	0.68	0.77	0.97	1 - 25	
800 0 63	0.70	0.80	0.80	0.90	$1 \cdot 20$	1.50	4.00

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100 0 · 04	0.06	0.05	0.13	0.16	0.23	0.75
200 0 05	0.09	0.06	0.14	0.20	0.24	1.00
400 0 06	0.13	0.07	0.20	0.27	0.37	1.25
600 0 07	0.16	0.10	0.25	0.34	0.45	1.86
800 0 10	0.17	$0 \cdot 11$	0.25	0.37	0.55	2.00
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T4	8 2G381T	OC81
75	8 2G382T	OC82
T6	8 2G344B	OC44
T7	8 2G345B	OC45
T8	8 2G378	OC78
T9	8 2G399A	2N1302
T10	8 2G417	AF117
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1~24	25-9	9	3	00 up
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U45

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NKT6917	27p	2N706	8p	NKT212	23p	NKT275	21p		
NKT 10339	23p	2N914	15p	NKT213	23p	NKT278	18p		
NKT10419	17p	2N918	28p	NKT214	21p	NKT301	70p		
NKT10439	25p	2N930	22p	NKT215	19p	NKT302	85p		
NKT10519	20p	2N 1990	22p	NKT217	48p	NKT303	70p		
						NKT304	76p		



S.T.C. RELAYS—BRAND NEW

PE .	CONTACT FORM	NOMINAL COIL VOLTAGE	COIL RESISTANCE (OHMS)	PRIC EACH					
ARO ABO	4 CHANGEOVER 4 CHANGEOVER	6V d.c. 48V d.c.	52 2,500	88 02 88 02					

TYPE
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SL7622715

CONTACT FORM 3 Pole on/off 2 Pole C/O

COIL VOLTAGE 12V a.c. 220V a.c.



CONTACT
FORM
Single Pole C/O
Single Pole C/O
Single Pole C/O
12V d.c.
18V d.c.

UNISELECTOR SWITCHES

UNISELECTOR SWITCHES
6 bank 25 way 75 coil 50V d.c. operation
Mounted on Modular Type Chassis with front
panel containing 20 illuminated Push Button
Switches Completely wired for operation
Price 115
P. A.P. 20.55



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2½ × 1 in 2 for 12p

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5 × 3½ in (plain) —

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13c × 3½ in (plain) —

13

IN4001 IN4002

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Sinclair Project 60



Active Filter Unit

(A.F.U.)

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The value of an efficient filtering system cannot be over emphasized in these days of very high quality reproduction since there are so often occasions where its use can mean the difference between comfortable and uncomfortable listening. On the low pass side the Sinclair A.F.U. will effectively reduce hiss from radio or tape, cut out heterodyne whistles on A.M. reception, greatly reduce record surface noise and other imperfections; on the high-pass side it will cut out motor rumble and other spurious low frequency intrusion. The unit is for use between pre-amp (including tape pre-amps) and power amplifiers, and operates in two sections, both stereo. The cut-off frequencies are continuously variable, and since attenuation in the rejection band is rapid (12dB/octave) there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is as easy to mount as the stereo 60 pre-amp/control unit which it matches in styling, along with the Stereo FM Tuner.

SPECIFICATIONS

The A.F. U employs two Sallen and Key type active filter stages, one rumble (high pass) and one scratch (low pass). The two stages use complementary transistors to minimise distortion.

Supply voltage: 15 to 35 volts Current 3mA maximum.

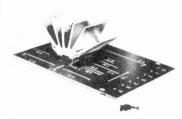
Gain at 1kHz: Filters flat 0 98 (—0.2 dB)

HF cut off: (—3dB) variable from 28 kHz
to 5 kHz at 12 dB/octave.

LF cut off: (—3dB) variable from 25Hz to 100Hz at 12dB/octave.

Distortion: at 1kHz (35 volt supply) 0.02% at rated output.

Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-ficonstructors with the IC, 10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC, 12, a most exciting advance over our griginal unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC, make possible! It is the equivalent of a 22 transaction.

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). 6-80. Frequency Response: 5Hz to 100KH2±1dB. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90dB (1,000,000,000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22×45×28mm including pins and heat sink.

Manual available separately 15p post-free

With FREE printed circuit board and 40 page manual. £2.98 Post free

The easy way to buy, and build Project 60 Project 605 is one pack containing one P25, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all

Project 605

Project 605 is one pack containing one P25, two 230's, one Stereo 60 and one Masterink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Taus all 30 identing and hunting for the odd part is eliminated. You will be able to add further Project 60s modules as they become available adapted to the Project 605 method of connecting.

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Z.30 & Z.50 power amplifiers

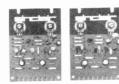
Built, tested and guaranteed with circuits and instructions manual z.30 £4.48 z.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8 Ω) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may he used in a far wider range of applications.

SPECIFICATIONS (2.50 units are interchangeable with 2.30s in all applications).—Power Outputs:

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts
Z.50 40 watts R.M.S. into 3 ohms using 40 volts 30 watts R.M.S. into 8 ohms using 50 volts.

Frequency response: 30 to 300,000Hz±1dB. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8 Ω). For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57mm.



Stereo 60 Pre-amp/control unit

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount.

SPECIFICATIONS—Input sensitivities: Radio — up to 3mV. Mag. p.u. 3mV correct to R.I.A.A. curve ±1dB 20 to 25,000 Hz. Ceramic p.u. — up to 3mV: Aux — up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE+12 to —12dB at 10KHz: BASS +12 to —12dB at 100Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.



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£9.98

Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in LC. Tuning range: 87.5 to 108MHz. Sensitivity: 7μV for lock-in over full deviation. Squelch level: Typically 20μV. Signal to noise ratio: >65dB. Audio frequency response: 10Hz = 15KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M.S. maximum Operating voltage: 25–30VDC. Indicators: Stereo on: tuning. Size: 93 x 40 x 207mm



Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential

Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

F.M. Stereo Tuner (£25) & A.F.U. (£5.98) may be added as required.







Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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AC128	11p	AUTH		BFY50	15p			2N 1304	25p		
AC176	25 p	BC 107		BFY51			13p		25p		
AC141K	20p	BC108		BSY95A	12p	OC83	20p	2N2646	47p		
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				ME0402	18p	OC200	25p	2N3053	20p	IN 4001	4p
AD14	40p	BC154		ME0404	14p	OC201	25p	2N3055	49p	IN4002	4p
AD150	44p	BC168		ME4401	10p		25p	2N3702	12p	IN4003	5p
ADIGI M	P55p	BC169		ME4102	12p	OC28	30p	2N3703	12p	IN4004	7p
ADIO5	-	BC182L	8ր	ME6002	14p	OC29	36p	2N3704	12p	OA90	бр
AF114	15p	BC183L	8p	ME6101	14p	OC35	25p	2N3705	12p	0.491	бр
AF115	15p	BC184L	8p		15p	OC36	36p	2N3706	10p	OA200	10p
AF116	15p	BC212L	8p		32p	TIP29A	48p	2N3707	10p	OA202	8p
AF117	15p	BC214L	8p		34p	TIP30A	55p	2N3708	9p	1844	10p
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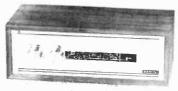
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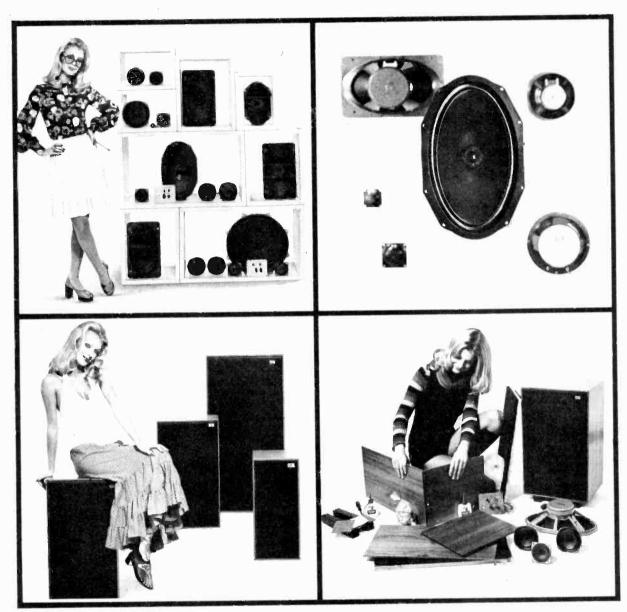
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100μΑ	£2.35	10 amp	£2.1
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$50\mu A$	£3.95	150V d.e	£3.10	50μA		
$50-0-50\mu A$	£3.40	300V d.c	£3-10	30-0-30	4A	
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5mA	£3.10	20 amp. a.c.				
10mA	£3-10	30 amp. a.c				
		as ampraici		10mA .		
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Type MR.52P.		quare Fronts.
50μA 50-0-50μA 100μA 100-0-100μA.		10V d.c
$50-0-50\mu A$	£2-85	20V d.c 22-20
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5mA	£2.20	S Meter 1mA. £2.30
10mA	£2-20	VU Meter £3-50
50mA 100mA	£2-20	I amp. a.c *22-20
100mA	£2-20	5 amp. a.c \$2.20
500mA	£2-20	10 amp. a.c *£2.20
lanıp,	£2-20	20 amp. a.c *22.20
5 anip	£2.20	30 amp. a.c *22.20

5			
5	Type MR.65P.	3;in. ×	3; in. Fronts
0	50μA	£3.70	110V d.c £2.
0		£3-00	20 V d.c 22.
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	100-0-100µA.	\$2.90	
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5	100mA	£2-40	VU Meter £3.
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5	1 amp	£2-40	100mA a.c *£2-4
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#1.55 F	2 amp	£1.75
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200μA	£2.05	300 V d.c	£1.85
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5 amp. d.c. . .

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	30 amp	
	50 amp	£2-15
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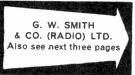


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MODEL TH-12

Overload pro-20,000 O.P.V. Overload pro-tection. Slide switch selector. 20,000 of the tection. Slide switch selector. 0/0·25/2·5/10/50/250/1,000V d.c. 0/10/50/250/1,000V a.c. 0/50µA/25/250mA d.c. 0/3K/ 30K/300K/3 meg. -20 +50dB. #4.97 Post Inn

MODEL TE-300, 30,000 O.P.V. Mirror scale, overload protection 0/0-6/3/15/60/300/ 0/6/30/120/600/ d.c. 1,200 V a.c. 0/30μA/6mA/ 60mA/300mA/600mA. 0/8K/ 80K/800K/8 meg. ohm -20 to -63dB. **25-97**, Post 15p.





PT.438 20k Ω/V d.c. 8k Ω/V Mirror scale a.c. Mirror scale. 0·6/3/12/30 /120 / 600 V d.c. 3/30/120/600 V a.c. 50/600μA/60/ 600mA. 10/100 K/ 1 Meg/10 Meg Ω.

-20 to +46dB. £6.97, Post 12p.

TMK MODEL TW-50K TMK MODEL TW-50K 46 angres, mirror scale, 50 k/V d.c. 5 k/V a.c. D.c.: Volts (125, 025, 125, 52.5, 5, 10, 25, 50, 125, 250, 500, 1,000V. A.c. Volts: 1-5, 30, 5, 10, 10,00V. A.c. 50, 500, 10,00V. A.c. Contract: 25, 50 c/4, 2-5, 5, 2-5, 5, 2-50, 2-50, 500, 10,000V. B.c. Current: OK, 100K, 1, 1 M kG, 10 M BG \(\Omega\$ \) Contract: 10K, 100K, 1 M kG, 10 M BG \(\Omega\$ \) Decibels: -20 to +81-5 dB. 28-50. Post 17 p. 28-50. Post 17p.



MODEL K228A Taut band suspension. suspension.
Overload protection.
Polarity reversing switch.
30,000 O.P.V. 69 69 69

0/0-5 / 2-5 / 15 0/03/23/10/100/2,500V d.c. 0/15/50/150/ 50/250/5000V a.c. 0/50µA/5/50/150/500mA/ 5A d.c. 0/3K/300K/3meg. **28-95.** Post 20p.



HIOKI MODEL 700X

100,000 O.P.V. Overload protection. Mirror scale: 0.3/0-6/1-2/1-5/3/6/12/30/60/ 120/300/600/1,200V d.c. 1-5/3/6/12/30/60/150/300/

| 15/36/12/2006/14/36/30/60/12/2006 | 15/36/μA/3/6/30/60/150/300mA | 6/12 amp. d.c. 2K/200K/2 2 Meg/20 Meg ohm —20 to +63dB. £13-50. Post 20p.



MODEL C-7080 EN Giant 6in mirror scale 20,000 O.P.V.

20,000 O.P.V. 0/0·25/1/2·5/10/50/250/ 1,000/5,000V d.c.0/2·5/10 /50/250/1,000/5,000V a.c. 0/50μA/1/10/100/500mA/ 10 amp. d.c. 0/2 K/200 K/ 20 meg. 20 to +50dB. 3.95. Post 35p

U4312 MULTIMETER

U4312 MULTIMETER
Extremely sturdy instrument
for general electrical use
667 O.P.V.
9/0-3/1-5/7-3/30/60/150/300/
600/900V d.c. and 75mV.
9/0-3/1-5/7-5/30/60/150/300/
600/900V a.c.
9/300µA/1-5/6/15/60/150
600MA/1-5/6 amp. d.c.
9/1-5/6/15/60/150/600MA/
1-5/6 amp. a.c.



£13-95.

Selected TEST EQUIPMENT

FTC-401 TRANSISTOR TESTER

FTC-401 TRANSISTOR TRSTI Full capabilities for mea-suring A, B and ICO. npn or pnp. Equally adapt-able for checking diodes. Supplied complete with in-structions, battery and leads. £7:50. Post 20p.



Models-100TR MULTIMETER/TRANSISTOR TESTER. 100,000 O.P.V. mirror scale/overload protec-tion. 0/0-12/0-6/3/12/30/120/ 600V d c 0/6/30/120/600V a.c 600V d.c. 0/6/30/120/600V a.c. 0/6/30/120/600V d.r. 0/12/600/24/12/3000m A/12 amp. d.c. 0/10 K/1 MEG/1/00 MEG. —20 to + 50dB. 0-01-2 MFD. Transistor tester measures Alpha, beta and Ico. Complete with batteries, instructions and leads. \$13-50. Post 25p.



MODEL 449A IN CIRCUIT TRANSIS-TOR TESTER

Checks true a.c. beta in/out. Checks Icbo. Checks diodes in/out. Checks SCR, etc. Beta H110-500 LO 2-50 Icho 0-5000µA

220/240V a.c. operation. £17-50. Post 25p

TE-20D RF SIGNAL GENERATOR



200

CHECKED

Accurate wide range signal generator covering and generator covering properties of bands. Directly collibrated Variable R.F. attenuator, and to output tenuator, and to output tenuator and tenuato Accurate wide range sig

MODEL LASS FET

MODEL L-55 FET V.O.M. 10put impedance 10 meg ohms. 0/0-3/1-2/6 30/120/600V d.c. 0/3/12/ 60/120/600V d.c. 0/18/100K/ 120mA d.c. 0/1K/100K/ 10 meg/100 meg ohms. £15-97. Post 25p.



. .

CI-5 PULSE OSCILLO-SCOPE For display of pulsed and periodic waveforms in electronic circuits.VERT. AMP. Bandwidth 10MHz. AMP. Bandwidth 10M Hz.
Sensitivity at 100 Hz.
V. RMS/mm. 0-1-25;
HOR. MMP. Bandwidth
500 kHz. Sensitivity at
0-3-25; Pre-set triggered awere 1-3,000 µcc.;
free running 20-200,000 Hz in filter ranges.

Calibrator pips. 220mm × 430mm, 115-230V a.c. operation. 360mm

TO-3 PORTABLE OSCILLOSCOPE



3in tube, Y amp. Sensitivity
0-1V p-p/CM. Bandwidth
1-5cps-1-5MHz. Input
imp. 2 meg Ω 25pF X amp.
sensitivity 0-0V. p-p/CM.
Bandwidth 1-5cps-8006Hz. Input imp. 2 meg Ω 20pF.
Time base. 5 ranges 10cps300kHz. Syuchronisation.
1. Internal/external. Illuminated scale 140mm × 215mm × 330mm. Weight 15ilb. 220/
240V a.e. Supplied brand new with handbook. 240-00. Carr. 50p.

RUSSIAN CI-16 DOUBLE BEAM OSCILLOSCOPE

JMHz Pass Band. Separate Y1 and Y2 amplifiers. Rectangular Jin X sin C.R.T. Calibrated triggered sweep from 0-2u/sec to 100 milli-sec per cm. Free running time base of DHz-1MHz. Built-in time base calibrator and amplitude calibrator and amplitude calibrator with the company of the calibrator and all accessories and instruction main \$37. Carr. paid. 0 0 0 0 0 0



TE-16A Transistorised Signal Generator, 5 ran-ges 400k Hz-30MHz. An inexpensive instrument tions and leads.

27-97. Post 25p.

TRANSISTORISED L.C.R. A.C. MEASURING BRIDGE



A new portable bridge offering ex-cellent range and accuracy at low cost. Ranges: R.

accuracy at low cost. Ranges: R. 10-111 meg Ω. Ranges $\pm 1\%$. Li $\mu H = -1$ 1 meg Ω. 11/1000 6 Ranges $\pm 2\%$. TURNS RATIO 11/1000-11/1000. Anges $\pm 1\%$. Poly Line working at 1,000cps. Operated from 9V 100 μA . Meter indication. Attractive 2 tone metal case. Size 73 in $\times 3$ in $\times 2$ in. 420. Post 25 in. Post 25p.

MODEL TEIS GRID DIP

METER Transistorised. Operates as Grid Dip, Oscillator, Transisturised. Operates as Grid Dip, Oscillator, Absorption Wave Meter and Oscillating Detector. Frequency range 440kHz-280MHz in 6 coils, 500µA meter. 9V battery operation. Size 180mm × 80mm × 40mm

× 40mm. £12-50. Post 20p.



BELCO AF-5A SOLID STATE SIBE
SQUARE WAVE C.R. OSCILLATOR
Sine 18-20,000 Hz.
Square 18-50,000
Hz. Outpit max.
4-10dB (10 K ohms)
Operation internal
batteries. Attractive 2-tone case
7 in × 5in × 25in
Price \$17-50. Carr.
170. 17p.



MODEL MG-100 BINE SQUARE WAVE AUDIO GENERATOR

Range 19-220,000 Hz. Sine Wave 19 — 100,000Hz. 19-220,000

19 — 100,000Hz. Square Wave. Out-put Sine or Square wave 10V. P. to P. Size 180mm × 90mm × 90mm. Operation 220/240V a.c.



DECADE ATTENUATOR Frequency re 0-200kHz.

Attenuator 0-111dB, 0-1dB step. Impedance

ohms. Max. input power 30dBm.

Size 180mm × 90mm × 55mm.

\$12.50. Post 37p.



Post 37p.

TE-65 VALVE VOLTMETER
28 ranges. D.c. volts
1:3-1,300V ac sistance
1:3-1,00V ac sistance
1:3-1,00V

MODEL U4311 SUB-STANDARD
MULTI-RANGE VOLT AMMETER
Sensitivity 330 ohms/Volt
a.c. and d.c. Accuracy 0.5%
d.c. 1° a.c. Scale length 100mm. 0/300/750μA/1·5/3/7·5/15/30/

0/300/7.50µA/1-3/3/7.5/15/30/
7.5/150/300/7.50mA/1-5/3/7.5
amp.d.c. 0/3/7.5/15/30/7.5/15/20/7.5/15/20/7.5/15/20/7.5/15/7.5/15/7.5/15/7.5/15/7.5/15/7.5/15/7.

G. W. SMITH & CO. (RADIO) LTD. Also see opposite page and next two pages



4 Bands covering 550kHz-30MHz. BFO. Built-in Speaker 220/240V a.c. Brand new with instructions, £15.75. Carr. 37p.



UR-1A SOLID STATE COMMUNICATION RECEIVER

4 Bands covering 550kHz-30MHz. FET. 8 Meter. Variable BFO for SSB, Built-in 8peaker, Bandspread, 8ensitivity Control. 220/240V a.c. or 12V d.c. 12∫n×4∫n×7in. Brand new with instructions. \$25, Carr. 37p.

SKYWOOD CX208 COMMUNICATION



North State. Coverage on 5 bands 200-420 kHz and 0-55 to 30MHz. Huntinated slide rule dial. Bandspread. Aerial tuning. BFO, AVC, ANL, "S" meter. AM/CW/SSB. Integrated apeaker and phone socket. Operation 220/240V a.c. or 12V d.c. Size 325 x 256 x 150 mm. Complete with instructions and circuit. #28.50, Carr. 50p.

LAFAYETTE HA-600 SOLID STATE RECEIVER



coverage 150-400kHz, 550 kHz-30MHz, FET front end, 2 mech. fliters, product detector, variable

BFO, noise limiter. 8 Meter, Bandspread. RF Gain. 15in. 9fin. 84in. 18ibs. 220/240V a.c. or 12V d.c. Brand new with instructions. 250. Carr. 50p.



9R59DS COMMUNI-CATION RECEIVER 4 band cover-ing 550kHz-30MHz con-

bandspread on netree electrical tinuous and tinuous and electrical bandspread on 10, 15, 20, 40 and 80 metres. 8 valve plus 7 diode circuit. 4/8 ohn output and phone Jack. SSB-CW. ANL. Variable BFO. 8 meter. Sep. bandspread dial. IF frequency 455kHz. Audio output 1-5W. Variable RF and AF gain controls 115/250V a.c. Size 71n×18ln×10in with instruction manual. 440-50 (zer paid. \$49.50. Carr. paid



EMI LOUDSPEAKERS

Model 350, 13in×8in with single tweeter/crossover, 20-20,000Hz. 15W RMS. Available 8 or 15 ohms. 27:25 each.

20,000Hz. 10W RMS, Available 8 or 15 ohms, £7:25 each. Post 37p. Model 450. 13in×8in with twin tweeter/crossover. 55-13,000Hz. 8W RMS. Available 8 or 15 ohms, £3-62 each. Post 25p.

8/



Can be pan bench mor Basic meter sures 1V d.c Can be panel or bench mounted.

Basic meter measures 1V d.c. but can be used to measure a wide range of a.c.

can be used to measure a wide range of a.c. and d.c. volt, current and ohms with optional plug in cards. Specification: Accuracy; 40.2, ±1 digit. Resolution: ImV. Number of digits: 3 plus fourth overrange digit. Voerrange: 100% (up to 1999). Input Impedance: 1009 Meg ohm. Measuring cycle: 1 per second. Adjustment: Automatic zeroing, full scale adjustment against an internal reference voltage. Overload: to 100V d.c. Input: Fully floating (3 poles). Input power: 110-230V a.c. 50/60 cycles. Overall size: 5½In x 2 ½In x 8 ½In. AVAILABLE BRAND NEW AND FULLY GUARANTEED. 433-50. Carr. 50p.



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Project 60 Package



offers.

2 × Z30 amplifier, stereo 60 pre-amp, PZ5
power supply. £15 98. Carr. 37p. Or with
PZ6 power supply. £15 90. Carr. 37p.
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power supply. £26 926. Carr. 37p.
Transformer for PZ8. £297 extra.
Add to any of the above £4 45 for active
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All other Sinclair products in stock.
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£28.50. Carr. 37p.: Neoteric Amp. £43.96.
Carr. 37p. IC12. £180. P. & P. 10p.
NEW PROJECT 605—£20.97. Carr. 37p.

WHARFEDALE MID-RANGE HI-FI UNITS

As used in world famous system. 5in dia. Impedance 4/8 ohms. High flux ceramic magnet. 20W RMS. Brand new £1.50, Carr. 37p.

SPECIAL OFFER!
GOODMANS
A XIOM 301
Hi-Fi 12in 20W twin cone full
range speaker. 30-16,000 Hz.
16,500 gauss. 8 ohm impedance. Brand new and boxed.
(List price \$21-72.) OUR
PRICE \$12-50 each. Carr. 30p.

EA.41 REVERBERATION AMPLIPIER
Self contained, transistorised, battery operated. Simply plug in microphone, guitar, etc., and output juto your amplioutput into your amplifier. Volume control, depth of reverberation control, walnut cabinet. 7\(\frac{1}{1}\text{in} \times \frac{3}{1}\text{in} \times \frac{4}{1}\text{in}. Post 15p.





SPECIAL OFFER! ROTEL RH700 STEREO

HEADPHONES 20-20,000Hz. 8-16 ohm. (List £9.95). OUR PRICE £6.75. Post 25p.



SPECIAL OFFER! STEREO SPEAKERS

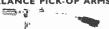
Matched pair of stereo bookshelf speakers. De-luxe teak veneered finish. Slze: 14½in×9in×7½in. 8 ohms. 8W RMS. 16W peak. Complete with DIN lead. £12.95. Carr. 50o.



HA-10 STEREO HEADPHONE

AMPLIFIER
All silicon transistor amplifer operates from magnetic, ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9V battery. Inputs 5MU/100MU. Output 50MW.

SPECIAL PURCHASE! NEAT G30J STATIC BALANCE PICK-UP ARMS



Identical specification to NEAT G30 arm but with two-tone chrome and black finish. Complete with head shell, pick-up rest and plug in phono leads. BRAND NEW--FULLY GUARANTEED. ONLY 48-95, Post 25p.



ARF-300 AF/RF
BIONAL GENERATOR
All transitorised, compact, fully portable. AF sine wave
18 Hz to 220 KHz. AF square wave 18 Hz to 100
KHz. Output sine/square
10v. P.P. RF 100 KHz to 200 MHz. Output 1v. maxinum. Operation 220/240v.
AC. Complete with instructions and leads. tions and leads \$29.95. Post 50p.

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5	GXC40 Cassette Rec	 £82-25
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GENUINE BARGAIN!



KOSS SP.3XC STEREO HEADPHONES

Response 10-15.000 Hz. 10-15,000 Hz.
Impedance 4-6 ohms.
Brand new.
Boxed and fully g'teed
(List £9-50). OUR
PRICE £6-50. Post 25p.

1021 STEREO LISTENING

STATION
For balancing and gain selection of loudspeakers with additional facility for stereo headphone

ior stereo headphone switching. 2 gain controls, speaker on-off slide switch, stereo headphone sockets. 6in×4in×2iin. 22:25. Post 15p.



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mr/ MIXER PREAMPLIFIER
5 microphone inputs each with
individual gain
facilities. Battery operated. 9 jin x 3 in.
Inputs Mics: 3 x 3 mV 50K: 2 x 3 mV 600
ohm. Phono neg. 4 mV 50K. Phono ceramic
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88-97. Post 20p.



TE-1035 STEREO HEADPHONES

HEADPHONES
Low cost high performance stereo headphones.
Foam rubber ear cups.
Adjustable head-band.
6 ohm impedance. 25—
18,000Hz. With lead and stereo jack plug. ONLY £1.97. Post 12p.

NEW GARRARD MODULES



Popular range of tiarratu with Shure cartridge fitted in deluxe plinth with hinged lid. SP25 III Module/M75-6 . \$23.50 AP76 Module/M75-6 AP96 Module/M75-6 Zero 1008 Module/M93E 252-60 Carr. 50p extra any item.

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controls. 8 ohm impedance 20-20,000cps Complete with spring lead & stereo jack plug \$7.97. Post 12p.

DOLBY SYSTEM NOISE REDUCTION UNIT



Improves the performance of cassette and semi-professional recorders. Reduces tape hiss by 3dB at 600Hz, 6dB at 1200Hz and 10dB for all frequencies above 3000Hz. Controls for input levels and noise reduction on record and Input levels and noise reduction on record and replay. 2 meters for Dolby level. Off tape monitoring. Frequency response: 20Hz to 15kHz±1dB 19kHz-35dB. Size 15kIn×9in×3jin. A.c. 200/250V.

OUR £32-50

Carr. 50p.

Carr. 50p.

HOSIDEN DHO-28 STEREO HEADPHONES



EREO HEADPHONES
Wonderful value
and excellent performance combined.
Adjustable headband. 8 ohm impedance. 20-12,000
cps. Complete with
lead and plug. lead and plug. ONLY \$2-37.

CASSETTES. Top quality Hi-Fi Low Noise in Library cases.

3 for 75p. 3 for £1-05 3 for £1-85 10 for £3:30 10 for 24-20

C120 Tape Head Cleaner 30p each. Post 10p extra.

RPECIAL PURCHASE! LEAK MINI-SANDWICH SPEAKERS

guaranteed. 8W, 8 ohm. Teak finish. (Rec. list £59.50 pr.) OUR PRICE £39.50 pr. Carr. £1.00. Brand new and fully guaranteed. 8W, 8 ohm. Teak finish.



TE 1018 DE J. U.S.

TE 1018 DE-LUXE MORO HIGH IMPE-DANCE HEADSET Sensitive, soft earps adjustable headband. Magnetic, impedance 2,600 ohms. £1.97. Post 15p.



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FANTASTIC OFFER!

NIKKO TRM50



17+17W r.m.s. stereo amplifier with inputs for Magnetic and Crystal phono, Tuner, Tape, Aux and Tape Monitor. Outputs for two pairs of stereo speakers and tape. Stereo headphone socker Full range of controls including loudness control, scratch filter. Full range of controls including lo etc. Size 13in × 9½in × 3½in.

Unrepeatable offer—limited stocks!

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NIKKO TRM50 17+ 17W rms stereo amplifier, BSR MP60, plinth and cover, Goldring G800 cart-ridge, pair of Linton 2 speakers and all leads.

£104.90

Carr. and

Amplifier, Turntable, pair

Wharfedale

OUR PRICE

Carr, and Ins. £1.27

Linton Linton

LEAK DELTA 30 SYSTEM



Leak Delta 30 stereo amplifier, Goldring GL75, plinth, cover and G800 cartridge. Pair of Leak 150 speakers and all leads.

OUR PRICE £122.50

Carr. and Ins. £1:50

AMSTRAD 8000 II **SYSTEM**

£105

WHARFEDALE

LINTON SYSTEM

Amstrad 8000 II 7+7W amplifler. BSR MP60, plinth and cover, Goldring G800 cartridge, pair of Apollo speakers and all leads.

£45.50 PRICE

Ins. €1 Amplifier only, £14.50. Carr. 50p

TELETON SAQ206B SYSTEM

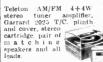
Teleton SAQ206B 8+8W amplifier. BSR MP60 plinth and cover, Goldring G800 cartridge, pair of Apollo speakers id all leads.

£54.40

PRICE

Carr, and Amplifier only, £22.95. Carr. 50p. Ins. £1.50

TELETON CRIOT/RG42 SYSTEM



OUR PRICE £35.50

8-TRACK CAR STEREO MW/LW TAPE PLAYER CAR RADIO





Tone, volume and balance controls. selector. Complete with matched pair of stereo speakers, connections and fittings.

SUPER BARGAIN!

£15.95

Post 30m

HOMER INTERCOMS



Ideal for home, office, stores, factories, etc. Supplied complete with batteries, cable and free instructions.

3 Station £5.25, Post 15p. 2 Station, £2-97, 3 Statio 4 Station £6-62. Post 17p.

BH.001 HEAD SET AND BOOM MICROPHONE

Moving coil. Ideal for Moving coil. Ideal for language teaching, communications. Headphone imp. 16 ohms. Microphone imp. 200 ohms. \$4.62. Post 15p.



Fully transistorised, dual waveband. Size 6\frac{1}{1}in \times 4\frac{2}{1}in \times 2in. 12V d.c. Neg. or pos. earth. Complete with fixing kit, speaker and leads.

£7.50

B.S.R. TD8S 8-TRACK STEREO TAPE PLAYER DECK

Integrated preamps (output 125mV) to feed into any stereo amplifier. Automatic and manual programme selector. 4 pole synchronous motor. 210/240V a.c. OUR PRICE £16.25

CREDIT TERMS FOR CALLERS

ACCESS & BARCLAYCARD WELCOME

HI-FI EQUIPMENT SAVE UP TO 33% OR MORE

SEND S.A.E. FOR FULL DISCOUNT PRICE LISTS AND PACKAGE OFFERS!

SAVE £££'s **PHILIPS GA308** TRANSCRIPTION **TURNTABLE**

2 speeds 333 and 45 r.p.m. Light-weight tubular counterbalanced arm. Belt driven low speed synchronous motor. Viscous damped pick-up lity device.



LEAK BARGAINS!



LIMITED OFFER!

ALL	STOCKS	BR	AND	NEW
	AND GUA	RAN	NTEEL)
Delta	30			£45.95
Delta	70			£55.95
				£55.95
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Delta	75			£125.00
Leak	150 pair		1.1	£37.50
	250 pair			£47-95
	600 each			£33-95
Post 5	Op extra ea	ch ite	m.	

ROTEL BARGAINS! ALL BRAND NEW AND GUARANTEED



RA210 Amp.			£23·35
RA310 Amp.			£35-95
RA610 Amp.			£48-25
RX150 Receiver		10.4	£48-95
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Post 50p extra any item.			

EAGLE TSA.150 STEREO AMPLIFIER



Housed in attractive Teak cabinet. 7.5+7.5 watts rms. Switched inputs for Mag. Cer. tape, tuner, bass, treble, volume, balance controls. Headphone socket. Output for main or remote speakers. List price £29.60.

OUR PRICE £16.50. Carr. and Ins. 50p.

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610/TPD1 510/TPD1 HT 70 HT70/G800

G800

Chassis BD2/SAU2/

Plinth/C

GARRARD

2025 T/C Stereo 40B Stereo

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SP25III/

M75-6 SL72B

SL95B

M75-6

SP25 III Module/ M75-6 \$23 SL65B £13

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GL69/2 £20.95 £27.50 £7.02 £3.25 GL72/P Plinth 69/72 LID 72 GL75 GL75P £26.95 £35.25 £7.35 £3.60 £18-95 Plinth 75 LID 75 G99 £19.25 £56.95 GL85P/C £20.35 LID 85 G101P/C £23.90 £9.25

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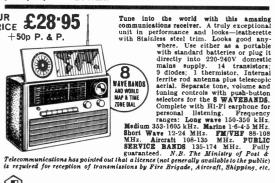
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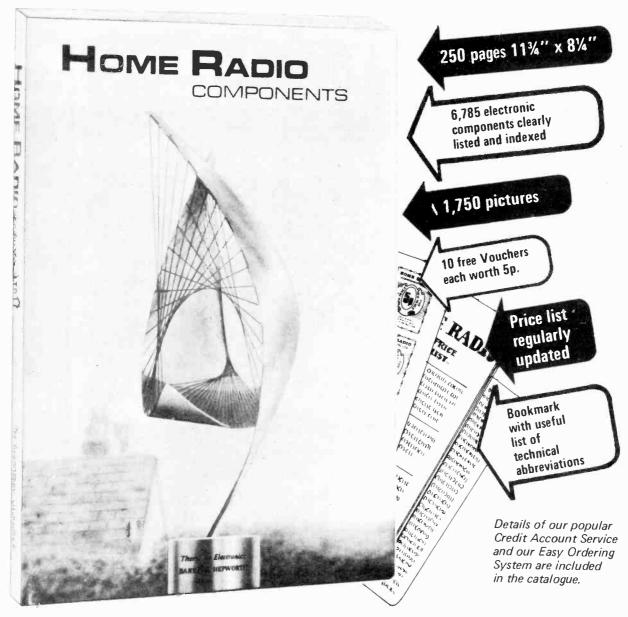
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THE WHOLE AND THE PARTS

Scope for the home constructor is widening the whole time, both in scale of circuitry and nature of application. Projects once considered highly ambitious and sophisticated are now well within the reach of the average amateur, thanks to the integrated circuit. Circuit arrangements that would be considered quite large in discrete component terms, are now likely to be found playing the part of some individual stage or section within the ramifications of some much more extensive circuit or system.

Despite miniaturisation and close packing, the extent of the circuitry involved in a sophisticated design may add up to a large and unwieldly piece of equipment. In such cases—and the present signs are that they will become more and more commonplace—the answer probably lies in unit or modular construction. This is a well-established practice in large commercial equipments. Now it is beginning to merit serious consideration in the home constructor field, for particular designs.

The modular form of construction can be seen as a further development of the plug-in circuit board arrangement, with carefully selected and clearly definable parts of the overall system assembled within mechanically independent units. The modular system offers a number of advantages. In some instances individual modules belonging to a system may be capable of serving other functions, either while remaining within the parent rack or cabinet, or as free-standing and independent units pressed into service at short notice for some ad hoc experiment or demonstration, for example.

The additional cost in hardware is therefore likely to be fully recompensed by the greater versatility provided by the constituents that go to make up the whole system. The maximum possible utilisation of valuable equipment can be assured. Operational flexibility is, of course, another important attribute of modular construction, as well as greater facility for the subsequent updating or improvement of particular sections of the system in the light of technical progress.

The P.E. Sound Synthesiser demonstrates some of the most valuable and desirable features of the modular approach. This project is certainly ambitious, in amateur terms; yet such is the current interest in the synthesis and manipulation of sound for all manner of divergent uses, that the popularity of this instrument is not in doubt. And it has this additional attraction: many of the modules have other possible applications, alone or in association with other equipment, outside the confines of the main system. The Sound Synthesiser series of articles can be considered in the whole—relating to one large and comprehensive design with great capabilities. Alternatively, the series may be viewed as a collection of separate designs, many of these having interesting possibilities as solo units in the wide and appealing field of creative and experimental sound.—F.E.B.

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SINGLE CHIP I.C. RADIO

By F. R. HEATH B.Sc. (Hons.) (Ferranti Ltd.)

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For the constructor there is, at least, a rest from some of the tedious coil-winding operations so often necessary in radio construction. There is no recourse to expensive alignment equipment, as no

setting up is required.

This article does not aim to stress an overall small size, such as in a matchbox radio, because the majority of constructors will want a radio with a speaker and cabinet, ferrite aerial, and room for a long lasting battery. To make full use of the superior sound quality available from the radio i.c. these items are essential. Anybody wishing to make a "micro-radio" or a medium and long wave tuner for an existing hi-fi system, will be able to adapt from the design in this article.

The "P.E. Triffid" design has been tried in most parts of the British Isles, from Exeter to Edinburgh, and gives good results on stations which are of normally reasonable signal strength for the area. The only problem (occurring with all t.r.f. designs) is when the receiver is being used very close to the transmitter. In such a case rotation of the rod aerial is necessary to find a null. Although desgined for reception of BBC Radio 1, 2, 3 and 4, the set works well on many foreign stations, especially Radio Luxemburg.

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Fig. 1. Cross section view through a CDI transistor

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The processes involved in the production of CDI devices are much simpler than for standard bipolar techniques. Only five masks are required which compare directly with MOS processing; four less than for conventional bipolar i.c. processes. The transistor size is much smaller due to the self isolating properties of CDI, and much thinner (1 micron) epitaxial layers can be used in processing.

This simplicity is of direct importance in achieving low cost and yielding large quantities, both factors being passed on to the consumer as cheaper i.c.s.

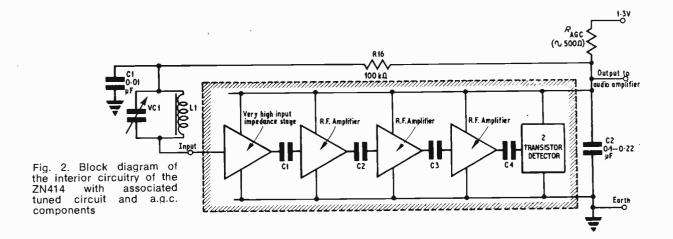
A cross-section of a CDI transistor is shown in Fig. 1. Buried n regions are diffused into a p-type substrate wherever transistors, diodes or resistors are required. A thin, high resistivity p-type epitaxial layer is then grown over the slice.

Table 1: BASIC CDI TRANSISTOR CHARACTERISTICS

V _{CBO}	7⋅5 volts
h _{fe}	60
fr	1GHz
Rsat	10 ohms
Voffset	5mV
Ісво	1.0pA
h _{fe (inverse)}	20 `
Cob	0∙3pF

A block diagram of the radio chip is shown in Fig. 2. Basically, the circuit is a 10 transistor t.r.f. tuner which will operate from 150kHz to 3MHz and requires about 1·3 volts power supply. Audio output is typically 30mV r.m.s.

The i.c. requires the minimum of external circuitry and effective a.g.c. action is available. Distortion from the chip is very low (typically 2%), which is three or four times better than in an average superhet. Current requirements for the i.c. are approximately 0.5mA and the characteristics are shown in Fig. 3 and 4 and in Table 2.



Isolation, deep collector contact, interconnection crossunders, and definition of base and resistor areas are all achieved by a single selective n_+ diffusion through this epitaxial layer. The isolating n_+ diffusion completely surrounds each buried layer island, complete isolation being provided by the p-type epitaxial layer and the substrate between the n_+ diffused regions. The p-type epitaxial layer which is completely enclosed is used to form transistor bases and p-type resistors (medium value resistors $2k\Omega$ to $50k\Omega$).

Another n_+ diffusion defines the transistor emitters, and can also be used for low value resistors. Contact holes are then cut and the basic aluminium interconnection pattern is evaporated onto the device.

The parameters of CDI devices are shown in Table 1.

RADIO CHIP DESIGN

The design of the ZN414 radio chip began in November 1970. A basic circuit was produced and then "breadboarded" using discrete CDI devices. As in many basic t.r.f. designs, instability was the major problem. Intensive development work culminated in a design that is stable provided certain external requirements are satisfied.

Many prototype experimental circuits were tried and found to be capable of excellent quality. The first i.c. radio was working in July 1971. The present day radio chips are predictable and consistent.

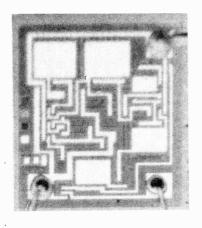
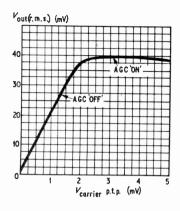
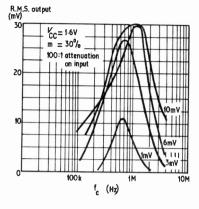


Table 2: MAIN CHARACTERISTICS OF THE ZN414

Supply volts
Temperature range
Supply current
Frequency range
R.F. input impedance
Output impedance
Sensitivity
Power gain

1.1–1.5 volts 0 to + 70°C 0.5mA maximum 200kHz–3MHz 1.5M Ω typical 500 Ω typical 100 μ V r.m.s. 70dB typical





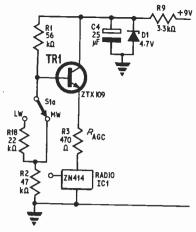


Fig. 3. Graph of voltage gain showing the effective a.g.c. region

Fig. 4. Bandwidth of the ZN414 on the medium wave band

Fig. 5. The integrated circuit is driven from a constant voltage source of 1.3 volts derived from a 9 volt supply

HIGH QUALITY RADIO SET

To obtain the best possible results from the ZN414, certain rules must be adhered to. All leads in the radio circuitry must be kept short, and the i.c. should preferably be soldered flush to a printed circuit board. The aerial coil should have a high Q or selectivity will suffer.

The only problem occurs when a very strong station swamps the front end. Here, rotating the set until a null is found will solve the problem. A demonstration radio gave better reception of Radio Luxemburg than a superhet, not because selectivity was better, but because the superhet gave out so many whistles and shrieks that any pleasure from the programme was impossible to achieve.

One other important requirement is to keep the a.g.c. resistor within the range 470 to 1,000 ohms,

A typical case used to house the P.E. Triffid receiver



and for best selectivity keep to the lower end. This means that if the radio is powered from a 9V battery, then a constant voltage source is needed to derive the 1·3 volts necessary. This is done using the circuit shown in Fig. 5.

Fig. 4. shows that the gain of the chip falls off at long wave frequencies. For this reason, a switch is fitted to increase the supply volts (and consequently increase the gain of the chip) on long wave so that the volume is kept approximately the same when the different bands are selected. Fig. 5 shows the circuit changes needed to accomplish this.

AMPLIFIER AND CASE

The output amplifier and loudspeaker should be of good quality to do justice to the signal from the receiver. Several i.c. amplifiers were tried. All gave some results, but most were tricky to stabilise and did not give the quality needed. For this reason a discrete amplifier was used, low power output at 500mA being suitable for a personal radio. Low cost and battery power consumption are kept to a minimum making this receiver suitable for the inexperienced radio constructor.

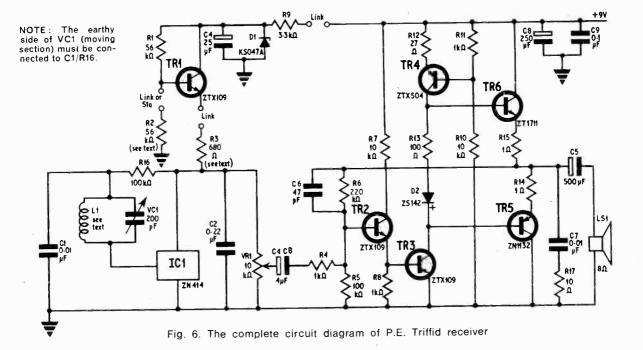
Cabinet and speaker design is dependent on personal taste so the following constructional details deal mainly with the circuitry aspect. Most constructors will want to design their own housing for the unit, and there are many cases available to cater for those who do not like woodwork.

The case must not contain large metal parts near to the ferrite rod, as this will damp the Q of the coil.

AMPLIFIER DESCRIPTION

The amplifier is not claimed to be a revolutionary design; rather it is intended to be easily built, and of good enough performance to match the radio i.c., whilst maintaining battery current economy and using inexpensive transistors.

The circuit in Fig. 6 shows a class-AB amplifier with a constant current source (TR4) enabling a



higher voltage gain from the drive stage TR2. The current in TR4, and consequently the quiescent current taken by the circuit, is around 5mA. This pnp current source was found to reduce distortion in the circuit. The voltage gain at 1kHz is approximately 80, thus the input sensitivity for full output (5.7 volts before clipping) is 70mV.

The value of R13 may be lowered to give less bias voltage at the expense of distortion. Replacing it with a wire link is recommended if other output transistors are used, or any modifications are tried, as this prevents the possibility of thermal runaway.

If a reduced ouput power is acceptable, ZTX300 and ZTX500 may be used as the output pair, or BFS60 and BFS96; both sets give good results. Distortion with the standard circuit is one per cent at 1kHz and 2 volts peak output, mainly second harmonic. No crossover distortion can be seen on an oscilloscope trace at 20kHz, indicating that distortion is due mainly to non-linearity in the whole amplifier rather than to crossover "spikes".

No heatsinks are necessary with the recommended output pair. Three layouts of the circuit were tried, all were stable and gave similar results.

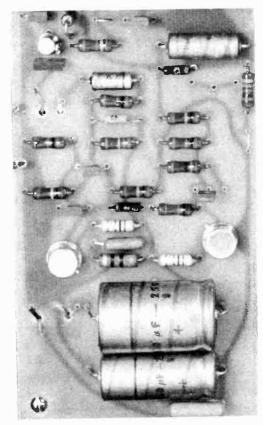
The amplifier is certainly of good enough performance to use as an amplifier for an f.m. tuner, or record player, and experimenters can easily modify the circuit to switch in to another function or functions.

CONSTRUCTION AND LAYOUT

Provided the layout is carried out as described earlier, almost any method of construction can be used. However, a printed circuit board is recommended as it offers reliably consistent results.

The combined amplifier and radio circuit is shown in Fig. 6, the p.c.b. pattern and layout in Fig. 7. Apart from essentially sound soldered joints, two further precautions must be observed: wires from the coil-capacitor tuned circuit must be kept away

from other circuitry, especially the battery leads and loudspeaker leads; the volume control must be $10k\Omega$ or greater, if it is not to affect the a.g.c. characteristics.



Layout of components on a printed circuit board

COMPONENTS ...

$\begin{array}{llllllllllllllllllllllllllllllllllll$	Integrated Circuit IC1 ZN414 (Ferranti) Transistors TR1, 2, 3 ZTX109 (3 off) TR4 ZTX504 TR5 ZN1132 TR6 ZT1711 Diodes D1 KS047A D2 ZS142 Tuning Coil L1 85 turns +250 turns 28 s.w.g. enamel wire wound on $\frac{3}{6}$ in dia. 6in ferrite rod (see text) Miscellaneous LS1 8\Omega loudspeaker B1 9V battery style PP9 Printed circuit board (see Fig. 7) Case and tuning scale
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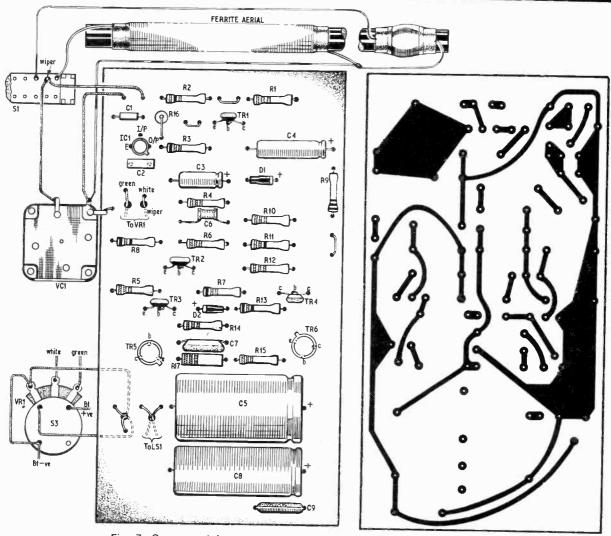


Fig. 7. Component layout and printed circuit board pattern (full size)

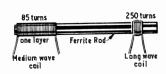
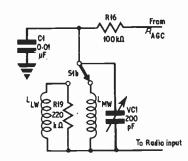


Fig. 8. Coil winding details and waveband selection



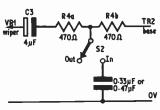


Fig. 9. A tone control circuit is inserted in the position of R4 as shown here with another capacitor

TUNING COIL

If the tuning range is tending towards the low frequencies, then fewer turns are needed on the coil. For a 6in ferrite rod with the coil feeding a 200pF tuning capacitor, about 85 turns of close wound enamelled copper or litz wire are needed; 28s.w.g. wire is suitable, but nothing is critical here, and adjustments are easy. It is better to wind more turns (say 100) and then remove some until the correct tuned frequency spread is reached. Litz wire gives highest Q coils and is highly recommended.

Constructors who wish to wind a long wave coil and fit a wave-change switch will find that, with the values above, the coil will need about 250 turns. Multilayering is best, but again this is not critical. Fig. 8 shows the long wave components necessary.

The type of ferrite rod affects the inductance, as does the type of wire, but it is easy to adjust the coil to suit the requirements of the rod obtained. Do not expect to adhere rigidly to the specified coil details for optimum results.

TESTING

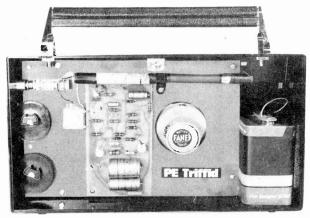
Building the circuit should present no problems if carried out in the following manner:

1. Build up the amplifier unit and volume control, and test it on suitable inputs. If no signal generator is available, see if a hum is produced when the input is touched. The output (before C5) should be at 4.5 volts ± 0.5 volts.

2. Wire up the radio drive circuit and put a $3.3k\Omega$ resistor between emitter of TR1 and earth. This should have 1.3 volts $\pm 0.2V$ across it.

3. Wire up the radio i.c. and test.

Interior of receiver showing the printed circuit board mounted on a plain board which also has the tuning capacitor, volume control and aerial mounted on it



Practical Electronics February 1973

If instability is encountered, the following procedure is used.

- (a). Short the tuning capacitor out, if instability continues then the radio supply voltage may be incorrect.
- (b). Radio frequencies generated in the amplifier may be feeding back to the i.e. To cure this a 47pF capacitor may be fitted across the $220k\Omega$ resistor, and/or a 30μ H choke placed in the supply before R9. (The link on the board is replaced by the choke.)
- (c). Leads to the tuning circuit may need re-routing.
- (d). If instability continues then replacing R2 by a $47k\Omega$ resistor, and replacing the link above R2 with a $20k\Omega$ preset, will facilitate greater control of radio supply voltage. This has an additional advantage; as the battery ages and its voltage drops, the set will still give good results (down to 6 volts with this preset in circuit.)

Happily, none of these problems occurs if neat systematic working is done, and normally the radio should work first time.

TUNING INDICATOR

A tuning indicator is very simply added to the set by inserting a 0-1mA (or 0-500 μ A) meter between TR1 emitter and the top end of R3. This should read approximately 0.3mA with no signal, but should read higher as one tunes through a station. The maximum reading indicates that the station is properly tuned, and depending on the signal strength, should give a reading around 0.5mA.

In normal circumstances this receiver should not drift and once set, the tuning should not need to

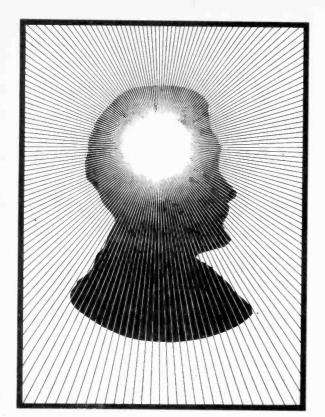
be altered.

TAPE RECORDER OUTPUT

Provided the circuitry of the tape recorder has an input impedance of several tens of kilohms, a screened lead can be taken from the "top" end of the volume control to the tape recorder input socket most suited for a 100mV flat response input signal. Care that the bias circuitry does not interfere with the radio is needed, so a fairly long lead is recommended.

TONE CONTROL

Fig. 9. shows a recommended tone control, which in its extreme position gives a 6dB/octave roll-off above 1kHz. To fit the tone circuit, the connection between C3 and R4 has to be cut. Apart from this the board is adaptable for the modification.



Biological Amplifier

By D. BOLLEN

This month we describe the construction of a brain rhythm frequency meter and cardiophone.

BRAIN RHYTHM FREQUENCY METER

The circuit in Fig. 8 can be employed to identify different brain rhythms, and will demonstrate, for example, how alcohol intake affects alpha frequency.

A signal taken from output 1 of the pre-amplifier is amplified by TR3 and squared by the Schmitt trigger TR4 and TR5. Differentiator C15 and VR4 converts the square wave into an a.c. signal of amplitude proportional to frequency. This is rectified and smoothed by D3, D4, and C16, with the resulting d.c. current being measured by ME2. VR4 calibrates the instrument, and VR3 adjusts sensitivity.

The frequency range covered by ME2 is 0-20Hz, and capacitor C8 in the pre-amplifier can be switched into circuit by S3 to give additional top-cut for noise and interference rejection, see Fig. 2.

In addition to the frequency meter, a voltage controlled unijunction oscillator TR7, gives an audio output into 8 ohm headphones of frequency proportional to the subsonic brain rhythm frequency, so that the user can sense changes of rhythm with his eyes closed. TR6 controls the charge rate of the unijunction emitter capacitor C17.

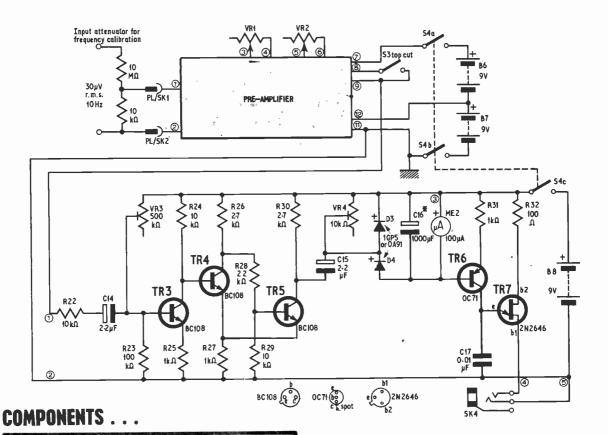
If interest is centred on either beta, theta, delta, or slow alpha rhythms, the centre frequency of the preamplifier can be modified according to the capacitor value listed in Fig. 3. Alternatively, a three-pole four-way wafer switch can be used to select twin-T filter capacitance values.

CONSTRUCTING AND USING THE FREQUENCY METER

Constructional details of the frequency meter output module are shown in Fig. 9. A suggested layout in a metal box, similar to that used for the alphaphone, will be found in Fig. 10. C16 is mounted on the meter terminals.

Plug headphones into SK4, leave the head electrodes disconnected from SK1 and SK2, and set VR1 and VR2 to minimum resistance, and VR3 and VR4 to maximum resistance. Switch on the





ADDITIONAL COMPONENTS FOR FREQUENCY METER

_				
R	PS	ist	0	rs

R26 2.7kΩ R30 2·7kΩ $10k\Omega$ R22 R31 $1k\Omega$ R27 $1 k\Omega$ R23 100kΩ R24 $10k\Omega$ R25 $1k\Omega$ R32 100Ω R28 $22k\Omega$ R29 $10k\Omega$

All ±10% ½ watt carbon

VR3 500k Ω sub-min horizontal pre-set VR4 10k Ω sub-min horizontal pre-set

Semiconductors

TR₆ OC71 TR3 BC108 TR4 BC108* TR7 2N2646 D3, D4 IGP5 or OA91 TR5 BC108

Capacitors

C14 2·2µF tantaium 35V C15 2·2µF tantaium 35V

C16 1,000 µF elect. 3V C17 0.01 µF polyester

M2 100μA edgewise type level indicator

Switches

\$3 single-pole, on-off sub-miniature

S4 3-pole, 2-way wafer

Socket SK4 3-pole jack

Batteries

B6, B7, B8 9 volt style PP3 (3 off)

Miscellaneous

8 ohm mono or stereo headphones, electrodes, battery connectors, metal box.

Fig. 8. Wiring of the pre-amplifier to the frequency meter circuit to measure brain rhythm rates

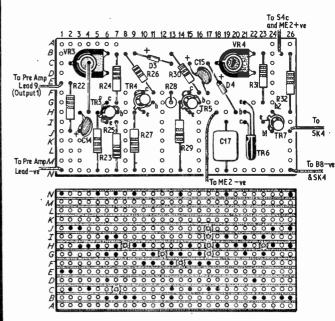


Fig. 9. Layout and wiring of the frequency meter board

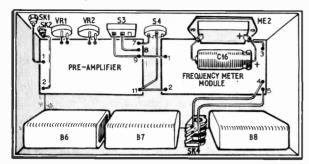


Fig. 10. Suggested layout of components for the brain rhythm frequency meter circuit shown in Fig. 8

instrument and listen for a steady low note in the phones. Advance VR3 until the audio note just starts to rise slightly.

If an accurately calibrated audio oscillator with an output of around 30 millivolts r.m.s. at 10Hz is available, connect this to the pre-amplifier input via a 10 megohm resistor, with a 10 kilohm resistor shunting SK1 and SK2. Set VR1 for a steady deflection of meter ME2, and adjust VR4 for a half full scale reading, corresponding to 10Hz.

In the absence of an audio oscillator, set up the frequency meter for alpha rhythms (with head electrodes on a subject who can generate steady alpha rhythms) and adjust VR4 for a mean meter reading of 10Hz. With the eyes open, ME2 should fluctuate between 2-7Hz, indicating the presence of random brain noise and low level theta.

As an experiment, measure a subject's alpha frequency and then ask them to have a drink (alcoholic). After 15-30 minutes the alpha frequency should fall by several hertz. A whole range of experiments can be conducted with the frequency meter, such as mental reactions to various stimuli, or the effect of dreams on sleep rhythms.

ELECTRODE SITING

With previous projects the earthed electrode (SK2) was sited on the forehead so that eyeblink signals

could be used to test equipment in the absence of alpha rhythms, but in some investigations eyeblink pulses can be a nuisance. Alpha, theta, and delta signals are best obtained from the back of the head, with the earthed electrode positioned an inch or two from the live electrode. For beta signals the electrodes can be placed on the forehead or near the cheeks, but watch for noise generated by facial muscles and eyes.

If the earthed electrode is placed on the neck, or other parts of the body, while observing brain rhythms, a strong heartbeat pulse will be superimposed, tending to block the brain signals.

CARDIOPHONE

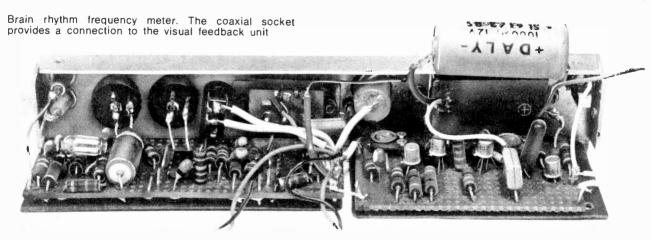
Stress situations, like running for a bus, attending an interview, sitting an exam, or appearing before an audience, are usually attended by an obvious increase in heartrate, but during the course of an uneventful day the heart also responds to numerous minor stress situations which normally pass unnoticed.

By making the heartbeat clearly audible, it is possible to detect these subtle changes, and perhaps learn to control them. This is really an example of bio-feedback. If the heart speeds up slightly in response to some unconscious stimulus, you become aware of it and seek to reduce it.

Conversely, it may also be possible to induce an artificial state of excitement by consciously trying to increase heartrate, and thereby cause more adrenalin to be released into the system.

In the cardiophone circuit (Fig. 11) transistor TR8 is in series with the emitter supply to astable multivibrator TR9 and TR10. In the absence of a heartbeat signal, TR8 base is grounded (by R16, Fig. 3) and the multivibrator is therefore switched off. Diode D1 in the pre-amplifier, rectifies a heartbeat signal and applies a positive going pulse to TR8 base, thus switching on TR8 and the multivibrator, and causing a 300Hz audio "bleep" tone to be heard in the earpiece X1.

Switch S5 in Fig. 11 gives additional top cut to suppress mains borne interference.



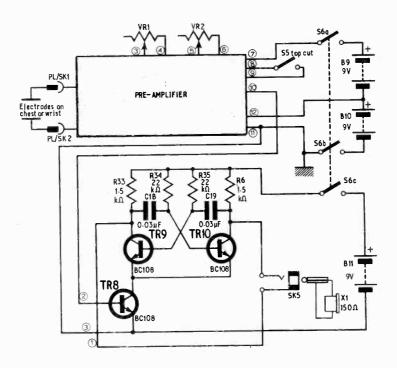


Fig. 11. The pre-amplifier used with a cardio-phone circuit

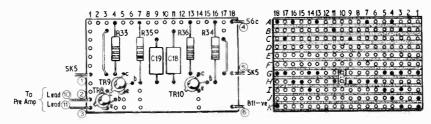


Fig: 12. Layout and wiring of the cardiophone output module

COMPONENTS . . .

ADDITIONAL COMPONENTS FOR CARDIOPHONE

Resistors

R33 1.5kΩ R34 22kΩ

R35 $22k\Omega$

R36 1.5kΩ

All $\pm 10\% \frac{1}{2}$ watt carbon

Capacitors

C18 $0.03\mu\text{F}$ polyester C19 $0.03\mu\text{F}$ polyester

Transistors

TR8 BC108 TR9 BC108

TR10 BC108

Earpiece X1 150 ohm magnetic

Switches

S5 Single-pole, on-off sub-miniature toggle S6 3-pole, 2-way wafer

Batteries

B9, B10, B11 9 volt style PP3 (3 off)

Socket

SK5 3.5mm 2 pole jack

Miscellaneous

Electrodes

Battery connectors

Metal box (see text)

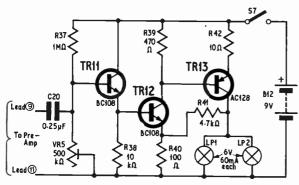


Fig. 13. Circuit of the visual feedback lamp driver

COMPONENTS . . .

ADDITIONAL COMPONENTS FOR VISUAL FEEDBACK LAMP DRIVER

Resistors

R37 $1M\Omega$ 10k Ω R38

R39

470Ω R40 1000

R41 4.7kΩ

R42 10Ω

All ±10% ½watt carbon

Potentiometer

VR5 500kΩ sub-miniature horizontal mounting preset

Capacitor

C20 0.25μF miniature polyester

Transistors

TR11 BC108

TR12 BC108

TR13 AC128

Switch

S7 Single-pole, on-off toggle or slide

LP1, LP2 6V 60mA m.e.s.

Battery

B12 9 volt style PP9



Brain rhythm frequency meter. The coaxial socket provides a connection to the visual feedback unit

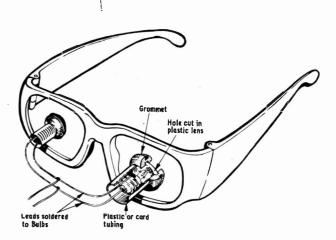


Fig. 14. The method of mounting the lamps in plastics lens sunglasses

CONSTRUCTING AND USING THE CARDIOPHONE

The cardiophone output module circuit board (Fig. 12) may be housed, along with the preamplifier module, in a metal box similar to that used for previous projects. Socket SK5 must be insulated from the box.

Electrodes for use with the cardiophone can either be positioned a few inches apart on the left side of the chest, or one on each wrist, and held in

place with elastic straps.

Set VR1 to minimum gain, and VR2 to wideband, with S5 open circuit. Plug earpiece X1 into SK5, the electrode leads into SK1 and SK2, and switch on. If no heartbeat "bleep" is heard, advance VR1. When the heartbeat is masked by interference, close S5, and adjust VR1 and VR2 for a clear signal.

Try using the cardiophone with a friend who is driving a car. The "bleep" rate will increase when negotiating roundabouts, traffic lights, and congested

streets, and will rise sharply when overtaking.

VISUAL FEEDBACK

The lamp driver circuit in Fig. 13 can be employed as an external unit to extend the scope of previous projects. An output taken from the pre-amplifier (output 1) is amplified to a level sufficient to flash two low consumption filament lamps (LP1 and LP2) which are mounted close to the eyes in a pair of cheap plastics lens sunglasses; see Fig. 14.

When driven by brain rhythms, visual feedback will produce an interesting variety of "strobe" effects while leaving the ears free to, say, listen to music or

other sound sources.

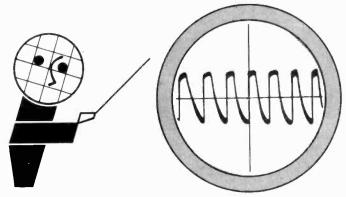
If the lamp driver circuit is housed in a small plastics box, it can be coupled to the alphaphone, alphameter, frequency meter, or cardiophone, via screened cable to a coaxial socket which connects with pre-amp output 1. VR5 is adjusted so that both lamps just glow when there is no signal. Setting up instructions are otherwise the same as for previous projects.

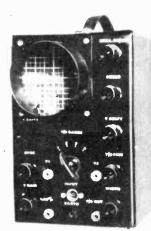
Note: pin 12 in the case interwiring diagram in Fig. 5 (last month) should be designated pin 11 to agree with the practical circuit.

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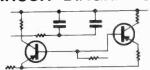
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100	60	3	8	8·9 × 8·0 × 7·7	2.39	36
61	100	5	12	10·2 × 8·9 × 8·3	2.62	52
30	200	9	8	12·0 × 10·3 × 10·0	4.39	52
62	250	12	4	$9.5 \times 12.7 \times 11.4$	5.80	67
55	350	15	0	14·0 × 10·8 × 12·4	7.77	82
63	500	27	0	17·1 × 11·4 × 15·9	11.20	*
92	1000	40	0	17·8 × 17·1 × 21·6	20.63	
128	2000	63	0	24·1 × 21·6 × 15·2	34-10	
		A	UT	SERIES (NOT ISOLATED)		

		A	UTC	SERIES (NO	OT ISOLA	(TED)		
Ref.	VA	W	eight			Tobs	Р	& P
No.	(Watts) Ib	oz			•	£	b
113	20		11	7:3 × 4:3 × 4	4 0-115-21	0-240	0.85	22
64	75	- 1	14	7.0 × 6.4 · 6	0 0-115-21	0-240	1.66	30
4	150	3	0	8:9 × 6:4 > 7	6 0-115-20	0-220-240	2.00	36
66	300	6	0	10·2 × 10·2 × 9	.5	11	3.89	52
67	500	12	8	14:0 × 10:2 × 11		11	5.78	67
84	1000	16	0	$11.4 \times 14.0 \times 14$	0 ,,	11	10.49	82
93	1500	28	9	13·5 × 14·9 × 16	-5	11:	15-20	*
95	2000	40	0	17.8 × 16.5 × 21		**	19.84	
73	3000	45	8	17-4 × 18-1 × 21		**	26.99	

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21310 05 1 0	8-3 × 5-1 × 5-1		1.01 22						
71 2 1 1 0	7.0 × 6.4 × 5.7		1.33 22						
18 4 2 2 4	8:3 × 7:0 × 7:0		1.86 36						
70 6 3 3 12	10.2 × 7.6 × 8.6		2-24 42						
108 8 4 5 4	10.0 × 8.3 × 8.2		2.48 52						
72 10 5 6 3	7.9 × 10.8 × 10.2		2.94 52						
17 16 8 7 8	12·1 × 9·5 × 10·2		4.54 52						
115 20 10 11 13	12-1 × 11-4 × 10-2		5.78 67						
	$13.3 \times 12.1 \times 12.1$ (10-67 82						
226 60 30 34 0	17-0 × 14-5 × 12-5 (0-12V at 30A ×2	19-61 *						
	30	VOLT RANGE							

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Ref.	Amps.	Weight	Size cm. Secondary Taps	P & P
No.		lb oz		£ p
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79	1.0	2 0	7.0 × 6.4 × 6.0	1-35 36
3	2.0	3 2	8.9 × 7.0 × 7.6	2.01 36
20	3.0	4 6	10·2 × 8·9 × 8·6	2.48 42
21	4.0	6 0	10·2 × 10·0 × 8·6	2.94 52
51	5.0	6 8	12·1 × 10·0 × 8·6	3.66 52
117	6.0	78	12·1 × 10·0 × 10·2	4-36 52
88	8.0	10 0	14·0 × 11·7 × 10·0	5-64 67
89	10.0	12 2	14·0.×10·2.×11·4	7-14 67
0-6	A	147. 1.4.	50 VOLT RANGE	

Ref.	Amps.	W	eight	Si	ze cm.		Second	ary Tops	P	& P	
No.		16	oz					,p.	6	Þ	
102	0.5	- 1	H	7·0 ×	7·0 ×	5.7	0-19-25-	33-40-50V	1.33	30	
103	1.0	2	10	8·3 ×	7·3 ×			71	1.94	36	
104	2.0	5	0	10-2 ×	8.9 ×	8.6	11	11	2.69	42	
105	3.0	6	0	10·2 ×	10.2 ×	8.3	11	**	3.65	52	
106	4-0	9	4	12·1 ×	11:4 × 1	10.2	,,	**	4.83	52	
107	6.0	12	4	12·1 ×	Hilx	13.3	- 11	11	7.14	67	
118	8.0	18	9	13·3 ×	13·3 × I	12-1	,		9.32	97	
119	10.0	19	12	16.5 ×	11-4×1	15.9	.,	1)	11.68	97	
						60		RANGE			

						- 01	, voli i	IANGE		
Ref.	Amps.	We	ight		ize cm.		Seconda	ry Tabe	ρ	& P
No.		IЬ	οz				000000	,	€	~ b
124	0.5	2	4	8:3:	< 9.5 ×	6.7	0-24-30-40	-48-60V	1.35	36
126	1.0	3	0	8-9	< 7.6 x	7.6			i.88	36
127	2.0	5	6	10.2	× 8.9 ×	8-6	.,	.,	2.94	42
125	3.0	8	8	11.9:	< 9.5 ×	10.0	**	.,		52
123	4.0	10	6	11:4:	× 9.5 ×	11.4	.,	.,	5.78	67
120	6.0	16	12	13:3:	< 12·1 ×	12-1	11	23	8.37	82
122	10-0	23	2	16.5	× 12.7 ×	16.5	.,	11	13-85	*
	1.6	A D		10 8		v -				
0.4		20	70	ים טי	21166	TC	HARGER	ITPES	>	

	LI	EAL) AC	ID BA	TTER	Y CH	IARGER	TYPES		
Ref.	Amps.	. W	eight	Si	ze cm.					& P
No.		iь	oz						6	b
45	1.5	1	9	7·0 ×	6-0 ×	6.0 \			1.34	30
5	4.0	3	1.1	10-2 ×	7·0 ×	8-3	Please n	ote, these		
86	6.0	5	12	10·2 ×	8-9 ×	8-3		not in-		
146	8.0	6	4	8.9 ×	10.2 ×	10.2	clude re		3.49	
50	12.5		14		10.8 ×	12-1 /			5.20	67
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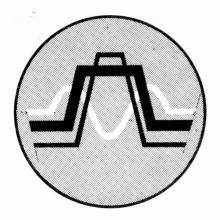
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Audio Frequency Discriminator

By G.F.A. HOFFMAN de VISME

A CIRCUIT for distinguishing between two notes whose frequencies are very close together and whose amplitudes may differ greatly is shown in Fig. 1. The operation of the circuit does not depend on the use of filters, and notes of any frequency may be distinguished by simple potentiometer adjustment.

The circuit was designed for a project in which it was necessary to distinguish between notes differing in frequency by as little as 20Hz, the mean frequency of the notes lying in the range 300 to 1500Hz. The amplitudes of the notes could differ by as much as a factor of ten, and the notes themselves were not free of distortion. In addition, a certain amount of acoustic noise was present during the experiment.

The requirement was that when the higher pitched note was sounded a bistable should be set, and when, after an unspecified period of silence, the lower pitched note was sounded the bistable should be reset. There was no need for undue speed in the response of the bistable since each note was sounded for some seconds.

Whilst audio frequency filters can be devised to meet the above demands, there are well known difficulties with these as regards the realisation of high Q at low frequency and as regards tuneability, and sensitivity to signal amplitude. The method described below is a simple alternative which achieves the required objectives without the use of filters or counting techniques.

Although originally designed for a project involving acoustic measurements such a circuit could be used in a variety of practical situations. For example it could be used to enable the driver of a moving vehicle to switch on (and switch off) a stationary warning light of some kind by sounding notes of appropriate frequencies. Alternatively an operator could use the circuit to control a model railway

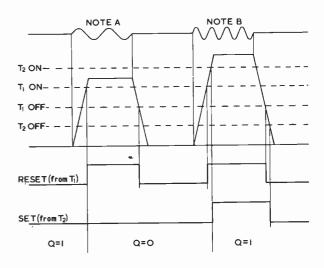


Fig. 2. Trip circuit switching levels and waveforms

acoustically, or, by sounding horns of different frequency, a motorist could open and close his garage doors from his driving seat.

Although the circuit as described here consists of discrete components, every part of it except the emitter followers and pump circuit is realisable using standard integrated circuit modules. In this form the circuit could be made extremely compact.

PRINCIPLE OF OPERATION

Fig. 1 is a block diagram of the circuit. The audio signal, after amplification, is squared by a Schmitt trigger circuit to yield a wave with sharp leading and trailing edges. The squared signal is applied to a diode pump circuit designed to give a d.c. output

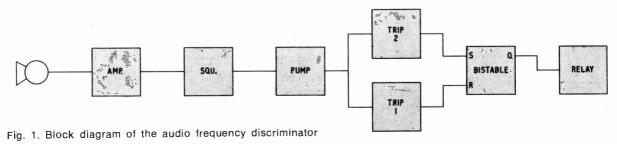
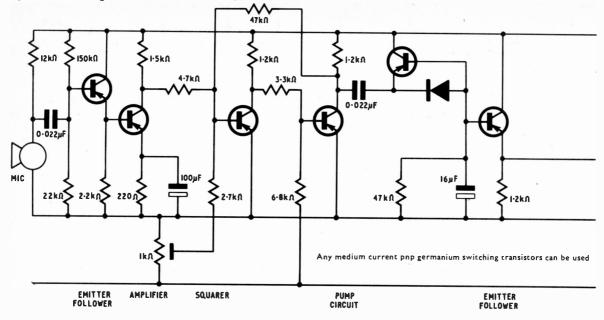


Fig. 3. Circuit diagram of the a.f. discriminator



as nearly as possible proportional to the signal frequency. Thus if a note A is sounded a voltage of, say, 4 volts appears at the output of the pump circuit, while if a higher pitched note B is sounded a voltage of, say, 5 volts appears there. It is required, therefore, that the bistable, if set, should be reset by the 4 volts signal due to note A, and if reset, it should be set by the 5 volt signal due to note B.

To achieve this the pump circuit output is applied simultaneously to two trip circuits. The switching levels of these are so arranged that when note A is sounded only Trip 1 switches, while when note B

is sounded both are switched. The signals from these trips are then used as the reset and set signals, respectively, of a bistable whose output controls a relay. In order to ensure that the bistable remains set after note B has ended the switch-off level of Trip 2 is made lower than the switch-off level of Trip 1. In this way the set signal produced by Trip 2 lasts until after the reset signal from Trip 1 has ended.

Fig. 2 shows the waveforms from Trip 1 and Trip 2 and the corresponding bistable output, resulting from notes A and B respectively.

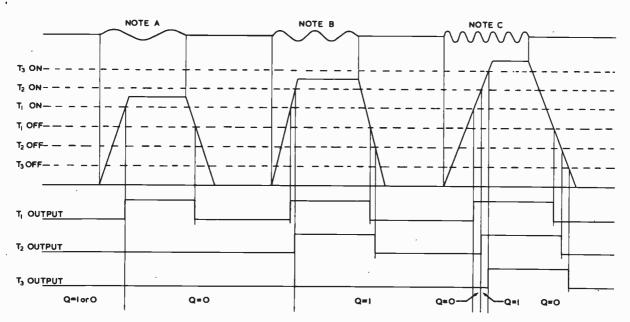
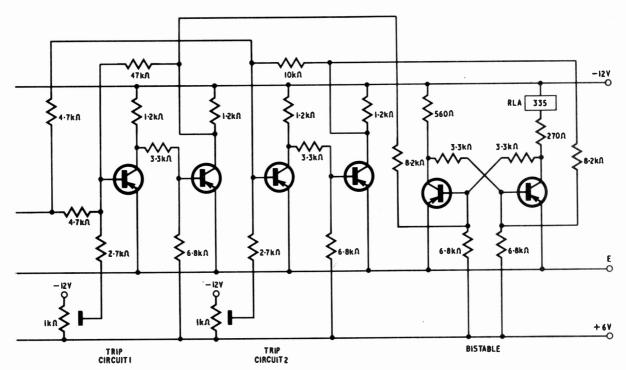


Fig. 4. Trip circuit and bistable outputs from selective discriminator



CIRCUIT FEATURES

Fig. 3 shows the circuit of the discriminator using all discrete components. Most of the circuitry is conventional, but suitable circuit values are included for the benefit of readers.

The only features worthy of note concern the pump circuit. To ensure a reasonably linear voltage-frequency characteristic from this stage capacitive loading of the previous stage must be small, hence the relatively small coupling capacitor $(0.022\mu\text{F})$, and a transistor must be used in the place of the usual shunt diode. Adequate sensitivity then demands a fairly large shunting resistor $(47~\text{k}\Omega)$, which therefore necessitates the inclusion of an emitter follower between the pump circuit and the trip circuits.

A large value $(16\mu\text{F})$ is used for the reservoir capacitor to slow down the speed of the response of the pump circuit and so minimise its sensitivity to background noise.

PERFORMANCE

The discrimination attainable by the above circuit was found to depend to a large extent on the purity of the notes used as signals. The following table shows how the pump circuit output varies with signal frequency, the signal being provided by a signal generator rather than a microphone:

Frequency (Hz) 300 400 500 600 700 Pump circuit output (volts) 2·7 3·6 4·5 5·3 6·1

By setting the switch-on and switch-off levels of Trip 1 to 3.8 and 3.1 volts, respectively, and those of Trip 2 to 5.3 and 1.6 volts, respectively, it was possible to distinguish signals of frequency 590Hz and 600Hz with complete reliability. Using a good quality microphone and real notes generated by a

loudspeaker the performance was almost as good (570Hz and 590Hz) even though the notes from the speaker were noticeably distorted. With a poor (carbon) microphone, however, the discrimination was much poorer due to frequency jitter at the output of the squarer.

BAND-PASS FILTERING

The above principle may readily be extended to provide selective discrimination, whereby, if A, B and C are notes of successively higher pitch, A or C reset a bistable which has been previously set by B. In this case three trip circuits are used, the switching levels of Trip 1 being arranged to lie within those of Trip 2, which in turn lie within those of Trip 3. As shown in Fig. 4, note A causes only Trip 1 to switch, note B causes Trip 1 and Trip 2 to switch, while note C causes all three to switch.

When notes A. B and C are sounded in turn the trip circuit outputs pursue sequences as shown in the following table. The required output Q from the bistable is shown alongside, the symbol Q' representing "the previous value of Q":

OUTPUTS	Note A	Note B	Note C
Trip 1	010	01100	0111000
Trip 2	000	00110	0011100
Trip 3	000	00000	0001110
Bistable (Q)	Q′00	Q'0111	Q'010000

From this table it is easy to deduce that the reset signal for the bistable has to be \overline{T}_1 (the inverse of the Trip 1 output), while the set signal has to be $\overline{T}_2 + \overline{T}_3$ (i.e. the inverse of the Trip 2 output or the Trip 3 output).



SATELLITE CAMERAS

Cameras that have been developed and used with such great success on satellites and other spacecraft have been mainly devoted to the obtaining of high definition. Similarly with television cameras where the task is much more difficult, the British company EMI have made a major contribution in this field. They developed a low light tube which was used in the ESRO TD-1 spacecraft launched in March 1972, and was part of a French experiment to map gamma rays from the galaxy. It was the first time that a European camera tube has been used in space.

The tube, known as the Ebitron, was developed at Hayes, Middlesex, by EMI Central Research Laboratories. It is an intensifier vidicon tube measuring 160mm by 64mm and is claimed to be the smallest tube of its type in the world. It formed the "seeing" part of the camera designed by the French company Engins Matra. The camera with its associated equipment is quite light, the camera itself weighing only 1.8kg

ing only 1.8kg.

The EMI tube was chosen because of its small size, low weight and its ability to "see" in near darkness. Its ease of operation, fast response, low light requirement made it ideal for recording the sparks caused in a gas chamber by the passage of gamma rays.

As gamma rays pass through the gas filled chamber the gas becomes ionised leaving trains of sparks. These are short lived (a few millionths of a second only) and of low intensity.

A series of mirrors is arranged so that two sides of the chamber can be viewed by the Ebitron thus enabling a three dimensional image to be obtained. The information is stored and transmitted to earth stations for analysis by computer.

The TD-1 is the first satellite to scan the whole sky and also the first to be able to operate in full daylight. The picture of the sky is built up over a period of six months from a polar orbit of some 500km altitude. The satellite is one of the most advanced in operation put into space. It was launched on a ThorDelta rocket from the Western Test Range in California.

ECOLOGICAL STUDIES FROM SPACE

Aboard the Earth Resources Satellite which was launched in July 1972 were cameras designed by RCA for high resolution TV. These cameras can detect crop deseases and pollution sources in the course of making their scanning passes.

The system which consisted of three cameras was designed by the Astro-Electronics Division of RCA at Princeton, N. Jersey. They have produced a picture which is some ten times sharper than the kind that appears on home television sets.

Each camera uses 4,000 horizontal scanning lines for the building of a picture. From a height of some 900km each camera will be able to view the same area of 180km². Each camera observes in a different part of the spectrum, one in red, one in infra-red and the third in green. After transmission to Earth the three images are combined and the composite picture can then be studied.

It is perhaps worthwhile to point out that this technique was used ten years ago by Ian Whitacker when studying the moon. Later other astronomers used the same technique.

Now its use has been extended to the study of the environment and has proved exceptionally valuable. Already the diseased areas of various food crops have been photographed, as well as silt movement from estuaries into the sea and the direction of ocean currents have also been mapped.

One of the advantages of this kind of photography is that the altitude of the satellite gives orthographic pictures so that the proper spacial relationships are directly seen. No corrections are required to show the real condition without the spacial distortion that arises from ordinary mapping.

As the orbit of the satellite is synchronised with the Sun the same lighting conditions exist for each area viewed, thus avoiding distortions that appear when using other methods of carrying cameras aloft which are subject to changing angle of the light of the Sun. The full significance of this aspect can be appreciated when it is understood that only 72 per cent of the habit-

able land has been mapped in detail and of this more than 50 per cent of those that exist are out of date.

The new mapping will now fill in this gap, and not only that, each area will be mapped 18 to 20 times a year.

INDIA AND SPACE ACTIVITY

India has been very active in the field of space development, as well as in radio astronomy. There are plans afoot to build the first all-India satellite for launch in 1974.

It is expected that the launch vehicle will be Russian and will carry a satellite weighing about 100kg. There will be three experiments on board which have been designed by ISRO (India Space Research Organisation) and will be built entirely in India.

Development is also proceeding on a design for a carrier vehicle expected to be ready by the end of 1974. It is a four stage design similar to the Scout rocket. It will be capable of putting a 40kg package into orbit at about 400km altitude.

It is planned that the first firing be made to gain experience. Later launchings will carry on-board experiments. This will be worked up eventually to a coverage for educational purposes.

By 1974 India will have access to the NASA satellite ATSF which will be launched in 1973. This will enable India to have the facility to cover some 5,000 villages for educational purposes. India will design and manufacture the small and rugged battery receivers needed and also the 10ft diameter aerials made of chicken wire.

There are two major satellite communications stations in India one at Avi and the other at Ahmedabad. The dishes at these sites are 30m dia. Most of the research is carried out at the National Aeronautical Laboratories in Bamgalore. There are divisions there covering Aerodynamics, Propulsion, Materials, Electronics, Instrumentation and Structures.

India suffered a severe blow with the death of their leading scientist Vikam Surabhai in 1971. However, such was the nature of his forward planning that India has today a very successful space research team.

India has contributed quite considerably already to the space programmes of other countries. From the launching sites at Thube near Travandram, which is U.S. sponsored. several hundred launchings have taken place. Rockets. probes. and satellites of British. French. Russian and Indian origin have already been launched from there.

A new site now being completed. the Shrihameola Range, will extend India's future space activities even further.

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report from AUSTRALIA

BY J. M. WALDIE

FM BROADCASTING

The Australian Broadcasting Control Board has been enquiring into the desirability of f.m. radio in Australia and has now issued its findings in a 100-page volume entitled "Frequency Modulation Broadcasting". The board examined some 150 written submissions and 70 formal exhibits, and employed its Technical Services Division to carry out an examination "of every technical problem considered to be possible".

The upshot of this deliberation is to recommend that f.m. broadcasting should be introduced, and this has been endorsed by the Government.

This is, in fact, the third time that official committees in one form or another have examined f.m. radio in Australia. The first was in 1942 and resulted in the installation of four experimental transmitters, operating in Sydney, Melbourne, Brisbane and Adelaide in 1948.

OBJECTIONS

In 1957, the board conducted a public enquiry and found "very real practical objections to the introduction of f.m. broadcasting". The four stations, which by then were transmitting for some 80 hours weekly using substantially the same material as was included in the more serious of the then two ABC programmes, were closed down in 1961 to allow for expansion of the television services from 10 to 13 channels.

This situation, in which the v.h.f. band is more or less saturated with television and other services, provided a large headache for the enquiry just completed. It was preferable to use the v.h.f. band for the projected radio service for obvious reasons: the technology was well known and the signal propagation would be relatively high. However, this meant the abolition or re-allocation of one or more television channels with obvious disadvantages and the possible need to use bandwidths of as low as 0.4MHz.

The alternative was to use the u.h.f. band, which is relatively uncluttered, but this, too, has disadvantages: no other country uses u.h.f. for f.m., and standardisation should be the aim; the technology

was virtually unknown; the coverage obtainable would be lower than with v.h.f.

However, the die is now cast: the recommended bandwidth (allowing 20 stations to cover each area) is 40MHz and the suggested frequency range is 470-510MHz. Local manufacturers have three years in which to decide on the technical standards for u.h.f. reception and transmission.

PLANS FOR THE FUTURE

The aim is to provide two national stations, one to transmit the current ABC network for provincial and country areas, and the second, city-based, to provide a second "fine music" network. Commercial stations will also be licensed. Finally, a new type of station will be introduced, on a non-profit basis, to cater for the needs of minority groups. All these stations can transmit stereophonically.

It has been suggested, with just a hint of patriotism, that Australia's venture into u.h.f. broadcasting might just be the shot in the arm that the local manufacturers claim is needed. It will be interesting to see if the Japanese will produce a u.h.f.-f.m./a.m. receiver for the Australian market by 1978.

AUDIO SHOW

There can be no doubt that hi-fi enthusiasts (at least in Sydney) have an extremely large selection of equipment available to them, if the 1972 Audio Show, held in Sydney on August 9-13, is any guide. It is equally true to say that the average buyer can not be badly off; the manufacturers and importers, in conjunction with Australian hi-fi, must be conscious of a considerable interest to stage an exhibition of this magnitude.

The show actually covered three floors of a moderately large multistorey motel. The ground floor was relegated to 16 large (silent) displays; two upper floors were used to demonstrate, in over 40 individual suites, the complete range from any one manufacturer or selected combinations.

More than half the equipment shown originated in Japan, with all the major names being present. British exhibitors included Garrard (the Zero 100 deck was used in many stands), Wharfedale, KEF (who have, along with Leak and Goodmans, commenced local production), Plessey, BSR, and B&W.

NEW DEVELOPMENTS

Interesting new developments for the cassette enthusiast included the new Sony deck (TC 165) with automatic and continuous reverse facilities, several new decks with inbuilt Dolby, including National, TEAC, Kenwood and Pioneer, and a C 180 cassette, and an endless loop cassette, both from TDK.

There were many four-channel units demonstrated, but by far the most impressive was one line-up consisting of a four-track TEAC 3340 deck, feeding two JVC PST 1000 stereo graphic equalisers, in turn feeding two phase linear power amplifiers whose 2,800 watts (r.m.s.) output was handled by four ESS transmission line speakers—and this in a room measuring about 12ft × 15ft! Cost—about £4,000, but trade-in's are acceptable.

OPTICAL COMMUNICATIONS

Australian communications may benefit from a new joint venture by Amalgamated Wireless (Australasia) Ltd., and the Tribophysics Division of the Commonwealth Scientific and Industrial Research Organisation (CSIRO). The CSIRO have developed a new type of optical fibre, consisting of a liquid-filled hollow glass tube.

Although finer than a human hair, the fibre could transmit more information than existing wide-band microwave and coaxial communication links. Using a helium-neon injection laser as a light source, for example, it is claimed that, using the new fibre, previous disadvantages of signal loss over long distances using light guides are overcome.

The system has been made available to the Australian Post Office for its research laboratories to evaluate the fibre's potential in the development of Australia's Telecommunications network.

It is certainly a far cry from that eventful day in 1870 when John Tyndall showed that light could be borne by a liquid around corners.

A VERSATILE INSTRUMENT FOR THE COMPOSER, MUSICIAN OR KEEN EXPERIMENTER IN THE CREATION OF SOUNDS IMITATIVE OR UNIQUE By G.D.SHAW NOISE CEN

effects by means of a variety of electionic devices has been possible for a good many years. The electronic organ, for example, was becoming rapidly accepted a decade before World War II. Of the vast range of electronic instruments now available, however, there are a few which are not aligned to operate around a conventional chromatic scale. Thus, for the performer, the appeal of such instruments would be based primarily on the effect of tone quality, ease of playing and novelty in design.

For the composer, however, the abundance of electronic instruments does little more than provide a range of alternatives to supplement or replace standard instruments of the orchestra. Out of such a situation the idea of musique concrete was born. This technique enabled composers to create and experiment with sound forms generated naturally or unnaturally by such unlikely sources as dustbins, rattling teacups, conversation or malplayed musical instruments. Some workers incorporated a system of manually operated oscillators. both groups linking their sound sources to one or more disc cutters or, later, tape recorders.

The task of creating and blending discrete tones into a coherent and recognisable musical work involved so much laborious effort that musique concrete established the reputation of being more of a technical exercise than a creative art form. Thus the publication of Moog's designs for voltage controlled amplifiers and oscillators about eight years ago was hailed with enthusiasm in many quarters of the musical world.

Moog's designs crystallised the ideas and requirements expressed by a number of serious composers whose creativity was hampered and frustrated by the confines of the accepted musical disciplines. The possibilities of, and extensions to, Moog's original circuits have led with great rapidity to the inception of a series of variably complex devices having the generic label of 'synthesiser'.

THE SYNTHESISER DEFINED

What exactly is a synthesiser? The word "synthesis" is defined as the building up of separate elements into a connected whole and this, very succinctly, describes the function of the synthesiser with respect to the formation of sound structures.

Essentially the instrument consists of a number of sound sources and sound treatments which may be combined together in an enormous diversity of ways to produce an equally varied range of sounds in a number of applications.

- 1. As a live performance instrument. A considerable company of popular artists and groups use a synthesiser, in one form or another, as a standard item of equipment either to supplement their normal methods of sound treatment or to play as an instrument in its own right.
- 2. As a sound effects unit. The use of the synthesiser is by no means restricted to musical circles and it is equally at home "producing" creaking doors, artillery fire, explosions, dripping water, birdsong and a virtually unlimited range of sounds similar to those featured in and popularised (for some) by the "Dr Who" series. Thus the tape recording enthusiast, amateur dramatic society, cine club and so on could easily find the synthesiser becoming a useful and indispensible tool.
- 3. As an audio-visual teaching aid (in conjunction with a good oscilloscope) the synthesiser can provide an invaluable insight into the fundamentals of electronic and acoustic waveform phenomena. In this respect there is a large potential field of application.

IMITATIVE OR UNIQUE

The term synthesiser carries the implication, for some, that the instrument is of an essentially imitative nature and/or that the sounds produced by it are ersatz. With regard to the former criticism, the degree of control which may be exercised in a well designed synthesiser is such as to allow it to imitate a wide range of musical instruments very effectively.

For the sound effects man, the ability of the instrument to produce imitations of a wide range of naturally occurring sounds is a feature which

cannot be lightly set aside.

In answer to the second criticism which implies that the sound forms produced by the synthesiser are, in a sense, unreal—nothing could be further from the truth. The nuance and timbre imparted by the synthesiser to a fundamental tone is no less real than the nuance and timbre imparted, to the same tone, by, say, a trumpet or a violin. In practice, the purity and exactitude of the tonal permutations made available by the synthesiser are frequently inspiring and possess a beauty which is peculiarly their own.

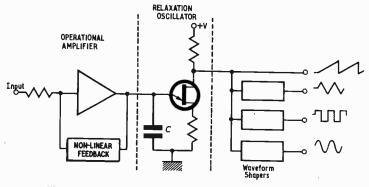


Fig. 1. Block diagram of a voltage controlled oscillator

VOLTAGE CONTROL

Various forms of voltage control have been known and exploited for a number of years but the application of the principle to the control of synthesiser circuits results in the appearance of a number of unique features. By way of illustration one could scarcely choose better than a form of voltage controlled oscillator based on the design published by Dr Moog. Fig. 1 shows such a device in block form.

The relaxation oscillator is driven by an operational amplifier the output current of which is proportional to the exponential of the input. As the output current increases so also will the rate at which the charge on capacitor "C" reaches the unijunction breakdown voltage. Thus the frequency is increased.

The unijunction sawtooth is fed to a series of waveform shaping circuits which provide a useful number of "in phase" outputs. By means of this system relatively wide frequency ranges may be obtained without the necessity of switched RC or inductively tuned networks.

The general principle of voltage control may similarly be applied to almost any parameter in any of the devices built into the synthesiser, e.g. amplifier gain, filter bandpass or band reject characteristics, degree of reverberation and so on. There are a number of distinct advantages in so doing, these are:

 Signal and control paths are quite separate from one another. Thus a device may be remotely controlled without compromising the signal in any way.

2. Devices can control one another in a continuously variable manner without the necessity of complicated, expensive and limited-range switching circuits. In certain circumstances a device may control or limit its own output by using part of the signal output as feedback to the control input.

 By provision of high input impedance to the control circuits each controlling device has a potentially large "fan-out" capability thus making multiple parameter control a possibility.

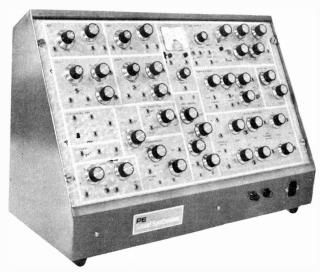
A specific example of voltage control is given later in this article and will serve to underline the flexibility and versatility of the system.

SYNTHESISER DESIGN

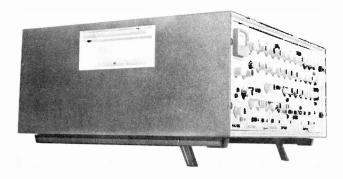
In designing a synthesiser care has to be taken to ensure that the system does not become so complex that it is impossible to operate effectively.

Consequently it is necessary to define the requirements of the instrument and to specify the means by which these requirements may be met. In this respect a form of modular construction offers the distinct advantage that one may start with a simple system and increase the size and complexity as and when required.

As a general rule most sounds have a fairly complex structure comprising a fundamental tone, one or more overtones or harmonics and, in some cases, an element of noise. It is usually the fundamental tone which dominates the sound structure and which provides the primary means by which the sound is observed.



The author's prototype synthesiser is shown above. Below is the final version built in modular form and housed in a Vero metal case



Another important feature concerns the way in which the sound structure is presented. The rapidity with which the sound becomes audible, the maximum volume attained and the rate at which the sound dies away together constitute a pattern, known generally as an envelope, which contributes very largely to the recognition of the sound. Variation in the rapidity of attack and the rate of decay of an otherwise unchanging sound structure can make an enormous difference to the auditory effect of the sound on an observer.

Two other factors play an important part with respect to the recognition of sound. These are timbre and nuance. Timbre is defined as the characteristic quality of sounds produced by each particular instrument or voice, depending upon the number and character of the overtones while nuance relates to the delicacy, or shade of meaning, of a sound.

ACHIEVING THE REQUIREMENTS

It is a relatively straightforward matter to provide hardware to meet three of the above requirements, i.e. fundamental tones may be provided by one or more oscillators; variation in sound presentation is achieved by means of an envelope shaper while timbre may be varied by selective filtering and additive mixing, either separately or in combination, together with a degree of reverberation.

Control of nuance cannot, however, be achieved by the application of a discrete piece of hardware but is controlled by the inter-adjustment of practically all the parameters involved in any particular sound structure.

PROGRAMMED MODULES

The hardware so far considered covers the basic necessities of sound formation but offers nothing that cannot be obtained from a selection of signal generators, reverberation amplifier and integrator, all of which are easily obtainable as discrete units and in a variety of forms. The next stage, therefore, is to devise a means whereby the principal function of the modules may be voltage controlled and to provide the means by which they may be programmed to produce a range of tone patterns or rhythms. Automatic programming may be achieved by provision of one or more ramp or random voltage generators.

If these latter devices are, themselves, made programmable then the possible control signal permutations, with only a small number of modules, becomes

SPECIFICATION

Stabilised Power Supply

+15V/O/-15V at 750mA per rail.

Max. ripple at 12 per cent overload is less than 15mV.

Two Input Amplifiers

Gain variable from unity to \times 50.

Two Ramp and Pulse Generators

Frequency range (a) 0.01Hz to 15Hz.

(b) 0.05Hz to 30Hz.

Manual and voltage control. Output voltage is 4V nominal ramp and -4V nominal pulse.

Two Triangular/Square Wave Oscillators

Frequency range (voitage control) less than 1Hz to 16-5kHz. Frequency range (manual control) 5Hz to 10kHz. Output voltage: Triangular 350mV p-p. Square IV p-p.

Two Output Amplifiers

Variable gain with manual and voltage control. Panning facility between channels. Input level 500mV. Maximum voltage gain +13dB.

Reverberation Amplifier

Variable gain manually controlled. Voltage control of reverberation. Unity gain with reverberation out. Frequency range of spring line -3dB at 80Hz and 4kHz. Input level 500mV.

Ring Modulator

Four quadrant multiplier based on interesponse circuit. Frequency effectively flat from d.c. to greater than 150kHz. Input levels 2×500 mV max. Output level 800mV max.

Tone Control

Tuneable active filter. Effective slope 7dB/octave. Overlapping bass and treble ranges allow extreme effects to be obtained.

Envelope Shaper

Produces an envelope of variable shape and period derived from internal constant voltage source and external trigger. May be triggered manually. Output waveforms variable from pulse, sawtooth, trapezoid, and triangular.

Noise Generator

Provides up to 3.5V white noise. Control of colouration by means of tuneable low pass filter.

Sample and Hold

Random voltage generator which can double as an additional ramp generator. Produces staircase waveforms of formal or random nature. Clock output is provided for synchronisation purposes. Output level -6V max.

Differential Amplifier

Provides additive and/or subtractive mixing facilities. Output level proportional to sum and/or difference of the four inputs provided, maximum 26V p-p.

Similar to above but with only two inverting inputs.

Meter Unit

A meter with precision rectifier circuit to read a.c./d.c. signals in two ranges, 0.5V and 1V.

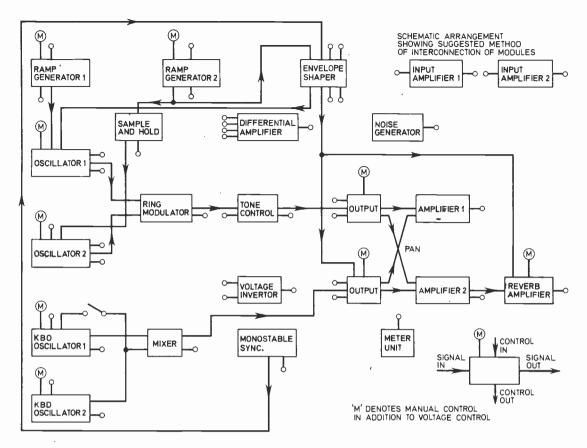


Fig. 2. Block diagram of the synthesiser

very wide indeed. If the frequency range of the ramp generators is sufficiently wide they may themselves be considered as sound sources and used for the direct provision of rhythms.

Similarly, with the control signal suitably attenuated and running at a frequency of between 6-8Hz, a single ramp generator may be used to provide a vibrato modulation to an oscillator thus adding greatly to the interest content of discrete tones.



Synthesiser keyboard with separate sustain, vibrato and oscillator units mounted on the left

ADDING A KEYBOARD

Perhaps the simplest method of programming the oscillators is by the addition of a keyboard. Since keying provides a range of control voltages to the oscillator the keyboard itself may be considered to be a manually operated staircase generator.

The keyboard may also be used to provide gating and synchronising pulses to initiate treatment or shaping sequences each time a key is depressed.

SOUND TREATMENTS

The only sound treatment so far given any degree of consideration is that of reverberation. There are, however, a number of others which can provide very useful extensions to the facilities offered by the synthesiser. Up to now the accent has been on synthesis by addition, but, equally, one can synthesise by subtraction.

In this latter case the starting point is a complex sound, such as white noise, from which the required elements are obtained by filtration. There is thus a place for one or more notch and/or band-pass filters the actual characteristics of which may be varied by means of voltage control.

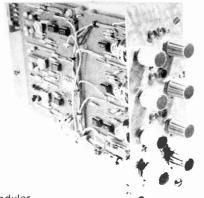
On the simpler side there is also a place for a form of tone control of sufficient range to enable extreme effects to be investigated.

INTERFACING

Finally, it is necessary to consider the best means of interfacing the synthesiser with external equipment so that it may accept as wide a range of inputs as possible without distortion and, on the output side, provide a similar widely compatible drive.

A block diagram of the synthesiser to be described is given in Fig. 2.

The idea of external connection compatibility for all modules was believed to be a prime requirement in view of the possibility that many constructors may wish to build only a limited number of the



The basic modular form of construction that will be used throughout the series

modules to be described as additions to existing synthesiser projects. In view of this situation it may seem somewhat paradoxical to provide modules labelled input and output amplifiers.

In point of fact these can be connected in virtually any position in a chain of modules the main limitation being due to the possible saturation of the amplifiers due to the input levels being exceeded.

The final stages of the output amplifiers are crosscoupled by "panning" controls thus enabling stereo and "floodsound" effects to be investigated.

INTERCONNECTIONS

Referring again to Fig. 2, it will be noted that many of the modules are shown with interconnections made between them.

Of the three most widely used systems of module interconnection the one most suited to the modular concept is that in which individual devices are coupled by means of patch cords. The great disadvantage of this system is that a complicated patch can render the front panel controls almost inaccessible.

With a view to relieving this situation modules may be connected internally in the manner in which they are most likely to be used. The actual method of internal connection is really a matter of the individual constructor's preference, those connections shown in Fig. 2 being intended as a guide rather than a mandatory requirement.

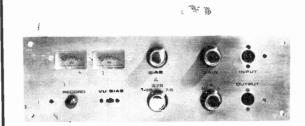
BUILDING THE SYNTHESISER

Full constructional details will be given on building the synthesiser shown and an outline specification of the instrument appears in this article.

Extensive use has been made of the 741 operational amplifier since the use of these devices invariably simplifies design and construction in comparison with circuits in which discrete semiconductors are employed. Furthermore, the 741 offers the feature of unconditional stability under almost any operating condition and is protected internally against "latch-up" and output short circuit and is readily available at economic prices from a variety of sources.

The only test equipment requirement is for a good oscilloscope, particularly during the setting up stages. Ideally the 'scope should be d.c. coupled but, failing this, a high resistance voltmeter will suffice to monitor the v.l.f. performance of the various modules.

Next month, constructional details for the stabilised p.s.u. will be given.



HI FI TAPE LINK

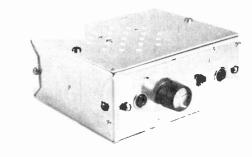
Bring hi-fi quality to your tape deck with this quarter track stereo tape link.

It features separate record and replay amplifiers using modern circuit technology to give low distortion and noise, and accurate replay characteristics.

Tape speeds of $1\frac{7}{8}$, $3\frac{3}{4}$ and $7\frac{1}{2}$ inches per second are catered for, and a switch is included for single track mono operation. Setting up requires only minimal circuit adjustments.

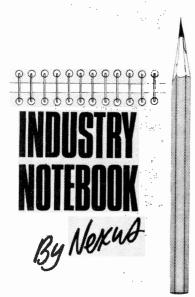
SIGNAL INJECTOR TRACER

Using a digital integrated circuit in a linear mode makes this Signal Injector and Tracer cheap and easy to build. Extremely useful for fault finding on radios, amplifiers and other audio equipment. A simply built r.f. probe makes the Tracer suitable for high frequency detection.





March issue on sale February 9



UK PRESENCE AT ELECTRONICA

The giant Electronica exhibition staged in Munich was the last of the great European shows before Britain's entry into the Common Market. And there was every sign that at long last the British were taking the ECM seriously.

One British journal organised a special charter aircraft for the show and took 117 people along, nearly all of them top executives from British companies. The British joint venture group sponsored by the Department of Trade and Industry numbered 55 companies and there were others with stands independently of the official group as well as many British products on stands of German Agents.

The Central Office of Information produced a splendid book "Electronic Components and Equipment from Great Britain" in support of the British effort. It had German text throughout its 62 wellillustrated pages and again this shows Britain waking up to the facts of life, one of which is to address your audience in their own language.

In all, there were 1,600 exhibitors from 22 countries. As this was only the fifth Electronica the growth rate of the exhibition must be regarded as truly startling.

The only gripe I heard in Munich was on prices. Munich has always been pricey by British standards but this year's combination of the floating pound (buying fewer marks) and the aftermath of the Olympic Games which has inflated local costs made our British high street and pub prices look really modest.

GREAT LEAP FORWARD

The year 1973 should be good for Solartron and the Schlumberger Group, of which Solartron is the U.K. member. I hear that the French companies in the Group have now virtually completed a rationalisation programme in which what was once a rag-bag of smallish companies has now been consolidated into major groupings of considerable strength.

In Britain, Solartron's Farnborough plant was as busy as I'd ever seen it when I called in last month. The Master Series, a range of a dozen digital voltmeters launched earlier this year, was described to me as having made a major impact in the market place with revenues already ahead of schedule. But the big new field is in radio frequency instrumentation and Solartron will be offering equipment for use up to 40GHz.

Another new Solartron activity is frequency synthesizers. This activity was previously concentrated in the Munich plant but now Farnborough engineers are involved in a joint development programme and new models will probably be manufactured in both locations.

Another bright product line is the realistic tank gunnery simulator known as "Simfire" for which Solartron recently won a Ministry contract worth £1.4 million following successful field trials by the 15th/19th Hussars in Germany. The system uses a low-power pulsed laser beam to simulate the firing of the shell and its trajectory. The target is fitted with detectors and if a hit is detected it triggers off a pyrotechnic display on the "killed" vehicle.

Solartron is spending plenty of cash on R and D to bring themselves into a leading position in Europe. Most companies think themselves pretty progressive if they plough back 10 per cent into R and D. The Solartron figure is currently running at 14 per cent on the instrument side of the business.

The biggest Schlumberger business, though, is still in oilfield instrumentation. Worldwide there are 30,000 employees operating in 50 countries.

LES FOLIES

One of the brightest of the new generation of electronic industry entrepreneurs, Tom Jermyn, has a keen eye for the ladies, in a strictly business sense of course. His company, Jermyn Industries, manufactures semiconductor accessories such as i.c. sockets, transistor pads and heatsinks for which there is a world-wide sale.

Nearly three years ago he set up a sales office in Munich, soon to be followed by another in San Francisco and now he has opened his third in Paris. They all have one

thing in common-all are managed by ladies, and all of them good lookers.

Heading up the Paris office (appropriately located in the rue de Londres!) is multi-lingual Stella Bornstein who now joins Lore von Kleist, Munich, and Janice Pascoe, San Francisco. Stella is as yet untested, having only just started, but Janice and Lore have easily outpaced the performance of the local agents they replaced, Lore for example having built up the German business to 50 per cent of the present Jermyn U.K. turnover.

The point of this story is not so much the girls but how some of our more thrusting companies are getting around the world and really sellina.

Incidentally, Jermyn is expanding manufacturing facilities beyond simple semiconductor accessories. Latest product is a 300W triac-controlled light dimmer which fits neatly in place of the common square MK light switch. The dimmer, designed by Jermyn engineers, is also available in kit form for home constructors.

NEW LINE ON DEFENCE

Defence contracts may be getting harder to come by but they are still very big business. A new lineup of Thorn Automation, the Kelvin Hughes and Aviation divisions of Smiths Industries, and Scott and Electromotors, will be in a stronger position to bid for contracts under the group name Defence Equipment. Between them they employ 11,000 people and have combined assets of £164 million and a turnover of £440 million.

One reason for the link-up is said to be the reduction in size of Ministry R and D establishments and the farming out of work to the larger companies.

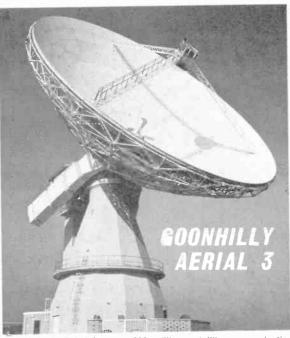
IN TRIPLICATE

Despite all the trials and tribulations experienced during the commissioning of the new traffic control system at West Drayton, Marconi Radar Systems has finally handed over the £5 million complex after a year of operational trials. The triplicated MYRIAD computer systems operate independently to give a reliability such that the system is only out of action for less than thirty seconds in five years.

Another Marconi achievement was the £1.5 million system for Eurocontrol based at Bretigny, near Paris. This has now also been handed over. Marconi led the international consortium which included Standard Elektrik Standard Elektrik Lorenz of Germany, and S.A.I.T. Electronics of Belgium. Altogether Marconi has completed 38 major ATC instal-

lations in the last decade.

ELECTRONORAMA



Goonhilly 3, Britain's new £22 million satellite-communication aerial, is significantly different from the two earlier aerials at the Post Office's earth station on Goonhilly Downs. It is specifically intended for tracking satellites in geo-stationary orbit, whereas Goonhilly 1 was designed for tracking fast-moving satellites, and Goonhilly 2 for both sub-synchronous and synchronous orbiting satellites.

REFLECTOR

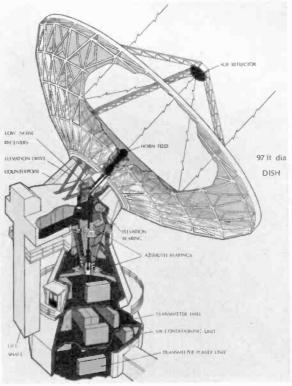
The 29-6-m diameter reflector of Aerial 3, although larger than those of aerials 1 and 2 (26m and 27-4m respectively) for improved performance, is considerably lighter, due to the use of 2mm aluminium sheet for the reflecting surface, instead of stainless and mild steel. The sub-reflector can be tilted under the control of an hydraulic system to deflect the aerial beam by up to 25 minutes of arc in azimuth or elevation without moving the main reflector.

DRIVE EQUIPMENT

Movement of the main reflector about each axis is effected by twin driving units each having two electric motors. Solid-state control devices are used instead of rotating machines as on aerials 1 and 2.

When the satellite starts to move out of the beam, error signals appear and activate the servo systems which steer the beam to eliminate the tracking error. Tracking can be accomplished by movement of the main reflector with the sub-reflector locked in a central position, or alternatively by movement of the sub-reflector





only

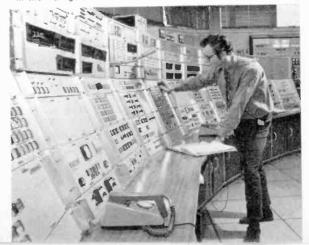
Goonhilly 3 is currently transmitting two and receiving 11 telephony carriers, although it is capable of being expanded ultimately to receive 33 carriers. The transmit carriers are radiated in the band 5.930 to 6.420GHz and received in the 3.705 to 4.195GHz band.

When required, Goonhilly 3 transmits and receives two television carriers, one for vision, the other for sound. It can also operate a transmit and receive contingency carrier arrangement to support services lost during failure of a transatlantic cable.

RECEIVING SYSTEM

The received signals pass through flexible waveguide to one of a pair of low-noise parametric amplifiers, cooled to 15 K (-258 C) by a closed-cycle gaseous-helium cryogenic system (bottom left).

The signal from the LNAs, further amplified by 40dB in a travelling-wave-tube amplifier, passes by waveguide down the centre of the king post to a rotating waveguide joint, and is then carried in the waveguide to the central control building (bottom right).





THE BOARD to be described this month is the all important ADDER board which forms the heart of the arithmetic section of the calculator. The name ADDER is a shortened name for what is really an adder/subtractor with carry store, but before going into the design of the board in detail it is necessary to recall some of the principles of binary and B.C.D. addition and subtraction.

BINARY ADDER

The principles involved in a simple single stage binary full-adder are fairly well known in this, the computer age, but for the sake of completeness it is

as well to run over them again here.

Fig. 8.1. shows the logic diagram of a typical binary adder which generates a SUM and CARRY output from the three inputs termed A, B, and CARRY IN. The word "typical" is quite meaningful in this connection because a circuit to perform binary addition can be made up in a number of different ways, the end result being the same, no matter which gating arrangement is used.

The performance of this sort of array is best described in terms of a truth-table which lists the circuit's output response to all possible input conditions, and the truth-table for the ADDER is also given in Fig. 8.1. If any reader is unfamiliar with the basic rules of binary addition, studying the truth-

table will tell all.

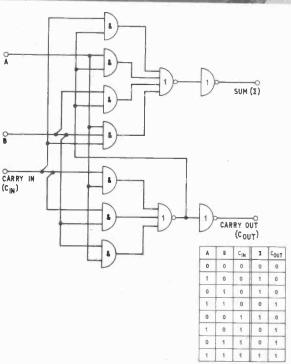


Fig. 8.1. Single binary full adder stage. The truth table defines all the outputs for all combinations of inputs

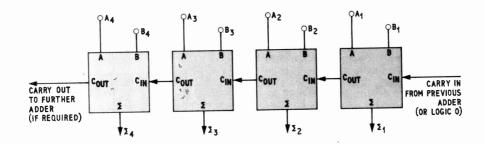


Fig. 8.2. A parallel binary adder to add two four-bit words. Each of the stages in this adder is identical to that shown in Fig. 8.1

PARALLEL BINARY ADDER

A binary adder stage like that of Fig. 8.1 is of limited use as it stands, being capable of adding together only a single pair of binary digits and a carry, whereas most sums a machine is asked to solve would stretch to a number of pairs of such digits. The simplest way to extend the capabilities of this circuit is to use a number together to form a parallel adder like the one in Fig. 8.2.

Each pair of binary digits in the two numbers to be added has its own adder circuit with the CARRY connected in series down the chain. This method of addition is widely used in binary computers but suffers from the disadvantages of large scale component use and slow propagation of the serial carry which has to "ripple-through" to the last stage

before the addition is complete.

A circuit arrangement which only uses a single adder stage to add two n-bit numbers is quite possible if the addition is carried out sequentially, i.e. one pair of digits at a time, in a system such as that shown in Fig. 8.3. This method of binary addition is called "serial addition" and requires a store to "remember" the CARRY from a previous addition so that it may be added in with the next.

The two basic addition methods are both employed in Digi-Cal, with some special modifications to allow

operation in the B.C.D. code.

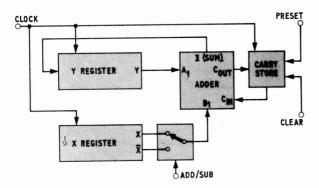


Fig. 8.3. Basic serial binary adder/subtractor. The ADD/SUBTRACT unit presents either the true or complemented output from the X REGISTER to the adder under the control of the FUNCTION CODE A signal

SUBTRACTION

Once the truth table required of a binary subtractor has been worked out it is quite easy to design a simple logic circuit to perform the operations required, but in practice this is very seldom done, because, by making the number to be subtracted negative, i.e. by complementing it, it is possible to achieve the effect of subtraction in an adder circuit of the types already described.

The principles underlying this method of subtraction are quite straightforward and it can be readily appreciated that adding a negative number is the same as subtracting a positive one. Turning a positive binary number into a negative equivalent is simply achieved by inverting all its digits so that all the ones become zeros and vice versa, and then adding a one in the least significant position, for example

binary three 0011 becomes 1100 plus 1 equals 1101

To show that this process does generate a negative equivalent we can add the result to say binary four:

binary four 0100
plus binary thirteen 1101 (complement of binary three)

equals 0001 which is correct

Note that the carry digit from the most significant stage is disregarded, being only an indication of whether the result is positive (as in this case) or negative (if no CARRY results).

The operation of these principles in a practical circuit can be seen in Fig. 8.3 which is a serial adder system with subtraction carried out by simply feeding the inverted version of the X REGISTER output to the ADDER, and arranging for a carry to be preset into the store before the start of the clock pulse series.

M.S.I. ADDERS

The TTL medium scale integration process has been used to produce several different binary adder circuits ranging from the very flexible SN7480 single, full adder to the compact SN7483 cricuit which contains four complete adders arranged as a four-bit parallel adder. It is this latter device which is used

in the 'Digi-Cal adder circuitry, where the four-bit length lends itself well to use with the binary coded decimal (B.C.D.) arithmetic process.

The SN7483 is used as a basic building block in the adder to be described and before venturing into the intricacies of B.C.D. addition and subtraction it is best to become familiar with its construction and operation in its intended role as a parallel binary arithmetic unit.

The equivalent logic circuit of the SN7483 is shown in Fig. 8.4 and comparison of this logic with Figs. 8.1 and 8.2 will show that this device is connected to add together two, four-bit binary numbers with a CARRY IN to the first (least significant) stage, termed C_0 , and a carry out from the final (most significant) stage termed C_4 .

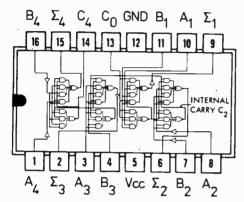


Fig. 8.4. The internal logic of the SN7483 four bit binary adder i.c.

The two four-bit words to be added to indicate the termed A and B with a suffix 1 to 4 to indicate the significance of each bit. The carry circuit delays have been reduced as far as possible by internal connection, the use of high-speed type gating, and the elimination of unnecessary inversion circuitry, so that the addition time is kept below 100ns.

BINARY VERSUS B.C.D.

The numbers stored in the registers of Digi-Cal are represented by groups of four binary digits conforming to the Binary Coded Decimal (B.C.D.) code. This code is not complicated since it is identical to straight binary except that only the values 0 to 9 inclusive are allowed in each four-bit group instead of the values 0 to 15.

With straight binary the word length can be any convenient value, depending on the quantities to be represented, each increment to the word length increasing the range of representable quantities by a factor of two.

In the B.C.D. system however the binary word length must not exceed four bits, and the value of each four-bit word must not exceed 9. Capacity is increased by adding extra four-bit B.C.D. words, each of which increases the range of representable quantities by a factor of ten. As an example of the contrast between the two systems:

0110 equals 6 equals 9 (In straight binary or B.C.D.)
01101001 in straight binary equals 105

0110,1001 in B.C.D. equals 69

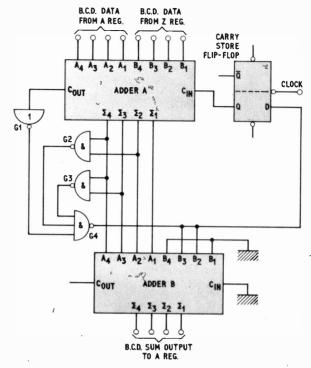


Fig. 8.5. Basic practical B.C.D. adder with a carry store flip-flop

The use of B.C.D. in calculators is desirable because of the simplicity in interfacing the logic with old fashioned human operators who insist on thinking in the decimal number system.

B.C.D. ADDITION

When two four-bit B.C.D. words and a possible B.C.D. carry bit are added together in a parallel binary adder a total of 19 different (four-bit + carry) sums can be produced. Since the largest quantity representable in the B.C.D. code is 9, it is obvious that the nine most significant sums will require correction, and will be responsible for the generation of a B.C.D. carry bit. A moment's thought reveals that the correction required by sums from ten to 19 is the subtraction of ten, e.g.

7 plus 6 equals 13
subtract 10
equals 3 plus a carry to the next decade.

As we have seen already, the subtraction of ten is readily achieved by adding its complement, which is 0110, or 6 if you prefer, and so the problem reduces to that of detecting sums in excess of nine so that the subtraction can be initiated.

The basic circuit of the B.C.D. adder used in Digi-Cal is shown in Fig. 8.5. Here the two B.C.D. words are added in ADDER A in the conventional binary fashion, the detection for sums in excess of nine being performed by gates G1, 2, 3, and 4. If any such sum is detected G4 feeds a carry to the carry-store flip-flop and inserts 0110 into ADDER B where it is added to the sum from ADDER A.

The output from the second adder is the corrected versions of sums over nine, but if a carry is not required because the sum is less than or equal to nine. ADDER B passes the sum from ADDER A through to its output in an unmodified form due to the addition of 0000 instead of 0110.

CARRY DETECTION LOGIC

The performance of gates G1, 2, 3 and 4 in detecting sums in excess of nine can be taken for granted if the reader prefers, but for those who would like to know how the gating arrangement was arrived at, and who have some previous logic experience, the design was carried out as follows.

The CARRY OUT from ADDER A is a ready made indication that the sum is in excess of 15, which reduces the problem to that of detecting sums of between 10 to 15 inclusive. To determine the gating required, the sums in question are plotted on a

Karnaugh map, as shown in Fig. 8.6.

The Karnaugh map is just a special way of drawing a truth table to make it easy to see what gating will be required to generate a specific function. It has the property that where adjacencies occur in the plots, the particular value, or values which change between the plots can be eliminated from the resulting logic equation.

As can be seen in Fig. 8.6 there are two distinct groups of plots, 10, 11, 14, 15, and 12, 14, 15, 13. In the first group the terms Σ_1 and Σ_3 change, and can be eliminated. In the second group the terms Σ_1 and Σ_2 change, resulting in the required gating function of (Σ_2 and Σ_4 or Σ_3 and Σ_4) or (Cout).

This function could be realised using two two-input and gates and a three-input or gate, but as the standard gating function of TTL is nand it is possible to invert $C_{\rm out}$ nand Σ_2 and Σ_4 and Σ_3 and Σ_4 , and feed these inverted functions to a further nand gate which carries out the Nor function because of the inverted nature of its inputs.

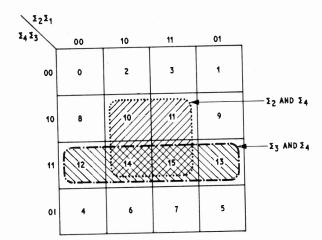


Fig. 8.6. The Karnaugh map used to determine the gating required to detect the sums from 10 to 15 inclusive

B.C.D. SUBTRACTION

The B.C.D. ADDER just described cannot be used for subtraction as it stands, and the method of addition of complements is complicated by the fact that it is not the straight binary complement which is required, but the decimal complement which can be defined as 10 minus the number to be subtracted. In practice the generation of the "tens complement" causes problems with the carry logic, and it is preferable to generate the "nines complement" by subtracting from nine and then use the carry logic to add in a 1.

The generation of the "nines complement" of the data from the Z REGISTER requires the addition of the circuit shown in Fig. 8.7, which employs yet

another SN7483 quad adder.

The principle behind this "nines complementer" is that the binary complement of the input data is added to binary nine to produce nine minus z, but since the binary complement of a number is its inverted version plus 1, in practice the circuit adds the inverted z data to binary 10 thus taking care of the extra 1 required by the complement.

The inversion of the z data is carried out in an SN7486 quad exclusive-or gate, which, when connected as shown, allows a true version of the input data through to the output when the common control input is a logic 0, and an inverted version when

the control is a logic 1.

This useful property of exclusive-or gates, along with the fact that it is the control input which inserts the required 1010 into the adder, allows the "nines complementer" to either pass the z data unmodified when Function Code A is a logic 0 indicating an addition is required, or pass the "nines complement" of the z data when the Function Code A line is a logic 1 indicating that subtraction is required.

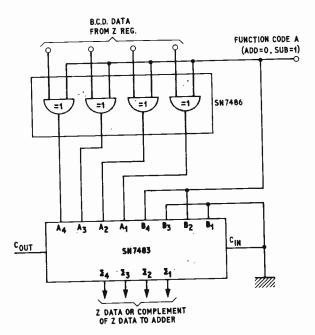


Fig. 8.7. B.C.D. nines complementer. This generates the output 9 minus Z when subtraction is required

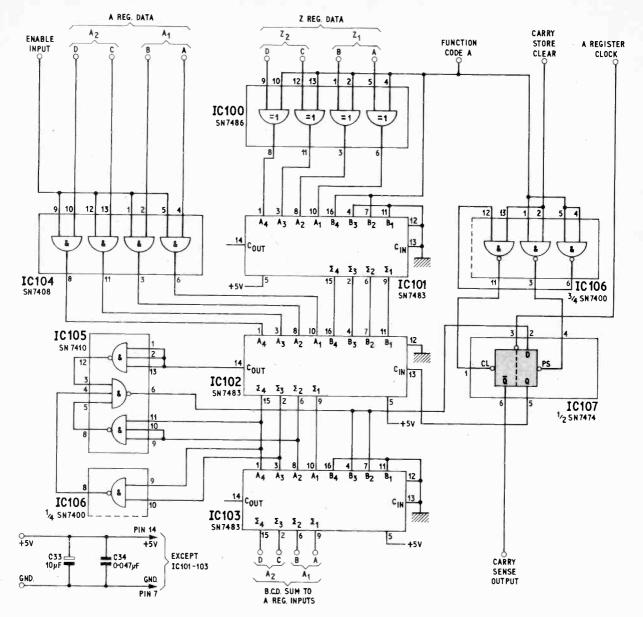


Fig. 8.8. Complete circuit diagram of the ADDER board

The details of the subtraction process are quite hard to grasp at first but the process may be easier to understand after working through the following example (right).

Note that the borrow function which would be generated if the answer to a subtraction is negative is stored in the carry store in the opposite sense to that of a carry in addition, i.e. a 1 stored means no borrow, and vice versa.

FULL CIRCUIT DIAGRAM

The complete circuit of the Digi-Cal adder/subtractor is shown in Fig. 8.8. This circuit is made up of a combination of the ADDER and COMPLEMENTER circuits already covered, with the addition of IC104 and gating for the CARRY STORE PRESET/CLEAR input.

A Register data 1000 (equals 8) в Register data 0110 (equals 6) Carry store No borrow from previous subtraction Function Code A

Subtraction

START ADDITION

Invert z data

Add to 1010 0011 Add to a data plus carry input 1100 B.C.D. carry generated Add 0110 0010 Equals 2, the required answer

1001

COMPONENTS . . .

ADDER BOARD

Capacitors

C33 10µF 15V elect.

C34 0.047µF

Integrated Circuits

IC100 SN7486

IC101-IC103 SN7483 (3 off)

IC104 SN7408

IC105 SN7410

IC106 SN7400

IC107 SN7474

Printed Circuit Board

Type DL109/22 (Shirehall)

IC104 is an SN7408 quad AND gate which is connected as an A REGISTER data inhibit, requiring its common ENABLE input to be a logic 1 before the A data is allowed through to the ADDER.

The purpose of this i.e. is to allow flexibility in the programming possibilities and, particularly, to inhibit data recirculation when the A REGISTER data is being normalised after a multiplication sequence.

The normalisation process was covered last month, and readers may recall that after multiplication, the A data are shifted to the right by the number of decimal places selected on the thumbwheel.

If the inhibit gates were not fitted the data which were to be discarded during normalisation would

recirculate and appear at the most significant end of the A REGISTER. The ENABLE input is controlled by the programme.

The purpose of the gating in the CARRY STORE PRESET and CLEAR inputs is to allow for the fact that a BORROW is stored in the opposite sense to a CARRY, requiring the store to be preset before a subtraction, and cleared before an addition. Since there is a single CARRY STORE CLEAR signal from the programme, the FUNCTION CODE A input is used to control two, two-input NAND gates which steer the CLEAR signal to the correct side of the CARRY STORE flip-flop

The only other part of the circuit worthy of note is the CARRY SENSE output which is used to inform other parts of Digi-Cal of the state of the CARRY STORE. One of its uses being to stop subtractions when a BORROW is produced after any tenth clock pulse during division, i.e. it senses when the A REGISTER contents are negative.

CONSTRUCTION

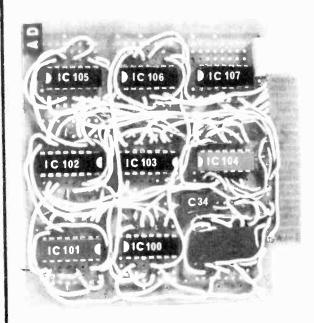
The construction and wiring of the ADDER board is quite straightforward since the circuit is housed on the usual Dualine card, in this case a DL109/22.

On this board almost all of the connections are carrying high speed data signals which must have a high integrity, and for this reason it is necessary to keep wiring as short as possible to minimise problems caused by line reflection.

The component layout and edge connector wiring

is shown in Figs. 8.9 and 8.10.

ADDER BOARD



CARRY CLEAR CLOCK 24 25 CBADCB 26 27 28 29 30 οῦτ INPUT 31 32 GND 33 .5 V CARRY SENSE spare CB 40 INPUT 41 FUNC CODE A

Fig. 8.9. Layout of the components on the DL109/22 printed circuit board

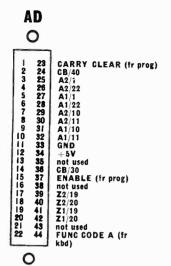


Fig. 8.10. Function of the edge contacts for the ADDER board

TESTING

Checking out this board in isolation is relatively easy since it is possible to check the sum responses to various dummy control and data inputs. The data values can be inserted by wiring each of the four data lines from the separate sources to ground, or leaving them open circuit, to simulate a particular B.C.D. number.

Providing the enable and function code a lines are also properly activated, a B.C.D. answer should appear on the sum outputs from IC103, and a Carry/borrow signal at the D input of IC107. The Carry Store clear input can also be tested in combination with function code a, monitoring the result at the Q or \overline{Q} output of the flip-flop.

Constructors who have followed the assembly sequence suggested will also be able to try the first complete calculations on their machine by judicious application of dummy control signals which would

normally emanate from the programme.

Numbers entered into the ENTRY REGISTER can be transferred to the z REGISTER by operation of the (cleared) A REGISTER by momentarily grounding the START CLOCK input to board CB. This process requires a large number of temporary control signals to be wired in, and may be daunting to some readers: the prospect has been suggested only to enable the more adventurous to experiment with the way the programme board (to be described next month) will be required to carry out the process of addition and subtraction automatically. Those who do attempt this type of test will learn a great deal about the intimate workings of Digi-Cal.

Note: In Part 4 (Oct. 72), Fig. 4.2, C13 on IC21 should be marked C9, and C8 should be $10\mu F$ not $22\mu F$

Next month: Programme Board

NEWS BRIEFS

COMPUTER '72

TAKING both the Grand and National Halls at Olympia, the COMPUTER '72 exhibition (December 4 to 8) attracted over 200 international companies who had data processing services to offer. The organisers of this show, the Business Equipment Trade Association, described its purpose as "explaining the benefits of electronic data processing to commercial and industrial management", thus the exhibition presented services rather than the actual hardware itself, though peripherals were much in evidence.

One of the most attractive stands was that of the Post Office. The display was a symbolic representation of their Datel services in multicoloured plastics, with some exhibits showing data transmission techniques of

he past.

On the hardware side, Hewlett-Packard presented their new minicomputer, Model 30. This computer is no larger than a good sized teletype terminal and provides an economical alternative to time-sharing, operating in BASIC, the language most used for time-shared systems. It has an internal cassette store with a capacity of 24,000 numbers. Its readout is via an 80 character alphanumeric display, though a printer is an optional extra.

As well as the main exhibition some light relief was provided by Honeywell who presented the winning entries to the Observer Colour Magazine children's "Paint-a-Computer" competition. Also on display was the Honeywell/Roland Emett forget-me-not computer. On the NCR stand a simulated game of cricket was being played through one of their computers and results were presented as the "game" progressed.

The bringing together of a large number of com-

The bringing together of a large number of companies in this way is obviously a great service to management and the success of this and future shows is

assured.

High Speed Printer Using a Laser

A NON-IPACT printer capable of writing 1,000 lines per minute is being developed by R.C.A. for the U.S. Army. The new printer uses a laser to transfer digital communications alphanumerics onto ordinary paper.

The printer is called the Material Transfer Recorder (MTR) and uses a dye-coated plastic ribbon scanned by the laser beam to record the messages on the ordinary

paper

There are no keys as in normal mechanical printers thus wear problems and maintenance are greatly reduced. Also the printer is almost silent because of the lack of impact.

Through its data interface the MTR can receive any type of digital signal from a wide variety of sources including satellite ground terminals. It can receive this information at the rate of 20,000 words per minute.

The MTR is easily transportable and can be used in the field in a van or any other military shelter.

BINDERS

Binders for P.E. are available price $\pounds I$, including postage and packing. State Volume Number required.

Orders for Binders should be addressed to Binding Dept., IPC Magazines Ltd., 68, Great Queen Street, London, W.C.2.

Colour Television I.C.'s

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TB	A500 £2.00	TBA550 £3.00	SL436B-E	£3.86	
		TBA560 £3.28	SL432A-T	£1.16	
		TBA750 £1.04	SL901B	5 21.10	
		TBA990 £3.99	SL435C-E	f2.66	
		CLADOD C4 ER	CI 017A		

I.C. Sockets

Dual-in-line or Zig-Zag (Quil), 14 and 16 pin Our Price 15p

Slider Pots

•	14C1 1 -	
Single .	Dual	log
10K	10 + 10K	10
25 K	25 + 25K	lin
50K	50 + 50K	
100K	100 + 100K	Knobs
30p	50p	10p

NEW LISTS
LOUDSPEAKERS
COILS AND INDUCTORS
TRANSFORMERS
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AA119 9p AA120 9p AA129 9p BA102 25p	BA156 15p BA243 56p OA47 10p OA79 9p	BY176 £1·50 BY182 £1·50 BY250 23p IN4001 6p
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VDR's & Thermistors

A15B CZ1 CZ4 CZ13A E298 E0 E298 ZZ GL16 £	/06	R53 R54	£1-32	VA1005 VA1026 VA1033 VA1040 VA1053 VA1055S VA1034	15p 13p 13p 10p 10p 10p 10p
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Resistors

½ watt 5% Carbon Film – low noise Hi-Stabs
All E24 values 1p each plus p. & p. 7p for up
to 50 Resistors and a further 2p for each
additional 50. Deduct 331% for 100 of one
type or 25% for mixed orders over £1 in value.
1 W 10% Carbon Composition 3p each
2 W 10% Carbon Composition 6p each
2 W 5% Wire wound 9p each
5 W Wire wound 9p each
10 W Wire wound 10p each
plus p. & p. 7p for up to 25 resistors plus 1p
for each additional 25.

Power Sections

	•••
ohms 7. 9. 10. 12. 14, 17-5, 20 22. 25, 28, 30, 33, 36 40, 47, 52, 56, 60, 63, 66 75, 87, 100, 120, 140, 160 180, 200, 220, 250, 270 300, 350, 400, 470, 560 100 plus p. & κp. 7p per section.	(a) 700mA 20p (a) 700mA 25p (a) 300mA 25p (a) 300mA 25p (a) 300mA 25p (a) 150mA 25p (a) 100mA 20p (a) 70mA 25p

Mains Droppers

$ \begin{array}{l} \text{(1) } 37\Omega + 31\Omega + 97\Omega + 26\Omega + 168\Omega \\ \text{(2) } 14\Omega + 26\Omega + 97\Omega + 173\Omega \\ \text{(3) } 30\Omega + 125\Omega + 2.85K\Omega \\ \text{plus p. \& p. 7p per dropper.} \end{array} $	50p 50p 50p
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Potentiometers



5ΚΩ 10ΚΩ 25ΚΩ	50ΚΩ 100ΚΩ 250ΚΩ	500K Ω 1M Ω 2M Ω	
og or lin	less switch with switch	(& 1KΩ lin)	12p 24p 40p
og only		, 100K & 1M less switch	52p 40p

Eliminators



The state of the s	
9 volt (# 20mA (PP3)	£1.25
6 volt (a 50mA	£1.50
9 volt (a 50mA	£1.50
6 +6 volt, 50mA	£2.50
9 9 volt, 50mA	£2.50
7½ volt for cassette recorders	£2.00
6, 71 or 9 volt	£3.00
3, 41, 6, 71, 9, 12 @ 500mA (illus.)	£3.99
Car Battery Converter fully stabil	ised to
provide 6, 7½ or 9 volts	£4.99
(p. & p 15p on all types)	

Presets

			1	
Vertic	al or Hori	zontal		-
0-1 was	tt 5p	0 25 wa	att 7p	
100	1 K Ω	10K Ω	100K Ω	1M Ω
250	· 2.5K Ω	25K Ω	250K Ω	2.5M 1
500	5K ()	50K Ω	500K Ω	5M 12

Capacitors

Ceramic	- pie		63V	(C3333)	i
1-8pf	8-2	pf	33	of	120pf
2-2pf	10	pf	39	of	150pf
3-3pf	12	pf	47	of	180pf
3-9pf	15	pf	56	of	220pf
4-7pf	18		68	of	270pf
5-6pf	22	pf	82	of	330pf
6-8pf	27	pf	100	of	
all 5p. ea	ch		-		
mylar fil	m		100V		
1000pf	2p	-01 μF	3p	1068µ	₹ 4p
2000pf	2p	·02μF	3p	·1µF	4p
5000pf	2p	04 µ F	3p	-2µF	5p
		05μF	3p		
metallise	on he	vester	250	V (C28	101

metallised p	olyester	25	OV (C280	")
-01μF 3p	-068µF	3½p	-47μF	8p
015uF 3p	-1 µF	4p	68µF	11p
022µF 3p	-15µF	4p	1µF	13p
033µF 3p	22µF	5 p	1.5uF	20p
-047μF 3p	33uF	6½p	2-2 µF	24p
0 17 μ. υ ρ	σομι	-26		
metallised p	olvester	- 4	100V (C2)	B1)
-01μF 44p	-047μF	6p	22µF	10p
-015μF 43p	068µF	6p	-33µF	
022µF 41p	-1μF	7p	47µF	15p
033uF 54p	15µF	8p	,	
000jii 02p	· Opi	Op.		
mixed dielec	tric	60	ωv	
-01 uF 7p	·047µF	7p	·22µF	16p
·022μF 7p	068µF	8p	471F	24p
.033µF 7p	1µF	8p	1µF	33p
-035µг 7р	1 341	op	+μ-	JJP
mixed dielec	tric	10	00V	
1000nf 6p		9p		12p

2200pf 3300pf 4700pf	6p 6p 6p	-01μF -022μF -047μF	9p 9p 12p	-22μF -47μF	22p 30p	
Ceram	ic					
12KV.c	12KV.d.c.		c.	HI-K 75	0V.	
10pf	9p	200pf	9p	1000pf	5p	
15pf	9p	220pf	9p	1500pf	5p	
22pf	9p	250pf	9p	2000pf	5p	
CO-4	2-	270-4	ō-	2000-4	65	

12KV.	d.c.	8KV.d	.с.	HI-K 750	V.
10pf	9p	200pf	9р	1000pf	5p
15pf	9p	220pf	9p	1500pf	5p
22pf	9p	250pf	9p	2000pf	5p
68pf	9p	270pf	9p	3000pf	5p
82pf	9p	300pf	9p	5000pf	5p
100pf	9p	750V E	DISC	10,000pf	5p
120pf	9p	470pf	5p	feed-	
140pf	9p	1000pf	5p	through	
150nf	9p	5000pf	5 p	-	
180pf	9p	10,000pf	5p	10 00 pf	5p
					•

GHROMASONIG electronics

Heat Sinks



	DIP10/2
	for SL403D
50p	15p

Veroboard

	Cop	Plain	
	0.1"	0.15"	0.15
2½" x 1" 2½" x 3½" 2½" x 5" 3½" x 3½" 3½" x 5" 17" x 2½" 17" x 3½" 17" x 5"	6p 20p 24p 24p 27p 67p 90p	6p 16p (9) 21p (7) 21p (8) 27p (10) 50p 70p	10p 12p 17p 37p 52p 75p
Spot-face Cutt	er 36n		

Spot-face Cutter 36p
Pin Insertion Tool 47p
Terminal Pins 18p per pack of 36

NEW LISTS	WILL WILL
BOXES, CHASSIS, etc.	No. 7
TRANSISTORS, I.C.'s, etc.	(soon)
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Aluminium Boxes neluding baseplate and screws

merc	Guig .	oa se pia	te and s	ere	
No.	L.	W.	D.	Price	p. & p.
(7)	2%"	x 5¼"	x 1½"	35p	8p
(8)	4"	x 4"	x 1½"	35p	8p
(9)	4"	x 2¾"	x 1½"	35p	8p
(10)	4"	x 5¼"	x 1½"	40p	8p
11	4"	x 2½"	x 2"	35p	8p
12	3"	x 2"	s.1"	32p	9p
13	6"	x 4"	x 2"	50p	10p
14	7"	x 5"	x 2½"	58p	12p
15	8"	x 6"	x 3"	75p	18p
16	10"	v 7"	v 3"	85n	20n

Transistors & Integrated Circuits

						-							
C107	25p	BC147	10p	BF196	15p	OC81	19p	2N1304		22p	2N5172	15p	
C126	17p	BC148	10p	BF197	15p	DC140	20 p	2N1711		25 p	BZY88	10p	
AC127	15p	BC149	10p	BF272	53p	OC170	23p	2N1893		30p	ZENERS	₽A.	
C128	15p	BC157	12p	BFY50	24 p	OC171	30p	2N2926	all	10 p	LO05TI	£1.50	
C176	15p	BC158	10p	BFY51	21 p	ZTX107	15p	2N3053		23 p	LO36T1	£1.50	
C187	25p	BC159	12p	BRY39	36p	ZTX108	12p	2N3054		50p	LO37TI	£1.50	
AC187K	25 p	BC169	15p	B\$X21	26 p	ZTX109	15 p	2N3055		49 p	MC1303L	£1.75	
A C188	25p	BC268	15p	B\$Y95A	14p	ZTX300	12p	2N3702		12p	MC1330	80 p	
AC188K	25p	BO115	67p	BU10S	£2	ZTX301	15p	2N3703		12p	MC1350	75p	
ACY20	20 p	BD131	70 p	MJE340	67p	ZTX302	20p	2N3704		10p	MC1351	£1.90	
AD140	40 p	BD132	70p	MPF192	40p	ZTX303	20 p	2N3705		10p	MC1352	£1.00	
AD149	40p	BD131/2	м Р.	MPF103	37p	Z T X 304	25 p	2N3706		10p	MFC4000	B 49p	
AD161 1	400		149p	MPF104	37p	ZTX341	20p	2N3707		15p	MFC4010	A 55p	
AD162	60p	BF160	21 p. 4	MPF105	40p	ZTX500	15p	2N3708		12p	PA234	£1.99	
A F114	18p	BF167	20 p	MPF106	45p	ZTX501	15p	2 N3709		12p	SL403D	£1.50	
AF115	18p	BF173	20p	O C 28	40p	ZTX502	20 p	2N3710		12p	TAD100	£1.50	
AF116	18p	BF180	25 p	OC35	40 p	ZTX503	17p	2N3711		12p	FILTER	£1.50	
AF117	18p	BF181	30p	OC44	15p	ZTX504	50p	2N3819		35p	LP1175	11.50	
A F139	28p	BF184	25 p	OC45	15p	Z T X 531	25 p	2N3903		15p	μA709C	45p	
3C107	10p	BF185	25 p	OC71	11p	2N697	18p	2N3904		17p	μA710	45 p	
3C108	10p	BF194	15 p	OC72	17p	2N706	12p	2 N 3905		21 p	μA723C	£1.05	
BC109	10p	BF195	15p	OC76	15p	2N708	15p	2N3906		12p	μA741C	50p	

THE TEXAN



Complete Kit (inc. Teak Case) £28.50 P&P 45p

20 Watts per channel integrated stereo amplifier developed by engineers of 'Texas Instruments Ltd.'
This designer approved kit, has a state-of-the-art specification, including distortion of only 0.09% at 20 Watts unlock 80 hims and a bandwidth of 5 – 35,000 at –304. The semiconductor compliment of this superb kit includes no less than 6 integrated circuits, 10 Silicon transistors, 4 rectifiers and 2 zeners. Controls include bass; treble; volume; balance; on/off; 'on' indicator; headphone sockets; seratch filter; rumble filter; inputs for magnetic phono; tuner; aux. or tape; tape head etc; input; selector; mono/stereo switch.

The construction of this kit was featured in 'Practical Wireless' May - Aug. 1972.

MAIL ORDERS: Where no p. 8. p. charge is shown, a minimum of 7p applies, p. 8. p. on overseas orders is charged at cost. ADDRESS TO. Mail Order Dept. 56, Fortis Green Road, London, N10 3HN. Telephone 01-883 3705 Mullard & Siemens Electrolytics

CAP	VOLTAGE									
μF	4	6.3	10	16	25	40	63			
1	_	_	_	_	-	_	6р			
1.5	_		_	_	-	_	бр			
2-2	_	_	_	-		_	6p			
3.3	_	_	_	-	_	-	6р			
4.7	_	_	_	-	_	_	6р			
6.8	-		_	_	-	6p	6р			
10		_	_	_	бр	-	60			
15	-	_	_	6р	-0.0	6p	6р			
22		_	6р		6р	_	6p			
33	-	6р	-	6р	_	6р	uka			
47	60	_	6р	_	6р	6p	6р			
68		6p	_	бр	_	_	10p			
100	6p	_	6p		6р	6p	12p			
150		6p	-	60	Бр	10p	12p			
220	60	_	6p	6p	10p	12p	18p			
330	6p	_	6р	10p			21 p			
470		6р	10p	_	12p	18p	40p			
680	_	10p	_	12p	18p	21p				
1000	10p	_	12p	18p	21 p	40p	60p			
1500	_	12p	18p	21 p	_	_				
2200	-	18p	21 p	40p	45p	55p	93 p			
3300		21 p	-	_	_	_	_			
4700	21 p	-	-	60 p	75p	93 p	-			

CAPI	VOLTA	GE		
μF	16	25	40	64
500			33p	40p
1250			50p	
1600			_	75p
2000	40p	50p	_	_
2500		_	75p	931
3200	50p	-	_	_
4000		75p	93p	_
5400	75p	93p	_	-

We still have large stocks of Multard C428 and C437 series capacitors and will continue to supply these upon request until stocks become exhausted

TV Electrolytics

	14p	32 µF		20p	
6µF 450V	15p	50µF	350V		
8µF; 450 V.W	18p	32 + 32 pF;	350 V.W		
+16µF; 450 V.W	20p	32 · 32 µF;	450 V.W	43p	
6 - 16 µF; 450 V.W	25p	$50 + 50 \mu F$;		35p	
6+100+100+300pF	; 275	V.W		£1.23	
2+100+125+200µF	: 275	V.W		£1.23	
2 + 100 + 200 + 200 µF	: 300	V.W		£1.23	
00 + 100 - 100 + 150	1504	F: 320 V.W		£1.66	
00 + 100 + 200 + 300 p	F: 27	5 V.W.		£1.23	
0+100 - 200µF; 300	V.W.			93p	
00 - 200 µF; 275 V.W				75p	
00 + 200 - 200 µF; 30	0 V.W			£1	
00 - 400 uF: 275 V.W				£1.15	
00uF; 275 V.W. 50	p 30	0 + 300 µF; 3	300 V W.	£1.90	

YATES EL ECTRONICS

(FLITWICK) LTD. ELSTOW STORAGE DEPOT KEMPSTON HARDWICK BEDFORD

C.W.O. PLEASE. POST AND PACKING PLEASE ADD 10p TO ORDERS UNDER 42.

Catalogue which contains data sheets for most of the components listed will be sent free on request. 10p stamp appreciated.

OPEN ALL DAY SATURDAYS

RESISTORS

W lakra high stability carbon film—very low noise—capless construction. W Mullard CR25 carbon film—very small body size 7:5 x 2:5mm. W 2% ELECTROSIL TRS

Power			Values	Pri	ce
watts	Tolerance	Range	available	1-99	100+
÷ ÷	5%	4·7Ω = 2·2M Ω	E24	l p	0.8p
ł	10%	3·3MΩ=10MΩ	E12	Ιp	0.8p
j.	2%	10B-IMB	E24	3·5p	3р
	10%	$1\Omega - 3.9\Omega$	E12	l p	0.8p
	.5%	4-7Ω-IMΩ	E12	l p	0·8p
4	10%	ΙΩ-10Ω	E12	6р	5.5p
Quantity	price applies	for any selection.	Ignore fractions	on total	order.

DEVELOPMENT PACK

0.5 watt 5% Iskra resistors 5 off each value 4.70 to IMO. E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70.

POTENTIOMETERS

Carbon track 5k\(\Omega\) to 2M\(\Omega\), log or linear (log \frac{1}{2}\text{W}, lin \frac{1}{2}\text{W}). Single, 12p. Dual gang (stereo), 40p. Single D.P. switch 24p.

SKELETON PRESET POTENTIOMETERS

Linear: $(100, 250, 500\Omega)$ and decades to SMO. Horizontal or vertical P.C. mounting (0.1 matrix). Sub-miniature 0.1 W, 5p each. Miniature 0.25 W, 6p each.

TRANSISTORS												
AC107 AC126 AC127 AC128 AC131 AC132 AC176 AC187 AC188 AD140 5 AD161 3 AD162 3 AD162 3 AF114 AF116 AF117	15p 112p 112p 112p 112p 112p 112p 112p 1	AF125 AF126 AF127 AF139 AF178 AF180 AF180 BC107 BC108 BC109 BC147 BC148 BC149 BC157 BC158 BC159 BC159 BC157 BC159	20p 20p 32p 32p 40p 9p 9p 13p 13p 14p 14p 14p 22p 75p	BD132 BD133 BF115 BF173 BF177 BF178 BF179 BF180 BF194 BF195 BF197 BF200 BFY50 BFY50 BFY50 BFY50 BC26	75p 75p 25p 20p 28p 32p 32p 32p 15p 15p 15p 20p 20p 20p 20p 225p	OC35 OC42 I OC45 I OC70 I OC70 I OC71 I OC81 I OC82D I 2N2926R 2N2926O 2N2926Y 2N2926G 2N2926G 2N3054 5	9p 9p 0p 8p		15p			
				-								

ZENER DIODES 400mW 5% 3:3V to 30V, 15p.	LINEAR I.C.'s (D.I.L.) 709 40p 741, 45p 710 45p 748, 45p	DIL Socket 14 and 16 pin. 16p
DIODES		

DIODES	S				
RECTIF	IER			SIGNAL	
BY127	1250V	IA	12p	OA85	7p
BZV10	800V	6A	25p	OA90	5p
BZY13	200V	6A	20p	OA9I	5p
IN4001	50V	IA	7p	O A 2 0 2	7 _P
IN4004	400V	IA	8p	IN4148	5p
IN4007	1000	1.A	12p	BAII4	8p

BRUSHED	ALUMINIU	M PANELS	
12in × 6in =	25p; 2in × 24	in = 10p; 9in	$\times 2in = 7p$

SLIDER POTENTIOMETERS SLIDER POTENTIOMETERS
86mm × 9mm × 16mm, length of track 59mm.
SINGLE 10K, 25K, 100K log. or lin. 40p.
DUAL GANG, 10K + 10K etc. log. or lin. 60p.
KNOB FOR ABOVE 12p.
FRONT PANEL 65p.
18 Gauge panel 12in × 4in with slots cut for use with slider pots. Grey or matt black finish complete with fixings for 4 pots.

THERMISTORS VA1055S VA1066S VA1077 R53 £

E

£1-35

COMPACT CASSETTES—IN PLASTIC LIBRARY BOX

MULLARD POLYESTER CAPACITORS C296 SERIES 400V: 0.001μF, 0.0015μF, 0.0015μF, 0.0015μF, 0.0015μF, 0.0015μF, 0.0022μF, 0.0033μF, 10-0.047μF, 2½p. 0.0068μF, 0.01μF, 0.015μF, 6p. 0.022μF, 7½p. 0.33μF, 11p. 0.47μF, 13p. 160V: 0.01μF, 0.015μF, 6p. 0.022μF, 7½p. 0.03μF, 10p. 0.1μF, 0.015μF, 6p. 0.15μF, 4½p. 0.022μF, 5p. 0.33μF, 6p. 0.47μF, 0.068μF, 11p. 1.0μF, 13p. 0.1μF 3½p. 0.15μF 4½p. 0.02μF, 5p. 0.33μF, 6p. 0.47μF, 7½p. 0.68μF, 11p. 1.0μF, 13p. 0.15μF 4½p. 0.015μF, 0.015μF, 0.015μF, 0.015μF, 1.0μF, 13p. 0.015μF, 0

MYLAR FILM CAPACITORS 100V 0·001μF, 0·002μF, 0·005μF, 0·01μF, 0·02μF, 2½p. 0·04μF, 0·05μF, 0·068μF, 0·1μF, 3½p.

CERAMIC DISC CAPACITORS 100pF to 10,000pF, 2p each.

ELECTROLYTIC CAPACITORS—MULLARD 015/6/7 RANGE REPLACES C426, C457 RANGES.

C457 RANGES. (µF/y) 1-0/63, 1-5/63, 2-2/63, 3-3/63, 4-7/63, 6-8/40, 10/25, 10/63, 15/16, 15/40, 15/63, 22/10, 22/25, 22/63, 33/6-3, 33/40, 47/4, 47/10, 47/25, 47/40, 47/63, 68/6-3, 68/16, 100/4, 100/10, 100/25, 100/40, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 150/6-3, 120/6-3, 150/6-3, 120/6-3, 120/6-3, 120/6-3, 120/6-3, 120/6-3, 120/6-3, 120/6-3, 120/6-3, 150/6-3,

SOLID TANTALUM E 0-1μF 35V 0-22μF 35V 0-47μF 35V 1-0μF 35V	2·2μF 35V 4·7μF 35V 6·8μF 25V	22μF 16V 33μF 10V 47μF 6-3V 100μF 3V	12 _p

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Some instrumentation or audio applications may require a greater output current capability than that provided by an integrated circuit on its own. The simplest way to achieve this is to include an emitter follower inside the feedback loop, as in Fig. 5.1.

Since the output is compared with the input the effect of the 0.7 volts base-emitter bias voltage is reduced by the feedback. If the input is zero then the output of the integrated circuit will be 0.7 volts, allowing the output of the arrangement to remain at zero, as shown in the diagram. Short circuit protection can be given by R3 and the gain is determined by R1 and R2 in the usual way.

Since this is a class-A circuit it is not suitable where load currents of hundreds of milliamps are required, and other booster circuits must be designed on the lines of class-B audio power stages. A straightforward class-B output stage is shown in Fig. 5.2.

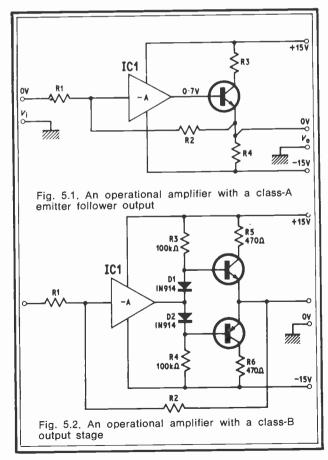
UNITY GAIN OUTPUT PAIR

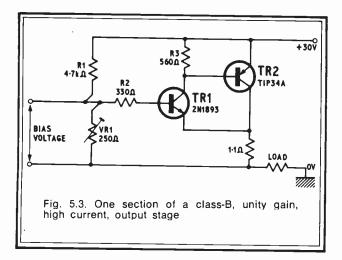
When load currents of several amps are needed a higher current gain output stage is required; one possible combination for one half of an output stage is shown in Fig. 5.3. It has several advantages, including good d.c. stability, and consists of two common emitter stages with 100 per cent negative feedback from the collector of the power transistor to the emitter of the driver transistor. This gives an overall voltage gain of unity and a high current gain.

For a positive going signal TR1 conducts, increasing the drive to TR2 which also conducts. Hence both transistors operate in class-B, apart from a small quiescent current.

For a collector current of 30mA it was found that a typical silicon power transistor required a base-emitter bias voltage of 0.56V. This seems lower than might be expected for a silicon transistor until we remember that 30mA is a small part of the 5A or so to which a power transistor can be driven.

(Indeed it is the range of currents over which a power stage has to be driven that causes many of the problems associated with this area).





The base-emitter voltage of the driver transistor was 0.65V for a 5mA collector current, and this becomes the input bias voltage required under quiescent conditions. For the other combination of a pnp driver and an npn power transistor the bias was 0.71V, and these values are typical.

PRECAUTIONS IN MEASURING CURRENTS

The quiescent current of the output transistor can only be measured in its collector lead if the d.c. conditions are not to be disturbed. Alternatively, the change in total supply current can be measured as the bias resistor is increased and the power transistor conducts.

Great care should be taken in making such tests because one careless move could result in a damaged meter or a heavy current through the transistors. A current limited power supply provides an extra measure of safety.

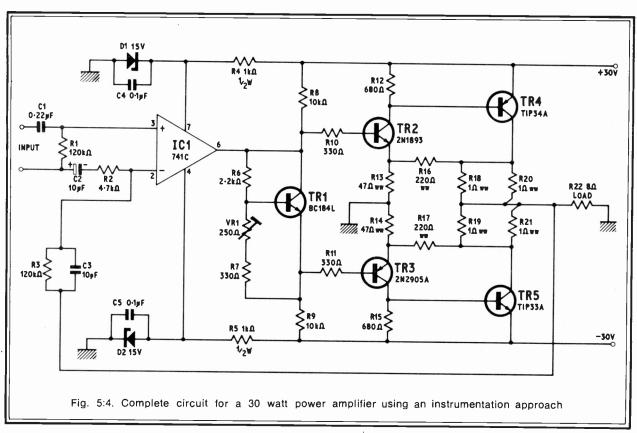
30 WATT POWER AMPLIFIER

If the unity gain power stage previously discussed is used, then the maximum output swing is limited to about 20V peak-to-peak from the integrated circuit. This would provide up to 5 watts into 8 ohms. Where more power is required the output stage can be modified to provide a small gain, five times is enough.

A complete power amplifier circuit is shown in Fig. 5.4. The required voltage gain is provided by the integrated circuit, supplemented by the output stage, while current gain is provided by the class-B output stage. The small signal driver transistor and the potentiometer allows the quiescent current to be set.

With the potentiometer at maximum resistance the transistor is bottomed and no current flows in the output stage. As the slider is brought towards minimum resistance the transistor takes less current and the collector current of the ouput transistors can be set to (say) 50mA.

There is 100 per cent overall negative feedback at d.c. to maintain the output close to earth potential under no signal conditions. Direct coupling to the

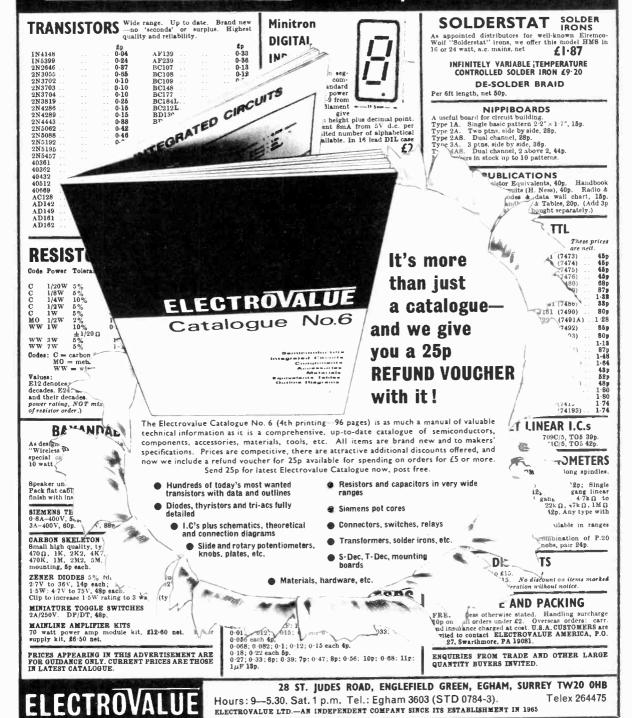


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1N21 1N23	0.20	AFZ12 A8Y26	1-00 0-25		0.85		0.82	, Z8170	0.10
1N85	0-88	A8Y27	0.82	DV710	0.32		0-45	Z8271	0.18
1N253 1N256	0-50	A8Y28	0.25	D 17 (77) ()	0.25	() A Z 224	0-45	ZT21 ZT43	0.25
1N645	0-50 0-25	ASY29 ASY36	0-30 0-25		1.00	U.1.6241	0.22	ZTX 107	0.25 0.15
1N725A	0.20	A8Y50	0.17	BYZ16	0.62		0.28 0.22	ZTX108	0.12
1N914	0.07	ASY51	0.40	BYZ88C	3 V 3	OAZ246	0.28	ZTX300	0.12
1N4007 18113	0-20 0-15	A8Y53 A8Y55	0.20 0.20		0-15 0-65	OAZ290	0.88	ZTX304	0.25
18130	0.18	A8Y62	0.25	CR81/05	0.25		0-80 0-88	ZTX 500	0.16
18181 18202	0·18 0·28	A8 Y86	0.88	CRS1/40	0-45	0010	0.87	ZTX503	0.17
2G371	0.22	A8Z21 A8Z23	0-42	C810B	2-50	0C20	0.85	ZTX531	0-25
2G381	0.25	AUY10	0-98	DD000	3·18 0·15	OC22 OC23	0.60	INTEGR	ATED
2G414 2G417	0-80 0-22	AUY10 AU101 BC107	1.60	DD003	0.15	OC24	0-60	CIRCUIT	8
2N 404	0.20	BC108	0·10 0·10	DD006 DD007	0·18 0·40	OC25	0.37	7400	0.20
2N697	0.15	BC109 BC113	0.10	DDOOR	0.88	OC26	0.25	7401	0.20
2N698 2N706	0.40 0.10	BC113 BC115	0·15 0·20	GD3	0.88	OC28	0.60	7402	0-20 0-20
2N706A	0.12	BC118	0.25	GD4 GD5	0.05 0.88	OC29	0.60	7403 7404	0.20
2N708	0-15	BC116 BC116A	0.80	GD8	0.25	OC30 OC35	0.40	7405	0.20
2N709 2N1091	0.68 0.88	BC118 BC121	0.25	GD12 GET102	0.08	OC36	0.00	7406 7407	0-30 0-30
2N1131	0.25	BC122	0.20 0.20	GET102	0-80 0-22	OC41	0.25	7408	0.20
2N1132	0.25	BC122 BC125	0.68	GET113	0.20	OC42	0.80	7409	0.45
2N1302 2N1303	0·18 0·18	BC126	0-65 0-65	GET114	0.15	0C42 0C43	0.40	7411	0.20 0.23
2N1304	0.22	BC140 BC147	0.15	GET115 GET116	0-45	0C44 0C44M	0·17 0·17	7412	0.42
2N1305	0.22	BC148	0.18	OFT190	0.25	OC44M OC45 OC45M	0.12	7413	0.80
2N1306 2N1307	0-25 0-25	BC149	0·15 0·15	GET872	0-80	OC45M	0.18	7416	0.30 0.30
2N1308	0.25	BC157 BC158	0.12	GET872 GET875 GET880	0-25 0-87	OC46 OC57	0·27 0·60	7420	0-20
2N2147	0.75	BC160	0.68	GET881	0.25	OC58	0.60	7422	0-48
2N2148 2N2160	0-60	BC169	0.20	I GET885	0.25	OC59 OC66 OC70	0-65	7423 7425	0·48 0·48
2N2218	0.20	BCY31 BCY32	0-35 0-55	GEX44	0.08	+ OC70	0.50 0.12	7427	0.42
2N2219 2N2369A	0-20	BCY32	0.25	GEX44 GEX45/	0-10	0C71 0C72 0C73	0-12	7428 7430	0.50 0.20
2N2444	1.99		0.80	GEX941 GJ3M	0·15 0·25	0072	0-20 0-80	7432	0.42
2N2613	0-28	BCY34 BCY38	0-40	GJ4M	0.88	0C74	0.80	7433	0.70
2N2646 2N2904	0.45	BCY 39	1.00 0.50	GJ5M	0.25	0C74 0C75	0-25	7437 7438	0-65 0-65
2N2904A	0.25	BCY40 BCY42	0.25	GJ7M HG1005	0-87 0-50	+ OC76	0-25 0-40	7440	0.20
2N2906	0.20	BCY70	0.15	H8100A	0.20	0C77 0C78	0.20	7441 VN	0.75
2N2907 2N2924	0-23 0-23	BCY70 BCY71 BCZ10 BCZ11	0.20 0.35	MAT100 MAT101	0.25	OC79	0.22	7442 7450	0.75
2N2925	0.16	BCZ11	0.50	MAT120	0-30 0-25	OC81 OC811)	0.20 0.20	7451	0·20 0·20
2N2926	0.10	BD121	0.65	MAT121	0.80	OC81M	0.20	7453	0.20
2N3054 2N3055	0-50 0-75	BD123 BD124	0-80 0-75	MJE520 MJE2955	0.87	OC81DM	0.18	7454 7460	0.20 0.20
2N3702	0-10	BDY11	1.62	MJE3055		OC81Z OC82	0.40 0.25	7470	0.30
2N3705	0-10	BF115 BF117	0.25	NKT128 NKT129	0.35	00821)	0.20	7472	0.80
2N3706 2N3707	0-28 0-12	BF117 BF167	0.50	NKT129	0.80	OC83	0.25	7473 7474	0-40 0-40
2N3709	0.10	BF173	0.25	NKT211 NKT213 NKT214	0-25 0-25	0C84 0C114	0.25 0.38	7475	0.58
2N3710 2N3711	0·10 0·10	BF181	0.85	NKT214	0.15	0C122 0C123	0.60	7476	0-45
2N3819	0.10	BF184 BF185	0.20 0.20	NKT216 NKT217	0-37 0-35	OC123	0.85	7480 7482	0-80 0-87
2N5027	0-58	BF194	0.17	NKT217 NKT218	1.13	OC139 OC140	0.25	7483	1.00
2N5088 28301	0.88	BF195 BF196	0.15	NKT219 NKT222 NKT224	0.38	OC141	0.60	7484	0-90
28304	0.76	BF197	0-15 0-15	NKT222	0.20	OC169 OC170	0.20	7486 7490	0-45 0-75
28501	0.87	RESEL	0-28	NKT251	0.24	0.00171	0.80	7491AN	1.00
28703 AA129	0-62 0-20	BFS98 BFX12	0.28	NKT271 NKT272	0.25	OC200 OC201 OC202	0-40	7492	0.76
AAZ12	0.80	BFX13	0.25	NKT273	0.25 0.15	0C201	0.70	7493 7494	0-75 0-80
AAZ13	0.12	BFX29	0.25	NKT274 NKT275	0.20	: OC203	0.40	7495	0.80
AC107 AC126	0-87 0-20	BFX30 BFX35	0.25 0.98	NKT275 NKT277	0.25	OC204 OC205	0.40	7496 7497	1.00 6-25
AC127	0.25	BFX35 BFX63	0.60	NKT278 NKT301	0.25	OC206	0.75	74100	2.50
AC128 AC187	0.20 0.25	BFX84	0.25		0.40	OC207 OC460	0.80	74107	0.50
AC188	0.25	BFX85 BFX86	0.30 0.25	NKT304	0.75 0.75	OC460 OC470	0.80	74110	0.80 1.45
ACY17	0-80	BFX87	0.25	NKT403 NKT404	0.55	OCP71	0.97	74111 74118	1.00
ACY17 ACY18 ACY19	0-25 0-25	BFX88 BFY10	0.20 1.00	NKT678	0.80 0.25	ORP12	0.60	74119	1.90
ACV20	0.20	BFY11	1.25	NKT713 NKT773	0.25	ORP60 ORP61	0-40 0-42	74121 74122	0.60 1.35
ACY21 ACY22	0.20 0.10	BFY17 BYF18	0.25 0.25	NKT777 078B	0.38	S19T	0-80	74122 74123	2.70
ACY27	0.25	BFY19	0.25	0.78B	0-28 0-20	SAC40	0.25	74141 74145	1.00
ACY28 ACY39	0.17	BFY24	0.45	OA6	0.12	SFT308 ST722	0.38	74150	1.50 3.35
ACY40	0-50	BFY44 BFY50	1-00 0-22	OA47	0·10 0·10	ST7231	0-68	74151	1.10
ACY41	0-15	BFY51	0.20	OA70 OA71	0.10	8X68 8X631	0.20	74154 74155	2.00
ACY44	0.25	BFY52	0.22	OA73	0.10	8X635	0.40	74156	1.55
AD140 AD149	0-50	BFY53 BFY64	0·17 0·42	OA74 OA79	0·10 0·10	SX 640	0.50	74157	1.80
AD161	0-87	BFY64 BFY90	0.65	0.481	0.08	8X641 8X642	0-55	74170 74174	4·10 2·00
AD162 AF106	0-87 0-80	B8X27	0.50	OA85	0.12	8X644	0.75	74175	1.35
AF114	0.25	B8X60 B8X76	0-98 0-15	OA86 OA90	0-15	8X645 V15/30P	0.75 0.50	74176	1.60
AF115	0.25	BSY26	0.18	OA91	0.07	V30/201P	0.75	74190 74191	1.95 1.95
AF116 AF117	0.25 0.25	BSY27 BSY51	0·17 0·50	OA95 OA200	0.07	V60/201	0.50	74192	2-00
AF118	0.62	BSY95A	0.12	OA202	0.07	V60/201P	0.75 0.10	74193	2.00
AF119	0.20	B8Y95	0-12	OA210	0.25	X A 102	0.18	74194 74195	2.50 1.85
AF124 AF125	0.25	BT102/50	0R 0-75	OA211 OAZ200	0.30	X A151	0.15	74196	1.50
AF126	0.17	BTY42	0.92	OAZ201	0.55	X A 152		74197	1.50
AF127	0.17	BTY79/1	00R	OAZ202	0.42		·0·25	74198 74199	4-60 4-60
AF139 AF178	0-80	BT Y79/40	0.75	OAZ203 OAZ204	0.42	X A 162 X B 101	0.49		
AF179	0.65		1.25	OAZ205	0.42	XB101 XB102	0-10	Plug in soc	
AF180 AF181		BY 100	0.15	OAZ206 OAZ207	0.42	X B103	0.25	low profi	
AF186	0.42	BY126 BY127	0·15 0·17	OAZ207 OAZ208	0.47	X B113	0-12	14 pin DH	0.15
AFY19	1·18 0·60	BY182	0.85	OAZ209		XB121	0.48	lii pin DH	i i
AFZ11	0.40	BY213	0.25	OAZ210	0-82	ZR24	0-68		0-17
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load allows a good low frequency response without using a large coupling capacitor. However, it could be argued that we have moved it back to the supply

to obtain the centre tap.

The a.c. feedback sets the gain to 26 times or 28dB. If the BC184 transistor is mounted on the same heat sink as the power transistors, it will tend to compensate for variations in quiescent current if they become warmer. The 330 ohm resistors limit the maximum drive if the load is accidentally shorted. When used as shown in the diagram the BC184 can be considered simply as a low value impedance.

Since in these circuits the power stages appear inside the feedback loop, extra care must be taken with frequency compensation to achieve closed loop stability. Measurements on a prototype show that distortion should be better than 0.2 per cent at

30 watts at 1kHz.

CONSTRUCTION

It is essential that the 10μ F capacitor is a low leakage tantalum type because if a leakage current flows through this component there will be a d.c. offset at the output which could cause a quiescent current to flow in the load.

The output offset voltage could be measured before the load is connected, or if a small d.c. current flows through the load as it is connected, this would be indicated by an unbalance in the current drawn from each supply. The offset should be small, less than 10mV. Each power transistor should be mounted on a heat sink of thermal resistance 2.8°C/watt or better. Each driver transistor should also have a small heat sink.

CONCLUSIONS

The final circuit given for a 30 watt power amplifier should be regarded as experimental because it has not been fully toleranced as regards transistor and integrated circuit variations. Some adjustment might be necessary for the 10pF capacitor in order to obtain the best possible square wave at 10kHz. For instrumentation applications the circuit can easily be direct coupled so that its response extends down to d.c.

Part 6 will look at basic memory circuits



SEMICONDUCTOR DIODE LASERS

By R. W. Campbell and F. M. Mims Published by Foulsham-Sams 192 pages, 9in \times 5½in. Price £1.90

PTOELECTRONICS is a field which is attracting a great deal of attention at the present time but semiconductor diode lasers are still very much in the development stage. Though the large manufacturers are producing them it appears that the price is still a prohibitive factor in their widespread use. One of the authors points out that "laser specifications of recent years should generally be reasonably accurate" showing that even the manufacturers are still not totally confident in the devices.

This new book originating in America (but with the usual Foulsham-Sams introduction for English readers) is thus directed more towards the researcher

and experimenter than the constructor.

The opening chapters give a description of the development of the laser diode with a description of light generation processes in both lasers and ordinary light emitting diodes (l.e.d.s). For those who have not met semiconductor lasers before, they differ from l.e.d.s in that they emit *coherent* light in an intense beam. The structure of lasers is different from l.e.d.s and they are usually used in the pulsed mode. mode.

Probably the main interest in the book will be in the practical laser diode driving circuits. Perhaps the most interesting design is of a laser transmitter and receiver using pulse frequency modulation which can be used for voice communication at up to 3½ miles range. Of course, sophisticated optics are needed to achieve such a range and this side of the design is not neglected.

For the interested amateur or the researcher this book provides an excellent introduction to semiconductor lasers and the techniques needed to use

them.

S.R.L.

SEMICONDUCTOR DATA HANDBOOK Published by the General Electric Company, U.S.A. 1,538 pages, $8\frac{1}{2}$ in× $10\frac{1}{2}$ in. Price £2·30.

This massive 1,538 page handbook embraces the full range of semiconductor devices manufactured by the General Electric Company. It contains data sheets, circuits application tips and hints, equivalent and device selector guides and indexes to application notes and technical publications.

Devices covered include silicon and germanium transistors from small signal to power types; signal and tunnel diodes and power rectifiers; unijunction switches and triggers; s.c.r.s and triacs; optoelectronic devices; voltage regulators, differential and Darlington amplifiers; selenium components; transistor and diode chips; military and high reliability types and associated mounting hardware.

The Semiconductor Data Handbook can be obtained from Jermyn Distribution, Vestry Estate,

Sevenoaks, Kent.

ELECTRONIC METRONOME

In BP 1 280 117 Andre Paquet of France details a simple but probably reliable electronic metronome for producing synchronised sound

and light signals.

In his circuit (see Fig. 1) the inventor uses a bi-stable multivibrator which can be switched from one of its states to the other by a time constant circuit R1, VR1, C1. In fairly conventional manner the capacitor C1 is charged via R1, VR1 to a voltage V (defined by R3 and R4) at which TR1 and TR2 transistors conduct. In this state the capacitor C1 discharges and a negative pulse is passed via C2 to the multivibrator. There follows a change of state of the multivibrator which energises the coil L1 and the lamp LP1 and the coil L2 and the lamp LP2 alternately in a "flip-flop" manner.

In one design the coils attract cores which strike a metal plate to produce a sound output. In another design, a sound output is produced by a loudspeaker connected in series with a thyristor controlled by an RC circuit.

Regulation of the range of frequency to be covered is by adjustment of the frequency control VR1. The other adjustment is of the absolute value of the frequency at predetermined point on the potentiometer-usually this is the minimum frequency required.

The main advantage claimed is that as the value of a potential U on the base of TR1 is defined with R4

respect to V by $\frac{1}{R3 + R4}$ period P between switching operations will depend only on the slope of the exponential of the charging

curve of the capacitor C1, i.e. on $(R1 + VR1) \times C1$, which is adjustable, of course, by means of the potentiometer.

Thus (discounting leakage currents) the frequency of switching of the multivibrator is independent of the voltage of the power source and thus the metronome will not speed up or slow down according to battery condition.

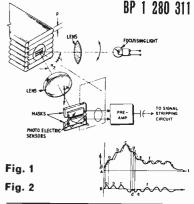
COUNTING STACKED ARTICLES

HEN flat articles such as envelopes, paper sheets or packages are stacked, counting them can be extremely difficult. main problem is that very low contrast gradients exist between adjacent stacked articles and so photoelectric sensing devices produce such poor signal-to-noise ratios that the final count is hopelessly unreliable.

One way round the problem is simply to weigh the stack and another proposal has been to enhance the signal from the photoelectric sensors by some means, such as a high pass filter. But so far (at least according to Spartanics Limited, of Illinois, USA, in BP 1 280 311) the overall results have been poor.

In this new British patent Spartanics suggest counting the discontinuities between adjacent stacked articles by an array of sensors having an effective thickness less than that of the stacked articles.

The sensors are photoelectric and (see Fig. 1) an area of the stack of articles is illuminated by means of a lens focusing light from a d.c. source. The axis of illumination (x1) is adjustable so as to give the maximum contrast possible at the article edges. A pair of cross coupled photoelectric



sensors are fronted by adjustable guillotine masks and an objective lens so that they scan a pair of areas lying both within the width (p) of a single stacked article. The axis of scan of these sensors (x2) is also adjusted to give the maximum possible contrast.

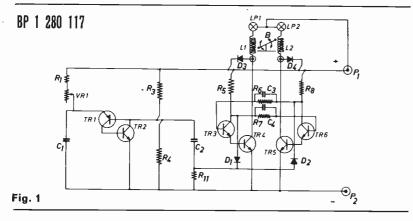
The sensor output is applied to a high gain amplifier which produces a square wave output in response to small deviations brightness from an average value. In this way the gaps between articles are detected and counted when the stack is moved past the sensors.

If a number of these sensor arrays are used, circuitry is provided for automatic subtraction from the count in respect of each array above one; using a larger number of sensor arrays will improve the signal characteristics when the available contrast is very low.

Circuit Fig. 2 shows the kind of wave form that can be expected when the stack of articles is moved past the sensor array. The letters a to f are used to denote the separate articles in Fig. 1.

Each of two sensors connected in parallel opposition produce a wave form as shown in the top part of Fig. 2 (at A) and their composite output wave train is as shown in the lower part of Fig. 2 (at B). The result is thus good ambient brightness rejection and resolution.

The patent contains many details of more sophisticated systems based on this general approach and among other suggestions for improving sensitivity is the proposal that a sensor array be assisted by a diffraction grating and a drum cam which is rotated to move the sensor and lens carriers until the vertical bars observed are at a minimum.



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16/450V	15p	1000/50V	47p	32+32/450V	331
32/450V	20p	8+8/450V	18p	350 + 50/325V	50
25/25V	10p	8+16/450V	20p	32+32+32/350V	43
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2N1483 90p 2N3826 23p 40602 46p BC145 2N1507 24p 2N3854 16p 40603 58p BC147 2N1613 20p 2N3854 16p 40603 58p BC148	21p BDY20 92p BSX20 14p 11p BDY38 65p BSX21 20p	P.E. SCORPIO IGNITION SYSTEM			
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200 200	130	THYRISTORS			
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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded

payment according to its merits.

Fig. 1. Circuit diagram of the sound/light modulator. The value of R2 was found to vary between 15 to 27 kilohms according to the load

If a microphone is to be used it should be of the carbon type and connected in the circuit as shown (dotted) in Fig. 1.

If the circuit is to be built in a cabinet or case the lamp should be positioned approximately ½in away from the l.d.r. (ORP12).

For a load greater than 500W the handling current of the thyristor should be increased. The potentiometer VR2 controls the brilliance of lamp LP2.

This circuit is open to a great deal of experiment, for instance three circuits could be built with the potentiometer in each adjusted to different stages to make a three channel unit.

The input is completely isolated from the mains.

C. Walker,

London, S.W.9

SOUND/LIGHT MODULATOR

READERS may be interested in my version of a sound/light modulator shown in Fig. 1. It is entirely adjustable and works out to be very cheap compared with other modulators which incorporate frequency band splitters and sync pulse generators.

Sensitivity is controlled by VR1, and resistor R1 is to protect the transistor in the instance of the bulb filament shorting. The value of R1 was 1000 rated at ½ watt which can be lowered depending on the bulb used. A 6V 0.06A or 0.1A bulb can be used quite satisfactorily.

TOUCH SWITCH

THE circuit in Fig. 1 detects voltage changes caused by the proximity of the hand on a sensitive plate or contact, causing a relay to operate. The characteristics of the circuit may be tailored to a particular application by choice of component values.

Typical component values are shown in Fig. 1. The transistors and diodes are general purpose silicon types. The relay coil resistance should be about 700 ohms to 1.5 kilohms, and the supply should be easily capable of operating the relay but not exceeding 25V.

Resistor R1 may be decreased to about 2.7 megohms if the circuit is required to operate only when contact is made to the input by one's fingers. Conversely, as a proximity detector the value of the resistance may be increased.

If the battery drain is an important factor, the resistor R2 may be increased so that the quiescent current is only a few microamps. Sensitivity may be increased by reducing the value of R2. If the sensitivity is increased too much the relay will remain permanently operated.

If the circuit is required to remain operated for some time after triggering, the value of C1 may be increased. The delay before the relay releases is about one second per microfarad. As the capacitor is charged up through R2, it may be necessary to reduce the value of R2 to give speedy operation.

reduce the value of R2 to give speedy operation.

The circuit may be used in a wide variety of applications such as burglar alarms, doorbells, practical jokes, and is particularly useful for switches which have to be found in the dark.

P. K. Webb, Malvern, Worcs.

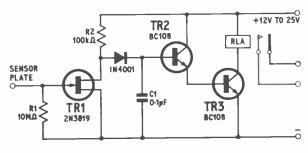


Fig. 1. Circuit diagram of a simple proximity switch

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

CATALOGUES

It is at this time of the year that we take stock of all of our component catalogues and usually receive all the new editions. Judging by the amount of catalogues we have already received and those acquired during the past year it seems a good time to mention just some of the many excellent catalogues in our files.

It seems that as more and more components are becoming available generally, particularly the more specialised types, as electronic techniques forge ahead so we are receiving a greater number of catalogues and firms are tending to specialise in particular fields.

Typical of this trend is LST Components who, through the component explosion, have found it increasingly difficult to maintain their excellent personal service to both the home constructor and the trade. Not wanting to lower their high standards they recently formed a new company called Arrow Electronics Ltd., to deal exclusively with the home consumer market. The parent company is now dealing with the trade only.

The new company have recently issued an excellent catalogue containing items from i.c.'s to switches. Copies of the catalogue can be obtained from Arrow Electronics Ltd., 7 Coptfold Road, Brentwood, Essex.

Another firm who tends to specialise, in this case in integrated circuits, is **Bywood Electronics.** Their catalogue lists such items as a Digital Clock Chip, LSI Calculator i.c.'s and several LED devices (including liquid crystal types).

The Bywood catalogue is available from Bywood Electronics, 181 Ebberns Road, Hemel Hempstead,

Hertfordshire.

From the other side of the coin GSPK (Sales) Ltd., who are well known trade distributors, have recognised the vast demands for components from the consumer side and have set up a special retail counter at their office. Also, they issue a very good mail order catalogue and are offering a great many

of their components which are not normally available to the constructor, unless ordered in large quantities, on a one-off basis.

Copies are available from GSPK (Sales) Ltd., Hookstone Park,

Harrogate, Yorkshire.

A catalogue we strongly recommend to our readers is the Audio Pack Trade Reference Catalogue from Tape Recorder Spares Ltd. This catalogue costs 35p, including postage, and covers over 600 items marketed under the name of "Audio Pack".

The catalogue seems to cover practically every conceivable arrangement for connecting up audio equipment. A special section is devoted to Garrard spares.

This catalogue is certainly an excellent audio spares reference source and should be very near the top of any "Catalogues Wanted" list. Copies are available from Tape Recorder Spares Ltd., 206-210 Ilderton Road, London SE15 1NS.

Finally, as proof of the component growth Home Radio Components have had to completely change the format of their cata-

logue.

The new 240-page catalogue contains over 8,000 items, 1,500 illustrations and still maintains the usual high standards of previous editions. The cost of the catalogue is 75p, including postage, but contains 10 redeemable vouchers worth 5p each when used as directed.

Included with the catalogue is a price supplement which will be updated from time to time and each page will have the date stamped on it. At the bottom of the price supplement is a note to the effect that when the supplement is six months old 10 per cent should be added to any item purchased and a new supplement be requested". Upon investigation it was pointed out that this was to avoid any unnecessary delay in dispatching of orders. Any difference between the remittance and the current price of goods ordered will be returned as a credit note with the option of a cash refund.

The Home Radio catalogue is probably one of the most useful reference sources for components on the market and copies can be obtained from Home Radio (Components) Ltd., 240 London Road, Mitcham, Surrey CR4 3HD.

SYNTHESISER MODULES

Commencing in this issue is the first part of the P.E. Synthesiser which we are sure will generate tremendous interest amongst our readers. This synthesiser will be described in great detail over the next few months and each circuit function will be described and complete constructional details given.

For those readers who do not wish to understand or construct



Two of the Dewtron synthesiser modules from D.E.W. Ltd.

each individual circuit as the series progresses but prefer to connect up "black boxes" (modules) then the Dewtron Project X Synthesiser modules from D.E.W. Ltd., may be worth looking into.

The Project X modules are completely sealed units which have a two year guarantee against failure and their range includes a voltage controlled oscillator, sample, hold and envelope shaper unit and a ring modulator module. The Project X Synthesiser is in NO way connected with the P.E. Synthesiser.

A list of modules and other musical effects units with prices are available from D.E.W. Ltd., 254 Ringwood Road, Ferndown, Dorset.

SLIDER CONTROLS

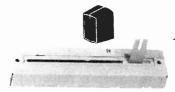
Whilst on the subject of effects units we often get requests for the slider type of controls which are used extensively in effects units. To, date, these type of controls have been difficult for the home constructor to obtain and a compromise has had to be made by using standard rotary potentiometers.

A range of slider potentiometers is now available direct from DJ Electronics (Hackney) Ltd. or from most component retailers. The sliders, complete with knob and fixing screws, are available as single or double gang types in both logarithmic and linear configurations.

A range of mounting plates are available separately and enable the constructor to make up numerous configurations. The plates are offered as single-way, double or triple-way.

The cost of the sliders are expected to be 61p for single gang types; and 81p for double gang. The mounting plates will cost 25p for single-way, 36p for double-way and 45p for three-way.

Addresses of nearest stockists can be obtained from DJ Electronics (Hackney) Ltd., 122 Balls Pond Road, London, NI 4AE.



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ROAMER SEVEN Mk. IV

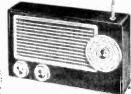


parts). Earpiece with plug and switched socket for private listening 30p extra. TOTAL BUILDING COSTS **£5.98** P. P. & INS. 45p (OVERSEAS P. & P. £1)



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WAVEBANDS:
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TRAW LER
BAND PLUS AN EXTRA MW BAND FOR EASIER
TUNING OF LUXEMBOURG, ETC. Sensitive ferrite
rod aerial and telescopic aerial for short waves. 3in
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case with red grille, dial and black knobs with
polished metal inserts. Size 9in × 5 in × 2 in approx.
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POCKET FIVE



3 TUNABLE WAVE-BANDS: MW, LW, TRAWLER BAND WITH EXTENDED MW BAND FOR EASIER TUNING OF LUXEM-BOURG, ETC. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil speaker. Attractive black and gold case. Size 5jin X 1jin X 3jin. Easy build plans and parts price list 10p (FREE with parts).

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8 TRANSISTORS AND 3 DIODES



167

AND 3 DIODES

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WAVEBANDS:
MW. LW.
SWI, SW2,
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TRAW LE SENSITIVE ferrite rod aerial for MW and LW.
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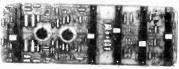
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DESIGNS PUBLISHED IN P.E.

AURORA (Apr./Aug. 71) Multichannel Sound Controlled Light S/c/s (excl. SCRs), Rs, Cs, Cores, Pots, 8 ch., £17-75; 4 ch., £10-15. Slider Pots and Knobs alternative extra, 8 ch., £17-0; 4 ch., £2-20. Power Supply (supplies 8 chans.), unstabilised, £2-85; stab., £3-65. PCB (4½in × 11in) for Pre-amp and 4 Chans. incl. all pots, £2-35. PCB (4½in × 6½in) for PSU, Sync Gen, 8 cores, 8 SCRs, £1-35.

A.F. SIGNAL GENERATOR (Nov. 72)
S/c's, Rs, Cs, Pots, Sw's £2 25. PCB (2½in 4in) also holds Sw's, 90p.

BIOLOGICAL AMPLIFIER—Details on request.

CALLERCORD (Jul./Aug. 72) Automatic Answering Machine S/c/s. Rs. Cs. Pots. Switches. Relays. Transformer, £12-15. PCB (4in × 7½in) holds circuit, relays. edgeconnectors, £1-50. Parrot Tape Recorder, £6-95. Pips Gen with PCB, £1-50.

DOOR BELL YODELLER (Apr. 71)—S/c's, Rs, Cs, Pots, £4:20. Transformer, £1:30. Loudspeaker, £1:30. PCB (3in × 3\frac{1}{2}in), 90p.

LECTRONIC PIANO (Sept. 72 Jan. 73)
Pre-Amp—Rs, Cs. Pots, £1:90. PCB as published, £1:20. Power Supply—
Rs, Cs. £1:5: PCB as published, 95p. Pitch 1:12—Rs, Cs. £2:10 each set. Pitch
13—Rs, Cs. £1:50, Pitch PCB as published £1:85 each. Discounts for Qty.

GEMINI STEREO AMP (Nov. 70/Mar. 71) Stereo Sets and PCBs
Pre-Amp—5/c's, Cs, Pots, Maks-Sw's—with ½w 2%, M.O. Rt, £13-45—with
½W 5%, C.F. Rs, £11 20.—with ½W 5%, C.F. Rs, £10.75.—with 51/der Pots and
Knobs extra, £1-65. PCB (3½in × 10½in) for kits with ½W M.O. or ½W C.F.
Rs. Holds pots and Maka-Sw's, £2.10. Main Amp—Rs, Cs, Pots, £4.30.
PCB (3½in × 5in), £1-40. PSU—Rs, Cs, Pot, £3.70. PCB (2in × 4in), 75p.

GEMINI STEREO TUNER (Apr./Jun. 72) Rs, Cs, Pot, £3-20. PCB as published, £1-80.

LOGICAL RADIO CONTROL (Dec. 71/Jan. 72)—Sets incl. Rs, Cs, S/c's and Pots (where requ.) but excl. l.C's. Coder I and Clock Pulse Gen., £2-95. Coder 2A, £2-80. Coder 2B, £3. Decoder, 55p. PCBs as pub., 75p each.

MODEL SERVO CONTROL (Feb./Mar. 72)—Sets incl. Rs. Cs. Sic's and Pots (where requ.) but excl. l.C's. Servo Amps: "A", £1-40; "B", £2-55; "C", £1-30. Fail-Safe, 65p. PCBs as published: "A" and "B", 60p each; "C" and Fail-Safe, 50p each;

MICROPHONE MIXER (Apr. 69)—S/c's, Rs, Cs, Pots, £2:90. Slider Pots and Knobs extra, £1:15. PCB (3½in × 4½in)—holds pots, £1:20.

and Knoos extra, E(13). PCB (3210 × 4210)—nolos pots, E(140.)
PHOTOPRINT PROCESS CONTROL (Jan./Feb. 72)
Finds exposure, controls timing, stabilises mains voltage.
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also holds pots, relay, Keyswitch, £1:20.

SOUND SYNTHESISER-Details on request.

TAPE NOISE LIMITER (Feb. 72)—Mono Circuit S/c's, Rs, Cs, Pot, PCB ($1 \sin x \sin x \cos x$) Regulated Power Supply (will feed 2 units) and PCB ($1 \sin x \sin x \cos x$) Regulated Power Supply (will feed 2 units) and PCB ($1 \sin x \cos x \cos x$)

VLTRASONIC TRANSMITTER-RECEIVER (May 72)
Rs, Cs, Pot, S/c's, T/ducers, Relay, £9·95. Dual PCB (2in × Sɨjin), 75p.

VERSATILE LIGHT EFFECTS UNIT (Jun. 72)—Single Channel Sound Controlled Light—also has built-in variable strobe generator. S/c's (excl. SCR), Rs, Cs, Pots, T/formers, Keyswitch, £8·85. PCB (Sɨjin × Sɨjin) also holds Pots, Sw. T/former (T/T7), £1·50. Slider Pots and Knobs (excl. 2SR Lin.—Rotary only), £1·10 extra.

SOME OTHER DESIGNS AVAILABLE

REVERBERATION UNIT (Practical Wireless Nov.-Dec. 72)
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BWATT AMPLIFIER (Practical Wireless Nov. 72)

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Pre-amp—S/c's, Rs, Cs; Pots, Maka-Sw., Mono, £2:90; Stereo, £5:20. Slider
Pots and Knobs extra, Mono, £1:26; Stereo, £1:52. PCB (3½n × 7½n)
(Stereo)—also holds all pots and Maka-Sw., £1:50.

I.C. 2-TW STEREO AMPLIFIER (Radio Constructor July 71)
Rs, Cs, Pots, I.C's complete with heatsinks, £7-50. PCB (4½in × 5in)—
(Stereo) also holds Pots, £1-20. Power Supply, £2-85. Slider Pots and Knobs extra, £1-35.

AURORA AUXILIARY CONTROL UNIT (2 variable frequency strobe generators and 4 variable amplitude frequency generators). Rs. Cs. Pots. S/c's £3·25. Slider Pots and Knobs extra, £2·34. PCB (3½in × S½in) holds all generators plus pots, £1·35.

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MOTOROLA MAC 11/6 PLASTIC TRIAC 400 PIV. 10 AMP Now available EX STOCK, Supplied with full data and applications sheet. Price £1-05. P. & P. 7p. Suitable DIAC (RCA 40583) 309 each.

STROBE! STROBE! STROBE!

Build a Strobe Unit, using the latest type Xenon white light flash tube. Solid state timing and triggering circuit. 230/250V a.c. operation. EXPERIMENTERS' ECONOMY KIT

Triggering circuit. 130/130V a.c. operation. EXPERIMENTERS: ECONOMY KIT Speed adjustable I to 30 flash per sec. All electronic components including Veroboard S.C.R. Unijunction Xenon Tube and instructions 66:30, plus 25p P. & P.

NEW INDUSTRIAL KIT Ideally suitable for schools, laboratories, etc. Roller tin printed circuit. New trigger coil, plastic thyristor. Speed adjustable I-80 f.p.s. approx. 1 output of Hy-Lyght.

Price £10:50. P. & P. 50p.

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Designed and produced for use in large rooms, halls and the photographic field and utilises a silica tube, printed circuit, also a special trigger coil. Speed adjustable 0-20 f.p.s. Light output approx. greater than many (so called 4 Joule) strobes. £12:00. P. & P. 50p. SPECIALLY DESIGNED.

THE *SUPER* HY-LYGHT KIT

THE 'SUPER' HY-LYGHT KIT

Approx. four times the light output of our well proven Hy-Lyght strobe. Incorporating:

proven Hy-Lyght strobe. Incorporating:

Heavy duty power supply.

Variable speed from 1-13 flash per sec.

Reactor control circuit producing an intense white light.

Never before a Strobe Kit with so HIGH an output at so LOW a price. ONLY £20 plus 75p.P. & P.

ATTRACTIVE, ROBUST, FULLY VENTILATED METAL CASE specially designed for the Super Hy-Lyght Kit including reflector £7:00 P. & P. 45p.

For Hy-Lyght Kit including reflector. £4:00.

7-inch POLISHED REFLECTOR

Ideally suited for above Strobe kits. Price 53p. P. & P. 13p or post paid with kits.

RAINBOW STROBE FOUR LIGHT CONTROL MODULE

In response to numerous requests, we now offer a mains operated fully isolated short-circuit-proof ready-built module, with variable flash rate, It will operate four of our Hy-Lyght or Super Hy-Lyght Strobes in either 1, 2, 3, 4 sequence; 2+2; or all together. Fantastic effects with or without colour filters. Modules can be connected together to operate 8 or 12 Strobes. Will work on long runs of up to 50 yards, so that your Strobes can be spaced out for maximum effect. Size of module is 3 % 8 1 Jin. easily fitted into your own equipment, or into a separate case. Thoroughly tesseed and reliable. Complete with full connection instruccions. Price: £18-30 plus 25p. P. & P. Send S.A.E. for details.

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Complete with oil-filled colour wheel. 100 watt lamp. 200/ 240V AC. Features extremely efficient op-tical system. £18-50+ 35p. P. & P. 6 INCH COLOUR WHEEL.



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BIG BLACK LIGHT

BIG BLACK LIGHT
400 Watt. Mercury vapour
ultra violet lamp. Outer bulb
designed to absorb visible
light and transmit u.v. rays.
Extremely compact and
powerful source of u.v.
Innumerable industrial applications also ideal for stage,
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is essential with these bulbs.
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BLACK FLUORESCENT U.V. TUBES
4ft. 40 watt. Price £5:80 incl. P. & P.
use in standard bi-pin fluorescent fitti



4ft. 40 watt. Price £5-80 incl. P. & P. (For use in standard bi-pin fluorescent fittings). MINI 9 in. 6 watt black light U.V. tube.

Superior Quality Precision Made NEW POWER RHEOSTATS

100 WATT. I ohm, 10A: 5 ohm, 47A: 10 ohm, 3A: 25 ohm, 2A: 50 ohm, 10A: 100 ohn, 2A: 50 ohm, 10A: 50 ohm, 0.7A: 500 ohm, 0.45A: 1 kΩ, 280 mk; 15 kΩ, 230mk; 2.5 kΩ, 2A: 35kΩ, 5 kΩ, 140mA. Diameter 3½in Shq. 140mA. Diameter 3½in

50 WATT. 1/5/10/25/50/100/250/500/[11-5/2-5/54].
All at £1-15 each. P. & P. 7-jp.
25 WATT. 10/25/50/100/250/30/500/[1/-5/2-5/3-5/54].
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Ijin. dia brass bush. Ideal for above Rheostats, I āp ea.

RELAYS SIEMENS, PLESSEY, Et

MINIATURE RELAYS								
Col.(1) Coil ohms	1	2	3	4				
Col. (2) Working d.c. volts	52 410 600	3-6 10-18 12-24	2 c/o 4 c/o 4 c/o	63p° 73p° 78p°				
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HD = Heavy duty *Incl. Base	1,250 2,500 2,400 9,000	24-36 36-45 30-48 40-70	4 c/o 6M 4 c/o 2 c/o	63p* 50p* 50p*				
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12 VOLT D.C. RELAY 140 ohm coil

Type 1: Three sets c/o contacts rated at 5 amps. 78p. incl. P. & P. (Similar to illustration below.) Type 2: One set of c/o contacts. 60p incl. P. & P. Type 3: 4-8 volt, 3 c/o HD, 67 ohm coil. 78p. 78p.

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Three sets c/o contacts rated at 5 amps.
PRICE: 50p. P. & P. 10p. (100 lots £40 including P. & P.)

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Manufactured by Clare-Elliott Ltd. Type F. 2 c/o permanent latching in either direction. Coil II 50 ohm, 15-30 Volt D.C. Size §* high, §* wide, §* thick. Complete with 3' I leads. New 73p, incl. P. & P.

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MT60/2 0-12-13-20-24-30V, IA— £1.95 plus 30p p. & p. MT60/1 0-5-20-30-40-60V, IA— £2.10 plus 30p p. & p. MT60/2 0-5-20-30-40-60V, 2A— £2.95 plus 34p p. & p. Charger CT/01 | A—£1:05 plus 26p p. & p. CT/02 2A—£1:30 plus 30p p. & p. CT/03 4A—£1:60 plus 30p p. & p. Secondaries—0-5-11-17V.

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Type L. W. D. Price p. & p.
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G812 3in 2 in 1 fin 33p 13p
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G813 6in 4in 2 fin 52p 18p
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6 in 4 in 2½ in 13p 13p
6 in 4 in 2½ in 13p 13p
6 in 4 in 2 in 32p 18p
6 in 4 in 2 in 52p 18p
6 in 4 in 3 in 52p 18p
7 in 5 in 2½ in 6 in 19p
8 in 6 in 3 in 8 lp 26p
10 in 7 in 3 in 92p 26p
7 These sizes fit
5 tandard
5 veroboards



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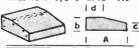
in plain aluminium, ideal for mixers,

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GB21 10 9 3½ 2 3 £1-58 30p.

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	0.1	0.15
Size	matrix	matrix
2∳in × 3∄in	22p	16p
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3∄in × 5in	27 p	29 p
17in × 2∔in	75p	57p
17in × 3∄in	£1	75p
Pins-either siz	e, packet (

1,000µF 1,000µF 2,000µF 2,000µF 2,500µF 2,500µF 3,000µF 5,000µF 5,000µF 25V 27p 50V 42p 2SV 39p 50V 53p 25V 45p 50V 60p 2SV 48p 2SV 60p 50V £1-10 19p 20p 14p 17p 18p 7p 10p 450 V 450 V 350 V 8μF 16μF 25μF 25μF 32μF

450V 450V 25V 50V 450V 25V 50V 25V 50V 25V 50V 27p 10p 32µF 50µF 100µF 100µF 250µF 250µF 8-8μF 8-16μF 16-16μF 16-32μF 32-32μF 50-50μF 450V 450V 450V 450V 450V 450V 350V

MIRE	IAIL	JKE	ELECTROL	7 116	, 5
IμF	63V	6p	47µF	167	7p
2.2µF	63V	6р	47µF	25V	6р
3 4F	63 V	6р	68µF	167	6р
1.7µF	63 V	6р	100µF	107	6р
8µF	40V	7p	220µF	16V	7p
10μF	25V	6p	330µF	16V	Hp
I OµF	64V	7p	470µF	107	Hp
I6μF	40 V	7p	1,000µF	16V	I9p
33μ F	167	6р	1,500µF	16V	23p

CASSETTE OWNERS!

For Philips and similar cassette recorders. PUI2 Power unit for connection to 12V + or – E car electrical systems, giving 7½V, stabilised £3.25 output.

PUIA As above but switched for £5.10
PP75 Mains power supply, output £1.95
7½V d.c.

All units are complete with cable and plug.

Top quality British made, low noise, complete with transparent library cases—C60—40p; C90—55p; C120—70p

BATTERY ELIMINATORS

suitable for transistor radios and similar light PP9 Input 240V a.c. Output 6V d.c. Price £1-50 plus 12p p, & p.

ILLUSTRATED CATALOGUE

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CONTROLS, Log. or Lin.

Single, less switch, 15p Single, D.P. switch, 24p Tandem, Iess switch, 40p 5kΩ, 10kΩ, 25kΩ, 50kΩ, 100kΩ, 250kΩ, 500kΩ, 11MΩ, 2MΩ

RESISTORS

Carbon
All 5%, high-stability, E+2 values. ±W, Ip;
±W, Ip; IW, 4p; 2W, 6p ₩, 1½p; 1W, 4p; Wire-wound 5W, 10p; 10W, 12p

SWITCHES

Toggle switches, standard size. SW20*S.P.S.T. 18p; SW21—D.P.D.T. 23p. Push Button, miniature, SWI-I3p. Wafer switches (rotary)—24p each.
SW4—I pole, 12 way.
SW5—2 pole, 6 way.
SW6—3 pole, 4 way.
SW8—4 pole, 2 way.

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B.A.F. wadding, 18in wide, 1in thick, The ideal lining for speaker enclosures. 30p per yard. p. & p. one yard 12p; each extra yard 4p.

TYGAN top quality loudspeaker covering material. Please send 6p for samples, sizes and prices.

MAGNETIC COUNTERS

Brand new, neat, 48 volt. 5 digit counters. 60p



PLUGS

Car aerial Car aerial
Co-axial
D.I.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 4 pin
D.I.N. 5 pin, 180°
D.I.N. 5 pin, 240°
D.I.N. 6 pin
Jack, 2½mm unscreened
Jack, 2½mm screened
Jack, 3½mm screened
Jack, ½in unscreened
Jack, ½in screened
Jack, ½in screened
Jack, ½in screened
Jack, in screened Jack, stereo, unscreened Jack, stereo, screened Phono, plastic top Phono, plated metal Wander, red or black Banana 4mm, red or black

LINE SOCKETS

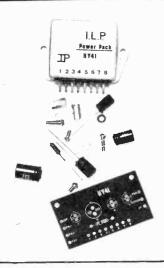
Car aerial Co-axial D.I.N. 2 pin (spea D.I.N. 3 pin D.I.N. 5 pin, 180° D.I.N. 5 pin, 240° pin (speaker) Jack, 3½mm Jack, ½in screened Jack, stereo, screened Phono, plated metal

SOCKETS

P	Car aerial	8p
p	Co-axial, surface	8p
p	Co-axial, flush	9p
p	D.I.N. 2 pin (speaker)	10p
	D.I.N. 3 pin	9p
Р	D.I.N. S pin, 180°	9p
P	D.I.N. 5 pin, 240°	9 _P
	Jack, 2+mm	100
	Jack, 34mm	100
Р	Jack, £in unswitched	15p
P	Jack, Jin switched	17p
P	Jack, stereo, switched	24p
P	Phono, single	5p
þ	Phono, 2 on a strip	
		7p
P	Phono, 3 on a strip	9p
Р	Phono, 4 on a strip	10p
P	Wander, single, red or black	
Р	Wander, twin strip	7p
D	Banana 4mm red. or black	60

CAPA	CITO	RS		0·0027μF	500V	S/M	15p
2-2pF	500V	S/M	7 tp	0 003µF 0 0033µF	500V	Cer. P.5.	5p 6p
3-3pF	500V	S/M	7 P	0.0033µF	500V	Poly.	6p
5pF	500 V	S/M	7 P	0.0033µF	1,0000	MDC	6р
10pF	125V	P.S.	5p	0 0036µF	500V	S/M	15p
10pF	500V	S/M	7 1 p	0 0047µF	125V	P.S.	9p
15pF	125V	P.S.	5p	0.0047µF	500V	Poly.	6p
15pF 18pF	500∨ 500∨	Cer. S/M	4p 7 t p	0 0047µF	500V	S/M	20p
22pF	1257	P.S.	/ 1P 5p	0·0047μF 0·005μF	1,000 V	MDC Mylar	6p
22pF	500V	S/M	710	0.005µF	500 V	Cer.	3 p 5 p
25pF	500V	S/M	7 p 7 p	0.0068µF	125	P.S.	10}p
27 pF	S00 V	Čer,	4p	0.0068µF	500 V	S/M	30p
33pF	125V	P.S.	5p	0.0068µF	500 V	Poly.	6p
33pF	\$00V	S/M	7łp	0.0082µF	125V	P.S.	101p
39pF	500 V	S/M	7 1 P	0.0082µF	500V	S/M	30p
47pF	12SV 500V	P.S.	5p	0.01µF	187	Disc	4p
47pF 50pF	500V	Cer. S/M	-4p	0 01μF	125V	P.S.	10 ¹ b
56pF	500 V	S/M	71p 71p	0·01μF 0·01μF	160 V 250 V	Poly. M.F.	4p 3p
68pF	125V	P.S.	5p	0.01µF	400V	Poly.	3p
68pF	500V	\$/M	7 1 P	0.01 µF	500 V	Cer.	5p
75pF	500V	S/M	7 P	0.0111F	500 V	5/M	30p
82pF	500V	5/M	7 P 7 P	0.01µF	600V	MDC	7p
100pF	125V	P.S.	5p	0.01µF	1,000V	MDC	9p
100pF 100pF	500V 500V	S/M	7 <u>1</u> p	0.015μF	160V	Poly.	3p
120pF	500 V	Cer. S/M	5p	0.015µF	400V	Poly.	3p
150pF	125	P.5.	7 <u>1</u> p 5p	0·02μF 0·022μF	180	Mylar	3p
150pF	500V	S/M	7 i p	0.022µF	250V	Disc M.F.	5p 3p
150pF	500 V	Čer.	5p	0.022µF	400 V	Poly.	3p
180pF	500 V	S/M	7 tp	0.022µF	600V	MDC	7 i p
200pF	500 V	S/M	7 i p	0 022µF	1,000V	MDC MDC	10p
220pF	125V	P.S.	5p	0·033µF	250V	M,F.	4p
220pF	500V	Cer.	5p	0 033µF	400V	Poly.	4p
250pF 270pF	500∨ 500∨	S/M	8p	0·047μF	127	Disc	6р
300pF	500 V	Cer. S/M	5р 8р	0·047μF	160V 250V	Poly.	3p
330pF	125V	P.S.	5p	0·047μF 0·047μF	400V	M.F. Poly.	3p 4p
330pF	500V	5/M	8p	0.047µF	600V	MDC	8p
390pF	500 V	S/M	8p	0.047µF	1.000V	MDC	10p
470pF	125V	P.S.	5p	0 IμF	30V	Disc	6р
470pF	750V	Disc	5p	0 1µF	250V	M.F.	4p
500pF	500 V	5/M	8p	0 IμF	400V	Poly.	5p
560pF 680pF	500V 125V	S/M	8р	0 IμF	600V	MDC	I0p
680pF	500V	P.S. S/M	6р 8р	0-1 / LF 0-15/LF	1.000V 250V	M.F.	14p
820pF	500 V	5/M	8p	0.22µF	160V	Poly.	5p 6p
0.001µF	1007	Mylar	3p	0.22µF	250 V	M.F.	5p
0.001µF	125V	P.Š.	6р	0-22µF	400 V	Foil	10p
0.001µF	400V	Poly.	3p	0·22μF	1,000V	MDC	I5p
0.001µF	500 V	5/M	10p	0·33μF	250V	M.F.	8p
0·001μF 0·001μF	500V 1,000V	Cer. MDC	5 p	0 47μF	250V	M.F.	8p
0.0015µF	400V	Poly.	6р 3р	0·47μF 0·47μF	400V	Foil MDC	15p 25p
0.0015µF	500V	S/M	100	1-0μF	250	M.F.	15p
0.0015µF	500V	Cer.	5 p	ιομι	230 1		13p
0 0018µF	500V	S/M	10p	Note:			
0·002μF	100V	Mylar	3р,	S/M == sil	ver mica lystyren	1% tol	
0·002μF 0·0022μF	500 V 125 V	Сег.	5p	P.S. = po	lystyren	e 2½%.	tol.
0·0022μF	500V	P.S. S/M	6p 10p		i.c. ratin Iullard m		
0.0022µF	1.000V	MDC	6р	Cer. = c		1011.	
	,						

MAIL ORDERS: Some items have a post and packing charge shown against them. Where p. & p. is not shown the charge is 12p for any selection. When both classes of goods are ordered the charge is 12p plus any p. & p. charges shown. Overseas extra.) Telephone 01-092 4412.



THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts

R.M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.

INPUT IMPEDANCE: 30K ohms at 1KHz. VOLTAGE GAIN: 30db at 1KHz

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

FREQUENCY RESPONSE: 5Hz-50KHz + 1db. SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: 0.8 amps maximum

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

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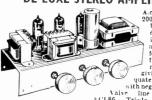


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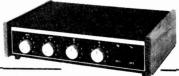
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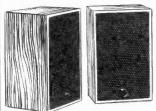


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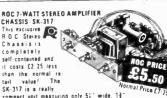
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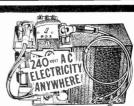
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TAPE HEADS

TAPE HEADS
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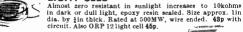
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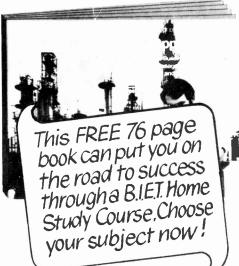
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C.&.G. Elec. Inst.
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