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ELECTRONICS

MARCH 1973

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IN4004	400	- 8
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IN4006	800	12
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ONE AMP	1×1	H
TUBULAR		
B1/05	5 Qu	25p
B1/10	100	25 p
B1/20	200	30p
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ONE AMP	(G.I.)	
TUBULAR		
W005	50	30p
W01	100	35p
W02	200	40p

9	W01	100	35p
0	W02	200	40p
- 3	W06	600	450
0	TWO AM	PS H ×	1 L
ρĺ	× å		
p	B2/05	50	35p
- 0	B2/100	100	40p
0 j	B2/200	200	45p
- 3	B2/600	600	50p
	B2/1000	1000	60p

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E AMP	(TO66		5.3
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VEN AN	IP (TO	48)	
8 7/100	100	60p	5- B
8 7/200	200	65p	1000
8 7/400	400	70p	
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22p 2N5172 25p BZY88

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dise cerami	c	low voltage	
01µF 18v	5p	0-1µF 30v	5 p
022µF 18v	5 p	0 · 22µF 6v	5p
047µF 12v	5p	0-47µF 3v	5p
ceramic pla	te	30 V	
1000pf	10 p	4700pf	10p
200pf	10p	10,000pf	10p

Ceramic - 1.8pf 2.2pf 3.3pf 3.9pf 4.7pf 5.6pf 6.8pf	Plate 8 2pf 10pf 12pf 15pf 18pf 22pf 27pf	63V (C333) 33pf 39pf 47pf 56pf 68pf 82pf 100pf	120pf 150pt 180pf 220pf 270pf 330pf
		100pf	

mylar film 01μF **02**μF 04μF 05μF 3p 3p 3p 1000pf 2p 2000pf 2p 5000pf 2p 5p

polystyrene 160 V-10pf to 10,000pf in multiples of 10, 15, 22, 33, 47 & 68. 3p each

metallised	polyester	25	0V (C28	30)
01 μF 3 p	-068µF	3⅓p	47μF	8p
·015μF 3p	-1μF	4p	68µF	11p
022μF 3 p	-15µF	4p	1μF	13p
-033μF 3p	22µF	5p	1.5µF	20p
-047μF 3p	33µF	61p	2 2 µF	24p
			001/10	204)

 metallised
 polyester

 ·01μF
 4½p
 ·047μF
 6p

 ·015μF
 4½p
 ·068μF
 6p

 ·022μF
 4½p
 ·1μF
 7p

 ·033μF
 5½p
 ·15μF
 8p
 100V (C281) 22μF 10p -33μF 14p -47μF 15p

 ailvered mica 1% (> 50pf) 500V

 2 2pf—820pf
 7p

 1 nf—2 2nf
 9p

 2 -7nF—3 6nF
 16p

 16m
 16m

 2 nf
 16m

 3 nf
 16m

 4 nf
 16m

 4 nf
 16m

 8 600V

mixed dielectric ·01μF 7p ·047μF 7p ·022μF 7p ·068μF 8p ·033μF 7p ·1μF 8p ·22μF ·47μF 1μF ORDERS: Where no p. & p. charge is shown, num of 7p applies, p. & p. on overseas orders

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AC107

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for SL403D 15p

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24p OC171 35p AC1676 15p 8C158 10p 8FV51 21p 271x107 15p AC1677 25p 8C159 12p 8FV51 26p 271x107 15p AC1678 25p 8C159 15p 8Sx21 26p 271x109 12p AC188 25p 8C158 15p 8Sx21 26p 271x109 12p AC188 25p 8C158 15p 8Sx21 26p 271x109 12p AC188 25p 8C158 17p 8V505 41p 271x300 12p AC188 25p 8D131 70p ME510 47p 271x300 22p AC180 40p 8D131 70p ME510 47p 271x300 22p AC190 40p 8D131 70p ME510 37p 271x300 22p AC190 40p 8D131 70p ME510 37p 271x300 22p AC190 40p 8D132 70p MFF109 37p 271x300 22p AC180 40p 8C158 21p MFF109 37p 271x301 22p AC1816 18p 8F167 22p MFF109 40p 271x300 15p AF114 18p 8F167 22p MFF109 45p 271x501 15p AF115 18p 8F167 32p MFF109 45p 271x501 15p AF116 18p 8F168 25p OC28 40p 271x503 47p AF117 18p 8F181 25p OC35 40p 271x503 47p AF119 48p 8F184 25p OC45 15p 271x501 35p AF119 48p 8F184 25p OC45 15p 271x501 35p BC107 10p 8F184 25p OC45 15p 271x501 35p BC107 10p 8F184 15p OC72 17p 28697 18p	AC188 25p 8C158 12p 8FY50 24p 0C171 30p 2N2926 AC176 15p 8C158 10p 8FY51 21p 2TX107 15p 2N3053 AC187 25p 8C159 12p 8RY39 36p 2TX108 12p 2N3054 AC187 25p 8C169 15p 8SX21 25p 2TX108 12p 2N3054 AC188 25p 8C169 15p 8SX21 25p 2TX100 12p 2N3054 AC188 25p 8C268 15p 8SY21 25p 2TX300 12p 2N3054 AC188 25p 8C268 15p 8SY21 25p 2TX300 12p 2N3054 AC188 25p 8C268 17p 8V155/20 21p 2TX300 12p 2N3703 AC188 25p 8C168 70p MP5103 21p 2TX300 20p 2N3703 AC188 25p 8C168 70p MP5103 37p 2TX300 20p 2N3703 AC190 40p 8C132 70p MP5103 37p 2TX300 20p 2N3705 AC190 40p 8C160 21p MP5103 37p 2TX301 20p 2N3706 AC188 25p 8C168 12p MP5103 37p 2TX301 20p 2N3706 AC188 25p 8C168 12p MP5103 37p 2TX301 20p 2N3706 AC188 25p 8C160 21p MP5103 44p 2TX500 15p 2N3706 AC1816 18p 8F167 20p MP5103 44p 2TX501 15p 2N3706 AF114 18p 8F167 20p MP5103 44p 2TX501 15p 2N3706 AF115 18p 8F167 20p MP5103 44p 2TX501 15p 2N3706 AF116 18p 8F167 20p MP5103 44p 2TX501 15p 2N3706 AF116 18p 8F167 20p MP5103 44p 2TX501 15p 2N3706 AF116 18p 8F168 25p 0C28 40p 2TX503 17p 2N3711 AF117 18p 8F181 30p 0C44 15p 2TX501 5p 2N3701 AF116 18p 8F184 25p 0C45 15p 2TX501 25p 2N3903 BC107 10p 8F184 15p 0C42 17p 2N9076 12p 2N3905	AC188 259 BC168 19p BFY50 24p CC171 30p 2N2288 all AC187 25p BC168 10p BFY51 21p ZTX107 15p 2N3053 AC187 25p BC169 15p BSX271 25p ZTX109 15p 2N3053 AC188 25p BC169 15p BSX271 25p ZTX109 15p 2N3055 AC188 25p BC169 15p BSX271 25p ZTX109 15p 2N3055 AC188 25p BC169 15p BSX271 25p ZTX109 15p 2N3055 AC188 25p BC169 15p BSX271 25p ZTX109 15p 2N3052 AC188 25p BC169 15p BSX271 25p ZTX109 15p 2N3052 AC188 25p BC169 47p MF169 47p ZTX300 12p 2N3703 AC189 AC190 40p BC161 70p MESSA 67p ZTX201 25p 2N3703 AC190 40p BC161 70p MESSA 67p ZTX302 25p 2N3705 AC189 40p BC161 40p BC162 40p BC162 40p ZTX303 25p 2N3705 AC189 40p BC162 40p ZTX303 25p 2N3705 AC189 40p BC162 40p ZTX303 40p ZTX304 25p 2N3705 AC189 40p ZTX304 25p 2N3705 AC189 40p ZTX304 25p 2N3705 AC1816 40p BC162 40p MF169 40p ZTX500 15p 2N3706 AC1816 40p BC162 40p MF169 40p ZTX500 15p 2N3706 AC1816 40p BC162 40p ZTX500 45p ZTX500	AC188 25p 8C158 10p 8FY50 24p 0C171 30p N2926 all 10p AC1676 15p 8C168 10p 8FY51 21p 2TX107 15p 8C3033 23p AC187 25p 8C159 115p 8N303 32p 32p AC187 25p 8C159 115p 8N321 26p 2TX108 12p 2N3035 23p AC187 25p 8C169 15p 8SX21 26p 2TX109 12p 2N3035 49p AC188 25p 8C268 15p 8SX21 26p 2TX109 12p 2N3035 12p 2N3032 12p AC188 25p 8C168 15p 8SX21 26p 2TX109 12p 2N3030 12p AC188 25p 8C168 16p 8V515 2TX301 12p 2N3030 12p AC189 20p 8D131 67p M2F610 47p 2TX302 20p 8D331 70p M2F610 47p 2TX302 20p 2N3703 12p AC190 40p 8D132 70p M2F610 37p 2TX302 20p 2N3703 10p AC161 40p 8D132 70p M2F610 37p 2TX301 20p 2N3703 10p AC161 40p 8D132 70p M2F610 37p 2TX301 20p 2N3703 10p AC161 40p 8D132 70p M2F610 37p 2TX301 20p 2N3703 10p AC161 40p 8D132 70p M2F610 47p 2TX301 15p 2N3701 15p AC161 40p 8D161 20p M2F610 45p 2TX501 15p 2N3701 12p AC161 40p 8D161 20p M2F610 45p 2TX501 15p 2N3708 12p AC161 40p 8D161 20p M2F610 45p 2TX501 15p 2N3708 12p AC161 40p 8D161 20p M2F610 45p 2TX501 15p 2N3708 12p AC161 40p 8D161 80p 8C63 40p 2TX502 20p 2N3710 12p AC161 40p 8D161 80p 8C63 40p 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			A STATE OF THE STA	- 2	
mixed die	electric	10	V00V		
1000pf 6	p 6800pf	9p	-1 µF	12p	
2200pf 6	p -01μF	9p	-22µF	22p	
3300pf 6	D 022 uF	9p	-47µF	30p	
4700pt 6	p -047µF	12p			
Ceramic					
12KV.d.c	8KV.d.	C.	HI-K 750	V.	
10pf 9p	200pf	9p	1000pf	5p	
15pf 9p	220pt	9p	1500pf	5p	
22pf 9p	250pf	9p	2000pf	5p	
68pf 9p	270pf	9p	3000pf	5p	
82pf 9p	300pf	9p	5000pf	5ρ	
100pf 9p	750V £	DISC	10,000pf	5p	
120pf 9p	470pf	5p	feed-		
140pf 9p	1000pf	5p	through		
150pf 9p	5000pf	5p			
180pf 9p	10,000pf	5p	1000pf	5p	

Mullard B Siemens Electrolytics

	CAP		VOLTAGE						
	μF	4	6.3	10	16	25	40	63	
	1	_	_	_	_	_	_	6p	
- 1	1.5	~~~	_	-	-	****	where	6p	
	2.2	_	_	_	_	_	_	60	
	3.3	_		with		_	_	5p	
-	4.7		-	_	_		_	бρ.	
- (6-8	_	-	_	-	_	6p	5p	
-1	10	_	_	_	_	5p	_	8p	
-1	15	_	-	_	6p	****	6p	6р	
- 1	22			6p	-	6p	-	5p	
- 1	33	_	6p	_	6p	_	6p	_	
п	47	6р	_	6р	_	6р	8р	6р	
н	68	_	6р	_	бp	_	_	10p	
ч	100	6p	_	6p	_	6p	6р	12p	
н	150	_	6p	_	80	6p	10p	12p	
	220	6p	_	6p	6p	10p	12p	18p	
	330	5p	_	6p	10p	-	_	21p	
-	470	_	6 p	10p		12p	18p	40p	
- 1	680	_	10p	-	12p	18p	21p	_	
	1000	10p	_	12p	18p	21p	40p	60p	
- 1	1500		12p	18p	21p	_	_	_	
	2200	_	18p	21p	40p	45p	55p	93p	
- 1	3300	_	21p	-	_	mps.c	_	-	
ı	4700	21p	_	-	60p	75p	93p		l
ł	CAP			,	/OLT/				
-1	μF				15	25	40	64	
1	500						33p	40p	
-1	1250						50p		
-1	1600						-	75p	
-1	2000				40p	50p			
- [2500				_	_	75p	93p	
ı	3200				50p	_	_	_	

Hi~Volt Electrolytics

Quantity Prices on application.

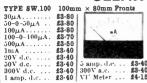
1: 2: 4. 8µF 450V	14p	32 u F	450V	20p
16µF 450V	15p	50µF		20p
8 - 8µF. 450 V.W	18p	32 - 32 µF;	350 V.W	25p
8 : 16µF; 450 V.W	20p	32 32µF:	450 V W	43p
16 - 16µF; 450 V.W	25p	50 · 50µF;	350 V.W	35p

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Type SD.830	82-5mm	× 110mm Fronts
1.1.1.1	, I	10mA £2-50 50mA £2-50
A		100mA £2-50 500mA £2-50

, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	10mA 50mA 100mA
A Starte	500mA .
	1 amp
0μΑ £2-75	
0-0-50μA £2-70 00μA £2-70	10V d.c 20V d.c
00-0-100µA. £2.70	50V d.c

	500mA	£2.50	
A CONTRACTOR OF THE PARTY OF TH	1 amp	£2-50	1
21765 SS 2 COM 15 15	5 amp	£2.50	5
A STATE OF THE PARTY OF THE PAR	10 amp	£2-50	1
50μA £2.75	5V d.c	£2.50	١.
50-0-50μA £2-70	10V d.c	£2-50	
100µA £2.70	20V d.c	22.50	I
100-0-100µA. £2.70	50V d.c	£2.50	
200µА	300V d.c	£2-50	15
500μA £2-55	15V a.c	£2-75	li
1mA £2-50	300V a.c	22-75	1
5mA £2-50	VI Meter		5
			ĭ
			15
Type SD.640 63-5mm	× 85mm Front	8	ľ

ı	Type SD.640	63-5mm	× 85mm Fronts	
l	30μA	£2-60	500mA £2.3	
ı	50-0-50μA		1 amp £2-3	5
	100µA		5 amp £2.31	
	100-0-100µA.		10 amp £2.31	
	200μΑ	£2.55	5Vd.c £2.31	
	500µA		20 V d.c £2.31	
	1mA	£2.35	50 V d.c £2.8	
	5mA	£2-35	300V d.c #2-31	
	10mA	£2.35	15V a.c #2:40	
	50mA	£2-35	300V a.c 22-40	
	100mA	£2-35	VU Meter \$2.70	
1				
ı				

Type SD.460 4	l6mm >	< 59-5mm Front	5
50μA	£2-40	1 amp	£2-15
50-0-50uA	£2-35	5 amp	£2-15
100μΑ	£2.35	10 amp	£2.15
100-0-100µA.	£2.35	5V d.c	£2.15
200μΑ	£2.35	10V d.c	22.15
500µA	£2-20	20V d.c	£2.15
1mA	£2-15	50 V d.c	£2.18
5mA	£2.15	300 V d.c	£2-15
10mA	£2 ⋅15	15V a.c	£2-30
50mA	£2·15		
100mA	£2-15	300V a.e	£2-30
500mA	£2-15	VV Meter	£2.55

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Type MR.85P. 4;in.	× 43in. Pron
(50mA
100 to 10	100mA
- total man	500mA
mA	1 amp
01	5 amp
20.00	15 amp
	30 amp
TAX REPORT - 100 (100 100 100 100 100 100 100 100 10	20 V d.c.

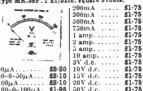
	Outly Solf
The second second	100mA £3-10
John Daries	500mA \$8-10
mA	1 amp £8-10
oti	5 amp £3.10
100 day	15 amp £8-10
	30 amp £3.20
15 (15 (15 (15 (15 (15 (15 (15 (15 (15 (20 V d.c £8-10
WWW.	50V d.c £8·10
50μA £3.95	150V d.c #3-10
50-0-50μA £3.40	300V d.c #3-10
100μΑ ±3-40	15V a.c 23-10
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200μA	S Meter 1mA. \$8.15
500μA £3-20	VU Meter £8-95
500-0-500μA. 23·10	l amp. a.c *£3-10
1mA £3-10	5 amp. a.c *£3-10
1-0-1mA £3-10	10 amp. a.c. *23.10
5mA £3.10	20 amp. a.c *23-10
10mA #3-10	30 amp. a.c *23-10

П			
ľ			
ŀ	Type MR.52P. 50μA 50-0-50μA 100μA	23in. s	quare Fronts.
ŀ	304A	£3.40	10V d.c \$2.20
ŀ	50-0-50µA	£2-85	20 V d.c £2.20
i	100μΑ	£2.85	50 V d.c \$2.20
ï	1100-0-100uA.	£2-75	300 V d.c \$2.20
)	500μΑ	£2-55	15V a.c £2.30
	1mA	£2-20	300 V a.c £2-80
-	1mA	£2-20	S Meter ImA. #2.30
	10mA	£2-20	VU Meter £3-50
í	50mA	£2-20	1 amp. a.c *22-20
í	50mA 100mA 500mA	£2-20	5 amp. a.c
í	500mA	£2-20	
í	1 amp.	£2-20	20 amp. a.c *£2.20
í	1 amp	£2.20	30 amp. a.c *22-20
;			•

5				
5	Type MR.65P. 3	Bain. ×	3 in. Fronts	
0	50μA	£8.70	10V d.c	£2-40
0	50-0-50μA	£3.00	20 V d.c	#2-40
0	100µA	£3.00	50V d.e	£2-40
- 1	100-0-100µA.	£2.90	150V d.c	£2-40
-	200μA	£2-90	300V d.c	22-40
	500μA	£2-65	15V a.c	£2.55
5	300-0-300µA.	£2.40	50V a.c	£2-55
5	1mA	£2-40	150V a.c	£2-55
5	5mA	#2-40	300V a.c	£2-55
5	10mA	£2-40	500V a.c	
5	50mA	£2-40	8 Meter ImA.	£2.60
5	100mA	£2.40	VU Meter	
5	500mA	£2-40	50mA a.c	
5	1 amp	£2-40	100mA a.c	
	5 amp	£2-40	200mA a.c	
0		£2.40	500mA a.c	
0	15 amp	#2-40	1 amp. a.c	*£2-40
5		£2.40	5 amp. a.c	*22.40
	30 amp	£2-55	10 amp. a.c	*22-40
_	50 amp	£2.75	20 amp. a.c	*42-40
	5V d.c	£2-40	30 amp. a.c	*£2-40

Send for illustrated brochure on SEW Panel Meters-discounts for quantities.

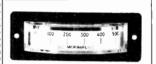
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100V d.c	£1-75
150V d.c	£1.75
300V d.c	£1.75
500V d.c	£1.75
750V d.c	£1.75
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50V a.c	£1.85
150V a.c	£1.85
300V a.c	£1.85
500V a.c	£1.85
8 Meter 1mA.	£1-85
VU Meter	£2-30
	15V d.c. 50V d.c. 50V d.c. 100V d.c. 150V d.c. 150V d.c. 300V d.c. 500V d.c. 150V d.c. 150V a.c. 150V a.c. 300V a.c. 300V a.c. 300V a.c. 300V a.c. 300V a.c.

Type MR.45P. 2in, square Fronts.

JULA	20.00	
$50-0-50\mu A$	£2.80	10V d.c £1.85
100μΑ	£2-30	20V d.c £1.85
100-0-100µA.	£2-05	50V d.c £1.85
$200\mu A \dots$	£2.05	300 V d.c £1-85
500μA	£1-95	15V a.c #2.00
500-0-500uA.	£1.85	300V a.c £2.00
1mA	£1-85	8 Meter 1mA. 22.05
5mA	£1-85	VU Meter \$2.50.
10mA	£1.85	1 amp. a.c. *21.85
50mA	£1-85	5 amp. a.c *21.85
100mA	£1.85	
500mA	£1-85	20 amp. a.c *21.85
1 amp	£1.85	30 amp. a.c *£1-85



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ı			1n
i	Type PE.70. 3	17/32in. × 1 15/32in. × a. deep. 10 500μA	50
١	271	a. deep.	10
١	50μA 23-	10 500μA £3-05	11
	50-0-50μA #3-	30 In 40.70	50
	100μA	80 3003	1
١	100-0-100μA. 23·	50 2004 a.c 25.10	12
	200μA	20 VU Meter #8-75	34

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Type MR.65. 3jin. square Fronts. 1 amp...... 5 amp...... 15 amp.....

€3-

89. #2·

#2. #2.

89. 42.

42-1



50μA 50–0–50μA 100μA 100–0–100μA

500μA...... 500-0-500μA.

1mA 1-0-1mA 5mA

50mA 100mA 500m 4

41.05

	5V d.c	#2-15
	10V d.c	£2-15
	20V d.c	£2·15
	50V d.c	£2-15
•	150V d.c	£2-15
	300 V d.c	#2-15
3.5	50mV d.c	\$2-40
00	100mV d.c	\$2-40
30	30V a.c.*	£2-20
30	50V a.c.	42-20
50	150V a.c.*	#2-20
15	300V a.c.*	£2-20
15	500mA a.c.* .	£2-15
15	1 amp. a.c.* .	£2-15
15	5 amp. a.c	£2-15
15	10 amp. a.c.*	£2-15
15	20 amp. a.c.	£2-15
1.5	30 amp. a.c.*	£2·15
LS	50 amp. a.c.	\$2-15
15	VU Meter	

30 amp.

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	\$8-40
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500μA	£8-05
1mA	£2.85
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1 amp. d.c	£2-85
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Tests 1CO and B. Pnp/npn. Operates from 9V battery. Complete with all instructions, etc. 28-95. Post 20p.



MCA.220 AUTOMATIC VOLTAGE STABILISER

Input 88-125V a.c. or 176-250V a.c. Output 120V a.c. or 240V a.c. 200VA rating. \$11-97, Post 50p.



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0/115/230V. Step up or step down. Fully shrouded 22·10 P. & P. 18p 22·70 P. & P. 18p 23·60 P. & P. 23p 25·25 P. & P. 38p 27·50 P. & P. 38p 210·20 P. & P. 43p 217·25 P. & P. 50p 235·00 P. & P. £1 80 W 150W 300W 500W 1000W 1500 V

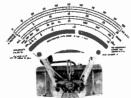


2250W 5000 W

230 VOLT A.C. 50 CYCLES **RELAYS**

Brand new. 3 sets of changeover contacts at 5 anp. rating. 50p each. Post 10p (100 lots £40) Quantities available.

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MODEL 1092 Testmeter.

5,000 O.P.V. 0/3/15/150/300/1,200V d.c. 0/6/30/300/600V a.c. 0/300// A /300M A 0/10K/1 meg Ω
Decibels -10 to +16 dB
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HIOKI MODEL 720X 20,000 O.P.V.

Overload protection 5/25/100/500/1.000V d.c. 10/50/250/1,000 V a.c. 50μA/250mA. 20K/ ohm. —5 to 20K/2 £4.97, Post 15p.



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30,000 O.P.V. Overload pro-6/30/60/300/600/ tection. 6/30/60/300/600/ 1,200V d.c. 12/60/120/600/ 1,200 V a.c. 12/60/120/600/1,200 V a.c. $60\mu A/30mA/300mA$. 2K/200K/2 megohm. -10 to +63 dB. **26-50**. Post 15p.



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20,000 O.P.V. 0/0-6/6/30/120/ 600/1,200/3,000/6,000V d.c. 0/6/30/120/600/1,200V a.c. 0/60μΑ/6/b0/600mA 0/6K/ 600K/6Meg./60 Meg. Ω 50pF. 0-2mFd. **25-97**. Post 17p.



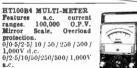


MODEL 500 30,000 O.P.V with overload protection mirror scale 0/0·5/2·5/10/25/ 100/250/500/1.000V d.c 100/250/500/1,000V d.c.
0/25/10/25/100/250/500/
1,000V a.c. 0/50μΑ/5/50/
500mA 12 amp d.c.
0/60/K/6 Meg./60 Meg Ω.
28-87. Post paid.

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HIOKI MODEL 750X 50,000 O.P.V. 43 ranges 0-0-3 to 1,200V d.c. 0-3 to 1,200V a.c. 0.3011 A /300ro A 0-3K/30 meg ohms.

+17dB. £8.97. Post 20p.



0/10/250µA/2·5/25/250MA/

10 amp. d.c. 10 amp. d.c. 10 amp. a.c. 0/20K/200K/2MEG/20 MEG. -20 +62dB. **£12-50**. Post 25p.

270 WTR MULTIMETER 370 WTK MULTIMETER Features a.c. current ranges. 20,000 O.P.V. 0/0·5/2·5 / 10 / 50 / 250/500/ 1,000V d.c. 0/2·5/10/50/250/500/1,000V

0/50µA/1/10 / 100mA / 1 / 10

amp. d.c. 0/100mA/1/10 amp. a.c. 0/5K/50K/500K/5MEG/50MEG. -20 +62dB. 215, Post 25p.

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Model U437 10,000 O.P.V. A first class versatile in-instrument manufactured in Instrument manufactured in U.S.S.R. to the highest standards. Ranges: 2-5/10/50/250/500/1,000V d.c. 2-5/10/50/250/500/1,000V a.c. D.c. current 100wA/1/10/100mA/1A. Resistance 300 ohms/3/30/300K/3m O. Complete with betteries Complete with batteries, test leads, instructions and sturdy steel carrying case. OUR PRICE \$5-97. Post 25p. Complete



ROUND SCALE TYPE PENCIL TESTER WODEL TRAS



Completely portable, simple to use pocket sized tester. Ranges 0/3/30/300V a.c. and d.c. at 2,000 O.P.V. Resistance 0°20K ohms. ONLY \$1.97. Post 13p.

LT 601 MULTI-

METER New style 20,000 O.P.V. pocket New style 20,000 O.P.V. pocket multimeter. 5/25/ 50/250/500/25.0600/ d.c. 10/50/100/500/ 1,000V ac. 50µA/ 250A. 6K/6 meg oluns. -20 to +22 dB. 38-75. Post 20p.



MODEL TH-12

MODEL TM-12 20,000 O.P.V. Overload pro-tection. Slide switch selector. 0/0-25/2-5/10/50/1250/1,000V d.c. 0/10/50/250/1,000V s.c. 0/50µA/25/250nA d.c. 0/3K/ 30K/300K/3 meg. -20 +50dB Post 15p

TE-300 MODEL TE-500.

O.P.V. Mirror scale, overload protection 0/0.6/3/15/60/300/ protection 1,200V d.c. 0/6/30/120/600/ 1,200V a.c. 0/30µA/6mA/6mA/60mA/300mA/300mA/600mA. 0/8K/80K/800K/8 meg. ohm -20 to -63dB. **25.97**. Post 15p.



MODEL PL486 20k Ω/V d.c. 8k Ω/V 20kH/V d.c. 8kH/V a.c. Mirror scale. 0-6/3/12/30 /120 / 600 V d.c. 3/30/120/600 V a.c. 50/600µA/60/ 600mA. 10/100 K/ Meg/10 Meg Ω -20 to +46dB. \$6.97, Post 12p.



TMK MODEL TW-50K 46 ranges, mirror scale, 50K/V a.c. Dc.: Volts 0:125, 0:25, 1:25, 2:5, 5, 10, 2:5, 50, 125, 0:20, 50, 1, 0:00V. A.c. Volts: 1:5, 3, 5, 10, 22, 50, 125, 50(A, 2:5, 50(A, 2:5, 50(A, 2:5, 50(A, 2:5, 50(A, 3:5), 10 aup. Resistance: 10K, 100K, 11 MEG Ω. Decibels: -20 to +81:5 dB. 28-50. Post 17p. Decibels: -20 **£8-50**, Post 17p.

MODEL

Taut band suspension Overload pro-tection. tection.
Polarity reversing switch. 30,000 O.P.V. 0/0.5 / 2.5 / 15

50/250/500/1,000/2,500V d.c. 0/15/50/150/ 500/1,000V a.c. 0/50µA/5/50/150/500mA/ d.c. 0/3K/300K/3meg. 28-95. Post 20p



HICKI MODEL 700X HOKI MODEL 700X 100,000 O.P.V. Overload protection. Mirror scale 0.3/0-6/1-2/1-5/3/6/12/30/60/ 120/300/600/1,200V d.c. 1.5/3/6/12/30/60/150/300/ 600/1.200V a.c.

15/30µA/3/6/30/60/150/300mA 6/12 amp. d.e. 2K/200K/ 2 Meg/20 Meg ohm -20 to +63dB. 213-50. Post 20p.



MODEL C-7080 EN Giant 6in mirror scale. 20,000 O.P.V 0/0.25/1/2.5/10/50/250 1.000/5.000V d.c. 0/2·5/10

1,000/3,000 V d.c. 0/2/3/10 /50/250/1,000/5,000 V a.c. 0/50μA/1/10/100/500mA/ 10 amp. d.c. 0/2K/200K/ 20 meg. -20 to +50dB. £13-95. Post 35p.

U4312 MULTIMETER Extremely sturdy instrument for general electrical use 667 O.P.V.

0/0 0/F.V. 0/03/1.5/7.5/30/60/150/300/ 600/900V d.c. and 75mV. 0/03/1.5/7.5/30/60/150/300/ 600/900V a.c. 600/900V a.c. 0/300µA/1·5/6/15/60/150 600MA/1·5/6 amp. d.c. 0/1·5/6/15/60/150/600MA/



Selected TEST EQUIPMENT

FTC-401 TRANSISTOR TESTER

Full capabilities for measuring A, B and ICO.

npn or pnp. Equally adaptnpn or pnp. Eduary adaptable for checking diodes. Supplied complete with instructions, battery and leads. 27-50. Post 20p.



Model S-100TR MULTIMETER/TRANSISTOR

Model S-100TR MULTIMETER, TESTER 100,000 O.P.V. mirror scale/overload protec-tion. 90.12/6-6/31/2/30/120/ 600V d.c. 9/8/30/120/600V a.c. 0/12/690/a./ 12/300m A/12 amp. d.c. 0/10 K/1 MEG/100 MEG. -20 to +50dB.0-01-2 MFD. Transistor tester measures Alpha, beta and Ico. Complete with batteries, instructions and leads. 213-50. Pest 25p.

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MODEL 449A IN CIRCUIT TRANSIS-TOR TESTER Checks true a.c. beta in/out. Checks Icbo. Checks diodes in/out.

cks SCR, etc Bets HI 10-500 Checks LO 2-50

LO 2-50 leho 0-5000 μ A. 220/240V a.c. operation. 217-50. Post 25p

TE-20D RF SIGNAL GENERATOR



63

810 MAL GENERATOR Accurate wide range sig-nal generator covering 120 kHz-300 MHz on 6 bands. Directly cali-brated Variable R.F. at-tennator, audio output, Xtal socket for calibra-tion. 220/240V a.c. Brand new with instructions. \$15. Carr. 37p. Size 140nm × 215mm × 170nm.

MODEL L-55 FET V.O.M. Input impedance 10 meg ohns. 0/0°3/1°2/8/ 30/120/600V d.c. 0/3/120/ 4/120mA d.c. 0/1K/100K/ 10 meg/100 meg ohns. \$15-97. Post 25p.



CI-5 PULSE OSCILLO-SCOPE For display of pulsed and

waveforms in electronic circuits. VERT. AMP. Bandwidth 10MHz. Sensitivity at 100kHz VRMS/mm. 0-1-25; HOR. AMP. Bandwidth 500kHz. Sensitivity at 100kHz. VRMS/mm. 0-1-25; Pre-set triggered sweep 1-3,000µsec.; free running 20-200,000Hz in nine ranges. Calibrator pips. 220mm × 360mm × 420mm. 115-230V a.c. operation.

TO-3 PORTABLE OSCILLOSCOPE



3in tube, Y amp, Sensitivity
0-1V p-p/CM. Bandwidth
1-5cps-1-3MHz. James 2-5pr N amp,
sensitivity 0-9V. p-p/CM.
Bandwidth 1-5cps-8900kHz.
Input imp. 2 meg Ω 20pF.
Time base. 5 ranges 10cps300kHz. synchronisation,
x 215mm x 330mm. Weight 134lb. 220/
240V a.c. Supplied brand new with handbook. \$40-00. Carr. 50p.

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RUSSIAN CI-16 DOUBLE BEAM

RUSSIAN CI-16 DOUBLE BEAM OSCILLOSCOPE

3MHz Pass Band. Separate Y1 and Y2
amplifiers. Rectangular
5in x 4in C.R.T. Calibrated triggered sweep
from 0-2L/sec to 100
milli-sec per cm. Free
running time base 56
Hz-1MHz. Built-in
time base calibrator and
amplitude calibrator
Supplied complete with
all accessories and instruction man
\$37. Carr. paid.



TRANSISTORISED L.C.R. A.C. MEASURING BRIDGE



TE-16A Transistorised

Signal Generator. 5 ranges 400kHz.—30MHz. An

ges 400k Hz.—30M Hz. An inexpensive instrument for the handyman. Operates on 9V battery.

Wide easy to read scale 800kHz modulation.

MEASURING BRIDGE

MEASURING BRIDGE

portable bridge offering extended to the color of the colo Post 25p.

MODEL TE15 GRID DIP METER

METER
Transistorised. Operates
as Grid Dip, Oscillator,
Absorption Wave Meter
and Oscillating Detector,
Frequency range 440kHz280MHz in 6 coils. 300µA
meter. 9V battery operation, Size 180mm × 80mm × 40mm. £12-50. Post 20p.

BELCO AF-5A SOLID STATE SINE SQUARE WAVE C.R. OSCILLATOR



Sine 18-200,000 Hz; Square 18-50,000 Square 18-50,000 Hz. Output max. +10dB (10 K ohms) Operation internal batteries. Attrac-tive 2-tone case 7% in × 5in × 2in. Price 217-50. Carr.

Tech O

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MODEL MG-100 SINE SQUARE WAVE AUDIO GENERATOR 19-220.000

Wave

Range 19 100 000Hz 19 — 100,000Hz. Square Wave. Out-put Sine or Square 180mm × 90mm × wave 10V. P. to P. Size

ini. Operation 220/240V a.c. Post 37p. #17-50



MODEL AT201 DECADE ATTENUATOR Frequency range 0-200kHz.

Attenuator 0-111dB. 0.1dB step. Impedance 600 a. Max. input power 30d Bm. 90mm × 55mm.

180mm × 90m 50. Post 37p TE-65 VALVE VOLTMETER



£12-50.

ALVE VOLTMETER
28 ranges, D.c. volts
1:3-1,500V a.c. volts
1:3-1,500V a.c. volts
1:3-1,000V. Resistance
up to 1,000 megohms.
200/240V a.c. operation. Complete with
probe and instructions.
217:50. Post 30p.
Additional probes available: R.F. 22:12; H.V.
22:50.

MODEL U4311 SUB-STANDARI

MULTI-RANGE VOLT AMMETER

Sensitivity 330 ohns/Volt
a.c. and d.c. Accuracy 0.5%
d.c. 1° a.c. Scale length

d.c. 1°₈ a.c. Scare length 165nms.
0/360/7.5 μ/1/5/3/7-5/15/30/
75/15/0/300/7.50 μ/1/5/3/7-5/15/30/
300/7.50 μ/1/5/3/7-5/15/30/
300/7.50 μ/1/5/3/7-5/15/30/
750 μ/1/5/3/7-5/15/30/
75/15/0/300/7.50 d.c. 0/
75/15/3/30/7.75/15/30/
75/15/3/0/7.75/16/30/
75/15/3/0/7.75 d.c. 0/

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4 Bands covering 550kHz-30MHz. Built-in Speaker 220/240V a.c. Brand with instructions, £15.75, Carr. 37p.



UR-1A SOLID STATE COMMUNICATION RECEIVER

4 Bands covering 550kHz-30MHz. FET. 8 Meter. Variable BFO for SSB, Built-in Speaker, Bandspread, Sensitivity Control. 220/240V a.c. or 12V d.c. 12in-x4in×7in. Brand new with instructions. 225. Carr. 37p.

SKYWOOD CX203 COMMUNICATION



Noild state. Coverage on 5 bands 200-420 kHz and 0-55 to 30MHz. Illuminated slide rule dial. Bandspread. Aerial tuning. BFO, AVC, ANL, '8' meter. AM/CW/88B. Integrated speaker and phone socket. Operation 220/240V a.c. or 12V d.c. 8ize 325 x 266 x 130 nm. Complete with instructions and circuit. 428-50. Carr. 30p.

LAFAYETTE HA-600 SOLID STATE RECEIVER



coverage z, 550



TRIO 9R59DS COMMUNI-CATION RECEIVER 4 band cover ing 550kHz-

tinuous and electrical bandspread on plus 7 diode circuit. 4/8 ohm output and phone jack. 88B-CW. ANL. Variable BFO. 8 meter. 8e. bandspread dist. IV forecast. 8 meter. Sep. bandspread dial. If frequency 455kHz. Audio output 1.5W. Variable RF and AF gain controls 115/250V a.c. Size 7in×13in×10in with instruction manual. 249-50. Carr. paid.



RMI LOUDSPEAKERS

Model 350. 13in×8in with single tweeter/crossover, 20-20,000Hz. 15W RMS. Available 8 or 15 ohms. 27.25 each. Post 37p. Model 450. 13in×8in with twin tweeter/crossover. 55-13,000Hz. 8W RMS. Available 8 or 15 ohns. 23-62 each. Post 25p.

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HONEYWELL DIGITAL VOLTMETER VT.100

Can be panel or bench mounted. Basic meter measure a wide range of a.c. and d.c. volt, current and ohnse with optional plug in cards. Specification: Accuracy: 40-2, ±1 (digit. Resolution: ImV. Number of digits: 3 plus fourth overrange digit. Overrange: 180% (up to 1999). Input Impedance: 180% (up to 1999). Input Impedance: 1800 Meg ohm. Measuring cycle of per second. Adjustment: Automatic zeroing, full scale adjustment against an internal reference voltage. Overload: to 180V d.c. Input: Fully floating (3 poles). Input power: 110-230V a.c. 50/60 cycles. Overall size: 5½in×2½in×8½in. AVAILABLE BRAND NEW AND FULLY GUARANTEED.



Project 60 Package



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2×Z30 amplifier, stereo 60 pre-amp, PZ5
power supply, \$15 98. Carr. 37p. Or with
PZ6 power supply, \$15 98. Carr. 37p. Or with
PZ6 power supply, \$25 98. Carr. 37p.
Transformer for PZ8. 2597 extra.
Add to any of the above \$4 45 for active
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NEW PROJECT 605—\$20.97. Carr. 37p.

WHARFEDALE MID-RANGE HI-FI UNITS As used in world famous system. 5in dis. Impedance 4/8 ohms. High flux ceramic magnet. 20W RMS. Brand new \$1.50. Carr. 37p.

SPECIAL OFFER!

Hi-Fi 12in 20W twin cone full range speaker. 30-16,000Hz. 16,500 gauss. 8 ohn imped-ance. Brand new and boxed. (List price £21-72). OUR PRICE £12-50 each. Carr. 50p.

AXIOM 301



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HA-10 STEREO HEADPHONE AMPLIFIER All silicon trans-

All silicon transistor amplifier operceramic or tuner inputs with twin stereo
headphone outputs and separate volume
controls for each channel. Operates from 9V
hattery. Inputs 5MU/100MU. Output 50MW.
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SPECIAL PURCHASE! NEAT G301 STATIC BALANCE PICK-UP ARMS



Identical specification to NEAT G30 arm but with two-tone chrome and black finish. Complete with head shell, pick-up rest and plug in phono leads. BRAND NEW—FULLY GUARANTEED.
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High quality instrument to test Reverse Leak current and D.C. current. current and D.C. current.
Amplification factor of
NPN, PNP, transistors,
dlodes, SCR's, etc. 4" ×
42" clear scale meter.
Operates from internal
batteries. Complete with
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KAMODEN HMG-500 INSULATION RE-SISTANCE TESTER

Range 0-1,000 Megohnis, 500 Volt. Megohnis, 500 Voit.
Battery operated.
Wide range clear
meter 4½" × 4".
Complete with deluxe carrying case,
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\$19.95. Post 30p.

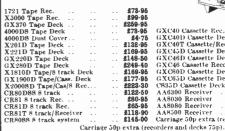




ARF-300 AF/RF SIGNAL GENERATOR All transistorised, com-pact, fully portable. AF sine wave 18 Hz to 220 sine wave 18 Hz to 220 KHz. AF square wave 18 Hz to 100 KHz. Output sine/square 10v.
P-P. RF 100 KHz to
200 MHz. Output 1v.
maximum. Operation
220/240v, AC. Complete

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SUPER MONEY SAVING OFFERS—BUY **NOW WHILE STOCKS LAST!** ALL BRAND NEW AND **FULLY GUARANTEED**





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1021 STEREO

1021 STEREO LISTENING STATION For balancing and gain selection of loudspeakers with additional facility for stereo head phone

on stereo neadphone switching. 2 gain controls, speaker on-off slide switch, stereo headphone sockets. 6in×4in×2½in. \$2.25. Post 15p.

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MP7 MIXER PREAMPLIFIER 5 microphone in-puts each with individual gain controls enabling complete mixing

facilities. Battery operated. 91nx Sinx Sin. Inputs Mics: 3×3mV 50K: 2×3mV 600 ohm. Phono meg. 4nV 50K. Phono ceramic 100mV 1 meg. Output 250mV 100K. 1 meg. Ou Post 20p.



TE-1035 STEREO HEADPHONES HEADPHORES
Low cost high performance stereo headphones.
Foam rubber ear cups.
Adjustable head-band.
8 ohm impedance. 2518,000Hz. With lead and stereo jack plug. ONLY £1.97. Post 12p.

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range of Garrard Popular Popular range of Garrard devices with Shure cartridge fitted in deluxe plinth with hinged lid. SP25 111 Module/M75-6 . \$23-50 AP76 Module/M75-6 . \$38-80 AP76 Module/M75-6 . \$38-76 Module/M75-6 . \$38 Zero 1008 Module/M93E 252-60 Carr. 50p extra any item



HOSIDEN DH-08S DE-LUXE STEREO
HEADPHONES
Features unique mechanical 2 way units and
fitted adjustable level
controls. 8 ohm impedance 20-20,000;
Complete with apringlead & stereo jack plug
£7-97. Post 12p.

DOLBY SYSTEM NOISE REDUCTION UNIT



Improves the performance of cassette and semi-professional recorders. Reduces tape hiss by 3dB at 560Hz, 6dB at 1200Hz and 10dB for all frequencies above 3000Hz. Controls for for all frequencies above 3000Hz, Controls for input levels and noise reginition on record and replay, 2 meters for Dubly level, Off tape nointforing, Frequency response; 20Hz to 15kHz = 13E 19kHz = 354B. Size 15fin× 9in×3fin, A.; 200/2505.

OUR £32-50
Carr. 50p.

HOSIDEN DHO-28 STEREO HEADPHONES



Wonderful value and excellent per-formance combined. Adjustable head-band. 8 ohm im-pedance. 20-12,000 pedance. cps. Complete with lead and ONLY 22:37.

TAPE CASSETTES Top
quality
Hi-Fi
Low Noise
in Library

cases. 3 for **75p**. 3 for **£1.05** 3 for **£1.35** 980 C120 10 for £4-20 Tape Head Cleaner 30p each Post 10p extra.

EA.41 REVERBERATION

Self-contained transistorised, battery operated. Simply plug in microphone, guitar, etc., and output into your ampli-

fler. Volume control, depth of reverberation control. Beautiful walnut cabinet. 7[in×3in×4]in. 25.97. Beautiful

TRANSISTORISED FM TUNER



RISED FM TUNEE

6 TRANSISTOR
HIGH QU'ALITY
TUNER, SIZE
ONLY 6 int 4 in x
21 in. 3 I.F. stages.
Double tuned discriminator. Ample
output to feed most

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amplifiers. Operates on 9V battery. Coverage 88-108MHz. Ready built ready for use. Fan-tastic value for money. 28-37. Post 12p Sterco multiplex adaptors 24-97.

TE 1018 DE-LUXE MONO HIGH IMPE-DANCE HEADSET
Sensitive, soft earpads, adjustable headband.
Magnetic, impedance 2,600 ohms. 21.97. Post 15p.



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FANTASTIC OFFER!



17+17W r.m.s. stereo amplifier with inputs for Magnetic and Crystal phono. Tuner, Tape, Aux and Tape Monitor. Outputs for two pairs of stereo speakers and tape. Stereo headphone socker. Full range of controls including loudness control, scratch filter, etc. Size 13in \times 9½in \times 3½in. Unrepeatable offer—limited stocks!

List price £59.50 OUR PRICE

Carriage 50p

NIKKO TRM 50 SYSTEM



NIKKO TRM50 17+ 17W rms stereo amplifier, BSR MP60, plinth and cover, Goldring G800 cart-ridge, pair of Linton 2 speakers and all leads.

PRICE

£104.90

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Ing #1:50

LEAK DELTA 30 SYSTEM



Leak Delta 30 stereo amplifier, Goldring GL75, plinth, cover and G900 cartridge. Pair of Leak 150 speakers and all

OUR PRICE £123.50

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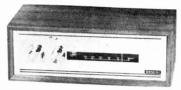
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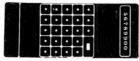
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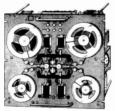
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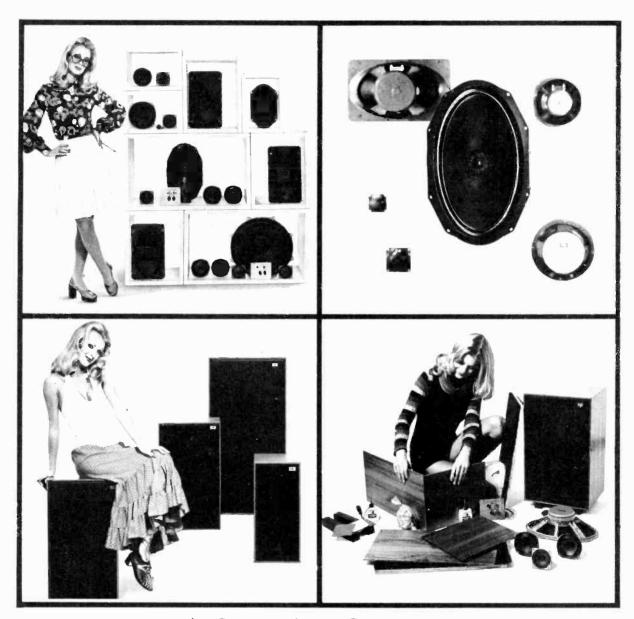
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AC142 AC142K AC151 AC154	0·14 0·17 0·15 0·20	AF139 AF178 AF179 AF180	0 · 30 0 · 50 0 · 50 0 · 50	BC169 BC170 BC171 BC172	0 · 12 0 · 12 0 · 14 0 · 14	BD188 BD189 BD190 BD195	0 · 70 0 · 75 0 · 75 0 · 85	BF272 BF273 BF274 BFW10	0.80 0.85 0.35 0.60	OC45 OC70 OC71 OC72	0·12 0·10 0·10 0·14	2N 404A 2N 524 2N 527 2N 598	0 · 28 0 · 42 0 · 49 0 · 42	2N2904A 0	21 21 21	2N3416 2N3417 2N3525 2N3646	0 · 28 0 · 28 0 · 75	2N5172 2N5457 2N5458	0·12 0·32 0·32
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AC176 AC177 AC178 AC179	0·20 0·24 0·28 0·28	A8Y29 A8Y50 A8Y51 A8Y52	0 · 25 0 · 25 0 · 25 0 · 25	BC182 BC182L BC183 BC183L	0·10 0·10 0·10 0·10	BD208 BDY20 BF115 BF117	0.95 1.00 0.24 0.45	BFY52 BFY53 BPX25 B8X19	0 · 20 0 · 17 0 · 85 0 · 15	OC83 OC84 OC139 OC140	0 20 0 20 0 20 0 20	2N711 2N717 2N717 2N718 2N718A	0·30 0·35 0·24 0·50	2N2926 (Y) 0 2N2926 (O)	12	2N3709 2N3710 2N3711 2N3819	0·09 0·09 0·28	28307 28321 28322 28322A	0 · 84 0 · 56 0 · 42 0 · 42
AC180 AC180 K AC181 AC181 K	0·17 0·20 0·17 0·20	A8Y55 A8Y56 A8Y57	0 · 25 0 · 25 0 · 25 0 · 25	BC184 BC184L BC186 BC187	0 12 0 12 0 28 0 28	BF118 BF119 BF121 BF123	0·70 0·70 0·45 0·50	B8X20 B8Y25 B8Y26 B8Y27	0 · 15 0 · 15 0 · 15 0 · 15	OC169 OC170 OC171 OC200	0 · 25 0 · 25 0 · 25 0 · 25	2N726 2N727 2N727 2N743 2N744	0·28 0·28 0·20 0·20	2N2926 (R) 0 2N2926 (B)		2N3820 2N3821 2N3823 2N3903	0·50 0·35 0·28 0·28	28323 28324 28325 28326	0·56 0·70 0·70 0·70
AC187 AC187 K AC188 AC188 K	0 · 22 0 · 20 0 · 22 0 · 20	A8Y58 A8Z21 BC107 BC108	0 · 25 0 · 40 0 · 09 0 · 09	BC207 BC208 BC209 BC212L	0·11 0·11 0·12 0·11	BF125 BF127 BF152 BF153	0 · 45 0 · 50 0 · 55 0 · 45	B8Y28 B8Y29 B8Y38 B8Y39	0·15 0·15 0·18 0·18	OC201 OC202 OC203 OC204	0 · 28 0 · 28 0 · 25 0 · 25	2N914 2N918 2N929 2N930	0·14 0·30 0·21 0·21	2N3010 0 · 2N3011 0 · 2N3053 0 ·	70 14	2N3904 2N3905 2N3906 2N4058	0·30 0·28 0·27 0·12	28327 28701 40361 40362	0 · 70 0 · 42 0 · 40 0 · 45
ACY17 ACY18 ACY19 ACY20	0 · 25 0 · 20 0 · 20 0 · 20	BC109 BC113 BC114 BC115	0·10 0·10 0·15 0·15	BC213L BC214L BC225 BC226	0·11 0·14 0·25 0·85	BF154 BF155 BF156 BF157	0.45 0.70 0.48 0.55	B8Y-0 B8Y41 B8Y95 B8Y95A	0 28 0 28 0 12 0 12	OC204 OC309 P346A P397	0 · 35 0 · 40 0 · 20 0 · 42	2N1131 2N1132 2N1302 2N1303	0 · 20 0 · 22 0 · 14			ES AND I			
ACY21 ACY22 ACY27 ACY28	0·20 0·16 0·18 0·19	BC116 BC117 BC118 BC119	0·15 0·15 0·10 0·30	BCY30 BCY31 BCY32 BCY33	0 · 24 0 · 26 0 · 30 0 · 22	BF158 BF159 BF160 BF162	0.55 0.60 0.40 0.40	Bu105 C111E C400 C407	2·00 0·50 0·80 0·25	OCP71 ORP12 ORP60 ORP61	0·48 0·48 0·40 0·40	2N1303 2N1304 2N1305 2N1306 2N1307	0·14 0·17 0·17 0·21	AA119 0- AA120 0- AA129 0- AAY30 0-	08 08 09	BY133 BY164 BYX38/3	0.42	OA10 OA47 OA70 OA79	0·85 0·07 0·07 0·07
ACY29 ACY30 ACY31 ACY34	0·85 0·28 0·28 0·21	BC120 BC125 BC126 BC132	0·80 0·12 0·18 0·12	BCY34 BCY70 BCY71 BCY72	0 25 0 14 0 18 0 14	BF163 BF164 BF165 BF167	0·40 0·40 0·40 0·22	C424 C425 C426 C428	0 · 20 0 · 50 0 · 85 0 · 20	8T140 8T141 TIS43 UT46	0·12 0·17 0·30 0·27	2N 1307 2N 1308 2N 1309 2N 1613 2N 1711	0 · 21 0 · 23 0 · 23 0 · 20 0 · 20	AAZ13 0- BA100 0- BA116 0- BA126 0- BA148 0-	10 21 22	BYZ10 BYZ11 BYZ12 BYZ13	0·35 0·30 0·30 0·25	OA81 OA85 OA90 OA91	0·07 0·09 0·06 0·06
ACY35 ACY36 ACY40 ACY41	0 · 21 0 · 28 0 · 17 0 · 18	BC134 BC135 BC136 BC137	0·18 0·12 0·15 0·15	BCZ10 BCZ11 BCZ12 BD121	0 · 20 0 · 25 0 · 25 0 · 60	BF173 BF176 BF177 BF178	0 · 22 0 · 35 0 · 35 0 · 30	C441 C442 C444 C450	0·30 0·30 0·35 0·22	2G301 2G302 2G303 2G304	0·09 0·19 0·19 0·24	2N 1889 2N 1890 2N 1893 2N 2147	0 · 32 0 · 45 0 · 37 0 · 72	BA154 0 BA155 0 BA156 0 BY100 0	12 14 13	BYZ16 BYZ17 BYZ18 BYZ19 CG62	0 · 40 0 · 85 0 · 85 0 · 28	OA95 OA200 OA202 8D10	0·07 0·06 0·07 0·05
ACY44 AD130 AD140 AD142	0 · 85 0 · 88 0 · 48 0 · 48	BC139 BC140 BC141 BC142	0 · 40 0 · 80 0 · 30 0 · 80	BD123 BD124 BD131 BD132	0 · 65 0 · 60 0 · 50 0 · 60	BF179 BF180 BF181 BF182	0·80 0·80 0·80 0·40	MAT100 MAT101 MAT120 MAT121	0·19 0·20 0·19 0·20	2G306 2G308 2G309 2G339	0 · 40 0 · 85 0 · 85 0 · 20	2N2145 2N2160 2N2192 2N2193	0·57 0·60 0·35 0·35	BY101 0 : BY105 0 :1 BY114 0 :1 BY126 0 :1	12 17 12	(Eg) OA9: CG651 (Eq) OA7	0.05	8D19 IN34 IN34A IN914 IN916	0·05 0·07 0·07 0·06 0·06
AD143 AD149 AD161	0:38 0:50 0:38	BC143 BC145 BC147	0·80 0·45 0·10	BD133 BD135 BD136	0·65 0·40 0·40	BF183 BF184 BF185	0 · 40 0 · 25 0 · 30	MPF102 MPF104 MPF105	0·42 0·87 0·87	2G339A 2G344 2G345	0·16 0·18 0·16	2N2194 2N2217 2N2218	0·35 0·22 0·20	BY127 0-1 BY128 0-1 BY130 0-1	15 15	OA79 OA5 OA58L	0 · 06 0 · 35 0 · 21	IN414B I8021 I8951	0·06 0·10 0·06

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TO5	TO66	TOR	TO6	TO4	3TO48	TO49	3 TO48	
50 0 23								
100 0 25	$0 \cdot 33$	0.47	0.47	0.50	0.58	0.63	$1 \cdot 40$	
200 0:35								
400 0 43	0.47	0.56	0.56	0.67	0.75	0.93	1.75	
600 O · 53	0.57	0.68	0.68	0.77	0.97	1.25	_	
800 0.63	0.70	0.80	0.80	0.90	1.20	1.50	4.00	

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PIV	300mA	750mA	1 A	1.5A	3 A	10A	30A
50	0.04	0.05	0.05	0.07	0.14	$0 \cdot 21$	0.60
100	0.04	0.06	0.05	0.13	0.16	0.23	0.75
200	0.05	0.09	0.06	0.14	0.20	0.24	1.00
400	0.06	$0 \cdot 13$	0.07	$0 \cdot 20$	0.27	$0 \cdot 37$	1.25
600	0.07	0.16	0.10	0.25	0.34	0.45	1.86
800	0 · 10	0.17	0.11	0.25	0.37	0.55	2.00
1000	0 · 11	0.25	0.14	0.30	0.46	0.63	2.50
1200	_	0.33	_	0.38	0.87	0.75	

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		25	100 +	(	1	25	100 -
SN7400	0:15	0.14	0:12	SN7489	£5:50	£5 25	£5.00
5N7401	0.15	0:14	0-12	SN7490	9.67	9.44	0:50
SN7402	0.15	0.14	0.12	SN7491	61.00	0.95	170
SN7403	0.15	0-14	0-12	SN7492	8-67	9 44	0.56
SN7404	0.15	0-14	0 12	SN7493	9-67	14	0.50
SN7405	0.15	0:14	0-12	SN7494	0.77	0.74	0.48
SN7406	0 35	0.31	0.28	SN7495	0.77	0.74	144
SN 7407	0.35	0 - 31	0 28	SN7496	0.67	0.04	0.78
SN 7408	0.18	0.17	0.16	SN74100	61 45	£1 40	£1:55
SN7409	0.18	0.17	0.16	SN74104	9.477	9.44	
SN7410	0 15	0:14	0-12	SN74105	9.97	0.94	1.0
SN7411	0 25	0.24	0-23	SN74107	0.40	0.30	1.5
SN7412	0.35	0.31	0 28	SN74110	0 55	0.53	0.50
SN7413	0.29	0 26	0 24	SN74111	61-25	£1 15	61-13
SN7416	0.43	0.40	0.30	SN74118	(1.00	0.95	0.40
SN7417	9.43	0.40	0.30	SN74119	£1:35	£1 ·25	£1-10
SN7420	0.15	0:14	0.12	SN74121	0.40	0.37	0.34
SN7422	0.50	0.40	0-45	SN74122	£1 40	£1-30	£1-10
SN 7423	0.50	141	45	SN74123	£2 00	62.70	£2 40
SN7425	0.50	0.48	0.45	SN74141	0.67	0 44	0 53
SN7427	0.45	0.42	0.40	SN74145	£1:50	(1-40	£1:30
SN7428	0.70	4.5		SN74150	£3 e0	62 70	£2:50
SN7430	0.15	14	0.12	SN74151	£1 ##	9.95	1.49
SN7432	0-45	0-42	1.40	SN74153	£1 20	£1·10	0.95
SN7433	0.00	0.75	9 79	SN74154	£1 89	61 70	£1 40
SN7437	144	0.62	44	SN74155	£1 40	61 30	£1 20
SN7438	4 44	0.62	144	SN74156	£1 40	61-30	£1 20
SN7440	0:15	0:14	0.12	SN74157	£1.40	£1:00	£1-70
SN7441	0.67	0.64	0.50	SN74160	£1 89	£1 70	£1 40
SN7442	0.67	0.64	1.58	SN74161	£1:00	£1*70	£1 40
SN7443	61:30	£1 25	61:20	SN74162	£4-00	63.75	63-50
SN7444	£1:30	61-25	£1:30	SN74163	£4 -00	£3-75	£3-50
SN7445	£1.89	£1:77	61-75	SN74164	£2 -20	£2:15	£2 · 10
SN7446	9.97	0.94	8-08	SN74165	£2·25	£2 -20	£2-15
SN7447	£1 ee	0.97	0.95	SN74166	£3 50	£3 · 25	£3 40
SN7448	£1 00	0.97	0.95	SN74174	£2:30	£2 20	£2 10
SN7450	0.15	0:14	0-12	SN74175	£1 40	£1 ·50	£1:40
SN7451	0.15	0:14	0.12	SN74176	£2 ·50	£2:40	£2 -30
SN7453	0.15	0-14	0-12	SN74177	£2:50	£2 40	£2 ·30
SN7454	0.15	0:14	0-12	SN74180	£2 -00	£1 <del>40</del>	£1-40
SN7460	0-15	0:14	0-12	SN74181	£5 50	£5 <b>00</b>	\$4.75
SN7470	8 - 29	0 - 26	8 24	SN74182	£2 40	£1 -80	£1 40
SN7472	0.29	0 - 36	8-24	SN74184	£3 ·50	£3 25	£3 ee
SN7473	0.37	0 - 35	0.32	SN74190	£1 <del>95</del>	£1 -90	£1:85
SN7474	0.37	0 - 35	0 - 32	SN74191	£1 90	£1 85	60 13
SN7475	0-45	0.43	0-42	SN74192	£1 45	£1.90	£1 45
SN7476	0 -40	6-39	0 - 36	SN74193	E2 400	£1-00	£1-75
SN7480	. 0 67	8-64	0 -58	SN74194	£2-70	£2 40	£2:50
SN7481	£1 30	£1-15	£1:10	SN74195	£2 00	£1.96	69-13
SN7482	9-87	0.06	0.65	SN74196	E1 00	£1 ·70	£1 40
SN7483	£1-10	£1 <del>0</del> 5	9-95	SN74197	£1 00	£1 ·79	£1 40
SN7484	69-13	9-95	8-90	SN74198	£5 50	25 40	£4 50
SN7485	£3 60	£3 :50	£3 40	SN74199	£5 ·50	£5 <b>60</b>	£4 · 50
SN7486	0.32	0.31	0:30				

#### LINEAR CC. --- FULL SPEC

		Price	
Type No.	1-24	25-99	100 up
BP201C \$1.201C	68p	58p	45p
BP701C \$1.701C	68p	50p	45p
BP702("-\$1.702("	48p	50p	45p
BP702-72702	53p	45p	40p
BP70972709	36p	340	30p
BP709P A709C	360	34p	300
BP71072710	44p	42p	400
BP711-4A711	45p	43p	40p
8P741-72741	75p	60p	50p
µA703€ —µA703€	28p	26p	24p
TAA263-	70p	60p	55p
TAA293	90p	75p	70p
TAA350	170p	158p	150p
S.G.S. FA1000 243			

#### ROCK BOTTOM PRICES LOGIC DTL 930 Series I.C's

Type		Price	
No.	1-24	25-99	100 up
BP930	12p	11p	LOp
BP932	13p	120	119
BP933	13p	12p	Hip
BP935	13p	12p	11p
BP936	13p	12p	Hp
BP944	13p	12p	Hp
BP945	25p	24p	22p
R P946	12p	Hp	10p
BP948	25p	24p	220
BP951	65p	60p	55p
BP962	12p	Hp	10p
BP9093	40p	36p	35p
BP9094	40p	36p	35 p
B P9097	40p	36p	35p
BP9099	40p	36p	35p
Devices may be	r mixed to	o qualif	y for
	Larger qu (DTI 930		prices only).

#### NUMERICAL INDICATOR TUBES



MODEL	CD66	GR116	3015F Minitron
Anode voltage (Vdc)	170min	175min	5
Cathode Current (mA)	2.3	14	8
Numerical Height (mm)	16	13	9 /
Tube Height (mm)	47	32	22
Tube Diameter (mm)	19	13	12 wide
I.C. Driver Rec.	BP41 or 141	BP41 or 141	BP47
PRICE RACH	#1-70	£1-55	#1-90

All indicators 0-9 + Decimal point. All side viewing. Full data for all types available

#### RTL MICROLOGIC CIRCUITS

Price each

Epoxy TO-5 case 1-24 25-99 100 up uL900 Buffer 35p 33p 87p uL914 Dual 21/p 23p 271 uL923 J-K flip-flop 50p 47p 450

Date and Circuits Booklet for Price 7p.

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DUAL-IN-LINE I.C's. PROFESSIONAL & NEW LOW COST. PROF. TYPE No. 1-24 25-99 100up. TSO 14 pin type 80p 27p 25p TSO 16 . . . . 85p 32p 30p

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105mm  $\times$  13mm.

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TRANSFORMER BMT80 £1.95 p. & p. 25p.

#### STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. the PA100 stereo pre-amplifier has been conceived from the latest circuit tecnniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon pianar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.

#### SPECIFICATION

Frequency Response Harmonic Distortion Inputs: 1. Tape Head
2. Radio, Tuner
3. Magnetic P.U. 20Hz - 20KHz  $\pm$  1dB better than 0·1% 1·25 mV into 50K  $\Omega$  35 mV into 50K  $\Omega$  $1\cdot 5$  mV into 50K  $\Omega$ 

All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within  $\pm$  1dB. from 20Hz to 20KHz.

Bass Control Bass Control
Treble Control
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio
Input overload Supply Dimensions

± 16dB at 20Hz ± 15dB at 20Hz ± 15dB at 20KHz 100Hz 8KHz better than - 65dB + 28dB + 26dB + 35 volts at 20mA 292mm × 82mm × ONLY £11 95

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Ref.         VA         Weight         Size cm.         Auto Tops         P & P           No.         (Wotts) Ib oz         6         £         6           113         20         11         7·3 × 4·3 × 4·4 0·115·210·240         0·85 22           64         75         1 14         7·0 × 6·4 × 6·0 0·115·210·240         1·66 32           4         150         3         0·89 × 6·4 × 7·6 0·115·200·220·240         2·00 36           66         300         6         0·10·2 × 10·2 × 9·5          3·89 52           67         500         12         8·14 · 0×10·2 × 11·4           5·78 67           84         1000         16         0·11·4 × 14·0 × 14·0           15·20           93         1500         28         9·13·5 × 14·9 × 16·5          15·20         •           95         2000         40         0·17·8 × 16·5 × 21·6          19·84         •
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PRIMARY 200-250 VOLTS 12 AND/OR 24 VOLT RANGE Ref. Amps. Weight No. 12V 24V 1b oz 111 0-5 0-25 12 7-6 × 57 × 4-4 0-12V at 0-25A × 2 0-85 22 131 1-0 0-5 1 0 83 × 51 × 5-1 0-12V at 0-5A × 2 1-01 22 71 2 1 1 0 7-0 × 64 × 57 0-12V at 0-5A × 2 1-01 22 71 2 1 1 0 7-0 × 64 × 57 0-12V at 0-5A × 2 1-01 22 70 6 3 3 12 10-2 × 76 × 8-6 0-12V at 0-5A × 2 1-01 22 70 6 3 3 12 10-2 × 76 × 8-6 0-12V at 0-5A × 2 1-08 8 4 5 4 10-0 × 8-3 × 8-2 0-12V at 0-5A × 2 1-08 2 72 10 5 6 3 7-9 \( 10 \) 10 0 × 10 × 2 \( 10 \) 10 0 × 10 × 2 \( 10 \) 10 0 × 10 × 2 \( 10 \) 10 1 1 1 3 \( 12 \) 10 1 1 1 4 \( 10 \) 10 1 2 2 2 4 4 4 2 2 4 4 5 2 1 1 1 5 20 10 11 13 \( 12 \) 12 1 1 1 4 \( 10 \) 2 0 1 2 2 2 1 1 1 0 A × 2 \( 10 \) 5 7-8 6 7 18 7 10 5 16 12 \( 13 \) 3 1 2 1 \( 12 \) 1 1 4 \( 14 \) 10 2 0 1 2 2 2 1 10 A × 2 \( 15 \) 7-8 6 7 8 2 226 60 30 34 0 17 0 \( 10 \) 17 0 \( 14 \) 5 \( 12 \) 5 0 12 \( 12 \) 2 2 3 3 \( 12 \) 12 1 2 1 3 3 \( 12 \) 12 1 2 1 0 1 2 2 2 2 3 3 \( 12 \) 10 0 0 1 7 0 \( 14 \) 5 \( 12 \) 5 0 12 \( 12 \) 2 1 3 3 \( 12 \) 1 1 1 2 1 2 1 3 3 \( 12 \) 1 2 1 2 1 0 1 2 2 2 1 3 3 \( 12 \) 1 2 1 2 1 1 1 2 1 3 3 \( 12 \) 1 2 1 2 1 1 1 2 1 3 3 1 2 1 1 2 1 1 1 2 1 1 1 2 1 3 1 2 1 3 1 2 1 1 2 1 1 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3 1 2 1 3
Ref. Amps.         Weight No.         Size cm.         Secondary Tops         P & P & P & P & P & P & P & P & P & P &
Ref. Amps. Weight Size cm. Secondary Taps & P & P & P & P & P & P & P & P & P &
Ref. Amps. Weight Size cm. Secondary Taps & P & P & P & P & P & P & P & P & P &
LEAD ACID BATTERY CHARGER TYPES  Amps. Weight Size cm.   15 0 5  15 0 1 9 7-0 × 6-0 × 6-0  5 4-0 3 11 10-2 × 7-0 × 8-3  6 6-0 5 12 10-2 × 8-9 × 8-3  146 8-0 6 4 8-9 × 10-2 × 10-2  146 8-0 6 4 8-9 × 10-2 × 10-2  146 8-0 6 4 8-9 × 10-2 × 10-2  146 8-0 6 4 8-9 × 10-2 × 10-2  146 8-0 6 4 8-9 × 10-2 × 10-2  147 2 1 1 14 13-3 × 10-8 × 12-1  All ratings are continuous. Standard construction: open with solder tags and wax impregnation. Enclosed styles to order.
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ANTAVOX STEREO LOUDSPEAKER SYSTEM

These high quality speaker enclosures are made of

tough black moulded plastic and have been designed fitting on to almost any vehicle surface. smart lowred fronts are silver trimmed and house heavy duty 5in (125mm) ceramic loudspeakers rated at 3/5 watts. 8 ohms impedance. Already wired with generous length connecting leads and supplied in packs of speaker pairs complete with fixing screws. Each cabinet measures 190 × 105 × 165mm; 0.556m

1052 FADER CONTROL

Neat, custom-made appearance slide fader control for balance of front and rear speaker volume. Simulated wood finish panel which can be quickly fitted below car dash. Supplied with generous connecting cable and fitting screws. Will suit 4, 8, 16 ohm installations.  $100 \times 38 \times 30$ mm (including knob but excluding fitting bracket).



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An extremely modestly priced yet efficient microscope capable of magnification up to 750 times with clear sharp This model is of the selfimages. illuminating type and incorporates an easily rotable four-position turret magnifying lens with rack and pinion focusing. The crackle black metal body houses the batteries for adjustable illumination. Packed in carton with built-in carrying handle and full notes for user. A sample slide also provided. 105mm at base; 180mm high: 0-40kg.

£4.95



#### G5555 PROFESSIONAL STEREO HEADPHONE

Lightweight materials are skilfully used in the construction of this model in black crackle moulding and kid-soft leathercloth with contrasting bright metal. Each ear pad houses a highly efficient 60mm reproducer unit and features ear muffs removable for cleaning. 10 self-coiled lead plugs fitted.

Freq. Response: 20-20,000Hz. Impedance: 4-16 ohms. Sensitivity: 110dB. Power: 0.5W. Weight: 0.39kg.

All for £4.70 "SPRITE" LIGHTWEIGHT STEREO HEADPHONE

An outstanding achievement following lengthy development by one of the world's leading audio manufacturers, the T.T.C. "Sprite" offers the manufacturers, the T following specification:

Extreme lightness (only 150 grammes-5oz); Instant wearing adjustment with sliding earpieces and flexible headband; Highly efficient Mylar reproducer units; Removable, washable foam padded ear muffs;

3 metre lightweight lead with stereo plug fitted Frequency Response: 30–13,000Hz. Sensitivity: 105dB. Impedance: 4–16 ohms. Power: 0-2W. Weight: 0-15kg. 22-25





#### ADASTRA "HI-TEN" 10in LOUDSPEAKER

The British made "Hi-Ten" unit has also had minor improvements of late including an extended top response and a new matt black chassis finish. This range 10in. loudspeaker handles up to 10 watts with convincing all round performance and total reliability. A high flux ceramic moulded magnet keeps the unit compact. An ideal unit for all full range music, audio and monitoring purposes and particularly suitable for column enclosures. Available in 8 or 15 ohm versions.

Frequency Response: 40-13,000Hz. Bass Resonance: 70Hz. Power Handling: 10W. Impedance: 8 and 15 ohms. Flux Density: 10,000 lines. Voice Coil: 25mm (lin.). Baffle Aperture: 228mm (9in). Fixing Centres: 244-5×6-4mm. Dimensions: 255-8×91-9mm. Weight: 0-91kg (21b).

K2006 HORN CONE TWEETER

Neat 3in (75mm) pressure driven tweeter with spun metal cone giving excellent H.F. response with up to 10 watts load. Designed for fitting into a rebate (80mm dia.) with fitting by four corner holes on outer flange. Screws provided. Polarised connections. 8 or 15/16 ohms, impedance matching.

Freq. Resp.: 1,500-16,000Hz. Crossover Freq.: 3,000Hz. Sensitivity: 104dB.



Size: 85 × 85 × 80 mm. Weight: 0-30kg. Impedance: 8 or 16 ohm versions.

K4004 VARIABLE CROSSOVER

Continuously variable from 2,500Hz to infinity and matching any Bass/H.F. unit combination this variable crossover is housed in a two-colour

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SPECIFICATION Power out

 SPECIFICATION

 Power output
 120W into 8 ohms

 Freq. response
 20-20,000Hz ± 2dB

 Input sensitivity
 200mV into 10K

 Construction
 Fibreglass board

 Size
 8in × 4in × 4in (Sin with supply)

 Low distortion parallel
 push-pull output stage.

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Handling the total of 3,000W (3kW) this unit is unique for its price in that not only bass middle and treble but also master controls are provided. Two amplifier sockets eliminate the need for split leads, etc. Supplied in tough white steel case with a blue 219.75 carr. hooded cover. Fully guaranteed.

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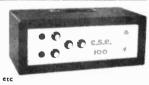
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Two decks, and full headphone monitoring. The unit is mains operated and measures 17½ in × 3 in × 4 in deep and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass, treble, headphone selector and volume, microphone volume, bass, treble, mains on/off. THIS IS A MUST FOR THE HOME BUILT HIGH QUALITY DISCOTHEQUE AND IS COMPARABLE TO UNITS AT OVER TWICE THE PRICE.

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**PS45** 



#### **OUR TRANSISTOR**

This seems a good time to reveal our own secret suspicions concerning the origin of the transistor. We admit that for long we have had an irresistible feeling that this device was in fact conceived with the private constructor expressly in mind. Yes indeed, and plenty of evidence points this way—other important users and impressive applications notwith-standing.

Forget, for a moment or two, those epic moon journeys monitored on colour television. Forget (if you can) those ubiquitous transistor radios. Forget those prodigious computers—and those in-vogue status setting personal appurtenances like pocket calculators and solid state wristwatches. Instead, reflect upon what the transistor has meant to us as private constructors and experimenters. For we as much as any other body of individuals have cause to be jubilant and grateful in respect of that revolutionary technological breakthrough a quarter century ago.

We suggest that if the trio of research physicists at Bell Labs had been working to a specification drawn up with the private constructor's interests foremost in mind, they could hardly have done better. Those readers able to cast their minds back to the pre-transistor days when the valve ruled the roost will certainly be appreciative of the transformation set in train by the solid state amplifying device. It ushered in an era of expansive amateur activities, by bringing within the private individual's reach, literally to his table top, previously undreamed of electronic techniques.

By comparison with the thermionic devices it was going to replace, the transistor when it made its debut seemed so ridiculously simple to handle, so small and undistinguished in appearance, so undemanding in power, as not to be true. Not that there were no headaches for the average constructor and experimenter initially, when trying to get to grips with strange new concepts involving solid state physics, with a little chemistry and metallography thrown in. It was rather a traumatic experience trying to adjust to the transistor's idiosyncrasies. (An h.t. line of minus 6 volts—what nonsense was this? Though we got our potentials right once again when the *npn* version arrived.) First attempts to make practical use of the strange component were accompanied with trepidation, for burnt-out transistors weren't uncommon in those pioneering days.

Seen now in retrospect, these were but little teething troubles. The advantages and rewards arising from the solid state device were soon made apparent. Without the transistor and its descendants amateur activity would never have reached the advanced technical stage, nor have been able to embrace such wide and diverse applications as it does today. Undoubtedly the basic simplicity of construction is the great single factor which has stirred up popular interest in solid state electronics. It is now an ideal sparetime hobby which can be pursued without difficulty in the home.

Yes, constructors and enthusiasts all, there is cause to be exuberant. And don't forget, without the transistor there could hardly be PRACTICAL ELECTRONICS. So we all owe a vote of thanks to Messrs. Bardeen, Brattain, and Shockley. And surely no true enthusiast will dare deny that our suspicions are well founded.—F.E.B.

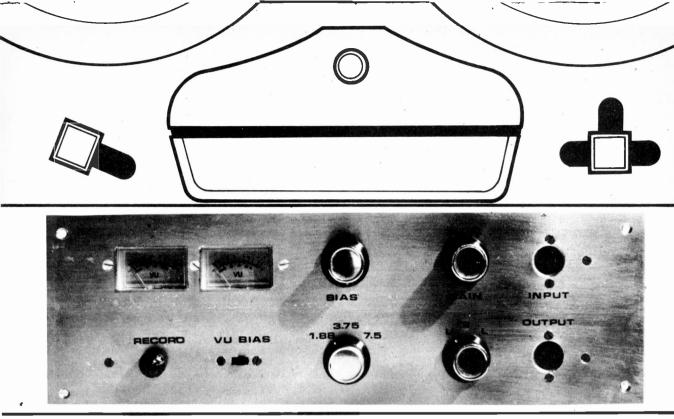
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# Hi-fi Tape Link by P. S. EWER

THERE must be many readers who possess a tape recorder whose quality does not match that of the rest of their hi-fi system and who would like to improve it to save the expense of buying a completely new deck.

This article describes how to convert a reasonable quality deck to hi-fi by renewing the electronics and the heads whilst retaining the original tape transport system. All that is required is a tape deck of reasonable quality, the author using a Collaro Studio. Full constructional details relating to the deck will be given.

Since it is assumed that the constructor will already possess a high quality amplifier, this will not be described. Microphone facilities are not included because in the author's opinion these are best provided by a comprehensive mixer.

#### **OVERALL SYSTEM**

A block diagram of the overall system is shown in Fig. 1. A six-pole three-way switch is used to select either upper track, lower track, or stereo operation (S3). A relay (RLA) is used to control record and playback modes. The relay itself is controlled by an external switch normally fitted to the tape deck. This switch is also used to control the supply to the bias and erase oscillator, which is on in the record position and off in the playback.

in the record position and off in the playback.

A ganged potentiometer (VR6, VR106) controls the gain of the record amplifier which is fed from the input signal via a DIN socket. The output of

the record amplifier is fed via a resistor and the relay contacts to the record/replay heads. It is also fed to the meter circuit which can also be used to read the bias voltage.

The resistor between the record amplifier and the head is used to achieve constant current drive.

In the record mode the relay contacts connect the heads to the record amplifier. The bias oscillator is on and feeds the erase heads. Two 50 kilohm potentiometers (VR7 and VR107) are used to control the bias. When only single track operation is selected then the unused output of the bias oscillator is grounded via a 10 kilohm resistor (R42).

In the playback mode the output of the heads is fed directly to the playback amplifier and then out via another DIN socket.

#### **HEAD REQUIREMENTS**

A tape recorder is only as good as its heads and to achieve the required performance heads of very high calibre are essential.

The characteristics required for the record/replay

1. Low eddy current loss at high frequency so that a high bias frequency can be used both to avoid interference (this being particularly important when recording stereo radio transmissions with its attendant sub-carrier output problems), and to enable the minimum pre-emphasis to be employed.

#### SPECIFICATION . . .

System

Quarter track stereo tape link intended for use in conjunction with a high fidelity system. Features Include two level indicators, adjustable metered bias, and single track mono operation

**Overall Frequency Response** 

7½ i.p.s. 30Hz-17kHz ±1dB 3½ i.p.s. 40Hz-11-5kHz +1, -1-5dB

1 i.p.s. 40Hz-6·5kHz ±2dB

Replay Characteristic

CCIR

70µS 71 i.p.s.

3 i.p.s. 140μS

17 i.p.s. 280µS

45dB Input

Crosstalk

Distortion

1% at 0VU

Signal to noise ratio

55mV r.m.s. to infinity at 10 kilohm

teristic and using low noise tape

Output

1 volt r.m.s. from near zero source impedance. Protected against accidental short circuit

60dB weighted according to the CCIF charac-

A well-engineered gap which is as close as possible to the mechanical gap width. This results in minimal gap losses at short wavelengths.

3. The magnetic core should have a low coercivity to prevent magnetic saturation occurring which would reduce the signal-to-noise ratio and cause second harmonic distortion. This is particularly important at low tape speeds or when using low noise tapes.

On the playback side the important characteristics are:

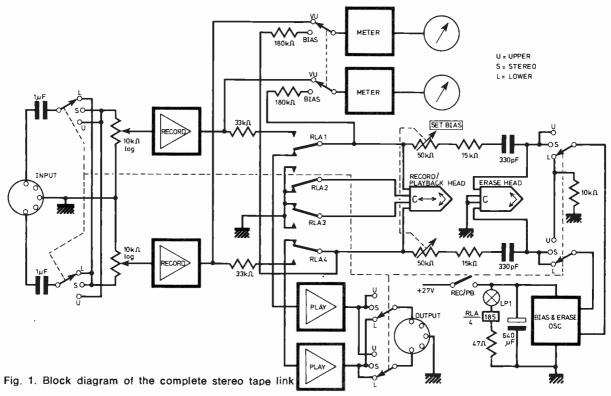
- Low source impedance consistent with a high output, which is required to enhance the signal-tonoise ratio.
- 5. A narrow gap width and a small gap depth.
- 6. A ripple free response at low frequencies.

The erase head should be very efficient, requiring a low input power and so causing minimal damping of the oscillator tuned circuit.

The heads specified for the recorder fulfil these requirements and are manufactured by Wolfgang Bogen of West Berlin. They are obtainable in the U.K. from Cole Electronics Ltd., the sole agents (see Components List for the address).

#### RECORD AMPLIFIER REQUIREMENTS

A recording amplifier raises the level of the input signal to an amplitude suitable for driving the head. It must incorporate pre-emphasis to compensate for the high frequency fall-off inherent in the head to tape characteristic, and provide a constant current output to the head.



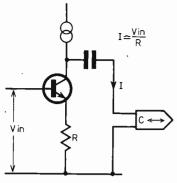


Fig. 2a. Constant current drive using the high output impedance of a transistor collector

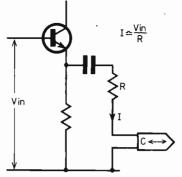


Fig. 2b. Constant current drive using the head in the feedback loop

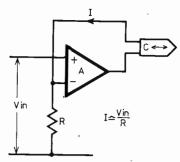


Fig. 2c. Actual method used which uses a series resistor to provide the constant current

Furthermore, even allowing for the full preemphasis required, there should be no overload, and the general distortion figure should be low.

CONSTANT CURRENT DRIVE

Because the record/replay head is an inductor its impedance rises with frequency. Therefore to induce a constant magnetic flux in the tape head the head should be driven from a constant current source. (This is the opposite of the constant voltage drive which requires a low output impedance from the amplifier.)

A high impedance in comparison with that of the head is thus required and there are many ways of

achieving this in practice.

Use can be made of the intrinsically high collector impedance of a transistor, or the head may be included in the feedback loop of an amplifier as shown in Figs. 2a and 2b. Both these approaches give an excellent approximation to the ideal current drive requirements.

However, both systems have the disadvantage of bias rejection problems and the consequent need for tuned circuits in series with the head. As this is considered to be a major drawback, the author has adopted a different method of obtaining this constant current.

#### **METHOD USED**

The basic recording amplifier has a very low output impedance and the record signal is fed to the head via a resistor of a value which is large in comparison with that of the head over the frequency range under consideration.

The bias signal is now attenuated by the resistor and the output impedance of the amplifier (see Fig. 2c).

The penalties to be paid for this solution are: firstly, the departure from accurate current drive (the source impedance is now no longer negligible in comparison with the head impedance); and secondly, the need for a high rail voltage if a reasonable value of series resistor is to be used.

The impedance of the specified Bogen head varies from 170 ohms to a maximum of 10 kilohms. At even the highest tape speed under consideration, the output from the head begins to drop at three kilohertz. Departure from constant current above this frequency can thus be compensated for in the recording pre-emphasis.

A value of 33 kilohms was chosen for the series resistor. Between 20Hz and 3kHz the variation in

#### RECORD AMPLIFIER CIRCUIT

The output required from the amplifier is 10.8 volts peak-to-peak for full modulation of the tape. Allowing for the full pre-emphasis to be utilised and for the saturation losses in the amplifier transistors, a rail voltage of at least 48 volts is required. In fact 55 volts are available thus allowing for a small overload.

the record current is truly negligible, and even up

to 18kHz the drop in current is only 3.7 per cent.

Referring to the circuit diagram (Fig. 3), it will be seen that the circuit is similar in conception to that commonly employed in audio power amplifier decion

Transistor TR1 forms a low noise input stage and has a gain of 4.5 times. TR2 is the workhorse of the amplifier. It has a boot-strapped collector load for high gain with low distortion due to the limited modulation index of the collector current, and forms the driver for the output stage.

Transistors TR3 and TR4 comprise the output stage which operates in class A, a requirement for low distortion when a large output is required.

The amplifier has good linearity even before feedback, and this, coupled with the high gain and hence large amount of allowable feedback, serves to reduce distortion to a very low level.

The overall loop gain at d.c. is unity giving exceptional stability of the mid-rail voltage. Components R5, R6, and C9 provide a.c. feedback, and the frequency response for the different speeds is shaped by L1 in conjunction with C5, C6, or C7, the frequency of maximum treble boost being switched according to the speed in use, and the amount being preset by the series resistors VR1 to VR3.

The nominal gain is approximately 70 and this gives an input sensitivity in the region of 55mV. C11 is a phase shifting capacitor required to give stability by preventing high frequency oscillation.

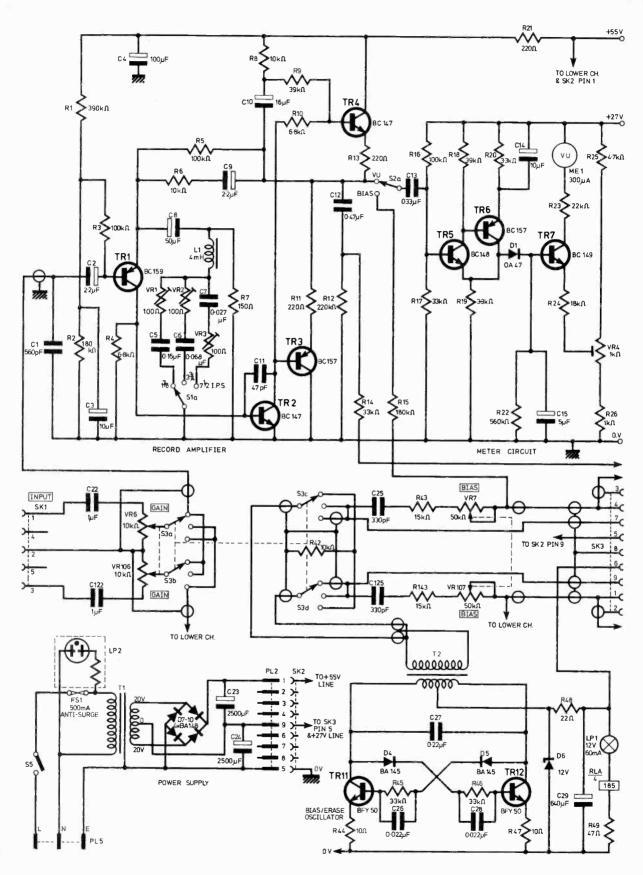
#### METERING CIRCUIT

It is the author's opinion that average reading meters of the volume unit (VU) variety allow short duration overloads to occur without any indication. The recording meters in this recorder are therefore of the peak reading kind having a fast attack, and a slow decay time of about 2.5 seconds.

This reduces the effect of meter movement inertia, for the pointer generally has less far to travel to

### COMPONENTS ...

Resistors			Inductors
R1, R101	390kΩ R26, R126	1kΩ	T1 20V-0-20V ½A (R.S. 20V Rectifier)
R2, R102	180kΩ <b>R27</b>	5.6kΩ	T2 Bias transformer \ (see next month for
R3, R103	100kΩ R28	1·2kΩ	L1, L101 4mH (2 off) fdetails)
R4, R104 R5, R105	6.8k $\Omega$ R29, R129 100k $\Omega$ R30, R130		
R6, R106	10kΩ R31, R131		Usada
R7, R107	150 Ω R32, R132	2·2kΩ	Heads EH1 Bogen erase head type UL296
R8, R108	10kΩ R33, R133	56 Ω	RPH1 Bogen universal head type UK207E
R9, R109	39k $\Omega$ R34, R134		
R10, R110			(These are available from Cole Electronics Ltd., 7-15 Lansdowne Road, Croydon CR9 2HB and
R11, R111	220Ω R36	270Ω 30kΩ	Brenell Engineering Co. Ltd., 231/5 Liverpool Road,
R12, R112 R13, R113			London, N.1 who also market a tape deck incorporat-
R14, R114			ing these heads).
R15, R115			
R16, R116	100kΩ R41, R141	10kΩ	
R17, R117		10kΩ	Transistors
R18, R118		15kΩ ½W 5%	TR1, TR101 BC159
R19, R119		10Ω ½W 2%	TR2, TR102 BC147
R20, R120 R21		3·3kΩ 3.3kΩ	TR3, TR103 BC157 TR4, TR104 BC147
R22, R122		3⋅3kΩ 10Ω ⅓W 2%	TR5, TR105 BC148
R23, R123		22 Ω 5W 5% wirewound	TR6, TR106 BC157
R24, R124		47Ω ½W 10%	TR7, TR107 BC149
R25, R125	4·7kΩ	_	TR8 BC158
AII 4W 5%	6 carbon film histab	unless otherwise	TR9, TR109 2N3823
	off of each except	R21, R27, R28, R42	TR10, TR110 BC159
and R44-	-R49		TR11, TR12 BFY50 All 2 off except TR8
			7 th 2 of choops tho
Capacitors	500 - F I 4		Diodes
C1, C101	560pF polystyrene		D1, D101 OA47 (2 off)
C2, C102 C3, C103	2·2μF 25V Tantalum 10μF 25V Tantalum		D2 BZY88C 27V 400mW Zener
C4, C104	100μF 64V elect.		D3 BZY88C 20V 400mW Zener
C5, C105	0·15μF 5% polyester	7	D4, D5 BA145 (2 off)
C6, C106	0.068µF 5% polyeste	er	D6 12V 1.5W Zener
C7, C107	0.027μF 5% polyeste	er	D7-D10 BA148 or 1N4002 (4 off)
C0 C400	(use 0.022μF and 0.	005μF in parallel)	, , , , , , , , , , , , , , , , , , , ,
C8, C108 C9, C109	50μF 25V elect. 2·2μF 25V Tantalum	n'	Integrated Circuit
	16μF 40V elect.	1	IC1, IC101 SN72741P or 741OPA (2 off)
	47pF 10% polystyre	ne	
	0·47μF polyester		Relay
C13, C113	0⋅33μF polyester		RLA 12V 185 $\Omega$ 4 changeover contacts (ITT)
C14, C114	10μF 10V Tantalum		••
	5μF 10V Tantalum 50μF 16V Tantalum		Meters
	2·2μF 16V Tantalum		ME1, ME101 VU meters. Sensitivity 1.228V a.c.
	0·1μF polyester		for 0dB (300μA) (2 off)
C19, C119	1,800pF 2% polystyr	ene	
	50μF 25V elect.		Switches S1 A pale 3 years (B.S. priminture Make a witch)
C21 C22, C122	50μF 40V elect.		S1 4 pole 3 way (R.S. miniature Maka-switch) S2 2 pole changeover miniature slide
C23, C24	1μF polyester 2,500μF 40V elect.		S3 6 pole 3 way (R.S. miniature Maka-switch)
C25, C125	330pF ceramic		S4 see text
C26	0.022 µF 10% polyes	ter	
C27	0.22μF 10% polyeste	er	Miscellaneous
C28	0.022μF 10% polyes	ter	SK1 5 pin 180° DIN socket
C29	640μF 25V elect. except C21 and C26-	C20	SK2, SK3 B9A valveholder (2 off)
2 on each	except C21 and C20-	-C29	SK4 5 pin 180° DIN socket
D - 4	4		PL2, PL3 B9A plug (2 off)
Potentiome			PL4 Mains plug Bulgin type P429
VR1, VR10	/1 /2 ≻100Ω preset (R.S.	Mouldtrim) (6 off)	LP1 12V 0.75W lamp and holder LP2 Mains neon with integral resistor
VR3, VR10		. modiașiini) (0 oii)	LP2 Mains neon with integral resistor 9½in × 5in 0⋅1in matrix plain Veroboard
VR4, VR10	$M^{T}$ 1k $\Omega$ submin skele	eton preset (2 off)	16 s.w.g. aluminium for chassis (see Pt. 2 for
VR5, VR10	)5 4·7kΩ submin ske	eleton preset (2 off)	dimensions), TO5 clip-on heatsinks (2 off),
VR6, VR10	6 $10 \mathrm{k}\Omega + 10 \mathrm{k}\Omega$ log	ganged pot	plastic cable clips (2 off), capacitor clips (2 off),
VR7, VR10	$07$ $50$ k $\Omega+50$ k $\Omega$ lin	ganged pot	21, 30 and 34 s.w.g. enamelled copper wire



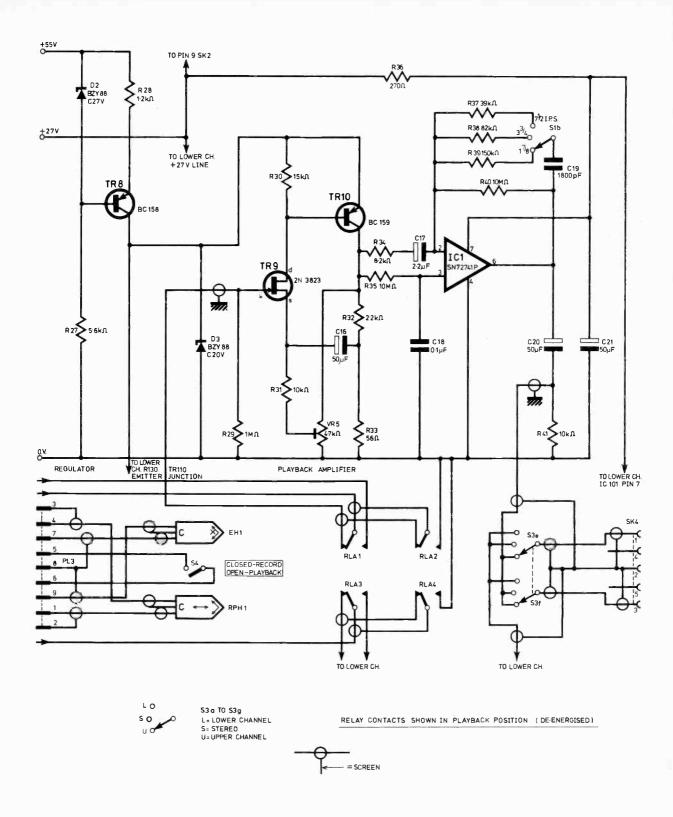


Fig. 3. Full circuit diagram of the stereo tape link. Only the upper channel has been shown; the lower channel electronics being identical to the upper channel. Components numbers of the lower channel are upper channel numbers plus 100

indicate a transient, and is easier for the eye to follow.

Referring now to the circuit diagram, transistors TR5 and TR6 comprise a unity gain voltage follower

having a very low output impedance.

The metering signal is rectified by diode D1 and stored in C15. Because of the low impedance of the voltage follower the major limitation on the charging time of C15 is the forward resistance of the diode which is a gold-bonded germanium type.

The discharge time is governed by the combination of the reverse resistance of the diode, R22 and the

input impedance of TR7.

In the absence of an input signal the base of TR7 is at 6.7 volts. Preset VR4 is set so that TR7 is just cut off and hence no current flows through the meter. As the signal input increases the charge on C15 increases positively hence forward biasing TR7. Resistor R23 provides the meter with overload protection.

#### **BIAS AND ERASE OSCILLATOR**

A very pure bias waveform is needed if the full dynamic range of the tape is to be realised. Also, due to the dependence of frequency response, output level, distortion and modulation noise on the bias amplitude, the oscillator amplitude should be drift free.

Push-pull operation is used to minimise even harmonic distortion and the rail voltage is regulated to ensure amplitude stability of the waveform.

So that adequate filtering of the oscillator harmonic output is assured, the tuned circuit must have a high working Q. This is achieved by the employment of a low impedance tuned circuit wound with thick wire on a low loss high permeability pot core. The tuning capacitor should have low dielectric losses as well.

The transistors are protected against reverse breakdown of their base emitter junctions by diodes D4 and D5. Although this breakdown does not interfere with the operation of the oscillator, it can, after a period of time, cause reduction in the current gain of the transistors.

Zener diode D6 regulates the voltage supplied to 12 volts. The bias is arranged to decay slowly by discharging C29 when switching off from record. This is essential if magnetisation of the heads is to be avoided.

In practice, the oscillator works well. The output rises by 0.25dB over the first minute of operation and is thereafter stable. The waveform is good, as indicated by the inaudible change in the tape noise after virgin tape has been passed by the erase head. It is important when performing this test to pull the tape away from the record head as this will record modulation noise. Modulation noise is inherent in all biased recorders and can be reduced only by the use of low noise tapes and careful design of the heads.

#### REPLAY AMPLIFIER

The output of the record/replay head when playing a tape rises at the rate of 6dB per octave (i.e. it doubles for every doubling of frequency) up to the point at which high frequency fall-off occurs.

The replay amplifier compensates for this characteristic, and provides a high level output signal suitable for feeding long screened cables.

When considering the connection of the head to the amplifier it is important that no appreciable direct current flows through it, as this would result in magnetisation of the head, and a consequent increase in the background hiss of the tape. It is thus inadvisable to couple the head via a capacitor as the charging current for it will pass through the head.

#### F.E.T. INPUT STAGE

The use of a field effect transistor as an input device allows direct connection of the head. Because of the very high input impedance of the f.e.t. it requires only a miniscule bias current (about 2nA) which is insufficient to affect the head. Compared to a bipolar transistor the f.e.t. also possesses a generally lower noise and distortion level.

The f.e.t. and TR10 comprise a complementary feedback pair operating at a gain of 50 from an input signal of 2.7mV at 1kHz and at  $7\frac{1}{2}$  inches per second. This stage has a flat frequency response. The f.e.t. has a considerable spread in the gate to source bias voltage for a given drain current, being anywhere from 0.5 to 7.5 volts. It is not easy to design away this variation, and a preset resistor (VR5) has therefore been provided for setting-up.

#### SUPPLY RIPPLE REDUCTION

An interesting feature of the input stage is the method of supply ripple reduction. Transistor TR8 is biased as a current source. Zener diode D2 maintains the base-emitter potential constant in the presence of ripple on the 55 volt line, reducing modulation of the collector current,

The high source impedance of the current combined with the low slope resistance of the Zener diode D3 attenuates the ripple to a negligible level.

#### **EQUALISATION**

The function of equalisation is left to the last stage, thus resulting in lower noise levels, and greater accuracy of equalisation which, if carried out earlier could cause variations in the input impedance.

The general purpose operational amplifier type 741 is the equaliser and output stage and is eminently suitable for this application. Because of its high gain and low output impedance it is capable of producing very accurate equalisation. It has its own internal frequency compensation for stability and its output is short circuit protected.

The d.c. source impedances of the inverting and non-inverting inputs are similar and the d.c. gain of the stage is set to unity to minimise drift of the quiescent output voltage with temperature.

The equalisation components R37-39 and C19 are selected according to the speed in use and set to the CCIR standards of 70, 140 and 280 microseconds.

#### **POWER SUPPLY**

The power supply is quite simple, providing two outputs of 55 volts and 27 volts. Full wave rectification and large value reservoir capacitors are employed to produce good supply regulation and low output ripple.

In the second part of this article, next month, construction of the Hi-Fi Tape Link will be described

#### ARE WE ALONE?

From time to time the question of other living entities, whether they be elementary forms or whether equivalent to homo sapiens or better, is revived. Over the past year or so the climate of acceptability has improved in these matters and there are less sceptics each year.

While all science fiction has been treated as having license in this direction, examination tends to show that in our galaxy, at least, the chances of bug-eyed monsters or intelligent vegetations being our companions is losing ground. In general all the findings so far point to a cycle of emergence to the present level of homo sapiens as the most likely, though minor variations could occur.

At the present state of knowledge the evidence is in favour of similar forms of life to that which exists now. This being the case the field is narrowed quite considerably and statistically it is known that there is a high possibility of life existing elsewhere, but the possibility of communication presents a major problem.

From several sources recently there have come new suggestions for contacting other intelligences. Some are based on the concept that if there are fundamental laws governing the matter, they would be the same for all. The use of mathematical constants and the geometric forms regarded as fundamental, is a natural step.

#### **ECHOES FROM SPACE?**

There have been two recent suggestions, one which relates to a cyclic condition of the movements of heavenly bodies and one which is based on the problem of long time echoes of known broadcasts.

The first of these suggestions involves the possibility of near approaches to the solar system by stars which might have a planetary system. Statistics show that there is a quite frequent approach to within 50 light years of the solar system.

A second line put forward is based on the phenomenon of echoes, first noted by Störmer and Van der Pol in 1928. While they appeared to be curious and puzzling at that time this is not really the case now.

However, renewed interest has been aroused by D. Lunan, who has studied available data over a long period and has offered certain suggestions as to the reason for the echoes.

One of the suggestions is that the echoes behave as though they were reflected from a point at or near the orbit of the moon. He has constructed maps which are very similar to the star maps of the northern hemisphere and suggests that the star Epsilon Boötes might



be the source from which a probe has been dispatched.

The probe may be in orbit and attempting to make earth beings aware of its existence by re-transmitting broadcasts. It is also suggested that the probe may have arrived in the solar system about 11,000 years ago.

Perhaps all the evidence has not been released but the matter was given considerable discussion at a meeting of the Interplanetary Society.

The echoes are both long-time, that is years, and short-time, that is 3 to 15 seconds and it is the latter that Lunan has investigated.

It is easier to offer an alternative for this suggestion because the periods are short enough to avoid the complication of dissipation of power. A short time of three seconds could be a direct reflection from the earth's other moon that has so frequently been postulated or even from the moon itself over a long path.

However, for both of the extremes of timing there is a simple answer which involves the model of the ionosphere that was considered satisfactory for a long time. This was a layer type model like the successive skins of an onion.

The ionosphere in fact is not a bit like that and not only are there now many doubts about propagation theories that have been held for so long, but the layer theory disappeared with the advent of Sputnik 1. In this connection there is much evidence that indicates that there is no homogenity about these layers at all.

Moreover, there is considerable variation in the density of the northern and southern hemispheres. This variation of density in the layers has a considerable effect on

the length of reflection paths. It is, therefore, possible for a signal to go round the earth several times before emerging at a particular angle that could be recorded as an echo.

It would be possible to expand on the Lunan theory, but suffice to say that the answer to the appearance of regular patterns can only come from a specific attempt to make a practical test of Lunan's work. It is in fact an experiment that could be undertaken by amateurs and perhaps here is an opportunity for UFO supporters to produce some practical answers to their claims.

#### USSR RESEARCH

As a result of finding amino acids in the Murchison meteorite the Russians have been carrying out further experiments on meteorites that have fallen in the past. They concluded — so state academicians Vinogradov and Vdovykin — that there is evidence for the chemical evolution of life.

They also state that it is not necessary for there to be special fortuitous circumstances for this to come about; in short, life could evolve anywhere where there is a dust accretion in the galaxy. This has been deduced from an examination of the Mighei meteorite which fell in the Ukraine in 1889.

The Murchison meteorite revealed amino acids and the Mighei meteorite shows an acid which is similar to *DNA* but has a spiral which is symmetrical. From this fact they conclude that it is not of biological derivation.

#### CRAB NEBULA AGAIN

The crab nebula has been much in the news of late. The original noting of this supanova by the Chinese astronomer Yang Wei-Tek was on July 4, 1054. Little other record of this occurrence is found in literature though it must have been an event of considerable note.

However. in 1955 W. C. Miller

However. in 1955 W. C. Miller discovered evidence that the North American Indians had recorded the event. Pictures were found showing the crescent moon with the nova nearby. This was thought to be a unique record and the date was confirmed as July 5, 1054.

Recently another discovery was made at Fern Cave in California. This cave was occupied at the time of the event in 1054 and so could be depicting an event during the formation of the settlement. The timing has been checked by four investigators and though no absolute claim for identification is made it seems unlikely that it records any other event.

The fact that the nova was more brilliant than Venus must have made it an outstanding sight.





#### SENSE OF SMELL

Apropos of our discussion some months back, relating to "sniffing", it seems that someone else has latched on to the idea of recruiting bugs to serve as extensions to our probosci. This time it's some form (goodness knows what) of marine bacteria which come as a packagedeal for detecting the smells associated with just about anything from bombs to pineapples.

These wonderful little "critters" can, I gather, be trained (presumably in the good old Pavlovian way) to glow whenever they sense or come in contact with a material of one's choosing. It is then simply a matter of detecting this light with a photocell (photomultiplier?) to identify the type of smell. Unlike previous attempts to make bugs useful in the role of an olfactory sense, this way would appear to be far more flexible.

The particular application to which this artificial nose might show some real worth ultimately is tele-olfaction.

Using this new way to sense smell at a distance ought not to be too difficult, but may be complicated by the fact that odours do not seem to be represented to us in the same way that, say, colour is; to wit, it is not simply a question of discovering primary odours then combining them to produce "hues" (or phews!).

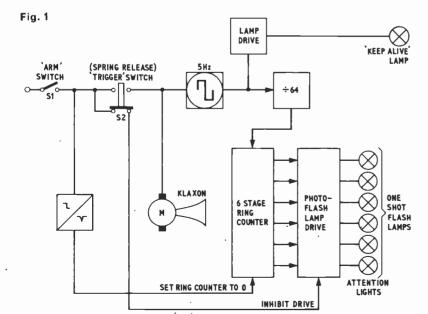
No doubt, the limitation would be

No doubt, the limitation would be on the number of trained bacteria packages one could incorporate in a transducer, since each package would only respond to a particular smell. Assuming a compromise could be accepted at around one hundred or so packages, that is one package for each of the more common smells, then by fanning air over the device, sequential interrogation of the bacterias' photocells would classify both type and amplitude of odour.

This, though, is only part way to the ultimate in communication. There still needs to be a method for reproducing the "pong" from the transducer output waveform. This should be a simpler job because, following receipt of this signal, it might then be decoded within the receiver and the resultant employed to address a corresponding set of control valves, so releasing the correct aromatic. As an alternative, heaters could be arranged to vapourise the material.

Whether there should be a delay between different signals is a moot point; naturally, it would not be the best of schemes to follow one smell by another when the chance existed that they might clash or produce some offensive "mixture".

Honestly, imagine one of these things going wrong. There is little doubt that TV servicemen would suddenly find new uses for the humble pair of bull-nosed pliers!



#### SHOCK THE VILLAINS

.Mugging, and the crop of pensioner-bashing cases we have witnessed lately must be distasteful to anyone with a sense of respect for their fellows. For a while now I have considered a number of possibilities for beating this, very real, public menace, but it is not something to be easily reckoned with.

Anyhow, having contacted the Chief Constable for my area and



discovered that, "no, you were not permitted to use portable high-voltage equipment with a view to shocking the villians into sub-mission", the only effective alternative seemed to be a notion based on the word "shock". The best deterrent thus appeared to be one that could attract a lot of attention to one's predicament by others in the vicinity of the incident.

An electronic device to meet our requirements generally needs to have quite bulky proportions, so probably the best "noise-maker" would be a small klaxon employing a miniature electric motor, this driving a coarse-pitch gear pinion bearing directly against a piece of bent metal (certainly noisier than any loud-speaker of twice the size). The metal "noise-maker" could be carved out of the lower part of a handheld lamp case the upper portion utilised for being photo-flash attention lamps.

This kind of alternative, at least, should come within the limits of the law and Fig. 1 gives the general picture of how such a set-up would function.

Two switches control the device. The "arm" switch (preferably concealed) connects a supply battery preparatory to possible operation. Simultaneously, photo-flash lamp drive is inhibited while a "set" pulse is fed to a six-stage ring counter whose outputs all go to logical "0".

Release of the spring-return "trigger" switch starts the klaxon and also causes the clock generator to run. In turn, a (deliberately over-run) "keep-alive" lamp rapidly flashes while the divider counts down the signal from the clock. Thus, every 13 or so seconds, the ring counter will be advanced one step and so fire (one at a time) the photo-flash lamps.

Naturally, the device ought not to be too inelegant physically, but should be of sufficient size to prevent any feeble-minded body-vandal shoving it in a convenient Gladstone bag!

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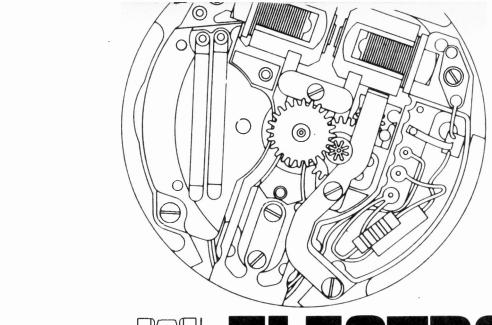
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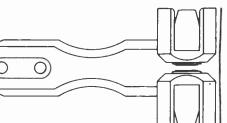
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# ELECTROMIC TIMEPIECES

### By JB **DANCE** M.sc.

Most watches and small clocks being manufactured at the present time still employ a mainspring as the source of power and a balance wheel plus hair spring as the timing mechanism. The basic design of such timepieces has remained essentially unaltered since Huygens developed the balance wheel mechanism in the 17th Century.

#### RECENT PROGRESS

The first battery powered wrist watch was marketed in 1952, but recent developments in micro-miniature integrated circuits have enabled high quality electronic watches to be produced which are much more accurate than the more common types of watch. Most of the quartz crystal controlled watches show an accuracy of about one minute per year.

Electronic watches do not have a spring which requires winding periodically, but their miniature battery must be replaced about once per year. Smaller movements suitable for ladies' watches are becoming available, but considerable problems arise in designing watches which can be powered by miniature mercury cells which must have the minimum acceptable life of one year.

#### **TYPES**

Some of the main types of electronic watches can be classified in the following way. Many variations of these main types are available.

First generation watches employ a conventional balance wheel and hair spring as the timing mechanism, but they are powered by a battery instead of

a main spring. They have the advantage that they do not have to be wound, but their accuracy is not generally so much greater than that of a conventional watch.

Second generation watches employ a tuning fork mechanism operating at about 300-500Hz as the timing device; a transistor circuit drives the tuning fork. Such watches have an accuracy of about one minute per month, this being considerably better than that of an ordinary watch. Tuning fork watches do not tick, but emit a slight hum.

Third generation watches employ a quartz crystal oscillator which normally operates at a frequency of between about 8kHz and 33kHz; most types have an accuracy of about one minute per year. The pulses from the quartz crystal are used to control the speed of a motor which drives the hands of the watch. Various techniques are employed to accomplish this.

Fourth generation watches do not employ hands to indicate the time, but incorporate a digital display which shows the time in actual figures. These watches have no moving parts and are completely electronic. They employ a quartz crystal oscillator and have an accuracy of about one minute per year. They are only just becoming available.

#### **PRICES**

Unfortunately the price of electronic watches is still quite high. The price of many watches is increased because a gold case is employed.

In the case of stainless steel cased watches, one finds tuning fork models ranging from just under

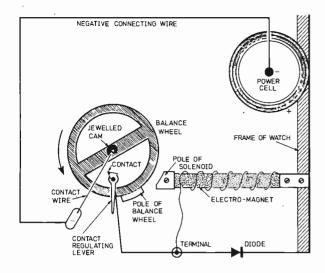


Fig. 1. The circuit diagram of the first electric watch

£40 upwards, with the smaller ladies' watches rather more expensive. The quartz crystal controlled watches are generally priced from about £100 upwards, but some of the watches providing a digital display are not so much more expensive than other quartz crystal controlled watches.

It seems fairly certain that the prices of electronic watches will fall during the next few years. The components of all electronic digital watches can be mass produced and assembled by relatively unskilled personnel. This will effect a great saving in labour costs at a time when the general trend is for labour costs to rise rapidly and integrated circuit production costs to fall—especially if large numbers are produced. Thus it seems we are experiencing a revolution in watch design.

Although one has the annual cost of the power cell replacement (typically £1), most electronic watches do not require servicing so frequently as ordinary watches. The forces in the transmission gearing are usually less than in conventional watches and therefore satisfactory functioning is almost independent of the increase of viscosity of the oil with time. In general the regular cleaning and preventative maintenance recommended for balance wheel watches are unnecessary with most electronic types; one only has the watch attended to if it stops or does not keep time with its normal accuracy.

#### **CLOCKS**

Electronic clocks are also available with either a digital display or with the analogue display provided by ordinary hands. Many electronic clocks are quartz crystal controlled and provide an accuracy of about one minute per year. Both battery powered and mains types are available.

Some of the main types of electronic timepieces will now be considered in reasonable detail. The development of electronic clocks has followed a rather similar pattern to that of watches (although the problems of size are not nearly so acute) and therefore clocks and watches will be discussed together

#### THE FIRST ELECTRIC WRIST WATCH

The first battery driven wrist watch was developed by the French Company LIP in collaboration with the Elgin Company of the U.S.A. This watch was introduced into the LIP range on 15th March 1952, but the same type of movement is still being produced by this Company. The Hamilton Company introduced a similar type of movement very shortly after the LIP watch became available.

Although this type of watch is electric rather than electronic, it will nevertheless be discussed, since it led to the development of some electronic types and has been described as the greatest advance in watch design for some centuries. The same basic principle has also been used in clocks manufactured by the Hamilton, Vedette, Bayard and Odo Companies.

#### PRINCIPLE OF OPERATION

The principle of operation of the LIP type R.148 movement is shown in Fig. 1. The R.184 is similar, but it also indicates the date.

As the balance wheel rotates in an anticlockwise direction, the jewelled cam on the balance wheel pivot pushes the contact wire onto the contact. A current then flows from the power cell through the electro-magnet and the contacts and back to the cell. The energising of the electro-magnet at the instant the pole of the balance wheel is approaching the pole of the magnet causes the two poles to be attracted together so that the balance wheel is given an impulse.

The balance wheel continues to rotate after the contact has been made and the wire returns to its normal position. When the balance wheel swings in the opposite direction, the cam merely pushes the contact wire away from the contact and the magnet is not energised. The electro-magnet passes a current which increases to about 1mA over a period of 3 milliseconds and then the current falls rapidly to zero. The current pulses occur every 0.4s. For simplicity a magnetic shunt employed in this type of watch is not shown in Fig. 1.

#### **SPARK SUPPRESSION DIODE**

A diode is connected in parallel with the electromagnet. When the contacts are joined little current flows through this diode, since the potential across the electro-magnet reverse biases the diode. When the contacts break, however, the current ceases to flow through the electro-magnet and a back e.m.f. is developed across the latter, owing to its inductance. The diode shorts out this back e.m.f. and thus prevents damage to the delicate contacts by sparking.

The cam illustrated in Fig. 1 consists of a jewel. The amplitude of the balance wheel oscillations can be controlled by adjusting the contact regulating lever; the latter rotates the contact arm on its axis.

The amplitude of the oscillations of the balance wheel remains fairly constant and this results in the watch keeping more accurate time than many watches which are powered by a main spring. There is some negative feedback, since if the amplitude of oscillation decreases, the contact time is increased and this provides more power which helps to stabilise the amplitude of oscillation.

The mean current taken from the 1.55V cell is normally  $5\mu$ A, but does not exceed  $7\mu$ A. A 100mA-hour battery therefore has a life of some 15 to 18 months.

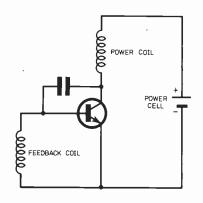
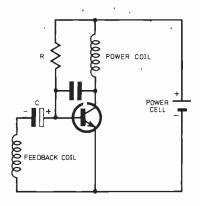


Fig. 2 (left). A circuit which can be used to drive the balance wheel of a watch

Fig. 3 (right). A circuit used in some self-starting watches and clocks for driving the balance wheel



#### ELECTRONIC WATCHES WITH A BALANCE WHEEL

The main problem with the type of electric watch just described is that the contacts must be very carefully designed and positioned if they are to have a reasonable life. In any case, the contact life tends to be limited.

The work of Marius Lovet of France has led to the development of electronic watches with balance wheels in which the switching is carried out by a transistor.

The balance wheel of such electronic timepieces carries small permanent magnets which move near to two coils—a feedback coil and a power coil. The currents induced in the feedback coil by the movement of the balance wheel magnets drive the transistor into conduction so that the power coil receives a pulse. The magnetic field developed by this coil acts on the magnets to give the balance wheel a driving pulse.

#### CIRCUIT

The type of circuit shown in Fig. 2 may be used in timepieces which employ an electronically driven balance wheel. If the latter is stationary, the base and emitter are at the same potential and therefore the collector current is extremely small.

When a magnet of the balance wheel moves past the feedback coil, however, the voltage induced in this coil causes the transistor to conduct. A current therefore flows in the power coil and an impulse is produced which powers the balance wheel. The pulse duration is typically 10 milliseconds. Spurious oscillations of the circuit can be suppressed by connecting a capacitor between the base and collector of the transistor. The resistance of the coils may be a few hundred to a few thousand ohms.

One of the disadvantages of this type of circuit is that the balance wheel does not commence to oscillate automatically. The watch must be rotated to start it. This difficulty can be avoided by connecting a resistor of about 100 to 200 kilohms in the base circuit (as shown in Fig. 3) so that a very small current flows in the base and collector circuit even when the balance wheel is stationary.

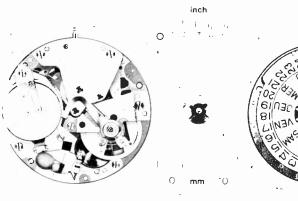
The current flowing through the power coil interacts with the magnets of the balance wheel and causes the latter to move. The minute oscillations are built up by transistor action until the normal amplitude of vibration is reached.

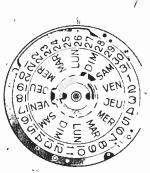
Although a current flows through the circuit continuously, this current can be eliminated by connecting an electrolytic capacitor in series with the feedback coil (as shown in Fig. 3).

Contactless circuits of this general type are widely employed in some of the more economical types of electronic watch. For example, the LIP movement type RE.50 (introduced in 1970) was the first electronic watch for ladies available anywhere in the world. Much of the internal volume is occupied by the 1.55V, 60mA-hour cell which is 7.9mm in diameter. One finds similar circuits in the 9154 "Dynotron" movement produced by Ebauches S.A.

The Swissonic 10 electronically driven balance wheel movement. The magnets can be seen fixed to the balance wheel and the power coil under the balance wheel. The first three letters of the days of the week are shown in French

The Nepro Elevox watch which incorporates an electronic alarm





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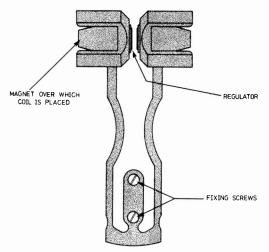


Fig. 4. The miniature tuning fork used in the Bulova 214 series of "Accutron" models

(a large group of Swiss watch manufacturers), in the Junghans 600.12 self starting wrist watch produced in Germany, etc.

Electronic clocks employing this type of movement are produced by Junghans (type ATO-MAT-WERK 726); the mean current consumption is less than 160µA at 1.4V or a total of less than 1.5A-hour per year. Similar types of clock are produced by the Jaz Company.

#### **ELECTRONIC ALARMS**

The first wrist watches with electronic alarm systems were introduced by the Nepro Company of Switzerland in 1972 after five years of development work. Although watches which have an alarm powered by a spring are available, the stored energy is rather small and this results in the intensity of sound being low and the duration limited. In addition, the alarm spring must be wound each time the alarm is used.

The Nepro watches employ a 1.5V battery of 40mA-hour capacity to power their wrist watch alarms. The current is about 8 to 12mA and the battery has a life of about a year with normal use. The alarms of these watches sound for five minutes unless cancelled by a push button.

#### **ALARM MODELS**

One type of wrist watch with an alarm produced by Nepro is the "Memotron". A vibrating membrane generates the sound in the MB 500 alarm system contained in this watch. This is the smallest electronic alarm in production, having a volume of only 0.8 cubic centimetres.

Watches using this type of alarm can be used to remind a person of appointments throughout the day and can therefore be used for many purposes for which normal alarm clocks are unsuitable. The Nepro Company also produce a range of very small alarm clocks with battery powered alarms.

#### TUNING FORK WATCHES

The first tuning fork movement was announced by the Bulova Company on 25th October 1960. This watch, which was the result of six years of research by Dr Hezel of Bulova, represented a real revolution

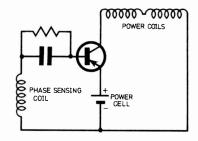


Fig. 5. The circuit of the Bulova 214 series of "Accutron" watches

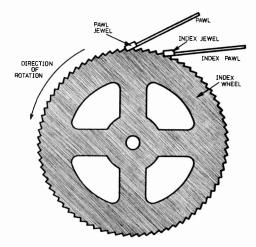


Fig. 6. The pawl mechanism used in the Bulova "Accutron" watches for converting the tuning fork vibrations into a rotary motion

in watch design. It was the first watch to employ an electronic mechanism and the first to use a timing mechanism not based on the balance wheel. In addition, it was the first watch to be delivered to the purchaser with a written guarantee of its time keeping accuracy; this is  $\pm 1$  minute per month.

The frequency of operation of the tuning fork watches made by Bulova for men is 360Hz. The mechanical loss of energy has been reduced to a very low level and this enables the low power consumption of about 8µW to be obtained. The tuning fork mechanism is relatively insensitive to shock.

The tuning fork employed in the Bulova 214 series is shown in Fig. 4. It is made of a special alloy which is little affected by changes of temperature. A strong conical magnet and a magnetic cup are fitted to each prong of the tuning fork.

A coil is fitted over each magnet. The coils must be fixed in position so that they are very close to the vibrating magnets but never touch them. The coils have a total of about 16,000 turns, comprising about 200 metres of insulated copper wire of diameter 0.015mm. About one quarter of the number of turns on the one coil is used for feedback purposes.

#### CIRCUIT

The circuit of the 214 series of Bulova watches is shown in Fig. 5. It consists of a simple transistor oscillator with a feedback coil (or "phase sensing

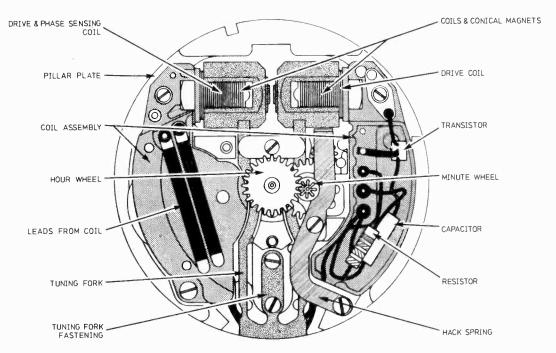


Fig. 7. The inside of a Bulova 214 series "Accutron" watch

coil") and two power coils. Indeed, it is basically very similar to the circuits of Figs. 2 and 3 which drive balance wheel watches.

The alternating voltages induced in the phase sensing coil are applied (via the battery and capacitor) to the base-emitter junction of the transistor. This diode junction rectifies these voltages and the capacitor is charged with such a polarity that the voltage across it opposes the power cell voltage.

The resistor in parallel with the capacitor allows the charge of the latter to leak away slowly so that a small pulse of current flows each time the voltage across the phase sensing coil is near to its maximum value and at a time when the polarity of the voltage induced in the power coils opposes that of the power cell.

If the total voltage induced in the power coils at the instant the transistor conducts were exactly equal to the cell voltage, no current would flow through them. At the correct amplitude of vibration, the voltage induced across the power coils at a time when the transistor conducts is about 10 per cent less than the cell voltage. A 10 per cent increase in the amplitude of vibration would therefore result in the current pulses to the power coils becoming zero and the amplitude would then quickly fall to its correct value. Similarly, a 10 per cent decrease in the amplitude would raise the current through the power coils to double its normal value and return the amplitude quickly to normal.

#### TRANSLATING THE VIBRATIONS

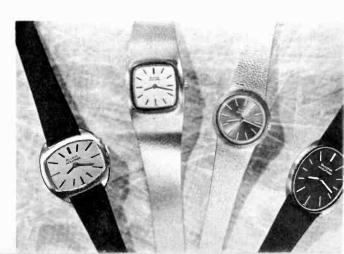
The vibrations of the tuning fork are converted into rotary motion by means of the rachet and pawl mechanism shown in Fig. 6. Attached to one arm of the tuning fork is a straight spring (the "index") tipped with a tiny jewel which engages ratchet teeth on an index wheel. The wheel advances one tooth for each complete vibration of the tuning fork. A

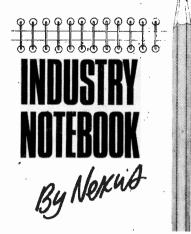
pawl holds the index wheel in position during the return stroke of the index jewel. Although the index wheel is only 2.4mm in diameter and 0.04mm in thickness, it has 300 teeth spaced at 0.025mm intervals. The index wheel drives a gear train which turns the hands of the watch.

The rate of rotation of the index wheel is unaffected by any normal changes in the amplitude of vibration of the tuning fork. The index wheel will move one tooth per vibration of the tuning fork when the index jewel moves any distance between just over one and just under three times the distance between adjacent teeth. If the index wheel moves a distance just over the distance between successive teeth, the pawl jewel will push it back during the time the index jewel returns; the net movement is then one tooth.

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Four small Accutron watches for ladies, using a tuning fork movement





#### YEAR OF THE HYBRID

This could be the year of the hybrid microcircuit. Thick film technology has made enormous strides through development of special inks for printing resistive networks, plenty of chip capacitors and active devices are available and potting techniques have also had their share of improvement. The result is a neat module of high reliability which has become extremely attractive to equipment manufacturers.

The manager of the very active hybrid microcircuit division of Welwyn Electric, Brian Attwood, tells me that although Welwyn started research on thin films some seven years ago and reached a high degree of perfection, the less expensive thick film technology has now reached the stage where it can do all the jobs of thin film. Welwyn are now fully concentrated in the thick film area with a plant capacity capable of handling £1 million worth of circuits a year, although he admits that actual production has not yet reached this figure.

Welwyn is engaged in the high technology end of the business with as many as a couple of dozen components in a single package. At any one time some 60 different circuits are going through the plant and some 500 types of circuits, all custom built by Welwyn, are in field service.

Also bidding for a big share of the hybrid market but in the higher volume area is Newmarket Transistors Ltd., a member of the Pye Group.

Two recently announced products are a low level audio amplifier, the performance of which can be adjusted as required by external components or links, and a self-contained hearing aid amplifier.

The company states that thick film hybrids have now reached a

stage where costs are becoming appreciably lower than discrete assemblies. So confident is Newmarket that they are inviting users of circuits using discrete components to send details to the Newmarket design team who will then evaluate it in hybrid terms free of charge and submit a quotation for supplies.

tion for supplies.
Yet another firm spreading itswings with hybrids is Coutant Electronics, best known as a supplier
of power supply units. Coutant
started a thick film facility for inhouse use manufacturing mainly
encapsulated voltage regulators
and over voltage protection units.
Now the company is offering a full
design and manufacturing service
to allcomers.

### POLLUTION MEASUREMENT

The big investment in design of pollution measurement equipment by Plessey looks as if it may be starting to pay off. The company's water quality monitoring equipment came through a four-month evaluation at the Water Pollution Research Laboratory, Stevenage, with flying colours and installations are now operating with the Sussex, Lancashire and Trent River Authorities. Orders have been taken from similar authorities in Sweden, Italy and France, the forerunners of a profitable export trade.

Another notable order, although valued only at £20,000 is for an environmental monitoring system at Lovisa, Finland, where that country's first nuclear power station is scheduled to come into operation in 1975. The Plessey installation measures meteorological, hydrographic and water quality data at the outfall of the station's water cooling system. A total of 38 separate parameters are automatically monitored and the resulting data should prove extremely valuable even before the station comes into operation.

### PROFESSIONAL COMPONENTS FOR THE AMATEUR

SDS Components at Portsmouth have opened a retail shop for the home constructor at their premises at Gunstore Road, Hilsea Trading Estate. This is not the first time a wholly professional supplier has turned to the amateur market for extra revenue and it will be interesting to see if the project fares better than some earlier attempts elsewhere which, in the end, proved uneconomic.

Many famous names are listed in the product list which can be obtained by sending 20p to SDS Components Ltd. Tim Curtis, managing director of SDS, says that he intends to break down the barriers between the amateur fraternity and industrial manufacturers.

#### NEW OUTLET FOR EVR

Electronic Video Recording — EVR — has been slow in market development but good business could result from its use at sea. Most ships now have TV for the use of the crew when in port and in coastal waters. In fact Marconi Marine has supplied more than 4,000 multi-standard receivers to vessels of all types.

Ships' crews are just like their shore-based counterparts and like to have TV on tap all the time. Hence the interest in EVR which will allow the TV to keep entertaining from video telecartridges when out of normal reception range.

Marconi Marine has entered an agreement with Telmar Programme Service for the supply of recorded programmes on the EVR film cartridge system which is manufactured at Basildon, Essex. The cartridges each give two 30-minute monochrome programmes or one 30-minute colour programme.

Many thousands of recorded programmes are available and ships will be able to exchange programmes at ports throughout the world. The playing units are manufactured by a number of companies under licence from the EVR partnership of ICI and CIBAGEIGY.

### RACAL AND THE YOUNGER MAN

Chairman and managing director of Racal Electronics, Ernest Harrison, believes in youth. He likes to spot likely managers early in life and then give them the opportunity to show what they can do.

Some recent promotions prove the point. Keith Thrower who heads up a newly-formed Advanced Development Team has made big progress on the engineering side. He now has a top job at the age of 38. David Elsbury, 36, has climbed the ladder to become managing director of Racal Mobil-cal Ltd., one of the most profitable of all Racal companies and the one that recently booked the largest ever contract for the company valued at \$1.8 million.

Two other youngsters who now have top jobs are Gerry Smith, heading up Racal's Singapore office, and Jim Diggins, who joined Racal at the age of 25 and is now managing director of Racal Communications Ltd.

Harrison told me that in general successful people need to be "well seen" before they are 30 years old. Very few good people, he says, ever leave the company because promotion prospects are good.





#### THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts R M S continuous.

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

LOAD IMPEDANCE: 4—16 ohms.
INPUT IMPEDANCE: 30K ohms at 1KHz.

VOLTAGE GAIN: 30db at 1KHz

at 1KHz FREQUENCY RESPONSE: 5Hz-50KHz + 1db

SUPPLY VOLTAGE: ± 22 5volts D.C. SUPPLY CURRENT: 0.8 amps maximum

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

#### UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection.

Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it

to be run off any unregulated power supply from 16-25 Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo pre-amplifier

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

Magnetic Pick-up (within ±1db RIAA curve)

2mV. 47K  $\Omega$ Tape Replay (external components to suit

head), 4mV,  $47K\Omega$ Microphone (flat) 10mV,  $47K\Omega$ Microphone (that) fum. 47k $_{\odot}$  (Ceramic Pick-up (equalized and satable) 20–2000mV, variable. Tunner (flat) 250mV, 100K  $_{\odot}$  Auxiliary 1 250mV, 47K $_{\odot}$  Auxiliary 2 2–20mV, 100K  $_{\odot}$ (equalized and compen-

#### OUTPUTS

Main Pre-amp output 500mV. Direct tape output 120mV

ACTIVE TONE CONTROLS (Bexendall) Treble + 12db. Bass + 12db.

INTERNAL STABILIZATION

Enables the HY5 to share an unregulated supply with the Power Amplifier.

SUPPLY VOLTAGE 16-25 volts

MONO: £3.60

SUPPLY CURRENT 6mA approx OVERLOAD CAPABILITY better than 26db on most sensitive input infinite on tuner and auxl. OUTPUT NOISE VOLTAGE: 0.5mV.

IP HY5





#### POWER SUPPLY PSU45

The versatile P.S.U.45 is designed to supply your HY41's ±HY5's in stereo or mono format.

#### Specification

Input: 200–240 Volts.
Output: ± 22.5 Volts at 2 amps.
Overall Dimensions: L. 7"; D. 3.8"; H. 3.1"

PRICE: £4.50 inc. P. & P.

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High stability, low noise, carbon film resistors. Tubular miniature, high power resistors.

Power	_		Values	Price	
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+	5%	2·2~10M Ω	E12	İp	0.8p
I	5%	2-2-10M Ω	E12	2 _D	1.5p
4	10%	$I-10M \Omega$	Fi2	án	

Quantity prices available for any selection. Ignore fractions on total

#### CAPACITORS

Electrolytics, general purpose, miniature, axial lead. Mullard O15, O16, O17 series.

lmf	63V	6р	22mf	63V	6р
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2-2mf	63V	6p	I00mf	40V	6p
3·3mf	63V	6p	150mf	25V	6p
4·7mf	63V	6p	220mf	25V	Hip
6·8mf	63V	6p	470mf	25V	13p
10mf	63V	6p	680mf	25V	20p
15mf	63V	6р	100mf	25V	25 p

#### POLYESTER FILM CAPACITORS Mullard C296 series. 400V d.c.

Mullard C296 series. 400V d.c. mf: 0:001, 0:0015, 0:0022, 0:0033, 0:0047, 0:0068, 0:01, 0:015, 0:022,

price 21p. mf: 0.033, 0.047, 0.068, 0.1, price 4p.

mf: 0-15, price 6p. mf: 0-15, price 6p. mf: 0-22, price 7p. mf: 0-33, price 10p. mf: 0-47, price 13p.

160V d.c.

mf: 0·1, 0·15, price 4p; 0·22, price 5p; 0·33, price 6p; 0·47, price 7p; 0·68, price 10p; 1·0, price 13p, Mullard 80 series P.C. mountings. 400V d.c. mf: 0·018, 0·015, 0·022, price 3p; 0·033, 0·047, price 4p.

mf: 0.068, 0.1, 0.15, price 4p.

mf: 0-22, 0-33, price 5p. mf: 0-47, price 7p; 0-68, price 10p; 1-0, price 11p.

CERAMIC DISC CAPACITORS
Working voltage 50V d.c., Plaquette body with 25in leads.
Range: 22pf-10,000pf, price 2p.

#### **POTENTIOMETERS**

Carbon track, IK-2m, log or linear, single gang, price 12p; 5K-2m, log or linear, dual gang, price 37p; 5K, 2m, log or linear, single gang with switch, 24p. Knobs for above 10p.

SLIDER POTENTIOMETERS Single 10K, 25K, 50K, 100K, log or linear, 31p. Dual gang, 10K plus 10K, etc., above values log or linear, 50p. Knobs for above @ 10p.

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Horizontal or vertical mountings, 0.25W, miniature, price 54p.

#### **VEROBOARDS**

	0.1	-15		0.1	0-15
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2∮in × 3∄in	22p	lép	17in × 2±in	75p	574p
2∮in × 5in	24p	24p	17in × 5in (pla	in) —	82p
3∄in × 3∄in	34p	24p	17in × 3∄in (pl	ain) —	60p
3∄in × 5in	27p	27 p	17in × 2‡in (pl		42p
Pins insertion t	ool, 52p. S	pot face	cutter, 42p. Pkt	s. of 50 pir	ns. both
sizes. 20p.					

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## SILVER JUBILEE

### THE FIRST TRANSISTOR

#### THE TEAM

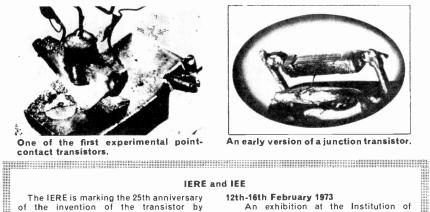
original transistor device was demonstrated in public for the first time on June 30, 1948, at Bell Telephone Laboratories' New York premises. This was the pointcontact transistor, invented by two physicists, John Bardeen and Walter Brattain, who had been researching into solid state materials. They formed part of a Bell Laboratories team led by William Shockley.

A few months following the successful experiment that resulted in the first practical solid state amplifying device. Shockley set out to formulate a theory to explain transistor action. He proposed, in fact, the junction transistor structure. This theory was later developed in practice and the junction transistor became the very successful successor to the pointcontact transistor and the was obsolete by about 1956.

A whole new field of semiconduction technology sprang from the exploitation of the pn junction. as originally proposed by Shockley. An amazing range of devices have been developed through the application of the pn junction principle. where conduction is performed through minority as well as majority current carriers-holes and electrons.

William Shockley was responsible for proposing the four layer pnpn device, which led to silicon controlled rectifier the (thyristor), and also for a different class of unipolar devices, based upon the field effect. These inventions followed within a few years of the junction transistor.

For their outstanding contributions to transistor physics. John Walter Brattain. Bardeen. William Shockley were awarded the 1956 Nobel Prize in Physics.





The IERE is marking the 25th anniversary of the invention of the transistor by devoting a specially enlarged issue of its Journal—The Radio and Electronic Engineer—to a unique collection of nearly 20 papers on semiconducting subjects contributed by leading British scientists and engineers who have worked in this field during the past quarter of a century.

This Transistor Issue of the Radio and Electronic Engineer which is dated January-February 1973, may be obtained from the IERE Publications Sales Department, 9 Bedford Square, London WC1B 3RG, price £2:00 per copy, post free.

To celebrate this silver Jubilee, the Institute of Electrical Engineers, in conjunction with the Institution of Electronic and Radio Engineers, has arranged a number of events which will take place between the 12 and 16 February 1973.

12th-16th February 1973

An exhibition at the Institution of Electronic transistor to complex integrated circuits.

13th February 1973 10.00 a.m.

A colloquium "The 25th anniversary of the Transistor" at the Royal Society.

14th February 1973 5.30 p.m.

A lecture by Dr William Shockley "The invention of the transistor: an example of creative-failure methodology" at the IEE.

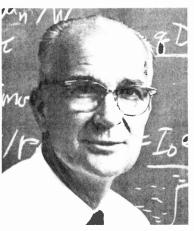
15th February 1973 10.30 a.m.

A half-day discussion meeting "What next in semiconductors" at the IEE.

15th February 1973 10.30 a.m.

A lecture by Dr W. E. J. Farvis "The influence of the transistor in our society and economy" at the IEE. of the invention of the transistor by

An exhibition at the Institution of



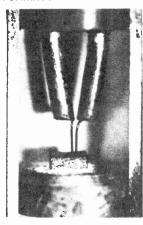
#### DR WILLIAM SHOCKLEY

Dr W. Shockley was born in London of American parents on February 13, 1910. Reared in California, he received his B.Sc. degree at the California Institute of Technology in 1932 and his Ph.D at the Massachusetts Institute of Technology in 1936. He joined Bell Telephone Laboratories in 1936. During the war he served as Director of Research for the U.S. Navy. Afterwards he returned to Bell and became director of the solid state physics research programme which saw the development of early junction transistors.

In 1963 Dr Shockley was named the first Alexander M. Poniatoff Professor of Engineering Science at Stamford University. He has received numerous awards for scientific achievement and public service, and serves on many top level Advisory Committees in the United States. Dr Shockley has contributed over one hundred articles to scientific journals, and more than 70 U.S. Patents have been granted for his inventions.

★Dr William Shockley is to lecture at the I.E.E. in London on February 14.

An early production version of the point-contact transistor.





#### FROM RECTIFYING CONTACTS TO PN JUNCTIONS

STARTINGLY new and revolutionary technical device rarely appears simply out of the blue. The invention or discovery is generally a culminant achievement by a research worker who has followed in the train of a number of earlier researchers and experimenters.

Experience suggests that requisite conditions for a momentous breakthrough are (1) a sufficiently advanced state of theoretical knowledge, (2) a large demand or potential need for a particular kind of device and (3) a sufficiently sophisticated technology capable of undertaking development and then quantity production of some innovation.

Amplification of electric currents is an essential part of electronics. The idea of a solid state amplifier had been a vision in the minds of many scientists and experimenters for many years before the triumph

of 25 years ago.

As beneficiaries of the electronic wonder of the century, it is appropriate for us to look back and try to pick out some of those stepping stones that formed a path, no matter how faint and discontinuous, which led to the ultimate success of Messrs. Bardeen, Bratain, and Shockley.

#### **EARLY INVESTIGATIONS**

With some justification we can identify the commencement of the trail to the transistor with Michael Faraday, who in 1833 recorded the non-linear characteristics of certain conductors of electricity. He found that silver sulphide had a negative temperature coefficient.

In 1873 Willoughby Smith discovered that light affected the resistance of crystalline selenium.

In 1876 Adams and Day observed non-linear conduction phenomena on light-sensitive selenium cells.

(A fascinating light beam wireless communication system was created by the American experimenter and inventor Alexander Graham Bell (1847-1922). Speech was transmitted some distance in space by modulating a light beam and then received upon a selenium element, which produced an electrical out-

put corresponding to the speech input.)

The earliest detailed investigation of the rectifying effect of dis-similar materials in contact, was carried out by the Austrian physicist Braun around 1874. Braun explored a variety of crystals, but mainly lead and ferrous sulphide, and used a base electrode and wire as a point-contact. He observed that the resistance was dependent upon the polarity of the applied voltage, as well as on the nature and condition of the contact surfaces. Braun likened this phenomena to the conduction between closely spaced electrodes in a gas.

Braun also appears to have been the first to observe the rectification effect produced by selenium.

Like many pioneers, Braun had his critics and his discoveries did not gain immediate recognition.

#### POINT-CONTACT RECTIFIERS

Point-contact rectifiers were first put to practical use as signal detectors in the early days of wireless, around 1904. Natural lead sulphide was commonly used. During the mid-1920's the crystal detector was finally ousted from radio receivers by the thermionic valve.

#### PLATE RECTIFIERS

Plate or "metal" rectifiers consist of thin semiconducting layers with metallic electrodes on either side. Cuprous oxide and selenium are the two most important materials that have been widely used.

The rectification effect of contacts between metals and cuprous oxide was already known to Braun. The first useful device appears to have been made

by Grondahl in 1920.

The cuprous oxide rectifier was used on a large scale for power rectification and for use in measuring instruments, from the mid-1920's to the late 1930's. Then it began to be replaced by the selenium rectifier which offered many advantages.

The selenium photocell was widely used during the

period 1930-40.

#### **NEW CONCEPTS**

Investigation into the properties of semiconducting materials appears to have received a great impetus in the 1930's. One important new concept was the "hole", introduced by A. H. Wilson in 1931 when formulating the transport theory of semiconductors based on the band theory of solids.

But the mechanism by which the widely used metal-semiconductor rectifiers ("metal" rectifiers) operated was not clearly understood. One theory that received general acceptance was based on the Schottky effect (1938), a concept similar to the ideas put forward to explain thermionic emission. According to Schottky, cold emission or field emission is produced by the application of a few volts across a thin film of semiconducting material (the copperoxide coating); and this is due to stable space charges in the semiconductor alone, without the presence of a chemical layer.

Also during the same period N. F. Mott offered a theory for swept-out metal semiconductor contacts

which is known as the Mott Barrier.

In 1938 Helsch and Pohl published an account of a solid-state amplifier. This consisted of a single crystal of potassium bromide with a single wire of platinum providing control of current through the crystal. No practical developments resulted.

#### WAR-TIME ADVANCES

The invention of radar just before the second World War stimulated a new interest in the solid state rectifier as a detector of microwaves. And so the silicon point-contact detector was developed.

During the 1940's the technique of crystal "doping" was introduced. Boron added to highly purified silicon was found to result in highly sensitive crystals. This arose from experiment and the theory behind

this effect could not then be explained.

This was a very significant period for the future of solid state. For one thing, the requirement for improved detectors for operation at centimetric wavelengths led to an intensive search for new materials. The discovery of germanium was one direct result of this activity.

#### POINT-CONTACT TRANSISTOR

Shortly after the war, Bardeen, Brattain, and Shockley were involved in research on copper oxide rectifiers. Bardeen showed that a Schottky barrier layer could exist at the free surface of a semiconductor. This layer makes the contact properties independent of thermionic work functions. Following upon this, Bardeen and Brattain initiated the series of experiments that led to the invention of the point-contact transistor.

They placed two point-contacts close together on the surface of a crystal. It was found that a current flowing through one could influence the current flowing through the second circuit. The first practical solid state amplifying device had arrived. This was

December 1947.

In working out the basic mechanism involved in point-contact transistors, Bardeen discovered the carrier-injection phenomena. This injection of extra current carriers into the semiconductor in the region of contact when forward bias voltage is applied produces the "transistor" action.

Later, Shockley carried out a research experiment to diagnose the surface phenomena of the original transistor. In the process, he found he had devised a new type of transistor. This was patented as the junction transistor. An account of this important discovery was published in 1949. Within a few years the pn junction device was to prove vastly superior to the point-contact device, both from manufacturing and application view points.

It is of interest to note that around the mid 1930's Shockley had instigated some research into copper oxide rectifiers in an attempt to invent a solid state

amplifying device. The results were negative.

#### DIFFERENT MECHANISMS

The rectifying properties of metal-semiconductor contacts are due to a different mechanism to that now understood to be responsible in the case of pn

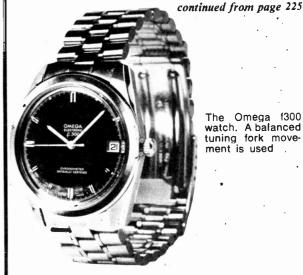
junctions.

During the last decade, the metal-semiconductor type of contact has returned to favour, albeit with new materials, and it has assumed a new prominence in special devices such as field effect or metal oxide semiconductor transistors (m.o.s.t.), and Schottky barrier diodes used for microwave purposes. The m.o.s. technique is extensively used in integrated circuit manufacture.

Thus it seems the circle has been completed. Development of the pn junction has stimulated further widespread research into solid state physics over these last 25 years, and a new interest has arisen in the rectifying phenomena which was the starting point of this "trail to the transistor". And so more devices seem likely to be developed in the future which make use of both mechanisms of current

transport.

#### ELECTRONIC TIMEPIECES



The Omega f300 watch. A balanced tuning fork movement is used

Regulation of the watch is effected by moving either of the small regulator plates which are attached to the ends of each side of the tuning fork. This makes an extremely minute change in the effective length of the fork. An adjustment of half a second per day can be made.

An interior view of the mechanism of the Bulova

214 series watches is shown in Fig. 7.

#### MODELS

The Bulova tuning fork watches are known by the name "Accutron", a word derived from "accuracy" and "electronics". In 1970 this Company introduced the first Accutron watches for ladies (series 230). These employ a power cell of the same size as that used in Accutron watches for men, but the frequency of the electronically driven tuning fork is 480Hz so that the movement can be made far smaller. The shape and construction of the tuning fork is different from that in the models for men, but the current consumption remains at 8-10µA.

A few other companies now offer tuning fork watches. Longines offer the Ebauches caliber 6312 "Mosaba" movement in their "Ultronic" watches. (Mosaba is a word derived from "Movement sans balance"). Baume and Mercier have given the name "Tronosonic" to their tuning fork watches, whilst Omega refers to such watches as "f300". Bulova also produce clocks with tuning fork mechanisms.

#### **GRAVITATIONAL EFFECTS**

The frequency of some types of tuning fork watches is dependent on their position owing to the pull of gravity on the prongs of the fork. When the prongs (or "tines") point downwards, the watch may run a few seconds per day faster than when the prongs are horizontal.

This disadvantage has been almost eliminated in the balanced Mosaba movement designed by Ebauches S.A. It operates at 300Hz and is marketed as the Swissonic 100 range by Longines in their "Ultronic". The Omega "f300" range also employs a balanced tuning fork movement.

Next month the final article will look at, among other things, quartz, cybernetic and digital watches.

# PE Sound Synthesiser G. D. SHAW

F the modular concept outlined last month, is to be followed in its entirety, this implies that not only must each circuit be entirely self contained but also that each circuit, complete with its various controls, should be capable of operating as a separate entity either within, or external to, the framework of the synthesiser as a whole.

These factors, coupled with the experience gained in building the prototype, contributed towards a decision to redesign the instrument into a fully modular form based on one of the many commercially available racking systems.

This month modifications to a standard racking system will be described together with constructional details of the twin stabilised power unit that will supply the various synthesiser card modules.

#### CHOICE OF RACKING SYSTEM

It was believed that, in the interests of economy, the Card Frame System 1 by Vero offered the greatest value. Utilisation of this particular system, however, means that the constructor will be obliged to manufacture his own modular inserts which may perhaps be a deterrent to those not having the facilities or experience to tackle sheet metal fabrication. In this case the modular racking system type 3E also by Vero has the advantage that it covers a range of components which may be easily assembled into modular inserts.

This latter system is extremely well designed and the component parts of the assemblies are precision made, these factors, naturally enough, being reflected in the price of the 3E System which is several times

greater than that of System 1.

Fig. 2.1 shows a general view of the assembly of the card frame to be used as the mainframe of the synthesiser chassis. The aluminium end plates are already pre-drilled to suit the standard Vero components normally used in the assembly of a System 1 Card Frame. It will be necessary, however, to provide additional holes to allow for modifications to the standard assembly and to provide mounting facilities for a number of components. Drilling details are shown.

#### MAINTAINING A TIGHT ASSEMBLY

The slotted card support sections are made of plastic and are secured to the end plates by means of

self tapping screws. Repeated removal and replacement of these screws will result in wearing of the threads which will, in turn, make the assembly sloppy. It is suggested therefore that assembly of the mainframe is only attempted when all necessary drillings, etc. have been completed, and that, once assembled, it is left so. If the constructor wishes, for any reason, to have the facility of stripping the assembly down repeatedly he would be well advised to redrill the securing screw holes and tap them to take a suitably sized metallic thread insert.

#### COMPONENTS ...

#### RACKING SYSTEM

#### Card Frame

Kit of parts for a System 1 Card Frame with a pair of guide mouldings to suit (Part No. CFMN/1)

SK7-SK13 8 pin McMurdo sockets (Part No. RS8) (7 off)

PL1-PL7 8 pin McMurdo plugs (Part No. RP8) (7 off)

Frame parts above available from Vero Electronics Ltd., Industrial Estate, Chandler's Ford, Eastleigh, Hants., SO5 3ZR

#### **MODULE FRONT PANELS**

Fig. 2.2 shows the composite front panel layout with dimensions. It will be seen that the panel is divided vertically into eight separate sections. These sections represent the front panels of individual modular units and, with the exception of the strip on the extreme right of the panel, can be removed from the mainframe complete with their respective card supports and circuitry.

The right hand strip is permanently fixed to the

mainframe by two small aluminium brackets.

The left-hand panel is slightly wider than the remainder mainly to act as "fill-in" on the full width of the front panel.

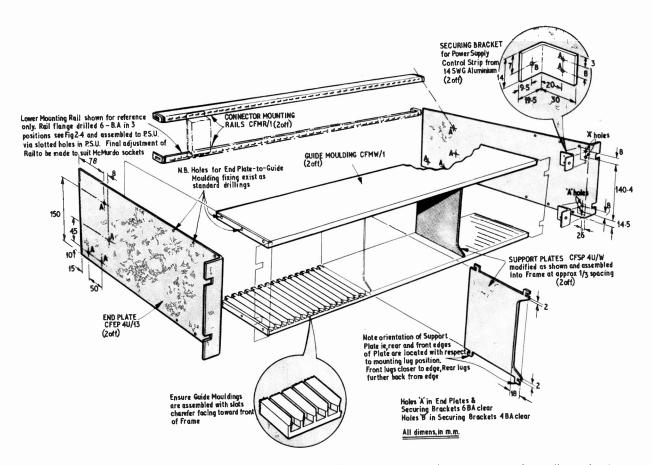


Fig. 2.1. Perspective view of the Card Frame System 1. The end slots on the upper mounting rail require to be elongated for future adjustment of McMurdo sockets

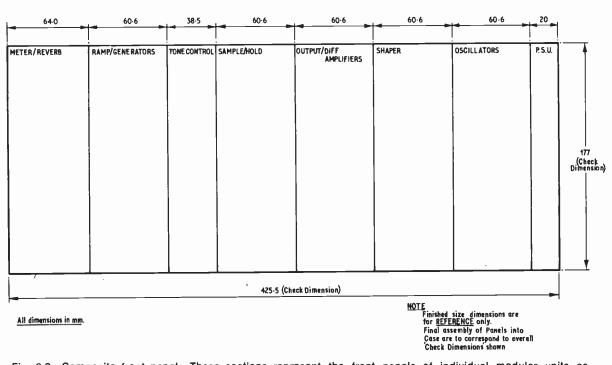


Fig. 2.2. Composite front panel. These sections represent the front panels of individual modular units as indicated

Fig. 2.3a. Drilling and bending details for circuit board support plate and McMurdo plug (b) details of retaining rod

#### MODULE SUPPORT PLATE

Circuit boards are supported on a plate to one end of which is attached the module front panel and to the other end a plug which mates with a socket at the rear of the mainframe assembly. Fig. 2.3a shows details of this support plate. Care should be taken in bending this item and the bends should be made as 156 tightly as possible. Lack of attention to this point will mean that the overall depth of the plate is greater than specified with the result that the front panel, when attached, will not be flush with the card support moulding in the main frame.

Modules are retained in the main frame by means of a  $^{2}_{16}$  in (4.5mm) rod, Fig. 2.3b, screwed 2B.A. at one end, which passes through the front panel and engages with a Rosan bush, or similar, in the power supply subframe. This arrangement also provides a means whereby the module may be withdrawn from the main frame and, for this purpose, a locking collar is provided to abut the lower lug on the circuit board support plate.

### 83-5* FRONT RP8 McMurdo RCUIT BOARD SUPPORT 14SWG Aluminium MODULE LOCKING 2 Holes 'X' 6BA clear 8 Holes 'B' 6BA clear & c/sunk 1 Hole 'C' 4BA clear 2 Holes 'D' 2BA clear (a) 3mm (1/g) dia socket he grub screws and Rod 4.5mm(3%) dia recessed to suit Threaded 2 B 247 From Aluminium or Dural

Dimensions shown thus are for reference only and are to be marked from Componen

#### P.S.U. SUB-FRAME ASSEMBLY

Fig. 2.4 shows the bending and drilling details of the power supply sub-frame. As with the circuit board support plate care should be taken that the clamping and bending is carried out as shown and that the bends are made as tightly as possible. Details have not been provided about the positioning of holes for Rosan bushes or components within the sub-frame.

#### **POWER SUPPLY UNIT**

In a project of this kind the predictability of circuit performance depends largely on the ability of the power supply to maintain its voltage rails within relatively close limits. This is particularly true where the oscillators and hold circuits are concerned since quite small variations in supply rail voltage can cause significant changes in the low frequency and "droop" characteristics respectively.

The power supply unit is based on one of the latest regulator i.e.s to appear from Fairchild, the  $\mu$ A7815: This particular device is capable of passing up to 1.5 amps without the necessity of external series regulating transistors, thus it is operating well within its maximum capability. Output ripple and noise is around 500 microvolts or less while load

regulation from zero to 400mA is better than 1 per cent. (Total current requirement for the basic synthesiser is 400mA per rail.)

The output voltage of the i.c. is specified as being plus or minus 5 per cent of its nominal rated voltage thus the constructor may find up to 1.5 volts variation across the two power supply rails. This is not necessarily a disadvantage since all the voltage dividers in the synthesiser which require an accurately set voltage are fitted with presets.

#### CIRCUIT

The circuit diagram of the power supply unit is shown in Fig. 2.5.

Construction is perfectly straightforward (see Fig. 2.6) the only recommendation being that the leads from the transformer to the bridge rectifiers be routed to avoid passing directly over the regulators and that they be twisted together in the interests of hum reduction.

Wires carrying a.c. to the power supply control strip on the front panel should pass through holes drilled in the rear of the sub-frame and fitted with rubber grommets. These leads should be 10in (254mm) in length measured from the rear face of the sub-frame.

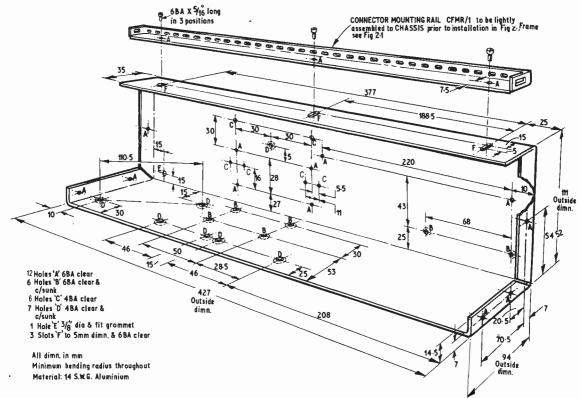


Fig. 2.4. Bending and drilling details of the p.s.u. sub-frame

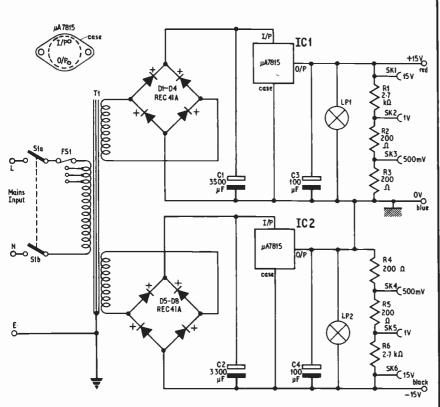


Fig. 2.5. Circuit diagram of twin stabilised p.s.u.

#### COMPONENTS . . .

### TWIN STABILISED P.S.U. Resistors P1 2.7k O R2-R5 200 (2 off

R1  $2.7k\Omega$  R2-R5  $200\Omega$  (2 off)

R6 2·7kΩ

All 2% ½ watt metal oxide

#### Capacitors

C1–C2 3,300μF 63V High ripple elect. (2 off)

C3-C4 100µF 25V elect. (2 off)

#### **Bridge Rectifiers**

D1-D8 REc 41 A (2 off)

#### **Integrated Circuits**

IC1-IC2 μA 7815 (Fairchild) Macro Marketing Ltd., 396 Bath Rd., Slough, Bucks.

#### Transformer

T1—Main transformer, primary 240V; secondary 30–0--30V at 1.5A

#### Miscellaneous

S1—Miniature double pole, single throw on/off switch

LP1-LP2 miniature 28V filament lamps,

FS1-500mA fuse,

SK1-SK6 1mm miniature sockets (6 off)

14 s.w.g. aluminium as required

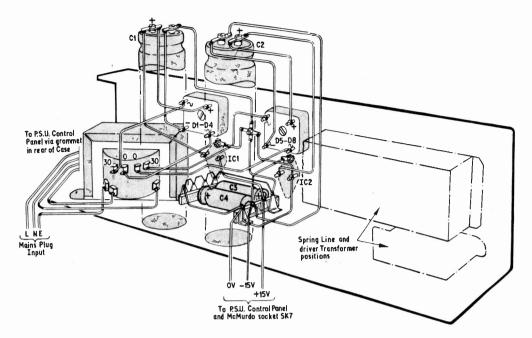


Fig. 2.6. Mounting and wiring details of p.s.u. components

Smoothed d.c. supplying the indicator lamps and calibrating voltage points is taken from the d.c. busbars coupling the McMurdo Red-Range sockets and thus may pass over the top of the sub-frame.

When the power supply unit has been wired up, with the exception of the d.c. to the indicators and calibrating voltage sockets, the mainframe assembly may be commenced.

#### ARRANGEMENT OF PANEL UNITS

Referring for a moment to Fig. 2.2, the constructor should decide at this stage the actual arrangement or order in which he wishes the panel units to be placed relative to one another. The arrangement shown need not be adhered to with the exception of the meter and reverberation unit and the power supply control strip, which have to be sited as shown at the extreme left- and right-hand sides of the front panel respectively.

This decision is necessary at this time in order that the support plates may be correctly placed between the slotted mouldings. Viewed from the front of the assembly, the correct position of these plates is in the slot immediately to the right of the one occupied by a circuit-board support plate.

Since component placement on all front panels offers very little clearance at the left-hand side of the panel it is necessary to cut out the front face of the support plates as shown in Fig. 2.1. The 18mm depth of the cut-out is adequate to clear potentiometers and sockets on all front panels except that of the output amplifiers which will be fitted with ganged "pan-pots".

The optimum position for the support plates is approximately one third of the distance in from the end plates, the exact point, of course, depending upon the module arrangement chosen by the constructor.

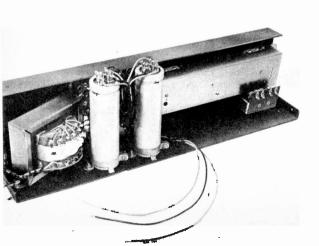
#### MAIN FRAME ASSEMBLY

Assembly of the main frame should be started by loosely securing the bottom slotted moulding between the end plates. The support plates may then be dropped into their respective slots and the upper slotted moulding placed over the lugs on the top edge of the panels and loosely secured between the end plates. Ensure that the chamfered edge of the slots in the mouldings are towards the front face of the assembly and that the vertical panels are in the same respective slot in both mouldings.

This being so, the securing screws may be fully tightened and lugs on the vertical panels twisted through 45 degrees where they protrude through the upper and lower faces of the mouldings.

#### SECURING THE P.S.U.

The power supply sub-frame may now be secured to the rear of the end plates. The lower socket support should be drilled to mate with the slotted holes in the power supply sub-frame (Fig. 2.4) and loosely secured in position. Similarly the upper socket support should be placed loosely in position.



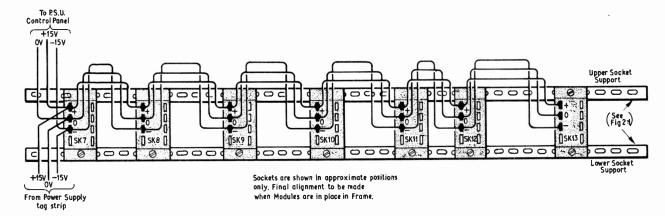


Fig. 2.7. Socket arrangement and wiring on connector mounting rails

#### POSITIONING THE SOCKET SUPPORTS

The final position of these latter supports is determined by inserting an assembled circuit support plate, complete with plug, into the slotted mouldings until the front panel is flush with the face of the mouldings.

A socket is now placed over the plug so that its securing lugs abut the supports at the rear face and the supports adjusted so that they align with the

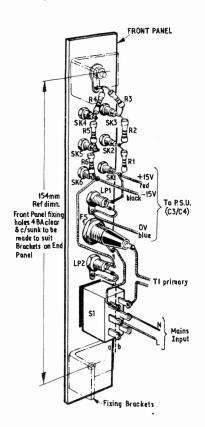


Fig. 2.8. Wiring details for rear of p.s.u. control strip

socket lugs and are parallel with the front face of the mouldings. The socket supports can now be secured firmly at this point and the socket placed in position for the first of the modules to be incorporated into the assembly.

Ideally all the sockets should be placed in position at this time; but if this is not possible the first socket to be positioned should be immediately adjacent to the power supply control module so that its terminals can provide a convenient jumping off point for the leads supplying d.c. to this latter assembly.

The arrangement for supplying power to the individual sockets is illustrated in Fig. 2.7, while Fig. 2.8 illustrates the arrangement for wiring up the rear of the power supply control strip.

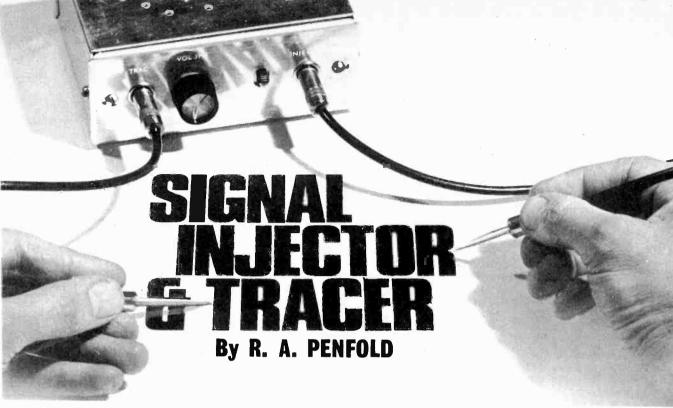
#### **TESTING THE P.S.U.**

The power supply may be tested on completion of assembly and wiring up the main frame. The main purpose of testing is to establish whether the ripple and noise and output voltage levels of each regulator are within their rated specification. Load regulation may also be checked by coupling a 30 ohm 10 watt wirewound resistor across each power rail and observing the change in output voltage on the oscilloscope. If the offset on the scope is not sufficient to enable the trace to be observed at a sufficient degree of sensitivity, a high resistance voltmeter should be used.

The level of change of output voltage at the moment of connecting the resistor across the power rails is likely to be of the order of 150 millivolts or less. Note that the resistor will be dissipating about 7.5 watts and is likely to get uncomfortably hot after a few moments across the power rails. It is best therefore to incorporate a switch in series with the resistor.

The main frame assembly is designed to be accommodated in a standard 19in case in the Vero range. A later article will include details of the types of cases which may be used and modifications necessary in order to fit a.c., d.c., and keyboard sockets to the rear of the case.

Next month: The operation and construction of the voltage controlled oscillators and voltage inverter will be given.



THIS project uses a single, inexpensive, TTL integrated circuit, type SN7402, and a few discrete components.

The SN7402 i.e. is a quad, two-input, positive, NOR gate, intended for switching rather than linear applications. However, this device is available for less than the price of many single transistors.

Although when used as a gate its usefulness to the home constructor is rather limited, with a little ingenuity it can be adapted to perform other functions.

#### THE SN7402 INTEGRATED CIRCUIT

Internal connections to the pins of the SN7402 are shown in Fig. 1.

It is housed in a dual-in-line 14 pin package. As will be seen from looking at Fig. 1, each gate has two inputs, and a single output. The output voltage of the gate will be high only if all the input voltages are low. The output potential will be low, if any of the inputs are at a high potential. Therefore, if one of the inputs is connected to earth, the input will be controlled by the remaining input alone.

The gate may now be biased into a linear operating condition, by connecting this input to earth through a suitable resistor. The value of this resistor must be such that the voltage at the output is approximately half the supply voltage.

#### INJECTOR CIRCUIT

The function of the gate under the conditions described above is that of a Class A amplifier. The input and the output are 180 degrees out of phase, and the stage thus has very similar characteristics to a single stage transistor amplifier.

By capacitively coupling two gates together, with each output connected to the input of the other gate.

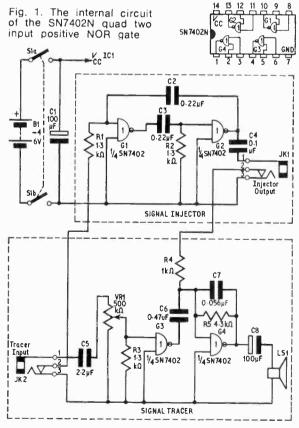


Fig. 2. Circuit diagram of the complete signal injector and tracer unit

a circuit similar to that of a free-running, or astable multivibrator, is obtained. A circuit diagram showing two gates connected in this fashion is shown in

the upper half of Fig. 2.

The circuit operates as follows. When the supply is connected, the voltages at the outputs will begin to rise, and due to slight variations in component tolerances in the circuit, one will start to rise more

quickly than the other.

For example, assume that the output voltage of gate 1 rises most quickly. This rise in voltage will be coupled by C3 to the input of gate 2. This will cause the output voltage of gate 2 to fall, this fall in voltage being coupled by C2 to the input of gate 1.

A further rise in the voltage at gate 1 output will occur, and this regenerative process will continue until this voltage is at its highest level, and gate 2

output is at its lowest level.

Capacitor C2 will now begin to charge through gate 1, and the voltage at gate 1 input will begin to rise, causing the output voltage to fall. This fall in voltage is coupled to gate 2, causing its output voltage to swing to a slightly higher level.

A regenerative action will again take place, until gate I output is very low, and gate 2 output is very high. C3 will now begin to charge through gate 2,

#### COMPONENTS . . .

#### INJECTOR AND TRACER

#### Resistors

R1, R2, R3  $1.3k\Omega$  (3 off)

R5 4.3kΩ

All ±5%, &W carbon

#### **Potentiometer**

VR1 500kΩ logarithmic

#### Capacitors

C1 100μF 6.4V elect.

C2, C3 0.22µF (2 off)

C4 0.1µF disc ceramic

C₅ 2·2μF non elect.

C₆ 0.47µF

C7 0.056µF

C8 100μF 6.4V elect.

#### **Integrated Circuit**

IC1 SN7402N positive NOR gate

#### Miscellaneous

Double pole single throw slider

JK1, JK2 3.5mm jack sockets with break contact

PL1, PL2 3.5mm jack plugs

15 to  $30\Omega$ ,  $2\frac{1}{2}$  to  $3\frac{1}{6}$  in speaker

1.6in × 2in 0.1in matrix Veroboard

Universal Chassis members:  $4in \times 2in$  side panels (2 off);  $5in \times 2in$  side panels (2 off);

5in × 4in plates (2 off) (Home Radio type CU51A, CU52A and CU156 respectively) 1½V batteries type U7 (4 off) and battery holder

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and the opposite will occur. The circuit will thus begin to oscillate continuously, the actual frequency of oscillation being determined by the value given to C3 and C2.

The output is taken through the isolating capacitor, C4, to the output socket. The output wave shape will be almost square, and harmonics of the fundamental frequency will thus be available up to frequencies of many megahertz.

#### TRACER CIRCUIT

The signal tracer circuit consists of the remaining two gates suitably biased, and coupled by a capacitor, C6. The circuit of the tracer is shown in the lower half of Fig. 2.

There is enough output available to drive a 25 ohm impedance loudspeaker. This should preferably have a fairly high efficiency, as the output is not very large, although perfectly adequate for this function.

Capacitor C7 is used to limit the high frequency response of the amplifier, which is otherwise so

good, that instability arises.

Resistors R4, and R5 bias the output stage, and as R5 is connected to the output, it also introduces a certain amount of negative feedback to the amplifier.

The input to the amplifier is taken through C5, and the potentiometer which is the sensitivity

control.

#### RADIO FREQUENCY DETECTOR

If the tracer is to be used with r.f. signals, a detector must be added at the input of the amplifier. This could be made an integral part of the unit, but in the prototype a separate r.f. probe was used. The circuit of this probe is shown in Fig. 3.

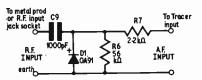


Fig. 3. The circuit of a simple detector which can be built into a small metal tube to enable the tracer to be used with radio frequencies

#### COMPONENTS . . .

#### R.F. DETECTOR

Resistors

R6 56k $\Omega$ R7 2.2kΩ

Capacitors

C9 1,000pF

Diode

D1 OA91

Miscellaneous

Metal tube for case plus metal for prod



Photograph of the completed signal injector and tracer unit showing the layout of the front panel. The box is built using universal chassis members

The casing, and metal prod for the probe will both have to be home made. They can be constructed from whatever suitable materials are at hand. Pen cases, pen light torch cases, and 35mm film containers are popular for housing this type of probe.

The metal prod can be a long bolt, or something similar. The hardware used for the prototype probe consists of a disused penlight torch case, some rubber grommets, and a steel knitting needle for the metal prod. The output should be taken through a screened lead to a 3.5mm jack plug. The components can be mounted on a small piece of 0.1in matrix Veroboard.

If the detector is to be an integral part of the unit, an extra jack socket will have to be mounted on the front panel. The break contact of this should be wired in parallel with that of the other input socket. The detector is wired between these two sockets.

same time. The internal wiring of the i.c. is such, that the power supply must be connected to all, or none of the gates.

The circuit has, therefore, to be arranged so that when the plug is inserted into the tracer input socket, the break contact of the jack disconnects one of the biasing resistors of the injector, thus disabling it. When the injector lead is plugged in, the result is the same, except that it is the tracer, output stage biasing which is removed.

The unit requires 6V at about 20 to 25mA, and this is supplied by four batteries wired in series. A supply of no more than 7V may be used, or the i.c. will be destroyed.

#### CONSTRUCTION

The circuit is built on a piece of 0·lin matrix Veroboard, measuring 2in × 1·6in. A diagram giving the layout of this board is given in Fig. 4.

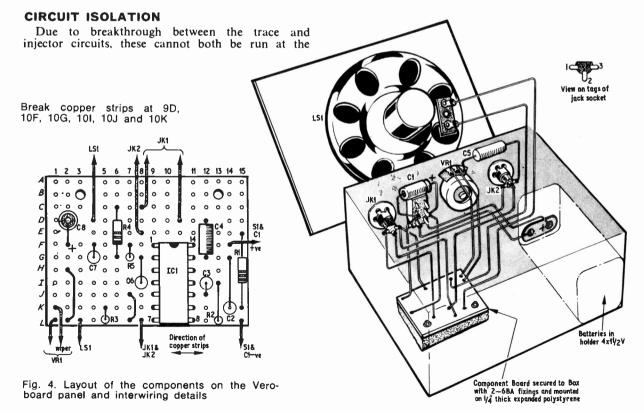
When completed this board is bolted to the rear right-hand side of the case and must be insulated from the case. This may be achieved by placing a piece of expanded polystyrene between the board and the case. C1 is not mounted on the board, but is mounted on switch \$1.

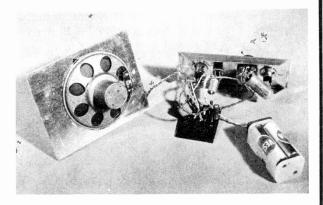
#### **ALUMINIUM CASE**

An aluminium case is constructed using Home Radio Universal Chassis Members, and measures  $5in \times 4in \times 2in$ .

The front, back, and side panels are bolted together using eight 2BA bolts, the holes for which are already drilled in the panels.

The base plate is fixed in place by four 6BA bolts.





Two 4BA self-tapping screws are required to hold the lid in place. The holes for these should be drilled centrally on the flanges of the side panels, using a No. 31 twist drill.

A drill of the same size may be used to drill the holes for the 6BA bolts. A No. 24 twist drill is used to make the mounting holes in the lid. The speaker should be mounted on the lid at any convenient place.

Details of the front panel can be seen in the photograph. The exact size of the mounting holes will vary according to the type of switch, or jack socket used, but the positioning of the holes will of course remain the same.

The batteries are positioned to the rear, and at the left-hand side of the case, opposite the main component board. They should be mounted in a battery holder of the type specified in the components list. Battery clips of the type used with PP3, or PP6 batteries are used to make the connection to the holder.

#### **USING THE UNIT**

Switch S1 is the main supply on-off switch.

As described earlier, the function of inject, or trace is obtained by merely inserting the appropriate

When using the injector, the first test would be to the speaker of the radio, or amplifier under test. Tests should then be made at the inputs of the earlier stages, working forwards towards the r.f. stages, or the amplifier input.

When a test is made, and no output comes from the speaker, the faulty stage has been located. It is the stage which lies between the last, and the penultimate one to be tested. Because the output of the injector is so rich in harmonics, it may be used to test the a.f., r.f., and i.f. stages.

#### **USING THE TRACER**

To use the tracer, the same procedure is used, except in reverse, with the first test being made at the input of the amplifier, and then working towards the speaker.

A signal of some kind must be connected at the input and when this signal is not received by the tracer the faulty stage has been located. It is again the one that lies between where this last test, and the previous one were made.

When testing i.f., or r.f. stages of a receiver, the r.f. probe must be substituted for the ordinary test leads.

### NEWS BRIEFS

#### **Tidal Monitoring System**

THE TASK of monitoring tidal conditions and wave height along the coast of Spain presents enormous difficulties using conventional monitoring techniques. To overcome this problem Plessey Environmental Systems have supplied pressure sensors and a digital logging system to the Spanish maritime authorities to provide precise information at 25 of the harbours around Spain's coastline, which is one of the longest in Europe.

The pressure sensors are accurate to  $\pm 0.3$  per cent of full scale and this measured pressure is encoded into a frequency modulated analogue signal which is transmitted to a central data collection unit in Madrid where it is stored on magnetic tape for subsequent

analysis by computer.

#### New Radar Testing Equipment for Europe's MRCA

EUROPE'S new multi-role combat aircraft (MRCA) uses a highly sophisticated radar system and efficient testing is vital for such a system. EMI Elec-Systems & Weapons Division have just announced that they are supplying radar testing equipment to assist in-flight testing.

Unlike conventional airborne radar testing methods which limit thorough evaluation of the radar to the period that the aircraft is in flight, the EMI systems will enable the radar's performance to be examined

in detail on the ground.

When fitted to the aircraft, the equipment will continuously record the video signal from the radars onto magnetic video tape which can later be replayed on ground equipment.

The new technique is expected to yield far more information from each test than was previously pos-

#### UK Tops Europe in Data Transmission

THE NUMBER of terminals sending and receiving computer data in the Post Office's Datel services has grown by more than a quarter over the last year.

Datel terminals in service reached a new peak of 22,214, a growth of 27 per cent. Although the UK has only a quarter of Europe's computers, there are more data-transmission terminals in Britain than in the rest of Europe combined.

### POINTS ARISING

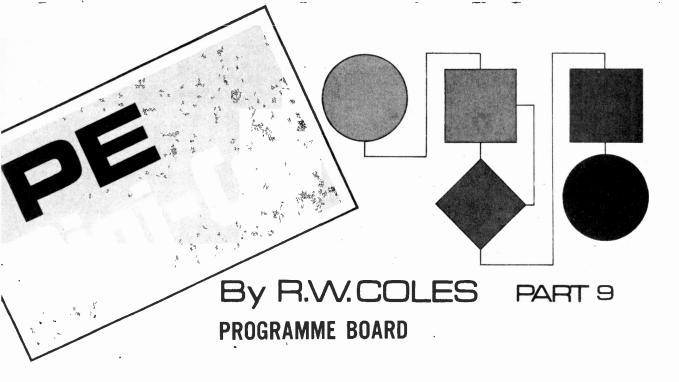
#### I.C. LINEAR OHMMETER (January 1973)

This article was the work of Charles Griffiths B.Sc (Eng). We apologise for the fact that an incorrect initial was attached to our author's name.

#### **BIOLOGICAL AMPLIFIER** (January 1973)

In Fig. 3, page 34, the value of resistor R5 should be  $5.6k\Omega$ . In the last paragraph under the side heading Alphaphone on page 38 reference to C10 should read C11.

Fig. 5, page 39, the pin numbers 9 and 10 should be transposed in both the circuit diagram and case interwiring. In the case interwiring pin 12 should be 11. These corrections bring Fig. 5 into agreement with the circuit diagram Fig. 3.



THE BULK of the Digi-Cal logic has now been described. Throughout the articles covering the logic boards from DISPLAY to ADDER, readers will constantly have encountered a variety of signals. attributed to a mysterious PROGRAMME BOARD.

The far-reaching influences of this board thus having been established, the time has arrived to delve into the method of deriving the plethora of programme output signals, a most important aspect of the calculator.

#### **DIGI-CAL PROGRAMME**

The requirements of Digi-Cal are humble, reprogramming not being required in the normal run of things and the tasks for which a programme is necessary, namely the four arithmetic functions of addition, subtraction, multiplication and division can be carried out with only a few programme steps and without recourse to any high level language facilities other than the press of an appropriate key.

Programming then is carried out at the basic level of logic gates and flip-flops, and the Digi-Cal philosophy is retained by making the programmes variable by wiring in diodes where required in a matrix arrangement.

The separate jobs to be controlled by the programme include shifts, transfers, register and counter clearing, routing and clock pulse initiation, all of which must be carried out in a strict sequence.

#### PRINCIPLES OF PROGRAMME GENERATION

The programmes for Digi-Cal are formed in a diode matrix in the form of a Read Only Memory or R.O.M. "Memory" because a number of separate addressable locations are provided, and "Read Only" because the instruction data in each address location is fixed at the wiring-up level and is not altered by the operator.

In the present system the R.O.M. array is addressed sequentially by means of a counter. In this

way each location in the memory is addressed in turn starting each time at address "1" and continuing to the final address of each R.O.M. in an incremental fashion.

It is not possible to jump back or forward in the sequence and random addressing of a particular location is likewise impossible.

Pausing during a sequence for an indefinite length of time is possible, as is aborting the sequence by clearing the address counter and stopping the clock.

#### **BASIC CIRCUIT**

The incremental ADDRESS COUNTER/R.O.M. programme system is best understood initially by means of a simplified circuit without any trimmings (Fig. 9.1).

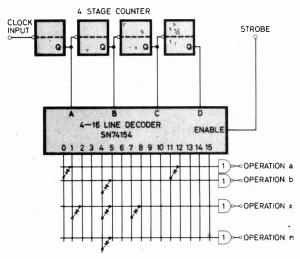


Fig. 9.1. Principles of Read Only Memory Programme generation

Here, a four stage binary counter with 16 possible states is driven continuously by a clock pulse train. The system states of the counter are individually decoded by gates which produce an active low output when inputs are in the appropriate states.

These gates are in the form of an SN74154 TTL M.S.I. decoder which has extra facilities to generate the complement versions of the four inputs required by the decoder gates and a common overriding enable, or strobe input which can be used to inhibit all outputs.

The pin connections of the SN74154 is shown in Fig. 9.2. Referring again to Fig. 9.1 with Fig. 9.2 in mind, it can be seen that, as the counter steps through the sequence, each output from the decoder is enabled in turn for one clock period, thus establishing the programme steps.

The number of operations to be controlled by the programme depends on the requirements of the machine controlled, and can be few or many as required only four being shown in the basic circuit.

All that remains to perform a particular operation in a particular programme step, is to connect a diode across the appropriate intersection where the step line crosses the operation line.

#### **DIODE MATRIX**

Inverters are used at the output end of the operation lines to act as what could be described as "sense amplifiers" in traditional memory terms. Another way of looking at the operation lines and inverters is as multi-input NOR gates with the number of inputs to each gate being determined by the number of times that an operation is used.

Note that each operation can be used any number of times and also that any number of different operations can be activated simultaneously.

The basic circuit has no facilities for stopping or starting the sequence which therefore runs continuously. Also only one programme is catered for and, because of the ripple-through counter circuit propagation delays combine to give spurious pulses of a few nanoseconds width on some of the step lines.

All of these disadvantages have to be overcome in the Digi-Cal circuit, which is shown in Fig. 9.3.

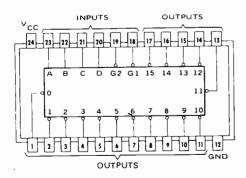


Fig. 9.2. The pin connections of the SN74154 four line to 16 line decoder

#### **FULL CIRCUIT**

The full circuit looks very much more complicated at first sight but the R.O.M. arrays can be easily identified, and the rest of the tangle breaks up into sections with specific jobs.

First out of the way are IC108, 109 and 110 which are simply there to divide the master (ungated) clock signal from board CB by a factor of a thousand, to allow the programme circuits to operate at slow speed.

This eases reflection and decoding problems while keeping the operation of the calculator logic tied to a master synchronising clock signal. The only special thing about these dividers is the fact that the three SN7490 are connected in the ÷10 mode which gives a 1:1 mark space output from the final stage.

This is arranged by connecting the A stage of the circuit after the B, C, D stage.

#### STOPPING AND STARTING

An SN7493 (IC112) is used as the programme counter, and it is made to stop or start counting by means of a gate in its clock line. Gate G1 itself is controlled by a latch flip-flop which is SET by a pulse from the EQUALS key monostable in the keyboard logic and RESET by the programmes themselves.

Setting the latch is accomplished by using the clock input with a permanent "1" on the D input and clearing is achieved by using the programme STOP PROGRAMME operation to energise the CLEAR input of the first flip-flop via a monostable formed from the other flip-flop and a couple of inverters.

This method of forming a monostable was described in the article covering the CLOCK BOARD, Fig. 7.5, a monostable being necessary in this case to prevent "race" conditions removing the RESET input before the latch was properly cleared.

#### **PROGRAMME SELECTION**

Three separate programmes are required in Digi-Cal; three rather than four because the sequences for ADDITION and SUBTRACTION are identical, the distinction being drawn by the fact that the ADDER BOARD operates either as a subtractor or an adder depending on the FUNCTION CODE which is produced directly by keyboard depressions.

The ADD/SUBTRACT programme is quite simple as might be expected and requires only a few steps. Seven steps are, however, provided to allow reprogramming if any "frills" such as round-off or true negative answer are considered possible later.

The MULTIPLY and DIVIDE programmes are separate and have a possible 15 steps each, to allow for the increased complexity of these operations. Some spare steps are also left in these operations, and can be employed as required.

The selection of the required programme is accomplished by utilising the GI/G2 ENABLE inputs on the SN74154 decoders providing the MULTIPLY and DIVIDE sequences, and by using the D input for the same purpose on the SN7442 of the shorter ADD/SUBTRACT sequence.

Using the D input as an enable is possible with the SN7442 because if the D input is high, the output selected must be greater than seven and since only outputs one to seven are used, a high D input means all programme steps are disabled even though they may be addressed by the A, B and C counter outputs.

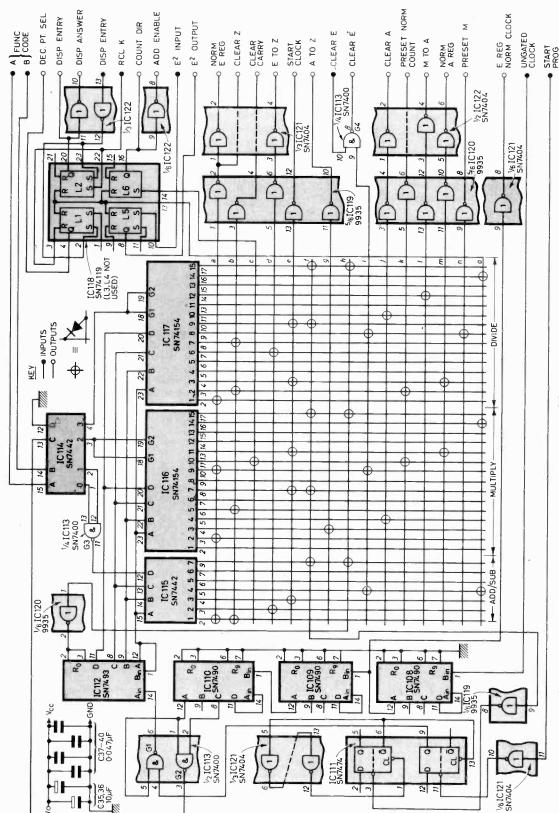


Fig. 9.3. The full circuit diagram of the PROGRAMME BOARD. Power supply connections to the SN74154 and SN74119 are shown in Figs. 9.2 and 9.6. All others have  $V_{\rm CC}$  to pin 14 and GND to pin 7 except the SN7490 and SN7493 which has  $V_{
m cc}$  to pin 5 and GND to pin 10, and SN7442 which has  $V_{
m cc}$  to pin 16 and GND to pin 8

#### COMPONENTS . . . Capacitors C35, C36 10µF 15V elect. (2 off) C37-C40 0.047µF (4 off) Diodes D104-D142 West Hyde type "red" (or any small silicon diode) (39 off) Integrated Circuits IC108-IC110 SN7490 (3 off) SN7474 IC111 IC112 SN7493 SN7400 IC113 IC114, IC115 SN7442 (2 off) IC116, IC117 SN74154 (2 off) SN74119 IC118 IC119, IC120 DTL9935 (2 off) IC121, IC122 SN7404 (2 off) **Printed Circuit Board** 0.1in Veroboard (8.2in × 3.4in) Edge Connector 32 way 0.1in pitch edge connector (optional)

#### STROBE SYSTEM

Enabling the appropriate programme decoder is not done in a d.c. manner, with a constant input throughout a particular sequence but in an a.c. manner by routing enabling or "strobe" pulses to the selected decoder which occur in the centre of each addressing period.

This scheme is used to kill two birds with one stone, since by enabling decoder outputs only in the middle of each address period the problem of spurious outputs or "glitches" is overcome.

By the time the enable pulse arrives the address counter is resting in a particular state and propagation delay problems are overcome.

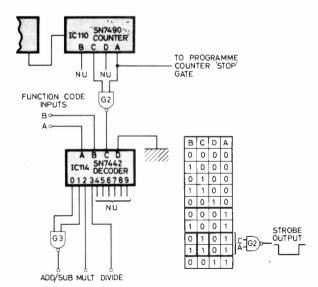


Fig. 9.4. Gate G2 is used to generate a strobe pulse by detecting simultaneous C and A outputs during the clock period as shown in the truth table. The decoder is used to select the appropriate part of the programme according to the FUNCTION CODE inputs

This selection system involves IC114, G2 and G3 and to make the principle clearer it is redrawn in an integrated way as Fig. 9.4. Two states of the final divider (IC110), count sequence are detected by gate G2 which gives a negative strobe pulse near the end of the run (see Truth Table).

The strobe pulse is applied to the c input of IC114 which is being under-used in this application as a two to four line decoder with strobe input.

One of the outputs zero to three is addressed by the two line FUNCTION CODE generated by the KEY-BOARD in response to the arithmetic selection made by the operator.

The selected output will remain high however, until the strobe pulse takes the c input low. The result of all this is that a continuous stream of strobe pulses is delivered, via the logic described, to the STROBE or ENABLE input of the selected programme decoder. Gate G3 is used as a negative logic NOR gate to ENABLE the single ADD/SUBTRACT programme whether addition or subtraction is called.

#### **PROGRAMME OUTPUTS**

Fifteen programme operations are possible on this board, and although more of these would be useful, board space is a limiting factor for the layout of the R.O.M. matrix.

Because of this limited number of available lines, some outputs do two or more jobs which seem to be unconnected. For example, line A is responsible for normalising the entry register, clearing the Z REGISTER, and clearing the EQUALS LATCH on the M COUNTER boards.

#### PROGRAMME OPERATION CODE ASSIGNATIONS

- a Normalise Entry Register Clear Z Register Clear M Counter Equals Latch
- b Clear Carry Store Clear M Counter (to 000000)
- c Set latch, changing clock count to DOWN and disabling A inputs to ADDER
- d Transfer the contents of the E register to the Z register
- e Start Arithmetic Clock
- f Stop programme sequence
- g Transfer the contents of the A register to the Z register
- h Clear the Programme Counter
- i Clear E register
- j Clear A register
- k Preset NORM code from the thumbwheel into the clock counter
- I Transfer contents of M counter to A register
- m A register NORM in progress
- n Preset M counter to 999999
- Clear latch array/select A register for display with point position determined by thumbwheel

These operations are not related and are grouped together because they do not interfere with each other if performed at the same time.

It must be remembered, however, that if a CLEAR Z signal is required by a programme, the other signals are also produced which may or may not be important if a "home-made" programme sequence is employed.

Programme outputs are arranged to be either "active high" or "active low" depending on the requirements of the logic they drive, and for this reason either one or two inverters are placed at the end of the operation lines.

The inverters connected directly to the R.O.M. lines are from the DTL family and are type 935 which do not have input diodes (Fig. 9.5). This enables the R.O.M. diodes to be used as an integral part of the circuit without reducing noise immunity.

#### **LATCH ARRAY**

The latch array performs a variety of jobs which are related to the programme, one of the most obvious of which is to stretch programme operations over a number of steps.

"Stretching" is achieved by using the programme to SET a latch in a particular step, and to RESET it in another. The latch output is then used to control a particular operation which must be continued for longer than one step.

Latch L6 is used in this way to control the CLOCK COUNTER direction and ADDER ENABLE during A REGISTER NORMALISATION in the MULTIPLY sequence. Latch L5 is used to control routing logic during an E² operation, being SET by pressing the E² key and RESET by the CLEAR LATCH ARRAY programme operation at the end of each sequence.

Latches L3 and L4 are not used, but are available if required, and L1 and L2 operate together to control the display selection.

Latch L1 controls the decimal point selection (fixed or floating) and L2 controls the register selection (A or E).

The i.c. used in this position is the very versatile SN74119, which like the SN74154 decoders is housed in a 24 pin dual-in-line package. The logic of this device is simply that of six cross-coupled gate latches with a common clear line, and is shown in Fig. 9.6.

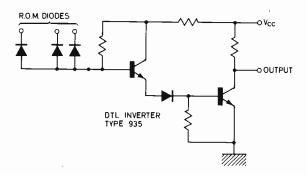


Fig. 9.5. This diagram shows how the R.O.M. diodes and the DTL inverters are used to form NOR gates

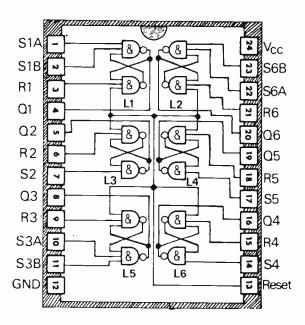


Fig. 9.6. Internal logic of the SN74119 hex SET/RESET LATCH

#### **CLOCK AND CLEAR**

There are only a couple of items left on the full circuit to be mentioned, the first of these being G4 which is used to NOR the CLEAR E output from the programme and the CLEAR E input from the CE key to give a combined signal.

Next, the E REGISTER normalising clock output is taken as a tapping from the divider-chain so that although much faster than the final programme clock, the normalising clock is slower than the arithmetic clock to prevent difficulties with the long line lengths used.

#### **PROGRAMMING**

The programmes used in the prototype are shown in Fig. 9.7, which presents the sequences as flow diagrams.

The operations inside the shaded boxes in the MULTIPLICATION and DIVISION programmes show the conditional branching operation carried out by the CLOCK GENERATING BOARD, and are included in the flow diagram for completeness.

Each of the square boxes corresponds to the programme step with which it is numbered, several operations being possible at each step. The spare steps do not give rise to any outputs from the board, but may be used to advantage if the basic programme is expanded or re-arranged.

Re-programming does not require any particular skill other than commonsense and a knowledge of the way the circuits operate.

The writer has had very little time to consider just what improvements could be programmed into the calculator, but with a little ingenuity and perhaps modification, true negative answers (as opposed to complement versions as the machine stands) should be possible.

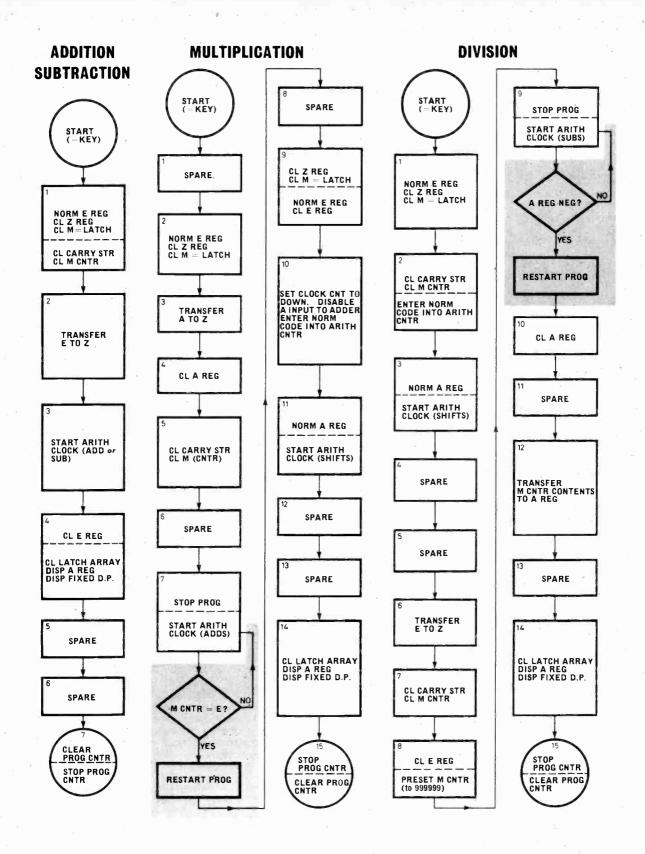


Fig. 9.7. This flow diagram shows the three programmes used on the PROGRAMME BOARD. The same programme is used for addition and subtraction as mentioned in the text

#### PROGRAMME BOARD

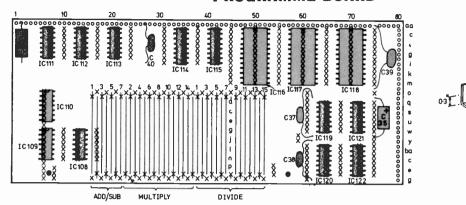
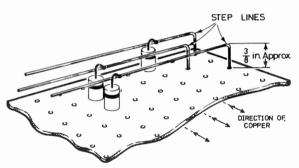


Fig. 9.8. The layout of the components on the Veroboard panel. Crosses show breaks in copper strips



Diode matrix construction

#### PROGRAMME BOARD WIRING DESTINATIONS

- aa not used START PROG (fr kbd) ab RECALL K (fr kbd) UNGATED CLK IN (fr CB/43) ac
- ad ae
- FUNC CODE A (fr kbd) DISP E (to disp) af
- ag
- ah
- E² (fr kbd)
  DISP E (fr kbd)
  FUNC CODE B (fr kbd) ai CNT DIR'N (to CB/28) ai
- ak
- CLEAR E (to ED/2) CLEAR E (fr kbd) al
- not used am GND an
- E2 (to E2 logic) ao ap
- CLEAR Z REG etc (to Z2/43, kbd (NORM) and aq
- CLEAR CARRY etc (to AD/23, M1/20, M2/20) ar
- as
- DISP A (to DISP) START CLK (to CB/44) at
- not used au DEC PT SEL'N (to kbd) av
- TRANSFER E TO Z (to Z1/24) E REG NORM CLK (to kbd) aw
- ax ADD ENABLE (to AD/37) av
- az
- NORM A REG (to CB/37)
  PRESET NORM CNT (to CB/27)
  TRANSFER M TO A (to CB/39) ba bb
- bc not used
- PRESET M (to M1/21, M2/21) bd
- CLEAR A REG (to A1/44, A2/44) TRANSFER A TO Z (to Z2/24)
- bf

#### CONSTRUCTION

This circuit is built on a Veroboard panel (Fig. 9.8) and carries a good deal of wiring on both sides. The R.O.M. operation lines are formed by the printed tracks on the board, but the step lines are formed from bare tinned copper wire running at right-angles to the tracks.

These are spaced from the board by about 3 in so that diodes may be soldered-in where required. Note that the diodes are inserted with their red ends uppermost, connected to the step lines.

Wiring is congested but not critical, thanks to the low programme speed, and both sides of the board carry wire interconnections.

An edge connector of 32 or more ways is recommended for use with this board, but it is not essential; connections can be soldered directly to the printed tracks if desired. If an edge connector is used it is necessary to clean the track ends thoroughly with fine emery paper and then coat them with a tarnish preventer and cleaner such as Electrolube.

#### **TESTING**

Programme selection and step sequences can be easily checked after construction by using a large value capacitor on the CLOCK BOARD to give a very slow programme sequence. Steps can then be followed with a multimeter set to a low voltage range.

Operational testing can be carried out only with the ADD/SUBTRACT programme until the M COUNTER boards and E² logic are constructed, but when this is working, little trouble should be experienced with the other programmes.

Note: In Fig. 6.10 (Dec. 72) Z1/22, Z1/43, Z2/22, and Z2/43 go to Z2/44 not CB/13. Z1/21, Z2/21 go to CB/23. A1/42, A2/42 go to CB/40. A1/43, A2/43 go to CB/38. In Fig. 7.7 (Jan. 73) CB/40 should go to A1/42, A2/42.

Next month: M Counter Boards



# Designing

### arated cuits

A.FOORD

Simple Memory Circuits

*HIS month we will show how simple memory circuits may be constructed from gates and how the master-slave bistable is developed. In the way that a transistor bistable can be made from two cross-coupled inverting stages, a bistable can also be made from two inverting gates. This is shown in Fig. 6.1 for NAND gates, although a similar NOR circuit is also possible.

If the clear and set inputs are at 1, and so have no effect, then for either gate a 1 at its input would produce a 0 at its output, and vice versa. Since the output of one gate is the input of the other, the two outputs must be in opposite states. If Q is 1 then

O must be 0, and vice versa.

If the clear input is 0 and the set input is 1, then  $\overline{Q}$  becomes 1 and Q becomes 0. If the set input is 0 and the clear input is 1 then the opposite state is

set up with O equal to 1 and  $\overline{Q}$  equal to 0.

If a momentary 0 input is applied to either the set or clear input the corresponding output will become a I and will remain in this state until a 0 is applied to the other input. The circuit can therefore act as a memory and can be used to eliminate the effects that are obtained from contact bounce on a mechanical switch. This could be checked as an experiment (Fig. 6.2).

From the truth table it can be seen that, if 0 levels are applied to both inputs, then both the Q and  $\overline{Q}$ outputs will be 1. For a true bistable circuit this

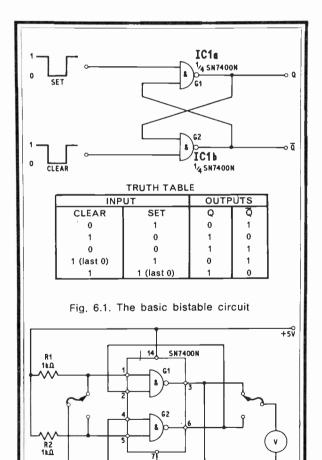
condition would be avoided.

#### **GATED MEMORY**

When input gates are added to the basic memory in Fig. 6.1, it can be made to respond to input levels only during a specific clock time interval, as shown in Fig. 6.3. While the clock input is at 0, gates 1 and 2 have a 1 at their outputs and the set and clear inputs are locked out of the memory. New information can only reach the memory when the clock input is at 1.

A 1 at the set input with a 0 at the clear input will give a 0 input to gate 3 and a 1 input to gate 4, then O will be a 1. The other possible states are

shown in the truth table.



momentary 0 on an INPUT sets corresponding OUTPUT

eliminate the effects of switch contact bounce

6.2. The basic bistable circuit used to

If both set and clear inputs are at 0 when the clock goes high the inputs to the memory remain at 1 and the output does not change from its previous state. In the truth table T_n represents the time during the clock pulse while  $\ddot{T}_{n+1}$  represents the time after the clock pulse. Similarly  $Q_n$  represent the state of the memory at the time of the clock pulse. (These are common terms used in manufacturers' data on digital i.c.s.)

When the sampling interval is over and the clock returns to 0, further changes in set and reset can have no effect until the next clock pulse. The memory is said to have "clocked", because the sampling point can be timed to occur when the required data is at the set and clear inputs, and data outside this time will be ignored. For this circuit the set and clear levels need not be pulses because input pulsing is provided by the clock.

#### DATA LATCH

The previous circuit had three useful conditions, Q_n, 0, and 1. In some applications the data latch

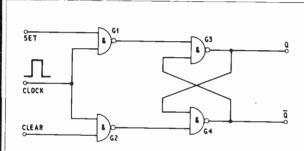
#### GLOSSARY

BISTABLE CIRCUIT A circuit in which the output has two stable states.

NAND GATE A logic circuit where all inputs must have 1 level signals to produce a 0 level output.

NOR GATE Any one input or more than one input having a 1 level signal will produce a 0 level output.

TRUTH TABLE A chart which tabulates all the combinations of possible states of the inputs and outputs of a circuit.

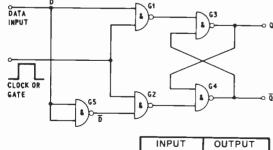


TRUTH TABLE INPUTS Tn OUTPUT Tn +tr CLEAR ۵ 0 Qn(Q at Tn) ٥ 1 0 0

Fig. 6.3. The gated memory with SET and CLEAR inputs

INDETERMINATE

1



D	Q
0	0
1	1

Fig. 6.4. The gated memory with a single data

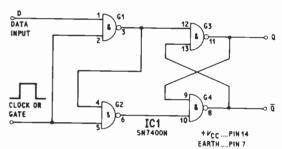
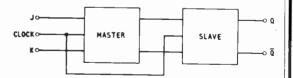
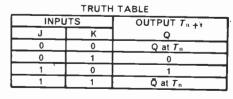


Fig. 6.5. The gated memory with a single data input and the minimum number of gates. It can be realised with an SN7400N







- 1 Isolate slave from master
- 3 Disenable inputs
- 2 Enter information to master
- 4 Transfer information from master to slave

Fig. 6.6. The basic action of a master-slave bistable circuit

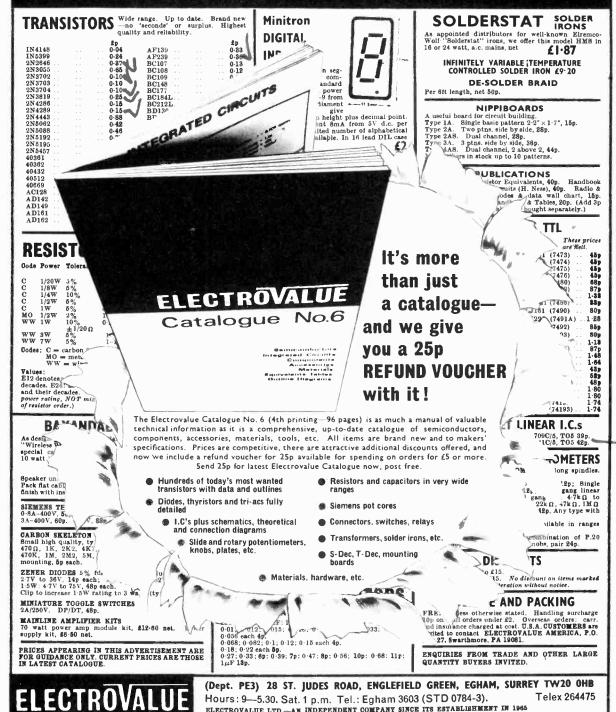
input

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1891			INTEGRA	TED	JIKC OTTS:	op +	p each ad	ided
1829	Ap	fp fp	11.7764.0	£p		#p		4p
1888	1N23 0.20	ASY26 0.25				0.82		0.10
1886	1N85 0-88	A8Y27 0.82			0 4 7 2 2 2 3	0.45		
187864	1N253 0-50	A8Y28 0.25			OAZ224	0-45		0.25
INP146	1N200 0-00 1N845 0-95				OAZ241	0.22		0.15
184130	1N725A #-20	ASY50 0.17						0.12
18113	-1N914 -0.07	ASY51 0.40	BYZ88C3		OAZ246	0.28		0.12
Billist  0	18113 0-15	ASY55 0.20	(211)		OAZ290		ZTX304	0.25
1839	18130 0-18	A8Y62 0.25	CR81/05	0.25	OC16T	0.88		0.16
20381		ASY86 0.33	CR81/40		OC19	0.87	ZTX 503	0.17
20381					OC20	0.85	ZTX531	0.50
20414	2G381 0.25	AUY10 0-98			OC23		INTEGR	ATED
18069	20414 . 0.80	AU101 1.50	DD003	0.15			CIRCUIT	8
287808	20417 0.22	BC107 0-10			OC25	0.87	7/00	0.20
287706	2N697 0-15	BC109 0-10	DD008	0.88			101	0.20
287708							7402	0.20
287709 0-63 BC118 0-25 0-25 0-30 0-30 1-30,0 0-25 28709 0-63 BC118 0-25 0-25 0-30 0-30 0-30 1-30,0 0-25 287109 0-83 BC121 0-20 0-20 0-20 0-20 0-20 0-20 0-20 0	2N706A 0-10	DOILE DOE		0.88			7404	0-20
Section   Color	2N708 0-15	BC116A 0.80	GD8	0.25			7405	0-20 0-30
201132	2N709 0-68	DCIIO V.ED	GD12					0-30
2N11302 0-18 BC125 0-68 GET113 0-10 CC13 0-40 7410 0-2 2N1303 0-18 BC140 0-16 GET114 0-16 CC13 0-40 7410 0-2 2N1306 0-22 BG144 0-16 GET116 0-50 OC444 0-17 7412 0-2 2N1306 0-22 BG147 0-16 GET116 0-50 OC444 0-17 7412 0-2 2N1306 0-28 BG147 0-16 GET870 0-28 OC456 0-12 7416 0-2 2N1306 0-28 BG147 0-16 GET872 0-30 OC456 0-12 7416 0-2 2N1306 0-28 BG147 0-16 GET872 0-30 OC456 0-12 7416 0-2 2N1306 0-28 BG147 0-16 GET872 0-30 OC456 0-12 7416 0-2 2N1307 0-28 BG167 0-16 GET872 0-30 OC456 0-12 7416 0-2 2N1307 0-28 BG167 0-16 GET872 0-30 OC456 0-12 7416 0-2 2N1408 0-00 BG168 0-13 GET881 0-26 OC466 0-7 7420 0-2 2N1408 0-00 BG168 0-13 GET881 0-26 OC86 0-06 7422 0-2 2N1408 0-00 BG168 0-13 GET881 0-26 OC86 0-06 7422 0-2 2N2128 0-20 BCV31 0-26 GEX44 0-08 OC70 0-12 7428 0-2 2N2128 0-20 BCV31 0-26 GEX44 0-08 OC70 0-12 7428 0-2 2N2304 0-20 BCV32 0-26 GEX44 0-08 OC70 0-12 7428 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC88 0-06 7422 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC75 0-25 7438 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC75 0-25 7438 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC75 0-25 7438 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC75 0-25 7438 0-2 2N2304 0-20 BCV34 0-30 GJ3N 0-25 OC75 0-25 7440 0-2 2N2305 0-15 BCV31 0-30 MAT100 0-35 OC75 0-30 7441 N 0-2 2N2305 0-15 BCV31 0-30 MAT100 0-35 OC75 0-30 7441 N 0-2 2N2305 0-15 BCV31 0-30 MAT100 0-35 OC75 0-30 7441 N 0-2 2N2305 0-15 BCV31 0-30 MAT100 0-35 OC81 0-20 7453 0-3 2N2306 0-10 BD112 0-65 MAT100 0-25 OC81 0-20 7453 0-3 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD112 0-65 MAT100 0-25 OC81 0-20 7453 0-3 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2307 0-23 BCC7 0-35 MAT100 0-35 OC81 0-20 7453 0-3 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD111 1-62 ME295 0-87 OC81 0-30 7441 N 0-2 2N2306 0-10 BD112 0-65 MAT100 0-25 OC81 0-30 7441 N 0-2 2N2306 0-10 BD12 0-65 MAT100 0-25 OC81 0		BC121 0-20					17408	0.20
Section   Sect	2N1132 0-25	BC125 0.68	GET113	₽.50	0C42			0-45
Section   Sect	2N1302 0-18	BC126 0-65	GET114 (	0.15		0.40	7410	0.28
2N1306 0-22 BIG148 0-13 GET120 0-28 CGL65 0-12   7118 0-28 CN1309 0-25 BIG157 0-15 GET872 0-30 CGL65M 0-12   7118 0-28 CN1309 0-25 BIG157 0-15 GET872 0-30 CGL65M 0-12   7118 0-28 CN1309 0-25 BIG158 0-12   GET875 0-25   CGL64 0-12   7147 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   7148 0-12   71	2N 1303 0-18 2N 1304 0.00	BC147 0-15	GET115	0.50	0044	0.17	7412	0.42
2N1306 0-25 BC149 0-15 GET875 0-26 CC46 0-18 7-41-2 0-2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2N1305 0.22	BC148 0.18	GET120	0.25	OC45	0.12	7413	0.30
2N1308 0.95   BC158 0.12   GETS80 0.37   CG7 0.26   7429 0.4   2N2148 0.60   BC180 0.13   GETS81 0.25   CG59 0.60   7423 0.4   2N21218 0.20   BC180 0.13   GETS82 0.25   CG59 0.60   7423 0.4   2N21218 0.20   BC192 0.85   GEX444   0.08   CG70 0.12   7425 0.6   2N21218 0.20   BC192 0.85   GEX444   0.08   CG70 0.12   7425 0.6   2N21218 0.20   BC193 0.85   GEX441   0.16   CG71 0.12   7429 0.6   2N21218 0.20   BC193 0.80   GIJM 0.25   CG73 0.30   7432 0.4   2N2213 0.22   BC193 0.40   GJM 0.25   CG73 0.30   7432 0.4   2N2213 0.22   BC193 0.40   GJM 0.25   CG73 0.30   7432 0.4   2N2204 0.25   BC193 0.40   GJM 0.25   CG73 0.30   7432 0.4   2N2204 0.25   BC194 0.50   GJM 0.35   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   GJM 0.35   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   GJM 0.35   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   GJM 0.30   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   MAT100 0.25   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   MAT100 0.25   CG76 0.25   7435 0.6   2N2204 0.25   BC194 0.50   MAT100 0.25   CG79 0.20   7434 0.5   2N2205 0.28   BC270 0.36   MAT101 0.30   CG81 0.20   7434 0.5   2N2205 0.28   BC270 0.36   MAT101 0.30   CG81 0.20   7435 0.5   2N2205 0.10   BC194 0.55   MAT102 0.25   CG79 0.22   7435 0.5   2N2205 0.10   BC194 0.55   MAT200 0.25   CG84 0.20   T435 0.5   2N2205 0.10   BC194 0.55   MI22255 0.37   CG81 0.20   7435 0.5   2N2205 0.10   BD113 0.80   MI2225 0.37   CG81 0.20   7435 0.5   2N2205 0.10   BD113 0.80   MI2225 0.37   CG81 0.20   7435 0.5   2N2205 0.10   BD114 0.75   MI2225 0.37   CG81 0.20   7435 0.5   2N2205 0.10   BD114 0.75   MI2225 0.37   CG81 0.20   7435 0.5   2N2205 0.10   BD115 0.25   MKT128 0.35   CG82 0.85   7473 0.5   2N2205 0.10   BD116 0.25   MKT128 0.35   CG82 0.85   7474 0.4   2N2205 0.10   BP184 0.25   MKT128 0.35   CG82 0.85   7474 0.4   2N2205 0.10   BP184 0.25   MKT128 0.35   CG82 0.85   7474 0.4   2N2205 0.10   BP185 0.25   MKT128 0.35   CG82 0.85   7474 0.4   2N2207 0.10   BP181 0.35   MKT128 0.35   CG20 0.6   2N2207 0.10   BP184 0.	2N1306 0-25	BC149 0-15	GET872	0.80	OC45M	0.18		0.30
2N2147 0-76 BC169 0-83 (ET882 0-25 0C59 0-60 7423 0-29 2019 0-20 BCY31 0-35 (ET882 0-25 0C59 0-65 7425 0-29 2019 0-20 BCY31 0-35 (ET885 0-25 0C59 0-65 7425 0-29 2019 0-20 BCY32 0-35 (EX44 0-9) BCY33 0-35 (EX44 0-9) BCY33 0-25 (EX44 0-9) BCY33 0-25 (EX44 0-9) BCY33 0-25 (EX44 0-9) BCY34 0-30 GJ3M 0-25 (C77 0-20 7432 0-22 2019 0-20 0-20 0-20 0-20 0-20 0-20 0-20 0-2	2N1308 0-9K	BC158 0.19			OC57		7420	0.20
2N2148 0-60 BC169 0-13 GET885 0-25 0C66 0-65 1-425 0-26 2N21219 0-20 BCY32 0-55 GEX444 0-08 0C70 0-12 1-425 0-26 2N21219 0-20 BCY32 0-55 GEX445 1-10 0-12 1-428 0-26 2N21219 0-20 BCY32 0-55 GEX445 1-10 0-12 1-428 0-26 2N21219 0-20 BCY34 0-30 0J3M 0-38 0C70 0-12 1-428 0-26 2N21219 0-20 BCY34 0-30 0J3M 0-38 0C71 0-30 1-432 0-42 2N2241 0-19 BCY34 0-30 0J3M 0-38 0C74 0-30 1-432 0-42 2N2240 0-45 BCY39 1-00 0J5M 0-25 0C75 0-25 1-437 0-26 2N2240 0-25 BCY42 0-25 He1000 0-50 0C77 0-00 1-432 0-42 2N2240 0-25 BCY42 0-25 He1000 0-50 0C77 0-00 1-432 0-22 2N2240 0-25 BCY42 0-25 He1000 0-50 0C77 0-00 1-434 0-00 0-22 2N2224 0-28 BCZ10 0-36 MAT101 0-36 0C81 0-20 1-434 0-00 0-22 2N2224 0-28 BCZ10 0-36 MAT101 0-36 0C81 0-20 1-434 0-00 0-22 2N2224 0-28 BCZ10 0-36 MAT101 0-30 0C81 0-20 1-434 0-00 0-22 2N2224 0-16 BCZ11 0-50 MAT120 0-26 0C81 0-20 1-434 0-00 0-22 2N2226 0-16 BCZ11 0-50 MAT120 0-26 0C81 0-20 1-434 0-00 0-22 2N2226 0-16 BCZ11 0-50 MAT120 0-26 0C81 0-20 1-434 0-00 0-22 2N2326 0-16 BCZ11 0-50 MAT120 0-26 0C81 0-20 1-434 0-00 0-22 2N3060 0-76 BD124 0-76 MJE2520 1-37 0C81Z 0-40 1-434 0-0 0-22 2N3060 0-76 BD124 0-76 MJE2520 1-37 0C81Z 0-40 1-434 0-0 0-22 2N3060 0-76 BD124 0-76 MJE2520 1-37 0C81Z 0-40 1-434 0-0 0-22 2N3070 0-10 BF116 0-28 NKT128 0-36 0C83 0-26 1-47 0-2 0-2 2N3070 0-10 BF116 0-32 NKT126 0-36 0C83 0-26 1-47 0-2 0-2 2N3070 0-10 BF116 0-32 NKT126 0-36 0C83 0-26 1-47 0-2 0-2 2N3070 0-10 BF116 0-32 NKT126 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF116 0-36 NKT127 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF116 0-36 NKT127 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF116 0-36 NKT126 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF116 0-36 NKT127 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF186 0-30 NKT126 0-36 0C83 0-26 1-47 0-3 0-2 2N3070 0-10 BF186 0-30 NKT126 0-36 0C83 0-26 0-26 0-26 0-26 0-26 0-26 0-26 0-26	2N2147 0.75	BC160 0-68	GET881	0.25	C141538	0.80	7422	0.48
Section   Sect	2N2148 0-60	BC169 0.13	GET882	0.25	OC59	0.65	7423	0·48 0·48
2N32916	2N2218 0-90		GEX 44	0.08	OC66		7427	0.42
2N34994 0-16 BCY39 0-30 G33NN 0-25 C77 0-30 7-33 0-2 N3636 0-46 BCY39 1-00 GJ3NN 0-25 C77 0-30 7-433 0-2 N3636 0-46 BCY39 1-00 GJ3NN 0-36 C77 0-30 7-433 0-2 N3636 0-46 BCY39 1-00 GJ3NN 0-37 C776 0-25 7-437 0-2 N37904 0-25 BCY42 0-25 H61005 0-57 C776 0-25 7-437 0-2 N37906 0-25 BCY10 0-30 MAT100 0-26 C77 0-20 7-441 \ N. 0 0-2 N37906 0-28 BCY10 0-30 MAT100 0-26 C77 0-20 7-441 \ N. 0 0-2 N37924 0-28 BCZ10 0-36 MAT101 0-30 C681 0-20 7-431 0-2 N37924 0-28 BCZ10 0-36 MAT101 0-30 C681 0-20 7-431 0-2 N37924 0-28 BCZ10 0-36 MAT101 0-30 C681 0-20 7-431 0-2 N37924 0-28 BCZ11 0-50 MAT102 0-26 C681 0-20 7-431 0-2 N37925 0-10 BCZ11 0-50 MAT102 0-26 C681 0-20 7-431 0-2 N37925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-2 N37925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-2 N37925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-2 N37925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-3 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-3 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C681 0-20 7-431 0-3 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-681 7-490 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-30 C683 0-50 C683 0-50 C79 0-7473 0-3 N3925 0-10 BCZ11 0-50 MAT102 0-3 N5025 0-10 BCZ11 0-10	2N2219 0.20		. GEX 45/1	0.10	OC71	0.12		0-50
2N32613			GEX941	0.15	OC72	0.20		0.20 0.42
2873904 0-28 BCY40 0-80 (37) M 0-29 (077 0-28) 7-434 N 0-29 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0-28 (27) 0	2N2613 0-28	BCY38 0-40			DC74		7433	0.70
2879904 0.926 BCY42 0.25 HG1005 0.50 C676 0.25 443 0.25 2879906 0.25 BCY20 0.15 HB100A 0.20 0C77 0.40 7441 AN 0.5 287907 0.23 BCY71 0.30 MAT100 0.25 0C78 0.20 7441 AN 0.5 287907 0.23 BCY71 0.30 MAT100 0.30 0C81 0.20 7441 AN 0.5 287907 0.23 BCY71 0.30 MAT100 0.30 0C81 0.20 7442 0.2 287922 0.16 BCZ11 0.50 MAT101 0.30 0C81 0.20 7453 0.2 287922 0.16 BCZ11 0.50 MAT101 0.30 0C81 0.20 7453 0.2 287922 0.16 BCZ11 0.50 MAT102 0.30 0C81 0.20 7453 0.2 287922 0.16 BCZ11 0.50 MAT102 0.30 0C81 0.20 7453 0.2 287932 0.10 BD121 0.55 MAT121 0.30 0C81 0.20 7453 0.2 2879306 0.50 BD123 0.80 MJE292 0.87 0C81DM 0.20 7453 0.2 2879306 0.75 BD124 0.75 MJE295 1.37 0C81DM 0.18 7454 0.2 2879306 0.10 BP116 0.20 NKT128 0.36 0C83 0.20 7472 0.2 2879306 0.10 BP116 0.20 NKT129 0.30 0C83 0.25 7474 0.2 2879306 0.10 BP116 0.20 NKT129 0.30 0C83 0.25 7474 0.2 287930 0.10 BP181 0.85 NKT211 0.25 0C84 0.25 7474 0.2 287930 0.10 BP181 0.25 NKT211 0.25 0C84 0.25 7474 0.2 287930 0.10 BP181 0.25 NKT213 0.25 0C84 0.25 7474 0.2 287930 0.10 BP181 0.25 NKT214 0.15 0C64 0.2 0.2 0KT215 0.2 0KT2	2N2646 •0-45	BCY39 1.00	GJ5M	0.25	OC75	0.25	7437	0.85
287906 0-29 BCY70 0-15 HS100A 0-20 C678 0-20 [7441AN 0-22 287927 0-28 BCY710 0-36 MAT100 0-36 C678 0-20 [745] 0-32 287922 0-16 BCZ11 0-50 MAT101 0-30 C681 0-20 [745] 0-32 287922 0-16 BCZ11 0-50 MAT102 0-36 C681 0-20 [745] 0-32 287922 0-16 BD121 0-55 MAT102 0-30 C681 0-20 [745] 0-32 287926 0-10 BD123 0-80 MAT102 0-30 C681 0-20 [745] 0-32 287936 0-50 BD124 0-75 MJE295 1-37 C681 0-20 [745] 0-32 287936 0-10 BDY11 1-82 MJE295 1-37 C681 0-30 [747] 0-32 287936 0-10 BDY11 1-82 MJE295 1-37 C681 0-30 [747] 0-32 287936 0-10 BDY11 1-82 MJE295 1-37 C681 0-30 [747] 0-32 287936 0-23 BF117 0-50 KKT129 0-30 C681 0-30 [747] 0-32 287936 0-32 BF117 0-50 KKT129 0-30 C681 0-30 [747] 0-32 287936 0-10 BF118 0-35 KKT211 0-35 C681 0-30 [747] 0-32 287930 0-10 BF181 0-35 KKT213 0-35 C61 0-38 [747] 0-32 287930 0-10 BF181 0-35 KKT213 0-35 C61 0-38 [747] 0-32 287930 0-10 BF181 0-35 KKT213 0-35 C61 0-38 [747] 0-32 287930 0-36 BF184 0-30 KKT216 0-35 (C613) 0-35 [748] 0-32 287930 0-38 BF185 0-20 KKT217 0-35 C6139 0-35 [748] 0-32 287930 0-38 BF185 0-30 KKT216 0-33 (C613) 0-35 [748] 0-32 287930 0-36 BF186 0-30 KKT216 0-33 (C613) 0-35 [748] 0-32 28793 0-38 BF186 0-30 KKT212 0-38 (C613) 0-35 [748] 0-32 28793 0-38 BF185 0-30 KKT212 0-32 (C613) 0-35 [748] 0-32 28793 0-38 BF185 0-38 KKT213 0-35 (C613) 0-35 [748] 0-32 28793 0-38 BF185 0-38 KKT212 0-35 (C613) 0-35 [748] 0-32 28793 0-36 BF186 0-38 KKT212 0-35 (C613) 0-35 [748] 0-32 28793 0-36 BF186 0-38 KKT212 0-35 (C613) 0-35 [749] 0-32 28793 0-36 BF186 0-38 KKT212 0-35 (C613) 0-30 [749] 0-32 28793 0-30 BF187 0-38 KKT213 0-35 (C613) 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [749] 0-30 [		BCY 40 0.80		0-87	OC76		7440	0.65
2N3925 0-16 BCZ11 0-50 MAT121 0-25 OC811 0-20 (4-91) 2-20 2N3926 0-10 BD121 0-65 MAT121 0-25 OC811 0-20 (4-91) 2-20 2N3926 0-75 BD124 0-75 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-76 BD124 0-75 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-85 OC82 0-85 (4-70) 0-20 2N3926 0-10 BD121 0-20 NKT129 0-30 OC88 0-85 (4-70) 0-20 2N3926 0-10 BD121 0-20 NKT129 0-30 OC88 0-85 (4-70) 0-20 2N39270 0-10 BF167 0-25 NKT211 0-25 OC84 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39271 0-10 BF184 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N39271 0-10 BF185 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N39271 0-10 BF185 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N3928 0-85 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N392 0-25 OC230 0-50 (4-74) 0-40 2N392 0-25 OC230 0-40 (4-74) 0-40 C740 0-40 2N392 0-25 OC230 0-40 (4-74) 0-40 C740 0-40 2N392 0-40	2N2906 -0.20	BCY 42 0.25 BCY 70 0.15			0077		7441AN	0.75
2N3925 0-16 BCZ11 0-50 MAT121 0-25 OC811 0-20 (4-91) 2-20 2N3926 0-10 BD121 0-65 MAT121 0-25 OC811 0-20 (4-91) 2-20 2N3926 0-75 BD124 0-75 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-76 BD124 0-75 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-87 OC812 0-40 (4-91) 2-20 2N3926 0-10 BD121 1-82 MJE2925 1-85 OC82 0-85 (4-70) 0-20 2N3926 0-10 BD121 0-20 NKT129 0-30 OC88 0-85 (4-70) 0-20 2N3926 0-10 BD121 0-20 NKT129 0-30 OC88 0-85 (4-70) 0-20 2N39270 0-10 BF167 0-25 NKT211 0-25 OC84 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39270 0-10 BF181 0-35 NKT214 0-35 OC83 0-25 (4-74) 0-40 2N39271 0-10 BF184 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N39271 0-10 BF185 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N39271 0-10 BF185 0-20 NKT216 0-37 OC123 0-85 (4-74) 0-40 2N3928 0-85 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N3928 0-33 BF195 0-15 NKT212 0-25 OC130 0-25 (4-74) 0-40 2N392 0-25 OC230 0-50 (4-74) 0-40 2N392 0-25 OC230 0-40 (4-74) 0-40 C740 0-40 2N392 0-25 OC230 0-40 (4-74) 0-40 C740 0-40 2N392 0-40	2N2907 0-28	BCY71 0-90	MAT100	0.25	OC79		7442	0.75
2N90268 * 0.10   BD121   0.85   MAT121   0.80   CS81M   0.80   7453   0.82   2N9055   0.76   BD124   0.75   MIE2250   1.87   0.87   0.812   0.40   7490   0.82   2N93706   0.10   BD141   1.82   MIE2250   1.87   0.82   0.88   7470   0.82   2N93706   0.10   BD141   1.82   MIE2250   1.87   0.82   0.88   7470   0.82   2N93706   0.28   BF117   0.50   0.8K129   0.80   0.683   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0.82   0		BCZIO 0.85	MAT101		OC81		7451	0·20 0·20
2N30054   0-56   BD123   0-80   MJEE295   0-87   OCS1DM   0-18   7454   0-52   2N3702   0-10   BDY11   1-62   MJE2955   0-87   OCS12   0-40   7470   0-52   2N3706   0-10   BF116   0-26   NKT128   0-85   OCS20   0-85   7473   0-82   2N3706   0-10   BF116   0-26   NKT128   0-85   OCS20   0-85   7473   0-82   2N3707   0-12   BF16   0-25   NKT211   0-25   OCS4   0-85   7473   0-82   2N3709   0-10   BF187   0-25   NKT211   0-25   OCS4   0-85   7474   0-82   2N3710   0-10   BF181   0-35   NKT211   0-25   OCS4   0-85   7474   0-82   2N3710   0-10   BF181   0-35   NKT214   0-18   OC122   0-60   7476   0-82   2N3910   0-85   BF185   0-20   NKT216   0-37   OC123   0-65   7482   0-82   2N5089   0-35   BF185   0-20   NKT216   0-37   OC123   0-65   7482   0-82   2N5089   0-33   BF195   0-15   NKT212   0-25   OC134   0-85   7482   0-82   2N5089   0-33   BF195   0-15   NKT212   0-25   OC134   0-85   7483   0-82   2N5080   0-37   BF861   0-28   NKT251   0-24   OC171   0-80   7491   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0-8   0			MAT120	0.80	OC81D	0.20	7453	0.20
2N3702	2N3054 0.50	BD123 0-80	MJE520	0.87	OC81DM	0.18	7454	0.20
2N3706 0-10   BF115	2N3055 0-75	BD124 0.75	MJE2955	1.87	OC81Z	0.40	7460	0.20
2N3706   0.28   BF117   0.50   NKT121   0.25   0.280   0.281   0.281   7473   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481   0.481	2N3702 0-10 2N3705 0-10	BDY11 1.02	MJE3055	0.85			7472	0-80
2N37109 0-10 BF181 0-85 KKT214 0-181 0-182 0-80 7476 0-4 2N3711 0-10 BF184 0-80 KKT214 0-181 0-102 0-80 7476 0-4 2N3819 0-85 BF185 0-90 KKT216 0-37   0-1023 0-85 7489 0-8 2N30807 0-83 BF195 0-15 KKT214 0-181 0-192 0-95 7489 0-8 2N5087 0-83 BF195 0-15 KKT216 0-37   0-1023 0-85 7489 0-8 2N5087 0-84 BF185 0-90 KKT217 0-35 0-139 0-95 7489 0-8 2R5091 0-50 BF196 0-15 KKT210 0-38   0-104 0-35 7489 0-8 2R5091 0-50 BF197 0-15 KKT210 0-38   0-104 0-80 7484 0-6 2R5091 0-75 BF197 0-15 KKT210 0-22   0-107 0-95 7490 0-7 2R501 0-37 BF861 0-38   0-104 0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107   0-107	2N3706 0-28	BF117 0.50	NKT129	0.80	OC83	0-25	7473	0.40
2N87110 0-10 BF181 0-20 NKT216 0-37   OCI223 0-80 74780 0-82 2N85027 0-83 BF184 0-20 NKT216 0-37   OCI232 0-85 0-7480 0-82 2N85027 0-83 BF194 0-17 NKT218 1-13 OCI44 0-85 7480 0-85 2N85027 0-83 BF194 0-17 NKT218 1-13 OCI44 0-85 7480 0-85 2N85027 0-83 BF195 0-15 NKT210 0-38 0-14 0-85 7480 0-85 2N85027 0-83 BF195 0-15 NKT210 0-38 0-14 0-85 7480 0-85 2N85027 0-80 0-80 0-80 0-80 0-80 0-80 0-80 0-8	2N3707 0-12	BF167 0.25	NKT211	0.25	OC84		7474	0-40 0-55
2N8511 0-10 BF184 0-20 NKT216 0-37   OC123 0-86   7480   OC28304 0-80   BF195   O-17 NKT218 1-13   OC140 0-35   7482   OC28304 0-76   BF195   O-16 NKT216 0-37   OC169   O-25   7482   OC28304 0-76   BF197   O-15 NKT218   O-13   OC140   O-35   7483   OC141   O-35   7482   OC28304   O-76   BF197   O-15 NKT218   O-13   OC140   O-35   7483   OC141   O-35   7483   OC141   O-35   O-36   O-37   O-36   O-36   O-37   O-36   O-36	2N3710 0-10	BF181 0-85	NKT914	0.15	OC114 LOC122	0.80	7476	0-45
2800027 0-83 BF195 0-16 NKT210 0-38 0C141 0-35 1-493 28500 0-30 BF196 0-15 NKT210 0-38 0C141 0-30 1-494 0-62 28504 0-75 BF197 0-15 NKT212 0-20 0C169 0-80 1-494 0-62 28504 0-75 BF197 0-15 NKT222 0-20 0C169 0-80 1-494 0-62 28504 0-75 BF197 0-15 NKT224 0-20 0C170 0-85 1-490 0-75 28504 0-75 BF197 0-15 NKT224 0-20 0C170 0-85 1-490 0-75 28504 0-75 BF197 0-15 NKT224 0-20 0C171 0-30 1-491 N 1-40 0-62 0-80 1-491 0-89 NKT251 0-24 0C171 0-30 1-491 N 1-40 0-62 0-80 1-491 0-89 NKT251 0-26 0C200 0-70 1-492 0-70 0-70 0-80 1-491 0-70 0-70 0-70 0-70 0-70 0-70 0-70 0-7	2N3711 0-10	BF184 0-20	NKT216	0.37	OC123	0.85	7480	0.80
28301	2N3019 -0.85	BF185 0-20	NKT217		OC139	0-25		0.87 1.00 (
28891         0-50         BF196         1-15         NKT222         0-80         OC168         0-26         1-490         0-7           28504         0-75         BF196         0-15         NKT224         0-22         OC170         0-28         1-490         0-7           28501         0-82         BF898         0-28         NKT251         0-24         OC171         0-30         7491AN         1-2           28702         0-80         BFX11         0-26         NKT271         0-25         OC200         0-70         7492         0-7           AAZ12         0-80         BFX13         0-26         NKT271         0-80         OC200         0-70         7492         0-7           AAZ13         0-12         BFX29         0-25         NKT274         0-30         OC20         0-60         7494         0-8           AC126         0-25         BFX39         0-25         NKT277         0-80         OC20         0-75         7499         0-8           AC128         0-25         BFX39         0-25         NKT276         OS26         OC20         0-75         7410         9-8           AC127         0-25         BFX85         0-80	2N5088 0-88	BF195 0-15	NKT210	0.88			7484	0.90
28501 0-87 BF861 0-28 NKT271 0-25 CC200 0-40 7492 0-2 AA129 0-80 BFX12 0-90 NKT272 0-25 CC200 0-40 7492 0-2 AA212 0-80 BFX13 0-35 NKT273 0-15 CC202 0-70 7493 0-8 AA213 0-12 BFX29 0-25 NKT274 0-90 CC203 0-40 7494 0-8 AC107 0-87 BFX39 0-25 NKT274 0-90 CC203 0-40 7494 0-8 AC107 0-87 BFX39 0-25 NKT275 0-90 CC204 0-40 7496 1-0 AC126 0-20 BFX35 0-98 NKT275 0-90 CC205 0-75 7497 0-8 AC128 0-20 BFX35 0-98 NKT275 0-90 CC206 0-76 7499 1-0 AC128 0-20 BFX85 0-80 NKT276 0-20 CC206 0-76 7496 1-0 AC128 0-20 BFX85 0-80 NKT276 0-20 CC206 0-76 7497 0-20 AC128 0-20 BFX85 0-80 NKT276 0-20 CC207 0-90 74100 0-20 AC128 0-20 BFX85 0-80 NKT276 0-20 CC207 0-90 74107 0-20 AC128 0-20 BFX85 0-80 NKT304 0-75 CC460 0-20 74110 0-2 AC128 0-20 BFX85 0-80 NKT304 0-75 CC460 0-20 74110 0-2 AC127 0-30 BFX87 0-25 NKT304 0-75 CC460 0-20 74110 0-2 AC128 0-20 BFX87 0-25 NKT304 0-75 CC460 0-20 74111 0-2 AC128 0-20 BFX87 0-25 NKT304 0-75 CC460 0-20 74111 0-2 AC129 0-25 BFX10 1-00 NKT678 0-80 ORP12 0-50 74119 1-2 AC129 0-25 BFX10 1-00 NKT678 0-80 ORP12 0-50 74119 1-2 AC120 0-20 BFY11 0-25 NKT777 0-82 SIBT 0-50 7412 0-6 AC127 0-25 BFY19 0-25 0-50 SB SIBT 0-80 NF777 0-80 SB SIBT 0-80 NF787 0-7 AC128 0-70 BFY19 0-70 0-70 NF778 0	28801 0-50	BF196 0-15	NKT222	0.20	OC169	0.20		0.45
28703 0-82 BF898 0-28 NKT271 0-25 OC200 0-40 7492 0-2 AAZ12 0-80 BFX12 0-20 NKT272 0-25 OC201 0-70 7493 0-7 AAZ12 0-80 BFX12 0-20 NKT272 0-25 OC201 0-70 7493 0-7 AAZ13 0-12 BFX29 0-25 NKT274 0-20 OC202 0-80 7494 0-7 CC107 0-87 BFX30 0-85 NKT277 0-80 OC203 0-40 7495 0-8 CC107 0-87 BFX30 0-85 NKT277 0-80 OC203 0-40 7495 0-8 CC108 0-90 BFX35 0-98 NKT277 0-80 OC203 0-40 7495 0-8 CC108 0-80 BFX35 0-98 NKT277 0-80 OC203 0-75 7497 0-8 CC108 0-80 BFX35 0-98 NKT277 0-80 OC203 0-90 74100 0-8 CC108 0-85 BFX86 0-85 NKT301 0-40 OC207 0-90 74107 0-8 CC108 0-85 BFX86 0-85 NKT301 0-40 OC207 0-90 74107 0-8 CC108 0-85 BFX86 0-85 NKT304 0-75 OC470 0-80 74111 1-8 CCY10 0-80 BFX17 0-25 NKT403 0-75 OC470 0-80 74111 1-8 CCY10 0-80 BFX19 1-00 NKT713 0-25 ORP10 0-80 74119 1-5 CCY20 0-90 BFY11 0-90 NKT713 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-95 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 NKT730 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 OA5 0-80 BFX30 0-80 NKT304 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 OA5 0-80 BFX30 0-80 NKT304 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY11 0-85 OA5 0-80 BFX30 0-80 NKT304 0-85 ORP10 0-40 74121 1-8 CCY21 0-80 BFY16 0-80 OA5 0-80 BFX30 0-80 NKT304 0-85 OA5 0-80 RFX30 0-80 NKT304 0-85 OA5 0-80 NKT304 0-85		BF197 0-15	NKT224	0.22	OC170			0.75 # 1.00
AAZ129 0-80 BFX13 0-86 KKT273 0-15   C0202 0-70   4493 0-80   AAZ13 0-12 BFX29 0-25 KKT274 0-50   C0203 0-40   7495 0-80   AAZ13 0-12 BFX29 0-25 KKT274 0-50   C0203 0-40   7495 0-80   AAZ13 0-12 BFX29 0-25 KKT274 0-50   C0203 0-40   7495 0-80   AAZ13 0-12 BFX29 0-25 KKT274 0-50   C0204 0-40   7496 1-6   C0204   C0205 0-75   C020	28703 0-62	BF898 0-28	NKT271	0.95	OC200	0-80	7492	0.75
AC126 0-26 BFX35 0-50 NKT278 0-25 C206 0-75 7497 0-80 AC127 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX35 0-30 NKT278 0-25 C207 0-90 74100 2-8 AC188 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-30 BFX87 0-25 NKT303 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC460 0-90 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT404 0-56 OCF71 0-97 74118 1-0 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 FX12 0-40 AC187 0-40 BFX17 0-25 NKT777 0-88 S18T 0-80 74123 2-7 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-	AA129 0.20	BFX 12 0:20	NKT272	0.25	0.0003	0.70	7493	0.75
AC126 0-26 BFX35 0-50 NKT278 0-25 C206 0-75 7497 0-80 AC127 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX35 0-30 NKT278 0-25 C207 0-90 74100 2-8 AC188 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-30 BFX87 0-25 NKT303 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC460 0-90 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT404 0-56 OCF71 0-97 74118 1-0 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 FX12 0-40 AC187 0-40 BFX17 0-25 NKT777 0-88 S18T 0-80 74123 2-7 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-	AAZ12 0-80	BFX13 0.25		0.36	OC202	0.80		0.80
AC126 0-26 BFX35 0-50 NKT278 0-25 C206 0-75 7497 0-80 AC127 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX36 0-50 NKT278 0-25 C206 0-90 74100 2-8 AC128 0-25 BFX35 0-30 NKT278 0-25 C207 0-90 74100 2-8 AC188 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-25 BFX35 0-30 NKT304 0-75 OC460 0-20 74110 0-8 AC187 0-30 BFX87 0-25 NKT303 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC460 0-90 74110 0-8 AC187 0-30 BFX87 0-25 NKT304 0-75 OC470 0-30 74110 0-8 AC187 0-30 BFX87 0-25 NKT404 0-56 OCF71 0-97 74118 1-0 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-25 BFX10 1-00 NKT713 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 74121 0-6 AC187 0-20 BFX11 0-25 ORF01 0-40 FX12 0-40 AC187 0-40 BFX17 0-25 NKT777 0-88 S18T 0-80 74123 2-7 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-70 BFX17 0-70 AC182 0-	AC107 0-87	BFX30 0-25	NKT275	0.25			7496	1.00
ACU18 0-25 BFX88 0-25 NKT-043 0-75 OC470 0-80 7-1111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AC126 0.20	BFX 35 0-98	NKT277	0.20	OC205	0-75	7497	6-25
ACU18 0-25 BFX88 0-25 NKT-043 0-75 OC470 0-80 7-1111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AC127 0-25	BEX83 0.80	NKT278	0.25	OC206	0.90		2-50 0-50
AC188 0-25 BFX88 0-25 NKT940 0-55 OC770 0-30 74111 1 1-4 AC117 0-30 BFX87 0-25 NKT940 0-55 OC771 0-97 74118 1-4 AC118 0-25 BFX81 0-25 NKT948 0-30 NKT973 0-25 ORP91 0-50 74119 1-6 AC1910 0-25 BFY10 1-00 NKT973 0-25 ORP96 0-40 74121 0-6 AC192 0-20 BFY11 0-25 NKT773 0-25 ORP96 0-40 74121 0-6 AC192 0-20 BFY11 0-25 OA5 0-20 SB718 0-38 SB17 0-30 74121 1-2 AC192 0-50 BFY18 0-25 OA5 0-20 SF7308 0-38 SB170 0-30 AF718 0-45 OA5 0-20 SF7308 0-38 SB170 0-30 AF718 0-45 OA5 0-20 SF7308 0-38 AC20 0-25 F7308 0-38 SB170 0-30 OA7 0-10 SF730 0-30 OA8 0-10 SF73	AC187 0-25	BFX85 0-80	NKT304	0.75	OC460			0-80
ACY18 0-25 BFY38 0-20 NKT673 0-25 ORP60 0-40 74121 0-6 ACY19 0-25 BFY10 1-00 NKT713 0-25 ORP60 0-40 74121 0-6 ACY20 0-20 BFY11 1-25 NKT773 0-25 ORP60 0-40 74121 0-6 ACY21 0-20 BFY11 0-25 NKT773 0-25 ORP60 0-40 74122 3-7 ACY22 0-10 BFY17 0-25 NKT773 0-25 SH20 0-20 0-20 SH218 0-25 ORP60 0-40 74123 2-7 ACY22 0-10 BFY18 0-25 ORP60 0-38 SH20 0-35 74141 1-6 ACY27 0-25 BFY19 0-25 OA5 0-20 SF730 0-38 AC40 0-25 74141 1-6 ACY27 0-25 BFY19 0-25 OA5 0-20 SF730 0-38 74150 1-2 ACY40 0-16 BFY44 1-00 0-47 0-10 ST231 0-63 74151 1-7 ACY40 0-16 BFY50 0-22 OA70 0-10 SK631 0-63 74151 1-7 ACY41 0-16 BFY50 0-20 OA71 0-10 SK631 0-80 74152 1-8 ACY41 0-25 BFY00 0-25 OA70 0-10 SK631 0-80 74155 1-8 ACY41 0-25 BFY00 0-45 OA81 0-08 SK642 0-50 74157 1-8 ACY41 0-25 BFY00 0-65 OA81 0-08 SK644 0-55 74174 2-6 ACY41 0-27 BFY90 0-65 OA81 0-08 SK644 0-55 74174 2-6 ACY41 0-27 BFY90 0-65 OA81 0-08 SK644 0-75 74175 1-8 ACY41 0-28 BSX76 0-10 OA85 0-12 SK641 0-55 74176 1-8 ACY11 0-25 BSX76 0-13 OA90 0-00 V16/30P 0-50 V30/201P 0-75 V4176 1-8 ACY11 0-25 BSX76 0-13 OA90 0-00 V30/201P 0-75 V4176 1-8 ACY11 0-25 BSX76 0-13 OA90 0-00 V30/201P 0-75 V4193 0-00 ACY11 0-25 BSX76 0-10 OA85 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-10 SK631 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-10 SK631 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-10 SK631 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-00 SK631 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-00 SK631 0-10 V30/201P 0-75 V4193 0-00 ACY11 0-00	AC188 0-25	BFX86 0-25	NKT403	0.75	OC470	0.80	74111	1.45
ACY20 0-20 BFY11 0-25 NKT777 0-25 NRP61 0-42 74122 1:2 ACY21 0-10 BFY18 0-25 078B 0-38 816T 0-30 74123 2:2 ACY22 0-10 BFY18 0-25 078B 0-38 816T 0-30 74123 2:2 ACY23 0-17 BFY24 0-45 0A5 0-20 8F7308 0-88 74145 1:0 ACY36 0-18 BFY44 1-00 0-45 0A7 0-10 8T723 0-88 74150 1:0 ACY40 0-16 BFY46 0-22 0A70 0-10 8T723 0-88 74151 1:0 ACY41 0-16 BFY56 0-20 0A70 0-10 8X631 0-83 74151 1:0 ACY41 0-18 BFY56 0-20 0A70 0-10 8X635 0-80 74154 1:0 ACY41 0-18 BFY56 0-22 0A73 0-10 8X635 0-80 74155 1:0 ACY41 0-28 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY69 0-66 0A81 0-08 8X641 0-550 74176 1:0 AD140 0-50 BFY69 0-66 0A81 0-08 8X644 0-75 74176 1:0 AD140 0-50 BF808 0-93 0A80 0-12 8X644 0-75 74176 1:0 AF116 0-25 B8X27 0-10 0A85 0-12 8X644 0-75 74176 1:0 AF116 0-25 B8X26 0-15 0A99 0-00 V16/30P 0-50 74199 1:0 AF118 0-26 B8X6 0-10 0A99 0-00 V16/30P 0-75 74191 1:0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74191 1:0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-75 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-26 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-55 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 2.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00	ACY17 0-80	BEX87 0.25	NKT404	0.85	OCP71	0.97		1.00
ACY20 0-20 BFY11 0-25 NKT777 0-25 NRP61 0-42 74122 1:2 ACY21 0-10 BFY18 0-25 078B 0-38 816T 0-30 74123 2:2 ACY22 0-10 BFY18 0-25 078B 0-38 816T 0-30 74123 2:2 ACY23 0-17 BFY24 0-45 0A5 0-20 8F7308 0-88 74145 1:0 ACY36 0-18 BFY44 1-00 0-45 0A7 0-10 8T723 0-88 74150 1:0 ACY40 0-16 BFY46 0-22 0A70 0-10 8T723 0-88 74151 1:0 ACY41 0-16 BFY56 0-20 0A70 0-10 8X631 0-83 74151 1:0 ACY41 0-18 BFY56 0-20 0A70 0-10 8X635 0-80 74154 1:0 ACY41 0-18 BFY56 0-22 0A73 0-10 8X635 0-80 74155 1:0 ACY41 0-28 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY68 0-42 0A73 0-10 8X635 0-40 74156 1:0 AD140 0-50 BFY69 0-66 0A81 0-08 8X641 0-550 74176 1:0 AD140 0-50 BFY69 0-66 0A81 0-08 8X644 0-75 74176 1:0 AD140 0-50 BF808 0-93 0A80 0-12 8X644 0-75 74176 1:0 AF116 0-25 B8X27 0-10 0A85 0-12 8X644 0-75 74176 1:0 AF116 0-25 B8X26 0-15 0A99 0-00 V16/30P 0-50 74199 1:0 AF118 0-26 B8X6 0-10 0A99 0-00 V16/30P 0-75 74191 1:0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74191 1:0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF119 0-20 B8X55 0-12 0A20 0-05 X1610 0-75 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-75 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-25 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-26 BRY01 0-80 0-80 X1610 0-16 74193 2.0 AF118 0-55 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 2.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-16 74193 4.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00 R 0A2200 0-55 X1610 0-10 VP1/01 1.0 AF118 0-56 BTY91/00	ACY19 -0-25	BFY10 1.00	NKT713	0.25			74121	1.90 0.80
ACY22 0-10 BYF18 0-25 078B 0-38 8AC40 0-25 74141 1-6 ACY27 0-25 BFY19 0-25 0A5 0-20 8F7308 0-38 74145 1-6 ACY28 0-17 BFY24 0-45 0A6 0-12 8T722 0-38 74151 1-2 ACY30 0-50 BFY44 1-00 0A47 0-10 8T7231 0-63 74151 1-2 ACY40 0-16 BFY50 0-22 0A70 0-10 8X681 0-80 74154 1-2 ACY41 0-16 BFY50 0-22 0A70 0-10 8X68 0-20 74154 1-2 ACY41 0-16 BFY50 0-22 0A70 0-10 8X681 0-80 74155 1-6 ACY41 0-25 BFY50 0-20 0A71 0-10 8X685 0-40 74156 1-6 ACY41 0-25 BFY50 0-42 0A73 0-10 8X635 0-40 74156 1-6 AD140 0-50 BFY50 0-42 0A73 0-10 8X635 0-40 74156 1-6 AD140 0-50 BFY50 0-42 0A73 0-10 8X635 0-40 74156 1-6 AD140 0-50 BFY50 0-45 0A81 0-08 8X642 0-55 74170 1-6 AD140 0-50 BFY50 0-65 0A81 0-08 8X642 0-55 74170 1-6 AF116 0-25 B8X27 0-10 0A85 0-12 8X644 0-75 74176 1-6 AF116 0-25 B8X26 0-13 0A98 0-10 8X644 0-75 74176 1-6 AF116 0-25 B8X26 0-13 0A98 0-10 8X644 0-75 74176 1-6 AF116 0-25 B8X26 0-13 0A98 0-00 V30/2019 0-75 74176 1-6 AF117 0-25 B8X26 0-10 0A91 0-00 V30/2019 0-75 74191 1-6 AF118 0-62 B8850 0-32 0A20 0-00 V30/2019 0-75 74193 2-0 AF118 0-62 B8850 0-32 0A20 0-05 XA101 0-10 74193 2-0 AF118 0-62 B8850 0-32 0A200 0-05 XA101 0-10 74193 2-0 AF118 0-62 B8850 0-32 0A200 0-05 XA101 0-10 74193 2-0 AF118 0-62 B8850 0-32 0A200 0-05 XA101 0-10 74193 2-0 AF125 0-20 BTY9100R 0A2201 0-05 XA101 0-10 74193 2-0 AF127 0-17 BTY9100R 0A2201 0-05 XA101 0-15 74191 1-6 AF118 0-62 B8860 0-75 0A2200 0-05 XA101 0-15 74193 1-6 AF118 0-65 BTY9100R 0A2201 0-05 XA101 0-15 74193 1-6 AF118 0-65 BTY9100R 0A2201 0-05 XA101 0-15 74193 1-6 AF118 0-65 BTY9100R 0A2201 0-04 XA101 0-15 74193 1-6 AF118 0-65 BTY9100R 0A2201 0-04 XA101 0-05 1-10 1-10 1-10 1-10 1-10 1-10 1	ACY20 0.20	BFY11 1.25	NKT773	0.25	ORP61	0.42	74122	1.85
ACY27 0.25 BFY19 0.25 OA5 0.20 BFT308 0.38 74145 1.6 ACY39 0.50 BFY44 1.00 OA47 0.10 BT7231 0.63 74151 3.3 ACY40 0.15 BFY56 0.22 OA70 0.10 BT231 0.63 74151 2.2 ACY41 0.15 BFY56 0.22 OA70 0.10 SK631 0.30 74154 2.0 ACY41 0.16 BFY56 0.22 OA70 0.10 SK631 0.30 74154 2.0 ACY41 0.15 BFY56 0.22 OA73 0.10 SK631 0.30 74154 2.0 ACY44 0.25 BFY56 0.22 OA73 0.10 SK631 0.30 74155 1.8 AD149 0.50 BFY68 0.21 OA74 0.10 SK631 0.50 74156 1.5 AD140 0.50 BFY69 0.25 OA73 0.10 SK630 0.50 74157 1.2 AD161 0.50 BFY69 0.42 OA79 0.10 SK640 0.55 74170 4.1 AD162 0.87 BSX27 0.40 0.485 0.12 SK640 0.55 74170 4.1 AD164 0.26 BSX67 0.45 0.486 0.48 SK642 0.60 74174 2.1 AF116 0.25 BSX27 0.40 0.485 0.12 SK646 0.75 74175 1.3 AF116 0.25 BSY27 0.17 0.485 0.18 OA90 0.00 V15/309 0.50 74190 1.8 AF116 0.25 BSY27 0.17 0.495 0.07 V60/201 0.50 74190 1.8 AF117 0.25 BSY27 0.17 0.45 0.40 0.00 V15/309 0.50 74190 1.8 AF118 0.25 BSY27 0.17 0.45 0.40 0.00 V15/309 0.50 74190 1.8 AF119 0.20 BSY25 0.12 0.400 0.07 V60/201 0.50 74190 1.8 AF124 0.25 BSY27 0.17 0.4020 0.07 V60/201 0.50 74190 1.8 AF125 0.20 BSY25 0.12 0.4020 0.50 SK162 0.10 1.10 74190 1.8 AF126 0.26 BSY26 0.12 0.4020 0.07 V60/201 0.50 74190 1.8 AF127 0.75 0.4020 0.4020 0.07 V60/201 0.75 74190 1.8 AF127 0.75 0.4020 0.4020 0.07 V60/201 0.75 74190 1.8 AF127 0.75 0.4020 0.4020 0.07 V60/201 0.75 74190 1.8 AF127 0.75 0.4020 0.4020 0.4020 0.10 74190 1.8 AF128 0.26 BY49 0.40 0.4020 0.40 0.40 0.10 74190 1.8 AF127 0.75 0.4020 0.4020 0.4020 0.10 0.10 74190 1.8 AF128 0.56 BY49 0.4020 0.4020 0.4020 0.10 0.10 74190 1.8 AF129 0.50 BY49 0.4020 0.4020 0.40 0.4020 0.10 0.10 74190 1.8 AF129 0.50 BY49 0.4020 0.4020 0.4020 0.4020 0.10 0.10 74190 1.8 AF129 0.50 BY49 0.4020 0.4020 0.4020 0.4020 0.10 0.10 74190 1.8 AF129 0.50 BY49 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020 0.4020	ACV21 0-20	BYFIS 0.05	1 NKT777	0.38	SIST	0.80	74123	2.70
ACY28 0-17 BFY24 0-40 0A6 0-12 BT722 0-88 74150 1-12 ACY30 0-16 BFY44 1-00 0A47 0-10 BT723 0-83 74151 1-12 ACY40 0-16 BFY50 0-22 0A70 0-10 8X681 0-80 74154 1-12 ACY41 0-18 BFY50 0-22 0A70 0-10 8X681 0-80 74154 1-12 ACY41 0-28 BFY50 0-22 0A73 0-10 8X685 0-80 74155 1-12 ACY41 0-28 BFY50 0-22 0A73 0-10 8X685 0-40 74156 1-12 ACY41 0-28 BFY50 0-22 0A73 0-10 8X685 0-40 74156 1-12 ACY41 0-29 BFY50 0-85 0A73 0-10 8X681 0-50 74157 1-12 ACY41 0-29 BFY50 0-85 0A85 0-12 8X641 0-55 74176 1-12 ACY41 0-29 BSX00 0-93 0A85 0-12 8X641 0-55 74176 1-12 ACY41 0-29 BSX00 0-93 0A85 0-12 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0A85 0-12 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0A85 0-12 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-93 0-10 8X641 0-75 74176 1-12 ACY41 0-29 BSX00 0-10 8X641 0-10 8	ACV97 0.0K	BFV19 0.25	OA5	0.20	8FT308		74145	1.50
ACY41 0-16 BFY61 0-20 0A71 0-10 8X633 0-80 74155 1-8 ACY44 0-25 BFY62 0-22 0A73 0-10 8X633 0-80 74155 1-8 AD149 0-50 BFY62 0-22 0A73 0-10 8X636 0-50 74157 1-8 AD149 0-50 BFY64 0-42 0A79 0-10 8X640 0-55 74157 4-7 AD161 0-87 BFY99 0-85 0A81 0-08 8X642 0-80 74176 4-7 AD162 0-87 BSX27 0-40 0-86 0-81 8X642 0-80 74176 1-8 AF106 0-80 BSX27 0-40 0-86 0-18 8X646 0-75 74175 1-8 AF116 0-25 BSX27 0-15 0-80 0-90 (715/30P 0-50 74175 1-8 AF116 0-25 BSY27 0-17 0-80 0-90 (715/30P 0-50 74190 1-8 AF117 0-25 BSY27 0-17 0-85 0-7 AF118 0-25 BSY27 0-17 0-85 0-7 AF119 0-80 BSY95 0-12 0-80 0-90 (715/30P 0-75 74194 1-8 AF114 0-85 BSY27 0-17 0-85 0-7 AF125 0-20 BSY95 0-12 0-80 0-90 (715/30P 0-10 74194 1-8 AF126 0-25 BSY27 0-17 0-80 0-80 0-90 (716/30P 0-10 74194 1-8 AF127 0-17 BSY95 0-12 0-80 0-90 (716/30P 0-10 74194 1-8 AF127 0-17 BTY79/100R 0-80 0-80 0-80 0-15 74199 1-8 AF139 0-80 BTY95/100R 0-80 0-80 0-80 0-80 0-80 0-80 0-80 0	ACY28 0.17	BFY24 0-46	OA6	0.12	ST722	0.38	74150	3-85
ACY41 0-16 BFY61 0-20 0A71 0-10 8X633 0-80 74155 1-8 ACY44 0-25 BFY62 0-22 0A73 0-10 8X633 0-80 74155 1-8 AD149 0-50 BFY62 0-22 0A73 0-10 8X636 0-50 74157 1-8 AD149 0-50 BFY64 0-42 0A79 0-10 8X640 0-55 74157 4-7 AD161 0-87 BFY99 0-85 0A81 0-08 8X642 0-80 74176 4-7 AD162 0-87 BSX27 0-40 0-86 0-81 8X642 0-80 74176 1-8 AF106 0-80 BSX27 0-40 0-86 0-18 8X646 0-75 74175 1-8 AF116 0-25 BSX27 0-15 0-80 0-90 (715/30P 0-50 74175 1-8 AF116 0-25 BSY27 0-17 0-80 0-90 (715/30P 0-50 74190 1-8 AF117 0-25 BSY27 0-17 0-85 0-7 AF118 0-25 BSY27 0-17 0-85 0-7 AF119 0-80 BSY95 0-12 0-80 0-90 (715/30P 0-75 74194 1-8 AF114 0-85 BSY27 0-17 0-85 0-7 AF125 0-20 BSY95 0-12 0-80 0-90 (715/30P 0-10 74194 1-8 AF126 0-25 BSY27 0-17 0-80 0-80 0-90 (716/30P 0-10 74194 1-8 AF127 0-17 BSY95 0-12 0-80 0-90 (716/30P 0-10 74194 1-8 AF127 0-17 BTY79/100R 0-80 0-80 0-80 0-15 74199 1-8 AF139 0-80 BTY95/100R 0-80 0-80 0-80 0-80 0-80 0-80 0-80 0	ACY40 0-50	BFY56 0.00			ST7231		74151	1·10 2·00
ACY44 0-28 BFY62 0-22 OA73 0-10 8X635 0-40 74156 1-8 AD140 0-50 BFY63 0-17 0A74 0-10 8X645 0-50 74157 1-8 AD140 0-50 BFY69 0-85 0A81 0-08 8X642 0-55 74170 4-20 AD140 0-37 BFY90 0-85 0A81 0-08 8X642 0-50 74174 2-0 AD161 0-37 BFY90 0-85 0A81 0-08 8X642 0-50 74174 2-0 AD162 0-37 BSX27 0-00 0A85 0-12 8X644 0-75 74175 1-8 AF166 0-30 BSX00 0-32 0A86 0-12 8X644 0-75 74176 1-8 AF167 0-25 BSX27 0-10 0A85 0-12 8X644 0-75 74176 1-8 AF116 0-25 BSX26 0-18 0A90 0-00 V15/30P 0-50 74176 1-8 AF116 0-25 BSX26 0-18 0A90 0-00 V15/30P 0-50 74191 1-8 AF116 0-25 BSX26 0-18 0A91 0-00 V39/2019 0-75 74191 1-8 AF116 0-25 BSX26 0-18 0A91 0-00 V39/2019 0-75 74191 1-8 AF118 0-28 BSX26 0-18 0A91 0-00 V39/2019 0-75 74191 1-8 AF118 0-82 BSX36 0-18 0A92 0-10 V39/2019 0-75 74193 2-0 AF125 0-30 BT102/30P 0-10 0-55 XA102 0-18 74195 1-8 AF125 0-30 BT102/30P 0-30 0-35 XA102 0-18 74195 1-8 AF127 0-17 BTY42 0-92 0-42 XA101 0-15 74197 1-5 AF127 0-17 BTY42 0-92 0-42 XA101 0-15 74197 1-5 AF128 0-50 BTY42 0-92 0-42 XA101 0-25 74197 1-5 AF127 0-17 BTY49/400R 0A2290 0-45 XA102 0-16 74197 1-5 AF127 0-17 BTY49/400R 0A2290 0-42 XA101 0-25 74197 1-5 AF139 0-30 AF139 0-30 0-75 0A2290 0-42 XA101 0-25 74199 1-5 AF139 0-55 BTY49/400R 0A2290 0-42 XA101 0-25 74199 1-5 AF139 0-55 BTY49/400R 0A2290 0-42 XA101 0-25 74199 1-5 AF139 0-56 BTY79/400R 0A2290 0-42 XA101 0-25 74199 1-5 AF180 0-52 BY400 0-15 0A2290 0-42 XA101 0-48 Plus in socket low profile	ACY41 0-15	BFY51 -0 20			SX631	0.20	74155	1.55
AD149 0-50 BFY64 0-42 0A79 0-10 8X641 0-55 74170 4.2 AD161 0-87 BFY99 0.65 0A81 0-68 8X642 0-80 74174 2-6 AD162 0-87 BSX27 040 0A85 0-12 8X644 0-75 74175 1.3 AF106 0-80 BSX68 0-93 0A85 0-12 8X644 0-75 74175 1.3 AF106 0-85 BSX76 0-15 0A99 0-00 V15/30P 0-50 74175 1.3 AF116 0-25 BSX76 0-15 0A99 0-00 V15/30P 0-50 74190 1.6 AF116 0-25 BSX76 0-15 0A91 0-00 V15/30P 0-50 74190 1.6 AF116 0-25 BSX76 0-15 0A91 0-00 V15/30P 0-50 74190 1.6 AF117 0-25 BSX76 0-10 0-20 0-07 V60/201 0-75 74190 1.6 AF118 0-25 BSX76 0-12 0A210 0-25 XA102 0-15 74194 2.6 AF126 0-17 BSX76 0-12 0A210 0-25 XA102 0-18 74196 1.6 AF126 0-17 BTY79/100R 0A2200 0-55 XA161 0-25 74198 4.6 AF127 0-17 BTY79/100R 0A2200 0-42 XA102 0-15 74199 4.6 AF181 0-55 BTY79/400R 0A2200 0-42 XA102 0-25 74199 4.6 AF181 0-55 BTY79/400R 0A2200 0-42 XA102 0-25 74199 4.6 AF181 0-55 BTY79/400R 0A2200 0-42 XA102 0-10 -10 V19/30P 0-10 0-10 0-10 0-10 0-10 0-10 0-10 0-	ACY44 0.25	BFY52 0.22	OA73	0.10	8X635	0.40	74156	1.55
AD181 0-87 BSY27 0-40 0-86 0-88 8X642 0-80 7-4174 2-8 AD182 0-87 BSX27 0-40 0-86 0-12 8X643 0-80 7-4174 1-7 1-8 AF106 0-80 BSX67 0-15 0-80 0-80 0-15 8X645 0-75 7-4175 1-8 AF116 0-25 BSX76 0-15 0-80 0-90 0-10 (15/309 0-50 7-4190 1-9 AF116 0-25 BSY27 0-17 0-85 0-18 0-89 0-90 (15/309 0-50 7-4190 1-9 AF116 0-25 BSY27 0-17 0-85 0-90 0-90 (15/309 0-50 7-4190 1-9 AF117 0-25 BSY27 0-17 0-85 0-90 0-90 (15/309 0-50 7-4190 1-9 AF118 0-25 BSY27 0-17 0-85 0-90 0-90 (15/309 0-10 0-50 7-4192 2-9 AF118 0-25 BSY27 0-17 0-85 0-12 0-80 0-90 (1-8 1-19 0-90 BSY25 0-12 0-820 0-90 (1-8 1-19 0-90 0-90 0-90 0-90 0-90 0-90 0-90	4 70 1 40 0 8 8 8	BFY64 0-42			8X640	0.50	74157	1.80
AF114         0.25         B8X76         0.16         OA90         0.00         V16/30P         0.50         74190         1.26           AF116         0.25         B8Y26         0.18         0.09         0.00         V30/201P         0.75         74191         1.9           AF116         0.25         B8Y51         0.50         0.0420         0.07         V60/201         0.50         74192         9.0           AF118         0.62         B8Y55         0.12         0.020         0.07         V60/201         0.75         74192         9.0           AF124         0.90         B8Y55         0.12         0.0210         0.25         X.0101         0.10         74194         2.6           AF124         0.92         B8Y50         0.12         0.0210         0.25         X.0101         0.10         74194         2.6           AF125         0.20         BT02/500R         0.0210         0.85         X.0162         0.15         74196         1.6           AF126         0.17         BTY42         0.92         0.42200         0.85         X.0162         0.15         74196         1.6           AF127         0.30         0.40         X.0162	AD161 0.87	BFY90 0.65	OA81	0.08	8X642	0.80	74174	2.00
AF114         0.25         B8X76         0.16         OA90         0.00         V16/30P         0.50         74190         1.26           AF116         0.25         B8Y26         0.18         0.09         0.00         V30/201P         0.75         74191         1.9           AF116         0.25         B8Y51         0.50         0.0420         0.07         V60/201         0.50         74192         9.0           AF118         0.62         B8Y55         0.12         0.020         0.07         V60/201         0.75         74192         9.0           AF124         0.90         B8Y55         0.12         0.0210         0.25         X.0101         0.10         74194         2.6           AF124         0.92         B8Y50         0.12         0.0210         0.25         X.0101         0.10         74194         2.6           AF125         0.20         BT02/500R         0.0210         0.85         X.0162         0.15         74196         1.6           AF126         0.17         BTY42         0.92         0.42200         0.85         X.0162         0.15         74196         1.6           AF127         0.30         0.40         X.0162	AD162 -0-87	BSX27 040	OA85	0.12	SX644	0.75	74175	1.35
AF116 0.95 BSY26 0.18 0.491 0.00 V30/0011 0.795 1.4191 1.6 AF116 0.95 BSY27 0.17 0.495 0.07 V50/2011 0.795 1.4192 2.6 AF117 0.25 BSY51 0.50 0.4200 0.07 V50/2011 0.795 1.4193 2.6 AF118 0.80 BSY55 0.12 0.4200 0.07 V50/2011 0.10 7.4193 2.6 AF126 0.26 BT102/500R 0.4211 0.30 0.18 7.4195 1.6 AF125 0.20 BT102/500R 0.4211 0.30 X.151 0.15 7.4195 1.6 AF126 0.17 BTY42 0.92 0.42210 0.55 X.102 0.15 7.4195 1.6 AF127 0.17 BTY79/100R 0.42201 0.50 X.102 0.15 7.4197 1.5 AF127 0.17 BTY79/100R 0.42201 0.42 X.161 0.25 7.4199 4.6 AF180 0.52 BY100 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF180 0.52 BY100 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF180 0.52 BY100 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF180 0.52 BY100 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.48 7.4199 4.6 AF181 0.42 BY126 0.15 0.42200 0.42 X.161 0.42 X.161 0.42 Y.161	AF114 0.9K	B8X76 0-18	OA90	0.00	8X645 V15/20P	0.50	74176	1.80
AF117         0-25         BSY95         0-90         A2020         0-10         60/201         0-75         74193         2.6           AF118         0-80         BSY95         0-12         OA210         0-10         XA101         0-10         74194         2.6           AF124         0-26         BT102/500R         0-20         0-25         XA102         0-18         74195         1.8           AF125         0-20         0-20         0-20         0-30         XA151         0-15         74194         1.6         1.6           AF126         0-17         BTY42         0-92         0-4220         0-55         XA162         0-15         74195         1.8           AF127         0-17         BTYF9/100R         0-820         0-55         XA161         0-25         74198         4.6           AF179         0-86         BTYF9/400R         0-4203         0-42         XB101         0-43         Plug in socket           AF180         0-52         BY100         0-15         0-4203         0-42         XB103         0-25         14 pin DIL           AF181         0-42         BY126         0-16         0-42207         0-42         XB103 <t< td=""><td>AF115 0.25</td><td>BSY26 0-18</td><td>1 OA91 🛰</td><td>0.01</td><td>V30/201P</td><td>0.75</td><td></td><td>1-95 1-95</td></t<>	AF115 0.25	BSY26 0-18	1 OA91 🛰	0.01	V30/201P	0.75		1-95 1-95
AF117         0-25         BSY95         0-90         A2020         0-10         60/201         0-75         74193         2.6           AF118         0-80         BSY95         0-12         OA210         0-10         XA101         0-10         74194         2.6           AF124         0-26         BT102/500R         0-20         0-25         XA102         0-18         74195         1.8           AF125         0-20         0-20         0-20         0-30         XA151         0-15         74194         1.6         1.6           AF126         0-17         BTY42         0-92         0-4220         0-55         XA162         0-15         74195         1.8           AF127         0-17         BTYF9/100R         0-820         0-55         XA161         0-25         74198         4.6           AF179         0-86         BTYF9/400R         0-4203         0-42         XB101         0-43         Plug in socket           AF180         0-52         BY100         0-15         0-4203         0-42         XB103         0-25         14 pin DIL           AF181         0-42         BY126         0-16         0-42207         0-42         XB103 <t< td=""><td>AF116 0.25</td><td>BSY27 0-17</td><td>OA95</td><td>0.07</td><td>V60/201</td><td>0.50</td><td></td><td>2.00</td></t<>	AF116 0.25	BSY27 0-17	OA95	0.07	V60/201	0.50		2.00
AF119         0-80         B8Y95         -12         OA210         0-26         XA102         0-18         7-1105         1-2           AF124         0-26         151102/500R         0-211         0-30         XA151         0-15         7-149         1-8           AF125         0-17         BTY42         0-92         0-80         XA152         0-15         7-149         1-8           AF127         0-17         BTY79/100R         0-4220         0-62         XA161         0-25         7-1419         1-8           AF139         0-80         0-75         0-4220         0-42         XA161         0-25         7-1419         1-8           AF179         0-80         0-75         0-4220         0-42         XA161         0-25         7-1419         4-8           AF180         0-55         BTY9400R         0-A2200         0-42         XB101         0-48         Plug in socket           AF181         0-42         BY160         0-15         0-A2206         0-42         XB103         0-20         14 pin DIL	AF117 0.25		OA200	0.07	V60/201P	0.75	74193	2.00
AF124         0-26         BT102/500R         OA211         0-30         XA151         0-15         74196         1-8           AF125         0-27         0-27         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75         0-75	AF119 0-20	B8Y95 0-12	OA210	0.25	XA102	0.18	74194	2.50 1.85
AF126 0-17 BTY42 0-92 OAZ201 0-50 X Xa161 0-25 74198 4-6 AF127 0-17 BTY79/100R OAZ202 0-42 Xa161 0-25 74198 4-6 AF189 0-36 BTY79/400R OAZ203 0-42 Xa162 0-25 74199 4-6 AF180 0-55 BTY79/400R OAZ204 0-80 XB101 0-48 Plng in socker AF180 0-52 BY100 0-15 OAZ206 0-42 XB102 0-10 -low profile AF181 0-42 BY126 0-15 OAZ206 0-42 XB102 0-25 14 pin DIL	AF124 0-25	BT102/500R	OA211	0.30	X A 151	0.15	74196	1-50
AF127         0-17   BTY79/100R         OAZ202         0-42   X-4101         0-25   AF199         4-6           AF178         0-36   BTY79/400R         OAZ203         O-42   X-4101         0-25   AF199         4-6           AF179         0-65   BTY79/400R         OAZ204         0-30   X-8101         0-43   Plng in socket           AF180         0-52   BY100         0-15   OAZ206         0-42   X-8102         0-10   -low profile           AF181         0-42   BY126         0-16   OAZ207         0-42   X-8103         0-25   14 pin DIL	AF125 0-20 AF126 0-17		OAZ200 OAZ201	0-50			74197	1.50
AF139 0-80 0-75 0AZ203 0-42 XA192 0-25 AF130 0-55 BTY79/400R 0AZ204 0-80 XB101 0-48 Plng in socket AF139 0-65 1-25 0AZ205 0-42 XB102 0-10 low profile AF181 0-42 BY126 0-15 0AZ206 0-42 XB102 0-25 14 pin DIL	AF127 0-17	BTY79/100R	OAZ202	0.42			74198	4-80 4-80
AF180 0.42 BY120 0.15 OAZ206 0.42 XB103 0.25 14 pin DIL	AF139 0.80		OAZ203	0.42		0.25		
AF180 0.42 BY120 0.15 OAZ206 0.42 XB103 0.25 14 pin DIL	AF179 0-85	1.25	OAZ205			0.10	Plug in se	ockets
AF181 U-AZ   BY120 U-15   UAZ2U U-47   TENTO	AF180 0.52	BY100 0-15	OAZ206	0.42			10 to pre	74741
AF186 0-40 BY127 0-17 OAZ208 0-82 XB113 0-12 0-1		BY126 0-15	OAZ207	0.47	X B113	0.12	ra pin O	0-15
AFY19 1-13 BY182 0-85 OAZ209 0-82 XB121 0-48 16 pin DIL	AFY19 1-18	BY182 0-85	OAZ209	0.82	XB121	0-48	16 pin Dl	IL.
AFZ11 0-60 BY213 0-25 OAZ210 0-82 ZR24 0-68 0-1	AFZ11 0-60	BY213 0.25	OAZ210	0.32	ZR24	0.68		0.17

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12p. 0-01, 0-015, 0-022, 0-033, 0-047, 0-068, 3p. 0-1, 3 p. 0-15, 4p. 0-22, 4p. 0-33, 5 p. 0-47, 7p. 0-68, 10p. 1-0, 12p.

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ing place.

If only the two middle entries in the truth table are required (as is usual) then a single data input can be used while the complement is obtained from an inverter, Fig. 6.4. The input data is up-dated during the clock pulse and retained when the clock goes low.

#### MINIMISED DATA LATCH

The circuit in Fig. 6.4 required five gates to realise it because the D was obtained by the direct inversion of D. However, D can be obtained from the output of gate 1, because D is only needed at the input to gate 2 when the clock is high; therefore, gate 1 will provide the required information.

The minimised circuit shown in Fig. 6.5 may be realised as an experiment using a single SN7400N. Data D will be entered into the memory while the clock is high and retained when the clock is low.

#### LOGIC GATE BISTABLES

In the previous circuits the inputs are coupled to the bistable circuit all the time the clock pulse is high, so that these circuits can only be made to toggle (divide by two) if the inputs are a.c. coupled. However, it is essential in logic circuits to overcome this problem without giving up the advantages of d.c. coupling, so circuits were developed which prevent the output transitions from altering the input information which was present when the leading edge of the clock occurred.

These circuits are usually designed in the form of two gated memories, one holds the output state and one holds the input information read in at the beginning of the clock pulse. Since this information is later transferred to the output memory, such a

circuit is called a "master-slave" bistable.

Several different versions are available but they all have the master-slave action shown in Fig. 6.6. Here the operation shown is the J-K function where information is transferred from master to slave on the falling edge of the clock pulse. From the truth table it can be seen that this J-K master-slave bistable will divide by two if J and K are taken to 1, and an input applied to the clock.

#### CONCLUSION

We have shown how the simple memory circuit develops into the master-slave bistable, with its many advantages.

Part 7 will describe counters and displays



### **BOAT SHOW '73**

HE Yachtsman's winter break, this year in the setting of a sunny Spanish harbour, the annual International Boat Show provides us with a shop window of marine electronics for small craft.

As in previous years there has been a steady develop-ment of the electronic gadgetry available, this year has seen the introduction of the l.e.d. (light emitting diode) to boat electronics, a new type of knotmeter and some

advancement in the receiver, transmitter field.

One firm whose name must be to the forefront when we consider this year's innovations is EMI; in fact one could call it their year of innovation, with no less than four completely new instruments available. The most

interesting new product is a magnetic log.

The new log operates by the transducer generating an a.c. magnetic field in the water surrounding it. As the boat moves through the water a small e.m.f., dependent on the boat speed, is produced and sensed by the transducer head. This induced signal, fed back through the system, is amplified to give a display of speed and distance. Housed in the normal EMI Electra range case the biggest advantage of this instrument is that there are no moving parts below the water and virtually no projection (only 3mm) below the hull surface.

The other innovations from EMI are an automatic direction finder, an f.m. radio telephone, and a gas detector and alarm. The direction finder is a three band receiver covering the range 175kHz to 3,000kHz. To use it, it is tuned to the required radio beacon and automatically gives an immediate and continuous bearing of the transmitter. The unit has its own internal supply or can be powered from a 12V or 24V ship's supply.

The Electra Gas Alarm uses a solid state imported detection unit and provides both visual and audible

alarms of dangerous concentrations of gases.

It is interesting to note that the Electrascan MKII radar has been ordered by the RNLI for use in lifeboats. Whilst on the subject of radar both Decca and Electronic Laboratories have introduced MKII radars and the Decca Super 101 MKII is now sold with a magnifier that increases picture size to 9 inches.

#### TECHNICAL INNOVATION

As far as real technical innovation goes, this is the first time that we have found a l.e.d. used in a depth sounder. Produced by Marine Electronics and available for about £39, the sounder works on the same principle as a neon type and probably has a similar accuracy.

Instead of providing a point of light at the depth reading, the l.e.d. is turned on when the pulse is transmitted and off when the pulse is received, thus providing

an arc of light showing the depth.

Brookes and Gatehouse-manufacturers of perhaps the most reliable and widely used instruments for the racing yachtsmen-have, we feel, done the sensible thing in offering most of their instruments for use on ship's supply. At last no more fiddling with batteries in a heavy seaway.

Baron Instruments, another contender for the "crack" racers' instrument panel, have redesigned their meter faces and introduced a new range—the Baron Sailboat Console—the meters are lit by l.e.d.'s and are  $4\frac{1}{2}$  inches in diameter. Provided the instruments can prove themselves at sea, with the new meters (which were in fact suggested by us last year) we feel that this range is the most likley to rival B. and G. this year.

Finally we think it is a pity to see Smiths Industries cashing in on the boat market with standard Radio-mobile car radios and tape units. Without the necessary marinisation we feel that these units will not stand up to marine use--particularly in salt water-and for Smiths

to push the standard product for this purpose is surely not good policy.

# 

#### WIRING HARNESSES FOR CARS

The Ford Motor Company patent No. 1 287 074 is concerned mainly with wiring harnesses for cars but most electronic enthusiasts will see far wider applications.

In a vehicle all the various electrics, such as sidelights, head-lights, stoplights and wipers are usually connected to a power source by separate power carrying cables. The electrics are conby switches (usually located inside the vehicle remote from the devices) in the power cables from one of the supply terminals. The vehicle chassis acts as a common return to complete the circuit to the other supply terminal.

Providing heavy duty power lines for each separate remote electrical function is uneconomical. The Ford system is based on the house "ring main" idea and uses a flat strip power conductor capable of handling the total current load for all the vehicle electrics, see Fig. 1.

The strip conductor is flexible and is coated with flexible insulating material. On the surface of the insulating material a thin conducting layer is deposited and etched away to form a parallel series of thin low current control conductors. Each of these has connecting pads spaced out along its length and Ford suggest that a practical system 20 to 30 control conductors can be used along with one main power conductor.

The vehicle power source is permanently connected to the power conductor by a pin connector which bites through the insulating material and into the conductor. Similar power connectors can be used to connect the power conductor to any electrical device which requires a permanent supply of power.

Each remote electrical function that requires only a switchable power supply (such as headlights, etc) is connected to the power connector by a gated plug. The gated plugs each house a transistor of which the emitter is permanently connected to the power conductor.

A resistor of around 1,000 ohms is connected between the base emitter of the transistor and the base of the transistor is also connected to the required control conductor of the wiring harness. The transistor collector is connected externally to whatever electrical function is to powered, Fig. 2.

The gate is controlled by a

trigger signal from the control conductor and will only pass current to its load when a control signal is present.

In Fig. 2, the electrical functions or loads are lamps LP1 and LP2. When manual switches S1 and S2 are "off" the base of transistors TR1 and TR2 are at the same potential as the emitters and neither transistor conducts; thus lamps LP1 and LP2 do not light.
If switch S1 is turned "on" the potential of control conductor CC1 falls, transistor TR1 is switched on and current flows through lamp LP1. Similarly if switch S2 is turned on, current flows through lamp LP2. The circuit takes into

account the high cold current surges involved in lighting most vehicle lamps.

Although SCR's may be used it is easier and cheaper to use switch resistors R1 and R2 (around 100 ohms each) which, together with the resistances connected between the emitters and bases of the transistors. form potential dividers which hold the base potentials constant at a level to which they fall on closing the switch. Current through the transistor can only increase until the voltage across the low emitter resistance (cable resistance, etc) raises the emitter potential to a similar value to the base potential.

#### **BIO-NOTES**

Readers of Gerry Brown's fascinating column will have noticed his comments in the January 1973 issue concerning "Electrophonic issue concerning Hearing" and his suggestion that the effect of feeding electric currents direct to the brain should be re-examined as a possible aid to the deaf.

Anyone wishing to follow this line of research will be interested by the content of two British patents Nos. 1 284 158 and 1 286 316 respectively from the ZCM Corporation of USA and Hermann Mengeler of Germany. patents were published some while ago but each contains useful technical information on the subject.

The ZCM patent details method of using an audio signal to pulse a microwave radio signal, the resultant pulses being then fed to electrodes which are capacitively coupled to the subject's skin. This is claimed to produce a brain sensation in some respects equivalent to hearing.

The Mengeler patent claims a comparable system for introducing video information to the brain. In brief, a miniature TV camera pro-duces a scanning voltage which is capacitively coupled to the subject's temples. This supposedly stimulates the optic nerve and produces sensations which the subject may train himself to equate with sight sensations.

Reference to these two patents before experimentation could well save readers wasted time and work -it could also save their subjects unnecessary electric shocks.

#### BP1 287 074

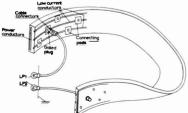


Fig. 1

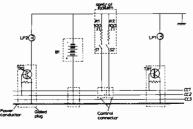
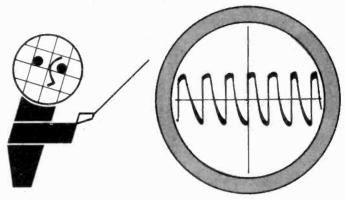


Fig. 2

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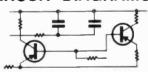
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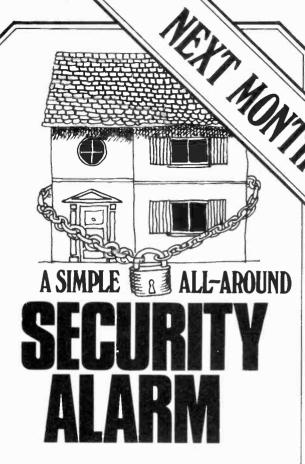
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# RONICS

**APRIL ISSUE ON SALE MARCH 9** 

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

#### LOW COST DIGITAL MULTIMETER

A new £49 digital multimeter from Sinclair Radionics promises to be a strong contender in the professional quality meter market having as it does a claimed high accuracy, high input impedance, portability, and relative low cost. It is aimed at the replacement market as an economical substitute for analogue multimeters.

Measuring  $190 \times 130 \times 58$ mm and weighing  $1\frac{1}{2}$ lb (0.6kg), the multimeter can easily be held in the hand when making measurements. The leads are fixed to the instrument and wrap around a recess in the lightweight polypropylene case. Simple yet effective finger plate selector switches form an integral part of the case.

The instrument has ranges extending from 1µA up to 1A d.c., 1mV to 1,000V d.c. and a.c., and resistance ranges from 1,000 ohms to  $1M\Omega$  full scale. Display is by three Nixies with a carry of one in a single neon. This gives an effective 3½ digits without using a fourth tube.

The measuring technique is such as to reduce current consumption to a minimum, in fact, the manufacturer's specification promises 80 hours of switched-on operation with a current drain of 12mA.

Input impedance is very high at  $1,000 M\Omega$  compared to analogue meters, as are the accuracy parameters of 0.4 per cent on volts d.c., and 1 per cent on a.c. with an f.s.d. error of  $\pm$  2 digits.

An interesting aspect of the circuit is that it is all discrete, with a component count of around 300 (including 100 transistors) all mounted on three p.c.b.s.

In operation all inputs are brought within a 1V range and the incoming signals are analogue-todigital converted to produce a pulse train the length of which is. proportional to the input level. The pulse train is passed to a chain of three cascaded pump circuits. Component values have been so chosen that the incoming pulse is summed

in units, tens, and hundreds.

A "ring-of-ten" counter strobes each Nixie numeral terminal in sequence and for each strobe "tops ' the pump circuits. This action is used to time the point in the strobe sequence when the supply is switched onto the relevant Nixie to illuminate the correct numeral.

This instrument is available, by mail order, direct from the makers, Sinclair Radionics Ltd., London Road, St. Ives, Huntingdonshire.

#### **CASES**

Encouraged by the success of their Contil Mod-2 range of instrument cases, West Hyde Developments recently launched a new complementary range designated Mod-3 types. range of cases

The Mod-3 cases have fixed sides, in scuff resistant p.v.c. coated steel, made of two parts rigidly locked together. A chassis is supplied with the case, this and the panels being made up first and then assembled afterwards in the case.

Interior drilled side flanges allow the chassis plate to be positioned in any convenient position. The side flanges also take the rear and front panel fixing screws.

Case dimensions vary from 3in  $\times$  7in to 6in  $\times$  11in and further details and price list can be obtained from West Hyde Developments Ltd., Ryefield Crescent, Northwood

#### WAFER SWITCHES

Hills, Northwood, Middlesex.

The wafer switch is still one of the widest used components in electronics, and Ultra Electronics (Components) Ltd are now marketing a range of wafer switch kits.

One of the advantages of the switch kit is its versatility and ease with which the designer can make up prototype switching assemblies and change them on the spot.

The Centralab Switchkits are packaged as separate components; the Series PA 1000 and PA 2000 kit contains. for example, 1.000 clips, 800 eyelets, 925 contacts, stators, rotors, nuts and packing washers, plus 25 index assemblies. 25 adjustable stops, eyeletting pliers and assembly tools and instructions.

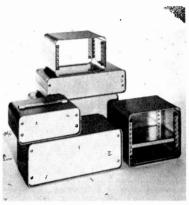
Forther information and details of the switch kits can be obtained from Ultra Flectronics (Components) Ltd.. Fassetts Road. Loudwater, Bucks.

Also available from Ultra Electronics is a free switch wallchart giving typical ratings and configurations

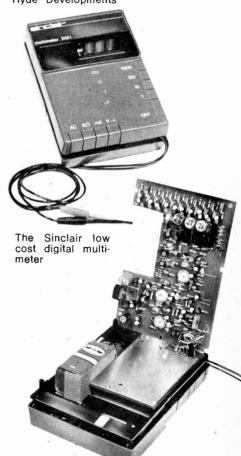
#### .SPECIAL OFFERS

Here is a chance to stock up with solid state devices at bargain prices. We have been advised by A. Mar-shall & Son Ltd., that their advertisement next month will list a series of special offers, available only to readers of this magazine.

This well-known component supplier will be disposing of a large amount of stock at reduced prices, prior to moving into new premises.



Contil Mod-3 cases from West Hyde Developments



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2 pin Din Speaker Plug/Socket
3 pin Din Line Socket
3-5mm Jack Plug Screened
Standard Jack Plug
Screened Standard Jack Plug
Screened Standard Jack Plug
Screened Stereo Jack Plug
Screened Stereo Jack Plug 18p 10p 13p 10p 10p 15p 18p 18p Phono Plugs: Red or Black 3p each. P.p. on above items 3 p. MAINS NEONS Red or Green. Size: jin x 1jin. 15p, p.p. 3jp. LEVER ACTION P.O.1000 TYPE SWITCHES
Lock 4-pole changeover, 15p, p.p. 3jp. Ex equip.
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AUDIO LEAD8

Screened Phono Leads 46in long. 15p.

3-5mm JACK/3-5mm JACK 7ft 6in long. 40p.

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MULLARD & MALLORY SCREW TERMINAL CAPACITORS 4,500μF 64V, 7,100μF 40V, 50p each 20,000 30V, 25,000 25V, 35,000 15V, 30p each p.p. 10p.

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GARDNER'S POTTED TRANSFORMER, 0-250V. Input:  $18V\ 500m/n$ ,  $50V\ 150m/a$ ,  $6V\ 250m/a$  output. Size:  $3in\times 21in\times 21in$ , \$1, p.p. 20p. Ex equip.

TELESCOPIC AERIALS Chromed 7in closed, 28in extended, 6 section ball jointed base, 23p, p.p. 8p new.

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PRINTED CIRCUIT BOARD/19 ACY 19's 10 OA200 Photes: I reed relay: 1 AZ 292 zenner ass. capacitor/
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Working voltage 330V a.c./d.c. current, max. 3 amp a.c./d.c. 7 pin plug and socket, 50p, p.p. 6p. 15 pin plug and socket, 50p, p.p. 6p. 15 pin plug and socket, 51, p.p. 6p. 31 WAY PLUG AND SOCKET, \$1.50, p.p. 6p.

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# Sinclair Project 60

# Project 60 Stereo FM Tuner





Built and tested. Post free. £25

# with phase lock-loop principle

Amongst the many advanced electronic features to be found in this remarkable stereo tuner, use of the phase lock loop principle ensures standards of audio quality better than from any other method of detection yet used. Varicap diode tuning, accurately formed printed circuit coils, an I.C. in the special stereo decoder section and switchable squelch circuit for silent tuning between stations contribute to the unsurpassed performance of this tuner, irrespective of price consideration. But the Project 60 FM Stereo Tuner is far from expensive – indeed, it offers fantastic value for money and will bring the thrill of stereo radio to many who previously may not have been able to afford it. The tuner may be used with any good system as well as Project 60, but if you use it with other Project 60 modules, you will find the matching front panels particularly impressive in appearance as well as function.

#### SPECIFICIATIONS

Number of transistors: 16 plus 20 in I.C.

Tuning range: 87-5 to 108MHz.

Sensitivity: 7µV for lock-in over full de-

Squetch level: typically 20 µV.

Signal to noise ratio: ±65dB.

Audio frequency response: 10Hz-15Khz (+1dB).

Total harmonic distortion: 0-15% for 30% modulation.

Stereo decoder operating level: 2 µV.

Cross talk: 40dB.

Output voltage: 2 x 150mV R.M.S. max.

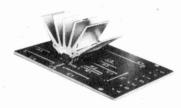
(typically 2 × 50mV, stereo)

Operating voltage: 25-30V DC at 100mA.

Indicators: Stereo on tuning.

Size: 93 × 40 × 207mm.

# Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-fic constructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 transistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

#### SPECIFICATIONS

Output power: 6 waits RMS continuous (12 waits peak), 6-80. Frequency Response: 5Hz to 100KH2 $\pm$ 1dB. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90dB (1,000,000,000 times) after feedback Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size:  $22 \times 45 \times 28$ mm including pins and heatsink.

Manual available separately 15p post free,

With FREE printed circuit board and 40 page manual.

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## **Project 605**



The easy way to buy and build Project 60

Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink, This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

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# the world's most advanced high fidelity modules

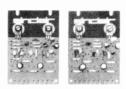
### Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual. 2.30 £4.48 2.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8 $\Omega$ ) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (2.50 units are interchangeable with 2.30s in all applications).—Power Outputs:

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts.
Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts.
Frequency response: 30 to 300.000Hz±1dB. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8 $\Omega$ ). For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57mm.



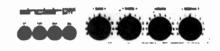
## Stereo 60 Pre-amp/control unit

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A. curve ±1dB.20 to 25,000 Hz. Ceramic p.u. – up to 3mV. Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE+12 to —12dB at 10KHz: BASS + 12 to -12dB at 100Hz Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.

Built, tested and guaranteed.

£9.98



## A.F.U. High & Low Pass Filter Unit

For use between Stereo 60 unit and two Z.30s or Z.50s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. There are two filter sections - rumble (high pass) and scratch (low pass). H.F. cut-off (-3dB) variable from 28KHz to 5KHz. L.F. cut-off (-3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Operating voltage from 15 to 35V. Current 3mA. Size: 66 x 40 x 90mm

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## **Power Supply Units**

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential

PZ.5 30 volts unstabilised £4.98 PZ.6 35 volts stabilised PZ.8 45 volts stabilised (less mains transformer)

PZ.8 mains transformer



#### Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

#### Guarantee

If, within 3 months of purchasing any product direct from Sincleir Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sincleir appointed Stockists also offer this same guarantee in co-operation with

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Powerful, continuously rated, 2-speed. Either 6 or 12 volt D.C. operation. PRICE £2 incl. P. & P.

#### 12 VOLT D.C. MOTOR

Powerful I amp. REVERSIBLE motor. Speed 3,750 r.p.m. complete with external ge complete with external gear train (removable) giving approx. final speed of either 125 r.p.m. or 240 r.p.m. Size: 44 in x 24 in dia. Either type price 95 p inc. post.

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post paid.

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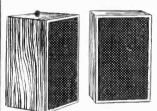
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As reviewed in

ROC PRICE £9-50 pair Normal Price £10:75

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POPULAR HI-FI February 1972 A superb hi-fi amplifier with all the features you've ever wanted - for under £46:00. Saving over £10:00 on the normal LILIN I ROC PRICE retail value. Up-to-the-minute slider controls for bass and treble. Separate volume and balance controls. Headphone socket on front panel. Push-button £35.20 volumis and delance controls recappiones socked on front panel, rush-outed input, controls — magnetic phono (high)/low) tuner, aux, mono, monitor Loudness push-button control for perfect sound at low output levels. Nor, Left and right push-button on/off switches for speakers. Noise filtering (f) and tape monitoring facilities. Two auxiliary AC outlets, Frequency response 20-20,000 Mz ± 1 db at full power. 15 watts rms per channel. Walnut cabinet with satin aluminum trims, Inputs, phono 2.5mV and 5mV RIAA. Tuner/aux 250mV. Hum £55.50

and noise; phono - 50db; tuner/aux - 65db. How's that for a specification!
Size 14½ wide, 3½ high, 10½ deep

OLSON RA-310 AM/FM/MPX

This ROC Tuner is especially designed to match the Olson AM-395 Stereo Amplifier. In price and value, as well as it's good look-ing design! But of course it's also

ideal for use with any other amplifier. The RA-310 costs £10:00 less than the normal retail value, and yet it is a highly sophisticated unit, incorporating the latest solid state techniques. Operation is drift free for sup-

reme station holding capability. You can connect this Tuner to a stereous dumal Price (50.00 ambility can be recorder, And of course it covers all the stations in the AM and FM bands, FM 87-100 MHz, AM 25-1005 KHz, 50.00 State (17.4 wide. 4 "Migh. 7") deep.

ROG PRICE £12.45

REALISTIC SA-100B 6-WATT RESTREED AMPLIFIER

Here's fabulous, exciting value in miniature! This high quality stereo amplifier measures only 9" wide × 3" high × 52" deep. And yet it has sepa-rate ganged volume, balance and tone con-trols. Plus speaker in/out, mono/stareo, phono/

tuner and power on/oft slide switches. The ends are oiled walnut, with matching enamelled metal top. The Iront panel is satin aluminium and walnut-brown enamel. Frequency response is 50 to 70,000 Hz + 3d8. Output 3 watts r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tuner

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When you want to listen to the radio all by yourself Then this will solve the problem Separate volume and tuning controls with to-use knobs. Frequency range is

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for the price of a ceramic! Is specially de signed to match top quality tone arms, end to get the very best from your hi-framplifier. 0.7 mil diamond stylus. Output: 7mV per channel, Frequency range, 20-21,000 Hz. Channel balance: <a href="mailto:100">± 1d8</a>, Channel separation: 28dB, Compliance: 12 x 10-6 cm/dyne ROC PRICE ES 37

OLSDN AM-395 40-WATT STEREO AMPLIFIER

An ideal unit for your new stereo separate system. It is more than £10.00 below the normal retail price! Making the AM-395 one of Britain's best hi-fi

buys. It takes in signals from magnetic or ceremic pick-ups, tuners (see Olsen RA-310) and taps decks. And it's got oet-puts for teping and for headphones. There are separate basis

e_s=" puts for teping and for headphones. There are separate bass and trable controls, separate Left and Right channel volume controls. And a loudness switch for boosting the bass and trabla notice when listening at lew autput levels. Frequency respense: 20-20.000 Hz ± 368. Output: 20 watts r.m.s. per channel into 8 ohme. Inputs: magnetic phano 3-0mV RIAA, crystal phone 100mV, tapp 150mV, tuner 180mV. Size 11½" wide, 4"high, 7½" deep. The specification reads well—sounds even better!



A-3000 38-WATT SOLID STATE STERED AMPLIFIER The A-3000 looks as good as it sounds! Giving you a big performance this suparb audio amplifiar has a full range of facilities on the front and rear panels. On the front all the controls you're ever likely to need plus a headphone socket. On the rear — signal inputs, speaker outputs and a line

fuse for circuit protection. Specifications: 18 watta rms per chennel into 8 ohms. Frequency response 20-35,000 Hz (± 2db) Inputs Magnetic, Ceramic, Tuner, Tape. Aux. Tape Play. Size: 345mm × 300mm × 130mm.

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# £15.70

OLSON AM408 4-WATT STEREO AMPLIFIER Here's marvellous value for someone just starting to set them-selves up in eudio! At only £10-50, you get a fine emplifier in a scratch resistant metal cebinet, with a smort brushed aluminium

front panel. It incorporates separate tone and volume controls for each channel. Inputs are provided for turntable (ceremic cer-tridge), tuner and tape deck or recorder, Frequency response; 70-20,000 Hz + 3d8, Output: 2 watts r.m.s. per channel into 8 phms Inputs: phono 80mV; tuner/aux 80mV. Size 8" wide, 2%" high

0 25-WATT 3-WAY CRYSLER LIVING AUDIO SPEAKER CE-56

This high quality speaker has its own built-in 3-way sound response aw giving you the ideal frequency response for hi-li, natural or mood music listening. Its

£39.95 aach. beautiful, heavy, piled walnut cabinet incorporates two separate speaker units an 8" weefer, mid-range with 2" concentric tweeter. Power handling

cospacity: 25 wetts r.m.s into 8 ohms. Overall frequency res – ponse: 35-20,000 Hz. Cabinet size:  $10\frac{1}{4}^{\circ} \times 7\frac{1}{8}^{\circ} \times 8\frac{3}{4}^{\circ}$ . Exactly right for matching the most modern decor. ROG PRICE



PALACE AM/FM/MPX STEREO TUMER AMPLIFIER SSA-18
This is one of the lowest priced stere tuner emplifiers the market. It covers the full range of both AM and FM broadcast frequencies. And when yew're switched to FM, en indicater lights up when steree signals raceived that's this time to switch to "Steree" I The SSA-18 has all the faceities you'd axpect to find en luners costing twice as much—separate synden controls. Selector switch for tape, phono, AM, FM, stereo, Jack sacks to n front panal for steree hadphones. Frequency range: FM 88-108 MHz.
535-1005 kHz. Frequency response: 50-10,000 Hz ± 3d8.
Power output: 4 wetts totel must power into two 8 ohm scekers. Size; 16" wide. 4½" high, 8" deep.

ROC 7-WATT STEREO AMPLIFIER CHASSIS SK-317
This axclusive
R O C Stereo Chassis is completely self-contained and costs £2-25 less than the normal re tail value! TI SK-317 is a realty The

tall verses. SK-317 is a really compact unit measuring only 5]* wide, 12; compact unit measuring only 5]* wide, 12; high and 82; deep. It contains its own mains power supply, and has a ganged volume control and saparate trable controls for each channel. Specification: frequency reserved. 17 nnn Mr. + 3d8, output 3.5 wetts music power per containing the second seco ponse 40-17 000 Mz ± 3dB; output 3 5 wetts music power per channel into 8 ohms; input, phono, 600mV; signal-te-noise

ratio better than 45dR



R.446 3-WAY MATCHEO SPEAKERS
These will do justice to your amplifier – and to your pocket, at only £20-00 a pair, they are real value-for-money. Each cabinet is heavily lagged and teak finished. They handle 16 watts rms (8 watts rms each). Each loudspeaker contains a 63" base unit plus tweeter. Frequency range: 40 to 19,000 Hz. Size 14" high, 9" wide, 61" deep.



OLSON AM-372 16-WATT STEREG AMPLIFIER 🕰 Here's e-raelly good amplifier at a really down-te-earth price — nearly £7 less than the normal retail value? Just look at whet the AM-372 will do for you – reproduce signals from ceramic or crystal certridges, AM and FM tuners, and tape recorders. And it gives you outputs for two sets of speakers, heedphones and tape recorders. Frequency response is 30 to 20,000 Hz  $\pm$  3dB. Output 3 wetts r.m.s. per channel music power into 8 ohm speakers. Phono input 200mV. Tuner input 200mV. Size: 121" wide. 31" high, 71" deap.

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#### **PRACTICAL ELECTRONICS** "SCORPIO" ELECTRONIC **IGNITION SYSTEM**



This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of Practical Electronics. It is suitable for incorporating in any 12V ignition system in cars, boats, go-karts, etc., system in cars, boats, go-karts, etc., of either pos. or neg. earth and up to six cylinders. The original coil, plugs, points and contact-breaker capacitor fitted in the vehicle are used. No extra or special components are required.

openents are required.
Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better highspeed performance, quicker engine warm-up and improved fuel economy. Eliminates excessive contact-breaker point burning and theneed to adjust point and spark-plug means with precision.

need to adjust point and spark-plug gaps with precision. Construction of the unit can easily be completed in an evening and installation should take no longer than half an hour. A complete complement of components is supplied with each kit together with ready-drilled roller-tinned professional quality fibre-glass printed-circuit board, custom-wound transformer and fully-machined die-cast case. All components are available separately. Case size 7½in × 4½in × 2in. approx.

approx.
Complete assembly and wiring manual 25p, refundable on purchase of kit. Price: £10-50 plus 50p P. & P.

**PSYCHODELIC LIGHTING** UNIT Mk. 3



This unit represents a natural progression from our phenomenally successful Mk. I and 2 Units. As before the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency signals into a three-coloured light display; the colour depending on the frequency of the signal and the intensity on the loudness of the audio source.

The unit is constructed on professional fibre-glass printed-circuit board material and uses latest full-wave triac circuitry. There is a master-level control, together with independent sensitivity controls have been redesigned permitting their use as faders; allowing dimming from max, to zero at the turn of a knob. R.F.I. suppression is now incorporated as standard as well as rovision for D.J. "Pulse-Flash" knob. R.F.I. suppression is now incorporated as standard as well as provision for D.J. "Pulse-Flash" controls. The choice of two inputs enables operation from both high and low power amplifiers. Max. power I-SkW per channel at 240V ar.

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Full instructions in this month's issue for versions with either four or six figures

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Easy to apply and ideal for an impressively professional finish.

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AC107	15p	AFI25	20p	BD132	75p	OC28	50p	2N3702	1304	N 52 W	UMI J
ACI26	12pm	AFI26	20p	BD133	75p	OC35	50p	2N3703	12p		IC CA
AC127	i2p	AF127	20p	BFI15	25p	OC42	12p	2N3704			
AC 128	120	AF139	32 ph	BF173	20p	OC 44	12p	2N3705			
ACI31	12.	AFI78	32p	BF177	28p	OC 45	12p	2N3706		VERGROARD	
ACI32	12p	AFI80	40p	BF178	32p	OC70	12p	2N3707	12p	VEROBOARD	0-1
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ADI40	50p	BC109	9p	BF194	15p	OC82D	12p	2N3711	Hp	131 × 5	27p
AD149	45 pm	BC147	13p	BF195	15p	2N2904	20p #	2N4062	12p	17 × 24	75p
ADI61	33 p	BC148	13p	BF197	15p 📠	2N29261		40360	35p	17 × 31	100p
AD162	36	BC149	13p	BF200	32p	2N29260		40361	35p	17 × 5 (plain)	
AFI14	20g	BC157	14p	BFY50	20p			40362	40 p	17 × 3} (plain)	
AF115	200	BC158	14p	BFY51	20p	2N2926		40408	40p	17 × 2+ (plain)	
AFII6	20p	BC159		BFY52	20p	2N2926		ZTX302		24 × 5 (plain)	
AFI 17	20p		14p			2012054	10p			24 × 32 (plain)	-
AFI17	38p	BC187	22p 🥙			2N3054	58p	ZTX500		Pin insertion to	ol 52p
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DIODES	5		0.00	Ÿ.	
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BZVI0	800V	6A	25p	OA90	5
BZY13	200V	6A	20p	OA91	5
IN4001	50V	ĪA	7p	QA202	7
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OLID TANTALU	M BEAD C	APACIT	ORS			12p
0·14F		2.2µF		22,,,F	16V	
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7401	20	18	16	14	7451	20	18	16	14	74141	100	95	90	85
7402	20 -	18	16		7452	20	18	16	14	74145	150 ~	145	140	135
7403	20	18	16	- 17	7453	20	iš	16	14	74150	330	285	260	210
7404	20 20	18	16	- iā I	7454	20	18 .	16	14	74151	110	95	90	85
7405	20	18	16	i4	7460	20	18	16	14	74153	120	115	110	100
7406	56	48	37	30	7470	38	32	27	23	74154	200	190	180	170
7407	56	48	37	30	7472	34	30	27	21	74155	150	125	100	85
7408	36	28	20	20	7473	40	37	30	27	74156	130	120	100	80
7409	36	28	20	20	7474	40	35	30	25	74159	130	120	110	90
7410	20	īš	Ĩ6	14	7475	60	56	30 52	50	74180	155	135	120	100
7411	23	21	20	20	7476	40	36	32	30	74190	195	185	180	175
7412	36	32	28	24	7480	80	75	70	65	74191	195	185	180	175
7413	34 #	32	28	22	7481	125	120	115	110	74192	200	180	165	150
7416	45	38	32	32	7482	87	75	70	65	74193	200	180	165	150
7420	20	18	16	14	7483	100	95	90	85	74196	200	180	165	150
7421	36	32	28	23	7484	110	106	104	100	74197	160	150	145	140
7422	48	44	38	35	7485	-250 /	245	240	235					
7426	32	29	25	20	7486	45	40	35	30	7 W 1	LIN	IEAR I	Cs	
7427	42	38	36	34	7490	75 -	70	65	55 75	N ^				320
7428	50	45	40	32	749 I A	100	90	80	75	709	- 1	4 pin DIL		34
7430	20	18	16	14	7492	75	70	65	90	74!		8 pin DIL		28p 4
7432	40	36	32	25	7493	80	70	65	55	741	-	4 pin DIL 4 pin DIL		90p
7440	20	18	16	14	7494	85	80	75	70	723	- !	4 pin DIL		80p
7441A	80	76	70	66	7495	85	80	75	70	747 748		8 pin DIL		34p
7442	80	76	70	66	7496	100	95	90	85			4 pin and	l 6 pin	16p
7443	100	96	94	90	74100	250	245	240	235	DIL socket,		T pin and	o piii	ТОР

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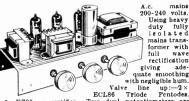
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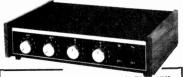
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NEW FURTHER IMPROVED MODEL WITH HIGHER OUTPUT AND INCORPORATING HIGH QUALITY READY DRILLED FIBRE GLASS PRINTED CIRCUIT BOARD WITH COMPONENT IDENTIFICATION CLEARLY COMPONENT ID: MARKED FOR STRUCTION EVEN EASIER

A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. (Very simple to modify to suit magnetic cartridge—instructions included). Output stage for any speakers from 6 to 15 ohms. Compact design, all parts supplied including drilled metal work, high quality ready drilled fibre glass printed circuit board, smart brushed anodised aluminium front panel with matching knobs, wire, solder, nuts, botte-mo extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Power output 14W r.m.s. per channel into 5 ohms. Frequency response ± 3dB 12-30,000Hz. Sensitivity better than 80mV into 1M Ω. Full power bandwidth ± 3dB 12-15,000Hz. Bass boost approx. to ± 12dB. Treble cut approx. to -16dB. Negative feedback 18dB over main amp. Power requirements 35V at 1-0 amp. Overall size-12* wide *8' deep × 24' nigh.
Fully detailed 7-page construction manual and parts list

ments 35 v at 1 v any.

**2\$ high.
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free with kit or send 18p plus large 8.A.E.

**PRICES** AMPLIFIER KYT 1 v and 1 v

CABINET. 28 P. & P 30p.
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Note: The above amplifier is suitable for feeding two mono sources into inputs (e.g. mike, radio, twin record decks, etc.) and will then provide mixing and fading facilities for medium powered Hi-Fi Discothegue use, etc.



3-VALVE AUDIO
AMPLIFIER HA34 MK II
Designed for Hi-Fi reproduction of records. A.C. Mains
operation. Ready built on
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tion of records. A.C. Mains operation. Ready built on plated heavy gauge metal chassis, size 71in w. ** vin. d. x 41in. b. Incorporates ECC83, EL84, EZ80 valves. Heavy duty, double wound mains transformer and output distance. We will be a speaker. Separate volume control and now with improved wide range tone controls giving bass and treble lift and cut. Negative feedback line. Output 44 watts. From panel can be detached and leads extended for remote mounting of controls. Complete with knobs, valves, etc., wired and tested for only \$4.95. P. & P. 35p.

HSL "FOUR" AMPLIFIER KIT, Similar in appearance to HA34 above but employs entirely different and advanced circuitry. Complete set of parts, etc. \$4·10. P. & P. 40p.

HARVERSON'S SUPER MONO AMPLIFIER MARVERSON'S SUPER MONO AMPLIFIER
A super quality gram amplifer using a double wound fully
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pentode valve as audio amplifer and power output stage.
Impedance 3 ohms. Output approx. 3-5 wats. Volume
and tone controls Chassis size only 71m. wide > 3in. deep ×
6in. high overall. AC mains 200/240V. Supplied absolutely
Brand New, completely wired and tested with good
output transformer.
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GEC 4 pole c/o 24V 670 ohm. GEC 2 pole on/off 24V 670 ohm. GEC 2 pole c/o 65V 5,000 ohm. STC 2 pole c/o 12V 170 ohm.

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PC102 Supply voltage 220-250V a.c. Output voltages: 21 Volts d.c. at 330MA 21 Volts a.c. at 540MA



#### NEWMARKET TRANSISTORS

NKT351   73p   NKT12399   27p   NKT223   30p   NKT218   23p   NKT2406   60p   NKT13329   27p   NKT22   30p   NKT221   30p   NKT221   30p   NKT221   30p   NKT221   30p   NKT221   30p   NKT223   30p   NKT232   31p   NKT240   37p								
NKT406   60p   NKT13329   27p   NKT72   25p   NKT222   18p	NKT351	73p	NKT12329	27p	2N2222	18p	NKT218	23p
NKT420   E1   90	NKT352	25p		27p	NKT12	30p	NKT'221	30p
NKT420	NKT406	60p	NKT13329	27p	NKT72	25p	NKT222	18p
NKT450   30p   NKT16229   27p   NKT121   2%p   NKT224   22p	NKT420	£1 80	NKT13429	27p	NKT73	22p	NKT223	250
NKT603   22p   NKT20329   28p   NKT124   28p   NKT227   23p   NKT6187   28p   NKT027   28p   NKT6187   30p   NKT60111   88p   NKT125   38p   NKT237   32p   NKT6171   8p   NKT6187   38p   NKT237   32p   NKT6171   8p   NKT6187   38p   NKT238   18p   NKT713   27p   8C108   8p   NKT128   23p   NKT249   29p   NKT736   30p   8C108   8p   NKT126   22p   NKT261   18p   NKT261   32p   8C108   8p   NKT126   22p   NKT261   18p   NKT261   22p   NKT270   22p   NKT270   23p   NKT271   18p   NKT261   22p   NKT362   23p   NKT361   22p   NK	NKT450	30p	NKT16229	27p	NKT121	2 LD	NKT224	
NKT613F   28p   NKT80111   88p   NKT125   38p   NKT237   21p	NKT603	22p	NKT20329	29p	NKT124		NKT227	
NKT674   30p   NKT80113   88p   NKT128   35p   NKT238   18p   NKT747   37p   NKT249   23p   NKT249   23p   NKT247   23p   NKT249   23p   NKT247   23p   NKT249   23p   NKT247   23p   NKT247   23p   NKT248   23p   NKT247   23p   NKT248   23p   NKT247   23p   NK	NKT613F	28p	NKT80111	65p	NKT125	38p	NKT237	
NKT677   18p   NKT60125   80p   NKT127   23p   NKT249   21p	NKT674	30p	NKT80113	98p	NKT126	35p	NKT238	
NKT713   27p   BC107   8p   NKT128   18p   NKT281   19p   NKT270   18p   NKT270	NKT677	180	NKT80125	80p	NKT 127		NKT249	
NKT734   24p   BC108   8p   NKT129   22p   NKT270   18p	NKT713	27p	BC107	8p M	NKT128	18p	NKT261	
NKT738   30p   BCY70   13p   NKT135   24p   NKT271   15p   NKT772   23p   BF51   17p   NKT135   30p   NKT271   15p   NKT0218   20p   BSY95A   10p   NKT142   48p   NKT273   15p   NKT3055   23p   24667   53p   NKT144   48p   NKT273   15p   NKT10339   23p   24p   24p   NKT24   48p   NKT274   15p   NKT10439   23p   24p   24p   NKT213   24p   NKT274   24p   NKT10439   25p   24p30   22p   NKT213   21p   NKT301   24p   NKT10439   20p   24p30   22p   NKT215   21p   NKT302   85p   NKT10439   20p   24p30   22p   NKT215   48p   NKT303   70p   NKT1045   20p   24p30   22p   NKT217   48p   NKT303   70p   NKT303   70p   NKT303   70p   NKT304   70p   NKT303   70p   NKT303   70p   NKT305   70p   NKT303   70p   NKT303   70p   NKT305   NKT305   70p   NKT303   70p   NKT305   NKT305   70p   NKT303   70p   NKT305   NKT305   70p   NKT305   70p   NKT305   NKT305   70p   NKT305   70p   NKT305   NKT305   70p   NKT305   70p   NKT305   NKT305   NKT305   70p   NKT305	NKT734	24p	BC108		NKT129		NKT270	
NKT773   23p   BFY51   17p   NKT137   30p   NKT272   15p   NKT0216   20p   BSy95A   10p   NKT142   48p   NKT273   18p   NKT3055   23p   2N697   13p   NKT143   48p   NKT274   16p   NKT6917   27p   2N706   8p   NKT212   23p   NKT274   15p   NKT10339   23p   2N914   15p   NKT213   23p   NKT275   15p   NKT10439   25p   2N914   28p   NKT214   21p   NKT301   70p   NKT10439   25p   2N930   22p   NKT215   19p   NKT301   70p   NKT10439   20p   2N1990   22p   NKT217   48p   NKT303   70p	NKT736	30p	BCY70		NKT135		NKT271	
NKT0216   20p   BSY95A   10p   NKT142   48p   NKT273   18p     NKT3055   23p   2Me97   13p   NKT143   48p   NKT274   48p     NKT8917   27p   2M706   8p   NKT212   23p   NKT275   21p     NKT10319   23p   23p   23p   NKT275   21p     NKT10419   17p   2M918   28p   NKT213   23p   NKT275   21p     NKT10419   17p   2M918   28p   NKT214   21p   NKT301   70p     NKT10519   20p   2M930   22p   NKT215   19p   NKT302   85p     NKT10519   20p   2M1990   22p   NKT217   48p   NKT303   70p     NKT303   70p   2M1990   2M199	NKT773	23p	BFY51	17p-	NKT137	30p	NKT272	
\[ \text{NKT3055} \] 23p \[ \text{NKT273} \] 27p \[ \text{NKT0776} \] 8p \[ \text{NKT143} \] 48p \[ \text{NKT274} \] 19p \[ \text{NKT275} \] 27p \[ \text{NKT066} \] 8p \[ \text{NKT275} \] 23p \[ \text{NKT275} \] 23p \[ \text{NKT275} \] 23p \[ \text{NKT275} \] 23p \[ \text{NKT276} \] 8p \[ \text{NKT276} \] 18p \[ \text{NKT303} \] 8p \[ \text{NKT302} \] 8p \[ \text{NKT303} \]	NKT0216	20p	BSY95A	10p	NKT142		NKT273	
NKT6917   27p   2N706   8p   NKT212   23p   NKT275   21p   NKT10339   23p   23p   23p   23p   23p   23p   23p   23p   NKT275   21p   NKT10419   17p   2N918   28p   NKT214   21p   NKT301   70p   NKT10439   25p   2N802   22p   NKT215   19p   NKT302   85p   NKT215   20p   2N990   22p   NKT215   48p   NKT303   70p   2NF215   2N	NKT3055	23p	2N697	13p #	NKT143		NKT274	
NKT10339 23p 2N914 15p NKT213 23p NKT278 18p NKT10439 17p 2N918 28p NKT214 21p NKT301 70p NKT10439 25p 2N930 22p NKT215 19p NKT302 85p NKT305 20p 2N990 22p NKT215 48p NKT303 70p	NKT6917	27p	2N706	8p 46	NKT212		NKT275	
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NKT10439 25p 2N930 22p NKT215 19p NKT302 85p NKT10519 20p 2N1990 22p NKT217 48p NKT303 70p	NKT10419	17p	2N918	28p	NKT214		NKT301	
NKT10519 20p 2N1990 22p NKT217 48p NKT303 70p		25p	2N930	22p	NKT215		NKT302	
	NKT10519	20p	2N 1990	22p	NKT217		NKT303	
							NKT304	



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TYPE			COIL RESISTANCE (OHMS)	PRICE EACH
250 ARO	4 CHANGEOVER	6V d.c.	52	88 03
250 ABO	4 CHANGEOVER	48V d.c.	2,500	88 02

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Single Pole C/O Single Pole C/O Single Pole C/O

COIL VOLTAGE 6V d.c. 12V d.c. 18V d.c.

COIL RESISTANCE 140 ohm 350 ohm 875 ohm

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Mounted on Modular Type Chassis with front
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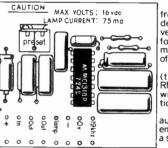
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complete set of parts from Jermyn to build a stereo decoder module that will convert your existing mono tuner for stereo reception whilst maintaining a high standard of reproduction.

The distortion is very low (typically 0.3% at 560 mV RMS composite input signal) with 40dB channel separation.

The stereo switching is automatic and there is a light emitting diode which acts as a stereo beacon.

The kit requires no coil and there are no alignment problems.

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Of course, if you have a modern mono tuner with a multiplex output our module simply plugs in.

The outputs go via a screened twin cable to the tuner inputs of your stereo amplifier.
And the cost? £4.90 for the Kit with 100% tested integrated circuit.

Also available assembled and aligned, checked and ready for use at £6.90 (includes 12 month guarantee). Beat that!

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Please rush me Kit(s). made up Stereo decoders. I enclose cheque/postal order for £

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Plays 12", 10" or 7" records.
Auto or Manual. A high
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reliability with 12 months'
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Size 18½ v. 11/in.
Above motor board 3 jin. below motor board 2 jin.



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E.M.I. WOOFER AND £5.75

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Comprising a fine example of a Woofer

102 × 6 fin. with a massive Ceramic

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Tweeter 3 lin. square has a special light
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10,000 lines. Crossover condenser and

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Lmpedance Standard

8 ohms

Maximum Power

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Useful Response

35 to 18,000 c/s

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SUITABLE ENCLOSURE 20 x 13 x 9in.
MODERN DESIGN. TEAK WOOD FINISH SPECIAL OFFER!

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16/450V	15p	1000/50V.	. 47p		. 3	3р
32/450V	20p	8+8/450V	18p	350 + 50/325V		Ôπ
25/25V	10p	8 + 16/450				
50/50V	10p			32 + 32 + 32/350		3
100/25V	10p	32 + 32/350	V 25p	100 + 50 + 50/8	50 V 4	8p
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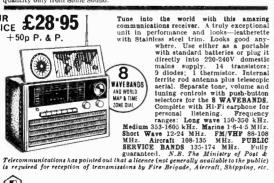




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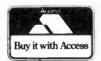
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Type	L.	w.		rice p	
GB7 *	5±in	2∄in	1±in	38p	15p
GB8 *	4in	4in	1 in	38p	15p
GB9 *	4in	2±in	1 in	38p	13p
GB10*	5±in	4in	1+in	44p	18p
GBII	4in	2tin	2in	38p	13p
GB12	3in	2in	lin	33p	13p
GB13	6in	4in	2in	52p	18p
GBI4	7in	5in	2+in	63p	19p
GB15	8in	6in	3in	8lp	26p
GBI6	loin	7in	3in	92p	26p
			These	sizes	fit
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1	-	-	verol	poard	s

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	0.1	0-15
Size	matrix	matrix
2∮in × 3∄in	22p	I6p
2∯in × Šin	24p	25p
3½in × 3½in	24p	25p
3∄in × 5in	27p	29p
l7in × 2∮in	75p	57p
l7in × 3∯in	£I	75p
Mina alabanai-		of 26 18m

#### **ELECTROLYTICS**

IμF	450V	19p	1,000µF	25V	27 p
2µF	450 V	20p	1,000µF	50 V	42p
4µF	350V	14p	2,000µF	25 V	39p
8µF	450 V	17p	2.000µF	50 V	53p
164F	450V	18p	2,500µF	25 V	45p
25µF	25V	7p	2,500µF	50 V	60p
25µF	50 V	10p	3,000µF	25 V	48p
32µF	450V	27 p	5.000 J.F	25	60p
50µF	50 V	IOp	5,000µF	50V	£1 10
100µF	25 V	10p	8-8uF	450V	18p
100µF	50 V	Hp	8-16µF	450V	20p
250µF	25V	14p	16-16µF	450V	27 p
250µF	50 V	17p	16-32µF	450V	63p
500µF	2SV	18p	32-32 ₄ F	450V	49p
500µF	50 V	25p	50-50µF	350V	38p

#### MINIATURE ELECTROLYTICS

14F	63V	6p	47µF	167	7p
2-2µF	63V	6p	47µF	25 V	6р
3-3µF	63V	6р	68 µF	167	6р
4-7µF	63V	6p	100µF	107	6р
8µF	40 V	7p	220µF	16V	7 _P
ΙOμF	25V	6p	330µF	167	Пp
10µF	64V	7 _p	470µF	107	Пp
16µF	40 V	7p	1,000µF	16V	19p
33/4F	167	6p	1,500µF	167	23p

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#### CONTROLS, Log. or Lin.

Single, less switch, 15p Single, D.P. switch, 24p Tandem, less switch, 40p 5kΩ, 10kΩ, 25kΩ, 50kΩ, 100kΩ, 250kΩ, 500kΩ, 11MΩ, 2MΩ

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Carbon
All 5%, high-scability, E12 values. ‡W, Ip;
‡W, Ip; 1W, 4p; 2W, 6p
Wire-wound
5W, 10p; 10W, 12p

#### **SWITCHES**

Toggle switches, standard size.
SW20—S.P.S.T. 18p; SW21—D.P.D.T. 23p. Push Button, miniature, SWI-13p.

Wafer switches (rotary)—13p, Wafer switches (rotary)—14p each. SW4—1 pole, 12 way. SW5—2 pole, 6 way. SW6—3 pole, 4 way, SW7—4 pole, 2 way. SW8—4 pole, 3 way.

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14p 9p 10p Car aerial
Co-axial
D.I.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 3 pin
D.I.N. 5 pin, 180
D.I.N. 5 pin, 240
D.I.N. 6 pin
Jack, 2 jmm unscreened
Jack, 2 jmm unscreened
Jack, 3 jmm unscreened
Jack, 3 jmm screened
Jack, in screened
Jack, in screened
Jack, sereo, unscreened
Jack, stereo, unscreened 13p 14p 13p 15p 15p Phono, plastic top Phono, plated metal Wander, red or black Banana 4mm, red or black 12

#### LINE SOCKETS

Car aerial Co-axial D.I.N. 2 pin (speaker) D.I.N. 3 pin D.I.N. 5 pin, 180° D.I.N. 5 pin, 240° Jack, 3½mm Jack, ½in screened Jack, stereo, screened Phono, plated meta¹

# CERT

0.0027µF

2	SOCKETS	
P	Car aerial	8р
	Co-axial, surface	8р
P	Co-axial, flush	9p
P	D.I.N. 2 pin (speaker)	10p
P	D.I.N. 3 pin	9p
Р	D.I.N. 5 pin, 180°	9 _D
P	D.I.N. 5 pin, 240°	9p
	Jack, 2+mm	10p
	Jack, 3+mm	10p
_	Jack, Jin unswitched	15p
Р		17p
P	Jack, £in switched	
P		24p
P	Phono, single	5p
P	Phono, 2 on a strip	7p
P	Phono, 3 on a strip	9p
p	Phono, 4 on a strip	10p
P	Wander, single, red or black	5p
p	Wander, twin strip	7p
D	Banana 4mm red, or black	6p

500V S/M

15p

#### CAPACITORS

9414	0110			0 003µF	500 V	Cer.	5p
2-2pF	500V	5/M	7 p	0.0033µF	125V	P.S.	6р
3-3pF	500V	5/M	71p	0 0033µF	500V	Poly.	6р
5pF	V002	S/M	7 i p	0.0033µF	1,000∨	MDC	6p
10pF	125∨	P.S.	5p	0 0036μF	500∨	S/M	I5p
10pF	500 V	S/M	7 1 p	0.0047µF	125∨	P.S.	9p
15pF	125	P.S.	5p	0.0047µF	500V	Poly.	6р
15pF	500 V	Cer.	4p	0.0047µF	500∨	S/M	20p
18pF	500 V	S/M	71p	0-0047µF	V000,1	MDC	6р
22pF	125	P.S.	5p	0.005µF	100∨	Mylar	3р
22pF	500V	5/M	7 1 p	0.005µF	S00∨	Cer.	5p
25pF	500V	S/M	7 ip	0.0068µF	125V	P.S.	10 p
27 p F	500 V	Cer.	4p	0 0068µF	500∨	S/M	30p
33pF	125V	P.S.	5p	0.0068µF	500 V	Poly.	6р
33pF	500∨	S/M	7 i p	0.0082µF	125V	P.S.	101p
39pF	500∨	S/M	7 ip	0.0082µF	500 V	S/M	30p
47pF	125V	P.S.	5p	0.01µF	187	Disc	4p
47pF	500V	Cer.	4p	0.01µF	125	P.S.	10 lp
50pF	500∨	5/M	7 p	0 0 I µ F	160V	Poly.	4p
56pF	500 V	S/M	7 ip	0.01µF	250 V	M.F.	3p
68pF	125∨	P.S.	_5p	0.01µF	400 V	Poly.	3p
68pF	500V	S/M	7 1 p	0 01 µF	500V	Cer.	5p
75pF	500 V	S/M	71P	0.01 trE	500 V	5/M	30p
82pF	500 V	5/M	7 <u>1</u> p	0.01µF	600V	MDC	7p
I OOp F	125V	P.S. S/M	5p 7 <del>1</del> p	0.01µF	1,000∨	MDC	9p
100pF	500 V	S/M	7 <u>}</u> p	0.015μF	160V	Poly.	3p
100pF	500∨	Cer.	_5p	0.015µF	400V	Poly.	3р
120pF	500V	S/M	7 1 p	0·02μF	100V	Mylar	3p
150pF	125V	P.S.	_5p	0 022µF	187	Disc	5p
150pF	500V	S/M	7 1 p	0 022μF	250V	M.F.	3p
150pF	500V	Cer.	.5p	0 022μF	400V	Poly. MDC	3p
180pF	500 V	S/M	7 i p	0·022μF	600V	MDC	7 1 p
200 pF	500V	S/M	7 jp	0.022µF	1,000∨	MDC	10p
220pF	125V	P.S.	5p	0 033μF	250V	M.F.	4p
220pF	500V	Cer.	5p	0.033µF	400V	Poly.	4p
250pF	500V	5/M	8p	0.047µF	120	Disc	6p
270pF	500V	Cer.	5p	0·047μF	160V	Poly.	3p
300pF	500V	S/M	8p	0.047jzF	250V	M.F.	3p
330pF	125V	P.S.	5p	0.047µF	400V	Poly.	4p
330pF	500V	S/M	8p	0·047μF	600V	MDC	8p
390pF	500V	S/M	8p	0.047µF	1,000∨ 30∨		10p
470pF 470pF	125 V 750 V	P.S.	5p	0.1 µF	250 V	Disc M.F.	6p
		Disc	5p	0.1µF	400V		4p 5p
500pF 560pF	500∨ 500∨	S/M S/M	8р	0·1μF 0·1μF	600V	Poly. MDC	10p
680pF	1257	P.S.	8p	0 1µF	1,000 V	MDC	14p
	500V	S/M	6р	0.15µF	250V	M.F.	5p
680pF 820pF	500V	S/M	8p	0.22µF	160V	Poly.	6p
0.001µF	1007	Mylar	8p 3p	0·22μF	250V	M.F.	5p
0.001 µF	125	P.S.	6p	0.22µF	400 V	Foil	10p
0 001µF	400V	Poly.	3p	0 22µF	1,000	MDC	15p
0 001µF	500 V	S/M	Q01	0·33µF	250V	M.F.	8p
0 001µF	500 V	Cer.	5p	0.47µF	250V	M.F.	8p
0 00 I µF	1.0000	MDC	6p	0.47µF	400 V	Foil	15p
0 0015µF	400V	Poly .	3p	0.47µF	1,000	MDC	25p
0 0015µF	500 V	S/M	100	1.0µ.F	250V	M.F.	15p
0.0015µF	500V	Cer.	5p	· Opti	250 4		.50
0.0018µF	500 V	S/M	10p	Note:			
0.002µF	100 V	Mylar	3p	S/M = si	lver mica	1% to	L.
0.002µF	500 V	Cer.	5p	P S. = D	olystyren	e 21%	tol.
0.0022µF	1257	P.S.	6p	MDC-	a.c. ratin	g = 300	V
0 0022µF	500V	S/M	IOp		fullard m		
0.0022µF	1,000V	MDC	6р	Cer. = c			
	.,000 1						

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Hex. Inverter,	BMC935	12p	Hp	10p
Hex. Inverter,	BMC936	12p	Hp	10p
Hex. Inverter,	BMC937	12p	Hp	10p
Hex. Inverter.	BMC940	120	Hp	10p
Hex. Inverter.	BMC941	12p	ile	10p
Type D Flip Flop,	BMC942	20p	18p	16p
Ex. 2/4-input Power,	BMC944	12p	Пp	100
Clocked Flip Flop,	BMC945	20p	180	16p
4/2 Input Nand Gate	BMC946	Hp	10p	9p
Clocked Flip Flop,	BMC948	20p	18p	16p
4/2 Input Nand Gate	BMC949	120	lip	10p
Pulsed Trig. Binary,	BMC950	20p	681	I6p
Monostable Multivib		25p		10p
			23p	21p
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Dual J/K Flip Flop,	BMC955	20p	18p	16p
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Quad. 2-input Power,		12p	Hp	10p
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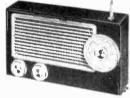
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* These sizes accept standard veroboard range. Nos. 12 to 16 available 15th January onwards.

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Precision made-as used in record decks and tape recorders-ideal also for extractor fan, blower, heaters, etc. New and perfect. Snip at 65p. Postage 20p for first one then 10p for each one ordered.



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#### ISA ELECTRICAL PROGRAMMER

PROGRAMMER
Learn in your sleep;
Have radio playing and
kettle boiling as you
awake—switch on lights
to ward off intruders—
have warm house to come
clock by famous maker with 15 amp. on/off
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memory jogger. A beautifulunit. Price \$\frac{1}{2}\text{0}\text{0}\text{p} \text{ a} \text{ p} \text{ or with lights}
extra.

RESETTABLE FIGURE 1.



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How long does it take you to renew a
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THERMOSTATS

Type "A" 15A for controlling room heaters, greenhouses, airing cupboards. Has spindle for pointer knobs. Quickly adjustable from 30-38 deg. F. 48p. Type "B" 10A. This is a 17in long rod type nusde by the famous Sunvic Co. Spindle adjusts this from 50-50 deg. F. Internal screw alters the setting so this could be adjustable over 30 deg. to 1,000 deg. F. Suitable for controlling furnace, oven, klin, immersion heater or to make flame-stat or fire alarm. Son blue 194 nost and flame-stat

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2kW. Model as above except 2 kilowatts \$25.50. Don't nilse this. Control Switch \$55, P. & P. 40p.



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This heading is not quite accurate because it is not a variable transformer that we are offering but a solid state device which serves the same purpose in almost all applications and, of course, much smaller. Made by Ultra Electronics, can be fitted into ordinary switch box. Engrave a circle on the front plate, mark this off in divisions, fit a pointer knob, calibrate with your volumeter (you will find the scale almost linear) you now have a power controller equal to a 5 anny variac costlang £12 or more.

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 8 way
 9 way
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#### POCKET BLEEPERS

POCKET BLEEPERS

These work on quite a low frequency, are carried in the pocket, and are mainly used in large buildings or areas so that key personnel may be contacted quickly. These contain two encapsulated circuits to energise the reisy and cause the bleep as well as rechargeable nickel cadmium cells. Quite costly things to buy. The ones we have are not new, but believed to be in good working order and sold on the understanding that if they are not, they will be replaced free. The size of the case, which is intended for carrying in top pocket, is approx. 4½ in long, 2in wide and 2in thick. Limited quantity at 22 each.

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Test continuity of any low resistance circuit, house wiring, car electrics. Tests polarity of diodes and rec-tifiers. Also ideal size for conversion to signal injector (circuit supplied). 30p or 2 for 50p post paid.



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THIS BALANCE KIT FREE Eagleeducational kits. Japanese made these are excellent value for money. We

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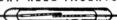
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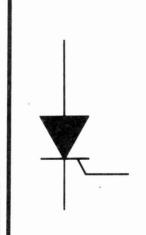
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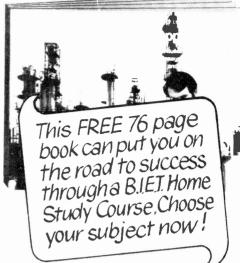
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