PRACTICAL

# El-ETRONICE JANUARY 1974 <br> 20p 



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 STEREO \& MONOPlays $12^{*}, 10^{*}$ or $7^{\prime \prime}$ records Auto of Manual. A high quality unit backed by BSR reliebility with 12 montha
guarantee. AC $200 / 250 \mathrm{~V}$ guarantee. 18 AC Size $18 \frac{1}{\frac{1}{2} \times 11 \frac{1}{4} \text { in. }}$ Above motor board 3 in. Below motor board 2$\}$ in. with STEREO and MONO XTAL $\mathbf{6 6 . 2 5}$ Post 25p.

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65.95 ${ }_{25 p}^{\text {Pont }}$

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COMPACT PORTABLE STEREO HI-FI Two full size loudspeakers $13 i \times 10 \times 3$ in. Player unit clips to loudapeakers making it extremely compact, overall size only 13$\} \times 10 \times 8 \frac{1}{2}$., 3 watt per channel, playi all recorda 33 r.p.m., $45 \mathrm{r} . \mathrm{p} . \mathrm{m}$. Separate volume and tone


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PRICE $\mathbf{4} \cdot 65$ or $\mathbf{6}$ pair. Post $25 p$ (PLEASE STATE TYPE A OR B WITH ORDER.) BLANK ALUMINIUM CEASSIS. 18 s.w.g. $2 \%$ in giden $6 \times 4$ in $45 p ; 8 \times 6$ in 53p; $10 \times 7$ in $65 p ; 12 \times 8 i n 85 p ;$
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 $14 \times 6 \mathrm{in} 28 \mathrm{p} ; 14 \times 9 \mathrm{in} 34 \mathrm{p} ; 12 \times 12 \mathrm{in} 40 \mathrm{p} ; 16 \times 10 \mathrm{in} 50 \mathrm{p}$. PAXOLIN PANEL $10 \times \sin 15 \mathrm{p}$.
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$16 / 450 \mathrm{~V}$ $16 / 450 \mathrm{~V}$
$32 / 500 \mathrm{~V}$ $32 / 500 \mathrm{~V}$ $50 / 50 \mathrm{~V}$ $100 / 25 \mathrm{~V}$ 14 p
14 p
18 p
22 p
50 p
10 D
10 p
10 p 250/25V $50+50 / 300 \mathrm{~V}$
$60+100 / 350 \mathrm{~V}$
$32+32 / 250 \mathrm{~V}$ $32+32 / 450 V$ $\begin{array}{ll} & 20 \mathrm{p} \\ 32+32 / 450 V & 60 \mathrm{p}\end{array}$ $16+16+16 / 275 \mathrm{~V} 45 \mathrm{p}$ $100+50+50 / 350 \mathrm{~V} 5 \mathrm{5p}$ $100 / 25 \quad 10 \mathrm{p} \left\lvert\, \begin{array}{ll}18+18 / 450 \mathrm{~V} \\ 32+32 / 350 \mathrm{~V} & 40 \mathrm{p}\end{array}\right.$ LOW VOLTAGE ELECTROIYTYCS
$1,2,4,5,8,16,25,30,50,100,200 \mathrm{mF} 15 \mathrm{~V} 10 \mathrm{p}$ $500 \mathrm{mF} 12 \mathrm{~V} 15 \mathrm{p} ; 25 \mathrm{~V} 20 \mathrm{p} ; 50 \mathrm{~V} 30 \mathrm{p}$.
$1000 \mathrm{mF} 12 \mathrm{~V} 20 \mathrm{p} ; 25 \mathrm{~V} 35 \mathrm{p} ; 50 \mathrm{~V} 47 \mathrm{p}$. $1000 \mathrm{mF} 12 \mathrm{~V} 20 \mathrm{p} ; 25 \mathrm{~V} 35 \mathrm{p} ; 50 \mathrm{~V} 47 \mathrm{D} ; 100 \mathrm{~V} 70 \mathrm{p}$. 2000 mF BV $25 \mathrm{p} ; 25 \mathrm{~F} 42 \mathrm{p} ; 50 \mathrm{~V} 57 \mathrm{p}$.
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The moving coil diaphragm gives a good radiation pattern to the higher frequencies and a amooth extontion of tokal response $31 \times 2$ in deep. Rating $10 \mathrm{~m} / \mathrm{size} 3 \frac{1}{4}$ Crossozer 95p

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Useful response
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Bass Remonance
Flux Density $14,000 \begin{gathered}30 \mathrm{cps} \\ \text { ganas }\end{gathered}$ Uselul response $25-16,000 \mathrm{cp}$ 8 or 15 ohma models.

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A high quality loudspeaket, its remarkable low cone
resonance ensures clear resonance ensures clear
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BYZ10 \& \(\left.\begin{array}{l}\text { Ap } \\
0.45 \\
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\end{tabular} \& OAZ209 \&  \& \& \({ }_{\substack{8 \\ 0.10}}\) \\
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\hline \(1{ }^{1} 25\) \& 0.20
0.05 \& \(\begin{array}{ll}\text { A8Y50 } \& 0.20 \\ \text { ASY51 } \& 0.40\end{array}\) \& BYZ88C3V3 \({ }_{0.10}\) \& \({ }_{0}^{0} \mathrm{AZ} 241\) \& 0.88 \& ZTX 300 \& 0.14 \\
\hline 1 N 914 \& 0.05 \& \begin{tabular}{ll} 
A8Y563 \& 0.40 \\
\hline A 20
\end{tabular} \& BZY88C3V3 \({ }^{0.10}\) \& \({ }_{\text {OAZ242 }}^{0}\) \& 0.28 0 \& \({ }_{\text {ZTX }}\) \& \({ }_{0}^{0.24}\) \\
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0.40 \&  \& crsi/05 0 0.80 \& \({ }_{0}^{0 \mathrm{CCl} 16 \mathrm{~T}}\) \& 0 \& \& \\
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0.85 \& \(\begin{array}{ll}\text { AsZ23 } \& 0.75\end{array}\) \&  \& OC19 \& 0.50 \& CIRCUIT \& \\
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\hline \(2 \mathrm{G417}\) \& 0.25 \& AUY10 1.00 \& DD000 0.15 \& 0c22 \& 1. \& \& 0.20 \\
\hline 2 N 404 \& 0.21 \& \(\begin{array}{ll}\text { BC107 } \\ \text { AC108 } \& 0.12 \\ 0.12\end{array}\) \& DD003
DD006 \& 0 C 23 \& 1.25 \& \({ }_{7402}\) \& \({ }_{0.20}\) \\
\hline \({ }^{2} \mathrm{~N}\) N697 \& 0.16
0.30 \& \(\begin{array}{ll}\text { AC109 } \& 0.12 \\ \text { B.12 }\end{array}\) \& \(\begin{array}{ll}\text { DD006 } \& 0.18 \\ \text { DD007 } \& 0.40\end{array}\) \& -0C25 \& 0 \& 7403 \& 0.20 \\
\hline \({ }_{2}{ }_{2} \mathrm{~N} 706\) \& 0.10 \& \(\begin{array}{ll}\text { BC113 } \& 0.18\end{array}\) \& \({ }^{\text {DD008 }} 00.88\) \& \(\mathrm{OC}_{26}\) \& 0.85 \& 7404 \& 0.20 \\
\hline \({ }_{2}\) N706A \& 0.12 \& \(\begin{array}{ll}\mathrm{BC115} \& 0.20\end{array}\) \& OD3 0.83 \& OC28 \& 0.65 \& \({ }_{7406}^{7405}\) \& \({ }_{0}^{0.40}\) \\
\hline 2 N 708 \& 0.16 \& \({ }_{\text {BC118 }} \quad 0.20\) \& \({ }^{\text {GD4 }} 00.10\) \& OC29 \& 0.8 \& \({ }^{7407}\) \& 0.40 \\
\hline 2 N 709 \& \({ }^{0.40}\) \& \(\begin{array}{ll}\text { BC118A } \& 0.28 \\ \text { BC1 } \& 0.15\end{array}\) \& \(\begin{array}{ll}\text { GD5 } \& 0.88 \\ \text { GD8 } \& 0.26\end{array}\) \& - \& 0.40 \& 7408 \& 0.25 \\
\hline \({ }_{2}^{2 N 1091}\) \& 0.05 \& \(\begin{array}{ll}\text { BC121 } \& 0.20\end{array}\) \& GD12 0.10 \& OC36 \& 0.65 \& 7409 \& 0.89 \\
\hline 2 N 132 \& 0.25 \& \({ }^{\text {BC }} 12200.20\) \& GET102 0.50 \& \(\mathrm{OC}^{0} 1\) \& 0.85 \& \({ }_{7411}\) \& 0.28 \\
\hline \({ }_{2}^{2 N 1302}\) \& \({ }_{0}^{0.18}\) \& \begin{tabular}{ll}
\({ }^{\text {BCL }}\) BC125 \& 0.88 \\
0.85 \\
\hline
\end{tabular} \& GET103 \({ }_{\text {GET } 113}^{0.40} 0\) \& OC42 \& 0.40
0.70 \& 7412 \& 0.28 \\
\hline \({ }_{2}^{2 N 1303}\) \& \({ }_{0}^{0.28}\) \& \({ }^{\text {BC }} 14000.85\) \& GET114 \({ }^{\text {GEP }}\) \& Oc44 \& 0.18 \& 7413 \& 0-90 \\
\hline 2 N 1305 \& 0.22 \& \(\begin{array}{ll}\text { BC147 } \& 0.12\end{array}\) \& GET115 00.75 \& \({ }^{\text {OC44 }}\) 4 \& 0.17 \& \({ }_{7416}\) \& 0.80 \\
\hline 2 N 1308 \& 0.88 \& \(\begin{array}{ll}\text { BC148 } \& 0.10 \\ \text { BC149 } \& 0.12\end{array}\) \& GET116 \({ }_{\text {GET }} \mathbf{0 . 8 5}\) \& \({ }^{\text {OC4 }}\) \& \({ }_{0}^{0.18}\) \& 7420 \& 0-20 \\
\hline \({ }_{2}^{2 N 1307}\) \& \({ }_{0}^{0.28}\) \&  \& \(\begin{array}{lll}\text { GET872 } \& 0.30\end{array}\) \& \({ }_{0} \mathrm{CL}^{6}\) \& \({ }_{0.27}\) \& \({ }_{7422}\) \& 0.28 \\
\hline 2 N 2147 \& 0.76 \& \({ }^{\text {BCL }} 500.12\) \& GET875 0.40 \& OC57 \& 0.80 \& \({ }_{7425}\) \& 0.40 \\
\hline \({ }_{2}{ }^{\text {N148 }}\) \& \({ }_{0}^{0.60}\) \& \(\begin{array}{ll}\text { BC160 } \& 0.83 \\ \text { BC169 } \& 0.14\end{array}\) \& \(\begin{array}{ll}\text { GET880 } \\ \text { GET891 } \& 0.65 \\ 0.25\end{array}\) \& OC58 \& \({ }_{0}^{0.80}\) \& 7427 \& 0.87 \\
\hline \({ }_{2 \times 2218}\) \& \({ }_{0}^{0.81}\) \& \(\begin{array}{ll}\text { BCY } 31 \& 0.45\end{array}\) \& \(\begin{array}{ll}\text { GET88.2 } \& 0.25 \\ 0.85\end{array}\) \& OC66 \& 0.50 \& 7428 \& 0.48 \\
\hline 2 N 2219 \& 0.25 \& \({ }^{\text {BCY }} 320.85\) \& \(\begin{array}{ll}\text { GET885 } \& 0.36\end{array}\) \& 0c70 \& 0.18 \& \({ }_{7432}\) \& \({ }_{0}^{0.20}\) \\
\hline 2 N 2369 A \& \({ }^{0.16}\) \& \begin{tabular}{ll} 
BCY33 \& 0.38 \\
BCY 34 \& 0.45 \\
\hline
\end{tabular} \& \({ }_{\text {GEX } 445 / 1}^{0.088}\) \& \({ }_{\text {OC71 }}^{\text {OC72 }}\) \& 0.15 \& 7433 \& 0.48 \\
\hline \({ }_{2}^{2 N} 24244\) \& 1.98
0.28 \& \(\begin{array}{ll}\text { BCY38 } \& 0.55\end{array}\) \& \(\begin{array}{lll}\text { GEX45/1 } \& 0.46 \\ \text { GEX941 }\end{array}\) \& OC73 \& 0.60 \& 7437 \& 0.48 \\
\hline \({ }_{2}\) N2646 \& 0.50 \& \({ }^{\text {BCY }} 391.00\) \& G33M \(\quad 0.60\) \& OC74 \& \(0 \cdot 30\) \& \({ }_{7440} 7438\) \& 0.48 \\
\hline 2 N 2904 \& 0.20 \& \({ }^{\text {BCY } 40} 0080\) \& \({ }_{\text {GJ4M }}\) \& 0075 \& 0.80 \& 7441AN \& \({ }_{0}^{0.85}\) \\
\hline 2N2904 \& \& BCY42
BCY70 \& \(\begin{array}{ll}\text { GJJ5M } \\ \text { GJ7M } \& 0.25 \\ 0.50\end{array}\) \& \({ }_{\text {OC76 }}^{\text {OC77 }}\) \& 0.30
0.55 \& 74 \& 0.85 \\
\hline \({ }^{2} \mathrm{~N} 2900 \mathrm{~A}\) \&  \& \(\begin{array}{ll}\text { BCY71 } \& 0.20\end{array}\) \& \({ }_{\text {HG1 } 1005}{ }^{\text {GJP50}}\) \& \(\bigcirc \mathrm{C} 78\) \& \({ }_{0.25}\) \& 7450 \& 0.20 \\
\hline \({ }^{2} \mathbf{2 N} 29297\) \& 0.28 \& BCZ10 0.60 \& HS100A \(\quad 0.20\) \& OC79 \& 0.80 \& 7451 \& 0.20 \\
\hline 2 N 2925 \& 0.15 \& \({ }^{\text {BC211 }} 0\) \& MAT100 0.20 \& OC81 \& 0.28 \& \({ }^{7453}\) \& \(0 \cdot 20\) \\
\hline 2N2926 \& 0.10 \& ED121 1.00 \& MATT101 0.25 \& \(0_{0}^{0 C 81 D}\) \& 0.28 \& 7460 \& \({ }_{0}^{0.20}\) \\
\hline \(2 \mathrm{~N}^{2054}\) \& 0.45 \&  \& MAT120 0.20 \& \({ }_{\text {OC81M }}^{\text {OC81DM }}\) \& \({ }_{0}^{0.20}\) \& 7470 \& 0.88 \\
\hline \({ }_{2}^{2 N 300 ̄ 5}\) \& \({ }_{0}^{0.46}\) \& \({ }_{\text {BDY } 11}{ }^{\text {B1/45 }}\) \& \begin{tabular}{lll} 
M JE 220 \& 0.65 \\
\hline 0.65
\end{tabular} \& \({ }_{\text {OC812 }}\) \& 0.45 \& 7472 \& 88 \\
\hline 2N3705 \& 0.12 \& \({ }^{\text {BF115 }} 0\) \& MJE2955 1.10 \& 0 C 82 \& 0-28 \& \({ }^{7474}\) \& \({ }^{0.44}\) \\
\hline 2 N 3708 \& 0.11 \& \({ }^{\text {BF }} 117{ }^{\text {d }}\) \& MJE3055 0.75 \& \({ }^{\text {OC822 }}\) \& 0.25 \& 7475 \& 0.69 \\
\hline 2N3707 \& 0.18 \& \begin{tabular}{ll} 
BF167 \& 0.28 \\
BF173 \& 0.25 \\
\hline 0
\end{tabular} \& NKT128 0.45 \& OC83 \& 0.25 \& 7476 \& 16 \\
\hline 2 N 3709 \& \({ }_{0}^{0.11}\) \& \(\begin{array}{ll}\text { BF181 } \& \\ \text { BF173 }\end{array}\) \& NKT211

NKT25 \& ${ }_{\text {OCl14 }}$ \& ${ }_{0}^{0.38}$ \& 7480 \& 0.80 <br>
\hline 2N3710 \& 0.11 \& BF184 0.22 \& NKT213 ${ }_{\text {N }}$ \& -C122 \& 1.00 \& 7482 \& 0.87 <br>
\hline $2{ }^{2} 3819$ \& 0.85 \& ${ }^{\text {BF185 }} 0.028$ \& NKT214 0.84 \& ${ }_{0}^{0} \mathrm{OCl}_{123}$ \& 1.10 \& ${ }^{7484}$ \& 1.20 <br>
\hline 2N5027 \& 0.53
0.33 \& $\begin{array}{ll}\text { BF194 } & 0.13 \\ \mathbf{B F 1 9} & \\ 0.13\end{array}$ \& $\begin{array}{lll}\text { NKT216 } & 0.40 \\ \text { NKT217 }\end{array}$ \& OC149 \& ${ }_{0}^{0.40}$ \& 7486 \& 0.50 <br>
\hline ${ }_{28301}$ \& ${ }_{0} 0.58$ \& ${ }^{\text {BF }} 19680.15$ \& $\begin{array}{lll}\text { NKT218 } & 1.18\end{array}$ \& ${ }^{\text {OCl141 }}$ \& 0.80 \& ${ }_{741 \mathrm{~A}}^{7490}$ \& 0.75
1.10 <br>
\hline 28304 \& 1.16 \& ${ }^{\text {BF197 }} 0$ \& NKT219 0.88 \& OC169 \& 0.20 \& 7492 \& 1.10
0.76 <br>
\hline 28501 \& 0.87 \& ${ }^{\text {BF861 }}$ \& NKT222 0.80 \& ${ }^{0} \mathrm{C} 170$ \& 0.25 \& ${ }_{7493}$ \& 0.0 <br>
\hline ${ }^{28703}$ \& 1.00
0.20 \& $\begin{array}{ll}\text { BF898 } \\ \text { BFX12 } & 0.25 \\ 0.20\end{array}$ \& $\begin{array}{lll}\text { NKT224 } & 0.25 \\ \text { NKT251 } & 0.24\end{array}$ \& OC171
0.200 \& ${ }_{0}^{0.35}$ \& ${ }^{7494}$ \& 0.85 <br>
\hline AAZ12 \& 0.75 \& $\begin{array}{ll}\text { BFX13 } & 0.25\end{array}$ \& $\begin{array}{lll}\text { NKT271 } & 0.20\end{array}$ \& OC201 \& 0.80 \& 7495 \& 0.85 <br>
\hline AAZ13 \& 0.10 \& BFx29 0.28 \& $\begin{array}{lll}\text { NKT272 } & 0.20\end{array}$ \& OC202 \& 0.90 \& ${ }_{7497}$ \& 1.88 <br>
\hline ${ }_{\text {ACl }}{ }^{\text {c }}$ \& 0.35 \& $\begin{array}{ll}\text { BFX330 } & 0.28 \\ \text { BFX33 } & 0.98\end{array}$ \& $\begin{array}{ll}\text { NKT273 } & 0.20 \\ \text { NKT274 } \\ 0.20\end{array}$ \& $\mathrm{OC203}$
OC 204 \& ${ }_{0}^{0.65}$ \& ${ }_{74100}$ \& 2.18 <br>
\hline ${ }_{\text {ACl2 }}$ \& ${ }_{0.25}^{0.25}$ \& ${ }_{\text {BFX63 }}{ }^{\text {Prese }}$ \& $\begin{array}{lll}\text { NKT274 } & 0.20 \\ \text { NKT275 } & 0.85\end{array}$ \& ${ }^{\text {OC205 }}$ \& 1.00 \& 74107 \& 0.51 <br>
\hline AC128 \& 0.20 \& ${ }^{\text {BFX84 }} 00.25$ \& NKT277 0.20 \& OC206 \& 1.10 \& 74111 \& ${ }_{0}^{0.88}$ <br>
\hline ${ }_{\text {AC187 }}$ \& 0.20 \& $\begin{array}{ll}\text { BFX85 } & 0.28 \\ \text { BFX86 } & 0.25\end{array}$ \&  \& OC207
OC460 \& 1.00
0.20 \& \& ${ }_{1.00}$ <br>
\hline ${ }_{\text {ACP17 }}$ \& ${ }_{0}^{0.80}$ \& $\begin{array}{ll}\text { BFX86 } & 0.28 \\ \text { BFX87 } & 0.25\end{array}$ \& NKT301 $\begin{array}{ll}\text { NKP35 } \\ \text { NKT304 } \\ 0.75\end{array}$ \& OC460 \& 0.20
0.80 \& 74119 \& 1.92 <br>
\hline ACY18 \& 0.27 \& BFX888 0.28 \& NKT403 0 \& OCP71 \& 1.00 \& ${ }_{74122}^{74121}$ \& 0.57 <br>
\hline ACY19 \& 0.27 \& $\begin{array}{ll}\text { BFY10 } \\ \text { BFY11 } & 1.00 \\ 1.25\end{array}$ \& NKT404 ${ }^{\text {N/80 }}$ \& ORP13 \& 0.65 \& ${ }_{74123}$ \& 1.44 <br>
\hline ${ }_{\text {ACY }}{ }^{\text {ACY }}$ \& ${ }_{0.22}^{0.22}$ \& $\begin{array}{ll}\text { BFY17 } & 0.25\end{array}$ \& NKT678 ${ }_{\text {NKT }}$ \& ORP61 \& 0.48 \& ${ }^{74141}$ \& 1.00 <br>
\hline ACY22 \& 0.18 \& BFY18 0.45 \& $\begin{array}{lll}\text { NKT773 } & 0.26\end{array}$ \& 819 T \& 0.30 \& ${ }^{74145}$ \& 1.48 <br>
\hline ACY27 \& 0.25 \& $\begin{array}{ll}\text { BFYY9 } & 0.58 \\ \text { BFY24 } & 0.45\end{array}$ \& $\begin{array}{ll}\text { NKTri77 } \\ \text { O78B } & 0.38 \\ 0.38\end{array}$ \& ${ }_{\text {SFT308 }}^{\text {SAC4 }}$ \& 0.25
0.88 \& ${ }^{74151}$ \& ${ }_{1.15}$ <br>
\hline ${ }_{\text {ACY }}{ }_{\text {ACY }}$ \& ${ }_{0}^{0.65}$ \& $\begin{array}{ll}\text { BFY444 } & 1.00\end{array}$ \&  \& ${ }_{\text {ST722 }}$ \& 0.88 \& 74154 \& 2.80 <br>
\hline ACY40 \& 0.22 \& BFY50 0.20 \& OA47 0.08 \& 8T7231 \& 0.88 \& ${ }^{74155}$ \& 1.15 <br>
\hline ${ }_{\text {ACY }}$ \&  \& $\begin{array}{ll}\text { BFY51 } & 0.20 \\ \text { BFY戸2 } & 0.80\end{array}$ \& OA70 0 0.10 \& 8X681 \& 0.20
0.45 \& ${ }_{74157}$ \& 1.08 <br>
\hline ACY44 \& ${ }_{0}^{0.38} 0$ \& ${ }^{\text {BFY }}$ \& $\begin{array}{ll}\text { OA71 } \\ \text { OA73 } & 0.10 \\ 0.15\end{array}$ \& ${ }_{8 \times 635}$ \& 0.55 \& 74170 \& 2.88 <br>
\hline AD149 \& 0.50 \& ${ }^{\text {BFY64 }}$ \& OA74 0-15 \& $8 \times 640$ \& 0.75 \& 74174 \& 1.80 <br>
\hline AD161 \& 0.39 \& BFY90 ${ }^{\text {B8X27 }} 0$ \& OA79 0.10 \& SX641 \& 0.75 \& 74175 \& 1.28 <br>

\hline AD162 \& | 0.88 |
| :--- |
| 0.80 |
| .80 | \& $\begin{array}{ll}\text { B8X } \\ \text { BRX } 60 & 0.98\end{array}$ \& $\begin{array}{ll}\text { OA81 } & 0.10 \\ \text { OA85 } & 0.15 \\ 0.15\end{array}$ \& 8X642 \& O.60 \& 74176 \& 1.44 <br>

\hline AF106 \& ${ }_{0}^{0.25}$ \& ${ }^{\text {B8X }} 760$ \& $\begin{array}{ll}\text { OA83 } \\ 0 \text { A86 } & 0.15 \\ 0.15\end{array}$ \& ${ }_{8 \times 645}^{8 \times 644}$ \& 0.85 \& 74190 \& 2.30 <br>
\hline AF115 \& 0.25 \& B8Y26 0.18 \& OA90 0.07 \& V15/30P \& 0.75 \& 74191 \& 2.80 <br>
\hline AF116 \& 0.25 \& B8Y27 0.18 \& 0 O91 0.07 \& V301201P \& 0.75 \& 74192 \& 2.80 <br>
\hline AF117 \& 0.20 \& $\begin{array}{ll}\text { B8Y51 } & 0.60 \\ \text { B8Y }\end{array}$ \& ${ }^{01950} 0007$ \& V60/201 \& 0.50 \& 74193 \& 2.30 <br>
\hline ${ }_{\text {AF119 }}$ \& \& $\begin{array}{ll}\text { B8Y95A } & 0.12 \\ \text { BSY95 } & 0.12\end{array}$ \& O.A200
OA202 \& V60/201P
$\times 10101$ \& 0.75
0.10 \& 74194 \& 1.72 <br>
\hline AF119 \& 0.20
0.80 \& ${ }_{\text {BSY }}$ \& $\begin{array}{ll}\text { OA202 } & 0.10 \\ \text { OA210 } & 0.25\end{array}$ \& XA101
X 4102 \& 0.10
0.18 \& 74195 \& 1.44 <br>
\hline AF125 \& 0.80 \& 0.76 \& 0 A211 0.80 \& ${ }^{\text {X }}$ A151 \& 0.15 \& 74196 \& 1.58 <br>
\hline AF126 \& 0.80 \& BTY42
BTY7900 \& OAZ200 0.50 \& XA152 \& 0.15 \& 74197 \& 1. 68 <br>
\hline AF127 \& 0.80
0.88 \& BTY79/100R \& OAZ201 0.45 \& Xalbi \& 0.25 \& 74198 \& 3.16 <br>
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0.55 \& ${ }_{400 \mathrm{R}}^{0.75}$ \& OAZ202 0.45 \& XA162 \& 0.25 \& 74199 \& 2.88 <br>
\hline ${ }_{\text {AF178 }}^{\text {AF179 }}$ \& 0.55
0.85 \& 1.10 \& OAZ203 0.45 \& XB101 \& 0.48 \& \& <br>
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\hline ${ }_{\text {AF181 }}$ \& 0.50 \& $\begin{array}{ll}\text { BY126 } & 0.14 \\ \text { BY127 }\end{array}$ \& $\begin{array}{ll}\text { OAZ205 } & 0.46 \\ \text { OAZ206 } & 0.45\end{array}$ \& XB103
$\mathrm{XBl13}$ \& 0.85
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\hline $\mathrm{AFP186}^{\text {a }}$ \& 0.40 \& $\begin{array}{ll}\text { BY127 } & 0.15 \\ \text { BY182 } & 0.85\end{array}$ \& ${ }^{\text {OAZ206 }}$ \& ${ }_{\text {X B } 113}$ \& 0.80 \& \& <br>
\hline AFY19 \& 1.18 \& BY182 0.85 \& OAZ207 0.46 \& XB121 \& 0.48 \& pin D \& <br>
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| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{ACl}^{2 \times 8}$ | 20p | OC2\% | 49 p | 2 N 3004 | 55 p |
| AC13 | 17p | $0 \mathrm{OL28}$ | 49p | - $2 \times 30 \mathrm{~s}$ | 49 p |
| AD144 | 47p | 0 O 3 | 49p | 2N3814 | 2-1p |
| A D161/2 | $69 p$ | OCd 4 | 20 p | 0.490 | 7 p |
| BCl0 | 10p | Oct | ${ }^{20 p}$ | 0.191 | 6 p |
| 1C108 | 10p | Tist3 | 28 p | 1 Nald | ${ }^{4} \mathbf{p}$ |
| 13 Cl 09 | 10p | $2 \mathrm{~N} 70{ }^{\circ}$ | 10p | 1N+14* | 4 p |
| $\mathrm{BCl4}^{-}$ | 10p | $\cdots 1304$ | 30p | $1 \times 1001$ | 6p |
| HCl48 | 10p | $\because$ - 111 | $24 p$ | $1 \mathrm{~N}+002$ | 6 p |
| BC149 | 12p | -3 42, 14 | 25p | 154003 | 7p |
| HC168 | 13 p | $\cdots \mathrm{N} 264 \mathrm{i}$ | 45p | 1 Sax (1) | 7+p |
| BC1690 | 12p | $\cdots \mathrm{N}: 90 \mathrm{C}$ | 3.1p |  | 8 8p |
| BC182L | 12p | $2 \mathrm{~N} 290{ }^{\circ}$ | 25p | As inct | $8+p$ |
| BC:24 | 14 p | - N 292 hol | 10p | ( $\mathrm{N}+\mathrm{HW})^{-}$ | ${ }^{9 p}$ |
| BC209C | 1.19 |  | 10p | wous | 30p |
| HD131 | 45p | 2X2926t, | 10 p | WOH | 4 p |
| HD13: | 54 p | TH1世 8 -pin MIL 38p |  |  |  |
| $13 \mathrm{DL31/2}$ | f1. 20 | 74C14-pin D1L 43D |  |  |  |
| BF194 | 15p | 131L Suckets 4-pin 20p |  |  |  |
| HFY's | $16 p$ | $14-p i n 150$ |  |  |  |

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| HV： | 11＊ | $\times$ | $6^{\prime \prime}$ | $\times$ | $3^{*}$ | 11.20 |
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D．I．N． 6 Pin
1）．I．N． 7 Pin
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P＇g 9 Jack 3 －onmen Plastic
PS 10 Jack 3.5 mm Screened
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The versatility of their design make them ideal for use in recorl players, tape recorders, stereo amplifers and cassette and cartridge tape players in the car and at home.

| Parameler | Conditiona | Pertormance |
| :---: | :---: | :---: |
| harmonic digtortion | Po $=3$ WATTS $1=1 \mathrm{KHz}$ | 0.25\% |
| LOAD IMPEDANCE | - | 8-160 |
| INPUT IMPEDANCE | $\mathrm{f}=1 \mathrm{KHz}$ | 100 kn |
| FREQUENCY RESPONSE - 311 B | Po $=2$ WATTS | $30 \mathrm{~Hz}-25 \mathrm{KHz}$ |
| SENBITIVITY for Rated o/P | $V_{B}=25 \mathrm{~V}, \mathrm{~K} 1=8 \mathrm{n} \quad \mathrm{l}=1 \mathrm{KHz}$ | 75 mV . RMs |
| dimensions | - | $3^{\prime \prime} \times 21^{\prime \prime}=1^{\prime \prime}$ |

The above table relates to the AL10. AL20 and AL30
modules. The following table outlinea the differences in their working conditions.

| Parameter | AL10 | aleo | AL30 |
| :---: | :---: | :---: | :---: |
| Maximum Supply Voltage | 25 | 30 | 30 |
| Power out for $2 \%$ T.H.D. $(\mathrm{RL}=8 \Omega \mathrm{I}=(\mathrm{KHz})$ | 3 watta RMS Min. | 5 watta RMS Min. | $\begin{aligned} & 10 \text { uattr } \\ & \text { RM8 Min. } \end{aligned}$ |

## AUDIO AMPLIFIER

 MODULESAL 10. 3 watts
AL 120. 5 watta
AL 30 .
it watt
POWER SUPPLIES PR 12. (Use with AL10 \& AL20) SPM 80. (Use with also AL30 \& ALH0) FRONT PANELS PA 12 with Knobs 23.25

## PRE-AMPLIFIERS

PA 12. (Usewith AL10\& AL20) 44.95 PA 100. (Use with AL30 \& AL50) 218-15

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T461 (Use with AL10) 21.38 P \& P (5p Tj̄38 (Use with AL20) 41.89 P \& P 15p BMT80 (Use with AL30 \& AL50) 28.15


## PA12 PRE-AMPLIFIER SPECIFICATION

The PAly pre-amplifler has been designed to match into
most builget stereo sygtems. It is compatible with the AL 10. AL 20 and AL 30 andio power amplifiers and it call be supplied from their asacoisted power supplies. There are two stereo inputa, one has been designed for use with *Ceramic cartridges while the auxiliary input will muit moet †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bess and treble. ize $102 \mathrm{~mm} \times 84 \mathrm{~mm} \times 3 \mathrm{mmm}$.

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$\pm 14 \mathrm{~dB}$ at 14 kHz .
€ $14 \cdot 45$

50W pk 25w (RMS)

## $0.1 \%$ DISTORTION!

 HI-FI AUDIO AMPLIFIER
## THE AL50

$\star$ Frequency Response 15 Hz to $100,000-1 \mathrm{~dB}$.

* Load-3, 4, 8 or 16 ohms.
$\star$ Distortion-better than $\cdot 1 \%$ at 1 KHz
$\star$ Signal to noise ratio 80 dB .


## ONLY

23-58 each

* Supply voltage $10-35$ Volts.
* Overall size 63 mm $105 \mathrm{~mm} \times 13 \mathrm{~mm}$.

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AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel aimultaneously. This module embodles the latest component and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transcormer MT80, the unit will provide outputa of up to 1.5 These units volts. Size: $63 \mathrm{~mm} \times 105 \mathrm{~mm} \times 30 \mathrm{~mm}$. Guality units enable you to build Audlo 8yatems of the highea quality at a hitherto unobtainable price. Also ideal for many
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## STEREO PRE-AMPLIFIER TYPE PA100

Built to a specifcation and NOT a price, and yet atlll the greateat value on the market the PA100 atereo pre-ampliher has been conceived from the lateat circuit techniques. Designed for use with the A L50 power amplifler syatem, this quality made unit incorporates no leas than eight silicon planar transistors, two of these are apecially selected low noise NPN devices for use in the input stages.
which switched atere which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controis.

## SPECIFICATION

 Frequency Response Harmonic Distortion
Inputs: 1 Inputs:
2. Tape Head
3. Radio, Tuner
$20 \mathrm{~Hz}-20 \mathrm{KHz} \pm 1 \mathrm{~dB}$
25 mV into $50 \mathrm{~K} \Omega$
35 mV into $50 \mathrm{~K} \Omega$
All input voltages are for an output of 250 mV . Tape and P.U. inputs equalised to RIAA curve within $\pm 1 \mathrm{~dB}$. from $20 \mathrm{~Hz}_{\text {z }}$ to 20 KHz .
liass Control $\pm 16 \mathrm{~dB}$ at 20 Hz
$\pm 15 \mathrm{~dB}$ at 20 KHz
Filters: Rumble (High Pass) 100 Hz
Signal/Nolse Ratio $\quad \begin{aligned} & \text { 8KHz } \\ & \text { better than }-66 d B\end{aligned}$
Input overload-
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| AC107 | 15p | AFI39 | 32p | BF177 | 28p | OC45 | 12p | N3710 | p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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| AC127 | 15p | AFI80 | 40p | BFI79 | 32p | OC71 | 12p | 2N3819 | 32p |
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| AFI 18 | 38 p | BF115 | 25p | $\bigcirc{ }^{\circ} \mathrm{C} 42$ | 12 p | 2N3708 | 10p |  |  |
| AFI 26 | 20p | BF173 | 20p | OC44 | $12 p$ | 2N3709 | If |  |  |

$400 \mathrm{~mW} 5 \%$ 3.3V to $30 \mathrm{~V}, 12 \mathrm{p} . \quad 50 \Omega$ and decades to $100 \mathrm{k} \Omega, 35 \mathrm{p}$.

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| RECT1 |  |  |  | SIGNAL |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BY127 | 1250 V | 1 A | .12p | OA85 | 7p |
| IN4001 | 50 V | IA | 7p | OA90 | 5p |
| IN4002 | 100V | 1 A | 8 p | OA91 | 5p |
| IN4004 | 400 V | 1 A | 8 p | OA202 | 7 p |
| IN4006 | 800 V | 1A | 10p | IN4148 | 5p |
| IN4007 | 1000V | 1 A | 10p | BAll4 | 8 p |

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[^2]

It's nice to see that Santa is still so sprightly that he can dance to the rock record he is using to test that stereo player. But Rudolph is getting impatientkeen to be up and away delivering the goods, especially all those Home Radio Components Catalogues Santa is using as speaker stands Probably your name and address is on that pile of requests pinned to the door. If not, don't despairsend us the coupon below with your cheque or P.O. for 77p and we'll see that the old chap brings you a
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## FUEL AND POWER

OUr almost total dependence upon the fossil fuels, coal and oil, has been brought home to everyone these last few weeks. Nothing concentrates the mind on such basic facts of life as a threatened fuel and power shortage.

But need it be so? Remember nuclear power, and how it was to solve all our energy problems in a few decades? Well, its present contribution to the national grid is very small. This is a great disappointment after the tremendous pioneering work performed by British scientists and engineers in the post 1946 years. The high hopes of generating electricity cheaply by nuclear fission have not been fulfilled, though the failure stems mainly from political decisions, rather than from any technical shortcomings.

The relationship between nucleonics and electronics is close and real. Present day electronic circuitry owes quite a lot to development work carried out expressly to meet the special instrumentation requirements of the first nuclear power stations.
When looking for future alternative sources of power, the possibility of harnessing solar energy on a large scale seems more conjectural. However, like nuclear power, any practical scheme for using radiation from the sun must involve electronic devices and techniques, so again there is a special relationship between these technologies.

Perhaps, arising out of our winter of discontent will come a renewal of interest in these exotic sources of energy. They evoke concepts different in the extreme, from the microscopic dimension of the nucleus, to the macrocosmic distance from earth to the sun. Here are the two most probable sources of energy that will ultimately succeed the fossil fuels we are recklessly consuming without thought for the hundreds of millions of years it has taken for the oil, gas and coal to be formed beneath the earth's crust. Yet, alas. the probability is that once the present fuel crisis is over complacency will take over again and the prodigious research effort required will not be made.

Aside from such thoughts on power generation necessitating a major national programme, the present difficult position will undoubtedly encourage further development work in certain areas by individuals and companies. One example is electroluminescent materials, since lighting panels with negligible power consumption obviously have a great future. And what of the long-awaited electric car? Work in this area will receive a new impetus, for sure.

And now, more to the point so far as our readers are concerned, there are the various ways in which electronics can help immediately to alleviate some of today's power and fuel problems-at home and on the road. Practical Electronics will be publishing some useful designs to help out. As a start there is this month an Ignition Timing Light. This simple device will help towards improved engine running, with attendant saving in fuel consumption. Those readers concerned with maintaining essential services in the home should note the announcement relating to next month's issue of this magazine.
F.E.B.

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MANY amateur photographers today make use of 35 mm or Instamatic 126 cameras. Because of the small size of the negatives produced by these cameras the amateur who wants to make his own prints will need to use an enlarger in order to get prints of a reasonable size.

If a number of prints are to be produced in this way then a very useful addition to the normal darkroom equipment is some form of automatic timer unit to control the length of the exposure in the enlarger.

This device is normally used to switch on the enlarger lamp for some pre-determined period of time to give an accurately reproduceable exposure with the minimum of effort on the part of the operator.

## DIGITAL TIMING

In the timer to be described, timing is carried out by the use of digital techniques with the frequency of the supply mains acting as a basic clock. No calibration is required and the timing will remain accurate to within about one fiftieth of a second.

A switch provides a series of fixed exposure times which should cover most of the requirements for both black and white and colour printing.

## EXPOSURE REQUIREMENTS

One of the standard methods for finding the optimum exposure time for printing from a particular negative is to produce a test strip print in which a series of steps of exposure are made across the strip. Usually the exposure for one step is twice that of the previous step.

A typical series of steps might be $2,4,8,16$ and 32 seconds. The resultant print usually shows a series of strips where the density of the image increases by roughly the same amount at each step. This is due to the logarithmic sensitivity characteristic of the average photographic emulsion.

For black and white work a satisfactory print will generally be obtained by selecting one of the steps of exposure on the test strip. Colour printing tends to be rather more critical and may require the use of intermediate values of exposure between two of the adjacent steps on the test strip. Provision has been made for this requirement in the design of the digital timer.

## SELECTOR SWITCH

A selector switch on the timer enables the operator to select the basic exposure times of $2,4,8,16,32$ and 64 seconds. A second switch has been provided by means of which the basic times may be increased by 50 per cent to give the intermediate exposures of $3,6,12,24,48$ and 96 seconds.

Finer adjustment of exposure between these 12 fixed exposure times can usually be catered for by using the aperture control on the enlarger lens. If desired it is possible, by giving multiple exposures, to achieve any exposure time equal to a whole number of seconds.

The circuit diagram of the digital timer unit is given in Fig. 1. It will be seen that the unit comprises a frequency divider using integrated logic circuits, a control logic circuit, a triac switch for the enlarger lamp and a low voltage power supply for the logic elements.

## FREQUENCY DIVIDER SECTION

Frequency variations in the 50 Hz mains supply are normally held to less than plus and minus one per cent by the Electricity Generating Board. By deriving the basic clock for the timer from the supply frequency the resultant timing accuracy will be more than adequate for all normal photographic requirements.

A small voltage at mains frequency is extracted from the low voltage power supply in the unit and applied via $C 2$ and $R 1$ to the base of transistor



Fig. 1. Complete circuit diagram of the Digital Exposure Timer. S1 sets the exposure time, S 2 is closed to increase the exposure time by 1.5 times and $\mathbf{S} 3$ is the expose switch

TR1. This transistor acts as a pulse shaper and produces at its collector a 50 Hz square wave of about four volts amplitude. Diode D6 is used to provide d.c. restoration to maintain optimum bias for TR1.

The collector output from TR1 provides a clock drive signal for IC1 which is a 7490 decade counter. The 7490 consists of four flip-flops arranged to give a divide-by-five counter and a divide-by-two counter. By connecting the two sections in cascade a division by ten is obtained.

A second 7490 counter module (IC2) has its clock driven by the output of IC1 and provides a further divide-by-ten count. The resultant output signal from
the final stage of $I C 2$ is a square wave having a frequency of one cycle every two seconds.

The two second clock output from IC2 is now divided down further in frequency by IC3 and IC4.

In the 7493, which is similar to the 7490, the four flip-flops are arranged as four separate divide-by-two counter stages. Only three of the four stages in each 7493 module are used and these are connected in cascade to form a six stage binary counter chain.

The output frequency from the final stage of this counter chain will be one cycle every 128 seconds. It is this counter chain which controls the basic exposure times.

## CONTROL LOGIC

One half of a 7474 dual D-type flip-flop module (IC5) is used to provide the control logic for the unit. This particular type of flip-flop was chosen for the purpose because it is edge triggered by the positive going edge of the clock pulse input.
Between exposures this flip-flop is in a dormant state with its Q output set at the logic 1 level ( +4 volts). This Q output is joined to the reset (R0) inputs of the four counter modules (ICl to 4).
When the reset line is held at the logic 1 level the counters are held in their reset state with all outputs at logic 0 ( 0 volts). On the 7490 counters only the (R0) input is connected to the reset line, the (R9) inputs being joined to the zero volt supply rail.

## TIMING CYCLE

To start a new exposure cycle the push-button switch S3 is made momentarily. This action sets the "clear" input of flip-flop IC5 at logic 0 which, in turn, causes its Q outpuit to change to logic 0 .
After S3 is released IC5 will remain in this "clear" state. It is arranged that when Q is at logic 0 the enlarger lamp is turned on to make the exposure. At the same time the reset line to the counters will also go to logic 0 and allow them to start counting the 50 Hz input clock pulses.
Switch. Sl is used to select the basic exposure time periods. One bank of this switch (S1b) is used to select one of the six outputs of the 7493 counters (IC3 and IC4) and route it via diode D8 to the clock input of flip-flop IC5.
When this selected signal goes from logic 0 to logic 1 level it will clock the flip-flop IC5. This flip-flop is connected so that when clocked it will return to its initial condition with Q at logic 1 thus turning off the enlarger lamp and terminating the exposure.

Let us assume that the switch S1 is set so that the output from stage B of IC3 is selected via SIb. At the start of the exposure period the output from B will be at logic 0. In the 7493 type counter the output will change on the falling edge of the clock input when it goes from logic 1 to 0 .

The clock for stage B is obtained from the output of IC2. The total frequency division in IC1 and IC2 is 100 so the output frequency from IC2 will be one cycle every two seconds.

Since the counters start off from zero the output of IC2 will go to logic 1 after one second of counting and will return to logic 0 after two seconds. Stage B of IC3 will therefore be clocked to logic 1 two seconds after the start of the exposure cycle. When stage B goes to logic 1 it clocks IC5 and ends the exposure.

Thus with switch S1 in this position the exposure period will be two seconds. In the same way the exposure times produced by the other positions of SI will be $4,8,16,32$ and 64 seconds as the selected output position is moved along the counter chain.

## INTERMEDIATE EXPOSURES

To obtain intermediate exposure times the switch S2 and a second bank of switch S1 are brought into play. The switch bank Sla is also used to select one of the outputs from the counter chain but it is wired so that it selects its output from the stage before the one selected by SIb.

When switch S 2 is closed the output from S1a is routed to the clock input of IC5 via diode D7. The


## Photograph of the completed Digital Exposure Timer

two diodes D7 and D8 form an and gate so that the outputs from Sla and Slb must both be at the logic 1 level before the flip-flop IC5 will be clocked.

Once again let us assume that switch S1 is set at its two second position but in this case $\mathbf{S} 2$ is closed. At one second after the start of the exposure cycle the output of IC2 will go to logic 1 and therefore Sla output will go to logic 1. The output of Sib will still be at logic 0 so no clock pulse will be applied to IC5 and the exposure goes on.

After two seconds the $S 1$ a output will go to logic 0 and SIb will go to logic 1 so that there will still be no clock pulse applied to IC5. After three seconds output Sla will go to logic 1 again but this time S1b will still be at logic 1 so a clock pulse is applied to IC5 and the exposure ends.
Closing switch .S2 will thus increase the normal two second exposure period to three seconds. In the same way the other positions of S1 will give exposure periods of $6,12,24,48$ and 96 seconds when S2 is closed.
It was found that the flip-flop IC5 tended to be triggered by mains transients picked up on the pushbutton switch input. This problem was overcome by connecting the capacitor C3 across the "clear" input of IC5.

## LAMP CONTROL SWITCH

Instead of using a relay contact to switch the supply to the enlarger lamp, this unit makes use of a triac as a solid-state switch. The triac acts in a similar fashion to a thyristor but conducts on both half cycles of the supply.
The triac CSR 1 is connected in series with the enlarger lamp and the mains supply. When the gate to cathóde voltage of the triac is held below 0.5 volt the triac does not conduct and the entarger lamp will be off.

If the gate to cathode voltage is increased so that about 15 to 20 mA gate current flows the triac will conduct between anode and cathode on both half cycles of the supply. Since the voltage drop across a conducting triac is of the order 1 volt, virtually the whole of the mains supply will now be applied to the lamp and it will operate at normal brilliance. When the gate voltage is again reduced below 0.5 volt the triac ceases to conduct and the lamp will be turned off.

 $\rightleftarrows$ MMOLCATES BREAK IN COPFER TRACK

Fig. 2. Layout of the components on the Veroboarcl with breaks in the copper strips


Fig. 3. Interwiring of the Digital Exposure Timer switches. Refer to Fig. 2 for connections to Veroboard

## TRIAC TRIGGERING

A gate control signal for the triac is obtained from the inverted ( Q ) output of the flip-flop IC5. Before an exposure cycle the Q output will be at logic 1 and therefore the Q output will be at zero.

The gate-cathode voltage on the triac will be low and the triac is not conducting.
When an exposure cycle occurs the $\overline{\mathrm{Q}}$ output will rise to the logic 1 level thus increasing the gate voltage to make the triac conduct and turn on the lamp. The output from IC5 itself is not capable of delivering the current required to operate the triac gate directly. An emitter follower buffer stage TR2 is therefore included to drive the triac gate.

Triac CSR1 is a TOS-can type rated at 400 volts and 2 amps. This device should be capable of handling all of the normal mains voltage enlarger lamps up to about 200 watts without the need for a heat sink.

## LOW VOLTAGE LAMPS

If the enlarger is fitted with a low voltage lamp it is not advisable to use this triac to switch the supply to the lamp directly. Low voltage lamps require much higher currents and would demand the use of a larger triac. The voltage drop produced by the triac will no longer be an insignificant part of the lamp supply and will result in the lamp being under-run with a corresponding loss in light output.

It is usual for low voltage lamps to be fed from the mains supply via a transformer. It is practicable to use the triac to switch the supply to the primary of the lamp transformer. Since the transformer can present an inductive load it will be necessary to wire a $0 \cdot 1, \mathrm{FF}$ capacitor and a 100 ohm resistor in series across the triac to protect it from switching transients. The capacitor used should have a working voltage of at least 500 volts.

## POWER SUPPLY

An internal power unit provides the 5 V supply for the counters and the control logic. This employs a small transformer giving an output of 6 V at about 150 mA .

Four 1 N4001 silicon diodes (D1 to D4) are used as a bridge rectifier with a $2,000 \mu \mathrm{~F}$ capacitor Cl acting as a reservoir and providing ripple filtering. The 4.7V Zener diode D5 operates as a shunt stabiliser to produce a d.c. output voltage of approximately five volts.

A signal taken from one of the a.c. inputs to the bridge, at the junction of D1 and D3, provides the clock frequency input to the base of transistor TR1.

## CONSTRUCTION

All circuit components, with the exception of the switches, are mounted on one circuit card. This is made up using $0 \cdot 1$ in matrix Veroboard which fits in conveniently with the pin spacing on the integrated circuits. The midget transformer used is small enough to be mounted directly onto the circuit card.

A compact assembly can be produced by mounting the circuit board behind the front panel on a set of spacing pillars.

The layout of components and wiring of the circuit board is shown in Fig. 2. To make the required breaks in the copper tracks either a Vero cutter or the tip of a ${ }^{3}{ }^{3}$ in twist drill may be used. Care must

## COMPONENTS . . .

## Resistors

| Resistors |  | R4 | $47 \Omega$ |
| :--- | :--- | :--- | :--- |
| R1 | $4.7 \mathrm{k} \Omega$ | R5 | $220 \Omega$ |
| R2 | $15 \mathrm{k} \Omega$ |  |  |
| R3 | $3.3 \mathrm{k} \Omega$ |  |  |

R3 $3.3 \mathrm{k} \Omega$
All $\frac{1}{4} W \pm 10 \%$ carbon
Capacitors

$$
\begin{aligned}
& \text { apacitors } \\
& \text { C1 } 2,000 \mu \mathrm{~F} 15 \mathrm{~V} \text { elect. C3 } 0.01 \mu \mathrm{~F} \\
& \mathrm{C} 2 \underset{0.1 \mu \mathrm{~F}}{ }
\end{aligned}
$$

C2 $01 \mu \mathrm{~F}$
Transistors
TR1, TR2 2N706 or similar npn general purpose (2 off)
Diodes
D1-D4 1N4001 (4 off)
D5 4.7V 1.5W Zener
D6-D8 OA95 or similar (3 off)
Triac
CSR1 400 V 2 A triac (TO5 can)
Integrated Circuits
IC1 SN7490N decade counter
IC2 SN7490N decade counter
IC3 SN7493N 4 bit binary counter
IC4 SN7493N 4 bit binary counter
IC5 SN7474N flip-flop

## Switches

S1 2-pole 6-way break before make rotary
S2 s.p.s.t. toggle
S3 push-to-make release-to-break push-button

## Transformer

T1 Mains primary, 3V-0-3V 200mA secondary
(R.S. Components)

## Miscellaneous

SK1 13A mains socket
Veroboard 0.1 in matrix $5 \mathrm{in} \times 3^{3} \mathrm{in}$
Case, approx. 7 in $\times 5$ in $\times 3$ in
be taken in this operation so that the minimum amount of material is removed from board under the copper track.

Flexible stranded wire is preferable for the wire links across the circuit card. Solid core wire tends to cut through its p.v.c. insulation when the links are soldered to the card.

For the spacing pillars 6 BA brass hexagon bar was used. The pillars are made $1 \frac{1}{4} \mathrm{in}$ in length and they are drilled and tapped at each end to take 6BA fixing screws. An alternative would be to use wood dowels for the pillars and to fix the card and the front panel using small wood screws.

## FRONT PANEL

The front panel is made from 16 s.w.g. aluminium. Component layout is shown in the photograph and interwiring between the Veroboard and the front panel is shown in Figs. 2 and 3.

For safety it is essential that the front panel should be solidly connected to the earth pin of the socket and to the earth wire of the mains lead. The mains cable itself should be anchored to the front panel by means of a cable clip.

A case for the unit can be readily made up from ${ }_{\frac{3}{8}}^{3}$ in plywood. The four sides and bottom may be glued or screwed together to form a box which should be at least $2 \frac{1}{4} \frac{1}{2}$ deep on the inside.

For neatness the fixing holes in the front panel should be countersunk. Instrument head or countersunk screws should then be used for fixing the panel to the spacing pillars and to the case.


Photograph showing the layout of the components on the Veroboard

## OPERATION

The enlarger mains lead is simply plugged into the socket on the unit. The timer itself may then be plugged into a suitable mains supply. When the unit is switched on at first there may be a brief flash from the enlarger lamp as the logic resets itself.
Whilst focusing and setting up the enlarger it is convenient to have the timer set to the 96 seconds time period, and to retrigger it as required. Once the enlarger has been set up the desired exposure is selected on the timer using S1 and S2. With the paper set up in the enlarger the exposure is initiated by pressing switch S3.

NEWS BRIEFS

## THE NEW REVOLUTION

The Royal Albert Hall, London - Victorian monument to the Industrial Revolution with friezes depicting arts and industry decorating the outside walls was the scene of the Imperial College of Science and Technology Commemoration Day Ceremony on October 25. To the impressive setting provided by the Hall, splendid colour was added by the gowns of the college dignitaries, professors, and associates assembled for this important occasion in the academic year.

Amongst the new Honorary Fellows introduced was Robert W. Sarnoff, Chairman of RCA. In his Special Visitor's Address, Mr. Sarnoff discussed the new electronic revolution which has ". . . begun amplifying the power of the mind just as the Industrial Revolution amplified the power of muscle." He spoke of the likely impact of electronics during the next decade or so, and remarked upon the modest requirements of electronics in terms of materials and energy, and on the absence of environmental pollution or urban blight arising from expansion in this field of technology. Wider dissemination of knowledge and information for private and business use through compact communication and computing systems was one of the great contributions the whole world would enjoy as the Electronic Revolution really gets under way.

## Polinis bilisin

## PARTY STROBE LIGHT (December 1973)

In Fig. 1 and the components list diodes D1 and D2 should have been identified as 1N4004.

SEMICONDUCTOR TESTER (November 1973)
The transistors shown in the Veroboard layout (Fig. 7) are 2 N 4062 K , an equivalent for the 2 N 4062 but with differing pin connections as shown:


In addition, the emitter and collector connections of TR3 are reversed and should be transposed.

VOICE OPERATED FADER (December 1973)
The printers apologise for omitting the title and the author's name.


Correct ignition timing is essential to the efficient and economic running of a car engine. Incorrect timing may produce poor acceleration and performance. overheating. loss of power and possibly reduced engine life.

Ignition timing is essentially stroboscopic. A powered timing light is triggered by the voltage from the spark plug to which it is connected, usually the No. 1 cylinder.

Using the light enables the operator to see how the actual timing compares with the specified timing while the engine is running. Any advancement or retardation is achieved by adjustment of the distributor.

## TWO TYPES

Two types of timing light are available using either the neon or xenon tube. With a neon, this can be operated directly by the spark plug voltage to which it is connected. However, the light output compared to the xenon tube is a lot less.


Fig. 1. Circuit diagram of Ignition Timing Light
feedback condition. as the original imbalance is now being reinforced by the differential drive to the transistors.

As the current in the primary winding increases, it causes an increase in magnetic flux in the core, which. however, has an upper limit set by the material used. When this limit is reached, the flux no longer increases and the core is said to be saturated. Since it is the rate at which the flux is changing which produces the e.m.f. in a winding, and the flux has now stopped increasing, it follows that the voltages on the feedback windings must fall to zero. Under these circumstances, the transistor which had been held off by the reduced bias applied to it now has a chance to conduct once more. The collector current through this transistor and its associated primary winding acts to produce a flux in opposition to the original direction. Thus there will now be an overall reduction in the magnetic flux in the core, and this reduction brings the transformer out of saturation and at the same time gives rise to e.m.f.s across the feedback windings of opposite polarity to the original e.m.f.s.

This time, the transistor which took the core up to saturation is turned off. while the other is turned on. Again, positive feedback holds one transistor off and the other transistor on until the core saturates with the flux in the other direction. When saturation takes place, the positive feedback disappears, and the transistors change state. Thus the process is continuous, and each flux reversal induces a high voltage across the output winding.


The encased electronic assembly

## D.C. OUTPUT

The secondary winding is connected to a conventional bridge rectifier and reservoir capacitor Cl. This feeds the discharge capacitor via a charging resistor R4 which eliminates any possibility of a continuous arc in the xenon tube, R3 is connected across the reservoir capacitor to discharge it after use. The voltage across this is about 350 V .


| Resistors |  |
| :--- | :--- |
| R1 | $100 \Omega$ |
| $\frac{1}{2}$ watt $10 \%$ |  |
| R2 | $1.5 \mathrm{k} \Omega$ |
| $\frac{1}{+}$ | watt $10 \%$ |
| R3 | $150 \mathrm{k} \Omega$ |
| 1 | watt $10 \%$ |
| R4 | $15 \mathrm{k} \Omega$ |
| R5 | $1 \mathrm{M} \Omega$ |
| $\frac{1}{2}$ watt $10 \%$ |  |
| $\therefore$ |  |

Capacitors
C1 $8 \mu \mathrm{~F}$ elect, 500 V
C2 $1 \mu \mathrm{~F} 600 \mathrm{~V}$
Transistors
TR1-TR2 BUY 80 Ferranti (2 off)
Transformer
T1 FX2239 pot cores (2 off) (Mullard) complete with bobbin, clips and tagboard (see text) (Gurneys Radio, 91 The Broadway, Southall, Middlesex)

## Diodes

D1-D4 ZS274 (Ferranti) (4-off)

## Miscellaneous

Eddystone box $4 \frac{1}{10}$ in $\times 3 \frac{1}{16}$ in $\times 2 \frac{1}{1}$ in, crocodile clips ( 3 off), transistor heat sinks (2 off), 30 and 40 s.w.g. wire as required (see text) LP1ED70 xenon tube


Fig. 2. Component and wiring details


## CONSTRUCTION

The majority of components are mounted on a 14 pin tag board as in Fig. 2. The most difficult item for construction is the transformer. To make this, first wind on the bobbin 24 turns of 30 s.w.g. enamelled wire. Centre tap this winding and identify the lead-out with coloured sleeves

On top of this primary winding, wind 300 turns of 40 s.w.g. enamelled wire keeping the ends bare.

Insulate these windings with p.v.c. tape, now wind on three turns of 30 s.w.g., then take off a centre and wind another three turns ensuring that the ends are colour coded to facilitate tag connections. The cores can now be assembled around the bobbin using the clips to fix it on the tag board.

After fixing the components according to Fig. 2, the board is attached to the base of a $4 \frac{11}{16}$ in $\times$ $3 \frac{11}{16}$ in $\times 2 \frac{1}{1,6}$ in Eddystone box using nuts, bolts and insulating spaces.
The handle housing the ED70 tube and R5 must be made of some insulating material such as p.v.c. or Tufnol capable of withstanding the spark plug e.h.t. In the prototype a turned Tufnol bar of $\frac{3}{3}$ in inside diameter and $1 \frac{1}{2}$ in outside was used. The overall length was $5 \frac{1}{2}$ in. The tube can be fixed using Araldite or silicon rubber compound within the barrel.
Home Radio supply $\frac{3}{3}$ in p.v.c. tube which can be used for this. They also supply push-on end caps.

## SET UP

The timing light requires the two input leads to be connected across the car's 12 volt battery. The other lead is then connected to No. 1 cylinder h.t. lead at the sparking plug. Then engine may now be started, but the revs should be kept at tickover (i.e. 500-600 r.p.m.).

By flashing the light on the crank pulley markings and the crank case markings, the state of the timing will be seen. Adjustment of the timing is achieved by the distributor micrometer vacuum screw, which can advance or retard the ignition to the manufacturers' figures.

The probe assembly with the xenon tube and R5 removed


## WEATHER SATELLITE WILL BEAM DATA TO ALL NATIONS

A Spacecraft launched by NASA on November 8th is now the primary weather watcher in the worldwide system. Known as NOAA-3, the new satellite is in a 942 mile high sun-synchronous orbit and observes every portion of the earth twice a day
A new feature of this satellite is that data will be beamed directly to nations around the world so that any nation equipped to receive the signals will be able to make use of the information.
The satellite, built by RCA under the direction of NASA's Goddard Space Flight Centre, will monitor the temperature of the atmosphere up to 20 miles above the earth. There is also a scanning radiometer which will transmit cloud cover pictures to 550 simple, inexpensive stations located in 80 countries around the world.

NEXT MONTH
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B Y FRANK W. H Y DE

## RESEARCH ROCKETS

In October 1973 the largest UK space rocket research project involving Skylark and Petrel rockets was launched from the rocket range at Andøya in Norway. This was the first project in which the objectives were dependent on the co-ordinated firing of the Petrel and Skylark.

Financed by the Science Research Council, under the control of the Radio and Space Research Station for the University space groups, the main objectives are the study of the auroral sub-storm phenomena at various stages of development and at different altitudes.

The whole project was made possible because of the facilities made available to the United Kingdom space scientists by the Royal Norwegian Council for Scientific and Industrial Research. The range on Andørya Island off the north coast of Norway at a latitude of $69^{\circ} \mathrm{N}$ was particularly suitable for the project.

The auroral sub-storms occur at high latitudes and at these times energetic particles are precipitated. At the same time there is increased ionisation of the atmosphere caused by the particles and the ionisation causes increased absorption of radio waves.

The particles themselves are believed to originate from the low energy plasma within the solar wind. These particles are precipitated at high energies before they are precipitated into the atmosphere.

The five main experiments examined the well defined phases of typical sub-storms. The experıments were devised so that a comprehensive study of the physical processes could be made.

The five main experiments were carried on the Skylark rockets, one to each. The supporting experiments were flown on the Petrel
vehicles. The nature of the investigations is complex and is reflected in the construction of the payloads. The procedure to launch was also complex and the timing of each rocket launch required considerable accuracy. Special design of payloads was required because of limited space available and also the need to avoid interaction between experiments on the same rocket.

The main experiments were arranged to investigate :

1. Particle acceleration which occurs at the onset of the negative phase of a sub-storm.
2. Particle storage and the onset of particle precipitation during the initial phase of a sub-storm.
3. The fine structure of the particle precipitation within the auroral area.
4. The ionospheric density of the electrons and their temperature ionospheric electric fields and thermospheric winds.
5. Wave-particle interactions during a sub-storm, and the effcts on the propogation of v.l.f. emissions in the ionosphere.
Onboard instruments operated at different levels, those in the Skylark at between 200 and 300 km altitude and those in the Pefrel at about 150 km . Thus the coverage of the two levels should add very much to the understanding of these mechanisms.

An additional feature used in the experiments was the tuned laser. This is being used to track sodium "dumping" from a rocket. For the first time also pulse coded modulated (PCM) telemetry was used.

The groups directing experiments were the Radio Space Research Station, and Universities from Birmingham, Sussex, Southampton, Sheffield, University College. A group from the Royal Institute of Technology, Stockholm, also collaborated with the Radio and Space Research Station.

The Skylark rockets are made by BAC and the Petrel rockets by Bristol Aerojet Ltd.

## NEWS FROM JUPITER

The satellite of Jupiter, Io, that has an effect on the radio radiations from the planet has an atmosphere of its own. This is thought to be mostly methane and ammonia like its parent. There is, however, a peculiar thing about this atmosphere. It has been noted on a number of occasions that after being eclipsed by another body, 10 on reappearance seems to be considerably brighter in the ultraviolet region. This brightness is seen to be enhanced for about 20 minutes after eclipse.

The phenomena was puzzling and unpredictable, but now it would seem that there is yet another possible solution. It was noted that the brightening took place when Jupiter
is at perihelion, and eclipses the satellite. It has been suggested by Cruikshank and Murphy at the Hawaii University, that the heavy gas of Io's atmosphere becomes frozen when the satellite passes behind Jupiter into an extremely low temperature region. There is good evidence that the time of twenty minutes agrees with such a mechanism. It would take about twenty minutes for the solid gas to evaporate and the very bright appearance is consistent with freezing as the explanation.

As Pioneer 10 will have been occulted by Io on December 3, data will have been acquired about the atmosphere of the satellite by using radio signals from the spacecraft to measure its properties.

Hitherto, it had been thought that lo had no atmosphere since the disappearance and the emergence of a star occulted by the satellite seemed to be instantaneous. This discovery comes at a time when the large satellite Ganymede has shown that it has a significant though not very hospitable atmosphere. The final acceptance of the fact that the atmosphere is a reality has come after a long period of observation started by Dr. G. E. Taylor of the Royal Greenwich Obervatory.

Well known for his work on the prediction of occultations Dr. Taylor predicted that an occultation of Ganymede was due. The difficulty of making an exact time of the event arises from the fact that the precise position of the star invloved is often not known.

## SPECIAL OBSERVATIONS

To put this matter right special observations were made from Perth and the Cape of Good Hope in order to fix the relative position of Ganymede and the star SA0 186800. The fix was accurate to $0.3 \mathrm{arc} /$ secs. This enabled the occultation observers in India, Java and Australia to monitor the event.

Australia were not able to carry out their task successfully since it turned out that they were 50 km south of the actual track across the Earth. However, the other two observers were successful and their observations clearly showed that the atmosphere existed by reason of the slow disappearance of the star and its subsequent emergence equally slow. Though the fall in light value was only 5 per cent (not very surprising when it is realised that the star is only of magnitude 8) neverthe less the indication was positive.

The received data has now made it possible to decide a more accurate estimate of the diameter of Ganymede, which turns out to be 250 km less than was thought. Again it is a fortunate period for this discovery since Pioneer 10 will be able to obtain more data.


## CRYSTAL BALL

The National Economic Development Office report "Industrial Review to 1977 - Electronics' (Neddy Books, Millbank Tower, London, SW1P 4QX, price 50p) is so fult of ifs and buts and windy generalisations that its value is limited. Of course, the authors are handicapped from the start by lack of reliable statistics, thus it is hard enough to interpret the immediate past, let alone attempt an intelligent forecast of the future. The chosen base year is 1971 and the report attempts to analyse the growth of the industry, sector by sector, for national economic growth rates of 3.5 per cent and 5 per cent per annum through to 1977.

Quite realistic assumptions with all the economic indicators pointing in the right direction when the words were written. How unfortunate, then, that the assumptions were overtaken at the very moment of publication by new factors such as the world energy crisis, political turmoil in the United States, industrial strife at home. And, of course, the as yet unmeasured consequences of Britain's entry into the EEC.

Electronics is a dynamic industry operating internationally in a dynamic political and economic framework. What the industry really needs is an annual report based on really up-to-date figures with short-term forecasting of trends. In fact if the trade associations would only standardise on the presentation of industry statistics in their annual reports I would settle for these alone, bound up into one handy volume.

Let us turn from people trying to analyse the industry to people
out and about actually working towards that magic 15 per cent growth, characteristic of the industry in its better years.

## PRODUCTIVITY

The grafters of the industrythose who churn out the "nuts and bolts" which keep the rest going -are all too often overlooked amid the glare of publicity afforded to glamour technology and super systems.

I take, as an example, the Mullard plant at Blackburn where production is measured by the million pieces and productivity is unashamedly the goal. It is a huge plant covering 46 acres and was established in a small way in 1938. Famous for its high volume valve production it is now busy on additional products following a slow run-down in valve production as solid state devices have become more widely used. But Mullard Blackburn still produces 27 million valves a year so don't imagine the valve is already dead.

Electrolytic capacitors is one of the many other lines produced at Blackburn, brought into production in 1969 with an output for the year of 10 million. Production has now risen to an annual level in excess of 80 million, with a forecast expansion of well over 100 million per year by 1975. Much the same story applies to foil capacitor production where production is approaching 200 million a year.

A new product is glass delay lines for PAL TV receivers. By refining production processes, including automatc testing and adjustment of delay characteristics, production is approaching 2 million a year.

There has also been a big upsurge in production of electronic modules. Speed control modules for washing machines, voltage multipliers for TV sets, radio and audio modules such as tuners, pre-amps, i.f. strips, stereo decoders and a.f. power modules.

It is heartening to see such dedication to productivity which is the name of the game if prices are to be held down.

## PIONEERS

It was equally heartening to ${ }^{\circ}$ spend a week at the Japan Electronics Show at Osaka and see at first hand how British products measured up to the Japanese market. BSR record players and autochangers are selling in the areas of Japan, Taiwan and South Korea at the rate of 600,000 a
year, a remarkable achievement based entirely on BSR's enormous productivity which lands the product in Japan at a quality/price ratio which leaves the local competition gasping for breath.

More interesting, however, was the group of 17 British companies which exhibited at the Show under the auspices of the British Overseas Trade Board in a group exhibit organised by the Electronic Engineering Association.

For most companies it was their first experience in penetrating the Japanese market and there was, naturally enough, some prior doubt on the value of the investment in time and money spent. They needn't have worried. The market is by no means wide open but there are plenty of business opportunities now that trade liberalisation is becoming a reality in Japan and this, coupled with a current exchange rate which gives British products a keen priceedge, augers well for a substantial trade build-up.

The Osaka show coincided in time with the opening of the British Marketing Centre in Tokyo at which regular exhibitions of British goods are to be held and which can be used by visiting executives for business meetings with agents and customers. Decca Radar was the first electronics comoany off the mark exhibiting at the opening show of marine eauioment sponsored by the British Marine Equipment Council. But electronics will not be at the Centre in force until mid-74 when Avionics will be the theme.

Meantime, a contingent of 35 British companies will be exhibiting at the Internepcon Tokyo Show in January 1974 and a big increase in British participation is already being forecast for the 1974 Japan Electronics Show.

## AW ARD

Congratulations to Pye TMC whose "Sphericall" automatic telephone dialler won the "best international product" award at the big Canadian Electronics exhibition at Toronto. Sphericall has already won a Council of Industrial Design award and ! can vouch personally for the interest it aroused when shown in Osaka, Japan.

Basically it is a simple attachment to an ordinary dial telephone but it has push-buttons and a 10-number store in which the user can programme his ten most used numbers. To call any of these you just press two buttons and Sphericall does the rest, including "try again'. It uses an Emihusdesigned MOS-LSI chip.

Sales could be enormous once the big PTT boys, including our own Post Office, grant approval for connecting it to domestic lines. private tuition in book form!


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AURORA Multichannel Sound Controlled Light (PE Apr./Aug
 4 ch . control (4itin $\times 10$ tin) Mk. 2-also holds
 SRs, 4 SCR-IA, 50p.
A. F. SIGNAL GENERATOR BIOLOGICAL AMPLIFIER (PE Nov. 72). S/c's, Rs, Cs, Pots, (PE Jan./Feb 73). P/A Set-S/c's, Sw's. PCB $\left(2 \frac{1}{2}\right.$ in $\left.\times 4 i \mathrm{in}\right)$ also holds Sw's, 43.15.

## LOUD-HAILER AND SIREN

(Pre-amp and Siren Generator) (PW Dec. 72). S/c's, Rs, Cs, Pot, PCB (2tin $\times 2$ inn). C2.20 (While stocks last).
Main Amp Module PC5 + obtainable Main Amp Module PCS
to special order, $46 \cdot 25$.

## PHONOSONICS

PCB's AND KITS<br>AT<br>LOW PRICES


(PE Mar./Apr. H3). S/c's, i.c.'s, Rs, pe-base, Pot Cores and pc-bases, Sw's, pots Panel Lamp-Mono, $\neq 11.80 ;$ Stereo, 188.70 . PSU, 43.58. PCB-Main Circuir (3zin $\times$ 9in) (Scereo) also holds relay and cores, ©1.85. PCB-Sub-Assembly. ( $2 \frac{1}{\frac{1}{2}} \mathbf{i n} \times 6 \frac{1}{2}$ in) (Stereo) Mk. 2 holds $\mathrm{Sw}_{\mathrm{w}}$, Rs, Cs, Presees and mounts on $\mathrm{Sw}^{2} \mathrm{~s}, 80 \mathrm{p}$.



$$
\begin{gathered}
\text { VIBRASONIC GUITAR } \\
\text { PRE-AMP }
\end{gathered}
$$

(PW Sept. 70). Incl. Mic P/A, 2Guitar P/A, Trem and Tone Controls, Master Volume. S/c's, Rs, Cs, LDR, Rotary Pots, Lamp, Coupling T/fmr, C6.65. PSU, 63.32. PCB ( 3 tin $x$
10 in) Mk. 2 , also holds 7 rotary or lotin) Mk. 2, 2150
slider pots, $\mathbf{C l}, 75$.

ULTRASONIC
TRANSMITTER-RECEIVER (PE May 72). S/c's, Rs. Cs, Pot,
Relay, Duai PCB ( 2 in $\times 5$ in), $£ 3.90$. T/ducers excluded.

PCBs as published (while stocks last) PIGITAL PSU (PE Aug. 72), 50p OSCILLOSCOPE P/A (PE Aug-72), 33p SCORPI (PE Feb. 73), 80p

DIGITRONIC (PWD
out PCB (Itin $\times 3 \frac{1}{3}$ in), 60 p .
(PE Feb. 72). S/c's, Rs, Cs, Pot, PCB (I in in $x$ 3in), ©2.30, Reg, PSU and PCB ( $1 \frac{1}{2}$ in $\times 2 \frac{1}{5}$ in), $\mathbf{4} 3.10$.

VERSATILE LIGHT EFFECTS Single Channel Sound Controlled Light with buitt-in variable strobe T/fmrs, Keyswitch, \&B.85. PCB (3tin x 71 in) Mk. 2, also holds pots, Sw,
T/T7 T/imr, $\mathrm{Cl}, 50$. SCRs-IA, 50p

## PHOTOPRINT PROCESS

 (PE Jan./Feb. 72 ). For colour and B \& W -finds exposure, controls timing, stabs. mains voltage. S/c's,Rs, Cs,
Pots, Relay,
Keyswiteh,
 holds pots, Sw, relay, \&i-20.

> SOUND SYNTHESISER $($ PE 1973 $)$

Details of PCBs \& Components in lists.

## SEMICONDUCTORS



## CAPACITORS

ELECTROLYTIC

CAPA
$(\mu \mathrm{F} / \mathrm{V})$


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are rotary unless stated as slider. All components are are rotary undess stated as slider. Alicemponents are


A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.
This is YOUR page and any idea published will be awarded payment according to its merits.

## RIAA PRE-AMPLIFIER

THE pre-amplifier described here employs the MFC8040 low-noise integrated circuit. The basic internal circuitry of the device is given in Fig. 1.

Fig. 2 shows the external components necessary to produce a pre-amplifier equalised in accordance with the RIAA playback characteristic.

The circuit provides a gain of 34 dB at 1 kHz with a typical input of 15 mV . Input impedance is 75 k !. A curve, given in Fig. 3, plots the response up to 20 kHz with the 0 dB reference point set at 770 mV output ( 15 mV input). An output filter is incorporated which rapidly attenuates the output above 80 kHz .

From the total harmonic distortion point of view the circuit performs very well, the figures being $0 \cdot 1$ per cent at 60 and $1,000 \mathrm{~Hz}$ rising to 0.2 per cent at 10 kHz with an output of 300 mV r.m.s.

However, one of the main features of the design is the low-noise which is typically only 1 mV and is predominantly low-frequency.
J. Francoz,

Geneva.

## 555 GIRCUIT MARK/SPACE RATIO

| N "Points Arising" in the October issue a reader has pointed out that a constructor attempting to use the 555 timer chip to construct a 1 : 1 markspace ratio monostable may run the risk of damaging TRI because of the reduction of RA below a suggested value of $1 \mathrm{k} \Omega$. Presumably the word "astable" should have been used instead of "monostable" in this sentence.

It should be pointed out that the current passed by the discharge transistor of the 555 is typically limited to 25 mA . Thus it appears impossible to damage the 555 device in this way.

The type of astable circuit shown in Fig. 1 can be used to provide a mark-space ratio of unity or any other reasonable value. The capacitor charging current flows through RA and D1, whilst the discharging current flows through RB and D2. The charging and discharging paths are therefore quite separate and the resistors in those paths can be selected quite independently of one another. The values of RA and RB should be equal for a $1: 1$ mark/space ratio.
J. B. Dance, Warwickshire.


Fig. 1. Internal circuit diagram of IC1


Fig. 2. Circuit diagram of the RIAA pre-amplifier


Fig. 3. Response curve of the pre-amplifier


Fig. 1. The 555 Timer astable ratio circuit

## PERODD PART5 RTUEPERNIIR EMCLOSDIE BY R.A.COLE

The loudspeaker enclosures for the Rondo system have been designed specifically to overcome many of the problems that beset the constructor attempting to produce loudspeakers equal in performance and finish to a shop bought product.

Each Rondo enclosure utilises the infinite baffle principle and can be considered to be in the medium size book-shelf category. It is however generally considered that although compact, the infinite baffle loudspeaker is lacking in bass response. The Rondo system is designed to overcome this deficiency.

## BASICS

In order to explain the basic principles of the Rondo enclosure, it is necessary to briefly deal with speaker drive units and their loading. A loudspeaker drive unit used in "free air" (not mounted in any way) has a very poor bass response. In fact its response falls off below 2 kHz (see Fig. 5.1). If it is mounted on a small baffle its response improves drastically. This improvement is caused by the reduction in interaction between the waveforms emitted from the front and back of the cone.

The larger the baffle, the lower the frequency at which this interaction takes effect. The interaction is caused by the waveforms from the back and front of the cone being out of phase and cancelling each other. The lowest frequency produced by a


Fig. 5.1. The response characteristic of a driver unit in free air and unmounted
baffle-mounted speaker has a wavelength equal to twice the distance from the cone to the edge of the baffle.

To produce 40 Hz without interaction, a baffle of $14 \mathrm{ft} \times 14 \mathrm{ft}$ is needed although in practice the walls and floor in proximity reduce this dimension somewhat. In order that there should be no air coupling between the front and rear of the cone, the baffle should theoretically be of infinite size. If a smaller baffle is "folded" back on itself to produce an air tight box round the speaker unit, there is also no interaction between the front and rear of the cone.

This box is called an infinite baffle enclosure.

## THE SEALED BOX

It is obvious, however, that movements of the cone will produce compressions and rarefactions of the air within this sealed box and, due to the elasticity of air, the loudspeaker cone will not accurately follow the electrical signals fed to its voice coil.

Sound waves from the rear of the cone will also be reflected from the back of this cabinet. These waves will then pass forward through the thin speaker cone, producing the undesirable effect known as "honking".

Standing waves within the cabinet will also produce serious colouration to the sound emitted by the system.
To reduce these effects the cabinet is filled with a loose packing of fibrous material. BAF wadding, cotton wool, fibre glass and wool fibre have all been used for this purpose.

The filling, damping the effect of the elasticity of the air, reduces distortion due to non-linear movement of the voice coil. It also reduces reflections from the interior walls and damps standing waves.

## THE CONE

The cone of a loudspeaker acts as a piston which pumps air. It is designed to follow, as accurately as possible, the electrical signal fed to its voice coil. In order to keep the voice coil centred within the poles of the magnet, a spider or diaphragm is needed. Peripheral suspensions provides a restoring force for cone movements.

Both these devices reduce the ability of the cone to follow the electrical signal applied to the voice coil. This non-linearity gives rise to distortion which only careful design can reduce. In a small enclosure the cone is of small diameter and, in order to pump a useful volume of air comparable to its bigger brothers in other systems, it has to travel back and forth with greater amplitude.

This is also a cause of non-linear distortion and its effect is reduced by using special soft Neoprene or rubber roll cone suspensions and very flexible spiders or diaphragms.

The pole pieces of the magnet also have to be longer to maintain the magnetic flux acting upon the voice coil during its long incursions. To maintain this flux over the longer poles, more powerful magnets are required. Ceramic magnets, with their higher flux-to-weight ratio, are commonly used.

These speakers are called "long throw" drive units.
To summarise, a sealed enclosure or infinite baffle loudspeaker needs specially designed long throw drive units. The cabinet also has to be lagged adequately to reduce reflections, standing waves and to damp the effects of the elasticity of the air sealed in the enclosure.

A long throw loudspeaker is designed to suit a cabinet of given volume. Provided the cabinet is of that volume, its general shape is of little importance. Ideally the front/back dimension is kept around $1 \frac{1}{2}$ times the diameter of the bass drive unit.

## DESIGN

It is possible to design single speaker drive units to cover the entire audio spectrum but due to the compromises made in such units to give a response that is well maintained throughout, it is more common to use specialised speakers for various parts of the sound spectrum. The simplest form is to use a bass drive unit together with a high frequency speaker.

A network is used to divide the spectrum electrically to feed each speaker with its particular frequency range as shown in Fig. 5.2. The spectrum is sometimes split into three parts with a bass unit, a mid-range unit, a high frequency unit and a suitable network to feed them (Fig. 5.3). Even more complex methods can be used to provide specialised speakers for various parts of the audible spectrum. Crossover networks for such systems become very complex. The bass, mid-range and high frequency speakers are called woofers, squawkers and tweeters respectively.

Fig. 5.4 shows the relative acoustic power plotted against frequency in speech and music. Most of the power is in the range 10 Hz to 300 Hz with a smaller proportion in the range 300 Hz to 5 kHz and an even smaller proportion in the range above 5 kHz .

The human ear is at its most sensitive in the midrange from 300 Hz to 5 kHz and good midrange quality is thus essential together with a smooth crossover from bass to midrange.

The Rondo enclosure utilises two identical bass drive units, each capable of good response up to 5 kHz . Both are used in the range up to 300 Hz whilst only one continues up to 5 kHz .

This provides extra power in the lower range by the use of two units to overcome the bass response deficiency of the infinite baffle enclosure.

Additionally, a smooth crossover to the mid-range is achieved by using speakers of the same tonal


Fig. 5.2. Simplified illustration of the division of the frequency spectrum to the two speakers in a doubledriver system


Fig. 5.3. The spectrum division used to feed a threedriver system.


Fig. 5.4. The relative accoustic power present in average speech and music, plotted against frequency.


Fig. 5.5. The theoretical response curve of the driver units
character. The upper range is covered by two tweeters in parallel: The crossover network shown in Fig. 5.7 provides the correct range to each unit.

The bass and mid-range units are in fact HIF 13J's with an impedance of $8 \Omega$, a flux density of 44,000 Maxwells, fundamental resonance of 35 Hz , 10W sine "wave power capacity and a frequency range of from 30 Hz to 5 kHz at the 3 dB points. The tweeters are TW6Bi units with an impedance of 15S to $16 \Omega$, flux density of 13,200 Maxwells, fundamental resonance at $2 \mathrm{kHz}, 2 \mathrm{~W}$ sine wave power capacity and a frequency range from 3 kHz to 20 kHz at the 4 dB points.

Fig. 5.5 shows the theoretical overall response curves for the drivers.

## THE PRACTICAL DESIGN

The cabinets should be as solidly built as possible. Rigidity of the cabinet wall is essential to avoid coloration caused by sounds emitted by the walls. High density chipboard, plywood or hard timber is advisaule for a cabinet of the volume of the Rondo system. The thicker the material the better but 15 mm is a good minimum value from the constructional point of view.

The author does not recommend veneered chipboard offered under various trade names. Many of these makes of board are of low density and are difficult to work due to the fibrous nature of the chipboard core. If chipboard is used it is essential to ensure that the board is of high density material.

The front baffle must be cut or formed so that the speakers can be mounted from the front. This precaution is important for both the mid-range unit and the tweeters as mounting from the back reduces the upper frequency response of the drive units by an effect known as "tunnel effect." In the case of the tweeter it also reduces the polar response. The polar response of the two tweeters properly mounted is wide but if mounted wrongly it will be limited to a narrow beam.

Fig. 5.6 and Table 5.1 shows the overall dimensions and directions for making the speaker enclosure.

Provided that a strong, reasonably air-tight and rigid cabinet is made, the constructor may fabricate it from raw materials and can use an assembly method suited to his particular tool kit, materials and skills. The two methods shown here exemplify the simpler forms of a fairly wide range available.

## COVERING

The choice of material for covering the front of the speaker is rather important. Only materials specifically manufactured for use in covering loudspeaker fronts should be used. Tygan and Vynair are two commonly available. Expanded aluminium mesh is also good, although perhaps a little dated in style. It is most important to back expanded aluminium with soft foam or cloth, with the appropriate apertures for the drive units cut out. This reduces vibration of the metal.
In recent months a new material called Declon has been introduced. It has all the best features for speaker fronts. It is an open pore foam that virtually passes all sounds in the audio spectrum without attenuation. It is black, but can be lightly sprayed with an aerosol paint to suit the constructor's taste. It is washable and seems the perfect solution to speaker fronts. A number of major

## ENCLOSURE MATERIALS

13 mm or thicker high density chipboard, blockboard or hard timber.
3 mm hardboard (If front baffle not routed from one part)
Outer coating material if used (PVC, Rexine, wood veneer, etc.) ,
Internal lagging material (see text), 6 lengths 2in thick and area of front baffle
Front cover material, Delcron or like to suit, same area as front baffle. Velcro strip to fit if required.
2 Bass and Mid-range speakers, HIF 13J, 8 ohm, $10 \mathrm{~W}, 5$ fin nominal dia.
2 Tweeters, TW6Bi, 15-16 ohm, $2 \mathrm{~W}, 2 \frac{9}{16}$ in nominal dia.
Independent parts or complete kits of parts are available from various advertisers.
speaker manufacturers are now using Declon, in high quality and expensive units. In addition, it can easily be held in place using one of the modern hooked plastic retainers such as Velcro strip.

## FILLING

Undoubtedly the best material for lagging is long hair wool followed by best quality cotton wool. It has been found that bonded acetate fibres (BAF) and materials such as Dacron and Terylene in similar form, give satisfactory results. They are easier to handle and can be contained within the cabinet without restraining bags (to stop loose hairs and fibres encroaching on the drive units). Six pieces cut to the size of the front baffle, 2 inches thick, are

## Table 5.1: ASSEMBLY SEQUENCE

1. Bond front baffe and facia together firmly
2. Mount speakers securely from front using $13 \mathrm{~mm} \times$ No. 6 gauge Rd.Hd. screws applying Sealastic prior to assembly if needed
3. Mount crossover network board to terminal board on rear bafile and set aside for final assembly
4. Apply adhesive to top and bottom edges of sides and to corresponding areas of top and bottom panels
5. Offer the parts up together making certain they are square and finalise the joints using 13 mm panel pins
6. Allow adhesive to set then offer up front baffe to the assembly using adhesive and pins as before
7. Connect the crossover network outputs to their respective speakers using fairly long flying leads to allow for insertion of the filling material
Insert filing material in rolls as shown Caulk the rear enclosure opening using Sealastic type material and offer up the rear bafile. Screw into place using 38 mm , No. 6 gauge C.S. woodscrews
8. Apply speaker covering or grille and finish enclosure to taste
 closure giving major dimensions only, for clarity


KIT CONSTRUCTION


Fig. 5.9. Alternative method of assembly using carefully mitred joints and the backing material as an assembly support element.
ideal. They are rolled loosely and set in the cabinet in two layers of three.

## THE CROSSOVER

The crossover network circuit diagram is shown in Fig. 5.7 and its printed circuit and layout in Fig. 5.8. The coil winding data is shown in Table 5.2 . The bobbins can readily be wound by hand. If the coils are neat and tight then anchoring to the PC board using the slots in the bobbins as guides will hold them in place. If the windings are rather loose or sloppy then masking tape can be used to bind them firmly in position.

The PC board layout used provides space for either two non-polarised polyester, paper or similar good quality capacitors, or two reversible electrolytic capacitors, or two pairs of polarised electrolytic capacitors back to back as shown in the layout.

The crossover network is placed in the back of the cabinet, firmly secured to the walls or back. It may be supported by the terminals used to connect the crossover electrically to the signal supply lines and indeed the PCB is suited to drilling for just this purpose as shown in Fig. 5.8.

The inputs may also be wired to a DIN socket and the outputs are connected to the appropriate speaker drive units.

## DECODER TESTING

Constructors who have the necessary test equipment may wish to carry out the performance verification test detailed below.

## EQUIPMENT REQUIRED

(a) An audio oscillator capable of 1.5 V r.m.s. output at 2.2 kHz .
(b) An a.c. millivoltmeter with $1 \mathrm{M} \Omega$ input impedance minimum.
(c) A $600 \Omega, \frac{1}{2} \mathrm{~W}, 5 \%$ resistor (two $1 \cdot 2 \mathrm{k} \Omega$ in parallel may be easier to obtain).
With the decoder totally disconnected from any equipment other than the test equipment and a +20 V well-smoothed d.c. supply connect the audio oscillator to $\mathrm{L}_{\mathrm{T}}$ and the a.c. millivoltmeter to $\mathrm{L}_{\mathrm{F}}$.


If one uses the method of construction shown in Fig. 5.9, where the corner joints are mitred and in fact the assembly is facilitated using a "skin" of plastic or veneer material this will require machines capable of producing perfect mitred joints in the main chipboard core leaving only the veneered surface uncut. The veneered surface is finished and polished with a flexible polisher, or cabinets may be finished with flexible coloured vinyl surfaces or the like.

Grooves for the front and back, together with the mitre grooves, are coated wih PVA glue and the skin is then simply "wrapped" round the front and back baffles. The whole comes together precisely, giving mitre and front-back seals. The operation is descriptively called "wrapping" and the product a "wrap-round".

Such an assembly will require fairly sophisticated woodworking equipment.

As it is important to ensure an airtight assembly it is quite easy to seal any small holes or gaps with a modern bath caulking material such as Sealastic. Note: The monnting socket for suitahle pick-ul inpuls was not shown in Fig. 3.4. Thas one or wo hole's are required for a Philips stereo socket or who Phomo sockets with associated wiring internally of the trough to the pre-amplifier inputs.

## Next month: Pick-ups and Turntables for Quadraphonics

Connect $R_{T}$ to earth through the $600 \Omega$ resistor and set the audio oscillator to 2.2 kHz and adjust its output, as measured by the a.c. millivoltmeter, to 1.0 V r.m.s.

Disconnect the millivoltmeter from $\mathrm{L}_{\mathrm{F}}$ and with it measure the other outputs, $L_{B}, R_{B}, R_{F}$, which should be:
$L_{B}, \quad 630 \mathrm{mV} \pm 80 \mathrm{mV} ; \quad R_{B}, \quad 630 \mathrm{mV} \pm 80 \mathrm{mV} ; \quad R_{F}$, between $50 \mathrm{~m} V$ and 100 mV .
Repeat the above steps with oscillator connected to $R_{T}$ and $L_{T}$ connected to earth through the $600 \Omega$ resistor. Outputs should now be, with $R_{F}$ set 1.0 V r.m.s.: $\mathrm{R}_{\mathrm{B}}, 630 \mathrm{mV} \pm 80 \mathrm{mV}$; $\mathrm{L}_{\mathrm{B},} 630 \mathrm{mV} \pm$ 80 mV ; $\mathrm{L}_{\mathrm{F}}$, between 50 mV and 100 mV .
If the results noted are not attainable careful re-examination of the board layout will, most probably show wrong component insertion.

# PE Sound Synthesiser 12 

## HEY:OMRI

## By G.D.SHAW

LAST month circuits for the keyboard unit divider network, hold circuits, modulation amplifiers and mixer were included. In Fig. 12.1 assembly details are given for these. The envelope shapers are mounted on a separate board shown in Fig. 12.2 which is. in turn. mounted on a small sub-chassis below the control panel. Constructional details of the control panel and envelope shaper sub-chassis are given in Figs. 12.4/3 respectively, while Fig. 12.5 shows the component and wiring arrangement of the control panel.

## ADJUSTING THE MAIN CIRCUIT BOARD

Power supply links are fitted only to IC1 and IC2 of the divider circuit then this procedure should be followed.

Temporarily connect VRI (Tune) and VR2 (Span) potentiometers and S1. With power on the board set $S 1$ to bring VR2 into circuit and, monitoring the output of IC1, check that full rotation of VR1 gives an output voltage swing of about 8 volts. Note that the position of VR2 will affect the actual value of the maximum and minimum voltages monitored but will have no effect on the range of VR1.

Next, monitor the output of IC2 whilst swinging VR2 through its full range. Here again the output voltage swing should be of the order of 8 volts. Set

S1 to the fixed span position and adjust VR1 so that the voltage at the junction of R51-R52 is 6 volts. Transfer the voltmeter leads so that they are now measuring the potential between the junctions of R3-R4 and R51-R52 and adjust VR3 so that a reading of 4 volts is obtained. Adjustment of VR1 should have no effect on this latter reading. The final tuning of the divider network will be described later in this article.

Setting up the hold circuits should follow the pattern described in Part 11 of the series after first connecting the power supply links to the i.c.s concerned. The relative simplicity of the modulation amplifiers and mixer is such that no particular setting up is required.

Note that VR1 is specified as being a semi-precision wirewound potentiometer. For the majority of purposes this type of control will be found to be quite adequate but when the keyboard is to be matched with other musical instruments of the acoustic type it will be found that the ease of matching is greatly facilitated by the substitution of a ten-turn potentiometer for the specified type.

Prototype keyboard unit with cover removed. The circuit board to the left is that detailed in Fig. 12.1, and to the right the v.c.o. assembly




Fig. 12.2. Circuit board layout for keyboard envelope shaper and v.c.a. Only one channel is shown. The second channel is identical

## ENVELOPE SHAPER ADJUSTMENT

On completion of assembly of the envelope shaper components make temporary connections to VR1, VR2 and S1, and, with power applied, measure the voltage at pin 2 of the MFC6040. This should be +6 V under quiescent. conditions, and, with SI off and -15 V applied to the non-inverting input of IC4, will fall to about $4 \cdot 3 \mathrm{~V}$. Monitor pin 2 of the MFC 6040 on the oscilloscope, set VR2. the attack control, to maximum and close S1.

The transient application of -15 V to the noninverting input of IC4 will now result in a negative going pulse at IC4 control input. The pulse width should be about 37.5 mS and depth about 2.3 V .

With both envelope shapers operating satisfactorily the circuit board may be assembled into its subchassis and permanent wire links made with the attack and decay controls.


Fig. 12.3. Drilling details of envelope shaper sub-chassis

## CONTROL PANEL AND MAIN WIRING HARNESS

Position the control panel components as shown in Fig. 12.5 and complete the component interwiring.

Making up and connecting the main harness requires the manipulation of a considerable number of wires and it is perhaps best to try and complete the operation at one sitting. Failing this it will be necessary to make a meticulous record of connections/colour codings in order to avoid the possibility of error.

The wiring operation is simplified if the main harness is broken down into a number of subharnesses. It was found expedient to have all the wires one metre in length and then to trim them as and when final connections were made. Connect all the wiring to the control panel first of all and bind


Showing how the potentiometers are arranged on envelope shaper sub-chassis


Fig. 12.5. Component layout and wiring of keyboard control panel



Fig. 12.6. Circuit diagram of one half of keyboard p.s.u. The negative rail half is identical. T1 is a miniature mains transformer with two separate 20 V secondaries each rated at $3 V A$. Resistors are $\frac{1}{2} \mathrm{~W} 5 \%$ carbon film and the electrolytics at 50 V


The completed power supply unit. The metal surround should be grounded to obviate hum pick-up

## POWER SUPPLY UNIT

Where it is decided to operate the keyboard as a unit independent of or separate to the modular unit a small power supply unit may be installed within the keyboard housing. In this latter case the output signal from the keyboard may be taken from SK6.

The circuit of the power supply unit is shown in Fig. 12.6. Because there is nothing critical about layout board wiring details are omitted.

The power supply unit, in its casing, should be mounted to the rear of the envelope shaper subchassis so that its associated mains plug will be shielded by the casing and thus reduce the possibility of inducting hum into the keyboard circuitry.

## Next month: Keyboard housing and final tuning

them loosely into the groups shown. Try to ensure that there are no two wires of the same colour in any one group.
The wiring groups should be brought out of the control panel on the long axis and passing over S6 (1) and (2). With the control panel upside down and with the front face away from the constructor, bend the wire groups at the near edge of the control panel so that they run to the right, and place the assembly to the rear of the keyboard housing with the control panel edge against the baseboard and directly in line with its normal position. In other words the control panel should present the appearance of having been hinged back from its normal, fixed position, and laid on the table. Starting with sub-group 1 the wiring may now be trimmed and scldered individually to its respective pins.

When all groups have been dealt with carefully check each connection and when satisfied of the correctness of each, bind them tightly together into a common harness. Wiring to the envelope shapers should be grouped with the signal input and output leads separate from those carrying the sync pulse and percussive attack signal.

# marhet PLACE 

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

## TV AND UHF SIGNAL BOOSTER

Ideally suited for readers in poor signal areas, Labgear Ltd. have just introduced a new high gain u.h.f. booster covering all TV and f.m. radio transmissions on bands 11 to V .

This masthead pre-amplifier has a gain of 22 dB and a typical noise level of 3.5 dB . Suitable for most standard u.h.f. Vagi aerials of 75 ohm impedance the maximum output for 1 per cent cross modulation is claimed to be 189 mV .

Further technical details of the CM6030 signal booster (price fll) and list of nearest stockists can be obtained from Labgear Ltd., Abbey Walk, Cambridge.

F.M. and TV Signal Booster from Labgear

## PRINTED WIRING BOARD

A quick and easy method of transferring circuits to practical layouts is claimed by Ringboard for their new Ringboard printed circuit.

Made from glass fibre material, the copper backing has areas of circular copper "islands" or rings which take the components that form junction points in the circuit diagram. The two remaining large copper areas on the board can be used as the supply lines.

The method of layout is as follows: where two or more components intersect on the circuit diagram a pencil mark should be made. Where these pencil circles appear it represents a copper ring. When the circuit diagram has been completely marked the components are joined from ring to ring or supply line.

In practice it was found ideal for simple circuits and add-on boards can be used for mounting integrated circuits.
Full particulars can be obtained from Ringboard, 259 Chesterfield Road, Sheffield S8 0RT.

## MULTIMETER

Just released onto the U.K. market is a range of high quality test instruments from Chinaglia Elettrocostruzioni, one of Italy's leading test gear manufacturers.

Amongst their new products is the Cortina Minor multimeter which should interest readers. Priced at £13, including VAT, this meter has a sensitivity of $20 \mathrm{k} \Omega / \mathrm{V}$ d.c. and $4 \mathrm{k} \Omega / \mathrm{V}$ a.c. and covers 39 ranges. The d.c. voltages covered range from $0-100 \mathrm{mV}$ to $0-1500 \mathrm{~V}$ in eight switched ranges. The a.c. voltages are 0.7 .5 V to 0.1500 V in six switched ranges. The d.c. current measurement available is $0-50 \mu \mathrm{~A}$ to $0-2 \cdot 5 \mathrm{~A}$, in five switched ranges, and a.c. current range is $0-25 \mathrm{~mA}$ to 12.5 A , in four switched ranges.

The ohmmeter coverage is in two switched ranges from $0.5 \Omega$ up to $10 \mathrm{M} \Omega$. The power reading facility ranges from -10 dB up to +69 dB . A further facility of the meter is a capacitance range from 100 to $100,000 \mu \mathrm{~F}$.
Supplied with each instrument is a shock proof carrying case, two test leads and a detailed instruction booklet. Also available as an extra ( $£ 7.80$ ) is a 30 kV high voltage probe. This increases the range of the meter and makes it suitable for television work and other high voltage work.

A catalogue covering the full range of test gear and any further information can be obtained from Chinaglia (UK) Ltd., 19. Mulbery Walk, London.

## TEST GEAR

Test equipment can, at times, seem, almost by virtue of its nature, to be both expensive and repetitious. Thus any efforts by manufacturers to reduce one or both of these factors is to be a pplauded.

In this context Racal Instruments have developed a laboratory test


Racal BWD 602 Test Set
piece capable of providing one signal generator, two amplifiers and three power sources all in the one case. Identified as the BWD Model 602. this unit is claimed to be capable of replacing more expensive and sophisticated equipment in both laboratory and workshop.
The 602 includes a sine/square wave generator covering 0.5 Hz to 500 kHz ; an amplifier with variable gain from 5 to 100 , over a bandwidth from 1 Hz to 50 kHz ; an 8 watt d.c. to 20 kHz amplifier; a high voltage d.c. stabilised power supply giving +300 V at 35 mA and -50 V at 1 mA ; a low voltage d.c. supply for 1 to 12 V at 2 A or 12 to 24 V at 1 A and finally an a.c. supply giving $55 \mathrm{~V}, 15 \mathrm{~V}$ and 6.3 V all at 1 A .
Inputs and outputs of the various items are available both at the front panel and, via an octal plug, at the rear for convenience in wiring in for semi-permanent set-ups.

The various sections can be linked up to form, for example, a 0.5 Hz to 20 kHz oscillator and an 8 W square wave generator.

The Model 602 is available at £150, not unreasonable for precision instrumentation of this multiplicity. and full details can be obtained from Racal Instruments Ltd.. Duke Street. Windsor, Berks, SL4 ISB.

## QUADRAPHONIC <br> HEADPHONES

Readers may be interested to note that among the many new products from Eagle International is a new four-channel headphone.


Designated type FF. 29 the four transducers in the head sets are, it is claimed, carefully angled in such a way that the effect achieved is similar to strategically placed loudspeakers.

Compatible with practically all quadraphonic systems the 'phones have a frequency range of 20 Hz to 20 kHz . The impedance of the FF. 29 is 8 ohms per channel and the matching impedance is 8 to 16 ohms.

The price of the Eagle FF. 29 headphones is $£ 16.80$ excluding VAT and they are available from most audio shops.

# FESTIUAL ANID FAIR 

## A look at the 1973 International Audio Fair held at Olympia, London

THIS year's Audio Fair has managed to present the public with a surprising number of new developments spread over the arts of both sound production and aesthetic appeal despite a rather slow start to the week. Indeed, the initial Trade and Press opening at Olympia was delayed by a matter of hours on the opening day whilst various labour problems were sorted out, and even then very few of the stands and displays were completed before the following day. In fact, it is understood that stand painting was still being completed as late as the Thursday, quite a tribute to the exhibitors who still managed to present a cheerful face and working exhibits despite such problems.

The show was the largest so far held, with a floor area of over 17,000 square metres, some 11,000 of which were taken up with stands. Not really surprising with the market turnover topping the £100 million in 1973. In fact audio is one of the big growth areas of the electronics industry at present.

In conjunction with the exhibition there was a series of lectures and demonstrations covering a wide range of interests, including the P.E. Sound Synthesiser by Douglas Shaw. Other subjects included quadraphonics, recent developments in sound reproduction, the current (and indeed fast growing) broadcast scene and demonstrations of pop music as well as the classics.

## LARGE VARIETY

The visitor could be forgiven if he were to have limited his stay to only a few stands in the exhibition hall, not because the displays were poor but for quite the reverse reason. In fact there was all too much to see, extending from cassette equipments to a multiplicity of new tuners and power amplifiers.

All tastes were catered for both in audio quality terms and styling. For example, provided only a sufficiency of cash one could examine and possibly purchase a set of headphones and associated amplifier for $£ 104$ obtaining, for this outlay, one of the best sounding headsets ever sampled. However, $£ 104$ is rather a lot. The unit in question was the Stax SR-X Mk II Superphone.

In the same sort of price range but as a total system rather than a part, there was the Dynatron 'Gunchest' HFC 65 tuner/amplifier and separate speakers, all housed in units resembling the duelling pistol cases of an earlier age. However, to achieve this sort of elegance one has to set aside £198 and attractive as such equipment is that does seem rather a lot.

However, in the same range from Dynatron there is even more opulence in the form of the "Dorchester" complete home entertainment centre. A tuner/ amplifier and Lenco GL 78 transcription deck with a cassette stereo recorder/player unit, all housed in a Queen Anne style cabinet and with associated similarly styled speaker enclosures. All that for a mere $£ 387$.

It is always difficult to imagine a large market for such equipments but no doubt quite a few must be sold to justify treir manufacture.

## KITS IN EVIDENCE

It was very interesting to note the upswing in the general electronic constructor kit market which is clearly gaining momentum. Josty were there in strength with a very wide range of kits extending from industrial control, through instrumentation to the audio, hi-fi and broadcast reception areas and the household gadget market. To support their effort they were introducing a book on electronics
covering the areas occupied by their kits.

Similarly equipped with an equally wide range of kits and some interesting cases and associated bits of hardware for the home constructor were Amtron. Indeed there are over 200 kits in the Amtron range, extending from a simple single transistor amplifier up to a digital clock.

Perhaps not quite considered as kit suppliers are Connoisseur (A. R. Sugden) who were showing both kit and pre-built units including the ever popular BD1 assembly and the latest SAU2 pick-up arm which has a rather attractive lowering mechanism and is, interestingly enough, suited to use with the BD1 and the P.E. Rondo quadraphonic system.

Both KEF and Wharfedale were displaying their ranges of loudspeaker kits including the Glendale 3 and Kingsdale 3 equipments from Wharfedale capable of handling 40 and 60 W respectively.

## NEW MODULE RANGE

Turning to amplification equipment, Sinclair used the exhibition as an opportunity to publicise their new Project 80 modules, intended to replace the wellknown Project 60 range. The new Project 80 is a series of modules of very attractive form and style which may be used singly or together to form a complete system. They include a pre-amplifier and control unit, an active filter unit, two power amplifiers, three power supply units and the Project $80 \mathrm{f} . \mathrm{m}$. tuner and stereo decoder.

Also new from the same stable is the System 4000 amplifier and a tuner. Both are designed as rugged equipments with attractive modern styling. The amplifier is capable of giving up to 60 W per channel stereo of music power



QAS market this glass-bowl


One of the Italian A.P. Sel mim "see-thru" speakers


A Saba 8035 stereo Tuner/Amplifier system


The Stax SR.X earphome sysbem is something to hear even at $£ 104$
into 4 ohms. A constant power balance control gives improved volume control without the need for adjustment of balance.

We understand that Sinclair are setting up a new distribution organisation which will involve using major distributors supplying up to 250 official retail stockists and supporting this with an increased field sales team and service back up.

## FOUR CHANNEL EQUIPMENT

It goes almost without saying that quadraphonics was of interest to many visitors and exhibitors. There were several interesting (though often not too impressive) demonstrations and it seems clear that this is a section of the market which has yet to settle down with established techniques and equipments.

Of interest in this area was an 8-track, 4-channel cassette deck from JVC using standard 0.15 inch tape. This equipment is indicative of the direction technology is taking. sound reproduction in terms of size and capability. The specification includes crosstalk figures of 25 dB at 1 kHz which is quite something in the circumstances. To do this it uses a special circuit using phase shift and cancellation techniques.

In addition the tape hiss and noise which must arise from using such small tracks is catered for using automatic noise reduction to give a signal-to-noise of 48 dB in the 4-channel mode.

Clearly cassettes are the area of the future in many minds. One of the latest developments is a so-called transcription cassette recorder (NEAL model 102) from North East Audio which uses a 3M Wollensak deck and Dolby B to achieve wow and flutter figures of less than 0.15 per cent i.m.s. DIN weighted. Record and replay amplifiers are claimed to have less than 0.1 per cent distortion and crosstalk is said to be better than 45 dB . With bandwidth figures of 35 Hz to $12 \mathrm{kHz},+1$ to -3 dB for ferric oxide tape and extended to 15 kHz for chromium dioxide this is quite a specification to live up to.

## NEW TREND

One factor stands out quite strongly from the exhibits, the inclusion of tuners in the basic amplifier equipment. With the advent of the varicap tuner system, phase locked loops, and integrated circuit decoders, it is now more the rule to find equipments, and indeed kits, offered as including the tuner.

Japanese exhibitions figured
strongly in new four-channel tuner/ amplifiers with all systems facilities (QS, SQ and CD-4). As we have come to expect from this sector styling and control handling were, in the main, impeccable.

## PERSPECTIVE STEREO

Stereo and quad are not to be left to battle it out alone! A threespeaker system demonstrated on the Brahms Manufacturing and Development Co. stand may well appeal to many audiophiles as a sensible compromise.

Described as a new concept in sound the Orthoperspecta system has been developed by Finland's largest audio manufacturers, Salora. A full range speaker placed centrally facing the listeners is reinforced by the outputs from two smaller "directional" speakers positioned either side of the listeners. The side units operate over a restricted range 300 Hz to $3,000 \mathrm{~Hz}$ and the strong reflection at these trequencies enhances the sound pattern and creates an impression of diffused sound, reminiscent of the concert hall.

The model 3000 Orthoperspecta tuner-amplifier employs a matrix system to obtain the necessary signal phasing for diffused sound from normal stereo programme sources.


## SEMICONDUCTORS FROM A TO Z By Phillip Dahlen

 Published by Foulsham-Tab L.td. 265 pages, $5 \frac{1}{2} \times 8 \frac{1}{2}$ in. Price $£ 1 \cdot 50$THIS book is for the man who wants to have everything he needs to know about the semiconductor "family" from the simplest diode to the most complex integrated circuit.

The author begins by defining semiconductors and adds a helpful chapter determining their various characteristics-current gain, voltage drops etc.

Succeeding chapters describe in detail the characteristics and then the applications of field-effect devices such as MOS f.e.t.s; tunnel diodes; varicaps; light-sensitive devices; unijunction transistors; Zener diodes, thyristors; diacs and triacs.

Modern developments are covered very well and even include a chapter on fibre optics!

It is important to note that this book was originally written in America which could cause one or two misunderstandings to the British reader because the mains input voltages towards the end of the book
are shown in accordance with American rather than British standard supplies.

Also confusing is the fact that current flow is shown as negative to positive in circuit diagrams instead of vice-versa as is usual in this country. However, there is a special chapter at the beginning of the book directed at the British reader clearing up any points which may arise.

At $£ 1.50$ this book is good value for money and a useful addition to the constructor's library.
I.L.

RAPID SERVICING OF TRANSISTOR EQUIP. MENT (2nd Ed)

## By Gordon J. King

## Published by Newnes-Butterworths

171 pages, $8 \frac{1}{2}$ in $\times 5 \frac{1}{2}$ in. Price $£ 1.90$

FIRST published in 1966 this handbook has now been updated to take into account modern developments. A section on integrated circuits has been included and all reference to valves has been removed.

This book concentrates mainly on the servicing of domestic equipment with numerous hints on rapid fault diagnosis. Some fundamental theory of electronics is included in the earlier part of the book so that some understanding of the circuits can be attained.

Though biased towards fault-finding this book provides a simple introduction to electronics and some useful practical advice.
S.R.L.


## Audio Millivoltmeter

An audio frequency millivoltmeter, with a basic sensitivity of 1 mV , a response from 30 Hz to above 50 kHz , with an input impedance, on all ranges, of $1 \mathrm{M} \Omega$. It features a separate probe to preserve high frequency accuracy. An amplified signal output is also provided.

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## Truly pocket-sized

 With all its calculating capability, the Cambridge still measures just $4 \frac{1}{2}^{\prime \prime} \times 2^{\prime \prime} \times \frac{11}{16}{ }^{\prime \prime}$. That means you can carry the Cambridge wherever you go without inconvenience - it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of life before replacement.
## Easy to assemble

All parts are supplied - all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

## The cost ? Just $£ \mathbf{2 7} \cdot \mathbf{4 5}$ !

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs $£ 32 \cdot 95$ - so you're saving $£ 5.50$ ! Of course we'll be happy to supply you with one ready-assembled if you prefer - it's still far and away the best calculator value on the market.

Features of the Sinclair Cambridge
*Uniquely handy package. $4 \frac{1}{2}{ }^{\prime \prime} \times 2^{\prime \prime} \times \frac{11}{16}{ }^{\prime \prime}$, weight $3 \frac{1}{2} \mathrm{oz}$. *Standard keyboard. All you need for complex calculations. *Clear-last-entry feature.

* Fully-floating decimal point.
*Algebraic logic.
*Four operators $(+,-, x, \div)$, with constant on all four.
* Constant acts as last entry in a calculation.
*Constant and algebraic
logic combine to act as a limited memory, allowing complex calculations on a calculator costing less than $£ 30$.
*Calculates to 8 significant digits, with exponent range from $10^{-20}$ to $10^{79}$.
*Clear, bright 8-digit display.
*Operates for weeks on four U16-type batteries. (MN 2400 recommended.)


## A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge.
Assembly time is about 3 hours.
Contents:

1. Coil.
2. Large-scale integrated circuit.
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4. Thick-film resistor pack.
5. Case mouldings, with buttons, window and light-up display in position.
6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.


This valuable book - free !
If you just use your Sinclair Cambridge for routine arithmetic - for shopping, conversions, percentages, accounting, tallying, and so on - then you'll get more than your money's worth.

But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.


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But that in itself wouldn't be enough. Sinclair also have a very long experience of producing and marketing electronic kits. You may have used one, and you've almost certainly heard of them - the Sinclair Project 60 stereo modules.
It seemed only logical to combine the knowledge of do-it-yourself kits with the knowledge of small calculator technology.
And you benefit!
Take advantage of this money-back, no-risks offer today
The Sinclair Cambridge is fully guaranteed. Return your kit within 10 days, and we'll refund your money without question. All parts are tested and checked before despatch - and we guarantee a correctly-assembled calculator for one year.
Simply fill in the preferential order form below and slip it in the post today.
Price in kit form: $\mathbf{£ 2 4 . 9 5} \mathbf{+} \mathbf{£ 2} \mathbf{5 0}$ VAT. (Total : $\mathbf{£ 2 7 . 4 5}$ )
Price fully built : $£ \mathbf{£ 9 . 9 5}+\mathbf{£ 3} \mathbf{3} \mathbf{0 0}$ VAT. (Total : $£ \mathbf{£ 2} \mathbf{2 9 5}$ )

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Please send me
$\square$ a Sinclair Cambridge calculator kit at $£ 24.95+£ 2.50$ VAT (Total: $£ 27.45$ )

Name

$\square$ a Sinclair Cambridge calculator ready
built at $£ 29.95+£ 3.00$ VAT
(Total: £32.95)
*I enclose cheque for $£$ , made
out to Sinclair Radionics Ltd, and crossed.
*Please debit my *Barclaycard/Access account. Account number $\qquad$
Address

# POWEM SiPRIV forl.C's <br> By J.LEWIS в.sc. 

Now that the cost of integrated circuits is so low many constructors are using them in projects and general experimentation.

The main difficulty which most people encounter is supplying power to the integrated circuits (i.c.s), as most of the linear types require a dual supply rail whose values can range from $\pm 6$ to $\pm 18$ volts with various combinations of these voltages (for instance the 702 requires +12 and -6 volts).

Dry batteries are expensive and can destroy an i.c. as they have no inherent current limitation. To overcome these disadvantages it was decided to build a small unit capable of providing the necessary voltages in the dual range of 5 to 18 volts with a built-in current limiting device.

Required voltages are selected by a switch, ensuring greater accuracy than a potentiometer control. The current limit trips at a preset level (nominally 100 mA ) turning off the supply rail and lighting an indicator lamp.

## TRIP CIRCUIT

The circuit of the complete power supply is shown in Fig. 1. The circuit is duplicated for positive and negative rails and so only the positive side is drawn.


Transistors TRI to TR4 form the current trip circuit and indicator, and TR5 and IC1 form the voltage regulator.

To follow the operation of the circuit let us first consider the trip circuit. As the current through R4 increases, the voltage drop across this resistor will also increase. The potentiometer VRI is used to tap off a preset fraction of this voltage and apply it to the base of TR2, the emitter of which is connected to the more positive side of VR1.

As the voltage drop increases a point will be reached where there is about 0.6 volts across the base-emitter junction of TR2 causing it to go from a non-conducting to a conducting state, which causes TR1, TR3 and TR4 to conduct also. TR1 has the indicator lamp as its collector load. TR3 keeps the circuit latched in the tripped condition by


Fig. 1. Circuit diagram of the Power Supply for i.c.s. Note that the circuit to the right of the transformer should be duplicated if a dual power supply is required. Position 8 of S3 is only used to anchor R14, the switch should be stopped at 7 positions
supplying base current to TR2 as it switches on, maintaining this state by regenerative action.

TR4 is also switched on by TR2 and this causes the base of the main regulator transistor (TR5) to be taken to near ground potential, thus reducing the output to near zero volts.

## REGULATOR CIRCUIT ACTION

The regulation circuit is of the common series type. ICl acts as an error detector and its output is used to control the power transistor TR5.

It will be seen that the inverting ( - ) input of the i.c. is directly coupled to the output via R15, whilst the non-inverting ( + ) input is connected to a reference voltage produced by the resistor chain R8 to R14.

Any difference between these two inputs is amplified by ICl and fed to the base of TR5 which acts
as an emitter follower, maintaining the output voltage at a level near the reference voltage (minus the base-emitter voltage of TR5).
The reference voltage is derived from Zener diode D5 which also supplies current to ICl . Because this diode only has a nominal rating of 20 V its actual value may lie between 18.9 and 21.2 volts. Potentiometer VR2 was thus included to bring the voltage at the top of the resistor chain to 18 V .

The resistors in the chain should be 1 per cent types, though if you have a large selection of, say, 5 per cent types and an ohmmeter, you may find some of the required values.

Regulation is better than 1 per cent. This means that the output voltage only changes by 1 per cent as the output current is varied from zero to maximum.

Photograph showing the completed power supply viewed from the rear. The rotary switches support the resistor chain and the output terminals support the C3s


COMPONENTS

| Resistors |  |  |  |
| :--- | :--- | :--- | :--- |
| R1 | $220 \Omega$ |  |  |
| R2 | $10 \mathrm{k} \Omega$ | R 8 | $1.5 \mathrm{k} \Omega$ |
| R3 | $10 \mathrm{k} \Omega$ | R 9 | $1.5 \mathrm{k} \Omega$ |
| R4 | $22 \Omega$ | R 10 | $1 \mathrm{k} \Omega$ |
| R5 | $150 \Omega$ | R 11 | $500 \Omega$ |
| R6 | $2.2 \mathrm{k} \Omega$ | R 12 | $1.5 \mathrm{k} \Omega$ |
| R7 | $1 \mathrm{k} \Omega$ | R 13 | $500 \Omega$ |
|  |  | R 14 | $2.5 \mathrm{k} \Omega$ |$\} 1 \%$

All $10 \% \frac{1}{4} \mathrm{~W}$ unless otherwise stated

## Potentiometers

VR1 $470 \Omega$ vertical skeleton preset
VR2 $25 \mathrm{k} \Omega$ (multiturn type, if available)

## Capacitors

| C1 | $1,000 \mu$ F 50 V elect |
| :--- | :--- |
| C2 | $0.15 \mu \mathrm{~F}$ |
| C3 | $100 \mu \mathrm{~F} 20 \mathrm{~V}$ elect |

Semiconductors

| TR1, TR3, TR4 | 2N3706 (3 off) |
| :--- | :--- |
| TR2 | 2N3702 |
| TR5 | BFY50 |
| D1-D4 | 1N4001 (4 off) |


| $\begin{aligned} & \text { D5 } \\ & \text { IC1 } \end{aligned}$ | BZY88 C20V <br> 741 (8 pin dual in line type) |
| :---: | :---: |
| The | components above are for one half of the |
|  | al power supply. Twice the number of |
|  | mponents above are needed for the unit |
| Transt | former |
| T1. | Mains primary, $0-20$ 0-20V r.m.s. 6 VA secondary (R.S. miniature mains type) |
| Switch |  |
|  | Double pole mains on/off toggle |
|  | Double pole double throw toggle (2 off) |
|  | 1-pole 7 -way rotary (Use R.S. miniature |
|  | Makaswitch components with 1-pole 12-way |
|  | wafer) (2 off) |
| Miscel | llaneous |
|  | Mains indicator neon with integral resistor |
|  | 14 V 0.75 W filament l.e.s. with holder (R.S.) (2 off) |
|  | 500 mA fuse with holder |
| $4 \frac{1}{2}$ in | $\times 7 \frac{1}{4}$ in diecast box |
|  | minals (3 off) |
| Vero | board 0.1 in matrix $2^{\frac{3}{6}} \mathrm{in} \times 3 \frac{3}{4} \mathrm{in}$ |
| Capa | acitor clips to fit C 1 |
| 4BA | and 6BA nuts and bolts, grommets, knobs |



Fig. 2. Construction of the Power Supply fori.c.s. As with the circuit diagram only half of the complete circuit has been shown, the other half being identical to this. The heading photo shows a suggested front panel layout with the S2s mounted either side of $\mathbf{S} 1$ and their associated lamps above

## CONSTRUCTION

The prototype was built into a diecast box, the majority of the components being mounted on a piece of $0 \cdot 1$ in matrix Veroboard as shown in Fig. 2. Note that only one of the two circuits needed is shown, the other being identical.
The prototype used multi-turn pots for VR2 as these enable the 18 V to be set with accuracy. In Fig. 2 both VR2s are bolted together at the top edge of the board. Skeleton pots may be used for economy but more care is needed in setting up.
Components can be mounted on the front panel as suggested in the photographs of the prototype, and the Veroboard mounted on a small aluminium bracket using nylon bolts or insulating washers to make sure that the board does not come into contact with the metal box which should be earthed.

Table 1: APPROXIMATE VOLTAGES in The circuit


Capacitor C3 is mounted directly on the output terminals. Note that in Fig. 2 C 3 of the unseen half of the board has its positive terminal to common and negative to the negative terminal. The resistors of the reference voltage chain, R8 to R14, are mounted on the switches which are seven-way types using R.S. Makaswitch components.
Take particular care when setting up as there are mains voltages present within the case.

## SETTING UP

Setting up is best done with the circuit not fixed in it's case. Using a voltmeter, adjust VR2 until the voltage across the resistor chain is as near as possible to 18 V . At the same time check that the voltages at points along the chain are those required. Repeat this operation for both supplies.

Connect an ammeter in series with a 3 W wirewound potentiometer and connect these across one supply. Switch the supply on and decrease the pot from maximum until the light comes on.

Adjust VR1 until the circuit just trips at 100 mA (or as required). Some time may be needed on this stage as the setting of VR1 is quite critical. Repeat for the other supply.

Disconnect the dummy load and place the voltmeter across the outputs in turn and see that the voltages are those required. If not a slight adjustment of VR2 may be needed.

If a fault is suspected the voltages given in Table 1 may be helpful in locating it. The voltages shown are those which would be expected with the output set to 15 V , both before and after the circuit has been tripped.

The 741 has output short circuit protection and is unlikely to be the cause of trouble. Suspect other components first.

## APPLICATIONS

The resulting power unit is very compact and versatile. It can be used for powering both linear and logic, i.c.s or, indeed, normal transistor circuits, as there is no need to switch both sides of the supply.

At 80 mA the ripple on the output was measured as being 5 mV peak to peak.

One point to note is that the circuit will trip if a mains borne transient occurs. It may also trip when the voltage setting is being changed. The best procedure to adopt when switching back on is mains off, rails on then mains on.

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LAST month we looked at some applications of phase locked loop integrated circuits concentrating on devices manufactured by Signetics. In this final part devices from other manufacturers will be described with more applications, in particular the use of phase locked loops in stereo decoders.

## HARRIS SEMICONDUCTORS

The Harris Semiconductor Company manufacture a range of phase locked loop integrated circuits. They produce two high frequency phase locked loops, types HA-2800 and HA-2805. These devices are essentially similar to one another, but the more expensive HA- 2800 can be used over a much wider temperature range and has closer tolerances on some of its parameters.

Both devices are supplied in a 16 pin dual-in-line encapsulation with the connections shown in Fig. 4.1 .

The maximum operating frequency of a typical device is 30 MHz , but all HA- 2800 devices are guaranteed to operate up to at least 25 MHz and all HA-2805 devices up to at least 20 MHz . These upper frequency limits are set by internal and external stray capacitance.

The manufacturers quote the low frequency limit as about 1 kHz , since extremely stable, low leakage capacitors cannot normally be obtained with a value exceeding about $10 \mu \mathrm{~F}$. The variation of the centre frequency with the timing capacitor value is shown in Fig. 4.2.

A special feature of these loops is the high impedance phase detector output which acts as a current source. This is connected externally to the current controlled oscillator (in contrast to the voltage controlled oscillator employed by most other manufacturers).

## POWER SUPPLIES

The HA-2800 and HA-2805 are operated from a dual power supply of between $\pm 5 \mathrm{~V}$ and the absolute maximum rating of $\pm 15 \mathrm{~V}$. The devices should not be operated with either power supply absent and each supply should be decoupled close to the device with a capacitor of not less than $0 \cdot 1 \mu \mathrm{~F}$. The current taken from each of the power supplies is typically 8 mA . The absolute maximum permissible power dissipation is 500 mW .

## INPUT

The input impedance to the phase detector is about $2 \mathrm{k} \Omega$. The maximum input voltage is 2 V r.m.s.

These phase locked loops are claimed to have a particularly low frequency drift with changes of supply voltage and with temperature.

## LOW FREQUENCY PLLs

Harris Semiconductor produce two low frequency phase locked loops, the HA-2825 and an equivalent type, the HA-2820, which can be used over a much wider temperature range.

These devices are produced in a 14 pin dual-in-line encapsulation for the frequency range of 0.01 Hz to greater than 3 MHz (up to 5 MHz for a typical device). The normal power supplies are in the range $\pm 6 \mathrm{~V}$ to $\pm 12 \mathrm{~V}$, the absolute maximum permissible total voltage across the device being 27 V .


Fig. 4.1. Internal block diagram of Harris Semiconductors phase locked loops type HA-2800 and HA-2805


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$\begin{array}{rrlll}350 & 15 & 0 & 14.0 \times 10.8 \times 11.8 & 9.40 \\ 500 & 19 & 8 & 140 \times 13.4 \times 11.8 & 13.55 \\ 750 & 29 & 0 & 17.2 \times 14.0 \times 14.0 & 19.26 \\ 1000 & 38 & 0 & 17.2 \times 16.6 \times 14.0 & 24.97\end{array}$
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3.55
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5.28
6.82
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4.41
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0.10 \& $P$ $p$
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22 | 27 |
| :---: |
| 70 | 12 $\begin{array}{llll}100 & 4 & 6.1 \times 5.8 \times 4.8 & 0.6,0.6 \\ 330,330 & 4.9 \times 2.6 \times 2.9 & 9.0 .9 \\ & 4.8 \times 2.9 \times 3.5 & 0.9 .0 .9\end{array}$

$500500 \quad 1006.1 \times 5.4 \times 4.8 \quad 0.8 .90 .8 .9$
$1 A, 1 A \quad 112 \quad 7.0 \times 6.4 \times 6.1 \quad 0.8 .9,0.8 .9$ $\begin{array}{llll}200,200 & 4 & 4.8 \times 2.9 \times 3.5 & 0.15,0.15 \\ 300,300 & 4.1 \times 5.8 \times 4.8 & 0.20 & 0.20\end{array}$ 300,300

700 (d.c.) $\begin{array}{llllll}700 \text { (d.c.) } & 1 & 8 & 7.0 \times 6.1 \times 6.1 & 20-12-0.12-20 \\ 1 A, 1 A & 2 & 12 & 8.3 \times 7.7 \times 7.0 & 0-15-20,0-15-10 \\ 500,500 & 2 & 4 & 8.3 \times 7.0 \times 70 & 0-15-27,0-15-2\end{array}$ | 204 | 1 | $8,1 \mathrm{~A}$ | 3 | 4 | $8.3 \times 7.0 \times 7.0$ | $0.15-27,0-15-27$ | 2.36 |
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Fig. 4.2. Variation of centre frequency with timing capacitor in the Harris phase locked loop i.c.s

A $1 \mu \mathrm{~F}$ capacitor will produce a frequency of about 300 Hz when using a 540 ohm timing resistor. The frequency can be altered over a $10: 1$ range by changing the value of the timing resistor.

The phase detector employed in these devices has a high output impedance for connecting to the oscillator control input through a suitable low-pass filter. The two phase detector outputs are isolated from one another, so different filters can be employed in each output circuit without any interaction.

These devices can be employed in f.m. modulators and demodulators, frequency shift keying (f.s.k.) applications, frequency multiplication, industrial speed control, etc.

## AVAILABILITY

The HA-2800 is available at $£ 23 \cdot 83$, the HA- 2805 at $£ 10 \cdot 34$, and the HA- 2825 at $£ 6 \cdot 66$ from G.D.S. (Marketing) Ltd., Bath Road, Salt Hill, Slough, Buckinghamshire, together with some application reports.


Fig. 4.3. Internal block diagram of the Exar XR-215 phase locked loop integrated circuit

## THE XR-215

A nother type of high frequency phase locked loop, the XR-215, is manufactured by EXAR Integrated Systems Incorporated. The maximum typical operating frequency is 35 MHz (minimum value 20 MHz for any device of this type). The minimum practical operating frequency is quoted as 0.5 Hz , when the timing capacitor is about $500 \mu \mathrm{~F}$.

The XR-215 device is supplied as a 16 pin dual-in-line integrated circuit, as in Fig. 4.3.

The XR-215 can be made into a complete loop by capacitively coupling the output of the voltage controlled oscillator to either of the phase comparator inputs and adding a low-pass filter across the phase comparator output terminals.

A special feature of the $X R-215$ is the internal operational amplifier it contains. This can be used as an audio pre-amplifier when the device is used as an f.m. demodulator or as a high speed comparator in frequency shift keying demodulators.

The voltage controlled oscillator has frequency sweep, on/off keying, synchronisation and digital programming facilities. Its frequency is very stable and is determined by a single external capacitor.

## POWER SUPPLY

The XR-215 has an absolute maximum power supply voltage rating of 26 V , but it can operate from a supply as low as 5 V . The current consumption is 8 to 15 mA at 12 V .

The absolute maximum power dissipation is 750 mW at $25^{\circ} \mathrm{C}$.

## FREQUENCY

The variation of the free-running frequency of the voltage controlled oscillator with the value of the capacitor connected between pins 13 and 14 is shown in Fig. 4.4 for two circuit conditions. The frequency is given by the approximate equation:

$$
f=\frac{200}{C}\left(1+\frac{0 \cdot 6}{R_{\mathrm{x}}}\right)
$$

where $C$ is the value of the capacitor connected between pins 13 and 14 in microfarads and $R_{\mathrm{X}}$ is the value of the resistor connected between pins 9 and 10 .
The tracking range is adjustable from $\pm 1$ per cent to $\pm 15$ per cent of the centre frequency.


Fig. 4.4. Variation of centre frequency with timing capacitor in the XR-215

## PHASE COMPARATOR INPUTS

The input signal is fed to one input of the phase comparator and the other input should be connected to the output of the voltage controlled oscillator to close the loop. Both phase comparator inputs should be returned to a potential mid-way between the supply line voltages.

## FREQUENCY SWEEP

The voltage controlled oscillator frequency can be swept over a wide range by applying a varying voltage to pin 12 of the device. The impedance looking into this pin is 50 ohm and a current limiting resistor should therefore be connected in series with this terminal when the facility is used. The maximum current which can safely be drawn from pin 12 is 5 mA .

If pin 10 is open circuited, the voltage controlled oscillator can be switched off by applying a positive pulse to pin 12 .

## FREQUENCY SYNTHESIS

The circuit of Fig. 4.5 shows how the XR-215 can be employed in a frequency synthesiser. A SN7493 (or an equivalent type) 4-bit binary counter is used to divide the output from the voltage controlled oscillator by a certain chosen factor; the output from this frequency divider is fed to the phase comparator. The loop locks when the input frequency is less than the oscillator frequently by this factor.

The low-pass filter capacitors, C3 and C5, are normally chosen to provide a cut-off frequency equal to 0.1 to 2 per cent of the signal frequency. The digital or analogue tuning characteristics of the voltage controlled oscillator can be used to extend the available range of frequencies of the system for any one value of the capacitor C 4 .

## AVAILABILITY

The XR-215 is manufactured in the U.S.A., but is available (together with a detailed data sheet) from Rastra Electronics Ltd., 275-281 King Street, Hammersmith, London, W6 9NF at about $£ 15 \cdot 20$ each in small quantities.

## THE XR-210

The XR-210 is another type of phase locked loop available from the same source at $£ 5 \cdot 25$ in small quantities. It has been designed especially for use as a frequency shift keying modulator/demodulator in the frequency range 0.5 Hz to 20 MHz , but can also be used for f.m. demodulation, frequency synthesis, etc. It is produced as a 16 pin dual-in-line device and has many features similar to the XR-215.

## cos/mOS LOOP

A special feature of the RCA phase locked loop type CD4046A is its very low power consumption. The operating voltage range is 5 to 15 V , but the current required is only about $100 \mu \mathrm{~A}$ from a 6 V supply when the operating frequency is 10 kHz . This is of the order of one hundred times less than the current required by most other monolithic loops. At 100 kHz the power supply current is $350 \mu \mathrm{~A}$ from a 6 V . supply and $630 \mu \mathrm{~A}$ from a 10 V supply. This device is ideal for use with battery powered equipment.

The low power consumption is achieved by the use of COS/MOS (complementary symmetry metal


Fig. 4.5. Diagram of the $X R-215$ used with a TTL divider to form a frequency synthesiser


Fig. 4.6. Internal block diagram of the R.C.A. CD4046A phase locked loop with the necessary external components to complete circuit
oxide semiconductor) circuits. This type of circuitry has many other applications where low power and small size are necessary-such as in quartz controlled wrist-watches.
The CD4046A contains a linear voltage controlled oscillator, two different types of phase comparator, a source follower and a 5.4 V Zener diode for power supply regulation.

The CD4046AE is encapsulated in a 16 pin dual-in-line plastic package and is priced at about $£ 3 \cdot 46$. Electrically equivalent devices are available in a dual-in-line ceramic package (CD4046AD) and as a flat pack (CD4046AK).

## BASIC CIRCUIT

The basic circuit of the CD4046A is shown in Fig. 4.6. An external timing capacitor, Cl , and one or two external resistors (R1 or R1 and R2) are connected in the oscillator circuit. R1 and C1 determine the oscillator frequency range, whilst R 2 enables the frequency to be offset if this is required. The typical maximum frequency is 500 kHz .

The input impedance of the voltage controlled oscillator is extremely high (one million megohms) and this simplifies the low-pass filter design. The output of the oscillator (pin 4) may be connected directly to the phase comparator input (pin 3) or through a COS/MOS frequency divider such as the RCA type CD4018AE presettable divide-by-"N" circuit. A very low power frequency synthesiser can thus be made.

## THE PHASE COMPARATORS

Most phase comparators used in phase locked loops employ analogue amplifiers, but it is not easy to make such amplifiers with well-controlled gain characteristics when using COS/MOS technology. Digital phase comparators are therefore employed in the CD4046A.

Phase comparator I is an exclusive-or network. When no noise or signal is present at the input, the mean output voltage from this comparator is the average of the supply line potentials. Thus under no signal conditions the oscillator operates at its centre frequency.

When phase comparator II is used under no signal conditions, however, the output of this comparator feeds a control signal to the low-pass filter which causes the oscillator to operate at the minimum frequency of the band.

## STEREO DECODERS

Many of the modern types of stereo decoder circuits employ a phase locked loop. In order to understand the operation of such circuits, we must first consider the nature of the stereo multiplex signal which must be decoded.

The demodulated f.m. stereo signal comprises the following parts, as depicted in Fig. 4.7:
(a) An audio signal containing the sum of the leftand right-hand audio channel signals; the maximum frequency contained in these signals is 15 kHz . If monaural reception is required, this signal is used as the audio output.
(b) A "left minus right" signal which is modulated onto a 38 kHz sub-carrier.
The sub-carrier itself is suppressed to an amplitude of less than one per cent.
(c) A low level 19 kHz "pilot tone" which is synchronised with the 38 kHz suppressed sub-carrier.
This pilot tone is used to indicate that a stereo signal is being transmitted, but it is also employed as a reference signal by means of which the 38 kHz sub-carrier can be generated in the receiver. This sub-carrier signal is required for use in the stereo signal decoder.


Fig. 4.7. Frequency spectrum of an f.m. stereo signal
The pilot tone is not present when a monaural signal is being transmitted.

Various forms of stereo decoding circuits have been designed which provide "left" and "right" audio signals from the demodulated f.m. signal. In the "switching" type of decoder, the 19 kHz pilot tone is extracted by means of a tuned circuit, doubled in frequency to 38 kHz and the resulting signal is used to switch the multiplexed input signal.

Such systems suffer from the disadvantage that optimum channel separation cannot be achieved and the inductors required are inconvenient circuit components.

The use of a phase locked loop decoder eliminates problems in setting up the circuit. Any reasonable changes of the component values with time or temperature will not matter, since the loop frequency will be locked to the input frequency.

## MONOLITHIC DECODERS

During the past two years, a number of manufacturers have introduced monolithic phase locked loops which have been especially designed for stereo decoding. They offer excellent channel separation (typically better than 40 dB ) and many of them require no inductors in the external circuit.

## THE CA3090

The RCA phase locked loop stereo decoder type CA3090 was introduced in 1971. It is available as the 16 pin CA3090Q quad-in-line device and also as the 16 pin dual-in-line device type CA3090E at about $£ 4 \cdot 20$. Devices of this type can be used in a simple decoding circuit consuming about 22 mA , but one adjustable 2 mH inductor must be employed.

The internal circuit of the CA 3090 (which contains 128 transistors) is shown in block form in Fig. 4.8 together with the external components required to form a complete stereo decoder circuit.

The demodulated multiplexed signal is applied to pin I of the CA3090 where the input impedance is about 50 kilohm. The signal is amplified before being fed to both the 19 kHz and the 38 kHz synchronous detectors.

The phase locked loop itself consists of a voltage controlled oscillator, two "divide-by-two" stages and a 19 kHz phase-lock detector (or phase comparator). The free-running frequency of the voltage controlled oscillator is set to 76 kHz by the circuit connected to pins 15 and 16.

## CIRCUIT OPERATION

The 76 kHz signal is divided in frequency to produce a 38 kHz signal and two 19 kHz signals in phase quadrature with one another. The 19 kHz signal present at the input is compared with one of
the internally generated 19 kHz signals by the phaselock detector and the phase difference signal is used to lock the oscillator to the pilot tone frequency in the normal way. The loop is thus employed to generate the 38 kHz suppressed sub-carrier.

A 19 kHz synchronous detector senses the presence of the pilot tone; it switches the Schmitt trigger when the level of this tone exceeds a certain amplitude determined by the resistor connected between pins 7 and 8. The Schmitt trigger circuit causes the lamp in the pin 12 circuit to be illuminated showing that a stereo signal is being received. In addition, the Schmitt trigger activates the 38 kHz synchronous "L-R" detector and switches the whole circuit to stereo operation.

A light emitting diode is used as the stereo indicator in the pin 12 circuit of Fig. 4.8. The maximum current which can be passed by the pin 12 circuit is about 14 mA , but a transistor amplifier can be used if it is desired to drive a lamp requiring more current. The circuit switches to stereo operation when the pilot tone level at the input is at least 4 mV with the values shown, but greater sensitivity can be obtained if necessary. However, at low signal levels monaural operation is to be preferred, since a better signal to noise ratio can be obtained.

## OUTPUTS

The output signal from the 38 kHz detector and the multiplex input signal are applied to a matrix circuit which provides the required left and right channel outputs. The internal amplifier in each channel provides enough gain for the output to be able to drive most types of amplifier directly. The channel separation is typically 40 dB and the total harmonic distortion 0.45 per cent.

The core of the 2 mH inductance is set half way between the points at which the indicator lamp becomes illuminated as the core adjustment is varied. The centre frequency of the voltage controlled oscillator is then very close to 76 kHz . The capture range of the loop is typically $\pm 10$ per cent of the centre frequency.

## MC1310P/SN76115N/LM1310

The Motorola MC1310P is a phase locked loop stereo decoder first introduced in 1972. It is available as a 14 pin dual-in-line plastic device at approximately $£ 3$. Equivalent devices are the Texas Instruments' SN76115N and the National Semiconductor type LM1310.
These devices have the advantage that no inductors are required in the external circuit with which

Fig. 4.8. Internal circuit of the RCA CA3090 stereo decoder with the necessary external


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they are used. This removes the possibility of unwanted couplng and the inconvenience of coil design. The only components required other than the integrated circuit itself are eight capacitors, four resistors, a variable resistor and an indicator lamp.

The functioning of these devices is essentially similar to that of the CA3090 and therefore it will not be described in detail. The voltage controlled oscillator operates at 76 kHz . Its frequency is determined by the values of a capacitor and a variable resistor in the pin 14 circuit (see Fig. 4.9). The oscillator signal is frequency divided to produce two 19 kHz signals in phase quadrature to each other and the 38 kHz signal required for the decoding.

## CIRCUIT ADJUSTMENTS

When the circuit is first used, the potentiometer VR1 of Fig. 4.9 must be adjusted so that the oscillator free running frequency is close to 76 kHz . (This operation is comparable with the adjustment of the core of the inductance of Fig. 4.8.)

The frequency adjustment may be carried out by connecting pin 10 to a frequency counter and altering the value of VR1 until the frequency at this pin ( 3 V peak) is 19 kHz . If a frequency counter is not available, VR1 should be adjusted to the point at which the indicator lamp remains illuminated at the lowest possible signal a mplitude.


Fig. 4.9. Diagram showing the MC1310P (or an equivalent) used as a stereo decoder


Fig. 4.10. Block diagram showing how the phase locked loop can be used in motor speed control

The capture range is typically $\pm 3$ per cent. It may be increased by reducing C2 and increasing R1 and VR1 in proportion, but this will result in increased beat note distortion at high signal levels due to oscillator phase jitter. Ideally the temperature coefficient of the time constant of Cl, R1 and VR1 should be minus 200 parts per million.

The capacitor C4 controls the stereo/monaural switching delay. The switching time constant is equal to C 4 multiplied by about 53 kilohm. If pin 8 is earthed; the circuit will operate in the monaural mode only.

## INDICATOR LAMP

The MC1310P circuit can drive an indicator lamp in the pin 6 circuit which requires up to 75 mA . (A surge limiting circuit is incorporated in the device which restricts the lamp current to about 250 mA when the lamp is cold.) The circuit switches to stereo operation when the amplitude of the pilot tone exceeds 16 mV at the input.

If a simpler circuit is required at the expense of performance, C 7 may be omitted if R4 is reduced to 100 ohm and C 8 to $0.25 \mu \mathrm{~F}$.

The audio outputs are 485 mV r.m.s. when the input is 560 mV . The total harmonic distortion is typically 0.3 per cent and the channel separation 40 dB at 1 kHz . The input impedance of the device is 50 kilohm.

The minimum value of the load resistors R2 and R3 is determined by the power supply voltage. It is $2.7 \mathrm{k} \Omega, 4.5 \mathrm{k} \Omega$ and $6.2 \mathrm{k} \Omega$ for supplies of 8,10 and 12 V respectively. C5 and C6 are the de-emphasis capacitors; their values should be chosen so that they give the desired time constant with R2 and R3 $(50 \mu \mathrm{~s}$ in the U.K.). If R2 $2=\mathrm{R} 3=2.7 \mathrm{k} \Omega, \mathrm{C} 5=$ $\mathrm{C} 6=18 \mathrm{nF}$, whilst if $\mathrm{R} 2=\mathrm{R} 3=6 \cdot 2 \mathrm{k} \Omega, \mathrm{C} 5=\mathrm{C} 6$ $=8 \mathrm{nF}$.

## MOTOR SPEED CONTROL

A basic circuit suitable for motor speed control is shown in block form in Fig. 4.10. The speed of rotation of the motor is "sensed" by a digital tachometer; the latter produces an output pulse frequency related to the motor speed. The phase detector compares a signal derived from the tachometer output with a very stable reference frequency (such as that from a crystal oscillator). The motor speed can thus be made as stable as the frequency of the reference source.

## CONCLUSIONS

Readers who have followed the whole of this series will begin to appreciate the vast number of applications for which phase locked loops can be employed. Indeed, the number of applications is limited only by the ingenuity of the user. Thus the relatively new devices which are coming onto the market offer a real challenge to the amateur experimenter as well as to the professional engineer.

It is difficult to forecast future progress in a field such as electronics, but the writer feels that phase locked loops will form part of many types of radio receivers in the future, including high fidelity systems, car radio receivers and communications receivers. From the point of view of the amateur enthusiast, applications in radio receivers are probably the most significant ones, but the professional circuit designer will find many other fields for phase locked loops also.

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$50,260,500,1,000 \mathrm{~V}$. D.c. current: 10 $1 \mathrm{~K}, 10 \mathrm{~K}, 100 \mathrm{~K}, 10 \mathrm{mes} 100 \mathrm{mes}$. Decibel -10 to +49 dB . Plantic case with carrylag handle. ilxe 7 in $\times 6 \operatorname{in} \times 3 i \mathrm{in}$. alo.es P. \& P. 25p.
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 Sensitivity 330 obmal
Volt e.c. and d.c. Accur scale length 165 mm . $0 / 300 / 750 \mu(14 / 1.5 / 3 / 7 \cdot 5)$ 5/30/75/150/300/
 $300 / 750 \mathrm{~mA} / 12.5 / 3 / 7$. amp. a.c. $0 / 70 / 150 / 300$ $750 \mathrm{mv} / 1 \cdot 6 / 3 / 7 \cdot 6 \cdot 15 \cdot 30 /$ $75 / 150 / 800 / 750 \mathrm{~V}$ d.c. 0 $750 \mathrm{mV} / 1 \cdot 6 / 3 / 7 \cdot 5 / 16 / 30$
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PS.800 REGULATTD P.I.J.
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protection $0 / 0-6 / 3 / 15 / 60 / 3001$ | protection $\begin{array}{l}0 / 0-6 / 3 / 15 / 60 / 300 / \\ 1,200 \mathrm{~V} \\ \text { d.c. } 0 / 6 / 30 / 120 / 600 /\end{array}$ |
| :--- | 1.200 V $0 / 30 / \mu \mathrm{A} / 6 \mathrm{ma}$ $\begin{array}{ll}1,200 \mathrm{~N} / 300 \mathrm{~mA} / 600 \mathrm{~mA} . & 0 / 8 \mathrm{~K} / \\ 60 \mathrm{~mA} / 2\end{array}$ $80 \mathrm{Z} / 800 \mathrm{X} / 8$, meg, ohm -20 to

MODEL TE-800. 20,000 O.P.V $\begin{array}{ll}\text { Mirror icale, overloed } \\ \text { tion. } & 0 / 5 / 25 / 125 / 1,000\end{array}$ tion. $0 / 5 / 25 / 125 / 1,000 \mathrm{~V}$ d.c. $0 / 10 / 50 / 250 / 1,000 \mathrm{~V}$ R.c. $0 / 50 \mu \mathrm{AA}$
250 mA . $0 / 60 \mathrm{~K} / 6 \mathrm{meg} \Omega .-20$ to $\begin{array}{ll}250 \mathrm{~mA} . & 0 / 60 \mathrm{~K} / 6 \mathrm{meg} \Omega, \\ +62 \mathrm{~dB} . & 6 \cdot 95 . \text { Poet } 15 \mathrm{p}\end{array}$

CI-6 PULSE O8OLLLOFor diapley of pulsed and periodic waveforms in electronic circulta VERT. AMP. Bandwidth 10 MHz . $\begin{array}{ll}\text { Senaltivity at } & 100 \mathrm{kHz} \\ \mathrm{V} \text { RMg/mm. } & 0.1-25 \text {; }\end{array}$ HOR. AMP. Bandwidth $\begin{array}{ll}500 \mathrm{kHz} . & \text { senaltivity at } \\ 100 \mathrm{kHz}, & \text { VMS/mm. }\end{array}$
 1002 0.3 ; Pre-set triggered sweep $1-3,000 \mu \mathrm{sec}$. $0.3-25$; Pre-set triggered sweep
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|  | $1 p$ | 1 p | ${ }^{2} \mathrm{p}$ |  | Ep | ${ }^{2}$ | ${ }^{\text {P }}$ | 4 | 2 p | ${ }^{5} \mathrm{p}$ | ip | ${ }^{\text {f }}$ p | sp |
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| 7438 | 0.77 | 0.74 | 0.71 | 7489 | 4.95 | 4.29 | 4.07 | 741612.18 | 2.05 | 1.94 |  |

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| 301 | DIL | $0.50 \mid 307$ | T099 | ${ }^{0.68}$ | 710 C | T099 0.46 | 748 C | DIL |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 301 | ${ }^{\text {T099 }}$ | 0.55307 | 8 Pin DIL | IL 0.88 | ${ }^{723 C}$ | DIL 0.99 | 748 C | TO99 | 0.42 |
| 301 | 8 Pin DIL | 0.48 308 | T099 | $86 \cdot 90$ | 723 C | T099 21.00 | 1437 | DIL | 21.30 |
| 301 A | DIL | 0.69 308A | T099 | 87.40 | ${ }^{741 \mathrm{C}}$ | 8 Pin DIL 0.35 | 1458 | T099 | 21.80 |
| 3014 | T099 | 0.897090 | DIL | 0.85 | 741 C | 14 Pin DIL0-36 |  |  |  |
| 3014 | 8 Pin DIL | $0.68 \quad 709 \mathrm{C}$ | T099 | 0.34 | ${ }^{741 \mathrm{C}}$ | T099 0.38 |  |  |  |
| 307 | DIL | $0.89{ }^{\text {c }}$ | DIL | 0.44 | 747 C | DIL 0.80 |  |  |  |
| Electrolytic Capacitors |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| $100 \mu \mathrm{~F}$ | 61p | $47 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | $1500 \mu \mathrm{~F}$ | 25p | 5000 F | 68 p | $2.2 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ |
| 220 ${ }^{\text {F }}$ | $6 \frac{1}{2} p$ | $100 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | 2000 $\mu \mathrm{F}$ | 43p | , |  | $4.7 \mu \mathrm{~F}$ | 61p |
| $330 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | 220 $\quad \mathrm{F}$ | 8p | 3300رF | 38p |  |  | $6 \cdot 8 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| 1000 ${ }^{\text {F }}$ | $F \quad 13 p$ | 330 ${ }^{\text {F }}$ | 10p 6 | 6800 $\mu \mathrm{F}$ | 65p | 40 VOL |  | $10 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| 4700 $\mu \mathrm{F}$ | $F$ 29p | 470 ${ }^{\text {F }}$ | 10 p |  |  | 6. $8 \mu \mathrm{~F}$ | $6 \frac{1}{4} p$ | $22 \mu \mathrm{~F}$ | ${ }^{61} \mathrm{t}$ p |
|  |  | $1000 \mu \mathrm{~F}$ $1500 \mu \mathrm{~F}$ | $11 p$ |  |  | $15 \mu \mathrm{~F}$ | 61 p | $68 \mu \mathrm{~F}$ | 10p |
| 33.3F | VOLT | $1500 \mu \mathrm{~F}$ | 20p | 25 V |  | $33 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | 100 ${ }^{\text {F }}$ | $11 p$ |
| $33 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{P}$ | 2200 F | 24p | $10 \mu \mathrm{~F}$ | $6 \frac{1}{1} \mathrm{p}$ | $47 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | $150 \mu \mathrm{~F}$ | 13p |
| 68 15 F | 61 p |  |  | $22 \mu \mathrm{~F}$ | ${ }^{6} \mathrm{t} p$ | $100 \mu \mathrm{~F}$ | 9p | 220 $\mu \mathrm{F}$ | 19p |
| $150 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | 6 VOL |  | $47 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | $150 \mu \mathrm{~F}$ | 10p | $330 \mu \mathrm{~F}$ | 22p |
| $470 \mu \mathrm{~F}$ | $11 p$ | $15 \mu \mathrm{~F}$ | 6 ${ }_{1}^{1} \mathrm{p}$ | $100 \mu \mathrm{~F}$ | 8p | 220 ${ }^{\text {F }} \mathrm{F}$ | $11 p$ | $470 \mu \mathrm{~F}$ | 26p |
| $680 \mu \mathrm{~F}$ | 13p | $33 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ - 1 | $150 \mu \mathrm{~F}$ | 8p | 470 ${ }^{\text {F }} \mathrm{F}$ | 19p | $1000 \mu \mathrm{~F}$ | 44p |
| $1500 \mu \mathrm{~F}$ | $F \quad 18 p$ | $68 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{P}$ 2 | 220, F | 10p | $680 \mu \mathrm{~F}$ | 25p |  |  |
| $2200 \mu \mathrm{~F}$ | $F \quad 18 \mathrm{p}$ | $150 \mu \mathrm{~F}$ | 8 p | 470 $\mu \mathrm{F}$ | 13p | $1000 \mu \mathrm{~F}$ | 25p |  |  |
| $3300 \mu \mathrm{~F}$ | F 26p | 220رF | 9 p 6 | 680 $\quad \mathrm{F}$ | 20p | 2200 $\mu \mathrm{F}$ | 44p |  |  |
| $6800 \mu \mathrm{~F}$ | $F \quad 40 p$ | $680 \mu \mathrm{~F}$ | 17p | $1000 \mu \mathrm{~F}$ | 22p | $3300 \mu \mathrm{~F}$ | 65p |  |  |

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| ACl07 | 18p | AD149 | 401 | EClS 7 | 13p | BFY50 | 17p | 2N3053 | 26p | 40636 | 68p | OA47 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ACl26 | 14D | AD161 | 32p | BC1.j8 | 12p | BFY 51 | 17p | 2N3054 | 50D |  |  | 0.481 |
| ACl27 | 14p | AD162 | 32p | BCi59 | 130 | BFY52 | 17 p | 2N3055 | 58p | DIODE |  | OA5s |
| AC128 | 14D | AF114 | 15p | BC168 | 11p | MP8111 | 35p | 2N3702 | 11p | 1N914 | 8 p | OA90 |
| ACl42K | 25p | AFl1s | 15p | BC169 | 11p | OC28 | 40p | 2N3703 | 11p | 1N918 | 8 p | OA91 |
| ACl41K | 28p | AF116 | 15p | Br 182 | 1\%p | 0 C 35 | 40p | 2N3704 | 11p | 1N4148 | ${ }_{5}{ }^{\text {p }}$ | OA95 |
| AC176 | 15p | AF117 | 15p | BC183 | 12p | 0 O 36 | 45p | 2N3705 | 11p | 1N4001 | $4{ }^{1}$ |  |
| AC187 | 14p | BC107 | 9p | BC184 | 12p | OC44 | 14p | 2N3706 | 11 D | 1 N 4002 | 410 |  |
| AC188 | 145 | BC108 | $8 \mathrm{9p}$ | BC212 | 12p | $0 \mathrm{OC45}$ | 14 p | 2N3707 | 11 p | 1 N 4003 | $5\}$ |  |
| AC187K | 25p | BC109 | 10p | BC213 | 12p | OC71 | 14p | 2N3708 | 11p | IN4004 | B ${ }^{\text {p }}$ |  |
| AC188K | 24p | BC147 | 11p | BC214 | 12p | 0C81 | 14p | 2N3709 | 11p | IN4005 | 8p |  |
| ACY20 | 22p | BC148 | 11p | BF194 | 15p | TIP41A | 79p | 2N3710 | 110 | 1N4006 | 9p |  |
| AD140 | 40p | BC149 | 12p | BF195 | 17p | TIP42A | 91p | 2N3819 | 28p | 1 N 4007 | 10p |  |


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| 22p | 24p |
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| 2N709 | 0.38 | $2 N 3709$ | $\begin{array}{llll}2 N 709 & 0.38 & 2 N 3709 & 0 \\ 2 N 711 & 0.30 & 2 N 3710\end{array}$ 2 N

2 N $\begin{array}{lllll}2 \mathrm{~N} 121 & 0.55 & 2 \mathrm{~N} 3714 & 1.88 & 40600 \\ 2 \mathrm{~N} 914 & 0.22 & 2 \mathrm{~N} 3715 & 1.40 & 40601\end{array}$ | 2N929 | 0.30 | $2 N 3779$ | 3.16 | 40604 |
| :--- | :--- | :--- | :--- | :--- |
| $2 N 930$ | 0.48 | $2 N 3790$ | 2.40 | 40636 |

 $\begin{array}{lllll}2 N 1091 & 0.32 & 2 N 3792 & 2.69 & \mathrm{ACl}^{-}\end{array}$


 \begin{tabular}{ll|ll|l}
$2 N 1304$ \& 0.24 \& $2 N 3823$ \& 1.48 \& ACl2 <br>
$2 N 1305$ \& 0.24 \& $2 N 3824$ \& 1.33 \& ACl

 

$2 N 1306$ \& $0-31$ \& $2 N 3826$ \& 0.23 \& AC128 <br>
2 ACl <br>
2 N 1307 \& 0.22 \& 2 N 3854 \& 0.18 \& ACl41K

 

$2 N N 1308$ \& 0.25 \& $2 N 3854 A$ \& 0.18 \& ACl42K <br>
$2 N 1309$ \& 0.35 \& $2 \mathrm{~N} 38 \overline{5} 5$ \& 0.18 \& $\mathrm{ACl5LV}$
\end{tabular}

 $\begin{array}{llllll}2 N 1613 & 0.33 & 2 N 3856 A A & 0.20 & \text { AC153 } \\ \text { AN } & \end{array}$ \begin{tabular}{ll|ll|l}
$2 N 1631$ \& 0.38 \& $2 N 3858$ \& 0.18 \& AC154 <br>
$2 N$ \& 637 \& 0.38 \& $2 N 3858 A$ \& 0.19 <br>
AC176

 

$2 N 1638$ \& 0.32 \& $2 N 3859$ \& 0.14 <br>
$2 N$ \& AC176K <br>
$2 N 1701$ \& 1.18 \& $2 N 3859$ A \& 0.19 <br>
AC187K
\end{tabular}

 49 A8Y50 $0.20 |$\begin{tabular}{ll|l|l|}
BCYB7 \& $\mathbf{3 . 5 4}$ \& BFYY

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\& 0.16 \& BC107 \& 0.16 <br>
BCY89

 .81 BC108 0.50 HC113 0.82 BC113 .50 BC115 0.82 BC116 0.48 BC1164 0.48 BC116A 

0.48 <br>
\hline $0.5 C 117$ <br>
HC1

 

0.50 \& HC118 <br>
0.81 \& BC1 19
\end{tabular} 0.46 BC121

 0.4
0.3
0.5
0.8 $\mathrm{BC126}$
BCl 32
$\mathrm{BC134}$
BC 3 S
BCl
0 0.16 BCY89 . 10 BCZ10 .18 12 is 1116 15 13D151 BD131

BD132 | 11 | BD13 |
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| BU13 |  | 0.42 BFY $\begin{array}{ll}0.07 & \mathrm{BFY} \\ \mathbf{0 . 3 5} & \mathrm{BFY} 2\end{array}$ 0.3 BHFY B 0.64 BFY29 $\begin{array}{ll}\mathbf{U} .75 & \mathrm{BFY} 37 \\ \mathbf{0 . 7 5} & \text { BFY }\end{array}$ 7b BFY4i



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## Project 80 new modules

## Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilled in the wood or plastic on which modules are to be mounted. All the electronics are contained within the $\frac{3}{4}$ " deep front panal! Connecung leads are taken away similarly out of sight Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders This enables exceptionally good environmental matching to be obtained Provision is made for magnetic and ceramic pick-ups.radio and tape in and out A virtual earth inpul stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources Generous overload margins are allowed on all inputs Clear instructions with template are supplied

TECHNICAL SPECIFICATIONS
Size $-260 \cdot 50 \cdot 20 \mathrm{~mm}$ ( $10 \frac{1}{4} \times 2 \cdot$. lns )
Finish - Black, with white markings
Inputs-Mag PU 3mV RIAA corrected, Ceramic P U. 300 mV Radı 300 mV . Tape 30 mV S/N ratio-60db
Frequency range -20 Hz to 15 KHz : $1 \mathrm{~dB} \quad 10 \mathrm{~Hz}$ to $25 \mathrm{KHz} \pm 3 \mathrm{~dB}$
Power requirements -20 to 35 volts
Outputs- $100 \mathrm{mV}+\mathrm{AB}$ monitoring for tape
Controls - Press button for tape radio and $\mathrm{P} U$ selection Volume.
Bass - 12 dB to -14 dB at 100 Hz . Treble +11 dB to -12 dB at 10 KHz


## Project 80 FM tuner <br> smaller, more efficient

A truly remarwable tuner in every way - its unbelievably compact size its original circuitry - its dependable performance - all this in a boldly destgned modern case measuring $85 \times 50 \times 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times 3$ ans). Greater adaptability (and possibly financial convenience) results from the tunet and stereo decoder section being made avalable separatelv
TECHNICAL SPECIFICATIONS

Tuning range -87 to 108 MHz
Detector-IC balanced coincidence, for good A M rejection
AFC - Switchable. with thermistor control to prevent from drift
One 26 transistor I.C.
Twin dual varicap tuning
Distortion-0 $3 \%$ at 1 KHz for 75 KHz deviation
Ceramic filter in I.F. section
Aerial impedance-75 $\Omega$ or 240-300 $\Omega$
Sensitivity - 4 microvolts for 30 dB quieting
Power requirements -12 to 45 volts


## Project 80 stereo decoder

Making the Project 80 decoder separate from the $F M$. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required This unit gives a 40 dB channel separation with an output of 150 mV per channel The gallum arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception

One 19 transistor I.C.

## new constructional techniques

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| 1962. | Micro-minature power amp small enough to stand on a <br> 1Op. piece. Slimline pocket receiver smaller than a 20 |
| :--- | :--- |
| cigarette pack |  |

1968 IC. 10 , the first ever integrated circuit for constructors use

## Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhule system where inputs may be from record, radio of tape. As with Stereo 80, separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment.

TECHNICAL SPECIFICATIONS
Size $-108 \times 50 \times 20 \mathrm{~mm}\left(4 \frac{1}{4} \times 2 \times \frac{3}{4}\right.$ ins $)$
Voltage gain - mınus 02 dB
Frequency response -36 Hz to 22 KHz . controls minımum
Distortion - at $1 \mathrm{KHz}-003 \%$ using 30 V supply
HF cut off (scratch) -22 KHz to $5 \cdot 5 \mathrm{KHz}, 12 \mathrm{~dB} /$ oct slope
L.F. cut off (rumble) -2.8 dB at $20 \mathrm{~Hz}, 9 \mathrm{~dB} /$ oct. slope

## Z. 40 \& Z. 60 power amplifiers totally short-circuit proof

Either of these entirely newpower amplifiers is intended for use in Project 80 installations although, of course, they are readily adaptable to an even wider range of applications Both $Z .40$ and $Z .60$ incorporate builtin protection against shortctrcuiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules.
Z.40 Technical Specifications Size $-55 \times 80 \times 20 \mathrm{~mm}$
$\left(2 \frac{1}{8} \times 3 \frac{1}{8} \times \frac{3}{3} 1 \mathrm{~ns}\right) 9$ transistors Input sensitivity -100 mV
Output -15 watts RMS contınuous
into $8 \Omega(35 \mathrm{~V}) .30$ watts music
powerlinto $4 \Omega(30 \mathrm{~V})$
Frequency response $-10 \mathrm{~Hz}-$
$100 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal to noise ratio -64 dB
Distortion - at 10 watts into $8 \Omega$
less than 0.1\%
Power requirements - 12-35 volts

Z 60 Technical Specifications Size $-55 \times 98 \times 20 \mathrm{~mm}$ ( $2 \frac{1}{1} \times 3 \frac{3}{2} \times$ 浆ins) 12 transistors Input sensitivity-100-250mV Output - 25 watts RMS into $8 \Omega(45 \mathrm{~V}) .50$ watts music power into $4 \Omega(50 \mathrm{~V})$
Distortion-typically 0 03\% Frequency response -10 Hz to more than $200 \mathrm{KHz} \pm 1 \mathrm{~dB}$ Signal to noise ratio - better than 70 dB
Built-in protection agaınst transient overload and short circuit
Load impedance $-4 \Omega$ min; max safe on open circuit

## Sinclair power supply units PZ. 8

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R.R.P. £4.98+0.49p

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[^4]1969 Q.16-improved version of Q. 14 Systems 2000 and 3000
Project 60 launched
1970 IC. 12 : Project 605
1971 Project 60 stereo FM tuner: Z.50: PZ. 8
1972 Improvements to Project 60 with Z.50 MK. 2 and PZ. 8 MK. 3
The Executive Calculator: Digital multi-meter:
Q. 30 speaker

1973 Cambridge Calculator
PROJECT 80 LAUNCHED
and next?


Recommended Project 80 applications

| Systern | The Units to use | Units cost |
| :---: | :---: | :---: |
| Simple battery record player | 2.40 | $\begin{aligned} & \mathbf{f 5 . 4 5} \\ & +54 p \vee A . T \end{aligned}$ |
| Mains powered record player | Z.40, PZ. 5 | $\begin{aligned} & \mathbf{f} 10.43 \\ & +E 104 \vee A T . \end{aligned}$ |
| 30W. RMS contınuous sine wave stereo amp. | $\begin{aligned} & 2 \times \text { Z.40s, Stereo } \\ & 80 ; \text { PZ. } 6 \end{aligned}$ | $\begin{aligned} & \mathbf{£ 3 0 . 8 3} \\ & +£ 308 \vee A . T \end{aligned}$ |
| $50 \mathrm{~W}(8 \Omega)$ RMS continuous sine wave de luxe stereo | $\begin{aligned} & 2 \times Z .60 \text { s, Stereo } \\ & 80 ; P Z .8 \end{aligned}$ | $\begin{aligned} & \mathbf{£ 3 3 . 8 3} \\ & +£ 3.38 \vee \cdot A . T \end{aligned}$ |
| amplifier Indoor P.A. | Z.60, PZ.8 | $\begin{aligned} & \mathbf{£ 1 4 . 9 3} \\ & +£ 1.49 \vee A T \end{aligned}$ |
| Car Radio | F.M. tuner, $2.40$ | $\begin{aligned} & \mathbf{f 1 6 . 4 0} \\ & +£ 1.64 \vee A T . \end{aligned}$ |

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