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## SEMICONDUCTORS



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## VOLUME 12 No. 1 JANUARY 1976

## CONSTRUCTIONAL PROJECTS

ROAD-ICE WARNING INDICATOR by A. M. Owen A simple early warning device for monitoring driving conditions
IC50 GUITAR AMPLIFIER-2 by B. W: Terrell \& C. F. Terrell This concluding article deals with construction and testing ..... 25
DIGITAL LOGIC CHECKER by D. Coles
A visual in-circuit pocket logic checker ..... 52
AUDIO COMPRESSOR by S. Whitt
Obtain better recordings with this inexpensive unit ..... 56
RANDOM TONE GENERATOR by W. G. Ross
An electronic doorbell which can provide a variety of "tunes" at the press of the door switch ..... 58
GENERAL FEATURES
INGENUITY UNLIMITED
Headlight Dimmer-Skin Resistance Indicator-Random Generator-Sawtooth Generator-
Sequencing Oscillator-Output Meter-Simple Lights Flasher-Temperature Sensing Device-
Time Switch-Voltage Controlled Zener-Lights-on Reminder-Voice Operated FaderModifications-Dwell Meter Modifications35
USING CMOS DIGITAL I.C.s-1 by D. B. Johnson-Davies \& A. M. Marshall
An introductory course to operating principles, practical guidance and experimental circuits for this fast moving technology ..... 44
SEMICONDUCTOR UPDATE by D. W. Coles ..... 48
A review of interesting devices
NEWS AND COMMENT
EDITORIAL-Small Mercies ..... 21
SPACEWATCH by Frank W. Hyde Jodrell Bank-Black Holes and White Holes ..... 31
BOOK REVIEWS
Selected new books we have received ..... 32
MARKET PLACE
Interesting new products ..... 42
INDUSTRY NOTEBOOK by Nexus What's happening inside industry ..... 55
NEWS BRIEFS
Viewdata Service—IERE Golden Jubilee ..... 60, 62
POINTS ARISING
Light Modulation Unit ..... 62
PATENTS REVIEW
Tape Noise Reduction-Electrostatic Loudspeaker-Patent News ..... 65
READOUT66
Our February issue will be published on Friday, January 9, 1976(for details of contents see page 49)

[^0]
trade enouiries welcomed

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| 7411 | 16 |
| 7413 | 35 |
| 7415 | 22 |
| 7416 | 22 |
| 74.7 | 22 |
| 7420 | 11 |
| 7422 | 22 |
| 7423 | 22 |
| 7425 | 22 |
| 7426 | 23 |
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| $\begin{aligned} & \text { Pos } V \text { reg } 15,6,8,12,15, \\ & 18.24) \end{aligned}$ | T0.3 | 1:20 |
| Pos Volt Reg <br> ( $6 \mathrm{~V} \cdot 8 \mathrm{~V} \cdot 12 \mathrm{~V} \cdot 15 \mathrm{~V} \cdot 18 \mathrm{~V} \cdot 24 \mathrm{~V}$ ) | TO 220 | 1.07 |
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| 50 ua . | c6.00 | I |  |
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| 100uA | ¢5.95 |  |  |
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| 1 mA | c5. 75 | : | \% |
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| 100 ma | C5.75 | 300 VaC | 65.85 |
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| 50.0 .50 ua | 13.85 | $\cdots{ }^{+1}$ |  |
| 100.0.100uA | ${ }^{\text {E 3 }}$. 70 |  |  |
| 5 ma | ${ }_{\text {¢ }}$ | แull |  |
| 10 ma | ${ }^{\text {c } 3.65}$ |  |  |
| 50 mA 100 mA | E3.65 |  |  |
| 500 ml A | ¢ 3.65 |  |  |
| 14 DC | ¢3.65 |  |  |
| 5ADC | ¢3.65 | 5 Merer 1mA | C4. 20 |
|  | ${ }^{2} 3.65$ | $1{ }_{\text {IAAC }}{ }^{\text {cher }}$ |  |
| SOVDC | ${ }_{6} \mathbf{3} 65$ | 5 AaC |  |
| 300 V DC | ¢3.65 | ${ }^{10 A A C}$ | ¢3.65: |
| 15 VaC | 63.75 | 20 AAC | ¢3.65. |
| 3nov AC | ¢375 | $30 \mathrm{~A} A \mathrm{C}$ | ${ }_{63.65}{ }^{\text {. }}$ |


| BAKELITE MODEL MR 65 Size: $80 \times 80 \mathrm{~mm}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 25 UA | ¢5.80 |  |  |
| SOUA | c 4.40 |  |  |
| 100 ua | ${ }^{6} 4.35$ |  |  |
| 500 ua 50.0 .50 ua | ${ }^{\text {c } 4.05}$ |  |  |
| 50.0 .504 A 100.0 .100 A | ${ }^{\text {ca }}$ ¢ 3.35 |  |  |
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| 1 mA | £3,95 |  |  |
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| $50 A D C$ $5 V D C$ | ¢4. 20 | $10 A A C$ $20 \triangle A C$ | ${ }_{\text {c }} \mathbf{3} 3.955^{\circ}$. |
| lov Dc | ${ }_{63} 3.95$ | $30 A A C$ | 63.95. |
| 15 VDC | f395 | $50 A A C$ | ¢3.95. |
| zov DC | ¢3.95 | 500 ma AC | ¢3.95 |
| SOVDC | c3.95 | 50 mVDC | [4.15 |
| 150 VC | E3.95 | roomvoc | [415 |

CLEAR PIASTIC MODEL MR $65 P$
Size: $86 \times 78 \mathrm{~mm}$

| Size: $88 \times 78$ | E4.35 |  |  |
| :---: | :---: | :---: | :---: |
| 100 u A | ¢4.25 | - $-\cdots$ |  |
| 200uA | ¢4.20 |  |  |
| $50.0-50 \mathrm{ua}$ | $\mathrm{ff}^{4} 25$ |  |  |
| 100.0.000uA | ¢4 20 |  |  |
| 1 ma . ${ }^{\text {a }}$ | E4.10 |  |  |
| 1.0 .7 mA | E4.10 |  |  |
| 5 ma | E4.10 | 300 VOC | 1410 |
| 10n) | C4.10 | 15 VaC |  |
| 50 mA | ¢. 10 | 50 VAC | $\mathrm{C}^{4.20}$ |
| 100 mA | C4 10 | 150VAC | $\mathrm{c}_{4} 20$ |
| 500 mA | ¢4.10 | 300 VaC | E4.20 |
| ${ }^{14} \mathrm{DC}$ | ¢4.10 | 500 ac | $\mathrm{E}^{4} 30$ |
|  | C4,10 | 5 Meter 1ma | C4, 85 |
| 10 ADC | E4.10 | Vumeter | c5.20 |
| 154 DC | C4 10 | $14.4 C$ | ${ }^{64.10}{ }^{\circ}$ |
| 204 DC | E420 | $5 A A C$ | $4.10{ }^{\circ}$ |
| 30 AC | ¢4.25 | $10 A A C$ | £4,10. |
| ${ }_{50 A D C}$ | ¢4.10 | 20 AC | E4,10* |
| SVOC | ¢4,10 | $30 A A C$ | E4,10. |
| 10 VDC | E4.10 | 50 AaC | E4.10 |
| 15 VDC | E4, 10 | 50 mAAC | f410. |
| 20 VC | ¢4.10 | 100 mAAC | C4, $10^{\circ}$ |
| 50 V DC 150 VDC | E4 10 | 200 mA AC | ¢4.10. |



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YAMABISHI VARIABLE VOLTAGE TRANSFORMERS Excellent guality at low cost. Input:
$230 \mathrm{E} 50 / 68 \mathrm{~Hz}$. Output $0-260 \mathrm{~V}$. MODEL SZ60 BENCH MOUNTING
 Build yourself a
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meter scale. movementan
rotaryrange selector read mounted in
 cabinet. All parts.
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U4312 MULTIMETER extrrmaly sturdy

instrument for anneral electrical Lso. 667 opv. | $500150 / 300 / 600 /$ |
| :--- |
| 900 |
| 15 mv |

 $000 \mathrm{AC} 0,1300 \mathrm{~A}$, $600 \mathrm{~mA} / 1 / 1.5 / 6 \mathrm{~A}$ C. 0/1.5/8/15/

1.5/6A AC. $0 / 200 / 3 \mathrm{k} / 30 \mathrm{k}$ ohms. DC sceursey 1\%. AC 1.5\%. Knito edge turdy maral cerrying case, leads and instructions
OUR.PRICE $\mathrm{f} 11.60 \mathrm{P} / \mathrm{P}$ \& ins $80_{\mathrm{p}}$
TMK MODEL TW50K



10 Mog ohme. -20 to +81.5 dB . OUR PRICE $513.50 \mathrm{p} / \mathrm{P}$ \& In Emp .
U4313 MULTIMETER
 $3 / 15 / 60 /$
$300 / 1.5 A$

15/30/60/1 50/300/600: DC resisTance $1 \mathrm{kohm} / 10 / 100 / 1.000,-10$ to
+12 dB , otc. Complete with steel carrying caseand leads, manual OUR PRICE f14.90
$\qquad$
U4317 MULTIMETER High seneitivity
instrument for fien and laborstony field
$K$ nife Knite edge pointar,
O6mm. mirror scale.

## Aanges: $100 \mathrm{mV} /$

$0.5 / 2.5 / 10 / 25 / 50 / 100 / 250 / 500 / 1000$ $500 / 1000 \mathrm{~V}$ AC. Current: 50 A/ 10 / $1 / 5 / 10 / 50 / 250 \mathrm{~mA} / 1 / 5 \mathrm{~A}$ DC. $0.25 /$ $0.5 / 1 / 5 / 10 / 50 / 250 \mathrm{~mA} / 1 / 5 \mathrm{AAC}$. Res;
istance: $0.5 / 10 / 100 / 200$ ohms/1/3/ istance: $0.6 / 10 / 100 / 200$ ohms/1/3/
$30 / 300 \mathrm{k}$ ohms. Decibets: -5 to +10 dB Battery operzted. Size: $210 \times 115 \times$ 90 mm . Supplied in carrying case com-
OUR PRICE $£ 18.35 \mathrm{p} / \mathrm{P}$ \& Ins 60 P

## U91 Clamp VOLT

 AMMETER For messuring AC voltbroaking circuit. Ranges: 300/600V AC. Curtint10/25/100/250/500A. 10/25/100/250/500A.
Aceursey
$94 \times 36 \mathrm{~mm}$. Complete $\mathbf{9 4 \times 3 6 m m}$. Complete OUR PRICE E15.10 P/P \& Ins 60 p


KAMOOEN 360 MULTIMETER Hegh sansitivity.
DC $100 \mathrm{kohm} / \mathrm{y}$ AC 10kohm/V
over
ed.
$2.5 / 1$
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$1 / 10$
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1 AC. Currant $500 \mathrm{~mA} / 10 \mathrm{~A}^{2} / 5 / 50 /$ Resistance: $0.1 /$
$1 / 10 / 100$ ohms/ $1 / 10 / 100 \mathrm{ohms} /$
$1 / 10 / 100 \mathrm{khms}$ ohm
 10/100M ohms.
+62 dB . Battery operated. Size: $180 \times$
$140 \times 80 \mathrm{~mm}$. Supplied complete OUR leads etc. Model HT100B4 MULTIMETER Overload protected, shock proof circuits.
9.5uA Matar with mirror scale. Sensitivity 100k. Polarity change,
switch. Panges $0.5 / 2.5 /$ 1/150/250/500/1.000
Volts DC. $2.5 / 10 / 50 /$
25011,000 Vols AC. $250 / 1,000$ Volss
0 C resisfence'
$200 \mathrm{k} / 2 / 20 \mathrm{Meg}$
200 currant:- $10 / 250$ it/2.5/25/250
$\mathrm{OA} / 10 \mathrm{~A}$. AC current: $-0-10 \mathrm{AA},-20$ $\mathrm{mA} / 10 \mathrm{~A}$. AC current:-0-10A. -20
to 462 dB . Operates from $2 \times 1.5 \mathrm{~V}$ OUR PRICE $\mathrm{f} 21.50 \mathrm{P} / \mathrm{P}$ \& Ins $60 \rho$

## KAMOOEN HM720B FET VOM

Input impedence 10
Megohms. Ranges:-
$0 / .25 / 1 / 2.5 / 0 / 50 /$
1000 V DC $0 / 2.5 / 1$ 1000 V DC. $0 / 2.5 / 10$
$50 / 250 / 1000 \mathrm{AC}$
$0 / 25 \mathrm{~A} / 25 / 25 / 250$ mA OC
$0 / 5 \mathrm{k} / 50 \mathrm{k} / 500 \mathrm{k} / 5 \mathrm{M}$ 500 Megohms
OUR PRICE


MODEL AF. 105 VOM 50.000 opv. M
scale. Meter
protection.
$0 / 3 / 3 / 12 / 60 / 120 /$ $300 / 600 / 1200 \mathrm{~V}$ DC 0/6/30/120/ $300 / 600 / 12$
$0 / 30 \mu \mathrm{~A} / 6 /$
$50 / 300 \mathrm{~mA}$
12 Amp. $0 / 10 \mathrm{~K}$ $1 \mathrm{~m} / 10 \mathrm{~m} / 100$ OUR PRICEE13.50p/P \& Ins 60p
 OUR PRICE f18.90p/P \& Ins 60p

## U4341 Multimeter $\&$

 Transistor Tester 27 ranges. 16,700 opv.Overload protected.
Rances: $0.3 / 1.5 / 6$ / Rangea: $0.3 / 1.5 / 6$ /
$30 / 60 / 150 / 300 / 900 \mathrm{~V}$ $30 / 60 / 150 / 300 / 900 \mathrm{~V}$
$\mathrm{DC} .1 .57 .5 / 3 \mathrm{C} / 150 /$ Current: 0.06 /0.6/ $6 / 60 / 600 \mathrm{mADC}$
$0.3 / 3 / 30 / 300 \mathrm{mAA}$
 0.6/2/6/20/60/200k ohms/2 Mohms. Batrery operated. Supplied complete
with probes, leads and stoel carrving with probos, leads and stoel carrying
case. Size: $115 \times 215 \times 90 \mathrm{~mm}$. OUR PRICEf11.85 P/P \& Ins 60p

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TRANSISTOR TESTER High quality
instrument to instrument to
test reverzo lab current and DC current. Ampli-
fication factos of
NPN PNP diode fication factor of
NPN, PNP. diodes. transistors. SC
stc. $4^{\prime \prime}$ square clear scale meter
Operates from inperates from Complete with instructions, iead
carry ing handle. OUR PRICE $£ 18.90$


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Ins 60 p
 Transistor tester measures Alpha. Beta
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For display of pulsed
and periodic wave-
and periodic wave-
forms in electronic
circuits. VERT circuits VERT. AMMP.
Bandwidth: 10 MHz . Bandwidth: 10 MHz .
Sensitivity at 100 kHz
VRMS/mm: $0.1-25$; VRMS/mm: 0.1-25 width: 500 kHz .00 kHz
Sensitivity $10 y=0.02$
VRMS $/ \mathrm{mm}: 0.3-25$ Preset riggered sweep
1-3000usec. Free ru

$\qquad$ ${ }^{\mathrm{kHz}} 20$ in nine ranges. Catibrg 20-200 $220 \times 360 \times 430 \mathrm{~mm}$. $115-230 \mathrm{~V}$ AC OUR PRICE $47.50 \begin{gathered}\text { P/P } 81 \mathrm{lns} \\ \mathrm{f} 1.50\end{gathered}$

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| AC. |
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| Deci |
| OUR |} KAMOOEN 72.200 Multitester High sansitivity

tester. 200,000 op
Overlo Over. 200,000 opv Ranger:-0/.06/.3
3/30/120/600/ $1200 V$ DC. $0 / 3$
$12 / 60 / 300 / 11200$ $V A C .0 / 6 u A /$
$1.2 \mathrm{~mA} / 120 \mathrm{~mA}$ $600 \mathrm{~mA} / 12 A D C$
$0 / 12 A$ AC. -20 0/12A. AC. -20 to
+63 dB . $0 / 2 \mathrm{k} / 200 \mathrm{k} /$
 OUR PRICE £24.30p/P \& Ins 60p
 GEN Size 1 eOmm $\times 215 \mathrm{~mm} \times 170 \mathrm{~mm}$
DUR PRICE $\mathbf{E 2 4 . 3 0 ~ P / P ~ \& ~ I n s ~} 60 \mathrm{p}$

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portable AF portable. AF sine-
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Sine 20 cps
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on 4 banish.
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cps to 30
kHz. Output
impedencs
5000 OHms.
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| Premer | Will measure $A C$ and $D C$ volts, $A C$ |
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| 805 - ${ }^{\text {a }}$ - polarity. Indication of positive and |  |
| Nowavailable | negative overload is also provided. |
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25 watt-ra. 20
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$26 / 25 V$ \& $10 p$ \& $8+16 / 860 \mathrm{~V}$ \& 50 p \& $82+82+82 / 850 \mathrm{~V}$ \& 8 p <br>
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$50 / 00 \mathrm{~V}$ \& 10 p \& $16+16860 \mathrm{~V}$ \& 50 p \& $800 / 860 \mathrm{~V}$ <br>
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## SMALL MERCIES

All in all it has been a pretty grim year, with the pound in the pocket shrinking month by month. And the economists and financial experts predict there's worse to come before things bottom-out and the slow upward haul to more prosperous and cheerful times begins. So there is every reason to be thankful for any small mercies, like the downward trend in semiconductor prices that has taken place during the last twelve months.

Digital i.c.s have shown a spectacular fall, and CMOS devices the most notable of all. Keen rivalry betweendevice manufacturers competing for a stake in the large and growing computer field has stimulated the development of new monolithic technologies, and CMOS is now established as a possible alternative to TTL. The battle is likely to continue with the bipolar protagonists fighting back with more recently developed techniques such as emitter coupled logic and integrated injection logic, to say nothing of charge coupled devices and CDI. All these different families of i.c.s have promising futures for each has some unique advantages to offer which will be important in specific applications.

The lively competition augers well for the future of the electronics industry because the constant aim is the worthy one of more circuit functions per chip for a lower cost with, wherever possible, enhanced operational performance. A commercial philosophy which could well be emulated by other industries, since all too often it seems some sacrifice of quality or quantity is the only way a price reduction can be realised.

It is fortunate that the chief building blocks of electronics are extremely viable in present day terms, with continuing downward tendencies in cost rather than the reverse. Fortunate for everyone in the long term-because electronics has a most vital part to play, directly or indirectly, in improving the economic wellbeing of the country and the standard of living of the individual.

The private designer and constructor already enjoys some of these benefits. Active devices are likely to account for the smaller portion of the total material cost in a modern design. Not unexpectedly there is sometimes a temptation to extravagance in the use of i.c. devices, simply because they are modestly priced. At least, this might be considered to be the case by those brought up with a more frugal outlook during the pre-semiconductor era. Yet however cheap and versatile the components, the project designer owes it to himself and to those who may imitate his work to observe sound design principles throughout and to strive for elegance in circuit arrangement and economy in component count, no less than in price. Small is beautiful, it is said. Good housekeeping is laudable in good and bad times alike. That goes without question.
F.E.B.

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ICE will begin to form on roads when air temperature is between $36^{\circ} \mathrm{F}$ and $32^{\circ} \mathrm{F}\left(2 \cdot 2^{\circ} \mathrm{C}-0^{\circ} \mathrm{C}\right)$ in our damp winter conditions. This device monitors the air temperature by means of a thermistor and gives warning of impending icy road conditions by variable flash duration of a light-emitting diode. The completed unit is so small that the entire assembly may be housed in a small metal cannister and fixed through the dash of a car by a single $\frac{3}{8}$ in bush.

## CIRCUIT FUNCTION

This circuit depends upon the ratios of currents flowing and is therefore insensitive to fluctuations in the car's battery potential and most interference derived from the vehicle's electrics. Power-line regulation is therefore unnecessary, but a $0 \cdot 1-1$ microfarad capacitor across the power input to the unit may be needed in extreme circumstances. (C2 in Fig. 1.)

Section ICla of the quad op-amp package (MC 3401) forms a comparator looking at the current through the thermistor compared with that flowing in the "CAL" network, and R3 defines the output gradient of the amplifier according to the required response to temperature. For $36^{\circ} \mathrm{F}\left(2 \cdot 2^{\circ} \mathrm{C}\right)$, the output is approximately 7.2 V and at $32 \mathrm{~F}, 3.6 \mathrm{~V}$.

The multivibrator IC1.b is similarly designed so that the upper and lower voltages across Cl are of the same order, determined by R4, 5, 6. The oscillator has a period of approximately 1 second.

The third section of the op-amp is used as a comparator looking at the charge on C1 and comparing this to the output of ICla. When the charge on Cl is lower than the output of ICla, the output of

IClc goes positive and current flows through the l.e.d. whose maximum drain is limited by R7 to about $22-25 \mathrm{~mA}$.

As IClb produces a rough sawtooth waveform across Cl the on-time of the l.e.d. varies, as only the peaks lower than ICla's output will cause ICIc to turn on. Thus we obtain flashes from the l.e.d., starting as very short ones, at about $36^{\circ} \mathrm{F}$, and gradually becoming longer as ICIc's trigger-level is shifted by the action of the thermistor through ICla passing less current as it gets cooler. Finally the l.e.d. will be on continuously at about $32^{\circ} \mathrm{F}$ as IC1c will never be cut off.

## SENSOR PROBE

The sensor probe consists simply of a thermistor of 15 kilohms resistance (at $25^{\circ} \mathrm{C}$ ) mounted in an enclosure to baffle it from moving air as this could cause false indication. The whole assembly should be mounted as close to the ground as is practical, perhaps the best place being below the front apron or scuttle of the vehicle. It is important to keep the probe unit well away from any hot engine or radiator parts.

It is suggested that the thermistor element be mounted in an old cigar tube to act as a baffe, and suspended therein by small annular pieces of thick polyethylene sheet. No filler should be used, as this increases the conductivity to the thermistor and the baffle effect of the tube will be degraded.

No short-circuits should occur when the printed circuit assembly is inserted into the tube/baffle. The thermistor and the printed circuit board must be protected from the ingress of moisture and/or condensation.


## ROAD-ICE WARNNIN INDICATOR



Fig. 1. Circuit diagram for the ice warning indicator

## COMPONENTS . . .

Resistors

| R1 | $18 \mathrm{k} \Omega)$ | R4 | $3 \cdot 3 \mathrm{M} \Omega$ | R7 |
| :--- | ---: | :--- | :--- | :--- |
| $470 \Omega$ |  |  |  |  |
| R2 | $3 \cdot 3 \mathrm{M} \Omega$ | R5 | $10 \mathrm{M} \Omega$ | R8 |
| R3 | $3 \mathrm{M} \Omega$ |  |  |  |
| R3 | $150 \mathrm{k} \Omega$ | R6 | $10 \mathrm{M} \Omega$ | R9 |
| All | $10 \% \frac{1}{4} \mathrm{~W}$ carbon |  |  |  |

## Capacitors

C1 $10 \mu \mathrm{~F}$ elect. 10 V
C2* $0 \cdot 1-1 \mu \mathrm{~F}$ as required
Semiconductors
IC1 MC3401 (Motorola)
D1 TIL209 or similar
Potentiometer
VR1 $22 \mathrm{k} \Omega$ linear (RS)


Thermistor
RT-VA1100 or VA1055S (Mullard)
Miscellaneous
Small screw top canister (such as a film can)


Fig. 3. Constructional details and wiring for the probe


Completed prototype circuit board. Note that the l.e.d. is mounted inside the $\frac{3}{8}$ in dashboard mounting bush

Ensure good isolation between the terminations of the thermistor by removing the copper from the track as shown in Fig. 3.
Coat the whole of the p.c. board with a thin layer of 5 -minute epoxy-resin to prevent moisture affecting the resistance of the assembly.

Faster response to temperature might be achieved by filling the bottom of the tube, prior to insertion of the thermistor assembly, with silicone grease, although this has not been tried in practice.

Size of printed circuit board used and shown in the diagram is only arbitrary and will of course vary depending on the size of mounting tube available.

## CONSTRUCTION

The unit has been desizned to be as small as possible and is non-critical in its layout. However, in order to ensure that the unit works properly after

Typical housings for the probe and circuit board



Thermistor mounted on the probe board and covered with an epoxy-resin
construction and remains a reliable device, it is well to be sure that no dry-joints or track-bridging or shorts between components have occurred during the course of construction. The upper leads of R1, 6,9 should be sleeved.

## CALIBRATION

This is very simply accomplished by wrapping the thermistor, before mounting in the baffle-tube, in a polyethylene bag, to keep away the ice and water mixture in which it is to be immersed. The assembly is then plunged into the well stirred saturated solution of ice and water.

After about a minute, and with the unit fully wired and connected to a 12 V source, adjust VR1 to the point where the l.e.d. just comes on steady. A very slight "wink" may be noticed due to a slight imbalance between the outputs of $\mathrm{ICI}, \mathrm{IClb}$ because of resistor tolerances.

If it is not possible to obtain a steady illumination of the l.e.d. when the thermistor is at $32^{\circ} \mathrm{F}$, it may be necessary to add a $10 \mathrm{M} \Omega$ ( R 10 ) at the -ve input (Pin 3) and connect the other end to chassis.

## OTHER APPLICATIONS

If the unit is provided with a suitable 12 V battery supply there is no reason why this instrument may not be used as a portable menitor to check for the possibility of ice forming on outdoor swimming pools or fish ponds so that precautionary measures may be taken.

The unit may also be made to operate on other temperature ranges by changing the values of R 1 , 2, 3.

In view of the low current drain it was not considered necesary to incorporate an on/off switch for the in-car device.


## GUITARAMPIIFIER

LAST month we discussed the power supplies, pre-amplifier and power amplifier circuits of the guitar amplifier; this month we conclude with the wiring, construction and testing procedures.

## PREAMPLIFIER BOARD

A full-size drawing of the preamplifier printed circuit board is shown in Fig. 8. The layout of the components on the topside is shown in Fig. 5.

Ensure that the fixing holes at each corner are drilled before commencing assembly, and begin by inserting and soldering in the p.c.b. pins.

Although the integrated circuits used in the preamplifier are tough devices, it is strongly recommended that integrated circuit sockets be used and that the latter be soldered in position with the i.c. removed, thus avoiding possible damage from the heat of the soldering iron. In the event of the i.c.s needing replacement, it will then be an easy matter not requiring the removal of the board and not involving desoldering, which can be tricky. The layout of the board has been designed so that all the i.c.s "face" the same way. Do likewise with the i.c. sockets to avoid confusion at a later stage.

Fig. 5. Component layout for the pre-amplifier board. A full size p.c.b. master is given in Fig. 8



The finished guitar amplifier showing positioning of all the boards

Special note should be taken to observe correct polarity when soldering in the electrolytic capacitors. Do not attach any flying, leads at this stage.

## POWER AMPLIFIER BOARD

The printed circuit board to accommodate the components associated with IC3 is shown full-size in Fig. 8. The layout of the components on the topside of the board is shown in Fig. 6. Before embarking on component assembly, ensure that the four fixing holes have been drilled and that all the printed circuit pins have been inserted and soldered in place. Construction is straightforward, but pay attention to capacitor polarities. Do not attach any flying leads yet.

## POWER SUPPLY BOARD

The smaller components of the power supply section are mounted on a printed circuit board; the layout of the components on this board can be seen in Fig. 7. The full-size drawing of the copper clad side are shown in Fig. 8.

When positioning and soldering these components in place, special attention should be paid to the diodes and capacitor polarities, as a mistake in this section could have disastrous (and expensive) effects. Do not solder in any lead-out wires at this stage.

## CHASSIS DETAILS

The prototype chassis was made from two Lshaped pieces of 1.5 mm thick aluminium sheet and


Fig. 6. Component layout for the power amplifier board


Fig. 7. Component layout for the power supply board. The p.c.b. master is shown opposite full size


Fig. 8. Full size printed circuit masters for the IC50 Guitar Amplifier


Fig. 9. Complete drilling details for the amplifier chassis. The front panel drilling can be marked from panel $\mathbf{B}$
bolted together, using the component and component board fixing bolts to form a U-shaped chassis. Complete drilling and marking out details are given in Fig. 9. Both sheets should be marked out and drilled according to the details, and all the holes drilled before bending. Drilling details for the base of sheet A are incomplete (intentional), only the transformer fixing holes are shown. It is recommended that sheet $A$ base section and sheet $B$ base section be drilled (as shown) and then bolted together, and then sheet B used as a template. This method ensures that the holes in each sheet will be correctly aligned, whereas separate drilling may cause problems.

Once all the holes are drilled the right-angled bends should be made as indicated. A bracket is necessary for holding the power supply smoothing capacitors. Details are given in Fig. 11.

The front panel drilling details are taken from Fig. 9. It has the same dimensions as the chassis front and is commercially available guillotined to this size. The holes on the front panel were punched out using Q-max cutters which give a clean finish. The choice of decoration and finish on the front panel is left to the individual requirements of the constructor. In the prototype coloured adhesive film was used, the lettering and borders done with Letraset, and was then sprayed with Letragloss for protection.


Fig. 11. Drilling and bending details for the capacitor clamp

Fig. 12. Constructional details for the wooden case shroud


Fig. 13. Interwiring details for the guitar amplifier

## ASSEMBLY

The positioning of components, circuit boards and complete interwiring details are shown in Fig. 13. Assembly will be found easiest if carried out in the following order.
Begin by securing the transformer in place on the two chassis sections using 4BA nuts, bolts and shakeproof washers, thereby forming a single U-shaped chassis. Next fix all the completed component boards to the chassis using 6BA nuts, bolts, shakeproof washers and 5 mm long spacers such that the undersides of the boards stand clear of the chassis base. The use of a lock-nut is recommended.
The control potentiometers, jack sockets, neon and rotary on/off switch should next be secured to the front panel through the chassis front. All the potentiometers should have their connecting tags uppermost. Now fix IC3 in position using some silicon grease on the area of contact between IC3 and chassis to ensure good thermal contact. Screw the output jack socket SK3 in position and fix the panel mounting fuse to the rear panel. Insert a rubber grommet in the mains feedthrough hole immediately below the fuseholder. Bolt the chassis earth tag in place and then the cable clips to hold the mains lead.

It is now necessary to interconnect the four smoothing capacitors C13 to C16. To hold these together during wiring up, a wrapping of Sellotape will be found useful. Take special care that capacitor polarities are obeyed. When they are satisfac-
torily wired up, place them in position in the chassis and bolt on the capacitor bracket. Now wire up according to Fig. 13. It will be found useful to tick off the connections as you make them and also to use different colours of connecting wire. Try and use brown wire for positive supply rails, blue for the negative rails and green for all earth connections. This way wire tracing will be more simple.

## TESTING

When completed, the wiring should be checked out thoroughly, especially in the vicinity of the power supply board and the power output board. In particular, check that SK3 is wired up correctly. If the latter is wired in the wrong way round, IC3 can be permanently damaged.

When you are completely satisfied with your wiring up, the fuses should be inserted, 2A types for the supply board and a IA type in the back panel fuseholder. Fit the knobs and turn all volume controls anti-clockwise and set the tone controls to their midway positions.
First of all, with no speaker connected, plug in to the mains and switch on. If any fuses blow, or smoke or burning components are observed, switch off immediately and investigate. If all appears well the supply rail voltages should be measured. The preamplifier rails should be $\pm 15$ volts and the main amplifier rails approximately $\pm 35$ volts.
continued on page 47

## JODRELL BANK

A grant of nearly $£ 2$ million has been made by the Science Research Council, for the purpose of setting up a multi-unit interferometer.

Three of the telescopes that will make up the new group are already in existence, the Mark 1 and the Mark 2 at Jodrell Bank together with the 80 ft dish at Malvern. The addition of the fourth unit will considerably assist the work controlled from Jodrell Bank.

The extension of facilities will enable a much greater resolution to be obtained and Jodrell bank are hoping to achieve an accuracy of 0.03 seconds of arc. The manner of the disposition of the units will reduce the data to some extent, but it is considered that the increased resolution will more than compensate.

In order to make the best use of the grant it has been decided that the fourth unit shall be an "off the line" dish from America. A regular production line dish 25 m in diameter and fitted on an altazimuth mounting is available from E Systems Inc of Dallas, Texas. It will be installed at Knockin, near Oswestry, and be linked by landline and a reserve back-up microwave system.

The work involved in the future observations will be a continuing story and will include the study of the detailed structure of novae, pulsars, quasars and the areas where star formation is active.

## BLACK HOLES

Until recently the writer and a small number of people were of the opinion, "that the rotating black hole was possibly the gateway to an alternative space time". This seems not to be true after all and according to an advertisement the Bacon Foundation is offering a prize of $£ 300$ for the solution to the problem of a space ship to make the journey.

The problem as stated is, according to current theory, that rotating black holes are the actual gateways to an alternative spacetime. How, therefore, could a space vehicle pass through a rotating black hole into another region of spacetime, without being crushed by the gravitational field of a singularity?

This is so near to the ideas found in space fiction that perhaps here begins the new thinking, making further progress in the inevitable revolution in physics. The outcome of this challenge will be eagerly awaited.


## WHITE HOLES

While white holes are not often in the news their claims are now being seriously advanced. There has been activity in this field for a number of years now and it is not surprising that the same sort of people as those concerned with black holes are involved.

However, in the past white holes have not been taken too seriously. This attitude is not really justified and some new light is thrown on this subject by Professors J. V. Narlikar and K. M. V. Apparao.

The name of Narlikar is closely associated with the continuous creation theory advocated by Fred Hoyle. Narlikar was in fact a protégé of Fred Hoyle and many papers were issued under their joint names.

At the Tata Institute and among cosmologists, Narlikar is known for his extreme views. The creation of matter in the universe is an idea not much removed from the possibility of singularities which are projecting their energy out into the universe and so interacting with the matter around.

To this end Narlikar and Apparao have been looking more closely at the kind of spectrum which should appear from a white hole. The term white hole is not really apt but since it implies the opposite of black it will no doubt continue to be used. They are suggesting that the Seyfert galaxies could be a white hole effect. They are able to offer an explanation for all the facts observed including the particle production.

There is another possibility and that is that if a black hole is the entrance to another region of space time, could not the white hole be the emergence of the other side of a black hole?

The idea of a white hole of necessity involves blue shift. The name of Kapp comes to mind in connection with blue shift. Several years ago when his book appeared it caused a stir, for the claim made was that matter was being concentrated in certain areas, and that it was moving towards the observer. thus the blue shift.

## CO-OPERATION

For the first time a United States series of experiments will be flown in a Soviet Spacecraft. The scheme was discussed during the joint working group meetings on space biology and space medicine.

Four NASA developed life science experiments will be taken on board the spacecraft in special containers manufactured in the Soviet Union. The maximum weight of the containers including the experiments will be less than 2.5 kilogrammes each.

A unique feature of the spacecraft is the onboard centrifuge. The U.S. experiments will be divided with some on the centrifuge platform and some on the stationary platform.

The four experiments are concerned with the investigation of sensitive plant systems. The effect of weightlessness on embryonic plant systems. A heavy particle radiation experiment, small lexan plastic nuclear track detectors will be inside the containers on the centrifuge and in the stationary biological containers. And finally, an experiment with minnows to discover the effect of weightlessness on the vestibular system of developing embryos.

## WIND ON THE MOON

When making an analysis of the lunar soil samples delivered to earth by Luna 16 and Luna 20. Soviet scientists found that the Luna 20 material contained four times as much mercury as Luna 16.

The unevenness is thought to come about by the emanation of mercury vapour during the Lunar day, at a temperature of $150^{\circ} \mathrm{C}$, toward the colder areas by the lunar wind. As it cools it would be deposited on the rocks in the cold areas.


AUDIO ON WHEELS<br>By Vivian Capel<br>Published by Newnes-Butterworths<br>199 pages, $142 \mathrm{~mm} \times 222 \mathrm{~mm}$. Price $\mathbf{£ 6 . 0 0}$ (Hardback)

$\mathbf{W}^{\text {ith the seemingly ever increasing interest in "in-car }}$ entertainment" it is surprising that, until now, very little information on installing audio equipment in the car has been published. Of course, this does not include manufacturers' literature, which invariably only give part of the story anyway.

This book is divided into two parts, Basic Principles and Practical Applications, and sets out, fairly successfully in my opinion, to cater for the radio engineer, motor mechanic and the amateur. It covers all aspects of in-car entertainment from basic principles of radio and tape recording to the installation of complete systems.
The different types of radio, cassette and cartridge equipment, including stereo and quad systems are discussed and assessed. The chapters on power supplies, aerials, loudspeakers and interference suppression on a.m. and f.m. is covered in some depth and are probably the most useful sections in the book.
The chapter on setting-up a workshop is interesting and the final chapter on "Repair and Maintenance" contains some very good pointers on fault diagnosis and basic test procedures, together with the necessary test equipment needed.

The only criticism I can find (apart from price) is that it's a pity that the interference suppression section could not have been expanded to cater for solid state or CDI (Capacitor Discharge Ignition) systems. This could easily have been accomplished by deleting the references to the ancient valve vibrator power supply circuits.
D.G.B.

## BASIC DIGITAL ELECTRONICS

## By Ray Ryan

Published by Tab Books (No. 728)
210 pages, $130 \mathrm{~mm} \times 210 \mathrm{~mm}$. Price $\$ 7.97$ Hardback, \$4.95 Paperback

## ADVANCED APPLICATIONS FOR POCKET CALCULATORS

## By Jack Gilbert

Published by Tab Books (No. 824)
304 pages, $130 \mathrm{~mm} \times 120 \mathrm{~mm}$. Price $\$ 8.95$ Hardback, \$5.95 Paperback

ALTHOUGH these two books are of American origin, they offer a good basic grounding in their relevant subjects. For the student or person who wants to realise the full potential of his calculator this book should prove a reasonable acquisition.

The main emphasis in the digital electronics book is on presenting the various types of digital circuits and describing the features pertinent to these circuits. Today, discrete circuits are seldom used and almost all logic is performed with integrated circuits. For this reason, there is a slight bias throughout towards the assumption that a given logic function is just that-a function.

The logic symbols used throughout are not to British Standards, but several chapters explain the basics of
logic and introduce the logic diagram and truth table. Because a system of one's and zero's probably seems strange to the uninitiated, the early chapters describe the binary number system and the different codes digital systems use in some depth. There is even a chapter on cmos logic.

The pocket calculator book covers 4 -function, scientific, programmable, electronic slide rules, metric converters and business units.

This book shows how the ability of the calculator to multiply and divide can be used to calculate square roots, cube roots, powers of numbers, logarithms and all the trigonometric functions to five or seven places. As an example the author shows how to perform the scientific computations above using an elementary 4 -function unit.

The book also shows how to solve such problems as quadratic equations, right angles, compound interest mortgage problems and even determine satellite orbits.
D.G.B.

## GUNN-EFFECT ELECTRONICS

## By B. G. Bosch and R. W. H. Engeimann Published by Pitman Publishing Ltd.

434 pages, $240 \mathrm{~mm} \times 160 \mathrm{~mm}$. . Price $£ 16.00$

WITH microwave technology very much on the increase, this book looks at one of the effects often used in microwave devices, that of the "transferred electron" or better known "Gunn" effect. The book is clearly aimed at those directly concerned with microwave device development or post-graduate students, and gives an authoritative account of the whole device technology.

Also the book serves to collate the great deal of work which has been done on the subject over the last few years not only through its own text, but also through the vast number of references that appear after each chapter.

The book commences by looking into the Gunn Effect in the strict sense (space-charge dipole domains) and then moves on to dipole-domain free operation. Mode classification, frequency limitations, efficiency, power and noise performance are then covered, followed by a detailed look at the actual manufacturing processes involved in producing Gunn devices.

The final few chapters deal with some application considerations and the book finishes by detailing the use of Gunn technology in logic circuits.
R.W.L.

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$10 \mu \mathrm{~F}$
16 V
7 p $10 \mu \mathrm{~F}$
10 V
$10 \mu \mathrm{~F}$
25 V
7 p $10 \mu \mathrm{~F}$
10 V
$10 \mu \mathrm{~F}$
63 V
1 p
$15 \mu \mathrm{p}$
16 p

7 p \begin{tabular}{ll}
$15 \mu \mathrm{~F}$ \& 16 V <br>
15 p <br>
$15 \mu \mathrm{~F}$ \& 6 P <br>
\hline 10

 $\begin{array}{lll}15 \mu \mathrm{~F} & 63 \mathrm{~V} & 7 \mathrm{p} \\ 16 \mu \mathrm{~F} & 40 \mathrm{~V} & 7 \mathrm{p}\end{array}$ $\begin{array}{ll}22 \mu \mathrm{~F} & 25 \mathrm{~V} \\ 2 \mathrm{p} \\ 22\end{array}$ 

$22 \mu \mathrm{~F}$ \& $63 \vee$ <br>
$32 \mu \mathrm{~F}$ <br>
\hline 0
\end{tabular} $32 \mu \mathrm{~F}$

310 V
$\mathbf{7 P}_{\mathrm{p}}$ $33 \mu \mathrm{~F} 16 \mathrm{~V} 7 \mathrm{p}$
$33 \mu \mathrm{~F} 40 \mathrm{~V} 7 \mathrm{p}$ $33 \mu \mathrm{~F} 40 \mathrm{~V} 7 \mathrm{p}$
$32 \mu \mathrm{~F}$
63 V
 $\begin{array}{lll}4 \mu \mathrm{~F} & 10 V & 7 \mathrm{p} \\ 47 \mu \mathrm{~F} & 25 V & 7 \mathrm{p} \\ 47 \mu \mathrm{~F} & 63 V & 8 \mathrm{p}\end{array}$ $\begin{array}{ll}47 \mu \mathrm{~F} 63 \mathrm{~V} 8 \mathrm{p} & \begin{array}{l}2200 \mu \mathrm{~F} 10 \mathrm{~V} 17 \mathrm{p} \\ 3300 \mu \mathrm{~F}\end{array} \mathrm{4V} 28 \mathrm{p}\end{array}$ MULTIMETER 22 Ranges plus AF/IF OscillaCor 20,000 ת/Volv dc- $0.5-1000 \mathrm{~V}$ $\mathrm{Vac}-2.5$ - 1000 V in 7 ranges ldc- $0.05-500 \mathrm{~mA}$ in 6 ranges Resistance- $5 \Omega$-IM $M$ in ranges. Accuracy $-5 \%$ of F.S.D OSCILLATOR-I KHz and $465 \mathrm{KHz}(\mathrm{A}, \mathrm{M}$.) at approx. I Volt Size一 $160 \times 97 \times 40 \mathrm{~mm}$. Supplied complete with carrying case. test leads and battery.
PRICE $E 8.64$ net P. \& P. 75 p.
$\qquad$ 34 Ranges. Hish sensitivity $20.000 \Omega / \mathrm{Volt}$. Overload protected. $\mathrm{Vdc}-0.6$ - 1200 V in 9 ranges. Vac-3-900V in 8 ranges. de -0.06 - 3 A in 6 ranges. ac-0.3-3A in 5 ranges. Resistance- $25 \Omega-5 M \Omega$ in 5 ranges Accuracy-de and R-2 $\% \%$ of F.S.D Size- $167 \times 98 \times 63 \mathrm{~mm}$ Supplied complese with storage case. PRICE \& 10.64 net P. \& P. 75 p


POTENTIOMETERS. Carbon Track $5 K \Omega$ co $2 M \Omega$, log or lin (and IKlin). Single. $17 \frac{1}{2}$ p Dual Gang 48p. Logsingle with switch 28 p . Slider Pots. $60 \mathrm{~mm}, 5 \mathrm{~K}-500 \mathrm{~K}$, log or lin. 45 p . Dual 55 p . Knob 10p.

| DIODES <br> IN4001 6: P | PLUGS <br> Din 2 Pin $12 p$ | ELECTROLYTIC CAPACITORS. Tubular \& Large Cans (UF/V): $1 / 25,2 / 25,4 / 25,4.7 / 10,5 / 25,8 / 25,10 / 10,10 / 50,16 / 25$. |
| :---: | :---: | :---: |
| IN4002 $7 \frac{1}{3} \mathrm{P}$ | 5 3 Pin 13p | 22/63, 25/25, 25/50, 32/25, 50/25, 100/10, 100/25, 7p. 50/50, 8p. |
| IN4003 9p | 5 Pin $180^{\prime \prime} 16 \mathrm{p}$ | 100/50, 200/25, 10p. 250/50, 18p. 500/10. 8p. 500/25, 17p. |
| IN4400 9p | Sid. Jack 20p | 500/50, 25p. 1000/10, 17p. 1000/25, 25p. 1000/50, 40p. 2000/10, |
| IN4005 12p | 2.5 mm jack 13 p | 20p. 1000/100. $61 \cdot 10.2000 / 25,35 p .2000 / 100$, \& $1 \cdot 20.2500 / 25$. |
| IN4006 14p | Phono 7p | 38p. 2500/50, 68p. 5000/25, 68p. 5000/50, £1.20. |
| IN914 7p | SOCKETS |  |
| $\begin{array}{ll} \text { IN916 } & 7 p \\ \text { 8A100 } & 10 p \end{array}$ | Din 2 Pin ${ }^{\text {P }}$ Pin 10 p | $16 / 450,38 \text { p. } 32 / 350,38 \text { p. } 50 / 250,40 \text { p. } 100 / 250,40 \text { p. }$ |
| OA5 42p | 5 Pin $180^{\circ} 12 \mathrm{p}$ | METALLISED PAPER CAPACITORS |
| OA47 9p | Std. Jack 18p | 250V: $0.05 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 6 \mathrm{p} .0 .25,6 \mathrm{p}, 0.5 \mu \mathrm{~F}, 7 \frac{1}{\text { P }}$. $1 \mu \mathrm{~F}, 9 \mathrm{p} .500 \mathrm{~V}$ : |
| OABI lip | 2.5 mm Jack 13p | 0.025, 0.05, 6p. 0.1, 6p. 0.25, 7ip. 0.5. 9p. $1000 \mathrm{~V}: 0.01$, |
| OA200 8p | Phono 7p | $11 \mathrm{p} .0 .022,13 \mathrm{p} .0 .047,0.1,19 \mathrm{p} .0 .22,28$ p. $0.47,36$ p, |

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$22 / 63,25 / 25,25 / 50,32 / 25,50 / 25,100 / 10,100 / 25,7 p .50 / 50,8 \mathrm{p}$.
. $100 / 50$. 200/25, $10 \mathrm{p} .250 / 50$, 18 p . $500 / 10$. 8p. $500 / 25$, 17 p .
 38 p . $2500 / 50,68$ p. $5000 / 25,68 \mathrm{p}$. $5000 / 50, \ldots 1 \cdot 20$.
HI-VOLT: 4/350, 20p. 8/350, 23p. 100/100, 27p. 16/350, 35p. $16 / 450,38$ p. $32 / 350,38$ p. $50 / 250,40$ p. $100 / 250,40$ p. METALLISED PAPER CAPACITORS
250 V : $0.05 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 6 \mathrm{p} .0 .25,6 \mathrm{p}, 0.5 \mu \mathrm{~F}, 7$ p. $1 \mu \mathrm{FF}, 9 \mathrm{p} .500 \mathrm{~V}$ :

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db scale- 10 to $+12 d b$. Accuracy-dc- $1 \frac{1}{2} \%$, ac- $2 \frac{1}{2} \%$ Accuracy-dr-15\%ach ach
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forms a potential divider, whose output voltage depends on skin resistance. Transistor TR1 compares the voltage with a reference and feeds a current proportional to the difference between the voltage and the reference to a multivibrator TR2 and TR3. The frequency of the multivibrator depends upon the current from TR1. A crystal microphone insert acts as a speaker. Simple electrodes may be made from a pair of thimbles to which wires have been soldered.

In operation the two thimbles would be put on two fingers of one hand, and VR1 rotated to give an intermediate tone pitch. Upon relaxing the tone pitch should fall slowly.
A. Russell,

Whinmoor.

## SKIN RESISTANCE INDICATOR

THERE is a relationship between the electrical resistance of a person's skin and and state of relaxation. A device to make people aware of changes in their skin resistance can tell them how relaxed they are (bio-feedback) and thus help them relax. The skin resistance indicator, Fig. 1, provides an audible tone which falls as the state of relaxation increases (skin resistance rises).
The circuit is shown in Fig. 1. Potentiometer VR1 and the skin resistance between the electrodes


## SIMPLE SAWTOOTH GENERATOR



Fig. 1

ASImple sawtooth generator may be constructed with the 555 timer and a germanium transistor. The circuit is shown in Fig. 1. TRI, D1 and RI form a constant current source. Cl thus charges at a constant rate until the 555 internal comparator triggers. Cl is then discharged quickly, and the cycle repeats itself. Variation of VR1 alters the charging current of Cl and thus the output freqency. A sawtooth output may be taken from Cl through a high impedance buffer. and a spike output of the same frequency is available from pin 3. Output frequency may be varied by about $50: 1$, and the sawtooth linearity is about $5 \%$.

A linear voltage versus period characteristic can be achieved by applying a modulating voltage to pin 5, which sets the comparator threshold.

## J. N. Paine, Oxford.

## a gated output random generator



Fig. 1

THE following circuit (Fig. 1) was devised to act as a random generator of similar type to those used in parapsychology or ESP experiments. That is to say, it has an "off" period when neither of the light emitting diodes is illuminated followed by an "on" period when one or other, but not both of the l.e.d.'s is lit. Which l.e.d. is lit during this period is unpredictable, and this is the random aspect of the circuit.

The circuit consists of two sections: the random generator, and the gating circuitry. The random generator consists of a noise source (TR1) whose output is amplified
and shaped by the following stages and fed to NOR gate G4 which acts as a buffer.

The gating circuitry functions as follows. While the clock input (pin 12) of the 7470 J.K. flip-flop is at " 0 ", its output is allowed to follow its input signal, i.e. it is changing state for every input pulse. This output is not seen on the l.e.d. display however, as the clock signal is inverted by gate G1 and used to disable l.e.d. driver NOR gates G2 and G3. When the clock signal goes to logic " 1 ", the output circuits of the SN7470 are isolated from its input gates and are held, one at logic " 1 ", the other at logic " 0 ".

The clock signal is again inverted by gate G1, and enables the appropriate nor gate G2 or G3, depending which is fed from the " 0 " output of the SN7470. Thus the appropriate l.e.d. is illuminated.

The clock input is shown as a simple push button switch in the diagram, but provision is made for an external clock. This should be a positive going square wave not exceeding five volts. The mark-space ratio of this square wave will give the "randomise" to "display" times of the unit.
C. Cartlidge, Stafford.


## HEADLIGHT DIMMER

His idea was suggested by an article in a motoring magazine concerning sidelight visibility. The circuit is capable of reducing the current to the headlamps (or to any other resistive load). Their output is thus reduced to sidelight level, whilst superior visibility is retained.

The limited space behind the dashboard made remote voltage control a necessity. The circuit generates a
square wave with a variable markspace ratio, thus the lamps are either on or off and no power is dissipated by the circuit.
The circuit consists of a voltage controlled multivibrator driving a monostable which in turn drives the headlamps. This arrangement does not permit full control of the headlamps, but with a 12 V supply and $Z$ on the diagram connected to point $\mathrm{X} 0-10 \mathrm{~V}$ was obtained, or $4-12 \mathrm{~V}$ with Z connected to Y . A
little experimentation with Cl and C2 may be necessary for optimum performance.
A supply voltage between 11 18 V is satisfactory, but $\mathrm{V}_{22}$ (which provides the current) must not be higher than $\mathrm{V}_{1}$, or more than 5 V lower. The maximum safe current is 10 amps . A suitable source of Vin is shown in the shaded portion.
J. A. Heathcote

Newport.

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## LIGHTS-ON REMINDER

THIS circuit (Fig. 1) can be used to remind one to switch on sidelights when darkness falls. During the day the l.d.r. is in a low resistance state, TR1 is turned on and the relay RLA energised. Contacts RLAI are thus open (RLA is a normally closed type).

When the ambient light drops to a level preset by VR1, TR1 turns off, contacts RLA1 close and RLB (normally open) is energised via the side and tail filaments causing the buzzer to sound. When the sidelights are switched on RLB drops off and the buzzer is thus silenced.
D. Doughton,

Merseyside.


Fig. 1

SIMPLE TIME SWITCH


Fig. 1

ATime switch to save wasteful use of lighting on a staircase is shown in Fig. 1. The circuit operates a lamp for several seconds and consumes no power when not in use.
When S 1 is momentarily depressed it becomes bypassed by the relay switch. After several seconds the relay loses holding current, and the supply to both timer and lamp is broken. The timing network consists of R2, R3 and C1. Charge build-up on the capacitor is prevented by R3.

The addition of a light dependent resistor to a conventional lamp dimmer will allow control of mains lighting-the lamp being optically coupled to the I.d.r
S. L. Thompson,

Stafford.

## SEQUENCING OSCILLATOR

THIS circuit (Fig. 1) uses a 7413 and a 7490 to produce a repeating series of ten notes. R1, C1, G1 (lCla) form a low frequency oscillator which drives the decade counter. G2 (IC1b), R2, C2, R3, R4, C4, R5. C5 form another oscillator. Sections of this oscillator can be disabled by holding the input terminals of the decade counter at $\mathrm{V}_{\mathrm{ce}}$.

The outputs of the decade counter (A, B, C and D) are connected to the input terminals of the oscillator ( $1,2,3$ and 4). Any combination of inputs and outputs can be used (one input to one output). As

the decade counter counts. different parts of the oscillator are disabled, resulting in a series of ten notes.

The frequency can be changed by altering the value of the capacitors. W. H. Montgomery, Lorne.

## VOICE OPERATED FADER MODIFICATIONS



WITH a little modification the Voice Operated Fader (P.E. December 1973) can be made to drive f.e.t.'s instead of the more expensive (and harder to get) MFC 6040. The original circuit is shown in Fig. Ia. The shaded section should be deleted and the circuitry in Fig. 1 b inserted.
The control voltage at the collec-
tor of TR4 is fed to the gates of the f.e.t.'s TR5 and TR6 via the presets VR2 and VR3. The presets are incorporated to prevent image shift problems arising due to the f.e.t.'s pinch-off voltages being different.
The circuit uses the f.e.t.'s property of being a voltage controlled resistor, in this case the f.e.t.'s are
off with no "voice" input (TR4 on) and are driven on when there is a "voice" input. This results in attenuation of the left and right channels when a "voice" signal is present.

Since this is a shunt attenuator it would not be suitable for direct connection to a ceramic cartridge as in the original arrangement. Note

## OUTPUT METER

THE record level meter in less expensive tape-recorders is not used in the replay mode. Where the drive to the meter is a rectified, smoothed version of the record amplifier output, a simple switch and circuit can be used to display the audio output:
Fig. 1 shows the arrangement for the modified meter. SI is operated where possible by the record button such that the meter is only driven by the existing circuitry when in the record mode. When in playback the speaker drive signal is rectified by DI (any germanium signal diode) and the response of the meter is damped by capacitor C1.


## Fig. 1

Since the meter is less than $\operatorname{ImA}$ f.s.d. the series potentiometer VRI limits the current to a safe value. The indication on the meter is therefore the positive peaks of
the audio with the attack/decay time set by CI and the deflection for a given signal by VRI.
J. C. Sadler, Altrincham.
temperature sensing device


THIS circuit (Fig. 1) uses the Schmitt properties of the dual 4 input nand gate 7413. A potential divider is formed with the thermistor R1 in parallel with VR1. and R2. When the voltage from the potential divider exceeds the Schmitt threshold. an oscillator formed around the remaining components is activated. Potentiometer VR1 allows adjustment of the threshold temperature.
The whole circuit may be built on a piece of Veroboard 5 cm by 5 cm .
P. R. G. Reynolds, Benfleet.

Fig. 1b

that the earth should be changed from the lower (negative) rail to the upper (positive), since the f.e.t.'s are working around the positive rail.

N . Valentine,
Angus.

## VOLTAGE CONTROLLED ZENER

The circuit shown in Fig. 1 can be used as a voltage controlled Zener diode. If the f.e.t. is replaced with a resistor R2 the standard "amplified diode" configuration is obtained.
The addition of a f.e.t. merely provides a voltage control of one of the resistors and thus a control over the voltage at which the transistor turns on.

## I. D. Evans, <br> Cambridge.

Fig. 1


## dWELL METER MODIFIGATIONS



Fig. 1

WITH the simple addition of a few more components the Dwell Meter (P.E. Dec. 74) can be used as a voltmeter, ohmmeter and to check the opening of the points-as well as the original capability of being a dwell meter.

Fig. 1 shows the modified circuit. It operates in the following way.

To read dwell angle $\boldsymbol{S} 1$ made; $\mathbf{S} \mathbf{2}$ to leit.

To read ohms; S1 made; S2 to right and adjust VR1 for full scale reading with terminals 1 and 2 shorted. (There is no need to cali-
brate the scale in ohms as one only requires an indication of good or bad continuity.)

To read volts; SI is open and with the $15 \mathrm{k} \Omega$ resistor in circuit a full scale reading of 15 V is obtained. It is advisable to use this range and calibrate the dial from $0-15 \mathrm{~V}$ accordingly, whereby a reasonable indication of 12 V is obtained. It may be necessary to adjust this on test to obtain an accurate reading.
W. E. Priest, Bradford-on-Avon

## SIMPLE LIGHT FLASHER

The circuit shown in Fig. 1 can
be used to flash Christmas tree lights. An 80W fluorescent lamp starter is placed in series with the set of lamps and it is this that causes them to flash. No suppression is required since the starter has a capacitor included. No radio or TV interfence was detected. The total power supplied should not exceed 80W.
S. Judson, Halifax


Fig. 1

# marinet PLACE 

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned. All quoted prices are those at the time of going to press.

## DIGITAL WATCH

The long awaited Sinclair digital watch has now been launched onto the market. Referred to as the "Black Watch", this instrument is a typical example of the individual styling expected from Sinclair. The watch is housed in a specially designed plastic case-almost unique in the field of digital watches in that the case is custom built and not just a normal type of watch housing.

Flexible diaphragms form an integral part of the plastics case and provide an economical and reliable solution to the switch problem. These "pressure pads" are easy and convenient to use. Another important feature for the user is the readily removable plug type of cover for the battery compartment.
The watch circuitry is contained within a single integrated circuit using injection logic technology ( $I^{2} \mathrm{~L}$ ). This bipolar process is claimed to have produced very high packing density and excellent speedpower product, with important production cost benefits. The chip was designed by Sinclair and has been produced by ITT in Britain. The other components are a crystal, a trimming capacitor, the l.e.d. display and two small mercury cells.

Hours and minutes or minutes and seconds are displayed depending which switch pad is depressed. The display is internally timed for one second or will stay on as long as the switch is closed. The third switch is on the rear of the case and is used for setting the watch and holding the time.
The display is fitted with a lens magnifier which allows brightness to be maintained at lower current consumption.
Sinclair guarantee an accuracy of better than one second per day. In principle, depending upon the precision to which the quartz crystal is trimmed, the watch is capable of maintaining time to within one or two minutes per year.

The watch comes complete with a black nylon reinforced polyurethane strap.

In kit form, price $£ 17.95$, the Sinclair digital watch appears likely to offer little problem to the average constructor. (We hope to include a review of assembling the watch in a future issue.)

## POWER SLAVES

It is at this time of the year that one starts to worry about the problems of winter and tries to prepare for the likelihood of any possible industrial unrest and service breakdowns.

With this in mind Jermyn's seem to have timed the launching of their new range of excellent invertors at the most opportune moment. These new invertors now use silicon transistors throughout their range. They claim this increases their reliability and back their claim with a one year guarantee.

Two versions are a vailable, type 150-3 with a load of 150 W powered from a 12 V car battery and a 300 W version, type $300-3$, powered from two 12 V car batteries.

A feature of the invertors is that if you are not at home when the mains faiis, the unit will automatically switch over to battery operation. The average running time for battery operation is 3 hours, depending on load. When the mains is restored the units automatically switch back to stand-by operation and recharge the battery.

Apart from lighting other typical applications are: running central heating (pumps and thermostats); tropical fish tank heaters; powering professional equipment, dentist
drills and telex machines, etc.; and office calculators and typewriters. Also the units are ideal for running any normal household mains equipment such as power drills, television and radio. For outdoor use when camping, caravaning or boating the invertors are invaluable.

Further details and prices can be obtained from Jermyn Manufacturing, Sevenoaks, Kent.

## CAR RADIO

Claimed as the first all British designed and built car a.m./f.m. stereo radio, the Radiomobile 1190FMS features an interference rejection circuit module in the f.m. stereo tuner. Known as AIR, active interference rejection, this module is their latest development in combating the problem of interference.

The set has an output of 5 W per channel with a bass/treble tone control. The six button tuner, combined with manual tuning, permits simple pre-setting of any three f.m., twwo medium and one long wave stations. The tunning ranges cover $87.5-104 \mathrm{MHz} \quad$ f.m., $\quad 525-1620 \mathrm{kHz}$ m.w. and $150-275 \mathrm{kHz}$ l.w.

Provision is provided for a tape input with a sensitivity of 30 mV for 5 W output per channel. In this connection Radiomoble are planning to introduce a "tape mate" at a later date.

No price has been announced for the 1190 FMS but further details can be obtained from Radiomobile Ltd, Goodwood Works, North Circular Rad, London, NW2 7JS.


Sinclair "Black' Watch"


The 1190FMS a.m./f.m. stereo radio from Radiomobile


Jermyn 300W invertor

## DIGITAL CAPACITOR METER

A new digital readout capacitance meter, type DCM 302, is announced by Aim Cambridge Ltd.

The meter automatically ranges over 6 decades of measurement, from 1999 pF to $19.9 \mu \mathrm{~F}$ full scale, and the $3 \frac{1}{2}$ digit seven segment display gives a resolution of 0.05 per cent of reading.

Designed for ease and speed of operation, no complex nulling or other adjustments are required, the only control is a touch pad which is used to initiate a measurement. If powered by batteries the meter automatically switches off after 10 seconds. Two 9V (PP3) high power batteries give a typical operating life of at least 6,000 measurements. A mains power pack is available.

The DCM 302 is of British design and is available direct from Aim Cambridge Ltd., Nuffield Road, Industrial Estate, St. Ives, Huntingdon. The price of the meter is $£ 89$.

## BATTERY

A dated battery with a stated shelf life is now being marketed by West Hyde Developments Lid.

Known as the "Wonder Top" each battery is date stamped at manufacture with a guaranteed shelf-life of up to two years. The batteries have a plastics/cap which operates a break-off cover protecting them against unwanted discharge. The protective cap is unscrewed for testing but is overscrewed to break the seal to allow installation in equipment.

Ideal for all types of battery operated equipment the batteries are claimed to give excellent performanice. For instance, the TOP 20 (HP20 etc.,) has a short circuit current of 6 A . A maximum electrical capacity of 7.8 Ah with a power of 2.5 W . Tested to the C.E.I. intermittent 5 ohm load (4 hours a day) the life is over 20 hrs to a voltage of 1 V , at 40 ohms this rises to 190 hrs .

The smallest of the three batteries offered, a pen cell, provides a 1.5 Ah maximum with a short circuit current of 3 A .

Full technical details of the complete range and addresses of nearest stockists can be obtained from West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middx, HAS INN.

## SWITCHES

A range of fire resistant plastics encapsulated rotary switches is now available from Lorlin Electronic Ltd.

These switches, type CK, are available in 1, 2, 3 or 4 -pole versions with 30 degree indexing up to 12 positions single pole. An adjustable stop allows the number of ways to be selected to individual requirements.
The silver plated brass contacts are rated at 150 mA at 250 V a.c. $/$ d.c. and 350 mA at 110 V a.c. $/$ d.c.

Further information on the complete range of Lorlin switches is available from Lorlin Electronic Co. Ltd., Daux Road, Billingshurst, Sussex.

"Wonder Top" batteries from West Hyde

Lorlin CK Rotary switches


## IN BRIEF

To coincide with the opening of two new audio shops in Reading and Notting Hill Gate, London, Henry-Lindair announce an audio part exchange scheme.

Customers who take their old equipment to any Henry's-Lindair store will, in future, be able to obtain a trade-in allowance which can be set against the purchase of new equipment from that particular store. The trade-in item is passed to the Service Department where it is tested and overhauled.

All selected trade-in items are then sold through one of the groups newly established "Bargain Centres" in Edgware Road, and Tottenham Court Road, Lonḍon, with a three month guarantee.

We understand that A. Marshall (London) Ltd. have signed an agreement to supply ITT Semiconductors components to both the trade and the amateur.
Initial stocks will mainly be confined to products such as transistors, diodes, and rectifiers, together with selected specialist integrated circuits for tele vision and other applications.
ITT Semiconductors manufacture specialised i.c.s. with applications in areas such as remote control, hi fi, clocks, watches and automobiles and Marshall's hope to introduce selected items and kits from this range into the consumer and amateur markets in the near future.

A new 24 -page MOS products catalogue entitled "It's Standard at AMI" has just been published by AMI Microsystems.

This short form catalogue is an up-to-date listing of all current, recently introduced and future AMI products. It includes sections dealing with micro-control systems, microprocessors, memories, interface circuits, communications modules, wristwatch, clock, calculator and electronic organ circuits and liquid crystal displays.

Copies of the catalogue can be obtained from AMI Microsystems Ltd., 108a, Commercial Road, Swindon, Wilts.

For readers interested in Disco equipment, Saxon Entertainments Ltd. have released brochures on their System 7000 sound and light modules.

Included amongst their amplifiers, mixers and lighting units is a Sound/Lite Sequencer capable of handling up to 1000 W per channel.

Copies of the brochures are available from Saxon Entertainments Ltd., 327-333 Whitehorse Road, Croydon, Surrey.

## NOTE

We regret that an incorrect address for Barclay Electronics was given last month. This should be: Barclay Electronics, 1115 Finchley Road, London, N.W.11.

Digital capacitor meter type DCM302 from Aim Cambridge



#### Abstract

This series of articles will acquaint the reader not only with the basic characteristics but also the practical applications of CMOS as succeeding parts will give tested circuits with full description of operation.

Readers who have never used any logic lamily, either due to lack of funds or lack of confidence will find CMOS an excellent introduction as it is well sulted to the experimenter. Its microwatt power consumption, single supply operation from non-regulated 3 to 15 V supplies, high noise immunity, abilitles to switch analogue signals and operate as high gain linear amplifiers are all qualities which make it Ideal for this role. Readers who have never used any operation.


THE first commercial complementary MOS device was shown by RCA in March 1967 at the New York IEEE show. The CD4000 range was launched the following year and by 1971 a wide range of plastic packaged devices with operation from 3 to 15 V was available. This was the year that cmos finally evolved into a fully-fledged rival to other logic families with Motorola announcing proprietary products of its own-the MC14500 series. The following years have seen a phenomenally rapid growth both in the range of devices and usage.
Prices have steadily fallen until, in the last year they have literally tumbled to, in many cases, below TTL prices. The one-off price of a 4 -gate package is now 17 p , while mSI packages which would require two TTL packages show a considerable price advantage. This year, despite the recession, RCA, which has a 40 per cent share of the cmos market, intends to introduce a further 40 new CD4000 series devices. This will bring the total number in the series to 182 .

## DEVELOPMENT

For a long time bipolar TTL has been the standard medium-speed logic family. In the last few years mos (metal oxide semiconductor) technology has made possible the fabrication of the high-density calculator, clock and, more recently, microprocessor integrated circuits.

It is the complementary form of mоs-смоsthat has developed into a comprehensive logic family with a number of significant new features that offer a serious challenge to tTL.
mos i.c.s are those fabricated entirely from mos field-effect transistors or mosfets. Basically a MOSFET consists of a metal gate electrode insulated from a channel of silicon by a thin oxide layer. It is this metal oxide semiconductor sandwich that gives the technology its name.
The channel is doped with one polarity and two other electrodes are formed by troughs of opposite polarity on each side of the gate. These are called the drain and the source. Two types are possible: an $n$-type or a $p$-type, according to the doping of the channel.

## MOSFET AS A SWITCH

The mOSFET behayes as an excellent switch, since when the gate voltage is raised to a critical level (known as the threshold voltage) the device switches on and current flows between the source and the drain. This gate voltage induces a change of polarity in the material under the gate, i.e. the channel, so that with an $n$-type a positive switching voltage is needed on the gate, and similarly a negative voltage with a $p$-type. Since the gate is electrically insulated from the silicon, MOSFETS have input impedances of the order of $10^{12}$ ohms (one million megohms). Therefore, to all intents and purposes, no current flows in the gate circuit, and switching is achieved by electrostatically induced charges.

## MOSFETs AS LOGIC ELEMENTS

Now the question arises-how are these basic electronic switches used to build logic elements? A pMOS inverter is shown in Fig. I.1(a); a low input
(below the threshold voltage) produces a high output and vice-versa.
Suppose we require the output to go high when any one of a number of inputs is low. The circuit of Fig. 1.1(b) satisfies this requirement, and its pmos equivalent is a 3 -input NOR gate. In other words the output is high if "NOT (A OR B OR C)".

## PMOS AND NMOS

In practice the resistor is replaced by a second $p$-type MOSFET which is biased on by a second supply line of about twice $\mathrm{V}_{\mathrm{ss}}$. This is called $\mathrm{V}_{\mathrm{kg}}$ since it is connected to the gates of the load devices. The resulting pmos inverter is shown in Fig. 1.1(c). In the on state a single pmos inverter has a significant power dissipation of about 10 mW .

The great advantage of PMOS is that very high packing densities can be achieved on a single chip since each gate is extremely simple. The disadvantage is the power dissipation-a typical clock chip consumes about 10 mA , as much as one of the displays it is driving. Furthermore, two power supply rails are generally needed and the speed of operation is fairly low.

Integrated circuits made entirely with $n$-channel mOSFETS give a greatly improved performance and density, but until recently, the inherent fabrication difficulties have prevented NMOs from being a viable production technology. Now that these difficulties have been resolved, NMOS is making possible a whole
new range of high speed, high density memories and microprocessors.

## COMBINING BOTH TYPES

A third way of using mOS is to combine $p$-type and $n$-type mOSFETS on the same chip. The formidable fabrication problems involved, especially at high production levels, were overcome by RCA by the late 1960 s . The inverter now becomes a $p$-type and an $n$-type connected in a complementary-symmetry (hence RCA's trade name cosmos) push-pull configuration across the supply rails. The gates are connected together to form the input-Fig. 1.1(d). The d.c. power dissipation of the PMOS inverter is now reduced virtually to zero, being a product of the nanowatt leakage current of the mosfers.

A new general purpose logic family was born. Its great versatility and unique features account for the fact that it has reached its present maturity in such a remarkably short time.

## MARKET GROWTH

RCA market the family as the CD4000 series with the trade name cosmos, and there are at present more than 140 devices in the family. The first major manufacturer to second-source the 4000 series was Motorola in 1971, using the trade name mсмоs. At the same time Motorola introduced devices of their own design, designated the 14500 series. Today there are more than a dozen suppliers with the latest


Fig. 1. 1(a) Operation of a p-type mosfer with load resistor as an inverter; (b) Implementation of a 3-input NOR gate; (c) Standard pmos inverter with load resistor replaced by a $\boldsymbol{p}$-type MOSFET; (d) cmos inverter consisting of an $\boldsymbol{n}$-channel and a $\boldsymbol{p}$-channel device connected in push-pull. When one device is on, the otheris off. This eliminates the high d.c. power dissipation of the PMOs inverter and requires only a single supply


Fig. 1.2. Typical cmos structure, showing a p-channel and an $n$-channel device diffused on the same substrate
entrant to the market being Philips with an initial introduction of 354000 and 4500 series cmos parts.

## CMOS FABRICATION

A cross section of the basic cmos element, a $p$-channel and an $n$-channel device on the same substrate is shown in Fig. 1.2. The starting substrate is made of $n$-type silicon into which is diffused a well, forming a $p$-type substrate for the $n$-channel transistor. Each substrate then has $p$ or $n$-type pockets diffused to form the sources and drains of the $p$ or $n$-channel transistor.

Protective guard bands are also diffused around the $D$ and $n$-type transistors, of opposite polarity to prevent leakage between the two types of device. The process generally requires seven masking steps, the last being to form the aluminium metallisation etched to form the appropriate circuit interconnections.

In spite of all this, cmos circuits have a much higher packing density when compared with bipolar


Fig. 1.3. Power versus speed comparison for cmos, pmos and trt. Power consumption of cmos approaches that of TTL at high speed, but at 1 kHz is only $1 \mu \mathrm{~W}$
technology. Less chip area is required per function through the elimination of resistors and capacitors and the extremely low power dissipation.

## INVERTER STATIC OPERATION

As mentioned, one of the basic building elements of cmos i.c.s is the complementary inverter. The $n$-channel device is connected to the negative supply and the $p$-channel device to the positive rail. When the input is at the negative supply potential, the $n$-channel device is off and appears as a resistance of several thousand megohms. The p-channel device is at the same time on and has a resistance of about 750 ohms. The output of the inverter is thus clamped to within a few millivolts of the positive supply rail.


Fig. 1.4. Switching characteristics of cmos, pmos and TTL. cMOS approximates far more closely to the ideal switch

Equally when the input to the inverter is at the positive rail, the output is virtually at the negative rail. In either state the static power consumption is of the order of a few nanowatts only.

The mosfets of the inverter have threshold voltages of around 45 per cent of $\mathrm{V}_{\text {DD }}$. This gives the inverter its highly symmetrical switching characteristic, coupled with high noise immunity. The transfer characteristic approaches that of an ideal switch more closely than that of any other inverter configuration--Fig. 1.4. Allowing for production spreads in threshold voltages, the guaranteed d.c. noise immunity is usually 30 per cent but will typically be 45 per cent of $\mathrm{V}_{\mathrm{DD}}$. Thus at a supply voltage of 5 V , the noise immunity will be about 2 V . This means that, as well as having a high immunity to input noise spikes, cmos does not require wellregulated power supplies. Simple RC smoothing is often all that is required.

## POWER DISSIPATION

Since the supply voltage is greater than the sum of the threshold voltages, both of the devices will be on simultaneously as the inverter switčhes during a transition of 10 per cent of $\mathrm{V}_{\mathrm{DD}}$. This causes a peak of current to be drawn from the supply. However, the majority of the dissipation does not come from the resistive flow through both the partly on transistors, but from the charging and discharging of stray and load capacitances.
The output is held at very nearly $\mathrm{V}_{\mathrm{SS}}$ or $\mathrm{V}_{\mathrm{DD}}$ during this simultaneous conduction period and the current is diverted to the capacitance itself. Thus the switching power dissipation of the смоs inverter is almost entirely due to capacitive loading and the more frequently the inverter passes through this mid-point region the higher will be the power dissipation until, at 10 MHz , it reaches that of TTL (Fig. I.3).

So in order to realise the micropower operation of cmos the operating frequency should be kept low. While the смоs inverter shows an idling or quiescent power dissipation, $\mathrm{P}_{0}$ of the order of nanowatts, when switching the power dissipation, $\mathrm{P}_{\mathrm{I}}$, is given by $P_{D}=P_{0}+C_{L} \cdot V_{D D}{ }^{2 \cdot f}$ (where $f$ is the operating frequency).

## OPERATING VOLTAGE RANGE

As we have seen the cmos inverter operates from a single supply (Fig. 1.1). Thus $\mathrm{V}_{\mathrm{SS}}$ is 0 V when the input swing is positive. However, if it is also negative, then $\mathrm{V}_{\mathrm{Ss}}$ must be negative by at least the same amount. Standard смоs devices operate from 3 to 15 V , with an output logic swing within a few millivolts of the supply rails.

## HANDLING AND USAGE

The extremely high input impedance of mos allows electrostatic charges to build up which could easily puncture the very thin input gate oxide layer. Present day cmos devices are pretty thoroughly protected against such charges by diode-resistorcapacitor input networks and, provided simple earthing precautions are taken, devices can be handled quite safely.

One precaution, however, must be emphasised. Devices can be destroyed when driven by low impedance sources, such as a signal generator or even the outputs of other cmos devices, if the $V_{\text {DI }}$, supply is disconnected. In this case one of the protective diodes may become forward biased causing possible damage to the diode or the input metallisation.

## UNUSED INPUTS

All unused inputs should be connected to one or other of the supply rails, as appropriate. Floating inputs not only waste power but can cause erratic operation of the rest of the device. The outputs of most devices are virtually short-circuit proof. This is because of the inherent current-limiting characteristic of the complementary inverter, whereby the output current is limited to one or two milliamps. The only restriction is that the total package dissipation of 200 mW should not be exceeded.

Next month: The other basic element from which CMOS i.c.s are built; the transmission gate. Also included are practical CMOS circuits.

## GUITAR AMPLIFIER

continued from page 30


The voltage reading at the output socket (SK3) should be almost zero. On the prototype this reading was minus 200 millivolts.
Swith off and replace FS1 with an ammeter. Switch on and measure the quiescent current. It should be in the order of 20 milliamps.
If all the above tests have been successful, a suitably rated 8 ohm loudspeaker can be connected and the amplifier tested with an input signal such as from a signal generator (if available-in which case further tests can be carried out) or from a guitar pick-up, microphone or eletronic organ.

Check the performance of the volume controls by slowly turning them clockwise to increase the volume. Clockwise rotation of the treble and bass controls should boost treble and bass frequencies.

## CASE

Construction detaits of the amplifier case as used in the prototype are given in Fig. 12. The material used was 12 mm thick blockboard, glue and nails being suitable for the butt joints. The inside front was faced with 10 mm quadrant glued and nailed all round, with mitred joints.
Two holes need to be drilled on the underside to align with the chassis fixing nuts, through which two 25 mm long 2BA bolts fitted with large washers will hold the chassis assembly firmly in position agaiast the quadrant facing.

Thoroughly sand down and fill in any indents there may be in the finished case and paint or cover the case as required. Black Rexine was used on the prototype case and glued on using pearl/crystal glue. To finish off, fit four rubber feet and a snapback flush carrying handle on the top, see photographs.

# SMIEDNOUTIDR <br> UPDAIIE Bosmenese 

| ULN2275 | AY-3-9400/10 |
| :--- | :--- |
| ULN2277 | M142 |
| ULX2276 | ILQ74 |

## STEREO TRIO

If you're like me, its possible that you sometimes wonder whether the integrated circuit manufacturers do not so much make the little blighters, as breed them! I must confess to having taken these suspicions a little further than reasonably necessary, because I once imprisoned a couple of 741 op-amps in a matchbox, just to see what would happen.
Well, to cut a long story short, I never actually caught them at it, and not so much as a bonny bouncing quad two $\mathrm{i} / \mathrm{p}$ nand gate ever resulted, but I still have nagging doubts, and these have been aroused once more by a.trio of new devices from Sprague.
If I'm wrong and Sprague actually do make i.c.s, they're doing a grand job, because these three new chips form a closeknit little family which promises to make audio amplifier problems a thing of the past. The type numbers are ULN 2275, ULN 2277 and ULX 2276, and each of these handy little 14 -pin i.c.s contains not one, but two audio amplifiers, each with an impressive specification

You may think that putting two audio amplifiers in one d.i.l. package will mean that their output power capability must be very restricted, but this certainly isn't so. The 2275 gives a creditable 1W per channel ot continuous power over a supply voltage range of from 9 to 20 V , for only 28 mV of signal input. The 2277 is even more powerful at 2 W per channel, and the 2276 (which is still undergoing evaluation tests) promises an incredible 4 W each side, making it a definite candidate for the Guinness Book of Records!

These powertul devices don't necessarily need special heatsinks either, since they can dissipate the heat, via their tabs, to the copper areas of the p.c.b. A trio of real thoroughbreds in fact!

## PHONE TONES

You may remember that I recently featured the Plessey MP 9100 dial code generator (October '75), which is intended for use with Strowgertype telephone systems. In the MP 9100, dialled digits are sent out as a series of slow on/off pulses to activate stepping uniselectors at the exchange. This is not the only
system in use for telephone dialling, and a new chip from General Instrument, the AY-3-9400, demonstrates the other point of view.

Like the MP 9100, the AY-3-9400 is intended for use with push-button telephones, but instead of sending out a string of pulses for each digit, the new chip sends out a pair of m.f. tones. The push buttons on the telephone instrument are arranged as a key-pad, or matrix, and when a single key is depressed, two signals, one tor the row position and one tor the column position, are generated. If the key-pad has 4 -rows and 3 -columns (i.e. 12 keys) it is possible to allocate a unique tone pair from seven basic tone generators.
The AY-3-9400 generates seven accurate tone frequencies between $695 \cdot 28 \mathrm{~Hz}$ and $1,631 \cdot 78 \mathrm{~Hz}$, and is controlled by a 559.7 KHz ceramic resonator (or crystal) external to the chip. The chip is made with an $n$-channel ion-implant m.o.s. technology which ensures operation from a single low voltage supply.
The operation of the circuitry is mainly digital, consisting of some keyboard logic, two` programmable prescaler counters to generate the necessary frequencies from the main clock oscillator, and two digital to analogue converters to give a fair approximation of a sinewave for each m.r. tone.

Now, I don't suppose that anyone is thinking of going into competition with the Post Office by providing an alternative telephone system, but this new device could be used for many other things besides. An obvious use is as a remote control tone generator for an ultrasonic or radio link, perhaps to control a T.V. set or model.
The 9400 comes in a 14 -pin package, but if seven tones and 12 key positions aren't sufficient for your needs, there is the 9410 version which handles 16 keys with eight tones and comes in a 16 -pin pack.

## BIGSHIFT

If you dabble in t.t.l. logic (and who doesn't) you may have occasionally cast envious glances at some of the logic power available in the more exotic m.o.s. technology. If you
have ever wanted a long shift register, for example, the prospects for building it with t.t.I. are a bit bleak, since an eight bit device is about the biggest available.
With $p$-m.o.s. on the other hand, registers very much longer are commonly available, but unfortunately they don't help much, because to put a p-m.o.s. register in a t.t.l. system often means extra power supplies and special interface circuits which makes the m.o.s. solution about as broad as it is long (no pun intended!).
Thanks to the relatively new $n$-m.o.s. technology, however, the mixing of m.o.s. power with t.t.l. versatility has now become a real possibility, even tor small amateur projects. Take, for example, the SGS-ATES M142 quad 80-bit static shift register (yes, that's right, four 80 -bit shift registers in a 16 -pin d.i.l.!). This common or garden $n$-m.o.s. device is fully t.t.l. compatible on all inputs and outputs, and even works from the standard +5 V t.t.l. supply rail. The data in the register can remain static if required, or can be shifted at a clock rate of up to 3 MHz .
Four 80 -bit registers in parallel could be used to store 80-b.c.d. digits (0-9) and so could provide a powerful but simple data storage system for many kinds of digital projects.

## QUAD COUPLER

Opto-couplers consist of an l.e.d. in close proximity to a photo diode or transistor, the whole thing being sealed in a small plastic or hermetic package. Input signals to the l.e.d. cause a light output which is sensed by the photo diode or transistor to produce an output. The name of the game is isolation, and by using light as the coupling medium, isolation resistances of 100 megohms and breakdown voltages of over $1,000 \mathrm{~V}$ can be achieved.

All this is history, but Litronix have recently introduced a new i.c., the ILQ74, which consists of no fewer than four opto-couplers in a single 16 -pin d.i.l.! Applications include thyristor triggering, high voltage stabilised power supplies and signal isolation circuits, with inputs and outputs being t.t.l. compatible.


PRACTICAL

## Now...the most exciting Sinclair kit ever

## The Black Watch kit

 At £17.95, it's * practical-easily built by anyone in an evening's straightforward assembly. * complete - right down to strap and batteries.* guaranteed. A correctlyassembled watch is guaranteed for a year. It works as soon as you put the batteries in. On a built watch we guarantee an accuracy within a second a day-but building it yourself you may be able to adjust the trimmer to achieve an accuracy within a
 second a week.



## The special features of The Black Watch

Smooth, chunky, matt-black case, with black strap. (Black stainlesssteel bracelet available as extrasee order form.)


Large, bright, red display-easily read at night.
Touch-and-see case-
no unprofessional buttons.


Runs on two hearing-aid batteries (supplied). Change your batteries yourself-no expensive jeweller's service


## The Black Watch-using the unique Sinclair-designed state-of-the-art IC.

The chip...
The heart of the Black Watch is a unique IC designed by Sinclair and custom-built for them using state-of-the-art technologyintegrated injection logic.

This chip of silicon measures only $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ and contains over 2000 transistors. The circuit includes
a) reference oscillator
b) divider chain
c) decoder circuits
d) display inhibit circuits
e) display driving circuits

The chip is totally designed and manufactured in the UK, and is the first design to incorporate all circuitry for a digital watch on a single chip.
...and how it works
A crystal-controlled reference is used to drive a chain of 15 binary dividers which reduce the frequency from $32,768 \mathrm{~Hz}$ to 1 Hz . This accurate signal is then counted into units of seconds, minutes, and hours, and on request the stored information is processed by the decoders and display drivers to feed the four 7 -segment LED displays. When the display is not in operation, special power-saving circuits on the chip reduce current consumption to only a few microamps.


## Complete kit STAF

## The kit contains

1. printed circuit board
2. unique Sinclair-designedIC
3. encapsulated quartz crystal
4. trimmer
5. capacitor
6. LED display
7. 2-part case with window in position
8. batteries
9. battery-clip
10. black strap (black staiñless ${ }^{-}$ steel bracelet optional extrasee order form)
11. full instructions for building and use.
All you provide is a fine soldering iron and a pair of cutters. If you've any queries or problems in building, ring or write to the Sinclair service department for help.

Take advantage of this no-risks, money-back offer today!
The Sinclair Black Watch is fully guaranteed. Return your kit within 10 days and we'll refund your money without question. All parts are tested and checked before despatchand correctly-assembled watches are guaranteed for one year. Simply fill in the FREEPOST order form and post it-today!
Price in kit form: £17.95 (inc. black strap, VAT, p\&p).


Sinclair Radionics Ltd, London Road, St Ives,
Huntingdon, Cambs., PE17 4HJ.
Tel:St Ives (0480) 64646.
Reg. no: 699483 England. VAT Reg. no: 213817088

To: Sinclair Radionics Ltd, FREEPOST, St Ives, Huntingdon, Cambs., PE17 4BR.

Please send me
(qty) Sinclair Black Watch kit(s) at £17.95 (inc. black strap, VAT, p\&p)
(qty) black stainless-steel bracelet(s) at £2.00 (inc. VAT, p\&p).

Total £

* I enclose cheque for $£$
made out to Sinclair Radionics Ltd and crossed
*Please debit my*Barclaycard/Access/ American Express account number

[^2]
# ITHIT IDAT BH:HER 

Several devices have recently appeared on the market which display the logic conditions of an incircuit i.c. upon a matrix of light emitting diodes. These devices cost about $£ 30$ and while they are of sophisticated design, they are out of the reach of many amateurs' pockets.
The device described below can be built for under $£ 4$ and, in the author's opinion, the lack of sophistication is more than balanced by the difference in cost.
Power for the logic checker is taken directly from the i.c. under test so that separate batteries are not required. High and low logic levels and the power supply are indicated by appropriate l.e.d.s being activated; the l.e.d. position indicating the i.c. pin in question. The checker can be used to display the logic states of any integrated circuit having up to 16 dual-in-line pins at a $0 \cdot 1$ in pitch.

## THE CIRCUIT

The circuit consists of a pair of electrical pathways between each pin connection and a common rail (see Fig. 1). Only one of each pair is open to current, the other being blocked by a diode or light emitting diode.

In order to demonstrate the circuit function in greater detail, the following assumptions are made for Fig. I: pin 16 is at logic level I, pin 15 is at logic level zero and pin I is ground or negative supply


Fig. 1. Four of the 16 networks needed

## COMPONENTS

## Resistors

R1-R16 $470 \Omega$ (16 off)
All $5 \% \frac{1}{⿱ ㇒ 日}$
Diodes
D1-D3-D5-D7-D9-D11-D13-D15-D18-D20-D22-D24-D26-D28-D30-D32 All RL54 l.e.d.s (A Marshall Ltd.)
D2-D4-D6-D8-D10-D12-D14-D16-D17-D19-D21-D23-D25-D27-D29-D31 All OA200

## Miscellaneous

Veroboard, edge connector contacts, plastic case, scrap perspex sheet

Conventional current flow will proceed from pin 16 to pin 1 via D18, R16 and D2; its passage along the alternate route being blocked by D17 and D1. D18 will be activated by the passage of current and the positive voltage on pin 16 will be indicated. Resistor R16 limits the current flowing in D18. In practice, some current will also flow from pin 16 to pin 15 via D18, R16 and D19.

Pin 15 is assumed to be at logic zero and will thus have a voltage of between zero and 0.4 volts; this is too low a voltage to overcome the forward voltage threshold of the l.e.d. and diode which lie in its path to ground. (In exceptional cases, the two thresholds may be overcome and a small but insignificant current will flow.)

In considering all 16 circuits networks, some current will flow between pins at logic level 1 and those at logic level zero as well as the ground pin. However, these do not upset the functioning of the circuit.

The positive supply pin is treated as a pin at logic level 1 and is also displayed by an illuminated 1.e.d. in the appropriate position


Fig. 2. Constructional details of the Digital Logic Checker


## CIRCUIT AND DISPLAY BOARD

A 16 by 12 hole piece of Veroboard of 0.1 in pitch is used for the circuit. Layout and the positions of the cuts in the copper strips are shown in Fig. 2. The resistors are mounted first followed by the diodes and, finally, the light emitting diodes. Care should be taken to avoid overheating the diodes and, particularly the 1.e.d.s which are very small and therefore particularly sensitive. The resistors are mounted vertically while the diodes are soldered in a horizontal position. The 1.e.d.s are mounted so that the plastic lens part is above the diodes and about on a level with the top edge of the resistors.

## THE SPRING CONTACT BOARD

A second piece of Veroboard is used for the base. The pitch is, again, $0 \cdot \operatorname{lin}$; with ten copper strips and six rows of holes. The outer two copper strips are scraped off with a sharp knife. The 16 spring contacts are fashioned from the individual contacts from an edge connector and soldered into the Veroboard, slight widening of the Veroboard holes with a knife will allow the contacts to be eased in without their bending. The sequence of operations for making the contacts is shown in Fig. 2; the gold plated contacts make excellent prongs for this project and, being individually sprung, they allow all 16 contacts to slide tightly over the i.c. pins.

It is important that the tips of all the contacts are arranged at the same height, alterations to the angle at which each contact is soldered can be made by bending each one slightly until they are all in line.

Flying leads of thin stranded wire are used to connect the two Veroboards together. In both cases the leads are attached on the copper side of the Veroboard.

Fourteen to 16 pin i.c. test clips are available from Guest Electronic Distribution Ltd. While this component would make a much more professional job of the i.c. contact assembly, the cost would increase by over 50 per cent and the case would require a different design.

## TESTING

A four and a half volt battery, or other power source, can be used for testing. Briefly touch the battery contacts against any of the spring contacts and, wherever the positive supply touches a contact, the appropriate l.e.d. should light. Faults may be due to
crossed leads, damaged l.e.d.s or diodes and l.e.d.s being connected in reverse.

## THE CASE

The shape of the case has been chosen to provide a convenient hand grip and a small sized base. The small base and tapering shape allow it to be inserted onto an in-circuit i.c. without interfering with neighbouring components.

Aluminium was chosen as the material but, because of the small size of the case, it is difficult to bend a single piece of aluminium at the necessary points. In order to avoid this difficulty, four separate pieces of aluminium were cut, bent and glued together with Araldite, the areas of metal covered by the glue being well roughened to give good adhesion. Fig. 2 shows the separate aluminium pieces and their assembly into a somewhat coffin-shaped box.
The display area where the l.e.d.s are viewed is covered by thin Perspex. Araldite is not recommended for securing Perspex and Evostik was used for this operation.

The small base end of the case is cut to provide a hole for the spring contacts to protrude through and this piece of Veroboard is secured into the base with generous amounts of Araldite. The copper strip side of the Veroboard is also smeared with Araldite to reinforce the soldered joints of the spring contacts.

The circuit and display board is fitted behind the Perspex window and wedged into position with small scraps of foam plastic. It is advisable to insulate the interior of the case with insulation tape to ensure that accidental shorting of the display board does not occur.

## USING THE LOGIC CHECKER

In use, the spring contacts are pushed over the operating i.c. to be tested, care being taken to ensure that the spring contacts do not bridge the small gaps between the i.c. pins.

The l.e.d.s on the display board will now glow and indicate the positive supply pin and those pins which are at logic level 1.

The constructor should be warned that where i.c.s are being used with capacitors, for instance, where gates are cross coupled to form an astable multivibrator, the checker will disturb and may freeze the circuit action. This is because alternative charge/discharge paths are set up through the checker which will significantly alter the time constants in the circuit.

At a nominal supply voltage of 5 volts, each 1.e.d. is limited to a current of about 10.5 mA by the series resistor. The l.e.d.s are quoted as a 40 mA device but the reduced current is still sufficient to provide a light output which can be easily seen in most conditions. Most d.i.1. i.c. devices can provide a logic 1 output of 160 mA , quite sufficient to power the checker. If an operating i.c. is already approaching its maximum fan-out (usually 10) it is a wise precaution to disconnect some of the devices being fed from the well loaded gate outputs before using the checker.

If two sewing pins are cut to about 5 mm length, heated and pushed into the Perspex window at either end, these can be used for attaching a piece of card or stiff paper. The block diagram of the i.c. can be sketched on the card with the input/output lines to each gate drawn to each l.e.d. The logic levels for each gate can then be seen with ease.


## OUTLOOK '76

The Autumn season of electronic exhibitions and a few company reports and news items gave forecasters for ' 76 little on which to base firm conclusions because the general economic outlook was, and is, filled with uncertainties.

Consumer electronics is still in the doldrums. Colour TV deliveries last August, for example, were 36 per cent down on the previous August. And, because of this, component suppliers really suffered. AB Electronic Components reported a heavy drop in volume of components supplied although inflation kept turnover at $£ 11.15 \mathrm{mil}$ lion compared with $£ 12.05$ million a year earlier.

Profits were down from a pretax figure of $£ 908,063$ to $£ 379,205$ reflecting lower margins. On the other hand $A B$ went ahead with a heavy investment programme showing confidence in the future but at the same time stated that more emphasis is being placed on business outside the area of consumer products.

Erie Electronics also suffered from the consumer slump and the sale of the UK operation to ITT Components Group Europe should be established, according to industry sources, by early in the New Year if not before.

Decca's big interests in TV. radio, audio and records, showed a decline in pre-tax profits from $£ 10.9$ million to $£ 6.8$ million but the balance was redressed by the radar, navigation, and other professional capital goods output which showed an increase in profit from $£ 6.7$ million to $£ 9.1$ million.

Fortunate indeed are those companies strong in capital goods. EMI Electronics has to thank its world-beating EMI-Scanner X-ray
equipment for a doubling in profit from $£ 7$ million to $£ 14.6$ million. The total order book for these machines has now topped 300, worth some $£ 60$ million. And as there is no competition there is a handsome profit on every delivery. Strange to say, this project was nearly abandoned at one stage.

If we look across the Atlantic, the Wescon show in San Francisco last September was full of optimism with strong support for the view that business was on the upturn although some cautious opinions were expressed that it would be a long haul and positive results may not be apparent before mid'76. European electronics would follow on, it was said, with a time lag of seven to eight months.

In Britain, the Internepcon/UK ' 75 show held in October'was the biggest ever and one of the busiest. The show concentrates on plant and equipment for electronics manufacture and there was plenty of evidence that manufacturers are investing now for future production. Perhaps not as heavily as they should in some cases, but there was movement and that's better than nothing.

The immediate outlook, then, is for consumer electronics to remain depressed but for capital goods to do well, especially in the export market where, with a devalued pound, British goods are very competitive.

## MOBILES AND PAGING

Every cloud has a silver lining. Vandalism and terrorism on London's famous double-decker bus fleet has brought Redifon Telecommunications back into mobile radio. The company has an initial order for 200 radiotelephones to enable bus crews to call for help if need be.

Apart from ordinary two-way telephony there will be a number of strategically sited emergency buttons on the bus which actuate an auto-alarm. But later, the sets will also be used for data transmission as part of a new scheme being introduced for en-route control of the fleet.

Pocket radio paging is to go ahead in the London area under a Post Office scheme due to start next Spring. This follows on from field trials in the Reading area. The Post Office expects to aet 20.000 subscribers initially and each one, of course, will need to be supplied with a pocket "bleeper" which will respond to a radio signal personally coded.

On the Reading trials the Post Office used pagers manufactured by Motorola. But for the London scheme they have ordered 10,000 units from the British company Multitone at a reported contract price of $£ 1$ million.

The Multitone equipment has already been proved in service in wide area paging systems in Toronto and Ottawa. One of its features is a muting switch which cuts out the "bleep" and stores the signal in a memory circuit. The user can access the memory to see if he has been paged when it is convenient for him to do so.

The use of the mobile radiotelephone continues its upward growth almost unnoticed. In 1971 there were 90,000 licences issued. Today there are some 200,000 mobiles operating in the UK including a staggering figure of 50,000 within a 50 -mile radius of Central London.

## REMSCON

A little-publicised sector of industry emerged into prominence in November with an international gathering of industrial telemetry experts for a three-day conference in London. The event was REMSCON with a strong panel of speakers led by conference chairman Professor H. C. A. Hankins of the University of Manchester Institute of Science and Technology.

The big users of remote control and supervisory equipment are water, gas and electricity authorities and petrochemical companies, with many of the larger systems now being controlled by computer. I hope to comment more fully on this event in a future issue.

## DEFENCE SCENE

Minister of Defence, Mr Roy Mason, is hinting hard at new methods of military procurement. His defence budget is under attack from the left wing of his party and he is now telling industry that he must buy in the cheapest market, even if this means shopping overseas. At the same time, his political colleagues are urging the nation to buy British. The Minister's posture on this occasion was clearly defensive following the cancellation of two British missile projects in favour of U.S. missiles.

Apart from any change in outright purchasing policy there also seems to be a move away from Ministry-sponsored R and D. There is a new tendency to look at PV (private venture) projects for military use and so the old-style development contracts which have kept many a laboratory in funds may soon be a thing of the past. If this is the case and risk capital goes on speculative development. it is bound to be reflected in the final product price and this, in turn, could affect defence exports.

Of course, Ministers don't always say what they mean, or mean what they say, but it is clear that the defence scene will become more intensely competitive.


## An easy-to-build device for the home recording enthusiast

THIS simple audio compressor can be built simply and cheaply, and probably with components from one's spares box. It will compensate for fading signals in a radio, prevent overmodulation of a transmitter and will adjust to whispers or shouts into a microphone.

Its basic function is to maintain a relatively constant amplitude output over a varying range of input amplitudes. Although it will cope with several hundred millivolts input, smaller inputs cause less harmonic distortion (low enough for most applications).

## CIRCUIT OPERATION

The circuit diagram of the compressor is shown in Fig. 1. The signal is first amplified by TR1 in the common emitter mode and then passed on to the next stage via C 4 . Large input signals cause a larger voltage to be induced in the secondary of T1. This voltage is rectified by D1 and reapplied as a negative-going d.c. voltage to the base of TR1, thus lowering the bias voltage and consequently lowe'ring the gain.


Fig. 1. Circuit diagram of the audio compressor


Fig. 2. Component layout and Veroboard cutting details

## TIME CONSTANT

When a small signal is applied though, the gain of this stage rises after about 50 ms (the time constant of C2R3). This time constant should maintain the gain between syllables of speech. It can, however, be easily altered to suit the application by varying either C2 or R3.

## TRANSFORMER

There is much room for experimentation, especially with T1, which must be a step-up transformer and should have impedances approximately as shown. However, an unlabelled driver transformer from an old radio was found to work just as well.

## CONSTRUCTION AND USE

The circuit was built on a small piece of Veroboard as shown in Fig. 2 and the layout is not at all critical.

The author found that when positioned directly after the volume control and before his headphones, the compressor all but eliminated fading in his receiver. It was also found to function well between a microphone and a tape recorder, compensating for varying voice levels and varying distances from the microphone.

## ALTERATIONS

If too large an input signal is applied, the negative a.g.c. voltage can be high enough to cause TR1 to clip the signal. If R2 is increased to $120 \mathrm{kS} \Omega$, apart from increasing the overall gain, it will allow higher input levels to be accommodated before clipping.

For small signals (such as microphone inputs) the original circuit could be used unaltered. A preset potentiometer (about $100 \mathrm{k} \Omega 2$ ) in series with R2 would make the compressor more versatile, however.

## COMPONENTS . . .

```
Resistors
    R1 100k\Omega
    R2 10k\Omega
    R3 1k\Omega-2.7k\Omega (see text)
    R4 470\Omega
    All resistors 10% tW
Capacitors
    C1 5\muF elect.
    C2 }10\mu\textrm{F}-32\mu\textrm{F}\mathrm{ elect. (see text)
    C3 50\muF elect.
    C4 5\muF elect.
    C5 50\muF elect.
    All capacitors 12V
Diode
    D1 OA91
Transformer
    T1 See text
Transistors
TR1 BC108, BC107 or other npm silicon (e.g.
    2N2926, 2N2925, etc.)
    Miscellaneous
    Veroboard (see Fig. 2). Phono socket, case
```


## RANTOMTINF GENERATOR By Ne ciless

THE Random Tone Generator was primarily designed as an electronic door bell which would produce an endless variety of "tunes" at the press of the door switch. Thus the boredom of continual repetition of a single tune along with the difficulty in selection of a suitable tune are removed. However, it is thought that the random tone generator may provide an aid to musical composition as well as providing amusement.
In operation it produces a train of notes which is seldom duplicated and musical interest is maintained by not only changes in pitch but in note duration.

## U.J.T. CLOCKS

The circuit (Fig. 1) uses two unijunction transistors, TR1 and TR2, as relaxation oscillators producing frequencies of approximately 50 kHz and 2 Hz respectively. The 50 k Hz pulses at the base 1 of TR1 are used to clock a decade counter type SN7490. The four output lines (A, B, C and D) are fed to a quad latch where the binary information is periodically sampled and stored. The sampling rate is determined by the oscillation frequency of TR2 and may be varied by means of VR1.


Fig. 1. Circuit diagram of Random Tone Generator

Decoding of the stored binary information is performed by a Nixie tube decoder/driver type SN7441 which provides 10 open-collector outputs. The output transistors of the decoder conduct randomly because of the wide frequency difference between the two unijunction oscillators and the temperature dependence of their frequency determining components.
Anr emitter coupled multivibrator provides a harmonically rich tone from TR4 collector, the frequency of which can be altered by variation of TR3 base voltage. This is achieved by using a potential divider comprising R5 and R6 to R19, the latter being selected randomly by the decoder. The values of R6 to R19 are chosen such that the notes generated correspond approximately to the musical scale over one octave.

Audio amplification is provided by a simple classB push-pull amplifier, TR5, TR6, TR7, driving a 3 ohm speaker. The unit is powered by a 9 volt battery, the 5 volt supply for the integrated circuits being obtained via resistor R27.


Generator housing


Fig. 2. Component layout and wiring details

## COMPONENTS . . .

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $10 \mathrm{k} \Omega$ | R14 | $15 \mathrm{k} \Omega$ |
| R2 | $10 \Omega$ | R15 | $33 \mathrm{k} \Omega$ |
| R3 | $8.2 \mathrm{k} \Omega$ | R16 | $4.7 \mathrm{k} \Omega$ |
| R4 | $100 \Omega$ | R17 | $330 \Omega$ |
| R5 | $4.7 \mathrm{k} \Omega$ | R18 | 8.2k $\Omega$ |
| R6 | 6.8k $\Omega$ | R19 | $680 \Omega$ |
| R7 | 8.2k $\Omega$ | R20 | $10 \mathrm{k} \Omega$ |
| R8 | $1 \cdot 2 \mathrm{k} \Omega$ | R21 | $5.6 \mathrm{k} \Omega$ |
| R9 | $12 \mathrm{k} \Omega$ | R22 | $100 \Omega$ |
| R10 | $18 \mathrm{k} \Omega$ | R23 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R11 | $2 \cdot 7 \mathrm{k} \Omega$ | R24 | $68 \mathrm{k} \Omega$ |
| R12 | $47 \mathrm{k} \Omega$ | R25 | $56 \Omega$ |
| R13 | $220 \mathrm{k} \Omega$ | R26 | $470 \Omega$ |

## C6 $0.01 \mu \mathrm{~F}$

C7 $220 \mu \mathrm{~F}$ elect. 25 V
C8 $470 \mu \mathrm{~F}$ elect. 25 V
C9 $100 \mu \mathrm{~F}$ elect. 25 V

## Potentiometer

VR1 $100 \mathrm{k} \Omega$ skeleton preset
Transistors

| TR1-TR2 | 2N2160 (2 off) |
| :--- | :--- |
| TR3-TR5 | BC207 (3 off) |
| TR6 | 2N1302 |
| TR7 | 2N1303 |

## Integrated Circuits

IC1 SN7490
IC2 SN7475
IC3 SN7441

## Miscellaneous

S1-Push switch, LS1-3 3 3in speaker, Veroboard $7 \frac{1}{8} \mathrm{in}(188 \mathrm{~mm}) \times 4 \frac{11}{16}(119 \mathrm{~mm}) \times 2 \frac{1}{1} \mathrm{in}(54 \mathrm{~mm})$.


CONSTRUCTION
All the components, with the exception of the battery and speaker, are soldered on to a single piece of $0 \cdot 1 \mathrm{lin}$ Veroboard. The prototype was built in a die-cast box which also contains the loudspeaker and battery. The Veroboard was cut to slot lengthwise into the box, as can be seen from the photograph. Soldering should be thoroughly inspected before power is applied as short circuits on adjacent copper tracks can cause some curious effects such as tone "hang-up" or no sound at all.

## TESTING

With assembly and inspection completed VR1 wiper should be adjusted to mid-range and power applied to the circuit. The Random Tone Generator should immediately start "composing" an endless train of note patterns. According to taste the rate can be varied by VRI. The frequency range of the output can be changed by altering the value of C4. $\star$

# NEWS BRIEFS 

## Post Office Unveils Viewdata

Aradically new telephone service, in which a wide range of information can be called up over the telephone and displayed quickly on an ordinary television set, is being planned by the Post Office.
Known as Viewdata, the service would be completely automatic, providing information at the touch of a button. Trials for the new system are due to start in January and a full public service could start in 1978-79.
With Viewdata, information on a wide range of subjects such as news, entertainment, holidays, job advertisements and commercial intelligence would be stored in a computer databank connected to the public telephone network. By having their telephone linked to their t.v. sets users would have access to the wide range of information services which Viewdata can provide. The user would control the entire service with a simple hand-held control unit.

To receive Viewdata information, users would first switch on the t.v. set and then call up the service over the 'phone by pressing a button on the control unit. They would not even have to lift the telephone receiver. Then, at another touch of the button, the Viewdata opening display (an index listing the subjects on which information is available) would appear on the t.v. screen. Following simple instructions displayed on the screen. users would select the information they wanted by pressing further buttons.

As an alternative to the telephone link to a domestic television. business users could have a purpose-made Viewdata terminal. with built-in controls and telephone.

## MAIL BAG

The on-going increase in postal and telephone charges does not seem to have made any difference to our post bag or our telephone bell. Enquiries continue to flood in.

We find that there are two points we are constantly mentioning. In the first place we just cannot afford to reply to any readers letters, particularly those not associated with projects we have pubished, unless they are accompanied by a stamped addressed envelope. Were we to undertake to do so our post bill would become astronomic.

We cannot deal with technical enquiries by telephone. Readers should write in, giving details of symptoms and perhaps some test point readings, when requesting technical help so that we can at least give the relevant author some idea of the problems involved.

Finally, whilst we normally supply details as to source of components in each project we do assume that the constructor refers to advertisements and has an awareness of general sources. Thus, where goods are generally available we do not specify a source. You could save the cost of a letter by reading the advertisement pages first.


THE Audio Fair this year was rather smaller than in previous years, with a lot of companies not exhibiting. The largest stand's at the Fair were taken for the most part by Japanese or foreign based firms and there was a distinctive lack of British representation.
It is difficult to guess the reasons behind this, but some say that the basic character of the Fair has altered and perhaps moved from the connoisseur to the consumer market, where electronic gadgetry is playing a greater and greater part.

Prices of equipments continue to boggle the mind and soar ever higher and higher. Sony have actually introduced a "Higher-Fi" range of equipment and both the equipment and the corresponding prices have to be heard to be believed (just one speaker in the top range costs $£ 700$ ).

## VFETs

One or two new terms are likely to be added to the hi-fi buff's repertoire after visiting the show. VFET is one of these terms and this at present is found in the specifications of a couple of popular Japanese manufacturers. It stands for Vertical Field Effect Transistor. The f.e.t.s are being used in the output stages of the amplifiers where they are replacing transistors with their attendant crossover and biasing problems. Yamaha and Sony are the two major pioneers in this field.

It will be interesting to see how Quad's recently released "currentdumping" amplifier compares with them. (They have got around' output stage problems by using novel circuit techniques.) Quad incidentally, were one of the British manufacturers not present at the show.

## LINEAR PHASE

Another relatively new term heard at the Fair is "linear phase". This is not a new guitar effect but describes the operation of a new development in loudspeakers. Bang and Olufsen have hit upon a method of overcoming phase dis-tortion-a rather nebulous quantity, the existence of which is apparently debatable. One of the effects of having no phase distortion is to enable speakers to reproduce square waves with minimum waveform distortion.

The system uses an extra drive unit known as a "Filler Driver" which operates in the crossover region of the base and mid-range units. The result is certainly a clean sounding speaker, whether or not it is attributable to the lack of phase distortion.

## TURNTABLES

The vogue in turntables has moved from idler drive to belt drive in its time. The latest trend is to electronic speed control with direct drive to the turntable. A relatively new firm, Strathearn Audio Limited, have produced several models with these features. Their SMA2 turntable also has touch start, stop, and speed controls and is attractively styled in a sleek case with a tinted dust cover.

Strathearn is also shortly to introduce a new speaker which uses ribbon techniques. The sound quality is equivalent to if not better

The Sony "High-Fi" speakers


New "Linear Phase" range from B \&

than that obtained with electrostatics and the speaker should have a very promising future.

Connoisseur, makers of the simple but very effective BD1 and BD2 turntables, have brought out a BD3 type which uses a servo-system for speed control. An external power source is also used to keep the possibilities of hum pick-up down.

## SOUND THEATRE

One of the major centres of interest at the Fair was the Sound Theatre. A fully functioning modern recording studio was constructed using high quality equipment from a large number of top manufacturers. The BBC, LBC and Capital Radio broadcast from the theatre, and various impressive quad and stereo demonstrations also took place. Procuring and setting up the studio equipment was very competently co-ordinated by Ian Grant.

One of the lectures given in the Theatre was by Doug Shaw on synthesiser techniques. He demonstrated the Minisonic Mk 2, and the highlight of the lecture was a live performance with several musicians and minisonics, and despite a last minute time change his lecture was very well attended.


Yamaha B1 amplifier with VFET output stage featured with their CT800 GL cassette deck


Strathearn SMA2 turntable with direct drive and servo amplifier


## CHANGE OF CHARACTER

It is interesting to note that where in the past there have been a multiplicity of technical lectures and demonstrations, this year's Fair saw very few. This tends to go along
with the observation that the Audio Fair is changing its character and pandering less and less to the connoisseur. Rather a pity. most will agree.

# NEWS BRIEFS 

## IERE GOLDEN JUBILEE

The Institution of Electronic and Radio Engineers celebrated its 50th anniversary during 1975. Last October, at the Annual General Meeting held in London, the Duke of Kent was installed as 25 th President of the Institution.

In his inaugural address, the new President reviewed some of the developments in electronics.
"I don't think any of you need reminding of the great changes that have swept over the world during this last half century; changes which are without question the widest and deepest that have taken place in any equivalent period of history. That this extraordinary epoch of social, political and economic revolution should have coincided with the growth of the new science of electronics is not I am sure an accident-although attribution of cause and effect is something for historians of the 20th century to argue over, not me.
"The fact is that throughout this period, electronics has evolved from the fledgling of 'wireless' to a great and in many cases dominant industry spanning a huge field from communications to data management. transport to process control and medicine to entertainment. It was the belief in the great future that lay ahead that stirred our founding fathers-not that even they could
have foreseen what was to come-to establish our Institution, despite some cynicism from the older institutions of that day."

The President then went on to predict probable advances of the next 50 years in communications, domestic equipment, manufacture, aircraft safety and medicine. The last example holding promise of some_very striking and praiseworthy achievements in alleviating the handicap of a few-"but if access and connection to the brain becomes a matter of standard practice, what dramatic developments might not ensue?." The possibilitv of contact with the brain via electromagnetic waves leads to the possibility of thought control, and this brings one on to some very tricky ground. The idea may be appalling-but it is essential that we recognize such possibilities even if for one reason or another they have eventually to be rejected.

## POInTS Bilsinn

## LIGHT MODULATION UNIT (October 1975)

The 40430 outline connections in Fig. 1 are incorrect. The MT1 and Gate terminals should be transposed.

In the circuit diagram MT1 and MT2 connections should also be transposed, i.e. MT2 terminals for CSR3 and 4 should be connected to L1 and L2 respectively.


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## TAPE NOISE REDUCTION

In BP 1382 096, Matsushita Electrical Industrial Co. Ltd. patents an automatic noise reduction system for use with tape recorders. Using compression and expansion techniques the block diagram of the system is shown in Fig. 1

The compression characteristic (a) on record, the expansion characteristic (b) on playback and the resultant, theoretical, linear characteristic (c) which follows from the combination of (a) and (b) is shown in Fig. 2. Thus, the process is complimentary and therefore the output should be a replica of the input.

Noise is reduced because it is introduced between the two stages and is thus subjected only to the expansion curve. In other words. process noise is reduced relative to programme content.

Because the expansion-compression effect is active only below a threshold point (where the curves in Fig. 2. (a) and (b) become linear), noise is reduced only when the signal level is low. This avoids overloading the tape with excessive signal and is acceptable because the subjective level of noise present in a high level signal is less noticeable because it is masked by the signal.

In practice, the compression and expansion operation is effected onlv in the presence of high frequency signal components. The circuit shown in the patent is designed to provide processing of only the high frequency signal components, because the majority of tape noise is in the upper frequency range, i.e. tape hiss.

The system outlined in the patent more closely resembles that marketed by JVC than Dolby.

## Electrostatic lounspeaker

## BPI 1387453

In BP 1387 453, Matsushita Electric Industrial Co. Ltd. describes an electrostatic loudspeaker which requires no d.c. polarising voltage.

A vibratile film electret, made of a polymer such as plastics resin and with a permanent surface charge, is coated on one side by a very thin layer of a conductive paint or metal. Fixed perforated electrodes permit acoustic radiation and are spaced one each side of the coated electret.

An a.c. audio frequency signal is applied between the fixed electrodes via a matching transformer, balance capacitors and a resistor which controls higher harmonic distortion. Alternatively, a push-pull transformer may be employed as the audio power source.

The conductive layer acts as an electrostatic earth, so the electric field due to the permanent charge on the film electret exists in one air gap between the electret and the fixed plates, but not in the other air gap. Thus no static electricity due to the charge is generated between the film and the non-charged electrode and the only force between the film and this electrode is generated by the audio signal.

However, the force between the film and the charged electrode is generated by the superposition of the electrostatic voltage due to the electret charge on to the audio signal. The resultant imbalance causes vibration of the electret and transduction of the audio signal into sound waves propagated through the perforations in the electrodes.


## PATENT NEWS

Of necessity, patents for inventions reported in this column are relatively simple. It is physically impossible to precis an invention covered by a hundred-page patent in a few lines of print. For this reason, the most complicated inventions and the most lengthy patents must usually pass unrecorded.

This is a pity, because a lengthy patent can be a valuable source of information. It can also be a very cheap one, because all British Patents cost only 33p each, regardless of length. They may also be studied free of charge by any member of the public at various libraries around the country, such as the Science Reference Library attached to the Patent Office at Southampton Buildings, Chancery Lane, London WC2.

With this in mind, we shall in future be referring simply by name, number and the briefest of explanatory comment to any lengthy new electronics patents that may be of value to readers with a specialist interest.

BP 1402 320-Sansui Electric Co. Ltd. Decoder for use in $4: 2: 4$ matrix playback system. One of many patents now appearing for the various four channel and quadraphonic systems, this one covers the Sansui Variomatrix principle. Separation between channels is enhanced by sensing the amplitude of signals in the various channels and varying the matrix parameters to accentuate them.

BP 1404 460-Standard Telephones \& Cables Ltd. Device for transmitting cursive script or drawing over a telephone. A matrix of metal conductive strips is mounted under a domestic telephone, to translate a sketched diagram into different resistance values which are transmitted via the telephone.

BP 1402 571—Mitches and Jeffrey. Method for identifying the components of a file. A system for reading the contents of any data file, which may for instance be a punched card, to aid automatic data retrieval. (See also BP 1402 572.)

## Rioidiont A SELECTION FROM OUR POSTBAG

Readers requiring a reply to any letter must include a stamped
addressed envelope. We regret that we cannot answer any
technical queries on the telephone technical queries on the telephone.

## Good-Bye ?

Sir,-This is a farewell letter. For nine years, to the exact month, I have enjoyed every issue of Practical Electronic's. Its specially written articles have added to my knowledge of electronics. Its construction projects have brightened my spare moments, and even helped in my work. Indeed, my subscriptions to P.E. have been one of the wisest investments I ever made.

But now, your publishers inform me that they are discontinuing the subscription service. This means that those of us outside the U.K. who had relied on subscriptions for obtaining regular supplies of P.E. can no longer do so. I know there must have been. genuine economic reasons for taking such decisions, but this seems to ignore the confidence we have had in you for a long time. It is, after all, very true, isn't it, that economic considerations are hardly the best recipe for maintaining a friendship. But then. even the publishers of P.E. are in business too!

So, it is good-bye to P.E. God bless.
A. J. Isong, Nigeria.
We trust this is not "farewell" as you suggest, but only ou revoir. Our agent in Nigeria should be able to supply you with PE regularly.
Other subscribers, home or overseas, please see notice on page 32.

## A Bit Flat

Sir,-l was interested to read your article in the November P.E. on an "Electronic Tuning Fork". I should like to point out that this device would not be suitable for tuning a piano.

I have already developed a tuner using a cathode ray tube for visual aid, I have experimented with the master oscillator 12 -note frequency derivative integrated circuit, but so far, I have not used it, as 1 am in favour of using a tapped oscillator coil for greater accuracy.

When tuning a piano, the treble end of the scale is slightly sharp and the bass end slightly flat. "Zero" deviation occurs at the centre of the keyboard.

Pianos are tuned only by aural means, and when tuned, become mathematically incorrect.

Therefore, by introducing a plus and minus frequency deviation switch, a much more realistic tuned piano is possible. On this theory. I claim that no frequency divider organs are in tune but nobody seems to mind, but I have tuned several pianos flat, but they are noticeable.
I don't suppose you were reallv trying to encourage your readers to put piano tuners out of business. so perhaps you may consider your circuit good enough.
D. Marquis, Essex.

Your observations on piano tuning are very interesting, I have, in fact, heard that some professional tuners do tune sharp at the top of the scale and flat at the bottom end. Unfortunately, nobody has told me why they do this, if in fact they do.

When researching this project, I took as my main source of reference a book entitled "The Physics of Music" by Alexander Wood (Pub Methuen), which goes into considerable detail on the subject of piano tuning. This book definitely states that pianos are tuned in perfect accordance with the tempered scale. Illustrated in the book (Page 200) are graphs of the state of tune three days after tuning has taken place. The trend is for the low notes to drop considerably whilst the upper notes show considerable variations but all on the high side. This deterioration is similar to their figures. I have taken these figures to be percentages of a semitone interval, as percentages of the actual frequency are clearly a nonsense for the values you give.

If indeed, pianos are tuned in this fashion, one wonders if the same applies for other orchestral instruments when played in the extreme registers.

Finally, l'm sure piano tuners aren't going to become redundant, perhaps this instrument will save some piano's from the scrap heap. Should any piano tuner feel threatened, he should retaliate. I'm sure you'll agree, there are tremendous prospects in the electronic musical instrument field!P.W.B.

## Happy Chance

Sir,-By a happy chance I have come across your article "Electronic Tuning Fork" in P.E. for Nov.

It would be much more convenient if each octave began on C according to usual musical usage, i.e. the $\mathrm{C} 2 \mathrm{Cl} \mathrm{c}^{\prime} \mathrm{c}^{\prime \prime}$ etc., notation, and the $16^{\prime} 8^{\prime} 4^{\prime}$ etc. of organ nomenclature. Would it be possible to incorporate a circuit to double the frequency of the $A \not \#$ and $B$ outputs from ICI? Or failing that, alternatively to halve the frequency of the other ten outputs?

For my purposes, I think the most convenient form of display would be a centre-zero meter calibrated to indicate the pitch difference in vibrations/second + or. - . Is this at all feasible?

For, many purposes the tuning errors of your instrument (maximum on C\# of -0.29 in an interval of 15.6 ) are not really acceptable and one would certainly have to make a correction according to the beat indication.
M. B. Card. Herts.

Your requirement for a range spanning C to Cl is simply facilitated by increasing the master oscillator frequency to 999.68 kHz . The tuning core of the coil LI will probably accommodate this, but should this be not so, decrease C5 and C4.
Your further requirements are not so easily satisfied; although it is possible to determine and indicate whether the pitch is greater or less than standard, the extra complexity would not be worthwhile as when using the "fork" it is at once obvious when the instrument is detuned, and opposite action is applied without thought.
A meter indication of your description would indeed be a great improvement, however, the problems involved are considerable. The advantages of the beat method are simplicity, but the drawback is a variation in accuracy over the range of the scale.

A meter performing the beat counting task would have to sample for at least the period between two beats which becomes infinite when the tuning is spot on.
Your final comment on the accuracy rests with the i.c. manufacturer. The worst case I concede is C \# which is less than $2 \%$ of the semitone interval or 2 cents in musical parlance. Ideally, errors should be less than one cent and it is unfortunate that General Instruments did not choose to divide by larger integers. especially as master clock frequencies of up to 2.5 MHz can be accommodated, so the top end of the scale need not be sacrificed.

In conclusion, it is well documented that a good piano will give errors greater than 10 per cent only three days after "perfect" tuning so I feel that only the most discerning ears will be grieved by our small inaccuracies.P.W.B.

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20 dB into $\mathrm{MM} \Omega$ DIN -47 dB into $100 \mathrm{~K} \Omega$. 0 utput levels Line out 20 dB into $1 \mathrm{M} \Omega$. DIN -47 dB into $100 \mathrm{~K} \Omega$. Output levels Line out -
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EMI 350 KIT $\mathbf{£ 7 . 2 5}+\mathfrak{f} 1.20 p \& p$. Complete with crossover Components and circuit diagram

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System consists of a $13^{\prime \prime} \times 8^{\prime \prime}$ approx. woofer with a $3^{\prime \prime}$ tweeter. crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz . Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

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CONTROLS: Push button ON/OFF, stereo/mono, scratch filter. 6 position rotary selector. Individual rotary controls for treble, bass., balance and volume. Headphone socket, tape out socket. Auk. mains output. Frequency response: 25 Hz to 25 KHz full rated output. Signal to noise ratio: better than -50 dB on all inputs. Tone control renge; Bass $\pm 15 \mathrm{~dB}$ e 50 Hz : Treble $\pm 12 \mathrm{~dB}$ - 10 KHz Power requirements: 200-250V A.C. mains e 60 watts. Approx. size: $15 \frac{1}{1 "}^{1^{\prime \prime}} \times 3^{\prime \prime} \times 10^{-1}$. MP60 type deck with maguetic cartridge, de luxe plinth and cover
Two Duo Type Ila matched speakers - Enclosure stze approx. $19 \frac{1}{2}{ }^{\prime \prime} \times 10 \frac{3^{\prime \prime}}{}{ }^{\prime \prime} \times 7 \frac{3}{6}{ }^{\prime \prime}$ in simulated teak. Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with $3^{\prime \prime}$ tweeter. I5 watts handling. 30 watis peak.
Complete System with these speakers $\mathbf{1 6 9 . 0 0} \mathbf{5 6 . 5 0} \mathrm{p} \& \mathrm{p}$.

System 2. £85.00
Viscount IV amplifier (As System 1a) MP60 type deck (As System Ial Two Duo Type III matched speakers - Enclosure size approx. $27^{\prime \prime} \times 13^{\prime \prime}$
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Complete only $£ \mathbf{2 3 . 2 0}+£ 3.00 \mathrm{p} \& \mathrm{p}$.
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Finish - Satin black mainplate with black turntable mat inlaid with brushed aluminium trim. Tonearm and controls in black and brushed aluminium.

Console size
Unit Closed $-17 \mathbf{l}^{\prime} \times 13$ " $\left.\times 8\right\}$ " 1 app.) Unit Open $-353^{\prime \prime} \times 13{ }^{1 \times} \times 4$ )" (app.) This disco console is ideally matched or the Reliant IV and Disco 50 or any ther quality amplifier:
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## Speciflcation

Output power 100 watts into $8 \Omega$. Input sensitivity 500 mV R.M.S. Input impedance $100 \mathrm{k} \Omega$. Signal/ noise ratio 96 dB at 100 watts. Power bandwidth $10 \mathrm{~Hz}-45 \mathrm{kHz}-3 \mathrm{~dB}$. Distortion $0.05 \%$ typical. Weight 1 kg (2-21b).
$£ 21 \cdot 20$
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(P.E. Feb. 1973 to Feb. 1974)

The well acclaimed and highly versatile largescale mains-operated Sound Synthesiser complete used independently, or intercannected. The greater the number of circuits, the greater the versatility Other circuits in our lists may be used with the Synthesiser to good advantage.

THE MAIN SYNTHESISER
Stabilised Power Supply
412.05

Two Linear Voltage Controlled Oscillators and one inverter-all 3 circuits:
PCB (2 are required)-each
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PCB (holds both and Noise Generator-
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Reverberation Amplifier
Amp
Ring Modulator
Peak Level Meter Circuit
$100 \mu \mathrm{~A}$ Panel Meter
$100 \mu A$ Panel Meter
PCB for Rev., R-Mod, \& Meter Ccts., Envelope Shaper, 65.24 ; PCB, fl. 42 Voltage Controlled Amp. and Diff. Amp PCB (holds both circuits)

## SYNTHESISERS AND KEYBOAROS

## P.E. JOANNA

## (P.E. May to Aug. 1975)

The new electronic piarro that has switchable alternative voicing of Piano Honky-Tonk and Harpsi chora. All PCB's are "as published"
Power Supply $\quad$ E8.85 Tone Generator and Top C Envelope Shaper $\uparrow 10.26$ Envelope Shaper
2 sets (full requirement)
$\begin{array}{ll}12 \text { sets (full requirement) } & £ 32.16 \\ \text { Set of } 12 \text { PCB's (full requirement) } & \text { \&15.00 }\end{array}$
Voicing and Pre-Amplifier Circuits
PCB for above circuits
Remaining circuits: prices in lists.

## KEYBOARDS

Kimber-Allen Keyboards as required for many published circuits, including the P.E. Joanna, turers claim that these are the finest moulded plastic keyboards made.
3 Octave Keyboard ( 37 notes $C$ to C) $\quad \mathbf{2 0 . 5 0}$ 4 Octave Keyboard ( 49 notes $C$ to C) $\quad \$ 23.50$ 5 Octave Keyboard (61 notes C to C) 627.00 Contact Assemblies for use with above keyboards: Single-pole change-over (SP) as for P.E. Joanna and P.E. Minisonic. Two-pole normally-open makebreak (2P) as for P.E. Synthesiser. Special contact assembly (4PS) having 4 poles, 3 of which are is a change-over contact-this. special assembly is a change-over contact-this. special assembly P.E. Synthesiser, P.E. Minisonic, and P.E. Synthesiser simultaneously thus avoiding the cost of more than one keyboard.
$\begin{array}{lllll} & & 3 \text { Octave } & 4 \text { Octave } & 5 \text { Octave } \\ \text { Contact } & \text { Each } & \text { Sot } & \text { Set } & \text { Set } \\ \text { SP } & 20 p & £ 7.40 & £ 9.80 & £ 12.20 \\ 2 P & 24 p & £ 8.88 & £ 11.76 & £ 14.64 \\ \text { 4PS } & 48 p & £ 17.76 & £ 23.52 & £ 29.28\end{array}$
Printed Circuit Boards for use with the above contacts and thus eliminating most of the inter-
wiring required, are available-details in our lists.

PHONOSONICS


## P.E. MINISONIC

(P.E. Nov. 1974 to March 1975)

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$\mathbf{6 5 . 2 5}$

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