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SEPTEMBER 2002 £3.10

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Promax MC377+ signal analyser

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The convergence myth

DTT licences awarded, digital TV update, scrap TV hazard, interactive TV, disc technology and other news items.

Hugh Cocks finds that this receiver, signal-strength meter and spectrum analyser, for analogue and digital terrestrial and satellite signals, is well suited to the day-to-day needs of an active aerial installation business.

There are limits to the possibilities with conventional silicon semiconductor technology. What might follow? The future could well lie with the carbon-based nanotube. Ralf Buckstone takes a look at a newly-developing technology that could be the basis of the next era in electronics.

Part 3 of Mark Paul's description of the circuit technology used in this chassis deals with the tuner, IF and video signal processing sections.

The concluding instalment in Donald M. Henry's series on this 17in. monitor describes the operation of the digital control system.

Terrestrial DX and satellite reception reports. News on TV broadcasting and satellite band changes. Moon-bounce reception. Roger Bunney reports.

An LNB problem, a satellite receiver fault and the latest digital channel update.

Guidance on repairing monitors and related equipment.

Hints and tips on repairing professional and consumer equipment.

Useful websites for TV professionals, technicians and enthusiasts.


Adrian Gardiner on storm damage, Vestel 11AK19 chassis fault-finding and a test equipment tip.

A meddler, a Sony TV repair, camcorder and CD trouble and a Philipsaver tip. Don Bullock's servicing commentary.

Next issue, dated October, on sale September 18th
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The convergence myth

A few visionaries left over from the dot.com age are probably still going on about convergence. The general idea was that the various media — broadcasting, films, publishing, PC systems, telecommunications and of course the internet — would converge. There’s a sort of initial plausibility, lots of synergy and all that sort of thing, about the idea: until you think about what ordinary people, the customers, might be able to make of it. After all they are the ones who have to pay the bills. A lot of money has been lost chasing after a sort of virtual world of interactive facilities: by virtual I mean that the facilities are there but no one takes much notice of them.

There are two ways of looking at the possibilities of media/communications convergence, from the point of view of the user and that of the service provider. Convergence is certainly easy enough to arrange for the user. TV sets can be used as monitors for web surfing, PCs can be turned into entertainment centres, and so on, but this doesn’t mean that such technology mingling is ever likely to become the norm. TV is basically about entertainment, also news and information. You switch the set on and expect it to deliver: you don’t expect to start cross-examining and tomfooling with it. Distractions are not what most people want once they’ve switched the set on. For effort-based screen-centred activity the PC is and will remain the logical tool.

One basic factor that separates active and passive screen use is the screen itself. The TV screen is based on broadcasting requirements. It’s bright, and the resolution is set by TV transmission limitations. The monitor screen is a different animal. For one thing the phosphors differ, so does the brightness — a monitor is designed for close viewing, not projecting an image across the room. And the resolution is quite different: you don’t need to be able to read small print on your TV screen. TV looks odd when displayed on a monitor screen — because that’s not what it’s for.

All this is pretty obvious, but was easy to overlook by those who got taken in by the convergence hype. And a lot of money can be lost getting this wrong. Alba lost quite a few million on its Bush Internet concept. It was a bright idea in some respects, but in practice was a compromise between different requirements. I can’t help feeling that it is rather like the debate years ago about electricity and gas. You can do all you need with electricity, so why bother to distribute gas? But of course gas is superior for some purposes, particularly heating. So the two are likely to coexist in our homes for the foreseeable future. The TV/PC situation is similar: we need them both. The confusion comes from the fact that once you digitise TV all sorts of things become possible. But this doesn’t mean that convergence is inevitable: what it means is that there are additional TV possibilities that can be exploited.

The other way of looking at all this is from the information source. Broadcasters are still good at what they do, though we might not find all their offerings to our taste. They have to be, or they would go out of business (well, not in the case of the BBC, but the Corporation still has to provide a reasonable performance to justify its licence revenue). Broadcasters have to aim at large audiences: what has been called narrowcasting is not their function. The latter is ideally catered for by the internet, which you can use for the most obscure requirements.

Yet huge organisations have got it wrong. Take AOL Time Warner, which seems to be falling apart. Some bright sparks, actually Roger Pittman of AOL and Gerald Levin of Time Warner, were carried away by convergence hype. What they felt was needed was a combination of on-line distribution (AOL) and the huge input of “content” that Time Warner could provide. So, two years ago, there came about the biggest merger in the history of the media, when AOL took over Time Warner, with its substantial cable TV amongst many other interests, for some $105bn. There would be “internet-fuelled profit growth”, and “cross-platform synergy”. Sounds good, doesn’t it? The merger was completed early last year, but it didn’t turn out as hoped.

Those of us who felt that it didn’t seem to make much sense have been proved right.

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Broadcasters have to aim at large audiences: what has been called narrowcasting is not their function.

The addition of Time Warner was not able to transform AOL, whose internet business subsequently became a big problem. It was assumed that increased advertising revenue would generate on-line profit growth, but this didn’t happen. In April, AOL Time Warner announced a first-quarter loss of $54bn, the largest ever recorded, and the share price collapsed. Gerald Levin quit as chief executive late last year. Robert Pittman resigned as chief operating officer in July. Executives from the Time Warner side of the business are now trying to clear up the mess. It seems that the two sides of the company wish they had never become involved with one another. Oh, and another thing: the Securities and Exchange Commission and the US Department of Justice have both started enquiries into AOL Time Warner’s accounting practices.

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DTT licences awarded

Following the collapse of ITV Digital the ITC has awarded the licences to broadcast digital terrestrial TV in the UK to the consortium headed by the BBC. The other members are Crown Castle, which owns the transmitters, and BSkyB, which will be providing three channels. The initial plan is for 24 free-to-view channels, including the analogue ones, ITV2, Turner Classic Movies and five news/sports news channels, plus interactive and radio services. A music and a general entertainment channel are planned. Nine channels will be provided by the BBC, with the other channels being funded by advertising. The full service is expected to start in October.

Existing ITV Digital set-top boxes should continue to be usable, though some retuning may be required, and units such as the Pace DTVA adapter are readily available at about £99. The interactive TV company TVCompass plans to release a DTT STB for £29, complete with remote-control unit, early next year. This is less than the cost of manufacturing the equipment, but the idea is to generate funds from deals with companies that offer interactive services, which would be accessed via the remote-control unit.

The modulation standard for DTT has been changed from 64QAM to 16QAM. This provides a more robust signal, increasing the service area and reception reliability. The change should not affect existing receivers and STBs.

In a survey conducted by Taylor Nelson Sofres for Pace, 38 per cent of respondents agreed that more choice of free-to-air channels would encourage them to switch to digital: 44 per cent would be encouraged to switch by latest release movies, 36 per cent by big sporting events and 36 per cent if offered a free-to-view package with a possible pay-TV upgrade.

Disc technology

Philips has announced the development of a 3cm optical disc that can store 1GB of data using blue laser technology, and a 56 x 34 x 7.5mm drive to go with it. Applications envisaged include digital cameras, mobile phones, PDAs and portable internet devices. A prototype is being field tested to determine parameters – which applications might need what capacities. The technology conforms to the Blu-ray laser standard. Key items are thinner active-focusing mechanics and a new objective lens to reduce the thickness of the drive.

The DVD Forum has set up two subgroups to study different approaches to developing the next generation of blue laser DVD formats. One will study an approach based on 0.6mm cover thickness technology, the other studying 0.1mm cover thickness technology. The Forum has also approved an optical specification for 3x DVD-RAM drive speed.

Digital update

Pace started downloading MHEG functionality to its DTVA (digital TV adapter) customers on July 22, giving them access to a range of free-to-view interactive services and digital teletext channels, including BBCi, ITV Text+ and FourText.

The download was transmitted via the BBC Engineering Channel. DTVA users should have received notification on a BBC channel that their adapters were ready to receive the software download. A set of simple on-screen instructions guided the user through the step-by-step process of receiving the download. There was also a telephone helpline and a dedicated free-to-view website – details of these were included with the on-screen instructions in case of any problems. The download takes approximately five-ten minutes to complete, after which the screen reverts to normal broadcast material.

Pace says that the downloads will be repeated twice in the near future to ensure that all adapters in the retail chain are updated.

BSkyB is to introduce new functions with its Sky+ box later this year. Thomson Multimedia has bought Grundig’s South Wales based STB business Digital Intermedia Systems.

Teletest’s move

Teletest Ltd., supplier of the neat little Ozan hand-held TV and PC test pattern generators, has moved to 4 Shelley Road, Bournemouth BH1 4HY. The phone number is 01202 646 100, fax number 01202 646 101 or you can e-mail purchasing@teletest.co.uk

There’s a website at www.teletest.co.uk

National retailer Crazy George’s has been rebranded BrightHouse. Set up by Thorn in 1994 to provide credit facilities for anyone, regardless of financial status, to buy premium-brand products and services with affordable weekly or monthly payments, it continues to offer the same shopping experience. The range of products available includes TV sets, VCRs, audio equipment, computers, white goods, bedroom furniture and upholstery. Payment can be weekly in store or by direct debit, there are cheque-cashing facilities and a Payzone – a new electronic top-up service for mobile phones and utility payments.

BrightHouse currently operates 101 stores in London, the Midlands, North East, North West, Yorkshire, Scotland and Wales, employing a staff of 1,000 nationwide. Store expansion is to continue, with another ten openings planned for the current year. The retailer offers an optional Service Cover package, providing full technical support in the event of product failure.
Scrap TV sets a hazard

By the end of the year scrap TV sets will be classified as hazardous waste, which means that they will have to be recycled or taken to specially-designated landfill sites. The problem is caused mainly the lead in the CRT, about 20 per cent of the content. It’s used to provide X-ray protection, strength and clarity, but can cause ground pollution when the glass is consigned to a landfill site. Unfortunately there’s no simple way of extracting the lead. The DTI has provided funding for research into techniques that involve melting and electrolysis, but the ICER (Industry Council for Electronic Equipment Recycling) points out that the energy required could make this processing unacceptable. The CRT screen phosphor is another pollutant. In addition components and PCBs contain a number of dangerous heavy metals and halogenated substances.

The Environmental Agency has estimated that the number of landfill sites able to accept hazardous waste could fall from 240 to fewer than a “couple of dozen” by 2004.

Disposal costs are likely to rise from the current £8-10 a tonne to £30-50. As a result, dealers are unlikely to be willing to take away old sets – about 2.5 million TV sets a year are scrapped in the UK. The Waste Electrical and Electronic Equipment (WEEE) directive, expected to come into force next year, will make it obligatory to recycle 75 per cent of the weight of every TV set.

Video news

Sharp has announced an LCD digital ViewCum, Model VL-DD10, which is a combined camcorder, digital still camera and TV unit. Use of a modular system called a camera unit exchange enables the three units to slot into one. The TV tuner is optional. The main unit has a 3in. LCD monitor. There are several ways to connect to a home PC. Digital video can be transferred using the built-in i-link port, while still photos can be downloaded via the USB port or by using an SD Memory or MultiMedia card. Production is running at 10,000 units a month, but no price details have been announced and there is so far no suggestion of a European launch.

Panasonic has introduced the first combined DVD and hard-disk recorder to go on sale in the UK. Model DMR-HS52 can record up to 52 hours on its hard disk in the EP mode, twelve hours on a 9-4GB double-sided DVD-RAM disc and six hours on a DVD-R disc. The user can watch programmes recorded on the hard disk or a DVD-RAM disc while recording on the other. A time-slip function enables a live programme to be viewed from the beginning while the rest of the programme is being recorded. Other features include a JPEG photoviewer, high-speed copying (up to twelve times) from the hard drive to a DVD-RAM disc, an IEEE 1394 (FireWire) input terminal, two scart sockets (composite video and RGB), an S-video socket and phono audio sockets. Price is about £1,000. Panasonic has also launched the DMR-E30 DVD-RAM recorder, which can record on DVD-R as well as DVD-RAM discs. Price is about £500.

Philips has launched two lower-priced DVD+RW recorders, Models DVD880 and DVD890, at £499 and £399 respectively. They use blank DVD+RW or write-once DVD-R discs and include an IEEE 1394 (FireWire) interface, MP3-CD playback and compatibility with Super Video CD, Video CD, audio CD, CD-R and CD-RW discs.

The latest Sony portable DVD player, Model DVD-PQ1, uses the new Precision Drive 2 system. This has a new high-speed stepping motor and helps to compensate for disc warp and other imperfections. The dynamic tilt compensation mechanism is designed to provide more accurate tracking.

Satellite news

According to SES, 10.3 million households in the UK are now receiving broadcast and broadband services from the company’s Astra satellites. The breakdown is 6.5 million via DTH/SMATV and 3.85 million via cable. BSkyB installation charges were increased in early June, from £50 to £60 for subscribers to the top-tier Sky World package and from £70 to £100 for other subscribers. Installation charges were last increased in the summer of 2001. The STB and dish remain free as part of the installation/subscription. BSkyB expects to have seven million subscribers by the end of the year.

BT has been carrying out broadband internet trials via satellite throughout the UK. The service would be sold to internet service providers at about £15 a month, suggesting an end-user charge of £20-£30 a month. The dish needed for reception would be likely to cost about £400.

Interactive TV

NTL is to add Two Way TV’s ArkT technology to its digital network, following a licensing deal between the two companies. The Ark system enables digital TV viewers to join in by voting, playing along with game shows and interacting with live programmes such as sports events and awards shows.

MTV launched WimbledonPong, an interactive tennis game based on the 1980s computer game Pong, during the Wimbledon fortnight. NDS technology was used to drive the system. It was the first time that gaming was introduced in UK TV during advertisement breaks. Access to the service was via the red interactive button on the SkyDigital remote-control unit. The simple linear graphics represented two 'rackets', with one player able to control them against the TV set with the two sides of the screen as the ends of the court. Ball powering was via the remote-control unit’s arrow keys. A set lasted as long as the advertisement break.

Philips has launched this 42in. plasma-display TV set, Model 42PF9964. Features include a 1,200-page hypertext and wordsearch (advanced tele-text navigation functions), a dual-screen mode for watching two different channels at the same time, Mosaic Screen which shows the main picture surrounded by eight smaller pictures from other channels, and Philips Digital Natural Motion, Digital Crystal Clear and Active Control technologies. The latter is designed to provide optimum picture quality from a variety of video sources such as TV, DVD or a games console. Price is likely to be about £5,800, without table stand. Philips plans to launch a 50in. version, Model 50PG9964, later this year.
Promax MC377+ signal analyser

 Hugh Cocks finds that this receiver, signal-strength meter and spectrum analyser, for analogue and digital terrestrial and satellite signals, is well suited to the day-to-day needs of an active aerial installation business

We've been using a Promax Prolink 3 signal analyser for some time now - I reviewed it in the March 2001 issue - and needed a second unit for day-to-day satellite dish and TV aerial alignment. Some of the more complex functions provided by the Prolink 3 wouldn't be required, so we decided that the simpler Promax MC377+ would be suitable.

Table 1 shows the basic specification for the MC377+. It's the same size physically as the Prolink 3, and comes with similar shock-absorbing rubber fittings and a rugged yellow carrying case. There isn't a separate mains adaptor, as with the Promax 3: the mains lead plugs directly into the lower right-hand side of the MC377+.

Controls and displays
Photo 1 shows the control and display panel of the MC377+. There are a lot more knobs and buttons than with the Prolink 3, but operation is straightforward.

The red button at the left-hand side switches the unit on and off, the signal input sockets being mounted at the right-hand side. The three attenuator buttons are at the bottom, near the input sockets. All three attenuators can be used with terrestrial signals. With satellite signals only the right-hand button can be used - it's coloured yellow to indicate this. There's a colour-code for the controls: yellow indicates a satellite-only function, blue anything to do with digital signal measurement.

Switches that control the 13/18V LNB supply and 22kHz tone switching for high-band universal LNB operation are mounted just to the left of the satellite input socket. Strangely, power is supplied to both input sockets simultaneously, though the short-circuit LED flashes to remind you to switch off the supply when a terrestrial aerial connection is made. It's useful to have a DC voltage supply at the TV socket as this can be used to power a mast-head amplifier to measure its output without having to connect the companion indoor power-supply unit.

There are blue digital channel-power and grey signal-level scales, in dBμV, above the CRT display. Below the screen there is a grey carrier-to-noise scale...
The two knobs nearest the CRT screen are for brightness and contrast control. The smaller knob to the right of the brightness control is for fine tuning, with the larger main tuning knob to the right of this.

The knob to the right of the contrast control is for volume adjustment. When this is pulled out analogue TV sound is available: when it's depressed an audio tone that varies with signal level can be heard from the speaker. To the right again there's the TV audio tuning knob, which gives fixed terrestrial audio when depressed and variable satellite audio when pulled out.

The right-most knob in this row varies the span of the spectrum-analyser display.

The buttons in the row at the bottom are fairly straightforward. For digital signal measurement you depress the right-hand button with the blue surround. The four buttons to the left of this one select the low or high VHF, the UHF or the satellite band. To the right of the on/off switch there's a button (STD BAND) for video polarity selection. Next to this there's the TV monitor/spectrum analyser selection button. The final button selects maximum or partial spectrum-analyser display span.

The digital display indicates the frequency of the TV channel being received. Alternatively, when the spectrum-analyser display span is switched to maximum the tuning knob moves a cursor to the required part of the band then, when the span button is depressed, a frequency readout is obtained. A disadvantage is that there's no reference anywhere to TV channel numbers, just to frequency, so you have to be familiar with the local TV frequencies.

**Physical features**

The unit is well built. Photo 2 shows the internal arrangements. The satellite and terrestrial TV tuners can be familiar with the local TV frequencies.

### Table 1: Basic specification for the Promax MC377+ signal analyser

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Specification</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Resolution</strong></td>
<td>VHF/UHF 10kHz. Satellite 100kHz.</td>
</tr>
<tr>
<td><strong>Sensitivity</strong></td>
<td>Terrestrial analogue 20dBpV (10μV) - 130dBpV (3-16V). Terrestrial digital 35dBpV-125dBpV. Satellite analogue 40dBpV-100dBpV. Satellite digital 45dBpV-95dBpV.</td>
</tr>
<tr>
<td><strong>Attenuation</strong></td>
<td>TV bands 50dB in 10 and 20dB steps. Satellite band 20dB.</td>
</tr>
<tr>
<td><strong>Inputs</strong></td>
<td>Separate BNC sockets for terrestrial/satellite bands. Belling Lee socket to BNC plug and F socket to BNC plug adaptors supplied. 0/13/18V selectable DC output at sockets with maximum current drain 350mA. LED on if current drain above 50mA and short-circuit warning, 22kHz selectable on/off.</td>
</tr>
<tr>
<td><strong>Accuracy</strong></td>
<td>TV bands ±4dB, satellite band ±6dB. Unit is supplied with measurement correction chart for all bands.</td>
</tr>
<tr>
<td><strong>AV connections</strong></td>
<td>Video and audio in/out via scart socket on side of unit. Input automatically selected with voltage applied to pin 8. Output is demodulated analogue video/audio (video 1V p-p at 75Ω).</td>
</tr>
<tr>
<td><strong>Video</strong></td>
<td>Switchable normal/inverted for C/Ku band analogue satellite and French terrestrial signals. 4:3in. monochrome CRT display. Signal level and video sync pulse representation can be superimposed on analogue picture, and carrier-to-noise ratio available in the spectrum-analyser mode for analogue and digital signals.</td>
</tr>
<tr>
<td></td>
<td><strong>Audio</strong>: Model MC377+ has terrestrial analogue preset to system B/G/H (5-5MHz). Model MC377+/4 switches between system I (UK, 6MHz) and system L (France, 6.5MHz AM). Model MC377+/1 has 4.5MHz audio (systems M, N). Model MC377+/2 has 6-5MHz audio for systems D/K. Terrestrial and satellite analogue audio tunable 5-6MHz. Output switchable to tone that varies with input signal level. Loudspeaker output 0.2W.</td>
</tr>
<tr>
<td><strong>Spectrum-analyser mode</strong></td>
<td>Spans entire band in max mode or between one third and very small amount in the span mode.</td>
</tr>
<tr>
<td><strong>Mains input</strong></td>
<td>110-125 and 220-240V AC (selectable). Consumption 55W.</td>
</tr>
<tr>
<td><strong>Battery operation</strong></td>
<td>12V 2-6A/hr. At full charge will run for one hour without LNB connected or about 60 per cent of this when supplying power to an LNB. Low battery voltage indicated by blinking colon in LCD display. Auto low-voltage shut-off. Charge time 8 hours with totally flat battery.</td>
</tr>
<tr>
<td><strong>Physical details</strong></td>
<td>31cm wide x 11.5cm deep x 26cm high (battery and rubber surround included). Weight 5.73kg.</td>
</tr>
</tbody>
</table>
Photo 4: C-band reception of Argentina ATV channel 7.

be clearly seen, near the front of the PCB, with the battery at the rear and the mains transformer at the right-hand side of the chassis. The mains tuning control is the large, blue multiturn potentiometer to the right of the CRT.

The unit switches to battery operation when no mains voltage is present. Battery time is as claimed: about an hour when there is no connection to an LNB, forty minutes when an LNB is connected.

The monochrome CRT provides good brightness and contrast outdoors. If need be the top of the carrying case can be used as a hood to screen out daylight.

Satellite operation

The spectrum-analyser scanning is vertical, which is the opposite to the Prolink 3, but one soon becomes used to the change. Photo 3 shows the full low-band vertical spectrum for Eutelsat at 13°E, with the RTP (11.727GHz, IF 1.977MHz) and BBC World (11.117GHz, IF 1.367MHz) analogue services marked. The cursor is at the middle of the range, which would be displayed as expanded if the span/max button was pressed, with the span knob controlling the amount of expanded spectrum displayed.

Interestingly, the block of signals just above BBC World is of considerably lower strength. These are mainly analogue RA1 (Italy) signals from the older Hotbird 1 satellite, which produces weaker signals here in southern Portugal. Some digital transponders can be seen above 11.727GHz, but the level from the LNB when switched to low band drops off sharply – it’s intended to go to only about 11.7GHz.

Photo 4 shows Argentina ATV Channel 7 TV received from the NSS 800 series satellite at 40.5°W. This is a C-band signal at about 4.175GHz, which results in an IF at 975MHz. Fortunately Argentina still uses the Fubk test card a lot during our morning hours – it’s so rare to see a test card these days! The level display has been activated by pressing the volume control knob. To help with dish alignment an audible tone is available along with the level display. The analogue LED at the top right is fit to indicate that the lower, analogue scale at the top of the screen must be used.

With a C-band LNB the local oscillator frequency is above that of the wanted signal, rather than below as with Ku-band operation. The IF spectrum is therefore inverted, with the high-frequency signals producing lower IFs. As a result the video is inverted, so the standard/band switch has to be pressed to receive a picture.

LNB skew setting is simple. Find a suitable signal from the satellite and adjust the span of the spectrum-analyser display so that the signal occupies most of the screen. Select the opposite polarisation and rotate the LNB slowly until the signal disappears from the display.

Terrestrial operation

Use of the unit with terrestrial signals is very similar to satellite operation. Photo 5 shows ch. 21 reception of Moroccan TV with the signal level at just below 70dBµV and the frequency display showing 471.25MHz (ch. 21).

The line sync pulse outline can be seen superimposed on the newsreader’s face (the colour burst is not displayed): when the signal starts to become noisy, ‘grass’ begins to appear on the outline. I’ve found the sync pulse useful when adjusting the video level input to some RF modulators. Crushing when the level is too high is immediately obvious, as the pulse becomes shorter and distorted.

To obtain the maximum bar reading at the top of the screen for accurate signal measurement I found it necessary to adjust the fine tuning for maximum signal once the main tuning control had been used to find the signal.

Photo 6 shows a close-up view of Spanish TVE-2 (second network) reception in ch. 45 or 663.25MHz as the MC377+ likes to call it, with the signal level at 65dBµV.

The readings obtained should be checked by referring to the correction chart that’s supplied with each unit, see Photo 7. This shows that 1dB needs to be added to the 65dBµV reading obtained at 663.25MHz whereas 1dB should be taken off the 70dBµV reading obtained for Moroccan TV in ch. 21 (471.25MHz).

Photo 8 shows a Spanish ch. 48 (687.25MHz) terrestrial digital TV signal. We’ve no DTT
transmissions at present here in Portugal, so I’ve no experience of local reception. To measure the signal, press the blue digital button. The digital channel power can then be read directly from the top scale. In this example it’s just over 55dBμV. Virtually no correction is required.

The bottom dark blue bar display indicates the carrier-to-noise ratio of the signal, at just over 25dB in this case. The noise-limit LED at the lower right-hand side of the screen is lit, which according to the manual indicates that the noise floor is below that of the receiver, so the actual C/N ratio is greater than that displayed. Digital signal measurement in the satellite band is identical.

Photo 9 shows four slightly weaker Spanish digital terrestrial TV channels in chs. 66-69. The topmost channels are slightly stretched in comparison with the lower ones. This may be because the terrestrial tuner has reached its tuning limit and requires higher tuning voltages to tune in the higher frequencies.

**Video input**

Video and audio signals can be fed into the unit via a scart connector. This is helpful, though I’ve never had to use the feature on site with the MC377+. It has proved very handy at times with the Prolink 3 however.

Unfortunately the facility is activated only when the control voltage at pin 8 of the connector goes high, as is normal practice with TV sets. Often one wants to know if video is present at the output from a scart lead, and there may be no switching voltage at pin 8. You can force the Prolink 3 into the AV mode via an on-screen menu. I’m tempted to make up some sort of switching arrangement to apply voltage to pin 8 of the MC377+ to force it to switch to an external source.

Demodulated video and audio are available at the MC377+’s scart socket, though not when in the spectrum-analysery mode. This could be useful in some circumstances.

**Verdict**

We’ve found that the Promax MC377+ fulfils our daily requirements very well and that there are not many occasions when we need the Prolink 3 to measure a signal that the MC377+ is not able to handle.

The MC377+ is available from Alban Electronics Ltd., the current list price being £895 plus delivery and VAT. This is a lot less than the Prolink 3. As a special offer to readers Alban can supply the MC377+ at £800 plus delivery at £10 and VAT at 17.5%. The price includes the carrying case, mains lead, calibration chart and manual. It’s money well spent if you are in the TV/satellite aerial business. Alban provides a back-up service should any problems be experienced.

More information can be downloaded from the Promax website (www.promax.es). Questions can be e-mailed to sales@promax.es - I’ve found that you get very prompt replies.

The UK agents are Alban Electronics Ltd., 6 Caxton Centre, Porters Wood, St. Albans, Herts AL3 6XT. Phone number is 01727 832 266, fax number 01727 810 546, or you can e-mail albanelectronics@cs.com
A look at nanotechnology

Over the past few decades semiconductor manufacturers have been getting more and more on to their ICs, basically by managing to fabricate smaller and smaller transistors. But there’s a physical limit to this reduction process. Beyond a certain point, a different technology will be required. We already know the direction in which the technology is likely to develop, because a lot of research and development work is being carried out on it. I’m referring to what has come to be known as nanotechnology. The carbon nanotube, which can emulate the action of transistors at molecular level, was first devised by Sumio Iijima of NEC in 1991.

Definitions

Nanotechnology is loosely defined as the study of functional structures with dimensions in the 1-1,000 nanometre range. It is rapidly emerging as a distinct and very promising field of research. A nanometre is a thousand million times smaller than a metre $(10^{-9})$. You can envisage what’s involved in this way. If a tennis ball could be expanded to the size of the earth, its individual atoms would become visible and would be about the size of a grape. Some three-four atoms, lined up together, fit inside a nanometre.

Organic chemists have for a number of years been designing and fabricating nanometre structures, using chemical synthesis. During the last decade however developments in surface microscopy, silicon fabrication, biochemistry and computational engineering have converged, providing remarkable ways of understanding, fabricating and manipulating structures at the atomic level. Research in nanoscience is advancing rapidly, partly because of the intellectual interest in constructing matter and molecules one atom at a time, and partly because of the prospect of new technical capabilities, devices and materials and the business prospects they could bring.

While nanotechnology is rooted in chemistry, other disciplines are now contributing to the research. At present there appear to be three distinct though highly interdependent nanotechnologies, as follows.

1) Wet nanotechnology. This is the study of biological systems that exist primarily in a water-based environment and have self-assembly attributes. The nanometre-scale structures of interest here are genetic material, enzymes and other cellular components. In fact the very stuff of life!

2) Dry nanotechnology. This relates to surface science and physical chemistry, focusing on the fabrication of carbon structures (fullerenes and nanotubes, about which more later), also silicon and other inorganic materials. Unlike wet nanotechnology, dry techniques can involve metals and semiconductors. Electron conduction in such materials will not allow operation in a wet environment. It is electron activity that makes dry nanostructures so promising, as electronic, magnetic and optical devices. An objective is to develop dry structures that possess...
some of the self-assembly characteristics exhibited by wet ones.

(3) Computational nanotechnology, which refers to the modelling and simulation of complex nanometre-scale structures. This predictive and analytical computational power is critical to the success of nanotechnology, by reducing the development time required to achieve working dry technology.

Over the past couple of years or so there has been a steady trickle of announcements about 'things nano', bringing back memories of how we initially heard about the development of the transistor, then ICs, then processors, memories and incredible and then desktops, and subsequently the internet. All this is now everyday technology. Nanotechnology is likely to evolve in a similar way. It could be a time before the technology has an impact on day-to-day electronics - which is as well, as it will give us time to adapt to the changes involved. It's too early to be talking about practical systems and devices, but there is already some history and we can report on the latest developments in this field.

**Fullerenes**

During the last decade of the twentieth century two major discoveries that are at the heart of nanotechnology were made. These are fullerenes and nanotubes. What exactly are they?

We've known about carbon for as long as we've known about fire. But the element keeps revealing new secrets. The fullerene is one such. It has implications for physics, chemistry and engineering, and the potential is only just becoming apparent. The rather odd name comes from the architect R. Buckminster Fuller, who designed and built the first geodesic dome structure for Expo '67, Montreal. The geodesic dome contains pentagons as well as hexagons, and in this respect resembles the carbon structure now known as a fullerene.

Natural carbon is the basic element of all living substances. Two pure forms are well known: graphite and diamond. Fullerenes are a third in the family. A fullerene is a large, carbon-cage molecule with a highly symmetrical structure, see Photo 1. It's hollow inside, the surface consisting of regular polygons of atoms - this closed molecular structure has been given the name 'atomic microcushion'.

By far the most common fullerene carbon structure is C_{60}, which is often referred to as a 'buckyball' - another reference to Buckminster Fuller. But C_{60} is only one molecule in the family of fullerenes: C_{28}-C_{240} have so far been detected. These molecular cages are very small, having a diameter of about a billionth of a metre, or six-ten times the size of an average atom. A C_{60} molecule consists of sixty carbon atoms, each of which has the same number of neighbours, all bonded together at the same relative angles in a structure rather like the shape of a football. The shape is called a 'truncated icosahedron', which is another way of saying that it consists of twenty hexagons and twelve pentagons.

There was much excitement when fullerenes were first discovered, because of some practical applications that were envisaged. There was speculation for example that buckyballs would make great lubricants, acting like small ball bearings between other molecules. Then there was the thought that drugs could be held inside the cages, targeted at various areas inside the body when released by a triggering mechanism. Another prospect is held out by the fact that when a single atom of gadolinium is inserted inside a buckyball its electrical resistance changes. Further, when pure C_{60} is doped with certain other atoms it becomes superconducting at high temperatures. So far however commercial applications of fullerene-cage molecules have yet to appear, despite efforts by research giants such as IBM, Xerox and DuPont.

**Nanotubes**

Nanotubes are a designed variant of the fullerene. The latter tend to form when a graphite sheet is 'rolled up', adding pentagons that create curvature. Each molecule becomes a cage (soccer-ball) structure. Carbon nanotubes - see Photo 2 - can be considered as elongated fullerenes with the ends cut off. This arrangement is referred to as a single-walled nanotube (SWNT). Instead of the combination of hexagons and pentagons that form a ball, the atoms in a straight-sided nanotube are arranged as sheets of hexagons. The result is a material that's quite different from the fullerene type, with extraordinary properties. A vital feature is that the properties depend on how the sheets are rolled.

If the sheet is rolled so that the hexagons line up straight along the nanotubes' axes, the tubes act as electrical conductors - like metal. If the sheet is rolled on the diagonal, with the hexagons spiralling along the axes of the nanotubes, they become semiconductors, with similar properties to the material at present used to make transistors and diodes. These unusual mechanical and electrical properties occur because each carbon nanotube is one giant molecule.

Photo 3 shows a comparison between various carbon molecular structures - diamond, graphite, C_{60} fullerene and 10, 10 nanotube.

**Development work**

Electronics is still overwhelmingly silicon-based, and it will take time for corporate thinking to get around to the new molecular upset in the form of carbon nanotubes. Initial developments will probably be in specialised fields such as biological applications, or space technology where weight and durability are more important than cost.

The nanoscale science group at the IBM Research Centre in the US is one of those at the cutting edge of this new technology. It has developed ways of manipulating nanotubes so that they work as electronic devices, but there are still many problems. For example the current passing through a nanotube semiconductor can vary with environmental conditions - a vacuum say, or when exposed to oxygen, or even when there is contact with another surface. When the shape of a nanotube is altered its electrical characteristics change, which may be the reason for such problems. Although the theoretical model of a nanotube has beautiful symmetry, practice may be somewhat different. It's possible that at present nanotubes routinely have defects, making specific electrical performance difficult to determine. So practical nanotube semiconductor device manufacture may be some time off.

Nevertheless the IBM researchers have created a simple logic circuit based on a carbon nanotube field-effect transistor. The claim is that such transistors are powerful enough to make large-scale ICs worthwhile.

Metal atoms can be added to the carbon structure to produce metal-carbon tubes, which have some interesting characteristics such as switching from insulation to metallic depending on the shape of the cylindrical region. Tubes don't have to be rolled 'straight', with the carbon chains forming circles to produce a cylindrical surface. They can be rolled with a twist, so that the carbon chains spiral along the cylinder, looking rather like a twisted bread stick. As the tube twists, it alternates between metallic (conducting) and insulating states.

Current nanotubes, smaller than strands of DNA, can be further reduced in size.
NEC researchers in Japan have achieved an 0.4 nanometre width, which represents the theoretical minimum limit.

**Possible applications**

Quite a number of possible applications, in various fields, have been suggested. Chemists hope to construct what are referred to as ‘bioreactors’. A nanotube could serve as a tiny test tube to hold a reagent (a substance with certain characteristic reactions) that could be used to carry out chemical analysis. Nanoscale machines such as pumps might be used to squirt the chemical where needed. A military application could be as a detector of poison gas or chemical weapons. Similarly, in the environmental field, water, soil or air could be monitored in the field to save sending samples to the laboratory for analysis. A device called a ‘nanogenerator’ has been devised and tested on mice. The tube holds a single highly-potent radioactive atom attached to an antibody that serves as a homing device to a cancer cell. Once it’s inside the cell, the atom breaks down, releasing high-density particles that destroy the cell.

Nanotubes can store hydrogen by absorbing it and packing it more densely than with present gas-compression methods. This could be the basis of a fuel-cell powered vehicle. There is hope that a string of metal atoms could be inserted down the centre of a cylindrical carbon cage, thus producing a ‘nanowire’ with incredible strength – the ultimate carbon fibre.

Chemists at Harvard have developed what they refer to as a ‘crossed-nanowire field-effect transistor’ which is readily applicable to high-density integration without using lithography. While it’s likely that by the end of the present decade lithographic processes might make it possible to produce a billion transistors on a chip, potentially a trillion carbon-nanotube transistors could be formed in the same space.

**Nanotube transistors and SRAMs**

Early attempts at producing a nanotube transistor resulted in a gain that was usually well under unity. The technology has moved on however, with improvements in thinning the oxide layer used as the gate area. This makes possible a gain of between 10 and 20, with transistors that can be used for making things like and and or gates and standard flip-flops (the basic memory unit).

Molecular logic has long been an aim in computer research. A research team at Delft University, the Netherlands, has claimed success if the is field, with the prospect of logic circuits that run at speeds from MHz to THz (tera Herz).

Various organisations have announced the development of carbon-nanotube transistors (CNTs). Current work aims at reducing the relatively large contact areas with their consequent high capacitance, which reduces operating speed.

When two Bell Labs scientists discovered the transistor effect in 1947 the device they created was as tall as the face of a wristwatch. Now a three-member Bell team at Lucent Technologies, consisting of physicist Hendrik Schon and chemists Zhenan Bao and Hong Meng, has made a single-molecule transistor – small enough for ten million to fit on the head of a pin. It was made of an unconventional organic semiconductor material using a novel fabrication technique, the channel space being one molecule.

The Bell team created what they termed ‘conjugated molecules’ from a carbon-based organic semiconductor material, known as thiols, that includes hydrogen and sulphur. Clearly the main problem in making nanotransistors is fabricating electrodes that are separated by only a few molecules, and then attaching electrical contacts. The Bell researchers overcame the problem by using a self-assembly technique and clever design.

A notch was carved in a silicon wafer and a layer of gold was deposited at the bottom to function as one of the three electrodes. The wafer was then dipped in a solution that contained a mixture of thiol molecules and some inert organic molecules – the inert molecules were added to dilute the concentration of thiols. This solution was allowed to dry. As it evaporated, a film exactly one molecule thick was left on the gold electrode. By careful adjustment of the ratio of thiol to inert molecules, it was possible to ensure that just one active molecule was present in the area on top of the gold electrode. A second gold electrode was deposited on top of the film, with the transistor’s third electrode at one side of the notch.

This self-assembly technique creates devices that are a hundred times smaller than those produced today, using the most advanced lithographic techniques, with a distance of about 1-3 nanometres. The size of a single molecule, between the transistor’s electrodes. Compare 1 nm, or 0.0013 μm, with the size of today’s latest commodity-chip lithography process, at 130nm – quite a difference! It’s claimed that the chemical self-assembly technique is relatively easy to implement, is inexpensive and, unlike silicon, does not require the clean-room technology currently used by chipmakers.

The Bell team has demonstrated molecular-scale transistor switching and amplification, and a two-transistor arrangement that acts as a voltage-inverter circuit.

An Infineon team lead by Dr Wolfgang Honlein, senior director of nanotechnology research, has modified a standard silicon IC production line to enable CNTs to be fabricated at predefined locations. Previously it was difficult to combine methods used to produce CNTs, such as laser ablation and arc discharge, with normal semiconductor manufacturing technology. According to Dr Honlein, “it’s very possible that nanotube technology could completely replace silicon-based semiconductor technology”. The low resistance of CNTs allows current flow up to three orders of magnitude higher than would melt copper. This is particularly important, as semiconductor scientists expect that within ten years the current densities in IC conductors will approach the point at which they fail thermally. CNTs would then be a saviour.

**Even smaller**

When it comes to atomic physics, a molecule is quite a large thing. In time, it may be possible to go a step further. California Nanosystems has reported that it can now continuously control the spin of an electron. According to the company the way to appreciate this is to think in terms of “spin engineering semiconductors” as opposed to current “charge engineered” devices. Spin-engineered electronics would be extremely fast and very dense, with low heat dissipation because only the spin of an electron changes. The heat required to flip the spin of an electron is infinitesimal in comparison to moving the charge in wire back and forth. Logic control could be achieved by spin variation, and could be stored in a semiconductor system that runs at far higher frequencies than today’s technology, working at room temperature.

When you consider the heat generated by millions of transistors in current chip design, a limiting factor with regard to future development, the spin-control approach could be the solution and take us into a totally different electronic world.
HELP WANTED


Wanted/for disposal: Require a U1 C7907 four-terminal TO220 device that's used for motor control in the Phillips N4520 reel-to-reel tape recorder. Anyone know a source? Have for disposal a Phillips three-socket V300 video camera with power supply and an N1520 electronic-edit VCR with many tapes, both free to collect. Phone Steve Ball on 01733 347 678 (Peterborough).

For disposal: An Alba mono TV Model T1924 (Thorn 1500 chassis) with original stand. Has new tube and is in excellent working order. B. Borrow. Borrow TV, 27 Russell Rise, Luton, Beds LU1 5ES. Phone 01522 734 501.

Wanted: Circuit diagram for the Matsui 14in. TV Model 1407. P. Guarini, 31 Alderson Avenue, Rawmarsh, Rotherham S62 7DE. 01709 371 188.

Wanted: Circuit diagrams for the Goodmans MS388 Micro System Hi-Fi reference HM0180103032, or details of where these could be obtained. Len Winstanley. Please e-mail: lenwink@blueyonder.co.uk

Wanted: Remote-control unit for the JVC VCR Model HRJ400EK, with LCD panel. Michael J. Levy, 19 Tottemhoe Close, Kenton, Harrow. Middx HA3 0HS. 020 8907 3620.

For disposal: 26in. IIT TV set in perfect working order complete with remote-control unit. The chassis is probably either the CVC20 or CVC30. The set is housed in a large wooden cabinet with stand, and features tambour doors. It's offered free to a museum or good home, but must be collected from Witney, Oxfordshire. Phone Morris Curtis on 01993 774 454.


Wanted: Jingle chip for the Harwood Kyoshu KTV41R. It's IC001, part no. 13-P47C434NP (ICMP47C43AN-CTS-140). Either a replacement or one salvaged from a faulty motherboard will do.

Phone Dick Hagan (Home Electronics) on 01689 830 036 (Orpington, Kent).

For disposal: As I'm moving abroad I have reluctantly to dispose of Television magazines from Vol. 29 (1979) to the current copy, all in binders with indexes. Phone Ray on 01268 697 622 (Essex).

Wanted: Help with an intermittent remote-control problem with the Panasonic VCR Model NV-HD685. The handset seems to be OK, checked with TV sets. Could it be the sensor in the VCR and, if so, has anyone the type/part number? David Forfar, 26 Noel Gate. Aughton, Nr Ormskirk, Lancs L39 5EG. Phone 01695 420 950, e-mail forfar@ucan.ac.uk

Wanted: Motor assembly for a FIBO 90cm motorised satellite dish and any associated mounting parts. Would prefer in working condition, but interested in whatever you may have for this equipment. Phone Dave Robinson on 01295 814 367 (work) or e-mail davj.robinson@lineone.net

For disposal: Sony KV32WS2U complete. Micro panel damaged by water. rest of set and tuner OK. Phone Martin Scobie on 01803 293 187 (Torquay).

Wanted: Service manuals for the Thorn (Ferguson) 850 and 950 chassis, and any Decca monochrome, K-B and RGB TV manuals. Harry Todd, 12 Oakhurst Close, London E17 3PZ. Phone 020 8520 8003.

Wanted: Line output transformer for the Dell 1025HE monitor, part no. FM0638-1292-8001. Allan Horsfield, 2 Church Street, Baston PE6 9PE. Phone 01778 560 274 or e-mail a_horsfield@hotmail.com

Wanted: A number of the now obsolete Global A/DX Plus Astra 1D converters, for a project. Must be the type with integral switch fitted. Phone Peter Atkinson, Camera Television Centre, on 01797 225 457 (East Sussex).

Wanted: Line driver transformer (L537) for the Pye Red Box Model 25KX120/05L. Phone John Horswill on 01244 579 123 (Chester) or e-mail chorswillandco@n1direct.co.uk


Wanted: Remote-control unit for the Samsung VCR Model SI3260. Programmable remotes will do everything — except put the machine in the standby mode. Phone Arthur Tomkinson on 020 8903 5574 (Wembley, Middx) or e-mail arthur@atomkinson.demon.co.uk

Wanted: Mains transformer for the Advance OS240 oscilloscope, part no. AI/34289, new or second-hand. Duncan T. Kidston, 102 Fergus Avenue, Livingston, West Lothian EH54 6BG. Phone 01506 433 371.

Wanted: Band selector/tuning control processor type TMS3757ANL, as used in the Loewe-Opta C8500 chassis and Philips Model 10CX1120. Phone Brian Treleaven on 01603 738 236 (Norfolk).

Wanted: Focus potentiometer for the Fidelity Model CTV14R (ZX2000 chassis) — Egen type 875 90001 or 876 90001. Alternatively does anyone have the kit referred to by S. Simon in the April 1986 issue of Television, or details on using theLOPT from the ZX3000 chassis? Mike Cooper, The Belfry, 53 Trethosa Road, St. Stephen, St. Austell, Cornwall PL26 7PZ. Phone 01726 822 280.

Wanted: A visor for the Sinclair Microvision early mono portable and a playback head for the Sony TC355 open-reel tape recorder. The latter is marked # PP30-2902. Can anyone explain line output transistor overheating with the Hitachi Model CPT2278 (NP38CQ Mk 2 chassis)? All relevant capacitors and the line driver transistor have been replaced and several LOPTs have been fitted. Replacement line output transistors last only about five hours. W. Milne. 20 Graham Road, W. Wimbledon, London SW19 3SR. Phone 020 8524 9542.

For disposal: B&O TV Model 4402 (with 26in. 20AX tube and ultrasonic remote control), Philips VR2334 VCR (V2000 type) and various B&O audio equipment from the Sixties and Seventies. Tim Jarman, 7 Cadet Way, Church Crookham, Fleet, Hampshire GU52 8UG. Phone 01252 616 938 (evenings).
Servicing the Sony FE-1 chassis

The FE-1 was introduced in 1998 as Sony’s core chassis for 50Hz Nicam models. It has much-simplified circuitry and physical layout in comparison with its predecessors. Giles Pilbrow describes the technical features of the chassis and provides fault-finding guidance, including a list of known faults.

The FE-1, introduced in 1998, became Sony’s core chassis for 50Hz Nicam models, taking over from the BE3D and BE5 chassis for 4:3 sets. It’s much simplified in comparison with the BE3D, most of the circuitry being housed on the single main board A. The RGB output stages are on board C, Nicam decoding is carried out on board S1, while the small front PCB H1 is used for the control buttons and front AV inputs.

To date, the following models incorporate the chassis: KV21X5U, KV25S5U, KV29S5U and KV29X5U. The remote-control unit for all these models is type RM883. In addition Model KV29FX20U, with remote-control unit type RM887, is fitted with the FE-1A chassis. This has some circuit variations to drive a Wega-type flat-faced CRT.

**Standby operation**

One major difference from previous Sony designs is the use of two separate power supplies. A small, efficient standby power supply keeps the consumption in this mode to less than 1W. Thanks to the TOP209 chopper chip (IC609) from Power Integrations Inc. the standby power supply, see Fig. 1, has a very low component count. IC609 contains all the active circuitry, including a 700V MOSFET power transistor.

The mains input is half-wave rectified by D626 and D621 (type ERC04-06S), producing about 180V across the reservoir capacitor C638. This supply is fed via the surge-limiting resistor R627 to pin 2 of the standby chopper transformer T602. Pin 1 of the transformer is connected to IC609’s drain connection, at pin 5. A snubber circuit consisting of D629, D628 and C646 is connected between pins 1 and 2 of the transformer to limit spikes that might damage IC609.

Operation of IC609 is governed by the voltage at pin 4. This is used for both regulation and start-up. At switch-on there will be no voltage at pin 4. A comparator within IC609 detects this condition and connects an internal resistor between pins 4 and 5, charging C640 and C639. Once the voltage at pin 4 has risen to 5.7V, the internal resistor is disconnected and drive is applied to the internal chopper transistor. During normal operation D627 provides the voltage for pin 4 of IC609, derived from winding 2-4 on the transformer. The voltage at pin 4 is then used to control the duty-cycle of the supply. It should be
exactly 5.7V when the supply is in operation.

Winding 5-7 on the secondary side of the transformer feeds rectifier D632 which produces about 8V across its reservoir capacitor C641. This is filtered and fed to the TYA7805CTV 5V regulator IC608. The standby 5V supply produced by this chip is used to power the microcontroller chip IC001, the EEPROM IC004, the logical keyboard multiplexer IC005, the reset chip IC003, the standby relay IC601 and the infra-red sensor chip IC900 (on board H1).

Standby circuit protection
If there's an overload on the standby 5V supply the voltages produced by T602 will fall. Thus the voltage at pin 4 of IC609 will also drop. Once this voltage falls below 4.7V IC609 will revert to its own start-up mode, charging C640. When the voltage across this capacitor reaches 5.7V IC609 will attempt to operate normally again. If the overload condition is still present the trip cycle will be repeated. Tripping to the safe state will continue as long as the overload persists.

Operation of the excess-current trip can be checked by measuring the voltage at pin 4 of IC609. In the trip condition it will ramp between 4.7V and 5.7V every few seconds.

IC609 will also shut down if its junction temperature exceeds 145°C, returning to normal operation once the device has cooled.

The main power supply
The main power-supply circuit is based on a Sanken STR-P6654 chip, IC606, which produces a regulated 135V HT (B+) output in all models. Fig. 3 shows the circuit. The input to the bridge rectifier D601 and the feed to the degaussing circuit is via relay RY601.

A start-up voltage is provided by R608 and R67, which are connected to pin 4 of IC606. The IC will start to operate normally once the voltage at pin 4 reaches 16V. When the set is running D603, which is fed from winding 7-8 on the chopper transformer T603, takes over the supply to pin 4 of IC606. In normal operation the voltage at this pin is between 15V and 16.8V.

Voltage control for regulation is applied at pin 1 of IC606 from the secondary side of the circuit via the optocoupler PH601. An SE135 stabiliser (IC603) is used to drive the optocoupler. It produces a variable current output at pin 2 depending on the voltage at pin 1, which is fed via R617 from the HT line. An increase in the HT voltage increases the current drawn by IC603. The LED in PH601 then shines more brightly, increasing the conduction of the phototransistor in the device. The feedback voltage at pin 1 of IC606 then rises and the on time of the drive waveform it produces is reduced. This in turn reduces the HT voltage. A decrease in the HT voltage has the opposite effect.

The net result is that the operating frequency of the main power supply varies between 120kHz at zero beam current and 80kHz with a bright white raster.

Primary excess-current protection
A short-circuit across any supply derived from T603 will decrease all the output voltages, including the supply to pin 4 of IC606. When the voltage at this pin falls below 10V IC606 will stop working and restart. This cycle will be repeated until the cause of the overload has been removed.

Over-voltage protection
If the voltage-regulation loop fails, the output voltages will all rise. When the voltage at pin 1 of IC606 reaches 22.5V it will switch off the drive to the chopper transistor. Unlike the excess-current protection, this triggers a latch within IC606. The chopper transistor drive is then removed until the mains supply is interrupted.

The over-voltage trip operates very quickly. The best way to determine whether it is being fired is to use an oscilloscope to monitor the HT voltage. If this is seen to rise significantly above 135V then fall to zero, check IC603 and PH601. Another clue is that IC606's start-up circuit will still be operating, with the voltage at pin 4 ramping between 10V and 16V as the circuits within IC606 come to life, draw current (at 16V), then the voltage falls because of the loading placed on the start-up circuit.
Secondary excess-current protection

Additional protection is incorporated to shut the set down in the event of a problem in the line output stage. The feed to the line output transformer T511 is via R572. Any increased loading will increase the voltage developed across this resistor. Once the voltage exceeds about 1.2V Q571 will conduct, in turn switching on Q574, which is connected to pin 18 of the colour decoder, a time-base generator chip IC301. As a result its line drive output will be disabled.

The excess-current signal produced by Q571 is also fed to pin 52 of the microcontroller chip IC001, which reacts by putting the set into standby via Q601/RT601 and indicating the presence of the fault by flashing the standby LED twice. To avoid false triggering, the microcontroller chip ignores the voltage at pin 52 for the first two seconds after switch on. Should the excess-current circuit be triggered during that time, the error code (LED flashes) produced will not be 2 but a code associated with no line drive, such as 4 (vertical protection) or 5 (no audio grey-scale feedback).

Fault finding

Once the excess-current circuit has operated it can be difficult to determine the cause, as the microcontroller chip has switched off the main power supply. The best way to tackle this is to disconnect pin 3 (HT) of the line output transformer. In this condition the trip should not operate and, if the problem is in the line output stage, the LED will no longer flash twice. It might flash four times to indicate that the field scanning no longer works.

If the standby LED continues to flash twice with pin 3 of T511 disconnected there may be a problem with the protection circuit. The resistors around Q571 occasionally change value, giving rise to an error code of 2. Check R541, R573 and R575, which are all 100kΩ, and R543 (47kΩ).

If the line output transistor or transformer has failed the current-sensing resistor R572 (1Ω, 2W) may have gone high in value. The result will be spurious shutting down.

Field output stage

The field output stage is based on an STV9379 chip, IC501, a device that Sony has used for some years. It gives little trouble, the usual cause of problems in this area being dry-joints. Q501 and Q575 are incorporated to detect field collapse. Should the field flyback pulses disappear Q575 will switch on, taking pin 15 of the jungle chip IC301 low. Pin 15 is connected to the internal V-protect register, which is regularly checked by the microcontroller chip. When the microcontroller chip detects a field problem it will mute the picture and flash the standby LED four times. Unlike previous Sony models, the set will remain on and not go to standby. If the line output stage is not running and the LED flashes four times, investigate other possibilities such as the excess-current trip circuit or no operation of the main power supply.

The line timebase

The line timebase is straightforward. IC301 produces a 5V peak-to-peak line drive signal at pin 19. This is fed to the base of the 2SC2688 line driver transistor Q535, which is coupled to the base of the 2SD2539 line output transistor Q533 via the driver transformer T531.

It is always a good idea to check the soldering in this area, as dry-joints at Q535 and T531 can be the cause of line output transistor failure.

East-west correction

A 2SK2251-01 MOSFET, Q532, is used to drive the EW diode modulator circuit. To reduce heat dissipation, the input to Q532 is a pulse-width modulated signal that's generated by an LM393N comparator chip, IC531. This IC receives a parabolic waveform input at pin 5 and line-frequency pulses at pin 6 (from pin 1). The duty cycle of its output therefore varies on a line-to-line basis, depending on the amplitude of the parabolic waveform. To stabilise the width, pin 5 of IC531 is also connected to the ABL output from the line output transformer (pin 11).

When there are width or pincushion-distortion problems it's a good idea to try the service-mode adjustments first (after noting down the existing values!) as some problems could simply be the result of misadjustment or memory corruption.

If Q532 becomes excessively hot, check replacing L535, C547 (750nF, 200V), C536 (1μF, 200V), T532 and L537. Not all these components will be fitted — it depends on the tube. Some of the coils may be linked out. The coils may show signs of overheating after a short period of use, possibly being warm to touch. This indicates shorted turns. The capacitors are a little harder to check: a capacitance meter may well give them a clean bill of health when they are actually faulty!

Audio

Audio signal detection is carried out by the IF chip IC101 (the exact type varies with model). The demodulated 6MHz mono audio output should be present at pin 8, the 6.552MHz Nicam carrier output at pin 12. Both signals are passed to IC1101 (TDA8753P) on board S1. IC101 also receives audio from the AV inputs as follows: from scart socket 1 at pins 33/34, and from scart socket 2 plus the front AV inputs at pins 36/37. This chip has a crystal (X1101) connected between pins 18 and 19; no adjustment is needed, as X1101 is trimmed by varicap diode D1101 whose control voltage is derived from the Nicam error rate.

L and R audio outputs appear at pins 61 and 60 respectively of IC1101. As this IC operates from a single 5V supply, there is insufficient audio voltage swing to drive the audio output chip. So an audio preamplifier chip, IC1102, is included. The output from this is passed to IC201 (TDA7495) on the mainboard.

The jungle chip

IC301, a Sony CAXA060AS chip, carries out colour decoding/video processing and timebase signal generation. There are two RGB inputs and two video inputs, and the chip can decode any colour standard signal. It's operated at 9V under the control of the IC bus.

RGB output stages

The RGB output stages are on the CRT base panel (board C). In each channel there's a cascode stage consisting of a 2SC1740 transistor driving a BF871 transistor. The output from this is fed to a BF421 emitter-follower transistor that's also used for auto-greyscale sensing. The collectors of these emitter-follower transistors are connected to a common line which is labelled IK. This abbreviation is found in many Sony circuits: I means current and K cathode. The IK line is connected to pin 21 of IC301.

If the IK signal is missing or distorted, here will be no picture. To indicate that there's an IK problem, the microcontroller chip flashes the standby LED five times (IK faults do not shut the set down). It's rather difficult to check the operation of the IK circuit, as any problem on board C is likely to result in a blank screen. The best method is to connect one channel of an oscilloscope to the IK line and the other to the R, G or B input to the board, then connect the trigger input to stable field-frequency pulses, from the field scan coils for example. It should be possible to see the individual R, G and B test lines produced by IC301. The test pulses fed to the board should be more or less identical, separated only by time. A correct IK signal will contain all three of these test lines. If there's a problem with the IK circuit, one line will be missing.
Fig. 3: The main power supply circuit used in the Sony FE-1 chassis.

Comparison of the timing of the missing line and the input signals will show which channel to concentrate on.

The circuitry on board C is generally reliable. It can suffer as a result of tube flashover however. In this event it is worthwhile checking all the semiconductor devices on the board. Pay particular attention to the three BF421 emitter-follower transistors. If damage has occurred on board C, the 3.9V zener diode D308 on the main board may well be short-circuit.

Control system
The FE-1 chassis uses a Philips SAA5497PS microcontroller chip (IC001). It’s based on the popular 80C51 with additional teletext decoding and on-screen display capabilities. An external 8K 12C EEPROM, IC004, holds the tuning memory and service adjustments. To prevent data corruption, IC004 has an additional control connection at pin 7: this has to be taken low before data can be sent to the device. The 12C bus is connected to CN001 at the rear of the chassis, enabling a set to be interfaced with a PC for diagnostics.

Pin 1 of IC003 provides the microcontroller chip with a reset pulse. The pin is low at power on, until the 5V supply has stabilised. The reset signal is also used, with Q014, to control the supply to the EEPROM – Q014 applies power to IC004 only when the reset pulse ends. This is an additional safeguard against memory corruption. The reset pulse applied to IC001 is inverted by Q010. Contrary to the information in the service manual that the reset pulse at pin 43 of the microcontroller chip is active high, the pin is normally at 0V, being held at 5V at switch on.

IC001 has an analogue input at pin 11. This is used to monitor the front keyboard and pin 8 (control) of each scart socket. IC005 enables all these functions to be carried out by one pin of IC001. It’s an analogue switch that multiplexes the different control signals for application to pin 11. IC005 can fail, the result being that the set continually changes channels, adjusts the volume or switches to AV. These symptoms can also be caused by a faulty tactile switch on board H1. To prove which item is the cause, disconnect SW902: if the problem persists, IC005 is faulty; otherwise, replace the switches.

Teletext
Teletext decoding is completely integrated into IC001. Video from pin 6 (MONOUT) of the jungle chip is fed to pin 24 of IC001. The same signal is used to feed the scart socket, via buffer transistor Q405. The no-teletext symptom (P100 only) can occur because Q405 is short-circuit. Only two external components are required by the data slicer in IC001: C033 for black-level clamping, and R077 as a load resistor for the voltage reference.

A separate 5V supply is used for IC001’s teletext and other analogue functions. It’s fed to pins 38 and 39.

The service mode
Entry to the service mode is by using the key sequence shown in Fig. 2 while the set is in standby. The service mode is indicated by the presence of ‘TT’ at the top right-hand corner of the screen. Some two-digit handset codes have special functions – the more useful are listed in Table 1.
Table 1: Useful TT codes

<table>
<thead>
<tr>
<th>Code</th>
<th>Meaning</th>
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<tr>
<td>00</td>
<td>Cancel service mode and return to normal operation</td>
</tr>
<tr>
<td>08</td>
<td>Shipping condition (resets customer settings to 'as new' values)</td>
</tr>
<tr>
<td>11</td>
<td>Sub-contrast adjustment</td>
</tr>
<tr>
<td>12</td>
<td>Sub-colour adjustment</td>
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<tr>
<td>13</td>
<td>Sub-brightness adjustment</td>
</tr>
<tr>
<td>14</td>
<td>Teletext horizontal position adjustment</td>
</tr>
<tr>
<td>18</td>
<td>Disables/enables inter-station muting</td>
</tr>
<tr>
<td>24</td>
<td>Sets sound IF and tuner band for UK</td>
</tr>
<tr>
<td>31</td>
<td>Disables/enables 15 minute auto-standby function</td>
</tr>
<tr>
<td>34</td>
<td>Toggles teletext character set between east and west (UK = west)</td>
</tr>
<tr>
<td>35</td>
<td>Toggles between wide and 4:3 CRT</td>
</tr>
<tr>
<td>36</td>
<td>Enables/disables velocity-modulation circuitry</td>
</tr>
<tr>
<td>49</td>
<td>Reprograms EEPROM to factory defaults (program 59 only)</td>
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Table 2: Error codes

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<th>LED flashes</th>
<th>Problem</th>
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<tr>
<td>2</td>
<td>Secondary excess-current protection</td>
</tr>
<tr>
<td>4</td>
<td>No field deflection</td>
</tr>
<tr>
<td>5</td>
<td>No auto-greyscale feedback</td>
</tr>
<tr>
<td>6</td>
<td>ICP clock or data low at power-on</td>
</tr>
<tr>
<td>7</td>
<td>EEPROM (IC004) gives no ICP bus acknowledgement at power on</td>
</tr>
<tr>
<td>8</td>
<td>Jungle chip (IC301) gives no ICP bus acknowledgement at power on</td>
</tr>
<tr>
<td>9</td>
<td>Tuner gives no ICP bus acknowledgement at power on</td>
</tr>
<tr>
<td>10</td>
<td>Nicam decoder chip (IC1101) gives no ICP bus acknowledgement at power on</td>
</tr>
</tbody>
</table>

Geometry and grey-scale adjustments are carried out by pressing the handset’s ‘menu’ button then choosing the appropriate option. Once an item has been adjusted it’s memorised automatically.

EEPROM reset
The EEPROM’s contents can be returned to factory-default settings by selecting programme 59, entering the service mode then, at the TT- prompt, entering 49 followed by 24 (for the UK) and 08. Finally, switch off at the mains.

Error codes
Table 2 lists the LED-flash error codes and their meanings.

The error-history display
Some intermittent faults fail to occur when a set is brought into the workshop. The set is able to count the number of times any particular error code has appeared. To display this information, put the set in standby then use the key sequence shown in Fig. 4.

The resulting display shows the number of times a fault code has occurred, up to a maximum count of 255 for each code. If the set has been in use for some time, there may be error counts in some or all locations. To reset the error count enter 8 then 0 on the remote-control handset.

Known faults
The following is a summary of fault conditions that have been experienced with this chassis.

No power at all (standby power supply not working): IC609 (TOP209) faulty. Also check C640 (47µF, 25V), D631 (MTZJ-12B), D628 (P6KE200), D629 (UF4005PKG23) and R627 (4.7Ω, 5%, 0.25W).

No power but relay operates (main power supply not working): IC606 (STR-F6654) faulty. Also check R659 and R660 (0.33Ω, and 0.39Ω respectively, 5%, 3W), R603 (0.1Ω, 0.5W fusible) and C625 (100µF, 25V).

Main power supply starts up but shuts down very quickly: IC603 (SE135N) faulty.

Set shuts down at start-up with 2, 4 or 5 flashes from the standby LED:
Check R541, R573, R575 (all 100KΩ) and R543 (47kΩ). These are all 5%, 1/10W chip resistors.

Set shuts down intermittently with 2, 4 or 5 LED flashes after displaying a bright red, green or blue raster: The CRT is faulty.

Set continually changes channels or adjusts the volume: S900, S901 or S902 on board H1 or IC005 (CD4052BCM-FL63) on board A is faulty.

Dark or no picture: R516 (56kΩ, 5%, 0.5W) or R517 (27kΩ, 5%, 0.25W) is high-resistance or open-circuit.

Excessive picture width: Q532 (2SK2251-01) is short-circuit. Check the other components in the EW circuit before returning the set to the customer.

A vertical band of interference is visible on the left-hand side of the screen with dark scenes: Add a 1,000pF, 2kV capacitor (part no. 1-161-731-81) in parallel with D539 in the EW diode modulator circuit.

A vertical purple line is visible on the picture: Replace IC301, type CXA2060AS, part no. 8-752-082-35.

Pressing the screen-format button displays wide, smart, zoom and 4:3 modes yet these settings have no effect on the picture: Enter TT35 in the service mode to select a 4:3 CRT.

One colour missing with teletext and on-screen displays: Check Q009 (red), Q007 (green) or Q008 (blue) as appropriate. These transistors are all type 2SC4212K.

No teletext, P100 only: Q405 (2SC2412K) is short-circuit.

No sound from cold: Check C618 (2.200µF, 25V).

No sound: Enter TT24 in the service mode. Alternatively Q202 (2SC2412K) could be leaky.

No remote-control operation: Check the remote-control sensor IC900 (type SDX1981-51, part no. 8-742-014-11) and D907 (MTZJ-9-1A) on board H1 and D023 (MTZJ-5-6B) on the main board as necessary.
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<td>25</td>
<td>1.2m 2 Phono Plug to Phono Plug Lead</td>
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Digital Satellite Receiver Repair Kit

LATER PSU TYPE REV 03

DSO - 0375 REV4

DSO - 0385 REV 5

Order Code: SATKIT34B

Price £ 10.00 + vat

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Check out our New Online Catalogue at [www.grandata.co.uk](http://www.grandata.co.uk)
Thomson's ICC17 technology

Part 3 of Mark Paul's description of the circuit technology used in this chassis deals with the signal-processing sections.

In this third installment in the series we will take a look at the signals-processing arrangements. The final part next month will cover the microcontroller, audio and signals-switching sections.

Multiband tuner

The Thomson CT15010 tuner used in this chassis is quite complex, with a TUA6010X IC that carries out, under the control of the IC bus, band switching, oscillator selection and frequency-synthesis tuning. The chip incorporates an IC interface and has separate VHF and UHF inputs. It operates with a 4MHz reference crystal that's connected to pins 13 and 14. Use of this reference frequency enables the tuning to be controlled to within 62.5kHz. The IF output is fed to a bipolar buffer transistor whose output is capacitively coupled to pin 11 of the tuner. There are also three gain-controlled MOSFET RF amplifier transistors in the tuner, one for each band. Band coverage is 48.25-112.25MHz, 119.25-399.25MHz and 407.25-863.25MHz.

The IC bus is connected to pins 4 (SCL) and 5 (SDA) of the tuner which requires two supplies, 5V at pin 6 and the 33V tuning supply at pin 9. There’s an AGC input at pin 1, the IF output appearing at pin 11. The tuner’s power consumption is approximately 375mW.

The IF strips

The IF output from the tuner is filtered to separate the vision and sound signals. Processing is then carried out by a 64-pin, flat-pack Philips TDA8855H chip, IV01, which incorporates separate vision and sound IF strips, a multi-standard colour decoder and, as mentioned in Part 2, the timebase generators. The IF section is multi-standard, using carrier-regeneration signal demodulation. This enables all standards used in Europe, including B/G/H/J/LL/DKK', to be accommodated. Switching control is via the IC bus. AM sound demodulation covers 45-6.5MHz. IV01 provides tuner AGC with rollover control and AFC via the IC bus. Fig. 1 shows in simplified block diagram form the signals sections of IV01.

The vision IF input at pins 1 and 2 of IV01 comes via a SAWF, FI10, which provides a balanced output. The signal is then amplified and demodulated, using a PLL carrier-regeneration technique. The carrier reference frequency is produced by a frequency and phase detector circuit that controls a voltage-controlled oscillator which operates at twice the IF. An inductor (FI30) connected to pins 13 and 14 is used for tuning. The resultant carrier is divided and used by both the video demodulator and the AFC detector, the AFC information being sent to the microcontroller chip IR01 via the IC bus. AFC filtering is carried out by an RC network that’s connected to pin 15.

The demodulated video is amplified and passed through a muting circuit before it appears at pin 16 of IV01. A feed between the amplifier and mute circuits goes to the AGC detector, which checks the sync pulse amplitude and peak white video to set the AGC voltage fed back to the tuner. The AGC reservoir capacitor is connected to pin 6.

The video output at pin 16 is fed via a buffer transistor to a sound trap and is then AC coupled by C163 (10uF) to pin 24 of IV01. A SAWF, FI20, is also used to provide in the sound IF feed to pins 8 and 9 of IV01, again with a balanced output. Prior to this there’s a trap which can be switched between 32-4MHz and 40-4MHz by means of transistor T110, which is controlled by IR01 (pin 42). The incoming sound IF signal is fed to two gain-controlled differential amplifiers. An AGC detector looks at both the AM and FM carriers and controls the gain of the two differential amplifiers to ensure that a constant IF signal is fed to the AM demodulator and the single-reference QSS (Quasi Split Sound) mixer. The reaction time of the AGC detector is set to ‘slow’ for normal video conditions. If the vision IF signal drops however the reaction time is set to ‘fast’. In the FM mode the reaction time is set to fast via the IC bus.

A phase-multiplier technique is used to demodulate the AM sound, which is then passed through a low-pass filter to remove any trace of carrier harmonics. The output from this demodulator appears at pin 27 of IV01. It’s not relevant with UK transmissions of course.

The FM sound carriers (6MHz mono and 6.552MHz Nicam) are generated by the QSS mixer. In this stage the FM sound is mixed with the vision PLL reference frequency. The output is then passed through a high-pass filter to reduce the
residual video-signal components and finally appears at pin 11 of IV01.

The audio outputs from IV01 are fed to IS40 for further amplification and processing. We'll return to this next month. The output from pin 11 is level-adjusted by transistor TS01 before application to IS40.

**Video processing**

IV01 contains all the circuitry required to decode the selected video signal to produce RGB drive outputs. It includes the following:

Two video input selector switches for internal video and video from the AV1, AV2 and front-panel connectors (AV3). Two luminance/chrominance to CVBS mixers. Luminance and chrominance separation circuitry. A variable luminance delay line with peaking and coring compensation. A multi-standard chroma decoder: once the signal has been identified, decoding needs only two crystals, 4.433MHz for PAL/NTSC/Secam and 3.58MHz for 60Hz NTSC. Two RGB input selector switches for AV1 and OSD/text inputs. Continuous CRT cathode-current calibration circuitry, and RGB drive preamplifiers.

There's an I2C bus transceiver for interfacing with the microcontroller chip IR01. The tuner, AV1 and AV2 video signals and the Y/C signals from AV1 and the front-panel connector are fed to the input selector switches. These, under the control of IR01, are selected and processed into Y/C components then converted to RGB. Selection is then made between the processed RGB signals and the external AV1 RGB inputs. Further processing occurs before the RGB outputs are sent to the CRT board.

A new circuit has been introduced in the video processing - blue stretch, which adjusts the level of the red and green signals to improve the white performance. The switched 8V line is connected to pin 23 to supply the video processing circuitry, with CV02 (100uF), CV03 (10uF) and LV02 for filtering.

Several integrated alignment-free filters and traps must be set and calibrated prior to any processing. Before the centre frequency of these traps and filters can be set, an initiation process must be carried out under the control of IR01.

IR01 downloads data relating to the two crystals QC01 and QC02, which are connected to pins 31 and 50 of IV01 respectively. Once this data has been logged, IV01 verifies the presence of the filters. On identification, the required crystal oscillator is calibrated and its frequency is used as a reference for the filters, traps and colour-difference signal demodulators. The line output drive at pin 56 is disabled while this process is taking place.

The decoded/switch-selected RGB signals are fed to a black-stretch circuit that monitors the incoming luminance - it looks for differences between the darkest point in the signal and the back-porch blanking level (during the burst period). Black level is detected by means of an internal integrating capacitor. Once detected, a correction value is added to the luminance signal to increase the overall grey-scale range. The value added depends on the luminance signal level. The black-level stretch circuit can be made inoperative via the I2C bus and customer menu.
Contrast and brightness control are applied following the black-level operation, also beam-current limiting (BCL) and average white level (AWL) compensation.

The beam-current information fed to pin 34 is detected at the earthy end of the EHT system in the line output transformer, across RL07/CL08 (see Fig. 6 last month, page 603). RL09 and CL09 provide integration while zener diode DL09 provides protection.

Blue-stretch is the next step in the signal processing. When the incoming RGB level exceeds 80 per cent, the red and green signals are reduced by approximately 17 per cent. This gives improved white rendering.

**Continuous cathode compensation**

The final processing before the RGB outputs leave IV01 is continuous cathode calibration (CCC), or automatic cut-off (black-level) adjustment. Information from the CRT base panel circuitry is fed back to pin 30 of IV01 via a simple T filter (RV08/RV15/CV14) to provide this black-level compensation/calibration. The action of the CCC loop is based on two test signals which are generated within IV01 on alternate fields to check beam-current leakage and black levels.

The process can be controlled by IR01 via the IIC bus, or by IV01 itself in the automatic mode. The RGB outputs are blanked while black-level detection is taking place. This is relevant when a no-picture fault is being investigated. CCC provides compensation for variation in certain CRT gun characteristics. CCC operation is quite complex.

The loop has to be initialised before any adjustment takes place. First, IV01’s RGB outputs are blanked off. The +8V supply is then switched on and a 1-5-second counter is started. At the end of the allotted time the feedback current from the CRT base panel is checked until either 8 or 20µA is detected.

When either of these currents is detected a 2-5-second counter is started. Once the timer period has elapsed, the RGB outputs are switched on and the CCC-loop carries out the alignment process. This routine is called 'cold start'.

Normal CCC-loop operation then starts. The system generates the first of two test lines, and measurement and adjustment procedures are activated. At line 18 the CRT’s leakage current is measured. Next, the black level for each of the CRT’s three guns is checked – at line 20 for red, line 21 green and line 22 blue. A second test line is generated in the next field. The same measurements are carried out on lines 330, 332, 333 and 334. The results are compared with internal reference currents and are used to control the black-level current and driver stage gain for optimum tube performance, virtually during its life. To provide a good grey scale the black level is set at almost the CRT’s cut-off level.

The important feature of this type of two-point stabilisation is that both the offset and the gain of the RGB signal paths is controlled by feedback. The maximum cathode drive currents are fixed by the relationship between the internal reference current, the test pulses and the gain setting in each path. A 「CRT Warm Detect」 block monitors the 「warm-start」 condition.

When the incoming current exceeds 130µA, the RGB driver stages are released and normal two-point stabilisation is activated.

High-pass filter networks are included in each RGB output path from IV01.

**CRT base board**

Fig. 2 shows the circuitry on the CRT base board. The RGB output stages are incorporated within a Philips TDA6107Q chip, IB01. This contains three independent high-voltage amplifiers whose gain and DC offset voltage are fixed, feedback resistors, input resistor networks and a voltage-reference source. Pin 6 is used for the HT supply, pin 4 is connected to chassis and pin 5 provides the CCC feedback information. The outputs at pins 7, 8 and 9 are connected to the CRT cathodes via series inductor-resistor networks, with diodes connected to the junction of these components to protect the IC against tube flashovers.

CRT switch-off spot suppression is provided by transistors TB01, TB02 and the associated components. In normal operation the base of TB02 is held high by the PO line, from pin 39 of IR01 via inverter transistor TR06. Thus TB02 and in turn TB01 are held conductive, and CB03 is charged via RB08 and DB04. The diode clamps the CRT’s grid voltages at +0.7V. At switch off the PO line goes low and TB01/2 switch off. The voltage across CB03 reverses, a large negative potential appearing at the CRT’s grids. The screen is therefore blanked and, because DB04 is reverse biased, the voltage remains negative for several minutes – until CB03 discharges via RB08 and RB07.

**Fig. 2: Circuitry on the CRT base board.**
Servicing the Mitsubishi TFS6705K monitor

This 17in. Trinitron-tube monitor’s production run lasted for several years. Large numbers were sold as the Dell VC7EN. In the concluding instalment in his series Donald M. Henry takes a look at the digital control system

In this concluding instalment we’ll take a look at the circuitry on the processor board and what it all does. Fig. 1 shows this area in block diagram form. There’s a processor (microcontroller) chip, IC101, an EEPROM (IC102), and many inputs and outputs: control of various functions is carried out via MUXes (multiplexers) and DACs (digital-to-analogue converters), with direct control of a few items.

The microcontroller chip IC101, type M38002M2, contains a central processor unit (CPU), registers galore, baud-rate generators, timers, serial and parallel ports, an area of working RAM and a ROM that contains the program code. It’s an 8-bit, 64-pin quad flat-pack device that’s also available in DIP (dual in-line) form. If you like data sheets, the web can be a fantastic source of information – sometimes too much! I downloaded a data sheet on the M38002M2 from www.mitsubishichips.com/data/datasheets/mcuc/mcupdf/um/e3800um.pdf and ended up with 173 pages!

At least, using the free Acrobat Reader software, you can print off individual pages of interest.

There’s a useful section on the software watch dog timer (SWDT), which helped to explain the purpose of the TA8030F chip IC103, which is a hardware WDT. There’s also some explanation of reset delays, and informative design hints on counter measures against noise. A lot of detail can be extracted: I discovered that the 2M2 part of the device’s number indicates that it has 384 bytes of RAM and is a mask-ROM version with 8,192 bytes of ROM.

Generating a display

At power-on or reset the CPU starts to read the code in the chip’s program ROM. It uses this program code to check the H- and V-rate inputs (at pins 6 and 17) and their respective polarities (at pins 51 and 52). These signals are derived from the H and V sync outputs from the PC’s graphics card. For a refresh on this, refer to Fig. 1, Part 2 (May issue, page 404). If the CPU detects a legitimate timing signal (within the limits described later) of identifiable H and V frequency, the program extracts certain data from the ROM. This data defines the various switch-selectable scan-control components that have to be brought into circuit. The data is neither factory-mode nor user adjustable. It’s classified as display-mode-dependent fixed data.

The microcontroller chip then activates the appropriate output port pins. For example, when looking at EHT generation in Part 3 we saw that C607 is open-circuited with H-rate signals above 38.8kHz. This switching is controlled by pin 49 of IC101. Similarly the s-correction capacitors C521-4 are brought into circuit in accordance with the H frequency: this is controlled by the outputs at pins 42-45, via buffer chip IC104 and the multiplexer chip IC502. The AFC network components are similarly controlled, by the outputs at pins 46-7. Line linearity relay RYS01 is activated by the ROM data when the frequency is above 44kHz. This control is exercised at pin 48. Depending on the V frequency detected, the vertical linearity components C404/5 and R404 and the precise resistor values connected to multiplexer IC450 are switched in and out of circuit under the control of pins 4 and 5 of IC101.

Multiplexer IC7V3, which also operates at frame rate, shares pins 4 and 5.

Multiplexed operation

The multiplexer chips that control the display-mode-dependent fixed components are addressed via pairs of select lines. For example with IC502, the multiplexer that selects H-osc and AFC network components, addressing is via buffers in the TD62504F chip IC104. The select line pair for the vertical linearity multiplexer is not buffered on the processor board: instead, Q452 and Q453 on the PWB-DEFL-SUB board provide buffering. Thereafter the pair is connected to the MC14052 multiplexer IC450, which in turn selects the relevant components (see Part 2, May)

IC450 shares its multiplexer select lines with IC7V3, which is part of the frame-rate sinc-genera-
Fig. 1: The circuitry on the processor board, shown in block diagram form.
tor. If, in some early production monitors, you don’t find IC7V3 on the PWB-DEFI-SUB panel it may be on a small piggy-back board, PCB-SINE.

Non-multiplexed control

The s-correction capacitors and the linearity coil are directly connected, i.e. there is no multiplexer chip, though the buffer chip IC104 also plays a part here. The tuning capacitor in the EHT generator circuit (switched in/out by Q605), and ‘fan-out’, the shunt-down circuit that activates Q953 should the fan speed fall, are buffered by transistors Q104 and Q103 respectively. IC101 also controls the degaussing circuit, at pin 41 via Q102 to the PWB-POWER-SUB board, where Q951 energises RY901 to pass AC through the degaussing coils for a few seconds.

Display-mode selection, cont

If the detected H and V frequencies match a recognised timing, the next step is determined by the H and V polarity. As previously mentioned, the exact display mode is determined by the combination of sync frequency and polarity. IC101 examines both to find out whether the signal conforms to one of six standard modes, see Table 1 and Fig. 2. In their manuals manufacturers usually specify timing in usecs and msecs: I’ve added frequency figures as these may mean more to TV engineers.

When a standard mode has been confirmed, IC101’s ROM program selects predetermined memory locations in the EEPROM chip IC102 (type M6M80021F – see later). IC101 then reads in the contents of these memory locations and loads them into its RAM area. Data on the RAM values is sent via the two serial ports to DAC chips to achieve the appropriate height, width, pincushion, key etc. settings.

When the monitor is new from the factory, the stored EEPROM values ensure that the timing of the line and frame scanning is such that the video appears to be centred on the screen – so long as the mode generated by the PC’s graphics card is standard. I’ve mentioned this point in earlier articles in the series, but it seems to be one that can never be made often enough. The microcontroller chip doesn’t care what the video content is, or even the time it arrives, so there’s no need for RGB information to be presented to IC101.

Timing tables are provided by manufacturers to show design and signal alignment conformity. Where the timing is found to be non-standard, the microcontroller chip allows for four sets of user-defined modes. Four user areas are reserved in the EEPROM for this. The user is free to adjust the picture as required for the non-standard mode, the results being stored in the EEPROM.

Common variables

Finally, brightness, contrast, RGB gain, RGB bias, DBF etc. are variables that are common to all modes. Brightness and contrast are very much user preferences, and the settings must be remembered between the last power-off and the next power-on – hence they are also stored in the EEPROM. Gain, bias and DBF, though not user adjustments, are factory-mode adjustable and must similarly be stored in the EEPROM.

Thus the adjustable items common to all modes, called non-mode-dependent variables, are stored in the EEPROM alongside the mode-dependent variable data. They are also read into the CPU and stored in RAM, and are fed out via the serial ports, in this case to DACs IC302, IC708 and IC452, IC304.

DAC connections

The multiplexer connections and those for other devices mentioned above have a nearly 1:1 relationship. That is, a pin from the microcontroller chip can be traced through to a specific item, and finding the cause of a particular digital-control fault is often possible using an ordinary meter. A DAC’s connections are in stark contrast.

When fault-finding in microcontroller and DAC circuitry it can be useful to think of certain groups of devices as being under the control of a particular output port. The DACs in the circuitry being consid-

Table 1: Signal timing for the six standard display modes

<table>
<thead>
<tr>
<th>Mode</th>
<th>H period µsec</th>
<th>H frequency kHz</th>
<th>H.a µsec</th>
<th>H.b µsec</th>
<th>H.c µsec</th>
<th>H.d µsec</th>
</tr>
</thead>
<tbody>
<tr>
<td>VGA 640 x 480</td>
<td>31-778</td>
<td>31-47</td>
<td>3-813</td>
<td>1-907</td>
<td>25-422</td>
<td>0-636</td>
</tr>
<tr>
<td>VGA 640 x 400</td>
<td>31-778</td>
<td>31-47</td>
<td>3-813</td>
<td>1-907</td>
<td>25-422</td>
<td>0-636</td>
</tr>
<tr>
<td>VGA 640 x 350</td>
<td>31-778</td>
<td>31-47</td>
<td>3-813</td>
<td>1-907</td>
<td>25-422</td>
<td>0-636</td>
</tr>
<tr>
<td>Apple Mac 1</td>
<td>20-676</td>
<td>48-37</td>
<td>2-092</td>
<td>2-462</td>
<td>15-754</td>
<td>0-360</td>
</tr>
<tr>
<td>Apple Mac 2</td>
<td>17-710</td>
<td>56-47</td>
<td>1-810</td>
<td>1-920</td>
<td>13-650</td>
<td>0-330</td>
</tr>
<tr>
<td>Apple Mac 3</td>
<td>17-710</td>
<td>56-47</td>
<td>1-810</td>
<td>1-920</td>
<td>13-650</td>
<td>0-330</td>
</tr>
</tbody>
</table>

Figure 2: Signal timing diagram, see Table 1.
ered control all the adjustable items such as width, brightness, gain, bias, height, DBF etc., so it helps to list adjustable functions related to each DAC, then map the set of functions to the relevant port.

In this circuit two serial ports, each with three connections (load/clock/data), address two separate pairs of cascaded DACs, from pins 53/4/5 and 56/8/9 respectively. These six interconnections control about two dozen functions.

Pins 53/4/5 are connected to the DACs IC302 and IC708, both type DAC8840 (see Fig. 1). The items they control are shown in Fig. 1. IC302 and IC708 are 8-channel, 8-bit CMOS devices for use with a three-wire serial interface: they are able to emulate eight variable-resistance controls. Some control operations, which work like a volume control, e.g. pincushion amplitude, have a signal applied to the relevant input. With others, e.g. RGB gain control, only a DC output control voltage is required: these use a reference-voltage input. Fig. 3 shows a functional block diagram of the DAC8840.

Pins 56/8/9 are connected to DACs IC452 (type M62358P) and IC304 (type M62359P). The former is an 8-bit, 12-channel DAC with buffered outputs, the latter an 8-channel version. The main difference between the Analogue Devices’ DAC8840 and these Mitsubishi DACs is that the latter provide only DC-control outputs and cannot emulate a variable-resistance trimmer — because there are no independent signal inputs. The analogue output range is variable between two reference levels, upper and lower.

To find data sheets, I’m in the habit of going to www.google.com and then launching a search based on the part number. Unless looking for spares, I head for the first .pdf file I see and, if the manufacturer’s name is in the title, I nearly always end up with what I am looking for. So why not try your own search for IC452 and IC304, then print out your own block diagram!

**Microcontroller inputs**

Apart from H and V sync inputs for analysis, the other inputs to IC101 are straightforward. There are ten push-button inputs, including reset and degauss, which are connected to pins 20, 21 and 25-32. The fan strobe input is connected to pin 11: the microcontroller responds by shutting down the power supply when this input is missing. Toggle switch SW9/1, on the PWB-POWER-SUB panel (see Fig. 3, Page 544, July), is earthed and is not connected to IC101 in normal use. The two active-low positions are connected to pins 39 and 40 of IC101, providing the factory mode (pin 39) or allowing the line oscillator to run without sync for setting up (pin 40). IC101’s clock crystal is connected to pins 22 and 23. A flyback pulse that represents the blanking interval arrives at pin 7, from IC305 via Q107.

Finally, the watch-dog timer chip IC103 (type TA8030F) provides a reset signal for the microcontroller chip and a couple of the DACs at power on, or in the event of IC101’s internal SWDT failing, or a fail in the voltage on the 5V rail. Further information can be obtained from [www.sumisho.co.kr/product/search/pdf/15001/TA8030F.pdf](http://www.sumisho.co.kr/product/search/pdf/15001/TA8030F.pdf).

**The EEPROM**

The EEPROM chip IC102, type M6M80021F, is a 2Kbyte MOS device with chip-select, clock, data in and data out connections. It’s simplest to think of it as a ‘memory map’ that has distinct areas for various uses, see Fig. 4.

First there’s an area which is common to all the six standard display modes and the four user-defined modes that are allowed. It contains values for RGD gain and bias, DBF H and V correction, contrast and brightness. None of this data alters when the user changes from one application to another, even though this might call for a different resolution. A technician can adjust the gain, bias, DBF etc. and establish new reset values in the factory mode. The user will

![Fig. 3: Block diagram of the DAC8840 digital-to-analogue converter chip.](http://example.com)
Fig. 4: EEPROM memory map concept.

<table>
<thead>
<tr>
<th>Area common to all display modes</th>
<th>Working area – user adjustable</th>
</tr>
</thead>
<tbody>
<tr>
<td>V position, H phase, height, width, H and V static convergence, H offset, pincushion, keyston, pin balance, etc.</td>
<td>V position, H phase, height, width, H and V static convergence</td>
</tr>
</tbody>
</table>

Want the monitor to remember the contrast and brightness settings when the monitor was last in operation. So, in this first area, there is factory-mode adjustable and user-adjustable data.

Next there are areas, used by the CPU, for the standard display mode settings and the user-defined mode settings. In each there is a table of values for line drive, H-osc control voltage, width (common with the HT), height, V position, H position (phase), pincushion correction, pincushion balance correction, key-stone correction, V and H static convergence, etc. The user has command over the width, height, H and V position and static convergence. The rest are technician-only adjustments.

The reset button restores the 'factory settings', which are in rewritable areas and are adjustable by a technician in the factory mode.

When the CPU reads data from the EEPROM and loads this into its RAM, it reads from the working part of the table then produces a screen display. A user who makes an adjustment tells the CPU to change the relevant RAM value.

The CPU follows up by writing this new value into the EEPROM's working area. Pressing the reset button restores from the factory-adjustable table, writing this into the EEPROM's working table. The CPU then reads IC102 again and, finding the new factory data in the working section, loads it into the RAM and continues as normal.

When an adjustment is made in the factory mode, the working data held in the RAM is stored in the EEPROM's working and factory areas. This is how new reset data is created.

**Purpose of IC105**

The 74LS508 chip IC105 is a latch that can isolate the H-rate signal feed to the deflection chip IC501, allowing the line oscillator to run free. The H-rate signal arrives at pin 2 of IC105 and, depending on the control input at pin 1 from pin 8 of IC101, the same signal may appear at pin 3 and pass to IC501 (this was dealt with in Part 2, May).

IC105 can also be controlled by the small toggle switch (SW951) at the front of the power supply board. When this is in the mid position, IC101 detects a low at pin 40 and its output at pin 8 prevents the H-rate signal passing through IC105. In normal operation, IC105 prevents the H-rate signal passing to IC501 when illegal timing signals are encountered. These are as follows: H-frequency less than 28.3KHz or more than 66KHz; V-frequency less than 45Hz or more than 135Hz; absence of either H- or V-sync; where the V- or H-frequency varies by more than 4Hz or 1.5KHz respectively. Otherwise the timing, whether standard or user-defined, is considered to be valid and IC101 leaves IC105 in the closed state.

**Fault-finding**

When it comes to fault-finding and repairs in the digital area of a monitor, relevant experience with TV sets applies. Check for damaged user buttons, defective crystal oscillator connections and confirm that the +5V and +12V supplies are present and correct. Ensure that the ICs aren’t overheating.

Carry out scope checks to ensure that the H-rate signal is being passed by IC105. This device has on occasions turned out to be faulty. The symptom is that the line scanning runs without line lock. If you doubt the toggle switch, which tells the microcontroller chip to continue or suspend the passage of the H signal via IC105, simply waggle it back and forth to see if there’s any change on the screen.

List DAC chip functions, identify serial ports, and use a scope to check for activity on the bus lines while pressing buttons. If you find that some functions don’t respond, see if they belong within a group. Check that data is being passed between one cascaded DAC and the following controlled device.

In one case the display had small, dark horizontal bands at the edge of the screen. It looked as if the line oscillator was behaving oddly but, by substitution, the processor panel was found to be the cause of the fault. The degaussing circuit was permanently on, the screen pattern being caused by the small residual current flowing through the potisitor. Surface-mounted transistor Q102 had gone short-circuit collector-to-emitter. Fortunately IC101 was OK.

**The CRT**

Before I close my book on the TFS6705K, a few points should be made about the Sony M41/KNP16X CRT. With Sony Trinitron tubes there are usually two thin horizontal lines visible on the screen, spaced about two inches from the top and bottom of the screen. They are caused by supports that provide stability for the aperture grille. I’ve had customers complain about them, suggesting that they are “phosphor burns”. It’s worth explaining this prior to sale of a monitor.

On one occasion a peculiar fault ‘developed’ after a repair. There was a thin black line down the centre of the screen. When I looked very closely I could see that two of the aperture grille wires had crossed and become tangled. Taking a new roll of solder, I whacked the side of the monitor’s bezel quite hard. Hey presto, the display was back in full. The same thing happened with another of these monitors next day. Weird and scary I thought. Then I noticed the junior technician having fun with the manual degaussing wand. After a short lesson the problem, strangely enough, never returned!
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June was a funny old month for DX-TV reception. Conditions during the late May–early June period were quite active but, as the month progressed, reception gradually declined. At least TVE (Spain) is still transmitting in Band I, despite various announcements to the contrary over the past year. Sporadic E propagation tended to be mainly along a north-south path, with lots of signals received in the UK from Italy, Spain and Scandinavia. Here’s the SpE log for the month:

1/6/02 NRK (Norway) chs. E2-4; SVT (Sweden) chs. E2-4; DR (Denmark) ch. E3; RAI (Italy) chs. IA; B; Tele-A (Italy) ch. E2--; TVE (Spain) chs. E2; 3; RTP (Portugal) chs. E2; 3; RTL Klub (Hungary) ch. R2; HRT (Croatia) ch. E4; IRIB (Iran) ch. E2; C+ (Canal Plus, France) chs. L2; 3; ARD (Germany) ch. E2; TVM (Moldova) ch. R2.
2/6/02 RTP E2; 3; TVE E2-4; Tele-A E2--; TVA (Italy) E3; PTP (Russia); LRT (Latvia) R2; RTL Klub R2; HRT E4; RTS (Serbia) E3; SVT E2.
3/6/02 RAI IA; B; Tele-A E2--; SLO (Slovenia) E3; ARD E3; C+ L3, 4; HRT E4; RTP E3; TVE E3; RTL Klub R2, ORT (Russia) R2; NRK E3; unidentified Arabic ch. E3 signal at 1345 hours.
4/6/02 ETV (Estonia) R2; SVT E2-4; LRT R2; NRK E2, 4; ORT R2; RAI IA. B.
5/6/02 NRK E2, 3; SVT E2, 3.
6/6/02 NRK E2-4; SVT E2-4; TVE E2.
7/6/2 ORT R2; TBK (Belarus) R1; C+ L2, 3; RTP E2; 3; RAI IA; B; Tele-A E2--; TVE E2-4; NRK E3; YLE (Finland) E4.
8/6/02 TVE E2-4; RAI IA; B; C+ L3.
9/6/02 ORT R2; SVT E3; RAI IA; B; Tele-A E2--; HRT E4; RTL Klub R2; TVE E2-4; RTP E3.
10/6/02 TVE E2; 3; RAI IA; B; Tele-A E2--; SVT E2.
11/6/02 RTP E2; 3; TVE E4; TBK R1. 2.
12/6/02 TVE E3, 4; RTP E3; RAI IA; B; Tele-A E2--.
14/6/02 RAI IA; TVE E2-4; HRT E4; ORT R2.
15/6/02 TVE E2-4; Tele-A E2--.
19/6/02 RTL Klub R2; HRT E4.
20/6/02 NRK E2; RTL Klub R2; ORT R1.
24/6/02 NRK E2; ORT R1.

I’ve heard that chs. A2 and A3 (North America) were received in the UK on June 14, and will provide more details about this when obtained. The Russian (ORT) ch. R1 signal received on June 24, in the early evening, was very strong and spread through to ch. E3, with inverted video. Odd! It obliterated the local 40MHz baby-alarm signals. Peter Schubert (Rainham, Essex) also commented on this signal.

Cyril Willis (King’s Lynn) has just returned from a holiday in Cyprus, where he received Syria ch. E3 and Arabic Band III and UHF signals daily.

June 3 was Jubilee time of course. BBC Radio Jersey and Radio Guernsey transmitted announcements that their normal UK network feed had failed and that in view of the day’s significance a DTH satellite feed from Astra digital at 28°E was being used. This source included an on-screen interactive red button, which BBC viewers were told was inoperative.

Satellite sightings
June was a relatively quiet month for those who monitor the Clarke Belt. It opened in fine Jubilee style, with the festivities around Buckingham Palace. An NTSC OB feed via NSS K (21.5°W) to the US on June 2 turned into more of a news item however. I found UK1-195 at 11:547GHz H (SR 5,632, FEC 3/4), with a reporter and friend discussing the events of the day inside a temporary glass-fronted Portacabin studio overlooking the Palace. A fire engine was driving through the gates and clearly something was happening. The fire in the State rooms was quickly put out, though the smoke from the roof suggested an early
start to the fireworks!

Sky News reported from the Palace for two days, using UK1-784 to uplink via Eutelsat W2 (16°E) at 12-522GHz H (SKY NEWS DSNG SKY 3). Sky took the output at each hour, inserting it into the rolling news. Interesting that the service identification “UK1-784 4.2 2.2” suggested MPEG 4.2.2, though in fact MPEG-2 was being used.

As an aside on this, the regional downlinks used by Anglia (TES-42) and Meridian (South TES-43, South East ‘Meridian 8MBT-TES-9’) have in recent weeks used MPEG-2. Occasionally the Southampton/Newbury TES-43 at 10-988GHz V jumps to MPEG 4.2.2, the result being either a “signal encrypted” message with blank screen or a mass of multi-coloured squares depending on MPEG-2 receiver design. These regional feeds are all carried by Intelsat 801 (31.5°W). During the evening of June 25 TES-42 was seen in an East Anglian gravel pit, reporting on the discovery of a mammoth’s tooth.

World Cup action came via C-band (4GHz) Intelsat capacity, with no Ku-band reports.

Whilst scanning across the empty wastes of Intelsat 801 I encountered activity at 11-487GHz V. The service identified itself as “Wetterstudio Gais”. This was at 1830 BST. There was no picture, just a blank raster, which disappeared at 1845. Intelsat 801 tends to be used for French/KUK feeds, with German feeds found at the Astra-3 (previously Kopernikus) slot – 23-5°E. For the record, Astra 1A has been moved into active retirement at 5°E, the Sirius slot.

There was much to see in the middle of the month on the latest Shuttle flight to the ISS. The station is still being built, and vivid pictures were downloaded from on-board cameras and those in space-suit helmets. NASA-TV is usually carried at via NSS K from the Johnson Space Centre. Houston in the evening. Tune to the three-channel multiplex at 11-590GHz V (20.145, 3/4). Good news with NSS K: “WNS-LONDON” at 11-566GHz H has dropped encryption. So Reuters news exchanges are in the clear – WNS is Reuters World News Service.

Dave Dyson (Accrington), who uses an RSD-300 (CI) receiver, reports that Vatican TV CTV (21°W) has moved to 11-618GHz V with the unusual SR 6.670. CTV-1 is encrypted, but CTV-2 is in the clear. CLN-ELPITEL has also been seen at this frequency, with SR 6.116, also Globecast NE with SR 5.700. CLN occasionally appears at 11-628GHz V, with SR 6.110. The common 6.110 SR may also be used at the former frequency – the pull-in range of the RSD-300 can read slightly off the correct parameter, particularly when the signal is strong.

On June 11 the Afghan feeds via Europe’s Star-1 (45°E) were brought into action for political developments. The former King decided not to stand, and a temporary head of state was appointed. The events of the day took place in large tent. Three uplinks were active during the afternoon: Tariqal Scopus at 11-556GHz V, and Fox News at 11-675GHz V and also at 11-471GHz V, all using 5.632 and 3.4. There was a jumble of identifications at the latter frequency, including ‘Globecast Nowforce UK1-579 BBC Kabul’ and ‘APTN Kabul’.

Edmund Snider (Littlehampton) is now using an 80cm dish. One new catch he reports is IRN (Independent Radio News) at 11-459GHz H (3.139, 3/4) via Intelsat 707 (11°W). “A little or a lot” will be present here depending on the time of day and part of the hour. When it’s busy there are the main news feeder, a tone (test whistle), commercials and other programming. He also found BFBS radio services (British Forces Broadcasting Service) at 11-561GHz V (6.000, 1/2) via Telstar 11 (37.5°W). In recent weeks this downlink has been either encrypted or in the clear.

The CNN and the Balkans air-surveillance downlinks from this satellite were still present, in the clear, at the end of June (11-495GHz H. 19.500, 2/3). There has been comment in the media about this surveillance. The US Military considers that there is no security problem with the civilian-operated service, which provides unclassified pictures.

Telstar 12 (15°W) has been seen carrying the Iranian propa-
These small, cigar-tube sized containers are filled with human cremation ashes, to be placed in Earth or Lunar orbit following a funeral service provided by Celestis Inc. of Dallas, Texas. The top right container carries the name of the deceased and the message “have a great flight Dad”.

early next year. Up to 36 channels are expected eventually in Riga and about 24 nationally, a mixture of FTA and subscription. The French broadcasting authorities have postponed the closing date for DTT applications until October 31; pending resolution of how the future administration of DTT is to be organised. Sweden is shortly to have a DTT channel dedicated to children’s programming. It will also be available via satellite and cable.

Channel news: The main Russian TV channel NTV nearly lost its transmission licence after breaching programme guidelines. The Federal Tender Committee has discussed the problem with management and it seems to have been resolved – the NTV licence has been extended until 2007.

An analogue entertainment channel for youth, called Tango TV, is being transmitted in the Vilnius region of Lithuania. TVS (or TV Sektr) started to broadcast on June 1 as a replacement for the previous TV6, which was banned. It’s devoted to news and light entertainment.

A dedicated news/current affairs channel was started by Pakistan Television on July 1.

Germany: The SFB-Berlin and ORB-Brandenburg broadcasting networks are to merge. The aim is to improve finances and enhance their position within the ARD operation.

Iran: A recent updated transmitter list shows a high level of broadcasting activity in Band I. There are five ch. E2 transmitters with ERPs from 6-100kW, eight ch. E3 transmitters with ERPs over 6kW and five ch. E4 transmitters. New Band I transmitters were being installed as recently as summer 1996. The E2 channels include Pishin at 316kW and Kuh e Nuh at 200kW ERP.

Portugal: State funding for RTP-2 is to end, having built up debts of over £600m. The service will either be closed or sold to a commercial broadcaster.

Isle of Wight: The ITC has received three bids for the island’s RSL-TV licence – the successful candidate will be announced in early July. Current holder TV 12 is confident that its licence will be renewed, from October 31. The other bids were from Solent TV and Wight TV.

Satellite news
Launch of the new 905 Intelsat craft into orbit at 24.5°W will provide 72 C-band and 22 Ku-band high-power transponders covering Europe, Africa, the Middle East and the Americas. The slot was first used by Intelsat 1 (Early Bird) in 1965. Intelsat 613, which was previously stationed at 24.5°W, has been moved to 178°E – over the Pacific.

The Spanish Via Digital DTH service is to introduce a set-top box that incorporates a hard-disk recorder with a programme storage capacity of sixteen hours. Consumer trials are to be carried out at Malaga, Alicante and Tarragona.

Moon-bounce reception
Hugh Cocks (Algarve, Portugal) has drawn my attention to investigations by Anthony Mann (Perth, Western Australia) into the possibility of moon-bounce DX-TV. Radio amateurs have for some years used moon-reflected transmission at VHF/UHF, with fairly high powers and very high-gain aerial systems. Not much has been published on this transmission mode, which is sometimes referred to as EME (earth-moon-earth). Basically, a high-power incident signal that reaches the moon’s surface can be reflected back to earth, during a calculable time “window” (access period) for the outward and back paths. Over such huge distances, with reflection involved, there is likely to be polarisation shift, suggesting the need for a circular-polarisation feed at the reception site.

Anthony noted that many UHF transmitters in the US use very high ERPs, typically up to 5MW. The signals travel outwards towards the horizon, and continue beyond. If the moon is suitably positioned they will arrive at its surface, in very much weakened form, and will be reflected and scattered. The scattered signal information may arrive back on earth, now severely weakened. Anthony has managed to receive and identify such signals.

We’re not talking about noise-free pictures, in fact there are no pictures. What Anthony has received is very, very narrow parts of the audio signal spectrum, with bandwidths down to a few Hz. The received signal is processed and fed into a computer. The signal ‘blip’ then appears on the monitor screen as a waveform pulse. As previously mentioned in this column, it’s now possible to measure TV transmission offsets to a few kHz. By using a PC, a suitable program and a stable radio scanner measurement can be taken down to a few Hz. Given just a sniff of a signal, its origin can be established by checking the nominal carrier, with any offset present, against transmitter parameter listings.

Anthony has calculated the send and receive angles, and thus the “window of opportunity”, for several high-power US UHF transmitters. The optimum condition is when the moon sinks down to the horizon and maximum transmitter power is ‘aimed’ at it. Anthony is not using a large dish. Instead he uses a standard long UHF Yagi array, similar to a Fuba XC391/Triax Unix 100. A GaAs FET head amplifier with a gain of 20dB and a noise figure of 2dB (sounds high to me) is mounted next to the dipole, and low-loss coaxial cable connects its output to an Icom R7000 scanner. This is a comprehensive though perhaps rather
mature receiver. I have one, and can confirm that it's a truly solid piece of gear! It incorporates SSB, and a very weak signal can usually be resolved when this is switched into circuit — that's how I first located the 250MHz domestic radio downlinks via the US Fleetsatcom craft at 20°W. see report in this column last November.

Anthony mounted the aerial on a 5ft high tripod and can adjust it to align with the moon. The exact carrier frequencies used by the selected US transmitters are known to the last Hz and can, with the calculated time window, be tapped into the scanner. But a further calculation is required. The earth and moon are both moving and, like a moving train with its whistle frequency that changes as it passes you, so a frequency variation needs to be calculated — to take into account the moon/earth movement and frequency shift (Doppler effect). Doppler correction is only a few Hz but changes during the receiving window period, which can be from four to 25 minutes. With a bandwidth of a few Hz, accuracy is essential.

This is an incredible technical exercise with extremely weak signals. Anthony has managed it using a basic aerial, head amplifier, scanner and computer: WNBU-16 (South Bend, Indiana), WAPT-16 (Jackson, Mississippi), KTXT-39 (Dallas, Texas), KDVT-14 (San Francisco, California), WFTT-50 (Tampa, Florida) and KWBT-19 (Muskogee, Oklahoma) were among the eleven transmitters he had received and identified by early June.

Printout spectrum scans show the DX signal sitting on top of the residual noise — an example can be seen in Fig. 1. But remember that it's a spike a few Hz wide. Our familiar DX-TV signals that provide a very poor-quality image with bandwidth limiting are over 1MHz wide. Nevertheless Hugh Cocks is attempting moon-bounce reception with a 2.8m dish and a helical aerial feed. Reception of the 860MHz signal from the Indian ATS-6 TV satellite in 1975-6 was more successful with home-constructed dishes than Yagi arrays.

I'll report further as more information and reception reports become available. Meanwhile my congratulations to Anthony on demonstrating a dramatic DX-TV propagation mode and the considerable effort he has put into what, for most of us, would seem to be something that's impossible. For updated information check the GM4JJ moon-bounce program (www.gm4jj.co.uk) and the Perth University site (www.physics.uwa.edu.au/~gmj).
**Channel freezing**

Mrs Gray phoned to complain that after a while some channels would freeze into "large squares", others remaining fine. She mentioned that the BBC and Discovery channels in particular were affected, while Sky News, CNN and TCM were OK. From this it was clear that the horizontally-polarised channels were affected, the ones with vertical polarisation being all right. So the cause of the problem lay with either the 18V horizontal-polarisation supply or the low-/high-band 22kHz tone selection system.

A replacement LNB cured the problem. But before installing the new one I connected the output from the old one to a spectrum analyser. This showed that over a few minutes the horizontally-polarised, high-band signals slowly reduced in level to nothing. The horizontally-polarised low-band signals remained constant and, once the change to low-band had been carried out by deleting the 22kHz tone, switching back to high-band produced signals again for a few minutes.

I've noticed that LNBS are sometimes prone to breakdown, either partially or completely, when there's a change of temperature over a relatively short time period. C.H.

**Humax IRC154000**

If the power supply is tripping with the red light on the front panel flashing, replace C7 (33µF, 50V), C9 (1.000µF, 10V) and C21 (1µF, 50V). Sometimes the 30V zener diode and the 100Ω, 1W resistor in the 30V line also fail. C.O.

**Digital channel update**

The latest channel additions at 28.2°E are listed in Table 1 — where assigned, the EPG number is shown in brackets after the channel name. The following EPG numbers have recently been assigned: 232 Rapture TV; 235 Avago TV; 455 Vibe TV.

Some Sky channels are being used to test transponder 31 (12.304GHz horizontal) aboard Astra 2B. Reception is not at present possible when these channels are added via the New Channels menu (see Photo 1) as it's blocked when a domestic Sky viewing card is used.

Nick Toons was due to start on July 22 via transponder 34, see Photo 2.

ESPN Classic Sports Italy has to be added manually via the New Channels menu: this can cause confusion as it at present has no name in the programme identification banner. C.H.
Acer 7299SL
This monitor would power up with a green LED light but no display. There was no EHT because the line drive was missing. Checks showed that there was no activity on the IC bus that connects the scan processor chip to the microcontroller chip. So the cause of the fault was likely to be in the microcontroller area. A few checks in this area brought to light the fact that the 12MHz clock crystal Y801 was inactive. A new crystal restored the display. G.M.

Dell D1028LR
This monitor was dead with no LED illumination or display. Checks at the primary side of the power supply showed that it was actually tripping, though silently, and that the UC3842 charger-control IC was driving a short-circuit. This turned out to be the 2SK1940 duty FET Tr6115, which was short-circuit gate-to-source. Strangely, there was no other damage and a replacement restored normal power supply operation and the display. Incidentally this monitor is fitted with a Philips chassis.

Fl Europe 1410
This strange monitor from the Netherlands had no front badge at all. In fact the front was completely blank, the model information being obtained from a sticker on the rear cover. It was to all intents and purposes dead – the power supply shut down almost instantly at switch on. I was not surprised to find that there was a short-circuit across the 90V line. Checks showed that the cause was the MR35 rectifier D857. The unit badly accepted an SF35 as a replacement, which cured the fault. G.M.

iiyama Vision Master Pro21
(Model MT-9021T)
This huge monitor powered up with green LED illumination but no display. A loud squealing noise could be heard coming from inside it. It’s a very complicated monitor that requires a major strip-down to gain access to the chassis. There are separate line output and EHT drive circuits, and checks in this area revealed that the 2SK2487 EHT driver transistor Q5C5 was leaky. Replacement of this device restored a very fine display. G.M.

It's part of a biasing circuit for a signal-type transistor that delivers a low voltage to pin 3 of the UC3842 charger-control IC to turn the monitor off. Pin 3 is the excess-current sensing pin, and in this design the soft-start switching makes use of it. Hence the tripping when the transistor’s biasing was upset because R024 was open-circuit. A replacement resistor cured the fault. G.M.

Hewlett-Packard Pavilion M50
(Model D5258A-60008, C5B chassis)
This monitor was totally dead because the start-up resistor R848 (470kΩ, 0.5W) was open-circuit. A replacement resistor restored normal operation. Note that although this monitor looks exactly like the one mentioned above, and has an almost identical model number, the chassis is completely different. G.M.

Dell P791 (PG chassis)
This smart black monitor powered up with a green LED light but there was no display. As the EHT supply was present and correct, attention was turned to the CRT base board. I found that the grid voltage was at −188V, which muted the video drive. When I carried out some checks on the main board I discovered that there was no line scanning. The 2SC5584 line output transistor Q405 and the SFP9634 B+ regulator FET Q406 were both short-circuit, while feed resistor R480 (2-21Ω, fusible) was open-circuit. Replacement of these items restored a perfect display – use an IRP9634 to replace the SFP9634. G.M.

Elonex MN009
(Philips TY619323 006545)
The complaint with this monitor was no line sync. When I tried it I found that the display was also over bright, and that the user control didn’t vary the brightness. Adjustment of the master line hold control, which is a few inches in-board from the vertical output stage heatsink, was attempted but line lock seemed to be outside its range. So I ran the TVGA Modest program supplied with the Trident video card. At mode 55 I was able to find a point where the display just drifted through.

There’s a small subpanel with a few presets at the other side of the chassis. Now some of these might be for frequency-to-voltage discriminator calibration, needing a manual, which I didn’t have, for correct setting up. So I gave each preset just enough torque to disturb it and returned it to its original position. Each one made a faint click as it was disturbed, which proved that no one else had been tampering with them. When disturbed, one of the last...
two presets produced line lock. A run through the Modetest program then proved that none of the modes had been lost.

The cause of the excessive brightness turned out to be a crack in the PCB, next to the line output transformer. The tracks to pins 3 and 4, and one nearby track towards the rear of the board, had been cut. Once these had been repaired the monitor worked as it should. A long soak test proved that all was now well. I.F.

**Huyundi HL4850**

This monitor was brought in after it had "blown up". I was told that there had been a strong smell of burning. To say that the soldering required attention would be a gross understatement. The BUH517 line output transistor Q503 and the IRF9610 B+ step-down buck regulator transistor Q714 were both short-circuit. L703, the inductor in the regulator circuit, looked somewhat charred.

Once the line output transistor has been replaced the next step is to isolate Q714 from the 180V supply and check the LOFT by running it from the 66V supply. This wasn’t possible because D716/735 (type S2L3D), which had been dry-jointed with early signs of arc erosion, were both short-circuit. Being unable to find any data on these devices, I replaced them with a pair of MR856s. As the power supply still didn’t work, I checked the voltages around the UC3842 chopper control chip IC701. The pins were all at 0V! When I unsoldered pin 7, the start-up components produced a voltage across C714 (100µF, 25V), so the chip was short-circuit. I replaced the IC and, while I was at it, checked the ESR of C714. It was OK.

This time the power supply started up when tried. After confirming that its output voltages were close to the values indicated alongside the transformer pins, I connected a flylead from C741/341 to C743/355 to feed 66V directly to the line output stage. The monitor then produced an almost full-screen display with severe pincushion distortion, proving that the LOFT was OK.

The last time I got unexpected width with a reduced B+ supply I wasted time looking for flyback tuning faults and shorts in the EWT correction circuit. It turned out that the servo-type EW error amplifier was so good that it almost managed to correct the extreme lack of drive! As I had more than enough prime suspects for the blow-up, I continued without this distraction.

An exact replacement inductor wasn’t readily available, so I opted for one from a Samsung chassis with a very similar type of step-down B+ buck regulator. The Samsung inductor is shorter and fatter: removing the white, square cover enabled it to fit more easily. Once it had been fitted, I replaced the buck regulator transistor. On test everything was found to be OK.

If the IRF9610 fails to conduct, check the zener diode ZD703 across its gate and source — this may be short-circuit, removing the drive. Its failure could indicate a severe breakdown in the line output stage — possibly the LOFT. But ZD703 was OK, so I had no reason to check on this. The MOSFET has a gate-oxide withstand voltage of 20V, and requires at least 12V (preferably 15V) of gate drive. The zener diode value most often found in this position is 18V. It’s rarely less than 16V. I.F.

**Elonex/AST TE1464G**

The problem with this monitor I had for refurbishment was no display with the power supply pulsing. I soon found that the BU2252AF line output transistor Q513 had failed. As a replacement I fitted a 2SC3688, which has a very similar specification but seems to be more robust. When the monitor was powered again it produced a distorted raster with kinks at the top of the scan, suggesting a faulty HT reservoir capacitor. The distortion started to reduce as the monitor warmed up, but the 2SC3688 blew after about five minutes.

These monitors turn up frequently, and quite often the CRT is broken. As luck would have it I had one I’d intended to scrap in the store room. So I decided that the simplest course would be to swap over the main PCBs. I had a nagging thought in my mind that if I was wrong about the faulty HT electrolytic the cause of the problem could be faulty scan coils, but after the swap the monitor powered up with excellent display geometry, needing only a grey-scale set-up.

The CRT base PCB in the scan monitor had been badly damaged by the force that had broken the CRT. The PCB wasn’t broken, but the metal screen’s solder pads had been pulled off. The monitor for refurbishment was no better — it had arrived with the CRT base screen hanging off! The solution is to ‘hemp’ the PCB slots with 20 or 22 SWG tinned-copper wire. Start by cleaning off the green varnish at either end of the slots. Bend a right-angle of TC wire and feed it through the slot: solder the end down, then ‘sew’ the wire through the slot, like winding a single-layer coil. The turns must be pulled as tightly as possible, without snapping the edge off the PCB, otherwise the turns will block the slot so that the screen won’t fit. With care, the turns of wire can be made to form a neat, even layer along the accessible side of the slot, and the screening can be securely soldered to this.

In many cases where the screening has pulled its solder pads off the CRT base PCB enough copper track is pulled up to result in an open-circuit earth route. If both ends of the wire binding are secured, it serves the dual purpose of repairing the earth return as well as replacing the screening solder points.

A further point is that there were distinct ‘track marks’ burnt into the dust around the CRT’s final anode connector. Two of these zigzag their away to the Aquadag coating, but one tracked under the scan yoke. This could have resulted is damaged semiconductor devices in the line timebase, but the replacement main PCB took care of this possibility. It could of course have been the cause of the original transistor failures. It’s important to clean pollution deposits from around any EHT components.

Mass resoldering is also worthwhile with this chassis, even if the soldering doesn’t look that bad. I.F.

**AST LR14**

I examined this monitor before applying power. To make a change C332 (680nF, 400V) instead of C322 (8.2nF) had burst. These capacitors were both resin-dipped types, which seem to last longer than the moulded-plastic type. No other damage was found, and after a quick resolder the monitor was reassembled and worked well. I.F.

**Gateway 700-069E**

When this monitor was switched on the EHT ruzted up but there was no display. A few quick checks showed that all the main circuit sections were working. When the heater voltage was measured at the CRT base however the reading was only 5-74V. So the tedious business of dismantling the chassis tray was undertaken to inspect the smoothing components in the 6.3V supply. The rectifier is already a Schottky-barrier type, so I had to be content with renewing all the electrolytics along the track and adding 1µF, 63V multilayer ceramic capacitors in parallel.

With the heater voltage a little nearer the correct value I carried out checks to determine whether the cathodes had been degraded. They hadn’t. The cause of the missing display was the fact that the class A transistors in the RGB output stages were cut off. Their common base-bias supply was low, and a quick search for dry-joints brought me to IC321. Its three pins were all dry-jointed. Once fresh solder had been applied the monitor powered up with an excellent display. I.F. ■
Akai VSG781EK
This VCR wouldn't accept a tape. Motors could be heard spinning, but no attempt was made to draw the cassette in. No broken parts were seen when the mechanism was removed, and manually loading a tape was OK. Nothing amiss was found when the connections to the end sensors and the centre LED were examined, but they were resoldered anyway.
I removed the mode-switch assembly and found that it was far from clean inside. Once it had been cleaned and lubricated the machine accepted tapes. B.F.

Panasonic NVHD605B (K deck)
A cassette that wouldn't eject was stuck in this VCR. The machine would just go into rewind for a while then switch off. With F03 in the display. After a few attempts the cassette did eject on its own, avoiding the need for a delicate removal operation.
The loading-motor coupling was OK, and there was nothing obviously wrong with the other gears. While looking at the main board for possible dry-joints at sensors I noticed that one of the four copper contacts on the mode switch connector had come out of its casing. This would give poor contact with the mode switch of course, and cause intermittent operation. Once the contact had been repositioned in its casing and the contacts had been cleaned the machine worked correctly - a long soak test proved that all was now well. B.F.

Sharp VCA43HM
Sometimes this machine wouldn't start up - it would just produce a high-pitched whistle from the power supply. Removal of the power supply didn't reveal anything that was obviously wrong, but when C907 was moved it was found to have an unsoldered leg. Reliable operation was obtained by resoldering C907. C906 and the plug connections at PA, and replacing C913 (47µF 16V) on the primary side of the power supply. B.F.

Ferguson FV61
This machine was lifeless apart from the loading motor, which was pulsating. The power supply output voltages were correct except for those at pins 1 and 2 of BP03. The voltages at pins 1 and 2, which should be 13-6V and 21-8V respectively, were both missing. The voltage at pin 3 was high at 20V instead of 5-9V. The cause of the fault was TR25 (U2559BF), a small IC on the large servo board. All was well once it had been replaced. B.F.

JVC HRD960
When this machine went into fast wind or rewind it would switch off. The brief slow wind or rewind before it unlinked and speeded up was OK. As no mechanical faults could be found, attention was turned to the power supply where C19 proved to be the culprit. B.F.

Sharp VCH84/86
If the tape plays back at high speed, check the amplitude of the waveform at pin 3 of the capstan motor. It should be 2V peak-to-peak. If it isn't, try moving the sensor on the motor closer to the edge of the pulley. In this machine the sensor was loose. Alternatively you could replace the motor, but the cost would probably mean that the VCR was not worth repairing. C.O.

Samsung C15A chassis (tele-video)
There was a cassette stuck in the VCR section of this combi unit. After releasing the cassette and cleaning the mode switch the unit no longer remained in standby. C.O.

Philips VR948
This top-of-the-range S-VHS machine had a cassette stuck inside. At power up a whirring sound was heard. which indicated that the gear was loose on either the loading shaft or its associated worm gear. A kit is available to deal with this. part no. 4822 310 10637. Replacing the shaft and worm gear did indeed cure the fault.
But other strange faults were found to be present when the machine was tested. Playback was OK, but when fast search was selected the capstan took several seconds to reach the normal "scanning + 9" speed. and when play was pressed to return to the normal speed the capstan took about ten seconds to gradually slow down to normal. When reverse search was selected, the capstan stopped and the picture froze despite the fact that the display showed "scanning - 9". And when the audio was switched to mono the display bargraphs went to maximum with no sound. During playback of any tape, including prerecorded films, the mono soundtrack was erased.
I decided to tackle the speed fault first, which was a wrong move! A replacement capstan motor made no difference. Then I thought that the UPD78134 microcontroller chip IC7060 might be faulty, as it controls the capstan motor directly. It's a difficult chip to replace, so I had to be pretty certain that a replacement would clear the problem. I went ahead, but the faults remained exactly the same.
I left the machine for a day, then spent ages checking the reset circuitry. After that I decided to tackle the sound fault. As I suspected, the mono line-in sound bias/erase oscillator was on all the time. The cause was the BC848B surface-mounted transistor Tr7242, which had collector-mitter
leakage. After fitting a replacement I tested the machine again, and was surprised to find that the faults had all been cured!

The only link between the two circuits is the reset line, which is connected to the emitter of Tr7242. It must have been corrupted somehow, affecting the microcontroller chip.

After reassembly and a final test I had to work out what to charge. Fortunately the customer was very understanding and very fond of the machine! M.C.

**Goodmans VN6000**

If the display is flashing, the power supply produces a slight buzz and the machine loads but doesn’t play, replace the main reservoir capacitor (82μF, 400V) in the power supply. Also clean the mode switch — a loop of tape may be left if this is not done. J.S.O.

**Matsui VX1105/VXA1100**

I’ve had several of these machines recently with the tape creasing complaint. Check the retainer clips on the take-up and supply guide poles — they can slip down, with the result that the guides don’t locate in the V blocks. Refit and add a small spot of Evostick to prevent the fault recurring. It pays to check both clutches and clean the mode switch while the deck is out. J.S.O.

**HTC TVR402**

I’ve repaired several of these 10in. TV/VCR combi units for a local caravan hire firm. All have had the same fault — no functions when the tape has loaded. The cure is to remove and clean grease from the mode switch. The deck is similar to that usually found in Daewoo models and other budget machines. It’s a straightforward job with this deck. J.S.O.

**Thorn VR202LV**

The owner of this machine complained that the picture was intermittently unstable, with tracking noise at the top of the screen. When I removed the cover I saw that the back-tension band’s felt pad had parted company with its backing, so I was fairly confident that a replacement and adjustment would cure the fault. But although there was an undoubted improvement when this had been done, the picture stability still left a lot to be desired. A look at one of the owner’s tapes proved the vital clue — there was slight crinkling along its edges. Correct operation was restored by cleaning the capstan and replacing the pinch roller. D.I.S.

**Panasonic NVHD620B**

There had been a gradual deterioration of playback of tapes recorded by this well-used VCR. The owner had tolerated this until tape-loading problems arose. He then asked me to look at both problems. Although I was rather concerned about the very evident head-drum surface wear, I had to tackle the loading problem first. I suspected yet another split loading-motor coupling, but this proved to be OK. The cause of the trouble was slow operation of the loading mechanism, which prevented full loading. Much time was spent cleaning and lubricating the mechanism before suspicion fell on the loading motor itself. Substitution of a known good loading motor proved the point.

Unfortunately the poor picture quality was down to excessive head-drum wear. At this point the owner declined the repair and bought a new VCR from Tesco — for slightly less than the cost of the head drum and loading motor from Panasonic. D.I.S.

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**Fidelity CTV3221NF**

For intermittent line faults, such as a
double image, line transformer screeching or
wrong line drive, replace Q601 (BF422)
even if it tests OK. Sometimes an intermit-
tent transistor in this position will result in
the chopper FET going short-circuit. M.D.

**Tatung T32W441S**

Field collapse plus lack of width was
caused by failure of the TDA8350Q chip
ICF1. When you get this fault you will
also have to replace the two 2 2Ω safety
resistors RF8 and RF9, and the 33Ω safety
resistor RF10.

The chassis is also used in a variety of
inexpensive sets, for example Bush models.
A common fault is failure of the line output
transistor, the cause being a pinhole in the
insulation of the line output transformer.
M.D.

**Sharp DV5161 (48SA chassis)**

Beware of sets that display a poor picture
– one that looks as if the CRT is worn out.
The cause of the fault is likely to be data
corruption in the EEPROM chip. There
may be another symptom, excessive or
lack of height. The poor picture can be
cured by resetting the colour drives in the
EEPROM, but if you simply reset these
the problem will return at a later date. To
prevent a recurrence, check R601 (0-682)
– it’s connected to pin 9 of the chopper
transformer. If its value has risen, replace
it. Also replace the 5V regulator chip

IC1003 (L7805), C604 (2,200μF), C1011
(47μF) and C1012 (10μ). M.D.

**Samsung CI6644N**

The cause of field collapse is usually the
TDA8350Q field/EW output chip. If,
after fitting a replacement, you find that
the six RGB test lines are visible at the
top of the screen, the cause is loss of the
46V flyback supply. Check the 10Ω safety
resistors R307 and R409. One or both of
them will be open-circuit. M.D.

**Grundig TVR3700**

This TV/VCR combi unit was brought in
by another dealer. He had fitted a new
pinch roller then, when he reassembled the
unit, he found that there was partial field
collapse which varied with the picture
brightness. Luckily for me he forgot to
bring the remote-control unit along, so I
tried to use the A1 preset to vary the
brightness. As I did so the field scanning
fell from about an inch to total collapse.

To provide picture breathing compensa-
tion, the beam current monitoring point at the
earthly end of EHT system is linked via
R3202 to the ramp generator within the
TDA8362 chip. A check at pin 42 of this
IC revealed that there was no field ramp
generator supply via R3201 – the only
feed was from the BCL line. In stripping
the unit down the dealer had caught the
print with something sharp, the result
being a cut between the 33V supply and
R3201. Once this had been repaired the
unit produced correct field scanning. M.D.

**Amstrad CTV3128**

The customer said there was line collapse,
and I could see a nice little earner. How
wrong! I noticed a large dry-joint at the
scan-coupling socket, attended to this and
switched on. I then found that the EHT
was low and that R711 on the stand-up
EW PCB was cooking. R711 was
replaced, along with the TDA8145 EW
correction chip and the EW bridge coil
L679 (10mH). The latter was burnt and
had shorted turns – I found a suitable
replacement in an old Vestel chassis. But
the set still failed to work. To cut a long
story short, the scan-correction/coupling
capacitor C620 (470nF, 250V) was open-
circuit.

Don’t unplug the EW board with the set
in the fault condition. When I tried this the
line output and chopper transistors both
blew.

So much for it being a nice little earner!
M.D.

**Decca D20TKG5**

(Tatung K chassis)

The EEPROM in this set was corrupt.
As a result, the sound was stuck in the
wrong system and there was lack of height. You don’t have to use a complicated button-pressing sequence to enter the service mode with this chassis. Just order a dealer service remote-control handset from Tatung. M.D.

**Philips 29PT6433/05 (MD1.2EAA chassis)**

There was a strange fault with this set. The customer complained about blue fly-back lines on teletext. The field engineer had called twice and had each time reduced the setting of the first anode preset on the line output transformer. As the fault persisted, I decided to replace the LOPT (part no. 4822 1401 0584). A long soak test proved that it had been the cause of the problem. P.S.

**Bush 2871NTX (11AK19 chassis)**

We seem to get a lot of these sets in for repair. When you consider that stores like Tesco, Aldi and Asda have been selling them this is probably not surprising. This one’s picture was too wide, with west-east distortion. It’s becoming a common fault. All that’s required is to resolder the dry-joint on the BUK444 EW driver transistor Q603, which is on a metal heatsink next to the line output transformer. P.S.

**Goodmans 206NS**

There was a picture shift problem with this set – it was up from the bottom. Geometry adjustment is carried out electronically, by going into the service menu, but I couldn’t get it into use the customer’s remote-control unit. A call to Comet revealed that a service remote-control unit, type DAEW48B1530VC, is required. This did the trick. P.S.

**Sharp 66DS-03H (CA10 chassis)**

It’s not unusual to get one of these sets with a short-circuit line output transistor because of dry-joints around C613. In a couple of them the mains fuses had also blown. In both cases a major power supply repair was required. The following items had to be replaced: Q701, R716, D712, R720 (surface-mounted), Q702 and Q703. You should also check R713/4 and R704/5 which can prevent start-up. M.S.D.

**Philips 28PW9512/05 (MD2.12A chassis)**

This was tripping, with flashes from the LED. Suspecting failure of the line output transformer, I carried out a quick check across the transistor. Sure enough there was a very low resistance reading. The transistor checked OK when measured out-of-circuit, and the short was still present when the transformer was disconnected. I then started to check the capacitors in the line output stage, as they seem to fail on a regular basis in today’s large-screen sets. Sure enough when C2433 (390nF, 250V) was checked it produced a reading of only a few ohms. The only clue that it was faulty was a very small amount of wax substance where the capacitor’s legs go through the board. Once a replacement had been fitted another very large, very heavy widescreen set departed from the workshop. G.L.

**GoldStar CF28C22F (PC33J chassis)**

There were lines at the top of the screen when this set was switched on. The obvious thing to do seemed to be to replace the TDA8350Q field/EW output chip IC301 but this made no difference. The chip has separate supplies at pins 4 and 8, both derived from the line output transformer. R304 (10Ω, 0.5W) in the ‘fly-back’ supply to pin 8 was open-circuit. There was correct scanning once a replacement had been fitted. G.L.

**Fidelity CTV3228NF**

The problem with this set was line collapse. Some checks with a capacitance meter revealed that C609 (0.47μF, 250V) was open-circuit. G.L.

**Ferguson A10R (TX80 chassis)**

This colour portable worked all right with a 240V mains supply but was dead with 12V operation. The DC-DC converter circuit is on a separate panel, and it didn’t take long to find that the two transistors here, TD701 and TD702 (type 7416-1), also diode DD707 (1S1888), were short-circuit. Once these items had been replaced and a new 8A fuse (FD702) had been fitted all was well.

According to most stockists the 7416-1 transistor is obsolete and is no longer available. Fortunately we had a few, but our supply is getting low. Does anyone know of a source or a suitable alternative, as we repair quite a lot of these sets. G.L.

**JVC AV295X1EK (JA chassis)**

I was called to see this set because of a no-picture fault. In view of its size, I hoped to be able to fix it in the customer’s home. When I replaced the TDA8350Q field/EW output chip IC401 there was a good picture, but four days later the customer was on the phone to say that the picture had gone again. This time I had to take the set back to the workshop for tests. I eventually found that a DMM check on FR552 (1Ω, 2W) produced a reading of 9Ω. It’s the surge-limit resistor in the rectifier circuit that provides the supply for pin 4 of IC401. Much to my relief, replacing FR552 cured the problem. G.L.

**Bush 6671 (11AK19 chassis)**

When this set was switched on the only result was a faintly audible pulsing from the power supply. The BU2508AF line output transistor Q605 was faulty. A replacement restored normal operation. D.G.

**Beko 14.1 chassis**

This widescreen set was dead. Checks showed that F1 (2.5A) was open-circuit and T601 (2SK2545) short-circuit. All was well once these items had been replaced. D.G.
**Samsung CLS937AN (Z68 chassis)**

There was partial field collapse — a black band about an inch deep at the top of the screen. As there are no controls to tweak/adjust, I decided to replace the TDA850Q field/EW output chip IC301. This action restored full field scanning.

D.G.

**JVC CS2180M**

This model has PAL/Secam/NTSC decoding capability. But there was tuner drift with all selected channels. Not unexpectedly, the cause of the trouble was on the tuner board, which is clearly marked SBX-M002A. There are four surface-mounted capacitors, C104-7, on this board. Replace them all and you will be rewarded with pictures that remain locked on channel. D.G.

**Bush 1407 (Onwa chassis)**

The customer complained that the sound became very distorted when the volume level was increased. I’ve had the problem before with various sets that use this chassis. The cure is to fit an 0.5μF electrolytic capacitor between output pin 5 of the TBA820M audio chip IC201 and a nearby chassis point. This will cure the distortion.

D.G.

**Grundig CUC5301 chassis**

If you get one of these sets with sound but no raster, check the soldered joints at the scan coil plug on the main PCB. They have a habit of drying out, the result being these symptoms. D.G.

**Samsung CL5412G (P585H chassis)**

This set would power on, the relay would click then, after a few seconds, the standby light would fade away. The chassis uses a TDA4601-based chopper power supply. As I expected, ESR checks on the electrolytic capacitors in this part of the chassis produced many high readings (C800, C811, C813, C820, C822 and C829 all read high). To achieve a reliable repair, I decided to replace all the electrolytic capacitors in the power supply and through to the line output stage. The result was a working set. D.G.

**Philips 32PW9630/05 (GFL2.30 chassis)**

This widescreen set would start up only intermittently, because the EW protection circuit was operating. After spending some time chasing around in the line timebase without result I disconnected the protection line. The result was a cloud of smoke from a faulty 510μF S-correction capacitor. I also had to replace the series switch — the IRF620 MOSFET in the HT feed to the line output stage — as it was short-circuit. Although failure of this item would not otherwise stop the set from working, it’s used to shut down the line timebase under certain fault conditions.

The microcontroller chip checks the switch when the set is started up: if the check fails, the set is placed in the protection mode. R.B.

**Toshiba 3357DB**

Two of these impressive 33in., 4:3 CRT sets came in during one week. The problem with the first one was no UHF reception: scan operation was OK. A new tuner was required. The second one tripped when brought out of standby because the audio output IC was short-circuit.

These were straightforward repairs, but the size and weight of the set makes each job a serious undertaking. R.B.

**Philips 46PP912A/05 (FL1-PTV chassis)**

There was a convergence problem with this 46in. projection set. Horizontal red and green lines at the top and bottom of the screen were regularly jumping — the effect was rather like poor interlace. In this chassis the convergence ‘power amplifiers’ have their own switch-mode power supply, which provides ±16V outputs from a separate PCB at the rear of the cabinet. Checks showed that the positive output was low with severe 50Hz ripple.

I at first suspected a capacitor problem on the primary side of the power supply, but the cause of the fault turned out to be the CNR50 feedback optocoupler. The ripple was caused by the large 50Hz component in the current drawn by the field convergence circuitry. R.B.

**Philips 28PW6305/05 (A10 chassis)**

The picture was OK when this set was cold, but after about ten minutes the contrast gradually decreased, leaving a dark picture with very washed whites. The teletext and on-screen graphics displays were always satisfactory. Careful use of heat and freezer brought me to the 1μF surface-mounted capacitor C2246 on the small-signals panel. It couples the video signal to the input of the comb-filter 7405 and was slightly leaky when warm. R.B.

**Philips 32PW9523/05 (MD2.25 chassis)**

The picture took on a red cast intermittently, sometimes with red flyback lines. This could have been caused by incorrect first-anode voltage setting but, while I was attempting to adjust this, I found from the cathode voltages that the emission of the CRT’s red gun appeared to differ from that of the other two guns. The red problem was still present when the red and green cathode drives had been swapped over, so the cause of the fault was proved to be in the tube.

A replacement CRT and readjustment of the A1 voltage produced an excellent picture. R.B.

**Sony KVX2972U (AE2B chassis)**

This set worked normally until the channel was changed or the aerial was disconnected. The loudspeakers then crackled. A Sony technical information sheet directed me to the mute circuit in the audio power amplifiers. Two new TDA7052 power amplifier ICs were required. R.B.

**Sharp 56FW53H (DA50W chassis)**

This set was dead with just light from the orange neon. Excessive HT problems can occur with this chassis, and seemed to be the cause of the trouble as the crowbar avalanche diode D735 across the 150V line was short-circuit. I replaced the diode and the feedback optocoupler IC705 but the power supply still refused to start. The two surface-mounted transistors Q702 and Q703 on the primary side were leaky and had to be replaced. R.B.

**Philips 32PW9616/05 (MD2.12 chassis)**

The sound from the centre speaker of this Dolby Pro-Logic set was badly distorted. Sound from the left, right and surround channels was OK. After some time spent checking the Dolby processor and power amplifiers, which all seemed to be OK, I decided to check the obvious thing: the drive unit was out of centre and had to be replaced. R.B.

**JVC AV24WT2EK**

This small widescreen set had exhibited field collapse before it went off. On inspection I found that the LA7841 field output chip IC401 had been overheating. Replacement resulted in brief screen illumination, then the set tripped off. IC401 is fed from split +14V supplies, and the –14V supply was missing. Feed resistor FR553 (1Ω, 1W) was open-circuit because capacitor C407 (100μF) was short-circuit. FR555 in the +14V feed had also risen slightly in value, so this item was also replaced. After that there was a very good picture. G.D.

**Ferguson C49F (Thomson TX90 chassis)**

After repairing an arc fault in the line output stage I was left with very low sound. The cause is usually C514 (1uF) in the IF unit, but not this time. The volume-control voltage reached only 3V, though the bar-graph indication increased. I then found that there was no access to the tuning function. I assume that the set was in the hotel mode, corrupted as a result of the arcing, but the manual doesn’t mention this. As I happened to have a scrap chassis I simply replaced the microcontroller chip, which cured the fault. Someone is sure to know how to unlock the micro! G.D.
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**V i r u s e s**

There have been letters and articles in the magazine recently about e-mails and viruses. I’ve had several e-mails with virus-infected attachments from commercial organisations that ought to have known better. I’ve also had a 6.4Mb e-mail that completely clogged my mailbox. Because of this I now use a freeware program called MailWasher. It gives access to the server and enables me to check who the e-mails are from, their size and if they have any attachments. I can then opt either to download, delete from the server or bounce them. Bouncing gives the sender the impression that the e-mail address is invalid, and is a useful way of dealing with spam and other unwanted messages. If the message reappears, it can be deleted.

**Alan Jones,\nPontrug, Caernarvon.**

**Mains switch problems**

In connection with David Smith’s letter on burnt mains switches in Philips TV sets (August), I covered the problems with switches that arc and burn in Philips sets in my article in the February 2001 issue of *Television*. The problem is not just to do with the switch, but with the fact that the only electrical protection for the switch and PCB is the 5A fuse in the mains plug – assuming of course that the customer hasn’t replaced this with a 13A fuse or a piece of silver foil! The point here is that the mains input fuse is on the wrong side of the switch, i.e. after the switch.

SEM can supply blank OEM PCBs for these sets. The boards are made of fibreglass and are therefore probably fire-resistant. Order codes are SWPCB1, SWPCB2 and SWPCB3.

With regard to the legalities of a set catching fire because of the switch, if you can show that the switch is a genuine Philips item then Philips is surely responsible? As these switches normally last for a couple of years, your customer may be hard-pressed to prove that you were the cause of such a fault. If you are unfortunate enough to get caught up in such a situation, my advice would be to place the matter in the hands of your public liability insurers who, I’m sure, would be happy to pass the case to Philips.

**Michael Maurice,\nWembley, Middx.**

Three failed switches found by one repairer in a short period of time suggests a common problem. Official Philips dealers may know about a bad batch of switches, and there might be a free-issue replacement scheme. But burn-ups as described shouldn’t happen, even after four years. Power switches are made with safety in mind: the demands of the safety standard EN 60065 are quite severe.

Incidentally the report of the Media Fusion distribution scheme (Power-line communications, page 588) indicates, if accurate, that the company claims knowledge hitherto unknown to science. It’s likely to remain so!

**John Woodgate,\nRayleigh, Essex.**

**Power-line communications**

J. LeJeune’s article on power-line communications (August) was an interesting read. Pylons have already been used for nationwide fibre-optic communications – it’s possible to see the fibre-optic cable wound around the uppermost earth wire. But suggestions that power lines should be used for telecommunications traffic is not good news at all.

The Radio Society of Great Britain and others, including radio broadcasters, have registered concern over the real possibilities of RFI caused by power-line telecommunications (PLT). Measured interference has been noted, particularly at MF and HF, during PLT tests. It could well disrupt MW, SW and related HF communications services. The potential problems have been described in *RadCom*’s bi-monthly EMC column during the past year-eighteen months (see in particular the October 2001 issue), and the subject is on the ITU’s agenda for discussion.

If PLT gets the go-ahead, the national grid would in effect be a vast aerial system radiating interference, disrupting radio communications at up to mid-HF. Perhaps the technology should be laid to rest now.

**Roger Bunney,\nRomsey, Hants.**

J. LeJeune discussed several problems with PLT systems in his article on Power-
line communications in the August issue, but omitted reference to the most significant problem. Any data transmission system that uses totally unscreened and unbalanced cables will radiate the signals into the surrounding area and beyond. If this radiation is not to cause interference with licensed radio services in the MW and HF spectrum, the levels on the lines must be reduced to the extent that the system won't work. Commercial broadcasters, the Radiocommunications Agency, Amateur Radio societies worldwide and others have for a number of years lobbied the proponents of PLT to prevent the widespread disruption of services that would arise if PLT became widespread.

I understand that this problem was one of the main reasons why NWEB abandoned its trials last year. There is at present a system in operation in Germany with radiation levels far in excess of what would be allowed in this country.

Dave Sergeant, G3YMC, B.Sc., C.Eng., MIEE, Bracknell, Berks.

Grundig GDS capacitor kits

In the July issue Satellite Notebook Pete Haylor mentioned power supply capacitor kits for Grundig GDS digiboxes. Kits have been available from SatCure for over a year. C1 (220µF, 400V) is at present not included, as we've never known one to fail. But we monitor repairs and, as equipment ages, additional parts are included in our kits as required. Our capacitors are slightly larger physically than the originals, in order to ensure the lowest possible ESR and best reliability.

Martin Pickering, Technical Director, SatCure. www.sature.co.uk

Knife-edge refraction

I was very interested to read Roger Bunney's account of signal refraction effects (DX and Satellite Reception, August). Years ago I used to install aerials on a fixed-price basis for a rental shop in Barnsley. The name of the game was to obtain acceptable reception as quickly and cheaply as possible, so every installation was limited to a basic ten-element array on a standard fixing.

There were a lot of customers in one particular pit village that was very close to the Emley Moor transmitter. Normally in that district the only problem would be the cost of an 18dB attenuator, but unfortunately the massive colliery waste tip obstructed the line-of-sight to the transmitter. The tip towered above the village, and reception from Emley Moor seemed at first sight to be a hopeless prospect. Because of the cost limitation, use of a high-gain aerial pointing at an alternative transmitter, with a masthead amplifier and all the trimmings, was out of the question.

To my surprise, I found that Emley Moor reception was in fact possible, but the height of the array was critical. The trick was to angle the array slightly upwards, so that it pointed at the edge of the tip in the direction of the transmitter, then move it bodily up and down on the mast without changing the upward tilt or the direction. Regularly-spaced nulls and peaks would be found as an array was raised or lowered, and a peak for one channel would generally work for the other two. Two? Yes, this was a long time ago! Signal levels would at best be 25dB below the line-of-sight figure, but this was good enough and, as there was nothing much to the rear to reflect the signal, the ghosting wasn't too bad.

The smooth top of the waste tip was undoubtably refracting the signal, and it seemed that a pattern of field strengths was produced, with shallow, horizontal zones of fairly strong signal interspersed with identical zones of little or no signal.

Once the critical height had been found, it was possible to fit another array at the same height on the other side of the chimney and get similar results. Sometimes the zone of maximum signal would be at the base of the chimney and the array had to be at the bottom of the mast, below the chimney bracket.

We have a very good view westwards towards the high Pennines where I live in South Yorkshire, but we certainly don't have line-of-sight to the Winter Hill transmitter "on the other side of the hill". Winter Hill reception is to all practical intents impossible in this area but, since the view in that direction is so clear, curiosity made me try it. I found that a very weak signal is available, but only at a certain height. Since our village is on the side of a hill, this contour is at roof height in one place and at ground level in another. But it doesn't matter where the aerial is located, as long as it is at the critical height. Reception is possible across a vertical distance of about 2m.

My own roof is much higher than this 'fuzzy contour'. There is no Winter Hill signal whatsoever up there. It's the same at the top of the tallest tree at the highest point in our garden, but an array on a short mast on the back shed works quite well — see accompanying photograph. This seems a bit bizarre, because the signal path must be under the branches of a nearby tree! The aerial is an Antiference XG21CD. Granada ch. 59 is received at 38dBuV, with a signal-to-noise ratio of 26dB. If the aerial is fixed much more than a metre higher or lower, the signal disappears under the noise.

The roof-mounted aerial at a nearby bungalow is at the critical height and, despite it being for the wrong channel group, it receives a very faint signal from Winter Hill. I conclude that the Winter Hill signal is refracted across the far-away Pennine hill tops and that the angle of refraction is very well defined. Since this is a coal-mining district, it seems appropriate to describe the phenomenon as being like a "seam" of relatively high field strength. The effect has been consistent for many years.

I have occasionally been troubled by...
signals that are refracted by trees. It seems that the tree, when in full leaf, re-radiates the signal. Whether this is true refraction or something else I don’t know. Typically the phenomenon occurs when there’s a small group of trees something like 300m away, standing slightly to one side of the direct signal path. The result is not ghosting, because the delay is not sufficient, but instead signal-cancellation because of the out-of-phase condition. It can seem very strange to have perfect line-of-sight to a high-powered transmitter yet receive very low signal levels. The first time this happened I was slapping the meter under the impression that it was faulty! Slight sideways or forward/backward movement of the array will usually restore almost normal signal levels, but unfortunately the effect is unpredictable and the low signal levels may recur. I have come across this situation only in summer near broad-leaved trees.

Incidentally my learned friend Alan Pemberton points out that we should be talking about knife-edge diffraction rather than refraction. The latter occurs when a wave passes through the interface between two media of differing refractive index. With the knife-edge phenomenon this is clearly not the case. Instead the signal passes close to an obstruction which “perturbs” it so that it arrives in the shadow area of the obstruction.

Bill Wright, Micklebring, Ratherham, S. Yorkshire. wrightsaerials@aol.com

**Telephone checks**

Do you need to test your phone bell ring, exchange line or caller ID display unit? Quite by accident. I’ve stumbled across BT exchange/telephone automatic test equipment. I’m not sure whether it’s a national number, but in my phone area – 0151, Merseyside – you just dial 175 and follow the instructions.

The answer you get is a female voice which says “you are connected to XXXX, your phone no. XXXX: start the test”. Replace the handset and wait for approximately thirty seconds. The phone will then automatically ring back, testing your phone bell. Answer, and you will hear “line testing OK” or “earth fault A”. Dial “next test”, then there’s a dial tone. Press 1 “start test” then dial a few digits. It seems to come back with “dial fault” (unsure, maybe someone could explain – new phone!). Dial next test, dial tone, press 1 and replace handset. If you have a caller ID display unit, a test data burst is sent and you should get the display 0123456789. If one is fitted, the ring LED flashes.

You need to experiment, but the service is free. Maybe a BT engineer could provide further information?

Alin Cranford, Birchend, Cheshire.

**Sharp 59D503H**

In the July TV fault-finding section there was a report about the 28in. version of this set being stuck in standby because of a short-circuit line output transistor caused by a dry-jointed capacitor. I’ve had a few of the 59cm sets with the same problem, but the transistor is a BUH515 and the dry-joint is at the adjacent capacitor C613. The transistor seems to go very low resistance (100Ω or so) base-to-collector rather than totally short-circuit all ways round. The result is the same though!

Nick Beer, Bideford, Devon.
Bench Notes

Stormy times
Many engineers seem to shy away from items that have been damaged during electrical storms. In my experience however these can provide profitable repair work. I always quote for a couple of hours’ labour, and allow a reasonable sum for parts. A total estimate of about £70 plus VAT should cater for most situations. As many such repairs are paid for by insurance companies, this is considered a reasonable sum.

When tackling the consequences of lightning damage, I always start with the power supply. Regardless of whether they have actually failed, I replace the chopper transistors, any driver transistors and the control IC. I then carry out cold checks on all the resistors in the primary side of the circuit, and check the optocoupler.

After replacing the main items in a Panasonic NV-HD660 VCR however there was still no operation. Quick checks in the primary side of the power supply revealed that there was no drive from the chopper control chip. After extensive tests and the replacement of many parts, I finally discovered that Panasonic provides a repair kit for this series. The part number is VUE4125K1T, and it contains 18 items. After fitting the kit I switched on and waited for the bang! To my relief the kit had provided a complete cure.

Another couple of storm-damaged items arrived recently, this time 28in. TV sets. They were both the same model, Matsui 28M1MK111, which is fitted with a Sanyo chassis. In each case the 2SC4429 chopper transistor was short-circuited, though no series resistor or fuse had blown! The first set was brought back to life by replacing the chopper transistor and its 2SC3807 driver transistor. The second one remained dead after this action however. R620 (120kΩ) in the start-up circuit had to be replaced.

If you still have problems after attending to the power supply in storm-damaged equipment, first check any protection circuits on the secondary side of the power supply. After that, suspect the microcontroller chip and the EEPROM. If you still have problems, remove the tuner unit and try again. Finally, if necessary, replace any jungle chips.

By now you should have achieved a successful repair, be within budget for parts and have made a healthy profit on your labour. Very rarely are line or field output stages affected by storm damage. I’ve only ever been caught out twice. The first time was with an older Ferguson set fitted with the ICCS chassis. After carrying out all the above measures, the line output transformer turned out to be shorts. The second case was with a Panasonic TV set that, after repair, had a very low-emission tube!

The Vestel 11AK19 chassis
I service a large number of sets that fitted with this chassis, many of them under warranty. They are popular with a number of distributors and can be used with a wide range of CRT’s, both 4:3 and widescreen. Here’s a list of common problems I’ve encountered.

Failure of the line output transistor is quite common, especially when a 2SD2579 is fitted. I always fit a BU2508AF, which most Bush sets use, as it’s more reliable. On several occasions I’ve had one of these sets that continued to trip after it had been to another dealer for attention. In each case I found that a BU2508AW had been fitted. As this transistor is not isolated, it shorts the line output stage to the heatsink. This is one to look out for.

If you encounter one of these sets with a blown-up power supply, suspect the TDA8351/8356 field output chip as being the cause. Its failure seems to take out a large number of components in the power supply. For a lasting repair, replace the chopper MOSFET Q802. R825 in its HT feed, diode D807 in the snubber network and diodes D826 and D827 which are in series with the tuning capacitor.

No picture is commonly caused by the RGB output chip IC901 on the CRT’s base panel, but can also be caused by the TDA884X 1F/colour decoder/timbase generator chip IC401. Another cause of no picture is C604 (47nF, 63V) in the beam limiter circuit. It can become leaky. I have had R617 (220kΩ) go high in value, the result being a washed-out picture.

EW problems are very common, particularly with widescreen sets. The usual culprit is a dry-joint at C630. This leads to the EW driver MOSFET’s drain circuit safety resistor R629 going open-circuit. Use a 2-7Ω fusible resistor in this position in 4:3 aspect ratio sets, or a 27Ω resistor in widescreen sets. On several occasions I’ve had to replace C630 because it has burnt while arcing. Various values are fitted depending on model. Make sure that you fit the correct replacement.

Although this is rare, I’ve come across sets that won’t accept a scar input. The cure has been to replace the TEA6415C video switching chip IC505.

Finally, don’t be put off repairing sets that are physically damaged. Bush is very reasonable when it comes to replacement cabinets. I recently ordered a front cabinet for a 28in. 4:3 model; the trade price was only £10 plus VAT.

Test equipment
Before I close this month, here’s a useful test equipment tip – but forgive me if you already use this method and I’ve been slow to catch on! I recently replaced my multimeter with an auto-ranging model that includes all the usual refinements plus several extras. Amongst these are a capacitance meter and a frequency counter.

Previously I would often fire up my scope to check the line drive with TV sets and monitors and the switching action with power supplies. One day however I accidentally connected my meter, while on its frequency-counter range, to the base of a line driver transistor. Hey presto, I was provided with a reading of 15-62kHz. I now always use the frequency-counter for these tests and find this much quicker for fault-finding. In fact I haven’t switched on my scope for over six weeks!

To follow
Next month I’ll take a look at cheap Daewoo VCRs and provide a roundup of faults experienced with the Beko C14 chassis, which has superseded the AK 19 in many Bush models.
Paul was on duty when our first caller of the day came in. It was Mr Meddler, a friendly little fellow with sticky fingers and a pocketful of money that he likes to spend on his hobby, which is pulling things to bits. He had a shopping trolley with him, and started to natter away as he struggled to open it.

"Hello Mr Bullock. Now, I've something in here. Where is it? It's catching. Why won't it come out? Ah, here it is now. This is it, Mr Bullock. It was all right, but it don't work now. Dunno why, really don't."

He had extracted a half-dismantled JVC video recorder. As he fished about for more bits he continued his commentary.

"Ah, there's the rubber drum thing, Mr Bullock. Came off. Dunno why. And this pulley thing. Funny, innit, the way these bits come off like."

Paul stood impassively and stony-faced until all the bits had been put on the counter. He then sent Mr Meddler on his way and started on the reassembly job.

"I wouldn't do it for anyone else" he said, "But he's such a polite and vulnerable chap, and he doesn't mind paying."

Paul soon had the machine working again. The cause of the trouble had been the usual one with this series of machines. There's a brass retaining boss on a shaft under the lacing guides. It's not supposed to move, but can slip down. The mechanism then seizes.

"Some engineers insert a bit of Rizla paper between the shaft and the boss to make a tighter fit" Paul commented, "but I use Araldite."

Most of Mr Meddler's bill will be for all the extra work he caused. He doesn't seem to mind and, since he pays. I don't either."

When Mr Meddler returned he was beaming and happily reached for his wallet. "Is it done, Mr Bullock?" he asked. "What was it then? One of the parts? Which one was it? The rubber drum thing, or maybe the pulley?"

Paul gave him a brief explanation, and off he went.

A massive Sony

We had a 29in. Sony set in later that day, Model KVE2922U (AEIC chassis). Its owner struggled in with it. "I'm Tim Breeze" he told us, "the sets seem to get bigger and heavier as I get older. This one is stuck in standby, and so am I."

Steven was in at the time and decided to take it on. It was dead, not stuck in standby. The 2SD1548LB chopper transistor Q602 had a base-emitter leak and the 4A mains fuse was blown. After checking for any obvious shorts, Steven fitted replacements and switched on. The fuse blew immediately, and the new transistor died. On further investigation Steven found that there was a dry-joint at the TEA2260 chopper control chip IC601 and that the 47μF, 50V base-drive coupling capacitor C611 was leaky. He decided to replace the chip as well as the capacitor and the other items. After that the set was OK.

"I expect you're wondering what I do for a living." Breeze said when he returned. "I'm a carpenter by trade, and sticks up the skittles at the Twelve Bells on Wednesday nights. I've had some cards printed -- look." He handed a card to Steven. It said "Timothy Breeze, carpenter and sticker up". Steven nodded and handed it back.

Camcorder trouble

A couple of weeks later he was back. this time with an Hitachi Model VMES688E camcorder which had a cassette jammed inside. Steven had gone out to have a look at the vicar's TV set, so Paul had a go at it.

He tried to eject the cassette but, although we could hear the motor, the carriage didn't move. He set about stripping the unit down and found that the loading motor, which is mounted vertically, just to the left of the video heads, had popped out of its flimsy plastic holder.

"I can only do what I've done before with these units" Paul said. He reinserted the motor and used a plastic cable tie to strap it in place.

Timothy Breeze had more news to impart when he called to collect it.

"You know that the BBC was inviting viewers to write and send in plays, don't you?" he said.

We didn't.

"Well, they wuz" Breeze continued. "so I wrote one and sent it in. Got a nice letter back from them saying 'nice try'. " He then reached into his inside pocket and pulled out a visiting card. "Just 'ad these done" he said, handing it to Paul. "Timothy Breeze" it said, "carpenter and sticker up, and BBC playwright."

Interlude

Just then Greeneyes came in with
our tea. "I'm not having tea myself today" she told me, "just lemon juice. So I'll stay slim enough for that pale peach costume."

"What pale peach costume?" I asked.

"The one you're going to buy me at Marks and Spencer" she replied. "Here, hold this glass while I squeeze some lemon juice into it."

I got a dose of it in my eye.

**Faulty equipment**

In a previous article I mentioned the very cheap Cookworks K8396 electric kettle that I obtained from Argos for only £8.95. We have found it very useful, but it's developed a couple of annoying traits. First, the water-level float tends to stick near the bottom of the visible water column, giving the impression that the kettle needs to be filled when it doesn't. Secondly its on/off switch tends to stick in the off position, so that if you want a cup of tea you have to rattle it up and down until the light in its little window comes on. Small things, I suppose, that might happen with any kettle.

I've also mentioned the compact and tidy little Aiwa digital audio system, a quite expensive Model NSX999, that I bought a year or so ago. The first thing I noticed about this was that it was so packed with unnecessary, gimmicky sound-effect features that it left you with the impression that it might not work at all. But, since it's so expensive, I suppose that that might happen with any piece of equipment.

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**CD trouble**

But Greeneyes soon complained that in addition to the Aiwa's thick sound (ideal for Wogan) it misbehaved when she played CDs. There was intermittent playing, skipping, long gaps between tracks and premature closing down. The CD performance with the Woolworths unit was much better, but occasionally dicey.

Now Paul specialises in VCR and audio rather than TV repairs, so I asked him to look at both players during his next visit to us. He popped a CD into the Aiwa machine first and tried it. "The usual TOC trouble" he announced, "almost every job I get with this trouble is an Aiwa. Got a cotton bud and a scope?"

"Scope?" I replied, "not here I haven't. I even hide the screwdrivers in this house. But I can probably manage a cotton-bud stick. Would you need a drop of alcohol as well?"

"Just a small glass of wine would be nice" he said. "I don't use any spirit on the cotton buds. It can cause blooming when used on some laser lenses, and there's the additional risk of loosening certain cements."

He cleaned the laser then played a CD, gently tapping the top of the cabinet with his fingernails to encourage the machine to skip, while carefully adjusting the beam-focus potentiometer. Within a minute or so the unit played the CD perfectly in spite of the tapping, and Paul pronounced it OK. "But not for ever" he added. "It'll need doing again in a few months' time. They always do, these Aiwas."

He then tried the Woolworths machine, using the same technique. This one also played up as he tapped it, but he was again able to get it going reliably by adjusting the laser-beam focusing potentiometer. "How did you know what the trouble was?" I asked.

"By looking at the display as I put the CD in" he replied. "If the TOC reading is uncertain or absent, focusing is usually the trouble."

Greeneyes was looking at him in admiration. "Then she looked at me, pointedly. "Didn't you know about that?" she asked.

"Of course I did" I replied, "in fact I think it was I who originally told Paul how to do it." "

**Philishavers**

But here's something I did discover recently, all by myself, though rather late in life. I've used Philishavers for years, and regard them as the single exception to my conviction that while Philips is tops for electronics the company's mechanical products tend to be inept and flimsy. Perhaps this is because of the miseries I suffered during my salad days trying to service Philips autocatchers, which were so full of bits of tin and thin-wire rods. Anyway, I'd come to the conclusion that the gradual deterioration with continued use of a Philishaver was caused by head wear. So, when my latest one got to providing me with a less than perfect shave, I decided to lash out on a new set of heads.

Sure enough they did the trick. Shaving became a pleasure again. But only for a week or two, despite my rigorous cleaning with the brush provided. Then I saw a big Philishave advertisement in a newspaper, announcing a new Philishave whose head assembly, it was said, could be washed out under the tap.

"But why only the latest Philishave head assembly?" I asked myself, "surely all Philishave heads are basically alike?"

So, after shaving, I thoroughly washed the head under the pressure of water from the cold tap, allowed it to dry thoroughly, then refitted it to the shaver. Next time it gave me a perfect shave, as good as a new head assembly. I've been doing this for a couple of months now. It certainly works for me!

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**Make sure of your copy of Television**

It can be difficult finding a copy of *Television* at local newsagents. The number of magazines being published keeps increasing, which means that newsagents have less shelf space for the display of individual titles. Specialist magazines in particular get crowded out.

There's a solution to the problem. Most newsagents provide "shop-save" and/or home-delivery services. There's no charge for a shop save. You simply ask your newsagent to order a copy for you: it will be kept on one side each month ready for you to collect. Home-delivered copies are ordered in the same way, but generally incur a delivery charge.

A newsagent can order any magazine for you, whether or not the shop normally stocks it. If you buy your copies of *Television* from a newsagent and want to make sure you get every issue, just ask at the counter.
Answer to Test Case 477
- page 677 -

During the rest of the day Service Manager’s belief that field servicing is money for old rope was to change for good – especially after he scraped the van on a wall and picked up a parking ticket in Hawkfield high street. The first problem was easily solved. Satellite TV was being delivered to the TV set via its aerial input socket, and digiboxes don’t incorporate a Nicam encoder! The solution was to link the twin via a scart lead. There was still no “stereo” caption on the screen with satellite TV – this happens only when a Nicam carrier is present – but there was certainly stereo sound.

The solution to the DVD disc-rejection problem was a bit more involved. Sage got Colin Doc to call up websites dvedviewer.co.uk and dvddebate.com. There’s a great deal of information there on adapting DVD players for multi-region use. ‘Handset hacks’ are available for many cheap DVD players, and the player concerned was amongst them. Service Manager followed the instructions to put it into the ‘bypass’ mode, after which all was well – until the customer inserted a Region 1 RCE (Region-Code-Enhanced) disc, which will not work with a ‘code-bypassed’ player. Colin Doc ensured that ‘Region 1’ rather than ‘bypass’ was selected with US-sourced RCE discs. Peace then reigned once more!

NEXT MONTH IN TELEVISION

A guide to the Panasonic Euro-7 chassis

The Euro-7 chassis was introduced in late 2000 for use in high-performance, large-screen TV sets, replacing and updating the ageing Euro-5 chassis. It has a number of features that were new to the Panasonic range, including progressive-scan technology, twin RGB inputs and twin UHF tuners. Other features include 3D on-screen graphics displays, advanced 100Hz processing, flash upgradeable on-board operating software, and AC3 and DTS audio processing. Brian Storm provides a description of the technology involved.

PIC-based TV pattern generator

Use of a PIC microcontroller chip has enabled Denis Mott to come up with this relatively simple (just three ICs and a handful of transistors) portable pattern generator, which is easy to use and produces a range of patterns for TV set assessment. It includes a modulator to provide a UHF output, and can be powered by four AA batteries or a 240V AC mains input.

DVD fault reports

Return of our DVD player page, with practical tips and fault-finding guidance.

The 3-D IC memory

Getting more into less space has been the story of IC development to date, particularly with memory devices. But a fundamental limit will be reached when gate size is as small as electron wavelength, transistors don’t work! One technique that could be used to increase storage capacity is to adopt 3-D instead of 2-D fabrication. Ralf Buckstone describes past work on this possibility and some recent advances.

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Board cameras all with 512x582 pixels 8.5mm 1/3 inch sensor and composite video output. All need to be housed in your own enclosure and have fragile exposed surface mount parts. They all require a power supply of between 10 and 12v DC 150mA.

- 47MR size 60x96x27mm with 6 infra red LEDs (gives the same illumination as a small torch but is not visible to the human eye) .................................................................................................................................................................................................................................................£37.00 + vat = £43.48
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1206 surface mount resistors £12 values 10 ohm to 1M ohm 100 of 1 value £1.00 + vat 1000 of 1 value £5.00 + vat 866 battery pack originally intended to be used with an orbitel mobile telephone it contains 10 1.6Ah sub C batteries (42x20x51 the size usually used in cordless screwdrivers etc.) the pack is new and unused and can be broken open quite easily ..................................................................................................................................................................................................................................................................£7.46 +vat = £8.77

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