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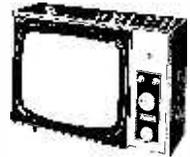
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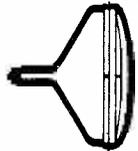


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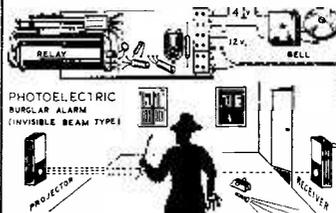
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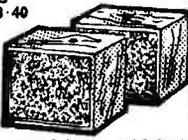
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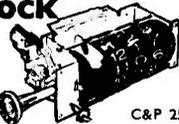


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	List Price	Lasky's Price	C&P
LINTON 2 Pair	£49.90	£38.75	£2
TRITON 3 Pair	£65.00	£51.50	£2
MELTON 2 each	£35.00	£25.50	£1
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ROSEDALE each	£65.00	£50.00	£1
UNIT 3 each	£12.50	£9.50	50p
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EXCLUSIVELY FROM LASKY'S
 The clock measures 4 1/2 W x 1 1/2 H x 3 1/2 D (overall from front of drum to back of switch). SPEC.: 210/240V a.c. 50Hz operation; switch rating 250V. 3A. Complete with instructions. **HUNDREDS OF APPLICATIONS**
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 • FORWARD AND BACKWARD TIME ADJUSTMENT • SILENT OPERATION
 • SHOCK AND VIBRATION PROOF
 • BUILT IN ALARM BUZZER
SPECIAL QUOTES FOR QUANTITIES



C&P 25p

LASKY'S PRICE **£6.50**

BSR TD8S

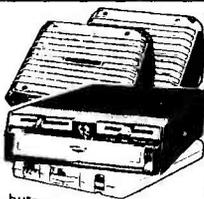
8 TRACK STEREO CARTRIDGE PLAYER
 The unit is switched on and off by the insertion of the cartridge. The TD8S is suitable for use with most modern stereo amplifiers and delivers a pre-amp output of 125mV. Power requirements: 210/250V AC, 50Hz. Frequency response: 50Hz-10KHz. 4 pole dynamically balanced synchronous motor maintains unwavering speed accuracy - independent of mains fluctuations. Compact in size the TD8S is housed in black and woodgrain plastic cabinet. Size: 8 1/2(W) x 3 1/2(H) x 10 1/2(D) in.
 List Price £24.20



TD8S is C&P 35p
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BELTEK 8 TRACK

Stereo car Player
 Accepts all standard pre-recorded 8 track stereo cartridges and other features include automatic head cleaner, channel select and channel repeat push buttons, slider type volume and tone controls, channel balance control. Tech spec. max output 10W (5 watts per channel), frequency response 50Hz-10KHz. Output imp. 4 ohms. size 4 1/2(W) x 1 1/2(H) x 6 1/2(D) in. Operates on 12V DC negative earth systems. Beautifully styled with black ivory and chrome trim finish.



BELTEK C5700 complete with mounting brackets and 8-track pre-recorded demonstration cartridge **£23.50**
 BELTEK C5700 with pair SP24 speakers C&P 25p each **£29.00**

Beltek SP24 speakers are available perfectly matching the C5700 in performance and finish specially designed for optimum performance in heavily damped car interior. Size: 7 1/2 in(W) x 6 in(D) x 4 1/2 in. rear, 2 1/2 in front (H). Comp with connecting leads. **£7.95** Pair

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1000 ohms/volt
 Lasky's new look top value TM-1 is a really tiny pocket multimeter providing "big" meter accuracy and performance. Precision movement calibrated to +3% of full scale. Click stop range selection switch. Beautifully designed and made impact resistant black case with white and metallic red/green figuring. Ohms zero adjustment.
1000's IN USE SIZE ONLY 2 1/2 x 3 1/2 x 1 1/2
 • DC/V: 0-10, 50-250-1000 at 1K/ohms/V • AC/V: 0-10-50-250-1000 at 1K/ohms/V • DC Current: 0-1mA, 100mA • Resistance: 0-150K ohms • Decibels: -10 + 22dB. • Complete with test leads
LASKY'S PRICE £1.85 C.&P. 15p



TM-5 TEST METER

5000 ohms/volt
 Another pocket multimeter from Lasky's. The "slimline" impact resistant case - size 4 1/2 in x 2 1/2 in x 1 1/2 in fitted with extra large 2 1/2 in square meter. Readability is superior on all lower ranges, making this an excellent instrument for servicing transistorised equipment. Zero ohms adjustment. Buff finish with crystal clear meter cover. • DC/V: 3-15-150-300-1,200 at 5K ohms/V. • AC/V: 6-30-300-600 at 2.5K/ohms/V. • DC Current: 0-300uA, 0-300mA. • Resistance: 0-10K/ohms 0-1M/ohms • Decibels: -10dB to 16dB.
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High precision low-mass counter-balanced pick-up arm, heavy balanced turntable, simple to operate controls, viscous cueing device, slide in cartridge carrier, 4 pole motor.
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BSR McDONALD UNITS & PACKAGES

A. Chassis only. B. Complete with Lasky's plinth and cover. C. Complete with Lasky's plinth, cover and AD76K cartridge. D. Comp. wired on BSR plinth with cover. E. As D plus AD76K cartridge.

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MP.60	10.95	15.30	18.50	18.75	22.00
HT.70	15.95	19.90	23.50	23.75	27.00
610	14.50	18.75	23.00	22.25	25.50
510	12.10	16.50	18.85	20.00	22.85
310	9.75	14.00	16.50	17.25	20.25

210 Complete with plinth, cover & BSR cartridge
 MP.60 TFD2 Styrene base 17.50 21.00

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W1/700 MW/LW
 A new two waveband all transistor car radio that covers full medium and long wavebands with slide switch wave change. Large easy to grip controls. Illuminated dial with "easy to read" tuning scale. Externally adjustable aerial trimmer ensures maximum output. Powerful output stage gives perfect reproduction through either one or two speakers. Operates on all 12 volt D.C. system. Negative or positive earth. Standard size 6 1/2 in (W) x 4 1/2 in (D) x 2 1/2 in (H). Black with chrome trim. Complete with speaker, baffle, leads, mounting brackets and instructions. Fully guaranteed. Complete with speaker, baffle & mounting bracket.
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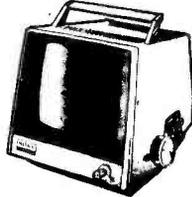


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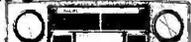
SONY TV SCOOP

TV-720UK—the world in 7"
 This miniature portable television can be operated by household current, rechargeable power pack or 12V car/boat battery. The special anti-glare screen gives a perfect picture even in sunlight. Attractively finished in ebony and chrome. Here's a portable companion that brings you a world of viewing wherever you are. Brief Spec.
 • Screen size 7in. measured diagonally. • System: 625 UHF. • Antenna system: Built-in loop aerial. External 300 and 75 ohm switchable. • 23 transistors, 15 diodes, 3 thermistors, 1 EHT rectifier (selenium). • Power source: AC 240V, 50Hz; DC 12V. • Power consumption: AC17W, DC 11W. • Dimensions: 9in. x 9 1/2 in. x 1 1/2 in. • Weight: 8lb. 13oz. • Accessories: Earphone, loop aerial; polishing cloth.
 List C.&P. £1.50
LASKY'S PRICE £42.00
 Price £59.75



CAR RADIOS FROM PHILIPS

MODEL RN 214/15
RN214 is a triumph of micro-miniaturisation. So compact and light mounted on its spindles only, it needs no feet support. The RN214 can be fixed quickly and easily. Spec: Power supply: 13 volt D.C. negative earth operation only. Power output: 5 watts. Wave ranges: Medium wave: 185m-586m (1622-512kHz). Long wave: 1030m-2000m (290-150 kHz). Intermediate frequency: 470kHz. Size: 7in x 1.6in x 3.6in. EN8893/05 general purpose mounting kit with loudspeaker £2.70 extra.
 List Price £19.25
LASKY'S PRICE £15.50 C.&P. 25p
MODEL RN 314/15
 The RN314 gives you big sound because of the high sensitivity from the tuned RF stage. Due to its compact size it can be mounted without any rear support. Spec: power supply: 12V DC neg earth only. Power output: 5 watts RMS. Wave ranges: Medium 185m-585m (1622-512kHz); Long 1030m-2000m (290-150kHz). Intermediate frequency: 470kHz. Size: 7in x 1.6in x 3.6in. EN8893/05 general purpose mounting kit with loudspeaker £2.70 extra.
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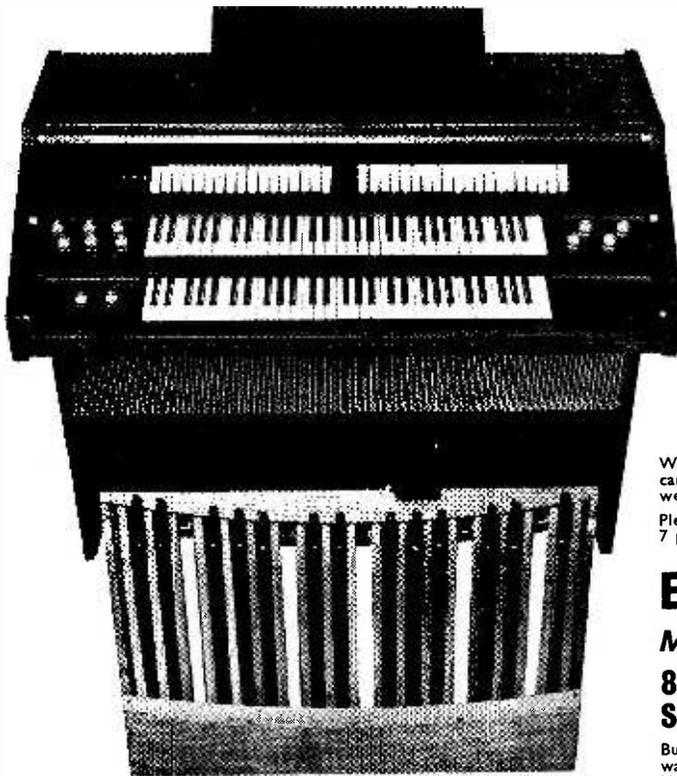
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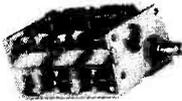
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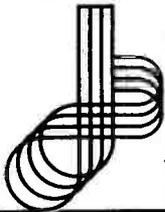
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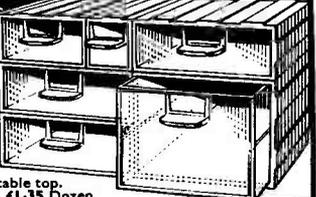
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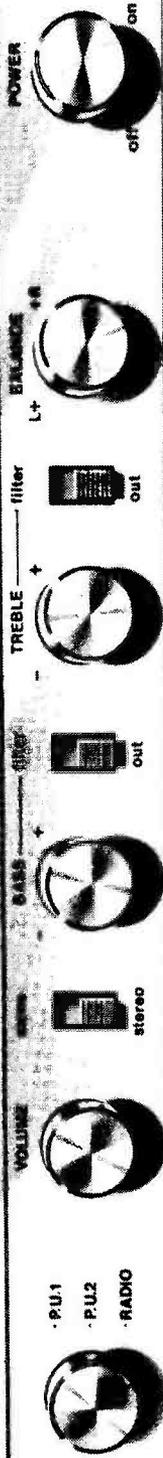
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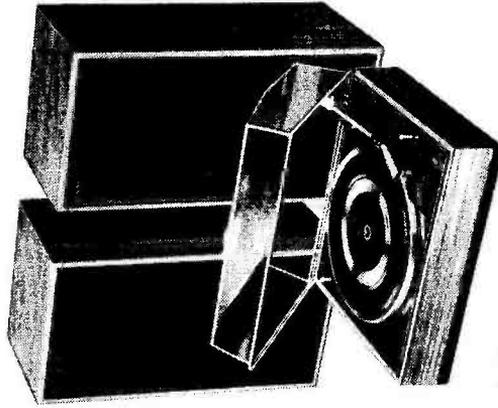
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14 watts per channel into 3 to 4 ohms. Total distortion @ 10W @ 1kHz 0.1%. P.U.1 (for ceramic cartridge) 150mV into 3 Meg. P.U.2 (for magnetic cartridge) 4mV @ 1kHz into 47k, equalised within \pm 1dB R.I.A.A. Radio 150mV into 220k. (Sensitivity given at full power). Tape out facilities: head-phones socket, power out 250mW per channel. Tone controls and filter characteristics. Bass: +12dB @ 17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble +12dB to -12dB @ 15k Hz. Treble filter: 12dB per octave. Signal to noise ratio: (All controls at max) R101—P.U.1 and radio—45dB. P.U.2—58dB. R100 same as R101 but P.U.2 (for crystal cartridge) 450mV into 3 Meg. Cross talk better than -35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 13 $\frac{1}{2}$ " x 9" x 3 $\frac{1}{2}$ ".



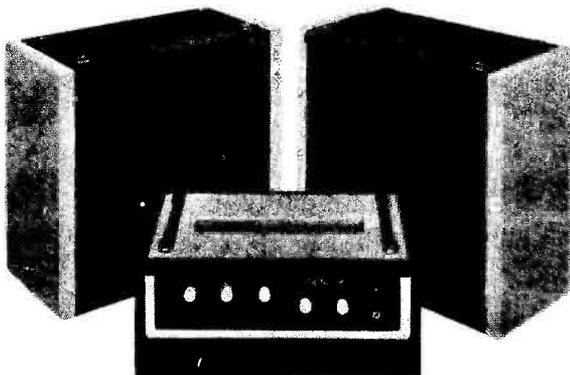
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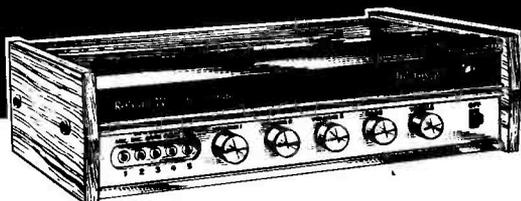
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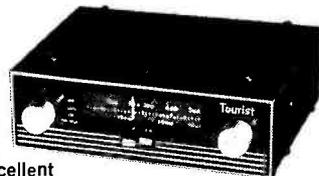
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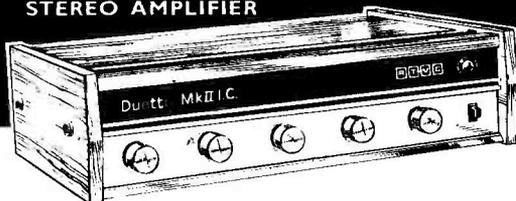
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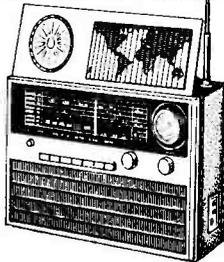
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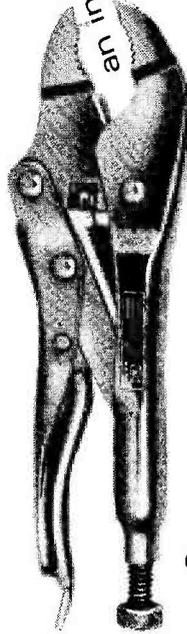


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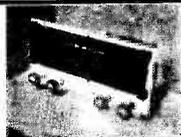
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CN.240 Miniature soldering iron 15 watt 240 volts, fitted with iron coated 3/32" bit. Up to 18 interchangeable spare bits obtainable. This iron can also be supplied for 220, 110, 50 or 24 volts. **Price £1.70**

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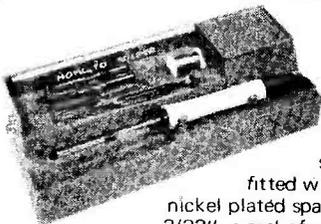
CCN.240 New model 15 watt 240 volts miniature soldering iron with ceramic shaft to ensure perfect insulation (4,000 v A.C.). Will solder live transistors in perfect safety; fitted with 3/32" iron coated bit. Spare bits 1/8" 3/16" and 1/4" available. Can also be supplied for 220 volts. **Price £1.80**

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E.240 20 watt 240 volts soldering iron fitted with 1/4" iron coated bit. Spare bits 3/32", 1/8" and 3/16" available. Can also be supplied for 220 and 110 volts. **Price £1.80.**

ES.240 25 watt 240 volts soldering iron fitted with 1/8" iron coated bit. Spare bits 3/32", 3/16" and 1/4" available. Can also be supplied for 220 and 110 volts. **Price £1.83**



**SK.1
SOLDERING
KIT**

The kit contains a 15 watt 240 volts soldering iron fitted with a 3/16" bit, nickel plated spare bits of 5/32" and 3/32", a reel of solder, heat sink, cleaning pad, stand and booklet "How to Solder". Also available for 220 volts.

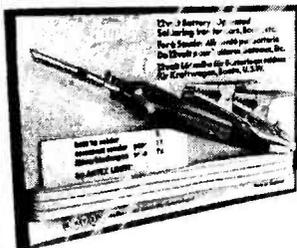
Price £2.75



**SK. 2
SOLDERING KIT**

This kit contains a 15 watt 240 volts soldering iron fitted with a 3/16" bit, nickel plated spare bits of 5/32" and 3/32", a reel of solder, Heat Sink, 1 amp fuse and booklet "How to Solder"

Price £2.40.



MES. 12

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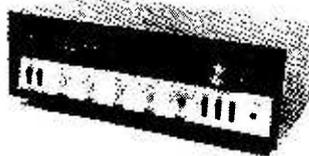


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1T4	-16	30C17	-76	EAF42	-50	EM81	-38	PCL84	-34	UBC41	-58
3B4	-26	30C18	-61	EB91	-10	EM84	-32	PCL85	-38	UBF80	-54
3V4	-37	30P5	-64	EBC33	-40	EM87	-34	PCL86	-38	UBF89	-58
5U4G	-31	30P11	-61	EB41	-54	EY11	-38	PCL88	-65	UCC84	-58
5V4G	-35	30P12	-69	EB90	-20	EY36	-59	PCL800	-75	UCC85	-56
5Y3GT	-26	30FL14	-68	EBF80	-32	EZ40	-48	PEN44	-77	UCF90	-52
5Z4G	-35	30L1	-89	EBF89	-29	EZ41	-43	PEN36C	-70	UCH42	-58
6/30L2	-54	30L15	-67	ECC81	-17	EZ80	-29	PFL200	-62	UCH81	-52
6AL5	-11	30L17	-67	ECC82	-20	EZ81	-23	PL36	-49	UCL82	-52
6AM6	-13	30P4	-67	ECC83	-35	GZ30	-34	PL81	-44	UCL83	-55
6AQ5	-22	30P12	-72	ECC85	-34	GZ32	-40	PL81A	-47	UF41	-56
6AT6	-20	30P19	-57	ECC804	-54	GZ34	-48	PL82	-31	UF89	-50
6AT6	-20	30P11	-60	ECP80	-31	KT41	-77	PL83	-33	UL41	-57
6BA6	-20	30P13	-59	ECP82	-26	KT61	-56	PL84	-20	UL84	-50
6BE6	-21	30P14	-65	ECH35	-55	KT66	-78	PL90	-63	UM84	-52
6B16	-41	35L6GT	-45	ECH42	-59	LN319	-63	PL504	-63	UY41	-59
6BW7	-52	35W4	-25	ECH81	-29	LN329	-72	PM84	-33	UY85	-25
6FL4	-40	35Z4GT	-25	ECH83	-40	LN339	-68	PX25	-95	UY4B	-77
6F23	-68	807	-45	ECH84	-36	N78	-97	PY32	-55	W77	-43
6F25	-58	AC/VP2	-77	ECL80	-30	N78	-97	PY33	-55	Z77	-22
6J7G	-24	B349	-65	ECL82	-31	PC86	-47	PY81	-25	Transistors	
6K7G	-12	B739	-62	ECL86	-35	PC88	-47	PY82	-25	AC107	-17
6K9G	-17	CCH35	-67	EP39	-38	PC96	-42	PY83	-22	AC127	-18
6Q7G	-35	CY31	-30	EP41	-30	PC97	-39	PY88	-38	AD140	-37
6N87GT	-30	DAF91	-22	EP80	-23	PC900	-31	PY800	-34	AP115	-20
6V6G	-28	DAF96	-36	EP85	-28	PC84	-29	PY801	-34	AP116	-20
6V6GT	-28	DF33	-38	EP86	-30	PC85	-25	R19	-30	AP117	-20
6X4	-22	DF91	-16	EP89	-26	PC88	-40	R20	-56	AP118	-48
6X5GT	-22	DF96	-36	EP91	-13	PC89	-46	R26	-64	AP125	-17
10P13	-58	DH77	-20	EP12	-30	PC189	-48	R28	-59	AP127	-17
12AT7	-17	DK32	-33	EP28	-55	PC805	-56	U47	-64	OC26	-26
12AU7	-20	DK91	-28	EP183	-22	PCP80	-28	U49	-56	OC44	-12
12AX7	-22	DK92	-28	EP184	-31	PCF82	-33	U50	-26	OC45	-12
19BG6G	-80	DL35	-45	EP90	-35	PCF86	-48	U52	-31	OC71	-12
20P2	-67	DL92	-26	EL34	-46	PCF801	-28	U191	-59	OC75	-12
20P3	-77	DL94	-37	EL41	-54	PCF802	-40	U251	-62	OC81	-12
20P4	-92	DL96	-38	EL84	-23	PCF805	-61	U301	-38	OC82	-12
25L6GT	-19	DY86	-24	EL90	-26	PCF806	-56	U329	-66	OC82D	-12
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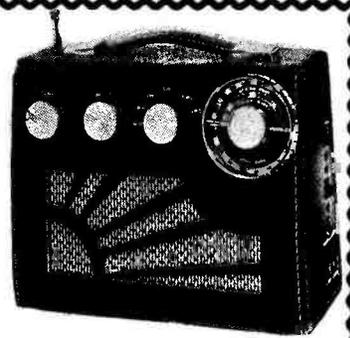
Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull output using 600mW Transistors. Car Aerial and Tape Record Sockets. Switched Earpiece Socket complete with Earpiece. 10 Transistors plus 3 Diodes. 8" x 2 1/2" Speaker. Air Spaced ganged Tuning Condenser with VHF section. Volume on/off, Wave Change and Tone Control. Attractive Case in black with silver blocking. Size 9" x 7" x 4". Easy to follow instructions and diagrams. Parts price list and easy build plans 30p (FREE with parts).

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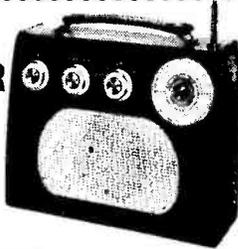
P. P. & Ins. 50p

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ROAMER EIGHT Mk I

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Total building cost **£6.98** P. P. & Ins. 41p.
(Overseas P. & P. £1)

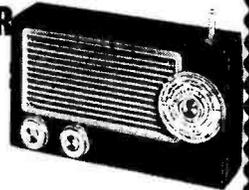
ROAMER SEVEN MK IV



7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for MW and LW. Retractable 4 section 24in. chrome plated telescopic aerial for SW. Socket for Car Aerial. Powerful push-pull output. 7 transistors and 2 diodes. Including Micro-Alloy R.F. Transistors. 8" x 2 1/2" speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning and wave change controls. Attractive case with carrying handle. Size 9" x 7" x 4 1/2". approx. Easy to follow instructions and diagrams. Parts price list and easy build plans 15p (FREE with parts). Earpiece with plug and switched socket for private listening, 30p extra.

Total building costs **£5.98** P. P. & Ins. 41p.
(Overseas P. & P. £1)

ROAMER SIX



6 Tunable Wavebands: MW, LW, SW1, SW2, Trawler band plus an extra M.W. band for easier tuning of Luxembourg etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker. 8 stages—6 transistors and 2 diodes including Micro-Alloy R.F. Transistors, etc. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9" x 5 1/2" x 2 1/2". approx. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£3.98** P. P. & Ins. 26p.
(Overseas P. & P. £1)

POCKET FIVE



3 Tunable Wavebands: MW, LW, Trawler Band with extended M.W. band for easier tuning of Luxembourg, etc. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil speaker. Attractive black and gold case. Size 6 1/2" x 1 1/2" x 3 1/2". Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2.23** P. P. & Ins. 21p.
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TRANSONA FIVE

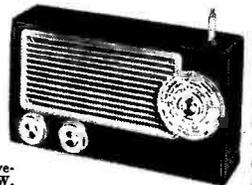


5 TRANSISTORS AND 2 DIODES

3 Tunable Wavebands: MW, LW and Trawler Band. 7 stages—5 transistors and 2 diodes, ferrite rod aerial, tuning condenser volume control, fine tone moving coil speaker. Attractive case with red speaker grille. Size 6 1/2" x 4 1/2" x 1 1/2". Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building costs **£2.50** P. P. & Ins. 22p.
(Overseas P. & P. 63p)

TRANS EIGHT



8 TRANSISTORS AND 3 DIODES

6 Tunable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9" x 6 1/2" x 2 1/2". approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 25p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

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Parts price list and plans for

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ARMSTRONG 521	59.00	42.95
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FERROGRAPH F307 Mk. II (cased)	64.00	46.95
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GOODMANS Maxamp	54.00	34.95
LEAK Delta 30 (cased)	65.00	48.50
LEAK Delta 70 (cased)	79.50	58.95
METRO SOUND ST20E	39.50	25.95
METRO SOUND ST60	70.00	48.95
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PHILIPS RH 590	52.00	37.95
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RANK Rotel 610	74.50	48.95
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ROGERS Ravensbourne (cased)	64.00	46.95
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SINCLAIR Project 60/2 x Z30/PZ5	23.90	15.95
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SINCLAIR PROJECT 605	29.95	21.95
SINCLAIR AFU	5.95	4.45
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TELETON 307	30.00	19.95
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*ARMSTRONG 524 FM	42.17	32.50
*ARMSTRONG M8 Decoder	9.50	7.50
*DULCI FMT.7 FM	25.10	17.95
DULCI FMT.75 Stereo	33.79	24.95
GOODMANS Stereomax	80.07	47.95
LEAK Delta F30	75.00	53.50
LEAK Delta AM/FM	89.50	68.95
PHILIPS RH 690	45.30	34.95
PHILIPS RH 691	85.80	69.95
PIONEER TX500 AM/FM	66.09	53.95
PIONEER TX900 AM/FM	147.15	116.00
RANK ROTEL 320	54.90	38.95
ROGERS Ravensbourne chassis	59.63	45.50
ROGERS Ravensbourne in teak case	64.45	48.95
ROGERS Ravensbrook chassis	43.37	34.95
ROGERS Ravensbrook (cased)	49.39	39.95
SINCLAIR 2000	45.00	32.95
SINCLAIR 3000	45.00	34.95
SINCLAIR Project 60 tuner (stereo)	25.00	19.25
TELETON GT 101	43.93	30.50

All above Tuners are complete with MPX Stereo Decoder except where starred.

TUNER/AMPLIFIERS

AKAI AA 8500	235.00	182.95
AKAI 6600	149.50	114.95
AKAI 6300	129.50	94.50
AKAI 6200	99.50	73.95
ARENA 2600	111.30	89.95
ARENA T9000	303.45	285.00
ARMSTRONG M8 Decoder	9.50	7.50
ARMSTRONG 525	92.77	69.95
ARMSTRONG 528	105.72	79.95
GOODMANS Module 80 35w. RMS	81.59	67.95
GOODMANS Module 80 Compact	165.00	129.00
GOODMANS Module 110 FM/MW/LW/SW 100w RMS	135.00	108.00
LEAK Delta 75	165.00	128.95
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PHILIPS RH 790	134.00	104.95
PIONEER SX770 AM/FM	139.23	109.95
PIONEER SX900 AM/FM	167.83	129.95
PIONEER 440	104.18	82.95
ROGERS Ravensbrook Chassis	99.39	81.95
ROGERS Ravensbrook (cased)	108.43	87.95
ROTEL RX190	69.90	53.50
TANDBERG 1171	110.00	82.50
TANDBERG TR200	99.00	82.95
TELETON F2000	51.50	28.50
TELETON 10A11 150w. RMS	160.00	94.00
TELETON TFS30	79.85	53.95
TELETON TFS50 LA MW/LW/FM	86.63	61.95
TELETON CR55	125.26	61.95
WHARFEDALE 100-1	139.00	92.95



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All the above Tuners and Tuner/Amplifiers take both ceramic and magnetic cartridges except Teleton F2000 which takes ceramic only. All include MPX Stereo Decoder with the exception of Armstrong where decoder is extra as listed.

CARTRIDGES

	Rec. Retail Price	Comet Price
AUDIO TECHNICA AT66	6.47	4.50
GOLDRING G850	6.27	3.95
GOLDRING G800	12.55	5.95
GOLDRING G800E	18.16	10.45
*GOLDRING G800 Super E	25.10	14.75
*GOLDRING CS90 Stereo	5.02	4.25
*GOLDRING CS91E	7.53	6.35
EMPIRE 1000ZE/X	60.34	46.95
EMPIRE 999VE/X	43.01	33.95
EMPIRE 999TE/X	25.09	19.95
EMPIRE 999SE/X	20.31	15.95
EMPIRE 999E/X	15.89	12.30
EMPIRE 999/X	12.55	8.85
EMPIRE 909E/X	12.36	9.60
EMPIRE 909/X	9.26	7.25
EMPIRE 909E/X	9.56	7.50
ORBIT Magnetic NM 22	Special Price	2.90
ORTOFON SL15E	28.62	22.95
ORTOFON S1 15K Transformer	7.00	4.95
ORTOFON M15E	29.08	23.50
SHURE M3DM	6.10	4.25
SHURE M31E	11.63	8.60
SHURE M32	10.73	8.00
SHURE M32-3	9.84	7.90
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SHURE M44-7	7.90	5.50
SHURE M-44C	7.90	5.50
SHURE M44E	8.60	5.95
SHURE M55E	9.70	6.75
SHURE M75G	14.70	9.95
SHURE M75-6	13.60	8.45
SHURE M75EJ	15.40	10.75
SHURE M75E	19.00	12.95
SHURE M75E/95G	20.80	14.95
SHURE V15-11	39.40	27.50

Starred cartridges above are ceramic. All others are magnetic.

PICKUP ARMS

GOLDRING Lenco 75	13.98	9.50
GOLDRING Lenco L69	10.04	6.50
SME 3009 with S2 Shell	33.26	24.90
SME 3012 with S2 Shell	35.42	26.45

TURNTABLES

The following Turntables are complete with base, plinth, perspex cover and cartridge. Fully wired and ready for use. All at special prices.

GARRARD SP25 Mk III with Goldring G.800	Special Price £18.90
GARRARD SP25 Mk III with Shure M.44/7	Special Price £20.95
GARRARD AP76 with Goldring G800	Special Price £29.90
GARRARD AP76 with Shure M55E	Special Price £33.95
GARRARD AP76 with Shure M75EJ	Special Price £35.95
GARRARD 2025 with Sonotone STAHC	Special Price £13.90
GOLDRING 705/P with G850	£26.00 £10.95
GOLDRING GL75 with G800	Special Price £40.95
THORENS 150 AB complete with TX11 cover Shure M55E cartridge	£64.83 £49.95

GARRARD SP25 Mk III	15.85	9.95
GARRARD SL65 B	20.48	13.40
GARRARD SL95 B	49.23	32.90
GARRARD AL71	39.26	27.40
GARRARD 502 B	31.83	23.90
GARRARD Zero 100	56.25	42.95
GARRARD Zero 100S	51.75	41.95

Rec. Retail Price Comet Price

GARRARD WB4 base Mk IIZ to fit Zero 100 & Zero 100S	6.40	4.95
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GARRARD AP76	27.85	18.85
GOLDRING GL69 Mk.II	27.60	18.95
GOLDRING GL69P Mk. II	36.21	26.95
GOLDRING GL75	40.15	28.95
GOLDRING GL75P	48.76	35.95
GOLDRING Covers for 69P and 72P Cover for 75P Deluxe	5.02	3.75
GOLDRING C99-plinth and cover for G99	11.05	9.75
GOLDRING G99	26.89	19.90
GOLDRING G101P	28.68	22.95
GOLDRING GL72 Chassis	28.68	22.95
GOLDRING GL72P	37.29	29.95
GOLDRING GL85	62.74	47.95
GOLDRING GL85P	72.78	55.95
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MCDONALD MP 60	15.20	10.95
MCDONALD 610	19.28	14.50
MCDONALD HT 70	21.22	15.45
MCDONALD HT70 inc. plinth & cov. Base and Cover for MP 60 and CELESTION Ditton 44	Special Price	4.25
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PHILIPS 308 transcription unit complete with base and cover	37.60	28.95
PIONEER PL12A with base & cover	48.34	36.25
THORENS TX25 cover	8.52	6.60
THORENS TD125	76.69	59.45
THORENS TD125AB	115.57	93.95
THORENS TD150 Mk. II	34.67	28.95
THORENS TD150A Mk. II	44.40	34.25
THORENS TD150AB Mk. II	48.05	38.95
THORENS TX11 Cover	4.26	3.75
WHARFEDALE Linter with base and cover and Shure M44/7 cartridge	35.00	27.95

SPEAKERS

ARENA HT 227 (pair)	42.00	26.95
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AKAI SD170	152.50	111.95
B & W DM3	63.00	47.95
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CELESTION Ditton 15	38.47	27.25
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GOODMANS Magister	62.50	39.50
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GOODMANS Mezzo 3	34.00	22.75
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GOODMANS Dimension 8	69.00	47.95
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KN600 3-speaker System (pair)	26.86	18.95
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KN1100 4-speaker System	20.40	14.95
KN2100 3-speaker System	25.20	18.95
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METRO SOUND 202	21.50	15.25
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METRO SOUND Duplex 25	52.00	36.95
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GOODMANS Axiom 401	17-86	12-25
GOODMANS Twin Axiom 10	9-86	7-25
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GOODMANS Audiom 10P	5-83	4-50
GOODMANS Audiom 12P	12-37	9-25
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GOODMANS Treble 100	9-60	6-25
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AKAI 4000D 4-track stereo deck	96-38	61-95
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AKAI X200D	162-52	103-00
AKAI 1800SD	130-71	105-00
AKAI 200SSD	297-50	229-00
AKAI GXC 40D Cassette Tape Deck	94-95	68-95
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BUSH D1 cassette DC70	21-19	16-95
BUSH TP60 Cassette tape recorder	28-38	23-95
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FERROGRAPH 702 2-track tape deck	220-22	175-00
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FERROGRAPH 722	256-52	195-00
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TELETON STP 801 Stereo 8 track tape Audio system complete with speakers	54-75	47-00
GARRARD AP76 with base cover and Shure M55E cartridge Arena 2600 AM/FM and SW Tuner/ Amp and 2 Goodmans Mezzo III speakers	229-43	148-00
GOLDRING GL75 complete with base and cover, G800 Cartridge, Wharfedale 100-1 Tuner/Amp and 2 Wharfedale Dovedale III speakers	294-79	189-00
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METROSOUND 448 8-track stereo play-back unit complete with 2 HFS 103 Speakers	83-56	70-95
LINTON System with Wharfedale Linton Amplifier, Linton Turntable with Shure M47 Cartridge and pair of Linton Mk II Speakers	144-90	107-95
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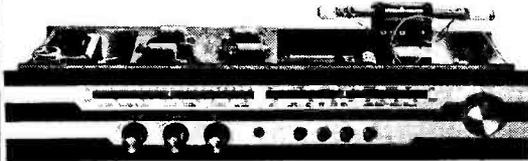
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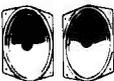
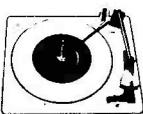


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PIV	300mA	750mA	1A	1.5A	3A	10A	30A
\$p	\$p	\$p	\$p	\$p	\$p	\$p	\$p
50	0.40	0.05	0.05	0.07	0.14	0.21	0.47
100	0.04	0.06	0.05	0.13	0.18	0.23	0.75
200	0.05	0.09	0.06	0.14	0.20	0.24	1.00
400	0.08	0.13	0.07	0.20	0.27	0.37	1.25
600	0.07	0.16	0.10	0.23	0.34	0.45	1.55
800	0.10	0.17	0.13	0.25	0.37	0.55	2.00
1000	0.11	0.25	0.15	0.30	0.44	0.63	2.50
1200	—	0.33	—	0.33	0.57	0.75	—

TRIACS

VBOM	2A	6A	10A
TO-1	TO-66	TO-88	
\$p	\$p	\$p	
100	30	50	75
200	50	60	90
400	70	75	1-10

LUCAS SILICON RECTIFIERS
35 amp, 400 p.p.s. stud type. \$1.10p each.

DIACS
FOR USE WITH TRIACS
BR100 (D32) 37p each

2A POTTED BRIDGE RECTIFIERS 200V 50p

UNIJUNCTION
UT46. Eqv. 2N2646, Eqv. T1843. BSN3000 27p each, 25-99 25p 100UP 20p.

NPN SILICON PLANAR
BC107/8/8, 10p each; 50-99 8p; 100 up, 8p each; 1,000 off, 7p each. Fully tested and coded TO-18 case.

FREE
One 50p Pak of your own choice free with orders valued \$4 or over.

AF239 PNP GERM. SIMEN'S VHF TRANSISTORS. RF MIXER & OSC. UP TO 900 MHZ. USE AS REPLACEMENT FOR AF139-AF186 & 100' OF OTHER USES IN VHF. OUR SPECIAL LOW PRICE—1.24 27p each, 25-99 34p each 100+ 30p each.

SPECIAL OFFER
2N2926 (Y) (O) 10 for 50p, 25 for \$1 20,000 TO CLEAR.

CADMIUM CELLS
ORP12 43p
ORP60, ORP61 40p each

PHOTO TRANS.
OCP71 Type. 43p

SIL. G.P. DIODES \$p
300mV 30. 0.60
40pIV(Min.) 100. 1.50
Sub-Min. 500 5.00
Full Tested, 1,000 9.00
Ideal for Organ Builders.

D13D1 Silicon Unilateral
switch 50p each.

A Silicon Planar, monolithic integrated circuit having the most electrical characteristics, but with an anode gate and a built-in "Zener" diode between gate and cathode. Full data and application circuits available on request.

JUMBO COMPONENT PAKS
MIXED ELECTRONIC COMPONENTS
Exceptionally good value

Resistors, capacitors, pots, electrolytics and coils plus many other useful items. Approximately 3lbs in weight. Price incl. P. & F. \$1.50 only
Plus your satisfaction or money back guarantee.

FULL RANGE OF ZENER DIODES
VOLTAGE RANGE 2-33V. 400mV (DO-7 Case) 18p ea. 14W (Top-Hat) 18p ea. 10W (80-10 Stud) 25p ea. All fully tested, 95% tol. and marked. State voltage required.

BRAND NEW TEXAS GERM. TRANSISTORS
Code and Guaranteed Pak No. QVOT
T1 8 2G3713 OC71
T2 8 D1374 OC75
T3 8 D1218 OC81D
T4 8 2G381T OC81
T5 8 2G392T OC82
T6 8 2G344B OC84
T7 8 2G345B OC45
T8 8 2G378 OC78
T9 8 2G398A 2N1307
T10 8 2G417 AF117
All 50p each pak.

2N8060 NPN SIL. DUAL TRANS. CODE D1699 TEXAS. Our price 25p each.
120V VCB MIXIE DRIVER TRANSISTOR. Sim. BSX21 & C407, 2N1893 FULLY TESTED AND CODED ND 120. 1-24 17p each. TO-5 N.P.N. 25 up 15p each.

Sil. trans. suitable for P.E. Organ. Metal TO-18 Eqv. ZTX300 5p each. Any Qty.

EX-EQUIPMENT MULLARD
AF117 transistors. Large can 4 leads type. Leads cut short but still usable, real value at 15 for 50p.

KING OF THE PAKS Unequaled Value and Quality
SUPER PAKS NEW BI-PAK UNTESTED SEMICONDUCTORS

Satisfaction GUARANTEED in Every Pak, or money back.

Pak No.	\$p
U1 120 Glass sub-min. general purpose germanium diodes	0.50
U2 60 Mixed germanium transistors AF/RF	0.50
U3 75 Germanium gold bonded diodes sim. OA5, OA47	0.50
U4 40 Germanium transistors like OC81, AC128	0.50
U5 60 200mA sub-min. Sil. diodes	0.50
U6 30 Silicon planar transistors NPN sim. BSY95A, 2N706	0.50
U7 16 Silicon rectifiers Top-Hat 750mA up to 1,000V	0.50
U8 60 Sil. planar diodes 250mA, OA/200/202	0.50
U9 20 Mixed volts 1 watt Zener diodes	0.50
U11 30 PNP silicon planar transistors TO-5 sim. 2N1132	0.50
U13 25 PNP-NPN sil. transistors OC290 & 28104	0.50
U14 150 Mixed silicon and germanium diodes	0.50
U15 25 NPN Silicon planar transistors TO-5 sim. 2N697	0.50
U16 10 3-Amp silicon rectifiers stud type up to 1000 PIV	0.50
U17 30 Germanium PNP AF transistors TO-5 like ACY 17-22	0.50
U18 8 6-Amp silicon rectifiers BZY133 type up to 600 PIV	0.50
U19 25 Silicon NPN transistors like BC105	0.50
U20 12 1.5 Amp silicon rectifiers Top-Hat up to 1,000 PIV	0.50
U21 30 A.F. germanium alloy transistors 2G300 series & OC71	0.50
U23 30 Mad'l's like MAT series PNP transistors	0.50
U24 20 Germanium 1-Amp rectifiers GJM up to 300 PIV	0.50
U25 25 300 Mc/s NPN silicon transistors 2N706, BSY37	0.50
U26 30 Fast switching silicon diodes like IN914 micro-min	0.50
U29 10 1-Amp SCR's TO-5 can up to 600 PIV CR81/25-600	1.00
U31 20 Sil. Planar NPN trans. low noise amp 3N3707	0.50
U32 25 Zener diodes 400mV DO7 case mixed volts, 3-18	0.50
U33 15 Plastic case 1 amp silicon rectifiers IN4000 series	0.50
U34 30 Sil. PNP alloy trans. TO-5 BCY26, 2B302/4	0.50
U35 25 Sil. planar trans. PNP TO-18 2N2906	0.50
U36 25 Sil. planar PNP trans. TO-5 BF750/51/52	0.50
U37 30 Sil. alloy trans. SO-2 PNP. OC200 28322	0.50
U38 20 Fast switching sil. trans. NPN. 400Mc/s 2N3011	0.50
U39 30 RF germ. PNP trans. 2N1303 5 TO-5	0.50
U40 10 Dual trans. 6 lead TO-5 2N2660	0.50
U41 25 RF germ. trans. TO-1 OC45 NKT72	0.50
U42 10 VHF germ. PNP trans. TO-1 NKT497, AF117	0.50
U43 25 Sil. trans. plastic TO-18 A.F. BC113/114	0.50
U44 20 Sil. trans. plastic TO-5 BC115/116	0.50
U45 7 3A SCR's TO-66 up to 600 PIV.	1.00

Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked.

NEW QUALITY TESTED PAKS

Pak Description	Price
Q1 20 Red apt. trans. PNP AF	0.50
Q2 16 White spot R.F. trans. PNP	0.50
Q3 4 OC77 type trans.	0.50
Q4 6 Matched trans. OC44/46/81/81D	0.50
Q5 4 OC75 transistors	0.50
Q6 4 OC72 transistors	0.50
Q7 4 AC128 trans. PNP high gain	0.50
Q8 4 AC126 trans. PNP	0.50
Q9 7 OC81 type trans.	0.50
Q10 7 OC7 type trans.	0.50
Q11 2 AC127/128 comp. pairs PNP/NPN	0.50
Q12 3 AF116 type trans.	0.50
Q13 2 AF117 type trans.	0.50
Q14 3 AC127 H.F. type trans.	0.50
Q15 5 2N2926 sil. epoxy trans.	0.50
Q16 2 6FT780 low noise germ. trans.	0.50
Q17 3 NPN 18T141 & 28T140	0.50
Q18 3 Mat'l's MAT 100 & MAT 120	0.50
Q19 3 Mat'l's MAT 101 & MAT 121	0.50
Q20 4 OC44 germ. trans. A.F.	0.50
Q21 3 AC127 NPN germ. trans.	0.50
Q22 20 NKT trans. A.F. R.F. coded	0.50
Q23 10 OA202 sil. diodes sub-min.	0.50
Q24 8 OA91 diodes	0.50
Q25 4 IN914 sil. diodes 75PIV 75mA	0.50
Q26 8 OA95 germ. diodes sub-min. IN69	0.50
Q27 2 10A 600PIV sil. rect. 1848F	0.50
Q28 2 Sil. power rect. BZY133	0.50
Q29 4 Sil. trans. 2 x 2N696, 1 x 2N697, 1 x 2N498	0.50
Q30 7 81W switch trans. 2N706 PNP	0.50
Q31 6 Sil. switch trans. 2N708 NPN	0.50
Q32 3 PNP sil. trans. 2 x 2N1131, 1 x 2N1132	0.50
Q33 3 Sil. NPN trans. 2N1711	0.50
Q34 7 Sil. PNP trans. 2N2369, 500MHZ	0.50
Q35 3 Sil. PNP TO-5 2 x 2N3904 & 1 x 2N905	0.50
Q36 7 2N3940 TO-18 plastic 300MHZ NPN	0.50
Q37 5 2N3053 NPN sil. trans	0.50
Q38 5 PNP trans. 4 x 2N3703, 3 x 2N3702	0.50
Q39 7 NPN trans. 4 x 2N3704, 3 x 2N3705	0.50
Q40 7 NPN amp. 4 x 2N3707, 3 x 2N3709	0.50
Q41 3 Plastic NPN TO-18 2N3904	0.50
Q42 6 NPN trans. 2N5172	0.50
Q43 7 BC107 NPN trans.	0.50
Q44 7 NPN trans. 4 x BC108, 3 x BC109	0.50
Q45 3 BC113 NPN TO-18 trans	0.50
Q46 3 RG115 NPN TO-3 trans.	0.50
Q47 6 NPN high gain 3 x BC167, 3 x BC168	0.50
Q48 4 BCY70 NPN trans. TO-18	0.50
Q49 4 NPN trans. 2 x BF751, 2 x BF752	0.50
Q50 7 BSY28 NPN switch TO-18	0.50
Q51 7 BS705A NPN trans. 300MHZ	0.50
Q52 8 BY104 sil. rect.	1.00
Q53 25 Sil. & germ. trans. mixed all marked new	1.50

PRINTED CIRCUITS—EX-COMPUTER

Packed with semiconductors and components. 10 boards give a guaranteed 30 trans and 20 diodes. Our price 10 boards, 50p 10p P. & F. 100 Boards \$3, P. & F. 30p.

NEW EDITION 1971 TRANSISTOR EQUIVALENTS BOOK. A complete cross reference and equivalents book for European, American and Japanese Transistors. Exclusive to BI-PAK 90p each.

F.E.T.'S

2N3819	35p
2N3820	50p
2N3821	35p
2N3823	30p
2N3845	50p
2N3849	40p
BFW 10	40p
MPP105	40p

PHOTO TRANS.
OCP71 Type. 43p

SILICON PHOTO TRANSISTOR. TO-18 Lens and 3 NPN Sim. to BP 235 and P21. BRAND NEW. Full data available. Fully guaranteed. Qty. 1-24 25-99 100p Price each 45p 40p 35p

Dual-in-Line Low Profile Sockets
14 and 16 Lead Sockets for use with Dual-in-Line Integrated Circuits

Price each
Order No. 1-24 25-99 100 up
T80 14 pin type 30p 27p 25p
T80 16 pin type 35p 32p 30p

POWER TRANSISTOR BONANZA!

GENERAL PURPOSE GERM. PNP
Coded GP100. BRAND NEW TO-3 CASE. POSS. REPLACE.—OC25-28-29-30-35-36. NKT 401-403-404-405-406-430-451-452-453. T13027-3028, 2N2650A, 2N456A-457A-458A, 2N511 A & B. 2G220-222, ETC. VCEO 80V VCEO 50V IC 10A PT. 30 WATTS Hfe 30-170.
PRICE 1-24 25-99 100 up
43p each 40p each 36p each

SILICON High Voltage 250V NPN
TO-3 case. G.P. Switching & Amplifier Applications. Brand new Coded B 2400 VCEO 250V VCEO 100V IC 6A/30 Watts. HFE type 20/1T 5MHZ.
OUR PRICE EACH :
1-24 25-99 100 up
50p 45p 40p

EX-STOCK TYPE EACH AS PRICED
OC20 50p OC28 40p AD149 43p BD131 70p BD139 75p
OC22 30p OC29 40p AL102 85p BD132 80p BD140 85p
OC23 35p OC35 33p AL103 85p BD135 70p BD155 75p
OC24 45p OC36 40p BD121 60p BD136 80p BU105 1.23
OC25 25p AD140 40p BD123 75p BD137 70p 2N3064 45p
OC26 25p AD142 40p BD124 70p BD138 80p

AD161 NPN
AD162 PNP
M/P COMP GERM. TRANS. OUR LOWEST PRICE OF 63p PER PAIR

2N3055
115 WATT SIL. POWER NPN 83p EACH

SILICON 50 WATTS MATCHED HF/PNP
BIP 19 NPN TO-3 Plastic.
BIP 20 PNP. Brand new.
VCEO 100V VCEO 50V IC 10A. HFE type 100/1T 3MHZ.
OUR PRICE PER PAIR :
1-24 25-99 100 prs. prs. prs.
80p 55p 50p

GENERAL PURPOSE NPN SILICON SWITCHING TRANS. TO-18 SIM. TO 2N706/8, BSY27/28/95A. All usable devices no open or short circuits. ALSO AVAILABLE IN PNP Sim. to 2N2906, BCY70. When ordering please state preference NPN or PNP.

20	For	25p	100	For	1.75
50	For	1.00	500	For	7.50
			1000	For	13.00

OUR STOCKS of individual devices are now too numerous to mention in this advertisement. Send S.A.E. for our listing of over 1,000 Semiconductors. All available Ex-Stock at very competitive prices.

RTL MICROLOGIC CIRCUITS
Price each
Epoxy TO-5 case 1-24 25-99 100 up
uL900 Buffer 35p 33p 27p
uL914 Dual 2i/p gate 35p 33p 27p
uL923 J-K flip-flop 50p 47p 45p
Date and Circuits Booklet for IC's Price 7p.

-the lowest prices!

74 Series T.T.L. I.C.'S DOWN AGAIN IN PRICE



Check our 74 Series List before you buy any I.C.'s. Our prices are the lowest possible. All devices ex-stock. Full spec. guaranteed

BI-PAK Order No.			Price and qty. prices 1-24 25-99 100 up			BI-PAK Order No.			Price and qty. prices 1-24 25-99 100 up			
	2p	3p	2p	3p	4p		2p	3p	4p	2p	3p	4p
BP00=8N7400	0.15	0.14	0.12	BP86=8N7486	0.82	0.80	0.88					
BP01=8N7401	0.15	0.14	0.12	BP90=8N7490	0.87	0.84	0.88					
BP02=8N7402	0.15	0.14	0.12	BP91=8N7491AN	0.87	0.84	0.78					
BP03=8N7403	0.15	0.14	0.12	BP92=8N7492	0.87	0.84	0.88					
BP04=8N7404	0.15	0.14	0.12	BP93=8N7493	0.87	0.84	0.88					
BP05=8N7405	0.15	0.14	0.12	BP94=8N7494	0.77	0.74	0.88					
BP07=8N7407	0.18	0.17	0.16	BP95=8N7495	0.77	0.74	0.88					
BP08=8N7408	0.18	0.17	0.16	BP96=8N7496	0.77	0.74	0.88					
BP09=8N7409	0.18	0.17	0.16	BP100=8N74100	1.75	1.65	1.55					
BP10=8N7410	0.15	0.14	0.12	BP104=8N74104	0.97	0.94	0.88					
BP13=8N7413	0.29	0.26	0.24	BP105=8N74105	0.97	0.94	0.88					
BP16=8N7416	0.43	0.40	0.38	BP107=8N74107	0.40	0.38	0.88					
BP17=8N7417	0.43	0.40	0.38	BP110=8N74110	0.55	0.53	0.60					
BP20=8N7420	0.15	0.14	0.12	BP111=8N74111	1.25	1.15	1.00					
BP30=8N7430	0.15	0.14	0.12	BP119=8N74119	1.00	0.95	0.90					
BP40=8N7440	0.15	0.14	0.12	BP119=8N74119	1.25	1.25	1.10					
BP41=8N7441	0.67	0.64	0.68	BP121=8N74121	0.67	0.64	0.68					
BP42=8N7442	0.67	0.64	0.68	BP141=8N74141	0.67	0.64	0.68					
BP43=8N7443	1.95	1.85	1.75	BP145=8N74145	1.50	1.40	1.30					
BP44=8N7444	1.95	1.85	1.75	BP150=8N74150	1.80	1.70	1.60					
BP45=8N7445	1.95	1.85	1.75	BP151=8N74151	1.00	0.95	0.90					
BP46=8N7446	0.97	0.94	0.88	BP153=8N74153	1.20	1.10	0.95					
BP47=8N7447	0.97	0.94	0.88	BP154=8N74154	1.80	1.70	1.60					
BP48=8N7448	0.97	0.94	0.88	BP155=8N74155	1.40	1.30	1.20					
BP60=8N7460	0.15	0.14	0.12	BP156=8N74156	1.40	1.30	1.20					
BP70=8N7470	0.29	0.26	0.24	BP157=8N74157	1.80	1.70	1.60					
BP72=8N7472	0.29	0.26	0.24	BP181=8N74181	1.80	1.70	1.60					
BP73=8N7473	0.37	0.35	0.32	BP164=8N74164	2.00	1.90	1.80					
BP74=8N7474	0.37	0.35	0.32	BP165=8N74165	2.00	1.90	1.80					
BP75=8N7475	0.47	0.45	0.42	BP181=8N74181	2.75	2.60	2.40					
BP76=8N7476	0.43	0.40	0.38	BP182=8N74182	0.97	0.94	0.88					
BP80=8N7480	0.67	0.64	0.68	BP190=8N74190	3.50	3.35	3.00					
BP81=8N7481	0.97	0.94	0.88	BP191=8N74191	3.50	3.35	3.00					
BP82=8N7482	0.97	0.94	0.88	BP192=8N74192	2.10	1.95	1.75					
BP83=8N7483	1.10	1.05	0.95	BP193=8N74193	2.10	1.95	1.75					
				BP196=8N74196	1.10	1.05	0.95					
				BP197=8N74197	1.80	1.70	1.60					
				BP198=8N74198	5.50	5.00	4.00					
				BP199=8N74199	5.50	5.00	4.00					

PRICE-MIX. Devices may be mixed to qualify for quantity prices. PRICES for quantities in excess of 500 pieces mixed, on application. Owing to the ever increasing range of TTL 74 Series, please check with us for supplies of any devices not listed above, as it is probably now in stock. WARE 3442.

NUMERICAL INDICATOR TUBE Type GRI 16

Cold Cathode gas-filled side-viewing numerals (0-9) and Decimal Point.

COLOUR: Neon Red.

DATA: Anode supply voltage 175 min Vdc.
Cathode current: 14mA dc. Nom

Ideal for use in constructing Digital Clocks, Desk Calculators etc., and many products described in this magazine. We recommend use of BP41 or BP141 to drive this tube.

Full data available on request.

PRICE 1-5 £1.55. 6-25 £1.40

ACTUAL
SIZE



BRAND NEW LINEAR I.C.'s—FULL SPEC.

Type No.	Case	Leads	Description	1-24	25-99	100 up
BP 201C—8L201C	TO-5	8	G.P. Amp	63p	53p	45p
BP 701C—8L701C	TO-5	8	OP Amp	63p	53p	45p
BP 702C—8L702C	TO-5	8	OP Amp Direct OP	63p	53p	45p
BP 702—72702	D.I.L.	14	G.P. OP Amp Wide Band)	53p	45p	40p
BP 709—72709	D.I.L.	14	High OP Amp	53p	45p	40p
BP 709P—8A709C	TO-5	8	High Gain OP Amp	53p	45p	40p
BP 710—73710	D.I.L.	14	Differential comparator	53p	45p	40p
BP 711—8A711	TO-5	10	Dual comparator	53p	45p	45p
BP 741—72741	D.I.L.	14	High Gain OP Amp (Protected)	75p	65p	50p
8A 709C—8A709C	TO-5	6	R.F.—I.F. Amp	43p	35p	27p
TAA 263—	TO-72	4	A.F. Amp	70p	60p	55p
TAA 293—	TO-74	10	G.P. Amp	90p	75p	70p
TAA 350	TO5	8	Wide band limiting amplifier	170p	155p	150p

STOP PRESS! NOW OPEN

BI-PAKS NEW COMPONENT SHOP

A wide range of all types of electronic components and equipment available at competitive prices.

18, BALDOCK ST. (A10), WARE, HERTS. Tel.: 61593
OPEN 9.15-6 TUES. to SATS. FRIDAYS UNTIL 8 p.m.

ANOTHER BI-PAK FIRST!

THE NEW S.G.S. EA 1000 AUDIO AMPLIFIER MODULE *GUARANTEED NOT LESS THAN 3 WATTS RMS



Especially designed by S.G.S. incorporating their proven Linear I.C. Audio Amp. TA(821) providing unlimited applications for the enthusiast in the construction of radios, record players, Audio and Stereo units. Also ideal for intercom systems, monitoring applications and phone answering machines.

OTHER USES: portable applications where supply rails as low as 9V are of prime importance.

- Sensitivity 40 mV for 1 watt. VOLTAGE GAIN 40dB but can be varied up to 78dB for some applications.
- Signal to Noise Ratio 86dB.
- Frequency response better than 50 Hz to 25 KHz for -3dB.
- Normal supply Voltage 9-24V.
- Suitable for 8-16 OHM Loads.
- Overall Size 2" x 3" x 1".
- Typical Total Harmonic distortion at 1 watt less than 1%.
- Supply voltage (V_s) = 24V 15ohm load. Module Tested and Guaranteed.

Quantity 1-9 10-25
Price each £2.63 £2.58
Larger quantities quoted on request.

Full hook-up diagrams and complete technical data supplied free with each module or available separately at 10p each.

NOTE THESE PRICES!

I.C.'s	DTL 930 SERIES	LOGIC	Price		
			1-24	25-99	100 up
BP930	Expandable dual 4-input NAND	...	18p	11p	10p
BP932	Expandable dual 4-input NAND buffer	...	18p	12p	11p
BP933	Dual 4-input expande	...	18p	12p	11p
BP938	Expandable Hex Inverter	...	18p	12p	11p
BP938	Hex Inverter	...	18p	12p	11p
BP944	Dual 4-input NAND expandable buffer without pull-up	...	18p	12p	11p
BP946	Master-slave JK or RS	...	25p	24p	22p
BP948	Quad, 2 input NAND	...	12p	11p	10p
BP951	Master-slave JK or RS	...	25p	24p	22p
BP951	Monostable	...	65p	60p	55p
BP982	Triple 3 input NAND	...	12p	11p	10p
BP9083	Dual Master-slave JK with separate clock	...	40p	38p	36p
BP9084	Dual Master-slave JK with separate clock	...	40p	38p	36p
BP9097	Dual Master-slave JK with Common Clock	...	40p	38p	36p
BP9099	Dual Master-slave JK Common Clock	...	40p	38p	36p

Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only).

DTL & TTL INTEGRATED CIRCUITS

Manufacturers' "Fall outs"—out of spec. devices including functional units and part function but classed as out of spec. from the manufacturers' very rigid specifications. Ideal for learning about I.C.'s and experimental work.

Pak No.	Function	Price	
UIC830 = 12 x μA 930	.. 50p	UIC948 = 8 x μA 948 .. 50p	
UIC832 = 12 x μA 932	.. 50p	UIC851 = 5 x μA 951 .. 50p	
UIC833 = 12 x μA 933	.. 50p	UIC961 = 12 x μA 961 .. 50p	
UIC935 = 12 x μA 935	.. 50p	UIC9083 = 5 x μA 9083 .. 50p	
UIC936 = 12 x μA 936	.. 50p	UIC9094 = 5 x μA 9094 .. 50p	
UIC944 = 12 x μA 944	.. 50p	UIC9097 = 5 x μA 9097 .. 50p	
UIC945 = 8 x μA 945	.. 50p	UIC9099 = 5 x μA 9099 .. 50p	
UIC946 = 12 x μA 946	.. 50p	UICX 9 25 Assorted 930 Series	£1.50

Packs cannot be split but 25 Assorted Pieces (our mix) is available as Pack UICX9 Data Booklet available for the BP930 Series. PRICE 13p

UIC00 = 12 x 7400N	50p	UIC46 = 5 x 7446N	50p	UIC81 = 5 x 7481N	50p
UIC01 = 12 x 7401N	50p	UIC47 = 5 x 7447N	50p	UIC82 = 5 x 7482N	50p
UIC02 = 12 x 7402N	50p	UIC48 = 5 x 7448N	50p	UIC83 = 5 x 7483N	50p
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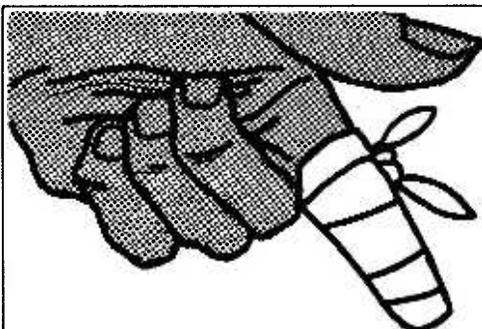
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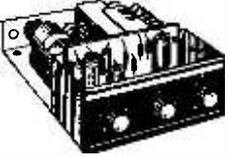


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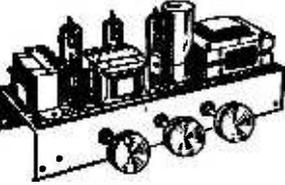
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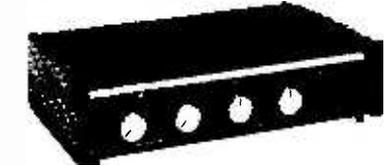
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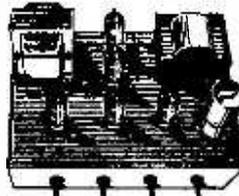
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Code	Power	Tolerance	Range in ohms	Values 1 to 9	10 to 99	100 up
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C	1/8W	5%	4.7-470K	E24	1	0-8
C	1/4W	10%	4.7-10M	E12	1	0-8
C	1/2W	5%	4.7-10M	E24	1-2	1
C	1W	5%	4.7-10M	E12	2-5	2
MO	1/2W	2%	10-1M	E24	4	3-5
WW	1W	10% ±1/20Ω	0-22-3-9	E12	7	7
WW	3W	5%	12-10K	E12	7	7
WW	7W	5%	12-10K	E12	9	9

Codes: C—carbon film high stability low noise
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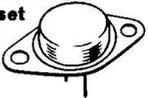
1N914	5p	AC142H	25p	BD131	75p
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1N1763A	24p	AC153K	29p	BD135	38p
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1N5399	21p	AC176K	17p	BDY20	92p
1N5402	28p	AC187K	17p	BF115	23p
1844	9p	ACT17	31p	BF167	18p
18940	5p	ACT18	15p	BF173	19p
2N3686	17p	ACT19	23p	BF177	25p
2N697	18p	ACT20	20p	BF194	14p
2N706	12p	ACT21	21p	BF195	15p
2N930	23p	ACT22	21p	BF254	14p
2N1132	29p	ACT39	63p	BF255	15p
2N1802	19p	ACT40	17p	BFX29	81p
2N1308	15p	ACT41	18p	BFX34	25p
2N1304	25p	ACT44	31p	BFX35	32p
2N1305	26p	AD142	50p	BFX37	29p
2N1306	33p	AD149	56p	BFX38	26p
2N1307	33p	AD150	50p	BFY50	25p
2N1309	36p	AD161/AD162	60p	BFY51	20p
2N1613	23p	matched pair	60p	BFY52	23p
2N1803	25p	AF114	22p	BFY50	18p
2N1893	54p	AF115	24p	BY164	45p
2N2147	95p	AF116	22p	BY238	18p
2N2218	34p	AF117	22p	BYX38-300	88p
2N2218A	44p	AF118	82p	BYX38-300R	38p
2N2219	38p	AF124	24p	C407	17p
2N2308	62p	AF126	24p	C702	23p
2N2360A	19p	AF126	22p	CA403	10p
2N2483	35p	AF127	22p	BE383	10p
2N2484	42p	AF139	33p	EC401	18p
2N2486	47p	AP239	37p	EC402	17p
2N2904	38p	APY26	27p	NKT211	26p
2N2905	44p	ARX27	36p	NKT212	20p
2N2906A	47p	ARX28	27p	NKT213	23p
2N2924	29p	ARX29	36p	NKT214	23p
2N2925	22p	AU111	97p	NKT217	50p
2N2926	11p	B30C260	24p	NKT261	21p
2N3053	27p	B1912	62p	NKT271	18p
2N3054	60p	B5041	79p	NKT274	18p
2N3702	13p	BA102	35p	NKT283	60p
2N3703	13p	BA130	22p	NKT284	79p
2N3704	13p	BA145	27p	NKT615F	80p
2N3705	13p	BA156	18p	NKT674F	24p
2N3706	13p	BB103/B	16p	OA47	8p
2N3708	10p	BB103/G	16p	OA90	6p
2N3709	11p	BC106	11p	CA91	6p
2N3710	13p	BC109	12p	OA95	6p
2N3711	13p	BC123	21p	OA200	9p
2N3794	15p	BC125	15p	OA202	10p
2N3819	23p	BC126	22p	OC19	50p
2N3820	53p	BC140	30p	OC25	42p
2N3864	33p	BC147	47p	OC29	23p
2N3906	35p	BC148	9p	OC35	60p
2N4036	55p	BC149	10p	OC36	65p
2N4058	13p	BC183	19p	OC41	42p
2N4059	10p	BC189	11p	OC44	49p
2N4060	11p	BC177	14p	OC70	23p
2N4081	11p	BC178	18p	OC71	38p
2N4124	18p	BC179	14p	OC75	40p
2N4126	27p	BC182L	11p	OC81	26p
2N4284	24p	BC183L	10p	OC81D	26p
2N4286	16p	BC184L	11p	OC83	25p
2N4289	15p	BC186	42p	OC84	25p
2N4291	15p	BC192L	16p	PS45A	26p
2N4410	24p	BC213L	16p	82CN1	10p
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2N5082	61p	BC287	9p	8D4	12p
2N5487	49p	BC269	9p	V763	28p
2N5489	49p	BC297	17p	W106B1	40p
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40251	89p	BC299	17p	WF09	95p
40361	59p	BC300	49p	ZTX300	14p
40382	68p	BC301	37p	ZTX301	16p
40602	52p	BC303	60p	ZTX302	22p
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OUTPUT: 15 watts R.M.S. (Continuous) into 8 ohms. 10 watts R.M.S. (Continuous) into 15 ohms. -2dB. 5dB Full Vol. HARMONIC DISTORTION FREQUENCY RESPONSE: -3dB 7Hz to 70kHz 0.1% at 1000 Hz 10 Watts TREBLE CONTROL: +18dB to -12dB at 14kHz BASS CONTROL: +7dB to -16dB at 40Hz CROSS TALK -58dB SENSITIVITIES: Disc Mag 2.5-50. Ceramic 35mV. Radio 120mV. Tape 120mV. REAR PANEL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio. (3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker connections.



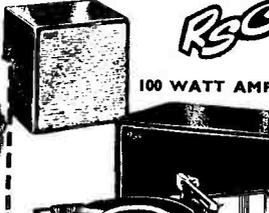
50 WATT SPEAKER

RSC DISCOTHEQUE EQUIPMENT

50 WATT SPEAKER



FAL
F.G.1/2A DISCO CONSOLE



100 WATT AMPLIFIER

SAVINGS ON PACKAGE OFFER

All units available separately

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- (2) 100W Power Amplifier
- (3) Pair High Quality Headphones
- (4) Matching Microphone fitted to Headphones
- (5) Pair 50W Speakers black rexine covered size approx. 18" x 18" x 8"

Incorporating twin Garrard SP85 Mk.III turntables and Sonotone STAEC Ceramic Cartridges with Diamond styl. Separate Vol. controls for each turntable. Also MONTONOR FACILITIES, plus Treble and Bass Controls. Separate input for 'mlks' with vol. control switch. Black Rexine covered Cabinet with lid. **£69**

Carr. 12.25
Shipping straps £1-85 extra

Terms: Deposit £15 and 9 monthly payments of £8.75 (Total £77.75)



TWIN TURNTABLE WITH PRE-AMP

HEADPHONES MICROPHONE

SEND S.A.E. FOR DISCO LEAFLET

£139-75

TOTAL COST OF ALL ILLUSTRATED UNITS Carr. £2-50

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R.S.C. COLUMN SPEAKERS IDEAL FOR VOCALISTS AND PUBLIC ADDRESS

All types 16 Ohms covered in Rexine and Vynal

TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

<p>TYPE C485 25-30 WATTS</p> <p>Fitted four 8" high flux 8 watt speakers Overall size approx. 48x10x5in. Terms: Dep. £3 and 9 monthly payments £2 (Total £31)</p> <p>Carr. 50p.</p>	<p>TYPE C4125 50 WATTS</p> <p>Fitted four 12" 11,000 line 16 watt speakers Overall size approx. 56x14x5in. Terms: Dep. £4 and 9 monthly payments £31</p> <p>Carr. 75p</p>
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TYPE C4100 100 WATTS Inc. four 12" 50 watt speakers for conservative rating. Extra heavy construction. Size approx. 58 x 16 x 10" (excluding top). Filled and pressurised. Terms: Dep. £11 and 9 monthly. **£65** (Total £77.75). Carr. £1

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Highly sensitive. Push-Pull high output. Hum level -70db. Response ±3dB 30-20,000 c/s. All high grade components. Valves EF86, EF88, ECC83, 90T, 6Z24. Separate Bass and Treble Controls. Sensitivity 36 millivolts. For High Impedance microphones. For Clubs, Schools, Theatres, Dance Halls, Outdoor Functions, etc. For Electronic Organ, Guitar, String Bass, etc. Gram, Radio or Tape. Two separate inputs with vol. controls permit such as "mlks" and Pick-up etc. to be used for mixing purposes. 200-250V. 50 c/s A.C. mains. For 3 and 15 ohm speakers. **£15-75**

Complete kit of parts with wiring diagram and instructions. Twin-handled perforated cover. **£19-75** Carr. 65p

TERMS: Deposit £4 and 9 monthly payments of £2-10 (Total £22-90). Send S.A.E. for leaflet.

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Primaries 200-250V. 50c/s. Screened

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- R.S.C. Branches listed below open all day Sat.
- BRADFORD** 10 North Parade (Half-day Wed.). Tel. 25349
 - BLACKPOOL** (Agents) O & C Electronics, 227 Church Street
 - BIRMINGHAM** 30/31 Great Western Arcade, Tel. 021-236 1279 (Half-day Wed)
 - DERBY** 26 Osmaston Rd. The Spot (Half-day Wed). Tel. 41361
 - DARLINGTON** 18 Priestgate (Half-day Wed.). Tel. 68043
 - EDINBURGH** 101 Lothian Rd. (Half-day Wed.).
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 - LIVERPOOL** 73 Dale Street (Half-day Wed.). Tel. 236 3573
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FAL ULTRA HIGH POWER LOUSPEAKERS

All power ratings are R.M.S. continuous. 2 YEARS' GUARANTEE High flux ceramic magnets. All carr. free.

<p>'POP' 100</p> <p>18" 100Watt 14,000 gauss 8/15Ω £22-95</p> <p>Dep. £22 and 9 monthly payments. £2-20 (Total £25-80)</p>	<p>'POP' 60</p> <p>15" 60 Watt 14,000 gauss 8/15Ω £12-90</p> <p>Dep. £3-30 and 9 monthly payments. £1-30 (Total £15).</p>	<p>'POP' 50</p> <p>12" 50 Watt 13,000 gauss 15Ω £10-90</p> <p>Dep. £2 and 9 monthly payments. £1-20 (Total £12-80)</p>
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FOR BASS GUITAR, ELECT. ORGAN, ETC. PAIR SUITABLE ALL PURPOSES

FAL LOUSPEAKERS 'POP' 25/2

12 in. 25 WATT

Dual Cone 15 Ω (for uses other than Bass Guitar or Electronic Organ) **£6-75** Carr. or Dep. £1 and 9 monthly payments 75p (Total £7-75).

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<p>F.A.L. PHASE 50 MK.III AMPLIFIER £34-85</p> <p>PR. FAL POP 55/2 50W L/SPEAKERS £13-50</p> <p>Terms: Deposit £6-50 and 9 monthly payments of £4.72 (Total £48.98)</p>	<p>PACKAGE PRICE</p> <p>£45</p> <p>£1</p>	<p>F.A.L. PHASE 50 MK.III AMPLIFIER £34-85</p> <p>PR. FAL POP 50 L/SPEAKERS £21-80</p> <p>Terms: Deposit £10 and 9 monthly payments of £5-25 (Total £57.26)</p>	<p>PACKAGE PRICE</p> <p>£52</p> <p>£1</p>
<p>F.A.L. PHASE 100 AMPLIFIER £61-95</p> <p>PR. LBS 50W L/S in cabinets £67-00</p> <p>Terms: Deposit £25 and 9 monthly payments of £19-50 (Total £135-50)</p>	<p>PACKAGE PRICE</p> <p>£123</p> <p>£22-50</p>	<p>F.A.L. PHASE 100 AMPLIFIER £61-95</p> <p>4 FAL POP 50 L/SPEAKERS £43-80</p> <p>Terms: Deposit £15-95 and 9 monthly payments of £10-50 (Total £110-45)</p>	<p>PACKAGE PRICE</p> <p>£99-95</p> <p>£2</p>

HIGH QUALITY LOUSPEAKER UNITS

TWO TONE REXINE AND VYNAIR FINISH

LBS 50 WATT Fitted pair of 12" 50 watt high flux speakers for conservative rating. Impedance 8-15 ohms. Or deposit **£33-50** 24-50 and 9 monthly payts. of £3-62. Total **£37-08** Carr. 75p

LBS 12" 25 WATT 10,000 lines 15 ohms. Also supplied in Rexine covered Carr. 50p.

LBS 12" 15" x 8" 10 Watt 11,000 lines 3 or 15 ohms. State impedance required. **£5-25** carr. 40p

FAL PHASE 50 Mk.III AMPLIFIER 50W

Solid state. 4 Separately controlled inputs Plus master vol. control. Ind. Bass and Treble Controls. Protective circuit to guard against damage from accidental shorts. Output for Speaker/ 3 to 30 ohms. Size 17" x 7" x 7 1/2"

200-250V. A.C. mains. Output 50 watts music rating. Or deposit **£7-25** & 9 monthly payments **£2-50**. Total **£34-95** Carr. 75p.

RSC BASS-REGENT 50 WATT AMPLIFIER

A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalist, gram, radio, tape. Peak Output rating Loudspeaker unit optional horizontal or vertical mounting.

- ★ Two extra heavy duty 12in. Loudspeakers.
- ★ Four Jack inputs and two Volume Controls for instant use of up to four pick-ups or "mlks".

Bass and Treble controls. Send S.A.E. for leaflet.

Credit Terms: Deposit **£16** and 9 monthly payments of **£6-08** (Total **£70-28**) **£63** Carr. £1-50

30 WATT HI-FI AMPLIFIER

For Guitar, Vocal or Instrumental Group.

A 4 input, 2 vol. control HI-FI unit with Separate Bass and Treble controls. Current valves. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. face. Neon indicator. For 200-250V. A.C. mains. For 3 or 15 ohm speakers.

Send S.A.E. for leaflet. Terms: Deposit **£4-50** and 9 monthly payments of **£2-28** (Total **£22-50**) Carr. 65p.



SOLE AGENT REQUIRED

The Amtron range of products will shortly be available in the U.K. and a sole agent is required to handle distribution. These are just four examples from their extensive range of equipment.

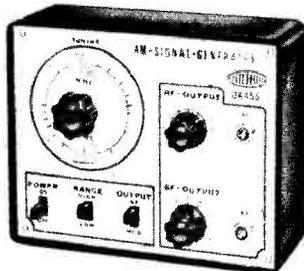


UK430/A

Wide-Band Millivoltmeter

The measurement of small AC voltages has assumed a great importance in the field of electronics. An essential requirement for instruments suitable for making these measurements is that their insertion into the circuit shall not disturb the circuit conditions. The UK430/A can be used for measuring background noise levels, residual ripple in power supplies and the measurement of frequency and gain in amplifiers.

Ratings and Characteristics: Voltage Ranges: 10-30-100 and 300mV, 1-3-10-30-100 and 300V. Decibel Range: -40 to +50dB. Frequency Range: 10Hz to 3MHz. Accuracy: 5%. Input Resistance: 500k ohms 10mV to 3V, 1 Megohm 3V to 300V. Power Source: 9V DC. Transistors: 4 x AF172, Diodes: 4 x AA138.

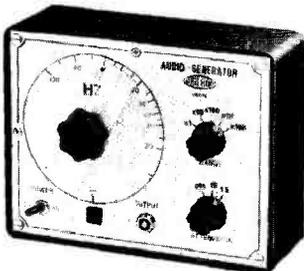


UK455

AM SIGNAL GENERATOR

This signal generator is a basic instrument for every technician, useful for AM radio receiver alignment, as well as for a wide range of measurements.

Radio Frequency Output voltage: 100mV. Frequencies: 400 to 900 kHz, and from 950 to 1600 kHz. Radio frequency attenuator: continuous variation. Modulation: internal at 1 kHz with depth of 30%, possibility of exclusion.

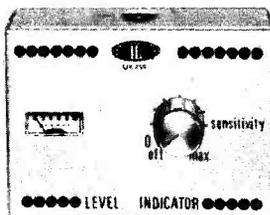


UK570

LOW FREQUENCY SIGNAL GENERATOR

Can be used to take various measurements, such as regulating equalizing circuits of amplifier inputs, tuning filters to separate low frequencies from high in electro acoustic producing apparatus.

Frequencies: 10 Hz to 1 MHz. Max. output voltage: 1.5 V. Attenuator: 15 mV; 150 mV; 1.5 V. Output impedance: 200 Ohm.



UK 255

Level Meter

This instrument is very useful whenever there is a need to know the level of a signal being fed into equipment. The unit is designed to be used in combination with the UKB10 Dynamic Compressor which is provided with an output point for connection to the Level Meter. The instrument embodies a 200µA full-scale-deflection meter, a signal of 5mV amplitude giving full scale deflection.

Ratings and Characteristics: Input voltage: 5mV max. Input Impedance: 47k ohms. Power Source: 8V DC. Transistors: 2 x BC108B. Diodes: OA85

Applications are invited from well established companies able to offer distribution facilities throughout the U.K. Please write with full details to:—

Box No. 102
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PRACTICAL WIRELESS

VOL 48 NO 1

Issue 783

MAY 1972

Up for the Cup!

At this time of year, all sorts of people are getting worked up on the outcome of *that* sporting event soon to take place in Wembley Stadium. In between bouts of waving their favours and whirling their rattles, the staff of P.W. have found themselves involved in the fate of another, though less spectacular, silver cup. They have been judging nominations for the P.W. Designer's Trophy for 1971.

In 1970 we launched *Project Autumn*, in which readers were invited to send in original articles on constructional projects within a specified period, the winner being the author of the work considered by the judges to be the best submitted. It was decided, however, to amend the rules slightly for the 1971 Trophy. Entries would be judged not in manuscript form but would be drawn from material actually published between the July 1971 and March 1972 issues.

Nominations would be judged, as before, on originality, ingenuity, construction, presentation, technical accuracy and other associated factors. However, under the revised arrangement, a new factor could be brought into play—call it 'workability', or Factor X. This allows the judges to take into consideration the trouble (or lack of it) in passing the articles through the editorial mill and noting any shortcomings not obvious in manuscript form. This permits a much fairer and realistic assessment to be made. The final results will be published in the next issue.

Although last year's crop of entries brought some new names to the pages of P.W., this year we want to see more and more! It has been suggested that the relative newcomer to technical writing has little chance when in competition with the regular and more experienced authors. There may, of course, be an element of truth in this, because on balance the "published" writer is experienced enough to have learned what is likely to be accepted for publication. On the other hand, P.W. has published many articles by new authors, sometimes at their first attempt.

However, in order to show faith in our stated objective of encouraging new writers, it has been decided that for the 1972 Cup *only writers who have never previously had articles published in P.W. will be eligible*. Describing the theory, construction and use of a piece of equipment can be a revealing exercise in testing the author's grasp of a subject (and the gaps in his knowledge), with the added incentive of some financial gain and, perhaps, a little glory! Full details next month.

So, keep those articles rolling—you may have just what we have been looking for and (who knows?) you may even win a cup!

W. N. STEVENS—*Editor*.

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SPECIAL FEATURE

Semiconductor Data Supplement

Part 8 of "Transistor Circuitry for Beginners" is held over.

**JUNE ISSUE WILL BE
PUBLISHED ON MAY 5th**

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Pacemakers

With surgical care, an electronic module for a long-lived heart pacemaker is assembled at Raytheon Company's Industrial Components Operation at Quincy, Mass. Aerospace reliability techniques are employed in the manufacture of the new devices to pace the beat of a human heart. The new medical aids will be powered by nuclear energy giving them a life expectancy of



10 years instead of two as presently experienced with units powered by mercury batteries. Raytheon is building the modules for ARCO Nuclear of Apollo, Pa., a wholly-owned subsidiary of Atlantic Richfield. The experimental programme is sponsored by the Atomic Energy Commission.

About 50,000 persons now depend upon pacemakers. It is estimated that an additional 5,000 to 10,000 will join their ranks annually as the reliability and longevity of the device is increased.

Mr. Regan, Raytheon's marketing manager, said the electronic circuitry of contemporary pacemakers outlasts the present mercury power sources but with the shift to nuclear energy and its 10-year life, the circuitry had to be upgraded. He said Raytheon had been selected for the task because of the company's experience and expertise in the manufacturing of sophisticated electronic modules. The company's performance with the ultra-reliability of the Apollo programme and compliance with NASA reliability standards were important factors in the selection, he said.

Atlantic Lock Out!!!

Mr. S. Valentine recently wrote to tell us of an amusing incident which occurred when he was doing a bit of S.W. listening one day.

He was tuned in to a QSO between two amateurs—one in the U.S.A. and the other in Scunthorpe. The American asked the "G3" to "let his wife in as it was raining outside." On hearing this, the Englishman was most astonished and enquired what was going on.

It transpired that the English lady of the house had allowed the door to lock behind her, and not being able to make her husband hear her, had contacted one of his pals to get on the air to the American to tell her husband to unlock the door!

1,000W Amp

Crown International of Elkhart Ind. have announced a new high power amplifier capable of providing 1,000 watts r.m.s. into a 4 ohms load. Available from Macinnes Laboratories in the U.K. the M600, is d.c.-coupled throughout although a front panel switch provides for an a.c.-coupled input if required. Power bandwidth at the 1,000 watts level is ± 1 dB from d.c. to 20kHz and THD at this level is below 0.1% throughout the frequency range. At 600 watts THD is below 0.05%. The intermodulation distortion is better than 0.1% at all levels from 0.01 watt to 1,000 watts, and the damping factor is greater than 200 from d.c. to 20kHz. Hum and noise are at least 110dB below 600 watts level. The M600 is equipped with its own two speed fan for cooling

"Radio Ear"

The present generation of mankind may be able to tune in on intelligent civilisations beyond Earth, if Congress appropriates the money to start building the VLA, America's proposed super-powerful radio observatory.

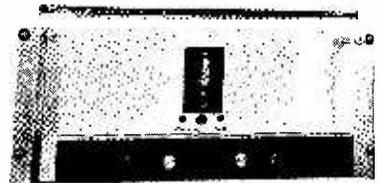
The National Science Foundation, under whose aegis the radiotelescope would be designed and constructed, said that an array of aerials resembling the giant "dishes" used to track spacecraft, would be set up in geometric patterns to pick up and focus signals emanating from the edge of the universe, 13,000 to 16,000 million light years away. The pattern would be an extension of the interferometer technique (placing aerials in a row or at right angles to one another) already widely used in radio-astronomy to enhance the strength of incoming radio signals.

A specific location has not yet been chosen for the new telescope, but it would be built in a pattern some 24 miles long at a high-altitude site in the south-western part of the United States, well away from earth-generated background noise.

It is likely that any new very large aerial would be used, at least part time, in "passive listening" for radio signals from other civilisations which many scientists believe must inhabit planetary systems around distant stars.

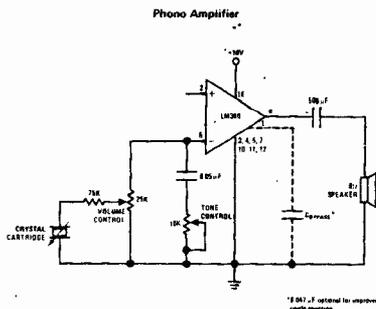
and on the rear panel is a switch offering six positions of operating modes. Weight is 80lb., and price inclusive of import duty, is £730.

Macinnes Laboratories Ltd., 71 Oakley Road, Chinnor, Oxon. Tel. Kingston Blount 52061.



The M600 amplifier

LM380 I.C.



D.T.V. Group Limited announce the LM380 audio power amplifier. The output has both short circuit current limiting and thermal overload current limiting to insure safe operation. Supply Voltage is 22V. Peak Current is 1.3A. Power output is 2W and input voltage is $\pm 0.5V$. Storage Temperature is $-65^{\circ}C$ to $150^{\circ}C$ and Operating Temperature $0^{\circ}C$ to $70^{\circ}C$. Lead Temperature (Soldering, 10 sec) $300^{\circ}C$. Price is £1.37^{1/2} + 10p postage and packing. D.T.V. Group Limited, 126 Hamilton Road, West Norwood, London, S.E.27.

Gas Radio

Reader R. Jenkins has told us of a Mr. Jack Hickson who has a Gas-Powered radio.

The radio at Mr. Hickson's home in Hadnock Road, Monmouth, takes its power from a thermo-electric generator which has gas burners. Electricity is generated by heating of copper plates. The generator charges a battery off which the 33-year-old radio is run.

The generator supplies enough electricity to charge accumulator batteries or even a car battery.

The generator was made in 1938 by a Yorkshire firm specially for providing power for battery radios.

But for gas board engineers carrying out North Sea conversion it was something they had never encountered before. They had to take the generator to Cardiff and it took them about a week to change the burners and adapt it for North Sea gas.

Audio Fair

Exhibitors at last year's International Audio Festival & Fair asked for more space in the 1972 show. In order to accommodate them, the organizers have arranged to move the Festival from the Empire Hall to the Grand Hall, Olympia, which will provide an additional 74,000 sq. ft. of space.

The 1972 Audio Fair, sponsored by the Sunday Mirror, will be held from October 23 to 28. It will allow the public to listen to the products of the world's leading manufacturers of sound reproduction equipment, specialist Hi-Fi, and a comprehensive display of accessories.

There will be many special attractions, including more than 75 specially constructed Audio Studios, and a Hi-Fi Theatre offering a daily programme of lectures and concerts.

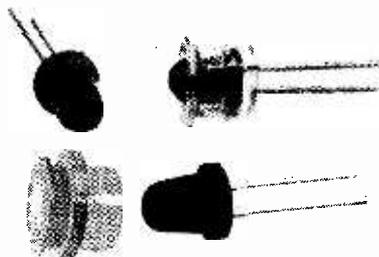
GaAs Light



GaAs Light indicates the state of p.n.p. or n.p.n. logic systems capable of driving at say 15mA at 1.6V or over. For the brightest display 40mA is recommended. The intensity is acceptable at only 10mA. The advantage of these lamps is the low cost (95p) and higher reliability.

Due to the low current and voltage requirement of small battery operated equipment it is now possible to run these GaAs lamps in series with the electronics, so reducing the indicating power to only 16mW. This power is therefore less than the power wasted by even a very small equipment being inadvertently left on. West Hyde Developments Limited, Ryefield Crescent, Northwood Hills, Northwood, Middx., HA6 1NN.

Led Lamps



Guest International announce the availability of a new range of solid state lamps using Gallium Arsenide Phosphide Diodes. The lamps are encapsulated in two main forms of package—one with a glass to metal seal and the other a moulded plastic case. Both employ a lens in front of the actual diode to alter the characteristics of the light emission, one type diffuses the light, whilst the other produces a point source each available in different colourations. The lamps combine extremely long life with very efficient operation making them ideal for use as panel lights or status indicators in modern equipment. There are currently 5 versions in the range given the generic title RED LIT series and luminosities as high as 2000ftL at 50mA are offered. Guest International Limited, Nicholas House, Brigstock Road, Thornton Heath, Surrey, CR4 7JA.

Philips Booklet

Philips have published a colour booklet entitled "All about Tape and Cassette recording". The booklet, which sets out the origins of tape recording and describes how magnetic tape works, is available to schools and students on request.

It has been published primarily as further study material for project work.

25,000 copies of the booklet have been printed and copies can be obtained from the Publicity Department, Philips Electrical Ltd., ELA Division, Century House, Shaftesbury Avenue, WC2H 8AS.



SINCE the original Treasure Tracer was built and described in this magazine, development work has continued. The author's own success with the prototype and the enthusiasm of readers has resulted in a considerable amount of experimenting and this article describes the improvements that have been made.

It has not been assumed that all readers will have seen the original article; for this reason much of the information given last time is repeated. This article should enable the new reader to build the project as described as well as enabling the reader who built up the original circuit to up-date his Treasure Tracer. To make matters simpler for these people, the original case has been retained with relatively few changes.

The cost of the original was not high but in fact the component cost for the Mark II will probably be marginally less, though the mechanical and construction side may cost more. The total cost for the Treasure Tracer Mk II should be something under £5 though this will vary depending on source of supply.

For those who did not see the original article, the principle of operation will be briefly described.

The circuit works in exactly the same way as the original. Two low frequency r.f. oscillators are arranged to beat together. One of these oscillators makes use of a tuned circuit working inside the case; we shall call this the reference oscillator. In operation this remains at one frequency though this is adjustable for "tuning up".

The second oscillator, working at essentially the same frequency, also makes use of a tuned circuit but in this case the inductor is external and becomes the "business end" of the circuit. We shall call this the search coil and the search oscillator.

If a small part of each of these oscillators is mixed together they will beat with each other. If the difference in frequency is small, this beat note will fall in the audio range. If the reference oscillator is working at say 130kHz and the search oscillator is at 131kHz, a beat note equivalent to that difference will be produced, in this case 1kHz; this audio signal can be amplified and fed to the speaker.

Now the search oscillator makes use of an external coil and if certain materials, especially metals, are brought into the vicinity of this coil, these will alter

THE PW TREASURE TRACER

HALVOR MOORSHEAD



The original Treasure Tracer, described in P.W., August 1971, was a very popular feature, judging by your letters and reports from components stockists. Few readers had difficulty in either building or using the metal locator. This article describes an improved version of this project.

the value of the coil inductance, which in turn will alter the frequency of oscillation.

A better known example of this change of inductance is the ferrite rod aerial. By moving the coil along the rod the inductance is changed; this is of course done every time a superhet is aligned. A ferrite rod will roughly double the inductance of a coil. Far smaller changes in inductance take place

in a metal locator—usually fractions of one percent—but because of the frequency used and the fact that it is compared to a standard frequency, the changes in the audio note will be considerable. Taking the frequency actually used in this circuit, a 0.1 per cent increase (or decrease) in the inductance will result in a 130Hz change in the audio note.

It would be possible to have both frequencies fixed at say a difference of 100Hz but there are so many factors that effect the frequency that it is easier to arrange for one of the oscillators to be adjustable in order that they can be brought close together.

In this circuit we are changing the frequency of the reference oscillator though it could just as well have been the search oscillator.



The original Treasure Tracer, described in the August 1971 issue. The text mentions several improvements that have been made, both to the circuit and the construction. The heading photograph shows the Mark II in operation.

MODIFICATIONS

In the light of experience and bearing in mind the comments of readers, the following modifications have been made to the prototype:

1. The original Treasure Tracer was not mechanically balanced. It was held at the end of the handle and while this worked quite well, it became very tiring to hold during long searches. The Mark II is balanced as can be seen from the photograph; it is easier and more comfortable to hold and there is no hand strain even after several hours.

2. The output volume was felt by some readers to be too low. In many cases this could have been due

to inefficient operation of the particular transistors used as the output of the prototype was found to be quite adequate. Even so, the sound level available in the Mark II has been increased and since this could be annoying in certain locations at maximum volume, a volume control has been included. To save extra drilling etc., the on-off switch (a miniature slide type in the prototype) is incorporated with the volume control.

3. The stability of the prototype left a little to be desired. Touching the metal case or the wires running from the search coil to the case caused a change in frequency. This was not too serious in practice once one got used to it but several changes have been made to the construction of the Mark II to improve the stability.

4. The construction of the search coil has been changed to make the windings much more rigid; this has proved to be much better than the principle originally employed. In addition the weight of the "head" has been reduced and this again helps with the balance.

5. Overseas readers (who account for a proportion of the magazine's readership) sometimes had difficulty in obtaining certain parts. This has been borne in mind and the parts should be available world-wide except for one component and the construction of this is described later.

6. Improvements have been made to the oscillator circuits. In the Mark I a Hartley oscillator and a Blocking oscillator were used for the search and reference oscillators respectively. Both of these have been changed to the more stable (and slightly simpler) Colpitt's type. In addition to these advantages, the search coil is now only a single winding (it was tapped in the Mark I) as is the coil used for the reference oscillator. This simplifies construction and reduces the cost slightly.

In addition to the above points a considerable number of other experiments have been tried but have not been incorporated for various reasons. For those who wish to experiment further, these are mentioned; they may give certain leads and possibly prevent the reader following fruitless paths.

The best frequency for operation was carefully investigated. Although the regulations limit operation below 150kHz, experiments were carried out at six widely differing frequencies and the results compared. Since for a given percentage change in inductance there will be a much larger change in the audio frequency using higher r.f. frequencies, it would appear that operating at say 2MHz would be better. In practice other factors start to come into it and ground capacity effects become serious. Bringing the coil towards plain earth causes a considerable change in frequency and even fitting a Faraday Shield only improved this slightly. About six different frequencies were tried but the only result was a confirmation that the original 130kHz or thereabouts is the best. Ground capacity effects are negligible and, although a Faraday shield was tried, this made no improvement and so has not been incorporated.

A meter was tried as the sensing indicator. Although a workable circuit was developed, it was found to be far less sensitive than the ears and very difficult to use. There was also considerable difficulty in filtering out all the r.f. before applying this to the frequency counting circuit. For this reason details are not included.

Several experiments were made with different diameters of search coil. A clear rule seems to apply

here. The larger the diameter of the coil, the greater the depth of penetration for large objects but at the same time the larger coils were less sensitive to small objects close by.

There is certainly room for experiment here. As long as the inductance of the coil remains the same, it doesn't matter at all what size it is, it could be lin. or 3ft. in diameter. The 6in. used here is the best compromise for general purposes; it is good for coins and not too bad for large objects reasonably close by. For those who are prepared to take the trouble, it should be possible to arrange for the coils to be changed depending on the nature of the search.

As a general guide the same length of wire should be used whatever the diameter of the coil, that is about 92ft. of wire. This is only a guide and turns may have to be added or taken off, to allow the frequency to be brought into the right range.

Encapsulating the coil in epoxy resin was tried and although this was an improvement over the Mark I as it prevented movement and consequent frequency changes, it did not help with the Mark II and only added to the weight of the search coil head.

THE CIRCUIT

The complete circuit is shown in Fig. 1. Tr1 and the components surrounding it form the search coil oscillator and, as can be seen, this connects to the search coil via a coaxial cable. Tr2 and the associated components form the reference oscillator, L2 being a long-wave winding (an inductance of just over 2mH) but fitted with a ferrite slug (not normally supplied). The one used in the prototype is primarily intended as a crystal set coil; a medium wave winding is also fitted but this is ignored.

This oscillator is adjustable by varying VC1 which is a 750pF compression trimmer and the combina-

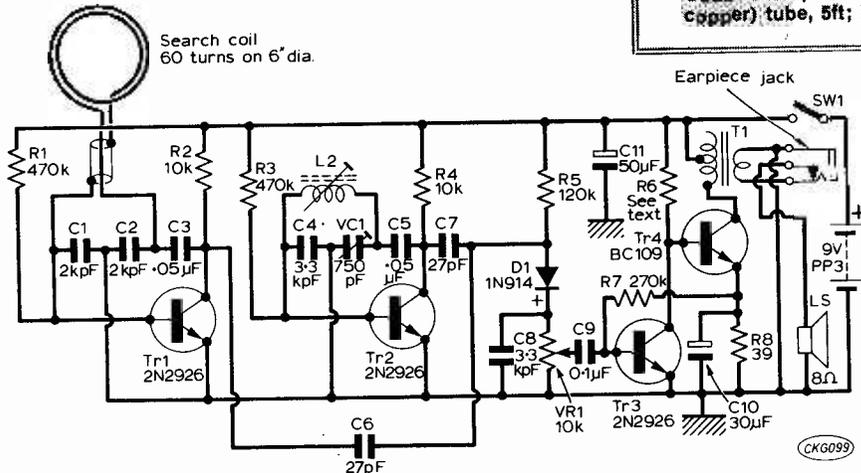


Fig. 1: The complete circuit of the Mark II. Although very similar to the original as far as operation is concerned, this is more stable and has a greater output.

tion of the variable core in the coil and VC1 enables this tuned circuit to be varied over a considerable range. Even if the search coil oscillator is way off the intended frequency it will be possible to tune the reference oscillator to it.

From the collectors of both oscillator transistors low value capacitors C6 and C7 feed to the detector diode which, being a silicon type, requires a standing

★ components list

Resistors

R1 470kΩ	R5 120kΩ
R2 10kΩ	R6 See text
R3 470kΩ	R7 270kΩ
R4 10kΩ	R8 39Ω
All resistors 1/4W, 5% types.	
VR1 10kΩ log pot with switch	

Capacitors

C1 2,000pF ceramic or polystyrene
C2 2,000pF ceramic or polystyrene
C3 0.05µF ceramic or mylar
C4 3,300pF ceramic or polystyrene
C5 0.05µF ceramic or mylar
C6 27pF polystyrene or mica
C7 27pF polystyrene or mica
C8 3,300pF ceramic or polystyrene
C9 0.1µF ceramic or mylar
C10 30µF 10V electrolytic
C11 50µF 10V electrolytic

Semiconductors

Tr1 2N2926	Tr4 BC109 or 2N2926
Tr2 2N2926	D1 1N914
Tr3 2N2926	

(Note that any colour of the 2N2926 can be used but the "G" or green is best for Tr3 and Tr4)

Miscellaneous

- L1 See text and Fig. 2
 - L2 Repenco Crystal Set Coil Type DRX1. This must be fitted with a ferrox tuning slug which is not provided.
 - T1 Transistor output transformer, Type LT700 or similar—see text.
 - L.S. Miniature 8Ω loudspeaker—see text
- Earphone jack, 3.5mm type with break switch; Battery, PP3, 9V; Case, 6½ × 2½ × 1½ in. in aluminium (available from H. L. Smith Ltd., 287/9 Edgware Road, London W.2, price 60p including postage); Coax cable; Connecting block; Aluminium (or copper) tube, 5ft; Plywood for former.

this will certainly work. Once operation of the main stages has been established, the correct value should be found by experiment. It should be chosen for maximum output compatible with reasonable current consumption (under 20mA).

Some readers had difficulty in obtaining the high impedance speakers used in the Mark I and for this reason the Mark II uses a standard 8Ω miniature loudspeaker. This necessitates using a transistor output transformer. Normally only push-pull types are available, that means that the primary is centre tapped, in this case only one half of the primary winding is used. The use of earphones is also easier as the impedance of 8Ω is far more common than the 80Ω used in the Mark I. For those who have high impedance speakers (anything from 35Ω to 80Ω) these can be used, in which case they go directly between the collector of Tr4 and the positive line. The fitting of an earphone socket for this will have to be worked out if required. R6 will be a different value if a high impedance speaker is used.

The whole circuit is operated by a PP3, 9V battery which will last a considerable while. The current consumption will depend on the value of R6 but will probably lie in the range 10-20mA.

For those who have the original Treasure Tracer article, it will be seen that although very similar in many aspects, this circuit is rather simpler as well as being a bit better. The choice of a BC109 transistor for Tr4 rather than the 2N2926 used previously is not important and a 2N2926 can be used here if required.

CONSTRUCTION

The construction of the Treasure Tracer Mark II can be regarded in two distinct sections; the electronics and the mechanics. It does not matter which is tackled first.

The search coil is wound on a wooden former cut from a piece of 1/4in. (6mm) plywood, see Fig. 2. This is circular in shape with a cut-out to reduce the weight although this is optional; it is a simple matter with a fret-saw or jig-saw but difficult otherwise. A groove should be cut into the edge of this circle to hold the wires. Many methods can be used to do this, the simplest way is to spin it in an electric drill and use a rasp to cut the groove. The search coil need not even be round, it could be square or triangular and many other methods of construction can be employed but the described shape has proved very successful. When this groove has been cut, two very small holes should be drilled diagonally from the groove to the top of the former as shown. Where these emerge, a connecting block can be screwed on to act as the winding anchoring point. Sixty turns in all are required; these should be neat and taut and once finished a band of tape can be wound around as shown in the photograph. An alternative would be to saturate the windings with a glue to hold them firmly in place. By sinking the windings in a groove they are protected to a considerable extent.

The handle of the device is made from aluminium tubing which is available from a number of sources. If difficulty is experienced in obtaining this it can be made from copper tubing with the same diameter, a plumber should be able to supply a suitable length. Five feet was found to be about the right length but this will depend on the height of the user.

The handle is fitted to the search coil former with a simple bracket, bolt and wing-nut as shown in Fig. 2. The connecting wire from the search coil to

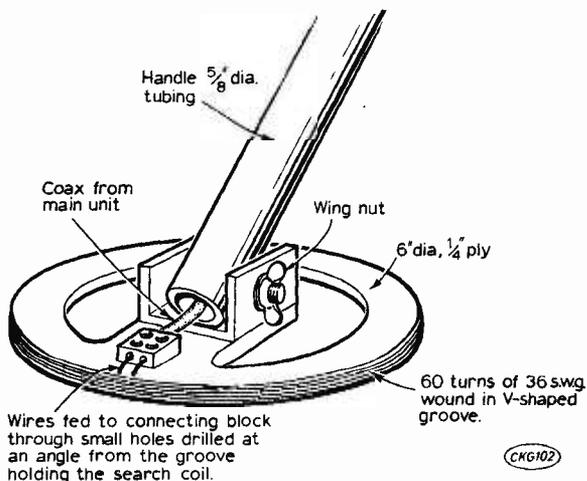
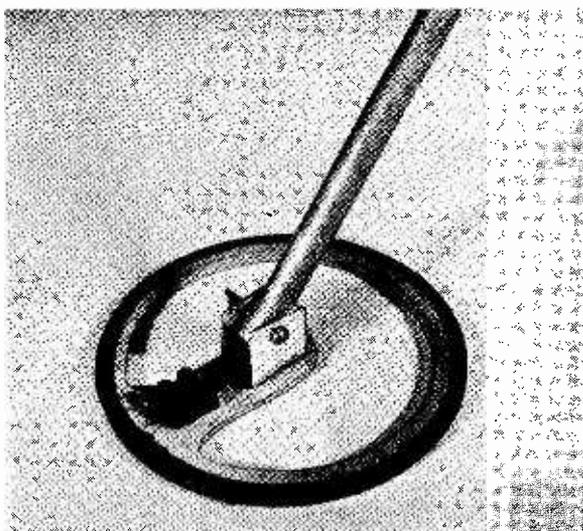


Fig. 2: The construction of the search coil. This design has been found to be excellent but as long as the inductance of the coil remains the same, any arrangement may be used.



A photograph of the search coil used in the Mark II.

the main circuit is a coax cable running up the tube. At the lower end this is fitted to the connecting block. The use of coax ensures that there will not be loose wires flopping about inside and that the capacity will remain constant. Coax is more rigid than twin wires and is also better for that reason.

The electronics is built into a aluminium case, available from the suppliers mentioned in the components list. This will have to be drilled to take the speaker and various other fittings. A drilling diagram is not shown as the siting will depend on the components used and in any case the siting is fairly obvious. A series of small holes can be drilled for the speaker or a large hole (1 1/2in. diameter at least) which can be fitted with some form of grille.

The majority of the components are mounted on a piece of Veroboard and the layout of this is shown in Fig. 3. Veropins are used for all the take-off points as this leads to a nice, neat appearance. The coil L2 is mounted directly onto the board as shown. Four corner mounting holes should be drilled for later fitting.

A number of breaks are needed in the copper strip of the Veroboard and these are indicated in Fig. 3. There is nothing complex about the wiring. R6, which will have to be found by experiment, has plenty of room around it. The easiest way of experimenting with this is to initially wire in the recommended 22kΩ resistor with fairly long leads. Once the general operation has been established this can be cut out leaving wires sticking out. These can form the anchoring point for the replacement.

Figure 4 shows the remainder of the wiring and also the anchoring of the coax cable from the search coil. All connecting points are coded with letters and no difficulty should be experienced in this part of the construction.

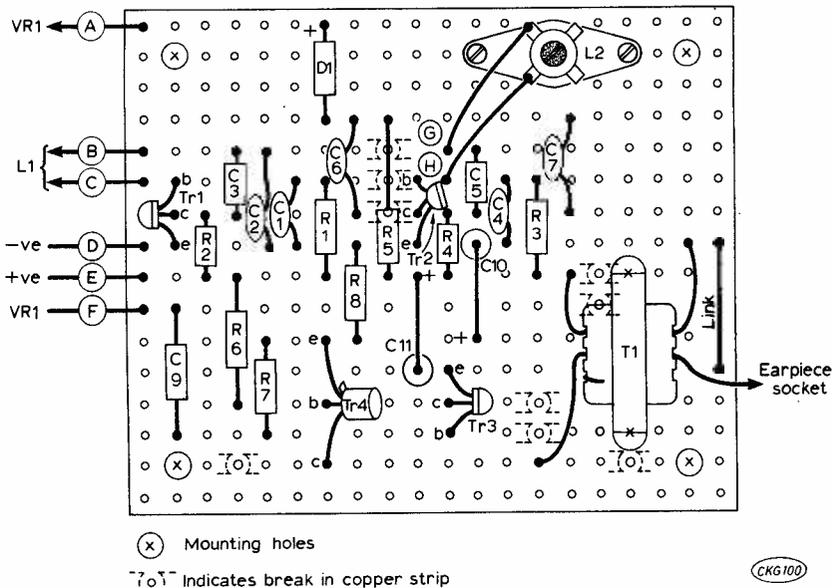


Fig. 3: The components layout on Veroboard. Veropins should be inserted at the points marked A to H.

TESTING

Once completed the unit can be tested. If all is well there will be a slight noise from the speaker which will be increased greatly by dabbing a finger onto the VR1 contact which runs to point A on the board. Set VC1 to roughly half compression and adjust the core of L2. A strong whistle should be heard at one point and this will be found to be tuneable by VC1 as well. Other lower level whistles may

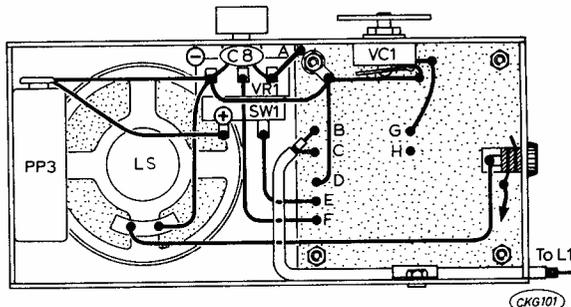
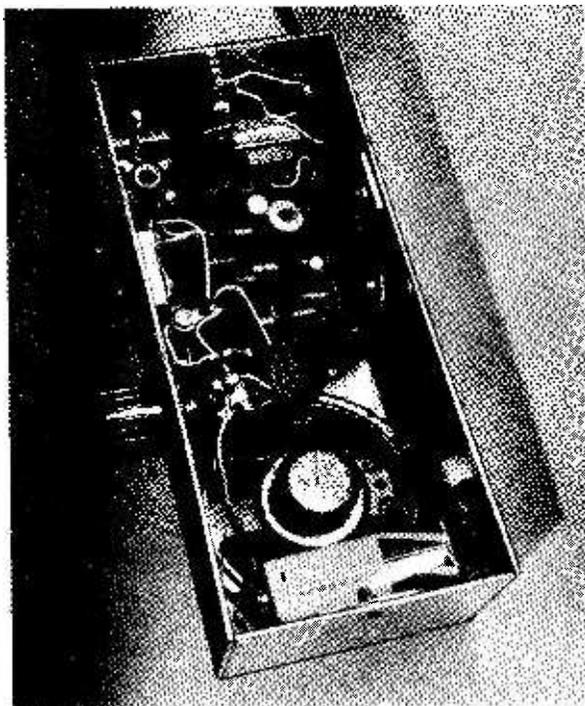


Fig. 4: The wiring inside the case. VC1 must be sited so that it does not foul the coil L2.



An internal view of the Treasure Tracer Mark II.

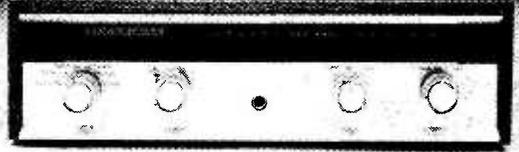
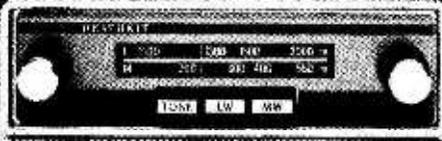
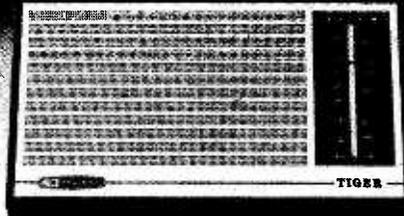
be heard, these are due to the oscillators beating with radio stations. In some cases it is possible to make the unit operate using only these but it will not be nearly as loud or as good. The level of the main beat note will be much louder and cannot be missed.

Once the beat note has been established, the Treasure Tracer is ready for use. We have deliberately avoided making any claims about the depth to which it will find objects. Commercial models frequently make wild claims which cannot be substantiated and we do not want to follow this example.

To conform with the Wireless Telegraphy Act (1949) a licence is required to use the Treasure Tracer described here.

Under Section 1(1) (Pipe Finder Licence) the band 16 to 150kHz can be used for equipment of this type.

A licence for five years costs 75p and can be applied for on a form obtainable from the Ministry of Posts and Telecommunications, Waterloo Bridge House, Waterloo Road, London S.E.1.



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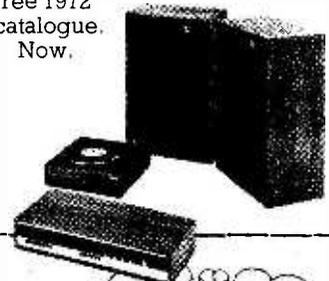
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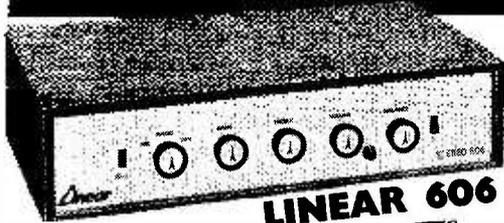
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1A7GT	45	6B16	50	6J7GT	45	7H7	45	7D5	60	19A05	50	50B5	50	50C5	50	50D1	50	50E5	50	50F7	50	50G7	50	50H7	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50	50X6	50	50Y6	50	50Z6	50	50A6	50	50B6	50	50C6	50	50D6	50	50E6	50	50F6	50	50G6	50	50H6	50	50I6	50	50J6	50	50K6	50	50L6	50	50M6	50	50N6	50	50O6	50	50P6	50	50Q6	50	50R6	50	50S6	50	50T6	50	50U6	50	50V6	50	50W6	50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DEPTH OF OPERATION

In the original article we showed exactly what we found and at what depths. Generally speaking coins can be detected at ranges of up to 4 or 5in. but this also depends on the size. Large objects can be detected at distances up to about a foot but the sensitivity falls off considerably over that distance.

Do not expect to become an expert as soon as you start to use the Treasure Tracer. The Mark II is considerably more stable than the Mark I and there will be fewer false signals; even so it takes an appreciable amount of practice before the small changes in the audio frequency are noticed. This point cannot be over-emphasised.

Using the Mark II one person was able to locate a 1/2p coin at 4in. every time, while another, who had never tried it before, had difficulty in finding a 50p coin at 2in. This illustrates the importance of practice.

The beat note is adjustable for either a rise or fall in frequency when a metal object is approached. The author prefers a falling note but this is only personal preference. It is usually better to work with a low frequency audio note—say 100Hz—as a 50Hz change at this frequency is very noticeable; at 1kHz the same change would not be so obvious.

FREQUENCY LOCKING

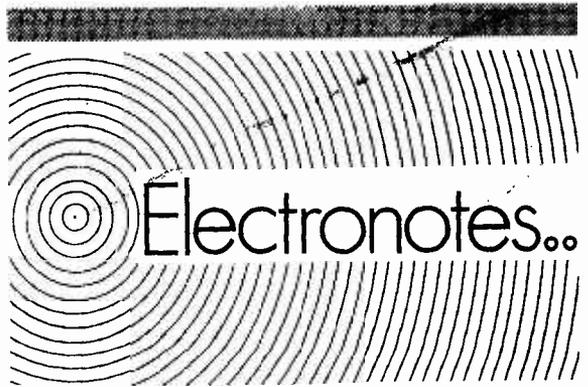
If the two notes are very close together, the two oscillators will lock together. The Mark II is slightly better than the Mark I in this respect and reducing the value of C6 and C7 will lower this locking frequency even further but no advantage was found in bringing it much lower. The prototype Mark II locked at about 20Hz.

VC1 has considerable range and it has been found better to arrange for it to be used at near maximum compression, compensating for this by readjusting the core of L2. This prevents a change in frequency due to the leaves of VC1 moving which they tend to do when there is little compression. A possible improvement would be to replace VC1 with a much lower value—say, around 100pF (compression trimmers in this range are available) and to wire fixed capacitors in parallel with it to obtain the correct value. This will mean that VC1 will have a narrower range, but still around the correct frequency, at the same time as reducing the likelihood of instability.

L2, as we have said, is a long-wave winding of a crystal set coil, the only modification being to fit a ferrite core (the former is already tapped to take this). It is possible, if tedious, to wind one's own coil on a 1/4in. outside diameter former; 350 turns of fine wire (39s.w.g. is used by the makers) pile wound will give the correct inductance.

One point must be repeated from the previous article. Users of metal locators are not very popular with many archaeologists because of the highly irresponsible way in which some people use theirs. A local archaeological society may be happy to use your services under their supervision but others may not welcome you. *Note that there are heavy penalties for using such a device in areas scheduled as being of historical interest without permission.* ■

We regret that issues of Practical Wireless, August 1971, which described the Mark I are not available.



S. GINSBERG

MANY people have expressed a mixture of interest and scepticism about the 50F (fifty Farad) "capacitors" which are contained within 1/3rd of a cubic inch. These are manufactured by Gould Ionics in the U.S. and are marketed in the U.K. by Lyons Instruments at Hoddesdon. Note: the price of these units for one-off is around £25 each and the company may well only supply the professional user.

How does your radio shop test those transistor radios and televisions? Bet they have an engineer prodding about with a multimeter. Of course, knowing exactly where to prod and why is the most important part.

In industry, it would take far too long to do this on the end of a fast-moving production line so other techniques have had to be employed. Automated test gear is a highly sophisticated subject, but it is becoming more commonly employed.

One piece of gear which does this has been introduced by Honeywell Limited. Designated the "Swift" digital tester, it is a portable equipment and is so simple to operate that even an unskilled person can use it successfully. It can be used for testing digital printed circuit boards when they are fully assembled. Amazing thing is the speed at which the tests can be carried out. The equipment can test at the rate of a million tests every second which is just a trifle faster than the average service engineer. A p.c.b. with some 64 connectors may be plugged in and tested and should a fault arise, this is indicated by a light which shows at which end connector the fault is.

Cable-Scan is another useful little test gadget marketed by Thomas & Betts International Inc. located at Cowcross Street, London. Imagine you had a bundle of wires to sort out. Which are the signal wires, which are earth etc? Well, Cable-Scan will tell you.

A clever idea is that the operator wears a small wrist strap which provides a signal. This is then cunningly transmitted via the operator's fingers so that all he has to do is to touch the wires. A digital readout is provided so there is no chance of an operator making an error through having to write data down—he can see at a glance. Up to 200 signal input circuits are catered for which means that the operator can tackle a mighty big bunch of wires and sort them out without any trouble.

Before you think of rushing out and buying an automated tester and setting up in business as a lightning radio and t.v. repair enterprise, the cost of the Honeywell Swift equipment is around £900. But it is still cheap for large production runs.

The "colonials"

I am writing in hope that you may like to enlighten "us Colonials" about some of your circuits that you print in that great little magazine P.W.

We in Australia cannot obtain quite a few components that you use, mainly coils and substitute transistors. Wouldn't it be possible to give information on coils, such as diameter, turns, gauge of wire, etc.

There is another favour you can do for your readers, don't change P.W., it's O.K. as it is.—**R. C. Shambler**, (Australia).

Editor's Note:

It would not really be practical to give all the information on the coils specified in P.W. However the majority of the larger advertisers in this magazine will supply components to overseas readers and even air mail postage on small items such as coils and transistors is surprisingly inexpensive. (To Australia the air mail postage is often only twice that of internal British mail).

Cassette deck

I agree with V. C. Watts (Bath) "Cassette deck" March '72. I have tried many companies in search of a deck for a home-made system. The only firm I have discovered who at one time did sell decks (made by Philips) has now stopped and according to their letter did not think they would be able to sell them again. Perhaps these and other letters may stir the component firms into action.—**A. R. Knight**, (Oxford).

Ebuc oidar

Leafing through my March copy of *Practical Wireless* I chanced upon the article on the Cube Radio. On closer inspection, I found that the photograph on page 998, a general view of the completed receiver, was shown as a mirror image. The lettering on the battery and the position of VRI show this. Is this because we have to use a battery providing positrons—the mirror—images of electrons?—**G. L. Manning**, (Middlesex).

Alice is not a member of our Staff—it's all done by mirrors— (Editor).

Tools for the job

The purpose of this letter is to comment on "Who makes What?" In Feb. issues's "Letters", as it has some bearing on my own experience, although with ancillary tools rather than radio parts.

Last May I got a kit for the "PW-12-12 Stereo", which is now, after some odd troubles working fantastically well. I was determined to get the tools for the job, which included special soldering irons and bits, the standard 'nipper' type of wire cutting pliers, and long nosed ordinary pliers, I was also determined to get British tools which I did; or thought I did. My comments hereunder refer to the pliers and wire nippers.

They were both on the modern type of display card, the long nosed pliers, with nicely red painted handles I saw were made in England. Quite a number of filing marks here and there on them, and a scratchless finish which looked like chrome plating. These nippers had the name in large headlines of the English company which 'made' them as I thought. A London firm. Surprisingly despite the perfect finish and insulated grip of the 'nippers' there was only 10% difference in the prices, and I thought that British tool makers at last were 'With it!'

When I got home I found that these perfect nippers were made in Japan, as quite properly announced in tiny print, for the English firm, and I felt aggrieved.

So I went to work on my Double-12 amplifier, and exactly a month later I found that the English made pliers had $\frac{1}{16}$ in lateral play at the plier points, showing either bad workmanship or bad material. After nine months the Japanese nippers are as when bought and when I'm sewing on a trouser button, I use them in preference to scissors to cut the cotton! Clean as a whistle.

I know this does not refer to radio parts, but such an experience reflects on all British products, and I wonder if this is the reason why it is now apparently expedient *not* to put the country of origin on the product.—**N. H. Hodgson**, (Middlesex).

CQ thanks

I should like to thank you for printing my problem in your C.Q. column. I have had several replies recently, including one offer from a Mr. Oldknow in Horsley, Woodhouse who is willing to turn a new pulley wheel from scratch on his lathe!—**W. R. Kennon**, (Derbyshire).

Dreams

I often dream of being a ship's radio operator between the spark-gap and the valve era, with big brass morse keys, large accumulator terminals, 4 pin valves and coils on 2in formers and not $\frac{1}{4}$ in. The transistor should never have been invented. Old and sentimental at 26 years of age!

Just in case I start a war as an inexperienced *nut* perhaps the following details provide my defence. My construction knowledge covers from a crystal receiver to a 9 valve communications receiver.

Operating experience — 42,000 miles of travel.

Operating a.m., s.s.b., c.w. and RTTY links plus Australia with the armed forces, presently employed as GPO Telegraphist.

Transistors are too small and don't leave enough room for any serious experiments, I'll still keep buying old battery valve sets for 50p and £1 and re-making them until they run out of supply and then I'll take up fishing.—**W. D. Logan**, (Hyde, Cheshire).

Nuvisitors

In "Letters" of March, Mr. K. Freeby remarks on the absence of information on nuvisitors. I have a copy of *Practical Television* dated December 1962 in which there is an illustrated article by K. Royal entitled "Practical Nuvisor Circuits". Mr. Freeby may have this magazine if he requires it.—**N. A. Hodgson**, (84 Lansbury Drive, Hayes, Middlesex).

*We would like to thank Mr. Hodgson for his kind offer and also to thank Mr. Laurence Mason who has kindly sent us some gen on nuvisor valves to pass on to Mr. Freeby—*Editor.

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Six speeds are available 500, 850 and 1,100 r.p.m. and 8,000; 12,000 & 15,500 r.p.m. shaft is 1/2 in. diameter 230/240v Its speed may be further controlled with the use of our Thyristor controller. Very powerful and useful motor unit approx. 2 in. dia. x 5 in. long. Price 85p plus 25p postage and insurance.



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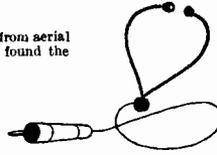
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2 poles	40p	70p	70p						
3 poles	40p	40p	40p	40p	70p	70p	70p	95p	95p
4 poles	40p	40p	40p	70p	70p	70p	70p	120p	120p
5 poles	40p	40p	70p	70p	95p	95p	95p	145p	145p
6 poles	40p	70p	70p	70p	95p	95p	95p	170p	170p
7 poles	70p	70p	70p	95p	95p	120p	120p	195p	195p
8 poles	70p	70p	70p	95p	95p	120p	120p	210p	210p
9 poles	70p	70p	95p	95p	145p	145p	145p	235p	235p
10 poles	70p	70p	95p	120p	145p	145p	145p	260p	260p
11 poles	70p	95p	95p	120p	170p	170p	170p	285p	285p
12 poles	70p	95p	95p	120p	170p	170p	170p	310p	310p

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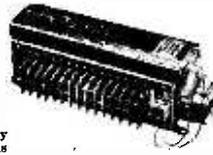


PW DIGITAL CLOCK

As featured in this issue. Send S.A.E. for parts list.

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This is a drum type timing device, the drum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 operations per switch per rotation. There are 15 changeover micro switches each of 10 amp type operated by the trips thus 15 circuits may be changed per revolution. Drive motor is mains operated 5 revs per min. Some of the many uses of this timer are Machinery control, Boiler firing, Dispensing and Vending machines, Display lighting and signal signalling, etc. Price from makers probably over 210 each. Special snip price 25.75 plus 25p post and insurance. Don't miss this terrific bargain.



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900 W Model. 14" long x 1 1/2" wide. Made by Backer. Price 75p or 10 for 26.75.
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Tricity Cooker Elements. We have quite an assortment of these and will describe them in future issues—but if in the meantime you are needing these then please let us have a sketch, we may have the exact one in stock.
Slide Switch. 2 pole change over panel mounting by two 6 BA screws, size approx. 1 1/2" x 3" rated 250v lamp, 6p each, 10 for 54p, 100 for 22.10, 500 for 224.

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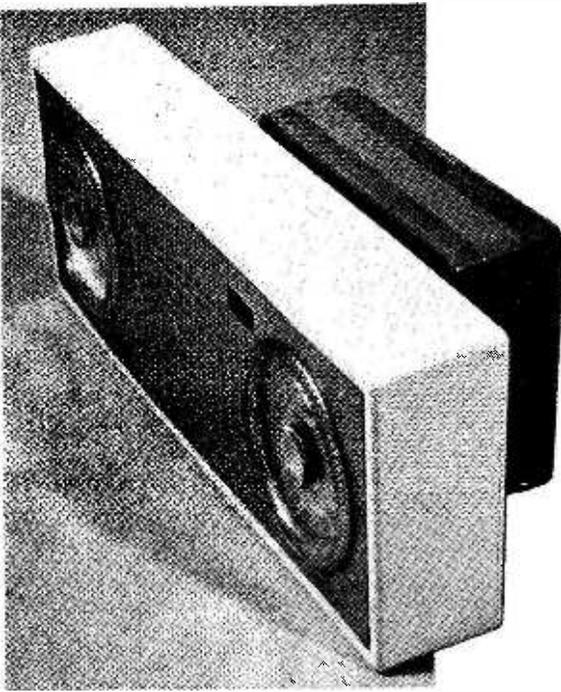
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ADD-A-VERTER FOR RADIO 2

ERIC DOWDESWELL

YOU want to listen to Radio 2 but you haven't got long waves or v.h.f. on your transistor portable. What to do? Just place the Add-a-Verter behind your radio and tune in Radio 2 at about 480 metres on the dial of your receiver. No connections or fiddling about with the innards of your squawk box.

How is it done? By picking up the Radio 2 signal on 200kHz (1500 metres) and mixing it with a local oscillator 429kHz in the Add-a-Verter thus producing a new signal on 629kHz which can be heard on the receiver on the medium wave band.

Cost of the bits and pieces bought new? About £2, plus the cost of the plastic box. The average constructor will be able to find most of the parts in his junk box.

L3 which presents a high impedance at the crystal frequency. The circuit will still oscillate if the bottom end of C1 is connected to the negative line. But more later on the operation of the crystal.

The Radio 2 signal is picked up on the ferrite rod aerial L1 and fed to the base of the transistor. The signal at the collector now consists of the oscillator frequency 429kHz plus and minus 200kHz as well as the basic oscillator frequency of 429kHz. However it is the sum frequency of 629kHz which interests us, since it falls in the m.w. band.

The output coil L2 is also in the form of a ferrite rod aerial and it is the signal from this coil on 629kHz that is picked up by the ferrite rod aerial in the adjacent receiver.

THE CRYSTAL

The use of a crystal may seem extravagant and unnecessary to some but in fact it costs just 25p and its use saves much time fiddling around with coils and capacitors trying to hit the right frequency. Its stability is also so very much better than an LC combination. It is worth noting that the crystal oscillated immediately the prototype was switched on for the first time. The only other adjustment then needed

CIRCUITRY

Nothing very complicated as can be seen in Fig. 1. A commonly available 2N2926 n.p.n. silicon transistor has a quartz crystal connected between its base and collector with the supply voltage being applied via

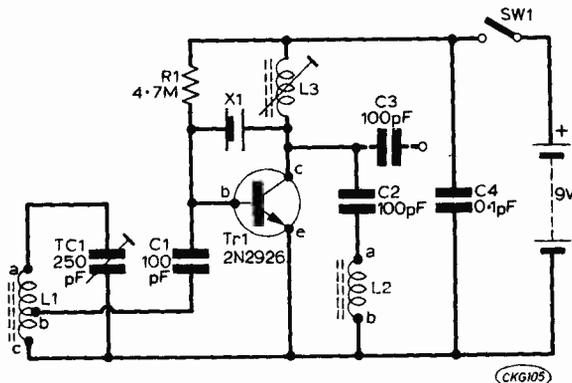
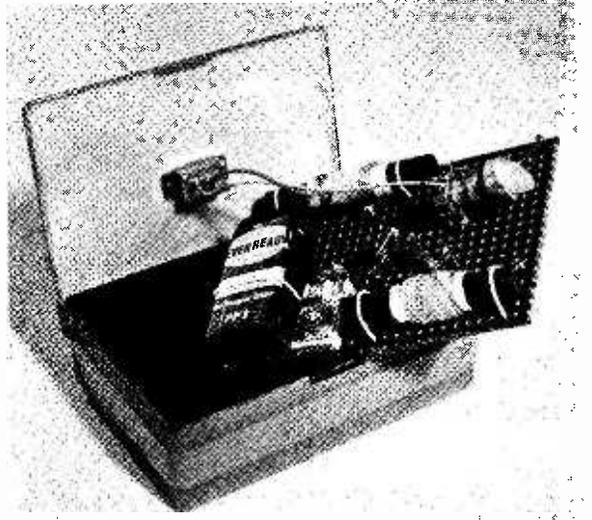


Fig. 1: The simple circuit of the Add-a-Verter. The output coil L2 is coupled to the ferrite rod aerial in the receiver, as shown in the heading photograph.



The only 'control' on the Add-a-Verter is the on-off switch!

was to peak trimmer TC1 for maximum strength of the Radio 2 signal.

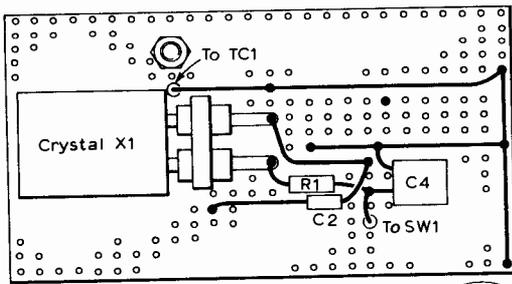
This particular type of crystal was originally used in equipment that multiplied its basic frequency fifty-four times so the crystal is designated as having an output frequency of 23.2 MHz which is shown on the crystal case as Channel 32. In fact its fundamental frequency is 429.630kHz. There is a whole range of similar crystals between about 370 and 540kHz. Some extremely useful tables showing the relationship between channel number, fundamental and output frequency can be found in the Radio Data Reference Book published by the RSGB.

To avoid interference with the converted Radio 2 signal from other stations on the medium wave band a search was made for a "quiet" spot at the l.f. end of the band but such a rarity disappeared a long time ago! The choice of the final frequency is therefore something of a compromise. What may seem a relatively quiet spot on the band in one part of the country may be alive with stations in another. However the Radio 2 signal appearing at the receiver was strong enough (in Surrey) to eliminate any other stations that can normally be heard at night on 629kHz. During the daytime there is no problem at all.

CONSTRUCTION

First obtain a plastic box, with lid, about 4x3in. with a minimum depth inside of about 1.4in. The inside dimensions of the box will determine the size of the board on which the Add-a-Verter is built. The box used in the prototype was 4.4x3x1.4in. so the following description and accompanying diagrams are based on this.

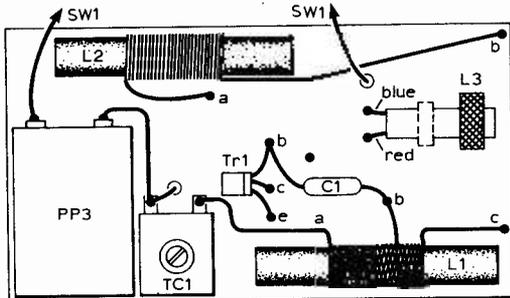
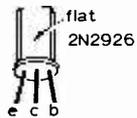
The important factors to be observed, regardless of



CKG106

▲ Fig. 2: Layout of the few components below the circuit board.

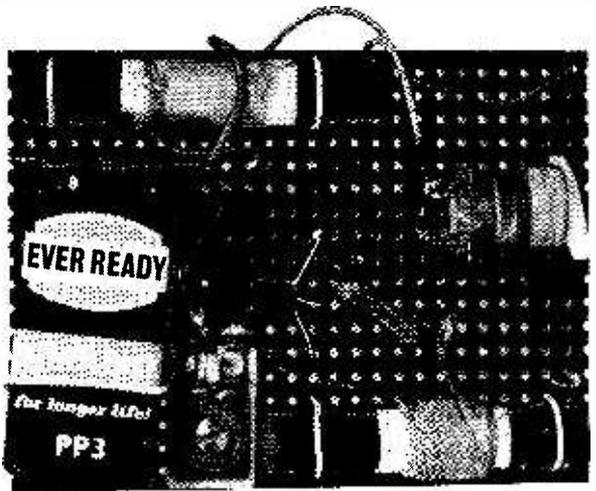
▼ Fig. 3: Component layout on top of the circuit board. Components are wired between Veroboard pins inserted in the board.



Board 4" x 2 3/4" but see text

● pins

CKG107



Top view of circuit board, which may be compared with Fig. 3

the size of the board, are maximum separation between L1 and L2 while keeping them parallel and horizontal and keeping L3 away from both L1 and L2 to minimise interaction.

Cut a piece of plain Veroboard to the size required and insert Veroboard pins as shown in Fig. 2. The use of copper strip board was considered unnecessary and a waste with so few components to be mounted. Coils L1 and L2 are part of a m.w./l.w. ferrite rod aerial although any similar rod aerial can be used.

First remove the coils from the rod and then cut off two pieces of the rod 2.4in. long. If space permits simply cut the rod in half. The cutting is best done by nicking the rod at the appropriate place with the sharp edge of a file. Either hold the rod in a vice and tap the free end or strike the rod smartly on the sharp edge of a table or bench. If the resulting ends are a bit rough, don't worry, it won't make any difference!

The connections to the coils L1 and L2 are shown in Fig. 4. L2 should have the few turns constituting the base winding removed although this is not strictly necessary provided the ends of this winding are not allowed to short together. If difficulty is experienced in identifying the windings connect an ohmmeter to

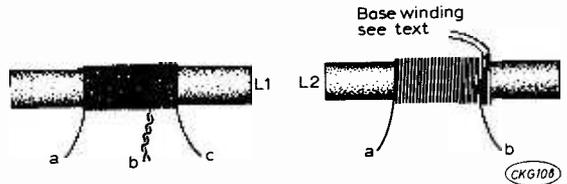


Fig. 4: Diagram of the lead-out wires of coils L1 and L2.

the single lead "a" and find the other end of the winding "b". The remaining ends will be the base winding.

Put the coils on the ferrite rods and attach the rods to the board with loops of thin insulated wire. Drill a hole and fix the compression trimmer TC1 to the board with the lock nut provided. Place the tags of the crystal holder over the appropriate pins on the underside of the board and solder, see Fig. 2. These pins provide anchoring points for the base and collector leads of the transistor on top of the board.

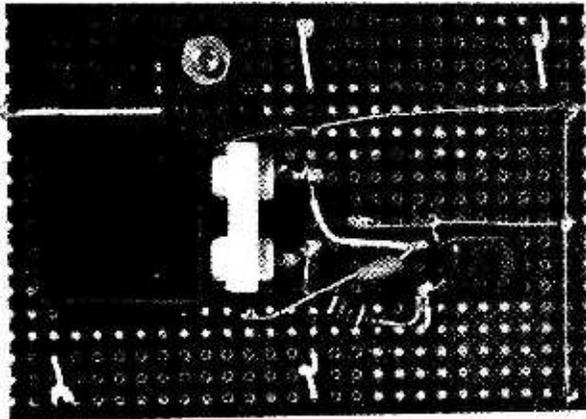
Coil L3 is the long wave winding of a l.w./m.w.

coil, freely available, and intended for use in a simple "crystal set" circuit. An iron core to suit the coil is required and should be bought at the same time as the coil since the core is not normally sold as part of the coil. In the prototype the red and blue tags of the l.w. winding were soldered directly to the appropriate pins in the board, Fig. 3, but if height permits mount the coil normally by its fixing lugs. Initially the core should be screwed in as far as possible.

Rather than cut off the excess of the coil lead-outs it is advisable to use the tinned ends as supplied, winding any surplus wire back on to the coil formers.

Complete the wiring in of the components as shown in Figs. 2 and 3 leaving the transistor until last. Hold the leads of the transistor in a pair of flat nosed pliers while tinning the ends and soldering them to their pins. Transistors are pretty tough these days but there is no point in tempting Fate!

Finally, attach the PP3 battery to the board with a wire loop as was done with the ferrite rods. The negative side of the battery clip goes to the general negative line while the positive side goes to the on-off switch, mounted on the lid of the box, and back to the positive side of the circuit. The current taken by the prototype was only 120 μ A so there was a temptation to omit the switch altogether! In this case the



Photograph of the underneath of the circuit board with connections as shown in Fig. 2.

working life of the battery would be about the same as its shelf life.

Plug in the crystal which should lie flat against the board but if necessary fix it to the board with another loop of wire.

SETTING UP

Put the board into the case where it should lie flat on the case of the crystal. No additional fixing was thought to be necessary. Connect a milliammeter in series with the positive battery lead. If using a multimeter set it to the maximum current range in case there are any short circuits! Switch on and if the crystal oscillates first time the current will be of the order of 120 μ A. If not the current will be about 200 μ A when the core of coil L3 should be unscrewed slowly the current dropping to a minimum and rising again. As a final check on the crystal, switch the unit on and off a few times. Each time the current should fall to around 120 μ A but if not readjust the core until it does. To be quite sure, remove the crystal, when the current should rise.

Switch on the portable radio and set the dial to

★ components list

- R1 4.7M Ω 1/4w
- C1 100pF
- C2 100pF
- C3 100pF (if required)
- C4 0.1 μ F 12VW
- TC1 250pF compression trimmer
- Tr1 2N2926 (orange, yellow or green coding)
- L1/L2 part of ferrite rod aerial (Type MW/LW/5FR Denco)
- L3 part of l.w./m.w. coil, with core (Type DRX1 Henrys)
- X1 crystal type FT241A, approx. 429kHz ("Channel 32-23-2MC", Henrys) and holder

Miscellaneous

- Miniature on/off switch, PP3.9V battery and clips.
- Veroboard 0.15in matrix or plain paxolin, 4 x 24in (see text). Plastic box.

around 480 metres on the medium wave band. Stand the Add-a-Verter close behind the radio so that the output coil is close to the ferrite rod aerial in the set and parallel to it. There is a fair chance that Radio 2 will now be audible but if not tune around 480m. on the set at the same time adjusting trimmer TC1 in the Add-a-Verter until Radio 2 is heard. Adjust the trimmer for maximum volume. To check, move the Add-a-Verter away from the set when the Radio 2 signal should disappear. For portability the Add-a-Verter can be attached to the radio with a couple of rubber bands.

Should the m.w. receiver not have ferrite rod aerial the Add-a-Verter can still be used by adding capacitor C3 from Tr1 to a terminal on the box and joining the terminal to the aerial socket on the receiver.

NOTES

Do not use a metal box since operation of the Add-a-Verter depends upon the coupling between coil L2 and the ferrite rod aerial in the receiver. A metal box will act as a screen preventing reception of Radio 2. A metal box is only permissible if L2 is mounted outside and at least 1/2in. clear of the metal box, but this is rather getting away from the original idea of the Add-a-Verter.

Don't forget that ferrite rod aerials are highly directional and that the set and Add-a-Verter must be orientated for maximum signal strength of Radio 2.

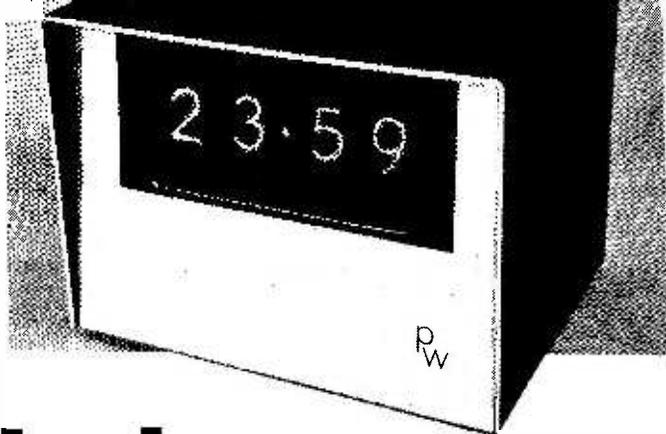
Switch off the Add-a-Verter when normal reception is required on the medium waves as otherwise interfering beat notes will be heard on stations.

Transistors type 2N2926 with orange, yellow and green coding were all tried and found satisfactory but difficulty may be experienced if the lower gain types, brown or red, are used. ■

BACK NUMBERS

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included in our 'CQ' section; there is no charge for this but it is a service between readers and P.W. are unable to meet any of these requests.

24 hour digital clock



J.G. MERCER

PART 2

NOTE:—In the Components List in Part 1 of the 24 Hour Digital Clock the reference number of the monolithic voltage regulator should have been shown as MVR5V and not MRV5V. The resistor marked R3 in Fig. 1 should have been shown as R4.

CONSTRUCTION

Construction commences with the assembly of four decade counter boards for the display module. First of all four holes should be drilled at the extreme corners of the boards in order to take the 6BA studding with which the display module is finally assembled, plus another below the edge connector, Fig. 7.

Each board has the component values and locations clearly marked together with the relevant notation for the edge connections. The resistor marked R1 on each of the P.C. boards corresponds to the R1's on the circuit diagram and has a value of 16kΩ for the recommended tube. Tinned copper wire should be used for all the links shown on the boards. The two types of integrated circuits should now be mounted on the boards paying especial attention that the indentations on the i.c.'s align with the marks on the P.C. board.

The numicator tube is now mounted with its leads straddling the board and viewing direction to the front. The pin connections for the tube are shown in Fig. 3 and the positions for these connections are clearly shown on the board itself.

All four boards are assembled in exactly the same way. Three of the four boards must now be slightly modified as shown in Fig. 6 (boards 2, 3 and 4). This modification is made to separate the two zero reset connections in order to be able to modify the counting sequence as described in the circuit operation.

The boards are now assembled on the studding as shown in Fig. 7 and spaced using extra 6BA

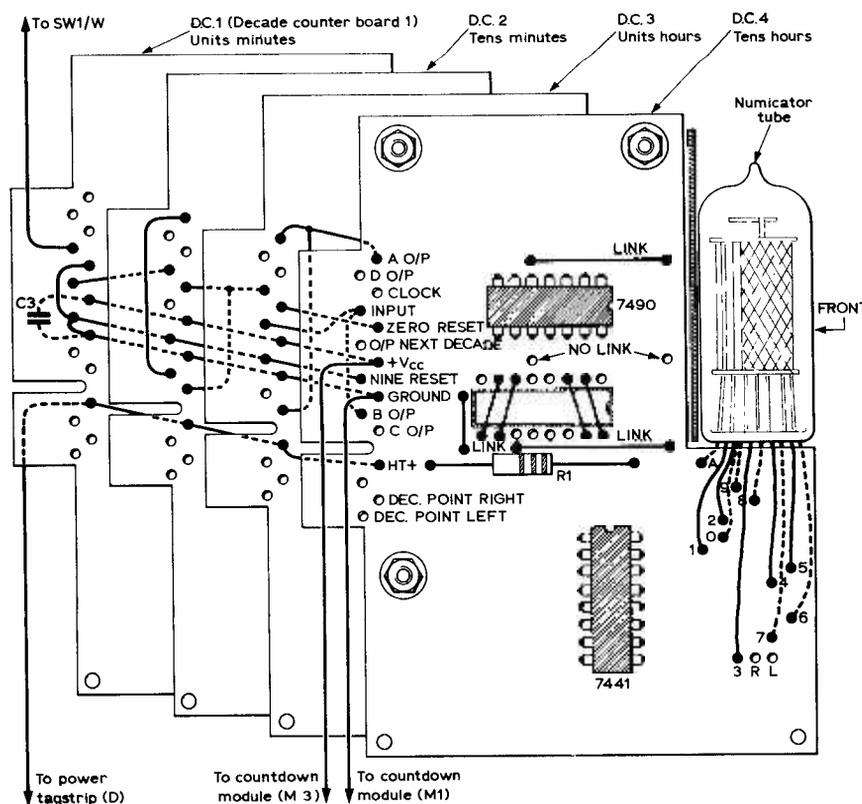
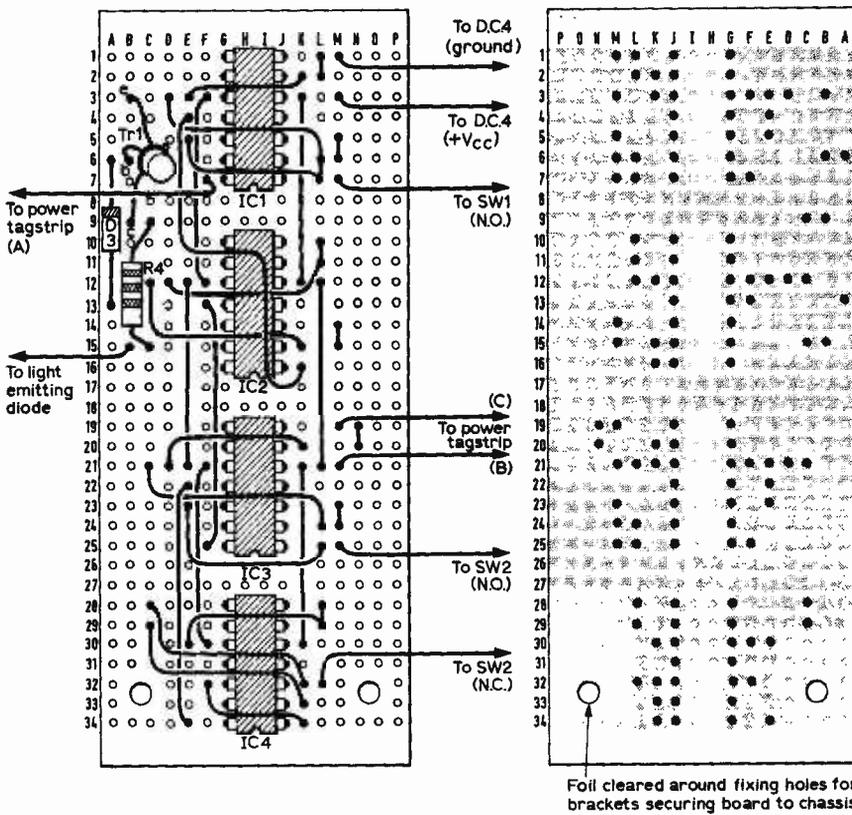
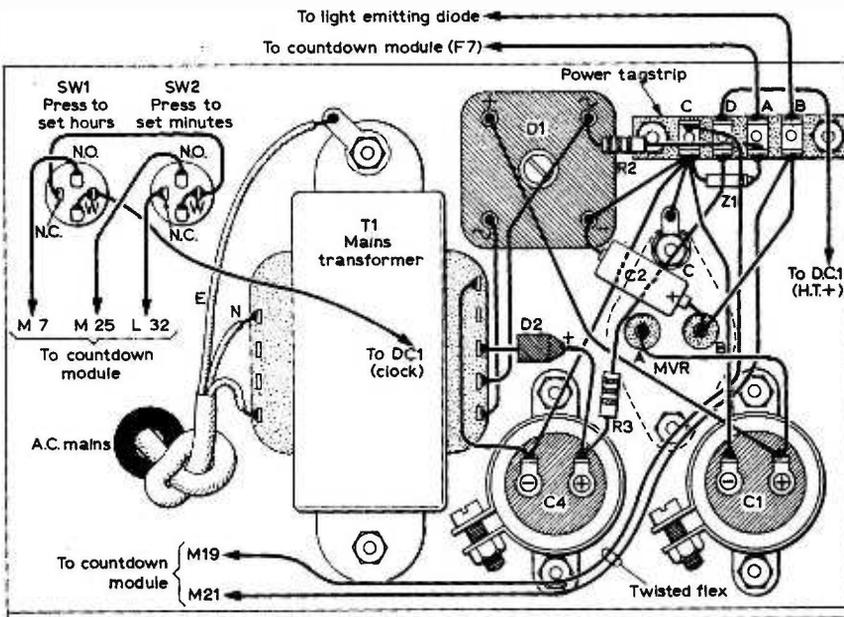


Fig. 7. Assembly and interconnecting wiring of the display module comprising the four decade counter boards.



▲ Fig. 8. Constructional details and wiring of the countdown board. Care must be taken to ensure that the copper strips are cleared from around the two fixing down brackets.

▼ Fig. 9. Layout of the power supply components and two reset switches on the back panel. The voltage regulator must be bolted directly on the back panel which acts as a heat sink.



nuts. Mounting feet are fitted to the P.C. boards—these can be seen in the photographs.

The interconnections at the rear of the boards are now made as shown in Fig. 7. Connections may be made with tinned copper wire through the holes in the edge connectors. Flying leads are connected for the input, +5V, chassis, and h.t. voltage. This completes the display module.

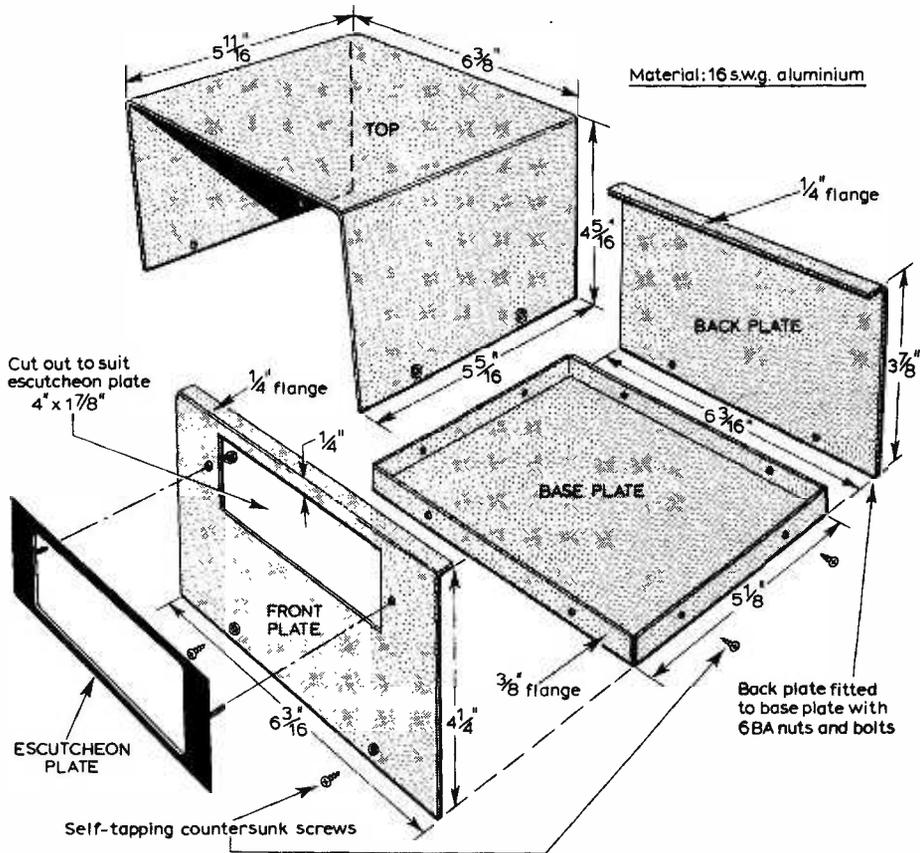
The countdown board is now assembled on a piece of 0.1in. matrix strip-board 3.4in. long by 1.4in. wide. The layout is exactly as shown in the circuit diagram, the only cuts to be made to the board are two complete lines along the length of the board between the rows of i.c. pins, Fig. 8.

All the chassis connections of the i.c.'s are commoned as are the 5V pins and flying leads added for connection to the power supply. Flying leads are also connected for the input, output and setting switches. This completes the countdown module.

The main chassis on which the power supply and other modules are mounted is simply an aluminium panel (18 s.w.g.) with an L cross section. The rear panel carries the setting switches and power supply while other modules are bolted to the base. The transformer is bolted to the rear panel as is the monolithic voltage regulator which uses the rear panel as its heat sink, Fig. 9.

The two large capacitors are also fixed to the rear panel with vertical fixing clips. The remaining power supply components may be soldered to the tags of the components already mentioned and the four outlets taken to a tag panel to permit easy connection to the other two modules.

The countdown board and display module are now bolted on to the basic chassis using angle



Dimensions and drilling details for the case and chassis which can be obtained as a kit. Note that the flanges on the base plate are uppermost. The backplate is $\frac{3}{8}$ in. shorter than the front plate thus leaving a slot along the back to provide essential ventilation. The metalwork shown in the various photographs of the Digital Clock was that used by the author in the prototype.

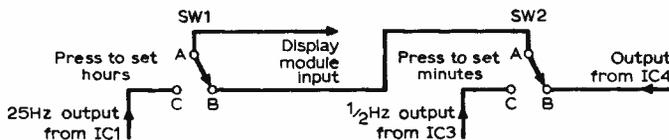
brackets and all the flying leads connected to the power supply and setting switches on the rear panel.

SETTING UP

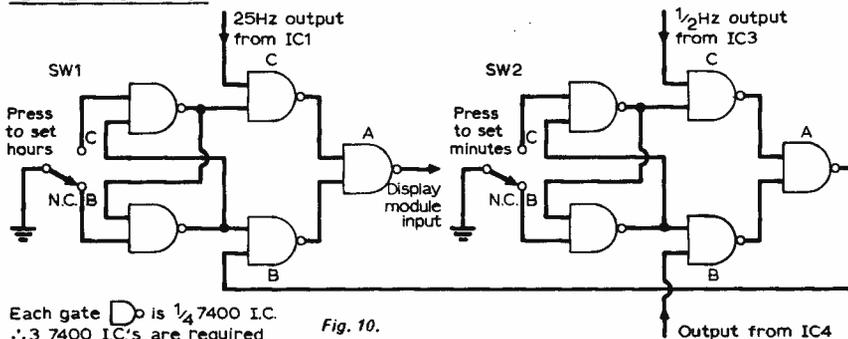
The initial setting of the clock to a particular time is carried out as follows:

SW1 is depressed to allow the clock to run at

PRESENT SETTING SYSTEM



NEW SETTING SYSTEM



Each gate \square is $\frac{1}{4}$ 7400 I.C.
 \therefore 3 7400 I.C.'s are required

Fig. 10.

1500 times normal speed and released at a displayed time at least half an hour before the required setting. SW2 is now depressed which allows the clock to run at a speed 30 times greater than normal. The button is released at the desired time setting. The clock will now run to an accuracy determined only by the accuracy at which the mains frequency is maintained. Resetting after a power cut or accidental disconnection may be carried out as described above.

In some cases and with some types of switches, contact bounce can cause overshoot on the initial setting. It is possible to use extra integrated circuits together with change-over switches to provide electrical rather than mechanical control of the initial setting. However, due to the fact that the clock will only infrequently need setting, the extra circuit complexity and expense was not considered justified. A circuit to overcome contact bounce is shown in Fig. 10.



IN NEXT MONTH'S

PRACTICAL WIRELESS

RECORD PLAYER 12W

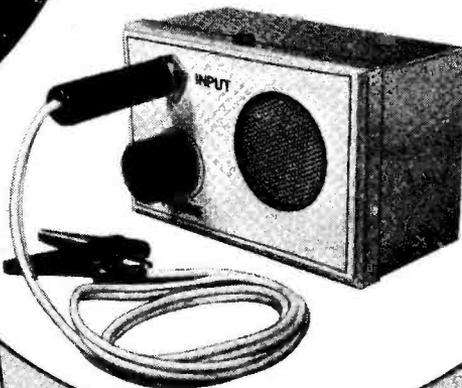
Judging by the feedback we get from readers, there are plenty of you who want details of a decent quality record player without the frills and expense of stereo: if you are one of these the *Estelle* is just for you. The quality is excellent with low distortion, full range tone controls and with a potential output of 12W r.m.s. Carefully thought-out design and construction add to the attractions of this project.

Estelle



TEST BENCH AMPLIFIER

Here's a good, simple, but handy project. A straightforward amplifier using four transistors with an output of about 200mW — just the job for trouble-shooting or for clipping onto a quick lash-up. As described it's a good, robust unit which takes only a few hours to complete.



MORE ON ELECTRONIC IGNITION PW SYSTEM

Last June we published a short article on the PW Electronic Ignition System, little realising the tremendous interest it would arouse. Thousands of these units have been built but many readers wrote in saying "I've got all the parts—what do I do next?" This follow-up article gives the answer to this question giving full circuit and constructional details.



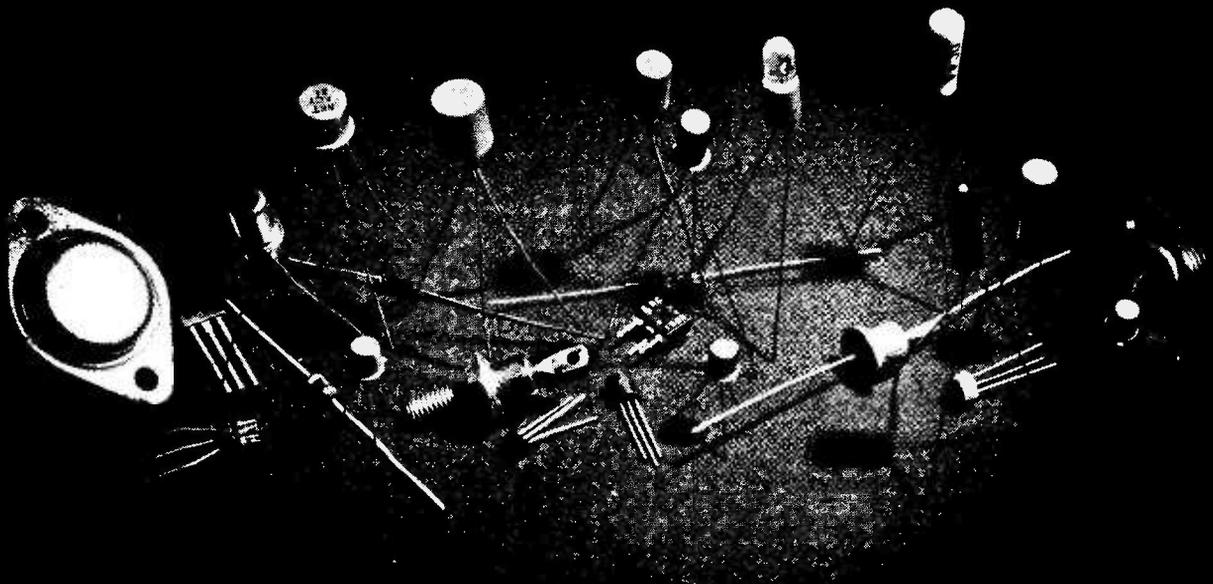
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semiconductor data

PRACTICAL WIRELESS SUPPLEMENT (MAY 1972)

PULL OUT



COMPILED FOR PRACTICAL WIRELESS BY D.A. LONGLAND, B.Sc., C. Eng., M.I.E.R.E. (ELECTROVALUE)

THIS SUPPLEMENT has been designed to present data to readers in a basic way. The technical details, parameters and capabilities of the more common types are given. The tables are broken down into categories by usage to simplify selection but of course many transistors could be included in several different headings. This has not been done as it would necessitate a considerable degree of duplication.

Transistors are used for many purposes, most of which may be reduced into the broad classification of increasing the power or level of a signal. This is effected by introducing the signal into the base-emitter (or gate-source circuit if a field effect transistor, f.e.t.) and thus causing an amplified variation of the signal in the collector-emitter circuit (or source drain circuit if an f.e.t.).

The important characteristics required of a transistor are determined by its application, that is, whether used for amplification of small a.c. or d.c. signals, for switching current or power amplification. Other characteristics may be important when a transistor is used near one of its limits, for example, high frequency, low noise, saturation, high power, very low current, or fast switching times.

Transistor characteristics

An ideal transistor will have a high transition frequency (f_T) and low feedback capacitance (for good high frequency response), stable characteristics, low noise level, low saturation voltage, fast rise and fall times (for low loss switching characteristics), high thermal conductivity (for high power handling capacity), low leakage (for ability to operate at very low currents), high gain (to reduce the number of stages for a given requirement) and low temperature effects (to reduce dependence on operating temperature and power dissipation).

It would be rare to find many extreme characteristics in one transistor for the technology used in producing an extreme in one characteristic may be incompatible with that used in producing an extreme in another. Hence, if a small signal, high frequency amplifier transistor were chosen it would have a medium gain at low currents, low feedback capacitance and high f_T , therefore it would be made on a small semiconductor chip. One would not therefore expect the same transistor to handle a high voltage, high power, or have a low saturation voltage at high current. This illustrates the need for com-

promise and in turn accounts for the large number of transistors available, many having their own individual collections of characteristics suited to particular applications.

In choosing a transistor, one has to start by determining the category in which the major characteristics fall, e.g. r.f. or a.f. amplification, switching, low or high power, high or low voltage, PNP or NPN. After choosing a range of transistors, the secondary characteristics may then be chosen.

1. In high frequency application, having chosen one with an f_T considerably higher than the operating frequency (if possible) and having a low feedback capacitance one would then seek a type having suitable voltage rating, power, dissipation, current or power gain, and if for switching, rise and fall time and saturation voltage.

2. For low frequency application, the f_T is relatively unimportant though with a high gain transistor, a transition frequency rather higher than the product of the current gain and highest frequency of operation should be sought: thus an amplifier using a transistor with an f_T of 1MHz and a current gain of 100 would be expected to fall in frequency response at 10kHz. A suitable voltage and power rating would then be chosen, keeping in mind any extremely low current or low saturation voltage characteristic required: thus an amplifier to operate at 1mA should have a collector-base leakage current rather less than 1mA divided by the desired maximum current gain of the transistor in order that the transistor will not saturate. A high gain transistor will give a higher input resistance than a low gain type, thus the high gain type would take less to drive power, but may cause a limitation in the frequency response.

3. For switching application it is desirable that the transistor conduct heavily with little voltage drop (i.e. low saturation voltage) when driven. For high speed switching the response time (i.e. rise, fall and storage) is important since the power dissipated in a slow transistor will be relatively high and may limit the power or frequency to be switched.

4. Other characteristics of a particular nature

may be sought, e.g. a given outline for incorporation into existing equipment, or ease of heat sinking (to reduce temperature rise if high power is to be dissipated), or high reverse base voltage for certain switching purposes, etc., etc. All must be considered in the design of equipment and in the selection of a suitable or substitute transistor.

The following tables are designed to assist in selection and substitution—it will be found that perhaps many transistors will serve one particular and non-demanding application whereas for another application only one or two will be found suitable. One factor to be considered is cost as it will be observed that a transistor which incorporates several special or extreme characteristics can be expensive. Good, common transistors which are relatively cheap and which will fulfil many needs are indicated by a dagger.

Dissipation in power transistors

Under the High Current Audio headings, the power dissipation is given in terms of thermal conductivity between junction and case in $mW/^\circ C$. There is some difficulty in expressing dissipation concisely as manufacturers are inclined to give dissipation ratings at different temperatures. It is felt that the thermal conductivity gives a more useful guide in the comparison between transistors.

In order to calculate the dissipation at a particular case temperature one must multiply the excess of maximum junction temperature above case temperature by the thermal conductivity. In some cases the manufacturer does not declare the dissipation at $25^\circ C$, therefore one should not assume that it would be safe to dissipate the maximum power as calculated above at $25^\circ C$ case temperature. One may assume it safe to operate at a case temperature midway between $25^\circ C$ and maximum junction temperature, this covering most practical requirements.

As a general guide, the maximum junction temperatures (which should not be exceeded by $20^\circ C$) are: Germanium (metal case) $90^\circ C$; Silicon (metal case) $200^\circ C$; Silicon (plastic case) $150^\circ C$ for types 2N-, MJE-, TIP- and $125^\circ C$ for types BD-.

Abbreviations			
†	Inexpensive types	Ib	Base current.
t	Typical.	Ic	Collector current.
max	Maximum.	Icbo	Collector-base current with emitter open-circuit.
min	Minimum.	NF	Noise factor.
Cob	Maximum common-base output capacitance.	PG	Power gain.
f	fhfb, Frequency at which the common-base current is reduced by 3dB.	Vcbo	Collector-base voltage with emitter open-circuit.
fT	Frequency at which the common-emitter current gain is unity.	Vce	Collector-emitter voltage.
hFE	Large signal current gain.	Vce(sat)	Collector-emitter voltage for saturated (fully conducting) operation.
hfe	Small signal current gain.	Veb	Base-emitter reverse voltage.
		*	Under Ic/Ib. These refer to Ic with the collector and base shorted.

GERMANIUM TRANSISTORS

R.F. Applications, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA @	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
NKT613F	40	40	1	10	80	*40 min	1	5			75t	2		14	100	TO7
AF114	20	20		10	60	*130t	1	8			75t	2.5		12.5	100	TO7
AF115	20	20		10	60	*130t	1	8			75t			10	100	TO7
AF116	20	20		10	60	*130t	1	8			75t			19	10.7	TO7
AF117	20	20		10	60	*130t	1	8			75t			40	0.45	TO7
AF118	70	70	1	30	375	*180t	1	6			175	2.3				TO7
AF124	20	20		10	60	*130t	1	8			75t	2.5		12.5	100	TO72b
AF125	20	20		10	60	*130t	1	8			75t			10	100	TO72b
AF126	20	20		10	60	*130t	1	8			75t			19	10.7	TO72b
AF127†	20	20		10	60	*130t	1	8			75t			40	0.45	TO72b
AF139	20	15	0.3	10	60	50t	1	8			500t			10	800	TO72a
AF201	25		0.3	10	225	50t	1	10								TO72b
AF239†	20	15	0.3	10	60	50t	1	8			700			14	800	TO72a
OC44	15		12	10	75	40-225	2	2			7.5f					TO1,RO9
OC45	15		12	10	75	25-125	2	2			9f					TO1,RO9

Low Noise, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA @	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
AC107	15	15	5	10	80	60t	0.3	13			0.3f	14	5			TO1,RO9
AC126	32	12	10	100	220	*130-300	2	10			2.3		10			TO1
AC151R†	32	24	10	200	150	80t	2	100			1.5	27				TO1

Small Signal Audio, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA @	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
NKT213	32	32	10	250	200	50-130	1	10	0.2	25/2.5	0.9f	60				TO1
NKT214†	32	32	10	250	200	*30-75	1	10	0.2	25/2.5	0.9f	60	10			TO1
NKT274†	15	15	5	250	200	*85-250	1	10			1		15			TO1
NKT275	15	15	5	250	200	*30-90	1	10			1		10			TO1
OC71	30	20	10	10	125	30-75	3	13			0.3f		16			TO1,RO9

Medium Current Audio, Small Output Types, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA @	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
AC128†	32	16	10	1000	220	40-110	300	10			1.5	100				TO1
AC142H	50	30	10	1200	220	40-110	400	14			1.2					TO1
AC142HK	50	30	10	1200	860	40-110	400	14			1.2					X9a
AC153	32	18	10	2000	220	50-250	300	200			1.5					TO1
AC153K†	32	18	10	2000	1000	50-250	300	200			1.5					X9a
NKT211†	32	30	10	1000	200	20-150	300	10	0.5	300/30	0.9f	60				TO1
NKT212	32	32	10	500	200	50-150	50	10	0.15	25/2.5	0.9f					TO1
NKT217	60	40	10	500	200	50-150	25	10	0.5	300/6	0.9f	80				TO1
NKT271	15	15	5	500	200	50-250	50	10			1f					TO1
OC72	32	32	10	250	125	30-90	80	15	0.25	125/12.5	1					TO1,RO9
OC81	32	32	10	500	240	50-250	50	10			1f					TO1
OC83	32	20	3	500	220	50-280	50	100	0.5	300/9	0.85					TO1
OC84†	32	20	10	500	220	60-200	50	100	0.5	300/9	0.85					TO1

GERMANIUM TRANSISTORS CONTINUED

Medium Current Audio, Small Output Types, NPN

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
AC127†	32	32	10	500	200	25-143	500	10	1	500/50	1.5					TO1
AC141H	50	25	10	1200	220	40-110	400	14	0.55	400*	3					TO1
AC141HK	50	25	10	1200	860	40-110	400	14	0.55	400*	3					X9a
AC176	32	20	5	300	220	52-180	500	100	0.6	500/10	1					TO1
AC176K†	32	20	5	300	1000	52-180	500	100	0.6	500/10	1					X9a
NKT713	30	30	15	500	150	50-150	50	15	0.15	50/5	1f					TO1
NKT773	15	15	5	300	150	50-150	50	15								TO1

High Current Audio, Power Output Types, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
AD140	55		10	3A	666	30-100	1000	100								TO3
AD142	80	50	10	10A	666	30-170	1000	5000	0.3	5000/250	0.45					TO3
AD149†	50	30	20	3.5A	500	30-100	1000	350			0.5					TO3
AD162†	32	20	10	1A	222	80-320	500	40			1					MD17c
AL102	130	60	2	6A	666	40-250	1000	1000	0.5	5000/250	4					TO3
NKT403†	80	32	40	10A	770	50-150	1000	150	0.42	1000/100	0.35					TO3
NKT405	60	32	20	5A	770	100-200	1000	150	0.42	1000/100	0.35					TO3
OC25	40	40	10	4A	500	15-80	1000	100								TO3
OC28	80	60	40	8A	666	20-55	1000	100	1.6	6000*	0.25f					TO3
OC29†	60	48	20	8A	666	45-130	1000	100	1.6	6000*	0.25f					TO3
OC35	60	48	20	8A	666	25-75	1000	100	1.4	6000*	0.25f					TO3
OC36	80	60	40	8A	666	30-110	1000	100	1.6	6000*	0.25f					TO3
2N2147	75	50	1.5	5A	666	100 min	1000	1000	0.6	5000/250	3					TO3

High Current Audio, Power Output Types, NPN

AD161†	32	20	10	1A	222	80-320	500	50			1					MD17c
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See note on power dissipation

Medium Current Switching, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
ACY17	70	32	12	500	260	50-150	300	10	0.3	300/15	1					TO5
ACY18	50	30	12	500	260	40-120	300	10	0.3	300/15	1					TO5
ACY19	50	30	12	500	260	80-250	300	10	0.3	300/15	1.5					TO5
ACY20	40	20	12	500	260	50-145	50	10	0.2	50/1.3	1					TO5
ACY21	40	20	12	500	260	90-250	50	10	0.2	50/1.3	1					TO5
ACY22	20	15	12	500	260	30-300	300	10	0.3	300/15	0.8					TO5
ACY39	110	40	12	500	260	50-150	300	10	0.3	300/15	1					TO5
2N1303	30	25	25	200	150	20 min	10	6	0.2	10/0.5	5	20				TO5
2N1305†	30	20	25	200	150	40-200	10	6	0.2	10/0.25	10	20				TO5
2N1307	30	15	25	200	150	60-300	10	6	0.2	10/0.17	15	20				TO5
2N1309	30	15	25	200	150	80 min	10	6	0.2	10/0.13	20	20				TO5
ASY26	30	15	20	300	150	30-80	20	7	0.25	50/2	8	15				TO5
ASY27	25	15	20	300	150	50-150	20	7	0.25	50/1.55	14	16				TO5

Medium Current Switching, NPN

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cb0} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
ASY28	30	15	20	200	150	30-80	20	35	0.25	50/2	14	16				TO5
ASY29	25	15	20	200	150	50-150	20	35	0.25	50/1.25	20	16				TO5
2N1302	25	25	25	200	150	20 min.	10	6	0.2	10/0.5	10	20				TO5
2N1304†	25	20	25	200	150	40-200	10	6	0.2	10/0.25	15	20				TO5
2N1306	25	15	25	200	150	60-300	10	6	0.2	10/0.17	20	20				TO5
2N1308	25	15	25	200	150	80 min.	10	6	0.2	10/0.13	30	20				TO5

GERMANIUM/SILICON TRANSISTORS

High Current Switching, PNP

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c max	P _{tot} max	h _{FE} *h _{fe}	I _c mA	I _{cbo} μA	V _{ce} (sat)	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
AU111	320		2	10A		15-80	6000		0.5	5000/250	2					TO3

The term switching above does not imply any discontinuity in the characteristics. Such transistors may be used as amplifiers, as may amplifier transistors be used for switching duty if their characteristics are suitable.

SILICON TRANSISTORS

R.F. Applications, NPN

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA (a)	I _{cbo} μA	V _{ce} (sat) (a)	I _c /I _b mA (a)	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BF115	50	30	5	30	145	100t	3				230t		4			TO72b
BF187	40	30	4	25	130	50t	4				350t		3.5			TO72b
BF173†	40	25	4	25	260	87t	7				550t					TO72b
BF194†	30	20	5	30	220	115t	1				260t		4			MM10b
BF195	30	20	5	30	220	67t	1				200t		4			MM10b
BF254†	30	20	5	30	220	115t	1				260t		4			TO92z
BF255	30	20	5	30	220	67t	1				200t		4			TO92z
BFY90	30	15	2.5	50	200	60t	2				1000	1.8	5	22t	500	TO72a
2N3663	30	12	3	25	200	75t	8	0.5			1250t	1.7	6.5	15	200	TO98
2N4292†	30	15	3	500	200	20 min	3	0.5			570t	2.2	6	29t	100	U29

Small Signal Audio, PNP

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA (a)	I _{cbo} μA	V _{ce} (sat) (a)	I _c /I _b mA (a)	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BC157†	50	45	6	100	220	*125-250	2	0.05	0.2t	100/5	130t					MM10a
BC158	30	20	5	100	220	*125-500	2	0.1	0.2t	100/5	130t					MM10a
BC177†	45	45	5	100	300	*125-260	2	0.05	0.2t	100/5	130t	4				TO18
BC178	20	20	5	100	300	*125-500	2	0.1	0.2t	100/5	130t	4				TO18
BC186	40	25	5	100	300	40 min	2				60	5				TO18
BC212L	60	50	5	100	360	60-300	2	0.015	0.2	10/0.5	200	10				TO92a
BC213L	45	30	5	100	360	80-400	2	0.015	0.2	10/0.5	200	10				TO92a
BC257†	50	45	5	100	220	*125-260	2	0.1	0.5	100/5	130t	6				TO92a
BC258	30	25	5	100	220	*125-500	2	0.1	0.5	100/5	130t	6				TO92a
BCY70	50	40	5	200	350	50 min.	10	0.01	0.25	10/1	250					TO18
BCY72	25	25	5	200	350	50 min.	10	0.1	0.25	10/1	200					TO18
ZTX500	25	25	5	500	300	50-300	10	0.2	0.35	50/5	150	6				X59
ZTX501	35	35	5	500	300	50-300	10	0.2	0.25	50/5	150	6				X59
ZTX502	35	35	5	500	300	100-300	10	0.2	0.25	50/5	150	6				X59
ZTX503	45	45	5	500	300	50-300	10	0.2	0.35	50/5	150	6				X59
ZTX504	70	70	5	500	300	50-300	10	0.2	0.35	50/5	150	6				X59
ZTX530	30	30	5	500	250	100-400	0.1	0.2	0.7	10/0.5	30	8				X59
ZTX531	45	45	5	500	250	40-120	0.01	0.2	0.7	10/0.5	30	8				X59
2N3906	40	40	5	200	310	100-300	10	0.05	0.25	10/1	250	4.5				TO92b
2N4126	25	25	4	200	310	120-360	2	0.05	0.4	50/5	250	4.5				TO92b
2N4059	30	30	6	30	250	45-660	1		0.7	10/0.5						TO92a
2N4060	30	30	6	30	250	45-185	1		0.7	10/0.5						TO92a
2N4061	30	30	6	30	250	90-330	1		0.7	10/0.5						TO92a
2N4062	30	30	6	30	250	180-660	1		0.7	10/0.5						TO92a
2N4289	60	45	7	500	250	160 min.	1	0.01	0.35	1/0.1	170t	8				U29

SILICON TRANSISTORS CONTINUED

Small Signal, Audio, NPN

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{FE}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
BC107†	45	45	5	100	300	*125-500	2	0-01	0.25	10/0-25	150	3-7	10			TO18
BC108	20	20	5	100	300	*125-900	2	0-01	0.25	10/0-5	150	3-7	10			TO18
BC147†	50	45	6	200	220	*125-500	2	0-02	0.25	10/0-5	300t	2-5	10			MM10a
BC148	30	20	5	100	300	*125-900	2	0-25	0.25	10/0-5	300t	2-5	10			TO92a
BC167†	50	45	6	100	300	*125-500	2	0-2	0.25	10/0-5	300t		10			TO92a
BC168	30	20	5	100	300	*125-900	2	0-2	0.25	10/0-5	300t		10			TO92a
BC182L	60	50	5	200	300	100-480	2	0-015			150	5				TO92a
BC183L	45	30	5	200	300	100-850	2	0-015			150	5				TO92a
BC267	50	45	6	1000	375	*125-500	2	0-015	0-22t	200/10	150		3t			TO18
BC268	30	20	6	1000	375	*125-900	2	0-015	0-22t	200/10	150		3t			TO18
ZTX300	25	25	5	500	300	50-300	10	0-2	0-35	50/5	150	6				X59
ZTX301	35	35	5	500	300	50-300	10	0-2	0-25	50/5	150	6				X59
ZTX302	35	35	5	500	300	100-300	10	0-2	0-25	50/5	150	6				X59
ZTX303	45	45	5	500	300	50-300	10	0-2	0-35	50/5	150	6				X59
ZTX304	70	70	5	500	300	50-300	10	0-2	0-35	50/5	150	6				X59
ZTX330	30	30	5	500	250	100-400	10	0-2	0-7	10/0-5	30	8				X59
ZTX331	45	45	5	500	250	40-120	10	0-2	0-7	10/0-5	30	8				X59
2N2924	25	25	5	100	200	*150-300	2	0-5			120t	12	2-5t			TO98
2N2925	25	25	5	100	200	*235-470	2	0-5			120t	12	2-5t			TO98
2N2926B	18	18	5	100	200	*35-70	2	0-5			120t	12	2-5t			TO98
2N2926R	18	18	5	100	200	*55-110	2	0-5			120t	12	2-5t			TO98
2N2926O	18	18	5	100	200	*90-180	2	0-5			120t	12	2-5t			TO98
2N2926Y†	18	18	5	100	200	*150-300	2	0-5			120t	12	2-5t			TO98
2N2926G†	18	18	5	100	200	*235-470	2	0-5			120t	12	2-5t			TO98
2N3708	30	30	6	30	250	45-660	1	0-1	1	10/0-5						TO92a
2N3709	30	30	6	30	250	45-165	1	0-1	1	10/0-5						TO92a
2N3710	30	30	6	30	250	90-330	1	0-1	1	10/0-5						TO92a
2N3711	30	30	6	30	250	180-660	1	0-1	1	10/0-5						TO92a
2N3904	60	40	5	100	310	100-300	10	0-1	0-2	10/1	200t	4				TO92b
2N4124	30	25	5	200	310	120-360	2	0-05	0-3	50/5	300	4				TO92b
2N4286†	30	25	6	500	250	100 min	0-1	0-05			280t	6				U29
2N5172	25	25	5	100	200	*100-750	10	0-1	0-25	10/1	120t	10				TO98

Low Noise, NPN

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{FE}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
BC109B†	20	20	5	100	300	*240-500	2	0-015	0-25	10/0-25	300t		4			TO18
BC109C†	20	20	5	100	300	*450-900	2	0-015	0-25	10/0-25	300t		4			TO18
BC149†	30	30	5	200	220	*240-900	2	0-02	0-25	10/0-25	300t		4			MM10a
BC169†	30	30	5	100	300	*240-900	2	0-02	0-25	10/0-25	300t		4			TO92a
BC184L	45	30	5	200	300	250min	2	0-015			150		4			TO92a
BC269	30	20	6	1000	375	*240-900	2	0-015	0-22t	200/10	150		4			TO18
2N930†	45	45	5	60	300	100-300	0-01	0-01			80t	8	3			TO18
2N2483	60	60	6	50	360	*40-120	0-01	0-01			60	6	4			TO18
2N2484	60	60	6	50	350	*100-500	0-01	0-01			60	6	3			TO18
2N3707	30	30	6	30	250	*100-400	0-1	0-1					5			TO92a
2N5088	35	30	3	50	310	*300-900	0-1	0-05			50	4	3			TO92b

Low Noise, PNP

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{FE}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz @	Base
BC153	40	40	5	100	200	50-135	0-1	0-002	0-25	10/0-5	40	6	2-5			RO97a
BC154†	40	40	5	100	200	160-330	0-1	0-002	0-25	10/0-5	40	6	2-5			RO97a
BC159†	30	20	5	100	200	*125-500	2	0-05	0-3t	100/5	200t	5	4			MM10a
BC179†	20	20	5	100	300	*125-900	2	0-05	0-3t	100/5	200t	4	4			TO18
BC214L	45	30	5	100	360	140-400	2	0-015	0-2	10/0-5	200	10	2			TO92a
BC259†	25	20	5	100	220	120-460	2	0-1	0-8	10/0-5	130	6	4			TO92a
BCY71	45	45	5	200	350	100 min	10	0-01	0-25	10/1	300					TO18
2N4058	30	30	6	30	250	100-400	0-1	0-1	0-7	10/1			5			TO92a

SILICON TRANSISTORS CONTINUED

Medium Current Audio, Small Output Types, NPN

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BC125	50	30	5		300	30 min	150	0.05	0.5	150/15	40	12				RO97
BC140-10	80	40	7	1000	750	20 min	1000	0.1	1	1A/100	50	25				TO5
BC301	90	60	7	1000	850	40-240	150	0.02	0.5	150/15	120t					TO5
BFX84†	100	60	6	1000	800	30 min	150	0.05	0.35	150/15	50					TO5
BFX85	100	60	6	1000	800	70 min	150	0.05	0.35	150/15	50					TO5
BFY50	80	35	6	1000	800	30 min	150	0.05	0.2	150/15	60					TO5
BFY51†	80	30	6	1000	800	40 min	150	0.05	0.35	150/15	50					TO5
BFY52	40	40	6	1000	800	60 min	150	0.5	0.35	150/15	150					TO5
MC140	80	40	7	1000	800	40-300	150	0.5	0.71	1A/100	100					X58b
2N696	60	40	5	500	600	20-60	150	1	1.5	150/15	40	35				TO5
2N697	60	40	5	500	600	40-120	150	1	1.5	150/15	50	35				TO5
2N1613	75		7	500	800	40-120	150	0.01	1.5	150/15	60	25				TO5
2N1711	75	30	7	1000	800	100-300	150	0.01	1.5	150/15	70	25				TO5
2N2270	60	45	7	1000	1000	50-200	150	0.05	0.9	150/15	60					TO5
2N3053†	60	40	5	700	1000	50-150	150	0.25	1.4	150/15	100					TO5
2N3704†	50	30	5	800	300	90-330	50		0.8	100/5	100	12				TO92a
2N3705	50	30	5	800	300	45-165	50		0.8	100/5	100	12				TO92a
2N3706	40	20	5	800	300	30-660	50		1.6	100/5	100	12				TO92a
2N3794	40	20	5	300	250	100 min	100	0.5	0.4	10/1	100	10				U29
40361†	70	70	4	700	1000	70-350	50	0.25	1.4	150/15	100					TO5
40412	250			1000	1000	40 min	30				10					TO5

Medium Current Audio, Small Output Types, PNP

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BC126	35	30	5	600	300	30-120	150	0.05	0.5	150/15	200t	5				RO97
BC160-10	40	40	5	1000	750	63 min	100	0.1			100t	20				TO5
BC303	90	65	7	1000	1000	40 min	150	0.02	0.65	150/15	60					TO5
BFX29†	60	60	5	800	500	50-200	10	0.075	0.4	150/15	100	12				TO5
BFX87	50	50	4	600	600	40 min	10	0.05	0.4	150/15	100	12				TO5
BFX88†	40	40	4	600	600	40 min	10	0.05	0.4	150/15	100	12				TO5
2N1131	50	35	5	600	600	20-45	150	1	1.5	150/15	50	45				TO5
2N1132	60	40	5	600	600	30-90	150	1	1.5	150/15	60	45				TO5
2N3702†	40	25	5	200	200	60-330	50	0.1	0.25	50/5	100	12				TO92a
2N3703	50	30	5	200	200	30-150	50	0.1	0.25	50/5	100	12				TO92a
2N4036	90	65	7	1000	1000	40-140	150	0.1	0.65	150/15	60					TO5
2N4291	40	30	6	500	250	100-300	100	0.5	0.4	100/10	150t	10				U29
40362†	70		4	700	1000	35-200	50		1.4	150/15	100t					TO5

High Current Audio, NPN

Type	V _{cb0} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	h _{FE} *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BD121	60	35	6	5A	303	30-100	1.5A	50	0.65	1A/100	95t					TO3
BD123	90	60	6	5A	303	30-100	1.5A	50	0.65	1A/100	85t					TO3
BD124	70	45	6	4A	133	30-150	500	2	0.25	500/50	60					MD17c
BD130†	100	60	7	15A	666	20-70	4A	5000	1.1	4A/400	1.1t					TO3
BD131†	70	45	6	4A	167	30-75	500				60					X58
BD135†	45	45	5	1.5A	100	40-100	150	0.1	0.6	500/50	50					X58
BD141	140	120	7	8A	666	20-70	2A		1	2A/200						TO3
BDY20	100	60	5	15A		20-100	4A		1.1	4A/400						TO3
MJ481†	60	60	5	4A	500	30-200	1A	1000	0.4	1A/100	4					TO3
MJE521	40	40	4	3A	320	40 min	1A				1					X58
MJE3055	70	60	5	10A	718	20-70	4A	1000	1.1	4A/400	2					X58c
TIP31A	60	60	5	3A	320	20-100	1A	500			3					X75b
2N3054	90	55	7	4A	142	25-250	500	1000	1	500/50	0.75					TO66
2N3055†	100	60	7	15A	660	20-70	4A	5000	1.1	4A/400	0.4					TO3
2N4915	80	80	5	5A	500	25-100	2.5A	100	1	2.5A/250	4					TO3
2N5192	80	80	5	4A	320	20-80	1.5A	100	0.8	1.5A/150	2					X58
40250	50	40	5	4A	166	20-100	1.5A	1000	1.5	1.5A/150	1.2t					TO66
40251	50	40	7	15A	666	15-60	8A	5000	1.5	8A/800	0.5t					TO3

SILICON TRANSISTORS CONTINUED

High Current Audio, PNP

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c max	P _{tot} max	hFE *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BD132†	45	45	4	2A	167	35-75	500	0.1	0.6	500/50	60					X58
BD136†	45	45	5	1.5A	100	40-100	150	1000	0.4	1A/100	50					X58
MJ491†	60	60	5	4A	500	30-200	1A				4					TO3
MJE371	40	40	4	3A	320	40 min	1A									X58
MJE2955	70	60	5	10A	718	20-70	4A	1000	1.1	4A/400	2					X58c
TJP32A	60	60	5	3A	320	20-100	1A	500			3					X75b
2N4906	80	80	5	5A	500	25-100	2.5A	100	1	2.5A/250	4					TO3
2N5195	80	80	5	4A	320	20-80	1.5A	100	1.4	1.5A/150	2					X58

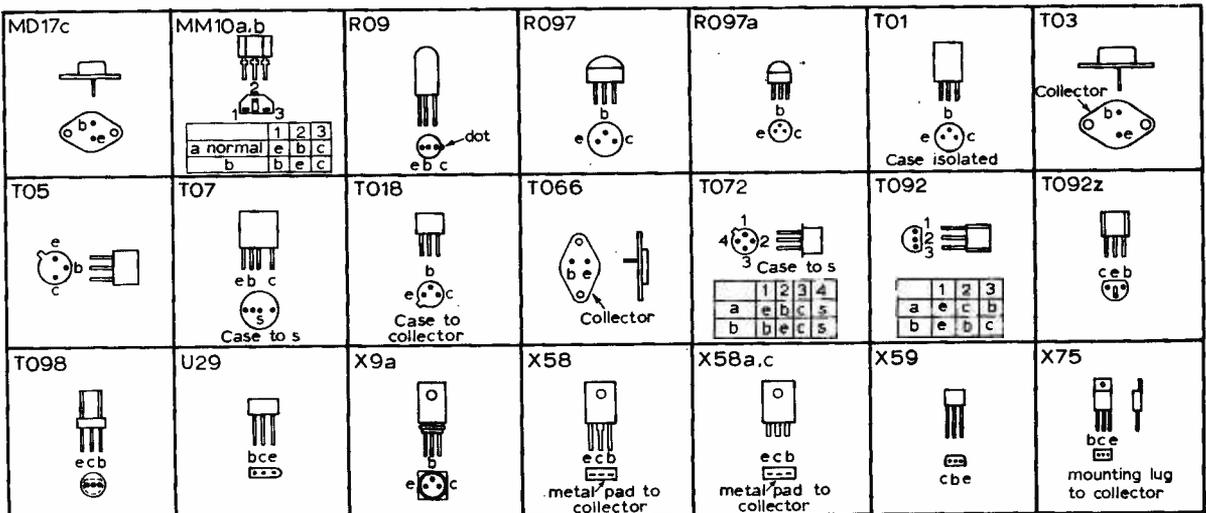
See notes on power dissipation.

Medium Current Switching, NPN

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	hFE *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
BSX20†	40	15	4.5	500	360	40-120	10	0.4	0.6	100/10	600					TO18
C762†	40	25	5	150	400	30-110	50	0.2	0.6	150/15	350	5				TO18
MPS6531	60	40	5	600	310	90-270	100	0.05	0.3	100/10	390†	3-5				TO92b
P346A	25	12	3	300	300	20 min	10	0.05	1	100/1	400	4				TO18
2N706	25	20	3	200	300	20 min	10	0.05	0.6	10/1	200	6				TO18
2N706A	25	15	5	300	300	20-40	10	10			200	3-5				TO18
2N2218	60	30	5	800	800	40-120	150	0.01	1.6	500/50	250	8				TO5
2N2218A	75	40	6	800	800	40-120	150	0.01	1	500/50	250	8				TO5
2N2219	60	30	5	800	800	100-300	150	0.01	1.6	500/50	250	8				TO5
2N2219A	75	40	6	800	800	100-300	150	0.01	1	500/50	250	8				TO5

Medium Current Switching, PNP

Type	V _{cbo} max	V _{ce} max	V _{eb} max	I _c mA max	P _{tot} max	hFE *h _{fe}	I _c mA @	I _{cbo} μA	V _{ce} (sat) @	I _c /I _b mA	f _T MHz	C _{ob} pF	NF dB max	PG dB @	MHz	Base
MPS6534	40	40	4	600	310	90-270	100	0.15	0.3	100/10	250	6				TO92b
V763†	25	25	5	400	400	30 min	50	0.05	1	150/15	300	6				TO18
2N2904	60	40	5	600	600	40-120	150	0.02	0.4	150/15	200	8				TO5
2N2904A	60	60	5	600	600	40-120	150	0.01	0.4	150/15	200	8				TO5
2N2905	60	40	5	600	600	100-300	150	0.02	0.4	150/15	200	8				TO5
2N2905A	60	60	5	600	600	100-300	150	0.01	0.4	150/15	200	8				TO5





The
TEXAN

20+20 WATT I.C. ST

IT is an unwritten law of electronics that whenever a group of engineers are gathered together then sooner or later a HiFi amplifier will be designed. Usually they, the amplifiers, that is, are assembled in such a way that even if they work well at the time they are quite impossible to reproduce.

The Texan is mainly a 'value-for-money' design which the average home constructor, armed with little more than a soldering iron, should be able to build successfully in a time which will allow him to remain on speaking terms with his wife.

The original design was produced for a house-publication* and was intended to promote the use of integrated circuit operational amplifiers for audio use. Also, since I have an aversion to printed-circuit boards bristling with capacitors—particularly electrolytics—it was designed to reduce these to an absolute minimum.

The present circuit is updated to use the latest devices and it includes extra facilities such as scratch and rumble filters.

The printed circuit board has also been completely changed so that most of the controls are mounted directly and very little spaghetti wiring is required.

Why use operational amplifiers?

By definition the main function of a preamplifier is to provide gain and to do it in a way which is well controlled with respect to frequency response and stability.

If someone made a transistor with a potential voltage gain 200,000, an f_T of 2MHz, a maximum phase shift of 90° , differential inputs with high common mode rejection and so on and so forth there would be little point in using an operational amplifier, but to the best of my knowledge they do not. However, operational amplifiers are now so easy to use that they can be treated simply as a transistor with eight legs.

More explicitly the operational amplifier has the following features:

- (1) A very high mid-band gain which allows accurate equalization while retaining sufficient loop gain to reduce distortion to very low levels.
- (2) Inherently high input impedance and low output impedance which make feedback networks simple to design and minimise the effect of loading.
- (3) Large potential output swing giving good overload ability.
- (4) Balanced design with d.c. coupling and very low offset voltages. This greatly reduces the number of electrolytic capacitors required in the amplifier and allows the output to operate without the need for manual setting up of the d.c. output conditions.
- (5) High supply ripple voltage rejection which means that the operational amplifiers will work on poorly regulated supplies and reduces the likelihood of low frequency instability, one of the most common faults in many amplifier designs.
- (6) Good common-mode rejection ratio of about 90dB. This describes the ability of the operational amplifier to see only the differential input and ignore voltages which are common to both input terminals so that spurious voltages appearing along a length of printed track, for example, can be almost totally rejected provided both inputs are referred to the same point on the track.

Operational amplifier theory

If you are familiar with operational amplifier theory skip the following. If not, read on.

Operational amplifiers are a very close approach, for most purposes, to the mythical 'black box' for which we make the following assumptions.

The theory shown in Fig. 1a is a device which has infinite voltage gain (A) for differential voltages appearing across the $+in$ and $-in$ terminals, for which no current flows into the inputs and whose output impedance is zero.

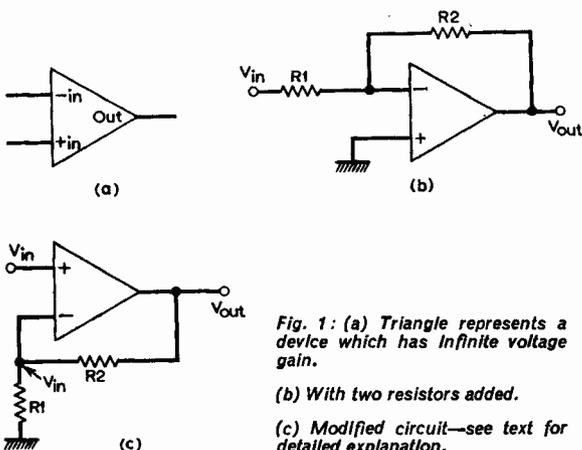


Fig. 1: (a) Triangle represents a device which has infinite voltage gain.

(b) With two resistors added.

(c) Modified circuit—see text for detailed explanation.

MAN

STEREO AMPLIFIER

RICHARD MANN*

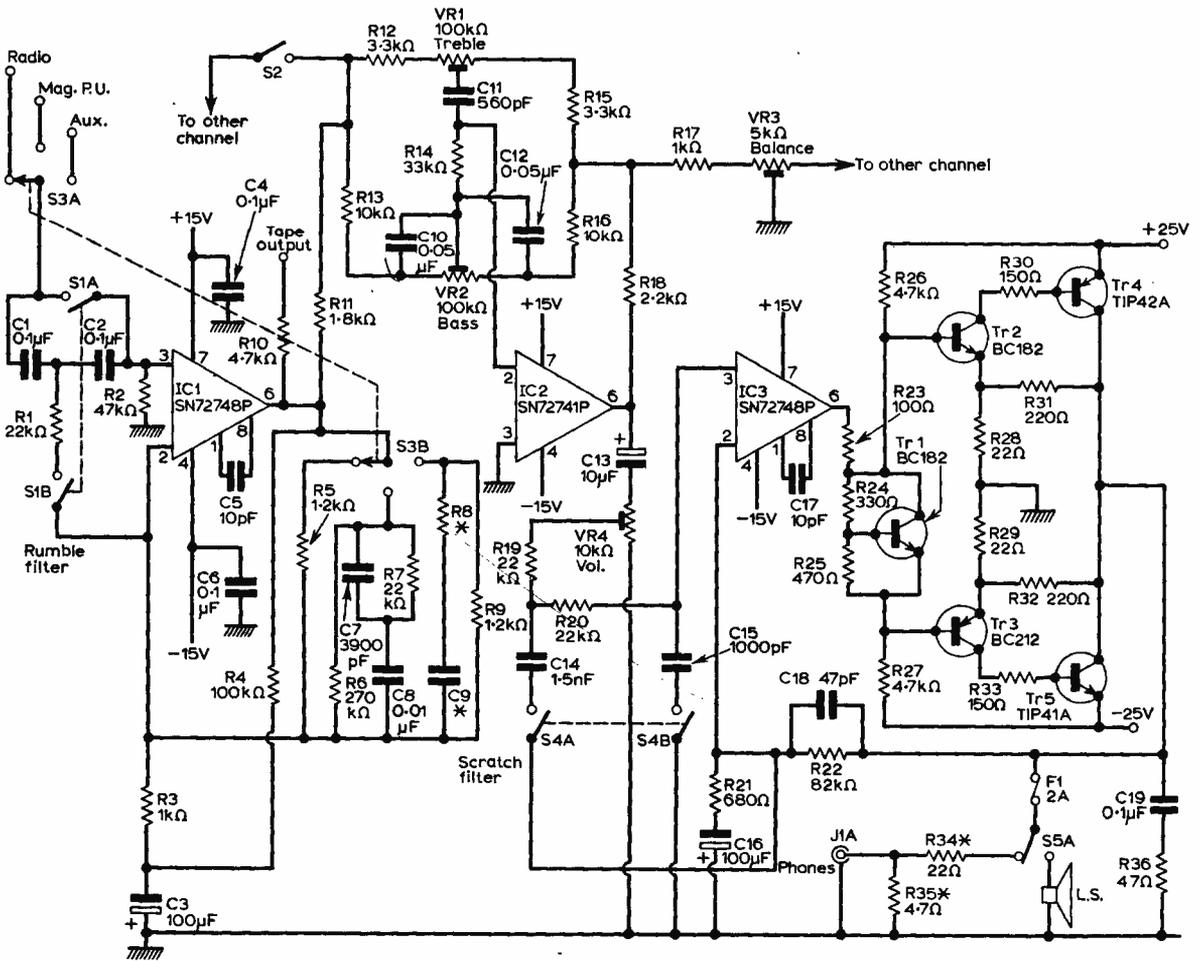


Fig. 2: One complete channel of the "Texan" stereo amplifier.

* Texas Instruments Limited.

Therefore, if we add two resistors as in Fig. 1b, since the + input is earthed and $A = \infty$ there is no difference in voltage between the terminals and the - input stays at ground potential becoming a 'virtual earth'. The current through R1, must therefore be $V_{in}/R1$.

As no current flows into the 'box' all input current must flow through R2 producing a voltage across it of $\frac{V_{in}}{R1} R2$ and since the current flows from the virtual earth point, V_{out} must be

$$\left(0 - \frac{V_{in}}{R1} R2\right)$$

Therefore, the closed loop gain of the circuit is

$$\frac{V_{out}}{V_{in}} = -\frac{R2}{R1}$$

If we modify the circuit as shown in Fig. 1c, we have a slightly different situation. The voltage at both input terminals becomes $+V_{in}$ so the feedback

current is still $\frac{V_{in}}{R1}$ but it now flows in the opposite

direction so that $V_{out} = \frac{V_{in}}{R1} (R1 + R2)$ and the closed

loop gain $= \frac{V_{out}}{V_{in}} \left(\frac{R1 + R2}{R1}\right)$

These two configurations are the classic 'inverting' and 'non inverting' amplifiers. The main differences, apart from polarity, are the input impedances, which for the former is R1 and for the latter is ∞ , and the fact that the non-inverting amplifier cannot have a gain of less than unity.

The SN72748P

Most integrated circuit manufacturers make at least one version of the popular '741' operational amplifier design. This ingenious device was designed to improve on the equally popular '709' which in turn was a vast improvement on earlier integrated circuits which were essentially monolithic versions of discrete component designs. Although the 741 now has competitors from the new range of 'superbeta' amplifiers it is likely to remain an industry standard for a long time mainly because it offers very good all round performance at a very low price.

The SN72748P and SN72741P are fairly typical scions of the 741 family. The difference between them is merely that the SN72741P has internal frequency compensation which allows 100% negative feedback to be applied without the circuit becoming unstable. The SN72748P requires one small capacitor (about 10pF) to be added externally and gives a higher gain-bandwidth than the 741. Physically, they are identical in 8 pin dual-in-line plastic packages.

Typical parameters for the SN72748P when operated at $\pm 15V$ supplies are:

Input resistance: $2M\Omega$ (higher with feedback).

Output resistance: 75Ω (much lower with feedback).

Gain: 200,000.

Input offset voltage (V_{IO}): 1mV (this represents the matching error of the input transistors).

Maximum output current: 15mA r.m.s.

Maximum output voltage: 9V r.m.s.

Input bias current (I_{IB}): $0.080\mu A$ (this is the current

★ Specification

Sensitivity to give 20 watts into 8Ω

Radio 30mV

Magnetic pickup 2.5mV

Auxiliary (see text)

Input impedance $47k\Omega$ 1kHz

Tape output (low level output) 130mV via $4.7k\Omega$ unaffected by tone or volume controls

Tone controls

Treble +10 -12dB at 15kHz

Bass ± 16 dB at 30Hz

Balance ± 8 dB one channel relative to other

Filters

Rumble—critically damped 2nd order corner frequency 50Hz, 12dB per octave roll-off

Scratch—critically damped 2nd order corner frequency 5.5kHz, 12dB per octave roll-off

Interchannel crosstalk

-51dB at 1kHz

-48dB at 10kHz

Unweighted signal-to-noise of complete amplifier with full amplifier bandwidth

-60dB magnetic pickup

-72dB radio

Dynamic range (equalisation and tone control stages)

-38dB before clipping (above nominal input level)

Power Output (both channels)

20 + 20 watts into 8Ω intermittent sine wave

16 + 16 watts into 8Ω continuous sine wave

15 + 15 watts into 15Ω continuous sine wave

Harmonic distortion

15 watts into 15Ω 0.05% at 1kHz

20 watts into 8Ω 0.09% at 1kHz

Low level distortion

0.16% at 1kHz 50mW into 15Ω

0.07% at 1kHz 50mW into 8Ω

Intermodulation distortion—wave analyser plots will appear later in this series

Frequency response (16 + 16 watts into 8Ω)

-1dB 7Hz to 22kHz

-3dB less than 5Hz to 35kHz

Stability—will drive electrostatic loudspeakers

Output impedance less than 1 milli ohm

Dimensions (less teak sleeve)

width 363mm 14.3in

height 48mm 1.9in

depth 149mm 5.9in

The following equipment was used to obtain the above measurements on the TEXAN amplifier:

Low Distortion Oscillator—Radford. Wave Analyser—Hewlett Packard 3590A/3593A. True R.M.S. Voltmeter—Hewlett Packard. Function Generator—Hewlett Packard 3300A/3305A. A.C. Digital Voltmeter—Pacific Measurements 1010. Oscilloscope—Hewlett Packard 181A. Test Oscillators (two)—Hewlett Packard 652A (intermodulation tests). X Y Recorder—Hewlett Packard 136A.

necessary to turn on the input transistors).
Supply ripple rejection: 20,000:1

More comprehensive details of the devices, including circuitry, can be obtained from manufacturers' data sheets.

Description of circuit

The complete amplifier circuit is given in Fig. 2, but components are referred to below for only one channel. In the components list, items for the other channel are +100 (i.e. R1, R101).

The input stage amplifies the various input signals to approximately 50mV, provides whatever equalization is required and gives the loop gain necessary for an active rumble filter. The feedback may look rather complex, but it breaks down into three parts as shown below.

(1) At d.c. the output is returned to the inverting input via R (Fig. 3a) which comprises R4 in parallel with R5, R6 or R9.

C3 blocks the path to ground so substituting in the equation for Fig. 1C we have a d.c. gain of $\frac{R+\infty}{\infty}$ (i.e. unity).

Since R2 refers the +ve input to ground, the -ve input will sit at a potential of V_{IO} (approx $\pm 1mV$) and the output will also take this d.c. level. This offset is so low that there is no need for a coupling capacitor into the next stage.

(2) At mid band a.c. the gain of the input stage becomes $\frac{Z+R3}{R3}$ where Z (Fig. 3b) is the impedance of the selected feedback network.

R4 has no effect on Z since the current through R4 is shunted to ground by C3. The feedback networks shown are designed to handle radio, magnetic pickup and auxiliary inputs and are discussed in more detail later in this series of articles.

The input impedance of the stage is inherently very high ($>2M\Omega$) but is shunted by the 47k Ω resistor R2 which provides the damping necessary for magnetic pickups and supplies the minute input bias current for the operational amplifier,

(3) A classic form of second order, high-pass active filter is shown in Fig. 3c.

The amplifier is ideally a unity gain buffer. Being a second order filter the low frequency response tends to roll off at 40dB/decade and the transitional region is a function of the damping factor (ζ) of the

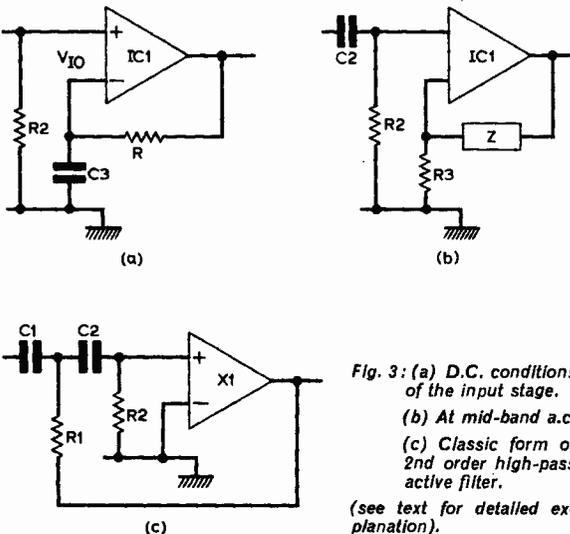


Fig. 3: (a) D.C. conditions of the input stage.
(b) At mid-band a.c.
(c) Classic form of 2nd order high-pass active filter.
(see text for detailed explanation).

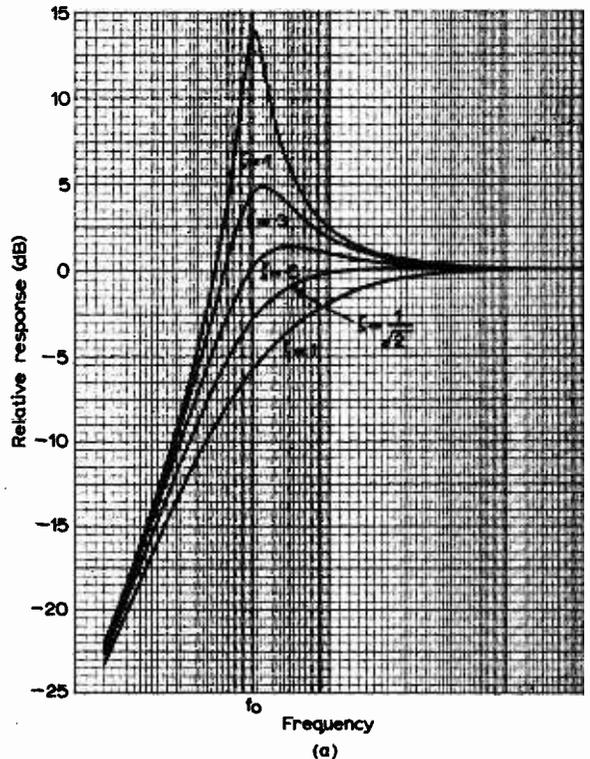


Fig. 4: (a) Theoretical response of 2nd order high pass filter for different values of ζ

filter. The effect of ζ is shown in Fig. 4a and has

optimum cut-off without peaking when $\zeta = \frac{1}{\sqrt{2}}$. The

damping factor is evaluated from $\zeta = \sqrt{\frac{R1}{R2}}$ and cut-

off frequency (f_0) from $f_0 = \frac{1}{2\pi \sqrt{R1 R2 C1 C2}}$

Since the operational amplifier has to supply a certain amount of gain in the equalization stage its output obviously does not provide a unity gain buffer. However, the inverting input terminal can be used for this purpose since its voltage exactly follows that of the non-inverting terminal.

The characteristic of the filter is modified slightly because any current flowing down R1, is not shunted to ground via R3 and C3, as one might think, but has to flow through the feedback impedance Z. Nevertheless the response is very close to a standard filter response as shown in Fig. 4b.

Placing the filter right at the front of the amplifier ensures that large inputs at sub-audio frequencies will not cause any intermodulation in IC1.

The push button switch S1 removes the filter when the button is out and a direct connection is made to the selected input.

This is permissible since the d.c. bias current to the operational amplifier is in the order of nano amps and causes no problems in the average pickup or tape head.

Facilities for coupling the equalised input signal to an external tape recorder are provided by taking the output of IC1 via a 4.7k Ω resistor R10. This

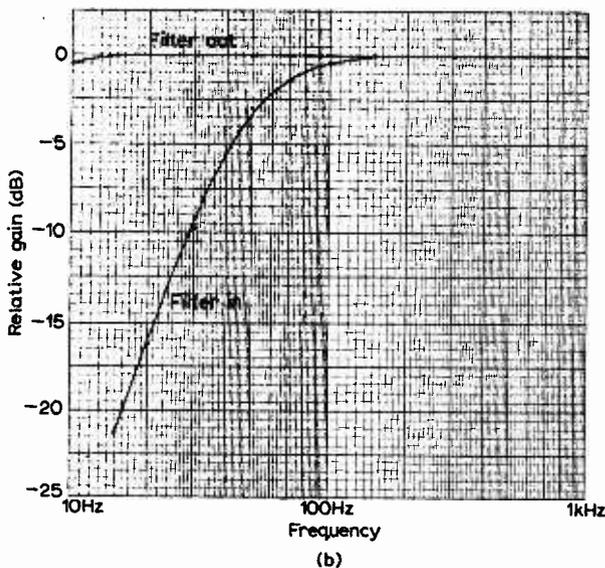


Fig. 4: (b) Rumble filter characteristic (measured).

series resistance allows the channels to be shorted externally if only a mono signal is required. The very low output impedance of IC1 ($<1\Omega$) means that no significant crosstalk is introduced in these circumstances.

The tone control stage

The tone control is a standard Baxandall circuit using an SN72741P to provide the loop gain. A fully compensated amplifier is necessary here since there is 100% feedback around the circuit in the cut position.

The time constants of the feedback network are chosen so that there is negligible interaction between the bass and treble controls. The control range is shown in Fig. 5.

The maximum levels of bass boost and cut are determined by the end stop resistors R13 and R16 respectively. Similarly the range of the treble control is limited by R12 and R15 although in this case the bass network does have a modifying influence which adds an extra limiting factor.

The transient response of the tone control with maximum treble boost is shown in the oscillogram, Fig. 6. It is well damped and shows no tendency to ring.

Two other functions are included in the tone control stage, the mono-stereo switch and the balance control.

Finding the optimum position for the mono switch was rather a problem since it should be before

the balance control if possible. The series resistor R11 was added so that the two channels could be shorted together by S2 without overloading the pre-amplifiers (IC1 IC101). However, the resistor is not high enough to have a significant effect on the tone control range with the value given.

The balance control is an active circuit giving a control range of $\pm 12\text{dB}$ for one channel relative to the other. This is a personal preference as I do not see much point in having 100% control range and it usually involves a waste of gain. However, anyone feeling strongly about it could cut out the relevant components and insert a dual gang pot between C13 and the volume control. The $10\mu\text{F}$ capacitor C13, incidentally, is the only d.c. block in the forward signal path which accounts for the good low frequency response and phase shift of the amplifier. A tantalum 'bead' capacitor is used in this position partly for its small size and partly because they will withstand a reverse polarizing voltage of 0.5V . Because the output voltage of IC2 depends mainly on its input offset it could be of either polarity but its magnitude will not exceed 200mV for any setting of the bass control (which determines the d.c. gain of the stage). A minor point here is that if the bass control is moved rapidly, a transient level shift may be heard from the loudspeaker. This effect can be removed by inserting a blocking capacitor of about $1\mu\text{F}$ between R13 and the junction of C10 and VR2, thereby fixing the d.c. gain of the stage at unity.

The scratch filter

The scratch filter is again based on a classic second order configuration as shown in Fig. 7. This low-pass circuit is the dual of the high-pass circuit used for the rumble filter (Fig. 3c). The

damping factor is $\sqrt{\frac{C1}{C2}}$ and the cut-off frequency

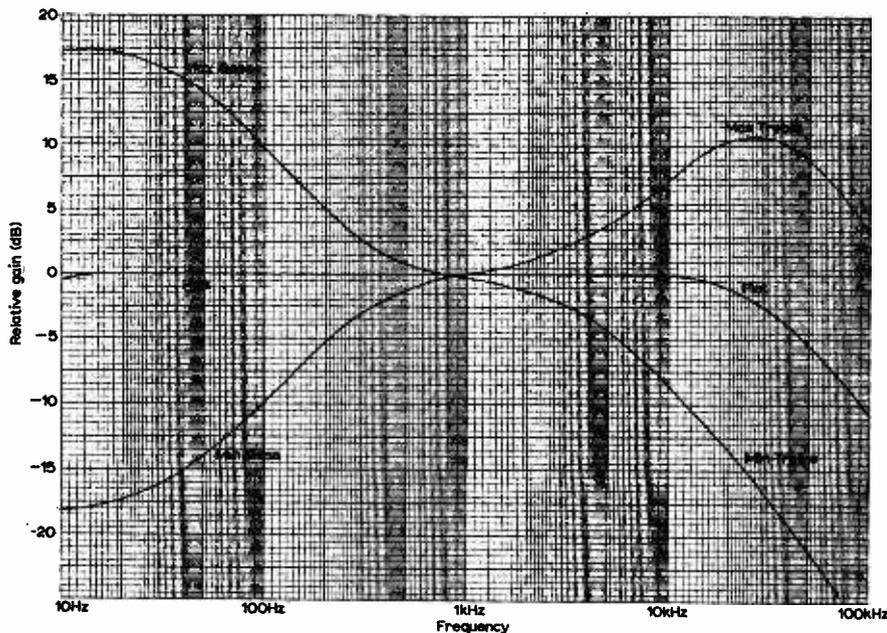
$$\frac{1}{2\pi \sqrt{C1 C2 R1 R2}}$$


Fig. 5: The control range of the bass and treble circuit.

TRANSISTORS

A SELECTION FROM OUR LIST

AA730	10p	BD115	75p	OC116	50p	2N1303	18p
AA742	15p	BD123	85p	OC20	85p	2N1304	22p
AAZ13	10p	BD124	80p	OC22	50p	2N1305	22p
AAZ10	10p	BD131	75p	OC23	60p	2N1306	25p
AAZ17	10p	BD132	80p	OC24	60p	2N1307	25p
AC107	35p	BDY11	OC25	60p	2N1307	25p	
AC126	25p		OC26	25p	2N1308	25p	
AC127	25p	BDY17	OC28	60p	2N1309	85p	
AC127Z	50p		OC29	60p	2N1613	20p	
AC128	20p	BDY38	OC35	50p	2N2147	75p	
AC176	20p	BDY60	OC36	60p	2N2160	60p	
AC187	25p		OC40	40p	2N2217	25p	
AC188	25p		OC43	50p	2N2218	20p	
AC177	20p	BF115	OC44	18p	2N2218A		
AC178	25p	BF154	OC61	15p			
AC179	25p	BF158	OC70	15p	2N2219	20p	
AC180	25p	BF159	OC71	15p	2N2219A		
AC181	25p	BF180	OC72	20p			
AC182	25p	BF194	OC75	25p	2N2220	25p	
AC183	25p	BF195	OC76	25p	2N2221	20p	
AC184	25p	BF196	OC77	25p	2N2221A		
AC185	25p	BF197	OC78	20p			
AC186	25p	BF198	OC79	20p	2N2222	20p	
AC187	25p	BF199	OC81	20p			
AC188	25p	BF200	OC82	20p			
AC189	25p	BF201	OC83	25p			
AC190	25p	BF202	OC84	25p	2N2369	15p	
AC191	25p	BF203	OC85	25p	2N2369A		
AC192	25p	BF204	OC86	25p			
AC193	25p	BF205	OC87	25p			
AC194	25p	BF206	OC88	25p			
AC195	25p	BF207	OC89	25p			
AC196	25p	BF208	OC90	25p			
AC197	25p	BF209	OC91	25p			
AC198	25p	BF210	OC92	25p			
AC199	25p	BF211	OC93	25p			
AC200	25p	BF212	OC94	25p			
AC201	25p	BF213	OC95	25p			
AC202	25p	BF214	OC96	25p			
AC203	25p	BF215	OC97	25p			
AC204	25p	BF216	OC98	25p			
AC205	25p	BF217	OC99	25p			
AC206	25p	BF218	OC100	25p			
AC207	25p	BF219	OC101	25p			
AC208	25p	BF220	OC102	25p			
AC209	25p	BF221	OC103	25p			
AC210	25p	BF222	OC104	25p			
AC211	25p	BF223	OC105	25p			
AC212	25p	BF224	OC106	25p			
AC213	25p	BF225	OC107	25p			
AC214	25p	BF226	OC108	25p			
AC215	25p	BF227	OC109	25p			
AC216	25p	BF228	OC110	25p			
AC217	25p	BF229	OC111	25p			
AC218	25p	BF230	OC112	25p			
AC219	25p	BF231	OC113	25p			
AC220	25p	BF232	OC114	25p			
AC221	25p	BF233	OC115	25p			
AC222	25p	BF234	OC116	25p			
AC223	25p	BF235	OC117	25p			
AC224	25p	BF236	OC118	25p			
AC225	25p	BF237	OC119	25p			
AC226	25p	BF238	OC120	25p			
AC227	25p	BF239	OC121	25p			
AC228	25p	BF240	OC122	25p			
AC229	25p	BF241	OC123	25p			
AC230	25p	BF242	OC124	25p			
AC231	25p	BF243	OC125	25p			
AC232	25p	BF244	OC126	25p			
AC233	25p	BF245	OC127	25p			
AC234	25p	BF246	OC128	25p			
AC235	25p	BF247	OC129	25p			
AC236	25p	BF248	OC130	25p			
AC237	25p	BF249	OC131	25p			
AC238	25p	BF250	OC132	25p			
AC239	25p	BF251	OC133	25p			
AC240	25p	BF252	OC134	25p			
AC241	25p	BF253	OC135	25p			
AC242	25p	BF254	OC136	25p			
AC243	25p	BF255	OC137	25p			
AC244	25p	BF256	OC138	25p			
AC245	25p	BF257	OC139	25p			
AC246	25p	BF258	OC140	25p			
AC247	25p	BF259	OC141	25p			
AC248	25p	BF260	OC142	25p			
AC249	25p	BF261	OC143	25p			
AC250	25p	BF262	OC144	25p			
AC251	25p	BF263	OC145	25p			
AC252	25p	BF264	OC146	25p			
AC253	25p	BF265	OC147	25p			
AC254	25p	BF266	OC148	25p			
AC255	25p	BF267	OC149	25p			
AC256	25p	BF268	OC150	25p			
AC257	25p	BF269	OC151	25p			
AC258	25p	BF270	OC152	25p			
AC259	25p	BF271	OC153	25p			
AC260	25p	BF272	OC154	25p			
AC261	25p	BF273	OC155	25p			
AC262	25p	BF274	OC156	25p			
AC263	25p	BF275	OC157	25p			
AC264	25p	BF276	OC158	25p			
AC265	25p	BF277	OC159	25p			
AC266	25p	BF278	OC160	25p			
AC267	25p	BF279	OC161	25p			
AC268	25p	BF280	OC162	25p			
AC269	25p	BF281	OC163	25p			
AC270	25p	BF282	OC164	25p			
AC271	25p	BF283	OC165	25p			
AC272	25p	BF284	OC166	25p			
AC273	25p	BF285	OC167	25p			
AC274	25p	BF286	OC168	25p			
AC275	25p	BF287	OC169	25p			
AC276	25p	BF288	OC170	25p			
AC277	25p	BF289	OC171	25p			
AC278	25p	BF290	OC172	25p			
AC279	25p	BF291	OC173	25p			
AC280	25p	BF292	OC174	25p			
AC281	25p	BF293	OC175	25p			
AC282	25p	BF294	OC176	25p			
AC283	25p	BF295	OC177	25p			
AC284	25p	BF296	OC178	25p			
AC285	25p	BF297	OC179	25p			
AC286	25p	BF298	OC180	25p			
AC287	25p	BF299	OC181	25p			
AC288	25p	BF300	OC182	25p			
AC289	25p	BF301	OC183	25p			
AC290	25p	BF302	OC184	25p			
AC291	25p	BF303	OC185	25p			
AC292	25p	BF304	OC186	25p			
AC293	25p	BF305	OC187	25p			
AC294	25p	BF306	OC188	25p			
AC295	25p	BF307	OC189	25p			
AC296	25p	BF308	OC190	25p			
AC297	25p	BF309	OC191	25p			
AC298	25p	BF310	OC192	25p			
AC299	25p	BF311	OC193	25p			
AC300	25p	BF312	OC194	25p			
AC301	25p	BF313	OC195	25p			
AC302	25p	BF314	OC196	25p			
AC303	25p	BF315	OC197	25p			
AC304	25p	BF316	OC198	25p			
AC305	25p	BF317	OC199	25p			
AC306	25p	BF318	OC200	25p			
AC307	25p	BF319	OC201	25p			
AC308	25p	BF320	OC202	25p			
AC309	25p	BF321	OC203	25p			
AC310	25p	BF322	OC204	25p			
AC311	25p	BF323	OC205	25p			
AC312	25p	BF324	OC206	25p			
AC313	25p	BF325	OC207	25p			
AC314	25p	BF326	OC208	25p			
AC315	25p	BF327	OC209	25p			
AC316	25p	BF328	OC210	25p			
AC317	25p	BF329	OC211	25p			
AC318	25p	BF330	OC212	25p			
AC319	25p	BF331	OC213	25p			
AC320	25p	BF332	OC214	25p			
AC321	25p	BF333	OC215	25p			
AC322	25p	BF334	OC216	25p			
AC323	25p	BF335	OC217	25p			
AC324	25p	BF336	OC218	25p			
AC325	25p	BF337	OC219	25p			
AC326	25p	BF338	OC220	25p			
AC327	25p	BF339	OC221	25p			
AC328	25p	BF340	OC222	25p			
AC329	25p	BF341	OC223	25p			
AC330	25p	BF342	OC224	25p			
AC331	25p	BF343	OC225	25p			
AC332	25p	BF344	OC226	25p			
AC333	25p	BF345	OC227	25p			
AC334	25p	BF346	OC228	25p			
AC335	25p	BF347	OC229	25p			
AC336	25p	BF348	OC230	25p			
AC337	25p	BF349	OC231	25p			
AC338	25p	BF350	OC232	25p			
AC339	25p	BF351	OC233	25p			
AC340	25p	BF352	OC234	25p			
AC341	25p	BF353	OC235	25p			
AC342	25p	BF354	OC236	25p			
AC343	25p	BF355	OC237	25p			
AC344	25p	BF356	OC238	25p			
AC345	25p	BF357	OC239	25p			
AC346	25p	BF358	OC240	25p			
AC347	25p	BF359	OC241	25p			
AC348	25p	BF360	OC242	25p			
AC349	25p	BF361	OC243	25p			
AC350	25p	BF362	OC244	25p			
AC351	25p	BF363	OC245	25p			
AC352	25p	BF364	OC246	25p			
AC353	25p	BF365	OC247	25p			
AC354	25p	BF366	OC248	25p			
AC355	25p	BF367	OC249	25p			
AC356	25p	BF368	OC250	25p			
AC357	25p	BF369	OC251	25p			
AC358	25p	BF370	OC252	25p			
AC359	25p	BF371	OC253	25p			
AC360	25p	BF372	OC254	25p			
AC361	25p	BF373	OC255	25p			
AC362	25p	BF374	OC256	25p			
AC363	25p	BF375	OC257	25p			
AC364	25p	BF376	OC258	25p			
AC365	25p	BF377	OC259	25p			
AC366	25p	BF378	OC260	25p			
AC367	25p	BF379	OC261	25p			
AC368	25p	BF380	OC262	25p			
AC369	25p	BF381	OC263	25p			
AC370	25p	BF382	OC264	25p			
AC371	25p	BF383	OC265	25p			
AC372	25p	BF384	OC266	25p			
AC373	25p	BF385	OC267	25p			
AC374	25p	BF386	OC268	25p			
AC375	25p	BF387	OC269	25p			
AC376	25p	BF388	OC270				

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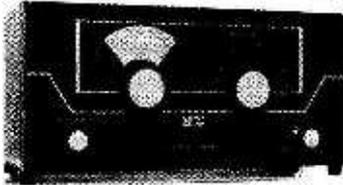


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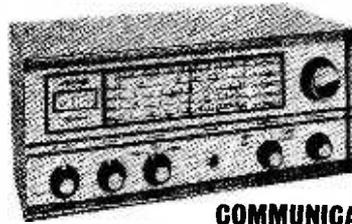


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★ components list

Resistors:

R1 R101 22kΩ 5% ½W	R22 R122 82kΩ 5% ½W
R2 R102 47kΩ 5% ½W	R23 R123 100Ω
R3 R103 1kΩ 5% ½W	R24 R124 330Ω 5% ½W
R4 R104 100kΩ	R25 R125 470Ω 5% ½W
R5 R105 1.2kΩ 5% ½W	R26 R126 4.7kΩ
R6 R106 270kΩ 5% ½W	R27 R127 4.7kΩ
R7 R107 22kΩ 5% ½W	R28 R128 22Ω 5% ½W
R8 R108 — 5% ½W	} see text next month
R9 R109 1.2kΩ 5% ½W	
R10 R110 4.7kΩ	R29 R129 22Ω 5% ½W
R11 R111 1.8kΩ	R30 R130 150Ω
R12 R112 3.3kΩ	R31 R131 220Ω 5% ½W
R13 R113 10kΩ	R32 R132 220Ω 5% ½W
R14 R114 33kΩ	R33 R133 150Ω
R15 R115 3.3kΩ	R34 R134 22Ω 10% 5W
R16 R116 10kΩ	wire wound.
R17 R117 1kΩ	R35 R135 4.7Ω 10% ½W
R18 R118 2.2kΩ	R36 R136 47Ω
R19 R119 22kΩ 5% ½W	R37 680Ω 10% ½W
R20 R120 22kΩ 5% ½W	R38 680Ω 10% ½W
R21 R121 680Ω 5% ½W	

All resistors 10% ½W high stability carbon film unless otherwise specified.

Potentiometers:

VR1 VR101 100kΩ twin-gang carbon linear
VR2 VR102 100kΩ twin-gang carbon linear
VR3 5kΩ single-gang carbon linear
VR4 VR104 10kΩ twin-gang carbon log

All pots have p.c. terminations—AB Metals type D45

Capacitors

C1 C101 0.1μF	
C2 C102 0.1μF	
C3 C103 100μF	3V tantalum
C4 C104 0.1μF	
C5 C105 10pF	10% 30V polystyrene
C6 C106 0.1μF	
C7 C107 3900pF	
C8 C108 0.01μF	
C9 C109	not normally required (see text, next month)
C10 C110 0.05μF	
C11 C111 560pF	5% 30V polystyrene or ceramic
C12 C112 0.05μF	
C13 C113 10μF	16V tantalum
C14 C114 1500pF	5% 30V polystyrene
C15 C115 1000pF	5% 30V polystyrene
C16 C116 100μF	3V tantalum
C17 C117 10pF	10% 30V polystyrene
C18 C118 47pF	10% 30V polystyrene
C19 C119 0.1μF	
C20 1000μF	25V electrolytic Daly
C21 1000μF	25V electrolytic Daly
C22 3500μF	50V electrolytic Daly
C23 3500μF	50V electrolytic Daly

All capacitors 10% 30V polyester or mylar, unless otherwise specified

Switches:

S1 4 pole 2 way	} push-on—push-off
S2 2 pole 2 way	
S3 4 pole 3 way make-before-break rotary	
S4 4 pole 2 way push-on—push-off	
S5 2 pole 2 way slide	
S6 single pole mains on-off rocker	

S1, S2 and S4 are for p.c. termination

Integrated Circuits & Semiconductors:

IC1 IC101 SN72748P	} Texas Instruments Ltd.
IC2 IC102 SN72741P	
IC3 IC103 SN72748P	
Tr1 Tr101 BC182	
Tr2 Tr102 BC182	
Tr3 Tr103 BC212	
Tr4 Tr104 TIP42A	
Tr5 Tr105 TIP41A	
D1 1N4002	
D2 1N4002	
D3 1N4002	
D4 1N4002	
ZD1 BZY88C15	
ZD2 BZY88C15	

Indicator:

N1 Neon mains indicator

Transformer:

T1 Mains transformer primary 240V secondary 20-0-20V 1A. (special design) Gardners SL20

Sockets:

SK1 5W DIN socket
SK2 5W DIN socket
SK3 5W DIN socket
SK4 speaker DIN socket
SK5 speaker DIN socket
J1 3 pole stereo jack socket

Fuses:

F1 F101 2A	1.25in. cartridge
F2 F102 2A	1.25in. cartridge
F3 1A	20mm anti-surge

IC Sockets:

8 pin DIL IC sockets (IC sockets must be used—it is a condition of IC guarantee from Henry's Radio Ltd.)

Miscellaneous:

2 off twin fuseholders (1.25in fuses); 1 off panel mounting 20mm fuseholder.

All components, including a ready drilled fibre glass printed circuit board, drilled and punched metalwork, finished front panel, will be available to home constructors and the trade, from Henry's Radio Ltd. A teak sleeve will also be available—more details next month.

As with the rumble filter, its response is modified slightly by the feedback impedance of the output stage which provides its loop gain. The response of the scratch filter is given in Fig. 8 and shows that the circuit is again critically damped and reaches a roll off of nearly 40dB/decade (12dB/octave).

The output stage

The configuration of the output stage is almost identical to that of the input stage with a few extra watts thrown in. The midband gain of the stage is

$\frac{R22+R21}{R21}$ and the reactance of C16 reduces this

to unity at d.c. so that the final offset of the power stage is only 3 or 4mV. This feature is of importance first because it removes the need for a level setting adjustment and secondly because it allows all normal loudspeakers to be connected directly without the need for a bulky blocking capacitor. Even a Quad electrostatic loudspeaker can be driven satisfactorily in spite of the low primary resistance of its matching transformer.

The power stage is rather unusual in that it provides about 20dB voltage gain unlike the normal Darlington or other 100% feedback configuration.

The gain is introduced by attenuating the feedback with R31 and R28 for positive excursions and

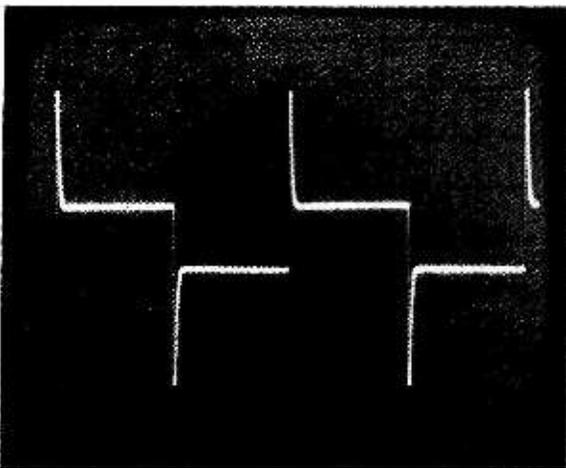


Fig. 6: Transient response of the tone control with maximum treble boost. Scale: X 200 μ S/div., Y 5V/div.

R32 and R29 for negative excursions. Voltage gain is necessary because the output swing of the operational amplifier is limited partly by its d.c. swing capability but mainly by its slew rate—the maximum rate in V/ μ S at which the output can change.

The transistors used in the power stage are low cost plastic encapsulated types. The drivers are a complementary pair of Texas Silect devices type BC182 and BC212. They have a continuous rating of 300mW in free air at 25°C which is quite adequate for driving the output transistors providing ballast resistors R30 and R33 are added to reduce their collector dissipations.

Quiescent current setting

This is always a knotty problem in class B or class AB amplifiers and is a process which frequently means instant death to the output transistors. This does not matter too much if you work for the firm which makes them but it is not so good if you have parted with hard earned cash. For this reason the circuit shows fixed resistors (R24 and R25) which set-up the potential across the V_{be} multiplier (Tr1). This potential, in conjunction with the d.c. feedback introduced by the emitter resistors R28 and R29, sets the current in the driver stage and hence, in the output transistors. If you are a purist you can sit down with a slide rule and data sheets and prove that this will give you a very wide variation of quiescent current. However, a more empirical

approach based on experience with about two dozen amplifier boards and transistors from different batches have indicated that the current usually sets up between 10mA and 40mA and anywhere in this range gives good crossover performance. This is partly due to the current, rather than voltage drive into the bases of the output transistors which have no shunt resistors to their emitters. Omitting these resistors slows down the power devices slightly but this is allowed for in the frequency compensation. The oscillograms in Figs 9a and 9b show the smooth crossover for an output power of 100mW r.m.s. with triangular inputs at 1kHz and 10kHz. Should the purist remain unconvinced, however, there is provision for a 470 Ω preset potentiometer on the printed circuit board. This is wired in place of R28 which should be omitted if the preset is used. There is also a link between the emitter of each TIP42A and the +25V rail which can be broken to give a current monitor point. This quiescent current in the output stage can then be set to 20mA.

Frequency compensation

It is vital to have an amplifier correctly compensated if good transient response is expected from an amplifier. All too often designs appear to have marginal stability which causes the home constructor endless problems. In the *Texan* a dominant pole is placed in the open loop response by the 10pF capacitor, C17. A further pole occurs naturally in the discrete stage which is cancelled by a zero introduced with the phase advance capacitor, C18. This gives nearly 90° of phase margin to the amplifier which allows it to cope quite well with highly capacitive loads. Fig. 10 shows the transient response when driving 20 watts into an 8 Ω resistor in parallel with 2 μ F—said to be equivalent to an electrostatic loudspeaker load. There is a small overshoot under these conditions since transistor parameters have an inconvenient habit of changing with collector current. However, the degree of overshoot is not enough to cause trouble.

A similar oscillogram, Fig. 11, shows the output waveform when driving a Quad electrostatic loudspeaker. The power level in this case was only 1W as higher levels proved rather unpopular with my colleagues!

In addition to the compensation components there is a dummy h.f. load (C19 and R36) which is not necessary when driving most loudspeakers but takes

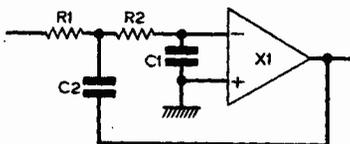
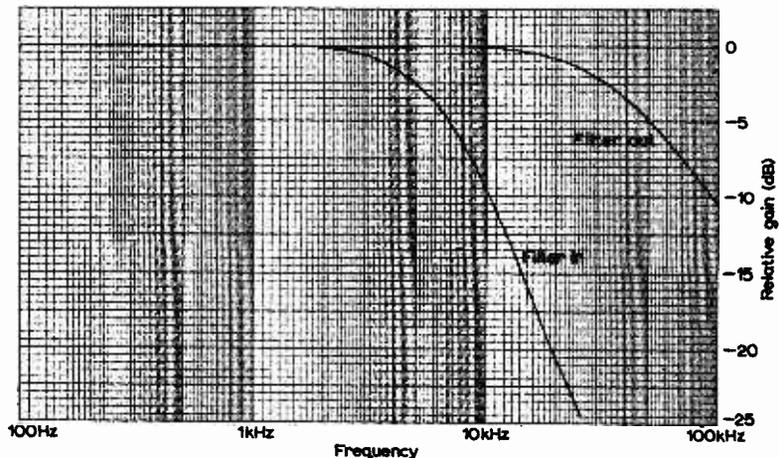
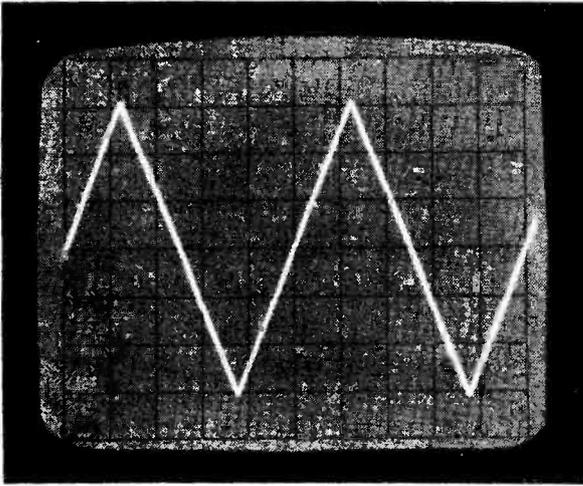


Fig. 7: (above) The scratch filter—classic 2nd. order configuration.

Fig. 8: (right) Scratch filter characteristic.





Oscillograms showing the smooth crossover for an output power of 100mW r.m.s. into 8Ω .
 9a (above): shows 1kHz triangular wave. Scales: X $200\mu\text{S}/\text{div.}$, Y $500\text{mV}/\text{div.}$
 9b (below): shows 10kHz triangular wave. Scales: X $20\mu\text{S}/\text{div.}$, Y $500\text{mV}/\text{div.}$

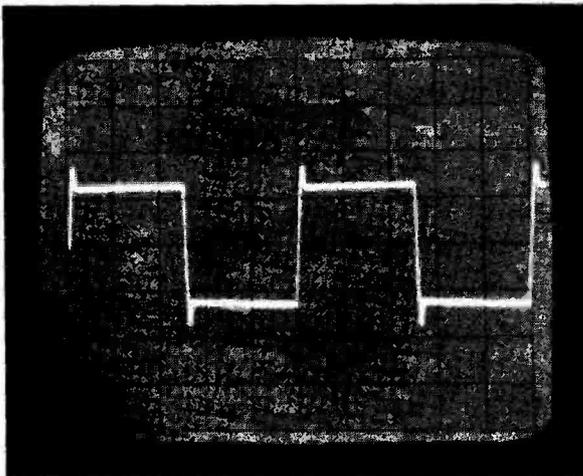
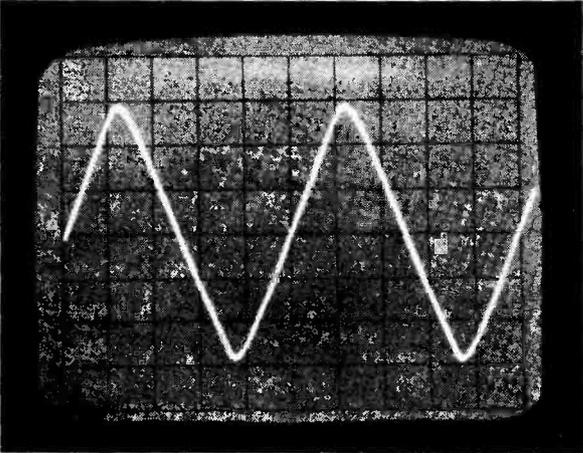


Fig. 10: Transient response driving 20W into 8Ω in parallel with $2\mu\text{F}$. Scales: X $200\mu\text{S}/\text{div.}$, Y $10\text{V}/\text{div.}$

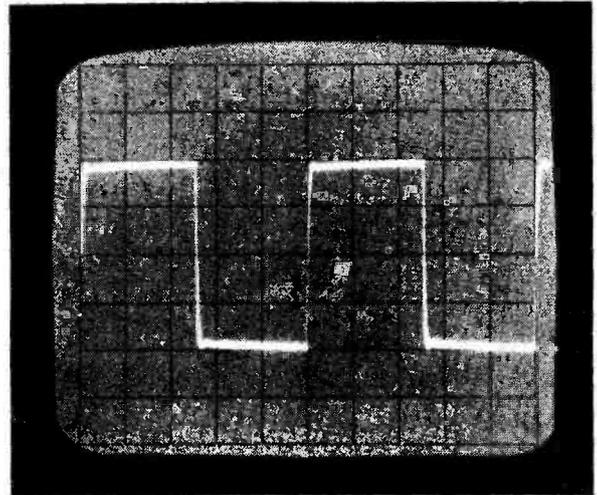


Fig. 11: Transient response when driving 1W into Quad electrostatic loudspeaker. Scales: X $200\mu\text{S}/\text{div.}$, Y $2\text{V}/\text{div.}$

care of the output under nearly no-load conditions. These arise when using headphones or with some loudspeaker crossover systems which look very inductive at higher frequencies.

Headphone output

This facility was added at popular request and originally consisted of a jack socket straight across the output. An arrangement which promptly ruined a brand new pair of Koss PRO-4AA Stereo headphones not to mention a near miss on my eardrums. Although the former were kindly repaired free of charge, thereafter an attenuator seemed a good idea. The attenuator values were chosen to give a listening level very roughly equivalent to that through the loudspeakers and to be capable of driving normal low impedance headphones as those mentioned.

Overload protection

This is another brain-teaser. It is very easy to get so carried away with protection circuitry that it becomes as complex as all the rest of the amplifier put together. Simple methods frequently introduce distortion and do not protect much anyway. In the *Texan* the only protection is provided by a fuse. It gives satisfactory protection against a short circuit on the output line since the TIP41A and TIP42A have a continuous collector rating of 6 amps which allows an adequate margin for the 2 amp fuse (1 amp for 15Ω loads) to blow.

One disadvantage of using a d.c. coupled output is that a fault in the output stage could put a large continuous current through the speaker. The fuse will also protect against gross overloads but this is, of course, rather dependent on the actual loudspeaker used. It is very unlikely that a catastrophic breakdown will occur but if belt and braces are required then the traditional large electrolytic could be inserted providing the loudspeaker is returned to the -25V supply line to polarise the capacitor.

The power supply for a class B amplifier is the part most likely to be the subject of compromise. If size, weight and most of all, cost are of no consequence then a huge transformer and vast electrolytics will give almost perfect regulation. Alternatively, a regulated power supply can be built

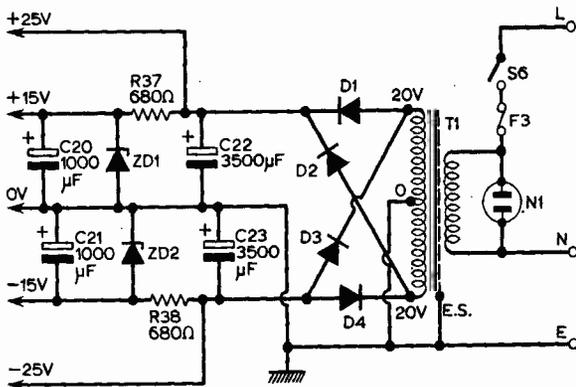


Fig. 12 Circuit of the mains power supply for the "Texan" stereo amplifier. Note that a 2A fuse (F2, 102) should be shown in the +25V and -25V supply rails respectively.

which cuts down on the electrolytics but adds at least one extra power transistor. Unless carefully designed they can also suffer from reactive output impedances or worse still instability which does not help the amplifier, of course.

The circuit diagram of the compromise chosen is shown in Fig. 12. For the output stage nominal $\pm 25V$ supplies are derived from an unregulated full wave circuit with $3500\mu F$ smoothing capacitors. The 25V rails in turn supply the $\pm 15V$ rails for the operational amplifiers.

The 15V supplies are stabilised by a pair of low cost zener diodes. Accuracy is not at all important here since the operational amplifiers will operate equally well with supplies between $\pm 12V$ and $\pm 18V$. The zeners are necessary more as clamps to ensure that the rail voltages do not exceed $\pm 18V$, the maximum rating for the operational amplifiers. In parallel with the zeners are two $1000\mu F$ capacitors, C20 and C21. These may seem rather high in value but with full bass boost and magnetic pickup equalization, an equivalent input in the order of $10\mu V$ at 20Hz will produce 20W at the output. It is, therefore, essential to reduce ripple feedback to a minimum. The same reason, of course, accounts for the ease with which careless earthing can introduce low frequency instability.

The mains transformer recommended for the Texan is of rather unusual construction. It is a new design for which the manufacturers claim very low stray magnetic field—a great help when positioning the amplifier near a magnetic pick-up.

It also has a height of only 1.5in. which gives the Texan its 'slim-line' dimensions.

The nominal secondary voltage is 20.0-20 at 1 amp continuous r.m.s. and measurements on the transformer in circuit showed a regulation of about 3V r.m.s. between no load and a continuous sine power of 20 watts into one 8Ω load. The d.c. rails variations are as follows:

Quiescent	$\pm 32V$
20W sine into 8Ω (one channel only)	$\pm 23V$
16W sine into 8Ω	
(both channels simultaneously)	$\pm 17V$

It is apparent from these figures that the power supply is a major influence on maximum output power and distortion when considering continuous sine wave inputs.

Although holders for the integrated circuits were not used on the prototype, it is however recommended that they are used by the constructor.

TO BE CONTINUED

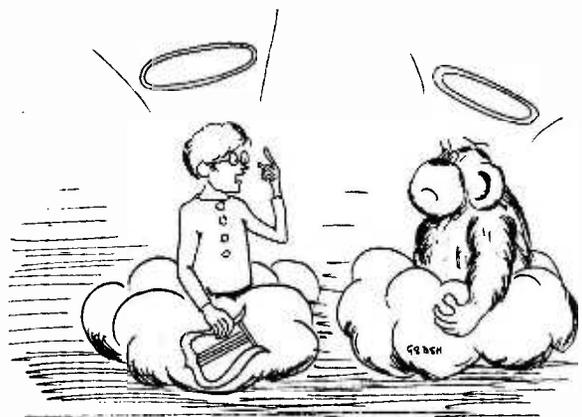


ISSUES WANTED

- ...A May 1971 and two June 1971.—Martin Cooper, 1 Cranston Road, Bramcote Hills, Beeston, Nottingham, NG9 3GU.
- ...P.W. May issue 1967.—P. G. Cooper, 14 Ruspsidge Road, Cindertord, Glos.
- ...P.W. August 1968.—P. Mitchell, 35 Inverton Road, Kirkcaldy, Fife, Scotland.
- ...Issue of P.W. which dealt with the construction of a continuous loop echo chamber (principle of record and fast/replay/erase tape recorder).—J. Peters, 83 Carlyon Road, Hayes, Middlesex.
- ...March 1966 issue of Practical Wireless.—M. Allmark, 4 Bowood Grove, Meanwood, Leeds, LS7 2PX.
- ...July, Oct., Dec. 1970, Feb. 1971, of P.W.—D. Knott, 39 Wychbury Road, Quarry Bk., Brierley Hill, Staffs., DY5 2XX.
- ...P.W. for August, September, October, November. All 1971.—F. Young, Church Hill, Holme Sp. Moor, York, YA4 4EE.
- ...P.W. April 1971.—H. R. Hodson, 61 Mollineux Road, Sheffield, S5 0JZ.
- ...January 1970 issue P.W.—M. Brown, 47 Stanmore Road, Nahoon, East London South Africa.
- ...Practical Wireless Jan. 1971.—B. P. Leite, Caixa Postal 8984, S. Paulo 01009, Brazil.
- ...Practical Wireless, Volume 45 (May 1969–April 1970 Inclusive), Practical Wireless for November 1971, Practical Electronics, Volume 5 (January 1968–December 1968).—Martin Ridge, 25 Broomfield Crescent, Leeds, LS6 3DD.
- ...June, July, August issues 1971 of Practical Wireless. All expenses refunded.—M. B. Spiller, 17 St. Andrew's Road, Halfeld, Sallsbury, Rhodesia.
- ...Back copies which cover "Digital Frequency Counter/Timer" by J. Thornton-Lawrence.—D. W. Barber, 28 Aldersey Road, Crewe, Cheshire, CW2 8NR.
- ...Issue of P.W. with the P.W. Treasure Locator.—J. Wholden, 4 Bewley Road, Trowbridge, Wilts.
- ...Jan. 1971 issue of Practical Wireless with an article on the P.W. Stereo Tape Recorder.—M. J. Brill, 43 Crockham Way, Eltham, London, SE9 3HD.
- ...Jan. 1971 issue of Practical Wireless.—A. W. Fletcher, 65 Waterloo Street, Hove, BN3 1AH, Sussex.
- ...January issue(s) of P.W. with the construction of a stereo tape recorder.—S. Savage, 13 Merton Road, Walthamstow, London, E.17.
- ...April 1971 issue Practical Wireless.—Mr. T. M. Fresson, Farnham, Surrey.
- ...Sept. 1970 of Practical Wireless.—Mr. B. A. Clark, London, S.E.18.
- ...July 1971 Practical Wireless.—K. M. Warford, 12 Bloomfield Drive, Shefford, Bedfordshire.
- ...Issue of P.W. containing the "Clubman" receiver on a car radio.—A. Rubin, The Barn, Castle Lane, Todmorden, Lancs.
- ...Circuit of a 50watt Bass amplifier.—R. U. H. Parratt, 35 Cabell Road, Park Bank, Guildford, Surrey.
- ...Issues June to November 1970 inclusive and June 1971 of P.W. wanted. Please state price.—G. G. Cooper, 139 Eltham Road, West Brldyford, Notts.
- ...February '71 P.W. Expressly. Part 2 of P.W. Stereo tape recorder.—R. J. Searle, 2 Pontings Close, Blunston, Wilts.
- ...A May 1964 Practical Wireless.—D. G. Robins, 21 Mountfield Road, Bramhall, Stockport, Cheshire.
- ...Wanted for cash or loan, the two editions of P.W. at the end of 1970 or the beginning of 1971 that described the construction of a tape recorder.—Fit. Lt. Stewart, Officers Mess, RAF Brize Norton, Oxon.
- ...Wanted issue of Practical Wireless dated February 1970, willing to pay full price.—M. J. Burrows, 7 Lyndhurst Road, Keynsham, Bristol.
- ...Wanted P.W. for: May 1967; Feb., March, Sept. and Oct. 1968; June 1969; Oct. 1970, and P.E. for Jan.–April 1967 inclusive line, supplement for April issue preferably. Also, borrow P.W. Sept. 1967.—A. Blay, 26 Bourne Close, Broxbourne, Herts.

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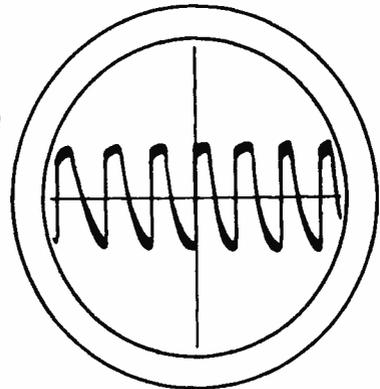


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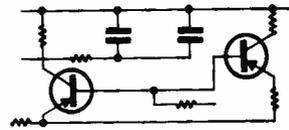
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0R2	.30	6BZ6	.31	6BA7M	.35	12SH7	.22	60L6GT	.45	EB91	.10	EL32	.18	KTW61	.63	PL82	.30	UCL83	.48	AA129	.15	BC107	.18	OA47	.10
0Z4	.25	6CB6A	.28	6BC7GT	.33	12K12	.22	90C1	.58	EB80	.10	EL32	.18	KTW61	.63	PL82	.30	UCL83	.48	AA129	.15	BC107	.18	OA47	.10
147GT	.33	6C4	.28	6BG7GT	.33	12K7	.24	150B3	.58	EBF80	.30	EL42	.28	N308	.95	PL504	.80	U7H81	.30	AA129	.15	BC107	.18	OA47	.10
1B3GT	.33	6C4	.28	6BH7	.33	12K7	.24	507	.59	EBF83	.38	EL41	.50	N339	.44	PL508	.80	U7H81	.30	AA129	.15	BC107	.18	OA47	.10
1H5GT	.33	6CD6G	1.06	6B37	.55			802	.80	EBF89	.27	EL83	.38	P61	.44	PL509	1.80	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
1L4	.18	6CG8A	.60	6BK7GT	.28	14H7	.48	5763	.50	EBL21	.60	EL84	.22	PAC80	.33	PL802	.75	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
184	.22	6CH6	.38	6BQ7GT	.38	14E7	.75	AC/PEN		EC86	.59	EL86	.40	P86	.47	PL84	.34	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
1R5	.28	6CL6	.43	6U4GT	.60	19A45	.24			EC88	.59	EL86	.40	P86	.47	PL84	.34	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
1U4	.29	6CM7	.50	6V6GT	.17	19B6G6	.85	AC/PEN		EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
1U5	.48	6CW4	.83	6X4	.30	19B6	.80	DD	.98	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
2021	.85	6E7	.50	6X5GT	.25	20P2	.65	AC/PEN		EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
2K5	.50	6DT6A	.50	7A7	.88	20L1	.98			EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3A4	.25	6E7W6	.55	7B6	.68	20P1	.50	AC/PTP	.98	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3D6	.19	6F1	.59	7B7	.82	20P3	.79	AL60	.78	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3Q4	.38	6F6	.83	7C6	.30	20P4	.89	ATP4	.12	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3Q5GT	.35	6F6G	.25	7H7	.28	20P5	1.00	AZ1	.40	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3R4	.25	6F13	.33	7R7	.65	25A6G	.29	AZ31	.46	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
3V4	.32	6F14	.42	7Y4	.60	25L6G	.38	AZ41	.63	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
4CB6	.50	6F18	.48	7Y4	.60	25L6	.38	AZ41	.63	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
5CG8	.50	6F23	.48	7Y4	.60	25V5G	.49	AZ41	.63	EC92	.34	EL91	.23	PC95	.53	PC25	.88	U7A1	.64	AA129	.15	BC107	.18	OA47	.10
5V4G	.34	6F24	.58	10C2	.49	25Z4G	.28	CY1	.53																
5Y3GT	.28	6F25	.54	10DE7	.50	25Z5	.40	CY31	.31	ECF80	.26	EY87	.60	PCF80	.40	PCF80	.40	PCF80	.40	PCF80	.40	PCF80	.40	PCF80	.40
6Z4G	.34	6F28	.60	10F1	.75	25Z6G	.43	DAP6	.20	ECF82	.26	EY88	.40	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6Y80L2	.35	6F28	.15	10P9	.45	30A5	.44	DAF96	.33	ECF86	.24	EY91	.58	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6AB4	.32	6F18A	.50	10L11	.55	30C13	.67	DF91	.34	ECF86	.24	EY91	.58	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6AC7	.15	6GK5	.80	10L11	.55	30C13	.67	DF91	.34	ECF86	.24	EY91	.58	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6AG5	.25	6G17	.50	10P13	.54	30C18	.80	DH76	.39	ECF86	.24	EY91	.58	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6AK6	.30	6H6GT	.15	10P14	1.08	30F5	.65	DK40	.55	ECB42	.42	EY87	.60	PCF86	.57	R10	.75	U404	.38	AF114	.25	FY11A	.38	OC81D	.11
6AM8A	.50	6J3G	.19	12A6	.68	30PL1	.80	DK92	.35	ECH81	.39	FW4/500	.75	PCL86	.35	TH4B	.58	U120A	.60	AF126	.17	GF118	.20	OC123	.23
6AN8	.49	6J3GT	.29	12AC6	.40	30PL2	.80	DK96	.35	ECH83	.39	FW4/500	.75	PCL86	.35	TH4B	.58	U120A	.60	AF126	.17	GF118	.20	OC123	.23
6AQ5	.22	6J3E	.19	12AD6	.40	30PL12	.89	DL96	.35	ECH84	.34	GZ30	.34	PD500	1.44	TH233	.98	U120A	.60	AF126	.17	GF118	.20	OC123	.23
6AR5	.30	6J7G	.24	12AE6	.48	30PL14	.68	DM70	.30	ECL80	.30	GZ32	.41	PEN4DD	1.38	UABCH0	.30	W107	.50	AF186	.55	GF128	.15	OC123	.23
6AT6	.18	6J7GT	.24	12B7E	.32	30L15	.58	DM71	.38	ECL82	.30	GZ33	.70			UABCH0	.30	W107	.50	AF186	.55	GF128	.15	OC123	.23
6AU6	.80	6J8A	.50	12AT7	.18	30L17	.40	DY776	.65	ECL83	.28	GZ34	.87	PEN45DD	.75	UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6AV6	.28	6K7G	.10	12AUG	.21	30PM4R	.55	DY602	.35	ECL84	.28	GZ37	.87	PEN45DD	.75	UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6AW8A	.64	6K7GT	.23	12AUG	.19	30P12	.88	E80F	1.20	ECL85	.45	HAB80	.44	PEN45DD	.75	UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6AX4	.30	6K8G	.18	12AV6	.28	30P19R	.58	E83C	1.20	ECL86	.35	HL23DD	.40	PEN45DD	.75	UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BB6	.13	6L1	.98	12AX7	.22	30P4	.58	E89CC	.60	EF22	.43	HL42DD	.98			UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BA6	.20	6L6GT	.39	12BA6	.30	30PL1	.59	E92CC	.40	EF40	.49	HL42DD	.98			UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BC6	.50	6L7	.39	12BB6	.30	30PL13	.75	E180F	.80	EF41	.48	HN309	1.40			UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BE6	.21	6L18	.44	12BB7	.27	30PL14	.85	E180F	.80	EF42	.48	HN309	1.40			UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BO6G	1.06	6L19	1.88	12J5GT	.30	30PL15	.87	E114R	.48	EF54	.38					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BH6	.43	6LD20	.48	12J7GT	.33	35A3	.48	EAB50	.18	EF73	.75					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BJ6	.30	6N7GT	.40	12K5	.50	35L0GT	.42	EAB78	.38	EF80	.22					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BQ7A	.38	6Q7	.43	12K7GT	.34	35W4	.33	EAB80	.30	EF83	.48					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BR7	.78	6Q7G	.27	12BA7GT		35Z4GT	.24	EAC91	.38	EF85	.29					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23
6BR8	.43	6R7	.58			40	35Z5GT	.30	EAP42	.48	EF86	.29			UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23	
6BW6	.72	6R7G	.35	12BC7	.35	50E8E	.55	E85A	.20	EF89	.23					UAC01	.45	X41	.50	AF239	.38	GF128	.15	OC123	.23

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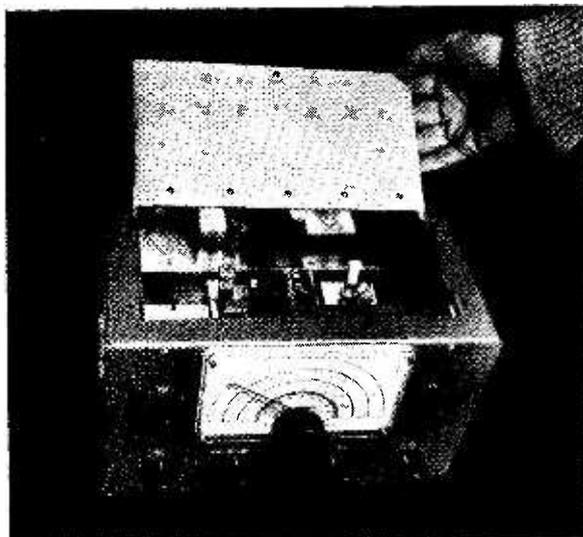
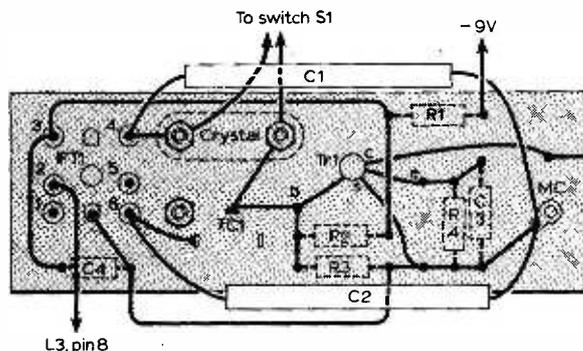
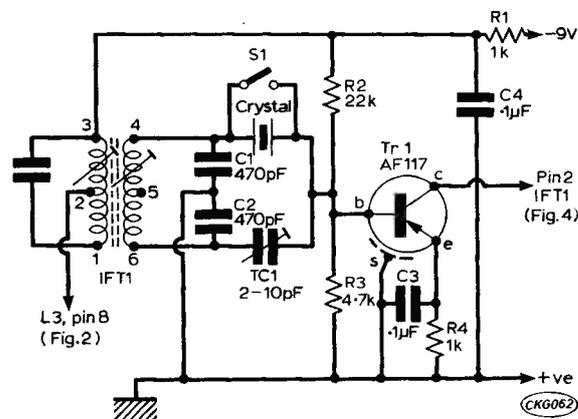
R. H. LONGDEN

CRYSTAL FILTER

Fig. 6 is the circuit of this unit and if fitted is placed between the oscillator coil L3 (Fig. 2) and the i.f. amplifier described. The filter i.f. transformer provides a balanced output at pins 4 and 6, TC1 being adjusted to compensate for stray capacity in the crystal and parallel switch. In these circumstances selectivity can be extremely high but as the crystal works into a moderately high impedance here the passband is wide enough for a.m. reception without too much deterioration of speech quality.

When the switch is closed, the crystal is out of use, and the selectivity is that provided by the four i.f.t.'s.

The filter i.f.t. has to be modified, to obtain a centre-tap (pin 5 is unsuitable). Pull the screening can off the i.f.t. A small capacitor is wired internally between pins 4 and 6 and this component is snipped off. (The similar capacitor between pins 1 and 3 must be left). The i.f.t. is then replaced in its can. The parallel capacitance is now provided by the two capacitors C1 and C2, wired externally.



Construction. The filter is assembled complete on a piece of paxolin or Veroboard 3×1in. as in Fig. 7.

A black flying lead (or pin) is provided for the negative connection. The unit is mounted by two 1in. bolts, with extra nuts which provide the chassis return. When the unit is fixed to the receiver chassis, the lead from pin 8 on the oscillator coil is near the filter i.f.t., and can be soldered to pin 2. The lead from pin 2 of i.f.t.1, (Fig. 4), is now soldered to the collector lead of the filter unit transistor or to a pin used as anchorage.

A hole must be drilled in the chassis to reach the lower core of the i.f.t. Two insulated leads are soldered to the crystal holder sockets passing directly down through holes to the crystal switch.

The crystal switch is fixed directly under the crystal. It can be a rotary switch, fitted to a bracket, with a coupling and extension spindle. Alternatively a switch wafer can be attached to the back chassis runner with 1/2in. spacers and operated by a 1/4in. dia. polystyrene rod cut to fit.

Filter Adjustment. A signal generator and output meter are helpful, though adjustment is possible by ear. The highest selectivity obtainable is very sharp so having adjustments a little off maximum is an advantage. Adjustment may need some patience, depending on how close the crystal and i.f.t. frequencies match at the beginning.

If alignment is badly out, no signals at all may be heard. If so, align the i.f.t.'s as described earlier, switch the crystal out (switch closed) and adjust the two filter cores for best volume. Set the phasing capacitor TC1 about half closed.

Fig. 6: (top left) shows the circuit for the optional crystal filter, IFT1 being modified as described in the text. Fig. 7: (left) gives the layout of the filter on its 3 x 1in. board.

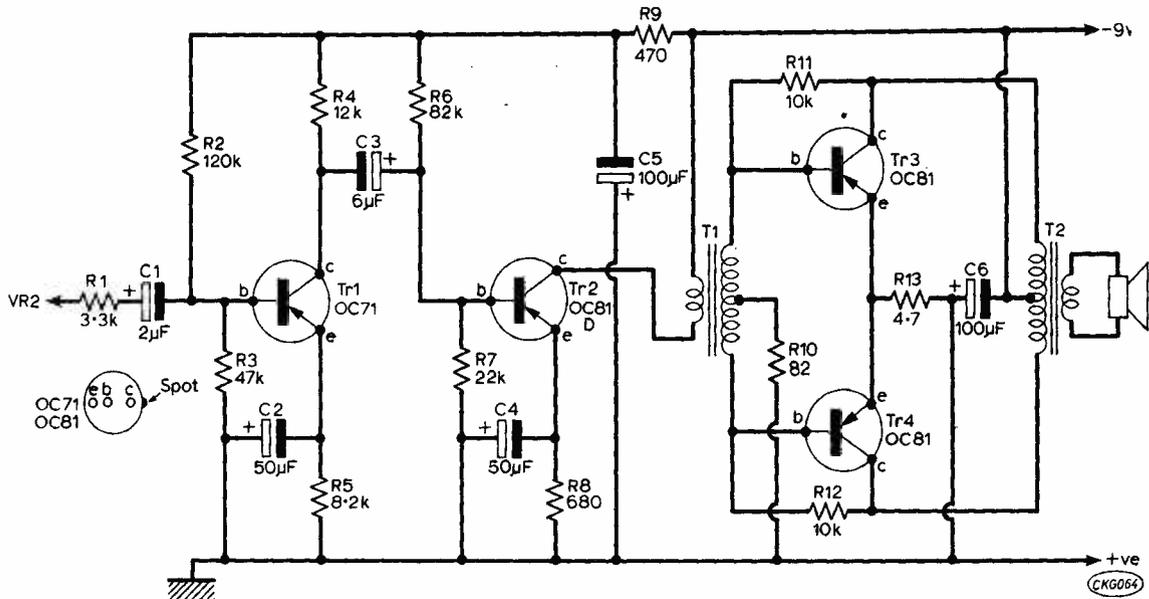


Fig. 8: Circuit of the audio stages, fed from the detector stage (Fig. 4, Part 1) via the volume control VR2 mounted on the front panel.

Open the crystal switch, and tune the receiver (or generator). If results are much as before, crystal and i.f.t.'s are by no means on the same frequency. Assuming no generator or other means of checking the frequency of the i.f.t.'s is available, switch the crystal out, adjust all seven i.f.t. cores about a half turn in the same direction, and re-peak them for best results. If bringing in the crystal now sharpens tuning, the shift made to the intermediate frequency was correct. If results seem little changed or worse, the shift was the wrong way, so all the cores have to be moved in the opposite direction.

When crystal and i.f.t.'s are approximately in agreement, tuning through a signal (or tuning the generator) will show two tuning points. One is extremely sharp, and is not changed by adjusting the cores of the i.f.t.'s in later stages. The other is flatter, and can be moved by rotating the cores. The sharp peak is the crystal resonance. Tune to it and then rotate each i.f.t. core to the same frequency, as indicated by a great increase in sensitivity and the eventual disappearance of the second, flatter response.

With i.f.t.'s aligned to the crystal frequency, tune through a signal (or tune the generator) while

adjusting the phasing capacitor TC1. If TC1 is completely unscrewed, a very sharp null will be found at one side of the signal, the signal re-appearing as this is passed. If TC1 is fully screwed down, the null arises at the other side of the signal, so it is adjusted to give a reasonably even response. Adjustments may make necessary very slight readjustment of the filter cores.

AUDIO AMPLIFIER

With an unlucky combination of values in the capacitors C1 and C2 the error could prevent phasing. If so, place a 30pF pre-set across C1 or C2, re-adjust the core, and adjust as described. It may be found that exchanging C1 for C2 will suffice. If selectivity worsens with the pre-set at any value, remove it and put it across the other 470pF capacitor.

The circuit for this is shown in Fig. 8. It requires a few more components than directly-coupled circuit but has the advantage that d.c. operating conditions for one stage do not depend on those of other stages, so that unsatisfactory working is not likely, while all items are easily obtained.

Construction. The parts are assembled on an insulated panel $3\frac{1}{2} \times 2$ in. as in Fig. 9. The amplifier can be easily tested by adding a speaker, 9V battery and providing some form of input, such as a pickup, or by connecting it to the receiver volume control.

The amplifier is mounted by two $\frac{1}{2}$ in. 6BA bolts, with extra nuts, which also secure tags, and act as a return to the receiver chassis. In the event of the amplifier drawing a very small current with no signal (say under 3mA) and exhibiting cross-over distortion, the 82Ω resistor R10 may be increased slightly in value, 100Ω being suggested.

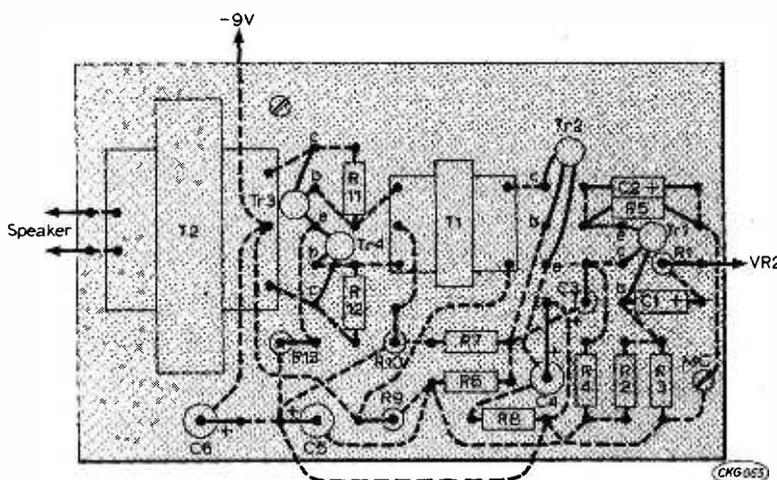


Fig. 9: Layout of the audio amplifier constructed on a $3\frac{1}{2} \times 2$ in. insulated board. It is mounted on top of the chassis with T2 at the rear, see Fig. 12 and photographs.

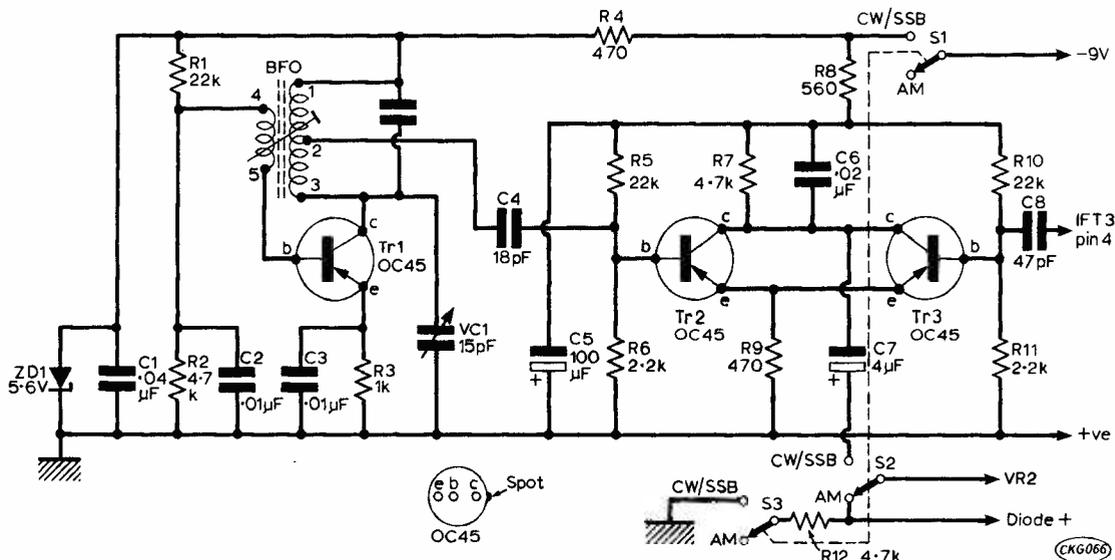


Fig. 10: Circuit of the b.f.o./product detector required for the reception of c.w. and s.s.b. The function switch S1, 2, 3 is mounted on the front panel.

BFO/PRODUCT DETECTOR

The receiver as described so far is intended for a.m. reception and is thus suitable for all normal short wave listening. In some cases it may be wished to receive Morse and single sideband transmissions, especially on the amateur bands. This can be done by using a beat-frequency oscillator/carrier oscillator, with product detector.

The circuit for this unit is shown in Fig. 10. Tr1 is the oscillator, operating at 1.6MHz. This frequency is varied by the panel pitch control VC1. The zener diode ZD1 provides a stable voltage for the oscillator.

Output from the oscillator goes to one of the pair Tr2/Tr3, with c.w. or s.s.b. signals fed in from the i.f. amplifier via C8.

For c.w. reception, VC1 is adjusted so that the required audio heterodyne note is produced.

For s.s.b. reception, Tr1 operates as carrier oscillator, to replace the carrier removed during s.s.b. transmission, thus allowing the s.s.b. signal to be resolved.

A rotary function switch provides for c.w./s.s.b. reception or a.m. Section S1 interrupts the negative line for a.m. reception, while section S2 switches the volume control VR2 to the product detector circuit, or existing a.m. diode detector, as required. Section S3 brings in R12 for c.w./s.s.b. to complete the diode circuit made through VR2 during a.m. reception.

Construction. The components are assembled on an insulated board as in Fig. 11. All components, including the b.f.o. coil, are on this side of the board, so it must be checked that coil connections are correct when turning the board over.

Flying leads are provided for external connections and the board mounted clear of the chassis by 1/2 in. bolts with extra nuts. The point MC is a tag locked to the board thus completing the circuit to the metal chassis when the assembly is mounted in place.

Capacitor C8 is near the final i.f.t. a lead being soldered to pin 4 of the latter and passing through the chassis to C8.

A black lead from R4 is connected to S1, which completes this circuit for c.w./s.s.b. reception only.

VR2 is disconnected from the diode circuit and taken to S2. This connects to C7 in the c.w./s.s.b. position and to the diode (as originally) for a.m. reception. R12 is wired directly to the switch as in Fig. 10.

Alignment. With the switch in the a.m. position, reception should be as before but the final i.f.t. core will require a slight adjustment for best results.

Set VC1 half closed, switch to c.w./s.s.b., and rotate the b.f.o. coil core until a strong heterodyne is heard. Leave the core at the central 'zero beat' position. Turning VC1 either way will now produce a heterodyne which rises in pitch.

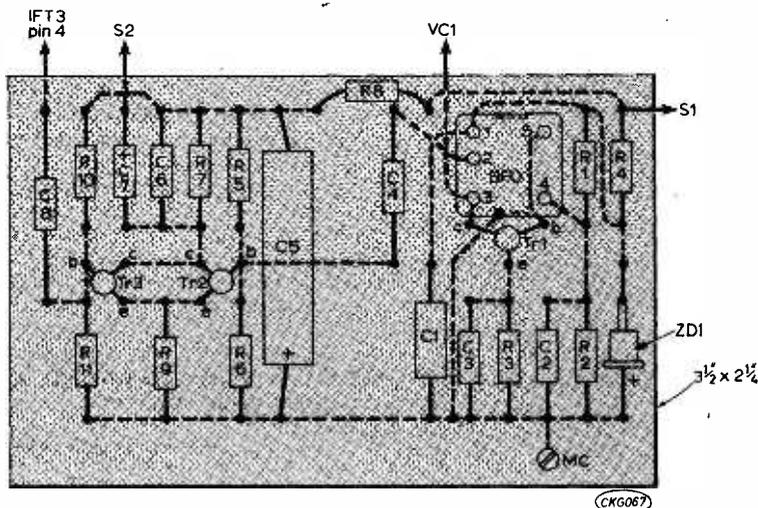


Fig. 11: Layout of the b.f.o./p.d. which is mounted under the chassis below the audio amplifier board.

★ components list

CRYSTAL FILTER

Resistors:

R1 1kΩ R2 22kΩ R3 4.7kΩ R4 1kΩ
All ½W 10%

Capacitors:

C1 470pF 1% silver mica C3 0.1μF
C2 470pF 1% silver mica C4 0.1μF
TC1 2—10pF trimmer (Jackson 'Tetter')

Miscellaneous:

Transistor Tr1, AF117. IFT1 (Denco IFT18/1-6 see text for modification). Crystal 1.6 MHz type HC6U (Senator Crystals) and holder. S1, Rotary on-off switch with extension spindle and coupling (see text). Veroboard, plain, 3 x 1in.

AF AMPLIFIER

Resistors:

R1 3.3kΩ R5 8.2kΩ R9 470Ω R13 4.7Ω
R2 120kΩ R6 82kΩ R10 82Ω
R3 47kΩ R7 22kΩ R11 10kΩ
R4 12kΩ R8 680Ω R12 10kΩ
All ½W 10% except R10, 11 and 12 5%

Capacitors:

C1 2μF 6V C3 6μF 6V C5 100μF 12V
C2 50μF 6V C4 50μF 6V C6 100μF 12V

Semiconductors:

Tr1 OC71 Tr2 OC81D T3-4 OC81

Miscellaneous:

T1, driver transformer (Home Radio TR64). T2, output transformer (Home Radio TR65A). Veroboard plain, 3½ x 2in.

BFO/PRODUCT DETECTOR

Resistors:

R1 22kΩ R5 22kΩ R9 470Ω
R2 4.7kΩ R6 2.2kΩ R10 22kΩ
R3 1kΩ R7 4.7kΩ R11 2.2kΩ
R4 470Ω R8 560Ω R12 4.7kΩ
All ½W 10%

Capacitors:

C1 0.04μF C4 18pF SM C7 4μF 12V
C2 0.01μF C5 100μF 12V C8 47pF SM
C3 0.01μF C6 0.02μF
VC1 15pF variable (Jackson Type C804)

Semiconductors:

Tr1 OC45 Tr2 OC45 Tr3 OC45
ZD1 zener diode 5.6V

Miscellaneous:

BFO (Denco IFT 17/1-6). S1-3, 3 pole 2-way rotary switch. Veroboard, plain 3½ x 2½in.

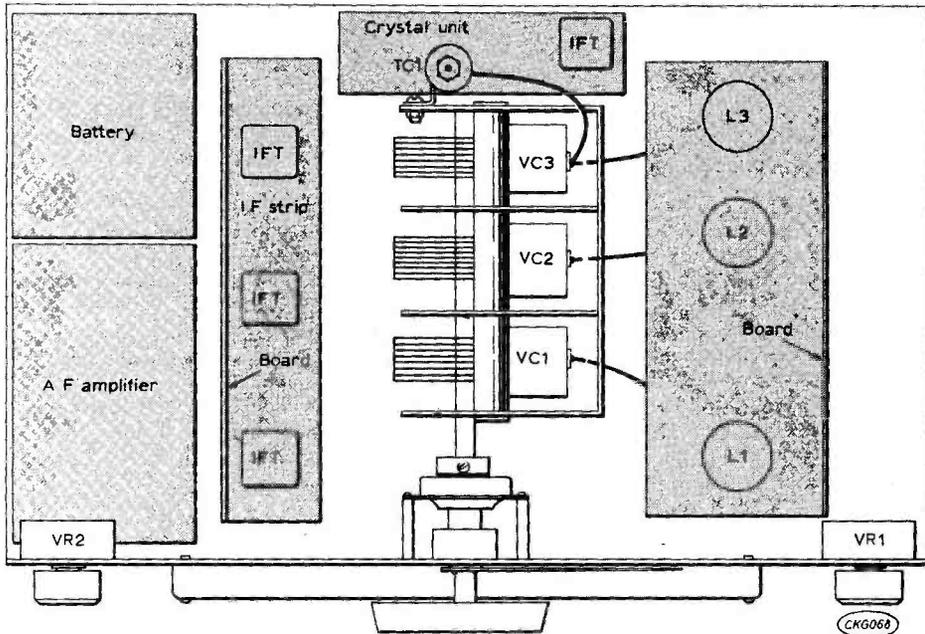


Fig. 12: Location of four of the units and the battery, the b.f.o./p.d. being mounted underneath. Compare with photographs. An aluminium screen was later fitted between L1 and L2 on the r.f. unit, to improve stability. This can be seen in the photographs. Mounting instructions are included with the tuning dial.

When a c.w. signal is tuned in adjust VC1 for best reception the b.f.o. being above or below the signal, whichever results in least interference from other signals.

When receiving s.s.b., VC1 is carefully adjusted to give best resolution of speech. If resolution is impossible, the oscillator is being tuned to the wrong side band of the s.s.b. signal. The same sideband is nor-

mally in use on any one amateur band, so the adjustment of VC1 will hold good for that band.

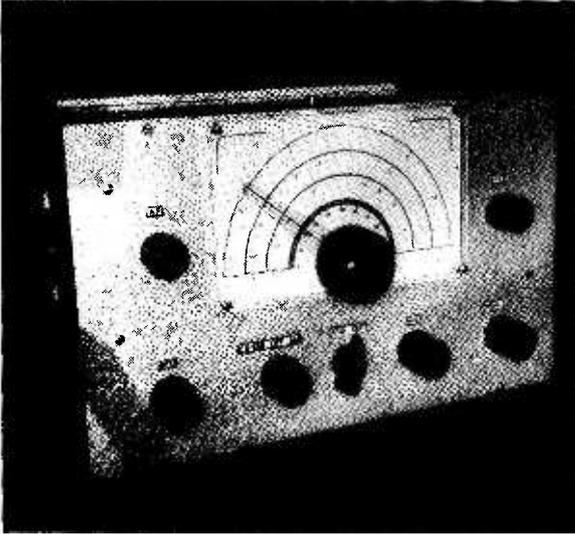
With s.s.b. it is normally necessary to reduce r.f. gain somewhat by operating VR1. If the crystal is in use, tune in the s.s.b. with the switch at a.m., then switch to s.s.b. and adjust VC1 for best resolution. VC1 can then be generally left untouched while tuning the band for other s.s.b. signals.

GENERAL CONSTRUCTION

Connections and placement of controls, etc., are as follows:

VR1. This is fitted at the right of the panel. Leads from the r.f. and i.f. units go to one outer tag. The centre and other outer tags are wired to chassis.

VR2. This fits at the left. ZD1 positive runs to one outer tag, the centre tag goes to the a.f. amplifier, and the other outer tag to chassis. (If rotating the



Panel layout. Top left, Volume control and top right, r.f. gain control. Left to right below:—b.f.o. tuning, function switch, crystal filter in/out, mixer and aerial tuning.

knob gives reversed control of volume, change over the leads to the outer tags. This also applies to VR1.) Connect one switch tag to chassis, and a red lead with positive clip to the other switch tag.

VC4. This is located between the crystal switch and VR1, and is connected to a lead from VC1. VC5 is similarly connected to VC2. Rotor tags are earthed to an adjacent tag bolted to the chassis.

Negatives. An insulated tag is bolted underneath the chassis near the a.f. amplifier, and is an anchor point for battery negative, and the negative leads running from each unit.

Aerial-Earth. Two sockets are fitted to the rear chassis runner. That for earth is connected to the chassis. The lead from pin 8, L1, runs to the Aerial socket.

Speaker. The secondary leads from T2 run to separate sockets, or a jack outlet. A 2/3 ohm speaker is required, fitted in a cabinet or attached to a baffle board. For c.w. reception low impedance headphones should be used.

Panel. This is secured to the chassis by the control bush nuts and two brackets. The tuning drive is fitted by the method described in the instructions supplied with it.

Cabinet. Holes are punched in the back, level with the sockets. An opening lid is made in order to reach the coils and the battery, which rests on the chassis near the a.f. amplifier. Small holes are drilled close together in order to start a metal-saw, and a piece about 10×5in. cut out. Two strips of metal about 6×1in. are fixed inside with countersunk screws, for the lid to close against. It swings on a 10in. hinge bolted at the back.

CO! CO! CO! CO! CO!

INFORMATION WANTED

...can anyone suggest a suitable speaker for use with my "Mellophone 3" set. It is mounted in a smart mahogany cabinet standing on legs. Valves used are PM2DX, PM1LF (2), and three PM2A's.—H. Owen, 34 Bentgate Street, Newhey, Rochdale, Lancashire.

...can anyone please lend me a copy of Modern Wireless No. 1.—L. A. Slack, 60 Parsons Road, Withington, Manchester, M20 3WQ.
...I have recently acquired a Carlton SG 4 receiver about 40 years old and I cannot find any gen on it at all (valves, types, etc.). Please can anyone help.—A. C. Lintoff, 3 Seaham Street, Silksworth, Sunderland, SR3 1EX.

...details and copies of radio circuits from early editions of radio magazines, as I wish to renovate some Vintage receivers.—S. Laffan, St. Kieran's College, Kilkenny Ireland.

...any gen on the μ A 703C i.c.—J. Rowley, 18 Old Park Road, Shirehampton, Bristol, BS11 0PW.

...any gen on the Rx type R1475 p.s.u. type R360 and tuner unit type 131.—C. Astbury, 16 Eaton Avenue, Handbridge, Chester, CH4 7HB.

...any gen on R4187 S.T.C. set 17 valve, 24 channel receiver circuit. Manual and mods for mains. Loan or buy. Also back nos. P.W. for last 10 years. Sell at cover price plus postage.—K. Armstrong, 11 Woodville Gardens, Ruislip, Middx.

...circuit and details of R209 Rx. Also gen on B2 (spy) receiver and layout if possible.

—I. L. Bishop, 27 Stratton Way, Biggleswade, Beds.

...any gen on Reiner Electronics Oscilloscope No. 556. Service Manual, modification details etc. Will return.—R. P. Davies, 61 Kenley Road, Kingston, Surrey.

...circuit or information on capacitor analyser (Solar) type CB-2U. Loan or purchase.

—R. Kirk, 22 BarnCraig Street, Buchhaven, Fife, Scotland.

...circuit diagram and gen on the R1155 Rx. I will copy and return.—A. McKenzie, 6 Moorfield, Newcastle upon Tyne, 2.

...service sheet for Pamphonic Reproducers Ltd. type 3000 stereo amplifier.—R. W. Parker, 11 Greenacres, Downton, Salisbury, Wilts.

...any gen on "Contessa" receiver which is 5 to 8 years old with 6 transistors and a diode and appears to be 2 i.f. stages. The tuning dial contains the word Contessa and at the bottom of the speaker fret it reads "transistor".—H. Gosling, 12 Ullswater Avenue, Halfway, Sheffield.

...any info on making a rumble and scratch filter.—N. Davidson, Leamington House, Dover College, Dover, Kent.

...any hints and mods of the p.s.u. of the 19 set so that we can remove dynamotors.—United World College of the Atlantic, St. Donat's Castle, Llantwit Major, Glamorgan, CF8 9WJ.

...instruction manual for Airmec 877 Teletest test set.—D. Wigley, 4 Sollons Avenue, Harlesden, London, N.W.10.

...any info on converting the 19 set Tx/Rx.—M. Saxon, Shepherd's Fennel, Hendon Wood Lane, London, NW7 4HR.

...circuit for a.m./f.m. tuner with a multiplex system.—A. G. Sobers, c/o Donnachie, 161 Octavia Court, Greenock, Renfrewshire, Scotland.

...circuit and any info on constructing an echo (depth) sounder.—R. Medland, 10 Northfield Way, Brighton, BN1 8SH.

...blueprint or practical circuit for the 4-transistor amplifier published in P.W. November 1961.—B. Edean, 25 Astley Gardens, Seaton Sluice, Whitby Bay, Northumberland.

...circuit diagram of an electronic echo chamber: the type which does not employ an endless tape with multiple heads but one which will produce both sustained echo

reversal and repetitive echo with a variable time factor.—M. Hale, 27 Rachel Gardens, S.W. Oak, Birmingham, B29 6N.

...the circuit diagram of a stylus organ or even the details of the one published in P.W. some years ago.—V. P. Kelly, L/103197 REM(A) Mess 6F1, H.M.S. Ark Royal, BFPO, London.

...blueprints for the following: "Celeste 7-transistor portable" (June 1963), "7Mc/s Transceiver" (June 1964), "Beginners S.W. Superhet" (December 1964) "Progressive S.W. Superhet" (February 1968) and "Mini-Amp" (November 1961).—A. Raza, P.O. Box 2671, Tripoli, Libya.

...circuit or manual for TS210, to loan or buy. Also, any useful mods would be welcome.—D. Millard, 20 Jubilee Road, Tipton, Staffs, DY4 0QP.

EQUIPMENT REQUIRED

...source of supply of small ferrite-cored r.f. chokes of 680 μ H, 470 μ H and 330 μ H.—M. J. Shepherd, 72 Westerland Avenue, Canvey Island, Essex, SS8 8JS.

...where can I obtain i.f. transformers for a Skyrover Radio.—J. B. Valentine, 10 Coleridge House Lane, Springfield, Wigan, Lancs.

...photocell fine line scanner and amplifier to work quick-acting solvent for lightweight equipment. Black and white, on and off.—D. Corbett, 41 Tintof Road, Bearsden, by Glasgow.

BOOKS WANTED

...copies of the Marconigraph, or any other old radio mags. pre 1930. Also a nice set of Harnsworth's Wireless Encyclopedia.—C. Riches, Practical Wireless Editorial Dept., Fleetway House, Farringdon Street, London, EC4A 4AD.

CORRESPONDENTS WANTED

...any one interested in electronics whether it be ham radio, Hi-Fi, audio, TV or any other aspect.—Des. Walsh, E15CD, "Coombe Down", Ballylynch, Carrick-on-Suir, Co. Tipperary, Ireland.

...P.E. May and July 1970. Will exchange for P.E. September to October 1969.—Des. Walsh, "Coombe Down", Ballylynch, Carrick-on-Suir, Co. Tipperary, Ireland.

ISSUES WANTED

...1950-1955 and Radio Const. 1950-1958.—Lurton, 12 The Vale, Acton, London, W3 7SB

...and March 1971 P.W.—R. Watson, 51 Woodbridge Road, Newbourne, N. Woodbridge, Suffolk.

...Television for Oct. 1967, Feb., March, April, May, June, July 1968; April, May, June, July 1969 and Dec. 1970.—P. F. Johnson, 21 Jubilee Drive, Sheringham, Norfolk.

...Radio Amateur Sept. 1953, RSGB Bulletin February 1953, S.W. Mag. Oct. 1948 and Dec. 1954.—I. Simpson, 2 Taylor Cottages, Derryhall, Portadown, Co. Armagh, N.I.

...Jan. to Nov. 1966, July 1967, Jan., Feb., March 1968, index for Vols. 41 to 46 (all P.W.), P. Electronics for Jan. to Nov. 1966, Nov., Dec. 1967, Jan., March 1968, Jan. to Nov. 1969, Nov. 1970, April 1971 and index for Vols. 1 to 6.—H. Ferns, 11 King Street, Coatbridge, Lanarkshire, Scotland.

...issue of P.W. Jan. 1962 containing "Minuette".—S. Grosvenor, 50 Countess Crescent, Bisham, Blackpool, FY2 9LQ.

...P.W. for June and July 1968 also Jan. 1971. P.E. issues Jan. to March 1970 inclusive.—A. Taylor, 89 Howth Drive, Woodley, Nr. Reading.

...P.W. September and October 1970.—W. R. Pitt, 26 Highdown Avenue, Worthing, Sussex.

...P.W. June 1971. F. J. Camm's "Beginners' Guide to Radio" (5th or 6th edition). Also "Elementary Course in 28 Lessons", and P.W. July 1948.—H. Howard Shepherd, 5 Paifford Avenue, Watcombe, Torquay, TQ2 8BS.

...The issue of P. Television containing the "Viewmaster".—E. Farrer, 108 Colne Road, Twickenham, Middx.

...P.W. Sept., Oct. and Dec. 1970 and Oct., Nov. and Dec. 1971.—C. J. Page, Flat 6, 17 Devonshire Terrace, Lancaster Gate, London, W.2.

...April 1971 issue of P.W.—T. M. Fresson, Fernilee, Churt, Farnham, Surrey.

...P.W. July 1960.—T. Richards, 22 Cookson Street, Liverpool, L1 5EH.

...P.W. August 1968 and issues containing the Portable Keyless Organ.—K. Oliver, 10 Mayflower Road, Shirley, Southampton, Hants.

...P.T. July 1971 with the 625 i.f. strip.—O. Collins, Landford, Germansweg, Bearworthy, Devon.

TAKE 20

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

THIS month's project is one for the DXers; it is a noise limiter circuit that can either be built into a receiver or used as a separate unit, in which case it fits between the headphones and the receiver.

Noise is a real curse when listening to weak, far off stations and of course its amplitude bears no relationship to that of the signal that you want to hear. A comparatively simple circuit, Fig. 1, will eliminate all signals above a certain level while unaffected those below that level. Our ears have a sort of a.g.c. system built into them, if they are subjected to a series of loud noises they will not be very sensitive to quieter passages in between those bursts, so, however loudly you turn up the volume, this will not improve intelligibility. By limiting the level of the peaks to that of the wanted signal there is a considerable improvement and signals which were quite lost in the noise can be heard comparatively well.

Let us assume that the unit is to be used from the output of the receiver. This output may be the equivalent of an external loudspeaker socket or a special headphone output, it depends on the design and type of receiver. If the socket is for an external loudspeaker and the output stage is a transistorised one, it is important that the output load is maintained and a resistor equivalent to the speaker impedance should be fitted, in the circuit shown as R1. If you are not sure what the value should be 10Ω will be satisfactory.

The input is connected via the level control VR1 to Tr1 where the signal is amplified. The output of this is fed via C3 to the back-to-back silicon diodes D1 and D2. These are not directly biased but as soon as the level of the signal across these goes over about 0.6V, they will conduct; one of them clips the positive peaks while the other takes care of the negative peaks. It doesn't matter how high the signal level is, anything above this level will appear as a maximum of 0.6V. Since we shall now always have the same level at this point we have removed our control over the listening volume and for this reason VR2 is included.

If the *wanted* signal level is above the critical 0.6V, this will introduce distortion and it is in this way that the controls are set. The receiver's volume control should be set for normal listening level and, with the unit connected, VR1 should be increased until the wanted signal becomes distorted and harsh; this should then be backed off slightly. VR2 is then set for a comfortable listening level.

The current consumption of the circuit is not high and a small PP3 battery will cope nicely. For fixing the circuit permanently into a set, VR1 can be the existing volume control, it doesn't matter even if the value of this is considerably higher than that

No. 36 NOISE LIMITER

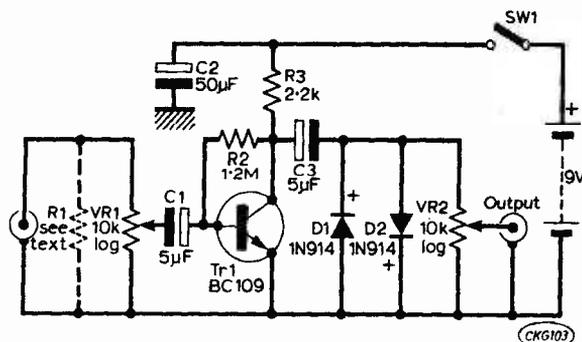


Fig. 1 (above): The circuit of the noise limiter.

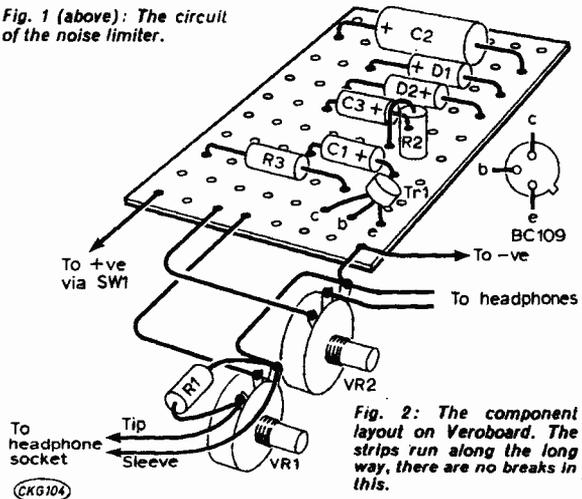


Fig. 2: The component layout on Veroboard. The strips run along the long way, there are no breaks in this.

★ components list

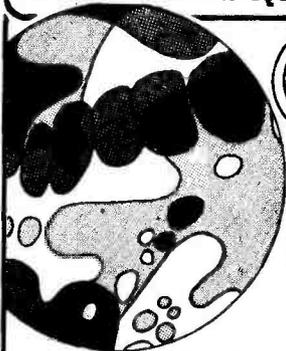
R1	10Ω, 5W—see text	—
R2	1.2MΩ 5%, ½W	1p
R3	2.2kΩ 5%, ½W	1p
C1	5µF 10V minimum	4p
C2	50µF 10V minimum	4p
C3	5µF 10V minimum	4p
Tr1	BC109	12p
D1	1N914	5p
D2	1N914	5p
VR1	10kΩ log. pot	12p
VR2	10kΩ log. pot	12p
SW1	On-off switch	10p
		70p

Prices are those recently advertised in Practical Wireless and may have changed. No allowance is made for minimum order costs or for postage and packing and these should be checked carefully before ordering.

shown. The output from VR2 can then be connected to the point that was previously fed from the volume control's slider. If used with a valve set the supply voltage can be taken from the h.t. line via a suitable dropping resistor to give 9V. A switch can also be included to switch the unit either in or out. ■

Discoscene

EFFECTS LIGHTING EQUIPMENT



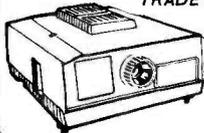
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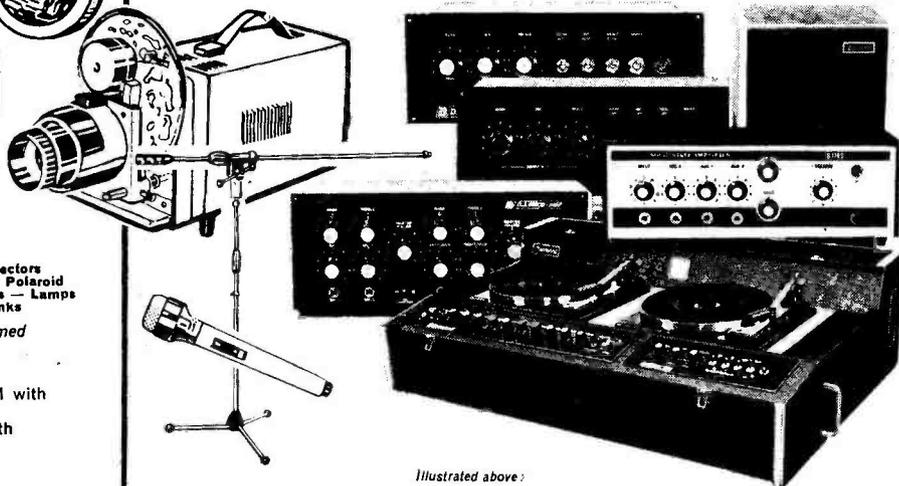
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DISCO SUPER. Two high quality turntables, pre-amp. cross-fade between decks, pre-fade and listen facilities, mic over-ride, aux inputs, full controls for all facilities, deck inputs via break-jacks. And VU meter for visual monitoring of inputs and outputs. Headphone monitor socket. Output 100 watts r.m.s. DJ 30L Mk. II Sound to Light Unit incorporated. Also available **DISCO-PLINTH, DISCO-IMP, DISCO MINI and DISCO STANDARD**, as 'Super' less Light Unit. 100 watts r.m.s.

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PSYCHEDELIC SOUND TO LIGHT CONTROL UNIT DJ 30L Mk. II 1,000 watts per channel over three channels—bass, mid, and treble

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SHORT WAVES

MONTHLY NEWS FOR DX LISTENERS

THE recent spell of cold weather seems to have kept most of the readers of this column in their shacks and at their writing desks, this is evidenced by the number of reports received—the record having been beaten yet again.

The first report comes from **Ian Howes** in Lowestoft who used his R209 Mk II receiver and TV antenna to log the following interesting stations:—

- 3375 AIR, *Gauhati* with Indian Music at 1700.
- 4780 R. *Carabobo, Venezuela*, Spanish at 0015.
- 4860 AIR, *Delhi*, Domestic Service at 1800.
- 4880 R. *Universo, Venezuela*, Spanish at 2315.
- 4965 SABC, Domestic Service at 2100.
- 5000 R. *Nepal* in Nepali at 1540.
- 5035 *Alma Ata, USSR* at 1600.
- 5035 *Bangui, Cent. Afr. Rep.*, French at 2230.
- 5047 R. *Lome, Togo*, news in French at 2200.
- 5052 R. *Singapore*, English Pops at 1600.
- 9660 ABC, *Brisbane*, Home Service at 1200.
- 11835 R. *El Espectador, Uruguay*, Spanish at 2304.
- 15430 *Voice of Free Korea* in English at 1130.

D. A. Hairon of St. Clement, Jersey has again used his Codar CR70A to good effect hearing:—

- 4915 R. *Accra, Ghana* in English at 2300.
- 6170 *Israel B.C.* in English at 2115.
- 9505 R. *Record, Brazil* in Portuguese at 0110.
- 9510 R. *Barquisimeto, Venezuela*, Spanish at 0035.
- 9625 BBC, *Cyprus relay* in Hindi at 0050.
- 11775 AIR in English at 1050.
- 11850 R. *Accra, Ghana* in English at 2030.
- 11875 R. *Soc. de Bahia, Brazil* at 0000.
- 15084 R. *Tehran* in Farsi at 1430.
- 15105 BBC, *Ascension Is.* relay at 0730.
- 15225 R. *Cultural de Bahia, Brazil* at 0100.
- 15230 RT *Belgium* in English at 0050.
- 17825 NHK, *Japan* in English at 0815.

Michael Berry of Dewsbury, Yorkshire is a new reporter to this column, his equipment consists of an Eddystone EB35 receiver and a 15 foot vertical antenna. Amongst the interesting stations heard were:—

- 4870 *Cotonou, Dahomy* in French at 2230.
- 4915 R. *Accra, Ghana* in vernacular at 2215.
- 4940 R. *Abidjan, Ivory Coast* in French at 2305.
- 6040 *Tashkent, USSR* in English at 1420.
- 9520 R. *New Zealand* in English at 0900.
- 9570 R. *Kaduna, Nigeria* in English at 2100.
- 9570 R. *Portales, Chile* in Spanish at 0005.
- 9850 R. *Bangladesh, Dacca* in English at 1515.
- 11710 R.A.E., *Argentina* in English at 2335.
- 11735 RTV *Morocco* in French at 1910.
- 11805 R. *Globo, Brazil* in Portuguese at 2105.
- 11865 R. *Kinshasa* in French at 2230.
- 11925 *Tashkent, USSR* in English at 1410.

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz ● Times in GMT

- 11925 R. *Bandierantes, Brazil* in Portuguese, 2145.
- 15190 ETLF, *Addis Ababa* in Arabic at 1430.
- 15520 R. *Bangladesh, Dacca* in English at 1230.

Julian V. Moss of Rayleigh used his Meridian 10 transistor superhet and 60 foot long-wire antenna to compile his latest log which includes:—

- 9515 R. *Ankara, Turkey* in English at 2200.
- 9525 AIR, *Delhi* in English at 1945.
- 9545 R. *Accra, Ghana* news in English at 2045.
- 9605 R. *Canada International*, English at 2100.
- 9695 RSA, *South Africa* in French at 2015.
- 11620 AIR, *Delhi* news in English at 1945.
- 11710 VOA, *Liberia* sign off at 2230.
- 11720 R. *Canada International*, English at 2207.
- 11780 HCJB, *Quito, Ecuador* in English at 2000.
- 11850 R. *Accra, Ghana* news in English at 2030.
- 11900 RSA, *South Africa* in English at 2235.
- 11910 ETLF, *Addis Ababa* in English at 2015.
- 11920 *Abidjan, Ivory Coast* in English at 1845.
- 11950 FEBA, *Seychelles* in English at 1730.
- 11970 RSA, *South Africa* in English at 2240.

Brian Ewing of Ilford is another reporter with a Codar CR70A receiver, this time used with a 50 foot long-wire antenna to hear:—

- 6010 RAI, *Rome, Italy* at 0110.
- 6155 R. *Renascena, Portugal* (tentative) at 0030.
- 9510 BBC, *Ascension Is.* relay at 0415.
- 9615 HCJB, *Quito, Ecuador* at 0330.
- 9695 RSA, *South Africa* noted at 2215.
- 9730 ETLF, *Ethiopia* at 0400.
- 11815 TWR, *Bonaire* noted at 0130.
- 11850 BBC, *Tebrau, Malaysia* relay at 2345.
- 11925 *Radio Kuwait* at 2040.
- 11930 WIBS, *Windward Islands* at 2031.
- 11955 *Radio Lebanon* at 0235.
- 15170 ELWA, *Liberia* at 2159.

The last reporter for this month is **Fred Wall** of Walthamstow who has a Plessey PR155 (short pause whilst your scribe goes green with jealousy) and a 20 foot long-wire enabling him to hear:—

- 9460 *Radio Pakistan* with music at 2020.
- 9520 *Radio New Zealand* in English at 0900.
- 9745 *Radio Baghdad* with music at 2040.
- 9755 *Radio New Zealand* at 1700.
- 15240 *Radio Australia* with news at 2153.
- 15245 RTV *Morocco*, news in Spanish at 1415.
- 15345 *Radio Kuwait*, Pop Music at 1600.
- 17820 *Radio Ankara*, news in English at 1330.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

SHORT WAVES

THE AMATEUR BANDS

David Gibson, G3JDG

Frequencies in kHz ● Times in GMT

THINGS are hotting up r.f.-wise at Moretons, Harrow. The "Dorms" are bedecked with sneaky antennas of varying shapes and sizes and are used by an enthusiastic band of s.w.l.s. **Jonathan Thackeray** is one and pleads guilty to listening on the Amateur bands by fixing an H.A.C. one-valver onto his modest 15ft. end fed. If you are having a chuckle at all this, observe Master Thackeray's log for 80 metres; JA5TY, JY1/B, UL7IAF, UP2TP, VE1FO, VE3QA, VK2LF, VO1MG, VP9UN, VQ9R, 4X4DP, 9H3B, 9K2AL. Definitely ten out of ten for that splendid effort. (Write out one hundred lines, "I must not receive better DX on eighty than G3JDG!")

It seems that most listeners kept their ears draped over the l.f. bands this past month. Log from **David Lawley** (Gravesend) shows a fair bit of activity on top band. Gear is a CR70A plus 220ft. folded long-wire with a quarter wave counterpoise earth for topband. All stations are c.w. unless marked; DJ4SS (s.s.b.), DL1CF, DL9KR, EI8BF, EI9BG, EI9J, GD3GM (s.s.b.), GM3-IGW, UKG, YCB, YOR, ZDH, GW3-UCB, UPK, YTO, HB9-CM, NL, OK1-ATP, AYY, KYS, MA, SBT, OL1AOH, OL5ANJ, PA0PN, W1BB/1, W1HGT. David bagged 195 countries last year, has already heard 85 this year and hopes to take the R.A.E. on May 9 (Gd lk OM).

John Runchman reports "A" level QRM but has managed a few late night/early morning sessions as a nice change from delta y tending to zero! Receiver is a homebrew two-valve t.r.f. (ECC83/ECL82—what funny transistor numbers) with a 20-metre dipole. Topband c.w. brought in: EI8H, HB9ANW, HB9CM, HB9NL, OK1ATP, OK1MAC, PA0PN. Just in case you think that two valves isn't very much you are quite right. The following log received on this set for 14MHz tends to add weight to the argument that it's what's between the headphones that counts; CN8GG, EA6BM/M, EA8HR, G3RFP/MM, LU2AJE, PJ2CL, PY1CBS, PY1DG (no relation!), PY1ZAN, PY2DVH, PY4AP, PY7OS, PZ1DR, UC2DX, VO1CU, VP2MZ, VP9CP, YV4AOW, YV6IP, 4S7SW (Ceylon), 4X4BL, 7X2BK, 9G1FF, 9H1CQ, 9Q5ITU, 9Q5RD. All this with a t.r.f., that should get some "reaction" from the superhet fraternity? Incidentally, John's QTH is South Norwood, London.

News from **Karl Muller** in the land of 3D6 (that's Swaziland in Southern Africa) that FL8HM and FL8MM both operate on band edge of 7MHz c.w. but he doesn't say the QTR. Karl has a Barlow-Wadley XCR-30 receiver with a 30ft. end fed and an a.t.u. The following made it into Swaziland on 7MHz c.w.; CM3LN, CR6AI, DK1EB, DU1IOR, FB8XX, FL8HM, FL8MM, HC2HM, JA1OHU, JA3EA, JA3PMB/6, JA5ADR, KP4DJE, KR6AY, LA2QI, OK2KYI, PY1BSN, PY3MU, TU2BK, VP2AAA, W6GRU, W7DI, ZD8BR, 4S7DA, 5R8BD, 6W8AL, 9M2CW. Incidentally, on ten metres Karl logged G3UGM.

He also asks if people who work s.s.b. have callsigns and enquires why certain YU and LZ stations spend half an hour calling CQ on top of DX stations? (Yeah, well...).

Patrick Funnell reports on a pirate station on topband signing G4NCC who, apparently, spends his hours taking the mickey out of Amateur radio. Be warned friend, in this transistor age many Amateurs have some very simple but excellent d.f. equipment. All it needs is two of them to hear you and get a fix, and where the lines cross—that's you. Patrick has a BC312 receiver and a "... piece of wire in the loft." This set-up logged these on topband: EI9J, GM3IGW, GM3YOR, GM4AGG, OK1ATP, OK1JAX, OK1KYS, OK1NRX, all on c.w. and heard between 1830kHz and 1840kHz.

Eighty metres seems to be a strange band. Some acclaim it as just great while others give a clear "thumbs down" sign, or something.

Steve Taylor (Abbey Wood, S.E.2) reckons there's a lot of "G" activity about judging by what he heard on his CR70A. **Stefan Kaye** (Witney, Oxon) sends in a good log of eighty metre happenings bagged with the aid of an AR88D and 180ft. long-wire which is untuned. Pickings include: EA8HA, OA4OS, VE1ADV, VE1AU, VP2LAT, WB0FFG/TF, XE1KB, ZL3GS, ZL3RK, ZL4AV, ZL4KE, 4X4UF, 9H1BX, 9H1C, 9H3B.

"My first log to the Amateur Bands", says **John Vaarnela** of Croydon Park, New South Wales, Australia. Receiver is a BC348Q and the antenna a dipole at 25ft. Squeaks of s.s.b. on 14MHz heard from: A2CAB, CE1LU, CN2CG, CP1DN, CR6GA, CR7GJ, CX4RZ, EA8GZ, EL0K/MM, ET3JH,, FB8ZZ, FB0WK, FK8ID, FL8MM, FO8DO, FO0TZ, FR7AB, HI8LC, HK1CKY, HK0BKX, HR1BK, HS1ADR, IC8CQS (Capri), JD1KAA, KC6QS, KG6SI, KH6AQ, KR6TQ, KP4DIW, KS6DH, KV4AA, KX6PQ, KZ5GB, LU1SE, MP4BBW, OA4PQ, PJ2MI, PY3ATW, TI2RT, VP1BH, VP9AT, VQ9NEW, VR1AB, VR4EE, VR5FX, VS5PW, VS6BS, VS9MT, VU2ED., XE1KB, XW8DO, YA1AG, YB0AT, YJ8BJ, YK1AA, YN1HC, YS1DET, YV6JB, ZD6HJ, ZD8RR, ZE2KV, ZP5KU, ZS2DH, 3B8CJ, 3D2FM, 4S7PB, 4W1AF, 4X4YT, 5H3LV, 5N2ABG, 5R8AB, 5V3RU, 5W1AU, 5X5NA, 5Z4KZ, 9H1ST, 9K2CP, 9M2GV, 9M8FMF, 9N1MM, 9V1VR. Who said twenty was dead?

Julian Iredale (Llandudno), JR50OSE, Codar PR30, 264ft. end fed got these goodies on 28MHz s.s.b.: K4AUV, K4HGG, VE4OCK, W2BLV, W4GJO, W8QUO, W0ZRX/MM (500 miles north of the Azores), WA5MAK, WB4BMV, WB5CTE, WB4WLI/YV1, ZC4GLW, 4Z4BG, 5R8AP, 7Q7AA, 9J2DG.

Logs, in alphabetical order please, to arrive by the 15th of the month to:

12 Cross Way, Harpenden, Herts.

practically wireless

commentary by HENRY

No. 89
Dim out

SLAVE to the whims and wishes of my readers—the whims of one and the wishes of the other, did I hear you say?—Henry sits here in the light of a flickering candle, like a Dickensian P.W. Editor.

Henry has been remiss. Not gifted with foresight, he to whom tea-leaves are a greater mystery than Rorschach blots failed to provide auxiliary illumination against the day when the power should be cut. The bulb's gone in me torch, innit?

I should have invented something electronic, on the spur of the moment, say the cold eyes around the blank TV. Like all great discoveries, the answer should have come in a blinding flash—well, perhaps that is not the best simile. . . .

As for example, when the transistor was born? Ah, but I'll bet it wasn't at all like that.

Shockley: Let's give it up. Nearly lunchtime.

Brattain: One more try. (He's the meticulous one. Like Spencer Tracy as Edison, he will not give up.)

S. I'm hungry. We are not going to get AFN without a tuning coil, and I'm sick of sharing the same bit of germanium.

B. Right. I'll just leave my cats-whisker here. You can do what you like with yours.



A Dickensian P.W. Editor

Shockley does.

They return, replete and burping. That Bell Laboratories Inc. canteen was notoriously shepherd-pie oriented.

B. Next step, then.

S. Oh., let's start again.

B. No, you measure, I'll inscribe.

S. Just a minute while I suck a—hey—what's this?

B. What's what?

S. Amplification. . . .

B. Well, it is a process of—

S. No, lout. Look! 1mV in, 100mV out. You fiddled the meters.

B. I did not, indeed!

S. Well, somebody did. Let's pack up and invent a fuel cell.

B.—and twenty makes four-hundred—no, listen Shock, we've got something here. We can transfer effective resistance over a link circuit. We can leap a barrier.

S. Don't get romantic. Have some bicarb.

B. Bicarb, hell! Don't you see, this is a breakthrough. No more pot-tiddling. Just stick a couple of cats' whiskers on a slab of germanium and the input resistance changes to a completely different output resistance just by an alteration of voltage. . . .

Of course, dear reader, it did not turn out like that. Some fussy, officious bookmaker from the front office came down to the bogfins' dimly-lit cellar (that's old Bell Inc. for you—my candle is getting low and smelly). He said: Pack it in chaps. Don't forget we own half the Varires company and control Pots Inc. You can't invent the noiseless pot. Let's put it to another use, or scrap it.

And so the transistor, as an amplifying device, was reluctantly dragged forth.

Well, that's my story. But the truth was probably quite different. Most inventions are the result of sweated persistence. 'Eureka' was probably Greek for 'the water's too hot.'

Henry has seen some of this dogged persistence in action. A great friend is an industrial de-



You fiddled the meters

signer. His development chief presents him with impossible problems a couple of times a week. He is given a pretty free hand—enviable job!— and the limiting factor is the utmost reliability and speed of construction. No jerry-built hook-ups for him. His tobacco-tin wizardry is made of cast-iron.

So I wonder how he is getting along in the dim-out? I only hope he did not try to follow the same circuit my colleague tried with the cadmium sulphide cell. Published, he told me, in Pr*ct*c*I *l*ctr*n*cs (R**lly? Ed.). It did not work, and there was no time to find out why.

So this chap being in his way a latter-day Brattain, persisted in racking his brains for past applications and came up with the trigger circuit for an oven control circuit. Problem—no unijunction transistor. Solution, use a pnp in an involuted hookup—good old Shockley's method.

The final result, with two transistors and four resistors, worked a treat. But as the CDS had to be the lower limiting factor of his resistor network, he now has the problem that there is enough infra-red reflected off the ceiling from a television screen to latch the circuit on.

So what, you say, if there is no power, there will be no telly.

That's where you'd be wrong, you see. The first thing he did was to rig up a battery driven inverter to feed the television receiver!

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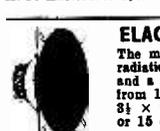
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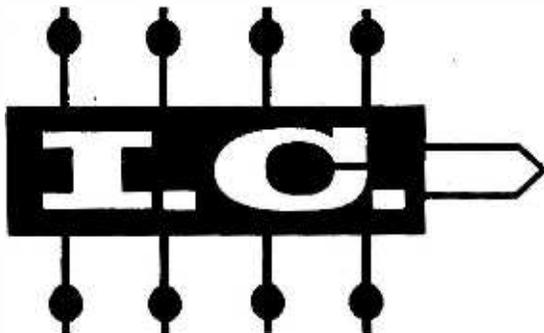
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OF THE MONTH

L.A.J. IRELAND

Number 29

GEC Silicon Switches 2N4990/1

IN the past a number of utility type i.c.'s were reviewed in the "I.C. of the Month" series such as the Mullard TAA320 Bifet or the D13V voltage regulator, etc., and it is quite some time now since any of these three or four terminal devices have appeared. Consequently this month's article is devoted to a review of two specialised monolithic i.c.'s namely the Silicon Unilateral and Bilateral Switch (SUS and SBS) which have recently been released by the General Electric Company. Some useful practical applications of the devices are given.

Operation

In appearance the SUS and SBS resemble a typical small signal transistor mounted in an epoxy TO-98 package, the electrical characteristics of the SUS closely resembling those of an ordinary four layer thyristor. The monolithic chip has a pair of complementary transistors, a zener diode and a resistor

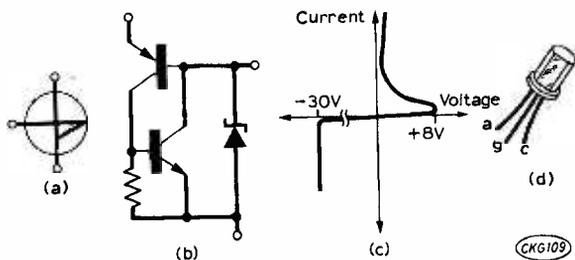
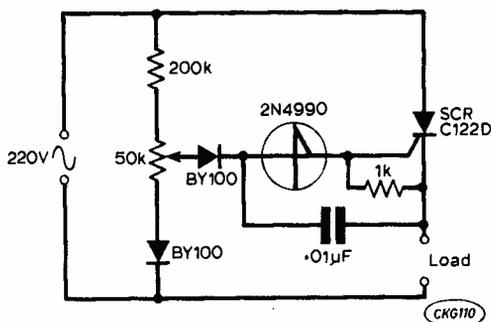


Fig. 1: Circuit symbol (a), equivalent electrical circuit (b), characteristics (c) and outline (d) of the Unilateral Switch 2N4990.

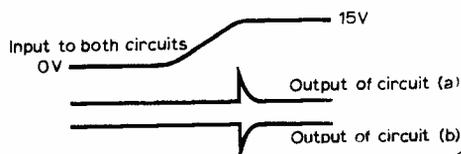
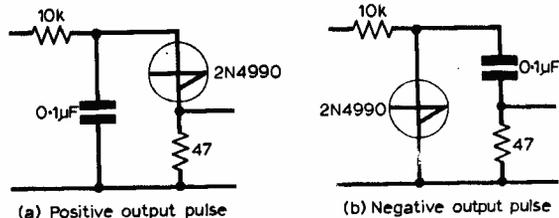
fabricated into it as is shown in Fig. 1. The resulting static electrical characteristics of the device, in which the applied voltage versus current is plotted, is also illustrated and from this graph it can be seen that once the applied voltage exceeds a typical value of about 8 volts rapid forward conduction takes place with the voltage across the device dropping almost to zero.

Applications

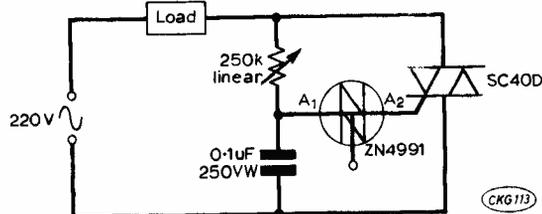
A gate lead is also provided to allow triggering at lower voltages in addition to providing transient-free wave forms, but in most applications this lead



The 2N4990 used as a motor speed control.



Here the 2N4990 SUS is used to generate a rapid pulse from a comparatively slow rising input. Can be used as an over-voltage sensor with the pulse firing a thyristor.

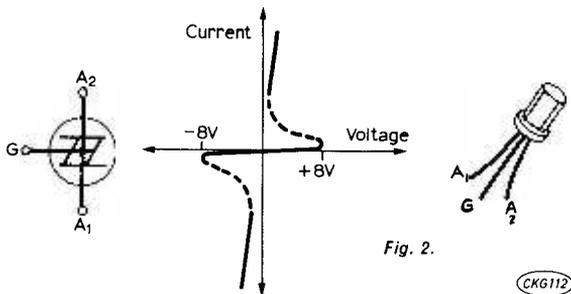


The Silicon Bilateral Switch 2N4991 (SBS) in a mains full wave power control unit.

may be left floating. The SUS therefore is admirably suited for such applications as over-voltage sensing, pulse sharpeners, and SCR triggering. In conjunction with an SCR an efficient and sensitive automatic

over-voltage cut-out sensor can be designed very simply and a number of typical applications of the SUS are given.

Just as the Triac can be considered as consisting of a pair of thyristors connected in inverse parallel so also is the SBS related to its counterpart, the SUS. A schematic diagram of the 2N4991 is illustrated in Fig. 2 accompanied by its static electrical characteristics. It fires in both directions so that in opera-



tion it resembles the ST2 Diac which has established itself as one of the most popular triggering devices in Triac power control circuits. However the 2N4991 has tighter specifications producing sharper pulses than the ST2 although it is offered in the same price bracket as the latter.

Both units are available from Jermyn Industries Ltd., Sevenoaks, Kent.

CHARLES MOLLOY

THE Medium Wave Column

DAVID RICHARDSON of West Ealing has been active on the medium waves with his Lafayette HA230 and medium wave loop antenna. He reports Radio Popular La Palmas on 836kHz; CKBW Bridgewater, Nova Scotia on 1000kHz; WHN New York City 1050kHz; CJRP Quebec, broadcasting in French on 1060kHz; WBAL Baltimore 1090kHz; CBI Sydney, Nova Scotia 1140kHz; CKCV Quebec, in French, 1280kHz; WABK Gardiner, Maine also on 1280kHz; WLAM Lewiston, Maine 1470kHz; WCKY Cincinnati, Ohio 1530kHz. David has also logged the Voice of America Okinawa 1178kHz at 1445hrs SINPO 22432, with a programme in Chinese. This outlet is usually heard in Europe during the afternoon in winter. It has a power of 1000kW, it beams westward into China and sometimes competes with Horby, Sweden on the same frequency when conditions are good.

W. Pennington who lives at Grimethorpe near Barnsley in Yorkshire has built the Radio Nederland MW Frame (Loop) aerial. His receiver is a B40D and on Tuesday February 8th he heard CJON St John's on 930kHz, WINS New York 1010kHz; CBA Moncton, New Brunswick 1070kHz. After midnight he logged CBN 640kHz in St John's; CJOX 710kHz Grand Bank, Nfld; Radio Demerara Guyana 760kHz; WHN 1050kHz and WNEW 1130kHz both in New York City. "I thought it was impossible to receive these stations in England but I have proved it for myself and I find it most interesting" he writes and he suggests that readers may like to write to Radio Nederland, Postbus 222, Hilversum, Holland and ask for a copy of The Frame Aerial leaflet, which gives constructional information on a medium wave loop antenna.

Mike Kerry of Golders Green sends an interesting log of Latin Americans heard on his Eddystone 750 and medium wave loop. These include YVQQ Radio Puerto Cruz, Venezuela on 760kHz; Radio Demerara 760kHz located in Georgetown Guyana, with programme in English; R.Oriental, Uruguay 770kHz; La Voz del Rio Cauca, Colombia 820kHz; Radio Mundial, Rio de Janeiro 860kHz; R.Tamandau, Recife 890kHz; Radio Jornal do Brasil 940kHz; Radio Belgrano, Buenos Aires 950kHz; R.Sutatenza, Colombia 960kHz; Radio Record, Sao Paulo 1000kHz; R.Margarita, Venezuela 1020kHz; R.Revolution Cuba 1060kHz; R.Nacional, Sao Paulo 1100kHz; WBMJ San Juan, Puerto Rico 1190kHz; R.Valera, Venezuela 1230kHz; R.Canaima, Ciudad Bolivar, Venezuela 1290kHz; R.Nacional, Santiago in the Dominican Republic 1380kHz. Mike also mentions the VOA Marathon Key, Florida on 1180kHz which broadcasts in Spanish. Latin Americans become prominent as the year advances and it is worth while listening between 0100hrs GMT and sunrise for the stations listed above.

Please send reports and information about the medium waves to the author at 132 Segars Lane, Southport, PR8 3JG.

TELEVISION

MAY ISSUE

PAL DECODER

This month we start on the construction of the TELEVISION Colour Receiver and go straight to the heart of things—the PAL-D decoder. This is built on a conveniently sized printed circuit board and uses well tried and tested circuitry. The board can of course be used as a separate module with other equipment if the reader wishes. In building this decoder you will have a real opportunity to learn about colour signal decoding through practical experience.

RENOVATING THE RENTALS

The Pye/Ekco T418/11U series gets our attention this month.

WIDEBAND BAND 1 AERIALS

Essential for DX use but not commonly available is the wideband Band 1 aerial. Along with details of practical designs Roger Bunney also presents information on the fundamentals of wideband television aerial design.

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2G381 22p	2N3672 37p	40326 37p	BCY39 60p	BSY11 27p	NKT451 62p
2N484 22p	2N3605 27p	40329 30p	BCY40 50p	BSY24 15p	NKT452 62p
2N696 20p	2N3607 27p	40344 27p	BCY42 15p	BSY25 15p	NKT453 47p
2N697 17p	2N3703 11p	40347 57p	BCY43 15p	BSY26 17p	NKT603P 32p
2N698 25p	2N3704 10p	40348 58p	BCY54 32p	BSY27 17p	NKT761P 82p
2N705 15p	2N3705 10p	40360 42p	BCY58 22p	BSY28 17p	NK P674F 30p
2N705A 15p	2N3705 10p	40362 47p	BCY59 22p	BSY29 17p	NK P677F 30p
2N708 15p	2N3706 09p	40370 32p	BCY70 20p	BSY36 25p	NK T771 30p
2N709 68p	2N3707 11p	40406 57p	BCY71 25p	BSY37 25p	NKT10419 30p
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2N726 30p	2N3709 09p	40408 53p	BCZ10 27p	BSY39 22p	NKT10519 37p
2N727 30p	2N3710 09p	40410 62p	BCZ11 42p	BSY40 32p	NKT20339 47p
2N911 17p	2N3745 11p	40467A 57p	BD116 11-12	BSY51 32p	NKT20359 32p
2N916 17p	2N3745 11p	40468A 57p	BD121 85p	BSY52 32p	NKT20359 37p
2N918 20p	2N3716 11-20	40600 57p	BD123 82p	BSY53 37p	NKT20359 47p
2N929 25p	2N3791 22-06	AC107 30p	BD124 60p	BSY54 40p	NKT20359 37p
2N980 27p	2N3819 35p	AC126 20p	BD131 75p	BSY56 90p	NKT80111 77p
2N1090 22p	2N3823 37p	AC127 25p	BD132 85p	BSY78 47p	NKT80112 97p
2N1091 22p	2N3854 27p	AC128 20p	BDY10 11-27	BSY79 45p	NKT80112 97p
2N1131 25p	2N3854A 27p	AC134 22p	BDY11 41-61	BSY82 52p	NKT80112 97p
2N1132 25p	2N3855 27p	AC136 25p	BDY17 11-50	BSY90 57p	NKT80112 97p
2N1302 17p	2N3854A 27p	AC137 62p	BDY18 11-75	BSY95A 12p	NKT80112 97p
2N1303 17p	2N3856 30p	AC178 27p	BDY19 11-71	BSW41 37p	NKT80211 97p
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2N1308 20p	2N3859A 38p	ACY21 25p	BDY62 11-25	C426 40p	NKT80216 97p
2N1309 30p	2N3860 13p	ACY22 15p	BDY63 11-25	C427 37p	NKT80216 97p
2N1507 17p	2N3866 11-50	ACY25 20p	BF117 47p	C744 37p	NKT80216 97p
2N1613 25p	2N3877 40p	ACY40 30p	BF163 37p	D16P1 37p	NKT80216 97p
2N1631 25p	2N3877A 40p	ACY41 25p	BF167 18p	D16P2 40p	NKT80216 97p
2N1632 30p	2N3900 37p	ACY44 40p	BF173 19p	D16P3 37p	NKT80216 97p
2N1638 27p	2N3900A 40p	AD140 49p	BF177 30p	D16P4 40p	NKT80216 97p
2N1639 27p	2N3901 40p	AD141 49p	BF178 30p	GET102 30p	NKT80216 97p
2N1671B 11-00	2N3903 35p	AD150 58p	BF179 30p	GET113 30p	NKT80216 97p
2N1711 25p	2N3904 35p	AD161 37p	BF180 35p	GET118 30p	NKT80216 97p
2N1889 32p	2N3905 27p	AD162 37p	BF181 32p	GET119 30p	NKT80216 97p
2N1893 37p	2N3906 27p	AF106 42p	BF184 25p	GET120 52p	NKT80216 97p
2N2147 82p	2N4085 17p	AF114 25p	BF185 42p	GET121 52p	NKT80216 97p
2N2148 57p	2N4089 10p	AF115 25p	BF194 17p	GET122 52p	NKT80216 97p
2N2160 57p	2N4090 10p	AF116 25p	BF195 15p	GET123 52p	NKT80216 97p
2N2183 30p	2N4061 15p	AF117 25p	BF196 45p	GET124 52p	NKT80216 97p
2N2193A 42p	2N4062 18p	AF118 62p	BF197 42p	GET125 52p	NKT80216 97p
2N2194A 30p	2N4244 47p	AF119 30p	BF198 42p	GET126 52p	NKT80216 97p
2N2217 27p	2N4286 17p	AF124 22p	BF200 52p	GET127 52p	NKT80216 97p
2N2218 23p	2N4286 17p	AF125 20p	BP224 14p	GET128 52p	NKT80216 97p
2N2219 23p	2N4287 17p	AF126 20p	BP225 19p	GET129 52p	NKT80216 97p
2N2220 25p	2N4288 17p	AF127 17p	BP226 37p	GET130 52p	NKT80216 97p
2N2221 25p	2N4289 17p	AF128 17p	BP227 37p	GET131 52p	NKT80216 97p
2N2222 30p	2N4290 17p	AF128 42p	BP244 23p	MJ421 11-21	OC70 15p
2N2270 47p	2N4291 17p	AF129 72p	BPW61 47p	MJ430 21-01	OC71 12p
2N2297 30p	2N4292 18p	AF180 58p	BF182 12p	MJ440 95p	OC72 12p
2N2368 17p	2N4293 17p	AF181 42p	BFX13 22p	MJ480 97p	OC73 32p
2N2369 17p	2N5027 55p	AF239 55p	BFX28 25p	MJ481 97p	OC74 32p
2N2369A 17p	2N5028 57p	AF279 47p	BFX30 30p	MJ480 21-00	OC75 25p
2N2410 42p	2N5029 47p	AF280 62p	BFX42 37p	MJ491 11-27	OC77 30p
2N2483 27p	2N5030 42p	AF211 32p	BFX44 37p	MJ1800 22-17	OC81 20p
2N2484 32p	2N5031 12p	AFY26 25p	BFX68 62p	MJ2340 62p	OC81D 22p
2N2485 32p	2N5032 12p	AFY27 25p	BFX74 25p	MJ2340 62p	OC82 25p
2N2490 25p	2N5033 12p	AFY28 27p	BFX85 32p	MJ2340 62p	OC83 25p
2N2613 35p	2N5176 45p	ASY29 27p	BFX86 25p	MPP102 42p	OC139 32p
2N2614 30p	2N5232A 30p	ASY36 25p	BFX87 27p	MPP103 37p	OC140 32p
2N2646 52p	2N5245 46p	ASY50 25p	BFX88 62p	MPP104 37p	OC170 30p
2N2696 32p	2N5246 45p	ASY51 32p	BFX89 62p	MPP105 37p	OC171 30p
2N2711 25p	2N5247 45p	ASY52 32p	BFX90 62p	MPP106 37p	OC172 30p
2N2712 25p	2N5265 23-25	ASY68 32p	BFY10 30p	MPS6538 32p	OC200 40p
2N2713 27p	2N5266 22-75	AY103 11-25	BFY11 42p	NKT124 42p	OC201 60p
2N2714 30p	2N5267 22-82	ARZ21 42p	BFY12 22p	NKT125 27p	OC202 75p
2N2865 62p	2N5306 37p	BC107 10p	BFY13 22p	NKT126 27p	OC203 42p
2N2904 30p	2N5306 30p	BC198 10p	BFY19 22p	NKT128 27p	OC205 90p
2N2905 37p	2N5307 37p	BC199 10p	BFY20 22p	NKT129 27p	OC207 75p
2N2905 37p	2N5308 37p	BC199 10p	BFY21 22p	NKT137 32p	OCPF1 42p
2N2906A 30p	2N5309 62p	BC115 15p	BFY24 25p	NKT210 30p	ORP12 50p
2N2906 25p	2N5310 42p	BC116A 15p	BFY25 45p	NKT211 30p	ORP61 50p
2N2906A 30p	2N5310 42p	BC118 10p	BFY26 20p	NKT212 30p	P346A 22p
2N2907 30p	2N5355 27p	BC121 20p	BFY28 50p	NKT213 30p	TIS84 62p
2N2926 15p	2N5356 32p	BC122 30p	BFY30 50p	NKT214 25p	TIS43 10p
2N2924 15p	2N5356 32p	BC125 30p	BFY41 62p	NKT215 25p	TIS44 10p
2N2925 15p	2N5366 32p	BC126 20p	BFY43 62p	NKT216 25p	TIS45 10p
2N2926 15p	2N5367 37p	BC140 37p	BFY50 25p	NKT217 42p	TIS46 11p
Green 14p	2N5457 37p	BC147 10p	BFY51 20p	NKT219 30p	TIS47 11p
Yellow 15p	28005 25p	BC148 10p	BFY52 25p	NKT223 27p	TIS48 12p
Orange 12p	28020 22-00	BC149 12p	BFY53 25p	NKT224 25p	TIS49 12p
2N3011 30p	2N1202 50p	BC152 10p	BFY54 25p	NKT225 27p	TIS49 17p
2N3014 32p	2N1203 25p	BC167 20p	BFY75 30p	NKT229 30p	TIS51 12p
2N3053 18p	2N1204 25p	BC158 11p	BFY76 42p	NKT237 25p	TIS52 12p
2N3054 46p	28501 32p	BC159 12p	BFY77 57p	NKT238 25p	TIS53 22p
2N3055 62p	28502 35p	BC160 62p	BFY90 67p	NKT240 27p	TIS60 22p
2N3133 25p	28503 37p	BC161 11p	BFY91 27p	NKT241 27p	TIS61 25p
2N3134 30p	3N83 40p	BC168B 10p	BFW59 55p	NKT242 30p	TIS92 27p
2N3135 25p	3N128 70p	BC168C 11p	BFW60 25p	NKT243 62p	TIP29A 50p
2N3136 25p	3N140 77p	BC169B 10p	BPX25 21-65	NKT244 17p	TIP30A 60p
2N3390 25p	3N141 77p	BC169C 12p	BPX29 21-80	NKT245 20p	TIP31A 62p
2N3391 20p	3N142 65p	BC170 12p	BPY10 11-45	NKT261 30p	TIP32A 75p
2N3391A 17p	3N143 67p	BC171 11p	BFY63 37p	NKT262 30p	TIP33A 75p
2N3392 17p	3N152 87p	BC172 15p	BX819 17p	NKT263 30p	TIP33A 75p
2N3393 15p	R.C.A. 52p	BC175 22p	BX820 17p	NKT271 20p	TIP34A 25-05
2N3394 15p	R.C.A. 52p	BC182 10p	BX821 37p	NKT272 20p	TIP36A 22-90
2N3402 22p	40251 32p	BC183 09p	BX822 45p	NKT274 20p	TIP36A 22-90
2N3403 22p	40309 32p	BC184 11p	BX827 47p	NKT275 20p	

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1-11 12-24		1-11 12-24		1-11 12-24	
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SN7402	SN7403	SN7404	SN7405	SN7406	SN7407
0.20 0.18	0.20 0.18	0.24 0.20	0.28 0.24	0.28 0.24	0.28 0.24
SN7408	SN7409	SN7410	SN7411	SN7412	SN7413
0.20 0.18	0.20 0.18	0.20 0.18	0.22 0.21	0.48 0.46	0.40 0.38
SN7414	SN7415	SN7416	SN7417	SN7418	SN7419
0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18
SN7420	SN7421	SN7422	SN7423	SN7424	SN7425
0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18
SN7426	SN7427	SN7428	SN7429	SN7430	SN7431
0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18
SN7432	SN7433	SN7434	SN7435	SN7436	SN7437
0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18	0.20 0.18

MULLARD SUB-MIN ELECTROLYTIC

C425 range axial lead 6p each
 Values: (μF/V): 0.64/64; 1/40; 1.6/25; 2.5/16; 2.5/64; 4/10; 4/40; 6.4/6.4; 6.4/25; 8/40; 10/16; 10/64; 12.5/25; 16/40; 20/16; 20/64; 25/6.4; 25/25; 32/10; 32/30; 32/64; 40/16; 50/6.4; 80/25; 80/40; 84/10; 80/2.5; 80/16; 80/25; 100/6.4; 125/10; 125/16; 200/10.

SILICON RECTIFIERS

PIV	50	100	200	400	600	800	1000	1200
1A	5p	10p	20					



AMPEX 7.5v. D.C. MOTOR.
This is an ultra-precision tape motor designed for use in the AMPEX model AG20 portable recorder. Torque 450GM/CM. Stall load at 500 ma. Draws 60 ma on run. 600 rpm + 5% speed adjustment. Internal AF/RF suppression. 1" dia. 1" spindle, motor 3" dia. 1 1/2". Original cost enclosure available 75p each.

SMITHS. 250v. 50 Hz. Available in the following R.P.M. 2-3-6-10-30-60. Price 75p each. Carr. paid.
CROUZET. 220/380v. 50/60 Hz. 250-300 rpm. 75p. Carr. paid.

MAINS INDUCTION MOTOR. Open frame, 1/2" spindle, weight 1 lb. Powerful. 88p each. P. & P. 12p.

GEARED MOTORS
ELECTRO CONTROL (CHICAGO). Shaded pole 240v. 50Hz. 200 rpm. 10lb. in. £2.50. P. & P. 25p.
MYCALEX. Open frame, shaded pole motors. 240v. 50 Hz 7 rpm. 28 lb. in. 80 rpm. 12 lb. in. £2.25 each. P. & P. 25p.

"CROUZET" TYPE 965. 115/240v. 50 Hz. 47/68 watts. 50 rpm. Scouty constructed. Size: 2 1/2" dia. x 3 1/2" long plus spindle. 1" x 1/2" dia. Anticlock. £2.75. P. & P. 25p.
TYPE 955. Same as above, but 3 rpm. £3.00 P. & P. 25p.

RELAYS

"FINDER" 240v. A.C. Octal Relay 2c/o 6 amp contacts. Perspex enclosed, 75p.

"B. & R." 3 c/o. 10 amp contacts (silver) operates on 2 volts D.C. Draws approx. 1 amp. Size: 2" x 1 1/2" x 1 1/2". £1.00.

"ENGEL & GIBBS" 240v. A.C. Plug-in relay 3 c/o perspex enclosed £1.00.

NEW "F.I.R.E." PLUG-IN RELAY. -115v. Coil 50/60 c.p.s. 3 heavy duty silver change-over contacts. Very robust. 63p.

NEW "ISKRA" 240v. A.C. RELAY. 3 x 6 amp. Changeover contacts. 63p.

SIEMENS HIGH SPEED RELAYS. Type 89L. 1,700Ω + 1,700Ω coil. New 63p each.

PROGRAMME TIMER BY HONEYWELL

A bank of 15 micro-switches are each independently operated by 15 pairs of cams which in turn are individually adjustable to give switching periods of zero to 12 seconds with infinitely variable combinations. A mains synchronous motor drives the cam shaft at 1 rev. per 12 seconds (5 rpm) Originally cost £15.00 plus. Many applications such as lighting effects, etc. New in original makers cartons. First class value at £5.75 plus 25p P. & P.

PRECISION FAN CO (SMITHS INDUSTRIALS) DOUBLE ENTRY CENTRIFUGAL FAN / BLOWER. This is a beautifully balanced particularly quiet running unit giving approx. 90 cubic ft./min. The motor is a 2 pole shaded pole Mycalex, drawing only 240 ma on run. Weight 2 1/2 lbs. Size: case dia. 3 1/2 ins., width (case only) 3 1/25 ins. Width overall (inc.) 5 25 ins. Aperture 3 1/25 ins. x 1 85 ins. Offered well below makers price at £2.95. P. & P. 25p.

"NORPLEX" (U.S.A.) FIBRE-GLASS COPPER-CLAD LAMINATE. - First quality, Woven Glass base Epoxy-resin, excellent mech. & elec. properties. Heat Resistant. Full spec. available. This is a special purchase and only available whilst stocks last. Sizes: 12" x 12", 24" x 12", 24" x 24" or full sheet 43" x 37" (11 sq. ft.). Single sided Copper in following thicknesses: 1/32", 1/16", 1/8", 3/16", price £1 per sq. ft. or £10 per full sheet. Double-sided Copper 1/32", 1/16", 1/8", £1.25 per sq. ft., £11 per full sheet. P. & P. up to 4 sq. ft. 25p. Any order over 4 sq. ft. post free.

ERNEST TURNER 800Ω METER. 160Ω movement, 2" case elliptic plastic front. Green-Red-Green uncalibrated scale £1.50 each. Carriage paid.

PAINTON BOURNS TRIMPOTS. 1k, 2k, 2.5k, 5k, 10k, 20k, 50k, 500k. Other Trimmer pots in stock: RIL 10k, MORGANITE 1k, MEC 200Ω (tubular) 50Ω. Any 3 for £1.10 carr. paid.
6 DIGIT NON-RESET COUNTER by E.N.M. Ltd. 240v. A.C. Size: 2 1/2" high x 1 1/2" x 1 1/2". £1.75

"SORENG" MAINS SOLENOID. 1" travel, 18lb. pull (approx.). Size: 2 1/2" long x 2 1/2" x 2 1/2" high. Powerful. £1.75. P. & P. 25p.

"DAVENSET" MAINS SOLENOID. 1" travel. 8lb. pull (approx.). Size: 2 1/2" long x 2 1/2" x 2" high. Similar in appearance as above. £1.25. P. & P. 25p.

"MAGNETIC DEVICES" Mains Solenoid. 2" x 1 1/2" x 1 1/2" approx. 2lb. pull. Plunger Travel 1 1/2". New in makers boxes; offered at half original cost. 75p. P. & P. 25p.

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VINKOR POT CORE ASS. TYPE LA2103. Normal price £1.48. Our price 75p.
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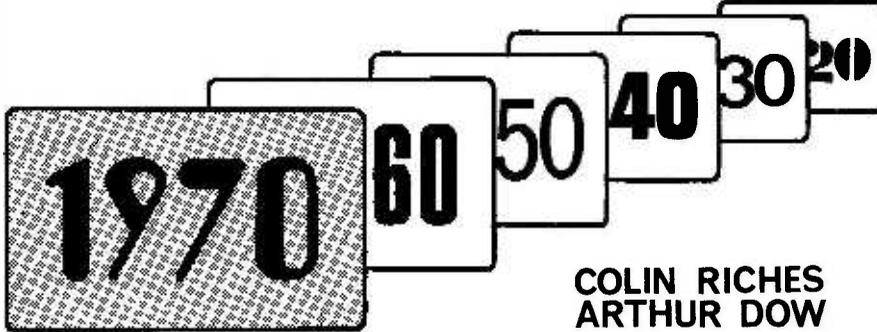
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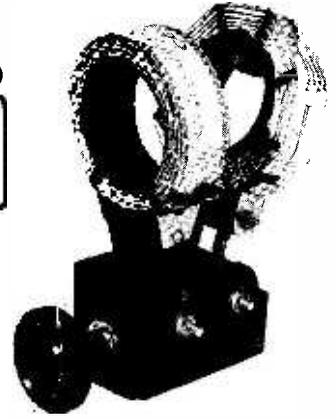
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GOING BACK...



COLIN RICHES
ARTHUR DOW



IT was on Wednesday, April 10th, sixty years ago that the s.s. *Titanic* left Southampton on her maiden voyage. Five days later, she sank to the bed of the ocean—a useless mass of twisted and torn steel, for on Sunday, April 14th, 1912, at about 11.40 p.m. the greatest peacetime disaster in maritime history took place when this ship, gross tonnage 46,328, struck an iceberg, 50-100ft. high, while on her maiden voyage to New York.

The blow on the starboard side of the ship ripped a hole 300 feet long and made many of the essential watertight compartments useless. She foundered within three hours, in water two miles deep.

Mr. H. S. Bride, the operator who survived the disaster described the way in which wireless played its all important role in saving those who were rescued. Mr. Bride was the second operator on the *Titanic* and was relieving his chief, Mr. Phillips at the time when the collision occurred. "I was standing by Mr. Phillips telling him to go to bed when

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"OLYMPIC," 45,324 tons, and "TITANIC" 45,000 tons, are the Largest Vessels in the World.

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"OLYMPIC" sails from Southampton and Cherbourg to New York regularly.

"TITANIC" sails from Southampton and Cherbourg on first voyage to New York
April 10, 1912

White Star Line

LIVERPOOL. LONDON. SOUTHAMPTON. NEW YORK

How the maiden voyage of the Titanic was advertised.

the captain put his head into the cabin. 'We have struck an iceberg!' he said, 'you had better get ready to send out a call for assistance. 'Don't send it until I tell you'. The captain went away but in ten minutes came back. We could hear terrible confusion outside but not the least thing to indicate any trouble. The wireless was working perfectly. 'Send a call for assistance' ordered the captain. 'What call shall I send?' Phillips asked. 'The regulation international call for help—just that' was the reply, and Phillips began to send the signal C.Q.D. (now replaced by S.O.S.). After a few minutes the Captain reappeared and said, 'Send S.O.S.—it may be your last chance.'

The *Titanic's* C.Q.D.'s and S.O.S.'s were first picked up by the German steamer, *Frankfurt* which was 153 miles away. Almost at the same time, the *Carthia's* wireless operator reported the emergency to his captain and was able to give the stricken liner's position 41 46N 50 14W. Immediately, the *Carthia*, which was 58 miles away, altered course to the rescue. The first message the *Carthia* picked up was, "COME AT ONCE, WE'VE STRUCK A BERG. IT'S C.Q.D. OM C.Q.D." C.Q.D. of course meant Come Quick, Danger, and was rather tricky to tap out in Morse. For this reason, the now universal distress signal S.O.S. was also used and this was the first occasion it had really been broadcast in earnest.

Fortunately, the *Carthia's* only wireless operator, although officially off watch had returned to



Jack G. Phillips, Chief Marconi Operator on board the *Titanic*.

his equipment and was putting out some routine traffic calls—including some to the *Titanic*. At 12.20 a.m. the distress calls were received and soon at least six ships were steaming to the disaster zone.

At 2.20 a.m. the *Californian* which for sometime past had been watching the lights of the 'unknown' vessel grow steadily dimmer, noted that they had finally disappeared. The optical illusion being that of seeing a ship disappearing into the darkness—not going under the waves. Those witnessing the scene from the decks of the *Californian* were not to know that they had been watching the death throes of the *Titanic* and that the sea around them was dotted with hundreds of human beings fighting for their lives. Two long hours were to elapse before the *Carpathia* arrived and began to pick up survivors. Among over 1,500 people lost on that fateful night was Jack Phillips, the *Titanic's* senior wireless operator, who remained at his post as the decks were awash. Mr. Bride, who showed an equal devotion to duty, was eventually rescued after nearly two hours in the sea.

As the decks were awash, Phillips was standing in the wireless room, still sending away giving the *Carpathia* details of how the *Titanic* was faring. He then picked up the *Olympic* and told her that *Titanic* was sinking by the head. As Phillips was sending the message, Harold Bride strapped his lifebelt to the wireless operator's back. He had already put on his overcoat and was wondering if he could get Phillips' boots on him while he was still sending.

The Captain's voice boomed, "Men, you have done your duty. You can do no more. Abandon your cabins now. It's every man for himself. You look out for yourselves. I release you—that's the way of it at this kind of time, every man for himself."

The boat deck was awash. Phillips clung on sending... sending. He clung for about fifteen minutes after the Captain released him—water washing the floor of the wireless cabin.



H. S. Bride, 2nd Operator on board the *Titanic*.



Cyril Evans, Marconi Operator on board the *Californian*.

From aft came the strains of music—the ship's band playing ragtime. Phillips ran aft and made his way to the deck. He swam to a life-raft but lay there exhausted until his last breath failed. Harold Bride later said of Phillips. "He was a brave man and stuck to his key until the very end. If he had had a chance to go to his room and get warmer clothing, as I did, he would probably be alive today. But duty was first with him."

When water flooded the upper decks, Second Officer Lightoller was up to his ankles in water and Captain Smith—a calm grave figure of a man realising that the end could not now be far off—stood calmly on the bridge. He spoke two words to the people who were crowding forward. Words which were a call to our traditions of race and manhood, "Be British!"

Besides calling the *Carpathia* and *Baltic*, Phillips had also contacted the *Frankfurt* again and vessels had also been sent to the rescue by the wireless station at Cape Race. They were however all very far away and even though they made all speed to the stricken *Titanic*, not one of them was near when the last terrible moment came.

The band still played on. They played until they were waist deep in the cold dark water and in that awful moment, W. Hartley, the conductor spoke to his colleagues and there rang out into the darkness the hymn NEARER MY GOD TO THEE.

Part 2 of the *Titanic* story will be published in "Going Back" next month.

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2G302	20p	2N3417	37p	2N5460	40p	BC116	15p	BFX12	22p	NKT224	27p
2G303	20p	2N3439	130p	2N5103	25p	BC118	15p	BFX13	22p	NKT225	27p
2G306	42p	2N3440	97p	2N5104	25p	BC119	15p	BFX29	25p	NKT229	30p
2G308	42p	2N3554	17p	2N5801	50p	BC121	15p	BFX30	25p	NKT235	30p
2G309	30p	2N3556	17p	2N5803	50p	BC122	15p	BFX37	30p	NKT238	30p
2G311	15p	2N3558	25p	2N5804	50p	BC123	15p	BFX40	30p	NKT240	30p
2G314	15p	2N3559	25p	2N5805	50p	BC124	15p	BFX84	25p	NKT241	30p
2G317	15p	2N3562	25p	2N5806	50p	BC125	15p	BFX85	30p	NKT242	30p
2G321	15p	2N3565	25p	2N5807	50p	BC126	15p	BFX86	30p	NKT243	30p
2G324	15p	2N3568	25p	2N5808	50p	BC127	15p	BFX87	30p	NKT244	30p
2G327	15p	2N3571	25p	2N5809	50p	BC128	15p	BFX88	25p	NKT245	30p
2G331	15p	2N3574	25p	2N5810	50p	BC129	15p	BFX89	25p	NKT246	30p
2G334	15p	2N3577	25p	2N5811	50p	BC130	15p	BFX90	25p	NKT247	30p
2G337	15p	2N3580	25p	2N5812	50p	BC131	15p	BFX91	25p	NKT248	30p
2G341	15p	2N3583	25p	2N5813	50p	BC132	15p	BFX92	25p	NKT249	30p
2G344	15p	2N3586	25p	2N5814	50p	BC133	15p	BFX93	25p	NKT250	30p
2G347	15p	2N3589	25p	2N5815	50p	BC134	15p	BFX94	25p	NKT251	30p
2G351	15p	2N3592	25p	2N5816	50p	BC135	15p	BFX95	25p	NKT252	30p
2G354	15p	2N3595	25p	2N5817	50p	BC136	15p	BFX96	25p	NKT253	30p
2G357	15p	2N3598	25p	2N5818	50p	BC137	15p	BFX97	25p	NKT254	30p
2G361	15p	2N3601	25p	2N5819	50p	BC138	15p	BFX98	25p	NKT255	30p
2G364	15p	2N3604	25p	2N5820	50p	BC139	15p	BFX99	25p	NKT256	30p
2G367	15p	2N3607	25p	2N5821	50p	BC140	15p	BFX99A	25p	NKT257	30p
2G371	15p	2N3610	25p	2N5822	50p	BC141	15p	BFX99B	25p	NKT258	30p
2G374	15p	2N3613	25p	2N5823	50p	BC142	15p	BFX99C	25p	NKT259	30p
2G377	15p	2N3616	25p	2N5824	50p	BC143	15p	BFX99D	25p	NKT260	30p
2G381	15p	2N3619	25p	2N5825	50p	BC144	15p	BFX99E	25p	NKT261	30p
2G384	15p	2N3622	25p	2N5826	50p	BC145	15p	BFX99F	25p	NKT262	30p
2G387	15p	2N3625	25p	2N5827	50p	BC146	15p	BFX99G	25p	NKT263	30p
2G391	15p	2N3628	25p	2N5828	50p	BC147	15p	BFX99H	25p	NKT264	30p
2G394	15p	2N3631	25p	2N5829	50p	BC148	15p	BFX99I	25p	NKT265	30p
2G397	15p	2N3634	25p	2N5830	50p	BC149	15p	BFX99J	25p	NKT266	30p
2G401	15p	2N3637	25p	2N5831	50p	BC150	15p	BFX99K	25p	NKT267	30p
2G404	15p	2N3640	25p	2N5832	50p	BC151	15p	BFX99L	25p	NKT268	30p
2G407	15p	2N3643	25p	2N5833	50p	BC152	15p	BFX99M	25p	NKT269	30p
2G411	15p	2N3646	25p	2N5834	50p	BC153	15p	BFX99N	25p	NKT270	30p
2G414	15p	2N3649	25p	2N5835	50p	BC154	15p	BFX99O	25p	NKT271	30p
2G417	15p	2N3652	25p	2N5836	50p	BC155	15p	BFX99P	25p	NKT272	30p
2G421	15p	2N3655	25p	2N5837	50p	BC156	15p	BFX99Q	25p	NKT273	30p
2G424	15p	2N3658	25p	2N5838	50p	BC157	15p	BFX99R	25p	NKT274	30p
2G427	15p	2N3661	25p	2N5839	50p	BC158	15p	BFX99S	25p	NKT275	30p
2G431	15p	2N3664	25p	2N5840	50p	BC159	15p	BFX99T	25p	NKT276	30p
2G434	15p	2N3667	25p	2N5841	50p	BC160	15p	BFX99U	25p	NKT277	30p
2G437	15p	2N3670	25p	2N5842	50p	BC161	15p	BFX99V	25p	NKT278	30p
2G441	15p	2N3673	25p	2N5843	50p	BC162	15p	BFX99W	25p	NKT279	30p
2G444	15p	2N3676	25p	2N5844	50p	BC163	15p	BFX99X	25p	NKT280	30p
2G447	15p	2N3679	25p	2N5845	50p	BC164	15p	BFX99Y	25p	NKT281	30p
2G451	15p	2N3682	25p	2N5846	50p	BC165	15p	BFX99Z	25p	NKT282	30p
2G454	15p	2N3685	25p	2N5847	50p	BC166	15p	BFX99AA	25p	NKT283	30p
2G457	15p	2N3688	25p	2N5848	50p	BC167	15p	BFX99AB	25p	NKT284	30p
2G461	15p	2N3691	25p	2N5849	50p	BC168	15p	BFX99AC	25p	NKT285	30p
2G464	15p	2N3694	25p	2N5850	50p	BC169	15p	BFX99AD	25p	NKT286	30p
2G467	15p	2N3697	25p	2N5851	50p	BC170	15p	BFX99AE	25p	NKT287	30p
2G471	15p	2N3700	25p	2N5852	50p	BC171	15p	BFX99AF	25p	NKT288	30p
2G474	15p	2N3703	25p	2N5853	50p	BC172	15p	BFX99AG	25p	NKT289	30p
2G477	15p	2N3706	25p	2N5854	50p	BC173	15p	BFX99AH	25p	NKT290	30p
2G481	15p	2N3709	25p	2N5855	50p	BC174	15p	BFX99AI	25p	NKT291	30p
2G484	15p	2N3712	25p	2N5856	50p	BC175	15p	BFX99AJ	25p	NKT292	30p
2G487	15p	2N3715	25p	2N5857	50p	BC176	15p	BFX99AK	25p	NKT293	30p
2G491	15p	2N3718	25p	2N5858	50p	BC177	15p	BFX99AL	25p	NKT294	30p
2G494	15p	2N3721	25p	2N5859	50p	BC178	15p	BFX99AM	25p	NKT295	30p
2G497	15p	2N3724	25p	2N5860	50p	BC179	15p	BFX99AN	25p	NKT296	30p
2G501	15p	2N3727	25p	2N5861	50p	BC180	15p	BFX99AO	25p	NKT297	30p
2G504	15p	2N3730	25p	2N5862	50p	BC181	15p	BFX99AP	25p	NKT298	30p
2G507	15p	2N3733	25p	2N5863	50p	BC182	15p	BFX99AQ	25p	NKT299	30p
2G511	15p	2N3736	25p	2N5864	50p	BC183	15p	BFX99AR	25p	NKT300	30p
2G514	15p	2N3739	25p	2N5865	50p	BC184	15p	BFX99AS	25p	NKT301	30p
2G517	15p	2N3742	25p	2N5866	50p	BC185	15p	BFX99AT	25p	NKT302	30p
2G521	15p	2N3745	25p	2N5867	50p	BC186	15p	BFX99AU	25p	NKT303	30p
2G524	15p	2N3748	25p	2N5868	50p	BC187	15p	BFX99AV	25p	NKT304	30p
2G527	15p	2N3751	25p	2N5869	50p	BC188	15p	BFX99AW	25p	NKT305	30p
2G531	15p	2N3754	25p	2N5870	50p	BC189	15p	BFX99AX	25p	NKT306	30p
2G534	15p	2N3757	25p	2N5871	50p	BC190	15p	BFX99AY	25p	NKT307	30p
2G537	15p	2N3760	25p	2N5872	50p	BC191	15p	BFX99AZ	25p	NKT308	30p
2G541	15p	2N3763	25p	2N5873	50p	BC192	15p	BFX99BA	25p	NKT309	30p
2G544	15p	2N3766	25p	2N5874	50p	BC193	15p	BFX99BB	25p	NKT310	30p
2G547	15p	2N3769	25p	2N5875	50p	BC194	15p	BFX99BC	25p	NKT311	30p
2G551	15p	2N3772	25p	2N5876	50p	BC195	15p	BFX99BD	25p	NKT312	30p
2G554	15p	2N3775	25p	2N5877	50p	BC196	15p	BFX99BE	25p	NKT313	30p
2G557	15p	2N3778	25p	2N5878	50p	BC197	15p	BFX99BF	25p	NKT314	30p
2G561	15p	2N3781	25p	2N5879	50p	BC198	15p	BFX99BG	25p	NKT315	30p
2G564	15p	2N3784	25p	2N5880	50p	BC199	15p	BFX99BH	25p	NKT316	30p
2G567	15p	2N3787	25p	2N5881	50p	BC200	15p	BFX99BI	25p	NKT317	30p
2G571	15p	2N3790	25p	2N5882	50p	BC201	15p	BFX99BJ	25p	NKT318	30p
2G574	15p	2N3793	25p	2N5883	50p	BC202	15p	BFX99BK	25p	NKT319	30p
2G577	15p	2N3796	25p	2N5884	50p	BC203	15p	BFX99BL	25p	NKT320	30p
2G581	15p	2N3799	25p	2N5885	50p	BC204	15p	BFX99BM	25p	NKT321	30p
2G584	15p	2N3802	25p	2N5886	50p	BC205	15p	BFX99BN	25p	NKT322	30p
2G587	15p	2N3805	25p	2N5887	50p	BC206	15p	BFX99BO	25p	NKT323	30p
2G591	15p	2N3808	25p	2N5888	50p	BC207	15p	BFX99BP	25p	NKT324	30p
2G594	15p	2N3811	25p	2N5889	50p	BC208	15p	BFX99BQ	25p	NKT325	30p
2G597	15p	2N3814	25p	2N5890	50p	BC209	15p	BFX99BR	25p	NKT326	30p
2G601	15p	2N3817	25p	2N5891	50p	BC210	15p	BFX99BS	25p	NKT327	30p
2G604	15p	2N3820	25p	2N5892	50p	BC211	15p	BFX99BT	25p	NKT328	30p
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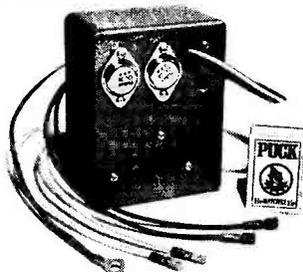
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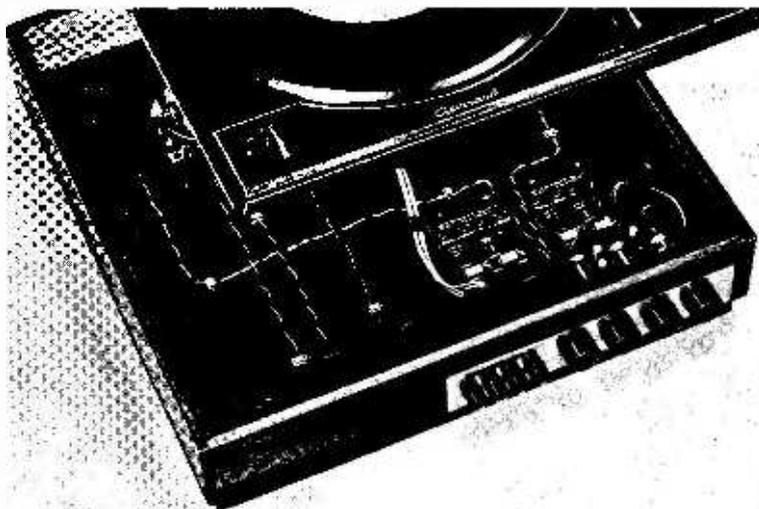
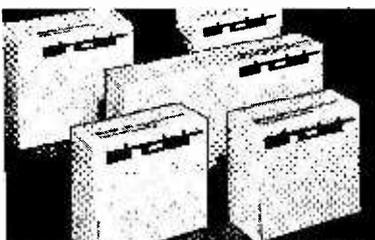
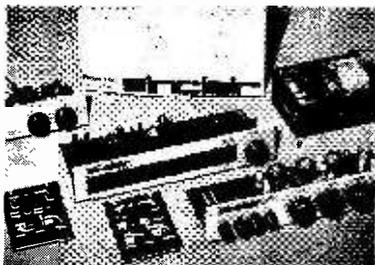
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Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world. Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

Project 60 modules are more versatile – using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all – price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications

System	The Units to use	together with	Cost of Units
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control etc.	£9.46
20 + 20 W. stereo amplifier for most needs	2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90
20 + 20 W. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
40 + 40 W. R.M.S. de-luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsrfrm	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

F.M. Stereo Tuner (**£25**) & A.F.U. Filter Unit (**£5.98**) may be added as required.

Project 60 Stereo F.M. Tuner

Built and tested. Post free. **£25**

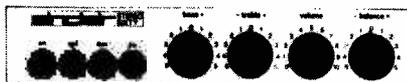


The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. **Tuning range:** 87.5 to 108 MHz. **Capture ratio:** 1.5dB. **Sensitivity:** 7 μ V for lock-in over full deviation. **Squelch level:** 20 μ V. **Signal to noise ratio:** > 65dB. **Audio frequency response:** 10 Hz – 15 KHz (\pm 1dB). **Total harmonic distortion:** 0.15% for 30% modulation. **Stereo decoder operating level:** 2 μ V. **Cross talk:** 40dB. **Output voltage:** 2 x 150mV R.M.S. **Operating voltage:** 25-30 VDC. **Indicators:** Stereo on; tuning. **Size:** 93 x 40 x 207 mm.

Stereo 60 Pre-amp/control unit

Built, tested and guaranteed. **£9.98**



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV; correct to R.I.A.A curve \pm 1dB: 20 to 25,000 Hz. Ceramic p.u. – up to 3mV; Aux – up to 3mV. **Output:** 250mV. **Signal to noise ratio:** better than 70dB. **Channel matching:** within 1dB. **Tone controls:** TREBLE + 12 to – 12dB at 10 KHz; BASS + 12 to – 12dB at 100Hz. **Front panel:** brushed aluminium with black knobs and controls. **Size:** 66 x 40 x 207 mm.

A.F.U. High & Low Pass Filter Unit

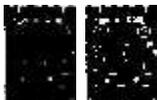
Built tested and guaranteed. **£5.98**



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1 KHz (35V. supply) 0.02% at rated output. **Size:** 66 x 40 x 90 mm.

Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual. **Z.30 £4.48** **Z.50 £5.48**



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8 Ω) and all lower outputs. Whether you

use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).

Power Outputs

Z.30 15 watts R.M.S. into 8 ohms using 35 volts;

20 watts R.M.S. into 3 ohms using 30 volts.

Z.50 40 watts R.M.S. into 3 ohms using 40 volts;

30 watts R.M.S. into 8 ohms using 50 volts.

Frequency response: 30 to 300,000Hz \pm 1dB.

Distortion: 0.02% into 8 ohms.

Signal to noise ratio: better than 70dB unweighted.

Input sensitivity: 250mV into 100 Kohms (for 15w

into 8 Ω)

For speakers from 3 to 15 ohms impedance.

Size: 14 x 80 x 57 mm.

Power Supply Units



Designed special for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ.5 30 volts un stabilised £4.98

PZ.6 35 volts stabilised £7.98

PZ.8 45 volts stabilised

(less mains transformer) £7.98

PZ.8 mains transformer £5.98

Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

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2nd I.F. Transformer	P50/2CC (For OC45)	P51/2 (For AF117)	36p
3rd I.F. Transformer	P50/3CC (For OC45)	P50/3V (For AF117)	36p

Rod Aerial	RA2W	72p
Driver Transformer	LFD1/4	58p
Output Transformer	OPT1	58p
Printed Circuit	PCA1	58p

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T41/2E	2nd I.F. Transformer	39p
T41/3T	3rd I.F. Transformer	57p
T41/3T	B.F.O. Coil	57p

Details of these and our other components are given in an illustrated folder which will be supplied on request with postage please.

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Ground Position Indicator. Contains 24 Volt Lamp. Prisms Mirror and Gears. Could interest schools and model makers. 75p. Carriage 75p.

Latest Air Ministry Release Radio Receiver. Type R4187. 2-8 to 18 MHZ in Three Bands. Complete with 17 miniature valves. 26 Volt Motor. Power supply motor and manually tuned. Very clean, but not tested. £5. Carriage and Insurance 75p.

Control Unit. Type 4190. Complete with three miniature valves. 1½" 500 µA Meter. Six Relays. Model makers Motor with Gears. 24 Press Buttons. Lots of spares. Clean condition. £1.50. Carriage and Insurance 75p.

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EBF89	12½p	PCF82	12½p	6F23	20p
ECC81	10p	PL36	20p	20P1	20p
ECC82	12½p	PL81	1½p	20P3	10p
ECL80	7½p	PY81	7½p	20D1	10p
EF80	7½p	PY33	17½p	30P4	20p
EF91	4p	PY82	7½p	30P12	20p
EY86	20p	PL82	7½p	30FL1	20p
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3V4	-37	30PL1	-58	EBF89	-27	EF184	-28	PCF802	-38	U25	-58
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6AQ5	-21	30PL14	-68	ECC82	-19	EL84	-22	PCL82	-30	U191	-57
6BW7	-50	DAT91	-21	ECC83	-21	EY51	-80	PCL83	-55	U261	-68
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6F23	-87	DF91	-14	ECH35	-53	EZ80	-20	PCL86	-37	U801	-78
6F25	-51	DF96	-35	ECH42	-58	EZ81	-21	PCL86	-37	UBF89	-89
68N7GT	-28	DK91	-25	ECH81	-26	KT61	-54	PFL200	-51	UC35	-34
25L6GT	-18	DK92	-35	ECL80	-29	LT96	-75	PL86	-47	UCH81	-30
30C15	-56	DK96	-43	ECC82	-29	N78	-85	PL81	-43	UCL82	-81
30C17	-78	DL92	-24	ECL86	-34	PC86	-45	PL82	-29	UF89	-26
30C18	-59	DL94	-37	EF93	-38	PC88	-45	PL83	-31	UL84	-29
30F5	-58	DL96	-36	EF80	-22	PC900	-30	PL84	-29	UY41	-37
30FL1	-59	DY86	-28	EF85	-26	PC984	-28	PL80	-81	UY85	-24
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REALISTIC HI-FI 36-WATT STEREO CONCERTMASTER FM-AM RECEIVER SYSTEM, MODEL 12-694

Brilliantly designed tuner/amplifier with two matching speakers. All three units in beautifully finished walnut cabinets with smart aluminium vertical trims. The tuning dial is fronted by unique black glass. Figures light up behind it in green when the unit is on. Separate easy-to-operate Left and Right volume controls. Microswitch for on/off. Programme selector. Separate bass and treble controls. Headphone socket on front panel for easy access. Single tuning knob for FM and AM. Built-in aerials, facilities for external FM aerial. Illuminated dial. Stereo broadcast indicator light. Each speaker has 6 1/2" bass and 3" treble units. Output: 9 watts r.m.s. per channel into 8 ohms. Frequency response: 30 to 20,000 Hz. FM: frequency range 80-108 MHz, sensitivity 2.5µV, stereo separation 30dB, image rejection 40dB.

AM: frequency range 530-1605 kHz, sensitivity 100µV. Sizes: speakers 8" wide, 12" high and 9 1/2" deep; receiver 8" wide, 12" high and 9 1/2" deep. And their sophisticated appearance matches the excellence of the specification.



ROC PRICE
£27.25

Normal Price £39.95 each.

25-WATT 3-WAY CHRYSLER 'LIVING AUDIO' SPEAKER CE-5b

This high quality speaker has its own built-in 3-way sound response switch, giving you the ideal frequency response for hi-fi, natural or mood music listening. Its beautiful, heavy, oiled walnut cabinet incorporates two separate speaker units an 8" woofer, and a 5" mid-range with 2" concentric tweeter. Power handling capacity: 25 watts r.m.s. into 8 ohms. Overall frequency response: 35-20,000 Hz. Cabinet size: 10 1/2" x 7 1/2" x 8 1/2". Exactly right for matching the most modern decor.



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REALISTIC 30-WATT STEREO AMPLIFIER MODEL SA-500

A superb hi-fi amplifier with all the features you've ever wanted - for under £68.00. Saving over £10.00 on the normal retail value. Up-to-the-minute slider controls for bass and treble. Separate volume and balance controls. Headphone socket on front panel. Push-button input controls - magnetic phono (high/low) tuner, aux, mono, monitor. Loudness push-button control for perfect sound at low output levels. Left and right push-button on/off switches for speakers. Noise filtering and tape monitoring facilities. Two auxiliary AC outlets. Frequency response 20-20,000 Hz + 1 db at full power. 15 watts r.m.s. per channel. Walnut cabinet with satin aluminium trims. Inputs: phono 2.5mV and 5mV RIAA; tuner/aux 250mV. Hum and noise: phono - 50db, tuner/aux - 85db. Size 14 1/2" wide, 3 1/2" high, 10 1/2" deep.

As reviewed in "POPULAR HI-FI" February 1972

ROC PRICE
£43.75

Normal Price £55.50



STEREO 8-TRACK TAPE DECK MODEL RP-1000ST

The popular Lear-Jet type recording unit is the heart of the fantastic RP-1000ST, which has full record and playback facilities. Automatic track change with manual override. Press to start button. Stereo headphone and Left and Right Mic sockets on front panel. Dual recording level meter, and Left and Right volume controls. Built-in pre-amp. Tape speed 3 3/4 ips (9.5 cms). Frequency response: playback 30-10,000 Hz; recording/playback 30-8,000 Hz. Line output: fully variable 0-500mV. The RP-1000ST incorporates all the features you'd expect in a top quality Cartridge Tape Deck. Size 16" wide, 4" high, 9" deep. Cabinet in walnut. Including connecting leads.

ROC PRICE
£33.20

Normal Price £42.00



OLSON RA-310 AM/FM/MPX STEREO TUNER

This ROC Tuner is especially designed to match the Olson AM-395 Stereo Amplifier. In price and value, as well as it's good looking design! But of course it's also ideal for use with any other amplifier. The RA-310 costs £10.00 less than the normal retail value, and yet it is a highly sophisticated unit, incorporating the latest solid state techniques. Operation is drift free for supreme station-holding capability. You can connect this Tuner to a stereo amplifier, to a tape deck or a tape recorder. And of course it covers all the stations in the AM and FM bands. FM: 87-108 MHz; AM: 525-1050 kHz. FM Sensitivity: 3µV; AM, 250µV. Stereo separation 30dB at 1kHz, image rejection 60dB. Size: 11 1/2" wide, 4" high, 7 1/2" deep.

ROC PRICE
£39.95

Normal Price £50.00



ROC PRICE
£39.95

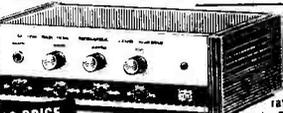
Normal Price £49.00

PALACE AM/FM/MPX STEREO TUNER AMPLIFIER SSA-16

This is one of the lowest priced stereo tuner amplifiers on the market. It covers the full range of both AM and FM broadcast frequencies. And when you're switched to FM, an indicator lights up when a stereo signal is received - that's the time to switch to 'Stereo'! The SSA-16 has all the facilities you'd expect to find on tuners costing twice as much - separate volume, bass, treble, balance and tuning controls. Selector switch for tape, phono, AM, FM, stereo. Jack socket on front panel for stereo headphones. Frequency range: FM 86-108 MHz. AM 535-1605 kHz. Frequency response: 50-10,000 Hz ± 3dB. Power output: 4 watts total music power into two 8 ohm speakers. Size: 16" wide, 4 1/2" high, 8" deep.

ROC PRICE
£5.50

Normal Price £7.75

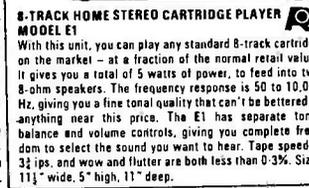


REALISTIC SA-100B 6-WATT STEREO AMPLIFIER

Here's fabulous, exciting value in miniature! This high quality stereo amplifier measures only 9" wide x 3" high x 5 1/2" deep. And yet it has separate gain, volume, balance and tone controls. Plus speaker in/out, mono (stereo, phono) and power on/off slide switches. The ends are oiled walnut, with matching enamelled metal top. The front panel is satin aluminium and walnut-brown enamel. Frequency response is 50 to 10,000 Hz + 3dB. Output 3 watts r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tuner.

ROC PRICE
£14.50

Normal Price £21.00



8-TRACK HOME STEREO CARTRIDGE PLAYER MODEL E1

With this unit, you can play any standard 8-track cartridge on the market - at a fraction of the normal retail value! It gives you a total of 5 watts of power, to feed into two 8-ohm speakers. The frequency response is 50 to 10,000 Hz, giving you a fine tonal quality that can't be bettered at anything near this price. The E1 has separate tone, balance and volume controls, giving you complete freedom to select the sound you want to hear. Tape speed is 3 3/4 ips, and wow and flutter are both less than 0.3%. Size: 11 1/2" wide, 5" high, 11" deep.

ROC PRICE
£7.75

Normal Price £10.00

REALISTIC TM-100 AM/FM/MPX STEREO TUNER



Here's another unit that gives you fabulous value in miniature! Designed specifically to match the Realistic SA-100B in both appearance, size and performance, the TM-100 is superb value-for-money. It gives you the full FM and AM ranges - FM, 88-108 MHz; AM, 535-1605 kHz. Sensitivities FM 5µV; AM 250µV. Image rejection 50dB.

ROC PRICE
£23.25

Normal Price £28.50



ROC PRICE
£17.80

Normal Price £25.00 per pair.

ROC 7-WATT STEREO AMPLIFIER CHASSIS SK-317

This exclusive ROC Stereo Chassis is completely self-contained, and it costs £2.25 less than the normal retail value! The SK-317 is a really compact unit measuring only 5 1/2" wide, 1 1/2" high and 6 1/2" deep. It contains its own mains power supply, and has a ganged tone control and separate volume controls for each channel. Specification: frequency response 40-17,000 Hz + 3dB; output 3.5 watts music power per channel into 8 ohms; input, phono, 600mV; signal-to-noise ratio better than 45dB.

ROC PRICE
£18.25

Normal Price £25.20



OLSON AM-395 40-WATT STEREO AMPLIFIER

An ideal unit for your new stereo separate system. It is more than £10.00 below the normal retail price! Making the AM-395 one of Britain's best hi-fi buys. It takes in signals from magnetic or ceramic pick-ups, tuners (see Olson RA-310) and tape decks. And it's got outputs for taping and for headphones. There are separate bass and treble controls, separate Left and Right channel volume controls. And a loudness switch for boosting the bass and treble notes when listening at low output levels. Frequency response 20-20,000 Hz + 3dB. Output: 20 watts r.m.s. per channel into 8 ohms. Inputs: magnetic phono 3-0mV RIAA, crystal phono 100mV; tape 160mV; tuner 160mV. Size 11 1/2" wide, 4" high, 7 1/2" deep. The specification reads well - sounds even better!

ROC PRICE
£29.00

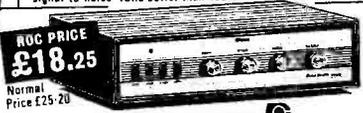
Normal Price £39.00

R. 446 3-WAY MATCHED SPEAKERS

These will do justice to your amplifier - and to your pocket. At only £16.40 a pair, they are real value-for-money. Each cabinet is heavily lagged and teak finished. They handle 16 watts rms (8 watts rms each). Each loudspeaker contains a large dual cone base unit, plus a separate tweeter. Frequency range: 40 to 19,000 Hz. Size 14" high, 9" wide, 6 1/2" deep.

OLSON AM-357 4-WATT STEREO AMPLIFIER

Here's marvellous value for someone just starting to set themselves up in audio! At only £10.50, you get a fine amplifier in a scratch resistant metal cabinet, with a smart brushed aluminium front panel. It incorporates separate tone and volume controls for each channel. Inputs are provided for turntable (ceramic cartridge), tuner and tape deck or recorder. Frequency response: 70-20,000 Hz + 3dB. Output: 2 watts r.m.s. per channel into 8 ohms. Inputs: phono 80mV; tuner/aux 80mV. Size 8" wide, 2 1/2" high, 4 1/2" wide.



OLSON AM-372 16-WATT STEREO AMPLIFIER

Here's a really good amplifier at a really down-to-earth price - nearly £7 less than the normal retail value! Just look at what the AM-372 will do for you - reproduce signals from ceramic or crystal cartridges, AM and FM tuners, and tape recorders. And it gives you outputs for two sets of speakers, headphones and tape recorders. Frequency response is 30 to 20,000 Hz + 3dB. Output 8 watts r.m.s. per channel music power into 8 ohm speakers. Phono input 200mV. Tuner input 200mV. Size: 12 1/2" wide, 3 1/2" high, 7 1/2" deep.

ROC PRICE
£10.50

Normal Price £14.70

units at lowest prices?..."

TOP VALUE · TOP QUALITY ACCESSORIES THAT EVERY HI-FI ENTHUSIAST NEEDS TO COMPLETE HIS SYSTEM

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exclusive unit

Every item shown here is the best of its kind within its price range. Buy them separately or at the same time as the other top-value audio products listed.

THORENS TD150AB/II
Transcription Turntable.
Complete with pick up arm,
plinth and cover. £52.31



R.328 STEREO HEADPHONE
If you're starting in hi-fi, and you discover the need for a pair of really good stereo headphones. The R.328 is ideal, at a price you can afford. They have padded ear cushions, a 6-foot cord and jack plug. Frequency range 30-15,000 Hz. Impedance 8 ohms per channel. **ROC PRICE £25.95**



EAGLE SE-80 STUDIO HEADPHONE
Here's the ultimate in headphone design! Apart from its fantastic ability to reproduce all the frequencies from 20 to 20,000 Hz, the SE-80 has eliminated the discomfort and strain associated with traditional headphone design. Eagle have designed and produced a pair of headphones which breaks with all previous concepts. You hear all the sounds crisp and clear. In fact, the reproduction is so good, that it compares favourably with the most expensive hi-fi speaker systems. Separate slider volume control on each earpiece. Impedance: 8 ohm per channel. **ROC PRICE £14.90**



R.108 STEREO JUNCTION BOX

If you want easy, fingertip control of headphones and loudspeakers, here's the ideal solution to the problem. All you do is connect it to your speakers and amplifier, plug in your headphones - and you're ready to take over! At the flick of a slide switch, you can have headphones alone, or speakers alone, or both together. Input: suitable for use with amplifiers rated up to 20 watts. Size: 2 1/4" x 3 1/2" x 1 1/2". **ROC PRICE £1.50**

EAGLE SE-30 STEREO HEADPHONE

This model is for the more discriminating listener. For a start the frequency range extends from 30 to 16,000 Hz. And you can adjust the volume of each earpiece independently. There's also a mono/stereo switch. For maximum comfort, the ear cushions are covered in soft leathers. **ROC PRICE £7.05**



TEC HR-007 HEADPHONE RADIO

When you want to listen to the radio all by yourself. Then this will solve the problem. Separate volume and tuning controls with easy-to-use knobs. Frequency range is 535 to 1605 kHz medium wave band. Maximum output is 300 mW. Normal Price £9.45 **ROC PRICE £7.65**

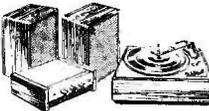


R.151 STEREO CAR SPEAKERS

Smart black, tough, plastic cases, each containing a high flux 110mm diameter speaker unit. Just what you need to go with the CS.8 Cartridge Player or any other car stereo system. Fitted with over three yards of connecting cable. Dimensions: 6 1/4" x 5 1/4" x 3 1/2". Impedance: 8 ohms per speaker. Rating: 5 watts max per speaker. **ROC PRICE £3.72**

HERE'S A RANGE OF AUDIO SYSTEMS BUILT AROUND EXCLUSIVE ROC AMPLIFIERS AND TUNERS

Now run your eye over the prices, select the System nearest to your budget - and you've hit on the best value that your money can buy! Supplied with all necessary leads and plugs, ready to use.



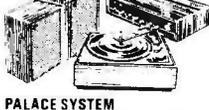
REALISTIC SA-100B SYSTEM
Realistic SA-100B Stereo Amplifier, Garrard 2025TC Autochanger with Stereo ceramic cartridge, plinth and cover and a pair of ROC R.446 Speakers. Matching TM-100 Stereo Tuner £23.25 extra if required. Normal Price £63.98 **ROC PRICE £47.60**



OLSON AM-395 SYSTEM
Olson AM-395 Stereo Amplifier, Garrard SP25 Mk III Record Player with Eagle LC07 Stereo Magnetic Cartridge, plinth and cover and a pair of Eagle DL.67 Speakers. Matching RA.310 Stereo Tuner £39.95 extra if required. Normal Price £106.65 **ROC PRICE £92.40**



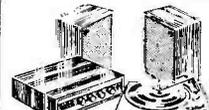
OLSON AM-357 SYSTEM
Olson AM-357 Stereo Amplifier, Garrard 2025 T/C Autochanger with Stereo ceramic cartridge, plinth and cover and a pair of ROC R.088 4 watt Speakers. Normal Price £45.28 **ROC PRICE £36.70**



PALACE SYSTEM
Palace SSA-16 Stereo Tuner Amplifier, Garrard 2025 T/C autochanger with stereo ceramic cartridge, plinth and cover and a pair of ROC R.446 Speakers. Normal Price £84.98 **ROC PRICE £66.30**



REALISTIC SA-500 SYSTEM
Realistic SA-500 Stereo Amplifier, Garrard SP25 Mk III Single Record Player with Eagle LC.07 Stereo Magnetic Cartridge, plinth and cover and a pair of Cyster CE-5b Speakers. Normal Price £157.95 **ROC PRICE £124.00**



OLSON AM-372 SYSTEM
Olson AM-372 Stereo Amplifier, Garrard 2025 T/C Autochanger with Stereo ceramic cartridge, plinth and cover and a pair of ROC R.446 Speakers. Normal Price £68.18 **ROC PRICE £51.53**



REALISTIC 12-694 SYSTEM
Realistic 12-694 Stereo Tuner Amplifier with matching Speakers and Garrard SP25 Mk III with Eagle LC.07 Stereo Magnetic Cartridge and plinth and cover. Normal Price £144.05 **ROC PRICE £124.50**



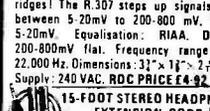
ROC E1 SYSTEM
ROC E1 8 track Stereo Cartridge Player complete with a pair of ROC R.088 4 watt Speakers. Normal Price £59.10 **ROC PRICE £49.45**



EAGLE 8-TRACK CAR STEREO PLAYER, CS.8
Drive to the sound of music - with this fabulous 8-Track Cartridge Player. It gives you superb tone and power to fill the car with stereo sound. Ideal for use with R.151 or R.152 speakers. Complete with all mounting accessories. For negative earth electrical systems only. Output: 2.5 watts per channel. Frequency range: 10-10,000 Hz. Wow and flutter: less than 0.3%. Tape speed: 3.5 cm/sec. Channel selector: automatic with manual override. Mounting dimensions: 5 1/4" x 5 1/2" x 2 1/4". **ROC PRICE £27.20**



RECORD CLEANERS
The original "Dust Bug" Automatic Record Cleaner keeps your records clean as they play. £1.20 Watts Disc Preener. Keeps new records like new - for perfect record reproduction. 35p



R.307 TRANSISTORIZED STEREO PRE-AMPLIFIER
Now your amplifier that could only reproduce ceramic or crystal pick-up cartridges, can accept signals from moving-magnet cartridges! The R.307 steps up signals from between 5-20mV to 200-800 mV. Input: 5-20mV. Equalisation: RIAA. Output: 200-800mV flat. Frequency range: 20-22,000 Hz. Dimensions: 3 1/2" x 1 1/2" x 2 1/2". Supply: 240 VAC. **ROC PRICE £4.92**



R.152 STEREO CAR SPEAKERS

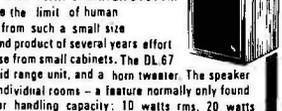
These sloping front speakers match the CS.8 Cartridge Player or any other car stereo system. Fitted with high flux 110mm diameter speaker unit, and over three yards of connecting cable. Dimensions: 6 1/4" x 3 1/2". Impedance: 8 ohms per speaker. Rating: 5 watts max per speaker. **ROC PRICE £4.96**



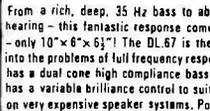
EAGLE LC.05 STEREO MAGNETIC CARTRIDGE
For fabulous reproduction at a very low price, you'll find it hard to beat. 0.7 mil diamond stylus. Output: 6mV per channel. Frequency range: 30-18,000 Hz. Channel balance: ±1.5dB. Channel separation: 20dB. Recommended stylus pressure: 2.4 grams. Compliance: 9-10.6 cm/dyne. **ROC PRICE £4.75**



EAGLE LC.07 STEREO MOVING-MAGNET CARTRIDGE
Here's your opportunity to own a transcription cartridge for the price of a ceramic! It's specially designed to match top quality tone arms, and to get the very best from your hi-fi amplifier. 0.7 mil diamond stylus. Output: 7mV per channel. Frequency range: 20-21,000 Hz. Channel balance: ±1dB. Channel separation: 28dB. Compliance: 12-10.6 cm/dyne. **ROC PRICE £6.37**



R.088 MATCHED STEREO LOUD-SPEAKERS
Here's real value in stereo speakers! Each unit comes complete with 10-foot lead and phono plug, and look really smart. Power handling per speaker: 4 watts rms, 8 watts peak. Frequency range: 40-16,000 Hz. Flux density: 8,500 gauss. Impedance: 8 ohms. Dimensions: 9" high, 9 1/2" wide, 4 1/2" deep. Finish: oiled walnut. **ROC PRICE £9.50 pair**



EAGLE DL.67 HIGH COMPLIANCE 3-WAY TEAK SPEAKER SYSTEM
From a rich, deep, 35 Hz bass to above the limit of human hearing - this fantastic response comes from such a small size - only 10" x 6" x 6 1/2"! The DL.67 is the end product of several years effort into the problems of full frequency response from small cabinets. The DL.67 has a dual cone high compliance bass mid range unit, and a horn tweeter. The speaker has a variable brilliance control to suit individual rooms - a feature normally only found on very expensive speaker systems. Power handling capacity: 10 watts rms, 20 watts peak. Frequency range: 35-20,000 Hz. Flux density: 11,000 gauss. Impedance: 8 ohms. Dimensions: 11 1/2" high x 8" wide x 6 1/2" deep. Finish: oiled teak. **ROC PRICE £18.80 each**

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- 3 pin Din Line Socket 13p "
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- Standard Jack Plug 10p "
- Screened Standard Jack Plugs 13p "
- Stereo Jack Plug 13p "
- Screened Stereo Jack Plug 13p "

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MULLARD SEW TERMINAL CAPACITORS. 4,500 at 64v. 7100 at 40v. 50p each pp 10p.

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TOGGLE SWITCHES. Single pole Double Throw ex-equip. new condition. 50p doz. pp 13p.

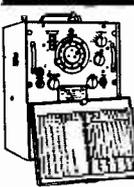
PAINTON PLUG SOCKETS Type 159 series working voltage 350v AC/DC current max. 3 amp AC/DC 7 pin plug & socket 50p pp 6p. 15 pin plug & socket £1 pp 6p. 31 WAY PLUG & SOCKET. £1-50. pp 6p.

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20" TELESCOPIC MASTS £2-75. Carr. £1.
 5' 2" Extension Sections to fit bottom of above mast to increase height. £1-25 each (any number supplied).
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AERIAL RODS 3ft. Screw-in 1 1/2" dia. sections. Brand New, green finish. Suitable for many other uses. 10 for £2. Carr. 50p. 25 for £5. Carr. Paid.

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Cylinder design 10" x 4 1/2". Precision calibrated scale. Suitable for tuning most aerials for increased signal strength. A must for serious operators for RC or TM. Full instructions. ONLY £1-75. P. & P. 25p.

R.F. ANTENNA TUNER (A.T.U.) OPEN TYPE

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Scaled 0-600 and 0-15V. Brand new, boxed £1-25 Post Paid. (Quantity prices on request.)

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ONLY £2-75. Carr. £1-25. Instruction Book for R.F. Amp. 37p Post Paid.

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 6V. 100/125AH. 15" x 11" x 7" 25-50. Last £1-25.
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2" diameter 27-50. p. & p. 25p

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Suitable for Farms, Building Sites etc. Communication up to 5 miles or more. Rugged construction, will last a lifetime. ONLY 25-25 PAIR. Carr. £1-25 (Twin telephone wire for above available—ask for price.) Many other Ex-Govt. Surplus Equipment items in stock. Receivers etc. in small quantities too numerous to mention. Enquiries invited. LIST 25p Post Paid. (Refundable against purchases over £2.)

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500P PURCHASE OF BRAND NEW CARBON RESISTORS. 10% tolerance 1/2 & 1 watt. Preferred values in packets of 10. Our price 50p per 100, 85p per 200, £1-35 per 300, 500 at £2-12. Our selection. p.p. 8p per 100 and 24p per extra 100.

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Huge release of valves for the 62 set TX/RX, in original rubber packing consisting of Q704/7" x 61M, AXP12 etc 10 valves in all at the bargain price as seen 87p plus 174p p.p

R209. Set of valves 621p. p.p. 25p.

NEW AERIAL WIRE ON BOARDS 7/32 UNCOVERED 75ft. 40p, 90ft. 47p, 100ft. 55p, p. & p. 20p.

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- This precision instrument can be used:
1. To Measure Gain up to 60 db.
 2. To Measure Loss up to 45 db.
 3. To Compare Power levels (A.F.).
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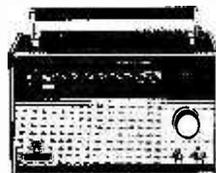
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EL822	1.30	PC8085	0.85	Y88	0.40	UC85	0.40
EL830	0.75	PC8086	0.80	Y800	1.00	UCF90	0.55
EL834	1.00	PCF80	0.30	Y800	0.40	UCF91	0.50
EM71	0.90	PCF82	0.35	Y801	0.50	UCF92	0.70
EM80	0.45	PCF84	0.60	Z30	0.35	UCF93	0.40
EM81	0.60	PCF86	0.60	QV09-2		UCF94	0.60
EM83	0.50	PCF87	0.90		2.25	UCF95	0.35
EM84	0.35	PCF801	0.50	QQV03-10		UCF98	0.60
EM86	1.70	PCF802	0.50		1.25	UF9	0.60
EM87	0.70	PCF803	0.50	QQV03-20		UF11	0.50
EM89	0.35	PCF804	0.70		5.25	UF14	0.60
EV61	0.40	PCF808	0.85	QQV06-40A		UF42	0.60
EV80	0.55	PCF2000.70			5.50	UF43	0.60
EV81	0.40	PCL81	0.50	T21	3.00	UF80	0.35
EV83	0.55	PCL82	0.35	T22	3.20	UF85	0.40
EV84	0.60	PCL83	0.65	TY2-125		UF89	0.40
EV87	0.45	PCL84	0.45		10.00	UL84	0.40
EV89	0.45	PCL85	0.45	U18-20	0.75	UM84	0.35
EZ40	0.50	PCL86	0.45	U25	0.80	UYIN	0.50
EZ41	0.50	PCL88	0.90	U26	0.80	UY11	1.00
EZ80	0.27	PCL800.92		U31	0.60	UY11	1.00
EZ81	0.29	PCL801.75		U37	2.10	UY41	0.45
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G23A	0.40	PF8	0.35	U76	0.35	UY85	0.40
G23B	0.40	PF818	0.35	U78	0.35	UY86	0.40
G231	0.35	PL1200.65		U91	0.75	WZ29	0.75
G232	0.45	PL133	0.35	U91	0.35	Z803U	1.20

TRANSISTORS

2N696	0.17	AC127	0.20	BD123	0.80
2N697	0.17	AC128	0.15	BD131	0.85
2N698	0.30	AC132	0.35	BD132	0.85
2N705	0.70	AC135	0.20	BF115	0.90
2N706	0.10	AC184	0.15	BF116	0.15
2N708	0.15	AC187	0.20	BF173	0.30
2N753	0.25	AC169	0.10	BF179	0.30
2N929	0.25	AC176	0.25	BF180	0.35
2N930	0.35	AC187	0.35	BF181	0.35
2N947	0.30	AC188	0.30	BF184	0.35
2N1131	0.25	AC177	0.75	BF185	0.20
2N1132	0.25	AC178	0.20	BF187	0.40
2N1184	1.25	ACY19	0.25	BF195	0.15
2N1301	0.40	ACY20	0.20	BF196	0.20
2N1302	0.75	ACY21	0.20	BF197	0.20
2N1304	0.25	AC183	0.20	BF209	0.55
2N1305	0.35	AD140	0.60	BF217	0.50
2N1306	0.25	AD149	0.50	BFW88	0.25
2N1307	0.30	AD161	0.35	BFW89	0.20
2N1308	0.25	AD162	0.35	BFW91	0.20
2N1309	0.30	ADZ11	1.25	BFX88	0.25
2N1313	0.25	ADZ12	1.25	BFY10	0.40
2N1711	0.55	AF114	0.20	BFY10	0.25
2N1756	0.75	AF115	0.20	BFY50	0.25
2N2147	0.75	AF116	0.20	BFY51	0.20
2N2160	0.65	AF117	0.20	BFY52	0.25
2N2217	0.30	AF118	0.45	BSY26	0.20
2N2218	0.30	AF127	0.20	BSY27	0.20
2N2219	0.35	AF127	0.20	BSY28	0.20
2N2369A	0.60	AF180	0.35	BSY65	0.20
2N2477	0.25	AF181	0.35	BSY95A	0.15
2N2646	0.60	AF196	0.40	OC16	0.50
2N2905	0.35	AF199	0.40	OC22	0.50
2N2923	0.15	AFZ11	0.45	OC23	0.60
2N2924	0.15	AS726	0.25	OC24	0.60
2N2926	0.125	AS727	0.20	OC25	0.35
2N3053	0.25	AS728	0.25	OC26	0.25
2N3054	0.60	AS729	0.30	OC28	0.60
2N3055	0.75	AS734	0.35	OC29	0.60
2N3132	0.30	ASZ15	0.70	OC30	0.75
2N3134	0.30	ASZ16	0.70	OC35	0.50
2N3391	0.20	ASZ17	0.75	OC36	0.60
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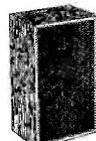
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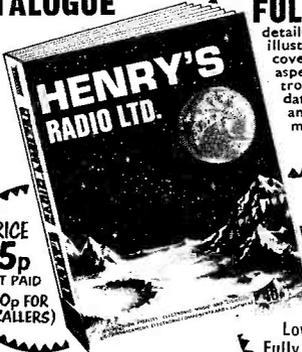
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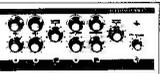
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